ASSESSMENT OF ADEQUACY OF PUBLIC SERVICES 1047 RICHMOND ROAD



Project No.: CCO-22-2242

Prepared for:

Fengate 2275 Upper Middle Rd. E, Suite 700 Oakville, ON L6H 0C3

Prepared by:

McIntosh Perry Consulting Engineers Ltd. 115 Walgreen Road Carp, ON K0A 1L0

July 14, 2023

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1.0 PROJECT OVERVIEW

1.1 Purpose

McIntosh Perry (MP) has been retained by Fengate to prepare this Assessment of Adequacy of Public Services Report in support of the Zoning By-law Amendment (ZBLA) application process for the contemplated development at 1047 Richmond Road, within the City of Ottawa.

The main purpose of this report is to demonstrate that the proposed servicing and stormwater management design for the development follows the recommendations and guidelines provided by the City of Ottawa (City), the Rideau Valley Conservation Authority (RVCA), and the Ministry of the Environment, Conservation and Parks (MECP). This report will address access to water, sanitary and storm servicing for the site, ensuring that existing services will adequately service the proposed development.

1.2 Site Description



Figure 1: Site Map

The subject property, herein referred to as the site, is located at 1047 Richmond Road within the Bay Ward in the City of Ottawa. The site covers approximately 1.02 ha and is located at the north east corner of the Richmond Road and New Orchard Avenue North intersection. The site is zoned for Traditional Mainstreet use (TM[2494] H[25]). Additional details are included on the Site Location Plan included in Appendix 'A'.

1.3 Proposed Development and Statistics

The contemplated development consists of three residential buildings ranging from 6 to 40-storeys and park land to be dedicated to the City. The *Site Plan* proposes 1,152 residential units and 859 m^2 of retail space. Refer to *Site Plan* prepared by Arcadis and included in *Appendix B* for further details.

1.4 Existing Conditions and Infrastructure

The site is currently developed as a car dealership with asphalt parking areas. Based on available mapping, the existing building appears to be serviced by the municipal infrastructure within Richmond Road.

Sewer and watermain mapping collected from the City of Ottawa indicate that the following services exist across the property frontages within the adjacent municipal right-of-ways:

- Ambleside Drive
 - 203 mm diameter PVC watermain; and
 - 300 mm diameter concrete storm sewer, tributary to the Ottawa River.
- New Orchard Drive
 - 203/152 mm diameter cast iron watermain;
 - 300 mm diameter concrete sanitary sewer, tributary to the West Nepean Collector; and
 - 675 mm diameter concrete storm Sewer, tributary to the Ottawa River.
- North of 1071 Ambleside Drive
 - 1220 mm diameter concrete feedermain; and
 - 1350 mm diameter concrete sanitary West Nepean Collector sewer.

1.5 Approvals

The contemplated development is subject to the City of Ottawa zoning by-law amendment approval process.

The development will be subject to the City of Ottawa site plan control approval process. Site plan control requires the City to review, provided concurrence and approve the engineering design package. Permits to construct can be requested once the City has issued a site plan agreement.

An Environmental Compliance Approval (*ECA*) through the Ministry of Environment, Conservation and Parks (*MECP*) is not anticipated to be required for the development. The stormwater management system is anticipated to meet the exemption requirements under O.Reg 525/90 since the development is located within a single parcel, is not tributary to a combined sewer system, and does not propose industrial usage.

2.0 BACKROUND STUDIES, STANDARDS AND REFERENCES

2.1 Background Reports / Reference Information

As-built drawings of existing services, provided by the City of Ottawa Information centre, within the vicinity of the site were reviewed in order to identify infrastructure available to service the contemplated development.

2.2 Applicable Guidelines and Standards

City of Ottawa:

- Ottawa Sewer Design Guidelines, City of Ottawa, SDG002, October 2012. (Ottawa Sewer Guidelines)
 - Technical Bulletin ISTB-2014-01 City of Ottawa, February 2014. (ISTB-2014-01)
 - Technical Bulletin ISTB-2018-01 City of Ottawa, January 2018. (ISTB-2018-01)
 - Technical Bulletin ISTB-2018-03 City of Ottawa, March 2018. (ISTB-2018-03)
 - Technical Bulletin ISTB-2019-01 City of Ottawa, January 2019. (ISTB-2019-01)
 - Technical Bulletin ISTB-2019-02 City of Ottawa, February 2019. (ISTB-2019-02)
- Ottawa Design Guidelines Water Distribution City of Ottawa, July 2010. (Ottawa Water Guidelines)
 - Technical Bulletin ISD-2010-2 City of Ottawa, December 15, 2010. (ISD-2010-2)
 - Technical Bulletin ISDTB-2014-02 City of Ottawa, May 2014. (ISDTB-2014-02)
 - Technical Bulletin ISTB-2018-02 City of Ottawa, March 2018. (ISTB-2018-02)
 - Technical Bulletin ISTB-2021-03 City of Ottawa, August 2021. (ISTB-2021-03)
- Stormwater management Design Criteria for the Pinecrest Creek/Westboro Area, City of Ottawa, May 2020. (Pinecrest Creek Study)

Ministry of Environment, Conservation and Parks:

- ◆ Stormwater Planning and Design Manual, Ministry of the Environment, March 2003. (MECP Stormwater Design Manual)
- ◆ Design Guidelines for Sewage Works, Ministry of the Environment, 2008. (*MECP Sewer Design Guidelines*)

Other:

♦ Water Supply for Public Fire Protection, Fire Underwriters Survey, 2020. (FUS Guidelines)

3.0 PRE-CONSULTATION SUMMARY

A pre-consultation meeting was conducted on October 14th, 2021 regarding the contemplated development at 1047 Richmond Road. Specific design parameters to be incorporated within this design include the following.

- RCVA to confirm quality controls requirements.
- ◆ Any storm events greater than 5 year, up to 100 year, and including 100-year storm event must be detained on site.
- Post-development to be restricted to the 2-year storm event, based on a calculated time of concentration and the lesser of either the calculated predevelopment rational method coefficient or 0.50. Time of concentration must be equal to or greater than 10 minutes.
- Confirm sanitary capacity with City of Ottawa staff.

The notes from the City of Ottawa pre-consultation can be found in *Appendix B*.

4.0 WATERMAIN

4.1 Existing Watermain

The subject site is located within the 1W pressure zone, as shown by the Water Distribution figure located in *Appendix C*. The following subsections outline the water infrastructure that exists within Richmond Road and New Orchard Drive.

4.1.1 Richmond Road

There is an existing 203 mm diameter PVC watermain within Richmond Road. Based on City of Ottawa mapping, the existing building is currently serviced by this watermain. In addition, there is an existing fire hydrant fronting the site along Richmond Road.

4.1.2 New Orchard Drive

There is an existing 203 mm diameter PVC watermain within New Orchard Avenue N. Approximately 79 m north of Richmond Road, the municipal system transitions from a 203 mm diameter watermain to a 152 mm diameter watermain. The watermain stops short of the 1220 mm diameter transmission main at the north end of New Orchard Ave N. In addition, there are two existing fire hydrants fronting the site along New Orchard Ave N.

4.2 Proposed Watermain

In accordance with Section 4.3.1 of the *Ottawa Water Guidelines*, service areas with a basic day demand greater than 50 m³/day require a dual connection to the municipal system. A dual connection will be required to service the contemplated development, based on the site statistics provided by the *Site Plan*.

The Fire Underwriters Survey 2020 (FUS) method was utilized to estimate the required fire flow for the site. Fire flow requirements were calculated per City of Ottawa Technical Bulletin *ISTB-2018-02*. The following parameters were provided by the building architect:

- Type of construction Non-Combustible Construction
- Occupancy type Limited Combustibility
- ◆ Sprinkler Protection Fully Supervised Sprinkler

The results of the calculations yielded a required fire flow of 10,000 L/min (166.7 L/s) for Tower A, 12,000 L/min (200.0 L/s) for Tower B and 7,000 L/min (116.7 L/s) for Building C. The detailed calculations for the FUS can be found in *Appendix C*.

The water demands for the proposed building have been calculated to adhere to *Ottawa Water Guidelines* and can be found in *Appendix 'C'*. The results have been summarized below:

Table 1: Water Supply Design Criteria and Water Demands

Site Area	1.02 ha
Residential	280 L/day/person
Residential 1 Bedroom & Bachelor Apartment	1.4 person/unit
(615 Units)	
Residential 2 Bedroom Apartment	2.1 person/unit
(519 Units)	
Residential 3 Bedroom Apartment	3.1 person/unit
(18 Units)	
Commercial Space	28,000 L/gross ha/day
Average Day Demand (L/s)	6.58 L/s
Maximum Daily Demand (L/s)	16.38 L/s
Peak Hourly Demand (L/s)	35.98 L/s
Building A - FUS Fire Flow Requirement (L/s)	166.7 L/s (10,000 L/min)
Building B - FUS Fire Flow Requirement (L/s)	200.0 L/s (12,000 L/min)
Building C - FUS Fire Flow Requirement (L/s)	116.7 L/s (7,000 L/min)

The City provided the estimated water pressures at both for the average day scenario, peak hour scenario and the max day plus fire flow scenario for the demands indicated by the correspondence in *Appendix C*. The resulting pressures for the boundary conditions results are shown in Table 2, below.

Scenario	Proposed Demands (L/s)	Connection HGL (m H₂O)*/kPa				
Average Day Demand	6.58	51.2 / 502.3				
Maximum Daily + Fire Flow Demand	216.38	145.0 L/s available @ 20 PSI				
Peak Hourly Demand	35.98	42.2 / 414.0				
*Adjusted for an estimated ground elevation of 64.8m above the connection point.						

It is anticipated that the existing municipal water infrastructure will be able to service the development as the normal operating pressure range would be 414 kPa to 502 kPa and will not be less than 275 kPa (40 psi) or exceed 689 kPa (100 psi).

Based on boundary conditions provided by the City, the local watermain network is capable of providing 8,700 L/min at the minimum operating pressure of 140 kPa. In accordance with the FUS, the existing watermain network can provide the required fire flow to building C. Buildings A and B however, may require a combination of fire resistive construction methods, fire separations or upgrades to the municipal infrastructure to meet the required fire flow. It is anticipated that one or more of these options will be implemented at the detailed design stage.

The requirement for fire pumps and or booster pumps will be evaluated with the aid of the mechanical consultant at the detailed design stage.

To confirm the adequacy of hydrant coverage to protect the proposed development, public and private fire hydrants within 150 m of the proposed building were accounted for per *ISTB 2018-03 Appendix I*. As demonstrated by *Table 3*, below.

Table 3: Fire Protection Confirmation

Building	Fire Flow Demand (L/min.)	Fire Hydrant(s) within 75m	Fire Hydrant(s) within 150m	Combined Fire Flow (L/min.)	
1047 Richmond	10,000 L/min – FUS				
Road	12,000 L/min – FUS	4 public	1 public	26,600	
	7,000 L/min – FUS				

Based on City guidelines (*ISTB-2018-02*), it is anticipated that the existing municipal hydrants can provide adequate fire coverage to the contemplated development.

