



J.F. Sabourin and Associates Inc.  
52 Springbrook Drive,  
Ottawa, ON K2S 1B9  
T 613-836-3884 F 613-836-0332

jfsa.com

Ottawa, ON  
Paris, ON  
Gatineau, QC  
Montréal, QC  
Québec, QC

June 09, 2023

Project Number: P2226

David Schaeffer Engineering Limited  
120 Iber Road, Unit 103  
Stittsville, ON  
K2S 1E9

**Attention:** Adam Fobert, P.Eng.

**Subject:** The Drummond (The Ridge Phase 3/4):  
Low Impact Development (LID) Design

---

## Introduction

As a part of the detailed design of the Drummond (The Ridge Phase 3/4) subdivision, located in Barrhaven within the City of Ottawa, J.F. Sabourin and Associates Inc. (JFSA) were commissioned to complete an in-depth analysis of the proposed Low Impact Development (LID) measures within the site to assess/ensure that the site's infiltration targets will be met under post-development condition. The detailed study area consists of **19.06 ha**, which includes **17.33 ha** of residential lands and **1.73 ha** of park. Note that lands external to the site, such as the Ridge Phase 1 & 2 have not been considered in this LID analysis, refer to JFSAs July 29, 2020, memo titled The Ridge (Brazeau) Low Impact Development (LID) Design for full LID/water budget details of that site. A detailed PCSWMM hydrologic/hydraulic model was developed to replicate the proposed development's water budget using historical rainfall data. The following memo outlines the proposed development's water budget and the aquifer recharge benefits that the proposed LIDs will provide.

## Site Infiltration Targets

As a part of the Master Servicing Study Barrhaven South Urban Expansion Area report completed by J.L. Richards in May 2018, it was determined that pre-development aquifer recharge within the study area accounted for **40%** of the overall sites water budget. The City and RVCA determined that pre-development aquifer recharge levels should be maintained under post-development conditions and that the infiltration should be provided across the development and not simply concentrated in one or two locations. The City and RVCA determined that the preferred infiltration servicing strategy for this area would be Etobicoke Exfiltration Systems (EES) and that these systems should be limited only to local roads and their respective catchments, with the intent to prohibit any infiltration of roadway runoff from either collector or arterial roads due to the salting practices applied at those locations.

## Etobicoke Exfiltration System (EES) Design

Within the Drummond development, there will be a total of **27** EESs implemented, to meet the aquifer recharge requirements outlined above. The EES units will be installed underneath storm sewers within the right-of-way (ROW) in specific areas as determined by David Schaeffer Engineering (DSEL) as a part of the development's detailed design. Each system will consist of one **250 mm** diameter perforated pipe surrounded by a **0.85 m** deep by **1.20 m** wide clear stone trench. Detailed drawings of the proposed EES units are provided in **Figure 1A**. The location and extent of each EES are indicated in **Figure 2**. **Figure 3** outlines the total drainage area to each of the units and the respective runoff coefficients.

Based on the areas provided in **Figure 3** the LID units (EES abd CB trenches) will service a total drainage area of **16.83 ha** (88% of the total development), with **9.75 ha** of area treated by LID that drainas to the Ridge Pond and **7.08 ha** treated by LID that drains to the Clarke Pond . Note that the application of EESs throughout the development is limited due to the presence of collector roads running through the southern extent and middle (north-south) of the development, although EESs have been implemented at all other practical locations within the site. **Table A1 to A3 in Attachment A** provides a full summary of the design parameters for each EES. Note that there are no LID measures proposed on private property (residential rear yards) or within the parklands.

### Catch Basin Exfiltration Trench (CB Trench) Design

Also within the Drummond development, there will be a total of **8** Catch Basin Exfiltration Trenches, to meet the aquifer recharge requirements outlined above. These CB trenches will capture runoff from the local street and rear yards that drain to each CB, like conventional CB, but will also be equipped with a perforated pipe/exfiltration trench system connected near the sump of the CB that will allow runoff captured by the CB to flow to an exfiltration trench, where it can exfiltrate back into the ground. The ICD/lead pipe for each CB will be set above the top of this trench ensuring that all the storage volume within the trench will need to be used before any runoff is conveyed to the minor system. All of these trenches will be **1.2m** wide, **40m** long and **0.4m** deep, filled with clear stone and equipped with a **250 mm** perforated sub-drain pipe throughout the length of the trench. Detailed drawings of the proposed CB trenches have been provided in **Figure 1B**. The location and extent of each CB trench are indicated in **Figure 2**. **Figure 3** outlines the total drainage area to each of the units and the respective runoff coefficients. **Table A1 to A3 in Attachment A** provides a full summary of the design parameters for each CB exfiltration Trench. Again note that there are no LID measures proposed on private property (residential rear yards) or within the parklands.

### Modelling Approach

The model used for this water budget analysis builds on the existing detailed PCSWMM model of the Drummond/Ridge development, which was created as a part of the stormwater management analysis. All components of this model remain unaltered, such as subcatchment parameters, SWM pond configuration, catch basins and the major and minor systems, with the only exception being the removal of the upstream portion of the model (Ridge development) which has no bearing on the water budget for the Drummond site, and significantly reduces model simulation run times.

The storage provided by each of the EESs and CB trenches has been represented in the model as storage nodes, with appropriate depth/area curves assigned to each LID based on the detailed design parameters. A porosity of **0.4** has been assumed for all LIDs, and as all units will contain a perforated PVC pipe to help disperse the runoff throughout the entire system, the storage volume provided by these pipes has also been accounted for in the LID storage volume curves.

The soil infiltration rate for the site, determined by Paterson Group (see below), was reduced by a factor of safety of **2.5** as per the guidance from Credit Valley and Toronto and Region Conservation Authorities on Low Impact Development. A specific outlet curve (depth/flow relationship) was developed for each LID, based on its respective geometry. Note that this analysis only considered infiltration through the bottom of the LID, resulting in a conservative estimate for the total infiltration benefits provided by each LID, as it is expected that runoff captured by the LID will be able to exfiltrate through the sides of the trench. The total flow through each outlet curve was then used to determine the total aquifer recharge provided by each LID.

The proposed EESs were connected to their respective maintenance holes in the model through an orifice of **250 mm** with a discharge coefficient of **0.82** (short pipe) to reflect any restriction that the proposed perforated pipe could have on conveying flow from the maintenance hole to the EES. Each perforated pipe has been reviewed for the more frequent events to ensure that the pipe inlet is not obstructing flows from getting into the system. Note that all EESs are named after the maintenance hole that they are connected to.

The proposed CB trenches are connected to their respective maintenance hole in the model through an orifice reflective of the proposed ICD to be implemented at each location, as mentioned above these orifices are set above the top of the trench to ensure the full storage volume of the trench is utilized before spilling to the minor system.

### **Soil Infiltration Rate**

Paterson Group conducted soil infiltration testing within the vicinity of the proposed LID measures, which determined a soil infiltration rate of **50 mm/hr** for the Drummond site. Email correspondence indicating the infiltration rate obtained by Paterson for the subject site has been included in **Attachment A**. For the subcatchments within the development, default Hortons infiltration values have been applied as per the City of Ottawa Sewer Design Guidelines (2012).

### **Evaporation & Evapotranspiration Parameters**

To ensure that the depression storage within the model subcatchments can regenerate after the first rainfall event, monthly evaporation rates have been applied. The Master Servicing Study provided no documentation on the surface evaporation rates used in that analysis, and as such monthly evaporation rates applied in this model are as per those specified in the City of Ottawa's PCSWMM Carp River model documentation. A summary of these monthly values can be found in **Attachment A Table A4**. To ensure that evapotranspiration is appropriately accounted for in the continuous simulation water budget, the groundwater routine within the model's hydrologic algorithm has been activated. Groundwater parameters have been applied as specified for type A soils in the J L Richards Master Servicing Study. Excerpts from this report regarding the groundwater parameters have been provided in **Attachment A**.

### **EES Drawdown Times**

As indicated above, all EES units will have a maximum depth of **850 mm** with an assumed porosity of **0.4**. Based on the site soil infiltration rate of **50 mm/hr**, determined by Paterson in the field, and assuming only bottom infiltration, this equates to a full EES having a drawdown time of approximately **6 hours**. Applying a safety factor of **2.5** to the site infiltration rate, the draw downtime is **17 hours**, with both values being substantially less than the 24 - 48-hour maximum drawdown times generally permitted.

### **CB Trench Drawdown Times**

As indicated above, all CB trench units will have a maximum depth of **400 mm** with an assumed porosity of **0.4**. Based on the site soil infiltration rate of **50 mm/hr**, determined by Paterson in the field, and assuming only bottom infiltration, this equates to a full CB trench having a drawdown time of approximately **3.2 hours**. Applying a safety factor of 2.5 to the site infiltration rate, the draw downtime is **8 hours**, with both values being substantially less than the 24 - 48-hour maximum drawdown times generally permitted.

## Continuous Simulations

The detailed PCSWMM model was run for **39** years, from 1967 to 2007, using hourly rainfall data from Environment Canada's Ottawa International Airport station. Note that there was no data available for the years 2001 and 2005 in this data set. The hourly rainfall data used in this analysis is a heavily reviewed and vetted product sold by Environment Canada, and only includes rainfall data and does not include any snowfall that occurred during this window.

**Table B1 in Attachment B** provides a full summary of the rainfall data used in this analysis. From this rainfall data, it is seen that the average yearly simulated rainfall for this window is **552.0 mm**. As specified by the Master Servicing Study, the proposed development should infiltrate **40%** of the annual runoff. As the hourly rainfall data used in this simulation does not extend the full year, the infiltration target for this analysis has been assumed to be **40%** of the average simulated rainfall volume (**552.0 mm**), which is calculated to be **220.8 mm or 42,090 m<sup>3</sup>** based on the **19.06 ha** study area.

## Simulation Results

Error! Reference source not found. outlines the average simulated infiltration volumes for each of the proposed LIDs contained within the development, as per the model simulations from 1967 - 2007. From this analysis, it was found that on average all LIDs will infiltrate **26,949 m<sup>3</sup> / 141.4 mm** per year, based on the simulated window. The total annual infiltration volumes for each LID have been provided in **Tables B2 in Attachment B**. Also provided in **Attachment B** are full summaries of the surface runoff, surface infiltration and groundwater evapotranspiration for each of the subcatchments within the model for each simulated year. Note that the surface infiltration volumes have not been considered as "truly infiltrated" in this water budget analysis, as these volumes are simply an indicator of the rainfall volume that is passed to the groundwater module. This volume will then either evapotranspire or infiltrate into the groundwater aquifer, based on the program's groundwater algorithms, the volume that is considered to return to the groundwater aquifer per the modelling results is considered as infiltrated.

