



**11061917 Canada Inc.**

## **Geotechnical Investigation**

**Type of Document:**

Updated Final Report (supersedes May 28, 2021 report)

**Project Name:**

Residential Development

365 Forest Street

Ottawa, Ontario

**Project Number:**

OTT-00252625-A0

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**Date Submitted:**

November 5, 2021

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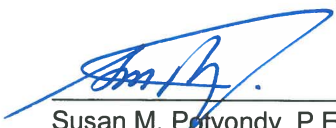
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## Executive Summary

EXP Services Inc. (EXP) is pleased to present the results of the two (2) geotechnical investigations completed in 2019 and 2021 for the proposed residential development to be located on the parcel of land identified by the following three (3) lot addresses; 365 Forest Street, 2583-2589 Bond Street and 1420 Richmond Road, Ottawa, Ontario. For purposes of this report, the parcel of land is identified by one (1) address, 365 Forest Street. Authorization to proceed with the geotechnical investigations was provided by Carmine Zayoun on behalf of 11061917 Canada Inc.

In addition to providing geotechnical services for this project, EXP is also providing civil engineering, environmental assessments and hydrogeological investigation services. The findings from the Phase One and Two Environmental Site Assessments and the hydrogeological investigation are reported under separate covers.

The proposed residential development will include two (2) buildings identified as Tower A and Tower B. Tower A and B will be each a twelve (12) story building with four (4) level underground parking garage with the lowest floor level at Elevation 62.6 m. The elevation of the ground floor will be at Elevation 75.6 m. The site grade raise will be up to approximately 1.5 m.

The fieldwork for this geotechnical investigation was completed in 2019 and 2021. The 2019 fieldwork for the geotechnical investigation was undertaken between April 24 and 30, 2019 and consists of twelve (12) boreholes (Borehole Nos. 19-01 to 19-12) advanced to auger refusal and termination depths of 5.9 m to 9.6 m below existing grade. The 2021 fieldwork was undertaken on October 5 and 6, 2021 and consists of two (2) boreholes (Borehole Nos. 21-13 and 21-14). advanced to termination depths of 12.8 m and 14.4 m below existing grade. The fieldwork was supervised on a full-time basis by EXP.

The geotechnical investigation revealed the subsurface conditions consist of fill, sandy silt to silty sand, glacial till underlain by limestone bedrock (with shaly partings) contacted at 6.1 m to 7.8 m below existing grade (Elevation 68.9 m to Elevation 67.6 m). The groundwater level at the site was established at depths ranging between 1.7 m and 6.6 m (Elevation 73.5 m to Elevation 67.8 m).

The results of the multi-channel analysis of surface waves (MASW) survey completed at the site indicate that the average seismic shear wave velocity is 1610.4 m/s for footings founded on the sound limestone bedrock as discussed in Section 8 of this report. Therefore, a site class A for seismic site response can be used in accordance with Table 4.1.8.4.A of the 2012 Ontario Building Code (OBC), as amended May 2, 2019.

The investigation revealed that some of the overburden soils are susceptible to liquefaction during a seismic event. However, the liquefiable soils along with all remaining overburden soil will be excavated from the building envelopes down to and into the bedrock to accommodate the proposed construction. Therefore, since the liquefiable soils will be removed, liquefiable soils is not a concern for the proposed development.

Based on the available information, the lowest floor slab in the parking garage will be at Elevation 62.6 m and therefore the most appropriate foundation for the proposed buildings is spread and strip footings designed to bear on the sound bedrock free of soil filled seams and below any fractured and weathered zones.

Spread and strip footings founded on the competent sound limestone bedrock, free of soil filled seams and below the weathered and fractured zones may be designed for a factored geotechnical resistance at



Ultimate Limit State (ULS) of 4500 kPa. The factored ULS value includes a resistance factor of 0.5. The Serviceability Limit State (SLS) bearing pressure of the bedrock, required to produce 25 mm settlement of the structure will be much larger than the recommended value for factored geotechnical resistance at ULS. Therefore, the factored geotechnical resistance at ULS will govern the design.

The lowest level floor slab in the underground parking garage may be designed as a slab-on-grade with perimeter and underfloor drainage systems. The floor slab should be set on a bed of well packed 19 mm clear stone at least 200 mm thick placed on an engineered fill pad at least 300 mm thick placed on the sound limestone bedrock.

Excavation of the overburden soils may be undertaken using large heavy mechanical equipment capable of removing debris within the fill as well as cobbles and boulders within the fill and glacial till. Excavation of the underlying bedrock will require line drilling and blasting techniques and should be undertaken by a specialized contractor. Pre-condition survey of surrounding buildings and infrastructure (such as roadways, sidewalks and underground services) should be undertaken at the site prior to start of construction as well as conducting vibration monitoring during blasting and rock excavation and construction operations.

Excavations within the soils for the proposed two (2) buildings will likely have to be undertaken within the confines of a shoring system that may consist of steel H soldier pile and timber lagging, steel interlocking sheeting and/or secant pile shoring system. The shoring system may be tied back by anchors grouted into the sound bedrock.

Excavations within the bedrock may be undertaken with near vertical sides subject to review by a geotechnical engineer. The rock face may require support in the form of rock bolts to maintain the integrity of the rock face. In the upper weathered/fractured zones of the bedrock, rock bolts in combination with wire mesh system and/or shotcrete may be required. This will be best established on-site during excavation.

Excavations above the groundwater may be dewatered by conventional sump pumping techniques. Excavations below the groundwater level and the water bearing sandy silt to silty and glacial till are expected to be more problematic and may result in greater water seepage, loss of ground and disturbance of the soils. Under these conditions, it is recommended that these excavations should be undertaken within the confines of a shoring system that is also designed to cut-off groundwater flows towards the excavation and minimize groundwater flows into the shored excavation. In this regard, seepage of groundwater into the shored excavation should still be anticipated but may be removed by collecting the water at low points within the excavation and pumping from sumps.

It is anticipated that all of the fill required for construction will have to be imported to the site and conform to the Ontario Provincial Standard Specification (OPSS) requirements for Granular A, B Type II and Select Subgrade Material (SSM).

The above and other related considerations are discussed in greater detail in the main body of this report.

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## 1 Introduction

EXP Services Inc. (EXP) is pleased to present the results of the two (2) geotechnical investigations completed in 2019 and 2021 for the proposed residential development to be located on the parcel of land identified by the following three (3) lot addresses; 365 Forest Street, 2583-2589 Bond Street and 1420 Richmond Road, Ottawa, Ontario. For purposes of this report, the parcel of land is identified by one (1) address, 365 Forest Street. Authorization to proceed with the geotechnical investigations was provided by Carmine Zayoun on behalf of 11061917 Canada Inc.

In addition to providing geotechnical services for this project, EXP is also providing civil engineering, environmental assessments and hydrogeological investigation services. The findings from the Phase One and Two Environmental Site Assessments and the hydrogeological investigation are reported under separate covers.

The proposed residential development will include two (2) buildings identified as Tower A and Tower B. Tower A and B will be each a twelve (12) story building with four (4) level underground parking garage with the lowest floor level at Elevation 62.6 m. The elevation of the ground floor will be at Elevation 75.6 m. The site grade raise will be up to approximately 1.5 m.

The two (2) geotechnical investigations were undertaken to:

- a) Establish the subsurface soil, bedrock and groundwater conditions at the fourteen (14) boreholes located on the site,
- b) Classify the site for seismic site response in accordance with the requirements of the 2012 Ontario Building Code (OBC) as amended May 2, 2019 and assess the potential for liquefaction of the subsurface soils during a seismic event,
- c) Comment on grade-raise restrictions,
- d) Make recommendations regarding the most suitable type of foundations, founding depth and bearing pressure at serviceability limit state (SLS) and factored geotechnical resistance at ultimate limit state (ULS) of the founding strata and comment on the anticipated total and differential settlements of the recommended foundation type,
- e) Discuss the feasibility of constructing the lowest floor slab as a slab on grade and provide comments regarding perimeter and underfloor drainage systems,
- f) Provide lateral earth pressure parameters (for static and seismic conditions) for the subsurface foundation walls of the proposed buildings,
- g) Comment on excavation conditions and de-watering requirements during construction,
- h) Discuss backfilling requirements and suitability of on-site soils for backfilling purposes,
- i) Recommend pavement structure thicknesses for paved surface parking lots and access roads; and
- j) Comment on subsurface concrete requirements and corrosion potential of subsurface soils to buried metal structures/members.

The comments and recommendations given in this report are based on the assumption that the above-described design concept will proceed into construction. If changes are made either in the design phase or during construction, this office must be retained to review these modifications. The result of this review may be a modification of our recommendations or it may require additional field or laboratory work to check whether the changes are acceptable from a geotechnical viewpoint.

## 2 Site Description

The subject site is bounded by Richmond Road on the north side, Bond Street on the south side, Forest Street on the west side and commercial type development on the east side. The 365 Forest Street lot site is occupied by a single storey multi-tenant building. The 2589 Bond Street lot is occupied by a single-storey building. The 1420 Richmond Road lot is currently vacant. The location of the site is shown in Figure 1.

Based on the ground surface elevations at the boreholes, the topography of the site ranges from Elevation 75.74 m to Elevation 74.13 m and gradually slopes downward to the south and southeast towards Bond Street. Ground cover of the site consists of asphalt and gravel surfaces with landscaped areas.

## **3 Geology of Site**

### **3.1 Surficial Geology**

The surficial geology map (Map 1506A – Surficial Geology, Ontario-Quebec, Geological Survey of Canada, printed by the Surveys and Mapping Branch, 1982) indicates that beneath any fill, the site is underlain by medium grained stratified sand with some silt.

### **3.2 Bedrock Geology**

The bedrock geology map (Map 1508A – Generalized Bedrock Geology, Ottawa-Hull, Ontario and Quebec, Geological Survey of Canada, printed by the Surveys and Mapping Branch, 1979) indicates the site is underlain by limestone (with shaly partings) bedrock of the Ottawa formation.



## 4 Investigation Procedure

### 4.1 Fieldwork

The fieldwork for this geotechnical investigation was completed in 2019 and 2021. The 2019 fieldwork for the geotechnical investigation was undertaken between April 24 and 30, 2019 and consists of twelve (12) boreholes (Borehole Nos. 19-01 to 19-12) advanced to auger refusal and termination depths of 5.9 m to 9.6 m below existing grade. The 2021 fieldwork was undertaken on October 5 and 6, 2021 and consists of two (2) boreholes (Borehole Nos. 21-13 and 21-14). advanced to termination depths of 12.8 m and 14.4 m below existing grade. The fieldwork was supervised on a full-time basis by EXP.

The borehole locations and elevations were established in the field by a survey crew from EXP. The geodetic elevation of Borehole Nos. 21-13 and 21-14 were estimated from spot elevations shown on the survey plan of the site and therefore, should be considered approximate. The borehole locations are shown in Figure 2.

The borehole locations were cleared from any underground services by USL-1 cable locators prior to start of drilling the boreholes. The boreholes were drilled with CME-75 truck-mounted and CME-850 track-mounted drill rigs equipped with continuous flight hollow-stem auger equipment and rock coring capabilities. Standard penetration tests (SPTs) were performed in the 2019 boreholes on a continuous basis and at 0.75 m and 1.5 m depth intervals. The 2021 boreholes were advanced by power augering technique from the ground surface to a 4.6 m depth, followed by conducting the SPT at 1.5 m depth interval to the bedrock surface. The presence of the bedrock was proven in selected boreholes by conventional coring techniques using NQ-size core barrel. A record of wash water return, colour of wash and any sudden drop of the drill rods were kept during rock coring operations.

32 mm and 38 mm diameter monitoring wells with a screened section were installed in selected boreholes for long-term monitoring of the groundwater levels and sampling of the groundwater. The installation configuration of each monitoring well is documented on the respective borehole log. All boreholes were backfilled upon completion of drilling and sampling operations.

### 4.2 Laboratory Testing Program

All soil samples were visually examined in the field for textural classification, logged, preserved in plastic bags and identified accordingly. Similarly, all rock cores were placed in core boxes, identified and visually examined and logged. On completion of the fieldwork, all the soil samples and rock cores were transported to the EXP laboratory located in the City of Ottawa.

The soil samples and rock cores were visually examined in the laboratory by a senior geotechnical engineer. The soil samples were classified in accordance with the Unified Soil Classification System (USCS). The rock cores were visually examined and logged in accordance with Section 3.2 of the 2006 Canadian Foundation Engineering Manual (Fourth Edition, CFEM) and photographs taken of the rock cores.

A summary of the soil and bedrock laboratory testing program is shown in Table I. The testing procedures for the corrosion analysis are referenced in Appendix A.

<b>Table I: Summary of Laboratory Testing Program</b>	
<b>Type of Test</b>	<b>Number of Tests Completed</b>
<b>Soil Samples</b>	
Moisture Content Determination	82
Unit Weight Determination	15
Grain Size Analysis	5
Corrosion Analysis (pH, sulphate, chloride and resistivity)	2
<b>Bedrock Cores</b>	
Unit Weight Determination	12
Unconfined Compressive Strength Test	12
Corrosion Analysis (pH, sulphate, chloride and resistivity)	2

#### 4.3 Multi-channel Analysis of Surface Waves (MASW) Survey

A multi-channel analysis of surface waves (MASW) survey was conducted on site on July 30, 2019 by Geophysics (GPR) International Inc. The MASW survey consists of one (1) survey line across the site in a north-south direction in order to measure the shear wave velocity and determine the site classification for seismic site response based on the shear wave velocity measurement. The procedure and report of the MASW survey are shown in Appendix B.

## 5 Subsurface Conditions and Groundwater Levels

A detailed description of the subsurface conditions and groundwater levels from the 2019 and 2021 boreholes are given on the attached Borehole Logs, Figure Nos. 3 to 16 inclusive. The borehole logs and related information depict subsurface conditions only at the specific locations and times indicated. Subsurface conditions and water levels at other locations may differ from conditions at the locations where sampling was conducted. The passage of time also may result in changes in the conditions interpreted to exist at the locations where sampling was conducted.

Boreholes were drilled to provide representation of subsurface conditions as part of a geotechnical exploration program and are not intended to provide evidence of potential environmental conditions. Reference is made to the Phase One and Two Environmental Site Assessments completed by EXP and reported under separate covers for evidence of potential environmental conditions.

It should be noted that the soil boundaries indicated on the borehole logs are inferred from non-continuous sampling and observations during drilling operations. These boundaries are intended to reflect approximate transition zones for the purpose of geotechnical design and should not be interpreted as exact planes of geological change.

The “Note on Sample Descriptions” preceding the borehole logs form an integral part of this report and should be read in conjunction with this report.

A review of the borehole logs indicates the following subsurface conditions with depth and groundwater level measurements.

### 5.1 Paved Areas - Pavement Structure

Borehole Nos. 19-03, 19-04, 19-06 and 19-07 are located in paved areas of the site. The pavement structure consists of 30 mm and 60 mm thick asphaltic concrete underlain by 150 mm to 250 mm thick granular fill base.

### 5.2 Unpaved Areas – Gravel Surface

The remaining boreholes are located in unpaved areas consisting of a surficial 100 mm to 500 mm thick granular fill layer.

### 5.3 Fill

Fill was contacted beneath the pavement structure and surficial granular layer in all the boreholes. The fill extends to depths ranging from 1.4 m to 3.0 m (Elevation 73.6 m to Elevation 71.8 m). Borehole No. 19-12 terminated within the fill at 4.4 m depth (Elevation 71.0 m). The fill consists of clayey silty sand to silty sand with gravel. The fill contains rootlets and brick debris. A petroleum odour was noted in the fill samples from Borehole Nos. 19-05. Based on the standard penetration test (SPT) N values of 1 to 16, the fill is in a very loose to compact state. The moisture content of the fill is 4 percent to 30 percent. The unit weight of the fill is 19.1 kN/m<sup>3</sup> to 22.9 kN/m<sup>3</sup>.

Grain size analysis of one (1) sample of the fill was conducted and the results are summarized in Table II. The grain size distribution curve is shown in Figure 17.

<b>Table II: Summary of Results from Grain-size Analysis – Fill Sample</b>					
<b>Borehole No. - Sample No.</b>	<b>Depth (m)</b>	<b>Grain-size Analysis (%)</b>			<b>Soil Classification (USCS)</b>
		<b>Gravel</b>	<b>Sand</b>	<b>Fines (Silt and Clay)</b>	
BH 19-10 – SS3	1.5 – 2.1	7	47	46	Silty Sand (SM)

Based on a review of the results from the grain size analysis, the fill may be classified as a silty sand (SM) in accordance with the Unified Soil Classification System (USCS).

#### **5.4 Sandy Silt to Silty Sand**

The fill in Borehole Nos. 19-01 to 19-03 is underlain by a sandy silt to silty sand layer from 1.4 m to 2.2 m depths (Elevation 73.6 m to Elevation 71.9 m). The SPT N values are 4 and 6 indicating the sandy silt to silty sand is in a loose state. The natural moisture content of the sandy silt to silty sand is 22 percent and 23 percent. The natural unit weight of the sandy silt to silty sand is 19.4 kN/m<sup>3</sup>.

#### **5.5 Glacial Till**

The fill and sandy silt to silty sand layer are underlain by glacial till that extends to depths of 6.1 m to 7.8 m (Elevation 68.9 m to Elevation 67.6 m). The glacial till ranges from a clayey silty sand to a silty sand with gravel. The glacial till is a silty clay in Borehole Nos. 19-03 to 19-05 from 2.2 m to 5.3 m depths (Elevation 72.8 m to Elevation 69.7 m). The glacial till contains shale fragments, cobbles and boulders. The SPT N values of the cohesionless silty clayey sand till ranges from 1 to 81 indicating the glacial till is in a very loose to very dense state. The SPT N values of the cohesive portion of the silty clay till of 2 to 4 indicates the silty clay till has a soft consistency. The natural moisture content and unit weight of the cohesionless silty clayey sand to silty sand with gravel till is 5 percent to 26 percent and 23.1 kN/m<sup>3</sup> to 23.9 kN/m<sup>3</sup>, respectively. The natural moisture content of the silty clay till ranges from 17 percent to 39 percent.

Grain size analysis of four (4) samples of the glacial till were conducted and the results are summarized in Table III. The grain size distribution curves are shown in Figures 18 to 21.

<b>Table III: Summary of Results from Grain-size Analysis – Glacial Till Samples</b>					
Borehole No. - Sample No.	Depth (m)	Grain-size Analysis (%)			Soil Classification (USCS)
		Gravel	Sand	Fines (Silt and Clay)	
BH 19-02 – SS5	3.8-4.4	13	45	42	Silty Sand (SM)
BH 19-04 – SS6	4.6-5.2	18	40	42	Silty Sand with Gravel (SM)
BH 19-08 – SS5	3.0-3.6	17	47	36	Silty Sand with Gravel (SM)
BH 19-11 – SS6	4.6-5.2	13	51	36	Silty Sand (SM)

Based on a review of the results from the grain size analysis, the glacial till may be classified as a silty sand (SM) to silty sand with gravel (SM) in accordance with the USCS. The glacial till contains shale fragments, cobbles and boulders.

## 5.6 Limestone Bedrock

Auger refusal was met in Borehole Nos. 19-01 to 19-05, 19-08, 19-09, 19-11, 21-13 and 21-14 at 6.1 m to 7.8 m depths (Elevation 68.9 m to Elevation 67.6 m). Conventional core drilling techniques were used to advance Borehole Nos. 19-01, 19-03, 19-08, 19-09, 19-11, 21-13 and 21-14 beyond the auger refusal depths to termination depths of 8.0 m to 14.4 m (Elevation 67.0 m to Elevation 60.8 m) confirming that auger refusal in these boreholes was met on limestone bedrock with shaly partings. Photographs of the bedrock cores are shown in Appendix C.

A summary of the auger refusal depth (elevation) on inferred boulders or limestone bedrock (with shaly partings) and the bedrock depths (elevations) is shown in Table IV.

<b>Table IV: Summary of Auger Refusal and Bedrock Depths (Elevations) in Boreholes</b>			
Borehole No.	Ground Surface Elevation (m)	Auger Refusal Depth (Elevation) (m)	Bedrock Depth (Elevation) (m)
19-01	74.13	6.5 (67.6)	6.5 (67.6)
19-02	74.37	6.2 (68.2)	-
19-03	75.02	7.0 (68.0)	7.0 (68.0)
19-04	74.98	6.6 (68.4)	-
19-05	74.82	6.7 (68.1)	-
19-08	75.51	7.3 (68.2)	7.3 (68.2)
19-09	75.65	7.6 (68.1)	7.6 (68.1)
19-11	75.71	7.8 (67.9)	7.8 (67.9)
21-13	75.20	6.3 (68.9)	6.3 (68.9)
21-14	74.30	6.1 (68.2)	6.1 (68.2)

A review of the above table indicates that the depth to the bedrock surface ranges from 6.1 m to 7.8 m below existing grade (Elevation 68.9 m to Elevation 67.6 m).

The upper 500 mm to 900 mm of the bedrock appears weathered and highly fractured in Borehole Nos. 19-01, 19-03, 19-11 and 21-14. The Total Core Recovery (TCR) of the bedrock is 80 percent to 100 percent. The Rock Quality Designation (RQD) ranges from 27 percent to 100 percent indicating the bedrock is of a poor to excellent quality. The weathered zone of the bedrock in Borehole No. 21-14 has an RQD of 0 percent indicating a very poor quality bedrock.

Unit weight determination and unconfined compressive strength tests were conducted on twelve (12) rock core sections and the results are summarized in Table V.

<b>Table V: Summary of Unconfined Compressive Strength Test Results – Bedrock Cores</b>				
<b>Borehole No.- Run No.</b>	<b>Depth (m)</b>	<b>Unit Weight (kN/m<sup>3</sup>)</b>	<b>Unconfined Compressive Strength (MPa)</b>	<b>Classification of Rock with respect to Strength <sup>(1)</sup></b>
BH 19-01 – Run 2	7.5 - 7.6	24.7	120.6	Very Strong
BH 19-03 – Run 1	7.5 – 7.6	24.5	176.2	Very Strong
BH 19-08 - Run 2	8.7 – 8.8	24.3	125.7	Very Strong
BH 19-09 – Run 1	8.6 – 8.7	25.6	138.2	Very Strong
BH 19-11 - Run 1	7.8 – 7.9	26.7	199.4	Very Strong
BH 21-13 – Run 3	9.5 – 9.7	24.9	135.1	Very Strong
BH 21-13 – Run 4	10.7 – 10.8	26.6	184.0	Very Strong
BH 21-13 – Run 5	12.1 – 12.2	25.7	153.9	Very Strong
BH 21-13 – Run 6	13.7 – 13.8	26.3	107.8	Very Strong
BH 21-14 – Run 3	9.0 – 9.1	24.6	138.6	Very Strong
BH 21-14 – Run 4	10.4 – 10.5	25.6	125.4	Very Strong
BH 21-14 – Run 5	12.0 – 12.1	25.4	149.4	Very Strong

**Note:**  
 (1) Reference: Fourth Edition – Canadian Foundation Engineering Manual (2006)

A review of the test results indicates the strength of the rock may be classified as very strong in accordance with the Canadian Foundation Engineering Manual (CFEM), Fourth Edition, 2006.

## 5.7 Groundwater Level Measurements

A summary of the groundwater level measurements from the monitoring wells installed in some of the boreholes is shown in Table VI. The monitoring well in Borehole No. 19-01 was damaged and as such, groundwater level measurements could not be made in the damaged monitoring well.