5.0 SANITARY DESIGN

5.1 Existing Sanitary Sewer

There is an existing 225 mm diameter sanitary sewer within Richmond Road and an existing 300 mm diameter sanitary sewer within New Orchard Drive available to service the site. Both sanitary sewers are tributary to the same outlet, the West Nepean Collector, at the north end of New Orchard Avenue N.

5.2 Proposed Sanitary Sewer

Table 4, below, summarizes the wastewater design criteria identified by the *Ottawa Sewer Guidelines*.

Table 4: Sanitary Design Criteria

Design Parameter	Value
Residential 1 Bedroom / Bachelor Apartment (615 Units)	1.4 persons/unit
Residential 2 Bedroom Apartment (519 Units)	2.1 persons/unit
Residential 3 Bedroom Apartment (18 Units)	3.1 persons/unit
Average Daily Demand	280 L/day/person
Commercial Space	2800 L/(1000m² /day)

It is anticipated that the contemplated development will be serviced by the 300 mm diameter sanitary sewer within New Orchard Drive.

Table 5, below, summarizes the estimated wastewater flow from the contemplated development. Refer to *Appendix D* for detailed calculations.

Table 5: Summary of Estimated Sanitary Flow

Design Parameter	Total Flow (L/S)
Total Estimated Average Dry Weather Flow	6.63
Total Estimated Peak Dry Weather Flow	20.12
Total Estimated Peak Wet Weather Flow	20.41

City staff were contacted on October 15th, 2020 to review contemplated wastewater flows from the site and advise if there were any downstream constraints. City staff confirmed on October 27th, 2020 that there were no concerns with the municipal system based on a contemplated flow of *22.77 L/s*. Revised site statistics were received after initial consultation, as demonstrated by *Table 5*, above.

Correspondence with City Staff is included in *Appendix D*.

6.0 STORM SEWER & STORMWATER MANAGEMENT DESIGN

6.1 Existing Storm Sewers

Stormwater runoff from the site is currently tributary to the Ottawa River within the Ottawa Central sub-watershed. The following subsections outline the storm infrastructure that exists within New Orchard Avenue N and Richmond Road.

6.1.1 New Orchard Avenue N

There is an existing 675 mm diameter storm sewer located within New Orchard Drive. The storm sewer slopes to the north and discharges directly into the Ottawa river approximately 300 m downstream.

6.1.2 Richmond Road

There is an existing 1050 mm diameter storm sewer located within Richmond Road. The storm sewer slopes to the west and connects to New Orchard Avenue N.

6.2 Proposed Storm Sewers

It is anticipated that runoff will be directed to the existing storm infrastructure at a restricted rate, as discussed in *Section 7.1*. It is anticipated that a combination of surface, subsurface, rooftop, and internal cistern storage will be required to meet the SWM criteria identified by the City of Ottawa. Further details on the storm sewer design to be provided for the Site Plan Control application.

7.0 STORMWATER MANAGEMENT

7.1 Design Criteria and Methodology

Stormwater management for the site will be maintained through positive drainage away from the contemplated building and towards the adjacent ROWs. The quantitative and qualitative properties of the storm runoff for both the pre- and post-development flows are further detailed below.

In summary, the following design criteria have been employed in developing the stormwater management design for the site as directed by the RVCA and City:

Quality Control

 Based on coordination with the RVCA, quality controls may not be required for the development if the grading is enhanced, and best management practices are incorporated. The RVCA will confirm this requirement when the Site Plan is reviewed as part of the Site Plan Control application.

Quantity Control

- Any storm events greater than 2 year, up to 100 year, and including 100-year storm event must be detained on site.
- Post-development to be restricted to the 2-year storm event, based on a calculated time of concentration and the lesser of either the calculated predevelopment rational method coefficient or 0.50. Time of concentration must be equal to or greater than 10 minutes.

7.2 Runoff Calculations

Runoff calculations presented in this report are derived using the Rational Method, given as:

$$Q = 2.78CIA$$
 (L/s)

Where: C = Runoff coefficient

I = Rainfall intensity in mm/hr (City of Ottawa IDF curves)

A = Drainage area in hectares

It is recognized that the Rational Method tends to overestimate runoff rates. As a result, the conservative calculation of runoff ensures that any stormwater management facility sized using this method is anticipated to function as intended.

The following coefficients were used to develop an average C for each area:

Roofs/Concrete/Asphalt	0.90
Undeveloped and Grass	0.20

As per the *Ottawa Sewer Guidelines*, the 2 or 5-year balanced 'C' value must be increased by 25% for a 100-year storm event to a maximum of 1.0.

7.3 Site Drainage

Based on the criteria listed in *Section 7.1*, the contemplated development will be required to restrict flow to the 2-year storm event. It is estimated that the target release rate during the 100-year event will be 108.60 L/s.

It has been assumed that the existing development contained no stormwater management controls for flow attenuation. The estimated pre-development peak flows for the 2, 5, and 100-year events are summarized below in *Table 6*.

Table 6: Pre-Development Runoff Summary

Drainaga	Aroo		Q (L/s)	
Drainage Area	Area (ha)	2-Year	5-Year	100-Year
A1	1.02	195.63	265.38	505.33

To meet the stormwater objectives the contemplated development may contain a combination of flow attenuation including surface and subsurface storage as well as building storage via an internal cistern and rooftops.

The following storage requirement estimate assumes that approximately 10% of the development area will be directed to the outlet without flow attenuation. The estimated post-development peak flows for the 2, 5 and 100-year events and the required storage volumes are summarized below in *Table 7*, below.

Table 7: Post Development Flow Rate and Storage Requirements

Drainage	Unrestricted Flow (L/S)		Restricted Flow (L/S)		Stora	ge Requir	red (m³)		
Area	2-year	5-year	100-Year	2-year	5-Year	100-Year	2-year	5-Year	100-Year
B1 (Restricted)	161.48	219.06	454.80	20.92	28.38	58.92	115.80	154.9	318.1
B2 (Unrestricted)	17.10	23.19	49.68	17.10	23.19	49.68			
Total	178.58	242.26	504.48	38.02	51.57	108.60			

It is anticipated that approximately 318 m³ of storage will be required on site to attenuate flow to the established release rate of 108.60 L/s. Flow and storage calculations can be found within Appendix G. Actual storage volumes will need to be confirmed at the detailed design stage based on a number of factors including site imperviousness and grading constraints.

8.0 SUMMARY

- Development including three residential ranging from 6 to 40-storeys and park land to be dedicated to the City is contemplated at 1047 Richmond Road;
- The FUS method estimated a maximum fire flow of 12,000 L/min is required for the contemplated development;
- The development is anticipated to have a peak wet weather flow of 20.41 L/s. Based on coordination with City staff, it is anticipated that the municipal system can accommodate the wastewater flow;
- Based on City of Ottawa guidelines, the development will be required to attenuate post-development 2, 5 and 100-year flows to the pre-development 2-year release rate of 108.60 L/s:
- To meet the stormwater objectives the contemplated development may contain a
 combination of flow attenuation including surface and subsurface storage as well as
 building storage via an internal cistern and rooftops. It is anticipated that
 approximately 318 m³ of onsite storage will be required to attenuate flow to the
 established release rate. Actual storage volumes will need to be confirmed at the
 detailed design stage based on a number of factors including site imperviousness and
 grading constraints;
- Based on coordination with the RVCA, quality controls may not be required for the
 development if the grading is enhanced, and best management practices are
 incorporated. The RVCA will confirm this requirement when the Site Plan is reviewed
 as part of the Site Plan Control application.

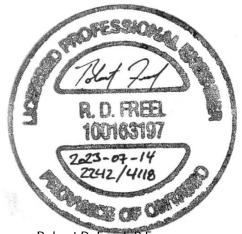
9.0 RECOMMENDATION

Based on the information presented in this report, we recommend that City of Ottawa approve this Assessment of Adequacy of Public Services in support of the proposed rezoning for 1047 Richmond Road.

This report is respectfully being submitted for approval.

Regards,

McIntosh Perry Consulting Engineers Ltd.



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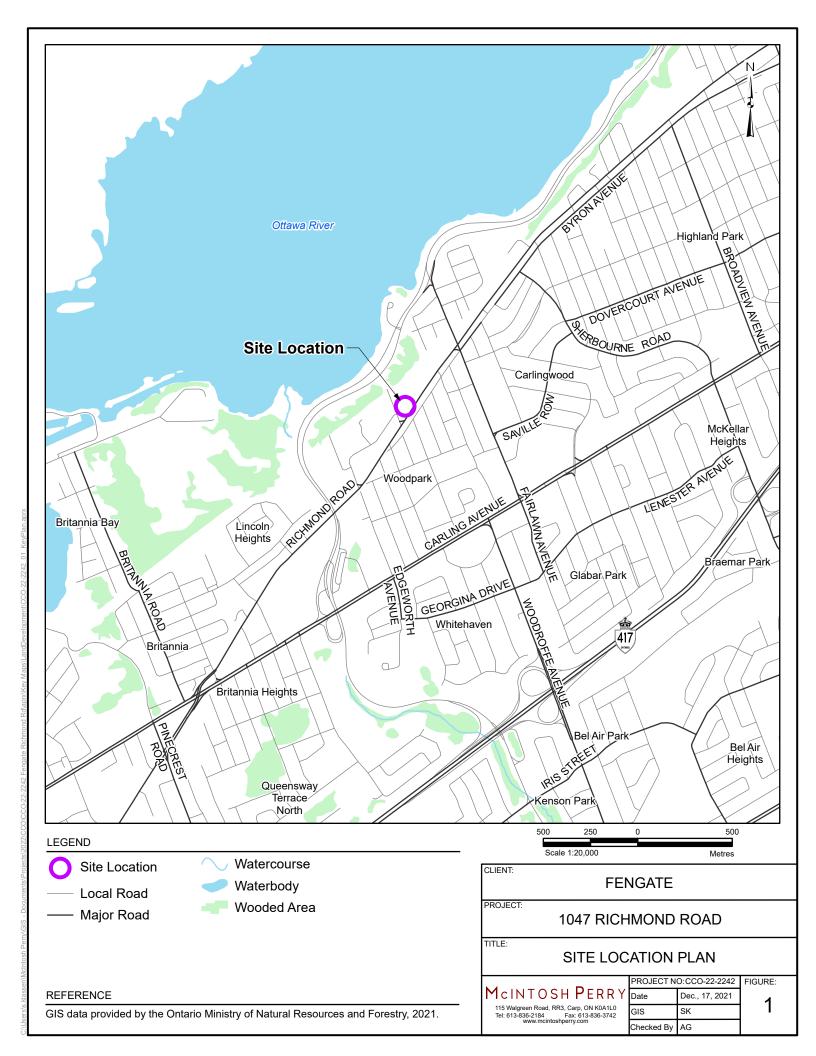
10.0 STATEMENT OF LIMITATIONS

This report was produced for the exclusive use of <u>Fengate</u>. The purpose of the report is to assess the existing stormwater management system and provide recommendations and designs for the post-construction scenario that are in compliance with the guidelines and standards from the Ministry of the Environment, Parks and Climate Change, City of Ottawa and local approval agencies. McIntosh Perry reviewed the site information and background documents listed in Section 2.0 of this report. While the previous data was reviewed by McIntosh Perry and site visits were performed, no field verification/measures of any information were conducted.

