# 2966 & 2978 Carp Road - Cheer **Training Facility**

Servicing and Stormwater Management Brief



Prepared for:

Nautical Lands Group

Prepared by:

Stantec Consulting Ltd.

September 16, 2025

Project/File: 160402064

## 2966 & 2978 Carp Road - Cheer Training Facility

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Project: 160401914

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Signature

Peter Moroz

**Printed Name** 





Project: 160401914

# **Table of Contents**

1	Introduction
1.1	Objective
	•
2	Background
3	Water Servicing
3.1	Background
• • •	
4	Wastewater Servicing
5	Stormwater Management
5.1	Existing System
• • •	
6	Conclusion
List of Ta	ables
Table 5.3	: Pond Storage and Outflow Characteristics
List of Fi	gures
Figure 1.	1: Key Plan of Site
List of A	ppendices
	x A Topographic Survey
	x B OBC Fire Flow Calculation
<b>Appendi</b>	x C Background Reports
C.1	Hydrogeological Assessment and Terrain Analysis – Re-zoning Application – 2966 and 2978
	Carp Road, Ottawa(Carp), Ontario, Paterson Group Consulting Engineers, October 23, 2025.
C.2	Servicing Report – 2978 Carp Road, Stantec, December 21, 2016
C.3	Environmental Compliance Approval (ECA)



Project: 160401914

## 1 Introduction

Stantec Consulting Ltd. has been commissioned by Nautical Lands Management Corporation to prepare the following Servicing and Stormwater Management Brief in support of the rezoning application for a proposed cheer training facility located at 2978 Carp Road and the residential dwelling with a municipal address of 2966 Carp Road, in the City of Ottawa, Ontario.

The approximately 1.3 ha site is situated southeast of the intersection of McGee Side Road and Carp Road, bounded by Carp Road to the Southwest, an undeveloped parcel to the North, and adjacent to a residential dwelling (2966 Carp Road) to the Southeast. The site is currently zoned as RC7 - Rural Commercial Zone. The key plan of the site is shown in **Figure 1.1** below. The intent of this brief is to demonstrate, to the City's satisfaction, that adequate services are available and can be allocated to support the proposal.



Figure 1.1: Key Plan of Site

The site currently consists of an existing 1,393.5 m<sup>2</sup> one-storey detached warehouse building, surface parking, and an existing 213.4m<sup>2</sup> residential dwelling with its associated landscaping area, well and septic system for servicing, and a dry pond to for stormwater management. The site currently has two asphalt



#### 2966 & 2978 Carp Road - Cheer Training Facility

Appendix A Topographic Survey

driveways with access to Carp Road in the Southwest. Nautical Lands Group has provided a topographic survey and site plan dated July 29, 2025, which is attached in **Appendix A** for more details about the existing site condition.

# 1.1 Objective

The objective of this servicing and stormwater management brief is to demonstrate that the existing site can accommodate the proposed demands associated with the new land uses. It is to be noted that given that the site is serviced with well and septic, the water and sanitary services have been assessed by Paterson Group in their Hydrogeological Assessment and Terrain Analysis, dated October 23, 2025, in support of this zoning application, and summarized herein.

Further, this brief confirms that the existing runoff coefficients and grading patterns are not being altered and confirms that the existing stormwater management design will not be impacted.



# 2 Background

Documents referenced in preparation of this stormwater and servicing report for the proposed 2966 & 2978 Carp Road site include:

- Hydrogeological Assessment and Terrain Analysis Re-zoning Application 2966 and 2978 Carp Road, Ottawa(Carp), Ontario, Paterson Group Consulting Engineers, October 23, 2025.
- Servicing Report 2978 Carp Road, Stantec, December 21, 2016.



# 3 Water Servicing

## 3.1 Background

The subject site is located in an area of the City of Ottawa that requires private servicing to provide a sufficient water supply for domestic and emergency fire flow. The current storage building, as outlined in the rezoning application, is serviced by a private well located in the north portion of the site via a 19mm building service connection. The site is also equipped with precast concrete underground firewater storage tanks located in the southern portion of the site. The storage tanks receive water from the wells and are filled during off-peak hours.

#### Water Quantity and Quality Aquifer Analysis

Based on the *Hydrogeological Assessment and Terrain Analysis* – *Re-zoning Application* – *2966 and 2978 Carp Road, Ottawa (Carp), Ontario,* by Paterson Group in October 2025, the existing well can provide water flow of approximately 21,600 L. This is approximately 3.2 times the maximum total daily design volume of effluent ((6,418 L/day) using 57% nitrate reduction required to support the Re-zoning Application. The 6,418 L/day is above the required flows as calculated under Part 8 – OBC for a subsequent application. Further discussion in the Terrain Analysis notes an additional technology that can support greater than 10,000 L/day.

A water quality aquifer analysis has been completed by the Paterson Group and the following conclusions were noted:

- The preferred water supply intercepted by existing well contains a water supply that is potable
  and contains only elevated concentrations of hardness and total dissolved solids (TDS). The
  noted parameters can be treated with current readily available water conditioning equipment.
- Total Coliforms were detected at 0 ct/100 mL, however, it is recommended that a UV system is installed to assist in the removal of any remnant Total Coliforms found in the groundwater, as a precautionary measure.
- If desired by the property owner, a commercial grade water softener can be used to facilitate the reduction of the hardness concentration and reduce scaling. If a water softener is used for the proposed development, the owner should be made aware that additional sodium will be added to the water to reduce hardness. If desired, a point-of-use reverse osmosis system can be used to provide a drinking tap source without increasing sodium levels.
- It is recommended that either a point-of-use reverse osmosis system be used to reduce the TDS concentration, or bulk bottled water is provided as a drinking water source.

Detailed potable water aquifer analysis has been conducted by Paterson Group and is presented in the background report attached in **Appendix C.1**.



#### 2966 & 2978 Carp Road - Cheer Training Facility

Appendix A Topographic Survey

#### **Fire Flow Calculation**

Assessment of required fire flows for the existing site was originally prepared within the *Servicing Report - 2978 Carp Road* (Stantec, 2016). At the time, fire flows were determined according to the Ontario Building Code (OBC) compendium Appendix A-3.2.5.7. Based on background information supplied by the Owner, it appears that the existing building has a larger volume than that initially assumed by the 2016 Servicing Report. As such, a revised fire flow calculation is presented below to account for the building volume discrepancy and to respect the recent Technical Bulletin (IWSTB-2024-05) to the *Ottawa Design Guidelines – Water Distribution*, First Edition, dated July 2010 (City of Ottawa).

The required fire flow has been calculated based on design drawings for the prefabricated building with building heights measuring on average 7.37m and satisfying the 'non-combustible with fire resistance ratings' construction type as per OBC Appendix A-3.2.5.7.

where:

Minimum supply of Water (Litres) =  $Q = K \times V \times S_{TOT}$ 

K = water supply coefficient

V = Total building volume in m3

S<sub>TOT</sub> = Total of spatial coefficient values from property line exposures on all sides

This subject site is outside the municipal water service network which requires on-site fire flow storage. Three precast concrete fire flow storage tanks have been installed with an approximate capacity of 150,000L as the fire water supply. The estimated OBC fire flow is **5,400L/min (90L/s)** and requires a total storage volume of **174,658L**. It is anticipated an additional tank in conjunction with the installed three onsite fire water storage tanks would be sufficient in support of this re-zoning application. A detailed OBC fire flow analysis is provided in the **Appendix B**. Alternatively, if the building is retrofitted with a sprinkler system meeting requirements of NFPA 13, the existing fire water supply may be sufficient for the proposed redevelopment. Analysis of required fire flows is to be reassessed at site plan control to confirm the above.



# 4 Wastewater Servicing

Paterson Group has conducted a terrain analysis for the on-site septic system, which provides sanitary servicing for the existing storage building and residential building, as part of this rezoning application. The subject site is currently outside the City of Ottawa's sanitary collection system.

According to the *Hydrogeological Assessment and Terrain Analysis – Re-zoning Application – 2966 and 2978 Carp Road, Ottawa (Carp), Ontario* (Paterson Group, October 2025), the subject site is sufficient in size to accommodate two new sewage systems and meet all of the regulatory separation criteria. As a precautionary measure, a 30 m setback should be maintained between the drinking water well and any septic system components. In addition, the following conclusions were noted:

- The subject site is sufficient in size to accommodate two new sewage systems and meet all of the regulatory separation criteria. As a precautionary measure, a 30 m setback should be maintained between the drinking water well and any septic system components.
- A maximum sewage flow volume of 1.58 m3/day at a nitrate concentration of 40 mg/L or 6.42m3/day at a nitrate concentration of 17.2 mg/L can be accommodated on the subject site based on the current layout and still be below the predictive nitrate concentration threshold of 10 mg/L at the property boundary.
- Onsite sewage disposal needs can be accommodated with a Class 4 Sewage System utilizing tertiary treatment technologies.
- A Sewage System Permit and Building Permit need to be issued prior to the commencement of construction on the proposed structures or amenities/services.
- The results of the Hydrogeological Assessment and Terrain Analysis have provided satisfactory
  evidence that the subject site can support the proposed zoning usage with respect to water
  quality, quantity and sewage system placement.



# 5 Stormwater Management

## 5.1 Existing System

Stormwater Management (SWM) for the site was designed and constructed as part of the site development for the existing warehouse building, and it provides the required quantity and quality control for the site. In 2016, Stantec conducted a detailed stormwater management analysis for the current site, and the key analysis results are summarized below.

- The grading design incorporates emergency overland flow routes in compliance with the City of
  Ottawa's stormwater management standards. These routes are intended to safely convey runoff
  from storm events exceeding the 100-year design threshold toward the eastern portion of the site,
  where existing major drainage systems are located.
- On-site storage and infiltration was incorporated in the design of the dry pond as the best approach to manage site runoff so as to not increase the total uncontrolled runoff from the site.
- The existing On-site Dry Pond controls post-development storm runoff to below pre-development target release rates through infiltration of all storm events up to and including the 100-year storm event. **Table 5.1** below summarizes the storage and outflow characteristics for the dry pond

Table 5.1: Pond Storage and Outflow Characteristics

ID	100-Year Discharge (L/s) (Infiltration)	100-Year Storage Required (m³)	Available Storage (m³)
Pond	9.8	385.3	389.6

On-site quality control with a minimum target of 70% TSS removal was established with a treatment train approach as per the requirements of MVCA. The grading design allows most of the surface runoff to flow through grassed areas for an initial infiltration and treatment of TSS. In addition, a vegetated buffer was incorporated around the dry pond to achieve a minimum 70% TSS removal efficiency as per the US EPA design manual for Low Impact Development (LID). As all pond outflow is through infiltration, site overall TSS removal rates would also achieve 80% TSS reduction to meet Enhanced criteria without additional modification.

The design was approved to meet the City of Ottawa Design Criteria and has received an Environmental Compliance Approval (Number: 9196-AQBQZV) on October 6, 2017 from the MECP. As there are no proposed increases to impervious areas on -site, it is anticipated that the existing SWM facility will be maintained to service the proposed use without additional modifications. Detailed SWM analysis is included in the *Site Servicing Report for 2978 Carp Roa*d included in **Appendix C.2**.



### 6 Conclusion

The water supply aquifer underlying the subject site is considered to be a sufficient water supply for domestic demands. The existing well contains supply that is potable and can be treated to reduce the elevated concentration of hardness and TDS, including total coliforms as a precautionary measure. The treatment can be easily accomplished with water softener, osmosis filter, and UV system. The existing fire flow storage can be expanded to accommodate the required fire flow for the development per OBC requirements.

The site is currently serviced by an on-site sewage system, which will need to be replaced with a new sewage system and meet all the regulatory separation criteria. Onsite sewage disposal needs can be accommodated with a Class 4 Sewage System utilizing tertiary treatment technologies. A Sewage System Permit and Building Permit needs to be issued prior to the commencement of construction on the proposed structures or amenities/services. The design and approval of the septic system will be completed as part of the SPA process.

The existing previously approved and constructed stormwater management system including an on-site dry pond and infiltration basin was designed and constructed to meet target discharge rates for all rainfall events up to and including the 100-year event. The system also provides sufficient quality control to meet 70% TSS removal criteria, although it can be immediately seen that the design would also meet an 'Enhanced' 80% TSS criteria given infiltration of all received runoff for up to the 100-year design storm event. Given that the existing runoff coefficients and grading patterns are not being altered, the existing stormwater management design will not be impacted, and is proposed to be maintained without additional modifications.

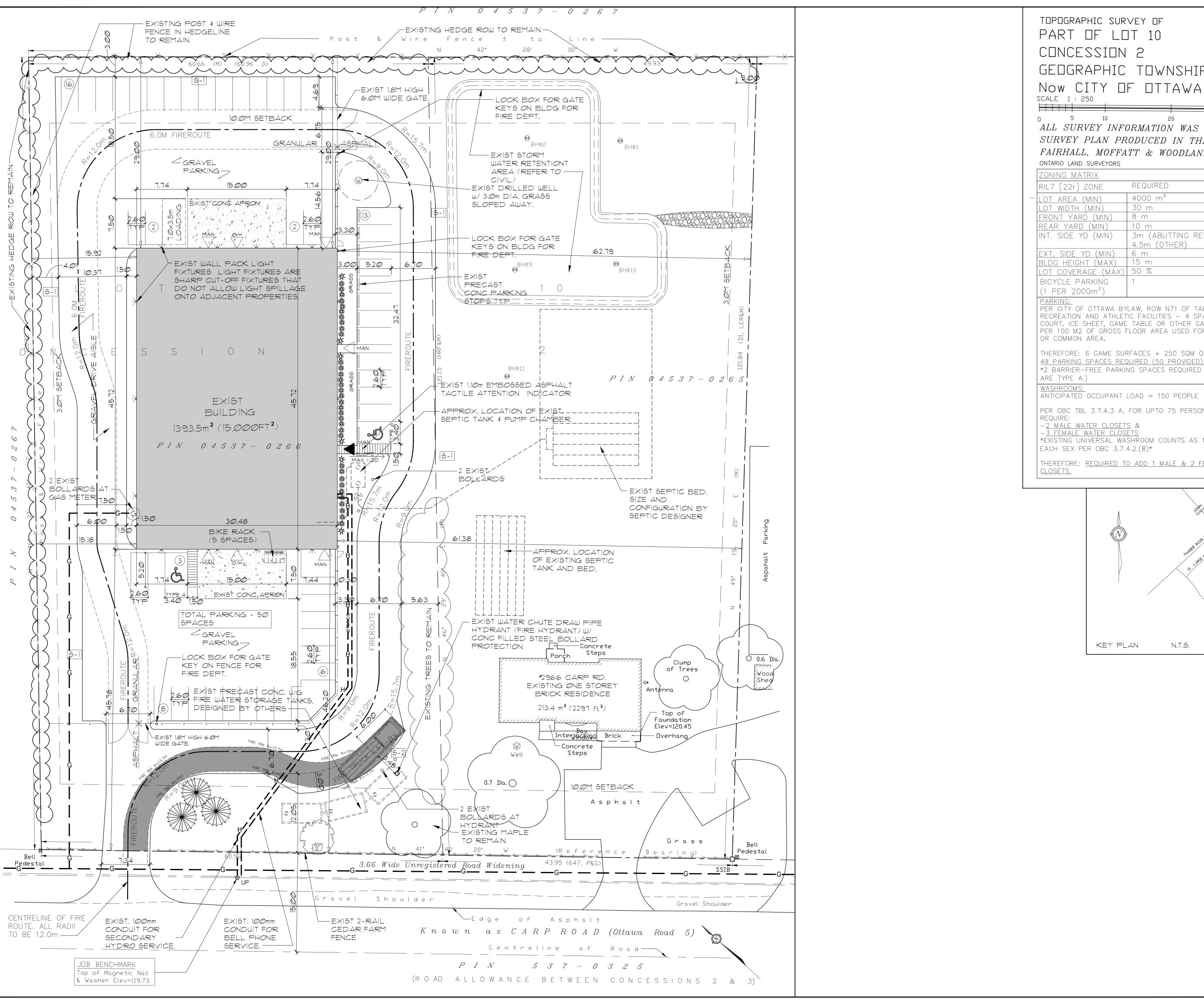


# **Appendices**



# Appendix A Topographic Survey





TOPOGRAPHIC SURVEY OF PART OF LOT 10 CONCESSION 2

GEOGRAPHIC TOWNSHIP OF HUNTLEY

ALL SURVEY INFORMATION WAS OBTAINED FROM A SURVEY PLAN PRODUCED IN THE OFFICES OF: FAIRHALL, MOFFATT & WOODLAND LIMITED

	OTT THE BUT SOIT FOR		
	ZONING MATRIX		
	RIL7 [22r] ZONE	REQUIRED	PROVIDED
_	LOT AREA (MIN)	4000 m²	13,039 m²
	LOT WIDTH (MIN)	30 m	104.89 m
	FRONT YARD (MIN)	8 m	79.1 m
	REAR YARD (MIN)	10 m	11.2 m
	INT. SIDE YD (MIN)	3m (ABUTTING RES.)	N/A
	, ,	4.5m (OTHER)	19.63 m
	EXT. SIDE YD (MIN)	6 m	N/A
	BLDG HEIGHT (MAX)	15 m	7.68 m
	LOT COVERAGE (MAX)	50 %	12.3 %
	BICYCLE PARKING	1	5
	(1 PER 2000m²)		

PER CITY OF OTTAWA BYLAW, ROW N71 OF TABLE 101 FOR RECREATION AND ATHLETIC FACILITIES - 4 SPACES PER ALLEY, COURT, ICE SHEET, GAME TABLE OR OTHER GAME SURFACE PLUS 10 PER 100 M2 OF GROSS FLOOR AREA USED FOR DINING, ASSEMBLY

THEREFORE: 6 GAME SURFACES + 250 SQM OF COMMON SPACE = 49 PARKING SPACES REQUIRED (50 PROVIDED). \*2 BARRIER-FREE PARKING SPACES REQUIRED AND PROVIDED. (BOTH

ANTICIPATED OCCUPANT LOAD = 150 PEOPLE

PER OBC TBL 3.7.4.3 A, FOR UPTO 75 PERSONS OF EACH SEX WE

\*EXISTING UNIVERSAL WASHROOM COUNTS AS 1 WATER CLOSET FOR

THEREFORE: REQUIRED TO ADD 1 MALE & 2 FEMALE WATER

SITE: 2978 CARP ROAD

N.T.S.

RAWING PREPARED BY:



555 LEGGET DRIVE, TOWER A, SUITE 920 OTTAWA, ONTARIO K2K 2X3 Ph: 613. 831.9039

\_andscape Architect:

Civil Engineer:

JUL29'25 ISSUED FOR COORDINATION IO DATE REVISION THIS DRAWING IS ISSUED FOR THE PURPOSE INDICATED BELOW:

CONSTRUCTION T IS THE RESPONSIBILITY OF THE APPROPRIATE CONTRACTOR TO CHECK AND YERIFY ALL DIMENSIONS ON SITE AND REPORT ALL ERRORS AND/ OR OMISSIONS TO THE ARCHITECT. ALL CONTRACTORS

MUST COMPLY WITH ALL PERTINENT CODES

ARCHITECT

AND BY-LAWS.

TENDER

APPROVED	REFUSED 🗌
)ATE	

Adam Brown, Manager, Development Review,

# 2978 CARP ROAD PROPOSED CHEER TRAINING FACITILTY ONTARIO

DRAWING TITLE SITE PLAN & LANDSCAPE PLAN

DATE

DRAWN

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NORTH		PROJE
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**A1** 

# **Appendix B OBC Fire Flow Calculation**



### Fire Flow Calculations as per Ontario Building Code 2024 (Appendix A)

Job#160401271Designed by:ZWDate16-Sep-25Checked by:DT

 $Q = KVS_{tot}$ 

Q = Volume of water required (L) V = Total building volume (m3)

K = Water supply coefficient from Table 1

 $S_{tot} = Sotal of spatial coefficient values from property line exposures on all sides as obtained from the formula$ 

 $S_{tot} = 1.0 + [S_{side1} + S_{side2} + S_{side3} + S_{side4}]$ 

1	Type of construction	Building Classification		Water Supply Coefficient
	Non-Combustible with Fire- Resistance Ratings	E, F-2		17
2	Area of one floor	number of floors	height of ceiling	Total Building Volume
	(m <sup>2</sup> )		(m)	(m <sup>3</sup> )
	1394	1	7.37	10,274
3	Side	Exposure		Total Spatial
		Distance (m)	Spatial Coefficient	Coeffiecient
	North	14.5	0	
	East	28.4	0	1
	South	30	0	<u> </u>
	West	45.4	0	
4	Established Fire	Reduction in		Total Volume
	Safety Plan?	Volume (%)		Reduction
	no	0%		0%
5				Total Volume 'Q' (L)
				174,658
				Minimum Required
				Fire Flow (L/min)
				5,400

<sup>\*</sup>NOTE: North spatial coefficient reduced to 0 as the north exterior building wall maintains a fire rating of 2.0h or more and has no unprotected openings.

Based on fire separation as provided on the site plan Average height of 6.0m assumed.

# **Appendix C Background Reports**



C-2 Project: 160401914

Appendix C Background Reports

C.1 Water Hydrogeological Assessment and Terrain Analysis – Re-zoning Application – 2966 and 2978 Carp Road, Ottawa(Carp), Ontario, Paterson Group Consulting Engineers, October 23, 2025.





October 23, 2025

#### PH5103-LET.01-REV.01

**Nautical Lands Group** 555 Legget Drive, Tower A, Suite 920 Kanata, Ontario K2K 3B8

Angela Mariani Attention:

#### **Consulting Engineers**

9 Auriga Drive Ottawa, Ontario **K2E7T9** Tel: (613) 226-7381

**Geotechnical Engineering Environmental Engineering** Hydrogeology **Materials Testing Building Science Rural Development Design Retaining Wall Design Noise and Vibration Studies** 

patersongroup.ca

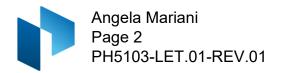
Subject: Hydrogeological Assessment and Terrain Analysis

> **Re-zoning Application** 2966-2978 Carp Road Ottawa (Carp), Ontario

#### INTRODUCTION

Paterson Group Inc. (Paterson) was retained by Nautical Lands Group to conduct a Hydrogeological Assessment and Terrain Analysis in support of a Re-zoning Application for a proposed cheer academy located at 2966-2978 Carp Road in Ottawa (Carp), Ontario. It is our understanding that the current property consists of a 1.28 hectares (ha) parcel with an existing dwelling in the southern portion of the site. The proposed re-zoning application aims to change the zoning of the existing warehouse footprint that is designated as Rural Commercial (RC7) to include instructional facility and athletic & recreational facility use. For specific planning details, please refer to the consultant report application package and to the attached Key Plan for the approximate site location.

The purpose of this work has been to determine the suitability of the water supply aquifer underlying the site and to carry out a sewage system impact assessment (terrain analysis) to determine the site's suitability for private on-site sewage systems. Specifically, the intent of the report is to determine the quality and quantity of water underlying the subject site, as well as to provide the maximum sewage flow volume which the subject site can support from a nitrate attenuation standpoint.



#### **BACKGROUND**

#### **Subject Site**

The subject property consists of a warehouse with associated landscaped areas and parking lots, and a residential dwelling with associated landscaped areas and driveways located at 2966 and 2978 Carp Road in the City of Ottawa (Carp), Ontario. The ground surface across the site is relatively flat, with a general downslope direction to the east. The general overburden groundwater flow direction is assumed to be north to northeast towards the Carp River.

The Carp Road corridor and buildings onsite are serviced by private services. The site is bordered to the northeast and northwest by undeveloped lands, to the southwest by Carp Road, followed by residential properties, and to the southeast by a commercial property.

The subject site is largely rectangular in shape with a total area of 1.28 ha. The site is currently zoned as RC7 (Rural Commercial). The land parcels to the north and east are zoned RC9 (Rural Commercial), and the residential properties to the west are zoned RR5 (Rural Residential Zone).

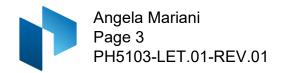
### **Regional Geology**

Published surficial geology mapping (OGS MRD128) for the area in the vicinity of the subject site indicates that the subject site is underlain predominantly by stone-poor silty sand to sandy silt-textured till on Paleozoic Terrain.

Published bedrock geology mapping (OGS MRD219) indicates that the subject lands are underlain by limestone and shale of the Simcoe Group and Verulam Formation. The available bedrock mapping coincides with the well driller's description on the Ministry of the Environment, Conservation and Parks (MECP) Water Well Records (WWR) for the surrounding well supplies installed within the subject area, which generally indicate a grey limestone.

#### **Karst Mapping**

Published karst mapping (OGS GRS005) for the area indicated that the subject site is not within a potential or inferred karst area.



#### MISSISSIPPI-RIDEAU SOURCE PROTECTION PLAN

The Mississippi-Rideau Source Protection Plan (MRSPP) provides guidance as to which policies apply to a given property, municipality or specific activity and if there are specific designations that apply to the area. The subject site has been designated as a Highly Vulnerable Aquifer (HVA within the MRSPP) and a Significant Groundwater Recharge Area (SGRA) and is identified as two of the four groundwater related vulnerable areas identified within the Clean Water Act (2006). The four vulnerable areas consists of HVA, SGRA, Intake Protection Zones (IPZ), and Wellhead Protection Areas (WHPA).

Based upon the designation, there are no restrictions of land uses on the subject site based upon its proposed usage. Therefore, there are no related requirements for an HVA or SGRA at this location.

#### **Hydrogeological Pre-Consultation**

A City of Ottawa pre-consultation was completed on August 27, 2025 to discuss the requirements for the hydrogeological assessment and terrain analysis of the subject site. Initial discussions were completed by email prior to the meeting.

### FIELDWORK PROGRAM

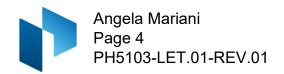
### Well Testing

As a means to demonstrate the adequacy of the aquifer underlying the subject lands, with respect to water quality and quantity, the existing drilled well (TW1) servicing the existing warehouse was tested. TW1 has a Water Well Record (WWR) Well ID of A212621. TW1 has a 150 mm diameter steel casing that extends to 6.82 m bgs with a 0.45 m stick up. The well itself extends to a depth of 58.9 m bgs. According to the water well record, limestone bedrock was recorded at a depth of approximately 4.34 m bgs. Based on available geological mapping, the drift thickness at TW1 varies from 2 to 3 m.

As a means to evaluate the water supply aquifer intercepted by the well, the well was subjected to a 8-hour constant rate pumping test. The pumping test was conducted on March 22, 2022 under the full-time supervision of Paterson personnel. Prior to the pumping test a data-logger was installed to monitor the background groundwater levels.

The existing submersible pump was used for the 8-hour pumping test. A licensed water well technician (Air Rock) completed the necessary plumbing related activities. The discharge line was placed at a sufficient distance to ensure that the discharge water was being directed away from the well and the septic system onsite. Upon completion of the test, the system was returned to its normal configuration.

The pumping test was carried out at a pumping rate of 45 L/min for a duration of 8 hours. During the pumping test, the pumping rate was periodically measured using the timed volume correlation method. The pumping rate was maintained within 5% of the selected



pumping rate. The static water level was recorded manually and an electric datalogger (VanEssen TD-Diver) was installed in the test well prior to the start of the pumping test.

The data logger recorded water levels at 30 second intervals. In addition, manual water level readings were taken at periodic intervals during the test.

Recovery data was collected from the well following the completion of the pumping. The well was noted to have achieved 100% recovery approximately 1 minute after the completion of pumping.

Groundwater samples were collected at 4 hours and 8 hours after the start of pumping. Prior to collection of the groundwater samples, the free chlorine residual was verified as non-detectable. The water samples were submitted for comprehensive testing of bacteriological, chemical, and physical water quality parameters consistent with the standard "Subdivision Supply" suite of parameters plus trace metals along with Volatile Organic Compounds (VOCs).

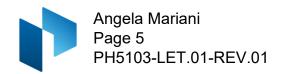
All samples were collected unfiltered and unchlorinated and were placed directly into clean bottles supplied by the analytical laboratory. Samples were placed immediately into a cooler with ice and were transported directly to Environmental Testing Canada Inc.(Eurofins) laboratory in Ottawa. All samples were received by the laboratory within 24 hours of collection.

A series of field tests of the pumped water were carried out at the well head during the 8-hour pumping test. The parameters tested at the well head included: pH, total dissolved solids, conductivity, turbidity, apparent colour, and temperature. Calibration / confirmation of calibration of all field-testing equipment was performed in Paterson's laboratory the day prior to the pumping test. Values are then confirmed again onsite prior to the start of the pumping test.

Total coliforms were detected in the analytical testing of TW1 during the pumping test at 19 ct/100 mL (TW1-GW1) in the sample taken 4 hours into the pumping test and at 23 ct/100 mL (Tw1-GW2) at 8 hours into the pumping test.

Paterson personnel went to site on April 1, 2022 to disinfect TW1 as per the Ministry of the Environment, Conservation and Parks (MECP) disinfection instruction sheet, attached. The existing submersible pump was used to circulate the water column ion order to ensure proper mixing of the disinfectant. Paterson personnel confirmed the presence and adequate mixing of the disinfectant.

On April 4, 2022, Paterson personnel confirmed the presence of free chlorine within the well water. The well was purged using the existing submersible pump to remove residual free chlorine prior to obtaining a bacteriological sample. The discharge locations were placed at a sufficient distance to ensure that the discharge water was being directed away from the wellhead.

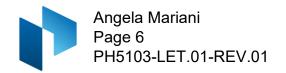


TW1 was pumped for 8 hours at a rate of approximately 15 L/min. Paterson personnel confirmed that the free chlorine residual was 0 mg/L prior to the collection of the bacteriological sample (GW1) at the end of 8 hours of purging the well.

All samples were collected unfiltered and unchlorinated and were placed directly into clean bottles supplied by the analytical laboratory. Sampled were placed immediately into a cooler with ice and were transported directly to the Eurofins Environmental Testing Canada Inc. (Eurofins) laboratory in Ottawa. All samples were received by the laboratory within 24 hours of collection.

Total Coliforms were reported as 4 ct/100 mL in the analytical testing of TW1 after the disinfection process. E. Coli was found to be non-detect as per the original results.

Additional sampling was completed on October 8, 2025 for the parameters of E.Coli, Total Coliforms and Nitrates/Nitrites. The sampling was completed by Nelson Water Inc. Total Coliforms and E.Coli were noted to be non-detect. Nitrate was found to be 0.25 mg/L and Nitrite was found to be non-detect.



## **Aquifer Analysis**

### Water Quantity

Pumping test data was analyzed using AQTESOLV Pro Version 4 aquifer analysis software package by HydroSOLVE Inc. Drawdown data was measured using an electronic water level tape and an electronic datalogger unit.

Table 1: SUMMARY OF WATER SUPPLY AQUIFER CHARACTERISTICS OF TW1						
AQUIFER PARAMETER	RESULT OF ANALYSIS					
Transmissivity (m²/day)	1,224					
Pumping Rate (L/min)	45					
Pre-test Static Water Level (m BTOC)	3.20					
Post-test Static Water Level (m BTOC)	3.26					
Maximum Drawdown (m BTOC)	3.34					
Available Drawdown (m)	55.7					
% Drawdown During Pumping Test (%)	0.3					
Specific Capacity (L/min/m drawdown)	321					

The drawdown data was analyzed using the Theis and Cooper Jacob methods of analysis. Aquifer transmissivity is estimated to be 1,224 m<sup>2</sup>/day. Refer to the Theis and Cooper Jacob methods of analysis data sheets attached to this report.

The pumping test results show that TW1 has a high yield to support the water demands that may be required. Overall maximum drawdown at a constant pumping rate for a period of 8 hours was approximately 0.14 m (0.3% of the available drawdown), but only 0.06 m at the end of the test period. 95% recovery was achieved approximately one minute after the end of pumping. It should be noted that the water level was measured to be increasing throughout the 8-hour constant rate pumping test.

The total volume of water pumped during the 8-hour pumping event was approximately 21,600 L. This is approximately 3.2 times the maximum total daily design volume of effluent (6,418 L/d) using 57% nitrate reduction required to support the Re-zoning Application. Further discussion in the Terrain Analysis notes an additional technology that can support greater than 10,000 L/day, however the 6,418 L/day is above the required flows as calculated under Part 8 – OBC for a subsequent application.

The suitability of the aquifer to support the proposed Re-zoning application was assessed using the methodology provided in the City of Ottawa Hydrogeological and Terrain Analysis Guidelines (HTAG).



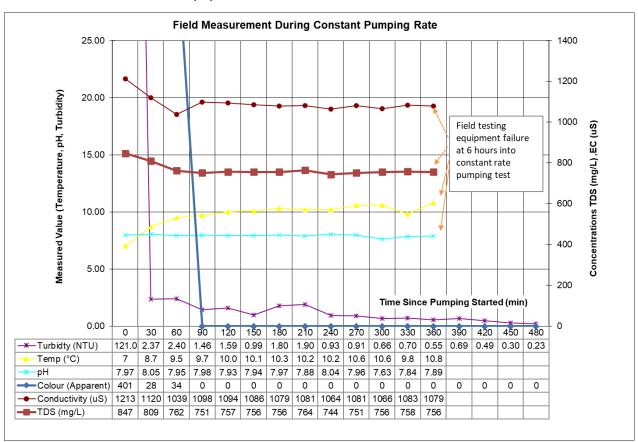
Based on the information summarized in Table 1, it is readily apparent that the water supply well has intercepted an adequately strong water supply aquifer which has sufficient quantity to service the proposed zoning usages.

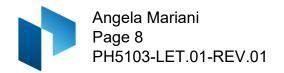
Given the analyses presented and summarized above, it is our opinion that there is an adequate supply of water to support the proposed Application.

### **Water Quality**

#### Field Data

Turbidity, electrical conductivity, total dissolved solids (TDS), pH, true color and temperature were measured at the wellhead during the pumping test. The measurements and time intervals for each of these parameters are summarized on the graphical representation below. In addition, a HACH Pocket Colorimeter II chlorine reader was used to measure the free chlorine residual level. No chlorine residual was detected in the discharged water prior to the collection of the water samples. During the constant rate pumping test, the field-testing equipment which tests for pH, TDS, EC, and temperature malfunctioned at the 6-hour point. These parameters were noted to have stabilized prior to the malfunction of the equipment.





### **Laboratory Data**

The Subdivision Package suite of parameters and trace metals laboratory water quality obtained from the pumping test of TW1 is provided in Table 2a, 2b, and 2c below and the laboratory analyses reports can be found attached. All laboratory test results can be found attached to this report.

TABLE 2a: GROUNDWATER MICROBIOLOGY & GENERAL GEOCHEMISTRY								
		OD	ws	TW1				
PARAMETER	UNITS	LIMIT	TYPE	GW1 (4 hr) 2022-03-22	GW2 (8 hr) 2022-03-22	GW1 2022-04-04		
MICROBIOLOGICAL			•	•	•	•		
Escherichia Coli (E.Coli)	ct/100mL	0	MAC	0	0	0		
Total Coliforms	ct/100mL	0	MAC	19	23	4		
<b>GENERAL CHEMICAL - HE</b>	ALTH RELA	TED						
Fluoride (F)	mg/L	1.5	MAC	<0.10	<0.10	-		
Ammonia (N-NH <sub>3</sub> )	mg/L	-	-	<0.010	<0.010	-		
Nitrite (N-NO <sub>2</sub> )	mg/L	1	MAC	<0.10	<0.10	-		
Nitrate (N-NO <sub>3</sub> )	mg/L	10	MAC	3.15	3.02	-		
Total Kjeldahl Nitrogen	mg/L	-	-	0.25	0.48	-		
Turbidity (Field)	NTU	1.0 (5.0)	MAC/AO	0.93	0.23	-		
Turbidity (Laboratory)	NTU	1.0 (5.0)	MAC/AO	0.50	0.50	-		
<b>GENERAL CHEMICAL - AE</b>	STHETIC RE	LATED						
Alkalinity (as CaCO3)	mg/L	30-500	OG	251	243	-		
Chloride (Cl)	mg/L	250	AO	135	142	-		
Colour	TCU	5	AO	<2	<2	-		
Colour (Field - Apparent)	TCU	5	AO	0	0	-		
Conductivity	uS/cm	-	-	1,180	1,180	-		
Dissolved Organic Carbon	mg/L	5	AO	2.40	2.40	-		
Hardness (as CaCO3)	mg/L	100	OG	454	451	-		
Ion Balance	unitless	-	-	0.97	0.97	-		
pН	unitless	6.5-8.5	AO	7.95	7.93	-		
Phenols	mg/L	-	-	<0.001	<0.001	-		
Sulphate (SO <sub>4</sub> )	mg/L	500	AO	182	175	-		
Sulphide (S <sub>2</sub> <sup>-</sup> )	mg/L	0.05	AO	<0.01	<0.01	-		
Tannin & Lignin	mg/L	-	-	1.00	1.00	-		
Total Dissolved Solids	mg/L	500	AO	767	767	-		

1. ODWS identifies the following types of parameters:

MAC = Maximum Allowable Concentration

AO = Aesthetic Objective

OG = Operational Guideline

2. Shaded Concentration Indicates an Exceedance of the ODWS Objective

TABLE 2b: GROUNDWATER GEOCHEMISTRY - METALS							
		OD	ws	TV	V1		
PARAMETER	UNITS	LIMIT	TYPE	GW1 (4 hr) 2022-03-22	GW2 (8 hr) 2022-03-22		
Volatiles	•		-1	•	1		
Aluminum (Al)	mg/L	0.1	OG	<0.01	<0.01		
Antimony (Sb)	mg/L	0.006	IMAC	<0.0005	<0.0005		
Arsenic (As)	mg/L	0.01	IMAC	<0.001	<0.001		
Barium (Ba)	mg/L	1.0	MAC	0.12	0.12		
Beryllium (Be)	mg/L	-	_	<0.0005	<0.0005		
Boron (B)	mg/L	5.0	IMAC	0.04	0.04		
Cadmium (Cd)	mg/L	0.005	MAC	<0.0001	<0.0001		
Calcium (Ca)	mg/L	-	-	162	161		
Chromium (Cr)	mg/L	0.05	MAC	<0.001	<0.001		
Cobalt (Co)	mg/L	-	-	<0.0002	<0.0002		
Copper (Cu)	mg/L	1.0	AO	<0.001	<0.001		
Iron (Fe)	mg/L	0.3	AO	< 0.03	< 0.03		
Lead (Pb)	mg/L	0.01	MAC	<0.001	<0.001		
Magnesium (Mg)	mg/L	-	-	12	12		
Manganese (Mn)	mg/L	0.05	AO	<0.01	<0.01		
Mercury (Hg)	mg/L	0.001	MAC	<0.0001	<0.0001		
Molybdenum (Mo)	mg/L	-	-	<0.005	< 0.005		
Nickle (Ni)	mg/L	-	-	<0.005	< 0.005		
Potassium (K)	mg/L	-	-	2	2		
Selenium (Se)	mg/L	0.05	MAC	<0.001	<0.001		
Silver (Ag)	mg/L	-	-	<0.0001	<0.0001		
Sodium (Na)	mg/L	200	AO	77	75		
Strontium (Sr)	mg/L	-	-	0.879	0.876		
Thallium (TI)	mg/L	-	-	<0.0001	<0.0001		
Uranium (U)	mg/L	0.02	MAC	<0.001	<0.001		
Vanadium (V)	mg/L		-	<0.001	<0.001		
Zinc (Zn)	mg/L	5.0	AO	<0.01	<0.01		

1. ODWS identifies the following types of parameters:

MAC = Maximum Acceptable Concentration

IMAC = Interim Maximum Acceptable Concentration

AO = Aesthetic Objective

OG = Operational Guideline

2. Shaded Concentration Indicates an Exceedance of the ODWS Objective

TABLE 2c: GROUNDWATER GEOCHEMISTRY - VOLATILES							
		OD	N/4				
DADAMETED	LIMITO	UNITS		TW1			
PARAMETER	UNITS	LIMIT	TYPE	GW1 (4 hr)	GW2 (8 hr)		
				2022-03-22	2022-03-22		
VOCs Surrogates							
1,2-dichloroethane-d4	%	-	-	100	119		
4-bromofluorobenzene	%	-	-	71	76		
Toluene-d8	%	_	_	91	98		
Volatiles			1				
1,1,1,2-tetrachloroethane	μg/L	-	-	<0.5	<0.5		
1,1,1-trichloroethane	μg/L	-	-	<0.4	<0.4		
1,1,2,2-tetrachloroethane	μg/L	-	-	<0.5	<0.5		
1,1,2-trichloroethane	μg/L	-	-	<0.4	<0.4		
1,1-dichloroethane	μg/L	-	-	<0.4	<0.4		
1,1-dichloroethylene	μg/L	14.0	MAC	<0.5	<0.5		
1,2-dichlorobenzene	μg/L	200.0	MAC	<0.4	<0.4		
1,2-dichloroethane	μg/L	5.0	IMAC	<0.2	<0.2		
1,2-dichloropropane	μg/L	-	-	<0.5	<0.5		
1,3,5-trimethylbenzene	μg/L	-	-	<0.3	<0.3		
1,3-dichlorobenzene	μg/L	-	-	<0.4	<0.4		
1,3-Dichloropropylene (cis+trans)	μg/L	-	-	<0.3	<0.3		
1,4-dichlorobenzene	μg/L	5.0	MAC	<0.4	<0.4		
Acetone	μg/L	-	-	<30	<30		
Benzene	μg/L	1.0	MAC	<0.5	<0.5		
Bromodichloromethane	μg/L	-	-	< 0.3	<0.3		
Bromoform	μg/L	-	-	<0.4	<0.4		
Bromomethane	μg/L	-	-	<0.5	<0.5		
c-1,2-Dichloroethylene	μg/L	-	-	<0.4	<0.4		
c-1,3-Dichloropropylene	μg/L	-	-	<0.2	<0.2		
Carbon Tetrachloride	μg/L	2.0	MAC	<0.2	<0.2		
Chloroethane	μg/L	_	-	<0.2	<0.2		
Chloroform	μg/L	-	-	<0.5	<0.5		
Dibromochloromethane	μg/L	-	-	<0.3	<0.3		
Dichlorodifluoromethane	μg/L	-	-	<0.5	<0.5		
Dichloromethane	μg/L	50	MAC	<4.0	<4.0		
Ethylbenzene	μg/L	140	MAC	<0.5	<0.5		
Ethylene Dibromide	μg/L	-	-	<0.2	<0.2		
Hexane	μg/L	ı	-	<5	<5		
m/p-xylene	μg/L	-	-	<0.4	<0.4		
Methyl Ethyl Ketone (MEK)	μg/L	-	-	<10	<10		
Methyl Isobutyl Ketone (MIBK)	μg/L	-	-	<10	<10		
Methyl Tert Butyl Ether (MTBE)	μg/L	15	AO	<2	<2		
Monochlorobenzene	μg/L	80	MAC	<0.5	<0.5		
o-xylene	μg/L	-	-	<0.4	<0.4		
Styrene	μg/L	-	-	<0.5	<0.5		
t-1,2-Dichloroethylene	μg/L	-	-	<0.4	<0.4		
t-1,3-Dichloropropylene	μg/L	-	-	<0.2	<0.2		
Tetrachloroethylene	μg/L	10	MAC	<0.3	<0.3		
Toluene	μg/L	60	MAC	<0.4	<0.4		
Trichloroethylene	μg/L	5	MAC	<0.3	<0.3		
Trichlorofluoromethane	μg/L	-	-	<0.5	<0.5		
Vinyl Chloride	μg/L	1	MAC	<0.2	<0.2		
Xylene; total	μg/L	90	MAC	<0.5	<0.5		

1. ODWS identifies the following types of parameters:

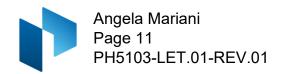
MAC = Maximum Acceptable Concentration

IMAC = Interim Maximum Acceptable Concentration

AO = Aesthetic Objective

OG = Operational Guideline

2. Shaded Concentration Indicates an Exceedance of the ODWS Objective



The bacteriological test results (Certificate of Analysis – Report No. 1973843) indicated that the test samples at the 4- and 8-hour interval were non-detect (0 ct/100 mL) for E.Coli, however, Total Coliforms were detected at concentrations of 19 ct/100 mL and 23 ct/100 mL, respectively.

