Hydrogeological Study 8520 McArton Road, Ottawa, Ontario

Revision: 0

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Executive Summary

Geofirma Engineering Ltd. was retained by the Ottawa Valley Wild Bird Care Center (OVWBCC) to complete a Hydrogeological Study in support of a Site Plan Control application for construction of a wild bird care center on a property located at 8520 McArton Road in Ottawa (Ashton), Ontario. The property is currently a vacant, relatively flat-lying, agricultural field.

Based on a review of surficial features at the site, shallow groundwater flow is interpreted to be eastward towards an on-site wetland complex. It is anticipated that deeper groundwater flow is to the east (i.e. the Rideau River).

This study has been completed in general accordance with Ontario Ministry of the Environment, Conservation and Parks (MECP) Procedures D-5-5 Private Wells: Water Supply Assessment (MECP, 1996a) and D-5-4 Individual On-Site Sewage Systems: Water Quality Impact Assessment (MECP, 1996b), as well as the City of Ottawa draft Hydrogeological and Terrain Analysis Guidelines (City of Ottawa, 2019).

In support of this study, Geofirma supervised the drilling and construction of a water supply well on the property in accordance with Ontario Regulation 903. The well was drilled to a total depth of approximately 53.3 meters below ground surface (mBGS) and casing was installed to approximately 12.8 mBGS. Bedrock was encountered at a depth of approximately 2.1 mBGS and static groundwater levels were approximately 4 mBGS.

An approximate 7-hour duration pumping test with a constant rate of approximately 122 L/min (32 USgpm) was completed for this water supply well on February 4, 2020. Total drawdown during this test was approximately 1 m and recovered within 60 seconds. Two water samples were collected during this pumping test (3h and 6.5h). The results from the pumping test and laboratory testing show the water quantity and quality are suitable to support the proposed development. Further, the groundwater samples meet all applicable health-related standards and guidelines at the present time. Some treatment may be desired for aesthetic objectives only.

Surficial soils are thin with approximately 0.4 to 2.4 m thick sandy till material above limestone bedrock. An assessment of nitrate attenuation following MECP Guideline D-5-4 indicates that the property size and conditions are suitable to support a conventional septic system as per the proposed development. Predicted nitrate-nitrogen levels are expected to be less than 7 mg/L according to these calculations.

The infiltration capacity of overburden material at the site should be confirmed using field percolation tests at the septic system design phase. Any septic systems should be constructed with all appropriate setbacks as per Ontario Regulations and the Ontario Building Code.

ii

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TABLE OF CONTENTS

1	INIK	ODUCTION	1
	1.1 E	Background	1
		Objectives and Scope of Work	
		•	
2	SITE	DESCRIPTION	2
	2.1 P	Physical Setting	2
		2.1.1 Site Location	
		2.1.2 Surrounding Properties and Land Use	
		learby MECP Water Well Records	
		Geological Setting	
		2.3.1 Surficial Geology	
		2.3.2 Bedrock Geology	
		lydrogeology	
	2	2.4.1 Overburden Aquifer	3
		2.4.2 Bedrock Aquifer	
	2	2.4.3 Groundwater Flow Direction	3
_			
3		HODOLOGY	
		Stimation of Water Demand	
	3.2 L	Itility Locates	4
	3.3 V	Vater Well Drilling	4
	3.4 V	Vater Well Pumping Test	4
	3	3.4.1 Test Equipment and Set-up	5
		3.4.2 Test Procedure	5
		3.4.3 Measurement of Field Parameters	
	3	3.4.4 Groundwater Sample Collection	5
4	UVD	ROGEOLOGICAL ASSESSMENT	7
4			
		Review of MECP Water Well Records	
		Vater Quantity	
		Vater Quality	
		I.3.1 Health-Based Standards	
		4.3.2 Aesthetic Objectives and Operational Guidelines	3
		1.3.3 Corrosion / Encrustation Potential - Langelier Saturation Index (LSI) and Ryznar	_
	S	Stability Index (RSI)	ბ
5	IMPA	CT ASSESSMENT	10
-		lydrogeological Sensitivity	
		Septic Assessment	
		5.2.1 Estimated Sewage Flow	
		5.2.2 Background Nitrate Concentrations	
	_	5.2.3 Nitrate Attenuation Assessment	
	•	Potential Sources of Contamination	
		Cumulative Impacts	
		Source Water Protection	
		Development Considerations	
	U.U L	/otolopillolit oolidikolkulla	. 4



6 CONCL	USIONS AND RECOMMENDATIONS	14
7 REFER	ENCES	16
8 CLOSU	IRE	17
	LIST OF FIGURES (APPENDIX A)	
Figure A.1	Site Location	
Figure A.2	Site Layout	
Figure A.3	MECP Water Wells	
Figure A.4	Surficial Geology	
Figure A.5	Bedrock Geology	
Figure A.6	Proposed Site Development Plan	
	LIST OF TABLES (APPENDIX B)	
Table 1	Summary of MECP Water Well Data Within 500m of Site	
Table 2	Summary of Measured Water Levels	
Table 3	Summary of Measured Flow Rates	
Table 4	Summary of Field Readings	
Table 5	Groundwater Quality Analytical Results	
	LIST OF ADDENDICES	
ADDENDIV	LIST OF APPENDICES	
APPENDIX APPENDIX		
APPENDIX	•	
APPENDIX		
APPENDIX	E Pumping Test Results and Analysis	
APPENDIX	F Laboratory Report	
APPENDIX	G Water Corrosive Index Calculations (LSI and RSI Index)	
APPENDIX	H Site Plan	
APPENDIX	I Nitrate Dilution Calculations	

iv



1 INTRODUCTION

Geofirma Engineering Ltd. was retained by the Ottawa Valley Wild Bird Care Center (OVWBCC) to complete a Hydrogeological Study in support of a Site Plan Control application for construction of a wild bird care center on a property located at 8520 McArton Road in Ottawa (Ashton), Ontario. The site location is provided on Figure A.1, Appendix A.

This report has been prepared to satisfy City of Ottawa requirements to demonstrate that the water well drilled at 8520 McArton Road is suitable for the proposed development on the site. This study has been completed in general accordance with Ontario Ministry of the Environment, Conservation and Parks (MECP) Procedures D-5-5 Private Wells: Water Supply Assessment (MECP, 1996a) and D-5-4 Individual On-Site Sewage Systems: Water Quality Impact Assessment (MECP, 1996b), as well as the City of Ottawa draft Hydrogeological and Terrain Analysis Guidelines (City of Ottawa, 2019).

1.1 **Background**

The owners of the property at 8520 McArton Road, the Ottawa Valley Wild Bird Care Center (OVWBCC), plan construct a bird care center on the 7.0 hectare (17.3 acre) property, which will include an approximately 623.25 m² single story building, outdoor bird cages, and a water retention pond. In addition, a paved parking lots (24 spaces) and a driveway and loading dock area will be constructed with a combined surface area of approximately 1000 m². The building will be serviced by a private water supply well (this study) and a septic system.

1.2 **Objectives and Scope of Work**

The objective of this hydrogeological study is to demonstrate adequate water quantity and water quality to support the proposed development. To meet the project objective, the scope of work included the following:

- Construction of a temporary access road and drilling a bedrock supply water well;
- Completion of a 7-hour pumping test from the drilled water well, and collection of representative groundwater samples;
- Review of surficial and bedrock geology from regional mapping studies (i.e. Ontario Geological Survey mapping);
- Review of surrounding water well information from the MECP water well database; and
- Preparation of a final report summarizing the site conditions, geological and hydrogeological setting, and providing an interpretation of site-specific water quality and water quantity information.



2 SITE DESCRIPTION

2.1 Physical Setting

2.1.1 Site Location

The property is located at 8520 McArton Road, in the rural western portion of the City Ottawa near the community of Ashton. The legal description of the site is Part of Lot 4, Concession 12, Goulbourn Township.

The current property is 7.0 hectare (17.3 acre) in size and does not have any permanent structures. Topography at the site is relatively flat and is composed of agriculture fields and some wooded areas. Manion Corners (Long Swamp) Wetland Complex is located along the east – northeast portion of the property, adjacent to Highway 7 and Upper Dwyer Hill Road (Figure A.2, Appendix A).

2.1.2 Surrounding Properties and Land Use

The property is primarily surrounded by agricultural fields and woodland to the north and west. There are several rural residential lots located along McArton Road, between Upper Dwyer Hill Side Road to the north and Lowe Road, to the south.

The location of the property relative to surrounding land uses is shown on Figure A.2, Appendix A.

2.2 Nearby MECP Water Well Records

The MECP Water Well Information System (WWIS) and on-line mapping tool (accessed July 2018) were reviewed to provide geological and hydrogeological information for the site. A total of nine water well records were identified within 500 m of the site.

Figure A.3 shows the location of MECP water wells referenced in this report. A summary of well record information is included in Table 1, Appendix B. Copies of the well records within 500 m of the site are included in Appendix C.

2.3 Geological Setting

2.3.1 Surficial Geology

The site is located within the Limestone Plains physiographic region, as mapped by Chapman and Putnam (1984), which is characterized by shallow soil cover overlying limestone bedrock. The Ontario Geological Survey (2010) identifies organic deposits covering the central and southeastern portion of the property and silty to sandy till covering most of the property. Recent drilling of six boreholes completed as part of a geotechnical investigation (Terrepex, 2019) confirmed the presence of thin topsoil and sandy till layers at the site, with depth to bedrock ranging from 0.4 to 2.4 meters below ground surface.

Surficial geology (based on OGS, 2010) for the site and surrounding area is illustrated on Figure A.4, Appendix A.



2.3.2 Bedrock Geology

The bedrock geology at the site is mapped as the Gull River Formation (Armstrong and Dodge, 2007). Williams (1991) describes the Gull River Formation as crystalline limestone with shaley partings and minor interbedded limestone and silty dolostone. The mapped geology is consistent with MECP well records for the area, which report bedrock as limestone, sandstone and sandy dolostone.

A bedrock geology map is presented on Figure A.5, Appendix A.

2.4 Hydrogeology

2.4.1 Overburden Aquifer

There is minimal overburden cover in the area, therefore it is not likely that an overburden aquifer is sustainable. All wells within 500 m are installed with steel casing through the overburden and groundwater is supplied from the underlying bedrock aquifer.

2.4.2 Bedrock Aquifer

All MECP water wells within 500 m, as summarized in Table 1, are completed within the bedrock. The average depth to bedrock is approximately 1 m BGS; however, some of the records reported depth to bedrock of zero and describe the upper unit as broken rock. Average well depth is 39.3 m and varies from 21.3 to 68.6 m.

The bedrock aquifer, consisting of limestone and sandy dolostone, is the primary aquifer within the study area. In many cases, bedrock aquifers are dominated by flow through fractures in the rock. The depth to water bearing zones (i.e. fractured zones) was identified on the water well records at depths ranging from 19.8 to 42.7 m, with an average depth of 30.5 m.

2.4.3 Groundwater Flow Direction

In general, shallow groundwater flow follows ground surface elevation/topography and is influenced by areas of groundwater recharge and discharge. Based on a review of surficial features, it is likely that shallow groundwater flows east, toward the wetland complex. The site is located within the Rideau Valley Conservation Authority boundary, near the drainage divide between the Mississippi River and Rideau River. It is anticipated that deeper groundwater flow is to the east (i.e. the Rideau River).



3 METHODOLOGY

3.1 Estimation of Water Demand

Estimation of water demand for the proposed bird care center at 8520 McArton Road was completed by Alfa Alliance Engineering Inc. Based on design specifications for the proposed development, the estimated daily demand is 4.5 to 7.4 cubic meters per day (3.1 to 5.2 L/min or 0.83 to 1.36 gal/min), with a peak flow rate demand of 132 liters per minute (35 gal/min). These values are based on 66 water supply fixture units (WSFU).

3.2 Utility Locates

Public utility locates for the 8520 McArton Road property were requested from Ontario One-Call by Geofirma and were fulfilled by Promark on December 6, 2019. No underground utilities (Ottawa Hydro, Hydro One) were identified in the locate package provided by Promark.

3.3 Water Well Drilling

Drilling was completed on January 16, 2020, by Air Rock Drilling, a MECP licensed water well contractor, under the supervision of Geofirma personnel. A 154 mm (~6 inch) diameter borehole was drilled to a depth of 53.3 m BGS using an air-rotary drilling rig. 170 mm outer diameter (OD) steel casing was installed and cemented from 12.8 m BGS to ground surface. Top of bedrock was encountered at 2.1 m BGS.

A well record was submitted to the MECP by Air Rock on behalf of the OVWBCC and is provided in Appendix D. The well construction details are summarized in the following table:

Water Supply Well Details - 8520 McArton Road				
Drilled Date	January 16, 2020			
Casing Depth 12.8 m BGS				
Casing Diameter	170 mm (outer diameter)			
Casing Diameter	164 mm (inner diameter)			
Casing Stickup	0.49 m AGS			
Borehole Diameter	154 mm			
Drilled Depth	53.3 m BGS			
Static Water Level	4.04 m BGS (Feb 4, 2020)			

3.4 Water Well Pumping Test

A 7-hour pumping test was completed in the drilled well at 8520 McArton Road by Geofirma personnel on February 4, 2020. The duration of the pumping test was extended from 6 hours to 7 hours account for a pumping rate (~122 L/min) lower than the estimated peak water demand (132 L/min). The total volume of water produced during the 7-hour test was equivalent to the volume that would be produced in 6 hours at the higher pumping rate.



3.4.1 Test Equipment and Set-up

The pumping test was completed using a submersible pump that was lowered to 27.4 m below ground surface (m BGS). Water produced during the test was discharged from a hose approximately 30 m from the well head, such that discharged water would not impact the results of the test.