**Table 1** below outlines that the proposed LIDs within the development will on average infiltrate **26,949 m<sup>3</sup> / 141.4 mm** per year (**25.8%** of the total precipitation) for the **19.06 ha** area serviced by the LID units. **Table 2** outlines the water budget breakdown of the development based on the 39 years of simulations, this includes evaporation (wetting losses), evapotranspiration, infiltration, and runoff from the various components within the development. From this analysis, it is seen that the pervious surfaces within the development will infiltrate **19,810 m<sup>3</sup> / 103.9 mm** (**17.8%** of the total precipitation) for the full development area of **19.06 ha**. Adding the average infiltration volumes provided by the EESs and pervious surfaces results in the average total infiltration for the site of **46,759 m<sup>3</sup> / 245.3 mm** (**43.5%** of the total precipitation). This exceeds the **40%** infiltration requirement set out by the Master Servicing study by **3.5%** (**4,668 m<sup>3</sup> / 24.5 mm**). Based on the continuous simulations using **39** years of historical rainfall data it was determined that the proposed water budget for the Drummond subdivision would be **20%** surface runoff, **36.4%** evaporation and **43.5%** infiltration.

**Table 1: The Drummond Development - LID  
Average Infiltration Values**

EES ID	Average Annual Infiltration (m³)
MH-502	1,672
MH-503	551
MH-504	1,506
MH-508	745
MH-509	84
MH-510	144
MH-511	1,618
MH-513	1,526
MH-517	1,504
MH-520	599
MH-521	21
MH-522	705
MH-524	1,272
MH-5240	862
MH-525	668
MH-534	1,426
MH-547	862
MH-548	336
MH-549	226
MH-550	1,001
MH-551	771
MH-553	1,847
MH-556	799
MH-557	626
MH-558	187
MH-560	968
MH-565	1,461
CB-109	428
CB-111	366
CB-116	397
CB-12	350
CB-126	352
CB-16	430
CB-4	332
CB-94	307
<b>Average (m³)</b>	770
<b>Total (m³)</b>	26,949
<b>Average* (mm)</b>	4.0
<b>Total* (mm)</b>	141.4

\*Based on the 19.06 ha serviced by the EES units

Table 2: The Drummond Development - Water Budget Summary

Year	Rainfall		Subcatchments				Ground water			EES	Water Budget Summary									
	[1] (mm)	[2] (m³)	[3] Surface Runoff	[2]-[3]-[5] Surface Evaporation	[5] Surface Infiltration	[6] Evapotranspiration	[5]-[6] Subsurface	[7] EES Infiltration	[3]-[7] Total Runoff	[4]+[6] Total Evaporation	[5]-[6]+[7] Total Aquifer									
1967	373	71,100	34,464	48%	5,022	7%	31,614	44%	13,139	18%	18,475	26%	18,885	27%	15,579	22%	18,161	26%	37,360	53%
1968	520.6	99,235	46,380	47%	9,042	9%	43,813	44%	27,528	28%	16,285	16%	24,704	25%	21,676	22%	36,570	37%	40,989	41%
1969	499	95,118	42,866	45%	10,293	11%	41,959	44%	27,335	29%	14,624	15%	25,537	27%	17,329	18%	37,628	40%	40,161	42%
1970	538.1	102,571	48,125	47%	10,401	10%	44,044	43%	27,156	26%	16,889	16%	26,136	25%	21,989	21%	37,557	37%	43,025	42%
1971	491	93,593	40,359	43%	12,255	13%	40,978	44%	26,239	28%	14,740	16%	23,544	25%	16,815	18%	38,494	41%	38,284	41%
1972	764.1	145,650	70,794	49%	12,416	9%	62,439	43%	25,159	17%	37,281	26%	35,495	24%	35,299	24%	37,575	26%	72,776	50%
1973	670.1	127,732	60,556	47%	11,483	9%	55,694	44%	26,338	21%	29,356	23%	32,045	25%	28,511	22%	37,821	30%	61,401	48%
1974	332.1	63,304	26,320	42%	9,287	15%	27,697	44%	27,838	44%	-141	0%	19,297	30%	7,023	11%	37,125	59%	19,156	30%
1975	497.7	94,870	44,783	47%	8,896	9%	41,191	43%	27,903	29%	13,288	14%	23,761	25%	21,022	22%	36,799	39%	37,049	39%
1976	467.5	89,113	38,117	43%	11,307	13%	39,689	45%	26,602	30%	13,087	15%	24,858	28%	13,259	15%	37,909	43%	37,945	43%
1977	587.6	112,006	51,900	46%	10,391	9%	49,715	44%	26,829	24%	22,886	20%	30,428	27%	21,472	19%	37,220	33%	53,314	48%
1978	558.2	106,402	47,899	45%	11,911	11%	46,592	44%	26,307	25%	20,285	19%	27,819	26%	20,080	19%	38,218	36%	48,104	45%
1979	753.6	143,649	70,303	49%	10,942	8%	62,404	43%	26,571	18%	35,833	25%	33,031	23%	37,272	26%	37,513	26%	68,864	48%
1980	555	105,792	47,144	45%	11,329	11%	47,319	45%	26,473	25%	20,846	20%	28,986	27%	18,158	17%	37,802	36%	49,832	47%
1981	840.9	160,290	79,293	49%	13,780	9%	67,217	42%	24,723	15%	42,494	27%	36,487	23%	42,806	27%	38,502	24%	78,981	49%
1982	542.6	103,429	47,157	46%	10,041	10%	46,231	45%	27,278	26%	18,952	18%	29,147	28%	18,010	17%	37,319	36%	48,099	47%
1983	537	102,361	45,666	45%	10,797	11%	45,898	45%	26,933	26%	18,965	19%	28,501	28%	17,165	17%	37,731	37%	47,466	46%
1984	416.2	79,335	36,514	46%	7,454	9%	35,367	45%	29,064	37%	6,304	8%	21,167	27%	15,347	19%	36,517	46%	27,471	35%
1985	456	86,921	39,485	45%	9,041	10%	38,396	44%	27,726	32%	10,670	12%	21,875	25%	17,610	20%	36,767	42%	32,545	37%
1986	814	155,162	73,337	47%	12,505	8%	69,320	45%	25,313	16%	44,006	28%	38,107	25%	35,230	23%	37,818	24%	82,113	53%
1987	602.9	114,923	52,287	45%	11,635	10%	51,000	44%	26,246	23%	24,754	22%	30,751	27%	21,536	19%	37,881	33%	55,505	48%
1988	610.2	116,314	54,707	47%	10,992	9%	50,616	44%	26,519	23%	24,097	21%	29,488	25%	25,219	22%	37,510	32%	53,585	46%
1989	512.8	97,748	43,394	44%	11,065	11%	43,289	44%	26,823	27%	16,467	17%	25,746	26%	17,648	18%	37,887	39%	42,213	43%
1990	651.2	124,130	55,724	45%	13,354	11%	55,052	44%	25,279	20%	29,772	24%	31,550	25%	24,174	19%	38,633	31%	61,322	49%
1991	520.4	99,197	43,581	44%	11,319	11%	44,297	45%	26,740	27%	17,556	18%	27,358	28%	16,223	16%	38,059	38%	44,914	45%
1992	621.2	118,411	55,399	47%	11,656	10%	51,356	43%	25,810	22%	25,545	22%	30,202	26%	25,197	21%	37,467	32%	55,747	47%
1993	643.5	122,662	53,877	44%	13,877	11%	54,908	45%	25,296	21%	29,612	24%	33,525	27%	20,352	17%	39,174	32%	63,137	51%
1994	514.5	98,072	45,339	46%	9,536	10%	43,197	44%	27,374	28%	15,823	16%	24,179	25%	21,160	22%	36,910	38%	40,002	41%
1995	443.6	84,558	41,305	49%	6,053	7%	37,200	44%	29,936	35%	7,264	9%	16,823	20%	24,482	29%	35,988	43%	24,087	28%
1996	476.8	90,886	40,956	45%	9,565	11%	40,365	44%	27,510	30%	12,855	14%	24,508	27%	16,448	18%	37,075	41%	37,363	41%
1997	363.6	69,308	30,296	44%	8,062	12%	30,951	45%	28,502	41%	2,449	4%	20,094	29%	10,202	15%	36,564	53%	22,543	33%
1998	440.3	83,929	36,390	43%	10,289	12%	37,250	44%	26,914	32%	10,336	12%	21,902	26%	14,488	17%	37,202	44%	32,238	38%
1999	424.4	80,898	36,135	45%	8,890	11%	35,873	44%	27,987	35%	7,887	10%	21,116	26%	15,019	19%	36,876	46%	29,003	36%
2000	535.9	102,152	43,916	43%	12,885	13%	45,350	44%	25,475	25%	19,875	19%	25,793	25%	18,123	18%	38,360	38%	45,668	45%
	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
2002	551.5	105,125	51,653	49%	8,372	8%	45,100	43%	27,892	27%	17,209	16%	25,320	24%	26,333	25%	36,264	34%	42,529	40%
2003	554.6	105,716	46,852	44%	11,684	11%	47,180	45%	26,059	25%	21,121	20%	26,671	25%	20,181	19%	37,743	36%	47,792	45%
2004	573.3	109,281	54,081	49%	10,506	10%	44,694	41%	26,788	25%	17,907	16%	22,377	20%	31,704	29%	37,294	34%	40,284	37%
	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
2006	723.4	137,892	64,611	47%	11,382	8%	61,900	45%	25,718	19%	36,181	26%	36,660	27%	27,951	20%	37,100	27%	72,841	53%
2007	550.7	104,973	46,845	45%	11,568	11%	46,560	44%	25,804	25%	20,756	20%	27,130	26%	19,715	19%	37,372	36%	47,886	46%
<b>Average</b>	<b>552.0</b>	<b>105,226</b>	<b>48,431</b>	<b>45.8%</b>	<b>10,546</b>	<b>10.2%</b>	<b>46,249</b>	<b>44.0%</b>	<b>26,439</b>	<b>26.3%</b>	<b>19,810</b>	<b>17.8%</b>	<b>26,949</b>	<b>25.8%</b>	<b>21,482</b>	<b>20.0%</b>	<b>36,985</b>	<b>36.4%</b>	<b>46,759</b>	<b>43.5%</b>

Notes:

Total drainage area 19.06 ha

Surface Infiltration not considered as a part of the total aquifer recharge, as this value is simply the volume that is passed to the groundwater component

## Erosion & Sediment Control During & After Construction

Silt and erosion control strategies shall be implemented during construction activities to optimize the operations of the LID once implemented and minimize the siltation of the systems during construction. The following measures should be implemented:

