

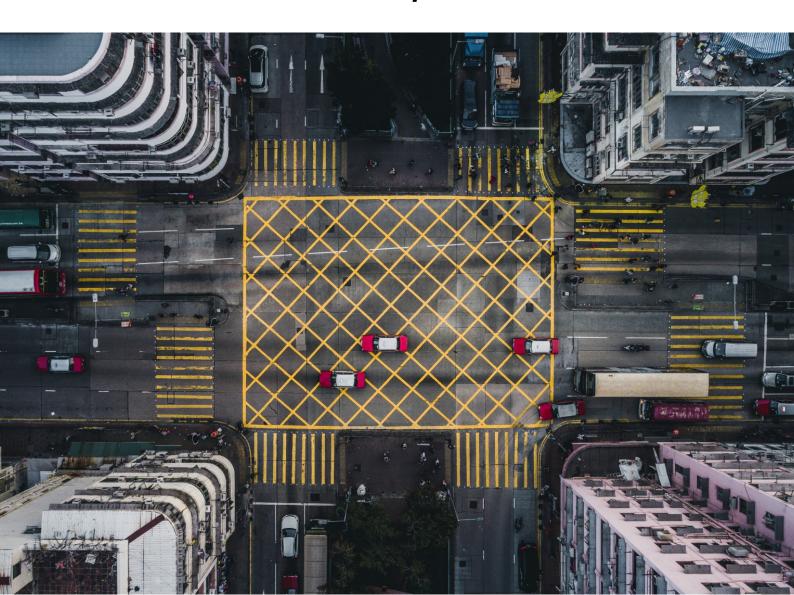
Hydrogeological Assessment

Large Sewage Disposal System, Rideau Road and Somme Street, Ottawa, Ontario

Consolidated Fastfrate (Ottawa) Holdings Inc.

2 November 2021

→ The Power of Commitment



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1. Introduction

This report presents the results of a hydrogeologic assessment that was completed by GHD Limited (GHD) in support of a large sewage disposal system (the System) for Consolidated Fastfrate (Ottawa) Holdings Inc. The System is to be constructed on lands located southeast of the intersection of Rideau Road and Somme Street, Ottawa, ON (herein referred to as "the Site"). The location of the Site is depicted on the **Site Plan Location**, **Figure 1**.

The Site consists of a vacant parcel and has an overall area of 7.02 hectares (17.35 acres). The proposed development is to consist of a warehouse, cross-docks and office building that will be privately serviced for water and septic. The Site will also consist of asphalt parking and a storm water pond. The proposed layout of the Site is illustrated on the **Concept Plan, Figure 2**.

Based upon design flow values provided to GHD, the sewage effluent discharged to the septic bed will be greater than 10,000 L/day. This assessment will be used to support an application for an Environmental Compliance Approval (ECA) with the Ministry of the Environment, Conservation and Parks (MECP) for a Chapter 22 Large Subsurface Sewage Disposal System.

This hydrogeological assessment was completed to evaluate the ability of the Site to support the sewage disposal system proposed for the development as the assessment is required by the MECP to review prior to a preconsultation meeting.

1.1 Terms of Reference

GHD was retained by Consolidated Fastfrate (Ottawa) Holdings Inc. (the Client) to complete this hydrogeological assessment in accordance with our proposal reference no. PG-5306, dated October 14, 2021.

GHD (formerly Inspec Sol and Conestoga-Rovers & Associates) completed a Geotechnical Investigation and Phase II Environmental Site Assessment for the Site in 2008 and 2009, respectively; a Geotechnical Investigation in 2020; a Hydrogeological Assessment related to pumping test of a water well in 2020 (report dated 2021); and a Septic Assessment and Percolation Rate Evaluation in 2021.

GHD has reviewed the following documents made available to us as part of this assessment:

- Phase II Environmental Site Assessment and Hydrogeological Assessment, Report Ref. No. 045804 (12), by Conestoga-Rovers & Associates, dated September 2008;
- Hydrogeological Investigation, Terrain Analysis and Impact Assessment, Proposed Industrial Subdivision,
 Report Ref. No. 08-1122-0215, by Golder Associates, dated December 2008;
- Geotechnical Study Subdivision Plan, Hawthorne Industrial Park, Report Ref. No. T020556-A1, by Inpec-Sol, dated May 4, 2009;
- Geotechnical Investigation Report, Report Ref. No. 11215612-A1 by GHD Limited, dated September 10, 2020;
- Hydrogeological Assessment Report, Report Ref. No. 11220832, by GHD Limited, dated January 19, 2021;
 and,
- Septic Assessment and Percolation Rate Evaluation, Report Ref. No. 11220832-01, by GHD Limited, dated April 12, 2021.

1.2 Purpose and Scope

The purpose of the hydrogeologic assessment was to define the prevailing hydrogeological conditions and demonstrate the ability of the Site to support a sewage disposal system. To accomplish the foregoing purposes, the following scope of work was conducted:

 A desktop review of groundwater information from existing monitoring wells and reports to assess the direction of groundwater flow. Reviewed soil stratigraphy from reports completed for the Site and local area;

- Reviewed available background information relevant to the Site such as geologic, physiographic and water resources reports and maps;
- Completed a Reasonable Use Concept (RUC) assessment for nitrate and assessed the potential for phosphorus impacts;
- Summarized our findings within this hydrogeological report to meet the general requirements of the MECP's Chapter 22 for Large Subsurface Sewage Disposal Systems.

1.3 Limitations

This report has been prepared by GHD for Consolidated Fastfrate (Ottawa) Holdings Inc., and may only be used and relied on by Consolidated Fastfrate (Ottawa) Holdings Inc., for the purpose agreed between GHD and Consolidated Fastfrate (Ottawa) Holdings Inc., as set out in Section 1.1 of this report.

GHD otherwise disclaims responsibility to any person other than Consolidated Fastfrate (Ottawa) Holdings Inc., arising in connection with this report. GHD also excludes implied warranties and conditions, to the extent legally permissible.

The services undertaken by GHD in connection with preparing this report were limited to those specifically detailed in the report and are subject to the scope limitations set out in the report.

The opinions, conclusions and any recommendations in this report are based on conditions encountered and information reviewed at the date of preparation of the report. GHD has no responsibility or obligation to update this report to account for events or changes occurring subsequent to the date that the report was prepared.

The opinions, conclusions and any recommendations in this report are based on information and assumptions made by GHD and described in this report. GHD disclaims liability arising from any of the assumptions being incorrect.

2. Site Conditions

The Site consists of vacant lands. The areas to the north, east and south are currently privately serviced. To the west is a quarry development and additional industrial / commercial properties that are municipally serviced. Surrounding land use within 500 m of the Site at the time of this report were observed to consist of:

- East undeveloped lands;
- West undeveloped lands; Hawthorne Road then industrial properties (Tomlinson Rideau Quarry and Plant; LaFarge);
- North Rideau Road, forested area then residential lots; and
- South Somme Street; undeveloped lands then industrial / commercial lots (gated equipment lay-down yard and stormwater ponds; then Renewi Canada Ltd.).

Within 500 m of the proposed development, one residential lot was observed at 4885 Hawthorne Road (north of the Site).

2.1 Topography

The regional topography is presented on **Figure 3**. The Site is relatively flat with the regional topography sloping from southwest to northeast. Based upon a survey plan reviewed by GHD, the topographic relief is on the order of 1 to 2 metres across the Site.

2.2 Physiography

The Site is situated within the physiographic region known as the Russell and Prescott Sand Plains. In the United Counties of Prescott and Russell, and the Regional Municipality of Ottawa-Carleton, there is a group of large sand plains separated by the clays of the lower Ottawa Valley. The plains cover an area of nearly 1,500 square

kilometres and a level surface of about 85 metres above sea level. The plains were originally a continuous delta that was built by the Ottawa River into the Champlain Sea. The plains are as thick as 6 to 10 m in some areas (Chapman and Putnam, 1984). The physiography of the area is illustrated on **Figure 4** showing the Site is within a sand plains with Peat and Muck to the north and Limestone Plains to the west.

2.3 Regional Geology

Surficial geology mapping presented on **Figure 5** indicates the Site is a mix of organic deposits, Paleozoic bedrock and coarse textured glaciolacustrine deposits.

The Quaternary geology is presented on **Figure 6** and suggests undifferentiated carbonate and clastic sedimentary rock exposed at surface or covered by a discontinuous thin layer of drift. Bedrock outcrops are common in the area.

The bedrock of this area, as presented on **Figure 7**, is comprised of shale, limestone, dolostone, and siltstone.

2.4 Local Geology

An investigation was previously conducted by GHD as part of an assessment of the soils and subsurface conditions in the area of the proposed septic system. The report is provided for reference in **Appendix A** of this document. An overview of our observations made during the subsurface exploration are presented in the following sub-sections.

2 4 1 Overburden Soil

On March 31, 2021, five (5) test pits were advanced under the supervision of GHD to depths ranging from 2.4 to 3.4 metres below ground surface (mbgs). The locations of the test pits are presented on Figure 2 of the report provided in Appendix A. Field logs were maintained of the underlying soil conditions throughout the test pit activities.

The soil stratigraphy consisted of fill at each location described as gravelly sand with silt trace clay to a silty sand with gravel and clay. Fill was observed to the bottom of each test pit. The fill also included a mix of asphalt, bricks and concrete at each location. Refusal was encountered at 2.4 m at TP-1 due to asphalt. Hydrometer testing of the fill material indicated 18 to 41% gravel, 36 to 47% sand, 12 to 23% silt, and 4 to 12% clay sized particles by weight. The percolation rate of the fill was estimated to have an average value of 12 to 20 min/cm with a medium permeability.

Based upon GHD's previous geotechnical work at the Site, the upper soils are comprised of fill to depths on the order of 6 mbgs (GHD, 2020). Underlying the fill at BH-1 documented in the geotechnical report was native silty sand to a depth of 8.2 mbgs where limestone bedrock was encountered (GHD, 2020).

Prior to GHD's investigations at the Site, drilling and test pits were advanced across the Site and a larger industrial park area as documented in Golder (2008). At the Site, monitoring well MW7-08 was drilled to a depth of 6.1 mbgs encountering fill to a depth of 5.4 mbgs then underlain by glacial till. The well is screened bridging the fill and till layers. Bedrock was not encountered. The borehole was terminated at 7 mbgs (Golder 2008).

In general, soils encountered in previous subsurface test holes at the Site and in this general area consisted of a layer of fill material described as gravelly sand with silt trace clay to a silty sand with gravel and clay overlying a native silty sand / sandy silt deposit followed by glacial till or limestone bedrock. The location of the test holes located on the Site are shown on Figure 8.

242 Bedrock

Bedrock was found at 8.5 mbgs based upon the well record for test well TW-2 and at a depth of 8.2 mbgs at BH-1. Bedrock was not encountered at MW7-08 to a depth of 7 mbgs and was not encountered in the test pits excavated in the area of the proposed septic bed area.

2.5 Description of Surface Water Features

No surface water features are present on the Site. There are no permanent water features (i.e. creeks, lakes, rivers etc) within 300 m of the Site.

3. Hydrogeology

The following section describes the regional and local hydrogeology including groundwater flow direction and hydrochemistry.

3.1 Regional Hydrogeology

Information regarding the groundwater characteristics of the area within 500 m of the Site was obtained from an inventory of existing MECP well records. A total of seventeen (17) water well records were identified for statistical breakdown. The data has been summarized in Table 1. The MECP well records and the approximate locations are provided in **Appendix B**.

3.2 Water Well Records

The information from the MECP data indicates a mix of overburden materials (fill, sand, clay, gravel etc.) overlying bedrock including shale, sandstone, limestone and quartz. Based upon the well records, there is one (1) primary bedrock aquifer in this immediate area that is tapped by drilled wells. Of the seventeen (17) records, seven (7) are monitoring wells and will not be considered further within this discussion.

