SERVICING & STORMWATER MANAGEMENT REPORT FIX AUTO ORLEANS – 1400 & 1410 YOUVILLE DRIVE



Project No.: CCO-23-0480

City File No.: D07-12-22-0130

Prepared for:

BBS Construction (Ontario) LTD. 1805 Woodward Drive Ottawa, ON. K2C 0P9

Prepared by:

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May 01, 2023

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1.0 PROJECT DESCRIPTION

1.1 Purpose

McIntosh Perry (MP) has been retained by BBS Construction (Ontario) LTD. to prepare this Servicing and Stormwater Management Report in support of the Site Plan Control process for the proposed automobile body shop, located at 1400 & 1410 Youville Drive within the City of Ottawa (City File No. D07-12-22-0130).

The main purpose of this report is to present a servicing design for the development in accordance with the recommendations and guidelines provided by the City of Ottawa (City), the Rideau Valley Conservation Authority (RVCA), and the Ministry of the Environment, Conservation and Parks (MECP). This report will address the water, sanitary and storm sewer servicing for the development, ensuring that existing and available services will adequately service the proposed development.

This report should be read in conjunction with the following drawings:

- CCO-23-0480, C101 Site Grading, Drainage & Sediment and Erosion Control Plan, and
- CCO-23-0480, C102 Site Servicing Plan,
- CCO-23-0480, PRE Pre-Development Drainage Area Plan (Appendix E)
- CCO-23-0480, POST Post-Development Drainage Area Plan (Appendix F)

1.2 Site Description



Figure 1: Site Map

The subject property, herein referred to as the site, is located at 1400 & 1410 Youville Drive within the Orleans ward in the City of Ottawa. It is described as Parts 1 and 3 on Plan 4R-6509. The land in question covers approximately 0.92 ha and is located north of the Youville Drive and St-Joseph Blvd intersection. The site is zoned for light industrial use (IL2). See Site Location Plan in *Appendix A* for more details.

1.3 Proposed Development and Statistics

The proposed development consists of a 2,115 m², one storey automobile body shop and service station complete with office space. Parking and drive aisles will be provided throughout the site along with access from Youville Drive. See *Appendix B* for further details.

1.4 Existing Conditions and Infrastructures

The existing site is currently developed with a car wash and Jim Keay Ford gravel parking areas. The existing car wash is serviced by a 50 mm diameter water service, a 150 mm diameter sanitary service, and a 250 mm diameter storm service all of which are serviced by the municipal infrastructure within Youville Drive.

Sewer and watermain mapping collected from the City of Ottawa indicate that the following services exist across the property frontages within the adjacent municipal rights-of-way(s):

Youville Drive

- o 762 mm diameter concrete backbone watermain,
- 305 mm diameter ductile iron watermain,
- o 50 mm concrete sanitary sewer tributary to the Orleans Collector, and a
- o 675 mm concrete storm sewer tributary to the West Bilberry Creek and ultimately tributary to the Ottawa River approximately 1.7 km downstream.

1.5 Approvals

The proposed development is subject to the City of Ottawa site plan control approval process. Site plan control requires the City to review, provided concurrence and approve the engineering design package. Permits to construct can be requested once the City has issued a site plan agreement.

An Environmental Compliance Approval (*ECA*) Amendment through the Ministry of Environment, Conservation and Parks (*MECP*) may be required due to the light industrial zoning. Requirements to be further discussed with City staff.

2.0 BACKROUND STUDIES

As-built drawings of existing services, provided by the City of Ottawa Information centre, within the vicinity of the proposed site were reviewed in order to identify infrastructure available to service the proposed development.

A topographic survey of the site was completed by Stantec Geomatics Ltd (Contract No. 161614550-111) dated March 29th, 2022.

The Site Plan (A010) was prepared by KWC Architects Inc and dated January 25, 2023 (Site Plan).

2.1 Applicable Guidelines and Standards

City of Ottawa:

- ◆ Ottawa Sewer Design Guidelines, City of Ottawa, SDG002, October 2012. (Ottawa Sewer Guidelines)
 - Technical Bulletin ISTB-2014-01 City of Ottawa, February 2014. (ISTB-2014-01)
 - Technical Bulletin PIEDTB-2016-01 City of Ottawa, September 2016. (PIEDTB-2016-01)
 - Technical Bulletin ISTB-2018-01 City of Ottawa, January 2018. (ISTB-2018-01)
 - Technical Bulletin ISTB-2018-03 City of Ottawa, March 2018. (ISTB-2018-03)
 - Technical Bulletin ISTB-2019-01 City of Ottawa, January 2019. (ISTB-2019-01)
 - Technical Bulletin ISTB-2019-02 City of Ottawa, February 2019. (ISTB-2019-02)
- Ottawa Design Guidelines Water Distribution City of Ottawa, July 2010. (Ottawa Water Guidelines)
 - Technical Bulletin ISD-2010-2 City of Ottawa, December 15, 2010. (ISD-2010-2)
 - Technical Bulletin ISDTB-2014-02 City of Ottawa, May 2014. (ISDTB-2014-02)
 - Technical Bulletin ISTB-2018-02 City of Ottawa, March 2018. (ISTB-2018-02)

Ministry of Environment, Conservation and Parks:

- ◆ Stormwater Planning and Design Manual, Ministry of the Environment, March 2003. (MECP Stormwater Design Manual)
- ◆ Design Guidelines for Sewage Works, Ministry of the Environment, 2008. (*MECP Sewer Design Guidelines*)

Other:

♦ Water Supply for Public Fire Protection, Fire Underwriters Survey, 2020. (FUS Guidelines)

3.0 PRE-CONSULTATION SUMMARY

A pre-consultation meeting was conducted on September 29, 2021, regarding the proposed site. Specific design parameters to be incorporated within this design include the following:

- o Pre-development and post-development flows shall be calculated using a maximum time of concentration (Tc) of 10 minutes.
- o Control 5 through 100-year post-development flows to the 5-year flows with a combined C value of 0.50.
- Quality control is required to be provided for this site (80% TSS Removal) as per RVCA requirements.

The notes from the City of Ottawa can be found in *Appendix B*.

4.0 WATERMAIN

4.1 Existing Watermain

The site is located within the 1E pressure zone, as per the Water Distribution System Mapping included in *Appendix C*. There are existing 762 mm diameter C01 and 305 mm diameter DI watermains within Youville Drive. The 305 mm diameter watermain services the existing car wash as well as the fire hydrants along the east side of Youville Drive. There are three municipal hydrants along Youville drive available to service the development.

4.2 Proposed Watermain

A new 150 mm diameter PVC water service will service the proposed building complete with a water valve located at the property line. The service will extend from the existing 305 mm diameter watermain within Youville Drive. Refer to drawing *C102* for a detailed servicing layout.

The Fire Underwriters Survey 2020 (FUS) method was utilized to determine the required fire flow for the site. The 'C' factor (type of construction) for the FUS calculation was determined to be 0.8 (non-combustible type construction). The total floor area ('A' value) for the FUS calculation was determined to be 2,113.1 m². The results of the calculations yielded a required fire flow of 7,000 L/min. A fire flow of 9,000 L/min was calculated using the Ontario Building Code (OBC) requirements. The detailed calculations for the FUS and OBC can be found in *Appendix C*.

The water demands for the proposed building have been calculated to adhere to the *Ottawa Design Guidelines – Water Distribution* manual and can be found in *Appendix C*. The results have been summarized below:

Site Area	0.92 ha
Industrial - Light	35,000 L/ha/day
Average Day Demand (L/s)	0.37
Maximum Daily Demand (L/s)	0.56
Peak Hourly Demand (L/s)	1.00
OBC Fire Flow Requirement (L/s)	150.00
FUS Fire Flow Requirement (L/s)	116.67

Table 1: Water Demands

The City provided the estimated water pressures at both for the average day scenario, peak hour scenario and the max day plus fire flow scenario for the demands indicated by the correspondence in *Appendix C*. The resulting pressures for the boundary conditions results are shown in *Table 2*, below.

Table 2: Boundary Conditions Results

Scenario	Proposed Demands (L/s)	Connection HGL (m H₂O)*/kPa		
Average Day Demand	0.37	53.1 / 520.9		
Maximum Daily + Fire Flow Demand	150.56	49.6 / 486.6		
Peak Hourly Demand	1.00	50.3 / 493.4		
*Adjusted for an estimated ground elevation of 61.50m above the connection point.				

The normal operating pressure range is anticipated to be 487 kPa to 530 kPa and will not be less than 275 kPa (40 psi) or exceed 689 kPa (100 psi).

To confirm the adequacy of fire flow to protect the proposed development, public fire hydrants within 150 m of the proposed building were analysed per City of Ottawa *ISTB 2018-02* Appendix I Table 1. Based on City guidelines (*ISTB-2018-02*), the existing hydrants can provide adequate fire protection to the proposed development. The results are summarized below.

Table 3: Fire Protection Confirmation

Building	Fire Flow Demand (L/min.)	Fire Hydrant(s) within 75m	Fire Hydrant(s) within 150m	Combined Fire Flow (L/min.)
1400-1410 Youville	7,000 (FUS)	2	1	15,200
Drive	9,000 (OBC)			

5.0 SANITARY DESIGN

5.1 Existing Sanitary Sewer

There is a 450 mm diameter concrete sanitary sewer within Youville Drive. Sanitary flow from the sewer is tributary to the Orleans Collector Sewer per the City of Ottawa Trunk Sewer Map figure available in *Appendix 'D'*.

5.2 Proposed Sanitary Sewer

It is proposed to repurpose the existing 150 mm diameter sanitary service currently connected to the existing car wash. The existing sanitary service is currently complete with a maintenance structure which is located just inside the property line as per the *City of Ottawa – Sewer Design Guidelines*, October 2012, Clause 4.4.4.7 and City of Ottawa Sewer-Use By-Law 2003-514 (14). The service connects to the existing 450 mm diameter sanitary sewer within Youville Drive. The existing 150 mm diameter gravity service has undergone CCTV inspection, however, the true condition of the existing service was not able to be determined. Per the recommendation of the CCTV report attached in *Appendix 'D'*, the service is to be flushed and re-examined prior to construction. Refer to drawing *C102* for a detailed servicing layout.

The proposed development consists of an automobile body shop and service station complete with office space. The peak design flows for the proposed buildings were calculated using criteria from the *Ottawa Sewer Guidelines* and are summarized in *Table 3*, below. Based on the unit occupancy statistics provided by the architect, the proposed site development will generate a flow of *1.79 L/s*. See *Appendix 'D'* of this report for more details.

Table 4: Sanitary Design Criteria

Design Parameter	Value
Site Area	0.92 ha
Industrial Demand (Light)	35,000 L/gross ha/d
Industrial Peaking Factor	6.80
Extraneous Flow Allowance	0.33 L/s/ha

Table 5 below, summarizes the estimated wastewater flow from the proposed development. Refer to *Appendix D* for detailed calculations.

Table 5: Summary of Estimated Sanitary Flow

Design Parameter	Total Flow (L/s)
Total Estimated Average Dry Weather Flow	0.42
Total Estimated Peak Dry Weather Flow	2.58
Total Estimated Peak Wet Weather Flow	2.84

It is anticipated that the existing service has a minimum full flow target velocity (cleansing velocity) of 0.6 m/s and a full flow velocity of not more than 3.0 m/s. The estimated capacity of the service lateral is 15.89 L/s based on an assumed slope of 1.0%. Due to the complexity of the downstream network, the City will need to advise of any downstream constraints.

6.0 STORM SEWER DESIGN

6.1 Existing Storm Sewers

The site is located within the Ottawa River East subwatershed. There is an existing 675 mm diameter concrete storm sewer within Youville Drive that outlets 0.3 Km downstream to Voyageur Creek. The site is currently serviced by a 250 mm diameter storm sewer network, which outlets to the existing 675 mm diameter storm sewer within Youville Drive.

6.2 Proposed Storm Sewers

A new 250-525 mm storm sewer network is proposed to extend from the existing 675mm sewer within Youville Drive in order to support the proposed development.

Runoff from the parking lot areas and drive aisles will be collected by existing and proposed catch basins. Based on architectural plans, drainage from the roof of the proposed building will be directed to the proposed sewer network within the parking lot area. Runoff collected from the site will be attenuated via an ICD on the outlet side of CBMH1.

Runoff collected by the storm sewer network will be treated by a proposed Hydro International Downstream Defender DD8 OGS unit or approved equivalent before stormwater is discharged to the existing storm outlet, as per drawing *C102*.

Foundation drainage for the proposed building will be conveyed via a 250 mm diameter storm service downstream of the on-site controls.

A maintenance structure (MH2) is proposed just inside the property line of the development to provide monitoring as per the *City of Ottawa – Sewer Design Guidelines*, October 2012, Clause 4.4.4.7 and City of Ottawa Sewer-Use By-Law 2003-514 (14). Refer to drawing *C102*.

See *CCO-23-0480 - POST* included in *Appendix F* of this report for more details. The Stormwater Management design for the subject property will be outlined in Section 7.0 of this report.

7.0 PROPOSED STORMWATER MANAGEMENT

7.1 Design Criteria and Methodology

Stormwater management for the proposed site will be maintained through positive drainage away from the proposed building and parking lot surface attenuation. Drainage from the roof of the building, the parking lot, and a landscaped external drainage area from the adjacent site will be collected by a series of catch basins. The collected parking lot flow will be restricted by a 200 mm diameter orifice before discharging towards a proposed OGS unit and finally an existing storm manhole within the site. Flow from the existing manhole will continue to convey stormwater to the 675 mm diameter storm sewer within Youville Drive. The quantitative and qualitative properties of the storm runoff for both the pre & post development flows are further detailed below.

In summary, the following design criteria have been employed in developing the stormwater management design for the site as directed by the RVCA and City:

Quality Control

o The site has been designed to achieve an 80% total suspended solids removal (*enhanced* level) using a proposed oil/grit separator.

Quantity Control

o Post-development flow 5/100-year is be restricted to match the 5-year pre-development flow with a maximum C value of 0.50.

7.2 Runoff Calculations

Runoff calculations presented in this report are derived using the Rational Method, given as:

Q = 2.78CIA (L/s)

Where: C = Runoff coefficient

= Rainfall intensity in mm/hr (City of Ottawa IDF curves)

A = Drainage area in hectares

It is recognized that the Rational Method tends to overestimate runoff rates. As a result, the conservative calculation of runoff ensures that any SWM facility sized using this method is expected to function as intended.

The following coefficients were used to develop an average C for each area:

Roofs/Concrete/Asphalt	0.90
Gravel	0.60
Undeveloped and Grass	0.20

As per the *City of Ottawa - Sewer Design Guidelines*, the 5-year balanced 'C' value must be increased by 25% for a 100-year storm event to a maximum of 1.0.

