

Environmental Noise Control Study

Proposed Residential Building

168 - 174 Murray Street
Ottawa, Ontario

Prepared for Mr. Changwan Yoo

Report PG6243-1 Revision 2 dated August 20, 2024

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1.0 Introduction

Paterson Group (Paterson) was commissioned by Mr. Changwan Yoo to conduct an environmental noise control study for the proposed residential building to be located at 168 – 174 Murray Street, in the City of Ottawa.

The objective of the current study is to:

- Determine the primary noise sources impacting the site and compare the projected sound levels to guidelines set out by the Ministry of Environment and Climate Change (MOECC) and the City of Ottawa.
- Review the projected noise levels and offer recommendations regarding warning classes, construction materials or alternative sound barriers.

The following report has been prepared specifically and solely for the aforementioned project which is described herein. It contains our findings and includes acoustical recommendations pertaining to the design and construction of the subject development as they are understood at the time of writing this report.

This study has been conducted according to City of Ottawa document - Engineering Noise Control Guidelines (ENCG), dated January 2016, and the Ontario Ministry of the Environment Guideline NPC-300.

2.0 Proposed Development

It is understood that the proposed residential building will consist of four (4) storey apartment building and rise approximately 13 metres above grade. One (1) basement level is anticipated at the building, consisting of residential units, and utilities area. A total of 18 residential units are expected at the building. Associated at-grade landscaped areas, walkways and bicycle parking areas. An outdoor living area is also anticipated as part of the proposed residential building consisting of an at-grade rear yard amenity area.

3.0 Methodology and Noise Assessment Criteria

The City of Ottawa outlines three (3) sources of environmental noise that must be analyzed separately:

- Surface Transportation Noise
- Stationary Noise
 - new noise-sensitive development applications (noise receptors) in proximity to existing or approved stationary sources of noise, and
 - new stationary sources of noise (noise generating) in proximity to existing or approved noise-sensitive developments
- Aircraft Noise

Surface Transportation Noise

Surface roadway traffic noise, equivalent to sound level energy L_{eq} , provides a measure of the time varying noise level over a period of time. For roadways, the L_{eq} is commonly calculated on the basis of 16-hour (L_{eq16}) daytime (07:00-23:00) and 8-hour (L_{eq8}) nighttime (23:00-7:00) split to assess its impact on residential, commercial and institutional buildings.

The City of Ottawa's Official Plan dictates that the influence area must contain any of following conditions to classify as a surface transportation noise source for a subject site:

- Within 100 m of the right-of-way of an existing or proposed arterial, collector or major collector road; a light rail transit corridor; bus rapid transit, or transit priority corridor
- Within 250 m of the right-of-way for an existing or proposed highway or secondary rail line
- Within 300 m from the right of way of a proposed or existing rail corridor or a secondary main railway line
- Within 500 m of an existing 400 series provincial highway, freeway or principle main railway line.

The Environmental Noise Guidelines for Stationary and Transportation Sources – NPC-300 outlines the limitations of noise levels in relation to the location of the receptors. These can be found in the following tables:

Table 1 – Noise Level Limit for Outdoor Living Areas	
Time Period	L_{eq} Level (dBA)
Daytime, 7:00-23:00	55
➤ Standard taken from Table 2.2a; Sound Level Limit for Outdoor Living Areas – Road and Rail	

Table 2 – Noise Level Limits for Indoor Living Areas			
Type of Space	Time Period	L_{eq} Level (dBA)	
		Road	Rail
General offices, reception areas, retail stores, etc.	Daytime 7:00-23:00	50	45
Theatres, places of worship, libraries, individual or semi-private offices, conference rooms, reading rooms, etc.	Daytime 7:00-23:00	45	40
Living/dining/den areas of residences , hospitals, nursing/retirement homes, schools, day-care centres	Daytime 7:00-23:00	45	40
Living/dining/den areas of residences , hospitals, nursing/retirement homes etc. (except schools or day-care centres)	Nighttime 23:00-7:00	45	40
Sleeping quarters of hotels/motels	Nighttime 23:00-7:00	45	40
Sleeping quarters of residences , hospitals, nursing/retirement homes, etc.	Nighttime 23:00-7:00	40	35
➤ Standards taken from Table 2.2b, Sound Level Limit for Indoor Living Areas – Road and Rail and Table 2.2c, Supplementary Sound Level Limits for Indoor Spaces – Road and Rail			

Predicted noise levels at the pane of window dictate the action required to achieve recommended noise levels. It is noted in ENCG that the limits outlined in Table 2 are for the noise levels on the interior of the window glass pane. An open window is considered to provide a 10 dBA noise reduction, while a standard closed window is capable to provide a minimum 20 dBA noise reduction. The noise level limits of residential building are 45 dBA daytime and 40 dBA nighttime. Therefore, where noise levels exceed 55 dBA daytime and 50 dBA nighttime, the ventilation for the building should consider the provision for central air conditioning. Where noise levels exceed 65 dBA daytime and 60 dBA nighttime, central air conditioning will be required, and the building components will require higher levels of sound attenuation.

When the noise levels are equal to or less than the specified criteria, no noise attenuation (control) measures are required.

When the exceedance of the recommended noise level limits is between 1 dBA and 5 dBA for outdoor living areas ($55 \text{ dBA} < L_{eq} \leq 60 \text{ dBA}$), the proposed development can be completed with no noise control measures incorporated into the site, but the prospective purchasers / tenants should be made aware by suitable Warning Clauses. When the exceedance of recommended noise level limits is more than 5 dBA for outdoor living areas ($L_{eq} > 60 \text{ dBA}$), noise control measures are required to reduce L_{eq} to below 60 dBA and as close as 55 dBA as it is technically and economically feasible.

Noise attenuation (control) measures include any or all of the following:

- Noise attenuation barrier
- Provisions for the installation of central air conditioning
- Central air conditioning
- Architectural components designed to provide additional acoustic insulation

In addition to the implementation of noise attenuation features, if required, the following Warning Clauses may be recommended to advise the prospective purchasers / tenants of affected units of potential environmental noise problem:

Table 3 – Warning Clauses for Outdoor Living Areas		
Leq (dBA)	Warning Clause	Description
$55 \text{ dBA} < L_{eq(16)} \leq 60 \text{ dBA}$	Warning Clause Type A	"Purchasers/tenants are advised that sound levels due to increasing road traffic (rail traffic) (air traffic) may occasionally interfere with some activities of the dwelling occupants as the sound levels exceed the sound level limits of the Municipality and the Ministry of the Environment."
$60 \text{ dBA} < L_{eq(16)}$	Warning Clause Type B	"Purchasers/tenants are advised that despite the inclusion of noise control features in the development and within the building units, sound levels due to increasing road traffic (rail traffic) (air traffic) may on occasions interfere with some activities of the dwelling occupants as the sound levels exceed the sound level limits of the Municipality and the Ministry of the Environment."
➤ Clauses taken from section C8 Warning Clauses; Environmental Noise Guidelines for Stationary and Transportation Sources - NPC-300		

Table 4 – Warning Clauses for Indoor Living Areas		
Leq (dBA)	Warning Clause	Description
55 dBA < $L_{eq(16)}$ ≤ 65 dBA 50 dBA < $L_{eq(8)}$ ≤ 60 dBA	Warning Clause Type C	"This dwelling unit has been designed with the provision for adding central air conditioning at the occupant's discretion. Installation of central air conditioning by the occupant in low and medium density developments will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the Municipality and the Ministry of the Environment."
65 dBA < $L_{eq(16)}$ 60 dBA < $L_{eq(8)}$	Warning Clause Type D	"This dwelling unit has been supplied with a central air conditioning system which will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the Municipality and the Ministry of the Environment."
➤ Clauses taken from section C8 Warning Clauses; Environmental Noise Guidelines for Stationary and Transportation Sources - NPC-300		

Stationary Noise

Stationary noise sources include sources or facilities that are fixed or mobile and can cause a combination of sound and vibration levels emitted beyond the property line. These sources may include commercial air conditioner units, generators and fans. Facilities that may contribute to stationary noise may include car washes, snow disposal sites, transit stations and manufacturing facilities.

The proposed residential development is not in proximity to any existing or approved stationary sources of noise. Therefore, a stationary noise analysis will not be required with respect to off-site stationary noise sources impacting the proposed development.

Aircraft / Airport Noise

The subject site is not located within the Airport Vicinity Development Zone. Therefore, this project will not require an aircraft/airport noise analysis. No warning clauses regarding aircraft or airport noise will be required.