A pressure transducer (Solinst Levelogger) was lowered to 22 m below top of well casing (m BTOC) to record water levels in the well during the pumping test. A second pressure transducer (Solinst Barologger) was installed at the well head to measure and account for barometric pressure change during the test.

3.4.2 **Test Procedure**

The depth to water was measured at 4.04 m BTOC prior to pumping. The pumping test was started at 8:37 am. For the purpose of this pumping test, the measured water level prior to the test is assumed to represent ambient static conditions. Weather conditions during the test were cold and dry, with a daily high of 5 degrees Celsius and no precipitation.

A pumping rate of ~122 L/min (~32.2 US gpm) was used for the test, which was lower than the anticipated peak water demand (132 L/min). After consulting with the City of Ottawa, a flow rate lower than the peak water demand was deemed acceptable, provided that the duration of the test was extended so that the total volume of water produced was equivalent to the volume that would be produced in 6 hours at the higher pumping rate.

Flow rate measurements were collected periodically during the test to confirm flow rate by measuring the time to took to fill a graduated 1000 L water tote. Manual water level measurements were also collected using an electronic water level tape to confirm the transducer measurements and correct for logger drift, if required. The water level in the well was monitored for an hour after the pump was shut off until it recovered to pre-test static conditions.

Manual water level and flow rate measurements collected during the test are provided in Tables 2 and 3, Appendix B.

3.4.3 Measurement of Field Parameters

A Horiba U-52 multimeter was used to collect field measurements of groundwater temperature, pH, conductivity, oxidation-reduction potential (ORP), turbidity and dissolved oxygen (DO). Measurements were collected at regular intervals during the pumping test in a bucket filled with water discharged from the borehole.

Chlorine residual and water colour were also tested in the field prior to sampling using a CHEMets® chlorine kit and a HACH Colorimeter, respectively.

A summary of the field parameter measurements is provided in Table 4, Appendix B.

3.4.4 **Groundwater Sample Collection**

Two representative groundwater samples were collected during the pumping test: one at 3 hours and second collected in the last hour of the pumping test. The samples were collected from the discharge



using a 10 L bucket, which was disinfected with a 10% bleach solution prior to sample collection. Chlorine residual was tested prior to collection of each sample and was reported as 0 mg/L for both samples.

Upon collection, the samples were stored in a cooler and shipped to Paracel Laboratories Ltd. following standard chain-of-custody and Geofirma QA/QC procedures. The samples were analyzed by Paracel for a suite of drinking water parameters generally referred to as the "Sub-division Package" that includes select anions, general inorganics, metals, and bacteriological parameters.



4 HYDROGEOLOGICAL ASSESSMENT

4.1 Review of MECP Water Well Records

A review of the MECP WWIS was completed to determine average depth of well, depth to bedrock surface and static water level, as well as the recommended depth of pump and pumping rates, as determined by the driller during well completion. In total, 9 well records were identified within the 500 m buffer zone of the proposed development. Key details from these 9 well records are summarized as follows:

Summary of MECP Well Records within 500 m of the Site

Well Record Parameter	Depth of Well (m)	Depth to Bedrock (m)	Static Water Level (m)	Recommended Pump Intake Depth (m)	Available Drawdown (m)	Recommended Pumping Rate (L/min)
Number of Records	9	9	9	9	9	9
Average (mean)	39.3	0.8	7.9	32.4	24.6	29.0
Range	21.3 – 69.6	0.0 – 4.0	1.8 – 15.8	15.9 – 53.4	10.1 – 40.9	18.9 – 56.8

Table 1, Appendix B, contains a more comprehensive list of well completion details for each individual well record within the buffer zone.

4.2 Water Quantity

Based on the results of the pumping test, presented in Appendix E, the well yield is enough to support the estimated peak water demand of 35 gal/min (132 L/min). A plot showing the manually measured and transducer recorded water levels during the pumping test and recovery is provided in Appendix E, Figure E.1.

The pumping test data were analyzed using AQTESOLV (version 4.5), a well test analysis software developed and sold by HydroSOLVE Inc. Using AQTESOLV, the transmissivity of the aquifer is estimated to be 4.2x10⁻³ m²/s (361 m²/day). Figure E.2, Appendix E, shows the measured drawdown during pumping test and the fitted curve from AQTESOLVE using the Theis analytical solution. During the test, the maximum measured drawdown of the well was 1.01 m (to 5.05 m BTOC). The water level in the well recovered to 99% of the pre-test static condition 60 minutes after terminating the pumping test.

A forward simulation was also completed in AQTESOLV to predict the drawdown from the well at a pumping rate equal to the estimated peak water demand (132 L/min) using the transmissivity and storativity estimated from the pumping test data. The forward simulation (Figure E.3, Appendix E) indicates that at a pumping rate of 132 L/min, drawdown in the well would stabilize at approximately 1.05 m after approximately 6 hours of pumping.



4.3 Water Quality

The results of the two water quality samples (3h and 6.5h into pumping test) are presented in Table 5, Appendix B. Complete laboratory reports are included in Appendix F.

4.3.1 Health-Based Standards

Based on a review of the Table 5, the following observations can be made with respect to health-based bacteriological, chemical and physical parameters outlined in Procedure D-5-5 (MECP, 1996):

- Total coliforms, E.Coli, and fecal coliforms were not detected (0 CFU/100 mL) in both samples collected during the pumping test; and
- Fluoride, nitrate and nitrite are reported below the laboratory detection limit.

4.3.2 Aesthetic Objectives and Operational Guidelines

Comparison of the water quality results in Table 5 to aesthetic, analytical and indicator parameters outlined in Procedure D-5-5 and the ODWS indicate the following:

- Hardness, reported at 283 mg/L and 290 mg/L, is above the operation guideline (OG) range of 80-100 mg/L. The ODWS states that hardness values greater than 200 mg/L, but less than 500 mg/L, are considered poor but tolerable. Hardness is easily treated with standard water softener systems (see Section 4.3.3 for further discussion).
- Iron, reported at 0.4 mg/L for both samples, is just above the aesthetic objective (AO) of 0.3 mg/L.
 Iron concentrations up to 5 mg/L are easily treated with a water softener or manganese greensand filter.
- Laboratory reported colour was 12 and 20 TCU for the 3-hour and 6-hour samples, respectively.
 However, colour was measured at 0 TCU for both samples in the field and there was no visible
 colour at the time of sampling. For these reasons, the elevated colour reported in the lab samples
 is attributed to the elevated level of iron in the water, which decreased during the pump test, and is
 considered acceptable and treatable.
- The concentration of all other aesthetic, analytical and indicator parameters satisfy applicable criteria.

4.3.3 Corrosion / Encrustation Potential - Langelier Saturation Index (LSI) and Ryznar Stability Index (RSI)

The Langelier Saturation Index (LSI) and the Ryznar Stability Index (RSI) are commonly used to assess the potential for water to dissolve or deposit calcium carbonate. LSI is more commonly used, especially with process water in cooling towers.

Hardness is a term used to describe the mineral content of the water and more specifically the levels of cations in the water (mostly due to calcium and magnesium). The water collected during the pumping test is considered to be very hard with concentrations of 283 mg/L and 290 mg/L compared to the recommended operational guideline of 80-100 mg/L, therefore treatment using a water softener would be required.

The Langelier Saturation Index (LSI) is a calculation that provides insight into how balanced the water is in terms of minerals, whereby water with a negative LSI is considered to be corrosive and water with

a positive LSI is considered to be scale forming. Generally, an LSI value between -0.3 and +0.3 is the widely accepted range with a value of 0 being ideal and represents perfectly balanced water.

The LSI can be calculated using a combination of factors involving pH, temperature, calcium hardness, total alkalinity and total dissolved solids (TDS) concentration. Appendix G summarizes the calculations of the LSI index for groundwater during the pumping test at 8520 McArton Road, resulting in a value of -0.88 which represents slightly corrosive water. Corrosive water will deteriorate faucets and appliances faster compared to less corrosive water. Additionally, corrosive water will deteriorate copper pipes more easily and therefore PEX piping may be preferred for new constructions.

Water with high hardness values is typically treated using water softeners that use some form of salt to remove calcium and magnesium by ion exchange with sodium. The by-product of water softeners is backwash water generated during the regeneration process which contains high levels of sodium chloride and calcium and magnesium. This backwash water may have detrimental impacts on septic system and tanks. Best management practices to minimize the impact of discharging this backwash water include discharging it to the subsurface (i.e. dry well) at least 30 m away from a water supply well and do not discharge into a septic system.



5 IMPACT ASSESSMENT

5.1 Hydrogeological Sensitivity

A review of MECP water wells within the study area (500 m buffer) and recent geotechnical drilling indicate that the thickness of soil cover ranges from 0 to 4 m near the study site, with most well records (8 of 9) identifying less than 2 m of overburden cover. At the wellhead, overburden is 2.1 m thick and is composed of sand and cobbles. Given the thin overburden cover (i.e. less than 2 m thick) the site is considered to be hydrogeologically sensitive, meaning the bedrock aquifer is potentially vulnerable to impacts from pathogens and chemicals from surrounding land uses and/or septic effluent disposal beds.

Surrounding land uses, which are primarily rural residential and agricultural, with a wetland complex to the south and east, are considered to be of minimal concern to potentially degrade water quality from the drilled bedrock well at the site. Furthermore, the water quality results from 8520 McArton Road were acceptable and nitrate impacts negligible, suggesting no current impacts to the bedrock aquifer from surrounding land use.

5.2 Septic Assessment

5.2.1 Estimated Sewage Flow

Based on the estimated average daily water demand (Section 3.1) of 4.5 to 7.4 m³/day, this equates to approximately 4,500 to 7,400 L of water pumped per day and potentially being disposed of through the on-site septic system. While considered a very high estimate, the upper value remains below the threshold (10,000 L/day) requiring an Environmental Compliance Approval (ECA) with the MECP. As such, an assessment of nitrate attenuation is appropriate by following the progressive three step assessment process outlined in Guideline D-5-4 (MECP, 1996b), whereby if the requirements of a given step are not satisfied, the assessment needs to proceed to the next step. The three-step process includes:

Consideration	Requirements to Meet	Applicable for 8520 McArton Rd	
Step 1 – Lot Size Minimum lot size of 1 ha (average) if can demonstrate area is not hydrogeologically sensitive		No Lot size is > 1ha but area is deemed to be hydrogeologically sensitive	
Step 2 – System Isolation	Areas were septic system is hydrogeologically isolated from the potable water source (e.g. City defines as >10 m clay extending >100 m downgradient)		
Step 3 – Contaminant Attenuation	If above two considerations are not met, must asses risk of individual sewage systems to cause nitrate-nitrogen in groundwater > 10 mg/L at the development property boundary	Yes	



Due to the fact that this site is deemed to be hydrogeologically sensitive, a predictive assessment of nitrate attenuation within the soil is appropriate and the following sections describe this assessment.

5.2.2 Background Nitrate Concentrations

No nearby wells were sampled and therefore no additional information on background nitrate concentrations were available for this study. Without additional data, background nitrate (NO₃) concentrations can be estimated by the using laboratory values during the pumping test, which were reported as below the laboratory method detection limit (MDL) of 0.1 mg/L. As such, a value 0.05 mg/L representing 50% of the laboratory MDL was used for the purposes of this report to represent background nitrate conditions.

5.2.3 Nitrate Attenuation Assessment

Appendix H provides a copy of the Site Plan for the proposed development. Future construction will involve several design elements that will create impermeable areas, including the future building (~622 m²), paved parking lot (~568 m²) and paved driveway and loading dock (~600 m²). In addition, an outdoor aviary (fly area outdoor porch) is designed (~380 m²). These areas (~2,170 m²) have the potential to reduce infiltration into the groundwater supply and therefore are removed from the total area available for infiltration as part of the calculations.

The annual moisture surplus was determined following the Thornthwaite method (see Ponce, 1996), using average monthly temperature and precipitation values from Environment Canada, for the Appleton monitoring station located approximately 8 km southwest of the subject property. A summary of climatic data and calculations completed using the Thornthwaite model is provided in Appendix I.

Appendix I also includes assumptions and summary calculations for post-development water budget at the subject property and nitrate dilutions calculations to assess the suitability of the site to support a conventional septic system. The following parameters summarize the water budget estimate for 8520 McArton Road post development conditions:

Parameter	Value	Rational
Average Annual Precipitation (per m²)	873 mm	Environment Canada climate data for Appleton 1993-2019
Annual Evapotranspiration (per m²)	595 mm	Thornthwaite (Appendix H)
Annual Water Surplus (per m²)	279 mm	Thornthwaite (Appendix H)
Infiltration Factor	0.68	calculated (Appendix I)
Total Site Area	69,940 m ²	Site Plan
Permeable Site Area	67,770 m ²	Site Plan - discussed above
Annual Water Surplus (for site)	19,499 m³/yr	Water budget calculations (Appendix I)
Total Annual Infiltration (for site)	12,848 m ³ /yr (190 mm/m ²)	Water budget calculations (Appendix I)
Total Estimated Runoff (for site)	6,240 m ³ /yr (89 mm/m ²)	Water budget calculations (Appendix I)



These estimates are supported by the observation of a thin soil cover consisting of sandy, clayey till surficial soils identified across much of the and relatively flat topography.

According to MECP Guideline D-5-4, a screening tool to look at the maximum allowable flow for an industrial or commercial development is to assume 1/3 of the available infiltration. Following this process, the maximum allowable flow for the septic system is approximately 4,283 m³/year which equates to approximately 11,733 L/day. This is significantly greater than the conservative estimate of 4,500 to 7,400 L/day based on average daily estimated water demand and therefore is acceptable.

As outlined in Appendix I, the cumulative nitrate impact for the commercial development proposed for 8520 McArton Road is estimated to be as high as 6.95 mg/L. Further, taking estimated background nitrate concentrations (Section 5.2.2) into account, the total nitrate loading is estimated to be well below the provincially mandated limit of 10 mg/L at the down-gradient property boundary. As such, Geofirma concludes that the proposed development will not have unacceptable impacts to the potable water supply.