Paterson personnel returned to site to disinfect the well. After the disinfection of the well and subsequent pumping, a bacteriological test was performed on the well water (Certificate of Analysis – Report No. 1974461) which indicated that E. Coli was not present (0 ct/100 mL) and that only 4 ct/100 mL Total Coliforms were present in the well water. Paterson personnel confirmed that the free chlorine residual was 0 mg/L prior to the collection of the bacteriological sample.

A water sample was taken by others on October 8, 2025. A bacteriological test was performed on the well water (Certificate of Analysis – Report No. 4491110) which indicated E.Coli and Total Coliforms were both non-detect (0 ct/100 mL). Additionally, Nitrate and Nitrite were analyzed (Certificate of Analysis – Report No. 4492546) with Nitrates at 0.25 mg/L and Nitrites at <0.1 mg/L.

The water quality of the subject water supply well meets all the Ontario Drinking Water Standards maximum acceptable concentrations (MAC). Furthermore, the water meets all of the Aesthetic Objectives (AO) and Operational Guidelines (OG) with the exception of the following.

Hardness (as CaCo	<b>O</b> 3)
Total Dissolved Sol	ids (TDS)

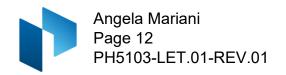
Exceedances of the above parameters are not uncommon of the water supply in the subject aquifer. Each of these groundwater parameters are discussed in detail below.

Should any water treatment be desired by the owner, it is recommended that a water treatment specialist be retained to ensure that water treatment occurs in a safe manner.

#### Hardness as CaCO<sub>3</sub>

Hardness, expressed as calcium carbonate, is an operation guideline and does not appear in the ODWS. Rather, it appears in the Technical Support Documents for Ontario Drinking Water Standards, Objectives and Guidelines as a parameter with an operational guideline at 100 mg/L. At the measured concentrations of 454 and 451 mg/L, the water is considered to be very hard, however, it is below the reasonable treatable limit of 500 mg/L specified in Table 3 of the MOECC guidance document Procedure D-5-5 (1996), thus, hardness can be treated with readily available technologies.

It is recommended that water hardness be treated using conventional technologies such as water softening or reverse osmosis, if desired by the owner. Without treating hardness, scaling can occur which can result in discolouration and residue buildup on water fixtures, or reduction in boiler efficiency due to scale build-up. According to Health Canada's *Guidelines for Canadian Drinking Water Quality - Summary Tables* "Although hardness



may have significant aesthetic effects, a guideline has not been established because public acceptance of hardness may vary considerably according to the local conditions; major contributors to hardness (calcium and magnesium) are not of direct public health concern".

#### **Total Dissolved Solids (TDS)**

TDS refers to the concentration of inorganic substances dissolved in water. The main constituents are typically chloride, sulphates, calcium, magnesium, and bicarbonates. The TDS concentration of 767 mg/L exceeds the Aesthetic Objective of 500 mg/L. At concentrations above 500 mg/L, some consumers may find the taste objectionable, however, as the objective is an aesthetic objective, no treatment is required. It is, however, recommended that a point-of-use reverse osmosis unit be installed or to provide bulk bottled water on an as-needed basis for drinking water purposes. As such, no taste problems will occur when the system is used, or bottled water is consumed.

The Langelier calculation provided an LSI of 0.7. Based on the evaluation of the result, the water is super saturated and tends to precipitate a scale layer of calcium carbonate (scale forming but non-corrosive). Based on the range of stability in the positive direction, it is recommended that water softening be used to prevent scaling. See Langelier Saturation Index Calculation attached for calculation details.

#### **Total Coliforms**

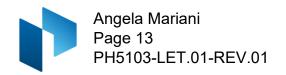
Total Coliforms are a type of bacteria which naturally occur in soil and decaying vegetation. Total Coliforms may also be associated with animal and/or human waste.

The maximum acceptable concentration (MAC) for Total Coliforms for potable drinking water in support of a Re-zoning application, as established by the City of Ottawa Hydrogeological and Terrain Analysis Guidelines (HTAG, 2021), is less than 6 ct/100 mL. According to the City of Ottawa HTAG, Total Coliforms counts of less than 6 per 100 mL sample shall be considered indicative of acceptable water quality.

Total Coliforms were detected at 19 and 23 count per 100 mL at the 4- and 8- hour mark of the pumping test, respectively. After disinfecting the well and purging the chlorinated water, Total Coliforms were detected at 4 ct/100 mL. 4 ct/100 mL Total Coliforms is below the City of Ottawa HTAG standard of less than 6 ct/100 mL.

As the site is not hydrogeologically sensitive (competent bedrock was encountered during the field investigations at depths of 2.4 to 5.9 m bgs), and is not located in an area which is mapped as potentially karstic, the Total Coliform level of 4 ct/100 mL. The subsequent analytical results in October 2025 indicate that Total Coliforms is non-detect (0 ct/100 mL) and is considered acceptable.

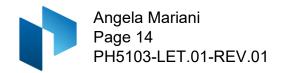
Consideration should be given to utilizing a Ultraviolet (UV) disinfection system on the water supply entering the existing warehouse and proposed development. Additionally,



the turbidity was less than 1 NTU, indicating that there should be no turbidity based interference in disinfection.

#### **Sodium**

Sodium (Na), an aesthetic parameter, was detected in the laboratory test sample at a concentration of 77 and 75 mg/L, which does not exceed the ODWS aesthetic objective of 200 mg/L. Although sodium is not toxic and no MAC has been set, concentrations above 20 mg/L require that the Medical Officer of Health be notified of the water quality results, so that this information may be passed on to local physicians for use in treatment of those requiring a sodium-restricted diet.



#### **TERRAIN ANALYSIS**

The fieldwork which was completed as part of a Geotechnical Investigation for the site (PH3834-1R, dated January 5, 2017; and PG3834-2, dated March 1, 2022) is used in support of this assessment. Additional information pertaining to this investigation was gathered from available geological mapping and surrounding WWRs.

### **Surficial Geology**

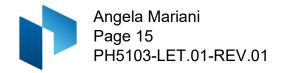
A series of test pits were excavated on the subject parcel to delineate the subsurface soil conditions as part of a Geotechnical Field Investigation. On February 8, 2022, seven (7) test pits were completed on the property. A previous investigation (PG3834-1R, dated January 5, 2017) was completed at the subject site in June and November 2016, during which fourteen (14) test pits were excavated and eleven (11) boreholes were completed onsite. The location of the test pits are delineated on the drawing PH5103-1-Test Hole Location Plan, attached. Note that the site plan on the drawing is not reflective of the proposed usage.

The test hole locations were recorded and the subsurface conditions, including the soil morphology and depth to the groundwater table (if encountered), were carefully observed and recorded. The soils encountered were classified texturally in the field and later reviewed in the laboratory.

The boreholes and test pits were advanced to a maximum depth of 5.9 and 3.4 m below ground surface (bgs), respectively. Bedrock was recorded in the WWR for TW1 at 4.34 m bgs. Refusal to excavation was recorded at depths ranging from 0.7 m to 5.9 m bgs on fractured bedrock. Competent bedrock was encountered at depths of 2.4 to 5.9 m bgs.

The subsurface profile generally consisted of topsoil extending to a maximum depth of 0.6 m bgs, underlain by silty sand to sandy silt with gravel, cobbles, boulders and trace clay which extend to a maximum depth of 1.9 m bgs. Frost heave/ frost shattered bedrock infilled with silty sand, gravel, cobbles, and boulders (unconsolidated soils) was observed under the silty sand to sandy silt with gravel, cobbles, boulders and trace clay. The testhole logs note split spoon sampling within this layer with significant sample recovery. TP1-22, TP2-22, TP6-22, and TP7-22 noted a fill of varying composition underlying the topsoil extending to depths of 1.75 m bgs. Groundwater was observed at depths between 3.6 to 4.3 m bgs in the boreholes and test pits.

Reference should be made to the borehole logs appended to this report for the details of the soil profiles encountered at each test hole location. The client should be aware that any information pertaining to soils are furnished as a matter of general information only and borehole descriptions are not to be interpreted as descriptive of conditions at locations other than those described by the boreholes themselves.



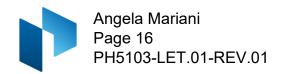
Materials encountered during Paterson's Geotechnical Investigation were generally consistent with the available surficial and bedrock geology mapping.

#### **Hydrogeological Sensitivity of the Site**

The subject site currently consists of a warehouse and residential dwelling. The dwelling is currently unoccupied. The topography of the site is generally sloping downwards to the east. The local flow direction of the surficial aquifer is expected to be in the northeasterly direction towards the Carp River. The regional groundwater flow is considered to be in the northeast direction towards the Ottawa River.

The onsite overburden generally consists of topsoil overlying a brown silty sand with gravel, cobbles, boulders and trace clay which is underlain by a fractured bedrock (frost heave/frost shatter) infilled with unconsolidated soils. The unconsolidated soils are noted to have 50 to 80% recovery during split spoon sampling within this stratum. Competent bedrock was encountered during the field investigations at depths of 2.4 to 5.9 m bgs. The frost heave bedrock noted during the borehole field investigation contained high amounts of interspersed silty sand to sandy silt (unconsolidated soils), and some clay with fragmented bedrock. For the purposes of hydrogeological sensitivity, the "fractured bedrock" unit is considered an unconsolidated soil which would provide separation form the ground surface and the underlying competent bedrock. Furthermore, based on hydraulic conductivity testing, the fastest onsite T-time was 13.8 min/cm, which is an order of magnitude slower than the T-time of less than 1 min/cm required for highly permeable soils. There were five additional test locations completed that have estimated T-times in the range of 20 to 40 mins/cm and are all considered to be not hydrogeologically sensitive. Based on this, the soils and underlying interbedded materials are not considered as highly permeable when reviewing against Ontario Building Code (OBC) Section 8.7.2.1 (1) (b)(i) and the MMAH Supplementary Standards SB-6.

Refusal to excavation was recorded on competent bedrock ranging from 2.4 to 5.9 m bgs. According to the geotechnical investigation, the overburden thickness (which includes the fractured bedrock unit with interspersed unconsolidated soils) was observed to be greater than 2 m at all borehole locations. The subject site does not have any mapped karst topography on site. Furthermore, from the TW1 WWR, bedrock was observed at a depth of 4.34 m bgs. As the proposed site does not have bedrock within 2 m of the ground surface, the site is not considered hydrogeologically sensitive. Although mitigative measures, such as increased separation distances, are not required, there is sufficient space onsite to keep the onsite well greater than 30 m away from any onsite septic components.



#### **Conceptual Lot Development**

As this Terrain Analysis is completed to support a Re-zoning Application, a Site Plan is not available.

#### Sewage System Design and Total Daily Design Sewage Flow

As this Terrain Analysis is completed to support a Re-zoning Application, a Site Plan is not available at this time. As such a sewage system design and flows have not yet been completed. A maximum predicted nitrate concentration will be determined for the site as a whole, and the current assessment will be completed based on existing conditions.

The proposed property will be analyzed as part of the Re-zoning Application to ensure the theoretical impacts are below the Ontario Drinking Water Objective maximum allowable concentration of 10 mg/L of nitrate in the groundwater prior to the property line.

#### PREDICTIVE NITRATE IMPACT ASSESSMENT

Nitrate is considered to be a critical parameter of concern when assessing impacts to groundwater quality downgradient of an onsite sewage system. The City of Ottawa annotated MECP Procedure D-5-4 in the Hydrogeological and Terrain Analysis Guidelines (HTAG) applies for the proposed development. For the purpose of this guideline, the Ontario Drinking Water Objective of 10 mg/L of nitrate is the maximum allowable concentration detectable in the groundwater prior to the property line.

A detailed impact assessment is required due to the proposed zoning of the site. In order to demonstrate that private services would adequately support the proposed Re-zoning Application, a predictive nitrate impact assessment for the subject site was completed. This calculation was completed to determine the maximum sewage flow volume which could be applied to the subject site with the current site conditions. As the site is within the Carp Road Corridor, the use of tertiary treatment systems (nitrate reducing systems) are allowed to be considered in support of re-zoning. The values shown in the Predictive Nitrate Impact Assessment calculation attached to this report are summarized below:

Site area	1.28 ha
Impervious area %	45 %
Concentration of nitrate in effluent (Value based on conventional effluent concentration)	40 mg/L
Concentration of nitrate in effluent	17.2 mg/L

Surplus Water	378 mm/year		
The surplus water value was estimated based on Environment Canada Climate Officalues with a soil type comprised of clay loam (urban lawn) and anthropogenic sources hich can be found attached.)			
Combined infiltration factor based on:	0.67		
<ul> <li>Topography infiltration factor</li> </ul>	0.25		
<ul> <li>Soil texture infiltration factor</li> </ul>	0.30		
<ul> <li>Cover infiltration factor</li> </ul>	0.12		

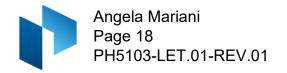
The topography infiltration factor of 0.25 is based upon a slope between "flat land" (<0.6 m/km) and "rolling land" (average slope of 2.8 to 3.8 m/km) based on available mapping.

The soil texture infiltration factor was based upon a soil that is between "open sandy loam" with a value of 0.4 and "medium combinations of clay and loam" with a value of 0.2 which is a reasonable generalization based upon the field investigation by Paterson, available geological mapping and surrounding WWRs.

The "vegetative cover infiltration factor" was calculated as 0.12 based upon the site being used as cultivated land with some trees throughout the site.

As part of the rezoning process, the City of Ottawa does not typically allow the use of tertiary treatment systems to support the re-zoning application, however, as the site is within the Carp Road Corridor, tertiary treatment systems can be used to support the re-zoning application. As a tertiary treatment system requires annual monitoring by the Ottawa Septic System Office (OSSO), and allows for advanced treatment of sewage effluent, a tertiary treatment system is being reviewed for the Subject Site. The mandatory monitoring required on tertiary treatment systems by the OSSO ensures that the system is properly maintained and replaced when required, whereas there is no mandatory monitoring on a conventional sewage system. In order to demonstrate the viability and sustainability aspects of private servicing on the subject site, a Nitrate Impact Assessment was completed using the above noted parameters.

The predicted nitrate concentration calculation for a conventional sewage system (system without nitrate reduction) results in a maximum of **1.58 m³/day** of effluent using a nitrate concentration of 40 mg/L. The inclusion of nitrate reduction technology (57 % nitrogen reduction in the of the effluent nitrate) would result in a maximum of **6.42 m³/day** of effluent using a nitrate concentration of 17.2 mg/L. The Waterloo-Biofilter technology (WaterNOx) is capable of up to 90% nitrate reduction, which would allow greater than **10 m³/day**. Both maximum sewage flow volumes with their respective reduced nitrate concentrations meet the nitrate concentration threshold of below 10 mg/L at the property boundary. Additional re-infiltration from stormwater (up to 10%) could be used to increase the dilution of septic effluent, if needed.



A sewage system installation application for a new sewage system on any site in the City of Ottawa with a sewage flow volume of less than 10 m<sup>3</sup>/day will require an OSSO application.

## **CONCLUSIONS**

Based on the information contained within the body of this report the following conclusions can be drawn:

- 1. The water supply aquifer underlying the subject site is considered to be adequate to support the water quantity demands for the proposed zoning uses.
- The preferred water supply intercepted by TW1 contains a water supply that is potable and contains only elevated concentrations of hardness and TDS. The noted parameters can be treated with current readily available water conditioning equipment.
- 3. Total Coliforms were detected at 0 ct/100 mL, however, it is recommended that a UV system is installed to assist in the removal of any potential Total Coliforms found in the groundwater, as a precautionary measure.
- 4. If desired by the property owner, a commercial grade water softener can be used to facilitate the reduction of the hardness concentration and reduce scaling. If a water softener is used for the proposed development, the owner should be made aware that additional sodium will be added to the water to reduce hardness. If desired, a point-of-use reverse osmosis system can be used to provide a drinking tap source without increasing sodium levels.
- 5. It is recommended that either a point-of-use reverse osmosis system be used to reduce the TDS concentration, or bulk bottled water is provided as a drinking water source.
- 6. The subject site is sufficient in size to accommodate two new sewage systems and meet all of the regulatory separation criteria. As a precautionary measure, a 30 m setback should be maintained between the drinking water well and any septic system components.
- 7. A maximum sewage flow volume of **1.58 m³/day** at a nitrate concentration of 40 mg/L or **6.42 m³/day** at a nitrate concentration of 17.2 mg/L can be accommodated on the subject site based on the current layout and still be below the predictive nitrate concentration threshold of 10 mg/L at the property boundary.



- 8. Onsite sewage disposal needs can be accommodated with a Class 4 Sewage System utilizing tertiary treatment technologies.
- 9. A Sewage System Permit and Building Permit need to be issued prior to the commencement of construction on the proposed structures or amenities/services.
- 10. The results of the Hydrogeological Assessment and Terrain Analysis have provided satisfactory evidence that the subject site can support the proposed zoning usage with respect to water quality, quantity and sewage system placement.

We trust that the current submission satisfies your immediate requirements.

Best Regards,

Paterson Group Inc.

M. S. KILLAM 100221103

Michael Ki

Alexander Schopf, PhD, EIT

Michael Killam, P.Eng

#### **Attachments:**

	Kev	Р	lan
_	rve v		ıaıı

- MECP Water Well Records 1973843 & 1974461
- Eurofins Certificate of Analysis
- ☐ Paterson PG3834 Test Pit and Borehole Logs
- □ AQTESOLV Pumping Test Analysis Reports
- Langelier Calculation
- ☐ Nitrate Impact Assessment Calculations
- ☐ Paterson Drawing PH5103-1 Test Hole Location Plan
- Well Disinfection Instruction Sheet

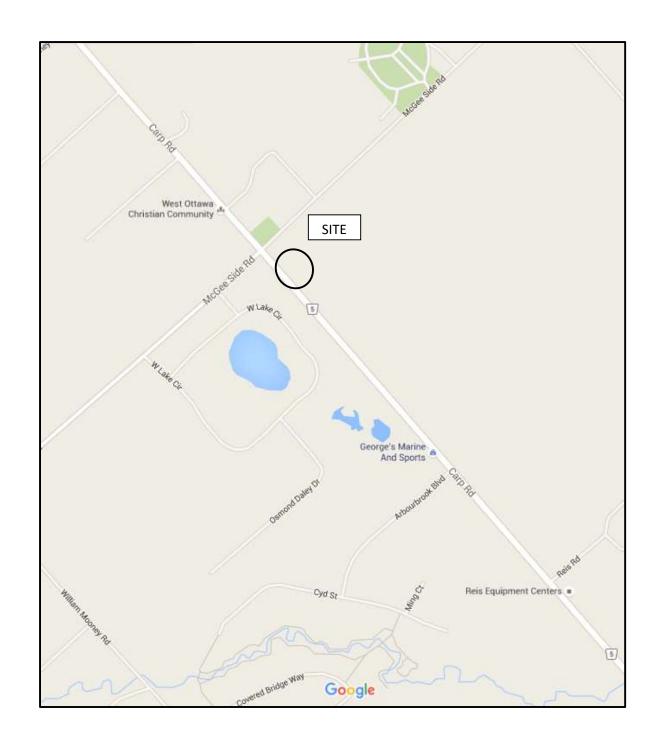


Figure 1 – Key Plan

#### Ministry of the Environment Well Tag No. (Place Sticker and/or Print Below) Well Record and Climate Change Tag#: A 212621 Regulation 903 Ontario Water Resources Act Page Well Owner's Information Last Name / Organization E-mail Address Mailing Address (Street Number/Name) ☐ Well Constructed by Well Owner Municipality Province Postal Code Telephone No. (inc. area code) Well Location Address of Well Location (Street Number/Name) Lot County/District/Municipality City/Town/Village Province Postal Code Ontario UTM Coordinates | Zone | Easting Northing Municipal Plan and Sublot Number NAD | 8 | 3 Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form) General Colour Most Common Material Other Materials Depth (m/ft) General Description and+grave gral

	7	Annular Space				Results of W	ell Yie	ld Testing		
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d) ia (m	/ft) Gas Other, spe	city		1000	00		1			

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Water found at Depth Kind of Water: Fresh Untested

Province Postal Code Business E-mail Address

Well Contractor and Well Technician Information

Bus.Telephone No. (inc. area code) Name of Well Technician (Last Name, First Name)

Well Technician's Licence No. Signature of Technician and/or Contractor Date Submitted

58,90 (m/ft) Gas Other, specify

Business Name of Well Contractor

Business Address (Street Number/Name)

(m/ft) Gas Other, specify

Well Owner's Copy

Municipality

Date Package Delivered Ministry Use Only Audit No. **Z**24243 DOININGS

417 HWY

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UTM 18 2 4 2 1 9 2 0 E GROUND WATER BRANCH 15 R 1501791010 N 6 1860 Elev. 4 R 031810 The Ontario Water Resources Commission Act, 1957 RECOURCES COMMISSION Basin 2 5 WATER WELL Carleton Township, Villago, Town or City Huntley
18 mar 1960 **RECORD** County or District..... ate completed 18 max Casing and Screen Record **Pumping Test** Inside diameter of casing 2/ " Static level 20 ' Total length of casing 24 Test-pumping rate 5 G.P.M. Pumping level 21' Type of screen None Length of screen Duration of test pumping /2 hv Depth to top of screen..... Water clear or cloudy at end of test Clear Diameter of finished hole..... Recommended pumping rate \_\_\_\_\_\_\_ G.P.M. Well Log **Water Record** Depth(s) Kind of water From ft. No. of feet Overburden and Bedrock Record found 41 Location of Well For what purpose(s) is the water to be used? in diagram below show distances of well from road and lot line. Indicate north by arrow. Is well on upland, in valley, or on hillside? Licence Number 484 Lot 10 Con 2 Form 5 15M-58-4149 TOWNS HIP HUNTLEY

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# MINISTRY OF THE ENVIRONMENT The Ontario Water Resources Act

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# WATER WELL RECORD

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PUMPING TEST METHOD 10 PUMPING RATE	5 PLASTIC	
71 1 PUMP 2 BAILER 25	5 GPM 15-16 17-18 HOURSMINS	
LEVEL END OF WATER LE	EVELS DURING  RECOVERY  30 MINUTES   45 MINUTES   60 MINUTES	IN DIAGRAM BELOW SHOW DISTANCES OF WELL FROM ROAD AND LOT LINE INDICATE NORTH BY ARROW.
D FEET FEET FEET FEET	7 20-31 1 32-34 C) 35-37 T FEET FEET FEET	25'] * WEZL
FEET FEET FEET FEET  IF FLOWING 38-41 PUMP INTAKE S  GYP  RECOMMENDED PUMP TYPE  RECOMMENDED PUMP TYPE  PUMP  PUMP	WATER AT END OF TEST 41	1 50
RECOMMENDED PUMP TYPE RECOMMENDED PUMP SETTING	GO FEET RATE COMMENDED 46-49  PUMPING GPM	
50-53		House
FINAL STATUS  1 WATER SUPPLY 2 OBSERVATION WELL		
OF WELL 4 RECHARGE WELL	7 UNFINISHED 9 DEWATERING	
WATER 3   IRRIGATION	5 COMMERCIAL  6 MUNICIPAL  7 PUBLIC SUPPLY	
USE 4   INDUSTRIAL   OTHER	■ ☐ COOLING OR AIR CONDITIONING ■ ☐ NOT USED	
METHOD 2 GROVE CONVENTY		CAVANBUIGH DRIVE
OF   3   ROTARY (REVERSE) CONSTRUCTION 4   ROTARY (AIR)		32740
NAME OF WELL CONTRACTOR	DIGGING OTHER	DRILLERS REMARKS
MANE OF WELL CONTRACTOR Sille	in Color Sumber 5 222	SOURCE STATE CONTRACTOR STATE PACE PACE PACE PACE PACE PACE PACE PAC
ADDRESS PRAY CAND	P.O. 437	SE
NAME OF WELL TECHNICIAN	WELL TECHNICIAN'S	A REMARKS
SIGNATURE OF TECHNICAN CONTRACTOR	SUBMISSION DATE	MDE WDE
MINISTRY OF THE ENVIRON	MENT COPY	FORM NO. 0506 (11/86) FORM 9



# The Ontario Water Resources Act WATER WELL RECORD

	1. PRINT ONLY IN 2. CHECK 🔀 CORR	SPACES PROVIDED RECT BOX WHERE APPLICABLE	1527	642 1500	25   CON	, 1 1622
COUNTY OR DISTRICT	- 3	TOWNSHIP, BOROUGH, CITY, TOWN, VILL		CON BLOCK, TRACT, S	URVEY ETC	LOT 25-27
		3	ton - Hunt]	•	DATE COMPLETED	10
		McGee Road	Carp,Onta	AC MASIN CODE	рау <u>20</u> мо <u>12</u>	2
1 2	N 10 12	17 16 24	25 26	30 31		1 1
GENERAL COLOUR	MOST	OG OF OVERBURDEN AND BEI	DROCK MATERI		DEPT	H · FEET
	COMMON MATERIAL	OTHER MATERIALS		GENERAL DESCRIPTION	FROM	то
Brown	Seil	Stones		· · · · · · · · · · · · · · · · · · ·		4
Gray	<u>Limestone</u>	Soft Lagers			4	155
	-					
				·		
31	<u></u>		11 11	1 1 1 1 1 1		
32		<del></del>		<u> </u>	<u> </u>	
	ER RECORD	51 CASING & OPEN HOL	E RECORD	SIZE(S) OF OPENING	\$5 31-33 DIAMETER 34-38	75 80 LENGTH 39-40
WATER FOUND AT - FEET	KIND OF WATER	INSIDE WALL THICKNESS INCHES INCHES	DEPTH - FEET FRUM TO	SIST NO )  MATERIAL AND TYPE	INCHES DEPTH TO TOP	FEET 41-44 30
74 2 -		5 174 1 STEEL 12 .188	0 22"	S	OF SCREEN	FEET
132	FRESH 3 SULPHUR 19 SALTY 4 MINERALS 6 GAS	3 CONCRETE 4 OPEN HOLE 5 PLASTIC			NG & SEALING RECO	RD
147 2	FRESH 3 SULPHUR 24 SALTY 6 GAS	1 USTEEL 2 GALVANIZED 3 CONCRETE	20-23	DEPTH SET AT - FEET FROM TO		NT GROUT
	FRESH 5 SULPHUR 29 SALTY 6 GAS	5 UPLASTIC  24-25 1 USTEEL 26	22 155	21 0 14-17	Grouted Cement	(4)
	FRESH 3 SULPHUR 34 10 4 MINERALS 6 GAS	2 □GALVANIZED 3 □CONCRETE 4 □OPEN HOLE 5 □PLASTIC		26-29 30-33 8	0	
71 PUMPING TEST METH		11-14 DURATION OF PUMPING		LOCATION	05.005.	
1 Dump 2	WATER LEVEL 25	8 GPM 15-16 17-1 MIN	15	LOCATION		
LEVEL 19-21	END OF WATER LEV PUMPING 22-24 15 MINUTES	ELS DURING  1 PUMPING 2 RECOVERY  30 MINUTES   45 MINUTES   60 MINUTES	LOT L	INE INDICATE NORTH BY	ARROW.	١,
U 14 FEET	85 FEET 76 FEET	29-31 32-34 35-3 85eet 85 feet 85 fe		O.C. *5		<del> </del>
IF FLOWING, GIVE RATE  RECOMMENDED PUMP	30-41 PUMP INTAKE SET	AT WATER AT END OF TEST 4:	11			
RECOMMENDED PUMP	PUMP	43-45 RECOMMENDED 46-4	1		÷	
0-53		UU FEET RATE 5 GPI				Road
FINAL STATUS	WATER SUPPLY Description well	S ABANDONED, INSUFFICIENT SUPPLY  B ABANDONED POOR QUALITY	]			a a
OF WELL	3 TEST HOLE 4 RECHARGE WELL	7 UNFINISHED  DEWATERING			i driveway	300
WATER	2 D STOCK S	COMMERCIAL MUNICIPAL				7 34
USE	3   IRRIGATION 7 4   INDUSTRIAL 8	☐ PUBLIC SUPPLY ☐ COOLING OR AIR CONDITIONING			36	/ 1
57	1 G CABLE TOOL 7501	• □ NOT USED	-			
METHOD OF	3 ROTARY (REVERSE)	7 DIAMOND  # DITTING	1/2/			
CONSTRUCTION	5 AIR PERCHISSION	DIGGING OTHER	DRILLERS REMARKS	s	138	065
NAME OF WELL CON		WELL CONTRACTOR'S	DATA		DATE RECEIVED	63-68 80
Capital W ADDRESS  BOX 490 NAME OF WELL T  NAME OF WELL T  SIGNATURE OF TEC	ater Supply Ltd	1558	O DATE OF INSPEC	1558 NSPECTOR	JAN 24 1994	
Box 490	Stittsville, On	WELL TECHNICIAN'S	S REMARKS			
S.Miller	J. Moore	TOO97/TOO96	OFFICE			
Wava	- April	DAY 29 NO 12 YR 93	<u> </u>		000.6	25
MINISTRY OF	THE ENVIRONME	NT COPY			FORM NO. 0506 (11)	/86) FORM 9

# The Ontario Water Resources Act

# WATER WELL RECORD

Ontario		SPACES PROVIDED RECT BOX WHERE APPLICABLE	11	1528	596	HUNICIP. 15005	con.	1 102
COUNTY OR DISTRICT	^	TOWNSHIP, BOROUGH, CITY,	RLETON	s Hunt		BLOCK TRACT, SURVEY	ETC	22 23 74 LOT 25-27
		21	70 L	Ac Cace	$\leq 1$	$\widehat{\mathcal{R}}_{\alpha}$	DATE COMPLETED  DAY 10 MO 5	
1 2	M 10 12	ING	<u>/                                    </u>	C. ELEVATION		MASIN CODE	" " " " " " " " " " " " " " " " " " "	
	<del></del>	OG OF OVERBURDEN	AND BEDR		ALS (SEE )	NSTRUCTIONS)		47
GENERAL COLOUR	MOST COMMON MATERIAL	OTHER MATE	ERIALS		GENER	AL DESCRIPTION	DEPTH FROM	- FEET
BROWN	SAND	STONES	Chry				0	7
GREY	LIMESTONE		,		ME	O, HARD	7'	110
GREY	LIMESTONE	BLACK	Limes	1		O HARD	110	150
GREY	HIMESTONE	BLACK-LIN	MESTU	∪Æ		9×1)	150	200
			. 448.4					
		,						
31					البلبا	111111		
1 Z 10	TER RECORD	51 CASING & O	PEN HOLE	RECORD.	SIZE(S	OF OPENING 31-3	65 13 DIAMETER 34-38 L	75 10 ENGTH 39-40
WATER FOUND AT - FEET	KIND OF WATER	INSIDE DIAM MATERIAL INCHES	WALL	DEPTH - FEET	U ISLOT	RIAL AND TYPE	DEPTH TO TOP	FEET 41-44 30
140	FRESH 3 SULPHUR  SALTY 4 MINERALS  6 GAS	1971 1 DSTEEL 12	188 (	22"	SC		OF SCREEN	FEET
1.101	FRESH 3 SULPHUR 4 MINERALS 5ALTY 6 GAS	3 CONCRETE 4 OPEN HOLE 5 PLASTIC	700	20-23	61	PLUGGING 8	SEALING RECO	
2 0	FRESH 3 SULPHUR 24 SALTY 6 GAS	1 STEEL 2 GALVANIZED 3 GONCRETE 4 BOPEN HOLE	2	Z' 200'	FROM	TO MATI		NT GROUT CKER ETC )
2 🗆	FRESH 3 SULPHUR 29 4 MINERALS 5 GAS	5 □ PLASTIC  24-25 1 □ STEEL 2 □ GALVANIZED		27-30	18.		MENT GR	out
	FRESH 3 SULPHUR 34 00 4 MINERALS SALTY 6 GAS	3 □ CONCRETE 4 □ OPEN HOLE 5 □ PLASTIC			26-2	9 30-33 40		
71 PUMPING TEST MET	HOD IO PUMPING RATE	11-14 DURATION OF PUM 2 15-16	17-18		L	OCATION OF	WELL	
STATIC LEVEL	WATER LEVEL 25 END OF WATER LE	VELS DURING PROPERTY REPORTS	ÜMPING	IN DIA		W SHOW DISTANCES O CATE NORTH BY ARRO	F WELL FROM ROAD AI W.	ND D
18 /8	22-24 15 MINUTES 26-28					4.GRESJ. R	ð.	
FEET F FLOWING. GIVE RATE  RECOMMENDED PUM	FEET FEE 38-41 PUMP INTAKE S	ET AT WATER AT END OF	TEST 42			-		
RECOMMENDED PUM	PUMP	FEET 1 CLEAR  43-45 RECOMMENDED PUMPING 2	2 CLOUDY 46-49					ĺ
SHALLOW	DEEP SETTING	/S FEET RATE	GPM	3	§ 5			_
FINAL STATUS	WATER SUPPLY 2 G OBSERVATION WELL	5 ABANDONED INSUFFI		4 6000	200			
OF WELL	3 TEST HOLE 4 RECHARGE WELL	7 UNFINISHED  DEWATERING		1 1				J
WATER	DOMESTIC  To STOCK  Registrion	5 COMMERCIAL 6 MUNICIPAL 7 PUBLIC SUPPLY			hema	- x	15' -	
USE	4   INDUSTRIAL   OTHER	COOLING OR AIR CONDITION  Output  Outp		1 1:	28	1-401		
METHOD	CABLE TOOL  CABLE TOOL  CONVENTE	6   BORING ONAL) 7   DIAMOND			4			
OF CONSTRUCTIO	3   ROTARY (REVERSE)	#   JETTING 9   DRIVING			<b>r</b>		1 4 0	574
NAME OF WELL CO		WELL C	OTHER	DRILLERS REMARK		TRACTOR 59.62 DATE		574
D ADDRESS	4 DRILLING	- INC SZ	ZZ	SOURCE DATE OF INSPEC	5		AUG 2 8 1995	
NAME OF VELLE	BOX 437	CARP, ON	ECHNICIAN'S	S REMARKS				
SIGNATURE OF T	ECHNICIAN CONTRACTOR		NUMBER	FFICE				
1.	Show	вач мо	YR	9		·	CSS.E	
MINISTRY C	OF THE ENVIRONM	ENT COPY					FORM NO. 0506 (11	/86) FORM 9

Ontario Ministry of the Environment	Well Tat 4 04970:	it Below)	Well Record
O I I COI I O	A049T	Regulation	on 903 Ontario Water Resources Ac Page of
Well Owner's Information			
First Name Last Name	E-mail Addres	SS	☐ Well Constructed
Mailing Address (Street Number/Name, RR)	Municipality	Province A Postal Code	by Well Owner  Telephone No. (inc. area code)
+2171 MEGE Side	Road Carp	CAT KOLAL	relephone No. (inc. area code)
Part A Construction and/or Major Alteration of a			44911111111
Address of Well Location (Street Number/Name, RR)	0 Township 0	Lot 11	Concession
County/District/Municipality	City/Town/Village	WITTER I	Province Postal Code
Otowa Cor leter	Car	0	Ontario Jan 1
UTM Coordinates Zone Easting Northing	GPS Unit Make Model	Mode of Operation:	Undifferentiated Averaged
NAD 8 3 1 5 4 5 9 4 1 9 9 10	121 Magellon	Differentiated, specify	
Overburden and Bedrock Materials (see instructions on General Colour Most Common Material	Other Materials	General Description	Depth (Metres)
Sand Go	20,00		From To
Carlo	205		
5,00	1100100		10/0
	A Market and the second and the seco		
		A PART OF THE PART	
~ 01	0000	· · · · · · · · · · · · · · · · · · ·	
ATRI	RIDKINE	210 W	
Annular Space/Abandonment Se			ell Yield Testing
Depth Set at (Metres) Type of Sealant Used From To (Material and Type)	Volume Placed (Cubic Metres)	Check box if after test of well yield, water was:	Draw Down Recovery Time Water Level Time Water Level
610 0 West Coment	5/400 1.2724	Clear and sand free	(Min) (Metres) (Min) (Metres)
	7	state  If pumping discontinued, give reason:	Static Static Level 34-70
		in puriping discontinued, give reason.	1708 1 3236
		Pumping test method	2 8 00 2 3 30
		Pump intake set at (Metres)	3 9 50 3 2 25
Method of Construction  ☐ Cable Tool ☐ Diamond ☐ Public	Water Use	The set adjustes	4 10 30 4 29 18
☐ Rotary (Conventional) ☐ Jetting ☐ Dőmestic	☐ Municipal ☐ Dewatering	Pumping rate (Litres/min)	5 11 20 5 20 20
☐ Rotary (Reverse) ☐ Driving ☐ Livestock ☐ Rotary (Air) ☐ Digging ☐ Irrigation	☐ Test Hole ☐ Monitoring ☐ Cooling & Air Conditioning	Duration of pumping	100
Air percussion Boring Industrial	A CONTRACT OF THE STATE OF THE	hrs + Omin	15, 22, 3
Other, specify  Status of Well		Final water level end of pumping (Metres)	15 18 60 15 20.
Water Supply Dewatering Well	Observation and/or Monitoring Hole	Recommended pump type	20 9, 40 20 1660
☐ Replacement Well ☐ Abandoned, Insufficient Supply ☐ Test Hole ☐ Abandoned, Poor Water Quality	☐ Alteration (Construction)	☐ Shallow ☐ Deep	25 23.87 25 1390
☐ Recharge Well ☐ Abandoned, other, specify		Recommended pump depth	30 26, 30 158
Location of Well		Recommended pump rate	40 2066 40 9 90
Please provide a map below showing: - all property boundaries, and measurements sufficient to locate	the well in relation to fixed points,	(Litrestimin))	50 2 7 60 50 1 80
<ul> <li>an arrow indicating the North direction</li> <li>detailed drawings can be provided as attachments no larger that</li> </ul>	an legal size (8.5" by 14")	If flowing give rate	60 34 90 60 6 30
- vidigital pictures of inside of well can also be provided	(NT)		I have a
	$\sim$	4	r Details of Water
			esh Salty Sulphur Minerals
IN IKM	160		of Water STEF
		Water found at Depth Kind	esh
0/2	171 MCGEE	•	esh
	171 -0000	Casing Used   Screen Used	d Casing and Well Details
7 40	3(DE)	Galvanized Galvanized	Diameter of the Hele (Centimetres)
		Steel Steel	Depth of the Hole (typeres)
Date Well Completed   Was the well owner's information   D	ate the Well Record and Package	Plastic Plastic	15231
C(yyy/mm/de/) 3 package delivered? No S	elivered to Well Owner (ywy/mm/dd)	Concrete Concrete	Wall Thickness (Metres)
Well Contractor and Well Technici	an Information	No Casing and Screen Used	Inside Diameter of the Casing (Metres)
Business Name of Well Contractor	Well Contractor's Licence No.	Dopen Hole (0 15235	11.1588
Business Address (Street No./Name, number, RR)	Municipality	D(sinfected?  Yes No	Depth of the Casing (Majtrds)
PRA I	RICHMOND		y Use Only
Province Rostal Code Business E-mail Ad		Audit No.	Well Contractor No.
Bus. Telephone No. (inc. area code) Name of Well Technician (L	aet Nama Firet Nama\	z 60149	Date of Jespestion (consider (14)
G B R A DI TA	api Ivaine, Filst Ivaine)	Date Received (yyyy/mm/dd)  OCT 1 5 2007	Date of Inspection (yyyy/mm/dd)
Well Technician's Licence No. Signature of Technician	Date Submitted (yyyy/mm/dd)	Remarks	
asses (4/2000)	0007-10-10		
0506E (11/2006)	Ministry's Copy		© Queen's Printer for Ontario, 2006



Measurements recorded in:

Well Owner's Information

Ministry of the Environment

Metric Imperial

Last Name / Organization

Well Tag No. (Place Sticker and/or Print Below)