As per the pre-consultation meeting with the City of Ottawa the time of concentration (Tc) used for pre-development shall be determined using a calculated Tc of no less than 10 minutes and post-development flows shall be calculated using a Tc of 10 minutes.

7.3 Pre-Development Drainage

It has been assumed that the site contains no stormwater management controls for flow attenuation. The estimated pre-development peak flows for the 5, and 100-year events are summarized below in *Table 5*. See CCO-23-0480 - *PRE* in *Appendix E* and *Appendix G* for calculations.

Drainage Area	Area (ha)	Q (L/s)	
	(1.12)	5-Year	100-Year
A1	0.92	188.01	376.59
A2 (External Drainage)	0.005	0.31	0.66
Total	0.92	188.31	377.25

Table 6: Pre-Development Runoff Summary

7.4 Post-Development Drainage

The proposed site drainage limits are demonstrated on the Post-Development Drainage Area Plan. See CCO-23-0480 - *POST* in *Appendix 'F'* of this report for more details. A summary of the Post-Development Runoff Calculations can be found below.

Drainage Area	Area (ha)	5-Year Peak Flow (L/s)	100-Year Peak Flow (L/s)	100-Year Storage Requirement (m³)	100-Year Storage Available (m³)
B1	0.82	114.91	116.68	172.8	189.3
B2	0.10	5.99	12.82	-	-
Total	0.92	120.90	129.50	172.8	189.3

Table 7: Post-Development Runoff Summary

Post development drainage will be restricted to a maximum release rate of 129.50 L/s based on a maximum release rate requirement of 133.38 L/s.

Runoff within Area B1 will be collected by the proposed catchbasin system and restricted by a 185 mm orifice installed on the outlet side of CBMH3. The flow will be restricted to a maximum release

rate of 116.68 L/S with $189.3 m^3$ of storage to be provided via surface ponding within the parking lot.

Runoff within Area B2 will sheet drain without flow attenuation towards the golf course to the west of the site and towards Youville Drive to the east of the site. Gravel drainage within the 1410 Youville Drive parcel of land currently drains towards the golf course. As per drawing *C101*, the drainage area is proposed to be significantly reduced and will only direct landscaping runoff towards the neighbouring property. As a result, the development proposes to improve the existing condition.

7.5 Quality Control

Based on coordination with the RVCA an enhanced water quality target (80% TSS removal) is required for the site. This will be achieved by treating runoff collected from area B1 with a Hydro International Downstream Defender DD8 OGS unit or approved equivalent. Runoff within Area B2 is proposed to flow off-site without quality treatment.

8.0 EROSION AND SEDIMENT CONTROL

8.1 Temporary Measures

Before construction begins, temporary silt fence, straw bale or rock flow check dams will be installed at all natural runoff outlets from the property. It is crucial that these controls be maintained throughout construction and inspection of sediment and erosion control will be facilitated by the Contractor or Contract Administration staff throughout the construction period.

Silt fences will be installed where shown on the final engineering plans, specifically along the downstream property limits. The Contractor, at their discretion or at the instruction of the City, Conservation Authority or the Contract Administrator shall increase the quantity of sediment and erosion controls on-site to ensure that the site is operating as intended and no additional sediment finds its way off site. The rock flow, straw bale & silt fence check dams and barriers shall be inspected weekly and after rainfall events. Care shall be taken to properly remove sediment from the fences and check dams as required. Fibre roll barriers are to be installed at all existing curb inlet catchbasins and filter fabric is to be placed under the grates of all existing catchbasins and manholes along the frontage of the site and any new structures immediately upon installation. The measures for the existing/proposed structures is to be removed only after all areas have been paved. Care shall be taken at the removal stage to ensure that any silt that has accumulated is properly handled and disposed of. Removal of silt fences without prior removal of the sediments shall not be permitted.

Although not anticipated, work through winter months shall be closely monitored for erosion along sloped areas. Should erosion be noted, the Contractor shall be alerted and shall take all necessary steps to rectify the situation. Should the Contractor's efforts fail at remediating the eroded areas, the Contractor shall contact the City and/or Conservation Authority to review the site conditions and determine the appropriate course of action. As the ground begins to thaw, the Contractor shall place silt fencing at all required locations as soon as ground conditions warrant. Please see the *Site Grading, Drainage and Sediment & Erosion Control Plan* for additional details regarding the temporary measures to be installed and their appropriate OPSD references.

8.2 Permanent Measures

It is expected that the Contractor will promptly ensure that all disturbed areas receive topsoil and seed/sod and that grass be established as soon as possible. Any areas of excess fill shall be removed or levelled as soon as possible and must be located a sufficient distance from any watercourse to ensure that no sediment is washed out into the watercourse. As the vegetation growth within the site provides a key component to the control of sediment for the site, it must be properly maintained once established. Once the construction is complete, it will be up to the landowner to maintain the vegetation and ensure that the vegetation is not overgrown or impeded by foreign objects.

9.0 SUMMARY

- A new automobile body shop, service station, and office is proposed at 1400 & 1410 Youville Drive.
- A 150 mm diameter water service is proposed to service the development, extending from the existing 300 mm diameter watermain with Youville Drive.
- It is proposed to repurpose the existing 150 mm diameter sanitary service to service to the proposed building.
- The proposed storm sewer system, ranging in diameter from 250 mm to 525 mm, will service the site. The storm service will discharge stormwater into the 675 mm sewer within Youville drive.
- Storage for the 5- through 100-year storm events will be provided within the parking lot areas above the proposed storm structures via surface storage.
- Quality Control will be provided via an OGS unit.

10.0 RECOMMENDATION

Based on the information presented in this report, we recommend that City of Ottawa approve this Servicing and Stormwater Management Report in support of the proposed automobile body shop 1400 & 1410 Youville Drive

This report is respectfully being submitted for approval.

Regards,

McIntosh Perry Consulting Engineers Ltd.



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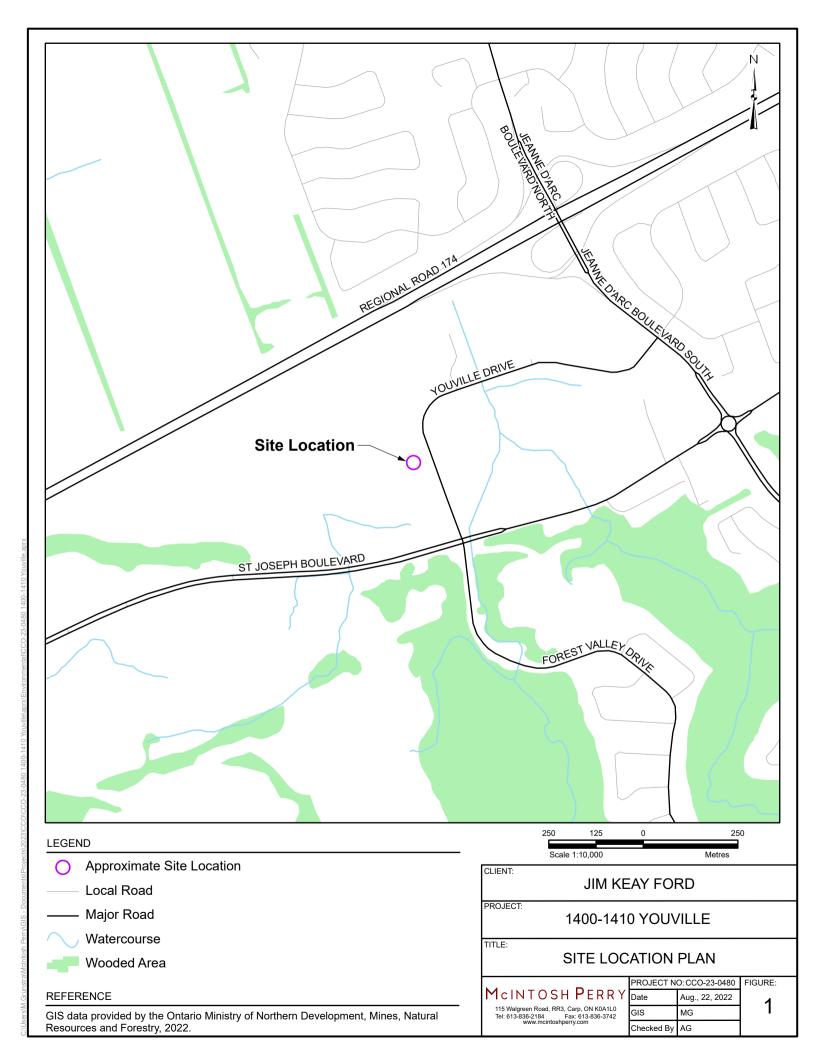
11.0 STATEMENT OF LIMITATIONS

This report was produced for the exclusive use of BBS Construction LTD. The purpose of the report is to assess the existing stormwater management system and provide recommendations and designs for the post-construction scenario that are in compliance with the guidelines and standards from the Ministry of the Environment, Conservation and Parks, City of Ottawa and local approval agencies. McIntosh Perry reviewed the site information and background documents listed in Section 2.0 of this report. While the previous data was reviewed by McIntosh Perry and site visits were performed, no field verification/measures of any information were conducted.

Any use of this review by a third party, or any reliance on decisions made based on it, without a reliance report is the responsibility of such third parties. McIntosh Perry accepts no responsibility for damages, if any, suffered by any third party as a result of decisions or actions made based on this review.

The findings, conclusions and/or recommendations of this report are only valid as of the date of this report. No assurance is made regarding any changes in conditions subsequent to this date. If additional information is discovered or becomes available at a future date, McIntosh Perry should be requested to re-evaluate the conclusions presented in this report, and provide amendments, if required.

APPENDIX A KEY PLAN



APPENDIX B BACKGROUND DOCUMENTS

Pre- Application Consultation 1410 (1438) Youville Drive (PC2021-0330) – City of Ottawa Internal Department Comments

Transportation:

- Follow Transportation Impact Assessment Guidelines
 - Submit a Screening form to start, a full Transportation Impact Assessment if any of the triggers on the screening form are satisfied. The Screening Form can be sent directly to <u>Josiane.Gervais@ottawa.ca</u>
 - Start this process asap. The application will not be deemed complete until the submission of the draft step 1-4, including the functional draft RMA package (if applicable) and/or monitoring report (if applicable).
 - Request base mapping asap if RMA is required. Contact Engineering Services (https://ottawa.ca/en/city-hall/planning-and-development/engineering-services)
- Clear throat requirement on a collector is 8m.
- Ensure site access meets the City's Private Approach Bylaw.
- Ensure drive aisle meets the City's Part 4 Parking, Queuing and Loading Provisions (Sections 100 to 114) Bylaw, i.e. minimum 6.7m width.
- The site falls just outside of the 600m radius from the existing Jeanne d'Arc transit station (and future Jeanne d'Arc LRT station).
- Include a new bus pad, as per City Standards.
- On site plan:
 - Show all details of the roads abutting the site up to and including the opposite curb; include such items as pavement markings, accesses and/or sidewalks.
 - Turning movement diagrams required for all accesses showing the largest vehicle to access/egress the site.
 - Turning movement diagrams required for internal movements (loading areas, garbage).
 - Show all curb radii measurements; ensure that all curb radii are reduced as much as possible and meet TAC Figure 8.5.1.
 - Show dimensions for site elements (i.e. lane/aisle widths, access width and throat length, parking stalls, sidewalks, pedestrian pathways, etc.)
- As the proposed site is for general public use, AODA legislation applies.
 Consider using the City's Accessibility Design Standards.
 - o Access aisles are required next to the accessible parking spaces.
 - Ensure all crosswalks located internally on the site provide a TWSI at the depressed curb, per requirements of the Integrated Accessibility Standards Regulation under the AODA.

Environmental:

Tree Conservation Report Requirements:

 If there are trees within the area impacted, contact Mark Richardson mark.richardson@ottawa.ca for information on the City's TCR requirements

Urban Design:

- A Design Brief is required as part of the submission. The Terms of Reference is attached for convenience.
- With respect to the proposed design:
 - Please consult OC-Transpo to explore opportunities to improve the bus stop. Considerations should be given to improvements such as a concrete pad for people to stand, a seat for people to sit, or a glass bus shelter.
 - Please provide a pedestrian walkway from the building main entrance to the bus stop.
 - Provide large canopy trees along the front to the extent possible. Given the location of the hydro lines, such trees will likely have to set back from the property line substantially and be located approximately at where the parking spaces are. Considerations should be given to relocate and reduce some front yard parking to create room for tree planting. (see attached diagram)
 - Provide a landscape buffer at the back of the site, approximately minimum
 3m to allow for some landscaping. (also see attached diagram)
 - The preliminary design shows a 7.5m area on the north side of the site for landscaping. Would it be beneficial to flip the site design so that the landscape area can be located on the sunny side of the site?

Policy Planning:

- The existing Official Plan designation is *General Urban Area*, which allows flexibility to permit the proposed use.
- The proposed New Official Plan designation is *Neighbourhood*, which allows flexibility to permit the proposed use.
- Advancing present and new Official Plans, the preliminary directions for the
 present Jeanne D'Arc Station Area study, part of the broader Orleans Corridor
 Secondary Plan study, envisions this south-west quadrant (south and west of
 Highway 174 and Jeannne D'Arc Boulevard, to St. Joseph Blvd.) as transitioning
 away from the largely light-industrial land use character to a character that is
 more transit-supportive based on primarily residential and commercial uses.
- While the envisioned vision will take many years to achieve, with the directions of the existing and future Official Plans in mind, the present proposal should advance site planning and design measures that will support and advance the transition to a more urban structure with more urban elements. A future application here should implement, for example, urban elements such as:
 - Building that is close to the street, with frontage that relates to people on the sidewalk, e.g. entrance that faces the street vs. a side parking lot
 - Items that support comfortable and inviting active transportation (walking or cycling), e.g. inclusion of medium to large street trees; support for transit infrastructure

- Site planning and design should anticipate the implementation of a municipal sidewalk in the future within the City right-of-way.
- Minimum and/or reduce large areas of asphalt (e.g. to transition from auto-oriented visual character of area to active transportation character; to reduce heat island effect; increase tree canopy)
- Refer to DRS Urban Design recommendations and for future ideas on how to best address these items.

Planning:

- Official Plan: The City's Official Plan (OP), Schedule B, designates the subject site "General Urban Area" for the entire depth of the property. General Urban Area designation permits many types and densities of housing, as well as employment, retail uses, service, industrial, cultural, leisure, greenspace, entertainment, and institutional uses. The General Urban Area permits uses that may generate traffic, noise or other impacts that have the potential to create conflicts with the surrounding residential community. More information can be found at: Section 3 Designations and Land Use | City of Ottawa.
- Zoning By-law 2008-250: The site is zoned Light Industrial Zone (IL2 H(14)). It
 is understood that the lands will be rezoned. The details of the proposed zoning
 can be discussed.

