



**Geotechnical Investigation  
Proposed Addition to Residential Building  
68 Sweetland Avenue  
Ottawa, Ontario**

**Client:**

Smart Living Properties  
226 Argyle Avenue  
Ottawa, Ontario K2P 1B9

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**Prepared By:**

Matthew Zammit, M.A.Sc., P.Eng.  
Geotechnical Engineer  
Geotechnical Services  
Earth and Environment

**Reviewed / Approved By:**

Susan M. Potyondy P.Eng.  
Senior Project Manager  
Geotechnical Services  
Earth and Environment

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## Executive Summary

EXP Services Inc. (EXP) is pleased to present the results of the geotechnical investigation completed for the proposed addition to the existing residential building at the address of 68 Sweetland Avenue, Ottawa, Ontario (Figure 1). Terms and conditions of this assignment were outlined in EXP's proposal number: OTT-22005690-A0 dated February 28, 2022. Authorization to proceed with this investigation was provided by Smart Living Properties via the EXP work authorization signed April 22, 2022. In conjunction with this geotechnical investigation, EXP completed a Phase One Environmental Site Assessment of the property and the results are reported under separate cover.

The grading, drainage, erosion and sediment control plan, Drawing No. C101, dated January 20, 2023 (Revision No. 1) and prepared by McIntosh Perry (MP), indicates the residential building addition will be an approximate 8.9 m by 15.8 m rectangular shaped structure extending westward from the west exterior wall of the existing building at 68 Sweetland Avenue. The proposed addition will have a basement. The elevation of the underside of footing will be at a design elevation of Elevation 65.79 m and the site grade raise will be a maximum of 0.4 m. The building section drawing, Drawing No. A112, dated May 16, 2022 and prepared by Woodman and Architect (Woodman) indicates the design elevation of the basement floor slab will be at Elevation 66.09 m and similar to the MP plan, the design elevation of the underside of the footings will be at Elevation 65.79 m.

This executive summary provides a synopsis of the findings from the geotechnical investigation and provides geotechnical engineering comments and recommendations for the proposed addition to the residential building.

The geotechnical investigation for this project consists of two (2) boreholes (Borehole Nos. 1 and 2) drilled to termination and cone refusal depths of 6.7 m and 15.8 m respectively. A monitoring well was installed in Borehole No. 2 for the purpose of monitoring the groundwater level over time.

The borehole information indicates the subsurface conditions consist of fill to a 1.4 m depth (Elevation 67.0 m) underlain by firm to hard native clay and clayey silt to a 13.7 m depth (Elevation 54.7 m) followed by compact glacial till. Boulders or bedrock are inferred at a 15.8 m depth (Elevation 52.6 m). The groundwater level is at a 5.4 m depth (Elevation 63.0 m).

Based on the borehole information and Table 4.1.8.4.A of the 2012 Ontario Building Code (OBC) as amended May 2, 2019, the site classification for seismic site response is estimated to be **Class D**. The subsurface soils are not susceptible to liquefaction during a seismic event. A higher site class may be obtained by conducting a shear wave velocity soundings survey of the site.

The grading, drainage, erosion and sediment control plan, Drawing No. C101, dated January 20, 2023 (Revision No. 1) and prepared by McIntosh Perry (MP), indicates the site grade raise will be a maximum of 0.4 m. Based on the borehole information, a maximum site grade raise of 0.5 m is considered acceptable. Therefore, a review of the grading of the site shown in the above referenced MP drawing is considered to be in general conformance with the recommendations of this geotechnical report.

Based on a review of the borehole information, it is considered feasible to support the proposed building addition by strip and spread footings founded at a maximum founding depth of 2.6 m below existing grade at the underside of footing design elevation of Elevation 65.79 m on the native clay. The existing fill is not considered suitable to support the footings for the proposed building addition. For strip footings having a maximum width of 1.0 m and square pad footings having a maximum width and length of 3.0 m founded on the native clay at a maximum depth

of 2.6 m below existing grade (Elevation 65.79 m), the footings may be designed for a bearing pressure at serviceability limit state (SLS) of 150 kPa and factored geotechnical resistance at ultimate limit state (ULS) of 225 kPa. The factored ULS value includes a geotechnical resistance factor of 0.5. The recommended SLS and factored ULS values are valid for the maximum footing founding depth of 2.6 m below existing grade on the native clay and for a maximum site grade raise of 0.5 m. Should the footings extend to greater depths below the maximum depth of 2.6 m below existing grade, EXP should be contacted to review and provide updated SLS and factored ULS values for the footings. The total and differential settlements of footings designed in accordance with the recommendations of this report and with careful attention to construction detail are expected to be less than 25 mm and 19 mm respectively.

To minimize the need to underpin the existing footings along the west wall of the existing building where the proposed new building addition will be located, it is recommended that the basement floor slab and footings for the new building addition be placed at the same depth as the existing lowest floor slab and the existing footings. This is valid for the footings, provided the native clay exposed at the same level as the bottom of the existing footings is capable of supporting the bearing pressure at serviceability limit state (SLS) and factored geotechnical resistance at ultimate limit state (ULS) recommended above for the footings.

A minimum of 1.5 m of earth cover should be provided to the exterior foundations of heated structures to protect them from damage due to frost penetration. The frost cover should be increased to 2.1 m for unheated structures if snow will not be removed from their vicinity and to 2.4 m if snow will be removed from the vicinity of the structure. When earth cover is less than the minimum required, an equivalent thermal combination of earth cover and rigid insulation or rigid insulation alone should be provided. EXP can provide additional comments in this regard, if required.

The basement floor may be designed as a slab-on-grade set on the native clay or on a minimum 300 mm thick engineered fill pad placed on the native clay and should consist of Ontario Provincial Standard Specification (OPSS) Granular B Type II compacted to 98 percent standard Proctor maximum dry density (SPMDD). The existing fill is not considered suitable to support the slab-on-grade and should be excavated and removed down to the native clay from within the floor slab footprint. The floor slab should be set on a bed of well-packed 19 mm clear stone at least 200 mm thick placed on the engineered fill pad or native clay. The clear stone would prevent the capillary rise of moisture from the sub-soil to the floor slab. Adequate saw cuts should be provided in the floor slab to control cracking.

A perimeter drainage system should be installed around the proposed new building addition. If the perimeter drainage system of the existing building is encountered during the construction of the new building addition, it should be reinstated following construction of the new building addition. An underfloor drainage system is not required for the proposed building addition.

The subsurface basement walls of the building should be backfilled with free draining material, such as OPSS Granular B Type II compacted to 95 percent SPMDD and equipped with a perimeter drainage system to prevent the buildup of hydrostatic pressure behind the walls. The walls should be designed to resist lateral earth pressure (force) for the static and seismic conditions.

The excavations may be undertaken by conventional excavation and shall be completed in accordance with the Occupational Health and Safety Act (OHSA), Ontario Reg. 213/91. Based on the definitions provided in OHSA, the subsurface soils on site are considered to be Type 3 and for open cut excavations, the side slopes of the excavation

must be cut back at 1H:1V from the bottom of the excavation. If side slopes noted above cannot be achieved due to space restrictions on site, such as the proximity of open cut excavations to the property limits, existing infrastructure or to foundations of adjacent existing buildings, the excavation for the new building addition construction would have to be undertaken within the confines of an engineered support system (shoring system).

Seepage of the surface and subsurface water into the excavations above the groundwater level is anticipated and it should be possible to collect water entering the excavations at low points and to remove it by conventional pumping techniques.

It is anticipated that the majority of the material required for engineered fill and for backfilling purposes for this project would have to be imported and should preferably conform to the specifications provided in the attached report.

The above and other related considerations are discussed in greater detail in the attached report.

## 1. Introduction

EXP Services Inc. (EXP) is pleased to present the results of the geotechnical investigation completed for the proposed addition to the existing residential building at the address of 68 Sweetland Avenue, Ottawa, Ontario (Figure 1). Terms and conditions of this assignment were outlined in EXP's proposal number: OTT-22005690-A0 dated February 28, 2022. Authorization to proceed with this investigation was provided by Smart Living Properties via the EXP work authorization signed April 22, 2022. In conjunction with this geotechnical investigation, EXP completed a Phase One Environmental Site Assessment of the property and the results are reported under separate cover.

The grading, drainage, erosion and sediment control plan, Drawing No. C101, dated January 20, 2023 (Revision No. 1) and prepared by McIntosh Perry (MP), indicates the residential building addition will be an approximate 8.9 m by 15.8 m rectangular shaped structure extending westward from the west exterior wall of the existing building at 68 Sweetland Avenue. The proposed addition will have a basement. The elevation of the underside of footing will be at a design elevation of Elevation 65.79 m and the site grade raise will be a maximum of 0.4 m. The building section drawing, Drawing No. A112, dated May 16, 2022 and prepared by Woodman and Architect (Woodman) indicates the design elevation of the basement floor slab will be at Elevation 66.09 m and similar to the MP plan, the design elevation of the underside of the footings will be at Elevation 65.79 m.

This geotechnical investigation was undertaken to:

- a) Establish the subsurface soil conditions and groundwater levels at two (2) boreholes located on the site,
- b) Provide classification of the site for seismic design in accordance with requirements of the 2012 Ontario Building Code (OBC) as amended May 2, 2019 and assess the liquefaction potential of the subsurface soils during a seismic event,
- c) Discuss grade raise restrictions,
- d) Provide the bearing pressure at Serviceability Limit State (SLS) and factored geotechnical resistance at Ultimate Limit State (ULS) of the most suitable type of foundation for the proposed building addition, as well as anticipated total and differential settlements,
- e) Comment on slab-on-grade construction and permanent drainage requirements,
- f) Discuss the lateral earth pressure (static and seismic conditions) against basement walls,
- g) Discuss excavation conditions and dewatering requirements during construction of the foundation for the proposed building addition,
- h) Comment on backfilling requirements and suitability of the on-site soils for backfilling purposes; and
- i) Discuss the subsurface concrete requirements and the corrosion potential of subsurface soils to buried metal structures/members.

The comments and recommendations given in this report assume that the above-described design concept will proceed into construction. If changes are made either in the design phase or during construction, this office must be retained to review these modifications. The result of this review may be a modification of our recommendations, or it may require additional field or laboratory work to check whether the changes are acceptable from a geotechnical viewpoint.

## **2. Site Description**

The property is located in a well-established, developed area of the City of Ottawa. The site is a rectangular-shaped property bounded along the east side by Sweetland Avenue, and residential properties to the north, south and west. The site is currently occupied by a multiple unit residential building with parking in the rear.