Well Record

A076883

A076883

E-mail Address

n 903 Ontario Water Resources Act

Page\_

First Name		Last Name /	Organization Star Ho				E-mail Ad	ldress				*****	Constructed ell Owner
Mailing Address (	Street Number/N		otar no	N	funicipality Stittsv	ille	Province Ontar		Postal Code KI2S 1A6				. area code)
Well Location				1			7-1-0-2-				<u> </u>		
	ocation (Street N	,		<b>I</b>	ownship	mloton		L	.ot 10		Concession	on 3	
245 West County/District/M	Lake Circ	re			West Ca				10	Provin	ice		Il Code
Ottawa C	arleton			<b>I</b>	Carp					Ont	ario		
UTM Coordinates	1 1 -		orthing		funicipal Pla	n and Sublo	ot Number			Other			
NAD   8   3	1   8    4217 d Bedrock Mate		501804		rd (see instn	ictions on the	back of this form	n)		2800 (325) 8		331.000.000	
General Colour	İ	ımon Material			er Materials		, <del></del>		Description	W. C.	200000000000000000000000000000000000000	De <sub>l</sub> From	oth ( <i>m/ft)</i> To
Brown	Hardpa	n	İ	Boul	ders	***************************************						0	2.43
Gray	Limest						Laver	ed & S	oft			2.43	6.09
Gray	Limest						Mediu					6.09	49.37
GLay	Lunest	OHE					110010					· · · · · · · · · · · · · · · · · · ·	
												***************************************	
									***************************************	,moras manus (1170)			
										***************************************			
		Annular	Space					Re	sults of We	ell Yiel	d Testing	ı	
Depth Set at (n From   T	n/ft)	Type of Sea (Material an	lant Used	******		Placed	After test of we	ell yield, wa	ter was:		aw Down	F	Recovery
		***************************************			.31n		Other, sp			(min)	Water Lev (m/ft)	et Time (min)	Water Level (m/ft)
7.31 0	Groute	d Cement	а веш	conrce	.311		If pumping dis	continued,	give reason:	Static Level	4.89		
										1	5.55	1	5.27
						***************************************	Pump intake		)	2	5.79	2	5.06
							Pumping rate	2.85	14.43	3	1	3	
	of Construction	. 6		_Well Us				4.6	ivi)	4	5.89	4	4.98
	☐ Diamoi ntional) ☐ Jetting	□ Do	mestic	☐ Commer ☐ Municipa		Not used Dewatering	Duration of p			5	5.96	5	4.93
☐ Rotary (Revers ☐ Boring	e) <b>Air</b> ☐ Driving ☐ Digging			☐ Test Hol	le 🔲 & Air Conditio	Monitoring	2 hrs + Final water lev				5.97		4.90
X Air percussion		☐ Ind	ustrial	ccoming	a 7 iii oonanie	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	1	5.23		10	6.07	10	
Other, specify_	201 - 1000-1000 - 1000-1000-1000-1000-10		er, specify_	1.074950085274710390	II alkala o par paran		If flowing give	rate (I/min	/ GPM)	15	6.10	15	
Inside Ope	Construction of Hole OR Material	Wall		( <i>m/ft</i> )	X Water S	of Well Supply	Recommende	ed pump de	epth (m/ft)	20	6.12	20	
Diameter (Gal (cm/in) Con	lvanized, Fibreglass, crete, Plastic, Steel)	Thickness (cm/in)	From	То	Replace		22	2.85		25	6.13	25	
15.86	Steel	.48	+.45	7.31	Recharg	ge Well	Recommende (I/min / GPM)	ed pump ra	ite	30	6.14	30	
			-		☐ Dewate ☐ Observa	_	Well production	5.5	2 (PAA)	40	6.17	40	
					Monitori	ng Hole	vveii productio	un (piimii) (	31 IVIJ	50	6.22	50	
		-			(Constri	uction)	Disinfected?	No		60	6.23	60	
	Construction	Pecord - Scre	en		Insuffici	ent Supply	GA 100 L		Map of W	ell l'or	**************************************		
Outside	Material		t	. ( <i>m/ft</i> )	☐ Abando Water C		Please provide	e a map be				back.	
Diameter (cm/in) (Piasi	tic, Galvanized, Stee	) Slot No.	From	То	│		- MAR SANGET STATE AND STATE AND ADDRESS.	MCKE	E 513	E l	as		
							7					1 111 111111	
					Other, s	specity							
	Water D				ole Diamet		/'						
	Pepth Kind of Wat Gas ☐ Other, <i>s</i>		Untested	Dept From	th ( <i>m/ft)</i> To	Diameter (cm/in)							
Water found at D	epth Kind of Wat	er: ☐Fresh	Untested	0	7.31	15.86				1257	-Lake	Ca	· _
49.07 <sub>m/ft)</sub> [	]Gas ☐ Other, <i>s</i>	ecify		7.31	49.37	15.23			l		Jak	- 1	LE
	epth Kind of Wat		Untested		1.2.07				1	6		1	
(111114)	Well Contrac		Technicia	n Informat	tion				l L		245 + 26	ļ	
Business Name o	f Well Contractor		<u> </u>	We	ll Contractor's				i	<u>L</u> 07 7	726	i	
-	later Suppl s (Street Number/N	-		1 Mu	.   5   nicipality	5   8	Comments:		<del></del>			vm	· · · · · · · · · · · · · · · · · · ·
Box 490	- /			1	Stittsvi	ille							
Province	Postal Code		E-mail Add				Well owner's	Date D	kage Delivere		788888 <b>98</b>	2422445	2/ <b>0</b> 21/28888
Ontario Bus.Telephone No	K2S 1A6				rater.ca First Name)	1	information package			- 1	Audit No	stry Us	pero resolvici, komigranice
613 836 1	766	Miller,	Steph	en			delivered	Z   0   0   Date Wor	9 1 0 k Completed	0 9	<sub> </sub> Z	LU.	1735
Well Technician's Li 0   0   9	cence No. Signatur		n and/or Co	,	le Submitted 0  0  9  1	مام امام	X Yes ☐ No	4	9  1  0	- 1	. FF	B 1 (	3 2010
0 0 9	I GAV	ypur-	-4	Z	פן טן ט	101019		KI N N	7  E  U	U   22	received	. D	

093679 Ministry of Well Record the Environment Regulation 903 Ontario Water Resources Act mperial Page of le Circle Province Postal Code Ontario Other Municipal Plan and Sublot Number NAD | 8 | 3 | 8 4M Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form) Depth (m(ft) Other Materials General Description From 9 01 Results of Well Yield Testing Annular Space Depth Set at (n(ft) After test of well yield, water was Volume Placed Recovery (Material and Type) (meft3) Time Water Level Time Water Level (min) (m/lt) (m/ft) Static Level L(') If pumping discontinued, give reason Pump intake set at (n/ft) 168" 3 Pumping rate (I/min GPM) Method of Construction Well Use Public Commercial ☐ Not used Rotary (Conventional) Domestic Jetting ☐ Municipal Dewatering 1118 hrs + min Rotary (Reverse) Driving Livestock Test Hole ☐ Monitoring Boring Digging ☐ Imigation Cooling & Air Conditioning Final water level end of pumping (m/ft) 10 Air percussion 56 Industrial Other, specify Other, specify 15 f flowing give rate (Vmin / GPM) Construction Record - Casing Status of Well 3'4" 20 Open Hole OR Material (Galvanized, Fibreglass Depth (m/ft) Water Supply
Replacement Well Wall Recommended pump depth (m/ft) Thickness 54-6" 25 100 To (cm/in) Concrete, Plastic, Steel) (cm/in) ☐ Test Hole C inded pump rate 188" 30 Recharge Well (GPM) Dewatering Well 40 Observation and/or Well production (Vmin GPM)
Disinfected? Monitoring Hole 50 5'8" Alteration (Construction) Pes No 60 Abandoned, Insufficient Supply Construction Record - Screen Map of Well Location Abandoned, Poor Please provide a map below following instructions on the back Outside Depth (m/ft) Water Quality Material Slot No (Plastic, Galvanized, Steel) Abandoned, other, From specify Other, specify Water Details Hole Diameter Depth (m/ft) Water found at Depth Kind of Water: Fresh Untested Diameter 52(n(tt)) Gas Other, specify To ( u Water, found at Depth Kind of Water: ☐ Fresh ☐ tested ☐ Other, specify 6 Vater found at Depth Kind of Water: Fresh Untested (m/ft) Gas Other, specify Well Contractor and Well Technician Information Well Contractor's Licence No. ess (Street Number/Name) ) () ( Comments: Etmond ostal Code Business E-mail Address ROAD 70 Well owner information Date Package Delivered Ministry Use Only Nechnician (Last Name, First Name) 010000 package 08236 10 Kathan delivered Yes Yes MAR 2 2 2010 00031 No 20100201 0506E (12/2007) Queen's Printer for Ontario, 2007 Ministry's Copy

A105394 Well Tay IVO. Well Record elow) Ministry of Regulation 903 Ontario Water Resources Act the Environment Metric | Imperial Page Measurements recorded in: of Well Location (Street Number/Name) Ontario Municipal Plan and NAD | 8 | 3 2029454 Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form) General Colour Other Materials General Description a Caravel ( Annular Space Results of Well Yield Testing Type of Sealant Used (Material and Type) Volume Placed After test of well yield, water was Depth Set at (pa/ft) Draw Down Recovery Time Water Level (m/ft) (m/ft) Static Level 162 11184 ation of pumping Method of Construction Well Use Diamond ■ Not used Cable Tool Public Commercial Domestic Rotary (Conventional) Jetting Municipal Dewatering hrs + O min Rotary (Reverse) Driving Livestock Test Hole ■ Monitoring ☐ Digging Boring ☐ Irrigation Cooling & Air Conditioning Final water level end of pumping (m/ft, wing give rate (I/min / GPM) Air percussion Industrial Other, specify Other, specify Construction Record - Casing Status of Well Open Hole OR Material (Galvanized, Fibreglass, Concrete, Plastic, Steel) mended pump depth (neft) Depth (met) Inside Wall Water Supply Replacement Well To Test Hole Recharge Well 28 -188 Dewatering Well 160 Observation and/or 120 Well production (Vm min (GPM) Monitoring Hole 50 Alteration (Construction) XYes No 60 Abandoned, Insufficient Supply Construction Record - Screen Map of Well Loy Abandoned, Poor Outside Please provide a map below following Depth (m/ft) Water Quality (Plastic, Galvanized, Steel) Abandoned, other, From (cm/in) specify 3KM Other, specify Water Details Water found at Depth Kind of Water: Fresh Watested Depth (m) Gas Other, specify found at Depth Kind of Water: Fresh Untested (m/ft) Gas Other, specify Water found at Depth Kind of Water: Fresh Untested (m/ft) Gas Other, specify Well Contractor and Well Technician Information Municipality Comments: 1CHMON Business E-mail Address Well owner's information package Ministry Use Only Well Technician (Last Name, First Name) 201001703 Ministry's Copy

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the Environment on 903 Ontario Water Resources Act A102298 A102298 Measurements recorded in: X Metric Imperial Page of Address of Well Location (Street Number/Name) Township Concession Lot 5 West Lake Estates West Carleton-Huntley 10 County/District/Municipality City/Town/Village Postal Code Ottawa Carleton Carp Ontario UTM Coordinates Zone Easting Northing Municipal Plan and Sublot Number Other NAD | 8 | 3 1 8 | 421718 | 5018158 Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form) Depth (m/ft) General Colour Most Common Material Other Materials General Description From 0 .60 Brown Soil. Brown Shale. Soft .60 5.48 Grey 70.40 Limestone Brown Layers Medium Soft 5.48 Annular Space Results of Well Yield Testing After test of well yield, water was: Depth Set at (m/ft) Type of Sealant Used Volume Placed Draw Down Recovery Clear and sand free Other, specify (Material and Type) (m3/ft3) Time Water Level Time Water Level .21m<sup>3</sup> (min) (m/ft) (m/ft) (min) 8.83 0 Grouted Cement Slurry Static If pumping discontinued, give reason: 6.38 Level 6.65 1 1 7.03 Pump intake set at (m/ft) 2 2 6.41 7.14 18.28 3 6.38 Pumping rate (I/min / GPM) 7.18 3 Method of Construction Well Use 45.5 Cable Tool 4 Diamond Public 7.19 4 Commercial ☐ Not used Duration of pumping X Domestic Rotary (Conventional) Jettina Municipal Dewatering 5 5 Driving 7.20 2 hrs + min X Rotary (Reverser Livestock Test Hole Monitoring Boring Final water level end of pumping (m/ft) Digging Irrigation Cooling & Air Conditioning 10 7.22 10 X Air percussion Industrial 7.46 Other, specify 15 7.26 15 If flowing give rate (I/min / GPM) Construction Record - Casing Status of Well 20 20 7.32 Open Hole OR Material Depth (m/ft) Wall X Water Supply Recommended pump depth (m/ft) (Galvanized, Fibreglass, Concrete, Plastic, Steel) Thickness From Replacement Well 18.28 25 7.40 25 To (cm/in) Test Hole Recommended pump rate (Vmin / GPM) 45.5 15.86 Recharge Well 30 30 +.45 8.83 Stee1 .48 7.45 Dewatering Well 40 40 Observation and/or Monitoring Hole Well production (I/min / GPM) 50 7.48 50 Alteration Disinfected? (Construction) 7.47 60 60 X Yes No Abandoned, Insufficient Supply Construction Record - Screen Map of Well Location Abandoned, Poor Outside Depth (m/ft) Water Quality Please provide a map below following instructions on the back Material (Plastic, Galvanized, Steel) Diamete (cm/in) Abandoned, other, From specify WEST LAKE ESTATES Other, specify Water Details Hole Diameter Water found at Depth Kind of Water: Fresh X Untested Diamete (cm/in) Depth (m/ft) From 70.10 m/h Gas Other, specify To LOT#5 0 8.83 Water found at Depth Kind of Water: Fresh Untested 15.86 (m/ft) Gas Other, specify 8.83 70.40 15.55 Water found at Depth Kind of Water: Fresh Untested (m/ft) Gas Other, specify Well Contractor and Well Technician Information Business Name of Well Contractor Well Contractor's Licence No. Capital Water Supply Ltd. 1 | 5 | 5 | 8 Business Address (Street Number/Name) Municipality Comments Box 490 Stittsville Province Postal Code Business E-mail Address office@capitalwater.ca K2S | 1A6 | Well owner's information Ontario Date Package Delivered Ministry Use Only Bus.Telephone No. (inc. area code) Name of Well Technician (Last Name, First Name) Audit No. 2 0 1 0 0 17 2 6 
 613 836 1766 | Miller, Stephen

 Well Technician's Licence No. Signature of echnician and/or Contractor Date Submitted

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Well Record

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asurements recorded in: X Metric | Imperial Well Owner's Information Last Name / Organization E-mail Address ☐ Well Constructed by Well Owner Shell Star Holdings Municipality Telephone No. (inc. area code) Mailing Address (Street Number/Name) Province Postal Code P.O. Box 569 Stittsville Ontario K2\$ 1A6 613 831 9041 Well Location Address of Well Location (Street Number/Name) Township Lot Concession Lot 30 West Lake Estates West Carleton - Huntley 10 Postal Code County/District/Municipality City/Town/Village Ottawa Carleton Carp Ontario UTM Coordinates Zone Easting Northing Municipal Plan and Sublot Number 421995 5017833 NAD 8 3 1 8 Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form) Depth (m/ft) General Colour Most Common Material General Description From 0 7.31 Brown Soil Large Boulders Grey Limestone Dark Layers Medium 7.31 83.20 Annular Space Results of Well Yield Testing After test of well yield, water was: Volume Placed Draw Down Recovery Depth Set at (m/ft) Type of Sealant Used (Material and Type)  $(m^2/\Pi^3)$ X Clear and sand free Time Water Level Water Level .548m<sup>3</sup> Other, specify (min) (m/ft) (m/ft) 10.36 0 Grouted Bentonite Slurry Statio If pumping discontinued, give reason: 4.14 Level 38.65 1 6.40 1 Pump intake set at (m/ft) 2 8.53 37.60 45.71 3 36.17 Pumping rate (I/min / GPM) Well Use Method of Construction 36.40 4 10.42 4 34.60 Cable Tool
Rotary (ConvMudhal) Diamond Public Commercial ☐ Not used Duration of pumping X Domestic Municipal Jettina Dewatering 1 hrs + 5 12.40 33.15 min ☐ Monitoring Rotary (Reverse) Driving Livestock Test Hole Cooling & Air Conditioning Final water level end of pumping (m/ft) Boring Digging Irrigation 16.50 10 10 26.60 Air percussion Industrial 41.0 Other, specify Other, specify 15 20.08 15 If flowing give rate (Vmin / GPM) 20.49 Construction Record - Casing Status of Well 20 22.20 20 17.30 Open Hole OR Material X Water Supply Recommended pump depth (m/ft) Wall (Galvanized, Fibreglass, Concrete, Plastic, Steel) Replacement Well 25 16.26 From 45.71 25.13 25 (cm/in) Test Hole Recommended pump rate Recharge Well 28.85 30 12.46 15.86 Stee1 .48 +.45 10.36 Dewatering Well 36.40 40 9.91 40 32.95 Observation and/or Well production (I/min / GPM) Monitoring Hole Alteration (Construction) 50 36.77 50 6.43 Disinfected? 60 41. 60 4.40 X Yes No Abandoned, Insufficient Supply Map of Well Location Construction Record - Screen Abandoned, Poor Depth (m/ft) Water Quality Please provide a map below following instructions on the back Diamete (cm/in) Abandoned, other, From specify WEST LAKE ESTATES 1 Other, specify Water Details Hole Diameter Water found at Depth Kind of Water: Fresh X Untested Depth (m/ft) Diameter 33.52(m/ft) Gas Other, specify 0 10.36 15.86 Water found at Depth Kind of Water: Fresh X Untested 6 79.24(m/ft) Gas Other, specify 10.36 83.20 15.39 Water found at Depth Kind of Water: Fresh Untested (m/ft) Gas Other, specify Well Contractor and Well Technician Information Business Name of Well Contractor Well Contractor's Licence No Capital Water Supply Ltd. 1 | 5 | 5 | 8 Business Address (Street Number/Name) Municipality Comments: Box 490 Stittsville Province Postal Code Business E-mail Address office@ capitalwater.ca Well owner's information Date Package Delivered Ministry Use Only Ontario K2S 1A6 Bus.Telephone No. (inc. area code) Name of Well Technician (Last Name, First Name) 201011111 package 5651 Miller, Stephen 613 886 1766 delivered  $z \perp$ Date Work Completed X Yes Well Technician's Licence No. Signature Technician and/or Contractor Date Submitted 0 0 9 201011115 2010110 7

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			nment Sealing	g Reco	rd (see instructions on the b	eack of this form)	Robbies	Mill		Don	tle (ma/fill)
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Air percu	ussion	☐ Inde	ustrial					0.080		2 15	
Other, s <sub>i</sub>			er, specify		Chatra of Wall	If flowing give rate (l	min / GPM)	15		15	
Inside	Construction Open Hole OR Material	Wall	Depth (m	/ft)	Status of Well Water Supply	Recommended pur	p depth (m/ft)	20		20	
Diameter (cm/in)	(Galvanized, Fibreglass, Concrete, Plastic, Steel)	Thickness (cm/in)	From	То	Replacement Well			25		25	
					☐ Test Hole . ☐ Recharge Well	Recommended puri	p rate	30		30	
1 1 1 1 1 1 1 1					Dewatering Well			40		40	
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0.44	Construction	Record - Scre			Abandoned, Poor	Please provide a maj	Map of W			ook	
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Box 49	Address (Street Number/	Name)		1 1	nicipality	Comments:					
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Ministry of the Environment Well Tag No. (Place Sticker and/or Print Below)

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Well Record

in 903 Ontario Water Resources Act

Page Imperial Measurements recorded in: X Metric Well Owner's Information ☐ Well Constructed E-mail Address Last Name / Organization First Name by Well Owner T. Goddard Construction Postal Code Telephone No. (inc. area code) Province Mailing Address (Street Number/Name) Municipality Carp Ontario KOA 1LO 613 227 7870 335 West Lake Circle Well Location Address of Well Location (Street Number/Name) Township West Carleton - Huntley Lot 29 West Lake Estates Postal Code Province City/Town/Village County/District/Municipality Ontario Ottawa Carleton Carp Municipal Plan and Sublot Number Other 5017894 Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form) Depth (m/ft) General Description Most Common Material Other Materials General Colour From 0 5.48 Large Boulders Brown Soil Grey 5.48 83.20 Limestone Dark Layers Results of Well Yield Testing Annular Space Draw Down After test of well yield, water was: Recovery Type of Sealant Used (Material and Type) Volume Placed Depth Set at (m/ft)  $(m^3/ft^3)$ Time Water Level Time Water Level X Clear and sand free (min) (m/ft) (min) (m/ft) Other, specify .46m<sup>3</sup> 0 Grouted Bentonite Slurry 8.53 Static If pumping discontinued, give reason: 3.65 Level 5.04 4.74 Pump intake set at (m/ft) 2 4.29 5.13 76.19 3 3 Pumping rate (I/min / GPM) 5.38 3.98 Method of Construction Well Use 45.5 5.56 3.87 Diamond
Jetting ☐ Commercial ☐ Municipal ☐ Not used ☐ Dewatering Cable Tool Public Duration of pumping X Domestic Rotary (Conventional) 1 hrs + 5 min 5.68 3.82 Livestock ☐ Monitoring Test Hole Rotary (Reverse) Driving ☐ Irrigation Final water level end of pumping (m/ft) Boring Digging Cooling & Air Conditioning 10 10 5.96 3.76 Industrial
Other, specify Air percussion 6.79 Other, specify 15 6.02 3.71 If flowing give rate (I/min / GPM) Construction Record - Casing Status of Well 20 20 3.68 Depth (m/ft) Water Supply Open Hole OR Material Recommended pump depth (m/ft) Inside N/Vall (Galvanized, Fibreglass, Concrete, Plastic, Steel) Diamete (cm/in) Thicknes (cm/in) Replaceme Replacement Well 25 22.85 From To 6.03 Recommended pump rate 30 Recharge Well 6.42 (I/min / GPM) 15.86 Steel 48 +.45 8.53 45.5 Dewatering Well 40 40 6.76 Observation and/or Monitoring Hole Well production (I/min / GPM) 50 6.78 Alteration Disinfected? (Construction) 60 X Yes No 6.79 Abandoned, Insufficient Supply Map of Well Location Construction Record - Screen Abandoned, Poor Please provide a map below following instructions on the back. Water Quality Depth (m/ft) Material (Plastic, Galvanized, Steel) Slot No. Abandoned, other, WEST LAKE (cm/in) specify M ESTATES LOT#29 Other, specify Water Details Hole Diameter Depth (m/ft) Water found at Depth Kind of Water; Fresh X Untested From 57.90(m/ft) Gas Other, specify Water found at Depth Kind of Water: Fresh X Untested 15.86 0 8.53 82.29(m/ft) Gas Other, specify 8.53 83.20 Water found at Depth Kind of Water: Fresh Untested (m/ft) Gas Other, specify Well Contractor and Well Technician Information Business Name of Well Contractor Well Contractor's Licence No. 1 | 5 | Capital Water Supply Ltd. 5 8 Comments: Business Address (Street Number/Name) Municipality Box 490 Stittsville Business E-mail Address Province Postal Code K2S 1A6 Well owner's information office @ capitalwater.ca Date Package Delivered Ministry Use Only Bus.Telephone No. (inc. area code) Name of Well Technician (Last Name, First Name) package 2 0 1 1 0 6 1 7 15728 613 836 1766 Miller, Stephen delivered Date Work Completed Well Technician's Licence No. Sign X Yes Technician and/or contractor Date Submitted NOV 0 2 2011 0 0 9 7 20110617 No 20110617



Ministry of the Environment

Well Tag No. (Place Sticker and/or Print Below)

Well Record

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Measurements recorded in:	Metric Imperial				4113020			Page	6000 50000	of
Well Owner's Informatio					E 1 A					
First Name	Last Name / Organizatio She11 Star Ho				E-mail Address					Constructed II Owner
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NAD   8   3   1   8   42 Overburden and Bedrock M		1 1 1	rd (see instructions on the	back	of this form)					1100
	Common Material		er Materials			al Description		-	-rom	th ( <i>m/ft)</i> To
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	Annular Space					Results of W				
Depth Set at (m/ft)	Type of Sealant Used	<sub>ga m</sub> ana ma desakana (1966 e 1968)	Volume Placed (m³/ft³)		er test of well yield, v		11	aw Down Water Level		ecovery Water Level
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				$\  \ $			1	8.30	1	9.50
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					60.95 Imping rate (I/min / 0	GPM)	3	9.50	3	8.00
Method of Construct		Well Us			36.40	GI WIY	4	9.81	4	7.59
☐ Cable Tool ☐ Di A Rotary (Conventional) ☐ Je	amond Public  Atting Domestic	☐ Comme	,	Di	uration of pumping	_1	5	10.10	5	7.20
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Other, specify	Other, specify			J If f	lowing give rate (I/n	nin / GPM)	15	11.36	15	6.59
	ion Record - Casing terial Wall Dep	th ( <i>m/ft</i> )	Status of Well  Water Supply	H <sub>R</sub>	ecommended pump	depth (m/ft)	20	11.54	20	
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15.86 Stee1	.40	1	Dewatering Well	11	min / GPM) 36 <b>.</b> 40	(0010)	40		40	
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	tion Record - Screen	oth ( <i>m/ft</i> )	Abandoned, Poor Water Quality	PI	ease provide a map				ack.	
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			Other, specify		WEST LAKE		a 14	b/		
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(m/ft) ☐ Gas ☐ Oth	er, specify	_		_		JE57 LP,	2	PREZE \		,
Well Cor Business Name of Well Contra	ntractor and Well Technic	ian Informa	ition 'ell Contractor's Licence No.							/
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Tag#: A137237 Well Record Ministry of the Environment Regulation 903 Ontario Water Resources Act H137237 Metric Imperial Page easurements recorded in: Well Owner's Information Last Name / Organization E-mail Address First Name Thomas Cayanash Construction ccollins whomas coward by Well Owner
Province Postal Code Telephorle No. (inc. area code) Mailing Address (Street Number/Name) 9094 Cavanagh KOA1BO6132572918 Well Location Address of Well Location (Street Number/Name) Concession West Lake Circle 305 Carleton - North 28 County/District/Municipality Province Postal Code Carleton Ontario Municipal Plan and Sublot Number Northing NAD 8 3 1 5 4 2 1 9 41 4m1316 50119412 Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form) Depth (m/ft) Most Common Material General Colour General Description From till, sand, gravela boulders 5.66 was the only well drilled It was tagged. **Annular Space** Results of Well Yield Testing Type of Sealant Used Depth Set at (m/ft) After test of well yield, water was Volume Placed Draw Down Recovery From Time Water Level (Material and Type)  $(m^3/ft^3)$ Clear and sand free Time Water Level Other, specify (min) (m/ft) (m/ft) (min, 2-31 hole plug Static If pumping discontinued, give reason: Level 1 1 Pump intake set at (m/ft) 2 2 3 Pumping rate (Ilmin / GPM) Method of Construction Well Use Cable Tool ☐ Diamond Public Commercial ☐ Not used Duration of pumping Municipal
Sest Hole Rotary (Conventional) ☐ Jetting Domestic ☐ Dewatering 5 5 hrs + min Rotary (Reverse) Livestock ☐ Monitoring Boring □ Digging Irrigation Cooling & Air Conditioning Final water level end of pumping (m/ft) 10 10 Air percussion
Other, specify HS Auger ☐ Industrial Other, specify 15 15 If flowing give rate (Ilmin / GPM) Construction Record - Casing Status of Well 20 20 Open Hole OR Material (Galvanized, Fibreglass, Concrete, Plastic, Steel) Inside Wall Depth (m/ft) Water Supply Recommended pump depth (m/ft) Replacement Well (cm/in) From 25 25 (cm/in) ☐ Test Hole Recommended pump rate Recharge Well 30 plastic 0.4 2.62 (l/min / GPM) Dewatering Well 40 40 Observation and/or Well production (Ilmin / GPM) Monitoring Hole 50 50 ☐ Alteration (Construction) Abandoned, Insufficient Supply Yes No Construction Record - Screen Abandoned, Poor Water Quality Map of Well Location Outside Depth (m/ft) Please provide a map below following instructions on the back. Material Diameter Slot No. (Plastic, Galvanized, Steel) Abandoned, other, (cm/in) From specify 6.0 2.62 5.66 plashe Other, specify Water Details Hole Diameter Water found at Depth Kind of Water: Fresh Untested Depth (m/ft) Diameter Tite plan and area 1.02 (m/ft) Gas Other, specify Nater found at Depth Kind of Water: Fresh Untested 0 1.37 map are enclosed. 22 
 (m/ft)
 ☐ Gas
 ☐ Other, specify

 Vater found at Depth
 Kind of Water:
 ☐ Fresh
 ☐ Untested
 5.66 Other, specify Well Contractor and Well Technician Information usiness Name of Well Contractor Well Contractor's Licence No OGS INC 6964 usiness Address (Street Number/Name) Comments 5518 of Wal Tachnidan (Last Name First Name) Well owner's information Date Package Delivered Ministry Use Only 66 Strude Tasa Name, Fi package delivered dalmim vivivi Z 163946 Date Work Completed Yes OH 6- tous 2013 6 1 47 \_\_ No 90130108 eddu 19 2012 © Queen's Printer for Ontario, 2007 Ministry's Copy



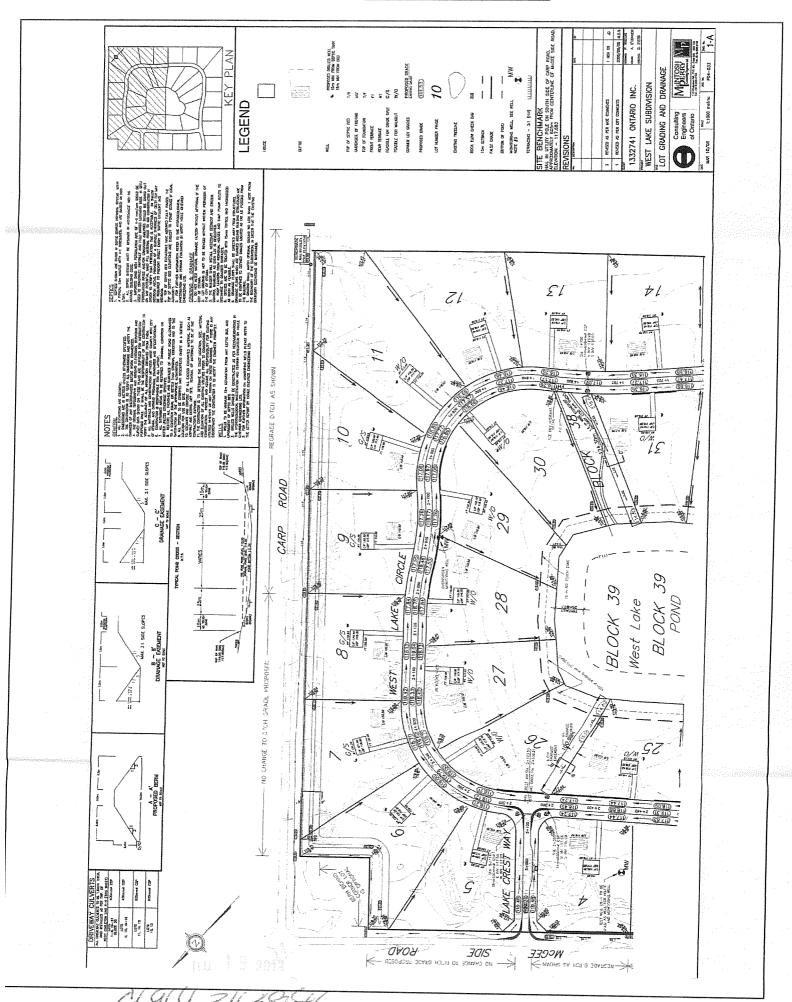
# Well Record for Well Cluster - Part 3 of 3 Detailed Drawing of All Well Locations

**Note**: This **Well Record for Well Cluster Part 3 - Detailed Drawing of all Well Locations**, must be attached to Parts 1 and 2. The drawing must include all property boundaries, an arrow indicating the North direction, all named roads and sufficient measurements to locate all wells in the cluster in relation to fixed points. The drawing must show the location of each well and each well must be numbered on the drawing to match number used for that well on the **Well Record for Well Cluster Parts 1 and 2**. The well with the well tag must be clearly identified on the Drawing.

UTM coordinates should appear beside each well, if space permits. Additional comments on wells can be included on the drawing

Well Tag Number: # A\37 237

"Well Record for Well Cluster" Form Audit Number: # \_ そ 1 し 3 9 寸 し





Client: Paterson Group

154 Colonnade Rd. South

Nepean, ON K2E 7T7

Mr. Oliver Blume

PO#:

Attention:

Invoice to: Paterson Group

 Report Number:
 1973843

 Date Submitted:
 2022-03-23

 Date Reported:
 2022-03-30

 Project:
 PH4484

 COC #:
 887701

#### **Dear Oliver Blume:**

Please find attached the analytical results for your samples. If you have any questions regarding this report, please do not hesitate to call (613-727-5692).

Page 1 of 14

Report Comments:

APPROVAL:

Addrine Thomas, Inorganics Supervisor

Addrine Thomas

All analysis is completed at Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) unless otherwise indicated.

Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) is accredited by CALA, Canadian Association for Laboratory Accreditation to ISO/IEC 17025 for tests which appear on the scope of accreditation. The scope is available at: <a href="http://www.cala.ca/scopes/2602.pdf">http://www.cala.ca/scopes/2602.pdf</a>.

Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) is licensed by the Ontario Ministry of the Environment, Conservation, and Parks (MECP) for specific tests in drinking water (license #2318). A copy of the license is available upon request.

Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) is accredited by the Ontario Ministry of Agriculture, Food, and Rural Affairs for specific tests in agricultural soils.

Please note: Field data, where presented on the report, has been provided by the client and is presented for informational purposes only. Guideline values listed on this report are provided for ease of use (informational purposes) only. Eurofins recommends consulting the official provincial or federal guideline as required. Unless otherwise stated, measurement uncertainty is not taken into account when determining guideline or regulatory exceedances.



**Environment Testing** 

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154 Colonnade Rd. South

Nepean, ON K2E 7T7

Attention: Mr. Oliver Blume

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 Project:
 PH4484

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Group	Analyte	MRL	Units	Lab I.D. Sample Matrix Sample Type Sampling Date Sample I.D.  Guideline	1615821 GW 2022-03-22 GW1	1615822 GW 2022-03-22 GW2
Anions	Cl	1 1	mg/L	AO 250	135	142
7(110113	F	0.10	mg/L	MAC 1.5	<0.10	<0.10
	N-NO2	0.10	mg/L	MAC 1.0	<0.10	<0.10
	N-NO3	0.10	mg/L	MAC 10.0	3.15	3.02
	SO4	1	mg/L	AO 500	182	175
General Chemistry	Alkalinity as CaCO3	5	mg/L	OG 30-500	251	243
	Colour (Apparent)	2	TCU	AO 5	<2	<2
	Conductivity	5	uS/cm		1180	1180
	DOC	0.5	mg/L	AO 5	2.4	2.4
	Hq	1.00		6.5-8.5	7.95	7.93
	Phenols	0.001	mg/L		<0.001	<0.001
	S2-	0.01	mg/L	AO 0.05	<0.01	<0.01
	TDS (COND - CALC)	1	mg/L	AO 500	767*	767*
	Turbidity	0.1	NTU	AO 5	0.5	0.5
Hardness	Hardness as CaCO3	1	mg/L	OG 80-100	454*	451*
Indices/Calc	Ion Balance	0.01			0.97	0.97
Mercury	Hg	0.0001	mg/L	MAC 0.001	<0.0001	<0.0001
Metals	Ag	0.0001	mg/L		<0.0001	<0.0001
	Al	0.01	mg/L	OG 0.1	<0.01	<0.01
	As	0.001	mg/L	IMAC 0.01	<0.001	<0.001
	В	0.01	mg/L	IMAC 5.0	0.04	0.04
	Ва	0.01	mg/L	MAC 1.0	0.12	0.12
	Be	0.0005	mg/L		<0.0005	<0.0005
	Ca	1	mg/L		162	161
	Cd	0.0001	mg/L	MAC 0.005	<0.0001	<0.0001

#### Guideline = ODWSOG

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**Environment Testing** 

Client: Paterson Group

154 Colonnade Rd. South

Nepean, ON K2E 7T7

Attention: Mr. Oliver Blume

PO#:

Invoice to: Paterson Group

Report Number: 1973843
Date Submitted: 2022-03-23
Date Reported: 2022-03-30
Project: PH4484
COC #: 887701

				Lab I.D. Sample Matrix Sample Type Sampling Date Sample I.D.	1615821 GW 2022-03-22 GW1	1615822 GW 2022-03-22 GW2
Group	Analyte	MRL	Units	Guideline		
Metals	Со	0.0002	mg/L		<0.0002	<0.0002
	Cr	0.001	mg/L	MAC 0.05	<0.001	<0.001
	Cu	0.001	mg/L	AO 1	<0.001	<0.001
	Fe	0.03	mg/L	AO 0.3	<0.03	<0.03
	К	1	mg/L		2	2
	Mg	1	mg/L		12	12
	Mn	0.01	mg/L	AO 0.05	<0.01	<0.01
	Мо	0.005	mg/L		<0.005	<0.005
	Na	1	mg/L	AO 200	77	75
	Ni	0.005	mg/L		<0.005	<0.005
	Pb	0.001	mg/L	MAC 0.010	<0.001	<0.001
	Sb	0.0005	mg/L	IMAC 0.006	<0.0005	<0.0005
	Se	0.001	mg/L	MAC 0.05	<0.001	<0.001
	Sr	0.001	mg/L		0.879	0.876
	TI	0.0001	mg/L		<0.0001	<0.0001
	U	0.001	mg/L	MAC 0.02	<0.001	<0.001
	V	0.001	mg/L		<0.001	<0.001
	Zn	0.01	mg/L	AO 5	<0.01	<0.01
Microbiology	Escherichia Coli	0	ct/100mL	MAC 0	0	0
	Total Coliforms	0	ct/100mL	MAC 0	19*	23*
Nutrients	N-NH3	0.010	mg/L		<0.010	<0.010
	Total Kjeldahl Nitrogen	0.100	mg/L		0,252	0.477
Subcontract	Tannin & Lignin	1	mg/L			1
	-	1.0	mg/L		1.0	
/OCs Surrogates	1,2-dichloroethane-d4	0	%		100	119

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154 Colonnade Rd. South

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Attention: Mr. Oliver Blume

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Invoice to: Paterson Group

Report Number: 1973843
Date Submitted: 2022-03-23
Date Reported: 2022-03-30
Project: PH4484
COC #: 887701

Group	Analyte	MRL	Units	Lab I.D. Sample Matrix Sample Type Sampling Date Sample I.D.  Guideline	1615821 GW 2022-03-22 GW1	1615822 GW 2022-03-22 GW2
VOCs Surrogates	4-bromofluorobenzene	0	%		71	76
	Toluene-d8	0	%		91	98
Volatiles	1,1,1,2-tetrachloroethane	0.5	ug/L		<0.5	<0.5
	1,1,1-trichloroethane	0.4	ug/L		<0.4	<0.4
	1,1,2,2-tetrachloroethane	0.5	ug/L		<0.5	<0.5
	1,1,2-trichloroethane	0.4	ug/L		<0.4	<0.4
	1,1-dichloroethane	0.4	ug/L		<0.4	<0.4
	1,1-dichloroethylene	0.5	ug/L	MAC 14	<0.5	<0.5
	1,2-dichlorobenzene	0.4	ug/L	MAC 200	<0.4	<0.4
	1,2-dichloroethane	0.2	ug/L	IMAC 5	<0.2	<0.2
	1,2-dichloropropane	0.5	ug/L		<0.5	<0.5
	1,3,5-trimethylbenzene	0.3	ug/L		<0.3	<0.3
	1,3-dichlorobenzene	0.4	ug/L		<0.4	<0.4
	1,3-Dichloropropylene (cis+trans)	0.3	ug/L		<0.3	<0.3
	1,4-dichlorobenzene	0.4	ug/L	MAC 5	<0.4	<0.4
	Acetone	30	ug/L		<30	<30
	Benzene	0.5	ug/L	MAC 1	<0.5	<0.5
	Bromodichloromethane	0.3	ug/L		<0.3	<0.3
	Bromoform	0.4	ug/L		<0.4	<0.4
	Bromomethane	0.5	ug/L		<0.5	<0.5
	c-1,2-Dichloroethylene	0.4	ug/L		<0.4	<0.4
	c-1,3-Dichloropropylene	0.2	ug/L		<0.2	<0.2
	Carbon Tetrachloride	0.2	ug/L	MAC 2	<0.2	<0.2
	Chloroethane	0.2	ug/L		<0.2	<0.2
	Chloroform	0.5	ug/L		<0.5	<0.5

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**Environment Testing** 

Client: Paterson Group

154 Colonnade Rd. South

Nepean, ON K2E 7T7

Attention: Mr. Oliver Blume

PO#:

Invoice to: Paterson Group

Report Number: 1973843
Date Submitted: 2022-03-23
Date Reported: 2022-03-30
Project: PH4484
COC #: 887701

Group	Analyte	MRL	Units	Lab I.D. Sample Matrix Sample Type Sampling Date Sample I.D.  Guideline	1615821 GW 2022-03-22 GW1	1615822 GW 2022-03-22 GW2
Volatiles	Dibromochloromethane	0.3	ug/L		<0.3	<0.3
	Dichlorodifluoromethane	0.5	ug/L		<0.5	<0.5
	Dichloromethane	4.0	ug/L	MAC 50	<4.0	<4.0
	Ethylbenzene	0.5	ug/L	MAC 140	<0.5	<0.5
	Ethylene Dibromide	0.2	ug/L		<0.2	<0.2
	Hexane	5	ug/L		<5	<5
	m/p-xylene	0.4	ug/L		<0.4	<0.4
	Methyl Ethyl Ketone (MEK)	10	ug/L		<10	<10
	Methyl Isobutyl Ketone (MIBK)	10	ug/L		<10	<10
	Methyl Tert Butyl Ether (MTBE)	2	ug/L	AO 15	<2	<2
	Monochlorobenzene	0.5	ug/L	MAC 80	<0.5	<0.5
	o-xylene	0.4	ug/L		<0.4	<0.4
	Styrene	0.5	ug/L		<0.5	<0.5
	t-1,2-Dichloroethylene	0.4	ug/L		<0.4	<0.4
	t-1,3-Dichloropropylene	0.2	ug/L		<0.2	<0.2
	Tetrachloroethylene	0.3	ug/L	MAC 10	<0.3	<0.3
	Toluene	0.4	ug/L	MAC 60	<0.4	<0.4
	Trichloroethylene	0.3	ug/L	MAC 5	<0.3	<0.3
	Trichlorofluoromethane	0.5	ug/L		<0.5	<0.5
	Vinyl Chloride	0.2	ug/L	MAC 1	<0.2	<0.2
	Xylene; total	0.5	ug/L	MAC 90	<0.5	<0.5

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154 Colonnade Rd. South

Nepean, ON K2E 7T7

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PO#:

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 Report Number:
 1973843

 Date Submitted:
 2022-03-23

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 2022-03-30

 Project:
 PH4484

 COC #:
 887701

#### **QC Summary**

Ar	nalyte	Blank		QC % Rec	QC Limits
<b>Run No</b> 418950 <b>Method</b> C SM2130B	Analysis/Extraction Date 20	022-03-23 <b>A</b> r	nalyst	AaN	
Turbidity		<0.1 NTU		99	70-130
Run No 418958 Method AMBCOLM1	Analysis/Extraction Date 20	022-03-24 <b>A</b> r	nalyst	DRA	
Escherichia Coli					
Total Coliforms					
Run No 418995 Method M SM3120B-3	Analysis/Extraction Date 20	)22-03-24 <b>A</b> r	nalyst	Z S	
Calcium		<1 mg/L		95	90-110
Potassium		<1 mg/L		96	87-113
Magnesium		<1 mg/L		95	76-124
Sodium		<1 mg/L		102	82-118
Run No 419016 Method EPA 350.1	Analysis/Extraction Date 20	022-03-24 <b>A</b> r	nalyst	SKH	
N-NH3		<0.010 mg/L		113	80-120
Run No 419027 Method EPA 351.2	Analysis/Extraction Date 20	022-03-24 <b>A</b> r	nalyst	SKH	
Total Kjeldahl Nitr	rogen	<0.100 mg/L		110	70-130

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**Environment Testing** 

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 PH4484

 COC #:
 887701

#### **QC Summary**

Analyte	Blank	QC % Rec	QC Limits
Run No 419078 Analysis/Extraction Date 20 Method EPA 8260	22-03-24 <b>A</b> na	alyst YH	
Tetrachloroethane, 1,1,1,2-	<0.5 ug/L	92	60-130
Trichloroethane, 1,1,1-	<0.4 ug/L	88	60-130
Tetrachloroethane, 1,1,2,2-	<0.5 ug/L	114	60-130
Trichloroethane, 1,1,2-	<0.4 ug/L	104	60-130
Dichloroethane, 1,1-	<0.4 ug/L	94	60-130
Dichloroethylene, 1,1-	<0.5 ug/L	93	60-130
Dichlorobenzene, 1,2-	<0.4 ug/L	104	60-130
Dichloroethane, 1,2-	<0.2 ug/L	115	60-130
Dichloropropane, 1,2-	<0.5 ug/L	106	60-130
1,3,5-trimethylbenzene	<0.3 ug/L	97	60-130
Dichlorobenzene, 1,3-	<0.4 ug/L	96	60-130
Dichloropropene,1,3-	<0.3 ug/L		
Dichlorobenzene, 1,4-	<0.4 ug/L	97	60-130
Acetone	<30 ug/L		60-130
Benzene	<0.5 ug/L	100	60-130
Bromodichloromethane	<0.3 ug/L	108	60-130

Guideline = ODWSOG

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 887701

## **QC Summary**

Analyte	Blank	QC % Rec	QC Limits
Bromoform	<0.4 ug/L	104	60-130
Bromomethane	<0.5 ug/L	93	60-130
Dichloroethylene, 1,2-cis-	<0.4 ug/L	98	60-130
Dichloropropene,1,3-cis-	<0.2 ug/L	103	60-130
Carbon Tetrachloride	<0.2 ug/L	93	60-130
Chloroethane	<0.2 ug/L	91	60-130
Chloroform	<0.5 ug/L	100	60-130
Dibromochloromethane	<0.3 ug/L	96	60-130
Dichlorodifluoromethane	<0.5 ug/L	86	60-130
Methylene Chloride	<4.0 ug/L	113	60-130
Ethylbenzene	<0.5 ug/L	85	60-130
Ethylene dibromide	<0.2 ug/L	98	60-130
Hexane (n)	<5 ug/L	110	60-130
m/p-xylene	<0.4 ug/L	93	60-130
Methyl Ethyl Ketone	<10 ug/L	100	60-130
Methyl Isobutyl Ketone	<10 ug/L		60-130
Methyl tert-Butyl Ether (MTBE)	<2 ug/L	110	60-130
Chlorobenzene	<0.5 ug/L	93	60-130

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#### **QC Summary**

Analyte	Blank	QC % Rec	QC Limits
o-xylene	<0.4 ug/L	84	60-130
Styrene	<0.5 ug/L	90	60-130
Dichloroethylene, 1,2-trans-	<0.4 ug/L	89	60-130
Dichloropropene,1,3-trans-	<0.2 ug/L	112	60-130
Tetrachloroethylene	<0.3 ug/L	91	60-130
Toluene	<0.4 ug/L	96	60-130
Trichloroethylene	<0.3 ug/L	82	60-130
Trichlorofluoromethane	<0.5 ug/L	87	60-130
Vinyl Chloride	<0.2 ug/L	88	60-130
Run No 419082 Analysis/Extraction Date 20 Method EPA 8260	022-03-25 <b>A</b> na	alyst YH	
Xylene Mixture			
Run No 419088 Analysis/Extraction Date 20 Method SM5530D/EPA420.2	022-03-25 <b>A</b> na	alyst IP	
Phenols	<0.001 mg/L	50	50-120
Run No 419093 Analysis/Extraction Date 20 Method C SM4500-S2-D	)22-03-25 <b>A</b> na	alyst AsA	
S2-	<0.01 mg/L	111	80-120

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#### **QC Summary**

An	alyte	Blank		,	QC % Rec	QC Limits
Run No 419123 Method C SM2120C	Analysis/Extraction Date 20	)22-03-28	Analy	/st A	\sA	
Colour (Apparent)		<2 TCU			106	90-110
Run No 419127 Method SM 4110	Analysis/Extraction Date 20	022-03-28	Analy	/st A	aN	
Chloride		<5 mg/L				90-110
N-NO2		<0.10 mg/L			103	90-110
N-NO3		<0.10 mg/L			104	90-110
SO4		<5 mg/L			105	90-110
Run No 419170 Method SUBCONTRAG	Analysis/Extraction Date 20	022-03-25	Analy	∕st A	ÆΤ	
Tannin & Lignin		<1.0 mg/L			106	
Run No 419184 Method SM2320,2510,	Analysis/Extraction Date 20 4500H/F	022-03-28	Analy	/st A	AsA	
Alkalinity (CaCO3)	)	<5 mg/L			98	90-110
Conductivity		<5 uS/cm			101	90-110
F		<0.10 mg/L			99	90-110
рН					100	90-110

Guideline = ODWSOG

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### **QC Summary**

Ar	nalyte	Blank	Ċ	QC % Rec	QC Limits
Run No 419188 Method SM 5310B	Analysis/Extraction Date 20	022-03-28 <b>A</b> n	alyst A	sA	
DOC		<0.5 mg/L		102	80-120
Run No 419190 Method SUBCONTRA	Analysis/Extraction Date 20	022-03-25 <b>A</b> n	alyst R	. <b>K</b>	
Tannin & Lignin		<1.0 mg/L		106	
<b>Run No</b> 419203 <b>Method</b> C SM2340B	Analysis/Extraction Date 20	022-03-29 <b>A</b> n	alyst A	ET	
Hardness as CaC	03				
Ion Balance					
TDS (COND - CA	LC)				
Run No 419228 Method EPA 200.8	Analysis/Extraction Date 20	022-03-29 <b>A</b> n	<b>alyst</b> S	D	
Silver		<0.0001 mg/L		82	80-120
Aluminum		<0.01 mg/L		111	80-120
Arsenic		<0.001 mg/L		97	80-120
Boron (total)		<0.01 mg/L		116	80-120
Barium		<0.01 mg/L		102	80-120
Beryllium		<0.0005 mg/L		105	80-120

Guideline = ODWSOG

\* = Guideline Exceedence

Results relate only to the parameters tested on the samples submitted. Methods references and/or additional QA/QC information available on request.



