René's Court 1000 Robert Grant Ave

Transportation Impact Assessment Report

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## René’s Court

# 1000 Robert Grant Ave 

TIA Report
prepared for:
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June 22, 2020

## Document Control Page

| CLIENT: | Lépine Corporation |
| :--- | :--- |
| PROJECT NAME: | Transportation Impact Assessment - René’s Court |
| REPORT TITLE: | René’s Court (1000 Robert Grant Ave) - TIA Report |
| PARSONS PROJECT NO: | 476799 - 01000 |
| VERSION: | Final |
| DIGITAL MASTER: | H:\ISO\476799\1000\DOCS\Step_5_TIA_Report - Submission \#2\476799- <br> LepineRenesCourt_TIA_06.19.20.docx |
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| HISTORY: | TIA Step 4 Submission - June 21, 2019 <br> TIA Step 5 Submission - November 11, 2019 <br> TIA Step 5 Re-submission - June 22, 2020 |



TIA Plan Reports
On 14 June 2017, the Council of the City of Ottawa adopted new Transportation Impact Assessment (TIA) Guidelines. In adopting the guidelines, Council established a requirement for those preparing and delivering transportation impact assessments and reports to sign a letter of certification.

Individuals submitting TIA reports will be responsible for all aspects of development-related transportation assessment and reporting, and undertaking such work, in accordance and compliance with the City of Ottawa's Official Plan, the Transportation Master Plan and the Transportation Impact Assessment (2017) Guidelines.

By submitting the attached TIA report (and any associated documents) and signing this document, the individual acknowledges that $\mathrm{s} / \mathrm{he}$ meets the four criteria listed below.

## CERTIFICATION

1. I have reviewed and have a sound understanding of the objectives, needs and requirements of the City of Ottawa's Official Plan, Transportation Master Plan and the Transportation Impact Assessment (2017) Guidelines;
2. I have a sound knowledge of industry standard practice with respect to the preparation of transportation impact assessment reports, including multi modal level of service review;
3. I have substantial experience (more than 5 years) in undertaking and delivering transportation impact studies (analysis, reporting and geometric design) with strong background knowledge in transportation planning, engineering or traffic operations; and
4. I am either a licensed ${ }^{1}$ or registered ${ }^{2}$ professional in good standing, whose field of expertise [check $\sqrt{ }$ appropriate field(s)] is either transportation engineering $\nabla$ or transportation planning $\square$.

1,2 License of registration body that oversees the profession is required to have a code of conduct and ethics guidelines that will ensure appropriate conduct and representation for transportation planning and/or transportation engineering works.

Dated at $\qquad$ this $\qquad$ day of June 2020. (City)

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## TIA Report

## 1. SCREENING FORM

The screening form was submitted in conjunction with the Scoping Report for review and confirmation of the need for a Transportation Impact Assessment (TIA). The Trip Generation, Location, and Safety triggers were met based on the unit count, proposed new driveway on a "Spine" cycling route and proximity to the Robert Grant/Bobolink and Robert Grant/Abbott roundabouts. The Screening Form and City of Ottawa comments and responses are provided in Appendix A.

## 2. SCOPING REPORT

### 2.1. EXISTING AND PLANNED CONDITIONS

### 2.1.1. PROPOSED DEVELOPMENT

Lépine Corporation has retained Parsons to complete the following TIA Report in support of a Zoning By-Law amendment application for a proposed residential development in Ward 6: Stittsville West. The proposed development is located at 1000 Robert Grant Ave and is expected to consist of three residential towers ranging from four to eighteen storeys with 504 units in total. Buildout has been assumed in a single phase, by 2023 based on current estimates. The subject site is currently vacant and zoned as AM - Arterial Mainstreet. The local context is provided in Figure 1 and the current concept plan is shown in Figure 2.

Figure 1: Local Context



Building A consists of a 4-6 storey building housing 107 apartment units. Building $B$ consists of a 9-storey building, housing 150 apartment units. Building $C$ consists of an 18 -storey building, housing 247 apartment units. Building AM is a 1 storey amenity space.

Two accesses are proposed to serve the development site. The main access is proposed via Robert Grant Avenue, which leads to an internal roundabout, a ramp to the underground parking garage (south of Building B) and sixteen surface parking spaces. The main access intersection with Robert Grant Ave is expected to permit right-in/right-out only vehicular movements only. It is expected the majority of site generated traffic will use this access.

A secondary access is proposed as a full movement driveway connection to Livery Street, which leads directly to the underground parking garage. This secondary access takes a more circuitous route but provides redundancy if the primary access off Robert Grant is ever unavailable.

### 2.1.2. EXISTING CONDITIONS

## Area Road Network

Fernbank Road is an east-west arterial road that runs between Dwyer Hill Road and Eagleson Road. Fernbank Road has a two-lane undivided rural cross section with paved shoulders. Within the study area, the posted speed limit is $80 \mathrm{~km} / \mathrm{h}$.

Robert Grant Avenue is a north-south arterial roadway that extends from Fernbank Road in the south to Abbott St E in the north. The roadway has a two-lane cross-section and the posted speed limit is $60 \mathrm{~km} / \mathrm{h}$.

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Abbott Street $E$ is an east-west major collector roadway east of Stittsville Main Street and a collector roadway west of Stittsville Main Street. Within the study area, it has a two-lane cross-section with auxiliary turn lanes provided at major intersections. The posted speed limit is $50 \mathrm{~km} / \mathrm{h}$. The Abbott St E connection to Terry Fox Drive was recently completed.

Bobolink Ridge is an east-west local roadway that extends from Robert Grant Avenue in the west and terminates at Asturcon Street in the east. It has a two-lane cross-section and an unposted speed understood to be $50 \mathrm{~km} / \mathrm{h}$.

Livery Street is a north-south local roadway that extends north from Bobolink Ridge, turns east and terminates at Tapadero Avenue. It has a two-lane cross-section and an unposted speed understood to be $50 \mathrm{~km} / \mathrm{h}$.

## Existing Study Area Intersections

## Abbott Street E/Robert Grant

The Abbott Street E/Robert Grant intersection is a threelegged, single lane roundabout intersection. All approaches consist of a single approach lane. All movements are permitted at this location.


## Bobolink/Robert Grant

The Bobolink/Robert Grant intersection is a four-legged roundabout intersection. All approaches consist of a single approach lane. All movements are permitted at this location.


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## Fernbank/Robert Grant

The Fernbank/Robert Grant intersection is a signalized ' T ' intersection. The southbound approach consists of a leftturn lane and a right-turn lane. The eastbound approach consists of a left-turn lane and a through lane. The westbound approach consists of a through lane and a rightturn lane. All movements are permitted at this location.


## Bobolink/Livery

The Bobolink/Livery intersection is an unsignalized ' $T$ ' intersection with STOP control in Livery Street. All approaches consist of a single all-movement lane. All movements are permitted at this location.


## Existing Driveways to Adjacent Developments

There are no existing driveways on either side of Robert Grant Avenue within 200 m of the proposed site access. On the east side of Livery Street there are approximately 17 private residential driveways within 200 m of the proposed site access.

## Existing Area Traffic Management Measures

Below are the existing area traffic management measures on the boundary streets:

Robert Grant Avenue

- Medians;
- Sidewalks;
- Streetscaping

Bobolink Ridge

- Sidewalks

Livery Street

- Sidewalks


## Pedestrian/Cycling Network

Sidewalks are provided on both sides of Robert Grant Avenue, on the north side of Abbott Street E, the north side of Bobolink Drive and the west side of Livery Street. There are no existing sidewalks on Fernbank Road. A multi-use pathway is provided on the south side of Abbott Street E. The Ottawa Pedestrian Plan (2013) does not identify any future projects within the study area.

The City of Ottawa's 2013 Cycling Plan identifies Robert Grant Avenue and Fernbank Road as Spine Routes, and Abbott Street E as a major pathway. Cycling facilities include cycle tracks on Robert Grant Avenue and a pathway on the south side of Abbott Street E. There are no existing cycling facilities on Fernbank Road.

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## Transit Network

There is currently no transit service provided north of Cope Dr along Robert Grant Ave. The OC Transpo routes that currently operate within the study area are as follows:

- Route \#62 (St-Laurent, Hurdman <-> Terry Fox, Stittsville): identified by OC Transpo as a "Rapid Route", Route \#62 operates at an average rate of every 30 minutes during weekday peak hour periods. The nearest bus stops to the site are available along Abbott St, as well as Iber Rd.
- Route \#167 (Terry Fox <-> Blackstone): identified by OC Transpo as a "Local Route", this route operates at a rate of every 30-or-60 minutes during weekday morning and afternoon peak hour periods. The nearest bus stops to the development site are available along Robert Grant Ave, as well as Cope Dr.
- Route \#252 (Mackenzie King <-> Fernbank): identified by OC Transpo as a "Connexion Route", this route operates during weekday rush-hours only at an average rate of every 10-to-15 minutes. The nearest bus stops to the site are available along Robert Grant Ave, as well as Cope Dr.

The noted OC Transpo route maps have been provided in Appendix B. Figure 3 below illustrates the area transit network, while Figure 4 provides the nearest bus stop locations to the development site.

Figure 3: Area Transit Network


Figure 4: Bus Stop Locations


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## Peak Hour Travel Demand

The existing peak hour traffic volumes within the study area, as illustrated in Figure 5, were obtained from the City of Ottawa or conducted by Parsons. The peak hour traffic volume count data has been provided in Appendix C.

Note, the traffic volumes on Robert Grant between Bobolink and Abbott E were balanced to the higher approach volume to represent the worst-case scenario. Furthermore, vehicles using the west leg of the Bobolink/Robert Grant roundabout were not included in the traffic volume figures as they represent a small number of vehicles accessing the construction site west of Robert Grant Ave.

Figure 5: Existing Peak Hour Traffic Volumes


## Existing Road Safety Conditions

The local road network is relatively new, hence there is limited history of collisions along the boundary streets. The collision data available for Robert Grant Avenue indicates that there were two collisions since the road was built: a sideswipe collision in July 2016 and an angle collision in October 2017. Both collisions resulted in property damage only and no pedestrians and cyclists were involved. The collision data as provided by the City of Ottawa and related analysis has been provided in Appendix D.

### 2.1.3. PLANNED CONDITIONS

## Planned Study Area Transportation Network Changes

Fernbank Road is identified as a transit priority corridor with isolated measures (City of Ottawa Transportation Master Plan (TMP) 2013, Ultimate Network) and widening has been proposed in the Network Concept Map 10 (TMP).

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Robert Grant Avenue is identified as a transit priority corridor with isolated measures in the Affordable Network Plan and a future Bus Rapid Transit (BRT) corridor in the Network Concept Plan. Additionally, Park and Rides have been proposed at the Abbot E/Robert Grant and Fernbank/Robert Grant intersections in the Affordable Network Plan, the Network Concept Plan and the Fernbank Community Design Plan.

A high-level design for Robert Grant Ave was completed as part of the West Transit Way Connections (Terry Fox Dr. to Fernbank Rd) EA study. The section of this design, along the proposed development frontage is shown in Figure 6. This section includes exclusive bus lanes along the roadway centreline, the future Abbott BRT station, and park and ride location.

Figure 6: Future Robert Grant Ave Concept


## Other Area Developments

The following developments are planned near the subject site based on the latest information from the City:

## 365 Haliburton Heights (Abbott-Fernbank Lands)

Eight two-storey buildings comprised of 96 apartments are proposed at the above noted address, located 750 m south of the subject development. The Transportation Impact Assessment (prepared by Novatech) projected approximately 45 to 50 veh/h during peak hours.

## 5611 Fernbank Road (Abbott-Fernbank Lands)

eQHomes is proposing a residential development, also in the Abbott-Fernbank Lands, located at the above address, directly south of the subject development. Based on a site visit completed January 14 ${ }^{\text {th }}, 2019$, it was determined that this development has almost reached full build-out. As such, it is reasonable to assume the majority of traffic generated by this development has been captured by the traffic counts completed in January 2019 and will not be accounted for in background traffic.

## 570 Hazeldean Road

Mattamy Homes is proposing a subdivision development consisting of approximately 227 single homes and 518 townhomes, located 1 km north of the subject development. The Transportation Brief (prepared by Stantec) projected approximately 230 veh/h during the morning peak hour and 360 veh/h during the afternoon peak hour.

## 590 Hazeldean Road

Richcraft Homes is proposing a subdivision development consisting of approximately 600 units, located 1 km north of the subject development. The Transportation Impact Study (prepared by Stantec) projected approximately 300 veh/h during the morning peak hour and 375 veh/h during the afternoon peak hour.

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5505 Fernbank Road (Blackstone South)
Mattamy Homes is proposing a subdivision development consisting of approximately 609 units, located 1.2km southeast of the subject development. The Transportation Impact Assessment (prepared by Parsons) projected approximately 264 veh/h during the morning peak hour and 327 veh/h during the afternoon peak hour.

## 5786 Fernbank Road (CRT Lands)

In 2011, the IBI Group submitted a Transportation Letter to the City of Ottawa for the development known as Claridge Homes - Fernbank Subdivision, located west of Robert Grant Ave, across from the future Lépine Development. The City has confirmed phase 1 of this development will be built-out in the next five-years, with 311 single-family homes and 265 townhome units built (see attached plan in Appendix F). Trip generation estimates for phase 1 were completed and incorporated in the future traffic analysis.

700 Cope Dr (Stittsville High School)
A two-phase construction of a high school (grades 7-12) is proposed by OCDSB at 700 Cope Dr, with an initial date of occupancy of 2022 and full buildout at 2024. Based on a recent TIA Report by Parsons, the school is expected to generate a total of 230 and $155 \mathrm{veh} / \mathrm{h}$ at full buildout during the morning and afternoon peak hours, respectively. These volumes were included in the future traffic analysis.

## 240 Livery Street

Cardel Homes is proposing to build eleven residential buildings, each containing twelve residential units (112 total). The development site is located approximately 400 m east of Robert Grant Ave and is expected to generate less than 60 veh/h. As such, vehicle trips generated by this development were accounted for in the future traffic analysis.

306 Livery Street
Construction is near completion for 8 low-rise apartment blocks consisting of 12 apartment units each ( 96 total), that was proposed by Abbott Fernbank Holdings Inc. and Phoenix Properties Inc. The development is located at the northwest corner of Livery St/Tapadero Ave and is expected to generate less than $60 \mathrm{veh} / \mathrm{h}$. As such, vehicle trips generated by this development were accounted for in the future traffic analysis.

The location of the site and the adjacent future developments are shown below in Figure 7.

Figure 7: Other Area Developments


### 2.2. STUDY AREA AND TIME PERIODS

As the proposed site is largely a residential development, the time periods assessed will be the weekday morning and afternoon peak hours. As identified by the TIA Guidelines (2017), the horizon years analyzed are the buildout date 2023 and five-years after buildout, 2028. The proposed study area is outlined below and highlighted in Figure 8.

Figure 8: Study Area


- Abbott E/Robert Grant intersection;
- Bobolink/Robert Grant intersection;
- Fernbank/Robert Grant intersection;
- Bobolink/Livery intersection;
- Site Access/Robert Grant intersection;
- Site Access/Livery intersection;
- Robert Grant Avenue adjacent to the site; and,
- Livery Street adjacent to the site.


### 2.3. EXEMPTION REVIEW

Based on the City's TIA guidelines and the subject site, the following modules/elements of the TIA process, summarized in Table 1, are recommended to be exempt in the subsequent steps of the TIA process:

Table 1: Exemptions Review Summary

| Module | Element | Exemption Consideration |
| :--- | :--- | :--- |
| Design Review <br> Component (4.1, 4.3, <br> $4.4)$ | All elements | Not required for rezoning applications. |
|  |  | The purpose of this Zoning By-Law Amendment Application is to make <br> changes to the existing zoning by increasing the permitted building height, <br> seek an exception to Section 101(6)(c) in the City of Ottawa Parking <br> Provisions, and providing an additional building setback to the south side of <br> the property. The maximum allowed residential unit density of the <br> development is no different for the proposed zoning than the existing zoning. <br> As such, section 4.8 is exempt. |
| Concept |  |  |

Typically, Module 4.2. Parking is exempt from the TIA since the application is only seeking a zoning by-law amendment. However, the City of Ottawa has requested Module 4.2 Parking be included to discuss parking implications.

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## 3. FORECASTING

### 3.1. DEVELOPMENT GENERATED TRAVEL DEMAND

### 3.1.1. TRIP GENERATION AND MODE SHARES

The proposed development will consist of 504 apartment dwelling units, housed within two mid-rise and one high-rise buildings. Appropriate trip generation rates were obtained from the 2009 TRANS Trip Generation Residential Trip Rates report, Table 6.3, which have been summarized in Table 2.

Table 2: TRANS Trip Generation Residential Trip Rates

| Land Use | Data | Trip Rates |  |
| :--- | :---: | :---: | :---: |
|  |  | AM Peak | PM Peak |
| Mid-Rise Apartments (3-10 floors) | TRANS | $\mathrm{T}=0.29(\mathrm{du}) ;$ | $\mathrm{T}=0.37(\mathrm{du}) ;$ |
| High-Rise Apartments (10+ floors) | TRANS | $\mathrm{T}=0.29(\mathrm{du}) ;$ | $\mathrm{T}=0.36(\mathrm{du}) ;$ |
| Notes:$T=$ Average Vehicle Trip Ends <br> $d u=$ Dwelling unit |  |  |  |

Using the trip rates shown in Table 2, the number of vehicles per hour were determined as shown in Table 3 below.
Table 3: Apartment Units Vehicle Trip Generation

| Land Use | Dwelling | AM Peak (Vehicles/h) |  |  |  | PM Peak (Vehicles/h) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | In | Out | Total | In | Out | Total |  |
| Mid-Rise Apartments (3-10 floors) | 257 | 18 | 57 | 75 | 58 | 37 | 95 |  |
| High-Rise Apartments (10+ floors) | 247 | 17 | 55 | 72 | 55 | 34 | 89 |  |

The total vehicle trips shown in Table 3 for the apartment units were then converted to total person trips using the auto mode share values in Table 3.13 of the TRANS report. New mode share percentages were then applied to the resulting total person trips values, based on the 2011 NCR Household Origin-Destination (OD) Survey and the Kanata/Stittsville district. Table 4 provides the resulting person trips/h values for each of the travel modes.

Table 4: Mode Shares for the Lépine Residential Buildings Development

| Travel Mode | Mode <br> Share | AM Peak (Person Trips/h) |  |  | PM Peak (Person Trips/h) |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Out | Total | In | Out | Total |  |
| Auto Driver | $60 \%$ | 47 | 154 | 201 | 155 | 96 | 251 |
| Auto Passenger | $15 \%$ | 12 | 37 | 49 | 37 | 25 | 62 |
| Transit | $15 \%$ | 11 | 39 | 50 | 38 | 25 | 63 |
| Walking | $10 \%$ | 8 | 26 | 34 | 26 | 16 | 42 |
| Cycling | $0 \%$ | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Person Trips | $100 \%$ | 78 | 256 | 334 | 256 | 162 | 418 |
| Total 'New' Auto Trips |  | $\mathbf{4 7}$ | $\mathbf{1 5 4}$ | $\mathbf{2 0 1}$ | $\mathbf{1 5 5}$ | $\mathbf{9 6}$ | $\mathbf{2 5 1}$ |

As shown in Table 4, the resulting number of total person trips expected to be generated by the proposed development are approximately 335 and 420 in the morning and afternoon peak hours respectively. The projected 'new' vehicle trips are approximately 200 and 250 in the weekday morning and afternoon peak hours respectively.

### 3.1.2. TRIP DISTRIBUTION AND ASSIGNMENT

Based on the 2011 NCR Household Origin-Destination Survey (Kanata - Stittsville district) and the location of adjacent arterial roadways and neighbourhoods, the distribution of site-generated traffic volumes was estimated as follows:

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- $5 \%$ to/from the north;
- $40 \%$ to/from the south;
- $50 \%$ to/from the east; and,
- $5 \%$ to/from the west.

The expected site-generated auto trips in Table 4 were then assigned to the road networks as shown in Figure 9 below.
Figure 9: Lépine Residential Development Site-Generated Traffic


```
xx AM Peak Hour Volumes
(yy) PM Peak Hour Volumes
```

O Roundabout Intersection

The development is proposing two access points, one on Robert Grant Ave and one on Livery St. The Robert Grant access is expected to be a right-in/right-out (RIRO) access only. As such, traffic coming from the north may either turn left at the Bobolink/Robert Grant roundabout and access the development from Livery St or make a U-turn at the roundabout to access the RIRO from the south.

### 3.2. BACKGROUND NETWORK TRAFFIC

### 3.2.1. TRANSPORTATION NETWORK PLANS

Refer to Section 2.1.3: Planned Study Area Transportation Network Changes.

### 3.2.2. BACKGROUND GROWTH

Historically, Fernbank Rd has experienced a decline in background growth, as observed by historical traffic counts data (years 2009, 2010, 2012, 2014 and 2017) on the West Leg of Fernbank/Eagleson. The percent change from 2009 has been summarized in Table 5. Detailed background traffic growth analysis is provided in Appendix E.

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Table 5: Fernbank/Eagleson Historical Traffic Growth (2009-2017)

| Time Period | Percent Change |
| :---: | :---: |
|  | West Leg |
| 8 hrs | $-1.51 \%$ |
| AM Peak | $-4.91 \%$ |
| PM Peak | $-1.17 \%$ |

Accounting for future developments, which are expected to reach full build-out by 2025, a $2 \%$ background growth rate per year was considered appropriate to estimate interim traffic growth along existing roadways within the study area. Figure 10 and Figure 11 show the estimated future background peak hour traffic volumes in the 2023 and 2028 horizons.

Figure 10: Future Background 2023


Figure 11: Future Background 2028


### 3.2.3. OTHER DEVELOPMENTS

Descriptions of the adjacent developments in the surrounding area that have initiated the development application process with the City were provided in Section 2.1.3: Other Area Developments.

The following surrounding developments were expected to be fully constructed within the analysis periods and have an impact on the study area of the proposed Lépine development, based on the latest information available from the City.

- Fernbank Crossing, Phase 3 (2015)
- Fernbank Crossing, Phase 4 (2017)
- Blackstone Subdivision, Phases 4-8 (2017) - 5505 Fernbank Rd
- CRT Lands, Phase 1 - 5786 Fernbank Rd
- Stittsville High School - 700 Cope Dr


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To produce the most accurate analysis results, the estimated trips generated by adjacent developments were recalculated and redistributed according to the current (2017) TIA requirements from the City. Many of the traffic studies supporting these developments were completed using the previous 2006 TIA requirements.

The most relevant changes were the trip generation rates and the mode share percentages; both were updated to follow the same trip generation process discussed in Section 3.1.1. The trip distribution applied to the adjacent developments was assumed to be the same as the percentages applied to the Lépine Development (see Section 3.1.2).

## Fernbank Crossing, Phases 3 and 4

A site visit confirmed the majority of Phase 3 was already constructed by the time traffic counts were conducted at intersections within the study area in January of 2019. However, it was assumed approximately 10\% (20 Single-Detached Units) of Phase 3 have yet to be constructed, as a conservative estimate. These remaining residential units were added to the trip generation calculations of Phase 4, which has not begun construction at the time of the report. Phase 4 proposes 100 Single-Detached units and 46 Townhouse units. Table 6 below provides the expected number of auto trips generated by Phases 3 and 4.

| Table 6: Fernbank Crossing Total New Auto Trips Generated |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |

As shown in Table 6 the expected number of vehicle trips generated by the remainder of Phase 3 and the entirety of Phase 4 are 119 and $133 \mathrm{veh} / \mathrm{h}$ in the morning and afternoon peak hours of travel. These auto trips are then distributed at Haliburton Heights, future Defense St and future Cope Dr extension. The majority of the trips would use the future Cope Dr to access eastern and northern regions of Ottawa. The remaining trips would access Defense St via Fernbank Rd (or viceversa) and a small percentage would utilize Robert Grant Ave.

## Blackstone South, Phase 4-8

The Blackstone South development is expected to reach full build-out by 2025 and features a total of 376 Townhouses, 423 Single-Detached Houses, a Residential Condominium Block, a Public High School and a Public Elementary School. Since this future development will connect to Fernbank Rd, Terry Fox Dr and the future extensions of Cope Dr and Rouncey Rd, it was assumed the majority of this development traffic will use those access points. For the following analysis, it was assumed approximately $10 \%$ of Townhouse units (45 Units) and 10\% of Single-Detached units (40 Units) would utilize Robert Grant Ave. Table 7 below provides the expected number of auto trips generated by the Blackstone South Development.

Table 7: Blackstone South Total New Auto Trips Generated

| Land Use | Dwelling Units | AM Peak (Vehicles/h) |  |  | PM Peak (Vehicles/h) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | In | Out | Total | In | Out | Total |
| Single-Detached Units | 40 | 8 | 23 | 31 | 20 | 13 | 33 |
| Townhouse Units | 45 | 9 | 18 | 27 | 16 | 15 | 31 |
| Total | 166 | 17 | 41 | 58 | 36 | 28 | 64 |

As shown in Table 7, the expected number of auto trips generated by the Blackstone South Development within the vicinity of the Lépine Development study area are 58 and $64 \mathrm{veh} / \mathrm{h}$ during the morning and afternoon peak hours of travel. The auto trips were then distributed reasonably at intersections within the study area.

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CRT Lands, Phase 1
The most recent traffic information available for this development is a Transportation Brief, submitted by the IBI Group in 2011. However, the City provided more recent information regarding the development which reveals that construction of phase 1 of the CRT Lands is currently underway and is expected to reach full build-out within the next five years, with a total of 311 single-family homes and 265 townhomes constructed. See Appendix F for the transportation brief and the plan sent by the City. Table 8 below provides the expected number of auto trips generated by phase 1 of the CRT Lands development.

Table 8: CRT Lands Total New Auto Trips Generated

| Land Use | Dwelling Units | AM Peak (Vehicles/h) |  |  | PM Peak (Vehicles/h) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | In | Out | Total | In | Out | Total |
| Single-Detached Units | 311 | 69 | 169 | 238 | 162 | 100 | 262 |
| Townhouse Units | 265 | 56 | 100 | 156 | 97 | 87 | 184 |
| Total | 576 | 125 | 269 | 394 | 259 | 187 | 446 |

As shown in Table 8, the total number of trips anticipated to be generated by phase 1 of the CRT Lands development is 394 and 446 veh/h during the morning and afternoon peak hour periods, respectively. The auto trips were distributed based on the distribution provided in the IBI Transportation Brief, as follows:

- $50 \%$ to/from Cope Dr;
- $35 \%$ to/from Bobolink Ridge; and
- $15 \%$ to/from a future access on Abbott Street East.


## Stittsville High School

Trip generation and traffic volumes assignment and distribution for Stittsville High School were obtained from the report that was recently submitted by Parsons. At initial occupancy in 2022, the high school is estimated to generate a total of 142 and 102 veh/h during the morning and afternoon peak hours, respectively. At full buildout in 2024, the high school is estimated to generate a total of 230 and $155 \mathrm{veh} / \mathrm{h}$ during the morning and afternoon peak hours, respectively.

## Total Adjacent Development Traffic

Some of the identified other area development are not expected to be fully constructed by horizon year 2023, but will be accounted for in horizon year 2028. The other area developments to be accounted for in each horizon year are listed below.

Horizon Year 2023
Fernbank Crossing
Stittsville High School Initial Occupancy

Horizon Year 2028
Fernbank Crossing
Blackstone South CRT Lands
Stittsville High School Full Buildout

Figure 12 and Figure 13 illustrate the traffic volumes expected to be generated by adjacent developments at horizon years 2023 and 2028.

PARSONS
Figure 12: 2023 Total Adjacent Development Traffic Volumes


## PARSONS

Figure 13: 2028 Total Adjacent Development Traffic Volumes


### 3.2.4. TOTAL BACKGROUND TRAFFIC

Total background traffic represents the summation of background traffic growth (based on the $2 \%$ growth rate) and adjacent development traffic.

By 2028, all adjacent development traffic was accounted for. This assumption represents the worst-case scenario, since the rate of development is highly dependent on future market conditions and its probable $100 \%$ buildout of all adjacent developments noted in this study will not be achieved by 2028.

The Future 2023 Total Background traffic volumes is illustrated in Figure 14, which is the sum of the future 2023 background traffic volumes in Figure 10 and the 2023 total adjacent development volumes in Figure 12. The Future 2028 Total Background traffic volumes is illustrated in Figure 15, which is the sum of the Future 2028 background traffic volumes from Figure 11 and 2028 total adjacent development volumes from Figure 13.

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Figure 14: Future 2023 Total Background Traffic Volumes


## PARSONS

Figure 15: Future 2028 Total Background Traffic Volumes


### 3.3. DEMAND RATIONALIZATION

The study area road network is expected to accommodate projected volumes. There are currently no anticipated capacity issues. The capacity of the roadways will be further explored in a more detailed review of the total projected traffic volumes and intersection design in the following analysis section.

## 4. ANALYSIS

### 4.1. DEVELOPMENT DESIGN

## Exempt - see Section 2.3.

### 4.2. PARKING

The subject site is located in "Area C" according to Schedule 1A within Part 4 - Parking, Queuing and Loading Provisions (Sections 100 to 112) of the City of Ottawa Zoning By-Law.

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## Auto Parking

The development is proposing to provide 666 auto parking spaces, with 650 spaces provided in an underground parking garage and 16 provided for visitors along the internal driveway of the site. Of the 650 underground parking spaces, 133 are allocated for Building A, 191 are allocated for Building B and 326 are allocated for Building $C$.

Based on the City of Ottawa Parking Provisions, auto parking is required at a rate of 1.2 for the residential units, with an added visitor parking rate of 0.2 . As such, a parking rate of 1.4 is required for the proposed development, which equates to approximately 706 parking spaces for the 504 residential units.

However, Section $101(6)(c)$ of the Parking Provisions states that parking spaces may be reduced by 20 spaces, if all parking spaces provided for a land use are located below grade (i.e. the underground parking garage). Building $B$ and Building $C$ parking spaces were each reduced by 20 spaces, thus resulting in a total of 666 proposed parking spaces. Although some parking spaces are proposed above ground, an exemption has been requested by the proponent to allow the reduction to take place. The premise of the exemption request is that, given that the proposed development is located in a suburban context (Area C), providing surface parking is more common than providing underground parking.

## Bicycle Parking

The City of Ottawa Zoning By-Law-Part 4, sections 100-114 Table 111A states that a minimum rate of 0.5 bicycle parking stalls be provided per dwelling unit for low, mid- and high-rise apartment buildings. The future development proposes to provide 252 bicycle parking spaces for the 504 residential units, thereby meeting the bicycle parking requirements.

### 4.3. BOUNDARY STREET DESIGN

Exempt - see Section 2.3.

### 4.4. ACCESS INTERSECTION DESIGN

Exempt - see Section 2.3.

### 4.5. TRANSPORTATION DEMAND MANAGEMENT

The TDM Measures checklist is attached in Appendix G.

### 4.6. NEIGHBOURHOOD TRAFFIC MANAGEMENT

The following section discusses the development's impact on local or collector roads of the surrounding neighbourhoods. Robert Grant Ave is classified as an arterial, which means it can be excluded from this analysis.

