# SITE SERVICING AND STORMWATER MANAGEMENT REPORT

Project Address – 5497 Manotick Main, Manotick, On

Owner/Client: Address: City file Number: Oligo Development 996-B St-Augustin Rd, Embrun ON

By Blanchard Letendre Engineering Ltd. Date – September 20, 2022 Our File Reference: 20-261

**First Submission** October 12, 2020

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## **APPENDIX TABLE**

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- Appendix C Watermain Design
- Appendix D Stormwater Underground Chamber \$ Stormwater Treatment Unit
- Appendix E Boundary Conditions
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# **1.0** INTRODUCTION

Blanchard Letendre Engineering Ltd. (BLEL) was retained by Bridor Development. to complete their site servicing and stormwater management for the new proposed site located at 5497 Manotick Main Road in Manotick. This report summarized proposed site servicing and stormwater management and should be read in conjunction with the engineering drawings prepare by BLEL. This report and site servicing plan have been prepared based on the site plan proposed by P-Square Concepts and the site survey completed by Annis O'Sullivan Vollebekk. The information contained herein is based on the provided drawings and if there is any discrepancy with the survey or site plan, BLEL should be informed in order to verify the information and complete the changes if required.

## 2.0 SITE PLAN

The proposed site is to be located at 5497 Manotick Main in Manotick, Ontario. As per the aerial picture in figure 1, the existing site (0.214ha) consist of and green space area at the rear of the property and an existing commercial building with a paved parking at the front of the property. The existing building and parking area will be demolished prior to construction. The land will be developed with a new mix use commercial and residential building with a new parking area at the behind the proposed building.



Figure 1- Existing site at 5497 Manotick Main, Manotick, Ontario

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# 3.0 STORM WATER MANAGEMENT

### 3.1 Existing Site Condition

The existing site currently has and existing parking area at the front of the property with some storm sewers that collect and convey the stormwater to the existing storm sewer on Manotick Main. The existing property has a split drainage where half the property drain towards the street and the other portion naturally grades towards the rideau river. The property is bounded by an existing residential home (north-west) and a commercial development (south-east). Refer to BL Engineering drawing C400 for the pre-development drainage area and existing grading showing the current drainage of the site.

### 3.2 Proposed Storm Water Management

The development of the site will consist of adding a new residential apartment building, which will have twenty-one (21) residential units. The site will be modified by adding a total of 629 square meter building, asphalt parking and driving area and amities at the rear. As the runoff coefficient will increase due to addition of hard surfaces, post-development stormwater quantity and quality will be implemented.

The site stormwater management has been prepared in correlation with the existing site grading. To minimize the fill and site work required, the stormwater management has been developed to follow the existing site grading which has a split drainage pattern. A portion of the property naturally drain to the Rideau River which mainly consist of grass area and will be left uncontrolled as no work is proposed in that area. The front portion of the property which already has some development drains towards Manotick Main Street. The affected area stormwater management will outlet to City storm sewer on Manotick Main Road whereas the overland flow route has also been designed to convey the storm runoff towards the city right away.

The stormwater generated by the new hard surfaces will be directed to a series of catchbasins which will capture and covey the water runoff to existing city storm sewer. The catchment areas have been delineated as per the proposed grading plan. Refer to Appendix 'A', for the catchment area and runoff coefficient. In order to respect the 5 year pre-development allowable release rate, the outlets will be controlled by undersized 200mm diameter storm pipe which will act as an orifice and limit the flow outletting to City storm sewer on Manotick Main Street. By throttling the flow, stormwater retention will be completed with the use of overland ponding and underground storage which was designed to hold the 100 year storm event. Refer to Appendix 'A' for the stormwater flow and storage calculations.

# 3.3 Proposed Storm Water Management

The pre-development flow of the 5-year storm was calculated using a 5-year storm and a 10-minute time of concentration for the affected area. The pre-development flow of the 100-year storm was calculated using a 5-year storm and a 10-minute time of concentration for the affected area. From intensity duration curves established for the Ottawa area, the intensity was evaluated at of 104.2 mm/hr for the 5yr predevelopment flow and 178.6mm/hr for the 100-year predevelopment flow. A run-off coefficient of 0.46 was used as per the evaluated pre-development runoff coefficient, see Appendix 'A' – Pre-Development Drainage Area table.

Using the Rational Method and considering the tributary areas of the affected area by the proposed (see Appendix 'A'), the pre-development allowable release rate for the site was evaluated at **25.32** L/s. See also the Storm Sewer Design Sheet in Appendix 'A'.

```
Allowable Release Rate (Q) = 2.78CIA (L/s)

I_5 = 998.071 / (Tc + 6.053)^{0.814}

C = 0.48

I = 104.2 mm/hr

Tc = 10 min

Total = 0.143 ha

Allowable Release Rate= 25.32 L/s
```

# 3.4 **Proposed Stormwater Quantity Control**

The proposed stormwater management for the site will be achieve primarily through the use of overland surface ponding and underground pipe storage. The grading of the site has been designed to direct the stormwater towards the series of catchbasins connected to the underground stormwater sewers before outleting south into the 350mm diameter storm city sewer. The proposed underground stormwater sewers and cathcbasins are shown on the attached drawings in Appendix 'E'.

The proposed site affected area has been graded to outlet overland onto Manotick Main on the south-west side of the property. As the site affected area is graded from the north side to the south side, the grades have been adjusted to suit this profile to minimize the grade raise of the site. All catchment areas were designed to directed the stormwater overland to the south-west corner and will be captured through a series of parking catchbasins.

The stormwater generated from site affected area will be discharged to the existing storm sewer on Manotick Main and be controlled using an orifice plate which will throttle the flow direct to the municipal sewer. The proposed 95mm diameter orifice plate will release a total of **6.64 L/s** with a maximum head of 1.22m (HWL = 87.70) during the 100 year event. As the flow will be restricted,  $46.96m^3$  of stormwater storage will be required for this area. This storage will be provided with overland parking ponding and underground sewers/ structures and chambers. The

overland storage will hold up to 12.45  $\text{m}^3$  with a HWL of 87.71 and the underground pipes/ structures and chambers will store up to 35.00  $\text{m}^3$ . Therefore with the outlet restriction and the provided stormwater storage, the post-development will meet the pre-development flow to the city main storm sewer on Manotick Main.

Area WS-04 which mainly consist of unit pavers, will be drained uncontrolled towards the city right away as there is no room to install a sewer between the building and the property line. As the un-affected area (WS-05) naturally grades towards the Rideau River, the stormwater generated from this area will remain uncontrolled as it flows to the river. This area has been accounted for in the design of the stormwater management to limit the water runoff directed to the existing city storm sewer. As the river is the main stormwater receiver for the rear of the property, this area has been maintained in the calculation which makes the calculations more conservative as the uncontrolled flow is more than 50% of the allowable release rate. These area will generate a maximum **18.72L/s** under a 100 year storm event before being capture by the nearest city road catchbasin located at the south corner of the property.

### 3.4.1 Roof Drainage

The proposed roofs are flat roof with roof drains. Drain and scuppers will be installed to drain the water onto the pavement area.

### 3.5 **Proposed Stormwater Quality Control**

A water quality control requirement of 80% TSS removal was set by the City of Ottawa. In order to meet the requirements, a storm treatment unit will be installed and the downstream end of the system. Using the Stormceptor sizing software, the EF04 was selected. The software generated report has been attached (See Appendix "D").

# 4.0 SANITARY SEWER DESIGN

### 4.1 Existing Site Conditions

The existing site is currently being service by an existing 135mm diameter service that is connected to the existing 600mm diameter sanitary main on Manotick Main Road. The existing connection will be removed and reinstated with a new connection that will service the new building.

### 4.2 Existing Site Conditions

The new mix use building, will discharge to the city via a new 150mm diameter sanitary service. The service will be located on the south face of the buildings and will discharge to the existing

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600mm diameter city sewer running along Manotick Main road. The proposed 150mm diameter service will be installed at a minimum of 1.00% slope directly to the city sewer. No monitoring manhole is proposed for the new connections. Refer to drawing C300 – Site Servicing Plan for the proposed sanitary service.

Based on the City of Ottawa Sanitary Design Guidelines, the sanitary peak loads were evaluated at **0.64 L/s.** As per the City specific design parameters, the sanitary flow was evaluated based on the residential unit counts, new building footprint and the total site area. Refer to Appendix 'B' for the sanitary sewer design calculation and design parameters set by the City of Ottawa.

# 5.0 WATER CONNECTION DESIGN

## 5.1 Existing Site Conditions

The existing site is currently being service by a 19mm diameter water house service which services the existing house and is connected to the existing 406mm diameter watermain on Manotick Main. The existing connection will be removed and reinstated with a new connection that will service the new building. There is currently one (1) city fire hydrant at the front of the property. The hydrant is located on the east side of Manotick Main within the 90m radius from the building main entrance. Refer to drawing C300 – Site Servicing Plan for the existing and proposed water services and city existing infrastructure.

### 5.2 Proposed Domestic Water Service

The new mix-use buildings water services were sized based on the City of Ottawa Design Guidelines. Based on the number of fixtures proposed and on the average water demand for the developments the daily water consumption was evaluated for the proposed building. As per the city guidelines, the average water demand per fixtures unit is **3.79L/min** per fixture was applied to the fixtures proposed in the new building. The daily and hourly peak factor of **2.5** and **2.2** respectively were applied to the water demand as stated in the City of Ottawa guideline. By using the average demand and peaking factors, the daily water demand for the new buildings were evaluated as follow:

		UNITS
Average Water Demand =	0.12	L/s
Maximum Daily =	0.29	L/s
Maximum Hourly =	0.64	L/s
Total Domestic Flow =	0.64	L/s
Total Fire Flow =	150.00	L/s

Refer to Appendix 'C' for the water flow calculation sheet.

# 5.3 Proposed Fire Demand

As the new mix use building will not have a fire suppression sprinkler system, the new service was sized to supply the daily water demand. Based on the Ontario building code calculations, the water flow was evaluated at **150.00L/s**. Refer to Appendix 'C' for the fire flow calculation sheet.

The proposed buildings will be serviced with a new 50mm water service which will connect to the existing 405mm diameter watermain on Manotick Main. The new services will be installed at the south elevation of the new buildings and be placed in the same trench as the other services.

# 5.4 Water Capacity Comments

The boundary conditions and HGL for hydraulic analysis for 5497 Manotick Main were requested to the city but not provided. obtained from the city, see attached copy in Appendix 'E'. From the boundary conditions, we noted that we have a minimum HGL of 146.6 m for the water main elevation at 87.8m and a maximum pressure estimate of 83.6 psi. As requested by the City, a water pressure reducing valve will be installed on the water service.

# 6.0 EROSION AND SEDIMENT CONTROL

During the construction, sediment and erosion protect will be implemented around the property to prevent any sediments from leaching off site. The construction and maintenance of the sediment controls must comply with the Ontario Provision Standard Specification OPSS 805. Refer to drawing C100 – Erosion and Sediment Control for the perimeter fence proposed.

# 7.0 CONCLUSION AND LIMITATION OF REPORT

### 7.1 Stormwater Management

The stormwater management proposed for the site will maintain the site to its pre-development release rate conditions and meet the requirements from the City of Ottawa. The post development release rate of the affected area will be maintained to its pre-development rate of **25.34 L/s** thought an inlet control device to the sewer main on Manotick Main. Stormwater quantity control will be achieved with 35.00m<sup>3</sup> underground pipes/structures and 12.45m<sup>3</sup> overland. The stormwater quality control will be met through the use of a stormwater treatment unit.