Potential Sources of Contamination 5.3

Given that the surrounding land use (within 500 m of the site) is residential and agricultural, potential sources of contamination to domestic water quality in the vicinity of the site include contamination due agricultural runoff (fertilizers, manure, pesticides etc.). Furthermore, road salting activities can contribute to elevated sodium and chloride concentrations in groundwater. These potential sources of contamination are mitigated by the installation of surface casing through the overburden and sealed into bedrock.

5.4 **Cumulative Impacts**

There are no anticipated additional impacts, or cumulative impacts, on water quality to groundwater users in the vicinity of the site likely to arise from the proposed development given that groundwater flows toward the wetland and there are no downgradient receptors. Based on a review of MECP water well records, there appears to be adequate water quantity and potential well interference from the additional water supply well is unlikely to cause significant impacts on the baseflow to the local environment or available drawdown of nearby wells.

5.5 Source Water Protection

The site is located within the Mississippi-Rideau Source Protection Region. The property is not within any well head protection zones or mapped as highly vulnerable; however, best management practices should be observed to protect groundwater quality. Additional information can be found at the following link:

https://www.mrsourcewater.ca/en/protect-your-drinking-water/protecting-regional-groundwater

5.6 **Development Considerations**

Based on the results of this study, the following site-specific measures are recommended to minimize potential impact to the bedrock aguifer at 8520 McArton Road resulting from thin soil conditions. Overall, the subject property is considered to be suitable for the proposed development and the



targeted bedrock groundwater supply is deemed to have sufficient quality and quantity for the proposed water demand. Further, the on-site sewage disposal needs can be accommodated with standard Class 4 sewage systems consisting of a septic tank and fully raised leaching bed, as per Part 8 of the Ontario Building Code.

Water Supply Well

- Keeping an increased the separation distance between well and septic bed from 15 m to 30 m;
- Installation of a permanent pump system in the well by a MECP-licensed well driller in accordance with Ontario Regulation 903;
- Maintain well design specifications as per Ontario Regulation 903 including sloping ground surface away from the wells to avoid water flowing toward well, adequate stickup above ground surface, proper well cap, etc;

Water Treatment

- While there is no evidence of bacteriological contamination, the use of disinfection, such as an ultraviolet (UV) system, may be desired for any potable water;
- The slightly corrosive nature of the water, based on the LSI and RSI calculations, while not a major issue, may warrant further assessment and possible treatment such as a neutralizing filter;
- For aesthetic reasons, water treatment such as softening or greensand filters may be desired;

Septic System

- The septic bed should be sited in an area of thicker soil cover, if possible, and may require import of additional suitable fill material;
- Due to the soil conditions a clay seal may be required below the septic leaching bed to ensure additional isolation from the underlying soil and bedrock; and,
- Ensure the septic bed is located downgradient from the well head (i.e. southeast of the well).

Figure A.6, Appendix A, provides a generalized lot development plan, showing the placement of the well and recommended location of the septic system. Note that installation of the well and septic shall, at a minimum, be constructed in accordance with O.Reg. 903 and the Ontario Building Code (Part 8), respectively. Appendix H provides a copy of the draft proposed Site Plan.



6 CONCLUSIONS AND RECOMMENDATIONS

A hydrogeological study was completed to support a proposal for construction of a wild bird care center on a 7.0 hectare (17.3 acre) property at 8520 McArton Road, Ashton, ON. The study included a review of site geology and hydrogeology, attaining public utility locates, drilling and installation of a bedrock water well, completion of a 7-hour pumping test, and collection of a representative water sample from the drilled well.

Based on the study, the following conclusions and recommendations are be made:

Water Quantity

- Well yield is very good and considered acceptable for the anticipated future water demand based on peak flow rate estimate for the proposed development (approximately 35 gallons per minute);
- The calculated transmissivity of the aquifer is 361 m²/day. During the pumping test (at 122 L/min) the maximum observed drawdown was approximately 1.01 m, to a depth of approximately 5.05 m BTOC. Within 60 minutes, the well had recovered to 99% of the inferred static water level (4.04 m BTOC);

Water Quality

- Water quality is acceptable, with no health-related parameters exceeding applicable Ontario Drinking Water Standards (ODWS);
- Hardness and iron are reported above the operational guideline and aesthetic objective but are tolerable if left untreated. Both hardness and low concentrations of iron are easily treatable with standard water softener systems;
- LSI calculations indicate slightly corrosive water that is tolerable if left untreated by may warrant consideration of a neutralizing filter;

Water Supply Well

- A pump system in the well should be installed in accordance with Ontario Regulation 903 by an MECP-licensed well driller/installer;
- Maintain proper water well design construction in accordance with Reg. 903 including sloping ground surface away from well to discourage water flowing towards or ponding at well, maintaining adequate stickup, vermin proof well cap, etc;

Sewage System Design

- An assessment of nitrate attenuation following MECP Guideline D-5-4 indicates that the property size and conditions are suitable to support a conventional septic system as per the proposed development. Predicted nitrate-nitrogen levels are expected to be less than 7 mg/L according to these calculations.
- The on-site sewage system should be designed and installed by a licensed contractor in accordance with Ontario Building Code (Part 8) specifications. A traditional Class 4 sewage system consisting of a septic tank and leaching bed is acceptable for use at the site.



- The leaching bed should be placed southeast (downgradient) of the well head and the separation distance between the well and bed should be a minimum of 30 m, while meeting all other setback requirements set out in the Building Code.
- The septic bed should be sited in an area of thicker soil cover, if possible, and may require import
 of additional suitable fill material.
- A clay seal may be warranted below the septic bed to increase isolation between the sewage output and the underlying bedrock aquifer.



7 REFERENCES

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8 CLOSURE

This report has been prepared for the exclusive use of the owners of 8520 McArton Road using a methodology for conducting a hydrogeological study that is acceptable within the profession. Data obtained from sampling represents the conditions at the time of sampling and are subject to variability in the future.

Geofirma Engineering Ltd. has exercised professional judgment in collecting and analyzing the information and in formulating recommendations based on the results of the study. The mandate at Geofirma is to perform the given tasks within guidelines prescribed by the client and with the quality and due diligence expected within the profession. No other warranty or representation expressed or implied, as to the accuracy of the information or recommendations is included or intended in this report.

Geofirma Engineering Ltd. hereby disclaims any liability or responsibility to any person or party, other than the party to whom this report is addressed, for any loss, damage, expense, fines or penalties which may arise or result from the use of any information or recommendations contained in this report by any other party. Any use of this report constitutes acceptance of the limits of Geofirma's liability. Geofirma's liability extends only to its client and only for the total amount of fees received from the client for this specific project and not to other parties who may obtain this report.

Respectfully submitted,

Geofirma Engineering Ltd.

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Sean Sterling, M.Sc., P.Eng., P.Geo. Principal / Manager of Geoscience

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Hydrogeological Study 8520 McArton Road, Ottawa, Ontario

APPENDIX A

Site Figures

Figure A.1 Site Location

Figure A.2 Site Layout

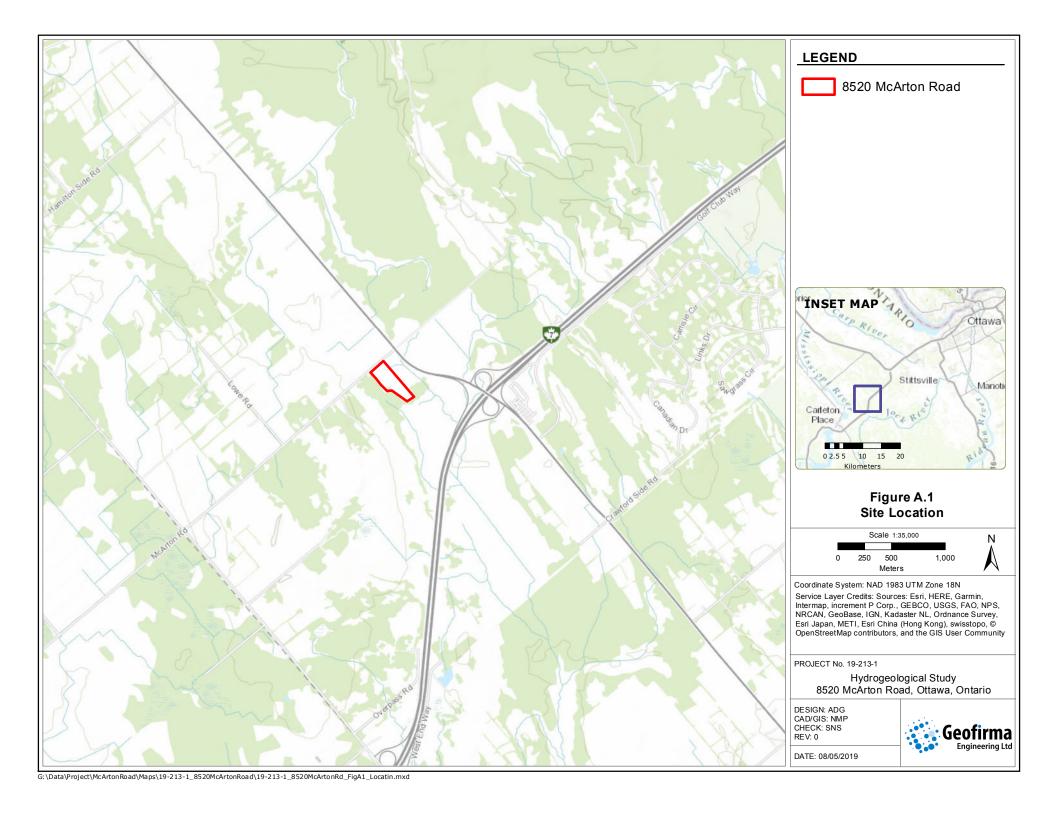
Figure A.3 MECP Water Wells

Figure A.4 Surficial Geology

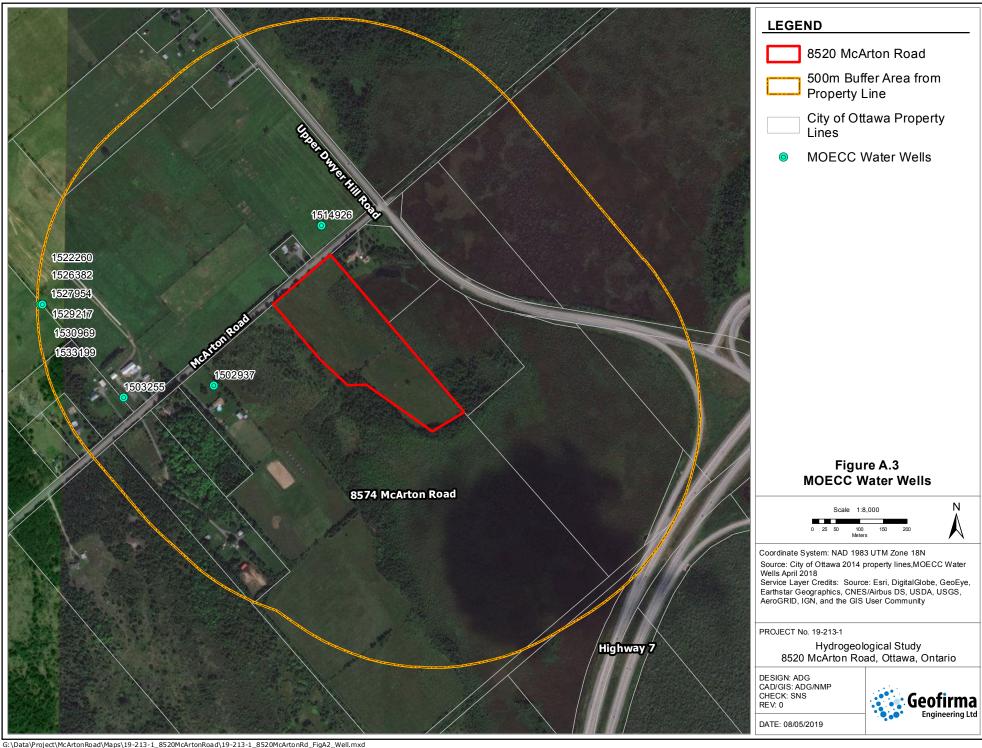
Figure A.5 Bedrock Geology

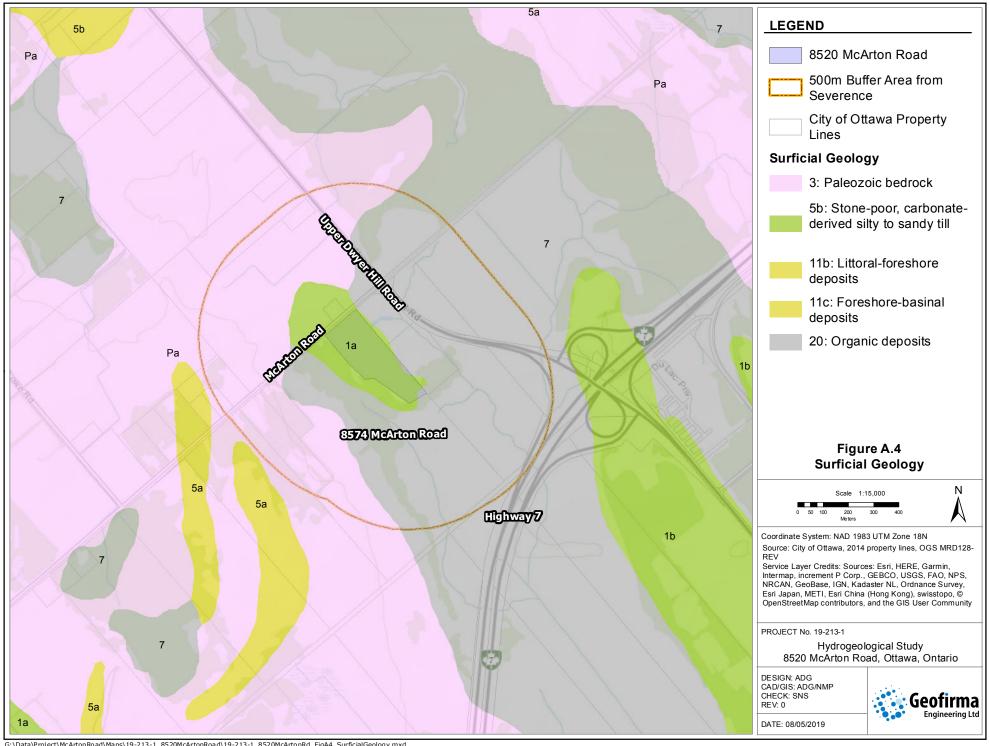
Figure A.6 Proposed Site Development Plan