Livery Street is classified as a Local Road; as per the City of Ottawa's TIA Guidelines (2017). The City recommends one-way traffic volumes on local roads to be in the vicinity of $120 \mathrm{veh} / \mathrm{h}$. The highest observed existing one-way traffic volume along Livery Street, north of Robert Grant Ave, was 52 veh/h in the afternoon peak hour. By the 2028 horizon year, with full buildout of proposed development and noted adjacent developments, the estimated one-way traffic volume at the same location was $106 \mathrm{veh} / \mathrm{h}$ in the afternoon peak hour. Therefore, no changes are recommended for the classification of Livery Street.

In response to community concerns with the Livery Street access, it is important to reiterate the operation of the proposed Livery Street driveway as a secondary entrance. The owners have similar experience with a secondary driveway entrance at a similar high-density residential development in the Kanata Town Centre called William's Court. The underground parking was designed so that the principal access is the most convenient and frequently used by the residents,

## PARSONS

approximately $80 \%$ of all trips in and out of the underground garage. Similar design considerations will be proposed for the subject site, which will be reviewed in detail by City staff during the Site Plan Application process.

Bobolink Ridge is also classified as a Local Road; the highest observed existing one-way traffic volume east of Robert Grant Ave was $107 \mathrm{veh} / \mathrm{h}$ in the afternoon peak hour. By the 2028 horizon year, with full buildout of proposed development and noted adjacent developments, the estimated one-way traffic volume at the same location was $230 \mathrm{veh} / \mathrm{h}$ in the afternoon peak hour. However, this volume drops to approximately 180 veh/h approaching Livery Street.

In this case, no changes were recommended to the classification of Bobolink Ridge for the following reasons (refer to Figure 16):

1. Although Bobolink is classified as a local road, the section between Elfin Grove and Robert Grant Ave has been constructed to a collector road standard, which the City recommends a one-way traffic volume in the vicinity of $300 \mathrm{veh} / \mathrm{h}$. The pavement width is approximately 11.5 m and there is no direct frontage. This transition is necessary when connecting a local road to an arterial road;
2. There are three intersecting streets along the collector road section, Janka, Shinny and Elfin, which will reduce traffic volumes as Bobolink transitions to a local road; and,
3. It is anticipated that once the Rouncey Rd and Cope Dr roadways are fully built further east, more adjacent development traffic will divert away from Robert Grant, thereby relieving traffic pressure on Bobolink as it transitions to a local road.

Overall, the classification of Bobolink was considered appropriate in this context.

It is noteworthy that field observations at the intersection of Bobolink/Livery showed some vehicles exceeded the $50 \mathrm{~km} / \mathrm{h}$ speed limit of Bobolink Ridge. As such, a neighbourhood traffic management study may need to be conducted by the City of Ottawa to determine if there are requirements for traffic calming measures, such as signage, bulb-outs or vertical deflections (speed humps/tables, etc.).


Finally, it is important to note that this is still a developing community and the area road network has yet to fully mature. Abbott St E was only recently connected to Terry Fox Drive and other gaps in the area road network, once filled, will help draw traffic away from local streets. Furthermore, transit service and active mode facilities will be constructed to help provide alternative travel choices for local residents.

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### 4.7. TRANSIT

Refer to Section 2.1.2: Transit Network, for a description of the existing bus services within the study area. For future conditions, the "Rapid Transit and Transit Priority Network - 2031 Affordable Network" map of the City of Ottawa's Transportation Master Plan, identifies Robert Grant Ave as a future Transit Priority Corridor (Isolated Measures), with three Park and Ride areas located at Robert Grant/Hazeldean, Robert Grant/Abbott (immediately north of the Lépine Development) and Robert Grant/Fernbank. As such, transit services are expected to be able to accommodate the future transit demand of the Lépine Development and other developments along Robert Grant Ave.

### 4.8. REVIEW OF NETWORK CONCEPT

## Exempt - see Section 2.3.

### 4.9. INTERSECTION DESIGN

### 4.9.1. INTERSECTION CONTROL

Bobolink/Robert Grant and Abbott/Robert Grant are both roundabouts, while the Fernbank/Robert Grant intersection is controlled by traffic signals. These are appropriate designs based on approved studies for Robert Grant completed by the City. STOP Control is expected to be implemented for vehicles exiting the site at the two proposed site access.

### 4.9.2. INTERSECTION DESIGN

Synchro 10 Trafficware was used to asses the intersection performance of signalized and unsignalized intersections within the study area. At signalized intersections, critical movements were assessed based on the movement at the intersection with the highest volume-to-capacity ( $\mathrm{v} / \mathrm{c}$ ) ratio and the corresponding Level of Service (LOS). The signalized intersections 'as a whole' were based on the weighted $\mathrm{v} / \mathrm{c}$ ratio of all the movements at the intersection and the corresponding Level of Service (LOS). Unsignalized intersection was assessed based on the movement with the highest average delay at the intersection and its corresponding LOS.

Roundabouts within the study area were assessed using Sidra software and results are based on the average delay of the critical movement and the overall delay.

Note that, as per TIA standards, the Peak Hour Factor (PHF) was set to 0.90 in existing conditions and 1.0 in all future background and total projected conditions.

The Synchro and Sidra detailed analysis results for existing and future conditions have been provided in Appendix $\mathbf{H}$.

## Existing Conditions

Table 9 below provides a summary of intersection performance within the study area based on existing traffic volumes, previously shown in Figure 5.

## PARSONS

Table 9: Existing Conditions Intersection Performance

| Intersection |  | Weekday AM Peak (PM Peak) |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Critical Movement |  |  |  | Intersection 'As a Whole' |  |  |
|  |  | max. v/c or <br> avg. delay (s) | Movement | Delay (s) | LOS | v/c |  |
| Fernbank/Robert Grant (S) | $\mathrm{B}(\mathrm{D})$ | $0.66(0.84)$ | WBT(WBT) | $21.1(27.9)$ | $\mathrm{A}(\mathrm{B})$ | $0.46(0.70)$ |  |
| Bobolink/Livery (U) | $\mathrm{A}(\mathrm{A})$ | $9.0(8.8)$ | $\mathrm{SB}(\mathrm{SB})$ | $3.4(3.3)$ | - | - |  |
| Bobolink/Robert Grant (R) | $\mathrm{A}(\mathrm{A})$ | $9.6(9.4)$ | WBL(WBL) | $5.0(5.2)$ | $\mathrm{A}(\mathrm{A})$ | - |  |
| Abbott/Robert Grant $(\mathrm{R})$ | $\mathrm{A}(\mathrm{A})$ | $8.8(9.0)$ | $\mathrm{NBL}(\mathrm{NBL})$ | $6.1(5.2)$ | $\mathrm{A}(\mathrm{A})$ | - |  |

Note: Analysis of signalized intersections assumes a PHF of 0.90 and a saturation flow rate of 1800 veh/h/lane.
(S) - Signalized intersection.
(U) - Unsignalized intersection.
(R) - Roundabout intersection.

As shown in Table 9, the signalized intersection of Fernbank/Robert Grant 'as a whole' operates at a LOS 'B' in the critical afternoon peak hour. The critical movement operates at a LOS 'D' in the afternoon peak hours. Critical movements of the unsignalized intersection of Bobolink/Livery operates at a LOS ' $A$ ' during both the morning and afternoon peak hour periods.

The roundabout intersections operate 'as a whole' with a LOS ' $A$ ' during both peak hours and the critical movements operate at a LOS ' $A$ ' during both peak hours.

## Future 2023 Total Background Conditions

The Future 2023 Background traffic volumes were shown in Figure 14. Table 10 below provides a summary of the critical Synchro analysis results at intersections within the study area, based on the future background 2023 traffic volumes.

It should be noted that the Fernbank/Robert Grant intersection signal timing was optimized in all future scenarios to ensure the most efficient operations.

Table 10: Future 2023 Total Background Intersection Performance

| Intersection |  | Weekday AM Peak (PM Peak) |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Critical Movement |  |  | Intersection 'As a Whole' |  |  |  |
|  |  | max. v/c or <br> avg. delay (s) | Movement | Delay (s) | LOS | v/c |  |
| Fernbank/Robert Grant (S) | $\mathrm{B}(\mathrm{D})$ | $0.66(0.83)$ | WBT(WBT) | $20.9(27.5)$ | $\mathrm{A}(\mathrm{B})$ | $0.46(0.68)$ |  |
| Bobolink/Livery (U) | $\mathrm{A}(\mathrm{A})$ | $8.9(8.7)$ | $\mathrm{SB}(\mathrm{SB})$ | $3.4(3.3)$ | - | - |  |
| Bobolink/Robert Grant (R) | $\mathrm{A}(\mathrm{A})$ | $9.7(9.5)$ | $\mathrm{WBL}(\mathrm{WBL})$ | $4.8(5.1)$ | $\mathrm{A}(\mathrm{A})$ | - |  |
| Abbott/Robert Grant (R) | $\mathrm{A}(\mathrm{A})$ | $8.8(9.0)$ | $\mathrm{NBL}(\mathrm{NBL})$ | $6.2(5.3)$ | $\mathrm{A}(\mathrm{A})$ | - |  |

Note: Analysis of signalized intersections assumes a PHF of 1.00 and a saturation flow rate of 1800 veh $/ \mathrm{h} /$ lane.
(S) - Signalized intersection.
(U) - Unsignalized intersection.
(R) - Roundabout intersection.

As shown in Table 10, the study area intersections 'as a whole' were shown to operate at a LOS ' B ' or better during peak hours. The critical movements were shown to operate at a LOS 'D' or better during peak hours.

## Future 2028 Total Background Conditions

The Future 2028 Total Background traffic volumes were shown in Figure 15. Synchro analysis results are summarized in Table 11 for critical movements and the intersection 'as a whole'.

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Table 11: Future 2028 Total Background Intersection Performance

| Intersection |  | Weekday AM Peak (PM Peak) |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Critical Movement |  |  | Intersection 'As a Whole' |  |  |  |
|  |  | max. v/c or <br> avg. delay (s) | Movement | Delay (s) | LOS | v/c |  |
| Fernbank/Robert Grant (S) | $\mathrm{B}(\mathrm{D})$ | $0.69(0.84)$ | WBT(WBT) | $21.5(27.6)$ | $\mathrm{A}(\mathrm{B})$ | $0.52(0.70)$ |  |
| Bobolink/Livery (U) | $\mathrm{A}(\mathrm{A})$ | $8.9(8.7)$ | $\mathrm{SB}(\mathrm{SB})$ | $3.4(3.3)$ | - | - |  |
| Bobolink/Robert Grant (R) | $\mathrm{B}(\mathrm{B})$ | $10.7(10.7)$ | $\mathrm{WBL}(\mathrm{EBL})$ | $5.5(5.5)$ | $\mathrm{A}(\mathrm{A})$ | - |  |
| Abbott/Robert Grant $(\mathrm{R})$ | $\mathrm{A}(\mathrm{A})$ | $9.0(9.1)$ | $\mathrm{NBL}(\mathrm{NBL})$ | $6.1(6.0)$ | $\mathrm{A}(\mathrm{A})$ | - |  |

Note: Analysis of signalized intersections assumes a PHF of 1.00 and a saturation flow rate of 1800 veh/h/lane.
(S) - Signalized intersection.
(U) - Unsignalized intersection.
(R) - Roundabout intersection.

As shown in Table 11, the study area intersection 'as a whole' were shown to operate at a LOS ' B ' or better during peak hours. The critical movements were shown to operate at a LOS 'D' or better during peak hours.

## Future 2023 Total Projected Conditions - Full Build-Out

The total projected 2023 traffic volumes were based on the site-generated traffic volumes (Figure 9) projected onto 2023 background traffic volumes (Figure 14). The resulting total projected traffic volumes are illustrated in Figure 17.


Table 12 below provides a summary of the critical Synchro analysis results at intersections within the study area, based on Future 2023 Total Projected traffic volumes.

## PARSONS

Table 12: Future 2023 Total Projected Performance at Study Area Intersections

| Intersection |  | Weekday AM Peak (PM Peak) |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Critical Movement |  |  | Intersection 'As a Whole' |  |  |
|  |  | max. v/c or <br> avg. delay (s) | Movement | Delay (s) | LOS | v/c |
| Fernbank/Robert Grant (S) | $\mathrm{B}(\mathrm{D})$ | $0.66(0.83)$ | WBT(WBT) | $20.9(26.4)$ | $\mathrm{A}(\mathrm{B})$ | $0.48(0.69)$ |
| Bobolink/Livery (U) | $\mathrm{A}(\mathrm{A})$ | $9.1(8.8)$ | SB(SB) | $5.0(4.8)$ | - | - |
| Bobolink/Robert Grant (R) | $\mathrm{A}(\mathrm{A})$ | $9.9(9.7)$ | WBL(WBL) | $5.5(5.9)$ | $\mathrm{A}(\mathrm{A})$ | - |
| Abbott/Robert Grant (R) | $\mathrm{A}(\mathrm{A})$ | $8.8(9.0)$ | NBL(NBL) | $5.9(5.6)$ | $\mathrm{A}(\mathrm{A})$ | - |

Note: Analysis of signalized intersections assumes a PHF of 1.00 and a saturation flow rate of $1800 \mathrm{veh} / \mathrm{h} /$ lane.
(S) - Signalized intersection. (U) - Unsignalized intersection. (R) - Roundabout intersection.

As shown in Table 12, the study area intersection 'as a whole' were shown to operate at a LOS 'B' or better during peak hours. The critical movements were shown to operate at a LOS ‘D' or better during peak hours.

## Future 2028 Total Projected Conditions -Build-Out plus Five Years

The Future 2028 Total Projected traffic volumes, shown in Figure 18, were derived by superimposing the site-generated traffic volumes (Figure 9) onto Future 2028 Total Background traffic volumes (Figure 15).

Figure 18: Future 2028 Total Projected Traffic Volumes


## PARSONS

Table 13 below provides a summary of the critical Synchro analysis results at intersections within the study area, based on Future 2028 Total Projected traffic volumes.

Table 13: Future 2028 Total Projected Performance at Study Area Intersections

| Intersection |  | Weekday AM Peak (PM Peak) |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Critical Movement |  |  | Intersection 'As a Whole' |  |  |
|  |  | max. v/c or <br> avg. delay (s) | Movement | Delay (s) | LOS | v/c |
| Fernbank/Robert Grant (S) | $\mathrm{B}(\mathrm{D})$ | $0.69(0.84)$ | WBT(WBT) | $21.8(27.4)$ | $\mathrm{A}(\mathrm{C})$ | $0.56(0.73)$ |
| Bobolink/Livery (U) | $\mathrm{A}(\mathrm{A})$ | $9.1(8.8)$ | $\mathrm{SB}(\mathrm{SB})$ | $5.0(4.8)$ | - | - |
| Bobolink/Robert Grant (R) | $\mathrm{B}(\mathrm{B})$ | $10.9(11.3)$ | $\mathrm{WBL}(\mathrm{EBL})$ | $6.1(6.2)$ | $\mathrm{A}(\mathrm{A})$ | - |
| Abbott/Robert Grant (R) | $\mathrm{A}(\mathrm{A})$ | $9.0(9.1)$ | NBL(NBL) | $6.0(6.2)$ | $\mathrm{A}(\mathrm{A})$ | - |

Note: Analysis of signalized intersections assumes a PHF of 1.00 and a saturation flow rate of 1800 veh/h/lane.
(S) - Signalized intersection.
(U) - Unsignalized intersection.
(R) - Roundabout intersection.

As shown in Table 13, the study area intersection 'as a whole' were shown to operate at a LOS ' C ' or better during peak hours. The critical movements were shown to operate at a LOS 'D' or better during peak hours.

## MMLOS Analysis for Signalized Intersections

A Multi-Modal Level of Service (MMLOS) analysis was conducted at the signalized intersection of Fernbank/Robert Grant. Since no changes are anticipated at this intersection in future horizon years, the analysis was conducted for existing conditions. Table 14 below provides a summary of the analysis results along with the respective targets provided in the City of Ottawa MMLOS Guidelines (Exhibit 22). The detailed MMLOS analysis sheet is provided in Appendix I. Red font indicates that the target LOS was not met.

Table 14: MMLOS Analysis at the Intersection of Fernbank/Robert Grant

| Signalized Intersection | Level of Service (LOS) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Pedestrian |  | Bicycle |  | Transit |  | Truck |  | Auto |  |
|  | PLOS | Target | BLOS | Target | TLOS | Target | TkLOS | Target | VLOS | Target |
| Fernbank / Robert Grant | B | C | F | C | E | D | E | E | D | D |

The target Levels of Service in Table 14 are based on a General Urban Area with an arterial road classification, spine route designation, transit priority (isolated measures) designation and no truck route. At the intersection of Fernbank/Robert Grant, the pedestrian, truck and auto LOS met their respective targets. However, the bicycle and transit LOS do not meet their respective targets.

With regards to cyclists, although cycle tracks are currently provided along both sides of Robert Grant Ave and a multi-use pathway along the north side of Fernbank Rd, the intersection does not meet the target LOS due to the high operating speeds along both Fernbank Rd and Robert Grant Ave, as well as the lack of a dedicated bike lane on the south side of Fernbank Rd. It should be noted that, based on the TIA Guidelines, the paved shoulders on the south side of Fernbank Rd do not count as a substitute for a dedicated bike lane in an urban setting.

With regards to transit, the target LOS is not met due to high delays to the SBL movement during the afternoon peak hour period only.

## 5. CONCLUSIONS AND RECOMMENDATIONS

The general findings, conclusions and recommendations from the preceding traffic analysis has been summarized below.

## PARSONS

In response to feedback received during the Public Open House on March 3rd, 2020, the following updates, as relevant to the TIA, were made to the proposal:

- The total number of apartment units was reduced to 504 total units.
- Construction of the tower portion (superstructure) of the 18 -storey building is subject to a holding provision until the extension of Robert Grant Ave from Abbott St to Hazeldean Rd is constructed.
- The request to reduce the parking ratios has been withdrawn by the proponent and replaced with a request to allow 16 surface parking spaces, while also allowing a reduction in the underground parking spaces based on Section 101(6)(c) in the City of Ottawa Parking Provisions.


## Proposed Development

- The proposed single-phase development will consist of 504 residential units, within one high-rise and two mid-rise apartment buildings and is expected to reach full build-out by 2023.
- Primary vehicle access is proposed via Robert Grant Avenue, which leads to an internal roundabout, a ramp to the underground parking garage and sixteen surface parking spaces.
- The main access intersection with Robert Grant Ave is expected to permit right-in/right-out only vehicular movements only.
- Secondary vehicular access is proposed via a full-movement driveway connection to Livery St, which leads directly to the underground parking garage.
- The proposed development is projected to generate 'new' two-way vehicle volumes of approximately 201 veh/h and 251 veh/h during the weekday morning and afternoon peak hours respectively.


## Existing and Background Conditions

- In existing conditions, all study area intersections operate at a LOS 'B' or better during morning and afternoon peak hours, with the exceptions of Fernbank/Robert Grant, which operates at LOS ‘D' during the afternoon peak hour.
- Multi-Modal Level of Service (MMLOS) analysis was conducted at the signalized intersection of Fernbank/Robert Grant. The analysis indicated that Bicycle LOS were not met due to the lack of a dedicated bike lane on the south side of Fernbank Rd, as well as the high operating speeds of Fernbank Rd and Robert Grant Ave. Transit LOS was also not met due to high delays in the SBL movement of the intersection. Pedestrian, Truck and Auto LOS all meet their respective MMLOS targets.
- Background traffic growth rate was assumed to be $2 \%$ at study area intersections.
- In future background 2023 and 2028 conditions, study area intersections are expected to operate similar to existing conditions, with slight variations in $\mathrm{v} / \mathrm{c}$ ratios and average delays.


## Projected Conditions

- In total projected 2023 and 2028 conditions, study area intersections operate similar to future background 2023 and 2028 conditions, with slight variations in v/c ratios and average delays.
- The study area intersections are expected to operate within City standards through to the 2028 horizon year.
- The adjacent road network classifications were shown to be appropriate based on the local context and projected traffic volumes.
- New road network modifications are not required to support this development based on the assumptions and results of this analysis.
- A total of 666 auto and 252 bicycle parking spaces are proposed. The parking proposed meets the parking provision requirements of the City of Ottawa, with an exemption applied for to permit 16 surface auto parking spaces.


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## Community Impacts

- Livery Street is a local road and projected traffic volumes are not expected to exceed the recommended thresholds.
- Bobolink is also classified as a local road, but transitions down from a collector road design at Robert Grant. The projected volumes reflect this transition, which was considered appropriate since Robert Grant is an arterial road, intended to accommodate higher traffic.
- It is important to remember that the surrounding community is still developing, and the area road network has yet to fully mature. Gaps in the neighbouring arterial/collector road network will be filled in, drawing traffic away from local streets, while transit service and active mode facilities will be constructed to help provide alternative travel choices for local residents.

Based on the foregoing results, the proposed Lépine Development can be accommodated by the adjacent transportation network and is recommended to proceed from a transportation perspective.

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Reviewed By:


Austin Shih, M.A.Sc., P.Eng. Senior Transportation Engineer

## Appendix A

Screening Form and Correspondence

City of Ottawa 2017 TIA Guidelines
Date
12/12/2018
TIA Screening Form

| Results of Screening | Project Number | $476799-01000$ |
| :--- | :---: | :---: |
| Development Satisfies the Trip Generation Trigger | Yes/No |  |
| Development Satisfies the Location Trigger | Yes |  |
| Development Satisfies the Safety Trigger | Yes |  |


| Module 1.1 - Description of Proposed Development |  |
| :--- | :--- |
| Municipal Address | 1000 Robert Grant |
|  | Midblock between Fernbernak Road and Abbott Street East, located <br> on the east side of Robert Grant Avenue. Currently vacant lots. |
| Description of location | Residential - Apartment |
| Land Use | 566 units |
| Development Size | 2 Total: 1 off Robert Grant/ 1 off Livery St |
| Number of Accesses and Locations | Assume Single Phase for Zoning |
| Development Phasing | 2024 (5 year horizon) |
| Buildout Year | See Figure 2 |
| Sketch Plan / Site Plan |  |


| Module 1.2 - Trip Generation Trigger |  |  |
| :--- | :---: | :--- |
| Land Use Type | Townhomes or Apartments |  |
| Development Size | 566 | Units |
| Trip Generation Trigger Met? | Yes |  |

## Module 1.3 - Location Triggers

Development Proposes a new driveway to a boundary street
that is designated as part of the City's Transit Priority, Rapid Yes
Transit, or Spine Bicycle Networks (See Sheet 3)
Development is in a Design Priority Area (DPA) or Transit-
oriented Development (TOD) zone. (See Sheet 3)
Location Trigger Met? Yes

| Module 1.4 - Safety Triggers |  | $<80$ |
| :--- | :--- | :--- |
| Posted Speed Limit on any boundary road h <br> Horizontal / Vertical Curvature on a boundary street limits  <br> sight lines at a proposed driveway  | No |  |
| A proposed driveway is within the area of influence of an <br> adjacent traffic signal or roundabout (i.e. within 300 m of <br> intersection in rural conditions, or within 150 m of <br> intersection in urban/ suburban conditions) or within auxiliary <br> lanes of an intersection; | Yes | No |
| A proposed driveway makes use of an existing median break <br> that serves an existing site <br> There is a documented history of traffic operations or safety <br> concerns on the boundary streets within 500 m of the <br> development <br> The development includes a drive-thru facility <br> Safety Trigger Met? | No |  |

19 June 2020

City of Ottawa
Development Review Services
110 Laurier Avenue West
Ottawa, ON K1P 1J1

Attention: Josiane Gervais, P.Eng.

Dear Josiane:

## Re: Rene's Court - 1000 Robert Grant Avenue Step 5 - Comment and Response Form

The following response form has been prepared to address City of Ottawa comments received on November 27th, 2019. City comments are noted in black with the corresponding responses from Parsons in blue.

## DEVELOPMENT REVIEW - TRANSPORTATION SECTION

Comment 1: Re Comment 1 above: Assuming a mode share target of $0 \%$ for cycling does not reflect the City's vision as outlined within the Ottawa Cycling Plan.

Response 1: Noted. A 0\% cycling value reflects a theoretical worst-case scenario (most conservative scenario).

Comment 2: At the preconsultation, there was no mention of a requested reduction of parking to be included within the re-zoning application. Since a reduction in parking is now sought, the applicant is to provide justification for the reduction in parking proposed. Module 4.2 - Parking is to be included within the TIA.

Response 2: The applicant has withdrawn the request to reduce the parking ratios of the proposed development. Instead, a new request is being made to allow 16 surface parking spaces to be provided, while also permitting the reduction in underground parking spaces based on Section 101(6)(C) of the City of Ottawa Parking Provisions. Further description is provided in Section 4.2 in the TIA report.

## Appendix B

Transit Route Maps

TERRY FOX STITTSVILLE
TUNNEY'S PASTURE

7 days a week / 7 jours par semaine
All day service
Service toute la journée

$=$ Transitway \& Station
IIIIIIIIII Monday to Friday only (limited evening service) Lundi au vendredi seulement (service de soirée limité)
Park \& Ride / Parc-o-bus
Timepoint / Heures de passage


Starting July 14, 2019 À partir du 14 juillet 2019

## Monday to Friday/ Lundi au vendredi

Selected time periods
Périodes selectionnées


O Transitway Station / Station du Transitway
(F) Park \& Ride / Parc-o-bus
$\Delta$ Timepoint / Heures de passage

Customer Service
Service à la clientèle . . . . . . . . . . . . . . . 613-741-4390
Lost and Found / Objets perdus......613-563-4011
Security / Sécurité
613-741-2478
Effective December 24, 2017
En vigueur 24 décembre 2017
INFO 613-741-4390 octranspo.com

## 252

## FERNBANK

TUNNEY'S PASTURE

## Connexion

## Monday to Friday / Lundi au vendredi

Peak periods only
Périodes de pointe seulement

$=$ Transitway \& Station
Limited stops: Off only in AM / No stop in PM Arrêts limités : Débarquement en AM seul. / Aucun arrêt en PM
AM: Off only - PM: Full Service AM: Débarquement seul. - PM: Service complet


## Future route after 0-Train Line 1 is open

Trajet du circuit après l'ouverture de la Ligne 1 de $\mathrm{I}^{\prime} 0$-Train

## Appendix C

Traffic Data

Turning Movement Count Summary, AM and PM Peak Hour

## Abbott Street (East) \& Robert Grant Avenue (Roundabout)

## Stittsville, ON




Turning Movement Count
Heavy Vehicle Summary Flow Diagram

Heavy Trucks, Buses, and School Buses

## Abbott Street (East) \& Robert Grant Avenue (Roundabout)



Abbott Street (East) \& Robert Grant Avenue (Roundabout)

Survey Date: Tuesday, 8 January 2019
Weather - AM: Overcast $-10^{\circ} \mathrm{C}$
Weather-PM: Overcast $+4^{\circ} \mathrm{C}$

| Time Period | Abbott St. (E) |  |  |  |  | Abbott St. (E) |  |  |  |  | Robert Grant Ave. |  |  |  |  | N/A |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | LT | Eastbound |  |  |  | Westbound |  |  |  |  | LT |  |  |  |  | Southbound |  |  |  |  |  |
| 0700-0800 | 0 | 3 | 5 |  | 9 | 2 | 3 | 0 | 0 | 5 | 4 | 0 | 1 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 19 |
| 0800-0900 | 0 | 2 | 14 | 0 | 16 | 3 | 5 | 0 | 0 | 8 | 8 | 0 | 1 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 33 |
| 0900-1000 | 0 | 1 | 6 | 1 | 8 | 0 | 1 | 0 | 0 | 1 | 11 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 0 |  | 20 |
| 1130-1230 | 0 | 1 | 2 | 0 | 3 | 1 | 1 | 0 | 0 | 2 | 4 | 0 | 3 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 12 |
| 1230-1330 | 0 | 3 | 9 | 0 | 12 | 0 | 3 | 0 | 0 | 3 | 5 | 0 | 0 | 0 | 5 | 0 | 0 | 0 |  | 0 | 20 |
| 1500-1600 | 0 | 2 | 11 | 0 | 13 | 0 | 3 | 0 | 0 | 3 | 8 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 24 |
| 1600-1700 | 0 | 0 | 4 | 0 | 4 | 0 | 2 | 0 | 0 | 2 | 11 | 0 | 2 | 0 | 13 | 0 | 0 | 0 | 0 | 0 | 19 |
| 1700-1800 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 3 |
| Totals | 0 | 12 | 52 | 2 | 66 | 6 | 18 | 0 | 0 | 24 | 53 | 0 | 7 | 0 | 60 | 0 | 0 | 0 | 0 | 0 | 150 |

Turning Movement Count
Pedestrian Crossings Summary and Flow Diagram

Stittsville, ON

## Abbott Street (East) \& Robert Grant Avenue (Roundabout)



Abbott Street (East) \& Robert Grant Avenue (Roundabout)
Survey Date: Tuesday, 8 January $2019 \quad$ Start Time:
Weather-AM Overcast $-10^{\circ} \mathrm{C}$ Survey Duration: 8 Hrs. Survey Hours:

0700
0700-1000, 1130-1330 \& 1500-1800

Weather - PM: Overcast $+4^{\circ} \mathrm{C}$

| Time Period | West Side Crossing Abbott St. (E) | $\begin{aligned} & \text { East Side Crossing } \\ & \text { Abbott St. (E) } \end{aligned}$ | $\begin{aligned} & \text { Streat } \\ & \text { Total } \end{aligned}$ | South Side Crossing Robert Grant Ave. | North Side Crossing N/A | $\begin{aligned} & \text { Street } \\ & \text { Total } \end{aligned}$ | $\begin{aligned} & \text { Grand } \\ & \text { Total } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0700-0800 | 0 | , | 1 | 4 | 0 | 4 | 5 |
| 0800-0900 | 2 | 2 | 4 | 2 | 0 | 2 | 6 |
| 0900-1000 | 5 | 1 | 6 | 5 | 0 | 5 | 11 |
| 1130-1230 | 2 | 0 | 2 | 6 | 0 | 6 | 8 |
| 1230-1330 | 10 | 5 | 15 | 8 | 0 | 8 | 23 |
| 1500-1600 | 20 | 0 | 20 | 29 | 0 | 29 | 49 |
| 1600-1700 | 3 | 2 | 5 | 8 | 0 | 8 | 13 |
| 1700-1800 | 0 | 0 | 0 | 1 | 0 | 1 | 1 |
| Totals | 42 | 11 | 53 | 63 | 0 | 63 | 116 |

## Abbott Street (East) \& Robert Grant Avenue (Roundabout)

Survey Date: Tuesday, 8 January 2019
Weather - AM: Overcast $-10^{\circ} \mathrm{C}$
Weather - PM: Overcast $+4^{\circ} \mathrm{C}$

Start Time: Survey Duration:

8 Hrs. Survey Hours: Surveyor(s):

0700
0700-1000, 1130-1330 \& 1500-1800
Carmody

|  | Abbott St. (E) |  |  |  |  | Abbott St. (E) |  |  |  |  |  | Robert Grant Ave. |  |  |  |  | N/A |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  |  |  | Westbound |  |  |  |  |  | Northbound |  |  |  |  | Southbound |  |  |  |  |  |  |
| Time Period | LT | ST | RT | UT | $\begin{array}{\|l\|} \hline \text { E/B } \\ \text { Tot } \end{array}$ | LT | ST | RT | UT | $\begin{aligned} & \text { W/B } \\ & \text { Tot } \end{aligned}$ | Street <br> Total | LT | ST | RT | UT | $\begin{aligned} & \text { N/B } \\ & \text { Tot } \end{aligned}$ | LT | ST | RT | UT | $\begin{aligned} & \mathrm{S} / \mathrm{B} \\ & \mathrm{Tot} \end{aligned}$ | $\begin{array}{\|c\|} \hline \text { Street } \\ \text { Total } \end{array}$ | $\begin{array}{c\|} \hline \text { Grand } \\ \text { Total } \\ \hline \end{array}$ |
| 0700-0800 | 0 | 25 | 81 | 6 | 112 | 7 | 31 | 0 | 0 | 38 | 150 | 176 | 0 | 15 |  | 192 | 0 | 0 | 0 | 0 | 0 | 192 | 342 |
| 0800-0900 | 0 | 22 | 117 | 16 | 155 | 14 | 52 | 0 | 2 | 68 | 223 | 204 | 0 | 21 |  | 226 | , |  | 0 | 0 | 0 | 226 | 449 |
| 0900-1000 | 0 | 32 | 81 | 27 | 140 | 14 | 30 | 0 | 1 | 45 | 185 | 164 | 0 | 14 | 2 | 180 | 0 | 0 | 0 | 0 | 0 | 180 | 365 |
| 1130-1230 | 0 | 22 | 101 | 6 | 129 | 11 | 25 | 0 |  | 36 | 165 | 89 | 0 | 26 | 0 | 115 | 0 | 0 | 0 | 0 | 0 | 115 | 280 |
| 1230-1330 | 0 | 31 | 116 | 5 | 152 | 10 | 33 | 0 | 0 | 43 | 195 | 126 | 0 | 17 | 0 | 143 | 0 | 0 | 0 | 0 | 0 | 143 | 338 |
| 1500-1600 | 0 | 52 | 194 | 28 | 274 | 24 | 54 | 0 | 1 | 79 | 353 | 156 | 0 | 8 | 0 | 164 | 0 | 0 | 0 | 0 | 0 | 164 | 517 |
| 1600-1700 | 0 | 19 | 210 | 2 | 231 | 13 | 43 | 0 | 0 | 56 | 287 | 154 | 0 | 8 | 0 | 162 | 0 | 0 | 0 | 0 | 0 | 162 | 449 |
| 1700-1800 | 0 | 38 | 193 | 2 | 233 | 11 | 40 | 0 | 0 | 51 | 284 | 151 | 0 | 4 |  | 156 | 0 | 0 | 0 | 0 | 0 | 156 | 440 |
| Totals | 0 | 241 | 1093 | 92 | 1426 | 104 | 308 | 0 | 4 | 416 | 1842 | 1220 | 0 | 113 | 5 | 1338 | 0 | 0 | 0 | 0 | 0 | 1338 | 3180 |

Equivalent 12 \& 24-hour Vehicle Volumes Including the Annual Average Daily Traffic (AADT) Factor Applicable to the Day and Month of the Turning Movement Count
$\Rightarrow$ Expansion factors are applied exclusively to standard weekday 8-hour turning movement counts

| Equivalent 12-hour vehicle volumes. These volumes are calculated by multiplying the 8-hour totals by the $8 \boldsymbol{\phi}$ 12 expansion factor of 1.39 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Equ. 12 Hr | 0 | 335 | 1519 | 128 | 1982 | 145 | 428 | 0 | 6 | 578 | 2560 | 1696 | 0 | 157 | 7 | 1860 | 0 | 0 | 0 |  | 01 | 1860 | 4420 |
| Average daily 12 -hour vehicle volumes. These volumes are calculated by multiplying the equivalent 12-hour totals by the AADT factor of: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| AADT 12-hr | 0 | 368 | 1671 | 141 | 2180 | 159 | 471 | 0 | 6 | 636 | 2816 | 1865 | 0 | 173 | 81 | 2046 | 0 | 0 | 0 | 0 | 0 | 2046 | 4862 |
| 24-Hour AADT. These volumes are calculated by multiplying the average daily 12 -hour vehicle volumes by the $\mathbf{1 2 \boldsymbol { m }} \mathbf{2 4}$ expansion factor of 1.31 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| AADT 24 Hr | 0 | 483 | 2189 | 184 | 2856 | 208 | 617 | 0 | 8 | 833 | 3690 | 2444 | 0 | 226 | 10 | 2680 | 0 | 0 | 0 | I | 0 | 2680 | 6370 |
| AM Peak Hour Factor $\Rightarrow 0.80$ |  |  |  |  | TOT | LT | ST | RT | UT | TOT S.tOT |  | LT | Highest Hourly Vehicle Volume between 0700h \& 1000h |  |  |  |  |  |  |  |  |  |  |
| AM Peak Hr | LT | ST | RT | UT |  |  |  |  |  |  |  | ST | RT | UT | TOT | LT | ST | RT | UT | TOT | S.TOT | G.TOT |
| 0745-0845 | 0 | 21 | 123 | 11 | 155 | 14 | 54 | 0 | 1 | 69 | 224 |  | 219 | 0 | 18 | 2 | 239 | 0 | 0 | 0 | 0 | 0 | 239 | 463 |
| OFF Peak Hour Factor $\Rightarrow \quad 0.88$ |  |  |  |  |  |  |  |  |  |  |  |  | Highest Hourly Vehicle Volume between 1130h \& 1330h |  |  |  |  |  |  |  |  |  |  |
| Off Peak Hr | LT | ST | RT | UT | TOT | LT | ST | RT | UT | TOT | S.TOT | LT | ST | RT | UT | TOT | LT | ST | RT | UT | TOT | S.TOT | G.TOT |
| 1230-1330 | 0 | 31 | 116 | 5 | 152 | 10 | 33 | 0 | 0 | 43 | 195 | 126 | 0 | 17 | 0 | 143 | 0 | 0 | 0 | 0 | 0 | 143 | 338 |
| PM Peak Hour Factor $\Rightarrow 0.80$ |  |  |  |  | TOT | LT | ST | RT | UT | TOT | S.TOT | LT |  |  | UT | TOT | LT | Volu | RT | UT | n 1500h \& 1800h |  |  |
| PM Peak Hr | LT | ST | RT | UT |  |  |  |  |  |  |  |  |  |  | TOT |  |  |  |  |  | S.TOT | G.TOT |
| 1515-1615 | 0 | 48 | 226 | 24 | 298 | 27 | 57 | 0 | 1 | 85 | 383 | 163 | 0 | 6 |  | 0 | 169 | 0 | 0 | 0 | 0 | 0 | 169 | 552 |

## Comments

Robert Grant Avenue not constructed north of Abbott Street. The majority of the eastbound U-Turns are associated with school related activity. There are quite a few homes under construction is this area with more land to be developed.

## Notes:

1. Includes all vehicle types except bicycles and electric scooters.
2. Expansion factors are not applied to turning movement counts if they are less than 8 -hours in duration.
3. When expansion and AADT factors are applied, the results will differ slightly due to rounding.

## Disclaimer:

The information contained in this data summary is for information purposes only, and may not apply to your situation. Every effort is made to ensure the traffic count information is accurate for the survey date provided on the summary and flow diagram forms. The author, publisher, and distributor provide no warranty about the content or accuracy of either the data summary or flow diagrams. Information provided is subjective. The author, publisher, and distributor shall not be liable for any loss of profit or any other commercial damages resulting from use of this data.

Turning Movement Count
Bicycle Summary
Flow Diagram


## Comments:

The majority of southbound drivers on Livery Street - either left turns or right turns do a rolling stop.

Turning Movement Count Summary, AM and PM Peak Hour

Flow Diagrams

Automobiles, Taxis, Light
Trucks, Vans, SUV's,
Motorcycles, Heavy Trucks, Buses, and School Buses

## Bobolink Ridge \& Livery Street

## Stittsville, ON



Turning Movement Count Summary, OFF and EVENING Peak Hour Flow Diagrams

Automobiles, Taxis, Light Trucks, Vans, SUV's, Motorcycles, Heavy Trucks, Buses, and School Buses

## Bobolink Ridge \& Livery Street

## Stittsville, ON



Turning Movement Count
Pedestrian Crossings Summary and Flow Diagram

Stittsville, ON


| Time Period | West Side Crossing <br> Bobolink Ridge | East Side Crossing <br> Bobolink Ridge | Street <br> Total | South Side Crossing <br> N/A | North Side Crossing <br> Livery St. | Street <br> Total | Grand <br> Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{0 7 0 0 - 0 8 0 0}$ | 0 | 0 | 0 | 0 | 1 | 1 | 1 |
| $0800-0900$ | 0 | 1 | 1 | 0 | 10 | 10 | 11 |
| $0900-1000$ | 1 | 1 | 2 | 0 | 1 | 1 | 3 |
| $1130-1230$ | 0 | 0 | 0 | 0 | 2 | 2 | 2 |
| $1230-1330$ | 0 | 0 | 0 | 0 | 2 | 2 | 2 |
| $1500-1600$ | 0 | 0 | 0 | 0 | 3 | 3 | 3 |
| $1600-1700$ | 1 | 0 | 1 | 0 | 5 | 5 | 6 |
| $1700-1800$ | 1 | 0 | 1 | 0 | 11 | 11 | 12 |
| Totals | 3 | 2 | 5 | 0 | 35 | 35 | 40 |

Comments:
The majority of southbound drivers on Livery Street - either left turns or right turns do a rolling stop.

# Turning Movement Count 

Summary Report
AADT and Expansion Factors


Equivalent 12 \& 24-hour Vehicle Volumes Including the Annual Average Daily Traffic (AADT) Factor Applicable to the Day and Month of the Turning Movement Count
Expansion factors are applied exclusively to standard weekday 8-hour turning movement counts conducted during the hours of $0700 \mathrm{~h}=1000 \mathrm{~h}, 1130 \mathrm{~h}=1330 \mathrm{~h}$ and $1500 \mathrm{~h}=1800 \mathrm{~h}$


## Comments:

The majority of southbound drivers on Livery Street - either left turns or right turns do a rolling stop.

## Notes:

1. Includes all vehicle types except bicycles, electric bicycles, and electric scooters.
2.When expansion and AADT factors are applied, the results will differ slightly due to rounding.

Turning Movement Count Summary, AM and PM Peak Hour

Flow Diagrams


Turning Movement Count Summary, OFF and EVENING PEAK Hour Flow Diagrams

## Bobolink Ridge \& Robert Grant Avenue (Roundabout)

## Stittsville, ON

 Turning Movement Count

Heavy Vehicle Summary and School Buses Flow Diagram

## Bobolink Ridge \& Robert Grant Avenue (Roundabout)

Stittsville, ON


Bobolink Ridge \& Robert Grant Avenue (Roundabout)

Survey Date: Tuesday, 8 January 2019
Weather - AM: Overcast $-10^{\circ} \mathrm{C}$
Weather - PM: Overcast $+4^{\circ} \mathrm{C}$

|  | Bobolink Ridge |  |  |  |  | Bobolink Ridge |  |  |  |  | Robert Grant Ave. |  |  |  |  | Robert Grant Ave. <br> Southbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Period | LT | ST | RT | UT | S. Tot | LT | ST | RT | UT | S. Tot | LT | ST | RT | UT | S. Tot | LT | ST | RT | UT | S. Tot | G.Tot. |
| 0700-0800 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 0 | 2 | 1 |  | 2 | 0 | 4 | 1 | 5 | 1 | 0 | 7 | 14 |
| 0800-0900 | 0 | 0 | 1 | 0 |  |  | 0 | 1 | 0 |  |  | 9 | 2 | 0 | 12 | 5 | 8 |  | 0 | 14 | 28 |
| 0900-1000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 |  | 3 | 10 | 0 | 0 | 13 | 1 | 6 | 0 | 0 | 7 | 21 |
| 1130-1230 | 1 | 0 | 3 | 0 | 4 | 1 | 0 | 2 | 0 | 3 | 2 | 4 | 0 | 0 | 6 | 0 | 4 | 0 | 0 | 4 | 17 |
| 1230-1330 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 2 | 4 | 1 | 0 | 7 | 2 | 5 |  | 0 | 8 | 17 |
| 1500-1600 | 1 | 0 | 1 | 0 | 2 | 2 | 0 | 1 | 0 | 3 | 1 | 6 | 1 | 0 | 8 | 1 | 10 | 1 | 0 | 12 | 25 |
| 1600-1700 | 2 | 0 | 3 | 0 | 5 | 2 | 0 | 3 | 0 | 5 |  | 8 | 0 | 0 | 9 | 1 | 3 | 0 | 0 | 4 | 23 |
| 1700-1800 | 0 | 0 | 0 |  | 0 | 0 | , | 1 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 1 | 1 |  | 0 | 2 | 4 |
| Totals | 5 | 0 | 8 | 0 | 13 | 5 | 0 | 13 | 0 | 18 | 11 | 43 | 6 | 0 | 60 | 12 | 42 | 4 | 0 | 58 | 149 | Turning Movement Count

Pedestrian Crossings Summary and Flow Diagram

Stittsville, ON

## Bobolink Ridge \& Robert Grant Avenue (Roundabout)



Robert Grant Ave.


Tuesday, 8 January 2019 0700-1000, 1130-1330 \& 1500-1800 8 Hours
City of Ottawa Ward 6


Bobolink Ridge \& Robert Grant Avenue (Roundabout)

Survey Date: Tuesday, 8 January 2019
Weather-AM Overcast $-10^{\circ} \mathrm{C}$
Weather - PM: Overcast $+4^{\circ} \mathrm{C}$

Start Time:
8 Hrs. Survey Hours:

0700
0700-1000, 1130-1330 \& 1500-1800

| Time Period | West Side Crossing Bobolink Ridge | East Side Crossing Bobolink Ridge | $\begin{aligned} & \text { Street } \\ & \text { Total } \end{aligned}$ | South Side Crossing Robert Grant Ave. | North Side Crossing Robert Grant Ave. | Street Total | $\begin{aligned} & \text { Grand } \\ & \text { Total } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0700-0800 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0800-0900 | 0 | 2 | 2 | 0 | 0 | 0 | 2 |
| 0900-1000 | 0 | 1 | 1 | 0 | 0 | 0 | 1 |
| 1130-1230 | 0 | 2 | 2 | 0 | 0 | 0 | 2 |
| 1230-1330 | 0 | 5 | 5 | 0 | 0 | 0 | 5 |
| 1500-1600 | 0 | 4 | 4 | 0 | 0 | 0 | 4 |
| 1600-1700 | 0 | 7 | 7 | 0 | 0 | 0 | 7 |
| 1700-1800 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Totals | 0 | 21 | 21 | 0 | 0 | 0 | 21 |

# Turning Movement Count Summary Report Including AM/PM Peak Hours, PHF, AADT and Expansion Factors 

|  |  | Tuesd <br> Overc <br> Overc | day, 8 <br> cast - <br> cast + |  | ry 2 |  | Surve | y Dura | ation: |  | Hrs. | Start Surv Surv | Time | urs: <br> s): |  | $\begin{aligned} & 0700 \\ & 0700- \\ & \text { Carm } \end{aligned}$ | $\begin{aligned} & -1000 \\ & \text { ody } \end{aligned}$ | $\text { , } 1130$ | $\begin{aligned} & \text { AAD } \\ & \text { D-1330 } \end{aligned}$ | TFa | $\begin{aligned} & \text { ctor: } \\ & 500-1 \end{aligned}$ |  | 1.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | obol | ink | Ridg |  |  |  | link | Ridg |  |  |  | ert | Gra | nt | Ave. |  | ert | Gran | nt | Ave. |  |  |
|  |  |  | stbound |  |  |  |  | estbound |  |  |  |  |  | thbou |  |  |  | Sou | thbou |  |  |  |  |
| Time Period | LT | ST | RT | UT | $\begin{aligned} & \text { E/B } / 8 . \end{aligned}$ | LT | ST | RT | UT | $\begin{gathered} \hline \text { W/B } \\ \text { Tot } \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { Street } \\ \text { Total } \end{array}$ | LT | ST | RT | UT | $\begin{aligned} & \hline \text { N/B } \\ & \text { Tot } \end{aligned}$ | LT | ST | RT | UT | $\begin{aligned} & \hline \mathrm{S} / \mathrm{B} \\ & \mathrm{Tot} \end{aligned}$ | $\begin{array}{\|c\|} \hline \text { Street } \\ \text { Total } \end{array}$ | $\begin{array}{\|c\|} \hline \text { Grand } \\ \text { Total } \end{array}$ |
| 0700-0800 | 1 | 0 | 0 | 0 | 1 | 20 | 0 | 57 | 0 | 77 | 78 | 5 | 138 | 7 | 0 | 150 | 12 | 70 | 4 | 0 | 86 | 236 | 314 |
| 0800-0900 | 0 | 0 | 3 | 0 | 3 | 23 | 0 | 73 | 0 | 96 | 99 | 2 | 163 | 16 | 0 | 181 | 28 | 99 | 3 | 0 | 130 | 311 | 410 |
| 0900-1000 | 0 | 1 | 2 | 0 | 3 | 19 | 1 | 60 |  | 81 | 84 | 6 | 105 | 14 | 0 | 125 | 20 | 70 | 4 | 0 | 94 | 219 | 303 |
| 1130-1230 | 3 | 1 | 6 | 0 | 10 | 11 | 4 | 38 | 0 | 53 | 63 | 4 | 67 | 15 | 0 | 86 | 36 | 77 | 2 |  | 116 | 202 | 265 |
| 1230-1330 | 4 | 0 | 4 | 0 | 8 | 13 | 0 | 39 | 0 | 52 | 60 | 8 | 94 | 18 | 0 | 120 | 43 | 79 | 3 | 0 | 125 | 245 | 305 |
| 1500-1600 | 4 | 1 | 3 | 0 | 8 | 17 | 1 | 42 | 0 | 60 | 68 | 1 | 120 | 22 | 0 | 143 | 65 | 148 | 2 |  | 216 | 359 | 427 |
| 1600-1700 | 3 | 2 | 4 | 0 | 9 | 21 | 0 | 35 | 0 | 56 | 65 | 1 | 128 | 34 |  | 164 | 61 | 158 | 3 |  | 222 | 386 | 451 |
| 1700-1800 | 2 | 1 | 3 | 0 | 6 | 13 | 0 | 39 | 0 | 52 | 58 | 0 | 117 | 30 | 0 | 147 | 72 | 132 | 1 | 0 | 205 | 352 | 410 |
| Totals | 17 | 6 | 25 | 0 | 48 | 137 | 6 | 383 | 1 | 527 | 575 | 27 | 932 | 156 | 1 | 1116 | 337 | 833 | 22 | 2 | 1194 | 2310 | 2885 |

## Equivalent 12 \& 24-hour Vehicle Volumes Including the Annual Average Daily Traffic (AADT) Factor Applicable to the Day and Month of the Turning Movement Count

$\Rightarrow$ Expansion factors are applied exclusively to standard weekday 8-hour turning movement counts

| Equivalent 12-hour vehicle volumes. These volumes are calculated by multiplying the 8 -hour totals by the $\mathbf{8} \boldsymbol{\$ 1 2}$ expansion factor of 1.39 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Equ. 12 Hr | 24 | 8 |  | I | 67 | 190 | 8 | 532 |  | 733 | 799 | 38 | 1295 | 217 |  | 1551 | 468 | 1158 | 31 |  | 1660 | 3211 | 4010 |
| Average daily 12-hour vehicle volumes. These volumes are calculated by multiplying the equivalent 12-hour totals by the AADT factor of: 1.0 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| AADT 12-hr | 24 | 8 | 35 | 01 | 67 | 190 | 8 | 532 |  | 733 | 799 | 38 | 1295 | 217 | 1 | 1551 | 468 | 1158 | 31 | 31 | 1660 | 3211 | 4010 |
| 24-Hour AADT. These volumes are calculated by multiplying the average daily 12 -hour vehicle volumes by the $12 \boldsymbol{\rightarrow} \mathbf{2 4}$ expansion factor of 1.31 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| AADT 24 Hr | 31 | 11 | 46 | I | 87\| | 249 | 11 | 697 |  | 960 | 1047 | 49 | 1697 | 284 | 2 | 2032 | 614 | 1517 | 40 | 4 | 2174 | 4206 | 5253 |
| AM Peak Hour Factor $\Rightarrow 0.90$ |  |  |  |  | TOT | LT | ST | RT | UT | $\begin{array}{r} \text { TOT } \\ \hline \quad 95 \\ \hline \end{array}$ | S.TOT | LT |  | Highest Hourly Vehicle Volume between 0700h \& 1000h |  |  |  |  |  |  |  |  |  |
| AM Peak Hr | LT | ST | RT | UT |  |  |  |  |  |  |  |  | ST | RT | UT | TOT | LT | ST | RT | UT | TOT | S.TOT | G.TOT |
| 0745-0845 | 1 | 0 | 2 | 0 | 3 | 22 | 0 | 73 | 0 |  | 98 | 2 | 164 | 12 | 0 | 178 | 28 | 105 | 5 | 0 | 138 | 316 | 414 |
| OFF Peak Hour Factor $\Rightarrow 0.91$ |  |  |  |  |  |  |  |  |  |  |  |  |  | Highest Hourly Vehicle Volume between 1130h \& 1330h |  |  |  |  |  |  |  |  |  |
| Off Peak Hr | LT | ST | RT | UT | TOT | LT | ST | RT | UT | TOT | S.TOT | LT | ST | RT | UT | TOT | LT | ST | RT | UT | TOT | S.TOT | G.TOT |
| 1230-1330 | 4 | 0 | 4 |  | 8 | 13 | 0 | 39 | 0 | 52 | 60 | 8 | 94 | 18 | 0 | 120 | 43 | 79 | 3 | 0 | 125 | 245 | 305 |
| PM Peak Hour Factor $\Rightarrow 0.93$ |  |  |  |  | TOT | LT | ST | RT | UT | TOT | S.TOT | LT | High |  | UT | TOT | LT | VT | RT | UT | TOT | Oh \& 1800h |  |
| PM Peak Hr | LT | ST | RT | UT |  |  |  |  |  |  |  |  |  |  | S.TOT |  |  |  |  |  |  | G.TOT |
| 1530-1630 | 3 | 0 | 7 | 0 | 10 | 18 | 1 | 35 | 0 | 54 | 64 | 2 | 126 | 35 |  | 0 | 163 | 72 | 182 | 4 | 0 | 258 | 421 | 485 |

## Comments

Bobolink Ridge, west of Robert Grant Avenue, is not yet open to traffic. It is currently a construction access only.

## Notes:

1. Includes all vehicle types except bicycles and electric scooters.
2. Expansion factors are not applied to turning movement counts if they are less than 8 -hours in duration.
3. When expansion and AADT factors are applied, the results will differ slightly due to rounding.

## Disclaimer:

The information contained in this data summary is for information purposes only, and may not apply to your situation. Every effort is made to ensure the traffic count information is accurate for the survey date provided on the summary and flow diagram forms. The author, publisher, and distributor provide no warranty about the content or accuracy of either the data summary or flow diagrams. Information provided is subjective. The author, publisher, and distributor shall not be liable for any loss of profit or any other commercial damages resulting from use of this data.

## Transportation Services - Traffic Services

## Turning Movement Count - Peak Hour Diagram

## FERNBANK RD @ ROBERT GRANT AVE

Survey Date: Thursday, August 30, 2018
Start Time: 07:00

WO No: 38041
Device: Miovision


Comments

## Transportation Services - Traffic Services

## Turning Movement Count - Peak Hour Diagram

## FERNBANK RD @ ROBERT GRANT AVE

Survey Date: Thursday, August 30, 2018
Start Time: 07:00

WO No: 38041
Device: Miovision


Comments

## Transportation Services - Traffic Services

## Turning Movement Count - Peak Hour Diagram

## FERNBANK RD @ ROBERT GRANT AVE

Survey Date: Thursday, August 30, 2018
Start Time: 07:00

WO No: 38041
Device: Miovision


Comments

## Transportation Services - Traffic Services

## Turning Movement Count - Peak Hour Diagram

## FERNBANK RD @ ROBERT GRANT AVE

Survey Date: Thursday, August 30, 2018
Start Time: 07:00

WO No: 38041
Device: Miovision


Comments

## ( $)$ ttawa Transportation Services - Traffic Services Turning Movement Count - Full Study Diagram

## FERNBANK RD @ ROBERT GRANT AVE

Survey Date: Thursday, August 30, 2018
WO\#: 38041
Device: Miovision


Comments

Transportation Services - Traffic Services

## Turning Movement Count - Full Study Summary Report

## FERNBANK RD @ ROBERT GRANT AVE

Survey Date: Thursday, August 30, 2018

| Total Observed U-Turns |  |  |  |
| :---: | :---: | :---: | :---: |
| Northbound: | 0 | Southbound: | 0 |
| Eastbound: | 0 | Westbound: | 2 |

AADT Factor
.90

Full Study
ROBERT GRANT AVE

|  | Northbound |  |  | Southbound |  |  |  |  |  | Eastbound |  |  |  | Westbound |  |  |  | $\begin{aligned} & \text { STR } \\ & \text { TOT } \\ & \hline \end{aligned}$ | Grand Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period | LT | ST | RT | $\begin{array}{r} \text { NB } \\ \text { TOT } \end{array}$ | LT | ST | RT | $\begin{array}{r} \text { SB } \\ \text { TOT } \end{array}$ | $\begin{aligned} & \text { STR } \\ & \text { TOT } \end{aligned}$ | LT | ST | RT | $\begin{array}{r} \text { EB } \\ \text { TOT } \end{array}$ | LT | ST | RT | $\begin{aligned} & \text { WB } \\ & \text { TOT } \end{aligned}$ |  |  |
| 07:00 08:00 | 0 | 0 | 0 | 0 | 114 | 0 | 13 | 127 | 127 | 25 | 302 | 0 | 327 | 0 | 122 | 128 | 250 | 577 | 704 |
| 08:00 09:00 | 0 | 0 | 0 | 0 | 125 | 0 | 27 | 152 | 152 | 28 | 329 | 0 | 357 | 0 | 179 | 152 | 331 | 688 | 840 |
| 09:00 10:00 | 0 | 0 | 0 | 0 | 114 | 0 | 18 | 132 | 132 | 27 | 246 | 0 | 273 | 0 | 187 | 126 | 313 | 586 | 718 |
| 11:30 12:30 | 0 | 0 | 0 | 0 | 154 | 0 | 23 | 177 | 177 | 23 | 208 | 0 | 231 | 0 | 223 | 142 | 365 | 596 | 773 |
| 12:30 13:30 | 0 | 0 | 0 | 0 | 102 | 0 | 17 | 119 | 119 | 20 | 211 | 0 | 231 | 0 | 227 | 118 | 345 | 576 | 695 |
| 15:00 16:00 | 0 | 0 | 0 | 0 | 200 | 0 | 41 | 241 | 241 | 26 | 260 | 0 | 286 | 0 | 332 | 161 | 493 | 779 | 1020 |
| 16:00 17:00 | 0 | 0 | 0 | 0 | 153 | 0 | 27 | 180 | 180 | 13 | 235 | 0 | 248 | 0 | 428 | 172 | 600 | 848 | 1028 |
| 17:00 18:00 | 0 | 0 | 0 | 0 | 163 | 0 | 17 | 180 | 180 | 14 | 241 | 0 | 255 | 0 | 402 | 175 | 577 | 832 | 1012 |
| Sub Total | 0 | 0 | 0 | 0 | 1125 | 0 | 183 | 1308 | 1308 | 176 | 2032 | 0 | 2208 | 0 | 2100 | 1174 | 3274 | 5482 | 6790 |
| U Turns |  |  |  | 0 |  |  |  | 0 | 0 |  |  |  | 0 |  |  |  | 2 | 2 | 2 |
| Total | 0 | 0 | 0 | 0 | 1125 | 0 | 183 | 1308 | 1308 | 176 | 2032 | 0 | 2208 | 0 | 2100 | 1174 | 3276 | 5484 | 6792 |
| EQ 12Hr | 0 | 0 | 0 | 0 | 1564 | 0 | 254 | 1818 | 1818 | 245 | 2824 | 0 | 3069 | 0 | 2919 | 1632 | 4554 | 7623 | 9441 |

Note: These values are calculated by multiplying the totals by the appropriate expansion factor.
1.39

| AVG 12Hr | 0 | 0 | 0 | 0 | 1407 | 0 | 229 | 1636 | 1636 | 220 | 2542 | 0 | 2762 | 0 | 2627 | 1469 | 4098 | 6860 | 8496 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Note: These volumes are calculated by multiplying the Equivalent 12 hr . totals by the AADT factor. . 90

| AVG 24Hr | 0 | 0 | 0 | 0 | 1844 | 0 | 300 | 2144 | 2144 | 288 | 3330 | 0 | 3618 | 0 | 3442 | 1924 | 5369 | 8987 | 11131 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Note: These volumes are calculated by multiplying the Average Daily 12 hr . totals by 12 to 24 expansion factor. 1.31

## Comments:

Note: U-Turns provided for approach totals. Refer to 'U-Turn' Report for specific breakdown.