Any use of this review by a third party, or any reliance on decisions made based on it, without a reliance report is the responsibility of such third parties. McIntosh Perry accepts no responsibility for damages, if any, suffered by any third party as a result of decisions or actions made based on this review.

The findings, conclusions and/or recommendations of this report are only valid as of the date of this report. No assurance is made regarding any changes in conditions subsequent to this date. If additional information is discovered or becomes available at a future date, McIntosh Perry should be requested to re-evaluate the conclusions presented in this report, and provide amendments, if required.

APPENDIX A KEY PLAN



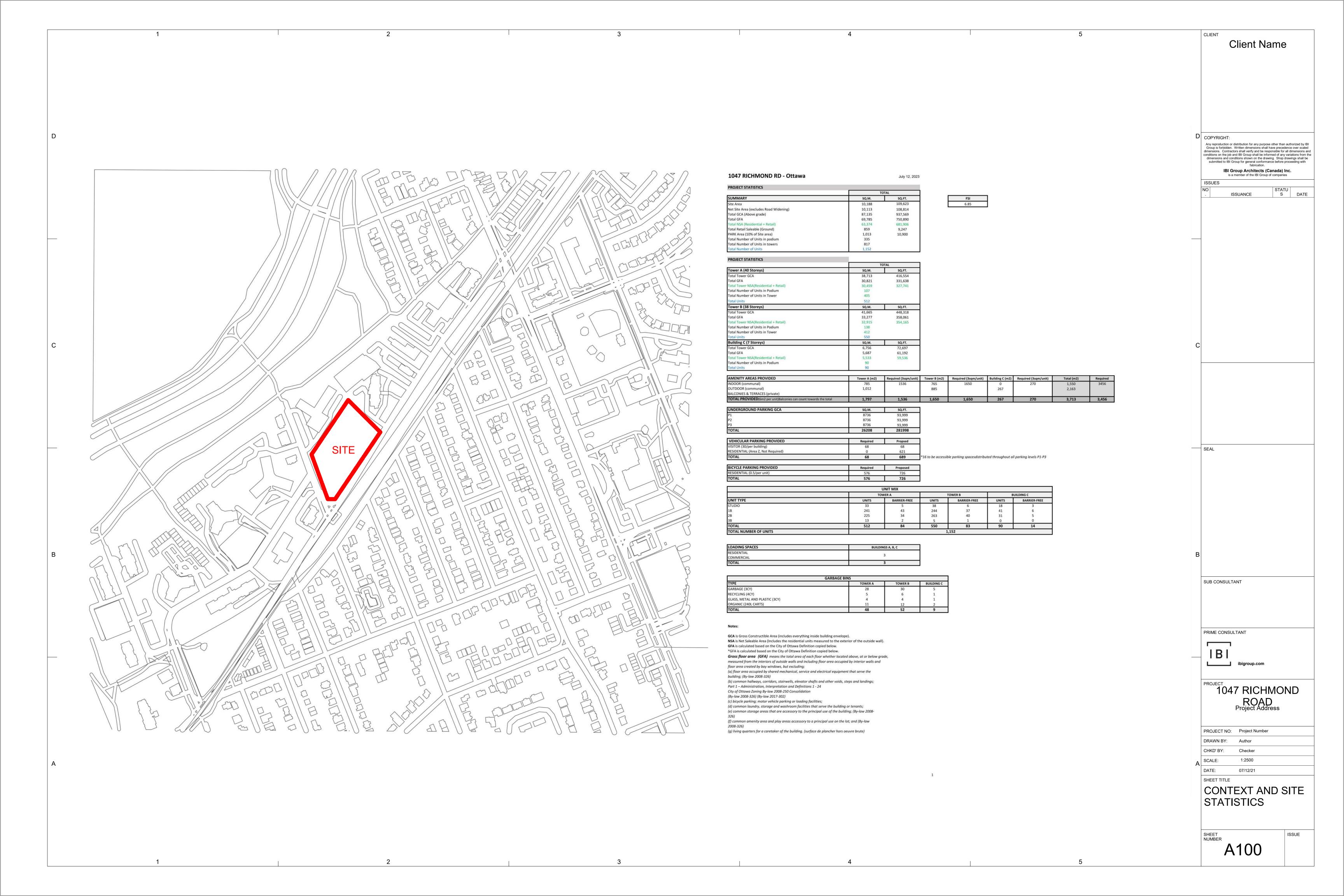
APPENDIX B BACKGROUND DOCUMENTS

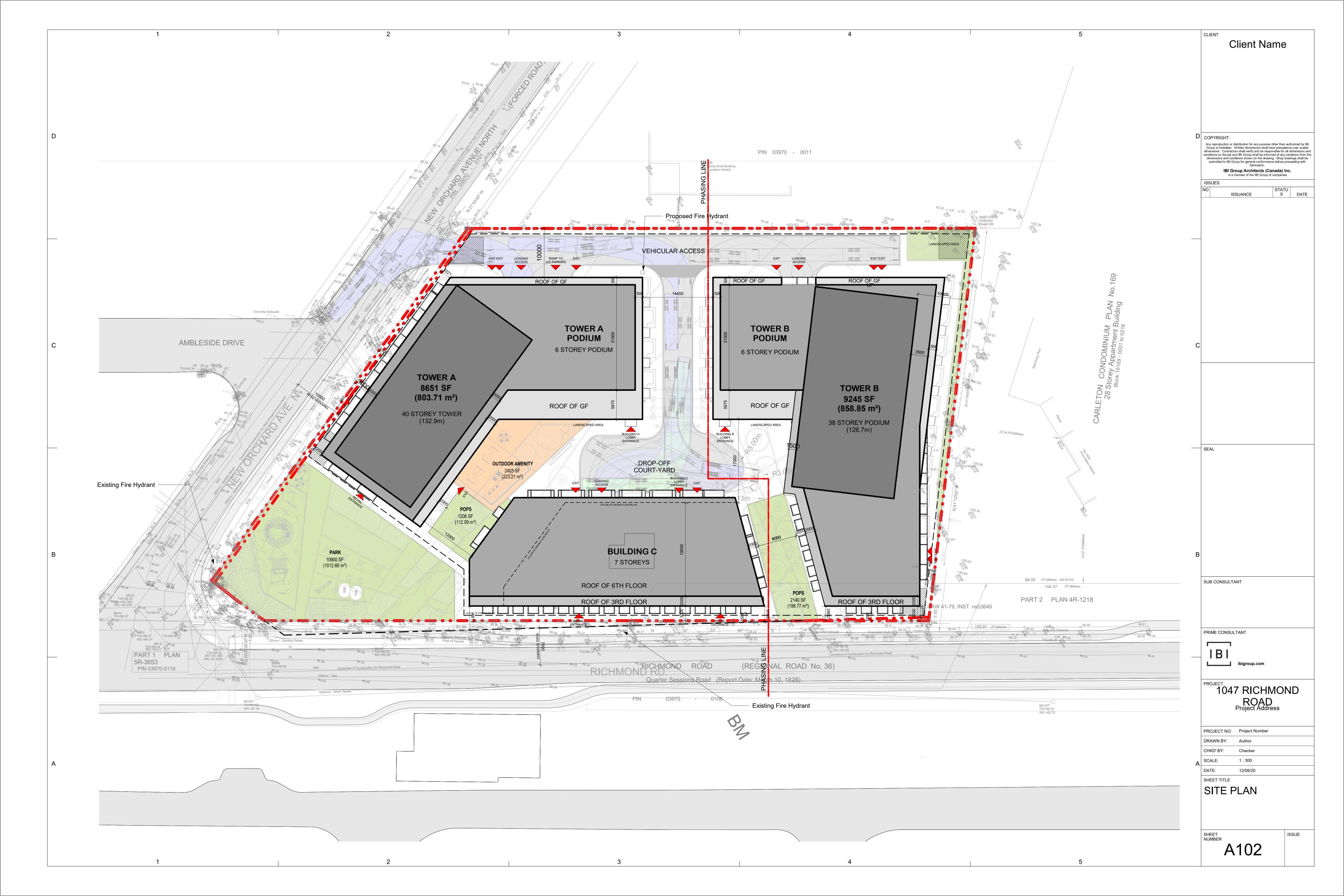
- The Servicing Study Guidelines for Development Applications are available at the following link: https://ottawa.ca/en/city-hall/planning-and-development-information-developers/development-application-review-process/development-application-submission/guide-preparing-studies-and-plans
- Record drawings and utility plans are available for purchase from the City's Information Centre. Contact the City's Information Centre by email at informationcentre@ottawa.ca or by phone at (613) 580-2424 x44455
- Stormwater quantity control criteria Control the 100-yr to the 2-yr allowable release rate using on site SWM. The allowable release rate is to be determined using the lesser of c=0.5 or existing. Tc is to be computed but not less than 10 minutes.
- As for the sanitary, the pipe on New Orchard is only 300 mm. Therefore, please
 provide the sanitary flow estimate from this site to determine if there is capacity
 available for this existing pipe or if the pipe needs to be upgraded. Note that west
 Nepean Collector is only 100 m away, so it would not be difficult to upgrade the
 pipe if required.
- Existing 203 mm dia. watermain is available on New Orchard Ave. N. for service connection.
- Looping may be required depends on the water demand.
- Stormwater quality control Consult with the Conservation Authority (RVCA) for their requirements. Include the correspondence with RVCA in the stormwater/site servicing report.
- Please note that as per Technical Bulletin PIEDTB-2016-01 section 8.3.11.1
 (p.12 of 14) there shall be no surface ponding on private parking areas during the
 2-year storm rainfall event. Depending on the SWM strategy proposed
 underground or additional underground storage may be required to satisfy this
 requirement.
- Please note that the minimum orifice dia. for a plug style ICD is 83mm and the minimum flow rate from a vortex ICD is 6 L/s in order to reduce the likelihood of plugging.
- Please provide an Existing Conditions/Removals Plan as part of the engineering drawing set. Any existing services are to be removed or abandoned in accordance with City standards.
- As per the City of Ottawa Slope Stability Guidelines for Development Applications an engineering report is required for any retaining walls proposed 1.0 m or greater in height within the subject site that addresses the global stability of the wall and provides structural details. A Retaining Wall Stability Analysis Report and Retaining Wall Structural Details are required to be provided from a Professional Engineer licensed in the Province of Ontario that demonstrates the proposed retaining wall structure has been assessed for global instability as per City standards. Please ensure the analysis and required documentation are provided as part of the submission to address this comment.
- Emergency routes will need to be satisfactory to Fire Services. Please show fire routes on the site plan. For information regarding fire route provisions, please