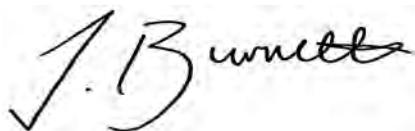
- Prior to site works, locations of the LIDs should be marked and vehicles to avoid this area other than during the installation of the LID drainage not to be directed to LID.
- Prior to the completion of landscape works, catch basins not connected to the LID practices can be used during construction for drainage.
- Heavy equipment and traffic should avoid travelling over the proposed location of the facility to minimize the compaction of the soil.
- To minimize siltation during construction, the EES units should be constructed with upstream and downstream plugs. During construction, these plugs will be implanted preventing sediments from entering the units. Once an occupancy of 80% is achieved, the upstream plug will then be removed and the EES units allow to operate as intended.
- Facilities should be kept “off-line” until construction is complete. They should never serve as a sediment control device during site construction. Sediment should be prevented from entering the infiltration facility using super silt fence, diversion berms or other means.
- Upland drainage areas need to be properly stabilized with a thick layer of vegetation, particularly immediately following construction, to reduce sediment loads.
- The facility should be excavated to design dimensions from the side using a backhoe or excavator. The base of the facility should be level or nearly level.
- The bottom of the facility should be scarified to improve infiltration. An optional 150 mm of sand could be spread for the bottom filter layer. The monitoring well should be anchored and stone should be added to the facility in 0.3-metre lifts.
- Geotextile fabric should be correctly installed in the soakaway or infiltration trench excavation. Large tree roots should be trimmed flush with the sides of the facility to prevent puncturing or tearing of the fabric during subsequent installation procedures. When laying out the geotextile, the width should include sufficient material to compensate for perimeter irregularities in the facility and for a 150 mm minimum top overlap. Voids may occur between the fabric and the excavated sides of the facility. Natural soils should be placed in any voids to ensure fabric conformity to the excavation sides

## Conclusion

In summary, the detailed PCSWMM model of the proposed Drummond development has been updated to include the LID measures proposed within the site. Continuous simulations using **39** years of historical rainfall data determined that the proposed water budget for the Drummond subdivision would be **20%** surface runoff, **36.4%** evaporation and **43.5%** infiltration. From this analysis, it was found that the proposed LIDs within the development will on average infiltrate **26,949 m<sup>3</sup> / 141.4 mm (25.8% of the total precipitation)** while the pervious surfaces within the development will infiltrate **19,810 m<sup>3</sup> / 103.9 mm (17.8% of the total precipitation)**. Adding the infiltration provided by the LIDs and the pervious surfaces results in the average total infiltration for the site being **46,759 m<sup>3</sup> / 245.3 mm (43.5% of the total precipitation)**. Exceeding the **40%** infiltration requirement set out by the Master Servicing study by **3.5%**.

It is important to consider that there are several conservative assumptions made within this analysis, that result in the simulated average infiltration values being lower than what is likely expected when the design is physically implemented. These assumptions include the reduction of the reported/observed soil infiltration rates by a factor of **2.5** and the consideration that exfiltration within the LID trenches only occurs through the bottom of the trench.

Yours truly,  
**J.F Sabourin and Associates Inc.**



Jonathon Burnett, B.Eng, P.Eng  
Water Resources Engineer

cc: J.F Sabourin, M.Eng, P.Eng  
Director of Water Resources Projects



## Figures

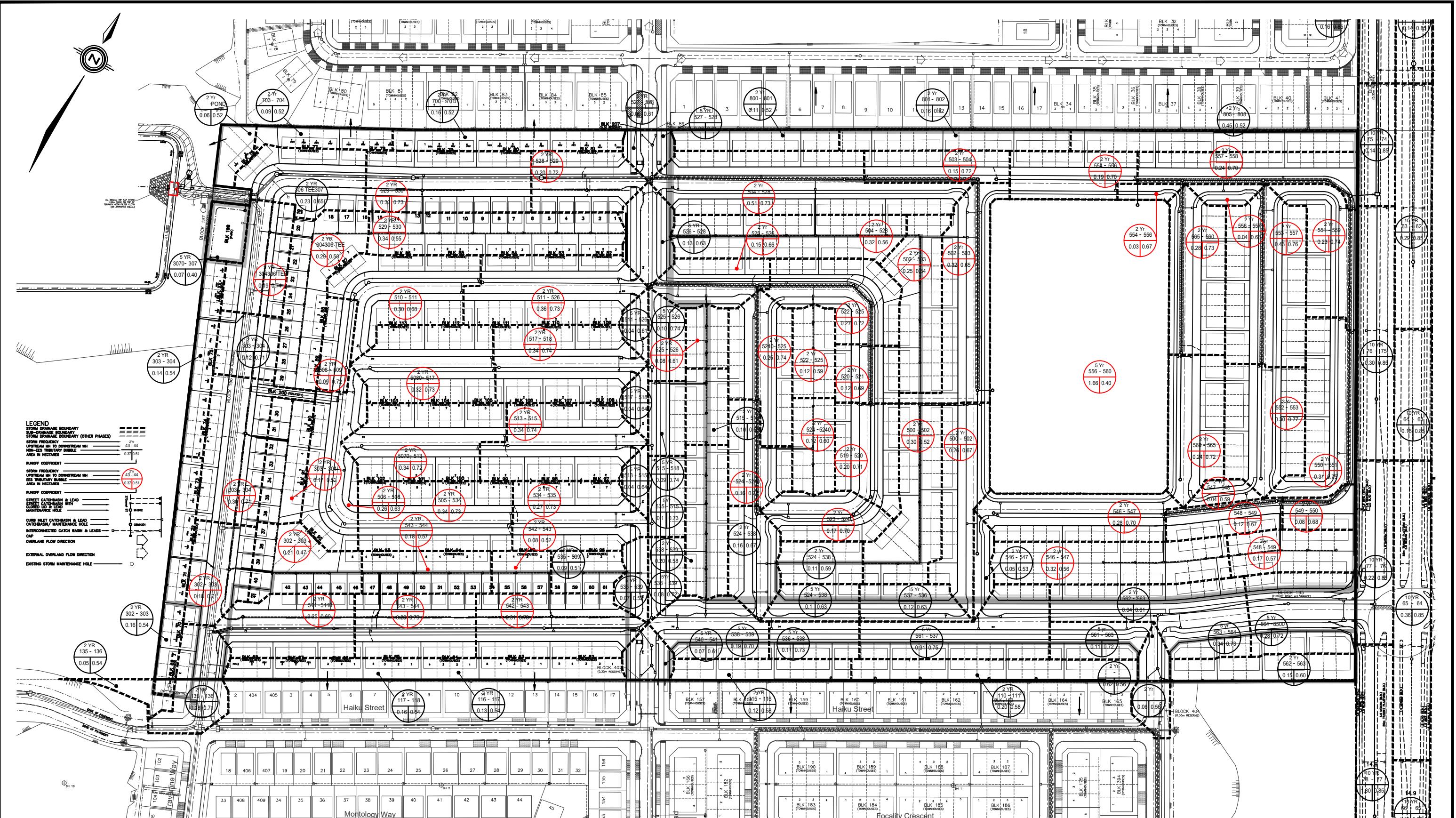
- Figure 1A: Exfiltration Trench System Details
- Figure 2A Catchbasin Exfiltration Trench Details
- Figure 2: LID Locations
- Figure 3: Exfiltration System Drainage Areas

## Tables

- Table 1: LID Infiltration Summary
- Table 2: Water Budget Summary

## Attachments

- Attachment A: Continuous Simulation Parameters & Background Information
- Attachment B: Continuous Simulation Results



120 Iber Road, Unit 103  
Stittsville, Ontario, K2S 1E9  
Tel. (613) 836-0856  
Fax. (613) 836-7183  
[www.DSEL.ca](http://www.DSEL.ca)

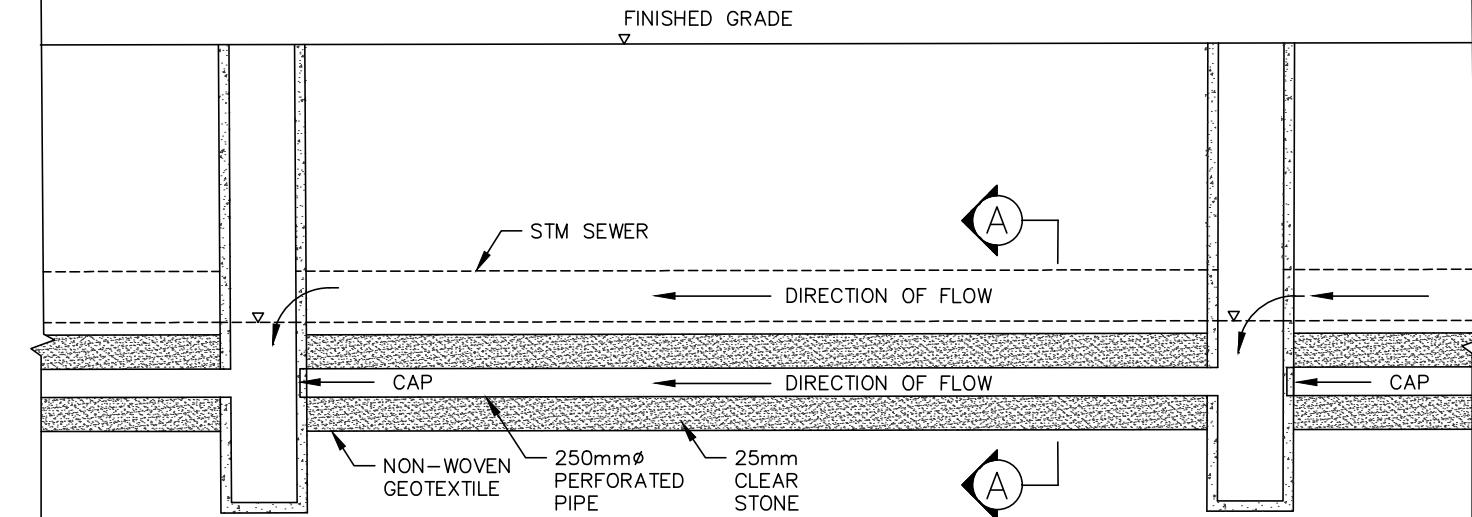
CAIVAN COMMUNITIES - THE RIDGE PHASE 3&4