## FERNBANK RD @ ROBERT GRANT AVE

| Survey Date: | Thursday, August 30, 2018 | Total Observed U-Turns |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  |  | Northbound: | 0 | Southbound: | 0 |
|  |  | Eastbound: | 0 | Westbound: | 2 |



| TOTAL: | 0 | 0 | 0 | 0 | 1125 | 0 | 183 | 1308 | 1308 | 176 | 2032 | 0 | 2208 | 0 | 2100 | 1174 | 3276 | 5484 | $\mathbf{6 7 9 2}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Note: U-Turns are included in Totals.
Comment:

Transportation Services - Traffic Services
Turning Movement Count - Cyclist Volume Report

## FERNBANK RD @ ROBERT GRANT AVE

Count Date: Thursday, August 30, 2018 Start Time: 07:00

| Time Period | ROBERT GRANT AVE |  |  | FERNBANK RD |  |  | Grand Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Northbound | Southbound | Street Total | Eastbound | Westbound | Street Total |  |
| 07:00 08:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:00 09:00 | 0 | 0 | 0 | 1 | 1 | 2 | 2 |
| 09:00 10:00 | 0 | 0 | 0 | 1 | 0 | 1 | 1 |
| 11:30 12:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 13:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:00 16:00 | 0 | 3 | 3 | 0 | 0 | 0 | 3 |
| 16:00 17:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:00 18:00 | 0 | 0 | 0 | 0 | 1 | 1 | 1 |
| Total .......... | 0 | 3 | 3 | 2 | 2 | 4 | 7 |

Comment:

## Turning Movement Count - Heavy Vehicle Report

FERNBANK RD @ ROBERT GRANT AVE

Survey Date: Thursday, August 30, 2018

ROBERT GRANT AVE

| Time Period |  | Northbound |  |  | Southbound |  |  |  | Eastbound |  |  |  |  | Westbound |  |  |  | $\begin{gathered} \text { w } \\ \text { TOT } \\ \hline \end{gathered}$ | $\begin{aligned} & \text { STR } \\ & \text { TOT } \\ & \hline \end{aligned}$ | Grand Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LT | ST | RT | $\begin{gathered} \mathrm{N} \\ \text { TOT } \end{gathered}$ | LT | ST | RT | $\begin{gathered} \mathrm{S} \\ \mathrm{TOT} \end{gathered}$ | $\begin{aligned} & \text { STR } \\ & \text { TOT } \end{aligned}$ | LT | ST | RT | $\begin{gathered} \text { E } \\ \text { TOT } \end{gathered}$ | LT | ST | RT |  |  |  |
| 07:00 | 08:00 | 0 | 0 | 0 | 0 | 14 | 0 | 2 | 16 | 16 | 5 | 3 | 0 | 8 | 0 | 7 | 12 | 19 | 27 | 43 |
| 08:00 | 09:00 | 0 | 0 | 0 | 0 | 6 | 0 | 4 | 10 | 10 | 7 | 4 | 0 | 11 | 0 | 8 | 15 | 23 | 34 | 44 |
| 09:00 | 10:00 | 0 | 0 | 0 | 0 | 9 | 0 | 1 | 10 | 10 | 3 | 4 | 0 | 7 | 0 | 6 | 8 | 14 | 21 | 31 |
| 11:30 | 12:30 | 0 | 0 | 0 | 0 | 9 | 0 | 1 | 10 | 10 | 1 | 6 | 0 | 7 | 0 | 7 | 9 | 16 | 23 | 33 |
| 12:30 | 13:30 | 0 | 0 | 0 | 0 | 6 | 0 | 4 | 10 | 10 | 4 | 9 | 0 | 13 | 0 | 7 | 5 | 12 | 25 | 35 |
| 15:00 | 16:00 | 0 | 0 | 0 | 0 | 18 | 0 | 6 | 24 | 24 | 3 | 9 | 0 | 12 | 0 | 6 | 15 | 21 | 33 | 57 |
| 16:00 | 17:00 | 0 | 0 | 0 | 0 | 12 | 0 | 6 | 18 | 18 | 0 | 8 | 0 | 8 | 0 | 10 | 12 | 22 | 30 | 48 |
| 17:00 | 18:00 | 0 | 0 | 0 | 0 | 9 | 0 | 2 | 11 | 11 | 1 | 8 | 0 | 9 | 0 | 3 | 8 | 11 | 20 | 31 |
| Sub | Total | 0 | 0 | 0 | 0 | 83 | 0 | 26 | 109 | 109 | 24 | 51 | 0 | 75 | 0 | 54 | 84 | 138 | 213 | 322 |
| U-Turns (Heavy Vehicles) |  |  |  |  | 0 |  |  |  | 0 | 0 |  |  |  | 0 |  |  |  | 0 | 0 | 0 |
| Total |  | 0 | 0 | 0 | 0 | 83 | 0 | 26 | 109 | 109 | 24 | 51 | 0 | 75 | 0 | 54 | 84 | 138 | 213 | 322 |

Heavy Vehicles include Buses, Single-Unit Trucks and Articulated Trucks. Further, they ARE included in the Turning Movement Count Summary.

Transportation Services - Traffic Services

## Turning Movement Count - Pedestrian Volume Report

FERNBANK RD @ ROBERT GRANT AVE
Count Date: Thursday, August 30, 2018
Start Time: 07:00

| Time Period | NB Approach (E or W Crossing) | SB Approach (E or W Crossing) | Total | EB Approach ( N or S Crossing) | WB Approach ( N or S Crossing) | Total | Grand Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 07:00 07:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 07:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 07:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 08:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:00 08:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:00 08:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:15 08:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:30 08:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:45 09:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:00 09:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 09:00 09:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 09:15 09:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 09:30 09:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 09:45 10:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 09:00 10:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 11:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 12:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:00 12:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:15 12:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 12:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 12:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 13:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 13:00 13:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 13:15 13:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 13:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:00 15:15 | 0 | 1 | 1 | 0 | 0 | 0 | 1 |
| 15:15 15:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:30 15:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:45 16:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:00 16:00 | 0 | 1 | 1 | 0 | 0 | 0 | 1 |
| 16:00 16:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:15 16:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:30 16:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:45 17:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:00 17:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:00 17:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:15 17:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:30 17:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:45 18:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:00 18:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total .......... | 0 | 1 | 1 | 0 | 0 | 0 | 1 |

Comment:

## Turning Movement Count - 15 Min U-Turn Total Report FERNBANK RD @ ROBERT GRANT AVE

| Survey Date: <br> Time Period |  | Thursday, August 30, 2018 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Northbound U-Turn Total | Southbound U-Turn Total | Eastbound U-Turn Total | Westbound U-Turn Total | Total |
| 07:00 | 07:15 | 0 | 0 | 0 | 0 | 0 |
| 07:15 | 07:30 | 0 | 0 | 0 | 0 | 0 |
| 07:30 | 07:45 | 0 | 0 | 0 | 0 | 0 |
| 07:45 | 08:00 | 0 | 0 | 0 | 0 | 0 |
| 08:00 | 08:15 | 0 | 0 | 0 | 0 | 0 |
| 08:15 | 08:30 | 0 | 0 | 0 | 0 | 0 |
| 08:30 | 08:45 | 0 | 0 | 0 | 1 | 1 |
| 08:45 | 09:00 | 0 | 0 | 0 | 0 | 0 |
| 09:00 | 09:15 | 0 | 0 | 0 | 0 | 0 |
| 09:15 | 09:30 | 0 | 0 | 0 | 1 | 1 |
| 09:30 | 09:45 | 0 | 0 | 0 | 0 | 0 |
| 09:45 | 10:00 | 0 | 0 | 0 | 0 | 0 |
| 11:30 | 11:45 | 0 | 0 | 0 | 0 | 0 |
| 11:45 | 12:00 | 0 | 0 | 0 | 0 | 0 |
| 12:00 | 12:15 | 0 | 0 | 0 | 0 | 0 |
| 12:15 | 12:30 | 0 | 0 | 0 | 0 | 0 |
| 12:30 | 12:45 | 0 | 0 | 0 | 0 | 0 |
| 12:45 | 13:00 | 0 | 0 | 0 | 0 | 0 |
| 13:00 | 13:15 | 0 | 0 | 0 | 0 | 0 |
| 13:15 | 13:30 | 0 | 0 | 0 | 0 | 0 |
| 15:00 | 15:15 | 0 | 0 | 0 | 0 | 0 |
| 15:15 | 15:30 | 0 | 0 | 0 | 0 | 0 |
| 15:30 | 15:45 | 0 | 0 | 0 | 0 | 0 |
| 15:45 | 16:00 | 0 | 0 | 0 | 0 | 0 |
| 16:00 | 16:15 | 0 | 0 | 0 | 0 | 0 |
| 16:15 | 16:30 | 0 | 0 | 0 | 0 | 0 |
| 16:30 | 16:45 | 0 | 0 | 0 | 0 | 0 |
| 16:45 | 17:00 | 0 | 0 | 0 | 0 | 0 |
| 17:00 | 17:15 | 0 | 0 | 0 | 0 | 0 |
| 17:15 | 17:30 | 0 | 0 | 0 | 0 | 0 |
| 17:30 | 17:45 | 0 | 0 | 0 | 0 | 0 |
| 17:45 | 18:00 | 0 | 0 | 0 | 0 | 0 |
| Total |  | 0 | 0 | 0 | 2 | 2 |

## Appendix D

City of Ottawa Collision Data

## City Operations - Transportation Services

## Collision Details Report - Public Version

From: January 1, 2013 To: December 31, 2017
Location: BOBOLINK RDG @ ROBERT GRANT AVE
Traffic Control: Roundabout Total Collisions: 1

| Date/Day/Time | Environment | Impact Type | Classification | Surface Cond'n | Veh. Dir | Vehicle Manoeuv | Vehicle type | First Event | No. Ped |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2017-Oct-05, Thu, 12:40 | Clear | Angle | P.D. only | Dry | West | Going ahead | Automobile, station wagon | Other motor vehicle |  |
|  |  |  |  |  | North | Going ahead | Automobile, station wagon | Other motor vehicle |  |

Location: FERNBANK RD @ ROBERT GRANT AVE
Traffic Control: Traffic signal
Total Collisions: 1

| Date/Day/Time | Environment | Impact Type | Classification | Surface Cond'n | Veh. Dir | Vehicle Manoeuve | Vehicle type | First Event | No. Ped |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2016-Jun-23, Thu,20:08 | Clear | Sideswipe | P.D. only | Dry | West | Changing lanes | Automobile, station wagon | Other motor vehicle |  |
|  |  |  |  |  | West | Going ahead | Automobile, station wagon | Other motor vehicle |  |

## Appendix E

Background Growth Analysis

## Fernbank/ Eagleson

8 hrs

| Year | Date | North Leg |  | South Leg |  | East Leg |  | West Leg |  | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | SB | NB | NB | SB | WB | EB | EB | WB |  |
| 2009 | Wednesday 17 June |  |  |  |  |  |  | 2148 | 2108 | 4256 |
| 2010 | Monday 17 May |  |  |  |  |  |  | 2139 | 1912 | 4051 |
| 2012 | Thursday 23 August |  |  |  |  |  |  | 1620 | 1242 | 2862 |
| 2014 | Friday 27 June |  |  |  |  |  |  | 1577 | 1442 | 3019 |
| 2017 | Tuesday 11 April |  |  |  |  |  |  | 1984 | 1984 | 3968 |

North Leg

| Year | Counts |  |  |  | \% Change |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NB | SB | NB+SB | INT | NB | SB | NB+SB | INT |
| 2009 |  |  |  | 4256 |  |  |  |  |
| 2010 |  |  |  | 4051 |  |  |  | $-4.8 \%$ |
| 2012 |  |  |  | 2862 |  |  |  | $-29.4 \%$ |
| 2014 |  |  |  | 3019 |  |  |  | $5.5 \%$ |
| 2017 |  |  |  | 3968 |  |  |  | $31.4 \%$ |

Regression Estimate 2009
Regression Estimate 2017

## Average Annual Change

West Leg

| Year | Counts |  |  |  |  |  |  |  |  |  | \% Change |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | WB | EB+WB | INT | EB | WB | EB+WB | INT |  |  |  |  |  |  |
| 2009 | 2148 | 2108 | 4256 | 4256 |  |  |  |  |  |  |  |  |  |  |
| 2010 | 2139 | 1912 | 4051 | 4051 | $-0.4 \%$ | $-9.3 \%$ | $-4.8 \%$ | $-4.8 \%$ |  |  |  |  |  |  |
| 2012 | 1620 | 1242 | 2862 | 2862 | $-24.3 \%$ | $-35.0 \%$ | $-29.4 \%$ | $-29.4 \%$ |  |  |  |  |  |  |
| 2014 | 1577 | 1442 | 3019 | 3019 | $-2.7 \%$ | $16.1 \%$ | $5.5 \%$ | $5.5 \%$ |  |  |  |  |  |  |
| 2017 | 1984 | 1984 | 3968 | 3968 | $25.8 \%$ | $37.6 \%$ | $31.4 \%$ | $31.4 \%$ |  |  |  |  |  |  |


$\begin{array}{ll}\text { Regression Estimate } & 2009 \\ \text { Regression Estimate } & 2017\end{array}$
Average Annual Change

South Leg

| Year | Counts |  |  |  | \% Change |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NB | SB | NB+SB | INT | NB | SB | NB+SB | INT |
| 2009 |  |  |  | 4256 |  |  |  |  |
| 2010 |  |  |  | 4051 |  |  |  | $-4.8 \%$ |
| 2012 |  |  |  | 2862 |  |  |  | $-29.4 \%$ |
| 2014 |  |  |  | 3019 |  |  |  | $5.5 \%$ |
| 2017 |  |  |  | 3968 |  |  |  | $31.4 \%$ |

Regression Estimate 2009
Regression Estimate 2017
Average Annual Change

Fernbank/ Eagleson
AM Peak

| Year | Date | North Leg |  | South Leg |  | East Leg |  | West Leg |  | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | SB | NB | NB | SB | WB | EB | EB | WB |  |
| 2009 | Wednesday 17 June |  |  |  |  |  |  | 315 | 309 | 624 |
| 2010 | Monday 17 May |  |  |  |  |  |  | 380 | 261 | 641 |
| 2012 | Thursday 23 August |  |  |  |  |  |  | 229 | 114 | 343 |
| 2014 | Friday 27 June |  |  |  |  |  |  | 158 | 157 | 315 |
| 2017 | Tuesday 11 April |  |  |  |  |  |  | 258 | 248 | 506 |

North Leg

| Year | Counts |  |  |  |  | \% Change |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NB | SB | NB+SB | INT | NB | SB | NB+SB | INT |  |
| 2009 |  |  |  | 624 |  |  |  |  |  |
| 2010 |  |  |  | 641 |  |  |  | $2.7 \%$ |  |
| 2012 |  |  |  | 343 |  |  |  | $-46.5 \%$ |  |
| 2014 |  |  |  | 315 |  |  | $-8.2 \%$ |  |  |
| 2017 |  |  |  | 506 |  |  |  |  |  |

Regression Estimate 2009
Regression Estimate 2017

## Average Annual Change

West Leg

| Year | Counts |  |  |  |  |  |  |  |  |  |  | \% Change |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | WB | EB+WB | INT | EB | WB | EB+WB | INT |  |  |  |  |  |  |  |
| 2009 | 315 | 309 | 624 | 624 |  |  |  |  |  |  |  |  |  |  |  |
| 2010 | 380 | 261 | 641 | 641 | $20.6 \%$ | $-15.5 \%$ | $2.7 \%$ | $2.7 \%$ |  |  |  |  |  |  |  |
| 2012 | 229 | 114 | 343 | 343 | $-39.7 \%$ | $-56.3 \%$ | $-46.5 \%$ | $-46.5 \%$ |  |  |  |  |  |  |  |
| 2014 | 158 | 157 | 315 | 315 | $-31.0 \%$ | $37.7 \%$ | $-8.2 \%$ | $-8.2 \%$ |  |  |  |  |  |  |  |
| 2017 | 258 | 248 | 506 | 506 | $63.3 \%$ | $58.0 \%$ | $60.6 \%$ | $60.6 \%$ |  |  |  |  |  |  |  |


$\begin{array}{ll}\text { Regression Estimate } & 2009 \\ \text { Regression Estimate } & 2017\end{array}$
Average Annual Change

South Leg

| Year | Counts |  |  |  | \% Change |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NB | SB | NB+SB | INT | NB | SB | NB+SB | INT |
| 2009 |  |  |  | 624 |  |  |  |  |
| 2010 |  |  |  | 641 |  |  |  | $2.7 \%$ |
| 2012 |  |  |  | 343 |  |  | $-46.5 \%$ |  |
| 2014 |  |  |  | 315 |  |  | $-8.2 \%$ |  |
| 2017 |  |  |  | 506 |  |  |  | $60.6 \%$ |

Regression Estimate 2009
Regression Estimate 2017

## Average Annual Change

Fernbank/ Eagleson
PM Peak

| Year | Date | North Leg |  | South Leg |  | East Leg |  | West Leg |  | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | SB | NB | NB | SB | WB | EB | EB | WB |  |
| 2009 | Wednesday 17 June |  |  |  |  |  |  | 356 | 398 | 754 |
| 2010 | Monday 17 May |  |  |  |  |  |  | 283 | 369 | 652 |
| 2012 | Thursday 23 August |  |  |  |  |  |  | 284 | 213 | 497 |
| 2014 | Friday 27 June |  |  |  |  |  |  | 317 | 241 | 558 |
| 2017 | Tuesday 11 April |  |  |  |  |  |  | 307 | 374 | 681 |

North Leg

| Year | Counts |  |  |  |  | \% Change |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NB | SB | NB+SB | INT | NB | SB | NB+SB | INT |  |
| 2009 |  |  |  | 754 |  |  |  |  |  |
| 2010 |  |  |  | 652 |  |  |  | $-13.5 \%$ |  |
| 2012 |  |  |  | 497 |  |  |  | $-23.8 \%$ |  |
| 2014 |  |  |  | 558 |  |  |  | $12.3 \%$ |  |
| 2017 |  |  |  | 681 |  |  |  | $22.0 \%$ |  |

Regression Estimate 2009
Regression Estimate 2017

## Average Annual Change

West Leg

| Year | Counts |  |  |  |  |  |  |  |  |  |  | \% Change |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | WB | EB+WB | INT | EB | WB | EB+WB | INT |  |  |  |  |  |  |  |
| 2009 | 356 | 398 | 754 | 754 |  |  |  |  |  |  |  |  |  |  |  |
| 2010 | 283 | 369 | 652 | 652 | $-20.5 \%$ | $-7.3 \%$ | $-13.5 \%$ | $-13.5 \%$ |  |  |  |  |  |  |  |
| 2012 | 284 | 213 | 497 | 497 | $0.4 \%$ | $-42.3 \%$ | $-23.8 \%$ | $-23.8 \%$ |  |  |  |  |  |  |  |
| 2014 | 317 | 241 | 558 | 558 | $11.6 \%$ | $13.1 \%$ | $12.3 \%$ | $12.3 \%$ |  |  |  |  |  |  |  |
| 2017 | 307 | 374 | 681 | 681 | $-3.2 \%$ | $55.2 \%$ | $22.0 \%$ | $22.0 \%$ |  |  |  |  |  |  |  |


$\begin{array}{ll}\text { Regression Estimate } & 2009 \\ \text { Regression Estimate } & 2017\end{array}$
Average Annual Change

South Leg

| Year | Counts |  |  |  | \% Change |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | NB | SB | NB+SB | INT | NB | SB | NB+SB | INT |
| 2009 |  |  |  | 754 |  |  |  |  |
| 2010 |  |  |  | 652 |  |  |  | $-13.5 \%$ |
| 2012 |  |  |  | 497 |  |  | $-23.8 \%$ |  |
| 2014 |  |  |  | 558 |  |  | $12.3 \%$ |  |
| 2017 |  |  |  | 681 |  |  |  | $22.0 \%$ |

Regression Estimate 2009
Regression Estimate 2017

## Average Annual Change

## Appendix F

5786 Fernbank Development


Amira Shetata, M. Eng., P.Eng.<br>Project Manager, Infrastructure Approvals<br>Planning and Growth Management Department<br>City of Ottawa<br>110 Laurier Avenue West<br>Ottawa, ON<br>K1P 1J1

Dear Ms. Shetata:

## Re: CRT Lands Phase 1 and 2 Fernbank Community Transportation Letter

CRT Development Inc. (CRT) wishes to proceed with the urban development of the subject lands in accordance with the policies set out by the Planning Department of the City of Ottawa. Part of the Plan of Subdivision process for the City includes provision of several documents in support of the subject development. IBI Group was retained by the Owners to complete a Transportation Letter in support of the application. The proposed development is located within the Fernbank Community in Stittsville Ward, as shown in Exhibit 1. The land-use policy is governed by the Fernbank Community Design Plan (FCDP).

## REPORT CONIEXT

Based on the City of Ottawa Transportation Impact Assessment Guidelines (2006), a Transportation Impact Study (TIS) would normally be required to support a draft plan application for a subdivision of this size. However, the location of the proposed development is currently undeveloped, with no existing intersections in the vicinity. The primary access intersections are proposed along the future North-South Arterial Road. The detailed design, including required intersection capacity analysis, of this roadway is currently underway, which is expected to account for traffic generated by the proposed development as well as adjacent residential developments in the Fernbank Community. As a result, it was agreed by City staff that a traditional TIS was not required; a modified Transportation Brief Letter was considered acceptable.

Based on the pre-consultation discussions with the City, the following objectives were formulated:

- Summarize the nature and extent of Phase 1 and 2 of the Claridge Fernbank Subdivision, and demonstrate how it is coherent with the transportation objectives and recommendations outlined in the Fernbank Community Design Plan (CDP);
- Review/ comment on the proposed site design with respect to infrastructure, geometrics, internal operation and active transportation; and,
- Analyze the trip generation and traffic distribution for Phase 1 and 2 of the Claridge Fernbank Subdivision.

All relevant support information and data have been attached.


IBI ског

Claridge Homes - Fernbank Subdivision Transportation Impact Study

EXHIBIT 1
Site Location

PROJECT No. 27970
DATE:
SCALE:

JANUARY 2011 |  |  |
| :--- | :--- |
| m | 0 |

## PROPOSED DEVELOPMENT

The current draft plan for the subject property is located in the Fernbank Community and is identified on Exhibit 2. The property covers a total area of about 60 ha and is bounded by Fernbank Road to the south, Abbott Street and the Trans Canada Trail to the north, Shea Road to the east and the North-South Collector Road in the FCDP to the east. The proposed land use for the subject property, which is in general conformance with the FCDP, will include a residential mix of single family units, townhouses and stacked townhouses. The draft plan also provides land for both an elementary and secondary school and both a neighbourhood and community park. Phase 1 and 2 of the CRT Lands are expected to be developed by the 2014 horizon year.

It is the Owners intent to develop the subject lands in at least two phases; Phase 1 immediately upon receipt of approvals, while the development timing of Phase 2 will be market determined.

In accordance with the FCDP, the draft plan proposes two new collector roads; one major collector road with a 26 m right-of-way (designated Street No. 9 on the draft plan) and one minor collector road with an 22 m right-of-way (designated Street No.1). Street No. 15 will be classified a local road with an 18 m right-of-way. All remaining streets will be local roads with 16.5 m rights-of-way. In all, three new community accesses will be provided to the adjacent network. Two accesses will be provided off the future North-South Arterial Road via Street No. 9 and Street No.15. The specific geometry and operation of these intersections are being examined as part of the detailed design of the North-South Arterial Road, along with intersection capacity analysis. At this time, it is our understanding that two lanes of the North-South Arterial between the Trans Canada Trail and Fernbank Road, and the extension of Abbott Street between the North-South Arterial and Iber Road will be constructed by an adjacent developer (for the Abbott-Fernbank Lands) as a condition of approval. The initial phase of the Abbott-Fernbank Lands is scheduled to be occupied by the 2014 horizon year, which coincides with the development schedule of the CRT Lands. A copy of the Transportation Brief for the Abbott-Fernbank Lands, completed by Novatech Engineering Consulting Ltd. (Novatech), is attached to this letter. A third access to the CRT Lands will be provided off Abbott Street via Street No.1.

The access intersections off the North-South Arterial Road (at Street No. 9 and Street No.15) are spaced approximately 270 m apart, which should be sufficient for signalization and arterial traffic progression should future signalization warrants be met.

## OVERAШ DEVELOPMENT CONTEXT.

The proposed CRT Lands is contained within the Fernbank Community, and is subject to the policies and recommendations outlined in the FCDP. One of the major supporting documents for the FCDP is the Fernbank Transportation Master Plan (FTMP). This document outlines the projects and initiatives that will be required to meet the specific transportation needs of the Fernbank Community, and help to service future growth in the surrounding region.

A major element in the FTMP is the North-South Arterial Road, which will bisect the Fernbank Community and provide it with links to the existing major arterial corridors in the area, such as Hazeldean Road and Fernbank Road. The City of Ottawa TMP outlines the need for this arterial link in the updated City of Ottawa TMP, 2008. The FTMP states a 2-lane cross-section is required for the North-South Arterial Road in order to accommodate estimated future demand by the 2031 horizon year. A right-of-way of 41.5 m has been provisioned to facilitate widening the roadway to a 4-lane urban cross-section when traffic volumes warrant it beyond the 2031 horizon year. The building setbacks within the CRT Lands will be set appropriately to provide for the future right-of-way.

## ACTIVE TRANSPORTATION

The FTMP established a transit modal split of $20 \%$ as a reasonable minimum target for the Hazeldean South Screenline. However, the level of transit ridership required to achieve this goal is only expected closer to the 2031 horizon year. As such, it is anticipated that the transit modal split for the CRT Lands will be low initially, but will increase over time as new transit facilities


and services (such as the extension of bus rapid transit on the North-South Arterial Road) are implemented in the Fernbank Community.

In the short term, transit facilities such as bus stops may be provided within the subject lands. Strategic placement of stops along Street No. 9 and Street No. 1 should ensure all units within the development are within 400 m of a bus stop, which is considered to be the maximum ideal walking distance for mobility impaired commuters using public transit. Existing transit service routes operating on Abbott Street may be diverted to accommodate the proposed development. The diverted route only impacts the section of Abbott Street between Iber Road and the proposed development access.

Concrete sidewalks should be provided along both sides of Street No. 9 and Street No.1. The location of sidewalks and pedestrian walkways will be determined at the detailed design stage. All streets shall conform to City of Ottawa standards. The FTMP identifies the requirement to provide on-road cycling facilities along the North-South Arterial Road. This will provide the Fernbank Community with a link to nearby cycle routes in the area that are proposed in the City of Ottawa's Primary Urban Cycling Network. On-site bicycle racks and storage areas should be provided at the proposed elementary school and high school as per the City of Ottawa Zoning By-law. These locations should be located near entrances.

## TRIP GENERATION

The updated site generated trips were calculated using the ITE Trip Generation Manual, $8^{\text {th }}$ Edition. The results are shown in Table 1 below.

TABLE1-Claridge Fernbank Subdivision Phase 1 and 2 Traffic Generation

| Land Use | Size <br> (DU or students) | Land Use Code | Peak Hour | Directional Split |  | Traffic Generated (veh/h) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | In | Out | In | Out | Total |
| Single Family Detached | 510 | 210 | AM | 25\% | 75\% | 92 | 275 | 367 |
|  |  |  | PM | 63\% | 37\% | 287 | 168 | 455 |
| Townhome | 364 | 230 | AM | 17\% | 83\% | 25 | 120 | 145 |
|  |  |  | PM | 67\% | 33\% | 116 | 57 | 173 |
| Elementary School | 500 | 520 | AM | 55\% | 45\% | 102 | 84 | 186 |
|  |  |  | PM | 49\% | 51\% | 37 | 38 | 75 |
| High School | 1000 | 530 | AM | 68\% | 32\% | 286 | 134 | 420 |
|  |  |  | PM | 47\% | 53\% | 61 | 69 | 130 |
| SUBTOTAL |  |  | AM |  |  | 504 | 614 | 1,118 |
|  |  |  | PM |  |  | 501 | 333 | 834 |
| Internal (Elementary School: 50\%) |  |  | AM |  |  | -194 | -109 | -303 |
|  |  |  | PM |  |  | -49 | -54 | -103 |
| Transit Modal Split (TMS 5\%) |  |  | AM |  |  | -16 | -25 | -41 |
|  |  |  | PM |  |  | -23 | -14 | -27 |
| TOTAL NEWTRIPS |  |  | AM |  |  | 295 | 479 | 774 |
|  |  |  | PM |  |  | 429 | 265 | 695 |


| Notes: |  |  |  |
| :---: | :---: | :---: | :---: |
| veh/h = vehicles per hour; DU = dwelling units |  |  |  |
| Formula for Land Uses: |  |  |  |
| Single Family: | Townhouse: | Elementary School | High School |
| AM $\quad T=0.70(X)+9.74$ | $T=e^{\wedge}(0.80 * L N(X)+0.26$ | $T=e^{\wedge}\left(1.14 * L N^{*}(X)-1.86\right)$ | $T=0.42$ ( X ) |
| $P M \quad T=e^{\wedge}(0.90 \operatorname{Ln}(X)+0.51)$ | $T=e^{\wedge}(0.82 * L N(X)+0.32)$ | $T=0.15^{*}(X)$ | $T=0.13$ ( $X$ ) |

At the time of the report, no information was available pertaining to the size of each school proposed onsite. As a result, it was assumed the elementary school and high school would have 500 and 1,000 enrolled students respectively. Based on these assumptions, the total traffic generation analysis results for the subject site are shown in Table 1. The CRT Lands is expected to generate approximately 770 vehicles and 700 vehicles in the morning and afternoon peak hours respectively. It is worth noting the afternoon peak hour of generation for the elementary school and high school occur well before the peak hour of generation for residential development, which is reflected in the lower trip generation results in Table 1.

Subsequent adjustment factors were applied to these results to account for the mixed-use nature and overall design of the proposed site. These adjustments are summarized below.

Internalization - A 50\% internal reduction factor was applied to the elementary school trip generation results; accounting for alternate modes. This factor also reflects the likelihood that many trips may travel within the development and never venture onto the adjacent road network.

Transit Modal Split (TMS) Reduction - Trip generation data in the ITE Manual was derived from local surveys, where the locations often have limited transit use. As noted previously, based on existing transit ridership levels and the lack of significant transit facilities in the immediate area, a lower TMS was assumed in the analysis than the $20 \%$ minimum threshold established in the FTMP. In this case, a 5\% transit modal split was considered reasonable and relatively conservative to apply in all horizon years.

## TRIP DISTRIBUTION

The external trip distribution was based on the Novatech Study, since the adjacent site possesses very similar land use characteristics. The assumed external trip distribution from the Novatech Study was summarized as follows:

- $85 \%$ to/ from the east and north (Hazeldean Road, Palladium Drive, Highway 417)
- $10 \%$ to/ from the south (Fernbank Road, Terry Fox Drive, Eagleson Road)
- $5 \%$ to/ from the west (Abbott Road, Fernbnak Road and Stittsville Main Street)

Based on the external trip distribution assumptions above and the design characteristics of the internal road network, the distribution of site generated traffic between the proposed access intersections was assumed to be as follows:

- $50 \%$ tol from Street No. 9
- $35 \%$ to/from Street No. 15
- $15 \%$ from Street No. 1

The North-South Arterial Road is expected to be the primary route for residents of the CRT Lands to enter and exit the development, as per the FTMP. As a result, the majority of trips (85\%) are expected to use these access intersections.

## SUMMARY

The key findings of this Transportation may be summarized as follows:

- The proposed land use for the subject property will include a residential mix of single family units, townhouses and stacked townhouses. The draft plan also provides land for both an elementary and secondary school and both a neighbourhood and community park.
- The subject site will be developed in two phases. Phase 1 and 2 of the CRT Lands are expected to be developed by the 2014 horizon year.
- The draft plan proposes three access intersections, two off the future North-South Arterial Road and one off Abbott Street.
- The detailed design of the North-South Arterial Road between Fernbank Road and Iber Road is currently underway, which is being completed as part of the conditions of approval for the adjacent Abbott-Fernbank Lands. The specific geometry and assessment of operation of intersections along the North-South Arterial Road are being reviewed during this process.
- The subject site is estimated to generate approximately 770 vehicles and 700 vehicles in the morning and afternoon peak hours respectively.
- The majority of site generated trips are expected to originate and depart to and from the north and east, where the North-South Arterial Road will provided the most direct connection to commercial and industrial centres, as well as the adjacent arterial network.
- The FTMP target transit modal split at the Hazeldean South Screenline is $20 \%$. This target is considered achievable if appropriate transit facilities and services (as outlined in teh FTMP) are provided to the area.
- The exact location and design of on-site transit, pedestrian and bicycle facilities (such as bus stops and sidewalks) shall be determined at the site plan stage.
- Coordination and communication between adjacent developers should be encouraged to achieve a final design of the North-South Arterial Road, and the associated intersections.

Should you have any questions or require clarification regarding the above letter, please do not hesitate to contact me at (613)-225-1311.