<b>Table VI: Summary of Groundwater Level Measurements</b>			
<b>Borehole No. (BH)</b>	<b>Ground Surface Elevation (m)</b>	<b>Date of Measurement (elapsed time from date of installation)</b>	<b>Groundwater Depth Below Ground Surface (Elevation), m</b>
BH 19-02	74.37	May 10, 2021 (~ 2 years)	2.2 (72.2)
		May 15, 2019 (17 days)	1.9 (72.5)
BH 19-06	75.28	May 10, 2021 (~ 2 years)	2.9 (72.4)
		May 15, 2019 (20 days)	2.4 (72.9)
BH 19-07	75.21	May 10, 2021 (~ 2 years)	1.7 (73.5)
		May 15, 2019 (22 days)	1.4 (73.8)
BH 19-08	75.51	May 10, 2021 (~ 2 years)	4.0 (71.5)
		May 15, 2019 (20 days)	5.7 (69.8)
BH 19-09	75.65	May 10, 2021 (~ 2 years)	5.7 (69.9)
		May 15, 2019 (21 days)	6.0 (69.7)
BH 19-10	75.74	May 10, 2021 (~ 2 years)	Monitoring Well Not Found
		May 15, 2019 (20 days)	2.3 (73.4)
BH 21-13	75.20	October 20, 2021 (13 days)	6.3 (68.9)
BH 21-14	74.30	October 20, 2021 (14 days)	6.6 (67.8)

Water levels were determined in the boreholes at the times and under the conditions stated in the scope of services. Note that fluctuations in the level of groundwater may occur due to a seasonal variation such as precipitation, snowmelt, rainfall activities, and other factors not evident at the time of measurement and therefore may be at a higher level during wet weather periods.

## **6 Site Classification for Seismic Site Response and Liquefaction Potential of Soils**

### **6.1 Site Classification for Seismic Site Response**

The MASW survey report is shown in Appendix B. The results of the MASW survey indicate that the average seismic shear wave velocity is 1610.4 m/s for footings founded on the sound limestone bedrock (with shaly partings) as discussed in Section 8 of this report. This will result in a Class A site class for seismic site response in accordance with Table 4.1.8.4.A of the 2012 Ontario Building Code (OBC), as amended May 2, 2019.

### **6.2 Liquefaction Potential of Soils**

The geotechnical investigation revealed that some of the overburden soils are susceptible to liquefaction during a seismic event. Since the construction of the four (4) level underground parking garage below both towers would require the removal of all overburden soils down and into the bedrock, inclusive of the potential liquefiable soils, liquefiable soils at the site is not an issue for the proposed development.



## 7 Grade Raise Restrictions

A review of the site grading plan, Drawing No. C200 (Revision No. 3 dated May 27, 2021) prepared by EXP revealed that a site grade raise of up to 1.5 m will be realized at the site as part of the proposed development.

Since the subsurface soils consist of cohesionless sandy soils that are not susceptible to consolidation settlement, there is no restriction to raising the grades at the site from a consolidation perspective. Therefore, the proposed 1.5 m site grade raise is considered acceptable from a geotechnical point of view.

## 8 Foundation Considerations

The borehole information indicates the subsurface conditions at the site consist of fill, sandy silt to silty sand, glacial till underlain by limestone bedrock (with shaly partings) contacted at 6.1 m to 7.8 m below existing grade (Elevation 68.9 m to Elevation 67.6 m). Based on a review of the groundwater level measurements the groundwater level ranges from 1.7 m to 6.6 m depths (Elevation 73.5 m to Elevation 67.8 m).

Since the proposed lowest floor slab of the parking garage will be at an approximate Elevation 62.6 m, the proposed buildings may be supported on spread and strip footings designed to bear on the competent sound limestone bedrock (with shaly partings) that is free of soil filled seams and is below all weathered and fractured zones. It has been assumed that all the overburden soils will be removed from the building envelopes down and into the bedrock.

Spread and strip footings founded on the competent sound limestone bedrock, free of soil filled seams and below the weathered and fractured zones, may be designed for a factored geotechnical resistance at Ultimate Limit State (ULS) of 4500 kPa. The factored ULS value includes a resistance factor of 0.5. The Serviceability Limit State (SLS) bearing pressure of the bedrock, required to produce 25 mm settlement of the structure will be much larger than the recommended value for factored geotechnical resistance at ULS. Therefore, the factored geotechnical resistance at ULS will govern the design.

Settlements of footing designed for the above recommended factored geotechnical resistance at ULS and properly constructed are expected to be less than 10 mm.

All the footing beds should be reviewed by a geotechnical engineer to ensure that the bedrock subgrade is capable of supporting the design ULS value. Where fractured rock is encountered, sub-excavation may be undertaken to the underlying more competent bedrock. Alternatively, the footings may be redesigned to a reduced factored geotechnical resistance at ULS. Any sub-excavation which extends below the underside of the footings would have to be raised using 15 MPa lean mix concrete. Also, if the surface of the excavated bedrock is not level, the bedrock surface may be levelled by the placement of concrete.

The resistance to sliding of the building footings will be provided by friction between the footing concrete and the sound limestone bedrock. The factored ULS coefficient of friction is 0.56 and includes a geotechnical resistance factor of 0.8.

A minimum of 1.5 m of earth cover should be provided to exterior footings of heated structures to protect them from damage due to frost penetration. The frost cover should be increased to 2.1 m for unheated structures if snow will not be removed from the vicinity of the footing and 2.4 m of earth cover if snow will be removed from the vicinity of the footing. In areas where earth cover will be less than the required, rigid insulation may be used to protect the footings. Alternatively, a combination of earth cover and rigid insulation may also be used to protect the footings. For this project it is anticipated that the required earth cover for the footings of the proposed buildings will be satisfied, since the footings are anticipated to be at depths greater than 1.5 m below the final grade.

The recommended factored geotechnical resistance at ULS has been calculated by EXP from the borehole information for the design stage only. The investigation and comments are necessarily on-going as new information of underground conditions becomes available. For example, more specific information is available with respect to conditions between boreholes when foundation construction is underway. The

interpretation between boreholes and the recommendations of this report must therefore be checked through field monitoring provided by an experienced geotechnical engineer to validate the information for use during the construction stage.

## 9 Floor Slab Construction and Drainage Requirements

The lowest floor slab of the parking garage below the proposed two (2) tower buildings may be designed as a slab-on-grade. The slab-on-grade should be set on a bed of well packed 19 m clear stone at least 200 mm thick placed on an engineered fill pad at least 300 mm thick placed on the sound limestone bedrock (with shaly partings). The required engineered fill pad should comprise of Ontario Provincial Standard Specification (OPSS)1010 Granular B Type II placed on top of the bedrock in 300 mm thick lifts and each lift compacted to 98 percent standard Proctor maximum dry density (SPMDD). The clear stone will prevent the capillary rise of moisture from the underlying soil to the floor slab. Adequate saw cuts should be provided in the floor slab to control cracking.

It is recommended that a perimeter drainage system around the proposed structure and an underfloor drainage system beneath the slab-on-grade (lowest floor) of the parking garage should be provided. The two (2) drainage systems may comprise of 150 mm diameter perforated pipe or equivalent covered at the top, sides and bottom with a minimum 150 mm thick layer of clear stone that is completely wrapped or covered with a non-woven geotextile such as Terrafix 270R or equivalent. The pipes for the underfloor drainage system should be set at least 300 mm below the underside of the floor slab and placed in parallel rows at 5 m to 6 m centres. The perimeter and underfloor drainage systems should be connected to separate sumps so that at least one system would be operational should the other fail and the design should include back up pumps and generators, in case of mechanical failure and/or power outage.

Reference is made to the November 5,2021 hydrogeological report prepared by EXP and reported under separate cover regarding the estimate of post-construction dewatering flow rates.

The finished exterior grade should be sloped away from the buildings to prevent surface ponding close to the exterior walls.

## 10 Lateral Earth Pressure Against Subsurface Walls

If the space between the subsurface walls and the rock face is to be backfilled, the subsurface walls will be subjected to lateral static earth pressure as well as lateral dynamic earth pressure during a seismic event. The lateral static earth pressure that the subsurface walls would be subjected to may be computed from equations (i) and (ii) and the lateral dynamic earth force from equation (iii) given below.

The equations given below assume that the backfill against the subsurface walls will be free-draining granular material and that subsurface drains will be provided to prevent build-up of hydrostatic pressure behind the wall. Equation (i) will be applicable to the portion of the subsurface wall in the overburden soil. Equation (ii) will be applicable to the portion of the subsurface wall in the bedrock where the earth pressure will be considerably reduced due to the narrow backfill between the subsurface wall and the rock face resulting in an arching effect (Spangler & Handy, 1984). The weight of the overburden soil and any surcharge load stress (such as traffic load at ground surface and foundations of existing adjacent buildings) should be considered as surcharge when computing lateral pressure using equation (ii).

The lateral static earth pressure against the subsurface walls may be computed from the following equation:

$$P = K_0 (\gamma h + q) \dots\dots\dots (i)$$

- where
- P = lateral earth pressure acting on the subsurface wall; kN/m<sup>2</sup>
  - K<sub>0</sub> = lateral earth pressure coefficient for 'at rest' condition for Granular B Type II backfill material = 0.50
  - γ = unit weight of free draining granular backfill; OPSS Granular B Type II = 22 kN/m<sup>3</sup>
  - h = depth of point of interest below top of backfill, m
  - q = surcharge load stress, kPa

Lateral static earth pressure due to narrow earth backfill between subsurface wall and rock face at depth z; σ<sub>n</sub>:

$$\sigma_n = \frac{\gamma B}{2 \tan \delta} \left( 1 - e^{-2k \frac{z}{B} \tan \delta} \right) + kq \dots\dots\dots (ii)$$

where

- γ = unit weight of backfill = 22 kN/m<sup>3</sup>
- B = backfill width (m)
- z = depth from top of wall (m)
- δ = friction angle between the backfill and wall and rock (assumed to be equal) = 17 degrees
- k = lateral earth pressure coefficient for 'at rest' condition = 0.50
- q = surcharge pressure including pressures from overburden soil, traffic at ground surface and foundations from existing adjacent buildings (kPa)

The lateral dynamic (seismic) thrust may be computed from the equation given below:

$$\Delta_{Pe} = \gamma H^2 \frac{a_h}{g} F_b \dots\dots\dots (iii)$$

- where
- $\Delta_{Pe}$  = dynamic thrust in kN/m of wall
  - H = height of wall, m
  - $\gamma$  = unit weight of free draining granular backfill; OPSS Granular B Type II = 22 kN/m<sup>3</sup>
  - $\frac{a_h}{g}$  = seismic coefficient = 0.32
  - $F_b$  = thrust factor = 1.0

The dynamic thrust does not take into account the surcharge load. The resultant force acts approximately at 0.63H above the base of the wall.

All subsurface walls should be properly waterproofed.

Where the basement walls will be poured against the bedrock or temporary shoring, vertical drainage board must be installed on the face of the excavation wall or temporary shoring to provide necessary drainage. Vertical drainage board such as Alidrain, Geodrain, Miridrain or equivalent may be used for this purpose. A schematic of the location of the drainage board is shown in Figure 22. Full coverage using drainage boards can be considered to minimize the risk of water penetration through the subsurface basement walls.

Where the upper portion of the subsurface basement wall is backfilled with granular material, the vertical drainage board should extend into the backfill to provide drainage of the backfill. The top of the drainage board should be covered with a fabric filter to prevent the loss of overlying soil into the drainage board.

The vertical drainage board should be connected to a solid discharge pipe that passes through the foundation wall and outlets to a solid pipe inside the building that leads to a sump, as shown in Figure 22. The solid pipe inside the building should be connected to a separate sump from the sumps used for the perimeter and underfloor drains, so that this system would be operational should one of the other drainage systems fail.

## 11 Excavations and De-Watering Requirements

### 11.1 Overburden Soil Excavation

The excavations in the soil may be undertaken using large heavy mechanical equipment capable of removing debris within the fill as well as cobbles and boulders within the fill and underlying glacial till.

All excavations must be undertaken in accordance with the Occupational Health and Safety Act (OHSA), Ontario Reg. 213/91. Based on the definitions provided in OHSA, the subsurface soils on site are considered to be Type 4 and as such must be cut back at 3H:1V from the bottom of the excavation. It is anticipated that due to the significant depth of the excavation and the proximity of the excavation to existing buildings and infrastructure, the excavations will likely have to be undertaken within the confines of a shoring system. The shoring system may consist of steel H soldier pile and timber lagging system, interlocking sheeting system and/or secant pile shoring system.

The type of shoring system required would depend on a number of factors including:

- Proximity of the excavation to existing structures and infrastructure;
- Type of foundations of the existing adjacent buildings and the difference in founding levels between the foundations of new buildings and existing adjacent buildings; and
- The subsurface soil, bedrock and groundwater conditions.

A conventional shoring system consisting of soldier pile and timber lagging is more flexible compared to the interlocking steel sheeting system and the secant pile shoring system. In areas where there is concern for lateral yielding of the soils and the potential of settlement of nearby structures and infrastructure, the use of a steel interlocking sheeting system or secant pile system can be considered. The steel interlocking sheeting and secant pile system also provide cut-off to groundwater flows into the excavation. In areas where the potential of settlement of the nearby structures is low, soldier pile and timber lagging system may be used. The shoring system will require lateral restraint provided by tiebacks consisting of rock anchors. Due to the presence of cobbles and boulders in the subsurface soils, pre-drilling may be required for the installation of the soldier piles and a thickened section may be required for the interlocking steel sheeting system.

The need for a shoring system, the appropriate type of shoring system and the design and installation of the shoring system should be determined/conducted by a professional engineer experienced in shoring design and by a contractor experienced in the installation of shoring systems. The shoring system should be designed and installed in accordance with OHSA and the 2006 CFEM (Canadian Foundation Engineering Manual (Fourth Edition)).

#### 11.1.1 Soldier Pile and Timber Lagging System

A conventional steel H soldier pile and timber lagging shoring system must be designed to support the lateral earth pressure given by the expression below:

$$P = k (\gamma h + q)$$

where  $P =$  the pressure, at any depth,  $h$ , below the ground surface

- k = applicable earth pressure coefficient; active lateral earth pressure coefficient = 0.33  
 'at rest' lateral earth pressure coefficient = 0.50
- $\gamma$  = unit weight of soil to be retained, estimated at 21 kN/m<sup>3</sup>
- h = the depth, in metres, at which pressure, P, is being computed
- q = the equivalent surcharge acting on the ground surface adjacent to the shoring system

The pressure distribution assumes that drainage is permitted between the lagging boards and that no build-up of hydrostatic pressure may occur.

The shoring should be designed using appropriate 'k' values depending on the location of any settlement-sensitive infrastructure (roadways sidewalks and underground services) and building structures. The traffic loads on the streets should be considered as surcharge. It may be necessary to toe the soldier piles into the sound rock below the soils. For guidance, if there is room to permit at least a 1.0 m of rock ledge around the perimeter of the excavation, the soldier piles could be toed into the upper levels of the rock provided that a rock bolt and plate arrangement is installed on the rock face to support the toe. The rock bolt should be designed to take the full toe pressure.

### 11.1.2 Secant Pile Shoring System

Groundwater cut-off shoring systems such as steel interlocking sheeting and secant pile shoring system should be designed to resist 'at rest' lateral earth thrust in addition to the hydrostatic thrust as given by the expression below:

$$P_0 = K_0 q (h_1 + h_2) + \frac{1}{2} K_0 \gamma h_1^2 + K_0 \gamma h_1 h_2 + \frac{1}{2} K_0 \gamma' h_2^2 + \frac{1}{2} \gamma_w h_2^2$$

Where:

- $P_0$  = 'at rest' earth and water thrusts acting against secant pile wall (kN/m)
- $K_0$  = 'at rest' lateral earth pressure coefficient = 0.50
- q = surcharge acting adjacent to the excavation (kPa)
- $h_1$  = height of shoring from the ground surface to groundwater table (m)
- $h_2$  = height of shoring from groundwater table to the bottom of excavation (m)
- $\gamma$  = estimated unit weight of the soil to be retained = 21 kN/m<sup>3</sup>
- $\gamma'$  = submerged unit weight of soil = 11 kN/m<sup>3</sup>
- $\gamma_w$  = unit weight of water = 9.8 kN/m<sup>3</sup>

If the secant walls are incorporated into the design of the structures, they should also be designed to resist soil dynamic thrust and hydrodynamic thrust due to a seismic event.

Secant pile walls consist of overlapping concrete piles that form a stronger watertight barrier compared with the sheeting system. They can be constructed with conventional drilling methods. Secant pile walls typically include both reinforced primary and un-reinforced secondary piles. The primary piles overlap the



secondary piles, with secondary piles essentially acting as concrete lagging. The reinforcement in the primary piles generally consists of steel reinforcing bar cages or steel beams. The result is a continuous intersecting line of concrete piles that are placed before any excavation is performed.

### 11.1.3 Additional Comments

A pre-construction condition survey of adjacent neighboring structures and infrastructure should be undertaken prior to the start of any construction activities.

The shoring system as well as adjacent settlement sensitive structures and infrastructure should be monitored for movement (deflection) on a periodic basis during construction operations.

Many geologic materials deteriorate rapidly upon exposure to meteorological elements. Unless otherwise specifically indicated in this report, walls and floors of excavations must be protected from moisture, desiccation, and frost action throughout the course of construction.

### 11.1.4 Rock Anchors

The shoring system will require lateral restraint by tiebacks in the form of grouted rock anchors. For tiebacks that encroach onto neighboring properties, permission will be required from adjacent property owners for the installation of the tiebacks. It is noted that if permission is not received from adjacent property owners for the installation of tiebacks, the shoring system may have to be supported by cross bracing or the use of rakers on the inside of the excavation.

Grouted rock anchors may fail in one or more of the following manners:

- a) Failure of the grout/tendon bond,
- b) Failure of the steel tendon or top anchorage,
- c) Failure of the rock/grout bond; or
- d) Failure of the rock mass.

Failure modes a) and b) require review by the structural engineer. Geotechnical related failure modes c) and d) for vertical grouted anchors are discussed below:

#### **Failure of the Rock/Grout Bond:**

- The unfactored ultimate limit state (ULS) bond strength of the sound rock/grout interface may be taken as 2000kPa (2.0 MPa). For semi-empirical analysis, the factored ULS bond strength is 800 kPa, using a geotechnical resistance factor of 0.4. The factored ULS bond strength may be taken as 1200 kPa and includes a geotechnical resistance factor of 0.6 based on conducting proof test on all anchors. The geotechnical resistance factors are in accordance with the 2006 CFEM. The unconfined compressive strength of the grout is assumed to be 35 MPa.

#### **Failure of the Rock Mass:**

- A 90-degree apex (45 degrees from the vertical) should be used to calculate the rock volume using the theoretical rock cone. The apex is located at the middle of the bonded length.
- The submerged unit weight of the bedrock equal to 15.6 kN/m<sup>3</sup> should be used in the calculations.

- The weathered and highly fractured zone of the limestone bedrock (with shaly partings) should not be included in the bond length when calculating the anchor capacity.
- The unbonded length of the anchor is equal to the height of the rock cone less half of the bonded length.
- The minimum bonded length is 3 m.
- For groups of rock anchors, the anchor group resistance to rock mass failure should be reduced to reflect the theoretical rock cone overlap.

Corrosion protection for the anchors should be in accordance with OPSS 942.

Pre-production or design performance tests on selected rock anchors should be conducted in accordance with the OPSS 942. Proof load tests should be conducted on all anchors and should be in accordance with the OPSS 942.

## 11.2 Rock Excavation

Excavation of the underlying bedrock will require line drilling and blasting techniques.

### 11.2.1 Rock Support

Excavations within the bedrock may be undertaken with near vertical sides subject to review by a geotechnical engineer. The rock face may require support in the form of rock bolts to maintain the integrity of the rock face. In the upper weathered/fractured zones of the bedrock, rock bolts in combination with wire mesh system and/or shotcrete may be required. The excavation will have to be undertaken in a staged approach with the rock excavated in a pre-determined depth interval (for example every 3 m). The exposed rock face in each stage will have to be examined by a geotechnical engineer to determine the number of rock bolts required. The rock bolt system should be installed in this manner to the bottom of the excavation. The design of the rock bolts should be in accordance with the design of the rock anchors in Section 11.1.4 of this report, except there is no stipulation regarding minimum bonded length.

### 11.2.2 Vibration Control

The vibration limits for blasting should be in accordance with City of Ottawa Special Provisions (SP No. 1201).

It is recommended that a pre-construction survey of adjacent building(s) and infrastructure be undertaken prior to any earth (soil) and rock excavation work as well as vibration monitoring during excavation, blasting and construction operations. Prior to the commencement of blasting, a detailed blast methodology should be submitted by the Contractor.

## 11.3 De-Watering Requirements

Excavations above the groundwater may be dewatered by conventional sump pumping techniques. Excavations below the groundwater level and the water bearing sandy silt to silty and glacial till are expected to be more problematic and may result in greater water seepage, loss of ground and disturbance of the soils. Under these conditions, it is recommended that these excavations should be undertaken within the confines of a shoring system that is also designed to cut-off groundwater flows towards the excavation

and minimize groundwater flows into the shored excavation. In this regard, seepage of groundwater into the shored excavation should still be anticipated but may be removed by collecting the water at low points within the excavation and pumping from sumps. In areas of high infiltration, a higher seepage rate should be anticipated and high-capacity pumps may be required to keep the excavation dry.

Reference is made to the hydrogeological investigation report dated November 5, 2021 prepared by EXP and reported under separate cover regarding estimated groundwater flows and Permit to Take Water (PTTW) requirements. Standard paragraphs regarding PTTW are presented in the following paragraphs.

The excavation for this project will necessitate groundwater removal from the site. It is noteworthy to mention that new legislation came into force in Ontario on March 29, 2016 to regulate groundwater takings for construction dewatering purposes. Prior to March 29, 2016, a Category 2 Permit to Take Water (PTTW) was required from the Ontario Ministry of the Environment, Conservation and Parks (MECP) for groundwater takings related to construction dewatering, where taking volumes in excess of 50 m<sup>3</sup>/day, but less than 400 m<sup>3</sup>/day, and the taking duration was no more than 30 consecutive days. The new legislation replaces the Category 2 PTTW for construction dewatering with a new process under the Environmental Activity and Sector Registry (EASR). The EASR is an on-line registry, which allows persons engaged in prescribed activities, such as water takings, to register with the MECP instead of applying for a PTTW.

To be eligible for the new EASR process, the construction dewatering taking must be less than 400 m<sup>3</sup>/day under normal conditions. The water taking can be groundwater, storm water, or a combination of both. It should be noted that the 30-consecutive day limit on the water taking under the old Category 2 PTTW process has been removed in the new EASR process. Also, it should be noted that the EASR process requires two technical studies be prepared by a Qualified Person, prior to any water taking. These studies include a Water Taking Report, which provides assurance that the taking will not cause any unacceptable impacts, and a Discharge Plan, which provides assurance that the discharge will not result in any adverse impacts to the environment. EXP has qualified persons who can prepare these types of reports, if required. A significant advantage of the new EASR process over the former Category 2 PTTW process, is that the groundwater taking may begin immediately after completing the on-line registration of the taking and paying the applicable fee, assuming the accompanying technical studies have been completed. The former PTTW process typically took more than 90 days, which had the potential to impact construction schedules.

Although this investigation has estimated the groundwater levels at the time of the fieldwork, and commented on dewatering and general construction problems, conditions may be present which are difficult to establish from standard boring and excavating techniques and which may affect the type and nature of dewatering procedures used by the contractor in practice. These conditions include local and seasonal fluctuations in the groundwater table, erratic changes in the soil profile, thin layers of soil with large or small permeabilities compared with the soil mass, etc. Only carefully controlled tests using pumped wells and observation wells will yield the quantitative data on groundwater volumes and pressures that are necessary to adequately engineer construction dewatering systems.