# 7.2 Sanitary Service

The current site will be services with a new 150mm sanitary connection onto Manotick Main. The estimated sanitary flow of **0.64 L/s** will be directed to the existing 600mm sanitary sewer along Manotick Main.

# 7.3 Water Service

Currently the existing building on site is serviced with an existing 19mm diameter water service that will be replaced with a new 50mm diameter water services to be connected to the existing 406mm diameter main on Manotick Main. The existing connection will be replaced with a new 50mm water service. The water demand for the building was evaluated at **0.64L/s** and the fire flow demand **150.00L/s.** Sprinkler system is not proposed for the site. There is also one (1) fire located around the property within 90m from every entrance doors.

### 8.0 LIMITATION

This report was prepared for **Bridor Developement.**, and is only applicable for the property at 5497 Manotick Main, Ottawa.

Any changes to the existing site may require a review by Blanchard Letendre engineering Ltd. to ensure all information is consistent with the proposed design.

Should you have any questions, please do not hesitate to contact the undersigned.

Sincerely Yours,



Guillaume Brunet, P. Eng.

# APPENDIX "A" Stormwater Management Design

# BLANCHARD LETENDRE ENGINEERING

File No.	20-261	Date:	September 11 - 2022
Project:	Proposed Multipurpose Building	Designed:	Benjamin Falconer
Project Address:	5497 Manotick Main, Manotick	Checked:	Guillaume Brunet
Client:	Bridor Development	<b>Drawing Reference:</b>	C300

### PRE-DEVELOPMENT DRAINAGE AREA

Catchmant Araa	R	unoff Coeffic	ient	Total Area (ha)	Combined C		
Catchinent Area	C = 0.20	C = 0.80	C = 0.90	Total Alea (lla)	Combined C		
E-01 - Un-affected	0.065	0.000	0.006	0.071	0.26		
E-02 - Affected	0.085	0.000	0.058	0.143	0.48		
TOTAL	0.150	0.000	0.064	0.214	0.41		

### POST-DEVELOPMENT DRAINAGE AREA

	R	unoff Coeffic	ient		Combined C		
Catchment Area	C = 0.20	C = 0.80	C = 0.90	Total Area (na)	Combined C		
WS-01	0.007	0.000	0.054	0.061	0.82		
WS-02 RAMP	0.000	0.000	0.004	0.004	0.90		
WS-03	0.000	0.000	0.064	0.064	0.90		
WS-04	0.005	0.000	0.008	0.013	0.63		
WS-05	0.065	0.000	0.006	0.071	0.26		
TOTAL	0.007	0.000	0.137	0.214	0.56		

### RUNOFF COEFFICIENT (C)

Grass	0.20
Gravel	0.80
Asphalt / rooftop	0.90



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Drawing Reference: C300

### STORM WATER MANAGEMENT DESIGN SHEET

SEWER DESIGN

	LOCATION					E OU												
	LOCATION			AREA (ha)				FLOW			STORM SEWER DATA							
WATERSHED /	From MH	To MH	C = 0.20	C = 0.80	C = 0.90	Indiv.	Accum.	Time of Conc.	Rainfall Intensity	Peak Flow Q	Pipe Diameter	Type	Slope (%)	Length (m)	Capacity Full (L/s)	Velocity	Time of Flow (min )	Ratio
STREET		101111	0.20	0.00	0.70	2.78AC	2.78AC	(min.)	(mm/hr)	(l/s)	(mm)	1 JPC	Biope (///	Longui (iii)	cupuenty I un (155)	Full (m/s)	11110 01 1 10 11 (11111)	$(Q/Q_{FULL})$
WS-01, WS-03	CB03	CB02	0.007	0.000	0.118	0.30	0.30	10.00	104.19	31.19	300	PVC	0.25%	12.2	48.4	0.68	0.30	0.65
WS-01, WS-03	CB02	MH01	0.000	0.000	0.000	0.00	0.30	10.30	102.65	30.73	300	PVC	0.25%	7.7	48.4	0.68	0.19	0.64
	MH01	STREET	0.000	0.000	0.000	0.00	0.30	10.48	101.70	30.45	250	PVC	0.25%	10.2	29.7	0.61	0.28	1.02

### DESIGN PARAMETERS NOTES

		Q = 2.78 AIC, where
Runoff Coefficient (C)		Q = Peak flow in Litres per second (L/s)
Grass	0.2	A = Area in hectares (ha)
Gravel	0.80	I = Rainfall Intensity (mm/hr)
Asphalt / rooftop	0.90	C = Runoff Coefficient

1.1

Ottawa Macdonald-Cartier International Airport IDF curve  $I_5=998.071~/~(T_c+6.053)^{0.814}$ Min. velocity = 0.76 m/s Manning's "n" = 0.013



File No.20-261Project:Proposed Multipurpose BuildingProject Address:5497 Manotick Main, ManotickClient:Bridor Development

Date: September 11 - 2022 Designed: Benjamin Falconer Checked: Guillaume Brunet Drawing Reference: C300

### STORM WATER MANAGEMENT DESIGN SHEET

SEWER DESIGN

LOCATI	LOCATION MANHOLE INFORMATION AVAILABLE STORAGE														
From MH	To MH	Up Invert (m)	Down Invert (m)	T/G Up Stream (m)	T/G Down Stream	Up Depth obv (m)	Down Depth obv (m)	Up Depth inv (m)	Pipe Storage 5 Year (m <sup>3</sup> )	Pipe Storage 100 year (m <sup>3</sup> )	Upstream CB/MH Size (m)	Water Depth 5 year (m)	Water Depth 100 year (m)	CB/MH Storage 5 year (m <sup>3</sup> )	CB/MH Storage 100 year (m <sup>3</sup> )
CB03	CB02	86.38	86.34	87.55	87.55	0.87	0.91	0.87	0.86	0.86	1.20	0.87	0.87	1.26	1.26
CB02	MH01	86.34	86.33	87.55	87.81	0.91	1.18	0.91	-	-	1.20	0.91	0.91	1.30	1.30
MH01	STREET	86.30	86.27	87.81	87.70	1.26	-	1.26	-	-	1.20	1.25	1.26	-	-
									0.86	0.86				2.56	2.56

HWL (5 Year)		87.55
HWL (100 Year)		87.80
TOTAL STORAGE	3.43	
TOTAL STORAG	GE - 100 YEAR	3.43



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STORM WATER MANAGEMENT DESIGN SHEET							

### **5 YEAR STORM EVENT**

### PRE-DEVELOPMENT STORMATER MANAGEMENT

Runoff	Catchment Area	Area			$\sum \mathbf{R}_5$
Un-Controlled	EWS-01	0.071	ha	R=	0.26
Controlled	EWS-02	0.143	ha	R=	0.48
	Total Uncontrolled =	0.214	ha	$\Sigma R=$	0.41

### PRE-DEVELOPMENT ALLOWABLE RELEASE RATE

Q = 2.78CIA (L/s)

C =	0.41	up to a maximum of 0.5 as per City of Ottawa Sewer Design Guidelines
I=	104.2	mm/hr
Tc =	10	min
Total =	0.214	ha
Allowable Release Rate=	25.34	L/s

### POST-DEVELOPMENT STORMATER MANAGEMENT

Runoff	Catchment Area	Area			$\sum \mathbf{R}_5$	$\sum R_{100}$
	WS-01	0.061	ha	R=	0.82	1.00
Controlled	WS-03	0.064	ha	R=	0.90	1.00
	Total Contolled =	0.125	ha	$\Sigma R=$	0.86	1.00
	WS-04	0.013	ha	R=	0.63	0.79
Un controlled	WS-02	0.004	ha	R=	0.90	1.00
Ull-controlled	WS-05 - Un-Affected	0.071	ha	R=	0.26	0.32
	Total Un-Controlled =	0.088	ha	$\Sigma R=$	0.30	0.38

### $I_5 = 998.071 / (Td + 6.053)^{0.814}$

			REQUIRED STOR			
Time (min)	Intensity (mm/hr)	Controlled Runoff (L/s)	Storage Volume (m <sup>3</sup> )	Controlled Release Rate (L/s)	Uncontrolled Runoff (L/s)	Total Release Rate (L/s)
10	104.2	31.19	14.74	6.62	5.33	11.95
15	83.6	25.02	16.55	6.62	4.27	10.90
20	70.3	21.03	17.29	6.62	3.59	10.22
25	60.9	18.23	17.41	6.62	3.11	9.74
30	53.9	16.14	17.14	6.62	2.76	9.38
35	48.5	14.53	16.60	6.62	2.48	9.10
40	44.2	13.23	15.85	6.62	2.26	8.88
50	37.7	11.27	13.95	6.62	1.93	8.55
60	32.9	9.86	11.66	6.62	1.69	8.31
80	26.6	7.95	6.38	6.62	1.36	7.98
90	24.3	7.27	3.50	6.62	1.24	7.86

#### STORMATER STORAGE REQUIREMENTS

Total Storage Required =	17.41 m <sup>3</sup>
Pipe Storage =	0.86 m <sup>3</sup>
CB/MH Storage =	$2.56 \text{ m}^3$
Underground Storage =	35.00 m <sup>3</sup>
Surface Storage =	$12.45 \text{ m}^3$
Total Available Storage =	50.88 m <sup>3</sup>

refer to Storm Sewer Design Sheet refer to Storm Sewer Design Sheet

 $I_5 = 998.071 / (Tc + 6.053)^{0.814}$ 



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	STORM WATER MANAGEMENT DESIGN SHEET		
	100 YEAR STORM EVENT		

PRE-DEVELOPMENT STORMATER MANAGEMENT

Runoff	Catchment Area Area		Area		$\sum R_5$
Un-Affected	EWS-01	0.071	ha	R=	0.26
Affected	EWS-02	0.143	ha	R=	0.48
	Total Area =	0.214	ha	$\Sigma R=$	0.41

PRE-DEVELOPMENT ALLOWABLE RELEASE RATE

Q = 2.78CIA (L/s)

### $I_5 = \ 998.071 \ / \ (Tc + 6.053)^{0.814}$

C = I =	0.41 104.2	up to a maximum of 0.5 as per City of Ottawa Sewer Design Guidelines mm/hr
Tc =	10	min
Total =	0.214	ha
Allowable Release Rate=	25.34	L/s
Allowable Release Rate=	12.67	L/s * 50% of Pre-Development Flow due to underground storage

POST-DEVELOPMENT STORMATER MANAGEMENT

POST-DEVELOPMENT STORMATER MANAGEMENT

Runoff	Catchment Area	Area			$\sum \mathbf{R}_5$	$\sum R_{100}$
	WS-01	0.061	ha	R=	0.90	1.00
Controlled	WS-03	0.064	ha	R=	0.90	1.00
	Total Contolled =	0.125	ha	$\Sigma R=$	0.90	1.00
	WS-04	0.013	ha	R=	0.63	0.79
Un controlled	WS-02	0.004	ha	R=	0.90	1.00
Un-controlleu	WS-05 - Un-Affected	0.071	ha	R=	0.26	0.32
	Total Un-Controlled =	0.088	ha	$\Sigma R=$	0.35	0.43

