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# **ADEQUACY OF SERVICES REPORT**

*FOR*

**BARRHAVEN CONSERVANCY  
DEVELOPMENT CORPORATION**

**BARRHAVEN CONSERVANCY EAST  
PHASE 5**

**CITY OF OTTAWA**

**PROJECT NO.: 20-1180**

**DECEMBER 2022 – 1<sup>ST</sup> SUBMISSION**

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- JFSA Memo: *BCDC Phase 5 – Preliminary HGL Analysis (October 2022)*
- JFSA Memo: *Review of Quantity Control Requirement for Jock River Reach 1 (March 2021)*

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## 1.0 INTRODUCTION

David Schaeffer Engineering Limited (DSEL) has been retained to update an Adequacy of Services Report (AES) in support of the Barrhaven Conservancy “Phase 5” development area on behalf of Barrhaven Conservancy Development Corporation (BCDC). This area (being referred to as “Phase 5”) is part of a previously approved draft plan of subdivision within the greater Barrhaven Conservancy development area (City file no. D07-16-20-0021).

The overall Conservancy land area is approximately 139.7 ha (all land use components) and is located within the City of Ottawa urban boundary in the Barrhaven ward. As illustrated in **Figure 1**, the site is located north of the Jock River, east of Highway 416, west of Greenbank Road (and the Kennedy-Burnett Stormwater Facility), and south of both McKenna Casey Drive and Strandherd Drive.

The focus of this report is for the **Conservancy East (Phase 5)** draft plan area consisting of vacant land that is located east of the existing Foster Ditch, which bisects the overall BCDC landholdings, and west of Borrisokane Road. The subject lands are an approximately 19.4 ha irregular parcel including parts of 3288, and 3300 Borrisokane Road. Of this, approximately 13.82 ha in area (including right-of-ways environmental areas and open space) are considered in the servicing review with the proposed updated development draft plan **Figure 2B** provided in the **Drawings** section of this report for reference. Also provided is Figure 2A which illustrates the portion of the prior approved draft plan and the “Phase 5” area being revised. The development area is planned to be developed with a mix of detached single homes, townhomes, park blocks, open spaces and a road network.

The Conservancy East Phase 5 development area is outside of the Jock River 100-year limit as confirmed by the Rideau Valley Conservation Authority (RVCA). Refer to the RVCA confirmation letter in **Appendix D**. The 100-year regulatory flood line is demonstrated in Drawing 1 (Grading) and Drawing 3 (Stormwater) in the **Appendix**.

The objective of this report is to provide sufficient detail to demonstrate that the updated development plan area can be supported by municipal services.

## 1.1 Existing Conditions

The **Conservancy East (Phase 5)** property is relatively flat with the existing elevations ranging from ~91.5 m in the north to 91 m in the south. All existing flows are either overland to the Jock River or conveyed to the Jock River by way of the Foster Ditch and Borrisokane Road ditches which is adjacent to the subject property. The property is within the Jock River watershed and is under the jurisdiction of the RVCA.

## 1.2 Summary of Pre-Consultation

The following provides a summary of the pre-consultation:

### 1.2.1 Ministry of the Environment, Conservation and Parks (MECP)

Prior consultations associated with the Conservancy Phase 2-4 development east of Borrisokane Road were previously undertaken for the approval of those phases of the development area.

A pre-consultation with the local MECP office has not yet been completed for the balance of the Conservancy development area until the functional design details and requirements have been finalized with the City of Ottawa.

### 1.2.2 Rideau Valley Conservation Authority (RVCA)

Multiple consultations, analysis and submissions were coordinated with the RVCA to establish that the development area is outside of the Jock River 100-year limit. See the RVCA documentation in **Appendix D** for reference.

## 1.3 Existing Permits / Approvals

Key approvals associated with the advancement of development of the Barrhaven Conservancy area, are presented in the following table. The most relevant approvals are the Environmental Compliance Approval (ECA) for the South Nepean Collector sanitary trunk sewer as well as sanitary sewer ECA for the Conservancy development area east of Borrisokane Road. The documents are provided in **Appendix A** for reference.

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**Table 1A: Existing Permits / Approvals**

Agency	Approval Type	Approval Number	Remarks
Ministry of the Environment, Conservation and Parks (MECP)	Environmental Compliance Approval	# 8129-AB7LDF (June 23, 2016)	South Nepean Collector existing approval (sanitary outlet for development area)
(MECP)	Environmental Compliance Approval	# 4357-CHMQEM (Sept. 1, 2022)	Sanitary and storm sewer approvals for Conservancy lands east of Borrisokane Road
MECP	Permit to take Water	#5633-C2RQPL (May 26, 2021)	Water taking from Building Excavation, Site Servicing, SWMW, In-Water Works, Ponded Surface Water
Rideau Valley Conservation Authority (RVCA)	RVCA Letter of Permission under O.Reg. 174/06	RV5-4419	Letter of permission related to placement of fill within a regulated area.

#### **1.4 Required Permits / Approvals**

The City of Ottawa must approve detailed engineering design drawings and reports prior to future construction of the municipal infrastructure identified in this report. This will occur as part of the Plan of Subdivision application process and detailed design.

Based on pre-consultation with City staff, the additional approvals and permits listed in the following table are expected to be required prior to construction of the municipal infrastructure detailed herein. Please note that other permits and approvals may be required, as detailed in the other studies to be submitted as part of the Plan of Subdivision application (e.g. *Tree Conservation Report*, *Environmental Impact Statement*, *Phase 1 Environmental Site Assessment*, *Headwater Drainage Feature Assessment*, etc.)

**Table 1B: Required Permits/Approvals**

Agency	Permit/Approval Required	Trigger	Remarks
MECP	Environmental Compliance Approval	Construction of new sanitary and storm sewers throughout the subdivision.	The MECP will review the sanitary and storm sewer design through the City of Ottawa transfer of review process.
MECP	Environmental Compliance Approval	Implementation of oil-grit separator units and LIDs for quality control.	The MECP will review the stormwater management appurtenance design through the City of Ottawa transfer of review process.

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MECP	Permit to Take Water	Construction of proposed land uses (e.g. basements for residential homes) and services.	Pumping of groundwater may be required during construction, given groundwater conditions and proposed land uses and on-site/off-site municipal infrastructure.
City of Ottawa	MECP Form 1 – Record of Watermains Authorized as a Future Alteration.	Construction of watermains throughout the subdivision	The City of Ottawa will review the watermains on behalf of the MECP through the Form 1 – Record of Watermains Authorized as a Future Alteration.
RVCA	Permit under Ontario Regulation 174/06, RVCA's Development, Interference with Wetlands and Alterations to Shorelines and Watercourses Regulation	Grading (proposed development & potential temporary access roads) within the subject lands (i.e. crossing of Fraser-Clarke Watercourse)	Supporting applications and documentation as required through consultation with the RVCA.
RVCA	Outlets to Jock River	In conjunction with issuance of MECP applications	Supporting applications and documentation as required through consultation with the RVCA.
RVCA	Alteration to Watercourses	As necessary through consultation with the RVCA	Supporting applications and documentation as required through consultation with the RVCA.
City of Ottawa	Commence Work Notification (CWN)	Construction of new sanitary and storm sewers throughout the subdivision	The City of Ottawa will issue a commence work notification for construction of the sanitary and storm sewers once an approval is issued by the MECP.

## 2.0 GUIDELINES, PREVIOUS STUDIES, AND REPORTS

### 2.1 Existing Studies, Guidelines, and Reports

The following studies were utilized in the preparation of this report.

- Ottawa Sewer Design Guidelines,  
City of Ottawa, SDG002, October 2012  
*(City Standards)*

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- Technical Bulletin ISDTB-2014-01  
City of Ottawa, February 5, 2014  
(ITSB-2014-01)
- Technical Bulletin PIEDTB-2016-01  
City of Ottawa, September 6, 2016  
(PIEDTB-2016-01)
- Technical Bulletin ISTB-2018-01  
City of Ottawa, March 21, 2018  
(ISTB-2018-01)
- Technical Bulletin ISTB-2018-04  
City of Ottawa, June 27, 2018  
(ISTB-2018-04)
- Ottawa Design Guidelines – Water Distribution  
City of Ottawa, July 2010.  
*(Water Supply Guidelines)*
  - Technical Bulletin ISD-2010-2  
City of Ottawa, December 15, 2010.  
(ISD-2010-2)
  - Technical Bulletin ISDTB-2014-2  
City of Ottawa, May 27, 2014.  
(ISDTB-2014-2)
  - Technical Bulletin ISTB-2018-02 / ISTB-2019-02  
City of Ottawa, March 21, 2018 / July 08, 2019  
(ISTB-2018-02 / ISTB-2019-02)
- Design Guidelines for Sewage Works,  
Ministry of the Environment, Conservation and Parks, 2008. (formerly MOECC)  
*(MECP Design Guidelines)*
- Stormwater Planning and Design Manual,  
Ministry of the Environment, March 2003.  
*(SWMP Design Manual)*
- City of Ottawa Official Plan,  
adopted by Council 2003.  
*(Official Plan)*
- City of Ottawa Secondary Plan – Former Nepean – South Nepean Urban Area –  
Areas 9 and 10,  
Adopted by Council 2003.  
*(Secondary Plan)*

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- South Nepean Collector: Phase 2 Hydraulics Review / Assessment Technical Memorandum  
Novatech, August 2015  
(*Novatech SNC Memo*)
- South Nepean Collector: Phase 2 Preliminary Design Report,  
Novatech, March 2016  
(*Novatech SNC Design Report*)
- Strandherd Drive Widening Project, South Nepean Collector: Phase 3 Sanitary Flow Calculations  
Novatech, May 2019  
(*2019 Novatech SNC Design Report*)
- Hydraulic Potable Water Assessment for Barrhaven Conservancy Development Corporation, March 2021  
(*Stantec Hydraulic Analysis*)
- Jock River Reach One Subwatershed Study  
Stantec, 2007  
(*Jock River SWS*)
- Geotechnical Investigation, Proposed Residential Development, Conservancy Lands East, Ottawa, Ontario  
Paterson Group, September 24, 2019 (Project No. PG5036-1)  
(*Geotechnical Report*)
- Environmental Impact Statement for Barrhaven Conservancy East  
Kilgour & Associates Ltd., July 29, 2020  
(*Kilgour EIS*)
- Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River): Water Distribution System Analysis, Stantec, June 2, 2022  
(*Stantec Hydraulic Analysis - East*)
- Adequacy of Services Report for Barrhaven Conservancy Development Corporation, Barrhaven Conservancy East  
David Schaeffer Engineering Ltd., July 2021  
(*DSEL East FSR*)
- Design Brief for Barrhaven Conservancy East – Phase 2, 3, & Jock River  
David Schaeffer Engineering Ltd., June 2022  
(*DSEL East Design Brief*)

## 3.0 WATER SUPPLY SERVICING

### 3.1 Existing Water Supply Services

The subject property is located adjacent to the City of Ottawa's Pressure Zone (PZ) 3SW (previously known as PZ BARR). PZ SUC services the lands that are east of the subject property, as well as south of the Jock River.

The City of Ottawa has recently reconfigured the pressure zones servicing Barrhaven and the South Urban Community (SUC) in order to improve reliability and efficiency and to increase pumping capacity to accommodate for future growth in the area. Work is ongoing. There are three pumping stations servicing Zone 3SW and Zone SUC as follows: the Fallowfield Road Pumping Station (FRPS), the Barrhaven Pumping Station (BPS) and the Ottawa South Pumping Station (OSPS).

There are future trunk watermains proposed in the vicinity of the subject property (i.e. along Greenbank Road) which will provide water service to development lands to the east and south of Conservancy East. These services will be further extended to provide the requisite water supply to the development area.

### 3.2 Water Supply Servicing Design

Stantec Consulting Limited was retained to perform a hydraulic assessment for the Conservancy East Lands. The ***Hydraulic Potable Water Assessment for Barrhaven Conservancy Development Corporation (Stantec Hydraulic Analysis)*** prepared by Stantec (March 2021) previously supported the advancement of the Conservancy East lands east of Borrisokane road. Subsequently, as part of the detailed design for the approved phases east of Borrisokane Road, Stantec prepared an updated study ***Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River): Water Distribution System Analysis*** (June 2022 – ***Stantec Hydraulic Analysis - East***) which is enclosed in ***Appendix B*** for reference. Note that phasing references have changed for the development area and the “Phase 4” area referenced in the Stantec study represents the “Phase 5” which is the subject of this updated draft plan – See Figure 1-2 of the ***Stantec Hydraulic Analysis – East*** study for reference. As well, the layout analyzed in the Stantec analysis differs slightly but is not expected to impact the serviceability.

The analysis reviewed the system requirements of the development area on the west and east sides of Borrisokane Road but only the detailed design of the areas east of Borrisokane Road were advanced to detailed design.

The proposed water servicing layout is presented in ***Figure 3***.

The following table summarizes the relevant Water Supply Design Criteria which will be employed in the design of the subject property.

**Table 2A: Water Supply Design Criteria**

Design Parameter	Value
<b><i>Extracted from Section 4: Ottawa Design Guidelines, Water Distribution (July 2010)</i></b>	
Residential – Detached Single	3.4 p/unit
Residential – Townhome/ Semi	2.7 p/unit
Residential – Apartment	1.8 p/unit
Minimum Watermain Size	150 mm diameter
Minimum Depth of Cover	2.4 m from top of watermain to finished grade
During normal operating conditions desired operating pressure is within	350 kPa and 480kPa
During fire flow operating pressure must not drop below	140 kPa
<b><i>Stantec Hydraulic Analysis, Stantec, July 20, 2017 for Population Exceeding 3000 Persons</i></b>	
Residential – Detached Single	180 L/cap/day
Residential – Rear Lane Town	198 L/cap/day
Residential – Back-to-Back	198 L/cap/day
Outdoor Water Demand	1049 L/unit/day (single detached)
Basic Day	Population x Demand
Max Day	Basic Day + Outdoor Water Demand

### 3.2.1 Fire Flow Demand

Fire Flow requirements are established in the boundary condition request found in **Appendix B** as prepared by Stantec. Based on anticipated unit configurations and separations the City's fire flow cap of 10,000 L/min for single dwellings and traditional townhomes as outlined in *ISDTB-2014-02* does not apply and separation of fire areas with units of ordinary construction, as well as architectural elements, are required to meet target fire flows. The fire flows are calculated in accordance with the Fire Underwriters Survey's Water Supply for Public Fire Protection Guideline (1999). Detailed FUS calculations can be found in the Stantec reporting.

### 3.2.2 Boundary Conditions

To support the preparation of a hydraulic analysis for the subdivision, boundary conditions were provided by the City of Ottawa for the anticipated water demands and are summarized in the following table. See **Appendix B** for full details of the boundary condition request submitted.

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**Table 2B: Boundary Conditions (from Stantec Hydraulic Analysis – East report)**

HGL (m) - Zone SUC Servicing Conditions			
Demand Scenario	Two Connections <sup>(5)</sup>		
	Connection 1 <sup>(1)</sup>	Connection 2 <sup>(2)</sup>	
AVDY	150.0	150.0	
PKHR	144.2	144.0	
AVDY +FF	138.7	135.1	
MXDY +FF	137.0	133.2	
Demand Scenario	Two Connections with Upgrades <sup>(4)</sup>		
	Connection 1 <sup>(1)</sup>	Connection 2 <sup>(2)</sup>	
AVDY	149.5	149.5	
PKHR	144.1	144.1	
AVDY +FF	138.6	139.8	
MXDY +FF	136.8	138.1	
Demand Scenario	Three Connections <sup>(5)</sup>		
	Connection 1 <sup>(1)</sup>	Connection 2 <sup>(2)</sup>	Connection 3 <sup>(3)</sup>
AVDY	149.5	149.5	149.5
PKHR	144.5	144.4	142.0
AVDY +FF	138.6	135.1	137.4
MXDY +FF	137.1	133.4	134.8

(1) Ground elevation at Connection 1 (Chapman Mills Drive) = 92.80 m  
 (2) Ground elevation at Connection 2 (Danson Gardens Grv / Darjeeling Ave) 91.80 m  
 (3) Ground elevation at Connection 3 (Flagstaff Dr) 92.10 m  
 (4) Upgrades to existing water distribution required to increase HGL at Connection 2; upsize existing 203mm diameter watermain on Danson Gardens Grv to a 305mm watermain  
 (5) For scenarios where ultimate conditions will include three connections, the boundary conditions for two connections (without upgrades) were used when only connections 1 and 2 are in place (i.e. for modelling Phases 2 and 3).

### 3.2.3 Water Demand Calculations

A summary of water demands for the subject site is presented in the following table as derived from the criteria above and the **Stantec Hydraulic Analysis** found in **Appendix B**.

**Table 2C: Water Demand Estimate**

	Unit Count Conservancy East	Pop <sup>(1)</sup>	AVDY <sup>(2)</sup> (L/s)	OWD <sup>(3)</sup> (L/s)	MXDY <sup>(4)</sup> (L/s)	PKHR <sup>(5)</sup> (L/s)
Single Family	782	2,659	8.62	9.49	21.55	47.38
Townhouse	606	1,636	5.30	0	13.25	29.17
<b>Totals</b>	<b>1,388<sup>(6)</sup></b>	<b>4,296</b>	<b>13.92</b>	<b>9.49</b>	<b>34.80</b>	<b>76.55</b>

(1) Population per unit is 3.4 for Single Family and 2.7 for Townhomes  
 (2) AVDY = Average Day  
 (3) OWD (outdoor water demand) = 1,049 L/unit/day for Singles  
 (4) MXDY = Maximum Day  
 (5) PKHR = Peak Hour  
 (6) Total unit count may vary slightly from final layouts but are estimated to be within +/- 2.5%.  
 (7) See Stantec Hydraulic Analysis in **Appendix B** for details.

### 3.3 Summary of Hydraulic Modeling Analysis

A watermain analysis has been prepared to confirm that the network is sized adequately, which is the greater of maximum day plus fire and maximum hour. City review comments on the current **Stantec Hydraulic Analysis - East** note that 'Option B' is the preferred system configuration (sizing and layout for three connections) and those results are presented below. For full details of the assessments refer to the **Stantec Hydraulic Analysis - East**, enclosed in **Appendix B**.

#### System Pressures

The modeling indicates that the development can be adequately serviced by the proposed watermain network. Modeled service pressures for the development are summarized the following table. The detailed pipe and junction tables are contained in the **Stantec Hydraulic Analysis**, enclosed in **Appendix B**.

**Table 2D: Summary of Available System Pressures**

	AVDY Maximum Pressure		Peak Hour Demand Minimum Pressure	
	kPa	psi	kPa	psi
<b>Option B – 3 Connections</b>	559	81.14 (J55, J60)	482	69.83 (J103)

*Note: See model results in the Appendix D of the Stantec Hydraulic Analysis memo (buildout of all phases).*

The generally accepted best practice is to design new water distribution systems to operate between 350 kPa (50 psi) and 480 kPa (70 psi) as outlined in the City of Ottawa Design Guidelines. Where pressures exceed 80psi pressure reducing valves (PRV) shall be implemented as per the Ontario Building Code.

#### Available Fire Flows

The minimum allowable pressure under fire flow conditions is 140 kPa (20 psi) at the location of the fire. A summary of the available fire flows is presented in the following table. The detailed fire flow reports are found in the **Stantec Hydraulic Analysis - East** enclosed in **Appendix B**.

**Table 2E: Summary of Available Fire Flows**

	Required Fire Flow (L/s)	Minimum Available Flow (L/s)	Junction ID
<b>Option B – 3 Connections</b>	217	250	J86, J87

*Note: See model results in the Appendix D of the Stantec Hydraulic Analysis – East memo (buildout of all phases). Exception is the phase west of Borrisokane Road where the anticipated cul-de-sac fire flow node can be managed by procedures noted in ISDTB-2018-02 (See Section 3.2 of Stantec report)*

As shown in the above table, the model predicts the network will be able to provide all required fire flows. Detailed results are included in the **Stantec Hydraulic Analysis - East**, enclosed in **Appendix B**.

### System Reliability

Various major watermain failure scenarios were reviewed by Stantec. Some scenarios resulted in potential reliability issues which have been resolved in the updated watermain layout with additional looping in the northwest area of the design. See discussion in Section 3.3 of the **Stantec Hydraulic Analysis -East**.

### 3.4 Water Supply Conclusion

The subject lands are have been reviewed by Stantec to confirm that servicing is feasible from the SUC pressure zone. Future watermain extensions from Nepean Town Centre development areas, being constructed as part of Phase 2-4 approvals, will facilitate servicing to the Conservancy East Phase 5 lands via watermain extension along the future Chapman Mills Drive extension and through the Claridge "Burnett Lands" development area. Future modelling at the detailed design stage will confirm phasing of the extensions of trunk watermains and sizing of the local watermain network. The proposed water supply design will conform to all relevant City and MECP Guidelines and Policies.

## 4.0 WASTEWATER SERVICING

### 4.1 Existing Wastewater Services

Per the **South Nepean Collector (SNC) Wastewater Servicing Study and Functional Design Report** by Dillon in October 2003 (**Dillon SNC Report**), the subject property is tributary to the South Nepean Collector (SNC) sewer as urban development land.

The SNC (previously called the Jock River Collector) sewer operates north of the subject property within Strandherd Drive prior to travelling south down a Chapman Mills Drive (CMD) and then turns eastward within the future CMD right-of-way (ROW).

The **South Nepean Collector Phase 2: Hydraulics Review / Assessment** memo was prepared by Novatech Engineering Consultants on August 20, 2015 (**Novatech SNC Memo**) to provide an update to the sanitary design flows for Phase 2 of the South Nepean Collector, as previously documented in the **South Nepean Collector (SNC) – Functional Design Report and Update** by Dillon in 2012 (**Dillon SNC Report and Update**).

### 4.2 South Nepean Collector Phase 3 – Preliminary Design

The 2015 **Novatech SNC Memo** contemplated that the Conservancy Phase 1 development area (north of the Fraser-Clarke Watercourse) would be serviced by the 900 mm diameter SNC sewer running adjacent to the property within the future extension of CMD. This is represented by area "A6-E" within the "*Sanitary Drainage Areas and Land Use – Fig.1*" plan within the 2015 Novatech memo (note that the actual tributary area and population varied slightly).

For the Phase 3 extension of the SNC, Novatech has prepared another review of sanitary flows within their technical memorandum titled "**Strandherd Drive Widening Project, South Nepean Collector Phase 3: Sanitary Flow Calculations**" May 30, 2019 (**2019 Novatech SNC Memo**). The memorandum along with the design sheet calculations from the Novatech memo are provided in **Appendix C** for reference along with DSEL annotations on key items in the figure and design sheets. The updated "*Sanitary Drainage Areas and Land Use – Fig.1*" (May 2019) plan is essentially reflective of the same tributary information that was provided in the 2015 study (the plan has been marked up to reflect the Conservancy areas as a frame of reference). The associated design sheet also reflects updated City wastewater design criteria that was not accounted for in the 2015 study and is discussed further in the following section.

Report excerpts are provided in **Appendix C** for the SNC Phase 2 analysis as well as draft information associated with the Phase 3 extension. The location of the SNC sewer is shown in **Figure 4**.

### 4.3 Wastewater Design

The subject property is planned to be serviced by an internal gravity sanitary sewer system that is to generally follow the local road network. The wastewater servicing plan can be seen in **Drawing 4**.

The prior report proposed that the drainage area of the SNC sanitary sewer be expanded to include the entirety of the Conservancy property. The sewer network will connect to the off-site SNC sanitary sewer within the future CMD at existing manhole 'SANMH8' as identified in the Novatech SNC Phase 2 design Drawing No. 20 provided in **Appendix C** for reference (City contract number ISD14-2033). As noted in the prior section, the 2015 **Novatech SNC Memo** was derived flows based on the City guideline parameters of the time (namely 350 L/capita/day, infiltration allowance of 0.28 L/s/ha and commercial properties at 50,000 L/ha/d). The following table summarizes the new City design guidelines and criteria to be applied to the **Conservancy East** sewer design as well for the determination of the projected flows to be tributary to the SNC along the frontage of the Conservancy Phase 1 development area.

**Table 3: Wastewater Design Criteria**

Design Parameter	Value
<b>Current Design Guidelines</b>	
Residential - Single Family	3.4 p/unit
Residential – Townhome/ Semi	2.7 p/unit
Residential – Apartment	1.8 p/unit
Average Daily Demand	280 L/d/person
Peaking Factor	Harmon's Peaking Factor. Max 4.0, Min 2.0
Commercial / Institutional Flows	28,000 L/ha/day
Commercial / Institutional Peak Factor	1.5
Infiltration and Inflow Allowance	0.33 L/s/ha
Park Flows	28,000 L/ha/d
Park Peaking Factor	1.0
Sanitary sewers are to be sized employing the Manning's Equation	$Q = \frac{1}{n} AR^{\frac{2}{3}} S^{\frac{1}{2}}$
Minimum Sewer Size	200mm diameter
Minimum Manning's 'n'	0.013
Minimum Depth of Cover	2.5m from crown of sewer to grade
Minimum Full Flowing Velocity	0.6m/s
Maximum Full Flowing Velocity	3.0m/s

*Extracted from Sections 4 and 6 of the City of Ottawa Sewer Design Guidelines, October 2012, and associated Technical Bulletins.*

The sanitary design sheet for the lands east of Borrisokane Road is provided in **Appendix C** for reference. Within that design sheet the area and flows from the lands west of Borrisokane Road are highlighted where flows enter that development area at the westward stub from MH10A. That design sheet projected a flow of 77.81 L/s. Based on the updated Phase 5 draft plan, and updated concept plans for the

Conservancy West development area (west of the Foster Ditch), the flows shown at the eastern limit of Phase 5 (see Phase 5 design sheet in **Appendix C**) is now ~68.96 L/s at MH 532A. As such, downstream systems are sufficient and no negative impacts given that flows are lower than the previously projected 77.81 L/s.

#### 4.4 Wastewater Servicing Conclusion

The subject property will be serviced by local sanitary sewers, an on-site trunk sanitary sewer, and the off-site SNC sanitary sewer as defined in previous reports. This AES continues to confirm that the expansion of the drainage areas from the **2019 Novatech SNC Memo** to include the entirety of the subject property has no negative impacts. There is residual capacity in the downstream SNC providing sufficient capacity for the peak sanitary flows for the subject property, including external commercial and community park flows.

## 5.0 STORMWATER CONVEYANCE

### 5.1 Existing Stormwater Drainage

The subject property is within the Jock River watershed. Per the existing topography characterized in available City of Ottawa base mapping, as well as site specific survey, all flows from the subject property are ultimately conveyed to the Jock River by a series of watercourses, sheet flow and minor ditches. The Foster Ditch, Borrisokane Road roadside ditches, are the main stormwater conveyances within the Conservancy East Phase 5 property that convey stormwater to the Jock River.

### 5.2 Proposed Stormwater Management Strategy

As documented in the previous AES, various stormwater strategies were discussed within the Master Infrastructure Review (MIR) prepared in parallel with the AES. Alternatives reviewed were:

#### **Alternative 1 – Oil and Grit Separators & Treatment Train to Naturalized Wetlands\***

Alternative 2 – Stormwater Management Wetland Facilities in the Floodplain

Alternative 3 – Stormwater Management Wetland Facilities out of the Floodplain

Alternative 4 – Modified Etobicoke filtration System (MEFS)

For the purposes of this AES update for Phase 5 Alternative 1 continues to be advanced as per the evaluation provided in the MIR and per discussions with the City of Ottawa on July 20, 2021. This alternative:

- A storm sewer system designed to capture at least the minimum design capture events in accordance with the amendment to the storm sewer and stormwater management elements of the Ottawa Design Guidelines – Sewer (Technical Bulletin PIEDTB-2016-01). The stormwater runoff will be treated before ultimately being released into the natural heritage features and the Jock River as per the **Jock River Reach One Subwatershed Study** prepared by Stantec in 2007 (**Jock River SWS**).
- All proposed units will be equipped with sump pumps due to local constraints;
- A treatment train approach to attain an Enhanced Level of Protection (80% total suspended solids (TSS) removal) per MECP guidelines consisting of:
  - Deep sump catchbasins;
  - The incorporation of infiltration-type LIDs within the right-of-way extending out from catchbasin locations (see **Figure 5** in the **Figures & Drawings** section). Future detailed grading will allow for the determination of suitable locations in order to yield optimal benefit from this LID. See Section 5.7 for additional LID discussion.

- Multiple oil and grit separators (OGS) units to provide TSS treatment with outlets that are above the 2-year event summer water levels on the Jock River;
- The storm systems will discharge the treated stormwater at multiple outlets located along the southern natural heritage corridor, connecting via channels. Discharge locations are demonstrated in the **Storm Tributary Area** plan in the **Figures & Drawings** section
- An on-site road network designed to maximize the available storage within right-of-ways for the 100-year design event, where possible; and
- An overland flow route designed to safely convey stormwater runoff flows in excess of the on-site road storage.

The design for the site proposes to have stormwater flows conveyed through the development area of the subject property via an underground sewer network. The stormwater runoff will be treated before ultimately being released into the Jock River as per the **Jock River Reach One Subwatershed Study** prepared by Stantec in 2007 (**Jock River SWS**).

The proposed stormwater design layout is shown on **Drawing 3** with the stormwater management design consisting of (similar to prior phases):

- A storm sewer system designed to capture at least the minimum design capture events in accordance with the amendment to the storm sewer and stormwater management elements of the Ottawa Design Guidelines – Sewer (Technical Bulletin PIEDTB-2016-01);
- All proposed units will be equipped with sump pumps due to local constraints;
- A treatment train approach to attain an Enhanced Level of Protection (80% total suspended solids (TSS) removal) per MECP guidelines consisting of:
  - Deep sump catchbasins to reduce catchbasin sump sediment re-suspension and optimize TSS removal;
  - Multiple oil and grit separators (OGS) units to provide TSS treatment with outlets that are above the 2-year event summer water levels of the Jock River;
  - The incorporation of infiltration-type LIDs within the right-of-way extending out from catchbasin locations (see **Figure 5** in the **Figures & Drawings** section). The future detailed grading will allow for the determination of preferred locations in order to yield optimal benefit from this LID. See Section 5.7 for additional LID discussion;

- The storm systems will discharge the treated stormwater at multiple outlets (2) located along the natural heritage corridor, connecting to the Foster Ditch via channels to support hydration of the wetlands and ultimately outletting to the Jock River. Discharge locations are demonstrated in **Drawing 3**;
- An on-site road network designed to maximize the available storage within right-of-ways for the 100-year design event, where possible, with controlled release of stormwater to the minor storm system; and
- An overland flow route designed to safely convey stormwater runoff flows in excess of the on-site road storage.

Although quantity control has not typically been required for this reach of the Jock River, as per the **Jock River SWS**, the quantity of stormwater runoff exiting from the subject property will be minimized by optimizing on-site storage in the sags of the proposed road network, which in turn minimizes the size of downstream storm sewer infrastructure. It is noted that the RVCA is currently reviewing the SWM requirements within the Jock River Reach 1 area. In consideration of this, J.F. Sabourin and Associates (JFSA) has undertaken a review of the existing quantity control recommendations and the existing, and proposed, development conditions for this area. The findings are presented in the JFSA memorandum *Review of Quantity Control Requirement for Jock River Reach 1 (March 2021)* provided in **Appendix D** which concludes that quantity controls will still not be required for this reach of the Jock River.

### 5.2.1 Post-Development Stormwater Management Targets

Stormwater management requirements for the proposed alternative Stormwater management scheme have been adopted from the **Jock River SWS**, **City Standards**, and the **MECP SWMP Manual**.

Given the general criteria mentioned above, the following specific standards are anticipated for stormwater management within the subject property:

- Enhanced quality treatment will be provided for stormwater runoff from the subject property, corresponding to a long-term average TSS removal efficiency of 80%, as defined by the MECP prescribed treatment levels;
- Downstream receiving watercourses will be assessed for responses to planned stormwater management outflows, and stabilization mitigation measures will be planned as required;
- Storm sewers on local roads are to be designed to provide at least a 2-year level of service without any ponding per the City's latest Technical Bulletin PIEDTB-2016-01;

- Storm sewers on collector roads are to be designed to provide at least a 5-year level of service without any ponding per the City's latest Technical Bulletin PIEDTB-2016-01;
- For less frequent storms (i.e. larger than 2-year or 5-year), the minor system sewer capture will be restricted with the use of inlet control devices to prevent excessive hydraulic surcharges;
- Under full flow conditions, the allowable velocity in storm sewers is to be no less than 0.80 m/s and no greater than 6.0 m/s;
- For the 100-year storm and for all roads, the maximum depth of water (static and/or dynamic) on streets, rear yards, public space and parking areas shall not exceed 0.35 m at the gutter;
- The major system shall be designed with sufficient capacity to allow the excess runoff of a 100-year storm to be conveyed within the public ROW, or adjacent to the ROW, provided the water level does not touch any part of the building envelope; must remain below all building openings during the stress test event (100-year + 20%); and must maintain 15 cm vertical clearance between spill elevation on the street and the ground elevation at the nearest building envelope;
- Flow across road intersections shall not be permitted for minor storms (generally 5-year or less);
- When catchbasins are installed in rear yards, safe overland flow routes are to be provided to allow the release of excess flows from such areas. A minimum of 30 cm of vertical clearance is required between the rear yard spill elevation and the ground elevation at the adjacent building envelope; and
- The product of the maximum flow depths on streets and maximum flow velocity must be less than 0.60 m<sup>2</sup>/s on all roads.

### 5.2.2 Quality Control

Per the **Jock River SWS**, Enhanced quality treatment will be provided for stormwater runoff from the subject property, corresponding to a long-term average TSS removal efficiency of 80%, as described by the MECP prescribed treatment levels. See Section 5.3 for quality control approach and discussion.

### 5.2.3 Quantity Control

As noted in the **Jock River SWS**, quantity control is not anticipated to be required for outlets to the Jock River, however, some quantity control may be provided by erosion storage, as erosion thresholds for any watercourses/outlets will be respected where required. As noted in Section 5.2, JFSA has reviewed the current/future development conditions contributing to this reach of the Jock River and concludes that quantity

control will still not be required. See “Review of Quantity Control Requirement for Jock River Reach 1 (JFSA March 2021) provided in **Appendix D**.

## 5.3 Stormwater Management Design

### 5.3.1 Treatment Train Approach

JFSA previously (June 2021 memo) prepared a review of various potential stormwater quality treatment options that were investigated for the development. These included options, and combinations of options, as summarized in the following updated table. Each of the options has an expected total suspended sediment (TSS) removal capability, varying from 5% to 88%. This review assessed how the required Enhanced Level of Protection (80% TSS removal) could be achieved when the options are used in a treatment train approach, consistent with the expected requirements of the upcoming MECP *Consolidated Linear Infrastructure* policy.

**Table 1: Quality Control Alternatives – Treatment Train to achieve 80% TSS Removal**

<u>Selection and comparison of alternatives</u>										
Method	TSS Removal	Alt. 1	Alt. 2	Alt. 3	Alt. 4	Alt. 5	Alt. 6	Alt. 7	Alt. 8	
Street Sweeping (Monthly)	5%									
Street Sweeping (Weekly)	10%									
Street Sweeping (Weekly with Elgin Eagle)*	88%	x								
Curb Cut with Grass Swales	75%			x						
Curb Cut with Infiltration Trenches	80%									
Catchbasin Inserts (CB Shield)*	27%		x		x	x		x		
Deep Sump Catch Basin	25%				x		x			x
Infiltration/ Filtration Trenches**	80%				x	x	x			
Infiltration at CBs, per MOE Table 3.2 (22.5m <sup>3</sup> /ha)	70%									x
OGS*	50%			x						x
JellyFish*	85%							x		
SWM Pond (Wet Pond)	80%		x							
<b>Overall Performance</b>										
Treatment Train Overall Performance = 1 - (1- TSS Removal Rate Method 1) x (1- TSS Removal Rate Method 2) x (1- TSS Removal Rate Method 3 x ...)										
88.0%      85.4%      87.5%      89.1%      85.4%      85.0%      89.1% <b>88.8%</b>										

The above table provides a summary of the TSS removal for the various methods that were considered. An option of infiltration LID measures located at catchbasin locations has been added as a method, and to Alternative 8 (see further discussion regarding this method below). The options, and combinations of options, have been assessed and shown to meet or exceed the required 80% TSS target.

For the development area, the updated Alternative 8 option demonstrates an estimated TSS removal of 88.8% for that particular treatment train approach which has been discussed with City staff for the approval of prior phases and will be the design being

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advanced. For the determination of the TSS removal of 70% for the infiltration LID at catchbasins, the *Table 3.2* of the MOECC (now MECP) publication entitled “*Stormwater Management Planning and Design Manual, March 2003*” sets the storage volume requirements for infiltration measures to achieve certain TSS removal rates.

**Table 3.2 Water Quality Storage Requirements based on Receiving Waters<sup>1, 2</sup>**

Protection Level	SWMP Type	Storage Volume (m <sup>3</sup> /ha) for Impervious Level			
		35%	55%	70%	85%
<i>Enhanced</i> 80% long-term S.S. removal	Infiltration	25	30	35	40
	Wetlands	80	105	120	140
	Hybrid Wet Pond/Wetland	110	150	175	195
	Wet Pond	140	190	225	250
<i>Normal</i> 70% long-term S.S. removal	Infiltration	20	20	25	30
	Wetlands	60	70	80	90
	Hybrid Wet Pond/Wetland	75	90	105	120
	Wet Pond	90	110	130	150
<i>Basic</i> 60% long-term S.S. removal	Infiltration	20	20	20	20
	Wetlands	60	60	60	60
	Hybrid Wet Pond/Wetland	60	70	75	80
	Wet Pond	60	75	85	95
	Dry Pond (Continuous Flow)	90	150	200	240

<sup>1</sup>Table 3.2 does not include every available SWMP type. Any SWMP type that can be demonstrated to the approval agencies to meet the required long-term suspended solids removal for the selected protection levels under the conditions of the site is acceptable for water quality objectives. The sizing for these SWMP types is to be determined based on performance results that have been peer-reviewed. The designer and those who review the design should be fully aware of the assumptions and sampling methodologies used in formulating performance predictions and their implications for the design.

<sup>2</sup>Hybrid Wet Pond/Wetland systems have 50-60% of their permanent pool volume in deeper portions of the facility (e.g., forebay, wet pond).

The required storage volume of 22.5 m<sup>3</sup>/ha is determined for the development area pro-rated from the above table based on an overall imperviousness of ~62.5%. Similar to prior phases it is anticipated that the extent of the site area for Conservancy East Phase 5 can be managed with the proposed LID. For prior phases it is noted that approximately 140 lineal meters of LID per hectare of area to be treated was required. With approximately 9.0 ha of area to be treated (which excludes rear yards similar to the prior phase) this equates to 140x9.0= ~1,260 m extent of LID required. Phase 5 has approximately 1,800 m of roadway to incorporate the LID infrastructure therefore sufficient roadway is available for use.

### 5.3.2 Oil-Grit Separator Units (OGS)

As shown on **Drawing 3**, two (2) OGS units at locations along the southern boundary of the property, discharging to the Jock River via the existing Foster Ditch. By way of an MECP Certificate of Technology Assessment and manufacturer's design report, the OGS units will demonstrate compliance with Enhanced Level of Protection requirements, with specific drainage area parameters for each area.

The manufacturer's reported efficiency of TSS removal of the OGS units is expected to be based on a 'fine distribution' particle size distribution in conformance with the following table, unless otherwise approved by the City of Ottawa, RVCA, and MECP. The particle size distribution is the generic particle size distribution accepted by the City of Toronto per the *Wet Weather Flow Management Guidelines* (City of Toronto, 2006) as a typical average stormwater particle size distribution, and is an excerpt from Table 3.3 of the *Stormwater Management Practices Planning and Design Manual* (MOECC, 1994).

**Table 4: Typical Stormwater Particle Size Distribution & Settling Velocities**  
**(Source: *Stormwater Management Practices Planning and Design Manual*,**  
**MOECC, 1994)**

Particle Size (microns) (NURP 1983)	% of Particle Mass	Average Settling Velocities (m/s)
< 20	0 - 20	0.00000254
20 - 40	20 - 30	0.00001300
40 - 60	30 - 40	0.00002540
60 - 130	40 - 60	0.00012700
130 - 400	60 - 80	0.00059267
400 - 4000	80 - 100	0.00550333

To allow for flexibility as detailed design advances, it is proposed that any OGS unit can be selected, given that it:

- Meets the requirements set out in the preceding sections;
- Ensures no significant negative impact on the upstream storm sewer system – to be determined via hydraulic modelling at detailed design; and
- Demonstrates suitability for meeting Enhanced water quality targets via a MECP Certificate of Technology Assessment.

The preliminary OGS units proposed in the following table have been sized to treat the stormwater runoff for the tributary areas noted in order to meet MECP Enhanced Level of Protection criteria prior to discharge to the Jock River via naturalized wetlands as

shown on **Drawing 3**. The OGS total suspended removal rates and preliminary OGS unit details have been attached for reference in **Appendix D**.

**Table 5: OGS Unit ID and Design Characteristics**

Area and Unit ID <sup>(1)(2)</sup>	Drainage Area Target (ha)	Estimated Weighted C Value	Unit Treatment Capacity (L/s)	Unit Model <sup>(1)</sup>
Area 9 – OGS9 <sup>(3)</sup>	7.21	0.72	212	CDS Model 4045-8
Area 10 – OGS10 <sup>(3)</sup>	6.61	0.70	212	CDS Model 4045-8
(1) Providing at minimum 80% TSS removal for a Fine Distribution				
(2) See <b>Drawing 3</b> for OGS unit locations				
(3) NOTE: the OGS numbering of OGS9 and OGS10 have been used to maintain consistency with prior functional servicing reports circulated in relation to this development area.				

The above OGS units will achieve required quality controls within the treatment train and, along with other elements, will have additional beneficial TSS mitigation.

### 5.3.3 Groundwater

Paterson Group has reviewed the anticipated long term groundwater condition for the development area. Paterson drawing PG5036-10A in **Appendix D** demonstrates the long term groundwater elevation across the Conservancy East Phase 5 development area. The lowest elevation of 88.70 is below the trunk sewer profiles shown in **Drawing No. 5** in the **Drawings** section and would be below any infiltration-type LID proposed within the development area.

## 5.4 Proposed Minor System

The subject property will be serviced by an internal gravity storm sewer system that will generally follow the local road network and proposed servicing easements as required. The drainage will be conveyed within the underground piped sewer system to headwall outlets located along the natural heritage corridor.

Street catchbasins will collect drainage from the streets and front yards, while rear yard catchbasins will capture drainage from backyards. Perforated catch basin leads will be provided in rear yards, except the last segment where they connect to the right-of-way which will be solid pipe, per City standards.

The rational method design of the minor system captures drainage for storm events up to and including the 2-year (local) and 5-year (collector) event within the subject property. The following table summarizes the standards employed in the detailed

design of the storm sewer network. The preliminary drainage area information can be found in **Drawing 3** and rational method design sheets are provided in **Appendix D**.

**Table 6: Storm Sewer Design Criteria**

Design Parameter	Value
Minor System Design Return Period	1:2 year (PIEDTB-2016-01) for local roads, without bonding 1:5 year (PIEDTB-2016-01) for collector roads, without bonding 1:100 year (PIEDTB-2016-01) for arterial road, without bonding
Major System Design Return Period	1:100 year
Intensity Duration Frequency Curve (IDF) 2-year storm event: $A=732.951   B=6.199   C=0.810$ 5-year storm event: $A = 998.071   B = 6.053   C = 0.814$	$i = \frac{A}{(t_c + B)^C}$
Minimum Time of Concentration	10 minutes
Rational Method	$Q = CiA$
Storm sewers are to be sized employing the Manning's Equation	$Q = \frac{1}{n} AR^{2/3} S^{1/2}$
Runoff coefficient for paved and roof areas	0.9
Runoff coefficient for landscaped areas	0.2
Minimum Sewer Size	250 mm diameter
Minimum Manning's 'n' for pipe flow	0.013
Minimum Depth of Cover	1.5 m from crown of sewer to grade
Minimum Full Flowing Velocity	0.8 m/s
Maximum Full Flowing Velocity	6.0 m/s
Clearance from 100-Year Hydraulic Grade Line to Building Opening	0.30 m
Design Parameter	Value
Max. Allowable Flow Depth on Municipal Roads	35 cm above gutter (PIEDTB-2016-01)
Extent of Major System	To be contained within the municipal ROW or adjacent to the ROW provided that the water level must not touch any part of the building envelope and must remain below the lowest building opening during the stress test event (100-year + 20%) and 15cm vertical clearance is maintained between spill elevation on the street and the ground elevation at the nearest building envelope (PIEDTB-2016-01)
Stormwater Management Model	DDSWMM (release 2.1), SWMHYMO (v. 5.02) and XPSWMM (v. 10)

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Model Parameters	Fo = 76.2 mm hr, Fc = 13.2 mm hr, DCAY = 4.14/hr, D.Stor.Imp. = 1.57 mm, D.Stor.Per. = 4.67 mm
Imperviousness	Based on runoff coefficient (C) where Percent Imperviousness = (C - 0.2) / 0.7 x 100%.
Design Storms	Chicago 3-hour Design Storms and 24-hour SCS Type II Design Storms. Maximum intensity averaged over 10 minutes.
Historical Events	July 1st, 1979, August 4th, 1988 and August 8th, 1996
Climate Change Street Test	20% increase in the 100-year, 3-hour Chicago storm
<i>Extracted from City of Ottawa Sewer Design Guidelines, October 2012, and ISSU, and based on recent residential subdivisions in City of Ottawa.</i>	

The peak design flows are calculated based on an average predicted runoff coefficient (C-value) of 0.67 and 0.80 for the development areas, 0.40 for park areas and 0.25 for grassed areas. As detailed design progresses, the runoff coefficients will be refined to reflect the proposed building envelopes, driveways and other details.

There are several trunk sewers proposed and the peak flows are described for the trunk sewers which correspond to the stormwater management design areas as summarized in the following table:

**Table 7: Minor System Trunk Sewer Outlets**

Area/Outlet # (from east to west)	Trunk Sewer Outlet Headwall	Peak Flow (L/s)
9 (HW9) <sup>(1)</sup>	1050 mm diameter @ 0.20%	894
10(HW10) <sup>(1)</sup>	1050 mm diameter @ 0.11%	739
(1) NOTE: the OGS numbering of OGS9 and OGS10 have been used to maintain consistency with prior functional servicing reports circulated in relation to this development area.		

The storm sewers tributary to the various outlets, and associated peak flows, are detailed in the rational method design sheet, enclosed in **Appendix D**.

The conceptual servicing layout is shown on **Drawing 2** in **Drawings**. As detailed design progresses, alignment and sizing of local storm sewers will be confirmed and additional servicing easements may be required, potentially triggering minor amendments to the proposed lot fabric in the concept plan. The preliminary sanitary and storm trunk plan and profiles are shown on **Drawing 5** in **Drawings**.

#### 5.4.1 Hydraulic Grade Line Analysis

A preliminary hydraulic grade line (HGL) modelling analysis has been completed by JFSA to demonstrate that the HGL will be maintained below the ground surface. See the JFSA memo entitled *BCDC Phase 5 – Preliminary HGL Analysis (December 1, 2022)* in **Appendix D** for details/results. The analysis has been evaluated for various scenarios for the Jock River (as per prior City requirements) in order to assess the appropriate HGL boundary condition:

- 100-year rainfall event on the development and a 5-year spring water level on the Jock River; or
- 5-year rainfall event on the development and a 100-year spring water level on the Jock River (deemed to be the critical event).

The HGL results in JFSA's Table 1 demonstrate that the worst case scenario freeboard to the ground surface ranges from 0.64m to 0.90m for the critical event noted above. The HGL is shown on the profile **Drawing 5** for reference.

An updated HGL analysis will be completed for the proposed system at the detailed design stage, based on the above noted events, including historical design storms and climate change stress test as required. Detailed grading design and storm sewer design will be modified as required to achieve the freeboard requirements (per PIEDTB-2016-01).

#### 5.5 Proposed Major System

Major system conveyance, or overland flow, will be provided to accommodate flows in excess of the minor system capacity. Overland flow is accommodated by generally storing stormwater up to the 100-year design event in road sags then routing additional surface flow along the road network and service easements towards the proposed stormwater outlets, discharging to the Jock River through the natural heritage corridors, as shown on **Drawing 1**. The grading design includes a saw-toothed-road design with 0.10% minimum grade from high point to high point in order to maximize available surface storage for management of flows up to the 100-year design event where possible.

#### 5.6 Foundation Drainage (Sump Pumps)

Due to the grade raise restrictions and the proposed storm and sanitary drainage schemes, the road centerlines do not allow for standard basements with a gravity connection to the storm sewer system. As such, because of the constraints on the subject property, sump pumps are proposed to be installed for all residential blocks and residential lots.

The City of Ottawa issued Technical Bulletin *ISTB-2018-04* and *2019-02* for the amendment of the *Ottawa Design Guidelines – Sewer, Second Edition*, October 2012 with respect to the screening criteria for the use of sump pump systems for foundation drainage in Greenfield developments on sites with clay soils. Similar to the development of Conservancy Phase 1, and Conservancy East (Phase 2-4) this site has also been assessed as meeting the required criteria for the use of sump pumps.

One of the screening criterion is with respect to the hydraulic grade line (HGL) for the development wherein the system should be reviewed to demonstrate that the HGL cannot reasonably be lowered any further due to outlet restrictions. The site grading is constrained by the close proximity of the Jock River, which is the receiver of stormwater outflows, and is also constrained by grade raise restrictions for the property.

For the Barrhaven Conservancy East Phase 5 Lands the grade raise restriction varies between 1.4 m and 1.8 m. Paterson's permissible grade raise plan is contained in **Appendix E** for reference (See Section 6 for discussion). Further investigations on the property and potential surcharging or lightweight fill (LWF) underneath garages could increase the permissible grade raise and will be investigated further as part of the detailed design.

The functional grading plan for the subdivision has been prepared with the grade raise restrictions in mind with grades being kept as low as possible.

The proposed centerline of road grades, and subsequently the house grades, do not allow for standard basements with a gravity connection to the storm sewer system. As such, the subdivision will be serviced entirely by sump pumps due to site constraints imposed by grade raise restrictions, HGL elevations and the proximity to the Jock River stormwater outlet.

## 5.7 Low Impact Development (LID) - Infiltration

The following general Low Impact Development (LID) techniques could be considered for implementation, where possible, as part of detailed design (noting that they have to be weighed against the objectives of the City's sump pump technical bulletins):

- Rear-yard swales should be designed with minimum grades where possible, to promote infiltration;
- Rear-yard catchbasin leads should be perforated (except for the last segment connecting to the storm sewer within the ROW), to promote infiltration; and,
- Where eavestroughs are provided on residential units, they are to be directed to landscaped surfaces, to promote infiltration.
- Furthermore, the following techniques can be examined as part of detailed landscaping design of the park block; and,
- Micro-grading can be considered to promote infiltration.

Generally, the LID techniques proposed above are most suitable due to the existing clay soils and high groundwater levels. The long term groundwater anticipated is demonstrated on Paterson Drawing *PG5036-10A* in **Appendix D** as previously noted. The proposed LID infiltration measure noted in Section 5.2 will contribute some infiltration benefits as first flush stormwater is conveyed into the filtration trench. The amount of infiltration is dependent upon the surrounding soils, but the proposed design will optimize the potential on the site.

## 5.8 Existing Watercourses

### 5.8.1 Foster Ditch

The Foster Ditch borders the western boundary of the Conservancy East Phase 5 development area. It originates south of Fallowfield Road, west of Cedarview Road and flows south until it converges with the Jock River South of McKenna Casey Drive. The ditch is approximately 3200 m long and has been artificially straightened. This non-municipal drain is a fish bearing tributary of the Jock River with approximately 335 ha of catchment area. The surrounding land use is urban and vacant lands. Riparian vegetation is very sparse consisting of mostly grasses with a few shrubs.

As noted in the **Jock River SWS**, to ensure protection of the aquatic habitat north of the Jock River, a development setback should be provided for all of the tributaries. Further studies will determine the development setback, which will be the greater of: 1) regulatory floodplain; 2) meander belt width; and 3) aquatic setback, whichever is greater.

## 5.9 Floodplain

On November 8<sup>th</sup>, 2019 the RCVA gave permission to Barrhaven Conservancy Development Corporation to cut and fill on the subject property under permit RV5 44/19 pursuant to review under Section 28 of the Conservation Authorities Act, regulation 174/06. The application and approval by the RVCA was supported by a 2D HEC-RAS model prepared by JFSA. The JFSA model identified the existing and proposed 100-year water levels and permissible extent of fill placement.

The works pursuant to the above-mentioned permit were completed and accepted by the RVCA on May 31st 2020. Options to complete the fill area boundary as set by JFSA included building a structural face of fill (retaining wall) to the limits of the 100-year floodplain boundary, or, building a berm with the toe of slope at the 100-year floodplain boundary. A vertical structural face of fill was not seen as a desirable or practical outcome and a berm was thus constructed. As-builts for the top of berm were subsequently provided and approved by the RVCA, resulting in the May 31st approval noted above and the current 100-year floodplain boundary delineation. The toe of the berm as constructed corresponds to the approved JFSA 100-year floodplain line and the current top of berm corresponds to the as-built top of berm.

## 5.10 Stormwater Servicing Conclusions

The Phase 5 stormwater runoff is designed to be captured by an internal gravity sewer system that will convey flows to multiple outlet locations equipped with end of line OGS units (two). A proposed treatment train arrangement of 1.0 m deep sump catchbasins, to optimize catchbasin sump retention of solids, as well as select catchbasin locations with connected infiltration-type subdrains will provide the required quality control treatment to achieve the Enhanced Level of protection. Downstream of the storm outlets along the southern development boundary will be channels within the natural heritage corridor where flows will be conveyed to the Foster Ditch prior to discharge to the Jock River. It is anticipated that quantity control is not required for the Jock River. Notwithstanding, some quantity control by means of erosion storage will be included.

A preliminary Hydraulic Grade Line (HGL) modelling analysis has been completed for the Conservancy East (Phase 5) development area at this time and demonstrates that the HGL is maintained below the ground surface with freeboards ranging from 0.64 m to 0.90 m. Further detailed HGL review will be completed for the proposed system at the detailed design stage. Due to the grade raise restrictions, and the proposed storm and sanitary drainage layouts, the road centerlines do not allow for standard basements with a gravity connection to the storm sewer system. As such, because of the constraints on the subject property, sump pumps are proposed to be installed for all residential blocks and residential lots.

The Conservancy East phase 5 development area will be outside of the Jock River's regulatory floodplain area.

Appropriate setbacks from existing watercourse are incorporated into the draft plan based on advancement/finalizing of studies to assess the various determining criteria.

## 6.0 GRADING

A site grading arrangement has been developed to optimize earthworks and provide major system conveyance to the receiving outlets, and naturalized wetland facilities, which ultimately outlet to the existing Jock River drainage network. The proposed grading can be found in **Drawing 1 in Drawings**.

The development area is outside of the Jock River regulatory flood plain limits. The site grading will be a minimum of 0.50m above the 100-year regulatory limit event of the Jock River.

### 6.1 Geotechnical Conditions

Paterson completed a geotechnical investigation for the Conservancy East lands as follows:

- *Geotechnical Investigation – Proposed Residential Development, Conservancy Lands East* (Paterson Group, September 24, 2019);

The existing ground surface across the site is relatively level with approximate ground surface elevation varying between 91.5 m and 91.0 m. The subsurface profile generally consists of an approximate 50 mm to 460 mm thick layer of topsoil underlain by a silty clay deposit.

Due to the presence of a silty clay deposit, permissible grade raise restrictions are recommended for this site. The recommended permissible grade raise varies between 1.4 m in the north area of the phase and 1.8 m in the south. Figure PG5036-2 ‘Permissible Grade Raise Plan’ by Paterson is enclosed in **Appendix E** for reference. At the time of detailed design, efforts will be made to mitigate any exceedances and detailed review and signoff by a licensed Geotechnical Engineer will be required. Where grade raises exceed the permissible levels the Engineer will recommend appropriate measures to mitigate where required (i.e. light weight fill or pre-consolidation etc).

The following additional grading criteria and guidelines will be applied to detailed design, per **City of Ottawa Guidelines**:

- Driveway slopes will have a maximum slope of 6%;
- Grading in grassed/landscaped areas to range from 2% to 3:1, with terracing required for slopes larger than 7%;
- Swales are to be 0.15m deep with 3:1 side slopes unless otherwise indicated on the drawings; and,
- Perforated pipe will be required for drainage swales if they are less than 1.5% in slope.

The geotechnical analysis of the site, published under separate cover in support of the development applications, provides additional information about the suitability of the site for the proposed services and grading scheme. At the time of detailed design, detailed review and signoff by a licensed Geotechnical Engineer will be required.

## 7.0 EROSION AND SEDIMENT CONTROL

Soil erosion occurs naturally and is a function of soil type, climate and topography. The extent of erosion losses is exaggerated during construction where vegetation has been removed and the top layer of soil becomes agitated.

Prior to topsoil stripping, earthworks or underground construction, erosion and sediment controls are implemented and will be maintained throughout any construction phase.

The following specific recommendations to the Contractor will be included in contract documents.

- Limit extent of exposed soils at any given time.
- Re-vegetate exposed areas as soon as possible.
- Minimize the area to be cleared and grubbed.
- Protect exposed slopes with plastic or synthetic mulches.
- Install silt fence to prevent sediment from leaving the site and entering existing watercourses, and clean and maintain throughout construction.
- Install catchbasin inserts during construction to protect from silt entering the storm sewer system.
- Install mud mats in order to prevent mud tracking onto adjacent roadways.
- No refueling or cleaning of equipment near existing watercourses.
- No material stockpiles within 30m of existing watercourses, unless otherwise permitted by RVCA and City of Ottawa.
- Provide sediment traps and basins during dewatering.
- Plan construction at proper time to avoid flooding.
- The Contractor will, at every rainfall, complete inspections to ensure proper performance.
- Erosion and sediment controls will remain in place until the working areas have been stabilized and re-vegetated.

## 8.0 UTILITIES

Utility services extending to the site may require connections to multiple existing infrastructure points: consultation with Enbridge gas, Hydro Ottawa, Rogers, and Bell is required as part of the development process to confirm the servicing plan for the subject lands.

## 9.0 CONCLUSION AND RECOMMENDATIONS

This AES provides details on the planned on-site municipal services for the subject property and demonstrates that adequate municipal infrastructure capacity is expected to be available for the planned development area.

- The subject lands have been reviewed by Stantec to confirm that servicing is feasible from the SUC pressure zone. Future watermain extensions from Nepean Town Centre development areas, being constructed as part of Phase 2-4 approvals, will facilitate servicing to the Conservancy East Phase 5 lands via watermain extensions along the future Chapman Mills Drive extension and through the Claridge “Burnett Lands” development area. Detailed modelling will confirm phasing of the extensions of trunk watermains and verify sizing of the local watermain network.
- The subject property will be serviced by local sanitary sewers, an on-site trunk sanitary sewer, and the off-site SNC sanitary sewer as defined in previous reports. This AES continues to confirm that the expansion of the drainage areas from the **2019 Novatech SNC Memo** to include the entirety of the subject property has no negative impacts. There is residual capacity in the downstream SNC providing sufficient capacity for the peak sanitary flows for the subject property, including external commercial and community park flows.
- Stormwater service is to be provided by capturing stormwater runoff by an internal gravity sewer system that will convey flows to various outlets along the southern boundary to the Foster Ditch which will convey flows to the Jock River. Prior to discharge from the development, any first flush stormwater will have passed through a treatment train of measures in order to provide the appropriate level of Enhanced quality control. The treatment train consists of deep sump catchbasins, LID infiltration trench at catchbasin locations and an end-of-line OGS unit. It is anticipated that quantity control will not be required for discharges to the Jock River.
- A preliminary Hydraulic Grade Line (HGL) modelling analysis has been completed at this time and demonstrates that the HGL is maintained below the ground surface. Another detailed HGL review will be completed for the proposed system at the detailed design level.

ADEQUACY OF SERVICES REPORT  
BARRHAVEN CONSERVANCY DEVELOPMENT CORPORATION

BARRHAVEN CONSERVANCY EAST PHASE 5

20-1180

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- Sump pumps are proposed to be installed for all units within residential blocks and lots;
- The proposed servicing and grading plans are anticipated to meet all City, RVCA, and MECP requirements as set out in background studies and current standards.
- Prior to detailed design of the infrastructure presented in this report, this AES will require approval under the Planning Act as supporting information for the Plan of Subdivision application. Project-specific approvals are also expected to be required for the infrastructure presented in this report from the City of Ottawa, MECP, and Rideau Valley Conservation Authority, among other agencies.

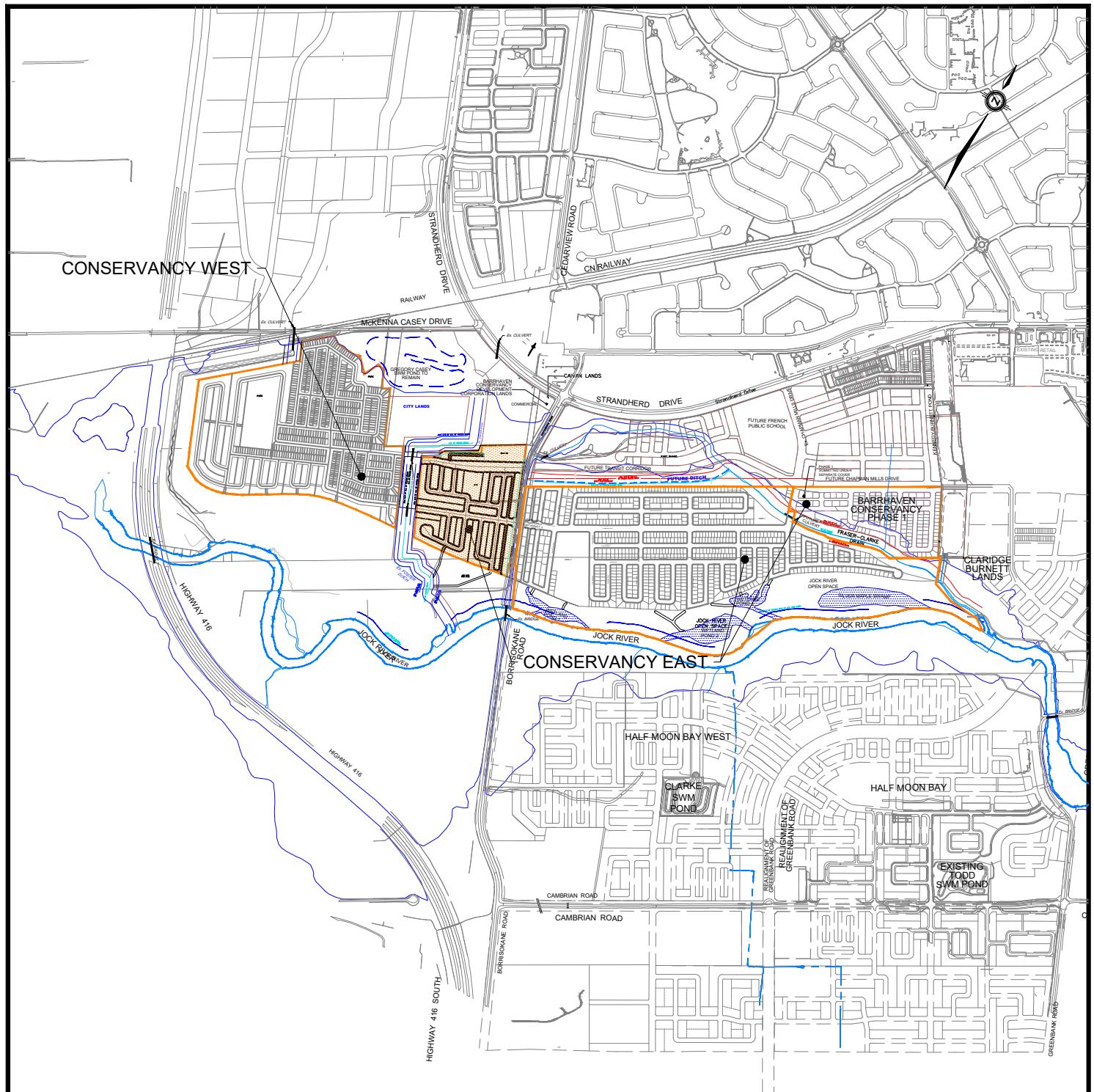
Prepared by,  
**David Schaeffer Engineering Ltd.**



Per: Kevin L. Murphy, P.Eng.

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20221202\_AES\_Conservancy East\_Ph5\_1st\_Subm.doc

## **FIGURES & DRAWINGS**



**DSEL**

120 Iber Road, Unit 103  
Stittsville, ON K2S 1E9  
TEL: (613) 836-0856  
FAX: (613) 836-7183  
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**BARRHAVEN CONSERVANCY  
EAST PHASE 5  
KEY PLAN**

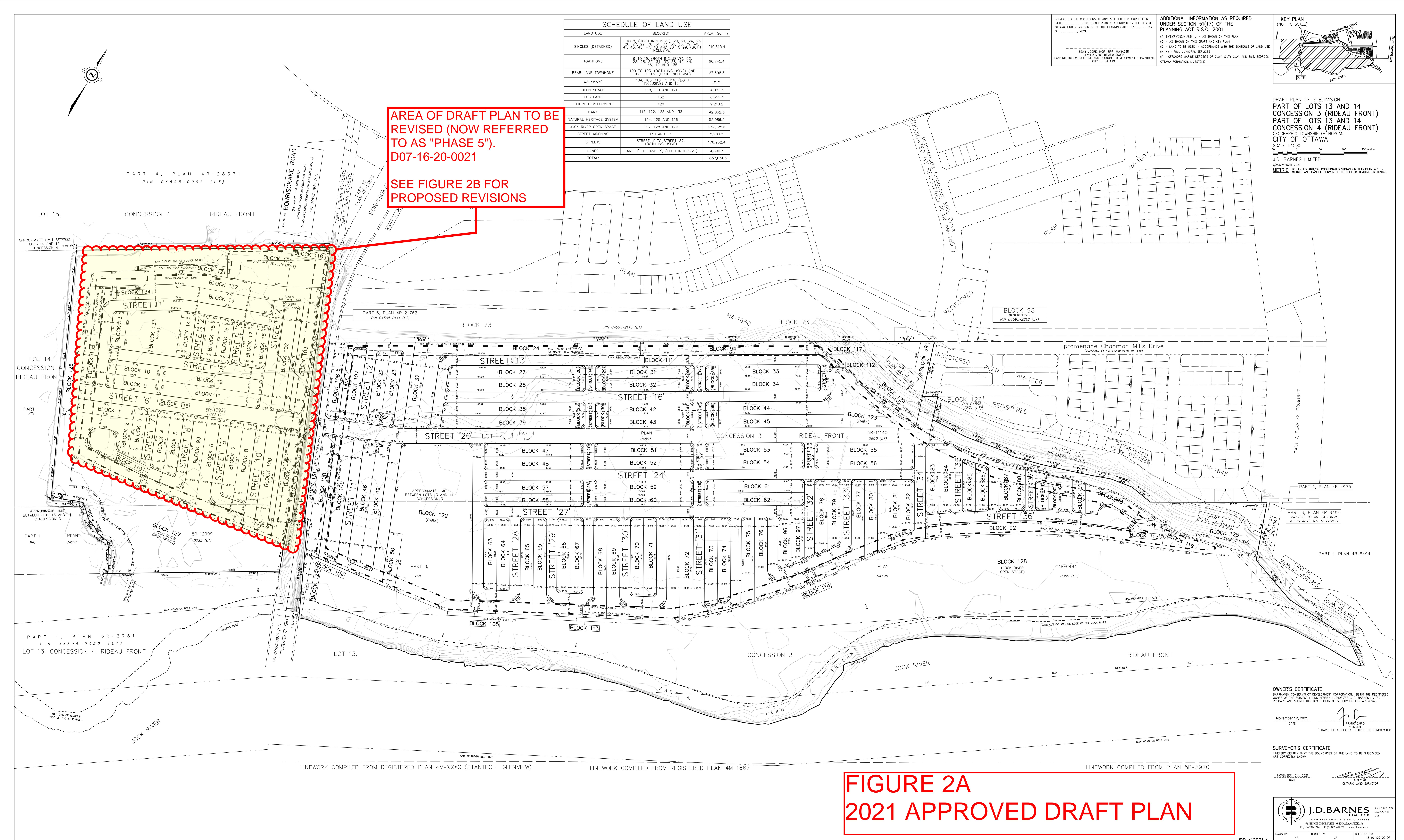
**CITY OF OTTAWA**

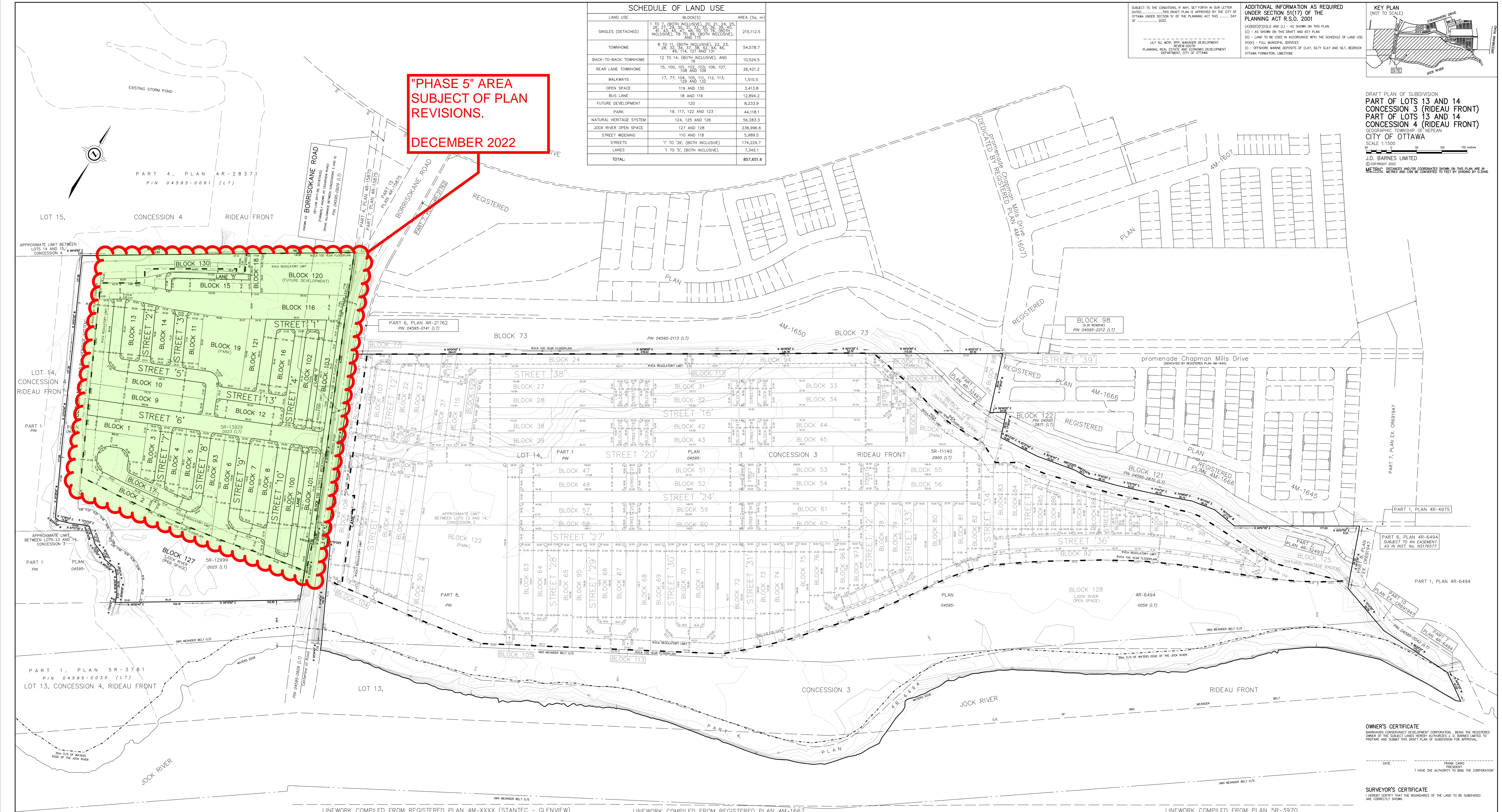
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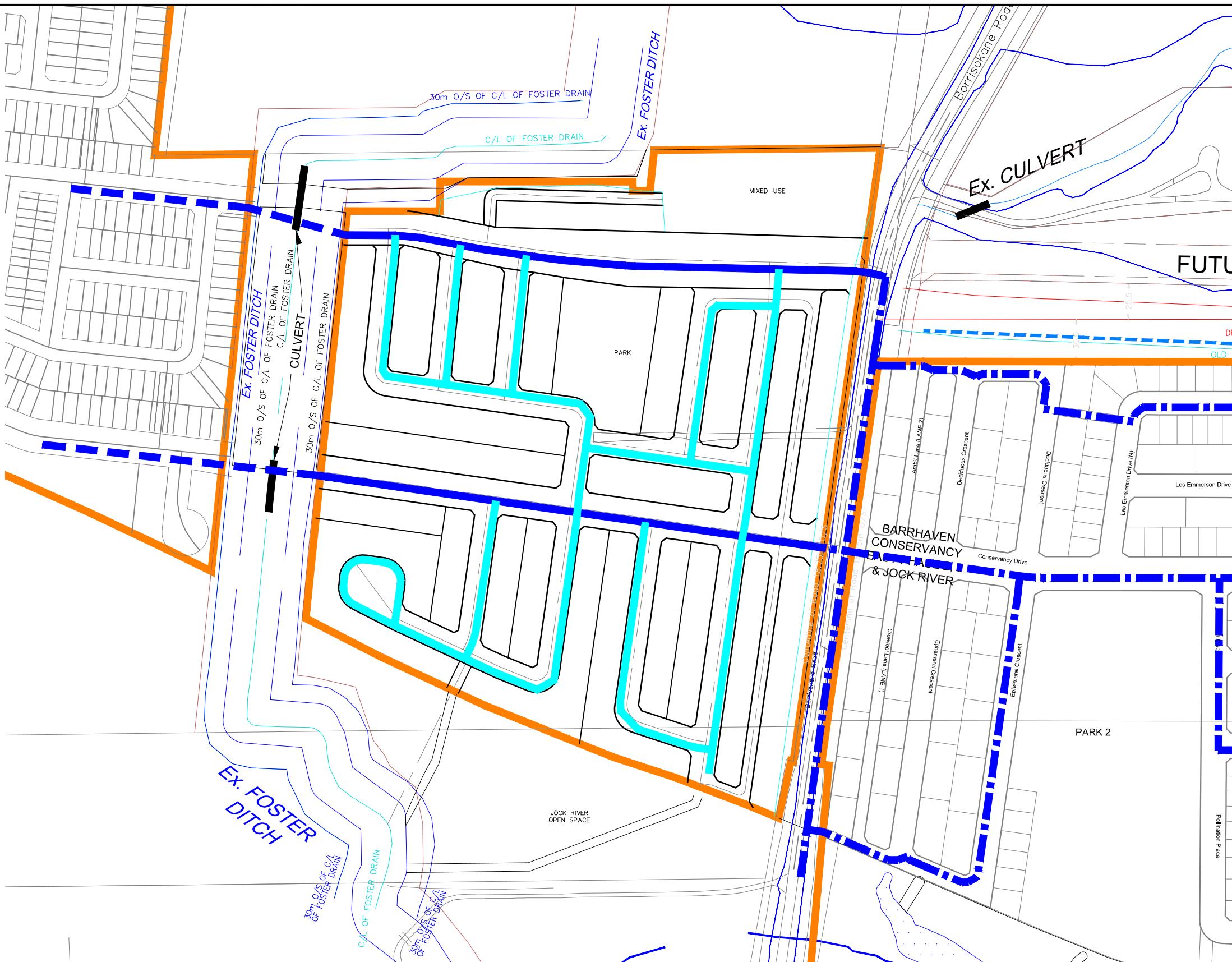
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**FIGURE: 1**





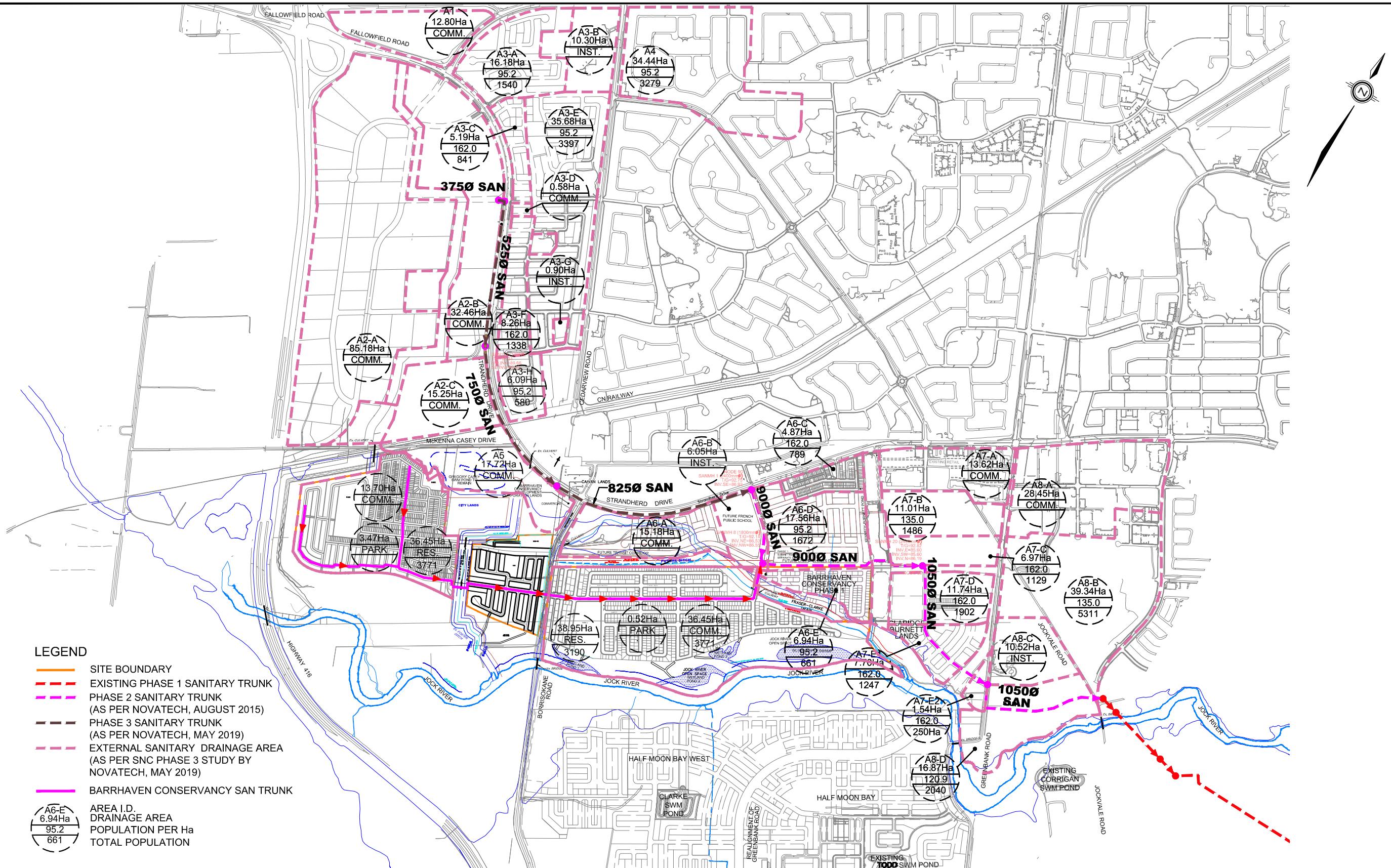
# FIGURE 2B 2022 PROPOSED REVISED DRAFT PLAN