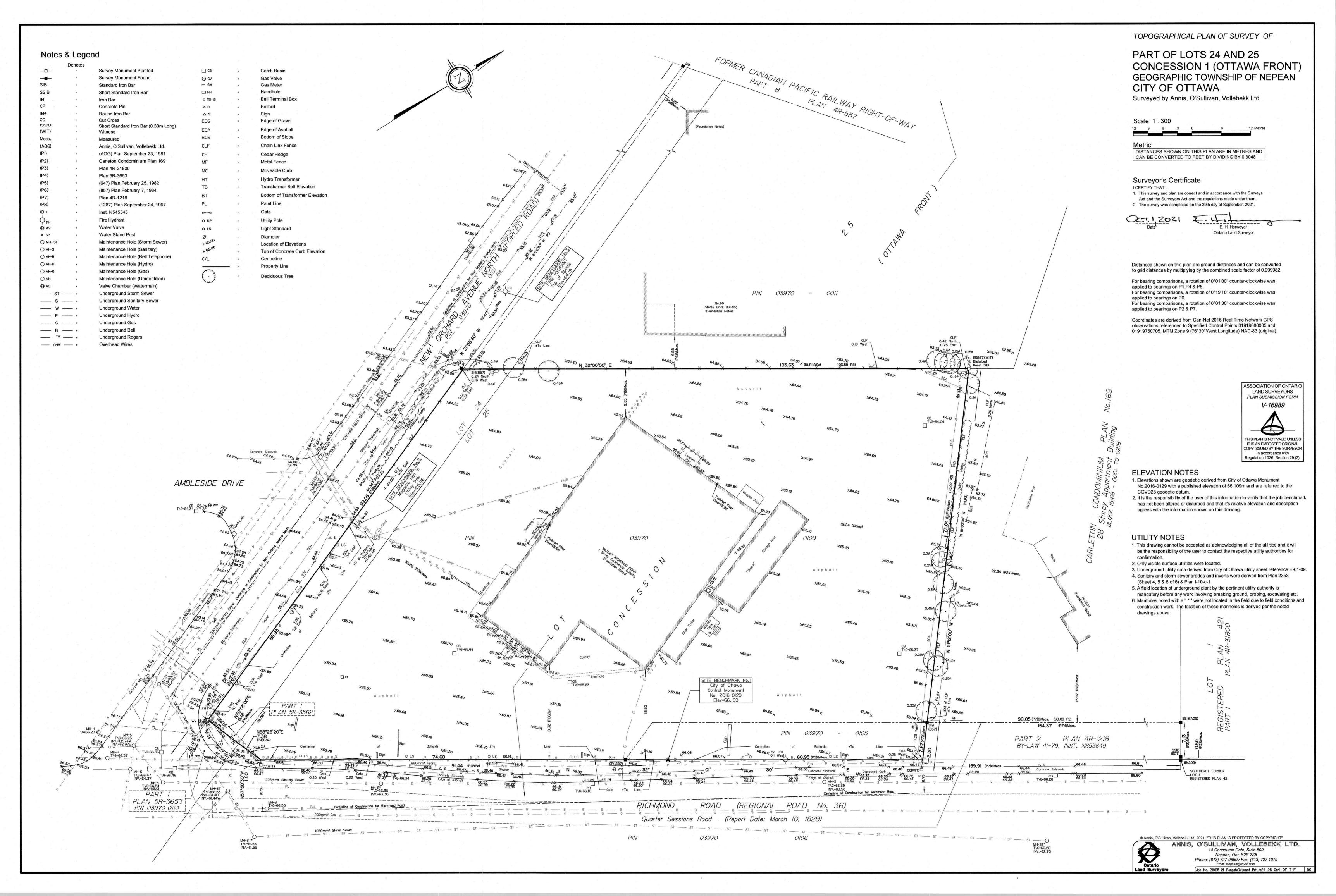
consult with Kevin Heiss at kevin.heiss@ottawa.ca.

- Clearly show and label the property lines on all sides of the property.
- Clearly show and label all the easements (if any) on the property, on all plans.
- When calculating the post development composite runoff coefficient (C), please provide a drawing showing the individual drainage area and its runoff coefficient.
- When using the modified rational method to calculate the storage requirements for the site, the underground storage should not be included in the overall available storage. The modified rational method assumes that the restricted flow rate is constant throughout the storm which, in this case, underestimates the storage requirement prior to the 1:100-year head elevation being reached. Alternately, if you wish to include the underground storage, you may use an assumed average release rate equal to 50% of the peak allowable rate. Otherwise, disregard the underground storage as available storage or provide modeling to support the design.
- Engineering plans are to be submitted on standard A1 size (594mm x 841mm) sheets.
- Phase 1 ESA and Phase 2 ESA must conform to clause 4.8.4 of the Official Plan that requires that development applications conform to Ontario Regulation 153/04.
- Provide the following information for water main boundary conditions:
 - 1. Location map with water service connection location(s).
 - 2. Average daily demand (I/s).
 - 3. Maximum daily demand (I/s).
 - 4. Maximum hourly demand (I/s).
 - 5. Fire flow demand (provide detailed fire flow calculations based on Fire Underwriters survey (FUS) Water Supply for Public Fire Protection). Exposure separation distances shall be defined on a figure to support the FUS calculation and required fire flow (RFF).
 - Hydrant capacity shall be assessed to demonstrate the RFF can be achieved. Please identify which hydrants are being considered to meet the RFF on a fire hydrant coverage plan as part of the boundary conditions request.
- If you are proposing any exterior light fixtures, all must be included and approved as part of the site plan approval. Therefore, the lights must be clearly identified by make, model and part number. All external light fixtures must meet the criteria for full cut-off classification as recognized by the Illuminating Engineering Society of North America (IESNA or IES), and must result in minimal light spillage onto adjacent properties (as a guideline, 0.5 fc is normally the maximum allowable spillage). In order to satisfy these criteria, the applicant must provide certification from an

- acceptable professional engineer. The location of all exterior fixtures, a table showing the fixture types (including make, model, part number), and the mounting heights must be included on a plan.
- As per Ottawa Sewer Design Guideline section 4.4.4.7, a monitoring maintenance hole shall be required just inside the property line for all nonresidential and multi residential buildings connections from a private sewer to a public sewer. See the sewer use By-law 2003-514(14) monitoring devices for details.







APPENDIX C WATERMAIN CALCULATIONS

CCO-22-2242 - 1047 Richmond Road - Water Demands - Total

 Project:
 1047 Richmond Road

 Project No.:
 CCO-22-2242

 Designed By:
 RP

Checked By: RF

Date: July 14, 2023

Site Area: 1.02 gross ha

Residential NUMBER OF UNITS UNIT RATE

89 units **Bachelor Apartment** 1.4 persons/unit 1 Bedroom Apartment 526 units 1.4 persons/unit 2 Bedroom Apartment 519 units 2.1 persons/unit 3 Bedroom Apartment 18 units 3.1 persons/unit

Total Population 2007 persons

 Commercial
 2409 m2

 Industrial - Light
 m2

 Industrial - Heavy
 m2

AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	
Residential	280	L/c/d	
Industrial - Light	35,000	L/gross ha/d	
Industrial - Heavy	55,000	L/gross ha/d	
Shopping Centres	2,500	L/(1000m² /d	
Hospital	900	L/(bed/day)	
Schools	70	L/(Student/d)	
Trailer Park with no Hook-Ups	340	L/(space/d)	
Trailer Park with Hook-Ups	800	L/(space/d)	
Campgrounds	225	L/(campsite/d)	
Mobile Home Parks	1,000	L/(Space/d)	
Motels	150	L/(bed-space/d)	
Hotels	225	L/(bed-space/d)	
Tourist Commercial	28,000	L/gross ha/d	
Other Commercial	28,000	L/gross ha/d	
	Residential	6.50	L/s
AVERAGE DAILY DEMAND	Commerical/Industrial		
	/Institutional	0.08	L/s

MAXIMUM DAILY DEMAND

DEMAND TYPE	Į.	AMOUNT	UNITS	
Residential	2.5	x avg. day	L/c/d	
Industrial	Industrial 1.5 x avg. day [L/gross ha/d	
Commercial	cial 1.5 x avg. day		L/gross ha/d	
Institutional	1.5	x avg. day	L/gross ha/d	
	Residential	16.26	L/s	
MAXIMUM DAILY DEMAND	Commerical/Industrial			
	/Institutional	0.12	L/s	

MAXIMUM HOUR DEMAND

DEMAND TYPE	Į.	AMOUNT	UNITS	
Residential	2.2	x max. day	L/c/d	
Industrial	1.8	x max. day	L/gross ha/d	
Commercial	Commercial 1.8		L/gross ha/d	
Institutional	1.8	x max. day	L/gross ha/d	
	Residential	35.77	L/s	
MAXIMUM HOUR DEMAND	Commerical/Industrial			
	/Institutional	0.21	L/s	

WATER DEMAND DESIGN FLOWS PER UNIT COUNT CITY OF OTTAWA - WATER DISTRIBUTION GUIDELINES, JULY 2010

AVERAGE DAILY DEMAND	6.58	L/s
MAXIMUM DAILY DEMAND	16.38	L/s
MAXIMUM HOUR DEMAND	35.98	L/s

CCO-22-2242 - 1047 Richmond Road - Fire Underwriters Survey - Building A

 Project:
 1047 Richmond Road

 Project No.:
 CCO-22-2242

 Designed By:
 RP

 Checked By:
 RF

 Date:
 July 14, 2023

From the Fire Underwriters Survey (2020)

From Part II – Guide for Determination of Required Fire Flow Copyright I.S.O.: City of Ottawa Technical Bulletin ISTB-2018-02 Applied Where Applicable

A. BASE REQUIREMENT (Rounded to the nearest 1000 L/min)

F = 220 x C x √A Where:

F = Required fire flow in liters per minute

C = Coefficient related to the type of construction.

A = The total floor area in square meters (Two largest addjoining floor areas plus 50% of all floors immediately above them up to a maximum of right) in the building being considered.

Construction Type Non-Combustible Construction

40 Storey Building

C 0.8 Gross Floor Area $37,760.8 \text{ m}^2$

Levels 1-7 = 1739.2 m² Per Floor Levels 7-40 = 803.7 m² Per Floor

A Total Effective Floor Area (per the 2020 FUS Page 22) 7,760.5 m

*Unprotected Vertical Openings

Calculated Fire Flow

15,504.5 L/min 16,000.0 L/min

B. REDUCTION FOR OCCUPANCY TYPE (No Rounding) From Page 24 of the Fire Underwriters Survey:

Limited Combustible

Fire Flow

C. REDUCTION FOR SPRINKLER TYPE (No Rounding)

Fully Supervised Sprinklered

-50%

-15%

R	eduction			-6,800.0) L/min		
D. INCR	EASE FOR EXPOSURE (No Roundi	ng)					
	Separation Distance (m)	Cons.of Exposed Wall	Length Exposed Adjacent Wall (m)	Height (Stories)	5 5		
Exposure 1	10.1 to 20	Fire Resistive - Non Combustible (Unprotected Openings)	31	2	62.0	6%	
Exposure 2	10.1 to 20	Fire Resistive - Non Combustible (Unprotected Openings)	42	6	252.0	8%	
Exposure 3	10.1 to 20	Fire Resistive - Non Combustible (Unprotected Openings)	21	38	798.0	8%	
Exposure 4	Over 30 m	Fire Resistive - Non Combustible (Unprotected Openings)	10	4	40.0	0%	
					% Increase*	22%	

Increase* 2,992.0 L/min

E. Total Fire Flow (Rounded to the Nearest 1000 L/min)

Fire Flow 9,792.0 L/min
Fire Flow Required** 10,000.0 L/min

 $^{^*\}mbox{In}$ accordance with Part II, Section 4, the Increase for separation distance is not to exceed 75%

 $^{^{\}star\star}\text{In accordance with Section 4 the Fire flow is not to exceed 45,000 L/min or be less than 2,000 L/min}$

CCO-22-2242 - 1047 Richmond Road - Fire Underwriters Survey - Building B

 Project:
 1047 Richmond Road

 Project No.:
 CCO-22-2242

 Designed By:
 RP

 Checked By:
 RF

 Date:
 July 14, 2023

From the Fire Underwriters Survey (2020)

From Part II – Guide for Determination of Required Fire Flow Copyright I.S.O.: City of Ottawa Technical Bulletin ISTB-2018-02 Applied Where Applicable

Α

A. BASE REQUIREMENT (Rounded to the nearest 1000 L/min)

F = 220 x C x √A Where:

F = Required fire flow in liters per minute

C = Coefficient related to the type of construction.