Comments:

- It is recommended to relocate the proposed building closer to Youville Drive and remove front yard parking to create an enhanced street presence.
- o Consider increasing the landscape buffer along the rear yard property line.
- Consider moving the location of the proposed loading zone further back from its current proposed location to reduce its visibility from the street.
- It is encouraged to not have any vehicles displayed for sale at the front of the property.
- Given the existing auto dominated nature of the Youville Drive Business Park, the proposed automotive related land use does not pose as a concern at this time.
- o There are no concerns of the proposed zoning change currently.

Engineering:

Please find attached the engineering comments for the proposed development.

Application Type and Fees:

• The Application Fees (2021 Rates) for the applications are as follows:

Application Type	Planning/ Legal Fee	Initial Engineering Design Review & Inspection Fee	Conservation Authority Fee (Initial)	Total
Zoning By-law Amendment (Major)	21,722.94	n/a	390	22,112.94
Site Plan Control Approval (New – Complex)	48,298.80	\$10,000 (incl. HST) services >\$300,000	1,040	59,338.80

Submission Requirements:

 Documents required in support of this application are highlighted in the attached Study and Plan Identification List

Links to Design Guidelines And Relevant Policy:

As part of Planning staff's review, we will evaluate your proposal against the relevant Official Plan policies and applicable Council-approved design guidelines. I have provided links to some of the more critical ones for your information.

- City Official Plan: https://ottawa.ca/en/planning-development-and-construction/official-plan-and-master-plans/official-plan
- Guidelines: For the following design guidelines, reference the following link: https://ottawa.ca/en/planning-development-and-construction/community-design/design-and-planning-guidelines/completed-guidelines

Please refer to the links to <u>Guide to preparing studies and plans</u> and <u>fees</u> for further information. Additional information is available related to <u>building permits</u>, <u>development charges</u>, and the <u>Accessibility Design Standards</u>. Be aware that other fees and permits may be required, outside of the development review process. You may obtain background drawings by contacting <u>informationcentre@ottawa.ca</u>.

These pre-application consultation comments are valid for one year. If you submit a development application(s) after this time, you may be required to meet for another preconsultation meeting and/or the submission requirements may change. You are as well encouraged to contact us for a follow-up meeting if the plan/concept will be further refined.

Alison Gosling

From: Jamie Batchelor < jamie.batchelor@rvca.ca>

Sent: August 15, 2022 11:23 AM

To: Ryan Robineau
Cc: Alison Gosling

Subject: RE: 1410 Youville Drive RVCA Requirement

Good Morning Ryan,

The water quality target would be enhanced (80% TSS removal). Given the erosive nature of Voyageur Creek, the stormwater from the site should demonstrate how the hydrology of the site is being maintained through the a water budget/balance. I will inquire further with our technical staff in this regard.

Jamie Batchelor, MCIP, RPP Planner, ext. 1191
Jamie.batchelor@rvca.ca



3889 Rideau Valley Drive PO Box 599, Manotick ON K4M 1A5 T 613-692-3571 | 1-800-267-3504 F 613-692-0831 | www.rvca.ca

This message may contain information that is privileged or confidential and is intended to be for the use of the individual(s) or entity n may contain confidential or personal information which may be subject to the provisions of the Municipal *Freedom of Information & I* you are not the intended recipient of this e-mail, any use, review, revision, retransmission, distribution, dissemination, copying, printing taking of any action in reliance upon this e-mail, is strictly prohibited. If you have received this e-mail in error, please contact the send and any copy of the e-mail and any printout thereof, immediately. Your cooperation is appreciated.

From: Ryan Robineau <r.robineau@mcintoshperry.com>

Sent: Monday, August 15, 2022 10:43 AM

To: Jamie Batchelor < jamie.batchelor@rvca.ca>

Cc: Alison Gosling < a.gosling@mcintoshperry.com>

Subject: 1410 Youville Drive RVCA Requirement

Good morning Jamie,

We wanted to touch base with you regarding a proposed development at 1410 Youville Drive.

The development involves the construction of a 1-storey automobile body shop and service station with surface parking. Drainage will be collected and conveyed to the 675mm dia storm sewer within Youville Drive. As shown by the attached figure, water travels approximately 0.30km to the Bilberry Creek (Outlet ID #09116). It is anticipated that drainage will be collected by catch basins.

We would like to know what SWM requirements the RVCA would have for the site.

Please let me know if you have any questions.



1 LOCATION PLAN
A010 N.T.S.

LEGAL DESCRIPTION:

PARCELS WW-8 AND WW-11 ON SEC 4M-152

PART OF BLOCK WW ON REGISTERED PLAN 4M-152

PARTS 1 AND 3 ON PLAN 4R-6509, FORMER CITY OF GLOUCESTER, NOW IN CITY OF OTTAWA

AS PREPARED BY STANTEC GEOMATICS LTD., 29 MARCH 2022

Project Zoning Review/Statistics

Municipality:City of OttawaMunicipal Address:1400-1410 Youville Drive

Registered Owner: Jim Keay

Lot Area: 9,188 sq.m. (98,894 sq.ft. (2.27 acres)) **Zoning By-law:** 2008-250

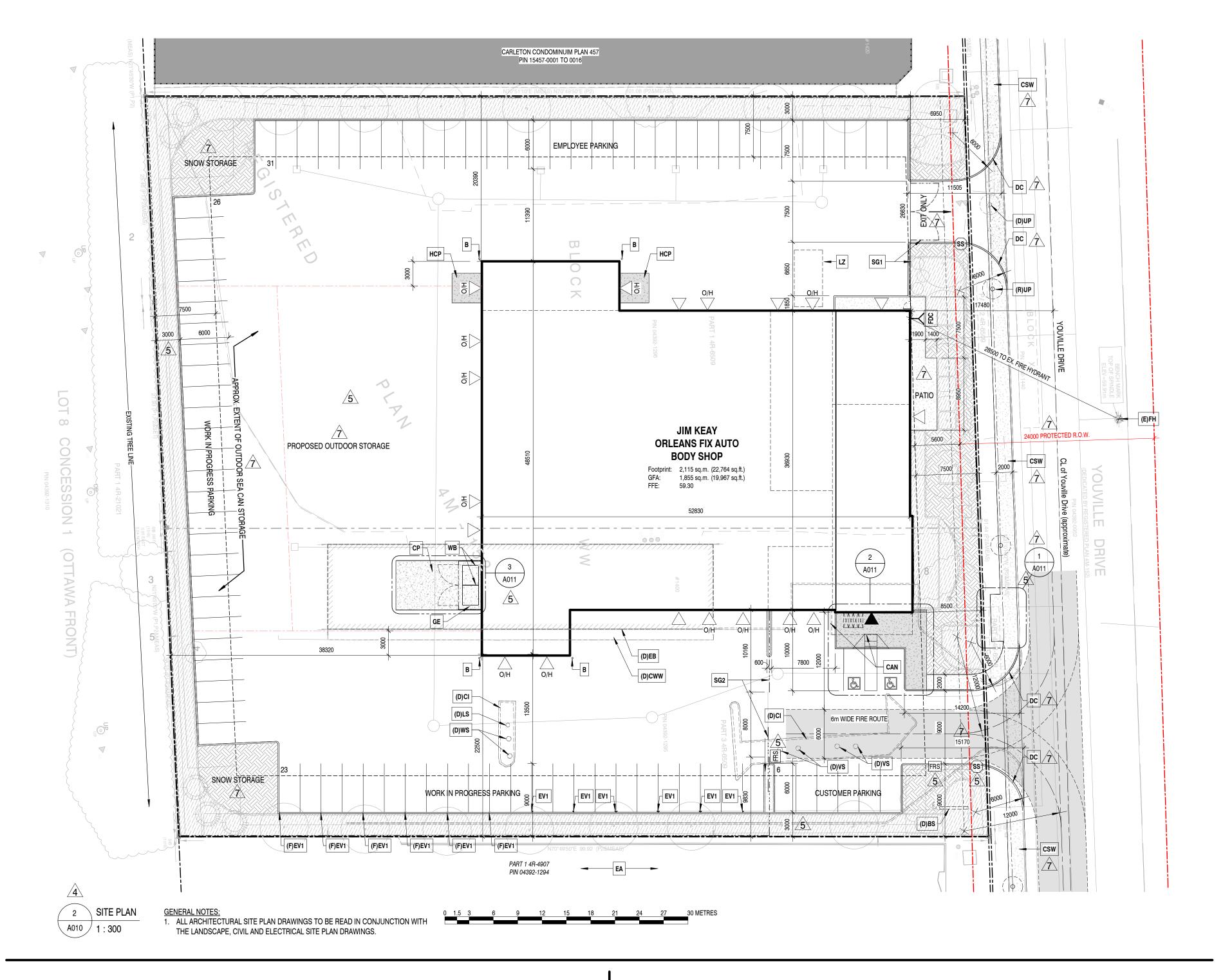
Zoning By-law: 2008-250
Zone: IL2 H(14) - Light Industrial

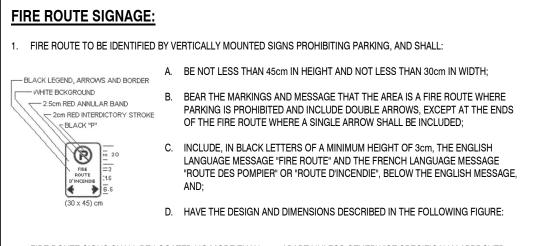
Proposed Use: Automobile Body Shop & Automobile Service Station

	Gross (out	-to-out)
	Sq.m.	Sq.ft
Proposed Development		
Ground Floor, Offices	291	3,130
Ground Floor, Body & Service Shop	1,596	17,177
Ground Floor, Parts	228	2,457
Total	2,115	22,764

Development Standards	D	D!.
	Required	Provided
Minimum Lot Area	2,000 sq.m.	9,188 sq.m.
Minimum Lot Width	No min.	91.3m
Minimum Required Yard		
Front Yard (min.)	7.5m	7.5m
Interior Side Yard (min.)	7.5m	20.39m
Rear Yard (min.)	7.5m	38.32m
Maximum Building Height	14m	8.01m
Maximum Lot Coverage	65%	22%
Maximum Floor Space Index	2	±0.2
Minimum Width of Landscaped Area		
Abutting a street	3m	6.95m
All other cases	No min.	3m

Existing Parking			
Parking Spaces (Minimum 2.6m x 5.2m)			
Offices	Required:	5 8	Area C of Schedule 1A
(2.4 spaces / 100 sq.m.)	Provided:	<u>7</u> 30	
Body Shop & Service Station	Required:	39	
(3 spaces per Service Bay @ 13 Service Bays)	Provided:	5 56	
Accessible Parking	Required:	2	
Section 111 of By-law 2017-301	Provided:	2	1x Type A & 1x Type B
Loading Spaces	Required:	1	
(3.5m x 9m)	Provided:	1	
Bicycle Parking	Required:	2	1x for Offices; 1x for Body Shop/Service Static
(Offices: 1 space / 250 sq.m.; All other: 1 space / 1,500 sq.m.)	Provided:	4	3x for Offices; 1x for Body Shop/Service Statio

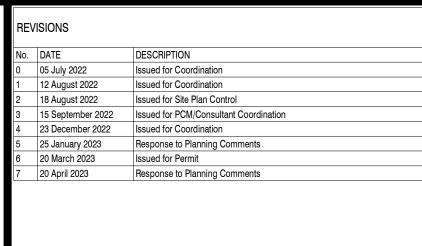




(30 x 45) cm	D.	HAVE THE DESIGN AND DIMENSIONS DESCRIBED IN THE FOLLOWING FIGURE:
	DNDI.	TED NO MORE THAN 25m APART UNLESS OTHERWISE SPECIFICALLY APPROVED FIONS OR THE FIRE ROUTE CONFIGURATION, AND THE LOWER EDGE OF EACH SIGN BOVE THE GROUND.

ICON	DESCRIPTION
	Existing Buildings
	Existing Buildings to be Demolished
	Proposed Buildings
	Property Lines
	Shared Property Lines
	— Setback Lines
	Landscape Buffer
	Overhead Wires
	- Fence
	Existing Concrete Curb
	Existing Concrete Curb to be Demolished
	Proposed Concrete Curb
	Depressed Concrete Curb
	Proposed Concrete Sidewalk
	Proposed Landscape Area
SS	Stop Sign
G	Barrier Free Parking Space
lacktriangle	Principal Entrance Door
	Exterior Door ("O/H" indicates Overhead Door)
	Exterior 6m Wide Fire Route (12m centerline radius on all turns, TYP.)

NOTE#	NOTE
(D)BS	Existing Signage to be Demolished - Project/Construction Manager to coordinate.
(D)CI	Existing Concrete Island to be Demolished
(D)CWW	Existing Concrete Walkway to be Demolished
(D)EB	Existing Building to be Demolished
(D)LS	Existing Light Standard to be Demolished
(D)UP	Existing Utility Pole, to be relocated. Refer also to Civil.
(D)VS	Existing Vacuum Station to be Demolished - refer to Electrical
(D)WS	Existing Windshield Wash Station to be Demolished - refer to Electrical
(E)FH	Existing Fire Hydrant to remain.
(F)EV1	Future Electric Vehicle Charging Station
(R)UP	Proposed relocation of Existing Utility Pole. Refer also to Civil
В	Bollard
CAN	Outline of Carport/Canopy above
СР	Concrete Pad - refer to Structural
CSW	Concrete Sidewalk
DC	Depressed Curb
EA	Existing Ashpalt
EV1	Electric Vehicle Charging Station; post-mounted level 2 dual-charging station by Owner
GE	Prefinished Metal Panel on Galvanized Steel framing Garbage Enclosure
HCP	12'-0" x 12'-0" Concrete Pad c/w In-slab Heating - refer to Mechanical & Structural
LZ	Loading Zone, 3.5m W x 7.0m L
SG1	Steel post & chain linked swinging gate, c/w locking mechanism
SG2	Steel post & chain linked sliding gate, c/w locking mechanism
WB	Waste Bins, by Owner

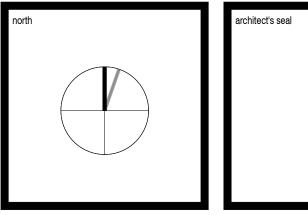


It is the responsibility of the appropriate contractor to check and verify all dimensions on site and report all errors and / or omissions to the Architect.

All contractors must comply with all pertinent codes and by-laws.

Do not scale drawings.

This drawing may not be used for construction until signed by KWC Architects Inc. and shall not be used without the Architect's consent.



383 Parkdale Avenue, Suite 201 Ottawa, Ontario, Canada, K1Y 4R4

KWC ARCHITECTS INC.