120 Iber Road, Unit 103  
Stittsville, ON K2S 1E9  
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FAX: (613) 836-7183  
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## BARRHAVEN CONSERVANCY EAST PHASE 5 WATERMAIN SERVICING PLAN CITY OF OTTAWA

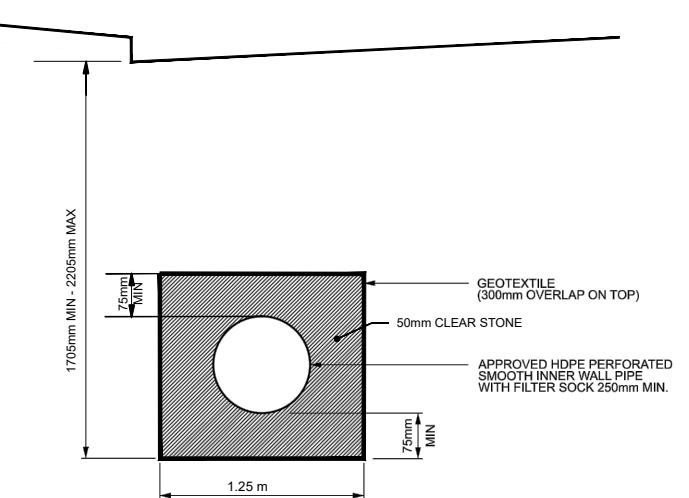
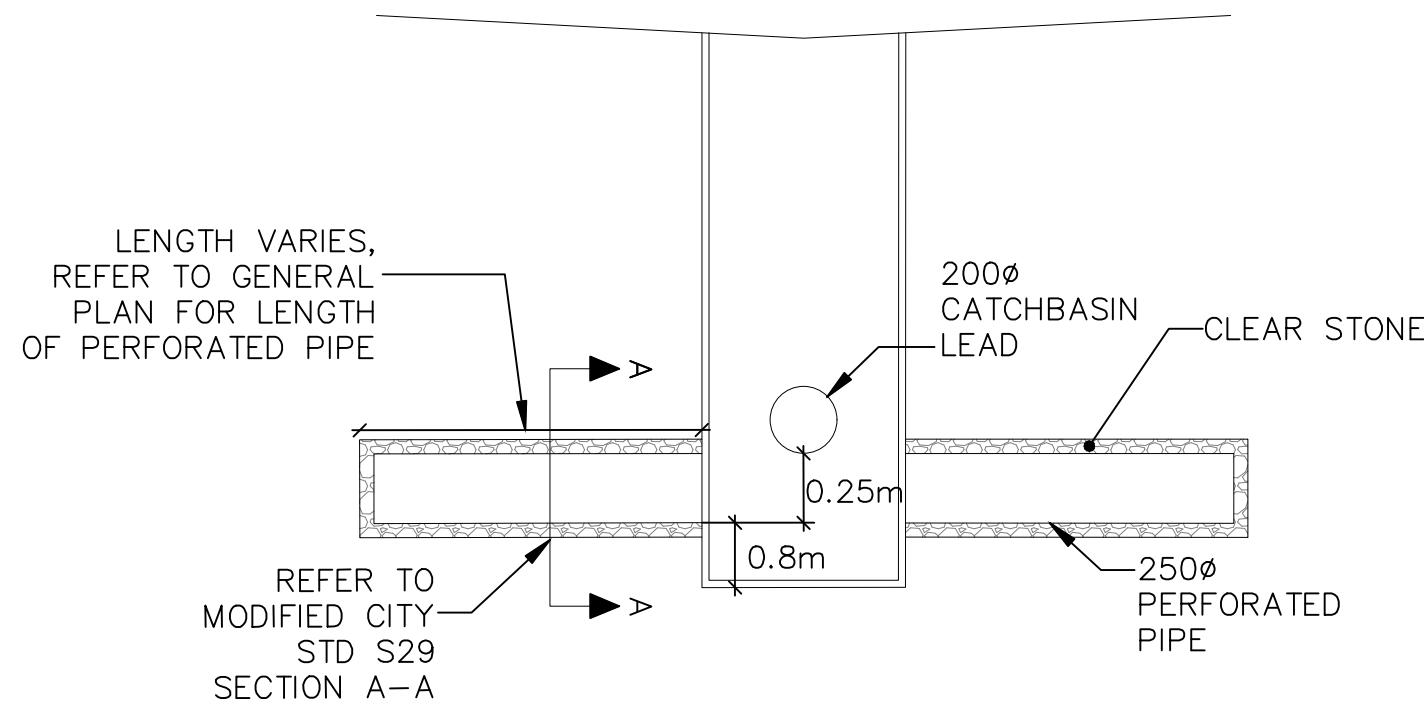
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DATE:	DECEMBER 2022
FIGURE:	3



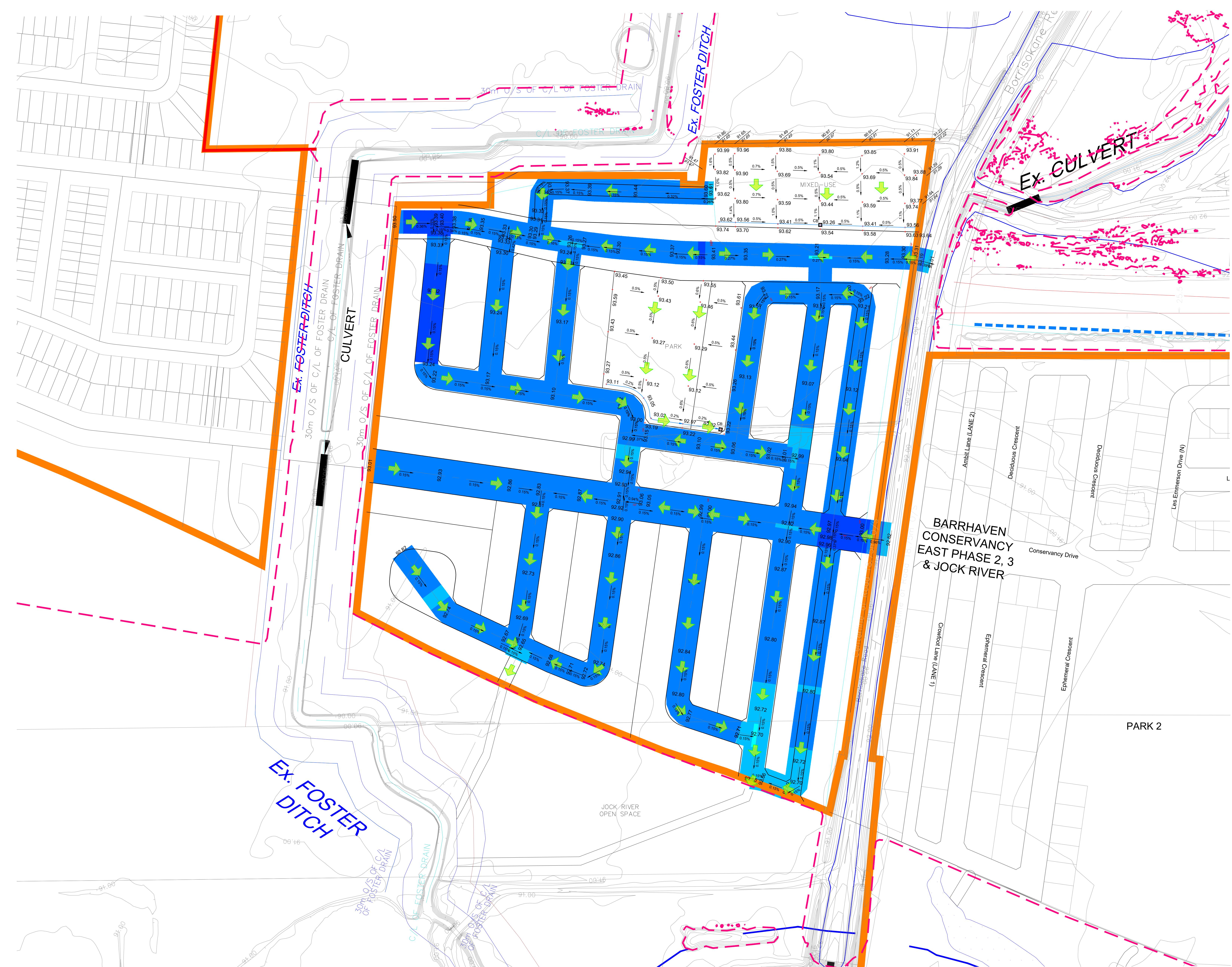
120 Iber Road, Unit 103  
Stittsville, ON K2S 1E9  
TEL: (613) 836-0856  
FAX: (613) 836-7183  
[www.DSEL.ca](http://www.DSEL.ca)

# BARRHAVEN CONSERVANCY EAST PHASE 5 EXTERNAL SANITARY SERVICING CITY OF OTTAWA

PROJECT No.:	20-1180 A-5
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DATE:	DECEMBER 2022
FIGURE:	4



SECTION A-A: MODIFIED CITY STD S29  
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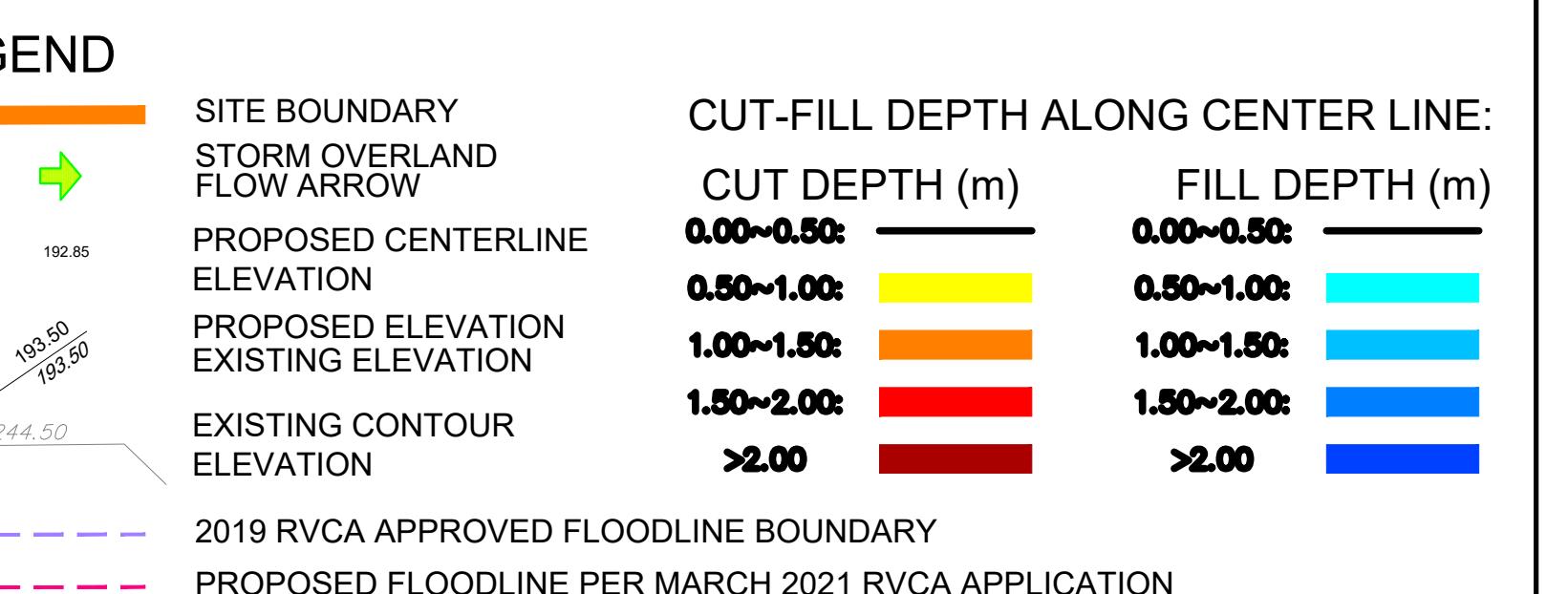


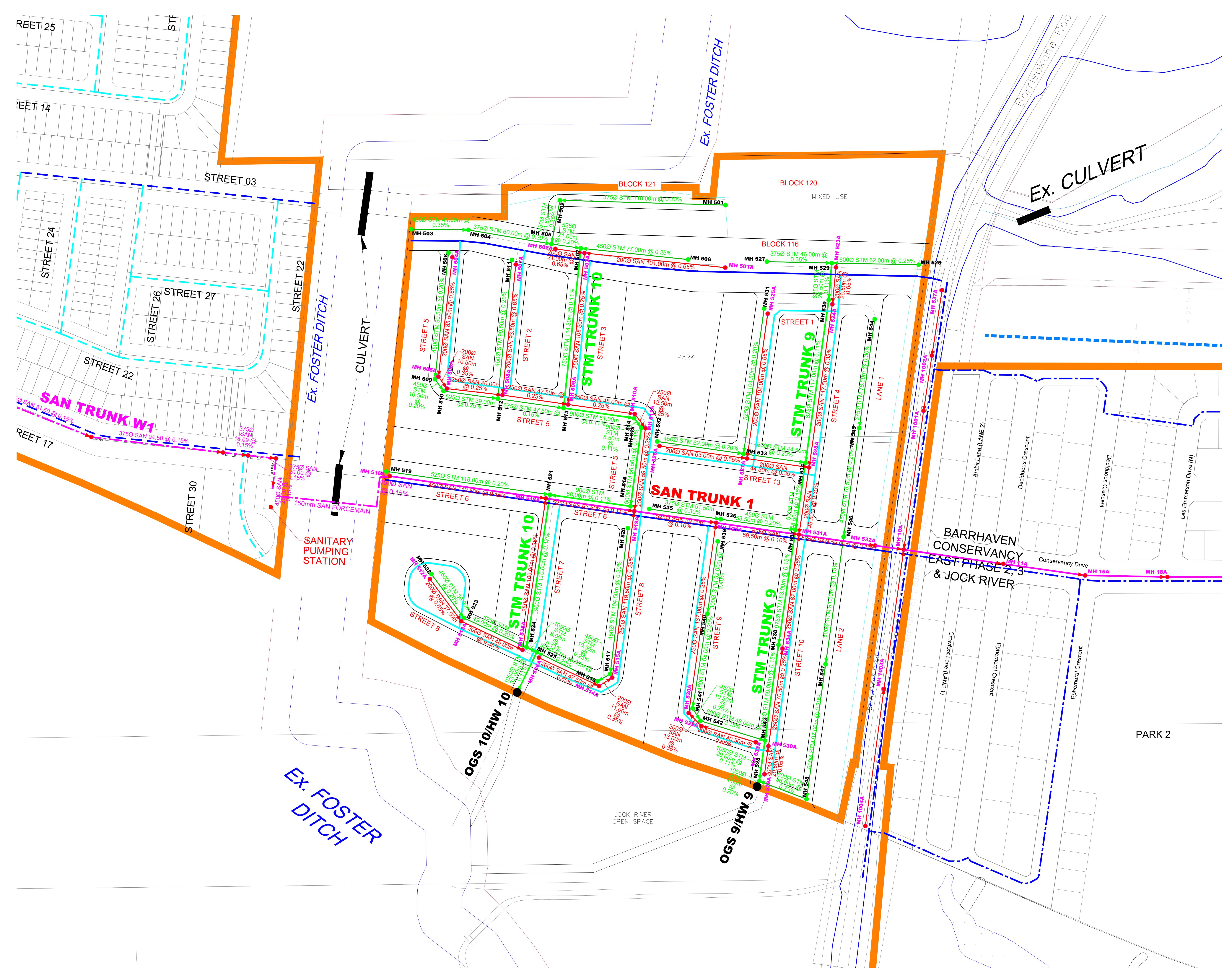
BARRHAVEN CONSERVANCY EAST PHASE 5  
CONCEPTUAL GRADING PLAN  
CITY OF OTTAWA



120 Iber Road, Unit 103  
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PROJECT No.: 20-1180 A-5  
SCALE: 1:1000  
DATE: DECEMBER 2022  
DRAWING No. 1





120 Iber Road, Unit 10  
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# BARRHAVEN CONSERVANCY EAST PHASE 5

## CONCEPTUAL SERVICING PLAN

### CITY OF OTTAWA

PROJECT No. : 20-1180 A-5

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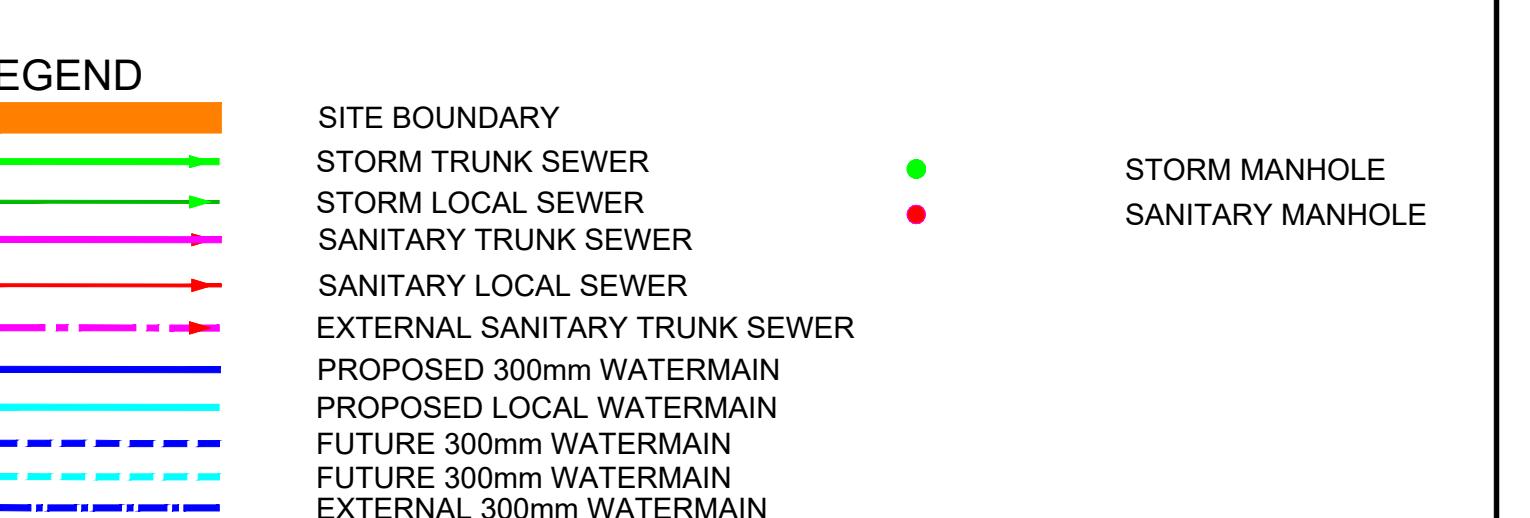
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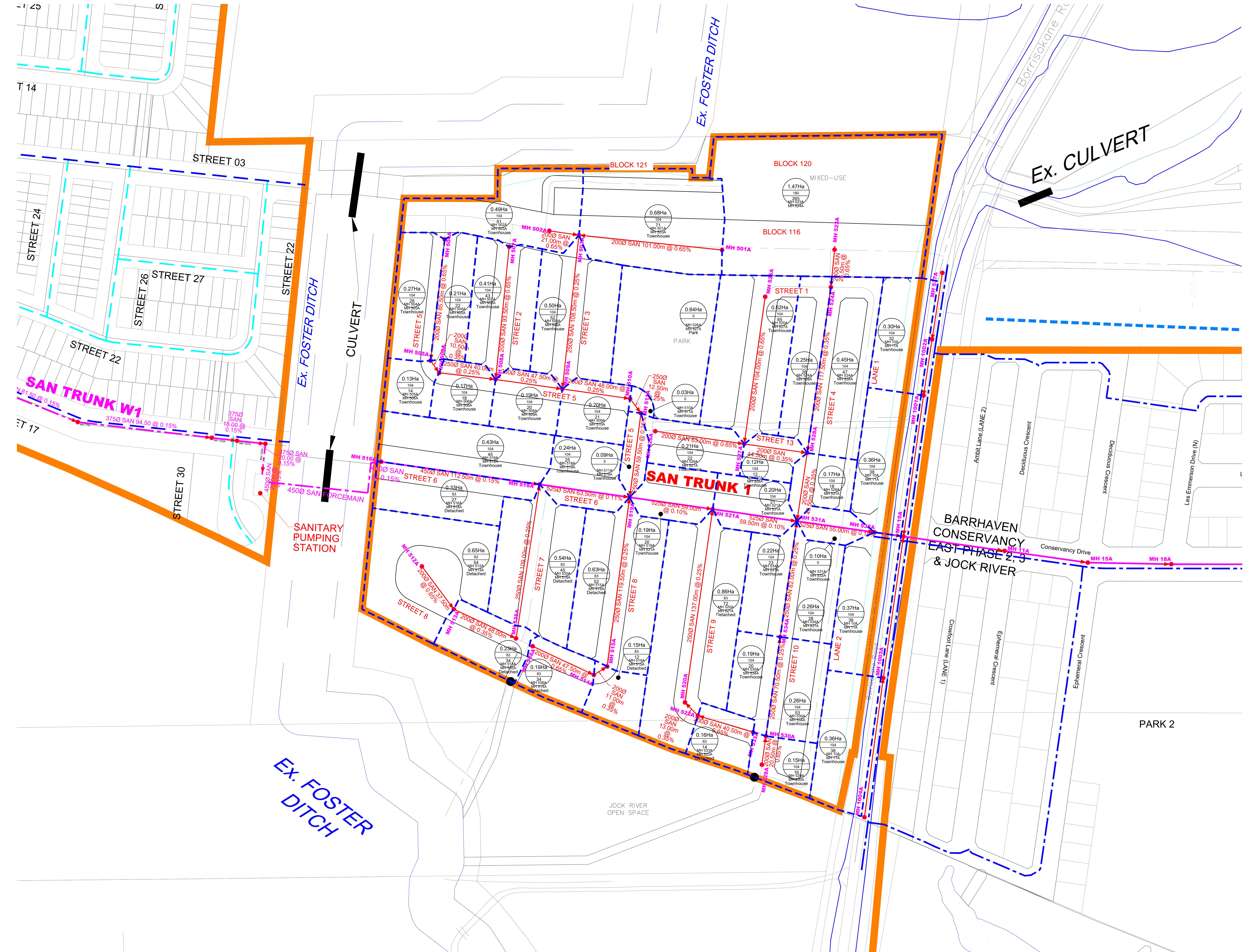
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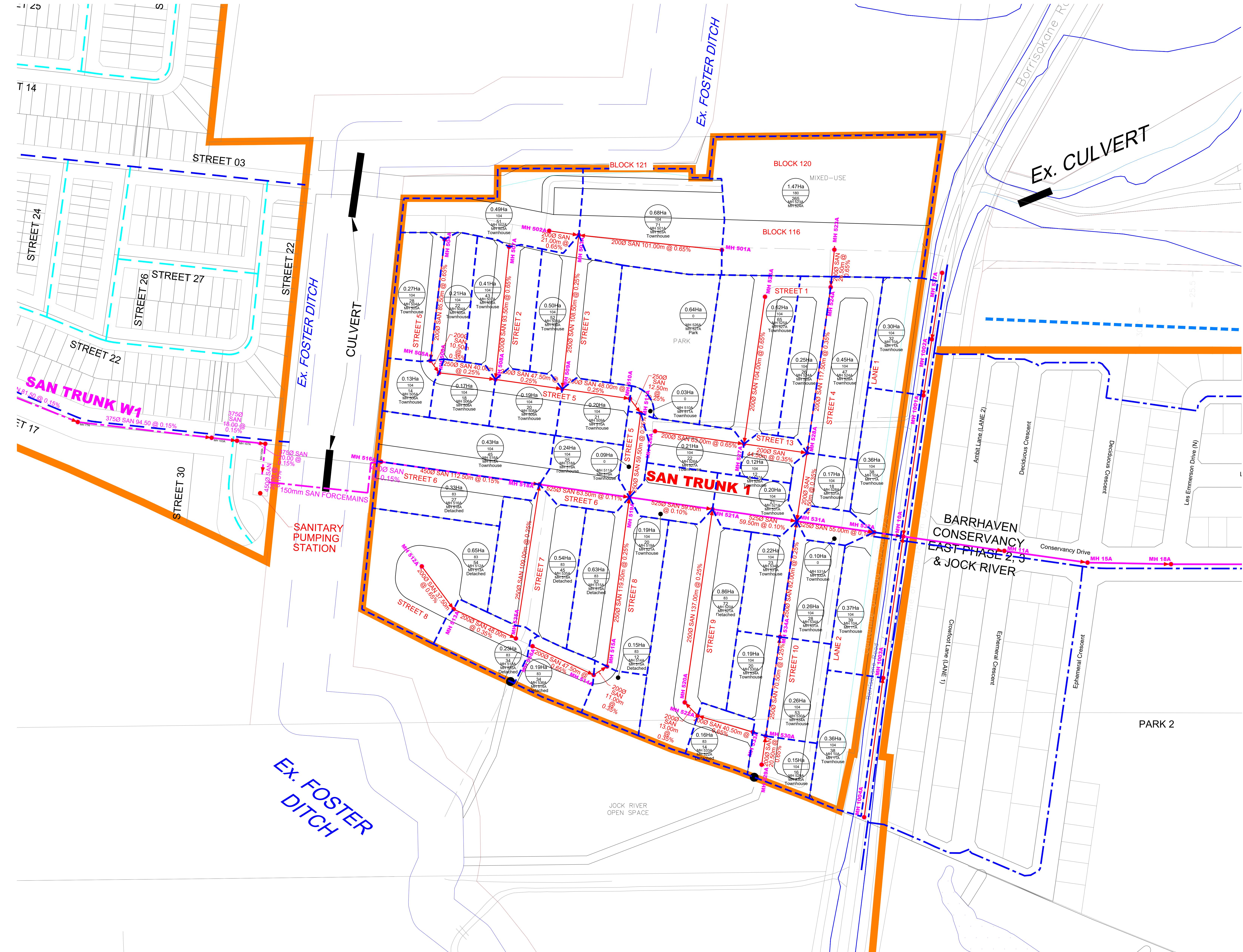
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DRAWING No. 2







**LEGEND**

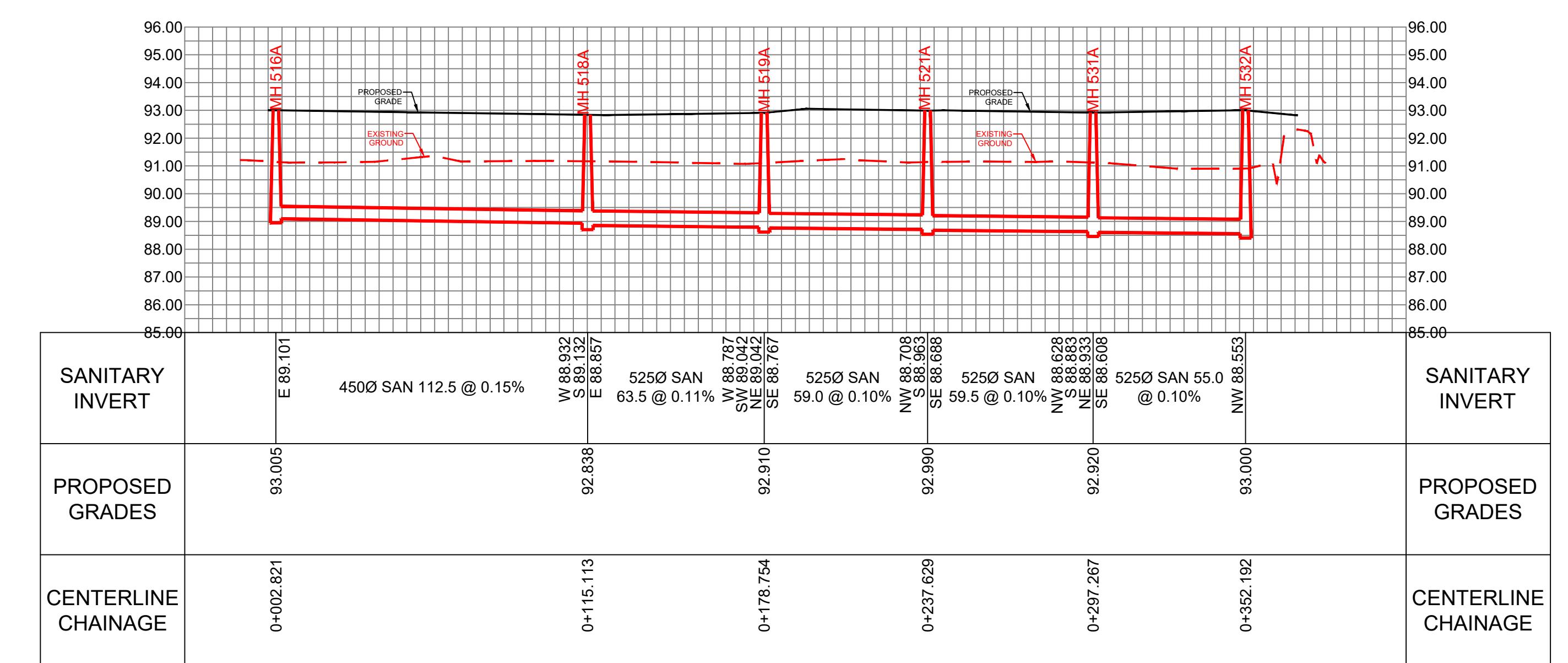
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104  
20  
MH 510A  
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Area Type

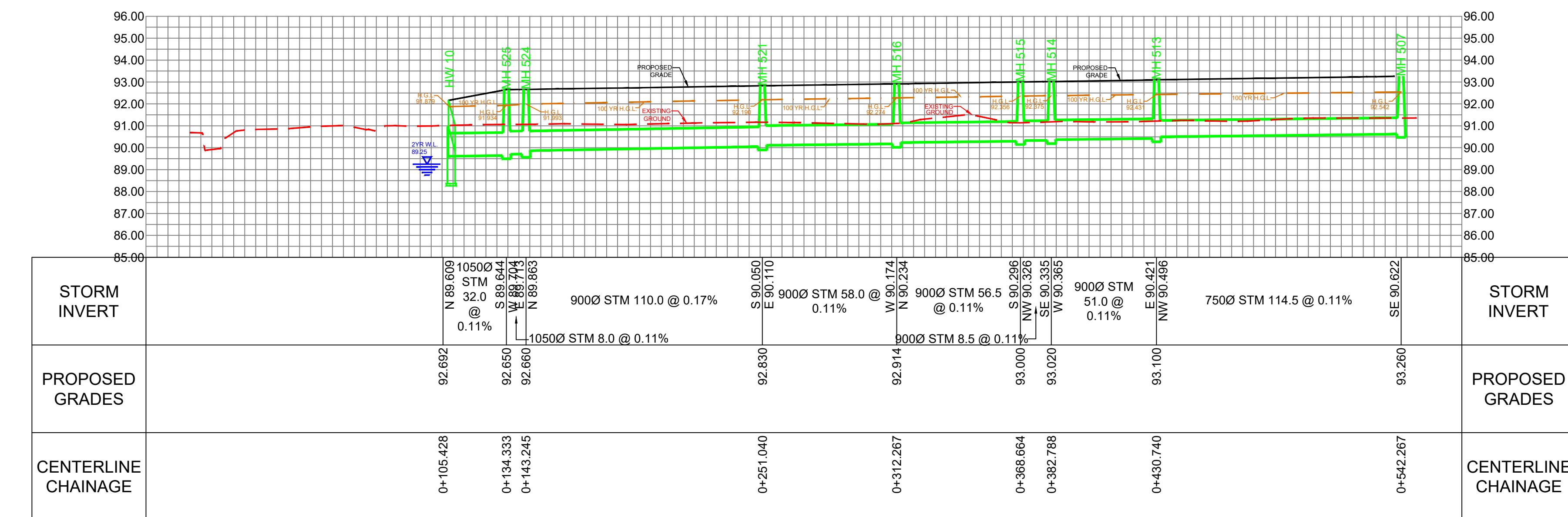
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POPULATION

BARRHAVEN CONSERVANCY EAST PHASE 5  
SANITARY TRIBUTARY AREA  
CITY OF OTTAWA

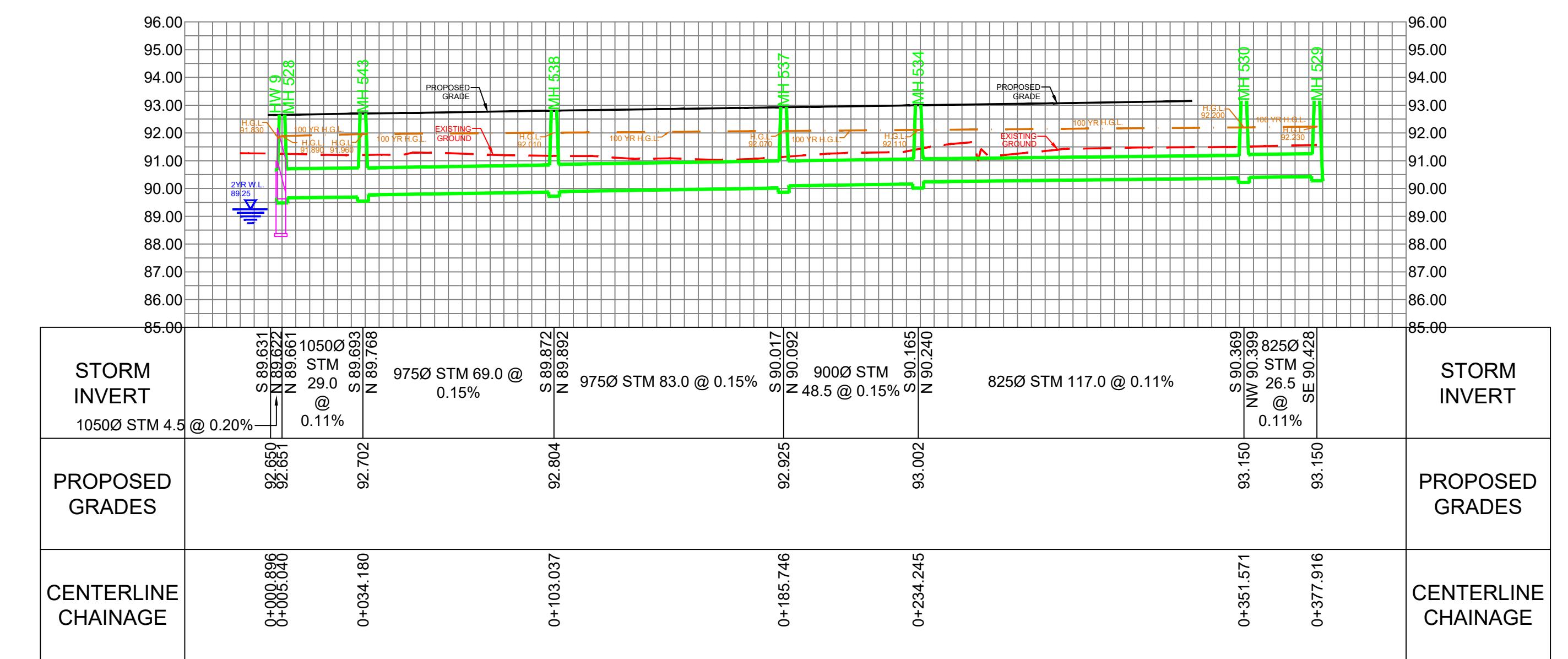
### SAN TRUNK 1



### STM TRUNK 10



### STM TRUNK 9



## **APPENDIX A**

### **GENERAL**

## Content Copy Of Original



Ministry of the Environment and Climate Change  
Ministère de l'Environnement et de l'Action en matière de changement climatique

### ENVIRONMENTAL COMPLIANCE APPROVAL

NUMBER 8129-AB7LDF

Issue Date: June 23, 2016

City of Ottawa  
100 Constellation Crescent West, 6th Floor  
Ottawa, Ontario  
K2G 6J8

Site Location: Jockvale Road and Strandherd Drive  
City of Ottawa, Ontario

*You have applied under section 20.2 of Part II.1 of the Environmental Protection Act , R.S.O. 1990, c. E. 19 (Environmental Protection Act) for approval of:*

sanitary sewers to be constructed in the City of Ottawa, on various vacant development lands (from Station 0+003 to Station 2+517), Greenbank Road (from Station 1+846 to Station 1+947), and Jockvale Road (from Station 2+430 to Station 2+517);

all in accordance with the application form from the City of Ottawa, dated June 22, 2016, including final plans and specifications prepared by Novatech Engineers, Planners and Landscape Architects.

*In accordance with Section 139 of the Environmental Protection Act, you may by written Notice served upon me and the Environmental Review Tribunal within 15 days after receipt of this Notice, require a hearing by the Tribunal. Section 142 of the Environmental Protection Act provides that the Notice requiring the hearing shall state:*

1. The portions of the environmental compliance approval or each term or condition in the environmental compliance approval in respect of which the hearing is required, and;
2. The grounds on which you intend to rely at the hearing in relation to each portion appealed.

*The Notice should also include:*

3. The name of the appellant;
4. The address of the appellant;
5. The environmental compliance approval number;
6. The date of the environmental compliance approval;
7. The name of the Director, and;
8. The municipality or municipalities within which the project is to be engaged in.

*And the Notice should be signed and dated by the appellant.*

*This Notice must be served upon:*

The Secretary\*  
Environmental Review Tribunal  
655 Bay Street, Suite 1500

AND

The Director appointed for the purposes of Part II.1 of the Environmental Protection Act

Toronto, Ontario  
M5G 1E5

Ministry of the Environment and  
Climate Change  
135 St. Clair Avenue West, 1st  
Floor  
Toronto, Ontario  
M4V 1P5

\* Further information on the Environmental Review Tribunal's requirements for an appeal can be obtained directly from the Tribunal at: Tel: (416) 212-6349, Fax: (416) 326-5370 or [www.ert.gov.on.ca](http://www.ert.gov.on.ca)

*The above noted activity is approved under s.20.3 of Part II.1 of the Environmental Protection Act.*

DATED AT TORONTO this 23rd day of June, 2016

Gregory Zimmer, P.Eng.  
Director  
appointed for the purposes of Part II.1 of  
the *Environmental Protection Act*

AF/

c: District Manager, MOECC Ottawa  
Water Supervisor, MOECC, Ottawa  
M. Rick O'Connor, City Clerk, City of Ottawa  
Luc Marineau, City of Ottawa  
Jonathan Knoyle, City of Ottawa  
Bob Dowdall, Novatech Engineers, Planners and Landscape Architects  
Edson Donnelly, Novatech Engineers, Planners and Landscape Architects





Ministry of the Environment, Conservation and Parks  
Ministère de l'Environnement, de la Protection de la nature et des Parcs

## ENVIRONMENTAL COMPLIANCE APPROVAL

NUMBER 4357-CHMQEM

Issue Date: September 1, 2022

Barrhaven Conservancy Development Corporation  
2934 Baseline Road, Suite 302  
Ottawa, Ontario  
K2H 1B2

Site Location: Barrhaven Conservancy East - Phase 2, 3 & Jock River  
Part of Lots 13 & 14 (Rideau Front)  
City of Ottawa, Ontario

*You have applied under section 20.2 of Part II.1 of the Environmental Protection Act, R.S.O. 1990, c. E. 19 (Environmental Protection Act) for approval of:*

the establishment of wastewater infrastructure Works located in the City of Ottawa, consisting of the following:

- **sanitary sewers** on Les Emmerson Drive (N)(from Station 0+000.000 to Station 0+720.000), Les Emmerson Drive (S) (from Station 0+000.000 to Station 0+660.000), Conservancy Drive (from Station 0-010.000 to Station 0+973.545), Peninsula Road (from Station 0+010.058 to Station 0+703.797), Sapling Grove (from Station 0+000.000 to Station 0+528.245), Canoe Street (from Station 0+000.000 to Station 0+491.136), Deciduous Crescent (from Station 0+002.000 to Station 0+328.189), Ephemeral Crescent (from Station 0+000.000 to Station 0+492.987), Mineral Street (from Station 0+242.832 to Station 0+000.000), Pollination Place (from Station 0+002.985 to Station 0+433.904), Gallium Crescent (from Station 0+002.728 to Station 0+321.940), Syringa Court (from Station 0+000.000 to Station 0+332.328), Anemone Mews (from Station 0+242.833 to Station 0+059.755), Ainsworth Crescent (from Station 0+002.715 to Station 0+353.228), Ecology Lane (from Station 0+205.411 to Station 0+007.658), Meander Way (from Station 0+002.747 to Station 0+333.559), Elation Heights (from Station 0+000.000 to Station 0+380.000), Jollity Crescent (from Station 0+001.794 to Station 0+221.612), Euphoria Crescent (from Station 0+000.000 to Station 0+170.000), and on Borrisokane Road (from Station 0+168.736 to Station 0+507.126), all discharging to the existing South Nepean Collector sanitary sewer; and

- **storm sewers** on Les Emmerson Drive (N) (from Station 0+002.919 to Station 0+718.915), Les Emmerson Drive (S) (from Station 0-002.269 to Station 0+676.895), Conservancy Drive (from Station 0+020.468 to Station 0+961.195), Peninsula Road (from Station 0-001.986 to Station 0+705.797), Sapling Grove (from Station 0-010.000 to Station 0+526.245), Canoe Street (from Station 0+000.000 to Station 0+493.136), Deciduous Crescent (from Station 0+004.500 to Station 0+324.827), Ephemeral Crescent (from Station 0-002.063 to Station 0+495.738), Mineral Street (from Station 0+244.847 to Station 0+002.015), Pollination Place (from Station 0+000.000 to Station 0+424.262), Gallium Crescent (from Station 0+000.000 to Station 0+325.307), Syringa Court (from Station 0-001.985 to Station 0+334.348), Anemone Mews (from Station 0+244.843 to Station 0+001.982), Ainsworth Crescent (from Station 0+000.000 to Station 0+354.443), Ecology Lane (from Station 0+207.411 to Station 0+006.523), Meander Way (from Station 0+016.643 to Station 0+335.359), Elation Heights (from Station 0+000.000 to Station 0+381.539), Jollity Crescent (from Station 0+003.277 to Station 0+220.000), Euphoria Crescent (from Station 0+003.400 to Station 0+157.175), Lane 1 (Crowfoot Lane) (from Station 0-002.000 to Station 0+201.525), and on Lane 2 (Ambit Lane) (from Station 0+002.000 to Station 0+127.5060), proposed storm sewers collect flows from the subdivision and discharge to the Jock River and the Fraser-Clarke Watercourse which is an existing tributary to the Jock River;

the modification of a section of the Fraser-Clarke Watercourse to accommodate stormwater outflows from Phase 2 of the Barrhaven Conservancy East Subdivision development, for the collection and transmission of stormwater runoff for all storm events up to and including the 100-year storm event, discharging to the Jock River, consisting of the following:

- **approximately 950 metres long modified channel**, located along the northern boundary of the Barrhaven Conservancy East Phase 2, 3 & Jock River, having a channel gradient of 0.09% and 3:1 side slopes, complete with low flow path and riffle-pool sequences and erosion protection structures, including two (2) 2.4 metre by 1.2 metre box culverts under the future Canoe Street crossing, discharging to the Jock River;

the establishment of stormwater management Works to serve the Barrhaven Conservancy East – Phase 2, 3 & Jock River development, located in the City of Ottawa, for the collection, transmission, treatment and disposal of stormwater runoff from a total catchment area of 44.17 hectares, to provide Enhanced Level protection and to provide on-site retention of 22.5 cubic metres per hectare, discharging to proposed storm sewers, consisting of the following:

- **subsurface infiltration trenches (catchment area 41.81 hectares)**, located on-site within proposed roadways, having a total length of 3,514 metres, a width of 1.75 metres, a base area of 6,150 square metres, a maximum allowable storage depth of 0.40 metres and a maximum available storage volume of 1,087 cubic metres, comprised of a 75 millimetre deep clear stone layer overlying a geotextile non-woven filter fabric, complete with a 250 millimetre diameter perforated storm sub-drain installed in the clear stone layer, installed at select street catch basin manhole locations;

the establishment of stormwater management Works to serve Steeves & Rozema Enterprises Limited, located in the City of Sarnia, consisting of the following:

- **oil and grit separator (catchment area 5.52 hectares):** one (1) oil and grit separator (OGS1), CDS Model PMSU4040-8 or Equivalent Equipment, located within the Canoe Street right-of-way, providing a Predicted Net Annual Load Removal Efficiency of 83%, having a sediment storage capacity of 4,270 litres, an oil storage capacity of 1,970 litres, a total storage volume of approximately 10,910 litres, and a maximum treatment rate of 170 litres per second, receiving inflow from the storm sewer located within the Canoe Street right-of-way, discharging via a 975 millimetre diameter outlet pipe to an outlet channel on Block 774 and connecting to the Jock River;
- **oil and grit separator (catchment area 5.59 hectares):** one (1) oil and grit separator (OGS2), CDS Model PMSU4040-8 or Equivalent Equipment, located within Servicing Block 767, providing a Predicted Net Annual Load Removal Efficiency of 82.1%, having a sediment storage capacity of 4,270 litres, an oil storage capacity of 1,970 litres, a total storage volume of approximately 10,910 litres, and a maximum treatment rate of 170 litres per second, receiving inflow from the storm sewer located within the Block 767 and Meander Way right-of-way, discharging via a 975 millimetre diameter outlet pipe to an outlet channel on Block 774 and connecting to the Jock River;
- **oil and grit separator (catchment area 6.77 hectares):** one (1) oil and grit separator (OGS3), CDS Model PMSU4045-8 or Equivalent Equipment, located within the Ainsworth Crescent right-of-way, providing a Predicted Net Annual Load Removal Efficiency of 82.4%, having a sediment storage capacity of 4,270 litres, an oil storage capacity of 2,149 litres, a total storage volume of approximately 11,510 litres, and a maximum treatment rate of 212 litres per second, receiving inflow from the storm sewer located within the Ainsworth Crescent right-of-way, discharging via a 975 millimetre diameter outlet pipe to an outlet channel on Block 774 and connecting to the Jock River;
- **oil and grit separator (catchment area 8.42 hectares):** one (1) oil and grit separator (OGS5), CDS Model PMSU5640-10 or Equivalent Equipment, located within Servicing Block 766, providing a Predicted Net Annual Load Removal Efficiency of 81.7%, having a sediment storage capacity of 6,672 litres, an oil storage capacity of 2,869 litres, a total storage volume of approximately 17,070 litres, and a maximum treatment rate of 255 litres per second, receiving inflow from the storm sewer located within Block 766 and the Gallium Crescent right-of-way, discharging via a 1050 millimetre diameter outlet pipe to an outlet channel on Block 774 and connecting to the Jock River;

- **oil and grit separator (catchment area 5.46 hectares):** one (1) oil and grit separator (OGS6), CDS Model PMSU3035-8 or Equivalent Equipment, located within Servicing Block 765, providing a Predicted Net Annual Load Removal Efficiency of 80.0%, having a sediment storage capacity of 4,270 litres, an oil storage capacity of 1,493 litres, a total storage volume of approximately 10,210 litres, and a maximum treatment rate of 108 litres per second, receiving inflow from the storm sewer located within Block 766 and the Pollination Place right-of-way, discharging via a 900 millimetre diameter outlet pipe to an outlet channel on Block 774 and connecting to the Jock River;
- **oil and grit separator (catchment area 5.05 hectares):** one (1) oil and grit separator (OGS7), CDS Model PMSU4040-8 or Equivalent Equipment, located within the Ephemeral Crescent right-of-way, providing a Predicted Net Annual Load Removal Efficiency of 82.3%, having a sediment storage capacity of 4,270 litres, an oil storage capacity of 1,970 litres, a total storage volume of approximately 10,910 litres, and a maximum treatment rate of 170 litres per second, receiving inflow from the storm sewer located within the Ephemeral Crescent right-of-way, discharging via a 900 millimetre diameter outlet pipe to an outlet channel on Block 774 and connecting to the Jock River;
- **oil and grit separator (catchment area 4.52 hectares):** one (1) oil and grit separator (OGS8), CDS Model PMSU4040-8 or Equivalent Equipment, located within Servicing Block 744, providing a Predicted Net Annual Load Removal Efficiency of 82.1%, having a sediment storage capacity of 4,270 litres, an oil storage capacity of 1,970 litres, a total storage volume of approximately 10,910 litres, and a maximum treatment rate of 170 litres per second, receiving inflow from the storm sewer located within the Borrisokane Road right-of-way, discharging via a 1200 millimetre diameter outlet pipe to an outlet channel on Block 774 and connecting to the Jock River;
- **oil and grit separator (catchment area 1.63 hectares):** one (1) oil and grit separator (OGS12), CDS Model PMSU2025-5 or Equivalent Equipment, located within Servicing Block 317, providing a Predicted Net Annual Load Removal Efficiency of 81.1%, having a sediment storage capacity of 1,668 litres, an oil storage capacity of 439 litres, a total storage volume of approximately 3,330 litres, and a maximum treatment rate of 45 litres per second, receiving inflow from the storm sewer located within the Les Emmerson Drive right-of-way, discharging via a 600 millimetre diameter outlet pipe to an outlet channel connecting to the Fraser-Clarke watercourse;
- **oil and grit separator (catchment area 1.21 hectares):** one (1) oil and grit separator (OGS13), CDS Model PMSU2020-5 or Equivalent Equipment, located within the Deciduous Crescent right-of-way, providing a Predicted Net Annual Load Removal Efficiency of 80.1%, having a sediment storage capacity of 1,668 litres, an oil storage capacity of 376 litres, a total storage volume of approximately 3,150 litres, and a maximum treatment rate of 31 litres per second, receiving inflow from the storm sewer located within the Deciduous Crescent right-of-way, discharging via a 600 millimetre diameter outlet pipe to an outlet channel connecting to the Fraser-Clarke watercourse;

including erosion/sedimentation control measures during construction and all other controls and appurtenances essential for the proper operation of the aforementioned Works;

all in accordance with the submitted application and supporting documents listed in Schedule "A" forming part of this Approval.

*For the purpose of this environmental compliance approval, the following definitions apply:*

1. "Approval" means this entire document and any schedules attached to it, and the application;
2. "Director" means a person appointed by the Minister pursuant to section 5 of the EPA for the purposes of Part II.1 of the EPA;
3. "District Manager" means the District Manager of the appropriate local District Office of the Ministry, where the Works are geographically located;
4. "EPA" means the *Environmental Protection Act*, R.S.O. 1990, c.E.19, as amended;
5. "Equivalent Equipment" means a substituted equipment or like-for-like equipment that meets the required quality and performance standards of the approved named equipment.
6. "Ministry" means the ministry of the government of Ontario responsible for the EPA and OWRA and includes all officials, employees or other persons acting on its behalf;
7. "Owner" means Barrhaven Conservancy Development Corporation, and includes its successors and assignees;
8. "OWRA" means the *Ontario Water Resources Act*, R.S.O. 1990, c. O.40 , as amended;
9. "Works" means the sewage Works described in the Owner's application, and this Approval.

*You are hereby notified that this environmental compliance approval is issued to you subject to the terms and conditions outlined below:*

## **TERMS AND CONDITIONS**

### **1. GENERAL CONDITIONS**

1. The Owner shall ensure that any person authorized to carry out work on or operate any aspect of the Works is notified of this Approval and the conditions herein and shall take all reasonable measures to ensure any such person complies with the same.

2. Except as otherwise provided by these Conditions, the Owner shall design, build, install, operate and maintain the Works in accordance with the description given in this Approval, and the application for approval of the Works.
3. Where there is a conflict between a provision of any document in the schedule referred to in this Approval and the conditions of this Approval, the conditions in this Approval shall take precedence, and where there is a conflict between the documents in the schedule, the document bearing the most recent date shall prevail.
4. Where there is a conflict between the documents listed in Schedule "A" and the application, the application shall take precedence unless it is clear that the purpose of the document was to amend the application.
5. The conditions of this Approval are severable. If any condition of this Approval, or the application of any requirement of this Approval to any circumstance, is held invalid or unenforceable, the application of such condition to other circumstances and the remainder of this Approval shall not be affected thereby.

## **2. EXPIRY OF APPROVAL**

1. This Approval will cease to apply to those parts of the Works which have not been constructed within five (5) years of the date of this Approval.
2. In the event that completion and commissioning of any portion of the Works is anticipated to be delayed beyond the specified expiry period, the Owner shall submit an application of extension to the expiry period, at least twelve (12) months prior to the end of the period. The application for extension shall include the reason(s) for the delay, whether there is any design change(s) and a review of whether the standards applicable at the time of Approval of the Works are still applicable at the time of request for extension, to ensure the ongoing protection of the environment.

## **3. CHANGE OF OWNER**

1. The Owner shall notify the District Manager and the Director, in writing, of any of the following changes within thirty (30) days of the change occurring:
  - a. change of Owner;
  - b. change of address of the Owner;
  - c. change of partners where the Owner is or at any time becomes a partnership, and a copy of the most recent declaration filed under the *Business Names Act*, R.S.O. 1990, c.B17 shall be included in the notification to the District Manager; or

- d. change of name of the corporation where the Owner is or at any time becomes a corporation, and a copy of the most current information filed under the *Corporations Information Act*, R.S.O. 1990, c. C39 shall be included in the notification to the District Manager.
2. In the event of any change in ownership of the Works, other than a change to a successor municipality, the Owner shall notify in writing the succeeding owner of the existence of this Approval, and a copy of such notice shall be forwarded to the District Manager and the Director.
3. The Owner shall ensure that all communications made pursuant to this condition refer to the number at the top of this Approval.

#### **4. OPERATION AND MAINTENANCE**

1. If applicable, any proposed storm sewers or other stormwater conveyance in this Approval can be constructed but not operated until the proposed stormwater management facilities in this Approval or any other Approval that are designed to service the storm sewers or other stormwater conveyance are in operation.
2. The Owner shall make all necessary investigations, take all necessary steps and obtain all necessary approvals so as to ensure that the physical structure, siting and operations of the Works do not constitute a safety or health hazard to the general public.
3. The Owner shall undertake an inspection of the condition of the Works, at least once a year, and undertake any necessary cleaning and maintenance to ensure that sediment, debris and excessive decaying vegetation are removed from the Works to prevent the excessive build-up of sediment, oil/grit, debris and/or decaying vegetation, to avoid reduction of the capacity and/or permeability of the Works, as applicable. The Owner shall also regularly inspect and clean out the inlet to and outlet from the Works to ensure that these are not obstructed.
4. The Owner shall construct, operate and maintain the Works with the objective that the effluent from the Works is essentially free of floating and settleable solids and does not contain oil or any other substance in amounts sufficient to create a visible film, sheen, foam or discoloration on the receiving waters.
5. The Owner shall maintain a logbook to record the results of these inspections and any cleaning and maintenance operations undertaken, and shall keep the logbook at the Owner's administrative office for inspection by the Ministry. The logbook shall include the following:
  - a. the name of the Works; and
  - b. the date and results of each inspection, maintenance and cleaning, including an estimate of the quantity of any materials removed and method of clean-out of the Works.

6. The Owner shall prepare an operations manual prior to the commencement of operation of the Works that includes, but is not necessarily limited to, the following information:
  - a. operating and maintenance procedures for routine operation of the Works;
  - b. inspection programs, including frequency of inspection, for the Works and the methods or tests employed to detect when maintenance is necessary;
  - c. repair and maintenance programs, including the frequency of repair and maintenance for the Works;
  - d. contingency plans and procedures for dealing with potential spills and any other abnormal situations and for notifying the District Manager; and
  - e. procedures for receiving, responding and recording public complaints, including recording any follow-up actions taken.
7. The Owner shall maintain the operations manual current and retain a copy at the Owner's administrative office for the operational life of the Works. Upon request, the Owner shall make the manual available to Ministry staff.

## **5. TEMPORARY EROSION AND SEDIMENT CONTROL**

1. The Owner shall install and maintain temporary sediment and erosion control measures during construction and conduct inspections once every two (2) weeks and after each significant storm event (a significant storm event is defined as a minimum of 25 mm of rain in any 24 hours period). The inspections and maintenance of the temporary sediment and erosion control measures shall continue until they are no longer required and at which time they shall be removed and all disturbed areas reinstated properly.
2. The Owner shall maintain records of inspections and maintenance which shall be made available for inspection by the Ministry, upon request. The record shall include the name of the inspector, date of inspection, and the remedial measures, if any, undertaken to maintain the temporary sediment and erosion control measures.

## **6. REPORTING**

1. One (1) week prior to the start-up of the operation of the Works, the Owner shall notify the District Manager (in writing) of the pending start-up date.
2. The Owner shall, upon request, make all reports, manuals, plans, records, data, procedures and supporting documentation available to Ministry staff.

3. The Owner shall prepare a performance report within ninety (90) days following the end of the period being reported upon, and submit the report(s) to the District Manager when requested. The first such report shall cover the first annual period following the commencement of operation of the Works and subsequent reports shall be prepared to cover successive annual periods following thereafter. The reports shall contain, but shall not be limited to, the following information:
  - a. a description of any operating problems encountered and corrective actions taken;
  - b. a summary of all maintenance carried out on any major structure, equipment, apparatus, mechanism or thing forming part of the Works, including an estimate of the quantity of any materials removed from the Works;
  - c. a summary of any complaints received during the reporting period and any steps taken to address the complaints;
  - d. a summary of all spill or abnormal discharge events; and
  - e. any other information the District Manager requires from time to time.

## **7. RECORD KEEPING**

1. The Owner shall retain for a minimum of five (5) years from the date of their creation, all records and information related to or resulting from the operation, maintenance and monitoring activities required by this Approval.

### **Schedule "A"**

1. Application for Environmental Compliance Approval, dated August 9, 2022 and received on August 17, 2022, submitted by Barrhaven Conservancy Development Corporation;
2. Transfer of Review Letter of Recommendation, dated August 17, 2022 and signed by Jeff Shillington, P.Eng., Senior Project Manager, Development Review, City of Ottawa , including the following supporting documents:
  - a. Final Plans and Specifications prepared by David Schaeffer Engineering Ltd.
  - b. Pipe Data Form - Watermain, Storm Sewer, Sanitary Sewer, and Force main Design Supplement to Application for Approval for Water and Sewage Works.
  - c. Hydraulic Design Sheets prepared by David Schaeffer Engineering Ltd.
  - d. Stormwater Management Report prepared by David Schaeffer Engineering Ltd.
  - e. Design brief, calculations and specifications prepared by David Schaeffer Engineering Ltd.
3. Email received on August 25, 2022 from Jeff Shillington, City of Ottawa.

*The reasons for the imposition of these terms and conditions are as follows:*

1. Condition 1 is imposed to ensure that the Works are constructed and operated in the manner in which they were described and upon which approval was granted. This condition is also included to emphasize the precedence of conditions in the Approval and the practice that the Approval is based on the most current document, if several conflicting documents are submitted for review.
2. Condition 2 is included to ensure that, when the Works are constructed, the Works will meet the standards that apply at the time of construction to ensure the ongoing protection of the environment.
3. Condition 3 is included to ensure that the Ministry records are kept accurate and current with respect to the approved Works and to ensure that subsequent owners of the Works are made aware of the Approval and continue to operate the Works in compliance with it.
4. Condition 4 is included as regular inspection and necessary removal of sediment and excessive decaying vegetation from the Works are required to mitigate the impact of sediment, debris and/or decaying vegetation on the treatment capacity of the Works. The Condition also ensures that adequate storage is maintained in the Works at all times as required by the design. Furthermore, this Condition is included to ensure that the Works are operated and maintained to function as designed.
5. Condition 5 is included as installation, regular inspection and maintenance of the temporary sediment and erosion control measures is required to mitigate the impact on the downstream receiving watercourse during construction until they are no longer required.
6. Condition 6 is included to provide a performance record for future references, to ensure that the Ministry is made aware of problems as they arise, and to provide a compliance record for all the terms and conditions outlined in this Approval, so that the Ministry can work with the Owner in resolving any problems in a timely manner.
7. Condition 7 is included to require that all records are retained for a sufficient time period to adequately evaluate the long-term operation and maintenance of the Works.

In accordance with Section 139 of the *Environmental Protection Act*, you may by written notice served upon me and the Ontario Land Tribunal within 15 days after receipt of this notice, require a hearing by the Tribunal. Section 142 of the *Environmental Protection Act* provides that the notice requiring the hearing ("the Notice") shall state:

- a. The portions of the environmental compliance approval or each term or condition in the environmental compliance approval in respect of which the hearing is required, and;
- b. The grounds on which you intend to rely at the hearing in relation to each portion appealed.

The Notice should also include:

1. The name of the appellant;
2. The address of the appellant;
3. The environmental compliance approval number;
4. The date of the environmental compliance approval;
5. The name of the Director, and;
6. The municipality or municipalities within which the project is to be engaged in.

And the Notice should be signed and dated by the appellant.

This Notice must be served upon:

Registrar\*  
Ontario Land Tribunal  
655 Bay Street, Suite 1500  
Toronto, Ontario  
M5G 1E5  
OLT.Registrar@ontario.ca

and

The Director appointed for the purposes of  
Part II.1 of the *Environmental Protection Act*  
Ministry of the Environment,  
Conservation and Parks  
135 St. Clair Avenue West, 1st Floor  
Toronto, Ontario  
M4V 1P5

\* Further information on the Ontario Land Tribunal's requirements for an appeal can be obtained directly from the Tribunal at: Tel: (416) 212-6349 or 1 (866) 448-2248, or [www.olt.gov.on.ca](http://www.olt.gov.on.ca)

The above noted activity is approved under s.20.3 of Part II.1 of the *Environmental Protection Act*.

DATED AT TORONTO this 1st day of September, 2022



---

Aziz Ahmed, P.Eng.  
Director  
appointed for the purposes of Part II.1 of the  
*Environmental Protection Act*

RR/

c: District Manager, MECP Ottawa District Office  
Clerk, City of Ottawa (File No. D07-16-20-0021)  
Jeff Shillington, P.Eng., Senior Project Manager, Development Review, City of Ottawa  
Kevin Murphy, David Shaeffer Engineering Ltd.

## **APPENDIX B**

## **WATER SUPPLY**



**Barrhaven Conservancy East  
(Phases 2, 3, 4 & Jock River):  
Water Distribution System Analysis**

Final Report

June 2, 2022

Prepared for:

David Schaeffer Engineering Ltd.

Prepared by:

Stantec Consulting Ltd.

Revision	Description	Author		Quality Check		Independent Review	
0	Final	TAW	20211213	JS	20211214	KA	20211216
1	Final	TAW/AMG	20220512	AMG	20220516	AP	20220518
2	Final	TAW/AMG	20220602	AMG	20220602	AP	20220602



**BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS**

This document entitled **Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River): Water Distribution System Analysis** was prepared by Stantec Consulting Ltd. ("Stantec") for the account of David Schaeffer Engineering Ltd. (the "Client"). Any reliance on this document by any third party is strictly prohibited. The material in it reflects Stantec's professional judgment in light of the scope, schedule and other limitations stated in the document and in the contract between Stantec and the Client. The opinions in the document are based on conditions and information existing at the time the document was published and do not take into account any subsequent changes. In preparing the document, Stantec did not verify information supplied to it by others. Any use which a third party makes of this document is the responsibility of such third party. Such third party agrees that Stantec shall not be responsible for costs or damages of any kind, if any, suffered by it or any other third party as a result of decisions made or actions taken based on this document.

Prepared by \_\_\_\_\_  
(signature)  
**Thomas Westwood, M.Eng., P.Eng.**

Prepared by \_\_\_\_\_  
(signature)  
**Alexandre Mineault-Guitard, M.Sc.A., ing., P.Eng.**

Reviewed by \_\_\_\_\_  
(signature)  
**Alexandre Mineault-Guitard, M.Sc.A., ing., P.Eng.**

Approved by \_\_\_\_\_  
(signature)  
**Ana Paerez, P.Eng.**



# BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

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**BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION  
SYSTEM ANALYSIS**

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## BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

Introduction  
June 2, 2022

# 1.0 INTRODUCTION

To support David Schaeffer Engineering Ltd (DSEL) with their conceptual design submission for the Barrhaven Conservancy East development lands (Phases 2, 3, 4 and Jock River), Stantec Consulting Ltd (Stantec) was requested to provide engineering services to complete a water distribution system analysis for this proposed development located within the City of Ottawa's (City) South Urban Community (SUC). The purpose of the analysis is to confirm associated watermain sizing and redundancy needs.

For this assignment, Stantec's scope of work included the following tasks:

- 1) Reviewing background information and establishing updated water demands for the Conservancy East development area based on the most current draft plan;
- 2) Preparing and submitting a boundary condition request to the City;
- 3) Preparing a stand-alone hydraulic model of the distribution system within the Conservancy East lands using boundary conditions provided by the City. The backbone watermain planning model used for previous planning-level analyses will be used as a base;
- 4) Assessing Fire Underwriters Survey (FUS) fire flow requirements;
- 5) Setting up and running model simulations for average day (AVDY), peak hour (PKHR), and maximum day (MXDY) plus fire flow demands to identify watermain sizing and redundancy needs required for the water distribution system within the development lands to meet design criteria; and,
- 6) Documenting the approach used, findings and recommendations from the analysis.

## 1.1 STUDY AREA

The study area, referred to as the Barrhaven Conservancy East development lands, is located in the City's southwestern suburban neighbourhood of Barrhaven. The lands are situated between Strandherd Dr to the north, the Jock River to the south, Fraser-Clark Drain to the east, and bisected by Borrisokane Rd through the western portion. Based on the current site plan provided by DSEL (dated October 13, 2021) and additional sub-phasing information (dated March 9, 2022), the proposed development is to be subdivided into four (4) phases, which are further described in **Section 1.2**. The proposed development will comprise a total of 782 single family home (SFH) units and 606 townhouse (MLT) units (consisting of a combination of rear-lane, back-to-back and standard townhouse units) for a total estimated population of 4,295 persons.

Based on a previously completed serviceability study for these lands (Stantec Consulting Ltd., 2021), this residential community, which is currently situated adjacent to Pressure Zone 3SW (previously known as



## BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

Introduction  
June 2, 2022

Zone BARR), is ultimately planned to be serviced by the future Zone SUC. In 2015, the City embarked on a large initiative to reconfigure the pressure zones servicing Barrhaven and the southern reaches of Ottawa (i.e., SUC). The City has indicated that the pressure zone reconfiguration is planned to be completed by the second quarter (Q2) of 2024. The purpose of the zone reconfiguration was to improve reliability and efficiencies, and to provide increased pumping capacity for future growth. As such, these development lands are to be serviced by two connections to the existing distribution network, both of which are currently part of Zone 3SW and will ultimately be part of Zone SUC. These include the following locations as shown in **Figure 1-1**:

- 1) The existing 305 mm stub extending from Chapman Mills Dr (east of Kennedy-Burnett Pond); and
- 2) The T-junction on the existing 203 mm watermain at Danson Gardens Grv and Darjeeling Ave.

Both connections would require crossing the Kennedy-Burnett Pond and the Fraser-Clarke Drain.

The City has also suggested that a third connection be considered, which is also illustrated in **Figure 1-1**. This potential third connection is located south of the Jock River, at a future 305 mm stub at the intersection of Flagstaff Dr and Borrisokane Rd, and would require crossing the Jock River to service the proposed development lands. The serviceability of the development lands using this third connection is also analyzed herein.

## 1.2 PHASING OF BARRHAVEN CONSERVANCY EAST

For the purpose of this assessment, development within Barrhaven Conservancy East, as shown in **Figure 1-2**, is assumed to occur in the following phasing order:

- 1) Phase 2 – Comprising 240 SFH units, 98 MLT units and two park areas. The townhouses in this phase are a combination of rear-lane and standard townhouse units. Phase 2 will consist of three (3) subphases:
  - Phase 2A – Comprising 102 SFH units and one park area.
  - Phase 2B – Comprising 129 SFH units.
  - Phase 2C – Comprising 9 SFH units, 98 MLT units and one park area.
- 2) Phase 3 – Comprising 128 SFH units and 197 MLT units. As with Phase 2, these townhouses are a combination of rear-lane and standard townhouse units. Phase 3 will consist of two (2) subphases:
  - Phase 2D – Comprising 42 SFH units and 47 MLT units.
  - Phase 2E – Comprising 86 SFH units and 150 MLT units.



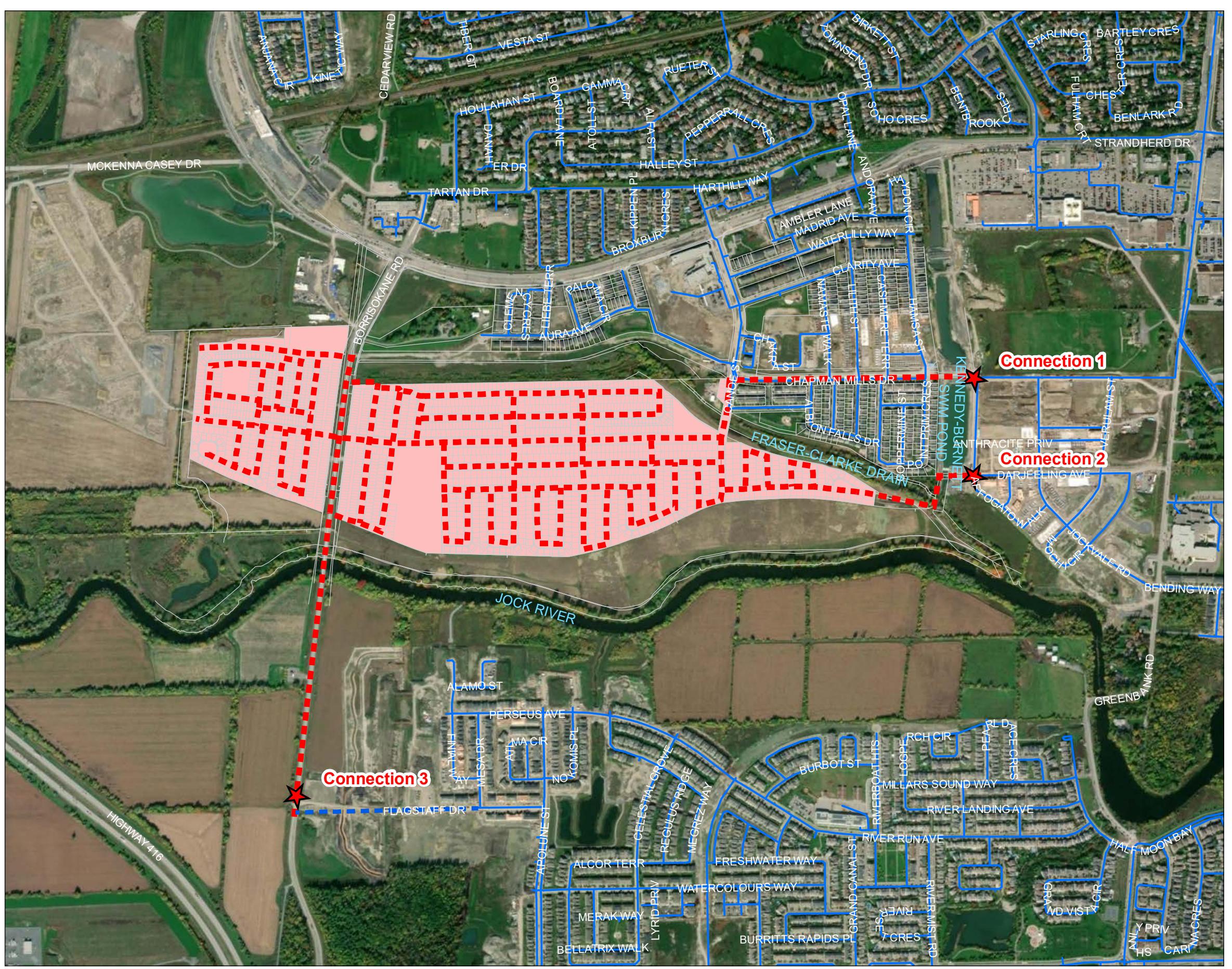
## **BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS**

Introduction  
June 2, 2022

- 3) Phase 4 - Comprising 86 SFH units, 311 MLT units and one park area. As with Phase 2 and 3, the townhouses in this phase are a combination of rear-lane and standard townhouse units, with additional blocks of back-to-back townhouses; and,
- 4) Jock River – Comprising 328 SFH units.

As previously mentioned, the development area will ultimately be serviced by the pressure Zone SUC, once the reconfiguration is complete (planned in Q2 of 2024). As such, the analysis and proposed watermain sizing and layout documented in this report only considers the Zone SUC servicing conditions.





## Legend

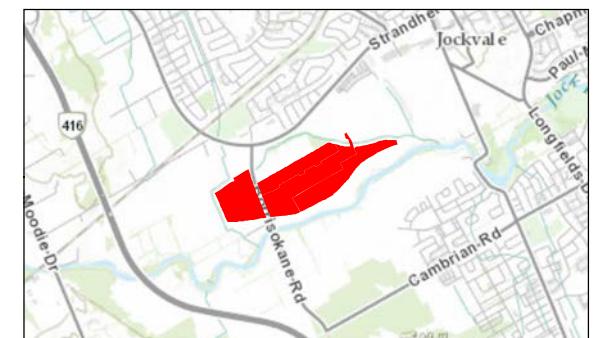
-  Barrhaven Conservancy East Lands
  -  Property Line
  -  Existing Distribution Watermain
  -  Future Distribution Watermain
  -  Connection Location
  -  Future Watermain to Service Barrhaven Conservancy East Lands

180 360 metres  
(At original document size of 11x17)  
11x17

(At original document size of 11x17)  
1:10,000

**Notes**

1. Coordinate System: NAD 1983 CSRS MTM 9
2. Background: Source: Esri, Maxar, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, AerialGRID, IGN, and the GIS User Community  
Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCan, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community



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*Project Location*

Client/Project  
David Schaeffer Engineering Ltd  
Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River)  
Water Distribution System Analysis

Water Dist.

1-1

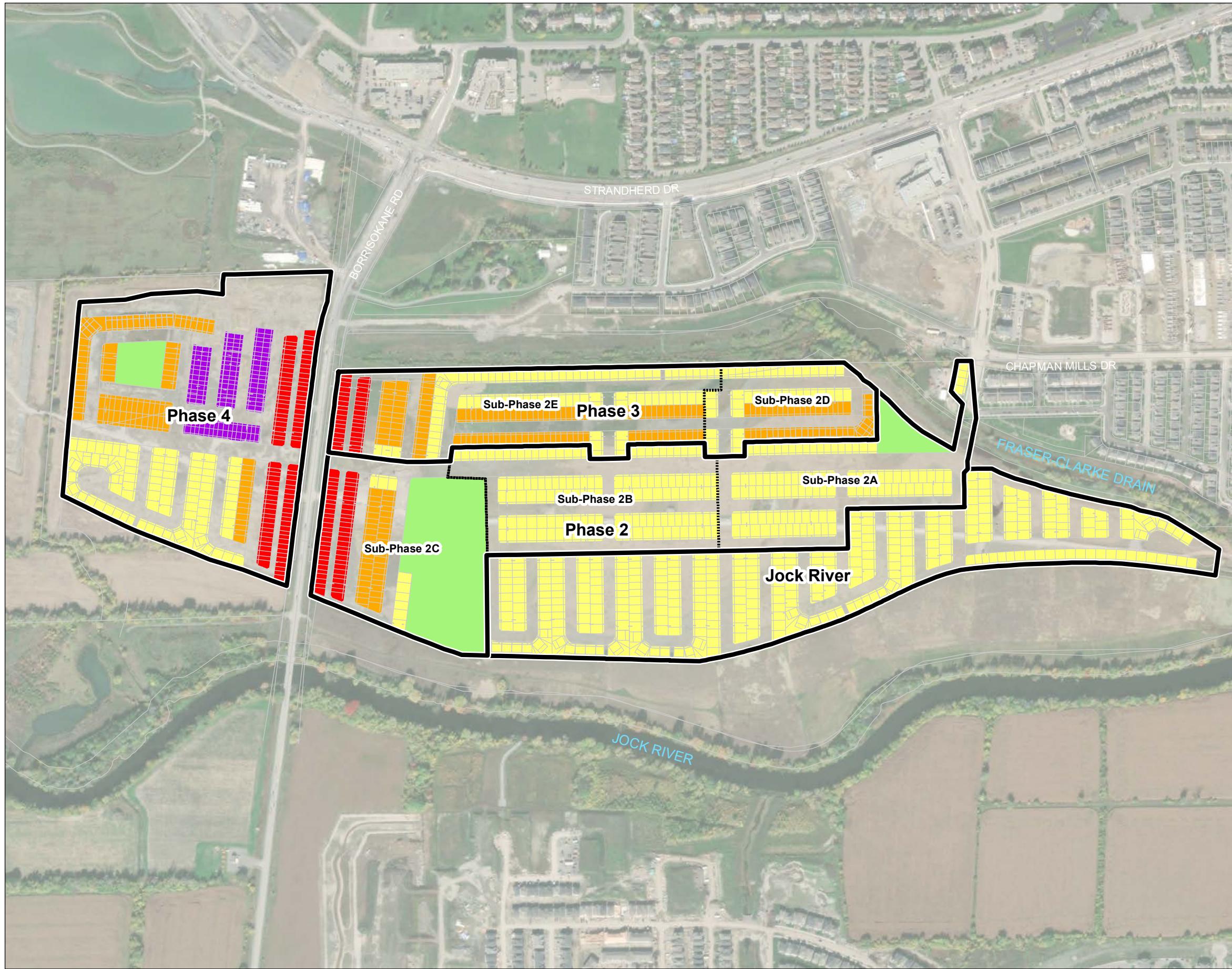
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**Title**

## Connections to Existing Water Distribution Network

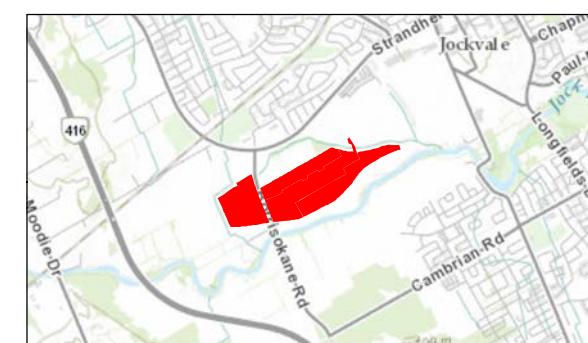
**Legend**

- Development Phase Boundary
- Development Sub-Phase Boundary
- Single Family Home (SFH)
- Standard Townhouse (STND TH)
- Rear-Lane Townhouse (RLTH)
- Back-to-Back Townhouse (B2B)
- Park
- Property Line



**Notes**

1. Coordinate System: NAD 1983 CSRS MTM 9
2. Background: Source: Esri, Maxar, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, AeroGRID, IGN, and the GIS User Community
- Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCan, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community



**Project Location**  
Ottawa, ON

**Client/Project**  
David Schaeffer Engineering Ltd  
Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River)  
Water Distribution System Analysis

**Figure No.**  
**1-2**

**Title**  
**Phasing Plan of Barrhaven Conservancy East**

## BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

Hydraulic Assessment  
June 2, 2022

## 2.0 HYDRAULIC ASSESSMENT

The City of Ottawa Water Design Guidelines (City of Ottawa, 2010) and criteria outlined in the 2013 Water Master Plan (WMP) were used to establish water demands, level of service and pressure objectives during normal and emergency conditions. As per the City's design guidelines and recently issued Technical Bulletin ISTB-2021-03, since this is a new development involving the design of new watermains, the design shall consider a required fire flow established using the calculation method published by the Fire Underwriters Survey (FUS).