A = The total floor area in square meters (Two largest addjoining floor areas plus 50% of all floors immediately above them up to a maximum of right) in the building being considered.

Construction Type Non-Combustible Construction

38 Storey Building

C 0.8 Gross Floor Area 39,820.0 $\,\mathrm{m}^2$

Levels 1-7 = $2034.0 \text{ m}^2 \text{ Per Floor}$ Levels 7 - $38 = 863.0 \text{ m}^2 \text{ Per Floor}$

Total Effective Floor Area (per the 2020 FUS Page 22) 8,999.0 m²

*Unprotected Vertical Openings

Calculated Fire Flow 16,695.9 L/min 17,000.0 L/min

B. REDUCTION FOR OCCUPANCY TYPE (No Rounding)
From Page 24 of the Fire Underwriters Survey:

Limited Combustible -15%

Fire Flow 14 450 0 L/min

C. REDUCTION FOR SPRINKLER TYPE (No Rounding)

Fully Supervised Sprinklered -50%

Reduction			-7,225.0 L/min				
D. INCR	EASE FOR EXPOSURE (No Roundin	ng)					
	Separation Distance (m)	Cons.of Exposed Wall	Length Exposed Adjacent Wall (m)	Height (Stories)	5 5		
Exposure 1	10.1 to 20	Fire Resistive - Non Combustible (Unprotected Openings)	55	2	110.0	8%	
Exposure 2	10.1 to 20	Fire Resistive - Non Combustible (Unprotected Openings)	30	28	840.0	8%	
Exposure 3	10.1 to 20	Fire Resistive - Non Combustible (Unprotected Openings)	20	6	120.0	8%	
Exposure 4	10.1 to 20	Fire Resistive - Non Combustible (Unprotected Openings)	20	40	800.0	8%	
	_	_	<u> </u>		% Increase*	32%	

Increase* 4,624.0 L/min

E. Total Fire Flow (Rounded to the Nearest 1000 L/min)

Fire Flow 11,849.0 L/min
Fire Flow Required** 12,000.0 L/min

 $^{^*\}mbox{In}$ accordance with Part II, Section 4, the Increase for separation distance is not to exceed 75%

 $^{^{\}star\star}\text{In accordance with Section 4 the Fire flow is not to exceed 45,000 L/min or be less than 2,000 L/min}$

CCO-22-2242 - 1047 Richmond Road - Fire Underwriters Survey - Building C

Project: 1047 Richmond Road Project No.: CCO-22-2242 Designed By: Checked By: July 14, 2023

From the Fire Underwriters Survey (2020)

Date:

From Part II – Guide for Determination of Required Fire Flow Copyright I.S.O.: City of Ottawa Technical Bulletin ISTB-2018-02 Applied Where Applicable

С

A. BASE REQUIREMENT (Rounded to the nearest 1000 L/min)

F = 220 x C x vA Where:

Calculated Fire Flow

F = Required fire flow in liters per minute

C = Coefficient related to the type of construction.

 $A = The\ total\ floor\ area\ in\ square\ meters\ (Two\ largest\ addjoining\ floor\ areas\ plus\ 50\%\ of\ all\ floors\ immediately\ above\ them\ up\ to\ a$ $maximum\ of\ right)\ in\ the\ building\ being\ considered.$

Construction Type Non-Combustible Construction

6 Storey Building

6,576.3 m²

11,591.4 L/min 12,000.0 L/min

10,200.0 L/min

Gross Floor Area 0.8

Levels 2-3 = 1209.3 m² Per Floor Levels 4-6 = 1089.4 m² Per Floor

4,337.6 m² Total Effective Floor Area (per the 2020 FUS Page 22)

*Unprotected Vertical Openings

Levels 1 = 889.5 m² Per Floor

B. REDUCTION FOR OCCUPANCY TYPE (No Rounding) From Page 24 of the Fire Underwriters Survey:

Limited Combustible

-15%

Fire Flow

C. REDUCTION FOR SPRINKLER TYPE (No Rounding)

Fully Supervised Sprinklered

-50%

R	eduction			-5,100.0) L/min		
D. INCR	EASE FOR EXPOSURE (No Roundi	ng)					
	Separation Distance (m)	Cons.of Exposed Wall	Length Exposed Adjacent Wall (m)	Height (Stories)	5 5		
Exposure 1	10.1 to 20	Fire Resistive - Non Combustible (Unprotected Openings)	43	40	1720.0	8%	
Exposure 2	10.1 to 20	Fire Resistive - Non Combustible (Unprotected Openings)	25	38	950.0	8%	
Exposure 3	Over 30 m	Fire Resistive - Non Combustible (Unprotected Openings)	15	2	30.0	0%	
Exposure 4	Over 30 m	Fire Resistive - Non Combustible (Unprotected Openings)	20	24	480.0	0%	
					% Increase*	16%	

1,632.0 L/min

E. Total Fire Flow (Rounded to the Nearest 1000 L/min)

Fire Flow Fire Flow Required**

^{*}In accordance with Part II, Section 4, the Increase for separation distance is not to exceed 75%

^{**}In accordance with Section 4 the Fire flow is not to exceed 45,000 L/min or be less than 2,000 L/min

CCO-22-2242 - 1047 Richmond Road - Boundary Condition Unit Conversion

Project: 1047 Richmond Road

Project No.: CCO-22-2242

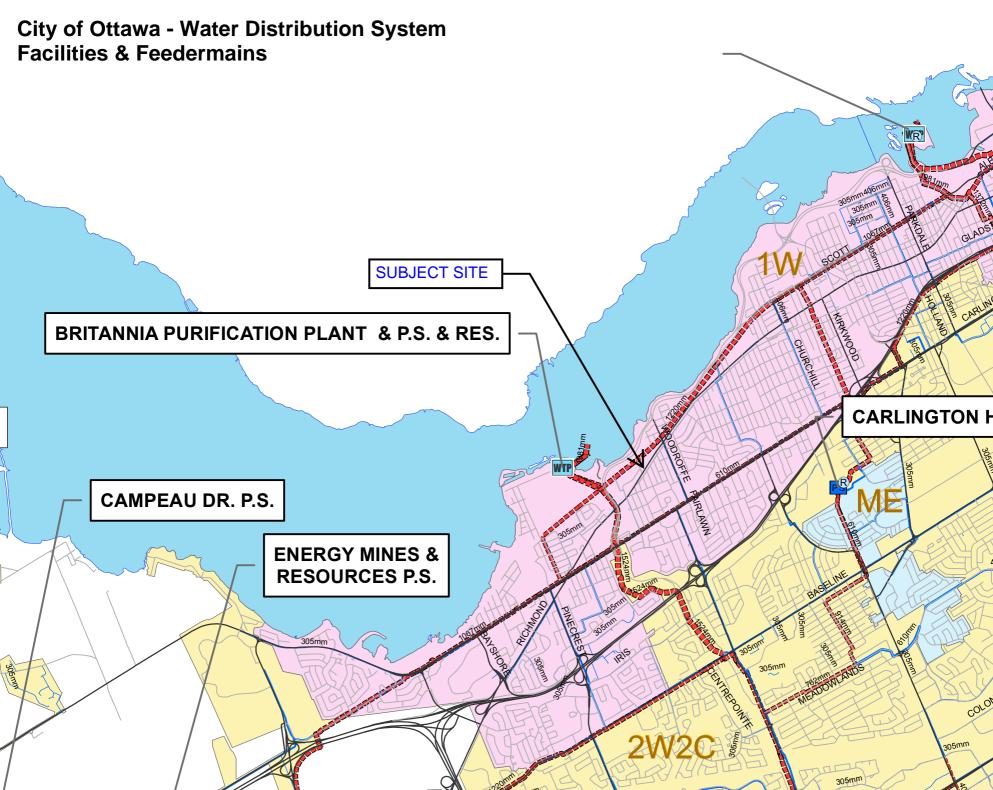
Designed By: RP Checked By: RF

Date: July 14, 2023

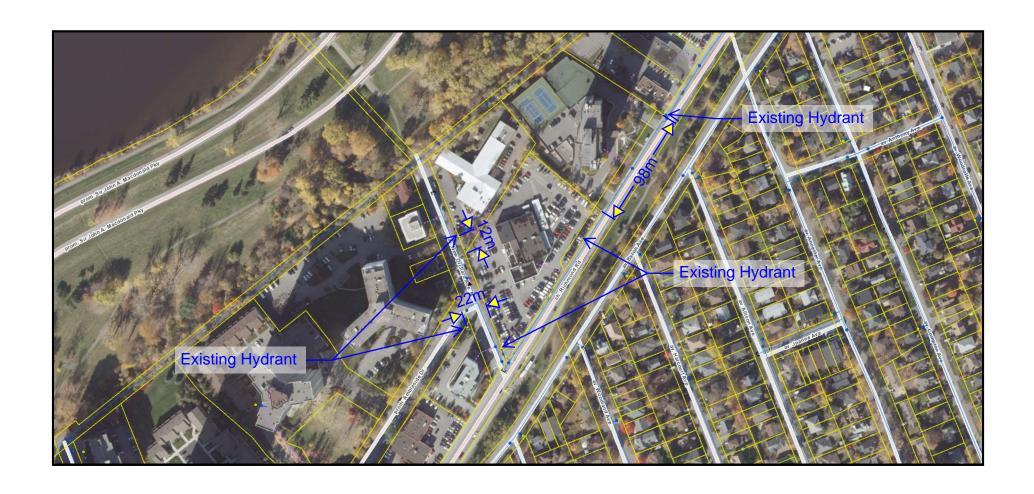
Boundary Conditions Unit Conversion

Richmond Rd./New Orchard Ave N.