4.0 Analysis

Surface Transportation Noise

The subject building is bordered to the north by Murray Street followed by commercial buildings and St. Patrick Street, to the east by residential dwellings and commercial buildings followed by Cumberland Street, to the south by commercial buildings followed by Clarence Street and residential dwellings, and to the west by commercial buildings. Murray Street, St. Patrick Street, Cumberland Street, and Clarence Street are identified within the 100 m radius of proposed building.

Based on the City of Ottawa's Official Plan, Schedule E, Murray Street is considered a 2 lane urban arterial road (2-UAU), and St. Patrick Street is also considered a 2 lane urban arterial road (2-UAU). Other roads within the 100 m radius of the proposed development are not classified as either arterial, collector or major collector roads and therefore are not included in this study. The major sources of traffic noise are due to the Murray Street and the St. Patrick Street to the north of the proposed building.

All noise sources are presented in Drawing PG6243-3 - Site Geometry located in Appendix 1.

The noise levels from road traffic are provided by the City of Ottawa, taking into consideration the right-of-way width and the implied roadway classification. It is understood that these values represent the maximum allowable capacity of the proposed roadways. The parameters to be used for sound level predictions can be found below.

Table 5 – Traffic and Road Parameters						
Segment	Roadway Classification	AADT Veh/Day	Speed Limit (km/h)	Day/Night Split %	Medium Truck %	Heavy Truck %
Murray Street	2-UAU	15000	50	92/8	7	5
St. Patrick Street	2-UAU	15000	50	92/8	7	5
➤ Data obtained from the City of Ottawa document ENCG						

Three (3) levels of reception points were selected for this analysis. The following elevations were selected from the heights provided on the survey plan for the subject building.

Table 6 – Elevations of Reception Points			
Floor Number	Elevation at Centre of Window (m)	Floor Use	Daytime / Nighttime Analysis
First Floor	1.5	Living Area/Bedroom	Daytime / Nighttime
Fourth Floor	10.5	Living Area/Bedroom	Daytime / Nighttime
At-Grade Rear Yard	1.5	--	Outdoor Living Area

For this analysis, a reception point was taken at the centre of each floor, at the first floor and top floor. Additionally, a receptor point for the outdoor living area was taken at 1.5 m above the ground surface. Reception points are detailed on Drawing PG6243-2 - Receptor Locations presented in Appendix 1.

All horizontal distances have been measured from the reception point to the edge of the right-of-way. The roadway was analyzed where it intersected the 100 m buffer zone, which is reflected in the local angles described in Paterson Drawings PG6243-3A to 3D - Site Geometry in Appendix 1.

Table 8 - Summary of Reception Points and Geometry, located in Appendix 1, provides a summary of the points of reception and their geometry with respect to the noise sources. The analysis is completed so that no effects of sound reflection off the building facade are considered, as stipulated by the ENG C.

The subject site is levelled and at grade with the neighbouring roads within 100 m radius.

The analysis was completed using STAMSON version 5.04, a computer program which uses the road and rail traffic noise prediction methods using ORNAMENT (Ontario Road Noise Analysis Method for Environment and Transportation) and STEAM (Sound from Trains Environment Analysis Method), publications from the Ontario Ministry of Environment and Energy.

5.0 Results

Surface Transportation Noise

The primary descriptors are the 16-hour daytime (7:00-23:00) and the 8-hour nighttime (23:00-7:00) equivalent sound levels, $L_{eq(16)}$ and $L_{eq(8)}$ for City roads.

The exterior noise levels due to roadway traffic sources were analyzed with the STAMSON version 5.04 software at all reception points. The input and output data of the STAMSON modeling can be found in Appendix 2, and the summary of the results can be found in Table 7.

Table 7: Exterior Noise Levels due to Roadway Traffic Sources				
Reception Point	Height Above Grade (m)	Receptor Location	Daytime $L_{eq(16)}$ (dBA)	Nighttime $L_{eq(8)}$ (dBA)
REC 1-1	1.5	Northern Elevation, 1st Floor	67	59
REC 1-4	10.5	Northern Elevation, 4th Floor	68	60
REC 2-1	1.5	Western Elevation, 1st Floor	59	52
REC 2-4	10.5	Western Elevation, 4th Floor	61	53
REC 3-1	1.5	Eastern Elevation, 1st Floor	59	52
REC 3-4	10.5	Eastern Elevation, 4th Floor	60	53
REC 4	1.5	Rear Yard Amenity Area	49	--

6.0 Discussion and Recommendations

6.1 Outdoor Living Areas

An at-grade rear yard was identified as an Outdoor Living Area (OLA). One (1) receptor point (REC 4) was selected in the centre of rear yard. Two analyses of the rear yard receptor were performed. The first analysis as demonstrated in Drawing 3D was performed taking into consideration “free field sound levels”. The STAMSON analysis indicated the noise level at the rear yard will be 57 dBA during the daytime period (7:00-23:00) which is above the 55 dBA threshold value as specified by the ENCG. Further analysis was performed taking into consideration the building orientation as per Table 2.3a of the City of Ottawa guidelines as demonstrated in Drawing 3E. The STAMSON analysis indicated, the noise level at rear yard will be 49 dBA during the daytime period (7:00-23:00) when taking into consideration the building orientation. This value is below the 55 dBA threshold value specified by the ENCG therefore, no further noise attenuation measures are required.

6.2 Indoor Living Areas and Ventilation

The results of the STAMSON modeling indicate that the noise levels will range between 59 dBA and 68 dBA during the daytime period (07:00-23:00) and between 52 dBA and 60 dBA during the nighttime period (23:00-7:00). The noise levels on the northern, eastern, and western elevations will exceed the limit for the exterior of the pane of glass (55 dBA) specified by the ENCG. It is also noted that the noise levels on the northern elevation will exceed 65 dBA. Therefore, units on the northern, eastern, and western elevations of this building should be supplied with a central air conditioning unit, along with the warning clause Type D.

This building does exceed the 65 dBA threshold for noise on the northern elevation. Therefore, an analysis of the building materials will be required. However, at this time the building materials and exterior wall construction details have not been finalized. Therefore, a review of the proposed building materials on the northern elevation will need to be completed.

Proposed Construction Specifications

It is understood that typical window and wall details are proposed for the residential buildings. The effectiveness of the noise insulation can be expressed as the Acoustical Insulation Factor (AIF), calculated as follows:

$$\text{AIF} = \text{Leq}(16)(\text{Exterior}) - \text{Leq}(16)(\text{Interior}) + 10 \log_{10}(N) + 2 \text{ dBA}$$

Where:

$\text{Leq}(16)(\text{Exterior})$ = Calculated value at the window pane

$\text{Leq}(16)(\text{Interior})$ = 45 dBA

N = number of components in the room

No floor plans or detailed design drawings were provided for this portion of the review. A conservative approach is to assume that there are 2 components per room. Therefore, the AIF would need to be at least 28 dBA.

A conversion from AIF to a Standard Transmission Class (STC) rating will require the knowledge of room dimensions in addition to the wall and window dimensions. However, a conservative approach would be to increase the AIF factor by 3. **Therefore, provided the building materials of either the windows and/or exterior walls have an STC rating of 31 or higher, this would be a sufficient noise attenuation device.**

A review of industry standards for construction material indicates that, as long as the exterior cladding of the northern elevation consist of brick or concrete panels and that all windows consist of double pane glass, these materials have an STC rating of greater than 31 and are considered acceptable. If alternative materials are to be utilized on the northern elevation, then a review will need to be completed once design details are finalized.

7.0 Summary of Findings

The subject site is located at 168 – 174 Murray Street, in the City of Ottawa. It is understood that the proposed building will consist of four (4) storey apartment building and rise approximately 13 metres above grade. There are two major sources of surface transportation noise to the proposed building: Murray Street and St. Patrick Street.

There is an at-grade rear yard that will serve as an Outdoor Living Area (OLA). The results of STAMSON modeling indicate that the noise level at the rear yard is expected to be 57 dBA during the daytime period. Further analysis was performed using mitigation measured provided by the City of Ottawa which reduced the levels to 49 dBA, which is below the 55 dBA threshold value specified by the ENCG. Therefore, no further noise attenuation measures are required.

Several reception points were selected for the surface transportation noise analysis, consisting of the centre of first level and top level. The results of STAMSON modeling indicate that the northern, eastern, and western elevations of the proposed building are expected to exceed the 55 dBA threshold specified by the ENCG. It is also noted that the noise level on the northern elevation will exceed 65 dBA. Therefore, the installation of a central air conditioning unit, along with a warning clause Type D, will be required for the units on the northern, eastern, and western elevations of proposed building. A review of industry standards for construction material indicates that, provided the exterior cladding of the northern elevation consist of brick or concrete panels and that all windows consist of double pane glass, these materials have an STC rating of greater than 31 and are considered acceptable.