### 2.1 SERVICEABILITY

#### 2.1.1 System Pressures

As per the City's Water Design Guidelines, the desired range of pressure under average day (AVDY), maximum day (MXDY) and peak hour (PKHR) demands is 345 to 552 kPa (50 to 80 psi) and no less than 276 kPa (40 psi) at ground elevation (i.e., at street level). The maximum pressure at any point in the water distribution system should not exceed 552 kPa (80 psi); pressure reducing measures are required to service areas where pressures greater than 552 kPa (80 psi) are anticipated.

Under emergency fire conditions, the system must be able to supply appropriate fire flow while maintaining a residual pressure of 138 kPa (20 psi).

**Figure 2-1** shows the elevations of each model junction based on the site's current grading plan. These range from 92.4 m to 93.5 m.

#### 2.1.2 Fire Flows

The City requires a fire flow assessment to be completed to demonstrate that local watermains can provide the objective fire flows. The detailed FUS Guidelines (long method; 1999 Version) was used to calculate the objective fire flows. Based on site plan information provided, the following characteristics were considered in the FUS calculations:

- All townhouse units will be of typical construction (e.g., wood frame, limited combustible building contents); firewalls are to be added where required to meet the study area's target fire flow;
- Single family home units will generally be of typical (wood frame) construction except where a break in fire area is required to meet the study area's target fire flow. At such locations, units will be of ordinary construction as described in the FUS guidelines.
  - With side yard separation distances of < 3.0 m between SFH units, the current site layout would contain several large blocks of contiguous SFH units if all were to be of wood frame construction. It is our understanding that the current rearyard setback for all SFH



## **BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS**

Hydraulic Assessment  
June 2, 2022

products will be 4.5 m, which in most locations throughout the development area results in rear yard separation distances of less than 10 m. As such, the City's cap of 10,000 L/min, as per Technical Bulletin ISDTB-2018-02, does not apply to these areas and measures such as separating fire areas with units of ordinary construction is required to meet the study area's target fire flow;

- All buildings will have 2 stories above grade (with basements more than 50% below ground level);
- Buildings are not sprinklered; and,
- Setbacks between adjacent units are greater than 3.0 m, with the exception of some proposed SFH units.
  - Per the FUS Guidelines, units with setbacks less than 3.0 m and of wood frame construction will be considered a single fire area.

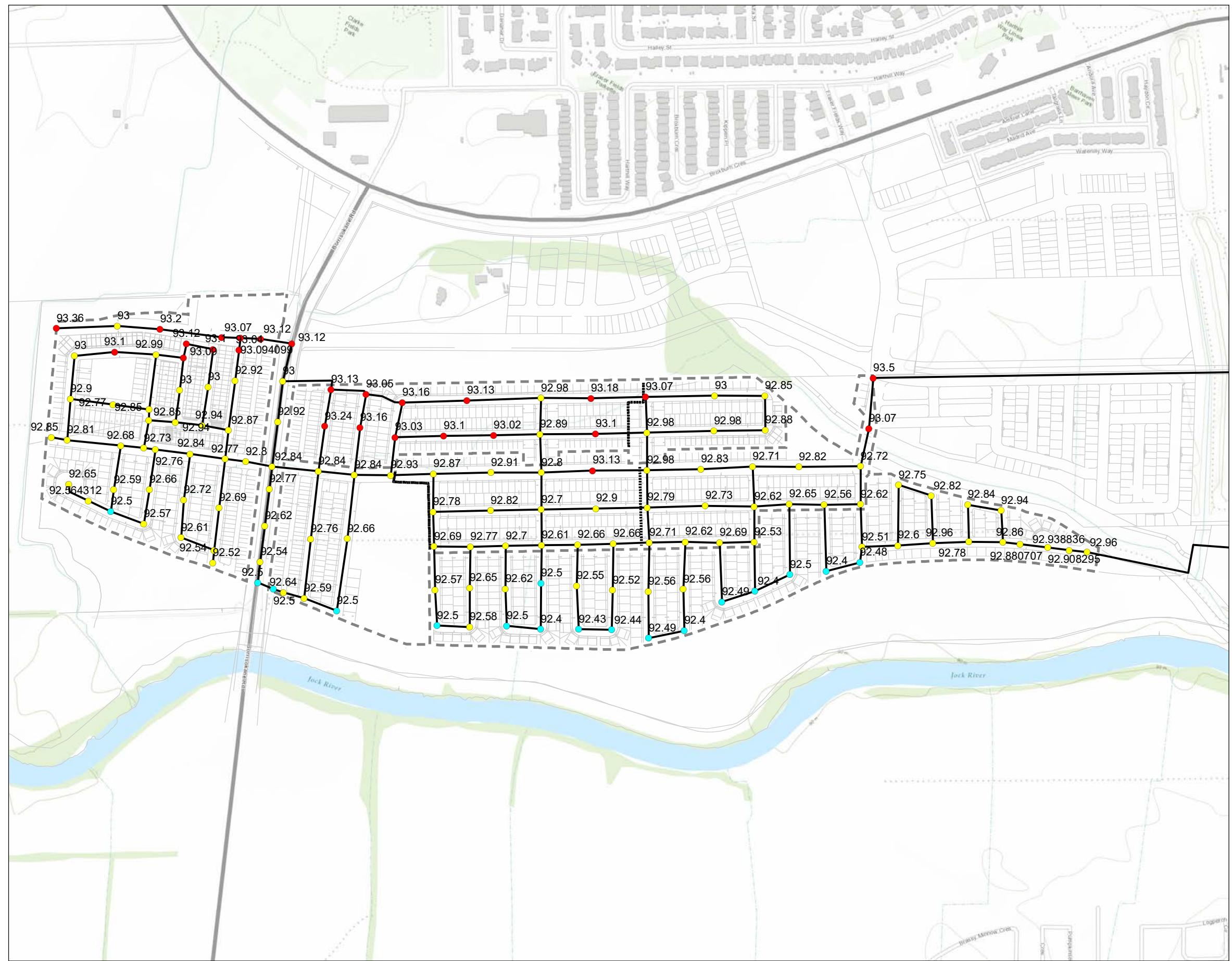
Based on the latest site plan dated October 2021 and subsequent architectural changes, the required fire flow (RFF) for the governing unit design (rear-lane townhouses, RLTH) was calculated to be 13,000 L/min (217 L/s). This is based on the understanding that, as previously noted, ordinary construction SFH units will be used to separate SFH blocks into fire areas that result in RFFs no greater than 13,000 L/min. Similarly, townhouse blocks will also have firewalls to limit fire areas such that the resulting RFFs will be no greater than 13,000 L/min. The local water mains must therefore be able to provide a minimum fire flow of 13,000 L/min at a residual pressure of 20 psi. The FUS fire flow calculations for the governing unit design and to meet the target fire flow are provided in **Appendix A**.

### **2.1.3 Water Age**

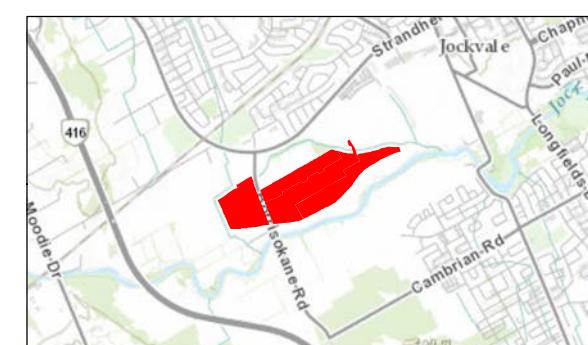
As per the City of Ottawa Design Guidelines, water mains should not be oversized as this may pose water quality degradation, assessed in terms of water age. The Design Guidelines recommend the following:

- A total travel time of 5 days or less during average day demand; and
- A maximum residence time of 8 days.





0 120 240 metres  
 (At original document size of 11x17)  
 1:6,500



**Project Location**  
Ottawa, ON

**Client/Project**  
David Schaeffer Engineering Ltd  
Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River)  
Water Distribution System Analysis

**Figure No.**

**2-1**

**Title**  
**Junction Elevations**

# BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

Hydraulic Assessment  
June 2, 2022

## 2.2 GROWTH PROJECTIONS

The estimated residential population for Barrhaven Conservancy East was estimated based on projected household sizes as per population densities (or persons per unit, PPU) specified in the City's Water Design Guidelines.

**Table 2-1** shows the estimated number of units per phase of these development lands and the projected populations based on the distribution of residential types. The total number of units is estimated to be 1,388 with a residential population of 4,295 persons.

**Table 2-1: Estimated Unit Counts and Populations for Barrhaven Conservancy East**

Phase	Sub Phase	Unit Types	Units	PPU	Population	
2	2A	Singles	102	3.4	347	
		Towns	0	2.7	0	
	2B	Singles	129	3.4	439	
		Towns	0	2.7	0	
	2C	Singles	9	3.4	31	
		Towns	98	2.7	265	
<i>Phase 2 Sub-total</i>			338	-	1,081	
3	2D	Singles	42	3.4	143	
		Towns	47	2.7	127	
	2E	Singles	86	3.4	292	
		Towns	150	2.7	405	
	<i>Phase 3 Sub-total</i>			325	-	967
	4	Singles	86	3.4	292	
		Towns	311	2.7	840	
		<i>Phase 4 Sub-total</i>		397	-	1,132
Jock River (JR)		Singles	328	3.4	1,115	
		Towns	0	2.7	0	
	<i>JR Phase Sub-total</i>		328	-	1,115	
<i>Total</i>			<b>1,388</b>		<b>4,295</b>	

# BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

Hydraulic Assessment  
June 2, 2022

## 2.3 DEMAND PROJECTIONS

Due to the size of the service area, the criteria outlined in the City's Water Design Guidelines and recently issued Technical Bulletin ISTB-2021-03 were followed to establish water demands in Barrhaven Conservancy East. As the buildout population of the proposed development is 4,925 (i.e., greater than 3,000), the City's Water Design Guidelines refer to the MECP Guidelines for consumption rates. The MECP Guidelines provide a consumption rate range of 270 L/cap/day to 450 L/cap/day. The City's Water Design Guidelines consumption rates for subdivisions of 501 to 3,000 persons fall within that range and are therefore applicable. The demand rates and peaking factors from the Water Design Guidelines and Technical Bulletin ISTB-2021-03 were applied to the population projections presented in **Table 2-1** based on land-use.

For residential land-use, SFH and MLT units were assigned an average day (AVDY) consumption rate of 280 L/cap/d. To determine maximum day (MXDY) demands, the AVDY demands were multiplied by a residential peaking factor of 2.5. Peak hour (PKHR) demands were established by multiplying MXDY demands by a residential peaking factor of 2.2. The projected AVDY, MXDY and PKHR demands were distributed to the model nodes by phase (and sub-phase) for the corresponding demand scenario.

Estimated AVDY, MXDY and PKHR demand projections are summarized in **Table 2-2**.

**Table 2-2: Estimated Demand Projections for Barrhaven Conservancy East**

Phase	Sub-Phase	Unit Types	AVDY (L/s)	MXDY (L/s)	PKHR (L/s)
2	2A	Singles	1.12	2.81	6.18
		Towns	0	0	0
	2B	Singles	1.42	3.55	7.82
		Towns	0	0	0
	2C	Singles	0.10	0.25	0.55
		Towns	0.86	2.14	4.72
			<b>Phase 2 Sub-total</b>	<b>3.50</b>	<b>8.75</b>
3	2D	Singles	0.46	1.16	2.55
		Towns	0.41	1.03	2.26
	2E	Singles	0.95	2.37	5.21
		Towns	1.31	3.28	7.22
				<b>Phase 3 Sub-total</b>	<b>3.13</b>
4		Singles	0.95	2.37	5.21
		Towns	2.72	6.80	14.97
				<b>Phase 4 Sub-total</b>	<b>3.67</b>
				<b>9.17</b>	<b>20.18</b>
Jock River (JR)		Singles	3.61	9.04	19.88
		Towns	0	0	0
				<b>JR Phase Sub-total</b>	<b>3.61</b>
			<b>Total</b>	<b>13.92</b>	<b>34.80</b>
					<b>76.55</b>

# BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

Hydraulic Assessment  
June 2, 2022

## 2.4 MODEL DEVELOPMENT

Innovyze's InfoWater (Suite 12.4, Update #9) was used to create a stand-alone hydraulic model of the water distribution system within the proposed development area for this analysis. The model was developed to reflect the most current site plan, including proposed watermain layout (based on proposed road alignment) and water demands.

Watermains added to the model were assigned Hazen-Williams coefficients ("C-Factors") in accordance with the City's Water Design Guidelines. These factors are listed in **Table 2-3**.

**Table 2-3: Hazen-Williams Coefficients by Watermain Size**

Watermain Diameter (mm)	Coefficient
152	100
203 - 305	110
350 - 600	120
> 600	130

### 2.4.1 Boundary Conditions

The proposed subdivision has two connection points to the existing water distribution system; the option to add a third connection point is also assessed (see **Section 1.1**). The boundary conditions provided by the City include hydraulic gradeline (HGL) values for Zone SUC servicing conditions. Values are provided in **Appendix B** and summarized in **Table 2-4**, and have been simulated in the hydraulic model using fixed head reservoirs to which HGLs have been applied for the respective demand scenarios.

Differences in HGL between connections 1 and 2 are observed under higher demand scenarios. While under AVDY and PKHR conditions, these differences are small (0.2 m or less), under MXDY+FF and AVDY+FF conditions, these differences increase to approximately 4 m. This is likely due to the fact that the Connection 1 is connected to a 305 mm diameter along Chapman Mills Dr, whereas Connection 2 is to a 203 mm diameter along Darjeeling Ave, and the two connection points are interconnected by a 203 mm diameter watermain along Danson Gardens Grv.

If the existing watermain along Danson Gardens Grv is upgraded to a 305 mm diameter watermain, the discrepancies in HGL between Connection 1 and Connection 2 decrease. A second set of boundary conditions (two connections with upgrades) reflecting these conditions was provided by the City.

Finally, a third set of boundary conditions was provided by the City, reflecting conditions with three connection points to the existing water distribution system. These boundary conditions do not consider any upgrades between Connection 1 and Connection 2, and as such the HGLs differ by 3.5 to 3.7 m under MXDY+FF and AVDY+FF conditions.



**BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS**

Hydraulic Assessment  
June 2, 2022

**Table 2-4: HGL Boundary Conditions**

HGL (m) Zone SUC Servicing Conditions		
Demand Scenario	Two Connections <sup>(5)</sup>	
	Connection 1 <sup>(1)</sup>	Connection 2 <sup>(2)</sup>
AVDY	150.0	150.0
PKHR	144.2	144.0
AVDY +FF	138.7	135.1
MXDY+FF	137.0	133.2
Demand Scenario	Two Connections with Upgrades <sup>(4)</sup>	
	Connection 1 <sup>(1)</sup>	Connection 2 <sup>(2)</sup>
AVDY	149.5	149.5
PKHR	144.1	144.1
AVDY +FF	138.6	139.8
MXDY+FF	136.8	138.1
Demand Scenario	Three Connections <sup>(5)</sup>	
	Connection 1 <sup>(1)</sup>	Connection 2 <sup>(2)</sup>
AVDY	149.5	149.5
PKHR	144.5	144.4
AVDY +FF	138.6	135.1
MXDY+FF	137.1	133.4

Notes:

- (1) Ground elevation @ Connection 1 (Chapman Mills Dr) = 92.8 m.
- (2) Ground elevation @ Connection 2 (Danson Gardens Grv / Darjeeling Ave) = 91.8 m.
- (3) Ground elevation @ Connection 3 (Flagstaff Dr) = 92.1 m.
- (4) Upgrades to existing water distribution required to increase HGL at Connection 2; upsize existing 203 mm diameter watermain on Danson Gardens Grv to a 305 mm diameter watermain.
- (5) For scenarios where ultimate conditions will include three connections, the boundary conditions for two connections (without upgrades) were used when only Connections 1 and 2 are in place, i.e., for modelling Phases 2 and 3.



## BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

Hydraulic Assessment  
June 2, 2022

### 2.4.2 Proposed Watermain Sizing & Layout

Two layouts and sizing of the watermains within the proposed development are presented. The first layout (Option A) is required to service the development if only two connections to the water distribution system (Connection 1 and Connection 2) are made. The second layout (Option B) is required to service the development if a third connection (south of the Jock River) is introduced.

#### 2.4.2.1 Option A: Watermain Sizing & Layout for Two Connections

The layout and sizing of the watermains within the proposed development for a scenario with two ultimate connections to the water distribution system are shown in **Figure 2-2**. The same layout and sizing are required with upgrades to the water distribution system along Danson Gardens Grv.

The network is proposed to consist of 152 mm, 203 mm, 305 mm, and 406 mm diameter watermains, with the 305 mm and 406 mm watermains acting as the hydraulic backbone throughout the development lands. The 406 mm diameter watermains run west from connections 1 and 2, interconnect at the east side of the development lands and continue westward across Borrisokane Rd into the Phase 4 lands. The 406 mm diameter watermains can thus serve as backbone if future developments extend further westward. Additional backbone loops added for reliability will be 305 mm watermains. The remaining local watermains will be 152 mm and 203 mm diameter watermains.

The dead-end watermain in the Phase 4 cul-de-sac is proposed to be 203 mm stepping down to 152 mm. Using the traditional “point load assumption” modelling approach to sizing new watermains, the resulting diameter that would be required to provide a fire flow of 13,000 L/min would be larger than the maximum of 152 mm specified in the City’s design guidelines for dead-end watermains. As such, to optimize sizing of this watermain, the alternative procedure outlined in Appendix I (Guidelines on Coordination of Hydrant Placement with Required Fire Flow) of the City’s Technical Bulletin ISDTB-2018-02 was employed. Additional nodes were added to the model network to represent hydrant locations, to which hydrant flows from Table 1 of Appendix I were applied. To achieve a fire flow of 13,000 L/min, two Class AA hydrants within 75 m (each with an assumed maximum flow capacity of 5,700 L/min) and an additional Class AA hydrant between 75 m and 150 m (with an assumed maximum flow capacity of 3,800 L/min) of the furthest unit along the cul-de-sac would provide a total fire flow of 15,200 L/min (i.e., > the RFF of 13,000 L/min). Other hydrant spacing combinations in accordance with the City’s Technical Bulletin ISDTB-2018-02 can also achieve a total fire flow greater than the RFF of 13,000 L/min.

For reliability, the second backbone feed (305 mm) is redirected north then west (i.e., north of the standard and rear-lane townhouse blocks) across to the Phase 4 lands. This alignment provides reliability of service to the lands west of Borrisokane Rd in the event of a failure at the current intersection of the backbone feeds situated within the Borrisokane Rd ROW. System reliability is further discussed in **Section 3.3**. West of Borrisokane Rd, the 305 mm section of backbone will serve as a service connection to future adjacent development. There are no direct Phase 4 property service connections anticipated



## **BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS**

Hydraulic Assessment  
June 2, 2022

along this temporary dead-end section of watermain; therefore, it is recommended that this section be isolated until it is required to provide flow to adjacent future lands.

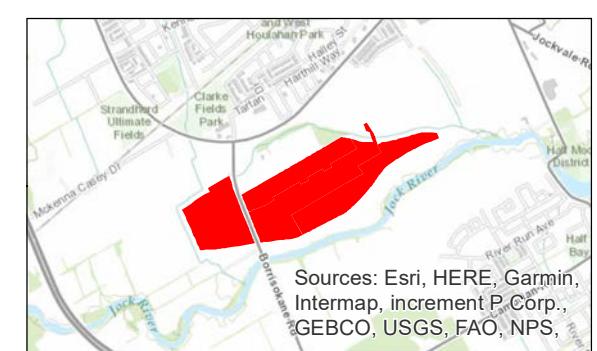
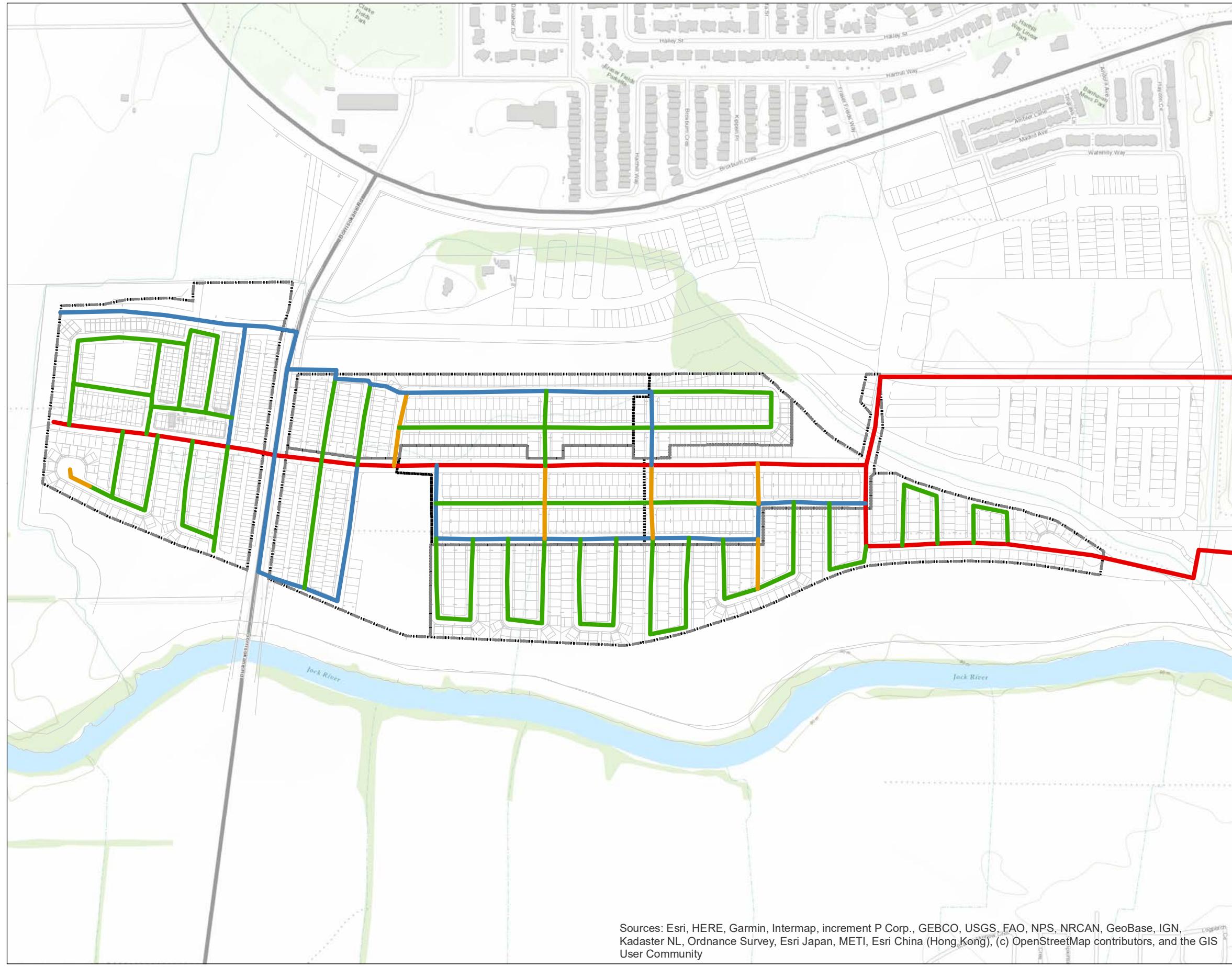
### **2.4.2.2 Option B: Watermain Sizing & Layout for Three Connections**

The layout and sizing of the watermains within the proposed development for a scenario with three ultimate connections to the water distribution system are shown in **Figure 2-3**.

The layout of the watermains is the same as in Option A (with two connections). However, with the third connection, the entire backbone can be reduced to 305 mm diameter watermains at all three connection points and throughout the development lands. The remaining watermain sizes are unchanged from Option A, with local watermains of 152 mm and 203 mm diameter watermains.

Based on the proposed phasing, the implementation of the third connection could be delayed until the development of the Phase 4 lands, west of Borrisokane Rd.



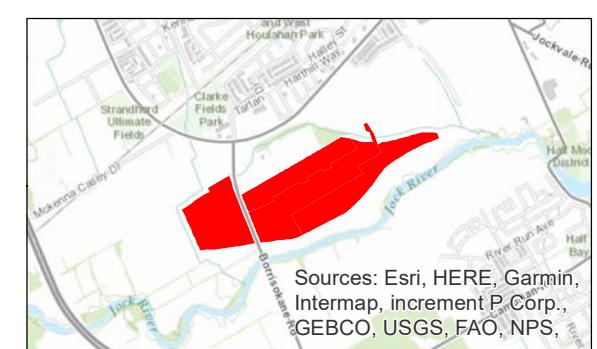
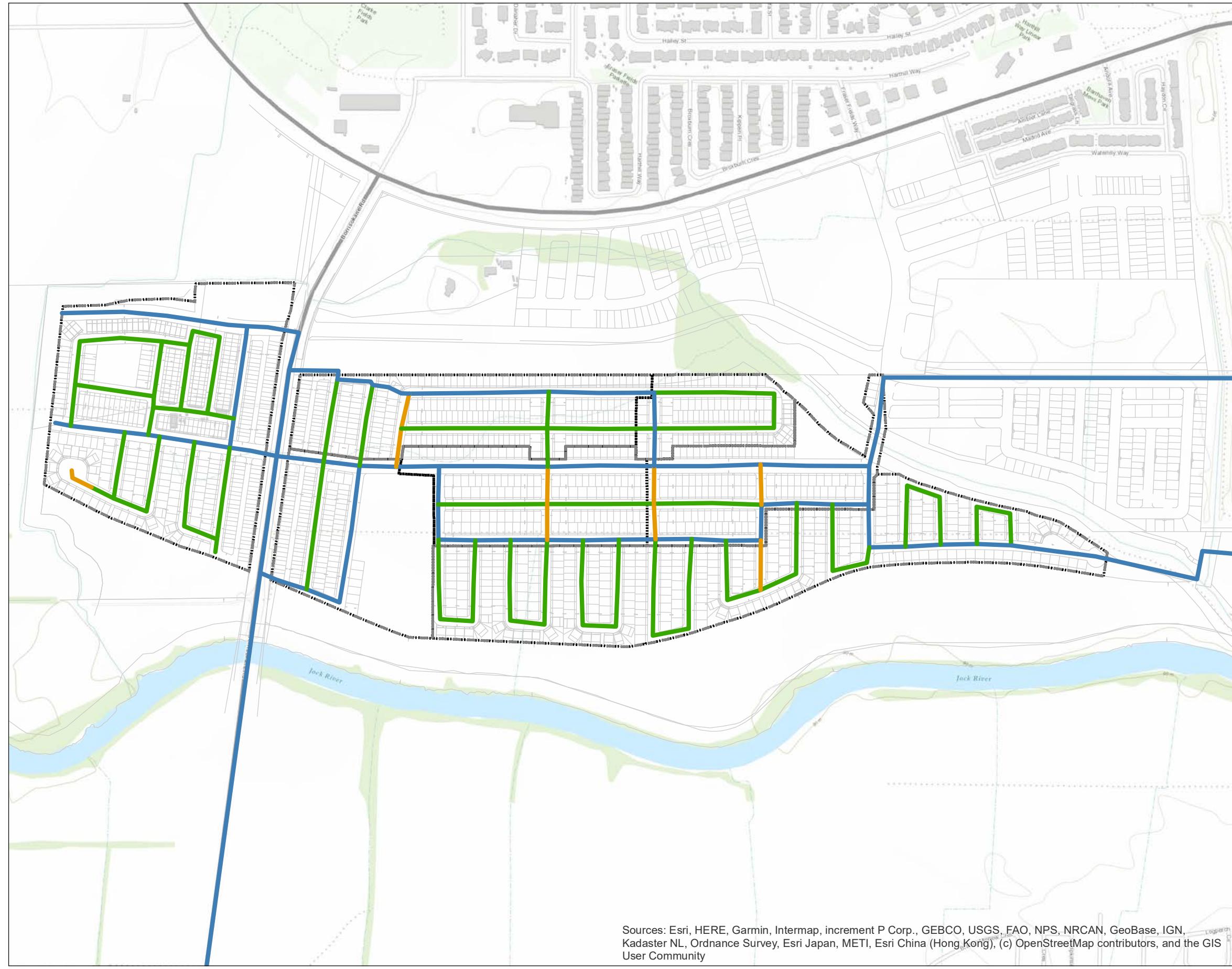


**Project Location**  
 Ottawa, ON

**Client/Project**  
 David Schaeffer Engineering Ltd  
 Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River)  
 Water Distribution System Analysis

**Figure No.**  
 2-2

**Title**  
**Proposed Watermain Sizing and Layout - Option A**



**Project Location**  
Ottawa, ON

**Client/Project**  
David Schaeffer Engineering Ltd  
Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River)  
Water Distribution System Analysis

**Figure No.**  
**2-3**

**Title**  
**Proposed Watermain Sizing and Layout - Option B**

## BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

Hydraulic Modelling Results  
June 2, 2022

### 3.0 HYDRAULIC MODELLING RESULTS

Hydraulic modelling was completed for interim phasing conditions and ultimate buildout conditions of the development lands, under SUC servicing conditions, to verify how the network would respond. The following sub-sections present the modelling results under AVDY, PKHR, and MXDY+FF demands, plus under emergency conditions in the event of a watermain break at key points within the proposed network. Detailed modelling results for all scenarios are provided in **Appendix D**.

#### 3.1 AVERAGE DAY & PEAK HOUR DEMANDS

Under AVDY demands with two connections to the water distribution system, maximum modelled pressures for each interim phase and buildout conditions are 82 psi. With three connections to the water distribution system, maximum modelled pressures for each interim phase and buildout conditions are 81 to 82 psi. These maximum pressures exceed the City's maximum pressure objective of 80 psi. As per the Ontario Building Code (OBC) in areas that may be occupied, the static pressure at any fixture shall not exceed 80 psi. Where pressures do exceed 80 psi, pressure control measures such as pressure reducing valves (PRVs) shall be considered.

Under PKHR demands with two connections to the water distribution system, minimum modelled pressures for each interim phase and buildout conditions are 72 psi. With three connections to the water distribution system, minimum modelled pressures for each interim phase and buildout conditions are also 72 psi. These pressures fall within the desired pressure range of 50 to 80 psi.

#### 3.2 MAXIMUM DAY PLUS FIRE FLOW

MXDY+FF demands were applied for the two connections and the three connections scenarios. Each phase was included sequentially to verify network response as the development phases are constructed and occupied.

With two connections to the water distribution system, available fire flow throughout each interim phase and buildout conditions were above the required 13,000 L/min throughout the network. Likewise, with three connections to the water distribution system, available fire flow throughout each interim phase and buildout conditions were above the required 13,000 L/min throughout the network. To optimize the sizing of the dead-end watermain in the Phase 4 cul-de-sac and to reduce potential water quality issues associated with a large-diameter dead-end watermain, the alternative procedure outlined in Appendix I of ISDTB-2018-02 was employed, as described in **Section 2.4.2**. As such, placing two Class AA hydrants within 75 m of the furthest unit along the cul-de-sac (each with an assumed maximum flow capacity of 5,700 L/min), and two Class AA hydrants between 75 m and 150 m (each with an assumed maximum flow capacity of 3,800 L/min), satisfies the fire flow requirement of 13,000 L/min for units along this cul-de-



## BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

Hydraulic Modelling Results  
June 2, 2022

sac. Other hydrant spacing combinations in accordance with the City's Technical Bulletin ISDTB-2018-02 may be implemented to achieve a total fire flow greater than the RFF of 13,000 L/min.

These results show that the proposed watermain sizing and layout meet serviceability requirements with two connections to the water distribution system without requiring further upstream upgrades along Danson Gardens Grv. Nonetheless, these upgrades would still be beneficial, as they would provide consistent HGLs between the two connection points.

### 3.3 RELIABILITY

As per the City of Ottawa Design Guidelines, the system must be able to provide average day demand plus fire flow (AVDY+FF) while meeting serviceability requirements during a major failure (i.e., watermain break). To assess reliability and resiliency against major failures, a number of reliability scenarios were completed to confirm sufficient pressure and flow can be achieved during a major failure. These scenarios included the following and are shown in **Figure 3-1** (for Option A, with two connections) and in **Figure 3-2: Reliability Analysis Watermain Break Locations – Option B**

(for Option B, with three connections):

- 1) **Break Scenario 1** – Break in the backbone watermain from Connection 1;
- 2) **Break Scenario 2** – Break in the backbone watermain from Connection 2;
- 3) **Break Scenario 3** – Break in backbone watermain at the northwest edge of the large Phase 2 (Phase 2C) park;
- 4) **Break Scenario 4** – Break along the east-west backbone watermain, immediately west of Borrisokane Rd;
- 5) **Break Scenario 5** – Break in the south backbone watermain through Phase 2 lands, immediately east of Borrisokane Rd;
- 6) **Break Scenario 6** – Break in the north backbone watermain through Phase 2 lands, immediately west of Borrisokane Rd; and,
- 7) **Break Scenario 7** (for Option B only) – Break in the backbone watermain from Connection 3 (crossing the Jock River).

Under break scenario 1, all junctions meet their respective required fire flows, both for Option A (with two connections) and Option B (with three connections).

Under break scenario 2, all junctions meet their respective required fire flows, both for Option A (with two connections) and Option B (with three connections).



## BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

Hydraulic Modelling Results  
June 2, 2022

Under break scenario 3, all junctions meet their respective required fire flows, both for Option A (with two connections) and Option B (with three connections). However, under the current phasing plan, a second feed would still be required to service the Phase 2 service area west of the park area (sub-phase 2C; containing more than 50 properties) in the interim until sufficient looping can be provided through the subsequent Phase 3 (sub-phase 2E) if current phasing plans remain unchanged. It is thus recommended that sub-phase 2C be developed after sub-phase 2E, to provide sufficient looping. However, some alternatives could be considered to proceed with sub-phase 2C in accordance with the City's Design Guidelines. First, if the construction of the rear-lane townhouse units (refer to **Figure 1-2**) under sub-phase 2C are delayed until sufficient looping is provided, 55 units will remain as part of sub-phase 2C. As per the City's Design Guidelines, up to 75 units can be serviced on a temporary basis by a dead-end water (or a single feed in this case), given that all pressure and demand objectives are met, and it will be looped by a future phase within 2 years. As such, the 55 units could be serviced from the single feed, given that a second loop is provided in a timely matter (2 years). Alternatively, delaying the construction of 6 other units, in addition to the rear-lane townhouses, to avoid the creation of a vulnerable service area (i.e., less than 50 units under sub-phase 2C until sufficient looping is provided) could be considered.

Under break scenario 4, all junctions meet their respective required fire flows, both for Option A (with two connections) and Option B (with three connections).

Under break scenario 5, all junctions meet their respective required fire flows, both for Option A (with two connections) and Option B (with three connections).

Under break scenario 6, all junctions meet their respective required fire flows, both for Option A (with two connections) and Option B (with three connections).

Under break scenario 7, all junctions meet their respective required fire flows. This break scenario would only occur if Option B (watermain layout with third connection across the Jock River) is selected.

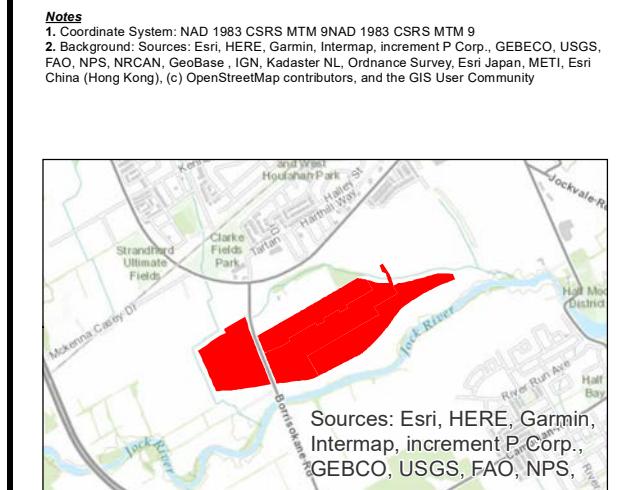
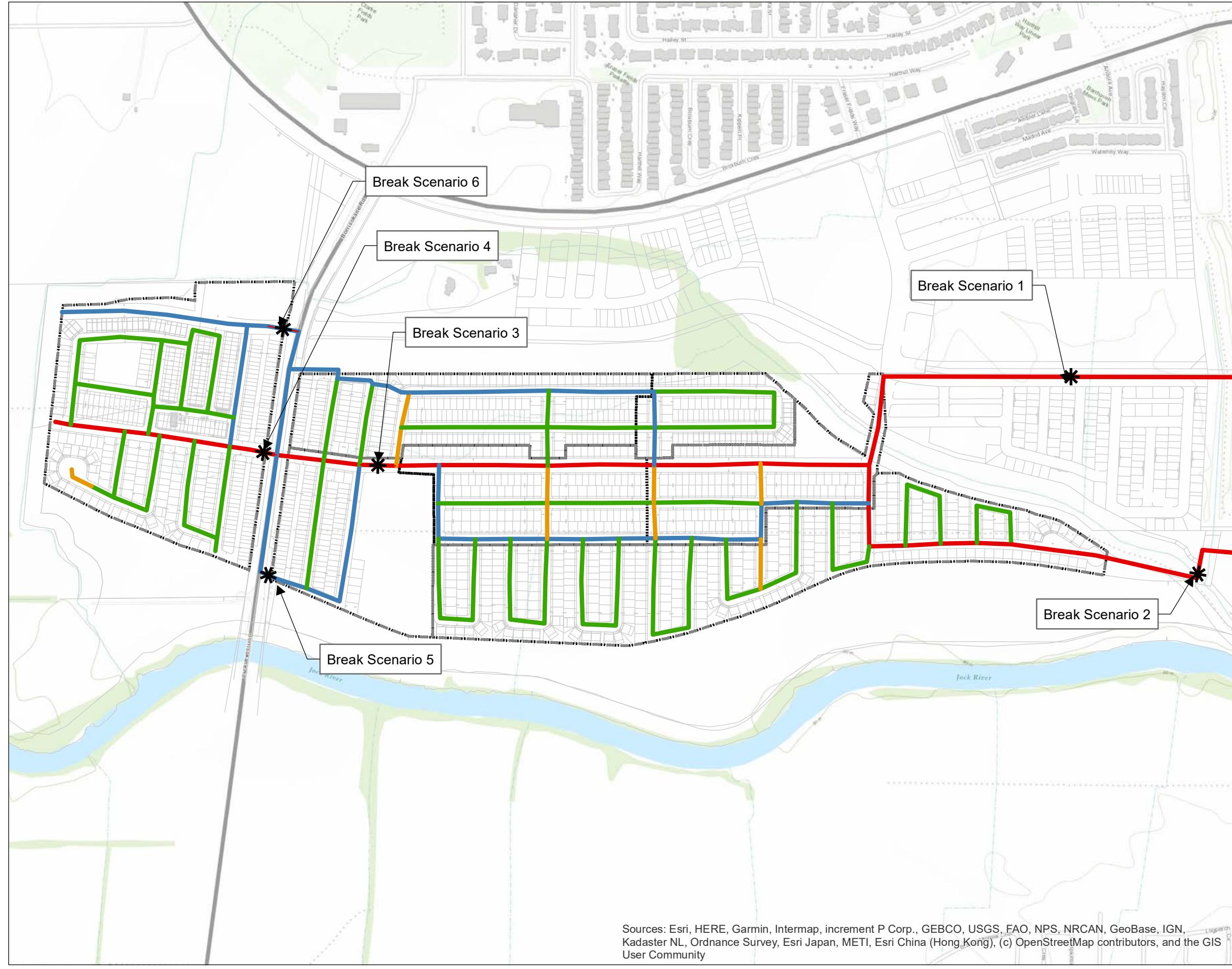
### 3.4 WATER AGE

Water age is calculated as the total pipe volume divided by the AVDY demand. For sizing Option A (with two connections), water age is highest (1.56 days) when Phase 2 is built. The water age upon buildout is 0.67 days. For sizing Option B (with three connections), water age is highest (1.05 days) when Phase 2 is built. The water age upon buildout is 0.57 days.

It should be noted that no water age boundary conditions at the connection points were available, therefore the total water age from the source or last point of rechlorination cannot be assessed. Nonetheless, this analysis shows that the residence time of water within the development lands does not exceed the limits per the City's Design Guidelines, and as such water age issues within the development are not anticipated.

Detailed calculations are provided in **Appendix E**.



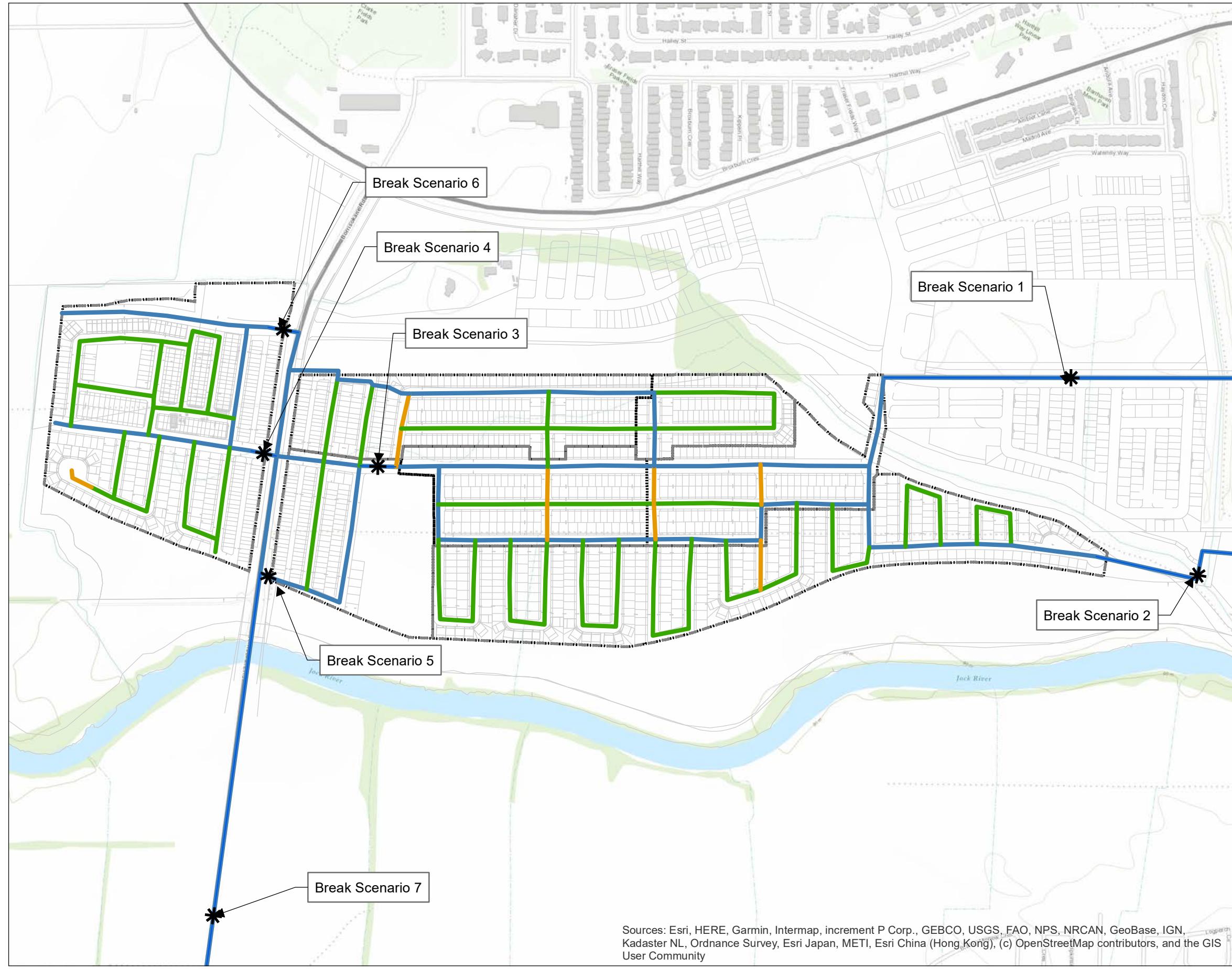


**Project Location**  
Ottawa, ON

**Client/Project**  
David Schaeffer Engineering Ltd  
Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River)  
Water Distribution System Analysis

**Figure No.**  
**3-1**

**Title**  
**Reliability Analysis Watermain Break Locations - Option A**



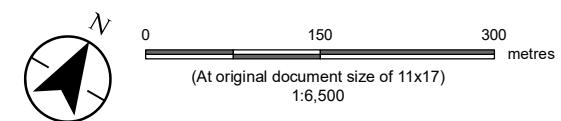
**Legend**

- Development Phase Boundary
- Development Sub-Phase Boundary
- Property Line

**Proposed Watermain Diameter (mm)**

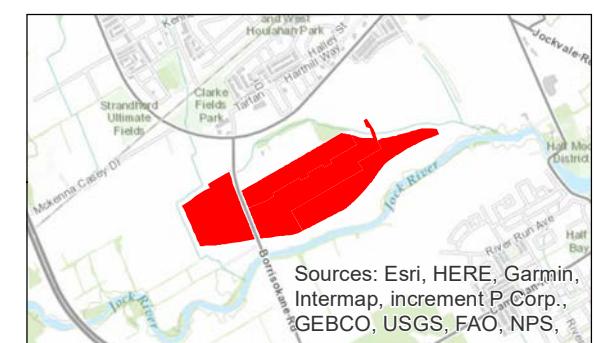
- 152
- 203
- 305

\* Watermain Break Locations



**Notes**

- Coordinate System: NAD 1983 CSRS MTM 9NAD 1983 CSRS MTM 9
- Background: Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community



**Project Location**  
Ottawa, ON

**Client/Project**  
David Schaeffer Engineering Ltd  
Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River)  
Water Distribution System Analysis

**Figure No.**  
**3-2**

**Title**  
**Reliability Analysis Watermain Break Locations - Option B**

## BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

Conclusion and Recommendations  
June 2, 2022

## 4.0 CONCLUSION AND RECOMMENDATIONS

A water distribution system hydraulic analysis was completed for the Barrhaven Conservancy East development lands. The purpose of this analysis was to confirm associated watermain sizing and redundancy needs. Based on the hydraulic analysis, the following conclusions and recommendations were made:

- Based on the most current site plan layout, the estimated AVDY, MXDY and PKHR demand projections for the development lands are 13.92 L/s, 34.80 L/s, and 76.55 L/s, respectively.
- The required fire flow for the governing unit design (rear-lane townhouses) was calculated to be 13,000 L/min (217 L/s). This is based on the understanding that ordinary construction single-family housing (SFH) units will be used to separate SFH blocks into fire areas that result in required fire flows (RFFs) no greater than 13,000 L/min. Similarly, townhouse blocks will have firewalls to limit fire areas such that the resulting RFFs will be no greater than 13,000 L/min.
  - As the watermain sizing presented herein is based on an RFF of 13,000 L/min, the final design of the units should meet the requirements for this RFF, per the FUS Guidelines.
- Two watermain layout and sizing are proposed:
  - The first option (Option A) would involve two connections to the water distribution system; the proposed sizing is recommended to include 406 mm diameter watermains from connections 1 and 2 as the hydraulic backbone of the network, with 305 mm diameter watermains for backbone looping. Watermains along local right-of-ways would be 152 mm and 203 mm diameter watermains. The dead-end watermain in the cul-de-sac at the western extent of the development would be 152 mm diameter. The proposed layout and sizing is shown in **Figure 2-2**.
  - The second option (Option B) would involve three connections to the water distribution system, with the third connection requiring crossing the Jock River. The proposed layout within the development is similar to Option A; the proposed sizing is recommended to include 305 mm diameter watermains for the hydraulic backbone of the network. Watermains along local right-of-ways would be 152 mm and 203 mm diameter watermains. The dead-end watermain in the cul-de-sac at the western extent of the development would be 152 mm diameter. The proposed layout and sizing is shown in **Figure 2-3**.
- The serviceability of the development lands was analysed, considering that they would be serviced by the pressure zone SUC.
- As part of the currently proposed watermain layout, the backbone watermain is proposed to extend west along the northern edge of the Phase 4 lands to serve as a service connection to future adjacent development. There are no direct Phase 4 property service connections



## BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

Conclusion and Recommendations  
June 2, 2022

anticipated along this temporary dead-end section of watermain; therefore, it is recommended that this section be isolated until it is required to provide flow to adjacent future lands.

- Under AVDY demand conditions, model results using boundary conditions provided by the City exceed the allowable maximum pressure of 80 psi in accordance with the City of Ottawa Design Guidelines. As per the OBC, the static pressure at any fixture shall not exceed 80 psi, in areas that may be occupied. Where pressures do exceed 80 psi, pressure control measures such as PRVs installed immediately downstream of the isolation valve to the home/building shall be considered.
- Under PKHR demand conditions, the minimum pressures are in accordance with the City's system pressure requirements.
- Under MXDY+FF demand conditions, the target required fire flow of 13,000 L/min can be achieved through the proposed network for all phases when the alternative procedure outlined in the Appendix I of ISDTB-2018-02 is applied to the dead-end watermain in the western extent of the development lands.
- If Option A (servicing with two connections) is selected, watermain upgrades along Danson Gardens Grv are recommended to provide similar HGLs at the two connection points under a fire flow scenario.
- To satisfy and improve system reliability in the event of an emergency break scenario at key points in the network, a second backbone feed was redirected north then west (i.e., north of the standard and rear-lane townhouse blocks) across to the Phase 4 lands. However, under the current phasing plan, a second feed would still be required to service the Phase 2 service area west of the park area (sub-phase 2C, containing more than 50 properties) in the interim until sufficient looping can be provided through the subsequent Phase 3 (sub-phase 2E) if current phasing plans remain unchanged. It is recommended that sub-phase 2C be developed after sub-phase 2E, to provide sufficient looping. However, sub-phase 2C could be serviced on an interim basis, from the single feed, given that the rear-lane townhouses proposed under sub-phase 2C are delayed until sufficient looping is provided. Alternatively, delaying the construction of 6 other units, in addition to the rear-lane townhouses, could be considered for sub-phase 2C, to avoid the creation of a vulnerable service area.
- A water age analysis shows that the residence time of water within the development lands does not exceed the limits per the City's Design Guidelines. No water age boundary conditions at the connection points were available, therefore the total water age from the source or last point of rechlorination cannot be assessed. As such, water age issues within the development are not anticipated.



## BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

References  
June 2, 2022

### 5.0 REFERENCES

- City of Ottawa. (2010). *Ottawa Design Guidelines - Water Distribution*. Ottawa.
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- Stantec Consulting Ltd. (2013). *City of Ottawa 2013 Water Master Plan*. Ottawa.
- Stantec Consulting Ltd. (2021). *Hydraulic Potable Water Assessment for Barrhaven Conservancy Development Corporation*. Ottawa.



**BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION  
SYSTEM ANALYSIS**

June 2, 2022

**Appendix A      FUS CALCULATION**





## FUS Fire Flow Calculation

Calculations based on: "Water Supply for Public Fire Protection" by Fire Underwriters' Survey, 1999

Stantec Project #: 163401660  
 Project Name: Barrhaven Conservancy  
 Date: November 29, 2021  
 Data inputted by: Jasmin Sidhu, P.Eng.  
 Data reviewed by:

Fire Flow Calculation #: 1  
 Building Type/Description/Name: Residential

*Single family house (SFH) block based on draft site plan dated September 20, 2021. Area assumes largest SFH unit size.*  
*Notes: Minimum spatial separation between the backs of adjacent units is <10m (i.e., City's cap of 10,000 L/min as per Technical Bulletin ISDTB-2018-02 does not apply).*  
*Assumed wood frame construction.*  
*Target fire flow = 13,000 L/min. Requires a maximum of 2 adjacent consecutive wood frame construction units.*

Table A: Fire Underwriters Survey Determination of Required Fire Flow - Long Method												
Step	Task	Term	Options	Multiplier Associated with Option	Choose:	Value Used	Unit	Total Fire Flow (L/min)				
<b>Framing Material</b>												
1	Choose Frame Used for Construction of Unit	Coefficient related to type of construction (C)	Wood Frame	1.5	Wood Frame	1.5	m					
			Ordinary construction	1								
			Non-combustible construction	0.8								
			Fire resistive construction (< 2 hrs)	0.7								
			Fire resistive construction (> 2 hrs)	0.6								
			<b>Floor Space Area</b>									
2	Choose Type of Housing (if TH, Enter Number of Units Per TH Block)	Type of Housing	Single Family	2	Single Family	2	Units					
			Townhouse - indicate # of units	1								
			Other (Comm, Ind, Apt etc.)	1								
2.2	# of Storeys	Number of Floors/Storeys in the Unit (do not include basement if 50% below grade):										
3	Enter Average Floor Area of Unit or Block of Units	Average Floor Area (A) (non-fire resistive construction):										
3.1	Obtain Total Effective Building Area	Total Effective Building Area (# of Storeys x Average Floor Area of Unit x # of Units):										
4	Obtain Required Fire Flow without Reductions	Required Fire Flow (without reductions or increases per FUS) ( $F = 220 * C * \sqrt{A}$ ) Round to nearest 1,000 L/min										
5	Apply Factors Affecting Burning	<b>Reductions/Increases Due to Factors Affecting Burning</b>										
5.1	Choose Combustibility of Building Contents	Occupancy content hazard reduction or surcharge	Non-combustible	-0.25	Limited combustible	-0.15	N/A	6,800				
			Limited combustible	-0.15								
			Combustible	0								
			Free burning	0.15								
			Rapid burning	0.25								
5.2	Choose Reduction Due to Presence of Sprinklers	Sprinkler reduction	Adequate Sprinkler conforms to NFPA13	-0.3	None	0	N/A	0				
			None	0								
			Water supply is standard for sprinkler and fire dept. hose line	-0.1	Water supply is not standard or N/A	0	N/A	0				
			Water supply is not standard or N/A	0								
5.3	Choose Separation Distance Between Units	Exposure Distance Between Units	Sprinkler Supervision Credit	-0.1	Sprinkler not fully supervised or N/A	0	N/A	0				
			Sprinkler system is fully supervised	-0.1								
			Sprinkler not fully supervised or N/A	0								
			Front Yard	20.1 to 30.1m	0.1	0.75	m	5,100				
			Side Yard (Left)	0 to 3.0m								
			Rear Yard	3.1 to 10.0m								
			Side Yard (Right)	0 to 3.0m								
6	Obtain Required Fire Flow, Duration & Volume	<b>Total Required Fire Flow, rounded to nearest 1,000 L/min, with max/min limits applied:</b>										
		<b>Total Required Fire Flow (above) in L/s:</b>										
		<b>Required Duration of Fire Flow (hrs)</b>										
		<b>Required Volume of Fire Flow (m³)</b>										



## FUS Fire Flow Calculation

Calculations based on: "Water Supply for Public Fire Protection" by Fire Underwriters' Survey, 1999

Stantec Project #: 163401660

Project Name: Barrhaven Conservancy

Date: November 29, 2021

Data inputted by: Jasmin Sidhu, P.Eng.

Data reviewed by:

Fire Flow Calculation #: 2

Building Type/Description/Name: Residential

*Single family house (SFH) block based on draft site plan dated September 20, 2021. Area assumes largest SFH unit size.*

*Notes: Minimum spatial separation between the backs of adjacent units is <10m (i.e., City's cap of 10,000 L/min as per Technical Bulletin ISDTB-2018-02 does not apply).*

*Assumed ordinary construction (i.e., more than 2/3 of the buildings' exterior walls are made of brick or masonry veneer).*

*Target fire flow = 13,000 L/min. Requires a maximum of 5 adjacent consecutive ordinary construction units.*

Table A: Fire Underwriters Survey Determination of Required Fire Flow - Long Method

Step	Task	Term	Options	Multiplier Associated with Option	Choose:	Value Used	Unit	Total Fire Flow (L/min)				
<b>Framing Material</b>												
1	Choose Frame Used for Construction of Unit	Coefficient related to type of construction (C)	Wood Frame	1.5	Ordinary construction	1	m					
			Ordinary construction	1								
			Non-combustible construction	0.8								
			Fire resistive construction (< 2 hrs)	0.7								
			Fire resistive construction (> 2 hrs)	0.6								
<b>Floor Space Area</b>												
2	Choose Type of Housing (if TH, Enter Number of Units Per TH Block)	Type of Housing	Single Family	5	Single Family	5	Units					
			Townhouse - indicate # of units	1								
			Other (Comm, Ind, Apt etc.)	1								
2.2	# of Storeys	Number of Floors/Storeys in the Unit (do not include basement if 50% below grade):										
3	Enter Average Floor Area of Unit or Block of Units	Average Floor Area (A) (non-fire resistive construction):										
3.1	Obtain Total Effective Building Area	Total Effective Building Area (# of Storeys x Average Floor Area of Unit x # of Units):										
4	Obtain Required Fire Flow without Reductions	Required Fire Flow (without reductions or increases per FUS) ( $F = 220 * C * \sqrt{A}$ ) Round to nearest 1,000 L/min										
5	Apply Factors Affecting Burning	<b>Reductions/Increases Due to Factors Affecting Burning</b>										
5.1	Choose Combustibility of Building Contents	Occupancy content hazard reduction or surcharge	Non-combustible	-0.25	Limited combustible	-0.15	N/A	7,650				
			Limited combustible	-0.15								
			Combustible	0								
			Free burning	0.15								
			Rapid burning	0.25								
5.2	Choose Reduction Due to Presence of Sprinklers	Sprinkler reduction	Adequate Sprinkler conforms to NFPA13	-0.3	None	0	N/A	0				
			None	0								
			Water supply is standard for sprinkler and fire dept. hose line	-0.1	Water supply is not standard or N/A	0	N/A	0				
			Water supply is not standard or N/A	0								
5.3	Choose Separation Distance Between Units	Exposure Distance Between Units	Sprinkler Supervision Credit	-0.1	Sprinkler not fully supervised or N/A	0	N/A	0				
			Sprinkler system is fully supervised	-0.1								
			Sprinkler not fully supervised or N/A	0								
			Front Yard	20.1 to 30.1m	0.1	0.25	m	5,738				
			Side Yard (Left)	0 to 3.0m								
			Rear Yard	3.1 to 10.0m								
			Side Yard (Right)	0 to 3.0m								
6	Obtain Required Fire Flow, Duration & Volume	<b>Total Required Fire Flow, rounded to nearest 1,000 L/min, with max/min limits applied:</b>										
		<b>Total Required Fire Flow (above) in L/s:</b>										
		<b>Required Duration of Fire Flow (hrs)</b>										
		<b>Required Volume of Fire Flow (m³)</b>										



## FUS Fire Flow Calculation

Calculations based on: "Water Supply for Public Fire Protection" by Fire Underwriters' Survey, 1999

Stantec Project #: 163401660  
 Project Name: Barrhaven Conservancy  
 Date: May 10, 2022  
 Data inputted by: Christèle Razafimaharo  
 Data reviewed by: Jasmin Sidhu, P.Eng.

Fire Flow Calculation #: 3  
 Building Type/Description/Name: Residential

Notes: Maximum GFA for a STND TH fire area to achieve a required fire flow (RFF) of 13,000 L/min.  
 Target fire flow = 13,000 L/min. Fire walls required at the back to achieve RFF.

Table A: Fire Underwriters Survey Determination of Required Fire Flow - Long Method												
Step	Task	Term	Options	Multiplier Associated with Option	Choose:	Value Used	Unit	Total Fire Flow (L/min)				
<b>Framing Material</b>												
1	Choose Frame Used for Construction of Unit	Coefficient related to type of construction (C)	Wood Frame	1.5	Wood Frame	1.5	m					
			Ordinary construction	1								
			Non-combustible construction	0.8								
			Fire resistive construction (< 2 hrs)	0.7								
			Fire resistive construction (> 2 hrs)	0.6								
2	Choose Type of Housing (if TH, Enter Number of Units Per TH Block)	<b>Floor Space Area</b>										
		Type of Housing	Single Family	1	Townhouse - indicate # of units	5	Units					
			Townhouse - indicate # of units	5								
2.2	# of Storeys	Number of Floors/Storeys in the Unit (do not include basement if 50% below grade):										
3	Enter Average Floor Area of Unit or Block of Units	Average Floor Area (A) (non-fire resistive construction):										
3.1	Obtain Total Effective Building Area	Total Effective Building Area (# of Storeys x Average Floor Area of Unit x # of Units):										
4	Obtain Required Fire Flow without Reductions	Required Fire Flow (without reductions or increases per FUS) ( $F = 220 * C * \sqrt{A}$ ) Round to nearest 1,000 L/min										
5	Apply Factors Affecting Burning	<b>Reductions/Increases Due to Factors Affecting Burning</b>										
5.1	Choose Combustibility of Building Contents	Occupancy content hazard reduction or surcharge	Non-combustible	-0.25	Limited combustible	-0.15	N/A	7,650				
			Limited combustible	-0.15								
			Combustible	0								
			Free burning	0.15								
			Rapid burning	0.25								
5.2	Choose Reduction Due to Presence of Sprinklers	Sprinkler reduction	Adequate Sprinkler conforms to NFPA13	-0.3	None	0	N/A	0				
			None	0								
			Water supply is standard for sprinkler and fire dept. hose line	-0.1	Water supply is not standard or N/A	0	N/A	0				
			Water supply is not standard or N/A	0								
5.3	Choose Separation Distance Between Units	Exposure Distance Between Units	Sprinkler system is fully supervised	-0.1	Sprinkler not fully supervised or N/A	0	N/A	0				
			Sprinkler not fully supervised or N/A	0								
			Front Yard	20.1 to 30.1m	0.6	m	4,590					
			Side Yard (Left)	3.1 to 10.0m								
			Rear Yard	Fire Wall								
			Side Yard (Right)	3.1 to 10.0m								
6	Obtain Required Fire Flow, Duration & Volume	<b>Total Required Fire Flow, rounded to nearest 1,000 L/min, with max/min limits applied:</b>										
		<b>Total Required Fire Flow (above) in L/s:</b>										
		<b>Required Duration of Fire Flow (hrs)</b>										
		<b>Required Volume of Fire Flow (m³)</b>										



## FUS Fire Flow Calculation

Calculations based on: "Water Supply for Public Fire Protection" by Fire Underwriters' Survey, 1999

Stantec Project #: 163401660  
 Project Name: Barrhaven Conservancy  
 Date: September 29, 2021  
 Data inputted by: Tom Westwood, P.Eng  
 Data reviewed by: Jasmin Sidhu, P.Eng.

Fire Flow Calculation #: 4  
 Building Type/Description/Name: Residential

**Notes:** Governing rear lane townhouse (RLTH) block based on draft site plan dated September 20, 2021. Block consists of 5 RLTH units where minimum spatial separation between the backs of adjacent units is <10m and gross floor area of block is > 600m<sup>2</sup> (i.e., City's cap of 10,000 L/min as per Technical Bulletin ISDTB-2018-02 does not apply).

Table A: Fire Underwriters Survey Determination of Required Fire Flow - Long Method

Step	Task	Term	Options	Multiplier Associated with Option	Choose:	Value Used	Unit	Total Fire Flow (L/min)
<b>Framing Material</b>								
1	Choose Frame Used for Construction of Unit	Coefficient related to type of construction (C)	Wood Frame	1.5	Wood Frame	1.5	m	
			Ordinary construction	1				
			Non-combustible construction	0.8				
			Fire resistive construction (< 2 hrs)	0.7				
			Fire resistive construction (> 2 hrs)	0.6				
<b>Floor Space Area</b>								
2	Choose Type of Housing (if TH, Enter Number of Units Per TH Block)	Type of Housing	Single Family	1	Townhouse - indicate # of units	5	Units	
			Townhouse - indicate # of units	5				
			Other (Comm, Ind, Apt etc.)	1				
2.2	# of Storeys	Number of Floors/Storeys in the Unit (do not include basement if 50% below grade):						
3	Enter Average Floor Area of Unit or Block of Units	Average Floor Area (A) (non-fire resistive construction):						
3.1	Obtain Total Effective Building Area	Total Effective Building Area (# of Storeys x Average Floor Area of Unit x # of Units):						
4	Obtain Required Fire Flow without Reductions	Required Fire Flow (without reductions or increases per FUS) ( $F = 220 * C * \sqrt{A}$ ) Round to nearest 1,000 L/min						
5	Apply Factors Affecting Burning	<b>Reductions/Increases Due to Factors Affecting Burning</b>						
5.1	Choose Combustibility of Building Contents	Occupancy content hazard reduction or surcharge	Non-combustible	-0.25	Limited combustible	-0.15	N/A	7,650
			Limited combustible	-0.15				
			Combustible	0				
			Free burning	0.15				
			Rapid burning	0.25				
5.2	Choose Reduction Due to Presence of Sprinklers	Sprinkler reduction	Adequate Sprinkler conforms to NFPA13	-0.3	None	0	N/A	0
			None	0				
		Water Supply Credit	Water supply is standard for sprinkler and fire dept. hose line	-0.1	Water supply is not standard or N/A	0	N/A	0
			Water supply is not standard or N/A	0				
		Sprinkler Supervision Credit	Sprinkler system is fully supervised	-0.1	Sprinkler not fully supervised or N/A	0	N/A	0
			Sprinkler not fully supervised or N/A	0				
5.3	Choose Separation Distance Between Units	Exposure Distance Between Units	Front Yard	20.1 to 30.1m	0.1			
			Side Yard (Left)	3.1 to 10.0m	0.2			
			Rear Yard	3.1 to 10.0m	0.2			
			Side Yard (Right)	3.1 to 10.0m	0.2			
<b>Total Required Fire Flow, rounded to nearest 1,000 L/min, with max/min limits applied:</b>								<b>13,000</b>
<b>Total Required Fire Flow (above) in L/s:</b>								<b>217</b>
<b>Required Duration of Fire Flow (hrs):</b>								<b>2.75</b>
<b>Required Volume of Fire Flow (m<sup>3</sup>):</b>								<b>2,145</b>



## FUS Fire Flow Calculation

Calculations based on: "Water Supply for Public Fire Protection" by Fire Underwriters' Survey, 1999

Stantec Project #: 163401660  
 Project Name: Barrhaven Conservancy  
 Date: September 29, 2021  
 Data inputted by: Tom Westwood, P.Eng.  
 Data reviewed by: Jasmin Sidhu, P.Eng.

Fire Flow Calculation #: 5  
 Building Type/Description/Name: Residential

**Notes:** Governing back-to-back townhouse (B2B TH) block based on draft site plan dated September 20, 2021. Block consists of 10 B2B TH units separated by one fire wall, resulting in a fire area comprising 5 units with no spatial separation between the backs of adjacent units and gross floor area of block is > 600m<sup>2</sup> (i.e., City's cap of 10,000 L/min as per Technical Bulletin ISDTB-2018-02 does not apply).  
 Target Fire Flow = 13,000 L/min. Fire walls required at the back to achieve target fire flow.

Table A: Fire Underwriters Survey Determination of Required Fire Flow - Long Method

Step	Task	Term	Options	Multiplier Associated with Option	Choose:	Value Used	Unit	Total Fire Flow (L/min)
<b>Framing Material</b>								
1	Choose Frame Used for Construction of Unit	Coefficient related to type of construction (C)	Wood Frame	1.5	Wood Frame	1.5	m	
			Ordinary construction	1				
			Non-combustible construction	0.8				
			Fire resistive construction (< 2 hrs)	0.7				
			Fire resistive construction (> 2 hrs)	0.6				
<b>Floor Space Area</b>								
2	Choose Type of Housing (if TH, Enter Number of Units Per TH Block)	Type of Housing	Single Family	1	Townhouse - indicate # of units	5	Units	
			Townhouse - indicate # of units	5				
			Other (Comm, Ind, Apt etc.)	1				
2.2	# of Storeys	Number of Floors/Storeys in the Unit (do not include basement if 50% below grade):						
3	Enter Average Floor Area of Unit or Block of Units	Average Floor Area (A) (non-fire resistive construction):						
3.1	Obtain Total Effective Building Area	Total Effective Building Area (# of Storeys x Average Floor Area of Unit x # of Units):						
4	Obtain Required Fire Flow without Reductions	Required Fire Flow (without reductions or increases per FUS) (F = 220 * C * √A) Round to nearest 1,000 L/min						
5	Apply Factors Affecting Burning	<b>Reductions/Increases Due to Factors Affecting Burning</b>						
5.1	Choose Combustibility of Building Contents	Occupancy content hazard reduction or surcharge	Non-combustible	-0.25	Limited combustible	-0.15	N/A	7,650
			Limited combustible	-0.15				
			Combustible	0				
			Free burning	0.15				
			Rapid burning	0.25				
5.2	Choose Reduction Due to Presence of Sprinklers	Sprinkler reduction	Adequate Sprinkler conforms to NFPA13	-0.3	None	0	N/A	0
			None	0				
		Water Supply Credit	Water supply is standard for sprinkler and fire dept. hose line	-0.1	Water supply is not standard or N/A	0	N/A	0
			Water supply is not standard or N/A	0				
		Sprinkler Supervision Credit	Sprinkler system is fully supervised	-0.1	Sprinkler not fully supervised or N/A	0	N/A	0
			Sprinkler not fully supervised or N/A	0				
5.3	Choose Separation Distance Between Units	Exposure Distance Between Units	Front Yard	3.1 to 10.0m	0.2			
			Side Yard (Left)	20.1 to 30.1m	0.1			
			Rear Yard	3.1 to 10.0m	0.2			
			Side Yard (Right)	20.1 to 30.1m	0.1			
6	Obtain Required Fire Flow, Duration & Volume	<b>Total Required Fire Flow, rounded to nearest 1,000 L/min, with max/min limits applied:</b>						
		<b>Total Required Fire Flow (above) in L/s:</b>						
		<b>Required Duration of Fire Flow (hrs)</b>						
		<b>Required Volume of Fire Flow (m<sup>3</sup>)</b>						

**BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION  
SYSTEM ANALYSIS**

June 2, 2022

**Appendix B      BOUNDARY CONDITIONS**

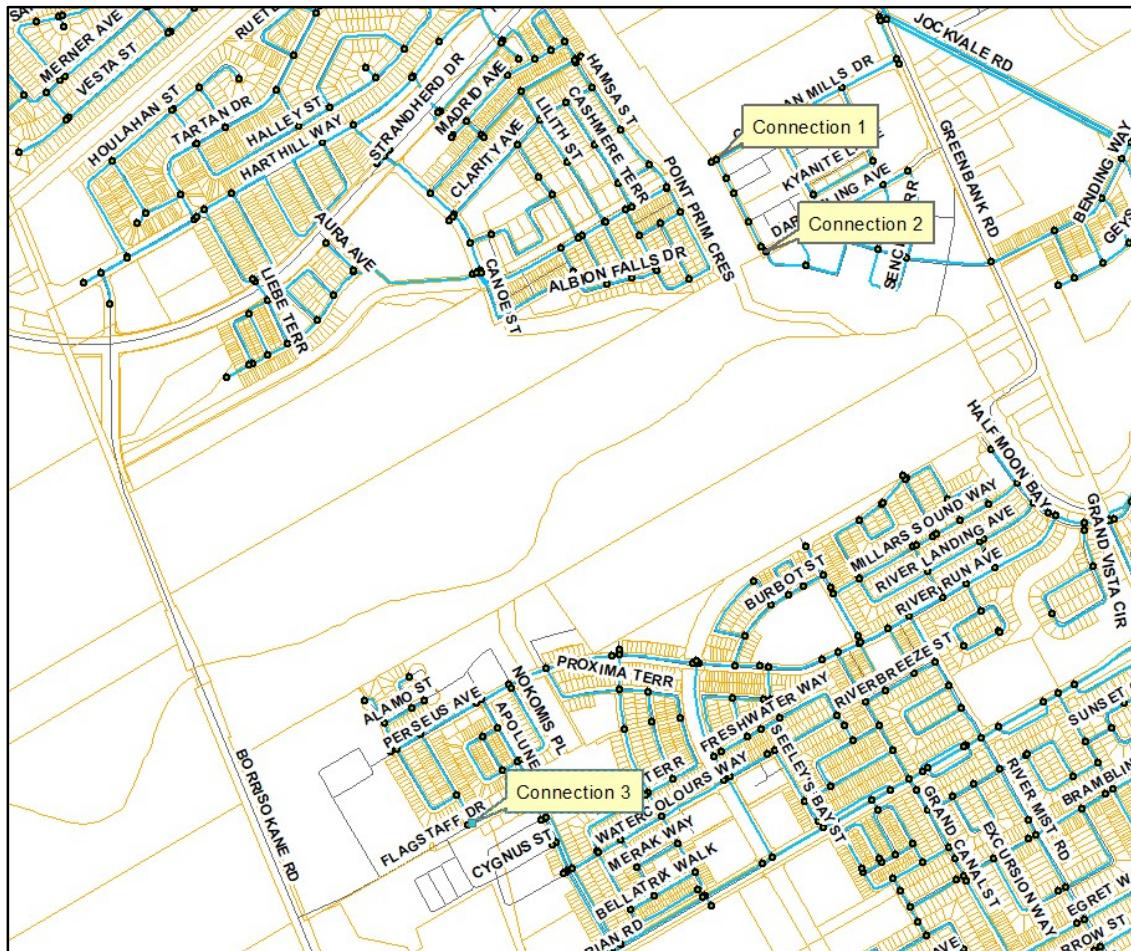


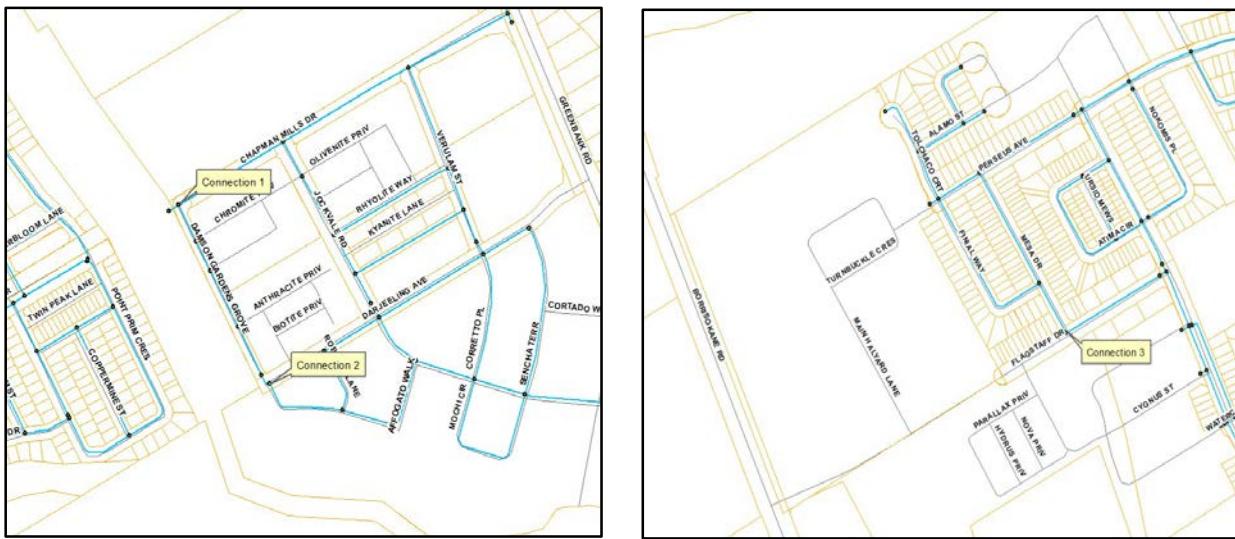
## Boundary Conditions Barrhaven Conservancy East

### Provided Information

Scenario	Demand	
	L/min	L/s
Average Daily Demand	832	13.87
Maximum Daily Demand	2,080	34.67
Peak Hour	4,576	76.27
Fire Flow Demand #1	13,000	216.67

### Location





### Results – Existing Conditions BSDY

#### Connection 1 – Chapman Mills Dr.

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	158.7	93.7
Peak Hour	142.6	70.7
Basic Day plus Fire 1	131.2	54.5

Ground Elevation = 92.8 m

#### Connection 2 – Danson Gardens Grove / Darjeeling Ave.

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	158.7	95.1
Peak Hour	142.5	72.1
Basic Day plus Fire 1	127.6	50.9

Ground Elevation = 91.8 m

#### Connection 3 – Flagstaff Dr.

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	158.6	94.5
Peak Hour	142.1	71.1
Basic Day plus Fire 1	129.9	53.7

Ground Elevation = 92.1 m

### Results – Existing Conditions MXDY

#### Connection 1 – Chapman Mills Dr.

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	157.0	91.2
Peak Hour	137.6	63.7
Max Day plus Fire 1	140.1	67.2

Ground Elevation = 92.8 m

**Connection 2 – Danson Gardens Grove / Darjeeling Ave.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	157.0	92.7
Peak Hour	137.6	65.0
Max Day plus Fire 1	136.4	63.4

Ground Elevation = 91.8 m

**Connection 3 – Flagstaff Dr.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	156.8	91.9
Peak Hour	136.9	63.7
Max Day plus Fire 1	137.7	64.8

Ground Elevation = 92.1 m

**Results – SUC Zone Reconfiguration BSDY****Connection 1 – Chapman Mills Dr.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	149.5	80.7
Peak Hour	147.3	77.5
Basic Day plus Fire 1	138.6	65.1

Ground Elevation = 92.8 m

**Connection 2 – Danson Gardens Grove / Darjeeling Ave.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	149.5	82.1
Peak Hour	147.3	78.9
Basic Day plus Fire 1	135.1	61.5

Ground Elevation = 91.8 m

**Connection 3 – Flagstaff Dr.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	149.5	81.5
Peak Hour	146.9	77.9
Basic Day plus Fire 1	137.4	64.3

Ground Elevation = 92.1 m

**Results – SUC Zone Reconfiguration MXDY****Connection 1 – Chapman Mills Dr.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	147.9	78.3
Peak Hour	144.5	73.4
Max Day plus Fire 1	137.1	62.9

Ground Elevation = 92.8 m

**Connection 2 – Danson Gardens Grove / Darjeeling Ave.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	147.9	79.7
Peak Hour	144.4	74.7
Max Day plus Fire 1	133.4	59.1

Ground Elevation = 91.8 m

**Connection 3 – Flagstaff Dr.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	147.5	78.8
Peak Hour	142.0	71.0
Max Day plus Fire 1	134.8	60.6

Ground Elevation = 92.1 m

**Notes**

1. As per the Ontario Building Code in areas that may be occupied, the static pressure at any fixture shall not exceed 552 kPa (80 psi.) Pressure control measures to be considered are as follows, in order of preference:
  - a. If possible, systems to be designed to residual pressures of 345 to 552 kPa (50 to 80 psi) in all occupied areas outside of the public right-of-way without special pressure control equipment.
  - b. Pressure reducing valves to be installed immediately downstream of the isolation valve in the home/ building, located downstream of the meter so it is owner maintained.