An approximate 1.0 m high retaining wall exists along the south property line and is constructed from wood.

The proposed building addition is planned to be located in the current parking area on the west side (rear) of the existing building.

The topography of the site is relatively flat, gradually sloping down from west to east from an approximate elevation of Elevation 68.4 m to Elevation 67.2 m based on the topographical survey plan of the site dated November 28, 2019 and prepared by Annis, O'Sullivan, Vollebakk Ltd. (AOV).



### 3. Procedure

The borehole fieldwork for the geotechnical investigation was completed on May 31, 2022 and consists of two (2) boreholes (Borehole Nos. 1 and 2) drilled to termination and cone refusal depths of 6.7 m and 15.8 m respectively. The borehole locations are shown on Figure 2. The fieldwork was supervised on a full-time basis by a representative from EXP.

Prior to the fieldwork, the locations of the boreholes were staked in the field and their locations cleared of any public and private underground services. The geodetic elevation of the ground surface at each borehole location was estimated from the topographical survey plan of the site dated November 28, 2019 and prepared by AOV. Therefore, the borehole ground surface elevations and the elevations of the soil boundaries and groundwater level shown in the borehole logs should be considered approximate.

The boreholes were drilled using a track-mounted drill rig equipped with hollow stem augers and operated by a drilling specialist subcontracted to EXP. Standard penetration tests (SPTs) were performed in all the boreholes at 0.75 m and 1.5 m depth intervals and the soil samples were retrieved by the split-spoon sampler. The undrained shear strength of the cohesive soil was measured by conducting penetrometer and in-situ vane tests. In Borehole No. 1, a dynamic cone penetration test (DCPT) was conducted from auger refusal at 14.9 m to a cone refusal depth of 15.8 m below ground surface.

A 38 mm diameter monitoring well (with 1.5 m slotted section) was installed in Borehole No. 2 for long-term monitoring of the groundwater level. The monitoring well was installed in accordance with EXP standard practice and the installation configuration is documented on the respective borehole log. The boreholes were backfilled upon completion of drilling and the installation of the monitoring well.

All soil samples were visually examined in the field for textural classification, logged, preserved in plastic bags and identified accordingly. On completion of the fieldwork, all the soil samples were transported to the EXP laboratory located in the City of Ottawa where they were visually examined by a geotechnical engineer and the borehole logs were prepared. The engineer also assigned the laboratory testing which consisted of performing the following tests on the soil samples:

Natural Moisture Content Determination .....	16 tests
Natural Unit Weight Determination.....	4 tests
Grain Size Analysis.....	3 tests
Atterberg Limits.....	1 tests
Chemical Analysis (pH, sulphate and chloride) .....	1 test

## 4. Subsurface Soil and Groundwater Conditions

A detailed description of the subsurface soil and groundwater conditions encountered in the boreholes is given on the borehole logs, Figures 3 and 4. The borehole logs and related information depict subsurface conditions only at the specific locations and times indicated. Subsurface conditions and water levels at other locations may differ from conditions at the locations where sampling was conducted. The passage of time may also result in changes in the conditions interpreted to exist at the locations where sampling was conducted.

The boreholes were drilled to provide representation of subsurface conditions as part of a geotechnical exploration program and are not intended to provide evidence of environmental conditions.

It should be noted that the soil boundaries indicated on the borehole logs are intended to reflect approximate transition zones for the purpose of geotechnical design and should not be interpreted as exact planes of geological change. The “Notes on Sample Descriptions” preceding the borehole logs forms an integral part of this report and should be read in conjunction with this report.

A review of the borehole logs indicates the following subsurface soil conditions with depth and groundwater level measurements.

### 4.1 Granular Fill

A surficial 100 mm and 150 mm thick granular layer was contacted in both boreholes.

The results from the grain-size analysis conducted on one (1) sample of the granular fill is summarized in Table I. The grain-size distribution curve is shown in Figure 5.

Borehole No. – Sample No.	Depth (m)	Grain-size Analysis (%)			Soil Classification (USCS)
		Gravel	Sand	Silt and Clay	
BH1 – SS1	0.0 – 0.1	26	59	15	Silty Sand with Gravel (SM)

Based on a review of the results of the grain-size analysis, the granular fill may be classified as a silty sand with gravel in accordance with the Unified Soil Classification System (USCS).

### 4.2 Fill

In both boreholes, the granular fill is underlain by heterogeneous fill that extends to a 1.4 m depth (Elevation 67.0 m) in both boreholes. The fill consists of a silty sand to silty clay to a mixture of silty sand and silty clay with gravel, topsoil inclusions and concrete and wood fragments. The standard penetration test (SPT) N values of the fill range from 3 to 23 indicating the fill is in a very loose to compact state. The moisture content of the fill is 16 percent to 41 percent. The unit weight of the fill is 18.4 kN/m<sup>3</sup>.

### 4.3 Clay

Native clay was encountered beneath the fill in both boreholes at 1.4 m depth (Elevation 67.0 m) and extends to a 7.5 m depth (Elevation 60.9 m) in Borehole No. 1. Borehole No. 2 terminated within the clay at a 6.7 m depth (Elevation 61.7 m). The clay consists of an upper desiccated brown clay crust to approximate 3.7 m and 5.9 m depths (Elevation 64.7 m and Elevation 62.5 m) underlain by an un-desiccated grey clay. The undrained shear strength of the brown clay crust ranges from 120 kPa to 250 kPa indicating the clay has a very stiff to hard consistency. The sensitivity values of the brown clay are 4.0 to 6.0 indicating the clay is sensitive. The lower grey clay has an undrained shear strength of 43 kPa and 72 kPa indicating the grey clay has a firm to stiff consistency. The sensitivity values of the grey clay range from 3.8 to 9.0 indicating the clay is sensitive to extra-sensitive.

The natural moisture content and unit weight of the brown clay crust is 34 percent to 74 percent and 16.8 kN/m<sup>3</sup> to 17.6 kN/m<sup>3</sup> respectively. The natural moisture content of the grey clay is 59 and 68 percent.

The results from the grain-size analysis and Atterberg limit determination conducted on one (1) sample of the brown clay crust is summarized in Table II. The grain-size distribution curve is shown in Figure 6.

Borehole (BH) No. – Sample (SS) No.	Depth (m)	Grain-Size Analysis (%)			Atterberg Limits (%)				
		Gravel	Sand	Fines (Silt and Clay)	Moisture Content	Liquid Limit	Plastic Limit	Plasticity Index	Soil Classification (USCS)
BH 2 – SS3	1.5 – 2.1	0	1	99	46	64	31	33	Clay of High Plasticity (CH)

Based on a review of the results of the grain-size analysis and Atterberg limits, the soil may be classified as a clay of high plasticity (CH) in accordance with the USCS.

### 4.4 Clayey Silt

The clay in Borehole No. 1 is underlain by clayey silt that extends to a 13.7 m depth (Elevation 54.7 m). The clayey silt exhibits slight plasticity. The undrained shear strength of the clayey silt is 62 kPa and 101 kPa indicating the clayey silt has a stiff to very stiff consistency. The sensitivity values of the clayey silt are 3.7 and 4.7 indicating the clayey silt is medium sensitive to sensitive. The natural moisture content of the clayey silt ranges from 28 percent to 42 percent.

The results from the grain-size analysis conducted on one (1) sample of the clayey silt is summarized in Table III. The grain-size distribution curve is shown in Figure 7.

Table III: Summary of Results from Grain-Size Analysis -  
 Clayey Silt Sample

Borehole (BH) No. – Sample (SS) No.	Depth (m)	Grain-Size Analysis (%)			
		Gravel	Sand	Fines (Silt and Clay)	Soil Classification (USCS)
BH 1 – SS7	7.6 – 8.2	0	15	85	Clayey Silt with Sand (ML)

Based on a review of the results of the grain-size analysis, the soil may be classified as a clayey silt with sand (ML) in accordance with the USCS.

#### 4.5 Glacial Till

Glacial till was contacted in Borehole No.1 below the clayey silt at a 13.7 m depth (Elevation 54.7 m). The glacial till is a silty sand with gravel and possible cobbles and boulders. The SPT N value of the glacial till is 14 indicating the glacial till is in a compact state. The natural moisture content of the glacial till is 8 percent.

#### 4.6 Inferred Boulders or Bedrock

A dynamic cone penetration test (DCPT) was conducted in Borehole No. 1 from a 14.9 m auger refusal depth to cone refusal at a 15.8 m depth (Elevation 52.6 m). Cone refusal may have been met on inferred boulders or bedrock.

#### 4.7 Groundwater Level

The groundwater level was measured in the monitoring well installed in Borehole No. 2 on June 7, 2022 (7 days after drilling) and indicates the groundwater level was at a 5.4 m depth (Elevation 63.0 m).

Groundwater levels were determined in the borehole at the time and under the condition stated in the scope of services. Note that fluctuations in the level of groundwater may occur due to a seasonal variation such as precipitation, snowmelt, rainfall activities, and other factors not evident at the time of measurement and therefore may be at a higher level during wet weather periods.

## 5. Seismic Site Classification and Liquefaction Potential of Soils

### 5.1 Site Classification for Seismic Site Response

Based on the borehole information and Table 4.1.8.4.A in the 2012 Ontario Building Code (as amended May 2, 2019), the site classification for seismic site response is **Class D**.

A higher site class may be obtained by conducting a shear wave velocity soundings survey of the site.

### 5.2 Liquefaction Potential of Soils

The subsurface soils are not considered to be liquefiable during a seismic event.

## **6. Grade Raise Restrictions**

The site is underlain by a clay deposit that is prone to consolidation settlement if overstressed by loads imposed on it by site grade raise, foundations and by the permanent lowering of the groundwater level following construction. Overstressing of the clay will result in its consolidation and subsequent settlement of foundations, which may exceed tolerable limits of the structure resulting in cracking of the structure.

The grading, drainage, erosion and sediment control plan, Drawing No. C101, dated January 20, 2023 (Revision No. 1) and prepared by McIntosh Perry (MP), indicates the site grade raise will be a maximum of 0.4 m. Based on the borehole information, a maximum site grade raise of 0.5 m is considered acceptable. Therefore, a review of the grading of the site shown in the above referenced MP drawing is considered to be in general conformance with the recommendations of this geotechnical report.

## 7. Foundation Considerations

The grading, drainage, erosion and sediment control plan prepared by MP and the building section plan prepared by Woodman indicate the design elevations of the basement floor slab will be at Elevation 66.09 m and the underside of footings will be at Elevation 65.79 m.

