SOUTH MERIVALE BUSINESS PARK 99 BILL LEATHEM DRIVE, 2 LEIKIN DRIVE AND 20 LEIKIN DRIVE OTTAWA, ONTARIO

SERVICEABILITY REPORT

Prepared by:

NOVATECH

Suite 200, 240 Michael Cowpland Drive Ottawa, Ontario K2M 1P6

March 25, 2021

Ref: R-2021-034 Novatech File: 120187 March 25, 2021

City of Ottawa Planning and Growth Management Department 110 Laurier Avenue West, 4th Floor Ottawa, Ontario K1P 1J1

Attention: Sean Moore RPP/MCIP

Dear Mr. Moore:

Re: SOUTH MERIVALE BUSINESS PARK

99 BILL LEATHEM DRIVE, 2 LEIKIN DRIVE AND 20 LEIKIN DRIVE

Serviceability Report Our File No.: 120187

Please find enclosed the complete pdf copy of the above noted report dated March 25, 2021. This report is submitted in support of a Rezoning Application and is hereby submitted for review and approval.

If you have any questions, please contact the undersigned.

Yours truly,

NOVATECH

Cara Ruddle, P.Eng.

Senior Project Manager, Land Development Engineering

Novatech

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1.0. INTRODUCTION

Novatech has been retained to review the servicing for a proposed development located at 99 Bill Leathem Drive, 2 Leikin Drive and 20 Leikin Drive within the South Merivale Business Park within the City of Ottawa to support a Rezoning Application. *Figure 1* is a Key Plan showing the site location. The purpose of this report is to demonstrate that the existing municipal infrastructure within South Merivale Business Park can support the proposed additional uses.

2.0. EXISTING AND PROPOSED DEVELOPMENT

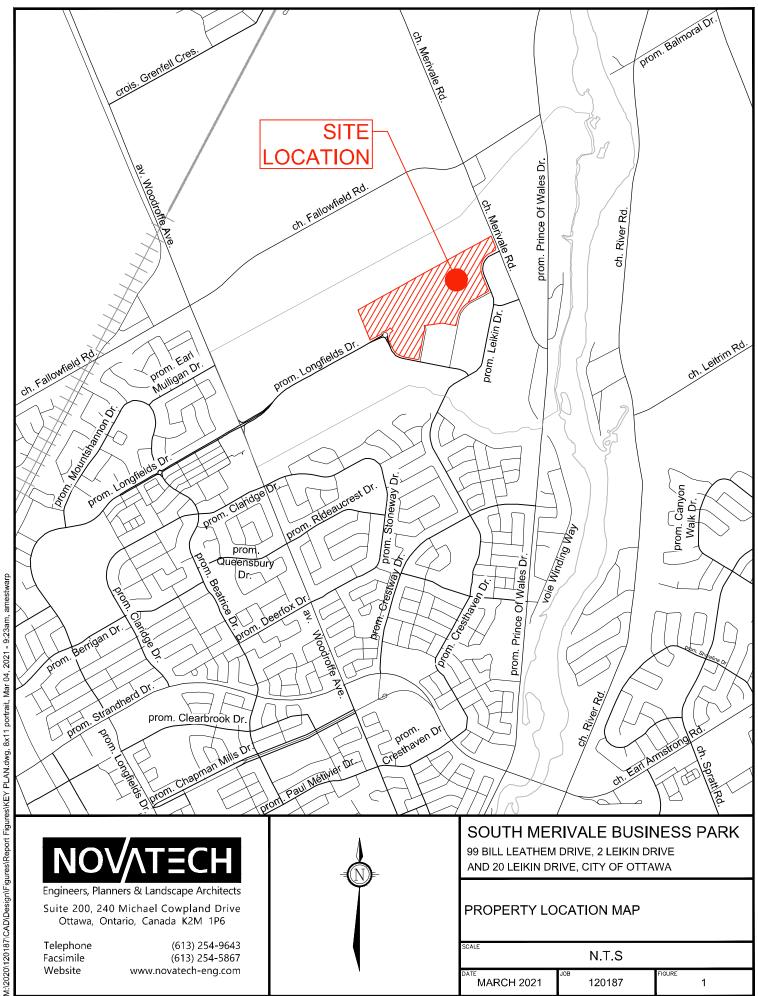
The property is approximately 30.57 hectares in size, and currently consists of undeveloped vacant land, and cultivated farm field. The property can be accessed from Bill Leathem Drive, Paragon Avenue, and Lekin Drive. There are existing easements containing a sanitary trunk sewer and overhead hydro lines that crosses through the property.

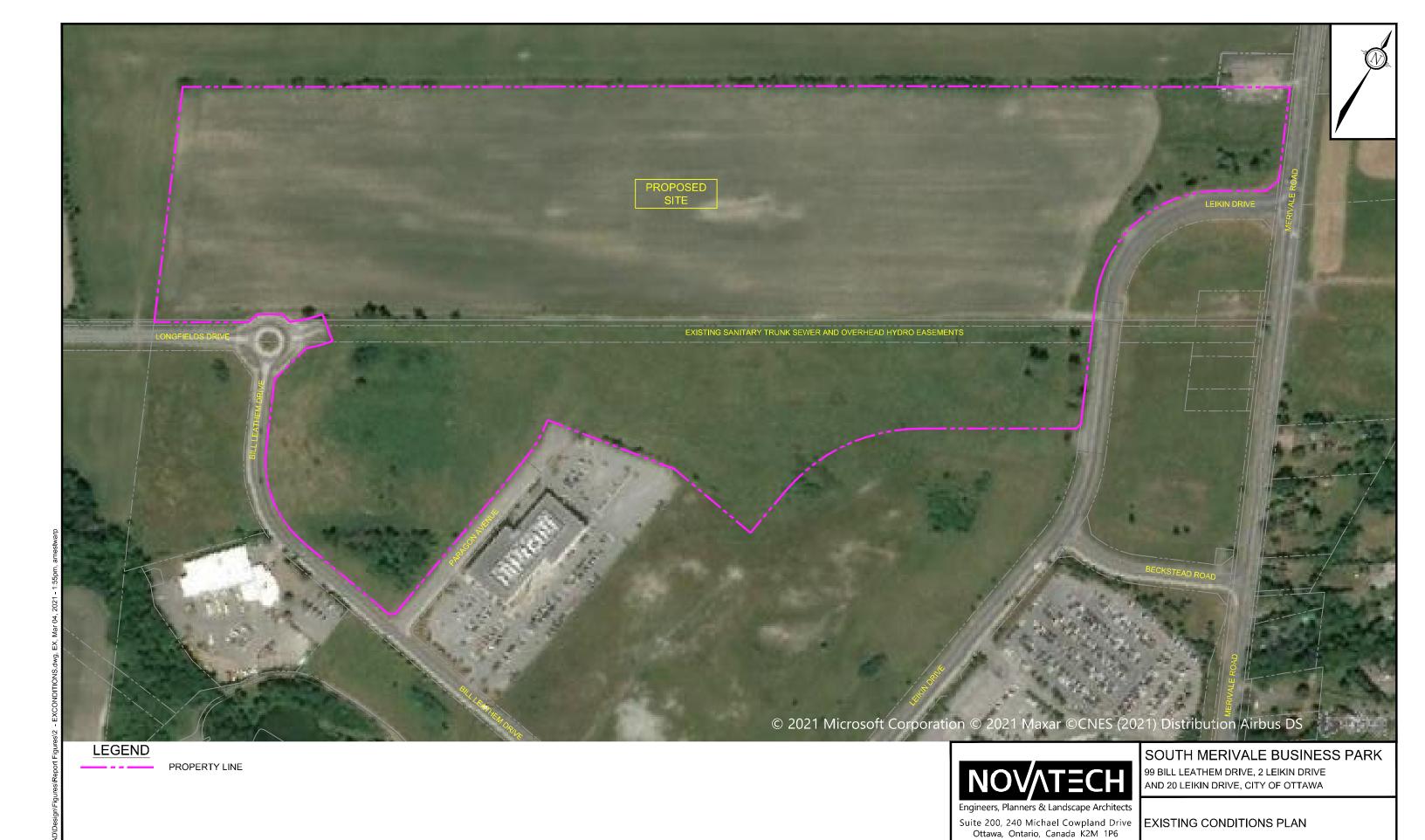
The property is bound by agricultural lands that are part of the City of Ottawa Greenbelt to the north and west and by the remainder of the South Merivale Business Park to the south and east including Leikin Drive, Paragon Avenue, Bill Leathem Drive, a 3-storey office building and vacant parcels. *Figure 2* shows the existing site conditions.

In 1992 the City of Nepean prepared a Development Plan (R-Plan by Farley, Smith & Murray Surveying Ltd.) for the South Merivale Business Park. However, this plan did not include a connection to Woodroffe Avenue via Longfields Drive. In 2009/2010 a connection between Woodroffe Avenue to Bill Leatham Drive was designed and constructed to provide westerly connectivity from the South Merivale Business Park. A contemplated draft plan was developed which revised the alignment of the future section of Bill Leatham Drive from Longfields Drive to Leikin Drive but was never deposited. In early 2021, the City of Ottawa removed the requirement for a connection from Bill Leatham Drive to Leikin Drive by returning unopened road allowances to the owners. Copies of the legal plans described above are provided in **Appendix A** for reference.

A servicing concept for the South Merivale Business Park has been completed and initial phases have been constructed (i.e. Leikin Drive, Bill Leathem Drive, Paragon Avenue). The servicing design information is provided in a report entitled 'City of Nepean, South Merivale Business Park, Phase II and III, Services Design Report' prepared by Novatech, dated June 23, 1992, hereafter referred to as SMBP Servicing Report. This report outlines the servicing for the roadways with consideration of future lot development. A copy of this report is provided in *Appendix E* for reference.

The proposed conceptual development consists of office, warehouse and truck transport uses. The site is expected to include a private east-west roadway that connects the Longfields roundabout, Paragon Avenue, and Leikin Drive. A preliminary Concept Plan is provided in **Appendix A** for reference. It is anticipated that the development will be phased.





^{ЈОВ} 120187

1 : 3000°

MARCH 2021

Telephone Facsimile

Website

(613) 254-9643 (613) 254-5867 www.novatech-eng.com

UT11V17 DMC - 270mmV122mm

3.0. WATER SERVICING

There are existing 300mm diameter watermains within Bill Leathem Drive and Paragon Avenue rights-of-ways, and an existing 400mm diameter watermain within the Leiken Drive right-of-way. There are also, existing 300mm diameter stubs at the end of Bill Leathem Drive, Paragon Avenue and Leiken Drive for use as future service connections to service the subject property. *Figure 3* shows the existing services surrounding the site.

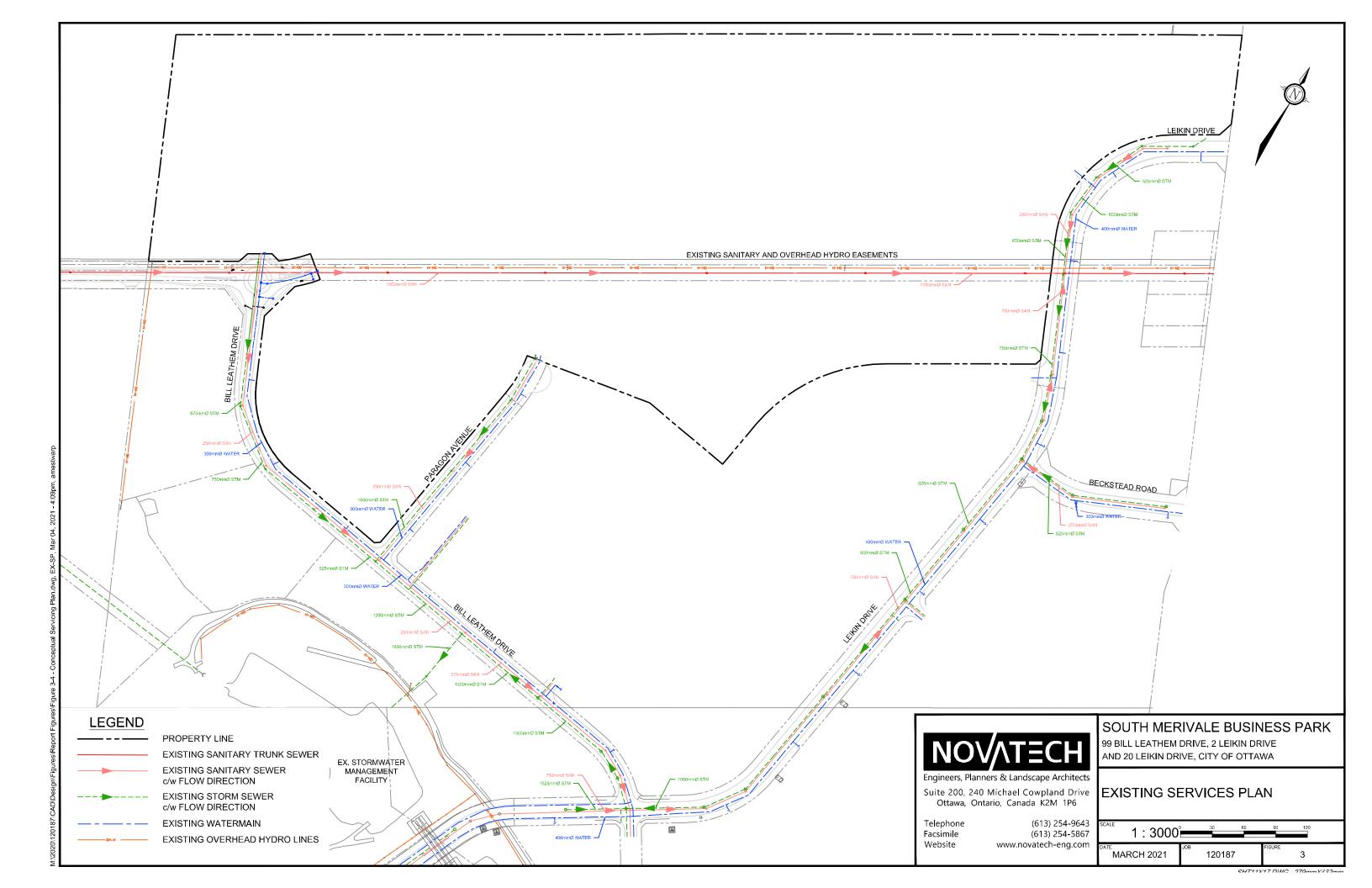
It is proposed to service the proposed development with private watermain and with connections between Bill Leathern Drive, Paragon Avenue and Leiken Drive to provide redundancy and watermain looping. *Figure 4* shows the conceptual service connection locations.

Water demand and fire flow calculations have been calculated from criteria in Section 4 of the City of Ottawa Design Guidelines for Water Distribution Systems. To determine the design flows for the proposed development it has been assumed that property will be 50% light industrial, and 50% commercial. The required fire demands for the subject site have been calculated using the Fire Underwriters Survey (CGI, 1999) document (FUS). Detailed FUS calculations were completed using assumptions on building construction and setback requirements. Preliminary water demand and fire flows are summarized in table below and supporting calculations are provided in **Appendix B**.

Table 3.1 Water Demand Summary

| Use | Ave. Daily | Max. Daily | Peak Hour | Fire Flow |
|---------------------------------|--------------|--------------|--------------|-----------|
| | Demand (L/s) | Demand (L/s) | Demand (L/s) | (L/s) |
| Light Industrial/ Commercial | 11.14 | 18.6 | 33.42 | 267 |

The above water demand information was submitted to the City of Ottawa for boundary conditions provided from the City's water model. The boundary conditions will determine whether the existing watermain infrastructure surrounding the development has capacity for the proposed development. The boundary conditions are provided in **Table 3.2**.



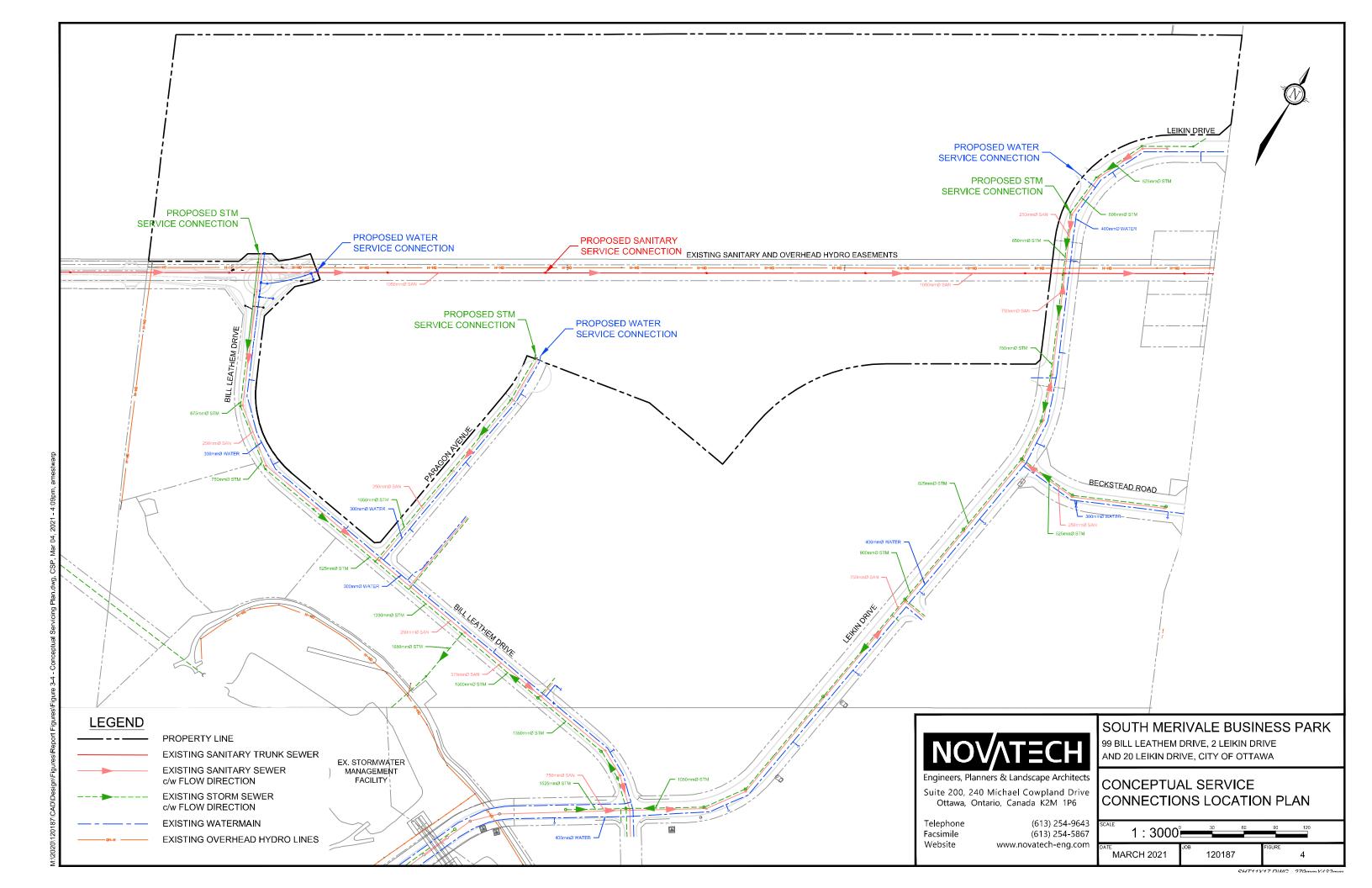


Table 3.2 Water Boundary Conditions

| Criteria | Head (m) | | | |
|---|-------------------|--|--|--|
| Connection to Existing 300mm Watermain Bill Leathem Drive | | | | |
| Minimum HGL | 132.7 | | | |
| Maximum HGL | 125.0 | | | |
| Max Day + Fire Flow HGL | 105.5 | | | |
| Connection to Existing 300mm Watermain | in Paragon Avenue | | | |
| Minimum HGL | 132.7 | | | |
| Maximum HGL | 125.0 | | | |
| Max Day + Fire Flow HGL | 109.9 | | | |
| Connection to Existing 300mm Watermain | in Leikin Drive | | | |
| Minimum HGL | 132.7 | | | |
| Minimum HGL | 125.0 | | | |
| Minimum HGL | 124.1 | | | |

The above boundary conditions were used to create a hydraulic model using EPANET for analyzing the performance of the proposed watermain system for three theoretical conditions: 1) High Pressure check under Average Day conditions, 2) Peak Hour demand, 3) Maximum Day + Fire Flow Demand. The following **Table 3.3** summarizes the results from the hydraulic water analysis.

Table 3.3 Water Analysis Results Summary

| Condition | Demand (L/s) | Min/Max Allowable Operating Pressures (psi) | Limits of Design Operating Pressures (psi) |
|---------------------|-----------------|---|--|
| High Pressure | 11.14 | 80psi (Max) | 60.4 |
| Max Day + Fire Flow | 285.6 | 20psi (Min) | 21.1 |
| Peak Hour | 33.42 | 40psi (Min) | 48.3 |

Through correspondence with the City it is understood that planned watermain improvements (SUC Zone reconfiguration), will result in altered boundary conditions for the site. The future boundary conditions are provided in **Table 3.4**.

Table 3.4 Future Water Boundary Conditions

| Criteria | Head (m) | | | |
|---|-------------------|--|--|--|
| Connection to Existing 300mm Watermain Bill Leathem Drive | | | | |
| Minimum HGL | 145.7 | | | |
| Maximum HGL | 143.1 | | | |
| Max Day + Fire Flow HGL | 118.1 | | | |
| Connection to Existing 300mm Watermain | in Paragon Avenue | | | |
| Minimum HGL | 145.6 | | | |
| Maximum HGL | 143.1 | | | |
| Max Day + Fire Flow HGL | 122.5 | | | |
| Connection to Existing 300mm Watermain | in Leikin Drive | | | |
| Minimum HGL | 132.3 | | | |
| Minimum HGL | 127.7 | | | |
| Minimum HGL | 114.4 | | | |

As per the above the SUC zone configuration will result in a notable increase in available head at the proposed Bill Leathem Drive, and Paragon Avenue connections, and a negligible decrease in the available head at the Leikin Drive connection. The future pressures at Bill Leathem Drive and Paragon avenue will be +/- 78 psi, which is just below the allowable 80 psi threshold. Thus, it is suggested that a pressure reducing valve be installed at the property limits to prevent high pressures within the private watermain system. The SUC Zone reconfiguration will improve the pressures to the site and will not adversely affect the feasibility of the subject development.

Based on the proceeding analysis it can be concluded that the watermain will provide adequate flow and pressures for the fire flow + maximum day demand and peak hour demand. Existing and proposed fire hydrants surrounding the development will provide fire protection for the proposed development. Refer to **Appendix B** for hydraulic calculations and City of Ottawa boundary conditions.

4.0. SANITARY SERVICING

There is existing 250m diameter sanitary sewers along Paragon Avenue, Bill Leathem Drive and Leiken Drive (north of the existing sanitary trunk sewer easement). There is an existing 750mm diameter sanitary sewer along Leikin Drive south of the easement and the trunk sewer within the easement is a 1050mm diameter sanitary sewer known as the Barrhaven Trunk Sanitary Sewer. Refer to **Figure 3** for existing servicing information.

The sanitary sewer outlet for the South Merivale Business Park is the Barrhaven Trunk Sanitary Sewer which flows to the West Rideau Collector Sewer. Existing sanitary manhole 62 is indicated as the outlet point to connect to the existing Barrhaven Trunk Sanitary Sewer which is located within the subject property. As envisioned in the SMBP Servicing Report, two drop pipes will be constructed to permit north and south access to the existing trunk sewer. It is also anticipated that clay seals will be required as part of sewer construction due to the depth of the existing sanitary sewer.

It is proposed to service the subject development with private sanitary services and connect directly to the Barrhaven Trunk Sanitary Sewer as per the original design intent. A sanitary drainage area plan for the proposed development is included in *Appendix C* for reference and shows the connection location to the existing sanitary sewer.

Preliminary sanitary flow calculations have been completed for the proposed development using criteria provided in the SMBP Servicing Report. Peak sanitary flows are calculated to be 48 L/s using a population equivalent of 100 persons per hectare as noted in the SMBP Servicing Report. Preliminary calculations are provided in *Appendix C* for reference.

The subject property was included in a previous design concept for the South Merivale Business Park to outlet to the Barrhaven Trunk Sanitary Sewer and the proposed rezoning sanitary sewer demands do not exceed the original sanitary flows from the previous Novatech design. Therefore, the existing infrastructure can service the proposed additional uses.

5.0. STORM SERVICING & STORMWATER MANAGEMENT

The topography of the site is generally flat and stormwater currently sheet drains in a southerly direction. There is an existing 675mm diameter storm sewer along Bill Leathem Drive with a similar size stub left for future development. There is an existing 1050mm diameter storm sewer along Paragon Avenue with a manhole provided for connection by future development. The existing storm sewer along Leikin Drive ranges in size from 650mm diameter to 900mm diameter. *Figure 3* shows the existing services surrounding the site.

The South Merivale Business Park is currently serviced by an existing stormwater management facility, south of Bill Leathem Drive, that flows into Barrhaven Creek. The subject property was included in the service area of the existing stormwater management facility. Coordination with the City has resulted in revised criteria for the stormwater management design for the site development. Correspondence with the City is provided in Appendix D. The stormwater management criteria for the subject property is as follows:

- Stormwater is to be controlled to a 5 year release rate using a runoff coefficient of 0.65 and a time of concentration of 15 minutes. Stormwater is to be controlled up to and including the 100 year storm event.
- Quality control of stormwater is provided by the existing stormwater management facility.

Preliminary stormwater management calculations have been completed for the proposed development. The allowable release rate was calculated using the above noted criteria and the original drainage areas from the original design concept for the South Merivale Business Park. The drainage areas from the original design concept are shown on the Existing Storm Drainage Areas Plan included in Appendix D.

The original concept included a portion of the site (area EX-04 on the Existing Storm Drainage Areas Plan) to drain to 'Street C' that has not been constructed. Therefore, this area does not currently have an outlet. It is proposed to redirect drainage from this area to another outlet within the subject property. Therefore, site drainage will need to be overcontrolled so as not to exceed the allowable release rate for the remaining existing drainage areas nor exceed the capacity of the existing downstream storm sewers. The allowable release rates are provided in the table below and detailed calculations are provided in **Appendix D**.

Table 5.1 - Allowable Release Rates

| Area | Outlet Location | Allowable Release Rate (L/s) | | | | |
|-------|--------------------|------------------------------|--|--|--|--|
| EX-01 | Bill Leathem Drive | 725.9 | | | | |
| EX-02 | Paragon Avenue | 3025.4 | | | | |
| EX-03 | Leikin Drive | 169.5 | | | | |

It is anticipated that stormwater storage could be provided within the proposed development on building roofs, on the surface around catchbasins or underground with orifice controls used to control the release of stormwater to the allowable release rate. Preliminary calculations were completed assuming a post-development runoff coefficient of 0.9. Stormwater storage requirements for each of the proposed drainage areas is summarized below and detailed calculations are included in Appendix D. This relates to a per hectare storage of approximately 222 m³/ha which is a reasonable quantity of storage to provide given the type of development.

Table 5.2 – Stormwater Storage Summary

| Area ID | Area (ha) | Outlet Location | 2 Year | 5 Year | 100 Year |
|---------|-----------|------------------|----------|----------|----------|
| | | | Required | Required | Required |
| | | | Storage | Storage | Storage |
| | | | (m^3) | (m³) | (m^3) |
| A-01 | 4.81 | Bill Leathem Dr. | 155.96 | 316.4 | 1065.42 |
| A-02 | 23.90 | Paragon Avenue | 950.07 | 1922.44 | 5931.60 |
| A-03 | 1.12 | Leikin Dr. | 36.40 | 73.88 | 248.78 |

It should be noted that the existing storm sewers at each of the potential connection points are 3 to 4m deep which means there is adequate cover to extend a storm sewer to service the subject property.

During storms in excess of the 100-year storm event, site grading will provide an overland flow route from the site. Per the original business park design, the overland flow route should be directed to existing road right-of-ways (Bill Leathern Drive, Paragon Avenue and Leikin Drive). These existing right-of-ways will direct overland storm drainage to the existing stormwater management facility and Barrhaven Creek.

In summary, the existing storm sewer infrastructure can service the proposed development and appropriate stormwater management methods can be used to meet the allowable release rate. Refer to **Appendix D** for preliminary stormwater management calculations and pre and post development drainage area figures.

6.0. EROSION AND SEDIMENT CONTROL MEASURES

Temporary erosion and sediment control measures will be required on-site during construction in accordance with the Best Management Practices for Erosion and Sediment Control. This includes the following temporary measures:

- Filter socks will be placed in existing catchbasins and manholes, and will remain in place until vegetation has been established and construction is completed;
- Silt fencing will be placed along the surrounding construction limits;
- Mud mats will be installed at the site entrances;
- The contractor will be required to perform regular street sweeping and cleaning as required, to suppress dust and to provide safe and clean roadways adjacent to the construction site;

The erosion and sediment control measures will be required prior to construction and will remain in place during all phases of construction. Regular inspection and maintenance of the erosion control measures will be undertaken

7.0. CONCLUSIONS AND RECOMMENDATIONS

The conclusions of this report are as follows:

- Water servicing, including both domestic and fire protection, can be provided by connection
 to the existing watermain infrastructure surrounding the site. It is proposed to provide
 internal watermain connections to Bill Leathern Drive, Paragon Avenue and Leikin Drive for
 looping and redundancy purposes.
- Sanitary servicing can be provided with an outlet to the existing Barrhaven Trunk Sanitary Sewer as per the original design concept for the business park.
- Storm servicing can be provided for the proposed development. Revised stormwater management criteria has been provided by the City. Stormwater quantity control can be provided within the proposed development through roof storage and/or underground storage tanks with orifice controls to control stormwater to the allowable release rate.
- An overland flow route will be provided to the existing surrounding right-of-ways which drain towards the existing stormwater management facility and Barrhaven Creek.
- Erosion and sediment control measures will be required during construction.

The preceding report is respectfully submitted for review and approval. Please contact the undersigned should you have any questions or require additional information.