**Disclaimer**

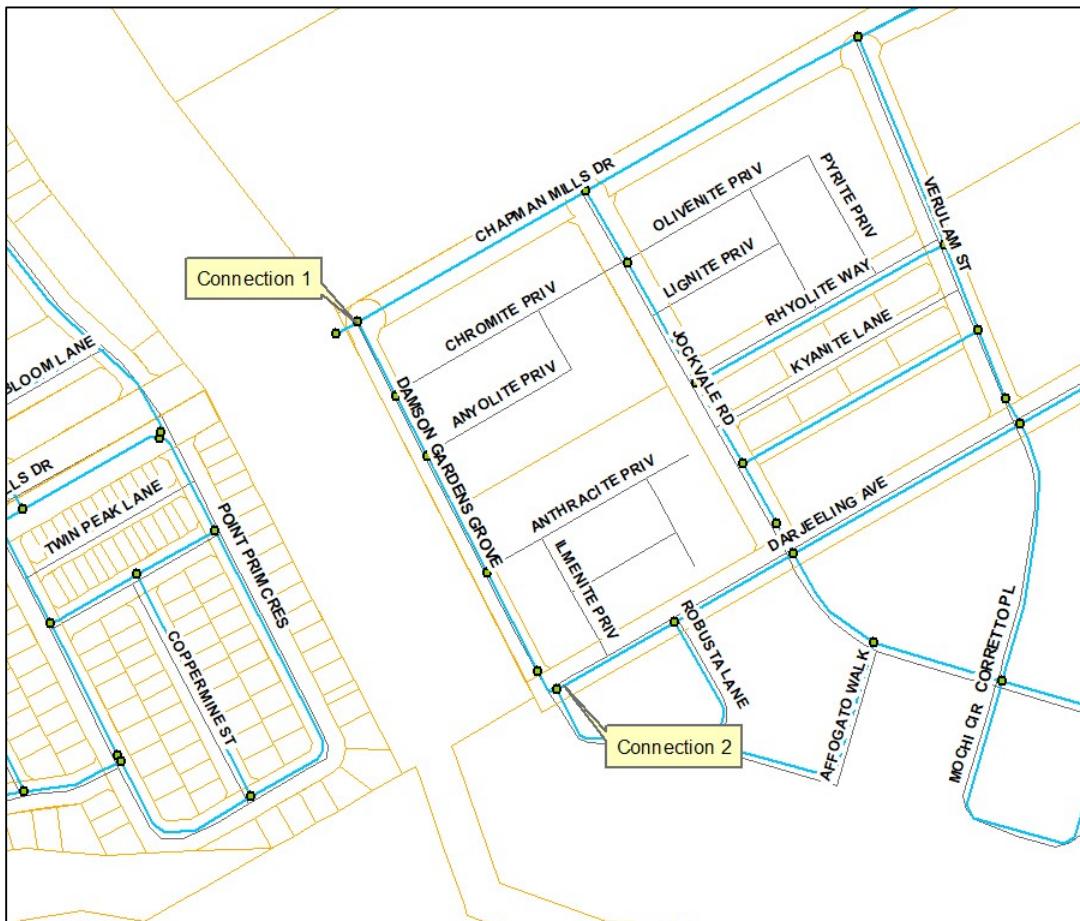
*The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of water mains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation. Fire Flow analysis is a reflection of available flow in the watermain; there may be additional restrictions that occur between the watermain and the hydrant that the model cannot take into account.*

## Boundary Conditions Barrhaven Conservancy East

### Provided Information

Scenario	Demand	
	L/min	L/s
Average Daily Demand	832	13.87
Maximum Daily Demand	2,080	34.67
Peak Hour	4,576	76.27
Fire Flow Demand #1	13,000	216.67

### Location



### Scenario 1 Results – Existing Conditions BSDY

#### Connection 1 – Chapman Mills Dr.

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	158.7	93.7
Peak Hour	142.5	70.7
Basic Day plus Fire 1	131.0	54.2

Ground Elevation = 92.8 m

**Connection 2 – Danson Gardens Grove / Darjeeling Ave.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	158.7	95.1
Peak Hour	142.5	72.1
Basic Day plus Fire 1	127.4	50.6

Ground Elevation = 91.8 m

**Scenario 1 Results – Existing Conditions MXDY****Connection 1 – Chapman Mills Dr.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	157.0	91.2
Peak Hour	137.5	63.5
Max Day plus Fire 1	139.6	66.5

Ground Elevation = 92.8 m

**Connection 2 – Danson Gardens Grove / Darjeeling Ave.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	157.0	92.6
Peak Hour	137.5	64.9
Max Day plus Fire 1	135.8	62.5

Ground Elevation = 91.8 m

**Scenario 1 Results – SUC Zone Reconfiguration BSDY****Connection 1 – Chapman Mills Dr.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	150.0	81.3
Peak Hour	147.6	77.9
Basic Day plus Fire 1	138.7	65.2

Ground Elevation = 92.8 m

**Connection 2 – Danson Gardens Grove / Darjeeling Ave.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	150.0	82.8
Peak Hour	147.6	79.2
Basic Day plus Fire 1	135.1	61.5

Ground Elevation = 91.8 m

**Scenario 1 Results – SUC Zone Reconfiguration MXDY****Connection 1 – Chapman Mills Dr.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	148.6	79.3
Peak Hour	144.2	73.0
Max Day plus Fire 1	137.0	62.8

Ground Elevation = 92.8 m

**Connection 2 – Danson Gardens Grove / Darjeeling Ave.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	148.6	80.7
Peak Hour	144.0	74.2
Max Day plus Fire 1	133.2	58.8

Ground Elevation = 91.8 m

**Scenario 2 Results – Existing Conditions BSDY****Connection 1 – Chapman Mills Dr.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	158.7	93.7
Peak Hour	142.5	70.7
Basic Day plus Fire 1	131.2	54.5

Ground Elevation = 92.8 m

**Connection 2 – Danson Gardens Grove / Darjeeling Ave.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	158.7	93.7
Peak Hour	142.5	70.7
Basic Day plus Fire 1	132.4	57.6

Ground Elevation = 91.8 m

**Scenario 2 Results – Existing Conditions MXDY****Connection 1 – Chapman Mills Dr.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	157.0	91.2
Peak Hour	137.5	63.6
Max Day plus Fire 1	139.9	66.9

Ground Elevation = 92.8 m

**Connection 2 – Danson Gardens Grove / Darjeeling Ave.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	157.0	92.6
Peak Hour	137.5	65.0
Max Day plus Fire 1	141.1	70.1

Ground Elevation = 91.8 m

**Scenario 2 Results – SUC Zone Reconfiguration BSDY****Connection 1 – Chapman Mills Dr.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	149.5	80.7
Peak Hour	147.3	77.5
Basic Day plus Fire 1	138.6	65.1

Ground Elevation = 92.8 m

**Connection 2 – Danson Gardens Grove / Darjeeling Ave.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	149.5	80.7
Peak Hour	147.3	77.5
Basic Day plus Fire 1	139.8	68.2

Ground Elevation = 91.8 m

**Scenario 2 Results – SUC Zone Reconfiguration MXDY****Connection 1 – Chapman Mills Dr.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	147.9	78.3
Peak Hour	144.1	72.9
Max Day plus Fire 1	136.8	62.6

Ground Elevation = 92.8 m

**Connection 2 – Danson Gardens Grove / Darjeeling Ave.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	147.9	79.7
Peak Hour	144.1	74.3
Max Day plus Fire 1	138.1	65.8

Ground Elevation = 91.8 m

**Notes**

1. The watermain on Darjeeling Ave. was upsized to a 300mm diameter pipe between Danson Gardens Grove and Jockvale Road during Scenario 2 for modelling purposes.
2. As per the Ontario Building Code in areas that may be occupied, the static pressure at any fixture shall not exceed 552 kPa (80 psi.) Pressure control measures to be considered are as follows, in order of preference:
  - a. If possible, systems to be designed to residual pressures of 345 to 552 kPa (50 to 80 psi) in all occupied areas outside of the public right-of-way without special pressure control equipment.
  - b. Pressure reducing valves to be installed immediately downstream of the isolation valve in the home/ building, located downstream of the meter so it is owner maintained.

**Disclaimer**

*The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation. Fire Flow analysis is a reflection of available flow in the watermain; there may be additional restrictions that occur between the watermain and the hydrant that the model cannot take into account.*

**BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION  
SYSTEM ANALYSIS**

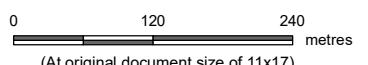
June 2, 2022

**Appendix C JUNCTION IDS**



**Legend**

- Development Phase Boundary
- Development Sub-Phase Boundary
- Property Line
- Future Watermain
- Model Junction

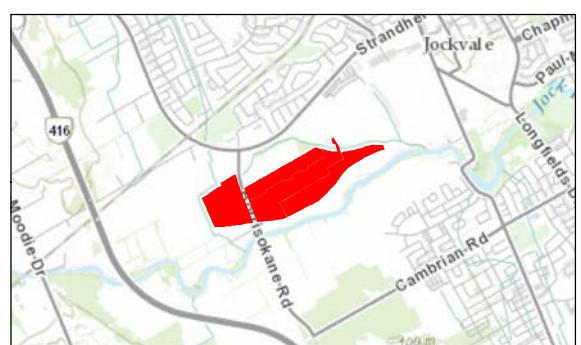


(At original document size of 11x17)  
1:6,500



**Notes**

1. Coordinate System: NAD 1983 CSRS MTM 9
2. Background: Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community



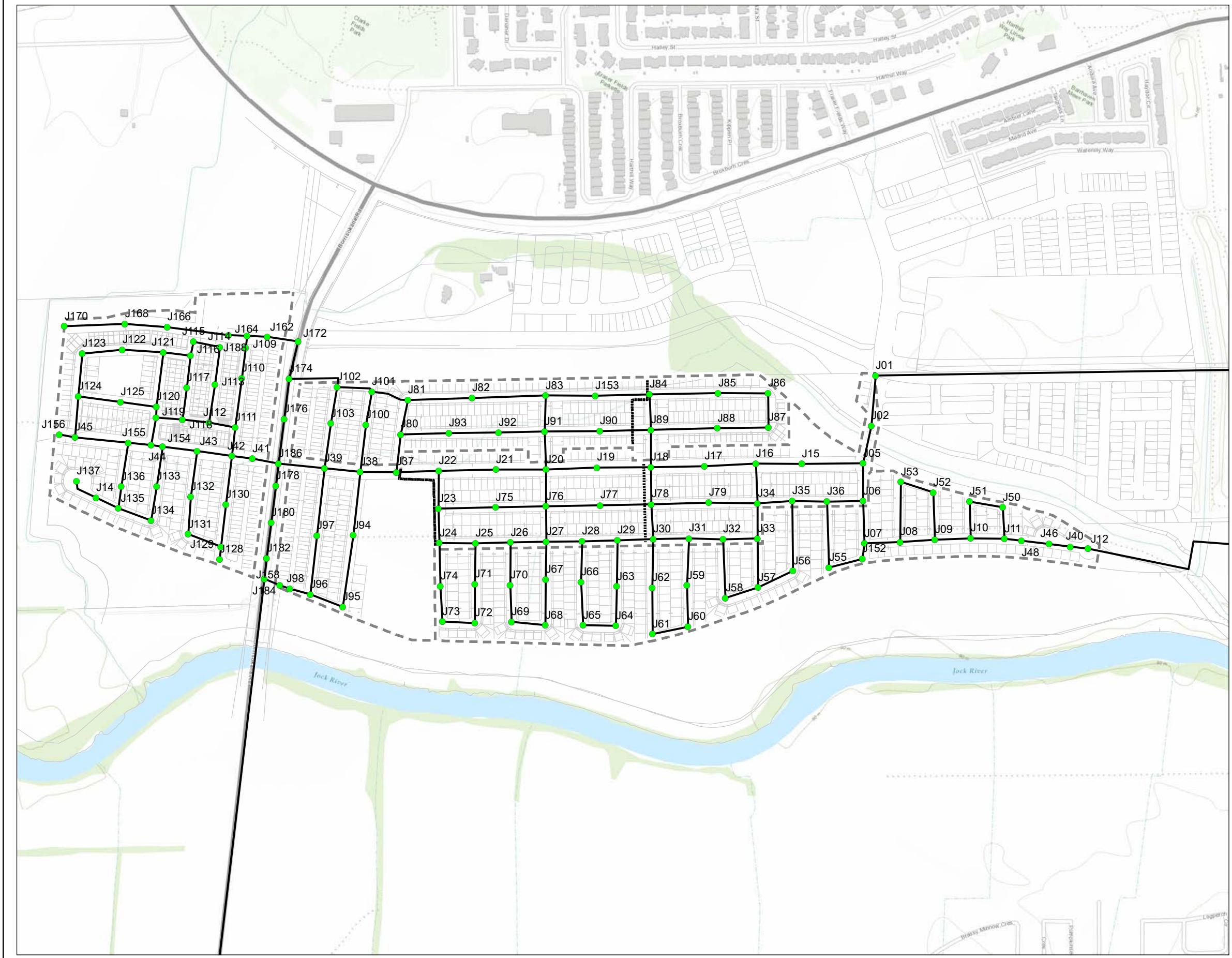
**Project Location**  
Ottawa, ON

**Client/Project**  
David Schaeffer Engineering Ltd  
Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River)  
Water Distribution System Analysis

**Figure No.**

**C1**

**Title**  
**Junction IDs**



**BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION  
SYSTEM ANALYSIS**

June 2, 2022

**Appendix D MODEL RESULTS**



Option A - 2 Connections - Phase 2 (2A, 2B, 2C)				Option A - 2 Connections with Upgrades on Danson Gardens Grv - Phase 2 (2A, 2B, 2C)				Option B - 3 Connections - Phase 2 (2A, 2B, 2C)			
Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)
Maximum	0.11	150.00	81.74	Maximum	0.11	149.50	81.03	Maximum	0.11	150.00	81.73
Minimum	0.00	150.00	80.32	Minimum	0.00	149.50	79.61	Minimum	0.00	149.99	80.31
J01	0.07	150.00	80.32	J01	0.07	149.50	79.61	J01	0.07	150.00	80.31
J02	0.00	150.00	80.32	J02	0.00	149.50	80.22	J02	0.00	150.00	80.92
J05	0.01	150.00	81.43	J05	0.01	149.50	80.45	J05	0.01	150.00	81.42
J06	0.07	150.00	81.57	J06	0.07	149.50	80.86	J06	0.07	150.00	81.56
J07	0.11	150.00	81.73	J07	0.11	149.50	81.01	J07	0.11	150.00	81.72
J08	0.11	150.00	81.60	J08	0.11	149.50	80.89	J08	0.11	150.00	81.59
J09	0.11	150.00	81.09	J09	0.11	149.50	80.38	J09	0.11	150.00	81.08
J10	0.11	150.00	81.34	J10	0.11	149.50	80.53	J10	0.11	150.00	81.34
J11	0.11	150.00	81.01	J11	0.11	149.50	80.52	J11	0.11	150.00	81.22
J12	0.11	150.00	81.09	J12	0.11	149.50	80.58	J12	0.11	150.00	81.08
J15	0.07	150.00	81.28	J15	0.07	149.50	80.57	J15	0.07	149.99	81.28
J158	0.00	150.00	81.74	J158	0.00	149.50	81.03	J158	0.00	149.99	81.73
J16	0.07	150.00	81.44	J16	0.07	149.50	80.73	J16	0.07	149.99	81.43
J17	0.07	150.00	81.27	J17	0.07	149.50	80.56	J17	0.07	149.99	81.26
J178	0.06	150.00	81.36	J178	0.06	149.50	80.56	J178	0.06	149.99	81.35
J18	0.07	150.00	81.06	J18	0.07	149.50	80.35	J18	0.07	149.99	81.05
J180	0.08	150.00	81.57	J180	0.08	149.50	80.86	J180	0.08	149.99	81.56
J182	0.08	150.00	81.68	J182	0.08	149.50	80.97	J182	0.08	149.99	81.68
J184	0.08	150.00	81.74	J184	0.08	149.50	81.03	J184	0.08	149.99	81.73
J186	0.08	150.00	81.26	J186	0.08	149.50	80.54	J186	0.08	149.99	81.25
J19	0.10	150.00	80.84	J19	0.10	149.50	80.19	J19	0.10	149.99	80.84
J20	0.01	150.00	81.01	J20	0.01	149.50	80.40	J20	0.01	149.99	81.31
J21	0.10	150.00	81.16	J21	0.10	149.50	80.45	J21	0.10	149.99	81.15
J22	0.10	150.00	81.21	J22	0.10	149.50	80.50	J22	0.10	149.99	81.21
J23	0.10	150.00	81.34	J23	0.10	149.50	80.63	J23	0.10	149.99	81.33
J24	0.10	150.00	81.47	J24	0.10	149.50	80.76	J24	0.10	149.99	81.46
J25	0.10	150.00	81.36	J25	0.10	149.50	80.54	J25	0.10	149.99	81.35
J26	0.00	150.00	81.26	J26	0.00	149.50	80.36	J26	0.00	149.99	81.45
J27	0.19	150.00	81.58	J27	0.19	149.50	80.87	J27	0.19	149.99	81.58
J28	0.10	150.00	81.51	J28	0.10	149.50	80.80	J28	0.10	149.99	81.51
J29	0.10	150.00	81.51	J29	0.10	149.50	80.80	J29	0.10	149.99	81.51
J30	0.07	150.00	81.44	J30	0.07	149.50	80.73	J30	0.07	149.99	81.43
J31	0.07	150.00	81.57	J31	0.07	149.50	80.86	J31	0.07	149.99	81.56
J32	0.07	150.00	81.01	J32	0.07	149.50	80.42	J32	0.07	149.99	81.46
J33	0.07	150.00	81.70	J33	0.07	149.50	80.59	J33	0.07	149.99	81.69
J34	0.07	150.00	81.57	J34	0.07	149.50	80.86	J34	0.07	149.99	81.56
J35	0.07	150.00	81.53	J35	0.07	149.50	80.82	J35	0.07	149.99	81.52
J36	0.07	150.00	81.65	J36	0.07	149.50	80.94	J36	0.07	149.99	81.65
J37	0.08	150.00	81.13	J37	0.08	149.50	80.42	J37	0.08	149.99	81.12
J38	0.08	150.00	81.26	J38	0.08	149.50	80.58	J38	0.08	149.99	81.25
J39	0.01	150.00	81.06	J39	0.08	149.50	80.44	J39	0.08	149.99	81.23
J40	0.11	150.00	81.12	J40	0.11	149.50	80.41	J40	0.11	150.00	81.11
J46	0.11	150.00	81.16	J46	0.11	149.50	80.45	J46	0.11	150.00	81.16
J48	0.11	150.00	81.20	J48	0.11	149.50	80.49	J48	0.11	150.00	81.20
J75	0.10	150.00	81.28	J75	0.10	149.50	80.57	J75	0.10	149.99	81.28
J76	0.10	150.00	81.17	J76	0.10	149.50	80.74	J76	0.10	149.99	81.45
J77	0.01	150.00	81.17	J77	0.10	149.50	80.77	J77	0.01	149.99	81.16
J78	0.07	150.00	81.33	J78	0.07	149.50	80.82	J78	0.07	149.99	81.32
J79	0.07	150.00	81.41	J79	0.07	149.50	80.70	J79	0.07	149.99	81.41
J94	0.08	150.00	81.51	J94	0.08	149.50	80.80	J94	0.08	149.99	81.50
J95	0.08	150.00	81.74	J95	0.08	149.50	81.03	J95	0.08	149.99	81.73
J96	0.08	150.00	81.61	J96	0.08	149.50	80.90	J96	0.08	149.99	81.60
J97	0.08	150.00	81.37	J97	0.08	149.50	80.65	J97	0.08	149.99	81.36
J98	0.09	150.00	81.54	J98	0.09	149.50	80.83	J98	0.09	149.99	81.53

Option A - 2 Connections - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E)				Option A - 2 Connections with Upgrades on Danson Gardens Grv - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E)				Option B - 3 Connections - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E)			
Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)
Maximum	0.15	150.00	81.73	Maximum	0.15	149.50	81.02	Maximum	0.15	149.99	81.71
Minimum	0.00	149.99	80.32	Minimum	0.00	149.49	79.61	Minimum	0.00	149.98	80.30
J01	0.07	150.00	80.32	J01	0.07	149.50	79.61	J01	0.07	149.99	80.30
J02	0.00	150.00	80.32	J02	0.00	149.50	80.22	J02	0.00	149.99	80.91
J05	0.07	150.00	81.42	J05	0.07	149.50	80.51	J05	0.07	149.98	81.41
J06	0.07	150.00	81.57	J06	0.07	149.50	80.86	J06	0.07	149.99	81.55
J07	0.11	150.00	81.72	J07	0.11	149.50	81.01	J07	0.11	149.99	81.71
J08	0.11	150.00	81.60	J08	0.11	149.50	80.88	J08	0.11	149.99	81.58
J09	0.11	150.00	81.08	J09	0.11	149.50	80.37	J09	0.11	149.99	81.07
J10	0.11	150.00	81.34	J10	0.11	149.50	80.63	J10	0.11	149.99	81.33
J100	0.15	149.99	80.00	J100	0.15	149.49	80.00	J100	0.15	149.98	80.78
J101	0.01	149.99	80.95	J101	0.01	149.49	80.24	J101	0.01	149.98	80.92
J102	0.15	149.99	80.84	J102	0.15	149.49	80.13	J102	0.15	149.98	80.82
J103	0.15	149.99	80.68	J103	0.15	149.49	79.97	J103	0.15	149.98	80.66
J11	0.11	150.00	81.23	J11	0.11	149.50	80.52	J11	0.11	149.99	81.22
J12	0.11	150.00	81.09	J12	0.11	149.50	80.37	J12	0.11	149.99	81.08
J15	0.07	150.00	81.50	J15	0.07	149.50	80.55	J15	0.07	149.98	81.26
J153	0.15	149.99	80.77	J153	0.15	149.49	80.56	J153	0.15	149.98	80.75
J158	0.00	149.99	81.73	J158	0.00	149.49	81.02	J158	0.00	149.98	81.71
J16	0.07	150.00	81.44	J16	0.07	149.50	80.73	J16	0.07	149.98	81.42
J17	0.07	150.00	81.27	J17	0.07	149.50	80.56	J17	0.07	149.98	81.25
J174	0.15	149.99	81.02	J174	0.15	149.49	80.31	J174	0.15	149.98	81.00
J176	0.15	149.99	81.14	J176	0.15	149.49	80.41	J176	0.15	149.98	81.12
J178	0.03	149.99	81.55	J178	0.03	149.49	80.54	J178	0.03	149.98	81.33
J18	0.07	150.00	81.05	J18	0.07	149.50	80.34	J18	0.07	149.98	81.03
J180	0.08	149.99	81.56	J180	0.08	149.49	80.85	J180	0.08	149.98	81.54
J182	0.08	149.99	81.68	J182	0.08	149.49	80.97	J182	0.08	149.98	81.66
J184	0.08	149.99	81.73	J184	0.08	149.49	81.02	J184	0.08	149.98	81.71
J186	0.08	149.99	81.25	J186	0.08	149.49	80.54	J186	0.08	149.98	81.23
J19	0.00	150.00	80.60	J19	0.00	149.50	80.39	J19	0.00	149.98	80.82
J20	0.19	150.00	81.31	J20	0.10	149.50	80.80	J20	0.10	149.98	81.23
J21	0.10	150.00	81.15	J21	0.10	149.50	80.44	J21	0.10	149.98	81.13
J22	0.10	150.00	81.21	J22	0.10	149.50	80.50	J22	0.10	149.98	81.19
J23	0.10	150.00	81.34	J23	0.10	149.50	80.63	J23	0.10	149.98	81.32
J24	0.10	150.00	81.46	J24	0.10	149.50	80.75	J24	0.10	149.98	81.44
J25	0.10	150.00	81.65	J25	0.10	149.50	80.85	J25	0.10	149.98	81.53
J26	0.19	150.00	81.45	J26	0.10	149.50	80.74	J26	0.10	149.98	81.43
J27	0.10	150.00	81.58	J27	0.10	149.50	80.87	J27	0.10	149.98	81.56
J28	0.10	150.00	81.51	J28	0.10	149.50	80.80	J28	0.10	149.98	81.49
J29	0.10	150.00	81.51	J29	0.10	149.50	80.80	J29	0.10	149.98	81.49
J30	0.07	150.00	81.44	J30	0.07	149.50	80.73	J30	0.07	149.98	81.42
J31	0.07	150.00	81.03	J31	0.07	149.50	80.35	J31	0.07	149.98	81.35
J32	0.07	150.00	81.47	J32	0.07	149.50	80.52	J32	0.07	149.98	81.45
J33	0.07	150.00	81.69	J33	0.07	149.50	80.98	J33	0.07	149.98	81.68
J34	0.07	150.00	81.57	J34	0.07	149.50	80.85	J34	0.07	149.98	81.55
J35	0.07	150.00	81.52	J35	0.07	149.50	80.81	J35	0.07	149.98	81.51
J36	0.07	150.00	81.65	J36	0.07	149.50	80.94	J36	0.07	149.99	81.64
J37	0.08	149.99	81.12	J37	0.08	149.49	80.41	J37	0.08	149.98	81.10
J38	0.08	149.99	81.26	J38	0.08	149.49	80.54	J38	0.08	149.98	81.23
J39	0.08	149.99	81.28	J39	0.08	149.49	80.54	J39	0.08	149.98	81.23
J40	0.11	150.00	81.12	J40	0.11	149.50	80.40	J40	0.11	149.99	81.11
J46	0.11	150.00	81.16	J46	0.11	149.50	80.45	J46	0.11	149.99	81.15
J48	0.11	150.00	81.20	J48	0.11	149.50	80.49	J48	0.11	149.99	81.19
J75	0.10	150.00	81.28	J75	0.10	149.50	80.57	J75	0.10	149.98	81.26
J76	0.10	150.00	81.04	J76	0.10	149.50	80.34	J76	0.10	149.98	81.43
J77	0.19	150.00	81.17	J77	0.10	149.50	80.46	J77	0.19	149.98	81.15
J78	0.07	150.00	81.32	J78	0.07	149.50	80.61	J78	0.07	149.98	81.30
J79	0.07	150.00	81.41	J79	0.07	149.50	80.70	J79	0.07	149.98	81.39
J80	0.15	149.99	80.98	J80	0.15	149.49	80.27	J80	0.15	149.98	80.96
J81	0.15	149.99	80.80	J81	0.15	149.49	80.08	J81	0.15	149.98	80.78
J82	0.15	149.99	80.95	J82	0.15	149.49	80.32	J82	0.15	149.98	80.92
J83	0.15	149.99	81.05	J83	0.15	149.49	80.54	J83	0.15	149.98	81.03
J84	0.15	150.00	80.92	J84	0.15	149.50	80.21	J84	0.15	149.98	80.90
J85	0.15	149.99	81.02	J85	0.15	149.49	80.31	J85	0.15	149.98	81.00
J86	0.15	149.99	81.24	J86	0.15	149.49	80.53	J86	0.15	149.98	81.22
J87	0.15	149.99	81.19	J87	0.15	149.49	80.48	J87	0.15	149.98	81.17
J88	0.15	149.99	81.68	J88	0.15	149.49	80.36	J88	0.15	149.98	81.03
J89	0.01	150.00	81.05	J89	0.15	149.50	80.44	J89	0.15	149.98	81.03
J90	0.15	150.00	80.88	J90	0.15	149.50	80.17	J90	0.15	149.98	80.86
J91	0.15	149.99	81.18	J91	0.15	149.49	80.47	J91	0.15	149.98	81.16
J92	0.15	149.99	80.99	J92	0.15	149.49	80.28	J92	0.15	149.98	80.98
J93	0.15	149.99	80.88	J93	0.15	149.49	80.17	J93	0.15	149.98	80.86
J94	0.08	149.99	81.04	J94	0.08	149.49	80.50	J94	0.08	149.98	81.49
J95	0.08	149.99	81.73	J95	0.08	149.49	80.45	J95	0.08	149.98	81.11
J96	0.08	149.99	81.61	J96	0.08	149.49	80.90	J96	0.08	149.98	81.59
J97	0.08	149.99	81.36	J97	0.08	149.49	80.65	J97	0.08	149.98	81.34
J98	0.00	149.99	81.53	J98	0.00	149.49	80.82	J98	0.00	149.98	81.52

Option A - 2 Connections - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E) + Phase 4				Option A - 2 Connections with Upgrades on Danson Gardens Grv - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E) + Phase 4				Option B - 3 Connections - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E) + Phase 4			
Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)
Maximum	0.15	150.00	81.72	Maximum	0.15	149.50	81.01	Maximum	0.15	149.42	81.00
Minimum	0.00	149.99	80.31	Minimum	0.00	149.49	79.60	Minimum	0.00	149.48	79.59
J01	0.07	149.99	80.31	J01	0.07	149.49	79.60	J01	0.07	149.49	79.59
J02	0.00	149.99	80.21	J02	0.00	149.49	80.21	J02	0.00	149.49	80.20
J05	0.07	149.99	81.42	J05	0.07	149.49	80.51	J05	0.07	149.48	80.70
J06	0.07	149.99	81.56	J06	0.07	149.49	80.51	J06	0.07	149.49	80.84
J07	0.11	149.99	81.72	J07	0.11	149.49	81.01	J07	0.11	149.49	81.00
J08	0.11	149.99	81.59	J08	0.11	149.49	80.88	J08	0.11	149.49	80.87
J09	0.11	150.00	81.08	J09	0.11	149.50	80.37	J09	0.11	149.49	80.36
J10	0.11	149.99	81.34	J10	0.11	149.50	80.63	J10	0.11	149.49	80.62
J100	0.15	149.99	80.86	J100	0.15	149.49	80.00	J100	0.15	149.48	80.06
J101	0.01	149.99	80.94	J101	0.01	149.49	80.23	J101	0.01	149.48	80.22
J102	0.15	149.99	80.83	J102	0.15	149.49	80.12	J102	0.15	149.48	80.11
J103	0.15	149.99	80.67	J103	0.15	149.49	79.96	J103	0.15	149.48	79.95
J109	0.11	149.99	80.96	J109	0.11	149.49	80.24	J109	0.11	149.48	80.23
J110	0.11	150.00	81.22	J111	0.11	149.50	80.51	J111	0.11	149.49	80.50
J111	0.11	149.99	81.00	J111	0.11	149.49	80.40	J111	0.11	149.48	80.40
J112	0.11	149.99	81.10	J112	0.11	149.49	80.39	J112	0.11	149.48	80.37
J113	0.11	149.99	81.01	J113	0.11	149.49	80.30	J113	0.11	149.48	80.29
J114	0.11	149.99	80.87	J114	0.11	149.49	80.16	J114	0.11	149.48	80.15
J115	0.11	149.99	80.84	J115	0.11	149.49	80.13	J115	0.11	149.48	80.12
J116	0.11	149.99	80.86	J116	0.11	149.49	80.11	J116	0.11	149.48	80.11
J117	0.11	149.99	81.01	J117	0.11	149.49	80.29	J117	0.11	149.48	80.29
J118	0.11	149.99	81.10	J118	0.11	149.49	80.39	J118	0.11	149.48	80.37
J119	0.11	149.99	81.23	J119	0.11	149.49	80.51	J119	0.11	149.48	80.50
J12	0.11	150.00	81.08	J12	0.11	149.50	80.37	J12	0.11	149.49	80.37
J120	0.11	149.99	81.23	J120	0.11	149.49	80.51	J120	0.11	149.48	80.50
J121	0.11	149.99	81.29	J121	0.11	149.49	80.32	J121	0.11	149.48	80.30
J122	0.11	149.99	80.93	J122	0.11	149.49	80.22	J122	0.11	149.48	80.15
J123	0.11	149.99	81.01	J123	0.11	149.49	80.30	J123	0.11	149.48	80.29
J124	0.11	149.99	81.15	J124	0.11	149.49	80.44	J124	0.11	149.48	80.43
J125	0.11	149.99	81.34	J125	0.11	149.49	80.63	J125	0.11	149.48	80.62
J128	0.00	149.99	81.69	J128	0.00	149.49	80.98	J128	0.00	149.48	80.97
J129	0.11	149.99	81.67	J129	0.11	149.49	80.96	J129	0.11	149.48	80.94
J130	0.11	149.99	81.60	J130	0.11	149.49	80.90	J130	0.11	149.48	80.89
J131	0.11	149.99	81.57	J131	0.11	149.49	80.86	J131	0.11	149.48	80.84
J132	0.11	149.99	81.41	J132	0.11	149.49	80.70	J132	0.11	149.48	80.69
J133	0.11	149.99	81.50	J133	0.11	149.49	80.78	J133	0.11	149.48	80.77
J134	0.11	149.99	81.62	J134	0.11	149.49	80.91	J134	0.11	149.48	80.90
J135	0.11	149.99	81.72	J135	0.11	149.49	81.01	J135	0.11	149.48	81.00
J136	0.11	149.99	81.69	J136	0.11	149.49	80.88	J136	0.11	149.48	80.87
J137	0.11	149.99	81.51	J137	0.11	149.49	80.60	J137	0.11	149.48	80.79
J14	0.11	149.99	81.63	J14	0.11	149.49	80.92	J14	0.11	149.48	80.91
J15	0.07	149.99	81.28	J15	0.07	149.49	80.57	J15	0.07	149.48	80.55
J153	0.15	149.99	80.76	J153	0.15	149.49	80.05	J153	0.15	149.48	80.04
J154	0.11	149.99	81.35	J154	0.11	149.49	80.64	J154	0.11	149.48	80.63
J155	0.11	149.99	81.47	J155	0.11	149.49	80.76	J155	0.11	149.48	80.74
J156	0.00	149.99	81.60	J156	0.00	149.49	80.96	J156	0.00	149.48	80.95
J158	0.09	149.99	81.72	J158	0.09	149.49	81.01	J158	0.09	149.48	81.00
J16	0.07	149.99	81.83	J16	0.07	149.49	80.72	J16	0.07	149.48	80.71
J162	0.00	149.99	80.84	J162	0.00	149.49	80.13	J162	0.00	149.48	80.12
J164	0.00	149.99	80.91	J164	0.00	149.49	80.20	J164	0.00	149.48	80.19
J166	0.00	149.99	80.73	J166	0.00	149.49	80.02	J166	0.00	149.48	80.01
J168	0.00	149.99	81.00	J168	0.00	149.49	80.68	J168	0.00	149.48	80.67
J17	0.07	149.99	81.26	J17	0.07	149.49	80.55	J17	0.07	149.48	80.54
J170	0.00	149.99	80.50	J170	0.00	149.49	79.79	J170	0.00	149.48	79.78
J172	0.00	149.99	80.84	J172	0.00	149.49	80.13	J172	0.00	149.48	80.12
J174	0.15	149.99	81.01	J174	0.15	149.49	80.30	J174	0.15	149.48	80.29
J176	0.15	149.99	81.13	J176	0.15	149.49	80.42	J176	0.15	149.48	80.40
J178	0.05	149.99	81.05	J178	0.05	149.49	80.85	J178	0.05	149.48	80.82
J180	0.08	149.99	81.04	J180	0.08	149.49	80.63	J180	0.08	149.48	80.62
J182	0.08	149.99	81.67	J182	0.08	149.49	80.96	J182	0.08	149.48	80.95
J184	0.08	149.99	81.72	J184	0.08	149.49	81.01	J184	0.08	149.48	81.00
J186	0.08	149.99	81.24	J186	0.08	149.49	80.53	J186	0.08	149.48	80.52
J188	0.00	149.99	80.80	J188	0.00	149.49	80.19	J188	0.00	149.48	80.18
J189	0.01	149.99	80.83	J189	0.01	149.49	80.59	J189	0.01	149.48	80.58
J21	0.10	149.99	81.14	J21	0.10	149.49	80.43	J21	0.10	149.48	80.42
J22	0.10	149.99	81.20	J22	0.10	149.49	80.49	J22	0.10	149.48	80.48
J23	0.10	149.99	81.33	J23	0.10	149.49	80.62	J23	0.10	149.48	80.60
J24	0.10	149.99	81.46	J24	0.10	149.49	80.74	J24	0.10	149.48	80.73
J25	0.10	149.99	81.40	J25	0.10	149.49	80.65	J25	0.10	149.48	80.62
J26	0.19	149.99	81.44	J26	0.19	149.49	80.73	J26	0.19	149.48	80.72
J27	0.10	149.99	81.57	J27	0.10	149.49	80.86	J27	0.10	149.48	80.85
J28	0.10	149.99	81.50	J28	0.10	149.49	80.79	J28	0.10	149.48	80.78
J29	0.10	149.99	81.50	J29	0.10	149.49	80.79	J29	0.10	149.48	80.78
J30	0.07	149.99	81.43	J30	0.07	149.49	80.72	J30	0.07	149.48	80.71
J31	0.07	149.99	81.60	J31	0.07	149.49	80.81	J31	0.07	149.48	80.80
J32	0.07	149.99	81.46	J32	0.07	149.49	80.75	J32	0.07	149.48	80.74
J33	0.07	149.99	81.69	J33	0.07	149.49	80.98	J33	0.07	149.48	80.96
J34	0.07	149.99	81.56	J34	0.07	149.49	80.85	J34	0.07	149.48	80.84
J35	0.07	149.99	81.52	J35	0.07	149.49	80.81	J35	0.07	149.48	80.79
J36	0.07	149.99	81.65	J36	0.07	149.49	80.94	J36	0.07	149.48	80.92
J37	0.08	149.99	81.66	J37	0.08	149.49	80.40	J37	0.08	149.48	80.39
J38	0.08	149.99	81.24	J38	0.08	149.49	80.53	J38	0.08	149.48	80.52
J39	0.08	149.99	81.24	J39	0.08	149.49	80.53	J39	0.08	149.48	80.52
J40	0.11	150.00	81.11	J40	0.11	149.50	80.40	J40	0.11	149.49	80.40
J41	0.11	149.99	81.30	J41	0.11	149.49	80.59	J41	0.11	149.48	80.57
J42	0.11	149.99	81.34	J42	0.11	149.49	80.63	J42	0.11	149.48	80.62
J43	0.11	149.99	81.20	J43	0.11	149.49	80.41	J43	0.11	149.48	80.40
J44	0.11	149.99	81.46	J44	0.11	149.49	80.64	J44	0.11	149.48	80.63
J45	0.11</										

Option A - 2 Connections - Buildout (Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E) + Phase 4 + Jock River)				Option A - 2 Connections with Upgrades on Danson Gardens Grv - Buildout (Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E) + Phase 4 + Jock River)				Option B - 3 Connections - Buildout (Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E) + Phase 4 + Jock River)			
Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)
Maximum	0.15	150.00	81.37	Maximum	0.15	149.50	81.16	Maximum	0.15	149.49	81.14
Minimum	0.00	149.98	80.31	Minimum	0.00	149.48	79.60	Minimum	0.00	149.47	79.58
J01	0.07	149.99	80.31	J01	0.07	149.49	79.60	J01	0.07	149.48	79.58
J02	0.00	149.99	80.92	J02	0.00	149.49	80.21	J02	0.00	149.48	80.19
J03	0.07	149.99	81.05	J03	0.07	149.49	80.34	J03	0.07	149.48	80.39
J06	0.07	149.99	81.56	J06	0.07	149.49	80.85	J06	0.07	149.48	80.93
J07	0.11	149.99	81.72	J07	0.11	149.49	81.00	J07	0.11	149.48	80.99
J08	0.11	149.99	81.59	J08	0.11	149.49	80.88	J08	0.11	149.48	80.86
J09	0.11	149.99	81.08	J09	0.11	149.49	80.37	J09	0.11	149.48	80.35
J10	0.11	149.99	81.33	J10	0.11	149.49	80.62	J10	0.11	149.48	80.61
J100	0.15	149.98	80.90	J100	0.15	149.48	80.00	J100	0.15	149.47	80.05
J101	0.15	149.98	80.94	J101	0.15	149.48	80.29	J101	0.15	149.47	80.11
J102	0.15	149.95	80.82	J102	0.15	149.48	80.11	J102	0.15	149.47	80.10
J103	0.15	149.98	80.67	J103	0.15	149.48	79.96	J103	0.15	149.47	79.94
J109	0.11	149.99	80.95	J109	0.11	149.49	80.24	J109	0.11	149.48	80.50
J11	0.11	149.99	81.22	J11	0.11	149.49	81.50	J11	0.11	149.47	81.59
J111	0.11	149.98	81.11	J111	0.11	149.48	80.45	J111	0.11	149.47	80.45
J112	0.11	149.98	81.09	J112	0.11	149.48	80.38	J112	0.11	149.47	80.36
J113	0.11	149.98	81.01	J113	0.11	149.48	80.30	J113	0.11	149.47	80.28
J114	0.11	149.98	80.86	J114	0.11	149.48	80.15	J114	0.11	149.47	80.14
J115	0.11	149.98	80.84	J115	0.11	149.48	80.12	J115	0.11	149.47	80.11
J116	0.11	149.98	80.88	J116	0.11	149.48	80.17	J116	0.11	149.47	80.15
J117	0.11	149.98	81.17	J117	0.11	149.48	80.47	J117	0.11	149.47	80.39
J118	0.11	149.98	81.09	J118	0.11	149.48	80.38	J118	0.11	149.47	80.36
J119	0.11	149.98	81.22	J119	0.11	149.48	80.51	J119	0.11	149.47	80.49
J12	0.11	150.00	81.08	J12	0.11	149.50	80.37	J12	0.11	149.49	80.36
J120	0.11	149.98	81.22	J120	0.11	149.48	80.51	J120	0.11	149.47	80.49
J121	0.11	149.98	81.02	J121	0.11	149.48	80.31	J121	0.11	149.47	80.29
J122	0.11	149.98	80.93	J122	0.11	149.48	80.32	J122	0.11	149.47	80.32
J124	0.11	149.95	81.15	J124	0.11	149.48	80.44	J124	0.11	149.47	80.42
J125	0.11	149.98	81.33	J125	0.11	149.48	80.62	J125	0.11	149.47	80.61
J128	0.00	149.98	81.69	J128	0.00	149.48	80.98	J128	0.00	149.47	80.96
J129	0.11	149.98	81.68	J129	0.11	149.48	80.95	J129	0.11	149.47	80.93
J130	0.11	149.98	81.65	J130	0.11	149.48	80.90	J130	0.11	149.47	80.72
J131	0.11	149.98	81.55	J131	0.11	149.48	80.85	J131	0.11	149.47	80.63
J132	0.11	149.98	81.40	J132	0.11	149.48	80.69	J132	0.11	149.47	80.68
J133	0.11	149.98	81.49	J133	0.11	149.48	80.78	J133	0.11	149.47	80.76
J134	0.11	149.98	81.62	J134	0.11	149.48	80.91	J134	0.11	149.47	80.89
J135	0.11	149.98	81.72	J135	0.11	149.48	81.01	J135	0.11	149.47	80.99
J136	0.11	149.98	81.59	J136	0.11	149.48	80.88	J136	0.11	149.47	80.86
J137	0.11	149.98	81.37	J137	0.11	149.48	80.17	J137	0.11	149.47	80.15
J14	0.11	149.98	81.63	J14	0.11	149.48	80.91	J14	0.11	149.47	80.90
J15	0.07	149.99	81.27	J15	0.07	149.49	80.56	J15	0.07	149.48	80.54
J152	0.11	149.99	81.76	J152	0.11	149.49	81.05	J152	0.11	149.48	81.03
J153	0.15	149.98	80.75	J153	0.15	149.48	80.04	J153	0.15	149.47	80.02
J154	0.11	149.98	81.35	J154	0.11	149.48	80.64	J154	0.11	149.47	80.62
J155	0.11	149.98	81.65	J155	0.11	149.48	80.93	J155	0.11	149.47	80.73
J156	0.00	149.98	81.22	J156	0.00	149.48	80.51	J156	0.00	149.47	80.49
J158	0.00	149.98	81.72	J158	0.00	149.48	81.01	J158	0.00	149.47	80.99
J16	0.07	149.99	81.43	J16	0.07	149.49	80.72	J16	0.07	149.48	80.70
J162	0.00	149.98	80.84	J162	0.00	149.48	80.13	J162	0.00	149.47	80.11
J164	0.00	149.98	80.91	J164	0.00	149.48	80.20	J164	0.00	149.47	80.18
J166	0.00	149.98	80.95	J166	0.00	149.48	80.26	J166	0.00	149.47	80.20
J168	0.00	149.98	81.01	J168	0.00	149.48	80.30	J168	0.00	149.47	80.28
J17	0.07	149.99	81.25	J17	0.07	149.49	80.54	J17	0.07	149.47	80.53
J170	0.00	149.98	80.49	J170	0.00	149.48	79.78	J170	0.00	149.47	79.77
J172	0.00	149.98	80.84	J172	0.00	149.48	80.13	J172	0.00	149.47	80.11
J174	0.15	149.98	81.01	J174	0.15	149.48	80.30	J174	0.15	149.47	80.28
J176	0.15	149.98	81.12	J176	0.15	149.48	80.41	J176	0.15	149.47	80.39
J178	0.05	149.98	81.05	J178	0.05	149.48	80.35	J178	0.05	149.47	80.31
J18	0.07	149.99	81.04	J18	0.07	149.49	80.33	J18	0.07	149.47	80.27
J180	0.08	149.98	81.55	J180	0.08	149.48	80.84	J180	0.08	149.47	80.82
J182	0.08	149.98	81.66	J182	0.08	149.48	80.95	J182	0.08	149.47	80.94
J184	0.08	149.98	81.72	J184	0.08	149.48	81.01	J184	0.08	149.47	80.99
J186	0.08	149.98	81.23	J186	0.08	149.48	80.52	J186	0.08	149.47	80.45
J188	0.08	149.98	81.38	J188	0.08	149.48	80.53	J188	0.08	149.47	80.51
J189	0.08	149.98	81.23	J189	0.08	149.48	80.52	J189	0.08	149.47	80.49
J190	0.00	149.98	80.86	J190	0.00	149.48	80.00	J190	0.00	149.47	80.00
J20	0.10	149.98	81.29	J20	0.10	149.48	80.58	J20	0.10	149.47	80.57
J21	0.10	149.98	81.14	J21	0.10	149.48	80.43	J21	0.10	149.47	80.41
J22	0.10	149.98	81.19	J22	0.10	149.48	80.48	J22	0.10	149.47	80.47
J23	0.10	149.98	81.32	J23	0.10	149.48	80.61	J23	0.10	149.47	80.59
J24	0.10	149.98	81.34	J24	0.10	149.48	80.64	J24	0.10	149.47	80.62
J25	0.10	149.98	81.34	J25	0.10	149.48	80.62	J25	0.10	149.47	80.61
J26	0.10	149.98	81.44	J26	0.10	149.48	80.72	J26	0.10	149.47	80.71
J27	0.10	149.98	81.56	J27	0.10	149.48	80.85	J27	0.10	149.47	80.84
J28	0.10	149.99	81.49	J28	0.10	149.48	80.78	J28	0.10	149.47	80.76
J29	0.10	149.98	81.29	J29	0.10	149.48	80.49	J29	0.10	149.47	80.37
J30	0.07	149.99	81.55	J30	0.07	149.49	80.70	J30	0.07	149.47	80.69
J31	0.11	149.99	81.51	J31	0.11	149.49	80.55	J31	0.11	149.48	80.55
J32	0.07	149.99	81.45	J32	0.07	149.49	80.74	J32	0.07	149.47	80.72
J33	0.07	149.99	81.68	J33	0.07	149.49	80.97	J33	0.07	149.48	80.95
J34	0.07	149.99	81.55	J34	0.07	149.49	80.84	J34	0.07	149.47	80.83
J35	0.07	149.99	81.51	J35	0.07	149.49	80.80	J35	0.07	149.48	80.78
J36	0.07	149.99	81.55	J36	0.07	149.49	80.85	J36	0.07	149.47	80.81
J37	0.07	149.99	81.55	J37	0.07	149.49	80.85	J37	0.07	149.47	80.80
J38	0.08	149.98	81.23	J38	0.08	149.48	80.52	J38	0.08	149.47	80.49
J39	0.08	149.98	81.39	J39	0.08	149.48	80.68	J39	0.08	149.47	80.66
J40	0.11	149.99	81.11	J40	0.11	149.49	80.94	J40	0.11	149.47	80.93
J41	0.11	149.98	81.29	J41	0.11	149.48	80.58	J41	0.11		

Option A - 2 Connections - Phase 2 (2A, 2B, 2C)				Option A - 2 Connections with Upgrades on Danson Gardens Grv - Phase 2 (2A, 2B, 2C)				Option B - 3 Connections - Phase 2 (2A, 2B, 2C)			
Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)
Maximum	0.58	144.12	73.34	Maximum	0.58	144.09	73.31	Maximum	0.58	144.01	73.15
Minimum	0.00	144.09	71.96	Minimum	0.00	144.06	71.90	Minimum	0.00	143.93	71.81
J01	0.39	144.12	71.96	J01	0.39	144.08	71.90	J01	0.39	144.01	71.81
J02	0.41	144.10	72.00	J02	0.41	144.08	72.51	J02	0.41	143.99	72.38
J05	0.39	144.10	73.05	J05	0.39	144.08	73.05	J05	0.39	143.97	72.83
J06	0.39	144.10	73.18	J06	0.39	144.08	73.15	J06	0.39	143.96	72.99
J07	0.58	144.10	73.34	J07	0.58	144.08	73.31	J07	0.58	143.96	73.15
J08	0.58	144.10	73.21	J08	0.58	144.08	73.18	J08	0.58	143.97	73.02
J09	0.58	144.10	72.70	J09	0.58	144.08	72.67	J09	0.58	143.97	72.51
J10	0.58	144.10	72.95	J10	0.58	144.08	72.93	J10	0.58	143.97	72.77
J11	0.58	144.10	72.70	J11	0.58	144.08	72.65	J11	0.58	143.97	72.66
J12	0.58	144.10	72.70	J12	0.58	144.08	72.68	J12	0.58	143.98	72.52
J15	0.39	144.10	72.90	J15	0.39	144.07	72.86	J15	0.39	143.96	72.70
J158	0.00	144.09	73.33	J158	0.00	144.06	73.30	J158	0.00	143.93	73.11
J16	0.39	144.10	73.05	J16	0.39	144.07	73.01	J16	0.39	143.95	72.85
J17	0.39	144.09	72.88	J17	0.39	144.07	72.84	J17	0.39	143.95	72.67
J18	0.44	144.09	72.60	J18	0.44	144.06	72.58	J18	0.44	143.93	72.47
J19	0.39	144.09	72.66	J19	0.39	144.07	72.62	J19	0.39	143.94	72.45
J180	0.44	144.09	73.16	J180	0.44	144.06	73.13	J180	0.44	143.93	72.94
J182	0.44	144.09	73.28	J182	0.44	144.06	73.24	J182	0.44	143.93	73.05
J184	0.44	144.09	73.33	J184	0.44	144.06	73.30	J184	0.44	143.93	73.11
J186	0.44	144.09	72.85	J186	0.44	144.06	72.81	J186	0.44	143.93	72.62
J20	0.56	144.09	72.45	J19	0.56	144.06	72.41	J19	0.56	143.94	72.23
J21	0.56	144.09	72.45	J21	0.56	144.06	72.38	J21	0.56	143.93	72.09
J22	0.56	144.09	72.81	J22	0.56	144.06	72.77	J22	0.56	143.93	72.53
J23	0.56	144.09	72.94	J23	0.56	144.06	72.90	J23	0.56	143.93	72.72
J24	0.56	144.09	73.07	J24	0.56	144.06	73.03	J24	0.56	143.93	72.84
J25	0.56	144.09	72.95	J25	0.56	144.06	72.92	J25	0.56	143.93	72.73
J26	0.56	144.09	73.06	J26	0.56	144.06	73.03	J26	0.56	143.93	72.83
J27	0.56	144.09	73.18	J27	0.56	144.06	73.14	J27	0.56	143.93	72.86
J28	0.56	144.09	73.11	J28	0.56	144.06	73.07	J28	0.56	143.94	72.89
J29	0.56	144.09	73.11	J29	0.56	144.06	73.07	J29	0.56	143.94	72.89
J30	0.39	144.09	73.04	J30	0.39	144.06	73.00	J30	0.39	143.94	72.83
J31	0.39	144.09	73.17	J31	0.39	144.06	73.13	J31	0.39	143.94	72.96
J32	0.39	144.09	73.17	J32	0.39	144.06	73.12	J32	0.39	143.94	72.96
J33	0.39	144.09	73.30	J33	0.39	144.07	73.26	J33	0.39	143.95	73.09
J34	0.39	144.09	73.17	J34	0.39	144.07	73.14	J34	0.39	143.95	72.97
J35	0.39	144.10	73.13	J35	0.39	144.07	73.10	J35	0.39	143.95	72.93
J36	0.39	144.10	73.27	J36	0.39	144.07	73.23	J36	0.39	143.96	73.07
J37	0.44	144.09	72.72	J37	0.44	144.06	72.69	J37	0.44	143.93	72.50
J38	0.44	144.09	72.88	J38	0.44	144.06	72.81	J38	0.44	143.93	72.62
J39	0.44	144.09	72.85	J39	0.44	144.06	72.81	J39	0.44	143.93	72.62
J40	0.58	144.10	72.73	J40	0.58	144.09	72.71	J40	0.58	143.97	72.55
J46	0.58	144.10	72.77	J46	0.58	144.08	72.75	J46	0.58	143.97	72.59
J48	0.58	144.10	72.81	J48	0.58	144.08	72.79	J48	0.58	143.97	72.63
J75	0.56	144.09	72.88	J75	0.56	144.06	72.84	J75	0.56	143.93	72.66
J76	0.56	144.09	73.04	J76	0.56	144.06	73.02	J76	0.56	143.93	72.83
J77	0.56	144.09	72.77	J77	0.56	144.06	72.77	J77	0.56	143.94	72.55
J78	0.39	144.09	72.93	J78	0.39	144.06	72.89	J78	0.39	143.94	72.71
J79	0.39	144.09	73.01	J79	0.39	144.07	72.98	J79	0.39	143.94	72.81
J94	0.44	144.09	73.11	J94	0.44	144.06	73.07	J94	0.44	143.93	72.88
J95	0.44	144.09	73.33	J95	0.44	144.06	73.30	J95	0.44	143.93	73.11
J96	0.44	144.09	73.21	J96	0.44	144.06	73.17	J96	0.44	143.93	72.98
J97	0.44	144.09	72.96	J97	0.44	144.06	72.93	J97	0.44	143.93	72.74
J98	0.00	144.09	73.14	J98	0.00	144.06	73.10	J98	0.00	143.93	72.91

Option A - 2 Connections - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E)				Option A - 2 Connections with Upgrades on Danson Gardens Grv - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E)				Option B - 3 Connections - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E)			
Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)
Maximum	0.83	144.04	73.19	Maximum	0.83	144.06	73.25	Maximum	0.83	143.88	72.89
Minimum	0.00	143.94	71.84	Minimum	0.00	143.98	71.85	Minimum	0.00	143.64	71.58
J01	0.39	144.04	71.84	J01	0.39	144.04	71.85	J01	0.39	143.85	71.58
J02	0.00	144.00	72.42	J02	0.00	144.00	72.42	J02	0.00	143.81	72.13
J05	0.39	144.00	72.42	J05	0.39	144.03	72.44	J05	0.39	143.77	72.58
J06	0.39	144.00	73.04	J06	0.39	144.03	73.09	J06	0.39	143.77	72.71
J07	0.58	144.00	73.19	J07	0.58	144.04	73.25	J07	0.58	143.78	72.89
J08	0.58	144.00	73.06	J08	0.58	144.04	73.13	J08	0.58	143.80	72.78
J09	0.58	144.00	72.55	J09	0.58	144.04	72.62	J09	0.58	143.81	72.28
J10	0.58	144.00	72.81	J10	0.58	144.08	72.88	J10	0.58	143.82	72.56
J100	0.58	143.94	72.00	J100	0.58	143.98	72.20	J100	0.83	143.65	71.77
J101	0.83	143.94	72.81	J101	0.83	143.98	73.10	J101	0.83	143.65	71.93
J102	0.83	143.94	72.24	J102	0.83	143.98	72.29	J102	0.83	143.64	71.81
J103	0.83	143.94	72.08	J103	0.83	143.98	72.13	J103	0.83	143.64	71.65
J11	0.58	144.00	72.70	J11	0.58	144.05	72.77	J11	0.58	143.84	72.47
J12	0.58	144.00	72.55	J12	0.58	144.06	72.65	J12	0.58	143.88	72.38
J15	0.39	143.95	72.42	J15	0.39	143.98	72.55	J15	0.39	143.74	72.59
J153	0.83	143.95	72.17	J153	0.83	143.98	72.22	J153	0.83	143.65	71.75
J158	0.00	143.95	73.13	J158	0.00	143.98	73.18	J158	0.00	143.64	72.71
J16	0.39	143.98	72.88	J16	0.39	144.01	72.93	J16	0.39	143.72	72.51
J17	0.39	143.97	72.70	J17	0.39	144.00	72.74	J17	0.39	143.69	72.30
J174	0.83	143.94	72.42	J174	0.83	143.98	72.47	J174	0.83	143.64	72.00
J176	0.83	143.95	72.55	J176	0.83	143.98	72.59	J176	0.83	143.64	72.11
J178	0.44	143.95	72.75	J178	0.44	143.98	72.80	J178	0.44	143.64	72.32
J18	0.39	143.98	72.47	J18	0.39	143.99	72.52	J18	0.39	143.67	72.05
J180	0.44	143.95	72.96	J180	0.44	143.98	73.01	J180	0.44	143.64	72.54
J182	0.44	143.95	73.08	J182	0.44	143.98	73.13	J182	0.44	143.64	72.65
J184	0.44	143.95	73.13	J184	0.44	143.98	73.18	J184	0.44	143.64	72.71
J186	0.44	143.95	72.65	J186	0.44	143.98	72.70	J186	0.44	143.64	72.22
J19	0.58	143.95	72.19	J19	0.58	143.99	72.29	J19	0.58	143.65	71.83
J20	0.58	143.95	72.73	J20	0.58	143.99	72.77	J20	0.58	143.66	72.20
J21	0.56	143.95	72.56	J21	0.56	143.98	72.61	J21	0.56	143.66	72.14
J22	0.56	143.95	72.61	J22	0.56	143.98	72.66	J22	0.56	143.65	72.20
J23	0.56	143.95	72.74	J23	0.56	143.98	72.79	J23	0.56	143.66	72.33
J24	0.56	143.95	72.87	J24	0.56	143.98	72.92	J24	0.56	143.66	72.46
J25	0.56	143.95	72.97	J25	0.56	143.98	72.98	J25	0.56	143.66	72.55
J26	0.56	143.95	72.88	J26	0.56	143.99	72.91	J26	0.56	143.66	72.45
J27	0.56	143.95	72.99	J27	0.56	143.99	73.04	J27	0.56	143.67	72.58
J28	0.56	143.95	72.92	J28	0.56	143.99	72.97	J28	0.56	143.67	72.52
J29	0.56	143.95	72.92	J29	0.56	143.99	72.97	J29	0.56	143.68	72.52
J30	0.39	143.96	72.86	J30	0.39	143.99	72.90	J30	0.39	143.68	72.46
J31	0.39	143.95	72.89	J31	0.39	143.99	73.01	J31	0.39	143.69	72.80
J32	0.39	143.97	72.89	J32	0.39	144.00	73.04	J32	0.39	143.70	72.51
J33	0.39	143.97	73.13	J33	0.39	144.00	73.17	J33	0.39	143.71	72.75
J34	0.39	143.97	73.00	J34	0.39	144.01	73.05	J34	0.39	143.72	72.64
J35	0.39	143.98	72.97	J35	0.39	144.02	73.02	J35	0.39	143.73	72.62
J36	0.39	143.99	73.11	J36	0.39	144.02	73.16	J36	0.39	143.75	72.77
J37	0.44	143.95	72.47	J37	0.44	143.98	72.57	J37	0.44	143.85	72.10
J38	0.44	143.95	72.68	J38	0.44	143.98	72.78	J38	0.44	143.85	72.23
J39	0.44	143.95	72.65	J39	0.44	143.98	72.70	J39	0.44	143.85	72.22
J40	0.58	144.00	72.58	J40	0.58	144.06	72.68	J40	0.58	143.87	72.40
J46	0.58	144.00	72.63	J46	0.58	144.06	72.71	J46	0.58	143.86	72.43
J48	0.58	144.00	72.67	J48	0.58	144.05	72.75	J48	0.58	143.84	72.45
J75	0.56	143.95	72.69	J75	0.56	143.98	72.73	J75	0.56	143.86	72.27
J76	0.56	143.95	72.70	J76	0.56	143.99	72.76	J76	0.56	143.86	72.45
J77	0.56	143.95	72.88	J77	0.56	143.99	72.83	J77	0.56	143.67	72.17
J78	0.39	143.96	72.74	J78	0.39	143.99	72.79	J78	0.39	143.68	72.34
J79	0.39	143.97	72.84	J79	0.39	144.00	72.89	J79	0.39	143.70	72.45
J80	0.83	143.94	72.38	J80	0.83	143.98	72.43	J80	0.83	143.65	71.96
J81	0.83	143.95	72.20	J81	0.83	143.98	72.24	J81	0.83	143.65	71.77
J82	0.83	143.95	72.26	J82	0.83	143.98	72.32	J82	0.83	143.65	71.52
J83	0.83	143.95	72.45	J83	0.83	143.98	72.50	J83	0.83	143.65	72.03
J84	0.80	143.95	72.33	J84	0.80	143.98	72.38	J84	0.80	143.65	71.91
J85	0.80	143.95	72.42	J85	0.80	143.98	72.47	J85	0.80	143.65	72.01
J86	0.80	143.95	72.64	J86	0.80	143.98	72.69	J86	0.80	143.65	72.22
J87	0.80	143.95	72.60	J87	0.80	143.98	72.64	J87	0.80	143.65	72.18
J88	0.80	143.95	72.68	J88	0.80	143.98	72.58	J88	0.80	143.65	72.04
J89	0.80	143.95	72.46	J89	0.80	143.98	72.51	J89	0.80	143.65	72.04
J90	0.83	143.95	72.29	J90	0.83	143.98	72.33	J90	0.83	143.65	71.87
J91	0.83	143.95	72.58	J91	0.83	143.98	72.63	J91	0.83	143.65	72.16
J92	0.83	143.95	72.40	J92	0.83	143.98	72.44	J92	0.83	143.65	71.97
J93	0.83	143.94	72.28	J93	0.83	143.98	72.33	J93	0.83	143.65	71.86
J94	0.44	143.95	72.19	J94	0.44	143.98	72.26	J94	0.44	143.65	72.48
J95	0.44	143.95	72.13	J95	0.44	143.98	72.20	J95	0.44	143.65	72.41
J96	0.44	143.95	73.01	J96	0.44	143.98	73.05	J96	0.44	143.64	72.58
J97	0.44	143.95	72.76	J97	0.44	143.98	72.81	J97	0.44	143.64	72.34
J98	0.00	143.95	72.93	J98	0.00	143.98	72.98	J98	0.00	143.64	72.51

Option A - 2 Connections - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E) + Phase 4				Option A - 2 Connections with Upgrades on Danson Gardens Grv - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E) + Phase 4				Option B - 3 Connections - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E) + Phase 4			
Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)
Maximum	0.83	143.99	73.12	Maximum	0.83	144.03	73.15	Maximum	0.83	143.84	72.34
Minimum	0.00	143.78	71.69	Minimum	0.00	143.79	71.71	Minimum	0.00	142.51	69.91
J01	0.39	143.99	71.77	J01	0.39	143.98	71.76	J01	0.39	143.49	71.07
J02	0.00	143.90	72.35	J02	0.00	143.97	72.35	J02	0.00	143.36	71.49
J05	0.39	143.94	72.36	J05	0.39	143.96	72.35	J05	0.39	143.36	71.64
J06	0.39	143.94	72.96	J06	0.39	143.96	72.98	J06	0.39	143.26	71.98
J07	0.58	143.94	73.12	J07	0.58	143.97	73.15	J07	0.58	143.34	72.26
J08	0.58	143.95	72.99	J08	0.58	143.97	73.03	J08	0.58	143.41	72.24
J09	0.58	143.95	72.49	J09	0.58	143.98	72.53	J09	0.58	143.49	71.83
J10	0.58	143.95	72.75	J10	0.58	143.99	72.80	J10	0.58	143.57	72.20
J10	0.58	143.95	71.60	J10	0.58	143.99	72.00	J10	0.58	142.69	70.26
J101	0.83	143.80	72.14	J101	0.83	143.81	72.15	J101	0.83	142.50	70.42
J102	0.83	143.79	72.02	J102	0.83	143.81	72.05	J102	0.83	142.57	70.28
J103	0.83	143.79	71.87	J103	0.83	143.81	71.88	J103	0.83	142.56	70.12
J109	0.59	143.79	72.14	J109	0.59	143.80	72.16	J109	0.59	142.53	70.36
J11	0.58	143.98	72.64	J11	0.58	144.00	72.70	J11	0.58	143.64	72.19
J110	0.59	143.98	72.60	J110	0.59	143.99	72.63	J110	0.59	142.53	70.53
J111	0.59	143.78	72.38	J111	0.59	143.80	72.40	J111	0.59	142.53	70.59
J112	0.59	143.78	72.27	J112	0.59	143.80	72.30	J112	0.59	142.52	70.48
J113	0.59	143.78	72.19	J113	0.59	143.79	72.21	J113	0.59	142.51	70.39
J114	0.59	143.78	72.04	J114	0.59	143.79	72.07	J114	0.59	142.51	70.24
J115	0.59	143.78	72.02	J115	0.59	143.79	72.04	J115	0.59	142.51	70.21
J116	0.59	143.78	72.00	J116	0.59	143.79	72.05	J116	0.59	142.51	70.26
J117	0.59	143.78	72.19	J117	0.59	143.79	72.21	J117	0.59	142.51	70.39
J119	0.59	143.78	72.40	J119	0.59	143.79	72.42	J119	0.59	142.51	70.60
J120	0.59	143.78	72.40	J120	0.59	143.79	72.42	J120	0.59	142.51	70.60
J121	0.59	143.78	72.20	J121	0.59	143.79	72.22	J121	0.59	142.51	70.40
J122	0.00	143.80	72.22	J122	0.00	143.80	72.22	J122	0.00	142.51	70.24
J123	0.59	143.78	72.19	J123	0.59	143.79	72.21	J123	0.59	142.51	70.38
J124	0.59	143.78	72.33	J124	0.59	143.79	72.35	J124	0.59	142.51	70.53
J125	0.59	143.78	72.51	J125	0.59	143.79	72.54	J125	0.59	142.51	70.71
J128	0.00	143.78	72.88	J128	0.00	143.80	72.90	J128	0.00	142.52	71.08
J129	0.59	143.78	72.85	J129	0.59	143.80	72.87	J129	0.59	142.52	71.05
J130	0.59	143.78	72.60	J130	0.59	143.80	72.60	J130	0.59	142.52	70.84
J131	0.59	143.78	72.75	J131	0.59	143.80	72.77	J131	0.59	142.52	70.95
J132	0.59	143.78	72.59	J132	0.59	143.80	72.61	J132	0.59	142.52	70.80
J133	0.59	143.78	72.67	J133	0.59	143.80	72.69	J133	0.59	142.51	70.87
J134	0.59	143.78	72.80	J134	0.59	143.79	72.82	J134	0.59	142.51	71.00
J135	0.59	143.78	72.90	J135	0.59	143.79	72.92	J135	0.59	142.51	71.09
J136	0.59	143.78	72.68	J136	0.59	143.80	72.70	J136	0.59	142.51	70.87
J137	0.59	143.78	72.68	J137	0.59	143.79	72.70	J137	0.59	142.51	70.88
J14	0.59	143.78	72.81	J14	0.59	143.79	72.83	J14	0.59	142.51	71.00
J15	0.39	143.91	72.63	J15	0.39	143.93	72.65	J15	0.39	143.12	71.51
J153	0.83	143.82	71.99	J153	0.83	143.83	72.01	J153	0.83	142.71	70.41
J154	0.59	143.78	72.53	J154	0.59	143.80	72.56	J154	0.59	142.52	70.73
J155	0.59	143.78	72.68	J155	0.59	143.80	72.69	J155	0.59	142.51	70.84
J156	0.00	143.78	72.40	J156	0.00	143.80	72.40	J156	0.00	142.51	70.60
J158	0.00	143.78	72.92	J158	0.00	143.81	72.94	J158	0.00	142.53	71.12
J16	0.39	143.89	72.76	J16	0.39	143.90	72.78	J16	0.39	142.52	71.52
J162	0.00	143.79	72.03	J162	0.00	143.80	72.05	J162	0.00	142.54	70.25
J164	0.00	143.79	72.10	J164	0.00	143.80	72.12	J164	0.00	142.54	70.32
J166	0.00	143.79	71.92	J166	0.00	143.80	71.94	J166	0.00	142.54	70.13
J168	0.00	143.79	72.05	J168	0.00	143.80	72.06	J168	0.00	142.54	70.42
J17	0.39	143.87	72.55	J17	0.38	143.88	72.57	J17	0.39	142.50	71.18
J170	0.00	143.79	71.69	J170	0.00	143.80	71.71	J170	0.00	142.54	69.91
J172	0.00	143.79	72.03	J172	0.00	143.81	72.05	J172	0.00	142.54	70.26
J174	0.83	143.79	72.20	J174	0.83	143.81	72.23	J174	0.83	142.55	70.43
J176	0.83	143.79	72.32	J176	0.83	143.81	72.34	J176	0.83	142.54	70.54
J178	0.44	143.87	72.38	J178	0.44	143.89	72.55	J178	0.44	142.51	70.75
J18	0.39	143.84	72.31	J18	0.39	143.86	72.35	J18	0.39	142.51	70.80
J180	0.44	143.79	72.75	J180	0.44	143.81	72.77	J180	0.44	142.53	70.95
J182	0.44	143.79	72.86	J182	0.44	143.81	72.88	J182	0.44	142.53	71.06
J184	0.44	143.79	72.92	J184	0.44	143.81	72.94	J184	0.44	142.52	71.11
J186	0.44	143.79	72.43	J186	0.44	143.81	72.45	J186	0.44	142.54	70.65
J188	0.00	143.79	71.88	J188	0.00	143.80	72.00	J188	0.00	142.54	70.29
J19	0.56	143.63	72.68	J19	0.56	143.85	72.68	J19	0.56	142.56	70.55
J20	0.56	143.83	72.54	J20	0.56	143.84	72.56	J20	0.56	142.73	70.98
J21	0.56	143.82	72.37	J21	0.56	143.84	72.40	J21	0.56	142.72	70.81
J22	0.56	143.81	72.42	J22	0.56	143.83	72.44	J22	0.56	142.71	70.84
J23	0.56	143.82	72.56	J23	0.56	143.83	72.58	J23	0.56	142.73	71.01
J24	0.56	143.82	72.69	J24	0.56	143.84	72.71	J24	0.56	142.74	71.16
J25	0.56	143.82	72.62	J25	0.56	143.84	72.65	J25	0.56	142.74	71.07
J26	0.56	143.83	72.68	J26	0.56	143.84	72.68	J26	0.56	142.78	71.19
J27	0.56	143.83	72.82	J27	0.56	143.85	72.84	J27	0.56	142.80	71.34
J28	0.56	143.84	72.75	J28	0.56	143.85	72.77	J28	0.56	142.82	71.31
J29	0.56	143.84	72.76	J29	0.56	143.86	72.78	J29	0.56	142.85	71.35
J30	0.39	143.85	72.70	J30	0.39	143.87	72.72	J30	0.39	142.88	71.31
J31	0.39	143.84	72.41	J31	0.39	143.86	72.43	J31	0.39	142.81	71.46
J32	0.39	143.87	72.75	J32	0.39	143.88	72.77	J32	0.39	142.95	71.44
J33	0.39	143.88	72.99	J33	0.39	143.89	73.01	J33	0.39	142.98	71.72
J34	0.39	143.89	72.88	J34	0.39	143.90	72.90	J34	0.39	143.02	71.65
J35	0.39	143.90	72.86	J35	0.39	143.92	72.88	J35	0.39	143.10	71.71
J36	0.39	143.92	73.01	J36	0.39	143.94	73.04	J36	0.39	143.17	71.95
J37	0.44	143.81	72.41	J37	0.44	143.82	72.43	J37	0.44	142.84	70.87
J38	0.44	143.80	72.44	J38	0.44	143.81	72.46	J38	0.44	142.86	70.72
J39	0.44	143.80	72.44	J39	0.44	143.81	72.46	J39	0.44	142.86	70.69
J40	0.58	143.97	72.54	J40	0.58	144.02	72.62	J40	0.58	143.80	72.30
J41	0.59	143.79	72.48	J41	0.59	143.80	72.51	J41	0.59	142.53	70.73
J42	0.59	143.79	72.52	J42	0.59	143.82	72.55	J42	0.59	142.52	70.63
J43	0.59	143.78	72.42	J43	0.59	143.80	72.45	J43	0.59	142.52	70.63
J44	0.59	143.7									