# CITY OF OTTAWA

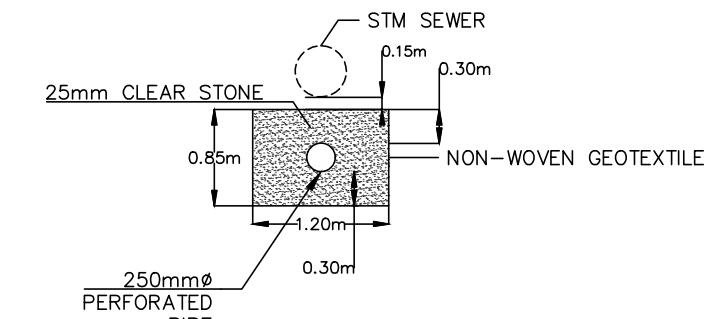
## EEA DRAINAGE AREA FIGURE

SCALE: 1:2000 PROJECT No.: 19-1123

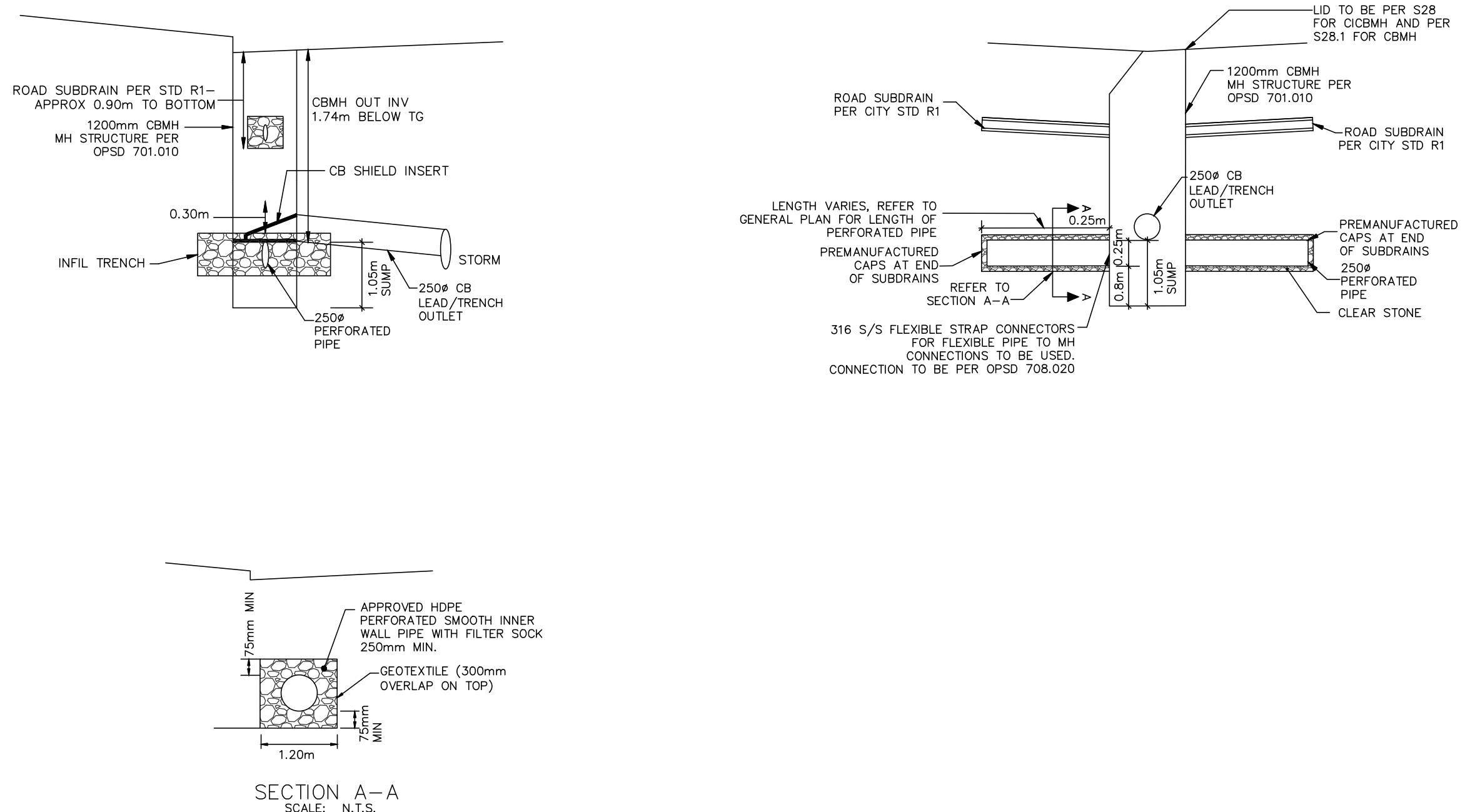
DATE: JUNE 2023 FIGURE: 1

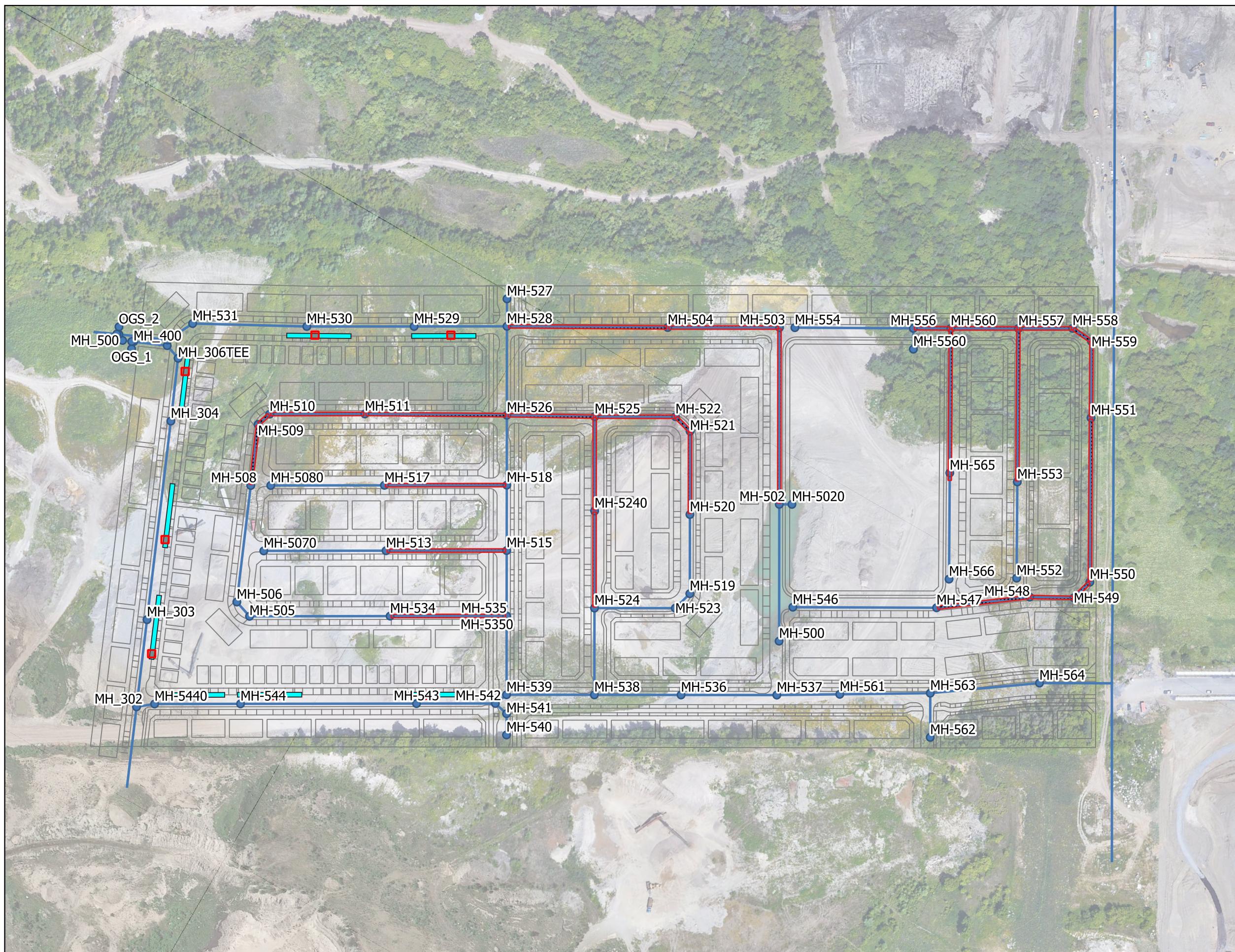


PROFILE  
SCALE N.T.S.



SECTION A-A





## Legend

- Etobicoke Exfiltration Systems (EES)
- Conduits
  - STM
- Junctions
  - MH
  - Catch Basin
- Catch Basin Exfiltration Trench
- Development Plan

SCALE: 1:2500

0 50 100 150 m

 J.F. Sabourin and Associates Inc.  
WATER RESOURCES AND ENVIRONMENTAL CONSULTANTS  
52 Springbrook Drive  
Ottawa, ON, K2S 1B9  
(613) 836-3884  
[www.jfsa.com](http://www.jfsa.com)

  
**dse**  
**david schaeffer engineering ltd**

Drummond Low Impact Development (LID) Design

Figure 2: EES Locations

PROJECT	2226
DRAWN	ON
DATE	JUNE 2023



J.F. Sabourin and Associates Inc.  
52 Springbrook Drive,  
Ottawa, ON K2S 1B9  
T 613-836-3884 F 613-836-0332

[jfsa.com](http://jfsa.com)

Ottawa, ON  
Paris, ON  
Gatineau, QC  
Montréal, QC  
Québec, QC

# Attachment A

Continuous Simulation Parameters & Background Information

**Table A1 - Etobicoke Exfiltration System - Parameters**

Parameter	EES_MH-502	EES_MH-503	EES_MH-504	EES_MH-520	EES_MH-521	EES_MH-522	EES_MH-524	EES_MH-525	EES_MH-547	EES_MH-548	EES_MH-549	EES_MH-550	EES_MH-551	EES_MH-553	EES_MH-556	EES_MH-557	EES_MH-558	EES_MH-560	EES_MH-565	EES_MH-5240
Number of Pipes	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
Pipe Diameter (mm)	250	250	250	250	250	250	250	250	250	250	250	250	250	250	250	250	250	250	250	250
Pipe Length (m)	118.5	75	108	56	14	54.5	65	59	63	29.5	15	110.5	51.5	103	25	36.5	15.5	45.5	97	63.5
Pipe Volume (m³)	5.82	3.68	5.30	2.75	0.69	2.68	3.19	2.90	3.09	1.45	0.74	5.42	2.53	5.06	1.23	1.79	0.76	2.23	4.76	3.12
Trench Width (m)	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2
Trench Height (m)	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85
Trench Length (m)	118.5	75	108	56	14	54.5	65	59	63	29.5	15	110.5	51.5	103	25	36.5	15.5	45.5	97	63.5
Void Ratio	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4
Trench Volume (m³)	46.02	29.13	41.94	21.75	5.44	21.17	25.24	22.91	24.47	11.46	5.83	42.91	20.00	40.00	9.71	14.18	6.02	17.67	37.67	24.66
Total Volume (m³)	51.8	32.8	47.2	24.5	6.1	23.8	28.4	25.8	27.6	12.9	6.6	48.3	22.5	45.1	10.9	16.0	6.8	19.9	42.4	27.8
Infiltration Rate (mm/hr)	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
Safety Factor	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5
Bottom Area (m²)	142.2	90	129.6	67.2	16.8	65.4	78	70.8	75.6	35.4	18	132.6	61.8	123.6	30	43.8	18.6	54.6	116.4	76.2
Infiltration Flow Rate (m³/s)	0.0008	0.0005	0.0007	0.0004	0.0001	0.0004	0.0004	0.0004	0.0004	0.0002	0.0001	0.0007	0.0003	0.0007	0.0002	0.0002	0.0001	0.0003	0.0006	0.0004
MH Invert	100.917	98.946	98.683	103.093	102.811	102.732	102.132	100.699	100.951	100.196	99.883	99.598	97.863	99.057	98.611	97.315	97.121	98.235	99.404	101.917
New MH Invert	100.367	98.396	98.133	102.543	102.261	102.182	101.582	100.149	100.401	99.646	99.333	99.048	97.313	98.507	98.061	96.765	96.571	97.685	98.854	101.367
Pipe Elevation	100.317	98.346	98.083	102.493	102.211	102.132	101.532	100.099	100.351	99.596	99.283	98.998	97.263	98.457	98.011	96.715	96.521	97.635	98.804	101.317
EES Bottom	100.017	98.046	97.783	102.193	101.911	101.832	101.232	99.799	100.051	99.296	98.983	98.698	96.963	98.157	97.711	96.415	97.335	98.504	101.017	