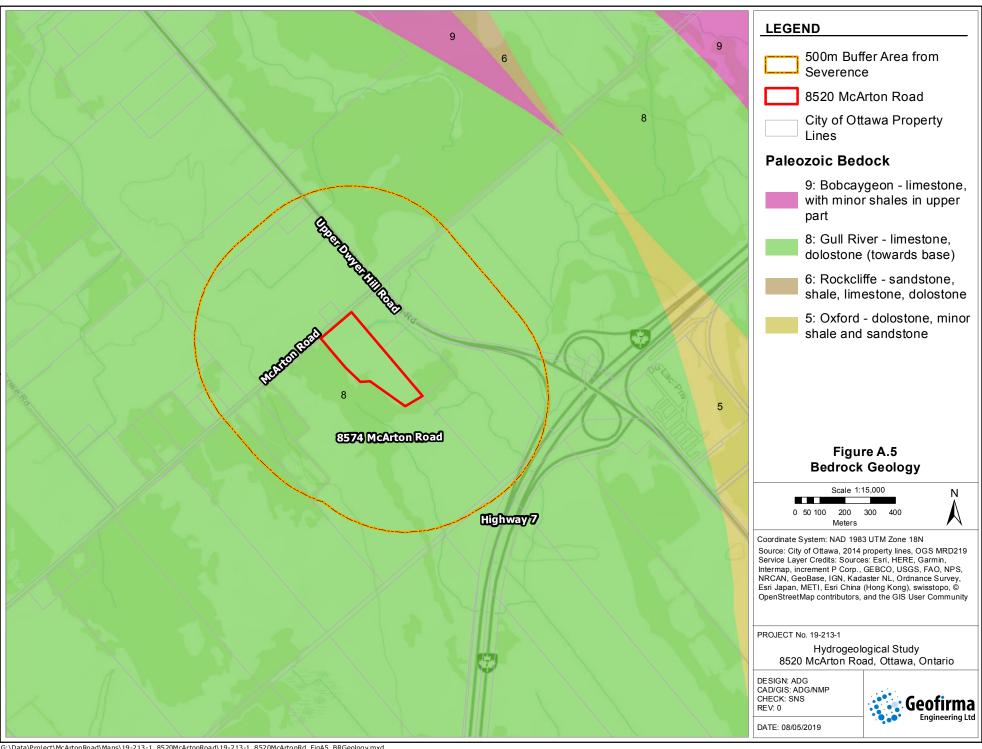


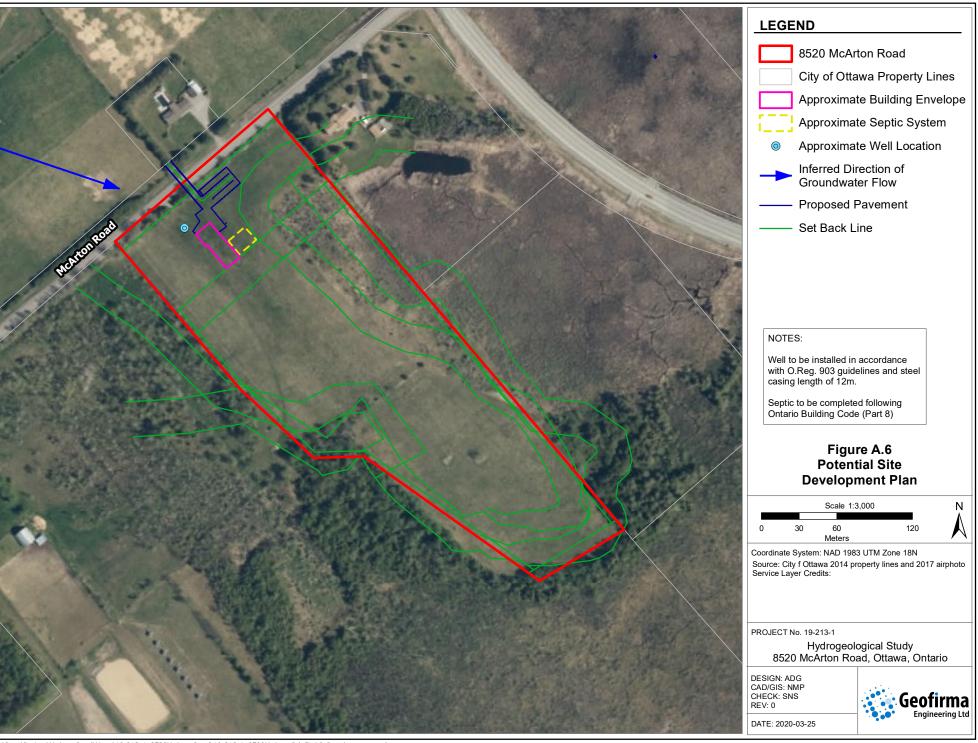












Hydrogeological Study 8520 McArton Road, Ottawa, Ontario

APPENDIX B

Tables

Table 1	Summary of MECP Water Well Data Within 500m of Site
Table 2	Summary of Measured Water Levels
Table 3	Summary of Measured Flow Rates
Table 4	Summary of Field Readings
Table 5	Groundwater Quality Analytical Results



Table B.1 - Summary of MOECC Water Well Data within 500 m of the Site

MOECC WWIS Well ID	Completion Date (dd/mm/yyyy)	Well Depth (m)	Depth to Bedrock (m)	Static Water Level (m)	Depth to Found Water ¹ (m)	. .	Recommended Pump Intake (m)	Available Drawdown (m)	Recommended Pumping Rate (L/min)
1502937	1962-07-14	33.5	0	5.5	29.0	2.7	27.4	21.9	18.9
1503255	1968-04-10	24.4	0.6	6.1	19.8	7.6	21.3	15.2	18.9
1514926	1975-09-04	21.3	4	5.8	20.1	7.6	15.9	10.1	18.9
1522260	1987-07-01	45.7	0	6.1	42.7	6.7	36.6	30.5	37.9
1526382	1992-06-19	43.3	0.3	12.2	41.8	6.1	39.6	27.4	56.8
1527954	1994-06-17	24.4	0.6	4	22.9	6.7	18.3	14.3	26.5
1529217	1996-07-11	48.5	1.8	15.8	37.2	6.1	36.6	20.8	37.9
1530969	1999-10-26	44.2	0	1.8	21.0	5.5	42.7	40.9	26.5
1533199	2002-09-10	68.6	0	13.4	39.6	6.9	53.4	40.0	18.9
Statistics	Statistics								
Numbe	er of Records	9	9	9	9	9	9	9	9
Aver	age (Mean)	39.3	0.8	7.9	30.5	6.1	32.4	24.6	29.0
M	laximum	68.6	4.0	15.8	42.7	7.6	53.4	40.9	56.8
N	1inimum	21.3	0.0	1.8	19.8	2.7	15.9	10.1	18.9

Notes:

Data collected from the MOECC WWIS, accessed July 2018

1 - Depth to found water is presented as first occurance of found water. In some cases, water bearing zones were noted at multiple depths.



Table B.2 - Summary of Measured Water Levels

Elapsed Time (sec)	Water Level (m BTOC)	Comments			
Start of Pumping Test @ 8:37 AM; Assumed Static WL = 4.04 m BTOC					
Pumping Water Levels					
60	4.689				
140	4.780				
170	4.795				
210	4.820				
240	4.830				
300	4.842				
360	4.855				
420	4.867				
600	4.889				
960	4.900				
1260	4.914				
1920	4.925				
2460	4.930				
3000	4.935				
3600	4.940				
4260	4.944				
5460	4.955				
6000	4.955				
6660	4.958				
8220	4.960				
9000	4.963				
10020	4.968				
10860	4.969				
13920	4.976				
14760	4.980				
17100	4.985				
19860	4.990				
21780	4.994				
24840	5.004				
26160	5.005				
Recovery Water Levels					
26687	4.790				
26692	4.640				
26697	4.600				
26702	4.550				
26707	4.500				
26722	4.500				
26737	4.400				
26742	4.390				
26747	4.380				

Prepared by: CAM Reviewed by: Date: 2020-02-10



Table B.2 - Summary of Measured Water Levels

Elapsed Time (sec)	Water Level (m BTOC)	Comments
26752	4.370	
26757	4.360	
26762	4.350	
26767	4.340	
26772	4.330	
26777	4.320	
26782	4.310	
26787	4.300	
26802	4.280	
26812	4.270	
26817	4.260	
26827	4.250	
26837	4.240	
26852	4.230	
26817	4.220	
26897	4.210	
26917	4.220	
26947	4.190	
26982	4.180	
27012	4.170	
27067	4.160	
28234	4.110	
28530	4.085	
28811	4.079	
28958	4.075	
29377	4.070	
30258	4.060	
30845	4.050	

Notes:

Water level measured using an electronic water level tape m TOC = meters below top of casing



Table B.3 - Summary of Measured Flow Rates

Elapsed Time (sec)	Flow Rate (L/min)	Comments
206	130	
206		
252	130	
292	150	
345	113	
396	118	
446	120	
493	128	
548	109	
1512	133	
1560	125	
1610	120	
1661	118	
1712	118	
1761	122	
1812	118	
1862	120	
3834	120	
3883	122	
3931	125	
4032	119	
4084	115	
4133	122	
4182	122	
6270	125	
6318	125	
6370	115	
6420	120	
6471	118	
6519	125	
6570	118	
6619	122	
9599	122	
9646	128	
9697	118	
9748	118	
9798	120	
9848	120	
9899	118	
14936	130	
14985	122	
15034	122	
15086	115	

Prepared by: CAM Reviewed by: Date: 2020-02-10



Table B.3 - Summary of Measured Flow Rates

Elapsed Time (sec)	Flow Rate (L/min)	Comments		
15136	120			
15186	120			
15236	120			
19445	118			
19493	125			
19540	128			
19591	118			
19641	120			
19693	115			
19743	120			
24463	125			
24508	133			
24558	120			
24609	118			
24658	122			
24708	120			
24760	115			

Notes:

Flow rate calculated by measuring the time it took to fill a graduated 1000L tote



Table B.4 - Summary of Field Readings

Elapsed Time (h:mm)	Temperature (°C)	рН	Oxidation-Reduction Potential (mV)	Electrical Conductivity (mS/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Chlorine (ppm)	Colour (TCU)	Sample Collected
0:41	6.91	5.84	86	0.690	3.6	4.30			
0:45	7.58	6.45	49	0.653	0.0	4.04			
1:10	7.75	6.76	36	0.651	0.0	2.17			
1:30	7.77	6.91	13	0.643	0.0	2.18			
2:30	7.93	7.02	6	0.643	0.0	2.35			
3:05	8.21	7.08	1	0.635	0.0	2.94	0.0	0.0	Yes
3:50	8.31	7.10	-5	0.639	0.0	2.84			
5:15	8.26	7.14	-7	0.641	0.0	2.72			
5:56	8.17	7.06	-4	0.637	0.0	2.26			
6:30	8.10	7.11	-9	0.637	0.0	2.33	0.0	0.0	Yes

Note:

Measurements collected using Horiba U-52 multimeter Chlorine Measured using CHEMets Chlorine Kit Colour Measured using HACH Colorimeter



Table B.5 - Groundwater Quality Analytical Results

				- Ontario Drin	8520 McArton Well	8520 McArton Well		
Parameter	Units	MDL	Standards, Objectives and Guidelines			(3-hour)	(6-hour)	
			MAC	AO	OG	(o nour)	(o nour)	
Microbiological Parameters								
E. Coli	CFU/100 mL	1	0 CFU/100 mL		-	ND (1)	ND (1)	
Fecal Coliforms	CFU/100 mL	1				ND (1)	ND (1)	
Total Coliforms ¹	CFU/100 mL	1	0 CFU/100 mL			ND (1)	ND (1)	
Heterotrophic Plate Count	CFU/ml	10			-	ND (10)	ND (10)	
General Inorganics								
Alkalinity, total	mg/L	5		500 mg/L		288	288	
Ammonia as N	mg/L	0.01				0.06	0.05	
Dissolved Organic Carbon	mg/L	0.5		5 mg/L		2.3	1.4	
Colour	TCU	2		5 TCU		<u>12</u>	<u>20</u>	
Conductivity	μS/cm	5				638	636	
Hardness	mg/L				80-100	<u>283</u>	<u>290</u>	
pН	pH Units	0.1			6.5-8.5	7.7	7.8	
Phenolics	mg/L	0.001				ND (0.001)	ND (0.001)	
Total Dissolved Solids	mg/L	10		500 mg/L	-	338	338	
Sulphide	mg/L	0.02		0.05 mg/L		ND (0.02)	ND (0.02)	
Tannin & Lignin	mg/L	0.1				ND (0.1)	ND (0.1)	
Total Kjeldahl Nitrogen	mg/L	0.1			-	0.1	0.1	
Turbidity	NTU	0.1		5 NTU		2.8	3.5	
Anions								
Chloride	mg/L	1		250 mg/L		19	20	
Fluoride	mg/L	0.1	1.5 mg/L			ND (0.1)	ND (0.1)	
Nitrate as N	mg/L	0.1	10 mg/L		-	ND (0.1)	ND (0.1)	
Nitrite as N	mg/L	0.05	1 mg/L			ND (0.05)	ND (0.05)	
Sulphate	mg/L	1		500 mg/L		19	19	
Metals								
Calcium	mg/L	0.1				77.9	80.7	
Iron	mg/L	0.1		0.3 mg/L		0.4	0.4	
Magnesium	mg/L	0.2				21.4	21.5	
Manganese	mg/L	0.005		0.05 mg/L		0.027	0.026	
Potassium	mg/L	0.1				1.4	1.5	
Sodium	mg/L	0.2		200 mg/L		5.2	5.6	
Field Readings			-			· · · · · · · · · · · · · · · · · · ·		
Colour	TCU			5 TCU		0	0	
Chlorine Residual ²	mg/L					0	0	

Notes:

- 2 Chlorine residual measured on-site, prior to sample collection
- -- = Not analyzed/No criteria

NA = Not applicable

ND = Not detected above MDL

MDL = Method Detection Limit

ODWS = Ontario Drinking Water Standards, Objectives and Guidelines, June 2003, revised 2008.