 $I_{100}=\ 1735.688\ /\ (Td+6.014)^{0.820}$ 

		REG	JUIRED STORAGI	5		
Time (min)	Intensity (mm/hr)	Controlled Runoff** (L/s)	Storage Volume (m <sup>3</sup> )	Controlled Release Rate (L/s)	Uncontrolled Runoff (L/s)	Total Release Rate (L/s)
10	178.6	62.10	33.29	6.62	18.72	25.34
15	142.9	49.70	38.77	6.62	14.98	21.61
20	120.0	41.72	42.11	6.62	12.58	19.20
25	103.8	36.12	44.24	6.62	10.89	17.51
30	91.9	31.95	45.59	6.62	9.63	16.26
35	82.6	28.72	46.40	6.62	8.66	15.28
40	75.1	26.13	46.83	6.62	7.88	14.50
50	64.0	22.24	46.86	6.62	6.71	13.33
60	55.9	19.44	46.14	6.62	5.86	12.48
70	49.8	17.32	44.91	6.62	5.22	11.84
90	41.1	14.30	41.45	6.62	4.31	10.93
100	37.9	13.18	39.36	6.62	3.97	10.60
110	35.2	12.24	37.09	6.62	3.69	10.31
120	32.9	11.44	34.69	6.62	3.45	10.07

STORMATER STORAGE REQUIREMENTS

Total Storage Required =	46.96 m <sup>3</sup>
Pipe Storage =	0.86 m <sup>3</sup>
CB/MH Storage =	2.56 m <sup>3</sup>
Underground Storage =	35.00 m <sup>3</sup>
Surface Storage =	12.45 m <sup>3</sup>
Total Available Storage =	50.88 m <sup>3</sup>

#### refer to Storm Sewer Design Sheet refer to Storm Sewer Design Sheet

Total Available Storage

### Inlet Control Device Parameters

Product	Orifice Plate	at CB02
HWL =	87.71	m (highest HWL)
Grate Level =	87.55	m from inv.
Invert Level =	86.34	m
Outlet Pipe Dia. =	300	mm
Max. Flow =	6.62	L/s
ICD Centerline =	86.49	
HWL Head =	1.22	m (from centerlin from centerline
C=	1.00	
Orifice Area =	0.006	m2
Orifice Diameter =	93	mm (min. 75mm)

# APPENDIX "B" Sanitary Design



File No.	20-261
Project:	Proposed Multipurpose Building
Project Address:	5497 Manotick Main, Manotick
Client:	Bridor Development

Date: September 11 - 2022 Designed: Benjamin Falconer Checked: Guillaume Brunet Drawing Reference: C300

SANITARY DESIGN SHEET
SEWER DESIGN

	LOCATION			RESIDENT	TIAL AREA	AND POPU	LATION		COMM	ERCIAL	П	NDUSTRIA	L	INSTITU	TIONAL	C+I+I	IN	FILTRATI	ON	TOTAL			PIP	Έ			MANHOL	Æ
STREET	FROM MH	ТО МН	AREA (Ha)	POP.	CUMM AREA (Ha)	ULATIVE POP.	PEAK FACT.	PEAK FLOW (l/s)	AREA (Ha)	ACCU. AREA (Ha)	AREA (Ha)	ACCU. AREA (Ha)	PEAK FACT.	AREA (Ha)	ACCU. AREA (Ha)	PEAK FLOW (l/s)	TOTAL AREA (Ha)	ACCU. AREA (Ha)	INFILT. FLOW (l/s)	FLOW (1/s)	LENGTH (m)	DIA. (mm)	MATERAIL	SLOPE (%)	CAP. (FULL) (l/s)	VEL. (FULL) (m/s)	UP INVERT (m)	DOWN INVERT (m)
SITE	PROP. BLDG	CITY	0.214	35.7	0.21	35.7	4.0	0.58	0.000	0.000	0.00	0.00	7.0	0.0	0.0	0.00	0.21	0.21	0.06	0.64	33.2	150	PVC	1.00%	15.23	0.86	84.95	82.90

### DESIGN PARAMETERS NOTES

Average Daily Flow = Commercial and Institutional Flow = Industrial Flow = Maximum Resedential Peak Flow =	280 L/p/day 50000 L/ha/da 35000.00 L/ha/da	Industrial Peak Factor = Extraneous Flow = Minimum Velocity = Mannings n =	7 as per Appendix 4-B 0.33 L/s/ha 0.76 m/s	Appartments: Bachelor = 1 Bedroom = 2 Bedroom =	Person Per Unit 1.4 1.4 2.1	Appartment 0 12 9	Total 0 16.8 18 9
Commection and Intitutional Peak Factor =	4 1.5	Mannings n =	0.013	2 Bedroom = 3 Bedroom =	2.1 3.1	9	0

# APPENDIX "C" Watermain Design



File No.	20-261			Date:	September 11 - 2022
Project:	New Residential - Comme	rcial Building		Designed:	Guillaume Brunet
Project Address:	5497 Manotick			Checked:	Guillaume Brunet
Client:	Oligo Development			<b>Drawing Referen</b>	nce:
WATER CONSUMPTION (	TALCULATION				
WATER CONSUMPTION C	ALCOLATION				
Total Building Floor Area =		663	m <sup>2</sup>		
Site Total Area =		0.214	ha		
Total Population =		35.7	ea.		
Average Demand Per People	=	280	L/c/d		
Average Water Demand =		9996.00	L/d		0.12 L/s
Maximum Daily Peak Factor :	=	2.5	* As per Cit	y of Ottawa	
Maximum Daily =		24990.00	L/d	-	0.29 L/s
Maximum Hourly Peak Factor	r =	2.2	* As per Cit	y of Ottawa	
Maximum Hourly =		54978.00	L/d	-	0.64 L/s
Total Domestic Flow =		0.64	L/s		
Total Fire Flow =		150.00	L/s		

	Unit Counts	WSFU	Total
Unrinal Flush Tank	21	2	42
Sinks	42	1	42
Bathub	21	4	84
Diswasher	21	1.5	31.5
Washing Machine	21	2	42
Total			241.5

Appartments:	Person Per Unit	Appartment	Total
Bachelor =	1.4	0	0
1 Bedroom =	1.4	12	16.8
2 Bedroom =	2.1	9	18.9
3 Bedroom =	3.1	0	0
Total		21	35.7



File No.	20-261
Project:	New Residential - Commercial Building
Project Address:	5497 Manotick
Client:	Oligo Development

Date:September 11 - 2022Designed:Guillaume BrunetChecked:Guillaume BrunetDrawing Reference:

Term	Options	Multiplier	Choose:	Value	unit	Fire Flow
	Wood Frame	1.5				
Coefficient C	Ordinary Construction	1.0				
related to the type of	Non-combustible construction	0.8	Non-combustible construction	0.8		
construction	Fire resistive construction <2 hrs	0.7				
	Fire resistive construction >2 hrs	0.6				
	Single family dwelling	0				
	Townhouse - no. of units	0	Building - no. of units per floor	8	unit	
Type of housing	Building - no. of units per floor	7				
	Number of floors excluding the basement	3		3	floor	
	Floor space per unit	varies	663	663	sq.m.	
Deguined fire flow		F: FI 000 0	a a0.5		L/min	8,000
Required life llow		Fire Flow = 220 x C	x Area <sup>x</sup>		L/s	133
	Non-combustible	-0.25				
	Limited combustible	-0.15				
Occupancy nazard	Combustible	0	Limited combustible	-0.15		
	Free burning	0.15			L/min	6,800
	Rapid burning	0.25	-		L/s	113
	Sprinklers (NFPA13)	-0.30	False	0		
Sprinkler reduction	Water supply is standard for both the system and fire department hose lines	-0.10	False	0	L/min	6,800
	Fully supervised system	-0.10	False	0	L/s	113
	North side	Over 45m	0			
Exposure distance	East side	20.1 to 30m	0.1			
between units	South side	Over 45m	0		L/min	8,500
	West side	10.1 to 20m	0.15	0.25	L/s	142
			Minimum required fire flow rate (rounded	to nearest 1000)	L/min	9,000
			Minimum requ	ired fire flow rate	L/s	150
			Required du	uration of fire flow	min	30

# APPENDIX "D" Underground Chambers & Stormwater Treatment Unit

ENGINEERED PRODUCT MANAGER	
ADS SALES REP	
PROJECT NO	



# 5497 MANOTICK MAIN STREET MANOTICK, CANADA

# SC-740 STORMTECH CHAMBER SPECIFICATIONS

- CHAMBERS SHALL BE STORMTECH SC-740. 1.
- CHAMBERS SHALL BE ARCH-SHAPED AND SHALL BE MANUFACTURED FROM VIRGIN, IMPACT-MODIFIED POLYPROPYLENE 2. COPOLYMERS.
- CHAMBERS SHALL BE CERTIFIED TO CSA B184, "POLYMERIC SUB-SURFACE STORMWATER MANAGEMENT STRUCTURES", AND MEET 3. THE REQUIREMENTS OF ASTM F2418, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORTS THAT WOULD Δ IMPEDE FLOW OR LIMIT ACCESS FOR INSPECTION.
- THE STRUCTURAL DESIGN OF THE CHAMBERS, THE STRUCTURAL BACKFILL, AND THE INSTALLATION REQUIREMENTS SHALL ENSURE THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS. SECTION 12.12, ARE MET FOR: 1) LONG-DURATION DEAD LOADS AND 2) SHORT-DURATION LIVE LOADS, BASED ON THE CSA S6 CL-625 TRUCK AND THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.
- CHAMBERS SHALL BE DESIGNED, TESTED AND ALLOWABLE LOAD CONFIGURATIONS DETERMINED IN ACCORDANCE WITH ASTM F2787, 6 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS". LOAD CONFIGURATIONS SHALL INCLUDE: 1) INSTANTANEOUS (<1 MIN) AASHTO DESIGN TRUCK LIVE LOAD ON MINIMUM COVER 2) MAXIMUM PERMANENT (75-YR) COVER LOAD AND 3) ALLOWABLE COVER WITH PARKED (1-WEEK) AASHTO DESIGN TRUCK.
- REQUIREMENTS FOR HANDLING AND INSTALLATION: 7
  - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
  - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 50 mm (2")
  - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION. a) THE ARCH STIFFNESS CONSTANT AS DEFINED IN SECTION 6.2.8 OF ASTM F2418 SHALL BE GREATER THAN OR EQUAL TO 550 LBS/FT/%. AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 23° C / 73° F), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.
- ONLY CHAMBERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. UPON REQUEST BY THE SITE DESIGN 8. ENGINEER OR OWNER. THE CHAMBER MANUFACTURER SHALL SUBMIT A STRUCTURAL EVALUATION FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE AS FOLLOWS:
  - THE STRUCTURAL EVALUATION SHALL BE SEALED BY A REGISTERED PROFESSIONAL ENGINEER.
  - THE STRUCTURAL EVALUATION SHALL DEMONSTRATE THAT THE SAFETY FACTORS ARE GREATER THAN OR EQUAL TO 1.95 FOR DEAD LOAD AND 1.75 FOR LIVE LOAD, THE MINIMUM REQUIRED BY ASTM F2787 AND BY SECTIONS 3 AND 12.12 OF THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS FOR THERMOPLASTIC PIPE.
  - THE TEST DERIVED CREEP MODULUS AS SPECIFIED IN ASTM F2418 SHALL BE USED FOR PERMANENT DEAD LOAD DESIGN EXCEPT THAT IT SHALL BE THE 75-YEAR MODULUS USED FOR DESIGN.
- CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY. 9