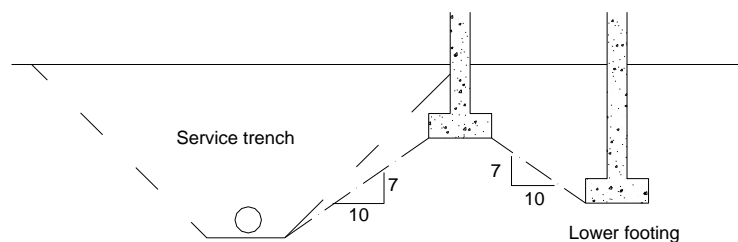
Based on a review of the borehole information, it is considered feasible to support the proposed building addition by strip and spread footings founded at a maximum founding depth of 2.6 m below existing grade at the underside of footing design elevation of Elevation 65.79 m on the native clay. The existing fill is not considered suitable to support the footings for the proposed building addition. For strip footings having a maximum width of 1.0 m and square pad footings having a maximum width and length of 3.0 m founded on the native clay at a maximum depth of 2.6 m below existing grade (Elevation 65.79 m), the footings may be designed for a bearing pressure at serviceability limit state (SLS) of 150 kPa and factored geotechnical resistance at ultimate limit state (ULS) of 225 kPa. The factored ULS value includes a geotechnical resistance factor of 0.5. The recommended SLS and factored ULS values are valid for the maximum footing founding depth of 2.6 m below existing grade on the native clay and for a maximum site grade raise of 0.5 m. Should the footings extend to greater depths below the maximum depth of 2.6 m below existing grade, EXP should be contacted to review and provide updated SLS and factored ULS values for the footings.

The total and differential settlements of footings designed in accordance with the recommendations of this report and with careful attention to construction detail are expected to be less than 25 mm and 19 mm respectively.

To minimize the need to underpin the existing footings along the west wall of the existing building where the proposed new building addition will be located, it is recommended that the basement floor slab and footings for the new building addition be placed at the same depth as the existing lowest floor slab and the existing footings. This is valid for the footings, provided the native clay exposed at the same level as the bottom of the existing footings is capable of supporting the bearing pressure at serviceability limit state (SLS) and factored geotechnical resistance at ultimate limit state (ULS) recommended above for the footings.

If deeper excavation is required for the new footings located adjacent to existing footings, underpinning of the existing footings may be required. EXP can provide additional recommendations regarding the underpinning of the existing footings.

Footings at different elevations should be located such that the higher footings are set below a line drawn up at 10 horizontal to 7 vertical (10H:7V) from the near edge of the lower footing. This concept should also be applied to service excavation, etc. to ensure that undermining is not a problem.



FOOTINGS NEAR SERVICE TRENCHES OR AT DIFFERENT ELEVATIONS

All footing beds should be examined by a geotechnical engineer to ensure that the founding soil is capable of supporting the bearing pressure at SLS and that the footings have been properly prepared.

It should be noted that the exposed clay subgrade surface is susceptible to disturbance due to movement of workers and construction traffic and the prevailing weather conditions during construction. To prevent disturbance to the clay subgrade, the approved footing beds should be covered or protected with a 50 mm thick concrete mud slab.

A minimum of 1.5 m of earth cover should be provided to the exterior foundations of heated structures to protect them from damage due to frost penetration. The frost cover should be increased to 2.1 m for unheated structures if snow will not be removed from their vicinity and to 2.4 m if snow will be removed from the vicinity of the structure. When earth cover is less than the minimum required, an equivalent thermal combination of earth cover and rigid insulation or rigid insulation alone should be provided. EXP can provide additional comments in this regard, if required.

The recommended bearing pressure at SLS and factored geotechnical resistances at ULS have been calculated by EXP from the borehole information for the design stage only. The investigation and comments are necessarily ongoing as new information of underground conditions becomes available. For example, more specific information is available with respect to conditions between boreholes when foundation construction is underway. The interpretation between boreholes and the recommendations of this report must therefore be checked through field monitoring provided by an experienced geotechnical engineer to validate the information for use during the construction stage.



## **8. Slab-on-Grade Construction and Permanent Drainage Systems**

The design elevation of the basement floor will be at Elevation 66.09 m and at this elevation, the subgrade is anticipated to consist of the native clay. The basement floor may be designed as a slab-on-grade set on the native clay or on a minimum 300 mm thick engineered fill pad placed on the native clay and should consist of Ontario Provincial Standard Specification (OPSS) Granular B Type II compacted to 98 percent standard Proctor maximum dry density (SPMDD). The existing fill is not considered suitable to support the slab-on-grade and should be excavated and removed down to the native clay within the floor slab footprint. The floor slab should be set on a bed of well-packed 19 mm clear stone at least 200 mm thick placed on the engineered fill pad or on the native clay. The clear stone would prevent the capillary rise of moisture from the sub-soil to the floor slab. Adequate saw cuts should be provided in the floor slab to control cracking.

A perimeter drainage system should be installed around the proposed new building addition. If the perimeter drainage system of the existing building is encountered during the construction of the new building addition, they should be reinstated. The perimeter drainage system may comprise of 150 mm diameter perforated pipe or equivalent covered at the top, sides and bottom with a minimum 150 mm thick layer of clear stone that is completely wrapped or covered with a non-woven geotextile such as Terrafix 270R or equivalent. The perimeter drainage system should be connected to a sump to provide positive drainage. An underfloor drainage system is not required for the proposed building addition.

The groundwater level is at a 5.4 m depth (Elevation 63.0 m) and is approximately 3.8 m below the basement floor of the proposed building addition. Since the perimeter drainage system for the new building addition will be above the groundwater level, the perimeter drainage system is not anticipated to lower the groundwater level over the long-term. Therefore, the perimeter drainage system is not anticipated to induce settlement of neighboring structures and infrastructure from a groundwater level perspective.

The finished exterior grade should be sloped away from the building to prevent ponding of surface water close to the exterior walls of the proposed building addition.

## 9. Lateral Earth Pressure on Subsurface Walls

The subsurface basement walls of the building addition should be backfilled with free draining material, such as OPSS Granular B Type II compacted to 95 percent SPMD and equipped with a perimeter drainage system to prevent the buildup of hydrostatic pressure behind the walls. The walls will be subjected to lateral static and dynamic (seismic) earth forces. The expressions below assume free draining backfill material, a perimeter drainage system, level backfill surface behind the wall and vertical face on the back side of the wall.

For design purposes, the lateral static earth thrust against the subsurface walls may be computed from the following equation:

$$P = K_0 h \left( \frac{1}{2} \gamma h + q \right)$$

where  $P$  = lateral earth thrust acting on the subsurface wall, kN/m

$K_0$  = lateral earth pressure at rest coefficient, assumed to be 0.5 for Granular B Type II backfill material

$\gamma$  = unit weight of free draining granular backfill; Granular B Type II = 22 kN/m<sup>3</sup>

$h$  = depth of point of interest below top of backfill, m

$q$  = surcharge load stress, kPa

The lateral dynamic thrust may be computed from the equation given below:

$$\Delta_{pe} = \gamma H^2 \frac{a_h}{g} F_b$$

where  $\Delta_{pe}$  = dynamic thrust in kN/m of wall

$H$  = height of wall, m

$\gamma$  = unit weight of backfill material = 22 kN/m<sup>3</sup>

$\frac{a_h}{g}$  = earth pressure coefficient = 0.32 for Ottawa area

$F_b$  = thrust factor = 1.0

The dynamic thrust does not take into account the surcharge load. The resultant force of the lateral dynamic thrust acts approximately at 0.63H above the base of the wall.

All subsurface walls should be properly waterproofed.

## 10. Excavation and De-Watering Requirements

### 10.1 Excess Soil Management

Ontario Regulation 406/19 specifies protocols that are required for the management and disposal of excess soils. As set forth in the regulation, specific analytical testing protocols need to be implemented and followed based on the volume of soil to be managed and the requirements of the receiving site. The testing protocols are specific as to whether the soils are stockpiled or in situ. In either scenario, the testing protocols are far more onerous than have been historically carried out as part of standard industry practices. These decisions should be factored in and accounted for prior to the initiation of the project-defined scope of work. EXP would be pleased to assist with the implementation of a soil management and testing program that would satisfy the requirements of Ontario Regulation 406/19.

### 10.2 Excavations

Excavations for the construction of the proposed building addition foundations are anticipated to extend a maximum of 2.5 m depth below existing ground surface. These excavations will extend through the fill and into the native clay and will be above the groundwater level.

The excavations may be undertaken by conventional heavy equipment capable of removing any construction debris within the fill (such as wood and concrete pieces).

All excavations must be undertaken in accordance with the Occupational Health and Safety Act (OHSA), Ontario Reg. 213/91. Based on the definitions provided in OHSA, the subsurface soils on site are considered to be Type 3 and for open cut excavations, the side slopes of the excavation must be cut back at 1H:1V from the bottom of the excavation. For zones along the sidewalls of the excavation of persistent water seepage, the excavation side slopes are expected to slough and eventually stabilize at a slope of 3H:1V to 2H:1V from the bottom of the excavation.

If side slopes noted above cannot be achieved due to space restrictions on site, such as the proximity of open cut excavations to the property limits, existing infrastructure or to foundations of adjacent existing buildings, the excavation for the new building addition construction would have to be undertaken within the confines of an engineered support system (shoring system).

The need for a shoring system, the most appropriate type of shoring system and the design and installation of the shoring system should be determined by the contractors bidding on this project. The design of the shoring system should be undertaken by a professional engineer experienced in shoring design and the installation of the shoring system should be undertaken by a contractor experienced in the installation of shoring systems. The shoring system should be designed and installed in accordance with latest edition of Ontario Regulation 213/91 under the OHSA and the 2006 Fourth Edition of the Canadian Foundation Engineering Manual (CFEM). The shoring system as well as adjacent settlement sensitive structures (buildings) and infrastructure should be monitored for movement (deflection) on a periodic basis during construction operations.

A pre-construction condition survey of buildings and infrastructure within the influence zone of the construction should be undertaken prior to start of construction activities.

It is recommended that vibration monitoring be conducted at the site and at adjacent existing buildings and infrastructure during the installation of the shoring system and during construction of the new building addition to ensure the existing structures and infrastructure are not damaged as a result of the construction activities.

Base heave type failure is not expected in excavations that extend into the native clay to a maximum 2.5 m depth below existing grade.