Phone: 613 238-2217
Fax: 613 238-6595
E-Mail: kwc@kwc-arch.com



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www.bbsconstruction.ca

JIM KEAY

project

'FIX AUTO' ORLEANS - AUTOMOBILE BODY SHOP

drawing title

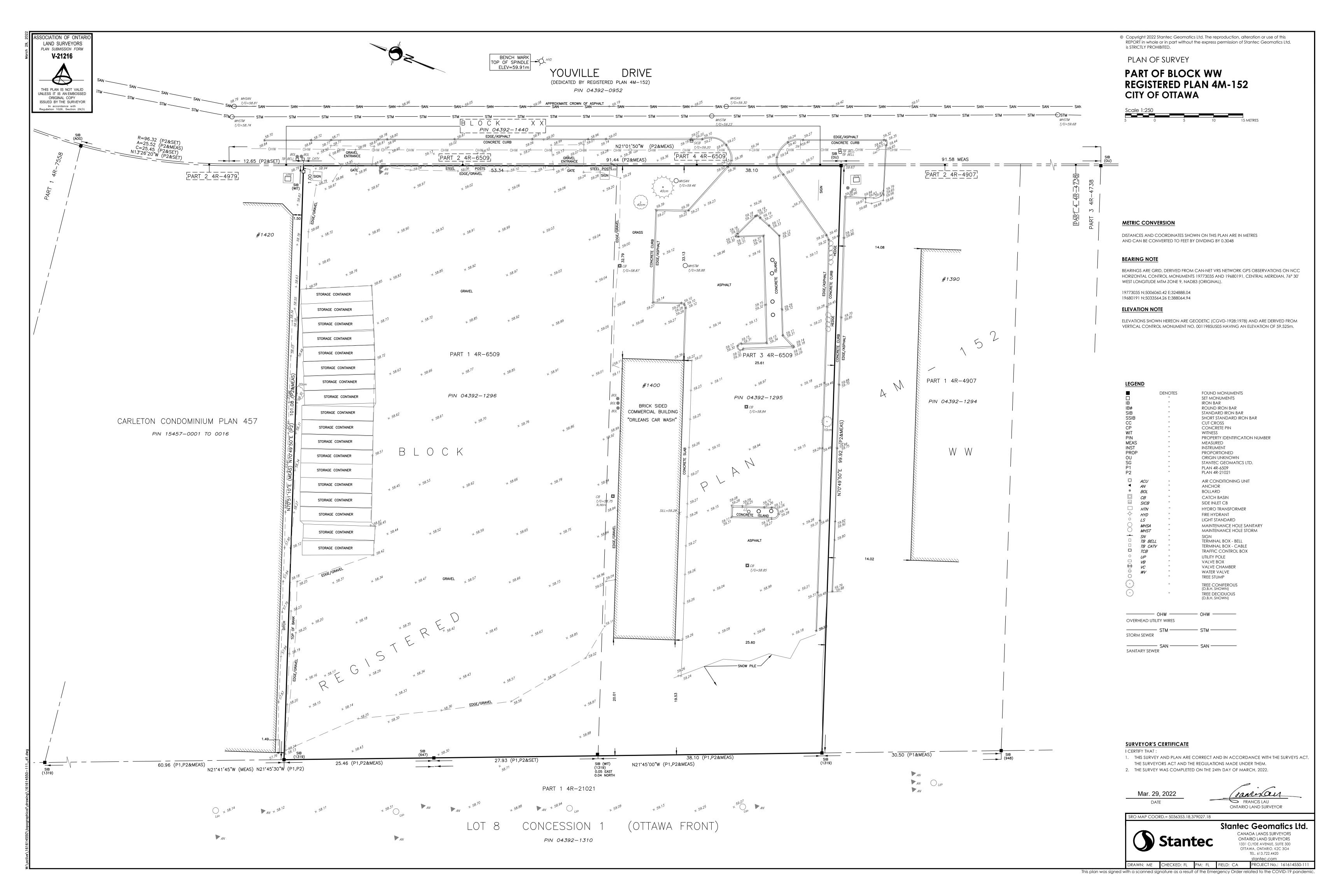
SITE PLAN

2023 JAN 3

2255
As indicated

A010

D07-12-22-0130



APPENDIX C WATERMAIN CALCULATIONS

CCO-22-0480 - Youville Drive - Water Demands

 Project:
 Youville Drive

 Project No.:
 CCO-22-0480

 Designed By:
 RRR

 Checked By:
 AJG

 Date:
 April 28, 2023

 Site Area:
 0.92 gross ha

Commercialm2Industrial - Light9188 m2Industrial - Heavym2

AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	
Residential	280	L/c/d	
Industrial - Light	35,000	L/gross ha/d	
Industrial - Heavy	55,000	L/gross ha/d	
Shopping Centres	2,500	L/(1000m² /d	
Hospital	900	L/(bed/day)	
Schools	70	L/(Student/d)	
Trailer Park with no Hook-Ups	340	L/(space/d)	
Trailer Park with Hook-Ups	800	L/(space/d)	
Campgrounds	225	L/(campsite/d)	
Mobile Home Parks	1,000	L/(Space/d)	
Motels	150	L/(bed-space/d)	
Hotels	225	L/(bed-space/d)	
Tourist Commercial	28,000	L/gross ha/d	
Other Commercial	28,000	L/gross ha/d	
	Residential		L/s
AVERAGE DAILY DEMAND	Commercial/Industrial/		
	Institutional	0.37	L/s

MAXIMUM DAILY DEMAND

DEMAND TYPE	A	UNITS	
Residential	9.5	x avg. day	L/c/d
Industrial	1.5	x avg. day	L/gross ha/d
Commercial	1.5	x avg. day	L/gross ha/d
Institutional	1.5	x avg. day	L/gross ha/d
	Residential	0.00	L/s
MAXIMUM DAILY DEMAND	Commercial/Industrial/		
	Institutional	0.56	L/s

MAXIMUM HOUR DEMAND

DEMAND TYPE	Д	UNITS	
Residential	14.3	x avg. day	L/c/d
Industrial	1.8	x max. day	L/gross ha/d
Commercial	1.8	x max. day	L/gross ha/d
Institutional	1.8	x max. day	L/gross ha/d
	Residential	0.00	L/s
MAXIMUM HOUR DEMAND	Commercial/Industrial/		
	Institutional	1.00	L/s

WATER DEMAND DESIGN FLOWS PER UNIT COUNT CITY OF OTTAWA - WATER DISTRIBUTION GUIDELINES, JULY 2010

AVERAGE DAILY DEMAND	0.37	L/s
MAXIMUM DAILY DEMAND	0.56	L/s
MAXIMUM HOUR DEMAND	1.00	L/s

CCO-22-0480 - Youville Drive - Fire Underwriters Survey

 Project:
 Youville Drive

 Project No.:
 CCO-22-0480

 Designed By:
 RRR

 Checked By:
 AJG

 Date:
 April 28, 2023

From the Fire Underwriters Survey (2020)

From Part II – Guide for Determination of Required Fire Flow Copyright I.S.O.: City of Ottawa Technical Bulletin ISTB-2018-02 Applied Where Applicable

A. BASE REQUIREMENT (Rounded to the nearest 1000 L/min)

 $F = 220 \times C \times VA$ Where: F = Required fire flow in liters per minute

C = Coefficient related to the type of construction.

A = The total floor area in square meters (including all storey's, but excluding basements at least 50 percent below grade)

in the building being considered.

Construction Type Non-Combustible Construction

C 0.8 A 2,115.0 m²

Total Floor Area (per the 2020 FUS Page 20 - Total Effective Area) 2,115.0 m²

-15%

*Unprotected Vertical Openings

Calculated Fire Flow 8,094.1 L/min

B. REDUCTION FOR OCCUPANCY TYPE (No Rounding)
From Page 24 of the Fire Underwriters Survey:

Limited Combustible

Fire Flow 6.800.0 L/min

C. REDUCTION FOR SPRINKLER TYPE (No Rounding)

Non-Sprinklered 0%

Reduction 0.0 L/min							
D. INCR	REASE FOR EXPOSURE (No Rounding)					
	Separation Distance (m)	Cons.of Exposed Wall	Length Exposed Adjacent Wall (m)	Height (Stories)	Length-Height Factor		
Exposure 1	20.1 to 30	Ordinary - Mass Timber (Unprotected)	93	2	186.0	5%	
Exposure 2	Over 30 m	Ordinary - Mass Timber (Unprotected)	20	1	20.0	0%	
Exposure 3	Over 30 m	Ordinary - Mass Timber (Unprotected)	50	2	100.0	0%	
Exposure 4	Over 30 m	Ordinary - Mass Timber (Unprotected)	20	1	20.0	0%	
				·	% Increase*	5%	•

Increase* 340.0 L/min

E. Total Fire Flow (Rounded to the Nearest 1000 L/min)

Fire Flow Required** 7,000.0 L/mi

^{*}In accordance with Part II, Section 4, the Increase for separation distance is not to exceed 75%

^{**}In accordance with Section 4 the Fire flow is not to exceed 45,000 L/min or be less than 2,000 L/min

CCO-22-0480 - Youville Drive - Boundary Condition Unit Conversion

 Project:
 Youville Drive

 Project No.:
 CCO-22-0480

 Designed By:
 RRR

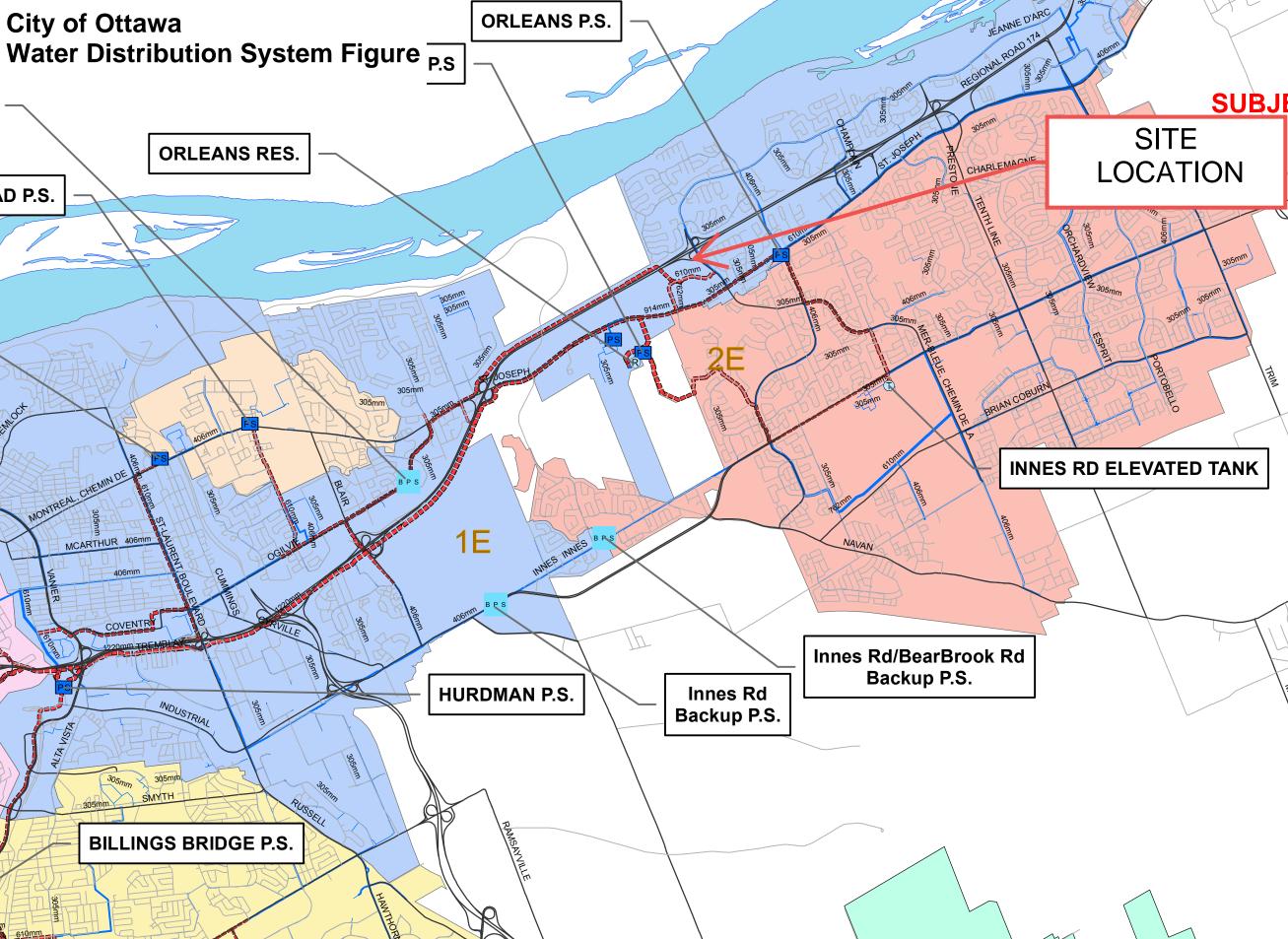
 Checked By:
 AJG

 Date:
 April 28, 2023

Boundary Conditions Unit Conversion

Youville Drive

Scenario	Height (m)	Elevation (m)	m H₂O	PSI	kPa
Avg. DD	114.6	61.5	53.1	75.6	520.9
Fire Flow (150L/s or 9,000 L/min)	111.1	61.5	49.6	70.6	486.6
Peak Hour	111.8	61.5	50.3	71.6	493.4



1400-1410 Youville Drive Hydrant Coverage Figure



Municipal Hydrants within 75m: 2

Municipal Hydrants within 150m: 1

Boundary Conditions 1400 & 1410 Youville Drive

Provided Information

Scenario	De	mand
Scenario	L/min	L/s
Average Daily Demand	22	0.37
Maximum Daily Demand	34	0.56
Peak Hour	60	1.00
Fire Flow Demand #1	9,000	150.00

Location



Results

Connection 1 – Youville Dr.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	114.6	75.5
Peak Hour	111.1	70.6
Max Day plus Fire 1	111.8	71.5