**Environment Testing** 

Client: Paterson Group

154 Colonnade Rd. South

Nepean, ON K2E 7T7

Attention: Mr. Oliver Blume

PO#:

Invoice to: Paterson Group

 Report Number:
 1973843

 Date Submitted:
 2022-03-23

 Date Reported:
 2022-03-30

 Project:
 PH4484

 COC #:
 887701

### **QC Summary**

Analyte	Blank	QC % Rec	QC Limits							
Cadmium	<0.0001 mg/L	101	80-120							
Cobalt	<0.0002 mg/L	99	80-120							
Chromium Total	<0.001 mg/L	94	80-120							
Copper	<0.001 mg/L	106	80-120							
Iron	<0.03 mg/L	99	80-120							
Manganese	<0.01 mg/L	104	80-120							
Molybdenum	<0.005 mg/L	99	80-120							
Nickel	<0.005 mg/L	101	80-120							
Lead	<0.001 mg/L	102	80-120							
Antimony	<0.0005 mg/L	83	80-120							
Selenium	<0.001 mg/L	108	80-120							
Strontium	<0.001 mg/L	97	80-120							
Thallium	<0.0001 mg/L	102	80-120							
Uranium	<0.001 mg/L	99	80-120							
Vanadium	<0.001 mg/L	98	80-120							
Zinc	<0.01 mg/L	108	80-120							
Run No 419288 Analysis/Extraction Date 2022-03-30 Analyst AaN  Method M SM3112B-3500B										

Guideline = ODWSOG

\* = Guideline Exceedence

Results relate only to the parameters tested on the samples submitted. Methods references and/or additional QA/QC information available on request.



Client: Paterson Group

154 Colonnade Rd. South

Nepean, ON K2E 7T7

Attention: Mr. Oliver Blume

PO#:

Invoice to: Paterson Group

 Report Number:
 1973843

 Date Submitted:
 2022-03-23

 Date Reported:
 2022-03-30

 Project:
 PH4484

 COC #:
 887701

### **QC Summary**

Analyte	Blank	QC % Rec	QC Limits
Mercury	<0.0001 mg/L	96	76-123

Guideline = ODWSOG

\* = Guideline Exceedence

Results relate only to the parameters tested on the samples submitted. Methods references and/or additional QA/QC information available on request.



Client: Paterson Group

154 Colonnade Rd. South

Nepean, ON K2E 7T7

Attention: Mr. Oliver Blume

PO#:

Invoice to: Paterson Group

Report Number: 1973843
Date Submitted: 2022-03-23
Date Reported: 2022-03-30
Project: PH4484
COC #: 887701

### Sample Comment Summary

Sample ID: 1615821 GW1 CI & SO4 MRL elevated due to matrix interference (dilution was done). Sediments not included for Hg analysis.

Sample ID: 1615822 GW2 CI & SO4 MRL elevated due to matrix interference (dilution was done). Sediments not included for Hg analysis.

Guideline = ODWSOG

\* = Guideline Exceedence

Results relate only to the parameters tested on the samples submitted. Methods references and/or additional QA/QC information available on request.

# eurofins | Environment Testing

### **Certificate of Analysis**

Client: Paterson Group

154 Colonnade Rd. South

Nepean, ON K2E 7T7

Attention: Mr. Oliver Blume

PO#: 32614

Invoice to: Paterson Group Page 1 of 2

Report Number: 1974461
Date Submitted: 2022-04-04
Date Reported: 2022-04-05
Project: PH4484
COC #: 889009

#### **Dear Oliver Blume:**

Please find attached the analytical results for your samples. If you have any questions regarding this report, please do not hesitate to call (613-727-5692).

Report Comments:

Dragana

Dzeletovic
Angara Inclutoric 2022.04.05

16:55:16

APPROVAL: -04'00'

Dragana Dzeletovic-Andric, Microbiology Team Lead

All analysis is completed at Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) unless otherwise indicated.

Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) is accredited by CALA, Canadian Association for Laboratory Accreditation to ISO/IEC 17025 for tests which appear on the scope of accreditation. The scope is available at: http://www.cala.ca/scopes/2602.pdf.

Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) is licensed by the Ontario Ministry of the Environment, Conservation, and Parks (MECP) for specific tests in drinking water (license #2318). A copy of the license is available upon request.

Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) is accredited by the Ontario Ministry of Agriculture, Food, and Rural Affairs for specific tests in agricultural soils.

Please note: Field data, where presented on the report, has been provided by the client and is presented for informational purposes only. Guideline values listed on this report are provided for ease of use (informational purposes) only. Eurofins recommends consulting the official provincial or federal guideline as required. Unless otherwise stated, measurement uncertainty is not taken into account when determining guideline or regulatory exceedances.

MRL

0

0



**Environment Testing** 

Analyte
Escherichia Coli

Total Coliforms

Client: Paterson Group

154 Colonnade Rd. South

Nepean, ON K2E 7T7

Attention: Mr. Oliver Blume

PO#: 32614

Group

Microbiology

Invoice to: Paterson Group

 Report Number:
 1974461

 Date Submitted:
 2022-04-04

 Date Reported:
 2022-04-05

 Project:
 PH4484

 COC #:
 889009

	Lab I.D. Sample Matrix Sample Type	1617476 GW
	Sampling Date	2022-04-04
	Sample I.D.	GW1
Units	Guideline	
ct/100mL	MAC 0	0
ct/100mL	MAC 0	4*

Guideline = ODWSOG

\* = Guideline Exceedence

Results relate only to the parameters tested on the samples submitted. **Analytical Method: AMBCOLM1** additional QA/QC information available on request.



146 Colonnade Rd, Unit 8, Ottawa, ON K2E 7Y1 (613) 727-5692

**OFFICIAL CERTIFICATE OF ANALYSIS: 4491110** 

WORK REQUEST : 100392148 Report Date : 2025-10-09

Reception Date: 2025-10-08

Project: NELSON WATER - Non-Regulated

Sampler: NA

PO Number: Not Applicable

Temperature: 14 °C

Analysis	Quantity	External Method
E.Coli and Total Coliforms (DC Plate)	1	Modified from MECP E3407

#### Criteria:

**Nelson Water** 

Carp, Ontario

K0A 1L0

248 Westbrook Rd.

A: Ontario Regulation 169/03 (Non-Regulated Drinking Water)

#### Sample status upon receipt :

Attention: Customer Service

9096463 Compliant

#### Notes :

- All analysis is completed at Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) unless otherwise stated.
- Eurofins Environment Testing Canada Inc. is accredited by CALA, Canadian Association for Laboratory Accreditation to ISO/IEC 17025 for tests which appear on the scope of accreditation. The scope is available at https://directory.cala.ca/
- Please note: Field data, where presented on the report, has been provided by the client and is presented for informational purposes only. Guideline or regulatory limits listed on this report are provided for ease of use (informational purposes) only. Eurofins recommends consulting the official guideline or regulation as required. Unless otherwise stated, measurement uncertainty is not taken into account when determining guideline or regulatory exceedances.

Legend :



146 Colonnade Rd, Unit 8, Ottawa, ON K2E 7Y1 (613) 727-5692

#### **OFFICIAL CERTIFICATE OF ANALYSIS - RESULTS**

Client: Nelson Water

Project: NELSON WATER - Non-Regulated Reception Date: 2025-10-08

			9096463					
			Drinking water					
		2025-10-07						
			York - HOP					
Microbiology				Criteria				
	RL	Unit	Α	В	С			
E.Coli and Total Coliforms (DC Plate)								
Escherichia coli (DC)	0	CFU/100mL	0			0		
Total Coliforms (DC)	0	CFU/100mL	0			0		

Approved by:

Jason Kennedy, Project Manager



146 Colonnade Rd, Unit 8, Ottawa, ON K2E 7Y1 (613) 727-5692

#### OFFICIAL CERTIFICATE OF ANALYSIS - QUALITY CONTROL

Client: Nelson Water

Project: NELSON WATER - Non-Regulated Reception Date: 2025-10-08

	Unit	RL	Blank	Q		Matrix S	Spike	Duplicate			
Parameter				Recovery %	Range %	Recovery %	Range %	RPD %	Range %		
.Coli and Total Coliforms (DC Plate)											
Method : Total C	Coliforms and E.C	Coli by MF (V	Water, DC plate)	. Internal meth	nod: OTT-M-	-BAC-WI45296					
Escherichia coli (DC)	CFU/100mL	0	0					-	0-30		
Total Coliforms (DC)	CFU/100mL	0	0					-	0-30		
	Associated	Samples : 9	096463				Δ	Prep Date: nalysis Date:	: 2025-10-08 : 2025-10-09		

Where RPD % is reported as "-" the calculation is not available because one or both of the duplicates is within 5 times the RL.



Page \_\_\_\_\_ of \_\_\_\_\_

### **DRINKING WATER CHAIN-OF-CUSTODY**

146 Colonnade Road, Unit #8, Ottawa, ON, KZE 7Y1 - Phone: 613-727-5692, Fax: 613-727-5222

	CLII	NT IN	FORMATION	0.7				-			100	DRIN	KING 1	NATER	SYSTE	M (DV	ŃS) IŅI	FORM	ATION		
Company: NELSC	ON WATER INC			* 4		æ.		· " Livi	DWS Name:											T 11 1	
contact: Juan O	spina .			· · · · · · · · · · · · · · · · · · ·			~		DWs #:		y		3 × 177			7		e de la composition della comp	11.		ž
Address: 248 We	estbrook Rd, Carp, Of	1, K0/	A 1L0						Contact:					,					1747		•
Telephone: 61383	318491	3. 0	3	is is is to be		16			Address:		8. 1	3	10	0.					8 8		
Email #1: Custom	erservice@nelsonwa	ter.co	m #2:						Telephone:					9							
Project:			* *** ***						Cett Phone:												
PO#:		-			<i>9</i> 17.	Quote f	l:		Email #1:					.,		#2;					
	w r .wa	ON/GU	JIDELINE REC	UIREC	) ,								TURN	-AROL	JND TI	ME (Bu	sines	Days)			
O, Reg. 1	70/03 C. Reg. 170/03, Sch. 15.1, Lend		Non-Regulated: (Ontario)	Z	Other:	. 2			1 Day* (10	10%)		2 Day**	(50%)		3-5 Days	[25%]			5-7 Days	(Standan	1)
O. Reg. 3	19/06 D. Reg. 243/07		Non-Regulated (Federal)					7.9	N			- 1 - 4 - 1 -		L11-L	Illes Coss	m	au analu	to much s	andea Ria	ta thut so	me tests (i.e. O. Reg. 170/03
Has an L	SN form been submitted to MECP of N	MOHLTC	Public Health Unit				30		Schedule 24 pesticide											te mat so	ine tests [1.0. O. Reg. 270/03
(If applica	(ff applicable)? Sample Detail					e Details			Si	ample /	inalysis	Regula	ed		Fie	eld Mea	sureme	ints	-		
cannot be frozen. Not reported where (and The COC must be com surcharge if required i grey).	ture conditions during transport a te that for drinking water samples how) applicable legislation requi- plete upon submission of the sam information is missing (required	, adverse es. ples, the fields a	results will be	Sample Type Code (see below)	Resample?	MECP/MCH Reportable radverse notification	# of Containers	SPI Code/Watertrax	Sample Location	E. COLI	TOTAL COLIFORMS	NITRATESMITRITES				3	H	Total Chlorine	Free Chlorine	Turbidity	Sample RN# (Lab Use Only)
York - HOP			/2025 3:24PM	DW	N	N	1		,	1	1			,							9096463
YORK - HOP	, i , , , , , , , , , , , , , , , , , ,	07/10	/2025 3:24PM	TW	N	N	1					1									<del></del>
,		>	1,1									3.3	2.0								
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			5 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -										6								
	× 2 2								•											3,000	
Sample Type Codes for D	Orinking Water; RW = Raw Water, TW g: Occasionally, situations arise in whi	Treated  th Furnish	d Water at POE to d	istribuțio ting Cana	on, TW-N	i = Untreat val is unab	ed Water le to proc	at POE to distribu	ition, DW = Distribution receipt. By signing this	RP = Ro	sidential 1 custody f	Plumbing, orm, the	NRP = No	n-Reside	ntial Plum urofins En	vironiser	Standing	Canada (	ied, PW = Ottawa) (	Private W	oli." Pract samples to a laboratory
that is accredited and, w	here applicable, holds a drinking wate	r licensa.	Agreements made	lu taksu	ce to sub	contract to	a specific	laboratory will b	g honored.							- 31					
M 5 .5	PRINT			SIGN	e e e		1	OCATION	PATE/1	IME	1,18		TEMP ('C	3		<u></u> -			-		
Sampled By:	Les Orr							_	07/10/2025	3:2	4PM		60 16								
Relinquished By:	Alejandro Ospina	a.							08/10/2025	1:5	0PM							1	1003	921	18
Received By:															1		11 11			 	
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OTT-P-SOP73681, Revision 11

Copies: White - Laboratory, Yellow - Sampler



146 Colonnade Rd, Unit 8, Ottawa, ON K2E 7Y1 (613) 727-5692

**OFFICIAL CERTIFICATE OF ANALYSIS: 4492546** 

WORK REQUEST : 100392167 Report Date : 2025-10-14

Reception Date: 2025-10-08

Project: NELSON WATER - Non-Regulated

Sampler: NA

PO Number: Not Applicable

Temperature: 14 °C

Analysis	Quantity	External Method
Nitrate and Nitrite (Water, Colorimetry)	1	Modified from SM 4500-NO3-F

#### Criteria:

**Nelson Water** 

Carp, Ontario

K0A 1L0

248 Westbrook Rd.

A: Ontario Regulation 169/03 (Non-Regulated Drinking Water)

#### Sample status upon receipt :

Attention: Customer Service

9096602 Compliant

#### Notes :

- All analysis is completed at Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) unless otherwise stated.
- Eurofins Environment Testing Canada Inc. is accredited by CALA, Canadian Association for Laboratory Accreditation to ISO/IEC 17025 for tests which appear on the scope of accreditation. The scope is available at https://directory.cala.ca/
- Please note: Field data, where presented on the report, has been provided by the client and is presented for informational purposes only. Guideline or regulatory limits listed on this report are provided for ease of use (informational purposes) only. Eurofins recommends consulting the official guideline or regulation as required. Unless otherwise stated, measurement uncertainty is not taken into account when determining guideline or regulatory exceedances.

Legend :

RL : Reporting limit N/A : Not applicable \* : Analysis conducted by external subcontracting QC : Reference material (QC) 1 : Results in annex ^ : Analysis not accredited



146 Colonnade Rd, Unit 8, Ottawa, ON K2E 7Y1 (613) 727-5692

#### **OFFICIAL CERTIFICATE OF ANALYSIS - RESULTS**

Client: Nelson Water

Project: NELSON WATER - Non-Regulated Reception Date: 2025-10-08

				Eurofins Sa	ample No :	9096602	
			Drinking water				
			2025-10-07				
			YORK - HOP				
Nutrients				Criteria			
	RL	Unit	Α	В	С		
Nitrate and Nitrite (Water, Colorimetry)							
Nitrate (as Nitrogen)	0.1	mg/L	10.0			0.25	
Nitrate + Nitrite (as Nitrogen)	0.1	mg/L				0.25	
Nitrite (as Nitrogen)	0.1	mg/L	1.0			<0.10	

Approved by:

Jason Kennedy,

Project Manager



146 Colonnade Rd, Unit 8, Ottawa, ON K2E 7Y1 (613) 727-5692

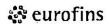
#### OFFICIAL CERTIFICATE OF ANALYSIS - QUALITY CONTROL

Client: Nelson Water

Project: NELSON WATER - Non-Regulated Reception Date: 2025-10-08

_ ,	Limit	D.	Blank	Q	2	Matrix S	Spike	Duplicate	
Parameter	Unit	RL		Recovery %	Range %	Recovery %	Range %	RPD %	Range %
Nitrate and Nitrite (Water, Colorimetry)									
Meti	od : Nitrates/Nitrate	s (Water, Co	olorimetry). Inte	rnal method: O	TT-I-NUT-W	146199.			
Nitrate (as Nitrogen)	mg/L	0.1	<0.10	99	80-120			8	0-20
Nitrate + Nitrite (as Nitrogen)	mg/L	0.1	<0.10	99	80-120	104	80-120	5	0-20
Nitrite (as Nitrogen)	mg/L	0.1	<0.10	106	80-120	104	80-120	-	0-20
	Associated	Samples : 9	096602	-!			A	Prep Date	2025-10-0

Where RPD % is reported as "-" the calculation is not available because one or both of the duplicates is within 5 times the RL.



### DRINKING WATER CHAIN-OF-CUSTODY

146 Colonnade Road, Unit #8, Ottawa, ON, K2E 7Y1 - Phone: 613-727-5692, Fax: 613-727-5222

CLIENTINFORMATION	<b>3.</b> 数据的 1. 数据 1. 数是 1. 数是 1. 数是 1. 数据 1. 数是 1. 数是 1. 数是 1. 数是 1. 数是 1. 数是 1. 数是 1. 数是 1. 数是 1. 数是 1.	PRINKING WATER SYSTEM (PWS) INFORMATION						
COMPANY: NELSON WATER INC	āti Kamenāti	DWS Names	ingles, he did to a		1 2 2 2 3 3 4 1 2 4 1			
Caniest Juan Ospina	are mulained	DWs MC		e Chabe	Lind Fair Al (n. 11			
Addies: 248 WestbrookiRd, Carp, ON: KOA 110		Connection						
Telephone 6138318491	之为。他上, 古报 <b>出</b>	Address						
Email #1: customerservice@nelsonwater.com #2:		Telephone:	24年,6月1日,1878年	White and the second	是也是在代表的			
Project:	Cett Phone:		<u> </u>					
PO#:	Quote#:	Email #1:	#2:		An escapasa an an an			
REGULATION/GUIDELINE REQUIRED  O Reg. 170/03		1 Day* (100%)	TURN: AROUND TIME:  2 Day** [50%] 3-5 Days [25%]  100 to determine rush availability. Surcharge  3 weeks to analyze]. Please see notes (on ce	may apply to rush service. Note that so	d)			
(if applicable)?	*Carrinle Details		Sample Analysis Required	Field Measurements				
The optimal temperature conditions during transport are 4 - 10 °C Sample(s) teamed be frozen. Note that for drinking water samples, adverse results will be reported where (and how) applicable legislation requires.  The COC must be complete upon submission of the samples, there will be a \$25 surcharge if required information is missing (required fields are shaded in grey).	MED VIOLE Reportable (always world action) for the second action of the	Sample Location (I.e. Kitchen, POE)	NIIATESNITATES	pH Total Chlorine Free Chlorine	Sample RN# (Lab Use Only)			
York - HOP 97/10/2025 3124PM DW N	N 1 1 1 1	V.V.		3	<b>2</b> 15.07			
YORK HOP 07/10/2025 3/24PM TW: N	Nie 1	area and the area	Was I a vie to		9096602			
or Sura Bakal the second will are to the fall		45000						
traditional designation of the property of the	State Live		100384329626268		-			
F2000年度入了。《西南京》(F2000年) F2000年		6.74 2		33				
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				in i				
Sumple Type Cases for Prinking WateriaW & Aust Waley TW a Trestor Water as PAS to Bistilbushes TW at	ENGINEARED WATER AT POS 19 STUILBY	Hort DW a Distribution RP & Residentia	Plumpers, NAR & Nou-Residential Beimpins	a a tenbios, F e Flyanes, PW a Poyete V	/PERSONAL PROPERTY			
Notics of Jubicangusting Occapios (), plystiant plos in which by under Environment I string Lenada (Cita that is accredited and, where spoilestia, holds a unburg yeter license. Asception it medel in edge my legale	ka) ja muahia 12 biotekka asaubin alika Kaninact to a charido jabalatary wili b	r repaipt, by diantria this she is of surrod) a honored	torm, the client agrees that Europin's Environ	ment Teeling Ceneva (Ottawa) may subco	United foundation laberatory			
PRINT CHARGE SIGN								
Sampled By: Les Orr		07/10/2025 3:24PM	1		}			
Alejandro Genina	TEST CHEST STATES	08/10/2025 1:50PM		100392	1167			
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Received By: Makeym Pur Lower To	077	Oct 8, 2015 6:26	140	## ###################################				
Comments:				Printed On: 2025-10	0-08 17:46:27			

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

**SOIL PROFILE AND TEST DATA** 

Geotechnical Investigation Proposed Office Building 2966 Carp Road - Ottawa, Ontario

**DATUM** Geodetic FILE NO. **PG3834 REMARKS** HOLE NO. TP 1-22 **BORINGS BY** Backhoe DATE 2022 February 8 **SAMPLE** Pen. Resist. Blows/0.3m Piezometer Construction STRATA PLOT **DEPTH** ELEV. **SOIL DESCRIPTION** 50 mm Dia. Cone (m) (m) N VALUE or RQD RECOVERY NUMBER Water Content % **GROUND SURFACE** 80 20 0+120.05**TOPSOIL** 1 FILL: Brown silty sand with gravel <u>0</u>.40 [∑ G 2 Brown SILTY SAND with gravel, cobbles and boulders, trace clay G 3 1 + 119.05Highly fractured **BEDROCK** interbedded with silty sand to sandy silt, some clay with fragmented G 4 bedrock End of Test Pit TP terminated on fractured bedrock surface at 1.83 m depth (TP dry upon completion) 40 60 80 100 Shear Strength (kPa) ▲ Undisturbed △ Remoulded

Proposed Office Building

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

**Geotechnical Investigation** 

**SOIL PROFILE AND TEST DATA** 

					29	oo Carp i	road - Oi	lawa	i, On	laric	)			
<b>DATUM</b> Geodetic										FIL	E NO	PC	33834	
REMARKS BORINGS BY Backhoe				n	ATE S	2022 Feb	ruary 8			НС	LE N	<sup>D.</sup> <b>TP</b>	2-22	
SOIL DESCRIPTION	PLOT		SAN	IPLE	AIE 2	DEPTH	ELEV.	Р				ows/0 a. Con	.3m	er
GOIL BLOOM HON	STRATA P	TYPE	NUMBER	% RECOVERY	N VALUE or RQD	(m)	(m)							Piezometer Construction
GROUND SURFACE	STR	TX	NUM	RECO	N or		400.05		O V	vate 40	ter Content % 40 60 80			S Pie
<b>TOPSOIL</b> 0.15		G	1			0-	-120.05							
FILL: Brown silty sand trace gravel, organics and metallic debris		G	2											
0.50		- G	3											
Brown <b>SILTY SAND</b> with gravel, cobbles and boulders, trace clay														
	1+119.0	-119.05												
		G	4											
		G	5											
Highly fractured <b>BEDROCK</b> interbedded with silty sand to sandy		<u></u>				2-	-118.05							
silt, some clay with fragmented 2.10 bedrock End of Test Pit		G	6											
TP terminated on fractured bedrock surface at 2.1 m depth														
(TP dry upon completion)														
											treng	50 th (kP	a)	00

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

**SOIL PROFILE AND TEST DATA** 

Geotechnical Investigation Proposed Office Building 2966 Carp Road - Ottawa, Ontario

154 Colonnade Road South, Ottawa, Ont	alio r	ZE /J	5		29	66 Carp I	Road - O	ttawa, On	tario		
DATUM Geodetic	'				FILE	NO. <b>PG383</b> 4	ļ				
REMARKS						= .			HOL	E NO. <b>TP 3-22</b>	
BORINGS BY Backhoe				D	ATE 2	2022 Feb	ruary 8	1		11 0-22	
SOIL DESCRIPTION	SAM SAM				DEPTH (m)	ELEV. (m)			Blows/0.3m Dia. Cone	Piezometer Construction	
	STRATA	TYPE	NUMBER	% RECOVERY	N VALUE or RQD	(,	(,	0 V	/ater	Content %	Szome
GROUND SURFACE	STI	Ĥ	NON	RECO	NON			20	40	60 80	<u>≅</u> 8
TOPSOIL 0.10		G	1			- 0-	119.19				
Brown <b>SILTY SAND</b> with gravel, cobbles and boulders		G	3			1-	-118.19				
Highly fractured BEDROCK interbedded with silty sand to sandy silt, some clay with fragmented bedrock 1.45  End of Test Pit  TP terminated on fractured bedrock surface at 1.45 m depth  (TP dry upon completion)		G 	4					20	40	60 80 on oth (I/Po)	100
									ır Stre	ength (kPa) △ Remoulded	.00

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

**SOIL PROFILE AND TEST DATA** 

Geotechnical Investigation Proposed Office Building 2966 Carp Road - Ottawa, Ontario

захт	NUMBER NO			2022 Feb	ruary 8	Pen. Re	HOLE N	TP 4-22											
\/		<b>I</b> PLE		DEPTH		Pen. Re	esist. B												
\/			岜〇		ELEV.	Pen. Re	PTION    SAMPLE   DEPTH   ELEV.   Pen. Resist. Blows/0.3m												
\/	NUMBER	° OVER	ᄪᄉ	(m)	(m)	• 50	) mm Di	eter											
\/	Z	Ü	N VALUE or RQD			0 W	ater Co	Piezometer Construction											
G		R	o N	0-	-110 22	20	40	60 80											
<b>/</b>	1			U	110.55														
G	2																		
G	3																		
				1-	-117.33														
						20	40	60 80 1											
	G	G 2	G 2	G 2	G 2 G 3	G 2	G 2  G 3  1-117.33  20 Shea	G 2  G 3  1-117.33  20 40 Shear Streng	G 2  G 3  1-117.33										

**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

**Geotechnical Investigation** Proposed Office Building

DATUM Geodetic					25	oo Carp i	nuau - U	ttawa, On	T	E NO.				
REMARKS											PG383	4		
BORINGS BY Backhoe					ATE	2022 Feb	ruary 8		HOI	LE NO	). TP 5-22	2		
SOIL DESCRIPTION	PLOT		SAN	MPLE		DEPTH (m)	ELEV. (m)			esist. Blows/0.3m 0 mm Dia. Cone				
	STRATA	TYPE	NUMBER	RECOVERY	VALUE r RQD	(111)	(111)	0 V	Vater	Cor	ntent %	Piezometer		
GROUND SURFACE	ST	H	) N	REC	N VZ or		447.00	20	40					
TOPSOIL 0.15	5	G	1			- 0-	117.88							
Brown <b>SILTY SAND</b> with gravel, cobbles and boulders		<u></u>												
		G	2											
0.65	5	<u>-</u>												
Highly fractured <b>BEDROCK</b> interbedded with silty sand to sandy silt, some clay with fragmented		G	3											
bedrock						1-	-116.88							
End of Test Pit	5													
TP terminated on fractured bedrock surface at 1.75 m depth														
(TP dry upon completion)														
								I .		reng	60 80 th (kPa)	100		

**Geotechnical Investigation** 

**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

**Proposed Office Building** 2966 Carp Road - Ottawa, Ontario

DATUM Geodetic					•				FILE NO.	3834					
REMARKS BORINGS BY Backhoe					ATE '	2022 Eab	aruony O		HOLE NO.	6-22					
BORINGS BY DACKING	E	DATE 2022 February 8							D D : 1 D1 100						
SOIL DESCRIPTION	PLOT				<b>H</b> -	DEPTH (m)	ELEV. (m)	1	0 mm Dia. Cone						
	STRATA	TYPE	NUMBER	% RECOVERY	N VALUE or RQD			0 <b>W</b>	/ater Content %	řezon					
GROUND SURFACE	Ω.		ğ	REC	z <sup>ö</sup>	0-	118.91	20	40 60 8	0					
<b>BEDROCK</b> 0.10		G G	1				110.31								
FILL: Brown silty sand with brick fragments, concrete and gravel		G	2												
		G	3												
		G	4			1-	-117.91								
End of Test Pit  TP terminated on fractured bedrock															
surface at 1.75 m depth															
(TP dry upon completion)								20 Shea ▲ Undist	40 60 8 ar Strength (kPa urbed △ Remou	1)					

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

**SOIL PROFILE AND TEST DATA** 

Geotechnical Investigation Proposed Office Building 2966 Carp Road - Ottawa, Ontario

								FILE	NO. <b>PG38</b> 3	34
								HOLE	: NO	
				ATE 2	2022 Feb	ruary 8				_
PLOT					DEPTH (m)	ELEV. (m)				eter
TRATA	IYPE	UMBER	COVER	VALUE r RQD			0 W	ater C	Content %	Piezometer Construction
Š	•	Ä	REG	zö	0	110.67	20	40	60 80	1 0
_	G	1			0-	110.07				
5	G	2								
	G	3								
	G	4			1-	-117.67				
0										
							20	40	60 80	100
	STRATA PLOT	STRATA  STRATA  O  O  O  O  O  O  O  O  O  O  O  O  O	STRATA PLO STRATA PLO G G A A A A A A A A A A A A A A A A A	SAMPLE STRATA PLOT A STRATA PL	STRATA PLOT STRATA PLOT STRATA PLOT  OR NUMBER  RECOVERY N VALUE OF ROD	SAMPLE SALEATA PLOT STRATA PLOT STRATA PLOT STRATA PLOT (m)  G 4  G 4	G 4  G 4  DEPTH (m)  C (m)  DEPTH (m)  G 1  G 2  G 3  DEPTH (m)  1-117.67	SAMPLE   DEPTH   ELEV. (m)   Pen. Re   50   50   1   1   1   1   1   1   1   1   1	SAMPLE   SAMPLE   DEPTH   ELEV. (m)   For many 8   SAMPLE   SO mm   SAMPLE   SAMPLE   BEPTH   ELEV. (m)   Fig. 20   40   60   80	

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

**SOIL PROFILE AND TEST DATA** 

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

DATUM

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation =

FILE NO.

119.73m.

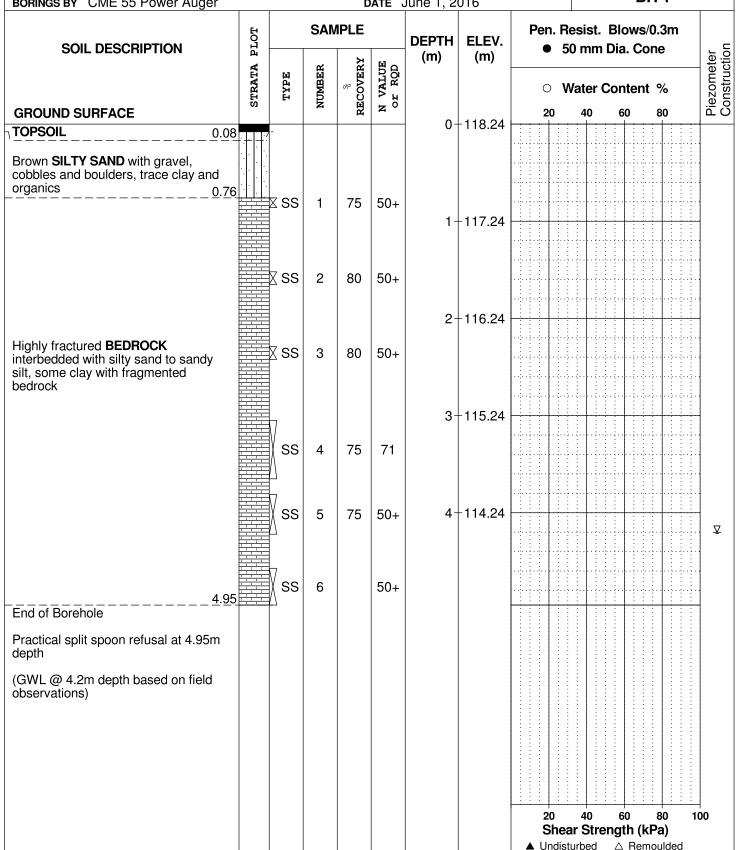
REMARKS

BORINGS BY CME 55 Power Auger

DATE June 1, 2016

PG3834

HOLE NO.
BH 1



**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

**DATUM** TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = 119.73m.

FILE NO. PG3834

**REMARKS** HOLE NO. **BH 2 DATE** June 1, 2016 BORINGS BY CME 55 Power Auger **SAMPLE** Pen. Resist. Blows/0.3m STRATA PLOT **DEPTH** ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) RECOVERY N VALUE or RQD NUMBER Water Content % **GROUND SURFACE** 80 20 0+118.42**TOPSOIL** 0.10 Brown SILTY SAND with gravel. cobbles and boulders, trace clay and organics 1+117.42SS 1 92 51 1.45 × SS 2 25 50+ 2+116.42 Highly fractured **BEDROCK** interbedded with silty sand to sandy silt, some clay with fragmented bedrock 3+115.42 $\mathbf{SS}$ 3 50 +50 4+114.42 4.80 SS 4 67 50+ End of Borehole Practical split spoon refusal at 4.80m depth (BH dry - June 6, 2016) 40 60 100 Shear Strength (kPa) ▲ Undisturbed △ Remoulded

**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

**Geotechnical Investigation** Proposed Storage Building - 2978 & 2966 Carp Road

▲ Undisturbed

△ Remoulded

Ottawa, Ontario TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = FILE NO. **DATUM PG3834** 119.73m. **REMARKS** HOLE NO. **BH 3 DATE** June 1, 2016 BORINGS BY CME 55 Power Auger **SAMPLE** Pen. Resist. Blows/0.3m STRATA PLOT **DEPTH** ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) N VALUE or RQD RECOVERY NUMBER Water Content % 80 **GROUND SURFACE** 20 0+118.29**TOPSOIL** 0.15 Brown SILTY SAND with gravel, cobbles and boulders, trace clay and organics SS 1 50+ Highly fractured **BEDROCK** 1+117.29interbedded with silty sand to sandy silt, some clay with fragmented bedrock End of Borehole Practical refusal to augering at 1.12m depth (BH dry upon completion) 40 60 100 Shear Strength (kPa)

**Geotechnical Investigation** Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

SOIL PROFILE AND TEST DATA

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

119.73m.

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation =

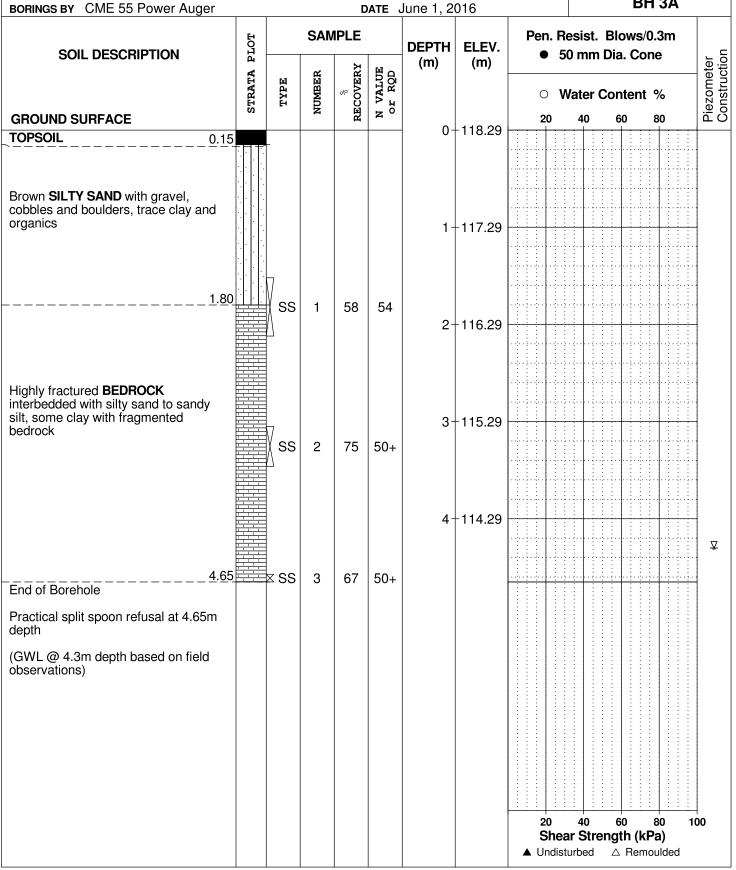
**REMARKS** 

**DATUM** 

FILE NO. **PG3834** 

HOLE NO.