The groundwater was generally described as "fresh" in the well records reviewed. The information from the MECP data indicates that all ten (10) wells were drilled bedrock wells averaging a depth of about 41 m. The bedrock wells encountered water at an average depth of 31 m with pumping rates averaging nearly 100 L/min. No flowing artesian wells were reported. A summary of the MECP well record data is presented in Table 1 below.

Table 1 Summary of Water Well Records

Total Number of Wells Inventoried: 17
Dug/Bored Wells: 0 (0%)
Drilled Wells (Overburden): 0 (0%)
Drilled Wells (Bedrock): 10 (59%)
Monitoring Wells*: 7 (41%)

Mornically volice. 7 (1170)									
Davamatava	Statistical Summary		Statistical Summary		Statistical Summary				
Parameters	Dug / B	ored Wells	Drilled –	Overburden	Drilled – Bedrock				
WELL YIELDS									
Range	L/min	USgpm	L/min	USgpm	19 to 680 L/min	5 to 180 USgpm			
Average	L/min	USgpm	L/min	USgpm	99.1 L/min	26.2 USgpm			
REPORTED YIELDS	Frequency								
Not Reported	0	0%	0	0%	0	0%			
Dry	0	0%	0	0%	0	0%			
0 to 1 USgpm	0	0%	0	0%	0	0%			
2 to 4 USgpm	0	0%	0	0%	0	0%			
5 to 9 USgpm	0	0%	0	0%	6	60%			
≥10 USgpm	0	0%	0	0%	4	40%			
STATIC WATER LEVELS									
Range	N/A	N/A	N/A	N/A	2.3 to 14.2 m	7.5 to 46.6 ft			
Average	N/A	N/A	N/A	N/A	8.4 m	27.6 ft			
WATER ENCOUNTERED									
Range	N/A	N/A	N/A	N/A	9.1 to 75.0 m	30 to 246 ft			
Average	N/A	N/A	N/A	N/A	31.2 m	103.5 ft			
WELL DEPTH									
Range	N/A	N/A	N/A	N/A	17.4 to 75.6 m	57 to 248 ft			
Average	N/A	N/A	N/A	N/A	40.8 m	133.9 ft			

Notes: Data based on MECP well record information (see Appendix B). L/m represents litres per minute, USgpm indicates US gallons per minute and m is metres. *Monitoring wells are not included in the statistical data summarized.

3.3 Groundwater

Based upon information reviewed, there are two hydrogeological units identified at the Site and in this general area. The first is a shallow zone of water within either the fill, the shallow native overburden or upper bedrock. Previous reports indicate that the groundwater flow in the shallow zone is to the northeast at a gradient of approximately 0.015 m/m (Golder, 2008). Groundwater was encountered within the overburden in each of the five (5) test pits advanced by GHD in 2021 at depths observed between 1.8 and 2.4 mbgs. At MW7-08, water was encountered at a depth of 3.65 mbgs. Water levels measured at MW7-08 in November 2020 indicated a water level at 3.00 mbgs. The shallow groundwater flow direction of northeast across the Site will be utilized during the RUC impact assessment for the proposed septic system.

A deeper confined aquifer found within the bedrock, generally at depths of 25 to 35 metres below ground surface. This aquifer is proposed for water supply for the development. Based upon the water levels collected by GHD in November 2020, the regional groundwater flow within the bedrock is also in a northeasterly direction. Previous studies have indicated the groundwater flow in the bedrock to be in a west to east direction at a gradient of approximately 0.005 m/m (Golder, 2008). Test well TW-2 is constructed within the deeper confined aquifer. During pumping tests conducted by others and by GHD in 2020, the testing indicated that there was no hydraulic connectivity between the shallow water zone and deeper confined aquifer.

3.3.1 Background Groundwater Chemistry

Background groundwater chemistry is provided in **Table 2**. Water samples were collected previously by CRA at MW7-08 on July 17, 2008 (CRA, 2008) and at TW-2 on November 19, 2020 during a pumping test conducted at this location (GHD, 2021).

The results of the chemical analysis from the original reports are summarized in **Table 2**. The analytical data is relatively low for nitrogen-based compounds within the shallow water zone and very low to non-detect within the drinking water aquifer. There were detections of bacteria within the shallow water zone; however, the deeper confined unit was non-detect for bacteria confirming there is a lack of connectivity hydraulically between the shallow and deeper units.

Table 2 Analytical Groundwater Data

	We	II Identifier		О	ODWS MAC AO/OG		
Parameter	MW7-08 TW-2*						
	July 17, 2008	Novemb	er 19, 2020*	MAC	AU/UG		
Alkalinity (as CaCO ₃)	840	269	267		30 to 500		
Ammonia	2.24	0.25	0.25				
Chemical Oxygen Demand	110						
Chloride	297	91	94		250		
Conductivity (µmho/cm)	2620	1390	1380				
Dissolved Organic Carbon	25	2.4	2.2				
Nitrate (N)	< 0.3	<0.01	<0.01	1.0			
Nitrite (N)	< 0.3	<0.05	<0.05	10			
рН	7.51	7.8	7.7				
Phenol	0.008						
Phosphorus	2.50						
Sulfate	271	378	389		500		
Total Dissolved Solids	1710	930	940		500		
Total Kjeldahl Nitrogen	4.20	0.3	0.4				
E.coli	5		Non-detect				
Total Coliform	3800		Non-detect				
Fecal Coliform	6		Non-detect				

	Well Id	dentifier		ODWS		
Parameter	MW7-08	TW-2*		MAC	A0/00	
	July 17, 2008	Novembe	r 19, 2020*	MAC AO/OG		
Heterotrophic Plate Count	<500		<10			

Notes:

(<) indicates below laboratory detection limit, **bolded** values exceed ODWS

Units are in mg/L unless otherwise stated.

MAC - Maximum Acceptable Concentration; AO - Aesthetic Objective; OG - Operational Guideline

4. Septic Design

The septic design is being completed by others. It is GHD's understanding that the daily design flow will be 12,800 L/day based upon the building size and warehouse loading bays. The daily design flow provided to GHD will be used to conduct the impact assessment.

As indicated within our Septic Assessment letter (Appendix A), the underlying soils was a mix of fill materials. It was recommended that the tile bed be a fully raised adsorption trench leaching bed due to the inconsistency of the fill materials observed and shallow groundwater seepage observed. The existing fill material is recommended to be compacted to ensure uneven settlement of the tiles does not occur.

The proposed tile bed area and the existing water well (i.e. TW-2) are a distance of about 50 m apart from each other. The minimum setback from a tile bed and drilled well is 15 m. It is our opinion that there is minimal potential for groundwater impact as a result of the planned development from a quality perspective provided that the septic system is constructed properly.

No further discussion of septic design is provided in this report.

5. Impact Assessment

5.1 Site Specific Considerations

Based upon our assessment, it is our opinion that the Site can be serviced with a fully raised adsorption trench leaching bed. The location of the proposed leaching bed and the dilution area, based on the groundwater flow direction is presented on **Figure 9**.

The potential impacts from the leaching bed are discussed in the following sections.

5.2 Nitrate Assessment

5.2.1 Nitrate Loading

Primarily, nitrate impact is of particular concern from a groundwater perspective. A conventional treatment system is proposed for the septic system. Nitrate dilution was calculated in order to assess the potential impact on the downgradient receptors. Section 22.5.7 of the MECP's Chapter 22 indicates that existing and background concentrations of critical contaminants should generally be used only for reference, not for calculation of allowable water quality limits. The following assumptions were used in the nitrate impact calculations:

- Nitrate in the untreated sewage is estimated to be on the order 40 mg/L;
- The dilution area for the leaching bed is assumed to be approximately 17,035 m² based on the proposed configuration of the leaching bed and general groundwater flow direction;
- The estimated recharge rate of 250 mm/year was used as specified in Chapter 22; and
- Design flow of 12,800 L/day.

^{*}TW-2 sampled during a pumping test after 1 hour of pumping and at the end of the test (6 hours)

The following equations were used to predict the potential impact of nitrate to the shallow groundwater:

Equations: Eq'n # $V_A = A_D \times k \qquad (1)$ $V_T = V_A + V_S \qquad (2)$ $C_{PB} = (C_S \times V_S) / V_T \qquad (3)$

Where:

 V_A = annual dilution volume [m³]

 A_D = dilution area [m²]

 V_T = total volume of water [m³]

V_S = annual sewage volume [m³]

C_{PB} = concentration at property boundary [mg/L]

Cs = concentration in sewage [mg/L]

k = 0.25 m Annual Dilution Precipitation Rate as per the MECP.

Based on our understanding of the groundwater flow direction and the daily design effluent loading, the following is presented:

 $A_D = 17,035 \text{ m}^2$ Infiltration area from **Figure 9**

 $V_A = 4,259 \text{ m}^3$ Annual dilution volume

 $V_S = 4,672 \text{ m}^3$ Loading of an average of 12,800 L/day

 $V_T = 8.931 \text{ m}^3$ Total water volume

C_S = 40 mg/L Effluent Nitrate Concentration

C_{PB} = 20.9 mg/L Nitrate concentration expected at site boundary

Using dilution only, the nitrate concentration generated from sewage at the Site is calculated to be 20.9 mg/L. The calculations are provided in **Appendix C**.

It is understood that the MECP generally targets a RUC value of 2.5 mg/L at the property boundary (25% of the Ontario Drinking Water Standard for nitrate which is 10 mg/L). Based upon the calculations to meet a nitrate concentration of 2.5 mg/L, treatment is required to reduce nitrate to 4.8 mg/L as it is discharged into the tile bed in order for dilution to reduce the nitrate concentration to meet the RUC value. The nitrate dilution calculations do not consider other factors such as denitrification or dilution within existing groundwater.

5.3 Phosphorus Impact Assessment

The main source of additional phosphorus loading from the Site would be associated with the treated wastewater effluent. The distance between the Site and the nearest water body is about 12 kilometres to the Rideau River (inferred to be upgradient of the Site). The nearest downgradient surface water receiver is greater than 12 kilometres. As per Chapter 22 for Large Subsurface Sewage Disposal Systems, a separation distance of 300 m between the area of sewage infiltration and a surface water body should be sufficient to ensure that there are no appreciable effects to surface water quality due to phosphorous.

6. Conclusions and Recommendations

The supporting data upon which our recommendations are based, have been presented in the foregoing sections of this report. Based on the results of this assessment, it is the opinion of GHD that the Site is suitable for a fully raised bed to service the facility provided tertiary treatment is utilized to reduce the expected nitrate concentrations. Based upon the information reviewed and assumptions made by GHD, the effluent of the sewage system will flow laterally toward the northeast with minimal vertically migration into the deeper underlying bedrock aquifer accessed by the Site's groundwater well. To the northeast beyond the Site, there are no downgradient wells in close proximity.

6.1 Groundwater

Shallow water was encountered within the fill in the area of the proposed fully raised bed. The shallow groundwater flow direction was indicated to be toward the northeast. Based on the information assessed, it is our opinion that good construction and mitigation techniques must be used to minimize the potential for impact.

It is our opinion that there is minimal potential for groundwater impact as a result of the planned development from a quality perspective provided that the septic system is constructed properly.

6.2 Impact Assessment

Based on the impact assessment, tertiary treatment will be required. Following treatment, there is minimal potential impact from the proposed septic system. This is based on the distance to downgradient wells (i.e. there are no groundwater receivers of the effluent in close proximity of the Site), the presence of relatively low permeable soils above the underlying bedrock aquifer, and no surface water within 300 m that would be adversely affected by phosphorous.