The clay stratum at the site is susceptible to disturbance due to the movement of construction equipment and personnel on its surface. It is therefore recommended that the excavation at the site should be undertaken by equipment that does not need to travel on the excavated surface, such as a gradall or mechanical shovel.

Extra care should be exercised during the excavation close to the existing building to prevent the undermining of the existing footings. Reference is made to Section 7 of this report regarding measures to prevent the undermining of existing footings.

The existing wood retaining wall located along the south property line will be removed as part of the construction of the proposed addition to the residential building.

Many geologic materials deteriorate rapidly upon exposure to meteorological elements. Unless otherwise specifically indicated in this report, walls and floors of excavations must be protected from moisture, desiccation, and frost action throughout the course of construction.

### **10.3 De-Watering Requirements**

Seepage of the surface and subsurface water into the excavations above the groundwater level is anticipated and it should be possible to collect water entering the excavations at low points and to remove it by conventional pumping techniques. High-capacity pumps may be required to keep the excavation dry in zones of persistent seepage where more permeable soil may exist along the side walls of the excavation.

Since the excavations are anticipated to be above the groundwater level, the dewatering of excavations on site during the short-term construction operations is not expected to induce settlement adjacent existing structures and infrastructure.

If less than 50 m<sup>3</sup> of water are to be pumped per day, no permits are required. If between 50 m<sup>3</sup> and 400 m<sup>3</sup> of water is to be pumped per day, then the activity should be registered on the Environmental Activity and Sector Registry (EASR), an online registry maintained by the Ministry of the Environment, Conservation and Parks (MECP). If more than 400 m<sup>3</sup> of water is to be pumped per day, then a Category 3 Permit to Take Water (PTTW) is required.

Since water taking can be groundwater, storm water, or a combination of both, the most likely potential for significant volumes of water requiring removal from an excavation at the site is storm water. If a major rain event occurs while a large excavation is open, then it is possible that the total accumulation of water within the excavation will exceed 50 m<sup>3</sup>. If that occurs, then it may be removed without a permit by pumping over several days during which no single-day water-taking is more than 50 m<sup>3</sup>. Alternatively, a maximum of 400 m<sup>3</sup> of water may be pumped per day once the online EASR application form is filled out and the fee is paid. The EASR application may be completed by the property owner or their delegate. EXP would be pleased to assist with the EASR, should it be deemed necessary. Per the terms of the EASR, the total quantities of water actually removed from the excavation must be reported to the MECP.

A scenario whereby a Category 3 PTTW would be required is not anticipated for this project. A Category 3 PTTW would require a complete hydrogeological assessment and would take at least 90 days for the MECP to process once the application is submitted.

Although this investigation has estimated the groundwater levels at the time of the fieldwork, and commented on dewatering and general construction problems, conditions may be present which are difficult to establish from standard boring and excavating techniques and which may affect the type and nature of dewatering procedures used by the contractor in practice. These conditions include local and seasonal fluctuations in the groundwater table, erratic changes in the soil profile, thin layers of soil with large or small permeabilities compared with the soil mass, etc. Only carefully controlled tests using pumped wells and observation wells will yield the quantitative data on groundwater volumes and pressures that are necessary to adequately engineer construction dewatering systems.

## 11. Pipe Bedding Requirements

It is recommended that the bedding for the underground services including material specifications, thickness of cover material and compaction requirements conform to municipal requirements and/or Ontario Provincial Standard Specification and Drawings (OPSS and OPSD).

The pipe subgrade material is anticipated to consist of firm to hard clay. In this case, it is recommended the pipe bedding consist of 300 mm thick of OPSS 1010 Granular A bedding material. The bedding material should be compacted to at least 98 percent SPMDD.

The bedding thickness may be further increased in areas where the clay subgrade becomes disturbed or below the water table. Trench base stabilization techniques, such as removal of loose/soft material, placement of crushed stone sub-bedding (Granular B Type II) that is completely wrapped in a non-woven geotextile, may also be used if trench base disturbance becomes a problem in wet or soft areas.

It is anticipated that paved surfaces may be located over service trenches. In this case, it is recommended that the trench backfill material within the frost zone up to 1.8 m below finished grade, should match the existing material in the paved roadway, provided the material is determined to be suitable for re-use as backfill material. The matching of materials minimizes differential frost heave of the subgrade material. If the trench backfill material is different than the material in the sidewalls of the trench, a 3H:1V frost taper should be provided to minimize differential frost heave. The trench backfill should be placed in 300 mm thick lifts and each lift compacted to 95 percent SPMDD.

If the backfill for the service trenches will consist of granular fill, clay seals should be installed in the service trenches at select intervals as required. The seals should be 1 m wide, extend over the entire trench width and from the bottom of the trench to the underside of the pavement structure. The clay should be compacted to 95 percent SPMDD. The purpose of the clay seals is to prevent the permanent lowering of the groundwater level. Reference is made to the City of Ottawa Drawing No. S8 regarding clay seals for pipe trenches.

The underground services should be installed in short open trench sections that are excavated and backfilled the same day.

## **12. Backfilling Requirements and Suitability of On-Site Soils for Backfilling Purposes**

The material to be excavated from the site will comprise of fill and native clay. Portions of the fill (free of topsoil and debris) may be re-used as backfill material in the landscaped areas, subject to additional geotechnical evaluation and testing at the time of construction. The excavated soils are not considered suitable for use under structural elements and for backfilling purposes and therefore must be disposed off-site or used in landscaped areas.

It is anticipated that the majority of the material required for engineered fill and for backfilling purposes for this project would have to be imported and should preferably conform to the following specification:

- Engineered fill under slab-on-grade - OPSS 1010 Granular B Type II placed in 300 mm thick lifts and each lift compacted to 98 percent SPMDD.
- Backfill in footing trenches and against foundation walls – OPSS 1010 Granular B Type II placed in 300 mm thick lifts and each lift compacted to 98 percent of the SPMDD inside the building and 95 percent SPMDD outside the building respectively.

### 13. Subsurface Concrete Requirements

Chemical tests limited to pH, chloride and sulphate determination were performed on one (1) sample of the brown clay soil sample. The laboratory certificate of analysis is attached in Appendix A and the results are summarized in Table IV below.

Table IV: Results of pH, Chloride and Sulphate Tests on Soil Sample					
Borehole No. (Sample No.)	Depth (m)	Soil Type	pH	Sulphate (%)	Chloride (%)
BH 2 – SS4	3.0 -3.6	Native Brown Clay	7.36	0.0048	0.0072

The test results indicate the native brown clay has a sulphate content of less than 0.1 percent. This concentration of sulphate in the native brown clay would have a negligible potential of sulphate attack on subsurface concrete. The concrete should be designed in accordance with Table Nos. 3 and 6 of CSA A.23.1-19. However, the concrete should be dense, well compacted and cured.



## 14. Tree Planting Restrictions

The site is underlain by marine clay. The test results of the native upper brown portion of the marine clay were compared with the document titled, “Tree Planting in Sensitive Marine Clay Soils – 2017 City of Ottawa Guidelines (2017 Guidelines)” and indicate the upper brown clay has a low/medium potential for soil volume change. For soils that have a low/medium potential for soil volume change, the 2017 Guidelines indicate that the tree to foundation setback distance and tree planting restrictions should be in accordance with the 2017 Guidelines. A landscape architect should be consulted to ensure the setbacks and tree planting restrictions are in accordance with the 2017 Guidelines.

## 15. General Comments

The comments given in this report are intended only for the guidance of design engineers. The number of boreholes required to determine the localized underground conditions, between boreholes affecting construction costs, techniques, sequencing, equipment, scheduling, etc., would be much greater than has been carried out for design purposes. Contractors bidding on or undertaking the works should, in this light, decide on their own investigations, as well, as their own interpretations of the factual borehole results, so that they may draw their own conclusions as to how the subsurface conditions may affect them.

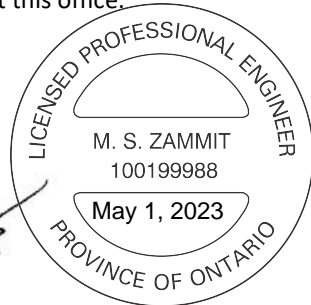
The information contained in this report is not intended to reflect on environmental aspects of the soils. Should specific information be required, including for example, the presence of pollutants, contaminants or other hazards in the soil, additional testing may be required.

We trust that the information contained in this report is satisfactory for your purposes. Should you have any questions, please contact this office.

Sincerely,



Matthew Zammit, M.A.Sc., P.Eng.  
Geotechnical Engineer  
Earth and Environment



Susan M. Potyondy P.Eng.  
Senior Project Manager  
Earth and Environment

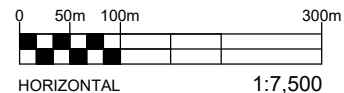
EXP Services Inc.

*Smart Living Properties  
Geotechnical Investigation, Proposed Addition to Residential Building  
68 Sweetland Avenue, Ottawa, ON  
OTT-22005690-A0  
May 1, 2023*

# Figures



**SITE LOCATION**



**EXP Services Inc. [www.exp.com](http://www.exp.com)**  
 t: +1.613.688.1899 | f: +1.613.225.7337  
 2650 Queensview Drive, Suite 100  
 Ottawa, ON K2B 8H6, Canada

DATE JUNE 2022		CLIENT: <b>SMART LIVING PROPERTIES</b> GEOTECHNICAL INVESTIGATION	project no. OTT-22005690-A0
DESIGN MZ	CHECKED IT		scale 1:7,500
DRAWN BY AS		TITLE: <b>SITE LOCATION PLAN</b> 68 SWEETLAND AVENUE, OTTAWA, ON	FIG 1