Yours Truly,

## IBI Group



Austin Shih, MASc., P.Eng.
Project Engineer

## ATTACHMENTS

| From: | Shehata, Amira [Amira.Shehata@ottawa.ca] |
| :--- | :--- |
| Sent: | January 19, 2011 2:10 PM |
| To: | Austin Shih |
| Subject: | RE: Claridge Fernbank Residential Subdivision |

Austin,
I assume that the analysis would be completed sometime in the near future. If the Claridge Lands Development is incorporated into the analysis you may need to refer to it in your report, no need for repetition. It should be noted that coordination and communication between each developer and consultants is required to achieve a final intersection design.

It would be acceptable to present a brief similar to that of the Regional Transportation Impact Brief.

Amira Shehata, P.Eng, M. Eng.|Project Manager, Infrastructure Approvals
Development Review - Rural Services
T. 613.580.2424 x 27737| Fax: 613-580-2576

Amira.Shehata@ottawa.ca

CITY OF OTTAWA - Planning and Growth Management
City Hall 110 Laurier Avenue West Ottawa, ON K1P 1J1 Canada

From: Austin Shih [mailto:austin.shih@IBIGroup.com]
Sent: January 19, 2011 12:30 PM
To: Shehata, Amira
Subject: RE: Claridge Fernbank Residential Subdivision

Thanks Amira. I hope you had a wonderful vacation.

Your direction on the scope of work would be appreciated. If analysis on the NS arterial intersections is still ongoing, I assume they would be incorporating Claridge's lands. Do we require repeating this work? Would it be acceptable to present a letter, similar to the Regional Traffic Letter attached, that outlines the characteristics of the development and confirms trip generation/assignment? I've attached the proposed draft plan w/ phasing for your information. Note the enrolment numbers for the schools are estimates, no data on the size is currently available.

I would like to reduce the amount of throw-away work involved with this project, but at the same time provide you with the level of comfort that the development can be accommodated on the network.

Regards,

## Austin Shih M.A.Sc., P.Eng.

 IBI GroupNOTE: This e-mail message and attachments may contain privileged and confidential information. If you have received this message in error, please immediately notify the sender and delete this e-mail message.
NOTE: Ce courriel peut contenir de l'information privilégiée et confidentielle. Si vous avez recu ce message par erreur, veuillez le mentionner immédiatement à l'expéditeur et effacer ce courriel.

From: Shehata, Amira [mailto:Amira.Shehata@ottawa.ca]
Sent: January 19, 2011 11:56 AM
To: Austin Shih
Subject: RE: Claridge Fernbank Residential Subdivision

Hi Austin,
Thank you for your message, I look forward to working on this project.
Analysis for the NS arterial intersections is not available yet.
Please note that I was away on vacation and just got back this week hence the delay in my response.
Contact me should you have questions.

Amira Shehata, P.Eng, M. Eng.|Project Manager, Infrastructure Approvals
Development Review - Rural Services
T. 613.580.2424 x 27737| Fax: 613-580-2576

Amira.Shehata@ottawa.ca

CITY OF OTTAWA - Planning and Growth Management
City Hall 110 Laurier Avenue West Ottawa, ON K1P 1J1 Canada

From: Austin Shih [mailto:austin.shih@।BIGroup.com]
Sent: January 10, 2011 4:07 PM
To: Shehata, Amira
Subject: Claridge Fernbank Residential Subdivision
Hi Amira,
I wanted to let you know that I will be work for on behalf of Claridge to assist in their draft plan application for residential lands in the Fernbank Community. I've attached a site plan showing the phases Claridge is planning to register. When I have more details, I will prepare a terms of reference.

I've also attached a brief completed by Novatech for the adjacent Regional Lands. It states that intersection analysis will be completed for hte NS arterial intersections during design. I was wondering if this information was available since I would need to include that in my analysis as background traffic. I would like to ensure my study is consistent with established approved studies.

Best regards,
Austin Shih M.A.Sc., P.Eng.
IBI Group
400-333 Preston Street
Ottawa ON K1S 5N4 Canada
tel 6132251311 ext 564
fax 6132259868
email austin.shih@IBIGroup.com
web www.ibigroup.com

## Single-Family Detached Housing

Average Vehicle Trip Ends vs: Dwelling Units<br>On a: Weekday,<br>Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.

Number of Studies: 286
Avg. Number of Dwelling Units: 194
Directional Distribution: $25 \%$ entering, $75 \%$ exiting
Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.75 | $0.33-2.27$ | 0.90 |

## Data Plot and Equation



## Single-Family Detached Housing (210)

Average Vehicle Trip Ends vs: Dwelling Units<br>On a: Weekday,<br>Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.

Number of Studies: 314
Avg. Number of Dwelling Units: 208
Directional Distribution: 63\% entering, 37\% exiting
Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 1.01 | $0.42-2.98$ | 1.05 |

Data Plot and Equation


# Residential Condominium/Townhouse (230) 

## Average Vehicle Trip Ends vs: Dwelling Units

## On a: Weekday, <br> Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.

Number of Studies: 59
Avg. Number of Dwelling Units: 213
Directional Distribution: 17\% entering, $83 \%$ exiting
Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.44 | $0.15-1.61$ | 0.69 |

## Data Plot and Equation



# Residential Condominium/Townhouse (230) 

Average Vehicle Trip Ends vs: Dwelling Units<br>On a: Weekday,<br>Peak Hour of Adjacent Street Traffic,<br>One Hour Between 4 and 6 p.m.

Number of Studies: 62
Avg. Number of Dwelling Units: 205
Directional Distribution: 67\% entering, 33\% exiting
Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.52 | $0.18-1.24$ | 0.75 |

Data Plot and Equation


## Elementary School

 (520)Average Vehicle Trip Ends vs: Students
On a: Weekday,
A.M. Peak Hour

Number of Studies: 48
Average Number of Students:
630
Directional Distribution: 55\% entering, 45\% exiting

Trip Generation per Student

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.45 | $0.11-0.92$ | 0.70 |

## Data Plot and Equation



Fitted Curve Equation: $\operatorname{Ln}(T)=1.14 \operatorname{Ln}(X)-1.86$

## Elementary School <br> (520)

## Average Vehicle Trip Ends vs: Students

On a: Weekday,
Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.

Number of Studies: 20
Average Number of Students: 687
Directional Distribution: 49\% entering, 51\% exiting
Trip Generation per Student

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.15 | $0.05-0.37$ | 0.40 |

Data Plot and Equation


## Average Vehicle Trip Ends vs: Students

On a: Weekday,

A.M. Peak Hour

Number of Studies: 68<br>Average Number of Students: 1,292<br>Directional Distribution: 68\% entering, 32\% exiting

Trip Generation per Student

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.42 | $0.14-1.15$ | 0.68 |

## Data Plot and Equation



## High School (530)

Average Vehicle Trip Ends vs: Students
On a: Weekday,
Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.

Number of Studies: 40<br>Average Number of Students: 1,352<br>Directional Distribution: 47\% entering, $53 \%$ exiting

Trip Generation per Student

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.13 | $0.03-0.38$ | 0.37 |

Data Plot and Equation


November 11, 2009
BY E-MAIL
Planning and Growth Management Department
110 Laurier Avenue West, $4^{\text {th }}$ Floor
Ottawa, Ontario
K1P 1J1

## Attention: Mr. Don Herweyer

Dear Mr. Herweyer:

## Reference: Abbott-Fernbank Holdings - Fernbank Community Lands Transportation Brief (R-2009-139) <br> Our File No: 108180

This Transportation Brief is prepared in support of a Draft Plan application to develop Phase 1A of the development of lands located between Abbott Street and Fernbank Road (henceforth referred to as the Abbott-Fernbank Lands).

### 1.0 Report Context

The objective of this report is to summarise the nature and extent of this phase of the AbbottFernbank Lands, and demonstrate how it is coherent with the transport-related objectives and recommendations as stated in the prevailing Fernbank Community Design Plan (CDP). A trip generation analysis and traffic distribution has been performed as part of this brief. Intersection analysis will be completed as part of the draft plan process, during the preliminary design of the North-South Arterial road.

### 2.0 Proposed Development

The location of the Abbott-Fernbank Lands is Lot 28, Concession 10 in the geographic township of Goulbourn, now in the City of Ottawa. The site is bounded by Fernbank Road to the south, the Trans Canada Trail to the north, the proposed North-South Arterial road to the west, and future residential development to the east as identified in the Fernbank CDP.

Phase 1A of the Abbott-Fernbank Lands will consist of the following:

- 126 single dwelling units,
- 63 private road townhouse units,
- 3 street townhouse units,
- An elementary school.

Phase 1A includes seven public roadways. Street 14 will be a major collector road with a 26 m right-of-way, Street 20 will be a local road with an 18m right-of-way, and the remaining streets will have 16.5 m rights-of-way. The proposed access configuration for Phase 1A consists of two roadway intersections along the proposed North-South Arterial Road. The specific geometry and operation

[^0]of each intersection is not being examined at this time; this will be completed as part of the preliminary design of the North-South Arterial Road, along with the intersection capacity analysis. The locations of the proposed intersections are shown on the attached draft plan. Two lanes of the North-South Arterial Road between the Trans Canada Trail and Fernbank Road, and the extension of Abbott Street between the North-South Arterial and Iber Road will be constructed for the Phase 1A development.

The site area for Phase 1A is approximately 14.04 hectares. The site area for the entire AbbottFernbank Lands is approximately 67.31 hectares. The remainder of the site will be developed later in Phases 1B and 2, which will add another 640 residential units, a second elementary school, and a mixed-use development. Phase 1A is located centrally within the Abbott-Fernbank Lands as shown in the attached site plan.

The lands to the east of the Abbott-Fernbank Lands are to be developed by the Monarch Corporation on a phased basis. Phase 1A of the Abbott-Fernbank Lands and Phase 1 of Monarch's development are scheduled for 2014. Phase 1 of the Monarch development will consist of 359 residential units. The remainder of the Monarch development will be completed in up to six additional phases, with the full development totalling approximately 1280 residential units. Phase 1 of the Monarch development is located adjacent to Phase 1A of the Abbott-Fernbank Lands, with full road connectivity to be provided between them.

The effect of the traffic generated by Phase 1 of the Monarch development has been acknowledged and accounted for in this study. The study parameters of the IBI Group's Transportation Impact Study for Phase 1 of the Monarch development have been used for assistance in this regard, to ensure that the respective analyses for both developments are consistent and coherent.

### 3.0 Overall Development Context

The Abbott-Fernbank Lands form a part of a larger area that is to become the Fernbank Community, and is subject to the objectives and recommendations of the Fernbank CDP. One of the major supporting documents for the CDP is the Fernbank Transportation Master Plan (TMP). This document outlines the projects and initiatives that will be required to meet the specific transport needs of the fully built-out Fernbank Community, and help to service future growth of the West Urban Community.

A major element of this transportation plan is the North-South Arterial road, which will bisect the Fernbank Community and provide it with links to the existing major arterial links in the area. The need to provide this road has been identified in the City of Ottawa's 2008 update to their Transportation Master Plan.

The Fernbank TMP concludes that a 2-lane cross-section will be required for the North-South Arterial, in order to accommodate estimated future transport needs up to and including 2031. A right-of-way of 41.5 m is identified to ensure that this road can be widened to a divided four-lane roadway when the traffic volumes warrant it in the years beyond 2031. The building setbacks of the proposed Phase 1A development along the North-South Arterial road shall be sufficient so as to provide this recommended right-of-way.
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### 4.0 Provisions for Non-Auto Modes

A transit modal split of $20 \%$ is identified in the Fernbank TMP as the reasonable minimum target for the Hazeldean South Screenline. However, it is stated that the level of transit ridership required to achieve this split is unlikely to be achieved until towards the end of the planning period. As such, it is anticipated that the transit modal split for Phase 1A of the Abbott-Fernbank Lands will be quite low initially, but will increase over time as the extent and quality of the public transit service improves in line with the overall development of the Fernbank Community. In order to achieve the target modal split for transit, an exclusive rapid transit corridor along the North-South Arterial has been identified as a viable transit solution.

Due to the proximity of the Phase 1A site to the North-South Arterial road, the implementation of such a project is expected to have a significant effect on the future transit modal split of trips generated by the development within Phase 1A. To assist in meeting the modal split targets outlined in the Fernbank TMP, it is recommended that OC Transpo bus stops are provided midway along Street 14 such that all Phase 1A development will be within 400 m of a bus stop - this is considered to be the maximum ideal walking distance for mobility impaired commuters using public transit. Future bus stop locations should be reviewed and determined by OC Transpo.

Concrete sidewalks should be provided along both sides of Street 14 and along one side of Street 20. The location of sidewalks and pedestrian walkways will be determined at the detailed design stage. The streets will be consistent with the ideal roadway cross-sections shown in the Fernbank CDP, and sufficient right-of-way widths will be provided to allow for their construction.

The Fernbank TMP identifies the requirement to provide on-road cycling facilities along the NorthSouth Arterial. This will provide the Fernbank Community with a link to nearby cycle routes in the Kanata area that are proposed as part of the City of Ottawa's Primary Urban Cycling Network.

It is recommended that on-site bicycle parking should be provided for the proposed elementary school as per the bicycle parking requirements identified in the City of Ottawa's Zoning By-law. The bicycle parking spaces should be located as near as is practicable to the main entrances to the proposed school. Exact locations should be determined at the detailed design stage.

### 5.0 Trip Generation and Distribution

Trips generated by Phase 1A of the development have been calculated for the weekday AM and PM peak hours using the Institute of Transportation Engineers (ITE) Trip Generation Manual (8 ${ }^{\text {th }}$ Edition).

It should be noted that the peak hours of generation for the school and the residential development are not necessarily coincidental. The AM peak hours of generation for a school and residential development are comparable, and the summation of their respective trip volumes is considered to represent an accurate estimation of the volume of trips likely to be generated by the entire development during the AM peak. However, during the afternoon the peak hour of generation for an elementary school generally occurs well before the peak hour of generation for residential development. Nevertheless, in the interest of providing a robust assessment no reduction factor has been applied to the 'critical' PM trip volumes.
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It has been assumed that the school will generate 20 two-way external trips during each of the peak hours, with the remaining trips attributable to the school assumed to be generated internally throughout the adjacent residential development. The internal trips will not be added onto the external road network when the intersection capacity analysis is performed. The following table outlines the trip generation based on the aforementioned draft plan.

Table 1: Trip Generation of Phase 1A

| Land Use | ITE <br> Code | \# of units | AM Peak |  |  | PM Peak |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | In | Out | Total | In | Out | Total |
| Single Residential Units | 210 | 126 | 25 | 72 | 97 | 82 | 46 | 129 |
| Private Road Townhouses | 230 | 63 | 5 | 22 | 28 | 21 | 12 | 33 |
| Public Street Townhouses | 230 | 3 | 0 | 1 | 1 | 1 | 1 | 2 |
| Elementary School | 520 | - | 20 | 20 | 40 | 20 | 20 | 40 |
| Total |  |  | 51 | 115 | 166 | 124 | 79 | 203 |

As shown in Table 1, all elements of the Phase 1A development are expected to generate a total of 166 trips during the weekday AM peak hour of generation, and 203 trips in the PM peak hour of generation. This is consistent with the Fernbank TMP's assumption that the trip rate for residential development within the Fernbank Community will be 1.1 trips per dwelling unit during the PM peak hour.

Based on the above table, the arrival-departure split is approximately $70 / 30$ in favour of departures in the AM, and $65 / 35$ in favour of arrivals in the PM. This is consistent with the findings of the Fernbank TMP, which states that residential trips will be split $65 / 35$ in the AM and PM peak hours of generation.

External trip distribution has been estimated based on a number of factors. These include:

- the objectives and recommendations of the Fernbank TMP;
- the nature of the proposed development within Phase 1A of the Abbott-Fernbank Lands;
- the existing and proposed transport infrastructure in the vicinity of the site and its current capacity;
- the demographic characteristics of the surrounding area and the likely location of future development sites that will generate transport demand.

The assumed external trip distribution can be summarized thus:

- $85 \%$ to/from the east and north (Hazeldean Rd, Palladium Drive, Hwy 417)
- $10 \%$ to/from the south (Fernbank Rd, Terry Fox Drive, Eagleson Rd)
- $5 \%$ to/from the west (Abbott Rd, Fernbank Rd, Stittsville Main St)

This distribution of development generated traffic is considered to be consistent with the findings of the Fernbank TMP, and is also broadly comparable to the trip distribution assumptions for the aforementioned Phase 1 Monarch development. Approximately 10\% of all trips generated by Phase 1 of the Monarch development are expected to originate from or depart to the west and south. These trips will likely pass through Phase 1A of the Abbott-Fernbank Lands to reach the North-South Arterial road, and should be accounted for at each of the proposed intersections when the intersection capacity analysis is performed.

By applying the same relevant trip generation rates to the Monarch development as those used for the Abbott-Fernbank Lands, it has been determined that Phase 1 of the Monarch development is expected to generate 221 and 283 trips in the AM and PM peak hours respectively. Assuming that $10 \%$ of these trips will be to/from the west/south, the number of trips generated by this development that will pass through the Abbott-Fernbank Lands in the AM and PM peak hours will be 22 and 28 respectively.

The distribution of site generated traffic between each of the proposed intersections (including the extra through trips generated by the Monarch development) is assumed to be 50/50.

### 6.0 Conclusions

In summary, the findings of our assessment of the proposed development are as follows:

- the total area of the Phase 1A development makes up approximately $20 \%$ of the area of the entire Abbott-Fernbank Lands, and it consists of 192 residential units and a school;
- the proposed access configuration consists of two intersections with the proposed NorthSouth Arterial road;
- the development of Phase 1A is forecast to generate 166 trips during the weekday AM peak, and 203 trips during the weekday PM peak;
- the construction of Phase 1 of the adjacent Monarch development will result in 22 and 28 trips passing through the Abbott-Fernbank Lands during the AM and PM peak hours respectively;
- most of the generated trips are expected to originate and depart to and from the north and east, where the North-South Arterial road will provide the quickest connection to commercial and industrial centres in the Kanata area, as well as other major arterial routes;

[^1]- the Fernbank TMP's target modal split for public transit for the Hazeldean South Screenline is $20 \%$, and this is considered achievable if public transit facilities of sufficient quality and coverage are provided throughout the area;
- bus stops, sidewalks, and locations for on-site bicycle parking will be determined at the detailed design stage.

We trust this letter adequately addresses the transportation characteristics of the proposed development. Please contact the undersigned if you have any questions or comments.

Yours truly,

## NOVATECH ENGINEERING CONSULTANTS LTD.

Prepared by:


Graham O'Neill, BE E.I.T.

Reviewed by:


Jennifer Luong, P.Eng.
Project Manager


## Appendix G

TDM Checklist

## TDM Measures Checklist:

Residential Developments (multi-family, condominium or subdivision)

## Legend

> | BASIC | $\begin{array}{l}\text { The measure is generally feasible and effective, and in most } \\ \text { cases would benefit the development and its users }\end{array}$ |
| :--- | :--- |
| BETTER | $\begin{array}{l}\text { The measure could maximize support for users of sustainable } \\ \text { modes, and optimize development performance }\end{array}$ |
| $\begin{array}{l}\text { The measure is one of the most dependably effective tools to } \\ \text { encourage the use of sustainable modes }\end{array}$ |  |

| TDM measures: Residential developments |  |  | Check if proposed \& add descriptions |
| :---: | :---: | :---: | :---: |
| 1. TDM PROGRAM MANAGEMENT |  |  |  |
| 1.1 Program coordinator |  |  |  |
| BASIC | * 1.1.1 | Designate an internal coordinator, or contract with an external coordinator | $\sqrt{ }$ Property Management staff of rental apartment building to serve as coordinator |
| 1.2 Travel surveys |  |  |  |
| BETTER | 1.2.1 | Conduct periodic surveys to identify travel-related behaviours, attitudes, challenges and solutions, and to track progress | $\square$ |
| 2. WALKING AND CYCLING |  |  |  |
| 2.1 Information on walking/cycling routes \& destinations |  |  |  |
| BASIC | 2.1.1 | Display local area maps with walking/cycling access routes and key destinations at major entrances (multi-family, condominium) | $\checkmark$ Display City of Ottawa maps and have on hand at Security Desk and Property Management Office |
|  | 2.2 | Bicycle skills training |  |
| BETTER | 2.2.1 | Offer on-site cycling courses for residents, or subsidize off-site courses | $\square$ |


|  | TDM measures: Residential developments |  |  <br> add descriptions |
| :--- | :--- | :--- | :--- | :--- |
|  | 3. | TRANSIT |  |
|  | 3.1 | Transit information |  |

TDM measures: Residential developments $\quad$ Check if proposed \& add descriptions

## 6. TDM MARKETING \& COMMUNICATIONS

### 6.1 Multimodal travel information

6.1.1 Provide a multimodal travel option information package to new residents

Provide multimodal travel option information in standard Welcome Manual for new residents (tenants)

### 6.2 Personalized trip planning

BETTER * 6.2.1 Offer personalized trip planning to new residents

## Appendix H

SYNCHRO and SIDRA Capacity Analysis

## Existing Conditions

## Existing AM

3: Fernbank Road \& Robert Grant Avenue

|  | $\gamma$ |  | $\longleftarrow$ | 4 | $\checkmark$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | \% | 4 | $\uparrow$ | 「 | \% | 「 |
| Traffic Volume (vph) | 28 | 296 | 195 | 157 | 152 | 26 |
| Future Volume (vph) | 28 | 296 | 195 | 157 | 152 | 26 |
| Lane Group Flow (vph) | 31 | 329 | 217 | 174 | 169 | 29 |
| Turn Type | Prot | NA | NA | Perm | Perm | Perm |
| Protected Phases | 5 | 2 | 6 |  |  |  |
| Permitted Phases |  |  |  | 6 | 4 | 4 |
| Detector Phase | 5 | 2 | 6 | - | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 16.2 | 52.2 | 52.2 | 52.2 | 30.0 | 30.0 |
| Total Split (s) | 26.2 | 83.4 | 57.2 | 57.2 | 36.0 | 36.0 |
| Total Split (\%) | 21.9\% | 69.8\% | 47.9\% | 47.9\% | 30.2\% | 30.2\% |
| Yellow Time (s) | 4.6 | 4.6 | 4.6 | 4.6 | 3.3 | 3.3 |
| All-Red Time (s) | 1.6 | 1.6 | 1.6 | 1.6 | 2.7 | 2.7 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.2 | 6.2 | 6.2 | 6.2 | 6.0 | 6.0 |
| Lead/Lag | Lead |  | Lag | Lag |  |  |
| Lead-Lag Optimize? | Yes |  | Yes | Yes |  |  |
| Recall Mode | Max | Min | Min | Min | Max | Max |
| Act Effct Green (s) | 20.0 | 41.8 | 15.6 | 15.6 | 30.1 | 30.1 |
| Actuated g/C Ratio | 0.24 | 0.50 | 0.19 | 0.19 | 0.36 | 0.36 |
| v/c Ratio | 0.09 | 0.37 | 0.66 | 0.43 | 0.28 | 0.05 |
| Control Delay | 27.6 | 14.3 | 42.0 | 8.2 | 22.0 | 8.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 27.6 | 14.3 | 42.0 | 8.2 | 22.0 | 8.1 |
| LOS | C | B | D | A | C | A |
| Approach Delay |  | 15.4 | 27.0 |  | 20.0 |  |
| Approach LOS |  | B | C |  | B |  |
| Queue Length 50th (m) | 3.9 | 30.9 | 32.6 | 0.0 | 19.0 | 0.0 |
| Queue Length 95th (m) | 11.6 | 48.1 | 54.0 | 15.1 | 37.8 | 5.7 |
| Internal Link Dist ( $m$ ) |  | 217.9 | 258.1 |  | 237.6 |  |
| Turn Bay Length (m) | 100.0 |  |  | 100.0 | 80.0 |  |
| Base Capacity (vph) | 329 | 1640 | 1073 | 938 | 593 | 539 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.09 | 0.20 | 0.20 | 0.19 | 0.28 | 0.05 |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 119.4 |  |  |  |  |  |  |
| Actuated Cycle Length: 84.1 |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.66 |  |  |  |  |  |  |
| Intersection Signal Delay: 21.1 |  |  |  | Intersection LOS: C |  |  |
| Intersection Capacity Utilization 39.2\% |  |  |  | ICU Level of Service A |  |  |

Analysis Period (min) 15

Existing AM
3: Fernbank Road \& Robert Grant Avenue
Splits and Phases: 3: Fernbank Road \& Robert Grant Avenue


Existing AM
8: Bobolink Ridge \& Livery Street

|  | $\rightarrow$ | $\leftarrow$ | $\checkmark$ |  |
| :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | WBT | SBL |  |
| Lane Configurations | $\uparrow$ | $\hat{\beta}$ | M |  |
| Traffic Volume (vph) | 35 | 64 | 2 |  |
| Future Volume (vph) | 35 | 64 | 2 |  |
| Lane Group Flow (vph) | 56 | 71 | 55 |  |
| Sign Control | Free | Free | Stop |  |
| $\frac{\text { Intersection Summary }}{\text { Control Type: Unsignalized }}$ |  |  |  |  |
|  |  |  |  |  |
| Intersection Capacity Utilization 19.5\% |  |  |  | ICU Level of Service A |
| Analysis Period (min) 15 |  |  |  |  |

## Existing AM

## 8: Bobolink Ridge \& Livery Street




## Existing PM

3: Fernbank Road \& Robert Grant Avenue

|  | $\gamma$ |  | $\longleftarrow$ | 4 | $\checkmark$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | \% | 4 | $\uparrow$ | 「 | \% | 「 |
| Traffic Volume (vph) | 17 | 245 | 440 | 176 | 163 | 25 |
| Future Volume (vph) | 17 | 245 | 440 | 176 | 163 | 25 |
| Lane Group Flow (vph) | 19 | 272 | 489 | 196 | 181 | 28 |
| Turn Type | Prot | NA | NA | Perm | Perm | Perm |
| Protected Phases | 5 | 2 | 6 |  |  |  |
| Permitted Phases |  |  |  | 6 | 4 | 4 |
| Detector Phase | 5 | 2 | 6 | - | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 16.2 | 52.2 | 52.2 | 52.2 | 30.0 | 30.0 |
| Total Split (s) | 26.2 | 94.4 | 68.2 | 68.2 | 36.0 | 36.0 |
| Total Split (\%) | 20.1\% | 72.4\% | 52.3\% | 52.3\% | 27.6\% | 27.6\% |
| Yellow Time (s) | 4.6 | 4.6 | 4.6 | 4.6 | 3.3 | 3.3 |
| All-Red Time (s) | 1.6 | 1.6 | 1.6 | 1.6 | 2.7 | 2.7 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.2 | 6.2 | 6.2 | 6.2 | 6.0 | 6.0 |
| Lead/Lag | Lead |  | Lag | Lag |  |  |
| Lead-Lag Optimize? | Yes |  | Yes | Yes |  |  |
| Recall Mode | Max | Min | Min | Min | Max | Max |
| Act Effct Green (s) | 20.1 | 59.9 | 33.5 | 33.5 | 30.2 | 30.2 |
| Actuated g/C Ratio | 0.20 | 0.58 | 0.33 | 0.33 | 0.29 | 0.29 |
| v/c Ratio | 0.06 | 0.27 | 0.84 | 0.32 | 0.38 | 0.07 |
| Control Delay | 37.8 | 10.9 | 45.1 | 4.7 | 33.6 | 11.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 37.8 | 10.9 | 45.1 | 4.7 | 33.6 | 11.6 |
| LOS | D | B | D | A | C | B |
| Approach Delay |  | 12.6 | 33.5 |  | 30.7 |  |
| Approach LOS |  | B | C |  | C |  |
| Queue Length 50th (m) | 3.1 | 24.6 | 88.8 | 0.0 | 28.3 | 0.0 |
| Queue Length 95th (m) | 10.3 | 37.4 | 126.2 | 13.7 | 55.5 | 7.1 |
| Internal Link Dist ( $m$ ) |  | 217.9 | 258.1 |  | 237.6 |  |
| Turn Bay Length (m) | 100.0 |  |  | 100.0 | 80.0 |  |
| Base Capacity (vph) | 339 | 1517 | 1087 | 974 | 476 | 427 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.06 | 0.18 | 0.45 | 0.20 | 0.38 | 0.07 |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 130.4 |  |  |  |  |  |  |
| Actuated Cycle Length: 102.4 |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.84 |  |  |  |  |  |  |
| Intersection Signal Delay: 27.9 |  |  |  | Intersection LOS: C |  |  |
| Intersection Capacity Utilization 44.1\% |  |  |  | ICU Level of Service A |  |  |

Analysis Period (min) 15

## Existing PM

3: Fernbank Road \& Robert Grant Avenue
Splits and Phases: 3: Fernbank Road \& Robert Grant Avenue


## Existing PM

8: Bobolink Ridge \& Livery Street


## Existing PM

## 8: Bobolink Ridge \& Livery Street




## MOVEMENT SUMMARY

## Site: [Existing - Abbott/Robert Grant]

AM Peak
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \end{aligned}$ |  | Deman Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \\ & \hline \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 243 | 2.0 | 0.172 | 8.8 | LOS A | 0.9 | 6.5 | 0.11 | 0.61 | 0.11 | 53.1 |
| 3 | R2 | 20 | 2.0 | 0.172 | 4.0 | LOS A | 0.9 | 6.5 | 0.11 | 0.61 | 0.11 | 51.9 |
| Appr |  | 263 | 2.0 | 0.172 | 8.5 | LOS A | 0.9 | 6.5 | 0.11 | 0.61 | 0.11 | 53.0 |
| East: Abbott Street East |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 16 | 2.0 | 0.067 | 8.4 | LOS A | 0.3 | 2.3 | 0.39 | 0.47 | 0.39 | 47.6 |
| 5 | T1 | 60 | 2.0 | 0.067 | 3.9 | LOS A | 0.3 | 2.3 | 0.39 | 0.47 | 0.39 | 47.5 |
| Approach |  | 76 | 2.0 | 0.067 | 4.8 | LOS A | 0.3 | 2.3 | 0.39 | 0.47 | 0.39 | 47.5 |
| West: Abbott Street E |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | T1 | 23 | 2.0 | 0.104 | 2.9 | LOS A | 0.6 | 4.1 | 0.09 | 0.38 | 0.09 | 49.0 |
| 12 | R2 | 137 | 2.0 | 0.104 | 2.9 | LOS A | 0.6 | 4.1 | 0.09 | 0.38 | 0.09 | 47.9 |
| Appr |  | 160 | 2.0 | 0.104 | 2.9 | LOS A | 0.6 | 4.1 | 0.09 | 0.38 | 0.09 | 48.1 |
| All V | icles | 499 | 2.0 | 0.172 | 6.1 | LOS A | 0.9 | 6.5 | 0.15 | 0.52 | 0.15 | 50.5 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## Site: [Existing-Abbott/Robert Grant]