**BH 3A DATE** June 1, 2016 BORINGS BY CME 55 Power Auger



**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = PG3834

REMARKS

PORTINGS BY CME 55 Power August

PATE | June 1, 2016

BORINGS BY CME 55 Power Auger				D	ATE .	June 1, 2	016		HOLE NO.	BH 4	
SOIL DESCRIPTION	PLOT		SAN	/IPLE		DEPTH (m)	ELEV. (m)		Pen. Resist. Blows/0.3m  ■ 50 mm Dia. Cone		
	STRATA	TYPE	NUMBER	% RECOVERY	N VALUE or RQD	()	(,		Vater Conte		Piezometer
GROUND SURFACE				<b>K</b>		0-	118.03	20	40 60	80	اقة ز
OPSOIL 0.08 brown SILTY SAND with gravel, obbles and boulders, trace clay and rganics 0.66		,- -									
		ss	1	50	46	1 -	-117.03				
lighly fractured <b>BEDROCK</b> nterbedded with silty sand to sandy ilt, some clay with fragmented edrock		ss	2		68	2-	-116.03				
		<u> </u>									
ractical refusal to augering at 2.59m											
epth BH dry upon completion)											
or any apoin completion)											
								20	40 60	80 10	00
								Shea ▲ Undist	ar Strength urbed △ R	( <b>kPa</b> ) emoulded	

**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = 119.73m.

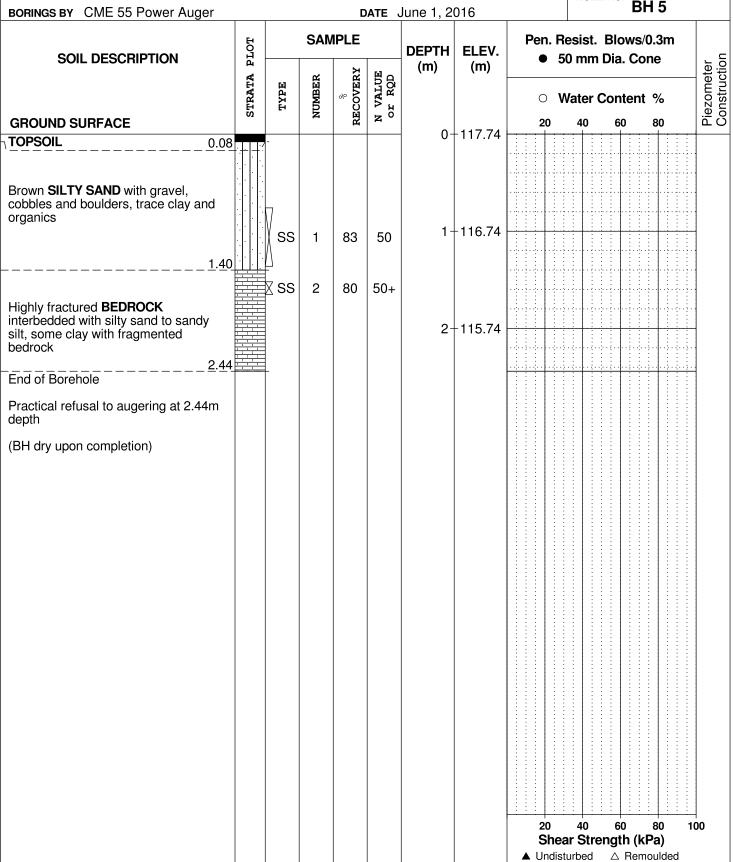
REMARKS

BORINGS BY CME 55 Power Auger

PATE June 1 2016

FILE NO. PG3834

HOLE NO. BH 5



SOIL PROFILE AND TEST DATA

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

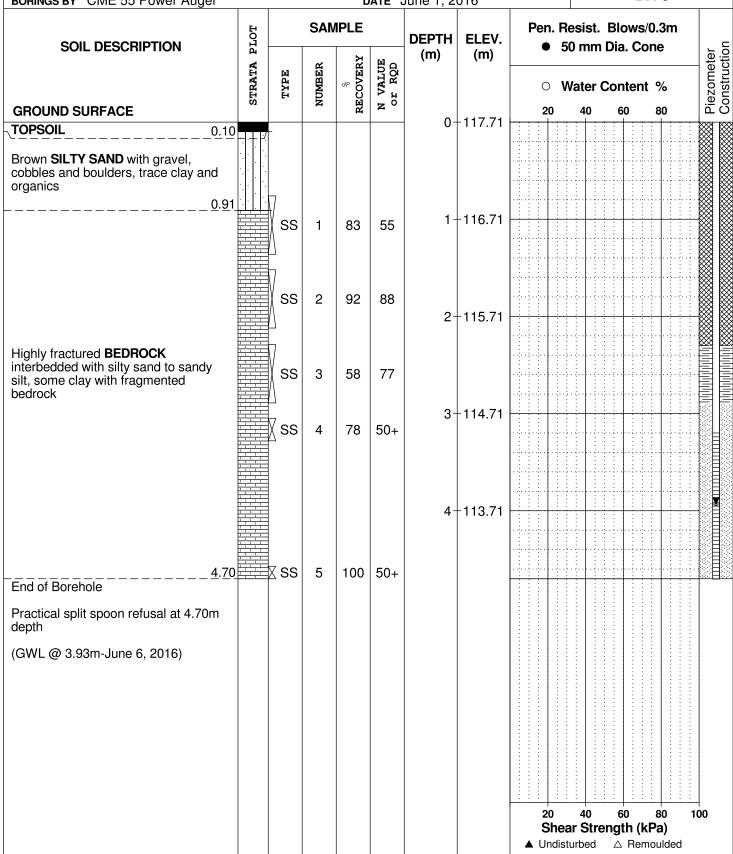
**Geotechnical Investigation** Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

**DATUM** 

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation =

FILE NO.

**PG3834** 119.73m. **REMARKS** HOLE NO. **BH 6 DATE** June 1, 2016 BORINGS BY CME 55 Power Auger



154 Colonnade Road South, Ottawa, Ontario K2E 7J5

SOIL PROFILE AND TEST DATA

**Geotechnical Investigation** Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

**DATUM** 

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation =

FILE NO.

40

▲ Undisturbed

Shear Strength (kPa)

60

△ Remoulded

100

**PG3834** 119.73m. **REMARKS** HOLE NO. **BH7 DATE** June 1, 2016 BORINGS BY CME 55 Power Auger **SAMPLE** Pen. Resist. Blows/0.3m PLOT DEPTH ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) RECOVERY N VALUE or RQD STRATA NUMBER Water Content % **GROUND SURFACE** 80 20 0 + 117.53**TOPSOIL** 0.30 Brown SILTY SAND with gravel. cobbles and boulders, trace clay and organics SS 1 80 50+ 1 + 116.532 SS 21 51 2+115.53Highly fractured **BEDROCK** interbedded with silty sand to sandy silt, some clay with fragmented bedrock 3+114.53SS 3 40 50 +⊻ 4+113.53⊠ SS 4 100 50 +End of Borehole Practical split spoon refusal at 4.65m depth (GWL @ 3.7m depth based on field observations)

SOIL PROFILE AND TEST DATA

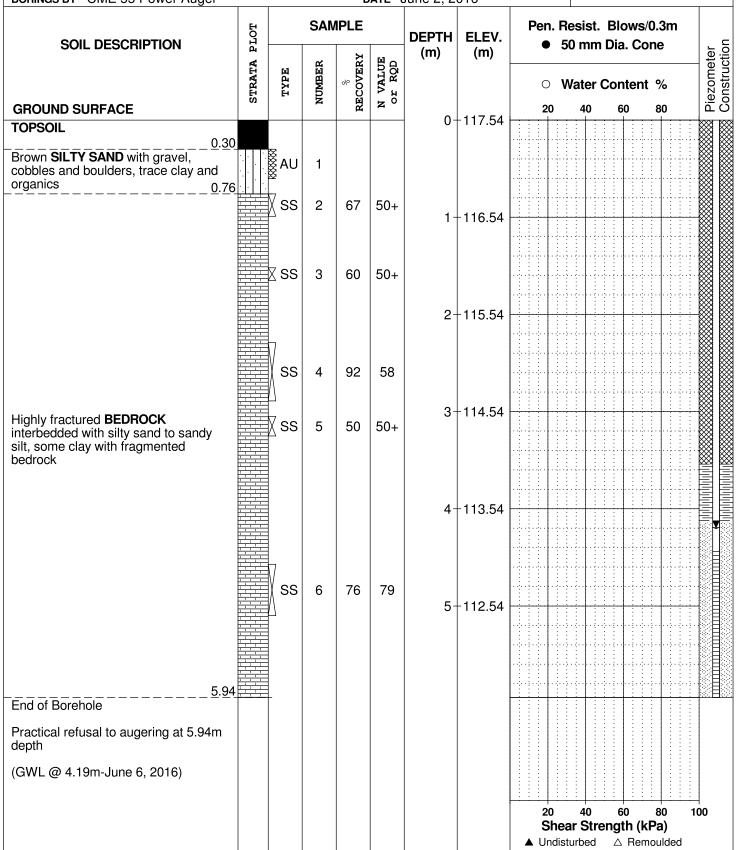
**Geotechnical Investigation** 

Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation =

FILE NO. **DATUM PG3834** 119.73m. **REMARKS** HOLE NO. **BH8 DATE** June 2, 2016 BORINGS BY CME 55 Power Auger **SAMPLE** Pen. Resist. Blows/0.3m ELEV.



SOIL PROFILE AND TEST DATA

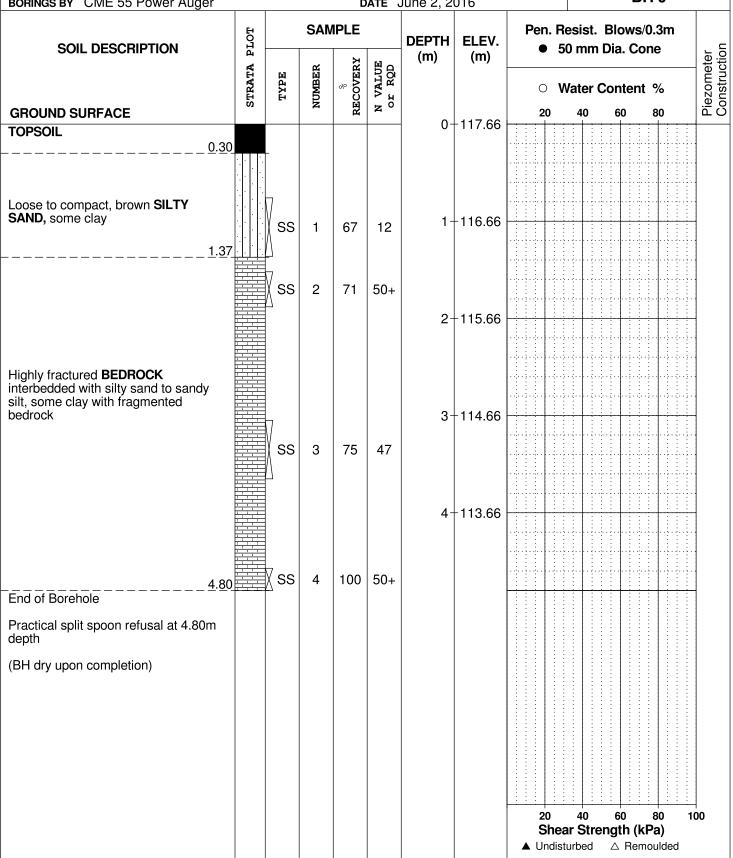
154 Colonnade Road South, Ottawa, Ontario K2E 7J5

**Geotechnical Investigation** Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

**DATUM** 

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation =

FILE NO. **PG3834** 119.73m. **REMARKS** HOLE NO. **BH9 DATE** June 2, 2016 **BORINGS BY** CME 55 Power Auger



SOIL PROFILE AND TEST DATA

▲ Undisturbed

△ Remoulded

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

**Geotechnical Investigation** Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = FILE NO. **DATUM PG3834** 119.73m. **REMARKS** HOLE NO. **BH10 DATE** June 2, 2016 BORINGS BY CME 55 Power Auger **SAMPLE** Pen. Resist. Blows/0.3m PLOT **DEPTH** ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) RECOVERY N VALUE or RQD STRATA NUMBER Water Content % **GROUND SURFACE** 80 20 0+117.46**TOPSOIL** 0.10 Loose to compact, brown SILTY SAND, some clay 1+116.46SS 1 75 21 1.37 2 SS 58 49 2+115.46Highly fractured **BEDROCK** interbedded with silty sand to sandy silt, some clay with fragmented bedrock 3+114.46SS 3 50+ 80 4 + 113.46End of Borehole Practical refusal to augering at 4.27m depth (GWL @ 3.62m-June 6, 2016) 40 60 100 Shear Strength (kPa)

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

SOIL PROFILE AND TEST DATA

**Geotechnical Investigation** Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

**DATUM** 

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = 119.73m.

FILE NO.

**PG3834** 

**REMARKS** HOLE NO. **BH11 DATE** June 2, 2016 BORINGS BY CME 55 Power Auger **SAMPLE** Pen. Resist. Blows/0.3m PLOT **DEPTH** ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) RECOVERY N VALUE or RQD STRATA NUMBER Water Content % 80 **GROUND SURFACE** 20 0+117.45**TOPSOIL** 1 0.60 Brown SILTY SAND with gravel, cobbles and boulders, trace clay and 1+116.45SS 2 70 11 organics SS 3 75 62 Highly fractured **BEDROCK** 2+115.45interbedded with silty sand to sandy silt, some clay with fragmented bedrock 3+114.45End of Borehole Practical refusal to augering at 3.05m (Piezometer blocked at 1.72m depth - June 6, 2016) 40 60 100 Shear Strength (kPa) ▲ Undisturbed △ Remoulded

1.30 ₽

**SOIL PROFILE AND TEST DATA** 

40

▲ Undisturbed

Shear Strength (kPa)

60

△ Remoulded

100

**Geotechnical Investigation** Proposed Storage Building - 2978 & 2966 Carp Road 154 Colonnade Road South, Ottawa, Ontario K2E 7J5 Ottawa, Ontario TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = FILE NO. **DATUM PG3834** 119.73m. **REMARKS** HOLE NO. TP 1 **BORINGS BY** Backhoe DATE November 3, 2016 **SAMPLE** Pen. Resist. Blows/0.3m STRATA PLOT **DEPTH** ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) N VALUE or RQD RECOVERY NUMBER Water Content % 80 **GROUND SURFACE** 20 0+117.72**TOPSOIL** 1 0.20 Brown SILTY SAND to SANDY SILT, some tree roots G 2 1+116.721.20

End of Test Pit

TP terminated on fractured bedrock surface at 1.30m depth

(TP dry upon completion)

Highly fractured **BEDROCK** with

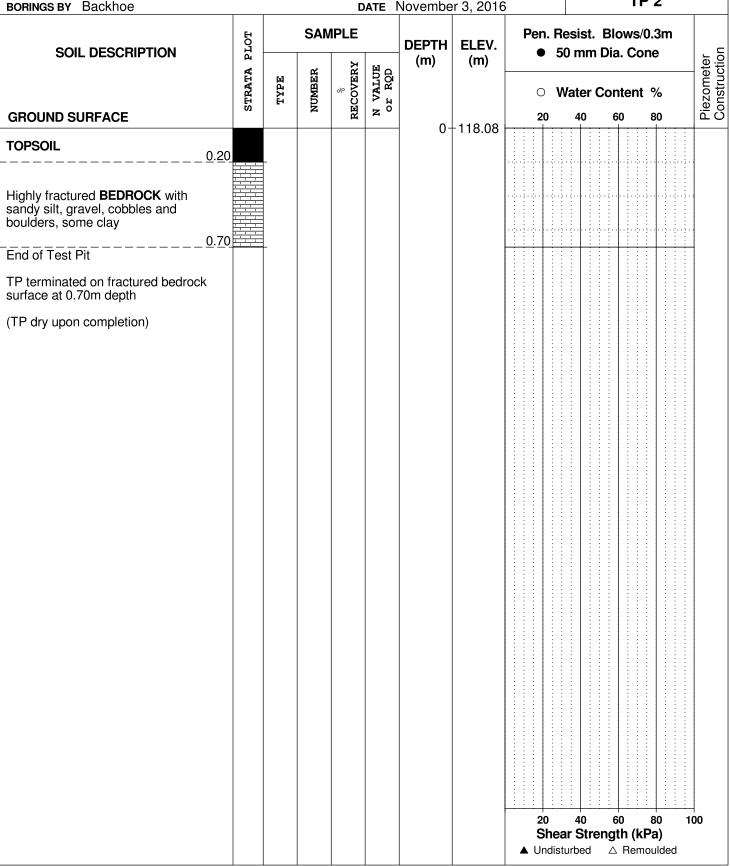
sandy silt, gravel, cobbles and

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

**Geotechnical Investigation** Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

**SOIL PROFILE AND TEST DATA** 

DATUM	TBM - Top of magnetic na 119.73m.	FILE NO. PG3834	
REMARKS BORINGS BY	r Backhoe	DATE November 3, 2016	HOLE NO. TP 2
Borning B	Backing	BAIL NOVOINSOI 0, 2010	



**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = FILE NO. **DATUM PG3834** 119.73m. **REMARKS** HOLE NO. TP 3 **BORINGS BY** Backhoe DATE November 3, 2016 **SAMPLE** Pen. Resist. Blows/0.3m PLOT DEPTH ELEV. Piezometer Construction **SOIL DESCRIPTION** • 50 mm Dia. Cone (m) (m) N VALUE or RQD RECOVERY STRATA NUMBER Water Content % **GROUND SURFACE** 80 20 0+117.47**TOPSOIL** 0.20 Brown SILTY SAND to SANDY SILT 0.50 Highly fractured **BEDROCK** with 1+116.47sandy silt, gravel, cobbles and boulders, some clay End of Test Pit TP terminated on fractured bedrock surface at 1.60m depth (TP dry upon completion) 40 60 100 Shear Strength (kPa) ▲ Undisturbed △ Remoulded

**SOIL PROFILE AND TEST DATA** 

**Geotechnical Investigation** 

Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = 119.73m.

FILE NO. PG3834

**REMARKS** 

**DATUM** 

PODINGS BY Rackhoo				<u> </u>	ATE I	Novembo	r 2 2016	<u>.</u>		Н	OLE	NO.	TP	4	
SOIL DESCRIPTION	PLOT			/IPLE		Novembe DEPTH (m)	ELEV. (m)	Pen. Resist. Blows/0.3			.3m	er			
	STRATA	TYPE	NUMBER	% RECOVERY	N VALUE or RQD		, ,		0	Wat	er C	onte	ent	%	Piezometer Construction
GROUND SURFACE	02			8	Z	0-	 -117.46	ļ	20	4	0	60		80	اعتِ ح
TOPSOIL	0	_ G	и 1	REC	N CO	. 0-	-117.46		20		0	60		80	

**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

Shear Strength (kPa)

△ Remoulded

▲ Undisturbed

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = FILE NO. **DATUM PG3834** 119.73m. **REMARKS** HOLE NO. TP 5 **BORINGS BY** Backhoe DATE November 3, 2016 **SAMPLE** Pen. Resist. Blows/0.3m PLOT **DEPTH** ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) N VALUE or RQD RECOVERY STRATA NUMBER Water Content % **GROUND SURFACE** 80 20 0+118.06**TOPSOIL** 0.20 Brown SANDY SILT with clay to G 1 SILTY SAND 0.50 Highly fractured **BEDROCK** with sandy silt, gravel, cobbles and boulders, some clay 1 + 117.06End of Test Pit TP terminated on fractured bedrock surface at 1.30m depth (TP dry upon completion) 40 60 100

**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

TBM - Top of magnetic nai 119.73m.	l in u	in utility pole on Carp Road. Geodetic elevation =					FILE NO. PG3834						
REMARKS BORINGS BY Backhoe	DATE November 3, 2016  HOLE NO. TP 6												
SOIL DESCRIPTION			SAN	IPLE		DEPTH	ELEV.	Pen. Re			ows/0.3 . Cone		r.
	STRATA PLOT	TYPE	NUMBER	% RECOVERY	N VALUE or RQD	(m)	(m)				tent %		Piezometer Construction
GROUND SURFACE	ST	H	Ŋ	REC	N			20	40	60			Piez
TOPSOIL 0.10						0+	-118.08						
Highly fractured <b>BEDROCK</b>													
End of Test Pit		-											
TP terminated on fractured bedrock surface at 0.40m depth													
(TP dry upon completion)													
								20	40	6	0 8	D 10	00
								Shea  ▲ Undisti	r Str	engt	h (kPa	)	

**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = FILE NO. **DATUM PG3834** 119.73m. **REMARKS** HOLE NO. TP 7 **BORINGS BY** Backhoe DATE November 3, 2016 **SAMPLE** Pen. Resist. Blows/0.3m PLOT DEPTH ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) N VALUE or RQD RECOVERY STRATA NUMBER Water Content % **GROUND SURFACE** 80 20 0+117.37TOPSOIL 0.15 Brown SILTY SAND 1 G Highly fractured **BEDROCK** with silty clay, sand, gravel, cobbles and boulders 1 + 116.37End of Test Pit TP terminated on fractured bedrock surface at 1.10m depth (TP dry upon completion) 40 60 100 Shear Strength (kPa) ▲ Undisturbed △ Remoulded

SOIL PROFILE AND TEST DATA

Shear Strength (kPa)

△ Remoulded

▲ Undisturbed

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation
Proposed Storage Building - 2978 & 2966 Carp Road
Ottawa, Ontario

Ottawa, Ontario TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = FILE NO. **DATUM PG3834** 119.73m. **REMARKS** HOLE NO. TP8 **BORINGS BY** Backhoe DATE November 3, 2016 **SAMPLE** Pen. Resist. Blows/0.3m STRATA PLOT **DEPTH** ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) N VALUE or RQD RECOVERY NUMBER Water Content % **GROUND SURFACE** 80 20 0+118.54Crushed stone 0.05 **TOPSOIL** 0.20 Brown SILTY SAND, trace gravel 0.80 1 + 117.54Highly fractured **BEDROCK** with brown silty sand, gravel and cobbles, trace boulders G 1 End of Test Pit TP terminated on fractured bedrock surface at 1.50m depth (TP dry upon completion) 40 60 100

SOIL PROFILE AND TEST DATA

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = FILE NO. **DATUM PG3834** 119.73m. **REMARKS** HOLE NO. TP 9 **BORINGS BY** Backhoe DATE November 3, 2016 **SAMPLE** Pen. Resist. Blows/0.3m STRATA PLOT DEPTH ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) RECOVERY N VALUE or RQD NUMBER Water Content % **GROUND SURFACE** 80 20 0+118.16**TOPSOIL** 0.20 Brown SILTY SAND with clay and fractured bedrock by 0.4m depth 0.65 G 1 Highly fractured **BEDROCK** with 1+117.16grey-brown silty sand, gravel, cobbles and boulders End of Test Pit TP terminated on fractured bedrock surface at 1.5m depth (TP dry upon completion) 40 60 100 Shear Strength (kPa) ▲ Undisturbed △ Remoulded

SOIL PROFILE AND TEST DATA

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

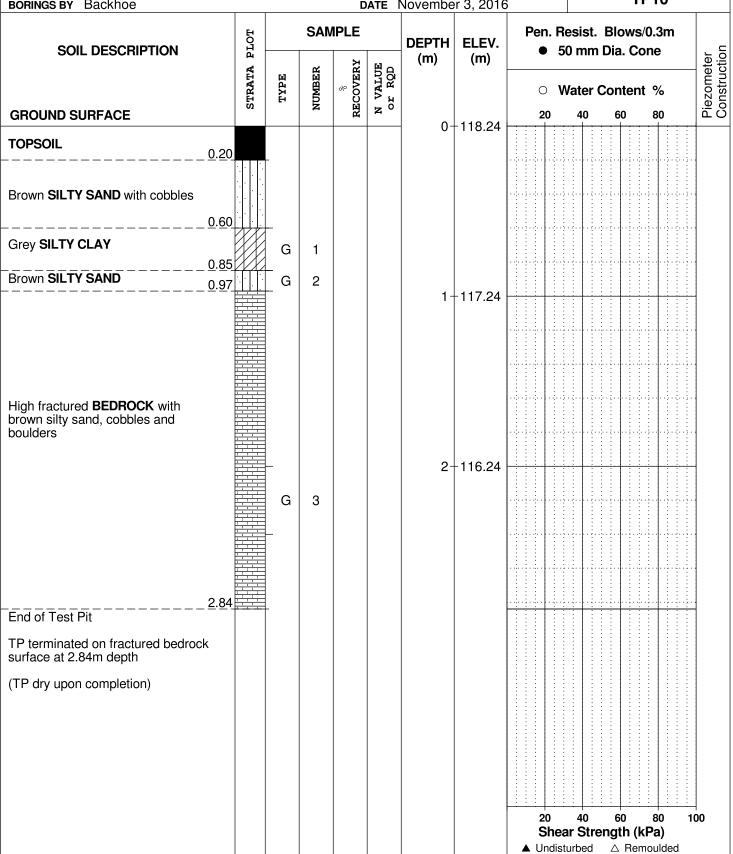
TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = PG3834

REMARKS

BORINGS BY Backhoe

DATE November 3, 2016

Pen. Resist. Blows/0.3m



**SOIL PROFILE AND TEST DATA** 

▲ Undisturbed

△ Remoulded

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = **DATUM** FILE NO. **PG3834** 119.73m. **REMARKS** HOLE NO. **TP11 BORINGS BY** Backhoe DATE November 8, 2016 **SAMPLE** Pen. Resist. Blows/0.3m PLOT DEPTH ELEV. Piezometer Construction SOIL DESCRIPTION 50 mm Dia. Cone (m) (m) RECOVERY N VALUE or RQD STRATA NUMBER Water Content % **GROUND SURFACE** 80 20 0+117.97TOPSOIL 0.15 Brown SILTY FINE SAND, some gravel, cobbles, boulders, trace clay and organics G 1 1 + 116.971.20 Highly fractured **BEDROCK** interbedded with sandy silt, some clay with fragmented bedrock throughout 2+115.97End of Test Pit TP terminated on fractured bedrock surface at 2.45m depth (TP dry upon completion) 40 60 100 Shear Strength (kPa)

**Geotechnical Investigation** 

Proposed Storage Building - 2978 & 2966 Carp Road

**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

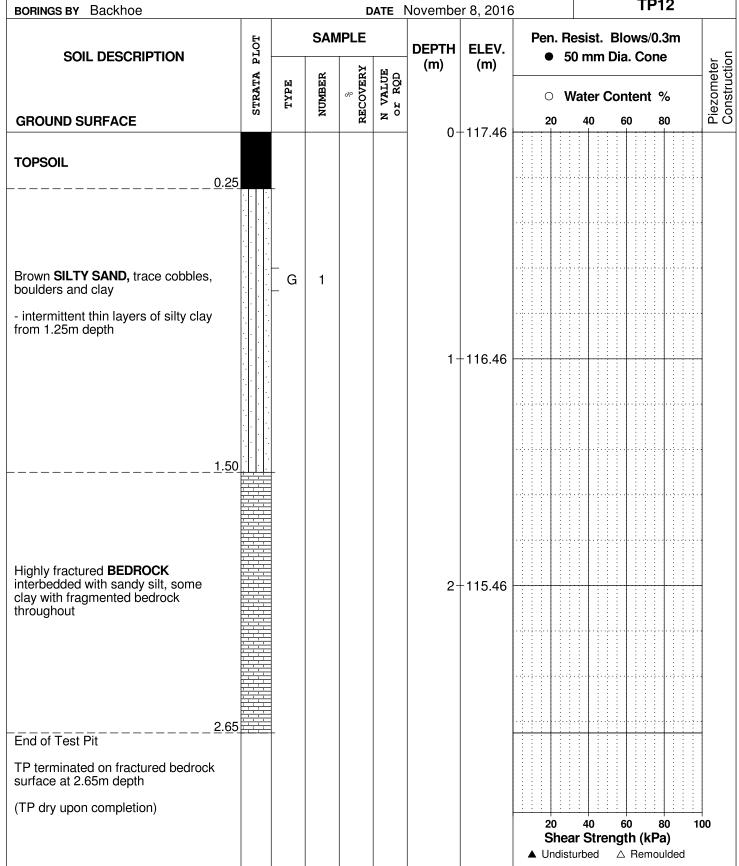
Ottawa, Ontario

**DATUM REMARKS**  TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = 119.73m.

FILE NO.

**PG3834** 

HOLE NO. **TP12** 



**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = FILE NO. **DATUM PG3834** 119.73m. **REMARKS** HOLE NO. **TP13 BORINGS BY** Backhoe DATE November 8, 2016 **SAMPLE** Pen. Resist. Blows/0.3m STRATA PLOT DEPTH ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) RECOVERY N VALUE or RQD NUMBER Water Content % 80 **GROUND SURFACE** 20 0+117.43**TOPSOIL** 0.25 Brown SILTY SAND, some clay and tree roots, trace gravel, cobbles and boulders G 1 1.00 1 + 116.43Highly fractured **BEDROCK** interbedded with sandy silt, some clay with fragmented bedrock throughout End of Borehole TP terminated on fractured bedrock surface at 1.80m depth (TP dry upon completion) 40 60 100 Shear Strength (kPa) ▲ Undisturbed △ Remoulded

**SOIL PROFILE AND TEST DATA** 

40

▲ Undisturbed

Shear Strength (kPa)

60

△ Remoulded

100

**Geotechnical Investigation** Proposed Storage Building - 2978 & 2966 Carp Road 154 Colonnade Road South, Ottawa, Ontario K2E 7J5 Ottawa, Ontario TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = **DATUM** FILE NO. **PG3834** 119.73m. **REMARKS** HOLE NO. **TP14 BORINGS BY** Backhoe DATE November 8, 2016 **SAMPLE** Pen. Resist. Blows/0.3m PLOT DEPTH ELEV. Piezometer Construction SOIL DESCRIPTION • 50 mm Dia. Cone (m) (m) RECOVERY N VALUE or RQD STRATA NUMBER Water Content % **GROUND SURFACE** 80 20 0+117.91**TOPSOIL** 0.20 Brown SILTY FINE SAND, some gravel, cobbles and boulders 0.55 1 + 116.91Highly fractured **BEDROCK** interbedded with sandy silt, some clay with fragmented bedrock G 1 throughout

End of Test Pit TP terminated on fractured bedrock at 1.85m depth (TP dry upon completion)

## **SYMBOLS AND TERMS**

#### **SOIL DESCRIPTION**

Behavioural properties, such as structure and strength, take precedence over particle gradation in describing soils. Terminology describing soil structure are as follows:

Desiccated	-	having visible signs of weathering by oxidation of clay minerals, shrinkage cracks, etc.
Fissured	-	having cracks, and hence a blocky structure.
Varved	-	composed of regular alternating layers of silt and clay.
Stratified	-	composed of alternating layers of different soil types, e.g. silt and sand or silt and clay.
Well-Graded	-	Having wide range in grain sizes and substantial amounts of all intermediate particle sizes (see Grain Size Distribution).
Uniformly-Graded	-	Predominantly of one grain size (see Grain Size Distribution).

The standard terminology to describe the strength of cohesionless soils is the relative density, usually inferred from the results of the Standard Penetration Test (SPT) 'N' value. The SPT N value is the number of blows of a 63.5 kg hammer, falling 760 mm, required to drive a 51 mm O.D. split spoon sampler 300 mm into the soil after an initial penetration of 150 mm.

Relative Density	'N' Value	Relative Density %		
Very Loose	<4	<15		
Loose	4-10	15-35		
Compact	10-30	35-65		
Dense	30-50	65-85		
Very Dense	>50	>85		

The standard terminology to describe the strength of cohesive soils is the consistency, which is based on the undisturbed undrained shear strength as measured by the in situ or laboratory vane tests, penetrometer tests, unconfined compression tests, or occasionally by Standard Penetration Tests.

Consistency	Undrained Shear Strength (kPa)	'N' Value
Very Soft	<12	<2
Soft	12-25	2-4
Firm	25-50	4-8
Stiff	50-100	8-15
Very Stiff	100-200	15-30
Hard	>200	>30

### **SYMBOLS AND TERMS (continued)**

### **SOIL DESCRIPTION (continued)**

Cohesive soils can also be classified according to their "sensitivity". The sensitivity is the ratio between the undisturbed undrained shear strength and the remoulded undrained shear strength of the soil.

Terminology used for describing soil strata based upon texture, or the proportion of individual particle sizes present is provided on the Textural Soil Classification Chart at the end of this information package.

#### **ROCK DESCRIPTION**

The structural description of the bedrock mass is based on the Rock Quality Designation (RQD).

The RQD classification is based on a modified core recovery percentage in which all pieces of sound core over 100 mm long are counted as recovery. The smaller pieces are considered to be a result of closely-spaced discontinuities (resulting from shearing, jointing, faulting, or weathering) in the rock mass and are not counted. RQD is ideally determined from NXL size core. However, it can be used on smaller core sizes, such as BX, if the bulk of the fractures caused by drilling stresses (called "mechanical breaks") are easily distinguishable from the normal in situ fractures.

RQD %	ROCK QUALITY
90-100	Excellent, intact, very sound
75-90	Good, massive, moderately jointed or sound
50-75	Fair, blocky and seamy, fractured
25-50	Poor, shattered and very seamy or blocky, severely fractured
0-25	Very poor, crushed, very severely fractured

#### SAMPLE TYPES

SS	-	Split spoon sample (obtained in conjunction with the performing of the Standard Penetration Test (SPT))
TW	-	Thin wall tube or Shelby tube
PS	-	Piston sample
AU	-	Auger sample or bulk sample
ws	-	Wash sample
RC	-	Rock core sample (Core bit size AXT, BXL, etc.). Rock core samples are obtained with the use of standard diamond drilling bits.

### **SYMBOLS AND TERMS (continued)**

#### **GRAIN SIZE DISTRIBUTION**

MC% - Natural moisture content or water content of sample, %

LL - Liquid Limit, % (water content above which soil behaves as a liquid)
PL - Plastic limit, % (water content above which soil behaves plastically)

PI - Plasticity index, % (difference between LL and PL)

Dxx - Grain size which xx% of the soil, by weight, is of finer grain sizes

These grain size descriptions are not used below 0.075 mm grain size

D10 - Grain size at which 10% of the soil is finer (effective grain size)

D60 - Grain size at which 60% of the soil is finer

Cc - Concavity coefficient =  $(D30)^2 / (D10 \times D60)$ 

Cu - Uniformity coefficient = D60 / D10

Cc and Cu are used to assess the grading of sands and gravels:

Well-graded gravels have: 1 < Cc < 3 and Cu > 4 Well-graded sands have: 1 < Cc < 3 and Cu > 6

Sands and gravels not meeting the above requirements are poorly-graded or uniformly-graded.

Cc and Cu are not applicable for the description of soils with more than 10% silt and clay

(more than 10% finer than 0.075 mm or the #200 sieve)

#### **CONSOLIDATION TEST**

p'<sub>o</sub> - Present effective overburden pressure at sample depth

p'c - Preconsolidation pressure of (maximum past pressure on) sample

Ccr - Recompression index (in effect at pressures below p'c)
Cc - Compression index (in effect at pressures above p'c)

OC Ratio Overconsolidaton ratio =  $p'_c / p'_o$ 

Void Ratio Initial sample void ratio = volume of voids / volume of solids

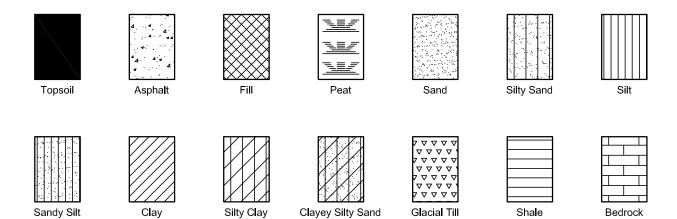
Wo - Initial water content (at start of consolidation test)

#### PERMEABILITY TEST

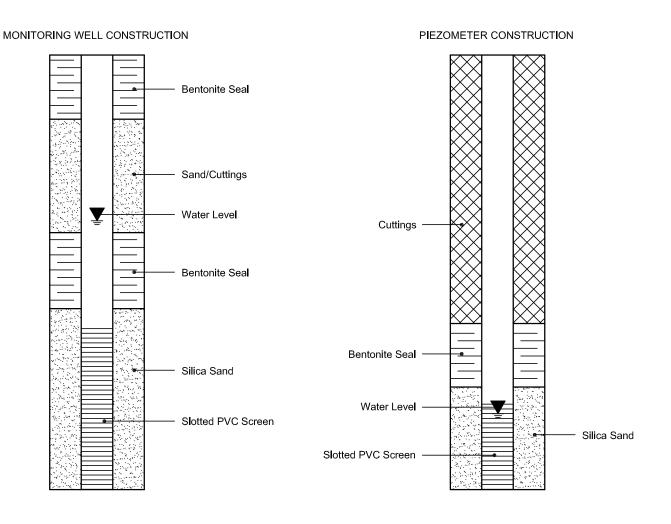
Coefficient of permeability or hydraulic conductivity is a measure of the ability of water to flow through the sample. The value of k is measured at a specified unit weight for (remoulded) cohesionless soil samples, because its value will vary with the unit weight or density of the sample during the test.

## SYMBOLS AND TERMS (continued)

### STRATA PLOT

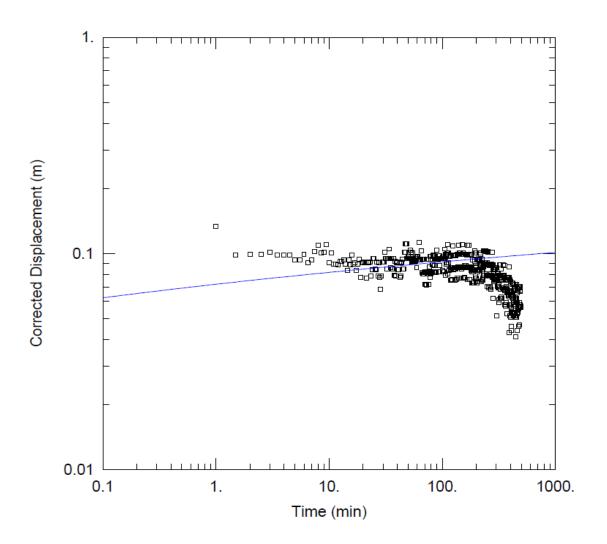


### MONITORING WELL AND PIEZOMETER CONSTRUCTION



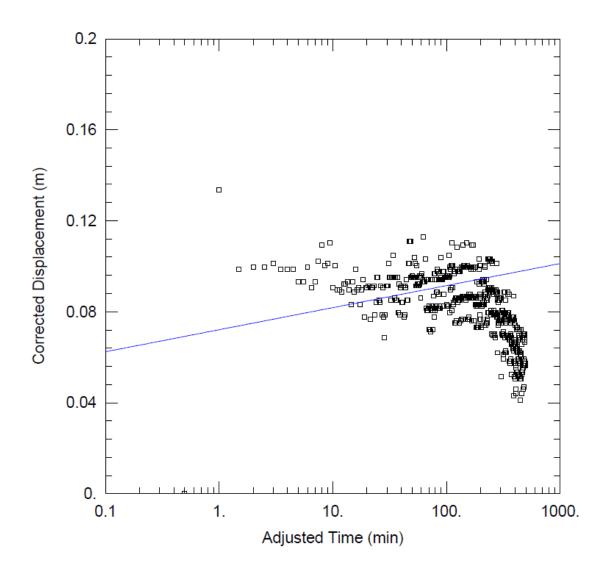
## **Pumping Test Analysis Report**

File No.	PH4484	Well ID:	TW1
Date:	April 13, 2022	Solution Method:	Theis
Client:	Nautical Lands Group	Transmissitivity (m2/day):	1224.1
Site Address:	2966 Carp Road, Ottawa	Discharge Rate (L/min)	45
Project:	Site Plan Application	Analysis performed by:	EA



## **Pumping Test Analysis Report**

File No.	PH4484	Well ID:	TW1
Date:	April 13, 2022	Solution Method:	Cooper-Jacob
Client:	Nautical Lands Group	Transmissitivity (m2/day):	1224.1
Site Address:	2966 Carp Road, Ottawa	Discharge Rate (L/min)	45
Project:	Site Plan Application	Analysis performed by:	EA



### **Pumping Test Analysis Report**

File No. PH4484

Date: April 13, 2022

Client: Nautical Lands Group

Site Address: 2966 Carp Road, Ottawa

Project: Site Plan Application

Summary Table:							
Solution Method:	Well ID:	Transmissitivity (m2/day):					
Theis	TW1	1224.1					
Cooper-Jacob	TW1	1224.1					
Average:		1224.10					

## patersongroup

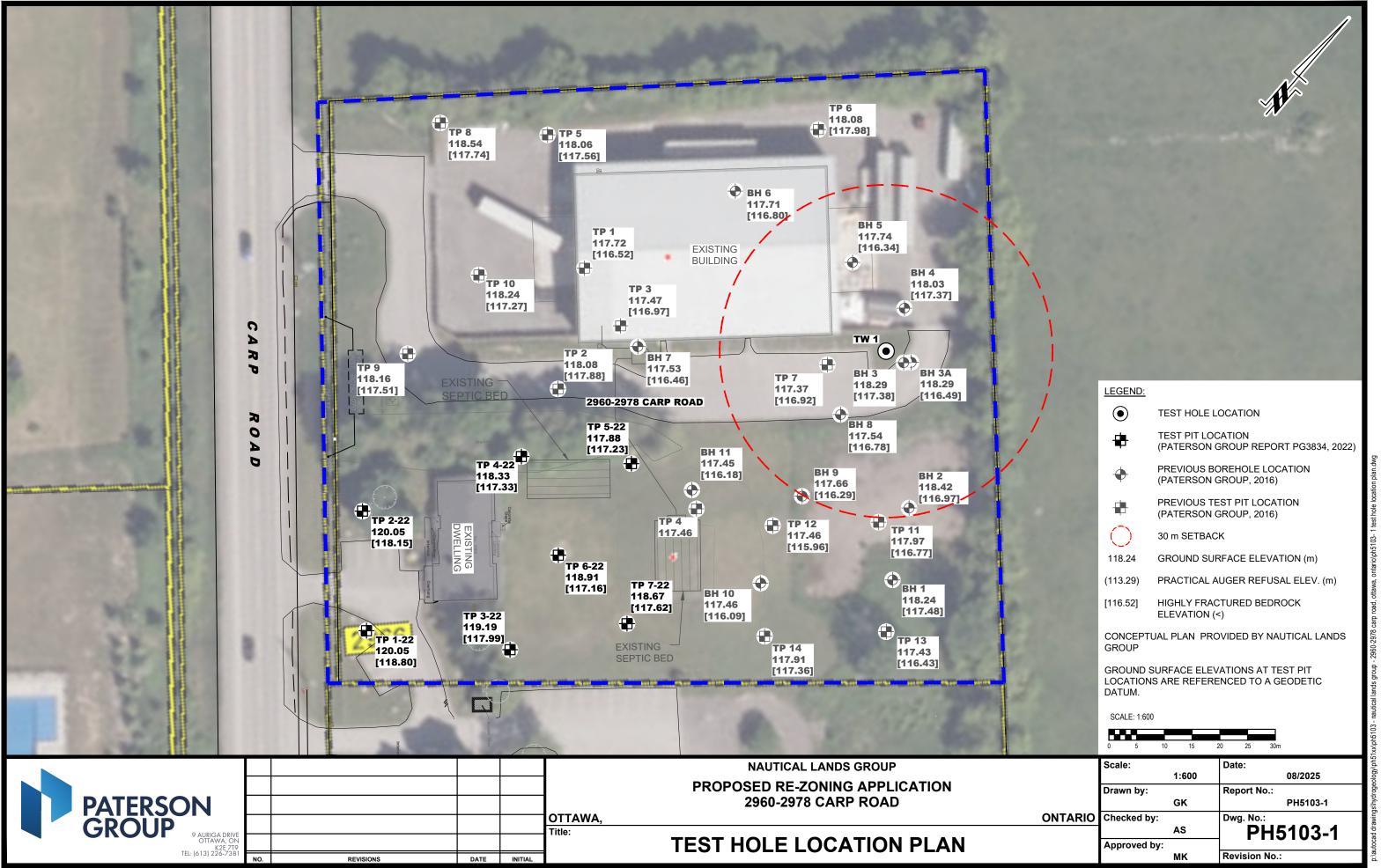
## 2966 Carp Road, Ottawa PH4484

TW1	inputs		
pН	7.93	A	0.19
TDS	767	В	2.37
Hardness	451	С	2.25
Alkalinity	243	D	2.39
Temp.	10.8		
		pHs =	7.215174149

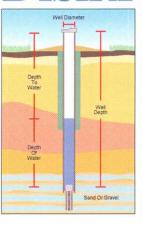
Langel	ier Saturation Index (LSI) Calcu	ulation	(Langelier, 1936)			
	LSI = pH - pHs $A = (Log10 [TDS] - 1) / 10$ pHs = $(9.3 + A + B) - (C + D)$ $B = -13.12 \times Log10 (oC + 273) + 34.55$ Where: $C = Log10 [Ca2 + as CaCO3] - 0.4$ D = Log10 [alkalinity as CaCO3]					
		LSI =	0.7			
LSI	Effect					
0.5 to 2	Water is super saturated and tends to precipitate a scale la	yer of calcium carbonate (scale	forming but non-corrosive)			
0 to 0.5	Water is super saturated and tends to precipitate a scale la	yer of calcium carbonate (sligh	tly scale forming and corrosiv	e).		
0	Water is saturated (in equilibrium) with calcium carbonate. A scale layer of calcium carbonate is neither precipitated nor dissolved.					
0 to -0.5	Water is under saturated and tends to dissolve solid calcium carbonate (slightly corrosivebut non-scale forming).					
-0.5 to -2	Water is under saturated and tends to dissolve solid calcium carbonate (seriously corrosive).					