## **12 Impact of Groundwater Lowering at the Site on Municipal Services in Adjacent Roadways and Adjacent Structures**

### **12.1 Municipal Services**

The impact of groundwater lowering at the site on the municipal underground services was assessed by reviewing the EXP November 5, 2021 hydrogeological report, the borehole information, the municipal service drawings along the sections of Forest Avenue, Bond Street and Richmond Road that border the site and by conducting settlement calculations. The settlement calculations were based on the assumption that the subsurface soil and bedrock conditions encountered in the boreholes on site are similar to the subsurface soil conditions in the assessed sections of the roadways noted above. The settlement calculations indicated the impact of short and long-term groundwater lowering at the site on the municipal services is negligible.

### **12.2 Adjacent Structures**

The impact of groundwater lowering at the site on adjacent surrounding building structures was assessed by reviewing the EXP November 5, 2021 hydrogeological report, the borehole information and by conducting settlement calculations. The settlement calculations were based on the assumption that the subsurface soil and bedrock conditions at the adjacent surrounding building structures are similar to the subsurface soil and bedrock conditions encountered in the boreholes on the site for the two (2) proposed buildings.

Details regarding the foundations of the existing 20 story high-rise building (with an underground parking garage) located next to the site along the east property line of the site of the two (2) proposed buildings were not available at the time of preparing this report. However, based on the assumption that the subsurface conditions of the property of the existing high-rise building are similar to the site for the proposed buildings, it is considered that the high-rise building is supported by foundations bearing on the bedrock, since the subsurface soils are not considered capable of supporting the foundation loads of a 20-story building. In this case, for foundations of the existing 20 story building founded on the bedrock, the temporary (short-term) and permanent (long-term) lowering of the groundwater table at the site for the two (2) proposed buildings is not anticipated to impact the adjacent existing 20 story building.

For the other adjacent surrounding buildings with assumed similar subsurface soil and bedrock conditions as the site for the proposed two (2) new buildings, settlement calculations indicate that settlement of the subsurface soils on adjacent surrounding building properties due to the temporary and permanent lowering of the groundwater table at the site of the two (2) proposed buildings is negligible. Therefore, the lowering of the groundwater table at the site is not expected to adversely impact the adjacent surrounding building structures.

While no impact to the existing adjacent surrounding structures is anticipated from the lowering of the groundwater level, it is considered prudent and therefore recommended that settlement monitoring of the existing adjacent surrounding buildings and infrastructure be conducted during the construction of the two (2) proposed buildings.

## 13 Backfilling Requirements and Suitability of On-Site Soils for Backfilling Purposes

The soils to be excavated from the site will comprise topsoil, silty sand with gravel fill, sandy silt to silty sand, glacial till and limestone bedrock. From a geotechnical perspective, these soils and the limestone bedrock are not considered suitable for reuse as backfill material in the interior or exterior of the building and should be discarded. It may be possible to use portions of the fill, sandy silt to silty sand and glacial till above the groundwater level in landscaped areas, subject to further examination and testing at time of construction. However, these soils are subject to moisture absorption due to precipitation and must be protected at all times from the elements.

Therefore, it is anticipated that all the material required for backfilling purposes in the interior and exterior of the proposed buildings and in the underground service trenches will need to be imported and should preferably conform to the following specifications:

- Engineered fill, underfloor fill including backfilling in service trenches inside the building - OPSS 1010 (as amended by SSP110S13) for Granular B Type II (50 mm minus) placed in 300 mm thick lifts with each lift compacted to 98 percent SPMDD beneath the floor slab,
- Backfill against exterior subsurface walls - OPSS 1010 Granular B Type II placed in 300 mm thick lifts and compacted to 95 percent SPMDD,
- Trench backfill outside building area, and fill placement to subgrade level for pavement - OPSS 1010 Select Subgrade Material (SSM), free of organics, debris and with a natural moisture content within 2 percent of the optimum moisture content. It should be placed in 300 mm thick lifts compacted to minimum 95 percent SPMDD; and
- Landscaped areas - Clean fill that is free of organics and deleterious material and is placed in 300 mm thick lifts with each lift compacted to 92 percent of the SPMDD.

To minimize settlement of the pavement structure over services trenches, the trench backfill material within the frost zone, to 1.8 m depth below final grade, should match the existing material along the trench walls to minimize differential frost heaving of the subgrade soil, provided this material is compactible. Otherwise, frost tapers may be required.

## 14 Access Roads and Parking Areas

### 14.1 Pavement Structures Constructed Over Earth

The subgrade for the parking lots and access roads at the site is anticipated to consist of imported granular fill (compacted to 95 percent SPMDD) used to raise the grades at the site. Pavement structure thicknesses required for light and heavy-duty traffic on the access roads and in parking lots were computed and are shown in Table VII. The pavement structure thicknesses are based upon an estimate of the properties of the imported granular fill subgrade and functional design life of eight (8) to ten (10) years. The proposed functional design life represents the number of years to the first rehabilitation, assuming regular maintenance is carried out.

<b>Table VII: Recommended Pavement Structure Thicknesses – Pavement Constructed Over Earth</b>			
<b>Pavement Layer</b>	<b>Compaction Requirements</b>	<b>Light Duty Parking Areas</b>	<b>Heavy Duty Parking Areas and Access Roads</b>
Asphaltic Concrete (PG 58-34)	Minimum 92% MRD	65 mm – SP12.5 Cat B or HL3	40 mm – 12.5 Cat B/HL3 50 mm – 19.0 Cat B/HL8
Granular A Base (OPSS 1010) (crushed limestone)	100% SPMDD	150 mm	150 mm
Granular B Sub-base, Type II (OPSS 1010)	100% SPMDD	300 mm	450 mm
SPMDD denotes Standard Proctor Maximum Dry Density, ASTM-D698-12e2 MRD denotes Maximum Relative Density, ASTM D2041			

The foregoing design assumes that construction is carried out during dry periods and that the subgrade is stable under the load of construction equipment. If construction is carried out during wet weather, and heaving or rolling of the subgrade is experienced, additional thickness of granular material and/or geotextile may be required.

Additional comments on the construction of the access roads and parking lots are as follows:

- (1) As part of the subgrade preparation, the proposed access road and parking lot areas should be stripped of unsuitable fill and other obviously unsuitable material. Fill required to raise the grades to design elevations should be organic-free and at a moisture content which will permit compaction to the densities indicated. After all the underground services have been installed, the subgrade should be properly shaped, crowned and proofrolled with a heavy roller in the full-time presence of a representative of this office. Any soft or spongy subgrade areas detected should be sub-excavated and properly replaced with suitable approved backfill compacted to 95 percent SPMDD.

- (2) The long-term performance of the pavement structure is highly dependent upon the subgrade support conditions. Stringent construction control procedures should be maintained to ensure that uniform subgrade moisture and density conditions are achieved. The need for adequate drainage cannot be over-emphasized. Sub-drains must be installed on both sides of the proposed access roadways. In the parking areas, they should be installed at low points and should be continuous between catch basins to intercept excess surface and subsurface moisture and to prevent subgrade softening. This will ensure no water collects in the granular course, which could result in pavement failure during the spring thaw. The location and extent of subdrainage required within the paved areas should be reviewed by this office in conjunction with the proposed site grading.
- (3) To minimize the problems of differential movement between the pavement and catchbasins/manhole due to frost action, the backfill around the structures should consist of free-draining granular preferably conforming to OPSS Granular B Type II material.
- (4) The finished pavement surface should be free of depressions and should be sloped (preferably at a minimum cross fall of 2 percent) to provide effective surface drainage towards catch basins. Surface water should not be allowed to pond adjacent to the outside edges of paved areas.
- (5) The granular materials used for pavement construction should conform to Ontario Provincial Standard Specifications (OPSS) for Granular A and Granular B Type II and should be compacted to 100 percent SPMDD. The asphaltic concrete and its placement should meet OPSS 1151 requirements. It should be placed and compacted to OPSS 311 and 313.

## 14.2 Pavement Structures Constructed Over Parking Garage Structure

The recommended pavement structures constructed on top of the parking garage structure are shown in Table VIII.

<b>Table VIII: Recommended Pavement Structure Thicknesses – Pavement Constructed Over Parking Structure</b>			
<b>Pavement Layer</b>	<b>Compaction Requirements</b>	<b>Light Duty Parking Areas</b>	<b>Heavy Duty Parking Areas and Access Roads</b>
Asphaltic Concrete (PG 58-34)	Minimum 92% MRD	50 mm – SP12.5 Cat B or HL3	40 mm – 12.5 Cat B/HL3 50 mm – 19.0 Cat B/HL8
Granular A Base (OPSS 1010) (crushed limestone)	100% SPMDD	150 mm	150 mm
Granular B Sub-base, Type II (OPSS 1010)	100% SPMDD	100 mm	100 mm
SPMDD denotes Standard Proctor Maximum Dry Density, ASTM-D698-12e2 MRD denotes Maximum Relative Density, ASTM D2041			



The granular materials used for pavement construction should conform to Ontario Provincial Standard Specifications (OPSS) for Granular A and Granular B Type II and should be compacted to 100 percent SPMDD. The asphaltic concrete and its placement should meet OPSS 1151 requirements. It should be placed and compacted to OPSS 311 and 313.

It is recommended that EXP be retained to review the final pavement structure design (constructed over earth and parking garage structure) and drainage plans prior to construction to ensure that they are consistent with the recommendations of this report.



## 15 Corrosion Potential of Subsurface Soils and Bedrock

Chemical tests limited to pH, sulphate, chloride and resistivity were undertaken on two (2) soil samples (fill and glacial till) and two (2) sections of bedrock cores. A summary of the results is shown in Table IX. The laboratory certificate of analysis is shown in Appendix A.

<b>Table IX: pH, Sulphate, Chloride and Resistivity Test Results on Soil Samples and Bedrock Cores</b>					
<b>Borehole No. (BH); Sample/Run No. (SS)</b>	<b>Depth (m)</b>	<b>pH</b>	<b>Sulphate (%)</b>	<b>Chloride (%)</b>	<b>Resistivity (ohm-cm)</b>
<b>Soil Samples</b>					
BH 19-03: SS5	3.0 – 3.6	8.00	0.0050	0.0120	2480
BH 19-12: SS4	2.3 – 2.9	8.17	0.0121	0.0114	1950
<b>Bedrock Cores</b>					
BH 19-01: Run 1	6.5 – 6.6	8.55	0.0042	0.0025	2490
BH 19-11: Run 1	7.8 – 7.9	8.59	0.0026	0.0021	2110

The sulphate test results indicate the soil samples and bedrock core sections have a negligible sulphate attack on subsurface concrete. The concrete should be in accordance with CSA A.23.1-14.

Based on a review of the resistivity test results, the soil samples and bedrock core sections are considered to be corrosive to mildly corrosive to bare steel as per the National Association of Corrosion Engineers (NACE). Appropriate measures should be undertaken to protect buried steel elements from corrosion.

## 16 General Comments

The comments given in this report are intended only for the guidance of the design engineers. The number of boreholes required to determine the localized underground conditions between boreholes affecting construction costs, techniques, sequencing, equipment, scheduling, etc., would be much greater than has been carried out for design purposes. Contractors bidding on or undertaking the works should in this light, decide on their own investigations, as well as their own interpretation of the factual borehole results to draw their own conclusions as to how the subsurface conditions may affect them.

The information contained in this report is not intended to reflect on environmental aspects of the soils. Reference is made to the Phase One and Two Environmental Site Assessments completed by EXP and reported under separate covers.

We trust this report will be satisfactory for your purposes. Should you have any questions, please do not hesitate to contact this office.

EXP Services Inc.

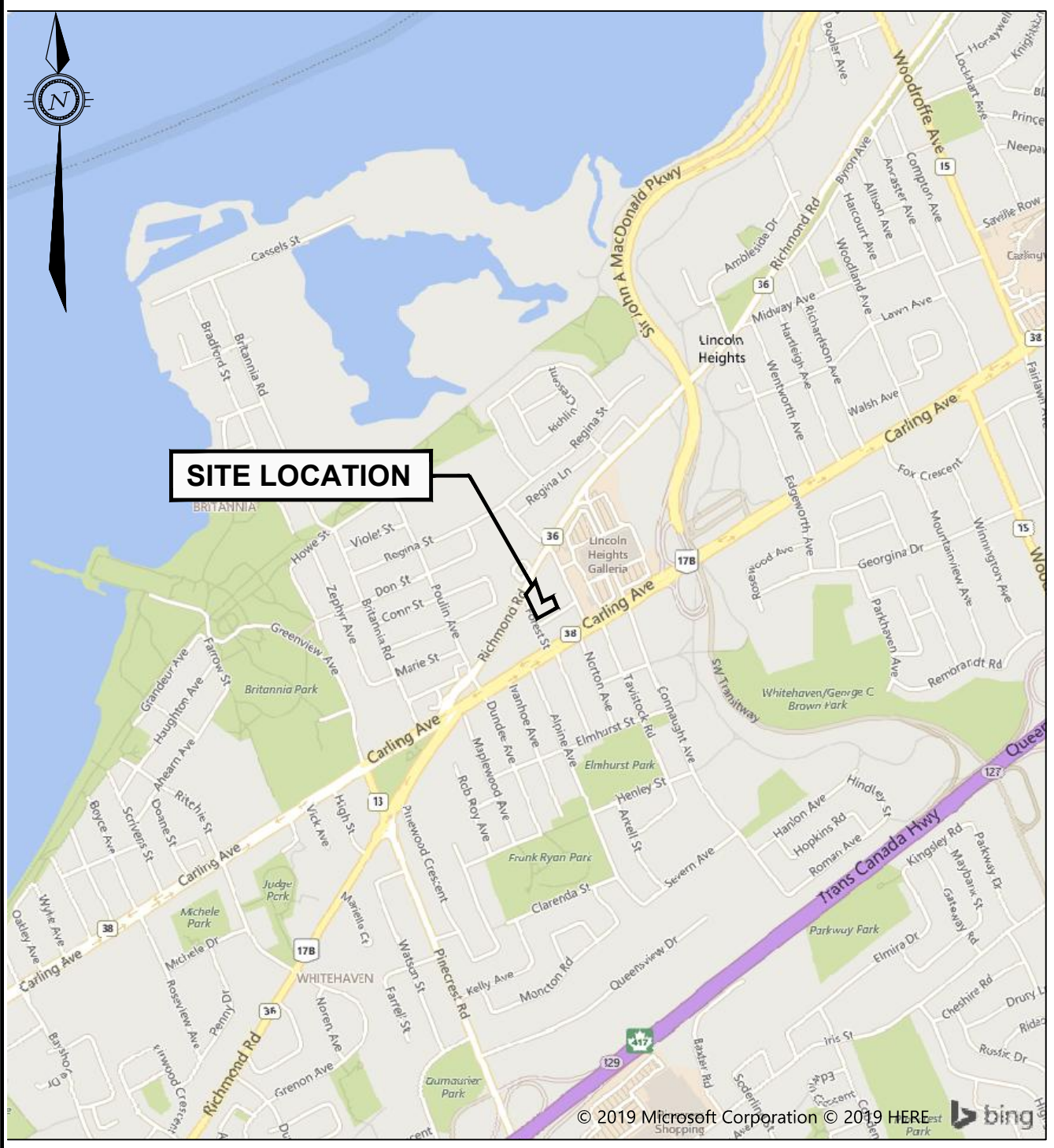
Client: 11061917 Canada Inc.  
Project Name: Geotechnical Investigation - Residential Development  
Location: 365 Forest Street, Ottawa, ON.  
EXP Project Number: OTT-00252625-A0  
Date: November 5, 2021

## Figures





**SITE LOCATION**



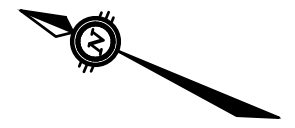
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 Last Plotted: 6/24/2019 1:56:20 PM  
 Pen Table: exp-64.ctb  
 Plotted by: NugentM




**EXP Services Inc.** [www.exp.com](http://www.exp.com)  
 t: +1.613.688.1899 | f: +1.613.225.7337  
 2650 Queensview Drive, Suite 100  
 Ottawa, ON K2B 8H6, Canada

DATE <b>MAY 2019</b>		CLIENT: <b>11061917 CANADA INC.</b>		project no. OTT-00252625-A0
DESIGN M.M.	CHECKED C.H.	TITLE: <b>SITE LOCATION PLAN</b>		scale N.T.S
DRAWN BY A.O.		365 FOREST ST., 1420 RICHMOND RD. & 2589 BOND ST., OTTAWA, ON		<b>FIG 1</b>

Filename: P:\Projects\Civil\252000\011-00252570-A0 - 365 Forest Ave - 11061917 Canada Inc\60-EXECUTION\64-DWG\252570-BH-UPDATED.dwg  
 Last Saved: Oct 28, 2021 7:08 AM Last Plotted: Oct 28, 2021 7:08 AM Plotted by: mckee

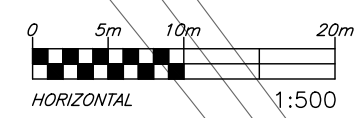
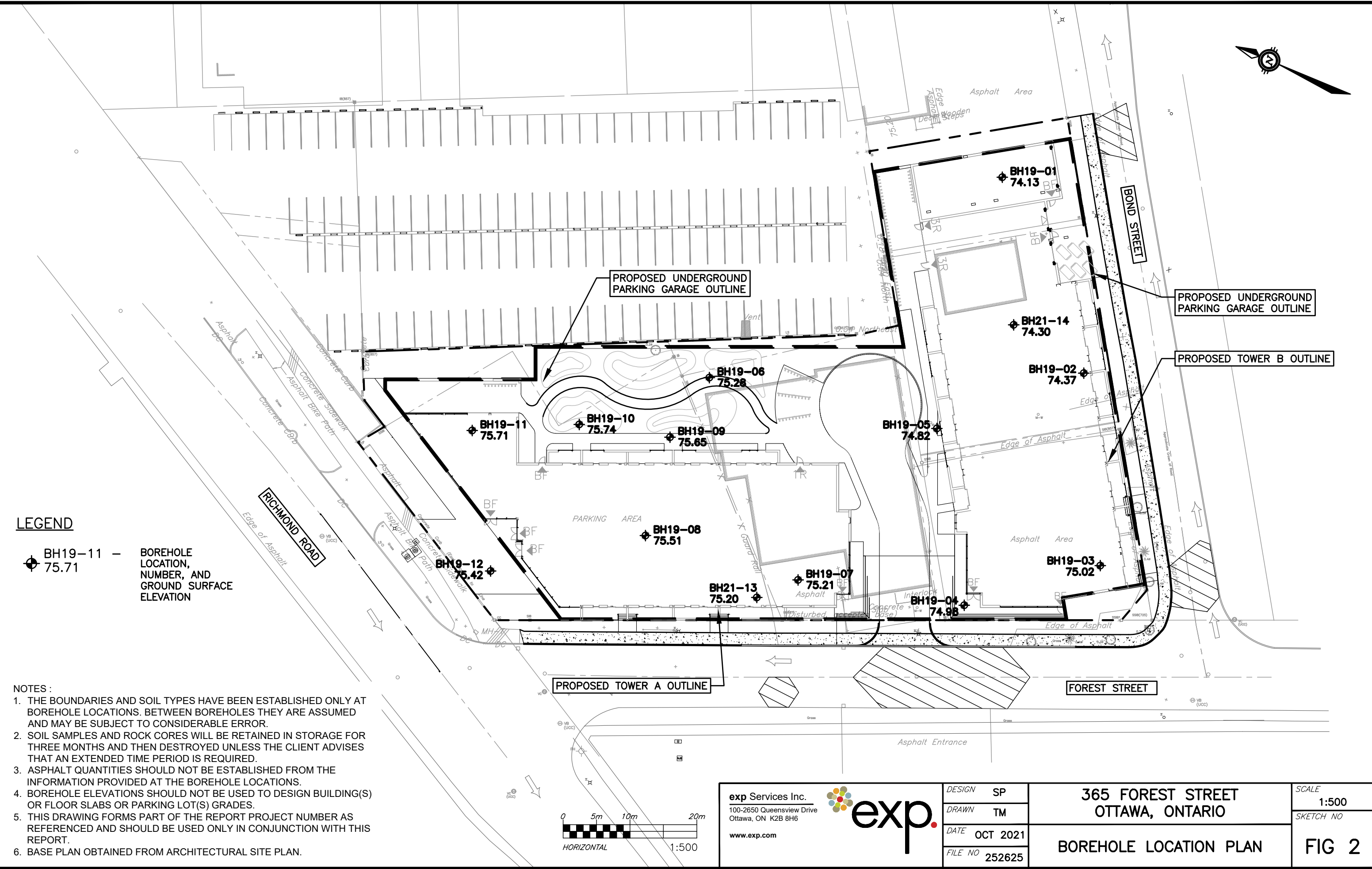


**LEGEND**


 BH19-11 - BOREHOLE LOCATION, NUMBER, AND GROUND SURFACE ELEVATION  
 75.71

**NOTES :**

1. THE BOUNDARIES AND SOIL TYPES HAVE BEEN ESTABLISHED ONLY AT BOREHOLE LOCATIONS. BETWEEN BOREHOLES THEY ARE ASSUMED AND MAY BE SUBJECT TO CONSIDERABLE ERROR.
2. SOIL SAMPLES AND ROCK CORES WILL BE RETAINED IN STORAGE FOR THREE MONTHS AND THEN DESTROYED UNLESS THE CLIENT ADVISES THAT AN EXTENDED TIME PERIOD IS REQUIRED.
3. ASPHALT QUANTITIES SHOULD NOT BE ESTABLISHED FROM THE INFORMATION PROVIDED AT THE BOREHOLE LOCATIONS.
4. BOREHOLE ELEVATIONS SHOULD NOT BE USED TO DESIGN BUILDING(S) OR FLOOR SLABS OR PARKING LOT(S) GRADES.
5. THIS DRAWING FORMS PART OF THE REPORT PROJECT NUMBER AS REFERENCED AND SHOULD BE USED ONLY IN CONJUNCTION WITH THIS REPORT.
6. BASE PLAN OBTAINED FROM ARCHITECTURAL SITE PLAN.

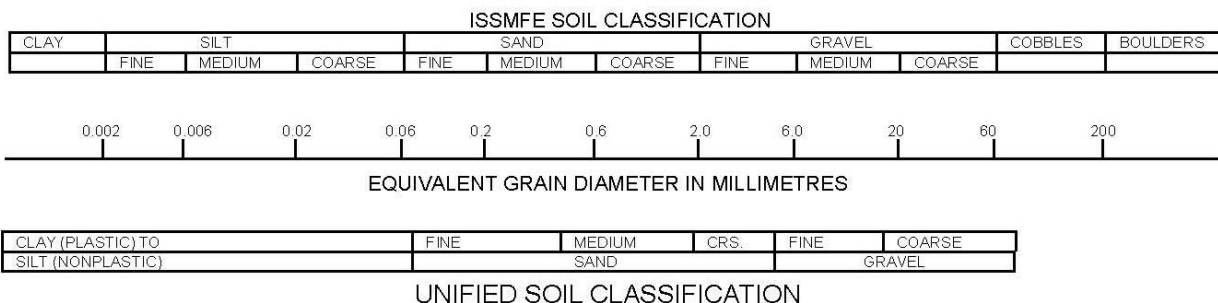


<b>exp Services Inc.</b> 100-2650 Queensview Drive Ottawa, ON K2B 8H6 www.exp.com	DESIGN	SP	<b>365 FOREST STREET</b> <b>OTTAWA, ONTARIO</b>	SCALE	1:500
	DRAWN	TM		<b>BOREHOLE LOCATION PLAN</b>	SKETCH NO
	DATE	OCT 2021			
	FILE NO	252625			



## Notes On Sample Descriptions

- All sample descriptions included in this report follow the Canadian Foundations Engineering Manual soil classification system. This system follows the standard proposed by the International Society for Soil Mechanics and Foundation Engineering. Laboratory grain size analyses provided by **exp** Services Inc. also follow the same system. Different classification systems may be used by others; one such system is the Unified Soil Classification. Please note that, with the exception of those samples where a grain size analysis has been made, all samples are classified visually. Visual classification is not sufficiently accurate to provide exact grain sizing or precise differentiation between size classification systems.