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Prepared |

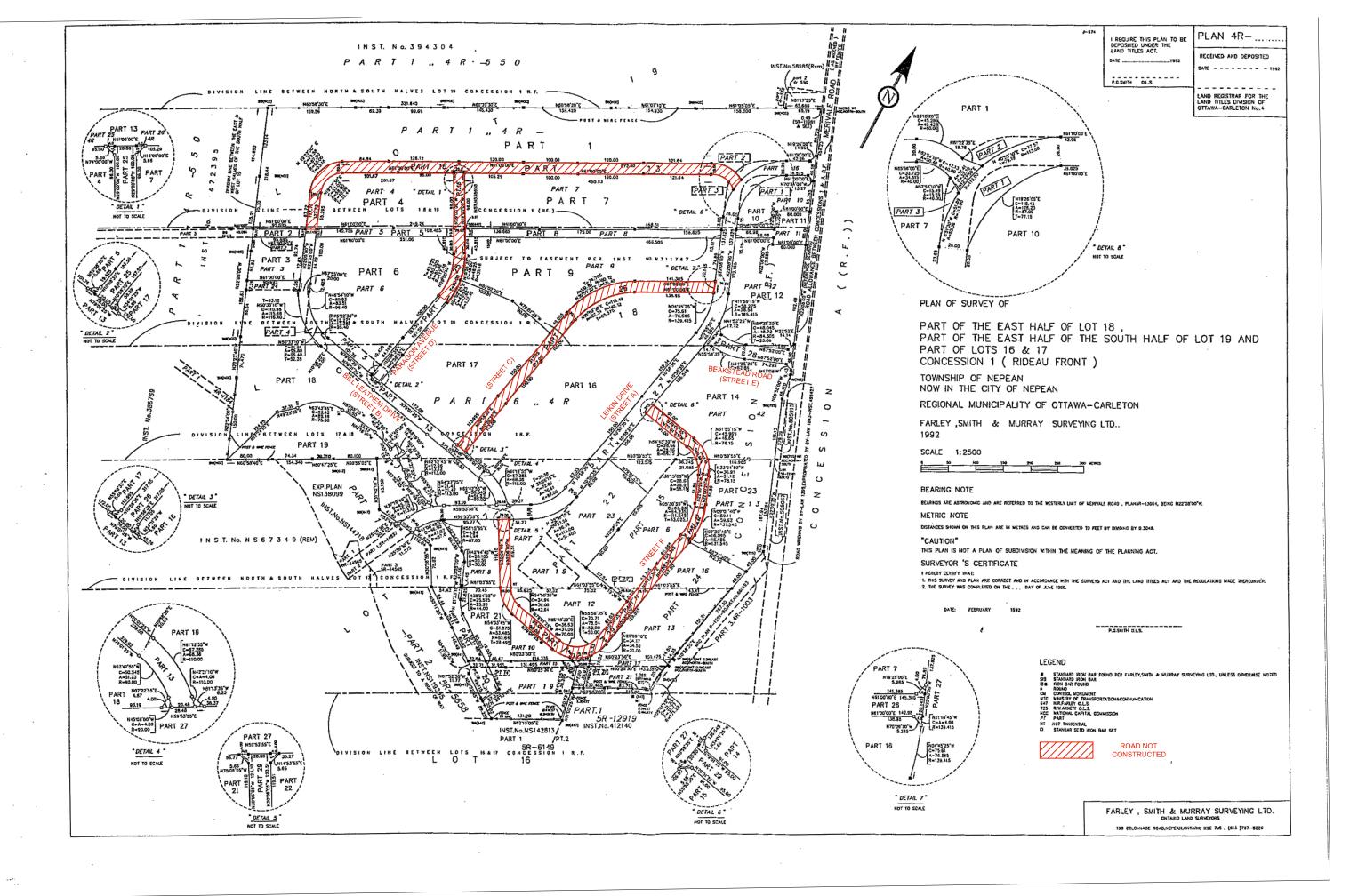
C.J. RUDDLE TO NOTE OF ON THE

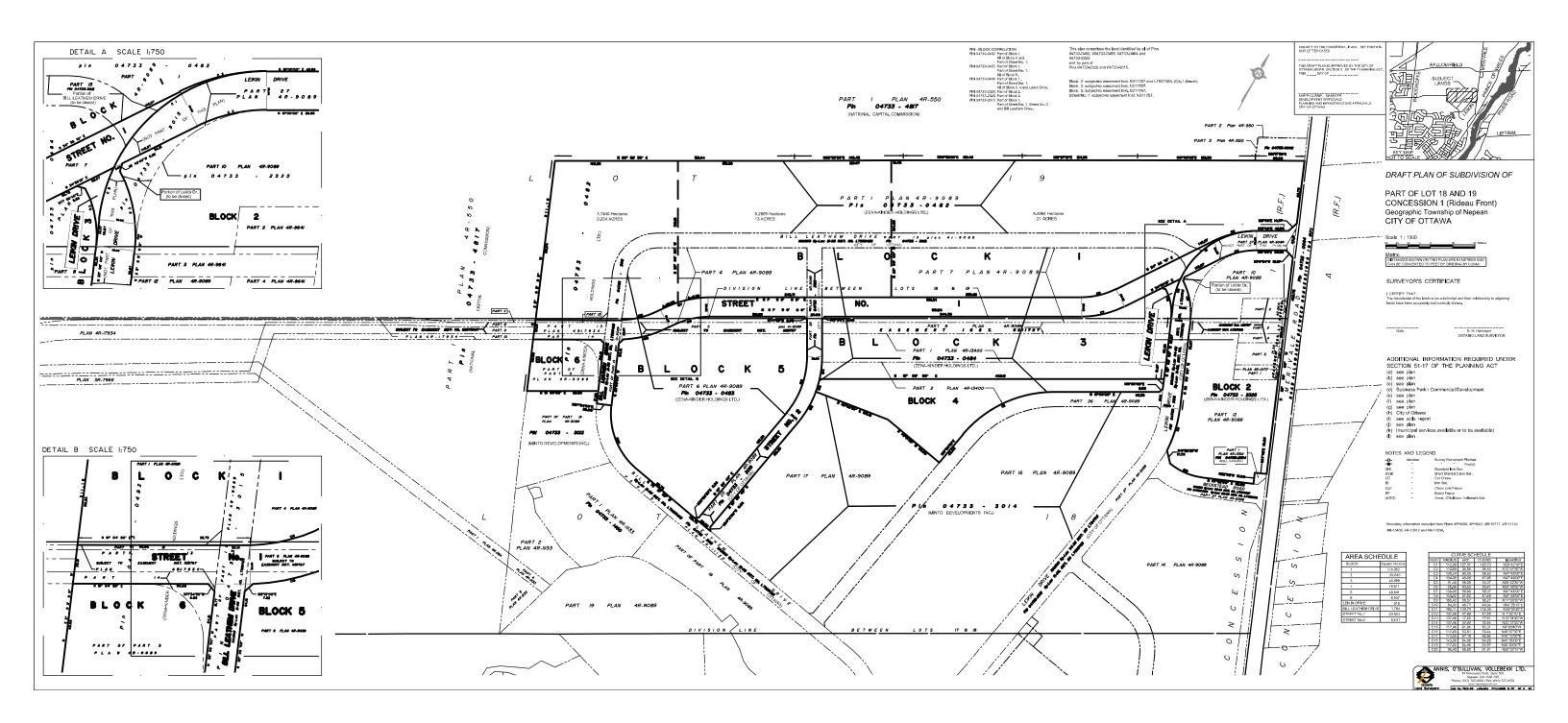
Cara Ruddle, P.Eng. Senior Project Manager Land Development Engineering Reviewed by:

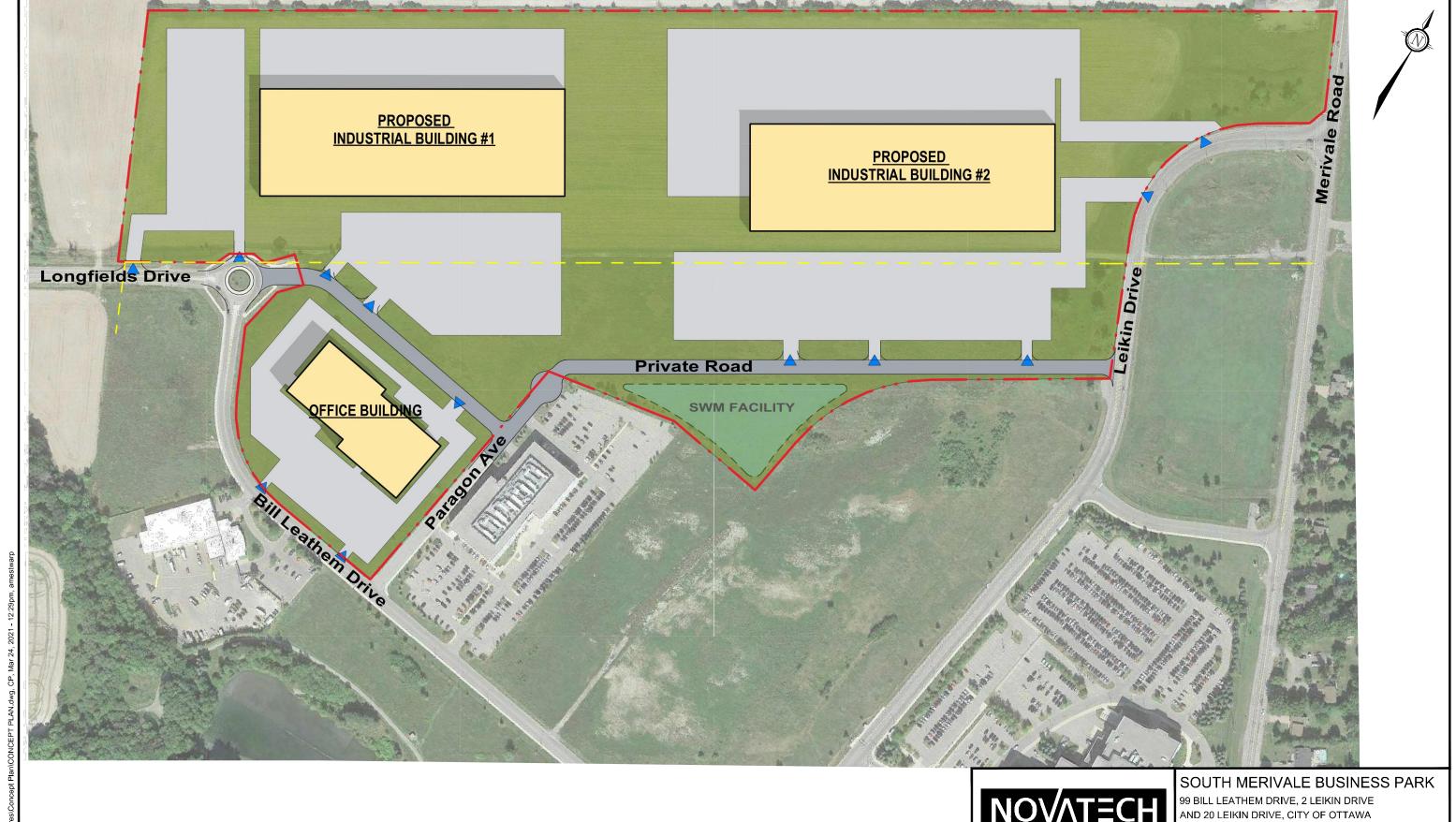
J. Lee Sheets, C.E.T.
Director
Land Development & Public Sector
Infrastructure

APPENDIX A

Legal Plans and Preliminary Concept Plan









Engineers, Planners & Landscape Architects Suite 200, 240 Michael Cowpland Drive Ottawa, Ontario, Canada K2M 1P6

Telephone Facsimile Website

(613) 254-9643 (613) 254-5867 www.novatech-eng.com

N.T.S MARCH 2021 120187

APPENDIX B

Watermain Information

DATE PREPARED: March, 2021

PROJECT #: 120187
PROJECT NAME: 99 BILL LEATHEM DRIVE,
2 LEIKIN DRIVE, AND 20 LEIKIN DRIVE
LOCATION: OTTAWA, ONTARIO



| Table 1 | | | | | |
|----------------------|------------------------|-----------|------------|-----------|--|
| | Wate | er Demand | | | |
| | Area (he) Demand (L/s) | | | | |
| | Area (ha) | Avg Day | Max. Daily | Peak Hour | |
| | | | | | |
| Light Industrial use | 15.29 | 6.19 | 11.14 | 20.05 | |
| Commercial Use | 15.29 | 4.95 | 7.43 | 13.37 | |
| | | | | | |
| Total | 30.57 | 11.14 | 18.6 | 33.42 | |

Avg. Daily Demand (City of Ottawa Sewer Design Guidelines):

- Light Industrial- Commercial35000L/ha/dayL/ha/day

Commercial / Industrial Peaking Factors (City of Ottawa Water Distrubution Guidelines)

Max. Daily Demand:1.5x Avg. DayPeak Hourly Demand:1.8x Max. Day

FUS - Fire Flow Calculations

As per 1999 Fire Underwriter's Survey Guidelines

Novatech Project #: 120187

Project Name: 99 Bill Leathern Dr., 2 Leikin Dr., and 20

Leikin Dr

Date: 3/4/2021

Input By: Anthony Mestwarp
Reviewed By: Cara Ruddle

Legend

Input by User

Engineers, Planners & Landscape Architects

No Information or Input Required

Building Description: Industrial

Fire Resistive Construction

| Step | | | Choose | | Value Used | Total Fire Flow (L/min) |
|------|-----------------|--|------------------|----------------|----------------|-------------------------------|
| | _ | Base Fire Flow | N | 1 | | |
| | Construction Ma | terial | | Multi | iplier | |
| 1 | Coefficient | Wood frame | | 1.5 | | |
| | related to type | Ordinary construction | | 1 | | |
| | of construction | Non-combustible construction | | 0.8 | i I | |
| | С | Modified Fire resistive construction (2 hrs) | Yes | 0.6 | | |
| | | Fire resistive construction (> 3 hrs) | | 0.6 | | |
| | Floor Area | | | | | |
| | | Building Footprint (m ²) | 37200 | | | |
| | Α | Number of Floors/Storeys | 5 | | | |
| 2 | | Protected Openings (1 hr) | Yes | | | |
| | | Area of structure considered (m ²) | | | 55,800 | |
| | F | Base fire flow without reductions | | | | 31,000 |
| | • | $F = 220 \text{ C } (A)^{0.5}$ | | | | 01,000 |
| | | Reductions or Surc | harges | | | |
| | Occupancy haza | ard reduction or surcharge | Reduction/Surcha | | /Surcharge | |
| | | Non-combustible | | -25% | | |
| 3 | (1) | Limited combustible | | -15% | | |
| 3 | | Combustible | Yes | 0% | 0% | 31,000 |
| | | Free burning | | 15% | | |
| | | Rapid burning | | 25% | | |
| | Sprinkler Reduc | tion | | Redu | ction | |
| | | Adequately Designed System (NFPA 13) | Yes | -30% | -30% | |
| 4 | (0) | Standard Water Supply | Yes | -10% | -10% | 45 500 |
| | (2) | Fully Supervised System | Yes | -10% | -10% | -15,500 |
| | | | Cun | nulative Total | -50% | |
| | Exposure Surch | arge (cumulative %) | | | Surcharge | |
| | | North Side | > 45.1m | | 0% | |
| 5 | | East Side | > 45.1m | | 0% | |
| 5 | (3) | South Side | > 45.1m | | 0% | 0 |
| | | West Side | > 45.1m | | 0% | |
| | | | Cun | nulative Total | 0% | |
| | | Results | | | | |
| | | Total Required Fire Flow, rounded to near | rest 1000L/mi | n | L/min | 16,000 |
| 6 | (1) + (2) + (3) | (2,000 L/min < Fire Flow < 45,000 L/min) | | or | L/s | 267 |
| | | (2,000 L/IIIII > FII6 FIOW > 40,000 L/IIIII) | | or | USGPM | 4,227 |
| | | Required Duration of Fire Flow (hours) | | | Hours | 3.5 |
| 7 | Storage Volume | Required Volume of Fire Flow (m ³) | | | m ³ | 3360 |
| | | rrequired volume of File Flow (III) | | | 111 | 5500 |

From: Sharif, Golam <<u>sharif.sharif@ottawa.ca</u>>
Sent: Tuesday, February 23, 2021 4:45 PM
To: Cara Ruddle <<u>c.ruddle@novatech-eng.com</u>>

Subject: RE: South Merivale Business Park - boundary conditions request

Hi Cara,

Please see the attached boundary condition. Please see the note, watermain looping is require to meet the pressure requirement. If you have any question, please let me know. Thanks.

Sharif

From: Cara Ruddle < c.ruddle@novatech-eng.com>

Sent: February 08, 2021 2:02 PM

To: Sharif, Golam < sharif.sharif@ottawa.ca>

Subject: RE: South Merivale Business Park - boundary conditions request

Please find attached a form which includes the FUS calculation as requested.

Thanks.

Cara Ruddle, P.Eng., Senior Project Manager | Land Development Engineering

NOVATECH Engineers, Planners & Landscape Architects

240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 Ext: 220 | Cell: 613.261.7719 | Fax: 613.254.5867

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From: Sharif, Golam <<u>sharif.sharif@ottawa.ca</u>>
Sent: Monday, February 8, 2021 12:53 PM
To: Cara Ruddle <<u>c.ruddle@novatech-eng.com</u>>

Subject: RE: South Merivale Business Park - boundary conditions request

Hi Cara,

Please provide the fire flow (FUS) calculation. Thanks.

Sharif

From: Cara Ruddle < <u>c.ruddle@novatech-eng.com</u>>

Sent: February 06, 2021 8:57 AM

To: Sharif, Golam <sharif.sharif@ottawa.ca>

Subject: FW: South Merivale Business Park - boundary conditions request

I tried to send the email below previously but I think I had your email address input incorrectly so I am resending my request for boundary conditions. Please let me know an approximate timeframe for receiving boundary conditions.

Thanks.

Cara Ruddle, P.Eng., Senior Project Manager | Land Development Engineering

NOVATECH Engineers, Planners & Landscape Architects

240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 Ext: 220 | Cell: 613.261.7719 | Fax: 613.254.5867

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From: Cara Ruddle

Sent: Tuesday, February 2, 2021 3:48 PM

To: 'sharif.golam@ottawa.ca' <sharif.golam@ottawa.ca>

Cc: Lee Sheets < l.sheets@novatech-eng.com>

Subject: South Merivale Business Park - boundary conditions request

Sharif:

I am looking to obtain boundary conditions for existing watermain for a potential development within the South Merivale Business Park to support an application to the City. Please find below water demand information for the proposed development (which includes addresses 99 Bill Leathem Drive, 2 Leikin Drive And 20 Leikin Drive). Also, attached is a key plan, showing the site location, and a geomap image showing the existing water infrastructure. Can you please provide boundary conditions for the existing watermain infrastructure at the round-about of Bill Leathem Drive and Longfield Drive, the end of Paragon Avenue, and the existing stub off of Leikin Drive, as highlighted on the attached plan as potential connection points, so we can review the servicing requirements for the site.

Water Demands proposed development:

AVG DAY = 11.14 L/s MAX DAY = 18.6 L/s PEAK HOUR = 33.42 L/s MAX DAY + FIRE =285.6 L/s

Please let us know if you require any further information.

Thanks,

Cara Ruddle, P.Eng., Senior Project Manager | Land Development Engineering

NOVATECH Engineers, Planners & Landscape Architects

240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 Ext: 220 | Cell: 613.261.7719 | Fax: 613.254.5867

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|--------|--|-----------|
| * | EPANET | * |
| * | Hydraulic and Water Quality | * |
| * | Analysis for Pipe Networks | * |
| * | Version 2.0 | * |
| ****** | ************************************** | ********* |

Input File: AD.net (Average Day-Existing)

120187 - South Merivale Business Park, 99 Bill Leathem Drive, 2 Leikin Drive, and 20 Lekin Drive

Link - Node Table:

| Link ID | Start Node | End Node | Length m | Diameter mm | |
|------------|---------------|-------------|-------------|----------------|--|
| 1 | RESERVOIR1 | 1 | 50 | 297 | |
| 2 | 1 | 2 | 148.5 | 297 | |
| 5 | 2 | 4 | 526 | 297 | |
| 6 | RESERVOIR3 | 4 | 10 | 297 | |
| 4 | 3 | RESERVOIR2 | 10 | 297 | |
| 3 | 2 | 3 | 111.2 | 297 | |

Node Results:

| Node ID | Demand LPS | Head m | Pressure m | Quality | |
|--|---|--|--|---------|-------------------------------------|
| 1 3 2 4 RESERVOIR1 RESERVOIR2 RESERVOIR3 | 3.71 3.71 0.00 3.71 -2.77 -4.33 -4.03 | 132.70 132.70 132.70 132.70 132.70 132.70 132.70 | 42.20 42.50 41.70 41.70 0.00 0.00 0.00 | 0.00 | Reservoir Reservoir Reservoir |

| Link ID | Flow LPS | VelocityUnit m/s | Headloss m/km | Status |
|------------|-------------|---------------------|------------------|--------|
| 1 | 2.77 | 0.04 | 0.01 | Open |
| 2 | -0.94 | 0.01 | 0.00 | 0pen |
| 5 | -0.32 | 0.00 | 0.00 | Open |
| 6 | 4.03 | 0.06 | 0.02 | Open |
| 4 | -4.33 | 0.06 | 0.02 | Open |
| 3 | -0.62 | 0.01 | 0.00 | Open |

Input File: PH.net (Peak Hour-Existing)

120187 - 120187 - South Merivale Business Park, 99 Bill Leathem Drive, 2 Leikin Drive, and 20 Lekin Drive

Link - Node Table:

| Link ID | Start Node | End Node | Length m | Diameter mm | |
|------------|---------------|-------------|-------------|----------------|--|
| 1 | RESERVOIR1 | 1 | 50 | 297 | |
| 2 | 1 | 2 | 148.5 | 297 | |
| 5 | 2 | 4 | 526 | 297 | |
| 6 | RESERVOIR3 | 4 | 10 | 297 | |
| 4 | 3 | RESERVOIR2 | 10 | 297 | |
| 3 | 2 | 3 | 111.2 | 297 | |

Node Results:

| Node ID | Demand LPS | Head m | Pressure m | Quality | |
|--|--|--|--|---------|-------------------------------------|
| 1 3 2 4 RESERVOIR1 RESERVOIR2 RESERVOIR3 | 11.14 11.14 0.00 11.14 -8.31 -13.00 | 125.00 125.00 125.00 125.00 125.00 125.00 125.00 | 34.50 34.80 34.00 34.00 0.00 0.00 | 0.00 | Reservoir Reservoir Reservoir |

| Link ID | Flow LPS | VelocityUni m/s | t Headloss m/km | Status | |
|------------|-------------|--------------------|--------------------|--------|--|
| 1 | 8.31 | 0.12 | 0.08 | Open | |
| 2 | -2.83 | 0.04 | 0.01 | Open | |
| 5 | -0.97 | 0.01 | 0.00 | 0pen | |
| 6 | 12.11 | 0.17 | 0.16 | 0pen | |
| 4 | -13.00 | 0.19 | 0.18 | 0pen | |
| 3 | -1.86 | 0.03 | 0.00 | 0pen | |

| ********** | ************ | * |
|-------------|-------------------|---|
| * E | PANET | * |
| * Hydraulic | and Water Quality | * |
| * Analysis | for Pipe Networks | * |
| * Ver | sion 2.0 | * |
| ********** | ************ | * |

Input File: MD-FF.net (Max Day + Fire Flow, Node 1-Existing)

120187 - 120187 - South Merivale Business Park, 99 Bill Leathem Drive, 2 Leikin Drive, and 20 Lekin Drive

Link - Node Table:

| Link ID | Start Node | End Node | Length m | Diameter mm | |
|------------|---------------|-------------|-------------|----------------|--|
| 1 | RESERVOIR1 | 1 | 50 | 297 | |
| 2 | 1 | 2 | 148.5 | 297 | |
| 5 | 2 | 4 | 526 | 297 | |
| 6 | RESERVOIR3 | 4 | 10 | 297 | |
| 4 | 3 | RESERVOIR2 | 10 | 297 | |
| 3 | 2 | 3 | 111.2 | 297 | |

Node Results:

| Node | Demand | Head | Pressure | Quality |
|--|---|--|--|--|
| ID | LPS | m | m | |
| 1 3 2 4 RESERVOIR1 RESERVOIR2 RESERVOIR3 | 273.20 6.20 0.00 6.20 -64.47 -21.65 -199.48 | 105.33 109.90 109.87 123.82 105.50 109.90 124.10 | 14.83 19.70 18.87 32.82 0.00 0.00 | 0.00 0.00 0.00 0.00 0.00 Reservoir 0.00 Reservoir |

| Link ID | Flow LPS | VelocityUnit m/s | Headloss m/km | Status |
|------------|-------------|---------------------|------------------|--------|
| 1 | 64.47 | 0.93 | 3.47 | Open |
| 2 | -208.73 | 3.01 | 30.58 | 0pen |
| 5 | -193.28 | 2.79 | 26.52 | Open |
| 6 | 199.48 | 2.88 | 28.12 | Open |
| 4 | -21.65 | 0.31 | 0.46 | Open |
| 3 | -15.45 | 0.22 | 0.25 | Open |

Input File: MD-FF.net (Max Day + Fire Flow, Node 3-Existing)

120187 - SMBP

Link - Node Table:

| Link ID | Start Node | End Node | Length m | Diameter mm |
|------------|---------------|-------------|-------------|----------------|
| 1 | RESERVOIR1 | 1 | 50 | 297 |
| 2 | 1 | 2 | 148.5 | 297 |
| 5 | 2 | 4 | 526 | 297 |
| 6 | RESERVOIR3 | 4 | 10 | 297 |
| 4 | 3 | RESERVOIR2 | 10 | 297 |
| 3 | 2 | 3 | 111.2 | 297 |

Node Results:

| Node ID | Demand LPS | Head m | Pressure m | Quality | |
|--|--|--|--|---------|-------------------------------------|
| 1 3 2 4 RESERVOIR1 RESERVOIR2 RESERVOIR3 | 6.20 273.20 0.00 6.20 163.21 -247.04 -201.77 | 106.47 109.48 109.55 123.81 105.50 109.90 124.10 | 15.97 19.28 18.55 32.81 0.00 0.00 0.00 | 0.00 | Reservoir Reservoir Reservoir |

| Link ID | Flow LPS | VelocityUnit m/s | Headloss m/km | Status |
|------------|-------------|---------------------|------------------|--------|
| 1 | -163.21 | 2.36 | 19.39 | Open |
| 2 | -169.41 | 2.45 | 20.78 | 0pen |
| 5 | -195.57 | 2.82 | 27.11 | 0pen |
| 6 | 201.77 | 2.91 | 28.72 | 0pen |
| 4 | -247.04 | 3.57 | 41.78 | 0pen |
| 3 | 26.16 | 0.38 | 0.65 | 0pen |

Input File: MD-FF.net (Max Day + Fire Flow, Node 4-Existing)

120187 - SMBP

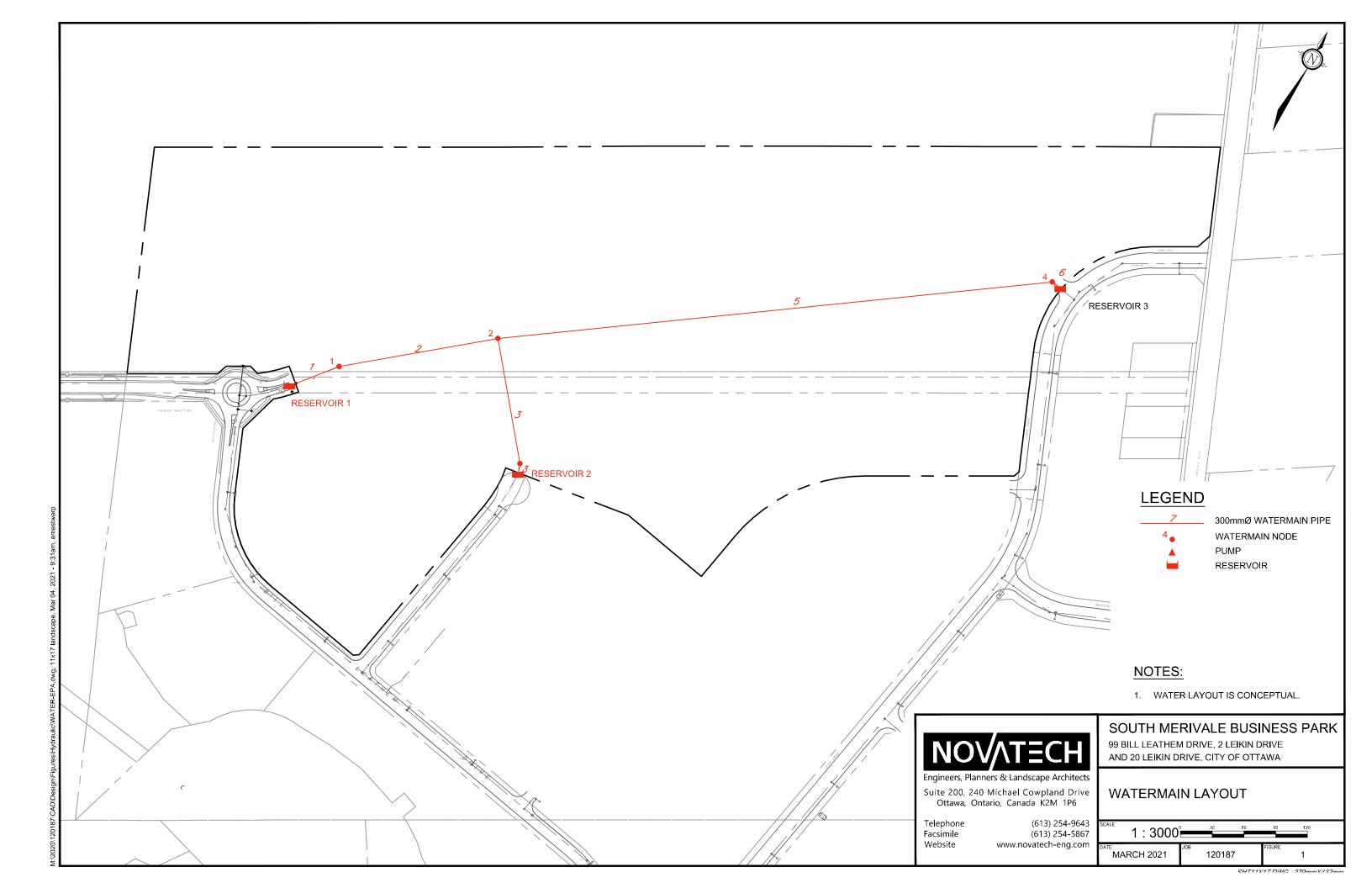
Link - Node Table:

| Link ID | Start Node | End Node | Length m | Diameter mm |
|------------|---------------|-------------|-------------|----------------|
| 1 | RESERVOIR1 | 1 | 50 | 297 |
| 2 | 1 | 2 | 148.5 | 297 |
| 5 | 2 | 4 | 526 | 297 |
| 6 | RESERVOIR3 | 4 | 10 | 297 |
| 4 | 3 | RESERVOIR2 | 10 | 297 |
| 3 | 2 | 3 | 111.2 | 297 |

Node Results:

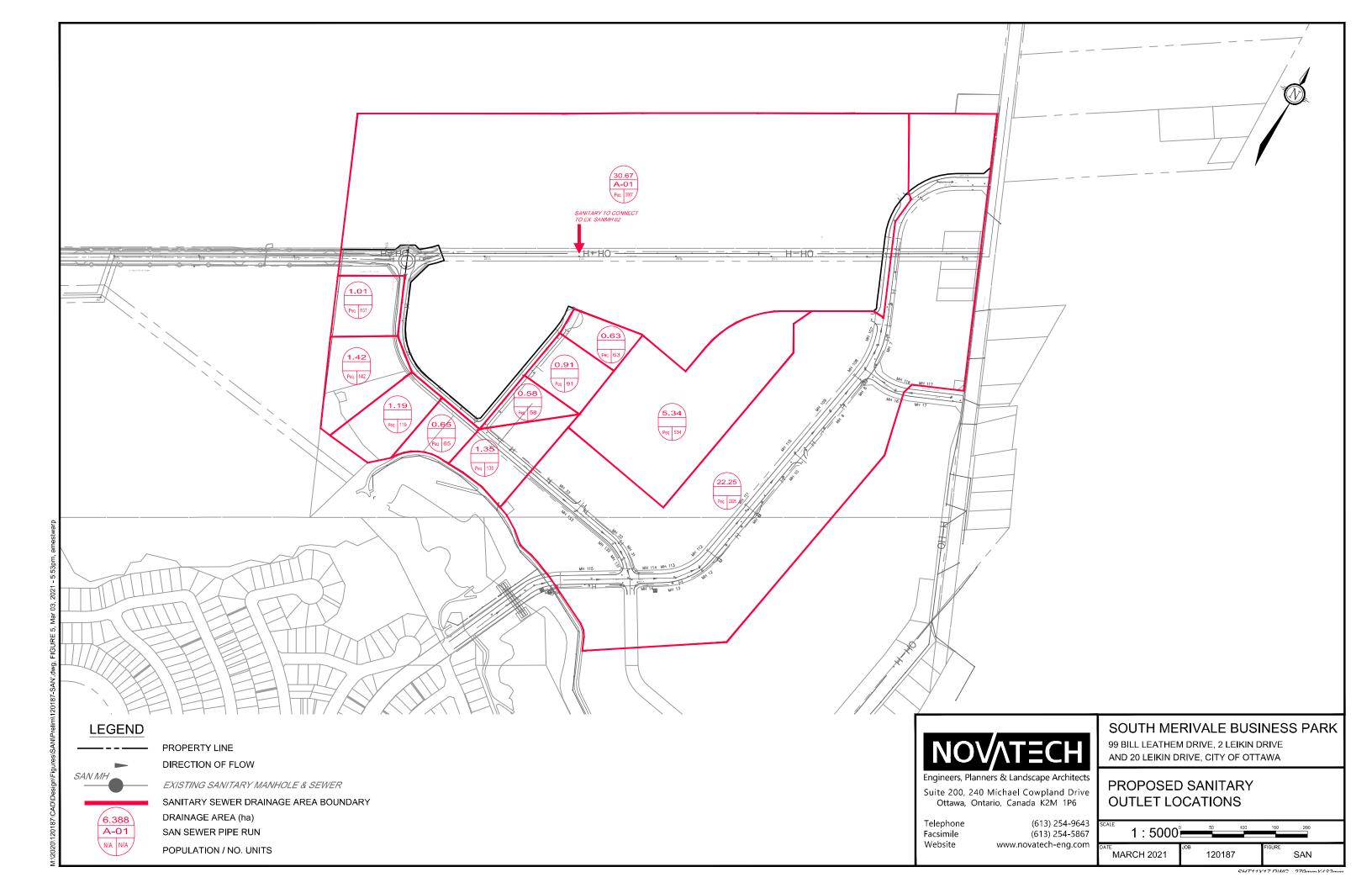
| Node ID | Demand LPS | Head m | Pressure m | Quality | |
|--|--|--|--|---------|-------------------------------------|
| 1 3 2 4 RESERVOIR1 RESERVOIR2 RESERVOIR3 | 6.20 6.20 0.00 273.20 170.95 1.77 | 106.56 109.90 109.91 122.79 105.50 109.90 | 16.06 19.70 18.91 31.79 0.00 0.00 | 0.00 | Reservoir Reservoir Reservoir |

| Link | Flow | VelocityUni | t Headloss | Status |
|------|---------|-------------|------------|--------|
| ID | LPS | m/s | m/km | |
| 1 2 | -170.95 | 2.47 | 21.13 | Open |
| | -177.15 | 2.56 | 22.57 | Open |
| 5 | -185.12 | 2.67 | 24.49 | Open |
| | 458.32 | 6.62 | 131.24 | Open |
| 4 | 1.77 | 0.03 | 0.00 | Open |
| 3 | 7.97 | 0.12 | 0.07 | Open |



APPENDIX C

Sanitary Sewer Information



Project No. 120187 Project Name: 99 Bill Leathem, 2 Leikin, 20 Leikin Drive Project Location: City of Ottawa



Date: October 2020

Sanitary Sewer Design Sheet

| | LOCATION | | | COM | IMERCIAL / II | NDUTRIAL F | LOW | | | PIPE | | | | | | |
|---------|----------|-----------|-----------|--------------------|--------------------------|----------------|--------------------|-----------------------------|-------------------------|-----------------------------|-------------------|-------------------|---------------|-------------------|-------------------|---------|
| AREA ID | FROM | то | AREA (ha) | ACCUM AREA (ha) | Equivalent Population | PEAK FACTOR | PEAK FLOW (I/s) | ACCUM PEAK FLOW (I/s) | INFIL. FLOW (I/s) | TOTAL PEAK FLOW (I/s) | PIPE SIZE (mm) | PIPE SLOPE (%) | LENGTH (m) | CAPACITY (I/s) | VELOCITY (m/s) | Q/Qfull |
| A-01 | SITE | EX. MH 62 | 30.670 | 30.670 | 3067 | 2.8 | 44.73 | 44.73 | 3.37 | 48.10 | 300 | 0.50 | 20.0 | 68.3 | 1.0 | 70.4% |

| Design Parameters: | | | | | | | | | |
|--|-------|-----------|--|--|--|--|--|--|--|
| (From: City of Nepean South Merivale Business Park Phase II and III Service: | | | | | | | | | |
| Design Report By Novatech Engineering consultants Ltd., Dated June | | | | | | | | | |
| 23,1992) | | | | | | | | | |
| Industrial Flow | 44880 | L/ha/day | | | | | | | |
| Average Daily per capita flow | 450 | L/cap/day | | | | | | | |
| Population Equivalent | 100 | Per/ha | | | | | | | |
| Peaking Factor (Light Industrial Flow) | 2.8 | | | | | | | | |
| Extraneous Flow | 0.11 | L/ha/s | | | | | | | |

APPENDIX D

Stormwater Management Calculations

PROJECT #: 120187 PROJECT NAME: 99 BILL LEATHEM DRIVE, 2 LEIKIN DRIVE, AND 20 LEIKIN DRIVE

LOCATION: OTTAWA, ONTARIO



| Pre-Development Runoff Coefficient "C" - EX-01 | | | | | | | |
|--|------------------|-------------------|--|--|--|--|--|
| Area | C _{avg} | *C ₁₀₀ | | | | | |
| Total | 0.65 | 0.81 | | | | | |
| 4.807 | 0.03 | 0.61 | | | | | |

Runoff Coefficient Equation

 $C = (A_{hard} \times 0.9 + A_{soft} \times 0.2)/A_{Tot}$

* Runoff

Pre-Development Flows - EX-01

| Outlet Options | Area (ha) | C _{avg} | Tc (min) | Q2 _{Year} (L/s) | Q _{5 Year} (L/s) | Q _{100 Year} (L/s) |
|----------------|--------------|------------------|----------|-----------------------------|------------------------------|--------------------------------|
| Street D | 4.807 | 0.65 | 15 | 536.6 | 725.9 | 1551.6 |

Pre-Development Runoff Coefficient "C" - EX-02

| Area | Surface | C _{avg} | *C ₁₀₀ | |
|--------|---------|------------------|-------------------|--|
| Total | Hard | 0.65 | 0.81 | |
| 20.037 | Soft | 0.00 | 0.01 | |

Runoff Coefficient Equation

 $C = (A_{hard} \times 0.9 + A_{soft} \times 0.2)/A_{Tot}$

* Runoff

Pre-Development Flows -EX-02

| Outlet Options | Area (ha) | C _{avg} | Tc (min) | Q2 _{Year} (L/s) | Q _{5 Year} (L/s) | Q _{100 Year} (L/s) |
|----------------|--------------|------------------|----------|-----------------------------|------------------------------|--------------------------------|
| Street D | 20.037 | 0.65 | 15 | 2236.4 | 3025.4 | 6467.2 |

Pre-Development Runoff Coefficient "C" - EX-03

| Area | C _{avg} | *C ₁₀₀ | |
|-------|------------------|-------------------|--|
| Total | 0.65 | 0.81 | |
| 1.123 | 0.00 | | |

Runoff Coefficient Equation

 $C = (A_{hard} \times 0.9 + A_{soft} \times 0.2)/A_{Tot}$

* Runoff

Pre-Development Flows - EX-03

| Outlet Options | Area (ha) | C _{avg} | Tc (min) | Q2 _{Year} (L/s) | Q _{5 Year} (L/s) | Q _{100 Year} (L/s) |
|----------------|--------------|------------------|----------|-----------------------------|------------------------------|--------------------------------|
| Street D | 1.123 | 0.65 | 15 | 125.3 | 169.5 | 362.3 |

 Equations: Flow Equation Q = 2.78 x C x I x A

Where:

C is the runoff coefficient

I is the rainfall intensity, City of Ottawa IDF

A is the total drainage area

100 year Intensity = 1735.688 / (Time in min + 6.014) $^{0.820}$ 5 year Intensity = 998.071 / (Time in min + 6.053) $^{0.814}$

2 year Intensity = $732.951 / (Time in min + 6.199)^{0.810}$

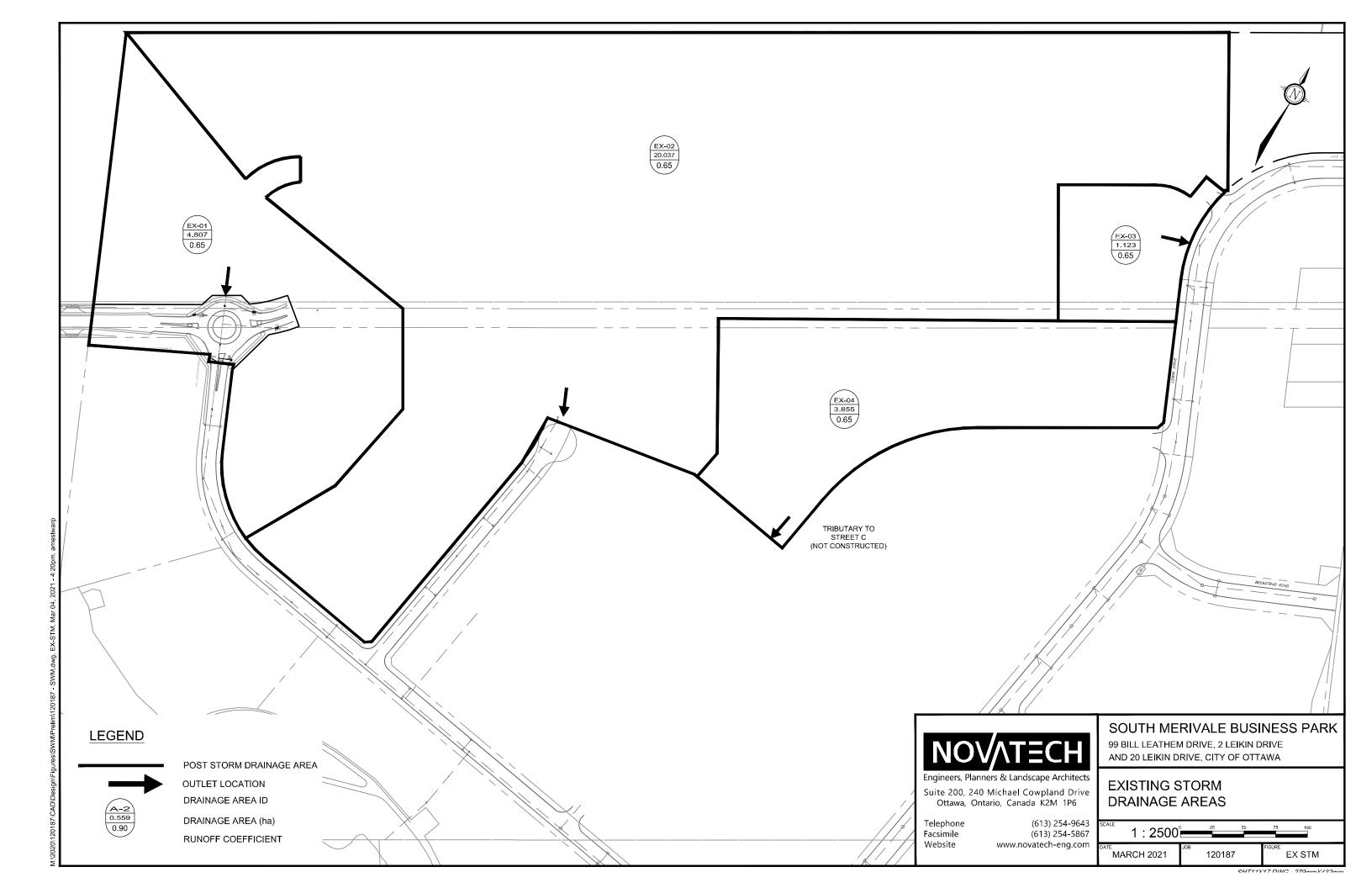




TABLE 1A: Post-Development Runoff Coefficient "C" - A-01

| 5 Year Ever | t 100 Ye | ar Event |
|-------------|----------|----------|
|-------------|----------|----------|

| Area | C_{avg} | *C _{avg} |
|-------|-----------|-------------------|
| Total | | |
| 4.807 | 0.90 | 1.00 |

TABLE 1B: 2 YEAR EVENT QUANTITY STORAGE REQUIREMENT - A-01

4.807 =Area (ha)

| | | | | | Net Flow | |
|--------|-------|-----------|---------|--------------|--------------|-------------------------|
| Return | Time | Intensity | Flow | Allowable | to be | Storage |
| Period | (min) | (mm/hr) | Q (L/s) | Runoff (L/s) | Stored (L/s) | Req'd (m ³) |
| 2 YEAR | -5 | 632.75 | 7610.70 | 725.9 | 6884.80 | -2065.44 |
| 2 TEAR | 0 | 167.22 | 2011.35 | 725.9 | 1285.45 | 0.00 |
| | 5 | 103.57 | 1245.76 | 725.9 | 519.86 | 155.96 |
| | 10 | 76.81 | 923.81 | 725.9 | 197.91 | 118.75 |
| | 15 | 61.77 | 742.94 | 725.9 | 17.04 | 15.33 |

TABLE 1C: 5 YEAR EVENT QUANTITY STORAGE REQUIREMENT - A-01

4.807 0.90 =Area (ha) = C

| | | | | | Net Flow | |
|--------|-------|-----------|---------|--------------|--------------|-------------------------|
| Return | Time | Intensity | Flow | Allowable | to be | Storage |
| Period | (min) | (mm/hr) | Q (L/s) | Runoff (L/s) | Stored (L/s) | Req'd (m ³) |
| | 0 | 230.48 | 2772.24 | 725.9 | 2046.34 | 0.00 |
| | 5 | 141.18 | 1698.09 | 725.9 | 972.19 | 291.66 |
| 5 YEAR | 10 | 104.19 | 1253.23 | 725.9 | 527.33 | 316.40 |
| | 15 | 83.56 | 1005.03 | 725.9 | 279.13 | 251.21 |
| | 20 | 70.25 | 844.98 | 725.9 | 119.08 | 142.90 |

TABLE 1D: 100 YEAR EVENT QUANTITY STORAGE REQUIREMENT - A-01

4.807 =Area (ha)

1.00

| | | | | | Net Flow | |
|----------|-------|-----------|---------|--------------|--------------|-------------------------|
| Return | Time | Intensity | Flow | Allowable | to be | Storage |
| Period | (min) | (mm/hr) | Q (L/s) | Runoff (L/s) | Stored (L/s) | Req'd (m ³) |
| | 5 | 242.70 | 3243.60 | 725.9 | 2517.70 | 755.31 |
| | 10 | 178.56 | 2386.34 | 725.9 | 1660.44 | 996.27 |
| 100 YEAR | 15 | 142.89 | 1909.70 | 725.9 | 1183.80 | 1065.42 |
| | 20 | 119.95 | 1603.07 | 725.9 | 877.17 | 1052.60 |
| | 25 | 103.85 | 1387.86 | 725.9 | 661.96 | 992.94 |

Equations: Runoff Coefficient Equation Flow Equation $C_5 = (A_{hard} \times 0.9 + A_{soft} \times 0.2)/A_{Tot}$ Q = 2.78 x C x I x A $C_{100} = (A_{hard} \times 1.0 + A_{soft} \times 0.25)/A_{Tot}$

Where:

C is the runoff coefficient I is the rainfall intensity, City of Ottawa IDF

A is the total drainage area

100 year Intensity = $1735.688 / (Time in min + 6.014)^{0.820}$

5 year Intensity = 998.071 / (Time in min + 6.053)^{0.814} 2 year Intensity = 732.951 / (Time in min + 6.199)^{0.810}



TABLE 2A: Post-Development Runoff Coefficient "C" - A-02

| | 3 Teal Event 100 Teal Even | | | | |
|--------|----------------------------|-------------------|--|--|--|
| Area | C _{avg} | *C _{avg} | | | |
| Total | | | | | |
| 23.896 | 0.90 | 1.00 | | | |

TABLE 2B: 2 YEAR EVENT QUANTITY STORAGE REQUIREMENT - A-01

23.896 =Area (ha)

| | | | | | Net Flow | |
|--------|-------|-----------|----------|--------------|--------------|-------------------------|
| Return | Time | Intensity | Flow | Allowable | to be | Storage |
| Period | (min) | (mm/hr) | Q (L/s) | Runoff (L/s) | Stored (L/s) | Req'd (m ³) |
| 2 YEAR | -5 | 632.75 | 37830.62 | 3025.4 | 34805.22 | -10441.57 |
| 2 TEAR | 0 | 167.22 | 9997.85 | 3025.4 | 6972.45 | 0.00 |
| | 5 | 103.57 | 6192.30 | 3025.4 | 3166.90 | 950.07 |
| | 10 | 76.81 | 4592.00 | 3025.4 | 1566.60 | 939.96 |
| | 15 | 61.77 | 3692.93 | 3025.4 | 667.53 | 600.78 |

TABLE 2C: 5 YEAR EVENT QUANTITY STORAGE REQUIREMENT - A-02

23.896 0.90 =Area (ha) = C

| | | | | | Net Flow | |
|--------|-------|-----------|----------|--------------|--------------|-------------------------|
| Return | Time | Intensity | Flow | Allowable | to be | Storage |
| Period | (min) | (mm/hr) | Q (L/s) | Runoff (L/s) | Stored (L/s) | Req'd (m ³) |
| | 0 | 230.48 | 13780.00 | 3025.4 | 10754.60 | 0.00 |
| | 5 | 141.18 | 8440.74 | 3025.4 | 5415.34 | 1624.60 |
| 5 YEAR | 10 | 104.19 | 6229.46 | 3025.4 | 3204.06 | 1922.44 |
| | 15 | 83.56 | 4995.69 | 3025.4 | 1970.29 | 1773.27 |
| | 20 | 70.25 | 4200.15 | 3025.4 | 1174.75 | 1409.71 |

TABLE 2D: 100 YEAR EVENT QUANTITY STORAGE REQUIREMENT - A-02 23.896 =Area (ha)

=Area (ha)

1.00

| | | | | | Net Flow | |
|----------|-------|-----------|----------|--------------|--------------|-------------------------|
| Return | Time | Intensity | Flow | Allowable | to be | Storage |
| Period | (min) | (mm/hr) | Q (L/s) | Runoff (L/s) | Stored (L/s) | Req'd (m ³) |
| | 10 | 178.56 | 11861.82 | 3025.4 | 8836.42 | 5301.85 |
| | 15 | 142.89 | 9492.57 | 3025.4 | 6467.17 | 5820.46 |
| 100 YEAR | 20 | 119.95 | 7968.40 | 3025.4 | 4943.00 | 5931.60 |
| | 25 | 103.85 | 6898.65 | 3025.4 | 3873.25 | 5809.87 |
| | 30 | 91.87 | 6102.88 | 3025.4 | 3077.48 | 5539.46 |

Equations: Runoff Coefficient Equation Flow Equation $C_5 = (A_{hard} \times 0.9 + A_{soft} \times 0.2)/A_{Tot}$ Q = 2.78 x C x I x A $C_{100} = (A_{hard} \times 1.0 + A_{soft} \times 0.25)/A_{Tot}$

Where:

C is the runoff coefficient

I is the rainfall intensity, City of Ottawa IDF

A is the total drainage area

100 year Intensity = $1735.688 / (Time in min + 6.014)^{0.820}$

5 year Intensity = 998.071 / (Time in min + 6.053)^{0.814} 2 year Intensity = 732.951 / (Time in min + 6.199)^{0.810}



TABLE 3A: Post-Development Runoff Coefficient "C" - A-03

5 Year Event 100 Year Event

| Area | C_{avg} | *C _{avg} |
|-------|-----------|-------------------|
| Total | | |
| 1.123 | 0.90 | 1.00 |

TABLE 3B: 2 YEAR EVENT QUANTITY STORAGE REQUIREMENT - A-03

1.123 0.90 =Area (ha)

| | | | | | Net Flow | |
|--------|-------|-----------|---------|--------------|--------------|-------------------------|
| Return | Time | Intensity | Flow | Allowable | to be | Storage |
| Period | (min) | (mm/hr) | Q (L/s) | Runoff (L/s) | Stored (L/s) | Req'd (m ³) |
| 2 YEAR | -5 | 632.75 | 1777.15 | 169.6 | 1607.59 | -482.28 |
| 2 TEAR | 0 | 167.22 | 469.66 | 169.6 | 300.10 | 0.00 |
| | 5 | 103.57 | 290.89 | 169.6 | 121.33 | 36.40 |
| | 10 | 76.81 | 215.72 | 169.6 | 46.16 | 27.69 |
| | 15 | 61.77 | 173.48 | 169.6 | 3.92 | 3.53 |

TABLE 3C: 5 YEAR EVENT QUANTITY STORAGE REQUIREMENT - A-03

1.123 0.90 =Area (ha) = C

| | | | | | Net Flow | |
|--------|-------|-----------|---------|--------------|--------------|-------------------------|
| Return | Time | Intensity | Flow | Allowable | to be | Storage |
| Period | (min) | (mm/hr) | Q (L/s) | Runoff (L/s) | Stored (L/s) | Req'd (m ³) |
| | 0 | 230.48 | 647.34 | 169.5 | 477.84 | 0.00 |
| | 5 | 141.18 | 396.52 | 169.5 | 227.02 | 68.10 |
| 5 YEAR | 10 | 104.19 | 292.64 | 169.5 | 123.14 | 73.88 |
| | 15 | 83.56 | 234.68 | 169.5 | 65.18 | 58.66 |
| | 20 | 70.25 | 197.31 | 169.5 | 27.81 | 33.37 |

TABLE 3D: 100 YEAR EVENT QUANTITY STORAGE REQUIREMENT - A-03

1.123 =Area (ha)

1.00

| | | | | | Net Flow | |
|----------|-------|-----------|---------|--------------|--------------|-------------------------|
| Return | Time | Intensity | Flow | Allowable | to be | Storage |
| Period | (min) | (mm/hr) | Q (L/s) | Runoff (L/s) | Stored (L/s) | Req'd (m ³) |
| | 5 | 242.70 | 757.40 | 169.5 | 587.90 | 176.37 |
| | 10 | 178.56 | 557.23 | 169.5 | 387.73 | 232.64 |
| 100 YEAR | 15 | 142.89 | 445.93 | 169.5 | 276.43 | 248.78 |
| | 20 | 119.95 | 374.33 | 169.5 | 204.83 | 245.79 |
| | 25 | 103.85 | 324.07 | 169.5 | 154.57 | 231.86 |

Equations: Runoff Coefficient Equation Flow Equation $C_5 = (A_{hard} \times 0.9 + A_{soft} \times 0.2)/A_{Tot}$ Q = 2.78 x C x I x A $C_{100} = (A_{hard} \times 1.0 + A_{soft} \times 0.25)/A_{Tot}$

Where:

C is the runoff coefficient

I is the rainfall intensity, City of Ottawa IDF

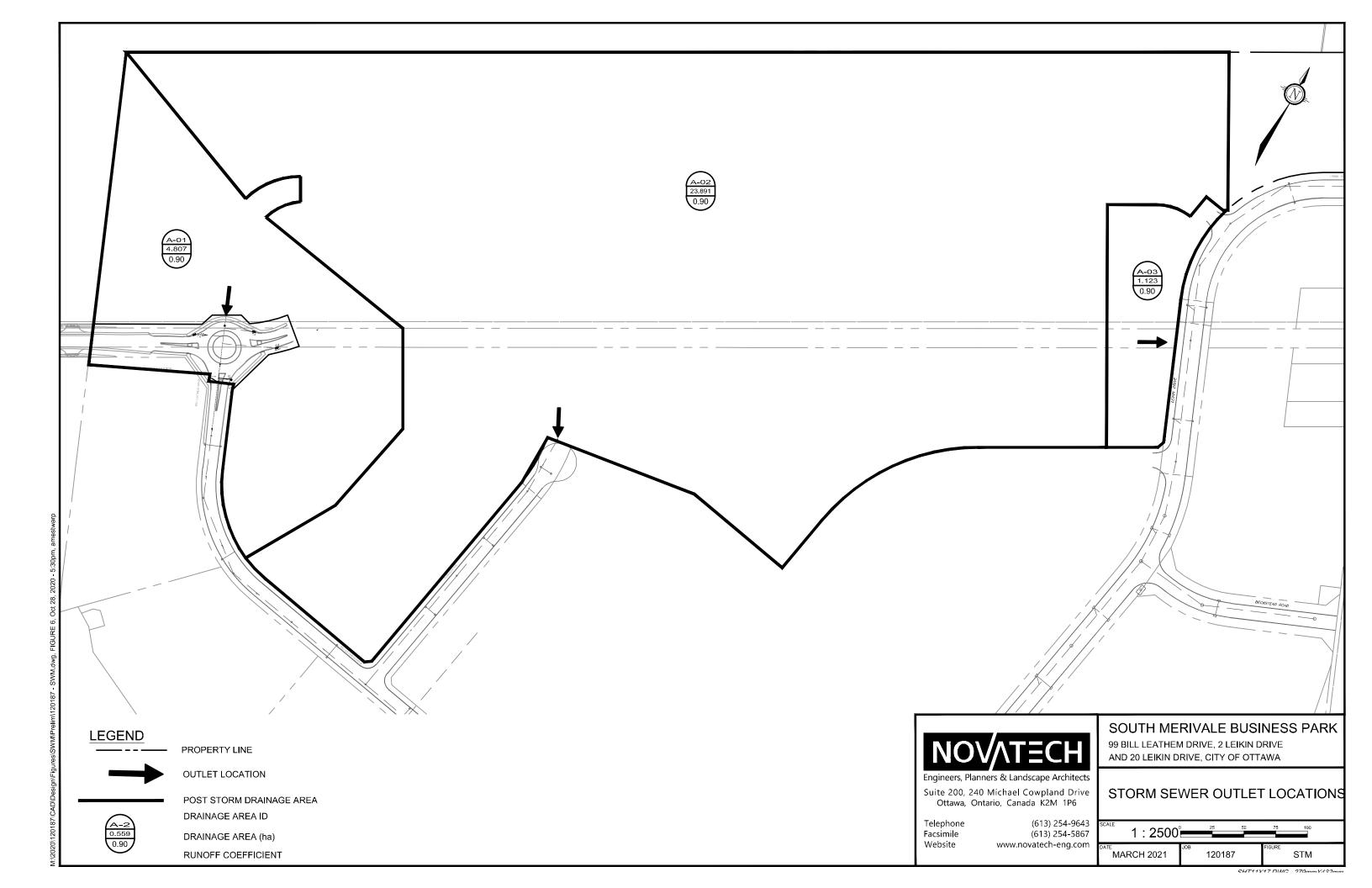
A is the total drainage area

100 year Intensity = $1735.688 / (Time in min + 6.014)^{0.820}$

5 year Intensity = 998.071 / (Time in min + 6.053)^{0.814} 2 year Intensity = 732.951 / (Time in min + 6.199)^{0.810}



| | Table 5: Post-Development Stormwater Mangement Summary | | | | | | | | | | | | | |
|---------|--|----------|------------------|-----------|-----------|-----------|----------|--|--|--|--|--|--|--|
| | | | | 2-yr | 5-yr | 100-yr | | | | | | | | |
| | | 1:5 Year | 1 | | | | Required | | | | | | | |
| Area ID | Area (ha) | Weighted | Oulet Location | Req'd Vol | Req'd Vol | Req'd Vol | storage | | | | | | | |
| | | Cw | | (cu.m) | (cu.m) | (cu.m) | per ha | | | | | | | |
| | | | | · | · | | (100-yr) | | | | | | | |
| A-01 | 4.807 | 0.90 | Bill Leathem Dr. | 155.96 | 316.4 | 1065.42 | 221.62 | | | | | | | |
| A-02 | 23.896 | 0.90 | Pargon Ave. | 950.07 | 1922.44 | 5931.60 | 248.23 | | | | | | | |
| A-03 | 1.123 | 0.90 | Leikin Dr. | 36.40 | 73.88 | 248.78 | 221.62 | | | | | | | |
| | Total | | 1 | 1142.4 | 2312.7 | 7245.8 | N/A | | | | | | | |



From: Shillington, Jeffrey < jeff.shillington@ottawa.ca>

Sent: Thursday, October 8, 2020 9:32 AM **To:** Lee Sheets < l.sheets@novatech-eng.com **Subject:** RE: South Merivale Business Park

Hi Lee,

I've confirmed with Eric Tousignant that the following SWM can be used for the South Merivale Business Park. His rational is below. I've also located the June 1992 and the link is below.

Regards,

Jeff Shillington, P.Eng.
Senior Project Manager, Development Review, South Branch
Planning, Infrastructure and Economic Development
City of Ottawa

tel: 580-2424 x 16960

email: jeff.shillington@ottawa.ca

From Eric T.:

The 1991 report was based on wrong assumptions, but to be fair, SWM was still in its infancy at the time and they did the best they could with the information at hand. I revised the analysis and came up with something more realistic. I therefore recommend that future development in this business park follow the conclusion below (I am pasting my original email below):

I looked at the 1991 Novatech report that you attached and I don't agree with the approach Novatech took to come up with the allowable release rate. I am explaining my thought process here, but you can simply jump to the conclusion if you want the recommended release rate.

First of all, the entire area is allowed a peak flow of 4.6 cms to the pond as per the pond's design report. It is also assumed that the vast majority of the flow will be contained in the areas and bled back into the minor system, therefore it can be assumed that no major system flow is spilling to the pond. Finally, is it assumed that the ultimate average runoff coefficient for the entire drainage area will be 0.75.

Novatech took the total allowable flow and divided it by the area to obtain an average release rate of 54.4 L/s/ha (assuming that all land is controlled equally and released constantly over the entire duration of the storm, which is <u>way too conservative</u> and unrealistic since is does not account for flow attenuation).

They then used the rational method equation and worked backwards from the peak flow to get the runoff coefficient that corresponds to the peak flow of 4.6 cms. This is where they made a mistake, They assume a 15 TC when this 84.4 ha drainage area will have a TC of somewhere between 70 and 75 minutes. Using a 70 minutes TC I get a 5 year intensity of approximately 29 mm/hr, therefore the Average runoff coefficient is more like 0.67 to come up with a flow of 4.6 cms and not 0.24 as noted in the report.

This means that C=0.67 of not far from the ultimate runoff coefficient of 0.75 for the entire area and means that the allowable release rate from the development sites does not have to be too restrictive

Novatech then tried to come up with an allowable release rate for each sub-area by subtracting the ROW release rate. The problem is that they apply an ICD release rate as a constant when even ICD flow is attenuated by the time it reaches the outlet due to the fact that the storm does not keep a peak intensity throughout its duration.

Therefore this is how I would account for the ROW flow:

Based on the existing roadway areas, there are approximately 12 CB per ha each but they are releasing approximately 15 L/s due to the use of ICDs (in fact two CB are connected together releasing a total of 30 L/s using a type B ICD). This means that the peak 5 year capture in the ROW is 180 L/s per ha. To generate this flow with a 5 year event and a TC of 15 minutes, we need a C=0.78. Therefore we can assume that the ROW is being controlled to a C=0.78. There are 8.8 ha or ROW within the 84.4 ha sewershed, therefore the remaining developable lands need to be controlled to a C=0.65 so that the overall 84.4 ha is controlled to an equivalent C=0.67

The allowable release rate for each site should therefore be based on the 5 year storm, using a C=0.65 and a computed TC of 15 minutes to remain consistent with the original storm sewer design that used a TC of 15 minutes.