Option A - 2 Connections - Buildout (Phase 2 (A, B, C) + Phase 3 (D, E) + Phase 4 + Jock River)				Option A - 2 Connections with Upgrades on Danson Gardens Grv - Buildout (Phase 2 (A, B, C) + Phase 3 (D, E) + Phase 4 + Jock River)				Option B - 3 Connections - Buildout (Phase 2 (A, B, C) + Phase 3 (D, E) + Phase 4 + Jock River)			
Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)
Maximum	0.83	143.94	73.17	Maximum	0.83	149.49	81.16	Maximum	0.83	149.49	81.14
Minimum	0.00	143.69	71.56	Minimum	0.00	143.70	71.69	Minimum	0.00	142.37	69.83
J01	0.39	143.94	71.70	J01	0.39	143.93	71.69	J01	0.39	143.31	70.81
J02	0.00	143.91	72.27	J02	0.00	143.91	72.27	J02	0.00	143.15	71.20
J03	0.59	143.88	72.25	J03	0.59	143.89	72.05	J03	0.59	143.65	70.52
J06	0.39	143.88	72.87	J06	0.39	143.89	72.89	J06	0.39	143.03	71.68
J07	0.58	143.88	73.03	J07	0.58	143.90	73.06	J07	0.58	143.09	71.90
J08	0.58	143.89	72.91	J08	0.58	143.91	72.95	J08	0.58	143.18	71.90
J09	0.58	143.90	72.41	J09	0.58	143.92	72.45	J09	0.58	143.25	71.49
J10	0.58	143.90	72.68	J10	0.58	143.94	72.68	J10	0.58	143.35	71.88
J100	0.83	143.71	71.00	J100	0.83	143.72	71.00	J100	0.83	143.26	69.97
J101	0.59	143.71	72.01	J101	0.59	143.72	72.01	J101	0.59	143.28	70.13
J102	0.83	143.70	71.89	J102	0.83	143.71	71.91	J102	0.83	142.36	69.99
J103	0.83	143.70	71.74	J103	0.83	143.71	71.75	J103	0.83	142.36	69.83
J109	0.59	143.70	72.01	J109	0.59	143.71	72.03	J109	0.59	142.33	70.07
J11	0.58	143.91	72.57	J11	0.58	143.95	72.63	J11	0.58	143.42	71.87
J110	0.59	143.89	72.18	J110	0.59	143.71	72.20	J110	0.59	143.35	70.04
J111	0.59	143.69	72.11	J111	0.59	143.70	72.27	J111	0.59	143.33	70.31
J112	0.59	143.69	72.14	J112	0.59	143.70	72.16	J112	0.59	142.32	70.19
J113	0.59	143.69	72.08	J113	0.59	143.70	72.07	J113	0.59	142.31	70.10
J114	0.59	143.69	71.91	J114	0.59	143.70	71.93	J114	0.59	142.31	69.96
J115	0.59	143.69	71.88	J115	0.59	143.70	71.90	J115	0.59	142.31	69.93
J116	0.59	143.69	71.93	J116	0.59	143.70	71.94	J116	0.59	142.31	69.97
J117	0.59	143.69	72.17	J117	0.59	143.70	72.17	J117	0.59	142.31	70.10
J118	0.59	143.69	72.14	J118	0.59	143.70	72.16	J118	0.59	142.31	70.19
J119	0.59	143.69	72.27	J119	0.59	143.70	72.29	J119	0.59	142.31	70.31
J12	0.58	143.93	72.46	J12	0.58	143.99	72.55	J12	0.58	143.68	72.10
J120	0.59	143.69	72.27	J120	0.59	143.70	72.28	J120	0.59	142.31	70.31
J121	0.59	143.69	72.07	J121	0.59	143.70	72.08	J121	0.59	142.31	70.11
J122	0.59	143.69	71.92	J122	0.59	143.70	71.93	J122	0.59	142.31	69.96
J123	0.59	143.69	72.05	J123	0.59	143.70	72.07	J123	0.59	142.31	70.13
J124	0.59	143.69	72.20	J124	0.59	143.70	72.21	J124	0.59	142.31	70.24
J125	0.59	143.69	72.38	J125	0.59	143.70	72.40	J125	0.59	142.31	70.43
J128	0.00	143.69	72.74	J128	0.00	143.70	72.76	J128	0.00	142.32	70.80
J129	0.59	143.69	72.72	J129	0.59	143.70	72.73	J129	0.59	142.32	70.77
J130	0.59	143.69	72.50	J130	0.59	143.70	72.50	J130	0.59	142.32	69.98
J131	0.59	143.69	72.53	J131	0.59	143.70	72.53	J131	0.59	142.32	70.67
J132	0.59	143.69	72.46	J132	0.59	143.70	72.48	J132	0.59	142.32	70.51
J133	0.59	143.69	72.54	J133	0.59	143.70	72.56	J133	0.59	142.31	70.58
J134	0.59	143.69	72.67	J134	0.59	143.70	72.68	J134	0.59	142.31	70.71
J135	0.59	143.69	72.77	J135	0.59	143.70	72.78	J135	0.59	142.31	70.81
J136	0.59	143.69	72.68	J136	0.59	143.70	72.68	J136	0.59	142.31	70.68
J137	0.59	143.69	72.65	J137	0.59	143.70	72.67	J137	0.59	142.31	70.69
J14	0.59	143.69	72.67	J14	0.59	143.70	72.69	J14	0.59	142.31	70.72
J15	0.39	143.84	72.53	J15	0.39	143.85	72.55	J15	0.39	142.89	71.18
J152	0.58	143.88	73.07	J152	0.58	143.89	73.09	J152	0.58	143.07	71.92
J153	0.83	143.73	71.86	J153	0.83	143.74	71.88	J153	0.83	142.49	70.09
J154	0.59	143.69	72.40	J154	0.59	143.70	72.42	J154	0.59	142.31	70.45
J155	0.59	143.69	72.56	J155	0.59	143.70	72.56	J155	0.59	142.31	70.59
J156	0.00	143.69	72.27	J156	0.00	143.70	72.29	J156	0.00	142.31	70.31
J158	0.00	143.70	72.79	J158	0.00	143.71	72.80	J158	0.00	142.34	70.85
J16	0.39	143.81	72.65	J16	0.39	143.83	72.66	J16	0.39	142.79	71.19
J162	0.00	143.70	71.90	J162	0.00	143.71	71.91	J162	0.00	142.33	70.03
J164	0.00	143.70	71.97	J164	0.00	143.71	71.98	J164	0.00	142.33	69.97
J166	0.00	143.70	71.96	J166	0.00	143.71	71.96	J166	0.00	142.33	69.95
J168	0.00	143.70	72.07	J168	0.00	143.71	72.08	J168	0.00	142.33	70.13
J17	0.38	143.79	72.44	J17	0.07	143.49	80.54	J17	0.07	143.47	80.53
J170	0.00	143.70	71.56	J170	0.00	143.48	79.78	J170	0.00	143.47	79.77
J172	0.00	143.70	71.90	J172	0.00	143.48	80.13	J172	0.00	143.47	80.11
J174	0.83	143.70	72.07	J174	0.15	143.48	80.30	J174	0.15	143.47	80.28
J176	0.44	143.70	72.40	J176	0.05	143.48	80.41	J176	0.15	143.47	80.29
J18	0.39	143.76	72.19	J18	0.07	143.49	80.45	J18	0.07	143.47	80.61
J180	0.44	143.70	72.61	J180	0.08	143.48	80.84	J180	0.08	143.47	80.82
J182	0.44	143.70	72.73	J182	0.08	143.48	80.95	J182	0.08	143.47	80.94
J184	0.44	143.70	72.79	J184	0.08	143.48	81.01	J184	0.08	143.47	80.99
J186	0.44	143.70	72.80	J186	0.08	143.48	81.02	J186	0.08	143.47	80.91
J188	0.44	143.70	72.87	J188	0.08	143.48	81.03	J188	0.08	143.47	80.92
J189	0.56	143.75	71.96	J189	0.10	143.49	80.11	J189	0.10	143.47	80.10
J20	0.56	143.74	72.41	J20	0.10	143.48	80.58	J20	0.10	143.47	80.57
J21	0.56	143.73	72.24	J21	0.10	143.48	80.43	J21	0.10	143.47	80.41
J22	0.56	143.72	72.29	J22	0.10	143.48	80.48	J22	0.10	143.47	80.47
J23	0.56	143.72	72.42	J23	0.10	143.48	80.61	J23	0.10	143.47	80.59
J24	0.56	143.72	72.43	J24	0.10	143.48	80.62	J24	0.10	143.47	80.62
J25	0.56	143.72	72.45	J25	0.10	143.48	80.62	J25	0.10	143.47	80.61
J26	0.56	143.73	72.54	J26	0.10	143.48	80.72	J26	0.10	143.47	80.71
J27	0.56	143.73	72.68	J27	0.10	143.48	80.85	J27	0.10	143.47	80.84
J28	0.56	143.74	72.61	J28	0.10	143.48	80.78	J28	0.10	143.47	80.76
J29	0.56	143.75	72.62	J29	0.05	143.48	80.78	J29	0.10	143.47	80.77
J30	0.59	143.77	72.71	J31	0.07	143.49	80.84	J31	0.07	143.47	80.82
J32	0.39	143.78	72.63	J32	0.07	143.49	80.74	J32	0.07	143.47	80.72
J33	0.39	143.79	72.88	J33	0.07	143.49	80.97	J33	0.07	143.48	80.95
J34	0.39	143.81	72.76	J34	0.07	143.49	80.84	J34	0.07	143.48	80.83
J35	0.39	143.82	72.75	J35	0.07	143.49	80.80	J35	0.07	143.48	80.78
J36	0.59	143.71	72.53	J36	0.10	143.49	80.93	J36	0.10	143.47	80.91
J37	0.59	143.71	72.55	J37	0.10	143.49	80.93	J37	0.10	143.47	80.91
J38	0.44	143.71	72.51	J38	0.08	143.48	80.52	J38	0.08	143.47	80.51
J40	0.58	143.93	72.49	J40	0.11	143.49	80.40	J40	0.11	143.49	80.39
J41	0.59	143.70	72.35	J41	0.11	143.48	80.58	J41	0.11	143.47	80.56
J42	0.59	143.69	72.43	J42	0.11	143.48	80.62	J42	0.11	143.47	80.61
J43	0.59	143.69	72.44	J44	0.11	143.48	80.68	J44	0.11	143.47	80.65
J45	0.59	14									

Option A - 2 Connections - Phase 2 (2A, 2B, 2C)					Option A - 2 Connections with Upgrades on Danson Gardens Grv - Phase 2 (2A, 2B, 2C)					Option B - 3 Connections - Phase 2 (2A, 2B, 2C)				
Junction ID	Base Demand (MXDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (MXDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (MXDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)
J01	0.18	13,000	59.93	64,000	J01	0.18	13,000	62.43	66,000	J01	0.18	13,000	51.23	28,000
J02	0.00	13,000	60.51	64,000	J02	0.00	13,000	63.01	66,000	J02	0.00	13,000	51.51	28,000
J05	0.18	13,000	61.00	64,000	J05	0.18	13,000	63.51	66,000	J05	0.18	13,000	51.87	28,000
J06	0.18	13,000	61.17	64,000	J06	0.18	13,000	63.67	66,000	J06	0.18	13,000	52.01	28,000
J07	0.27	13,000	61.40	64,000	J07	0.27	13,000	63.90	66,000	J07	0.27	13,000	52.34	28,000
J08	0.27	13,000	61.35	65,000	J08	0.27	13,000	63.84	67,000	J08	0.27	13,000	52.46	28,000
J09	0.27	13,000	60.94	65,000	J09	0.27	13,000	63.43	67,000	J09	0.27	13,000	52.27	28,000
J10	0.27	13,000	61.31	67,000	J10	0.27	13,000	63.80	69,000	J10	0.27	13,000	52.97	29,000
J11	0.27	13,000	61.33	68,000	J11	0.27	13,000	63.82	70,000	J11	0.27	13,000	53.36	30,000
J12	0.27	13,000	61.41	75,000	J12	0.27	13,000	65.01	77,000	J12	0.27	13,000	54.51	30,000
J15	0.18	13,000	60.14	55,000	J15	0.18	13,000	52.64	57,000	J15	0.18	13,000	49.27	25,000
J158	0.00	13,000	53.27	29,000	J158	0.00	13,000	55.77	30,000	J158	0.00	13,000	33.14	16,000
J16	0.18	13,000	59.88	52,000	J16	0.18	13,000	62.38	53,000	J16	0.18	13,000	48.40	24,000
J17	0.18	13,000	59.23	48,000	J17	0.18	13,000	61.73	50,000	J17	0.18	13,000	46.84	23,000
J178	0.20	13,000	54.17	31,000	J178	0.20	13,000	56.67	32,000	J178	0.20	13,000	33.01	16,000
J18	0.20	13,000	53.69	48,000	J18	0.20	13,000	60.01	47,000	J18	0.20	13,000	45.81	22,000
J180	0.20	13,000	53.53	30,000	J180	0.20	13,000	58.93	30,000	J180	0.20	13,000	32.83	16,000
J182	0.20	13,000	53.25	29,000	J182	0.20	13,000	55.76	30,000	J182	0.20	13,000	32.86	16,000
J184	0.20	13,000	53.24	29,000	J184	0.20	13,000	55.74	30,000	J184	0.20	13,000	33.00	16,000
J186	0.20	13,000	54.90	33,000	J186	0.20	13,000	57.40	34,000	J186	0.20	13,000	33.32	16,000
J19	0.25	13,000	57.93	43,000	J19	0.25	13,000	60.43	45,000	J19	0.25	13,000	44.33	21,000
J20	0.25	13,000	58.04	42,000	J20	0.25	13,000	60.54	43,000	J20	0.25	13,000	44.19	21,000
J21	0.25	13,000	57.56	40,000	J21	0.25	13,000	60.59	41,000	J21	0.25	13,000	43.51	20,000
J22	0.25	13,000	57.21	39,000	J22	0.25	13,000	59.71	40,000	J22	0.25	13,000	42.93	20,000
J23	0.25	13,000	56.74	37,000	J23	0.25	13,000	59.24	38,000	J23	0.25	13,000	43.28	20,000
J24	0.25	13,000	56.19	35,000	J24	0.25	13,000	58.69	36,000	J24	0.25	13,000	43.20	20,000
J25	0.25	13,000	55.70	34,000	J25	0.25	13,000	58.20	35,000	J25	0.25	13,000	43.14	20,000
J26	0.25	13,000	55.73	34,000	J26	0.25	13,000	58.23	35,000	J26	0.25	13,000	43.53	21,000
J27	0.25	13,000	55.65	33,000	J27	0.25	13,000	58.35	35,000	J27	0.25	13,000	44.21	21,000
J28	0.25	13,000	55.56	34,000	J28	0.25	13,000	58.36	35,000	J28	0.25	13,000	44.36	21,000
J29	0.25	13,000	55.58	34,000	J29	0.25	13,000	58.48	35,000	J29	0.25	13,000	44.80	21,000
J30	0.18	13,000	56.30	35,000	J30	0.18	13,000	58.80	36,000	J30	0.18	13,000	45.41	22,000
J31	0.18	13,000	56.47	36,000	J31	0.18	13,000	58.97	37,000	J31	0.18	13,000	45.83	22,000
J32	0.18	13,000	56.69	36,000	J32	0.18	13,000	59.19	38,000	J32	0.18	13,000	46.25	22,000
J33	0.18	13,000	56.73	36,000	J33	0.18	13,000	59.20	38,000	J33	0.18	13,000	46.30	22,000
J34	0.18	13,000	57.53	39,000	J34	0.18	13,000	60.97	44,000	J34	0.18	13,000	48.53	24,000
J35	0.18	13,000	58.47	43,000	J35	0.18	13,000	61.29	46,000	J35	0.18	13,000	49.22	25,000
J36	0.18	13,000	59.70	49,000	J36	0.18	13,000	62.20	50,000	J36	0.18	13,000	50.43	26,000
J37	0.20	13,000	56.39	37,000	J37	0.20	13,000	58.89	38,000	J37	0.20	13,000	39.38	19,000
J38	0.20	13,000	55.90	35,000	J38	0.20	13,000	58.40	36,000	J38	0.20	13,000	36.58	17,000
J39	0.20	13,000	56.52	34,000	J39	0.20	13,000	57.62	35,000	J39	0.20	13,000	34.87	17,000
J40	0.27	13,000	61.54	73,000	J40	0.27	13,000	64.63	75,000	J40	0.27	13,000	54.51	30,000
J46	0.27	13,000	61.47	71,000	J46	0.27	13,000	63.96	73,000	J46	0.27	13,000	54.12	31,000
J48	0.27	13,000	61.38	69,000	J48	0.27	13,000	63.88	71,000	J48	0.27	13,000	53.63	30,000
J75	0.25	13,000	47.92	23,000	J75	0.25	13,000	50.42	24,000	J75	0.25	13,000	35.45	17,000
J76	0.25	13,000	52.46	28,000	J76	0.25	13,000	54.96	29,000	J76	0.25	13,000	40.42	19,000
J77	0.25	13,000	47.31	22,000	J77	0.25	13,000	51.24	24,000	J77	0.25	13,000	35.92	17,000
J78	0.18	13,000	52.36	29,000	J78	0.18	13,000	55.45	30,000	J78	0.18	13,000	42.61	22,000
J79	0.18	13,000	49.39	25,000	J79	0.18	13,000	51.89	25,000	J79	0.18	13,000	38.99	18,000
J94	0.20	13,000	53.82	30,000	J94	0.20	13,000	56.32	31,000	J94	0.20	13,000	34.35	17,000
J95	0.20	13,000	53.35	29,000	J95	0.20	13,000	55.85	30,000	J95	0.20	13,000	33.61	16,000
J96	0.20	13,000	53.38	29,000	J96	0.20	13,000	55.88	30,000	J96	0.20	13,000	33.46	16,000
J97	0.20	13,000	44.98	21,000	J97	0.20	13,000	47.48	22,000	J97	0.20	13,000	24.84	14,000
J98	0.00	13,000	53.12	29,000	J98	0.00	13,000	55.62	30,000	J98	0.00	13,000	33.06	16,000

Option A - 2 Connections - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E)					Option A - 2 Connections with Upgrades on Danson Gardens Grv - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E)					Option B - 3 Connections - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E)				
Junction ID	Base Demand (MXDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (MXDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (MXDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)
J01	0.18	13,000	59.80	64,000	J01	0.18	13,000	62.31	66,000	J01	0.18	13,000	50.62	27,000
J02	0.00	13,000	60.36	63,000	J02	0.00	13,000	62.87	65,000	J02	0.00	13,000	50.82	27,000
J05	0.18	13,000	60.85	63,000	J05	0.18	13,000	63.35	65,000	J05	0.18	13,000	51.13	27,000
J06	0.18	13,000	61.62	63,000	J06	0.18	13,000	65.65	65,000	J06	0.18	13,000	51.57	27,000
J07	0.27	13,000	61.26	64,000	J07	0.27	13,000	63.76	66,000	J07	0.27	13,000	51.66	27,000
J08	0.27	13,000	61.22	64,000	J08	0.27	13,000	63.72	66,000	J08	0.27	13,000	51.83	28,000
J09	0.27	13,000	60.82	65,000	J09	0.27	13,000	63.31	67,000	J09	0.27	13,000	51.69	28,000
J10	0.27	13,000	61.20	66,000	J10	0.27	13,000	63.69	69,000	J10	0.27	13,000	52.43	29,000
J100	0.38	13,000	49.95	26,000	J100	0.38	13,000	52.45	27,000	J100	0.38	13,000	35.22	17,000
J101	0.25	13,000	52.25	34,000	J101	0.25	13,000	57.25	35,000	J101	0.25	13,000	40.51	19,000
J102	0.28	13,000	54.95	34,000	J102	0.28	13,000	57.45	35,000	J102	0.28	13,000	40.23	19,000
J103	0.38	13,000	49.43	25,000	J103	0.38	13,000	51.93	26,000	J103	0.38	13,000	34.33	17,000
J11	0.27	13,000	61.23	68,000	J11	0.27	13,000	63.72	70,000	J11	0.27	13,000	52.87	29,000
J12	0.27	13,000	61.54	75,000	J12	0.27	13,000	64.02	77,000	J12	0.27	13,000	54.55	32,000
J15	0.18	13,000	59.95	55,000	J15	0.18	13,000	62.45	57,000	J15	0.18	13,000	48.44	24,000
J153	0.25	13,000	53.65	34,000	J153	0.25	13,000	57.55	35,000	J153	0.25	13,000	41.41	20,000
J158	0.00	13,000	54.39	31,000	J158	0.00	13,000	58.89	32,000	J158	0.00	13,000	39.17	19,000
J16	0.18	13,000	59.66	51,000	J16	0.18	13,000	62.16	53,000	J16	0.18	13,000	47.54	24,000
J17	0.18	13,000	58.98	48,000	J17	0.18	13,000	61.48	49,000	J17	0.18	13,000	45.98	22,000
J174	0.38	13,000	54.59	33,000	J174	0.38	13,000	57.09	34,000	J174	0.38	13,000	39.49	19,000
J176	0.38	13,000	54.99	33,000	J176	0.38	13,000	57.49	34,000	J176	0.38	13,000	39.61	19,000
J178	0.20	13,000	55.46	44,000	J178	0.20	13,000	57.95	35,000	J178	0.20	13,000	39.88	19,000
J18	0.20	13,000	55.42	45,000	J18	0.20	13,000	57.93	47,000	J18	0.20	13,000	44.45	23,000
J180	0.20	13,000	54.75	32,000	J180	0.20	13,000	57.25	33,000	J180	0.20	13,000	39.34	19,000
J182	0.20	13,000	54.42	31,000	J182	0.20	13,000	56.92	32,000	J182	0.20	13,000	39.12	19,000
J184	0.20	13,000	54.39	31,000	J184	0.20	13,000	56.89	32,000	J184	0.20	13,000	39.13	19,000
J186	0.20	13,000	56.29	37,000	J186	0.20	13,000	58.79	38,000	J186	0.20	13,000	40.47	19,000
J19	0.25	13,000	57.74	35,000	J19	0.25	13,000	60.23	45,000	J19	0.25	13,000	43.44	21,000
J20	0.25	13,000	53.41	43,000	J20	0.25	13,000	56.41	44,000	J20	0.25	13,000	44.01	21,000
J21	0.25	13,000	57.59	41,000	J21	0.25	13,000	60.09	43,000	J21	0.25	13,000	42.20	21,000
J22	0.25	13,000	57.50	41,000	J22	0.25	13,000	60.00	42,000	J22	0.25	13,000	43.66	21,000
J23	0.25	13,000	56.85	38,000	J23	0.25	13,000	59.34	39,000	J23	0.25	13,000	43.55	21,000
J24	0.25	13,000	56.22	36,000	J24	0.25	13,000	58.72	37,000	J24	0.25	13,000	43.23	21,000
J25	0.25	13,000	55.68	34,000	J25	0.25	13,000	58.18	36,000	J25	0.25	13,000	42.96	20,000
J26	0.25	13,000	55.67	34,000	J26	0.25	13,000	58.15	36,000	J26	0.25	13,000	43.00	20,000
J27	0.25	13,000	55.58	35,000	J27	0.25	13,000	58.48	36,000	J27	0.25	13,000	43.75	21,000
J28	0.25	13,000	55.76	34,000	J28	0.25	13,000	58.26	35,000	J28	0.25	13,000	43.80	21,000
J29	0.25	13,000	55.86	35,000	J29	0.25	13,000	58.36	36,000	J29	0.25	13,000	44.15	21,000
J30	0.18	13,000	56.16	35,000	J30	0.18	13,000	58.66	37,000	J30	0.18	13,000	44.70	21,000
J31	0.18	13,000	56.32	36,000	J31	0.18	13,000	58.82	37,000	J31	0.18	13,000	45.09	22,000
J32	0.18	13,000	56.53	36,000	J32	0.18	13,000	59.53	37,000	J32	0.18	13,000	45.48	22,000
J33	0.18	13,000	57.58	38,000	J33	0.18	13,000	59.88	40,000	J33	0.18	13,000	46.51	23,000
J34	0.18	13,000	58.29	42,000	J34	0.18	13,000	60.79	44,000	J34	0.18	13,000	47.71	24,000
J35	0.18	13,000	58.61	44,000	J35	0.18	13,000	61.11	45,000	J35	0.18	13,000	48.42	24,000
J36	0.18	13,000	59.53	49,000	J36	0.18	13,000	62.03	50,000	J36	0.18	13,000	49.65	25,000
J37	0.20	13,000	57.05	39,000	J37	0.20	13,000	59.55	41,000	J37	0.20	13,000	42.47	20,000
J38	0.20	13,000	56.87	39,000	J38	0.20	13,000	59.00	40,000	J38	0.20	13,000	41.73	20,000
J39	0.20	13,000	56.60	37,000	J39	0.20	13,000	58.10	39,000	J39	0.20	13,000	41.02	19,000
J40	0.27	13,000	61.64	73,000	J40	0.27	13,000	63.94	75,000	J40	0.27	13,000	54.14	31,000
J46	0.27	13,000	61.38	71,000	J46	0.27	13,000	63.87	73,000	J46	0.27	13,000	53.69	31,000
J48	0.27	13,000	61.28	69,000	J48	0.27	13,000	63.77	71,000	J48	0.27	13,000	53.16	30,000
J75	0.25	13,000	47.66	23,000	J75	0.25	13,000	50.36	24,000	J75	0.25	13,000	35.09	17,000
J76	0.25	13,000	52.35	28,000	J76	0.25	13,000	54.85	29,000	J76	0.25	13,000	39.80	19,000
J77	0.25	13,000	54.73	23,000	J77	0.25	13,000	56.40	24,000	J77	0.25	13,000	38.01	19,000
J78	0.18	13,000	52.76	29,000	J78	0.18	13,000	55.26	30,000	J78	0.18	13,000	41.05	19,000
J79	0.18	13,000	49.20	24,000	J79	0.18	13,000	51.70	24,000	J79	0.18	13,000	38.11	18,000
J80	0.38	13,000	44.54	21,000	J80	0.38	13,000	47.04	22,000	J80	0.38	13,000	30.88	16,000
J81	0.38	13,000	54.92	34,000	J81	0.38	13,000	57.42	35,000	J81	0.38	13,000	40.86	20,000
J82	0.38	13,000	54.56	33,000	J82	0.38	13,000	57.06	34,000	J82	0.38	13,000	40.86	20,000
J83	0.38	13,000	55.65	33,000	J83	0.38	13,000	58.35	35,000	J83	0.38	13,000	42.12	20,000
J84	0.36	13,000	55.99	36,000	J84	0.36	13,000	58.39	37,000	J84	0.36	13,000	42.46	20,000
J85	0.36	13,000	39.05	18,000	J85	0.36	13,000	41.55	19,000	J85	0.36	13,000	25.76	15,000
J86	0.36	13,000	35.38	17,000	J86	0.36	13,000	37.88	18,000	J86	0.36	13,000	22.09	14,000
J87	0.36	13,000	35.40	17,000	J87	0.36	13,000	37.90	18,000	J87	0.36	13,000	22.11	14,000
J88	0.36	13,000	39.53	19,000	J88	0.36	13,000	42.03	19,000	J88	0.36	13,000	26.24	15,000
J89	0.36	13,000	55.87	39,000	J89	0.36	13,000	59.31	40,000	J89	0.36	13,000	43.58	21,000
J90	0.36	13,000	45.31	24,000	J90	0.36	13,000	51.21	25,000	J90	0.36	13,000	35.01	17,000
J91	0.38	13,000	54.96	33,000	J91	0.38	13,000	57.46	34,000	J91	0.38	13,000	41.62	20,000
J92	0.38	13,000	44.36	21,000	J92	0.38	13,000	48.86	22,000	J92	0.38	13,000	30.91	16,000
J93	0.38	13,000	41.24	19,000	J93	0.38	13,000	43.7						

Option A - 2 Connections - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E) + Phase 4					Option A - 2 Connections with Upgrades on Danson Gardens Grv - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E) + Phase 4					Option B - 3 Connections - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E) + Phase 4				
Junction ID	Base Demand (MDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (MDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (MDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)
J01	0.18	13,000	59.64	63,000	J01	0.18	13,000	62.15	65,000	J01	0.18	13,000	51.27	32,000
J02	0.00	13,000	60.19	63,000	J02	0.00	13,000	62.69	65,000	J02	0.00	13,000	51.95	33,000
J05	0.18	13,000	60.66	63,000	J05	0.18	13,000	63.16	65,000	J05	0.18	13,000	52.67	35,000
J06	0.18	13,000	60.84	63,000	J06	0.18	13,000	63.34	65,000	J06	0.18	13,000	52.68	33,000
J07	0.27	13,000	61.09	63,000	J07	0.27	13,000	63.59	65,000	J07	0.27	13,000	52.23	33,000
J08	0.27	13,000	61.06	64,000	J08	0.27	13,000	63.56	66,000	J08	0.27	13,000	51.74	32,000
J09	0.27	13,000	60.67	65,000	J09	0.27	13,000	63.16	67,000	J09	0.27	13,000	51.02	32,000
J10	0.27	13,000	61.07	66,000	J10	0.27	13,000	63.56	68,000	J10	0.27	13,000	51.18	32,000
J100	0.38	13,000	49.50	29,000	J100	0.38	13,000	52.00	26,000	J100	0.38	13,000	42.61	22,000
J101	0.38	13,000	54.02	34,000	J101	0.38	13,000	57.42	35,000	J101	0.38	13,000	47.49	27,000
J102	0.38	13,000	54.71	34,000	J102	0.38	13,000	61.21	35,000	J102	0.38	13,000	47.78	27,000
J103	0.38	13,000	48.97	25,000	J103	0.38	13,000	51.47	25,000	J103	0.38	13,000	42.01	21,000
J109	0.27	13,000	53.11	30,000	J109	0.27	13,000	55.60	31,000	J109	0.27	13,000	45.57	24,000
J111	0.27	13,000	61.11	68,000	J111	0.27	13,000	63.59	70,000	J110	0.27	13,000	51.09	32,000
J110	0.27	13,000	53.44	31,000	J110	0.27	13,000	55.93	32,000	J110	0.27	13,000	45.69	24,000
J112	0.27	13,000	49.93	26,000	J112	0.27	13,000	52.43	27,000	J112	0.27	13,000	49.97	25,000
J113	0.27	13,000	42.04	20,000	J113	0.27	13,000	44.54	21,000	J113	0.27	13,000	32.84	17,000
J114	0.27	13,000	40.92	19,000	J114	0.27	13,000	43.42	20,000	J114	0.27	13,000	31.60	16,000
J115	0.27	13,000	43.55	21,000	J115	0.27	13,000	46.05	21,000	J115	0.27	13,000	34.12	17,000
J116	0.27	13,000	48.41	23,000	J116	0.27	13,000	48.91	23,000	J116	0.27	13,000	36.87	18,000
J117	0.27	13,000	41.08	21,000	J117	0.27	13,000	47.19	22,000	J117	0.27	13,000	35.27	18,000
J119	0.27	13,000	50.84	27,000	J119	0.27	13,000	53.34	28,000	J119	0.27	13,000	40.92	20,000
J120	0.27	13,000	61.44	74,000	J120	0.27	13,000	63.92	75,000	J120	0.27	13,000	51.55	34,000
J121	0.27	13,000	49.48	25,000	J121	0.27	13,000	51.98	26,000	J121	0.27	13,000	39.53	20,000
J122	0.27	13,000	46.63	23,000	J121	0.27	13,000	49.13	24,000	J122	0.27	13,000	36.83	18,000
J123	0.27	13,000	40.39	19,000	J123	0.27	13,000	42.89	20,000	J123	0.27	13,000	30.42	16,000
J124	0.27	13,000	40.70	20,000	J124	0.27	13,000	43.20	20,000	J124	0.27	13,000	30.46	16,000
J125	0.27	13,000	47.66	24,000	J125	0.27	13,000	50.16	24,000	J125	0.27	13,000	36.96	18,000
J128	0.00	6,000	56.19	16,000	J128	0.00	6,000	58.67	16,000	J128	0.00	6,000	51.01	14,000
J129	0.27	13,000	38.85	18,000	J129	0.27	13,000	41.35	19,000	J130	0.27	13,000	33.75	17,000
J131	0.27	13,000	38.62	19,000	J131	0.27	13,000	40.52	19,000	J131	0.27	13,000	30.21	16,000
J132	0.27	13,000	42.91	20,000	J132	0.27	13,000	45.10	21,000	J132	0.27	13,000	33.62	17,000
J133	0.27	13,000	43.72	21,000	J133	0.27	13,000	46.22	21,000	J133	0.27	13,000	33.07	17,000
J134	0.27	13,000	40.65	19,000	J134	0.27	13,000	43.15	20,000	J134	0.27	13,000	29.95	16,000
J135	0.27	13,000	41.13	19,000	J135	0.27	13,000	43.62	20,000	J135	0.27	13,000	30.33	16,000
J136	0.27	13,000	43.13	20,000	J136	0.27	13,000	45.63	21,000	J136	0.27	13,000	32.25	16,000
J137	0.27	13,000	37.37	19,000	J137	0.27	13,000	40.00	19,000	J137	0.27	13,000	31.75	7,000
J14	0.27	13,000	55.51	15,000	J14	0.27	13,000	57.05	15,000	J14	0.27	13,000	49.43	13,000
J15	0.18	13,000	59.70	54,000	J15	0.18	13,000	62.20	56,000	J15	0.18	13,000	50.86	31,000
J153	0.38	13,000	54.70	34,000	J153	0.38	13,000	57.19	35,000	J153	0.38	13,000	47.25	26,000
J154	0.27	13,000	54.45	33,000	J154	0.27	13,000	56.95	34,000	J154	0.27	13,000	43.80	22,000
J155	0.27	13,000	54.16	32,000	J155	0.27	13,000	56.66	33,000	J155	0.27	13,000	42.64	21,000
J156	0.00	13,000	53.00	31,000	J156	0.00	13,000	55.50	31,000	J156	0.00	13,000	48.86	28,000
J157	0.00	13,000	53.51	31,000	J157	0.00	13,000	56.42	31,000	J157	0.00	13,000	49.01	28,000
J16	0.18	13,000	59.39	51,000	J16	0.18	13,000	61.88	52,000	J16	0.18	13,000	50.62	30,000
J162	0.00	13,000	53.12	31,000	J162	0.00	13,000	55.62	32,000	J162	0.00	13,000	45.76	24,000
J164	0.00	13,000	51.58	28,000	J164	0.00	13,000	54.08	29,000	J164	0.00	13,000	44.11	23,000
J166	0.00	13,000	46.47	23,000	J166	0.00	13,000	48.97	23,000	J166	0.00	13,000	39.00	19,000
J168	0.00	13,000	43.35	21,000	J168	0.00	13,000	45.85	21,000	J168	0.00	13,000	35.88	18,000
J17	0.18	13,000	56.67	30,000	J17	0.18	13,000	59.70	30,000	J17	0.18	13,000	49.00	20,000
J170	0.00	13,000	37.98	18,000	J170	0.00	13,000	40.48	19,000	J170	0.00	13,000	39.51	16,000
J172	0.00	13,000	53.56	31,000	J172	0.00	13,000	56.06	32,000	J172	0.00	13,000	46.34	25,000
J174	0.38	13,000	54.79	34,000	J174	0.38	13,000	57.29	35,000	J174	0.38	13,000	47.73	27,000
J176	0.38	13,000	54.67	33,000	J176	0.38	13,000	57.17	34,000	J176	0.38	13,000	47.56	26,000
J178	0.20	13,000	54.00	34,000	J178	0.20	13,000	57.48	35,000	J178	0.20	13,000	48.31	27,000
J179	0.18	13,000	57.07	49,000	J179	0.18	13,000	60.47	50,000	J179	0.18	13,000	49.36	23,000
J21	0.25	13,000	57.19	41,000	J21	0.25	13,000	59.69	42,000	J21	0.25	13,000	48.74	28,000
J22	0.25	13,000	57.08	40,000	J22	0.25	13,000	59.58	42,000	J22	0.25	13,000	49.50	29,000
J23	0.25	13,000	56.45	38,000	J23	0.25	13,000	59.85	39,000	J23	0.25	13,000	49.00	28,000
J24	0.25	13,000	55.84	35,000	J24	0.25	13,000	58.34	36,000	J24	0.25	13,000	48.43	27,000
J25	0.25	13,000	55.32	34,000	J25	0.25	13,000	57.82	35,000	J25	0.25	13,000	47.94	26,000
J26	0.25	13,000	55.20	34,000	J26	0.25	13,000	57.62	35,000	J26	0.25	13,000	47.07	26,000
J27	0.25	13,000	56.64	34,000	J27	0.25	13,000	58.13	35,000	J27	0.25	13,000	48.30	27,000
J28	0.25	13,000	55.43	34,000	J28	0.25	13,000	57.93	35,000	J28	0.25	13,000	48.10	26,000
J29	0.25	13,000	55.54	34,000	J29	0.25	13,000	58.04	35,000	J29	0.25	13,000	48.22	27,000
J30	0.18	13,000	55.86	35,000	J30	0.18	13,000	58.36	36,000	J30	0.18	13,000	48.53	27,000
J31	0.18	13,000	56.02	35,000	J31	0.18	13,000	58.52	36,000	J31	0.18	13,000	48.69	27,000
J32	0.18	13,000	56.65	35,000	J32	0.18	13,000	59.74	36,000	J32	0.18	13,000	48.00	27,000
J33	0.18	13,000	57.11	36,000	J33	0.18	13,000	59.61	36,000	J33	0.18</			

Option A - 2 Connections - Bulldout (Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E) + Phase 4 + Jock River)								Option A - 2 Connections with Upgrades on Danson Gardens Grv - Bulldout (Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E) + Phase 4 + Jock River)								Option B - 3 Connections - Bulldout (Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E) + Phase 4 + Jock River)								
Junction ID	Base Demand (MXDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (MXDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (MXDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)										
J01	0.18	13,000	59.57	64,000	J01	0.18	13,000	62.08	66,000	J01	0.18	13,000	51.10	32,000	J01	0.18	13,000	51.76	33,000	J01	0.18	13,000	52.47	35,000
J02	0.00	13,000	60.11	63,000	J02	0.00	13,000	62.61	65,000	J02	0.00	13,000	51.76	33,000	J02	0.00	13,000	51.76	33,000	J02	0.00	13,000	52.47	35,000
J05	0.18	13,000	60.58	63,000	J05	0.18	13,000	63.08	65,000	J05	0.18	13,000	52.47	35,000	J05	0.18	13,000	53.21	35,000	J05	0.18	13,000	52.26	34,000
J06	0.18	13,000	60.95	63,000	J06	0.18	13,000	63.45	65,000	J06	0.18	13,000	52.47	35,000	J06	0.18	13,000	51.78	33,000	J06	0.18	13,000	51.11	32,000
J07	0.27	13,000	61.00	64,000	J07	0.27	13,000	63.50	66,000	J07	0.27	13,000	51.78	33,000	J07	0.27	13,000	51.11	32,000	J07	0.27	13,000	51.26	32,000
J08	0.27	13,000	60.99	64,000	J08	0.27	13,000	63.48	66,000	J08	0.27	13,000	51.78	33,000	J08	0.27	13,000	51.11	32,000	J08	0.27	13,000	51.26	32,000
J09	0.27	13,000	60.59	65,000	J09	0.27	13,000	63.08	67,000	J09	0.27	13,000	51.78	33,000	J09	0.27	13,000	51.11	32,000	J09	0.27	13,000	51.26	32,000
J10	0.27	13,000	60.99	66,000	J10	0.27	13,000	63.48	68,000	J10	0.27	13,000	51.78	33,000	J10	0.27	13,000	51.11	32,000	J10	0.27	13,000	51.26	32,000
J100	0.38	13,000	49.55	26,000	J100	0.38	13,000	52.00	26,000	J100	0.38	13,000	49.55	26,000	J100	0.38	13,000	42.51	22,000	J100	0.38	13,000	47.99	27,000
J101	0.00	13,000	54.51	34,000	J101	0.00	13,000	57.00	34,000	J101	0.00	13,000	54.51	34,000	J101	0.00	13,000	47.68	27,000	J101	0.00	13,000	41.91	21,000
J102	0.38	13,000	54.70	34,000	J102	0.38	13,000	57.20	35,000	J102	0.38	13,000	54.70	34,000	J102	0.38	13,000	45.47	24,000	J102	0.38	13,000	51.16	32,000
J103	0.38	13,000	48.97	25,000	J103	0.38	13,000	51.47	26,000	J103	0.38	13,000	48.97	25,000	J103	0.38	13,000	44.77	21,000	J103	0.38	13,000	49.47	24,000
J109	0.27	13,000	53.11	31,000	J109	0.27	13,000	55.60	32,000	J109	0.27	13,000	51.16	32,000	J109	0.27	13,000	45.60	24,000	J109	0.27	13,000	49.12	25,000
J11	0.27	13,000	61.02	68,000	J11	0.27	13,000	63.50	69,000	J11	0.27	13,000	51.16	32,000	J11	0.27	13,000	48.11	23,000	J11	0.27	13,000	49.81	23,000
J110	0.27	13,000	53.44	31,000	J110	0.27	13,000	55.93	32,000	J110	0.27	13,000	51.16	32,000	J110	0.27	13,000	45.60	24,000	J110	0.27	13,000	49.12	25,000
J111	0.27	13,000	53.44	31,000	J111	0.27	13,000	55.93	32,000	J111	0.27	13,000	51.16	32,000	J111	0.27	13,000	45.60	24,000	J111	0.27	13,000	49.12	25,000
J112	0.27	13,000	49.93	26,000	J112	0.27	13,000	52.43	27,000	J112	0.27	13,000	49.93	26,000	J112	0.27	13,000	32.75	17,000	J112	0.27	13,000	31.50	16,000
J113	0.27	13,000	42.04	20,000	J113	0.27	13,000	44.54	21,000	J113	0.27	13,000	42.04	20,000	J113	0.27	13,000	34.02	17,000	J113	0.27	13,000	36.78	18,000
J114	0.27	13,000	40.92	19,000	J114	0.27	13,000	43.42	20,000	J114	0.27	13,000	40.92	19,000	J114	0.27	13,000	35.13	18,000	J114	0.27	13,000	36.78	18,000
J115	0.27	13,000	43.55	21,000	J115	0.27	13,000	46.05	21,000	J115	0.27	13,000	43.55	21,000	J115	0.27	13,000	32.75	17,000	J115	0.27	13,000	31.50	16,000
J116	0.27	13,000	46.41	23,000	J116	0.27	13,000	48.91	23,000	J116	0.27	13,000	46.41	23,000	J116	0.27	13,000	34.02	17,000	J116	0.27	13,000	36.78	18,000
J117	0.27	13,000	44.65	21,000	J117	0.27	13,000	47.00	22,000	J117	0.27	13,000	44.65	21,000	J117	0.27	13,000	33.65	17,000	J117	0.27	13,000	35.13	18,000
J118	0.27	13,000	45.19	25,000	J118	0.27	13,000	47.65	25,000	J118	0.27	13,000	45.19	25,000	J118	0.27	13,000	40.83	20,000	J118	0.27	13,000	47.62	26,000
J119	0.27	13,000	50.84	27,000	J119	0.27	13,000	53.34	28,000	J119	0.27	13,000	50.84	27,000	J119	0.27	13,000	47.14	26,000	J119	0.27	13,000	49.28	26,000
J120	0.27	13,000	41.37	25,000	J120	0.27	13,000	43.86	26,000	J120	0.27	13,000	41.37	25,000	J120	0.27	13,000	38.91	19,000	J120	0.27	13,000	42.55	21,000
J121	0.27	13,000	40.39	19,000	J121	0.27	13,000	42.89	20,000	J121	0.27	13,000	40.39	19,000	J121	0.27	13,000	36.86	18,000	J121	0.27	13,000	43.30	20,000
J122	0.27	13,000	47.66	24,000	J122	0.27	13,000	50.16	24,000	J122	0.27	13,000	47.66	24,000	J122	0.27	13,000	50.94	14,000	J122	0.27	13,000	36.05	18,000
J124	0.27	13,000	44.58	21,000	J125	0.27	13,000	47.08	22,000	J125	0.27	13,000	44.58	21,000	J125	0.27	13,000	44.02	23,000	J125	0.27	13,000	45.66	24,000
J128	0.00	6,000	56.11	16,000	J128	0.00	6,000	58.63	16,000	J128	0.00	6,000	54.09	16,000	J128	0.00	6,000	50.43	10,000	J128	0.00	6,000	53.65	12,000
J130	0.27	13,000	42.37	20,000	J130	0.27	13,000	44.87	21,000	J130	0.27	13,000	42.37	20,000	J130	0.27	13,000	38.91	19,000	J130	0.27	13,000	42.55	21,000
J131	0.27	13,000	39.62	18,000	J131	0.27	13,000	42.12	19,000	J131	0.27	13,000	39.62	18,000	J131	0.27	13,000	36.05	18,000	J131	0.27	13,000	42.55	21,000
J132	0.27	13,000	42.61	20,000	J132	0.27	13,000	45.10	21,000	J132	0.27	13,000	42.61	20,000	J132	0.27	13,000	39.53	17,000	J132	0.27	13,000	42.55	21,000
J133	0.27	13,000	43.72	21,000	J133	0.27	13,000	46.22	21,000	J133	0.27	13,000	43.72	21,000	J133	0.27	13,000	32.97	17,000	J133	0.27	13,000	39.53	17,000
J134	0.27	13,000	40.65	19,000	J134	0.27	13,000	43.15	20,000	J134	0.27	13,000	40.65	19,000	J134	0.27	13,000	32.44	16,000	J134	0.27	13,000	39.85	19,000
J135	0.27	13,000	43.50	20,000	J135	0.27	13,000	46.05	21,000	J135	0.27	13,000	43.50	20,000	J135	0.27	13,000	32.16	16,000	J135	0.27	13,000	39.85	19,000
J136	0.27	13,000	54.16	22,000	J136	0.27	13,000	56.65	23,000	J136	0.27	13,000	54.16	22,000	J136	0.27	13,000	42.55	21,000	J136	0.27	13,000	49.48	24,000
J137	0.27	13,000	53.50	20,000	J137	0.27	13,000	56.05	21,000	J137	0.27	13,000	53.50	20,000	J137	0.27	13,000	42.55	21,000	J137	0.27	13,000	49.48	24,000
J138	0.27	13,000	54.50	20,000	J138	0.27	13,000	57.05	21,000	J138	0.27	13,000	54.50	20,000	J138	0.27	13,000	42.55	21,000	J138	0.27	13,000	49.48	24,000
J139	0.27	13,000	53.92	21,000	J139	0.27	13,000	56.42	22,000	J139	0.27	13,000	53.92	21,000	J139	0.27	13,000	42.55	21,000	J139	0.27	13,000	49.48	24,000
J140	0.27	13,000	59.33	21,000	J140	0.27	13,000	61.83	22,000	J140	0.27	13,000	59.33	21,000	J140	0.27	13,000	42.55	21,000	J140	0.27	13,000	49.48	24,000
J141	0.27	13,000	53.12	21,000	J141	0.27	13,000	55.62	22,000	J141	0.27	13,000	53.12	21,000	J141	0.27	13,000	42.55	21,000	J141	0.27	13,000	49.48	24,000
J142	0.27	13,0																						

Option A - 2 Connections - Break Scenario 1 (Connection 1 Break)					Option A - 2 Connections with Upgrades on Danson Gardens Grv - Break Scenario 1 (Connection 1 Break)					Option B - 3 Connections - Break Scenario 1 (Connection 1 Break)				
Junction ID	Base Demand (AVDY, L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (AVDY, L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (AVDY, L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)
J01	0.07	13,000	48.30	27,000	J01	0.07	13,000	54.98	30,000	J01	0.07	13,000	37.19	18,000
J02	0.00	13,000	49.76	29,000	J02	0.00	13,000	56.44	31,000	J02	0.00	13,000	41.82	20,000
J05	0.07	13,000	50.90	30,000	J05	0.07	13,000	57.59	33,000	J05	0.07	13,000	45.39	23,000
J06	0.07	13,000	51.55	31,000	J06	0.07	13,000	58.24	34,000	J06	0.07	13,000	46.71	24,000
J07	0.11	13,000	52.50	33,000	J07	0.11	13,000	59.07	35,000	J07	0.11	13,000	47.54	24,000
J08	0.11	13,000	52.93	33,000	J08	0.11	13,000	59.62	37,000	J08	0.11	13,000	47.74	23,000
J09	0.11	13,000	53.00	35,000	J09	0.11	13,000	59.68	38,000	J09	0.11	13,000	47.66	25,000
J10	0.11	13,000	53.93	37,000	J10	0.11	13,000	60.61	41,000	J10	0.11	13,000	48.59	26,000
J100	0.15	13,000	40.21	20,000	J100	0.15	13,000	46.89	22,000	J100	0.15	13,000	38.32	19,000
J101	0.15	13,000	44.42	23,000	J101	0.15	13,000	51.10	25,000	J101	0.15	13,000	42.23	21,000
J102	0.15	13,000	45.10	22,000	J102	0.15	13,000	49.78	24,000	J102	0.15	13,000	40.98	20,000
J103	0.11	13,000	39.35	21,000	J103	0.15	13,000	43.03	21,000	J103	0.15	13,000	37.72	18,000
J109	0.11	13,000	42.95	22,000	J109	0.11	13,000	49.63	23,000	J109	0.11	13,000	40.22	19,000
J111	0.11	13,000	54.37	39,000	J111	0.11	13,000	61.05	43,000	J111	0.11	13,000	48.99	26,000
J110	0.11	13,000	43.52	22,000	J110	0.11	13,000	50.21	24,000	J110	0.11	13,000	40.61	20,000
J111	0.11	13,000	44.86	23,000	J111	0.11	13,000	51.54	25,000	J111	0.11	13,000	41.48	20,000
J112	0.11	13,000	40.47	20,000	J112	0.11	13,000	47.16	22,000	J112	0.11	13,000	36.41	18,000
J113	0.11	13,000	39.43	21,000	J113	0.11	13,000	46.83	23,000	J113	0.11	13,000	36.24	18,000
J114	0.11	13,000	31.53	16,000	J114	0.11	13,000	38.20	18,000	J114	0.11	13,000	27.10	15,000
J115	0.11	13,000	34.15	17,000	J115	0.11	13,000	40.83	19,000	J115	0.11	13,000	29.62	16,000
J116	0.11	13,000	37.01	18,000	J116	0.11	13,000	43.69	20,000	J116	0.11	13,000	32.38	16,000
J117	0.11	13,000	35.28	18,000	J117	0.11	13,000	41.96	19,000	J117	0.11	13,000	30.71	16,000
J118	0.11	13,000	39.76	20,000	J118	0.11	13,000	46.44	21,000	J118	0.11	13,000	35.26	17,000
J119	0.11	13,000	41.42	20,000	J119	0.11	13,000	48.01	22,000	J119	0.11	13,000	36.41	18,000
J120	0.11	13,000	55.23	20,000	J120	0.11	13,000	54.59	21,000	J120	0.11	13,000	50.84	20,000
J121	0.11	13,000	37.23	18,000	J121	0.11	13,000	43.91	20,000	J121	0.11	13,000	32.34	16,000
J122	0.11	13,000	31.00	16,000	J122	0.11	13,000	37.69	17,000	J122	0.11	13,000	25.92	15,000
J123	0.11	13,000	31.31	16,000	J123	0.11	13,000	37.99	18,000	J123	0.11	13,000	25.98	15,000
J124	0.11	13,000	38.25	19,000	J124	0.11	13,000	44.93	20,000	J124	0.11	13,000	32.46	18,000
J125	0.11	13,000	35.17	16,000	J125	0.11	13,000	46.83	20,000	J125	0.11	13,000	35.63	18,000
J128	0.00	6,000	51.77	14,000	J128	0.00	6,000	58.45	15,000	J128	0.00	6,000	51.87	13,000
J129	0.11	13,000	29.43	16,000	J129	0.11	13,000	36.12	17,000	J129	0.11	13,000	25.60	15,000
J130	0.11	13,000	32.94	17,000	J130	0.11	13,000	39.62	18,000	J130	0.11	13,000	29.19	15,000
J131	0.11	13,000	29.61	16,000	J131	0.11	13,000	36.29	17,000	J131	0.11	13,000	25.68	15,000
J132	0.11	13,000	33.18	17,000	J132	0.11	13,000	39.86	18,000	J132	0.11	13,000	29.08	15,000
J133	0.11	13,000	34.63	17,000	J133	0.11	13,000	40.51	18,000	J133	0.11	13,000	34.54	15,000
J134	0.11	13,000	31.27	16,000	J134	0.11	13,000	37.95	17,000	J134	0.11	13,000	25.49	15,000
J135	0.11	13,000	31.76	16,000	J135	0.11	13,000	38.44	18,000	J135	0.11	13,000	25.89	15,000
J136	0.11	13,000	33.75	17,000	J136	0.11	13,000	40.43	18,000	J136	0.11	13,000	27.79	15,000
J137	0.11	6,000	33.09	8,000	J137	0.11	6,000	39.78	8,000	J137	0.11	6,000	32.75	7,000
J14	0.11	6,000	50.72	13,000	J14	0.11	6,000	57.40	14,000	J14	0.11	6,000	50.37	12,000
J15	0.07	13,000	50.17	29,000	J15	0.07	13,000	56.85	32,000	J15	0.07	13,000	44.44	22,000
J152	0.11	13,000	47.28	16,000	J152	0.11	13,000	54.03	22,000	J152	0.11	13,000	42.47	20,000
J153	0.15	13,000	45.43	24,000	J153	0.15	13,000	52.11	26,000	J153	0.15	13,000	42.54	21,000
J154	0.11	13,000	45.00	23,000	J154	0.11	13,000	51.68	25,000	J154	0.11	13,000	39.26	19,000
J155	0.11	13,000	44.71	23,000	J155	0.11	13,000	51.39	25,000	J155	0.11	13,000	38.12	18,000
J156	0.00	13,000	43.55	22,000	J156	0.00	13,000	50.23	24,000	J156	0.00	13,000	34.49	17,000
J158	0.00	13,000	44.71	22,000	J158	0.00	13,000	56.00	24,000	J158	0.00	13,000	43.24	23,000
J160	0.00	13,000	49.97	31,000	J160	0.00	13,000	56.63	31,000	J160	0.00	13,000	44.68	22,000
J162	0.00	13,000	42.67	21,000	J162	0.00	13,000	49.36	23,000	J162	0.00	13,000	40.09	19,000
J164	0.00	13,000	41.33	20,000	J164	0.00	13,000	48.01	22,000	J164	0.00	13,000	38.65	19,000
J166	0.00	13,000	36.22	18,000	J166	0.00	13,000	42.90	19,000	J166	0.00	13,000	33.54	17,000
J168	0.00	13,000	33.10	17,000	J168	0.00	13,000	39.78	18,000	J168	0.00	13,000	30.42	16,000
J17	0.07	13,000	49.36	28,000	J17	0.07	13,000	56.04	30,000	J17	0.07	13,000	44.42	22,000
J170	0.00	13,000	42.73	21,000	J170	0.00	13,000	49.42	23,000	J170	0.00	13,000	40.27	20,000
J174	0.15	13,000	43.32	22,000	J174	0.15	13,000	50.00	24,000	J174	0.15	13,000	40.97	20,000
J176	0.15	13,000	44.32	22,000	J176	0.15	13,000	51.00	24,000	J176	0.15	13,000	42.07	20,000
J178	0.08	13,000	45.63	23,000	J178	0.08	13,000	52.31	26,000	J178	0.08	13,000	44.20	22,000
J18	0.07	13,000	48.76	27,000	J18	0.07	13,000	55.45	30,000	J18	0.07	13,000	44.83	22,000
J19	0.06	13,000	46.97	27,000	J19	0.06	13,000	53.80	30,000	J19	0.06	13,000	45.15	22,000
J20	0.10	13,000	45.50	27,000	J20	0.10	13,000	55.15	30,000	J20	0.10	13,000	44.77	22,000
J21	0.10	13,000	44.99	27,000	J21	0.10	13,000	55.41	30,000	J21	0.10	13,000	44.41	22,000
J22	0.10	13,000	47.99	26,000	J22	0.10	13,000	54.67	28,000	J22	0.10	13,000	45.14	23,000
J23	0.10	13,000	47.41	25,000	J23	0.10	13,000	54.09	27,000	J23	0.10	13,000	44.54	22,000
J24	0.10	13,000	46.87	25,000	J24	0.10	13,000	53.55	27,000	J24	0.10	13,000	43.94	22,000
J25	0.10	13,000	46.48	24,000	J25	0.10	13,000	53.16	26,000	J25	0.10	13,000	43.45	21,000
J26	0.10	13,000	45.53	24,000	J26	0.10	13,000	53.21	26,000	J26	0.10	13,000	43.45	21,000
J27	0.10	13,000	45.61	24,000	J27	0.10	13,000	53.37	26,000	J27	0.10	13,000	43.51	21,000
J29	0.10	13,000	48.82	24,000	J29	0.10	13,000	53.51	27,000	J29	0.10	13,000	43.51	21,000
J30	0.07	13,000	47.20	25,000	J30	0.07	13,000	53.88	27					

Option A - 2 Connections - Break Scenario 2 (Connection 2 Break)					Option A - 2 Connections - Break Scenario 2 (Connection 2 Break)					Option B - 3 Connections - Break Scenario 2 (Connection 2 Break)				
Junction ID	Base Demand (AVDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (AVDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (AVDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)
J01	0.07	13,000	57.11	37,000	J01	0.07	13,000	56.97	37,000	J01	0.07	13,000	49.66	25,000
J02	0.00	13,000	56.77	35,000	J02	0.00	13,000	56.63	34,000	J02	0.00	13,000	49.38	25,000
J05	0.07	13,000	56.55	33,000	J05	0.07	13,000	56.40	33,000	J05	0.07	13,000	49.29	24,000
J06	0.07	13,000	56.19	32,000	J06	0.07	13,000	56.05	32,000	J06	0.07	13,000	48.21	23,000
J07	0.11	13,000	55.73	31,000	J07	0.11	13,000	55.59	31,000	J07	0.11	13,000	46.50	22,000
J08	0.11	13,000	54.98	29,000	J08	0.11	13,000	54.83	29,000	J08	0.11	13,000	42.48	20,000
J09	0.11	13,000	53.96	29,000	J09	0.11	13,000	53.82	29,000	J09	0.11	13,000	40.35	19,000
J10	0.11	13,000	53.60	28,000	J10	0.11	13,000	53.46	28,000	J10	0.11	13,000	37.71	18,000
J100	0.15	13,000	45.49	21,000	J100	0.15	13,000	45.35	21,000	J100	0.15	13,000	40.77	19,000
J101	0.15	13,000	49.70	24,000	J101	0.15	13,000	49.55	24,000	J101	0.15	13,000	44.70	21,000
J102	0.15	13,000	48.38	23,000	J102	0.15	13,000	48.23	23,000	J102	0.15	13,000	43.44	20,000
J103	0.15	13,000	44.03	23,000	J103	0.15	13,000	43.88	23,000	J103	0.15	13,000	40.16	19,000
J109	0.11	13,000	48.22	23,000	J109	0.11	13,000	48.08	23,000	J109	0.11	13,000	42.60	20,000
J111	0.11	13,000	53.00	28,000	J111	0.11	13,000	52.85	27,000	J111	0.11	13,000	35.63	17,000
J110	0.11	13,000	48.80	23,000	J110	0.11	13,000	48.65	23,000	J110	0.11	13,000	42.99	20,000
J111	0.11	13,000	50.13	25,000	J111	0.11	13,000	49.98	25,000	J111	0.11	13,000	43.87	21,000
J112	0.11	13,000	45.74	21,000	J112	0.11	13,000	45.60	21,000	J112	0.11	13,000	38.79	18,000
J13	0.11	13,000	39.40	17,000	J13	0.11	13,000	37.78	17,000	J13	0.11	13,000	36.71	16,000
J14	0.11	13,000	36.79	17,000	J14	0.11	13,000	36.63	17,000	J14	0.11	13,000	29.48	15,000
J15	0.11	13,000	39.42	18,000	J15	0.11	13,000	39.28	18,000	J15	0.11	13,000	32.01	16,000
J16	0.11	13,000	42.28	20,000	J16	0.11	13,000	42.14	20,000	J16	0.11	13,000	34.76	17,000
J17	0.11	13,000	40.55	19,000	J17	0.11	13,000	40.41	19,000	J17	0.11	13,000	33.10	16,000
J18	0.11	13,000	45.03	21,000	J18	0.11	13,000	44.89	21,000	J18	0.11	13,000	37.64	18,000
J19	0.11	13,000	46.89	22,000	J19	0.11	13,000	46.55	22,000	J19	0.11	13,000	38.80	18,000
J20	0.11	13,000	50.25	21,000	J20	0.11	13,000	50.14	21,000	J20	0.11	13,000	42.65	21,000
J21	0.11	13,000	42.50	20,000	J21	0.11	13,000	42.36	20,000	J21	0.11	13,000	34.73	17,000
J22	0.11	13,000	36.27	17,000	J22	0.11	13,000	36.13	17,000	J22	0.11	13,000	28.31	15,000
J23	0.11	13,000	36.58	17,000	J23	0.11	13,000	36.44	17,000	J23	0.11	13,000	28.37	15,000
J24	0.11	13,000	43.52	20,000	J24	0.11	13,000	43.37	20,000	J24	0.11	13,000	34.85	17,000
J25	0.09	13,000	44.44	20,000	J25	0.09	13,000	44.33	20,000	J25	0.09	13,000	32.93	16,000
J28	0.00	6,000	56.92	15,000	J28	0.00	6,000	56.77	15,000	J28	0.00	6,000	54.54	14,000
J29	0.11	13,000	34.70	17,000	J29	0.11	13,000	34.56	17,000	J29	0.11	13,000	27.99	15,000
J30	0.11	13,000	38.21	18,000	J30	0.11	13,000	38.07	18,000	J30	0.11	13,000	31.58	16,000
J31	0.11	13,000	34.88	17,000	J31	0.11	13,000	34.74	17,000	J31	0.11	13,000	28.06	15,000
J32	0.11	13,000	38.45	18,000	J32	0.11	13,000	38.31	18,000	J32	0.11	13,000	31.47	16,000
J33	0.11	13,000	39.50	17,000	J33	0.11	13,000	39.45	17,000	J33	0.11	13,000	36.87	16,000
J34	0.11	13,000	35.54	17,000	J34	0.11	13,000	36.03	17,000	J34	0.11	13,000	27.87	15,000
J35	0.11	13,000	37.03	17,000	J35	0.11	13,000	36.89	17,000	J35	0.11	13,000	28.27	15,000
J37	0.11	6,000	38.24	8,000	J37	0.11	6,000	38.10	8,000	J37	0.11	6,000	35.41	8,000
J4	0.11	6,000	55.87	14,000	J4	0.11	6,000	55.73	14,000	J4	0.11	6,000	53.04	13,000
J5	0.07	13,000	55.63	32,000	J5	0.07	13,000	55.49	32,000	J5	0.07	13,000	47.65	23,000
J53	0.11	13,000	50.72	25,000	J53	0.15	13,000	50.58	25,000	J53	0.15	13,000	45.05	21,000
J54	0.11	13,000	50.27	25,000	J54	0.11	13,000	50.12	25,000	J54	0.11	13,000	41.65	19,000
J55	0.11	13,000	49.98	24,000	J55	0.11	13,000	49.84	24,000	J55	0.11	13,000	40.50	19,000
J56	0.00	13,000	48.82	23,000	J56	0.00	13,000	48.68	23,000	J56	0.00	13,000	36.88	17,000
J58	0.00	13,000	49.85	24,000	J58	0.00	13,000	49.84	24,000	J58	0.00	13,000	46.50	23,000
J60	0.07	13,000	55.36	31,000	J60	0.07	13,000	55.23	31,000	J60	0.07	13,000	47.69	23,000
J62	0.07	13,000	47.94	23,000	J62	0.00	13,000	47.80	23,000	J62	0.00	13,000	42.47	20,000
J64	0.00	13,000	46.80	22,000	J64	0.00	13,000	46.45	22,000	J64	0.00	13,000	41.03	19,000
J66	0.00	13,000	41.49	19,000	J66	0.00	13,000	41.35	19,000	J66	0.00	13,000	35.93	17,000
J68	0.00	13,000	38.37	18,000	J68	0.00	13,000	38.23	18,000	J68	0.00	13,000	32.81	16,000
J7	0.07	13,000	54.79	30,000	J7	0.07	13,000	54.56	30,000	J7	0.07	13,000	47.16	23,000
J72	0.00	13,000	33.00	17,000	J72	0.00	13,000	32.97	17,000	J72	0.00	13,000	34.54	16,000
J74	0.00	13,000	48.01	23,000	J74	0.00	13,000	47.87	23,000	J74	0.00	13,000	42.66	20,000
J76	0.15	13,000	48.59	23,000	J76	0.15	13,000	48.45	23,000	J76	0.15	13,000	43.36	20,000
J78	0.08	13,000	50.99	25,000	J78	0.08	13,000	50.76	25,000	J78	0.08	13,000	46.58	22,000
J8	0.07	13,000	54.07	21,000	J8	0.07	13,000	53.93	21,000	J8	0.07	13,000	47.41	23,000
J9	0.07	13,000	52.36	21,000	J9	0.07	13,000	52.23	21,000	J9	0.07	13,000	47.26	23,000
J21	0.10	13,000	52.66	21,000	J21	0.10	13,000	52.53	21,000	J21	0.10	13,000	46.14	22,000
J23	0.10	13,000	52.26	21,000	J23	0.10	13,000	52.12	21,000	J23	0.10	13,000	47.59	23,000
J25	0.10	13,000	52.67	27,000	J25	0.10	13,000	52.52	27,000	J25	0.10	13,000	46.99	23,000
J26	0.10	13,000	53.26	27,000	J26	0.10	13,000	53.13	27,000	J26	0.10	13,000	46.37	22,000
J28	0.10	13,000	52.67	27,000	J28	0.10	13,000	52.53	27,000	J28	0.10	13,000	46.67	22,000
J29	0.10	13,000	51.98	26,000	J29	0.10	13,000	51.81	26,000	J29	0.10	13,000	45.84	22,000
J30	0.07	13,000	52.30	27,000	J30	0.07	13,000	52.16	27,000	J30	0.07	13,000	46.09	22,000
J31	0.07	13,000	52.53	27,000	J31	0.07	13,000	52.39	27,000	J31	0.07	13,000	46.23	22,000
J32	0.07	13,000	52.85	27,000	J32	0.07	13,000	52.71	27,000	J32	0.07	13,000	46.41	22,000
J33	0.07	13,000	53.45	27,000	J33	0.07	13,000	53.31	27,000	J33	0.07	13,000	46.89	22,000
J34	0.07	13,000	54.03	29,000	J34	0.07	13,000	53.89	29,000	J34	0.07	13,000	47.33	23,000
J35	0.07	13,000	54.38	29,000	J35	0.07	13,000	54.22	29,000	J35	0.07	13,000	47.40	23,000
J36	0.07	13,000	55.24	30,000	J36	0.07	13,000	55.10	3					

Option A - 2 Connections - Break Scenario 3					Option A - 2 Connections - Break Scenario 3					Option B - 3 Connections - Break Scenario 3				
Junction ID	Base Demand (AVDY, L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (AVDY, L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (AVDY, L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)
J01	0.07	13,000	58.88	64,000	J01	0.07	13,000	62.42	67,000	J01	0.07	13,000	54.26	34,000
J02	0.00	13,000	59.33	64,000	J02	0.00	13,000	62.99	66,000	J02	0.00	13,000	55.02	35,000
J05	0.07	13,000	59.72	64,000	J05	0.07	13,000	63.49	66,000	J05	0.07	13,000	55.82	36,000
J06	0.07	13,000	59.80	64,000	J06	0.07	13,000	63.66	66,000	J06	0.07	13,000	55.83	36,000
J07	0.11	13,000	59.91	64,000	J07	0.11	13,000	63.86	67,000	J07	0.11	13,000	55.59	35,000
J08	0.11	13,000	59.94	65,000	J08	0.11	13,000	64.84	67,000	J08	0.11	13,000	55.69	34,000
J09	0.11	13,000	59.91	65,000	J09	0.11	13,000	63.41	66,000	J09	0.11	13,000	54.37	34,000
J10	0.11	13,000	59.45	66,000	J10	0.11	13,000	63.79	69,000	J10	0.11	13,000	54.48	34,000
J100	0.15	13,000	35.77	17,000	J100	0.15	13,000	39.59	18,000	J100	0.15	13,000	43.83	21,000
J101	0.15	13,000	43.09	21,000	J101	0.15	13,000	46.91	22,000	J101	0.15	13,000	50.19	27,000
J102	0.15	13,000	40.83	20,000	J102	0.15	13,000	44.65	21,000	J102	0.15	13,000	49.36	26,000
J103	0.11	13,000	33.95	16,000	J103	0.15	13,000	40.03	17,000	J103	0.15	13,000	43.12	21,000
J109	0.11	13,000	37.06	18,000	J109	0.11	13,000	40.88	19,000	J109	0.11	13,000	46.67	23,000
J111	0.11	13,000	59.34	67,000	J111	0.11	13,000	63.80	71,000	J111	0.11	13,000	54.34	34,000
J110	0.11	13,000	37.31	18,000	J110	0.11	13,000	41.13	19,000	J110	0.11	13,000	46.79	23,000
J111	0.11	13,000	38.13	18,000	J111	0.11	13,000	41.95	19,000	J111	0.11	13,000	47.31	23,000
J112	0.11	13,000	33.57	17,000	J112	0.11	13,000	37.39	17,000	J112	0.11	13,000	42.15	20,000
J113	0.11	13,000	24.50	13,000	J113	0.11	13,000	24.50	13,000	J113	0.11	13,000	24.50	13,000
J114	0.11	13,000	24.58	14,000	J114	0.11	13,000	28.40	15,000	J114	0.11	13,000	32.83	16,000
J115	0.11	13,000	27.21	15,000	J115	0.11	13,000	31.03	16,000	J115	0.11	13,000	35.36	17,000
J117	0.11	13,000	28.33	15,000	J117	0.11	13,000	32.15	16,000	J117	0.11	13,000	36.45	18,000
J118	0.11	13,000	32.81	16,000	J118	0.11	13,000	36.64	17,000	J118	0.11	13,000	40.99	19,000
J119	0.11	13,000	34.45	17,000	J119	0.11	13,000	38.27	18,000	J119	0.11	13,000	42.14	20,000
J120	0.11	13,000	35.27	17,000	J120	0.11	13,000	38.91	17,000	J120	0.11	13,000	40.75	19,000
J121	0.11	13,000	30.27	16,000	J121	0.11	13,000	34.09	16,000	J121	0.11	13,000	38.07	18,000
J122	0.11	13,000	24.03	14,000	J122	0.11	13,000	27.86	15,000	J122	0.11	13,000	31.65	16,000
J123	0.11	13,000	24.33	14,000	J123	0.11	13,000	28.15	15,000	J123	0.11	13,000	31.71	16,000
J124	0.11	13,000	31.25	16,000	J124	0.11	13,000	35.09	17,000	J124	0.11	13,000	38.19	18,000
J125	0.09	13,000	55.45	13,000	J125	0.11	13,000	62.63	15,000	J125	0.11	13,000	55.63	17,000
J128	0.00	6,000	53.34	13,000	J128	0.00	6,000	55.37	13,000	J128	0.00	6,000	54.39	14,000
J129	0.11	13,000	22.43	14,000	J129	0.11	13,000	26.25	15,000	J129	0.11	13,000	31.31	16,000
J130	0.11	13,000	25.93	15,000	J130	0.11	13,000	29.75	15,000	J130	0.11	13,000	34.90	17,000
J131	0.11	13,000	22.60	14,000	J131	0.11	13,000	26.43	15,000	J131	0.11	13,000	31.39	16,000
J132	0.11	13,000	26.18	15,000	J132	0.11	13,000	30.00	15,000	J132	0.11	13,000	34.79	17,000
J133	0.11	13,000	23.43	14,000	J133	0.11	13,000	24.15	15,000	J133	0.11	13,000	28.41	17,000
J134	0.11	13,000	24.28	14,000	J134	0.11	13,000	28.81	15,000	J134	0.11	13,000	31.21	16,000
J135	0.11	13,000	24.77	14,000	J135	0.11	13,000	28.59	15,000	J135	0.11	13,000	31.61	16,000
J137	0.11	6,000	34.66	8,000	J137	0.11	6,000	36.70	8,000	J137	0.11	6,000	35.26	8,000
J14	0.11	6,000	52.29	12,000	J14	0.11	6,000	54.33	13,000	J14	0.11	6,000	52.89	13,000
J15	0.07	13,000	56.83	35,000	J15	0.07	13,000	62.63	35,000	J15	0.07	13,000	54.10	32,000
J152	0.11	13,000	56.25	35.00	J152	0.11	13,000	60.34	36,000	J152	0.11	13,000	59.63	37,000
J153	0.15	13,000	52.72	31,000	J153	0.15	13,000	56.54	33,000	J153	0.15	13,000	51.15	28,000
J154	0.11	13,000	38.00	18,000	J154	0.11	13,000	41.83	19,000	J154	0.11	13,000	44.98	22,000
J155	0.11	13,000	37.72	18,000	J155	0.11	13,000	41.54	19,000	J155	0.11	13,000	43.84	21,000
J156	0.00	13,000	36.56	18,000	J156	0.00	13,000	40.39	19,000	J156	0.00	13,000	40.22	19,000
J158	0.00	13,000	36.83	18,000	J158	0.00	13,000	40.65	19,000	J158	0.00	13,000	40.53	25,000
J160	0.07	13,000	55.37	35.00	J160	0.07	13,000	62.63	35,000	J160	0.07	13,000	53.84	32,000
J162	0.00	13,000	37.17	18,000	J162	0.00	13,000	40.99	19,000	J162	0.00	13,000	46.88	23,000
J164	0.00	13,000	35.57	17,000	J164	0.00	13,000	39.39	18,000	J164	0.00	13,000	45.22	22,000
J166	0.00	13,000	30.46	16,000	J166	0.00	13,000	34.28	17,000	J166	0.00	13,000	40.11	19,000
J168	0.00	13,000	27.34	15,000	J168	0.00	13,000	31.16	16,000	J168	0.00	13,000	36.99	18,000
J17	0.07	13,000	57.92	48,000	J17	0.07	13,000	61.74	50,000	J17	0.07	13,000	53.35	31,000
J172	0.00	13,000	37.47	18,000	J172	0.00	13,000	41.56	19,000	J172	0.00	13,000	47.47	24,000
J174	0.15	13,000	39.29	19,000	J174	0.15	13,000	43.12	20,000	J174	0.15	13,000	48.90	25,000
J176	0.15	13,000	38.64	19,000	J176	0.15	13,000	42.46	19,000	J176	0.15	13,000	48.63	25,000
J178	0.08	13,000	38.14	18,000	J178	0.08	13,000	41.97	19,000	J178	0.08	13,000	49.15	25,000
J18	0.07	13,000	57.29	48,000	J18	0.07	13,000	61.11	49,000	J18	0.07	13,000	53.36	31,000
J19	0.10	13,000	39.65	19,000	J19	0.10	13,000	46.81	20,000	J19	0.10	13,000	52.10	29,000
J20	0.10	13,000	57.09	43,000	J20	0.10	13,000	60.82	45,000	J20	0.10	13,000	52.67	30,000
J21	0.11	13,000	55.33	42,000	J21	0.11	13,000	60.41	43,000	J21	0.11	13,000	51.53	32,000
J22	0.10	13,000	56.33	40,000	J22	0.10	13,000	60.15	42,000	J22	0.10	13,000	51.54	28,000
J23	0.10	13,000	58.81	38,000	J23	0.10	13,000	59.63	40,000	J23	0.10	13,000	51.54	28,000
J24	0.10	13,000	56.16	39,000	J24	0.10	13,000	59.98	40,000	J24	0.10	13,000	52.74	30,000
J25	0.10	13,000	56.65	39,000	J25	0.10	13,000	60.51	40,000	J25	0.10	13,000	53.63	30,000
J26	0.10	13,000	57.38	43,000	J26	0.10	13,000	61.21	45,000	J26	0.10	13,000	54.97	32,000
J27	0.07	13,000	57.76	46,000	J27	0.07	13,000	61.59	47,000	J27	0.07	13,000	54.31	32,000
J28	0.07	13,000	56.77	38,000	J28	0.07	13,000	59.50	40,000	J28	0.07	13,000	49.32	25,000
J29	0.08	13,000	38.93	19,000	J29	0.08	13,000	42.75	20,000	J29	0.08	13,000	48.87	25,000
J30	0.07	13,000	39.65	19,000	J30	0.07	13,000	42.90	20,000	J30	0.07	13,000	49.53	25,000
J31	0.07	13,000	55.82	37,000	J31	0.07	13,000	59.65	39,000	J31	0.07	13,000	52.38	29,000

Option A - 2 Connections with Upgrades on Danson Gardens Grv - Break Scenario 4					Option A - 2 Connections - Break Scenario 4					Option B - 3 Connections - Break Scenario 4				
Junction ID	Base Demand (AVDY, L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (AVDY, L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (AVDY, L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)
J01	0.07	13,000	58.88	64,000	J01	0.07	13,000	62.42	67,000	J01	0.07	13,000	54.45	34,000
J02	0.00	13,000	59.33	64,000	J02	0.00	13,000	62.99	66,000	J02	0.00	13,000	55.26	35,000
J05	0.07	13,000	59.72	64,000	J05	0.07	13,000	63.49	66,000	J05	0.07	13,000	56.09	37,000
J06	0.07	13,000	59.80	64,000	J06	0.07	13,000	63.65	66,000	J06	0.07	13,000	56.12	37,000
J07	0.11	13,000	59.91	64,000	J07	0.11	13,000	63.84	67,000	J07	0.11	13,000	55.84	36,000
J08	0.11	13,000	59.94	65,000	J08	0.11	13,000	63.84	67,000	J08	0.11	13,000	55.89	35,000
J09	0.11	13,000	59.91	65,000	J09	0.11	13,000	63.41	66,000	J09	0.11	13,000	54.56	34,000
J10	0.11	13,000	59.45	66,000	J10	0.11	13,000	63.79	69,000	J10	0.11	13,000	54.64	34,000
J100	0.15	13,000	48.98	26,000	J100	0.15	13,000	52.80	27,000	J100	0.15	13,000	46.57	23,000
J101	0.15	13,000	54.27	35,000	J101	0.15	13,000	58.09	36,000	J101	0.15	13,000	51.83	29,000
J102	0.15	13,000	53.96	34,000	J102	0.15	13,000	57.78	35,000	J102	0.15	13,000	51.53	29,000
J103	0.15	13,000	48.65	33,000	J103	0.15	13,000	53.03	33,000	J103	0.15	13,000	45.59	23,000
J109	0.11	13,000	45.11	22,000	J109	0.11	13,000	48.94	23,000	J109	0.11	13,000	42.65	20,000
J111	0.11	13,000	59.34	67,000	J111	0.11	13,000	63.80	71,000	J111	0.11	13,000	54.48	34,000
J110	0.11	13,000	42.73	21,000	J110	0.11	13,000	46.55	22,000	J110	0.11	13,000	40.26	19,000
J111	0.11	13,000	38.74	19,000	J111	0.11	13,000	42.56	19,000	J111	0.11	13,000	36.28	17,000
J112	0.11	13,000	33.38	17,000	J112	0.11	13,000	37.21	17,000	J112	0.11	13,000	30.46	15,000
J13	0.11	13,000	25.63	11,000	J13	0.11	13,000	29.20	11,000	J13	0.11	13,000	22.71	4,000
J14	0.11	13,000	24.16	14,000	J14	0.11	13,000	29.21	15,000	J14	0.11	13,000	21.00	14,000
J15	0.11	13,000	26.76	15,000	J15	0.11	13,000	30.59	16,000	J15	0.11	13,000	23.48	14,000
J16	0.11	13,000	29.56	16,000	J16	0.11	13,000	33.39	16,000	J16	0.11	13,000	26.19	15,000
J17	0.11	13,000	27.87	15,000	J17	0.11	13,000	31.69	16,000	J17	0.11	13,000	24.55	14,000
J18	0.11	13,000	32.38	16,000	J18	0.11	13,000	36.20	17,000	J18	0.11	13,000	29.11	15,000
J19	0.11	13,000	35.73	17,000	J19	0.11	13,000	37.55	17,000	J19	0.11	13,000	30.95	16,000
J20	0.11	13,000	35.97	17,000	J20	0.11	13,000	37.23	17,000	J20	0.11	13,000	34.69	30,000
J21	0.11	13,000	29.65	16,000	J21	0.11	13,000	33.47	16,000	J21	0.11	13,000	26.08	15,000
J22	0.11	13,000	23.34	14,000	J22	0.11	13,000	27.17	15,000	J22	0.11	13,000	19.60	13,000
J23	0.11	13,000	23.56	14,000	J23	0.11	13,000	27.38	15,000	J23	0.11	13,000	19.60	13,000
J24	0.11	13,000	30.36	16,000	J24	0.11	13,000	34.18	16,000	J24	0.11	13,000	26.00	15,000
J25	0.11	13,000	22.45	15,000	J25	0.11	13,000	30.25	16,000	J25	0.11	13,000	23.52	14,000
J28	0.00	6,000	53.07	12,000	J28	0.00	6,000	55.10	13,000	J28	0.00	6,000	51.18	12,000
J29	0.11	13,000	20.88	14,000	J29	0.11	13,000	24.70	14,000	J29	0.11	13,000	18.33	13,000
J30	0.11	13,000	24.37	14,000	J30	0.11	13,000	28.19	15,000	J30	0.11	13,000	21.86	14,000
J31	0.11	13,000	21.07	14,000	J31	0.11	13,000	24.90	14,000	J31	0.11	13,000	18.46	13,000
J32	0.11	13,000	24.67	14,000	J32	0.11	13,000	28.49	15,000	J32	0.11	13,000	21.92	14,000
J33	0.11	13,000	24.53	14,000	J33	0.11	13,000	28.43	15,000	J33	0.11	13,000	21.41	14,000
J34	0.11	13,000	22.97	14,000	J34	0.11	13,000	26.80	15,000	J34	0.11	13,000	18.78	13,000
J35	0.11	13,000	23.47	14,000	J35	0.11	13,000	27.29	15,000	J35	0.11	13,000	19.20	13,000
J36	0.11	13,000	25.46	15,000	J36	0.11	13,000	29.29	15,000	J36	0.11	13,000	21.11	14,000
J37	0.11	6,000	34.45	8,000	J37	0.11	6,000	36.49	8,000	J37	0.11	6,000	32.18	7,000
J4	0.07	13,000	50.00	13,000	J4	0.07	13,000	54.11	13,000	J4	0.07	13,000	49.80	12,000
J5	0.07	13,000	50.63	13,000	J5	0.07	13,000	57.25	13,000	J5	0.07	13,000	54.58	33,000
J6	0.07	13,000	55.41	13,000	J6	0.07	13,000	62.65	13,000	J6	0.07	13,000	52.40	32,000
J53	0.15	13,000	54.09	13,000	J53	0.15	13,000	57.91	13,000	J53	0.15	13,000	51.14	28,000
J54	0.11	13,000	36.69	18,000	J54	0.11	13,000	40.51	19,000	J54	0.11	13,000	32.53	16,000
J55	0.11	13,000	36.45	18,000	J55	0.11	13,000	40.28	18,000	J55	0.11	13,000	31.48	16,000
J56	0.00	13,000	35.33	17,000	J56	0.00	13,000	39.16	18,000	J56	0.00	13,000	27.90	15,000
J58	0.00	13,000	52.43	31,000	J58	0.00	13,000	57.25	31,000	J58	0.00	13,000	52.44	30,000
J60	0.07	13,000	55.57	32,000	J60	0.07	13,000	62.65	32,000	J60	0.07	13,000	53.25	31,000
J62	0.07	13,000	47.64	24,000	J62	0.07	13,000	51.47	25,000	J62	0.07	13,000	45.18	22,000
J64	0.00	13,000	44.58	22,000	J64	0.00	13,000	48.39	23,000	J64	0.00	13,000	42.10	20,000
J66	0.00	13,000	39.45	19,000	J66	0.00	13,000	43.28	20,000	J66	0.00	13,000	36.99	18,000
J68	0.00	13,000	36.33	18,000	J68	0.00	13,000	40.16	18,000	J68	0.00	13,000	33.87	17,000
J7	0.07	13,000	57.93	18,000	J7	0.07	13,000	61.74	19,000	J7	0.07	13,000	53.59	31,000
J72	0.00	13,000	50.22	27,000	J72	0.00	13,000	54.05	28,000	J72	0.00	13,000	47.76	24,000
J74	0.15	13,000	53.58	33,000	J74	0.15	13,000	57.39	34,000	J74	0.15	13,000	51.10	28,000
J76	0.15	13,000	53.99	33,000	J76	0.15	13,000	57.81	35,000	J76	0.15	13,000	51.44	28,000
J78	0.08	13,000	54.49	34,000	J78	0.08	13,000	58.31	36,000	J78	0.08	13,000	52.27	29,000
J8	0.07	13,000	57.30	46,000	J8	0.07	13,000	61.12	49,000	J8	0.07	13,000	53.59	32,000
J9	0.06	13,000	57.26	46,000	J9	0.06	13,000	61.05	49,000	J9	0.06	13,000	53.46	32,000
J10	0.07	13,000	52.53	41,000	J10	0.07	13,000	56.35	43,000	J10	0.07	13,000	52.41	31,000
J12	0.07	13,000	53.46	41,000	J12	0.07	13,000	57.15	43,000	J12	0.07	13,000	52.81	29,000
J14	0.07	13,000	53.49	41,000	J14	0.07	13,000	57.28	43,000	J14	0.07	13,000	53.30	30,000
J16	0.07	13,000	57.38	43,000	J16	0.07	13,000	61.21	45,000	J16	0.07	13,000	54.48	33,000
J18	0.08	13,000	49.29	24,000	J18	0.08	13,000	52.52	25,000	J18	0.08	13,000	45.31	22,000
J20	0.07	13,000	56.08	23,000	J20	0.07	13,000	59.91	24,000	J20	0.07	13,000	54.51	33,000
J22	0.19	13,000	55.12	35,000	J22	0.19	13,000	58.95	37,000	J22	0.19	13,000	52.26	29,000
J29	0.10	13,000	55.25	36,000	J29	0.10	13,000	59.07	37,000	J29	0.10	13,000	52.38	29,000
J30	0.07	13,000	55.60	37,000	J30	0.07	13,000	59.43	39,000	J30	0.07	13,000	52.72	30,000
J31	0.07	13,000	55.84	37,000	J31	0.07	13,000	59.67	39,000	J31	0.07	13,000	52.95	30,000
J32	0.07	13,000	56.17	39,000	J32	0.07	13,000	60.00	40,000	J32</				