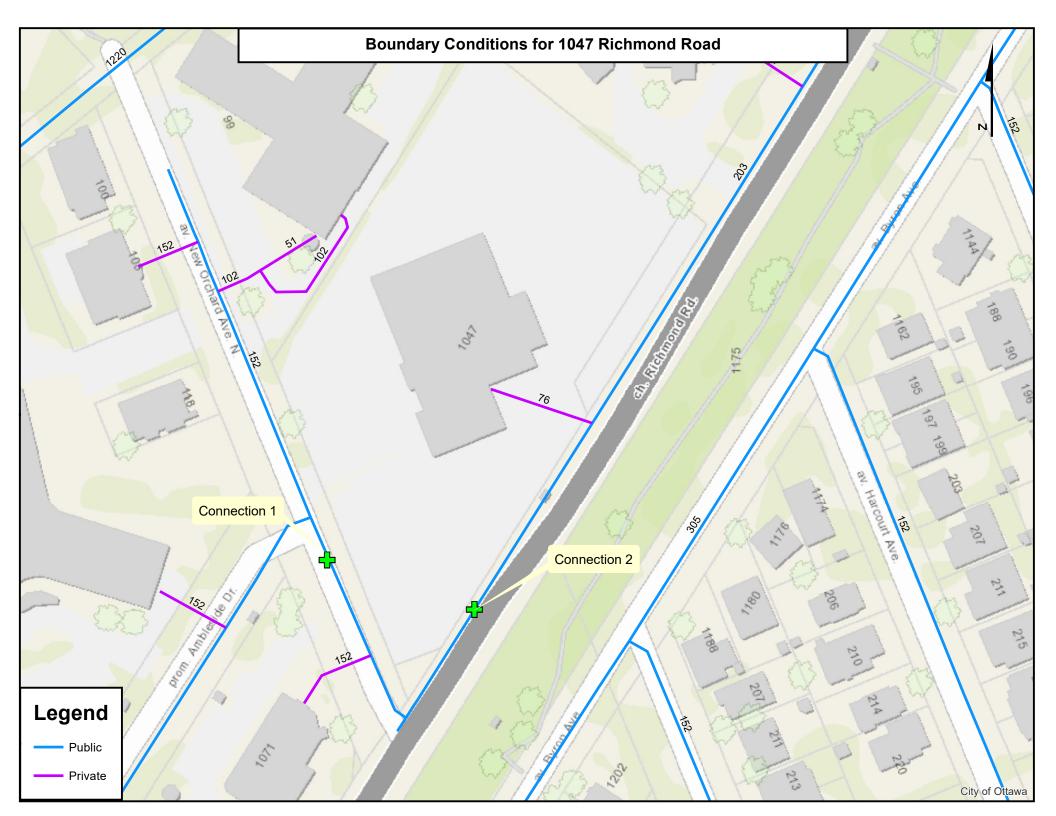
Scenario	Height (m)	Elevation (m)	m H₂O	PSI	kPa				
Avg. DD	116.0	64.8	51.2	72.8	502.3				
Fire Flow (200 L/s or 12,000 L/min)	ow (200 L/s or 12,000 L/min) Fire flow available @ 20 PSI = 145 L/s or 8,700 L/min								
Peak Hour	107.0	64.8	42.2	60.0	414.0				



1047 Richmond Road Hydrant Coverage Figure



https://maps.ottawa.ca/geoOttawa/



Ryan Robineau

From: Armstrong, Justin < justin.armstrong@ottawa.ca>

Sent: July 11, 2023 9:20 AM

To: Ryan Robineau

Cc: Robbie Pickard; Robert Freel; Surprenant, Eric

Subject: RE: 1047 Richmond Road Boundary Condition Request

Attachments: 1047 Richmond Road July 2023.pdf

Hi Ryan,

Received the following from the water group this morning. Note for future reference, that their typical turnaround timeline for water boundary condition requests is 2 weeks (10 business days).

Please note 12,000 L/min FF is too high and should be reduced.

The following are boundary conditions, HGL, for hydraulic analysis at 1047 Richmond Road, (zone 1W) assumed to be connected to the 203 mm watermain on Richmond Road and the 203 mm on Old Orchard Avenue (see attached PDF for location).

Min HGL: 107.0 m Max HGL: 116.0 m

Available fire flow at 20 psi: 145 L/s, assuming ground elevation of 64.8m

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

Regards, Justin

Justin Armstrong, P.Eng.

Project Manager

Planning, Real Estate and Economic Development Department – Direction générale de la planification, des biens immobiliers et du développement économique

Development Review - West Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste 21746, justin.armstrong@ottawa.ca

From: Ryan Robineau <r.robineau@mcintoshperry.com>

Sent: July 10, 2023 4:29 PM

To: Armstrong, Justin < justin.armstrong@ottawa.ca>

Cc: Robbie Pickard <r.pickard@mcintoshperry.com>; Robert Freel <r.freel@mcintoshperry.com>; Surprenant, Eric

<Eric.Surprenant@ottawa.ca>

Subject: RE: 1047 Richmond Road Boundary Condition Request

Good afternoon Justin.

I hope your are well.

Just following up to see if the water group has provided an update on the boundary condition request.

Regards,

Ryan Robineau, EIT

Civil Engineering Technologist

T. 613.714.6611

r.robineau@mcintoshperry.com | www.mcintoshperry.com





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Platinum member

From: Armstrong, Justin < justin.armstrong@ottawa.ca>

Sent: June 28, 2023 2:30 PM

To: Ryan Robineau <r.robineau@mcintoshperry.com>

Cc: Robbie Pickard <r.pickard@mcintoshperry.com>; Robert Freel <r.freel@mcintoshperry.com>; Surprenant, Eric

<Eric.Surprenant@ottawa.ca>

Subject: RE: 1047 Richmond Road Boundary Condition Request

Hi Ryan,

I have sent off the request for boundary conditions to the City's water group. I will let you know once I receive the results.

Thanks,

Justin

Justin Armstrong, P.Eng.

Project Manager

Planning, Real Estate and Economic Development Department – Direction générale de la planification, des biens immobiliers et du développement économique

Development Review - West Branch City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste 21746, justin.armstrong@ottawa.ca

From: Ryan Robineau < r.robineau@mcintoshperry.com >

Sent: June 26, 2023 10:23 AM

To: Armstrong, Justin < justin.armstrong@ottawa.ca>

Cc: Robbie Pickard <r.pickard@mcintoshperry.com>; Robert Freel <r.freel@mcintoshperry.com>; Surprenant, Eric

< Eric. Surprenant@ottawa.ca>

Subject: RE: 1047 Richmond Road Boundary Condition Request

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Hello Justin,

Please see the attached revised water calculations for the below boundary condition request.

A breakdown of area per floor has been added to the FUS calculation and a C value of 0.8 has been determined for the buildings per further coordination with the architect.

- The estimated fire flow is 12,000 L/min based on the 2020 FUS
- Average daily demand: 6.61L/s
- Maximum daily demand: 16.44 L/s
- Maximum hourly daily: 36.13L/s

If you require any further clarification please do not hesitate to contact me.

Regards,

Ryan Robineau, EIT

Civil Engineering Technologist

T. 613.714.6611

r.robineau@mcintoshperry.com | www.mcintoshperry.com

McINTOSH PERRY

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APPENDIX D SANITARY CALCULATIONS

McINTOSH PERRY

CCO-22-2242 - 1047 Richmond Road - Sanitary Demands

1047 Richmond Road Project: Project No.: CCO-22-2242 Designed By: RP Checked By: RDF July 14, 2023 Date: 1.02 Gross ha Site Area 89 1.40 Persons per unit Bachelor 1 Bedroom 526 1.40 Persons per unit 2 Bedroom 519 2.10 Persons per unit 3 Bedroom 18 3.10 Persons per unit **Total Population** 2007 Persons Commercial Area 859 m' **Amenity Space** 1550 m^3

DESIGN PARAMETERS

Institutional/Commercial Peaking Facto

Residential Peaking Factor 3.07 * Using Harmon Formula = $1+(14/(4+P^0.5))*0.8$

1.5

where P = population in thousands, Harmon's Correction Factor = 0.8

Mannings coefficient (n) 0.013

Demand (per capita) 280 L/day Infiltration allowance 0.33 L/s/Ha

EXTRANEOUS FLOW ALLOWANCES

Infiltration / Inflow	Flow (L/s)
Dry	0.05
Wet	0.29
Total	0.34

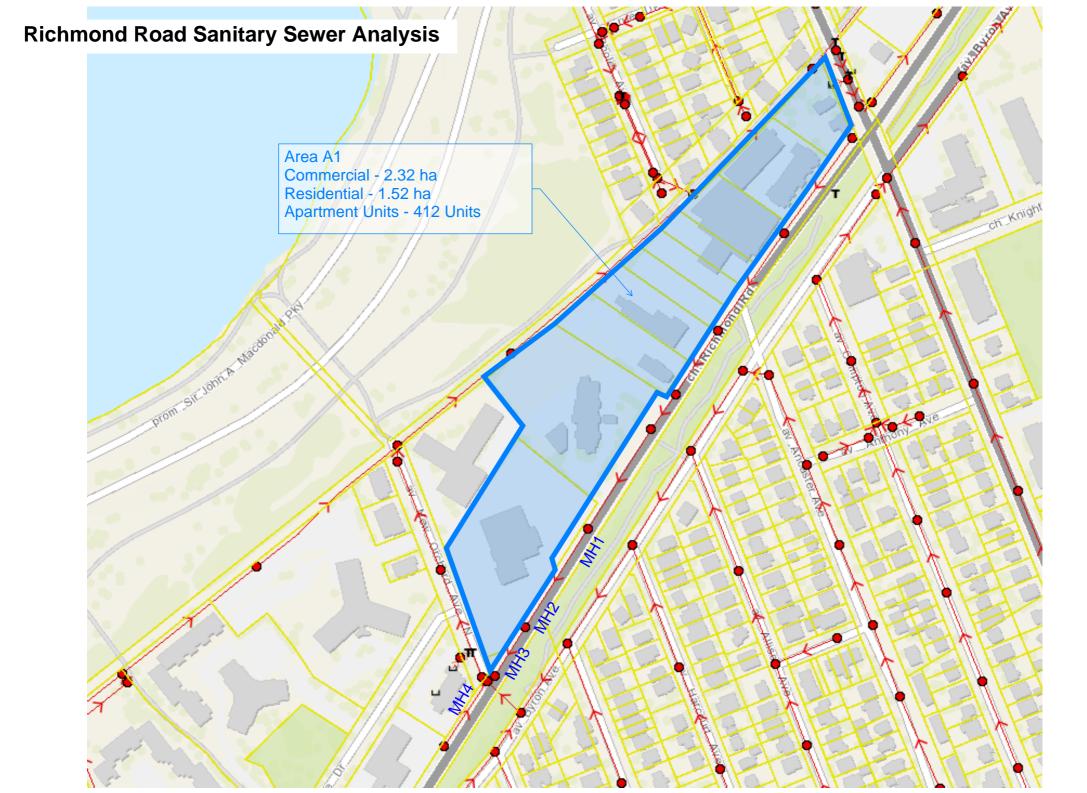
AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	POPULATION / AREA	Flow (L/s)
Residential	280	L/c/d	2007	6.50
Industrial - Light**	35,000	L/gross ha/d		0
Industrial - Heavy**	55,000	L/gross ha/d		0
Commercial / Amenity	2,800	L/(1000m² /d)	2409	0.08
Hospital	900	L/(bed/day)		0
Schools	70	L/(Student/d)		0
Trailer Parks no Hook-Ups	340	L/(space/d)		0
Trailer Park with Hook-Ups	800	L/(space/d)		0
Campgrounds	225	L/(campsite/d)		0
Mobile Home Parks	1,000	L/(Space/d)		0
Motels	150	L/(bed-space/d)		0
Hotels	225	L/(bed-space/d)		0
Office	75	L/7.0m ² /d		0
Tourist Commercial	28,000	L/gross ha/d		0
Other Commercial	28,000	L/gross ha/d		0