Conclusion: Based on the above analysis, 4.6 cms is equivalent to a 5 year release rate for a 84.4 ha area having a C=0.67. If we remove the allowance for the ROW drainage (C=0.78), the allowable release rate for the remaining development lands should be based on a C=0.65.

I would therefore ask that they provide SWM to control the 100 year event to a release rate based on the 5 year event, with a C=0.65 and TC=15 minutes.

From: Lee Sheets <1.sheets@novatech-eng.com>

Sent: October 06, 2020 9:24 AM

To: Shillington, Jeffrey <jeff.shillington@ottawa.ca>

Subject: South Merivale Business Park

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I'm trying to understand the SWM criteria for the remaining lands in the SMBP. I understand that quality control is handled in the Belanger SWM facility. The quantity control requirements are the reason for my e-mail.

Please feel free to give me a call on my cel if you have any questions.

J. Lee Sheets, C.E.T., Director | Land Development & Public Sector Infrastructure

NOVATECH Engineers, Planners & Landscape Architects

240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 Ext: 209 | Cell: 613.262.3121 | Fax: 613.254.5867

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APPENDIX E

Novatech SMBP Phase II and III Services Design Report



CITY OF NEPEAN -SOUTH MERIVALE BUSINESS PARK PHASE II AND III SERVICES DESIGN REPORT

Prepared by:

NOVATECH ENGINEERING CONSULTANTS LTD.

June 23, 1992



July 10, 1992

CIVIL ENGINEERS AND PLANNERS

BY COURIER

City of Nepean
Engineering Department
101 Centrepointe Drive
3rd Floor
Nepean, Ontario
K2G 5K7

Attention: Ms. Sue Johns, P.Eng.

Dear Madam:

Re: South Merivale Business Park

Our File No. 92019

We are pleased to submit two copies of the Services Design Report for your review.

The report outlines sanitary, watermain and surface works servicing for the above noted project. In addition an overall earthwork calculation is provided for the full Business Park.

We ask that you provide comments to us as soon as is convenient. If you have any questions that are best addressed immediately, please do not hesitate to contact us.

Yours truly,

NOVATECH ENGINEERING CONSULTANTS LTD.

LJ/ml

c.c. Udo Boehme

Lee Jablonski, P.Eng.

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| Appendix A | Sanitary Sewer Design Sheets |
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| Appendix C | Industrial Sewage Flow - Peaking Factors |
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| Appendix E | Sanitary Drainage Area Plan |

1.0 INTRODUCTION

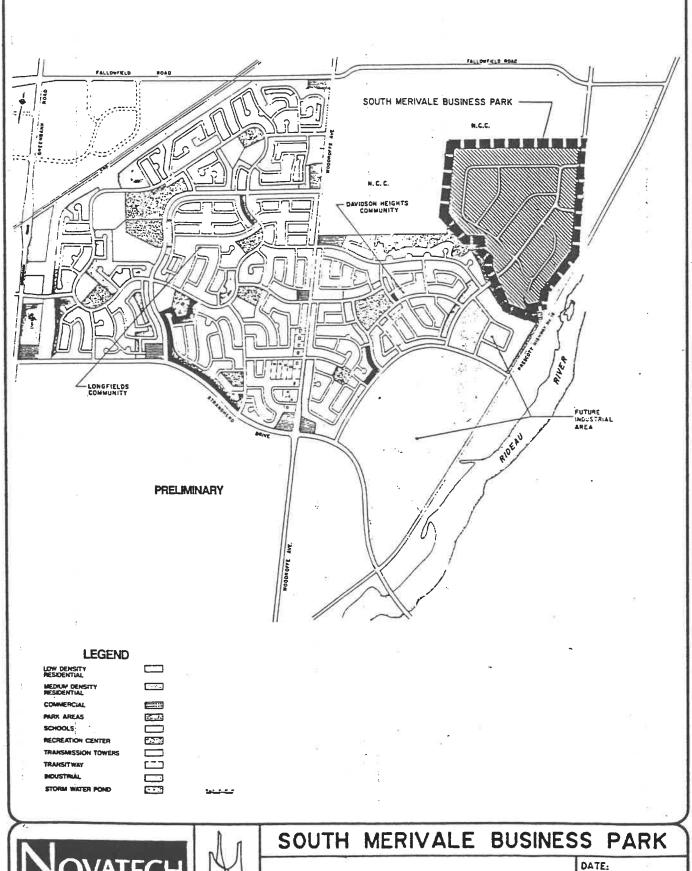
The South Merivale Business Park (SMBP) consists of approximately 85 hectares. It is bounded on the north and the northwest by the National Capital Commission (NCC) Greenbelt on the south and southwest by Barrhaven Creek and the Longfields/Davidson Heights Stormwater Management Facility and on the east by Merivale Road and Queen Anne Crescent. The site location is shown on Figure 1.

Land within the SMBP will be fully serviced within a dedicated right-of-way. Complete sanitary, storm sewer, water and utility servicing will be constructed under an urban section roadway in preparation for future lot development by individual owners.

Construction of the SMBP site servicing has been phased. Construction of Phase I expected to be complete by Summer 1992. Services Design Report [Novatech Engineering December 31, 1992] outlines the information and design assumptions used to prepared Phase I construction drawings, it also provided a summary for full subdivision servicing. This report updates criteria and design assumption used for the preparation of construction drawings for the proposed SMBP Phase II and III.

Figure 1A shows the updated phasing schedule for the SMBP and is detailed below for each street.

| Phase | <u>Street</u> | Construction of Services |
|-------|---------------|--------------------------|
| 1 | Α | 1992 |
| 2 | E,F | 1993 |
| 3 | B,D | 1993 |
| 4 | C | 1994 |



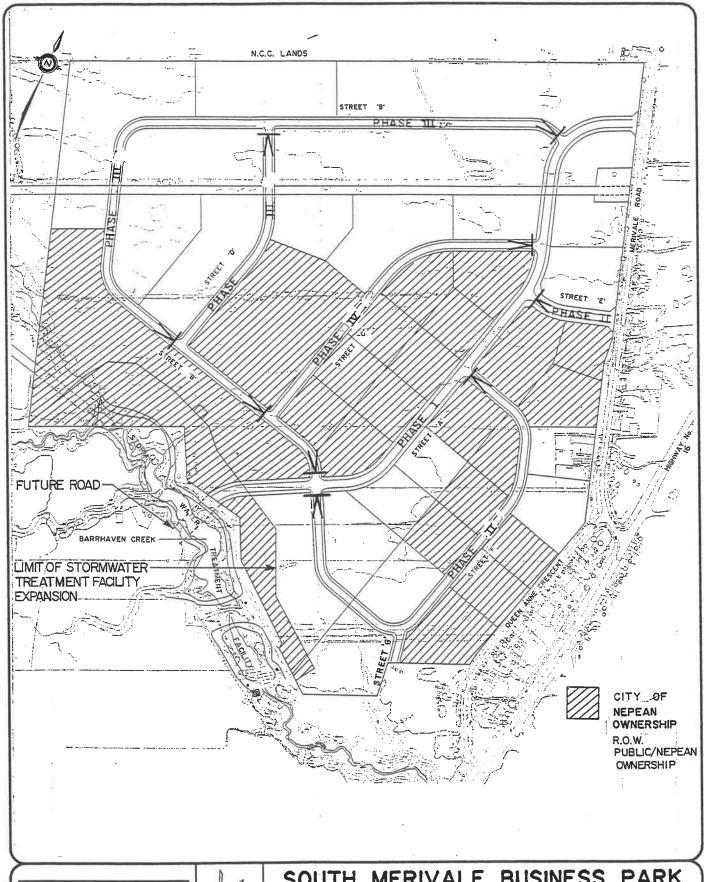


ENGINEERING CONSULTANTS LTD OTTAWA, ONTARIO



KEY PLAN

AUG. 91 FIG. No. 1





OTTAWA, ONTARIO

CITY OF NEPEAN

SOUTH MERIVALE BUSINESS PARK

PHASING AND OWNERSHIP PLAN DATE: JULY 1992

FIG. No.

IA

2.1 Sanitary Sewer Outlet

The sanitary sewer outlet for the SMBP is the Barrhaven Trunk Sanitary Sewer (BTSS). The BTSS originates east of Greenbank Road and flows in an easterly direction to the Merivale Road Pumping Station at Merivale Road. The 1050 mm BTSS is shown on Drawing No. 92019-S2 where it crosses the SMBP within an existing easement.

The Merivale Road Pumping Station will be eliminated when the West Rideau Collector is extended south along Merivale to intercept the BTSS. The Regional Municipality of Ottawa-Carleton (RMOC) Environmental Services Department has indicated that this is scheduled to occur in 1994 or 1995. The capacity of the Pumping Station is 152 L/s. Of this, 86 L/s has been reserved for anticipated flows from the Barrhaven community leaving 66 L/s of theoretically available capacity.

Table 1 is based on growth projections provided by the City of Nepean for Davidson Heights, Longfield and SMBP and shows that if there is no increase in projected flow from Barrhaven, the 152 L/s capacity of the Pumping Station will not be reached until 1992/1993. If Barrhaven flows increase or if development proceeds at a higher rate, then modifications will be required to increase the Pumping Station capacity. This expansion is currently being studied.

A 750 mm diameter trunk sanitary sewer is proposed along Street A. This trunk sewer will provide sanitary outlet for a substantial portion of the Davidson Heights Community. Due to the constraining elevation at the proposed Barrhaven Creek crossing, the connection to the existing 1050 mm sanitary is invert to invert. Based on the timing of the West Rideau Collector and coupled with the growth projections for the Davidson Heights and Longfields Communities, excessive surcharging of the 750 diameter sanitary is not expected.

TABLE 1
PROJECTED GROWTH AND SANITARY FLOWS

| | | RESIDENTI | INDUSTRIAL | PEAK FLOW | |
|------|-------|-----------|------------|--------------|-----|
| YEAR | UNITS | AREA (ha) | POPULATION | AREA (ha) | L/S |
| 1991 | 500 | 38 | 1524 | - | 33 |
| 1992 | 1300 | 100 | 3965 | 8 | 99 |
| 1993 | 2500 | 192 | 7625 | 16 | 176 |
| 1994 | 3800 | 292 | 11590 | 24 | 250 |
| 1995 | 5000 | 384 | 15250 | 32 | 320 |

2.2 Internal Sanitary Sewer System

A sanitary sewer system layout and design has been prepared for the SMBP during the Phase I detailed design. The sanitary drainage areas are shown on the Sanitary Drainage Area Plan (Drawing No. 92019-SAN). Sewer routing and manhole locations for Phases II and III are shown on the General Plan of Services (Drawing No. 92019-S1).

Sanitary sewers will be constructed on Street B, D and F and connections made from these sewers to those previously constructed along Street A. During Phase I a 240 mm length of 375 mm sanitary pipe was constructed under Street B. Provision was made at that time for connection of a 250 mm sanitary upstream of MH 34. Connection will be made at the point during this construction phase. Sanitary pipe from approximately station 4 + 240 F, 4 + 750 on Street B and station 7 + 000 to 7 + 250 on Street D will route flows to this point.

Sanitary flows generated from properties adjacent to Street F will be conveyed to previously constructed 250 mm diameter connection stubs at Street A.

The remaining sanitary flows generated adjacent to Streets B and D will be conveyed to an existing manhole 62. Two drop pipes will be constructed to permit north and southward access to the existing 1050 mm BTSS.

Water stops are proposed for inclusion in the trenches to prevent groundwater movement through the bedding material. The groundwater table is above the top of the sanitary pipe in most locations. Clay barriers are required to maintain the existing groundwater table height. Lowering of the groundwater table adjacent the trench could result in settlement of nearby structures.

2.3 Sanitary Sewer Design Sheets

The sanitary sewer design sheets for Phase II and III of the business park are included in Appendix 'A'. The design assumptions are as follows:

External sanitary flow:

```
Peak design flow = Q = 249.45 L/s (from Delcan correspondence, dated Oct. 21/91 - Appendix B)
```

Population equivalent:

```
P<sub>eq</sub> = 100 persons/ha
Industrial flow = 44,880 L/ha/day
(from City of Nepean Standard Subdivision Agreement)
```

Average daily per capita flow = q = 450 L/cap/day

$$P_{eq} = 44,880 \text{ L/ha/day x}$$
 $\frac{1}{450 \text{ L/cap/day}}$ = 100 persons/ha

Peaking factor:

Sanitary sewer design sheets for Phase I are included to confirm that flows calculated for Phases II and III can be conveyed by sewers detailed during the Phase I design.

2.4 Sanitary Service Connections

Private sanitary service connections will be made at the development stage of each site when capacity and location requirements are known.

3.1 Background

The Regional Municipality of Ottawa-Carleton, in consultation with Nepean and Gloucester, has been developing a trunk watermain scheme to serve the South Urban Community. This includes Longfields, Davidson Heights and the SMBP on the Nepean Side. The layout currently being contemplated consists of an extension of the 1050 mm watermain at Fallowfield and Woodroffe south along Woodroffe to the realigned Strandherd Drive watermain. Feeder mains will connect to this trunk off Woodroffe to service the Davidson Heights and Longfields Communities, as well as future areas to the south (Figure 2). Eventually, this trunk will extend eastward to cross the Rideau River in one or possibly two locations and continue through the Gloucester portion of the South Urban Community.

3.2 Watermain Supply Source

The SMBP will be supplied by twin 400 mm mains extending into the business park from the northeast sector of the Davidson Heights development. These mains will be the extension of the distribution system originating from the proposed 1050 mm trunk on Woodroffe and routed along the Davidson Heights street alignments.

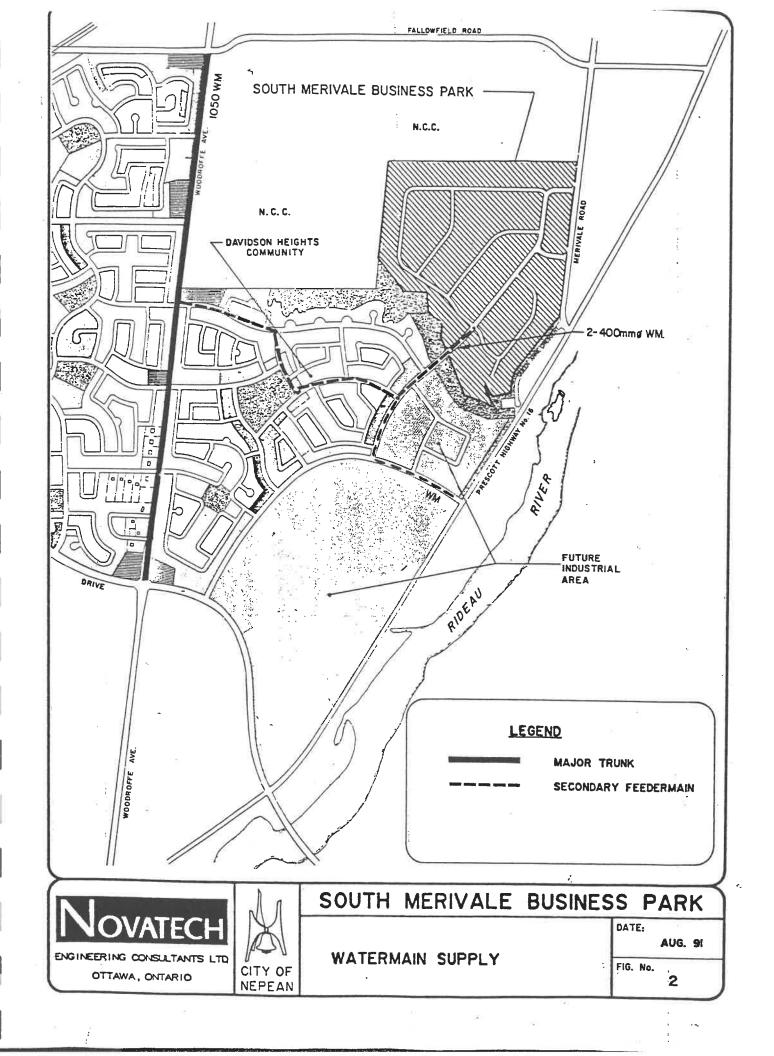
Extension of the 1050 Woodroffe Avenue watermain is complete.

3.3 Internal Watermain System

The internal watermain design is shown on the General Plan of Services (Drawing Nos. 92019-S1, S2 and S3). The pipe sizes have been confirmed by RMOC Environmental Services and are as follows:

Trunk Watermain 400 mm diameter Secondary Watermain 300 mm diameter

Delcan has designed the twin 400 mm diameter watermains across the Longfields/Davidson Heights Stormwater Management Facility expansion. The twin 400 mm diameter watermains on Street 'A' of the business park has been connected to these watermains at the property limit. A 400 mm diameter link has been installed between the two watermains at the intersection with Street A and B to provide a looped system.



3.4 Thrust Block Design

Thrust block design calculations for the 400 mm diameter watermain are summarized in the following table. The design is based on a test pressure of 1035 KPa (150 psi). Because of the width of excavation that will be required to install the sanitary sewer, imported material will be used to support the watermain. The bearing capacity of the soil is assumed to be 95.7 KPa for sand and 143.6 KPa for sand and gravel. Fondex Ltd. has confirmed that this bearing capacity can be achieved by compacting the imported material to 100%.

| Fitting | Thrust | Thrust Block (m ²) | | | | | | | |
|----------------------------|-----------------|--------------------------------|-----------------|--|--|--|--|--|--|
| (400 mm dia. watermain) | (N per 150 psi) | Sand | Sand and Gravel | | | | | | |
| Valves, Tees, Dead Ends | 134,100 | 1.40 | 0.93 | | | | | | |
| 90° Bends | 187,800 | 1.96 | 1.31 | | | | | | |
| 45° Bends | 102,750 | 1.07 | 0.71 | | | | | | |
| 22½° Bends | 53,100 | 0.55 | 0.37 | | | | | | |
| 11¼° Bends | 26,850 | 0.28 | 0.19 | | | | | | |

The 300 mm watermain thrust blocks will be constructed as per OPSD detail 1103.01.

3.5 Phase II and III Construction

Several 300 mm diameter watermain loops will be constructed in SMBP that branch from the main 400 mm on Street A. A 300 mm diameter and loop will be completed on Streets B and F and a sub-loop will be constructed on Street D providing connections at the north and south intersection with Street B. A stub complete with a cap and thrust block for future connection will be constructed on Street E.

4.0 STORM SEWER DESIGN

A comprehensive Stormwater Management Report, dated June, 1992 has been prepared by Novatech Engineering Consultants Ltd. for the SMBP Phase II and III. The report contains the criteria used to design the storm sewer system. The report is prepared under separate cover.

5.0 MERIVALE ROAD/STREET 'E' INTERSECTION

5.1 Final Design

Final intersection design is currently underway. Discussions have taken place with the Regional Transportation Department to establish geometrics and criteria. The design shall accommodate future widening of Merivale Road to provide a 4 lane facility.

Initially, the minimum requirements include a northbound left turn lane and southbound right turn taper which will be provided during first phase of development. Subsequent improvements to ultimate design will be undertaken as warranted by demand/capacity. The ultimate intersection design for Street A is complete and given approval at RMOC staff level. Final intersection design drawings for Street E and Merivale Road are currently being prepared and will be forwarded separately for approval.

6.0 UTILITIES

A composite utility plan will be prepared when the requisite information and design criteria has been assembled. The plan will be submitted separately for approval.

7.0 ROADS AND GRADING

7.1 Street Layout

Street layout for Phases II and III construction along Streets B, D, E and F is as described in previous preliminary design reports and as outlined on Figure 1A.

7.2 Cross Section

The local streets developed during Phase II and III will have a 20 m wide right-of-way and will have a roadway width of 12.0 m except for Street E which has a 26 m right-of-way and an 11.0 m roadway width. All streets are proposed to be constructed to a typical urban cross section complete with barrier curbs and boulevards that slope upwards to the property line. Figure 7-1 details the typical roadway cross section for these phases.

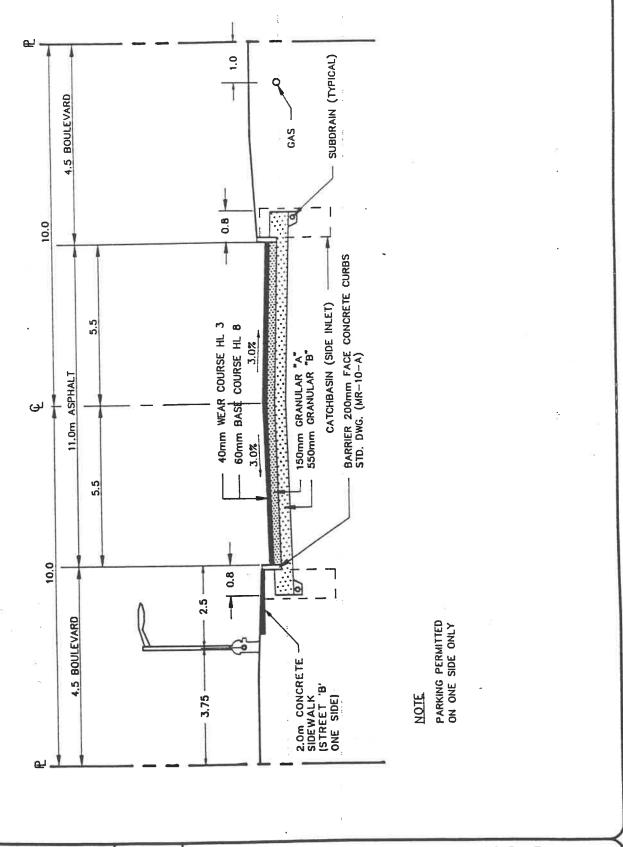
7.3 Grading

The topography of the SMBP site is relatively flat and gradually slopes to Barrhaven Creek. The lack of physical relief is disadvantageous when consideration of the grading is concerned. A grading design seeks to establish a compromise between the following two objectives.

- 1) balancing the cut/fill i.e. minimizing costs required to haul material onto or off the site,
- 2) provide a major overland flow route for the most infrequent storm events.

Because the area is relatively flat, it will have to be shaped to allow major overland flow to drain along the streets and the back lot areas to the Barrhaven Treatment facility. Initially the grading plan was constructed based upon two assumptions:

- i) 0.2 to 0.3 m of topsoil would be stripped from the entire site, and
- ii) fill originating from the construction of the Barrhaven Creek Facility would be available.



ENGINEERING CONSULTANTS LTD OTTAWA, ONTARIO



SOUTH MERIVALE BUSINESS PARK

TYPICAL CROSS SECTION 20.0m R.O.W.

DATE:

NOV.30, 1990

FIG. No.

7-1

7.4 Cut/Fill Analysis

A cut/fill analysis for the entire SMBP site was completed to determine the impact that the absence of Barrhaven Treatment Facility fill would have on Phase II and III cut/fill quantities.

The overall grading plan presented in the Phase I construction drawings was used as a first step to determining the required cut and/or fill. This initial analysis determined that if the grades were established as shown on this plan, then approximately 250,000 m³ of fill would be required.

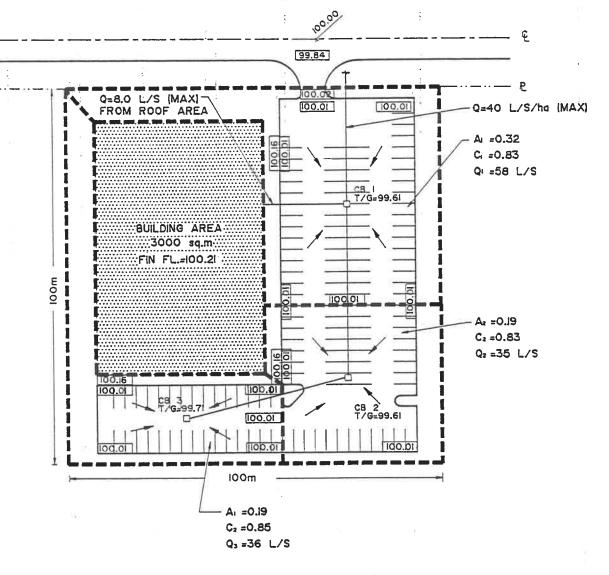
A second calculation of the required cut/fill was conducted. For this calculation, the final grade elevations along all the streets and property corners was lowered by 0.3 m. Street C was lowered marginally more. Because construction had begun on Street A, no change was made to the final grades. Street F has also been left as originally designed to provide gravity outlet for private storm systems and maintain overland major system flow routing.

Appendix D includes tables that detail the calculations used to quantity the cut/fill required along the right-of-way and the individual lots, Along the right-of-way a total of 18,148 m³ of fill will be generated by the removal of overburden material for the pipe installation. On the private lots, a total of 93,673 m³ of fill will be required to raise the sites to final grades which permit major overland flow drainage. This results in a total fill requirement of approximately 75,000 m³ and represents a fill depth of about 100 mm over the site area.

The analysis was based on a typical site plan design as presented in Figure 7-2.

7.5 Final Grading

Drawing 92019-GR1 details the proposed grading for the proposed Phase II and III construction. The grading plan reflects the lower final elevations along the Streets B, C, D, E and F and adjacent property limits.



REQUIRED DETENTION = $\frac{(58.5 + 35 + 36 + 8) - 40 \text{ L/S} \times 35 \text{min.} \times 60 \text{min.}}{1000 \text{ L/m}^3}$

= 203.7m ³

DEPTH OF PONDING DURING 1:100 YEAR STORM EVENT APPROXIMATELY 0.3m ABOVE T/G AT CB $\ensuremath{\mathsf{I}}$



ENGINEERING CONSULTANTS LTD OTTAWA, ONTARIO



SOUTH MERIVALE BUSINESS PARK

TYPICAL SITE GRADING PLAN

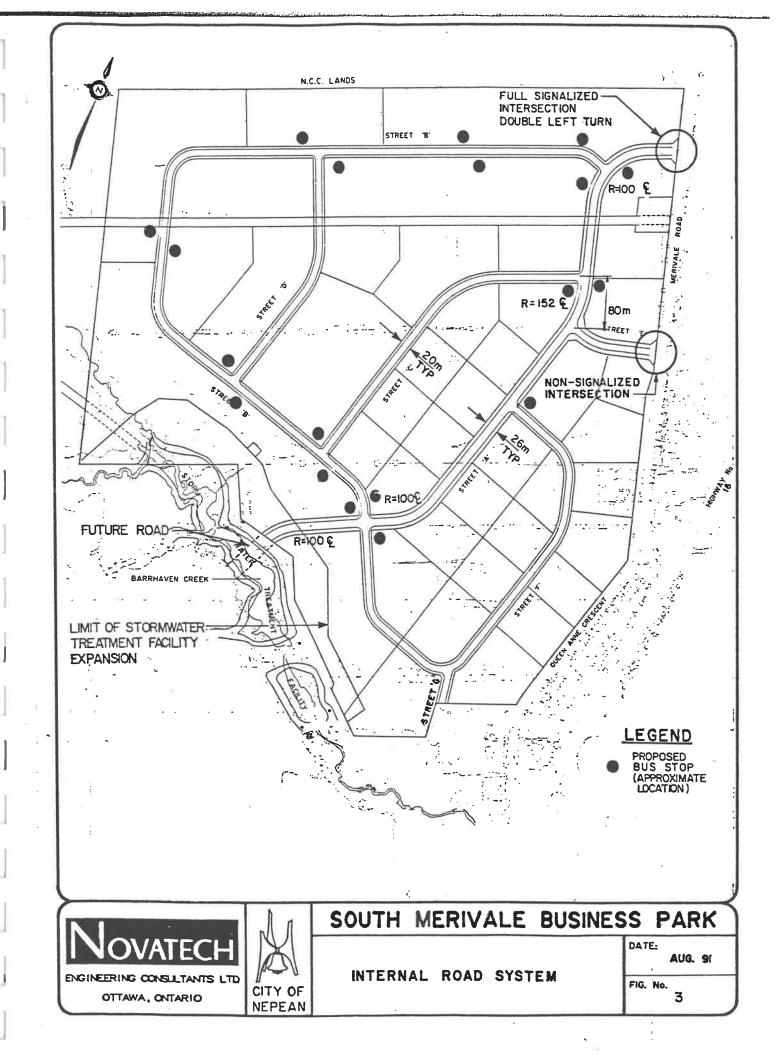
DATE: july, 1990 FIG. No. 7-2

8.0 BUS SERVICE AND POSTAL SERVICE

OC Transpo will provide bus service to the SMBP, however at this time they cannot confirm when service will be initiated. OC Transpo Operational Planning has confirmed:

- the bus stop locations shown on Figure 3
- that bus bays are not required
- that the requirement for bus shelter bases will be specified as a condition of site plan approval

Canada Post has confirmed that the business park will be serviced via group mail boxes, supplied by Canada Post, as required. Buildings with three or more businesses can install a centralized mailing facility. The purchasing, installation and maintenance of this facility is the building owner or developer's responsibility.



CORPORATE AUTHORIZATION

| This document entitled City of Nepean South Services Design Report was prepared by Novato | Merivale Business Park, Phase 2 and ech Engineering Consultants Ltd. |
|--|--|
| | |
| Prepared by: | Reviewed By: |
| Lee Jablonski, P.Eng. | Udo Boehme, P.Eng. |

APPENDIX A

SANITARY SEWER DESIGN SHEETS

SANITARY SEWER DESIGN SHEET

SOUTH MERIVALE BUSINESS PARK Phases II and III NOVATECH ENGINEERING CONSULTANTS LTD. CITY OF NEPEAN DEVELOPER: ENGINEERS: PROJECT: DESIGNED BY : LJ CHECKED BY :

DATE: June 22, 1992 Revision:

PAGE: 1 of 5

| | | | _ | | _ | | _ | | _ | _ | _ | | _ | _ | _ | _ | $\overline{}$ |
|----------------|--------------|----------------|---|-------|-------|--------|---|-------|---|-------|---|-------|---|---|-----|-------|---------------|
| | FULL FLOW | VELOCITY (m/s) | | 79.0 | | . 19.0 | | 0.67 | | 29.0 | | 79.0 | | | | 29.0 | |
| 8 | CAPACITY | (L/s) | | 33.98 | | 33.98 | | 33.98 | | 33.98 | | 33.98 | | | | 33.98 | |
| PROPOSED SEWER | GRADE | ж | | 0.30 | | 0.30 | | 0.30 | | 0.30 | | 0.30 | | | | 0.30 | |
| PRC | TYPE OF | PIPE | | PVC | | PVC | | PVC | | PVC | | PVC | | | | PVC | |
| | PIPE SIZE | (mm) | | 250 | | 250 | | 250 | | . 250 | | 250 | | | | 250 | |
| | LENGTH P | (m) | | 154.0 | | 58.0 | | 80.0 | | 111.0 | | 80.0 | | | | 0.49 | |
| PEAK DESIGN | FLOW Q (d) | (1/s) | | 2.98 | | 1.88 | | 5.18 | | 9.10 | | 11.45 | | | | 17.41 | |
| PEAK EXTRAN. | FLOW Q (1) | (1/s) | | 0.21 | | 0.13 | | 0.36 | | 0.64 | | 0.80 | | | | 1.22 | |
| POP FLOW | (d) b | (L/s) | | 2.77 | | 1.75 | | 4.81 | | 8.46 | | 10.65 | | | | 16.19 | |
| PEAKING | FACTOR | I | | 2.80 | | 2.80 | | 2.80 | | 2.80 | | 2.80 | | | | 2.80 | |
| CUMMULATIVE | AREA | (ha) | | 1.9 | | 1.2 | | 3,3 | | 5.8 | | 7.3 | | | | 11.1 | |
| CUMMU | 908 | | | 190 | | 120 | | 330 | | 580 | | 730 | | | | 1110 | |
| INDIVIDUAL | AREA | (ha) | | 1.9 | | 1.2 | | 2.1 | | 2.5 | | 1.5 | | | 1.7 | 2.1 | |
| IND | P09 | | | 190 | | 120 | | 210 | | 250 | | 150 | | Manhole | 170 | 210 | |
| | 0t | ж.к. | | 5 | | 12 | | 22 | | 23 | | 54 | | pment Into | | 26 | |
| | FROM | #.H. | | 19 | | 20 | | 12 | | 22 | | 23 | | ure Develo | | 54 | |
| LOCATION | STREET | | | 141 | | Ē | | 141 | | .F. | | 151 | | Flow From Future Development Into Manhole | | 13: | |

q = average daily per cap. flow (450 L/cap. d)

I = unit of peak extraneous flow (0.11 L/ha/s)

M = peaking factor =2.8

q (p) = peak population flow (L/s) Q (i) = peak extraneous flow (L/s)

Q (d) = peak design flow (L/s)

 $Q(p) = (P^*q^*N)/(86,400)$ (L/s)

q (i) = I*A (L/s), A in hectares

(s/1) (i) b + (d) b = (p) b

SANITARY SEWER DESIGN SHEET

DESIGNED BY : LJ

SOUTH MERIVALE BUSINESS PARK Phases II and III

Page: 2 of 5

DATE: SEPTEMBER 6, 1990

CHECKED BY :

CITY OF NEPEAN DEVELOPER:

ENGINEERS:

PROJECT:

NOVATECH ENGINEERING CONSULTANTS LTD.