Option A - 2 Connections with Upgrades on Danson Gardens Grv - Break Scenario 5					Option A - 2 Connections - Break Scenario 5					Option B - 3 Connections - Break Scenario 5				
Junction ID	Base Demand (AVDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (AVDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (AVDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)
J01	0.07	13,000	58.88	64,000	J01	0.07	13,000	62.42	67,000	J01	0.07	13,000	54.31	34,000
J02	0.00	13,000	59.33	64,000	J02	0.00	13,000	62.99	66,000	J02	0.00	13,000	55.09	35,000
J05	0.07	13,000	59.72	64,000	J05	0.07	13,000	63.49	66,000	J05	0.07	13,000	55.90	37,000
J06	0.07	13,000	59.80	64,000	J06	0.07	13,000	63.65	66,000	J06	0.07	13,000	55.92	37,000
J07	0.11	13,000	59.91	64,000	J07	0.11	13,000	63.82	67,000	J07	0.11	13,000	55.48	36,000
J08	0.11	13,000	59.94	65,000	J08	0.11	13,000	63.84	67,000	J08	0.11	13,000	55.45	35,000
J09	0.11	13,000	59.91	65,000	J09	0.11	13,000	63.41	66,000	J09	0.11	13,000	54.43	34,000
J10	0.11	13,000	59.45	66,000	J10	0.11	13,000	63.79	69,000	J10	0.11	13,000	54.53	34,000
J100	0.15	13,000	49.00	26,000	J100	0.15	13,000	52.83	27,000	J100	0.15	13,000	46.25	23,000
J101	0.15	13,000	54.39	35,000	J101	0.15	13,000	58.21	36,000	J101	0.15	13,000	51.70	29,000
J102	0.15	13,000	54.18	35,000	J102	0.15	13,000	58.00	36,000	J102	0.15	13,000	51.55	29,000
J103	0.15	13,000	48.47	31,000	J103	0.15	13,000	52.05	32,000	J103	0.15	13,000	45.51	23,000
J109	0.11	13,000	52.53	31,000	J109	0.11	13,000	56.36	32,000	J109	0.11	13,000	49.58	26,000
J111	0.11	13,000	59.34	67,000	J111	0.11	13,000	63.80	71,000	J111	0.11	13,000	54.38	34,000
J110	0.11	13,000	52.86	31,000	J110	0.11	13,000	56.68	32,000	J110	0.11	13,000	49.72	26,000
J111	0.11	13,000	53.86	33,000	J111	0.11	13,000	57.68	34,000	J111	0.11	13,000	50.27	26,000
J112	0.11	13,000	49.40	26,000	J112	0.11	13,000	53.22	27,000	J112	0.11	13,000	45.11	22,000
J113	0.11	13,000	49.53	26,000	J113	0.11	13,000	53.41	27,000	J113	0.11	13,000	45.71	23,000
J114	0.11	13,000	49.43	19,000	J114	0.11	13,000	44.26	20,000	J114	0.11	13,000	38.80	17,000
J115	0.11	13,000	43.08	21,000	J115	0.11	13,000	46.89	22,000	J115	0.11	13,000	38.32	18,000
J116	0.11	13,000	45.92	23,000	J116	0.11	13,000	49.74	24,000	J116	0.11	13,000	41.07	20,000
J117	0.11	13,000	44.19	21,000	J117	0.11	13,000	48.01	22,000	J117	0.11	13,000	39.41	19,000
J118	0.11	13,000	48.67	25,000	J118	0.11	13,000	52.49	26,000	J118	0.11	13,000	43.95	21,000
J119	0.11	13,000	50.32	27,000	J119	0.11	13,000	54.14	28,000	J119	0.11	13,000	46.10	22,000
J120	0.11	13,000	50.37	27,000	J120	0.11	13,000	54.09	27,000	J120	0.11	13,000	45.71	21,000
J121	0.11	13,000	46.13	23,000	J121	0.11	13,000	49.96	24,000	J121	0.11	13,000	41.03	20,000
J122	0.11	13,000	39.90	19,000	J122	0.11	13,000	43.73	20,000	J122	0.11	13,000	34.62	17,000
J123	0.11	13,000	40.20	19,000	J123	0.11	13,000	44.03	20,000	J123	0.11	13,000	34.67	17,000
J124	0.11	13,000	47.14	24,000	J124	0.11	13,000	50.96	25,000	J124	0.11	13,000	41.15	20,000
J125	0.09	13,000	44.07	24,000	J125	0.09	13,000	52.05	25,000	J125	0.09	13,000	38.65	18,000
J128	0.00	6,000	57.00	16,000	J128	0.00	6,000	59.04	17,000	J128	0.00	6,000	54.73	15,000
J129	0.11	13,000	38.32	18,000	J129	0.11	13,000	42.15	19,000	J129	0.11	13,000	34.28	17,000
J130	0.11	13,000	41.82	20,000	J130	0.11	13,000	45.65	21,000	J130	0.11	13,000	37.86	18,000
J131	0.11	13,000	38.50	18,000	J131	0.11	13,000	42.32	19,000	J131	0.11	13,000	34.35	17,000
J132	0.11	13,000	42.07	20,000	J132	0.11	13,000	45.89	21,000	J132	0.11	13,000	37.76	18,000
J133	0.11	13,000	45.31	21,000	J133	0.11	13,000	48.41	22,000	J133	0.11	13,000	38.41	18,000
J134	0.11	13,000	40.16	19,000	J134	0.11	13,000	43.99	20,000	J134	0.11	13,000	34.17	17,000
J135	0.11	13,000	40.65	19,000	J135	0.11	13,000	44.47	20,000	J135	0.11	13,000	34.57	17,000
J136	0.11	13,000	42.64	20,000	J136	0.11	13,000	46.47	21,000	J136	0.11	13,000	36.47	17,000
J137	0.11	6,000	38.33	8,000	J137	0.11	6,000	40.36	8,000	J137	0.11	6,000	35.60	8,000
J14	0.11	6,000	55.95	15,000	J14	0.11	6,000	57.99	15,000	J14	0.11	6,000	53.23	14,000
J15	0.07	13,000	58.83	15,000	J15	0.07	13,000	60.56	15,000	J15	0.07	13,000	54.15	15,000
J16	0.07	13,000	58.45	15,000	J16	0.07	13,000	62.63	15,000	J16	0.07	13,000	53.67	15,000
J162	0.00	13,000	52.56	31,000	J162	0.00	13,000	56.38	32,000	J162	0.00	13,000	49.74	26,000
J164	0.00	13,000	51.01	28,000	J164	0.00	13,000	54.83	29,000	J164	0.00	13,000	48.11	24,000
J166	0.00	13,000	45.90	23,000	J166	0.00	13,000	49.73	24,000	J166	0.00	13,000	43.00	21,000
J168	0.00	13,000	42.78	21,000	J168	0.00	13,000	46.61	21,000	J168	0.00	13,000	39.88	19,000
J17	0.07	13,000	57.93	48,000	J17	0.07	13,000	61.74	50,000	J17	0.07	13,000	53.34	31,000
J172	0.00	13,000	52.99	32,000	J172	0.00	13,000	56.81	33,000	J172	0.00	13,000	50.29	27,000
J174	0.15	13,000	54.23	34,000	J174	0.15	13,000	58.05	36,000	J174	0.15	13,000	51.64	28,000
J176	0.15	13,000	54.08	34,000	J176	0.15	13,000	57.91	35,000	J176	0.15	13,000	51.52	28,000
J178	0.08	13,000	53.48	32,000	J178	0.08	13,000	57.30	33,000	J178	0.08	13,000	52.30	29,000
J18	0.07	13,000	57.30	46,000	J18	0.07	13,000	61.12	48,000	J18	0.07	13,000	53.31	31,000
J180	0.07	13,000	59.71	46,000	J180	0.07	13,000	54.55	48,000	J180	0.07	13,000	51.65	36,000
J182	0.08	13,000	47.96	24,000	J182	0.08	13,000	50.07	25,000	J182	0.08	13,000	51.62	28,000
J184	0.08	13,000	46.35	23,000	J184	0.08	13,000	50.17	24,000	J184	0.08	13,000	51.46	27,000
J186	0.08	13,000	55.18	36,000	J186	0.08	13,000	59.00	38,000	J186	0.08	13,000	52.59	30,000
J188	0.00	13,000	52.47	31,000	J188	0.00	13,000	56.30	32,000	J188	0.00	13,000	49.57	26,000
J189	0.08	13,000	55.90	39,000	J189	0.08	13,000	59.72	40,000	J189	0.08	13,000	52.66	30,000
J190	0.08	13,000	56.60	39,000	J190	0.08	13,000	59.85	37,000	J190	0.08	13,000	52.53	30,000
J191	0.07	13,000	55.84	37,000	J191	0.07	13,000	59.43	39,000	J191	0.07	13,000	52.46	29,000
J192	0.07	13,000	56.17	39,000	J192	0.07	13,000	59.67	39,000	J192	0.07	13,000	52.69	29,000
J193	0.07	13,000	56.93	39,000	J193	0.07	13,000	52.57	26,000	J193	0.07	13,000	49.01	21,000
J194	0.07	13,000	56.29	39,000	J194	0.07	13,000	52.05	26,000	J194	0.07	13,000	47.63	23,000
J195	0.07	13,000	56.53	39,000	J195	0.07	13,000	56.74	37,000	J195	0.07	13,000	51.42	28,000
J196	0.11	13,000	54.92	36,000	J196	0.11	13,000	58.56	36,000	J196	0.11	13,000	50.83	27,000
J197	0.11	13,000	54.74	35,000	J197	0.11	13,000	58.02	35,000	J197	0.11	13,000	49.19	25,000
J198	0.11	13,000	53.81	33,000	J198	0.11	13,000	57.63	34,000	J198	0.11	13,000	44.50	21,000
J199	0.11	13,000	52.77	33,000	J199	0.11	13,000	56.59	32,000	J199	0.11	13,000	44.51	21,000
J200	0.11	13,000	53.12	68,000	J200	0.11	13,000	58.95	70,					

Option A - 2 Connections with Upgrades on Danson Gardens Grv - Break Scenario 6					Option A - 2 Connections - Break Scenario 6					Option B - 3 Connections - Break Scenario 6				
Junction ID	Base Demand (AVDY, L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (AVDY, L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (AVDY, L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)
J01	0.07	13,000	58.88	64,000	J01	0.07	13,000	62.42	67,000	J01	0.07	13,000	54.45	34,000
J02	0.00	13,000	59.33	64,000	J02	0.00	13,000	62.99	66,000	J02	0.00	13,000	55.26	35,000
J05	0.07	13,000	59.72	64,000	J05	0.07	13,000	63.49	66,000	J05	0.07	13,000	56.09	37,000
J06	0.07	13,000	59.80	64,000	J06	0.07	13,000	63.65	66,000	J06	0.07	13,000	56.12	37,000
J07	0.11	13,000	59.91	64,000	J07	0.11	13,000	63.82	67,000	J07	0.11	13,000	55.85	36,000
J08	0.11	13,000	59.94	65,000	J08	0.11	13,000	63.84	67,000	J08	0.11	13,000	55.99	35,000
J09	0.11	13,000	59.91	65,000	J09	0.11	13,000	63.41	66,000	J09	0.11	13,000	54.56	34,000
J10	0.11	13,000	59.45	66,000	J10	0.11	13,000	63.79	69,000	J10	0.11	13,000	54.64	34,000
J100	0.15	13,000	48.99	26,000	J100	0.15	13,000	52.81	27,000	J100	0.15	13,000	46.58	23,000
J101	0.15	13,000	54.29	35,000	J101	0.15	13,000	58.11	36,000	J101	0.15	13,000	51.85	29,000
J102	0.15	13,000	53.99	34,000	J102	0.15	13,000	57.81	35,000	J102	0.15	13,000	51.56	29,000
J103	0.15	13,000	48.67	23,000	J103	0.15	13,000	52.99	24,000	J103	0.15	13,000	48.01	23,000
J109	0.11	13,000	46.16	23,000	J109	0.11	13,000	49.99	24,000	J109	0.11	13,000	40.28	19,000
J115	0.11	13,000	59.34	67,000	J115	0.11	13,000	63.80	71,000	J115	0.11	13,000	54.48	34,000
J116	0.11	13,000	48.81	25,000	J116	0.11	13,000	52.64	26,000	J116	0.11	13,000	42.93	20,000
J117	0.11	13,000	52.84	31,000	J117	0.11	13,000	56.66	32,000	J117	0.11	13,000	46.95	23,000
J118	0.11	13,000	48.94	25,000	J118	0.11	13,000	52.77	27,000	J118	0.11	13,000	42.54	20,000
J119	0.11	13,000	50.06	27,000	J119	0.11	13,000	53.88	28,000	J119	0.11	13,000	42.79	20,000
J120	0.11	13,000	59.37	67,000	J120	0.11	13,000	52.52	26,000	J120	0.11	13,000	41.40	20,000
J121	0.11	13,000	45.85	23,000	J121	0.11	13,000	49.68	24,000	J121	0.11	13,000	38.69	18,000
J122	0.11	13,000	39.64	19,000	J122	0.11	13,000	43.46	20,000	J122	0.11	13,000	32.29	16,000
J123	0.11	13,000	39.96	19,000	J123	0.11	13,000	43.78	20,000	J123	0.11	13,000	32.37	16,000
J124	0.11	13,000	45.92	23,000	J124	0.11	13,000	50.74	24,000	J124	0.11	13,000	38.88	18,000
J125	0.09	13,000	49.35	24,000	J125	0.09	13,000	52.05	25,000	J125	0.09	13,000	36.51	17,000
J128	0.00	6,000	56.96	16,000	J128	0.00	6,000	59.00	16,000	J128	0.00	6,000	54.32	14,000
J129	0.11	13,000	38.15	18,000	J129	0.11	13,000	41.98	19,000	J129	0.11	13,000	32.15	16,000
J130	0.11	13,000	41.66	20,000	J130	0.11	13,000	45.48	21,000	J130	0.11	13,000	35.74	17,000
J131	0.11	13,000	38.33	18,000	J131	0.11	13,000	42.15	19,000	J131	0.11	13,000	32.21	16,000
J132	0.11	13,000	41.89	20,000	J132	0.11	13,000	45.72	21,000	J132	0.11	13,000	35.61	17,000
J133	0.11	13,000	45.63	24,000	J133	0.11	13,000	48.53	25,000	J133	0.11	13,000	36.51	17,000
J134	0.11	13,000	39.98	19,000	J134	0.11	13,000	43.89	20,000	J134	0.11	13,000	31.96	16,000
J135	0.11	13,000	40.47	19,000	J135	0.11	13,000	44.29	20,000	J135	0.11	13,000	32.36	16,000
J136	0.11	13,000	42.46	20,000	J136	0.11	13,000	46.28	21,000	J136	0.11	13,000	34.26	17,000
J137	0.11	6,000	53.70	8,000	J137	0.11	6,000	40.32	8,000	J137	0.11	6,000	35.18	8,000
J14	0.11	6,000	55.91	15,000	J14	0.11	6,000	57.95	15,000	J14	0.11	6,000	52.80	13,000
J15	0.07	13,000	50.53	35,000	J15	0.07	13,000	62.63	35,000	J15	0.07	13,000	54.58	33,000
J152	0.11	13,000	54.93	35,000	J152	0.11	13,000	63.04	36,000	J152	0.11	13,000	55.24	32,000
J153	0.15	13,000	54.09	34,000	J153	0.15	13,000	57.91	36,000	J153	0.15	13,000	51.15	28,000
J154	0.11	13,000	53.70	32,000	J154	0.11	13,000	57.53	34,000	J154	0.11	13,000	45.74	22,000
J155	0.11	13,000	53.42	32,000	J155	0.11	13,000	57.24	33,000	J155	0.11	13,000	44.58	21,000
J156	0.00	13,000	52.26	30,000	J156	0.00	13,000	56.08	31,000	J156	0.00	13,000	40.94	19,000
J158	0.00	13,000	52.45	31,000	J158	0.00	13,000	57.25	32,000	J158	0.00	13,000	52.54	30,000
J160	0.07	13,000	53.57	35,000	J160	0.07	13,000	62.44	35,000	J160	0.07	13,000	54.20	33,000
J162	0.00	13,000	45.49	21,000	J162	0.00	13,000	47.31	22,000	J162	0.00	13,000	37.60	18,000
J164	0.00	13,000	43.67	21,000	J164	0.00	13,000	47.49	22,000	J164	0.00	13,000	37.79	18,000
J166	0.00	13,000	38.56	19,000	J166	0.00	13,000	42.39	19,000	J166	0.00	13,000	32.68	16,000
J168	0.00	13,000	35.44	17,000	J168	0.00	13,000	39.26	18,000	J168	0.00	13,000	29.56	15,000
J17	0.07	13,000	57.93	48,000	J17	0.07	13,000	61.74	50,000	J17	0.07	13,000	53.59	31,000
J172	0.00	13,000	50.38	27,000	J172	0.00	13,000	54.20	29,000	J172	0.00	13,000	47.91	24,000
J174	0.15	13,000	53.62	33,000	J174	0.15	13,000	57.45	34,000	J174	0.15	13,000	51.15	28,000
J176	0.15	13,000	54.02	34,000	J176	0.15	13,000	57.84	35,000	J176	0.15	13,000	51.47	28,000
J178	0.08	13,000	54.48	34,000	J178	0.08	13,000	58.31	36,000	J178	0.08	13,000	52.26	29,000
J18	0.07	13,000	57.39	46,000	J18	0.07	13,000	61.12	48,000	J18	0.07	13,000	53.59	32,000
J19	0.10	13,000	57.62	44,000	J19	0.10	13,000	60.54	45,000	J19	0.10	13,000	52.46	30,000
J20	0.10	13,000	57.02	43,000	J20	0.10	13,000	57.25	45,000	J20	0.10	13,000	53.25	31,000
J21	0.10	13,000	56.54	42,000	J21	0.10	13,000	60.44	42,000	J21	0.10	13,000	52.51	30,000
J22	0.10	13,000	56.53	41,000	J22	0.10	13,000	60.35	43,000	J22	0.10	13,000	52.43	31,000
J23	0.10	13,000	55.93	39,000	J23	0.10	13,000	59.75	40,000	J23	0.10	13,000	52.96	30,000
J24	0.10	13,000	55.37	36,000	J24	0.10	13,000	59.20	38,000	J24	0.10	13,000	52.45	29,000
J25	0.10	13,000	54.97	35,000	J25	0.10	13,000	57.49	36,000	J25	0.10	13,000	52.07	29,000
J26	0.10	13,000	55.09	35,000	J26	0.10	13,000	58.82	37,000	J26	0.10	13,000	52.12	29,000
J27	0.01	13,000	55.46	35,000	J27	0.01	13,000	59.41	36,000	J27	0.01	13,000	54.51	33,000
J28	0.19	13,000	55.12	35,000	J28	0.19	13,000	58.95	37,000	J28	0.19	13,000	52.26	29,000
J29	0.10	13,000	55.25	36,000	J29	0.10	13,000	59.07	37,000	J29	0.10	13,000	52.38	29,000
J30	0.07	13,000	55.60	37,000	J30	0.07	13,000	59.43	39,000	J30	0.07	13,000	52.73	30,000
J31	0.07	13,000	55.84	37,000	J31	0.07	13,000	59.67	39,000	J31	0.07	13,000	52.95	30,000
J32	0.07	13,000	56.17	39,000	J32	0.07	13,000	60.00	40,000	J32	0.07	13,000	53.25	31,000
J33	0.07	13,000	56.49	39,000	J33	0.07	13,000	60.36	40,000	J33	0.07	13,000	53.64	31,000
J34	0.07	13,000	57.38	43,000	J34	0.07	13,000	61.21	45,000	J34	0.07	13,000	54.39	33,000
J35	0.07	13,000	57.76	46,000	J35	0.07	13,000	61.59	47,000	J35	0.07	13,000	54.68	33

Option B - 3 Connections - Break Scenario 7 (Connection 3 Break)				
Junction ID	Basis Demand (AVDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)
J01	0.07	13,000	50.75	28,000
J02	0.00	13,000	50.85	28,000
J05	0.07	13,000	51.07	28,000
J06	0.07	13,000	51.13	28,000
J07	0.11	13,000	51.35	28,000
J08	0.11	13,000	51.37	28,000
J09	0.11	13,000	51.02	28,000
J10	0.11	13,000	51.58	29,000
J100	0.15	13,000	35.85	17,000
J101	0.15	13,000	41.53	20,000
J102	0.15	13,000	40.97	20,000
J103	0.15	13,000	36.54	18,000
J109	0.11	13,000	38.31	18,000
J11	0.11	13,000	51.74	29,000
J110	0.11	13,000	38.43	18,000
J111	0.11	13,000	38.95	19,000
J112	0.11	13,000	33.79	17,000
J113	0.11	13,000	30.07	15,000
J114	0.11	13,000	24.46	14,000
J115	0.11	13,000	27.00	15,000
J116	0.11	13,000	29.75	16,000
J117	0.11	13,000	28.09	15,000
J118	0.11	13,000	32.63	16,000
J119	0.11	13,000	33.78	17,000
J12	0.11	13,000	32.49	20,000
J120	0.11	13,000	32.39	16,000
J121	0.11	13,000	29.71	16,000
J122	0.11	13,000	23.29	14,000
J123	0.11	13,000	23.35	14,000
J124	0.11	13,000	29.83	16,000
J125	0.00	13,000	27.47	15,000
J128	0.00	6,000	51.65	13,000
J129	0.11	13,000	22.95	14,000
J130	0.11	13,000	26.54	15,000
J131	0.11	13,000	23.03	14,000
J132	0.11	13,000	26.43	15,000
J133	0.11	13,000	26.53	15,000
J134	0.11	13,000	22.85	14,000
J135	0.11	13,000	23.25	14,000
J136	0.11	13,000	25.15	14,000
J137	0.11	6,000	32.53	7,000
J14	0.11	6,000	50.15	12,000
J15	0.07	13,000	48.53	25,000
J152	0.11	13,000	23.44	20,000
J153	0.15	13,000	42.30	20,000
J154	0.11	13,000	36.63	18,000
J155	0.11	13,000	35.48	17,000
J156	0.00	13,000	31.86	16,000
J158	0.00	13,000	39.93	19,000
J16	0.07	13,000	37.76	24,000
J162	0.00	13,000	38.51	19,000
J164	0.00	13,000	38.88	18,000
J166	0.00	13,000	31.75	16,000
J168	0.00	13,000	28.63	15,000
J17	0.07	13,000	46.35	23,000
J170	0.00	13,000	34.43	18,000
J172	0.00	13,000	39.11	19,000
J174	0.15	13,000	40.55	19,000
J176	0.15	13,000	40.26	19,000
J178	0.08	13,000	40.57	19,000
J18	0.07	13,000	45.44	22,000
J180	0.08	13,000	40.56	19,000
J182	0.08	13,000	39.80	19,000
J184	0.08	13,000	39.81	19,000
J186	0.08	13,000	41.19	20,000
J188	0.00	13,000	38.32	18,000
J19	0.10	13,000	43.99	21,000
J20	0.01	13,000	44.59	22,000
J21	0.10	13,000	41.41	21,000
J22	0.10	13,000	44.32	22,000
J23	0.10	13,000	44.26	21,000
J24	0.10	13,000	44.01	21,000
J25	0.10	13,000	43.82	21,000
J26	0.10	13,000	44.10	21,000
J27	0.10	13,000	44.01	21,000
J28	0.10	13,000	44.71	22,000
J29	0.10	13,000	45.04	22,000
J30	0.07	13,000	45.65	22,000
J31	0.07	13,000	46.08	23,000
J32	0.07	13,000	46.61	23,000
J33	0.07	13,000	47.47	24,000
J34	0.07	13,000	48.16	24,000
J35	0.07	13,000	48.80	25,000
J36	0.07	13,000	50.10	26,000
J37	0.08	13,000	43.11	21,000
J38	0.08	13,000	42.37	20,000
J39	0.08	13,000	47.07	20,000
J40	0.11	13,000	52.89	31,000
J41	0.11	13,000	40.08	19,000
J42	0.11	13,000	39.51	19,000
J43	0.11	13,000	37.87	18,000
J44	0.11	13,000	36.34	18,000
J45	0.11	13,000	33.18	17,000
J46	0.11	13,000	36.01	19,000
J48	0.11	13,000	51.93	30,000
J50	0.11	13,000	44.52	22,000
J51	0.11	13,000	44.20	21,000
J52	0.11	13,000	41.04	20,000
J53	0.11	13,000	40.35	19,000
J56	0.11	13,000	40.56	20,000
J57	0.11	13,000	37.12	18,000
J58	0.11	13,000	39.08	19,000
J59	0.11	13,000	37.63	18,000
J60	0.11	13,000	33.31	16,000
J61	0.11	13,000	29.37	15,000
J62	0.11	13,000	34.56	15,000
J63	0.11	13,000	33.01	16,000
J64	0.11	13,000	32.97	16,000
J65	0.11	13,000	29.56	15,000
J66	0.11	13,000	33.75	17,000
J67	0.11	13,000	33.92	17,000
J68	0.11	13,000	34.59	15,000
J69	0.11	13,000	29.46	15,000
J70	0.11	13,000	32.92	16,000
J71	0.11	13,000	32.99	16,000
J72	0.11	13,000	29.36	15,000
J73	0.11	13,000	29.53	15,000
J74	0.11	13,000	30.53	16,000
J75	0.10	13,000	35.75	17,000
J76	0.10	13,000	40.43	19,000
J77	0.10	13,000	35.66	17,000
J78	0.07	13,000	41.59	20,000
J79	0.07	13,000	38.58	18,000
J80	0.03	13,000	35.03	16,000
J81	0.15	13,000	41.51	20,000
J82	0.15	13,000	41.49	20,000
J83	0.15	13,000	42.73	21,000
J84	0.15	13,000	43.17	21,000
J85	0.15	13,000	26.43	15,000
J86	0.15	13,000	22.78	14,000
J87	0.14	13,000	24.49	14,000
J88	0.15	13,000	26.90	15,000
J89	0.15	13,000	44.16	21,000
J90	0.15	13,000	35.62	17,000
J91	0.15	13,000	42.23	20,000
J92	0.15	13,000	31.56	18,000
J93	0.15	13,000	35.56	15,000
J94	0.08	13,000	40.38	19,000
J95	0.08	13,000	39.95	19,000
J96	0.08	13,000	39.97	19,000
J97	0.08	13,000	31.50	16,000
J98	0.00	13,000	39.70	19,000

**BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION  
SYSTEM ANALYSIS**

June 2, 2022

**Appendix E      WATER AGE CALCULATIONS**



## 163401660 - Barrhaven Conservancy

### Water Age Assessment

Sizing Option A	Pipe Dimensions			Average Day Demand		Water Age		
	Phase	Pipe Diameter	Pipe Length	Pipe Volume	(L/s)	(m³/s)	(s)	(h)
		(mm)	(m)	(m³)				
2		406	2,609	337.81	3.50	0.004	96,464	26.80 1.12
2		305	1,442	105.38	3.50	0.004	30,091	8.36 0.35
2		203	742	24.00	3.50	0.004	6,853	1.90 0.08
2		152	305	5.54	3.50	0.004	1,581	0.44 0.02
2	Total			472.73	3.50	0.004	134,989	37.50 1.56
3		406	2,609	337.81	6.64	0.007	50,906	14.14 0.59
3		305	2,326	169.96	6.64	0.007	25,612	7.11 0.30
3		203	2,001	64.75	6.64	0.007	9,757	2.71 0.11
3		152	427	7.75	6.64	0.007	1,167	0.32 0.01
3	Total			580.27	6.64	0.007	87,442	24.29 1.01
4		406	2,977	385.42	10.30	0.010	37,402	10.39 0.43
4		305	2,982	217.89	10.30	0.010	21,145	5.87 0.24
4		203	3,747	121.28	10.30	0.010	11,769	3.27 0.14
4		152	474	8.60	10.30	0.010	835	0.23 0.01
4	Total			733.20	10.30	0.010	71,151	19.76 0.82
Ultimate		406	2,977	385.42	13.92	0.014	27,691	7.69 0.32
Ultimate		305	2,982	217.89	13.92	0.014	15,654	4.35 0.18
Ultimate		203	6,024	194.98	13.92	0.014	14,008	3.89 0.16
Ultimate		152	555	10.08	13.92	0.014	724	0.20 0.01
Ultimate	Total			808.38	13.92	0.014	58,078	16.13 0.67

Sizing Option B	Pipe Dimensions			Average Day Demand		Water Age		
	Phase	Pipe Diameter	Pipe Length	Pipe Volume	(L/s)	(m³/s)	(s)	(h)
		(mm)	(m)	(m³)				
2		406	0	0.00	3.50	0.004	0	0.00 0.00
2		305	3,933	287.37	3.50	0.004	82,059	22.79 0.95
2		203	742	24.00	3.50	0.004	6,853	1.90 0.08
2		152	305	5.54	3.50	0.004	1,581	0.44 0.02
2	Total			316.90	3.50	0.004	90,493	25.14 1.05
3		406	0	0.00	6.64	0.007	0	0.00 0.00
3		305	4,817	351.95	6.64	0.007	53,036	14.73 0.61
3		203	2,001	64.75	6.64	0.007	9,757	2.71 0.11
3		152	427	7.75	6.64	0.007	1,167	0.32 0.01
3	Total			424.45	6.64	0.007	63,960	17.77 0.74
4		406	0	0.00	10.30	0.010	0	0.00 0.00
4		305	5,841	426.75	10.30	0.010	41,413	11.50 0.48
4		203	3,747	121.28	10.30	0.010	11,769	3.27 0.14
4		152	474	8.60	10.30	0.010	835	0.23 0.01
4	Total			556.64	10.30	0.010	54,017	15.00 0.63
Ultimate		406	0	0.00	13.92	0.014	0	0.00 0.00
Ultimate		305	6,619	483.60	13.92	0.014	34,744	9.65 0.40
Ultimate		203	6,024	194.98	13.92	0.014	14,008	3.89 0.16
Ultimate		152	555	10.08	13.92	0.014	724	0.20 0.01
Ultimate	Total			688.66	13.92	0.014	49,477	13.74 0.57



**Kennedy-Burnett Potable  
Water Master Servicing Study**



Prepared for:  
City of Ottawa  
100 Constellation Crescent  
Ottawa, ON K2G 6G8

Prepared by:  
Stantec Consulting Ltd.  
400-1331 Clyde Avenue  
Ottawa, ON K2C 3G4

File No. 1634-01221

April 29, 2014

## KENNEDY-BURNETT POTABLE WATER MASTER SERVICING STUDY

Hydraulic Assessment  
April 29, 2014

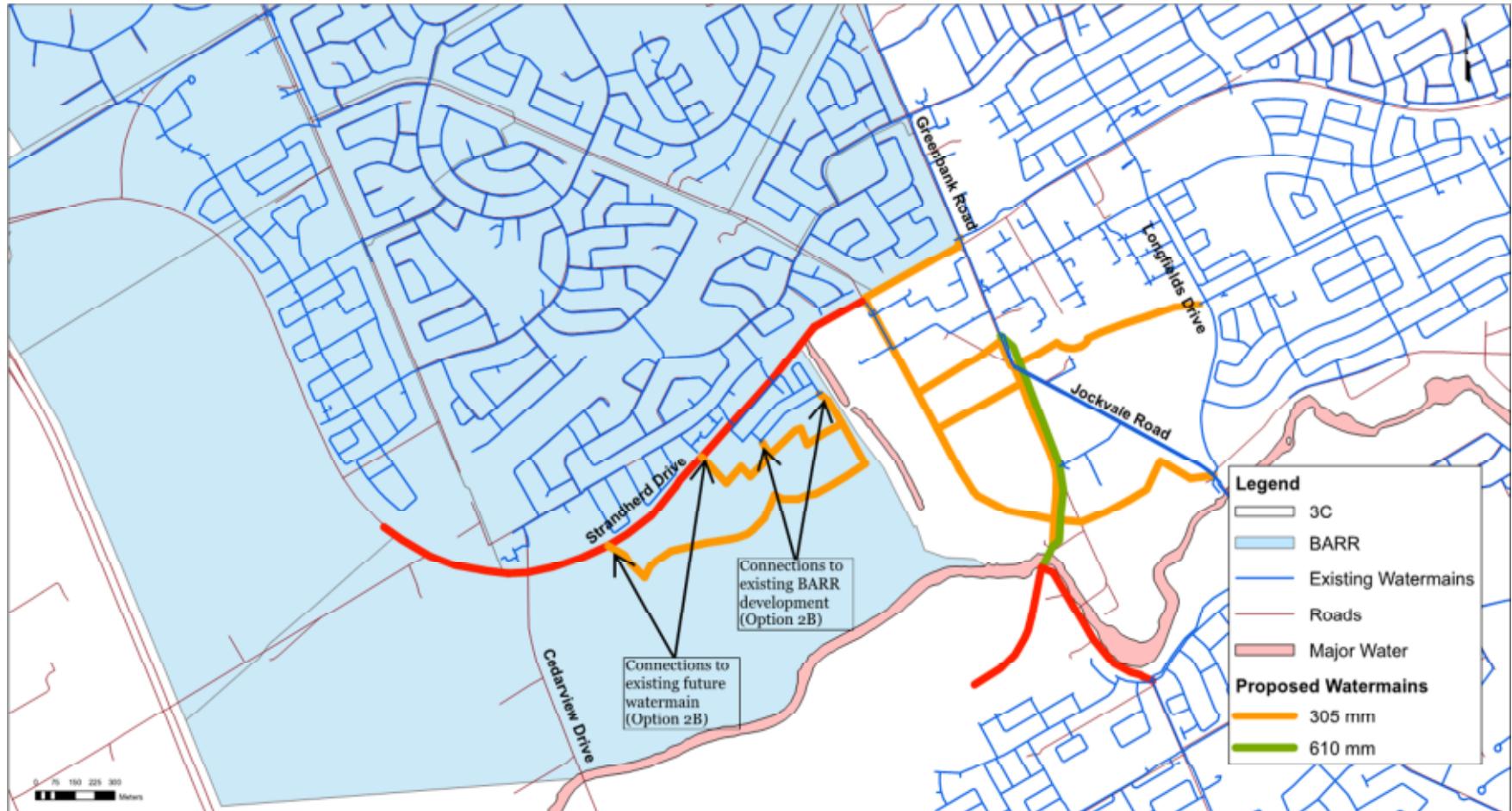


Figure 2-6: Proposed Pipe Layout Post Zone Reconfiguration – Scenario 2B

## **APPENDIX C**

### **SANITARY**

# MEMORANDUM

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**DATE:** MAY 30, 2019  
**TO:** JOSÉE VALLEE – CITY OF OTTAWA  
**FROM:** CONRAD STANG – NOVATECH  
**RE:** STRANDHERD DRIVE WIDENING PROJECT  
SOUTH NEPEAN COLLECTOR PHASE 3: SANITARY FLOW CALCULATIONS  
**CC:** EDSON DONNELLY – NOVATECH

---

## 1.0 PURPOSE

This memorandum provides the sanitary sewer flow calculations and design sheet for Phase 3 of the proposed South Nepean Collector (SNC), as part of the Strandherd Drive Widening Project. Sanitary design flows have been estimated for both current-day operational flows and future development peak design flows. They are based on the latest available planning information for the vacant lands within the SNC sewershed.

## 2.0 BACKGROUND

In January 1998, the Master Servicing Study for the South Nepean Urban Area provided a conceptual plan for water, wastewater and stormwater infrastructure. The preferred alternative for wastewater servicing was an east/west trunk sewer alignment that was to be completed in several phases. The proposed sanitary trunk sewer was initially called the Jock River Collector, but was renamed the South Nepean Collector during the original functional design study completed in 2003.

Phase 1 of the South Nepean Collector was completed in 2005 and currently terminates at a 2400mm maintenance hole located east of Longfields Drive, north of Bren-Maur Road. Phase 2 was completed in 2016 and currently terminates at a 2400mm maintenance hole located at the intersection of Strandherd Drive and Fraser Fields Way.

Phase 3 will extend the trunk sewer along Strandherd Drive to the intersection of Kennevale Drive. Here it will connect with the existing sanitary trunk sewer that was constructed as part of the 2014 works to improve Strandherd Drive and develop the CitiGate Lands.

The sanitary sewer flows were previously documented in the *South Nepean Collector – Functional Design Report and Update* (Dillon, 2012). Novatech (2016) completed a Hydraulics Review / Assessment of the sanitary flows presented in the Dillon Report (attached). This was based on the latest planning information for the vacant lands within the SNC sewershed. The results of the Hydraulics Review / Assessment (Novatech, 2016) were similar to the results from the Dillon (2012) analysis.

### 3.0 DESIGN PARAMETERS AND POPULATION ESTIMATES

#### 3.1 Design Parameters

The sanitary design flow were calculated using the parameters from the City of Ottawa Sewer Design Guidelines (October 2012), revised per Technical Bulletin ISTB-2018-01 (March 2018). These parameters are summarized in **Table 1** and **Table 2**.

**Table 1: Peak Design Flow Parameters**

Land Use	Average Daily Flow	Peaking Factor	Peak Extraneous Flows
Residential	280 L/cap/day	Harmon Equation, K=0.8 (1.6 min – 3.2 max)	0.33 L/s/ha
Commercial	28,000 L/ha/day	1.0 – 1.5*	
Institutional	28,000 L/ha/day	1.0 – 1.5*	
Other†	0 L/ha/day	N/A	

\*Peak Factor = 1.5 if contributing area is >20%; Peak Factor = 1.0 if contributing area is <20%

†Open Space, Arterial ROW, SWM Blocks, etc. with no sanitary flow contribution (extraneous flow only)

**Table 2: Operational Design Flow Parameters**

Land Use	Average Daily Flow	Peaking Factor	Peak Extraneous Flows
Residential	200 L/cap/day	Harmon Equation, K=0.6 (1.2 min – 2.4 max)	0.30 L/s/ha
Commercial	17,000 L/ha/day	1.0 (non-coincident peak)	
Institutional	17,000 L/ha/day	1.0 (non-coincident peak)	

\*There are no industrial areas identified within the tributary area.

$$\text{Harmon Equation} = 1 + \frac{14}{4 + \left(\frac{P}{1000}\right)^{\frac{1}{2}}} \times K$$

Where:

P = Population

K = Correction Factor:

- Peak Flow = 0.8
- Operational = 0.6

#### 3.2 Land Use Designations & Population Estimates

Population densities and unit counts for future residential development are based on the Novatech (2016) Hydraulics Review / Assessment; refer to **Table 3**. They are based on the concept plans provided by the developers of the future residential areas.

**Table 3: Residential Land Use Population Densities**

Residential Land Use	Units per ha	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

The land use designations shown in **Table 4** have been applied for the areas within Phases 2 & 3 of the SNC (Node 70 to 130). The Hydraulics Analysis / Review delineated the sewershed areas and land use designations using aerial photos (existing development) and conceptual site plans (future development).

**Table 4: Land Use Designations**

Land Use Designation	
Secondary Plan	SNC Design
Residential	Residential (Low / Medium / High Density)
Institutional / Office	Institutional
Commercial	Commercial
Recreational	
Business Park	
Prestige Business Park	
Park/Open Space Area	Other*
Ex. Snow Disposal Facility (future commercial)	
Stormwater Management Facility	
Conservation Lands	
Arterial Right-of-Ways	

\* No sanitary flow contribution - extraneous flows (inflow/infiltration) only.

The overall residential population estimate and sewershed area for Phases 2 and 3 of the SNC is provided in **Table 5** below. It is assumed that the snow dump facility at the Stranderd Drive and McKenna Casey Drive will ultimately be re-zoned for commercial development.

**Table 5: Population Estimates and Areas**

Existing / Future	Estimated Population / Area	Novatech (2015)
Existing	Estimated Population	6,944 persons
	Gross Residential Area	60.09 ha
	Gross Commercial / Institutional Area	64.37 ha
	Total Sewershed Area	124.5 ha
Future (full service)	Estimated Population	27,312 persons
	Gross Residential Area	248.48 ha
	Gross Commercial / Institutional Area	228.82 ha
	Total Sewershed Area	477.3 ha

#### 4.0 SANITARY DESIGN FLOWS

The sanitary flow allocations for Phases 2 and 3 of the SNC are provided in **Table 6**. The corresponding sanitary drainage area plan is provided as **Figure 1**. Sanitary sewer flow calculations for Phases 2 and 3 and detailed sanitary sewer design sheets for Phase 3 are attached to this memorandum.

The estimated sanitary design flows from Phase 3 of the SNC (entering Node 90) are as follows:

- Present-Day Operational Design Flows (Theoretical) = 55.1 L/s
- Future Peak Design Flows = 282.5 L/s

The outlet for Phase 3 of the SNC is the existing 900mm outlet pipe at the 2400mm maintenance hole (Node 90) located at the intersection of Strandherd Drive and Fraser Fields Way. Given a minimum design slope of 0.10%, this 900mm sanitary trunk sewer would have a full flow capacity of 597.2 L/s. Therefore, the downstream sanitary trunk sewer would be at 64% capacity, based on the future peak design flow being 282.5 L/s.

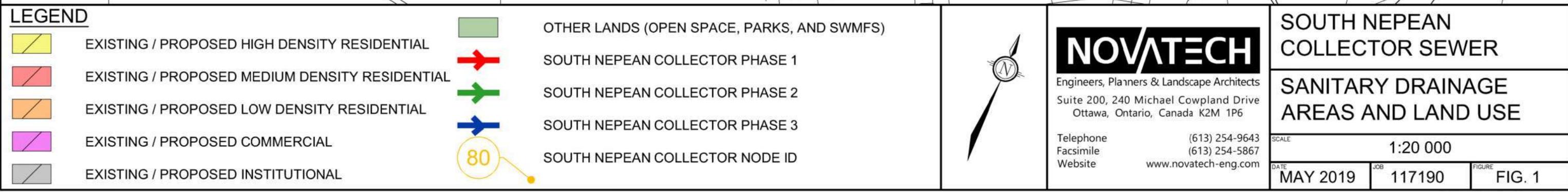
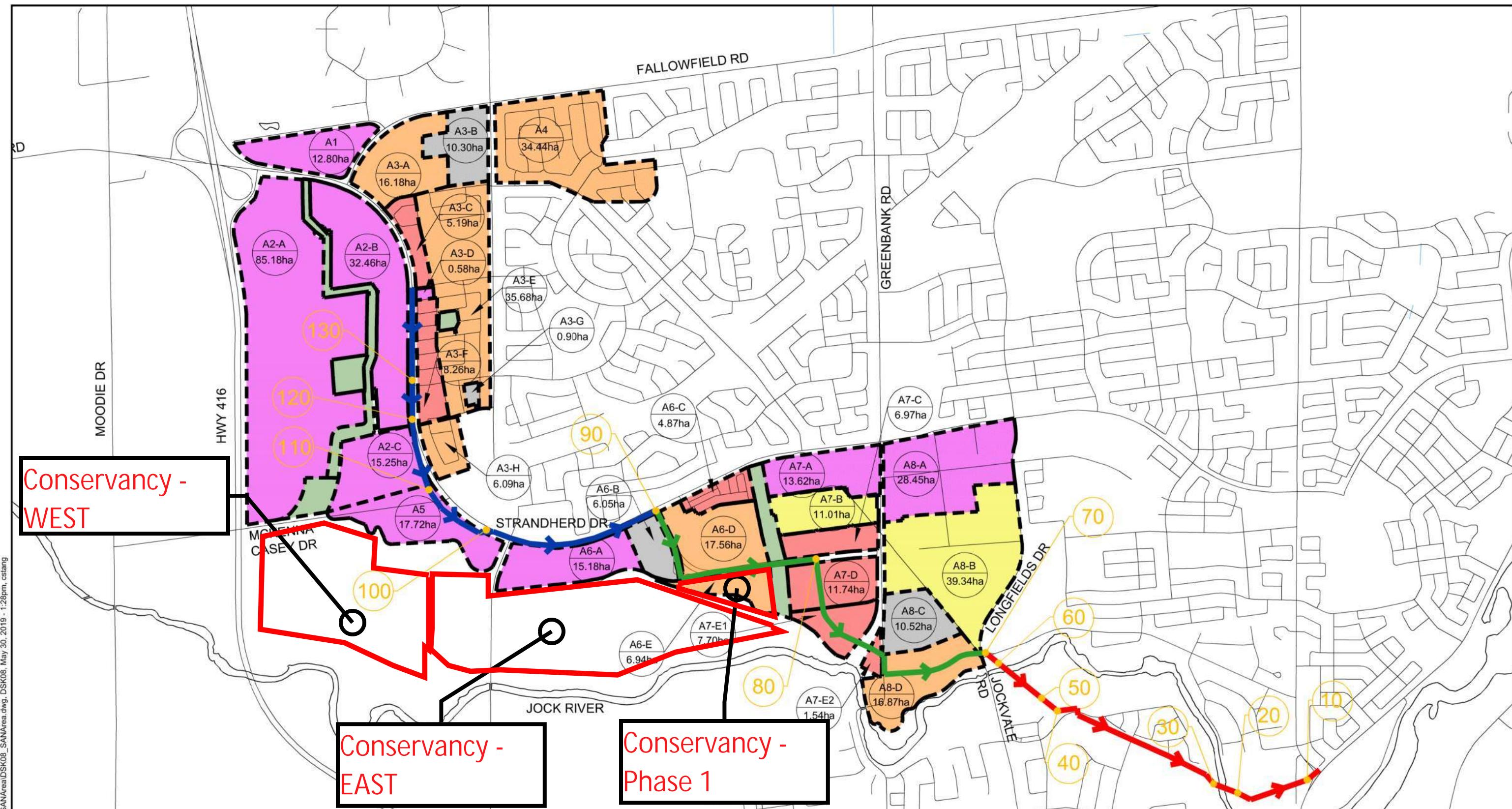
#### **ATTACHMENTS:**

- Figure 1: Sanitary Drainage Areas and Land Use
- Sanitary Sewer Flow Calculations
- Sanitary Sewer Design Sheets (Phase 3)
- South Nepean Collector Phase 2: Hydraulics Review / Assessment (Novatech, 2016)
- Excerpts from Dillion (2012)



**Table 6: Updated Allocation of Commercial, Institutional and Residential Demands to Phases 2 & 3 (Nodes 70 – 130) of the SNC by Collection Area**

Collection Area	Upstream Node	Existing / Proposed Development	Existing / Proposed Land Use	Area (ha)	Estimated Number of Residential Units	Population Density (persons / ha)	Comment	Reference
A1	130	Proposed	Commercial	12.80	-	-	O'Keefe Court – Conceptual site plan shows proposed commercial.	Conceptual Plans for O'Keefe Court
A2-A	130	Proposed	Commercial	85.18	-	-	CitiGate – Analysis uses same approach as the design for CitiGate.	Detailed Servicing and SWM Report (Phase 1) (Novatech, 2014)
A2-B	130	Proposed	Commercial	32.46	-	-		
A2-C	120	Proposed	Commercial (ex. Snow dump)	15.25	-	-	Existing snow dump facility assumed to be future commercial.	Functional Design Report and Update – SNC Phase 2 and 3 (Dillon, 2012)
A3-A	130	Proposed	Low Density Residential	16.18	461	95.2	Havencrest – Existing single family units.	Havencrest Design Report (IBI, 2013)
A3-B	130	Existing	Institutional	10.30	-	-	Cedarview Middle School and Cedarview Alliance Church.	Aerial Photos / Site Visits
A3-C	130	Existing	Medium Density Residential	5.19	311	162	Existing townhouse units.	
A3-D	130	Existing	Commercial	0.58	-	-	Existing commercial buildings.	
A3-E	130	Existing	Low Density Residential	35.68	999	95.2	Existing single family units.	
A3-F	130	Existing	Medium Density Residential	8.26	496	162.0	Existing townhouse units.	
A3-G	130	Existing	Institutional	0.90	-	-	Ottawa Torah Centre Chabad.	
A3-H	120	Existing	Low Density Residential	6.09	171	95.2	Existing single family units.	
A4	130	Existing	Low Density Residential	34.44	964	95.2	Existing single family units currently serviced by Jockvale pump station; to be redirected to SNC.	Functional Design Report and Update – SNC Phase 2 and 3 (Dillon, 2012); based on 2011 Census.
A5	110	Proposed	Commercial	17.72	-	-	Proposed commercial south of McKenna Casey Drive.	Site Visits
A6-A	100	Proposed	Commercial	15.18	-	-	Proposed commercial south of Strandherd Drive; east of Borrisokane Road.	Conceptual Plan for Lands Adjacent the Kennedy-Burnett SWMF provided by Minto (2015)
A6-B	100	Proposed	Institutional	6.05			Proposed school site on Minto property.	
A6-C	90	Existing	Medium Density Residential	4.87	292	162.0	Existing townhouse units.	
A6-D	90	Proposed	Low Density Residential	17.56	492	95.2	Proposed single family units on lands owned by Minto / Mion.	Conceptual Plans for Lands Adjacent the Kennedy-Burnett SWMF provided by land owners.
A6-E	90	Proposed	Low Density Residential	6.94	203	95.2	Proposed single family units on lands owned by Pavic / Braovac.	
A7-A	80	Existing	Commercial	13.62	-	-	Existing large retail stores (commercial).	Aerial Photos
A7-B	80	Proposed	High Density Residential	11.01	826	135.0	Proposed high density units on lands owned by Richcraft / Trinity.	Conceptual Plans for Lands Adjacent the Kennedy-Burnett SWMF provided by land owners.
A7-C	80	Proposed	Medium Density Residential	6.97	418	162.0	Proposed Medium density units on lands owned by Mion.	
A7-D	80	Proposed	Medium Density Residential	11.74	704	162.0	Proposed Medium density units on lands owned by Caivan.	
A7-E1/E2	80	Proposed	Medium Density Residential	9.24	554	162.0	Proposed Medium density units on lands owned by Claridge.	
A8-A	80	Existing	Commercial	28.45	-	-	Existing Barrhaven Market Place (commercial).	Aerial Photos / Site Visits
A8-B	80	Proposed	High Density Residential	39.34	2951	135.0	Future development similar to Ampersands development.	Site Visits
A8-C	80	Existing	Institutional	10.52	-	-	Existing St. Joseph High School.	Aerial Photos / Site Visits
A8-D	80	Proposed	Low Density Residential	16.87	1012	162.0	Proposed 600 low density residential units.	Functional Design Report and Update – SNC Phase 2 and 3 (Dillon, 2012)



PROJECT #: 117190  
 DESIGNED BY: CMS  
 CHECKED BY: RJD  
 DATE: December 5, 2018

### SANITARY SEWER DESIGN SHEET

#### South Nepean Collector - Phase 2 & 3

Theoretical Current Operational Peak Wastewater Flow



Location			Areas				Population				Individual Design Flows			Cumulative Design Flows				
Area I.D.	Existing Land Use	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Total Gross Area (ha)	Residential Population Density (people / ha)	Individual Residential Population	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn <sup>1</sup> )	Commercial Peak Flow Rate <sup>2</sup> (17,000 L/ha/d) (L/s)	Institutional Peak Flow Rate <sup>2</sup> (17,000 L/ha/d) (L/s)	Infiltration / Inflow Rate (0.3 L/s/ha) (L/s)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (200 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)
A1	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A2-A	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A2-B	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A3-A	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A3-B	Institutional	130				10.30					0.0	2.0	3.1	0.0	2.0	3.1	0.0	5.1
A3-C	Medium Density Residential	130				5.19	5.19	162.0	841	841	2.40	0.0	1.6	0.0	2.0	4.6	4.7	11.3
A3-D	Commercial	130	0.58			0.58				841	2.40	0.1	0.2	0.1	2.0	4.8	4.7	11.6
A3-E	Low Density Residential	130				35.68	35.68	95.2	3397	4238	2.39	0.0	0.0	10.7	0.1	2.0	15.5	23.4
A3-F	Medium Density Residential	130				8.26	8.26	162	1338	5576	2.32	0.0	0.0	2.5	0.1	2.0	18.0	29.9
A3-G	Institutional	130				0.90				5576	2.32	0.0	0.2	0.3	0.1	2.2	18.3	29.9
A4	Low Density Residential*	130				0.00				5576	2.32	0.0	0.0	0.0	0.1	2.2	18.3	29.9
A2-C	Snow Dump Facility	120				0.00				5576	2.32	0.0	0.0	0.0	0.1	2.2	18.3	29.9
A3-H	Low Density Residential	120				6.09	6.09	95.2	580	6155	2.30	0.0	0.0	1.8	0.1	2.2	20.1	32.7
A5	Open Space	110				0.00				6155	2.30	0.0	0.0	0.0	0.1	2.2	20.1	32.7
A6-A	Open Space	100				0.00				6155	2.30	0.0	0.0	0.0	0.1	2.2	20.1	32.7
A6-B	Open Space	100				0.00				6155	2.30	0.0	0.0	0.0	0.1	2.2	20.1	32.7
A6-C	Medium Density Residential	90				4.87	4.87	162.0	789	6944	2.27	0.0	0.0	1.5	0.1	2.2	21.6	36.4
A6-D	Open Space	90				0.00				6944	2.27	0.0	0.0	0.0	0.1	2.2	21.6	36.4
A6-E	Open Space	90				0.00				6944	2.27	0.0	0.0	0.0	0.1	2.2	21.6	36.4
A7-A	Commercial	90	13.62			13.62				6944	2.27	2.7	0.0	4.1	2.8	2.2	25.6	36.4
A7-B	Open Space	90				0.00				6944	2.27	0.0	0.0	0.0	0.0	2.2	25.6	36.4
A7-C	Open Space	90				0.00				6944	2.27	0.0	0.0	0.0	0.0	2.2	25.6	36.4
A7-D	Open Space	90				0.00				6944	2.27	0.0	0.0	0.0	0.0	2.2	25.6	36.4
A7-E1/E2	Open Space	90				0.00				6944	2.27	0.0	0.0	0.0	0.0	2.2	25.6	36.4
A8-A	Commercial	80	28.45			28.45				6944	2.27	5.6	0.0	8.5	8.4	2.2	34.2	36.4
A8-B	Open Space	80				0.00				6944	2.27	0.0	0.0	0.0	0.0	2.2	34.2	36.4
A8-C	Institutional	80				10.52				6944	2.27	0.0	2.1	3.2	8.4	4.3	37.3	36.4
A8-D	Open Space	80				0.00				6944	2.27	0.0	0.0	0.0	4.3	37.3	36.4	86.4
ROW Along SNC Sewer Alignment	-	80				14.34				6944	2.27	0.0	0.0	4.3	8.4	4.3	41.6	36.4
<b>TOTAL</b>		<b>80</b>	<b>42.65</b>	<b>21.72</b>	<b>60.09</b>	<b>138.80</b>	-	<b>6944</b>	<b>6944</b>	<b>2.27</b>	<b>8.4</b>	<b>4.3</b>	<b>41.6</b>	<b>8.4</b>	<b>4.3</b>	<b>41.6</b>	<b>36.4</b>	<b>90.7</b>

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

Notes:

Reported Design Flows / Assumptions:

1. Harmon Equation =  $1 + [14 / (4+(P/1000)^{1/2})] \times K$

Where: P = population; K = correction factor = 0.6

2. Institutional / Commercial Peaking Factor = 1.0

1. Area A4: Existing single family units currently serviced by Jockvale pump station; currently not directed to SNC

SANITARY SEWER DESIGN SHEET

South Nepean Collector - Phase 2 & 3

Theoretical Future Full Service Peak Wastewater Flow

Location			Areas				Population				Individual Design Flows			Cumulative Design Flows					
Area I.D.	Existing / Proposed Land Use	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Total Gross Area (ha)	Residential Population Density (people / ha)	Individual Residential Population	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn <sup>1</sup> )	Commercial Peak Flow Rate <sup>2</sup> (28,000 L/ha/d) (L/s)	Institutional Peak Flow Rate <sup>2</sup> (28,000 L/ha/d) (L/s)	Infiltration / Inflow Rate (0.33 L/s/ha) (L/s)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (280 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)	
A1	Commercial	130	12.80			12.80				3.14	6.2	0.0	4.2	6.2	0.0	4.2	0.0	10.4	
A2-A	Commercial	130	85.18			85.18				3.14	41.4	0.0	28.1	47.6	0.0	32.3	0.0	80.0	
A2-B	Commercial	130	32.46			32.46				3.14	15.8	0.0	10.7	63.4	0.0	43.0	0.0	106.5	
A3-A	Low Density Residential	130			16.18	16.18	95.2	1540	1540	3.14	0.0	0.0	5.3	63.4	0.0	48.4	15.7	127.5	
A3-B	Institutional	130		10.30		10.30				3.14	1540	0.0	3.3	63.4	3.3	51.8	15.7	134.2	
A3-C	Medium Density Residential	130		0.58		5.19	5.19	162.0	841	2381	3.02	0.0	1.7	63.4	3.3	53.5	23.3	143.6	
A3-D	Commercial	130				0.58				3.02	2381	0.3	0.0	0.2	63.7	3.3	53.7	23.3	144.0
A3-E	Low Density Residential	130				35.68	35.68	95.2	3397	5778	2.75	0.0	0.0	11.8	63.7	3.3	65.5	51.5	184.0
A3-F	Medium Density Residential	130				8.26	8.26	162	1338	7116	2.68	0.0	0.0	2.7	63.7	3.3	68.2	61.8	197.0
A3-G	Institutional	130				0.90				2.68	7116	0.0	0.3	0.3	63.7	3.6	68.5	61.8	197.6
A4	Low Density Residential	130				34.44	34.44	95.2	3279	10395	2.55	0.0	0.0	11.4	63.7	3.6	79.9	85.9	233.1
A2-C	Commercial (ex. snow dump)	120	15.25			15.25				2.55	10395	7.4	0.0	5.0	71.1	3.6	84.9	85.9	245.5
A3-H	Low Density Residential	120				6.09	6.09	95.2	580	10974	2.53	0.0	0.0	2.0	71.1	3.6	86.9	90.0	251.7
A5	Commercial	110	17.72			17.72				2.53	10974	8.6	0.0	5.8	79.7	3.6	92.7	90.0	266.1
A6-A	Commercial	100	15.18			15.18				2.53	10974	7.4	0.0	5.0	87.1	3.6	97.7	90.0	278.5
A6-B	Institutional	100		6.05		6.05				2.53	10974	0.0	2.0	2.0	87.1	5.6	99.7	90.0	282.5
A6-C	Medium Density Residential	90				4.87	4.87	162.0	789	11763	2.51	0.0	0.0	1.6	87.1	5.6	101.4	95.6	289.6
A6-D	Low Density Residential	90				17.56	17.56	95.2	1672	13435	2.46	0.0	0.0	5.8	87.1	5.6	107.1	107.2	307.0
A6-E	Low Density Residential	90				6.94	6.94	95.2	661	14096	2.44	0.0	0.0	2.3	87.1	5.6	109.4	111.7	313.8
A7-A	Commercial	90	13.62			13.62				2.44	14096	6.6	0.0	4.5	93.7	5.6	113.9	111.7	324.9
A7-B	High Density Residential	90				11.01	11.01	135.0	1486	15582	2.41	0.0	0.0	3.6	93.7	5.6	117.6	121.7	338.5
A7-C	Medium Density Residential	90				6.97	6.97	162.0	1129	16711	2.38	0.0	0.0	2.3	93.7	5.6	119.9	129.2	348.3
A7-D	Medium Density Residential	90				11.74	11.74	162.0	1902	18613	2.35	0.0	0.0	3.9	93.7	5.6	123.7	141.6	364.6
A7-E1/E2	Medium Density Residential	90				9.24	9.24	162.0	1497	20110	2.32	0.0	0.0	3.0	93.7	5.6	126.8	151.2	377.3
A8-A	Commercial	80	28.45			28.45				2.32	20110	13.8	0.0	9.4	107.5	5.6	136.2	151.2	400.5
A8-B	High Density Residential	80				39.34	39.34	135.0	5311	25421	2.24	0.0	0.0	13.0	107.5	5.6	149.2	184.4	446.7
A8-C	Institutional	80		10.52		10.52				2.24	25421	0.0	3.4	3.5	107.5	9.0	152.6	184.4	453.6
A8-D	Low Density Residential	80				16.87	16.87	120.9	2040	27461	2.21	0.0	0.0	5.6	107.5	9.0	158.2	196.9	471.6
ROW Along SNC Sewer Alignment		-	80			14.34				2.21	27461	0.0	0.0	4.7	107.5	9.0	162.9	196.9	476.3
<b>TOTAL</b>		<b>80</b>	<b>221.24</b>	<b>27.77</b>	<b>230.38</b>	<b>493.73</b>	<b>-</b>	<b>27461</b>	<b>27461</b>	<b>2.21</b>	<b>107.5</b>	<b>9.0</b>	<b>162.9</b>	<b>107.5</b>	<b>9.0</b>	<b>162.9</b>	<b>196.9</b>	<b>476.3</b>	

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

Notes:

1. Harmon Equation =  $1 + [14 / (4+(P/1000)^{1/2})] \times K$
- Where: P = population; K = correction factor = 0.8
2. Commercial Peaking Factor = 1.5; Institutional Peaking Factor = 1.0

Reported Design Flows / Assumptions:

1. Area A4: Existing single family units currently serviced by Jockvale pump station to be redirected to SNC
2. Area A8-D: proposed 600 medium density residential units

See Note (2) in the DSEL "Barrhaven Conservancy - Evaluation of SNC Flows" design sheet

THE PRIOR NOVATECH SNC DESIGN SHEET HAD FLOWS AT 423.6 L/s AFTER AREA ID "A6-E".  
 THIS UPDATED NOVATECH 'PHASE 3' EVALUATION HAS A FLOW OF 313.8 L/s.  
 THE DSEL EVALUATION OF SANITARY FLOWS WITH THE NEW CITY DESIGN PARAMETERS AT THIS SAME NODE (WITH CONSERVANCY WEST AND EAST INCLUDED) IS ~401.58 L/s (WHICH IS LESS THAN THE PRIOR 423.6 L/s NOTED ABOVE)

**SOUTH NEPEAN COLLECTOR (PHASE 3)  
SANITARY SEWER DESIGN SHEET**

**DECEMBER 5 2018  
JOB# 117190**

**NOVATECH**  
Engineers, Planners & Landscape Architects

LOCATION			Area				Population		Cumulative Design Flows					PROPOSED SEWER						
From MH	To MH	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Total Gross Area (ha)	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn <sup>1</sup> )	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (280 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)	Length (m)	Pipe Size (mm)	Type	Slope %	Capacity (L/s)	Full Flow Velocity (m/s)	Ratio (Q/Qfull)
SA 22	SA 21	120	146.27	11.20	105.84	263.31	10974	2.53	71.1	3.6	86.9	90.0	251.7	131.9	750	CONC	0.10	367.3	0.81	69%
SA 21	SA 20	120											251.7	90.6	750	CONC	0.10	367.3	0.81	69%
SA 20	SA 19	120											251.7	90.0	750	CONC	0.10	367.3	0.81	69%
SA 19	SA 18	120											251.7	72.1	750	CONC	0.10	367.3	0.81	69%
SA 18	SA 17	120											251.7	71.9	750	CONC	0.10	367.3	0.81	69%
SA 17	SA 16	120											251.7	71.4	750	CONC	0.10	367.3	0.81	69%
SA 16	SA 15	110	163.99	11.20	105.84	281.03	10974	2.53	79.7	3.6	92.7	90.0	266.1	73.2	750	CONC	0.10	367.3	0.81	72%
SA 15	SA 14	110											266.1	67.5	750	CONC	0.10	367.3	0.81	72%
SA 14	SA 13	110											266.1	56.6	750	CONC	0.10	367.3	0.81	72%
SA 13	SA 12	110											266.1	133.5	750	CONC	0.10	367.3	0.81	72%
SA 12	SA 11	110											266.1	150.0	750	CONC	0.10	367.3	0.81	72%
SA 11	SA 10	100	179.17	17.25	105.84	302.26	10974	2.53	87.1	5.6	99.7	90.0	282.5	97.8	750	CONC	0.10	367.3	0.81	77%
SA 10	SA 9	100											282.5	76.7	750	CONC	0.10	367.3	0.81	77%
SA 9	SA 8	100											282.5	79.7	750	CONC	0.10	367.3	0.81	77%
SA 8	SA 7	100											282.5	75.3	750	CONC	0.10	367.3	0.81	77%
SA 7	SA 6	100											282.5	84.9	750	CONC	0.10	367.3	0.81	77%
SA 6	SA 5	100											282.5	77.1	750	CONC	0.10	367.3	0.81	77%
SA 5	SA 4	100											282.5	78.9	750	CONC	0.10	367.3	0.81	77%
SA 4	SA 3	100											282.5	80.5	750	CONC	0.10	367.3	0.81	77%
SA 3	SA 2	100											282.5	150.0	750	CONC	0.10	367.3	0.81	77%
SA 2	SA 1	100											282.5	114.6	750	CONC	0.10	367.3	0.81	77%
SA 1	EX 80	100											282.5	12.4	750	CONC	0.10	367.3	0.81	77%

**Design Parameters:**

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles / semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row / townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

Notes:

1. Harmon Equation =  $1 + [14 / (4+(P/1000)^{1/2})] \times K$

Where: P = population; K = correction factor = 0.8

2. Commercial Peaking Factor = 1.5; Institutional Peaking Factor = 1.0

Reported Design Flows / Assumptions:

1. Area A4: Existing single family units currently serviced by Jockvale pump station to be redirected to SNC

2. Area A8-D: proposed 600 medium density residential units



# MEMORANDUM

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**DATE:** MAY 26, 2016  
**TO:** JONATHAN KNOYLE – CITY OF OTTAWA  
**FROM:** CONRAD STANG – NOVATECH  
**RE:** SOUTH NEPEAN COLLECTOR PHASE 2: SANITARY FLOW CALCULATIONS  
**CC:** EDSON DONNELLY – NOVATECH

---

## 1.0 PURPOSE

This memorandum provides the sanitary sewer flow calculations and design sheet for Phase 2 of the proposed South Nepean Collector (SNC). Sanitary design flows have been estimated for both current-day operational flows and future development peak design flows, based on the latest available planning information for the vacant lands within the SNC sewershed.

## 2.0 BACKGROUND

In January 1998, the Master Servicing Study for the South Nepean Urban Area provided a conceptual plan for water, wastewater and stormwater infrastructure. The preferred alternative for wastewater servicing was an east/west trunk sewer alignment that was to be completed in several phases. The proposed sanitary trunk sewer was initially called the Jock River Collector, but was renamed the South Nepean Collector during the original functional design study completed in 2003.

Phase 1 of the South Nepean Collector was completed in 2005 and currently terminates at a 2400mm maintenance hole located east of Longfields Drive, north of Bren-Maur Road. Phase 2 will extend the trunk sewer to Strandherd Drive at the intersection of the proposed transitway along the proposed extension to Chapman Mills Drive. Phase 3 will extend the trunk sewer along Strandherd Drive to the intersection of Maravista Drive.

The sanitary sewer flows were previously documented in the *South Nepean Collector – Functional Design Report and Update* (Dillon, 2012). A review of the sanitary flows provided in the Dillon Report based on the latest planning information for the vacant lands within the SNC sewershed was documented in the technical memorandum titled South Nepean Collector Phase 2: Hydraulics Review / Assessment (Novatech, 2015), which is attached to this memorandum. The results of the Hydraulics Review / Assessment (Novatech, 2015) were very similar to the results from the Dillon (2012) analysis.

### 3.0 DESIGN PARAMETERS AND POPULATION ESTIMATES

#### 3.1 Design Parameters

The sanitary design flow were calculated using the parameters from the City of Ottawa Sewer Design Guidelines (October 2012), and are summarized in **Table 1** and **Table 2**.

**Table 1: Peak Design Flow Parameters**

Land Use	Average Daily Flow	Peaking Factor	Peak Extraneous Flows
Residential	350 L/cap/day	Harmon Equation, K=1 (2.0 min – 4.0 max)	0.28 L/s/ha
Commercial	50,000 L/ha/day	1.5	
Institutional	50,000 L/ha/day	1.5	
Other*	0 L/ha/day	N/A	

\*Open Space, Arterial ROW, SWM Blocks, etc. with no sanitary flow contribution (extraneous flow only)

**Table 2: Operational Design Flow Parameters**

Land Use	Average Daily Flow	Peaking Factor	Peak Extraneous Flows
Residential	300 L/cap/day	Harmon Equation, K=0.6 (1.2 min – 2.4 max)	<u>Dry weather</u> 0.05-0.08 L/s/ha  <u>Wet Weather</u> 0.15 - 0.20 L/s/ha (typical events) 0.28 L/s/ha (large/annual events) 0.30 - 0.50 L/s/ha (extreme events)
Commercial	17,000 L/ha/day	1.0 (non-coincident peak)	
Institutional	10,000 L/ha/day	1.0 (non-coincident peak)	

\*There are no industrial areas identified within the tributary area.

$$\text{Harmon Equation} = 1 + \frac{14}{4 + \left(\frac{P}{1000}\right)^{\frac{1}{2}}} \times K$$

Where:

P = Population

K = Correction Factor:

- Peak Flow = 1
- Operational = between 0.4 to 0.6 (0.6 used)

#### 3.2 Land Use Designations & Population Estimates

Population densities and unit counts for future residential development are based on the current concept plans for these areas, and are presented in **Table 3**.

**Table 3: Residential Land Use Population Densities**

Residential Land Use	Units per ha	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

The land use designations shown in **Table 4** have been applied for the areas within Phases 2 and 3 of the SNC (Node 70 to 130). The sewersheds areas and land use designations were delineated using aerial photos (existing development) and conceptual site plans (future development).

**Table 4: Land Use Designations**

Land Use Designation	
Secondary Plan	SNC Design
Residential	Residential (Low / Medium / High Density)
Institutional / Office	Institutional
Commercial	Commercial
Recreational	
Business Park	
Prestige Business Park	
Park/Open Space Area	Other*
Ex. Snow Disposal Facility (future commercial)	
Stormwater Management Facility	
Conservation Lands	
Arterial Right-of-Ways	

\* No sanitary flow contribution - extraneous flows (inflow/infiltration) only.

The overall residential population estimate and sewershed area for Phases 2 and 3 of the SNC is provided in **Table 5** below. It is assumed that the snow dump facility at the Stranderd Drive and McKenna Casey Drive will ultimately be re-zoned for commercial development.

**Table 5: Population Estimates and Areas**

Existing / Future	Estimated Population / Area	Novatech (2015)
Existing	Estimated Population	6,944 persons
	Gross Residential Area	60.09 ha
	Gross Commercial / Institutional Area	64.37 ha
	Total Sewershed Area	124.5 ha
Future (full service)	Estimated Population	27,312 persons
	Gross Residential Area	248.48 ha
	Gross Commercial / Institutional Area	228.82 ha
	Total Sewershed Area	477.3 ha

#### 4.0 SANITARY DESIGN FLOWS

The sanitary flow allocations for Phases 2 and 3 of the SNC are provided in **Table 6**. The corresponding sanitary drainage area plan is provided as **Figure 1**. Sanitary sewer flow calculations for Phases 2 and 3 and detailed sanitary sewer design sheets for Phase 2 are attached to this memorandum.

The estimated sanitary design flows from Phases 2 and 3 of the SNC (entering Node 70) are as follows:

- Present-Day Operational Design Flows (Theoretical) = 72.5 L/s
- Future Peak Design Flows = 634.2 L/s

The outlet for Phase 2 of the SNC is the existing 1050mm outlet pipe at the 2400mm maintenance hole (Node 70) located east of Longfields Drive, north of Bren-Maur Road. Given a minimum design slope of 0.10%, this sanitary trunk sewer would have a full flow capacity of 900.5 L/s. Therefore, the downstream sanitary trunk sewer would be at 70% capacity, based on the future peak design flow being 634.2 L/s.