AVERAGE RESIDENTIAL FLOW	6.50	L/s
PEAK RESIDENTIAL FLOW	19.95	L/s
AVERAGE ICI FLOW	0.08	L/s
PEAK INSTITUTIONAL/COMMERCIAL FLOW	0.12	L/s
PEAK INDUSTRIAL FLOW	0.00	L/s
TOTAL PEAK ICI FLOW	0.12	L/s

TOTAL SANITARY DEMAND

TOTAL ESTIMATED AVERAGE DRY WEATHER FLOW	6.63	L/s
TOTAL ESTIMATED PEAK DRY WEATHER FLOW	20.12	L/s
TOTAL ESTIMATED PEAK WET WEATHER FLOW	20.41	L/s



SANITARY SEWER DESIGN SHEET

PROJECT: 1047 RICHMOND ROAD

LOCATION:

CLIENT: FENGATE

McINTOSH PERRY

	LOC	ATION							RESIDENTIA	۱L							ICI AREAS				INFILTR	ATION ALLO	WANCE	FLOW				SEWER DA	TA		
1	2		3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
						UN	IT TYPES		AREA	POPU	LATION		PEAK			ARE	\ (ha)			PEAK	AREA	A (ha)	FLOW	DESIGN	CAPACITY	LENGTH	DIA	SLOPE	VELOCITY	AVAI	ILABLE
STREET	AREA	ID	FROM	то	CE.	SD	TH	APT	(ha)	IND	сим	PEAK	FLOW	INSTITU	ITIONAL	COMN	IERCIAL	INDU	STRIAL	FLOW	IND	сим	(L/s)	FLOW	(L/s)	(m)	(mm)	(%)	(full)	CAP	PACITY
			MH	MH	31	30	- 111	AFI	(IIa)	IND	COIVI	FACTOR	(L/s)	IND	CUM	IND	CUM	IND	CUM	(L/s)	IND	COIVI	(L/3)	(L/s)	(L/3)	(111)	(11111)	(70)	(m/s)	L/s	(%)
Richmond Road	A-1		MH1	MH2				412	1.52	947.6	947.6	3.25	9.99		0.00	2.32	2.32		0.00	1.13	3.84	3.84	1.27	12.38	26.91	91.44	225	0.33	0.656	14.53	53.99
Richmond Road			MH2	MH3						0.0	947.6	3.25	9.99		0.00		2.32		0.00	1.13	0.00	3.84	1.27	12.38	30.72	44.20	225	0.43	0.748	18.34	59.69
Richmond Road			MH3	MH4						0.0	947.6	3.25	9.99		0.00		2.32		0.00	1.13	0.00	3.84	1.27	12.38	44.19	9.66	225	0.89	1.077	31.81	71.98
																															1
Design Parameters:					Notes:							Designed:		AJG			No.					Revision							Date		
					1. Manni	ings coeffici	ent (n) =		0.013								1.				Du	e Diligence E	Brief						2021-10-08		
Residential		ı	ICI Areas		2. Dema	nd (per capi	ta):	28	0 L/day																						
SF 3.4 p/p/u				Peak Factor	3. Infiltra	ation allowa	nce:	0.3	3 L/s/Ha			Checked:		AJG																	
TH/SD 2.7 p/p/u	INST	28,000	L/Ha/day	1.5	4. Reside	ential Peakir	g Factor:																								
APT 2.3 p/p/u	COM	28,000	L/Ha/day	1.5		Harmon	Formula = 1	+(14/(4+P^0.	5)*0.8)																						
Other 60 p/p/Ha	IND	35,000	L/Ha/day	MOE Chart		where P	= population	in thousand	S			Project No	.:	CCO-22-224	12															-	
																		•											Sheet No:		
																													1 of 1		

Alison Gosling

Subject: RE: 1047 Richmond Road -

From: Kuruvilla, Santhosh <Santhosh.Kuruvilla@ottawa.ca>

Sent: October 27, 2021 10:48 AM

To: 'Anthony Girolami' <anthony.girolami@fengate.com>; Alison Gosling <a.gosling@mcintoshperry.com>

Cc: Robert Freel <r.freel@mcintoshperry.com>

Subject: RE: 1047 Richmond Road -

Hello All

Following is the response I received from our Asset Management Branch regarding the existing sanitary sewer capacity:

"I have no concerns with the proposed sanitary flows."

Thanks,

Santhosh

From: Kuruvilla, Santhosh

Sent: October 19, 2021 1:06 PM

To: 'Anthony Girolami' <anthony.girolami@fengate.com>; 'Alison Gosling' <a.gosling@mcintoshperry.com>

Cc: Robert Freel < <u>r.freel@mcintoshperry.com</u>>

Subject: RE: 22-2242 Richmond Road - Sanitary HGL Analysis

Thanks Anthony. Yes, I did attend the pre-application consultation meeting for 1047 Richmond Rd.

I will forward the sanitary flow information provided below to our Asset Management to assess if the existing sanitary sewer has adequate capacity to receive this flow or not and get back to you.

Thanks,

Santhosh

From: Anthony Girolami <anthony.girolami@fengate.com>

Sent: October 19, 2021 12:47 PM

To: Kuruvilla, Santhosh <Santhosh.Kuruvilla@ottawa.ca>; 'Alison Gosling' <a.gosling@mcintoshperry.com>

Cc: Robert Freel < r.freel@mcintoshperry.com >

Subject: RE: 22-2242 Richmond Road - Sanitary HGL Analysis

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Hi Santhosh,

The project is located at 1047 Richmond Road and our pre-con was held last Thursday, October 14th at 1:30. Laurel McCreight was the Planner on the file.

Thank you,

Anthony Girolami

Development Manager, Real Estate

FENGATE Asset Management

C: 289-230-1014

anthony.girolami@fengate.com | fengate.com

From: Kuruvilla, Santhosh < Santhosh.Kuruvilla@ottawa.ca >

Sent: October 19, 2021 10:11 AM

To: 'Alison Gosling' < a.gosling@mcintoshperry.com >

Cc: Robert Freel <r.freel@mcintoshperry.com>; Anthony Girolami <anthony.girolami@fengate.com>

Subject: RE: 22-2242 Richmond Road - Sanitary HGL Analysis

You don't often get email from santhosh.kuruvilla@ottawa.ca. Learn why this is important

WARNING: EXTERNAL EMAIL

Good morning Alison,

Hope you are doing well.

I don't remember attending a pre-application consultation meeting for 2242 Richmond Road. Could you please provide me the correct address of this site and who (planner and the project manager) attended the pre-application consultation meeting from the City side?

Thanks,

Santhosh

From: Alison Gosling <a.gosling@mcintoshperry.com>

Sent: October 15, 2021 4:04 PM

To: Kuruvilla, Santhosh < Santhosh. Kuruvilla@ottawa.ca >

Cc: Robert Freel <r.freel@mcintoshperry.com>; Anthony Girolami <anthony.girolami@fengate.com>

Subject: 22-2242 Richmond Road - Sanitary HGL Analysis

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ATTENTION : Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.

Good afternoon Santhosh,

Hope this message finds you well.

We wanted to touch base with you regarding the 300 mm diameter sanitary sewer within New Orchard Avenue North. Due to the proximity to trunk infrastructure, we would like to request an HGL and capacity analysis from Asset Management. The contemplated sanitary flows are summarized below.

TOTAL ESTIMATED AVERAGE DRY WEATHER FLOW	7.47	L/s
TOTAL ESTIMATED PEAK DRY WEATHER FLOW	22.49	L/s
TOTAL ESTIMATED PEAK WET WEATHER FLOW	22.77	L/s



Figure 1: 300mm diameter Sanitary Sewer - New Orchard Ave N

Please let us know if you have any questions.

Thank you,

Alison Gosling, P.Eng.

Project Engineer, Land Development
115 Walgreen Road, Carp, ON, K0A 1L0
T. 613.714.4629
a.gosling@mcintoshperry.com | www.mcintoshperry.com

APPENDIX G STORMWATER MANAGEMENT CALCULATIONS

McINTOSH PERRY

CCO-22-2242 - 1047 Richmond Road

Job Name

1 of 4

Tc (min)		Intensity (mm/hr)				
(11111)	2-Year	5-Year	100-Year		C-Va	alues
10	76.8	104.2	178.6	PRE-DEVELOPMENT	Impervious	0.90
10	76.8	104.2	178.6	POST-DEVELOPMENT	Gravel	0.60
					Pervious	0.20

Pre-Development Runoff Coefficient

Drainage	Impervious	Gravel	Pervious Area	Average C	Average C
Area	Area (m²)	(m²)	(m²)	(5-year)	(100-year)
A1	9,743	0	0	0.90	

Pre-Development Runoff Calculations

Drainage	Drainage Area C C To	Tc	Q (L/s)				
Area	(ha)	2/5-Year	100-Year	(min)	2-Year	5-Year	100-Year
A1	1.02	0.90	1.00	10	195.63	265.38	505.33
Total	1.02				195.63	265.38	505.33

Post-Development Runoff Coefficient

	Drainage Area	Impervious Area (m²)	Gravel (m²)	Pervious Area (m²)	Average C (2/5-year)	Average C (100-year)	
ſ	B1	7,677	0	1,485	0.83	1.00	Restricted (Assumed to be 90% of the total area)
	B2	853	0	165	0.79	0.98	Unrestricted (Assumed to be 10% of the total area)

Post-Development Runoff Calculations

Drainage	Area	ſ	ſ	Tc		Q (L/s)		
Area	(ha)	2/5-Year	100-Year	(min)	2-Year	5-Year	100-Year	
B1	0.92	0.83	1.00	10	161.48	219.06	454.80	Restric
B2	0.10	0.79	0.98	10	17.10	23.19	49.68	Unrest
Total	1.02				178.58	242.26	504.48	1

Required Restricted Flow

Drainage	Area	С	Tc	Q (L/s)
Area	(ha)	2/5-Year	(min)	2-Year
A1	1.02	0.50	10	108.60

Post-Development Restricted Runoff Calculations

Drainage Area	Unrestricted Flow (L/S)		Restricted Flow (L/S)		Storage Required (m3)				
Area	2-year	5-year	100-Year	2-Year	5-Year	100-Year	2-Year	5-Year	100-Year
B1	161.48	219.06	454.80	20.92	28.38	58.92	115.80	154.9	318.1
B2	17.10	23.19	49.68	17.10	23.19	49.68			
Total	178.58	242.26	504.48	38.02	51.57	108.60			