Ground Elevation = 61.5 m

APPENDIX D SANITARY CALCULATIONS

CCO-23-0480 - 1410 Youville Drive - Sanitary Demands

 Project:
 1410 Youville Drive

 Project No.:
 CCO-23-0480

 Designed By:
 RRR

 Checked By:
 AJG

 Date:
 August 26, 2022

Site Area 0.92 Gross ha

DESIGN PARAMETERS

Institutional/Commercial Peaking

Factor 1.5 Industrial Peaking Factor 6.8

Residential Peaking Factor 3.80 * Using Harmon Formula = $1+(14/(4+P^0.5))*0.8$

where P = population in thousands, Harmon's Correction Factor = 0.8

Mannings coefficient (n) 0.013

Demand (per capita) 280 L/day Infiltration allowance 0.33 L/s/Ha

EXTRANEOUS FLOW ALLOWANCES

Infiltration / Inflow	Flow (L/s)
Dry	0.05
Wet	0.26
Total	0.30

AVERAGE DAILY DEMAND

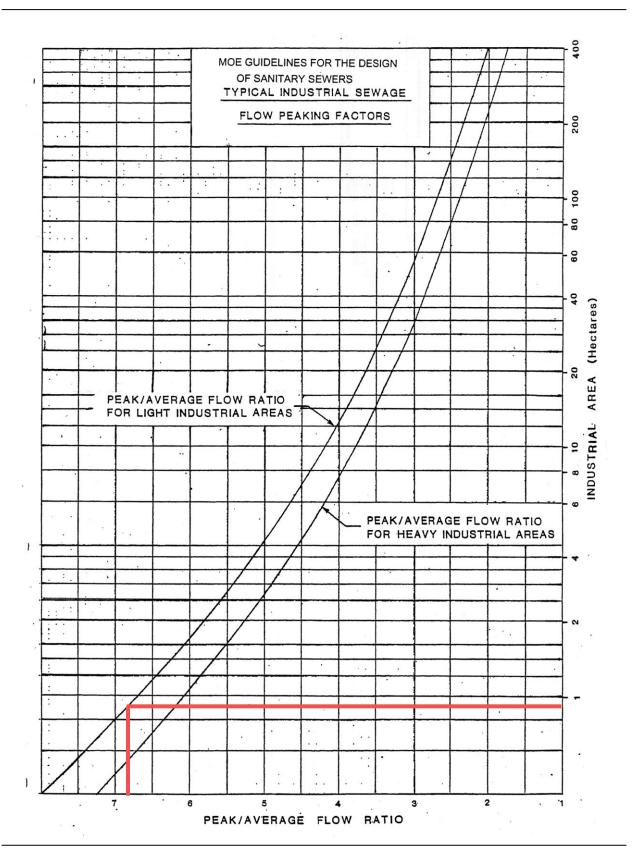
DEMAND TYPE	AMOUNT	UNITS	POPULATION / AREA	Flow (L/s)
Residential	280	L/c/d	0	0.00
Industrial - Light**	35,000	L/gross ha/d	0.92	0.37
Industrial - Heavy**	55,000	L/gross ha/d		0
Commercial / Amenity	2,800	L/(1000m²/d)	0.00	0.00
Hospital	900	L/(bed/day)		0
Schools	70	L/(Student/d)		0
Trailer Parks no Hook-Ups	340	L/(space/d)		0
Trailer Park with Hook-Ups	800	L/(space/d)		0
Campgrounds	225	L/(campsite/d)		0
Mobile Home Parks	1,000	L/(Space/d)		0
Motels	150	L/(bed-space/d)		0
Hotels	225	L/(bed-space/d)		0
Office	75	L/7.0m ² /d		0
Tourist Commercial	28,000	L/gross ha/d		0
Other Commercial	28,000	L/gross ha/d		0

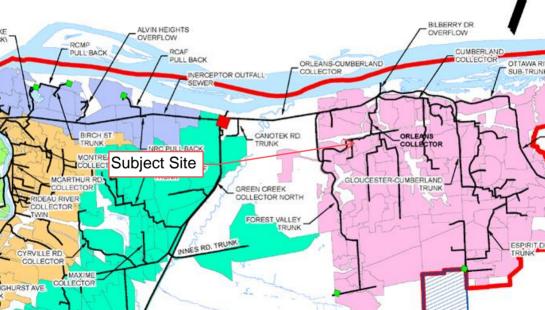
AVERAGE RESIDENTIAL FLOW	0.00	L/s
PEAK RESIDENTIAL FLOW	0.00	L/s
AVERAGE ICI FLOW	0.00	L/s
PEAK INSTITUTIONAL/COMMERCIAL FLOW	0.00	L/s
PEAK INDUSTRIAL FLOW	2.53	L/s
TOTAL PEAK ICI FLOW	2.53	L/s

TOTAL SANITARY DEMAND

TOTAL ESTIMATED AVERAGE DRY WEATHER FLOW	0.42	L/s
TOTAL ESTIMATED PEAK DRY WEATHER FLOW	2.58	L/s
TOTAL ESTIMATED PEAK WET WEATHER FLOW	2.84	L/s

^{**} PEAK INDUSTRIAL FLOW PER CITY OF OTTAWA SEWER DESIGN GUIDELINES APPENDIX 4B







McINTOSH PERRY

SANITARY SEWER LATERAL CCTV CONDITION ASSESSMENT JOB LOCATION: 140 YOUVILLE STREET OTTAWA, ONTARIO

JOB DATE:

Monday, April 24, 2023

Sewerteks Inc.



To the table of content Page 1 of 18



TABLE OF CONTENT

Cover Page	pages 1-1
Fable of contents	pages 2-2
Project summary	pages 3-4
Sanitary Detail Inspections	pages 5-14
Мар	pages 15-15
WRC Code Descriptions	pages 16-18

Sewerteks Inc.



To the table of content Page 2 of 18



PROJECT SUMMARY

The following is the result from the camera inspections of the sanitary sewer located at 140 Youville Street Ottawa. Ontario.

COMBINE SYSTEM

The sewer system is combine in the building. The first access point was a Roof Drain stack CO. The line was labeled COMB1. When the camera was at 2.2 meters into the line, one of the washroom toilets was flushed and found out that the connection at 2.2 meters from the stack CO, connected to the toilet line. A reversal inspection was done because of the excessive debris sediment in the line.

CLEANING

The lines were not cleaned prior to the CCTV condition assessment.

PLR

Each inspected pipe segment has a unique identification ID. This unique ID is the Pipe Line Reference ID or PLR. All the IDs are labeled in the map.

REPORT NAVIGATION

The PLR is used to navigate this report online. It's a link to the video inspection and video file. You can jump from the Summary to the actual inspection details by clicking the PLR link. The report also has a table of contents that are also link to each section of the report. In addition, the report has a link to re-direct you to the table of contents in every page.

DVD/USB DRIVE

The DVD or USB drive contains the digital report and videos.

STRUCTURAL AND OPERATIONAL DEFECTS

The following table#1 below describes the structural and operational defects of each individual pipe segment inspected identified by its unique ID or PipeLine Reference ID. The comments depict any additional information about each segment inspected.

Sewerteks Inc.



To the table of content Page 3 of 18



Table#1 below describes the structural and operational defects of each individual sanitary pipe segment inspected identified by its unique ID or PipeLine Reference ID.

PIPELINE REF. ID (PLR)	STRUCTURAL DEFECTS	OPERATIONAL DEFETCS	COMMENTS
COMB1	*TBD	DE	The sewer line has excessive amounts of debris sediment. The wye connection at 2.2 meters is the connection to the washroom toilet line. At the same time. It alsopicks up atleast one roof drain. The inspection was abandoned at 21.2 meters due to debris sediment and multiple line deviations. However, by the line tracing technique, it was traced to a manhole in the property as shown in the map of this report. The reversal inspection is this liine starts from the manhole.
COMB1-R	*TBD	*TBD	The camera was under water trhroughout the survey. However, the camera was pushed and traced up to the 18.2 meter mark where line SAN1 from the stack CO inside the building ended. The sewer line needs to b e flushed and re-camera in order to determine the true condition of the pipe.
COMB2	*TBD	DE	The camera was under water a few pipe segments. And excessive pockets of debris sediment were found. The inspection ended at the city sewer main line at 12.6 meters from manhole MHSA. The sewer line needs to be flushed and recamera in order to determine the true condition of the pipe.

*TBD: To Be Determined

Sewerteks Inc.



To the table of content Page 4 of 18



Date	4/24/2023	Sewe	er Type	COMBIN	NE		Pi	pe Size (mm)	100MM
Client	McINTOSH PERRY				Wo	ork ord	ler	531	
Contact	CURTIS MELANSON				Pip	e Mat	erial	ABS/PV	2
Start	STACKCO (RD1)				Ca	mera I	Directio	n With Flo	w
End	21.2 METERS TO MHSA1				DV	D#/US	B#	1	
Further Location	THE ACCESS STACK CO				Vid	leo na	me (PL	R) COMB1.	mpg
Details	THE BUILDING AS SHOW REPORT.	/IN IIN I H	E MAP OF	· IHIS	Re	port N	0	1	
Job Address	140 YOUVILLE STREET C	TTAWA,	ONTARIO)	Op	erator		Saul Ce	erna
Comments	The sewer line has excess the washroom toilet line. at 21.2 meters due to de	At the sa	ame time	. It alsopic	ks up a	least	one ro	of drain. The ir	spection was abandoned
DISTANCE (m)	CODE DESCRIPTION	%	SIZE (mm)	LENGTH (m)	CLOC		LOCK TO	REMARKS	
0.0	Start of inspection							Start at acces	s point STACKCO (RD1).
0.0	Line deviates down			0.6				Drop into the I	ine.
0.6	Water Level	0							
0.6	Line deviates down			2.6					
0.6	Dimesion of Sewer Changes		150						
1.6	Connection		100		12			At the drop	

75

Sewerteks Inc.

50

60

5

10

30

Connection

Water Level

Water Level

Water Level

Water Level

Debris

Debris

Camera Under Water

Line Deviates Right

2.2

3.0

3.8

4.0

5.0

5.6

6.0

11.6

12.8



Washroom toilet line

Sediment

Sediment

Camera under murky water

To the table of content Page 5 of 18

1.0



Date	4/24/2023	Sewe	er Type	COMBIN	NE			Pipe	e Size (mm)	100MM
Client	McINTOSH PERRY				,	Work	order		531	
Contact	CURTIS MELANSON					Pipe N	/lateria	al	ABS/PV0	2
Start	STACKCO (RD1)					Came	ra Dire	ection	With Flo	w
End	21.2 METERS TO MHSA1					DVD#/	USB#		1	
Further Location	THE ACCESS STACK CO					Video	name	(PLR)	COMB1.	mpg
Details	REPORT.	IN IIN I II	E MAP OF	1112		Repor	t No		1	
Job Address	140 YOUVILLE STREET O	TTAWA,	ONTARIO			Opera	tor		Saul Ce	erna
Comments	The sewer line has excess the washroom toilet line. at 21.2 meters due to det	At the sa	ame time.	It alsopic	ks up	atlea	st on	e roof	drain. The ir	nspection was abandoned
DISTANCE (m)	CODE DESCRIPTION	%	SIZE L	ENGTH		OCK ROM	CLO		REMARKS	
13.0	Camera Under Water									
15.8	General observation								camera under	murky water
21.2	Survey Abandoned									

Sewerteks Inc.



To the table of content Page 6 of 18



PROJECT NAME VIDEO NAME

SANITARY SEWER LATERAL CCTV CONDITION ASSESSMENT

SAN1

Figure#1: Start of inspection at access point STACKCO (RD1)



Figure#3: A view to the 0% water level and downward deviation at 0.6 meters from the top of STACKCO (RD1).



Figure#5: A view to the 75mm 1 o'clock connection to the washroom toilet line at 2.0 meters from the top STACKCO



0.0 m

m

1.4

Figure#2: A view to the line deviation downwards at 0.0 meters from the top of STACKCO (RD1).



Figure#4: A view to the 100mm 12 o'clock connection at 1.4 meters from the top STACKCO (RD1).



Figure#6: A view to the 40% water level at 2.8 meters from the top of STACKCO (RD1).

2.8 m



Sewerteks Inc.



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PROJECT NAME VIDEO NAME

SANITARY SEWER LATERAL CCTV CONDITION ASSESSMENT

m

Figure#7: A view to the camera under murky water at 3.8 meters from the top of STACKCO (RD1).

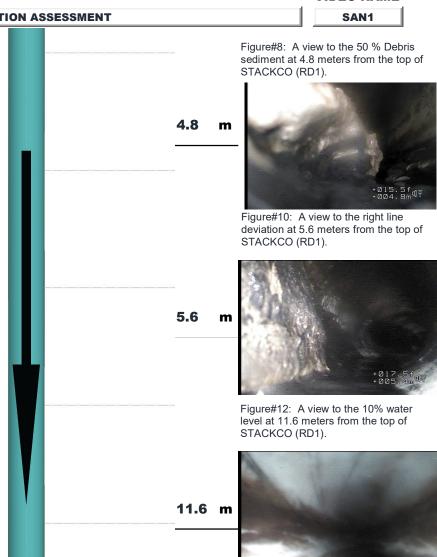


Figure#9: A view to the 60 % Debris sediment at 5.0 meters from the top of STACKCO (RD1).



Figure#11: A view to the 5% water level at 6.6 meters from the top of STACKCO (RD1).





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PROJECT NAME VIDEO NAME SANITARY SEWER LATERAL CCTV CONDITION ASSESSMENT SAN1 Figure#13: A view to the 30% water Figure#14: A view to the camera under level at 12.8 meters from the top of murky water at 15.8 meters from the top STACKCO (RD1). of STACKCO (RD1). 12.8 m 15.8 m Figure#15: Abandoned due to debris under the murky water and debris sediment at 21.2 meters from the stack 21.2 m m m m

Sewerteks Inc.



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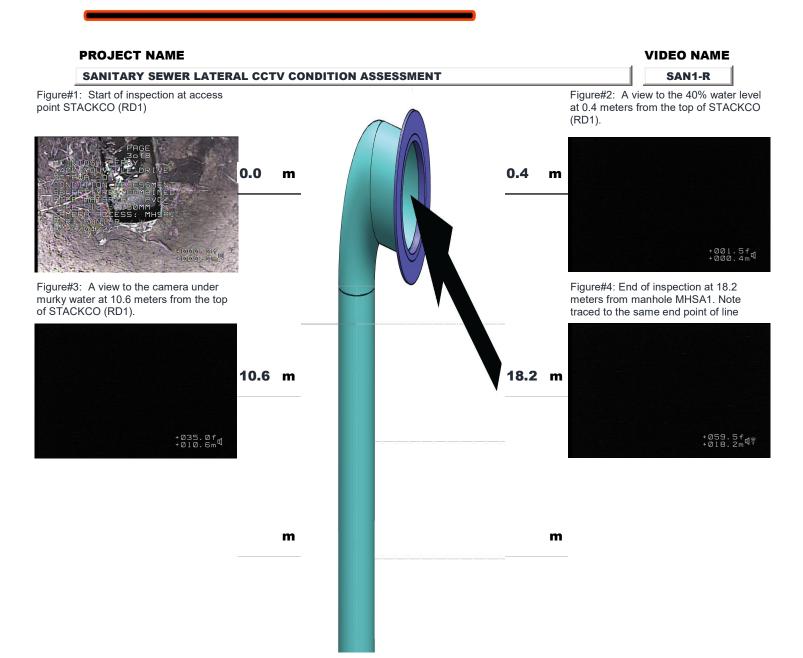
Date	4/24/2023	Sewer T	уре	СОМВІ	NE			Pipe	Size (mm)	100/150MM
Client	McINTOSH PERRY					Work	order	•	531	
Contact	CURTIS MELANSON						Pipe Material		ABS/PV0	
Start	MHSA1					Came	ra Dir	ection	Against	Flow
End	18.2 METERS TO STACKO	O (RD1)				DVD#	/USB#	‡	1	
Further Location	THE ACCESS MANHOLE M BUILDING AS SHOWN IN					Video	name	e (PLR)	COMB1-	R.mpg
Details	BUILDING AS SHOWN IN	THE MAP	סנחוז אל	KEPUKI		Repoi	t No		1	
Job Address	140 YOUVILLE STREET OT	TAWA, ON	ITARIO			Opera	itor		Saul Ce	erna
Comments	The camera was under wa 18.2 meter mark where lir flushed and re-camera in o	ne SAN1 fr	om the	stack CÓ	insi	de the	build	ing en	ded. The sew	
DISTANCE (m)	CODE DESCRIPTION		IZE L	ENGTH		OCK ROM	CLC	OCK O	REMARKS	
0.0	Start of inspection								Start at acces	s point STACKCO (RD1).
0.0	Water Level	40		j						
0.4	Camera Under Water								Murky water	
10.6	General observation								camera under	murky water
18.2	Finish Survey								End atline SAI	N1

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Sewerteks Inc.