PM Peak
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | Turn | Demand <br> Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | $\begin{aligned} & \text { Deg. } \\ & \text { Satn } \\ & \text { v/c } \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 181 | 2.0 | 0.134 | 9.0 | LOS A | 0.7 | 4.9 | 0.18 | 0.61 | 0.18 | 52.7 |
| 3 | R2 | 7 | 2.0 | 0.134 | 4.1 | LOS A | 0.7 | 4.9 | 0.18 | 0.61 | 0.18 | 51.6 |
| Appr |  | 188 | 2.0 | 0.134 | 8.8 | LOS A | 0.7 | 4.9 | 0.18 | 0.61 | 0.18 | 52.7 |
| East: Abbott Street East |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 30 | 2.0 | 0.079 | 8.1 | LOS A | 0.4 | 2.8 | 0.34 | 0.48 | 0.34 | 47.6 |
| 5 | T1 | 63 | 2.0 | 0.079 | 3.6 | LOS A | 0.4 | 2.8 | 0.34 | 0.48 | 0.34 | 47.4 |
| Approach |  | 93 | 2.0 | 0.079 | 5.1 | LOS A | 0.4 | 2.8 | 0.34 | 0.48 | 0.34 | 47.4 |
| West: Abbott Street E |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | T1 | 53 | 2.0 | 0.202 | 2.9 | LOS A | 1.2 | 8.6 | 0.14 | 0.38 | 0.14 | 48.9 |
| 12 | R2 | 252 | 2.0 | 0.202 | 3.0 | LOS A | 1.2 | 8.6 | 0.14 | 0.38 | 0.14 | 47.7 |
| Appr |  | 306 | 2.0 | 0.202 | 3.0 | LOS A | 1.2 | 8.6 | 0.14 | 0.38 | 0.14 | 47.9 |
| All Ve | icles | 587 | 2.0 | 0.202 | 5.2 | LOS A | 1.2 | 8.6 | 0.19 | 0.47 | 0.19 | 49.3 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## Site: [Existing - Bobolink/Robert Grant]

AM Peak
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Demand Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | $\begin{aligned} & \text { Deg. } \\ & \text { Satn } \\ & \text { v/c } \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 1 | 2.0 | 0.134 | 8.9 | LOS A | 0.7 | 4.9 | 0.13 | 0.40 | 0.13 | 56.1 |
| 2 | T1 | 182 | 2.0 | 0.134 | 4.3 | LOS A | 0.7 | 4.9 | 0.13 | 0.40 | 0.13 | 56.2 |
| 3 | R2 | 13 | 2.0 | 0.134 | 4.0 | LOS A | 0.7 | 4.9 | 0.13 | 0.40 | 0.13 | 54.8 |
| Appr |  | 197 | 2.0 | 0.134 | 4.3 | LOS A | 0.7 | 4.9 | 0.13 | 0.40 | 0.13 | 56.1 |
| East: Bobolink Drive |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 24 | 2.0 | 0.090 | 9.6 | LOS A | 0.4 | 3.2 | 0.34 | 0.54 | 0.34 | 54.9 |
| 5 | T1 | 1 | 2.0 | 0.090 | 5.0 | LOS A | 0.4 | 3.2 | 0.34 | 0.54 | 0.34 | 54.9 |
| 6 | R2 | 81 | 2.0 | 0.090 | 4.8 | LOS A | 0.4 | 3.2 | 0.34 | 0.54 | 0.34 | 53.6 |
| Appr |  | 107 | 2.0 | 0.090 | 5.9 | LOS A | 0.4 | 3.2 | 0.34 | 0.54 | 0.34 | 53.9 |
| North: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 31 | 2.0 | 0.104 | 8.9 | LOS A | 0.6 | 4.0 | 0.12 | 0.45 | 0.12 | 55.5 |
| 8 | T1 | 121 | 2.0 | 0.104 | 4.2 | LOS A | 0.6 | 4.0 | 0.12 | 0.45 | 0.12 | 55.6 |
| 9 | R2 | 1 | 2.0 | 0.104 | 4.0 | LOS A | 0.6 | 4.0 | 0.12 | 0.45 | 0.12 | 54.2 |
| Approach |  | 153 | 2.0 | 0.104 | 5.2 | LOS A | 0.6 | 4.0 | 0.12 | 0.45 | 0.12 | 55.5 |
| West: Bobolink Drive |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 1 | 2.0 | 0.003 | 9.5 | LOS A | 0.0 | 0.1 | 0.31 | 0.49 | 0.31 | 54.4 |
| 11 | T1 | 1 | 2.0 | 0.003 | 4.8 | LOS A | 0.0 | 0.1 | 0.31 | 0.49 | 0.31 | 54.5 |
| 12 | R2 | 1 | 2.0 | 0.003 | 4.6 | LOS A | 0.0 | 0.1 | 0.31 | 0.49 | 0.31 | 53.2 |
| Appr |  | 3 | 2.0 | 0.003 | 6.3 | LOS A | 0.0 | 0.1 | 0.31 | 0.49 | 0.31 | 54.1 |
| All V | icles | 460 | 2.0 | 0.134 | 5.0 | LOS A | 0.7 | 4.9 | 0.18 | 0.45 | 0.18 | 55.4 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## Site: [Existing - Bobolink/Robert Grant]

PM Peak
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman Total veh/h | ows HV $\%$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 1 | 2.0 | 0.135 | 9.1 | LOS A | 0.7 | 4.9 | 0.23 | 0.43 | 0.23 | 55.7 |
| 2 | T1 | 140 | 2.0 | 0.135 | 4.5 | LOS A | 0.7 | 4.9 | 0.23 | 0.43 | 0.23 | 55.8 |
| 3 | R2 | 39 | 2.0 | 0.135 | 4.3 | LOS A | 0.7 | 4.9 | 0.23 | 0.43 | 0.23 | 54.5 |
| Appr |  | 180 | 2.0 | 0.135 | 4.5 | LOS A | 0.7 | 4.9 | 0.23 | 0.43 | 0.23 | 55.5 |
| East: Bobolink Drive |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 20 | 2.0 | 0.049 | 9.4 | LOS A | 0.2 | 1.7 | 0.30 | 0.54 | 0.30 | 54.6 |
| 5 | T1 | 1 | 2.0 | 0.049 | 4.7 | LOS A | 0.2 | 1.7 | 0.30 | 0.54 | 0.30 | 54.7 |
| 6 | R2 | 39 | 2.0 | 0.049 | 4.5 | LOS A | 0.2 | 1.7 | 0.30 | 0.54 | 0.30 | 53.4 |
| Appr |  | 60 | 2.0 | 0.049 | 6.1 | LOS A | 0.2 | 1.7 | 0.30 | 0.54 | 0.30 | 53.8 |
| North: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 80 | 2.0 | 0.184 | 8.8 | LOS A | 1.1 | 7.5 | 0.11 | 0.48 | 0.11 | 55.2 |
| 8 | T1 | 202 | 2.0 | 0.184 | 4.2 | LOS A | 1.1 | 7.5 | 0.11 | 0.48 | 0.11 | 55.3 |
| 9 | R2 | 1 | 2.0 | 0.184 | 4.0 | LOS A | 1.1 | 7.5 | 0.11 | 0.48 | 0.11 | 54.0 |
| Appr |  | 283 | 2.0 | 0.184 | 5.5 | LOS A | 1.1 | 7.5 | 0.11 | 0.48 | 0.11 | 55.3 |
| West: Bobolink Drive |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 1 | 2.0 | 0.003 | 10.0 | LOS B | 0.0 | 0.1 | 0.41 | 0.51 | 0.41 | 54.1 |
| 11 | T1 | 1 | 2.0 | 0.003 | 5.4 | LOS A | 0.0 | 0.1 | 0.41 | 0.51 | 0.41 | 54.2 |
| 12 | R2 | 1 | 2.0 | 0.003 | 5.2 | LOS A | 0.0 | 0.1 | 0.41 | 0.51 | 0.41 | 52.9 |
| Appr |  | 3 | 2.0 | 0.003 | 6.8 | LOS A | 0.0 | 0.1 | 0.41 | 0.51 | 0.41 | 53.7 |
| All V | icles | 527 | 2.0 | 0.184 | 5.2 | LOS A | 1.1 | 7.5 | 0.18 | 0.47 | 0.18 | 55.2 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Future Background 2023

|  | $\rangle$ |  | $\leftarrow$ | 4 |  | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | \% | 4 | 4 | 「 | \% | 「 |
| Traffic Volume (vph) | 43 | 322 | 211 | 183 | 175 | 37 |
| Future Volume (vph) | 43 | 322 | 211 | 183 | 175 | 37 |
| Lane Group Flow (vph) | 43 | 322 | 211 | 183 | 175 | 37 |
| Turn Type | Prot | NA | NA | Perm | Perm | Perm |
| Protected Phases | 5 | 2 | 6 |  |  |  |
| Permitted Phases |  |  |  | 6 | 4 | 4 |
| Detector Phase | 5 | 2 | 6 | 6 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 16.2 | 52.2 | 52.2 | 52.2 | 30.0 | 30.0 |
| Total Split (s) | 26.2 | 83.4 | 57.2 | 57.2 | 36.0 | 36.0 |
| Total Split (\%) | 21.9\% | 69.8\% | 47.9\% | 47.9\% | 30.2\% | 30.2\% |
| Yellow Time (s) | 4.6 | 4.6 | 4.6 | 4.6 | 3.3 | 3.3 |
| All-Red Time (s) | 1.6 | 1.6 | 1.6 | 1.6 | 2.7 | 2.7 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.2 | 6.2 | 6.2 | 6.2 | 6.0 | 6.0 |
| Lead/Lag | Lead |  | Lag | Lag |  |  |
| Lead-Lag Optimize? | Yes |  | Yes | Yes |  |  |
| Recall Mode | Max | Min | Min | Min | Max | Max |
| Act Effct Green (s) | 20.0 | 41.5 | 15.3 | 15.3 | 30.1 | 30.1 |
| Actuated g/C Ratio | 0.24 | 0.50 | 0.18 | 0.18 | 0.36 | 0.36 |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.13 | 0.36 | 0.66 | 0.45 | 0.29 | 0.07 |
| Control Delay | 27.9 | 14.2 | 41.9 | 8.4 | 21.9 | 7.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 27.9 | 14.2 | 41.9 | 8.4 | 21.9 | 7.4 |
| LOS | C | B | D | A | C | A |
| Approach Delay |  | 15.8 | 26.3 |  | 19.4 |  |
| Approach LOS |  | B | C |  | B |  |
| Queue Length 50th (m) | 5.4 | 30.0 | 31.6 | 0.0 | 19.6 | 0.0 |
| Queue Length 95th (m) | 14.6 | 47.1 | 52.7 | 15.5 | 38.8 | 6.3 |
| Internal Link Dist (m) |  | 217.9 | 258.1 |  | 237.6 |  |
| Turn Bay Length (m) | 100.0 |  |  | 100.0 | 80.0 |  |
| Base Capacity (vph) | 330 | 1646 | 1077 | 944 | 596 | 546 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.13 | 0.20 | 0.20 | 0.19 | 0.29 | 0.07 |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 119.4 |  |  |  |  |  |  |
| Actuated Cycle Length: 83.8 |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.66 |  |  |  |  |  |  |
| Intersection Signal Delay: 20.9 |  |  |  | Intersection LOS: C |  |  |
| Intersection Capacity Utilization 41.5\% |  |  |  | ICU Level of Service A |  |  |

Analysis Period (min) 15

Future Background 2023 AM
3: Fernbank Road \& Robert Grant Avenue
Splits and Phases: 3: Fernbank Road \& Robert Grant Avenue



## Intersection Summary

Control Type: Unsignalized
Intersection Capacity Utilization 19.5\%
ICU Level of Service A
Analysis Period (min) 15

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3.4 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | F |  |  |  |
| Traffic Vol, veh/h | 15 | 35 | 64 | 0 | 2 | 48 |
| Future Vol, veh/h | 15 | 35 | 64 | 0 | 2 | 48 |
| Conflicting Peds, \#/hr | 8 | 0 | 0 | 8 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - None | - | None |  |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, $\%$ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 15 | 35 | 64 | 0 | 2 | 48 |



|  | $\rangle$ |  | $\leftarrow$ | 4 |  | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | \% | $\uparrow$ | $\uparrow$ | 「 | \% | 「 |
| Traffic Volume (vph) | 30 | 269 | 476 | 197 | 187 | 36 |
| Future Volume (vph) | 30 | 269 | 476 | 197 | 187 | 36 |
| Lane Group Flow (vph) | 30 | 269 | 476 | 197 | 187 | 36 |
| Turn Type | Prot | NA | NA | Perm | Perm | Perm |
| Protected Phases | 5 | 2 | 6 |  |  |  |
| Permitted Phases |  |  |  | 6 | 4 | 4 |
| Detector Phase | 5 | 2 | 6 | 6 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 16.2 | 52.2 | 52.2 | 52.2 | 30.0 | 30.0 |
| Total Split (s) | 26.2 | 94.4 | 68.2 | 68.2 | 36.0 | 36.0 |
| Total Split (\%) | 20.1\% | 72.4\% | 52.3\% | 52.3\% | 27.6\% | 27.6\% |
| Yellow Time (s) | 4.6 | 4.6 | 4.6 | 4.6 | 3.3 | 3.3 |
| All-Red Time (s) | 1.6 | 1.6 | 1.6 | 1.6 | 2.7 | 2.7 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.2 | 6.2 | 6.2 | 6.2 | 6.0 | 6.0 |
| Lead/Lag | Lead |  | Lag | Lag |  |  |
| Lead-Lag Optimize? | Yes |  | Yes | Yes |  |  |
| Recall Mode | Max | Min | Min | Min | Max | Max |
| Act Effct Green (s) | 20.1 | 58.9 | 32.6 | 32.6 | 30.2 | 30.2 |
| Actuated g/C Ratio | 0.20 | 0.58 | 0.32 | 0.32 | 0.30 | 0.30 |
| v/c Ratio | 0.09 | 0.26 | 0.83 | 0.33 | 0.39 | 0.08 |
| Control Delay | 37.4 | 10.9 | 44.8 | 4.8 | 33.3 | 10.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 37.4 | 10.9 | 44.8 | 4.8 | 33.3 | 10.4 |
| LOS | D | B | D | A | C | B |
| Approach Delay |  | 13.6 | 33.1 |  | 29.6 |  |
| Approach LOS |  | B | C |  | C |  |
| Queue Length 50th (m) | 4.8 | 24.3 | 85.5 | 0.0 | 28.9 | 0.0 |
| Queue Length 95th (m) | 14.2 | 37.0 | 122.1 | 13.7 | 56.2 | 7.8 |
| Internal Link Dist (m) |  | 217.9 | 258.1 |  | 237.6 |  |
| Turn Bay Length (m) | 100.0 |  |  | 100.0 | 80.0 |  |
| Base Capacity (vph) | 343 | 1531 | 1097 | 982 | 481 | 436 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.09 | 0.18 | 0.43 | 0.20 | 0.39 | 0.08 |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 130.4 |  |  |  |  |  |  |
| Actuated Cycle Length: 101.4 |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.83 |  |  |  |  |  |  |
| Intersection Signal Delay: 27.5 |  |  |  | Intersection LOS: C |  |  |
| Intersection Capacity Utilization 47.5\% |  |  |  | ICU Level of Service A |  |  |

Analysis Period (min) 15

Future Background 2023 PM
3: Fernbank Road \& Robert Grant Avenue
Splits and Phases: 3: Fernbank Road \& Robert Grant Avenue


|  |  | $\leftarrow$ |  |
| :--- | ---: | ---: | ---: |
|  | $\rightarrow$ |  |  |
| Lane Group | EBT | WBT | SBL |
| Lane Configurations | $\uparrow$ | $\ominus$ |  |
| Traffic Volume (vph) | 75 | 34 | 1 |
| Future Volume (vph) | 75 | 34 | 1 |
| Lane Group Flow (vph) | 124 | 37 | 31 |
| Sign Control | Free | Free | Stop |

## Intersection Summary

Control Type: Unsignalized
Intersection Capacity Utilization 23.7\%
ICU Level of Service A
Analysis Period (min) 15

Future Background 2023 PM
8: Bobolink Ridge \& Livery Street

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3.3 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | F |  |  |  |
| Traffic Vol, veh/h | 49 | 75 | 34 | 3 | 1 | 30 |
| Future Vol, veh/h | 49 | 75 | 34 | 3 | 1 | 30 |
| Conflicting Peds, \#/hr | 11 | 0 | 0 | 11 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - None | - | None |  |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, $\%$ | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, $\%$ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 49 | 75 | 34 | 3 | 1 | 30 |


| Major/Minor $\quad$ N | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 48 | 0 | - | 0 | 220 | 47 |
| Stage 1 | - | - | - | - | 47 | - |
| Stage 2 | - | - | - | - | 173 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1559 | - | - | - | 768 | 1022 |
| Stage 1 | - | - | - | - | 975 | - |
| Stage 2 | - | - | - | - | 857 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1544 | - | - | - | 730 | 1012 |
| Mov Cap-2 Maneuver | - | - | - | - | 730 | - |
| Stage 1 | - | - | - | - | 934 | - |
| Stage 2 | - | - | - | - | 849 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 2.9 |  | 0 |  | 8.7 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT WBR SBLn1 |  |  |
| Capacity (veh/h) |  | 1544 | - | - | - | 1000 |
| HCM Lane V/C Ratio |  | 0.032 | - | - | - | 0.031 |
| HCM Control Delay (s) |  | 7.4 | 0 | - | - | 8.7 |
| HCM Lane LOS |  | A | A | - | - | A |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | - | 0.1 |

## MOVEMENT SUMMARY

## Site: [BG2023 - Abbott/Robert Grant]

AM Peak
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Demand Total veh/h | ows HV $\%$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 247 | 2.0 | 0.188 | 8.8 | LOS A | 1.0 | 7.4 | 0.11 | 0.60 | 0.11 | 53.3 |
| 3 | R2 | 43 | 2.0 | 0.188 | 4.0 | LOS A | 1.0 | 7.4 | 0.11 | 0.60 | 0.11 | 52.2 |
| Appr |  | 290 | 2.0 | 0.188 | 8.1 | LOS A | 1.0 | 7.4 | 0.11 | 0.60 | 0.11 | 53.2 |
| East: Abbott Street East |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 40 | 2.0 | 0.087 | 8.5 | LOS A | 0.4 | 3.1 | 0.40 | 0.53 | 0.40 | 47.2 |
| 5 | T1 | 58 | 2.0 | 0.087 | 4.0 | LOS A | 0.4 | 3.1 | 0.40 | 0.53 | 0.40 | 47.0 |
| Appr |  | 98 | 2.0 | 0.087 | 5.8 | LOS A | 0.4 | 3.1 | 0.40 | 0.53 | 0.40 | 47.1 |
| West: Abbott Street E |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | T1 | 23 | 2.0 | 0.119 | 3.0 | LOS A | 0.7 | 4.7 | 0.16 | 0.38 | 0.16 | 48.8 |
| 12 | R2 | 147 | 2.0 | 0.119 | 3.0 | LOS A | 0.7 | 4.7 | 0.16 | 0.38 | 0.16 | 47.7 |
| Approach |  | 170 | 2.0 | 0.119 | 3.0 | LOS A | 0.7 | 4.7 | 0.16 | 0.38 | 0.16 | 47.8 |
| All Vehicles |  | 558 | 2.0 | 0.188 | 6.2 | LOS A | 1.0 | 7.4 | 0.18 | 0.52 | 0.18 | 50.3 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## Site: [BG2023 - Abbott/Robert Grant]

PM Peak
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman Total veh/h | $\begin{array}{r} \text { lows } \\ \text { HV } \\ \% \end{array}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 186 | 2.0 | 0.153 | 9.0 | LOS A | 0.8 | 5.8 | 0.18 | 0.60 | 0.18 | 53.1 |
| 3 | R2 | 30 | 2.0 | 0.153 | 4.1 | LOS A | 0.8 | 5.8 | 0.18 | 0.60 | 0.18 | 51.9 |
| Appr |  | 216 | 2.0 | 0.153 | 8.3 | LOS A | 0.8 | 5.8 | 0.18 | 0.60 | 0.18 | 52.9 |
| East: Abbott Street East |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 45 | 2.0 | 0.090 | 8.2 | LOS A | 0.5 | 3.2 | 0.35 | 0.51 | 0.35 | 47.3 |
| 5 | T1 | 62 | 2.0 | 0.090 | 3.7 | LOS A | 0.5 | 3.2 | 0.35 | 0.51 | 0.35 | 47.1 |
| Approach |  | 107 | 2.0 | 0.090 | 5.6 | LOS A | 0.5 | 3.2 | 0.35 | 0.51 | 0.35 | 47.2 |
| West: Abbott Street E |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | T1 | 52 | 2.0 | 0.210 | 3.0 | LOS A | 1.3 | 8.9 | 0.18 | 0.38 | 0.18 | 48.8 |
| 12 | R2 | 254 | 2.0 | 0.210 | 3.1 | LOS A | 1.3 | 8.9 | 0.18 | 0.38 | 0.18 | 47.6 |
| Appr |  | 306 | 2.0 | 0.210 | 3.0 | LOS A | 1.3 | 8.9 | 0.18 | 0.38 | 0.18 | 47.8 |
| All V | icles | 629 | 2.0 | 0.210 | 5.3 | LOS A | 1.3 | 8.9 | 0.21 | 0.48 | 0.21 | 49.4 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## Site: [BG2023-Bobolink/Robert Grant]

AM Peak
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | Turn | Deman Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | $\begin{aligned} & \text { Deg. } \\ & \text { Satn } \\ & \text { v/c } \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 1 | 2.0 | 0.151 | 8.9 | LOS A | 0.8 | 5.6 | 0.13 | 0.40 | 0.13 | 56.2 |
| 2 | T1 | 212 | 2.0 | 0.151 | 4.2 | LOS A | 0.8 | 5.6 | 0.13 | 0.40 | 0.13 | 56.2 |
| 3 | R2 | 12 | 2.0 | 0.151 | 4.0 | LOS A | 0.8 | 5.6 | 0.13 | 0.40 | 0.13 | 54.9 |
| Appr |  | 225 | 2.0 | 0.151 | 4.3 | LOS A | 0.8 | 5.6 | 0.13 | 0.40 | 0.13 | 56.2 |
| East: Bobolink Drive |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 22 | 2.0 | 0.083 | 9.7 | LOS A | 0.4 | 2.9 | 0.37 | 0.55 | 0.37 | 54.8 |
| 5 | T1 | 1 | 2.0 | 0.083 | 5.1 | LOS A | 0.4 | 2.9 | 0.37 | 0.55 | 0.37 | 54.9 |
| 6 | R2 | 73 | 2.0 | 0.083 | 4.9 | LOS A | 0.4 | 2.9 | 0.37 | 0.55 | 0.37 | 53.5 |
| Appr |  | 96 | 2.0 | 0.083 | 6.0 | LOS A | 0.4 | 2.9 | 0.37 | 0.55 | 0.37 | 53.8 |
| North: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 28 | 2.0 | 0.125 | 8.8 | LOS A | 0.7 | 4.9 | 0.12 | 0.44 | 0.12 | 55.7 |
| 8 | T1 | 158 | 2.0 | 0.125 | 4.2 | LOS A | 0.7 | 4.9 | 0.12 | 0.44 | 0.12 | 55.8 |
| 9 | R2 | 1 | 2.0 | 0.125 | 4.0 | LOS A | 0.7 | 4.9 | 0.12 | 0.44 | 0.12 | 54.4 |
| Approach |  | 187 | 2.0 | 0.125 | 4.9 | LOS A | 0.7 | 4.9 | 0.12 | 0.44 | 0.12 | 55.7 |
| West: Bobolink Drive |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 1 | 2.0 | 0.003 | 9.6 | LOS A | 0.0 | 0.1 | 0.34 | 0.49 | 0.34 | 54.3 |
| 11 | T1 | 1 | 2.0 | 0.003 | 5.0 | LOS A | 0.0 | 0.1 | 0.34 | 0.49 | 0.34 | 54.4 |
| 12 | R2 | 1 | 2.0 | 0.003 | 4.7 | LOS A | 0.0 | 0.1 | 0.34 | 0.49 | 0.34 | 53.1 |
| Appr |  | 3 | 2.0 | 0.003 | 6.4 | LOS A | 0.0 | 0.1 | 0.34 | 0.49 | 0.34 | 54.0 |
| All Ve | icles | 511 | 2.0 | 0.151 | 4.8 | LOS A | 0.8 | 5.6 | 0.17 | 0.44 | 0.17 | 55.6 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## Site: [BG2023-Bobolink/Robert Grant]

PM Peak
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | Turn | Deman <br> Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 1 | 2.0 | 0.151 | 9.1 | LOS A | 0.8 | 5.6 | 0.22 | 0.42 | 0.22 | 55.8 |
| 2 | T1 | 170 | 2.0 | 0.151 | 4.5 | LOS A | 0.8 | 5.6 | 0.22 | 0.42 | 0.22 | 55.8 |
| 3 | R2 | 35 | 2.0 | 0.151 | 4.2 | LOS A | 0.8 | 5.6 | 0.22 | 0.42 | 0.22 | 54.5 |
| Appr | ch | 206 | 2.0 | 0.151 | 4.4 | LOS A | 0.8 | 5.6 | 0.22 | 0.42 | 0.22 | 55.6 |
| East: Bobolink Drive |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 18 | 2.0 | 0.045 | 9.5 | LOS A | 0.2 | 1.6 | 0.33 | 0.54 | 0.33 | 54.5 |
| 5 | T1 | 1 | 2.0 | 0.045 | 4.9 | LOS A | 0.2 | 1.6 | 0.33 | 0.54 | 0.33 | 54.6 |
| 6 | R2 | 35 | 2.0 | 0.045 | 4.7 | LOS A | 0.2 | 1.6 | 0.33 | 0.54 | 0.33 | 53.3 |
| Appr |  | 54 | 2.0 | 0.045 | 6.3 | LOS A | 0.2 | 1.6 | 0.33 | 0.54 | 0.33 | 53.7 |
| North: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 72 | 2.0 | 0.189 | 8.8 | LOS A | 1.1 | 7.9 | 0.11 | 0.47 | 0.11 | 55.4 |
| 8 | T1 | 221 | 2.0 | 0.189 | 4.2 | LOS A | 1.1 | 7.9 | 0.11 | 0.47 | 0.11 | 55.5 |
| 9 | R2 | 1 | 2.0 | 0.189 | 4.0 | LOS A | 1.1 | 7.9 | 0.11 | 0.47 | 0.11 | 54.1 |
| Approach |  | 294 | 2.0 | 0.189 | 5.3 | LOS A | 1.1 | 7.9 | 0.11 | 0.47 | 0.11 | 55.4 |
| West: Bobolink Drive |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 1 | 2.0 | 0.003 | 10.0 | LOS B | 0.0 | 0.1 | 0.42 | 0.51 | 0.42 | 54.1 |
| 11 | T1 | 1 | 2.0 | 0.003 | 5.4 | LOS A | 0.0 | 0.1 | 0.42 | 0.51 | 0.42 | 54.1 |
| 12 | R2 | 1 | 2.0 | 0.003 | 5.2 | LOS A | 0.0 | 0.1 | 0.42 | 0.51 | 0.42 | 52.9 |
| Appr |  | 3 | 2.0 | 0.003 | 6.9 | LOS A | 0.0 | 0.1 | 0.42 | 0.51 | 0.42 | 53.7 |
| All V | cles | 557 | 2.0 | 0.189 | 5.1 | LOS A | 1.1 | 7.9 | 0.17 | 0.46 | 0.17 | 55.3 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Future Background 2028

Total Future Background 2028 AM
3: Fernbank Road \& Robert Grant Avenue

|  | $\rangle$ |  | $\leftarrow$ | 4 |  | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | \% | 4 | $\uparrow$ | 「 | \% | 「 |
| Traffic Volume (vph) | 55 | 359 | 241 | 235 | 257 | 44 |
| Future Volume (vph) | 55 | 359 | 241 | 235 | 257 | 44 |
| Lane Group Flow (vph) | 55 | 359 | 241 | 235 | 257 | 44 |
| Turn Type | Prot | NA | NA | Perm | Perm | Perm |
| Protected Phases | 5 | 2 | 6 |  |  |  |
| Permitted Phases |  |  |  | 6 | 4 | 4 |
| Detector Phase | 5 | 2 | 6 | 6 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 16.2 | 52.2 | 52.2 | 52.2 | 30.0 | 30.0 |
| Total Split (s) | 26.2 | 83.4 | 57.2 | 57.2 | 36.0 | 36.0 |
| Total Split (\%) | 21.9\% | 69.8\% | 47.9\% | 47.9\% | 30.2\% | 30.2\% |
| Yellow Time (s) | 4.6 | 4.6 | 4.6 | 4.6 | 3.3 | 3.3 |
| All-Red Time (s) | 1.6 | 1.6 | 1.6 | 1.6 | 2.7 | 2.7 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.2 | 6.2 | 6.2 | 6.2 | 6.0 | 6.0 |
| Lead/Lag | Lead |  | Lag | Lag |  |  |
| Lead-Lag Optimize? | Yes |  | Yes | Yes |  |  |
| Recall Mode | Max | Min | Min | Min | Max | Max |
| Act Effct Green (s) | 20.0 | 43.3 | 17.0 | 17.0 | 30.1 | 30.1 |
| Actuated g/C Ratio | 0.23 | 0.51 | 0.20 | 0.20 | 0.35 | 0.35 |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.17 | 0.40 | 0.69 | 0.50 | 0.44 | 0.08 |
| Control Delay | 29.6 | 14.4 | 42.1 | 7.9 | 25.3 | 7.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 29.6 | 14.4 | 42.1 | 7.9 | 25.3 | 7.3 |
| LOS | C | B | D | A | C | A |
| Approach Delay |  | 16.5 | 25.2 |  | 22.7 |  |
| Approach LOS |  | B | C |  | C |  |
| Queue Length 50th (m) | 7.2 | 34.4 | 36.8 | 0.0 | 31.4 | 0.0 |
| Queue Length 95th (m) | 18.1 | 52.9 | 59.6 | 17.0 | 58.7 | 7.1 |
| Internal Link Dist (m) |  | 217.9 | 258.1 |  | 237.6 |  |
| Turn Bay Length (m) | 100.0 |  |  | 100.0 | 80.0 |  |
| Base Capacity (vph) | 323 | 1612 | 1055 | 949 | 583 | 541 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.17 | 0.22 | 0.23 | 0.25 | 0.44 | 0.08 |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 119.4 |  |  |  |  |  |  |
| Actuated Cycle Length: 85.6 |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.69 |  |  |  |  |  |  |
| Intersection Signal Delay: 21.5 |  |  |  | Intersection LOS: C |  |  |
| Intersection Capacity Utilization 47.9\% |  |  |  | ICU Level of Service A |  |  |

Analysis Period (min) 15

Total Future Background 2028 AM
3: Fernbank Road \& Robert Grant Avenue
Splits and Phases: 3: Fernbank Road \& Robert Grant Avenue


|  |  | $\leftarrow$ |  |
| :--- | ---: | ---: | ---: |
|  | $\rightarrow$ |  |  |
| Lane Group | EBT | WBT | SBL |
| Lane Configurations | $\uparrow$ | $\uparrow$ | $\mathbf{Y}$ |
| Traffic Volume (vph) | 35 | 64 | 2 |
| Future Volume evph | 35 | 64 | 2 |
| Lane Group Flow (vph) | 50 | 64 | 50 |
| Sign Control | Free | Free | Stop |

## Intersection Summary

Control Type: Unsignalized
Intersection Capacity Utilization 19.5\%
ICU Level of Service A
Analysis Period (min) 15