It is the professional opinion of GHD that the proposed sewage system will have no significant impact on the groundwater aquifer, shallow water or any downgradient receptors that utilize groundwater.

6.3 Signatures

The following signatures are provided of GHD staff that prepared and conducted the hydrogeological assessment. Should questions arise regarding any aspect of our report, please contact the undersigned or our office.

Nect.

Sincerely,

GHD

Steven Gagné, H.B.Sc. Associate, Project Director

Steven Granie

/KG/bn/sg

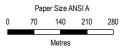
Robert Neck, P. Geo. (Limited) ONTARIO
Associate Project Director

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Figures







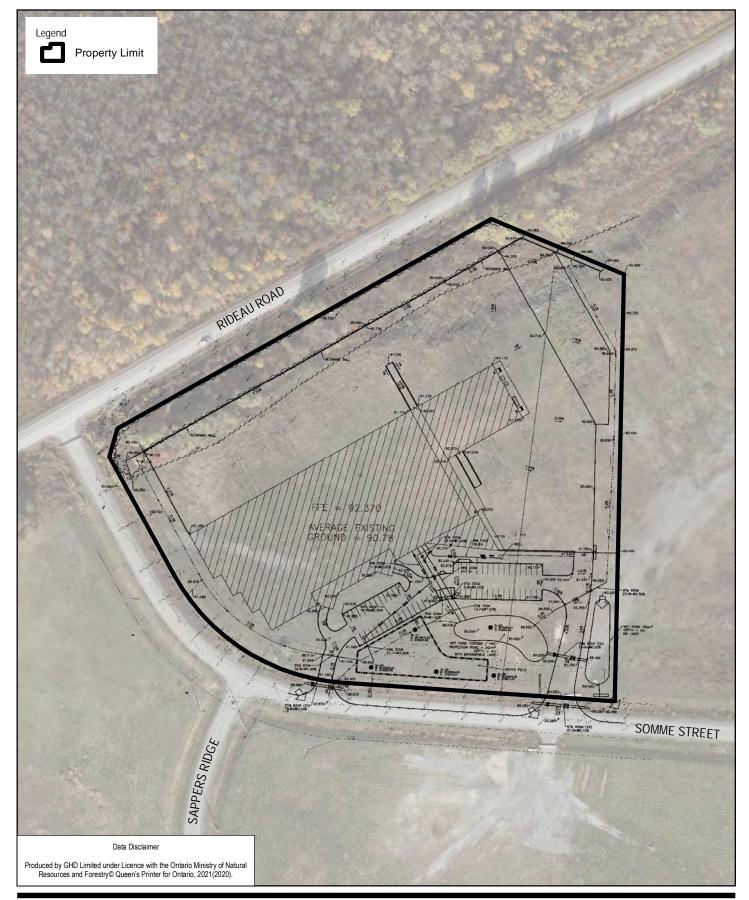
GHD

CONSOLIDATED FASTFRATE (OTTAWA) HOLDINGS LTD.
301 SOMME STREET, OTTAWA, ON

301 SOMME STREET, OTTAWA, NN PT LOT 26, CON 6 FROM RIDEAU RIVER GEOGRAPHIC TOWNSHIP OF GLOUCESTER CITY OF OTTAWA

HYDROGEOLOGICAL ASSESSMENT-ON-SITE SEWAGE SYSTEM SITE LOCATION PLAN Project No. 12565773 Revision No.

Date Oct 29, 2021









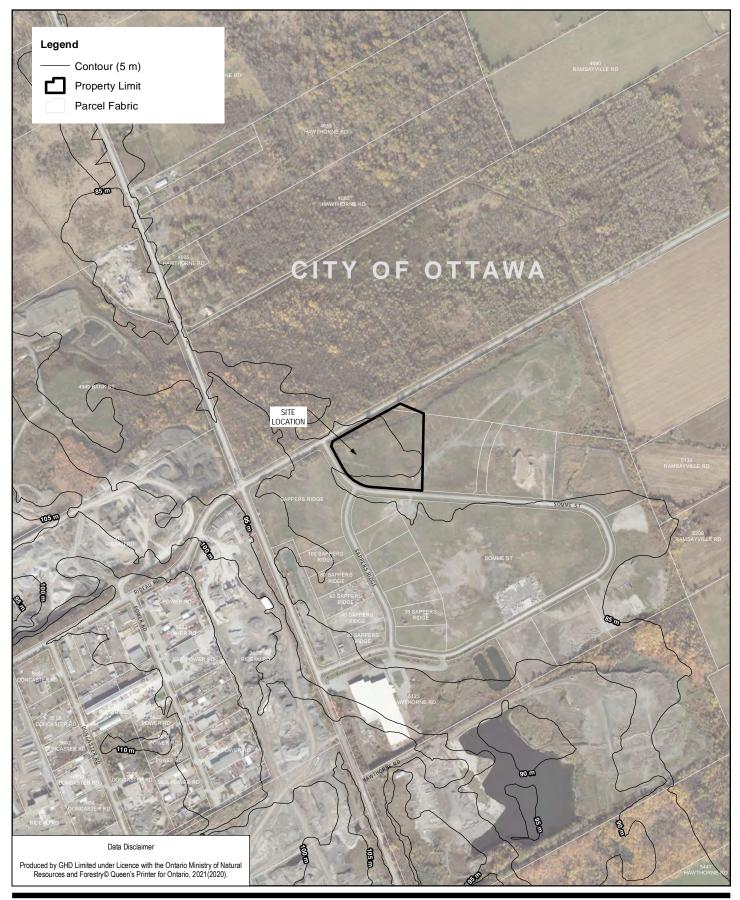
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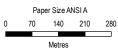
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HYDROGEOLOGICAL ASSESSMENT-ON-SITE SEWAGE SYSTEM **CONCEPT PLAN**

12565773 Project No. Revision No.

Date Oct 29, 2021







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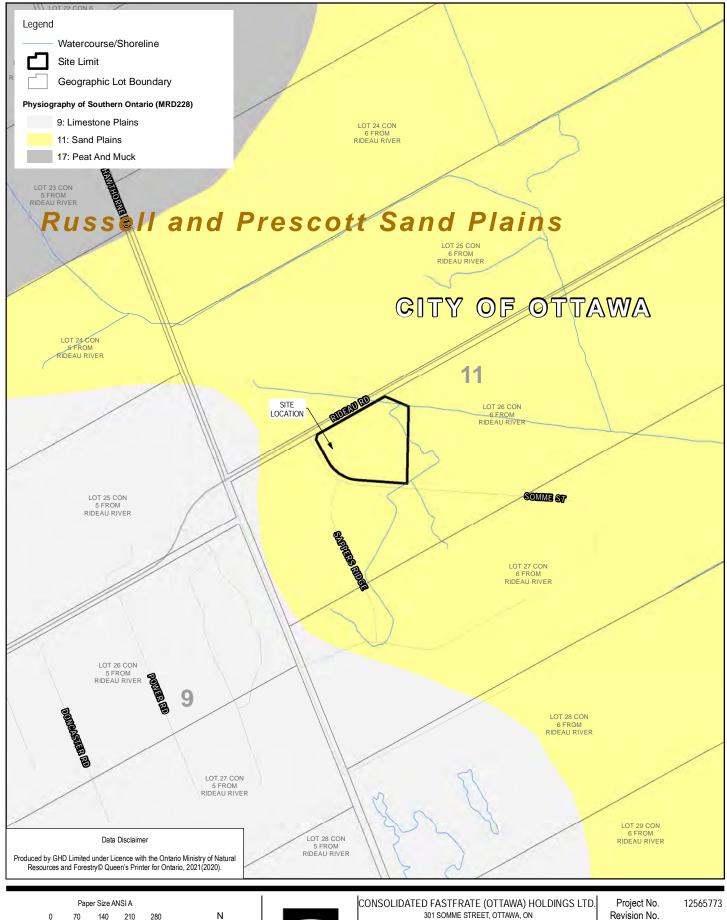
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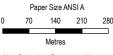
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Date Oct 29, 2021





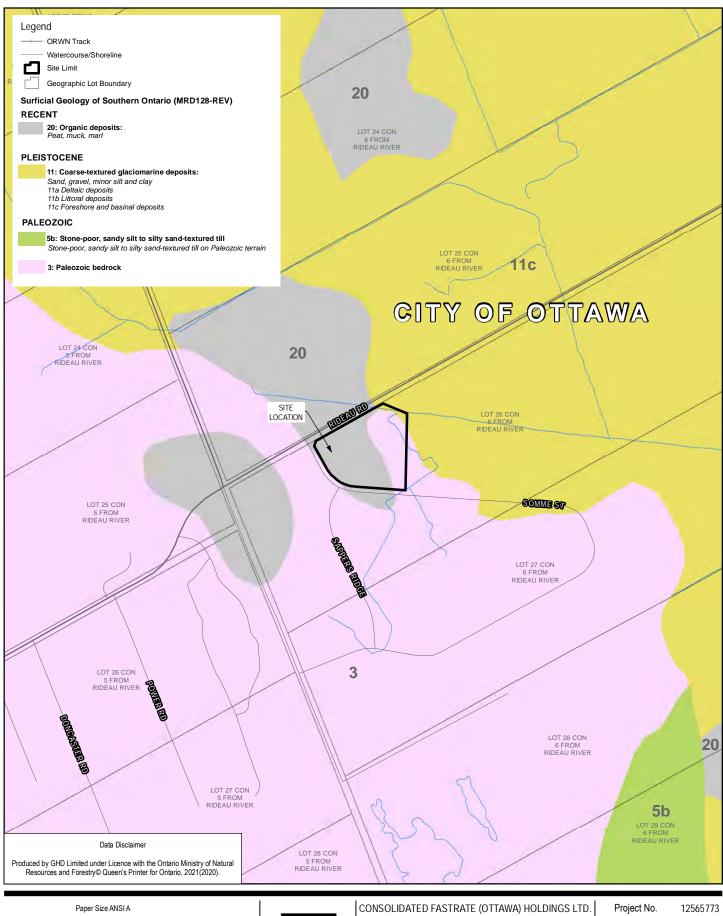


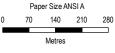
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PT LOT 26, CON 6 FROM RIDEAU RIVER GEOGRAPHIC TOWNSHIP OF GLOUCESTER CITY OF OTTAWA

HYDROGEOLOGICAL ASSESSMENT-ON-SITE SEWAGE SYSTEM **PHYSIOGRAPHY**

Date Oct. 2021







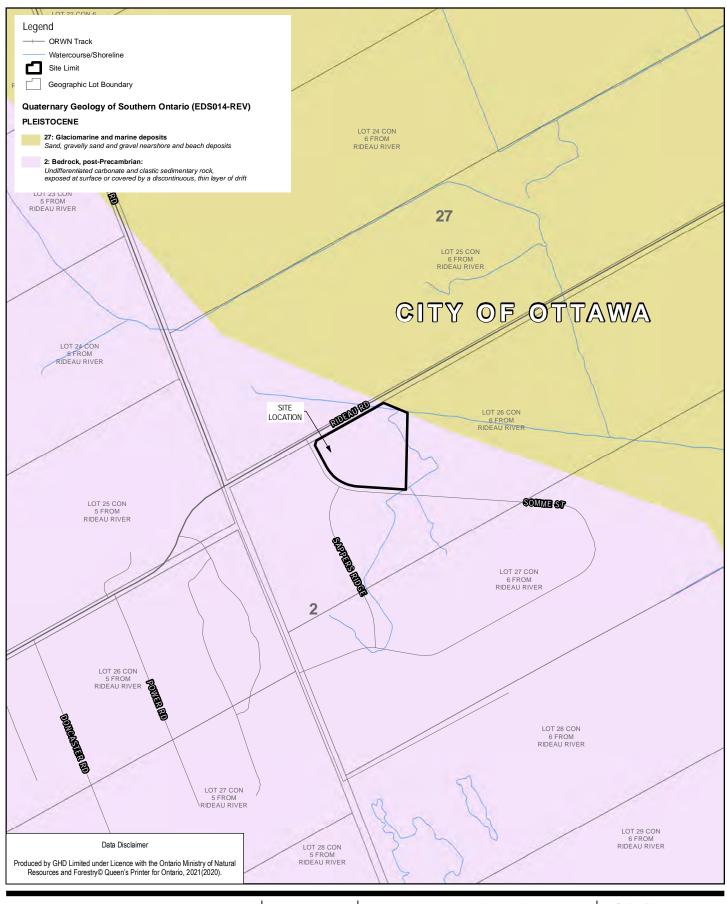
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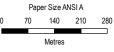
PT LOT 26, CON 6 FROM RIDEAU RIVER GEOGRAPHIC TOWNSHIP OF GLOUCESTER CITY OF OTTAWA

HYDROGEOLOGICAL ASSESSMENT-ON-SITE SEWAGE SYSTEM SURFICIAL GEOLOGY

Revision No.