The following warning clause is to be included on all Offers of Purchase and Sale and/or lease agreements:

"This dwelling unit has been supplied with a central air conditioning system which will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the Municipality and the Ministry of the Environment."

8.0 Statement of Limitations

The recommendations made in this report are in accordance with our present understanding of the project. Our recommendations should be reviewed when the project drawings and specifications are complete.

The present report applies only to the project described in this document. Use of this report for purposes other than those described herein or by person(s) other than Mr. Changwan Yoo or his agent(s) is not authorized without review by this firm for the applicability of our recommendations to the altered use of the report.

Paterson Group Inc.



Otilia McLaughlin B.Eng.



Stephanie A. Boisvenue, P.Eng.

Report Distribution:

- ☐ Mr. Changwan Yoo (email copy)
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APPENDIX 1

TABLE 8 - SUMMARY OF RECEPTION POINTS AND GEOMETRY

DRAWING PG6243-1 - SITE PLAN

DRAWING PG6243-2 - RECEPTOR LOCATION PLAN

DRAWING PG6243-3 - SITE GEOMETRY

DRAWING PG6243-3A - SITE GEOMETRY (REC 1-1 and REC 1-4)

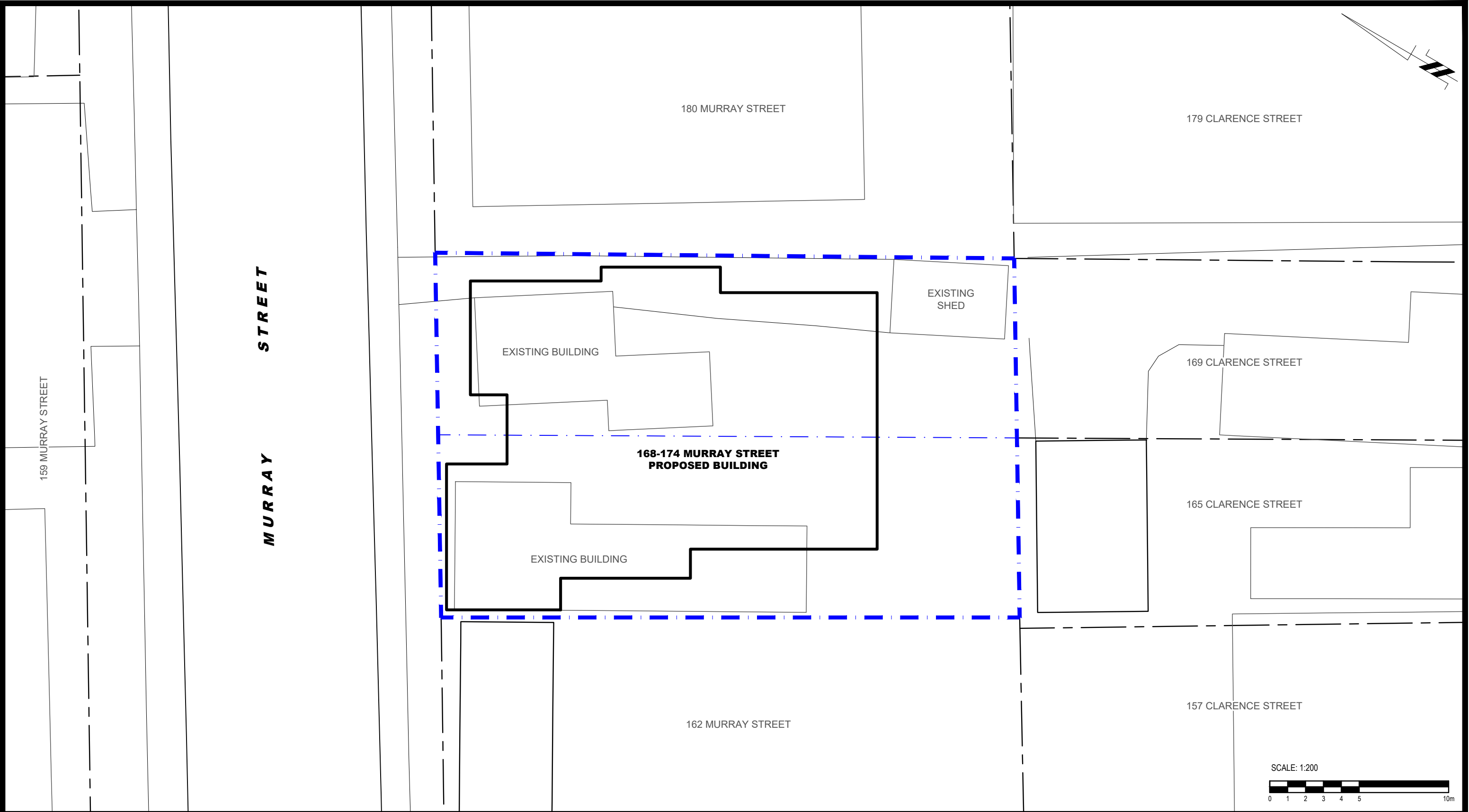
DRAWING PG6243-3B - SITE GEOMETRY (REC 2-1 and REC 2-4)

DRAWING PG6243-3C - SITE GEOMETRY (REC 3-1 and REC 3-4)

DRAWING PG6243-3D - SITE GEOMETRY (REC 4V1)

DRAWING PG6243-3E – SITE GEOMETRY (REC 4V2)

Table 8 Revision 2 - Summary of Reception Points and Geometry 168 - 174 Murray Street															
Point of Reception	Location	Leq Day (dBA)	Leq Night (dBA)	Murray Street						St. Patrick Street					
				Horizontal (m)	Vertical (m)	Total (m)	Local Angle (degree)	Number of Rows of Houses	Density (%)	Horizontal (m)	Vertical (m)	Total (m)	Local Angle (degree)	Number of Rows of Houses	Density (%)
REC 1-1	Northern Elevation, 1st Floor	67	59	15	1.5	15.1	-89, 86	n/a	n/a	85	1.5	85.0	-37, 35	2	40
REC 1-4	Northern Elevation, 4th Floor	68	60	15	10.5	18.3	-89, 86	n/a	n/a	85	10.5	85.7	-37, 35	2	40
REC 2-1	Western Elevation, 1st Floor	59	52	25	1.5	25.0	-82, 0	1	20	95	1.5	95.0	-31, 0	2	40
REC 2-4	Western Elevation, 4th Floor	61	53	25	10.5	27.1	-82, 0	1	20	95	10.5	95.6	-31, 0	2	40
REC 3-1	Eastern Elevation, 1st Floor	59	52	25	1.5	25.0	0, 79	1	20	95	1.5	95.0	0, 27	2	40
REC 3-4	Eastern Elevation, 4th Floor	60	53	25	10.5	27.1	0, 79	1	20	95	10.5	95.6	0, 27	2	40
REC 4	Rear Yard Amenity Area	49		15	4.5	15.7	-18, 27	n/a	n/a	90	4.5	90.1	-18, 27	2	40





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1	UPDATED BUILDING LAYOUT	18/09/2023	YT
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MR. CHANGWAN YOO
NOISE ATTENUATION STUDY
PROPOSED RESIDENTIAL DEVELOPMENT
168-174 MURRAY STREET