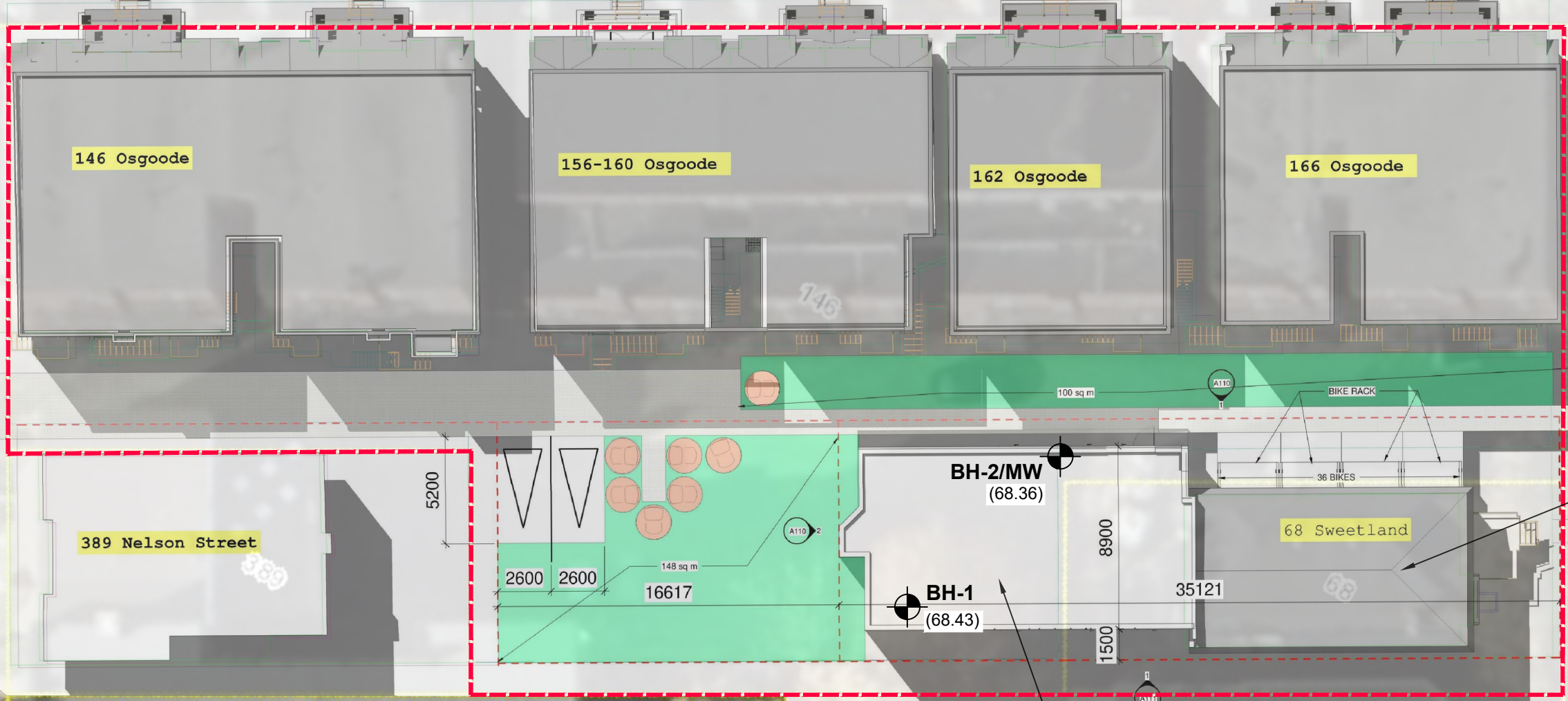
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 Last Saved: Jun 1, 2022 8:06 AM  
 Last Plotted: Jun 15, 2022 8:06 AM  
 Plotted By: Walid

rue Osgoode St.



rue Nelson St.

AV. Sweetland/Ave.



146 Osgoode

156-160 Osgoode

162 Osgoode

166 Osgoode


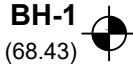

389 Nelson Street

68 Sweetland

BH-2/MW  
(68.36)

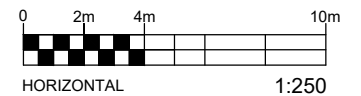
BH-1  
(68.43)

**LEGEND**

-  PROPERTY LINE
-  BOREHOLE LOCATION, NUMBER APPROXIMATE ELEVATION IN METRES
-  BOREHOLE + MONITORING WELL APPROXIMATE ELEVATION IN METRES

**NOTES:**

1. THE BOUNDARIES AND SOIL TYPES HAVE BEEN ESTABLISHED ONLY AT BOREHOLE LOCATIONS. BETWEEN BOREHOLES THEY ARE ASSUMED AND MAY BE SUBJECT TO CONSIDERABLE ERROR.
2. SOIL SAMPLES WILL BE RETAINED IN STORAGE FOR THREE MONTHS AND THEN DESTROYED UNLESS THE CLIENT ADVISES THAT AN EXTENDED TIME PERIOD IS REQUIRED.
3. TEST HOLE ELEVATIONS SHOULD NOT BE USED TO DESIGN BUILDING(S) OR FLOOR SLABS OR PARKING LOT(S) GRADES.
4. THIS DRAWING FORMS PART OF THE REPORT PROJECT NUMBER AS REFERENCED AND SHOULD BE USED ONLY IN CONJUNCTION WITH THIS REPORT.
5. BASE PLAN INFORMATION OBTAINED FROM W.J. JOHNSTON SURVEYING LTD DATED APRIL 28, 2020.



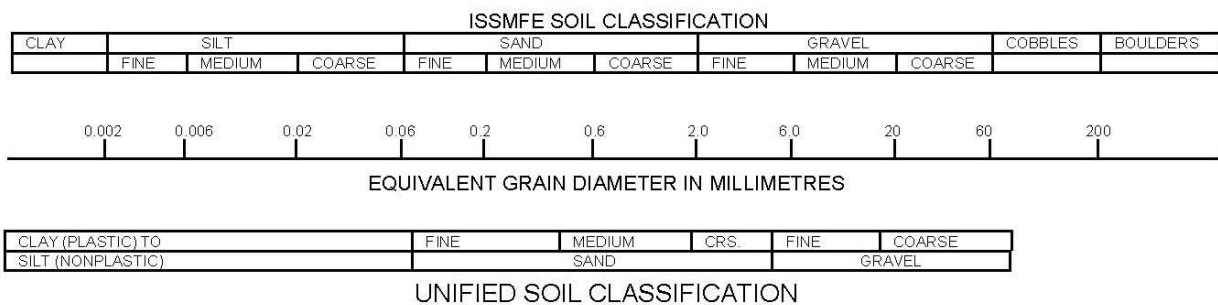
**EXP Services Inc. www.exp.com**  
 t: +1.613.688.1899 | f: +1.613.225.7337  
 2650 Queensview Drive, Suite 100  
 Ottawa, ON K2B 8H6, Canada

DATE JUNE 2022		CLIENT: <b>SMART LIVING PROPERTIES</b>		project no. OTT-22005690-A0
DESIGN MZ	CHECKED IT	TITLE: <b>GEOTECHNICAL INVESTIGATION</b>		scale 1:250
DRAWN BY AS		<b>BOREHOLE LOCATION PLAN</b>		<b>FIG 2</b>
68 SWEETLAND AVENUE, OTTAWA, ON				

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 Last Plotted: Jun 15, 2022 8:05 AM  
 Plotted by: Walid

## Notes On Sample Descriptions

1. All sample descriptions included in this report follow the Canadian Foundations Engineering Manual soil classification system. This system follows the standard proposed by the International Society for Soil Mechanics and Foundation Engineering. Laboratory grain size analyses provided by **exp** Services Inc. also follow the same system. Different classification systems may be used by others; one such system is the Unified Soil Classification. Please note that, with the exception of those samples where a grain size analysis has been made, all samples are classified visually. Visual classification is not sufficiently accurate to provide exact grain sizing or precise differentiation between size classification systems.



2. **Fill:** Where fill is designated on the borehole log it is defined as indicated by the sample recovered during the boring process. The reader is cautioned that fills are heterogeneous in nature and variable in density or degree of compaction. The borehole description may therefore not be applicable as a general description of site fill materials. All fills should be expected to contain obstruction such as wood, large concrete pieces or subsurface basements, floors, tanks, etc., none of these may have been encountered in the boreholes. Since boreholes cannot accurately define the contents of the fill, test pits are recommended to provide supplementary information. Despite the use of test pits, the heterogeneous nature of fill will leave some ambiguity as to the exact composition of the fill. Most fills contain pockets, seams, or layers of organically contaminated soil. This organic material can result in the generation of methane gas and/or significant ongoing and future settlements. Fill at this site may have been monitored for the presence of methane gas and, if so, the results are given on the borehole logs. The monitoring process does not indicate the volume of gas that can be potentially generated nor does it pinpoint the source of the gas. These readings are to advise of the presence of gas only, and a detailed study is recommended for sites where any explosive gas/methane is detected. Some fill material may be contaminated by toxic/hazardous waste that renders it unacceptable for deposition in any but designated land fill sites; unless specifically stated the fill on this site has not been tested for contaminants that may be considered toxic or hazardous. This testing and a potential hazard study can be undertaken if requested. In most residential/commercial areas undergoing reconstruction, buried oil tanks are common and are generally not detected in a conventional geotechnical site investigation.
3. **Till:** The term till on the borehole logs indicates that the material originates from a geological process associated with glaciation. Because of this geological process the till must be considered heterogeneous in composition and as such may contain pockets and/or seams of material such as sand, gravel, silt or clay. Till often contains cobbles (60 to 200 mm) or boulders (over 200 mm). Contractors may therefore encounter cobbles and boulders during excavation, even if they are not indicated by the borings. It should be appreciated that normal sampling equipment cannot differentiate the size or type of any obstruction. Because of the horizontal and vertical variability of till, the sample description may be applicable to a very limited zone; caution is therefore essential when dealing with sensitive excavations or dewatering programs in till materials.