# **IMPORTANT - NOTES FOR THE BIDDING AND INSTALLATION OF THE SC-740 SYSTEM**

- STORMTECH SC-740 CHAMBERS SHALL NOT BE INSTALLED UNTIL THE MANUFACTURER'S REPRESENTATIVE HAS COMPLETED A 1 PRE-CONSTRUCTION MEETING WITH THE INSTALLERS.
- 2.
- 3 CHAMBERS ARE NOT TO BE BACKFILLED WITH A DOZER OR AN EXCAVATOR SITUATED OVER THE CHAMBERS. STORMTECH RECOMMENDS 3 BACKFILL METHODS:
  - STONESHOOTER LOCATED OFF THE CHAMBER BED.
  - BACKFILL AS ROWS ARE BUILT USING AN EXCAVATOR ON THE FOUNDATION STONE OR SUBGRADE.
  - BACKFILL FROM OUTSIDE THE EXCAVATION USING A LONG BOOM HOE OR EXCAVATOR.
- THE FOUNDATION STONE SHALL BE LEVELED AND COMPACTED PRIOR TO PLACING CHAMBERS. 4.
- JOINTS BETWEEN CHAMBERS SHALL BE PROPERLY SEATED PRIOR TO PLACING STONE. 5.
- MAINTAIN MINIMUM 150 mm (6") SPACING BETWEEN THE CHAMBER ROWS. 6.
- EMBEDMENT STONE SURROUNDING CHAMBERS MUST BE A CLEAN, CRUSHED, ANGULAR STONE 20-50 mm (3/4-2"). 7.
- 8 THE CONTRACTOR MUST REPORT ANY DISCREPANCIES WITH CHAMBER FOUNDATION MATERIALS BEARING CAPACITIES TO THE SITE DESIGN ENGINEER.
- ADS RECOMMENDS THE USE OF "FLEXSTORM CATCH IT" INSERTS DURING CONSTRUCTION FOR ALL INLETS TO PROTECT THE SUBSURFACE 9. STORMWATER MANAGEMENT SYSTEM FROM CONSTRUCTION SITE RUNOFF.

### NOTES FOR CONSTRUCTION EQUIPMENT

- 1.
- 2. THE USE OF CONSTRUCTION EQUIPMENT OVER SC-740 CHAMBERS IS LIMITED:
  - NO EQUIPMENT IS ALLOWED ON BARE CHAMBERS.
  - WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".
- 3. FULL 900 mm (36") OF STABILIZED COVER MATERIALS OVER THE CHAMBERS IS REQUIRED FOR DUMP TRUCK TRAVEL OR DUMPING.

### USE OF A DOZER TO PUSH EMBEDMENT STONE BETWEEN THE ROWS OF CHAMBERS MAY CAUSE DAMAGE TO THE CHAMBERS AND IS NOT AN ACCEPTABLE BACKFILL METHOD. ANY CHAMBERS DAMAGED BY THE "DUMP AND PUSH" METHOD ARE NOT COVERED UNDER THE STORMTECH STANDARD WARRANTY.

CONTACT STORMTECH AT 1-888-892-2694 WITH ANY QUESTIONS ON INSTALLATION REQUIREMENTS OR WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT.





STORMTECH SC-740 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".

STORMTECH SC-740 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE"

NO RUBBER TIRED LOADERS, DUMP TRUCKS, OR EXCAVATORS ARE ALLOWED UNTIL PROPER FILL DEPTHS ARE REACHED IN ACCORDANCE

WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT CAN BE FOUND IN THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".

	PROPOSED LAYOUT	PROPOSED ELEVATIONS				1
13	STORMTECH SC-740 CHAMBERS	MAXIMUM ALLOWABLE GRADE (TOP OF PAVEMENT/UNPAVED):	89.578	PART TYPE		DESCRIPTION
8	STORMTECH SC-740 END CAPS	MINIMUM ALLOWABLE GRADE (UNPAVED WITH TRAFFIC):	87.749			600 mm BOTTOM PREFABRICATED EZ END CAP, PART#: SC740E0
152	STONE ABOVE (mm)	MINIMUM ALLOWABLE GRADE (UNPAVED NO TRAFFIC):	87.596	PREFABRICATED EZ END CAP	A	BOTTOM CONNECTIONS AND ISOLATOR PLUS ROWS
40	STONE BELOW (mm)	MINIMUM ALLOWABLE GRADE (TOP OF HIGH CONCALTE FAVEMENT):	87.596	FLAMP	В	INSTALL FLAMP ON 600 mm ACCESS PIPE / PART#: SC74024RAM
	INSTALLED SYSTEM VOLUME (m <sup>3</sup> )	TOP OF STONE:	87.292	MANIFOLD		300 mm x 300 mm TOP MANIFOLD, ADS N-12
36.7	(PERIMETER STONE INCLUDED)	TOP OF SC-740 CHAMBER:	87.139			(300 mm x 300 mm TOP MANIFOLD, ADS N-12 (DESIGN BY ENGINEER / PROVIDED BY OTHERS)
00.1	(COVER STONE INCLUDED)		86.695	NYLOPLAST (INLET W/ ISO		
62.1	SYSTEM AREA (m <sup>-</sup> )	600 mm ISOLATOR ROW PLUS INVERT	86.380	PLUS ROW)	F	750 mm DIAMETER (610 mm SUMP MIN)
34.3	SYSTEM PERIMETER (m)	600 mm ISOLATOR ROW PLUS INVERT:	86.380	)	1	
		BOTTOM OF SC-740 CHAMBER:	86.377	7		
1		BOTTOM OF STONE:	86.225	5		





PLACE MINIMUM 3.810 m OF ADSPLUS125 WOVEN GEOTEXTILE OVER BEDDING STONE AND UNDERNEATH CHAMBER FEET FOR SCOUR PROTECTION AT ALL CHAMBER INLET ROWS

NOTES
 MANIFOLD SIZE TO BE DETERMINED BY SITE DESIGN ENGINEER. SEE TECH NOTE #6.32 FOR MANIFOLD SIZING GUIDANCE.
 DUE TO THE ADAPTATION OF THIS CHAMBER SYSTEM TO SPECIFIC SITE AND DESIGN CONSTRAINTS, IT MAY BE NECESSARY TO CUT AN COMPONENTS IN THE FIELD.
 THE SITE DESIGN ENGINEER MUST REVIEW ELEVATIONS AND IF NECESSARY ADJUST GRADING TO ENSURE THE CHAMBER COVER REQ.
 THIS CHAMBER SYSTEM WAS DESIGNED WITHOUT SITE-SPECIFIC INFORMATION ON SOIL CONDITIONS OR BEARING CAPACITY. THE SITE DETERMINING
 THE SUITABILITY OF THE SOIL AND PROVIDING THE BEARING CAPACITY OF THE INSITU SOILS. THE BASE STONE DEPTH MAY BE INCREASED OF PROVIDED.
 <u>NOT FOR CONSTRUCTION:</u> THIS LAYOUT IS FOR DIMENSIONAL PURPOSES ONLY TO PROVE CONCEPT & THE REQUIRED STORAL

BED LIMITS

# ACCEPTABLE FILL MATERIALS: STORMTECH SC-740 CHAMBER SYSTEMS

	MATERIAL LOCATION	DESCRIPTION	AASHTO MATERIAL CLASSIFICATIONS	COMF
D	FINAL FILL: FILL MATERIAL FOR LAYER 'D' STARTS FROM THE TOP OF THE 'C' LAYER TO THE BOTTOM OF FLEXIBLE PAVEMENT OR UNPAVED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE 'D' LAYER.	ANY SOIL/ROCK MATERIALS, NATIVE SOILS, OR PER ENGINEER'S PLANS. CHECK PLANS FOR PAVEMENT SUBGRADE REQUIREMENTS.	N/A	PREPA INSTA
С	INITIAL FILL: FILL MATERIAL FOR LAYER 'C' STARTS FROM THE TOP OF THE EMBEDMENT STONE ('B' LAYER) TO 18" (450 mm) ABOVE THE TOP OF THE CHAMBER. NOTE THAT PAVEMENT SUBBASE MAY BE A PART OF THE 'C' LAYER.	GRANULAR WELL-GRADED SOIL/AGGREGATE MIXTURES, <35% FINES OR PROCESSED AGGREGATE. MOST PAVEMENT SUBBASE MATERIALS CAN BE USED IN LIEU OF THIS LAYER.	AASHTO M145 <sup>1</sup> A-1, A-2-4, A-3 OR AASHTO M43 <sup>1</sup> 3, 357, 4, 467, 5, 56, 57, 6, 67, 68, 7, 78, 8, 89, 9, 10	BEGIN CC THE CHAM 6" (150 mr WELL GF PROC VEHICLE
В	EMBEDMENT STONE: FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE ('A' LAYER) TO THE 'C' LAYER ABOVE.	CLEAN, CRUSHED, ANGULAR STONE	AASHTO M43 <sup>1</sup> 3, 357, 4, 467, 5, 56, 57	
А	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE CHAMBER.	CLEAN, CRUSHED, ANGULAR STONE	AASHTO M43 <sup>1</sup> 3, 357, 4, 467, 5, 56, 57	PLATE C

PLEASE NOTE:

THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY. THE STONE MUST ALSO BE CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR NO. 4 (AASHTO M43) STONE". 1.

STORMTECH COMPACTION REQUIREMENTS ARE MET FOR 'A' LOCATION MATERIALS WHEN PLACED AND COMPACTED IN 6" (150 mm) (MAX) LIFTS USING TWO FULL COVERAGES WITH A VIBRATORY COMPACTOR. 2

WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION, FOR STANDARD DESIGN LOAD CONDITIONS, A FLAT SURFACE MAY BE ACHIEVED BY RAKING OR DRAGGING WITHOUT COMPACTION EQUIPMENT. FOR SPECIAL LOAD DESIGNS, CONTACT STORMTECH FOR 3. COMPACTION REQUIREMENTS.

ONCE LAYER 'C' IS PLACED, ANY SOIL/MATERIAL CAN BE PLACED IN LAYER 'D' UP TO THE FINISHED GRADE. MOST PAVEMENT SUBBASE SOILS CAN BE USED TO REPLACE THE MATERIAL REQUIREMENTS OF LAYER 'C' OR 'D' AT THE SITE DESIGN ENGINEER'S DISCRETION. 4



# NOTES:

- CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2418, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS". 1.
- 2. SC-740 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2787 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE (ALLOWABLE BEARING CAPACITY) OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH 3 CONSIDERATION FOR THE RANGE OF EXPECTED SOIL MOISTURE CONDITIONS.
- 4. PERIMETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH VERTICAL AND SLOPED EXCAVATION WALLS.
- 5. REQUIREMENTS FOR HANDLING AND INSTALLATION:
  - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
  - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 2".
  - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT SHALL BE GREATER THAN OR EQUAL TO 550 LBS/FT/%. THE ASC IS DEFINED IN SECTION 6.2.8 • OF ASTM F2418. AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 73° F / 23° C), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.

### PACTION / DENSITY REQUIREMENT

ARE PER SITE DESIGN ENGINEER'S PLANS. PAVED LLATIONS MAY HAVE STRINGENT MATERIAL AND PREPARATION REQUIREMENTS.

MPACTIONS AFTER 12" (300 mm) OF MATERIAL OVER BERS IS REACHED. COMPACT ADDITIONAL LAYERS IN m) MAX LIFTS TO A MIN. 95% PROCTOR DENSITY FOR RADED MATERIAL AND 95% RELATIVE DENSITY FOR ESSED AGGREGATE MATERIALS. ROLLER GROSS WEIGHT NOT TO EXCEED 12,000 lbs (53 kN). DYNAMIC FORCE NOT TO EXCEED 20,000 lbs (89 kN).