**Table A2 - Etobicoke Exfiltration System - Infiltration Curves ( $m^3/s$ )**

Depth	EES_MH-502	EES_MH-503	EES_MH-504	EES_MH-520	EES_MH-521	EES_MH-522	EES_MH-524	EES_MH-525	EES_MH-547	EES_MH-548	EES_MH-549	EES_MH-550	EES_MH-551	EES_MH-553	EES_MH-556	EES_MH-557	EES_MH-558	EES_MH-560	EES_MH-565	EES_MH-5240
0.000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
0.005	0.00079	0.00050	0.00072	0.00037	0.00009	0.00036	0.00043	0.00039	0.00042	0.00020	0.00010	0.00074	0.00034	0.00069	0.00017	0.00024	0.00010	0.00030	0.00065	0.00042
5.000	0.00079	0.00050	0.00072	0.00037	0.00009	0.00036	0.00043	0.00039	0.00042	0.00020	0.00010	0.00074	0.00034	0.00069	0.00017	0.00024	0.00010	0.00030	0.00065	0.00042

**Table A3 - Etobicoke Exfiltration System - Storage Curves ( $m^2$ )**

**Table A1 - Etobicoke Exfiltration System - Parameters**

**Table A2 - Etobicoke Exfiltration System - Infiltration Curves ( $m^3/s$ )**

**Table A3 - Etobicoke Exfiltration System - Storage Curves ( $m^2$ )**

**Table A2 - Monthly Evaporation Rates**

Month	Evaporation Rate (mm/Day)
January	0
February	0
March	0
April	1.133
May	2.516
June	3.933
July	4.516
August	3.871
September	2.367
October	1.387
November	0.2
December	0

Source: Table 10- MODEL DEVELOPMENT PROGRAM – CARP RIVER RESTORATION PLAN - Appendices, City of Ottawa (Feb 2014)

**From:** David Gilbert <[DGilbert@Patersongroup.ca](mailto:DGilbert@Patersongroup.ca)>  
**Sent:** August 29, 2019 5:30 PM  
**To:** Susan Murphy <[susan.murphy@caivan.com](mailto:susan.murphy@caivan.com)>; Steve Pichette <[SPichette@dsel.ca](mailto:SPichette@dsel.ca)>  
**Cc:** Michael Killam <[MKillam@Patersongroup.ca](mailto:MKillam@Patersongroup.ca)>  
**Subject:** Drummonds and Brazeau Pit - Infiltration information

Hi guys,

I spoke with Bobby Pettigrew at JL Richards and he used 40% of area precipitation to be infiltrated over a 30 year period using the infiltration system. Annual precipitation in water budget was noted to be 844 mm, so infiltration of 40% would be 338 mm. He noted that this amount was equivalent to full infiltration of a 22 mm rain event. The infiltration rate for system design for Brazeau Pit is 75 mm/hour and for Drummond Pit is 50 mm/hour. We are working on the groundwater contour plan based on our current groundwater observations for both sites. This drawing should be ready tomorrow.

Dave

David Gilbert, P.Eng.  
Senior Geotechnical Engineer

**paternongroup**  
solution oriented engineering  
over 60 years serving our clients

154 Colonnade Road South  
Ottawa, Ontario, K2E 7J5  
Tel: (613) 226-7381 Ext. 205

### 3.0 GROUNDWATER

#### 3.1 Groundwater Parameters

Parameter	Units	Description																				
Aquifer Name	-	<p>Name of the aquifer representing soil conditions. Four Aquifers were created based on different soil conditions from OSG mapping. Only two of the aquifers are used within the study area.</p> <table border="1"> <thead> <tr> <th>Aquifer</th><th>Description</th><th>Clay content (%)</th><th>Sand content (%)</th></tr> </thead> <tbody> <tr> <td>A</td><td>Sand</td><td>5</td><td>92</td></tr> <tr> <td>B</td><td>Sandy Loam</td><td>10</td><td>65</td></tr> <tr> <td>C (not used)</td><td>Sandy Clay Loam</td><td>28</td><td>60</td></tr> <tr> <td>D (not used)</td><td>Clay Loam</td><td>34</td><td>33</td></tr> </tbody> </table>	Aquifer	Description	Clay content (%)	Sand content (%)	A	Sand	5	92	B	Sandy Loam	10	65	C (not used)	Sandy Clay Loam	28	60	D (not used)	Clay Loam	34	33
Aquifer	Description	Clay content (%)	Sand content (%)																			
A	Sand	5	92																			
B	Sandy Loam	10	65																			
C (not used)	Sandy Clay Loam	28	60																			
D (not used)	Clay Loam	34	33																			
Receiving Node	-	Name of the receiving node for groundwater outflow to baseflow. This is based on the groundwater subwatershed delineation.																				
Surface Elevation	m	<p>Elevation of the ground surface for the subcatchment was averaged from the Patterson report.</p> <p><b>Value: 107</b></p>																				
Coefficients		<p>The coefficients were set for the saturated groundwater zone to represent a storage reservoir where outflow is linear proportional to the water table depth without surface water interaction. It was considered that the nearest open water channels were sufficiently far to have negligible impact on groundwater levels. The groundwater equation used is:</p> $f_G = A1 (d_L - h_{sw})$ <p>Where:</p> <ul style="list-style-type: none"> <li><math>f_G</math> = groundwater flow</li> <li><math>d_L</math> = depth of the lower saturated subsurface zone</li> <li><math>h_{sw}</math> = height of surface water above the bottom of the groundwater zone</li> <li><math>A1</math> = Calibration factor (estimated at 0.05)</li> </ul> <p><b>Value: 0.05</b></p>																				
Surface Water Depth	m	<p>Set as 0.5 metres to allow flow from the water table to surrounding watercourses.</p> <p><b>Value: 0.5</b></p>																				

Parameter	Units	Description
Initial Elevation	m	Initial elevation of the water table <b>Value: 95.5</b>
		All other parameters used as per the receiving node or aquifer

### 3.2 Aquifer Parameters

Parameter	Units	Description / Values										
Porosity	Fraction	<p>The following values were used for the volumetric water content of the soil at saturation (i.e. volume of water per total volume):</p> <table border="1"> <thead> <tr> <th>Soil Group</th> <th>A</th> <th>B</th> <th>C</th> <th>D</th> </tr> </thead> <tbody> <tr> <td>Porosity</td> <td>0.436</td> <td>0.450</td> <td>0.432</td> <td>0.472</td> </tr> </tbody> </table> <p>(Source: SPAW Calculator)</p>	Soil Group	A	B	C	D	Porosity	0.436	0.450	0.432	0.472
Soil Group	A	B	C	D								
Porosity	0.436	0.450	0.432	0.472								
Wilting Point	Fraction	<p>This is soil moisture contact at which plants cannot obtain sufficient moisture from the soil to meet transpiration requirements and they will die. It is roughly equivalent to the moisture content of soil at 15 atmospheres. The following values were used:</p> <table border="1"> <thead> <tr> <th>Soil Group</th> <th>A</th> <th>B</th> <th>C</th> <th>D</th> </tr> </thead> <tbody> <tr> <td>Wilting Point</td> <td>0.050</td> <td>0.081</td> <td>0.183</td> <td>0.213</td> </tr> </tbody> </table> <p>(Source: SPAW Calculator)</p>	Soil Group	A	B	C	D	Wilting Point	0.050	0.081	0.183	0.213
Soil Group	A	B	C	D								
Wilting Point	0.050	0.081	0.183	0.213								
Field Capacity	Fraction	<p>Considered to be the amount of water a well-drained soil holds after free water has drained off. The following values were used:</p> <table border="1"> <thead> <tr> <th>Soil Group</th> <th>A</th> <th>B</th> <th>C</th> <th>D</th> </tr> </thead> <tbody> <tr> <td>Field Capacity</td> <td>0.094</td> <td>0.179</td> <td>0.283</td> <td>0.350</td> </tr> </tbody> </table> <p>(Source: SPAW Calculator)</p>	Soil Group	A	B	C	D	Field Capacity	0.094	0.179	0.283	0.350
Soil Group	A	B	C	D								
Field Capacity	0.094	0.179	0.283	0.350								
Conductivity	mm/hr	<p>Within the Aquifer Parameters, the soil saturated conductivity is a governing parameter of the percolation rate between the upper unsaturated soil layer and the lower saturated soil layer. This is not the same as any hydraulic conductivity used for the surface infiltration. The values have been selected from the SPAW calculator and are:</p> <table border="1"> <thead> <tr> <th>Soil Group</th> <th>A</th> <th>B</th> <th>C</th> <th>D</th> </tr> </thead> <tbody> <tr> <td>Conductivity (mm/hr)</td> <td>114</td> <td>50.3</td> <td>7.8</td> <td>4.6</td> </tr> </tbody> </table> <p>(Source: SPAW Calculator)</p>	Soil Group	A	B	C	D	Conductivity (mm/hr)	114	50.3	7.8	4.6
Soil Group	A	B	C	D								
Conductivity (mm/hr)	114	50.3	7.8	4.6								