Date Oct. 2021







GHD

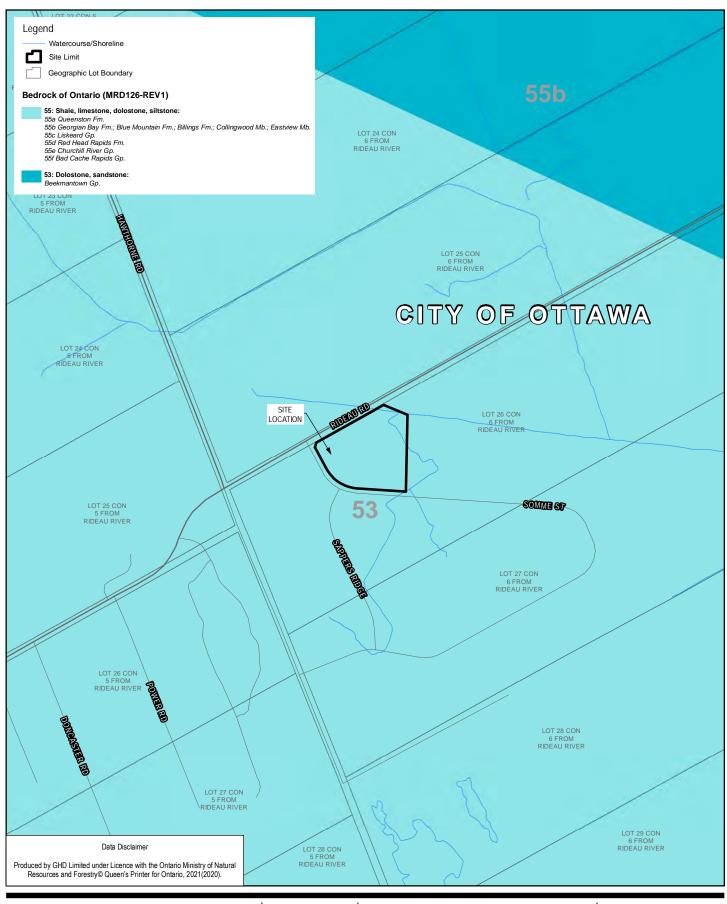
CONSOLIDATED FASTFRATE (OTTAWA) HOLDINGS LTD.

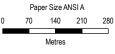
301 SOMME STREET, OTTAWA, ON

301 SOMME STREET, OTTAWA, ON PT LOT 26, CON 6 FROM RIDEAU RIVER GEOGRAPHIC TOWNSHIP OF GLOUCESTER CITY OF OTTAWA

HYDROGEOLOGICAL ASSESSMENT-ON-SITE SEWAGE SYSTEM QUATERNARY GEOLOGY Project No. 12565773 Revision No.

Date Oct. 2021







GHD

CONSOLIDATED FASTFRATE (OTTAWA) HOLDINGS LTD. 301 SOMME STREET, OTTAWA, ON PT LOT 26, CON 6 FROM RIDEAU RIVER

PT LOT 26, CON 6 FROM RIDEAU RIVER GEOGRAPHIC TOWNSHIP OF GLOUCESTER CITY OF OTTAWA

ON-SITE SEWAGE & SEPTIC ASSESSMENT BEDROCK GEOLOGY

Project No. 12565773 Revision No.

Date Oct. 2021







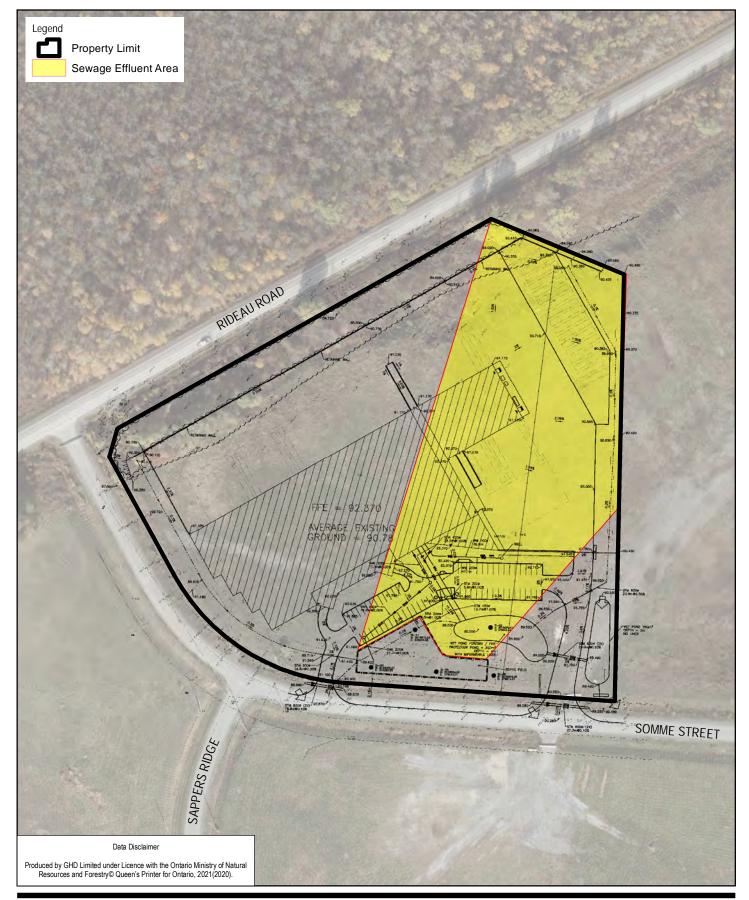
CONSOLIDATED FASTFRATE (OTTAWA) HOLDINGS LTD.
301 SOMME STREET, OTTAWA, ON
PT LOT 26, CON 6 FROM RIDEAU RIVER
GEOGRAPHIC TOWNSHIP OF GLOUCESTER

ON-SITE SEWAGE & SEPTIC ASSESSMENT TEST HOLE PLAN

CITY OF OTTAWA

Project No. 12565773 Revision No.

Date Oct. 2021









CONSOLIDATED FASTFRATE (OTTAWA) HOLDINGS LTD.

301 SOMME STREET, OTTAWA, ON
PTI OT 26, CON 6 FROM RIDEAU RIVER

301 SOMME STREET, OTTAWA, ON PT LOT 26, CON 6 FROM RIDEAU RIVER GEOGRAPHIC TOWNSHIP OF GLOUCESTER CITY OF OTTAWA

HYDROGEOLOGICAL ASSESSMENT-ON-SITE SEWAGE SYSTEM SEPTIC EFFLUENT AREA Project No. 12565773 Revision No.

Date Oct. 2021

Appendices

Appendix A

Septic Assessment and Percolation Rate Evaluation Letter 347 Pido Road Peterborough, Ontario K9J 6X7 Canada www.ghd.com



Our ref: 11220832-01

12 April 2021

Consolidated Fastfrate (Ottawa) Holdings Inc. c/o Pierre Courteau CBRE Limited 333 Preston Street, 7th Floor Ottawa, Ontario K1S 5N4

Re: Septic Assessment and Percolation Rate Evaluation Proposed Commercial Development Rideau Road and Somme Street Gloucester Con 6 from Rideau River, Lot 26 Ottawa, Ontario

Dear Mr. Courteau:

1. Introduction

GHD Limited (GHD) is pleased to provide you (the Client) with the following letter documenting excavation activities completed in the general locations of a proposed septic tile bed and stormwater pond. The locations were requested by CIMA. This letter also provides a summary of approximate percolation rate (T-time) values based upon soil collected from the test pit locations.

The general location is illustrated on the Site Location Plan, Figure 1. The test pit locations are illustrated on the Test Pit Location Plan, Figure 2.

2. Field Activities

Test pits were advanced under the supervision of GHD on March 31, 2021. The test pits were excavated at five (5) locations to depths ranging from 2.4 to 3.4 m. The soil stratigraphy consisted of fill at each location described as gravelly sand with silt trace clay to a silty sand with gravel and clay. Fill was observed to the bottom of each test pit. The fill also included a mix of asphalt, bricks and concrete at each location. Refusal was encountered at 2.4 m at TP-1 due to asphalt. Test pit logs are provided in Appendix A.

Soil samples were collected from each test pit. Hydrometer testing was conducted at GHD's laboratory. The grain size data, included in Appendix A, indicated:

18 – 41% gravel; 36 – 47% sand; 12 – 23% silt; and, 4 – 12% clay size particles by weight.

Groundwater seepage was encountered at each test pit. The shallow groundwater was observed between 1.8 and 2.4 metres below ground surface (mbgs). Test pits TP-2, TP-3, TP-4 and TP-5 encountered groundwater at 1.8 mbgs.

Based upon the Supplementary Guidelines to the Ontario Building Code 1997, the percolation rate is estimated (based upon the gradation test results only) to have an average value of 12 to 20 min/cm with a medium permeability.

3. Conclusions and Recommendations

Due to the inconsistency of the fill materials observed and shallow groundwater seepage encountered it is recommended the septic disposal system be a fully raised bed absorption trench leaching bed. It is recommended prior to placement if the imported fill that any surficial organics be removed from the tile bed and mantle area. It is also suggested that that the existing fill material be compacted to ensure uneven settlement of the tiles does not occur.

The waste disposal system should meet Ontario Regulation 350/06 made under the Building Code Act, 1992 and incorporate the following design features:

- 1. Organics should be stripped from the area of the leaching bed and downgradient mantle.
- 2. The exposed subgrade below the tile bed should be trimmed and scarified, and provided with a gentle slope of 0.5% in the direction of the mantle.
- The tile bed should be constructed as a fully raised leaching type bed up to the full height of at least 1
 m above existing grade. The raised bed should consist of clean, granular fill capable of providing an
 in-place T-time of 4 to 8 min/cm.
- 4. The mantle should be constructed along the downgradient margin of the raised bed. Each mantle should extend along the full width of the bed and for a minimum of 15 m downgradient from the bed. The mantle should consist of similar granular fill raised to a minimum of 250 mm above the surrounding grade. Surface runoff should be diverted away from the leaching bed by means of proper site drainage.
- 5. The waste disposal system should be kept clear of surface drainage swales, roof leader drains, and other sources of surface water.
- 6. The tile bed should be kept away from shade trees and a healthy cover of vegetation should be developed and maintained over the bed to promote evapotranspiration.
- 7. When sighting a tile bed on sloping ground, it is recommended that procedures outlined in the Building Code be followed closely.
- 8. Minimum set back distances from septic tank (plus 2 times height raised):
 - Building 1.5 m
 - Drilled well 15 m

- Property line 3 m
- Open water course 15 m
- 9. Minimum set back distances from septic tile bed (plus 2 times height raised):
 - Building 5 m
 - Drilled well, properly sealed 15 m
 - Open water course 15 m

- Property line 3 m
- Shallow well 30 m

10. The layout, design and construction of the waste disposal bed should be subject to inspection by experienced hydrogeologic personnel.