NO COMPACTION REQUIRED.

COMPACT OR ROLL TO ACHIEVE A FLAT SURFACE.<sup>2,3</sup>

4	4640 TRUEMAN BLVD					5497 MANOTIC	K MAIN STRFFT
3	1-800-733-7473	StormTach®					
sн С						MANOTIC	CK, CANADA
EE )F		Chamber System				DATE.	
T							
6		888-892-2694   WWW.STORMTECH.COM	DATE	DRW CHK	DESCRIPTION	PROJECT #:	CHECKED: N/A
	THIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PRO RESPONSIBILITY OF THE SITE DESIGN ENGINEER TO ENSURE THAT 1	VIDED TO ADS UNDER THE DIRECTION OF THE SITE DESIGN ENGINEE THE PRODUCT(S) DEPICTED AND ALL ASSOCIATED DETALS MEET ALL	ER OR OTHER	PROJECT REPRESE LAWS, REGULATIO	ENTATIVE. THE SITE DESIGN ENGINEER SH NS, AND PROJECT REQUIREMENTS.	ALL REVIEW THIS DRAWING PRIOR TO	CONSTRUCTION. IT IS THE ULTIMATI



### SC-740 ISOLATOR ROW PLUS DETAIL

NTS

### **INSPECTION & MAINTENANCE**

#### INSPECT ISOLATOR ROW PLUS FOR SEDIMENT STEP 1)

- A. INSPECTION PORTS (IF PRESENT)
  - A.1. REMOVE/OPEN LID ON NYLOPLAST INLINE DRAIN
  - A.2. REMOVE AND CLEAN FLEXSTORM FILTER IF INSTALLED
  - USING A FLASHLIGHT AND STADIA ROD, MEASURE DEPTH OF SEDIMENT AND RECORD ON MAINTENANCE LOG LOWER A CAMERA INTO ISOLATOR ROW PLUS FOR VISUAL INSPECTION OF SEDIMENT LEVELS (OPTIONAL) A.3.
  - A.4.
  - A.5. IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.
- B. ALL ISOLATOR PLUS ROWS
- B.1. REMOVE COVER FROM STRUCTURE AT UPSTREAM END OF ISOLATOR ROW PLUS
- USING A FLASHLIGHT, INSPECT DOWN THE ISOLATOR ROW PLUS THROUGH OUTLET PIPE B.2.
  - i) MIRRORS ON POLES OR CAMERAS MAY BE USED TO AVOID A CONFINED SPACE ENTRY ii) FOLLOW OSHA REGULATIONS FOR CONFINED SPACE ENTRY IF ENTERING MANHOLE
- B.3. IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.
- STEP 2) CLEAN OUT ISOLATOR ROW PLUS USING THE JETVAC PROCESS
  - A. A FIXED CULVERT CLEANING NOZZLE WITH REAR FACING SPREAD OF 45" (1.1 m) OR MORE IS PREFERRED
  - APPLY MULTIPLE PASSES OF JETVAC UNTIL BACKFLUSH WATER IS CLEAN Β.
  - C. VACUUM STRUCTURE SUMP AS REQUIRED
- STEP 3) REPLACE ALL COVERS, GRATES, FILTERS, AND LIDS; RECORD OBSERVATIONS AND ACTIONS.
- STEP 4) INSPECT AND CLEAN BASINS AND MANHOLES UPSTREAM OF THE STORMTECH SYSTEM.

### NOTES

- 1. INSPECT EVERY 6 MONTHS DURING THE FIRST YEAR OF OPERATION. ADJUST THE INSPECTION INTERVAL BASED ON PREVIOUS OBSERVATIONS OF SEDIMENT ACCUMULATION AND HIGH WATER ELEVATIONS.
- 2. CONDUCT JETTING AND VACTORING ANNUALLY OR WHEN INSPECTION SHOWS THAT MAINTENANCE IS NECESSARY.

				VOVEN GEOTEXTILE BETWEEN AMBERS DUS FABRIC WITHOUT SEAMS		SC-740 END CAP	
	4640 TRUEM	IAN BLVD					ŀ
4	HILLIARD, OF 1-800-733-747	H 43026 73	StormTach®				_ 
sн С		0				MANOTICK, CANADA	
EET DF			Chamber System			DATE: DRAWN: HN	
6			888-892-2694   WWW.STORMTECH.COM	DATE DRW CHK	DESCRIPTION	PROJECT #: CHECKED: N/A	
;	THIS DRAWING HAS BEEN PREPARED BASED ON IN RESPONSIBILITY OF THE SITE DESIGN ENGINEER T	INFORMATION PROV	HE PRODUCT(S) DEPICTED AND ALL ASSOCIATED DETAILS MEET ALL	R OR OTHER PROJECT REPRESENTA APPLICABLE LAWS, REGULATIONS, A	TVE. THE SITE DESIGN ENGINEER SHAL ND PROJECT REQUIREMENTS.	L REVIEW THIS DRAWING PRIOR TO CONSTRUCTION. IT IS THE UL	TIMATE
							]





SIZE (W X H X INSTALLED LENGTH)
CHAMBER STORAGE
MINIMUM INSTALLED STORAGE*
WEIGHT

PART #	STUB	Α	
SC740EPE06T / SC740EPE06TPC	6" (150 mm)	10.9" (277 mm)	
SC740EPE06B / SC740EPE06BPC	0 (130 mm)	10.9 (277 1111)	
SC740EPE08T /SC740EPE08TPC	8" (200 mm)	12.2" (310 mm)	
SC740EPE08B / SC740EPE08BPC	0 (200 mm)	12.2 (310 1111)	
SC740EPE10T / SC740EPE10TPC	10" (250 mm)	13 //" (3/0 mm)	
SC740EPE10B / SC740EPE10BPC	10 (200 mm)	10.4 (040 mm)	
SC740EPE12T / SC740EPE12TPC	12" (300 mm)	14 7" (373 mm)	
SC740EPE12B / SC740EPE12BPC	12 (300 mm)	14.7 (373 1111)	
SC740EPE15T / SC740EPE15TPC	15" (375 mm)	18 //" (/67 mm)	
SC740EPE15B / SC740EPE15BPC	13 (373 1111)	10.4 (407 1111)	
SC740EPE18T / SC740EPE18TPC	18" (450 mm)	19.7" (500 mm)	
SC740EPE18B / SC740EPE18BPC		13.7 (300 mm)	
SC740ECEZ*	24" (600 mm)	18.5" (470 mm)	



### NOTES

- 1. 8-30" (200-750 mm) GRATES/SOLID COVERS SHALL BE DUCTILE IRON PER ASTM A536 GRADE 70-50-05
- 12-30" (300-750 mm) FRAMES SHALL BE DUCTILE IRON PER ASTM A536 GRADE 70-50-05
   DRAIN BASIN TO BE CUSTOM MANUFACTURED ACCORDING TO PLAN DETAILS
- DRAINAGE CONNECTION STUB JOINT TIGHTNESS SHALL CONFORM TO ASTM D3212 4.
- FOR CORRUGATED HDPE (ADS & HANCOR DUAL WALL) & SDR 35 PVC 5. FOR COMPLETE DESIGN AND PRODUCT INFORMATION: WWW.NYLOPLAST-US.COM
- 6. TO ORDER CALL: 800-821-6710

Α	PART #	GRATE/S	SOLID COVER (	OPTIONS
8" (200 mm)	2808AG	PEDESTRIAN LIGHT DUTY	STANDARD LIGHT DUTY	SOLID LIGHT DUTY
10" (250 mm)	2810AG	PEDESTRIAN LIGHT DUTY	STANDARD LIGHT DUTY	SOLID LIGHT DUTY
12"	2812AG	PEDESTRIAN	STANDARD AASHTO	SOLID
(300 mm)		AASHTO H-10	H-20	AASHTO H-20
15"	2815AG	PEDESTRIAN	STANDARD AASHTO	SOLID
(375 mm)		AASHTO H-10	H-20	AASHTO H-20
18"	2818AG	PEDESTRIAN	STANDARD AASHTO	SOLID
(450 mm)		AASHTO H-10	H-20	AASHTO H-20
24"	2824AG	PEDESTRIAN	STANDARD AASHTO	SOLID
(600 mm)		AASHTO H-10	H-20	AASHTO H-20
30"	2830AG	PEDESTRIAN	STANDARD AASHTO	SOLID
(750 mm)		AASHTO H-20	H-20	AASHTO H-20

5497 MANOTICK MAIN STREET		MANOTICK, CANADA	DATE. DRAWN: HN		PROJECT #: CHECKED: N/A	ILL REVIEW THIS DRAWING PRIOR TO CONSTRUCTION. IT IS THE ULTIMATE
					DESCRIPTION	TATIVE. THE SITE DESIGN ENGINEER SH/ S, AND PROJECT REQUIREMENTS.
					DATE DRW CHK	ER OR OTHER PROJECT REPRESEN L APPLICABLE LAWS, REGULATIONS
	Nvinniset <sup>®</sup>				770-932-2443   WWW.NYLOPLAST-US.COM	DED TO ADS UNDER THE DIRECTION OF THE SITE DESIGN ENGINEE IE PRODUCT(S) DEPICTED AND ALL ASSOCIATED DETAILS MEET AL
4640 TRUEMAN BLVD	1-800-733-7473					THIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROVII RESPONSIBILITY OF THE SITE DESIGN ENGINEER TO ENSURE THAT TH
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NO PRODUCT SUBSTITUTIONS SHALL BE ACCEPTED UNLESS SUBMITTED 10 DAYS PRIOR TO PROJECT BID DATE, OR AS DIRECTED BY THE ENGINEER OF RECORD.