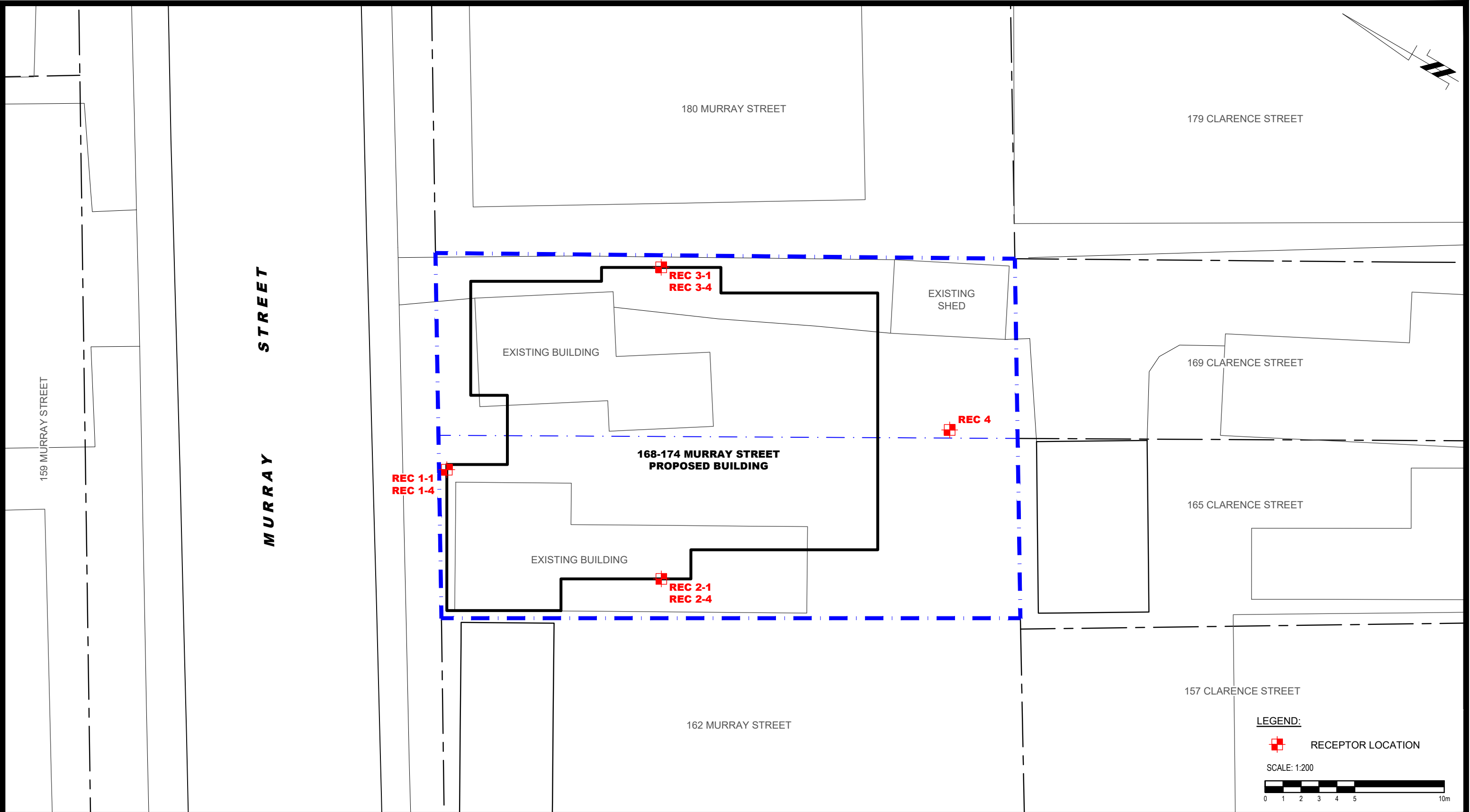
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SITE PLAN

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Approved by:	SB	Revision No.:	1

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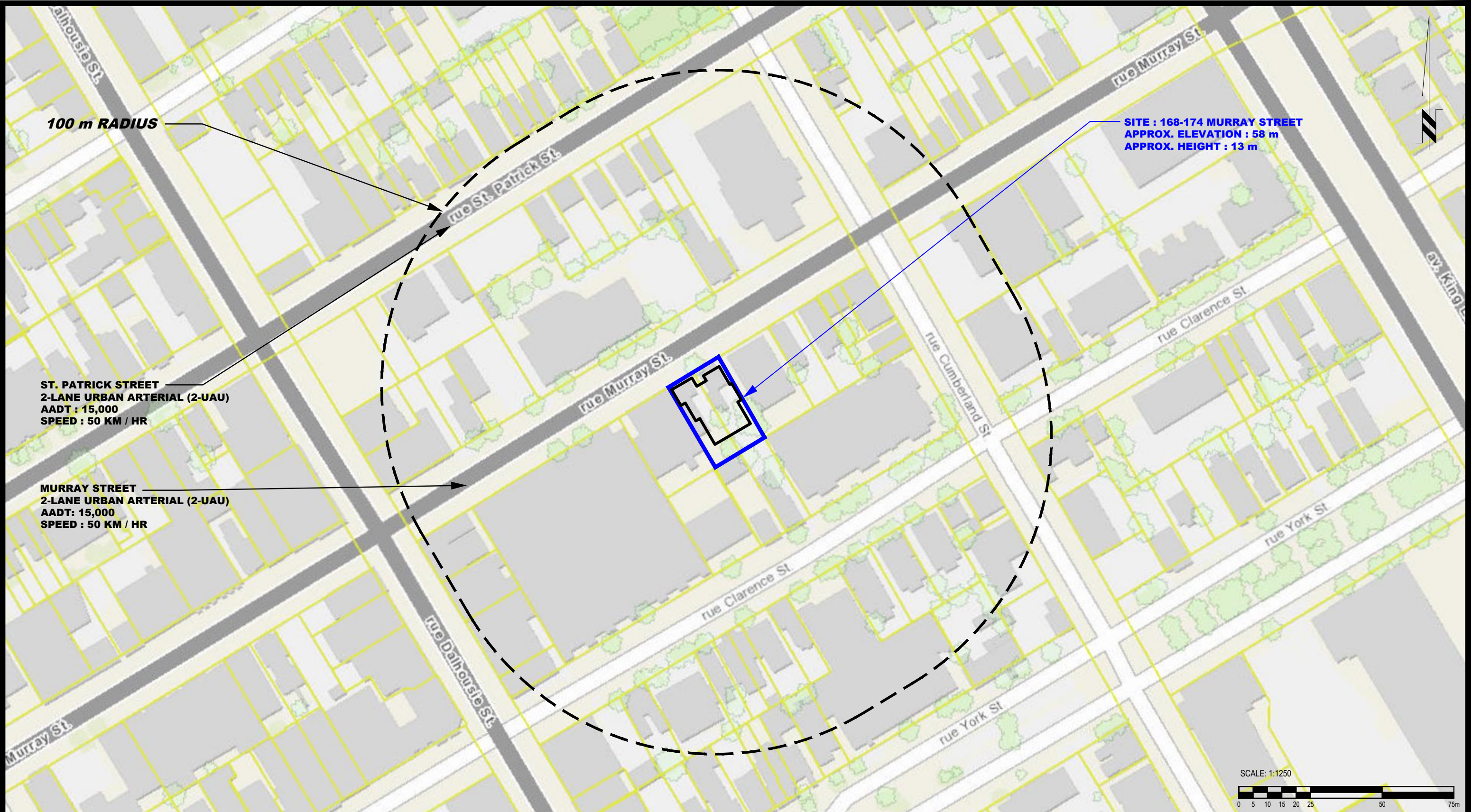
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168-174 MURRAY STREET

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RECEPTOR LOCATION PLAN

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Approved by:	SB	Revision No.:	1