Revision:

| | FULL FLOW | VELOCITY (m/s) | 79.0 | | 29.0 | 79.0 | 79.0 | | 0.67 | 29.0 | 36 | 79.0 | |
|----------------|------------------|----------------|--------|-----|-------|-------|-------|--|-------|-------|----|-------|--|
| £ | CAPACITY | (1/s) | 33.98 | × | 33.98 | 33.98 | 33.98 | | 33.98 | 33.98 | | 33.98 | |
| PROPOSED SEVER | GRADE | ж | 0.30 | | 0.30 | 0.30 | 0.30 | | 0.30 | 0.30 | | 0.31 | |
| PRC | TYPE OF | PIPE | PVC | 100 | PVC | PVC | PVC | | PVC | PVC | | PVC | |
| | LENGTH PIPE SIZE | (mm) | 250 | | 250 | 250 | 250 | | 250 | 250 | | 250 | |
| | LENGTH | (m) | 64.0 | | 0.99 | 24.0 | 150.0 | | 0.44 | 87.0 | | 110.0 | |
| PEAK DESIGN | FLOW Q (d) | (r/s) | 19.45 | | 21.33 | 22.27 | 23.37 | | 2.04 | 5.02 | | 06.9 | |
| PEAK EXTRAN. | FLOW & (f) | (r/s) | 1.36 | | 1.50 | 1.56 | 1.64 | | 0.14 | 0.35 | | 0.48 | |
| POP FLOW | (d) b | (L/s) | 18.08 | | 19.83 | 20.71 | 21.73 | | 1.90 | 79.4 | | 6.42 | |
| PEAKING | FACTOR | × | 2.80 | | 2.80 | 2.80 | 2.80 | | 2.80 | 2.80 | | 2.80 | |
| HMULATIVE | AREA | (ha) | 12.4 | | 13.6 | 14.2 | 14.9 | | 1.3 | 3.2 | | 4-4 | |
| ССИНИП | og. | | 1240.0 | | 1360 | 1420 | 1490 | | 130 | 320 | | 440 | |
| THDIVIDUAL | AREA | (ha) | 1.3 | | 1.2 | 0.6 | 0.7 | | 1.3 | 1.9 | | 1.2 | |
| TINDI | 9 | | 130 | | 120 | 99 | 22 | | 130 | 190 | | 120 | |
| | 2 | н.н. | 27 | Œ. | 82 | & | 14 | | 59 | 88 | | 35 | |
| | FROM | м.н. | 92 | - | 27 | 28 | ۶ì | | 29 | 26 | | 28 | |
| LOCATION | STREET | | Ŀ | | Ŀ | 1. | 19. | | ١٥٠ | ٥ | | ιđι | |

(450 L/cap. d) q = average daily per cap. flow

1 = unit of peak extraneous flow (0.11 L/ha/s)

M = peaking factor = 2.8

Q (p) = peak population flow (L/s)

Q (i) = peak extraneous flow (L/s) a (d) = peak design flow (L/s)

q (i) = I*A (L/s), A in hectares

n = 0.013

Q(p) = (p*q*M)/(86,400) (L/s)

q (d) = Q (p) + Q (i) (L/s)

9

DESIGNED BY: SG

CHECKED BY: LJ

DEVELOPER: ENGINEERS:

PROJECT:

SOUTH MERIVALE BUSINESS PARK Phases II and III

CITY OF NEPEAN

NOVATECH ENGINEERING CONSULTANTS LTD.

PAGE: 3 of 5 DATE: June 22, 1992

Revision:

VELOCITY (m/s) FULL FLOW 19.0 0.67 19'0 0.67 0.67 0.67 79.0 0.67 n = 0.013 LENGTH PIPE SIZE TYPE OF GRADE CAPACITY (L/s) 33.98 33.98 33.98 33.98 33.98 33.98 33.98 33.98 PROPOSED SEWER Q (p) = (P*q*M)/(86,400) (L/s) 0.30 0.30 0.30 0.30 0.30 36 0.30 0.30 0.30 PIPE PVC PVC PVC PVC PVC PYC PVC PVC (mm) 250 250 250 250 250 250 250 520 113.0 106.0 110.0 113.0 (w 61.0 75.0 95.0 60.8 PEAK EXTRAN. PEAK DESIGN FLOW Q (d) (s/J) 11.92 14.43 15.84 24.78 5.65 7.53 4.55 9.41 FLOW Q (I) (1/s) 0.84 1.1 1.74 0.35 0.53 0.40 99.0 1.0 Q (p) = peak population flow (L/s) POP FLOW (d) O 13.42 14.73 11.08 23.04 (L/s) 5.25 7.00 8.75 4.23 PEAKING FACTOR 2.80 2.80 2.80 2.80 2.80 2.80 2.80 2.80 Σ CUMMULATIVE AREA 15.8 10.1 (ha) 3.6 0.9 7.6 9.2 2.9 4.8 РОР 1580 1010 360 260 290 480 900 920 AREA (ha) 6. 2.9 6.1 3.6 5.4 9. 9. 0.9 INDIVIDUAL q = average daily per cap. flow (450 L/cap. d) РОР 190 160 130 290 360 240 160 8 ō H.H. 39 88 27 34 42 5 38 32 FROM Μ. Ή. 42 9 39 38 98 53 4 37 LOCATION STREET ĝα ģ è b è įω ğ ĝ

O (i) = I*A (1/s), A in hectares

Q (i) = peak extraneous flow (L/s)

I = unit of peak extraneous flow (0.11 Vha/s)

SOUTH MERIVALE BUSINESS PARK Phases II and III Page: 4 of 5

CITY OF NEPEAN

DEVELOPER: ENGINEERS:

DESIGNED BY : LJ

CHECKED BY :

PROJECT:

NOVATECH ENGINEERING CONSULTANTS LTD.

Revision:

DATE: SEPTEMBER 6, 1990

| LOCATION | | | IND | INDIVIDUAL | CUMMUL | JLATIVE | PEAKING | POP FLOW | PEAK EXTRAN. | PEAK DESIGN | | | PR | PROPOSED SEVER | JER. | |
|----------|------|------|-----|------------|--------|---------|---------|----------|--------------|-------------|--------|------------------|---------|----------------|----------|----------------|
| STREET | FROM | 5 | ş | AREA | ğ | AREA | FACTOR | (d) g | FLOW Q (i) | FLOW Q (d) | LENGTH | LENGTH PIPE SIZE | TYPE OF | GRADE | CAPACITY | FULL FLOW |
| | ж.н. | н.н. | | (ha) | | (ha) | × | (T/s) | (L/s) | (۲/8) | Œ | (mm) | PIPE | 3-6 | (L/s) | VELOCITY (m/s) |
| | | | | | | | | | | | | | | | | |
| 181 | 67 | 47 | 170 | 1.7 | 170 | 1.7 | 2.80 | 2.48 | 0.19 | 2.67 | 105.0 | 250 | PVC | 0.30 | 33.98 | 29.0 |
| | | i l | W | | : | | | | | | | | | - | | |
| | 25 | 95 | 200 | 2.0 | 370 | 3.7 | 2.80 | 5.40 | 0.41 | 5.80 | 86.0 | 250 | PVC | 0.30 | 33.98 | 79.0 |
| | | | | | | | | | | | | | | | | 8 |
| 181 | 97 | 45 | 220 | 2.2 | 290 | 5.9 | 2.80 | 8.60 | 0.65 | 9.25 | 0.66 | 250 | PVC | 0.30 | 33.98 | 29.0 |
| | | | | | | | | | | | | | | - | | |
| - | 53 | 2 | 230 | 2.3 | 820 | 8.2 | 2.80 | 11.96 | 0.00 | 12.86 | 101.0 | 250 | PVC | 0.30 | 33.98 | 29.0 |
| | | | | | | | | | | | | | | | | |
| -81 | 3 | 27 | 160 | 1.6 | 980 | 9.8 | 2.80 | 14.29 | 1,08 | 15.37 | 97.0 | 250 | PVC | 0.30 | 33.98 | 79.0 |
| | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| ٠¢. | 43 | 62 | 120 | 1.2 | 1580 | 15.8 | 2.80 | 23.04 | 1.74 | 24.78 | 118.0 | 250 | PVC | 0.30 | 33.98 | 29.0 |
| | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| 101 | 19 | 62 | 160 | 1.6 | 160 | 1.6 | 2.80 | 2,33 | 0.18 | 2.51 | 38.0 | 250 | PVC | 0.30 | 33.98 | 79.0 |
| 19 | | | | | | | | | | | | | | | | |

q = average daily per cap. flow (450 L/cap. d)

I = unit of peak extraneous flow (0.11 (/ha/s)

M = peaking factor = 2.8

Q (i) = peak extraneous flow (L/s)

Q (p) = peak population flow (L/s)

q (d) = peak design flow (L/s)

 $Q(p) = (p^4q^4M)/(86,400)$ (L/s) $Q(i) = 1^4A$ (L/s), A in hectares

n = 0.013

q (d) = Q (p) + Q (i) (L/s)

SOUTH MERIVALE BUSINESS PARK Phases II and III

PROJECT:

DATE: June 22, 1992 Revision:

PAGE: 5 of 5

DEVELOPER: ENGINEERS: DESIGNED BY : LJ CHECKED BY :

NOVATECH ENGINEERING CONSULTANTS LTD. CITY OF NEPEAN

VELOCITY (m/s) FULL FLOW 29.0 (r/s) CAPACITY 33.98 PROPOSED SEVER GRADE 0.30 TYPE OF PIPE PVC LENGTH PIPE SIZE (mm) 520 611 Ê FLOW Q (d) PEAK DESIGN (L/s) 88. PEAK EXTRAN. FLOW Q (i) (L/s) 0.13 POP FLOW (d) **0** (r/s) ۲. ۲. PEAKING FACTOR 2.80 1.2 AREA (ha) CUMMULATIVE 120 ğ AREA (ha) 7:5 INDIVIDUAL 22 ğ M.H. ø ဥ ¥. 쭚 1 LOCATION STREET 1

(450 L/cap. d) q = average daily per cap. flow

(0.11 l/ha/s) I = unit of peak extraneous flow M = peaking factor = 2.8

Q (p) = peak population flow (L/s)

Q (i) = peak extraneous flow (L/s) Q (d) = peak design flow (L/s)

Q (i) = I*A (L/s), A in hectares (b) = (b*q*M)/(86,400)

n = 0.013

q(d) = q(p) + q(i) (L/s)

DESIGNED BY: SG

SOUTH MERIVALE BUSINESS PARK - PHASE 1

CITY OF NEPEAN

DATE: NOV. 5, 1991 PAGE: 1 of 3

CHECKED BY: LJ

DEVELOPER: ENGINEERS:

PROJECT:

NOVATECH ENGINEERING CONSULTANTS LTD.

Revision: Dec. 31/91

| 07 | LOCATION | | MON | INDIVIDUAL | CUMU | CUMULATIVE | PEAKING | POP FLOW | POP FLOW PEAK EXTRAN. PEAK DESIGN | PEAK DESIGN | | | PRO | PROPOSED SEWER | WER | |
|----------------------------------|------------|--------|-------------|-------------|-------------|---------------|---|----------|-----------------------------------|-------------|--------|------------------|---------|----------------|----------|----------------|
| STREET | FROM | 2 | POP | AREA | POP | AREA | FACTOR | (d) O | FLOW 0 (I) | FLOW Q (d) | LENGTH | LENGTH PIPE SIZE | TYPE OF | GRADE | CAPACITY | FULL FLOW |
| | X. | M.H. | | (ha) | | (ha) | ₹ | (6/3) | (n/s) | (s/٦) | (m) | (mm) | PIPE | 24 | (C/s) | VELOCITY (m/s) |
| .×. | EXT. | 15A | Constant Fi | low from La | ngfield-Dav | idson Heights | Constant Flow from Langfield-Davidson Heights = 249.45 L/s* | | | 249.45 | | 750 | CONC | 0.15 | 449.81 | 0.99 |
| | | | | | | | | | | | | | | | 12. | |
| | 15A | 15 | | | | | | | | 249.45 | 18.0 | 750 | CONC | 0.15 | 449.81 | 0.99 |
| | | | | | | | | | | | | | | | | 8 |
| | 15 | 7 | 500 | 2.0 | 200 | 2.0 | 2.80 | 2.82 | 0.22 | 252.59 | 105.0 | 750 | CONC | 0.15 | 449.81 | 0.89 |
| | | | | | | | | | | | | | - | | 17 | |
| | | | | | | | | | | | | | | | | |
| Flow from Street 'B' Into MH 34: | 'B' into N | 4H 34: | 1580 | 15.8 | | | | | | | | | | | | |
| ġ0 | 34 | 33 | 170 | 1.7 | 1750 | 17.5 | 2.80 | 25.52 | 1.93 | 27.45 | 94.0 | 375 | CONC | 0.18 | 77.60 | 0.68 |
| | | | | | | | | | | | | | | | | |
| | | | >5 | | | | | | | | | | | | | |
| Flow from Street 'C, Into MH 33: | C' Into | WH 33: | 830 | 8.3 | • | | | | | | | | | | | |
| .8. | 8 | 32 | 110 | 7 | 2690 | 56.9 | 2.80 | 39.23 | 2.96 | 42.19 | 78.0 | 375 | CONC | 0.18 | 77.60 | 0.68 |
| | | | | | | | | | | | | | | | | |
| | 32 | 31 | | | 2690 | 56.9 | 5.80 | 39.23 | 5.96 | 42.19 | 27.5 | 375 | SONO | 0.18 | 77.60 | 99:0 |
| | | | | | | | | | | | 0,00 | 35.0 | 0,000 | 9,0 | 1100 | 88.0 |
| | 9 | 7 | | | 2690 | 26.9 | 2.80 | 39.23 | 5.96 | 42.18 | 34.0 | 3/3 | | 6.78 | 3.5 | 0.00 |

Constant flow from external area = 249.45 (/s per Delcan Design Sheel dated 91.10.21

q = average deally per cap, flow (450 L/cap, d)

I = unit of peak extraneous flow (0.11 (/ha/s)

M = peaking factor = 2.8 for Light industrial land use

Q (p) = peak population flow (L/s)

O (i) = peak extraneous flow (1/s)

Q (d) = peak design flow (L/s)

Q (i) = 1*A (L/s). A in hectares Q (p) = (p*4?M)/(86,400) (L/s) Q (q) = Q (p) + Q (l) (L/s)

n = 0.013

DESIGNED BY: SG

CHECKED BY: LJ

DEVELOPER: PROJECT:

ENGINEERS:

SOUTH MERIVALE BUSINESS PARK . PHASE 1

NOVATECH ENGINEERING CONSULTANTS LTD. CITY OF NEPEAN

DATE: NOV. 4, 1891

PAGE: 2 of 3

Revision: Dec. 31/91

| MOLTADOL | | | VIGNI | INDIVIDUAL | CUMU | CUMULATIVE | PEAKING | POP FLOW | PEAK EXTRAN. PEAK DESIGN | PEAK DESIGN | | | PROF | PROPOSED SEWER | WER | |
|--------------|--------------------------------|--------|-------|------------|------|------------|---------|----------|--------------------------|-------------|--------|------------------|---------------|----------------|----------|----------------|
| STRFFT | FROM | 10 | POP | AREA | POP | AREA | FACTOR | <u>©</u> | FLOW Q () | FLOW Q (d) | LENGTH | LENGTH PIPE SIZE | TYPE OF GRADE | GRADE | CAPACITY | FULL FLOW |
| | W.H. | M.H. | | (ha) | | (ha) | Σ | (1/s) | (1/s) | (Us) | Œ | (mm) | 괾 | × | (L/s) | VELOCITY (m/s) |
| ow from Sir | low from Street F' Into MH 14: | AH 14: | 1540 | 15.4 | | | | | | | | | | | | |
| × | 14 | 13 | 120 | 12 | 4550 | 45.5 | 2.80 | 66.35 | 5.01 | 320.81 | 72.0 | 750 | CONC | 0.14 | 434.56 | 0.95 |
| | | | | | | | | | | | | | | | | |
| | 13 | 12 | 120 | 1.2 | 4670 | 46.7 | 2.80 | 68.10 | 5.14 | 322.69 | 40.5 | 750 | CONC | 0.14 | 434.56 | 0.95 |
| | | | | | | | | | | | | | | | | |
| | 12 | F | 220 | 2.2 | 4890 | 48.9 | 2.80 | 71.31 | 5.38 | 326.14 | 119.0 | 750 | CONC | 0.15 | 449.81 | 0.89 |
| | | | | | | | | | | | | | | | | |
| | = | 9 | 260 | 5.6 | 5150 | 51.5 | 2.80 | 75.10 | 5.67 | 330.22 | 115.0 | 750 | CONC | 0.15 | 449.81 | 0.99 |
| | | | | | | 8 | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| low from St. | low from Street F' into MH 10: | MH 10: | 190 | 1.9 | | | | | | | | | | | | |
| × | 10 | | 180 | 1.8 | 9250 | 55.2 | 2.80 | 80.50 | 6.07 | 336.02 | 86.5 | 750 | CONC | 0.15 | 449.81 | 66:0 |
| | 8 | 8 | 140 | 1.4 | 2660 | 96.6 | 2.80 | 82.54 | 6.23 | 338.22 | 0.98 | 750 | CONC. | 0.15 | 449.81 | 0.99 |
| | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |

q = average daily per cap. flow (450 L/cap. d)

M = peaking factor = 2.8 for Light industrial land use i = unit of peak extraneous flow (0.11 (ha/s)

Q (p) = peak population flow (Us) Q (i) = peak extraneous flow (L/s)

Q (d) = peak design flow (L/s)

O (1) = 1*A (L/s). A in hectares $Q(p) = (P^4q^4M)/(86,400)$ (U/s)

Q (q) = Q (b) + Q (j) (1/s)

n = 0.013

DESIGNED BY: SG

Revision: Dec. 31/91 DATE: NOV.4, 1991

PAGE: 3 of 3

SOUTH MERIVALE BUSINESS PARK . PHASE 1 NOVATECH ENGINEERING CONSULTANTS LTD. CITY OF NEPEAN DEVELOPER: ENGINEERS: PROJECT: CHECKED BY : LJ

| TO POP AREA POP AREA FACTOR O (b) | | | | i dia | NIN IAI | TA HAMINA | I ATIVE | PEAKING | POP FLOW | PEAK EXTRAN. | PEAK EXTRAN. PEAK DESIGN | | | PROF | PROPOSED SEWER | WER | |
|--|------------|--------------|------------|-------------|---------|-----------|---------|---------|----------------|--------------|--------------------------|--------|--------------|-------------|----------------|----------|-----------------|
| Hath Math | | LOCATION | | | MIDDAL | COM | 4 | | 1 | 2 | 27 0 270 | HENGTH | _ | TYPE OF | GRADE | CAPACITY | FULL FLOW |
| N. H. M. H. M. H. M. (I.b.) M. (I.b.) (I. | STREET | FROM | 2 | POP | AREA | POP | AREA | FACTOR | <u>@</u> | FLOW G (i) | FLOW G (a) | LENGIN | | 100 | * | 2/2 | VFI OCITY (m/s) |
| | | M.H. | M.H. | | (ha) | | (ha) | Σ | (c/s) | (L/s) | (C/s) | E | (E) | 2 | R | (en) | |
| Record R | v from Str | eet 'E' into | MH 8: | -120 | 1.2 | | | | | | | | | 0,100 | 9,0 | 45.457 | 100 |
| 2.5 6280 62.8 2.80 91.56 681 347.84 86.0 750 CONC 0.16 464.57 2.3 6280 62.8 2.80 91.56 681 347.84 86.0 750 CONC 0.16 464.57 2.3 230 2.3 2.80 3.35 0.25 3.61 2.35 250 PVC 0.30 33.86 1.9 420 4.2 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.89 420 4.2 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.89 420 2.8 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.89 420 2.8 2.80 6.13 0.45 6.59 56.0 250 PVC 1.00 62.04 2.9 2.9 2.80 4.23 0.32 4.55 2.0 PVC 1.00 62.04 | × | 8 | 7 | 520 | 2.5 | 6030 | 60.3 | 2.80 | 67.94 | 6.63 | 344.02 | 44.0 | 8 | NO. | 9.0 | ic.Pos | 201 |
| 2.5 6280 62.8 2.80 81.56 6.81 347.84 66.0 750 CONC 0.16 464.57 2.5 6280 62.8 2.80 81.56 6.81 347.84 66.0 750 CONC 0.16 464.57 2.3 230 2.3 2.80 3.35 0.25 3.61 23.5 250 PVC 0.30 33.89 2.3 230 2.3 2.80 3.35 0.25 3.61 23.5 250 PVC 0.30 33.89 1.9 420 4.2 2.80 6.13 0.46 6.59 43.0 250 PVC 0.30 33.89 1.9 420 4.2 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.89 2.9 2.9 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 | | | | | | | | | | | | | | | | | |
| 2.5 6280 62.8 2.80 81.58 6.91 347.84 96.0 750 CONC 0.16 464.57 2.3 230 2.3 2.80 3.35 0.25 3.61 23.5 250 PVC 0.30 33.86 2.3 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.89 33.89 2.80 4.2 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.89 2.90 2.9 2.80 4.23 0.32 4.55 2.50 PVC 1.00 62.04 2.3 2.80 6.13 0.46 6.59 56.0 250 PVC 1.00 62.04 2.3 2.80 6.13 0.46 6.59 56.0 250 PVC 1.00 62.04 2.3 2.80 62.04 2.3 2.80 6.13 0.45 6.59 2.50 PVC 1.00 62.04 2.3 2.80 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.3 | | 7 | 9 | | | 6030 | 60.3 | 2.80 | 87.94 | 6.63 | 344.02 | 44.0 | 750 | CONC | 0.16 | 464.57 | 1.02 |
| 2.5 6280 62.8 2.80 81.58 6.81 347.84 96.0 750 CONC 0.16 464.57 2.3 230 2.3 2.80 3.35 0.25 3.61 23.5 250 PVC 0.30 33.98 2.3 230 2.3 2.80 3.35 0.25 3.61 49.0 250 PVC 0.30 33.98 1.9 420 4.2 2.80 6.13 0.46 6.59 560 250 PVC 0.30 33.98 420 4.2 2.80 6.13 0.46 6.59 560 250 PVC 0.30 33.98 2.80 2.80 4.23 0.32 4.55 7.0 1.00 62.04 2.80 2.80 4.23 0.32 4.55 7.0 1.00 62.04 2.80 2.80 4.20 0.30 33.98 2.80 2.80 4.20 6.13 0.46 6.59 560 250 PVC 0.30 33.98 2.80 2.80 4.20 6.13 0.46 6.59 560 250 PVC 1.00 62.04 2.80 2.80 4.23 0.32 4.55 7.0 1.00 62.04 | | | | | | | | | | | | | | | | | |
| 2.3 2.20 2.3 2.80 3.35 0.25 3.61 23.5 250 PVC 0.30 33.86 2.3 2.20 2.3 2.80 3.35 0.25 3.61 49.0 250 PVC 0.30 33.86 1.8 420 42 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.86 420 42 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.86 2.90 2.9 2.80 4.23 0.32 4.55 2.50 PVC 1.00 62.04 2.90 2.9 2.90 4.23 0.32 4.55 2.50 PVC 1.00 62.04 | | 9 | 10 | 250 | 2.5 | 6280 | 62.8 | 2.80 | 91.58 | 16.91 | 347.94 | 96.0 | 750 | CONC | 0.16 | 464.57 | 1.02 |
| 23 230 2.3 2.80 3.35 0.25 3.61 23.5 PVC 0.30 33.98 33.88 250 2.3 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.98 33.88 33.88 2.80 4.2 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.98 33.88 2.80 4.2 2.80 4.2 2.80 6.13 0.35 4.55 2.50 PVC 0.30 33.98 33.88 2.80 4.2 2.80 4.2 2.80 4.2 2.80 6.13 0.35 4.55 2.50 PVC 0.30 33.88 2.80 PVC 0.30 33.88 2.80 PVC 0.30 33.88 2.80 PVC 0.30 33.88 2.80 PVC 0.30 2.9 PVC 0. | | ۲. | | | | | | | | | | | | | | | |
| 23 230 2.3 2.80 3.35 0.25 3.61 23.5 PVC 0.30 33.86 230 2.3 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.88 1.9 420 4.2 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.88 420 4.2 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.88 290 2.8 2.80 4.23 0.32 4.55 0.90 PVC 1.00 62.04 C (p) = peak population flow (L/s) | | | | | | | | | | | | | | | | | |
| 1.8 420 4.2 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.98 1.80 420 4.2 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.98 2.90 4.23 0.32 4.55 2.50 PVC 1.00 62.04 2.90 2.90 4.23 0.32 4.55 2.50 PVC 1.00 62.04 2.90 2.90 2.90 2.90 2.90 2.90 2.90 2.90 | .4. | - | 2 | 230 | 2.3 | 230 | 2.3 | 2.80 | 3.35 | 0.25 | 3.61 | 23.5 | 550 | SC | 0:30 | 33.98 | 0.67 |
| 1.8 420 4.2 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.98 420 4.2 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.98 420 4.2 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.98 290 2.8 2.80 4.23 0.32 4.55 2.50 PVC 1.00 62.04 C (p) = peak population flow (L/s) | | | | - | | | | | | | | | | | | | |
| 1.8 420 4.2 2.80 6.13 0.46 6.59 43.0 250 PVC 0.30 33.88 420 4.2 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.88 2.80 4.2 2.80 4.2 0.32 4.55 2.50 PVC 1.00 62.04 C.04 6.2 0.30 2.80 PVC 1.00 62.04 C.04 6.2 0.30 2.80 PVC 1.00 62.04 PVC 1.00 PVC 1.0 | | | | | | | 1 | Og c | 3.35 | .0.25 | 361 | 49.0 | 250 | PVC | 0.30 | 33.98 | 29'0 |
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| 1.8 420 42 2.80 6.13 0.46 6.59 43.0 250 PVC 0.30 33.88 420 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.88 2.80 4.23 0.32 4.55 2.50 PVC 1.00 62.04 C.00 2.9 2.9 2.80 4.23 0.32 4.55 0.00 (D) = (P*q*M)/(86,400) (U/s) | | | | | | | | | | | | | | | | | |
| 420 4.2 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.98 33.98 250 2.90 2.9 2.80 4.23 0.32 4.55 250 PVC 1.00 62.04 (L/s) | | 6 | 4 | 96- | 1.9 | 450 | 4.2 | 2.80 | 6.13 | 0.46 | 6.59 | 43.0 | 520 | 2 | 98.9 | 33.88 | 0.0 |
| 420 4.2 2.80 6.13 0.46 6.59 56.0 250 PVC 0.30 33.88 33.88 2.80 2.80 4.23 0.32 4.55 2.50 PVC 1.00 62.04 2.90 2.9 2.80 4.23 0.32 4.55 2.50 PVC 1.00 62.04 2.90 2.9 2.90 4.23 0.32 4.55 2.50 PVC 1.00 62.04 2.90 2.90 2.90 2.90 2.90 2.90 2.90 2.90 | | | | | | | | | | | | | | | | | |
| 290 2.9 2.80 4.23 0.32 4.55 2.50 PVC 1.00 62.04 (L/s) 0.32 0.00 (D) = (P*q*M)/(86,400) (L/s) | | 1 | 2 | | | 420 | 4.2 | 2.80 | 6.13 | 0.46 | 6.59 | 26.0 | 520 | SC SC | 0.30 | 33.98 | 0.67 |
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| 290 2.9 2.90 4.23 0.32 4.55 250 PVC 1.00 62.04 (Colored Colored Colore | .e | | Connection | ns: | | | | | | | | | | | | | |
| Q (p) = peak population flow (L/s) Q (p) = (p) = (p) = (p) = (L/s) (L/s) | | | 8 | _ | | 290 | 2.9 | 2.80 | 4.23 | 0.32 | 4.55 | | 520 | PVC PVC | - 1 | 25.02 | 1.22 |
| 41 6 6 | | - | | 1000 | - | - | | (a) c | k population 8 | ow (L/s) | | | Q (p) • (P*c | q*M)/(86,44 | | | n = 0.013 |
| | = average | dayy per ca | ap. now | (450 L/Cap. | 5 | | | - | | | | | 41 | A 141 A | in harderes | | |

i ... unit of peak extraneous flow (0.11 kha/s)

M = peaking factor = 2.8 for Light industrial land use

Q (i) = peak extraneous flow (Us) Q (d) = peak design flow (L/s)

Q (() = 1'A (4's), A in nection (d) = Q (d) + Q (() (1/s)

10 service connections - worst case @ manhole S9

* Note:

APPENDIX B DELCAN CORRESPONDENCE DATED OCTOBER 21, 1991





1991 10 21

Our Ref: 04-19:

04-1917-G-00

Mrs. Susan Gordon, P.Eng.
Novatech Engineering Consultants Ltd.
Suite 17
77 Auriga Drive
Nepean, Ontario
K2E 7Z7

Dear Susan:

We are pleased to transmit herein, on behalf of the City of Nepean, copies of the sanitary sewer design sheets, dated October 91, for Longfields/Davidson as prepared by Oliver, Mangione, McCalla and Associates Limited and Delcan's design sheet for the sanitary sewers located in the collector road crossing the ravine. Sanitary sewer design for the collector road sewers is based on OMM design flows as shown. Please note that the review of the derivation of these flows is beyond our terms of reference.

Should you have any questions, please do not hesitate to call.