Parameter	Units	Description / Values										
Conductivity Slope	-	<p>Conductivity slope measures the rate at which a soil's hydraulic conductivity decreases with decreasing moisture content. Regression analysis has shown it can be estimated with the following relationship:</p> $\text{Conductivity Slope} = 0.48(\% \text{ Sand}) + 0.85(\% \text{ Clay})$ <p>Based on this relationship the following values were used:</p> <table border="1" style="margin-left: auto; margin-right: auto;"> <thead> <tr> <th>Soil Group</th><th>A</th><th>B</th><th>C</th><th>D</th></tr> </thead> <tbody> <tr> <td>Conductivity Slope</td><td>48</td><td>40</td><td>53</td><td>45</td></tr> </tbody> </table>	Soil Group	A	B	C	D	Conductivity Slope	48	40	53	45
Soil Group	A	B	C	D								
Conductivity Slope	48	40	53	45								
Tension Slope		Used for backward compatibility in the software and not used in this model										
Upper Evaporation Factor	Fraction	<p>This factor determines the fraction of available subsurface evaporation rate used in the upper subsurface zone (compared to the lower subsurface zone). A higher evaporation rate is associated with looser soils, lower water table elevations and shallow root zones. It was assumed that in all soils 80% of the available subsurface evaporation would be used in the upper zone due to the depth of the water table.</p> <p><b>Value: 0.8</b></p>										
Lower Evaporative Depth	m	<p>The depth of the lower subsurface zone which can be used for evapotranspiration should be approximate to the expected average depth of root penetration. The following values were used:</p> <table border="1" style="margin-left: auto; margin-right: auto;"> <thead> <tr> <th>Soil Group</th><th>A</th><th>B</th><th>C</th><th>D</th></tr> </thead> <tbody> <tr> <td>Evaporative Depth (m)</td><td>1.5</td><td>2.4</td><td>3.0</td><td>5.2</td></tr> </tbody> </table> <p>(Source: Shah et al 2007 from EPA 2015)</p>	Soil Group	A	B	C	D	Evaporative Depth (m)	1.5	2.4	3.0	5.2
Soil Group	A	B	C	D								
Evaporative Depth (m)	1.5	2.4	3.0	5.2								
Lower Groundwater Loss Rate	mm/hr	<p>This is the rate of percolation from the lower subsurface zone to a deep aquifer and is approximate to the rate at which the water table elevation will drop over a prolonged dry period. The saturated hydraulic conductivity of a compacted clay soil was used in all cases.</p> <p><b>Value: 0.004</b></p>										
Bottom Elevation	m	<p>The elevation of the bedrock as averaged from the Patterson 2016 report.</p> <p><b>Value: 85</b></p>										

Parameter	Units	Description / Values				
Unsaturated Zone Moisture		The moisture content of the unsaturated upper subsurface zone at the start of the simulation. Cannot be less than the wilting point and cannot be more than porosity. Assumed to be an approximate value between the wilting point and porosity fractions.				
		Soil Group	A	B	C	D
		Evaporative Depth (m)	0.25	0.22	0.32	0.35



Ottawa. ON  
Paris. ON  
Gatineau. QC  
Montréal. QC  
Québec. QC

# Attachment B

Continuous Simulation Results

**Table B1 - Yearly Precipitation**

Year	Rainfall	
	(mm)	(m³)
1967	373	71,100
1968	520.6	99,235
1969	499	95,118
1970	538.1	102,571
1971	491	93,593
1972	764.1	145,650
1973	670.1	127,732
1974	332.1	63,304
1975	497.7	94,870
1976	467.5	89,113
1977	587.6	112,006
1978	558.2	106,402
1979	753.6	143,649
1980	555	105,792
1981	840.9	160,290
1982	542.6	103,429
1983	537	102,361
1984	416.2	79,335
1985	456	86,921
1986	814	155,162
1987	602.9	114,923
1988	610.2	116,314
1989	512.8	97,748
1990	651.2	124,130
1991	520.4	99,197
1992	621.2	118,411
1993	643.5	122,662
1994	514.5	98,072
1995	443.6	84,558
1996	476.8	90,886
1997	363.6	69,308
1998	440.3	83,929
1999	424.4	80,898
2000	535.9	102,152
2001	-	-
2002	551.5	105,125
2003	554.6	105,716
2004	573.3	109,281
2005	-	-
2006	723.4	137,892
2007	550.7	104,973
<b>Average</b>	<b>552.0</b>	<b>105,226</b>

Notes:

Total drainage area 19.06 ha

Table B2 - Etobicoke Extrifiltration System  
Yearly Infiltration Volumes (m<sup>3</sup>)

Node	MH-502	MH-503	MH-504	MH-508	MH-509	MH-510	MH-511	MH-513	MH-517	MH-520	MH-521	MH-522	MH-524	MH-5240	MH-525	MH-534	MH-547	MH-548	MH-549	MH-550	MH-551	MH-553	MH-556	MH-557	MH-558	MH-560	MH-565	CB-109	CB-111	CB-116	CB-12	CB-126	CB-16	CB-4	CB-94	Total	
1967	1183	430	1062	515	70	116	1103	1010	1002	435	11	513	834	611	489	960	611	254	162	734	532	1259	470	428	195	772	1017	303	262	282	250	252	303	236	219	18,885	
1968	1557	578	671	89	186	1451	1368	1344	574	26	676	1148	794	656	1274	806	335	214	969	703	1651	694	546	153	747	1330	393	345	369	331	333	393	314	291	24,704		
1969	1574	473	1418	710	77	95	1540	1454	1430	544	14	663	1215	814	599	1360	812	308	211	895	725	1767	784	608	157	1131	1389	409	342	376	326	328	290	25,537			
1970	1607	499	1452	734	69	145	1604	1505	1484	569	31	669	1249	838	612	1411	827	312	216	948	757	1829	761	614	176	977	1434	416	344	380	328	330	419	308	281	26,136	
1971	1608	468	1296	656	52	121	1436	1179	717	513	21	606	1179	717	576	1296	808	288	197	847	660	1657	745	597	139	774	1262	363	308	335	294	296	365	273	250	25,544	
1972	2223	784	1594	966	123	25	2007	1949	1932	820	41	950	1594	966	1136	1830	1148	461	303	1409	1002	263	964	800	238	172	1244	571	494	533	447	477	573	447	416	355	
1973	1480	731	1779	874	110	233	1893	1781	1753	730	34	858	1488	1014	804	1664	1026	415	272	1356	805	738	251	1188	500	434	467	415	410	502	390	369	32,045				
1974	1024	261	941	497	25	34	1092	1068	1044	344	9	418	900	531	364	981	529	186	136	554	504	1260	2107	445	96	1161	947	278	223	252	209	211	280	197	178	18,297	
1975	1462	486	1319	661	66	162	1442	1373	1354	532	30	614	1144	754	582	1283	756	289	198	893	678	1654	715	550	166	760	1287	369	314	341	301	303	372	286	265	23,761	
1976	1512	443	1360	679	62	78	1483	1414	1391	518	4	626	1183	767	600	1320	776	299	202	847	693	1704	704	622	245	1324	1319	393	332	362	316	319	395	300	271	24,658	
1977	1901	597	1719	855	95	127	1864	1743	1725	668	18	793	1449	988	737	1642	979	369	257	1119	884	2129	862	704	223	1009	1669	485	407	446	387	390	486	364	338	30,428	
1978	1761	567	1585	775	98	109	1689	158	1565	617	9	732	1319	908	723	1482	910	353	239	1024	810	1917	793	644	201	838	1526	432	376	401	362	365	435	348	319	27,819	
1979	2098	767	1889	908	128	300	1954	1775	1767	785	66	894	1463	1109	868	1687	1084	440	288	1326	800	810	745	271	966	1811	519	454	487	437	440	521	419	380	30,031		
1980	1822	556	1641	818	81	104	1769	1632	1617	628	11	752	1351	957	717	1542	933	360	243	1035	852	2013	776	686	232	1042	1604	467	396	431	378	380	470	364	322	28,986	
1981	2253	767	2026	1004	110	254	2183	2086	2040	820	46	956	1745	1144	915	1930	1165	454	306	1386	1035	2497	1045	825	208	1348	1960	573	494	473	476	577	449	415	36,487		
1982	1789	531	1616	815	76	106	1782	1709	1673	625	10	748	1419	918	1580	922	351	241	1023	840	2018	818	816	196	1156	462	391	427	372	374	465	351	320	29,447			
1983	1541	487	1574	804	62	91	1756	1621	1650	500	17	717	1409	895	658	1561	538	231	978	816	1772	677	1172	464	395	426	374	375	466	351	320	29,531					
1984	1349	448	1216	577	88	110	1236	1136	1128	487	7	566	933	711	555	1074	695	270	182	800	612	1404	505	504	167	835	1159	341	309	322	288	290	343	275	253	21,157	
1985	1433	480	1280	601	105	107	1293	1161	1158	510	10	597	957	678	612	1107	744	298	198	836	659	1444	570	491	188	592	1237	339	305	329	293	295	340	285	261	21,875	
1986	2372	875	2137	1045	122	302	2261	2118	2089	897	42	1016	1762	975	1883	1221	493	322	1521	1090	2579	1008	861	253	1170	2057	612	532	512	515	616	496	460	38,107			
1987	1826	580	1644	833	73	162	1818	1744	1712	650	28	764	1459	933	707	1614	970	359	243	1086	851	2052	888	766	187	1938	1616	479	400	446	381	383	482	358	332	30,751	
1988	1822	652	1634	811	89	190	1763	1696	1661	666	27	789	1424	916	745	1567	946	384	250	1137	825	2020	929	662	157	466	395	430	379	381	468	351	334	29,488			
1989	1581	511	1428	722	67	129	1578	1518	1488	567	16	567	1272	806	609	1402	815	312	213	951	735	1805	775	618	160	802	1399	409	345	377	329	331	411	309	289	25,746	
1990	1957	650	1767	883	95	177	1910	1815	1785	706	27	834	1515	1009	709	1691	1008	391	264	2191	906	723	200	981	1721	514	432	474	411	414	517	383	359	31,550			
1991	1670	552	1505	761	72	104	1660	1601	1573	597	0	709	1347	843	653	1484	859	332	224	1016	769	1714	814	618	191	966	1468	442	376	409	357	360	445	338	310	27,758	
1992	1894	637	1705	836	102	150	1813	1729	1701	678	19	804	1447	970	768	1606	980	391	260	1127	864	2070	883	683	186	926	1647	476	411	443	396	398	479	373	350	30,202	
1993	2094	500	1911	950	99	99	2009	1949	1916	718	11	889	1638	1097	1815	1805	401	295	1151	976	2009	783	203	1018	793	203	1022	886	550	465	510	442	445	554	419	378	35,325
1994	1529	585	1846	631	103	168	1413	1305	1298	526	26	654	1105	784	637	1240	800	320	210	1002	691	1604	675	542	105	762	1301	368	324	345	314	370	361	297	279	24,747	
1995	1027	366	936	469	45	160	1015	947	935	388	41	443	785	530	403	891	528	208	138	654	470	1164	453	395	118	507	393	277	235	226	227	278	313	202	18,623		
1996	1509	499	1362	683	69	115	1495	1430	1403	541	12	636	1197	770	595	1325	776	303	203	808	706	1714	688	573	144	794	1239	397	326	366	311	323	400	306	279	25,508	
1997	1267	314	1149	579	59	13	1258	1181	1168	415	0	513	980	673	463	1107	650	232	167	661	601	1433	552	503	160	633	1140	331	274	305	258	260	333	243	219	20,094	
1998	1396	451	1255	604	85	81	1313	1230	1213	490	3	579	1023	728	570	1150	719	283	188	810	645	1488	615	500	157	656	1210	351	305	330	292	293	352	282	255	21,902	
1999	1354	426	1224	589	74	80	1279	1182	1171	469	10	552	978	719	552	1110	697	264	183	789	639	1341	533	482	156	666	1182	332	286	309	274	275	332	267	240	21,116	
2000	1583	537	1425	700	79	137	1525	1447	1429	570	14	671	1204	816	637	1351	816	322	215	957	732	1744	747	610	179	1147	1381	405	348	377	3						