Total Future Background 2028 AM
8: Bobolink Ridge \& Livery Street

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3.4 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | F |  |  |  |
| Traffic Vol, veh/h | 15 | 35 | 64 | 0 | 2 | 48 |
| Future Vol, veh/h | 15 | 35 | 64 | 0 | 2 | 48 |
| Conflicting Peds, \#/hr | 8 | 0 | 0 | 8 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, $\#$ | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, $\%$ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 15 | 35 | 64 | 0 | 2 | 48 |


| Major/Minor M | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 72 | 0 | - | 0 | 137 | 72 |
| Stage 1 | - | - | - | - | 72 | - |
| Stage 2 | - | - | - | - | 65 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1528 | - | - | - | 856 | 990 |
| Stage 1 | - | - | - | - | 951 | - |
| Stage 2 | - | - | - | - | 958 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1518 | - | - | - | 835 | 983 |
| Mov Cap-2 Maneuver | - | - | - | - | 835 | - |
| Stage 1 | - | - | - | - | 935 | - |
| Stage 2 | - | - | - | - | 951 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 2.2 |  | 0 |  | 8.9 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT WBR SBLn1 |  |  |
| Capacity (veh/h) |  | 1518 | - |  | - | 976 |
| HCM Lane V/C Ratio |  | 0.01 | - | - | - | 0.051 |
| HCM Control Delay (s) |  | 7.4 | 0 | - | - | 8.9 |
| HCM Lane LOS |  | A | A | - | - | A |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | - | 0.2 |

Total Future Background 2028 PM
3: Fernbank Road \& Robert Grant Avenue

|  | $\rangle$ |  | - | 4 |  | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | \% | $\uparrow$ | 4 | 「 | \% | 「 |
| Traffic Volume (vph) | 41 | 304 | 532 | 269 | 254 | 44 |
| Future Volume (vph) | 41 | 304 | 532 | 269 | 254 | 44 |
| Lane Group Flow (vph) | 41 | 304 | 532 | 269 | 254 | 44 |
| Turn Type | Prot | NA | NA | Perm | Perm | Perm |
| Protected Phases | 5 | 2 | 6 |  |  |  |
| Permitted Phases |  |  |  | 6 | 4 | 4 |
| Detector Phase | 5 | 2 | 6 | 6 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 16.2 | 52.2 | 52.2 | 52.2 | 30.0 | 30.0 |
| Total Split (s) | 26.2 | 94.4 | 68.2 | 68.2 | 36.0 | 36.0 |
| Total Split (\%) | 20.1\% | 72.4\% | 52.3\% | 52.3\% | 27.6\% | 27.6\% |
| Yellow Time (s) | 4.6 | 4.6 | 4.6 | 4.6 | 3.3 | 3.3 |
| All-Red Time (s) | 1.6 | 1.6 | 1.6 | 1.6 | 2.7 | 2.7 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.2 | 6.2 | 6.2 | 6.2 | 6.0 | 6.0 |
| Lead/Lag | Lead |  | Lag | Lag |  |  |
| Lead-Lag Optimize? | Yes |  | Yes | Yes |  |  |
| Recall Mode | Max | Min | Min | Min | Max | Max |
| Act Effct Green (s) | 20.2 | 63.8 | 37.3 | 37.3 | 30.2 | 30.2 |
| Actuated g/C Ratio | 0.19 | 0.60 | 0.35 | 0.35 | 0.28 | 0.28 |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.12 | 0.29 | 0.85 | 0.39 | 0.55 | 0.10 |
| Control Delay | 40.7 | 10.8 | 45.0 | 4.3 | 40.0 | 10.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 40.7 | 10.8 | 45.0 | 4.3 | 40.0 | 10.6 |
| LOS | D | B | D | A | D | B |
| Approach Delay |  | 14.3 | 31.3 |  | 35.6 |  |
| Approach LOS |  | B | C |  | D |  |
| Queue Length 50th (m) | 7.1 | 28.1 | 99.9 | 0.0 | 44.5 | 0.0 |
| Queue Length 95th (m) | 18.7 | 41.5 | 139.8 | 14.9 | 82.5 | 9.2 |
| Internal Link Dist (m) |  | 217.9 | 258.1 |  | 237.6 |  |
| Turn Bay Length (m) | 100.0 |  |  | 100.0 | 80.0 |  |
| Base Capacity (vph) | 328 | 1463 | 1048 | 977 | 459 | 424 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.13 | 0.21 | 0.51 | 0.28 | 0.55 | 0.10 |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 130.4 |  |  |  |  |  |  |
| Actuated Cycle Length: 106.3 |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.85 |  |  |  |  |  |  |
| Intersection Signal Delay: 28.2 |  |  |  | Intersection LOS: C |  |  |
| Intersection Capacity Utilization 61.0\% |  |  |  | ICU Level of Service B |  |  |

Analysis Period (min) 15

Total Future Background 2028 PM
3: Fernbank Road \& Robert Grant Avenue
Splits and Phases: 3: Fernbank Road \& Robert Grant Avenue


|  |  | $\leftarrow$ |  |
| :--- | ---: | ---: | ---: |
|  | $\rightarrow$ |  |  |
| Lane Group | EBT | WBT | SBL |
| Lane Configurations | $\uparrow$ | $\ominus$ |  |
| Traffic Volume (vph) | 75 | 34 | 1 |
| Future Volume (vph) | 75 | 34 | 1 |
| Lane Group Flow (vph) | 124 | 37 | 31 |
| Sign Control | Free | Free | Stop |

Intersection Summary
Control Type: Unsignalized
Intersection Capacity Utilization 23.7\%
ICU Level of Service A
Analysis Period (min) 15

Total Future Background 2028 PM
8: Bobolink Ridge \& Livery Street


| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 48 | 0 | - | 0 | 220 | 47 |
| Stage 1 | - | - | - | - | 47 | - |
| Stage 2 | - | - | - | - | 173 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1559 | - | - | - | 768 | 1022 |
| Stage 1 | - | - | - | - | 975 | - |
| Stage 2 | - | - | - | - | 857 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1544 | - | - | - | 730 | 1012 |
| Mov Cap-2 Maneuver | - | - | - | - | 730 | - |
| Stage 1 | - | - | - | - | 934 | - |
| Stage 2 | - | - | - | - | 849 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 2.9 |  | 0 |  | 8.7 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT WBR SBLn1 |  |  |
| Capacity (veh/h) |  | 1544 | - | - | - | 1000 |
| HCM Lane V/C Ratio |  | 0.032 | - | - | - | 0.031 |
| HCM Control Delay (s) |  | 7.4 | 0 | - | - | 8.7 |
| HCM Lane LOS |  | A | A | - | - | A |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | - | 0.1 |

## MOVEMENT SUMMARY

## Site: [BG2028 - Abbott/Robert Grant]

AM Peak
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Demand Total veh/h | ows HV $\%$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 278 | 2.0 | 0.322 | 9.0 | LOS A | 2.1 | 15.3 | 0.22 | 0.56 | 0.22 | 54.0 |
| 3 | R2 | 197 | 2.0 | 0.322 | 4.2 | LOS A | 2.1 | 15.3 | 0.22 | 0.56 | 0.22 | 52.8 |
| Appr |  | 475 | 2.0 | 0.322 | 7.0 | LOS A | 2.1 | 15.3 | 0.22 | 0.56 | 0.22 | 53.5 |
| East: Abbott Street East |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 122 | 2.0 | 0.181 | 8.8 | LOS A | 1.0 | 7.1 | 0.46 | 0.60 | 0.46 | 46.6 |
| 5 | T1 | 78 | 2.0 | 0.181 | 4.3 | LOS A | 1.0 | 7.1 | 0.46 | 0.60 | 0.46 | 46.4 |
| Appr |  | 200 | 2.0 | 0.181 | 7.0 | LOS A | 1.0 | 7.1 | 0.46 | 0.60 | 0.46 | 46.5 |
| West: Abbott Street E |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | T1 | 52 | 2.0 | 0.176 | 3.4 | LOS A | 1.0 | 7.3 | 0.32 | 0.43 | 0.32 | 48.4 |
| 12 | R2 | 171 | 2.0 | 0.176 | 3.5 | LOS A | 1.0 | 7.3 | 0.32 | 0.43 | 0.32 | 47.2 |
| Approach |  | 223 | 2.0 | 0.176 | 3.4 | LOS A | 1.0 | 7.3 | 0.32 | 0.43 | 0.32 | 47.5 |
| All Vehicles |  | 898 | 2.0 | 0.322 | 6.1 | LOS A | 2.1 | 15.3 | 0.30 | 0.54 | 0.30 | 50.2 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## Site: [BG2028 - Abbott/Robert Grant]

PM Peak
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman <br> Total veh/h | lows HV \% | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 211 | 2.0 | 0.253 | 9.1 | LOS A | 1.6 | 11.5 | 0.26 | 0.57 | 0.26 | 53.8 |
| 3 | R2 | 139 | 2.0 | 0.253 | 4.3 | LOS A | 1.6 | 11.5 | 0.26 | 0.57 | 0.26 | 52.6 |
| Appr |  | 350 | 2.0 | 0.253 | 7.2 | LOS A | 1.6 | 11.5 | 0.26 | 0.57 | 0.26 | 53.3 |
| East: Abbott Street East |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 189 | 2.0 | 0.243 | 8.5 | LOS A | 1.4 | 10.1 | 0.43 | 0.59 | 0.43 | 46.6 |
| 5 | T1 | 94 | 2.0 | 0.243 | 4.0 | LOS A | 1.4 | 10.1 | 0.43 | 0.59 | 0.43 | 46.4 |
| Appr |  | 283 | 2.0 | 0.243 | 7.0 | LOS A | 1.4 | 10.1 | 0.43 | 0.59 | 0.43 | 46.5 |
| West: Abbott Street E |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | T1 | 76 | 2.0 | 0.300 | 3.9 | LOS A | 1.9 | 13.8 | 0.44 | 0.49 | 0.44 | 48.0 |
| 12 | R2 | 284 | 2.0 | 0.300 | 3.9 | LOS A | 1.9 | 13.8 | 0.44 | 0.49 | 0.44 | 46.9 |
| Approach |  | 360 | 2.0 | 0.300 | 3.9 | LOS A | 1.9 | 13.8 | 0.44 | 0.49 | 0.44 | 47.1 |
| All Vehicles |  | 993 | 2.0 | 0.300 | 6.0 | LOS A | 1.9 | 13.8 | 0.37 | 0.55 | 0.37 | 48.9 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## Site: [BG2028 - Bobolink/Robert Grant]

AM Peak
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | Turn | Deman Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | $\begin{aligned} & \text { Deg. } \\ & \text { Satn } \\ & \text { v/c } \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 8 | 2.0 | 0.248 | 9.3 | LOS A | 1.5 | 10.7 | 0.31 | 0.45 | 0.31 | 55.2 |
| 2 | T1 | 306 | 2.0 | 0.248 | 4.7 | LOS A | 1.5 | 10.7 | 0.31 | 0.45 | 0.31 | 55.3 |
| 3 | R2 | 12 | 2.0 | 0.248 | 4.5 | LOS A | 1.5 | 10.7 | 0.31 | 0.45 | 0.31 | 53.9 |
| Appr |  | 326 | 2.0 | 0.248 | 4.8 | LOS A | 1.5 | 10.7 | 0.31 | 0.45 | 0.31 | 55.2 |
| East: Bobolink Drive |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 22 | 2.0 | 0.096 | 10.7 | LOS B | 0.5 | 3.6 | 0.52 | 0.62 | 0.52 | 54.3 |
| 5 | T1 | 1 | 2.0 | 0.096 | 6.1 | LOS A | 0.5 | 3.6 | 0.52 | 0.62 | 0.52 | 54.3 |
| 6 | R2 | 73 | 2.0 | 0.096 | 5.9 | LOS A | 0.5 | 3.6 | 0.52 | 0.62 | 0.52 | 53.0 |
| Appr |  | 96 | 2.0 | 0.096 | 7.0 | LOS A | 0.5 | 3.6 | 0.52 | 0.62 | 0.52 | 53.3 |
| North: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 28 | 2.0 | 0.196 | 8.9 | LOS A | 1.2 | 8.4 | 0.15 | 0.43 | 0.15 | 55.8 |
| 8 | T1 | 223 | 2.0 | 0.196 | 4.3 | LOS A | 1.2 | 8.4 | 0.15 | 0.43 | 0.15 | 55.9 |
| 9 | R2 | 43 | 2.0 | 0.196 | 4.0 | LOS A | 1.2 | 8.4 | 0.15 | 0.43 | 0.15 | 54.5 |
| Approach |  | 294 | 2.0 | 0.196 | 4.7 | LOS A | 1.2 | 8.4 | 0.15 | 0.43 | 0.15 | 55.7 |
| West: Bobolink Drive |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 82 | 2.0 | 0.088 | 10.0 | LOS B | 0.4 | 3.2 | 0.42 | 0.64 | 0.42 | 52.4 |
| 11 | T1 | 1 | 2.0 | 0.088 | 5.4 | LOS A | 0.4 | 3.2 | 0.42 | 0.64 | 0.42 | 52.5 |
| 12 | R2 | 15 | 2.0 | 0.088 | 5.2 | LOS A | 0.4 | 3.2 | 0.42 | 0.64 | 0.42 | 51.3 |
| Appr |  | 98 | 2.0 | 0.088 | 9.3 | LOS A | 0.4 | 3.2 | 0.42 | 0.64 | 0.42 | 52.3 |
| All Ve | icles | 814 | 2.0 | 0.248 | 5.5 | LOS A | 1.5 | 10.7 | 0.29 | 0.48 | 0.29 | 54.8 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## Site: [BG2028 - Bobolink/Robert Grant]

PM Peak
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | Turn | Deman <br> Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 15 | 2.0 | 0.230 | 9.4 | LOS A | 1.3 | 9.5 | 0.33 | 0.47 | 0.33 | 55.1 |
| 2 | T1 | 244 | 2.0 | 0.230 | 4.8 | LOS A | 1.3 | 9.5 | 0.33 | 0.47 | 0.33 | 55.2 |
| 3 | R2 | 35 | 2.0 | 0.230 | 4.6 | LOS A | 1.3 | 9.5 | 0.33 | 0.47 | 0.33 | 53.8 |
| Appr | ch | 294 | 2.0 | 0.230 | 5.0 | LOS A | 1.3 | 9.5 | 0.33 | 0.47 | 0.33 | 55.0 |
| East: Bobolink Drive |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 18 | 2.0 | 0.051 | 10.2 | LOS B | 0.3 | 1.8 | 0.45 | 0.59 | 0.45 | 54.1 |
| 5 | T1 | 1 | 2.0 | 0.051 | 5.6 | LOS A | 0.3 | 1.8 | 0.45 | 0.59 | 0.45 | 54.2 |
| 6 | R2 | 35 | 2.0 | 0.051 | 5.4 | LOS A | 0.3 | 1.8 | 0.45 | 0.59 | 0.45 | 52.9 |
| Appr |  | 54 | 2.0 | 0.051 | 7.0 | LOS A | 0.3 | 1.8 | 0.45 | 0.59 | 0.45 | 53.4 |
| North: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 72 | 2.0 | 0.304 | 8.9 | LOS A | 2.0 | 14.0 | 0.17 | 0.45 | 0.17 | 55.5 |
| 8 | T1 | 310 | 2.0 | 0.304 | 4.3 | LOS A | 2.0 | 14.0 | 0.17 | 0.45 | 0.17 | 55.6 |
| 9 | R2 | 82 | 2.0 | 0.304 | 4.1 | LOS A | 2.0 | 14.0 | 0.17 | 0.45 | 0.17 | 54.2 |
| Approach |  | 464 | 2.0 | 0.304 | 5.0 | LOS A | 2.0 | 14.0 | 0.17 | 0.45 | 0.17 | 55.3 |
| West: Bobolink Drive |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 59 | 2.0 | 0.075 | 10.7 | LOS B | 0.4 | 2.8 | 0.50 | 0.66 | 0.50 | 52.4 |
| 11 | T1 | 1 | 2.0 | 0.075 | 6.1 | LOS A | 0.4 | 2.8 | 0.50 | 0.66 | 0.50 | 52.5 |
| 12 | R2 | 16 | 2.0 | 0.075 | 5.8 | LOS A | 0.4 | 2.8 | 0.50 | 0.66 | 0.50 | 51.3 |
| Appr |  | 76 | 2.0 | 0.075 | 9.6 | LOS A | 0.4 | 2.8 | 0.50 | 0.66 | 0.50 | 52.2 |
| All V | cles | 888 | 2.0 | 0.304 | 5.5 | LOS A | 2.0 | 14.0 | 0.27 | 0.48 | 0.27 | 54.8 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## Total Projected 2023

Total Projected 2023 AM
3: Fernbank Road \& Robert Grant Avenue

|  | $\rangle$ |  | $\leftarrow$ | 4 |  | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | \% | $\uparrow$ | 4 | 「 | \% | 「 |
| Traffic Volume (vph) | 43 | 322 | 211 | 206 | 221 | 37 |
| Future Volume (vph) | 43 | 322 | 211 | 206 | 221 | 37 |
| Lane Group Flow (vph) | 43 | 322 | 211 | 206 | 221 | 37 |
| Turn Type | Prot | NA | NA | Perm | Perm | Perm |
| Protected Phases | 5 | 2 | 6 |  |  |  |
| Permitted Phases |  |  |  | 6 | 4 | 4 |
| Detector Phase | 5 | 2 | 6 | 6 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 16.2 | 52.2 | 52.2 | 52.2 | 30.0 | 30.0 |
| Total Split (s) | 26.2 | 83.4 | 57.2 | 57.2 | 36.0 | 36.0 |
| Total Split (\%) | 21.9\% | 69.8\% | 47.9\% | 47.9\% | 30.2\% | 30.2\% |
| Yellow Time (s) | 4.6 | 4.6 | 4.6 | 4.6 | 3.3 | 3.3 |
| All-Red Time (s) | 1.6 | 1.6 | 1.6 | 1.6 | 2.7 | 2.7 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.2 | 6.2 | 6.2 | 6.2 | 6.0 | 6.0 |
| Lead/Lag | Lead |  | Lag | Lag |  |  |
| Lead-Lag Optimize? | Yes |  | Yes | Yes |  |  |
| Recall Mode | Max | Min | Min | Min | Max | Max |
| Act Effct Green (s) | 20.0 | 41.5 | 15.3 | 15.3 | 30.1 | 30.1 |
| Actuated g/C Ratio | 0.24 | 0.50 | 0.18 | 0.18 | 0.36 | 0.36 |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.13 | 0.36 | 0.66 | 0.48 | 0.37 | 0.07 |
| Control Delay | 27.9 | 14.2 | 41.9 | 8.4 | 23.1 | 7.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 27.9 | 14.2 | 41.9 | 8.4 | 23.1 | 7.4 |
| LOS | C | B | D | A | C | A |
| Approach Delay |  | 15.8 | 25.4 |  | 20.8 |  |
| Approach LOS |  | B | C |  | C |  |
| Queue Length 50th (m) | 5.4 | 30.0 | 31.6 | 0.0 | 25.6 | 0.0 |
| Queue Length 95th (m) | 14.6 | 47.1 | 52.7 | 16.3 | 48.5 | 6.3 |
| Internal Link Dist (m) |  | 217.9 | 258.1 |  | 237.6 |  |
| Turn Bay Length (m) | 100.0 |  |  | 100.0 | 80.0 |  |
| Base Capacity (vph) | 330 | 1646 | 1077 | 953 | 596 | 546 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.13 | 0.20 | 0.20 | 0.22 | 0.37 | 0.07 |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 119.4 |  |  |  |  |  |  |
| Actuated Cycle Length: 83.8 |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.66 |  |  |  |  |  |  |
| Intersection Signal Delay: 20.9 |  |  |  | Intersection LOS: C |  |  |
| Intersection Capacity Utilization 44.1\% |  |  |  | ICU Level of Service A |  |  |

Analysis Period (min) 15

Total Projected 2023 AM
3: Fernbank Road \& Robert Grant Avenue
Splits and Phases: 3: Fernbank Road \& Robert Grant Avenue



## Intersection Summary

Control Type: Unsignalized
Intersection Capacity Utilization 23.9\%
ICU Level of Service A
Analysis Period (min) 15

Total Projected 2023 AM
8: Bobolink Ridge \& Livery Street

| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 5 |  |  |  |  |  |
| Movement E | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | $\uparrow$ |  | * |  |
| Traffic Vol, veh/h | 31 | 35 | 64 | 0 | 2 | 102 |
| Future Vol, veh/h | 31 | 35 | 64 | 0 | 2 | 102 |
| Conflicting Peds, \#/hr | 8 | 0 | 0 | 8 | 0 | 0 |
| Sign Control F | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | \# | 0 | 0 | - | 0 | - |
| Grade, \% |  | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 31 | 35 | 64 | 0 | 2 | 102 |


| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 72 | 0 | - | 0 | 169 | 72 |
| Stage 1 | - | - | - - | - | 72 | - |
| Stage 2 | - | - | - - | - | 97 | - |
| Critical Hdwy | 4.12 | - | - - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1528 | - | - - | - | 821 | 990 |
| Stage 1 | - | - | - - | - | 951 | - |
| Stage 2 | - | - | - - | - | 927 | - |
| Platoon blocked, \% |  | - | - - | - |  |  |
| Mov Cap-1 Maneuver | 1518 | - | - - | - | 792 | 983 |
| Mov Cap-2 Maneuver | - | - | - - | - | 792 | - |
| Stage 1 | - | - | - - | - | 924 | - |
| Stage 2 | - | - | - - | - | 921 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 3.5 |  | 0 |  | 9.1 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT WBR SBLn1 |  |  |
| Capacity (veh/h) |  | 1518 | - | - | - | 978 |
| HCM Lane V/C Ratio |  | 0.02 | 2 | - | - | 0.106 |
| HCM Control Delay (s) |  | 7.4 | 0 | - | - | 9.1 |
| HCM Lane LOS |  | A | A | - | - | A |
| HCM 95th \%tile Q(veh) |  | 0.1 | , | - | - | 0.4 |

Total Projected 2023 PM
3: Fernbank Road \& Robert Grant Avenue

|  | $\rangle$ |  | $\leftarrow$ | 4 |  | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | \% | $\uparrow$ | $\uparrow$ | 「 | \% | 「 |
| Traffic Volume (vph) | 30 | 269 | 476 | 274 | 216 | 36 |
| Future Volume (vph) | 30 | 269 | 476 | 274 | 216 | 36 |
| Lane Group Flow (vph) | 30 | 269 | 476 | 274 | 216 | 36 |
| Turn Type | Prot | NA | NA | Perm | Perm | Perm |
| Protected Phases | 5 | 2 | 6 |  |  |  |
| Permitted Phases |  |  |  | 6 | 4 | 4 |
| Detector Phase | 5 | 2 | 6 | 6 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 16.2 | 52.2 | 52.2 | 52.2 | 30.0 | 30.0 |
| Total Split (s) | 26.2 | 94.4 | 68.2 | 68.2 | 36.0 | 36.0 |
| Total Split (\%) | 20.1\% | 72.4\% | 52.3\% | 52.3\% | 27.6\% | 27.6\% |
| Yellow Time (s) | 4.6 | 4.6 | 4.6 | 4.6 | 3.3 | 3.3 |
| All-Red Time (s) | 1.6 | 1.6 | 1.6 | 1.6 | 2.7 | 2.7 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.2 | 6.2 | 6.2 | 6.2 | 6.0 | 6.0 |
| Lead/Lag | Lead |  | Lag | Lag |  |  |
| Lead-Lag Optimize? | Yes |  | Yes | Yes |  |  |
| Recall Mode | Max | Min | Min | Min | Max | Max |
| Act Effct Green (s) | 20.1 | 59.1 | 32.7 | 32.7 | 30.2 | 30.2 |
| Actuated g/C Ratio | 0.20 | 0.58 | 0.32 | 0.32 | 0.30 | 0.30 |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.09 | 0.26 | 0.83 | 0.42 | 0.45 | 0.08 |
| Control Delay | 37.6 | 10.9 | 44.5 | 4.8 | 34.6 | 10.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 37.6 | 10.9 | 44.5 | 4.8 | 34.6 | 10.6 |
| LOS | D | B | D | A | C | B |
| Approach Delay |  | 13.6 | 30.0 |  | 31.2 |  |
| Approach LOS |  | B | C |  | C |  |
| Queue Length 50th (m) | 4.8 | 24.3 | 85.5 | 0.0 | 34.1 | 0.0 |
| Queue Length 95th (m) | 14.1 | 36.9 | 121.8 | 15.5 | 65.4 | 7.9 |
| Internal Link Dist (m) |  | 217.9 | 258.1 |  | 237.6 |  |
| Turn Bay Length (m) | 100.0 |  |  | 100.0 | 80.0 |  |
| Base Capacity (vph) | 342 | 1529 | 1095 | 1010 | 480 | 435 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.09 | 0.18 | 0.43 | 0.27 | 0.45 | 0.08 |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 130.4 |  |  |  |  |  |  |
| Actuated Cycle Length: 101.6 |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.83 |  |  |  |  |  |  |
| Intersection Signal Delay: 26.4 |  |  |  | Intersection LOS: C |  |  |
| Intersection Capacity Utilization 49.2\% |  |  |  | ICU Level of Service A |  |  |

Analysis Period (min) 15

Splits and Phases: 3: Fernbank Road \& Robert Grant Avenue


|  |  | $\leftarrow$ |  |
| :--- | ---: | ---: | ---: |
|  | $\rightarrow$ |  |  |
| Lane Group | EBT | WBT | SBL |
| Lane Configurations | $\uparrow$ | $\ominus$ |  |
| Traffic Volume (vph) | 75 | 34 | 1 |
| Future Volume (vph) | 75 | 34 | 1 |
| Lane Group Flow (vph) | 178 | 37 | 65 |
| Sign Control | Free | Free | Stop |

## Intersection Summary

Control Type: Unsignalized
Intersection Capacity Utilization 27.8\%
ICU Level of Service A
Analysis Period (min) 15

Total Projected 2023 PM
8: Bobolink Ridge \& Livery Street

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 4.8 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | F |  |  |  |
| Traffic Vol, veh/h | 103 | 75 | 34 | 3 | 1 | 64 |
| Future Vol, veh/h | 103 | 75 | 34 | 3 | 1 | 64 |
| Conflicting Peds, \#/hr | 11 | 0 | 0 | 11 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - None | - | None |  |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, $\%$ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 103 | 75 | 34 | 3 | 1 | 64 |


| Major/Minor $\quad$ N | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 48 | 0 | - | 0 | 328 | 47 |
| Stage 1 | - | - | - | - | 47 | - |
| Stage 2 | - | - | - | - | 281 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1559 | - | - | - | 666 | 1022 |
| Stage 1 | - | - | - | - | 975 | - |
| Stage 2 | - | - | - | - | 767 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1544 | - | - | - | 608 | 1012 |
| Mov Cap-2 Maneuver | - | - | - | - | 608 | - |
| Stage 1 | - | - | - | - | 899 | - |
| Stage 2 | - | - | - | - | 760 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 4.3 |  | 0 |  | 8.8 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT WBR SBLn1 |  |  |
| Capacity (veh/h) |  | 1544 | - | - | - | 1002 |
| HCM Lane V/C Ratio |  | 0.067 | - | - | - | 0.065 |
| HCM Control Delay (s) |  | 7.5 | 0 | - | - | 8.8 |
| HCM Lane LOS |  | A | A | - | - | A |
| HCM 95th \%tile Q(veh) |  | 0.2 | - | - | - | 0.2 |

## MOVEMENT SUMMARY

## Site: [FT2023 - Abbott/Robert Grant]

AM Peak
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 250 | 2.0 | 0.255 | 8.8 | LOS A | 1.5 | 10.9 | 0.12 | 0.57 | 0.12 | 54.1 |
| 3 | R2 | 148 | 2.0 | 0.255 | 4.0 | LOS A | 1.5 | 10.9 | 0.12 | 0.57 | 0.12 | 52.9 |
| Appr |  | 398 | 2.0 | 0.255 | 7.0 | LOS A | 1.5 | 10.9 | 0.12 | 0.57 | 0.12 | 53.7 |
| East: Abbott Street East |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 63 | 2.0 | 0.107 | 8.5 | LOS A | 0.5 | 3.9 | 0.40 | 0.56 | 0.40 | 46.9 |
| 5 | T1 | 58 | 2.0 | 0.107 | 4.0 | LOS A | 0.5 | 3.9 | 0.40 | 0.56 | 0.40 | 46.8 |
| Appr |  | 121 | 2.0 | 0.107 | 6.4 | LOS A | 0.5 | 3.9 | 0.40 | 0.56 | 0.40 | 46.9 |
| West: Abbott Street E |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | T1 | 23 | 2.0 | 0.125 | 3.1 | LOS A | 0.7 | 4.9 | 0.21 | 0.39 | 0.21 | 48.7 |
| 12 | R2 | 148 | 2.0 | 0.125 | 3.1 | LOS A | 0.7 | 4.9 | 0.21 | 0.39 | 0.21 | 47.6 |
| Appr |  | 171 | 2.0 | 0.125 | 3.1 | LOS A | 0.7 | 4.9 | 0.21 | 0.39 | 0.21 | 47.7 |
| All V | icles | 690 | 2.0 | 0.255 | 5.9 | LOS A | 1.5 | 10.9 | 0.19 | 0.52 | 0.19 | 50.8 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: C:IHome Workl476799 - LepineFernbankl1000IDATAISIDRA\AM Peak.sip8

## MOVEMENT SUMMARY

## Site: [FT2023 - Abbott/Robert Grant]

PM Peak
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \\ & \hline \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 188 | 2.0 | 0.198 | 9.0 | LOS A | 1.2 | 8.2 | 0.19 | 0.57 | 0.19 | 53.8 |
| 3 | R2 | 96 | 2.0 | 0.198 | 4.1 | LOS A | 1.2 | 8.2 | 0.19 | 0.57 | 0.19 | 52.6 |
| Appr |  | 284 | 2.0 | 0.198 | 7.3 | LOS A | 1.2 | 8.2 | 0.19 | 0.57 | 0.19 | 53.4 |
| East: Abbott Street East |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 119 | 2.0 | 0.153 | 8.3 | LOS A | 0.8 | 5.8 | 0.37 | 0.57 | 0.37 | 46.7 |
| 5 | T1 | 62 | 2.0 | 0.153 | 3.7 | LOS A | 0.8 | 5.8 | 0.37 | 0.57 | 0.37 | 46.6 |
| Approach |  | 181 | 2.0 | 0.153 | 6.7 | LOS A | 0.8 | 5.8 | 0.37 | 0.57 | 0.37 | 46.7 |
| West: Abbott Street E |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | T1 | 52 | 2.0 | 0.238 | 3.4 | LOS A | 1.4 | 10.3 | 0.33 | 0.43 | 0.33 | 48.4 |
| 12 | R2 | 257 | 2.0 | 0.238 | 3.5 | LOS A | 1.4 | 10.3 | 0.33 | 0.43 | 0.33 | 47.2 |
| Appr |  | 309 | 2.0 | 0.238 | 3.5 | LOS A | 1.4 | 10.3 | 0.33 | 0.43 | 0.33 | 47.4 |
| All V | icles | 774 | 2.0 | 0.238 | 5.6 | LOS A | 1.4 | 10.3 | 0.29 | 0.51 | 0.29 | 49.3 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: C:IHome Workl476799 - LepineFernbank\1000IDATAISIDRAIPM Peak.sip8