#### **ATTACHMENTS:**

- Figure 1: Sanitary Drainage Areas and Land Use
- Sanitary Sewer Flow Calculations
- Sanitary Sewer Design Sheets (Phase 2)
- South Nepean Collector Phase 2: Hydraulics Review / Assessment (Novatech, 2015)

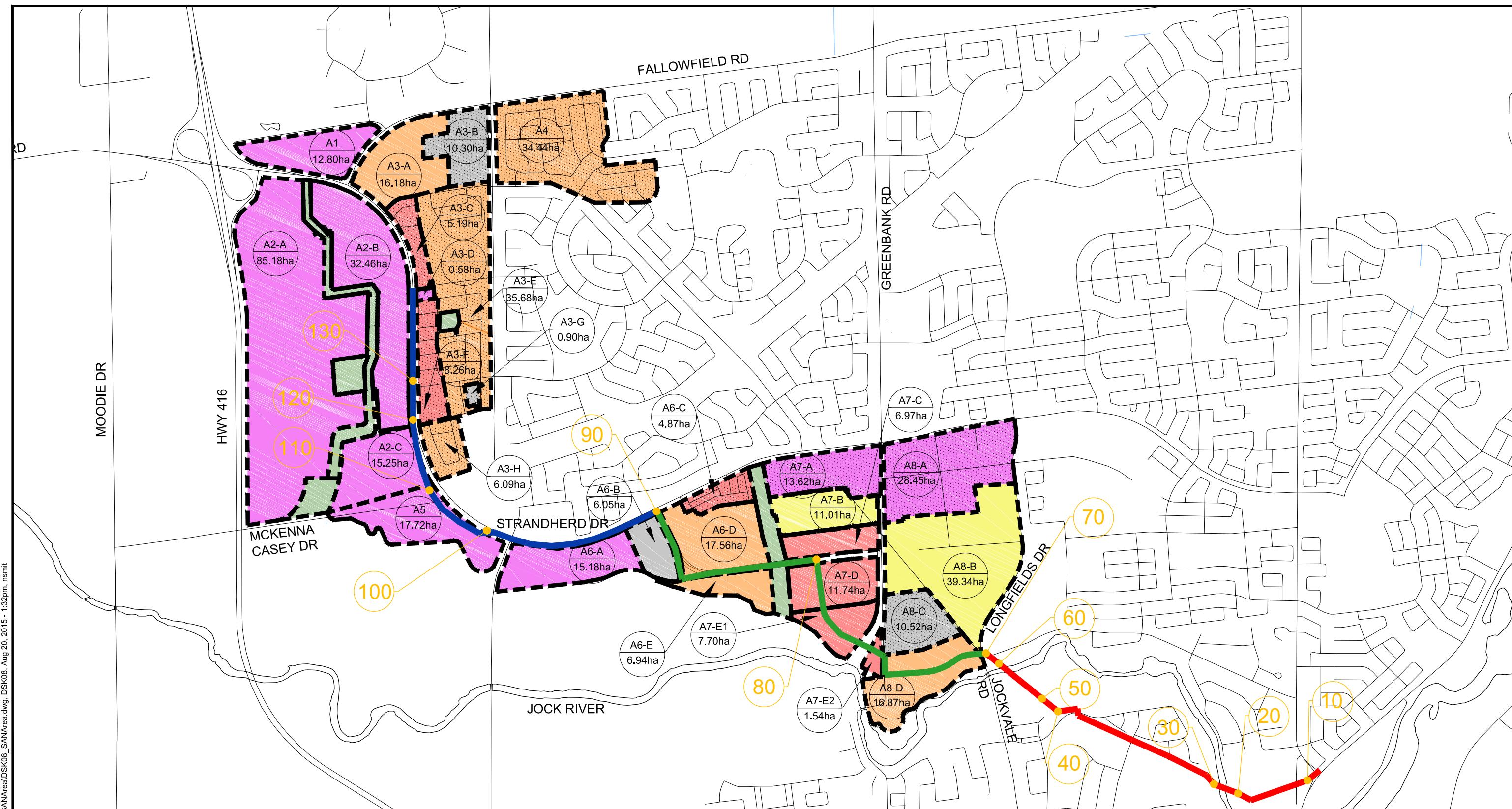


**Table 6: Updated Allocation of Commercial, Institutional and Residential Demands to Phases 2 & 3 (Nodes 70 – 130) of the SNC by Collection Area**

Collection Area	Upstream Node	Existing / Proposed Development	Existing / Proposed Land Use	Area (ha)	Estimated Number of Residential Units	Population Density (persons / ha)	Comment	Reference
A1	130	Proposed	Commercial	12.80	-	-	O'Keefe Court – Conceptual site plan shows proposed commercial.	Conceptual Plans for O'Keefe Court
A2-A	130	Proposed	Commercial	85.18	-	-	CitiGate – Analysis uses same approach as the design for CitiGate.	Detailed Servicing and SWM Report (Phase 1) (Novatech, 2014)
A2-B	130	Proposed	Commercial	32.46	-	-		
A2-C	120	Proposed	Commercial (ex. Snow dump)	15.25	-	-	Existing snow dump facility assumed to be future commercial.	Functional Design Report and Update – SNC Phase 2 and 3 (Dillon, 2012)
A3-A	130	Proposed	Low Density Residential	16.48	461	95.2	Havencrest – Existing single family units.	Havencrest Design Report (IBI, 2013)
A3-B	130	Existing	Institutional	10.30	-	-	Cedarview Middle School and Cedarview Alliance Church.	Aerial Photos / Site Visits
A3-C	130	Existing	Medium Density Residential	5.19	311	162	Existing townhouse units.	
A3-D	130	Existing	Commercial	0.58	-	-	Existing commercial buildings.	
A3-E	130	Existing	Low Density Residential	35.68	999	95.2	Existing single family units.	
A3-F	130	Existing	Medium Density Residential	8.26	496	162.0	Existing townhouse units.	
A3-G	130	Existing	Institutional	0.90	-	-	Ottawa Torah Centre Chabad.	
A3-H	120	Existing	Low Density Residential	6.09	171	95.2	Existing single family units.	
A4	130	Existing	Low Density Residential	34.44	964	95.2	Existing single family units currently serviced by Jockvale pump station; to be redirected to SNC.	Functional Design Report and Update – SNC Phase 2 and 3 (Dillon, 2012); based on 2011 Census.
A5	110	Proposed	Commercial	17.72	-	-	Proposed commercial south of McKenna Casey Drive.	Site Visits
A6-A	100	Proposed	Institutional	20.70	-	-	Proposed school site on Minto property.	Conceptual Plan for Lands Adjacent the Kennedy-Burnett SWMF provided by Minto (2015)
A6-B	90	Existing	Medium Density Residential	4.87	292	162.0	Existing townhouse units.	Aerial Photos / Site Visits
A6-C	90	Proposed	Low Density Residential	10.11	283	95.2	Proposed single family units on lands owned by Minto.	
A6-D	90	Proposed	Low Density Residential	5.59	157	95.2	Proposed single family units on lands owned by Mion.	
A6-E	90	Proposed	Low Density Residential	7.24	203	95.2	Proposed single family units on lands owned by Pavic / Braovac.	
A7-A	80	Existing	Commercial	13.62	-	-	Existing large retail stores (commercial).	Aerial Photos
A7-B	80	Proposed	High Density Residential	11.01	826	135.0	Proposed high density units on lands owned by Richcraft / Trinity.	Conceptual Plans for Lands Adjacent the Kennedy-Burnett SWMF provided by land owners.
A7-C	80	Proposed	Medium Density Residential	6.97	418	162.0	Proposed Medium density units on lands owned by Mion.	
A7-D	80	Proposed	Medium Density Residential	11.74	704	162.0	Proposed Medium density units on lands owned by Caivan.	
A7-E1/E2	80	Proposed	Medium Density Residential	9.24	554	162.0	Proposed Medium density units on lands owned by Claridge.	
A8-A	80	Existing	Commercial	28.45	-	-	Existing Barrhaven Market Place (commercial).	Aerial Photos / Site Visits
A8-B	80	Proposed	High Density Residential	39.34	2951	135.0	Future development similar to Ampersands development.	Site Visits
A8-C	80	Existing	Institutional	10.52	-	-	Existing St. Joseph High School.	Aerial Photos / Site Visits
A8-D	80	Proposed	Low Density Residential	16.87	1012	162.0	Proposed 600 low density residential units.	Functional Design Report and Update – SNC Phase 2 and 3 (Dillon, 2012)

**Attachment 1**

**Sanitary Drainage Areas and Land Use**

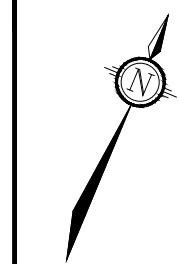


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LEGEND				SOUTH NEPEAN COLLECTOR SEWER
	EXISTING / PROPOSED HIGH DENSITY RESIDENTIAL		OTHER LANDS (OPEN SPACE, PARKS, AND SWMFS)	SANITARY DRAINAGE AREAS AND LAND USE
	EXISTING / PROPOSED MEDIUM DENSITY RESIDENTIAL		SOUTH NEPEAN COLLECTOR PHASE 1	SCALE 1:20 000
	EXISTING / PROPOSED LOW DENSITY RESIDENTIAL		SOUTH NEPEAN COLLECTOR PHASE 2	DATE MAY 2016
	EXISTING / PROPOSED COMMERCIAL		SOUTH NEPEAN COLLECTOR PHASE 3	JOB 115075
	EXISTING / PROPOSED INSTITUTIONAL		SOUTH NEPEAN COLLECTOR NODE ID	FIGURE FIG. 1

**NOVATECH**

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**Attachment 2**  
**Sewer Flow Calculations**

PROJECT #: 115075  
 DESIGNED BY: CMS  
 CHECKED BY: MJP  
 DATE: August 20, 2015

## SANITARY SEWER DESIGN SHEET

### South Nepean Collector - Phase 2 & 3

Theoretical Current Operational Peak Wastewater Flow



Location			Areas				Population				Individual Design Flows			Cumulative Design Flows					
Area I.D.	Existing Land Use	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Total Gross Area (ha)	Residential Population Density (people / ha)	Individual Residential Population	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn <sup>1</sup> )	Commercial Peak Flow Rate <sup>2</sup> (17,000 L/ha/d) (L/s)	Institutional Peak Flow Rate <sup>2</sup> (10,000 L/ha/d) (L/s)	Infiltration / Inflow Rate (0.05 L/s/ha) (L/s)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (300 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)	
A1	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
A2-A	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
A2-B	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
A3-A	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
A3-B	Institutional	130				10.30					0.0	1.2	0.5	0.0	1.2	0.5	0.0	1.7	
A3-C	Medium Density Residential	130				5.19	5.19	162.0	841	841	2.71	0.0	0.3	0.0	1.2	0.8	7.9	9.9	
A3-D	Commercial	130	0.58			0.58				841	2.71	0.1	0.0	0.1	1.2	0.8	7.9	10.0	
A3-E	Low Density Residential	130				35.68	35.68	95.2	3397	4238	2.39	0.0	0.0	1.8	0.1	1.2	2.6	35.1	39.0
A3-F	Medium Density Residential	130				8.26	8.26	162	1338	5576	2.32	0.0	0.0	0.4	0.1	1.2	3.0	44.9	49.2
A3-G	Institutional	130				0.90				5576	2.32	0.0	0.1	0.0	1.3	3.0	44.9	49.4	
A4	Low Density Residential*	130				0.00				5576	2.32	0.0	0.0	0.0	1.3	3.0	44.9	49.4	
A2-C	Snow Dump Facility	120				0.00				5576	2.32	0.0	0.0	0.0	1.3	3.0	44.9	49.4	
A3-H	Low Density Residential	120				6.09	6.09	95.2	580	6155	2.30	0.0	0.0	0.3	0.1	1.3	3.4	49.1	53.8
A5	Open Space	110				0.00				6155	2.30	0.0	0.0	0.1	1.3	3.4	49.1	53.8	
A6-A	Open Space	100				0.00				6155	2.30	0.0	0.0	0.1	1.3	3.4	49.1	53.8	
A6-B	Open Space	100				0.00				6155	2.30	0.0	0.0	0.1	1.3	3.4	49.1	53.8	
A6-C	Medium Density Residential	90				4.87	4.87	162.0	789	6944	2.27	0.0	0.0	0.2	0.1	1.3	3.6	54.6	59.6
A6-D	Open Space	90				0.00				6944	2.27	0.0	0.0	0.0	0.1	1.3	3.6	54.6	59.6
A6-E	Open Space	90				0.00				6944	2.27	0.0	0.0	0.0	0.1	1.3	3.6	54.6	59.6
A7-A	Commercial	90	13.62			13.62				6944	2.27	2.7	0.0	0.7	2.8	1.3	4.3	54.6	63.0
A7-B	Open Space	90				0.00				6944	2.27	0.0	0.0	0.0	2.8	1.3	4.3	54.6	63.0
A7-C	Open Space	90				0.00				6944	2.27	0.0	0.0	0.0	2.8	1.3	4.3	54.6	63.0
A7-D	Open Space	90				0.00				6944	2.27	0.0	0.0	0.0	2.8	1.3	4.3	54.6	63.0
A7-E1/E2	Open Space	90				0.00				6944	2.27	0.0	0.0	0.0	2.8	1.3	4.3	54.6	63.0
A8-A	Commercial	80	28.45			28.45				6944	2.27	5.6	0.0	1.4	8.4	1.3	5.7	54.6	70.0
A8-B	Open Space	80				0.00				6944	2.27	0.0	0.0	0.0	8.4	1.3	5.7	54.6	70.0
A8-C	Institutional	80				10.52				6944	2.27	0.0	1.2	0.5	8.4	2.5	6.2	54.6	71.8
A8-D	Open Space	80				0.00				6944	2.27	0.0	0.0	0.0	8.4	2.5	6.2	54.6	71.8
ROW Along SNC Sewer Alignment	-	80				14.34				6944	2.27	0.0	0.0	0.7	8.4	2.5	6.9	54.6	72.5
<b>TOTAL</b>		<b>80</b>	<b>42.65</b>	<b>21.72</b>	<b>60.09</b>	<b>138.80</b>	-	<b>6944</b>	<b>6944</b>	<b>2.27</b>	<b>8.4</b>	<b>2.5</b>	<b>6.9</b>	<b>8.4</b>	<b>2.5</b>	<b>6.9</b>	<b>54.6</b>	<b>72.5</b>	

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

Notes:

Reported Design Flows / Assumptions:

1. Harmon Equation =  $1 + [14 / (4+(P/1000)^{1/2})] \times K$

Where: P = population; K = correction factor = 0.6

2. Institutional / Commercial Peaking Factor = 1.0

1. Area A4: Existing single family units currently serviced by Jockvale pump station; currently not directed to SNC

PROJECT #: 115075  
 DESIGNED BY: CMS  
 CHECKED BY: MJP  
 DATE: August 20, 2015

### SANITARY SEWER DESIGN SHEET

#### South Nepean Collector - Phase 2 & 3

Theoretical Future Full Service Peak Wastewater Flow



Location			Areas				Population				Individual Design Flows			Cumulative Design Flows					
Area I.D.	Existing / Proposed Land Use	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Total Gross Area (ha)	Residential Population Density (people / ha)	Individual Residential Population	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn <sup>1</sup> )	Commercial Peak Flow Rate <sup>2</sup> (50,000 L/ha/d) (L/s)	Institutional Peak Flow Rate <sup>2</sup> (50,000 L/ha/d) (L/s)	Infiltration / Inflow Rate (0.28 L/s/ha) (L/s)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (350 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)	
A1	Commercial	130	12.80			12.80				3.67	11.1	0.0	3.6	11.1	0.0	3.6	0.0	14.7	
A2-A	Commercial	130	85.18			85.18				3.67	73.9	0.0	23.9	85.1	0.0	27.4	0.0	112.5	
A2-B	Commercial	130	32.46			32.46				3.67	28.2	0.0	9.1	113.2	0.0	36.5	0.0	149.8	
A3-A	Low Density Residential	130			16.18	16.18	95.2	1540	1540	3.67	0.0	0.0	4.5	113.2	0.0	41.1	22.9	177.2	
A3-B	Institutional	130		10.30		10.30				3.67	1540	0.0	8.9	113.2	8.9	43.9	22.9	189.0	
A3-C	Medium Density Residential	130		0.58		5.19	5.19	162.0	841	2381	3.53	0.0	1.5	113.2	8.9	45.4	34.0	201.6	
A3-D	Commercial	130				0.58				3.53	2381	0.5	0.0	0.2	113.7	8.9	45.6	34.0	202.2
A3-E	Low Density Residential	130				35.68	35.68	95.2	3397	5778	3.19	0.0	0.0	10.0	113.7	8.9	55.5	74.6	252.8
A3-F	Medium Density Residential	130				8.26	8.26	162	1338	7116	3.10	0.0	0.0	2.3	113.7	8.9	57.9	89.4	269.9
A3-G	Institutional	130				0.90				3.10	7116	0.0	0.8	0.3	113.7	9.7	58.1	89.4	270.9
A4	Low Density Residential	130				34.44	34.44	95.2	3279	10395	2.94	0.0	0.0	9.6	113.7	9.7	67.8	123.7	314.9
A2-C	Commercial (ex. snow dump)	120	15.25			15.25				2.94	10395	13.2	0.0	4.3	127.0	9.7	72.0	123.7	332.4
A3-H	Low Density Residential	120				6.09	6.09	95.2	580	10974	2.91	0.0	0.0	1.7	127.0	9.7	73.7	129.6	340.0
A5	Commercial	110	17.72			17.72				2.91	10974	15.4	0.0	5.0	142.4	9.7	78.7	129.6	360.3
A6-A	Commercial	100	15.18			15.18				2.91	10974	13.2	0.0	4.3	155.5	9.7	82.9	129.6	377.8
A6-B	Institutional	100		6.05		6.05				2.91	10974	0.0	5.3	1.7	155.5	15.0	84.6	129.6	384.7
A6-C	Medium Density Residential	90				4.87	4.87	162.0	789	11763	2.88	0.0	0.0	1.4	155.5	15.0	86.0	137.4	393.9
A6-D	Low Density Residential	90				17.56	17.56	95.2	1672	13435	2.83	0.0	0.0	4.9	155.5	15.0	90.9	153.8	415.2
A6-E	Low Density Residential	90				6.94	6.94	95.2	661	14096	2.81	0.0	0.0	1.9	155.5	15.0	92.9	160.2	423.6
A7-A	Commercial	90	13.62			13.62				2.81	14096	11.8	0.0	3.8	167.4	15.0	96.7	160.2	439.2
A7-B	High Density Residential	90				11.01	11.01	135.0	1486	15582	2.76	0.0	0.0	3.1	167.4	15.0	99.8	174.3	456.4
A7-C	Medium Density Residential	90				6.97	6.97	162.0	1129	16711	2.73	0.0	0.0	2.0	167.4	15.0	101.7	184.9	468.9
A7-D	Medium Density Residential	90				11.74	11.74	162.0	1902	18613	2.68	0.0	0.0	3.3	167.4	15.0	105.0	202	489.7
A7-E1/E2	Medium Density Residential	90				9.24	9.24	162.0	1497	20110	2.65	0.0	0.0	2.6	167.4	15.0	107.6	215.9	505.8
A8-A	Commercial	80	28.45			28.45				2.65	20110	24.7	0.0	8.0	192.0	15.0	115.5	215.9	538.5
A8-B	High Density Residential	80				39.34	39.34	135.0	5311	25421	2.55	0.0	0.0	11.0	192.0	15.0	126.6	262.4	596.0
A8-C	Institutional	80		10.52		10.52				2.55	25421	0.0	9.1	2.9	192.0	24.1	129.5	262.4	608.1
A8-D	Low Density Residential	80				16.87	16.87	120.9	2040	27461	2.52	0.0	0.0	4.7	192.0	24.1	134	279.8	630.2
ROW Along SNC Sewer Alignment		-	80			14.34				2.52	27461	0.0	0.0	4.0	192.0	24.1	138.2	279.8	634.2
<b>TOTAL</b>		<b>80</b>	<b>221.24</b>	<b>27.77</b>	<b>230.38</b>	<b>493.73</b>	<b>-</b>	<b>27461</b>	<b>27461</b>	<b>2.52</b>	<b>192.0</b>	<b>24.1</b>	<b>134.2</b>	<b>192.0</b>	<b>24.1</b>	<b>138.2</b>	<b>279.8</b>	<b>634.2</b>	

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

Notes:

1. Harmon Equation =  $1 + [14 / (4+(P/1000)^{1/2})] \times K$

Where: P = population; K = correction factor = 1.0

2. Institutional / Commercial Peaking Factor = 1.5

Reported Design Flows / Assumptions:

1. Area A4: Existing single family units currently serviced by Jockvale pump station to be redirected to SNC

2. Area A8-D: proposed 600 medium density residential units

THIS PRIOR NOVATECH SNC DESIGN SHEET HAD DESIGN FLOWS AT 423.6 L/S AFTER AREA ID "A6-E".

THE DSEL EVALUATION WITH NEW PARAMETERS AT THIS SAME NODE WITH CONSERVANCY WEST AND EAST INCLUDED IS ~401.58 < 423.6 L/S

Attachment 3

Sanitary Sewer Design Sheets (Phase 2)

## **SOUTH NEPEAN COLLECTOR (PHASE 2) SANITARY SEWER DESIGN SHEET**

MAY 26, 2016  
JOB# 115075

Location			Area					Population				Individual Design Flows			Cumulative Design Flows					Proposed Sewer						
From MH	To MH	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Right-of-Way (ha)	Total Gross Area (ha)	Residential Population Density (people / ha)	Individual Residential Population	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn')	Commercial Peak Flow Rate <sup>2</sup> (50,000 L/ha/d) (L/s)	Institutional Peak Flow Rate <sup>2</sup> (50,000 L/ha/d) (L/s)	Infiltration / Inflow Rate (0.28 L/s/ha) (L/s)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (350 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)	Length (m)	Pipe Size (mm)	Type	Slope %	Capacity (L/s)	Full Flow Velocity (m/s)	Ratio (Q/Qfull)
MHSA 1	MHSA 2	90	192.79	17.25	174.17	0.00	384.21	1678	20110	20110	2.65	167.352	14.97	107.58	167.4	15.0	107.6	215.9	505.8	57.3	900	CONC	0.10	597.2	0.91	85%
MHSA 2	MHSA 3	90																	505.8	57.3	900	CONC	0.10	597.2	0.91	85%
MHSA 3	MHSA 4	90																	505.8	73.9	900	CONC	0.10	597.2	0.91	85%
MHSA 4	MHSA 5	90																	505.8	34.6	900	CONC	0.10	597.2	0.91	85%
MHSA 5	MHSA 6	90																	505.8	42.8	900	CONC	0.10	597.2	0.91	85%
MHSA 6	MHSA 7	90																	505.8	84.4	900	CONC	0.10	597.2	0.91	85%
MHSA 7	MHSA 8	90																	505.8	16.5	900	CONC	0.10	597.2	0.91	85%
MHSA 8	MHSA 9	90																	505.8	85.4	900	CONC	0.10	597.2	0.91	85%
MHSA 9	MHSA 10	90																	505.8	70.6	900	CONC	0.10	597.2	0.91	85%
MHSA 10	MHSA 11	90																	505.8	70.6	900	CONC	0.10	597.2	0.91	85%
MHSA 11	MHSA 12	90																	505.8	77.8	900	CONC	0.10	597.2	0.91	85%
MHSA 12	MHSA 13	90																	505.8	77.8	900	CONC	0.10	597.2	0.91	85%
MHSA 13	MHSA 14	90																	505.8	77.8	900	CONC	0.10	597.2	0.91	85%
MHSA 14	MHSA 15	90																	505.8	25.4	900	CONC	0.10	597.2	0.91	85%
MHSA 15	MHSA 16	90																	505.8	34.2	900	CONC	0.10	597.2	0.91	85%
MHSA 16	MHSA 17	90																	505.8	86.7	900	CONC	0.10	597.2	0.91	85%
MHSA 17	MHSA 18	90																	505.8	34.3	900	CONC	0.10	597.2	0.91	85%
MHSA 18	MHSA 19	90																	505.8	68.6	900	CONC	0.10	597.2	0.91	85%
MHSA 19	MHSA 20	90																	505.8	65.5	900	CONC	0.10	597.2	0.91	85%
MHSA 20	MHSA 21	80	221.24	27.77	230.38	14.34	493.73	256	7351	27461	2.52	192.049	24.11	138.24	192.0	24.1	138.2	279.8	634.2	18.2	1050	CONC	0.10	900.9	1.01	70%
MHSA 21	MHSA 22	80																	634.2	81.9	1050	CONC	0.10	900.9	1.01	70%
MHSA 22	MHSA 23	80																	634.2	84.7	1050	CONC	0.10	900.9	1.01	70%
MHSA 23	MHSA 24	80																	634.2	77.4	1050	CONC	0.10	900.9	1.01	70%
MHSA 24	MHSA 25	80																	634.2	45.5	1050	CONC	0.10	900.9	1.01	70%
MHSA 25	MHSA 26	80																	634.2	35.8	1050	CONC	0.10	900.9	1.01	70%
MHSA 26	MHSA 27	80																	634.2	83.3	1050	CONC	0.10	900.9	1.01	70%
MHSA 27	MHSA 28	80																	634.2	74.4	1050	CONC	0.10	900.9	1.01	70%
MHSA 28	MHSA 29	80																	634.2	77.3	1050	CONC	0.10	900.9	1.01	70%
MHSA 29	MHSA 30	80																	634.2	83.8	1050	CONC	0.10	900.9	1.01	70%
MHSA 30	MHSA 31	80																	634.2	42.3	1050	CONC	0.10	900.9	1.01	70%
MHSA 31	MHSA 32	80																	634.2	100.6	1050	CONC	0.10	900.9	1.01	70%
MHSA 32	MHSA 33	80																	634.2	13.9	1050	CONC	0.10	900.9	1.01	70%
MHSA 33	MHSA 34	80																	634.2	99.9	1050	CONC	0.10	900.9	1.01	70%
MHSA 34	MHSA 35	80																	634.2	99.9	1050	CONC	0.10	900.9	1.01	70%
MHSA 35	MHSA 36	80																	634.2	88.7	1050	CONC	0.10	900.9	1.01	70%
MHSA 36	MHSA 37	80																	634.2	88.8	1050	CONC	0.10	900.9	1.01	70%
MHSA 37	MHSA 38	80																	634.2	90.3	1050	CONC	0.10	900.9	1.01	70%
MHSA 38	MHSA 39	80																	634.2	87.5	1050	CONC	0.10	900.9	1.01	70%

#### **Design Parameters:**

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles / semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row / townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

### Notes:

### Reported Design Flows / Assumptions:

- Harmon Equation =  $1 + [14 / (4 + (P/1000)^{1/2})] \times K$

Where: P = population; K = correction factor = 1.0

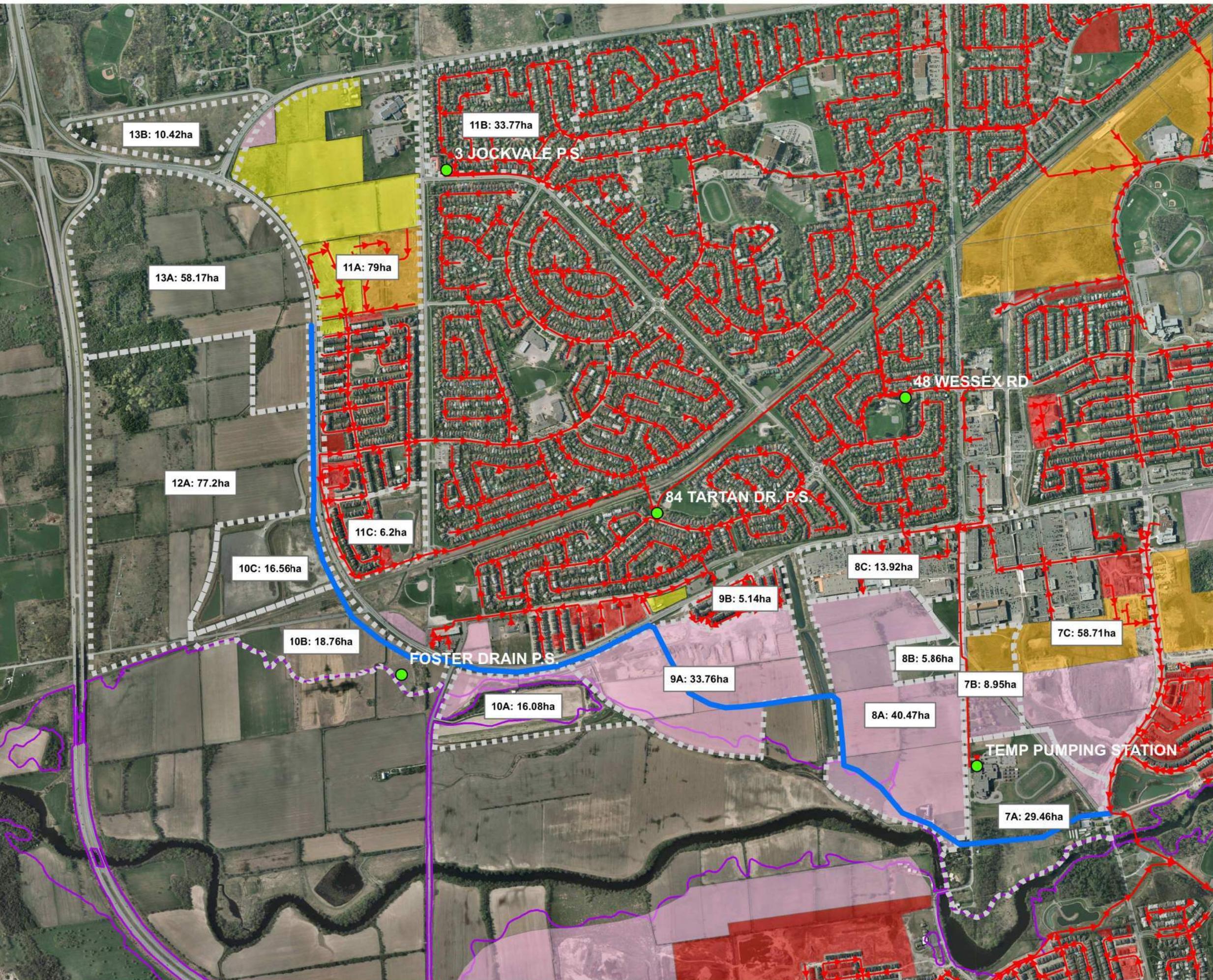
  - Institutional / Commercial Peaking Factor = 1.5

1. Area A4: Existing single family units currently serviced by Jockvale pump station to be redirected to SNC
  2. Area A8-D: proposed 600 medium density residential units



**City of Ottawa**  
South Nepean Collector

**Figure 01**  
Existing Sanitary Network and Collection Areas



NOT TO SCALE

MAP DRAWING INFORMATION:  
DATA PROVIDED BY THE CITY OF OTTAWA

MAP CREATED BY: BC  
MAP CHECKED BY: MBM  
MAP PROJECTION: NO PROJECTION

FILE LOCATION: \\Dillon.ca\\dillon\_dfs\\Ottawa\\Ottawa.CA\\CAD\\2011\\115681\\Design\_GIS\\MXD\\Figure01\_c\_ExistingSanitaryNetwork.mxd



PROJECT: 11-5681  
STATUS: FINAL  
DATE: 18/07/12

**Table 5.1: Allocation of Commercial/Institutional and Residential Demands to SNC by Collection Area**

Collection Area	Discharging Node	Estimated from GIS			City of Ottawa VURL Data			Other Space <sup>1</sup> (ha)	Population (PE)	Residential Density (PE/net ha)	Comments	Additional Source(s)
		Gross Institutional/Commercial (ha)	Gross Residential (ha)	Gross Area (ha)	Net Residential (ha)	Units (#)	Unit Density (#/ha)					
7A	70	13.5	7.4	29.5	4.0	605	0.3	9.1	1637	4.25	Flow calculations include St Joseph H.S. Pump Station firm capacity of 7.0 L/s Additional 600 units (TAC)	3.4ppu (TAC)
7B		0.0	9.24	9.24	6.23	1474	136.7	3.0	3321	638.8	Population from split VURL allocated by area. VURL parcel id 323 - inconsistency between net and gross reported area.	2.7ppu (TAC)
8A		0.0	40.0	40.0	24.1	4462	185.1	15.9	12047.4	499.9		2.7ppu (TAC)
8B		5.9	0.0	5.9	0.0	0	0	0.0			Future Commercial area	
8C		13.9	0.0	13.9	0.0	0	0	0.0			Commercial area includes Home Depot	
9A	80	0.0	33.8	33.8	18.6	635	34.1	15.2	2210	116.2		3.4ppu (TAC)
10A	90	0.0	16.1	16.1	9.7	451	28.0	6.4	1533.4	158.0	Assume net population = 60% gross.	3.4ppu (TAC)
10B	100	18.8	0.0	35.3	0.0	0	0	16.5			Allocated as potential future I/C use as directed by TAC	
10C	110	16.6	0.0	35.3	0.0	0	0	18.7			Area includes current Municipal Snow Dump. Flow allowance is made for potential future I/C use	
11C		0.0	6.2	6.2	Note 2			2.5	306	82.7	This area is south of '11 block' in the existing development	From IBI Apr 2010 Report Figure 1
11A	120	12.5	66.5	79.0				26.6	3923	98.3	Institutional includes 4.38ha church site and 6.89 ha institution at northeast corner, as well and Claridge Commercial (0.56ha) and DCR/Phoenix Commercial (0.64ha)	From IBI Apr 2010 Report Figure 1
11B		0.0	37.0	37.0				14.8	1550	69.8	Presently serviced by Jockvale pump station; to be redirected to SNC.	Estimated from 2011 Census Block data
12A		77.2	0.0	77.2				0.0			Allow sanitary peak flow 79.0 L/s	Novatech, Employment Lands Report, Revised Jan 2012
13A	130	58.5	0.0	58.5				0.0			Allow sanitary peak flow 62.8 L/s plus Collection Area 13B, total 82.2 L/s	
13B		12.5	0.0	12.5				0.0			Allow sanitary peak flow 19.4 L/s; gravity discharge to Collection Area 13A	IBI/Novatech

Notes:

1. Other space includes other residential space accounting for the difference between gross area (measured with GIS) and net area (provided in VURL data), such as sidewalks, roads, greenspace, etc.
2. Collection Area 11A and 11B population and land use as identified under Additional Source(s). Other space reported as 60% of gross residential area, consistent with VURL average.

**SOUTH NEPEAN COLLECTOR SEWER**  
**SANITARY SEWER DESIGN SHEET - Operational Service (Average Flow Design Parameters)**

Sheet 1 of 1



Project 11-5681

CHECKED		
TODAY:		7/18/201

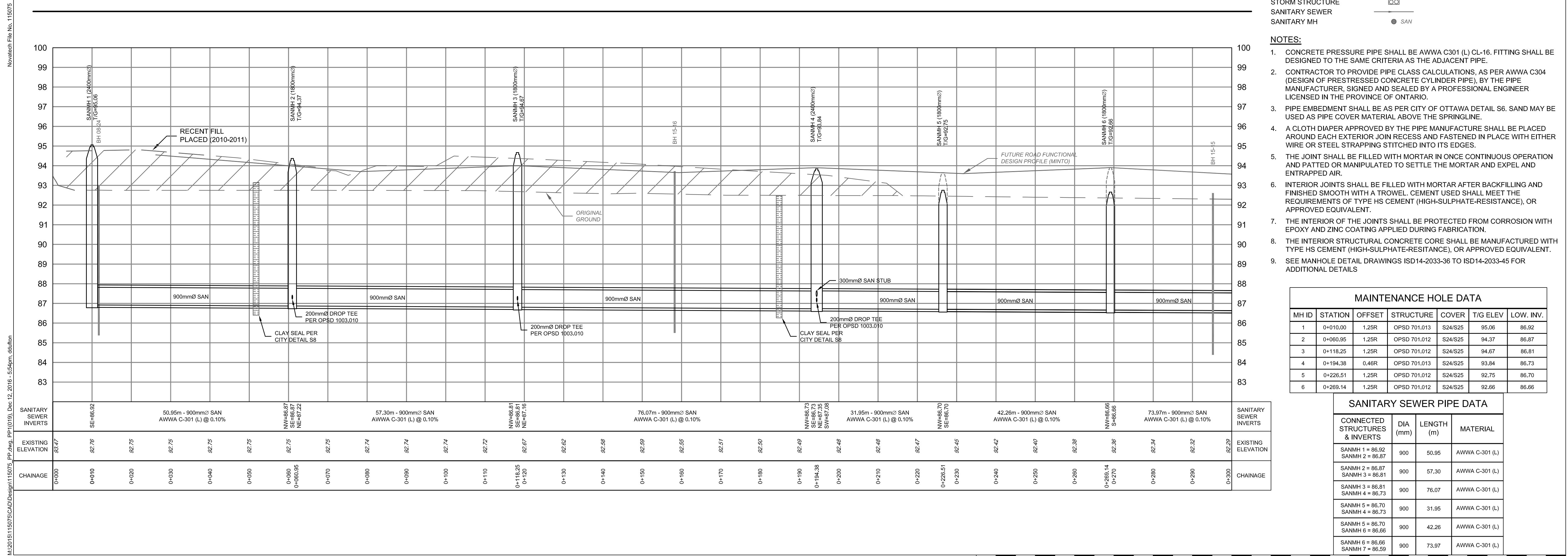
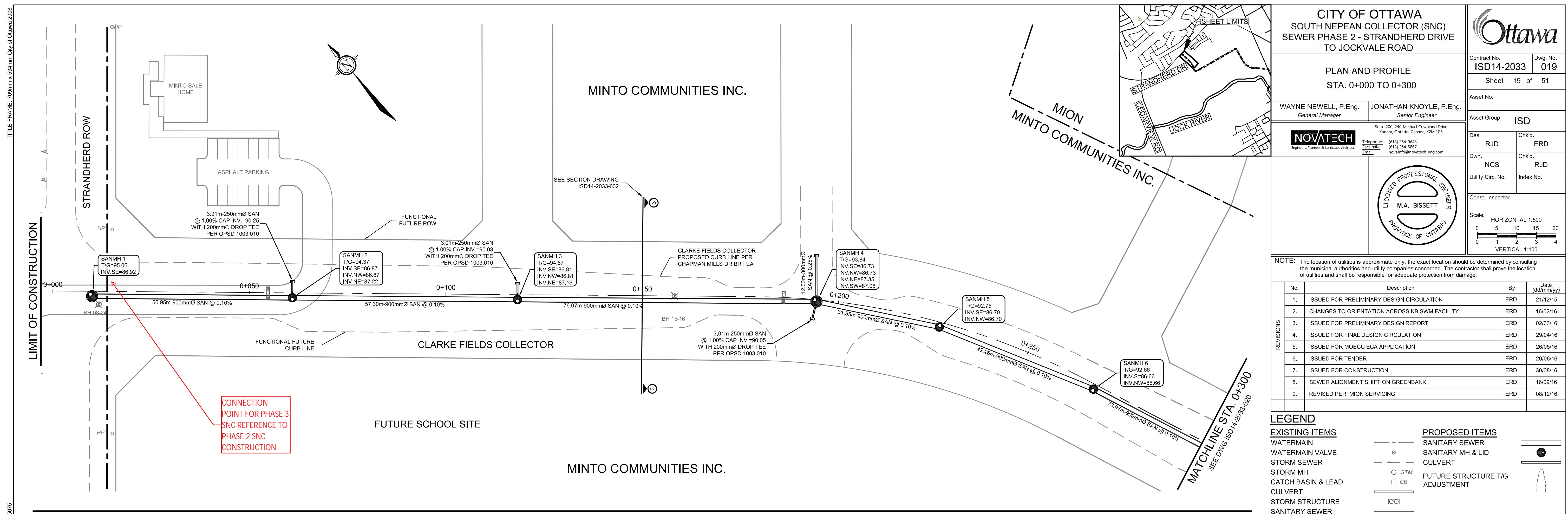
## SOUTH NEPEAN COLLECTOR SEWER

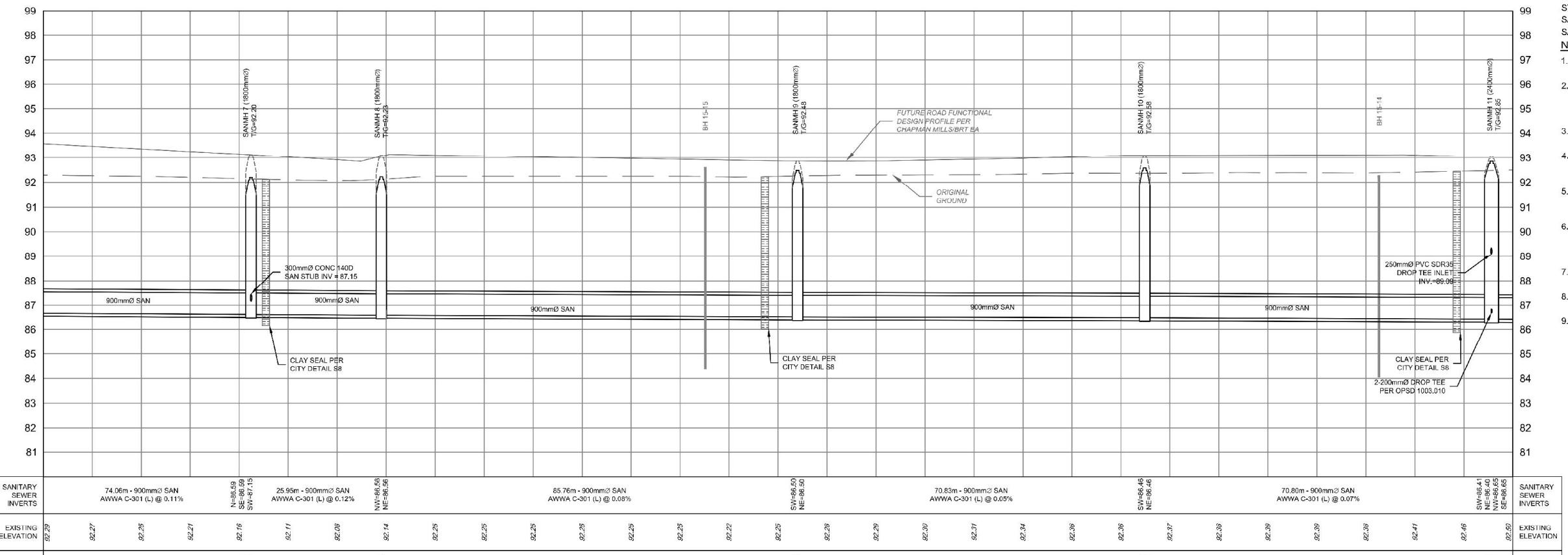
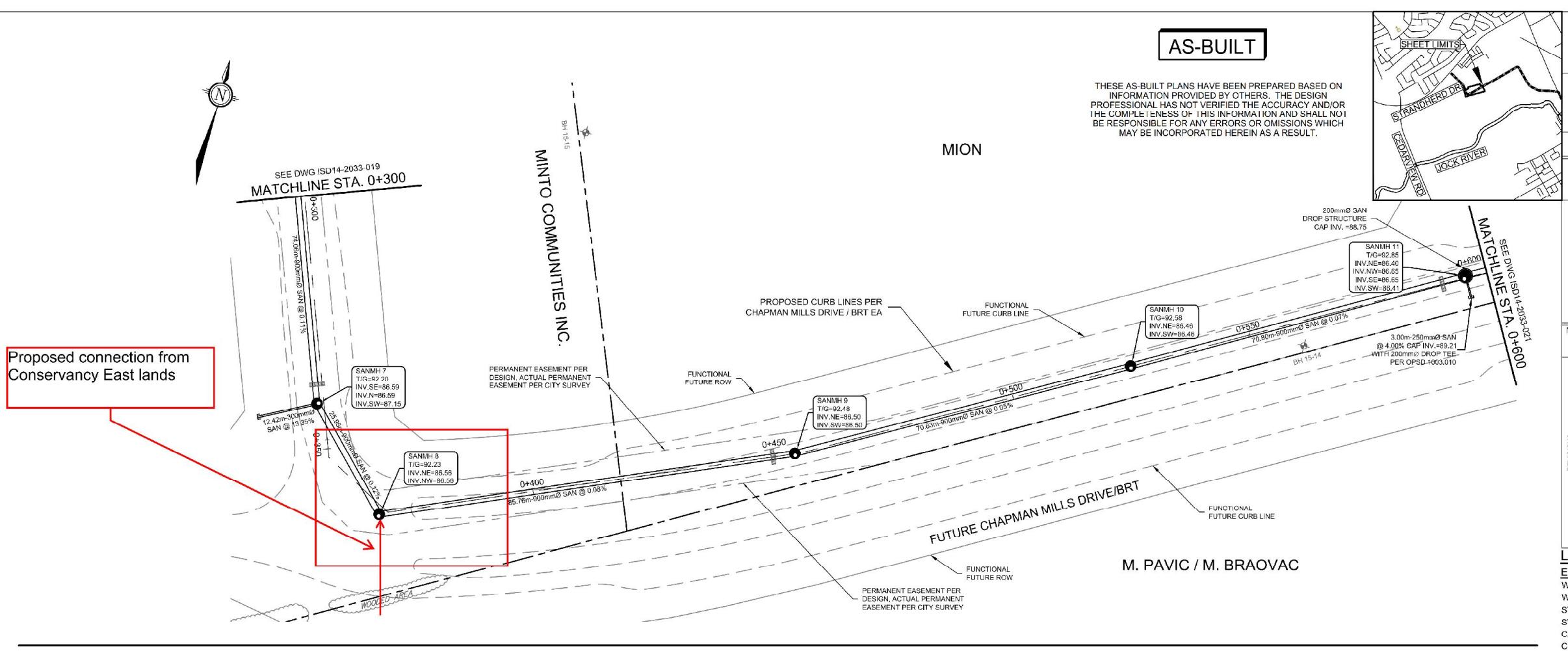
## SANITARY SEWER DESIGN SHEET - Full Service (Peak Flow Design Parameters)

Sheet 1 of 1

TRIBUTARY AREA	LOCATION	AREA (ha)								INDIVIDUAL		CUMULATIVE		RESIDENTIAL		COMMERCIAL & INSTITUTION		INFIL. INFLOW	PEAK DESIGN	PROPOSED SEWER						PEAK DESIGN											
		Design Factors	FROM	TO	Gross ICI	Net ICI	Other ICI space (Green, Sidewalks, roads)	Gross RESIDENTIAL Area	Net Residential Area	Other Res (Sidewalks, roads)	TOTAL AREA (Gross ICI plus Gross Residential)	POP	DENSITY	POP	Total I/C and Res AREA	PEAKING FACTOR	RESIDENT_FLOW	I/C CUM. AREA	I/C FLOW (l/s)	Q(p)	FLOW Q(d)	LENGTH	GROUND ELEVATION	DEPTH OF COVER	PIPE SIZE	INVERT 1	INVERT 2	PIPE TYPE	GRADE	CAPACITY	Q(d)/Q(c)	VELOCITY at capacity	DEPTH	VELOCITY			
												(pers/net ha.)	(ha.)	(L/s)	(L/s)	(L/s)	(L/s)	(L/s)	(L/s)	(L/s)	(L/s)	(m)	(m)	(m)	(m)	(m)	(m)	(m)	(L/s)	(m/s)	(m)	(m/s)					
13A	1				58.5	43.9	14.6	0.0	0.0	0.0	58.5	0		0	58.5	4.50	0.00	1.50	58.50	50.90	16.38	67.28															
13B	1		Node 130		12.5	9.4	3.1	0.0	0.0	0.0	12.5	0		0	71.0	4.50	0.00	1.50	71.00	61.77	19.88	81.65															
12A	1		Node 130		77.2	57.9	19.3	0.0	0.0	0.0	77.2	0		0	148.2	4.50	0.00	1.50	148.20	128.93	41.50	170.43															
11A	1				12.5	9.4	3.1	66.5	39.9	26.6	79.0	3923	98.32	3923	227.2	3.34	53.09	1.50	160.70	139.81	63.62	256.52															
11B	1		Node 120		0.0	0.0	0.0	37.0	22.2	14.8	37.0	1550	69.82	5473	264.2	3.21	71.13	1.50	160.70	139.81	73.98	284.92	531.89	93.60	4.42	0.750	88.96	88.43	Conc.	0.10%	353.24	0.81	0.80	0.53	0.90		
11C			Node 120		0.0	0.0	0.0	6.2	3.7	2.5	6.2	306	82.26	5779	270.4	3.19	74.59	1.50	160.70	139.81	75.71	290.1															
10C	1		Node 110		16.6	12.5	4.2	0.0	0.0	0.0	16.6	0		0	5779	287.0	3.19	74.59	1.50	177.30	154.25	80.36	309.20	497.82	93.44	4.76	0.750	88.43	87.93	Conc.	0.10%	353.24	0.88	0.80	0.55	0.91	
10B	1		Node 110	Node 100	18.8	14.1	4.7	0.0	0.0	0.0	18.8	0		0	5779	305.8	3.19	74.59	1.50	196.10	170.61	85.62	330.82	603.17	93.03	4.95	0.750	87.93	87.33	Conc.	0.10%	353.24	0.94	0.80	0.58	0.92	
10A	1		Node 100	Node 90	0.0	0.0	0.0	16.1	9.7	6.4	16.1	1533	158.04	7312	321.9	3.09	91.48	1.50	196.10	170.61	90.13	352.22	430.49	93.75	6.03	0.825	87.33	86.90	Conc.	0.10%	455.17	0.77	0.85	0.55	0.95		
9A	1		Node 90	Node 80	0.0	0.0	0.0	33.8	18.6	15.2	33.8	2161	116.18	9473	355.7	2.98	114.28	1.50	196.10	170.61	99.60	384.48	1268.65	92.37	5.84	0.900	86.90	85.63	Conc.	0.10%	573.71	0.67	0.90	0.55	0.97		
8A	1		Node 80		0.0	0.0	0.0	40.0	24.1	15.9	40.0	12047	499.88	21520	395.7	2.62	228.45	1.50	196.10	170.61	110.80	509.85															
8B	1				5.9	4.4	1.5	0.0	0.0	0.0	5.9	0		0	21520	401.6	2.62	228.45	1.50	202.00	175.74	112.45	516.64														
8C	1				13.9	10.4	3.5	0.0	0.0	0.0	13.9	0		0	21520	415.5	2.62	228.45	1.50	215.90	187.83	116.34	532.62														
7A	1				13.5	10.1	3.4	16.5	5.2	11.3	30.0	1637	314.81	23157	445.5	2.59	242.84	1.50	229.40	199.58	124.74	567.6															
7B	1		Node 70		0.0	0.0	0.0	9.2	6.2	3.0	9.2	3980	636.84	27137	454.7	2.52	277.05	1.50	229.40	199.58	127.32	603.94	1448.96	91.24	6.01	1.050	85.63	84.18	Conc.	0.10%	864.51	0.70	1.00	0.64	1.07		
					225.3	129.7		454.7	27.137.0																												
				</																																	







CITY OF OTTAWA  
SOUTH NEPEAN COLLECTOR (SNC)  
SEWER PHASE 2 - STRANDHERD DRIVE  
TO JOCKVALE ROAD



Contract No. ISD14-2033 Dwg. No. 020  
Sheet 20 of 51  
Asset No.  
Asset Group ISD

Des RJD Chkd. ERD  
Dwn. NCS Chkd.  
Utility Circ. No. Index No.  
Const. Inspector

Scale: HORIZONTAL 1:500  
0 5 10 15 20  
0 1 2 3 4  
VERTICAL 1:100

NOTE: The location of utilities is approximate only, the exact location should be determined by consulting the municipal authorities and utility companies concerned. The contractor shall prove the location of utilities and shall be responsible for adequate protection from damage.

No.	Description	By (dd/mm/yy)
1.	ISSUED FOR PRELIMINARY DESIGN CIRCULATION	FRN 21/12/15
2.	CHANGES TO ORIENTATION ACROSS KB SWM FACILITY	ERD 16/02/16
3.	ISSUED FOR PRELIMINARY DESIGN REPORT	ERD 02/03/16
4.	ISSUED FOR FINAL DESIGN CIRCULATION	ERD 29/04/16
5.	ISSUED FOR MOECC ECA APPLICATION	ERD 26/05/16
6.	ISSUED FOR TENDER	ERD 20/06/16
7.	ISSUED FOR CONSTRUCTION	ERD 30/08/16
8.	SEWER ALIGNMENT SHIFT ON GREENBANK	ERD 16/09/16
9.	REVISED FOR MION SERVICING	ERD 08/12/16
10.	MINTO LANDS MANHOLE UPDATE	ERD 24/04/17
11.	ISSUED FOR AS-BUILT	ERD 26/09/17

#### LEGEND

<b>EXISTING ITEMS</b>	<b>PROPOSED ITEMS</b>
WATERMAIN	SANITARY SEWER
WATERMAIN VALVE	SANITARY MH & LID
STORM SEWER	CULVERT
STORM MH	● STM
CATCH BASIN & LEAD	□ CR
CULVERT	FUTURE STRUCTURE T/G ADJUSTMENT
STORM STRUCTURE	□ CR
SANITARY SEWER	● SAN
SANITARY MH	

- NOTES:**
- CONCRETE PRESSURE PIPE SHALL BE AWWA C301 (L) CL-16. FITTING SHALL BE DESIGNED TO THE SAME CRITERIA AS THE ADJACENT PIPE.
  - CONTRACTOR TO PROVIDE PIPE CLASS CALCULATIONS, AS PER AWWA C304 (DESIGN OF PRESTRESSED CONCRETE CYLINDER PIPE), BY THE PIPE MANUFACTURER, SIGNED AND SEALED BY A PROFESSIONAL ENGINEER LICENCED IN THE PROVINCE OF ONTARIO.
  - PIPE EMBEDMENT SHALL BE AS PER CITY OF OTTAWA DETAIL S6. SAND MAY BE USED AS PIPE COVER MATERIAL ABOVE THE SPRINGLINE.
  - A CLOTH DIAPER APPROVED BY THE PIPE MANUFACTURE SHALL BE PLACED AROUND EACH EXTERIOR JOIN RECESS AND FASTENED IN PLACE WITH EITHER WIRE OR STEEL STRAPPING STITCHED INTO ITS EDGES.
  - THE JOINT SHALL BE FILLED WITH MORTAR IN ONCE CONTINUOUS OPERATION AND PATTED OR MANIPULATED TO SETTLE THE MORTAR AND EXPEL ANY ENTRAPPED AIR.
  - INTERIOR JOINTS SHALL BE FILLED WITH MORTAR AFTER BACKFILLING AND FINISHED SMOOTH WITH A TROWEL. CEMENT USED SHALL MEET THE REQUIREMENTS OF TYPE HS CEMENT (HIGH-SULPHATE-RESISTANCE), OR APPROVED EQUIVALENT.
  - THE INTERIOR OF THE JOINTS SHALL BE PROTECTED FROM CORROSION WITH EPOXY AND ZINC COATING APPLIED DURING FABRICATION.
  - THE INTERIOR STRUCTURAL CONCRETE CORE SHALL BE MANUFACTURED WITH TYPE HS CEMENT (HIGH-SULPHATE-RESISTANCE), OR APPROVED EQUIVALENT.
  - SEE MANHOLE DETAIL DRAWINGS ISD14-2033-36 TO ISD14-2033-45 FOR ADDITIONAL DETAILS

MAINTENANCE HOLE DATA					
MH ID	STATION	OFFSET	STRUCTURE	COVER	T/G ELEV
7	0+342.41	1.41R	OPSD 701.012	S24/S25	92.20
8	0+369.03	1.50R	OPSD 701.012	S24/S25	92.23
9	0+453.99	0.07L	OPSD 701.012	S24/S25	92.48
10	0+524.84	0.04L	OPSD 701.012	S24/S25	92.58
11	0+595.64	0.41L	OPSD 701.013	S24/S25	92.85
					86.40

SANITARY SEWER PIPE DATA				
CONNECTED STRUCTURES & INVERTS	DIA (mm)	LENGTH (m)	MATERIAL	
SANMH 6 = 86.68 SANMH 7 = 86.59	900	74.06	AWWA C-301 (L)	
SANMH 8 = 86.56 SANMH 9 = 86.55	900	25.95	AWWA C-301 (L)	
SANMH 8 = 86.55 SANMH 9 = 86.50	900	85.76	AWWA C-301 (L)	
SANMH 10 = 86.46 SANMH 11 = 86.41	900	70.83	AWWA C-301 (L)	
SANMH 10 = 86.40 SANMH 12 = 86.32	900	78.15	AWWA C-301 (L)	



## SANITARY SEWER CALCULATION SHEET



Manning's n=0.013

## SANITARY SEWER CALCULATION SHEET



Manning's n=0.013

Lower flows than what was previously projected (77.81 L/s) in the Phase 2, 3, & 4 sanitary design sheet downstream.

DESIGN PARAMETERS						Designed:	PROJECT:
Park Flow =	9300	L/ha/da	0.10764	I/s/Ha	Industrial Peak Factor = as per MOE Graph		
Average Daily Flow =	280	I/p/day	Extraneous Flow = 0.286 L/s/ha			Checked:	LOCATION:
Comm/Inst Flow =	28000	L/ha/da	0.3241	I/s/Ha	Minimum Velocity = 0.600 m/s	Barrhaven Conservancy East Phase 5	
Industrial Flow =	35000	L/ha/da	0.40509	I/s/Ha	Manning's n = (Conc) 0.013 (Pvc) 0.013	City of Ottawa	
Max Res. Peak Factor =	4.00	Townhouse coeff= 2.7			Dwg. Reference:	Date:	Sheet No:
Commercial/Inst./Park Peak Factor =	1.00	Single house coeff= 3.4			Sanitary Drainage Plan, Dwgs. No.	01 Dec 2022	of 2
Institutional =	0.32	I/s/Ha					

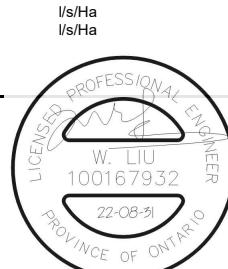


# SANITARY SEWER CALCULATION SHEET



Manning's n=0.013

LOCATION			RESIDENTIAL AREA AND POPULATION								COMM		INSTIT		PARK		C+H		INFILTRATION			PIPE										
STREET	FROM M.H.	TO M.H.	AREA (ha)	UNITS Singles	UNITS Townhouse	POP.	CUMULATIVE		PEAK FACT.	PEAK FLOW (l/s)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	PEAK FLOW (l/s)	TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	DIST (m)	DIA (mm)	SLOPE (%)	CAP. (FULL) (l/s)	RATIO Q act/Q cap	VEL.					
							AREA (ha)	POP.																								
Ainsworth Crescent	80A	81A	0.51	10	10	34	0.51	34	3.68	0.41	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.51	0.51	0.17	0.57	69.0	200	0.65	26.44	0.02	0.84	0.34				
	81A	82A	0.38	11	11	38	0.89	72	3.62	0.85	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.38	0.89	0.29	1.14	70.0	250	0.25	29.73	0.04	0.61	0.29				
To Sapling Grove, Pipe 82A - 85A							0.89	72			0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.89														
	78A	59A	0.07	1	1	4	0.07	4	3.76	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.07	0.07	0.02	0.07	13.0	200	0.65	26.44	0.00	0.84	0.17				
	59A	60A	0.45	11	11	38	0.52	42	3.66	0.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.45	0.52	0.17	0.67	76.0	250	0.25	29.73	0.02	0.61	0.24				
	60A	61A	0.41	12	12	41	0.93	83	3.61	0.97	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.41	0.93	0.31	1.28	75.0	250	0.25	29.73	0.04	0.61	0.30				
To Sapling Grove, Pipe 61A - 82A							0.93	83			0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.93														
Syringa Court	55A	56A	0.14	2	2	7	0.14	7	3.74	0.08	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.14	0.14	0.05	0.13	11.0	200	0.65	26.44	0.00	0.84	0.22				
	56A	57A	0.42	11	11	38	0.56	45	3.66	0.53	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.42	0.56	0.18	0.72	67.0	250	0.65	47.94	0.01	0.98	0.35				
	57A	58A	0.34	10	10	34	0.90	79	3.62	0.93	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.34	0.90	0.30	1.22	67.5	250	0.25	29.73	0.04	0.61	0.29				
To Sapling Grove, Pipe 58A - 61A							0.90	79			0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.90														
	55A	53A	0.17	3	3	11	0.17	11	3.73	0.13	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.17	0.17	0.06	0.19	45.5	200	0.65	26.44	0.01	0.84	0.24				
	53A	49A	0.08	1	1	4	0.25	15	3.72	0.18	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.08	0.25	0.08	0.26	9.0	250	0.25	29.73	0.01	0.61	0.18				
	49A	50A	0.44	11	11	38	0.69	53	3.65	0.63	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.44	0.69	0.23	0.85	68.5	250	0.25	29.73	0.03	0.61	0.27				
To Sapling Grove, Pipe 51A - 58A							1.03	87	3.61	1.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.34	1.03	0.34	1.36	66.5	250	0.25	29.73	0.05	0.61	0.31				
Ecology Lane	880A	88A	0.44	10	10	34	0.44	34	3.68	0.41	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.44	0.44	0.15	0.55	76.0	200	0.65	26.44	0.02	0.84	0.33				
Contribution From Sapling Grove, Pipe 85A - 88A							5.48	453			0.00	0.00	0.00	0.00	0.00	0.00	0.00	5.48		5.92												
	88A	91A	0.18	4	4	14	6.10	501	3.38	5.49	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.18	6.10	2.01	7.50	60.0	250	0.25	29.73	0.25	0.61	0.50				
Contribution From Peninsula Road, Pipe 90A - 91A							0.78	79			0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.78	6.88													
	91A	92A	0.08			0	6.96	580	3.35	6.30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.08	6.96	2.30	8.60	62.5	250	0.25	29.73	0.29	0.61	0.52				
To Conservancy Drive, Pipe 92A - 93A							6.96	580			0.00	0.00	0.00	0.00	0.00	0.00	0.00	6.96														
Anemone Mews							0.09		0	0.09	0		0.00	0.00	0.00	0.00	0.00	0.00	0.09	0.09												
Contribution From Peninsula Road, Pipe 62A - 63A							0.95	90			0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.95		1.04												
Contribution From Peninsula Road, Pipe 89A - 63A							0.17	14			0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.17		1.21												
	63A	75A	0.09			0	1.30	104	3.59	1.21	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.09	1.30	0.43	1.64	62.5	250	0.25	29.73	0.06	0.61	0.32				
To Conservancy Drive, Pipe 75A - 76A							1.30	104			0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.30														
Contribution From Les Emmerson Drive (N), Pipe 70A - 72A							1.09	99			0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.09														
	72A	74A	0.27	6	6	21	3.61	336	3.45	3.75	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.25		3.34												
Contribution From Les Emmerson Drive (N), Pipe 71A - 72A							1.30	132			0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.30		4.91												
Contribution From Les Emmerson Drive (S), Pipe 69A - 74A							0.71	76			0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.71		5.62												
Contribution From Les Emmerson Drive (S), Pipe 73A - 74A							5.88	565	3.36	6.15	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.26	5.88	1.94	8.09	52.0	250	0.25	29.73	0.27	0.61	0.51				
	74A	750A	0.26	6	6	21	5.88	565	3.36	6.15	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	5.89	1.94	8.09	10.5	250	0.25	29.73	0.27	0.61	0.51				
	750A	75A	0.01			0	5.89	565	3.36	6.15	0.00	0.00	0.00	0.00	0.00	0.00	0.00	5.89														
To Conservancy Drive, Pipe 75A - 76A							5.89	565			0.00	0.00	0.00	0.00	0.00	0.00	0.00															
Gallium Crescent	30A	31A	0.37	10	10	34	0.37	34	3.68	0.41	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.37	0.37	0.12	0.53	65.0	200	0.65	26.44	0.02	0.84	0.33				



Industrial Peak Factor = as per MOE Graph  
 Extraneous Flow = 0.330 L/s/ha  
 Minimum Velocity = 0.600 m/s  
 Manning's n = (Conc) 0.013 (Pvc) 0.013  
 Commercial/Inst./Park Peak Factor = 4.00  
 Commercial/Inst./Park Peak Factor = 1.50  
 Institutional = 0.32 l/s/Ha

Designed: A.K.  
 Checked: W



# SANITARY SEWER CALCULATION SHEET



Manning's n=0.013

LOCATION			RESIDENTIAL AREA AND POPULATION								COMM		INSTIT		PARK		C+H		INFILTRATION			PIPE								
STREET	FROM M.H.	TO M.H.	AREA (ha)	UNITS	UNITS Singles	UNITS Townhouse	POP.	CUMULATIVE		PEAK FACT.	PEAK FLOW (l/s)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	PEAK FLOW (l/s)	TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	DIST (m)	DIA (mm)	SLOPE (%)	CAP. (FULL) (l/s)	RATIO Q act/Q cap	VEL.		
								AREA (ha)	POP.																					
Mineral Street																														
	430A	46A	0.29	6	6		21	0.29	21	3.70	0.25		0.00		0.00		0.00	0.00	0.29	0.29	0.10	0.35	45.5	200	0.65	26.44	0.01	0.84	0.29	
Contribution From Les Emmerson Drive (S), Pipe 45A - 46A								0.87	95				0.00		0.00		0.00	0.00	0.87	1.16										
To Conservancy Drive, Pipe 47A - 48A		46A	47A	0.29	6	6	21	1.45	137	3.56	1.58		0.00		0.00		0.00	0.00	0.29	1.45	0.48	2.06	62.5	250	0.25	29.73	0.07	0.61	0.34	
Contribution From Sapling Grove, Pipe 32A - 37A								1.45	137				0.00		0.00		0.00	0.00	1.45											
Contribution From Gallium Crescent, Pipe 36A - 37A								1.16	91				0.00		0.00		0.00	0.00	1.16	4.07										
	37A	39A	0.08				0	4.15	315	3.46	3.53		0.00		0.00		0.00	0.00	0.08	4.15	1.37	4.90	60.0	250	0.25	29.73	0.16	0.61	0.44	
Contribution From Peninsula Road, Pipe 38A - 39A								1.05	83				0.00		0.00		0.00	0.00	1.05	5.20										
	39A	47A	0.08				0	5.28	398	3.42	4.41		0.00		0.00		0.00	0.00	0.08	5.28	1.74	6.15	62.5	250	0.25	29.73	0.21	0.61	0.47	
To Conservancy Drive, Pipe 47A - 48A								5.28	398				0.00		0.00		0.00	0.00	5.28											
Les Emmerson Drive (S)																														
	44A	17A	0.39	16		16	44	0.39	44	3.66	0.52		0.00		0.00		0.00	0.00	0.39	0.39	0.13	0.65	73.0	200	0.65	26.44	0.02	0.84	0.35	
To Les Emmerson Drive (N), Pipe 17A - 18A								0.39	44				0.00		0.00		0.00	0.00	0.39											
	44A	45A	0.64	27		27	73	0.64	73	3.62	0.86		0.00		0.00		0.00	0.00	0.64	0.64	0.21	1.07	111.0	200	0.65	26.44	0.04	0.84	0.41	
	45A	46A	0.23	8		8	22	0.87	95	3.60	1.11		0.00		0.00		0.00	0.00	0.23	0.87	0.29	1.40	61.5	250	0.25	29.73	0.05	0.61	0.31	
To Mineral Street, Pipe 46A - 47A								0.87	95				0.00		0.00		0.00	0.00	0.87											
	730A	73A	0.46	20		20	54	0.46	54	3.65	0.64		0.00		0.00		0.00	0.00	0.46	0.46	0.15	0.79	74.0	200	0.65	26.44	0.03	0.84	0.37	
	73A	74A	0.25	8		8	22	0.71	76	3.62	0.89		0.00		0.00		0.00	0.00	0.25	0.71	0.23	1.13	68.5	250	0.25	29.73	0.04	0.61	0.29	
To Anemone Mews, Pipe 74A - 750A								0.71	76				0.00		0.00		0.00	0.00	0.71											
	65A	66A	0.17	5		5	14	0.17	14	3.72	0.17		0.00		0.00		0.00	0.00	0.17	0.17	0.06	0.22	37.5	200	0.65	26.44	0.01	0.84	0.26	
	66A	67A	0.14	3		3	9	0.31	23	3.70	0.28		0.00		0.00		0.00	0.00	0.14	0.31	0.10	0.38	11.0	250	0.25	29.73	0.01	0.61	0.20	
	67A	69A	0.58	24		24	65	0.89	88	3.61	1.03		0.00		0.00		0.00	0.00	0.58	0.89	0.29	1.32	100.0	250	0.25	29.73	0.04	0.61	0.30	
To Anemone Mews, Pipe 74A - 750A								69A	74A	0.41	16	44	1.30	132	3.57	1.53	0.00	0.00	0.41	1.30	0.43	1.95	93.0	250	0.25	29.73	0.07	0.61	0.34	
Les Emmerson Drive (N)																														
	16A	17A	0.22	4	4		14	0.22	14	3.72	0.17		0.00		0.00		0.00	0.00	0.22	0.22	0.07	0.24	52.5	200	0.65	26.44	0.01	0.84	0.26	
Contribution From Les Emmerson Drive (S), Pipe 44A - 17A								0.39	44				0.00		0.00		0.00	0.00	0.39	0.61										
To Conservancy Drive, Pipe 18A - 23A		17A	18A	0.22	5	5	17	0.83	75	3.62	0.88		0.00		0.00		0.00	0.00	0.22	0.83	0.27	1.15	63.0	250	0.25	29.73	0.04	0.61	0.29	
	64A	70A	0.44	10	10		34	0.44	34	3.68	0.41		0.00		0.00		0.00	0.00	0.44	0.44	0.15	0.55	70.5	200	0.65	26.44	0.02	0.84	0.33	
	70A	72A	0.65	19	19		65	1.09	99	3.60	1.15		0.00		0.00		0.00	0.00	0.65	1.09	0.36	1.51	119.0	250	0.25	29.73	0.05	0.61	0.31	
To Anemone Mews, Pipe 72A - 74A								1.09	99				0.00		0.00		0.00	0.00	1.09											
	16A	40A	0.07	1	1		4	0.07	4	3.76	0.05		0.00		0.00		0.00	0.00	0.07	0.07	0.02	0.07	10.0	200	0.65	26.44	0.00	0.84	0.17	
	40A	41A	0.36	10	10		34	0.43	38	3.67	0.45		0.00		0.00		0.00	0.00	0.36	0.43	0.14	0.59	58.0	250	0.65	47.94	0.01	0.98	0.33	
	41A	42A	0.63	20	20		68	1.06	106	3.59	1.23		0.00		0.00		0.00	0.00	0.63	1.06	0.35	1.58	108.5	250	0.25	29.73	0.05	0.61	0.32	
	42A	43A	0.31	7	7		24	1.37	130	3.57	1.50		0.00		0.00		0.00	0.00	0.31	1.37	0.45	1.96	64.5	250	0.25	29.73	0.07	0.61	0.34	
	43A	71A	0.50	14	14		48	1.87	178	3.53	2.04		0.00		0.00		0.00	0.00	0.50	1.87	0.62	2.66	98.0	250	0.25	29.73	0.09	0.61	0.37	
	71A	72A	0.38	11	11		38	2.25	216	3.51	2.46		0.00		0.00		0.00	0.00	0.38	2.25	0.74	3.20	76.5	250	0.25	29.73	0.11	0.61	0.39	
To Anemone Mews, Pipe 72A - 74A								2.25	216				0.00		0.00		0.00	0.00	2.25											
DESIGN PARAMETERS																														
Park Flow =	9300	L/ha/da	0.10764	I/s/Ha	</td																									

# SANITARY SEWER CALCULATION SHEET



Manning's n=0.013

LOCATION			RESIDENTIAL AREA AND POPULATION								COMM		INSTIT		PARK		C+H	INFILTRATION			PIPE												
STREET	FROM M.H.	TO M.H.	AREA (ha)	UNITS	UNITS Singles	UNITS Townhouse	POP.	CUMULATIVE		PEAK FACT.	PEAK FLOW (l/s)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	PEAK FLOW (l/s)	TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	DIST (m)	DIA (mm)	SLOPE (%)	CAP. (FULL) (l/s)	RATIO Q act/Q cap	VEL.					
								AREA (ha)	POP.																								
Deciduous Crescent																																	
	8A	9A	0.44	17		17	46	0.44	46	3.66	0.55		0.00		0.00		0.00		0.44	0.44	0.15	0.69	62.0	200	0.65	26.44	0.03	0.84	0.36				
		9A	11A	0.26	10		10	27	0.70	73	3.62	0.86		0.00		0.00		0.00	0.26	0.70	0.23	1.09	66.0	250	0.25	29.73	0.04	0.61	0.29				
To Conservancy Drive, Pipe 11A - 15A										0.70	73									0.70													
	12A	13A	0.09	2		2	6	0.09	6	3.75	0.07		0.00		0.00		0.00		0.09	0.09	0.03	0.10	7.5	200	0.65	26.44	0.00	0.84	0.20				
		13A	14A	0.38	15		15	41	0.47	47	3.66	0.56		0.00		0.00		0.00	0.38	0.47	0.16	0.71	66.0	250	0.25	29.73	0.02	0.61	0.25				
		14A	15A	0.30	11		11	30	0.77	77	3.62	0.90		0.00		0.00		0.00	0.30	0.77	0.25	1.16	69.5	250	0.25	29.73	0.04	0.61	0.29				
To Conservancy Drive, Pipe 15A - 18A										0.77	77									0.77													
Ephemeral Crescent																																	
	2A	3A	0.16	1	1		4	0.16	4	3.76	0.05		0.00		0.00		0.00		0.16	0.16	0.05	0.10	13.0	200	0.70	27.44	0.00	0.87	0.19				
			0.25	5	5		17	0.41	21				0.00		0.00				0.25	0.41													
	3A	4A	0.31	13		13	36	0.72	57	3.64	0.67		0.00		0.00		0.00	0.31	0.72	0.24	0.91	107.5	250	0.25	29.73	0.03	0.61	0.27					
		4A	15A	0.35	9		9	25	1.07	82	3.61	0.96		0.00		0.00		0.00	0.35	1.07	0.35	1.31	112.0	250	0.25	29.73	0.04	0.61	0.30				
To Conservancy Drive, Pipe 15A - 18A										1.07	82									1.07													
	5A	500A	0.14	6		6	17	0.14	17	3.71	0.20		0.00		0.00		0.00	0.14	0.14	0.05	0.25	21.0	200	0.65	26.44	0.01	0.84	0.26					
		500A	6A	0.45	22		22	60	0.59	77	3.62	0.90		0.00		0.00		0.00	0.45	0.59	0.19	1.10	78.5	250	0.25	29.73	0.04	0.61	0.29				
		6A	11A	0.48	21		21	57	1.07	134	3.57	1.55		0.00		0.00		0.00	0.48	1.07	0.35	1.90	104.5	250	0.25	29.73	0.06	0.61	0.34				
To Conservancy Drive, Pipe 11A - 15A										1.07	134									1.07													
Borrisokane Road																																	
	1002A	1001A	0.18	4		4	11	0.18	11	3.73	0.13		0.00		0.00		0.00	0.18	0.18	0.06	0.19	40.0	200	0.65	26.44	0.01	0.84	0.24					
		1001A	10A	0.40	12		12	33	0.58	44	3.66	0.52		0.00		0.00		0.00	0.40	0.58	0.19	0.71	100.0	250	0.25	29.73	0.02	0.61	0.25				
To Conservancy Drive, Pipe 10A - 11A										0.58	44									0.58													
	1004A	1003A	0.50	14		14	38	0.50	38	3.67	0.45		0.00		0.00		0.00	0.50	0.50	0.17	0.62	98.5	200	0.65	26.44	0.02	0.84	0.35					
		1003A	10A	0.41	13		13	36	0.91	74	3.62	0.87		0.00		0.00		0.00	0.41	0.91	0.30	1.17	100.0	250	0.25	29.73	0.04	0.61	0.29				
To Conservancy Drive, Pipe 10A - 11A										0.91	74									0.91													
Conservancy Drive								12.88																									
	PLUG	10A	36.45						3771	49.33	4953	2.80	44.93	13.70	17.91	0.00	3.47	4.05	9.36	53.62	71.29	23.53	77.81	20.5	525	0.10	136.00	0.57	0.63	0.65			
Contribution From Borrisokane Road, Pipe 1001A - 10A										0.58	44			0.00		0.00			0.58	71.87													
Contribution From Borrisokane Road, Pipe 1003A - 10A										0.91	74			0.00		0.00			0.91	72.78													
	10A	11A	0.15					0	50.97	5071	2.79	45.87		17.91	0.00	4.05	9.36	0.15	72.93	24.07	79.30	71.5	525	0.10	136.00	0.58	0.63	0.65					
Contribution From Ephemeral Crescent, Pipe 6A - 11A									1.07	134			0.00		0.00			1.07	74.00														
Contribution From Deciduous Crescent, Pipe 9A - 11A									0.70	73			0.00		0.00			0.70	74.70														
	11A	15A	0.30	6	6		21	53.04	5299	2.78	47.69		17.91	0.00	4.05	9.36	0.30	75.00	24.75	81.80	59.0	525	0.10	136.00	0.60	0.63	0.66						
Contribution From Deciduous Crescent, Pipe 14A - 15A									0.77	77			0.00		0.00			0.77	75.77														
Contribution From Ephemeral Crescent, Pipe 4A - 15A									1.07	82			0.00		0.00			1.07	76.84														
	15A	18A	0.12					0	55.00	5458	2.77	48.95		17.91	0.00	4.05	9.36	0.12	76.96	25.40	83.71	58.5	525	0.10	136.00	0.62	0.63	0.66					
Contribution From Les Emerson Drive (N), Pipe 17A - 18A									0.83	75			0.00		0.00			0.83	77.79														
Contribution From Park (Block 773), Pipe 210A - 18A									0.00	0.00			0.00		0.00			3.22	81.01														
	18A	23A	0.31	5	5		17	56.14	5550	2.76	49.68		17.91	0.00	4.05	9.36	0.31	81.32	26.84	85.88	76.5	525	0.10	136.00	0.63	0.63	0.66						
		23A	24A	0.49	11	11	38	56.63	5588	2.76	49.98		17.91	0.00	4.05	9.36	0.49	81.81	27.00	86.34	71.0	525	0.10	136.00	0.63	0.63	0.66						
		24A	47A	0.61	15	15	51	57.24	5639	2.76	50.38		17.91	0.00	4.05	9.36																	

# SANITARY SEWER CALCULATION SHEET



Manning's n=0.013

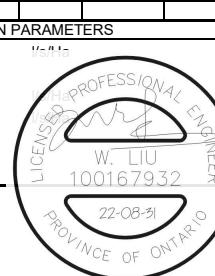
LOCATION			RESIDENTIAL AREA AND POPULATION								COMM		INSTIIT		PARK		C+H		INFILTRATION			PIPE								
STREET	FROM M.H.	TO M.H.	AREA (ha)	UNITS	UNITS Singles	UNITS Townhouse	POP.	CUMULATIVE		PEAK FACT.	PEAK FLOW (l/s)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	PEAK FLOW (l/s)	TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	DIST (m)	DIA (mm)	SLOPE (%)	CAP. (FULL) (l/s)	RATIO Q act/Q cap	VEL.		
								AREA (ha)	POP.																					
Contribution From Mineral Street, Pipe 39A - 47A								5.28	398				0.00	0.00	0.00	0.00	0.00	0.00	5.28	87.70										
Contribution From Mineral Street, Pipe 46A - 47A								1.45	137				0.00	0.00	0.00	0.00	0.00	0.00	1.45	89.15										
	47A	48A	0.56	14	14		48	64.53	6222	2.72	54.94		17.91	0.00	4.05	9.36	0.56	89.71	29.60	93.90	99.0	525	0.10	136.00	0.69	0.63	0.68			
	48A	75A	0.42	10	10		34	64.95	6256	2.72	55.20		17.91	0.00	4.05	9.36	0.42	90.13	29.74	94.30	76.5	525	0.10	136.00	0.69	0.63	0.68			
Contribution From Anemone Mews, Pipe 63A - 75A								1.30	104				0.00	0.00	0.00	0.00	0.00	0.00	1.30	91.43										
Contribution From Anemone Mews, Pipe 750A - 75A								5.89	565				0.00	0.00	0.00	0.00	0.00	0.00	5.89	97.32										
	75A	76A	0.31	7	7		24	72.45	6949	2.69	60.53		17.91	0.00	4.05	9.36	0.31	97.63	32.22	102.11	62.0	525	0.10	136.00	0.75	0.63	0.69			
	76A	77A	0.39	11	11		38	72.84	6987	2.69	60.82		17.91	0.00	4.05	9.36	0.39	98.02	32.35	102.52	60.0	525	0.10	136.00	0.75	0.63	0.69			
	77A	92A	0.33	9	9		31	73.17	7018	2.68	61.05		17.91	0.00	4.05	9.36	0.33	98.35	32.46	102.87	53.0	525	0.10	136.00	0.76	0.63	0.69			
Contribution From Ecology Lane, Pipe 91A - 92A								6.96	580				0.00	0.00	0.00	0.00	0.00	0.00	6.96	105.31										
	92A	93A	0.51	12	12		41	80.64	7639	2.66	65.75		17.91	0.00	4.05	9.36	0.51	105.82	34.92	110.03	90.5	525	0.10	136.00	0.81	0.63	0.70			
To Canoe Street, Pipe 119A - 120A								81.01	7660				17.91	0.00	4.57			106.71												
<b>Meander Way</b>																														
	84A	85A	0.50	13	13		45	0.50	45	3.66	0.53		0.00	0.00	0.00	0.00	0.00	0.00	0.50	0.50	0.17	0.70	92.5	200	0.65	26.44	0.03	0.84	0.36	
To Sapling Grove, Pipe 85A - 88A								0.50	45				0.00	0.00	0.00	0.00	0.00	0.00												
	84A	86A	0.16	1	1		4	0.16	4	3.76	0.05		0.00	0.00	0.00	0.00	0.00	0.00	0.16	0.16	0.05	0.10	13.0	200	0.65	26.44	0.00	0.84	0.20	
	86A	87A	0.22	4	4		14	0.38	18	3.71	0.22		0.00	0.00	0.00	0.00	0.00	0.00	0.22	0.38	0.13	0.34	50.5	250	0.65	47.94	0.01	0.98	0.28	
	87A	114A	0.23	5	5		17	0.61	35	3.67	0.42		0.00	0.00	0.00	0.00	0.00	0.00	0.23	0.61	0.20	0.62	58.0	250	0.25	29.73	0.02	0.61	0.24	
	114A	115A	0.07	1	1		4	0.68	39	3.67	0.46		0.00	0.00	0.00	0.00	0.00	0.00	0.07	0.68	0.22	0.69	10.0	250	0.25	29.73	0.02	0.61	0.25	
	115A	116A	0.63	17	17		58	1.31	97	3.60	1.13		0.00	0.00	0.00	0.00	0.00	0.00	0.63	1.31	0.43	1.56	110.5	250	0.25	29.73	0.05	0.61	0.32	
To Peninsula Road, Pipe 116A - 117A								1.31	97				0.00	0.00	0.00	0.00	0.00	0.00												
<b>Peninsula Road</b>																														
	89A	63A	0.17	4	4		14	0.17	14	3.72	0.17		0.00	0.00	0.00	0.00	0.00	0.00	0.17	0.17	0.06	0.22	41.0	200	0.65	26.44	0.01	0.84	0.26	
To Anemone Mews, Pipe 63A - 75A								0.17	14				0.00	0.00	0.00	0.00	0.00	0.00												
	380A	38A	0.45	8	8		28	0.45	28	3.69	0.33		0.00	0.00	0.00	0.00	0.00	0.00	0.45	0.45	0.15	0.48	57.0	200	0.65	26.44	0.02	0.84	0.32	
	38A	39A	0.60	16	16		55	1.05	83	3.61	0.97		0.00	0.00	0.00	0.00	0.00	0.00	0.60	1.05	0.35	1.32	108.5	250	0.25	29.73	0.04	0.61	0.30	
To Mineral Street, Pipe 39A - 47A								1.05	83				0.00	0.00	0.00	0.00	0.00	0.00												
	620A	62A	0.50	13	13		45	0.50	45	3.66	0.53		0.00	0.00	0.00	0.00	0.00	0.00	0.50	0.50	0.17	0.70	83.0	200	0.65	26.44	0.03	0.84	0.36	
	62A	63A	0.45	13	13		45	0.95	90	3.60	1.05		0.00	0.00	0.00	0.00	0.00	0.00	0.45	0.95	0.31	1.36	82.0	250	0.25	29.73	0.05	0.61	0.31	
To Anemone Mews, Pipe 63A - 75A								0.95	90				0.00	0.00	0.00	0.00	0.00	0.00												
	89A	90A	0.41	13	13		45	0.41	45	3.66	0.53		0.00	0.00	0.00	0.00	0.00	0.00	0.41	0.41	0.14	0.67	67.0	200	0.65	26.44	0.03	0.84	0.35	
	90A	91A	0.37	10	10		34	0.78	79	3.62	0.93		0.00	0.00	0.00	0.00	0.00	0.00	0.37	0.78	0.26	1.18	68.5	250	0.75	51.50	0.02	1.05	0.42	
To Ecology Lane, Pipe 91A - 92A								0.78	79				0.00	0.00	0.00	0.00	0.00	0.00												
	91A	116A	0.18	4	4		14	0.18	14	3.72	0.17		0.00	0.00	0.00	0.00	0.00	0.00	0.18	0.18	0.06	0.23	58.5	200	0.65	26.44	0.01	0.84	0.26	
Contribution From Meander Way, Pipe 115A - 116A								1.31	97				0.00	0.00	0.00	0.00	0.00	0.00												
	116A	117A	0.23	6	6		21	1.72	132	3.57	1.53		0.00	0.00	0.00	0.00	0.00	0.00	0.23	1.72	0.57	2.09	58.5	250	0.25	29.73	0.07	0.61	0.34	
Contribution From Elation Heights, Pipe 109A - 117A								0.74	55				0.00	0.00	0.00	0.00	0.00	0.00												
	117A	118A	0.18	3	3		11	2.64	198	3.52	2.26		0.00	0.00	0.00	0.00	0.00	0.00	0.18	2.64	0.87	3.13	59.0	250	0.25	29.73	0.11	0.61	0.39	