PREDICTIVE NITRATE I	<b>MPACT</b>	<b>ASSESS</b>	EMENT
Infiltration Factors			
Topography		0.25	
Soil		0.30	
Cover		0.12	
Total		0.67	
Site Characteristics			
Area of Site :		12832	$m^2$
Total of roof areas:		1713	$m^2$
Total area of paved driveway areas:		4051	$m^2$
Roof + paved driveway areas		5764	$m^2$
Impervious Area		5764	$m^2$
Percent Impervious Area =		45	%
Infiltration Area =		7068	$m^2$
Septic Effluent			
Concentration of Effluent (Cs) =		17.2	mg/L
Infiltration Calculation			
Nitrate concentration in precipitation (C <sub>i</sub> ) =		0	mg/L
Surplus Water (Environment Canada)		378	mm/yr
Factored Water Surplus =		253	mm/yr
Infiltration % due to stormwater management measures		-	%
Infiltration rate from stormwater management measures =		0	mm/yr
Infiltration Flow Entering the System (Q <sub>i</sub> ) =		5	m³/day
Mass Balance Model (MOEE, 1995)			-
$C_T = (Q_b C_b + Q_e C_e + Q_i C_i)/(Q_b + Q_e + Q_i$	) = Cumulative N	itrate Concentration	n
Q <sub>b</sub> = flow entering the system across the upgradient area		0	m³/day
C <sub>b</sub> = background nitrate concentration		0.25	mg/L
Cs = concentration of nitrates in the septic effluent		17.2	mg/L
Q <sub>i</sub> = flow entering the system from infiltration		5	m <sup>3</sup> /day
C <sub>i</sub> = Concentration of nitrates in the infiltrate		0	mg/L
	C <sub>T</sub> =	9.75	mg/L
Maximum Allowable Sewage Flow Volume			-
Daily Sewage Flow (Qs)=	6	3.418279445	$m^3$

PREDICTIVE NITRATE	<b>IMPAC</b>	T ASSESSE	EMENT
Infiltration Factors			
Topography		0.25	
Soil		0.30	
Cover		0.12	
Total		0.67	
Site Characteristics			
Area of Site :		12832	$m^2$
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Roof + paved driveway areas		5764	$m^2$
Impervious Area		5764	$m^2$
Percent Impervious Area =		45	%
Infiltration Area =		7068	$m^2$
Septic Effluent			
Concentration of Effluent (Cs) =		40	mg/L
Infiltration Calculation			
Nitrate concentration in precipitation (C <sub>i</sub> ) =		0	mg/L
Surplus Water (Environment Canada)		378	mm/yr
Factored Water Surplus =		253	mm/yr
Infiltration % due to stormwater management measures		-	%
Infiltration rate from stormwater management measures =		0	mm/yr
Infiltration Flow Entering the System (Q <sub>i</sub> ) =		5	m³/day
Mass Balance Model (MOEE, 1995)			
$C_{T} = (Q_{b}C_{b} + Q_{e}C_{e} + Q_{i}C_{i})/(Q_{b} + Q_{e} + Q_{e}C_{e})$	ગુ <sub>i</sub> ) = Cumulativ	e Nitrate Concentration	
Q <sub>b</sub> = flow entering the system across the upgradient area		0	m³/day
C <sub>b</sub> = background nitrate concentration		0.25	mg/L
Cs = concentration of nitrates in the septic effluent		40	mg/L
Q <sub>i</sub> = flow entering the system from infiltration		5	m³/day
C <sub>i</sub> = Concentration of nitrates in the infiltrate		0	mg/L
	C <sub>T</sub> =	9.75	mg/L
Maximum Allowable Sewage Flow Volume			
Daily Sewage Flow (Qs)=		1.580700227	$m^3$



# Disinfection Instruction Sheet



If your drinking water continues to test positive on repeated submissions, consult your local health unit, which can help you interpret the results of your tests and provide you with advice on what measures you can take to safeguard your drinking water.

The first step in identifying the reason for repeated adverse water quality is to conduct a visual inspection of your well. Start with a close look at your well. The area around it should be

clear of any potential contaminant sources, such as pets, lawn care products, and gardens. Once you're satisfied that the area around your well is okay, take a good, close look at the well itself. If you have an older well, make sure that the cap and the sealant around the well casing isn't cracked or damaged. If it is, you need to fix or replace it right away. If the source of the problem can't be detected, consult a licensed well contractor right away to identify the source of the problem and eliminate it. You can save yourself a lot

a licensed well contractor right away to identify the source of the problem and eliminate it. You can save yourself a lot of money by doing this instead of rushing out to buy a home treatment device that may be expensive to install, operate, and maintain. And it may not eliminate the source of your trouble.

(If you have a cistern, please talk to your public health unit about disinfection requirements.)

- 1. Measure the diameter of the well.
- 2. Measure the well depth and the static or resting water level, then calculate the depth of water in the well.
- 3. Using the table on this sheet, measure out the amount of bleach needed. (The table gives the volume of bleach needed for different well sizes.) Then, pour the mixture into your well.
- 4. If possible, mix the water in the well. This can be accomplished by attaching a hose to a tap, running water from the well, through the hose and back into the well.
- 5. After adding chlorine to the well, remove or bypass any carbon filters that are in the system for water treatment. If you don't, these filters will remove the chlorine from the water, and any pipes beyond the filter will not get disinfected. Replace with new filters after chlorination to avoid reintroducing bacteria into the system.
- 6. Run water at every faucet in the house (and barn, if you have one) until a strong chlorine odour is detected. Be aware that your nose may lose its ability to detect chlorine.
- 7. If there is no chlorine smell or it is very weak, add more bleach to the well and repeat Step 6 above.

10. Let the chlorinated water

stand in the system for at

11. Clear chlorine from the well by running an outside hose to the ground surface.

Then, run clear water through

no longer smells of chlorine.

12. Avoid putting too much

chlorine into the septic system

because the bacteria needed

for septic decomposition may

13. Do not drink the water

without boiling it until test

results show the water is

safe to drink.

the faucets until the water

least 12 hours.

- 8. Drain the water heater and fill with chlorinated water.
- 9. Backflush the water softener and all water filters (except carbon filters).

Casing Di	ameter	Volume of Unscented Bleach (5.25% solution)		
'es	Inches	Millilitres		
	2	6		
	4	30		
	6	60		
	8	100		
	10	200		
	12	250		
	16	400		
	20	650		
	24	900		
	36	2000 (2 litres)		

**For example:** If you have 6 metres (20 feet) of water in your well and it has a casing diameter of 100 mm or 4 inches, you would add 60 mm or 2 fluid ounces of bleach.

48

Volume of Bleach to Add for Every 3 Me

\* For questions or more information on how to disinfect your well, contact your local health unit.

## For more information

### Ontario Government Ministry Abbreviations

Ministry of Health and Long-Term Care MOHLTC (also MOH)

Ministry of the Environment MOE (also MOEE)

Millimetr

50

100

150

200

250

 $\frac{300}{400}$ 

500 600

900

1200

Ontario Ministry of Agriculture and Food OMAF (also OMAFRA)

## Ontario Government Information Lines

MOE Public Information Centre: 1-800-565-4923

MOE Water Well Records: 1-888-396-9355

MOHLTC INFOline: 1-800-268-1154

OMAF Agricultural Information Contact Centre: 1-877-424-1300

#### Ontario Government Web Sites

MOE: www.ene.gov.on.ca

MOHLTC: www.health.gov.on.ca

OMAF: www.gov.on.ca/omaf

## Publications available on-line

Health Canada: www.hc-sc.gc.ca

3600 (3.6 litres)

- ${\color{red} \bullet}\ A\ Guide\ to\ Well\ Water\ Treatment\ and\ Maintenance;$
- Water treatment devices for disinfection of drinking water.

## MOHLTC: www.health.gov.on.ca

- How to use water safely during a "Boil Water Advisory";
- E. coli Bacteria;
- List of Public Health Units in Ontario.

#### OMAF: www.gov.on.ca/omaf

- Assessing the Potential for Ground Water Contamination on Your Farm, Publication 97-017;
- Best Management Practices: Water Wells, OMAFRA and Agriculture and Agri-Food Canada, 2003 (to order).

#### MOE: www.ene.gov.on.ca

- Important Facts About Water Well Construction, Publication 3788;
- Water Wells and Groundwater Supplies: The Protection of Water Quality in Bored and Dug Wells, Information Sheet PIB 601b;
- Water Wells and Groundwater Supplies: The Protection of Water Quality in Drilled Wells, Information Sheet PIB 602b.



C.2 Servicing Report - 2978 Carp Road, Stantec, December 21, 2016



## Servicing Report – 2978 Carp Road

Project # 160401271



Prepared for: Nautical Lands Group

Prepared by: Stantec Consulting Ltd.

December 21, 2016

Revision	Description	Author		Quality Check		Independent Review	
1	1 st	T.Rathnasooryia	2016/08/17	A.Lynch	2016/08/18	K. Kilborn	2016/08/17
	submission						
2	2 <sup>nd</sup>	T.Rathnasooryia	2016/11/22	A.Lynch	2016/11/24	K.Kilborn	2016/11/21
	submission						
3	3 <sup>rd</sup>	T.Rathnasooryia	2016/12/13	A.Lynch	2016/12/13	K.Kilborn	2016/12/13
	submission						
4	4 <sup>th</sup>	T.Rathnasooryia	2016/12/20	A.Lynch	2016/12/20	K.Kilborn	2016/12/21
	submission						

## Sign-off Sheet

This document entitled Servicing Report – 2978 Carp Road was prepared by Stantec Consulting Ltd. ("Stantec") for the account of Nautical Lands Group (the "Client"). Any reliance on this document by any third party is strictly prohibited. The material in it reflects Stantec's professional judgment in light of the scope, schedule and other limitations stated in the document and in the contract between Stantec and the Client. The opinions in the document are based on conditions and information existing at the time the document was published and do not take into account any subsequent changes. In preparing the document, Stantec did not verify information supplied to it by others. Any use which a third party makes of this document is the responsibility of such third party. Such third party agrees that Stantec shall not be responsible for costs or damages of any kind, if any, suffered by it or any other third party as a result of decisions made or actions taken based on this document.

Prepared by

(signature)

Thakshika Rathnasooriya, EIT

Reviewed by

(signature)

Amanda Lynch, P.Eng.





## **Table of Contents**

1.0	INTRODUCTION	1.1
2.0	BACKGROUND	2.1
<b>3.0</b> 3.1 3.2	WATER SUPPLY SERVICING  BACKGROUND  PORTABLE WATER DEMANDS	3.1 3.1
3.3	SUMMARY OF FINDINGS	
<b>4.0</b> 4.1	WASTEWATER SERVICING	
<b>5.0</b> 5.1 5.2 5.3	STORMWATER MANAGEMENT.  OBJECTIVES	5.1 5.1 5.1
5.4	5.3.1 Allowable Release Rate	5.2 5.3 5.4 5.6
6.0	GRADING AND DRAINAGE	
7.0	UTILITIES	
8.0	APPROVALS	8.1
9.0	EROSION CONTROL DURING CONSTRUCTION	9.1
10.0	GEOTECHNICAL INVESTIGATION AND ENVIRONMENTAL ASSESSMENT	10.1
<b>11.0</b>	CONCLUSIONS	11.1
11.2 11.3 11.4	STORMWATER SERVICINGGRADINGUTILITIES	11.1
11.5	APPROVALS/PERMITS	



LIST OF TABLE	S
---------------	---

Table	: 1: Allowa	ble Surface Release Rates	5.2
		ary of Infiltration Rates	
		ary of Groundwater and Bedrock Elevations	
		, 100 Year Discharge from Uncontrolled Catchments	
		ar Peak Surface Volume and Controlled Discharge Summary	
		ary of Total Uncontrolled 5 and 100 Year Event Release Rates	
		ent Structure – Car Only Parking Areas	
		ent Structure – Access Lanes	
LIST C	F FIGURES		
Fiaure	e 1: Locati	on Plan	1.1
90	3 11 LOOG!!!		•••••
LIST C	F APPEND	ICES	
APPE	NDIX A	WATER SUPPLY SERVICING	A.1
A.1	Fire Flow	Requirements Per OBC	A.1
APPE	NDIX B	STORMWATER MANAGEMENT	В.1
B.1		Method Calculations	
B.2		vater Mounding Calculations	
В.3		l Rates for Buffer Strips-US EPA design manual for Low Impact	
		ment (LID)	B.3
	·	, ,	
		GEOTECHNICAL INVESTIGATION	
C.1	Excerpts	from Patersongroup Investigation	C.1
A DDE	NDIX D	DRAWINGS	D 1
MLLE	NDIV D	DRAWINGS	ו.ע



Introduction December 21, 2016

### 1.0 INTRODUCTION

Stantec Consulting Ltd. has been commissioned by Nautical Lands Group to prepare a servicing study in support of Site Plan Control submission of the proposed development located at 2978 Carp Road. Currently the site is divided into two parcels of land and is under approval to merge as one, 2978 and 2966 Carp Road (PIN 04537-0266 and 04537-0265). The site is situated southeast of the intersection of McGee Road and Carp Road within the City of Ottawa. The proposed development comprises approximately 1.30ha of land, and would replace a vacant property with a 15,000sq. ft pre-engineered steel storage building on the northern portion of the site. The site is zoned under Rural Commercial. The conceptual site development plan used for the purpose of this servicing brief is shown as **Figure 1**. The intent of this report is to provide a servicing scenario for the site that is free of conflicts, provides on-site servicing in accordance with City of Ottawa design guidelines, and utilizes the existing local infrastructure in accordance with the guidelines outlined per consultation with City of Ottawa staff.

Figure 1: Location Plan





Background December 21, 2016

## 2.0 BACKGROUND

Documents referenced in preparation of the design for the 2978 Carp Road development include:

- Geotechnical Investigation Proposed Storage Building 2978 and 2966 Carp Road, Patersongroup Consulting Engineers, November 11, 2016.
- City of Ottawa Sewer Design Guidelines, October 2012
- Low Impact Development Stormwater Management Planning and Design Guide, Credit Valley Conservation and Toronto Region Conservation Authority, 2010



Water Supply Servicing December 21, 2016

## 3.0 WATER SUPPLY SERVICING

#### 3.1 BACKGROUND

The proposed development comprises one pre-engineered steel storage building, complete with above ground parking and access areas. An existing well feeds the 1 storey building located on the south portion of the site. The proposed storage building will be serviced via a 19mm building service connection from a proposed drilled well located on the north portion of the property directly east of the proposed building. As per the Ministry of Ontario regulations the proponent must hire licensed well contractors which use licensed well technicians for installation of the onsite well, the second of two existing wells is located to the south of the access road and will be decommissioned.

#### 3.2 PORTABLE WATER DEMANDS

Water demands for the development were estimated using the Ministry of Environment's Design Guidelines for Drinking Water Systems (2008).

The assessment for fire flow requirements was completed according to the Ontario Building Code (OBC) criteria using a "non-combustible with fire resistance" rating. The OBC indicates that low hazard occupancies include apartments, dwellings, dormitories, hotels, and schools, and as such, low hazard occupancy / limited combustible building contents credit was applied. Based on calculations per the OBC (**Appendix A.1**), the maximum required fire flows for this development are 75 L/s (4,500 L/min).

Utilizing water storage to supplement low yielding wells to meet fire flow water demands is common practice. Added water storage can be achieved by use of intermediate potable water storage tanks. The storage tanks will receive water from the well that are filled during off peak hours. The facility's water demand requires three portable storage tanks with a total 150,000 L capacity (50,000 L per tank) which is sufficient for the required volume of 149,532 L.

## 3.3 SUMMARY OF FINDINGS

The proposed development is located in an area of the City that will require private servicing to obtain the required domestic and emergency fire flows. The proposed servicing plan will provide sufficient water supply for fire flows for the proposed development based on OBC guidelines and as per the City of Ottawa water distribution guidelines.



Wastewater Servicing December 21, 2016

## 4.0 WASTEWATER SERVICING

### 4.1 BACKGROUND

The subject site is located outside of the City's sanitary collection area. There are no special constraints for the proposed development to be serviced by a private sewage system other than those related to the Ontario Building Code (OBC) requirements. As a result, an existing septic tank and bed with private service is located on the eastern portion of PIN 04537-0265. The proposed building will require installation of a new septic tank and bed located east of the proposed storage building. Mississippi Valley authority permit approval is required. The proposed location is identified on the servicing and grading plans in **Appendix D.1** as provided by the geotechnical consultant.



Stormwater Management December 21, 2016

### 5.0 STORMWATER MANAGEMENT

#### 5.1 OBJECTIVES

The objective of this stormwater management plan is to determine the measures necessary to control the quantity/quality of stormwater released from the proposed development, and to provide sufficient detail for approval and construction.

#### 5.2 SWM CRITERIA AND CONSTRAINTS

Criteria were established by combining current design practices outlined by the City of Ottawa Design Guidelines (2012), and through consultation with City of Ottawa staff. The following summarizes the criteria, with the source of each criterion indicated in brackets:

#### General

- Wherever feasible and practical, site-level measures should be used to reduce and control
  the volume and rate of runoff. (City of Ottawa)
- Assess impact of 100 year event outlined in the City of Ottawa Sewer Design Guidelines on major & minor drainage system (City of Ottawa)
- Water quality treatment to a 'Normal' level (70% TSS reduction) is required for the site per the Mississippi Valley Conservation Authority (MVCA)

#### Surface Storage & Overland Flow

- Building openings to be a minimum of 0.30m above the 100-year water level of any surface storage areas (City of Ottawa)
- Provide adequate emergency overflow conveyance off-site (City of Ottawa)

#### Site Specific Criteria

Site topography indicates that no legal surface outlet exists for the site that would be
feasible to discharge to. As such, on-site storage and infiltration is considered the best
approach to manage site runoff so as to not increase the total uncontrolled runoff from the
site (City of Ottawa and MVCA)

### 5.3 WATER QUANTITY CONTROL

The Modified Rational Method (MRM) was employed to assess the rate and volume of runoff generated during post-development conditions. The site was subdivided into subcatchments



Stormwater Management December 21, 2016

(subareas) tributary to stormwater controls as defined by the location of the proposed dry pond. A summary of subareas and runoff coefficients is provided in **Appendix B.1**, and **Drawing SD-1** indicates the stormwater management subcatchments. A clear stone base is proposed below the dry pond to provide additional storage and encourage infiltration.

#### 5.3.1 Allowable Release Rate

The predevelopment release rate for the area has been determined using the rational method. Existing buildings, paved access areas and gravel access areas were considered as hard surfaces (C=0.9 paved, C=0.75 gravel), while the remainder of the site is grassed (C=0.2). A time of concentration for the predevelopment area (30 minutes) was assigned based on the Airport Method calculations for the relatively pervious nature of the proposed site. Runoff coefficient values have been increased by 25% for the 100-year storm event based on the City of Ottawa Sewer Design Guidelines. Peak flow rates have been calculated using the rational method as follows:

Q = 2.78 CIA
Where: Q = peak flow rate, L/s
A = drainage area, ha
I = rainfall intensity, mm/hr (per Ottawa IDF curves)
C = site runoff coefficient

The allowable release rate for surface discharge for the site is summarized in **Table 1** below:

Table 1: Allowable Surface Release Rates

Design Storm	Target Flow Rate (L/s)
5- Year	50.7
100- Year	86.3

#### 5.3.2 In-situ Infiltration Testing

Field testing was completed by Paterson Group to establish in-situ saturated hydraulic conductivity rates using a Pask Permeameter. The methodology outlined in the Credit Valley Conservation LID Design Guidelines – Appendix C (CVC, 2012) was then used to calculate the infiltration rate and safety factor for each test location. Test results and calculations results are attached for reference and a summary is included in **Table 2** below.



Stormwater Management December 21, 2016

Table 2: Summary of Infiltration Rates

Auger hole ID	K <sub>fs</sub> (cm/min)	Testing Depth below surface (m)	Infiltration Rate (i) (mm/hr)	Safety factor	Corrected Infiltration (mm/hr)
TP 1	3.20E-07	0.90	9.94		3.98
TP 4	9.40E-07	0.60	13.27		5.31
TP 5	9.40E-08	0.70	7.16	2.50	2.87
TP 11	5.30E-06	0.90	21.08	2.50	8.43
TP 12	1.20E-05	1.10	26.23		10.49
TP 13	5.30E-06	1.00	21.08		8.43

#### 5.3.3 Groundwater and Bedrock Elevations

Groundwater level measurements were obtained from the on-site piezometers on June 2016 by Paterson Group. **Table 3** below summarizes the groundwater elevations (a reference plan with borehole locations is included in the attached Paterson letter). Test-pits excavated during the infiltration testing indicated shallow depths to highly fractured bedrock (previously identified as glacial till from the soil cores examined during borehole drilling). In most locations the groundwater elevation is identified to be lower than the fractured bedrock interface. As such, the bedrock elevation was considered to be controlling in establishing the dry pond elevation and footprint.



Stormwater Management December 21, 2016

Table 3: Summary of Groundwater and Bedrock Elevations

Stand-	Top of	Groundwater Elevations			Bedrock Elevation
pipe well ID	Riser Elevation (m)	Date measured (d/m/y)	Groundwater Depth (m) below top of riser	Groundwater Elevation (m)	
BH1	118.24	01/06/16	4.20	114.04	117.48
BH2	118.42	01/06/16			116.97
внз	118.29	01/06/16			117.38
внза	118.29	01/06/16	4.30	113.99	116.49
BH4	118.03	01/06/16			117.37
ВН5	117.74	01/06/16			116.34
ВН6	117.71	01/06/16	3.93	113.78	116.80
BH7	117.53	01/06/16	3.70	113.83	116.46
вн8	117.54	01/06/16	4.19	113.35	116.78
ВН9	117.66	01/06/16			116.29
BH10	117.46	01/06/16	3.62	113.84	116.09
BH11	117.45	01/06/16			116.18

## 5.3.4 Storage Requirements

The site requires quantity control measures to meet the restrictive stormwater release criteria. It is proposed that surface grading (for a dry pond) be used to store site runoff to be infiltrated and limit surface release rates to the allowable existing condition rates.

#### 5.3.4.1 Post-development Uncontrolled Catchments

Due to grading constraints, two catchments have been designed without a storage component (EXT-1 & EXT-2). These areas flow offsite uncontrolled. Areas that discharge offsite without entering the proposed stormwater management system must be compensated for in areas with controls. **Table 4** summarizes the peak 5 and 100-year catchment release rates for catchments that are released uncontrolled.



Stormwater Management December 21, 2016

Table 4: 5 and 100 Year Discharge from Uncontrolled Catchments

Catchment ID	5-Year Peak Discharge (L/s)	100-Year Peak Discharge (L/s)
EXT-1	16.8	36.0
EXT-2	3.5	7.5

Peak 5 and 100 year discharge values in the above table are based on minimum time of concentration values (10 minutes).

#### 5.3.4.2 Surface Storage/Subsurface Storage

It is proposed to detain all stormwater in the pond to reduce peak surface discharge from the proposed site. The modified rational method (MRM) was employed to determine the peak volume required to be stored in surface ponding areas and subsurface clear stone storage basin and trenches.

The stormwater management dry pond and clear stone storage areas were sized using an iterative approach between pond grading, infiltration calculations and the MRM calculations to provide enough storage to restrict runoff from the 100 year event and meet the target release rates from the overall site and external areas. The release rate from the pond storage was calculated based on infiltration rates and pond footprint and was then input into the MRM calculations as the "controlled release rate" from drainage area STM-1. Note that the average flow rate over the pond storage depth was used. The entirety of the required storage volume is provided within the dry pond. Drawdown calculations indicate that a minimum infiltration rate of 8.3mm/hr would be needed to achieve a pond drawdown time of 48hr. In-situ infiltration testing included testing at two test pits (TP 11 and TP 12) in the footprint of the infiltration area and based on the values in Table 2 would have an average measured infiltration rate of approximately 9.46mm/hr. Therefore, it is estimated that the facility would drawdown in less than 48hrs following a 100-yr event.

**Table 5** summarizes the estimated pond discharge rate resulting from infiltration and corresponding storage volume during the 100-year event.

Table 5: 100 Year Peak Surface Volume and Controlled Discharge Summary

	100-Year Event				
ID	Discharge Rate (L/s)	Vrequired (m³)	Vavailable (m³)		
Pond	9.8	385.3	389.6		

100-year volume available based on surface storage and a maximum spill depth not to exceed 0.40m, where required.



Stormwater Management December 21, 2016

**Table 6** demonstrates the proposed stormwater management plan and confirms that the estimated release rates from the site are less than the allowable rate.

Table 6: Summary of Total 5 and 100 Year Event Surface Release Rates

	5-Year Peak Discharge (L/s)	100-Year Peak Discharge (L/s)
Uncontrolled (EXT-1 & EXT-2)	20.3	43.5
Allowable	50.7	86.3

### 5.3.5 Groundwater Mounding Check

Geotechnical investigations indicated shallow depths to highly fractured bedrock but did not encounter groundwater before the fractured bedrock interface. Therefore, the clearance from bedrock was the control in setting the base elevation of the infiltration basin area. The clearance from the bottom of the infiltration area and the referenced bedrock elevation is less than 1m, therefore mounding calculations were completed as a final check for the longer-term function of the infiltration area. Groundwater mounding calculations were completed using spreadsheet analysis tool developed by the USGS that applies the Hantush (1967) equation for groundwater mounding beneath an infiltration basin. Standard values for site soils and measured hydraulic conductivity rates were used. The maximum mounding depth was calculated to be approximately 0.002m resulting in a clearance from infiltration bottom to mounded groundwater of 0.11m. Spreadsheet calculations are included in **Appendix B.2.** 



Stormwater Management December 21, 2016

### 5.4 WATER QUALITY CONTROL

Water quality treatment to a 'Normal' level of protection (70% TSS removal) is required for the site per the MVCA. In order to achieve this level of treatment several a treatment train approach is proposed for the site. The proposed site drainage allows for most of the site to sheet drain across the grassed area around the dry pond rather than concentrated flow into the pond. This will allow for an initial filtering and settling of solids. Secondly, a 33m long (measured perpendicular to flow direction) vegetated buffer is proposed around the dry pond. Based on **Figure 5-4** from the US EPA design manual for Low Impact Development (LID) (see **Appendix B.3**), it is estimated that this configuration would provide an initial treatment rate of 60% to 90% TSS reduction before the runoff enters the dry pond. However, lower removal rates are anticipated in areas of steeper slopes. Additionally, these values assume that the design buffer width (in direction of flow) can be achieved in all areas. Equation 5-2 of the EPA LID manual defines the minimum buffer width as

W<sub>G</sub>= 0.2L<sub>I</sub> or 8ft (whichever is greater)

Where,  $W_G$  = Design width (m)

 $L_{l}$  = length of flow path of upstream sheet flow (m)

Using an average flow path length of 55m would require a minimum vegetated buffer of 11.0m. Due to area and constraints the proposed vegetated buffer length will vary between 3.5m and 10m along the north and east sides of the pond. Therefore, it is estimated that some areas may provide lower or higher filtration of solids, but an average of near 70% removal could be achieved.

While the vegetated buffer will provide significant pre-treatment of runoff, additional settling and filtration will occur in the dry pond. The MOECC SWM Design Manual (2003) recognizes dry ponds as providing approximately 60% TSS removal. This removal rate is identified for a typical dry pond with a gravity outlet to a sewer or watercourse and does not include the filtration benefits achieved from the infiltration outlet of the proposed dry pond.

Therefore, with the various proposed measures it is estimated that at least 70% TSS removal will be achieved through the system.



Grading and Drainage December 21, 2016

## 6.0 GRADING AND DRAINAGE

The proposed development site measures approximately 1.30ha (3.22 acre) in area and is currently partly developed. The topography across the site is relatively flat, and the entirety of the site currently drains from west to east. A detailed grading plan (see **Drawing GP-1**) has been provided to satisfy the stormwater management requirements for the site. Site grading has been established to provide emergency overland flow routes required for stormwater management in accordance with City of Ottawa requirements.

The subject site maintains emergency overland flow routes for runoff from events exceeding the 100-year design event to the eastern portion of the development where major system flows are presently draining as depicted in **Drawing GP-1**.



Utilities
December 21, 2016

### 7.0 UTILITIES

Hydro overhead lines exist along Carp Road. It is anticipated that existing infrastructure will be sufficient to provide a means of distribution for the proposed site under interim and ultimate conditions. Consultation with Hydro Ottawa will continue throughout the Composite Utility Planning process. Exact size, location, and routing of hydro utilities, as well as required transformer locations, will be finalized after design circulation.

Bell lines are expected to be able to service the proposed site via infrastructure within Carp Road. Bell may require easements for their respective cabinets and vaults. Easement requirements and location of telecommunication infrastructure will be determined as part of the Composite Utility Planning process, following design circulation.

### 8.0 APPROVALS

Consultation with the Ministry of the Environment and Climate Change (MOECC) will be completed to confirm whether an Environmental Compliance Approval (ECA, formerly Certificates of Approval (CofA) will be necessary for stormwater management (Correspondence included in **Appendix D**).

Will require approval for septic tank, line and bed from the Ottawa Septic System Office by way of OSSO permit. The Mississippi Valley Conservation authority permit approval is required for the septic tank and bed.



Erosion Control During Construction December 21, 2016

### 9.0 EROSION CONTROL DURING CONSTRUCTION

Erosion and sediment controls must be in place during construction. The following recommendations to the contractor will be included in contract documents.

It is noted that the site stormwater management is dependent on infiltration for release of stored runoff. As such, all infiltration trenches and basins shall be constructed after all other site grading and construction is complete. The SWM dry pond depression may be excavated during construction if they are required for stormwater management during construction. However, they should not be excavated to the depth of the infiltration areas until all other site works are complete. All accumulated sediment will need to be excavated from the pond and infiltration testing shall be completed before placing clear stone and geotextiles etc.

- 1. Implement best management practices to provide appropriate protection of the existing and proposed drainage system and the receiving water course(s).
- 2. Limit extent of exposed soils at any given time.
- 3. Re-vegetate exposed areas as soon as possible.
- 4. Minimize the area to be cleared and grubbed.
- 5. Protect exposed slopes with plastic or synthetic mulches.
- 6. Provide sediment traps and basins during dewatering.
- 7. Plan construction at proper time to avoid flooding.
- 8. Installation of a mud matt to prevent mud and debris from being transported off site.
- 9. Installation of silt fence to prevent sediment runoff.

The contractor will, at every rainfall, complete inspections and guarantee proper performance. The inspection is to include:

10. Verification that water is not flowing under silt barriers.

Refer to **Drawing EC-1** for the proposed location of silt fences, straw bales and other erosion control structures.



Geotechnical Investigation and Environmental Assessment December 21, 2016

# 10.0 GEOTECHNICAL INVESTIGATION AND ENVIRONMENTAL ASSESSMENT

A geotechnical Investigation Report was prepared by Patersongroup on November 11, 2016. The report summarizes the existing soil conditions within the subject area and construction recommendations. For details which are not summarized below, please see the original Paterson report.

Subsurface soil conditions within the subject area were determined from 11 boreholes and 14 test pits across the proposed site. The investigation concluded that the site is underlain by dense silty sand with gravel layer of 1.1 to 6.0m below ground surface overlaid by a thin layer of topsoil. Bedrock is anticipated to lie within subjected area and is in the form of limestone and Verulam. In addition, six constant head pask permeameter tests were completed to verify existing hydraulic conductivity of the soils below the proposed area for infiltration.

Expected long-term groundwater levels were measured on June 6, 2016 and vary in elevation from 2.5m to 3.5m in depth.

The required pavement structure for proposed hard surfaced areas are outlined in **Table 7 and Table 8** below:

Table 7: Pavement Structure – Car Only Parking Areas

Thickness (mm)	Material Description
50	Wear Course – HL-3 or Superpave 12.5 Asphaltic Concrete
150	Base – OPSS Granular A Crushed Stone
300	Subbase - OPSS Granular B Type II
-	Subgrade – Either fill, in situ soil, or OPSS Granular B Type I or II material placed over in situ soil or fill.

Table 8: Pavement Structure – Access Lanes

Thickness (mm)	Material Description
40	Wear Course – HL-3 or Superpave 12.5 Asphaltic Concrete
50	Binder Course – HL-8 or Superpave 19.0 Asphaltic Concrete
150	Base – OPSS Granular A Crushed Stone
400	Subbase - OPSS Granular B Type II
-	Subgrade – Either fill, in situ soil, or OPSS Granular B Type II material placed over in situ soil or fill.



Conclusions
December 21, 2016

### 11.0 CONCLUSIONS

### 11.1 WATER SERVICING

The proposed new well is considered to be capable of supplying sufficient water supply for fire flows. Based on the OBC calculations the maximum required fire flow for the site is 45 L/s (2,700 L/min). Fire suppression will be provided through two onsite 53,000L water storage tanks.

### 11.2 STORMWATER SERVICING

The proposed stormwater management plan is in compliance with the goals specified through consultation with the City of Ottawa. Onsite storage will be provided for all runoff in excess of existing surface release rates. All stored stormwater up to the 100-year event will be infiltrated as existing site grading is such that no feasible surface outlet exists for the captured stormwater on the site.

#### 11.3 GRADING

Grading for the site has been designed to provide an emergency overland flow route as per City requirements and reflects any restrictions recommended in the Geotechnical Investigation Report prepared by Patersongroup on November 11, 2016. Erosion and sediment control measures will be implemented during construction to reduce the impact on existing facilities.

#### 11.4 UTILITIES

Utility infrastructure exists within overhead lines within the Carp Road ROW at the south western boundary of the proposed site. It is anticipated that existing infrastructure will be sufficient to provide a means of distribution for the proposed site. Exact size, location and routing of utilities will be finalized after design circulation.

## 11.5 APPROVALS/PERMITS

An MOECC ECA is not expected to be required for the subject site as site will remain private, under single ownership, however due to the infiltration component of the proposed stormwater management consultation with the MOECC will be required to confirm whether an ECA is required for stormwater management. A Permit to Take Water is not anticipated to be required for pumping requirements for service lateral/building footing installation. The Mississippi Valley Conservation Authority will need to be consulted in order to obtain municipal approval for site Water Supply Servicing.



Appendix A Water Supply Servicing December 21, 2016

# Appendix A WATER SUPPLY SERVICING

## A.1 FIRE FLOW REQUIREMENTS PER OBC



## Fire Flow Calculations as per Ontario Building Code 2006 (Appendix A)

Job# 160401271 Designed by: TRK
Date 20-Dec-16 Checked by: KJK

# $Q = KVS_{tot}$

Q = Volume of water required (L)

V = Total building volume (m3)

K = Water supply coefficient from Table 1

 $S_{tot} = Sotal of spatial coefficient values from property line exposures on all sides as obtained from the formula$ 

 $S_{tot} = 1.0 + [S_{side1} + S_{side2} + S_{side3} + S_{side4}]$ 

1	Type of construction	Building Classification		Water Supply Coefficient
	Non-Combustible with Fire- Resistance Ratings	E, F-2		17
2	Area of one floor	number of floors	hieght of ceiling	Total Building Volume
	(m <sup>2</sup> )		(m)	(m <sup>3</sup> )
	1394	1	6.31	8,796
3	Side	Exposure		Total Spatial
		Distance (m)	Spatial Coefficient	Coeffiecient
	North	14.5	0	
	East	28.4	0	1
	South	30	0	1
	West	45.4	0	
	-			
4	Established Fire	Reduction in		Total Volume
	Safety Plan?	Volume (%)		Reduction
	no	0%		0%
5				Total Volume 'Q' (L)
				149,532
				Minimum Required
				Fire Flow (L/min)
				4,500

Appendix B Stormwater Management December 21, 2016

# **Appendix B STORMWATER MANAGEMENT**

## **B.1** RATIONAL METHOD CALCULATIONS



File No: **160401271** Project: 2978 CARP ROAD
Date: 18-Aug-16

SWM Approach: Post-development to Pre-development flows

#### Pre-Development Site Conditions:

#### Overall Runoff Coefficient for Site and Sub-Catchment Areas

Sub-catchment Area			oefficient Table Area Runoff (ha) Coefficient				Overall Runoff	
Catchment Type	ID / Description		"A"		"C"	"A	x C"	Coefficient
Uncontrolled - Tributary	ET	Hard Soft	0.112 1.192		0.9 0.2	0.101 0.238		
	S	ubtotal	02	1.303896	0.2	0.200	0.339013	0.260
Total				1.304			0.339	
Overall Runoff Coefficient= C:								0.26

Total Roof Areas	0.000 ha
Total Tributary Surface Areas (Controlled and Uncontrolled)	1.304 ha
Total Tributary Area to Outlet	1.304 ha
Total Uncontrolled Areas (Non-Tributary)	0.000 ha
Total Site	1.304 ha

## Project #160401271, 2978 CARP ROAD Modified Rational Method Calculatons for Storage

5 yr Intensity	$I = a/(t + b)^c$	a =	998.071	t (min)	I (mm/hr)
City of Ottawa		b =	6.053	5	141.18
		c =	0.814	10	104.19
				15	83.56
				20	70.25
				25	60.90
				30	53.93
				35	48.52
				40	44.18
				45	40.63
				50	37.65
				55	35.12
				60	32.94

#### 5 YEAR Predevelopment Target Release from Portion of Site

Subdrainage Area: Predevelopment Tributary Area to Outlet
Area (ha): 1.3030
C: 0.26

Typical Time of Concentration

tc	I (5 yr)	Qtarget
(min)	(mm/hr)	(L/s)
30	53.93	50.79

#### 5 YEAR Modified Rational Method for Entire Site

Uncontrolled - Tributary

tc	I (5 yr)	Qactual	Qrelease	Qstored	Vstored
(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m^3)
5	141.18	133.05	133.05		
10	104.19	98.20	98.20		
15	83.56	78.75	78.75		
20	70.25	66.21	66.21		
25	60.90	57.39	57.39		
30	53.93	50.82	50.82		
35	48.52	45.73	45.73		
40	44.18	41.64	41.64		
45	40.63	38.29	38.29		
50	37.65	35.49	35.49		
55	35.12	33.10	33.10		
60	32.94	31.05	31.05		

#### SUMMAR

RY TO OUTLET			
		Vrequired Vavai	lable*
Tributary Area	0.000 ha		
Total 5yr Flow to Sewer	0 L/s	0	0 m <sup>3</sup> Ok
Non-Tributary Area	1.304 ha		
Total 5yr Flow Uncontrolled	133 L/s		
Total Area	1.304 ha		
Total 5yr Flow	133 L/s		
Target	51 L/s		

## Project #160401271, 2978 CARP ROAD Modified Rational Method Calculatons for Storage

100 yr Intensity	I = a/(t + b)	a =	1735.688	t (min)	I (mm/hr)
City of Ottawa		b =	6.014	5	242.70
		c =	0.820	10	178.56
	_			15	142.89
				20	119.95
				25	103.85
				30	91.87
				35	82.58
				40	75.15
				45	69.05
				50	63.95
				55	59.62
				60	55.89

#### 100 YEAR Predevelopment Target Release from Portion of Site

Subdrainage Area: Predevelopment Tributary Area to Outlet
Area (ha): 1.3030
C: 0.26

Estimated Time of Concentration after Development

tc	I (100 yr)	Q100yr
(min)	(mm/hr)	(L/s)
30	91.87	86.52

#### 100 YEAR Modified Rational Method for Entire Site

Uncontrolled - Tributary

tc	I (100 yr)	Qactual	Qrelease	Qstored	Vstored
(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m^3)
10	178.56	210.36	210.36		
20	119.95	141.31	141.31		
30	91.87	108.23	108.23		
40	75.15	88.53	88.53		
50	63.95	75.34	75.34		
60	55.89	65.85	65.85		
70	49.79	58.66	58.66		
80	44.99	53.00	53.00		
90	41.11	48.43	48.43		
100	37.90	44.65	44.65		
110	35.20	41.47	41.47		
120	32.89	38.75	38.75		

#### SUMMARY TO OUTLET

Vrequired Vavailable\* Tributary Area Total 100yr Flow to Sewer 0.000 ha 0 0 m<sup>3</sup> Ok 0 L/s Non-Tributary Area Total 100yr Flow Uncontrolled 1.304 ha 210 L/s Total Area Total 100yr Flow Target 1.304 ha 210 L/s 87 L/s

File No: **160401271** Project: 2978 Carp Road
Date: 17-Nov-16

SWM Approach: Post-development to Pre-development flows

#### Post-Development Site Conditions:

#### Overall Runoff Coefficient for Site and Sub-Catchment Areas

		Runoff C	oefficient Table				
Sub-catchr Area	ment		Area (ha)	Run Coeffic			Overall Runoff
Catchment Type	ID / Description		"A"	"C	" "A	x C"	Coefficien
Controlled - Tributary	STM-1	Hard	0.456	0.9	0.410		
		Soft	0.684	0.2	0.137		
	Su	ubtotal		1.14		0.5472	0.480
Uncontrolled - Non-Tributary	EXT-2	Hard	0.000	0.0	0.000		
		Soft	0.060	0.2	0.012		
	Su	ubtotal		0.06		0.012	0.200
Uncontrolled - Non-Tributary	EXT-1	Hard	0.054	0.0	0.049		
•		Soft	0.046	0.2	0.009		
	Sı	ubtotal		0.1		0.058	0.580
Total				1.300		0.617	
rerall Runoff Coefficient= C:							0.47

Total Roof Areas	0.000 ha
Total Tributary Surface Areas (Controlled and Uncontrolled)	1.140 ha
Total Tributary Area to Outlet	1.140 ha
Total Uncontrolled Areas (Non-Tributary)	0.160 ha
Total Site	1.300 ha