MAC = Maximum Acceptable Concentration of health-based standards

AO = Aesthetic Objective for parameters that may impair taste, odour or colour of water

OG = Operational Guidelines for parameters that, if not controlled, may negatively effect treatment, disinfection or distribution of the water

Bold/Underline = Indicates parameter exceeds aesthetic objective or operational guideline
Bold/Highlight = Indicates parameter exceeds a maximum acceptable concentration



^{1 -} While the ODWO for total coliform is 0, for the purpose of studies completed under Guideline D-5-5 total coliform counts of less than 6 per 100 mL of sample (and 0 for E.coli and fecal coliforms) is indicative of acceptable water quality.

APPENDIX C

MECP Water Well Records



AUG 1 6 1962 UTM / 8 2 41/171/12/5 E ONTARIO SVATENO RESOURCES COMMISSION 5005875he Ontario Water Resources Commission Act Township, Village, Town or City Date completed **Pumping Test** Casing and Screen Record Inside diameter of casing 6 4 Static level Total length of casing 9 Test-pumping rate Pumping level. Type of screen Duration of test pumping 30 Length of screen Water clear or cloudy at end of test Depth to top of screen Recommended pumping rate 5. G.P.M. Diameter of finished hole 90 with pump setting of..... feet below ground surface Water Record Well Log Depth(s) at Kind of water From which water(s) (fresh, salty, Overburden and Bedrock Record found sulphur) Cayers of amostore 110 Location of Well For what purpose(s) is the water to be used? In diagram below show distances of well from road and lot line. Indicate north by arrow. Is well on upland, in valley, or on hillside? HUNTLE Drilling or Boring Firm M. () More also Licence Number Name of Driller or Borer Malulla Fangl Address Oakto and GOULBOURN (Signature of Licensed Drilling or Boring Contractor) Form 7 10M-62-1152

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15-18 1 FRESH 3 SULPHUR 19 2 SALTY 4 MINERAL 17-18 1 STEEL 19 2 GALVANIZED 188. 0 025 61 PLUGGING & SEA DEPTH SET AT - FEET MATERIAL AI	ND TYPE (CEMENT GROUT,
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PRINTING OF WELL STATUS OF WELL STATUS OF WELL OF WE	20-23 1 [SALTY 4 MINERALS 6 GAS	7 5 PLASTIC 17-18 1 STEEL 2 GALVANIZED 3 CONCETE 4 OPEN HOLE	19	20-2	DEPTH SET	AT - FEET		CEM (CEM	ENT GROUT
STATIC STATIC	30-33	SALTY 6 GAS FRESH 3 SULPHUR 34 BC	1 USTEEL 2 GALVANIZED 3 CONCRETE 4 COPEN HOLE	26	27-30					
STATIC VALUE	11)					LO	CATION (OF WEL	L	
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FORM NO. 0506 (11/86) FORM 9

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The Ontario Water Resources Act P \A/FI | PFCORD

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32)					
41 WA	TER RECORD	51 CASING &	OPEN HOLE	RECORD	Z SIZE (S	54 S) OF OPENING NO)	31-33 DIAME	TER 34-38 L	75 40 ENGTH 39-40
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	15-56 1 DOMESTIC	5 COMMERCIAL				<u></u>		ise.	
WATER USE	2 STOCK 3 IRRIGATION 4 INDUSTRIAL		DITIONING			* W-L	46		
U3E	OTHER	9 NO							
METHOD	CABLE TOOL CONVEN								
OF CONSTRUCTI	ION BOTARY (REVERSION A BOTARY (AIR)	E)	OTHER					14	1176
NAME OF WELL		WEL	L CONTRACTOR'S	DRILLERS REMA		ONTRACTOR 59-62	DATE RECEIVED	-	
1 a,	Wall Std.	2	558	SOURCE DATE OF INS	PECTION	2558	JUN	3 0 199	P
mc mc	Donalds Co	rnes Ont		SE					
ADDRESS ON ADDRESS NAME OF WE SIGNATURE OF	LL TÉCHNICIAN COOBLI	WEI	L TECHNICIAN'S						
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The Ontario Water Resources Act

WATER WELL RECORD

Ontario	1. PRINT ONLY IN	I SPACES PROVIDED RECT BOX WHERE APPLICABLE	11	1529	217	MUNICIP 15005		י או	1.11.1
OTTAWA-	CARLETON	TUP OF UEST	CARUTE	W/Hunt	(4) CON	BLOCK TRACT, SURVE	Y ETC		22 23 74 LOT 25-27
		aux i	Rel, As	htor One	/ /		DATE COM		
	10 12	17 18	1 1 24	RC. ELEVATION	RC.	BASIN CODE	1,		,,,
		OG OF OVERBURDEN	AND BEDF	OCK MATERI					47
GENERAL COLOUR	COMMON MATERIAL	OTHER MAT	TERIALS		GENER	AL DESCRIPTION		DEPTH FROM	TO TO
BROWN	5/10/5	FILL						0	4
GRAN	LINESTONE	SAINT LOVOR	1175	147	W WAS	<u> </u>		4	6
GREY-GAM	SHALE	SANDY DOCOM	SANASZ	use CER	YIMR	<u>0, </u>		170	120
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1 2 10	TER RECORD	51 CASING & C	PEN HOLE	RECORD.	SIZE S	OF OPENING	65 17-33 DIAMET	ER 34-38 L	75 B0 ENGTH 39-40
WATER FOUND AT - FEET	KIND OF WATER	INSIDE DIAM MATERIAL	WALL THICKNESS	DEPTH - FEET ROM TO	C MATER	IAL AND TYPE		INCHES DEPTH TO TOP	FEET
122 15	FRESH 3 SULPHUR 14	10-11 STEEL 12		13 -16	SC			OF SCREEN	41-44 30 FEET
	FRESH 3 SULPHUR 19 SALTY 4 MINERALS G GAS	64 3 CONCRETE 4 OPEN HOLE 5 PLASTIC	.188 +7		61	PLUGGING	& SEAL	NG RECO	RD
2	FRESH 3 SULPHUR 24 4 MINERALS SALTY 6 GAS	1 STEEL 2 GALVANIZED 3 CONCRETE 4 POPEN HOLE 5 PLASTIC	1	o 159	FROM	10	ATERIAL AND		IT GROUT CKER, ETC)
	FRESH 3 SULPHUR 29 4 MINERALS SALTY 6 GAS	24-25 26		27:30	5 18-2		oxit.		
	FRESH 3 SULPHUR 34 10 4 SALTY 6 GAS	2 □ GALVANIZED 3 □ CONCRETE 4 □ OPEN HOLE 5 □ PLASTIC			26-21	30-33 80			
71 PUMPING TEST METH		11-14 DURATION OF PUN	(PING 17-18		LC	CATION O	F WELL		
STATIC LEVEL	WATER LEVEL 25			IN DIA	GRAM BELOV	V SHOW DISTANCES CATE NORTH BY ARE	OF WELL F	ROM ROAD AN	D
TEST 5Z	22-24 15 MINUTES	30 MINUTES 45 MINUTES 2-34	60 MINUTES	H	,,,,	THE HONTH DI ARE			
UN IF FLOWING GIVE RATE	FEET FEET 38-41 PUMP INTAKE SE	TAT WATER AT END OF						1	\setminus \mid
RECOMMENDED PUMP	GPM RECOMMENDED PUMP	FEET 1 CLEAR 43-45 RECOMMENDED	2 CLOUDY			-	ه ره س		*
SHALLOW		PUMPING A	0/O _{GPM}		1	<u>· ·C</u>	SKM.		7
FINAL	WATER SUPPLY	S ABANDONED, INSUFF			,	vell			2
STATUS OF WELL	2 TOBSERVATION WELL 3 TEST HOLE 4 RECHARGE WELL	6 ABANDONED POOR Q 7 UNFINISHED DEWATERING	UALITY	100	, +	vec			Z
55-5	DOMESTIC STOCK	5 GOMMERCIAL 6 MUNICIPAL		7	F				ALT
WATER USE	4 ☐ INDUSTRIAL	7 PUBLIC SUPPLY COOLING OR AIR CONDITI			l dr	e Road :	/		16
3	OTHER CABLE TOOL	9 NOT U	SED		ruga	C KOUZ	•		
METHOD OF	2 ROTARY (CONVENTION 3 ROTARY (REVERSE)	DNAL) 7 DIAMOND B JETTING						74	•
CONSTRUCTION	N 1 ROTARY (AIR) S AIR PERCUSSION	P DRIVING DIGGING [OTHER	DRILLERS REMARKS	S			15 0	474
MAME OF WELL CO	ON DRKLING	INC LICENS	ONTRACTOR'S	DATA	58 11	By E. es	TE RECEIVED	7 1996	63-68 80
ADDRESS ADDRESS ADDRESS NAME OF WELL SIGNATURE OF THE		n, Ont. KOA:	240	SOURCE O DATE OF INSPEC	TION	INSPECTOR	ULI	1 1 1330	
ANTE OF WELL	TECHNICIAN Stonton	WELL T	ECHNICIAN'S	O REMARKS					
SIGNATURE OF TE	ECHNICIA / CONTRACTOR	SUBMISSION DATE	Co.	OFFICE				aca ma	
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The Ontario Water Resources Act WATER WELL RECORD

Print only in spaces provided.

Mark correct box with a checkmark, where applicable.

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Municipality	Con.		
15005	COK	111	11

0506 (11/98) Front Form 9

County or District	NA CARELION	Township/Borough/City/Town	n/Village CARELTO/		plock tract surve	y, etc. L	ot
		Address	RTEN RO	ASHTO	Date completed	26 day	10 99 month year
21		Northing Label Lab	RC Elevatio	n RC Basin C	ode ii		 v
	LOG OF	OVERBURDEN AND BEDROC	K MATERIALS (see	instructions)			1.
General colour	Most common material	Other materials		General description	on .	From	th - feet To
GREY	LIMESTONE						145
	-				***************************************		
		;					
	1004				***		
		A Paragraph					
<u></u>						1.1.1.1.1	
2 10 10	15 37	32	43			ليلنا	
ater found	R RECORD Kind of water 51 Inside diam	CASING & OPEN HOLE REC	Depth - feet	Sizes of opening (Slot No.)	31-33 Diameter	34.38 Ler inches	ngth 3645
- feet	inches	Inches	From To	Material and type		Depth at top	
	Sairty Gas Gas Sulphur G	4 Open hole 7,00	762 18 E	"			feet
70 2 0	Salty 6 Gas	5 Plastic	25.23	PLUGG Annular s	NG & SEALING	RECOR Abandon	
2 🛄	Salty 5 Gas	Galvanized Galvanized Goncrete For Open hole	8 145	Depth set at - feet From To	Material and type (Ce	ement grout, l	pentonite, etc.)
·	Fresh	1 Steel 25 Galvanized	2-30	19:21 32:26	poment	grow	U
30-33 t = 2] Fresh ³ ☐ Sulphur ^{34 l50} 4 ☐ Minerals] Salty ⁵ ☐ Gas	Graduation Concrete		26-29 30-33 5			
Pumping test m	ethod 10 Pumping rate 2 11-11	Duration of pumping 7:18		LOCATION	OF WELL		
Static level W	leter level	Hours Mins ☐ Pumping ☐ Macovery	In diagram b Indicate nor	elow show distance		road and I	ot line.
6 feet If flowing give ra	15 minutes 30 minutes 28 31	45 minutes 32:34 60 minutes 35:37		·		1	/)
If flowing give ra	feet 6 feet 7 feet 8 fe	t O feet O feet Water at end of test	, -			J	n 1
Recommended po		Recommended 46-49				I	/V _
☐ Shallow	Deep pump setting 40 fee	pump rate 7 GPM	ı	200			**
INAL STATUS				€ > 0,	1		
Water supply Description 1 Water supply Description 2 Description 3 Description 1 Desc	on well 6 Abandoned, poor quality 7 Abandoned (Other)	10 Replacement well	1	130	0 1		
- Recharge	well 5 Dewatering 55.96			V	· · · · · · · · · · · · · · · · · · ·		<u>.</u>
Domestic Stock	5 ☐ Commercial 6 ☐ Municipal	9 Not use 10 Other	80	505 MG	CARTEN		-
□ Irrigation□ Industrial	 Public supply Cooling & air conditioning 				OWY: R O .	ER H	111
METHOD OF C	5 (X Air percussion	⁹ □ Driving			RD.	1 KM	
2 Rotary (co 3 Rotary (rev 4 Rotary (air	verse) ⁷ Diamond	10 Digging 11 Other				210	758
			Deta	Contracto	50.00 Dit-		
T SA	UNDERS DRILLI	Well Contractor's Licence No. 4879	source	4879	59-62 Date rece		1999
Address			Date of inspection	inspector			•
lame of Well Techni		Well Technician's Licence No.	Remarks			· ~ ~ -	
Gignature of Technic		Subgrission date	<u>s</u>			CSS.	ES0



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Mark correct box with a checkmark, where applicable.