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Date	4/24/2023	Sewer	Туре	COMBI	NE		Pipe Siz	ze (mm)	150MM
Client	McINTOSH PERRY	·			Work	order		531	
Contact	CURTIS MELANSON				Pipe I	Material		ABS/PV	2
Start	MHSA1				Came	ra Direct	tion	With Flo	w
End	CITY MAIN LINE				DVD#	/USB#		1	
Further	THE ACCESS MANHOLE					name (F	PLR)	COMB2.	mpg
Location Details	BUILDING AS SHOWN I	N THE MAP	OF THI	S REPORT.	Repoi	rt No		1	
Job Address	140 YOUVILLE STREET	OTTAWA, O	NTARIC)	Opera	ator		Saul Ce	erna
Comments	The camera was under winspection ended at the conflushed and re-camera in	city sewer r	main line	e at 12.6 r	neters fror	n manh	ole MHS		
DISTANCE (m)	inspection ended at the	city sewer in order to	main line determi	e at 12.6 r ne the true	neters from condition	m manho of the p	ole MHS pipe.		
DISTANCE	inspection ended at the of flushed and re-camera in	city sewer in order to	main line determi	e at 12.6 r ne the true	neters fror condition	m manho of the p	ole MHS pipe.	SA. The s	
DISTANCE (m)	inspection ended at the of flushed and re-camera in	city sewer in order to	main line determi	e at 12.6 r ne the true	neters from condition	m manho of the p	ole MHS pipe.	SA. The s	ewer line needs to b e
DISTANCE (m) 0.0	inspection ended at the of flushed and re-camera in CODE DESCRIPTION Start of inspection	city sewer ron order to	main line determi	e at 12.6 r ne the true	neters from condition	m manho of the p	ole MHS pipe.	SA. The s	ewer line needs to b e
0.0 0.0	inspection ended at the of flushed and re-camera in CODE DESCRIPTION Start of inspection Water Level	city sewer ron order to	main line determi	e at 12.6 r ne the true	neters from condition	m manho of the p	ole MHS pipe. K RE	SA. The s	ewer line needs to b e
0.0 0.0 0.0	inspection ended at the of flushed and re-camera in CODE DESCRIPTION Start of inspection Water Level Camera Under Water	city sewer in order to	main line determi	e at 12.6 r ne the true	neters from condition	m manho of the p	ole MHS pipe. K RE Sta	EMARKS rt at acces	ewer line needs to b e
0.0 0.0 0.0 4.6	inspection ended at the of flushed and re-camera in CODE DESCRIPTION Start of inspection Water Level Camera Under Water Debris	city sewer in order to	main line determi	e at 12.6 r ne the true	neters from condition	m manho of the p	ole MHS pipe. K RE Sta	EMARKS rt at acces	ewer line needs to b e
0.0 0.0 0.0 0.0 4.6 5.0	inspection ended at the of flushed and re-camera in CODE DESCRIPTION Start of inspection Water Level Camera Under Water Debris General observation	city sewer in order to	main line determi	e at 12.6 r ne the true	neters from condition	m manho of the p	Sta Sed Carr	EMARKS rt at acces	s point MHSA1.
0.0 0.0 0.0 4.6 5.0	inspection ended at the of flushed and re-camera in CODE DESCRIPTION Start of inspection Water Level Camera Under Water Debris General observation Camera Above Water	city sewer in order to	main line determi	e at 12.6 r ne the true	neters from condition	m manho of the p	Sta Sed Carr To tl	MARKS rt at acces	s point MHSA1. locked by sediment

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PROJECT NAME VIDEO NAME

SANITARY SEWER LATERAL CCTV CONDITION ASSESSMENT

SAN2

Figure#1: Start of inspection at access point MHSA1



0.0 m

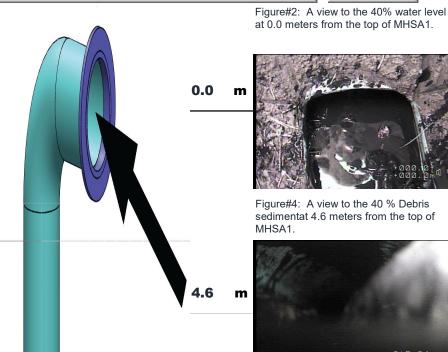
m

Figure#3: A view to the camera under the murky water at 0.0 meters from the top of MHSA1.



Figure#5: A view to the Camera lens blocked by sediment at 5.4 meters from the top of MHSA1.





11.0 m

Sewerteks Inc.



Figure#6: A view to the camera abovce

water at 11.0 meters from the top of

MHSA1.

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PROJECT NAME VIDEO NAME

SANITARY SEWER LATERAL CCTV CONDITION ASSESSMENT

SAN2

Figure#7: A view to the line deviation downwards at 11.4 meters from the top of MHSA1.



11.4 m

Figure#9: A view to the end point CITY MAIN LINE at 12.4 meters from the top of MHSA1.



12.6 m

m

Figure#8: A view to the line deviation downwards at 11.8 meters from the top of MHSA1

11.8 m



m

m

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Observations

Problem

Structural Condition - Brickwork

DB – Displaced Bricks DI – Dropped Invert MB – Missing Bricks

Structural Condition - Mortar Missing

MM - Mortar missing medium MS - Mortar missing slight MT - Mortar missing total

<u>Structural Condition - Surface damage</u>

SSL - Spalling large SSM - Spalling medium SSS - Spalling slight SWL - Wear large SWM - Wear medium SWS - Wear slight

<u>Structural Condition – Joint Displaced</u>

JDL – Joint Displaced Large JDM – Joint Displaced Medium

Structural Condition - Open Joint

OJL – Open Joint Large OJM – Open Joint Medium

<u>Structural Condition – Cracked</u>

CC – Crack Circumferential CL – Crack Longitudinal CM – Crack multiple

Structural Condition - Fractured

FC – Fracture Circumferential FL – Fracture Longitudinal FM – Fracture Multiple

Structural Condition – Broken (pipe sewers)

B- Broken H – Hole

<u>Structural Condition – Deformed</u>

D – Deformed Sewer

Structural Condition – Collapsed

X – Collapsed

Construction Features - Connection

CN – Connection

CNI – Connection intruding CX – Connection defective

CXI - Connection defective intruding

WYE - End point connection / End of a line

Construction Features – Junction

JN – Junction

JX – Junction Defective

Construction Features – Lining defect

LN – Lining defect

Construction Features – Major branch

BR – Branch major

Construction Features – Manhole/node

MH – Manhole/Node

Miscellaneous Features

CU – Camera underwater

DC – Dimension of sewers changes

GO - General Observation

GP – General Photograph

LC – Lining Change

MC – Material change

PC – Pipe length change

SC – Shape change

V – Vermin (rats and/or mice)

WL - Water Level

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Service Defects – Roots

RF – Roots fine

RFJ – Roots fine at joint

RM – Roots mass

RMJ – roots mass at joint

RT – Roots tap

RJ – Roots tap at joint

<u>Service Defects – Infiltration</u>

ID – Infiltration dripper

IDJ – Infiltration dripper at joint

IG – Infiltration gusher

IGJ – Infiltration gusher at joint

IR – Infiltration runner

IRJ – Infiltration runner at joint

IS – Infiltration seeper

ISJ – Infiltration seeper at joint

Service Defects – Encrustation

EH – Encrustation heavy

EHJ – Encrustation heavy at joint

EL – Encrustation light

ELJ – Encrustation light at joint

EM – Encrustation medium

EMJ – Encrustation medium at joint

Service Defects – Debris

DE – Debris

DEG – Debris grease

DES – Debris silt

Service Defects – Line

LD – Line deviates down

LL – Line deviates left

LR – Line deviates right

LU – Line deviates up

Service Defects – Obstruction

OB – Debris grease

Other Codes

Inspections

CID – Continue inspection downstream

CIU – Continue inspection upstream

FH - Finish Survey

SA – Survey abandoned

ST – Start of Survey

Weather

- 1- Dry
- 2- Heavy Rain
- 3- Light Rain
- 4- Showers
- 5- Snow

Reasons & Purpose

- A- Structural or service condition defects
- **B-** Infiltration
- C- Assessment of complete remedial or renovation works
- D- Pre-adoption
- E- Pre-acceptance
- F- Sample survey to determine asset condition
- G- Associated with future capital scheme including drainage area planning
- H- Resurvey for any reason
- X- Other
- Z- Not known

Surface Type & Location

- A- Main road (urban)
- B- Main road (suburban/rural)
- C- Light road
- D- Footpath or verge (within the highway boundary)
- E- Fields (farmland and public open space)
- F- Gardens (within private property)
- G- Woodland
- X- Difficult access (motorway, railway, watercourse, inside building)

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Pipe Type

AC – Alkathene

AK – Alkathene

BR – Brick

CC – Concrete box culvert

CI – Cast Iron

CO – Concrete

CSB – Concrete segments (bolted)

CSU – Concrete segments (unbolted)

DI – Ductile Iron

GRC – Glass reinforced cement

GRP – Glass reinforced plastic

MAC – Masonry (in regular courses)

MAR – Masonry (randomly coursed)

PE – Polyethylene

PF - Pitch fibre

PP – Polypropylene

PSC – Plastic/steel composite

PVC – Polyvinyl chloride

RPM – Reinforced plastic matrix

SI – Spun (grey) iron

ST – Steel

TRA - Transite

VC – Vitrified clay

XXX – Other

ZZZ – Not known

Pipe Shape

A- Arched (with flat bottom)

B- Barrel

C- Circular

E- Egg shaped

H- Horseshoe

O- Oval

R- Rectangular

S- Square

T- Trapezoidal

U- U-shaped with flat top

X- Other

Use of Sewer

A- Combined

F- Foul

S- Surface water

T- Trade effluent

W- Watercourse (culverted)