**Table B3 - Subcatchments  
Yearly Runoff Volumes ( $m^3$ )**

			Table B3 - Subcatchments: Yearly Runoff Volumes (m³)																																											
Node	Area	1967	1968	1969	1970	1971	1972	1973	1974	1975	1976	1977	1978	1979	1980	1981	1982	1983	1984	1985	1986	1987	1988	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	Average			
A528NW	0.050	117	158	146	160	138	236	204	90	150	132	177	163	235	163	262	158	126	135	251	179	184	149	192	151	187	187	154	139	141	105	125	124	152	-	174	162	175	-	223	161	165				
A528R1	0.188	46	59	46	107	44	153	107	20	93	1	50	55	150	16	208	26	8	28	44	61	47	106	31	43	9	86	0	71	79	31	5	22	34	12	-	75	12	192	-	36	39	58			
A528S	0.047	109	147	136	149	128	220	190	84	140	123	165	152	219	152	244	151	148	117	126	234	167	171	139	178	141	174	174	143	129	131	98	117	116	142	-	162	151	163	-	207	150	153			
A528SW	0.052	141	189	175	192	166	282	244	108	180	159	213	195	282	196	312	195	196	151	162	302	215	220	179	230	181	224	225	185	167	169	126	150	148	182	-	207	195	208	-	267	193	198			
A529N	0.107	273	367	340	373	321	548	474	210	349	308	413	379	547	380	606	376	369	292	314	585	471	427	347	445	352	434	436	358	324	327	244	292	289	354	-	403	378	405	-	518	374	383			
A529R	0.070	126	170	157	173	148	254	219	97	161	142	190	176	252	175	281	175	175	151	184	145	270	193	197	160	205	162	201	201	167	149	151	134	164	-	173	174	189	-	239	179	177				
A529R1	0.153	25	41	32	60	26	112	80	12	57	36	88	107	7	153	16	2	17	29	40	29	21	26	64	0	54	52	3	11	10	8	-	58	142	-	22	21	40								
A529R3	0.191	28	42	32	86	24	124	84	13	71	0	38	40	109	3	174	13	1	14	29	40	29	84	20	25	2	72	0	40	50	18	2	7	14	8	-	68	9	163	-	21	18	41			
A529S	0.107	262	351	326	357	307	525	454	201	334	295	395	363	524	363	581	362	352	280	300	560	399	409	322	427	337	416	417	343	311	313	234	279	276	338	-	387	361	389	-	496	358	367			
A529SW	0.054	141	189	176	192	166	282	245	109	180	159	213	195	282	196	312	195	196	151	162	302	215	221	179	230	181	224	225	185	167	169	126	150	149	182	-	208	195	209	-	267	193	198			
A534NE	0.143	373	502	466	510	439	750	548	288	477	422	565	519	748	520	829	518	399	429	801	571	584	475	609	481	594	593	490	442	444	335	401	396	484	-	551	517	555	-	709	513	525				
A534SW	0.123	302	408	378	415	356	609	525	234	387	342	458	421	607	422	673	420	410	323	348	649	464	474	385	493	390	482	488	390	356	364	272	326	321	393	-	448	419	451	-	575	416	426			
A535NE	0.066	106	144	134	149	125	220	186	82	137	121	161	150	216	149	245	148	145	114	123	167	136	173	178	173	171	140	126	128	96	115	113	139	-	164	148	165	-	203	147	151					
A535SW	0.059	242	327	303	332	285	488	421	187	310	275	367	338	486	338	537	329	377	259	279	520	372	380	309	396	313	386	388	319	287	298	216	258	215	315	-	358	336	361	-	461	333	341			
A536NE	0.107	270	363	337	369	317	542	468	208	345	305	407	375	541	376	576	394	365	370	579	413	423	340	440	343	554	320	242	290	286	350	-	399	373	401	-	513	370	379							
A537NE	0.117	236	316	294	324	278	478	411	182	302	267	357	329	475	329	531	377	306	370	319	280	300	304	377	377	310	280	281	211	252	249	306	-	354	326	356	-	448	324	332						
A538AV	0.083	204	274	279	295	236	354	307	154	251	250	250	260	360	250	360	255	255	218	258	247	250	259	252	252	252	252	252	252	252	252	252	252	-	260	260	266	-	363	280	286					
A538R	0.052	16	20	16	37	15	52	37	7	17	17	20	19	52	37	7	9	3	10	15	21	37	29	11	15	29	0	28	11	15	29	0	25	6	14	25	6	14	20							
A538R2	0.143	29	39	31	75	26	107	74	13	63	0	34	36	102	8	14	8	17	28	39	29	74	20	26	5	61	0	44	51	19	3	12	19	8	-	54	8	137	-	22	22	38				
A538S	0.034	64	87	81	90	76	132	113	50	83	73	98	91	130	90	146	90	88	69	74	139	99	101	82	105	83	104	103	83	104	103	84	80	99	90	99	-	123	89	91	-	123	89	91		
A538SW	0.032	56	76	71	78	66	116	99	44	73	64	86	79	114	72	79	78	77	60	65	121	87	89	72	93	71	90	90	74	74	68	61	60	74	-	86	78	87	-	107	78	80				
A540NE	0.033	68	92	86	94	80	139	119	53	88	77	103	96	137	95	154	95	93	73	79	146	105	107	87	111	88	110	109	90	82	62	74	73	89	-	102	95	104	-	130	90	96				
A540RN	0.034	65	87	81	90	76	132	113	50	83	73	98	91	130	90	146	90	88	68	74	139	99	102	85	104	84	104	103	85	84	69	74	73	89	-	123	89	91	-	123	89	91				
A542NE	0.086	219	294	273	298	257	439	380	168	280	247	331	303	438	304	486	303	295	234	321	478	344	324	278	348	349	287	280	262	196	233	231	283	-	313	302	325	-	415	300	307					
A542SW	0.079	196	263	244	267	230	394	324	151	250	220	296	271	392	272	435	271	264	210	225	319	272	308	246	319	312	256	233	234	234	234	234	234	-	289	270	291	-	371	268	275					
A543NE	0.100	248	333	308	338	291	497	430	191	316	279	374	344	497	344	551	343	334	265	285	531	378	388	314	405	401	415	337	342	343	348	314	313	310	305	303	309	308	-	393	367	396	-	503	364	373
A543NW	0.019	58	77	72	78	68	115	100	44	74	65	87	81	124	80	115	80	80	75	82	124	94	97	73	91	92	76	70	69	69	69	69	69	69	-	84	80	85	-	109	79	81				
A543R	0.175	47	57	44	62	50	137	101	15	189	24	50	45	137	15	189	24	26	47	43	97	49	40	29	28	8	78	0	65	28	28	28	28	28	28	-	68	11	174	-	33	36	33			
A544NE	0.148	21	31	24	65	17	93	62	10	53	0	28	30	2	131	9	0	10	21	29	21	63	15	18	1	54	0	29	37	13	1	4	9	6	-	53	6	123	-	15	13	31				
A545SE	0.114	265	357	331	311	534	636	408	264	377	322	457	404	526	365	523	405	425	246	244	393	325	305	298	285	284	284	281	284	284	284	-	393	367	396	-	503	364	373							
A551NW	0.050	109	148	137	150	129	221	190	85	140	124	166	153																																	