We trust that this report meets your immediate requirements. Should you have any questions, please contact our office.

Regards

GHD

Robert Neck, M.Eng., P.Geo. (Broject Manager

Encl.: Appendix A (Test Pit Logs and Gradation Results)

Email to Pierre Courteau

Cc: Christian Lavoie-Lebel (Christian.Lavoie-Lebel@cima.ca)

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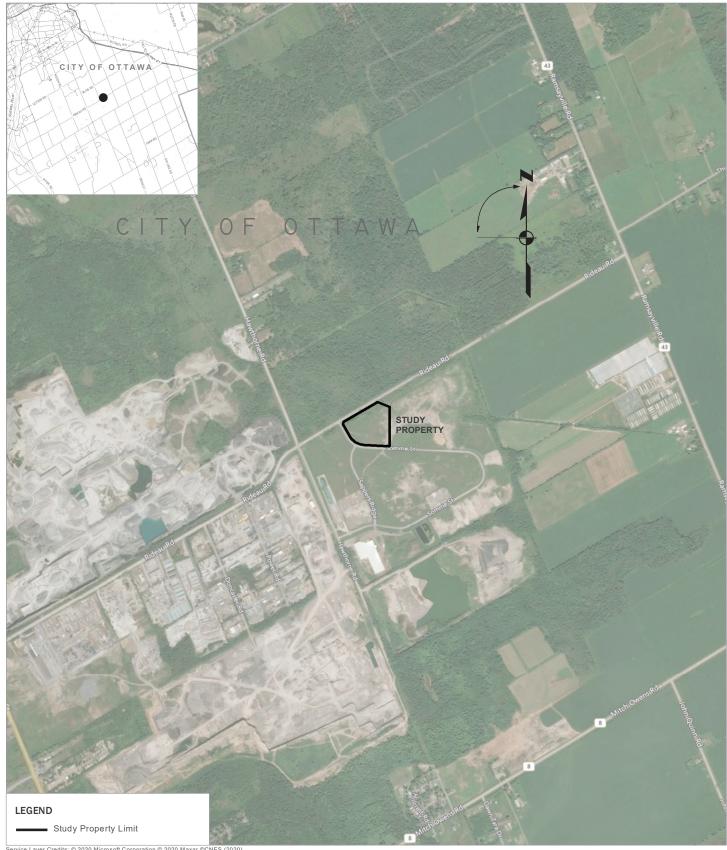
• Property line – 3 III



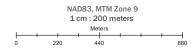
C. McILVE

Attachment 1

Figures



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Distribution Airbus DS © 2020 HERE



ATTRIBUTION STATEMENTS

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Consolidated Fastfrate (Ottawa) Holdings Inc.

RIDEAU ROAD & SOMME STREET CITY OF OTTAWA ONTARIO

SEPTIC ASSESSMENT SITE LOCATION PLAN

Project No. 11220832-01

Revision No. 1

Date Apr 2021



NAD83, MTM Zone 9 1 cm : 16 meters

ATTRIBUTION STATEMENTS

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Consolidated Fastfrate (Ottawa) Holdings Inc.

RIDEAU ROAD & SOMME STREET CITY OF OTTAWA ONTARIO

SEPTIC ASSESSMENT **TEST HOLE LOCATION PLAN**

Project No. 11220832-01

Revision No. 1

Apr 2021

Appendix A

Test Pit Logs and Gradation Results

REFERENCE No.: 11220832 ENCLOSURE No.: ____ A-1 TEST HOLE No.: TP-1 **TEST HOLE REPORT** Existing grade **ELEVATION:** Page: 1 of 1 **LEGEND** Consolidated Fastfrate CLIENT: ___ ☐ GS - GRAB SAMPLE PROJECT: Septic Assessment Ţ - WATER LEVEL DATE: 31 March 2021 LOGGED BY: J. Scott EXCAVATION COMPANY: Goldie Mohr Ltd. METHOD: Backhoe NOTES: <u>18T E: 456548 N: 5017167</u> m Below Existing Grade Shear test (Cu) Sensitivity (S) △ Field Stratigraphy Moisture Content Type and Number **COMMENTS** ☐ Lab Water content (%) Depth **DESCRIPTION OF** Atterberg limits (%) SOIL AND BEDROCK ft 0.0 10 20 30 40 50 60 70 80 90 m **GROUND SURFACE** TOPSOIL (178mm) 0.2 SM - Gravelly sand (fill), with silt, trace clay, concrete, brick, asphalt, compact, 1 - Test pit open upon brown, moist completion 0.5 2 - GS-1 37% Gravel GS-1 47% Sand 12% Silt 3 -4% Clay - 1.0 1.5 6 1.8 With clay, loose - GS-2 41% Gravel GS-2 - 2.0 36% Sand 16% Silt 7 2.1 Wet 7% Clay - Groundwater infiltration observed at TEST HOLE LOG GEOTECH 11220832 TEST PIT GINT LOGS.GPJ GEOLOGIC.GDT 12/4/2/ approximately 2.1 mbgs 2.4 END OF TEST HOLE 2.5 - Refusal at 2.4m (asphalt) 9 3.0 10-3.5 12-13-4.0 14 4.5

ENCLOSURE No.: ____ REFERENCE No.: 11220832 TEST HOLE No.: TP-2 **TEST HOLE REPORT** Existing grade **ELEVATION:** Page: 1 of 1 **LEGEND** CLIENT: ____ Consolidated Fastfrate ☐ GS - GRAB SAMPLE PROJECT: Septic Assessment Ţ - WATER LEVEL DATE: 31 March 2021 LOGGED BY: J. Scott EXCAVATION COMPANY: Goldie Mohr Ltd. METHOD: Backhoe NOTES: <u>18T E: 456572 N: 5017175</u> m Below Existing Grade Shear test (Cu)
Sensitivity (S)
Water content (%) △ Field Stratigraphy Moisture Content Type and Number **COMMENTS** □ Lab Depth **DESCRIPTION OF** Atterberg limits (%) SOIL AND BEDROCK ft 0.0 10 20 30 40 50 60 70 80 90 m **GROUND SURFACE** TOPSOIL (102mm) 0.1 SM - Gravelly sand (fill), with silt, concrete, brick, asphalt, brown, moist 1 -- Test pit open upon completion 0.5 2 3 -- 1.0 GS-1 1.5 6 1.8 Wet - Groundwater infiltration observed at - 2.0 approximately 1.8 mbgs 7 TEST HOLE LOG GEOTECH 11220832 TEST PIT GINT LOGS.GPJ GEOLOGIC.GDT 12/4/2/ 2.5 2.7 9 END OF TEST HOLE 3.0 10-3.5 12-13-4.0 14 4.5

REFERENCE No.: 11220832 ENCLOSURE No.: _ A-3 TEST HOLE No.: _ TP-3 **TEST HOLE REPORT** Existing grade **ELEVATION:** Page: 1 of 1 **LEGEND** Consolidated Fastfrate CLIENT: _ ☐ GS GRAB SAMPLE PROJECT: Septic Assessment ¥ - WATER LEVEL __ DATE: <u>31 March 2021</u> LOGGED BY: J. Scott EXCAVATION COMPANY: Goldie Mohr Ltd. METHOD: Backhoe NOTES: <u>18T E: 456599 N: 5017156</u> m Below Existing Grade Shear test (Cu)
Sensitivity (S)
Water content (%) △ Field Stratigraphy Type and Number Moisture Content **COMMENTS** ☐ Lab Depth **DESCRIPTION OF** Atterberg limits (%) SOIL AND BEDROCK $-0.2 \, \text{m}$ ft 0.0 10 20 30 40 50 60 70 80 90 **GROUND SURFACE** TOPSOIL (152 mm) 0.2 SM - Gravelly sand (fill), with silt, concrete, asphalt, brown, moist 1 - Test pit open upon completion 0.5 2 3 -- 1.0 1.2 Grey, cobbles GS-1 1.5 6 1.8 Wet - Groundwater infiltration observed at 2.0 approximately 1.8 mbgs 7 TEST HOLE LOG GEOTECH 11220832 TEST PIT GINT LOGS.GPJ GEOLOGIC.GDT 12/4/2/ 2.5 9 - 50 mm diameter monitoring well installed GS-2 to 2.7 mbgs 3.0 10-3.0 END OF TEST HOLE 11-3.5 12-13-4.0 14 4.5

REFERENCE No.: 11220832 ENCLOSURE No.: TEST HOLE No.: __ TP-4 **TEST HOLE REPORT** Existing grade **ELEVATION:** Page: 1 of 1 **LEGEND** CLIENT: ___ Consolidated Fastfrate ☐ GS - GRAB SAMPLE PROJECT: Septic Assessment Ţ - WATER LEVEL DATE: 31 March 2021 LOGGED BY: J. Scott EXCAVATION COMPANY: Goldie Mohr Ltd. METHOD: Backhoe NOTES: <u>18T E: 456656 N: 5017172</u> m Below Existing Grade Shear test (Cu)
Sensitivity (S)
Water content (%) △ Field Stratigraphy Moisture Content Type and Number **COMMENTS** □ Lab Depth **DESCRIPTION OF** Atterberg limits (%) SOIL AND BEDROCK ft 0.0 10 20 30 40 50 60 70 80 90 m **GROUND SURFACE** TOPSOIL (102mm) 0.1 SM - Gravelly sand (fill), with silt, with clay, concrete, asphalt, brown, moist 1 -- Test pit open upon completion 0.5 2 3 -- GS-1 - 1.0 32% Gravel GS-1 44% Sand 17% Silt 7% Clay 1.5 6 1.8 Wet - Groundwater infiltration observed at - 2.0 approximately 1.8 mbgs 7 TEST HOLE LOG GEOTECH 11220832 TEST PIT GINT LOGS.GPJ GEOLOGIC.GDT 12/4/2/ 2.5 3.0 10-GS-2 3.4 END OF TEST HOLE 3.5 12-13-4.0 14 4.5

REFERENCE No.: 11220832 ENCLOSURE No.: ____ A-5 TEST HOLE No.: _ TP-5 **TEST HOLE REPORT** Existing grade **ELEVATION:** Page: 1 of 1 **LEGEND** CLIENT: ___ Consolidated Fastfrate ☐ GS - GRAB SAMPLE PROJECT: Septic Assessment ¥ - WATER LEVEL __ DATE: <u>31 March 2021</u> LOGGED BY: J. Scott EXCAVATION COMPANY: Goldie Mohr Ltd. METHOD: Backhoe NOTES: <u>18T E: 456601 N: 5017160</u> m Below Existing Grade Shear test (Cu) Sensitivity (S) △ Field Stratigraphy Moisture Content Type and Number □ Lab **COMMENTS** Depth Water content (%) **DESCRIPTION OF** Atterberg limits (%) SOIL AND BEDROCK ft 0.0 10 20 30 40 50 60 70 80 90 m **GROUND SURFACE** TOPSOIL (102mm) 0.1 SM - Silty sand (fill), with gravel, with clay, with asphalt, concrete, brown, 1 -- Test pit open upon completion 0.5 2 3 -- 1.0 GS-1 1.2 Grey 1.5 6 1.8 Wet - Groundwater infiltration observed at - 2.0 approximately 1.8 mbgs 7 TEST HOLE LOG GEOTECH 11220832 TEST PIT GINT LOGS.GPJ GEOLOGIC.GDT 12/4/2/ 2.5 9 - GS2 18% Gravel GS-2 47% Sand 3.0 23% Silt 10-3.0 END OF TEST HOLE 12% Clay 11-3.5 12-13-4.0 14 4.5