X- Other

Z- Not known

Lining Method

BL – Bitumen

CL – Cement

CPP – Cured in place

IS – Soft inversion type liner

PL – Plastic

RL – Resin

XXX – Other

ZZ – Not known

Pre-Cleaning

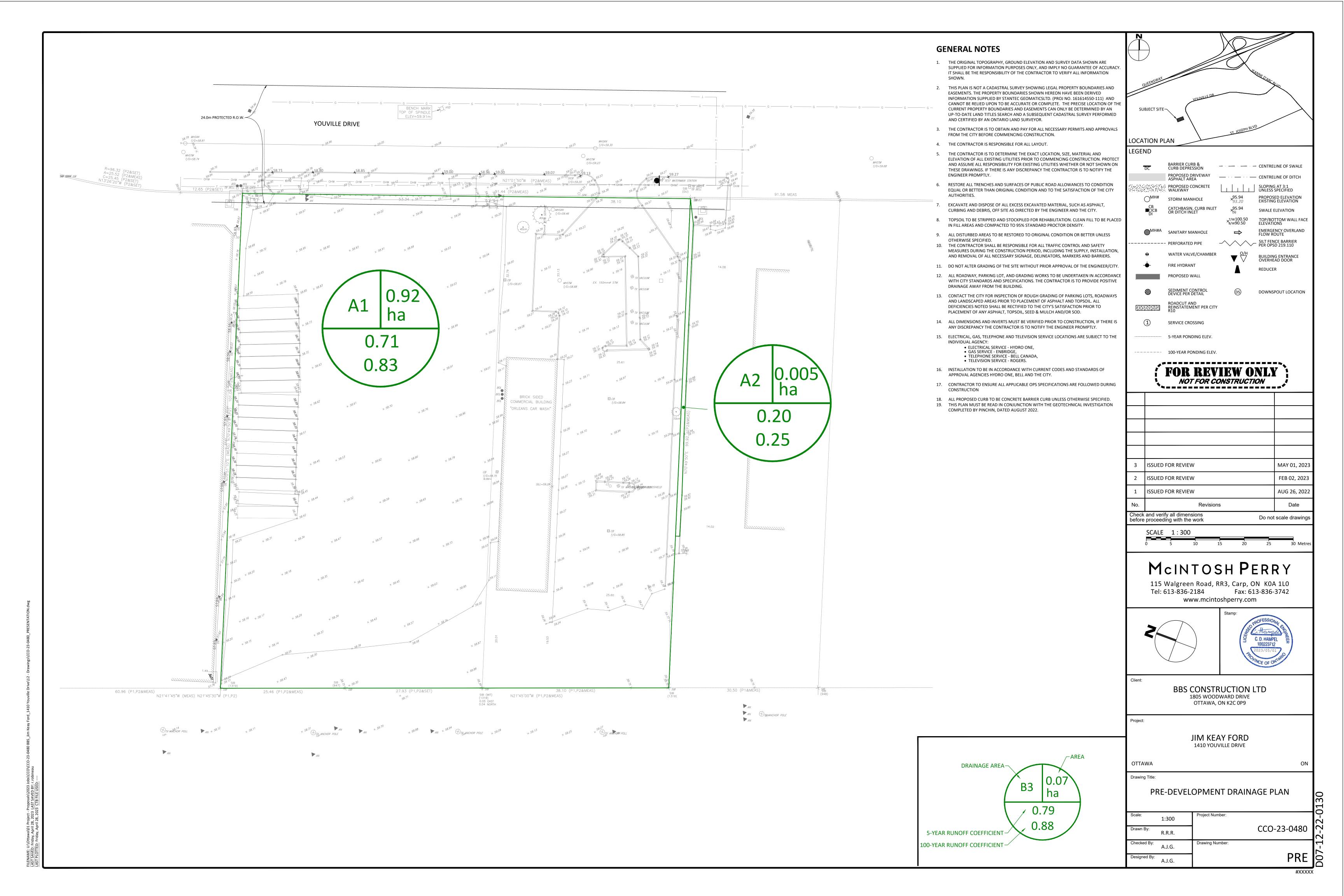
N- No pre-cleaning

Y- Pre-cleaning was carried out

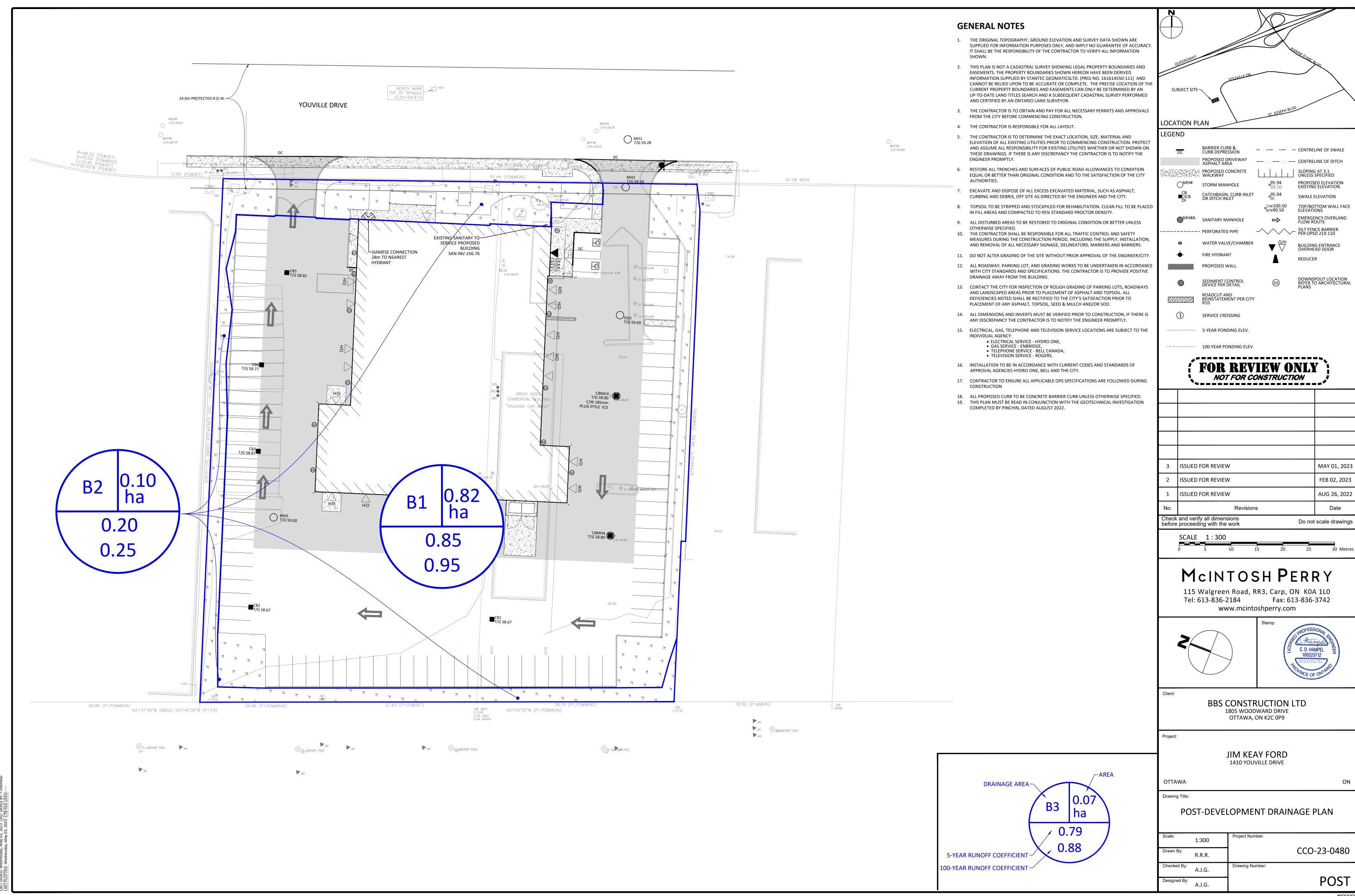
Z- Not known

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APPENDIX E PRE-DEVELOPMENT DRAINAGE PLAN



APPENDIX F POST-DEVELOPMENT DRAINAGE PLAN



APPENDIX G STORMWATER MANAGEMENT CALCULATIONS

CO-22-0480 - Youville Drive - SWM Calculations

1 of 4

Tc (min)		nsity n/hr)	
(11111)	5-Year	100-Year	
10	104.2	178.6	PRE-DEVELOPMENT
10	104.2	178.6	POST-DEVELOPMENT

C-Values								
Impervious	0.90							
Gravel	0.60							
Pervious	0.20							

Pre-Development Runoff Coefficient

Drainage Area	Impervious Area (m²)	Gravel (m²)	Pervious Area (m²)	Average C (5-year)	Average C (100-year)
A1	4,214	4,258	716	0.71	0.83
A2	0	0	54	0.20	0.25

Pre-Development Runoff Calculations

Drainage	Area	Area C C		Tc	Q (L/s)	
Area	(ha)	5-Year	100-Year	(min)	5-Year	100-Year
A1	0.92	0.71	0.83	10	188.01	376.59
A2	0.005	0.20	0.25	10	0.31	0.66
Total	0.92				188.31	377.25

*External drainage

Post-Development Runoff Coefficient

Drainage Area	Impervious Area (m²)	Gravel (m²)	Pervious Area (m²)	Average C (5-year)	Average C (100-year)
B1	7,610	0	598	0.85	0.95
B2	0	0	1,033	0.20	0.25

Post-Development Runoff Calculations

Drainage	Area	С	C	Tc	Q (L/s)	
Area	(ha)	5-Year	100-Year	(min)	5-Year	100-Year	
B1	0.82	0.85	0.95	10	201.86	385.20	Restricted
B2	0.10	0.20	0.25	10	5.99	12.82	Unrestricted
Total	0.92				207.85	398.03	

Required Restricted Flow

Drainage	Area	С	Tc	Q (L/s)	
Area	(ha)	5-Year	(min)	5-Year	
A1	0.92	0.50	10	133.07	Ī
A2	0.005	0.20	10	0.31	*Exteri
Total				133.38	Ī

*External Drainage area added to target flow rate

Post-Development Restricted Runoff Calculations

Drainage Area	Unrestricted Flow (L/S)		Restricted Flow (L/S)		Storage Required (m³)		Storage Provided (m³)	
Alea	5-year	100-Year	5-Year	100-Year	5-Year	100-Year	5-Year	100-Year
B1	201.86	385.20	114.91	116.68	51.0	172.8	60.1	189.3
B2	5.99	12.82	5.99	12.82	-	-	-	-
Total	207.85	398.03	120.90	129.50				

CO-22-0480 - Youville Drive - SWM Calculations

Storage Requirements for Area B1

5-Year Storm Event

Tc (min)	l (mm/hr)	Runoff (L/s)	Allowable Outflow	Runoff to be Stored	Storage Required
. ,	, ,	B1	(L/s)	(L/s)	(m ³)
1	203.5	394.26	114.91	279.35	16.76
6	131.6	254.96	114.91	140.05	50.42
11	99.2	192.19	114.91	77.28	51.01
16	80.5	155.96	114.91	41.05	39.41
21	68.1	131.94	114.91	17.03	21.45

Maximum Storage Required 5-year = 51 m³

100-Year Storm Event

Tc (min)	l (mm/hr)	Runoff (L/s) B1	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
1	351.4	758.07	116.68	641.39	38.48
6	226.0	487.55	116.68	370.87	133.51
11	169.9	366.52	116.68	249.84	164.90
16	137.5	296.63	116.68	179.95	172.75
21	116.3	250.89	116.68	134.21	169.11
26	101.2	218.32	116.68	101.64	158.56
31	89.8	193.73	116.68	77.05	143.30
36	81.0	174.74	116.68	58.06	125.41
41	73.8	159.21	116.68	42.53	104.62
46	68.0	146.70	116.68	30.02	82.84

Maximum Storage Required 100-year = 173 m³

5-Year Storm Event Storage Summary

		Wate	er Elev. (m) =	58			
	Location	T/G	INV. (out)	Depth (m)	Head (m)	Volum	e (m³)
	CBMH3	58.80	56.21	0.09	2.59	60).1

Storage Available (m³) = 60.1 Storage Required (m³) = 51.0

100-Year Storm Event Storage Summary

		Wate	er Elev. (m) =	58	.97	
Location	T/G	INV. (out)	Depth (m)	Head (m)	Volume (m	3)
CBMH3	58.80	56.21	0.17	2.67	189.3	

Storage Available (m³) = 189.3 Storage Required (m³) = 172.8 2 of 4

^{*}Available Storage calculated from AutoCAD

CO-22-0480 - Youville Drive - SWM Calculations

For Orifice Flow, C= 0.60
For Weir Flow, C= 1.84

	Orifice 1	Orifice 2	Weir 1	Weir 2
invert elevation	56.21	Х	X	X
center of crest elevation	56.30	Х		Χ
orifice width / weir length	185 mm	Х	X	X
weir height				X
orifice area (m²)	0.027	X	Х	X

Elevation Discharge Table - Storm Routing

Elevation	Orif	ice 1		ice 2		eir 1	W€	eir 2	Total	Ī	
Elevation	H [m]	Q [m ³ /s]	Q [L/s]								
56.21	Х	Х	Х	Х	Х	Х	Х	Х	0.00		
56.22	Х	Х	Х	Х	Х	Х	Х	Х	0.00		
56.23	Х	Х	Х	Х	Х	Х	Х	Х	0.00		
56.24	Х	Х	Х	Х	Х	Х	Х	Х	0.00		
56.25	Х	Х	Х	Х	Х	Х	Х	Х	0.00		
56.26	Х	Х	Х	Х	Х	Х	Х	Х	0.00		
56.27	Х	Х	Х	Х	Х	Х	Х	Х	0.00		
56.28	Х	Х	Х	Х	Х	Х	Х	Х	0.00		
58.64	2.34	0.11	Х	Х	Х	Х	Х	Х	109.22		
58.65	2.35	0.11	Х	Х	Х	Х	Х	Х	109.46		
58.66	2.36	0.11	Х	Х	Х	Х	Х	Х	109.69		
58.67	2.37	0.11	Х	Х	Х	Х	Х	Х	109.92	1	
58.68	2.38	0.11	Х	Х	Х	Х	Х	Х	110.15]	
58.69	2.39	0.11	Х	Х	Х	Х	Х	Х	110.38		
58.70	2.40	0.11	Х	Х	Х	Х	Х	Х	110.62]	
58.71	2.41	0.11	Х	Х	Х	Х	Х	Х	110.85		
58.72	2.42	0.11	Х	Х	Х	Х	Х	Х	111.08		
58.73	2.43	0.11	Х	Х	Х	Х	Х	Х	Х	111.31	
58.74	2.44	0.11	Х	Х	Х	Х	Х	Х	111.53		
58.75	2.45	0.11	Х	Х	Х	Х	Х	Х	111.76		
58.76	2.46	0.11	Х	Х	Х	Х	Х	Х	111.99		
58.77	2.47	0.11	Х	Х	Х	Х	Х	Х	112.22		
58.78	2.48	0.11	Х	Х	Х	Х	Х	Х	112.45		
58.79	2.49	0.11	Х	Х	Х	Х	Х	Х	112.67		
58.80	2.50	0.11	Х	Х	Х	Х	Х	Х	112.90		
58.81	2.51	0.11	Х	Х	Х	Х	Х	Х	113.12		
58.82	2.52	0.11	Х	Х	Х	Х	Х	Х	113.35		
58.83	2.53	0.11	Х	Х	Х	Х	Х	Х	113.57		
58.84	2.54	0.11	Х	Х	Х	Х	Х	Х	113.80	ļ	
58.85	2.55	0.11	Х	Х	Х	Х	Х	Х	114.02	1	
58.86	2.56	0.11	Х	Х	Х	Х	Х	Х	114.25	1	
58.87	2.57	0.11	Х	Х	Х	Х	Х	Х	114.47	1	
58.88	2.58	0.11	Х	Х	Х	Х	Х	Х	114.69		
58.89	2.59	0.11	Х	Х	Х	Х	Х	Х	114.91	5-Yea	
58.90	2.60	0.12	Х	Х	Х	Х	Х	Х	115.14		
58.91	2.61	0.12	Х	Х	Х	Х	Х	Х	115.36	1	
58.92	2.62	0.12	Х	Х	Х	Х	Х	Х	115.58	<u> </u>	
58.93	2.63	0.12	Х	Х	Х	Х	Х	Х	115.80	<u> </u>	
58.94	2.64	0.12	Х	Х	Х	Х	Х	Х	116.02	1	
58.95	2.65	0.12	Х	Х	Х	Х	Х	Х	116.24		
58.96	2.66	0.12	Х	Х	Х	Х	Х	Х	116.46		
58.97	2.67	0.12	Х	Х	Х	Х	Х	Х	116.68	100-Y	

Notes: 1. For Orifice Flow, User is to Input an Elevation Higher than Crown of Orifice.

- 2. Orifice Equation: Q = cA(2gh)^{1/2}
- 3. Weir Equation: Q = CLH^{3/2}
- ${\it 4. These \ Computations \ Do \ Not \ Account \ for \ Submergence \ Effects \ Within \ the \ Pond \ Riser.}$
- 5. H for orifice equations is depth of water above the centroide of the orifice.
- $\ensuremath{\mathsf{6}}.\ensuremath{\,\mathsf{H}}$ for weir equations is depth of water above the weir crest.