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Municipality 5005	CON	1	1	1	1	Į.	ı	
10 37	15				22	23	24	

0506 (07/00) Front Form 9

County or District	<u></u>	Township/Borough/City/Tow	/n/Village	Con block tract su	rvey, etc. Lo	25-27
Ottava C	'arleton	West Carleton	- Huntley	11		48-53
		Address R.R. #4 796 G	olden Line Rd. A	Date complete	ted 10 day 9 m	on 62 year
	U)	Northing	RC Elevation	RC Basin Code ii ntario KOA 1AC	iii	iv
21	M 10 12	17 18	24 25 26	NO 31		47
-	LOG OF	OVERBURDEN AND BEDROC	K MATERIALS (see instru	ctions)	Depti	ı - feet
General colour	Most common material	Other materials	Gen	eral description	From	То
Brown	Soil	Broken Rock			0	12
	Limestone				12	95
Gray						
Grey & R	ed Shale				95	220
Gray	Limestone				220	225
						,
	Note:	Casing was left 1.	5 feet above gro	und level		
		at time of drillin	ng	<u></u> .		
31						ا لىلى
32						يا ليلن
	# 15 21 51 51	CASING & OPEN HOLE REC	CORD Size	s of opening 31-33 Diam		75 80 th 39-40
Water found at - feet	Kind of water Inside diam	Material Wall thickness	Depth - feet Sion	t No.)	inches	feet
	Fresh 3 Sulphur 14 inches 6 10-74	1 € Steel 12 188	Depth - feet From To O 22.165	erial and type	Depth at top	of screen 41-44
15.19	Safty 6 ☐ Gas	2 Galvanized 3 Concrete 4 Open hole				feet
219	☐ Salty 6 ☐ Gas	5 ☐ Plastic	20-23	PLUGGING & SEAL		
20-23	Fresh 4 D Minerals	1 Steel 2 Galvanized 3 Concrete	Depth:	Annular space	Abandonm	
25.20	Salty 6 Gas 5 7/8	4 Open hole 5 □ Plastic	22.5 225 From	10	e (Cement grout, be	
[[] [☐ Fresh 3 ☐ Sulpritir 29 ☐ Salty 6 ☐ Gas ☐ Gas	1 Steel 26 2 Galvanized	27-30 210-13	0 Grouted	- Cement	(3)
	Fresh ³ Sulphur ³⁴ ⁶⁰	3 Concrete 4 Open hole	26-29	30-33 80		
2	☐ Salty 6 ☐ Gas	5 Plastic				
Pumping test n		Duration of pumping 15-16 17-18 Mins		LOCATION OF WELL		
Static level	Water level 25 Water levels during 11	Pumping 2 Recovery	In diagram below s Indicate north by a	how distances of well fro	om road and lot	t line.
19-21	end of pumping valer levels during 22-24 15 minutes 26-28 30 minutes 29-31	·	indicate north by a	now.		
5		1	1			
UNION If flowing give r	150 feet 220 feet 200 feet	Water at end of test	of mag	rton Rd		
Recommended p	GPM feet pump type Recommended 43-45		7111717	1 101/1/4		
☐ Shallow	pump setting 175 fee	pump rate	4			
50-53			y [\$ # 8591	_	
FINAL STATU		upply ⁹ ☐ Unfinished	+ L	1035	JPump#	
1 Water sup 2 ☐ Observati 3 ☐ Test hole	ion well 6 Abandoned, poor quality 7 Abandoned (Other)	10 ☐ Replacement well	d	r .	Toof	wose
4 ☐ Recharge					7 406	
WATER USE	55-56 5 ☐ Commercial	9 ☐ Not use	A.			
2 → Stock 3 ☐ Irrigation	6 ☐ Municipal 7 ☐ Public supply	10 Other	F	L	ļJ	
4 🗀 Industrial		·	Ĭ			
METHOD OF	CONSTRUCTION 57					
¹ ☐ Cable too ² ☐ Rotary (c	onventional) ⁶ 🗗 Boring	9 Driving 10 Digging				
3 ☐ Rotary (re 4 ☐ Rotary (a	everse) 7 🔲 Diamond	11 Other			250	408
Name of Well Cont		Well Contractor's Licence No.	Data 58 Contraction		CT 25 2	007
Capital Address	Water Supply Ltd.	1558	Date of inspection	Inspector	,,, LU L	,,,,,
P.O. Box	k 490 Stittsville, O	ntario K2S 1A6	SS			
Name of Well Tech	nician	Well Technician's Licence No.	Remarks	rage - sa		۸,۸
S. Mille Signature of Jechn		T0097 Submission date	SE	US CO	SS.ES	2
1 MX	1 1	10 - 00 - 02	▼ i			

Hydrogeological Study 8520 McArton Road, Ottawa, Ontario **APPENDIX D** 8520 McArton Road, MECP Water Well Record

CERTIFICATE OF WELL COMPLIANCE



I (Jeremy Hanna) AIR ROCK DRILLING CO. LTD DO HEREBY CERTIFY
that I am licensed to drill water wells in the Province of Ontario, and that I have
supervised the drilling of the water well on the property of:
OWNER: OTTAWA VALLEY WILD BIRD CARE CENTER
Location: # 8520 MCARTON ROAD, Ashton
LOT: 4 CON: 12 PLAN# \times S/L# \times
Ottawa-Carleton / Geographical Township of Soulbourn
I CERTIFY FURTHER that, I am aware of the well drilling requirements, the guidelines, recommendations and regulations of the Ministry of the Environment governing well installations in the Province of Ontario, and the standards specified in any subdivision agreement and hydrogeological report applicable to this site and City Standards.
AND DO HEREBY CERTIFY THAT the said well has been drilled, cased, grouted (cement or bentonite) as applicable and constructed in strict conformity with the standards required.
Signed this 16TH Day of JANUARY, 2080
lune Tem
Jeremy Hanna (T3632) Air Rock Drilling Co. Ltd. (C-7681)
The Engineer on behalf of the Landowner set out above, Certifies that he/she has inspected the well and it was constructed in accordance with the specifications in O.Reg 903, this report and the Hydrogeological Report with regards to casing length and grouting requirements.
Signed this7th day ofApril,2020
Sean Sterling THG A 25 28 13 GEOFIRMA
(Engineer)

Shaping our future together Ensemble, formons notre avenir

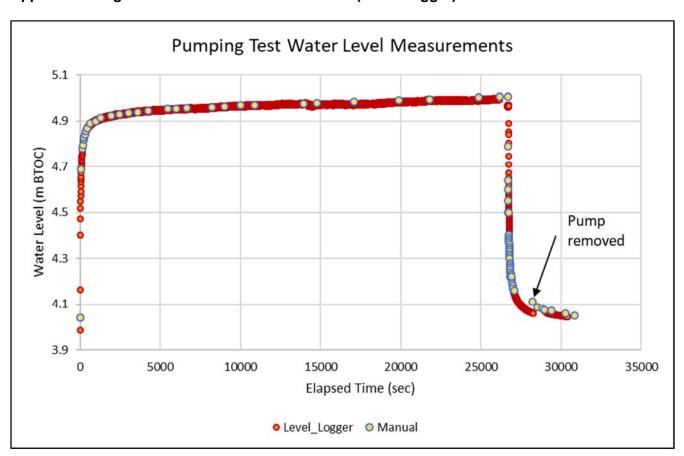
Clty of Ottawe Client Service Centre 8763 Victoria Street

Yille d'Ottawa Centre de service R243, me Victoria

Ontario	Ministry of the Environment and Climate Change	Well Tag#:A	252813 _{t Below)}	7	Well Record	
Measurements recorded i	· ~ Å	A252	813	Regulation 903 Ont	tario Water Resources Act Page of	t -
Well Owner's Informa						Personal Per
First Name Ottawa Volle	Last Name / Organiza	ore Cent	E-mail Address	FIRMA_	Well Constructed by Well Owner	_
Mailing Address (Street Number 1997)	Ltd 1 Royn	Municipality Trees	-, Sol 200, E	Halid &	HIKIRIAA	
Well Location Address of Well Location (S		Township	n .		oncession	Edito.
# 8520 M County/District/Municipality	CARTON R	City/Town/Village	Jourson Br	Province		- 1
OTTAWA- UTM Coordinates Zone , E.	asting Northing	Municipal Plan a	SHOON, and Sublot Number	Ontai	.io	_
NAD 8 3 18		286	ons on the back of this form)			
THE PARTY CONTRACTOR OF THE PROPERTY OF THE PARTY CONTRACTOR OF THE PARTY CONT	ost Common Material	Other Materials		neral Description	Depth (mag) From To	<u> </u>
21	Send a	Douldon S			0' 7'	-
6000	Black hi	NESPAO			60' 175'	<u>,</u>
						-
						-
		:				-
						-
	Annular Space			Results of Well Yield	Testing	
Depth Set at (m(tt)) From To	Type of Sealant Use (Material and Type)	d Volume Pla (m³/8©)		d, water was: Draw	V Down Recovery Vater Level Time Water Level	•
42' 0' N	leat Cements	slurry 17.	Other, specify_ If pumping discontinu	ued, give reason: (min)	(m/ft) (min) (m/ft) 1311 151 911	ī
			$\parallel \chi$	Level	5.5 1 4.3	
			Pump inflake set at (n	2	15.5 2 14.3	-
Method of Constru		Well Use	Pumping rate (Vmin &		5.6 3 14.2	
Rotary (Conventional)	Diamond ☐ Public Jetting ☐ Domestic Driving ☐ Livestock		watering Duration of pumping	- 1	5.6 4 14.0° 5.6 5 1	
	Driving	Cooling & Air Conditioning	Final water level end	of pumping (m@) 10 he	5.6 10	
Other, specify	Other, specify		If flowing give rate (l/n	nin / GPM) 15	5.6 15	
Inside Open Hole OR I (Galvanized, Fib	Material Wall De	pth (max) Water Supp	ly Recommended pump	p deptin (mag)	5.7 20	
(cm/6) Concrete, Plastic	c, Steel) (cm/db From	To Replacement To Test Hole Recharge W	Recommended numr	p rate	5-7 ²⁵ 5-7 ³⁰	
64 5000	-188" +2'	☐ Dewatering ☐ Observation	Well and/or Well production (//min	O+ 40 C	5.7 40	
6 Spring	100	Monitoring H Alteration (Constructio	tole 1200t	The state of the s	5.8 50	
		Abandoned,	Supply No	60)	5.8 60 7	
Outside Material		oth (m/ft) Water Qualit	Please provide a ma	Map of Well Locati ap below following instruct		
(cm/in) (Plastic, Galvanize	Erem	To Abandoned, specify	Oniei,		B	
		Other, specia	ý S	#8520	£ 7	
CALLET SALECTED IN THE SECURITY AND A SECURITY OF SECURITY AND A SECURITY A	ater Details of Water: ☐ Fresh Wunteste	Hole Diameter ed Depth (<i>m/</i> ∰) Dia	ameter Y V	2 ARTOH	" It	
	ther, <i>specify</i> of Water: ☐ Fresh hteste	_ / _ /	3/44	KOAD	K	,
Water found at Depth Kind	ther, specifyof Water: Fresh Nunteste	42' 175' 6	<u>u</u>			7
69 (m/10 Gas 0	ther, specify	_		TAL	3KM (F	ķ
Business Name of Well Cont	ے اے <i>ا</i> کے اندو	Well-Contractor's Lice	ence No.	Jack Jack		
Business Address (Street Nu	mper/Name)	D C 76 81	Comments:			
Province Postal C		ddress LCh Minn	2 1HP-0	66pm 3	4@100M	
Bus Telephone No. (inc. area c	ode) Name of Well Technician	(Last Name, First Name)	information package	Package Delivered	Ministry Use Only Idit No. Z276954	
Well Technician's Licence No. S	ignature of Technician and/or	tontractor Date Submitted	Date V	Work Completed		
0506E (2014/11)	Hund	Acado ON Ministry's	Gepy OFX		ceived © Queen's Printer for Ontario, 2014	

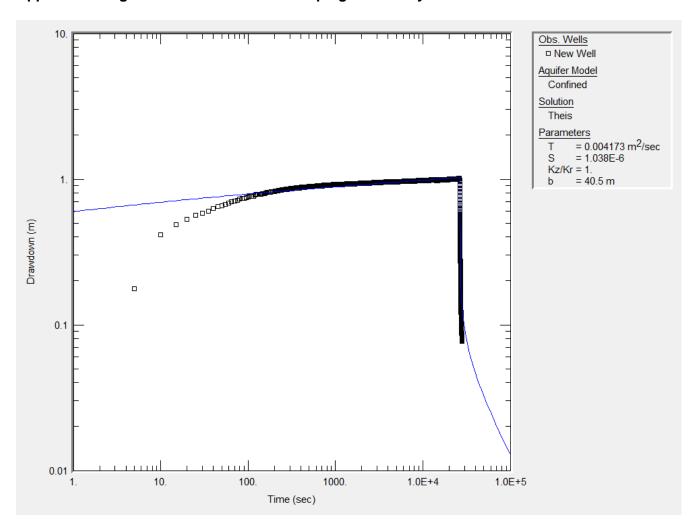
Hydrogeological Study 8520 McArton Road, Ottawa, Ontario **APPENDIX E Pumping Test Results and Analysis**

Appendix E: Figure E.1 – Manual and Transducer (Level Logger) Water Level Measurements



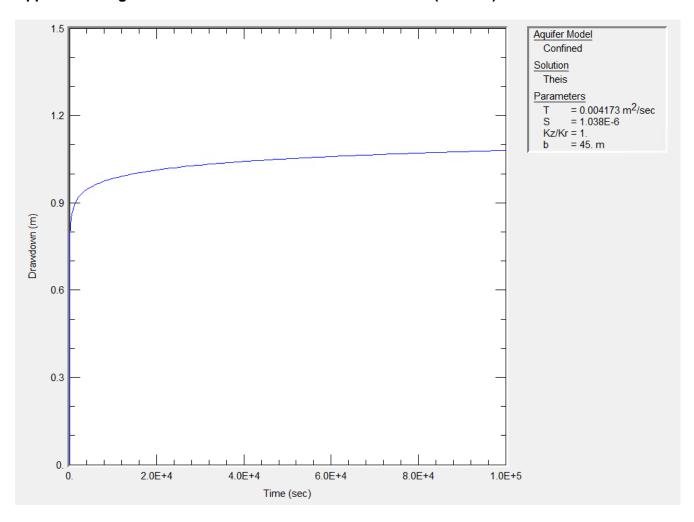


Appendix E: Figure E.2 - AQTESOLVE Pumping Test Analysis





Appendix E: Figure E.3 – Simulated Drawdown at 132 L/min (35 GPM)





Hydrogeological Study 8520 McArton Road, Ottawa, Ontario **APPENDIX F Laboratory Report**



300 - 2319 St. Laurent Blvd Ottawa, ON, K1G 4J8 1-800-749-1947 www.paracellabs.com

Certificate of Analysis

Geofirma Engineering Ltd.