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PROPOSED RESIDENTIAL DEVELOPMENT
168-174 MURRAY STREET

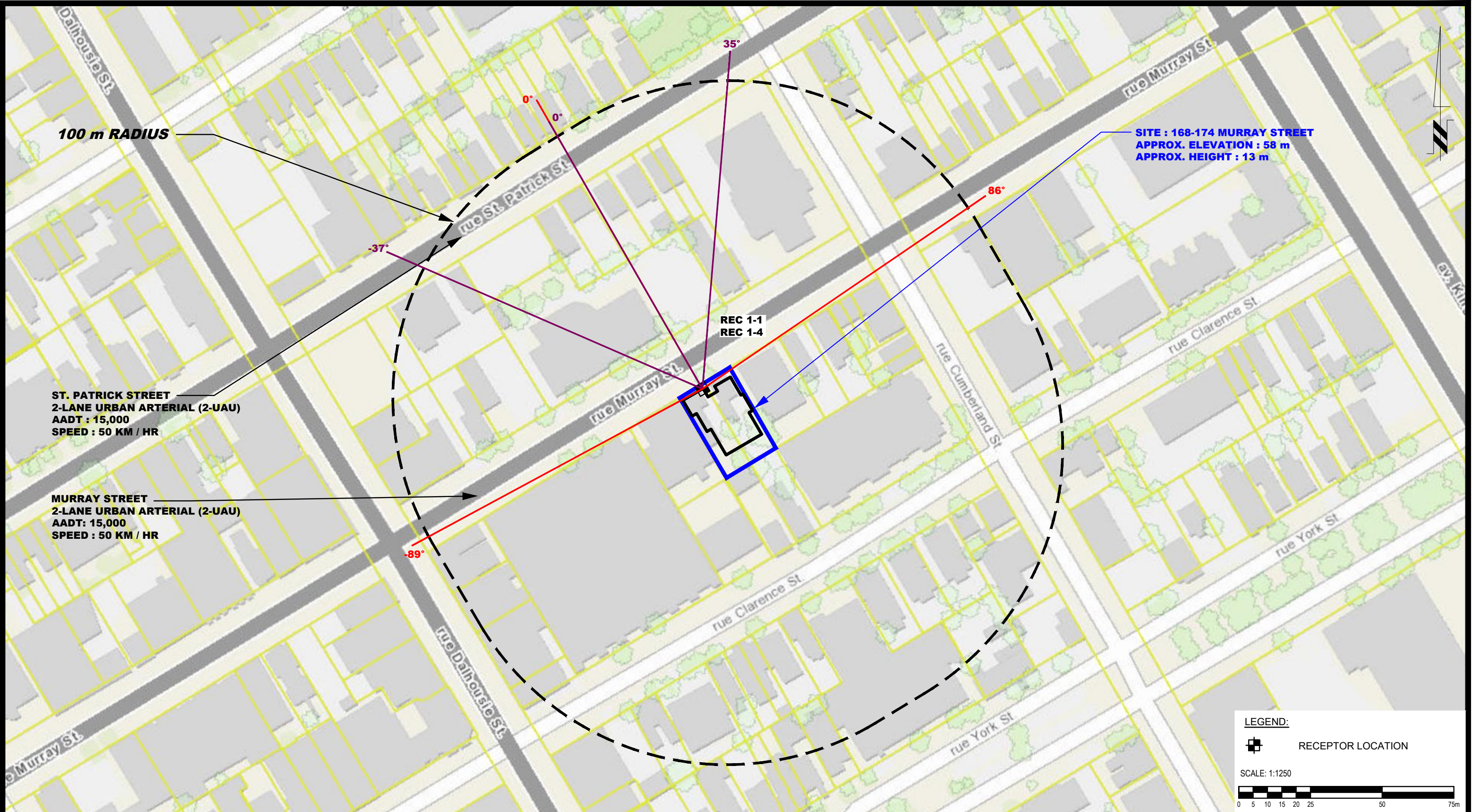
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SITE GEOMETRY

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Approved by: SB

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Revision No.: 1

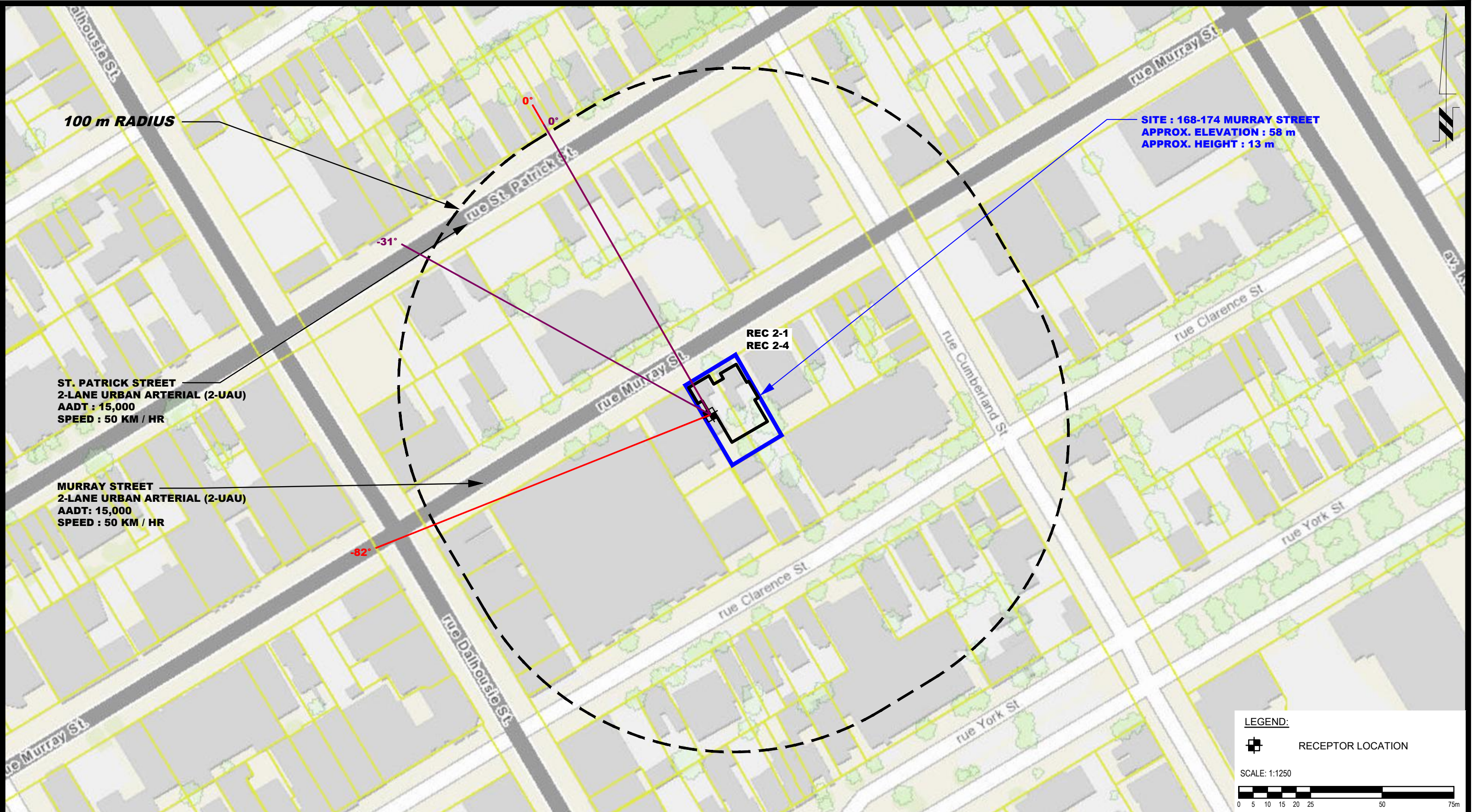
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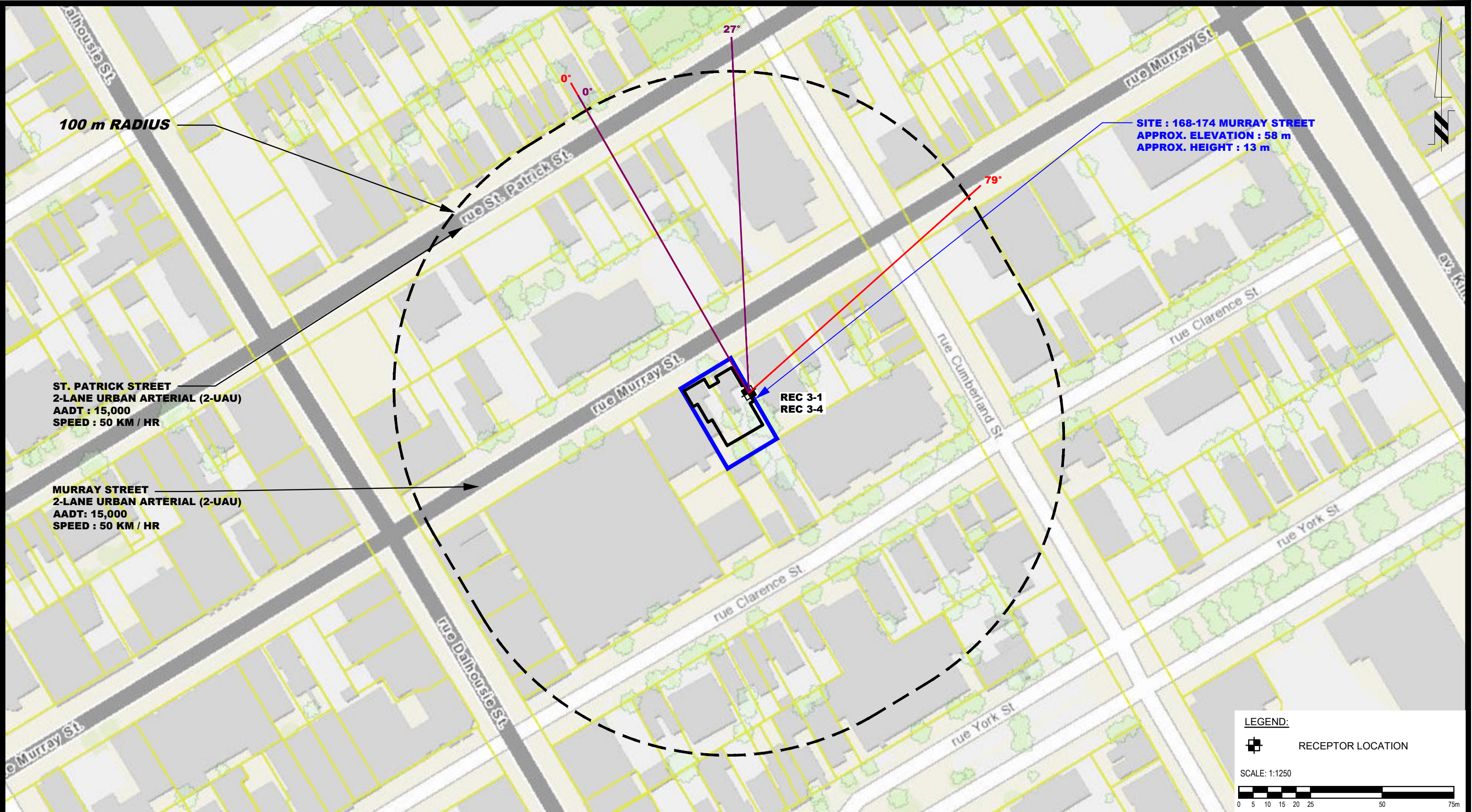
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SITE GEOMETRY - REC 2-1 AND REC 2-4