Node	Area	Yearly Surface Infiltration Volumes (m³)																																								
		1967	1968	1969	1970	1971	1972	1973	1974	1975	1976	1977	1978	1979	1980	1981	1982	1983	1984	1985	1986	1987	1988	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007
A303NE	0.046	56	78	75	80	74	113	101	50	89	84	113	89	82	81	92	72	89	97	77	98	82	97	92	99	72	55	66	64	81	109	83	83	83	83	83	83					
A303NE	0.046	39	45	45	52	46	52	52	53	49	49	62	59	59	58	57	54	44	48	48	55	54	54	54	54	54	54	54	54	54	54	54	54	54	54	54	54	54	54	54	54	54
A302NW	0.043	43	60	58	62	57	87	77	39	58	54	68	64	64	64	64	64	64	64	64	64	64	64	64	64	64	64	64	64	64	64	64	64	64	64	64	64	64	64	64	64	64
A302R1	0.059	329	453	432	441	417	635	567	282	414	416	517	480	633	499	675	485	486	369	395	728	530	509	450	571	466	526	581	441	379	326	387	372	473	475	495	431	655	484	478		
A303R2	0.206	719	989	948	986	919	1,403	1,248	621	925	892	1,125	1,044	1,419	1,072	1,507	1,052	1,039	805	873	1,578	1,158	1,134	974	1,249	1,001	1,148	1,238	887	852	913	698	843	817	1,020	-	1,019	1,065	983	1,412	1,057	1,044
A303R2	0.064	214	294	280	287	271	417	368	183	269	270	335	312	412	323	439	315	315	240	247	472	344	332	291	371	302	341	376	247	213	251	244	307	-	306	321	281	425	314	310		
A303S1	0.042	42	58	58	65	55	74	37	56	52	53	68	61	61	61	61	61	61	61	61	61	61	61	61	61	61	61	61	61	61	61	61	61	61	61	61	61	61	61	61	61	
A302SW	0.113	110	143	147	157	145	220	197	98	146	138	173	163	220	163	158	123	134	240	178	180	151	192	153	181	190	152	131	140	107	130	125	158	-	156	163	163	213	162	162		
A303N1	0.062	79	110	106	113	105	156	141	70	105	99	124	117	152	118	114	88	97	172	128	129	109	130	130	136	109	94	101	77	93	90	114	-	112	117	117	153	117				
A303N2	0.062	51	71	68	73	67	102	91	45	68	64	80	76	102	76	111	74	73	57	62	62	111	82	83	70	89	71	84	88	70	61	65	50	60	58	73	-	72	76	75	99	75
A303N3	0.066	94	54	75	72	71	104	98	46	80	86	108	117	98	87	88	93	96	93	94	94	94	94	94	94	94	94	94	94	94	94	94	94	94	94	94	94	94	94	94	94	
A303N4	0.066	94	127	122	130	120	183	143	81	121	114	143	135	182	136	156	126	136	198	133	131	103	103	103	111	147	149	159	157	150	157	150	157	150	157	150	157	150				
A303N5	0.063	47	66	63	68	62	95	85	42	63	63	95	75	70	71	103	69	68	53	58	65	70	77	65	83	66	78	82	65	65	61	54	68	61	67	61	67	61	67	61	67	
A303R1	0.016	53	73	70	71	67	103	92	45	67	67	83	78	102	81	103	78	76	60	64	118	84	82	73	92	75	85	94	71	61	68	63	60	67	66	67	66	67	66	67		
A303R2	0.262	364	351	339	320	306	506	453	229	379	336	414	384	502	400	538	290	392	296	315	584	424	419	387	424	380	381	357	405	309	294	382	401	340	327	385	382	380	382			
A303R3	0.019	574	798	775	781	731	913	961	401	720	696	843	854	1,138	863	1,136	843	843	951	952	953	954	955	956	957	958	959	959	959	959	959	959	959	959	959	959	959	959	959			
A303R4	0.091	81	114	109	120	107	165	143	73	108	106	128	127	177	119	191	100	124	114	124	114	124	114	124	114	124	114	124	114	124	114	124	114	124	114	124	114	124	114			
A303R5	0.091	102	142	136	145	134	204	182	91	136	128	160	151	202	152	221	148	147	114	124	222	165	167	140	178	121	130	121	130	121	130	121	130	121	130	121	130					
A304N1	0.088	77	108	104	110	102	155	138	97	109	105	125	122	156	134	165	120	127	120	127	120	127	120	127	120	127	120	127	120	127	120	127	120	127	120	127	120					
A304N2	0.087	288	396	377	385	364	554	524	496	424	362	364	452	420	554	434	583	425	425	434	463	446	393	500	407	460	507	386	322	367	573	413	325	417	325	417	325	417	325	417	325	
A304N3	0.095	159	222	238	269	246	303	285	175	262	251	307	287	347	242	300	251	251	247	247	325	283	283	279	240	258	258	258	258	258	258	258	258	258	258	258						
A304N4	0.095	203	293	268	279	266	329	314	207	293	279	324	317	329	260	312	291	291	287	287	324	292	292	272	309	261	290	273	309	261	290	273	309	261	290	273	309	261				
A304N5	0.095	13	17	17	17	16	18	16	21	22	32	29	14	21	20	25	24	24	23	28	21	28	22	26	21	26	21	26	21	26	21	26	21	26	21	26	21	26	21	26	21	
A304N6	0.034	84	117	104	117	104	156	149	101	156	149	181	172	156	149	181	172	156	149	181	172	156	149	181	172	156	149	181	172	156	149	181	172	156	149	181	172	156	149			
A304N7	0.034	147	182	172	171	155	214	204	154	214	204	234	221	204	214	204	234	221	204	214	204	234	221	204	214	204	234	221	204	214	204	234	221	204	214	204	234	221				
A304N8	0.034	164	228	219	234	216	322	288	143	216	205	258	243	328	244	328	243	328	243	328	243	328	243	328	243	328	243	328	243	328	243	328	243	328	243	328	243					
A305N1	0.054	164	224	216	248	234	357	319	223	281	265	355	365	287	259	317	281	265	305	276	317	293	281	305	276	317	293	281	305	276	317	293	281	305	276	317	293	281	305			
A305N2	0.050	156	205	197	202	181	305	276	199	261	230	216	249	210	224	210	224	210	224	210	224	210	224	210	224	210	224	210	224	210	224	210	224	210	224	210	224	210				
A305N3	0.049	88	128	121	128	118	175	166	104	175	166	197	187	175	166	197	187	175	166	197	187	175	166	197	187	175	166	197	187	175	166	197	187	175	166	197	187	175	166			
A305N4	0.049	114	159	152	160	150	204	103	152	143	169	149	168	149	168	149	168	149	168	149	168	149	168	149	168	149	168	149	168	149	168	149	168	149	168	149	168	149				
A305N5	0.049	88	123	121	128	122	204	196	85	123	121	175	166	204	196	196	187	196	187	196	187	196	187	196	187	196	187	196	187	196	187	196	187	196	187	196	187	196	187			
A305N6	0.049	121	173	166	173	166	204	196	103	173	166	204	196	19																												

Node	Area	Yearly Surface Infiltration Volumes (m³)																																									
		1967	1968	1969	1970	1971	1972	1973	1974	1975	1976	1977	1978	1979	1980	1981	1982	1983	1984	1985	1986	1987	1988	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	Average
A537NE	0.119	170	228	243	224	341	305	152	227	213	253	341	245	208	206	271	279	278	234	297	237	280	254	235	200	218	166	201	194	245	-	242	203	252	330	251	251						
A538NE	0.103	133	144	149	134	156	147	145	92	137	163	153	203	195	115	136	147	146	143	181	144	170	178	143	132	149	146	145	145	145	145	145	145	145	145	145	145						
A538NW	0.083	80	112	108	115	106	161	144	72	107	101	127	120	170	117	116	90	98	176	130	132	111	141	112	132	139	111	96	103	78	95	92	116	-	114	120	119	156	119	118			
A538R1	0.062	203	280	267	272	256	391	350	174	255	259	320	297	389	309	416	301	320	228	244	451	328	314	278	353	289	325	361	271	233	260	202	239	229	294	-	295	308	264	298	295		
A538R2	0.143	476	654	623	637	602	916	818	406	598	500	746	693	915	719	974	701	700	534	571	1,050	764	736	648	825	671	759	836	638	549	606	469	558	536	681	-	685	715	621	945	698	689	
A538S	0.034	55	76	73	78	72	109	97	49	81	109	81	119	79	61	67	119	88	89	79	95	65	70	53	64	62	78	-	77	81	81	106	81	80									
A538SW	0.056	58	78	75	74	103	150	50	75	70	88	88	112	82	91	63	69	72	92	77	98	78	92	97	77	73	74	66	64	81	79	83	83	83	83	83							
A540NE	0.033	47	65	63	67	62	93	83	42	62	59	74	69	93	70	102	68	67	52	57	102	76	76	64	82	65	77	81	65	56	60	53	67	66	70	69	91	69	69				
A540NW	0.034	55	76	73	78	72	109	97	49	72	68	86	81	109	81	118	79	61	67	119	88	75	95	76	89	94	75	65	70	53	64	72	78	-	77	81	81	80					
A540R1	0.028	100	138	132	138	126	195	174	87	130	124	156	145	198	148	212	146	144	111	112	218	161	159	135	174	139	160	171	137	119	127	97	117	113	142	-	141	148	140	195	147	145	
A540R2	0.030	100	138	132	138	126	195	174	87	130	124	156	145	198	148	212	146	144	111	112	218	161	159	135	174	139	160	171	137	119	127	97	117	113	142	-	141	148	140	195	147	145	
A542NE	0.075	70	97	94	100	92	129	113	60	93	88	104	140	144	152	162	103	108	84	82	164	122	123	103	131	105	124	130	104	89	96	73	89	86	108	-	107	112	111	146	111	111	
A542R1	0.060	200	276	263	269	254	386	345	171	252	252	314	292	386	303	411	295	295	225	240	442	322	312	273	340	283	320	352	270	232	255	197	236	226	287	-	288	301	263	398	294	290	
A542R2	0.114	381	524	499	511	483	734	655	325	479	479	597	555	734	578	611	560	560	457	427	457	840	612	745	420	485	375	447	430	545	-	548	571	499	756	559	552						
A543NE	0.063	76	103	99	108	95	148	132	66	98	97	139	140	148	116	160	107	106	90	101	151	120	101	120	137	127	127	127	127	127	127	127	127	127	127	127	127	127					
A543NW	0.076	74	103	99	105	97	132	118	66	109	147	130	160	160	107	106	82	90	90	161	129	103	121	137	127	127	127	127	127	127	127	127	127	127	127	127	127	127	127	127	127		
A543R1	0.100	93	130	125	133	123	187	167	83	124	117	147	138	187	129	130	104	114	204	151	152	128	163	130	153	161	129	111	119	91	110	104	132	-	132	139	138	181	138	137			
A543R2	0.175	585	804	766	784	741	1,126	1,000	499	736	736	916	851	1,126	883	1,198	861	860	656	656	701	796	1,013	824	922	1,025	1,025	787	676	745	576	687	661	836	-	841	877	766	1,160	858	847		
A544NE	0.083	89	121	118	121	117	157	142	97	99	118	131	139	117	158	117	159	117	159	117	159	137	159	134	159	134	159	134	159	134	159	134	159	134	159	134	159	134	159	134	159	134	159
A544NW	0.071	27	37	34	35	34	54	48	24	36	34	42	40	54	58	39	39	33	43	44	37	47	37	44	46	32	31	39	38	40	40	52	40	52	40	52	40	52	40	52	40	52	40
A544R1	0.117	183	256	245	262	241	367	328	163	244	230	239	289	272	367	273	399	267	264	205	224	400	296	303	252	320	301	316	253	218	234	179	216	209	263	-	260	273	271	355	271	270	
A545NE	0.137	163	156	162	154	204	230	194	79	171	187	194	184	230	194	230	174	174	184	153	143	163	143	143	143	143	143	143	143	143	143	143	143	143	143	143	143	143	143	143	143	143	
A545NW	0.122	95	132	127	135	125	190	176	84	126	119	149	141	190	141	166	126	155	153	153	153	153	153	153	153	153	153	153	153	153	153	153	153	153	153	153	153	153	153				
A545R1	0.059	53	88	86	98	88	143	125	53	79	75	114	104	140	135	141	137	137	137	137	137	137	137	137	137	137	137	137	137	137	137	137	137	137	137	137	137	137	137	137			
A550NE	0.169	101	140	133	144	132	208	180	90	134	126	159	150	202	150	129	147	145	113	123	220	163	165	139	176	141	166	139	176	141	166	139	176	141	166	139	176	141	166	139	176	141	166
A550NW	0.076	79	111	106	113	105	159	142	71	106	99	125	118	159	118	172	115	114	89	97	113	128	123	109	139	111	130	137	109	94	101	94	111	117	117	117	117	117	117	117			
A551NE	0.056	63	88	85	91	83	123	116	56	92	109	127	124	157	113	127	124	126	126	126	126	126	126	126	126	126	126	126	126	126	126	126	126	126	126	126	126	126	126	126			
A551SE	0.135	96	119	115	122	113	173	153	76	114	107	135	127	171	127	186	125	125	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123				
A551SW	0.126	84	108	104	114	108	164	148	43	64	57	29	43	40	51	48	64	48	46	36	39	70	52	52	44	56	45	53	44	38	41	31	38	37	46	-	46	48	47	47	47		
A550SPK1	1.660	4,396	6,132	5,881	6,296	5,787	8,870	7,875	3,914	5,861	5,510	6,925	5,649	8,822	6,541	9,572	6,395	5,374	9,594	7,106	6,044	7,675	6,133	7,258	5,604	5,228	4,285	5,189	5,002	6,316	-	6,271	6,537	6,541	8,526	6,491	6,477						
A557NE	0.056	81	98	76	116	104	142	130	82	77	73	92	86	126	85	84	65	71	127	94	96	80	101	95	100	89	69	74															

Table B5- Groundwater  
Yearly Sub-Surface Evap Volumes (m<sup>3</sup>)

**Table B5- Groundwater  
Yearly Sub-Surface Evap Volumes (m<sup>3</sup>)**