- Fill:** Where fill is designated on the borehole log it is defined as indicated by the sample recovered during the boring process. The reader is cautioned that fills are heterogeneous in nature and variable in density or degree of compaction. The borehole description may therefore not be applicable as a general description of site fill materials. All fills should be expected to contain obstruction such as wood, large concrete pieces or subsurface basements, floors, tanks, etc., none of these may have been encountered in the boreholes. Since boreholes cannot accurately define the contents of the fill, test pits are recommended to provide supplementary information. Despite the use of test pits, the heterogeneous nature of fill will leave some ambiguity as to the exact composition of the fill. Most fills contain pockets, seams, or layers of organically contaminated soil. This organic material can result in the generation of methane gas and/or significant ongoing and future settlements. Fill at this site may have been monitored for the presence of methane gas and, if so, the results are given on the borehole logs. The monitoring process does not indicate the volume of gas that can be potentially generated nor does it pinpoint the source of the gas. These readings are to advise of the presence of gas only, and a detailed study is recommended for sites where any explosive gas/methane is detected. Some fill material may be contaminated by toxic/hazardous waste that renders it unacceptable for deposition in any but designated land fill sites; unless specifically stated the fill on this site has not been tested for contaminants that may be considered toxic or hazardous. This testing and a potential hazard study can be undertaken if requested. In most residential/commercial areas undergoing reconstruction, buried oil tanks are common and are generally not detected in a conventional geotechnical site investigation.
- Till:** The term till on the borehole logs indicates that the material originates from a geological process associated with glaciation. Because of this geological process the till must be considered heterogeneous in composition and as such may contain pockets and/or seams of material such as sand, gravel, silt or clay. Till often contains cobbles (60 to 200 mm) or boulders (over 200 mm). Contractors may therefore encounter cobbles and boulders during excavation, even if they are not indicated by the borings. It should be appreciated that normal sampling equipment cannot differentiate the size or type of any obstruction. Because of the horizontal and vertical variability of till, the sample description may be applicable to a very limited zone; caution is therefore essential when dealing with sensitive excavations or dewatering programs in till materials.

# Log of Borehole BH 19-01



Project No: OTT-00252625-A0  
 Project: Residential Development  
 Location: 365 Forest Street, Ottawa, Ontario  
 Date Drilled: April 30, 2019  
 Drill Type: CME-75 Truck Mounted Drill Rig  
 Datum: Geodetic Elevation  
 Logged by: M.L. Checked by: I.T.

Figure No. 3  
 Page. 1 of 1

- Split Spoon Sample
- Auger Sample
- SPT (N) Value
- Dynamic Cone Test
- Shelby Tube
- Shear Strength by Vane Test
- Combustible Vapour Reading
- Natural Moisture Content
- Atterberg Limits
- Undrained Triaxial at % Strain at Failure
- Shear Strength by Penetrometer Test

G W L	SOIL DESCRIPTION	Geodetic Elevation m	Depth	Standard Penetration Test N Value				Combustible Vapour Reading (ppm)			Natural Unit Wt. kN/m <sup>3</sup>
				Shear Strength kPa				Natural Moisture Content % Atterberg Limits (% Dry Weight)			
				20	40	60	80	250	500	750	
	<b>GRANULAR FILL</b> ~200 mm Crushed gravel with silt and sand, grey, damp	74.13	0								
	<b>FILL</b> Silty sand with gravel, brick debris, grey and brown, wet, (loose)	73.9	0								
	<b>SANDY SILT</b> With clay and gravel, brown and grey, wet, (loose)	72.6	1	6				0	X		SS1
	<b>GLACIAL TILL</b> Silty clayey sand with gravel, cobbles and boulders, grey, wet, (very loose to loose)	71.9	2	4				30	X		SS2
			3	3				35	X		SS3
			3	3				25	X		SS4
			4	4				35	X		SS5
	<b>GLACIAL TILL</b> Silty sand with gravel, cobbles and boulders, grey, wet, (loose)	69.6	5	4				40	X		SS6
	Cobbles and boulders from 5.8 m to 6.5 m depths		6	9 then 50/25 mm				25	X		SS7
	<b>LIMESTONE BEDROCK</b> Ottawa formation limestone with shaly partings, grey, (poor to good quality)	67.6	7								Run 1
	Weathered and highly fractured zone from 6.5 m to 7.3 m depths		8								Run 2
	<b>Borehole Terminated at 8.3 m Depth</b>	65.8									

NOTES:  
 1. Borehole data requires interpretation by EXP before use by others  
 2. A 32 mm diameter monitoring well installed in borehole as shown.  
 3. Field work supervised by an EXP representative.  
 4. See Notes on Sample Descriptions  
 5. Log to be read with EXP Report OTT-00252625-A0

WATER LEVEL RECORDS		
Date	Water Level (m)	Hole Open To (m)
Completion	N/A	
Damaged	N/A	
Damaged	N/A	
Damaged	N/A	

CORE DRILLING RECORD			
Run No.	Depth (m)	% Rec.	RQD %
1	6.5 - 7.2	90	29
2	7.2 - 8.3	100	84

LOG OF BOREHOLE BH LOGS - 252625 FOREST.GPJ TROW OTTAWA.GDT 11/4/21

# Log of Borehole BH 19-02



Project No: OTT-00252625-A0  
 Project: Residential Development  
 Location: 365 Forest Street, Ottawa, Ontario  
 Date Drilled: April 29, 2019  
 Drill Type: CME-75 Truck Mounted Drill Rig  
 Datum: Geodetic Elevation  
 Logged by: M.L. Checked by: I.T.

Figure No. 4  
 Page. 1 of 1

- Split Spoon Sample
- Auger Sample
- SPT (N) Value
- Dynamic Cone Test
- Shelby Tube
- Shear Strength by Vane Test
- Combustible Vapour Reading
- Natural Moisture Content
- Atterberg Limits
- Undrained Triaxial at % Strain at Failure
- Shear Strength by Penetrometer Test

GWL	SOIL DESCRIPTION	Geodetic Elevation m	Depth	Standard Penetration Test N Value				Combustible Vapour Reading (ppm)			Natural Unit Wt. kN/m <sup>3</sup>
				Shear Strength kPa				250	500	750	
				20	40	60	80	Natural Moisture Content % Atterberg Limits (% Dry Weight)			
	<b>GRANULAR FILL</b> ~500 mm Crushed gravel with silt and sand, grey, damp	74.37	0								
	<b>FILL</b> Silty sand with gravel, brown and grey, wet, (loose)	73.9	0								
	<b>SANDY SILT</b> With clay and gravel, grey, wet, (loose)	73.0	1	6				5	X		SS1 20.6
	<b>GLACIAL TILL</b> Silty clayey sand with gravel, cobbles, and boulders, grey wet, (very loose to loose)	72.272.17	2	8				10	X		SS2 19.4
	<b>GLACIAL TILL</b> Silty clayey sand with gravel, cobbles, and boulders, grey wet, (very loose to loose)	72.272.17	2	5				20	X		SS3
	<b>GLACIAL TILL</b> Silty sand with gravel, cobbles and boulders, grey, wet, (very loose to loose)	70.7	3	1				25	X		SS4
	<b>GLACIAL TILL</b> Silty sand with gravel, cobbles and boulders, grey, wet, (very loose to loose)	70.7	4	4				20	X		SS5
			5	3							SS6
	<b>Auger Refusal at 6.2 m Depth</b>	68.2	6					50 for 75 mm			SS7

LOG OF BOREHOLE BH LOGS - 252625 FOREST.GPJ TROW OTTAWA.GDT 11/4/21

- NOTES:**
- Borehole data requires interpretation by EXP before use by others
  - A 32 mm diameter monitoring well installed in borehole as shown.
  - Field work supervised by an EXP representative.
  - See Notes on Sample Descriptions
  - Log to be read with EXP Report OTT-00252625-A0

WATER LEVEL RECORDS		
Date	Water Level (m)	Hole Open To (m)
Completion	5.2	
May 10, 2019	1.8	
May 15, 2019	1.9	
May 10, 2021	2.2	

CORE DRILLING RECORD			
Run No.	Depth (m)	% Rec.	RQD %



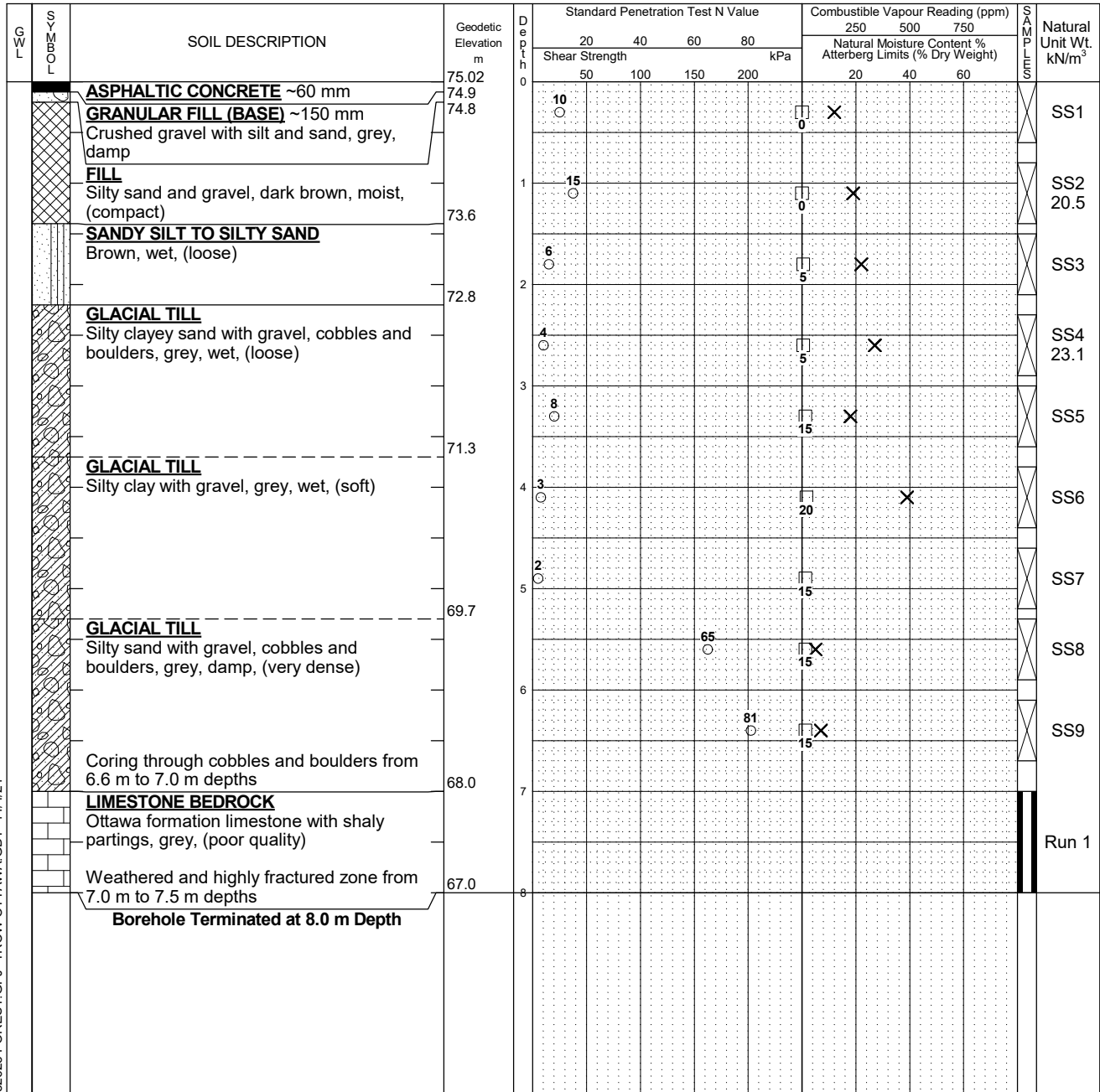
# Log of Borehole BH 19-03



Project No: OTT-00252625-A0  
 Project: Residential Development  
 Location: 365 Forest Street, Ottawa, Ontario  
 Date Drilled: April 30, 2019  
 Drill Type: CME-75 Truck Mounted Drill Rig  
 Datum: Geodetic Elevation  
 Logged by: M.L. Checked by: I.T.

Figure No. 5  
 Page. 1 of 1

Split Spoon Sample  Combustible Vapour Reading   
 Auger Sample  Natural Moisture Content   
 SPT (N) Value  Atterberg Limits   
 Dynamic Cone Test  Undrained Triaxial at % Strain at Failure   
 Shelby Tube  Shear Strength by Penetrometer Test   
 Shear Strength by Vane Test



LOG OF BOREHOLE BH LOGS - 252625 FOREST.GPJ TROW OTTAWA.GDT 11/4/21

**NOTES:**

- Borehole data requires interpretation by EXP before use by others
- Borehole backfilled upon completion of drilling.
- Field work supervised by an EXP representative.
- See Notes on Sample Descriptions
- Log to be read with EXP Report OTT-00252625-A0

WATER LEVEL RECORDS		
Date	Water Level (m)	Hole Open To (m)
Completion	N/A	8.0

CORE DRILLING RECORD			
Run No.	Depth (m)	% Rec.	RQD %
1	7 - 8	100	40

# Log of Borehole BH 19-04



Project No: OTT-00252625-A0  
 Project: Residential Development  
 Location: 365 Forest Street, Ottawa, Ontario  
 Date Drilled: April 29, 2019  
 Drill Type: CME-75 Truck Mounted Drill Rig  
 Datum: Geodetic Elevation  
 Logged by: M.L. Checked by: I.T.

Figure No. 6  
 Page. 1 of 1

Split Spoon Sample   
 Auger Sample   
 SPT (N) Value   
 Dynamic Cone Test   
 Shelby Tube   
 Shear Strength by Vane Test   
 Combustible Vapour Reading   
 Natural Moisture Content   
 Atterberg Limits   
 Undrained Triaxial at % Strain at Failure   
 Shear Strength by Penetrometer Test

G W L	SOIL DESCRIPTION	Geodetic Elevation m	Depth	Standard Penetration Test N Value				Combustible Vapour Reading (ppm)			Natural Unit Wt. kN/m <sup>3</sup>	
				Shear Strength kPa				Natural Moisture Content %				
				20	40	60	80	250	500	750		
	<b>ASPHALTIC CONCRETE</b> ~60 mm	74.98	0									
	<b>GRANULAR FILL (BASE)</b> ~250 mm Crushed gravel with silt and sand, grey, damp	74.9 74.7	0		30				X			SS1
	<b>FILL</b> Clayey silty sand to silty sand with gravel, brown, moist to wet, (loose)		1	5						X		SS2 19.1
			2	5						X		SS3
	<b>GLACIAL TILL</b> Silty clay with sand and gravel, cobbles and boulders, grey, wet, (soft)	72.8	3	4						X		SS4
			4	3						X		SS5
	<b>GLACIAL TILL</b> Silty sand with gravel, cobbles and boulders, grey, wet, (compact to very dense)	70.9	5							X		SS6 23.9
			6							X		SS7
	<b>Auger Refusal at 6.6 m Depth</b>	68.4	6									

LOG OF BOREHOLE BH LOGS - 252625 FOREST.GPJ TROW OTTAWA.GDT 11/4/21

- NOTES:
- Borehole data requires interpretation by EXP before use by others
  - Borehole backfilled upon completion of drilling.
  - Field work supervised by an EXP representative.
  - See Notes on Sample Descriptions
  - Log to be read with EXP Report OTT-00252625-A0

WATER LEVEL RECORDS		
Date	Water Level (m)	Hole Open To (m)
Completion	5.5	6.6

CORE DRILLING RECORD			
Run No.	Depth (m)	% Rec.	RQD %

# Log of Borehole BH 19-05



Project No: OTT-00252625-A0  
 Project: Residential Development  
 Location: 365 Forest Street, Ottawa, Ontario  
 Date Drilled: April 30, 2019  
 Drill Type: CME-75 Truck Mounted Drill Rig  
 Datum: Geodetic Elevation  
 Logged by: M.L. Checked by: I.T.

Figure No. 7  
 Page. 1 of 1

Split Spoon Sample   
 Auger Sample   
 SPT (N) Value   
 Dynamic Cone Test   
 Shelby Tube   
 Shear Strength by Vane Test   
 Combustible Vapour Reading   
 Natural Moisture Content   
 Atterberg Limits   
 Undrained Triaxial at % Strain at Failure   
 Shear Strength by Penetrometer Test

G W L	SOIL C O M P O S I T I O N	SOIL DESCRIPTION	Geodetic Elevation m	D e p t h	Standard Penetration Test N Value				Combustible Vapour Reading (ppm)			Natural Unit Wt. kN/m <sup>3</sup>	
					Shear Strength kPa				Natural Moisture Content %				
					20	40	60	80	250	500	750		
		<b>GRANULAR FILL</b> ~100 mm Crushed gravel with silt and sand, grey, damp	74.82 74.7	0						40	X		SS1
		<b>FILL</b> Clayey silty sand to silty sand with gravel, rootlets, brown and grey, moist to wet, petroleum odour, (loose)		1						40	X		SS2 20.5
				2						200	X		SS3
				3						60	X		SS4 22.9
		<b>GLACIAL TILL</b> Silty clay with sand and gravel, grey, wet, (soft)	71.8	3						45	X		SS5
		<b>GLACIAL TILL</b> Silty clayey sand with gravel, cobbles and boulders, grey, wet, petroleum odour, (very loose)	71.1	4						30	X		SS6
				5									
				6						15	X		SS7
		<b>Auger Refusal at 6.7 m Depth</b>	68.1	6									

LOG OF BOREHOLE BH LOGS - 252625 FOREST.GPJ TROW OTTAWA.GDT 11/4/21

- NOTES:
- Borehole data requires interpretation by EXP before use by others
  - Borehole backfilled upon completion of drilling.
  - Field work supervised by an EXP representative.
  - See Notes on Sample Descriptions
  - Log to be read with EXP Report OTT-00252625-A0

WATER LEVEL RECORDS		
Date	Water Level (m)	Hole Open To (m)
Completion	4.6	5.5

CORE DRILLING RECORD			
Run No.	Depth (m)	% Rec.	RQD %

# Log of Borehole BH 19-06



Project No: OTT-00252625-A0  
 Project: Residential Development  
 Location: 365 Forest Street, Ottawa, Ontario  
 Date Drilled: April 25, 2019  
 Drill Type: CME-75 Truck Mounted Drill Rig  
 Datum: Geodetic Elevation  
 Logged by: M.L. Checked by: I.T.

Figure No. 8  
 Page. 1 of 1

- Split Spoon Sample
- Auger Sample
- SPT (N) Value
- Dynamic Cone Test
- Shelby Tube
- Shear Strength by Vane Test
- Combustible Vapour Reading
- Natural Moisture Content
- Atterberg Limits
- Undrained Triaxial at % Strain at Failure
- Shear Strength by Penetrometer Test

Depth m	SOIL DESCRIPTION	Geodetic Elevation m	Standard Penetration Test N Value				Combustible Vapour Reading (ppm)			Natural Unit Wt. kN/m <sup>3</sup>
			Shear Strength kPa				Natural Moisture Content % Atterberg Limits (% Dry Weight)			
			20	40	60	80	250	500	750	
0	<b>ASPHALTIC CONCRETE</b> ~30 mm <b>GRANULAR FILL (BASE)</b> ~200 mm Crushed gravel with silt and sand, grey, damp <b>FILL</b> Silty clayey sand to silty sand with gravel, brick debris, brown, moist to wet, (loose)	75.28 75.2 75.0								SS1
1										SS2
2										SS3
3	<b>GLACIAL TILL</b> Silty sand with gravel, cobbles and boulders, grey, wet, (very loose to loose)	72.7 72.38								SS4
4										SS5
5										SS6
6										SS7
7										SS8
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- NOTES:
- Borehole data requires interpretation by EXP before use by others
  - A 32 mm diameter monitoring well installed in borehole as shown.
  - Field work supervised by an EXP representative.
  - See Notes on Sample Descriptions
  - Log to be read with EXP Report OTT-00252625-A0

WATER LEVEL RECORDS		
Date	Water Level (m)	Hole Open To (m)
Completion	4.6	
May 10, 2019	2.5	
May 15, 2019	2.4	
May 10, 2021	2.9	

CORE DRILLING RECORD			
Run No.	Depth (m)	% Rec.	RQD %

LOG OF BOREHOLE BH LOGS - 252625 FOREST.GPJ TROW OTTAWA.GDT 11/4/21

# Log of Borehole BH 19-07



Project No: OTT-00252625-A0  
 Project: Residential Development  
 Location: 365 Forest Street, Ottawa, Ontario  
 Date Drilled: April 24, 2019  
 Drill Type: CME-75 Truck Mounted Drill Rig  
 Datum: Geodetic Elevation  
 Logged by: M.L. Checked by: I.T.