FOR CIRCULATION

| | 59. | | |
|--|------------|--------|------|
| Yours very truly, | INFO | ACTION | NAME |
| | | | МН |
| | 12 | | DM |
| A | | | JR |
| R. Allen, P.Eng. | 1 | 1 | UB |
| Project Manager | | 77 | RC |
| | | | BA |
| PJH:lmb | | | JD |
| Encl. | | | GM |
| Elici. | | | DW |
| cc: Wayne Newell, P.Eng. | | | ED |
| City of Nepean | | | TG |
| | | ÷ | KS |
| | 1 | | PF |
| DELCAN CORPORATION | | | AH |
| 2001 THURSTON DRIVE, P.O. 80X 8004, OTTAWA, ONTARIO, K1G 3H6 • (613) 735-4160 TELEX FAX: (613) 735-7105 | 05-9666-89 | 3 | GC |
| ST JOHNS TORONTO, MONTREAL, MAMILTON NIASZPA FALLS, LONDON, THUNDER BAY, WINNIPEG PEGINA, SASK CALGARY, VICTORIA VANCOUVER NANAMO | ATPON | | LC |
| | - | | CAD |
| | 1 | | 56. |

Job: 87-5765

October 18, 1991

Sanitary Sewer Computation Sheets

Criteria Used

The following flows were utilized in the design of the sanitary trunk sewer system.

| Description | Design Criteria | Peaking Factor |
|---------------|------------------------------------|----------------------------|
| Residential | 454 L/cap/day | Harmon William Equation |
| Commercial | 37,128 L/ha/day (85 persons/ha) | Harmon William Equation |
| Institutional | 37,128 L/ha/day (85 persons/ha) | Harmon William Equation |
| Infiltration | 0.11 L/ha/day | MOE Graph |

The following densities taken from the City of Nepean Planning Committee report, South Urban Center.

- 1. Low and medium density residential is assumed to consist of 44.5 people per ha.
- 2. Medium and high density residential 190 people per ha.
- 3. Transitway and parkland have been included as low and medium density residential.



| 4 average I aunit of M a peaking | q = average daily per capita flow (L/cap.d) munit of peak extraneous flow (L/ha.s) m = peaking factor q(p) = peak population flow (L/s) | oita fic ous flow low (L/s | , ([[[| (cap.d) /ha.s | SANI | SANITARY | SEWE | R DES | SEWER DESIGN SHEET | HEET | | 4 (d) b | 14 + po Pgh (L. | H = 1 + $\frac{14}{4 + pos}$ where P = $\frac{0}{4}$ (L/s) | 4 | tion in | 1000.4 |
|---|---|----------------------------------|------------|------------------|------------|------------|--------------------|------------|--------------------|------------|--------------------------------|----------------------|---------------------|--|---|------------------|-----------|
| Q(i) = peak Q(d) = peak | extraneous fl design flow | ow (L/s | | | : | | | | | | | (P) b | 1A (L/s Q(p) + (| = IA (L/s) where A = Q(p) + Q(i)(L/s) | R - | area in hectures | 167 |
| 7007 | LOCATION | | INDIVIDUAL | DUAL | CUMULATIVE | TIVE | Peaking | Pop. (10m | | | | | PAC | PROPOSED SEVER | | | |
| | Ш | | | factores? | Pop. | [hectores] | factor H | 145 7 | 100 | 0(4) (1/1) | Length [m] | Pipe titre | lype of p.pe | Grade 1 | A11324(1) | elaciey faft. | 10 10 10 |
| "Collector Hd. So | South F. II. North F. L | 1 | | | C700 | 65.19 | | 75.4 | 5.89 | <u>-1</u> | | | | | | | |
| | | | | | | | | | | Ţ., | 1:1 | 678 | Conc | 0.15% | 339.5 | 0.95 | |
| | | | | | | | | | | | 28 | 2-450 | Conc | 0.35\$ | 352,4 | 1.073 | |
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| | | + | 1 | 1 | | | | | | | | | Ì | İ | | İ | |
| *See Oliver Mangione McCalla Design Sheets Dated Oct. | ne McCalla De | Sion Sh | sets Dat | ed Oct | 1661 | 1 | | | | - | 1 | | | | | | 1 |
| DelCen | | c | ē | | | DES | DESIGN J.R | J.R. Allen | | PROJECT | - 1 | Long fields/Davidson | avidson | | | SHEE | SHEET NO. |
| CONSTANT PAGE PAGE STREET AND PARTY OF | Car Descri | | ٠ | | | 벙 | CHECKED P.J. Ihint | . Ihint | | Storm | Stormwater Management Facility | gement | Facility | | | 7 | |
| | | | | | | DATE | E 91.10.21 | .21 | | | | | | | | | |
| | | | | | | - | | | | | | | | | | | |

OLIVER, MANGIONE, McCALLA & ASSOCIATES LIMITED CONSULTING ENGINEERS
194 COLONNADE ROAD SOUTH.
NEPEAN, ONTARIO K2E 7JS

Sanitary Sewer Design Sheet

87-5765 PROJECT: LONGFIELDS CONMUNETY DEVELOPER:

ENGINEER: -

PAGE 1.11. 9

007. 1991 400

DESIGNED BY:

CHECKED BY:

DATE:_

| The same of the sa | | | VIONI | INDIVIDIAL | CUMULATIVE | ATIVE | | Papulation | **** | 1 | - | PRO | PROPOSED | SEWER | | |
|--|---------|----------|-------|------------|------------|-------------|------|------------|-------|--------|--------|------|----------|-------|----------|----------|
| LOCATION | NO | | | 7,13 | | *** | 1 | 3 5 | (100m | | Longib | | | 6/061 | Copecity | ful flam |
| AREA No | MANHOLE | MANHOLE. | | (hecteres) | - | theethern I | | 11/11 | | | 3 | (an) | | | . 00.1 | |
| 59,41,42,60 | 39 | 14 | 110 | 10.69 | 510 | 10.69 | 3,95 | 18.60 | 2.27 | 1088 | 220. | 2 50 | 440. | 1.5 | 74.0 | / 50 |
| | | | | | | 2000 | 37. | 25 011 | 1111 | 1 23 | 7 2.7 | 00.0 | 770 | | 0 01 | 777 |
| 15,41,63,67,67 | 1/6 | 45 | 1636 | /// | 7 5 / 7 | 70.70 | | 45.75 | 1000 | 3 | | - 1 | 1 | . [| , | |
| • | | | | | | | | | | | | | | | | |
| | | | | | | ., | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| 301, 302, 303, 304, 305 | 55 | 53 | 1366 | 30.7 | | | | | | | | | | | | |
| 30.81 92.198 | | | 623 | 14.0 | 661 | 444 | 3.59 | 37.52 | 4.92 | 42.44 | 80 | 275 | come. | 0.15 | 30.8 | 0.00 |
| | | | | | | | | | | | | | | | | - |
| 77,78,79 | 53 | 21 | 102 | 229 | 2091 | 66.9% | 3.57 | 39 23 | 5.13 | 04.40 | 101 | 335 | Cont | 0.17 | 20.8 | 0.0 |
| | | | | | | | | | | | | | | | | |
| 73,74,75,76 | 51 | 6/2 | 1076 | 34.18 | 3/67 | 31.17 | 3.42 | 16.05 | 7.83 | 64.34 | 851 | 375 | CJMC. | 0,15 | 70.8 | 290 |
| | | | | | | | | 2 | | | | | | | | |
| 71,72,52 | 49 | 44 | 330 | 7.4 | 3446 | 78.57 | 3.39 | 62.23 | 90.0 | 70.91 | 63 | 375 | 3.5 | 0.15 | 722 | 062 |
| | | | | | | | | | | | | | | | | |
| , 69., 70, 573 | 47 | 4 | 51 | 4.78 | 3709 | 8835 | 236 | 65.46 | 211 | 7.65 | 155 | 335 | ליטיני | 0.17 | 2 55 | 0.67 |
| | | | | | | | | | | | | | | | | |
| AREAS SALT H ACE. | | | 5785 | 1100 | | | | | | | | | | | | |
| AAFA SOUTH COMM. | | | 4165 | 0.64 | | | | | | | | | | | | |
| | 345 | 45 | | | 9950 | 179 | 695 | 154.1 | 1967 | 178.89 | 620 | 000 | CONC | 010 | 202.55 | 820 |

q = Auruge daily per capting from $\{\Sigma_{k}^{*}\Sigma_{k}^{*}L,\ell$ esp. d.) I e dust of posts autonomous from $\{\Sigma_{k}^{*}L,\ell$ esc.) is a Postbag factor

dig o from population flow (L/3) 0(1)-from entroncour flow (L/3) 0(4)-from design flow (L/3)

offil + fath/El Where A = Ares in Mechanis 9(4) - 9(p) + 9(1) (L/8)

Molt 14 4+ pe.8 Where P . Pepulenes is 1000'8

(5/7) - 1 1 1 1 (1/2)

OLIVER, MANGIONE, MCALLA & ASSOCIATES LIMITED CONSULTING ENGINEERS 154 COLONNADE ROAD SOUTH, NEPENI, ONTARIO, KZE 7.15

Sanitary Sewer Design Sheet

22-5965 COMMUNEEY PROJECT: LONGE FEET 105

DATE: OCT DESIGNED BY:_ CHECKED BY:

PAGE 2 DE 9

DEVELOPER! -

ENGINEER: -

| | | | A COLO | I VIII C | CHAIN ATIVE | ATIVE | | Papulation | : | 1 | | PRO | PROPOSED | SEWER | ~ | |
|-------------------|------|-----|------------|--------------|--|------------|---------|------------|--|--------|-----|--------|----------|--------|----------|--------|
| LOCATION | NO | | NON! | Area Area | TOWN OF THE PROPERTY OF THE PR | Area | rected. | - 10 | ************************************** | 1 | | 15.5 | 1,11 | 67.040 | Capacoly | Ŀ |
| AREA No. | FROM | TO | Population | Checieres | Pasadation | (hactures) | 3 | 11/41 | 83 | 6.5 | | (E E E | - 1 | 3 | 1.0:0:0 | (m/ci) |
| SH - 14 HW | | | 7/0,5 | 1841 | | | | | | | | | | | | |
| - 47- 45 | 45 | | 5025 | 83.35 | | | | | | | | | | | İ | |
| 15 50 51 68 | 1/5 | 307 | 118 | 18 15 | 16,612 325,0 | 325.0 | 2.25 | 7882 | 3611 | 27165 | 430 | 600 | CONC | 018 | 9 | 0.8% |
| 42 85 , 12, 58 | 307 | 210 | 1133 | 25.48 | | 354.48 | 2.7/ | 252.04 | 38 99 | 291.04 | 270 | 563 | cone) | 0.12 | 303,69 | 0.75 |
| | | | | | | | | | 3 | | | | | | | |
| 1.2.3 | | | 901 | 2.40 | | | | | | | 155 | 250 | P. K.C. | 1.0 | 63.5 | 133 |
| 200, 1 commercias | | ۳ | 211 | 14.39 | 617 | 16.79 | 3.92 | 12.7 | 1.84 | 1454 | | | | | | |
| 4,5 | m | 4 | 134 | 3.90 | 549 | 65.19 | 3.91 | 13.25 | 2.77 | 16.02 | 135 | 250 | P.Y.C. | 0.7 | 67.0 | 127 |
| (9) | \n | R | 25 | 0.56 | 670 | 25.75 | 3.90 | (52) | 2 83 | 19.29 | 25 | 250 | 37.5 | 6.7 | 63.0 | 127 |
| 7,8,9,16,15 | 4 | 6 | 249 | 1685 | 14/18 | 42.58 | e in | 27.56 | 465 | 32.25 | 30 | 250 | PYC. | 0 0 | 5. P. Z | 0 95 |
| 10,11,17,18 | 6 | × | 878 | 15.02 | 1007 | 2860 | 8.5.8 | 37.75 | 11.9 | 48.86 | 06/ | 250 | P.VC. | 000 | 183 | 285 |
| 12.14 | " | 203 | 350 | 7.87 | 1354 | 63.47 | 5.5.2 | 43.66 | 6.98 | 50.67 | 205 | 350 | P.VC. | 730 | 30 55 | 0 78 |
| | 3 | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |

G(pl. Pest population flow (L/S)
G(1)-Pest attractors flow (L/S)
G(d)-Pest design flow (L/S)

Q(I) + [A (L/S) Where A + Ares is Macheres 0141 - 0(p) + 4(l) (L/1)

Mait 14 po. 8 Where F . Population is 1000's

060) + 19 H (1.75)

OLIVER, MANGIONE, MCCALLA & ASSOCIATES LIMITED CONSULTING ENGINEERS 154 COLOMNADE ROAD SOUTH. NEPEAN, ONTARIO KZE 7J5

Sanitary Sewer Design Sheet

87.5765 PROJECT: LOWFFEELDS COMMUNITY

DEVELOPER:-ENGINEER:

Och. 1991 800 DATE DESIGNED BY: CHECKED BY:

PAGE 3 OF 9

| | 14: | 46 | 0.67 | 69.0 | - ie | 9.76 | 2 | Z | |
|-------------|------------------------------|-------|-------------|-----------------|-------------|--------------|---------|------------|--|
| | - | 0 | 1 1 | 0 | 0,0 | 0.1 | 0 | LF. C | |
| _ | 20. | 39.2 | 0.7.0 | 7 7 2 | 2% | 55.3 | 2 / 40 | <u>(0)</u> | |
| SEWER | *** | 0.40 | 0.30 | 0.30 | 0.30 | 6.33 | 0 20 | 0.25 | |
| PROPOSED | 1 - 1 | PKC. | P.Y.C. | P.V.C. | D VC | 6 Y.C. | 62.006. | Cowe. | |
| PROP | ::[| 250 | 2 50 | 25.6 | 250 | 0 0 | 375 | 375 | |
| | 4 î | 250. | 0000 | 345 | 230 | \n. | 95 | 75% | |
| :: | | 1205 | 07.77 | 17.10 | 11.39 | 25.82 | 32.52 | 34:09 | |
| : | Pow Offi Offi (L/a) | | 17 | 00. | 61.1 | 2,62 2 | 3.22 | 37.78 | |
| 1 | | 15.20 | 00.00 | 15.35 | DIS, | 33.19 | 29.27 3 | 3/15 3 | |
| | , | 388 | 400 | 3.89 | 400 | 3.78 | 3.68 2 | 3 | |
| TIVE | | | 6.72 | 60.7/ | 0.8% | 26.02 | 1981 3 | 3400 5 | |
| CUMUL ATIVE | Population | 146 | 477 | 151 | 483 | 936 2 | 1445 | 1629 3 | |
| DITAI | | 16.77 | 12.0 | 58.9/ | 28.97 | 2.82 | 5.97 | 61% | |
| INDIVI | | 246 | 427 | / /5/ | 463 | 453 | 798 | 5 £ 8/ | |
| | TO | 209 | 211 | 215 | 3/ | 33 | 35 | 4/4 | |
| | MON | 15 | 6/ | и С. | 29 | 3/ | 3 3 | 35 | |
| | AREA No. | | 25,26,27,28 | £30,31,32,51,56 | 35,37,30,39 | 746 (44, 14 | Oh | нь. | |

9(i) - 1A(L/M) Where A - Ared in Mechanes 9(d) - 8(p) + 9(i) (L/B)

O(pl Pack papelation time (L/S) O(t) Pack entreasons time (L/S) O(d) Pack design from (L/S)

Most 14 4+ po. B Where P. Populetten is 1000's

O(p) - P1 M (1 / S)

Sanitary Sewer Design Sheet

PAGE 4 DE

| 18.87 | | | f.4 fine (m/e) | 1 | 0 . 3 | 0 65 | 66.0 | 2.27 | O LF | 0.49 | 0 20 | | |
|--|---|------------|-------------------------|-------------|----------------|-------------|---------|-------------|----------|--------|-------|---|--|
| 1,00 | N. S. | ~ | 11,11 | 34.0 | 3,5 | 01 8% | 39.2 | (c) | 34.5 | 439 | 43.9 | | |
| DATE: | CHECKED BY: | SEWER | 3,4 | 0 8 | C) | 790 | 2.0 | 2, | 0.7 | 0.30 | 0 2.2 | | |
| _ | CHECK | PROPOSED | <u>:</u> - : | PVC | PVC | DVC | PVC | pvc | pv.c. | PVC. | PVE | | |
| \$ | | PRO | įij | 255 | 250 | 03.0 | 25.2 | 25.5 | 250 | 21.3 | 2.2 | | |
| المد | 1.1 | | 416×43 (m) | 320. | 113 | 200 | | 129 | 200 | | | T | |
| 3965-68 | | | | 14.01 | 25.39 | echh | 9.3% | 19.95 | 30.3% | C 4 () | 70.7 | | |
| ; | | **** | | 65.7 | 325 | 5.27 | 0 4. | 8/.6 | 3.16 | 2 10 | 3,0 | | |
| COMMUNET | | Pagulatian | 4(4) | 15 61 | 26 35 | 39.56 | 9.36 | 12.27 | 22.08 | 2.93 | 3 58 | | |
| . 1 | | Prebling | Tector M | 3 93 | 3 22 | 3.57 | 4.02 | 3.83 | 330 | 422 | 61.7 | | |
| 76.5164 | | ATIVE | Area (hecteres) | 13.62 | 29.89 | 49.40 | 75.4 | 19.85 | 29.63 | 2.76 | 3.66 | | |
| PROJECT: LOWETE LE LOS | ER: | CUMULATIVE | Populotion | 909 | /330 | 2109 | 346 | 893 | /393 | 54 | 16.3 | | |
| PROJEC | DEVELOPER: ENGINEER: | INDIVIDUAL | Area A (hecieras) | 13.62 | 423/ | 12.51 | % % | 19.85 | 9.81 | 2.74 | 3.66 | | |
| : :: | | VIONI | Population | 909 | 725 | 779 | 396 | 883 | 210 | 17.3 | 163 | П | |
| « | | | TO TANKE | 601 | 105 | 410 | 219 | 6/6 | 5/2 | 5/2 | 2/1 | | |
| , McCALL | SOUTH. 7.15 | NO | FROM | 53 | 601 | 105 | 1 | 6/8 | 6/6 | 1 | 1 | | |
| OLIVER, MANGIONE, McCALLA & ASSOCIATES LIMITED | CONSULTING ENGINEERS 154 COLONNADE ROAD SOUTH NEPEAN, ONTARIO K2E 7JS | LOCATION | AREA No | £6 86 58 48 | 76 50 68 68 78 | 54,85,91,92 | 98,93 | 54,44,54,54 | 646, 846 | ė.S | 90. | | |
| | | | | | | | | | | | | | |

(8/7) (1)8.+ (4)8 + (8)0 O(d) - Peak population flow (L/S) O(l) - Peak antenness flow (L/S) D(d) - Peak design flow (L/S)

Q(I) + FA (L/R) Where A + Ares is Hechers

Mait id where P . Papulanes is 1000's

Oral + 21 M. 11 / 11

OLIVER, MANGIONE, McCALLA & ASSOCIATES LIMITED CONSULTING ENGINEERS 154 COLONNAGE ROAD SOUTH, NEFEAN, ONTARIO KZE 7J5

Sanitary Sewer Design Slieet

PROJECT: DAVE 050N NE CANTS RG-7257

DEVELOPER:-

DESIGNED BY: R.PP CHECKED BY:

PAGE 5. UL. 2.

| MOLENCO | 1 20 | | VIONI | /IDUAL | CUMULATIVE | ATIVE | Peables | Papulation | : | : | | PRO | PROPOSED | SEWER | | |
|------------------------------|---------|-----|-------|-----------|------------|------------|------------|------------|-------|-------------|--------|-------|----------|-------|----------|-----------|
| רססטו | | 4 | | | | Area | , sector ; | 3 | 110.0 | | Length | 1 | 17.00 | Grade | Capacity | Fud Blass |
| AREA No | MANHOLE | 3 | | (hectore) | | (hoctores) | | 16/21 | 11/11 | : : : | Ī | 1 | | 3 | , o | |
| /39 , /43 | 111 | //3 | 2116 | 5.52 | 246 | 5.52 | 11.4 | 15.31 | 10.0 | 5.92 | /30 · | 253 | PVC. | 0.40 | 352 | 0.77 |
| 5.7 | | | 3 | | | | | | | | | | | | | |
| hhl | //3 | 115 | 16.8 | 3.78 | 414 | 9.30 | 4.32 | 8.77 | 7.52 | 266 | 154 | 250 | pvc | 0.70 | 392 | 0.33 |
| | | | | | | | | | | | | | | | | |
| . SAI | 115 | 113 | 24 | 0.53 | 438 | 9.83 | 00% | 921 | 1.08 | 10.29 | 20 | 2 23 | DYC. | 0.70 | 334 | 0 22 |
| | | | | | | | | | | | | | | | | |
| 146,147 | 411 | 121 | 139 | 5./2 | 597 | 79.95 | 3.9€ | 11.94 | 1.42 | /3.36 | 157 | . 050 | PVC. | 0.00 | 352 | 660 |
| | | | 3 | | | | | | | | | | | | | |
| 140, 141, 142, 146, 149, 150 | 121 | 754 | 620 | 13.94 | | | | | | | | | | | | |
| 351,531 | | | 991 | 3.93 | 1363 | 30.62 | 74.5 | 26.53 | 3.17 | 29.95 | 240 | 300 | ダベム | 0.30 | 1.54 | 9 |
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q - Average dolly per captes from (2.5% L/cop.d.) I - that of peak antroacces from (2.4% L/coc) is recibing factor

Olds from population firm (1/3)
Olive population firm (1/3)
Olive property of the (1/3)
Olive property of the (1/3)

Q(I) • [A(L/3) Where A • Area in Nectores Q(4) • Q(p) + Q(I) (L/4)

Mait 14 po.6 Where P # Population is 1000's

060 - Pg H (1 / S)

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Sanitary Sewer Design Sheet

6326-65 HEIGHTS PROJECT: DAVEDSON

DEVELOPER:

Oct. 1991 RPP DESIGNED BY: CHECKED BY:

1.22 69.0 0.62 0 02 0.02 23.0 0.0 08.0 0 .. p.e.3 630 73.02 73.62 3 3 75.7 1.5% 1.8% 91.30 SEWER 0.30 0.30 0 . 0 70 0.14 500 0.0 \$ 0% 91.0 P.Y.C. D.V.C. P.V.C. P.V.C. cone. DVG. PROPOSED 13 1.6 1 1 1 Cove. 253 : : : 252 305 3.5 375 300 300 366 375 = 06/ 138 750 130 411 100 105 97 8 22.55 5.12 32.44 17.83 28.37 25.31 8022 51.80 28.9% Prek effenses (in (i./e) AS O 99.6 2.77 60.2 1.89 3.43 3.44 80.9 5.77 Papulahan Has O(p) (L/s) 5.05 73.54 15.94 22.5r 30.11 45.32 14:14 27.2 25.38 4/3 1 3.96 3.80 3, 74 3.08 3. 94 3.55 3.51 89.65 3.33 5.27 17.30 37:28 32.18 33.03 (heriteres) 25.19 55.23 49.42 CUMULATIVE Area Population 24739 233 1490 28€ 1001 2230 2434 55.23 4020 14/1 1411 ENGINEER Area 5.24 7.85 13.43 0.50 18:5 71.11 76.7 3.02 2.96 INDIVIDUAL 30.62 400 Population 1363 43 233 122 598 210 134 349 452 /32 178 TO MANHOLE 63 49 4 77 10 23 63 756 4 OLIVER, MANGIONE, MCCALLA & ASSOCIATES LIMITED CONSULTING ENGINEERS 194 COLONNADE ROAD SOUTH REFEAN, ONTARIO R2E 735 FROM 29 65 63 63 35 10 33 69 16 LOCATION FREM POSS (MILLEL MITS) 49 100 199 ARA NO ESTA 123. 112.113.114.115.114.119.12e AK75-375 107, 108, 109, 110 AREA No. 101, 102, 105 133,134, 135 100 (com) 150 444 103,104 111.451.161 101

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O(p) - Peak population flow (L/S) O(1) - Peak antroness flow (L/S) O(d) - Peak design flow (L/S)

Gill - TA (L/4) Where A + Aree In Hechica 0(4) + 0(b) + 0(l) (F/8)

Meit 14 peg Where P a Population to 1000's

Conc.

(6) + 13 1/2 (1 /5)

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Sanitary Sewer Design Sheet

DANTOSON HETERITS

DESIGNED BY: R "P CHECKED BY:

> DEVELOPER: ENGINEER:

OLIVER, MANGIONE, McCALLA & ASSOCIATES LIMITED CONSULTING ENGINEERS 134 COLOMNADE ROAD SOUTH. NEPEAN, ONTARIO KZE 7J5

| 10114001 | 100 | | AIDNI | IDUAL | CUMULATIVE | ATIVE | Position | Papulation | | :: | | PROF | POSED | PROPOSED SEWER | | |
|-----------------------|---------|--------------|------------|---------------|------------|--------------|----------|--|-------|---|-------|---------|-------|----------------|-------------------|----------|
| LOCAL | | | | | | | fector | | | 40,100 | | -0.0 | 1,111 | | Capacile ful flam | fut flor |
| AREA No. | FROM TO | TO SALANIA E | Papulation | A (h.c.le/es) | Pesulotten | A (hectares) | 1 | 67.1 | 9(1) | (3) | | 1 4 4 5 | | * | 4./.13 cm/41 | Cm/m3 |
| 127.129.137.138 | 22 | 95 | 377 | 6.43 | 4397 | 98.31 | 3.30 | 76.24 | 18.01 | 8.47 4397 98.31 3.30 76.24 10.81 67.06 290. 375 | . 064 | 335 | 1306. | 24.0 | 91.50 080 | 0 80 |
| | | | | | | | | | | | | | | | | |
| 128,136, 154 | 44 | 18 | 1/52 | 10.16 | 1845 | 108.48 | 3.65 | 81.80 | 11.53 | 10.11 1845 108.48 3.15 81.80 11.93 94.34 50 | 5.0 | 375 | 200) | 0.35 | 0.30 (030 088 | 0 88 |
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| MH-39-0 MHBI | 18 | 3484 58 | 5484 | 108.48 | | | | | | | | | | | | |
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| 1/30 1/3/1/132 1/35 | | | 15/5 | 11.57 | | | | | | | | | | | | |
| Consolar Tree last of | | | | 42.25 | | 42.25 | 3.20 | 42.85 3.20 70.4 464 7504 | 464 | 7504 | | | | | | |
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Offic Peek population list. [L/5] Offic Peak advances from [L/5] Offic Peak design flow [L/5]

Q(4) + Q(6) + Q(1) (L/4)

Oill + IA (L/8) Where A + Area in Hechera

Me it 14 4+ pe.8 Where P o Pepulation in 1000's

(5/1) - 13 1 (1/5)

Sanitary Sewer Design Sheet

67-5765 COMMUNITY PROJECT: LONG FILL DS

DEVELOPER:-

DESIGNED BY: 5P CHECKED BY:_

PAGE 6 DE. 2

Tel Box Telecity (m/e) 4.36 1.68 139 168 1.28 1.18 SEWER 7066 (L/0) 1011 126 2000 6.26.2 2066 ; ; 33: 7 , 14 1 3 CONE PROPOSED CONC <u>:::</u> conk CONC CONC Cauc 750 750 200 200 200 005 15.0 • 200 110 240 187 150 630.80 608.3 622.02 450.12 30% 350 Feet (5.73) 510,69 101.35 F1001 52759 103.21 543.23 /04.82 52.7 15 5. Population flow 0 (p) (L/s) 508.2 2876 5.8 Peable factor 2.67 6.63 1.33 2.31 3 6.3 43278 93833 132 Area A i 911 44 971.16. 42050 910 72 CUMULATIVE 477 414 10277 Pagalallen 16,41 44,517 C.76 44 759 ENGINEER: -Area A A (h. c) area l 1677 63.47 921.44 63 7 12355 35448 42,030 910.72 42527 921.44 63.71 4763 12.00 INDIVIDUAL 11/4 47.4 414 18,173 43E7 6.35% 21.19 16,13 12557 Paper 246 417 5017 751 123 TO statement 503 0/2 1 6/7 117 5/7 OLIVER, MANGIONE, MCCALLA & ASSOCIATES LIMITED CONSULTING ENGINEERS 154 COLONNADE ROAD SOUTH. NEPEAN, ONTARIO, KZE 7.15 TOHITTE NO. 113 103 5/2 203 27 1/7 LOCATION ENT BAKKNAYEN ELISS. SOKKHBYKU AXIST. BARRHAVKN CXINTING SAWEL 217 105-217 307 - 110 607 - 51 23.82 112-61 11-03 11-103

& Awrest delity per outlie flow (__L/cop.d.)
I'v that of pool antidoces flow (__L/coc)
iii v Pooliss (cotor

4(4) + 4(p) + 4(l) (L/4)

Olph Peak papaloiles flow (L/S) Olib Peak extrement flow (L/S) Oldb Peak design flow (L/S)

Q[I] a TA [L/T] Where A a Area to Hartwees

Mait 14 to po. | Where P a Population in 1000's

(5/7) - 14 1 (1/5)

OLIVER. MANGIONE, MCCALLA & ASSOCIATES LIMITED CONSULTING ENGINEERS

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Sanitary Sewer Design Sheet

87-5785 KINANCOCOOS PROJECT: LONG FINELD S

DEVELOPER:-ENGINEER:

1651 9 DATE: DESIGNED BY:_ CHECKED BY:

PAGE 9 0F 9

| 154 COLONNADE ROAD SOUTH, NEPEAN, ONTARIO K2E 7J5 | SOUTH. | | | DEVELOPER: — ENGINEER: — | | | | | | | 1.1 | | CHECKE | CHECKED BY: | | |
|---|--|------------|-------|-----------------------------|-----------------|---------------------|------|------------|--------------|------|-----|---------------------------------------|----------|-------------|--------------------------------|----------|
| | 140% | | INDIX | INDIVIDUAL | CUMULATIVE | ATIVE | | Pepulation | : | : | | PROF | PROPOSED | SEWER | | |
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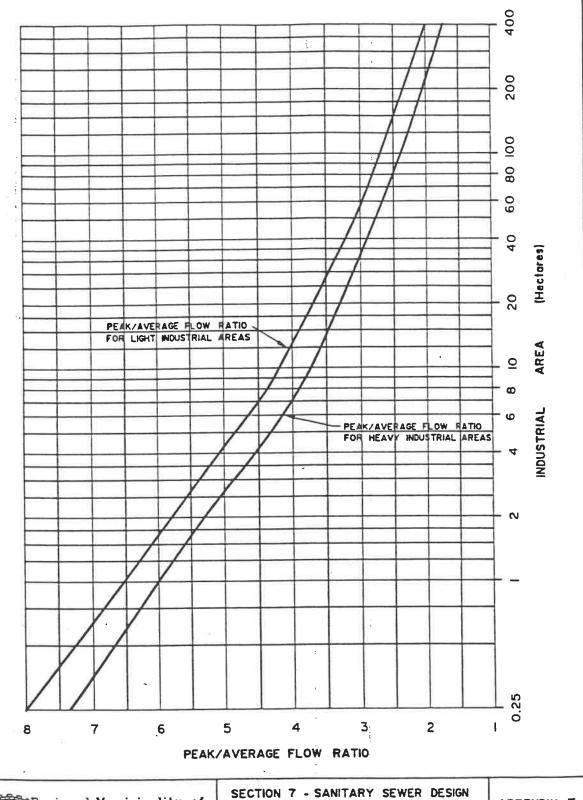
O(A-Pesh papaiotion flow (L/S) O(1)-Pesh defendent flow (L/S) O(A)-Pesh design flow (L/S)

qiil o fail./#1 Where A . Ares is Hecteres 4(4) - 4(b) + 4(l) (1./6)

Melt to per unere P o Population to 1000's

15/1) - 14 1 (L/S)

APPENDIX C INDUSTRIAL SEWAGE FLOW - PEAKING FACTORS





Regional Municipality of Ottawa - Carleton Environmental Services Department

DESIGN GUIDELINES

APPENDIX E

TYPICAL INDUSTRIAL SEWAGE

FLOW PEAKING FACTORS

Date: JUNE 1991

Rev.:

Figure:

1

APPENDIX D

CUT/FILL TABLES AND INFORMATION SHEETS FOR LOTS AND RIGHT-OF-WAY

South Merivale Business Park Cut Fill Analysis

Total Cut / 3446 390 340 527 527 298 245 220 220 -724 -724 匵 San/Stm 1076 -145 -145 -286 -547 -258 -125 -125 -246 -234 -233 -219 Ö <u></u> Cut Area Trench 5.82 5.82 5.80 5.77 5.67 5.04 4.99 4.99 4.87 4.42 4.42 **Trench** 3.30 3.30 3.30 3.30 3.40 3.10 3.10 2.96 2.96 2.96 2.64 Area **Trench** Width 85.16 85.26 85.26 85.26 85.59 85.59 85.62 85.73 85.76 Trench Base 0.00
86.22
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86.48 Stm 86.96 87.04 87.14 87.17 87.21 87.24 87.35 87.35 96.76 86.81 T/Stm Elev. San Trench 5.23 2.52 2.50 2.47 2.27 2.02 1.89 1.89 1.81 1.85 1.72 Area 28 22.12 25. **French** Width 84.26 84.69 84.69 85.02 85.20 85.18 85.18 85.33 85.50 Trench 82.31 82.24 82.24 82.08 82.00 81.92 81.96 81.66 81.66 81.28 81.28 81.28 81.28 81.28 81.28 81.28 81.36 81.28 81.36 81.36 81.36 81.36 81.36 81.36 81.36 81.36 81.36 81.36 83.82 84.19 Base San Cut/Fill Volume -245 -195 -390 20 -40 -120 -340 -490 -490 Average Cut / Fill -15.8 -15.8 -11.8 3.8 8.5 4.2 5.8 5.8 5.8 6.9 6.9 8.9 8.9 Delta E 0.02 -0.37 0.43 -0.37 0.81 = 14 m 89.10 89.27 89.27 89.21 89.21 89.26 89.21 89.46 89.31 89.46 89.51 89.67 89.69 89.76 89.76 90.19 90.21 Sub-bas 89.70 89.55 89.67 89.70 89.65 = 12 m88.49 88.36 88.74 88.62 89.11 Elev. Lane Width 90.50 90.45 90.50 90,35 90.47 Lane width 90.41 90.47 90.49 90.63 90.56 90.99 91.01 91.05 89.54 89.42 89.91 90.12 90.07 90.01 90.06 90.06 90.21 90.16 90.16 90.16 90.26 Finai 26 m 89.25 m 89.30 m 89.30 m 89.30 m 89.30 m 89.30 m 89.30 m 89.25 m 89.25 m 89.25 m 89.30 m 89.40 m 8 Existing 90.04 90.60 89.33 89.17 89.43 89.50 89.68 90.08 90.07 = 20 m Station R.O.W. 4525 4550 4275 4300 4350 4450 4500 4600 4250 R.O.W. 1000 1050 1150 1150 1250 1350 1450 1450 1550 1550 1550 1600 1700 1700 1850 1850 1850 1850 1850 June 12, 1992 Street

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JTF XI

| South | South Merivale Business Park Cut Fill Analysis | Business | Park | Cut Fill | Analysis | | | | | | | | | | | | | | |
|---------|--|---------------|------|-------------------|----------|---------|------------|----------|------------|------------|---|-------------|------------|--------|--------|--------|----------|------------------|-------------|
| June 1: | June 12, 1992 | | | | | | Average | Cut/Fill | Base | San | San | _ | - | Base | | Stm | | San/Stm | |
| Street | Station | Existing | | Final | Sub-bas | Delta E | Cut / Fill | Volume | San | Trench | - | | T/Stm | | Trench | Trench | Trench | Cut | Total Cut / |
| | | Elev. | | Elev. | Elev. | | Area | | Trench | Width | th Area | | Elev. T | French | Width | Area | Cut Area | Vol | ≣ |
| | 4800 | 90.61 | * | 90.65 | 89.85 | -0.51 | -5.8 | -390 | 87.06 | 1.00 | 0 1.73 | | 88.79 | 87.46 | 2.00 | 5.66 | 4.39 | | -380 |
| | 4850 | 90.64 | * | 90.50 | 89.70 | -0.69 | -9.8 | -390 | 86.91 | 1.00 | 0 1.79 | | 88.70 | 87.37 | 2.00 | 5.66 | 4.45 | -221 | -611 |
| | 4900 | 90.65 | * | 90.75 | 89.95 | -0.45 | -5.8 | -390 | 86.76 | 1.00 | 0 1.85 | | 88.61 | 87.28 | 2.00 | 5.66 | 4.51 | -224 | -614 |
| | 4950 | 90.52 | * | 90.50 | 89.70 | -0.57 | -7.8 | -340 | 86.58 | 1.00 | 0 1.97 | | 88.55 | 87.07 | 2.00 | 2.96 | 4.93 | -236 | -576 |
| | 5000 | 90.56 | # | 90.65 | 89.85 | -0.46 | -5.8 | -340 | 86.43 | 1.00 | 0 2.06 | | 88.49 | 87.01 | 2.00 | 2.96 | 5.02 | -249 | -589 |
| | 5025 | 09 06 | * | 90.52 | 89.72 | -0.63 | -7.8 | -170 | 92,66 | 1.00 | 0 2.56 | | 88.22 | 86.59 | 2.00 | 3.26 | 5.82 | -136 | -306 |
| | 5050 | 90.60 | # | 90.50 | 89.70 | -0.65 | 9.6 | -220 | 85.74 | 1.00 | 0 2.51 | | 88.25 | 86.62 | 2.00 | 3.26 | 5.77 | -145 | -365 |
| | 5075 | 90.58 | * | 90.40 | 89.60 | -0.73 | 9.6 | -245 | 85.81 | 1.00 | 0 2.47 | | 88.28 | 86.65 | 2.00 | 3.26 | 5.73 | -144 | -389 |
| | 5100 | 90.65 | * | 90.65 | 89.85 | -0.55 | -7.8 | -220 | 85.89 | 1.00 | | | 88.31 | 89.98 | 5.00 | 3.26 | 5.68 | -143 | -363 |
| | 5150 | 90.56 | * | 90.50 | 89.70 | -0.61 | -7.8 | -390 | 86.07 | 1.00 | 0 2.28 | | 88.35 | 86.80 | 2.00 | 3.10 | 5.38 | -277 | -667 |
| | 5250 | 90.59 | * | 90.70 | 89.90 | -0.44 | 8.6 | -580 | 86.39 | 1.00 | 0 2.12 | | 88.51 | 87.04 | 2.00 | 2.94 | 5.06 | -522 | -1102 |
| | 5300 | 90.60 | 40 | 90.65 | 89.85 | -0.50 | 5,8 | -240 | 86.47 | 1.00 | 0 2.10 | | 88.57 | 87.10 | 2.00 | 2.94 | 5.04 | -253 | -493 |
| | 5325 | 90 66 | # | 80.67 | 89.87 | -0.54 | -5.8 | -145 | 86.65 | 1.00 | 1.95 | | 88.60 | 87.28 | 2.00 | 2.64 | 4.59 | -120 | -265 |
| | 5400 | 90.64 | # | 90.65 | 89.85 | -0.54 | -5.8 | 435 | 86.88 | 1.00 | 1.85 | | 88.73 | 87.41 | 2.00 | 2.64 | 4.49 | -341 | -776 |
| | 5425 | 90.56 | N. | 90.76 | 89.96 | -0.35 | -3.8 | -120 | 86.97 | 1.00 | 0 1.83 | | 88.80 | 87,48 | 5.00 | 2.64 | 4.47 | -112 | -232 |
| | 5450 | 90.46 | * | 90.88 | 90.08 | -0.13 | 2.2 | -50 | 87.04 | 1.00 | 0 1.80 | | 88.84 | 87.52 | 2.00 | 2.64 | 4.44 | Ŧ | -131 |
| | 5525 | 90.41 | | 90.79 | 89.99 | -0.42 | -3.8 | 09- | 87.27 | 1.00 | 1.71 | | 88.98 | 87.65 | 2.00 | 5.66 | 4.37 | -330 | -390 |
| | 5550 | 90.30 | * | 90.60 | 89.80 | -0,25 | -1.8 | -70 | 0.00 | ** 0.00 | 00.00 | | 00.0 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | į |
| t | | | | | | | Subtotal | -10010 | | | | | | | | | | | |
| O | R.O.W. = 20 m | | Lan | Lane Width = 12 m | : 12 m | | | | | | | | | | | | | | |
| | 0006 | 89.46 | | 89.49 | 69.88 | -0.77 | -11.8 | | | | | | | | | | , | ; | i |
| | 9040 | 90.00 | , | 89.64 | . 88.84 | -1.16 | -19.8 | -632 | Detailed d | esign to I | Detailed design to be completed in future. | d in futur | 69 | | | | 4.00 | & | -712 |
| | 9110 | 90.05 | | 89.64 | 88.84 | -1.21 | -19.8 | -1386 | Trench Cu | ıt areas a | Trench Cut areas assumed similar to other stations. | ilar to oth | ner statio | ns. | | | 4.00 | -280 | -1666 |
| | 9150 | 90.02 | | 89.44 | 88.64 | -1.41 | -23.8 | -872 | | | | | | | | | 9.00 | 091- | -1032 |
| | 9220 | 90.07 | | 89.79 | 88.99 | -1.08 | -17.8 | -1456 | | | | | | | | | 6.00 | 087 | -1736 |
| | 9270 | 20.05 | | 89.59 | 88.79 | -1.28 | -21.8 | 066- | | | | | | | | | 4.00 | 500 | 0811- |
| 9.0 | 9340 | 90.10 | | 89.94 | 89.14 | -0.96 | -15.8 | -1316 | | | | | | | | | 4.00 | 092- | 0801- |
| | 9380 | 90.20 | | 89.74 | 88.94 | -1.26 | -21.8 | -752 | | | | | | | | | 4.00 | 091 - | -912 |
| | 9420 | 90.20 | | 90.09 | 89.29 | -0.91 | -13.8 | -1246 | | | | | | | | | 4.00 | -580 | -1526 |
| | 9200 | 90.45 | | 89.94 | 89.14 | -1.31 | -21.8 | -890 | ~ | | | | | | | | 4.00 | -500 | -1090 |
| | | | | | | | Subtotal | -9540 | | | | | | | | | | | |
| ۵ | R.O.W. | R.O.W. = 20 m | Lan | Lane Width | = 12 m | | | | | | | | | | ; | C | | | |
| | 7000 | 89.50 | | 89.95 | 89.15 | -0.35 | -3.8 | | 84.75 | 7. | | | 87.54 | 85.54 | 5.00 | 4.00 | 6.79 | | |
| | 7025 | 89.66 | | 90,25 | 89.45 | -0.21 | 0.2 | -45 | 84.83 | 7. | 1.00 2.73 | | 87,56 | 85.56 | 5.00 | 4.00 | 6.73 | 69L- | 412- |
| | | | | | | | | | | | | | | | | | | | |

-cutherland

| |) to () to () | lotal Cut / | E. | -238 | -336 | -460 | -1109 | -1638 | -442 | -364 | -422 | -433 | -435 | -967 | -483 | -483 | | | 1000 | 523 | 1305 | | | | | -57 | -147 | 127 | 252 | 759 | 357 | 314 | 692 | 840 | 1391 | 683 |
|---------------|-----------------|-----------------|----------|-------|-------|-------|-------|-------|-------|---------|-------|---------|-------|----------|-------|---------|----------|-------------------|-------|-------|-------|----------|-----|------------|--------|----------|-------|-------|-------|-------|-------|--------------|-------|-------|-------|-------|
| Can/Stm | • | | Vol | -168 | -166 | -165 | -319 | -453 | -147 | -119 | -127 | -163 | -190 | -427 | -213 | -213 | | | 7,10 | 2/1- | -379 | | | | | -56 | -207 | -103 | -103 | -201 | -98 | . | -168 | -170 | -276 | 404 |
| | } | Trenich | Cut Area | 6.67 | 6.63 | 6.57 | 6.17 | 5.90 | 5.85 | 3.70 | 6.46 | 6.61 | 8.56 | 8.51 | 8.51 | 8.51 | | 2 47 | 7 | 3.41 | 3,29 | | 9.7 | | 4.13 | 4.13 | 4.13 | 4.13 | 4.13 | 3.93 | 3.83 | 3.36 | 3.37 | 3.44 | 3.91 | |
| Š | | Trench | Area | 4.00 | 4.00 | 4.00 | 3.70 | 3.70 | 3.70 | 3.70 | 3.70 | 3.70 | 2.70 | 5.70 | 5.70 | 5.70 | | 90 | 96.1 | 1.96 | 1.96 | | | | 1.96 | 1.96 | 1.96 | 1.96 | 1.96 | 1.96 | 1.96 | 1.96 | 1.96 | 1.96 | 2.24 | |
| | | Trench | Width | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2:00 | 5.00 | 5.00 | 5.00 | 2.00 | | 5 | 2.00 | 2.00 | 5.00 | | | | 5.00 | 5.00 | 5.00 | 5.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | |
| Ċ | Dase | Stm | Trench | 85.58 | 85.60 | 85.62 | 85.85 | 85.99 | 86.02 | 96.05 | 86.13 | 86.17 | 85.20 | 85.23 | 85.26 | 85.29 | | 03 44 | 11.70 | 87.20 | 87.39 | | | | 85.55 | 85.56 | 85.65 | 85.69 | 85.73 | 85.84 | 82.88 | 87.28 | 87.19 | 87.06 | 96.86 | |
| | į | T/Stm | Elev. | 87.58 | 87.60 | 87.62 | 87.70 | 87.84 | 87.87 | 87.90 | 84.98 | 88.02 | 88.05 | 88.08 | 88.11 | 88.14 | | 9 | 80.03 | 88.18 | 88.37 | | | | 86,53 | 86.54 | 86.63 | 86.67 | 86.71 | 86.82 | 96.86 | 88:26 | 88.17 | 88.04 | 87.98 | |
| • | San | Trench | Area | 2.67 | 2.63 | 2.57 | 2.47 | 2.20 | 2.15 | 0.00 | 2.76 | 2.91 | 2.86 | 2.81 | 2.81 | 2.81 | | i | 1.51 | 1.45 | 1.33 | | | | 2.17 | 2.17 | 2.17 | 2.17 | 2.17 | 1.97 | 1.97 | 1.40 | 1.41 | 1.48 | 1.67 | |
| (| San | Trench | Width | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 99. | 1.00 | 1.00 | | | | 1,00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1,00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| | Base | San | rench | 34.91 | 34.97 | 35.05 | 35.23 | 35.64 | 35,72 | ** 00.0 | 35.22 | 35.11 | 35.19 | 35.27 | 35.30 | 85.33 | | ; | 86.58 | 86.73 | 87.04 | | | | 84.36 | 84.37 | 84.46 | 84.50 | 84.54 | 84.85 | 84.89 | 96.86 | 96.76 | 86.56 | 86.31 | |
| | | | <u></u> | -70 | | | | | | | -295 | | | | | _ | -4985 | | | | 1684 | 3079 | | | | <u>ئ</u> | 09 | 230 | 355 | 096 | 455 | 405 | 860 | 1010 | 1666 | |
| | | Cut / Fill / | Area | 5.8 | -7.8 | -15.8 | -15.8 | -15.8 | -7.8 | -11.8 | 1.8 | -9.8 | -9.8 | -11.8 | 8.0- | -11.8 | Subtotal | 5 | 30.5 | 25.3 | 4.5 | Subtotal | | | -5.8 | -3.8 | 6.2 | 12.2 | 16.2 | 22.2 | 14.2 | 18.2 | 16.2 | 24.2 | 20.2 | ! |
| | | | | -0.46 | -0.60 | 1.04 | -1.03 | -0.95 | -0.62 | -0.84 | -0.78 | -0.72 | 0.70 | -0.78 | -0.70 | -0.78 | | | 0.81 | 0.55 | -0.17 | | | | -0.53 | -0.44 | 0.13 | 0.42 | 0.61 | 0.86 | 0.47 | 0.65 | 0.57 | 0.99 | 0.76 | |
| i | | Sub-bas Delta E | Elev. | 89.42 | 89.29 | 89.40 | 89.36 | 89.44 | 89.59 | 89.48 | 89.52 | 89.64 | 89.51 | 89 68 | 89.60 | 89.57 | | = 11 m | 89.66 | 89.57 | 89.04 | | | = 12 m | 89.32 | 89.11 | 89.68 | 89.56 | 89.63 | 89,75 | 89.68 | 89.81 | 89.79 | 90.12 | 89.89 | 1 |
| | | Final | E S | 90.22 | 80 08 | 90.20 | 90.16 | 90.24 | 60.39 | t 90.28 | 00.20 | P 00 44 | 10031 | \$ 90 4B | 90.40 | * 90.37 | | Lane Width = 11 m | 90.46 | 90.37 | 89.84 | * | | Lane Width | 90.12 | 89.91 | 90.48 | 90.36 | 90.43 | 90.55 | 90.48 | 90.61 | 90,59 | 90,92 | 62 06 | 1 |
| | | Existing | Flev | 89.88 | 89.89 | 90.44 | 80.39 | 80.39 | 90.00 | 90.57 | 90.57 | 90.61 | 00 4R | 2 12 00 | 90.55 | 90.60 | | | 88.85 | 89.02 | 89.21 | | | 20 m | 89.85 | 89.55 | 89.55 | 89.14 | 89.02 | 88.89 | 89.21 | 89.16 | 89.22 | 89.13 | 89 23 | 5 |
| 2, 1992 | | Station | | 7050 | 7075 | 2100 | 7150 | 7225 | 7250 | 7075 | 7300 | 7305 | 7950 | 200 | 7425 | 7450 | | R.O.W. = | 8000 | 8050 | 8163 | 121 | | R.O.W. = | 3093.6 | 3100 | 3150 | 3175 | 3200 | 3250 | 3275 | 3300 | 3350 | 3400 | 3475 |) |
| June 12, 1992 | | Street | | | | | | | | | | | | | | | | ш | | | | | | 14. | | | | | | | | | | | | |

| Analysis | |
|-------------|----------|
| 置 | |
| Park Cut | |
| Business Pa | |
| Aerivale 1 | 1992 |
| South N | June 12, |
| | |

| | Fotal Cut / | į | Ξ . | 1015 | 442 | 235 | 200 | 609 | 200 | | 96 | | 2 | 203 | 2 | -18148 | | |
|---------------|-----------------------|-----------|------------|---------|-------|-------|-------|-------|--------|------------------|-------|-------|-------|-------|-------|---------|----------|-------|
| San/Stm | Cut | | | | | | | | | | | | | | | | | |
| | Trench | , | Cut Area | 4.13 | 4.57 | 9 6 | 00.0 | 5.17 | . E 93 | 33.0 | 5.32 | | 5.42 | 5 + 2 | 31.0 | | | |
| Stm | Trench | | Area | 2.24 | 260 | 9 6 | 2.80 | 2.86 | 700 | 7.0 4 | 2.86 | i | 2.86 | 30 0 | 00.7 | | | |
| | Trench | | Width | 2.00 | 900 | F.00 | 5.00 | 2.00 | 0 | 2.00 | 000 | 3 | 5.00 | 5 | 2.00 | | | |
| Base | Stm | | Trench | 86.63 | 06 90 | 00,00 | 86.22 | 86.12 | 100 | 80.00 | 85.01 | | 85.76 | 100 | 80.31 | | | |
| | T/Stm | | Elev. | 87.75 | 07.60 | 00.70 | 87.65 | 87,55 | | 87.47 | 07.94 | 5.60 | 87.19 | | 86.74 | | | |
| San | Trench | | Area | 1.89 | 7 | /B: 1 | 2.14 | 2.31 | | 2.38 | 0 46 | 4.4 | 2.56 | | 2.26 | | | |
| Gan | Trench | | Width | 1 00 | 00: | 1.00 | 1.00 | 1 00 | | 9. | 5 | 3. | 1.00 | | 1.00 | | | |
| Baco | San | 3 | Trench | 85.86 | 2 1 | 85.71 | 85.51 | 85.24 | 1 | 85.09 | 000 | 84.88 | R4 63 | | 84.48 | | | |
|) in (| Volume | A CIGILIE | | 1420 | 1450 | 099 | 355 | odo | 000 | 460 | | 360 | 300 | 3 | 09 | | 07011 | 80 |
| V. Carolina | Avelage Out / FIII | = - H | Area | 1 C Y + | 4. | 12.2 | 16.2 | 0 0 | 10.5 | 8.2 | ! ! | 6.2 | 4.0 | į | -1.8 | 1.4.4.0 | Subtotal | Total |
| | 1 4 C | Della C | | | | | | | | | | | | | | | | |
| | 1.0 | Spo-one | Ž | 3 6 | 2.00 | 89.61 | R9 67 | 70.00 | 40.00 | 89 45 | 2 | 89.50 | 04.00 | 24.50 | 89.16 | | | |
| | i | rinai | ü | בופאי | 7C'08 | 90.41 | On 47 | 100 | 90.34 | 90.25 | 9 | 90.30 | 0 | 30.22 | 89.96 | | | |
| | | Existing | | Elev. | 89.32 | 89.21 | 80.05 | 09:00 | 89.21 | 80.08 | 03.50 | 89.39 | 77 | 69.41 | 89.48 | | | |
| , 1992 | ; | Station | | | 3625 | 3675 | 0020 | 3 | 3775 | 3006 | 2063 | 3875 | . 1 | 3920 | 4000 | | | |
| June 12, 1992 | į | Street | | | | | | | | | | | | | | | | |

* Existing Elevation Less assumed 0.25 m Layer of Topsoil ** No Storm or Sanitary Sewer Between this and previous Statton.

| | | | June 11, 1992 | | | |
|----------|----------------|---------------------|--------------------|----------------------------------|-----------------------|--|
| Street | Lot | Average Existing | Final Average | Average Cut / Fill Depth,m | Lot Area ha (d) | Volume Cut / Fill (c) * (d) *10000 |
| 13 | | Elevation,m (a) | Elevation,m (b) | =-(a-b+0.6) | (-) | m3 |
| : | | \ - / | 4-7 | (c) | | |
| A : | A0 * | 89.53 | 89.96 | 0.08 | : 0.74 | 592 |
| ^ | A1 * | 89.46 | 90.11 | 0.30 | 0.93 | 2790 |
| | A2 * | 89.49 | 90.33 | 0.49 | 1.47 | 7203 |
| | A3 * | 89.45 | 90.18 | 0.38 | 0.77 | 2926 |
| • | A4 * | 89.43 | 90.39 | 0.61 | 1.06 | 6466 |
| : | A5 | 89.38 | 90.25 | 0.27 | 0.88 | 2376 |
| | A6 | 89.27 | 90.45 | 0.58 | 0.84 | 4872 |
| | A7 | 89.37 | 90.31 | 0.34 | 0.91 | 3094 |
| | A8 | 89.28 | 90.51 | 0.63 | 1.16 | 7308 3330 |
| - | A9 | 89.41 | 90.38 | 0.37 | .: 0.90 1.25 | 9500 |
| | A10 | 89.23 | 90.59 | 0.76 | 1.03 | 3605 |
| | A11 | 89.66 | 90.61 | 0.35 0.08 | 1.26 | 1008 |
| | A12 | 89.41 | 90.09 | 0.41 | 1.33 | 5453 |
| | A13 * | 90.10 | 90.86 90.84 | 0.61 | 1.44 | 8784 |
| | A14 * | 89.88 90.07 | 91.19 | 0.77 | 1.13 | 8701 |
| | A15 * A16 * | 90.25 | 91.13 | 0.53 | 1.39 | 7367 |
| | VIO | 50.25 | 31.10 | 0.00 | | |
| В | В0 | 89.64 | 89.93 | -0.31 | 0.86 | -2666 |
| | B1 | 89.63 | 89.49 | -0.74 | 0.77 | -5698 |
| | B2 | 89.80 | 89.80 | -0.60 | 0.67 | -4020 |
| | B3 | 89.67 | 89.78 | -0.49 | 0.60 | -2940 |
| | 84 | 89.69 | 90.06 | -0.23 | 0.72 | -1656 |
| | B5 | 89.79 | 90.14 | -0.25 | 0.86 | -2150 |
| | 86 | 89.81 | 90.36 | -0.05 | 0.82 | -410 |
| | B7 | 89.58 | 90.35 | 0.17 | 1.27 | 2159 |
| | B8 * | 90.09 | 90.60 | 0.15 | 1.04 | 1664 |
| | B9 * | 89.86 | 90.50 | 0.29 | 1.03 | 2987 |
| | B10 * | 90.45 | 90.61 | -0.19 | 1.02 | -1938 364 |
| | 811 * | 90.48 | 90.87 | 0.04 | 0.91 | -2662 |
| | B12 * | 90.61 | 90.74 | -0.22 | 1.21 0.78 | -2730 |
| | B13 * | 90.60 | 90.60 | -0.35 -0.30 | 1.31 | -3930 |
| | B14 * | 90.59 | 90.64 | -0.50 | 1.28 | -6400 |
| | B15 * | 90.65 | 90.50 90.68 | -0.27 | 1.22 | -3294 |
| | 816 * 817 * | 90.60 90.58 | 90.65 | -0.28 | 1.30 | -3640 |
| | 818 * | 90.58 | 90.64 | -0.29 | 1.14 | -3306 |
| | B19 * | 90.57 | 90.66 | -0.26 | 1.21 | -3146 |
| | B20 * | 90.58 | 90.66 | -0.27 | 1.07 | -2889 |
| | B21 * | 90.61 | 90.74 | -0.22 | 1.05 | -2310 |
| | B22 * | 90.63 | 90.71 | -0.27 | 0.99 | -2673 |
| | B23 * | 90.67 | 90.78 | -0.24 | 0.99 | -2376 |
| | B24 * | 90.38 | 90.75 | 0.02 | 1.56 | 312 |
| | B25 * | 90.64 | 90.82 | -0.17 | 0.91 | -1547 |
| | B26 * | 90.49 | 90.75 | -0.09 | 0.94 | -846 |
| | | | | | 0.76 | -6156 |
| C | C1 | 90.15 | 89.94 | -0.81 | 0.76 | -4982 |
| | C2 | 89.90 | 89.97 | -0.53 | 0.94 | -7280 |
| | C3 | 90.20 | 90.00 | -0.80 -0.48 | 0.95 | -4560 |
| | C4 | 89.95 | 90.07 90,16 | -0.59 | 1.08 | -6372 |
| | C5 * C6 * | 90.40 90.00 | 90.25 | -0.10 | 1.04 | -1040 |
| | C7 * | 90.40 | 90.23 | -0.52 | 1.08 | -5616 |
| | C8 * | 90.40 | 90.32 | -0.43 | 0.83 | -3569 |
| | | 30.70 | | | ti . | |
| D | D1 * | 90.23 | 90.44 | -0.14 | 0.70 | -98 0 |
| - | D2 | 90.17 | 90.19 | -0.58 | 0.76 | -4408 |
| 63 | D3 * | 90.51 | 90.53 | -0.33 | 1.22 | -4026 |
| | D4 * | 90.38 | 90.36 | -0.37 | 0.75 | -2775 |
| | D5 * | 90.48 | 90.45 | -0.38 | 1.18 | -4484 |
| | | • | | - | 0.00 | 49498 |
| E | E1 | 88.99 | 90.93 | 1.34 | 0.98 | 13132 |
| F | F1 | 88.94 | 90.59 | 1.05 | 1.23 | 12915 |
| | F2 | 89.21 | 90.78 | 0.97 | 0.82 | 7954 |

LOTCUT2.XLS

| | | | | June 11, 1992 | | | |
|--------|-----|-------|---|--|---|-----------------------|---|
| Street | Lot | | Average Existing Elevation,m (a) | Final Average Elevation,m (b) | Average Cut / Fili Depth,m =-(a-b+0.6) | Lot Area ha (d) | Volume Curt / Fill (c) * (d) *10000 m3 |
| | | | 2: | | (c) | | |
| | | F3 | 89.05 | 90.63 | 0.98 | 0.99 | 9702 |
| | | F4 | 89.17 | 90.85 | 1.08 | 1.14 | 12312 |
| | | F5 : | 89.30 | 90.81 | 0.91 | 0.85 | 7735 |
| | | F6 | 89.23 | 90.90 | 1.07 | 1.09 | 11663 |
| | | F7 = | 89.36 | 90.75 | 0.79 | 0.82 | 6478 |
| | | FB | 89.25 | 90.80 | 0.95 | 1.03 | 9785 |
| | | F9 | 89.30 | 90.68 | 0.78 | 1.13 | 8814 |
| | 1 | F10 | 89.27 | 90.74 | 0.87 | 1.11 | 9657 |
| | | F11 | 89.26 | 90.47 | 0.61 | 0.96 | 5856 |
| | | F12 * | 89.46 | 90.15 | 0.34 | 1.26 | 4284 |
| | | | | | Total | 71.63 | 93673 |

Additional 0.25 m fill added for 0.25 m topsoil stripping.
 c = - (a - b + 0.6 - 0.25)
 Negative volume indicates cut.
 Positive volume indicates fill.