Particle-Size Analysis of Soils (Geotechnical) (USCS) (ASTM D422)

Client:	Consolidated Fastfrate Rideau Street & Somme Street, Ottawa, ON			_Lab No.:	S	SS-21-25		
Project/Site:				Project No.:	11220832			
Borehole no.:	Т	P1	_	Sample no.:	(GS1		
Depth:	Depth: 0.6 - 0.9 m			Enclosure:	,	A-6		
100 90 80 80 60 60 40 40 30 20							0 10 20 30 Forcent Retained 60 70 80	
10							90	
0.001	0.01	0.1 Diame	eter (mm)		10		100	
	Clay & Silt		Sand		Grav	Gravel		
		Fine Unified Soil C	Mediu		Fine	Fine Coarse		
	Soil Description		Gravel (%)	Sand (%)	Cla	Clay & Silt (%)		
			37 47			16		
Ol-	Silt-size particles (%): y-size particles (%) (<0.002)mm):		12				
	y-3126 particles (/0) (>0.002				·			
Remarks: Moist	ure Content = 7.1% as pe	r, ASTM D221	6.					
Performed by:	Jos	h Sullivan		_ Date:	Ар	ril 7, 2021		
Verified by:	Joe Sullivan	and	Date:	Ap	ril 7, 2021			



Particle-Size Analysis of Soils (Geotechnical) (USCS) (ASTM D422)

Client:	Consolidated Fastfrate Rideau Street & Somme Street, Ottawa, ON			Lab No.:		SS-21-25		
Project/Site:				Project No.:	11220832			
Borehole no.:	TP1		_	Sample no.:	(GS2		
Depth:	1.8 - 2.1	m		Enclosure:		A-7		
90							0 10	
80							20	
Percent Passing 90							30 An	
40							50 Bercera	
20							70	
0.001	0.01	0.1	1		10		90	
		Diamet	er (mm)					
	Clay & Silt	Fine	Sand Fine Medium Coarse		Gravel Fine Coarse			
	U		assification System		I		ı	
	Soil Description		Gravel (%) Sand		%) Clay & Silt (%			
			41	36	23			
Cla	Silt-size particles (%): y-size particles (%) (<0.002mn	m):		16 7				
Remarks: Moist	ure Content = 8.7% as per, A	ASTM D2216						
Performed by:	Josh S	ullivan		Date:	Ap	oril 7, 2021		
Verified by:	Joe Sullivan) S	Man	Date:	Ap	oril 7, 2021		



Particle-Size Analysis of Soils (Geotechnical) (USCS) (ASTM D422)

Client:	Consolidate	ed Fastfrate		Lab No.:		SS-21-25	
Project/Site:	Rideau Street & Somn	ne Street, O	ttawa, ON	Project No.:	11220832		
Borehole no.:	TP4		_	Sample no.:		GS1	
Depth:	0.9 - 1.2	2 m		Enclosure:		A-8	
100 90 80 70 60 40 30 20							0 10 20 30 Forcent Retained 60 70 80 90
0.001	0.01	0.1 Diame	1 eter (mm)		10		100
			Sand		Gra	vel	
	Clay & Silt	Fine			Fine	Coarse	
		Inified Soil C	lassification Syste	I			
	Soil Description		Gravel (%)	Sand (%)	Cla	ny & Silt (%)	
		32 44 24		24			
	Silt-size particles (%):			17			
Cla	y-size particles (%) (<0.002mn	11):		7			
Remarks: Moist	ure Content = 10.6% as per,	ASTM D22	16.				
Performed by:	Josh S	ullivan		Date:	Ap	oril 7, 2021	
Verified by:	Joe Sullivan	J= 5		Date:	Ap	oril 7, 2021	



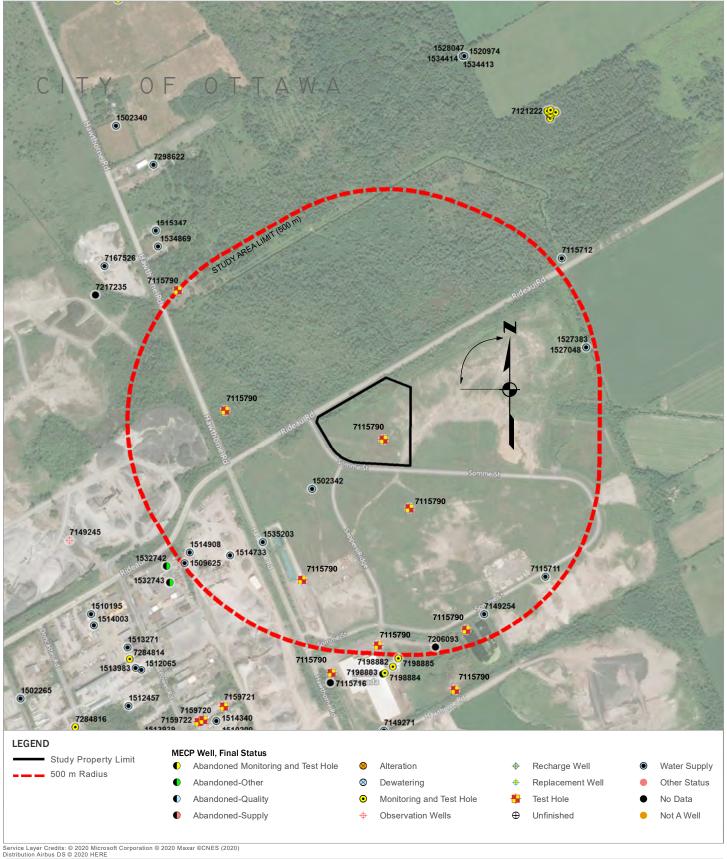
Particle-Size Analysis of Soils (Geotechnical) (USCS) (ASTM D422)

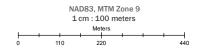
Client:	Consolid	lated Fastfrate		_Lab No.:		SS-21-25	
Project/Site:	Rideau Street & Sc	omme Street, C	Ottawa, ON	_Project No.:		11220832	
Borehole no.:		⁻ P5	_	Sample no.:		GS2	
Depth:	2.75 -	3.05 m		Enclosure:		A-9	
100 90 80 70 40 40 20							0 10 20 30 40 Bercent Retained 60 70 80 90
0.001	0.01	0.1 Diame	eter (mm)	1	10		100
			Sand		Gra	avel	
	Clay & Silt	Fine		um Coarse	Fine	Coarse	
		Unified Soil C	Classification Syst	em			
	Soil Description		Gravel (%)	Sand (%)	CI	ay & Silt (%)	
			18	18 47 35			
	Silt-size particles (%):)		23 12			
Cia	y-size particles (%) (<0.002	<u></u>			-		
Remarks: Moist	cure Content = 22.4% as p	oer, ASTM D22	116.				
Performed by:	Jos	h Sullivan		Date:	A	pril 7, 2021	
Verified by:	Joe Sullivan	2	Sullan	_ Date:	A	pril 7, 2021	



→ The Power of Commitment

Appendix B MECP Water Well Records





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Consolidated Fastfrate (Ottawa) Holdings Inc. RIDEAU ROAD & SOMME STREET CITY OF OTTAWA ONTARIO

HYDROGEOLOGY ASSESSMENT **MECP WATER WELLS**

Project No. 12565773 Revision No. -

Date Jan 21

APPENDIX B

WELL RECORD LISTINGS

Ministry of the Environment Conservation & Parks (MECP)

Database Currency: 2020-04-30 Date Accessed: 2020-11-13

Project ID: 11220832 Office: Peterborough, ON



 Lot:
 LOT 27
 Well ID:
 7206093

 Con:
 CON 6 FROM RIDEAU RIVER
 Borehole ID:
 1004500104

Township:GLOUCESTERCompletion Date:7/18/2013County:OTTAWA-CARLETONReceived Date:8/12/2013

Street: 35 SAPPERS RIDGE Tag: A089801

City: Ottawa Audit No: Z103282

Site: Contractor License: 3749

Elevation: 89.57 masl.

UTM: 18 E 456749 N 5016668 Long/Lat: -75.552, 45.302

DETAILS

Primary Use: Public Secondary Use: Public Final Status:

Well Depth: 47.2 m Depth to Bedrock: 0 m Static Level: 7.6 m Well Type:

Pump Rate: 10 GPM Boring Method: Rotary (Convent.)

CASING DETAILS DEPTH IN METERS

 Material
 Diameter (cm)
 Top
 Bottom

 STEEL
 14.29
 12.19
 -0.61

FORMATION DETAILS DEPTH IN METERS

 Colour
 Material
 Top
 Bottom

 LIMESTONE
 7.32
 47.24

 FILL
 0.00
 2.44

 GREY
 CLAY
 2.44
 7.32

 Lot:
 LOT 27
 Well ID:
 7115790

 Con:
 CON 6 FROM RIDEAU RIVER
 Borehole ID:
 1002782554

 Township:
 GLOUCESTER
 Completion Date:
 7/7/2008

County:OTTAWA-CARLETONReceived Date:11/26/2008Street:HAWTHORNE ROAD AT RIDEAU ROADTag:A074584

City: Ottawa Audit No: M02897

Site: Contractor License: 1844

Elevation: 90.95 masl.

UTM: 18 E 456598 N 5016675 **Long/Lat:** -75.554, 45.302

DETAILS

Primary Use: Monitoring Secondary Use: Monitoring Final Status: Test Hole

Well Depth: 0 m Depth to Bedrock: 0 m Static Level: 1 m Well Type:

Diameter (cm)

Pump Rate: Boring Method:

Material

H.S.A.

CASING DETAILS DEPTH IN METERS

			
FORMATIO	N DETAILS	DE	EPTH IN METERS
Colour	<u>Material</u>	<u>Тор</u>	- <u>Bottom</u>
BROWN	FILL	0.27	1.43
GREY	SAND	1.43	1.83
BROWN	TILL	1.83	2.32
GREY	FINE SAND	0.00	0.27

Top

Bottom

Contractor License:

1844

LOT 27 7115790 Lot: Well ID: CON 6 FROM RIDEAU RIVER 1002782518 Con: Borehole ID: Township: **GLOUCESTER Completion Date:** 7/7/2008 County: OTTAWA-CARLETON **Received Date:** 11/26/2008 Street: HAWTHORNE ROAD AT RIDEAU ROAD A074584 Tag: City: Ottawa **Audit No:** M02897

Elevation: 94.41 masl.

Site:

UTM: 18 E 456831 N 5016712 Long/Lat: -75.551, 45.303

DETAILS

Primary Use: Monitoring Secondary Use: Monitoring Final Status: Test Hole

Well Depth: $0 \ m$ Depth to Bedrock: $0 \ m$ Static Level: $1.3 \ m$ Well Type:

Pump Rate: Boring Method: H.S.A.

CASING DETAILS DEPTH IN METERS

<u>Material</u>	Diameter (cm)	<u>Тор</u>	-	Bottom
STEEL	15.86	-0.45		6.40

FORMATION DETAILS

DEPTH IN METERS

7149254

Colour	<u>Material</u>	<u>Top</u>	-	<u>Bottom</u>
GREY	SANDSTONE	1.30		9.10
BROWN	TOPSOIL	0.00		1.30

Lot: LOT 27 Well ID:

Con: CON 6 FROM RIDEAU RIVER Borehole ID: 1003262503

Township: GLOUCESTER Completion Date: 5/25/2010

County: OTTAWA-CARLETON Received Date: 8/4/2010

 Street:
 TW#7 HOAWTHORNE RD.
 Tag:
 A082844

 City:
 GLOUCESTER
 Audit No:
 Z101832

Site: Contractor License: 1558

Elevation: 88.61 masl.