### Project #160401271, 2978 Carp Road

		I, 2978 Ca Method Ca		for Storage	)		
	5 yr Intens	ity	I = a/(t + b)°	a =	998.071	t (min)	l (mm/hr)
	City of Otta	awa		b = c =	6.053 0.814	5 10	141.18 104.19
			'	<u> </u>	0.014	15	83.56
						20 25	70.25 60.90
						30 35	53.93 48.52
						40	44.18
						45 50	40.63 37.65
						55 60	35.12 32.94
					L		•
	5 YEA	AR Predeve	elopment Ta	arget Releas	e from Por	tion of Site	!
Subdrai	nage Area: Area (ha):	Predevelop	ment Tributar	y Area to Outle	et		
	C:	0.26					
	Typical Tim	ne of Concen	tration				
	tc	I (5 yr)	Qtarget	l			
	(min) 30	(mm/hr) 53.93	(L/s) 50.67				
	5 YEAR I	vioditied Ra	ational Meti	nod for Entir	e Site		
Subdrai	nage Area:	STM-1				Controlle	ed - Tributary
	Area (ha): C:	1.14 0.48					•
	tc	I (5 yr)	Qactual	Qrelease	Qstored	Vstored	
	(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m^3)	
	5 10	141.18 104.19	214.76 158.50	3.09 3.09	211.67 155.41	63.50 93.25	
	15	83.56	127.11	3.09	124.02	111.62	
	20 25	70.25 60.90	106.87 92.64	3.09 3.09	103.78 89.55	124.53 134.32	
	30 35	53.93 48.52	82.04 73.81	3.09 3.09	78.95 70.72	142.10 148.50	
	40	44.18	67.21	3.09	64.12	153.90	
	45 275	40.63 10.14	61.80 15.42	3.09 3.09	58.71 12.33	158.53 203.42	
	280	9.99	15.20	3.09	12.11	203.43	
	285	9.85	14.99	3.09	11.90	203.42	
Storage:	: Above CB						
		Stage	Head	Discharge	Vreq	Vavail	Volume
5-vear \	Nater Level		(m) 1.95	(L/s) 3.09	(cu. m) 203.43	(cu. m) 389.64	Check OK
0 ,00	74.0. 2070.	1.00	1.00	0.00	200.10	000.01	O.K
Subdrai	nage Area:	EXT-2			Und	controlled - N	Ion-Tributary
	Area (ha): C:	0.06 0.20					
	tc	I (5 yr)	Qactual	Qrelease	Qstored	Vstored	
	(min) 5	(mm/hr) 141.18	(L/s) 4.71	(L/s) 4.71	(L/s)	(m^3)	
	10	104.19	3.48	3.48			
	15 20	83.56 70.25	2.79 2.34	2.79 2.34			
	25 30	60.90 53.93	2.03 1.80	2.03 1.80			
	35	48.52	1.62	1.62			
	40 45	44.18 40.63	1.47 1.36	1.47 1.36			
	50	37.65	1.26	1.26			
	55 60	35.12 32.94	1.17 1.10	1.17 1.10			
Subdrai	nage Area: Area (ha):	EXT-1 0.10			Und	controlled - N	Ion-Tributary
	C:	0.58					
	tc (min)	I (5 yr)	Qactual	Qrelease	Qstored	Vstored	
	(min) 5	(mm/hr) 141.18	(L/s) 22.76	(L/s) 22.76	(L/s)	(m^3)	
1	10 15	104.19 83.56	16.80 13.47	16.80 13.47			
	20	70.25	11.33	11.33			
	25 30	60.90 53.93	9.82 8.70	9.82 8.70			
	35	48.52	7.82	7.82			
	40 45	44.18 40.63	7.12 6.55	7.12 6.55			
	50 55	37.65 35.12	6.07 5.66	6.07 5.66			
	60	32.94	5.31	5.31			

Project #160401271, 2978 Carp Road

Modified F							
	100 yr Inte	nsity	I = a/(t + b)	a =	1735.688	t (min)	l (mm/hr)
	City of Ott	awa		b =	6.014	5	242.70
				c =	0.820	10	178.56
						15	142.89
						20	119.95
						25	103.85
						30	91.87
						35	82.58
						40	75.15
						45 50	69.05 63.95
						55	59.62
						60	55.89
100 YEAR Predevelopment Target Release from Portion of Site							
	100 YE	AR Predeve	elopment T	arget Releas	se from Po	rtion of Si	te
Subdrair		Predevelopr	ment Tributa	ry Area to Outl	et		
	Area (ha): C:	1.3000 0.26					
	٥.	0.20					
	Estimated '	Time of Cond	entration af	ter Developme	nt		
1	tc	I (100 yr)	Q100yr	ı			
	(min)	(mm/hr)	(L/s)				
	30	91.87	86.32				
	400 VEAF	N N N	D-4'1 84	. 4b 1 f F	···· 0'4 -		
	100 YEAR	k woaltied l	kational M	ethod for En	ure Site		
Subdrair	nage Area:	STM-1				Controll	ed - Tributary
	Area (ha):	1.14					
	C:	0.60					
1	tc	I (100 yr)	Qactual	Qrelease	Ostored	Vstored	
	(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m^3)	
	10	178.56	339.53	9.78	329.75	197.85	•
	20	119.95	228.09	9.78	218.31	261.97	
	30	91.87	174.69	9.78	164.91	296.84	
	40	75.15	142.89	9.78	133.11	319.46	
	50	63.95	121.61	9.78	111.83	335.49	
	60	55.89	106.28	9.78	96.50	347.42	
	70	49.79	94.68	9.78	84.90	356.56	
	80	44.99	85.55	9.78	75.77	363.70	
	100	37.90	72.07	9.78	62.29	373.76	
	100 171	37.90 24.89	72.07 47.34	9.78 9.78	62.29 37.56	373.76 385.34	
	171 172	24.89 24.78	47.34 47.12	9.78 9.78	37.56 37.34	385.34 385.34	
	171	24.89	47.34	9.78	37.56	385.34	
Storage:	171 172 173	24.89 24.78 24.67	47.34 47.12 46.90	9.78 9.78	37.56 37.34	385.34 385.34	
Storage:	171 172 173	24.89 24.78	47.34 47.12 46.90	9.78 9.78	37.56 37.34	385.34 385.34	
Storage:	171 172 173	24.89 24.78 24.67	47.34 47.12 46.90 CB	9.78 9.78 9.78 9.78	37.56 37.34 37.12 Vreq	385.34 385.34 385.34 Vavail	Volume
	171 172 173 Surface Sto	24.89 24.78 24.67 prage Above	47.34 47.12 46.90 CB	9.78 9.78 9.78 9.78	37.56 37.34 37.12 Vreq (cu. m)	385.34 385.34 385.34 Vavail (cu. m)	Check
	171 172 173	24.89 24.78 24.67 prage Above	47.34 47.12 46.90 CB	9.78 9.78 9.78 9.78	37.56 37.34 37.12 Vreq	385.34 385.34 385.34 Vavail	
100-year V	171 172 173 Surface Sto	24.89 24.78 24.67 orage Above Stage 2.10	47.34 47.12 46.90 CB	9.78 9.78 9.78 9.78	37.56 37.34 37.12 Vreq (cu. m) 385.34	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30	Check OK
100-year V	171 172 173 Surface Sto	24.89 24.78 24.67 prage Above	47.34 47.12 46.90 CB	9.78 9.78 9.78 9.78	37.56 37.34 37.12 Vreq (cu. m) 385.34	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30	Check
100-year V	171 172 173 Surface Sto	24.89 24.78 24.67 orage Above Stage 2.10	47.34 47.12 46.90 CB	9.78 9.78 9.78 9.78	37.56 37.34 37.12 Vreq (cu. m) 385.34	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30	Check OK
100-year V	171 172 173 Surface Ste Vater Level nage Area: Area (ha):	24.89 24.78 24.67 orage Above Stage 2.10 EXT-2 0.06	47.34 47.12 46.90 CB	9.78 9.78 9.78 9.78	37.56 37.34 37.12 Vreq (cu. m) 385.34	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30	Check OK
100-year V	171 172 173 Surface Sto Vater Level nage Area: Area (ha): C: tc (min)	24.89 24.78 24.67 prage Above  Stage 2.10  EXT-2 0.06 0.25  I (100 yr) (mm/hr)	47.34 47.12 46.90 CB Head (m) 2.10	9.78 9.78 9.78 9.78 Discharge (L/s) 9.78	37.56 37.34 37.12 Vreq (cu. m) 385.34	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30	Check OK
100-year V	171 172 173 Surface Ste Vater Level nage Area: Area (ha): C: tc (min) 10	24.89 24.78 24.67 24.67  Stage  2.10  EXT-2 0.06 0.25  I (100 yr) (mm/hr) 178.56	47.34 47.12 46.90 CB Head (m) 2.10	9.78 9.78 9.78 9.78 Discharge (L/s) 9.78	37.56 37.34 37.12 Vreq (cu. m) 385.34	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 ontrolled - I	Check OK
100-year V	171 172 173 Surface Sto Vater Level  age Area: Area (ha): C: tc (min) 10 20	24.89 24.78 24.67 24.67 24.67 Stage  2.10  EXT-2 0.06 0.25  I (100 yr) (mm/hr) 178.56 119.95	47.34 47.12 46.90 CB Head (m) 2.10 Qactual (L/s) 7.45 5.00	9.78 9.78 9.78 9.78 Discharge (L/s) 9.78 Qrelease (L/s) 7.45 5.00	37.56 37.34 37.12 Vreq (cu. m) 385.34	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 ontrolled - I	Check OK
100-year V	171 172 173 Surface Str Vater Level nage Area: Area (ha): C: tc (min) 10 20 30	24.89 24.78 24.67  prage Above  Stage  2.10  EXT-2 0.06 0.25  1(100 yr) (mm/hr) 178.56 119.95 91.87	47.34 47.12 46.90 CB Head (m) 2.10 Qactual (L/s) 7.45 5.00 3.83	9.78 9.78 9.78 9.78 Discharge (L/s) 9.78 Qrelease (L/s) 7.45 5.00 3.83	37.56 37.34 37.12 Vreq (cu. m) 385.34	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 ontrolled - I	Check OK
100-year V	171 172 173 Surface Str  Vater Level  nage Area: Area (ha): C:  tc (min) 10 20 30 40	24.89 24.78 24.67  brage Above  Stage 2.10  EXT-2 0.06 0.25  I (100 yr) (mm/hr) 178.56 119.95 91.87 75.15	47.34 47.12 46.90 CB Head (m) 2.10 Qactual (L/s) 7.45 5.00 3.83 3.13	9.78 9.78 9.78 9.78 Discharge (L/s) 9.78 Qrelease (L/s) 7.45 5.00 3.83 3.13	37.56 37.34 37.12 Vreq (cu. m) 385.34	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 ontrolled - I	Check OK
100-year V	171 172 173 Surface Ste Vater Level nage Area: Area (ha): C: tc (min) 10 20 30 40 50	24.89 24.78 24.67  prage Above  Stage  2.10  EXT-2 0.06 0.25  I (100 yr) (mm/hr) 178.56 119.95 91.87 75.15 63.95	47.34 47.12 46.90 CB Head (m) 2.10 Qactual (L/s) 7.45 5.00 3.83 3.13 2.67	9.78 9.78 9.78 9.78 Discharge (L/s) 9.78 Qrelease (L/s) 7.45 5.00 3.83 3.13 2.67	37.56 37.34 37.12 Vreq (cu. m) 385.34	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 ontrolled - I	Check OK
100-year V	171 172 173 Surface Sto Vater Level tage Area: Area (ha): C: tc (min) 10 20 30 40 50 60	24.89 24.78 24.67  orage Above  Stage  2.10  EXT-2 0.06 0.25  I (100 yr) (mm/hr) 178.56 119.95 91.87 75.15 63.95 55.89	47.34 47.12 46.90 CB Head (m) 2.10 Qactual (L/s) 7.45 5.00 3.83 3.13 2.67 2.33	9.78 9.78 9.78 9.78 Discharge (L/s) 9.78 Qrelease (L/s) 7.45 5.00 3.83 3.12 2.67 2.33	37.56 37.34 37.12 Vreq (cu. m) 385.34	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 ontrolled - I	Check OK
100-year V	171 172 173 Surface Sto Vater Level  nage Area: Area (ha): C: tc (min) 10 20 30 40 50 60 70	24.89 24.78 24.67  prage Above  Stage  2.10  EXT-2 0.06 0.25 1(100 yr) (mm/hr) 178.56 119.95 91.87 75.15 63.95 55.89 49.79	47.34 47.12 46.90 CB Head (m) 2.10 Qactual (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.08	9.78 9.78 9.78 9.78 Discharge (L/s) 9.78 Qrelease (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.08	37.56 37.34 37.12 Vreq (cu. m) 385.34	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 ontrolled - I	Check OK
100-year V	171 172 173 Surface Std Vater Level  lage Area: Area (ha): C: tc (min) 10 20 30 40 50 60 70 80	24.89 24.78 24.67  prage Above  Stage  2.10  EXT-2 0.06 0.25  I (100 yr) (mm/hr) 178.56 119.95 91.87 75.15 63.95 55.89 49.79 44.99	47.34 47.12 46.90 CB Head (m) 2.10 2.10 Qactual (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.08	9.78 9.78 9.78 9.78 9.78 Discharge (L/s) 9.78 Qrelease (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.08	37.56 37.34 37.12 Vreq (cu. m) 385.34	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 ontrolled - I	Check OK
100-year V	171 172 173 Surface Std Vater Level nage Area: Area (ha): C: tc (min) 10 20 30 40 50 60 70 80 90	24.89 24.78 24.67  prage Above  Stage  2.10  EXT-2 0.06 0.25  I(100 yr) (mm/hr) 178.56 119.95 91.87 75.15 63.95 95.89 44.99 44.191	47.34 47.12 46.90 CB Head (m) 2.10 Qactual (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.08 1.81	9.78 9.78 9.78 9.78 0.78 0.78 0.78 0.78 0.745 0.03 0.383 0.313 0.267 0.233 0.208 1.88	37.56 37.34 37.12 Vreq (cu. m) 385.34	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 ontrolled - I	Check OK
100-year V	171 172 173 Surface Std Vater Level  lage Area: Area (ha): C: tc (min) 10 20 30 40 50 60 70 80	24.89 24.78 24.67  prage Above  Stage 2.10  EXT-2 0.06 0.25  I (100 yr) (mm/hr) 178.56 119.95 91.87 75.15 63.95 55.89 49.79 44.99 41.11 37.90	47.34 47.12 46.90 CB Head (m) 2.10 2.10 Qactual (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.08 1.88 1.71	9.78 9.78 9.78 9.78 9.78 Discharge (L/s) 9.78 Qrelease (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.08	37.56 37.34 37.12 Vreq (cu. m) 385.34	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 ontrolled - I	Check OK
100-year V	171 172 173 Surface Ste Vater Level lage Area: Area (ha): C: tc (min) 10 20 30 40 50 60 70 80 90 100	24.89 24.78 24.67  prage Above  Stage  2.10  EXT-2 0.06 0.25  I(100 yr) (mm/hr) 178.56 119.95 91.87 75.15 63.95 95.89 44.99 44.191	47.34 47.12 46.90 CB Head (m) 2.10 Qactual (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.08 1.81	9.78 9.78 9.78 9.78 9.78 0.78 9.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0	37.56 37.34 37.12 Vreq (cu. m) 385.34	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 ontrolled - I	Check OK
100-year V	171 172 173 Surface Str Vater Level nage Area: Area (ha): C: tc (min) 20 30 40 50 60 70 80 90 100 110 120	24.89 24.78 24.67  prage Above  Stage  2.10  EXT-2 0.06 0.25  1(100 yr) 178.56 119.95 55.89 49.79 44.99 41.11 37.90 35.20 32.89	47.34 47.12 46.90 CB Head (m) 2.10 2.10 Qactual (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.08 1.88 1.71 1.58	9.78 9.78 9.78 9.78 9.78 9.78 9.78 Qrelease (L/s) 9.74 7.45 7.45 7.45 7.45 7.45 7.45 7.45 7	37.56 37.34 37.12 Vreq (cu. m) 385.34 Unc Qstored (L/s)	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 controlled - I	Check OK
100-year V	171 172 173 Surface Str Vater Level  lage Area: Area (ha): C: tc (min) 10 20 30 40 50 60 70 80 90 110	24.89 24.78 24.67  prage Above  Stage  2.10  EXT-2 0.06 0.25  1(100 yr) 178.56 119.95 55.89 49.79 44.99 41.11 37.90 35.20 32.89  EXT-1 0.10	47.34 47.12 46.90 CB Head (m) 2.10 2.10 Qactual (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.08 1.88 1.71 1.58	9.78 9.78 9.78 9.78 9.78 9.78 9.78 Qrelease (L/s) 9.74 7.45 7.45 7.45 7.45 7.45 7.45 7.45 7	37.56 37.34 37.12 Vreq (cu. m) 385.34 Unc Qstored (L/s)	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 controlled - I	Check OK
100-year V	171 172 173 Surface Ste Vater Level  lage Area: Area (ha): C: tc (min) 10 20 30 40 50 60 70 80 90 110 120 lage Area:	24.89 24.78 24.67  prage Above  Stage  2.10  EXT-2 0.06 0.25  I (100 yr) (mm/hr) 178.56 119.95 91.87 75.15 63.95 63.95 63.95 44.99 44.19 44.99 44.19 37.90 35.20 32.89  EXT-1	47.34 47.12 46.90 CB Head (m) 2.10 2.10 Qactual (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.08 1.88 1.71 1.58	9.78 9.78 9.78 9.78 9.78 9.78 9.78 Qrelease (L/s) 9.74 7.45 7.45 7.45 7.45 7.45 7.45 7.45 7	37.56 37.34 37.12 Vreq (cu. m) 385.34 Unc Qstored (L/s)	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 controlled - I	Check OK
100-year V	171 172 173 Surface Str Vater Level nage Area: Area (ha): C: tc (min) 20 30 40 50 60 70 80 90 100 110 120  nage Area: Area (ha):	24.89 24.78 24.67  prage Above  Stage  2.10  EXT-2 0.06 0.25  1(100 yr) 178.56 119.95 55.89 49.79 44.99 41.11 37.90 35.20 32.89  EXT-1 0.10	47.34 47.12 46.90 CB Head (m) 2.10 2.10 Qactual (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.08 1.88 1.71 1.58	9.78 9.78 9.78 9.78 9.78 9.78 9.78 Qrelease (L/s) 9.74 7.45 7.45 7.45 7.45 7.45 7.45 7.45 7	37.56 37.34 37.12 Vreq (cu. m) 385.34 Unc Qstored (L/s)	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 controlled - I	Check OK
100-year V	171 172 173 Surface Str Vater Level nage Area: Area (ha): C: tc (min) 20 30 40 50 60 70 80 90 100 110 120 nage Area: Area (ha): C:	24.89 24.78 24.67  24.67  24.67  24.67  24.67  25.10  EXT-2 0.06 0.25  1(100 yr) 178.56 119.95 91.87 75.15 63.95 95.89 44.99 44.191 37.90 35.20 32.89  EXT-1 0.10 0.73	47.34 47.12 46.90 CB Head (m) 2.10  2.10  Qactual (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.08 1.81 1.71 1.58 1.47 1.37	9.78 9.78 9.78 9.78 9.78 9.78 9.78 9.78	37.56 37.34 37.12  Vreq (cu. m) 385.34  Unc  Qstored (L/s)	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 vontrolled - l	Check OK
100-year V	171 172 173 Surface Str Vater Level rage Area: Area (ha): C: tc (min) 10 20 30 40 50 60 70 80 90 110 110 110 110 110 110 110 110 110	24.89 24.78 24.67  prage Above  Stage  2.10  EXT-2 0.06 0.25  1(100 yr)  178.56 119.95 91.87 75.15 63.95 55.89 44.99 41.11 37.90 35.20 32.89  EXT-1 0.10 0.73	47.34 47.12 46.90  CB  Head (m) 2.10  Qactual (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.18 1.58 1.77 1.37	9.78 9.78 9.78 9.78 9.78 9.78 9.78 9.78	37.56 37.34 37.12  Vreq (cu. m) 385.34  Unc  Qstored (L/s)  Unc	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 vontrolled - l	Check OK
100-year V	171 172 173 Surface Str Vater Level  lage Area: Area (ha): 10 20 30 40 50 60 70 80 90 110 120 lage Area: Area (ha): C: tc (min)	24.89 24.78 24.67  prage Above  Stage  2.10  EXT-2 0.06 0.25  I (100 yr) (mm/hr) 178.56 6119.95 91.87 75.15 63.95 49.79 44.99 35.20 32.89  EXT-1 0.10 0.73 I (100 yr) (mm/hr) I (100 yr) (mm/hr) I (100 yr) (mm/hr)	47.34 47.12 46.90  CB  Head (m) 2.10  2.10  Qactual (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.08 1.71 1.58 1.47 1.37	9.78 9.78 9.78 9.78 9.78 9.78 9.78  Grelease (L/s) 1.59 1.47 1.37  Grelease (L/s) 2.67 2.33 2.08 1.71 1.59 2.67 2.33 2.08 2.67 2.33 2.08 2.69 2.47 2.33 2.40 2.80 2.80 2.80 2.80 2.80 2.80 2.80 2.8	37.56 37.34 37.12  Vreq (cu. m) 385.34  Unc  Qstored (L/s)  Unc	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 vontrolled - l	Check OK
100-year V	171 172 173 Surface Str Vater Level rage Area: Area (ha): C: tc (min) 10 20 30 40 50 60 70 80 90 110 110 110 110 110 110 110 110 110	24.89 24.78 24.67  orage Above  Stage  2.10  EXT-2 0.06 0.25  1(100 yr) (mm/hr) 37.90 32.89  EXT-1 0.10 0.73  I (100 yr) (mm/hr) 178.56	47.34 47.12 46.90  CB  Head (m) 2.10  Qactual (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.18 1.58 1.77 1.37	9.78 9.78 9.78 9.78 9.78 9.78  Orelease (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.167 1.58 1.47 1.59 1.437	37.56 37.34 37.12  Vreq (cu. m) 385.34  Unc  Qstored (L/s)  Unc	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 vontrolled - l	Check OK
100-year V	171 172 173 Surface Ste Vater Level  lage Area: Area (ha): 10 20 30 40 50 60 70 80 90 110 120 lage Area: Area (ha): C: tc (min) 10 20 30 40 50 60 70 60 70 60 70 60 70 60 70 60 70 60 70 80 90 110 120 120 120 120 120 120 120 120 12	24.89 24.78 24.67  brage Above  Stage  2.10  EXT-2 0.06 0.25  I (100 yr) (mm/hr) 178.56 119.95 94.79 44.99 44.99 44.99 44.99 44.11 37.90 35.20 32.89  EXT-1 0.10 0.73  I (100 yr) (mm/hr) 178.56 119.95	47.34 47.12 46.90  CB  Head (m) 2.10  2.10  Qactual (L/s) 7.45 5.00 3.83 3.13 2.067 2.33 2.188 1.71 1.37	9.78 9.78 9.78 9.78 9.78 9.78 9.78  Grelease (L/s) 1.59 1.47 1.37  Grelease (L/s) 2.67 2.33 2.08 1.71 1.59 2.67 2.33 2.08 2.67 2.33 2.08 2.69 2.47 2.33 2.40 2.80 2.80 2.80 2.80 2.80 2.80 2.80 2.8	37.56 37.34 37.12  Vreq (cu. m) 385.34  Unc  Qstored (L/s)  Unc	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 vontrolled - l	Check OK
100-year V	171 172 173 Surface Str Vater Level Dage Area: Area (ha): C: tc (min) 20 30 40 50 100 110 120 Tage Area: Area (ha): C: tc (min) 10 20 30 40 50 60 70 80 90 100 110 120 120 30 40 50 60 60 60 70 80 90 100 110 120 50 60 60 70 80 90 100 110 120 50 60 60 70 80 90 100 110 120 50 60 60 60 60 60 60 60 60 60 60 60 60 60	24.89 24.78 24.67  prage Above  Stage  2.10  EXT-2 0.06 0.25  I(100 yr) (mm/hr) 178.56 119.95 44.99 41.11 37.90 35.20 32.89  EXT-1 0.10 0.73  I(100 yr) (mm/hr) 178.56 119.95 91.87	47.34 47.12 46.90  CB  Head (m) 2.10  2.10  7.45 5.00 3.83 3.13 2.67 2.33 2.08 1.88 1.47 1.37	9.78 9.78 9.78 9.78 9.78 9.78 9.78   Orelease (L/s) 7.45 5.05 5.05 1.83 3.13 2.67 2.33 2.10 1.47 1.37   Orelease (L/s) 35.99 24.18 18.52 15.18	37.56 37.34 37.12  Vreq (cu. m) 385.34  Unc  Qstored (L/s)  Unc	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 vontrolled - l	Check OK
100-year V	171 172 173 Surface Str Vater Level rage Area: Area (ha): C: tc (min) 10 20 30 40 50 60 70 110 110 110 120 130 Area: Are	24.89 24.78 24.67  prage Above  Stage  2.10  EXT-2 0.06 0.25  I(100 yr) (mm/hr) 178.56 119.95 91.87 75.15 63.95 55.89 49.79 41.91 0.10 0.73  I(100 yr) (mm/hr) 178.56 119.95 91.87 55.89	47.34 47.12 46.90  CB  Head (m) 2.10  2.10  Qactual (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.18 1.71 1.37  Qactual (L/s) 1.58 1.47 1.37	9.78 9.78 9.78 9.78 9.78 9.78 9.78  Qrelease (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.10 1.58 1.47 1.37	37.56 37.34 37.12  Vreq (cu. m) 385.34  Unc  Qstored (L/s)  Unc	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 vontrolled - l	Check OK
100-year V	171 172 173 Surface Str Vater Level Dage Area: Area (ha): C: tc (min) 20 30 40 50 100 110 120 Tage Area: Area (ha): C: tc (min) 10 20 30 40 50 60 70 80 90 100 110 120 120 30 40 50 60 60 60 70 80 90 100 110 120 50 60 60 70 80 90 100 110 120 50 60 60 70 80 90 100 110 120 50 60 60 60 60 60 60 60 60 60 60 60 60 60	24.89 24.78 24.67  prage Above  2.10  EXT-2 0.06 0.25  1(100 yr) 178.56 119.95 55.89 44.79 44.11 37.90 35.20 32.89  EXT-1 0.10 0.73  1(100 yr) 1(1	47.34 47.12 46.90  CB  Head (m) 2.10  2.10  7.45 5.00 3.83 3.13 2.67 2.33 2.67 2.33 2.10  2.11 1.58 1.47 1.37	9.78 9.78 9.78 9.78 9.78 9.78  Orelease (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.08 1.88 1.71 1.37	37.56 37.34 37.12  Vreq (cu. m) 385.34  Unc  Qstored (L/s)  Unc	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 vontrolled - l	Check OK
100-year V	171 172 173 Surface Str Vater Level  large Area: Area (ha): C: tc (min) 10 20 30 40 50 100 1120 120 120 120 120 120 120 120 1	24.89 24.78 24.67  prage Above  Stage  2.10  EXT-2 0.06 0.25  I(100 yr) (mm/hr) 178.56 119.95 91.87 75.15 63.95 55.89 49.79 41.91 0.10 0.73  I(100 yr) (mm/hr) 178.56 119.95 91.87 55.89	47.34 47.12 46.90  CB  Head (m) 2.10  2.10  Qactual (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.18 1.71 1.37  Qactual (L/s) 1.58 1.47 1.37	9.78 9.78 9.78 9.78 9.78 9.78 9.78  Qrelease (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.10 1.58 1.47 1.37	37.56 37.34 37.12  Vreq (cu. m) 385.34  Unc  Qstored (L/s)  Unc	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 vontrolled - l	Check OK
100-year V	171 172 173 Surface Str Vater Level  lage Area: Area (ha): C: tc (min) 20 30 40 100 110 120  lage Area: Area (ha): C: tc (min) 30 40 50 60 70 80 90 100 20 30 40 100 100 100 100 100 100 100 100 100	24.89 24.78 24.67  24.78 24.67  24.67  24.67  25.60  25.60  25.70  2.10	47.34 47.12 46.90 CB Head (m) 2.10  2.10	9.78 9.78 9.78 9.78 9.78 9.78 9.78   Orelease (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.08 1.87 1.37   Orelease (L/s) 1.47 1.37	37.56 37.34 37.12  Vreq (cu. m) 385.34  Unc  Qstored (L/s)  Unc	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 vontrolled - l	Check OK
100-year V	171 172 173 Surface Str Vater Level  rage Area: Area (ha): C: tc (min) 10 20 30 40 50 60 70 80 90 1120  tc (min) 10 20 30 40 60 70 80 90 100 110 10 20 30 40 50 60 70 80 90 100 110 100 100 100 100 100 100 100	24.89 24.78 24.67  parage Above  2.10  EXT-2 0.06 0.25  1(100 yr) (mm/hr) 178.56 119.95 55.89 49.79 44.99 41.11 0.10 0.73  I(100 yr) (mm/hr) 178.56 6119.95 91.87 75.15 63.95 55.89 49.79 44.99 41.11 37.90 32.89	47.34 47.12 46.90  CB  Head (m) 2.10  7.45 5.00 3.83 3.13 2.67 2.33 2.16 1.58 1.47 1.37  Qactual (L/s) 1.58 1.47 1.37  Qactual (L/s) 2.90 2.08 1.81 2.10 2.09 2.08 2.08 2.08 2.08 2.08 2.08 2.08 2.08	9.78 9.78 9.78 9.78 9.78 9.78 9.78  Qrelease (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.16 1.58 1.47 1.57 1.58 1.47 1.59 2.4.18 18.52 1.51 12.89 9.07 8.29 9.7 8.49 9.07 8.29 9.7 8.29	37.56 37.34 37.12  Vreq (cu. m) 385.34  Unc  Qstored (L/s)  Unc	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 vontrolled - l	Check OK
100-year V	171 172 173 Surface Str Vater Level  lage Area: Area (ha): C: tc (min) 20 30 40 100 110 120  lage Area: Area (ha): C: tc (min) 30 40 50 60 70 80 90 100 20 30 40 100 100 100 100 100 100 100 100 100	24.89 24.78 24.67  24.78 24.67  24.67  24.67  25.60  25.60  25.70  2.10	47.34 47.12 46.90 CB Head (m) 2.10  2.10	9.78 9.78 9.78 9.78 9.78 9.78 9.78   Orelease (L/s) 7.45 5.00 3.83 3.13 2.67 2.33 2.08 1.87 1.37   Orelease (L/s) 1.47 1.37	37.56 37.34 37.12  Vreq (cu. m) 385.34  Unc  Qstored (L/s)  Unc	385.34 385.34 385.34 Vavail (cu. m) 389.64 4.30 vontrolled - l	Check OK

# Project #160401271, 2978 Carp Road Modified Rational Method Calculatons for Storage

SUMMARY TO OUTLET			
		Vrequired Vavai	lable*
Tributary Area	1.140 ha		
Total 5yr Flow to Sewer	10 L/s	0	0 m <sup>3</sup> O
Non-Tributary Area	0.160 ha		
Total 5yr Flow Uncontrolled	27 L/s		
Total Area	1.300 ha		
Total 5yr Flow	37 L/s		
Target	51 L/s		

# Project #160401271, 2978 Carp Road Modified Rational Method Calculatons for Storage

SUMMARY TO OUTLET						l
			Vrequired	Vavailable*		ı
Tributary Area	1.140	ha	· ·			L
Total 100yr Flow to Sewer	10	L/s	0	C	) m <sup>3</sup>	0
Non-Tributary Area	0.160	ha				l
Total 100yr Flow Uncontrolled	43	L/s				l
Total Area	1.300	ha				l
Total 100yr Flow	53	L/s				ı
Target	86	L/s				ı

#### Infiltration Trench and Basin Sizing

#### 1) Summary of Site Areas

Area ID	area (ha)	% imp	imperv area (ha)
STM-1	1.14	44.74	0.51

a.) 100year rainfall depth	96.00 mm	12hr rainfall event per Carp River Model critical event
b.) Total site impervious area	0.51 ha	
c.) 100year runoff volume	489.6 m3	$c = a \times b \times 10,000/1,000$
d.) Volume to be infiltrated in pond	489.6 m3	d = c
e.) MRM Storage Volume Required 3) Dry Pond Volume	<b>385.34</b> m3	From Modified Rational Method calculation sheets used iteratively with infiltration calculations
f.) Bottom area	740.00 m2	Per design drawings
g.) Top area	912.22 m2	Per design drawings
h.) depth	0.50 m	Per design drawings
i.) dry pond freeboard	0.10 m	Per design drawings
j.) active depth	0.40 m	Per design drawings
k.) Pond volume	330.44 m3	$k = ((f + g) / 2) \times j$

#### 4) Infiltration Basin Under Pond for Trench Spillover Volume

I.) area	740.00 m2	Per design drawings
m.) depth	0.20 m	Per design drawings
n.) volume	148.00 m3	n = l x m
o.) Porosity of clearsone basin	0.40	
p.) Infiltration basin storage volume	59.20 m3	p = n x o

#### 5) Calculate min infiltration rate for drawdown time

q.) Total storage volume	<b>389.64</b> m3	q = k + p
r.) Total water depth	0.40 m	r = j
s.) Target drawdown time	48.00 hr	Standard
t.) Required infiltration rate	8.33 mm/hr	t = r / s

u.) Measured infiltration rate 9.46 mm/hr Per field testing (average of TP 11&12)

#### 6) Calculate Flow Rate Through Pond Bottom

Q=KA(h2-h1)/L

depth to g/w from surface of pond 1.15 m TP 11 & BH 10 per Paterson Investigation

K =	8.50E-06 m/s	Per field testing
h2 =	1.15 m	
h1 =	0.45 m	
L=	0.45 m	
A=	740.00 m2	
Q=	0.00978 m3/s	
	0.78 l/e	controlled flow rate that can be input to MRM sheet

Appendix B Stormwater Management December 21, 2016

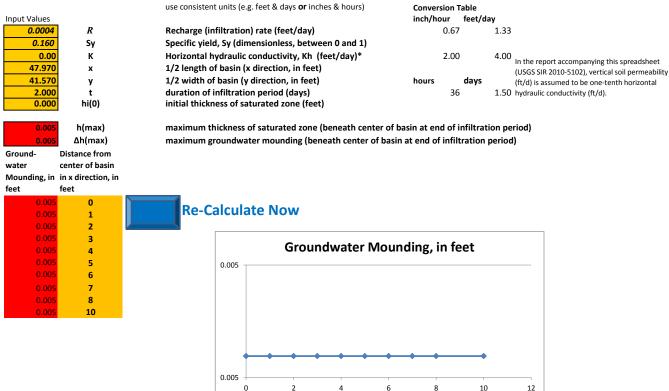
## **B.2 GROUNDWATER MOUNDING CALCULATIONS**



This spreadsheet will calculate the height of a groundwater mound beneath a stormwater infiltration basin. More information can be found in the U.S. Geological Survey Scientific Investigations Report 2010-5102 "Simulation of groundwater mounding beneath hypothetical stormwater infiltration basins".

The user must specify infiltration rate (R), specific yield (Sy), horizontal hydraulic conductivity (Kh), basin dimensions (x, y), duration of infiltration period (t), and the initial thickness of the saturated zone (hi(0), height of the water table if the bottom of the aquifer is the datum). For a square basin the half width equals the half length (x = y). For a rectangular basin, if the user wants the water-table changes perpendicular to the long side, specify x as the short dimension and y as the long dimension. Conversely, if the user wants the values perpendicular to the short side, specify y as the short dimension, x as the long dimension. All distances are from the center of the basin. Users can change the distances from the center of the basin at which water-table aquifer thickness are calculated.

Cells highlighted in yellow are values that can be changed by the user. Cells highlighted in red are output values based on user-specified inputs. The user MUST click the blue "Re-Calculate Now" button each time ANY of the user-specified inputs are changed otherwise necessary iterations to converge on the correct solution will not be done and values shown will be incorrect. Use consistent units for all input values (for example, feet and days)



#### **Disclaimer**

This spreadsheet solving the Hantush (1967) equation for ground-water mounding beneath an infiltration basin is made available to the general public as a convenience for those wishing to replicate values documented in the USGS Scientific Investigations Report 2010-5102 "Groundwater mounding beneath hypothetical stormwater infiltration basins" or to calculate values based on user-specified site conditions. Any changes made to the spreadsheet (other than values identified as user-specified) after transmission from the USGS could have unintended, undesirable consequences. These consequences could include, but may not be limited to: erroneous output, numerical instabilities, and violations of underlying assumptions that are inherent in results presented in the accompanying USGS published report. The USGS assumes no responsibility for the consequences of any changes made to the spreadsheet. If changes are made to the spreadsheet, the user is responsible for documenting the changes and justifying the results and conclusions.

Appendix B Stormwater Management December 21, 2016

# B.3 REMOVAL RATES FOR BUFFER STRIPS-US EPA DESIGN MANUAL FOR LOW IMPACT DEVELOPMENT (LID)



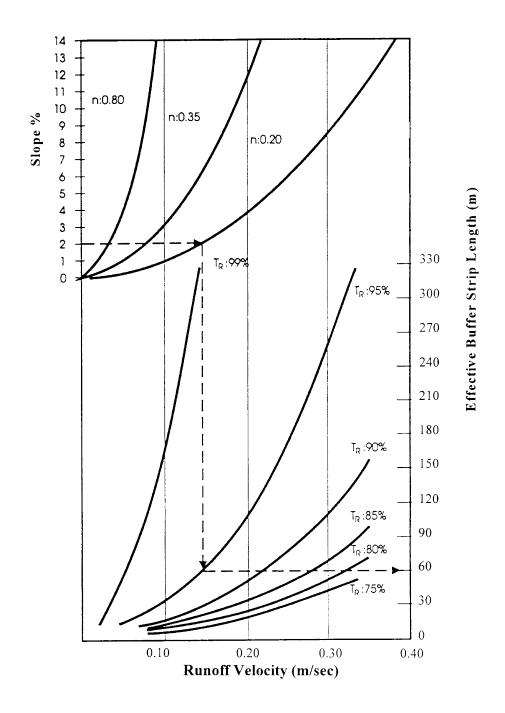


Figure 5-4 Removal rates (TR) for Buffer Strips (Wong and McCuen, 1982) (Reprinted with Permission of ASCE)

There are some significant limitations to design chart method as it does not take into account the particle size of the material or the infiltration rate of the soils. Consequently it over predicts trapping efficiency of soils with low permeability and under predicts trapping efficiency of soils with high permeability. For these reasons, the design

Appendix C Geotechnical Investigation December 21, 2016

# Appendix C GEOTECHNICAL INVESTIGATION

## C.1 EXCERPTS FROM PATERSONGROUP INVESTIGATION



Geotechnical Engineering

Environmental Engineering

**Hydrogeology** 

Geological Engineering

**Materials Testing** 

**Building Science** 

**Archaeological Services** 

# patersongroup

### **Geotechnical Investigation**

Proposed Storage Building 2978 and 2966 Carp Road Ottawa, Ontario

**Prepared For** 

York-HOP Inc.

## **Paterson Group Inc.**

Consulting Engineers 154 Colonnade Road South Ottawa, Ontario Canada K2E 7J5

Tel: (613) 226-7381 Fax: (613) 226-6344 www.patersongroup.ca November 11, 2016

Report PG3834-1R



Table 1 - Su	mmary of Groundw	ater Level Reading	s	
Test hole Number	Ground Surface Elevation (m)	Groundwater Depth (m)	Groundwater Elevation (m)	Date
BH 2	118.42	Dry	-	June 6, 2016
BH 6	117.71	3.93	113.78	June 6, 2016
BH 8	117.54	4.19	113.35	June 6, 2016
BH 10	117.46	3.62	113.84	June 6, 2016
BH 11	117.45	Blocked	-	June 6, 2016

Groundwater is subject to seasonal fluctuations and therefore, groundwater could vary at the time of construction.

### 4.4 Pask Permeameter Testing

A total of six (6) constant head Pask permeameter tests were conducted at the test locations to verify the existing hydraulic conductivities of the soils below the proposed infiltration system at the subject site. The permeameter test locations were selected by Stantec in a manner to provide general coverage of proposed infiltration system. The hydraulic conductivity ( $K_{fs}$ ) values for each test hole location is presented in Table 2.

Table 2 - Hydraulic Conductivity Values						
Test hole	<b>D</b> (1 ( 1 )	18T	IZ ( a la cara)			
Number	Depth (m bgs)	Easting (m)	Northing (m)	K <sub>fs</sub> (m/sec)		
TP 1	0.9	421970	5018202	3.20E-07		
TP 4	0.6	422013	5018181	9.40E-07		
TP 5	0.7	421951	5018215	9.40E-08		
TP 11	0.9	422035	5018200	5.30E-06		
TP 12	1.1	422021	5018187	1.20E-05		
TP 13	1.0	422049	5018186	5.30E-06		

The values measured within the test hole locations are consistent with similar material Paterson has encountered on other sites. These values typically range from 1 x  $10^{-5}$  to 1 x  $10^{-7}$  m/sec due to the variability of the material encountered.



Table 3 - Recomme	nded Pavement Structure - Car Only Parking Areas
Thickness (mm)	Material Description
50	Wear Course - HL-3 or Superpave 12.5 Asphaltic Concrete
150	BASE - OPSS Granular A Crushed Stone
300	SUBBASE - OPSS Granular B Type II
	<b>SUBGRADE</b> - Either fill, in situ soil, or OPSS Granular B Type II material placed over in situ soil or fill

Table 4 - Recommended Pavement Structure - Access Lanes						
Thickness (mm)	Material Description					
40	Wear Course - HL-3 or Superpave 12.5 Asphaltic Concrete					
50	Binder Course - HL-8 or Superpave 19.0 Asphaltic Concrete					
150	BASE - OPSS Granular A Crushed Stone					
400	SUBBASE - OPSS Granular B Type II					
	SUBGRADE - Either fill, in situ soil, or OPSS Granular B Type II material placed over in situ soil or fill					

Minimum Performance Graded (PG) 58-34 asphalt cement should be used for this project. The pavement granular base and subbase should be placed in maximum 300 mm thick lifts and compacted to a minimum of 100% of the material's SPMDD using suitable compaction equipment.

It is our understanding that consideration is being taken to using a gravel pavement structure for car parking, access lanes and fire routes as part of the proposed development. The gravel pavement structure is further detailed in Table 5. It is expected that the gravel pavement structure may require annual maintenance, such as regrading and padding in poor performing areas.

Table 5 - Gravel Pavement Structure - Car Parking, Access Lanes and Fire Routes						
Thickness (mm) Material Description						
300	BASE - OPSS Granular A Crushed Stone					
	SUBGRADE - Either fill, in situ soil, or OPSS Granular B Type II material placed over in situ soil or fill					

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

**SOIL PROFILE AND TEST DATA** 

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

DATUM

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation =

FILE NO.

119.73m.