CCO-22-2242 - 1047 Richmond Road

Storage Requirements for Area B1

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2-Year Storm Event

Tc (min)	l (mm/hr)	Runoff (L/s) B1	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
10	76.8	161.47	20.92	140.55	84.33
15	61.8	129.93	20.92	109.01	98.11
20	52.0	109.33	20.92	88.41	106.09
25	45.2	95.03	20.92	74.11	111.17
30	40.0	84.10	20.92	63.18	113.72
35	36.1	75.90	20.92	54.98	115.46
40	32.9	69.17	20.92	48.25	115.80
45	30.2	63.50	20.92	42.57	114.95
50	28.0	58.87	20.92	37.95	113.85

Maximum Storage Required 5-year = 116 m³

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5-Year Storm Event

Tc (min)	l (mm/hr)	Runoff (L/s) B1	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
10	104.2	219.08	28.38	190.70	114.42
15	83.6	175.77	28.38	147.39	132.65
20	70.3	147.80	28.38	119.42	143.31
25	60.9	128.04	28.38	99.66	149.49
30	53.9	113.32	28.38	84.94	152.90
35	48.5	101.97	28.38	73.59	154.54
40	44.2	92.93	28.38	64.55	154.92
45	40.6	85.36	28.38	56.98	153.85
50	37.7	79.26	28.38	50.88	152.65

Maximum Storage Required 5-year = 155 m³

100-Year Storm Event

Tc (min)	l (mm/hr)	Runoff (L/s) B1	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
10	178.6	454.90	58.92	395.98	237.59
15	142.9	363.97	58.92	305.05	274.55
20	120.0	305.64	58.92	246.72	296.07
25	103.8	264.38	58.92	205.46	308.19
30	91.9	234.07	58.92	175.15	315.28
35	82.6	210.39	58.92	151.47	318.08
40	75.1	191.28	58.92	132.36	317.67
45	69.1	176.00	58.92	117.08	316.12
50	64.0	163.01	58.92	104.09	312.27
55	59.6	151.80	58.92	92.88	306.52

Maximum Storage Required 100-year = 318 m³

CO-22-0480 - Youville Drive - SWM Calculations

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Time of Concentration Pre-Development

Drainage Area	Sheet Flow	Slope of	Tc (min)	Tc (min)
ID	Distance (m)	Land (%)	(5-Year)	(100-Year)
A1	48	1.97	4	2

Therefore, a Tc of 10 can be used

Tc= (3.26(1.1-c)L^0.5/S^0.33)

c = Balanced Runoff Coefficient L = Length of drainage area S = Average slope of watershed

APPENDIX H CITY OF OTTAWA DESIGN CHECKLIST

McINTOSH PERRY

City of Ottawa

4. Development Servicing Study Checklist

The following section describes the checklist of the required content of servicing studies. It is expected that the proponent will address each one of the following items for the study to be deemed complete and ready for review by City of Ottawa Infrastructure Approvals staff.

The level of required detail in the Servicing Study will increase depending on the type of application. For example, for Official Plan amendments and re-zoning applications, the main issues will be to determine the capacity requirements for the proposed change in land use and confirm this against the existing capacity constraint, and to define the solutions, phasing of works and the financing of works to address the capacity constraint. For subdivisions and site plans, the above will be required with additional detailed information supporting the servicing within the development boundary.

4.1 General Content

Criteria	Location (if applicable)
Executive Summary (for larger reports only).	N/A
Date and revision number of the report.	On Cover
Location map and plan showing municipal address, boundary, and layout of proposed development.	Appendix A
☐ Plan showing the site and location of all existing services.	N/A
Development statistics, land use, density, adherence to zoning and official plan, and reference to applicable subwatershed and	1.1 Purpose
watershed plans that provide context to which individual developments must adhere.	1.2 Site Description
	6.0 Stormwater Management
☐ Summary of pre-consultation meetings with City and other approval agencies.	Appendix B
Reference and confirm conformance to higher level studies and reports (Master Servicing Studies, Environmental Assessments,	1.1 Purpose
Community Design Plans), or in the case where it is not in conformance, the proponent must provide justification and	1.2 Site Description
develop a defendable design criteria.	6.0 Stormwater Management
\square Statement of objectives and servicing criteria.	3.0 Pre-Consultation Summary



☐ Identification of existing and proposed infrastructure available in the immediate area.	N/A
☐ Identification of Environmentally Significant Areas, watercourses and Municipal Drains potentially impacted by the proposed development (Reference can be made to the Natural Heritage Studies, if available).	N/A
Concept level master grading plan to confirm existing and proposed grades in the development. This is required to confirm the feasibility of proposed stormwater management and drainage, soil removal and fill constraints, and potential impacts to neighbouring properties. This is also required to confirm that the proposed grading will not impede existing major system flow paths.	N/A
☐ Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts.	N/A
☐ Proposed phasing of the development, if applicable.	N/A
Reference to geotechnical studies and recommendations concerning servicing.	Section 2.0 Background Studies, Standards and References
 All preliminary and formal site plan submissions should have the following information: Metric scale North arrow (including construction North) Key plan Name and contact information of applicant and property owner Property limits including bearings and dimensions Existing and proposed structures and parking areas Easements, road widening and rights-of-way Adjacent street names 	N/A

4.2 Development Servicing Report: Water

Criteria	Location (if applicable)
☐ Confirm consistency with Master Servicing Study, if available	N/A
Availability of public infrastructure to service proposed development	N/A
☐ Identification of system constraints	N/A
☐ Identify boundary conditions	Appendix C
☐ Confirmation of adequate domestic supply and pressure	N/A
 Confirmation of adequate fire flow protection and confirmation that fire flow is calculated as per the Fire Underwriter's Survey. Output should show available fire flow at locations throughout the development. 	Appendix C
 Provide a check of high pressures. If pressure is found to be high, an assessment is required to confirm the application of pressure reducing valves. 	N/A
 Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defined phases of the project including the ultimate design 	N/A
☐ Address reliability requirements such as appropriate location of shut-off valves	N/A
☐ Check on the necessity of a pressure zone boundary modification.	N/A
Reference to water supply analysis to show that major infrastructure is capable of delivering sufficient water for the proposed land use. This includes data that shows that the expected demands under average day, peak hour and fire flow conditions provide water within the required pressure range	Appendix C, Section 4.2

Description of the proposed water distribution network, including locations of proposed connections to the existing system, provisions for necessary looping, and appurtenances (valves, pressure reducing valves, valve chambers, and fire hydrants) including special metering provisions.	N/A
 Description of off-site required feedermains, booster pumping stations, and other water infrastructure that will be ultimately required to service proposed development, including financing, interim facilities, and timing of implementation. 	N/A
☐ Confirmation that water demands are calculated based on the City of Ottawa Design Guidelines.	Appendix C
Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference.	N/A

4.3 Development Servicing Report: Wastewater

Criteria	Location (if applicable)
Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitored flow data from relatively new infrastructure cannot be used to justify capacity requirements for proposed infrastructure).	N/A
☐ Confirm consistency with Master Servicing Study and/or justifications for deviations.	N/A
☐ Consideration of local conditions that may contribute to extraneous flows that are higher than the recommended flows in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers.	N/A
Description of existing sanitary sewer available for discharge of wastewater from proposed development.	Section 5.2 Proposed Sanitary Sewer

☐ Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable)	Section 5.3 Proposed Sanitary Design
☐ Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format.	N/A
 Description of proposed sewer network including sewers, pumping stations, and forcemains. 	Section 5.2 Proposed Sanitary Sewer
Discussion of previously identified environmental constraints and impact on servicing (environmental constraints are related to limitations imposed on the development in order to preserve the physical condition of watercourses, vegetation, soil cover, as well as protecting against water quantity and quality).	N/A
 Pumping stations: impacts of proposed development on existing pumping stations or requirements for new pumping station to service development. 	N/A
☐ Forcemain capacity in terms of operational redundancy, surge pressure and maximum flow velocity.	N/A
☐ Identification and implementation of the emergency overflow from sanitary pumping stations in relation to the hydraulic grade line to protect against basement flooding.	N/A
☐ Special considerations such as contamination, corrosive environment etc.	N/A

4.4 Development Servicing Report: Stormwater Checklist

Criteria	Location (if applicable)
 Description of drainage outlets and downstream constraints including legality of outlets (i.e. municipal drain, right-of-way, watercourse, or private property) 	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
Analysis of available capacity in existing public infrastructure.	N/A
 A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns, and proposed drainage pattern. 	Pre & Post-Development Plans
Water quantity control objective (e.g. controlling post-development peak flows to pre-development level for storm events ranging from the 2 or 5-year event (dependent on the receiving sewer design) to 100-year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
☐ Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
 Description of the stormwater management concept with facility locations and descriptions with references and supporting information. 	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
Set-back from private sewage disposal systems.	N/A
☐ Watercourse and hazard lands setbacks.	N/A
Record of pre-consultation with the Ontario Ministry of Environment and the Conservation Authority that has jurisdiction on the affected watershed.	N/A
Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists.	N/A
Storage requirements (complete with calculations) and conveyance capacity for minor events (1:5-year return period) and major events (1:100-year return period).	Appendix G

☐ Identification of watercourses within the proposed development and how watercourses will be protected, or, if necessary, altered by the proposed development with applicable approvals.	N/A
☐ Calculate pre-and post development peak flow rates including a description of existing site conditions and proposed impervious areas and drainage catchments in comparison to existing conditions.	Section 7.0 Proposed Stormwater Management Appendix G
☐ Any proposed diversion of drainage catchment areas from one outlet to another.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
 Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and stormwater management facilities. 	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
☐ If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post-development flows up to and including the 100-year return period storm event.	N/A
☐ Identification of potential impacts to receiving watercourses	N/A
☐ Identification of municipal drains and related approval requirements.	N/A
 Descriptions of how the conveyance and storage capacity will be achieved for the development. 	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
100-year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading.	N/A
☐ Inclusion of hydraulic analysis including hydraulic grade line elevations.	N/A

 Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors. 	N/A
☐ Identification of floodplains — proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions.	N/A
☐ Identification of fill constraints related to floodplain and geotechnical investigation.	N/A

4.5 Approval and Permit Requirements: Checklist

The Servicing Study shall provide a list of applicable permits and regulatory approvals necessary for the proposed development as well as the relevant issues affecting each approval. The approval and permitting shall include but not be limited to the following:

Criteria	Location (if applicable)
☐ Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act.	N/A
☐ Application for Certificate of Approval (CofA) under the Ontario Water Resources Act.	N/A
☐ Changes to Municipal Drains.	N/A
 Other permits (National Capital Commission, Parks Canada, Public Works and Government Services Canada, Ministry of Transportation etc.) 	N/A

4.6 Conclusion Checklist

Criteria	Location (if applicable)
Clearly stated conclusions and recommendations	Section 8.0 Summary
	Section 9.0 Recommendations
☐ Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency.	All are stamped
☐ All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario	All are stamped