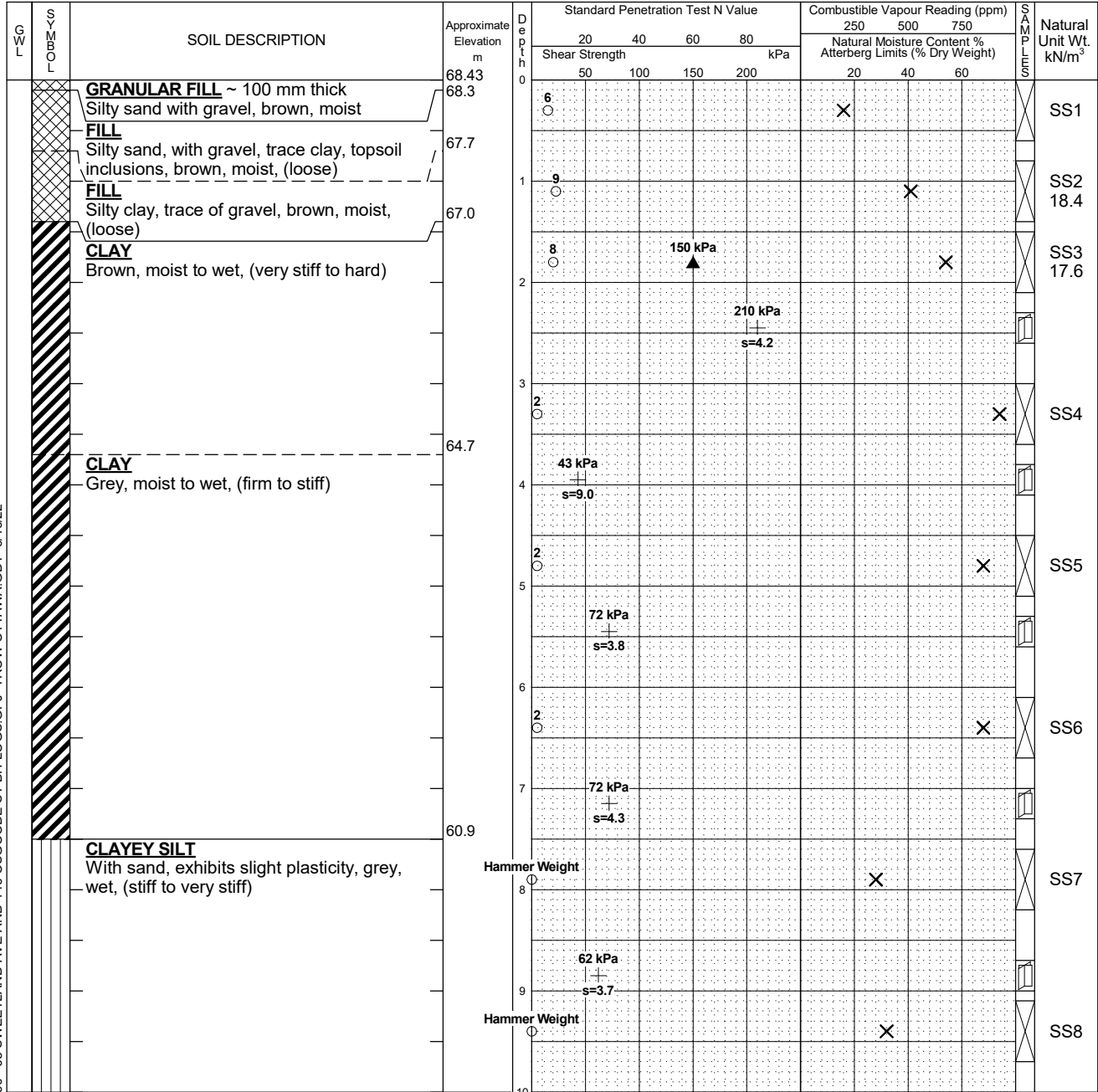
# Log of Borehole BH-01



Project No: OTT-22005690-A0  
 Project: Proposed Addition to Residential Building  
 Location: 68 Sweetland Avenue, Ottawa, Ontario  
 Date Drilled: May 31, 2022  
 Drill Type: CME-45 Track Mounted Drill Rig  
 Datum: Approximate Elevation  
 Logged by: M.Z. Checked by: I.T.

Figure No. 3  
 Page. 1 of 2

Split Spoon Sample  Combustible Vapour Reading   
 Auger Sample  Natural Moisture Content   
 SPT (N) Value  Atterberg Limits   
 Dynamic Cone Test  Undrained Triaxial at % Strain at Failure   
 Shelby Tube  Shear Strength by Penetrometer Test   
 Shear Strength by Vane Test



Continued Next Page

- NOTES:
- Borehole data requires interpretation by EXP before use by others
  - Borehole backfilled upon completion of drilling.
  - Field work supervised by an EXP representative.
  - See Notes on Sample Descriptions
  - Log to be read with EXP Report OTT-22005690-A0

WATER LEVEL RECORDS		
Date	Water Level (m)	Hole Open To (m)
Upon Completion	9.8	13.7

CORE DRILLING RECORD			
Run No.	Depth (m)	% Rec.	RQD %

LOG OF BOREHOLE OTT-22005690 - 68 SWEETLAND AVE AND 146 OSGOODE ST BH LOGS.GPJ TROW OTTAWA GDT 6/16/22

# Log of Borehole BH-01



Project No: OTT-22005690-A0

Figure No. 3

Project: Proposed Addition to Residential Building

Page. 2 of 2

SOIL TYPE	SOIL DESCRIPTION	Approximate Elevation m	Standard Penetration Test N Value				Combustible Vapour Reading (ppm)			Natural Unit Wt. kN/m <sup>3</sup>
			20	40	60	80	250	500	750	
			Shear Strength kPa				Natural Moisture Content % Atterberg Limits (% Dry Weight)			
	<b>CLAYEY SILT</b> With sand, exhibits slight plasticity, grey, wet, (stiff to very stiff) ( <i>continued</i> )	58.43	50	100	150	200	20	40	60	
	With sand seams below a 12.0 m depth									
										SS9
	<b>GLACIAL TILL</b> Silty sand with gravel, some clay, possible cobbles and boulders, brown, wet, (compact)	54.7								
	Dynamic Cone Penetration Test (DCPT) conducted from 14.9 m to cone refusal at 15.8 m depth	53.5								SS10
	<b>Cone Refusal at 15.8 m Depth</b>	52.6								

LOG OF BOREHOLE OTT-22005690 - 68 SWEETLAND AVE AND 146 OSGOODE ST BH LOGS.GPJ TROW OTTAWA.GDT 6/16/22

- NOTES:
- Borehole data requires interpretation by EXP before use by others
  - Borehole backfilled upon completion of drilling.
  - Field work supervised by an EXP representative.
  - See Notes on Sample Descriptions
  - Log to be read with EXP Report OTT-22005690-A0

WATER LEVEL RECORDS		
Date	Water Level (m)	Hole Open To (m)
Upon Completion	9.8	13.7

CORE DRILLING RECORD			
Run No.	Depth (m)	% Rec.	RQD %





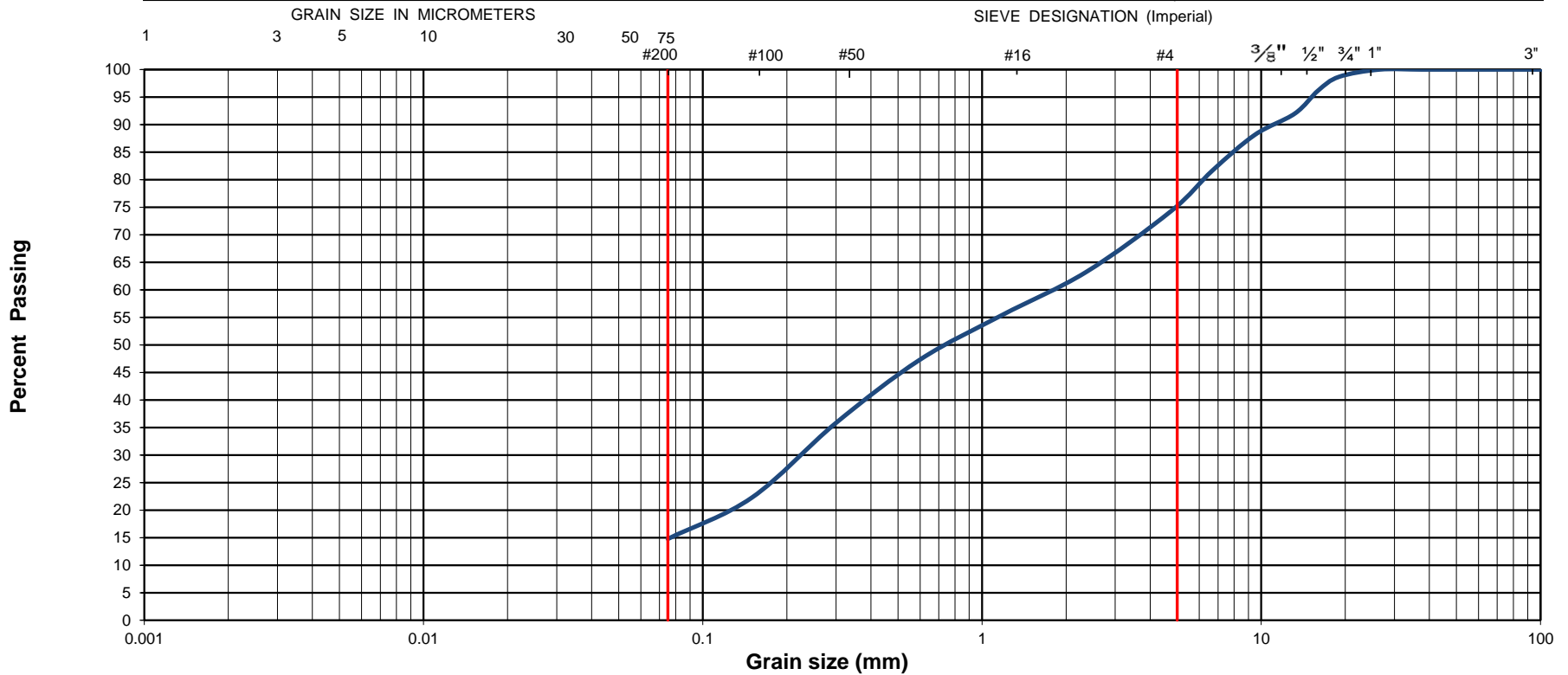


## Grain-Size Distribution Curve Method of Test For Sieve Analysis of Aggregate ASTM C-136

**EXP Services Inc.**  
100-2650 Queensview Drive  
Ottawa, ON K2B 8H6

### Unified Soil Classification System

CLAY AND SILT			SAND			GRAVEL	
			Fine	Medium	Coarse	Fine	Coarse



EXP Project No.:	OTT-22005690-A0	Project Name :	Proposed Addition to Residential Building			
Client :	Smart Living Properties	Project Location :	68 Sweetland Avenue, Ottawa, Ontario			
Date Sampled :	May 31, 2022	Borehole No:	BH1	Sample:	SS1	
Sample Composition :	Gravel (%)	26	Sand (%)	59	Silt & Clay (%)	15
Sample Description :	<b>GRANULAR FILL: Silty Sand with Gravel (SM)</b>				Figure :	5