Note:

Cross-Section Cut Fill Analysis

| Area of Cut/Fill for Varying Depths of Cover. H | II for Varving | Depths of C | Sover. H | | | | | | | | | | | | |
|---|----------------|-------------|-----------|------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| # # # | 26 m | Ÿ | Row g = | * * o c | | | | | | | | | | | |
| | | | I | | | | | | | | | | | | |
| | T | | -0.9 | | -0.8 | | -0.7 | | 9.0- | | -0.5 | | 4.0 | | 6.0 |
| • | Elevation Dis | Distance | Elevation | Distance | | | | | | | | | | | |
| a subbase | 99.00 | 0.00 | 99.10 | 0.00 | 99.20 | 0.00 | 99.30 | 0.00 | 99.40 | 0.00 | 99.50 | 0.00 | 99.60 | 0.00 | 99.70 |
| į . | 98 78 | 2.00 | 98.89 | 7.00 | 98.99 | 7.00 | 99.09 | 7.00 | 99.19 | 7.00 | 99.29 | 7.00 | 99.39 | 2.00 | 99.49 |
| 2 (| 99.59 | 2.00 | 69'66 | 7.00 | 99.79 | 7.00 | 99.89 | 7.00 | 99.99 | 7.00 | 100.09 | 7.00 | 100.19 | 7.00 | 100.29 |
| י כ | 99.71 | 13.00 | 99.81 | 13.00 | 99.91 | 13.00 | 100.01 | 13.00 | 100.11 | 13.00 | 100.21 | 13.00 | 100.31 | 13.00 | 100.41 |
| 5 4 | 100.001 | 13.00 | 100.00 | 13.00 | 100.00 | 13.00 | 100.00 | 13.00 | 100.00 | 13.00 | 100.00 | 13.00 | 100.00 | 13.00 | 100.00 |
| f evicting | 00 001 | 000 | 100.00 | 0.00 | 100.00 | 0.00 | 100.00 | 0.00 | 100.00 | 0.00 | 100.00 | 0.00 | 100.00 | 0.00 | 100.00 |
| Fillions 1 | 100 00 | -13.00 | 100.00 | -13.00 | 100.00 | -13.00 | 100.00 | -13.00 | 100.00 | -13.00 | 100.00 | -13.00 | 100,00 | -13.00 | 100.00 |
| ב כ | 99.71 | -13 00 | 99.81 | -13.00 | 99.91 | -13.00 | 100.01 | -13.00 | 100.11 | -13.00 | 100.21 | -13.00 | 100.31 | -13.00 | 100.41 |
| - | 00 50 | 2002 | 69.66 | | 99.78 | -7.00 | 99.83 | -7.00 | 99.99 | -7.00 | 100.09 | -7.00 | 100.19 | -7.00 | 100.29 |
| | 98.79 | -7.00 | 98.89 | -7.00 | 98.99 | -7.00 | 99.09 | -7.00 | 99.19 | -7.00 | 99.29 | -7.00 | 99.39 | -7.00 | 99.49 |
| Area,m2 | -19.67 | | -17.07 | | -14.47 | | -11.87 | | -9.27 | | -6.67 | | -4.07 | | -1.47 |

| 9.0 | 100.60 | 100.39 | 101.19 | 101.31 | 100.00 | 100.00 | 100.00 | 101.31 | 101.19 | 100.39 | 21.93 |
|-----------------|--------|--------|--------|--------|---------|--------|--------|--------|--------|--------|-------|
| | 0.00 | 7.00 | 7.00 | 13.00 | 13.00 | 0.00 | -13.00 | -13.00 | -7.00 | -7.00 | |
| 0.5 | 100.50 | 100.29 | 101.09 | 101.21 | 100.00 | 100.00 | 100.00 | 101.21 | 101.09 | 100.29 | 19.33 |
| | 0.00 | 7.00 | 7.00 | 13.00 | 13.00 | 00.0 | -13.00 | -13.00 | -7.00 | -7.00 | |
| 0.4 | 100.40 | 100.19 | 100.99 | 101.11 | 100.00 | 100.00 | 100.00 | 101.11 | 100.99 | 100.19 | 16.73 |
| | 0.00 | 7.00 | 7.00 | 13.00 | 13.00 | 0.00 | -13.00 | -13.00 | -7.00 | -7.00 | |
| 0.3 | 100.30 | 100.09 | 100.89 | 101.01 | 100.00 | 100.00 | 100.00 | 101.01 | 100.89 | 100.09 | 14.13 |
| | 00'0 | 7.00 | 7.00 | 13.00 | 13.00 | 00.0 | -13.00 | -13.00 | -7.00 | -7,00 | |
| 0.5 | 100.20 | 99.99 | 100.79 | 100.91 | 100.00 | 100.00 | 100.00 | 100.91 | 100.79 | 99.99 | 11.53 |
| | 0.00 | 7.00 | 7.00 | 13.00 | 13.00 | 00.0 | -13.00 | -13.00 | -7.00 | -7.00 | |
| 0.1 | 100.10 | 99.89 | 100.69 | 100.81 | 100.00 | 100.00 | 100.00 | 100.81 | 100.69 | 99.89 | 8.93 |
| | 0.00 | 2,00 | 7.00 | 13.00 | 13.00 | 0.00 | -13.00 | -13.00 | -7.00 | -7.00 | |
| 0 | 100.00 | 99.79 | 100.59 | 100.71 | 100.00 | 100.00 | 100.00 | 100.71 | 100,59 | 99.79 | 6.33 |
| | 00'0 | 2.00 | 2.00 | 13.00 | 13.00 | 0.00 | -13.00 | -13.00 | -7.00 | -7.00 | |
| 0 .1 | 99.90 | 69 66 | 100.49 | 100.61 | 100 00 | 100.00 | 100.00 | 10001 | 100.49 | 99.69 | 3.73 |
| | 0.00 | 7.00 | 7.00 | 13.00 | 13.00 | 000 | -13 00 | -13.00 | -7.00 | -7.00 | |
| 0.2 | 99.80 | 99.59 | 100.39 | 100.51 | 100 001 | 100.00 | 100 00 | 100.51 | 100.39 | 99.59 | 1.13 |
| | 000 | 202 | 2 00 | 13.00 | 00.61 | 000 | 19.00 | 13.00 | 2002- | -7.00 | |

| | | | | | | | | | | _ | |
|-----|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|
| | 0.00 | 7.00 | 7.00 | 13.00 | 13.00 | 0.00 | -13.00 | -13.00 | -7.00 | -7.00 | |
| - | 101.00 | 100.79 | 101.59 | 101.71 | 100.00 | 100.00 | 100.00 | 101.71 | 101,59 | 100.79 | 32.33 |
| | 0.00 | 7.00 | 7.00 | 13.00 | 13.00 | 00'0 | -13.00 | -13.00 | -7.00 | -7.00 | |
| 0.9 | 100.90 | 100.69 | 101.49 | 101.61 | 100.00 | 100.00 | 100.00 | 101.61 | 101.49 | 100.69 | 29.73 |
| | 0.00 | 7.00 | 7.00 | 13.00 | 13.00 | 0.00 | -13.00 | -13.00 | -7.00 | -7.00 | ١ |
| 0.8 | 100.80 | 100.59 | 101.39 | 101.51 | 100.00 | 100.00 | 100.00 | 101.51 | 101.39 | 100.59 | 27.13 |
| • | 0.00 | 7.00 | 7.00 | 13.00 | 13.00 | 0.00 | -13.00 | -13.00 | -7.00 | -7.00 | |
| 0.7 | 100.70 | 100.49 | 101.29 | 101.41 | 100.00 | 100.00 | 100.00 | 101.41 | 101.29 | 100.49 | 24,53 |
| | 0.00 | 2.00 | 7.00 | 13.00 | 13.00 | 0.00 | -13.00 | -13.00 | -7,00 | -7.00 | |

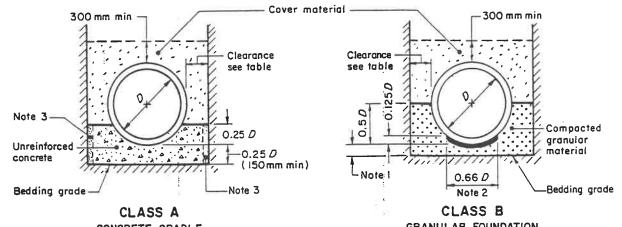
Cross-Section Cut Fill Analysis

| | 6.3 | 1.70 | 32 | 00. | 0 0 1 | 100.40 100.32 99.52 | -1.80 |
|--|---------|-------------------------|----------------|-----------------|----------------|---------------------------|-------------------|
| | ' | | | • | | | • |
| | | 0.00 | 6.00 | 10.00 | 0.00 -10.00 | -10.00 | |
| | 0.4 | 99.60 | 100:22 | 100.00 | 100.00 | 100.30 | 3.80 |
| | | 0.00 | 6.00 | 10.00 | -10.00 | -10.00 -6.00 | 00.0 |
| | -0.5 | 99.50 | 100.12 | 100.00 | 100.00 | 100.20 | 5.80 |
| | | 0.00 | 0.00 | 10.00 | 0.00 | -10.00 | 90.6 |
| | 9.0- | 99.40 | 100.02 | 100.00 | 100.00 | 100.10 | 7.80 |
| | | 0.00 | 0.00 | 10.00 | 0.00 | -10.00 | .6 .00 |
| | -0.7 | 99.30 | 99.92 | 100.00 | 100.00 | 100.00 | 99.12 -9.80 |
| | | 0.00 | 0.00 | 10.00 | 0.00 | -10.00 | -6.00 |
| | 6.0 | 99.20 | 99.02 | 99.90 100.00 | 100.00 | 99.90 99.82 | 99.02 |
| & 4 % % | | 0.00 0.00 | 6.00 6.00 | 10.00 10.00 | 0.00 | -10.00 | 9.00 |
| er, H Road s = ROW g = | 6.0 | 9.10 | 96.92 99.72 | 99.80 100.00 | 100.00 | 99.80 99.72 | 98.92 |
| Area of Cut/Fill for Varying Depths of Cover, H L= 12 m Road R= 20 m ROW | | nce Elevation 0.00 § | 6.00 6.00 | 10.00 | 0.00 | -10.00 | -6.00 |
| Varying Der 12 m 20 m | 77 | on Distance 99.00 0 | 98.82 99.62 | 99.70 | 00.00 | 99.70 99.62 | 98.82 -15.80 |
| t/FIII for \ | i | Elevati | •. | ~ ~ | · # # | , == - * | |
| Area of Cuty L= R= | | a, subbase | o 0 | 5 0 | f, existing | n = | j Area,m2 |

| 9.0 | 100.60 | 100.42 | 101.22 | 101.30 | 100.00 | 100.00 | 100.00 | 101.30 | 101.22 | 100.42 | 16.20 |
|------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|
| | 0.00 | 9.00 | 9.00 | 10.00 | 10.00 | 0.00 | -10.00 | -10.00 | -6.00 | -6.00 | |
| 0.5 | 100.50 | 100.32 | 101.12 | 101.20 | 100.00 | 100.00 | 100.00 | 101.20 | 101.12 | 100.32 | 14.20 |
| | 0.00 | 9.00 | 00'9 | 10.00 | 10.00 | 0.00 | -10.00 | -10.00 | -6.00 | -6.00 | |
| 0.4 | 100.40 | 100.22 | 101.02 | 101.10 | 100.00 | 100.00 | 100.00 | 101.10 | 101.02 | 100.22 | 12.20 |
| | 0.00 | 00.9 | 00.9 | 10.00 | 10.00 | 0.00 | -10.00 | -10.00 | 9.00 | -6.00 | |
| 0.3 | 100,30 | 100.12 | 100.92 | 101.00 | 100.00 | 100.00 | 100.00 | 101.00 | 100.92 | 100.12 | 10.20 |
| | 0.00 | 6.00 | 9.00 | 10.00 | 10.00 | 0.00 | -10.00 | -10.00 | -6.00 | -6.00 | |
| 0.2 | 100.20 | 100.02 | 100.82 | 100.90 | 100.00 | 100.00 | 100.00 | 100.90 | 100.82 | 100.02 | 8.20 |
| | 0.00 | 9.00 | 00.9 | 10.00 | 10.00 | 00.0 | -10.00 | -10,00 | -6.00 | 9.00 | |
| 0.1 | 100.10 | 99.95 | 100.72 | 100.80 | 100.00 | 100.00 | 100.00 | 100.80 | 100.72 | 99.95 | 6.20 |
| | 0.00 | 00.9 | 9.00 | 10.00 | 10.00 | 0.00 | -10.00 | -10.00 | -6.00 | -6.00 | |
| 0 | 100,00 | 99.82 | 100.62 | 100.70 | 100.00 | 100.00 | 100.00 | 100.70 | 100.62 | 99.82 | 4.20 |
| | 0.00 | 00.9 | 00.9 | 10.00 | 10.00 | 00.0 | -10.00 | -10.00 | 900 | 9.00 | |
| -0.1 | 99.90 | 99.72 | 100.52 | 100.60 | 100.00 | 100.00 | 100 00 | 100 60 | 100.52 | 99.72 | 2.20 |
| | 000 | 909 | 900 | 10.00 | 10.00 | 000 | -10 00 | 10.00 | 909 | 9.00 | |
| -0.2 | 99 80 | 99.62 | 100 42 | 100.50 | 100.00 | 100 00 | 100.00 | 100.50 | 100.42 | 99.62 | 0.20 |
| | 0 | 90.8 | 800 | 10.00 | 10.00 | 000 | 10.00 | 00.01 | 00.01 | 9.00 | |

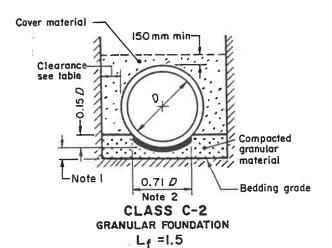
| | | | | | | | · | · | · · · 6.00 | | _ |
|-----|--------|--------|--------|--------|--------|--------|--------|--------|------------|--------|-------|
| • | 101.00 | 100.82 | 101.62 | 101.70 | 100.00 | 100.00 | 100.00 | 101.70 | 101.62 | 100.82 | 24.20 |
| | 0.00 | 9.00 | 6.00 | 10.00 | 10.00 | 0.00 | -10.00 | -10.00 | -6.00 | -6.00 | |
| 6.0 | 100.90 | 100.72 | 101.52 | 101.60 | 100.00 | 100.00 | 100.00 | 101.60 | 101.52 | 100.72 | 22.20 |
| | 00.0 | 9.00 | 9.00 | 10.00 | 10.00 | 0.00 | -10,00 | -10.00 | -6.00 | -6.00 | |
| 0.0 | 100.80 | 100.62 | 101.42 | 101.50 | 100,00 | 100.00 | 100.00 | 101.50 | 101.42 | 100.62 | 20.20 |
| | 0.00 | 00.9 | 9'00 | 10.00 | 10.00 | 0.00 | -10.00 | -10.00 | -6.00 | -6.00 | |
| 7.0 | 100.70 | 100.52 | 101.32 | 101.40 | 100.00 | 100.00 | 100.00 | 101.40 | 101.32 | 100.52 | 18.20 |

0.00 6.00 10.00 10.00 -10.00 -10.00 -6.00



CONCRETE CRADLE $L_f = 2.8$

GRANULAR FOUNDATION Lf = 1.9



NOTES:

- I The min dimension shall be 0.15 D or 150 mm whichever is the greater except in an unyielding foundation the min dimension shall be 0.25 D or 300 mm whichever is the lesser.
- 2 The pipe bed is to be carefully shaped to receive the bottom of the pipe.
- 3 In rock excavation provide a 50 mm layer of compressible material between the trench walls and concrete cradle.
- A This standard to be applied in stable conditions or after trench has been brought to stable conditions.
- B Where the trench is sheathed, the clearance is the distance between the inside face of sheathing and the pipe.

| Pipe Inside diameter (mm) | Clearance (mm) |
|-----------------------------------|--------------------|
| 900 or less | 300 |
| Over 900 | 500 |

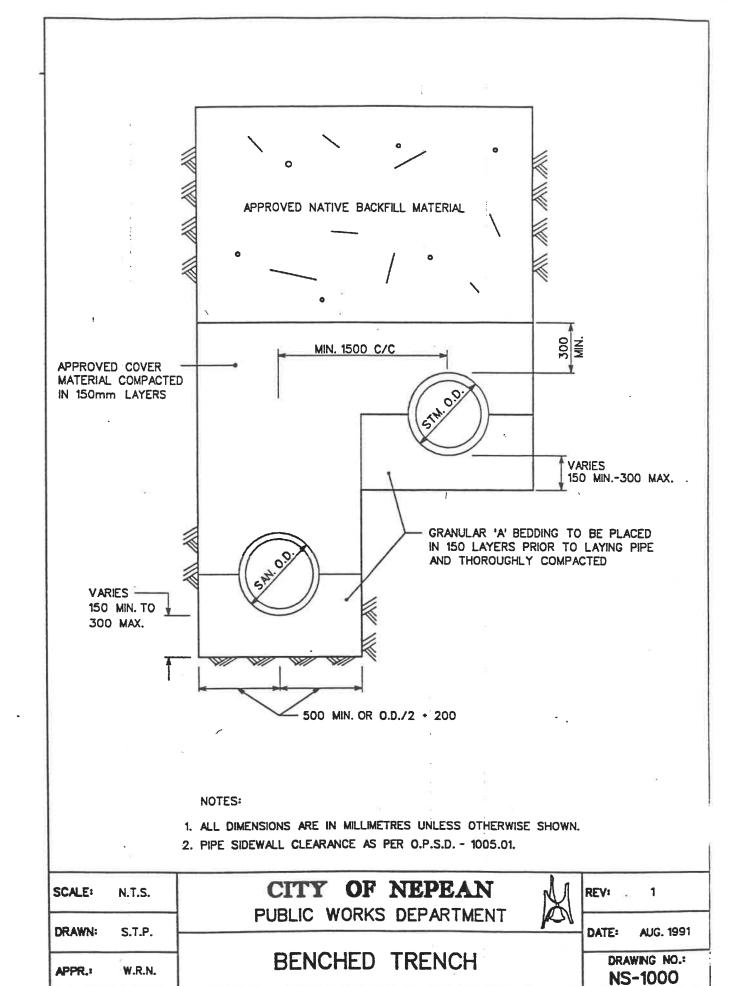
LEGEND:

Lf = Load factor

D = Inside diameter

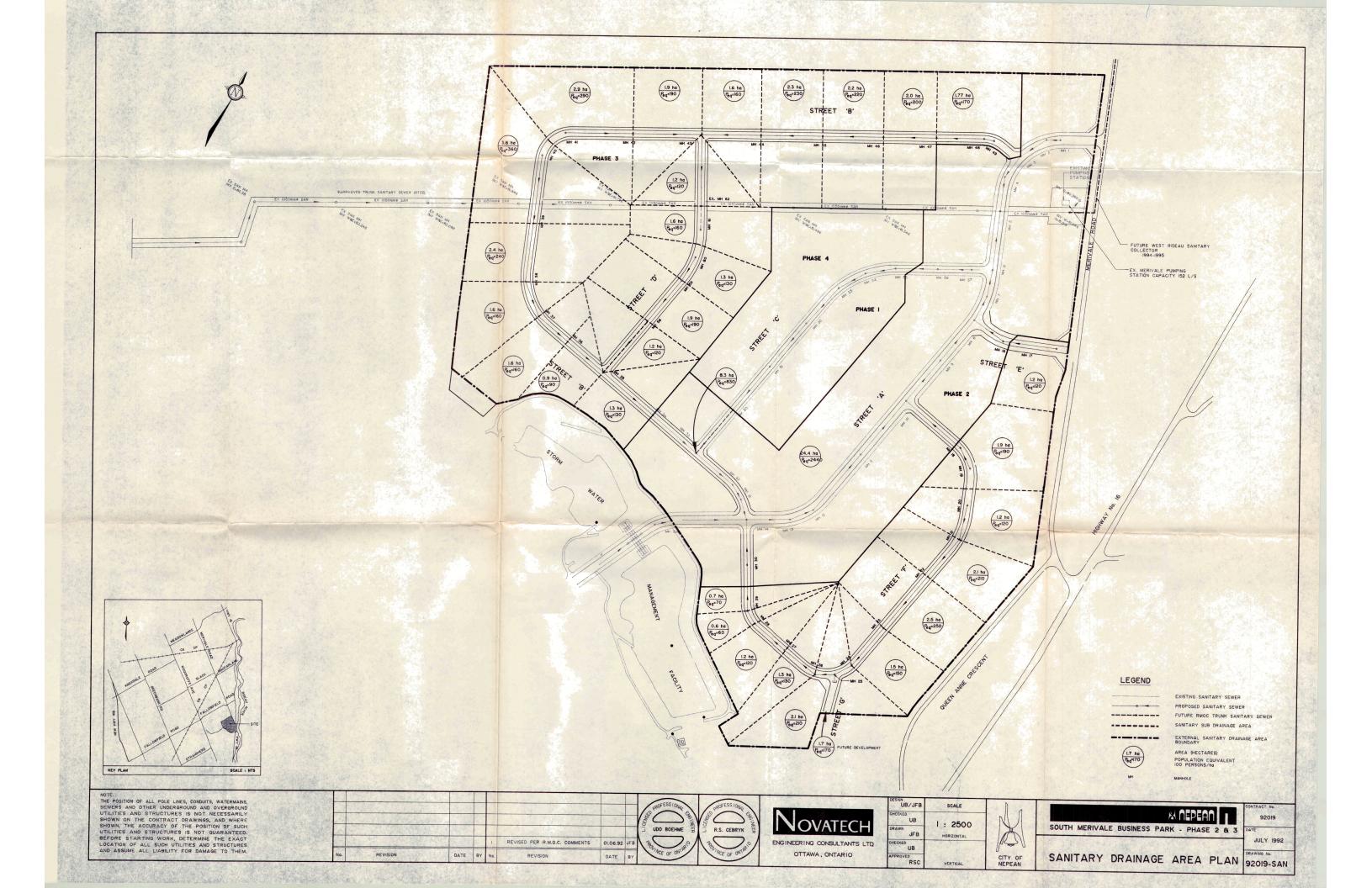
- C Lf = The load factor used for the calculation of the bedding class.
- D Backfill according to OPSD-803.04.
- E All dimensions are in millimetres unless otherwise shown.

| ONTARIO PROVINCIAL STANDARD DRAWING | Date | 1989 05 01 | Rev | 2 | | | |
|---|--------------|------------|-----|---|--|--|--|
| TRENCH BEDDING FOR SANITARY SEWERS UP TO 1800mm Dia | Date | | | | | | |
| | OPSD-1005.01 | | | | | | |

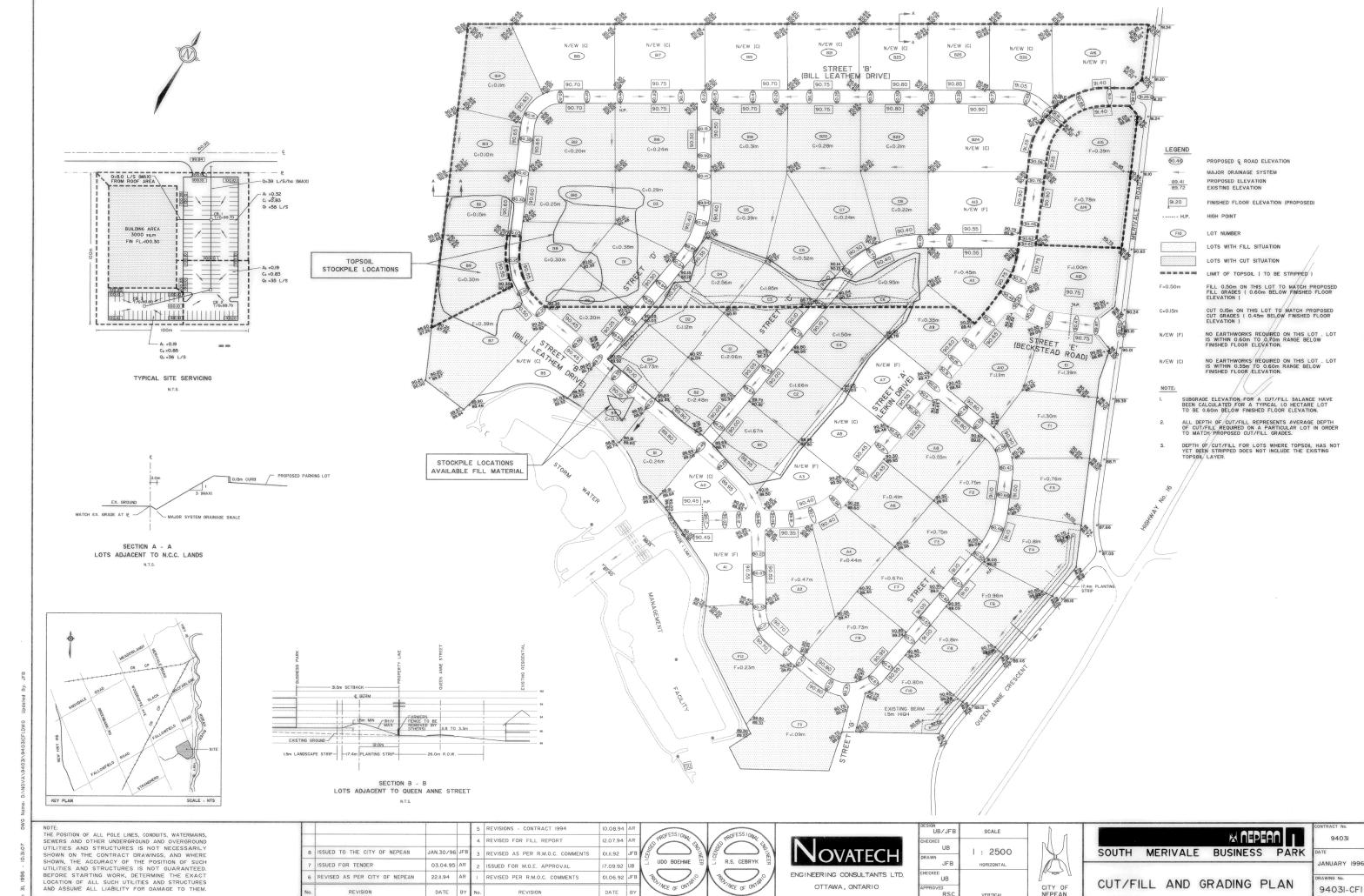


APPENDIX E

SANITARY DRAINAGE AREA PLAN

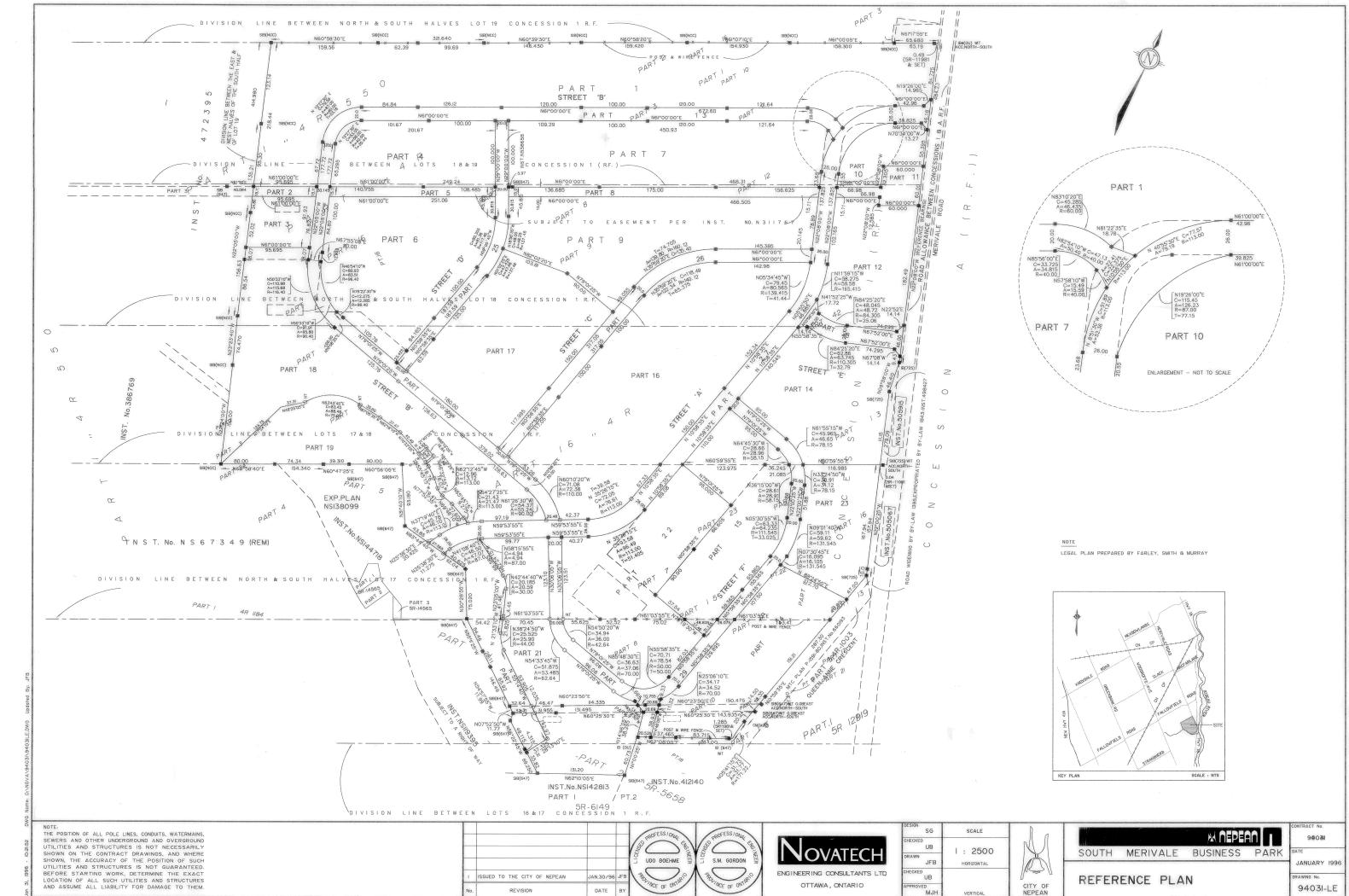


APPENDIX F SMBP ENGINEERING DRAWINGS

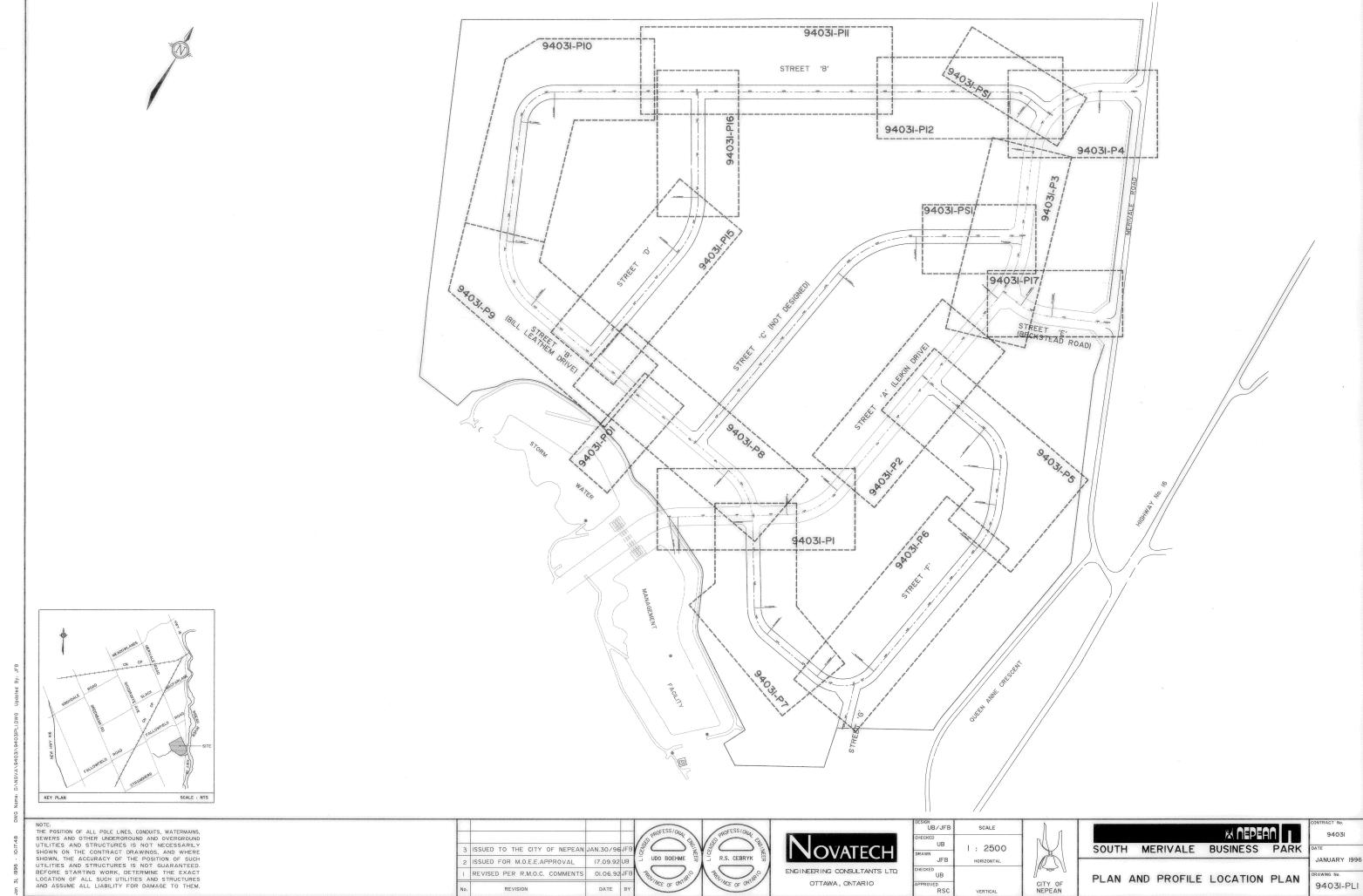


DATE

DATE



9403I-LE



REVISED PER R.M.O.C. COMMENTS

REVISION

01.06.92JF

DATE BY

UB

RSC

CITY OF NEPEAN

OTTAWA, ONTARIO

PLAN AND PROFILE LOCATION PLAN

9403I-PLI