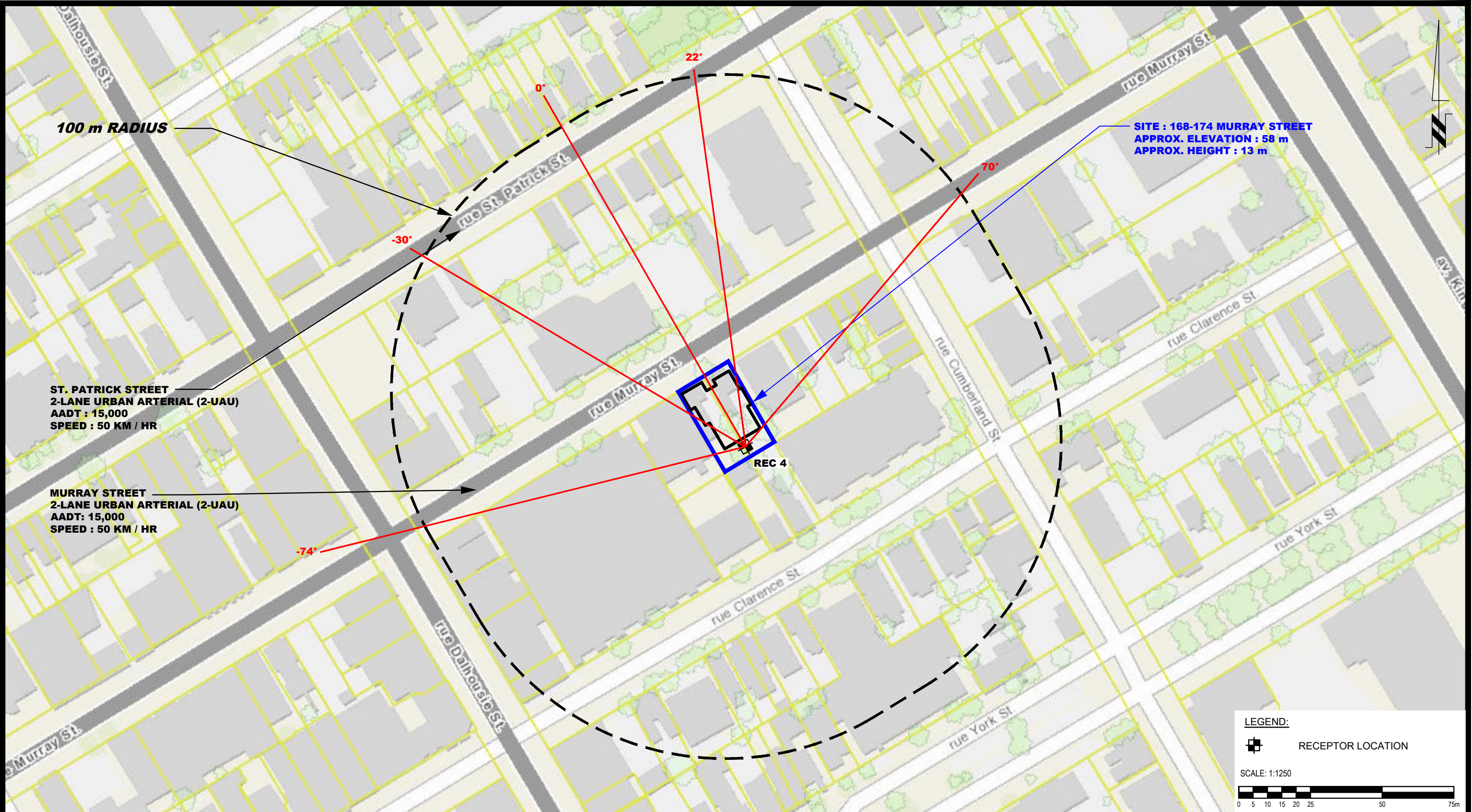
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Approved by:	SB	Revision No.:	1

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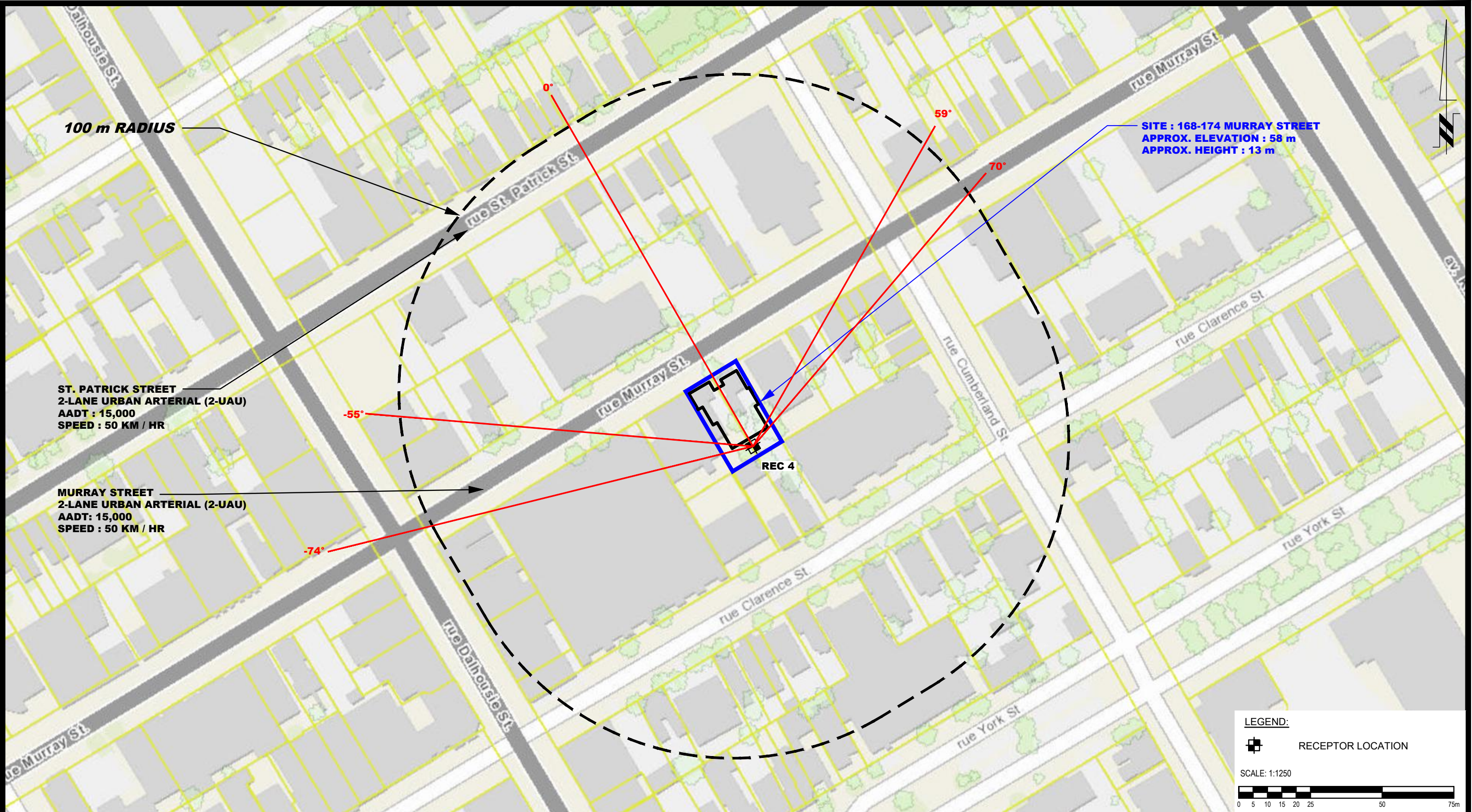
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SITE GEOMETRY - REC 4V1