UTM: 18 E 456879 N 5016752 **Long/Lat:** -75.550 , 45.303

DETAILS

Primary Use: Monitoring Secondary Use: Monitoring Final Status: Water Supply

Well Depth: 29.9 m Depth to Bedrock: 0 m Static Level: 4.4 m Well Type:

Pump Rate: 27.3 LPM Boring Method: Rotary (Reverse)

CASING DETAILS DEPTH IN METERS

 Material
 Diameter (cm)
 Top
 Bottom

 STEEL
 15.86
 -0.45
 6.40

 FORMATION DETAILS
 DEPTH IN METERS

 Colour
 Material
 Top
 Bottom

 GREY
 SANDSTONE
 1.30
 9.10

 BROWN
 TOPSOIL
 0.00
 1.30

Page 3 of 13

Lot: LOT 26 Well ID:

Con:CON 6 FROM RIDEAU RIVERBorehole ID:1001905211Township:GLOUCESTERCompletion Date:7/14/2008

7115790

County: OTTAWA-CARLETON Received Date: 11/26/2008

 Street:
 HAWTHORNE ROAD AT RIDEAU ROAD
 Tag:
 A074584

 City:
 Ottawa
 Audit No:
 M02897

Site: Contractor License: 1844

Elevation: 89.13 masl.

UTM: 18 E 456400 N 5016852 **Long/Lat:** -75.556, 45.304

DETAILS

Primary Use: Monitoring Secondary Use: Monitoring Final Status: Test Hole

Well Depth: 7.6 m Depth to Bedrock: 0 m Static Level: 1.7 m Well Type:

Diameter (cm)

Pump Rate: Boring Method: H.S.A.

Material

CASING DETAILS DEPTH IN METERS

FORMATION DETAILS		DEP.	TH IN	METERS	
Colour	<u>Material</u>		Тор	-	Bottom
GREY	FINE SAND		0.00		0.27
BROWN	FILL		0.27		1.43
BROWN	TILL		1.83		2.32
GREY	SAND		1.43		1.83

Bottom

<u>Top</u>

LOT 27 Lot: Well ID: 7115711 CON 6 FROM RIDEAU RIVER Borehole ID: 1001904894 Con: Township: **Completion Date: GLOUCESTER** 9/26/2008 County: OTTAWA-CARLETON **Received Date:** 12/2/2008 TW #5 Street: Tag: A068335 **GLOUCESTER** Z84410 City: **Audit No:** 1558 Site: Contractor License:

Elevation: 87.38 masl.

UTM: 18 E 457043 N 5016848 **Long/Lat:** -75.548 , 45.304

DETAILS

Primary Use: Domestic Secondary Use: Domestic Final Status: Water Supply

Well Type: Bedrock Well Depth: 29.9 m Depth to Bedrock: 0 m Static Level: 6.8 m

Pump Rate: 180 GPM Boring Method: Cable Tool

> **CASING DETAILS DEPTH IN METERS**

<u>Material</u>	Diameter (cm)	<u>Тор</u>	-	Bottom
STEEL	25.40			5.49
OPEN HOLE	22.86			58.52

FORMATION DETAILS		DEPTH IN METERS		
Colour	<u>Material</u>	<u>Тор</u> -	<u>Bottom</u>	
BROWN	SANDSTONE	0.00	15.85	
GREY	QUARTZITE	15.85	21.95	
WHITE	SANDSTONE	21.95	48.77	
GREY	SANDSTONE	48.77	58.52	

Well ID:

Tag:

Audit No:

Borehole ID:

Completion Date:

Contractor License:

DEPTH IN METERS

Received Date:

1509625

10031657

5/4/1968

6/12/1968

3002

Lot: LOT 26

Con: CON 5 FROM RIDEAU RIVER

GLOUCESTER Township:

OTTAWA-CARLETON County:

Street:

City:

Site: Elevation: 103.27 masl.

UTM: 18 E 456091 N 5016902 Long/Lat: -75.560, 45.304

DETAILS

Primary Use: Domestic Secondary Use: Domestic Final Status: Water Supply

Well Depth: 58.5 m Depth to Bedrock: 0 m Static Level: 11 m Well Type: Bedrock

Pump Rate: 180 GPM Boring Method: Cable Tool

CASING DETAILS

Material Diameter (cm) <u>Top</u> **Bottom** OPEN HOLE 22.86 58.52

Page 5 of 13

STEEL	25.40	5.49
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FORMATION DETAILS		DEPTH I	N METERS
Colour	<u>Material</u>	<u>Top</u> -	<u>Bottom</u>
BROWN	SHALE	0.61	3.05
BROWN	TOPSOIL	0.00	0.61
GREY	LIMESTONE	3.05	35.36

 Lot:
 LOT 26
 Well ID:
 1514733

 Con:
 CON 5 FROM RIDEAU RIVER
 Borehole ID:
 10036703

Township:GLOUCESTERCompletion Date:4/15/1975County:OTTAWA-CARLETONReceived Date:7/8/1975

Street: Tag:

City: Audit No:

Site: Contractor License: 1517

Elevation: 99.42 masl.

UTM: 18 E 456211 N 5016920 Long/Lat: -75.559, 45.304

DETAILS

Primary Use: Commerical Secondary Use: Commerical Final Status: Water Supply

Well Depth: 35.4 m Depth to Bedrock: 0.6 m Static Level: 12.m Well Type: Bedrock

Pump Rate: 10 GPM Boring Method: Cable Tool

CASING DETAILS DEPTH IN METERS

<u>Material</u>	Diameter (cm)	<u>Top</u>	-	<u>Bottom</u>
OPEN HOLE	12.70			35.36
STEEL	12.70			5.49

FORMATION DETAILS DEPTH IN METERS

Colour	<u>Material</u>	<u>Top</u>	-	Bottom
BROWN	TOPSOIL	0.00		0.61
BROWN	SHALE	0.61		3.05
GREY	LIMESTONE	3.05		35.36

 Lot:
 LOT 26
 Well ID:
 1514908

 Con:
 CON 5 FROM RIDEAU RIVER
 Borehole ID:
 10036875

Township:GLOUCESTERCompletion Date:8/15/1975County:OTTAWA-CARLETONReceived Date:9/11/1975

Street: 3500 RIDEAU ROAD Tag: A018916

City: GLOUCESTER Audit No: Z19099

Site: Contractor License: 1119

Elevation: 90.37 masl.

UTM: 18 E 456105 N 5016929 Long/Lat: -75.560, 45.304

DETAILS

Primary Use: Domestic Secondary Use: Domestic Final Status: Water Supply

Well Depth: 75.6 m Depth to Bedrock: 0 m Static Level: 12...m Well Type: Bedrock

Pump Rate: 75.71 LPM Boring Method: Air Percussion

CASING DETAILS DEPTH IN METERS

<u>Material</u>	Diameter (cm)	<u>Тор</u>	- <u>Bot</u>	<u>tom</u>
OPEN HOLE		6.09	42	.67
STEEL	15.88	0.00	6.7	70

FORMATION DETAILS		DEPTH	IN METERS
Colour	<u>Material</u>	Тор	- <u>Bottom</u>
GREY	LIMESTONE	10.68	13.01
GREY	SANDSTONE	0.37	10.68
	GRAVEL	0.00	0.37

Lot: <null> Well ID: 1535203

 Con:
 Borehole ID:
 11172955

 Township:
 GLOUCESTER
 Completion Date:
 10/27/2004

County: OTTAWA-CARLETON Received Date: 11/26/2004

Street: 3500 RIDEAU ROAD Tag: A018916

Z19099

Audit No:

Site: Contractor License: 1119

Elevation: 90.37 masl.

GLOUCESTER

City:

UTM: 18 E 456298 N 5016953 **Long/Lat:** -75.557, 45.305

DETAILS

Primary Use: Domestic Secondary Use: Domestic Final Status: Water Supply

Well Depth: 42.7 m Depth to Bedrock: 1.2 m Static Level: 14..m Well Type: Bedrock

Pump Rate: 75.71 LPM Boring Method: Air Percussion

CASING DETAILS DEPTH IN METERS

Page 7 of 13

FORMATI	ON DETAILS	DEPTH I	N METERS
Colour	<u>Material</u>	<u>Тор</u> -	<u>Bottom</u>
GREY	FINE SAND	0.00	0.27
GREY	SAND	1.43	1.83

<u>Top</u>

1.83

0.27

Bottom

2.32

1.43

Contractor License:

1844

Diameter (cm)

TILL

FILL

LOT 26 Lot: Well ID: 7115790 CON 6 FROM RIDEAU RIVER Con: Borehole ID: 1002782572 Township: **Completion Date:** GLOUCESTER 7/15/2008 OTTAWA-CARLETON **Received Date:** 11/26/2008 County: Street: HAWTHORNE ROAD AT RIDEAU ROAD A074584 Tag: City: Ottawa Audit No: M02897

Elevation: 85.10 masl.

Site:

UTM: 18 E 456687 N 5017036 **Long/Lat:** -75.552, 45.305

DETAILS

Primary Use: Monitoring Secondary Use: Monitoring Final Status: Test Hole

Well Depth: 0 m Depth to Bedrock: 0 m Static Level: 3 m Well Type:

Pump Rate: Boring Method:

<u>Material</u>

BROWN

BROWN

CASING DETAILS DEPTH IN METERS

H.S.A.

<u>Material</u>	Diameter (cm)	<u>Top</u>	<u> </u>	<u>Bottom</u>
FORMATIO	N DETAILS	D	EPTH IN	METERS
<u>Colour</u>	<u>Material</u>	<u>Top</u>	<u> </u>	<u>Bottom</u>
BROWN	TILL	1.8	3	2.32
BROWN	FILL	0.2	7	1.43
GREY	SAND	1.4	3	1.83

Page 8 of 13

GREY FINE SAND 0.00 0.27

Lot: LOT 26 Well ID: 1502342

Con:CON 6 FROM RIDEAU RIVERBorehole ID:10024385Township:GLOUCESTERCompletion Date:11/30/1950

County: OTTAWA-CARLETON Received Date: 12/6/1951

Street: Tag:

City: Audit No:

Site: Contractor License: 3504

Elevation: 87.74 masl.

UTM: 18 E 456431 N 5017092 Long/Lat: -75.556 , 45.306

DETAILS

Primary Use: Livestock Secondary Use: Livestock Final Status: Water Supply

Well Depth: 17.4 m Depth to Bedrock: 8.2 m Static Level: 4 m Well Type: Bedrock

Pump Rate: 1 GPM Boring Method: Cable Tool

CASING DETAILS DEPTH IN METERS

 Material
 Diameter (cm)
 Top
 Bottom

 STEEL
 12.70
 8.23

 OPEN HOLE
 12.70
 17.37

FORMATION DETAILS DEPTH IN METERS

 Colour
 Material
 Top
 Bottom

 PREV. DRILLED
 0.00
 8.23

 SANDSTONE
 8.23
 17.37

 Lot:
 LOT 26
 Well ID:
 7115790

 Con:
 CON 6 FROM RIDEAU RIVER
 Borehole ID:
 1002782563

 Township:
 GLOUCESTER
 Completion Date:
 7/14/2008

 County:
 OTTAWA-CARLETON
 Received Date:
 11/26/2008

Street: HAWTHORNE ROAD AT RIDEAU ROAD Tag: A074584

City: Ottawa Audit No: M02897

Site: Contractor License: 1844

Elevation: 84.01 masl.