Figure No. 9  
 Page. 1 of 1

- Split Spoon Sample
- Auger Sample
- SPT (N) Value
- Dynamic Cone Test
- Shelby Tube
- Shear Strength by Vane Test
- Combustible Vapour Reading
- Natural Moisture Content
- Atterberg Limits
- Undrained Triaxial at % Strain at Failure
- Shear Strength by Penetrometer Test

Depth (m)	SOIL DESCRIPTION	Geodetic Elevation (m)	Standard Penetration Test N Value				Combustible Vapour Reading (ppm)			Natural Unit Wt. kN/m <sup>3</sup>
			Shear Strength (kPa)				Natural Moisture Content % Atterberg Limits (% Dry Weight)			
			20	40	60	80	250	500	750	
0	<b>ASPHALTIC CONCRETE</b> ~60 mm <b>GRANULAR FILL (BASE)</b> ~220 mm Crushed gravel with silt and sand, grey, damp <b>FILL</b> Silty sand with gravel, brown, moist to wet, (loose)	75.21 75.1 74.9								
1									SS1 19.4	
2		73.51 73.0							SS2	
3	<b>GLACIAL TILL</b> Silty sand with gravel, cobbles and boulders, grey, wet, (loose to compact) Shale fragments from 3.0 m to 3.6 m depths								SS3	
4									SS4	
5									SS5	
6									SS6	
7									SS7	
69.3	<b>Borehole Terminated at 5.9 m Depth</b>									

LOG OF BOREHOLE BH LOGS - 252625 FOREST.GPJ TROW OTTAWA.GDT 11/4/21

- NOTES:**
- Borehole data requires interpretation by EXP before use by others
  - A 32 mm diameter monitoring well installed in borehole as shown.
  - Field work supervised by an EXP representative.
  - See Notes on Sample Descriptions
  - Log to be read with EXP Report OTT-00252625-A0

WATER LEVEL RECORDS		
Date	Water Level (m)	Hole Open To (m)
Completion	5.2	6.1
May 10, 2019	1.4	
May 15, 2019	1.4	
May 10, 2021	1.7	

CORE DRILLING RECORD			
Run No.	Depth (m)	% Rec.	RQD %

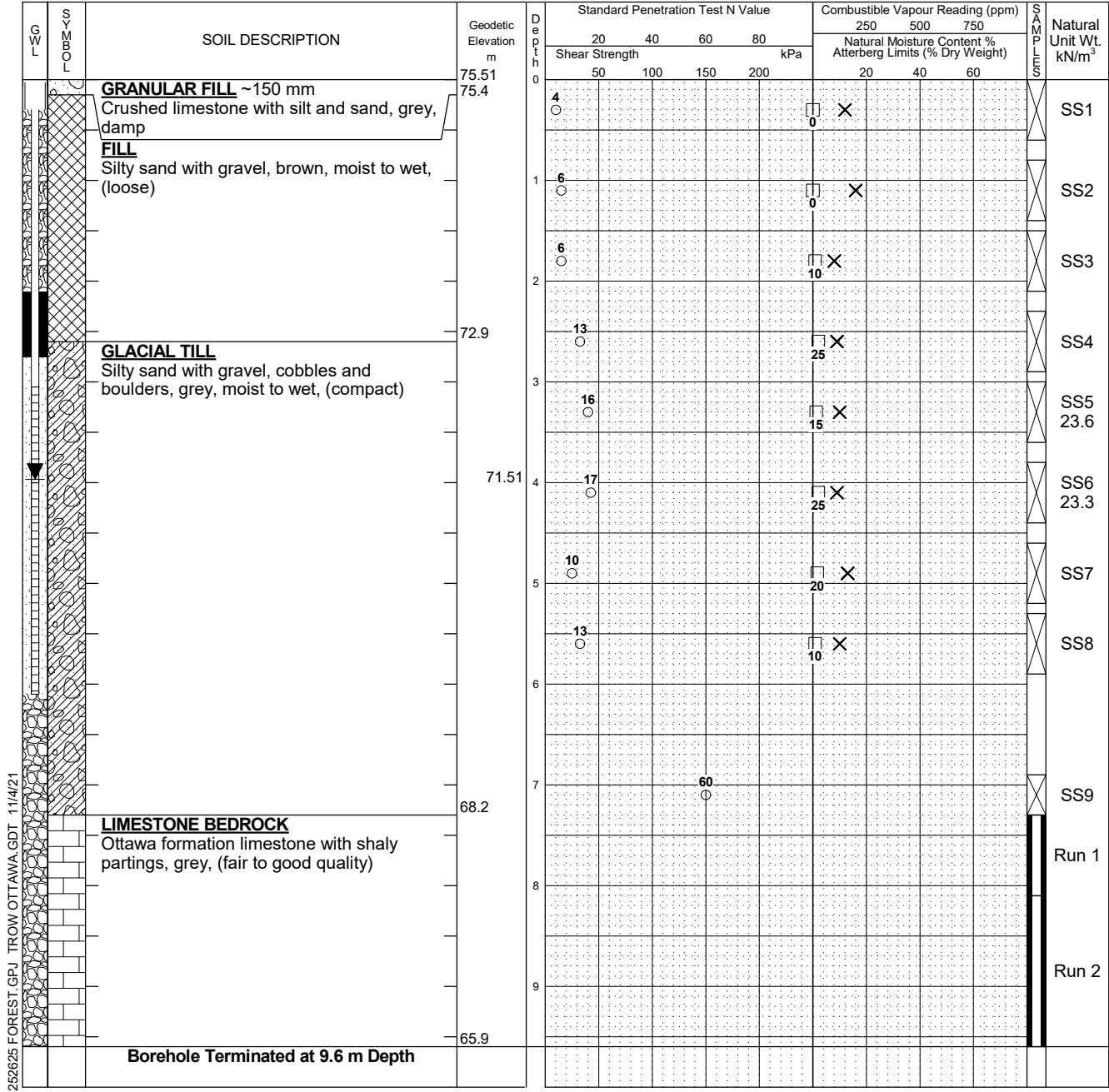
# Log of Borehole BH 19-08



Project No: OTT-00252625-A0  
 Project: Residential Development  
 Location: 365 Forest Street, Ottawa, Ontario  
 Date Drilled: April 25, 2019  
 Drill Type: CME-75 Truck Mounted Drill Rig  
 Datum: Geodetic Elevation  
 Logged by: M.L. Checked by: I.T.

Figure No. 10  
 Page. 1 of 1

- Split Spoon Sample
- Auger Sample
- SPT (N) Value
- Dynamic Cone Test
- Shelby Tube
- Shear Strength by Vane Test
- Combustible Vapour Reading
- Natural Moisture Content
- Atterberg Limits
- Undrained Triaxial at % Strain at Failure
- Shear Strength by Penetrometer Test



**NOTES:**

- Borehole data requires interpretation by EXP before use by others
- A 32 mm diameter monitoring well installed in borehole as shown.
- Field work supervised by an EXP representative.
- See Notes on Sample Descriptions
- Log to be read with EXP Report OTT-00252625-A0

WATER LEVEL RECORDS		
Date	Water Level (m)	Hole Open To (m)
Completion	N/A	N/A
May 10, 2019	5.6	
May 15, 2019	5.7	
May 10, 2021	4.0	

CORE DRILLING RECORD			
Run No.	Depth (m)	% Rec.	RQD %
1	7.3 - 8.1	94	53
2	8.1 - 9.6	100	78

LOG OF BOREHOLE BH LOGS - 252625 FOREST.GPJ TROW OTTAWA.GDT 11/4/21



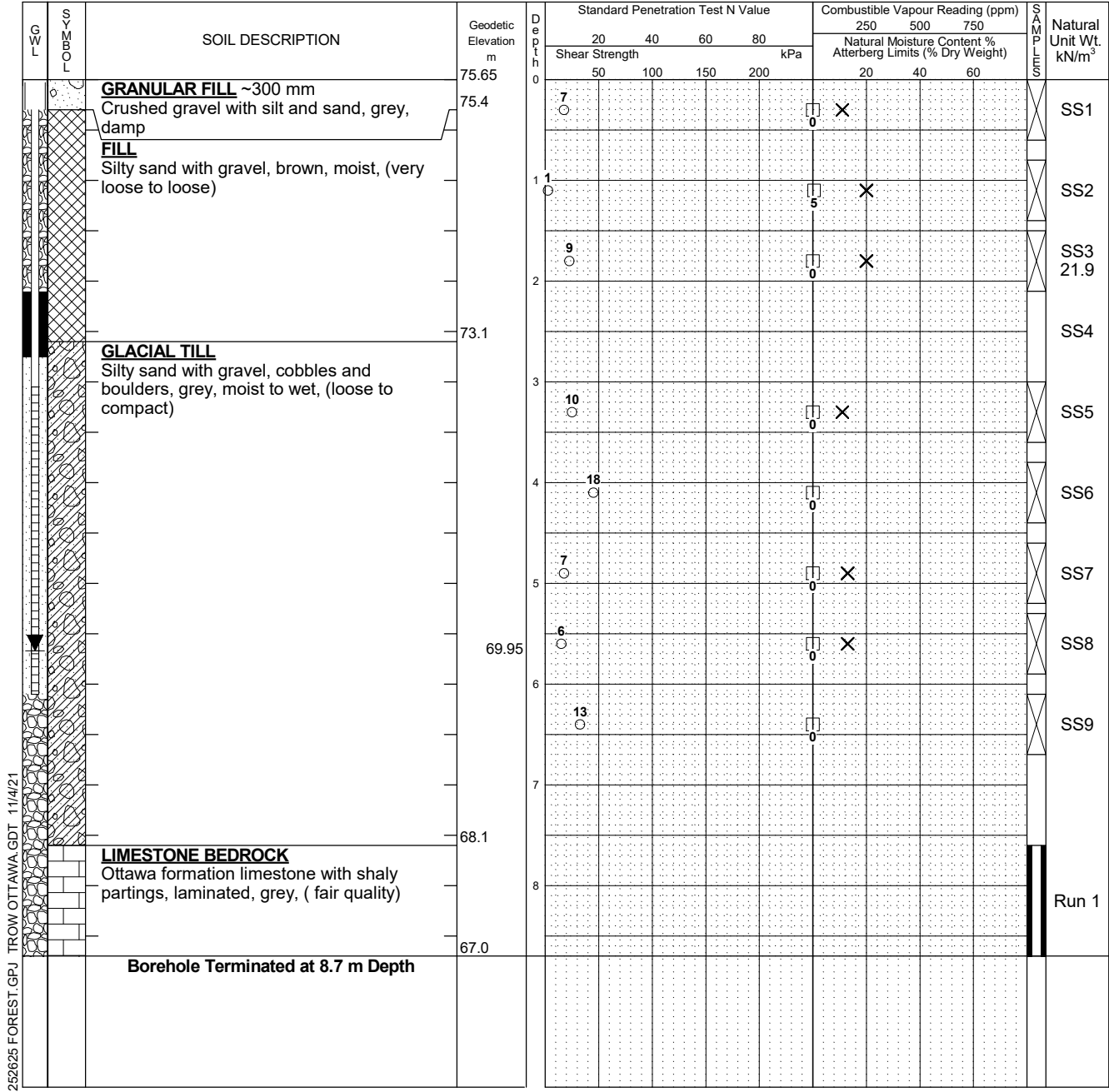
# Log of Borehole BH 19-09



Project No: OTT-00252625-A0  
 Project: Residential Development  
 Location: 365 Forest Street, Ottawa, Ontario  
 Date Drilled: April 24, 2019  
 Drill Type: CME-75 Truck Mounted Drill Rig  
 Datum: Geodetic Elevation  
 Logged by: M.L. Checked by: I.T.

Figure No. 11  
 Page. 1 of 1

- Split Spoon Sample
- Auger Sample
- SPT (N) Value
- Dynamic Cone Test
- Shelby Tube
- Shear Strength by Vane Test
- Combustible Vapour Reading
- Natural Moisture Content
- Atterberg Limits
- Undrained Triaxial at % Strain at Failure
- Shear Strength by Penetrometer Test



- LOG OF BOREHOLE BH LOGS - 252625 FOREST.GPJ TROW OTTAWA.GDT 11/4/21
- NOTES:
- Borehole data requires interpretation by EXP before use by others
  - A 32 mm diameter monitoring well installed in borehole as shown.
  - Field work supervised by an EXP representative.
  - See Notes on Sample Descriptions
  - Log to be read with EXP Report OTT-00252625-A0

WATER LEVEL RECORDS		
Date	Water Level (m)	Hole Open To (m)
Completion	N/A	N/A
May 15, 2019	6.0	
May 10, 2021	5.7	

CORE DRILLING RECORD			
Run No.	Depth (m)	% Rec.	RQD %
1	7.6 - 8.7	95	61

# Log of Borehole BH 19-10



Project No: OTT-00252625-A0  
 Project: Residential Development  
 Location: 365 Forest Street, Ottawa, Ontario  
 Date Drilled: April 25, 2019  
 Drill Type: CME-75 Truck Mounted Drill Rig  
 Datum: Geodetic Elevation  
 Logged by: M.L. Checked by: I.T.

Figure No. 12  
 Page. 1 of 1

- Split Spoon Sample
- Auger Sample
- SPT (N) Value
- Dynamic Cone Test
- Shelby Tube
- Shear Strength by Vane Test
- Combustible Vapour Reading
- Natural Moisture Content
- Atterberg Limits
- Undrained Triaxial at % Strain at Failure
- Shear Strength by Penetrometer Test

G W L	SOIL DESCRIPTION	Geodetic Elevation m	Depth m	Standard Penetration Test N Value				Combustible Vapour Reading (ppm)			Natural Unit Wt. kN/m <sup>3</sup>
				Shear Strength				250	500	750	
				20	40	60	80	Natural Moisture Content % Atterberg Limits (% Dry Weight)			
				50	100	150	200	20	40	60	
	<b>GRANULAR FILL</b> ~150 mm Crushed gravel with silt and sand, grey	75.74 75.6	0								SS1
	<b>FILL</b> Silty sand, brown and grey, moist, (loose to compact)		1								SS2
			2								SS3 20.9
	<b>GLACIAL TILL</b> Silty sand with gravel, grey, moist to wet, (loose to dense)	73.6 73.44	3								SS4 23.6
			4								SS5
			5								SS6
			6								SS7
			7								SS8
	<b>Borehole Terminated at 5.9 m Depth</b>	69.8	8								

LOG OF BOREHOLE BH LOGS - 252625 FOREST.GPJ TROW OTTAWA.GDT 11/4/21

- NOTES:**
- Borehole data requires interpretation by EXP before use by others
  - A 32 mm diameter monitoring well installed in borehole as shown.
  - Field work supervised by an EXP representative.
  - See Notes on Sample Descriptions
  - Log to be read with EXP Report OTT-00252625-A0

WATER LEVEL RECORDS		
Date	Water Level (m)	Hole Open To (m)
Completion	5.2	N/A
May 10, 2019	2.2	
May 15, 2019	2.3	
May 10, 2021	Not Found	

CORE DRILLING RECORD			
Run No.	Depth (m)	% Rec.	RQD %



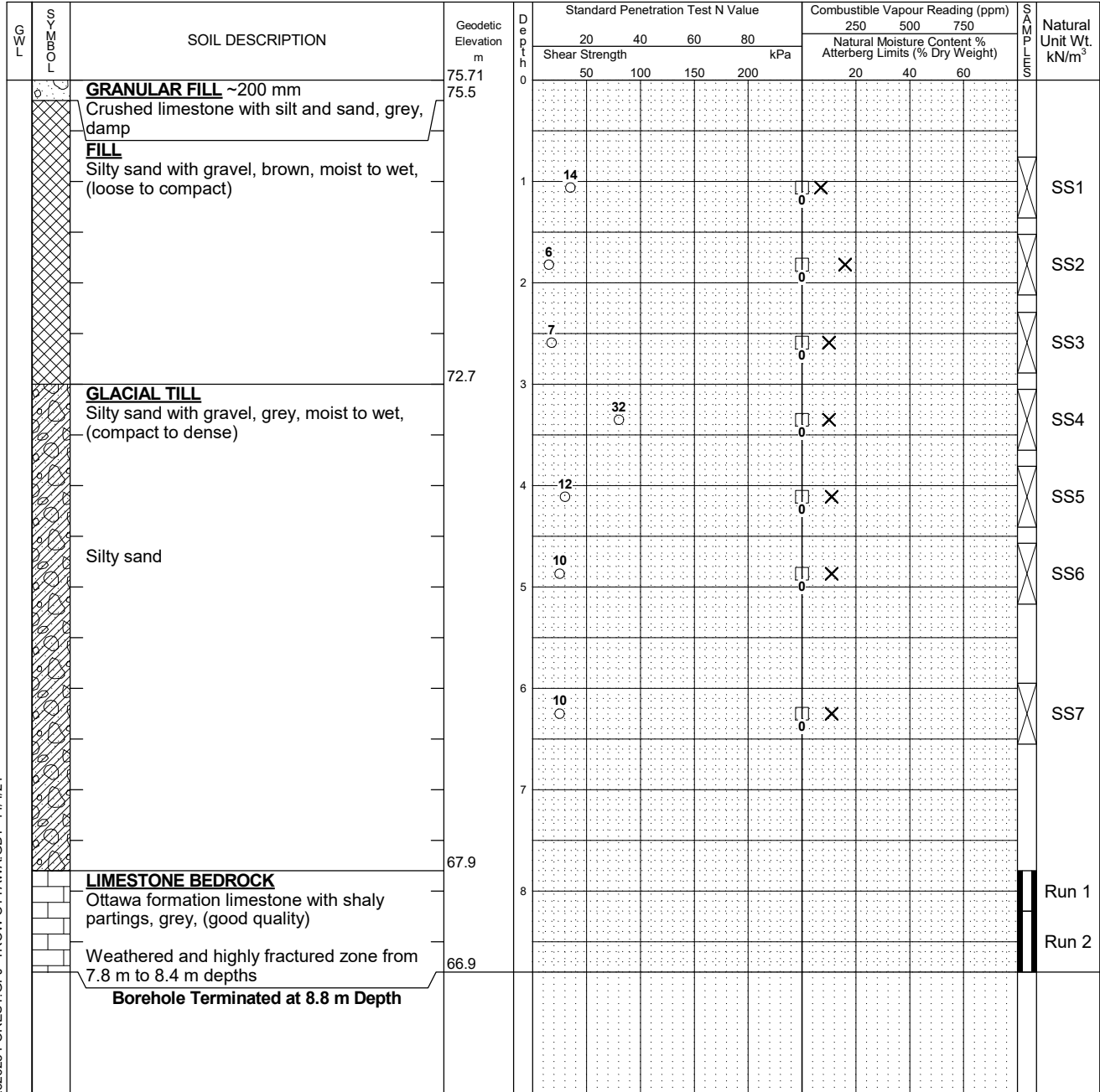
# Log of Borehole BH 19-11



Project No: OTT-00252625-A0  
 Project: Residential Development  
 Location: 365 Forest Street, Ottawa, Ontario  
 Date Drilled: April 29, 2019  
 Drill Type: CME-75 Truck Mounted Drill Rig  
 Datum: Geodetic Elevation  
 Logged by: M.L. Checked by: I.T.

Figure No. 13  
 Page. 1 of 1

Split Spoon Sample   
 Auger Sample   
 SPT (N) Value   
 Dynamic Cone Test   
 Shelby Tube   
 Shear Strength by Vane Test   
 Combustible Vapour Reading   
 Natural Moisture Content   
 Atterberg Limits   
 Undrained Triaxial at % Strain at Failure   
 Shear Strength by Penetrometer Test



LOG OF BOREHOLE BH LOGS - 252625 FOREST.GPJ TROW OTTAWA.GDT 11/4/21

- NOTES:
- Borehole data requires interpretation by EXP before use by others
  - Borehole backfilled upon completion of drilling.
  - Field work supervised by an EXP representative.
  - See Notes on Sample Descriptions
  - Log to be read with EXP Report OTT-00252625-A0

WATER LEVEL RECORDS		
Date	Water Level (m)	Hole Open To (m)
Completion	N/A	8.8

CORE DRILLING RECORD			
Run No.	Depth (m)	% Rec.	RQD %
1	7.8 - 8.2	94	77
2	8.2 - 8.8	100	86

# Log of Borehole BH 19-12



Project No: OTT-00252625-A0  
 Project: Residential Development  
 Location: 365 Forest Street, Ottawa, Ontario  
 Date Drilled: April 24, 2019  
 Drill Type: CME-75 Truck Mounted Drill Rig  
 Datum: Geodetic Elevation  
 Logged by: M.L. Checked by: I.T.

Figure No. 14  
 Page. 1 of 1

Split Spoon Sample   
 Auger Sample   
 SPT (N) Value   
 Dynamic Cone Test   
 Shelby Tube   
 Shear Strength by Vane Test   
 Combustible Vapour Reading   
 Natural Moisture Content   
 Atterberg Limits   
 Undrained Triaxial at % Strain at Failure   
 Shear Strength by Penetrometer Test

G W L	S O B Y L	SOIL DESCRIPTION	Geodetic Elevation m	D e p t h m	Standard Penetration Test N Value				Combustible Vapour Reading (ppm)			S O B Y L	Natural Unit Wt. kN/m <sup>3</sup>	
					Shear Strength kPa				Natural Moisture Content %					
					20	40	60	80	250	500	750			
		<b>GRANULAR FILL</b> ~150 mm Crushed gravel with silt and sand, damp, grey	75.42 75.3	0										
		<b>FILL</b> Silty sand with gravel, brown, moist to wet, (loose to compact)		1	4									SS1
				2	12									SS2
				3	16									SS3
				4	7									SS4 22.4
				5	7									SS5
				6	5									SS6
		<b>Borehole Terminated at 4.4 m Depth</b>	71.0											

LOG OF BOREHOLE BH LOGS - 252625 FOREST.GPJ TROW OTTAWA.GDT 11/4/21

- NOTES:
- Borehole data requires interpretation by EXP before use by others
  - Borehole backfilled upon completion of drilling.
  - Field work supervised by an EXP representative.
  - See Notes on Sample Descriptions
  - Log to be read with EXP Report OTT-00252625-A0

WATER LEVEL RECORDS		
Date	Water Level (m)	Hole Open To (m)
Completion	Dry	3.8

CORE DRILLING RECORD			
Run No.	Depth (m)	% Rec.	RQD %

# Log of Borehole BH 21-13



Project No: OTT-00252625-A0  
 Project: Residential Development  
 Location: 365 Forest Street, Ottawa, Ontario  
 Date Drilled: October 6, 2021  
 Drill Type: CME-850 Track Mounted Drill Rig  
 Datum: Geodetic Elevation  
 Logged by: M.Z. Checked by: I.T.

Figure No. 15  
 Page. 1 of 2

Split Spoon Sample   
 Auger Sample   
 SPT (N) Value   
 Dynamic Cone Test   
 Shelby Tube   
 Shear Strength by Vane Test   
 Combustible Vapour Reading   
 Natural Moisture Content   
 Atterberg Limits   
 Undrained Triaxial at % Strain at Failure   
 Shear Strength by Penetrometer Test

G W L	S Y M B O L	SOIL DESCRIPTION	Geodetic Elevation m	D e p t h	Standard Penetration Test N Value				Combustible Vapour Reading (ppm)			Natural Unit Wt. kN/m <sup>3</sup>
					Shear Strength kPa				250	500	750	
					20	40	60	80	Natural Moisture Content % Atterberg Limits (% Dry Weight)			
		Borehole advanced by power augering technique from ground surface to 4.6 m depth.	75.2	0								
				1								
				2								
				3								
				4								
		<b>GLACIAL TILL</b> Silty sand with gravel, shale fragments, cobbles and boulders, grey, wet, (compact)	70.6	5								SS1
				6								SS2
		<b>LIMESTONE BEDROCK</b> Ottawa formation limestone with shaly partings, grey, (very poor to excellent quality)	68.9 68.9	7								Run 1
				8								Run 2
				9								Run 3
				10								

LOG OF BOREHOLE - 252625 FOREST.GPJ TROW OTTAWA.GDT 11/4/21

Continued Next Page

- NOTES:
- Borehole data requires interpretation by EXP before use by others
  - A 38 mm diameter monitoring well installed in borehole as shown.
  - Field work supervised by an EXP representative.
  - See Notes on Sample Descriptions
  - Log to be read with EXP Report OTT-00252625-A0

WATER LEVEL RECORDS		
Date	Water Level (m)	Hole Open To (m)
Oct. 20, 2021	6.3	

CORE DRILLING RECORD			
Run No.	Depth (m)	% Rec.	RQD %
1	6.3 - 6.7	92	27
2	6.7 - 8.2	80	18
3	8.2 - 9.8	100	79
4	9.8 - 11.3	100	83
5	11.3 - 12.9	100	100
6	12.9 - 14.4	98	92

# Log of Borehole BH 21-13



Project No: OTT-00252625-A0

Figure No. 15

Project: Residential Development

Page. 2 of 2

SOIL LOG	SOIL DESCRIPTION	Geodetic Elevation m	Standard Penetration Test N Value				Combustible Vapour Reading (ppm)			Natural Unit Wt. kN/m <sup>3</sup>
			20	40	60	80	250	500	750	
			Shear Strength kPa				Natural Moisture Content % Atterberg Limits (% Dry Weight)			
	<b>LIMESTONE BEDROCK</b> Ottawa formation limestone with shaly partings, grey, (very poor to excellent quality) <i>(continued)</i>	65.2	50	100	150	200	20	40	60	Run 4
										Run 5
										Run 6
		60.8								
<p><b>Borehole Terminated at 14.4 m Depth</b></p> <p>NOTE: 1) The geodetic elevation of the borehole is considered approximate.</p>										

LOG OF BOREHOLE BH LOGS - 252625 FOREST.GPJ TROW OTTAWA.GDT 11/4/21

- NOTES:
- Borehole data requires interpretation by EXP before use by others
  - A 38 mm diameter monitoring well installed in borehole as shown.
  - Field work supervised by an EXP representative.
  - See Notes on Sample Descriptions
  - Log to be read with EXP Report OTT-00252625-A0

WATER LEVEL RECORDS		
Date	Water Level (m)	Hole Open To (m)
Oct. 20, 2021	6.3	

CORE DRILLING RECORD			
Run No.	Depth (m)	% Rec.	RQD %
1	6.3 - 6.7	92	27
2	6.7 - 8.2	80	18
3	8.2 - 9.8	100	79
4	9.8 - 11.3	100	83
5	11.3 - 12.9	100	100
6	12.9 - 14.4	98	92

# Log of Borehole BH 21-14



Project No: OTT-00252625-A0  
 Project: Residential Development  
 Location: 365 Forest Street, Ottawa, Ontario  
 Date Drilled: October 5, 2021  
 Drill Type: CME-850 Track Mounted Drill Rig  
 Datum: Geodetic Elevation  
 Logged by: M.Z. Checked by: I.T.