# STANDARD DETAIL NOT FOR CONSTRUCTION

							The design and information shown on this drawing is provided as a service to the project owner, engineer	and contractor by Imbrium Systems ("Imbrium"). Neither this drawing, nor any part thereof, may be used provided of our anones (if not	the prior written consent of imbrium. Failure to comply is done at the user's own risk and imbrium expression	discialms any liability or responsibility for such use. If discrementias halveen the summind information incom	which the drawing is based and actual field conditions are encountered as site work progresses, these	the reprint of the design imbrum accepts to the factor of the design imbrum accepts to the factor of the factor of the design imbrum accepts to the factor of the design improvement of the design impro	inaccurate imormaticon supplete py consta.
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INLET #2

OUTLET

# Stormceptor<sup>®</sup>



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### **Stormceptor Net Annual Sediment Load Reduction Sizing Tool Project Summary** Site Details Sizing Result < Back **Save Sizing Report** Cancel Project Name: 5497 Manotick Main, On Site Name: Manotick Main Location: Manotick / ON Site has been saved successfully. **Download Stormceptor Specifications & Drawings Download Stormceptor EFO Sizing Report Design Summary** Net Annual Sediment (TSS) Load **Reduction Sizing Summary** TSS Removal **Stormceptor Model** Provided (%) EFO4 90 92 EFO6 EFO8 93 EFO10 93 EFO12 93

- Recommended Stormceptor EFO Model: EFO4
- Estimated Net Annual Sediment (TSS) Load Reduction (%): 90
  - Water Quality Runoff Volume Capture (%): > 90

			Upstrear	n Flow Co	ntrolled Resu	lts		
Rainfall Intensity (mm/hr)	Percent Rainfall Volume	Cumulative Rainfall Volume	Flow Rate (L/s)	Flow Rate (L/min)	Surface Loading Rate (L/min/m <sup>2</sup> )	Removal Efficiency (%)	Incremental Removal (%)	Cumulative Removal (%)

pcswmm.stormceptor.com/Project/UpdateSite?ProjectHeaderId=MzMzNzE%3D&SiteId=NDI5MjY%3D&RequestFromSiteList=False&RedirectToSizingResult=1

#### 10/22/2020

### CreateProjectWithNetAnnual

1	51.3%	51.3%	0.21	12.6	10.5	93	47.7	47.7
2	8.7%	60.0%	0.42	25.2	21.0	93	8.1	55.8
3	5.8%	65.8%	0.63	37.8	31.5	93	5.4	61.2
4	4.6%	70.4%	0.84	50.4	42.0	93	4.3	65.5
5	4.2%	74.6%	1.05	63.1	52.5	92	3.9	69.3
6	3.2%	77.8%	1.26	75.7	63.1	91	2.9	72.2
7	2.6%	80.4%	1.47	88.3	73.6	90	2.3	74.6
8	2.4%	82.8%	1.68	100.9	84.1	89	2.1	76.7
9	1.9%	84.7%	1.89	113.5	94.6	88	1.7	78.4
10	1.6%	86.3%	2.10	126.1	105.1	87	1.4	79.8
11	1.3%	87.6%	2.31	138.7	115.6	86	1.1	80.9
12	1.1%	88.7%	2.52	151.3	126.1	85	0.9	81.8
13	1.3%	90.0%	2.73	163.9	136.6	84	1.1	82.9
14	1.1%	91.1%	2.94	176.5	147.1	83	0.9	83.8
15	0.6%	91.7%	3.15	189.2	157.6	81	0.5	84.3
16	0.8%	92.5%	3.36	201.8	168.1	80	0.6	85.0
17	0.7%	93.2%	3.57	214.4	178.6	79	0.6	85.5
18	0.5%	93.7%	3.78	227.0	189.2	77	0.4	85.9
19	0.6%	94.3%	3.99	239.6	199.7	76	0.5	86.4
20	0.5%	94.8%	4.20	252.2	210.2	75	0.4	86.7
21	0.2%	95.0%	4.41	264.8	220.7	74	0.1	86.9
22	0.4%	95.4%	4.62	277.4	231.2	73	0.3	87.2
23	0.5%	95.9%	4.83	290.0	241.7	72	0.4	87.5
24	0.4%	96.3%	5.04	302.6	252.2	72	0.3	87.8
25	0.1%	96.4%	5.25	315.3	262.7	71	0.1	87.9
26	0.3%	96.7%	5.46	327.9	273.2	70	0.2	88.1
27	0.4%	97.1%	5.67	340.5	283.7	69	0.3	88.4
28	0.2%	97.3%	5.88	353.1	294.2	68	0.1	88.5
29	0.2%	97.5%	6.09	365.7	304.7	67	0.1	88.6
30	0.2%	97.7%	6.31	378.3	315.3	66	0.1	88.8
31	0.1%	97.8%	6.52	390.9	325.8	65	0.1	88.8
32	0.2%	98.0%	6.73	403.5	336.3	64	0.1	89.0
33	0.1%	98.1%	6.94	416.1	346.8	63	0.1	89.0
34	0.1%	98.2%	7.15	428.7	357.3	63	0.1	89.1
35	0.1%	98.3%	7.36	441.4	367.8	62	0.1	89.2
36	0.2%	98.5%	7.57	454.0	378.3	61	0.1	89.3
37	1.5%	100.0%	7.78	466.6	388.8	60	0.9	90.2
38	0.1%	100.1%	7.99	479.2	399.3	58	0.1	90.2
39	0.1%	100.2%	8.20	491.8	409.8	58	0.1	90.3
40	0.1%	100.3%	8.41	504.4	420.3	57	0.1	90.3

pcswmm.stormceptor.com/Project/UpdateSite?ProjectHeaderId=MzMzNzE%3D&SiteId=NDI5MjY%3D&RequestFromSiteList=False&RedirectToSizingResult=1

#### 10/22/2020

### CreateProjectWithNetAnnual

41	0.1%	100.4%	8.62	517.0	430.8	57	0.1	90.4
42	0.1%	100.5%	8.83	529.6	441.4	57	0.1	90.5
43	0.2%	100.7%	9.04	542.2	451.9	57	0.1	90.6
44	0.1%	100.8%	9.25	554.8	462.4	56	0.1	90.6
45	0.1%	100.9%	9.46	567.5	472.9	56	0.1	90.7
46	-0.9%	100.0%	9.67	580.1	483.4	56	N/A	N/A
47	0.1%	100.1%	9.88	592.7	493.9	55	0.1	90.2
48	-0.1%	100.0%	10.09	605.3	504.4	55	N/A	N/A
49	0.0%	100.0%	10.30	617.9	514.9	55	0.0	90.2
50	0.0%	100.0%	10.51	630.5	525.4	54	0.0	90.2

**Download Stormceptor Specifications & Drawings** 

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# APPENDIX "E" Boundary Conditions

### Boundary Conditions 5497 Manotick Main Street

### Provided Information

Secondria	Demand	
L/min L/s	L/s	
Average Daily Demand	7	0.12
Maximum Daily Demand	17	0.29
Peak Hour	38	0.64
Fire Flow Demand #1	9,000	150.00

### Location



### **Results – Existing Conditions**

Connection 1 – Manotick Main St.

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	156.9	98.3
Peak Hour	140.3	74.6
Max Day plus Fire 1	127.1	55.9

Ground Elevation = 87.8 m

### Results – SUC Zone Reconfiguration

### Connection 1 – Manotick Main St.

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	146.6	83.6
Peak Hour	141.0	75.7
Max Day plus Fire 1	121.0	47.2

Ground Elevation = 87.8 m

### Notes

- 1. As per the Ontario Building Code in areas that may be occupied, the static pressure at any fixture shall not exceed 552 kPa (80 psi.) Pressure control measures to be considered are as follows, in order of preference:
  - a. If possible, systems to be designed to residual pressures of 345 to 552 kPa (50 to 80 psi) in all occupied areas outside of the public right-of-way without special pressure control equipment.
  - b. Pressure reducing valves to be installed immediately downstream of the isolation valve in the home/ building, located downstream of the meter so it is owner maintained.

### Disclaimer

The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation. Fire Flow analysis is a reflection of available flow in the watermain; there may be additional restrictions that occur between the watermain and the hydrant that the model cannot take into account.

# APPENDIX "F" Engineering Drawings

### EROSION AND SEDIMENT CONTROL MEASURES:

\*\* CONTRACTOR IS RESPONSIBLE FOR ALL INSTALLATION, MONITORING, REPAIR AND REMOVAL OF ALL EROSION AND SEDIMENT CONTROL FEATURES \*\*

# 1. PRIOR TO START OF CONSTRUCTION:

- 1.1. PRIOR TO THE REMOVAL OF ANY VEGETATIVE COVER, MOVING OF ANY SOIL, AND CONSTRUCTION:
  1.1.1. INSTALL SILT FENCE IMMEDIATELY DOWNSTREAM FROM AREAS TO BE DISTURBED (SEE PLAN FOR
- LOCATION). 1.1.2. INSTALL INSERTS WITH AN OVERFLOW IN ALL THE DOWNSTREAM CATCH BASINS AND MANHOLES. GEOSOCK
- DOWNSTREAM CATCH BASINS AND MANHOLES. GEOSOC AS REQUESTED BY THE CITY. 1.1.3. INSTALL FILTERS IN ALL CONCRETE CATCH BASIN
- STRUCTURES. 1.1.4. INSPECT MEASURES IMMEDIATELY AFTER INSTALLATION.
- 2. DURING CONSTRUCTION:
- 2.1. WORK TO BE DONE IN THE VICINITY OF MAJOR
- WATERWAYS TO BE CARRIED OUT FROM JULY TO SEPTEMBER ONLY.
- 2.2. MINIMIZE THE EXTENT OF DISTURBED AREAS AND THE DURATION OF EXPOSURE.
- 2.3. PROTECT DISTURBED AREAS FROM RUNOFF.2.4. PROVIDE TEMPORARY COVER SUCH AS SEEDING OR
- MULCHING IF DISTURBED AREA WILL NOT BE REHABILIATED WITHIN 30 DAYS. 2.5. INSPECT SILT FENCE, FILTER CLOTHS, AND CATCH BASIN
- SUMPS WEEKLY AND AFTER EVERY MAJOR STORM EVENT. CLEAN AND REPAIR WHEN NECESSARY 2.6. PLAN TO BE REVIEWED AND REVISED AS REQUIRED
- 2.0. I DAN TO BE REVIEWED AND REVISED AS REQUIREDDURING CONSTRUCTION.2.7. EROSION CONTROL FENCING TO BE ALSO INSTALLED
- 2.7. EROSION CONTROL PENCING TO BE ALSO INSTALLED AROUND THE BASE OF ALL STOCKPILES.
  2.8. DO NOT LOCATE TOPSOIL PILES AND EXCAVATION MATERIAL CLOSER THAN 2.5m FROM ANY PAVED SURFACE,
- MATERIAL CLOSER THAN 2.5m FROM ANY PAVED SURFACE, OR ONE WHICH IS TO BE PAVED BEFORE PILE IS REMOVED. ALL TOPSOIL PILES ARE TO BE SEEDED IF THEY ARE TO REMAIN ON SITE LONG ENOUGH FOR SEEDS TO GROW (30 DAYS).

# LEGEND:

### EXISTING PROPERTY LINE TO REMAIN PROPOSED EASEMENT PROPOSED TERRACING (3:1 MIN.) PROPOSED DOOR ENTRANCE/EXIT ×50.00 PROPOSED ELEVATION ×50.00HP PROPOSED HIGH POINT ELEVATION ×50.00SW PROPOSED SWALE ELEVATION ×50.00SD PROPOSED SIDEWALK ELEVATION ×50.00EX MATCH INTO EXISTING ELEVATION PROPOSED BOTTOM OF WALL ×50.00BW ×50.00TW PROPOSED TOP OF WALL × 70.19 EXISTING ELEVATION PROPOSED OVERLAND MAJOR FLOW ROUTE PROPOSED SILT FENCE AS PER OPSD 219.110 ---->s ----->s ----->s ----->s ---- PROPOSED 100mmØ PERFORATED SUBDRAIN --- STM ----- STM ---- PROPOSED STORM SEWER - SAN - SAN - SAN - PROPOSED SANITARY SEWER - SAN - SAN - SAN - EXISTING SANITARY SEWER EXISTING WATERMAIN - WTR - WTR -PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN PROPOSED CURB STOP 8 PROPOSED PIPE INSULATION PROPOSED 100 YEAR HIGH WATER LEVEL STORM WATERSHED EXTENT WS-XX - AREA IN HECTARES PROPOSSED GRASS AREA PROPOSED CONCRETE FEATURES/SLAB PROPOSED HEAVY DUTY ASPHALT PROPOSED LIGHT DUTY ASPHALT PROPOSED GRAVEL AREA PROPOSED RIP RAP AS PER OPSD 810.010 PROPOSED WATER METER PROPOSED ACCESS GATE $\vdash$