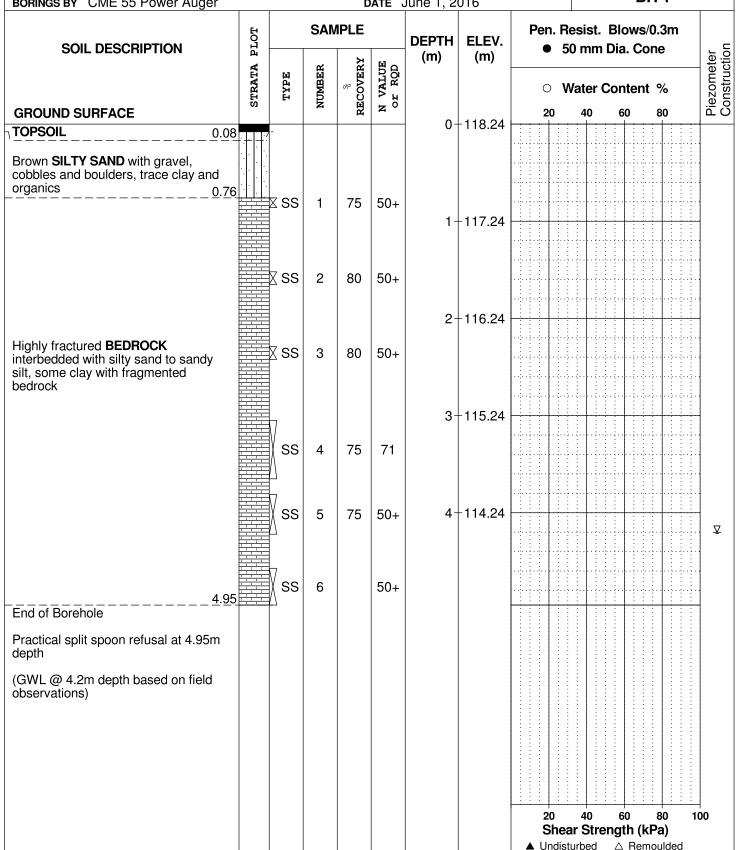
REMARKS

BORINGS BY CME 55 Power Auger

DATE June 1, 2016

PG3834

HOLE NO.
BH 1



**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

**DATUM** TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = 119.73m.

FILE NO. PG3834

**REMARKS** HOLE NO. **BH 2 DATE** June 1, 2016 BORINGS BY CME 55 Power Auger **SAMPLE** Pen. Resist. Blows/0.3m STRATA PLOT **DEPTH** ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) RECOVERY N VALUE or RQD NUMBER Water Content % **GROUND SURFACE** 80 20 0+118.42**TOPSOIL** 0.10 Brown SILTY SAND with gravel. cobbles and boulders, trace clay and organics 1+117.42SS 1 92 51 1.45 × SS 2 25 50+ 2+116.42 Highly fractured **BEDROCK** interbedded with silty sand to sandy silt, some clay with fragmented bedrock 3+115.42 $\mathbf{SS}$ 3 50 +50 4+114.42 4.80 SS 4 67 50+ End of Borehole Practical split spoon refusal at 4.80m depth (BH dry - June 6, 2016) 40 60 100 Shear Strength (kPa) ▲ Undisturbed △ Remoulded

**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

**Geotechnical Investigation** Proposed Storage Building - 2978 & 2966 Carp Road

▲ Undisturbed

△ Remoulded

Ottawa, Ontario TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = FILE NO. **DATUM PG3834** 119.73m. **REMARKS** HOLE NO. **BH 3 DATE** June 1, 2016 BORINGS BY CME 55 Power Auger **SAMPLE** Pen. Resist. Blows/0.3m STRATA PLOT **DEPTH** ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) N VALUE or RQD RECOVERY NUMBER Water Content % 80 **GROUND SURFACE** 20 0+118.29**TOPSOIL** 0.15 Brown SILTY SAND with gravel, cobbles and boulders, trace clay and organics SS 1 50+ Highly fractured **BEDROCK** 1+117.29interbedded with silty sand to sandy silt, some clay with fragmented bedrock End of Borehole Practical refusal to augering at 1.12m depth (BH dry upon completion) 40 60 100 Shear Strength (kPa)

**Geotechnical Investigation** Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

119.73m.

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation =

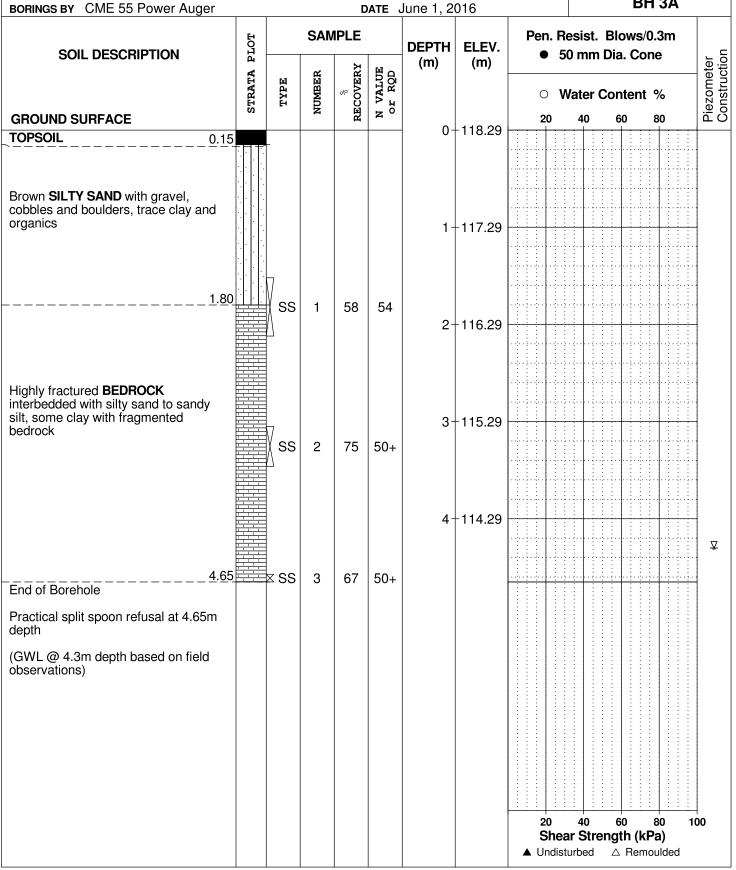
**REMARKS** 

**DATUM** 

FILE NO. **PG3834** 

HOLE NO.

**BH 3A DATE** June 1, 2016 BORINGS BY CME 55 Power Auger



**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = PG3834

REMARKS

PORTINGS BY CME 55 Power August

PATE | June 1, 2016

BORINGS BY CME 55 Power Auger				D	ATE .	June 1, 2	016		HOLE NO.	BH 4	
SOIL DESCRIPTION	PLOT		SAN	SAMPLE		DEPTH (m)	ELEV. (m)	Pen. Resist. Blows/0.3n  • 50 mm Dia. Cone			
	STRATA	TYPE	NUMBER	% RECOVERY	N VALUE or RQD	()	()		Vater Conte		Piezometer
GROUND SURFACE				<b>A</b>		0-	118.03	20	40 60	80	凸
OPSOIL 0.08 brown SILTY SAND with gravel, obbles and boulders, trace clay and rganics 0.66		,- -									
		ss	1	50	46	1 -	-117.03				
lighly fractured <b>BEDROCK</b> nterbedded with silty sand to sandy ilt, some clay with fragmented edrock		ss	2		68	2-	-116.03				
		<u> </u>									
ractical refusal to augering at 2.59m											
epth BH dry upon completion)											
or any apoin completion)											
								20	40 60	80 10	00
								Shea ▲ Undist	ar Strength urbed △ R	( <b>kPa</b> ) emoulded	

**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = 119.73m.

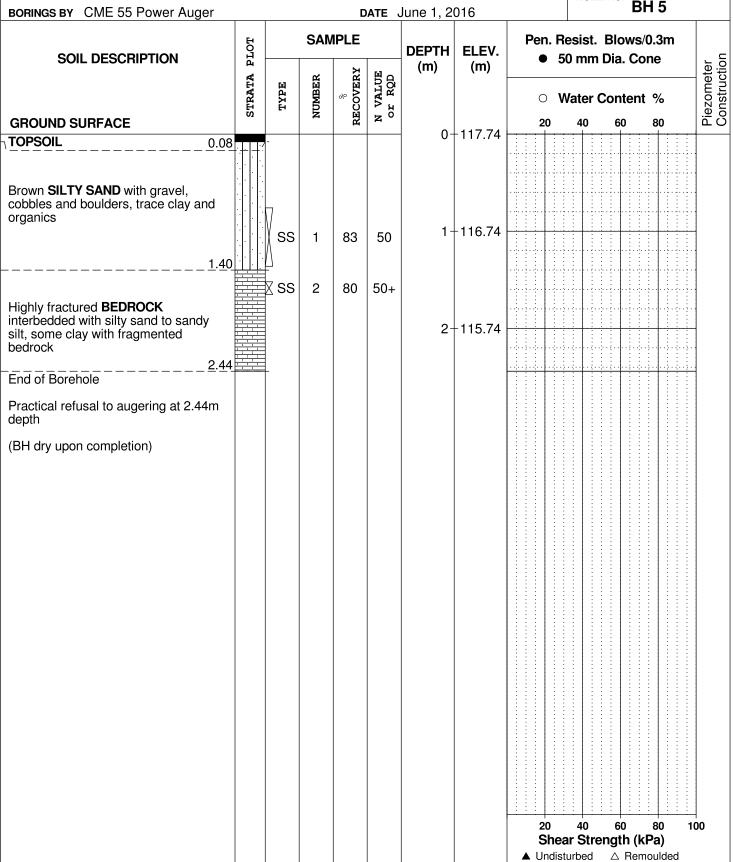
REMARKS

BORINGS BY CME 55 Power Auger

PATE June 1 2016

FILE NO. PG3834

HOLE NO. BH 5



**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

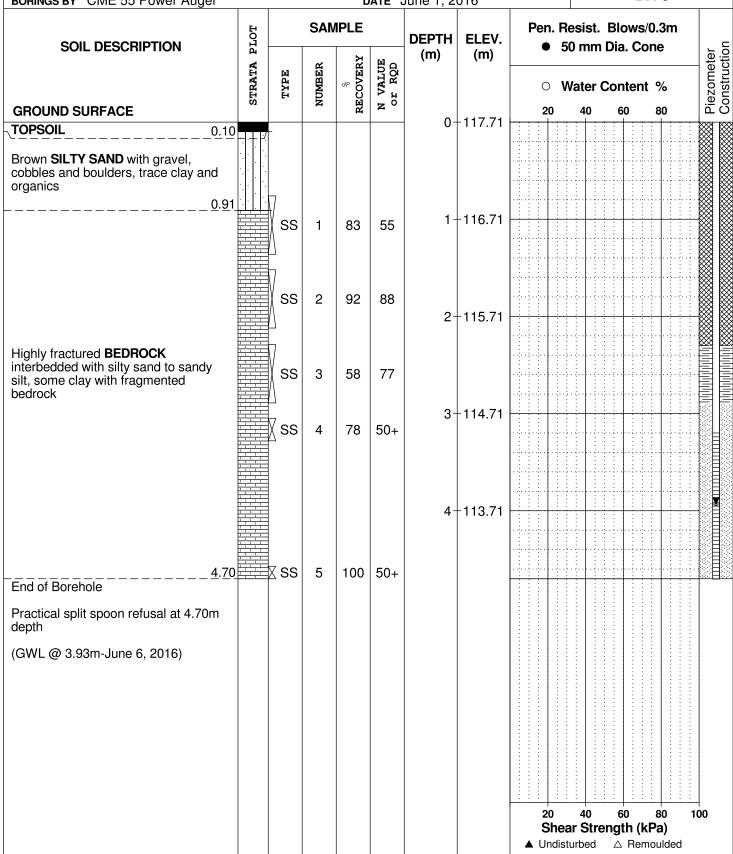
**Geotechnical Investigation** Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

**DATUM** 

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation =

FILE NO.

**PG3834** 119.73m. **REMARKS** HOLE NO. **BH 6 DATE** June 1, 2016 BORINGS BY CME 55 Power Auger



154 Colonnade Road South, Ottawa, Ontario K2E 7J5

**SOIL PROFILE AND TEST DATA** 

**Geotechnical Investigation** Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

**DATUM** 

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation =

FILE NO.

40

▲ Undisturbed

Shear Strength (kPa)

60

△ Remoulded

100

**PG3834** 119.73m. **REMARKS** HOLE NO. **BH7 DATE** June 1, 2016 BORINGS BY CME 55 Power Auger **SAMPLE** Pen. Resist. Blows/0.3m PLOT DEPTH ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) RECOVERY N VALUE or RQD STRATA NUMBER Water Content % **GROUND SURFACE** 80 20 0 + 117.53**TOPSOIL** 0.30 Brown SILTY SAND with gravel. cobbles and boulders, trace clay and organics SS 1 80 50+ 1 + 116.532 SS 21 51 2+115.53Highly fractured **BEDROCK** interbedded with silty sand to sandy silt, some clay with fragmented bedrock 3+114.53SS 3 40 50 +⊻ 4+113.53⊠ SS 4 100 50 +End of Borehole Practical split spoon refusal at 4.65m depth (GWL @ 3.7m depth based on field observations)

**SOIL PROFILE AND TEST DATA** 

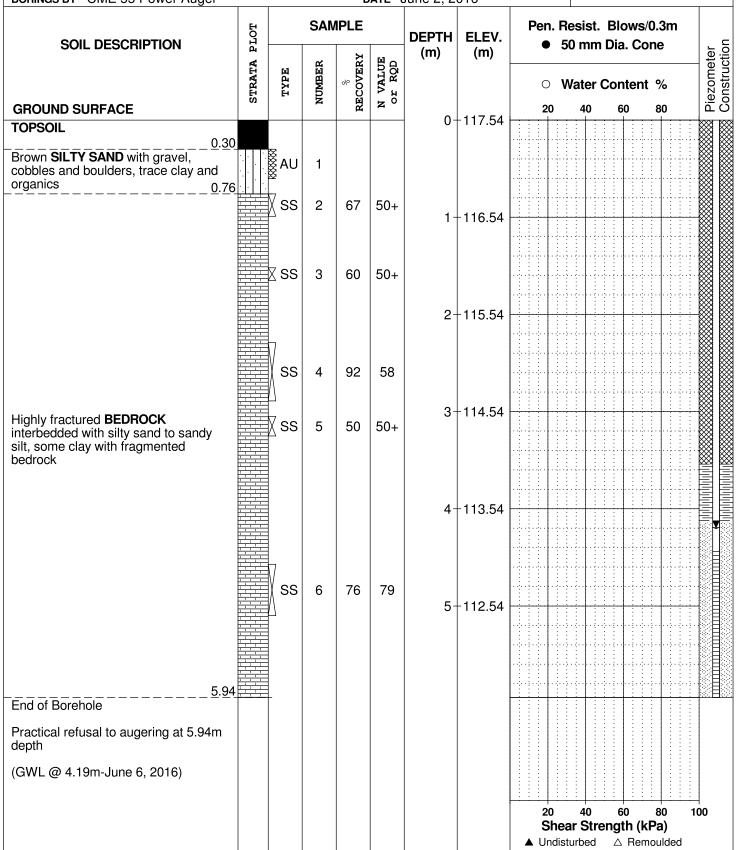
**Geotechnical Investigation** 

Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation =

FILE NO. **DATUM PG3834** 119.73m. **REMARKS** HOLE NO. **BH8 DATE** June 2, 2016 BORINGS BY CME 55 Power Auger **SAMPLE** Pen. Resist. Blows/0.3m ELEV.



**SOIL PROFILE AND TEST DATA** 

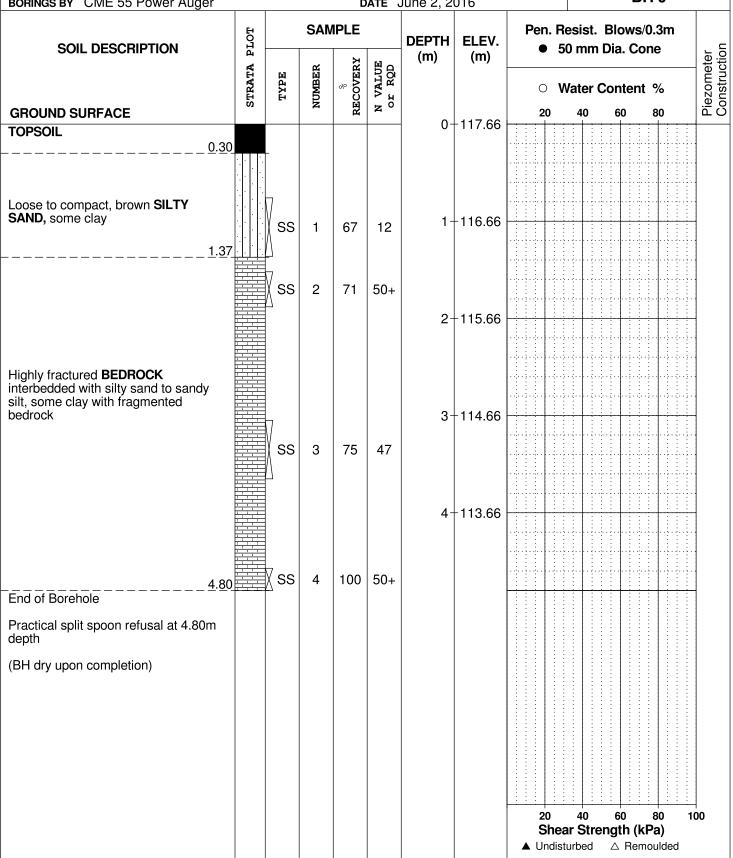
154 Colonnade Road South, Ottawa, Ontario K2E 7J5

**Geotechnical Investigation** Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

**DATUM** 

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation =

FILE NO. **PG3834** 119.73m. **REMARKS** HOLE NO. **BH9 DATE** June 2, 2016 **BORINGS BY** CME 55 Power Auger



**SOIL PROFILE AND TEST DATA** 

▲ Undisturbed

△ Remoulded

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

**Geotechnical Investigation** Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = FILE NO. **DATUM PG3834** 119.73m. **REMARKS** HOLE NO. **BH10 DATE** June 2, 2016 BORINGS BY CME 55 Power Auger **SAMPLE** Pen. Resist. Blows/0.3m PLOT **DEPTH** ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) RECOVERY N VALUE or RQD STRATA NUMBER Water Content % **GROUND SURFACE** 80 20 0+117.46**TOPSOIL** 0.10 Loose to compact, brown SILTY SAND, some clay 1+116.46SS 1 75 21 1.37 2 SS 58 49 2+115.46Highly fractured **BEDROCK** interbedded with silty sand to sandy silt, some clay with fragmented bedrock 3+114.46SS 3 50+ 80 4 + 113.46End of Borehole Practical refusal to augering at 4.27m depth (GWL @ 3.62m-June 6, 2016) 40 60 100 Shear Strength (kPa)

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

SOIL PROFILE AND TEST DATA

**Geotechnical Investigation** Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

**DATUM** 

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = 119.73m.

FILE NO.

**PG3834** 

**REMARKS** HOLE NO. **BH11 DATE** June 2, 2016 BORINGS BY CME 55 Power Auger **SAMPLE** Pen. Resist. Blows/0.3m PLOT **DEPTH** ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) RECOVERY N VALUE or RQD STRATA NUMBER Water Content % 80 **GROUND SURFACE** 20 0+117.45**TOPSOIL** 1 0.60 Brown SILTY SAND with gravel, cobbles and boulders, trace clay and 1+116.45SS 2 70 11 organics SS 3 75 62 Highly fractured **BEDROCK** 2+115.45interbedded with silty sand to sandy silt, some clay with fragmented bedrock 3+114.45End of Borehole Practical refusal to augering at 3.05m (Piezometer blocked at 1.72m depth - June 6, 2016) 40 60 80 100 Shear Strength (kPa) ▲ Undisturbed △ Remoulded

1.30 ₽

**SOIL PROFILE AND TEST DATA** 

40

▲ Undisturbed

Shear Strength (kPa)

60

△ Remoulded

100

**Geotechnical Investigation** Proposed Storage Building - 2978 & 2966 Carp Road 154 Colonnade Road South, Ottawa, Ontario K2E 7J5 Ottawa, Ontario TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = FILE NO. **DATUM PG3834** 119.73m. **REMARKS** HOLE NO. TP 1 **BORINGS BY** Backhoe DATE November 3, 2016 **SAMPLE** Pen. Resist. Blows/0.3m STRATA PLOT **DEPTH** ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) N VALUE or RQD RECOVERY NUMBER Water Content % 80 **GROUND SURFACE** 20 0+117.72**TOPSOIL** 1 0.20 Brown SILTY SAND to SANDY SILT, some tree roots G 2 1+116.721.20

End of Test Pit

TP terminated on fractured bedrock surface at 1.30m depth

(TP dry upon completion)

Highly fractured **BEDROCK** with

sandy silt, gravel, cobbles and

**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = FILE NO. **DATUM PG3834** 119.73m. **REMARKS** HOLE NO. TP 2 **BORINGS BY** Backhoe DATE November 3, 2016 **SAMPLE** Pen. Resist. Blows/0.3m STRATA PLOT **DEPTH** ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) N VALUE or RQD RECOVERY NUMBER Water Content % 80 **GROUND SURFACE** 20 0+118.08**TOPSOIL** 0.20 Highly fractured **BEDROCK** with sandy silt, gravel, cobbles and boulders, some clay 0.70 End of Test Pit TP terminated on fractured bedrock surface at 0.70m depth (TP dry upon completion) 40 60 100 Shear Strength (kPa) ▲ Undisturbed △ Remoulded

**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = FILE NO. **DATUM PG3834** 119.73m. **REMARKS** HOLE NO. TP 3 **BORINGS BY** Backhoe DATE November 3, 2016 **SAMPLE** Pen. Resist. Blows/0.3m PLOT DEPTH ELEV. Piezometer Construction **SOIL DESCRIPTION** • 50 mm Dia. Cone (m) (m) N VALUE or RQD RECOVERY STRATA NUMBER Water Content % **GROUND SURFACE** 80 20 0+117.47**TOPSOIL** 0.20 Brown SILTY SAND to SANDY SILT 0.50 Highly fractured **BEDROCK** with 1+116.47sandy silt, gravel, cobbles and boulders, some clay End of Test Pit TP terminated on fractured bedrock surface at 1.60m depth (TP dry upon completion) 40 60 100 Shear Strength (kPa) ▲ Undisturbed △ Remoulded

**SOIL PROFILE AND TEST DATA** 

▲ Undisturbed

△ Remoulded

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = FILE NO. **DATUM PG3834** 119.73m. **REMARKS** HOLE NO. TP 4 **BORINGS BY** Backhoe DATE November 3, 2016 **SAMPLE** Pen. Resist. Blows/0.3m STRATA PLOT **DEPTH** ELEV. Piezometer Construction • 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) N VALUE or RQD RECOVERY NUMBER Water Content % 80 **GROUND SURFACE** 20 0+117.46**TOPSOIL** 0.30 Brown SILTY SAND to SANDY SILT, some clay, gravel, cobbles and boulders G 1 - clay content increasing with depth 0.80 End of Test Pit TP terminated on dense glacial till at 0.80m depth (TP dry upon completion) 40 60 100 Shear Strength (kPa)

**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

▲ Undisturbed

△ Remoulded

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = FILE NO. **DATUM PG3834** 119.73m. **REMARKS** HOLE NO. TP 5 **BORINGS BY** Backhoe DATE November 3, 2016 **SAMPLE** Pen. Resist. Blows/0.3m PLOT **DEPTH** ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) N VALUE or RQD RECOVERY STRATA NUMBER Water Content % **GROUND SURFACE** 80 20 0+118.06**TOPSOIL** 0.20 Brown SANDY SILT with clay to G 1 SILTY SAND 0.50 Highly fractured **BEDROCK** with sandy silt, gravel, cobbles and boulders, some clay 1 + 117.06End of Test Pit TP terminated on fractured bedrock surface at 1.30m depth (TP dry upon completion) 40 60 100 Shear Strength (kPa)

**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = 119.73m.							FILE NO. PG3834						
REMARKS BORINGS BY Backhoe		DATE November 3, 2016											
SOIL DESCRIPTION		SAMPLE				DEPTH EL	ELEV.	Pen. Resist. Blows/0.3m  • 50 mm Dia. Cone				7 5	
	STRATA PLOT	TYPE	NUMBER	% RECOVERY	N VALUE or RQD	(m)	(m)	O Water Content %				Piezometer Construction	
GROUND SURFACE	ST						Piez						
TOPSOIL 0.10						0+	-118.08						
Highly fractured <b>BEDROCK</b>													
End of Test Pit		-											
TP terminated on fractured bedrock surface at 0.40m depth													
(TP dry upon completion)													
								20	40	6	0 8	D 10	00
								Shea  ▲ Undisti	r Str	engt	h (kPa	)	

**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = FILE NO. **DATUM PG3834** 119.73m. **REMARKS** HOLE NO. TP 7 **BORINGS BY** Backhoe DATE November 3, 2016 **SAMPLE** Pen. Resist. Blows/0.3m PLOT DEPTH ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) N VALUE or RQD RECOVERY STRATA NUMBER Water Content % **GROUND SURFACE** 80 20 0+117.37TOPSOIL 0.15 Brown SILTY SAND 1 G Highly fractured **BEDROCK** with silty clay, sand, gravel, cobbles and boulders 1 + 116.37End of Test Pit TP terminated on fractured bedrock surface at 1.10m depth (TP dry upon completion) 40 60 100 Shear Strength (kPa) ▲ Undisturbed △ Remoulded

SOIL PROFILE AND TEST DATA

40

▲ Undisturbed

Shear Strength (kPa)

60

△ Remoulded

100

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = FILE NO. **DATUM PG3834** 119.73m. **REMARKS** HOLE NO. TP8 **BORINGS BY** Backhoe DATE November 3, 2016 **SAMPLE** Pen. Resist. Blows/0.3m STRATA PLOT **DEPTH** ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) N VALUE or RQD RECOVERY NUMBER Water Content % **GROUND SURFACE** 80 20 0+118.54Crushed stone 0.05 **TOPSOIL** 0.20 Brown SILTY SAND, trace gravel 0.80 1 + 117.54Highly fractured **BEDROCK** with brown silty sand, gravel and cobbles, trace boulders G 1 End of Test Pit TP terminated on fractured bedrock surface at 1.50m depth (TP dry upon completion)

SOIL PROFILE AND TEST DATA

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = FILE NO. **DATUM PG3834** 119.73m. **REMARKS** HOLE NO. TP 9 **BORINGS BY** Backhoe DATE November 3, 2016 **SAMPLE** Pen. Resist. Blows/0.3m STRATA PLOT DEPTH ELEV. Piezometer Construction 50 mm Dia. Cone **SOIL DESCRIPTION** (m) (m) RECOVERY N VALUE or RQD NUMBER Water Content % **GROUND SURFACE** 80 20 0+118.16**TOPSOIL** 0.20 Brown SILTY SAND with clay and fractured bedrock by 0.4m depth 0.65 G 1 Highly fractured **BEDROCK** with 1+117.16grey-brown silty sand, gravel, cobbles and boulders End of Test Pit TP terminated on fractured bedrock surface at 1.5m depth (TP dry upon completion) 40 60 100 Shear Strength (kPa) ▲ Undisturbed △ Remoulded

**SOIL PROFILE AND TEST DATA** 

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

Geotechnical Investigation Proposed Storage Building - 2978 & 2966 Carp Road Ottawa, Ontario

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = 119.73m.

REMARKS

BORINGS BY Backhoe

TBM - Top of magnetic nail in utility pole on Carp Road. Geodetic elevation = PG3834

HOLE NO. TP10

**SAMPLE** Pen. Resist. Blows/0.3m PLOT DEPTH ELEV. Piezometer Construction **SOIL DESCRIPTION** 50 mm Dia. Cone (m) (m) RECOVERY N VALUE or RQD STRATA NUMBER Water Content % **GROUND SURFACE** 80 20 0+118.24**TOPSOIL** 0.20 Brown SILTY SAND with cobbles 0.60 **Grey SILTY CLAY** G 1 0.85 Brown SILTY SAND 2 1+117.24 High fractured **BEDROCK** with brown silty sand, cobbles and boulders 2+116.24G 3 2.84 End of Test Pit TP terminated on fractured bedrock surface at 2.84m depth (TP dry upon completion) 40 60 100 Shear Strength (kPa) ▲ Undisturbed △ Remoulded

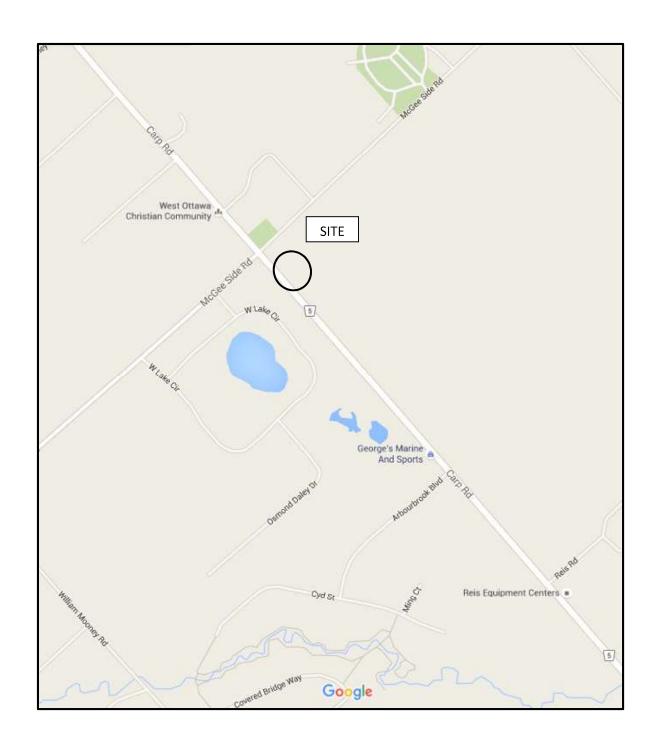
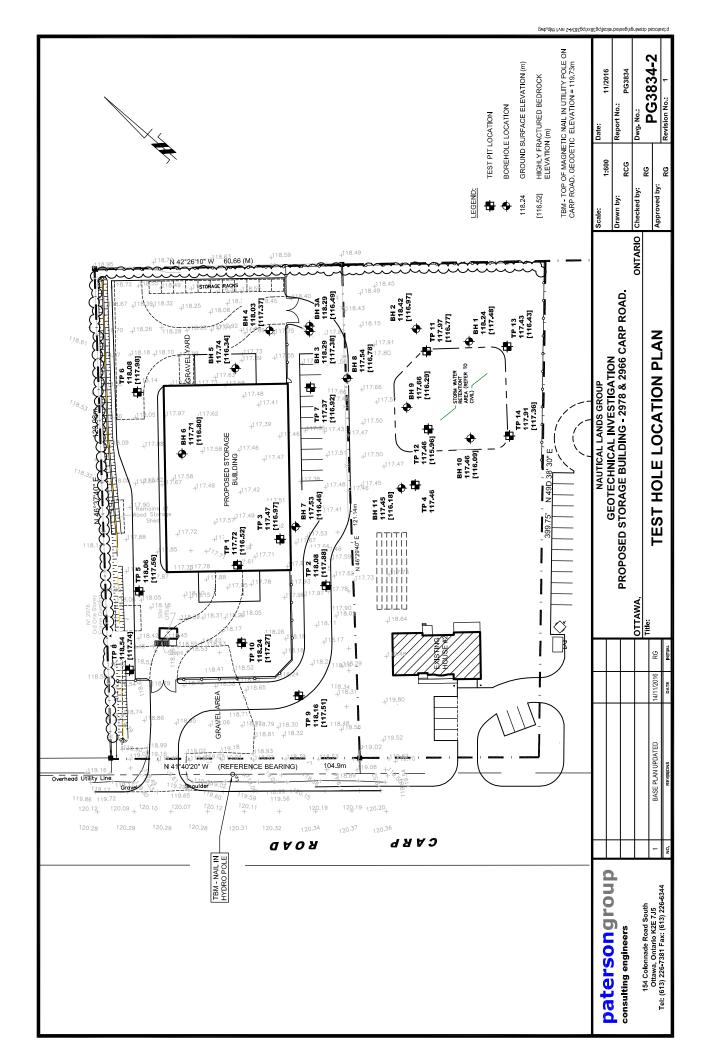


Figure 1 – Key Plan



### **SERVICING REPORT - 2978 CARP ROAD**

Appendix D Drawings December 21, 2016

## Appendix D DRAWINGS



## **C.3** Environmental Compliance Approval (ECA)



### **Content Copy Of Original**



Ministry of the Environment and Climate Change Ministère de l'Environnement et de l'Action en matière de changement climatique

### **ENVIRONMENTAL COMPLIANCE APPROVAL**

NUMBER 9196-AQBQZV Issue Date: October 6, 2017

York-Hop Corp. 2962 Carp Road Ottawa, Ontario K0A 1T0

Site Location: 2978 and 2966 Carp Road

City of Ottawa

You have applied under section 20.2 of Part II.1 of the Environmental Protection Act, R.S.O. 1990, c. E. 19 (Environmental Protection Act) for approval of:

the establishment of stormwater management works to service the 1.30 hectare warehouse storage site at 2978 and 2966 Carp Road, in the City of Ottawa, for the collection, treatment and disposal of stormwater run-off, to provide Normal Level quality control and erosion protection, and to infiltrate and attenuate the post-development peak flows for all storm events up to and including the 100-year storm to allowable release rates, consisting of the following:

**infiltration basin (catchment area 1.14 ha)** located at the southeast corner of the site, with vegetated buffer area providing pre-treatment, comprising of 200 millimetre thick layer of 50 millimetre diameter clear stone covered by filter fabric, to store and infiltrate stormwater run-off from the site, having a total storage volume of approximately 389.6 m 3, with an emergency overland flow in excess of the 100-year storm to the neighbouring property to the south;

including erosion/sedimentation control measures during construction and all other controls and appurtenances essential for the proper operation of the aforementioned Works;

all in accordance with the submitted supporting documents listed in Schedule "A" forming part of this Approval.

For the purpose of this environmental compliance approval, the following definitions apply:

- 1. "Approval" means this entire document and any schedules attached to it, and the application;
- 2. "Director" means a person appointed by the Minister pursuant to section 5 of the EPA for the purposes of Part II.1 of the EPA;
- 3. "District Manager" means the District Manager of the appropriate local District Office of the Ministry, where the Works are geographically located;
- 4. "EPA" means the Environmental Protection Act, R.S.O. 1990, c.E.19, as amended;
- 5. "Ministry" means the ministry of the government of Ontario responsible for the EPA and OWRA and includes all officials, employees or other persons acting on its behalf;
- 6. "Owner" means York-Hop Corp., and includes its successors and assignees;
- 7. "OWRA" means the Ontario Water Resources Act, R.S.O. 1990, c. O.40, as amended;
- 8. "Works" means the sewage works described in the Owner's application, and this Approval.

You are hereby notified that this environmental compliance approval is issued to you subject to the terms and conditions outlined below:

### **TERMS AND CONDITIONS**

#### 1. GENERAL CONDITIONS

- 1. The Owner shall ensure that any person authorized to carry out work on or operate any aspect of the Works is notified of this Approval and the conditions herein and shall take all reasonable measures to ensure any such person complies with the same.
- 2. Except as otherwise provided by these Conditions, the Owner shall design, build, install, operate and maintain the Works in accordance with the description given in this Approval, and the application for approval of the Works.
- 3. Where there is a conflict between a provision of any document in the schedule referred to in this Approval and the conditions of this Approval, the conditions in this Approval shall take precedence, and where there is a conflict between the documents in the schedule, the document bearing the most recent date shall prevail.
- 4. Where there is a conflict between the documents listed in Schedule "A" and the application, the application shall take precedence unless it is clear that the purpose of the document was to amend the application.
- 5. The conditions of this Approval are severable. If any condition of this Approval, or the application of any requirement of this Approval to any circumstance, is held invalid or unenforceable, the application of such condition to other circumstances and the remainder of this Approval shall not be affected thereby.
- 6. The issuance of, and compliance with the conditions of, this Approval does not:
  - a. relieve any person of any obligation to comply with any provision of any applicable statute, regulation or other legal requirement, including, but not limited to, the obligation to obtain approval from the local conservation authority/MNR necessary to construct or operate the sewage works; or
  - b. limit in any way the authority of the Ministry to require certain steps be taken to require the Owner to furnish any further information related to compliance with this Approval.

### 2. EXPIRY OF APPROVAL

- 1. This Approval will cease to apply to those parts of the Work which have not been constructed within five (5) years of the date of this Approval.
- 2. In the event that completion and commissioning of any portion of the Works is anticipated to be delayed beyond the specified expiry period, the Owner shall submit an application of extension to the expiry period, at least twelve (12) months prior to the end of the period. The application for extension shall include the reason(s) for the delay, whether there is any design change(s) and a review of whether the standards applicable at the time of Approval of the Works are still applicable at the time of request for extension, to ensure the ongoing protection of the environment.

### 3. CHANGE OF OWNER

- 1. The Owner shall notify the District Manager and the Director, in writing, of any of the following changes within thirty (30) days of the change occurring:
  - a. change of Owner;
  - b. change of address of the Owner;

- c. change of partners where the Owner is or at any time becomes a partnership, and a copy of the most recent declaration filed under the *Business Names Act*, R.S.O. 1990, c.B17 shall be included in the notification to the District Manager; or
- d. change of name of the corporation where the Owner is or at any time becomes a corporation, and a copy of the most current information filed under the *Corporations Information Act*, R.S.O. 1990, c. C39 shall be included in the notification to the District Manager.
- 2. In the event of any change in ownership of the Works, other than a change to a successor municipality, the Owner shall notify in writing the succeeding owner of the existence of this Approval, and a copy of such notice shall be forwarded to the District Manager and the Director.
- 3. The Owner shall ensure that all communications made pursuant to this condition refer to the number at the top of this Approval.

### 4. OPERATION AND MAINTENANCE

- 1. If applicable, any proposed storm sewers or other stormwater conveyance in this Approval can be constructed but not operated until the proposed stormwater management facilities in this Approval or any other Approval that are designed to service the storm sewers or other stormwater conveyance are in operation.
- 2. The Owner shall make all necessary investigations, take all necessary steps and obtain all necessary approvals so as to ensure that the physical structure, siting and operations of the Works do not constitute a safety or health hazard to the general public.
- 3. The Owner shall inspect and ensure that the design minimum liquid retention volume is maintained in the Works at all times, except when maintenance is required.
- 4. The Owner shall undertake an inspection of the condition of the Works, at least once a year, and undertake any necessary cleaning and maintenance to ensure that sediment, debris and excessive decaying vegetation are removed from the Works to prevent the excessive build-up of sediment, oil/grit, debris and/or decaying vegetation, to avoid reduction of the capacity and/or permeability of the Works, as applicable. The Owner shall also regularly inspect and clean out the inlet to and outlet from the Works to ensure that these are not obstructed.
- 5. The Owner shall design, construct and operate the Works with the objective that the effluent from the Works is essentially free of floating and settleable solids and does not contain oil or any other substance in amounts sufficient to create a visible film, sheen, foam or discoloration on the receiving waters.
- 6. The Owner shall ensure the immediate clean-out of the Works after a fuel or oil spill capture.
- 7. The Owner shall ensure that equipment and material for the containment, clean-up and disposal of fuel and oil and materials contaminated with such, is on hand and in good repair for immediate use in the event of:
  - a. loss of fuel or oil to the Works; or
  - b. a spill within the meaning of Part X of the EPA.
- 8. The Owner shall maintain a logbook to record the results of these inspections and any cleaning and maintenance operations undertaken, and shall keep the logbook at the Owner's administration office for inspection by the Ministry. The logbook shall include the following:
  - a. the name of the Works;
  - b. the date and results of each inspection, maintenance and cleaning, including an estimate of the quantity of any materials removed and method of clean-out of the Works; and
  - c. the date of each spill within the catchment area, including follow-up actions and remedial measures undertaken.
- 9. The Owner shall prepare an operations manual prior to the commencement of operation of the

Works that includes, but is not necessarily limited to, the following information:

- a. operating and maintenance procedures for routine operation of the Works;
- b. inspection programs, including frequency of inspection, for the Works and the methods or tests employed to detect when maintenance is necessary;
- c. repair and maintenance programs, including the frequency of repair and maintenance for the Works;
- d. contingency plans and procedures for dealing with potential spills and any other abnormal situations and for notifying the District Manager; and
- e. procedures for receiving, responding and recording public complaints, including recording any follow-up actions taken.
- 10. The Owner shall maintain the operations manual current and retain a copy at the location of the Works for the operational life of the Works. Upon request, the Owner shall make the manual available to Ministry staff.

### 5. TEMPORARY EROSION AND SEDIMENT CONTROL

- 1. The Owner shall install and maintain temporary sediment and erosion control measures during construction and conduct inspections once every two (2) weeks and after each significant storm event (a significant storm event is defined as a minimum of 25 mm of rain in any 24 hours period). The inspections and maintenance of the temporary sediment and erosion control measures shall continue until they are no longer required and at which time they shall be removed and all disturbed areas reinstated properly.
- 2. The Owner shall maintain records of inspections and maintenance which shall be made available for inspection by the Ministry, upon request. The record shall include the name of the inspector, date of inspection, and the remedial measures. if any, undertaken to maintain the temporary sediment and erosion control measures.

### 6. REPORTING

- 1. One (1) week prior to the start-up of the operation of the Works, the Owner shall notify the District Manager (in writing) of the pending start-up date.
- 2. The Owner shall, upon request, make all manuals, plans, records, data, procedures and supporting documentation available to Ministry staff.
- 3. The Owner shall prepare and submit a performance report to the District Manager on an annual basis, within ninety (90) days following the end of the period being reported upon. The first such report shall cover the first annual period following the commencement of operation of the Works and subsequent reports shall be submitted to cover successive annual periods following thereafter. The reports shall contain, but shall not be limited to, the following information:
  - a. a description of any operating problems encountered and corrective actions taken;
  - b. a summary of all maintenance carried out on any major structure, equipment, apparatus, mechanism or thing forming part of the Works, including an estimate of the quantity of any materials removed from the Works;
  - c. a summary of any complaints received during the reporting period and any steps taken to address the complaints;
  - d. a summary of all spill or abnormal discharge events; and
  - e. any other information the District Manager requires from time to time.

### 7. SPILL CONTINGENCY PLAN

1. Within six (6) months from the issuance of this Approval, the Owner shall implement a spill contingency plan - that is a set of procedures describing how to mitigate the impacts of a spill within the area serviced by the Works. The Owner shall, upon request, make this plan available to Ministry staff. This plan shall include as a minimum:

Stantec is a global leader in sustainable engineering, architecture, and environmental consulting. The diverse perspectives of our partners and interested parties drive us to think beyond what's previously been done on critical issues like climate change, digital transformation, and future-proofing our cities and infrastructure. We innovate at the intersection of community, creativity, and client relationships to advance communities everywhere, so that together we can redefine what's possible.