Figure No. 16  
 Page. 1 of 2

- Split Spoon Sample
- Auger Sample
- SPT (N) Value
- Dynamic Cone Test
- Shelby Tube
- Shear Strength by Vane Test
- Combustible Vapour Reading
- Natural Moisture Content
- Atterberg Limits
- Undrained Triaxial at % Strain at Failure
- Shear Strength by Penetrometer Test

G W L	S Y M B O L	SOIL DESCRIPTION	Geodetic Elevation m	D e p t h	Standard Penetration Test N Value				Combustible Vapour Reading (ppm)			S O I L T E M P E R A T U R E	Natural Unit Wt. kN/m <sup>3</sup>			
									250	500	750					
									Natural Moisture Content % Atterberg Limits (% Dry Weight)							
				Shear Strength kPa												
				50 100 150 200				20 40 60								
		Borehole advanced by power augering technique from ground surface to a 4.6 m depth.	74.3	0												
				1												
				2												
				3												
				4												
			69.7	5												
		<b>GLACIAL TILL</b> Silty sand with gravel, rock fragments, cobbles and boulders, grey, wet		5									SS1			
			68.2	6												
		<b>HIGHLY WEATHERED LIMESTONE BEDROCK</b> Greenish grey, shaly partings, interbedded with layers of clay	67.7	6									SS2			
			67.3	7									Run 1			
		<b>LIMESTONE BEDROCK</b> Ottawa formation limestone with shaly partings, grey, (very poor to excellent quality)		7									Run 2			
				8												
				9												
				10									Run 3			

LOG OF BOREHOLE BH LOGS - 252625 FOREST.GPJ TROW OTTAWA.GDT 11/4/21

Continued Next Page

- NOTES:
- Borehole data requires interpretation by EXP before use by others
  - A 38 mm diameter monitoring well installed in borehole as shown.
  - Field work supervised by an EXP representative.
  - See Notes on Sample Descriptions
  - Log to be read with EXP Report OTT-00252625-A0

WATER LEVEL RECORDS		
Date	Water Level (m)	Hole Open To (m)
Oct. 20, 2021	6.6	

CORE DRILLING RECORD			
Run No.	Depth (m)	% Rec.	RQD %
1	6.3 - 6.7	100	0
2	6.7 - 8.2	92	46
3	8.2 - 9.8	98	53
4	9.8 - 11.3	100	75
5	11.3 - 12.8	95	95

# Log of Borehole BH 21-14



Project No: OTT-00252625-A0

Figure No. 16

Project: Residential Development

Page. 2 of 2

L W G	S O B Y L	SOIL DESCRIPTION	Geodetic Elevation m	D e p t h	Standard Penetration Test N Value				Combustible Vapour Reading (ppm)			Natural Unit Wt. kN/m <sup>3</sup>
					20	40	60	80	250	500	750	
					Shear Strength kPa				Natural Moisture Content % Atterberg Limits (% Dry Weight)			
					50	100	150	200	20	40	60	
		<b>LIMESTONE BEDROCK</b> Ottawa formation limestone with shaly partings, grey, (very poor to excellent quality) (continued)	64.3	10								
				11								Run 4
				12								Run 5
		<b>Borehole Terminated at 12.8 m Depth</b>	61.5									
		NOTE:  1) The geodetic elevation of the borehole is considered approximate.										

LOG OF BOREHOLE BH LOGS - 252625 FOREST.GPJ TROW OTTAWA.GDT 11/4/21

- NOTES:
- Borehole data requires interpretation by EXP before use by others
  - A 38 mm diameter monitoring well installed in borehole as shown.
  - Field work supervised by an EXP representative.
  - See Notes on Sample Descriptions
  - Log to be read with EXP Report OTT-00252625-A0

WATER LEVEL RECORDS		
Date	Water Level (m)	Hole Open To (m)
Oct. 20, 2021	6.6	

CORE DRILLING RECORD			
Run No.	Depth (m)	% Rec.	RQD %
1	6.3 - 6.7	100	0
2	6.7 - 8.2	92	46
3	8.2 - 9.8	98	53
4	9.8 - 11.3	100	75
5	11.3 - 12.8	95	95

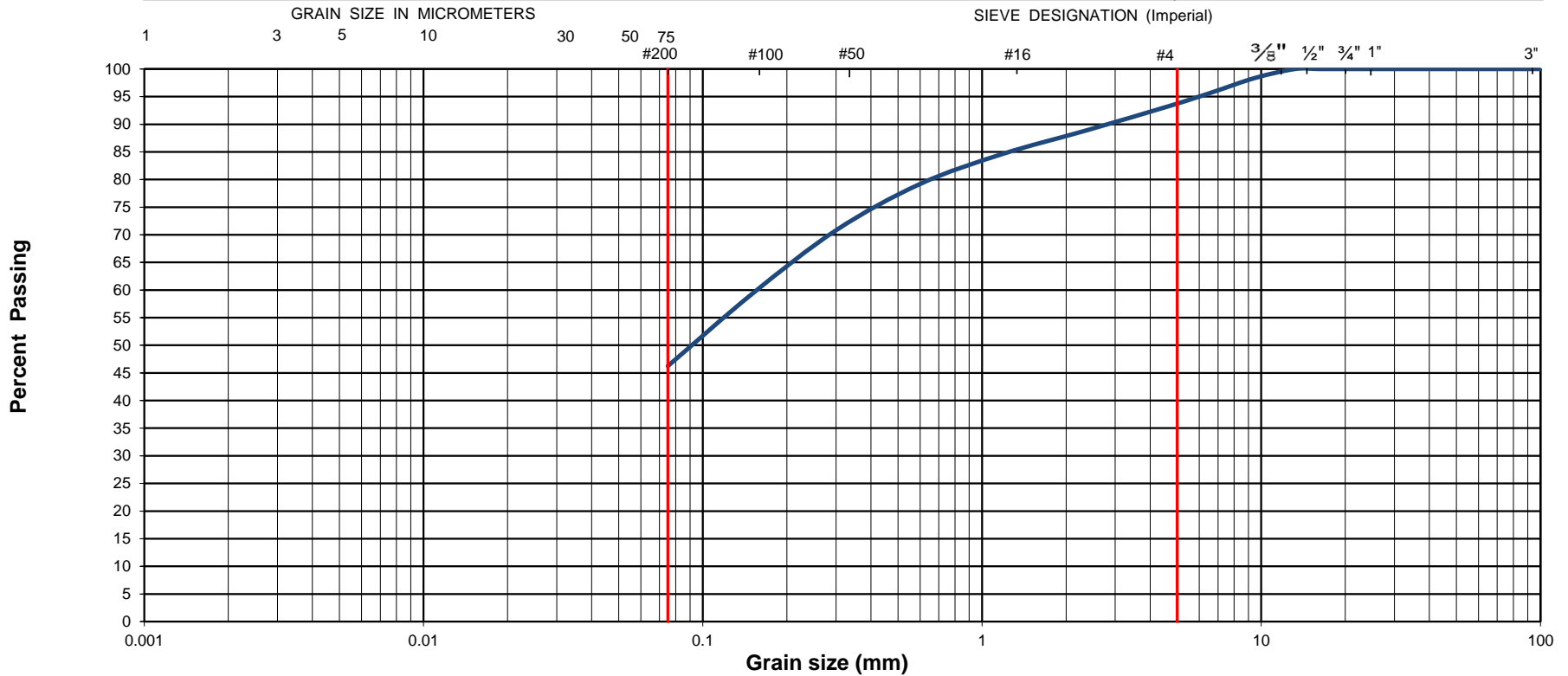


## Grain-Size Distribution Curve Method of Test For Sieve Analysis of Aggregate ASTM C-136

**EXP Services Inc.**  
100-2650 Queensview Drive  
Ottawa, ON K2B 8H6

### Unified Soil Classification System

CLAY AND SILT			SAND			GRAVEL	
			Fine	Medium	Coarse	Fine	Coarse



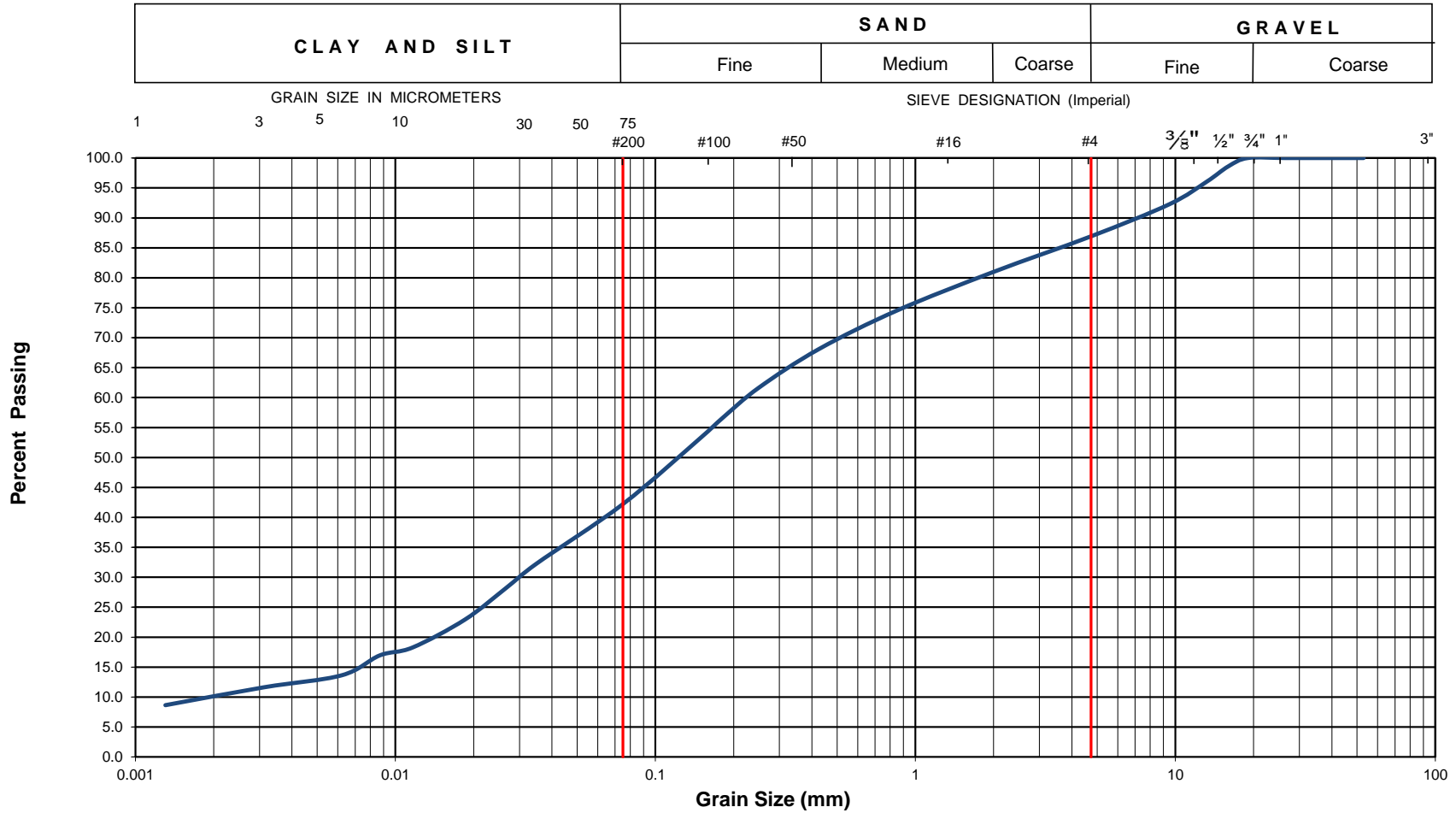
<b>EXP Project No.:</b> OTT-00252625-A0		<b>Project Name :</b> Residential Development	
<b>Client :</b> 11061917 Canada Inc.		<b>Project Location :</b> 365 Forest Ave, Ottawa, ON.	
<b>Date Sampled :</b> April 25, 2019		<b>Borehole No:</b> 19-10	<b>Sample:</b> SS3
<b>Sample Composition :</b>		<b>Gravel (%)</b> 7	<b>Sand (%)</b> 47
<b>Sample Description :</b>		<b>Silt &amp; Clay (%)</b> 46	<b>Figure :</b> 17
<b>FILL: Silty Sand (SM)</b>			



## Grain-Size Distribution Curve Method of Test For Particle Size Analysis of Soil ASTM C-136/ASTM D422

**EXP Services Inc.**  
100-2650 Queensview Drive  
Ottawa, ON K2B 8H6

### Unified Soil Classification System



EXP Project No.:	OTT-00252625-A0	Project Name :	Residential Development		
Client :	11061917 Canada Inc.	Project Location :	365 Forest Ave, Ottawa, ON.		
Date Sampled :	April 29, 2019	Borehole No:	BH 19-02	Sample No.: SS5	
Sample Description :	% Silt and Clay	42	% Sand	45	
Sample Description :			% Gravel	13	
Sample Description :	GLACIAL TILL: Silty Sand (SM)			Figure :	18
Sample Description :					



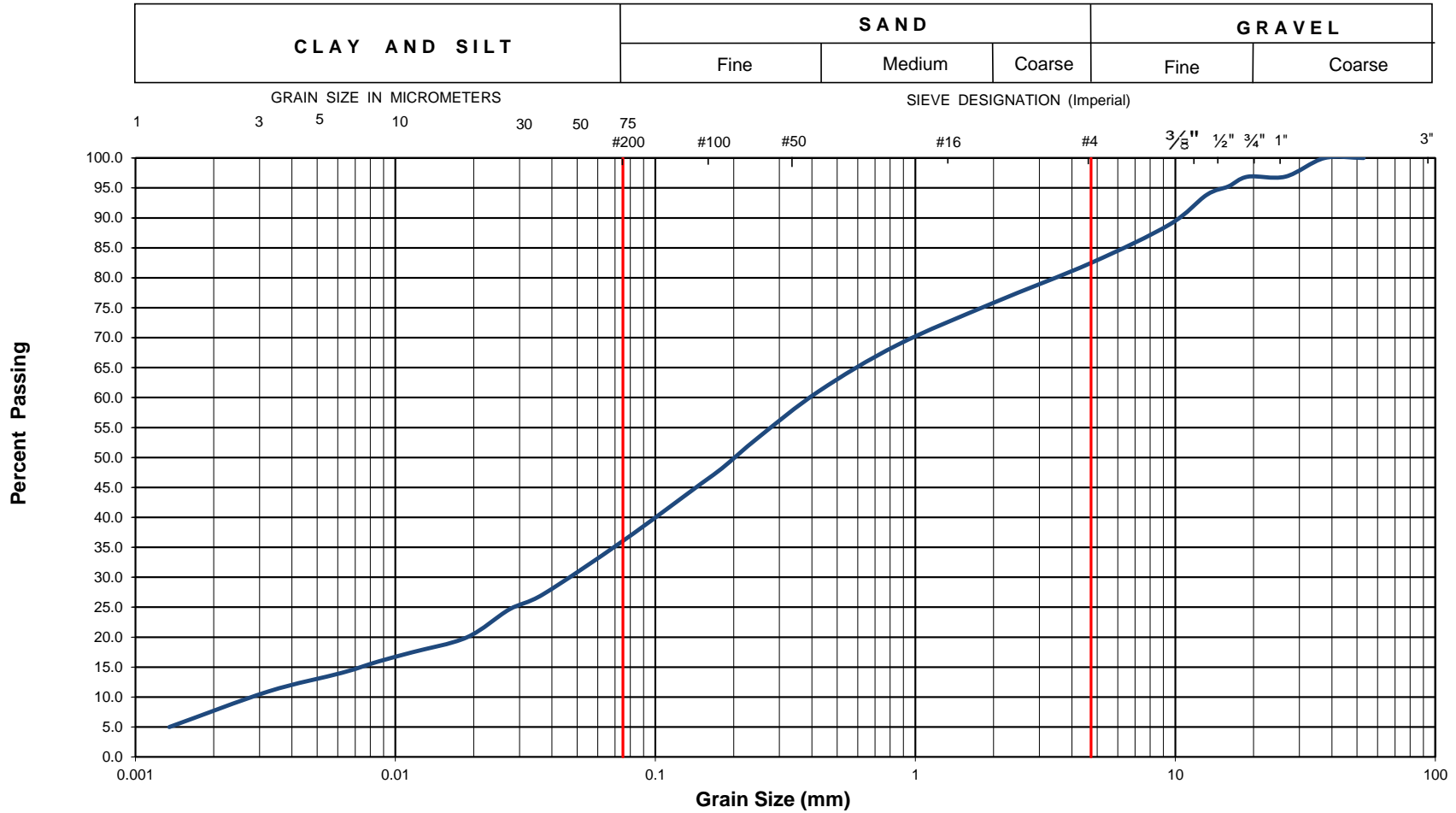




## Grain-Size Distribution Curve Method of Test For Particle Size Analysis of Soil ASTM C-136/ASTM D422

**EXP Services Inc.**  
100-2650 Queensview Drive  
Ottawa, ON K2B 8H6

### Unified Soil Classification System



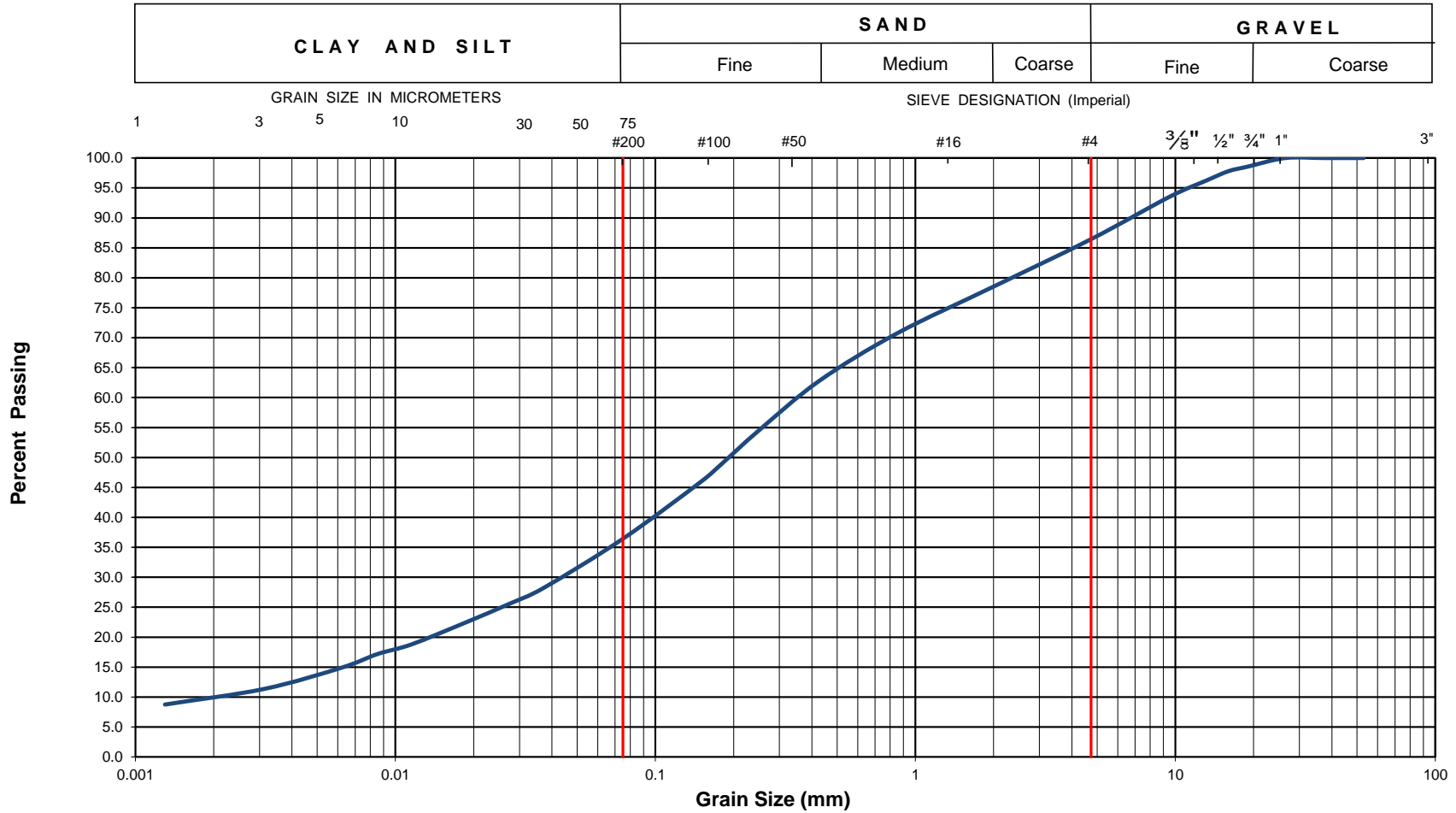
EXP Project No.:	OTT-00252625-A0	Project Name :	Residential Development		
Client :	11061917 Canada Inc.	Project Location :	365 Forest Ave, Ottawa, ON.		
Date Sampled :	April 25, 2019	Borehole No:	BH 19-08	Sample No.: SS5	
Sample Description :	% Silt and Clay	36	% Sand	47	
Sample Description :	GLACIAL TILL: Silty Sand with Gravel (SM)			% Gravel	17
Sample Description :				Figure :	20



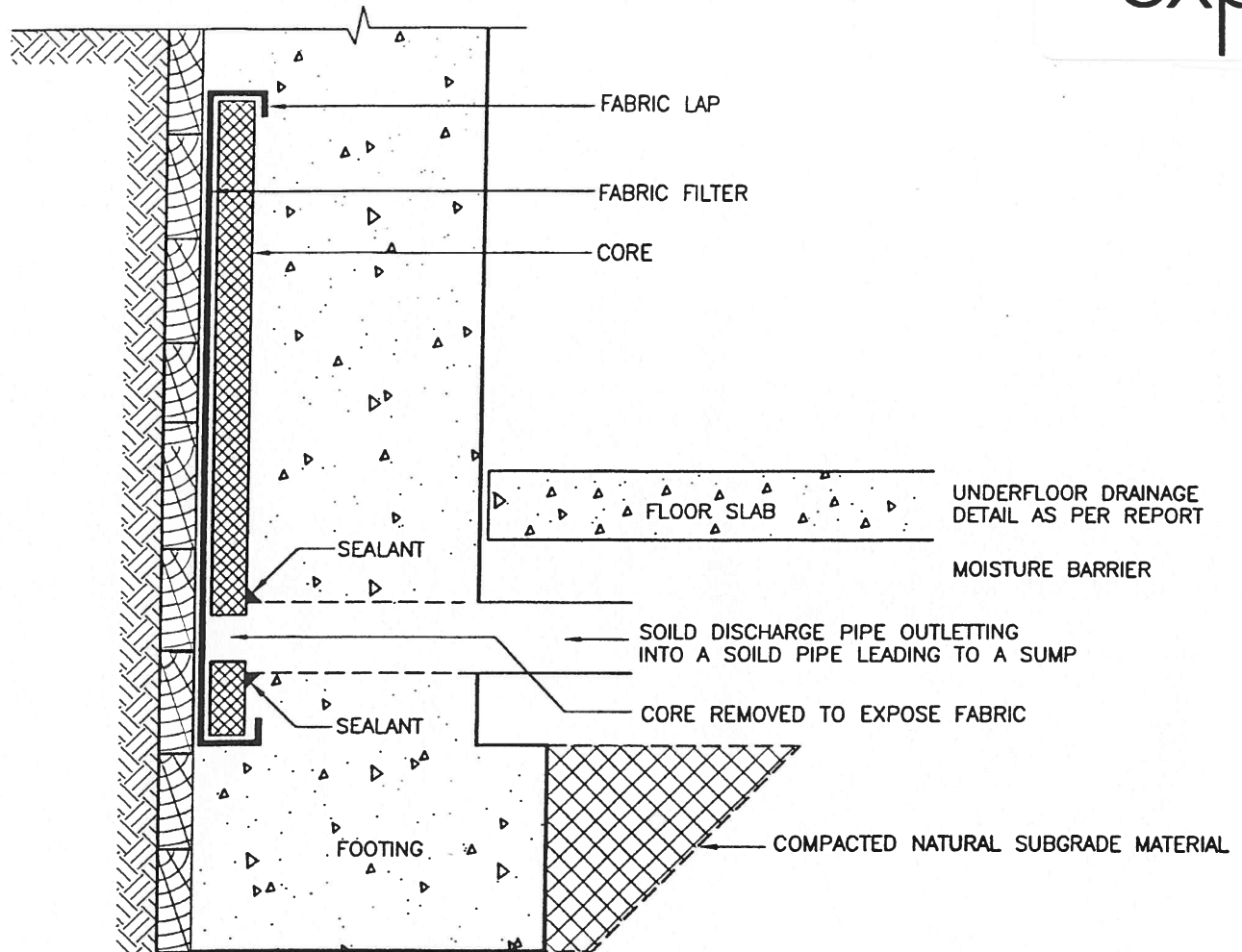
## Grain-Size Distribution Curve Method of Test For Particle Size Analysis of Soil ASTM C-136/ASTM D422

**EXP Services Inc.**  
100-2650 Queensview Drive  
Ottawa, ON K2B 8H6

### Unified Soil Classification System



EXP Project No.:	OTT-00252625-A0	Project Name :	Residential Development	
Client :	11061917 Canada Inc.	Project Location :	365 Forest Ave, Ottawa, ON.	
Date Sampled :	April 24, 2019	Borehole No:	BH 19-11	Sample No.: SS6
Sample Description :	% Silt and Clay	36	% Sand	51
			% Gravel	13
Sample Description :	GLACIAL TILL: Silty Sand (SM)			Depth (m) : 4.6-5.2
				Figure : 21



SECTION AT DISCHARGE PIPE

NOTES:

1. DRAINAGE CORE AND CLOTH TO BE TERRADRAIN 200 OR EQUIVALENT.
2. INSTALLATION INSTRUCTIONS AS PER MANUFACTURES SPECIFICATION.
3. TO BE FULL WIDTH UNLESS OTHERWISE RECOMMENDED BY THE ENGINEER.
4. FINAL DETAIL MUST BE APPROVED BEFORE SYSTEM IS CONSIDERED ACCEPTABLE.
5. TERRADRAIN 200 SHOULD BE KEPT A MINIMUM OF 1.2 m BELOW EXTERIOR FINISHED GRADE.