Scale:	1:1250	Date:	04/2022
Drawn by:	YA	Report No.:	PG6243-1
Checked by:	YT	Dwg. No.:	PG6243-3D
Approved by:	SB	Revision No.:	1

p:\autocad\drawings\geotechnical\pg6243\pg6243-3-site geometry (rev.01).dwg





**PATERSON
GROUP**

9 AURIGA DRIVE
OTTAWA, ON
K2E 7T9
TEL: (613) 226-7381

1	UPDATED BUILDING LAYOUT	18/09/2023	YT
NO.	REVISIONS	DATE	INITIAL

MR. CHANGWAN YOO
NOISE ATTENUATION STUDY
PROPOSED RESIDENTIAL DEVELOPMENT
168-174 MURRAY STREET

OTTAWA,
Title: **SITE GEOMETRY - REC 4V2**ONTARIO

Scale:	1:1250	Date:	04/2022
Drawn by:	YA	Report No.:	PG6243-1
Checked by:	YT	Dwg. No.:	PG6243-3E
Approved by:	SB	Revision No.:	1

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APPENDIX 2

STAMSON RESULTS

STAMSON 5.0 NORMAL REPORT Date: 04-05-2022 11:26:11
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: rec11.te Time Period: Day/Night 16/8 hours
Description: Receptor Point 1-1

Road data, segment # 1: Murray St (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Murray St (day/night)

Angle1 Angle2 : -89.00 deg 86.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 15.00 / 15.00 m
Receiver height : 1.50 / 1.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 2: StPatrick St (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00

Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: StPatrick St (day/night)

 Angle1 Angle2 : -37.00 deg 35.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 2 / 2
 House density : 40 %
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 85.00 / 85.00 m
 Receiver height : 1.50 / 1.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00

↑

Results segment # 1: Murray St (day)

 Source height = 1.50 m

ROAD (0.00 + 67.01 + 0.00) = 67.01 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-89	86	0.66	68.48	0.00	0.00	-1.47	0.00	0.00	0.00	67.01

Segment Leq : 67.01 dBA

↑

Results segment # 2: StPatrick St (day)

 Source height = 1.50 m

ROAD (0.00 + 48.30 + 0.00) = 48.30 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-37	35	0.66	68.48	0.00	-12.51	-4.17	0.00	-3.50	0.00	48.30

Segment Leq : 48.30 dBA

Total Leq All Segments: 67.07 dBA

↑

Results segment # 1: Murray St (night)

Source height = 1.50 m

ROAD (0.00 + 59.41 + 0.00) = 59.41 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-89	86	0.66	60.88	0.00	0.00	-1.47	0.00	0.00	0.00	59.41

Segment Leq : 59.41 dBA

↑

Results segment # 2: StPatrick St (night)

Source height = 1.50 m

ROAD (0.00 + 40.71 + 0.00) = 40.71 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-37	35	0.66	60.88	0.00	-12.51	-4.17	0.00	-3.50	0.00	40.71

Segment Leq : 40.71 dBA

Total Leq All Segments: 59.47 dBA

↑

TOTAL Leq FROM ALL SOURCES (DAY): 67.07
(NIGHT): 59.47

↑

↑

Filename: rec14.te Time Period: Day/Night 16/8 hours
Description: Receptor Point 1-4

Road data, segment # 1: Murray St (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Murray St (day/night)

Angle1 Angle2 : -89.00 deg 86.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 15.00 / 15.00 m
Receiver height : 10.50 / 10.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 2: StPatrick St (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00

Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: StPatrick St (day/night)

 Angle1 Angle2 : -37.00 deg 35.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 2 / 2
 House density : 40 %
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 85.00 / 85.00 m
 Receiver height : 10.50 / 10.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00



Results segment # 1: Murray St (day)

 Source height = 1.50 m

ROAD (0.00 + 67.48 + 0.00) = 67.48 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-89	86	0.39	68.48	0.00	0.00	-1.00	0.00	0.00	0.00	67.48

Segment Leq : 67.48 dBA



Results segment # 2: StPatrick St (day)

 Source height = 1.50 m

ROAD (0.00 + 50.41 + 0.00) = 50.41 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-37	35	0.39	68.48	0.00	-10.47	-4.09	0.00	-3.50	0.00	50.41

Segment Leq : 50.41 dBA

Total Leq All Segments: 67.56 dBA



Results segment # 1: Murray St (night)

Source height = 1.50 m

ROAD (0.00 + 59.89 + 0.00) = 59.89 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-89	86	0.39	60.88	0.00	0.00	-1.00	0.00	0.00	0.00	59.89

Segment Leq : 59.89 dBA

↑

Results segment # 2: StPatrick St (night)

Source height = 1.50 m

ROAD (0.00 + 42.82 + 0.00) = 42.82 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-37	35	0.39	60.88	0.00	-10.47	-4.09	0.00	-3.50	0.00	42.82

Segment Leq : 42.82 dBA

Total Leq All Segments: 59.97 dBA

↑

TOTAL Leq FROM ALL SOURCES (DAY): 67.56

(NIGHT): 59.97

↑

↑

Filename: rec21.te Time Period: Day/Night 16/8 hours
Description: Receptor Point 2-1

Road data, segment # 1: Murray St (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Murray St (day/night)

Angle1 Angle2 : -82.00 deg 0.00 deg
Wood depth : 0 (No woods.)
No of house rows : 1 / 1
House density : 20 %
Surface : 1 (Absorptive ground surface)
Receiver source distance : 25.00 / 25.00 m
Receiver height : 1.50 / 1.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 2: StPatrick St (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000

Percentage of Annual Growth : 0.00
 Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: StPatrick St (day/night)

 Angle1 Angle2 : -31.00 deg 0.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 2 / 2
 House density : 40 %
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 95.00 / 95.00 m
 Receiver height : 1.50 / 1.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00

↑

Results segment # 1: Murray St (day)

 Source height = 1.50 m

ROAD (0.00 + 59.34 + 0.00) = 59.34 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-82	0	0.66	68.48	0.00	-3.68	-4.56	0.00	-0.90	0.00	59.34

Segment Leq : 59.34 dBA

↑

Results segment # 2: StPatrick St (day)

 Source height = 1.50 m

ROAD (0.00 + 43.89 + 0.00) = 43.89 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-31	0	0.66	68.48	0.00	-13.31	-7.78	0.00	-3.50	0.00	43.89

Segment Leq : 43.89 dBA

Total Leq All Segments: 59.46 dBA

↑

Results segment # 1: Murray St (night)

$$\text{ROAD } (0.00 + 51.74 + 0.00) = 51.74 \text{ dBA}$$

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-82	0	0.66	60.88	0.00	-3.68	-4.56	0.00	-0.90	0.00	51.74

Segment Leq : 51.74 dBA

Results segment # 2: StPatrick St (night)

Source height = 1.50 m

$$\text{ROAD } (0.00 + 36.29 + 0.00) = 36.29 \text{ dBA}$$

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-31	0	0.66	60.88	0.00	-13.31	-7.78	0.00	-3.50	0.00	36.29

Segment Leq : 36.29 dBA

Total Leq All Segments: 51.86 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 59.46
(NIGHT): 51.86

↑

↑

Filename: rec24.te Time Period: Day/Night 16/8 hours
Description: Receptor Point 2-4

Road data, segment # 1: Murray St (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Murray St (day/night)

Angle1 Angle2 : -82.00 deg 0.00 deg
Wood depth : 0 (No woods.)
No of house rows : 1 / 1
House density : 20 %
Surface : 1 (Absorptive ground surface)
Receiver source distance : 25.00 / 25.00 m
Receiver height : 10.50 / 10.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 2: StPatrick St (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000

Percentage of Annual Growth : 0.00
 Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: StPatrick St (day/night)

 Angle1 Angle2 : -31.00 deg 0.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 2 / 2
 House density : 40 %
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 95.00 / 95.00 m
 Receiver height : 10.50 / 10.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00

↑

Results segment # 1: Murray St (day)

 Source height = 1.50 m

ROAD (0.00 + 60.36 + 0.00) = 60.36 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-82	0	0.39	68.48	0.00	-3.08	-4.14	0.00	-0.90	0.00	60.36