CO-22-0480 - Youville Drive - SWM Calculations

4 of 4

Time of Concentration Pre-Development

Drainage Area	Sheet Flow	Slope of	Tc (min)	Tc (min)
ID	Distance (m)	Land (%)	(5-Year)	(100-Year)
A1	51	1.54	8	6

Therefore, a Tc of 10 can be used

Tc= (3.26(1.1-c)L^0.5/S^0.33)

c = Balanced Runoff Coefficient
 L = Length of drainage area
 S = Average slope of watershed

STORM SEWER DESIGN SHEET

PROJECT: Jim Keay Ford

LOCATION: 1400-1410 Youville Drive
CLIENT: BBS Construction

	LOCATION				CONTRIBUTING AREA (ha)							RATIO	ONAL DESIGN	FLOW									SEWER DATA	A								
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28					
STREET	AREA ID	FROM	TO	C-VALUE	AREA	INDIV	CUMUL	INLET	TIME	TOTAL	i (5)	i (10)	i (100)	5yr PEAK	10yr PEAK	100yr PEAK	FIXED	DESIGN	CAPACITY	LENGTH		PIPE SIZE (mm)	SLOPE	VELOCITY	AVAIL C	AP (5yr)					
JIKELI	AKLATO	MH	MH	C-VALUE	ANLA	AC	AC	(min)	IN PIPE	(min)	(mm/hr)	(mm/hr)	(mm/hr)	FLOW (L/s)	(L/s)	(m)	DIA	W	Н	(%)	(m/s)	(L/s)	(%)									
	B1	CB5	MH5	0.85	0.45	0.38	0.38	10.00	0.99	10.99	104.19	122.14	178.56	110.70				110.70	131.34	47.31	450			0.20	0.800	20.65	15.72%					
		MH5	CBMH4	0.85	0.21	0.18	0.56	10.99	1.09	12.08	99.26	116.33	170.02	155.25				155.25	162.91	65.07	450			0.30	0.992	7.67	4.71%					
		CBMH4	CBMH3	0.85	0.16	0.14	1.08	12.08	0.33	12.41	94.36	110.56	161.56	283.51				283.51	300.97	26.97	525			0.45	1.347	17.46	5.80%					
		CBMH3	OGS	-	-	-	1.08	12.41	0.19	12.61	92.97	108.93	159.15	279.33				279.33	300.97	15.62	525			0.45	1.347	21.64	7.19%					
		OGS	MH2	-	-	-	1.08	12.61	0.30	12.91	92.19	108.00	157.80	276.98				276.98	300.97	24.27	525			0.45	1.347	23.99	7.97%					
		MH2	MH1	-	-	-	1.08	12.91	0.11	13.02	91.00	106.60	155.74	273.40				273.40	300.97	9.22	525			0.45	1.347	27.57	9.16%					
D C 111				N						DDD			NI.					L														
Definitions:				Notes:				Designed:		RRR			No.					Revision							Date							
Q = 2.78CiA, where:				Mannings coefficient (n)	=		0.013																									
Q = Peak Flow in Litre																																
A = Area in Hectares								Checked:		AJG																						
	in millimeters per hour (mi																															
[i = 998.071 / (TC+6		5 YEAR																														
[i = 1174.184 / (TC-	+6.014)^0.816]	10 YEAR						Project No.:		CCO-23-0480					-									-								
[i = 1735.688 / (TC-	+6.014)^0.820]	100 YEAR															Da	ate:							Sheet No:							
																	2023	-01-31							1 of 1							

Hydro Downstream Defender®



99.9%

Net Annual Water Quality Worksheet
Rev. 11.1 Net Annual Removal Model: DD8 Project Name: 1400-1410 Youville Drive Report Date: Paste DD8 **Weighted Net** Fraction of Street: City: Ottawa Intensity⁽¹⁾ Removal Annual Rainfall⁽¹⁾ Province: Ontario Country: Canada Efficiency⁽²⁾ Efficiency⁽⁴⁾ email: Designer: (mm/hr) (%) (%) (%) 0.50 0.1% 100.0% 0.09% Treatment Parameters 1.00 14.1% 100.0% 14.11% **RESULTS SUMMARY** Structure ID:
TSS Goal: 80 % Removal 1.50 14.2% 100.0% 14.20% 2.00 14.1% 100.0% 14.12% Model TSS Volume TSS Particle Size: Fine 2.50 4.2% 100.0% 4.16% DD4 76.0% 97.5% *Area:* 0.82 ha DD6 86.0% 99.5% 3.00 1.5% 97.3% 1.45% Percent Impervious: 93% DD8 3.50 8.5% 94.9% 8.11% 91.0% 99.9% Rational C value: 0.95 Calc Cn DD10 94.0% 100.0% 4.00 5.4% 92.9% 5.04% Rainfall Station: Ottawa, ONT DD12 96.0% 99.9% 4.50 1.2% 91.1% 1.06% Peak Storm Flow: 116.68 L/s
Peak Storm Return: 100 yrs 5.00 5.5% 89.5% 4.95% 6.00 4.3% 86.9% 3.76% 7.00 4.5% 3.83% 84.8% **Model Specification** 8.00 3.1% 82.9% 2.56% 9.00 2.3% 1.90% 81.4% Select Model DD8 2.05% 10.00 2.6% 80.0% Diameter: 2400 mm 20.00 9.2% 71.4% 6.60% 30.00 2.6% 66.9% 1.75% Peak Flow Capacity: 425.00 L/s OK 40.00 1.2% 63.9% 0.74% **Sediment Storage:** 3.56 m³ 50.00 0.5% 63.9% 0.34% Oil Storage: 2044.00 L 0.7% 100.00 63.9% 0.46% 150.00 0.04% 0.1% 63.9% Installation Configuration 200.00 0.0% 63.9% 0.00% Placement: Online **Total Net Annual Removal Efficiency:** 91.0%

Outlet Pipe Size: 525 mm 600 to 525 matched invert coupler required

Inlet Pipe 1 Size: 525 mm OK
Inlet Pipe 2 Size: mm OK

Rim Level: 59,000 m Calc Invs. Outlet Pipe Invert: 56.120 m OK Invert Pipe 1: 56.140 m OK

Invert Pipe 2:

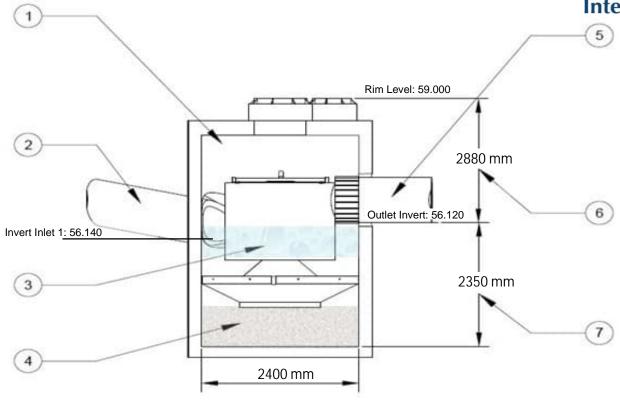
Total Annual Runoff Volume Treated: Rainfall Data: 1960:2007, HLY03, Ottawa, ONT, 6105976 & 6105978.

- 2. Based on third party verified data and appoximating the removal of a PSD similar to Rainfall adjusted to 5 min peak intensity based on hourly average.
- 4. Factored to account for bypass flow.

Designer Notes:

Hydro Downstream Defender®





All drawing elevations are metres.

DD8 Specification

1	Vortex Chamber Diameter	2400 mm
2	Inlet Pipe Diameter	525 mm
3	Oil Storage Capacity	2044 L
4	Min. Provided Sediment Storage Capacity	3.56 m ³
5	Outlet Pipe Diameter	525 mm
6	Rim to Outlet Invert	2880 mm
7	Outlet Invert to Sump	2350 m
	Total Depth	5230 mm

Notes:	
T. D	

The Downstream Defender is certified by Canada ETV

APPENDIX H
CITY OF OTTAWA DESIGN CHECKLIST

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City of Ottawa

4. Development Servicing Study Checklist

The following section describes the checklist of the required content of servicing studies. It is expected that the proponent will address each one of the following items for the study to be deemed complete and ready for review by City of Ottawa Infrastructure Approvals staff.

The level of required detail in the Servicing Study will increase depending on the type of application. For example, for Official Plan amendments and re-zoning applications, the main issues will be to determine the capacity requirements for the proposed change in land use and confirm this against the existing capacity constraint, and to define the solutions, phasing of works and the financing of works to address the capacity constraint. For subdivisions and site plans, the above will be required with additional detailed information supporting the servicing within the development boundary.

4.1 General Content

Criteria	Location (if applicable)
Executive Summary (for larger reports only).	N/A
Date and revision number of the report.	On Cover
 Location map and plan showing municipal address, boundary, and layout of proposed development. 	Appendix A
$\ \square$ Plan showing the site and location of all existing services.	Site Servicing Plan (C102)
Development statistics, land use, density, adherence to zoning and official plan, and reference to applicable subwatershed and watershed plans that provide context to which individual.	1.1 Purpose1.2 Site Description
watershed plans that provide context to which individual developments must adhere.	·
	6.0 Stormwater Management
 Summary of pre-consultation meetings with City and other approval agencies. 	Appendix B
 Reference and confirm conformance to higher level studies and reports (Master Servicing Studies, Environmental Assessments, 	1.1 Purpose
Community Design Plans), or in the case where it is not in conformance, the proponent must provide justification and	1.2 Site Description
develop a defendable design criteria.	6.0 Stormwater Management
\square Statement of objectives and servicing criteria.	3.0 Pre-Consultation Summary



☐ Identification of existing and proposed infrastructure available in the immediate area.	N/A
☐ Identification of Environmentally Significant Areas, watercourses and Municipal Drains potentially impacted by the proposed development (Reference can be made to the Natural Heritage Studies, if available).	Site Grading Plan (C101)
☐ Concept level master grading plan to confirm existing and proposed grades in the development. This is required to confirm the feasibility of proposed stormwater management and drainage, soil removal and fill constraints, and potential impacts to neighbouring properties. This is also required to confirm that the proposed grading will not impede existing major system flow paths.	Site Grading Plan (C101)
 Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts. 	N/A
☐ Proposed phasing of the development, if applicable.	N/A
Reference to geotechnical studies and recommendations concerning servicing.	Section 2.0 Background Studies, Standards and References
 All preliminary and formal site plan submissions should have the following information: Metric scale North arrow (including construction North) Key plan Name and contact information of applicant and property owner Property limits including bearings and dimensions Existing and proposed structures and parking areas Easements, road widening and rights-of-way Adjacent street names 	Site Grading Plan (C101)

4.2 Development Servicing Report: Water

Criteria	Location (if applicable)
☐ Confirm consistency with Master Servicing Study, if available	N/A
 Availability of public infrastructure to service proposed development 	N/A
☐ Identification of system constraints	N/A
☐ Identify boundary conditions	Appendix C
☐ Confirmation of adequate domestic supply and pressure	N/A
 Confirmation of adequate fire flow protection and confirmation that fire flow is calculated as per the Fire Underwriter's Survey. Output should show available fire flow at locations throughout the development. 	Appendix C
 Provide a check of high pressures. If pressure is found to be high, an assessment is required to confirm the application of pressure reducing valves. 	N/A
 Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defined phases of the project including the ultimate design 	N/A
☐ Address reliability requirements such as appropriate location of shut-off valves	N/A
☐ Check on the necessity of a pressure zone boundary modification.	N/A
Reference to water supply analysis to show that major infrastructure is capable of delivering sufficient water for the proposed land use. This includes data that shows that the expected demands under average day, peak hour and fire flow conditions provide water within the required pressure range	Appendix C, Section 4.2

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 Description of the proposed water distribution network, including locations of proposed connections to the existing system, provisions for necessary looping, and appurtenances (valves, pressure reducing valves, valve chambers, and fire hydrants) including special metering provisions. 	Site Servicing Plan (C101)
 Description of off-site required feedermains, booster pumping stations, and other water infrastructure that will be ultimately required to service proposed development, including financing, interim facilities, and timing of implementation. 	N/A
☐ Confirmation that water demands are calculated based on the City of Ottawa Design Guidelines.	Appendix C
 Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference. 	N/A

4.3 Development Servicing Report: Wastewater

Criteria	Location (if applicable)
☐ Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitored flow data from relatively new infrastructure cannot be used to justify capacity requirements for proposed infrastructure).	N/A
Confirm consistency with Master Servicing Study and/or justifications for deviations.	N/A
☐ Consideration of local conditions that may contribute to extraneous flows that are higher than the recommended flows in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers.	N/A
Description of existing sanitary sewer available for discharge of wastewater from proposed development.	Section 5.2 Proposed Sanitary Sewer

☐ Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable)	Section 5.3 Proposed Sanitary Design
☐ Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format.	N/A
 Description of proposed sewer network including sewers, pumping stations, and forcemains. 	Section 5.2 Proposed Sanitary Sewer
☐ Discussion of previously identified environmental constraints and impact on servicing (environmental constraints are related to limitations imposed on the development in order to preserve the physical condition of watercourses, vegetation, soil cover, as well as protecting against water quantity and quality).	N/A
 Pumping stations: impacts of proposed development on existing pumping stations or requirements for new pumping station to service development. 	N/A
☐ Forcemain capacity in terms of operational redundancy, surge pressure and maximum flow velocity.	N/A
☐ Identification and implementation of the emergency overflow from sanitary pumping stations in relation to the hydraulic grade line to protect against basement flooding.	N/A
☐ Special considerations such as contamination, corrosive environment etc.	N/A

4.4 Development Servicing Report: Stormwater Checklist

Criteria	Location (if applicable)
 Description of drainage outlets and downstream constraints including legality of outlets (i.e. municipal drain, right-of-way, watercourse, or private property) 	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
☐ Analysis of available capacity in existing public infrastructure.	N/A
 A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns, and proposed drainage pattern. 	Pre & Post-Development Plans
☐ Water quantity control objective (e.g. controlling post-development peak flows to pre-development level for storm events ranging from the 2 or 5-year event (dependent on the receiving sewer design) to 100-year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
☐ Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
 Description of the stormwater management concept with facility locations and descriptions with references and supporting information. 	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
Set-back from private sewage disposal systems.	N/A
☐ Watercourse and hazard lands setbacks.	N/A
Record of pre-consultation with the Ontario Ministry of Environment and the Conservation Authority that has jurisdiction on the affected watershed.	N/A
☐ Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists.	N/A
☐ Storage requirements (complete with calculations) and conveyance capacity for minor events (1:5-year return period) and major events (1:100-year return period).	Appendix G

☐ Identification of watercourses within the proposed development and how watercourses will be protected, or, if necessary, altered by the proposed development with applicable approvals.	Site Grading Plan
Calculate pre-and post development peak flow rates including a description of existing site conditions and proposed impervious areas and drainage catchments in comparison to existing conditions.	Section 7.0 Proposed Stormwater Management Appendix G
Any proposed diversion of drainage catchment areas from one outlet to another.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
 Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and stormwater management facilities. 	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
☐ If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post-development flows up to and including the 100-year return period storm event.	N/A
☐ Identification of potential impacts to receiving watercourses	N/A
Identification of municipal drains and related approval requirements.	N/A
 Descriptions of how the conveyance and storage capacity will be achieved for the development. 	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
100-year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading.	Site Grading Plan (C101)
☐ Inclusion of hydraulic analysis including hydraulic grade line elevations.	N/A

 Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors. 	Section 8.0 Sediment & Erosion Control
☐ Identification of floodplains – proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions.	N/A
 Identification of fill constraints related to floodplain and geotechnical investigation. 	N/A

4.5 Approval and Permit Requirements: Checklist

The Servicing Study shall provide a list of applicable permits and regulatory approvals necessary for the proposed development as well as the relevant issues affecting each approval. The approval and permitting shall include but not be limited to the following:

Criteria	Location (if applicable)
☐ Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act.	N/A
☐ Application for Certificate of Approval (CofA) under the Ontario Water Resources Act.	N/A
☐ Changes to Municipal Drains.	N/A
 Other permits (National Capital Commission, Parks Canada, Public Works and Government Services Canada, Ministry of Transportation etc.) 	N/A

4.6 Conclusion Checklist

Criteria	Location (if applicable)
Clearly stated conclusions and recommendations	Section 9.0 Summary
	Section 10.0 Recommendations
☐ Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency.	All are stamped
☐ All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario	All are stamped