UTM: 18 E 456622 N 5017219 Long/Lat: -75.553 , 45.307

DETAILS

Primary Use: Monitoring Secondary Use: Monitoring Final Status: Test Hole

Well Depth: 0 m Depth to Bedrock: 0 m Static Level: 3.6 m Well Type:

Diameter (cm)

Pump Rate: Boring Method:

Material

H.S.A.

CASING DETAILS DEPTH IN METERS

<u>Top</u>

Bottom

FORMATIO	N DETAILS	DEP	TH IN	METERS
<u>Colour</u>	<u>Material</u>	<u>Top</u>	-	<u>Bottom</u>
GREY	FINE SAND	0.00		0.27
BROWN	TILL	1.83		2.32
BROWN	FILL	0.27		1.43
GREY	SAND	1.43		1.83

Lot: LOT 25 **Well ID:** 7115790

Con: CON 6 FROM RIDEAU RIVER Borehole ID: 1002782590

Township:GLOUCESTERCompletion Date:7/15/2008County:OTTAWA-CARLETONReceived Date:11/26/2008

Street: HAWTHORNE ROAD AT RIDEAU ROAD Tag: A074584

City:OttawaAudit No:M02897Site:Contractor License:1844

Elevation: 84.01 masl.

UTM: 18 E 456206 N 5017303 Long/Lat: -75.559, 45.308

DETAILS

Primary Use: Monitoring Secondary Use: Monitoring Final Status: Test Hole

Well Depth: 0 m Depth to Bedrock: 0 m Static Level: 1.6 m Well Type:

Pump Rate: Boring Method:

CASING DETAILS DEPTH IN METERS

H.S.A.

Page 10 of 13

<u>Material</u>	Diameter (cm)	<u>Тор</u>	-	Bottom
OPEN HOLE	15.24			30.48
STEEL	15.24			11.89

FORMATION DETAILS		DEPT	H IN	METERS
Colour	<u>Material</u>	<u>Top</u>	-	Bottom
GREY	SANDSTONE	8.53		30.48
GREY	HARDPAN	1.52		8.53
BROWN	SAND	0.00		1.52

Well ID:

Tag:

Borehole ID:

Completion Date:

Received Date:

1527383

10049033

8/16/1993

9/21/1993

LOT 26 Lot:

Con: CON 6 FROM RIDEAU RIVER

Township: **GLOUCESTER**

County: OTTAWA-CARLETON

Street:

City: **Audit No:** 135946 Site: **Contractor License:** 1558

Elevation: 82.18 masl.

UTM: 18 E 457162 N 5017453 Long/Lat: -75.546, 45.309

DETAILS

Primary Use: Domestic Secondary Use: Domestic Final Status: Water Supply

Well Type: Bedrock Well Depth: 30.5 m Depth to Bedrock: 8.5 m Static Level: 2.1 m

Pump Rate: 20 **GPM** Boring Method: Air Percussion

> **CASING DETAILS DEPTH IN METERS**

<u>Material</u>	Diameter (cm)	<u>Top</u>	-	<u>Bottom</u>
STEEL	15.24			11.89
OPEN HOLE	15.24			30.48

FORMATION DETAILS DEPTH IN METERS <u>Colour</u> <u>Material</u> **Bottom** <u>Top</u> **BROWN** SAND 0.00 1.52

Page 11 of 13

GREY	HARDPAN	1.52	8.53
GREY	SANDSTONE	8.53	30.48

Well ID:

Tag: Audit No:

Borehole ID:

Completion Date:

Contractor License:

DEPTH IN METERS

Received Date:

1527048

10048727

4/19/1993

5/6/1993

130025

1558

Lot: LOT 26

Con: CON 6 FROM RIDEAU RIVER

Township: GLOUCESTER

County: OTTAWA-CARLETON

or many of the contract of

Street:

82.18 masl.

Site:

City:

Elevation:

UTM: 18 E 457162 N 5017453 Long/Lat: -75.546 , 45.309

DETAILS

Primary Use: Domestic Secondary Use: Domestic Final Status: Water Supply

Well Depth: 41.1 m Depth to Bedrock: 0 m Static Level: 9.4 m Well Type: Bedrock

Pump Rate: 15 GPM Boring Method: Air Percussion

CASING DETAILS

<u>Material</u>	Diameter (cm)	<u>Top</u>	-	Bottom
OPEN HOLE	15.24			22.86
STEEL	15.24			9.45
OPEN HOLE	15.24			41.15

FORMATION DETAILS		DEPTH	I IN METERS
Colour	<u>Material</u>	<u>Top</u>	- <u>Bottom</u>
WHITE	SANDSTONE	10.06	41.15
GREY	HARDPAN	2.74	4.57
BROWN	CLAY	0.00	2.74
GREY	LIMESTONE	4.57	10.06

 Lot:
 LOT 26
 Well ID:
 1527384

 Con:
 CON 6 FROM RIDEAU RIVER
 Borehole ID:
 10049034

 Township:
 GLOUCESTER
 Completion Date:
 8/16/1993

County: OTTAWA-CARLETON Received Date: 9/21/1993

Street: Tag:

City: Audit No: 135944
Site: Contractor License: 1558

Elevation: 82.18 masl.

UTM: 18 E 457162 N 5017453 Long/Lat: -75.546, 45.309

DETAILS

Primary Use: Domestic Secondary Use: Domestic Final Status: Water Supply

Well Depth: 30.5 m Depth to Bedrock: 0 m Static Level: 6.7 m Well Type: Bedrock

Pump Rate: 15 GPM Boring Method: Air Percussion

CASING DETAILS DEPTH IN METERS

 Material
 Diameter (cm)
 Top
 Bottom

 STEEL
 15.24
 6.71

 OPEN HOLE
 15.24
 30.48

FORMATION DETAILS DEPTH IN METERS

ColourMaterialTop-BottomGREYSANDSTONE0.0030.48



The Ontario Water Resources Act

WATER WELL RECORD

Ontario	1. PRINT ONLY IN	SPACES PROVIDED	15273	383 [5002] [60	N
COUNTY OR DISTRICT		TOWNSHIP, BOROUGH, CITY, TOWN, VILLAGE	· · · · · · · · · · · · · · · · · · ·	CON . BLOCK, TRACT, SURVEY ETC	LOT 25-27
		icester	M - M	DATE COMP	8 93
		Box 4208 stn.		NA Ontario KIS 5B2 DAY 10	MO VR VR
	M 10 12	OG OF OVERBURDEN AND BEDRO		AIS (CEE INCIDICATIONS)	47
GENERAL COLOUR	MOST COMMON MATERIAL	OTHER MATERIALS	JCK WATERIA	GENERAL DESCRIPTION	DEPTH - FEET FROM TO
Brown	Sand	Stone			0 5
Gray	Hardpan	Boulders			5 28
Gray	Sandstone			Hard	28 100
	· _	·			
31				1.1.1111	
32					
41 WA	TER RECORD	51 CASING & OPEN HOLE	RECORD-	SIZE(-S) OF OPENING SI-33 DIAME	75 80 TER 34-34 LENGTH 39-40
WATER FOUND AT - FEET	KIND OF WATER 14 FRESH 3 SULPHUR	inches	DEPTH - FEET ROM TO	MATERIAL AND TYPE	INCHES FEET DEPTH TO TOP 41-44 3D OF SCREEN
58 ' '	SALTY 4 MINERALS 6 GAS	6 1/4 1 STEEL 12 .188	0 39		FEET
200	FRESH 3 SULPHUR 4 MINERALS 6 GAS	4 □ OPEN HOLE 5 □ PLASTIC	20-2	MATERIAL ANI	CEMENT CROUT
2 (SALTY 6 GAS	2 GALVANIZED 3 CONCRETE 4 POPEN HOLE 5 PLASTIC	39 100	FROM TO 10-13 14-17	- Grouted
2 (FRESH 3 SULPHUR SALTY 6 GAS	F625 1 □STEEL 26	27-30	37.53 U CERRETIC	- Grouted
	☐ FRESH 3 ☐ SULPHUR 34 00 4 ☐ MINERALS ☐ SALTY 6 ☐ GAS	3 □ CONCRETE 4 □ OPEN HOLE 5 □ PLASTIC		26-29 30-33 80	
71 PUMPING TEST NE		15-16 17-18		LOCATION OF WEL	L .
STATIC	WATER LEVEL 25	LEVELS DURING THE PUMPING THE PUMPING THE PUMPING THE PUMPING THE PUMPING		IAGRAM BELOW SHOW DISTANCES OF WELL LINE INDICATE NORTH BY ARROW.	FROM ROAD AND
19-21 19-21	22-24 15 MINUTES 26-2	8 29-31 32-34 35-37		Rideau Rd	
	14'6" 13'11' PUMP INTAKE		 	Rideau Rd 380 meters	
IF FLOWING. GIVE RATE RECOMMENDED PL	GPM UMP TYPE RECOMMENDED	D 43-45 RECOMMENDED 46-49 PUMPING		-	
SHALLO	W TEP SETTING	50 FEET RATE 5 GPM	1 2	1,50) meters
FINAL	1 WATER SUPPLY	5 ABANDONED, INSUFFICIENT SUPPLY			
STATUS OF WELL	2 OBSERVATION WEI 3 TEST HOLE 4 RECHARGE WELL	LL 6 ABANDONED POOR QUALITY 7 UNFINISHED DEWATERING	4	ł	
 	DOMESTIC 2 STOCK	5 COMMERCIAL 6 MUNICIPAL	cuthory	¥	
WATER USE	3 IRRIGATION 4 INDUSTRIAL OTHER	7 ☐ PUBLIC SUPPLY ■ ☐ COOLING OR AIR CONDITIONING 9 ☐ NOT USED	3	× <e5×< td=""><td>ν, **</td></e5×<>	ν, **
	57 CABLE TOOL	BORING		760	
METHOD OF	2 ROTARY (CONVENT) 3 ROTARY (REVERSE	E) # 🗆 JETTING			
CONSTRUCT	S AIR PERCUSSION	9 DRIVING DIGGING OTHER	DRILLERS REMA		135946
NAME OF WELL		WELL CONTRACTOR'S LICENCE NUMBER	DATA SOURCE O DATE OF INS	1558 SEP	2 1 1993 "" "
5	Water Supply		w		
Box 490		Ontario K2S 1A6 WELL TECHNICIAN'S LICENCE NUMBER 1	REMARKS	·	
SIGNATURE OF	F / ECHNICIAN / CO TRACTOR	SUBMISSION DATE	OFFICE		
	OF THE ENVIRON	DAY <u>18 MO 8 YR 23</u> MENT COPY		FC	DRM NO. 0506 (11/86) FORM 9

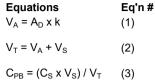
Appendix C

Nitrate Loading Calculations

Appendix C

Mass Balance Calculation - Nitrate Loading using Average Flows

Calculations based upon Septic Effluent Area, Figure 9.



Where:

 V_A = annual dilution volume [m³]

 A_D = dilution area [m^2]

 V_T = total volume of water [m³] V_S = annual sewage volume [m³]

C_{PB} = concentration at property boundary [mg/L]

C_S = concentration in sewage [mg/L]

k = 0.25 m (Precipitation rate - can be adjusted. Assumed rate from MECP document)

Therefore, if 40 mg/L of nitrate is in the effluent, 20.9 mg/L will be at the property boundary.

 $C_S = (C_{PB} \times V_T) / V_S \qquad (4)$

 C_{PB} = 2.5 mg/L As per MECP guidance manual Chapter 22

C_S = 4.8 mg/L Nitrate concentration into leaching bed to meet 2.5 mg/L downgradient at property boundary

Tertiary treatment would be required to reduce Nitrate to 4.8 mg/L or lower in order to meet 2.5 mg/L at the property boundary.

Note: MECP Design Guidelines for Sewage Works (2008) used in above calculations (Chapter 22)



→ The Power of Commitment