Segment Leq : 60.36 dBA

↑

Results segment # 2: StPatrick St (day)

 Source height = 1.50 m

ROAD (0.00 + 46.11 + 0.00) = 46.11 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-31	0	0.39	68.48	0.00	-11.14	-7.72	0.00	-3.50	0.00	46.11

Segment Leq : 46.11 dBA

Total Leq All Segments: 60.52 dBA

↑

Results segment # 1: Murray St (night)

$$\text{ROAD } (0.00 + 52.76 + 0.00) = 52.76 \text{ dBA}$$

Segment Leq : 52.76 dBA

Source height = 1.50 m

$$\text{ROAD } (0.00 + 38.52 + 0.00) = 38.52 \text{ dBA}$$

Segment Leq : 38.52 dBA

STAMSON 5.0 NORMAL REPORT Date: 04-05-2022 11:44:30
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: rec31.te Time Period: Day/Night 16/8 hours
Description: Receptor Point 3-1

Road data, segment # 1: Murray St (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Murray St (day/night)

Angle1 Angle2 : 0.00 deg 79.00 deg
Wood depth : 0 (No woods.)
No of house rows : 1 / 1
House density : 20 %
Surface : 1 (Absorptive ground surface)
Receiver source distance : 25.00 / 25.00 m
Receiver height : 1.50 / 1.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 2: StPatrick St (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000

Percentage of Annual Growth : 0.00
 Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: StPatrick St (day/night)

 Angle1 Angle2 : 0.00 deg 27.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 2 / 2
 House density : 40 %
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 95.00 / 95.00 m
 Receiver height : 1.50 / 1.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00

↑

Results segment # 1: Murray St (day)

 Source height = 1.50 m

ROAD (0.00 + 59.28 + 0.00) = 59.28 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	79	0.66	68.48	0.00	-3.68	-4.62	0.00	-0.90	0.00	59.28

 Segment Leq : 59.28 dBA

↑

Results segment # 2: StPatrick St (day)

 Source height = 1.50 m

ROAD (0.00 + 43.33 + 0.00) = 43.33 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	27	0.66	68.48	0.00	-13.31	-8.35	0.00	-3.50	0.00	43.33

 Segment Leq : 43.33 dBA

Total Leq All Segments: 59.39 dBA

↑

Results segment # 1: Murray St (night)

$$\text{ROAD } (0.00 + 51.68 + 0.00) = 51.68 \text{ dBA}$$

Segment Leq : 51.68 dBA

Source height = 1.50 m

$$\text{ROAD } (0.00 + 35.73 + 0.00) = 35.73 \text{ dBA}$$

Segment Leq : 35.73 dBA

Filename: rec34.te Time Period: Day/Night 16/8 hours
Description: Receptor Point 3-4

Road data, segment # 1: Murray St (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Murray St (day/night)

Angle1 Angle2 : 0.00 deg 79.00 deg
Wood depth : 0 (No woods.)
No of house rows : 1 / 1
House density : 20 %
Surface : 1 (Absorptive ground surface)
Receiver source distance : 25.00 / 25.00 m
Receiver height : 10.50 / 10.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 2: StPatrick St (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000

Percentage of Annual Growth : 0.00
 Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: StPatrick St (day/night)

 Angle1 Angle2 : 0.00 deg 27.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 2 / 2
 House density : 40 %
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 95.00 / 95.00 m
 Receiver height : 10.50 / 10.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00

↑

Results segment # 1: Murray St (day)

 Source height = 1.50 m

ROAD (0.00 + 60.27 + 0.00) = 60.27 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	79	0.39	68.48	0.00	-3.08	-4.23	0.00	-0.90	0.00	60.27

Segment Leq : 60.27 dBA

↑

Results segment # 2: StPatrick St (day)

 Source height = 1.50 m

ROAD (0.00 + 45.53 + 0.00) = 45.53 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	27	0.39	68.48	0.00	-11.14	-8.30	0.00	-3.50	0.00	45.53

Segment Leq : 45.53 dBA

Total Leq All Segments: 60.41 dBA

↑

Results segment # 1: Murray St (night)

$$\text{ROAD } (0.00 + 52.67 + 0.00) = 52.67 \text{ dBA}$$

Segment Leq : 52.67 dBA

Source height = 1.50 m

$$\text{ROAD } (0.00 + 37.94 + 0.00) = 37.94 \text{ dBA}$$

Segment Leq : 37.94 dBA

Total Leq All Segments: 52.81 dBA

↑
↑

STAMSON 5.0 NORMAL REPORT Date: 05-06-2024 13:10:20
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: REC4.te Time Period: Day/Night 16/8 hours
Description: REC 4 - Outdoor Living Area - " Free Field "

Road data, segment # 1: Murray St (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Murray St (day/night)

Angle1 Angle2 : -74.00 deg 70.00 deg
Wood depth : 0 (No woods.)
No of house rows : 1 / 1
House density : 60 %
Surface : 1 (Absorptive ground surface)
Receiver source distance : 35.00 / 35.00 m
Receiver height : 1.50 / 1.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 2: St Pat St (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000

Percentage of Annual Growth : 0.00
 Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: St Pat St (day/night)

 Angle1 Angle2 : -30.00 deg 22.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 1 / 1
 House density : 60 %
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 117.00 / 117.00 m
 Receiver height : 1.50 / 1.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00

↑

Results segment # 1: Murray St (day)

 Source height = 1.50 m

ROAD (0.00 + 56.88 + 0.00) = 56.88 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-74	70	0.66	68.48	0.00	-6.11	-1.81	0.00	-3.68	0.00	56.88

 Segment Leq : 56.88 dBA

↑

Results segment # 2: St Pat St (day)

 Source height = 1.50 m

ROAD (0.00 + 44.76 + 0.00) = 44.76 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-30	22	0.66	68.48	0.00	-14.81	-5.50	0.00	-3.41	0.00	44.76

 Segment Leq : 44.76 dBA

Total Leq All Segments: 57.14 dBA

↑

Results segment # 1: Murray St (night)

Source height = 1.50 m

ROAD (0.00 + 49.28 + 0.00) = 49.28 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-74	70	0.66	60.88	0.00	-6.11	-1.81	0.00	-3.68	0.00	49.28

Segment Leq : 49.28 dBA

↑

Results segment # 2: St Pat St (night)

Source height = 1.50 m

ROAD (0.00 + 37.17 + 0.00) = 37.17 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-30	22	0.66	60.88	0.00	-14.81	-5.50	0.00	-3.41	0.00	37.17

Segment Leq : 37.17 dBA

Total Leq All Segments: 49.54 dBA

↑

TOTAL Leq FROM ALL SOURCES (DAY): 57.14
(NIGHT): 49.54

↑

↑

STAMSON 5.0 NORMAL REPORT Date: 19-09-2023 14:47:46
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: rec4.te Time Period: Day/Night 16/8 hours
Description: Receptor Point 4

Road data, segment # 1: Murray St A (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Murray St A (day/night)

Angle1 Angle2 : -76.00 deg -55.00 deg
Wood depth : 0 (No woods.)
No of house rows : 1 / 1
House density : 60 %
Surface : 1 (Absorptive ground surface)
Receiver source distance : 35.00 / 35.00 m
Receiver height : 1.50 / 1.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 2: Murray St B (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000

Percentage of Annual Growth : 0.00
 Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: Murray St B (day/night)

 Angle1 Angle2 : 59.00 deg 73.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 1 / 1
 House density : 60 %
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 35.00 / 35.00 m
 Receiver height : 1.50 / 1.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00

↑

Results segment # 1: Murray St A (day)

 Source height = 1.50 m

ROAD (0.00 + 46.79 + 0.00) = 46.79 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-76	-55	0.66	68.48	0.00	-6.11	-11.90	0.00	-3.68	0.00	46.79

Segment Leq : 46.79 dBA

↑

Results segment # 2: Murray St B (day)

 Source height = 1.50 m

ROAD (0.00 + 45.00 + 0.00) = 45.00 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
59	73	0.66	68.48	0.00	-6.11	-13.69	0.00	-3.68	0.00	45.00

Segment Leq : 45.00 dBA

Total Leq All Segments: 49.00 dBA

↑

Results segment # 1: Murray St A (night)

$$\text{ROAD } (0.00 + 39.19 + 0.00) = 39.19 \text{ dBA}$$

Segment Leq : 39.19 dBA

Source height = 1.50 m

$$\text{ROAD } (0.00 + 37.40 + 0.00) = 37.40 \text{ dBA}$$

Segment Leq : 37.40 dBA

Total Leq All Segments: 41.40 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 49.00
(NIGHT): 41.40

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