1 Raymond St.,Suite 200 Ottawa, ON K1R 1A2 Attn: Chris Morgan

Client PO:

Project: 19-213-1

Custody:

Report Date: 11-Feb-2020 Order Date: 5-Feb-2020

Order #: 2006334

This Certificate of Analysis contains analytical data applicable to the following samples as submitted:

 Paracel ID
 Client ID

 2006334-01
 MCW-3h

 2006334-02
 MCW-6h

Approved By:

Mark Foto

Mark Foto, M.Sc. Lab Supervisor



Certificate of Analysis

Client: Geofirma Engineering Ltd.

Client PO:

Report Date: 11-Feb-2020 Order Date: 5-Feb-2020 Project Description: 19-213-1

Analysis Summary Table

Analysis	Method Reference/Description	Extraction Date	Analysis Date
Alkalinity, total to pH 4.5	EPA 310.1 - Titration to pH 4.5	6-Feb-20	6-Feb-20
Ammonia, as N	EPA 351.2 - Auto Colour	7-Feb-20	7-Feb-20
Anions	EPA 300.1 - IC	6-Feb-20	6-Feb-20
Colour	SM2120 - Spectrophotometric	6-Feb-20	6-Feb-20
Conductivity	EPA 9050A- probe @25 °C	6-Feb-20	6-Feb-20
Dissolved Organic Carbon	MOE E3247B - Combustion IR, filtration	11-Feb-20	11-Feb-20
E. coli	MOE E3407	5-Feb-20	5-Feb-20
Fecal Coliform	SM 9222D	5-Feb-20	5-Feb-20
Heterotrophic Plate Count	SM 9215C	5-Feb-20	5-Feb-20
Metals, ICP-MS	EPA 200.8 - ICP-MS	11-Feb-20	11-Feb-20
pH	EPA 150.1 - pH probe @25 °C	6-Feb-20	6-Feb-20
Phenolics	EPA 420.2 - Auto Colour, 4AAP	7-Feb-20	7-Feb-20
Hardness	Hardness as CaCO3	11-Feb-20	11-Feb-20
Sulphide	SM 4500SE - Colourimetric	10-Feb-20	11-Feb-20
Tannin/Lignin	SM 5550B - Colourimetric	6-Feb-20	6-Feb-20
Total Coliform	MOE E3407	5-Feb-20	5-Feb-20
Total Dissolved Solids	SM 2540C - gravimetric, filtration	10-Feb-20	11-Feb-20
Total Kjeldahl Nitrogen	EPA 351.2 - Auto Colour, digestion	6-Feb-20	7-Feb-20
Turbidity	SM 2130B - Turbidity meter	6-Feb-20	6-Feb-20

Client: Geofirma Engineering Ltd.

Certificate of Analysis

Order #: 2006334

Report Date: 11-Feb-2020

Client PO: Project

Order Date: 5-Feb-2020

Project Description: 19-213-1

			I MOVALOU		
	Client ID: Sample Date:	MCW-3h 04-Feb-20 11:45	MCW-6h 04-Feb-20 15:10	-	-
	Sample Date: Sample ID:	2006334-01	2006334-02	-	-
	MDL/Units	Drinking Water	Drinking Water	-	-
Microbiological Parameters					
E. coli	1 CFU/100 mL	ND	ND	-	-
Fecal Coliforms	1 CFU/100 mL	ND	ND	-	-
Total Coliforms	1 CFU/100 mL	ND	ND	-	-
Heterotrophic Plate Count	10 CFU/mL	<10	<10	-	-
General Inorganics					
Alkalinity, total	5 mg/L	288	288	-	-
Ammonia as N	0.01 mg/L	0.06	0.05	-	-
Dissolved Organic Carbon	0.5 mg/L	2.3	1.4	-	-
Colour	2 TCU	12	20	-	-
Conductivity	5 uS/cm	638	636	-	-
Hardness	mg/L	283	290	-	-
рН	0.1 pH Units	7.7	7.8	-	-
Phenolics	0.001 mg/L	<0.001	<0.001	-	-
Total Dissolved Solids	10 mg/L	338	338	-	-
Sulphide	0.02 mg/L	<0.02	<0.02	-	-
Tannin & Lignin	0.1 mg/L	<0.1	<0.1	-	-
Total Kjeldahl Nitrogen	0.1 mg/L	0.1	0.1	-	-
Turbidity	0.1 NTU	2.8	3.5	-	-
Anions					
Chloride	1 mg/L	19	20	-	-
Fluoride	0.1 mg/L	<0.1	<0.1	-	-
Nitrate as N	0.1 mg/L	<0.1	<0.1	-	-
Nitrite as N	0.05 mg/L	<0.05	<0.05	-	-
Sulphate	1 mg/L	19	19	-	-
Metals			•		
Calcium	0.1 mg/L	77.9	80.7	-	-
Iron	0.1 mg/L	0.4	0.4	-	-
Magnesium	0.2 mg/L	21.4	21.5	-	-
Manganese	0.005 mg/L	0.027	0.026	-	-
Potassium	0.1 mg/L	1.4	1.5	-	-
Sodium	0.2 mg/L	5.2	5.6	-	-



Certificate of Analysis

Order #: 2006334

Report Date: 11-Feb-2020 Order Date: 5-Feb-2020

 Client:
 Geofirma Engineering Ltd.
 Order Date: 5-Feb-2020

 Client PO:
 Project Description: 19-213-1

Method Quality Control: Blank

		Reporting		Source				RPD	
Analyte	Result	Limit	Units	Result	%REC	Limit	RPD	Limit	Notes
Anions									
Chloride	ND	1	mg/L						
Fluoride	ND	0.1	mg/L						
Nitrate as N	ND	0.1	mg/L						
Nitrite as N	ND	0.05	mg/L						
Sulphate	ND	1	mg/L						
General Inorganics			-						
Alkalinity, total	ND	5	mg/L						
Ammonia as N	ND	0.01	mg/L						
Dissolved Organic Carbon	ND	0.5	mg/L						
Colour	ND	2	TČU						
Conductivity	ND	5	uS/cm						
Phenolics	ND	0.001	mg/L						
Total Dissolved Solids	ND	10	mg/L						
Sulphide	ND	0.02	mg/L						
Tannin & Lignin	ND	0.1	mg/L						
Total Kjeldahl Nitrogen	ND	0.1	mg/L						
Turbidity	ND	0.1	NTU						
Metals									
Calcium	ND	0.1	mg/L						
Iron	ND	0.1	mg/L						
Magnesium	ND	0.2	mg/L						
Manganese	ND	0.005	mg/L						
Potassium	ND	0.1	mg/L						
Sodium	ND	0.2	mg/L						
Microbiological Parameters									
E. coli	ND	1	CFU/100 mL						
Fecal Coliforms	ND	1	CFU/100 mL						
Total Coliforms	ND	1	CFU/100 mL						
Heterotrophic Plate Count	ND	10	CFU/mL						

Certificate of Analysis

Order #: 2006334

Report Date: 11-Feb-2020 Order Date: 5-Feb-2020

 Client:
 Geofirma Engineering Ltd.
 Order Date: 5-Feb-2020

 Client PO:
 Project Description: 19-213-1

Method Quality Control: Duplicate

		Reporting		Source		%REC		RPD	
Analyte	Result	Limit	Units	Result	%REC	Limit	RPD	Limit	Notes
Anions									
Chloride	19.6	1	mg/L	19.5			0.4	10	
Fluoride	ND	0.1	mg/L	ND			NC	10	
Nitrate as N	ND	0.1	mg/L	ND			NC	10	
Nitrite as N	ND	0.05	mg/L	ND			NC	10	
Sulphate	19.5	1	mg/L	19.3			1.3	10	
General Inorganics									
Alkalinity, total	284	5	mg/L	288			1.1	14	
Ammonia as N	0.012	0.01	mg/L	0.018			NC	17.7	
Dissolved Organic Carbon	2.3	0.5	mg/L	2.3			3.2	37	
Colour	21	2	TCU	20			4.9	12	
Conductivity	635	5	uS/cm	638			0.5	5	
рН	7.8	0.1	pH Units	7.7			0.9	3.3	
Phenolics	ND	0.001	mg/L	ND			NC	10	
Total Dissolved Solids	336	10	mg/L	338			0.6	10	
Sulphide	ND	0.02	mg/L	ND			NC	10	
Tannin & Lignin	ND	0.1	mg/L	ND			NC	11	
Total Kjeldahl Nitrogen	0.12	0.1	mg/L	0.11			9.6	16	
Turbidity	2.8	0.1	NTU	2.8			2.5	10	
Metals									
Calcium	9.1	0.1	mg/L	9.2			0.3	20	
Iron	0.2	0.1	mg/L	0.2			3.3	20	
Magnesium	2.5	0.2	mg/L	2.6			3.7	20	
Manganese	0.008	0.005	mg/L	0.008			0.8	20	
Potassium	0.7	0.1	mg/L	0.7			3.1	20	
Sodium	15.7	0.2	mg/L	16.1			2.6	20	
Microbiological Parameters									
E. coli	ND	1	CFU/100 mL	ND			NC	30	
Fecal Coliforms	ND	1	CFU/100 mL	ND			NC	30	
Total Coliforms	ND	1	CFU/100 mL	ND			NC	30	
Heterotrophic Plate Count	ND	10	CFU/mL	ND			NC	30	

Client: Geofirma Engineering Ltd.

Certificate of Analysis

Client PO:

Order #: 2006334

Report Date: 11-Feb-2020 Order Date: 5-Feb-2020

Project Description: 19-213-1

Method Quality Control: Spike

Analyte	Result	Reporting Limit	Units	Source Result	%REC	%REC Limit	RPD	RPD Limit	Notes
Anions									
Chloride	29.3	1	mg/L	19.5	97.4	77-123			
Fluoride	1.08	0.1	mg/L	ND	108	79-121			
Nitrate as N	1.05	0.1	mg/L	ND	105	79-120			
Nitrite as N	0.936	0.05	mg/L	ND	93.6	84-117			
Sulphate	28.3	1	mg/L	19.3	90.2	74-126			
General Inorganics									
Ammonia as N	0.291	0.01	mg/L	0.018	109	81-124			
Dissolved Organic Carbon	11.2	0.5	mg/L	2.3	89.6	60-133			
Phenolics	0.025	0.001	mg/L	ND	101	69-132			
Total Dissolved Solids	96.0	10	mg/L	ND	96.0	75-125			
Sulphide	0.52	0.02	mg/L	ND	103	79-115			
Tannin & Lignin	1.0	0.1	mg/L	ND	104	71-113			
Total Kjeldahl Nitrogen	2.07	0.1	mg/L	0.11	97.7	81-126			
Metals									
Calcium	18100	0.10	mg/L	9170	89.7	80-120			
Iron	2510	0.10	mg/L	241	90.9	80-120			
Magnesium	11500	0.20	mg/L	2600	89.3	80-120			
Manganese	60.8	0.01	mg/L	7.98	106	80-120			
Potassium	10400	0.10	mg/L	696	96.9	80-120			
Sodium	23900	0.20	mg/L	16100	78.2	80-120		Q	M-07



Order #: 2006334

Report Date: 11-Feb-2020 Order Date: 5-Feb-2020 Project Description: 19-213-1

Client: Geofirma Engineering Ltd.
Client PO: Project

Qualifier Notes:

Login Qualifiers:

Certificate of Analysis

Container(s) - Bottle and COC sample ID don't match -

Applies to samples: MCW-6h

Sample Qualifiers:

QC Qualifiers:

QM-07: The spike recovery was outside acceptance limits for the MS and/or MSD. The batch was accepted based on

other acceptable QC.

QS-02: Spike level outside of control limits. Analysis batch accepted based on other QC included in the batch.

Sample Data Revisions

None

Work Order Revisions / Comments:

None

Other Report Notes:

n/a: not applicable ND: Not Detected

MDL: Method Detection Limit

Source Result: Data used as source for matrix and duplicate samples

%REC: Percent recovery. RPD: Relative percent difference.