- 2.9. CONTROL WIND-BLOWN DUST OFF SITE TO ACCEPTABLE LEVELS BY SEEDING TOPSOIL PILES AND OTHER AREAS
- TEMPORARILY (PROVIDE WATERING AS REQUIRED). 2.10. ALL EROSION CONTROL STRUCTURE TO REMAIN IN PLACE UNTIL ALL DISTURBED GROUND SURFACES HAVE BEEN STABILIZED EITHER BY PAVING OR RESTORATION OF
- VEGETATIVE GROUND COVER. 2.11. NO ALTERNATE METHODS OF EROSION PROTECTION SHALL BE PERMITTED UNLESS APPROVED BY THIS CONSULTING ENGINEER AND THE CITY DEPARTMENT OF PUBLIC WORKS. "TO PREVENT UNNECESSARY SEDIMENT DISCHARGE, THE CONTRACTOR IS PERMITTED TO PLACE ADDITIONAL SEDIMENT AND EROSION CONTROL MEASURES IN A TIMELY MANNER, IF REQUIRED. THE CONTRACTOR TO ADVISE CONSULTANT ONCE INSTALLED FOR INSPECTION."
- 2.12. CONTRACTOR RESPONSIBLE FOR CITY ROADWAY AND SIDEWALK TO BE CLEANED OF ALL SEDIMENT FROM VEHICULAR TRACKING ETC, AT THE END OF EACH WORK DAY
- 2.13. DURING WET CONDITIONS, TIRES OF ALL VEHICLES/EQUIPMENT LEAVING THE SITE ARE TO BE SCRAPED.
- 2.14. ANY MUD/MATERIAL TRACKED ONTO THE ROAD SHALL BE REMOVED IMMEDIATELY BY HAND OR RUBBER TIRE LOADER.
  2.15. TAKE ALL NECESSARY STEPS TO PREVENT BUILDING MATERIAL, CONSTRUCTION DEBRIS OR WASTE BEING SPILLED OR TRACKED ONTO ABUTTING PROPERTIES OR PUBLIC STREETS DURING CONSTRUCTION AND PROCEED IMMEDIATELY TO CLEAN UP ANY AREAS SO AFFECTED.
- 3. AFTER CONSTRUCTION:
- 3.1. PROVIDE PERMANENT COVER CONSISTING OF TOPSOIL
  AND SEED TO DISTURBED AREA.
  3.2. INSPECT AND CLEAN CATCH PASIN SUMPS AND STORM
- 3.2. INSPECT AND CLEAN CATCH BASIN SUMPS AND STORM SEWERS.



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		THICKN	IESS (mm)	CON
COURSE	MATERIAL	AUTOMOBILE PARKING	TRUCK ROUTE (HEAVY TRAFFIC)	 مر
SURFACE	HL.3 A/C (PG 58-28)	50	40	
BINDER	HL.8 A/C (PG 58-28)		50	
BASECOURSE	GRANULAR "A"	150	150	
SUBBASE	GRANULAR "B" TYPE <b>II</b>	350	450	

NOTE: IN PREPARATION FOR PAVEMENT CONSTRUCTION AT THIS SITE, ANY SURFICIAL OR NEAR SURFACE/SUBGRADE LEVEL TOPSOIL AND ANY SOFT, WET OR DELETERIOUS MATERIALS SHOULD BE REMOVED FROM THE PROPOSED PAVED AREAS. THE EXPOSED SUBGRADE SHOULD BE INSPECTED AND APPROVED BY GEOTECHNICAL PERSONNEL AND ANY SOFT AREAS EVIDENT SHOULD BE SUBEXCAVATED AND REPLACED WITH SUITABLE EARTH BORROW APPROVED BY THE GEOTECHNICAL ENGINEER. THE SUBGRADE SHOULD BE SHAPED AND CROWNED TO PROMOTE DRAINAGE OF THE SITE DRAINAGE STRUCTURES. FOLLOWING APPROVAL OF THE PREPARATION OF THE SUBGRADE, THE PAVEMENT GRANULARS MAY BE PLACED.





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		ENGINEERING STAMP
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		G. L. BRUNET E 100191036 "108/2022 BOWINCE OF ONTARIO
		#8 #7 #6
		#0       #1         #5          #4       ISSUED AS PER CITY COMMENTS       11 / 08 / 2022         #3       ISSUED FOR SPA       12 / 10 / 2021         #2       ISSUED FOR SPA       06 / 08 / 2021         #1       ISSUED FOR SPA       10 / 03 / 2021         NO.       REVISION       DATE (DD/MM/YYYY)
		B BLANCHARD LETENDRE ENGINEERING
SITE BENCHMARK FIRE HYDRANT TOP OF SPINDLE ELEV. = 88.50	04 X	767, Notre Dame, Local 42, Embrun, Ontario, KOA WI (613) 693-0700 blengheering.ca
— san	50 - SAN - SAN	12213559 CANADA INC. 996-B ST. AUGUSTIN RD. EMBRUN, ON
<ul> <li>WTR WTR WTR WTR WTR WTR</li> </ul>		PROJECT: NEW MULTIPURPOSE DEVELOPMENT 5497 MANOTICK MAIN ST, MANOTICK, ON
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1m 3m 5m — stm — SCALE: 1:200 stm — stm — stm —	15m 	PAPER FORMAT: 24x36 PAGE:
		DRAWN BY: BF + GB CHECKED BY: GB DATE: 09-2022 SCALE: 1:200 PROJECT NUMBER: 20-261