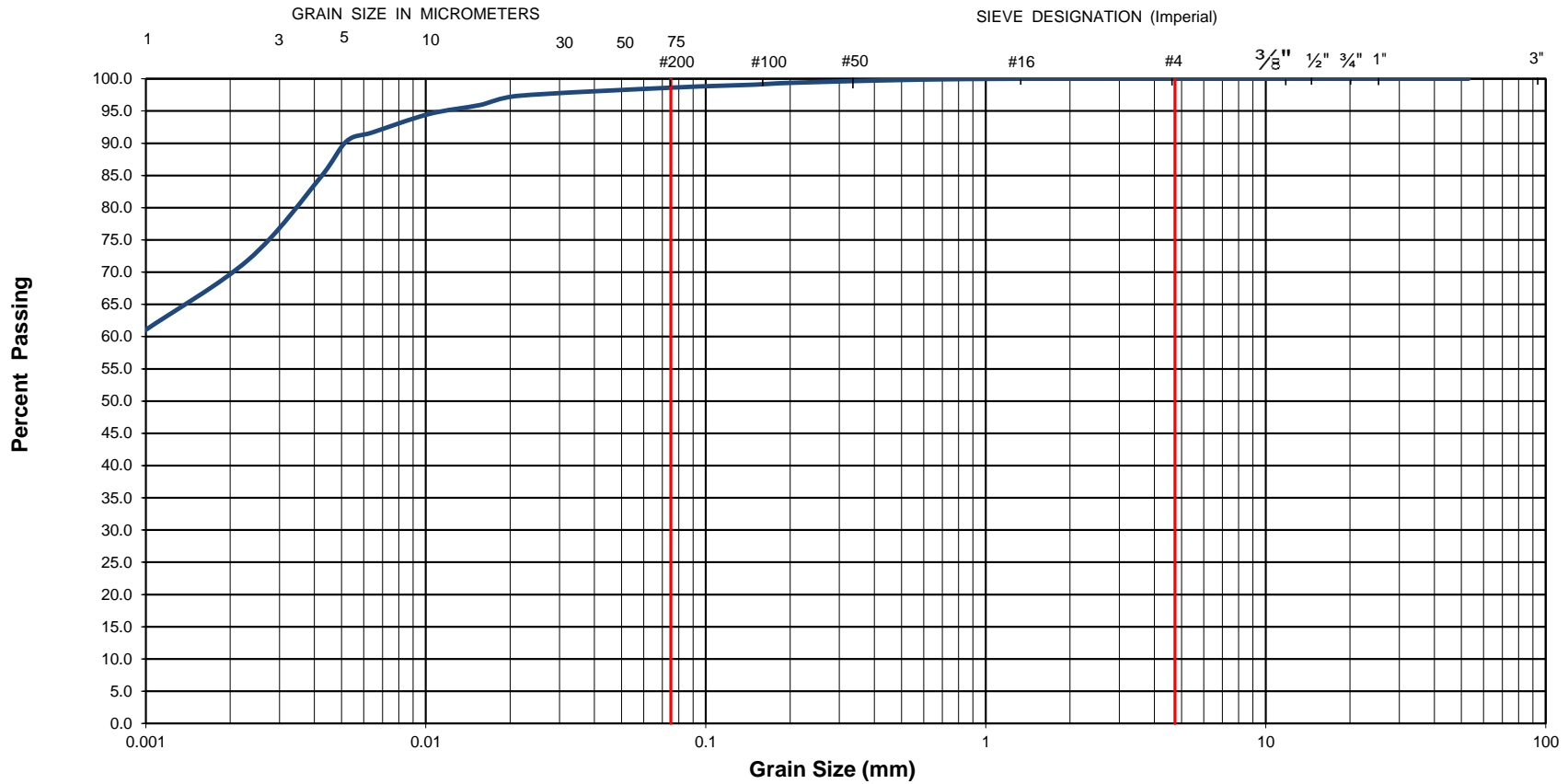


## Grain-Size Distribution Curve Method of Test For Particle Size Analysis of Soil ASTM C-136/ASTM D422

**EXP Services Inc.**  
100-2650 Queensview Drive  
Ottawa, ON K2B 8H6

### Unified Soil Classification System

<b>CLAY AND SILT</b>	<b>SAND</b>			<b>GRAVEL</b>	
	Fine	Medium	Coarse	Fine	Coarse



EXP Project No.:	OTT-22005690-A0	Project Name :	Proposed Addition to Residential Building		
Client :	Smart Living Properties	Project Location :	68 Sweetland Avenue, Ottawa, Ontario		
Date Sampled :	May 31, 2022	Borehole No:	BH 2	Sample No.: SS3	
Sample Description :	% Silt and Clay	99	% Sand	1	
Sample Description :			% Gravel	0	
Sample Description :	CLAY of High Plasticity (CH)			Figure :	6
Sample Description :					

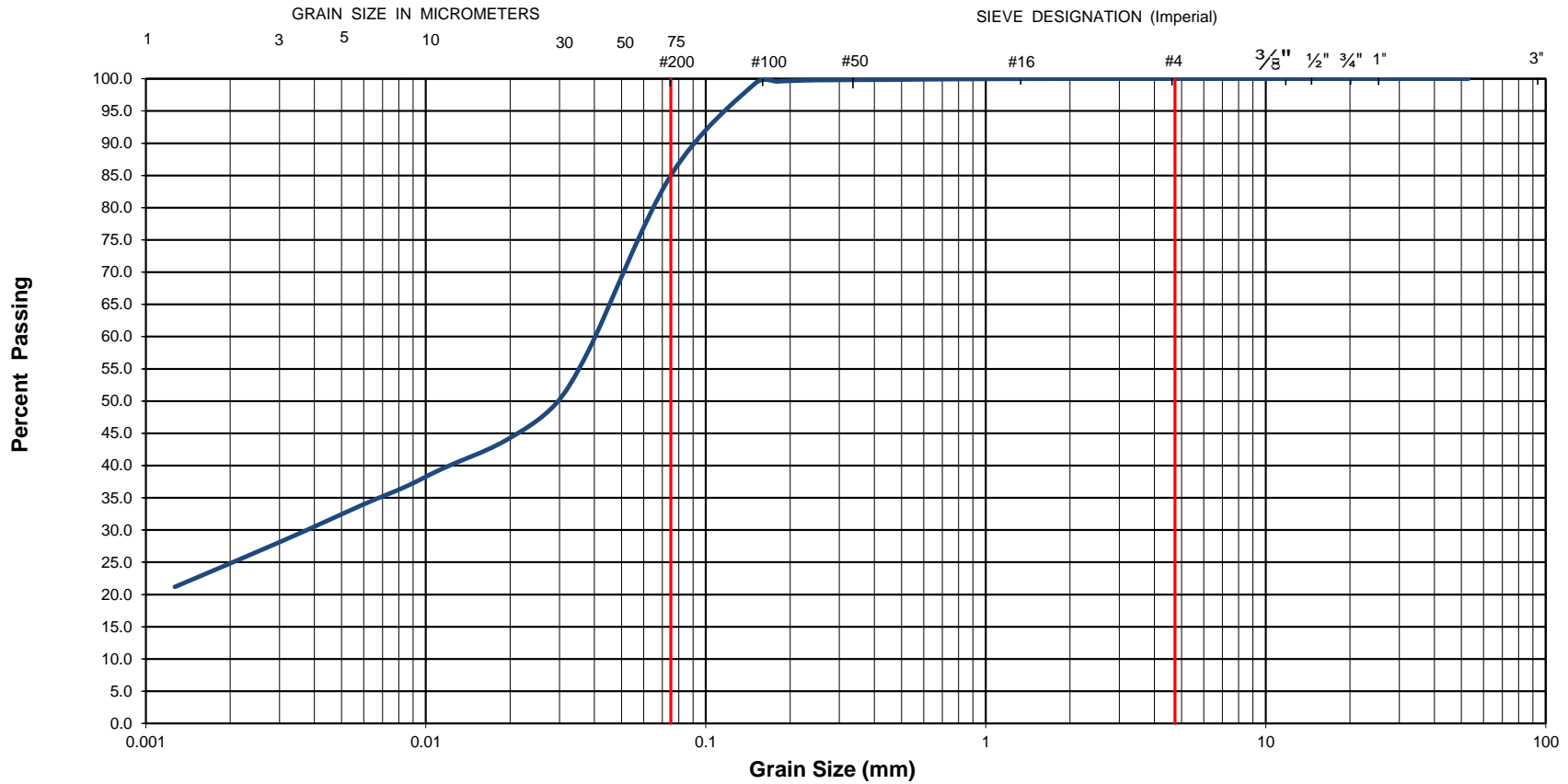


## Grain-Size Distribution Curve Method of Test For Particle Size Analysis of Soil ASTM C-136/ASTM D422

**EXP Services Inc.**  
100-2650 Queensview Drive  
Ottawa, ON K2B 8H6

### Unified Soil Classification System

<b>CLAY AND SILT</b>	<b>SAND</b>			<b>GRAVEL</b>	
	Fine	Medium	Coarse	Fine	Coarse



EXP Project No.:	OTT-22005690-A0	Project Name :	Proposed Addition to Residential Building				
Client :	Smart Living Properties	Project Location :	68 Sweetland Avenue, Ottawa, Ontario				
Date Sampled :	May 31, 2022	Borehole No:	BH 1	Sample No.:	SS7	Depth (m) :	7.6-8.2
Sample Description :	% Silt and Clay	85	% Sand	15	% Gravel	0	Figure : 7
Sample Description :	CLAYEY SILT with Sand (ML)						

EXP Services Inc.