SUGGESTED EXTERIOR DRAINAGE AGAINST SOLDIER PILE  
AND LAGGING SHORING SYSTEM

EXP Services Inc.

Client: 11061917 Canada Inc.  
Project Name: Geotechnical Investigation - Residential Development  
Location: 365 Forest Street, Ottawa, ON.  
EXP Project Number: OTT-00252625-A0  
Date: November 5, 2021

## **Appendix A: Laboratory Certificate of Analysis**



**CLIENT NAME: EXP SERVICES INC  
2650 QUEENSVIEW DRIVE, UNIT 100  
OTTAWA, ON K2B8H6  
(613) 688-1899**

**ATTENTION TO: Susan Potyondy**

**PROJECT: OTT-252625-A0**

**AGAT WORK ORDER: 19Z484141**

**SOIL ANALYSIS REVIEWED BY: Nivine Basily, Inorganics Report Writer**

**DATE REPORTED: Jul 02, 2019**

**PAGES (INCLUDING COVER): 5**

**VERSION\*: 1**

Should you require any information regarding this analysis please contact your client services representative at (905) 712-5100

**\*NOTES**

**All samples will be disposed of within 30 days following analysis. Please contact the lab if you require additional sample storage time.**



## Certificate of Analysis

AGAT WORK ORDER: 19Z484141

PROJECT: OTT-252625-A0

5835 COOPERS AVENUE  
MISSISSAUGA, ONTARIO  
CANADA L4Z 1Y2  
TEL (905)712-5100  
FAX (905)712-5122  
<http://www.agatlabs.com>

CLIENT NAME: EXP SERVICES INC  
SAMPLING SITE: 365 Forest Street

ATTENTION TO: Susan Potyondy  
SAMPLED BY: exp

### Inorganic Chemistry (Soil)

DATE RECEIVED: 2019-06-25

DATE REPORTED: 2019-07-02

Parameter	Unit	SAMPLE DESCRIPTION:		BH1 Run1	BH3 SS5 10'-12'	BH11 Run1	BH12 SS4
		SAMPLE TYPE:		21'3"-23'7"	25'8"-26'9"	7'6"-9'6"	
		DATE SAMPLED:		Soil	Soil	Soil	Soil
		G / S	RDL	2019-04-30	2019-04-30	2019-04-30	2019-04-30
pH (2:1)	pH Units	N/A		8.55	8.00	8.59	8.17
Resistivity (2:1)	ohm.cm	1		2490	2480	2110	1950
Chloride (2:1)	µg/g	2		25	120	21	114
Sulphate (2:1)	µg/g	2		42	50	26	121

**Comments:** RDL - Reported Detection Limit; G / S - Guideline / Standard  
**301670-301673** pH was determined on the 0.01M CaCl<sub>2</sub> extract obtained from 2:1 leaching procedure (2 parts extraction fluid:1 part wet soil).  
 Chloride & Sulphate were determined on the extract obtained from the 2:1 leaching procedure (2 parts DI water: 1 part soil).  
 Resistivity is a calculated parameter.

**Certified By:**

*Divine Basily*

## Quality Assurance

**CLIENT NAME:** EXP SERVICES INC  
**PROJECT:** OTT-252625-A0  
**SAMPLING SITE:** 365 Forest Street

**AGAT WORK ORDER:** 19Z484141  
**ATTENTION TO:** Susan Potyondy  
**SAMPLED BY:** exp

Soil Analysis															
RPT Date:			DUPLICATE				Method Blank	REFERENCE MATERIAL			METHOD BLANK SPIKE			MATRIX SPIKE	
PARAMETER	Batch	Sample Id	Dup #1	Dup #2	RPD	Measured Value		Acceptable Limits		Recovery	Acceptable Limits		Recovery	Acceptable Limits	
								Lower	Upper		Lower	Upper		Lower	Upper

**Inorganic Chemistry (Soil)**

pH (2:1)	301670	301670	8.55	8.50	0.6%	NA	101%	90%	110%						
Chloride (2:1)	301670	301670	25	26	3.9%	< 2	109%	70%	130%	99%	70%	130%	98%	70%	130%
Sulphate (2:1)	301670	301670	42	43	2.4%	< 2	101%	70%	130%	105%	70%	130%	109%	70%	130%

Comments: NA signifies Not Applicable.  
 pH duplicates QA acceptance criteria was met relative as stated in Table 5-15 of Analytical Protocol document.

**Certified By:** \_\_\_\_\_

*Divine Basily*





## Method Summary

CLIENT NAME: EXP SERVICES INC

PROJECT: OTT-252625-A0

SAMPLING SITE:365 Forest Street

AGAT WORK ORDER: 19Z484141

ATTENTION TO: Susan Potyondy

SAMPLED BY:exp

PARAMETER	AGAT S.O.P	LITERATURE REFERENCE	ANALYTICAL TECHNIQUE
<b>Soil Analysis</b>			
pH (2:1)	INOR 93-6031	MSA part 3 & SM 4500-H+ B	PH METER
Resistivity (2:1)	INOR-93-6036	McKeague 4.12, SM 2510 B,SSA #5 Part 3	EC METER
Chloride (2:1)	INOR-93-6004	McKeague 4.12 & SM 4110 B	ION CHROMATOGRAPH
Sulphate (2:1)	INOR-93-6004	McKeague 4.12 & SM 4110 B	ION CHROMATOGRAPH



EXP Services Inc.

Client: 11061917 Canada Inc.  
Project Name: Geotechnical Investigation - Residential Development  
Location: 365 Forest Street, Ottawa, ON.  
EXP Project Number: OTT-00252625-A0  
Date: November 5, 2021

## **Appendix B: Multi-channel Analysis of Surface Waves (MASW) Survey**





**GEOPHYSICS GPR INTERNATIONAL INC.**

100 – 2545 Delorimier Street    Tel. : (450) 679-2400  
Longueuil (Québec)            Fax : (514) 521-4128  
Canada J4K 3P7                    info@geophysicsgpr.com  
www.geophysicsgpr.com

August 23<sup>th</sup>, 2019

Transmitted by email: [ismail.taki@exp.com](mailto:ismail.taki@exp.com)  
Our Ref.: GPR-19-01572-D

Mr. Ismail Taki, M.Eng., P.Eng.  
Manager, Geotechnical Services  
**exp** Services inc.  
100 - 2650 Queensview Drive  
Ottawa (ON) K2B 8H6

**Subject:    Shear Wave Velocity Sounding for the Site Class Determination**  
**365 Forest Street, Ottawa (ON)**

[ Project: OTT-00252625-A0]

Dear Sir,

Geophysics GPR International Inc. has been requested by **exp** Services Inc. to carry out seismic shear wave surveys on a parking lot located east of the intersection of Forest Street and Richmond Road, in Ottawa (ON). The geophysical investigations used the Multi-channel Analysis of Surface Waves (MASW), the Extended SPatial AutoCorrelation (ESPAC), and the seismic refraction methods. From the subsequent results, the seismic shear wave velocities values were calculated for the soil and the rock, and the Site Class was identified.

The surveys were carried out on July 30<sup>th</sup>, 2019, by Mr. Dominic Dérap and Mr. Jacques-Olivier Joly. Figure 1 shows the regional location of the site and Figure 2 illustrates the location of the seismic spreads. Both figures are presented in the Appendix.

The following paragraphs briefly describe the survey design, the principle of the test method, and the results in graphic and table format.

## MASW PRINCIPLE

The *Multi-channel Analysis of Surface Waves* (MASW) and the *Extended SPatial AutoCorrelation* (ESPAC or MAM for *Microtremors Array Method*) are seismic methods used to evaluate the shear wave velocities of subsurface materials through the analysis of the dispersion properties of the Rayleigh surface waves (“ground roll”). The MASW is considered an “active” method, as the seismic signal is induced at known location and time in the geophones spread axis. Conversely, the ESPAC is considered a “passive” method, using the low frequency “signals” produced far away. The method can also be used with “active” seismic source records. The dispersion properties are expressed as a change of phase velocities with frequencies. Surface wave energy will decay exponentially with depth. Lower frequency surface waves will travel deeper and thus be more influenced by deeper velocity layering than the shallow higher frequency waves. The inversion of the Rayleigh wave dispersion curve yields a shear wave ( $V_s$ ) velocity depth profile (sounding). Figure 3 schematically outlines the basic operating procedure for the MASW method.

Figure 4 illustrates an example of one of the MASW/ESPAC records, the corresponding spectrogram analysis and resulting 1D  $V_s$  model. The ESPAC method allows deeper  $V_s$  soundings, but generally with a lower resolution for the surface portion. Its dispersion curve can then be merged with the higher frequency one from the MASW to calculate a more complete inversion.

## INTERPRETATION

The main processing sequence involved data inspection and edition when required; spectral analysis (“phase shift” for MASW, and “cross-correlation” for ESPAC); picking the fundamental mode; and 1D inversion of the MASW and ESPAC shot records using the SeisImagerSW™ software. The data inversions used a nonlinear least squares algorithm.

In theory, all the shot records for a given seismic spread should produce a similar shear-wave velocity profile. In practice, however, differences can arise due to energy dissipation, local surface seismic velocities variations, and/or dipping of overburden layers or rock. In general, the precision of the calculated seismic shear wave velocities ( $V_s$ ) is of the order of 15% or better.

More detailed descriptions of these methods are presented in *Shear Wave Velocity Measurement Guidelines for Canadian Seismic Site Characterization in Soil and Rock*, Hunter, J.A., Crow, H.L., et al., Geological Surveys of Canada, General Information Product 110, 2015.



## **SURVEY DESIGN**

The seismic acquisition spreads were located on a parking lot, east of the intersection of Forest Street and Richmond Road. The geophone spacing for the main spread was 3 metres, using 24 geophones. A shorter seismic spread, with geophone spacing of 1 metre, was dedicated to the near surface materials.

The seismic records counted 4096 data, sampled at 1000  $\mu$ s for the MASW surveys, and 50  $\mu$ s for the seismic refraction. The records included a pre-trig portion of 10 ms. A stacking procedure was also used to improve the Signal / Noise ratio for the seismic records.

The shear wave depth sounding can be considered as the average of the bulk area within the geophone spread, especially for its central half-length. The seismic records were produced with a seismograph Terraloc MK6 (from ABEM Instrument), and the geophones were 4.5 Hz. A 9 kg sledgehammer was used as the energy source with impacts being recorded off both ends of the seismic spreads.

## **RESULTS**

From seismic refraction, the rock depth was calculated between 5.5 and 9 metres, with an average depth of 7.2 metres (+/- 1 metre), and its seismic shear wave velocity was calculated between 1580 and 1625 m/s for its upper portion. These results were used as initial parameters for the basic geophysical model, prior to the MASW dispersion curves modeling and inversions. The MASW calculated  $V_s$  results are illustrated at Figure 5 and they are also presented at Table 1.

The  $\bar{V}_{s30}$  value results from the harmonic mean of the shear wave velocities, from the surface to 30 metres deep. It is calculated by dividing the total depth of interest (30 metres) by the sum of the time spent in each velocity layer from the surface up to 30 metres. This value represents an equivalent homogeneous single layer response.

The  $\bar{V}_{s30}$  value for the actual site is 581.7 m/s (cf. Table 1), corresponding to the Site Class "C". The planned foundation depth being 8.6 metres, the  $\bar{V}_{s30}^*$  value would be 1610.4 m/s (cf. Table 2), allowing the use of the Site Class "A".



## CONCLUSION

Geophysical surveys were carried out on a parking lot, located east of the intersection of Forest Street and Richmond Road, in Ottawa (ON). The seismic surveys used the MASW and ESPAC analysis methods, and the seismic refraction as complement. The  $\bar{V}_{S30}$  calculation, for the actual site, is presented in Table 1.

The calculated  $\bar{V}_{S30}$  value of the actual site is 582 m/s corresponding to the Site Class "C" ( $360 < \bar{V}_{S30} \leq 760$  m/s), as determined through the MASW and ESPAC methods, Table 4.1.8.4.A of the NBC, and the Building Code, O. Reg. 332/12. As the planned foundation depth is 8.6 metres, the corresponding  $\bar{V}_{S30}^*$  value would be 1610 m/s, allowing to use the Site Class "A" (Table 2).

It must be noted that other geotechnical information gleaned on site; including the presence of liquefiable soils, quick and highly sensitive clays, high moisture content etc. can supersede the Site Classification provided in this report based on the  $\bar{V}_{S30}$  value.

The  $V_s$  values calculated are representative of the in-situ materials and are not corrected for the total and effective stresses.



Jean-Luc Arsenault, M.A.Sc., P.Eng.  
Senior Project Manager



2019-08-23

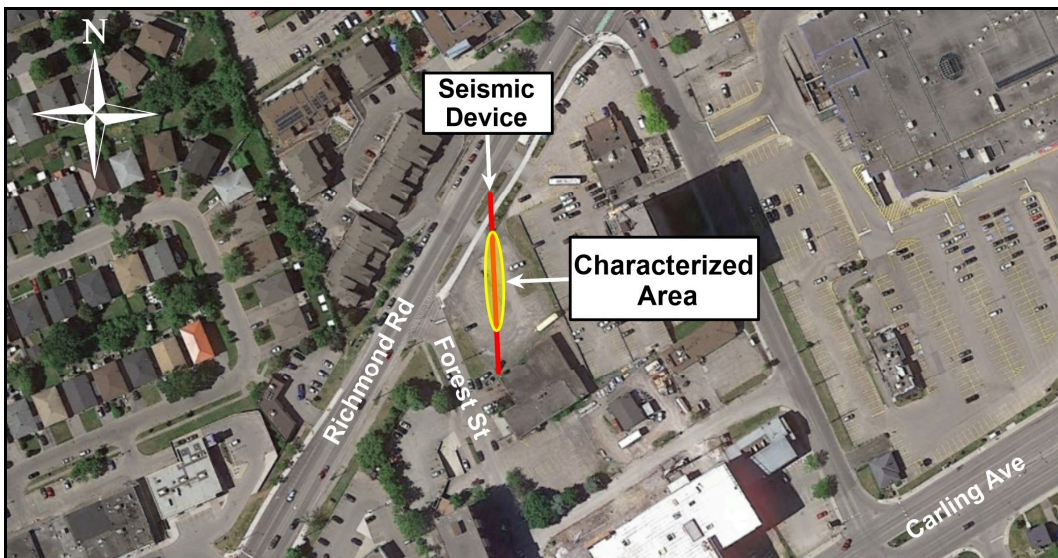






**Figure 1: Regional location of the Site**

(source: *OpenStreetMap*©)

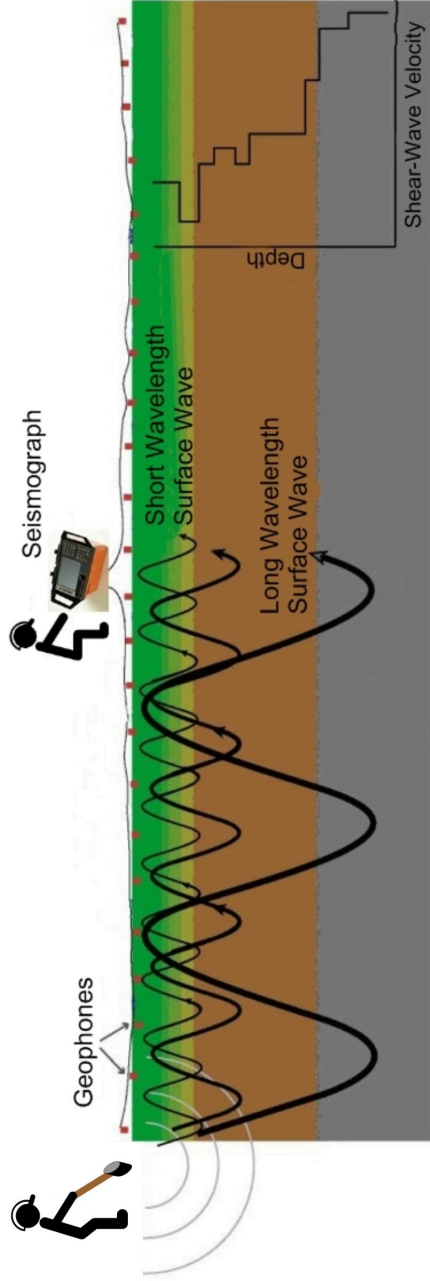


**Figure 2: Location of the seismic spreads**

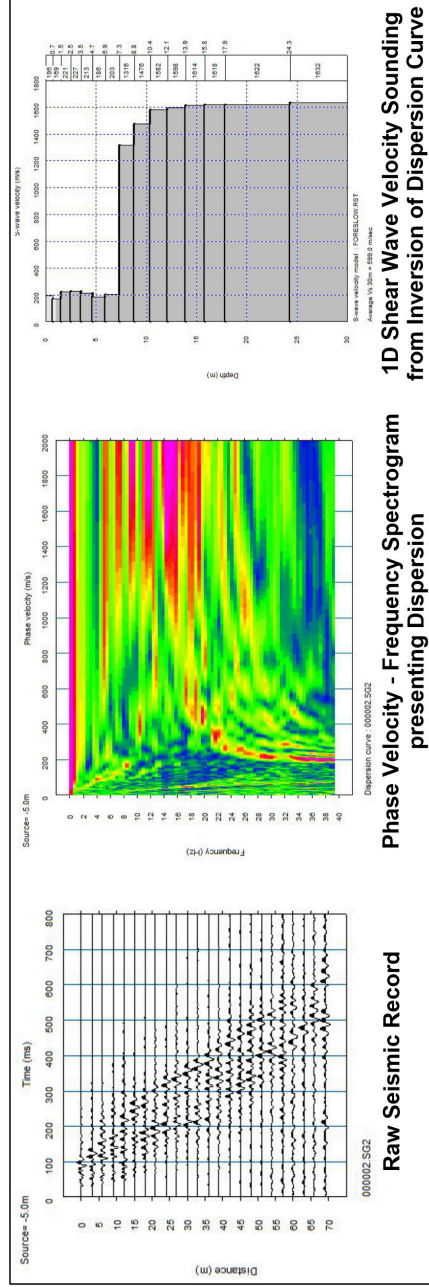
(source: *GoogleEarth*©)

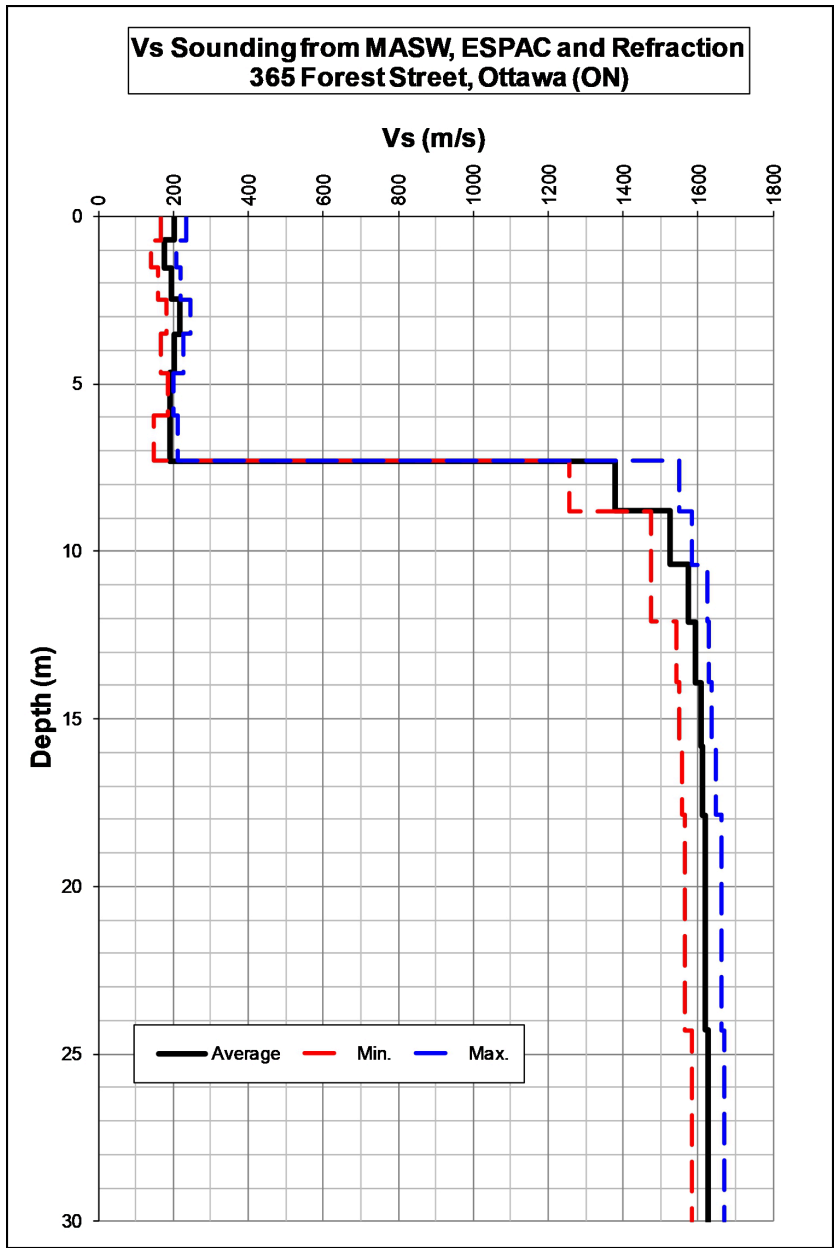






**Figure 3: MASW Operating Principle**





**Figure 5: MASW Shear-Wave Velocities Sounding**



**TABLE 1**  
**V<sub>S30</sub> Calculation for the Site Class (actual site)**

Depth (m)	Vs			Thickness (m)	Cumulative Thickness (m)	Delay for Avg Vs (s)	Cumulative Delay (s)	Average Vs at given Depth (m/s)
	Min. (m/s)	Average (m/s)	Max. (m/s)					
0	165.3	201.0	235.9					
0.71	139.5	175.8	208.2	0.71	0.71	0.003554	0.003554	201.0
1.54	161.2	195.9	221.3	0.82	1.54	0.004688	0.008242	186.7
2.47	181.7	219.0	246.7	0.93	2.47	0.004767	0.013009	190.1
3.52	168.3	202.3	226.8	1.04	3.52	0.004766	0.017775	197.8
4.67	186.0	191.2	202.4	1.15	4.67	0.005704	0.023479	198.9
5.93	148.5	190.7	213.8	1.26	5.93	0.006610	0.030089	197.2
7.31	1258.0	1379.9	1548.7	1.37	7.31	0.007203	0.037291	196.0
8.79	1475.8	1524.5	1582.9	1.48	8.79	0.001075	0.038367	229.1
10.38	1525.2	1575.0	1624.9	1.59	10.38	0.001045	0.039412	263.5
12.09	1540.0	1593.8	1626.3	1.70	12.09	0.001081	0.040493	298.5
13.90	1550.1	1605.7	1637.2	1.81	13.90	0.001138	0.041631	333.9
15.82	1555.4	1611.5	1647.9	1.92	15.82	0.001198	0.042829	369.5
17.86	1563.9	1618.2	1662.5	2.03	17.86	0.001262	0.044090	405.0
24.29	1583.9	1627.7	1669.3	6.43	24.29	0.003973	0.048063	505.3
<b>30</b>				5.71	30.00	0.003511	0.051573	581.7