LEGEND:         PROPOSED EASEMENT         PROPOSED TERRACING (3: MIN.)         PROPOSED DOOR ENTRANCE/EXIT         %50.00F       PROPOSED DOOR ENTRANCE/EXIT         %50.00F       PROPOSED SIDE LEVATION         %50.00SD       PROPOSED SIDE VALE ELEVATION         %50.00SD       PROPOSED SIDTOM OF WALL         %50.00SD       PROPOSED SOTTOM OF WALL         %50.00SD       PROPOSED SOTOM OF WALL         %50.00SD       PROPOSED SOTOM OF WALL         %50.00SD       PROPOSED SOTOM SPENEN         %60.00TW       PROPOSED SOTAM SPENEN         %000TW       PROPOSED SOTAM SPENEN         %000TW       PROPOSED SOTAM SPENEN         %00TW       EXISTING SANTARY SEVER         %00TW       EXISTING SANTARY SEVER <td< th=""></td<>
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PROPOSED EASEMENT PROPOSED TERRACING (3:1 MIN.) PROPOSED DOOR ENTRANCE/EXIT *50.001 PROPOSED DELEVATION *50.005W PROPOSED ELEVATION *50.005W PROPOSED SUBWALK ELEVATION *50.005W PROPOSED SOLEWALK ELEVATION *50.005W PROPOSED BOTTOM OF WALL *50.001W PROPOSED BOTTOM OF WALL *50.001W PROPOSED BOTTOM OF WALL *50.001W PROPOSED SOLE LEVATION *50.005W PROPOSED SOLEWALK ELEVATION *50.005W PROPOSED SOLEWALK ELEVATION *50.005W PROPOSED SOLEWALK ELEVATION *50.005W PROPOSED SOLEWALK *50.001W PROPOSED
PROPOSED TERRACING (3:1 MIN.) PROPOSED DOOR ENTRANCE/EXIT ×50.005 PROPOSED ELEVATION ×50.005W PROPOSED SWALE ELEVATION ×50.005W PROPOSED SWALE ELEVATION ×50.005W PROPOSED SUBWALK ELEVATION ×50.005W PROPOSED BOTTOM OF WALL ×50.005W PROPOSED BOTTOM OF WALL ×50.007W PROPOSED DOT OF WALL ×50.007W PROPOSED DOT OF OF WALL ×50.007W PROPOSED OT OF OF WALL ×50.007W PROPOSED OT OF OF WALL ×50.007W PROPOSED SWATCH AND MAJOR FLOW ROUTE PROPOSED OVERLAND MAJOR FLOW ROUTE PROPOSED SUIT FENCE AS PER OPSD 219,110 PROPOSED SUIT FENCE AS PER OPSD 219,110 PROPOSED SITT SWEER SMM SAN PROPOSED SANTARY SEVER SMM SAN PROPOSED SANTARY SEVER SMM SAN PROPOSED SANTARY SEVER SMM SAN PROPOSED CANTARY SEVER PROPOSED CANTARY SEVER PROPOSED COLOR STOP PROPOSED COLOR STOP PROPOSED CURB STOP PROPOSED STOP PROPOSED STOP PROPOSED STOP PROPOSED STOP PROPOSED STOP PROPOSED STOP PR
PROPOSED DOOR ENTRAINCE/EXIT       ×50.00     PROPOSED ELEVATION       ×50.005D     PROPOSED SUBLEVATION       ×50.005W     PROPOSED SUBWALE ELEVATION       ×50.005W     PROPOSED SUBWALE ELEVATION       ×50.005W     PROPOSED SUBWALE ELEVATION       ×50.005W     PROPOSED BOTOM OF WALL       ×50.005W     PROPOSED TOP OF WALL       ×50.005W     PROPOSED SUT FENCE AS PER OPSD 219.110       PROPOSED SULT FENCE AS PER OPSD 219.110       PROPOSED SANTARY SEWER       WITH     WITH       WITH     WITH       WITH     EXISTING SANTARY SEWER       PROPOSED CURB STOP       PROPOSED DU VEAR HIGH WATER LEVEL       STORM WATERSHED EXTENT       VITH       VITH       VITH
*50.00       PROPOSED ELEVATION         *50.00HP       PROPOSED HIGH POINT ELEVATION         *50.00SW       PROPOSED SUBWALK ELEVATION         *50.00SD       PROPOSED SUBWALK ELEVATION         *50.00EX       MATCH INTO EXISTING ELEVATION         *50.00SW       PROPOSED DOT OF WALL         *50.00TW       PROPOSED TOP OF WALL         *50.00TW       PROPOSED TOP OF WALL         *50.00TW       PROPOSED OVERLAND MAJOR FLOW ROUTE         PROPOSED SULT FENCE AS PER OPSD 219.110         PROPOSED SONTARY SEWER         *50.00TW       PROPOSED SONTARY SEWER         *50.00TW       PROPOSED SONTARY SEWER         *50.00TW       PROPOSED CATCHBASINMANHOLE/CATCHBASIN         PROPOSED OPER INSULATION       PROPOSED OPER INSULATION         *50.00TW       PROPOSED OPER EXTENT         *50.00TW       PROPOSED OPER INSULATION         *60.00TW       PROPOSED CATCHBASINMANHOLE/CATCHBASIN         *60.00TW       PROPOSED CATCHBASINMANHOLE/CATCHBASIN         *77.01       WITR       WITR         *77.01
*50.00HP       PROPOSED HIGH POINT ELEVATION         *50.00SW       PROPOSED SWALE ELEVATION         *50.00SD       PROPOSED SIDEWALK ELEVATION         *50.00SK       MATCH INTO EXISTING ELEVATION         *50.00FX       PROPOSED TOP OF WALL         *50.00TW       PROPOSED TOP OF WALL         *70.19       EXISTING ELEVATION         *70.19       PROPOSED OVERLAND MAJOR FLOW ROUTE         PROPOSED DION PROPOSED STORM SEWER       PROPOSED STORM SEWER         *55.00       BAN       SAN         *51.10       SINT       EXISTING SANITARY SEWER         *100       PROPOSED CUBB STOP       PROPOSED CUB STOP         *100 VERA HIGH WATER LEVEL       STORM WATERSHED EXTENT         *100 VERA HIGH WATER LEVEL       STORM WATERSHED NAME         *100 VERTO
*50.00SW       PROPOSED SWALE ELEVATION         *50.00SD       PROPOSED SIDEWALK ELEVATION         *50.00EX       MATCH INTO EXISTING ELEVATION         *50.00BW       PROPOSED DOTOM OF WALL         *50.00TW       PROPOSED TOP OF WALL         *7019       EXISTING ELEVATION         PROPOSED OVERLAND MAJOR FLOW ROUTE       PROPOSED OVERLAND MAJOR FLOW ROUTE         PROPOSED SULT FENCE AS PER OPSD 219.110       PROPOSED SIDEM SEWER         *5M       SAN         SAN       SAN         SAN       SAN         PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN         PROPOSED TOB         PROPOSED CONSED VALERMAIN         PROPOSED CONSED VALERMAIN         PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN         PROPOSED CONSED VIRE TIGH         PROPOSED TOP FOR VALE         PROPOSED TOR WATERSHED EXTENT         WATE WITH       WATERSHED NAME         RUNOFF COEFFICIENT         AREA IN HECTARES         PROPOSED GRASS AREA
*50.00SD       PROPOSED SIDEWALK ELEVATION         *50.00EX       MATCH INTO EXISTING ELEVATION         *50.00BW       PROPOSED BOTTOM OF WALL         *50.00TW       PROPOSED TOP OF WALL         *7019       EXISTING ELEVATION         *7019       EXISTING ELEVATION         *7019       PROPOSED OVERLAND MAJOR FLOW ROUTE         PROPOSED SULT FENCE AS PER OPSD 219.110         *5       PROPOSED MAILK SEWER         *5M       SAN
*50.00EX       MATCH INTO EXISTING ELEVATION         *50.00BW       PROPOSED BOTTOM OF WALL         *50.00TW       PROPOSED TOP OF WALL         *7019       EXISTING ELEVATION         *7019       PROPOSED OVERLAND MAJOR FLOW ROUTE         PROPOSED SILT FENCE AS PER OPSD 219.110         PS       PROPOSED STORM SEWER         SMA       STM         SMA       PROPOSED STORM SEWER         SMA       PROPOSED ANITARY SEWER         WITR       WITR         PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN         PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN         PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN         PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN         PROPOSED COURS STOP         PROPOSED DIO YEAR HIGH WATER LEVEL         STORM WATERSHED EXTENT         WATERSHED NAME         RUNOFF COEFFICIENT         AREA IN HECTARES         PROPOSED GRASS AREA
<ul> <li>\$50.00BW PROPOSED BOTTOM OF WALL</li> <li>\$50.00TW PROPOSED TOP OF WALL</li> <li>70.19 EXISTING ELEVATION</li> <li>PROPOSED OVERLAND MAJOR FLOW ROUTE</li> <li>PROPOSED SOLUT FENCE AS PER OPSD 219.110</li> <li>PROPOSED STORM SEWER</li> <li>SAN SAN PROPOSED STORM SEWER</li> <li>SAN SAN PROPOSED SANITARY SEWER</li> <li>WITR WITR PROPOSED SANITARY SEWER</li> <li>WITR WITR EXISTING SANITARY SEWER</li> <li>PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN</li> <li>PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN</li> <li>PROPOSED DIO YEAR HIGH WATER LEVEL</li> <li>STORM WATERSHED NAME</li> <li>WUTR WATERSHED NAME</li> <li>WATERSHED NAME</li> <li>WATERSHED NAME</li> <li>PROPOSED GRASS AREA</li> </ul>
*7019       EXISTING ELEVATION         *7019       EXISTING ELEVATION         *7019       PROPOSED OVERLAND MAJOR FLOW ROUTE         *7019       PROPOSED OVERLAND MAJOR FLOW ROUTE         *7019       PROPOSED SILT FENCE AS PER OPSD 219.110         ************************************
PROPOSED OVERLAND MAJOR FLOW ROUTE PROPOSED OVERLAND MAJOR FLOW ROUTE PROPOSED SILT FENCE AS PER OPSD 219.110 PROPOSED SILT FENCE AS PER OPSD 219.110 PROPOSED STORM SEWER SAM SAM SAM PROPOSED STORM SEWER SAM SAM SAM PROPOSED WATERMAIN SAM SAM SAM PROPOSED WATERMAIN SAM SAM SAM PROPOSED WATERMAIN SAM SAM SAM PROPOSED WATERMAIN SAM SAM SAM PROPOSED WATERMAIN PROPOSED CURB STOP PROPOSED CURB STOP PROPOSED 100 YEAR HIGH WATER LEVEL STORM WATERSHED EXTENT WATERSHED NAME RUNOFF COEFFICIENT AREA IN HECTARES PROPOSSED GRASS AREA
PROPOSED OVERLAND MAJOR FLOW ROUTE PROPOSED SILT FENCE AS PER OPSD 219.110 PROPOSED SILT FENCE AS PER OPSD 219.110 PROPOSED STORM SEWER SIM SIM SIM PROPOSED SANITARY SEWER SIM SIM SIM PROPOSED SANITARY SEWER WIR WIR PROPOSED WATERMAIN PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN PROPOSED CUB STOP PROPOSED CUB STOP PROPOSED CUB STOP PROPOSED DI0 YEAR HIGH WATER LEVEL STORM WATERSHED EXTENT WATERSHED NAME RUNOFF COEFFICIENT AREA IN HECTARES PROPOSED GRASS AREA
PROPOSED SILT FENCE AS PER OPSD 219.110         ->S       ->S         >SIM       SIM         SIM       SIM         PROPOSED STORM SEWER         SAN       SAN         PROPOSED SANITARY SEWER         WIR       WIR         WIR       PROPOSED WATERMAIN         SAN       SAN         SAN       SAN         PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN         PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN         PROPOSED CURB STOP         PROPOSED CURB STOP         PROPOSED IOU YEAR HIGH WATER LEVEL         STORM WATERSHED EXTENT         WATERSHED NAME         CONTROLLED         RUNOFF         AREA IN HECTARES         PROPOSSED GRASS AREA
Image: Signal Strip Strip       PROPOSED 100mmid PERFORATED SUBDRAIN         Image: Strip
STM       STM       PROPOSED STORM SEWER         SAN       SAN       PROPOSED SANITARY SEWER         WTR       WTR       PROPOSED WATERMAIN         SAN       SAN       EXISTING SANITARY SEWER         WTR       WTR       EXISTING SANITARY SEWER         PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN       PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN         PROPOSED 100 YEAR HIGH WATER LEVEL       STORM WATERSHED NAME         WS-XX       WATERSHED NAME         WOFF       AREA IN HECTARES         WTR       PROPOSSED GRASS AREA
SAN     SAN     PROPOSED WATERMAIN       WTR     WTR     PROPOSED WATERMAIN       SAN     SAN     EXISTING SANITARY SEWER       WTR     WTR     EXISTING WATERMAIN       PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN     PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN       PROPOSED CUB STOP     PROPOSED CUB STOP       PROPOSED DID USEAR HIGH WATER LEVEL     STORM WATERSHED EXTENT       VWATERSHED NAME     RUNOFF COEFFICIENT       AREA     IN HECTARES       PROPOSED GRASS AREA
SAN     SAN     EXISTING SANITARY SEWER       WIR     WIR     EXISTING WATERMAIN       PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN       PROPOSED CURB STOP       PROPOSED CURB STOP       PROPOSED DID YEAR HIGH WATER LEVEL       Storm WATERSHED EXTENT       WATERSHED NAME       RUNOFF COEFFICIENT       AREA IN HECTARES       PROPOSSED GRASS AREA
WIR WIR EXISTING WATERMAIN PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN PROPOSED CURB STOP PROPOSED CURB STOP PROPOSED 100 YEAR HIGH WATER LEVEL STORM WATERSHED EXTENT WATERSHED NAME RUNOFF COEFFICIENT AREA IN HECTARES PROPOSSED GRASS AREA
<ul> <li>PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN</li> <li>PROPOSED CURB STOP</li> <li>PROPOSED CURB STOP</li> <li>PROPOSED PIPE INSULATION</li> <li>PROPOSED 100 YEAR HIGH WATER LEVEL</li> <li>STORM WATERSHED EXTENT</li> <li>WATERSHED NAME</li> <li>RUNOFF COEFFICIENT</li> <li>AREA IN HECTARES</li> <li>PROPOSSED GRASS AREA</li> </ul>
PROPOSED PIPE INSULATION PROPOSED 100 YEAR HIGH WATER LEVEL STORM WATERSHED EXTENT WATERSHED NAME RUNOFF COEFFICIENT AREA IN HECTARES PROPOSSED GRASS AREA
PROPOSED 100 YEAR HIGH WATER LEVEL STORM WATERSHED EXTENT WS-XX WATERSHED NAME RUNOFF COEFFICIENT AREA RUNOFF COEFFICIENT AREA IN HECTARES PROPOSSED GRASS AREA
STORM WATERSHED EXTENT WS-XX CONTROLLED RUNOFF COEFFICIENT AREA RUNOFF AREA IN HECTARES PROPOSSED GRASS AREA
WS-XX CONTROLLED RUNOFF COEFFICIENT AREA RUNOFF AREA IN HECTARES PROPOSSED GRASS AREA
RUNOFF COEFFICIENT AREA RUNOFF AREA IN HECTARES PROPOSSED GRASS AREA
AREA IN HECTARES AREA IN HECTARES PROPOSSED GRASS AREA
PROPOSSED GRASS AREA
PROPOSED CONCRETE FEATURES/SLAB
PROPOSED HEAVY DUTY ASPHALT
PROPOSED LIGHT DUTY ASPHALT
PROPOSED GRAVEL AREA
PROPOSED RIP RAP AS PER OPSD 810.010
(M) PROPOSED WATER METER
PROPOSED ACCESS GATE





LEGEND:	
	EXISTING PROPERTY LINE TO REMAIN
	PROPOSED EASEMENT
	PROPOSED TERRACING (3:1 MIN.)
▼	PROPOSED DOOR ENTRANCE/EXIT
×E0.00	
×50.00	
~50.00HF	
×50.00SW	PROPOSED SWALE ELEVATION
×50.00SD	PROPOSED SIDEWALK ELEVATION
×50.00EX	
×50.00BW ×50.00TW	PROPOSED TOP OF WALL
× 70.19	EXISTING ELEVATION
	PROPOSED OVERLAND MAJOR FLOW ROUTE
······································	- PROPOSED SILT FENCE AS PER OPSD 219.110
	PROPOSED 100mmØ PERFORATED SUBDRAIN
— STM — STM — STM —	- PROPOSED STORM SEWER
— SAN — SAN — SAN —	- PROPOSED SANITARY SEWER
WTR WTR WTR	- PROPOSED WATERMAIN
— SAN — SAN — SAN —	- EXISTING SANITARY SEWER
— WTR — WTR — WTR —	
	PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN
0	
	STORM WATERSHED EXTENT
	WATERSHED NAME
AREA RUNOFF	-RUNOFF COEFFICIENT
	AREA IN HECTARES
<u>* * * *</u> * * * *	PROPOSSED GRASS AREA
	PROPOSED CONCRETE FEATURES/SLAB
	PROPOSED HEAVY DUTY ASPHALT
	PROPOSED LIGHT DUTY ASPHALT
	PROPOSED GRAVEL AREA
	PROPOSED RIP RAP AS PER OPSD 810.010
M	PROPOSED WATER METER
⊢ I	PROPOSED ACCESS GATE







NOTE: ALL DIMENSIONS ARE NOMINAL

SHEET 5 OF 6