*Smart Living Properties  
Geotechnical Investigation, Proposed Addition to Residential Building  
68 Sweetland Avenue, Ottawa, ON  
OTT-22005690-A0  
May 1, 2023*

# **Appendix A: Laboratory Certificate of Analysis**

**CLIENT NAME: EXP SERVICES INC**  
**2650 QUEENSVIEW DRIVE, UNIT 100**  
**OTTAWA, ON K2B8H6**  
**(613) 688-1899**

**ATTENTION TO: Matthew Zammit**  
**PROJECT: OTT-22005690-A0**  
**AGAT WORK ORDER: 22Z903265**

**SOIL ANALYSIS REVIEWED BY: Amanjot Bhela, Inorganic Lab Manager**  
**DATE REPORTED: Jun 10, 2022**  
**PAGES (INCLUDING COVER): 5**  
**VERSION\*: 1**

Should you require any information regarding this analysis please contact your client services representative at (905) 712-5100

\*Notes

*Disclaimer:*

- *All work conducted herein has been done using accepted standard protocols, and generally accepted practices and methods. AGAT test methods may incorporate modifications from the specified reference methods to improve performance.*
- *All samples will be disposed of within 30 days after receipt unless a Long Term Storage Agreement is signed and returned. Some specialty analysis may be exempt, please contact your Client Project Manager for details.*
- *AGAT's liability in connection with any delay, performance or non-performance of these services is only to the Client and does not extend to any other third party. Unless expressly agreed otherwise in writing, AGAT's liability is limited to the actual cost of the specific analysis or analyses included in the services.*
- *This Certificate shall not be reproduced except in full, without the written approval of the laboratory.*
- *The test results reported herewith relate only to the samples as received by the laboratory.*
- *Application of guidelines is provided "as is" without warranty of any kind, either expressed or implied, including, but not limited to, warranties of merchantability, fitness for a particular purpose, or non-infringement. AGAT assumes no responsibility for any errors or omissions in the guidelines contained in this document.*
- *All reportable information as specified by ISO/IEC 17025:2017 is available from AGAT Laboratories upon request.*



## Certificate of Analysis

AGAT WORK ORDER: 22Z903265

PROJECT: OTT-22005690-A0

5835 COOPERS AVENUE  
MISSISSAUGA, ONTARIO  
CANADA L4Z 1Y2  
TEL (905)712-5100  
FAX (905)712-5122  
<http://www.agatlabs.com>

CLIENT NAME: EXP SERVICES INC  
SAMPLING SITE: 146 Osgoode Street

ATTENTION TO: Matthew Zammit  
SAMPLED BY: EXP

### (Soil) Inorganic Chemistry

DATE RECEIVED: 2022-06-02

DATE REPORTED: 2022-06-10

		SAMPLE DESCRIPTION:		BH#2 SS4
		SAMPLE TYPE:		10'-12'
		DATE SAMPLED:		Soil
				2022-05-31
Parameter	Unit	G / S	RDL	3938610
Chloride (2:1)	µg/g		2	72
Sulphate (2:1)	µg/g		2	48
pH (2:1)	pH Units		NA	7.36

Comments: RDL - Reported Detection Limit; G / S - Guideline / Standard

**3938610** pH, Chloride and Sulphate were determined on the extract obtained from the 2:1 leaching procedure (2 parts DI water: 1 part soil). Resistivity is a calculated parameter.

Analysis performed at AGAT Toronto (unless marked by \*)

**Certified By:**



## Quality Assurance

**CLIENT NAME:** EXP SERVICES INC  
**PROJECT:** OTT-22005690-A0  
**SAMPLING SITE:** 146 Osgoode Street

**AGAT WORK ORDER:** 22Z903265  
**ATTENTION TO:** Matthew Zammit  
**SAMPLED BY:** EXP

Soil Analysis															
RPT Date: Jun 10, 2022			DUPLICATE				Method Blank	REFERENCE MATERIAL			METHOD BLANK SPIKE		MATRIX SPIKE		
PARAMETER	Batch	Sample Id	Dup #1	Dup #2	RPD	Measured Value		Acceptable Limits		Recovery	Acceptable Limits		Recovery	Acceptable Limits	
								Lower	Upper		Lower	Upper		Lower	Upper

**(Soil) Inorganic Chemistry**

Chloride (2:1)	3935532		85	86	1.2%	< 2	91%	70%	130%	99%	80%	120%	103%	70%	130%
Sulphate (2:1)	3935532		106	102	3.8%	< 2	98%	70%	130%	104%	80%	120%	99%	70%	130%
pH (2:1)	3935532		7.53	8.06	6.8%	NA	100%	80%	120%	NA			NA		

Comments: NA signifies Not Applicable.  
 pH duplicates QA acceptance criteria was met relative as stated in Table 5-15 of Analytical Protocol document.

Duplicate NA: results are under 5X the RDL and will not be calculated.

Certified By:






## Method Summary

CLIENT NAME: EXP SERVICES INC

AGAT WORK ORDER: 22Z903265

PROJECT: OTT-22005690-A0

ATTENTION TO: Matthew Zammit

SAMPLING SITE: 146 Osgoode Street

SAMPLED BY: EXP

PARAMETER	AGAT S.O.P	LITERATURE REFERENCE	ANALYTICAL TECHNIQUE
<b>Soil Analysis</b>			
Chloride (2:1)	INOR-93-6004	modified from SM 4110 B	ION CHROMATOGRAPH
Sulphate (2:1)	INOR-93-6004	modified from SM 4110 B	ION CHROMATOGRAPH
pH (2:1)	INOR 93-6031	modified from EPA 9045D and MCKEAGUE 3.11	PH METER



# AGAT Laboratories

Large

5835 Coopers Avenue  
Mississauga, Ontario L4Z 1Y2  
Ph: 905.712.5100 Fax: 905.712.5122  
webearth.agatlabs.com

## Laboratory Use Only

Work Order #: 177903265  
Cooler Quantity: n/a - 1 bag  
Arrival Temperatures: 23.6 | 23.9 | 23.5  
LT: 2.8  
Custody Seal Intact:  Yes  No  N/A  
Notes: Bagged ICE

## Chain of Custody Record

If this is a Drinking Water sample, please use Drinking Water Chain of Custody Form (potable water consumed by humans)

### Report Information:

Company: EXP Services Inc. Ottawa  
Contact: Matthew Zammit  
Address: 2650 Queensview Dr Unit 100  
Ottawa, ON, K2B 8H6  
Phone: 613-688-1899 Fax: \_\_\_\_\_  
Reports to be sent to:  
1. Email: matthew.zammit@exp.com  
2. Email: \_\_\_\_\_

### Regulatory Requirements:

(Please check all applicable boxes)

Regulation 153/04  Excess Soils R406  Sewer Use  
 Sanitary  Storm

Table Indicate One Table Indicate One  
 Ind/Com  Res/Park  Agriculture  Regulation 558  Prov. Water Quality Objectives (PWQO)  
 Other

Soil Texture (Check One)  Coarse  CCME  Other  
 Fine  Fine

Indicate One

### Turnaround Time (TAT) Required:

Regular TAT (Most Analysis)  5 to 7 Business Days  
Rush TAT (Rush Surcharges Apply)  
 3 Business Days  2 Business Days  Next Business Day  
OR Date Required (Rush Surcharges May Apply): \_\_\_\_\_

### Project Information:

Project: OTT - 2200 5690-A0  
Site Location: 146 Osgoode street  
EXP  
Sampled By: \_\_\_\_\_  
AGAT ID #: \_\_\_\_\_ PO: \_\_\_\_\_  
Please note: If quotation number is not provided, client will be billed full price for analysis.

### Is this submission for a Record of Site Condition?

Yes  No

### Report Guideline on Certificate of Analysis

Yes  No

Please provide prior notification for rush TAT  
\*TAT is exclusive of weekends and statutory holidays

For 'Same Day' analysis, please contact your AGAT CPM

### Invoice Information:

Bill To Same: Yes  No

Company: \_\_\_\_\_  
Contact: \_\_\_\_\_  
Address: \_\_\_\_\_  
Email: \_\_\_\_\_

### Sample Matrix Legend

**B** Biota  
**GW** Ground Water  
**O** Oil  
**P** Paint  
**S** Soil  
**SD** Sediment  
**SW** Surface Water

Field Filtered - Metals, Hg, CrVI, DOC	O. Reg 153	O. Reg 558	O. Reg 406	Potentially Hazardous or High Concentration (Y/N)
Metals & Inorganics	Metals - <input type="checkbox"/> CrVI, <input type="checkbox"/> Hg, <input type="checkbox"/> HWSB BTEX, F1-F4, PHCs Analyze F4G if required <input type="checkbox"/> Yes <input type="checkbox"/> No	Landfill Disposal Characterization TOLP: TCLP: <input type="checkbox"/> M&I, <input type="checkbox"/> VOCs, <input type="checkbox"/> ABNS, <input type="checkbox"/> B(a)P, <input type="checkbox"/> PCBs	Excess Soils SPLP Rainwater Leach SPLP: <input type="checkbox"/> Metals, <input type="checkbox"/> VOCs, <input type="checkbox"/> SVOCs Excess Soils Characterization Package pH, ICPIWS Metals, BTEX, F1-F4 Salt - EC/SAR	<u>pH</u> <u>Sulphate</u> <u>chloride</u> <u>resistivity</u>
PAHs				
Total PCBs				
VOC				
Aroclor				

Sample Identification	Date Sampled	Time Sampled	# of Containers	Sample Matrix	Comments/ Special Instructions	Y / N
<u>OH # 2 854 10-12'</u>	<u>May 3/22</u>	<u>AM</u>	<u>1</u>	<u>S</u>		
		<u>PM</u>				
		<u>AM</u>				
		<u>PM</u>				
		<u>AM</u>				
		<u>PM</u>				
		<u>AM</u>				
		<u>PM</u>				
		<u>AM</u>				
		<u>PM</u>				
		<u>AM</u>				
		<u>PM</u>				

Samples Relinquished By (Print Name and Sign): <u>Jeff MacMillan</u> <u>JM</u>	Date: <u>June 2/22</u> Time: <u>4:40</u>	Samples Received By (Print Name and Sign): <u>C. G. Smith</u>	Date: <u>JUN 02 2022</u> Time: <u>16h50</u>
Samples Relinquished By (Print Name and Sign): <u>CA to inspector</u>	Date: <u>JUN 03 2022</u> Time: <u>16h00</u>	Samples Received By (Print Name and Sign): <u>Arineet Minhas AM</u>	Date: <u>June 4/22</u> Time: <u>10:35am</u>
Page <u>1</u> of <u>1</u>			No: <u>T 122952</u>

EXP Services Inc.

*Smart Living Properties  
Geotechnical Investigation, Proposed Addition to Residential Building  
68 Sweetland Avenue, Ottawa, ON  
OTT-22005690-A0  
May 1, 2023*

## **Appendix B: Legal Notification**

EXP Services Inc.

*Smart Living Properties  
Geotechnical Investigation, Proposed Addition to Residential Building  
68 Sweetland Avenue, Ottawa, ON  
OTT-22005690-A0  
May 1, 2023*

## Legal Notification

This report was prepared by EXP Services Inc. (EXP) for the account of Smart Living Properties.

Any use which a third party makes of this report, or any reliance on or decisions to be made based on it, are the responsibility of such third parties. EXP accepts no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions based on this project.



## Report Distribution

Corey Kou <corey@smartlivingproperties.ca>;  
Jules Lauzon <jules@smartlivingproperties.ca>;  
Curtis Melanson <c.melanson@mcintoshperry.com>;  
Juan Gomez <gomez@woodmanarchitect.com>;  
Robert Woodman <bob@woodmanarchitect.com>;  
Ahmad Saltaji <ahmadsa@smartlivingproperties.ca>  
Jeremy Silburt <Jeremy@smartlivingproperties.ca>  
Haris Khan, Fotenn – khan@fotenn.com