## MOVEMENT SUMMARY

## Site: [FT2023 - Bobolink/Robert Grant]

AM Peak
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | Turn | Deman <br> Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 1 | 2.0 | 0.175 | 9.0 | LOS A | 1.0 | 6.8 | 0.19 | 0.41 | 0.19 | 55.9 |
| 2 | T1 | 221 | 2.0 | 0.175 | 4.4 | LOS A | 1.0 | 6.8 | 0.19 | 0.41 | 0.19 | 56.0 |
| 3 | R2 | 26 | 2.0 | 0.175 | 4.1 | LOS A | 1.0 | 6.8 | 0.19 | 0.41 | 0.19 | 54.6 |
| Appr |  | 248 | 2.0 | 0.175 | 4.4 | LOS A | 1.0 | 6.8 | 0.19 | 0.41 | 0.19 | 55.8 |
| East: Bobolink Drive |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 68 | 2.0 | 0.130 | 9.9 | LOS A | 0.7 | 4.9 | 0.39 | 0.60 | 0.39 | 53.9 |
| 5 | T1 | 1 | 2.0 | 0.130 | 5.2 | LOS A | 0.7 | 4.9 | 0.39 | 0.60 | 0.39 | 54.0 |
| 6 | R2 | 81 | 2.0 | 0.130 | 5.0 | LOS A | 0.7 | 4.9 | 0.39 | 0.60 | 0.39 | 52.7 |
| Appr |  | 150 | 2.0 | 0.130 | 7.2 | LOS A | 0.7 | 4.9 | 0.39 | 0.60 | 0.39 | 53.3 |
| North: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 52 | 2.0 | 0.154 | 9.1 | LOS A | 0.9 | 6.2 | 0.23 | 0.47 | 0.23 | 54.9 |
| 8 | T1 | 158 | 2.0 | 0.154 | 4.4 | LOS A | 0.9 | 6.2 | 0.23 | 0.47 | 0.23 | 55.0 |
| 9 | R2 | 1 | 2.0 | 0.154 | 4.2 | LOS A | 0.9 | 6.2 | 0.23 | 0.47 | 0.23 | 53.7 |
| Approach |  | 211 | 2.0 | 0.154 | 5.6 | LOS A | 0.9 | 6.2 | 0.23 | 0.47 | 0.23 | 54.9 |
| West: Bobolink Drive |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 1 | 2.0 | 0.003 | 9.9 | LOS A | 0.0 | 0.1 | 0.40 | 0.50 | 0.40 | 54.1 |
| 11 | T1 | 1 | 2.0 | 0.003 | 5.3 | LOS A | 0.0 | 0.1 | 0.40 | 0.50 | 0.40 | 54.2 |
| 12 | R2 | 1 | 2.0 | 0.003 | 5.0 | LOS A | 0.0 | 0.1 | 0.40 | 0.50 | 0.40 | 52.9 |
| Appr |  | 3 | 2.0 | 0.003 | 6.7 | LOS A | 0.0 | 0.1 | 0.40 | 0.50 | 0.40 | 53.7 |
| All V | cles | 612 | 2.0 | 0.175 | 5.5 | LOS A | 1.0 | 6.8 | 0.25 | 0.48 | 0.25 | 54.9 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: C:\Home Workl476799 - LepineFernbankl1000IDATAISIDRA\AM Peak.sip8

## MOVEMENT SUMMARY

## Site: [FT2023 - Bobolink/Robert Grant]

PM Peak
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | Deman Total veh/h | lows HV $\%$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 1 | 2.0 | 0.228 | 9.6 | LOS A | 1.3 | 9.2 | 0.35 | 0.48 | 0.35 | 55.2 |
| 2 T1 | 201 | 2.0 | 0.228 | 4.9 | LOS A | 1.3 | 9.2 | 0.35 | 0.48 | 0.35 | 55.3 |
| 3 R2 | 82 | 2.0 | 0.228 | 4.7 | LOS A | 1.3 | 9.2 | 0.35 | 0.48 | 0.35 | 54.0 |
| Approach | 284 | 2.0 | 0.228 | 4.9 | LOS A | 1.3 | 9.2 | 0.35 | 0.48 | 0.35 | 54.9 |
| East: Bobolink Drive |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 47 | 2.0 | 0.076 | 9.7 | LOS A | 0.4 | 2.8 | 0.37 | 0.59 | 0.37 | 53.7 |
| $5 \quad$ T1 | 1 | 2.0 | 0.076 | 5.1 | LOS A | 0.4 | 2.8 | 0.37 | 0.59 | 0.37 | 53.7 |
| 6 R2 | 40 | 2.0 | 0.076 | 4.8 | LOS A | 0.4 | 2.8 | 0.37 | 0.59 | 0.37 | 52.5 |
| Approach | 88 | 2.0 | 0.076 | 7.4 | LOS A | 0.4 | 2.8 | 0.37 | 0.59 | 0.37 | 53.1 |
| North: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 150 | 2.0 | 0.254 | 9.0 | LOS A | 1.6 | 11.4 | 0.20 | 0.51 | 0.20 | 54.5 |
| 8 T1 | 221 | 2.0 | 0.254 | 4.4 | LOS A | 1.6 | 11.4 | 0.20 | 0.51 | 0.20 | 54.6 |
| 9 R2 | 1 | 2.0 | 0.254 | 4.1 | LOS A | 1.6 | 11.4 | 0.20 | 0.51 | 0.20 | 53.3 |
| Approach | 372 | 2.0 | 0.254 | 6.2 | LOS A | 1.6 | 11.4 | 0.20 | 0.51 | 0.20 | 54.5 |
| West: Bobolink Drive |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 1 | 2.0 | 0.003 | 10.6 | LOS B | 0.0 | 0.1 | 0.49 | 0.52 | 0.49 | 53.8 |
| 11 T1 | 1 | 2.0 | 0.003 | 5.9 | LOS A | 0.0 | 0.1 | 0.49 | 0.52 | 0.49 | 53.8 |
| 12 R 2 | 1 | 2.0 | 0.003 | 5.7 | LOS A | 0.0 | 0.1 | 0.49 | 0.52 | 0.49 | 52.6 |
| Approach | 3 | 2.0 | 0.003 | 7.4 | LOS A | 0.0 | 0.1 | 0.49 | 0.52 | 0.49 | 53.4 |
| All Vehicles | 747 | 2.0 | 0.254 | 5.9 | LOS A | 1.6 | 11.4 | 0.28 | 0.51 | 0.28 | 54.5 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

SIDRA INTERSECTION 8.0 | Copyright © 2000-2018 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: PARSONS | Processed: Monday, June 15, 2020 4:17:50 PM
Project: C:\Home Workl476799 - LepineFernbankl1000IDATAISIDRAIPM Peak.sip8

## Total Projected 2028

Total Projected 2028 AM
3: Fernbank Road \& Robert Grant Avenue

|  | $\rangle$ |  | $\leftarrow$ | 4 |  | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | \% | $\uparrow$ | $\uparrow$ | 「 | \% | 「 |
| Traffic Volume (vph) | 55 | 359 | 241 | 258 | 303 | 44 |
| Future Volume (vph) | 55 | 359 | 241 | 258 | 303 | 44 |
| Lane Group Flow (vph) | 55 | 359 | 241 | 258 | 303 | 44 |
| Turn Type | Prot | NA | NA | Perm | Perm | Perm |
| Protected Phases | 5 | 2 | 6 |  |  |  |
| Permitted Phases |  |  |  | 6 | 4 | 4 |
| Detector Phase | 5 | 2 | 6 | 6 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 16.2 | 52.2 | 52.2 | 52.2 | 30.0 | 30.0 |
| Total Split (s) | 26.2 | 83.4 | 57.2 | 57.2 | 36.0 | 36.0 |
| Total Split (\%) | 21.9\% | 69.8\% | 47.9\% | 47.9\% | 30.2\% | 30.2\% |
| Yellow Time (s) | 4.6 | 4.6 | 4.6 | 4.6 | 3.3 | 3.3 |
| All-Red Time (s) | 1.6 | 1.6 | 1.6 | 1.6 | 2.7 | 2.7 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.2 | 6.2 | 6.2 | 6.2 | 6.0 | 6.0 |
| Lead/Lag | Lead |  | Lag | Lag |  |  |
| Lead-Lag Optimize? | Yes |  | Yes | Yes |  |  |
| Recall Mode | Max | Min | Min | Min | Max | Max |
| Act Effct Green (s) | 20.0 | 43.3 | 17.0 | 17.0 | 30.1 | 30.1 |
| Actuated g/C Ratio | 0.23 | 0.51 | 0.20 | 0.20 | 0.35 | 0.35 |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.17 | 0.40 | 0.69 | 0.53 | 0.52 | 0.08 |
| Control Delay | 29.6 | 14.4 | 42.1 | 8.0 | 27.0 | 7.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 29.6 | 14.4 | 42.1 | 8.0 | 27.0 | 7.3 |
| LOS | C | B | D | A | C | A |
| Approach Delay |  | 16.5 | 24.5 |  | 24.5 |  |
| Approach LOS |  | B | C |  | C |  |
| Queue Length 50th (m) | 7.2 | 34.4 | 36.8 | 0.0 | 38.4 | 0.0 |
| Queue Length 95th (m) | 18.1 | 52.9 | 59.6 | 17.8 | 70.0 | 7.1 |
| Internal Link Dist (m) |  | 217.9 | 258.1 |  | 237.6 |  |
| Turn Bay Length (m) | 100.0 |  |  | 100.0 | 80.0 |  |
| Base Capacity (vph) | 323 | 1612 | 1055 | 958 | 583 | 541 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.17 | 0.22 | 0.23 | 0.27 | 0.52 | 0.08 |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 119.4 |  |  |  |  |  |  |
| Actuated Cycle Length: 85.6 |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.69 |  |  |  |  |  |  |
| Intersection Signal Delay: 21.8 |  |  |  | Intersection LOS: C |  |  |
| Intersection Capacity Utilization 50.6\% |  |  |  | ICU Level of Service A |  |  |

Analysis Period (min) 15

Total Projected 2028 AM
3: Fernbank Road \& Robert Grant Avenue
Splits and Phases: 3: Fernbank Road \& Robert Grant Avenue



## Intersection Summary

Control Type: Unsignalized
Intersection Capacity Utilization 23.9\%
ICU Level of Service A
Analysis Period (min) 15

Total Projected 2028 AM
8: Bobolink Ridge \& Livery Street

| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 5 |  |  |  |  |  |
| Movement E | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | $\uparrow$ |  | * |  |
| Traffic Vol, veh/h | 31 | 35 | 64 | 0 | 2 | 102 |
| Future Vol, veh/h | 31 | 35 | 64 | 0 | 2 | 102 |
| Conflicting Peds, \#/hr | 8 | 0 | 0 | 8 | 0 | 0 |
| Sign Control F | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | \# | 0 | 0 | - | 0 | - |
| Grade, \% |  | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 31 | 35 | 64 | 0 | 2 | 102 |


| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 72 | 0 | - | 0 | 169 | 72 |
| Stage 1 | - | - | - - | - | 72 | - |
| Stage 2 | - | - | - - | - | 97 | - |
| Critical Hdwy | 4.12 | - | - - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1528 | - | - - | - | 821 | 990 |
| Stage 1 | - | - | - - | - | 951 | - |
| Stage 2 | - | - | - - | - | 927 | - |
| Platoon blocked, \% |  | - | - - | - |  |  |
| Mov Cap-1 Maneuver | 1518 | - | - - | - | 792 | 983 |
| Mov Cap-2 Maneuver | - | - | - - | - | 792 | - |
| Stage 1 | - | - | - - | - | 924 | - |
| Stage 2 | - | - | - - | - | 921 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 3.5 |  | 0 |  | 9.1 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT WBR SBLn1 |  |  |
| Capacity (veh/h) |  | 1518 | - | - | - | 978 |
| HCM Lane V/C Ratio |  | 0.02 | 2 | - | - | 0.106 |
| HCM Control Delay (s) |  | 7.4 | 0 | - | - | 9.1 |
| HCM Lane LOS |  | A | A | - | - | A |
| HCM 95th \%tile Q(veh) |  | 0.1 | , | - | - | 0.4 |

Total Projected 2028 PM
3: Fernbank Road \& Robert Grant Avenue

|  | $\rangle$ |  | $\leftarrow$ | 4 |  | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ | $\uparrow$ | F | \% | 「 |
| Traffic Volume (vph) | 41 | 304 | 532 | 346 | 283 | 44 |
| Future Volume (vph) | 41 | 304 | 532 | 346 | 283 | 44 |
| Lane Group Flow (vph) | 41 | 304 | 532 | 346 | 283 | 44 |
| Turn Type | Prot | NA | NA | Perm | Perm | Perm |
| Protected Phases | 5 | 2 | 6 |  |  |  |
| Permitted Phases |  |  |  | 6 | 4 | 4 |
| Detector Phase | 5 | 2 | 6 | 6 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 16.2 | 52.2 | 52.2 | 52.2 | 30.0 | 30.0 |
| Total Split (s) | 26.2 | 94.4 | 68.2 | 68.2 | 36.0 | 36.0 |
| Total Split (\%) | 20.1\% | 72.4\% | 52.3\% | 52.3\% | 27.6\% | 27.6\% |
| Yellow Time (s) | 4.6 | 4.6 | 4.6 | 4.6 | 3.3 | 3.3 |
| All-Red Time (s) | 1.6 | 1.6 | 1.6 | 1.6 | 2.7 | 2.7 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.2 | 6.2 | 6.2 | 6.2 | 6.0 | 6.0 |
| Lead/Lag | Lead |  | Lag | Lag |  |  |
| Lead-Lag Optimize? | Yes |  | Yes | Yes |  |  |
| Recall Mode | Max | Min | Min | Min | Max | Max |
| Act Effct Green (s) | 20.2 | 64.4 | 37.9 | 37.9 | 30.2 | 30.2 |
| Actuated g/C Ratio | 0.19 | 0.60 | 0.35 | 0.35 | 0.28 | 0.28 |
| v/c Ratio | 0.13 | 0.29 | 0.84 | 0.46 | 0.62 | 0.10 |
| Control Delay | 41.0 | 10.7 | 44.1 | 4.4 | 42.5 | 10.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 41.0 | 10.7 | 44.1 | 4.4 | 42.5 | 10.8 |
| LOS | D | B | D | A | D | B |
| Approach Delay |  | 14.3 | 28.4 |  | 38.2 |  |
| Approach LOS |  | B | C |  | D |  |
| Queue Length 50th (m) | 7.1 | 28.1 | 99.9 | 0.0 | 50.7 | 0.0 |
| Queue Length 95th (m) | 18.9 | 41.5 | 139.4 | 16.5 | 93.7 | 9.3 |
| Internal Link Dist (m) |  | 217.9 | 258.1 |  | 237.6 |  |
| Turn Bay Length ( m ) | 100.0 |  |  | 100.0 | 80.0 |  |
| Base Capacity (vph) | 326 | 1455 | 1043 | 1005 | 457 | 422 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.13 | 0.21 | 0.51 | 0.34 | 0.62 | 0.10 |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 130.4 |  |  |  |  |  |  |
| Actuated Cycle Length: 106.9 |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.84 |  |  |  |  |  |  |
| Intersection Signal Delay: 27.4 |  |  |  | Intersection LOS: C |  |  |
| Intersection Capacity Utilization 62.7\% |  |  |  | ICU Level of Service B |  |  |

Analysis Period (min) 15

Total Projected 2028 PM
3: Fernbank Road \& Robert Grant Avenue
Splits and Phases: 3: Fernbank Road \& Robert Grant Avenue


|  |  | $\leftarrow$ |  |
| :--- | ---: | ---: | ---: |
|  | $\rightarrow$ |  |  |
| Lane Group | EBT | WBT | SBL |
| Lane Configurations | $\uparrow$ | $\ominus$ |  |
| Traffic Volume (vph) | 75 | 34 | 1 |
| Future Volume (vph) | 75 | 34 | 1 |
| Lane Group Flow (vph) | 178 | 37 | 65 |
| Sign Control | Free | Free | Stop |

## Intersection Summary

Control Type: Unsignalized
Intersection Capacity Utilization 27.8\%
ICU Level of Service A
Analysis Period (min) 15

Total Projected 2028 PM
8: Bobolink Ridge \& Livery Street


| Major/Minor $\quad$ N | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 48 | 0 | - | 0 | 328 | 47 |
| Stage 1 | - | - | - | - | 47 | - |
| Stage 2 | - | - | - | - | 281 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1559 | - | - | - | 666 | 1022 |
| Stage 1 | - | - | - | - | 975 | - |
| Stage 2 | - | - | - | - | 767 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1544 | - | - | - | 608 | 1012 |
| Mov Cap-2 Maneuver | - | - | - | - | 608 | - |
| Stage 1 | - | - | - | - | 899 | - |
| Stage 2 | - | - | - | - | 760 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 4.3 |  | 0 |  | 8.8 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT WBR SBLn1 |  |  |
| Capacity (veh/h) |  | 1544 | - | - | - | 1002 |
| HCM Lane V/C Ratio |  | 0.067 | - | - | - | 0.065 |
| HCM Control Delay (s) |  | 7.5 | 0 | - | - | 8.8 |
| HCM Lane LOS |  | A | A | - | - | A |
| HCM 95th \%tile Q(veh) |  | 0.2 | - | - | - | 0.2 |

## MOVEMENT SUMMARY

7 Site: [FT2028 - Abbott/Robert Grant]
AM Peak
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | Deman Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 281 | 2.0 | 0.391 | 9.0 | LOS A | 2.9 | 20.4 | 0.24 | 0.54 | 0.24 | 54.3 |
| 3 R2 | 302 | 2.0 | 0.391 | 4.2 | LOS A | 2.9 | 20.4 | 0.24 | 0.54 | 0.24 | 53.1 |
| Approach | 583 | 2.0 | 0.391 | 6.5 | LOS A | 2.9 | 20.4 | 0.24 | 0.54 | 0.24 | 53.7 |
| East: Abbott Street East |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 145 | 2.0 | 0.203 | 8.8 | LOS A | 1.1 | 8.1 | 0.47 | 0.61 | 0.47 | 46.5 |
| 5 T1 | 78 | 2.0 | 0.203 | 4.3 | LOS A | 1.1 | 8.1 | 0.47 | 0.61 | 0.47 | 46.3 |
| Approach | 223 | 2.0 | 0.203 | 7.2 | LOS A | 1.1 | 8.1 | 0.47 | 0.61 | 0.47 | 46.4 |
| West: Abbott Street E |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 52 | 2.0 | 0.181 | 3.5 | LOS A | 1.1 | 7.6 | 0.35 | 0.44 | 0.35 | 48.3 |
| 12 R 2 | 172 | 2.0 | 0.181 | 3.6 | LOS A | 1.1 | 7.6 | 0.35 | 0.44 | 0.35 | 47.1 |
| Approach | 224 | 2.0 | 0.181 | 3.6 | LOS A | 1.1 | 7.6 | 0.35 | 0.44 | 0.35 | 47.4 |
| All Vehicles | 1030 | 2.0 | 0.391 | 6.0 | LOS A | 2.9 | 20.4 | 0.31 | 0.54 | 0.31 | 50.5 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Organisation: PARSONS | Processed: Monday, June 15, 2020 3:49:23 PM
Project: C:IHome Workl476799 - LepineFernbankl1000IDATAISIDRA\AM Peak.sip8

## MOVEMENT SUMMARY

$\sqrt[7]{ }$ Site: [FT2028 - Abbott/Robert Grant]
PM Peak
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Demand <br> Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | $\begin{aligned} & \text { Deg. } \\ & \text { Satn } \\ & \text { v/c } \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 213 | 2.0 | 0.299 | 9.1 | LOS A | 2.1 | 14.6 | 0.28 | 0.55 | 0.28 | 54.0 |
| 3 | R2 | 205 | 2.0 | 0.299 | 4.3 | LOS A | 2.1 | 14.6 | 0.28 | 0.55 | 0.28 | 52.8 |
| Appr |  | 418 | 2.0 | 0.299 | 6.8 | LOS A | 2.1 | 14.6 | 0.28 | 0.55 | 0.28 | 53.5 |
| East: Abbott Street East |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 263 | 2.0 | 0.304 | 8.6 | LOS A | 1.9 | 13.5 | 0.45 | 0.61 | 0.45 | 46.3 |
| 5 | T1 | 94 | 2.0 | 0.304 | 4.0 | LOS A | 1.9 | 13.5 | 0.45 | 0.61 | 0.45 | 46.2 |
| Approach |  | 357 | 2.0 | 0.304 | 7.4 | LOS A | 1.9 | 13.5 | 0.45 | 0.61 | 0.45 | 46.3 |
| West: Abbott Street E |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | T1 | 76 | 2.0 | 0.328 | 4.4 | LOS A | 2.2 | 15.3 | 0.53 | 0.55 | 0.53 | 47.8 |
| 12 | R2 | 287 | 2.0 | 0.328 | 4.4 | LOS A | 2.2 | 15.3 | 0.53 | 0.55 | 0.53 | 46.7 |
| Appr |  | 363 | 2.0 | 0.328 | 4.4 | LOS A | 2.2 | 15.3 | 0.53 | 0.55 | 0.53 | 46.9 |
| All V | icles | 1138 | 2.0 | 0.328 | 6.2 | LOS A | 2.2 | 15.3 | 0.41 | 0.57 | 0.41 | 48.9 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Organisation: PARSONS | Processed: Monday, June 15, 2020 4:17:49 PM
Project: C:IHome Work1476799 - LepineFernbank\1000IDATAISIDRAIPM Peak.sip8

## MOVEMENT SUMMARY

## Site: [FT2028 - Bobolink/Robert Grant]

AM Peak
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathrm{Mov} \\ & \mathrm{ID} \end{aligned}$ | Turn | Demand Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \\ \hline \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 8 | 2.0 | 0.273 | 9.5 | LOS A | 1.7 | 11.9 | 0.35 | 0.47 | 0.35 | 55.0 |
| 2 | T1 | 315 | 2.0 | 0.273 | 4.9 | LOS A | 1.7 | 11.9 | 0.35 | 0.47 | 0.35 | 55.1 |
| 3 | R2 | 26 | 2.0 | 0.273 | 4.6 | LOS A | 1.7 | 11.9 | 0.35 | 0.47 | 0.35 | 53.8 |
| Appr |  | 349 | 2.0 | 0.273 | 4.9 | LOS A | 1.7 | 11.9 | 0.35 | 0.47 | 0.35 | 55.0 |
| East: Bobolink Drive |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 68 | 2.0 | 0.151 | 10.9 | LOS B | 0.8 | 6.0 | 0.54 | 0.67 | 0.54 | 53.4 |
| 5 | T1 | 1 | 2.0 | 0.151 | 6.3 | LOSA | 0.8 | 6.0 | 0.54 | 0.67 | 0.54 | 53.5 |
| 6 | R2 | 81 | 2.0 | 0.151 | 6.0 | LOS A | 0.8 | 6.0 | 0.54 | 0.67 | 0.54 | 52.2 |
| Appr |  | 150 | 2.0 | 0.151 | 8.2 | LOS A | 0.8 | 6.0 | 0.54 | 0.67 | 0.54 | 52.8 |
| North: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 52 | 2.0 | 0.231 | 9.1 | LOS A | 1.5 | 10.4 | 0.26 | 0.47 | 0.26 | 55.1 |
| 8 | T1 | 223 | 2.0 | 0.231 | 4.5 | LOS A | 1.5 | 10.4 | 0.26 | 0.47 | 0.26 | 55.1 |
| 9 | R2 | 43 | 2.0 | 0.231 | 4.3 | LOSA | 1.5 | 10.4 | 0.26 | 0.47 | 0.26 | 53.8 |
| Approach |  | 318 | 2.0 | 0.231 | 5.2 | LOS A | 1.5 | 10.4 | 0.26 | 0.47 | 0.26 | 54.9 |
| West: Bobolink Drive |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 82 | 2.0 | 0.094 | 10.4 | LOS B | 0.5 | 3.5 | 0.48 | 0.66 | 0.48 | 52.3 |
| 11 | T1 | 1 | 2.0 | 0.094 | 5.8 | LOS A | 0.5 | 3.5 | 0.48 | 0.66 | 0.48 | 52.3 |
| 12 | R2 | 15 | 2.0 | 0.094 | 5.6 | LOS A | 0.5 | 3.5 | 0.48 | 0.66 | 0.48 | 51.1 |
| Appr |  | 98 | 2.0 | 0.094 | 9.6 | LOS A | 0.5 | 3.5 | 0.48 | 0.66 | 0.48 | 52.1 |
| All V | icles | 915 | 2.0 | 0.273 | 6.1 | LOS A | 1.7 | 11.9 | 0.37 | 0.52 | 0.37 | 54.3 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## Site: [FT2028 - Bobolink/Robert Grant]

PM Peak
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | Deman Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \\ \hline \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 15 | 2.0 | 0.314 | 10.0 | LOS A | 1.9 | 13.7 | 0.44 | 0.53 | 0.44 | 54.7 |
| 2 T1 | 275 | 2.0 | 0.314 | 5.4 | LOS A | 1.9 | 13.7 | 0.44 | 0.53 | 0.44 | 54.7 |
| 3 R2 | 82 | 2.0 | 0.314 | 5.1 | LOS A | 1.9 | 13.7 | 0.44 | 0.53 | 0.44 | 53.4 |
| Approach | 372 | 2.0 | 0.314 | 5.5 | LOS A | 1.9 | 13.7 | 0.44 | 0.53 | 0.44 | 54.4 |
| East: Bobolink Drive |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 47 | 2.0 | 0.085 | 10.4 | LOS B | 0.5 | 3.3 | 0.49 | 0.64 | 0.49 | 53.3 |
| $5 \quad$ T1 | 1 | 2.0 | 0.085 | 5.8 | LOS A | 0.5 | 3.3 | 0.49 | 0.64 | 0.49 | 53.4 |
| 6 R2 | 40 | 2.0 | 0.085 | 5.6 | LOS A | 0.5 | 3.3 | 0.49 | 0.64 | 0.49 | 52.1 |
| Approach | 88 | 2.0 | 0.085 | 8.2 | LOS A | 0.5 | 3.3 | 0.49 | 0.64 | 0.49 | 52.8 |
| North: Robert Grant Avenue |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 150 | 2.0 | 0.374 | 9.1 | LOS A | 2.7 | 19.3 | 0.26 | 0.49 | 0.26 | 54.7 |
| 8 T1 | 310 | 2.0 | 0.374 | 4.5 | LOS A | 2.7 | 19.3 | 0.26 | 0.49 | 0.26 | 54.8 |
| 9 R2 | 82 | 2.0 | 0.374 | 4.3 | LOS A | 2.7 | 19.3 | 0.26 | 0.49 | 0.26 | 53.5 |
| Approach | 542 | 2.0 | 0.374 | 5.7 | LOS A | 2.7 | 19.3 | 0.26 | 0.49 | 0.26 | 54.6 |
| West: Bobolink Drive |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 59 | 2.0 | 0.082 | 11.3 | LOS B | 0.4 | 3.2 | 0.58 | 0.70 | 0.58 | 52.0 |
| 11 T1 | 1 | 2.0 | 0.082 | 6.7 | LOS A | 0.4 | 3.2 | 0.58 | 0.70 | 0.58 | 52.1 |
| 12 R2 | 16 | 2.0 | 0.082 | 6.5 | LOS A | 0.4 | 3.2 | 0.58 | 0.70 | 0.58 | 50.9 |
| Approach | 76 | 2.0 | 0.082 | 10.3 | LOS B | 0.4 | 3.2 | 0.58 | 0.70 | 0.58 | 51.8 |
| All Vehicles | 1078 | 2.0 | 0.374 | 6.2 | LOS A | 2.7 | 19.3 | 0.37 | 0.53 | 0.37 | 54.2 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## Appendix I

MMLOS Analysis for Signalized Intersections

Multi-Modal Level of Service - Intersections Form

| Consultant <br> Scenario Comments | Parsons |  | Project Date | 476799-01000 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Existing |  |  | November 4th, 2019 |  |
|  |  |  |  |  |  |
| INTERSECTIONS |  | Fernbank Road / Robert Grant Avenue |  |  |  |
|  | Crossing Side | NORTH | South | EAST | WEST |
|  | Lanes | 3 |  | 3 | 3 |
|  | Median | No Median - 2.4 m |  | No Median - 2.4 m | No Median - 2.4 m |
|  | Conflicting Left Turns | Protected |  | Permissive | No left turn / Prohib. |
|  | Conflicting Right Turns | Permissive or yield control |  | No right turn | Permissive or yield control |
|  | Right Turns on Red (RToR) ? | RTOR allowed |  | RTOR allowed | RTOR prohibited |
|  | Ped Signal Leading Interval? | No |  | No | No |
|  | Right Turn Channel | No Channel |  | No Channel | No Right Turn |
|  | Corner Radius | 15-25m |  | 10-15m | No Right Turn |
|  | Crosswalk Type | Std transverse markings |  | Std transverse markings | Std transverse markings |
|  | PETSI Score | 76 |  | 75 | 91 |
|  | Ped. Exposure to Traffic LoS | B | - | B | A |
|  | Cycle Length |  |  |  |  |
|  | Effective Walk Time |  |  |  |  |
|  | Average Pedestrian Delay |  |  |  |  |
|  | Pedestrian Delay LoS | - | - | $\cdot$ | - |
|  |  | B | - | B | A |
|  | Level of Service | B |  |  |  |
|  | Approach From | NORTH | SOUTH | EAST | WEST |
| $\begin{aligned} & \frac{0}{0} \\ & \frac{\mathrm{U}}{0} \end{aligned}$ | Bicycle Lane Arrangement on Approach | Curb Bike Lane, Cycletrack or MUP |  | Curb Bike Lane, Cycletrack or MUP | Mixed Traffic |
|  | Right Turn Lane Configuration | Not Applicable |  | Not Applicable | $\leq 50 \mathrm{~m}$ |
|  | Right Turning Speed | Not Applicable |  | Not Applicable | $\leq 25 \mathrm{~km} / \mathrm{h}$ |
|  | Cyclist relative to RT motorists | Not Applicable | - | Not Applicable | D |
|  | Separated or Mixed Traffic | Separated | $\cdot$ | Separated | Mixed Traffic |
|  | Left Turn Approach | 1 lane crossed |  |  | One lane crossed |
|  | Operating Speed | $>50$ to $<60 \mathrm{~km} / \mathrm{h}$ |  |  | $\geq 60 \mathrm{~km} / \mathrm{h}$ |
|  | Left Turning Cyclist | D | - | - | F |
|  | Level of Service | D | - | - | F |
|  |  | F |  |  |  |
|  | Average Signal Delay | $\leq 40 \mathrm{sec}$ | $\leq 10 \mathrm{sec}$ |  |  |
|  | Level of Service | E | - | B | - |
|  |  | E |  |  |  |
| 들 | Effective Corner Radius | > 15 m | 10-15 m |  |  |
|  | Number of Receiving Lanes on Departure from Intersection | 1 |  | 1 |  |
|  | Level of Service | C | - | E | - |
|  |  | E |  |  |  |
| $\frac{0}{3}$ | Volume to Capacity Ratio | 0.81-0.90 |  |  |  |
|  | Level of Service | D |  |  |  |


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