NC: Not Calculated



Paracel ID: 2006334



Paracel Order Number

Chain Of Custody Ontario Drinking Water Samples

Nº

11116

Client	Name:	Geofirma		Project Ref:	19-213-1 Waterworks Name:						Samples Taken By: KAM Name: Kyle McCrae												
Conta	ct Name:	Chris Mor	gan	Quote #:							Waterworks !	Number:			Name:	me: Kyle McCsap							
Addre	ss:	1 Raymond	Št	PO#:							Address:				Signati	ire:							
After I	Hours Contact:	,		E-mail:	CMOT	der	161	160/	(Co	ns.Lo	3					,				f 1 Requ			
Teleph	nonė:	613-402-	1701	Fax:		7		1			Public Health	Unit:									M 4 d	iay	
u 0	les Submitted IN REG 170/03 IN REG 243/03		,		Sample Type: R = Raw; T = Source Type: G = Ground				Water; S = S	urface Water						Requ	uired	Anal	/ses				
		n submitted to MOE/MOF					ortab	le: Re	quir	es AWQ	reporting as	s per Regulation - Y = Ye	s; N = 1			ilo				di	1		
		or human consumption?:	THE RESERVE AND ADDRESS OF THE PARTY OF THE	2110 \$11/1		T/D/P	5/5	N/A			SAMPLE	COLLECTED	2	hlorin /L	hed:	/E. Coli				C			
		n must be completed b	A STATE OF THE PARTY OF THE PAR	s will be pro	essed.	e: R/	ype: 6	ble: Y	Resample				ntaine	oed C	Flus EG 24	iform	HPC	Lead	MHZ	3,4			
	LOCAT	TION NAME		SAMPLE ID		Sample Type: R/T/D/P	Source Type: G / S	Reportable:	Resa		DATE	TIME	# of Containers	Free/Combined Chlorine Residual mg/L	Standing / Flushed S / F (REG 243)	Total Coliform/E.				Subdivisto			
1	800 N	1cActon	MCW	-3h		R	(,	V	N	04.7	Feb-19	11:45	8	0						X	\dagger	\top	1
2		McArton	MON			R	G	N			Feb-19		8	0						X	T	\top	1
3																					T		1
4							-					,											1
5											-			,						\top	\top	\top	1
6																				\top	\top		1
7																					十	\top	1
8																				1	\top	\top	1
9																					T		1
10																			\exists		\top	T	1
Comm	nents: SQ	mple 2 read	Mch	-G.5h											Method	lof Di	elivery	1	Ní	n			
Reling	uished By (Sign):	Morgon		Receive Driver/C							Receiv Lab:	MASS	S	-	Verified	By:	M	2	1	4	h	1	-
Relino	uished By (Print)	W.		Date/Ti	ne:						Date/	Time: 2) - OS	2	15150	Date/Ti	me:	07	2-0	05	5-2	10	20)
Date/	Time: 05-	Feb-19/1	5:00	Temper	ature:					°C	Temp	erature: 68	0	c	pH Veri	ied:	Ø	Ву:	M	4		15	BU

Hydrogeological Study 8520 McArton Road, Ottawa, Ontario **APPENDIX G** Water Corrosive Index Calculations (LSI and RSI Index)

Langelier Saturation Index (LSI)

LSI is an important and widely used calculation to determine a solution's ability to dissolve or deposit calcium carbonate. It is widely used to assess the corrosivity of water for planning water treatment equipment.

LSI is calculated as the difference between measured pH and calculated pH.

LSI < 0 corrosive (-0.5 = mildly corrosive, -2 = moderately corrosive, -5 = severly corrosive)

LSI > 0 scale forming (0.5 = slight scale, 1 - mild scale, 2.5 - moderate scale, 4 = severe scale forming)

LSI = 0 neutral, balanced water

 $LSI = pH - pH_s$

where,

pH is the measured water pH

pHs is the pH at saturation in calcite or calcium carbonate and is defined as:

pHs = (9.3 + A + B) - (C + D)

where:

A = (Log10 [TDS] - 1) / 10

 $B = -13.12 \times Log10 (oC + 273) + 34.55$

C = Log10 [Ca2+ as CaCO3] - 0.4

D = Log10 [alkalinity as CaCO3]

Temperature	8.17 °C
рН	7.06
Calcium Hardness	77.9 mg/L
Total Alkalinity	288 mg/L
TDS	338 mg/L

p(Ca++) =	3.11
p(Alk) =	2.24
A =	2.38
B =	0.20
C =	0.00

pHs =	7.94	
Langelier Index =	-0.88	(Corrosive)
Ryznar Index =	8.81	(Corrosive)

Ryznar Saturation Index (RSI)

The Ryznar stability index (RSI) attempts to correlate an empirical database of scale thickness observed in municipal water systems to the water chemistry.

RSI = 2(pHs) - pH

where,

pH is the measured water pH

pHs is the pH at saturation in calcite or calcium carbonate

RSI << 6 the scale tendency increases as the index decreases

RSI >> 7 the calcium carbonate formation probably does not lead to a protective corrosion inhibitor film

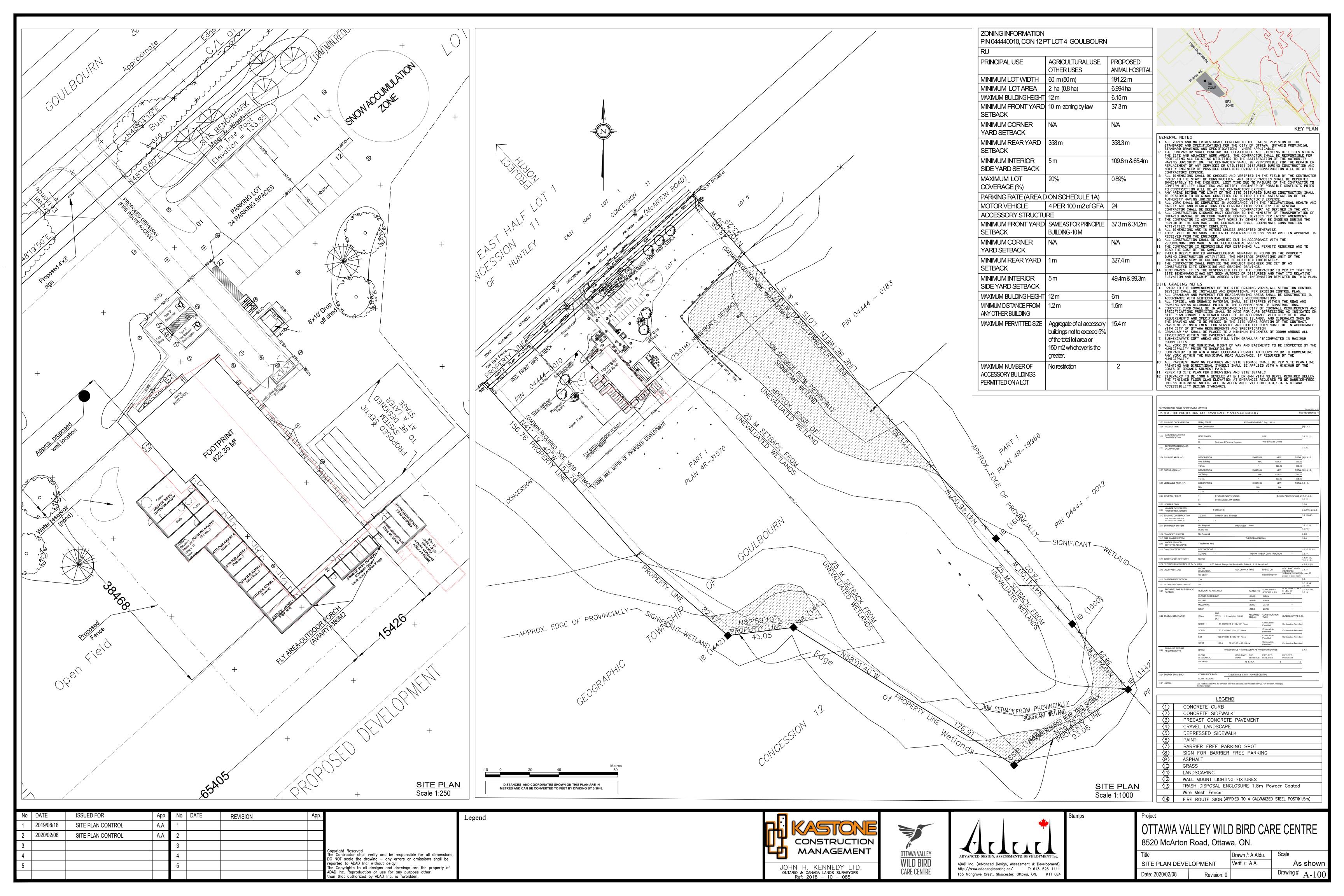
RSI >> 8 mild steel corrosion becomes an increasing problem.

Prepared by: SNS Reviewed by: CAM

Calculator_LangelierRyznar



Hydrogeological Study 8520 McArton Road, Ottawa, Ontario **APPENDIX H** Site Plan



Hydrogeological Study 8520 McArton Road, Ottawa, Ontario **APPENDIX I Nitrate Dilution Calculations**

Site - Infiltration Area

Lot Size	69,940.0 m ²	6.994 ha
Building footprint (roof)	<mark>622.4</mark> m ²	
Parking lot footprint (paved)	568.3 m ²	
Driveway and loading dock (paved)	600.0 m ²	
Outdoor Aviary	380.0 m ²	
Subtotal impervious	2,170.7 m ²	
Subtotal pervious	67,769.3 m ²	

calculated value constant input value

Infiltration Factors Total Site I_{factor} 0.68

MOEE, 1995 - Stormwater Management Planning and Design Manual

Topography	I _{factor}	% Site	Site I _{factor}
Flat Land, average slope < 0.6 m/km	0.3	100%	0.3
Rolling Land, average slope 2.8 m to 3.8 m/k	0.2	0%	0
Hilly Land, average slope 28 m to 47 m/km	0.1	0%	0
Soils			
Tight impervious clay	0.1	0%	0
Medium combinations of clay and loam	0.2	60%	0.12
Open Sandy loam	0.4	40%	0.16
Cover			
Cultivated Land	0.1	100%	0.1
Woodland	0.2	0%	0

Post-Devlopment Water Budget Estimatation

lot area	69,940.0 m	ı²
subtotal impervious area	2,170.7 m	1 ²
net area for infiltration (subtotal pervious)	67,769.3 m	1 ²
moisture surplus (from Thornthwaite)	0.279 n	
moisture surplus (for entire site)	19,499.5 m	1 ³
Total Site I _{factor}	0.7	
annual moisture infiltration	189.586 m	nm/m²
annual moisture infiltration (site)	12,848.1 m	1 ³
annual estimated runoff (site)	6,239.8 m	1 ³

Maximum Allowable Daily Flow

Qi = Q_Infiltration	12,848.1 m³/year	Pervious Area x Available Infiltration (Thornthwaite)	1
Q_max	4,282.7 m³/year	Q_Infiltration / 3 as per Procedure D-5-4	
	11,733.5 L/d		

Nitrate Dilution Calculation

Mass Balance Equation, $Q_T C_T = Q_e C_e + Q_i C_i + Q_b C_b$

effluent loading (sewage flow)	$Q_{\rm e}$	7.4	m³/day
nitrate concentration in effluent	C_e	40.0	mg/L
sewage effluent input (nitrate)	Q_eC_e	296	g/day
available dilution water (infiltration)	Q_{i}	12,848.1	m³/year
nitrate concentration in precipitation	C _i	0.0	mg/L
infiltration input (nitrate)	Q_iC_i	0.0	g/day
available dilution sewage flow	Q_{e}	2,701.0	m³/year
total available dilution flow	$Q_T = Q_i + Q_e$	15,549.1	m³/year
calculated septic (nitrate) loading	$C_T = Q_e C_e / (Q_i + Q_e)$	6.95	mg/L
background nitrate concentration	C_b	0.05	mg/L
total predicted nitrate conc. at boundary	$C_T + C_b$	7.0	mg/L



Prepared by: SNS Reviewed by: CAM

Thornthwaite Analysis to Determine Annual Moisture Surplus

Month	Mean Temp. (°C)	Average Monthly Preciptiation (mm)	ı	PET(0) cm/month	K (40deg)	K (50deg)	К	PET(L) cm/month
January	-9.6	61.5	0	0	0.8	0.71	0.7532	0
February	-8.1	46.8	0	0	0.89	0.84	0.864	0
March	-2.1	53.4	0	0	0.99	0.98	0.9848	0
April	5.7	73.7	1.2	2.5	1.1	1.14	1.1208	2.9
May	13.2	64.6	4.4	6.3	1.2	1.28	1.2416	7.9
June	18.4	97.1	7.2	9.1	1.25	1.36	1.3072	11.8
July	20.8	92.3	8.6	10.4	1.23	1.33	1.282	13.3
August	19.7	88.6	7.9	9.8	1.15	1.21	1.1812	11.5
September	15.6	83.3	5.6	7.6	1.04	1.06	1.0504	8.0
October	8.5	76.7	2.2	3.9	0.93	0.9	0.9144	3.6
November	1.6	71.9	0.17	0.6	0.83	0.76	0.7936	0.5
December	-5.4	63.6	0	0	0.78	0.68	0.728	0

calculated value constant input value

Annual PET 59.5 cm

J 37.31

c 1.09

Latitude (between 40 and 50) 45.2 45 deg 12' 18"

Average Annual Precipitation 873.3 mm (based on Environment Canada climate data for Appleton 1993-2019)

Annual Moisture Surplus 279 mm

Where: $\underline{c = 0.000000675J^{3} - 0.0000771J^{2} + 0.01792J + 0.49239}$

 $\underline{\mathsf{PETi}(\mathsf{L}) = \mathsf{K} \; \mathsf{PETi}(\mathsf{0})} \qquad \underline{\mathsf{PETi}(\mathsf{0}) = 1.6(10\mathsf{Ti}/\mathsf{J})^{\mathsf{c}}}$

 $\frac{\text{Ii} = (\text{Ti/5})^1.514}{\text{J} = \sum(\text{Ii})}$