<b>V<sub>S30</sub> (m/s)</b>	<b>581.7</b>
<b>Class</b>	<b>C</b>

**TABLE 2**  
**V<sub>S30</sub>\* Calculation for the Site Class (foundation at 8.6 metres deep)**

Depth (m)	Vs			Thickness (m)	Cumulative Thickness (m)	Delay for Avg Vs (s)	Cumulative Delay (s)	Average Vs at given Depth (m/s)
	Min. (m/s)	Average (m/s)	Max. (m/s)					
0	165.3	201.0	235.9					
0.71	139.5	175.8	208.2					
1.54	161.2	195.9	221.3					
2.47	181.7	219.0	246.7					
3.52	168.3	202.3	226.8					
4.67	186.0	191.2	202.4					
5.93	148.5	190.7	213.8					
7.31	1258.0	1379.9	1548.7					
<b>8.6</b>	1258.0	1379.9	1548.7					
8.79	1475.8	1524.5	1582.9	0.19	0.19	0.000139	0.000139	1379.9
10.38	1525.2	1575.0	1624.9	1.59	1.78	0.001045	0.001184	1507.6
12.09	1540.0	1593.8	1626.3	1.70	3.49	0.001081	0.002265	1539.7
13.90	1550.1	1605.7	1637.2	1.81	5.30	0.001138	0.003403	1557.8
15.82	1555.4	1611.5	1647.9	1.92	7.22	0.001198	0.004601	1570.3
17.86	1563.9	1618.2	1662.5	2.03	9.26	0.001262	0.005862	1579.2
24.29	1583.9	1627.7	1669.3	6.43	15.69	0.003973	0.009835	1594.9
<b>38.6</b>				14.31	30.00	0.008794	0.018629	1610.4

<b>V<sub>S30</sub>* (m/s)</b>	<b>1610.4</b>
<b>Class</b>	<b>A</b>

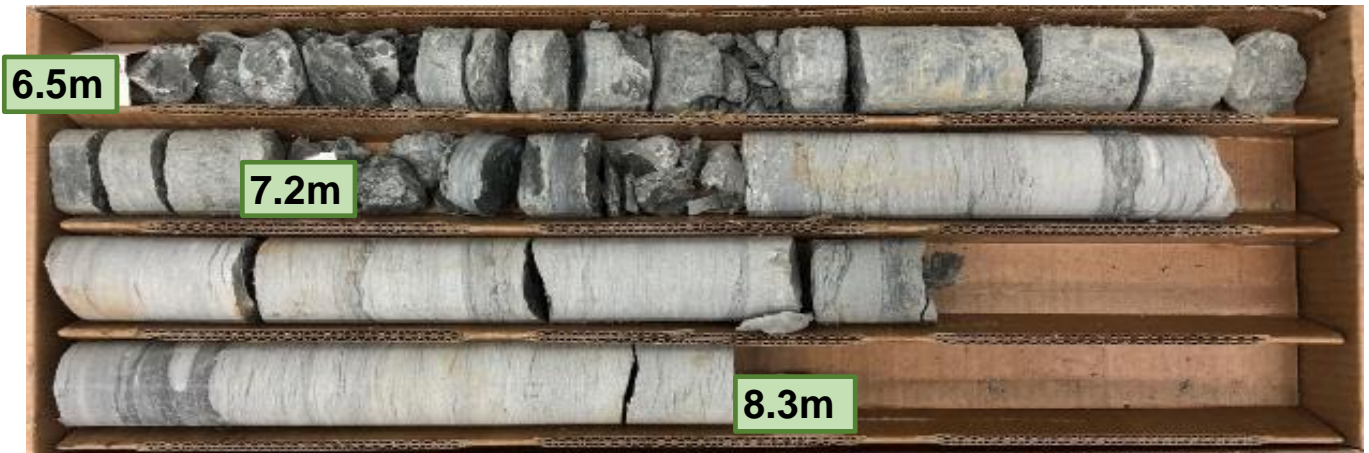


EXP Services Inc.

Client: 11061917 Canada Inc.  
Project Name: Geotechnical Investigation - Residential Development  
Location: 365 Forest Street, Ottawa, ON.  
EXP Project Number: OTT-00252625-A0  
Date: November 5, 2021

## **Appendix C: Bedrock Core Photographs**

**DRY BEDROCK CORES**



**WET BEDROCK CORES**



**exp Services Inc.**

t: +1.613.688.1899 | f: +1.613.225.7337  
 2650 Queensview Drive, Suite 100  
 Ottawa, ON K2B 8H6  
 Canada

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borehole no. <b>BH 19-01</b>	core runs Run 1: 6.5m-7.2m Run 2: 7.2m-8.3m	PROJECT <b>RESIDENTIAL DEVELOPMENT 365 FOREST AVENUE, OTTAWA, ON.</b>	project no. OTT-00252625-A0
date cored Apr 30, 2019		<b>BEDROCK CORE PHOTOGRAPHS</b>	<b>FIG. C-1</b>



**DRY BEDROCK CORES**



**WET BEDROCK CORES**



**exp Services Inc.**

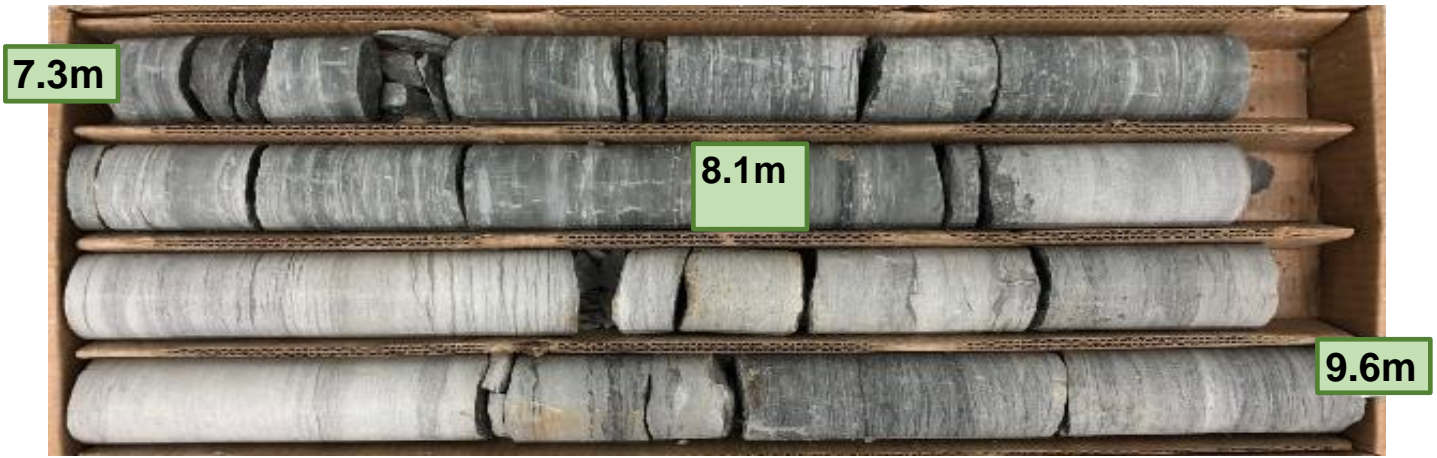
t: +1.613.688.1899 | f: +1.613.225.7337  
 2650 Queensview Drive, Suite 100  
 Ottawa, ON K2B 8H6  
 Canada

[www.exp.com](http://www.exp.com)

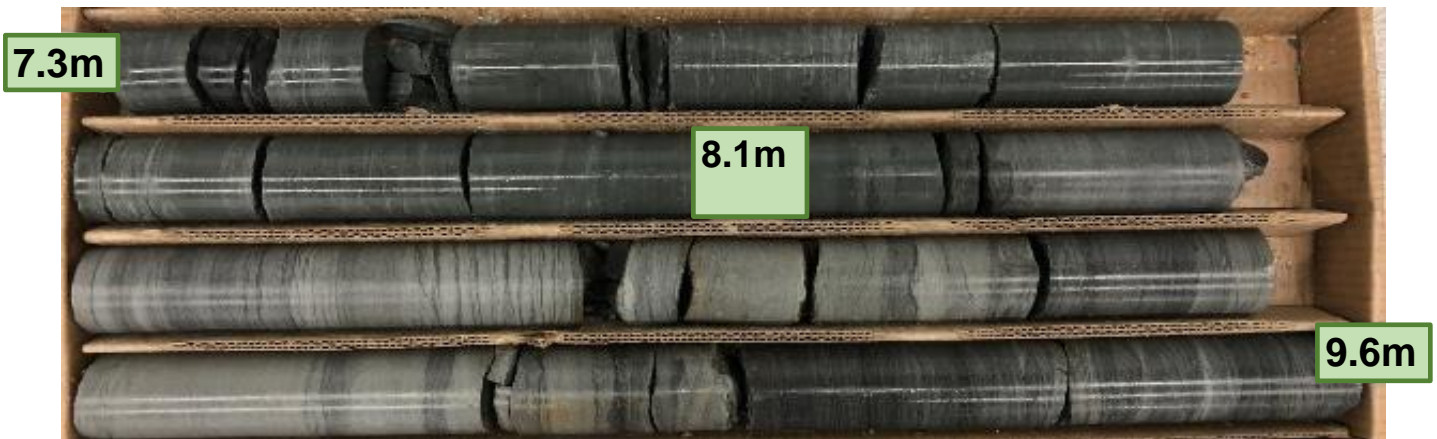
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- INDUSTRIAL • INFRASTRUCTURE • SUSTAINABILITY •

borehole no. <b>BH 19-03</b>	core runs Run 1: 7.0m-8.0m	PROJECT RESIDENTIAL DEVELOPMENT 365 FOREST AVENUE, OTTAWA, ON.	project no. OTT-00252625-A0
date cored Apr 30, 2019		BEDROCK CORE PHOTOGRAPHS	FIG. C-2

**DRY BEDROCK CORES**



**WET BEDROCK CORES**



**exp Services Inc.**

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2650 Queensview Drive, Suite 100

Ottawa, ON K2B 8H6

Canada

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borehole no. <b>BH 19-08</b>	core runs Run 1: 7.3m-8.1m Run 2: 8.1m-9.6m	PROJECT RESIDENTIAL DEVELOPMENT 365 FOREST AVENUE, OTTAWA, ON.	project no. OTT-00252625-A0
date cored Apr 25, 2019		BEDROCK CORE PHOTOGRAPHS	FIG. C-3

**DRY BEDROCK CORES**



**WET BEDROCK CORES**



**exp Services Inc.**

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2650 Queensview Drive, Suite 100

Ottawa, ON K2B 8H6

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- INDUSTRIAL • INFRASTRUCTURE • SUSTAINABILITY •

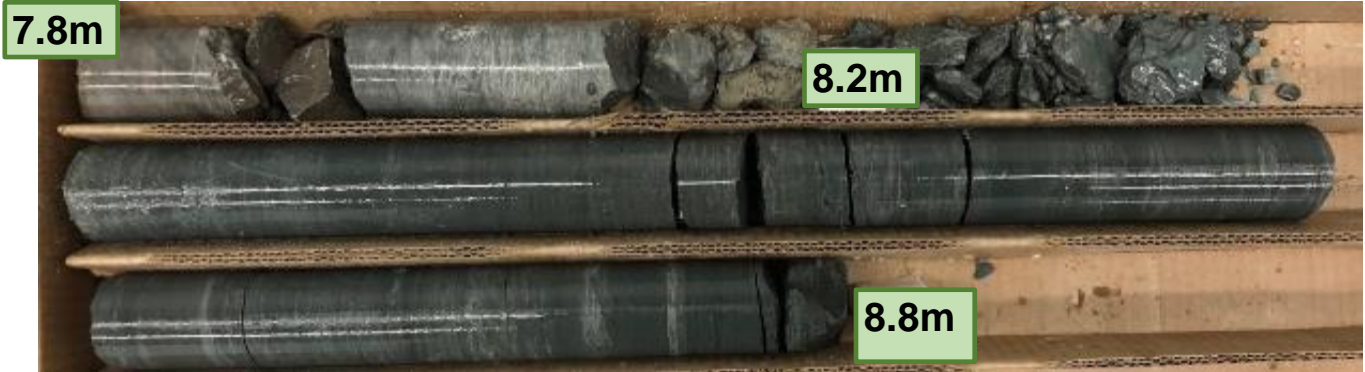
borehole no. <b>BH 19-09</b>	core runs Run 1: 7.6m-8.7m	PROJECT RESIDENTIAL DEVELOPMENT 365 FOREST AVENUE, OTTAWA, ON.	project no. OTT-00252625-A0
date cored Apr 24, 2019		BEDROCK CORE PHOTOGRAPHS	FIG. C-4



**DRY BEDROCK CORES**



**WET BEDROCK CORES**



**exp Services Inc.**

t: +1.613.688.1899 | f: +1.613.225.7337

2650 Queensview Drive, Suite 100

Ottawa, ON K2B 8H6

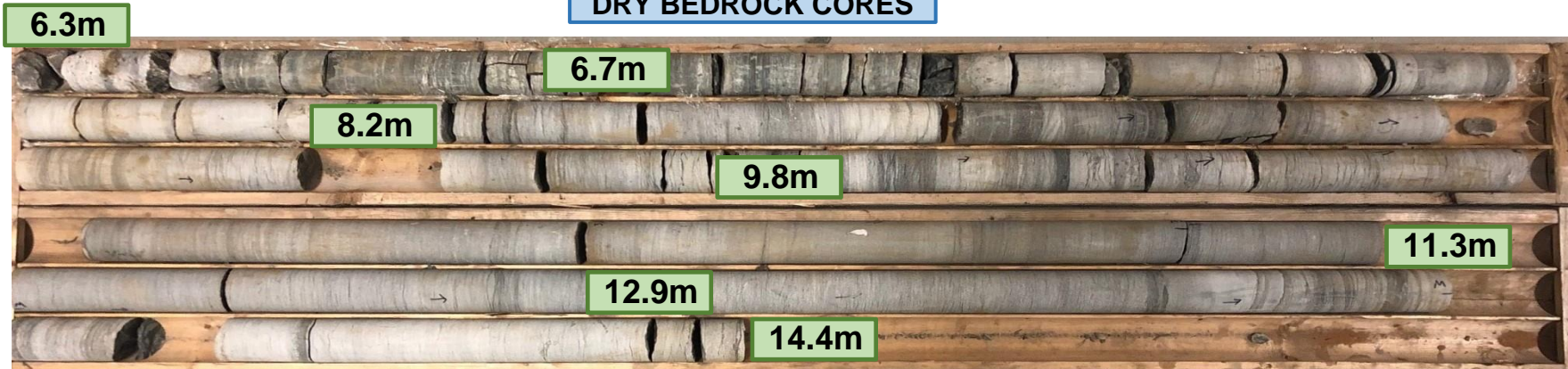
Canada

[www.exp.com](http://www.exp.com)

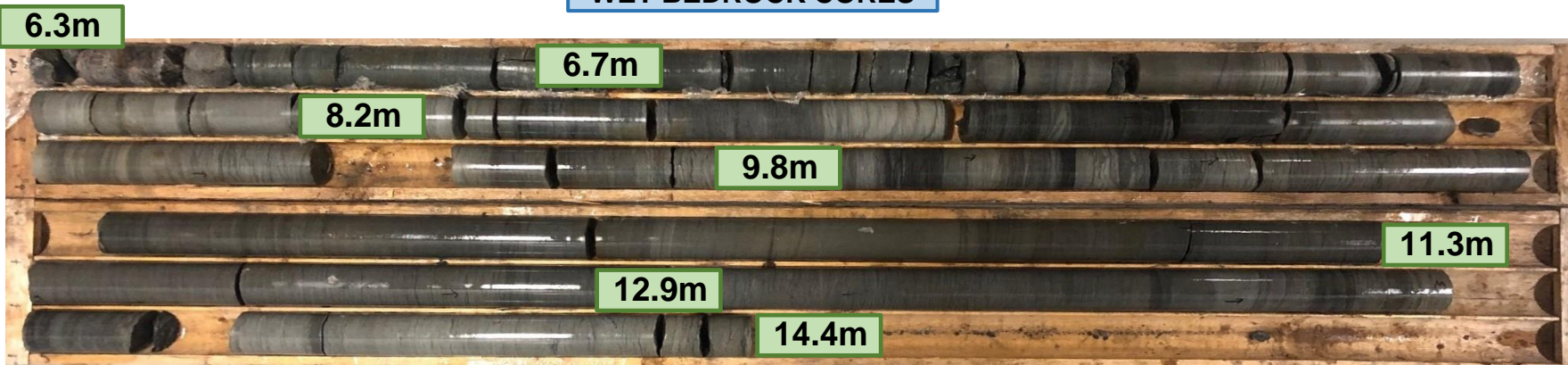
- BUILDINGS • EARTH & ENVIRONMENT • ENERGY •
- INDUSTRIAL • INFRASTRUCTURE • SUSTAINABILITY •

borehole no. <b>BH 19-11</b>	core runs Run 1: 7.8m-8.2m Run 2: 8.2m-8.8m	PROJECT <b>RESIDENTIAL DEVELOPMENT</b> 365 FOREST AVENUE, OTTAWA, ON.	project no. OTT-00252625-A0
date cored Apr 29, 2019		<b>BEDROCK CORE PHOTOGRAPHS</b>	<b>FIG. C-5</b>

**DRY BEDROCK CORES**



**WET BEDROCK CORES**



EXP Services Inc. [www.exp.com](http://www.exp.com)

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2650 Queensview Drive, Suite 100

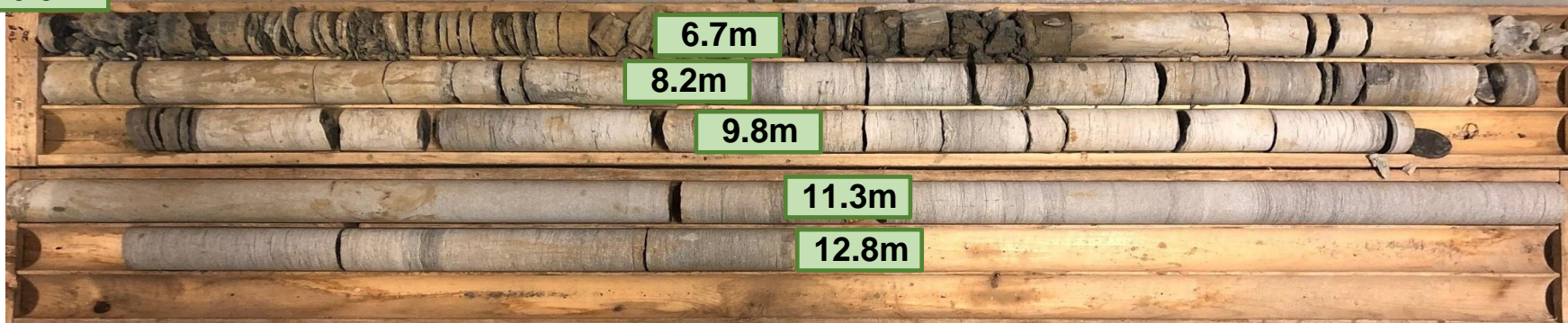
Ottawa, ON K2B 8H6, Canada

borehole no.  <b>BH21-13</b>	core runs Run 1: 6.3m - 6.7mm Run 2: 6.7m - 8.2mm Run 3: 8.2m - 9.8m	project  Location: 365 Forest Street, Ottawa, ON	project no.  OTT-00252625-A0
date cored  Oct 06, 2021	Run 4: 9.8m - 11.3m Run 5: 11.3m - 12.9m Run 6: 12.9m - 14.4m	Rock Core Photographs	FIG C-6



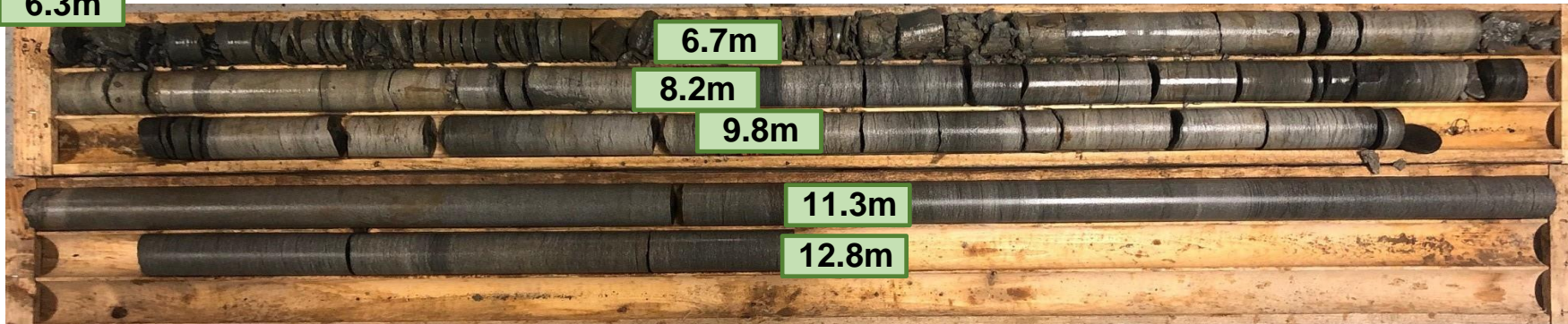
**DRY BEDROCK CORES**

6.3m



**WET BEDROCK CORES**

6.3m



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borehole no.  <b>BH21-14</b>	core runs Run 1: 6.3m - 6.7mm Run 2: 6.7m - 8.2mm Run 3: 8.2m - 9.8m	project  Location: 365 Forest Street, Ottawa, ON	project no.  OTT-00252625-A0
date cored  Oct 05, 2021	Run 4: 9.8m - 11.3m Run 5: 11.3m - 12.8m	Rock Core Photographs	FIG C-7

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