# SANITARY SEWER CALCULATION SHEET



Manning's n=0.013

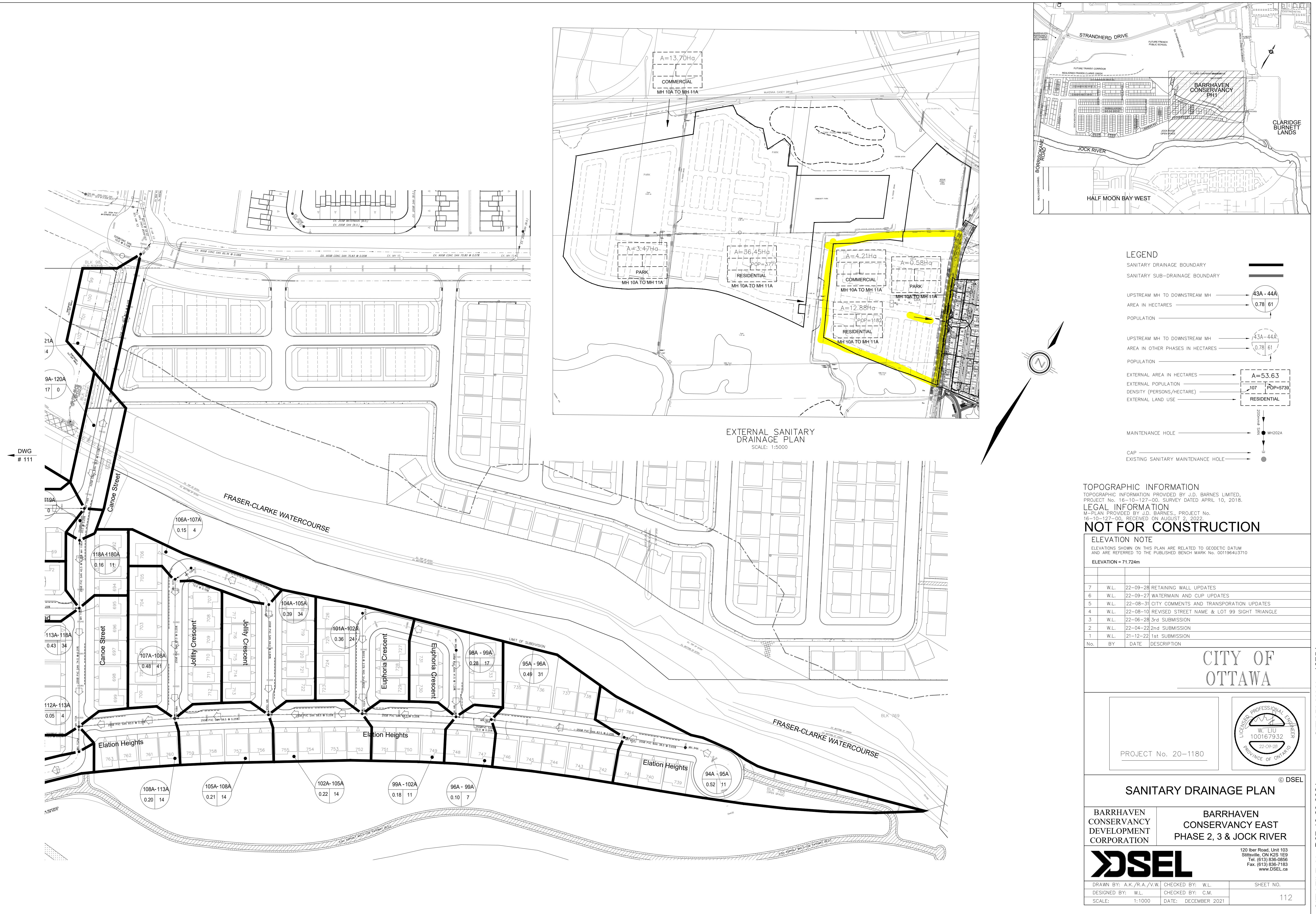
LOCATION			RESIDENTIAL AREA AND POPULATION								COMM		INSTIIT		PARK		C+H		INFILTRATION			PIPE							
STREET	FROM M.H.	TO M.H.	AREA (ha)	UNITS Singles	UNITS Townhouse	POP.	CUMULATIVE		PEAK FACT.	PEAK FLOW (l/s)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	PEAK FLOW (l/s)	TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	DIST (m)	DIA (mm)	SLOPE (%)	CAP. (FULL) (l/s)	RATIO Q act/Q cap	VEL.		
							AREA (ha)	POP.																					
Elation Heights																													
	112A	113A	0.05	1	1	4	0.05	4	3.76	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.05	0.02	0.07	15.5	200	0.65	26.44	0.00	0.84	0.17		
To Canoe Street, Pipe 113A - 118A							0.05	4			0.00	0.00	0.00	0.00	0.00	0.00	0.05												
	110A	109A	0.16	1	1	4	0.16	4	3.76	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.16	0.16	0.05	0.10	13.5	200	0.65	26.44	0.00	0.84	0.20		
	109A	117A	0.58	15	15	51	0.74	55	3.64	0.65	0.00	0.00	0.00	0.00	0.00	0.00	0.58	0.74	0.24	0.89	103.0	250	0.25	29.73	0.03	0.61	0.27		
To Peninsula Road, Pipe 117A - 118A							0.74	55			0.00	0.00	0.00	0.00	0.00	0.00	0.74												
Jollity Crescent																													
	104A	105A	0.39	10	10	34	0.39	34	3.68	0.41	0.00	0.00	0.00	0.00	0.00	0.00	0.39	0.39	0.13	0.53	69.0	200	0.80	29.34	0.02	0.93	0.35		
To Canoe Street, Pipe 105A - 108A							0.39	34			0.00	0.00	0.00	0.00	0.00	0.00	0.39												
	106A	107A	0.15	1	1	4	0.15	4	3.76	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.15	0.15	0.05	0.10	12.0	200	0.70	27.44	0.00	0.87	0.19		
	107A	108A	0.48	12	12	41	0.63	45	3.66	0.53	0.00	0.00	0.00	0.00	0.00	0.00	0.48	0.63	0.21	0.74	87.0	250	0.25	29.73	0.02	0.61	0.25		
To Canoe Street, Pipe 108A - 113A							0.63	45			0.00	0.00	0.00	0.00	0.00	0.00	0.63												
Euphoria Crescent																													
	101A	102A	0.36	7	7	24	0.36	24	3.70	0.29	0.00	0.00	0.00	0.00	0.00	0.00	0.36	0.36	0.12	0.41	62.5	250	0.65	47.94	0.01	0.98	0.30		
To Canoe Street, Pipe 102A - 105A							0.36	24			0.00	0.00	0.00	0.00	0.00	0.00	0.36												
	98A	99A	0.28	5	5	17	0.28	17	3.71	0.20	0.00	0.00	0.00	0.00	0.00	0.00	0.28	0.28	0.09	0.30	41.5	200	1.20	35.93	0.01	1.14	0.33		
Canoe Street																													
	94A	95A	0.52	3	3	11	0.52	11	3.73	0.13	0.00	0.00	0.00	0.00	0.00	0.00	0.52	0.52	0.17	0.30	38.5	200	0.65	26.44	0.01	0.84	0.28		
	95A	96A	0.49	9	9	31	1.01	42	3.66	0.50	0.00	0.00	0.00	0.00	0.00	0.00	0.49	1.01	0.33	0.83	83.5	250	0.25	29.73	0.03	0.61	0.26		
Contribution From Euphoria Crescent, Pipe 98A - 99A							0.28	17			0.00	0.00	0.00	0.00	0.00	0.00	0.28	1.39											
	99A	102A	0.18	3	3	11	1.57	77	3.62	0.90	0.00	0.00	0.00	0.00	0.00	0.00	0.18	1.57	0.52	1.42	58.5	250	0.25	29.73	0.05	0.61	0.31		
Contribution From Euphoria Crescent, Pipe 101A - 102A							0.36	24			0.00	0.00	0.00	0.00	0.00	0.00	0.36	1.93											
	102A	105A	0.22	4	4	14	2.15	115	3.58	1.33	0.00	0.00	0.00	0.00	0.00	0.00	0.22	2.15	0.71	2.04	58.5	250	0.25	29.73	0.07	0.61	0.34		
Contribution From Jollity Crescent, Pipe 104A - 105A							0.39	34			0.00	0.00	0.00	0.00	0.00	0.00	0.39	2.54											
	105A	108A	0.21	4	4	14	2.75	163	3.54	1.87	0.00	0.00	0.00	0.00	0.00	0.00	0.21	2.75	0.91	2.78	58.5	250	0.25	29.73	0.09	0.61	0.38		
Contribution From Jollity Crescent, Pipe 107A - 108A							0.63	45			0.00	0.00	0.00	0.00	0.00	0.00	0.63	3.38											
	108A	113A	0.20	4	4	14	3.58	222	3.50	2.52	0.00	0.00	0.00	0.00	0.00	0.00	0.20	3.58	1.18	3.70	60.0	250	0.25	29.73	0.12	0.61	0.41		
Contribution From Elation Heights, Pipe 112A - 113A							0.05	4			0.00	0.00	0.00	0.00	0.00	0.00	0.05	3.63											
	113A	118A	0.43	10	10	34	4.06	260	3.48	2.94	0.00	0.00	0.00	0.00	0.00	0.00	0.43	4.06	1.34	4.27	74.0	250	0.25	29.73	0.14	0.61	0.43		
Contribution From Peninsula Road, Pipe 117A - 118A							2.64	198			0.00	0.00	0.00	0.00	0.00	0.00	2.64	6.70											
	118A	1180A	0.16	3	3	11	6.86	469	3.39	5.15	0.00	0.00	0.00	0.00	0.00	0.00	0.16	6.86	2.26	7.42	42.5	250	0.25	29.73	0.25	0.61	0.50		
	1180A	119A	0.03			0	6.89	469	3.39	5.15	0.00	0.00	0.00	0.00	0.00	0.00	0.03	6.89	2.27	7.43	20.0	250	0.25	29.73	0.25	0.61	0.50		
Contribution From Conservancy Drive, Pipe 93A - 119A							81.01	7660			17.91	0.00	4.57		106.71	113.60													
	119A	120A	0.17			0	88.07	8129	2.63	69.41	17.91	0.00	4.57	9.44	0.17	113.77	37.54	116.40	75.0	525	0.10	136.00	0.86	0.63	0.71				
	120A	121A	0.21	4	4	14	88.28	8143	2.63	69.51	17.91	0.00	4.57	9.44	0.21	113.98	37.61	116.57	87.5	525	0.10	136.00	0.86	0.63	0.71				
	121A	Ex. MH 8					88.28	8143	2.63	69.51	17.91	0.00	4.57	9.44	0.00	113.98	37.61	116.57	10.0	525	0.10	136.00	0.86	0.63	0.71				
Park (Block 773)																													
	210A	18A					0.00				0.00	0.00	3	3.22	0.52	3.22	3.22	1.06	1.58	11.5	200	0.65	26.44	0.06	0.84	0.46			
To Conservancy Drive, Pipe 18A - 23A							0.00	0			0.00	0.00	3	3.22		3.22	3.22												



INDUSTRIAL PEAK FLOW = as per MOE Graph  
 Extraneous Flow = 0.330 L/s/ha  
 Minimum Velocity = 0.600 m/s  
 Manning's n = 0.013 (Conc) 0.013 (Pvc)  
 Industrial Flow = 0.40509  
 Max Res. Peak Factor = 4.00  
 Commercial/Inst./Park Peak Factor = 1.50  
 Institutional = 0.32 l/s/Ha

Dwg. Reference:  
 Sanitary Drainage Plan, Dwgs. No. 110-112

</div



## **APPENDIX D**

## **STORMWATER**

# Conservation Partners Partenaires en conservation



May 31, 2020

City of Ottawa  
110 Laurier Avenue,  
Ottawa, ON K1P 1J1

Attention: Doug James

Subject: Barrhaven Conservancy Development Corporation  
Status of As-Built Grading  
Related: RVCA Permit # RV5-4419 and RV5-1718)  
Vacant land on the north side of the Jock River generally bounded by Highway 416 and the Fraser Clarke Creek, City of Ottawa

Dear Mr. James:

The RVCA has reviewed information recently submitted by David Schaeffer Engineering Ltd. including as-built grades in support of works approved by the Rideau Valley Conservation Authority under Section 28 of the Conservation Authorities Act (Permit File Number: RV5-4419 and RV5-1718). The RVCA offers the following comments related to future development proposed for the area within the scope of approved the permits.

The subject lands as identified as part of Lots 11, 12, 13, 14, 15 former geographic Township of Nepean, Concessions 3 & 4, now in the City of Ottawa have been addressed through the general placement of fill and the formal construction of a berm around the perimeter of four blocks within the subject lands. The site specific elevations of the berm have been reviewed by the RVCA and are generally accepted as being appropriate as removing these lands from the floodplain in accordance with the aforementioned approved permits.

The detailed grading plans submitted by David Schaeffer Engineering Ltd. titled As Constructed plan of Berms and Cut Areas – Barrhaven Conservancy”, dated May 27, 2020, prepared by Adam Fobert, P.Eng. of DSEL, DSEL File Number 16891 using the following resources:

- Orthoimagery Survey, dated April 20, 2020, acquired and processed by First Base Solutions a division of JD Barnes Ltd and certified by Chris Fox, O.L.S., A.L.S., P. Eng. of JD Barnes Ltd, file reference number 2037OTTA0001;
- Topographic Detail of Part of Lot 13, 14,&15 Concession 3&4, dated May 6, 2020, certified by Chris Fox, O.L.S., A.L.S., P. Eng. of JD Barnes Ltd, file reference number 16-10-127-00;



- Contractor as-built collected by the Tomlinson Group of Companies of Phase 1 dated May 15, 2020, reviewed by Jeremy Chouindard, EIT and certified by Stephen Pichette, P.Eng. of DSEL

The above information indicates that land within the berm have generally been raised to exceed the flood elevation cross sections throughout the project area. However, it is noted that as this is considered an active construction site the presence of lower areas to manage construction, on-site erosion and sediment control show lower elevations. These areas will be addressed through the construction process, as sufficient material is presently stockpiled for this purpose to ensure. For the purposes of the floodplain, these areas are considered removed by virtue of the berm.

### **Conclusion:**

The grade modifications, including construction of the berm and filling behind the berm, as documented in the above noted "as constructed" plans, have been completed in accordance with the plans approved by the RVCA under permits RV5-4419 and RV5-1718.

Please feel free to contact our office with any questions or comments you may have.

Respectfully,

Terry Davidson, P.Eng  
Director of Engineering and Regulations  
Rideau Valley Conservation Authority  
613-692-3571 x1107  
[terry.davidson@rvca.ca](mailto:terry.davidson@rvca.ca)

attach:      Technical memorandum by Evelyn Liu, M.Asc., P.Eng. Water Resources  
Engineer, RVCA dated May 29, 2020



# STORM SEWER CALCULATION SHEET (RATIONAL METHOD)

Local Roads Return Frequency = 2 years  
 Collector Roads Return Frequency = 5 years  
 Arterial Roads Return Frequency = 10 years

Manning 0.013



Location	From Node	To Node	AREA (Ha)												FLOW							SEWER DATA											
			2 YEAR				5 YEAR				10 YEAR				100 YEAR				Time of Conc.	Intensity 2 Year (mm/h)	Intensity 5 Year (mm/h)	Intensity 10 Year (mm/h)	Intensity 100 Year (mm/h)	Peak Flow Q (l/s)	DIA. (mm)	DIA. (mm)	Type	Slope	Length	Capacity (m)	Velocity (l/s)	Time of (m/s)	Ratio Q/Q full
			Area (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	Area (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	Area (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	Area (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	(min)	(mm/h)	(mm/h)	(mm/h)	(mm/h)	(actual)	(nominal)	(%)	(m)	(l/s)	(m/s)	Low (min)	Q/Q full		
Centerline7 - 07																																	
	501	502	0.32	0.67	0.60	0.60			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	46	375	375	PVC	0.30	118.0	96.0323	0.8695	2.2619	0.477
	502	505	0.02	0.67	0.04	0.63			0.00	0.00			0.00	0.00			0.00	0.00	12.26	69.09	93.59	109.66	160.23	44	450	450	CONC	0.25	31.5	142.5531	0.8963	0.5857	0.307
To Centerline15 - 15, Pipe 505 - 507						0.63																											
Centerline4 - 04																																	
Contribution From Centerline15 - 15, Pipe 505 - 507			0.63						0.69				0.00				0.00			13.24													
Contribution From Centerline15 - 15, Pipe 506 - 507			0.00						0.00				0.85				0.00			11.43													
	507	513	0.22	0.80	0.49	1.12			0.00	0.69			0.00	0.85			0.00	0.00	13.24	66.26	89.71	105.08	153.51	261	750	750	CONC	0.11	114.5	369.2322	0.8358	2.2833	0.707
To Centerline11 - 11, Pipe 513 - 514			0.29	0.67	0.54	1.66			0.00	0.69			0.85				0.00			15.52													
Centerline2 - 02																																	
	511	512	0.42	0.80	0.93	0.93			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	72	450	450	CONC	0.20	99.5	127.5033	0.8017	2.0685	0.563
To Centerline11 - 11, Pipe 512 - 513			0.93						0.00				0.00				0.00			12.07													
Centerline11 - 11																																	
	508	509	0.20	0.80	0.44	0.44			0.00	0.00			0.00	0.00			0.00	0.00															
	509	510	0.29	0.67	0.54	0.98			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	76	450	450	CONC	0.20	90.5	127.5033	0.8017	1.8814	0.593
	509	510	0.12	0.67	0.22	1.21			0.00	0.00			0.00	0.00			0.00	0.00	11.88	70.26	95.20	111.56	163.01	85	450	450	CONC	0.20	10.5	127.5033	0.8017	0.2183	0.666
	510	512	0.16	0.67	0.30	1.51			0.00	0.00			0.00	0.00			0.00	0.00	12.10	69.58	94.27	110.46	161.40	105	525	525	CONC	0.20	39.0	192.3297	0.8885	0.7316	0.545
Contribution From Centerline2 - 02, Pipe 511 - 512			0.93						0.00				0.00				0.00			12.07													
	512	513	0.19	0.67	0.35	2.79			0.00	0.00			0.00	0.00			0.00	0.00	12.83	67.41	91.29	106.95	156.24	188	675	675	CONC	0.15	47.5	325.5584	0.9098	0.8702	0.579
Contribution From Centerline4 - 04, Pipe 507 - 513			1.66						0.69				0.85				0.00			15.52													
	513	514	0.21	0.67	0.39	4.85			0.00	0.69			0.00	0.85			0.00	0.00	15.52	60.56	81.90	95.90	140.03	431	900	900	CONC	0.11	51.0	600.4123	0.9438	0.9006	0.718
	514	515	0.03	0.67	0.06	4.90			0.00	0.69			0.00	0.85			0.00	0.00	16.43	58.60	79.22	92.75	135.41	421	900	900	CONC	0.11	8.5	600.4123	0.9438	0.1501	0.700
	515	516	0.09	0.67	0.17	5.07			0.00	0.69			0.00	0.85			0.00	0.00	16.58	58.28	78.79	92.25	134.67	428	900	900	CONC	0.11	56.5	600.4123	0.9438	0.9978	0.713
To Centerline1 - 01, Pipe 516 - 521			5.07						0.69				0.85				0.00			17.57													
Centerline3 - 03																																	
Contribution From Centerline1 - 01, Pipe 516 - 521			5.07						1.15				0.85				0.00			18.60													
Contribution From Centerline1 - 01, Pipe 519 - 521			0.00						1.40				0.00				0.00			12.21													
	521	524	0.55	0.67	1.02	6.10			0.00	2.55			0.00	0.85			0.00	0.00	18.60	54.40	73.49	86.01	125.53	592	900	900	CONC	0.17	110.0	746.4104	1.1733	1.5626	0.793
To Centerline10 - 10, Pipe 524 - 525			6.10						2.55				0.85				0.00			20.16													
Centerline10 - 10																																	
	520	517	0.62	0.67	1.15	1.15			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	89	450	450	CONC	0.20	104.5	127.5033	0.8017	2.1725	0.696
	517	518	0.17	0.67	0.32	1.47			0.00	0.00			0.00	0.00			0.00	0.00	12.17	69.36	93.97	110.10	160.87	102	450	450	CONC	0.25	10.5	142.5531	0.8963	0.1952	0.716
	518	525	0.18	0.67	0.34	1.81			0.00	0.00			0.00	0.00			0.00	0.00	12.37	68.77	93.15	109.14	159.47	124	525	525	CONC	0.20	48.0	192.3297	0.8885	0.9004	0.646
To Centerline5 - 05, Pipe 525 - HW10			1.81						0.00				0.00				0.00			13.27													
	522	523	0.65	0.67	1.21	1.21			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	93	450	450	CONC	0.20	39.0	127.5033	0.8017	0.8108	0.729
	523	524	0.21	0.67	0.39	1.60			0.00	0.00			0.00	0.00			0.00	0.00	10.81	73.83	100.10	117.32	171.47	118	525	525	CONC	0.20	49.0	192.3297	0.8885	0.9192	0.615
Contribution From Centerline3 - 03, Pipe 521 - 524			6.10						2.55				0.85				0.00			20.16													
	524	525	0.00	7.70	</td																												

## STORM SEWER CALCULATION SHEET (RATIONAL METHOD)

Local Roads Return Frequency = 2 years  
Collector Roads Return Frequency = 5 years  
Arterial Roads Return Frequency = 10 years



Manning 6

#### **Definitions:**

$\Omega = 2.78 \text{ AIR}$  where

$Q = 2.78 \text{ AIR}$ , where

**Q = Peak Flow in L**

A = Areas in hectares (ha)

I = Rainfall Intensi

R = Runoff Coefficient

Nao

- Notes:

  - 1) Ottawa Rainfall-Intensity Curve
  - 2) Min. Velocity = 0.80 m/s

signed:

## PROJECT:

Barrhaven Conservancy East Phase 5

A.S.

#### **LOCATION**

City of Ottawa

W.L./V.W.

1

Date: \_\_\_\_\_ Sheet No. \_\_\_\_\_

# STORM SEWER CALCULATION SHEET (RATIONAL METHOD)

Local Roads Return Frequency = 2 years  
 Collector Roads Return Frequency = 5 years  
 Arterial Roads Return Frequency = 10 years

Manning 0.013



Location	LOCATION		AREA (Ha)												FLOW							SEWER DATA								
	From Node	To Node	AREA (Ha)	R	2 YEAR		5 YEAR		10 YEAR		100 YEAR		Time of Conc. (min)	Intensity 2 Year (mm/h)	Intensity 5 Year (mm/h)	Intensity 10 Year (mm/h)	Intensity 100 Year (mm/h)	Peak Flow Q (l/s)	DIA. (mm)	DIA. (mm)	Type	Slope	Length	Capacity (m)	Velocity (l/s)	Time of (m/s)	Ratio (Q/Q full)			
					Indiv. 2.78 AC	Accum. 2.78 AC							(actual)	(nominal)	(%)	(m/s)	(m)	(l/s)	(m)											
Centerline14 - 14																														
Contribution From Centerline15 - 15, Pipe 526 - 529			2.07																											
Contribution From Centerline15 - 15, Pipe 527 - 529			0.00																											
529 530 0.52 0.80 1.16 3.22			0.00	0.00			0.00	1.16			0.00	0.00	10.95	73.33	99.42	116.52	170.30	371	825	825	CONC	0.11	26.5	476.0801	0.8906	0.4959	0.780			
530 534			0.00	3.22			0.00	0.00			0.00	1.16		0.00	0.00	11.45	71.66	97.12	113.81	166.33	363	825	825	CONC	0.11	117.0	476.0801	0.8906	2.1895	0.762
Contribution From Centerline6 - 06, Pipe 533 - 534			2.67																											
534 537 0.11 0.80 0.24 6.14			0.00	0.00			0.00	1.16			0.00	0.00	13.64	65.18	88.24	103.36	150.97	520	900	900	CONC	0.15	48.5	701.1305	1.1021	0.7334	0.742			
To Centerline13 - 13, Pipe 537 - 538			6.14				0.00				1.16			0.00	0.00	14.37														
Centerline13 - 13																														
Contribution From Centerline14 - 14, Pipe 534 - 537			6.14				0.00				1.16			0.00	0.00	14.37														
Contribution From Centerline1 - 01, Pipe 536 - 537			0.00				0.87				0.00			0.00	0.00	12.10														
537 538 0.28 0.67 0.52 6.66			0.00	6.14	0.06	0.67	0.11	0.98			0.00	1.16		0.00	0.00															
538 543 0.25 0.67 0.47 7.13			0.00	0.98			0.00	1.16			0.00	0.00	14.37	63.29	85.65	100.31	146.50	622	975	975	CONC	0.15	83.0	867.9562	1.1625	1.1899	0.716			
Contribution From Centerline8 - 08, Pipe 542 - 543			1.92				0.00				0.00			0.00	0.00	15.56	60.48	81.79	95.77	139.84	622	975	975	CONC	0.15	69.0	867.9562	1.1625	0.9892	0.717
543 528 0.05 0.67 0.09 9.14			0.00	0.98			0.00	1.16			0.00	0.00	16.55	58.34	78.86	92.33	134.80	717	1050	1050	CONC	0.11	29.0	905.6791	1.0459	0.4621	0.792			
Contribution From Centerline12 - 12, Pipe 548 - 528			3.24				0.09				0.00			0.00	0.00	17.17														
528 HW9			0.00	12.38			0.00	1.07			0.00	1.16		0.00	0.00	17.17	57.08	77.15	90.32	131.84	894	1050	1050	CONC	0.20	4.5	1221.2174	1.4103	0.0532	0.732
Definitions:																														
Q = 2.78 AIR, where																									Designed: A.S.					
Q = Peak Flow in Litres per second (L/s)																									PROJECT: Barrhaven Conservancy East Phase 5					
A = Areas in hectares (ha)																									Checked: W.L./V.W.					
I = Rainfall Intensity (mm/h)																									LOCATION: City of Ottawa					
R = Runoff Coefficient																									Dwg. Reference: File Ref: Date: Sheet No.					
																									01 Dec 2022 SHEET 3 OF 3					





**CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION  
BASED ON THE RATIONAL RAINFALL METHOD  
BASED ON A FINE PARTICLE SIZE DISTRIBUTION**



**Project Name:** 891 Conservancy East

**Location:** Ottawa, ON

**OGS #:** 9

**Engineer:** DSEL

**Contact:** K. Murphy

**Report Date:** 20-Oct-22

**Area** 7.21 ha  
**Weighted C** 0.72  
**CDS Model** 4045 (OFFLINE)

**Rainfall Station #** 215  
**Particle Size Distribution** FINE  
**CDS Treatment Capacity** 212 l/s

<u>Rainfall Intensity<sup>1</sup> (mm/hr)</u>	<u>Percent Rainfall Volume<sup>1</sup></u>	<u>Cumulative Rainfall Volume</u>	<u>Total Flowrate (l/s)</u>	<u>Treated Flowrate (l/s)</u>	<u>Operating Rate (%)</u>	<u>Removal Efficiency (%)</u>	<u>Incremental Removal (%)</u>
1.0	10.6%	19.8%	14.4	14.4	6.8	96.9	10.3
1.5	9.9%	29.7%	21.6	21.6	10.2	95.9	9.5
2.0	8.4%	38.1%	28.9	28.9	13.6	95.0	8.0
2.5	7.7%	45.8%	36.1	36.1	17.0	94.0	7.2
3.0	5.9%	51.7%	43.3	43.3	20.4	93.0	5.5
3.5	4.4%	56.1%	50.5	50.5	23.8	92.0	4.0
4.0	4.7%	60.7%	57.7	57.7	27.2	91.1	4.2
4.5	3.3%	64.0%	64.9	64.9	30.6	90.1	3.0
5.0	3.0%	67.1%	72.2	72.2	34.0	89.1	2.7
6.0	5.4%	72.4%	86.6	86.6	40.8	87.2	4.7
7.0	4.4%	76.8%	101.0	101.0	47.6	85.2	3.7
8.0	3.5%	80.3%	115.5	115.5	54.4	83.3	2.9
9.0	2.8%	83.2%	129.9	129.9	61.2	81.3	2.3
10.0	2.2%	85.3%	144.3	144.3	67.9	79.4	1.7
15.0	7.0%	92.3%	216.5	212.4	100.0	68.9	4.8
20.0	4.5%	96.9%	288.6	212.4	100.0	51.7	2.3
25.0	1.4%	98.3%	360.8	212.4	100.0	41.3	0.6
30.0	0.7%	99.0%	432.9	212.4	100.0	34.4	0.2
35.0	0.5%	99.5%	505.1	212.4	100.0	29.5	0.1
40.0	0.5%	100.0%	577.3	212.4	100.0	25.8	0.1
						87.1	

$$\begin{aligned} \text{Removal Efficiency Adjustment}^2 &= 6.5\% \\ \text{Predicted Net Annual Load Removal Efficiency} &= 80.6\% \\ \text{Predicted Annual Rainfall Treated} &= 97.1\% \end{aligned}$$

1 - Based on 42 years of hourly rainfall data from Canadian Station 6105976, Ottawa ON

2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.

3 - CDS Efficiency based on testing conducted at the University of Central Florida

4 - CDS design flowrate and scaling based on standard manufacturer model & product specifications



**CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION  
BASED ON THE RATIONAL RAINFALL METHOD  
BASED ON A FINE PARTICLE SIZE DISTRIBUTION**



**Project Name:** 891 Conservancy East

**Location:** Ottawa, ON

**OGS #:** 10

**Engineer:** DSEL

**Contact:** K. Murphy

**Report Date:** 20-Oct-22

**Area** 6.61 ha  
**Weighted C** 0.70  
**CDS Model** 4045 (OFFLINE)

**Rainfall Station #** 215  
**Particle Size Distribution** FINE  
**CDS Treatment Capacity** 212 l/s

<u>Rainfall Intensity<sup>1</sup> (mm/hr)</u>	<u>Percent Rainfall Volume<sup>1</sup></u>	<u>Cumulative Rainfall Volume</u>	<u>Total Flowrate (l/s)</u>	<u>Treated Flowrate (l/s)</u>	<u>Operating Rate (%)</u>	<u>Removal Efficiency (%)</u>	<u>Incremental Removal (%)</u>
1.0	10.6%	19.8%	12.9	12.9	6.1	97.1	10.3
1.5	9.9%	29.7%	19.3	19.3	9.1	96.3	9.5
2.0	8.4%	38.1%	25.7	25.7	12.1	95.4	8.0
2.5	7.7%	45.8%	32.2	32.2	15.1	94.5	7.3
3.0	5.9%	51.7%	38.6	38.6	18.2	93.6	5.6
3.5	4.4%	56.1%	45.0	45.0	21.2	92.8	4.0
4.0	4.7%	60.7%	51.5	51.5	24.2	91.9	4.3
4.5	3.3%	64.0%	57.9	57.9	27.3	91.0	3.0
5.0	3.0%	67.1%	64.3	64.3	30.3	90.2	2.7
6.0	5.4%	72.4%	77.2	77.2	36.3	88.4	4.8
7.0	4.4%	76.8%	90.0	90.0	42.4	86.7	3.8
8.0	3.5%	80.3%	102.9	102.9	48.4	85.0	3.0
9.0	2.8%	83.2%	115.8	115.8	54.5	83.2	2.3
10.0	2.2%	85.3%	128.6	128.6	60.6	81.5	1.8
15.0	7.0%	92.3%	192.9	192.9	90.8	72.8	5.1
20.0	4.5%	96.9%	257.3	212.4	100.0	58.0	2.6
25.0	1.4%	98.3%	321.6	212.4	100.0	46.4	0.7
30.0	0.7%	99.0%	385.9	212.4	100.0	38.6	0.3
35.0	0.5%	99.5%	450.2	212.4	100.0	33.1	0.2
40.0	0.5%	100.0%	514.5	212.4	100.0	29.0	0.2
						88.4	

Removal Efficiency Adjustment<sup>2</sup> = 6.5%

**Predicted Net Annual Load Removal Efficiency = 81.9%**

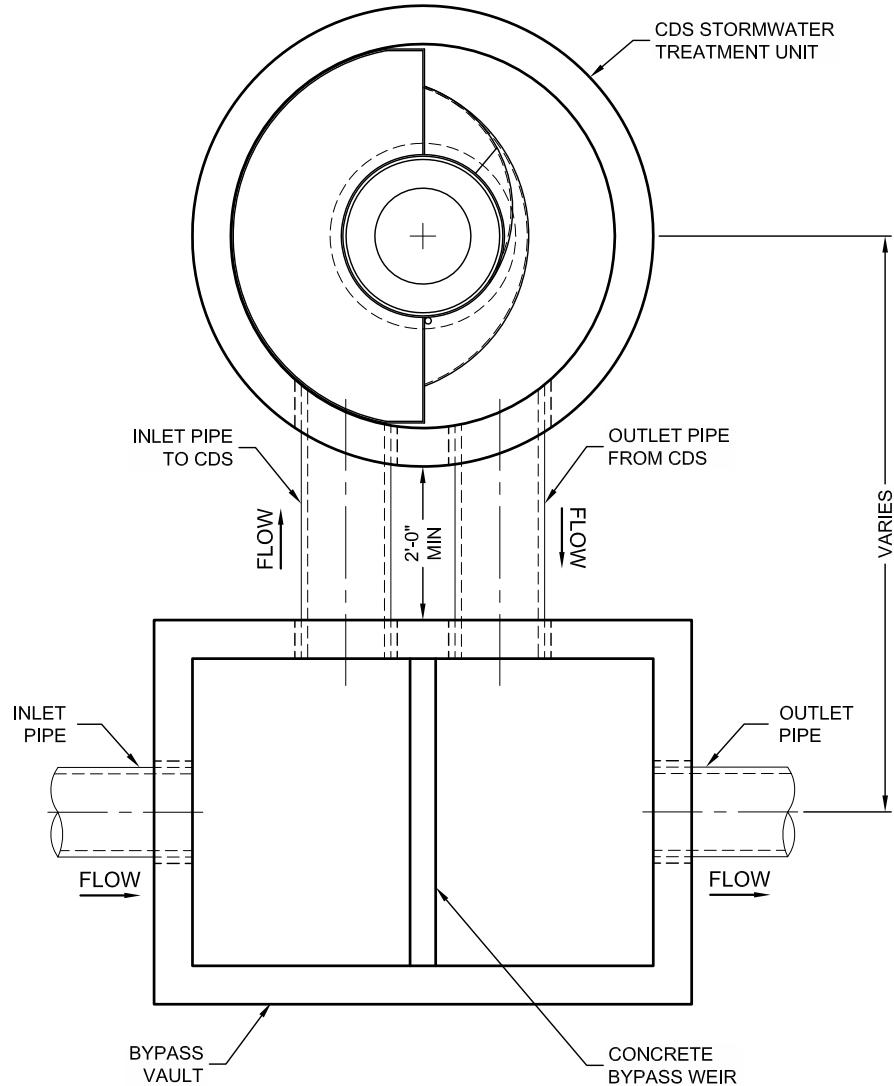
**Predicted Annual Rainfall Treated = 97.8%**

1 - Based on 42 years of hourly rainfall data from Canadian Station 6105976, Ottawa ON

2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.

3 - CDS Efficiency based on testing conducted at the University of Central Florida

4 - CDS design flowrate and scaling based on standard manufacturer model & product specifications



THIS PRODUCT MAY BE PROTECTED BY ONE OR MORE OF THE  
FOLLOWING U.S. PATENTS: 5,788,848; 6,641,720; 6,511,595; 6,581,783;  
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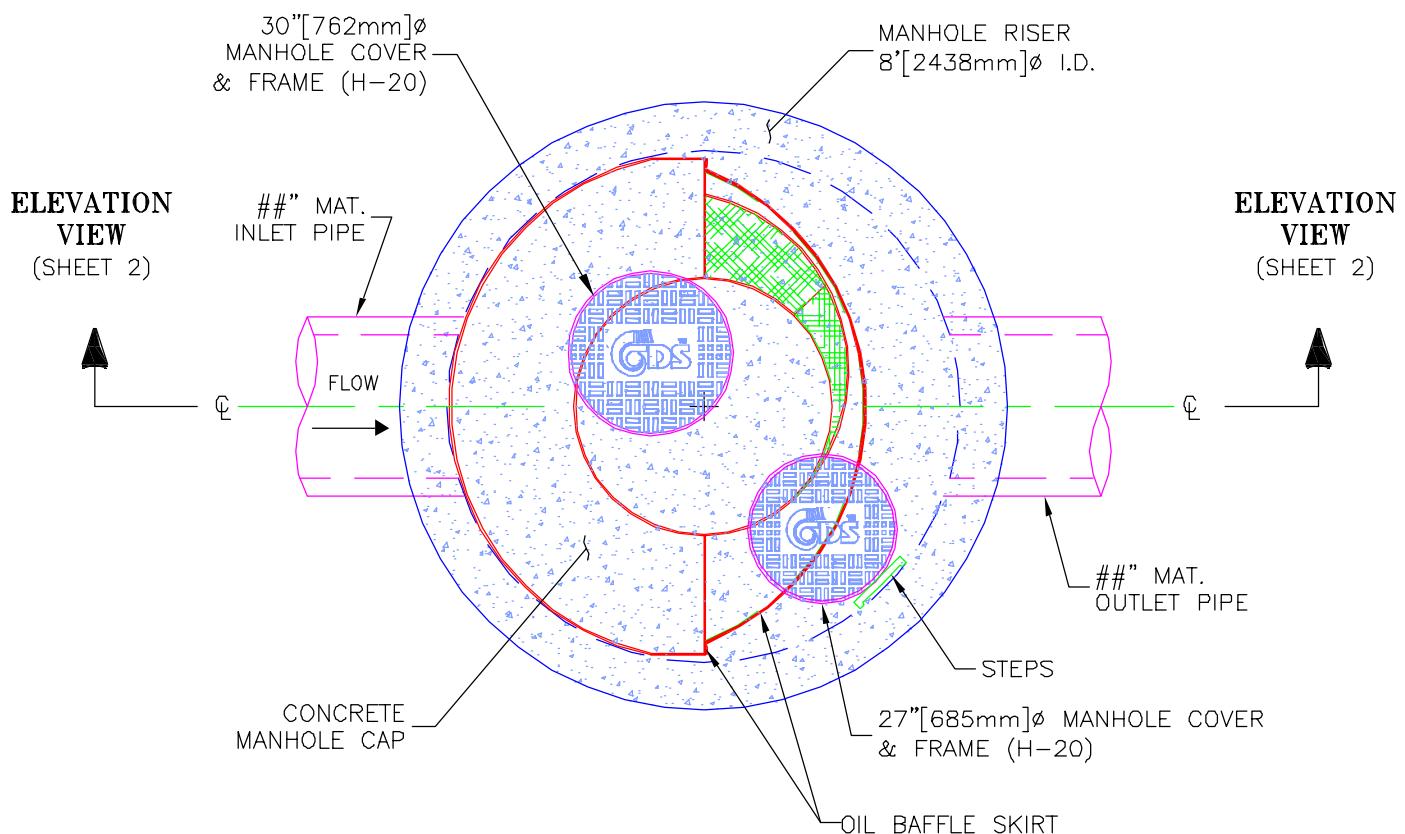
9025 Centre Pointe Dr., Suite 400, West Chester, OH 45069

800-338-1122 513-645-7000 513-645-7993 FAX

## CDS STORMWATER TREATMENT SYSTEM TYPICAL OFFLINE LAYOUT WITH BYPASS VAULT STRUCTURE



## PLAN VIEW



CDS MODEL PMSU40\_45m, 7.5 CFS TREATMENT CAPACITY  
STORM WATER TREATMENT UNIT

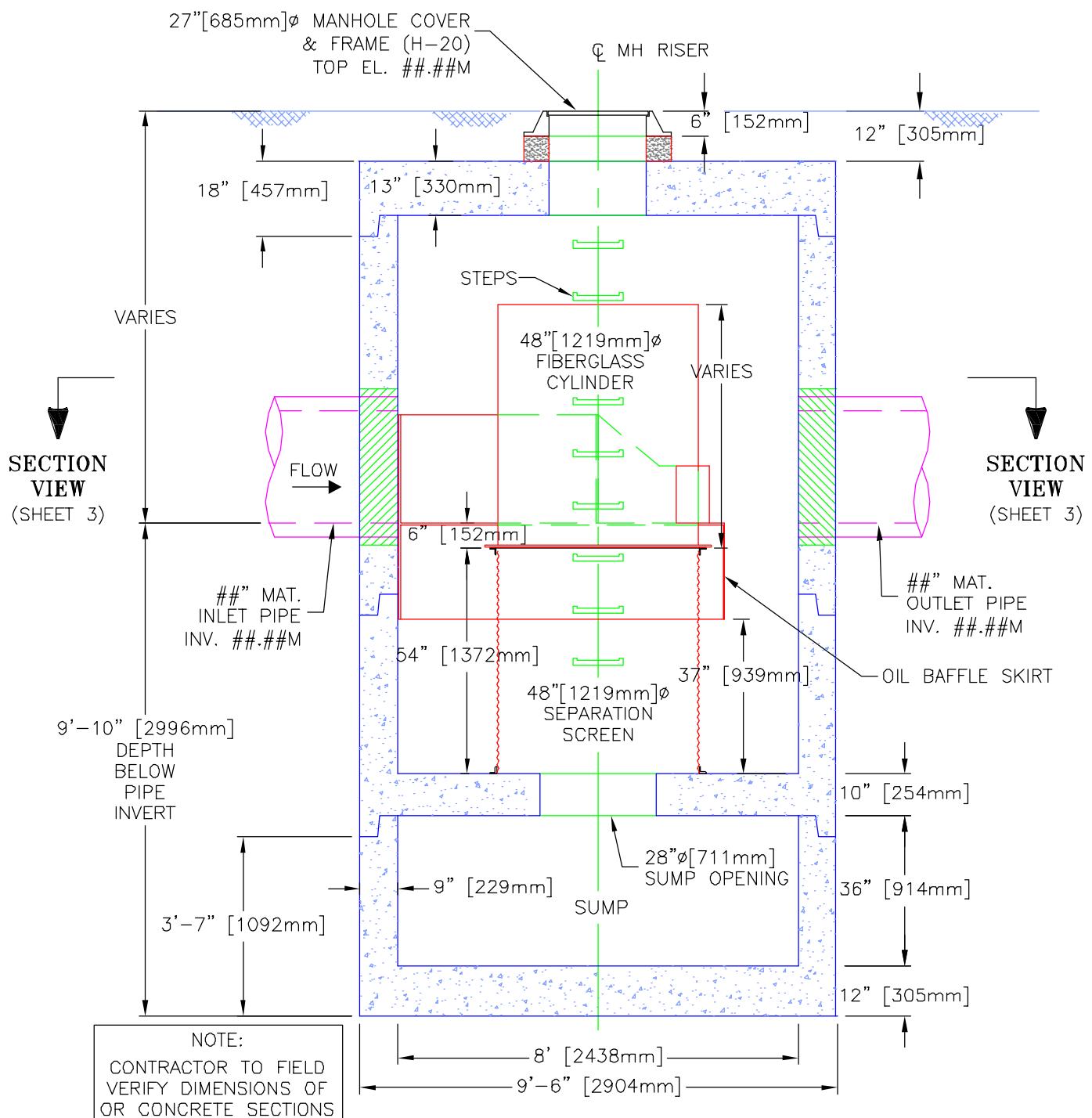


PROJECT NAME  
CITY, STATE

JOB#	XX-##-##	SCALE 1" = 3'
DATE	##/##/##	SHEET
DRAWN	INITIALS	
APPROV.		1



## ELEVATION VIEW



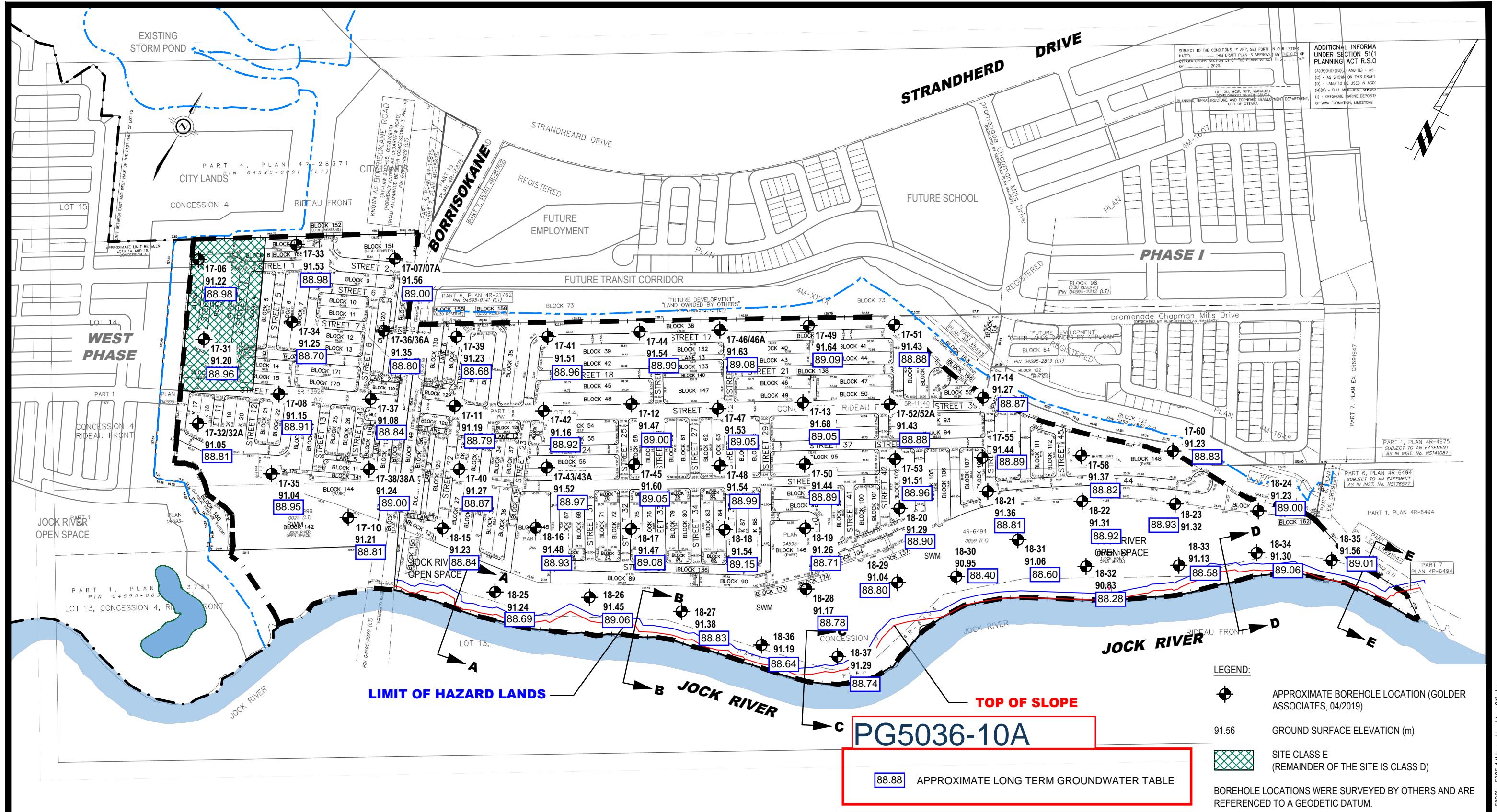
CDS MODEL PMSU40\_45m, 7.5 CFS TREATMENT CAPACITY  
STORM WATER TREATMENT UNIT



PROJECT NAME  
CITY, STATE

JOB#	XX-#-#/#	SCALE 1" = 3'
DATE	#/#/#	SHEET
DRAWN	INITIALS	
	APPROV.	2





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**CAIVAN COMMUNITIES**  
**GEOTECHNICAL INVESTIGATION**  
**PROP. RESIDENTIAL DEVELOPMENT - CONSERVANCY LANDS EAST**  
**OTTAWA, ONTARIO**  
Title:  
**TEST HOLE LOCATION PLAN**

Scale:	1:6000	Date:	09/2019
Drawn by:	MPG	Report No.:	PG5036-1
Checked by:	SD	Dwg. No.:	PG5036-1
Approved by:	DJG	Revision No.:	1





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December 01, 2022

Project Number: 1474(03)

David Schaeffer Engineering Ltd  
120 Iber Road, Unit 103  
Ottawa, Ontario  
K2S 1E9

**Attention:** Kevin Murphy, P.Eng

**Subject:** BCDC Phase 5 – Preliminary HGL Analysis

---

## Introduction

Phase 5 of the Barrhaven Conservancy Development is located in Barrhaven, Ontario, north of the Jock River, east of the Foster Creek and West of Borrisokane Road. The proposed development is approximately **13.17 ha** that will primarily comprise of single and townhouse residential lots along with a **0.64 ha** park. The following outlines the preliminary hydraulic grade line (HGL) assessment for the site, to ensure that the proposed minor system within the development is adequately sized to safely convey flows to the Jock River under various conditions. As such the following memo outlines the approach taken in assessing the development's HGL and summarises the findings of this analysis.

## Analysis Approach

Preliminary hydraulic grade line calculations for the proposed BCDC Phase 5 development were completed using PCSWMM modelling software. Pipe data, trunk storm sewer layout and Rational Method flows in the storm sewer are as provided by DSEL. The Rational Method flows were calculated based on the 2-, 5- or 10-year level of service requirements, and the 100-year flows in the hydraulic grade line calculations were estimated as 14% greater than the Rational Method flows, to account for the additional flows captured by catchbasin grates, lead pipes and/or inlet control devices under the higher surface water depths of the 100-year storm.

The 14% increase in flows for the 100-year event is based on the assumption that the head on a lead pipe/ICD will increase by 35 cm (maximum allowable major system ponding depth) during the 100-Year event. Taking a typical 250 mm lead pipe and assuming that the head on the pipe is just below the top of the grate (assumed at 1.38 m) results in a peak flow of 209 L/s, then assuming that the head is increased by 35 cm during the 100-Year (head of 1.730m) the flow through the lead pipe would increase to 234.5 L/s, which results in a 12% increase in peak flows. It is important to note that a 12% increase is observed when the same calculations are applied to the various lead pipe and ICD sizes. An additional 2% is added as a safety factor to allow some flexibility in the design, as it is likely that not all lead pipes will have a head of 1.38 m (just below the top of MH) for the level of service specified.

The proposed storm sewer infrastructure data was extracted from DSEL's drawings and incorporated into a PCSWMM model, and flows derived by DSEL's Rational Method calculations were then applied to each Maintenance Hole (MH) in the model as steady flows (using the baseflow option). Exit losses were applied to all storm sewer pipes in the system based on the angle of the downstream connection.

As in line with all other works completed for the BCDC development phases, the preliminary HGL analysis was completed under two conditions:

- 100-year rainfall event on the development and a 5-year spring water level on the Jock River
- Level of service (2/5/10-year) rainfall event on the development and a 100-year spring water level on the Jock River

Note that the water level along the Jock River through the length of this development varies, and as such the nearest corresponding upstream water surface elevation calculated by RVCA's HEC-RAS floodplain mapping model of the Jock River was applied at each of the respective storm sewer outlets. Also, note that assuming a 5-year spring water level on the Jock River for a 100-year rainfall event on the development is an inherently conservative assumption, as the critical storm for the proposed development is a summer (intense rainfall) event while the critical storm for the Jock River is a spring (snowmelt + rainfall) event. A preliminary Single Station Flood Frequency analysis was completed by JFSA using only summer flows (from May 15 to October 31) based on historical flow data recorded at the Moodie Drive Water Survey Canada gauge. This analysis found that the 100-year summer flow on the Jock River is around **99 m<sup>3</sup>/s**, while the 5-year spring flow is around **123 m<sup>3</sup>/s**, therefore the downstream boundary condition applied is conservative.

Within the proposed development Oil and Grit Separators (OGS) units in conjunction with LID measures will be implemented to ensure the site meets quality control requirements. Preliminary OGS units and associated by-pass weir elevations have also been included in the model, based on similar drainage areas and imperviousness seen in BCDC Phase 2.

Trunk Sewer 9 will have a drainage area of **7.21 ha** at **75%** imperviousness, Trunk Sewer 10 has a drainage area of **6.56 ha** at **80%** imperviousness. In a preliminary consultation with the OGS manufacturer, it was suggested that the closest match to the detailed OGS sizing for BCDC Phase 2 is **OGS 3**, which used a **PMSU 4045-8** OGS unit with a weir height of **0.65m**, this unit had a drainage area of **6.77 ha** at **64%** imperviousness.

## Results

The maximum HGL obtained at each MH has been extracted from the level of service (2/5/10-year) event / 100-year Jock River water level scenario and the 100-year event / 5-year Jock River water level scenario, with the results from this analysis provided in Tables 1 & 2, respectively. As all proposed units within this development will have sump pumps, the simulated HGL was compared against the top of MH elevation to ensure that all storm sewers infrastructure is sufficiently sized and is not surcharging to the major system during the assessed events.

From this analysis, it was found that the critical scenario for HGL within the development was the level of service development event and 100-year water level on the Jock River scenario. Based on this scenario, no MHs will have an HGL elevation above the top of MH (minimum freeboard of **0.64 m** at **MH-514** to **MH-516** and **MH-521**), with an average freeboard of **0.74 m** from the top of MH throughout the proposed development.

For the 100-year event and 5-year water level on the Jock River, no MHs will have HGL elevations above the top of MH (minimum freeboard of **1.22 m** at **MH-514** and **MH-515**), with an average freeboard of **1.38 m** from the top of MH throughout the proposed development. As such it can be concluded that the proposed storm sewer infrastructure is sufficiently sized, to safely convey minor system flows from the development under various extreme conditions.

## Conclusion

A preliminary HGL analysis for Phase 5 of the Barrhaven Conservancy Development was completed using PCSWMM based on storm sewer and flow details provided by DSEL. From this analysis, it was found that the proposed storm sewer infrastructure is sufficiently sized to convey all minor system flows to the Jock River and will not result in any MHs surcharging to the street under extreme events such as 100-year rainfall events on the development and a 5-year spring water level on the Jock River and a level of service (2/5/10 Year) rainfall event on the development and a 100-year spring water level on the Jock River, with the former being the more critical scenario for the HGL within the development.

Yours truly,  
**J.F Sabourin and Associates Inc.**



Jonathon Burnett, P.Eng  
Water Resources Engineer

cc: J.F Sabourin, M.Eng, P.Eng  
Director of Water Resources Projects



## Figures

Figure 1: PCSWMM Model Overview

## Tables

Table 1: HGL Result Tables - Level of service (2/5/10-year) BCDC Development &

100-Year Jock River

Table 2: HGL Result Tables - 100-Year BCDC Development & 5-Year Jock River

## Attachments

Attachment A: DSEL Rational Method Calculations

## Modelling Files - Provided Electronically

PCSWMM: BCDC-P5\_HGL\_v01.1-2-5-10-YrDev-100YrJock.inp

BCDC-P5\_HGL\_v01.1-100-YrDev-5YrJock.inp



## Legend

- Junctions
- ▲ Outfalls
- Conduits
- Weirs
- Site Plan

SCALE: 1:2500  
0 50 100 150 m

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WATER RESOURCES AND ENVIRONMENTAL CONSULTANTS  
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Barrhaven Conservancy Development  
Phase 5

Figure 1: Preliminary HGL Analysis  
Model Overview

PROJECT	1474(03)-21
DRAWN	JB
DATE	December 2022

**Table 1: BCDC Phase 5 - Preliminary HGL Analysis**  
**Level of Service (2/5/10 Year) BCDC Development & 100-Year Jock River**

MH-ID	Invert Elevation	Top of MH (m)	Max HGL (m)	Freeboard (m)
MH-507	90.62	93.26	92.54	0.72
MH-513	90.42	93.10	92.43	0.67
MH-514	90.34	93.02	92.38	0.64
MH-515	90.30	93.00	92.36	0.64
MH-516	90.17	92.91	92.27	0.64
MH-521	90.05	92.83	92.19	0.64
MH-524	89.71	92.66	91.99	0.67
MH-525	89.64	92.65	91.93	0.72
MH-525-1	89.63	92.64	91.88	0.76
MH-528	89.63	92.67	91.89	0.78
MH-528-1	89.63	92.67	91.83	0.84
MH-529	90.43	93.01	92.23	0.78
MH-530	90.37	93.01	92.20	0.81
MH-534	90.17	92.99	92.11	0.88
MH-537	90.02	92.91	92.07	0.84
MH-538	89.87	92.91	92.01	0.90
MH-543	89.69	92.65	91.96	0.69
			<b>Min</b>	0.64
			<b>Max</b>	0.90
			<b>Average</b>	0.74

Note: Analysis assumes 100 year spring water level on the Jock River

Model Name:BCDC-P5\_HGL\_v01.1-2-5-10-YrDev-100YrJock.inp

**Table 2: BCDC Phase 5 - Preliminary HGL Analysis**  
**100-Year BCDC Development & 5-Year Jock River**

MH-ID	Invert Elevation	Top of MH (m)	Max HGL (m)	Freeboard (m)
MH-507	90.62	93.26	92.02	1.24
MH-513	90.42	93.10	91.87	1.23
MH-514	90.34	93.02	91.81	1.22
MH-515	90.30	93.00	91.78	1.22
MH-516	90.17	92.91	91.67	1.24
MH-521	90.05	92.83	91.56	1.27
MH-524	89.71	92.66	91.29	1.37
MH-525	89.64	92.65	91.22	1.43
MH-525-1	89.63	92.64	91.16	1.48
MH-528	89.63	92.67	91.19	1.48
MH-528-1	89.63	92.67	91.12	1.55
MH-529	90.43	93.01	91.63	1.38
MH-530	90.37	93.01	91.59	1.42
MH-534	90.17	92.99	91.47	1.52
MH-537	90.02	92.91	91.42	1.49
MH-538	89.87	92.91	91.34	1.57
MH-543	89.69	92.65	91.27	1.38
			<b>Min</b>	1.22
			<b>Max</b>	1.57
			<b>Average</b>	1.38

Note: Analysis assumes 5 year spring water level on the Jock River

Model Name:BCDC-P5\_HGL\_v01.1-100-YrDev-5YrJock.inp



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# Attachment A

DSEL Rational Method Calculations

## STORM SEWER CALCULATION SHEET (RATIONAL METHOD)

Local Roads Return Frequency = 2 years  
Collector Roads Return Frequency = 5 years  
Arterial Roads Return Frequency = 10 years



Manning 6

LOCATION		AREA (Ha)												FLOW							SEWER DATA													
		2 YEAR				5 YEAR				10 YEAR				100 YEAR				Time of	Intensity	Intensity	Intensity	Intensity	Peak Flow	DIA. (mm)	DIA. (mm)	Type	Slope	Length	Capacity	Velocity	Time of	Ratio		
Location	From Node	To Node	Area (Ha)	R	Indiv.	Accum.	Area (Ha)	R	Indiv.	Accum.	Area (Ha)	R	Indiv.	Accum.	Area (Ha)	R	Indiv.	Accum.	Conc.	2 Year	5 Year	10 Year	100 Year	Q (l/s)	(actual)	(nominal)	(%)	(m)	(l/s)	(m/s)	Low (min Q/Q full)			
Centerline7 - 07																																		
	501	502	0.32	0.67	0.60	0.60			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	46	375	375	PVC	0.30	118.0	96.0323	0.8695	2.2619	0.477	
		502	505	0.02	0.67	0.04	0.63			0.00	0.00			0.00	0.00			0.00	0.00	12.26	69.09	93.59	109.66	160.23	44	450	450	CONC	0.25	31.5	142.5531	0.8963	0.5857	0.307
To Centerline15 - 15, Pipe 505 - 507						0.63				0.00							0.00	0.00	12.85															
Centerline4 - 04																																		
Contribution From Centerline15 - 15, Pipe 505 - 507			0.63							0.69							0.00	0.00	13.24															
Contribution From Centerline15 - 15, Pipe 506 - 507			0.00							0.00							0.85	0.00	11.43															
	0.22	0.80	0.49	1.12					0.00	0.69			0.00	0.85			0.00	0.00	13.24	66.26	89.71	105.08	153.51	261	750	750	CONC	0.11	114.5	369.2322	0.8358	2.2833	0.707	
To Centerline11 - 11, Pipe 513 - 514			1.66							0.69							0.85	0.00	15.52															
Centerline2 - 02																																		
	511	512	0.42	0.80	0.93	0.93			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	72	450	450	CONC	0.20	99.5	127.5033	0.8017	2.0685	0.563	
To Centerline11 - 11, Pipe 512 - 513			0.93							0.00							0.00	0.00	12.07															
Centerline11 - 11																																		
	0.20	0.80	0.44	0.44					0.00	0.00			0.00	0.00			0.00	0.00	0.00	0.00	0.00	0.00												
	508	509	0.29	0.67	0.54	0.98			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	76	450	450	CONC	0.20	90.5	127.5033	0.8017	1.8814	0.593	
	509	510	0.12	0.67	0.22	1.21			0.00	0.00			0.00	0.00			0.00	0.00	11.88	70.26	95.20	111.56	163.01	85	450	450	CONC	0.20	10.5	127.5033	0.8017	0.2183	0.666	
	510	512	0.16	0.67	0.30	1.51			0.00	0.00			0.00	0.00			0.00	0.00	12.10	69.58	94.27	110.46	161.40	105	525	525	CONC	0.20	39.0	192.3297	0.8885	0.7316	0.545	
Contribution From Centerline2 - 02, Pipe 511 - 512			0.93							0.00							0.00	0.00	12.07															
	512	513	0.19	0.67	0.35	2.79			0.00	0.00			0.00	0.00			0.00	0.00	12.83	67.41	91.29	106.95	156.24	188	675	675	CONC	0.15	47.5	325.5584	0.9098	0.8702	0.579	
Contribution From Centerline4 - 04, Pipe 507 - 513			1.66						0.69				0.85	0.00			0.00	0.00	15.52															
	513	514	0.21	0.67	0.39	4.85			0.00	0.69			0.00	0.85			0.00	0.00	15.52	60.56	81.90	95.90	140.03	431	900	900	CONC	0.11	51.0	600.4123	0.9438	0.9006	0.718	
	514	515	0.03	0.67	0.06	4.90			0.00	0.69			0.00	0.85			0.00	0.00	16.43	58.60	79.22	92.75	135.41	421	900	900	CONC	0.11	8.5	600.4123	0.9438	0.1501	0.700	
	515	516	0.09	0.67	0.17	5.07			0.00	0.69			0.00	0.85			0.00	0.00	16.58	58.28	78.79	92.25	134.67	428	900	900	CONC	0.11	56.5	600.4123	0.9438	0.9978	0.713	
To Centerline1 - 01, Pipe 516 - 521			5.07						0.69				0.85	0.00			0.00	0.00	17.57															
Centerline3 - 03																																		
Contribution From Centerline1 - 01, Pipe 516 - 521			5.07						1.15				0.85	0.00			0.00	0.00	18.60															
Contribution From Centerline1 - 01, Pipe 519 - 521			0.00						1.40				0.00	0.00			0.00	0.00	12.21															
	521	524	0.55	0.67	1.02	6.10			0.00	2.55			0.00	0.85			0.00	0.00	18.60	54.40	73.49	86.01	125.53	592	900	900	CONC	0.17	110.0	746.4104	1.1733	1.5626	0.793	
To Centerline10 - 10, Pipe 524 - 525			6.10						2.55				0.85	0.00			0.00	0.00	20.16															
Centerline10 - 10																																		
	520	517	0.62	0.67	1.15	1.15			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	89	450	450	CONC	0.20	104.5	127.5033	0.8017	2.1725	0.696	
	517	518	0.17	0.67	0.32	1.47			0.00	0.00			0.00	0.00			0.00	0.00	12.17	69.36	93.97	110.10	160.87	102	450	450	CONC	0.25	10.5	142.5531	0.8963	0.1952	0.716	
	518	525	0.18	0.67	0.34	1.81			0.00	0.00			0.00	0.00			0.00	0.00	12.37	68.77	93.15	109.14	159.47	124	525	525	CONC	0.20	48.0	192.3297	0.8885	0.9004	0.646	
To Centerline5 - 05, Pipe 525 - HW10			1.81						0.00				0.00	0.00			0.00	0.00	13.27															
	522	523	0.65	0.67	1.21	1.21			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	93	450	450	CONC	0.20	39.0	127.5033	0.8017	0.8108	0.729	
	523	524	0.21	0.67	0.39	1.60			0.00	0.00			0.00	0.00			0.00	0.00	10.81	73.83	100.10	117.32	171.47	118	525	525	CONC	0.20	49.0	192.3297	0.8885	0.9192	0.615	
Contribution From Centerline3 - 03, Pipe 521 - 524			6.10						2.55				0.85	0.00			0.00	0.00	20.16															
	524	525	0.00	7.70					2.55				0.00	0.85			0.00	0.00	20.16	51.78	69.90	81.80	119.35	646	1050	1050	CONC	0.11	8.0	905.6791	1.0459	0.1275	0.714	
To Centerline5 - 05, Pipe 525 - HW10			7.70						2.55				0.85	0.00			0.00	0.00	20.29															
Centerline5 - 05																																		
Contribution From Centerline10 - 10, Pipe 518 - 525			1.81						0.00				0.00	0.00			0.00	0.00	13.27															
Contribution From Centerline10 - 10, Pipe 524 - 525			7.70						2.55				0.85	0.00			0.00	0.00	20.29															
	525	HW10	0.02	0.67	0.04	9.54			0.00	2.55			0.00	0.85			0.00	0.00	20.29	51.57	69.63	81.48	118.87	739	1050	1050	CONC	0.11	32.0	905.6791	1.0459	0.5099	0.816	
Centerline12 - 12																																		
Contribution From Centerline9 - 09, Pipe 545 - 546			1.38						0.00				0.00	0.00			0.00	0.00	13.14															
			0.00	1.38	0.05	0.67	0.09	0.09		0.00	0.00		0.00	0.00			0.00	0.00																
	546	547	0.36	0.80	0.80	2.18			0.00	0.09			0.00	0.00			0.00	0.00	13.14	66.55	90.10	105.55	154.20	153	600	600	CONC	0.15	91.5	237.8056	0.8411	1.8132	0.645	
	547	548	0.45	0.80	1.00	3.18			0.00	0.09			0.00</																					

B. S. 11

### Definitions:

$Q = 2.78 \text{ AIR}$ , where

**Q = Peak Flow in L**

A = Areas in hectare

I = Rainfall Intensity

N

#### Notes:

### 1) Ottawa Rainfall-Intensity

2) Min. Velocity = 0.80 m/s

1 PROJECT

signed: A. S. PROJECT

### Part 3: Summary

CHI - 5 CHI

W.L.V.W.

City of Ottawa

## STORM SEWER CALCULATION SHEET (RATIONAL METHOD)

Local Roads Return Frequency = 2 years  
Collector Roads Return Frequency = 5 years  
Arterial Roads Return Frequency = 10 years



Manning 0

LOCATION		AREA (Ha)												FLOW							SEWER DATA													
		2 YEAR				5 YEAR				10 YEAR				100 YEAR				Time of	Intensity	Intensity	Intensity	Intensity	Peak Flow	DIA. (mm)	DIA. (mm)	Type	Slope	Length	Capacity	Velocity	Time of	Ratio		
		Area (Ha)	R	Indiv.	Accum.	Area (Ha)	R	Indiv.	Accum.	Area (Ha)	R	Indiv.	Accum.	Area (Ha)	R	Indiv.	Accum.	Conc.	2 Year	5 Year	10 Year	100 Year	Q (l/s)	(actual)	(nominal)	(%)	(m)	(l/s)	(m/s)	Low (min)	Q/Q full			
Location	From Node	To Node																																
	548	528	0.03	0.67	0.06	3.24			0.00	0.09			0.00	0.00			0.00	0.00	16.61	58.20	78.68	92.12	134.48	196	600	600	CONC	0.25	36.0	307.0058	1.0858	0.5526	0.637	
To Centerline13 - 13, Pipe 528 - HW9						3.24													0.00	17.17														
Centerline8 - 08																																		
	539	540	0.32	0.67	0.60	0.60			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	46	300	300	PVC	0.40	52.0	61.1589	0.8652	1.0017	0.749	
	540	541	0.41	0.67	0.76	1.36			0.00	0.00			0.00	0.00			0.00	0.00	11.00	73.16	99.18	116.24	169.89	99	450	450	CONC	0.20	68.0	127.5033	0.8017	1.4137	0.780	
	541	542	0.13	0.67	0.24	1.60			0.00	0.00			0.00	0.00			0.00	0.00	12.42	68.63	92.96	108.91	159.13	110	450	450	CONC	0.25	10.5	142.5531	0.8963	0.1952	0.771	
	542	543	0.17	0.67	0.32	1.92			0.00	0.00			0.00	0.00			0.00	0.00	12.61	68.05	92.17	107.98	157.76	131	600	600	CONC	0.15	48.0	237.8056	0.8411	0.9512	0.549	
To Centerline13 - 13, Pipe 543 - 528						1.92												0.00	13.56															
Centerline1 - 01																																		
	519	521			0.00	0.00	0.75	0.67	1.40	1.40			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	146	525	525	CONC	0.20	118.0	192.3297	0.8885	2.2136	0.757	
To Centerline3 - 03, Pipe 521 - 524						0.00			1.40				0.00				0.00	12.21																
	535	536			0.00	0.00	0.21	0.80	0.47	0.47			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	49	375	375	PVC	0.30	51.5	96.0323	0.8695	0.9872	0.507	
	536	537			0.00	0.00	0.18	0.80	0.40	0.87			0.00	0.00			0.00	0.00	10.99	73.21	99.25	116.32	170.01	86	450	450	CONC	0.20	53.5	127.5033	0.8017	1.1122	0.675	
To Centerline13 - 13, Pipe 537 - 538						0.00			0.87				0.00				0.00	12.10																
Contribution From Centerline11 - 11, Pipe 515 - 516						5.07			0.69				0.85				0.00	17.57																
	516	521			0.00	5.07	0.25	0.67	0.47	1.15			0.00	0.85			0.00	0.00	17.57	56.29	76.07	89.05	129.98	449	900	900	CONC	0.11	58.0	600.4123	0.9438	1.0242	0.748	
To Centerline3 - 03, Pipe 521 - 524						5.07			1.15				0.85				0.00	18.60																
Centerline9 - 09																																		
	531	533	0.25	0.80	0.56	0.56			0.00	0.00			0.00	0.00			0.00	0.00																
To Centerline6 - 06, Pipe 533 - 534			0.36	0.67	0.67	1.23			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	94	525	525	CONC	0.20	104.5	192.3297	0.8885	1.9603	0.490	
	544	545	0.36	0.36	0.80	0.80	0.80			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	61	375	375	PVC	0.30	78.5	96.0323	0.8695	1.5047	0.640
	545	546	0.26	0.80	0.58	1.38			0.00	0.00			0.00	0.00			0.00	0.00	11.50	71.47	96.86	113.51	165.88	99	450	450	CONC	0.20	78.5	127.5033	0.8017	1.6320	0.773	
To Centerline12 - 12, Pipe 546 - 547						1.38			0.00				0.00				0.00	13.14																
Centerline6 - 06																																		
	532	533	0.20	0.80	0.44	0.44			0.00	0.00			0.00	0.00			0.00	0.00																
To Centerline14 - 14, Pipe 534 - 537			0.64	0.40	0.71	1.16			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	89	450	450	CONC	0.20	62.0	127.5033	0.8017	1.2889	0.697	
	533	534	0.13	0.80	0.29	2.67			0.00	0.00			0.00	0.00			0.00	0.00	11.96															
	544	545	0.13	0.80	0.26	2.67			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	61	375	375	PVC	0.30	78.5	96.0323	0.8695	1.5047	0.640	
To Centerline14 - 14, Pipe 534 - 537						2.67			0.00				0.00				0.00	12.72																
Centerline15 - 15																																		
	506	507			0.00	0.00			0.00	0.00	0.36	0.85	0.85	0.85			0.00	0.00	10.00	76.81	104.19	122.14	178.56	104	450	450	CONC	0.25	77.0	142.5531	0.8963	1.4318	0.729	
To Centerline4 - 04, Pipe 507 - 513						0.00			0.00			0.85				0.00	0.00	11.43																
	526	529			0.00	0.00			0.23	0.85	0.54	0.54					0.00	0.00																
To Centerline14 - 14, Pipe 529 - 530			0.93	0.80	2.07	2.07			0.00	0.00		0.54				0.00	0.00	10.00	76.81	104.19	122.14	178.56	225	600	600	CONC	0.25	62.0	307.0058	1.0858	0.9517	0.734		
	527	529			0.00	0.00			0.00	0.00	0.26	0.85	0.61	0.61			0.00	0.00	10.00	76.81	104.19	122.14	178.56	75	375	375	PVC	0.35	46.0	103.7267	0.9392	0.8163	0.723	
To Centerline14 - 14, Pipe 529 - 530						0.00			0.00			0.61				0.00	0.00	10.82																
	503	504			0.00	0.00	0.10	0.85	0.24	0.24			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	25	300	300	PVC	0.35	41.0	57.2089	0.8093	0.8443	0.430	
	504	505			0.00	0.00	0.14	0.85	0.33	0.57			0.00	0.00			0.00	0.00	10.84	73.71	99.94	117.13	171.19	57	375	375	PVC	0.30	60.0	96.0323	0.8695	1.1501	0.590	
Contribution From Centerline7 - 07, Pipe 502 - 505						0.63			0.00			0.00				0.00	0.00	12.85																
	505	507			0.00	0.63	0.05	0.85	0.12	0.69			0.00	0.00			0.00	0.00	12.85	67.36	91.22	106.87	156.13	105	525	525	CONC	0.20	21.0	192.3297	0.8885	0.3939	0.547	
To Centerline4 - 04, Pipe 507 - 513						0.63			0.69			0.00				0.00	0.00	13.24																
Definitions:																									Designed:	PROJECT:								
Definitions:																									Designed:	PROJECT:								
Definitions:																									Designed:	PROJECT:								
Definitions:																									Designed:	PROJECT:								

#### **Definitions:**

Definitions.

$Q = 2.78 \text{ AIR, When } Q = \text{ Back Flow in L}$

$Q = \text{Peak Flow in L/min}$

A = Areas in hecta

I = Rainfall Intensi

Na

- Notes:  
1) Ottawa Rainfall-Intensity Curve  
2) Min. Velocity = 0.80 m/s

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A S

A.S.

Barrhaven Conservancy East Phase 5

Barrhaven Conservancy East Phase 5

Ch. 6 Ch.

City of Ottawa

# STORM SEWER CALCULATION SHEET (RATIONAL METHOD)

Local Roads Return Frequency = 2 years  
 Collector Roads Return Frequency = 5 years  
 Arterial Roads Return Frequency = 10 years

Manning 0.013



Location	LOCATION		AREA (Ha)												FLOW							SEWER DATA																														
			2 YEAR		5 YEAR		10 YEAR		100 YEAR		Time of	Intensity	Intensity	Intensity	Intensity	Peak Flow	DIA. (mm)	DIA. (mm)	Type	Slope	Length	Capacity	Velocity	Time of	Ratio																											
	From Node	To Node	Area (Ha)	R	Indiv.	Accum.	Area (Ha)	R	Indiv.	Accum.	Area (Ha)	R	Indiv.	Accum.	Conc.	2 Year	5 Year	10 Year	100 Year	Q (l/s)	(actual)	(nominal)	(%)	(m)	(l/s)	(m/s)	Low (min)	Q/Q full																								
<b>Centerline14 - 14</b>																																																				
Contribution From Centerline15 - 15, Pipe 526 - 529			2.07						0.00				0.64			0.00	10.95																																			
Contribution From Centerline15 - 15, Pipe 527 - 529			0.00						0.00				0.61			0.00	10.82																																			
529 530 0.52 0.80 1.16 3.22			0.00 0.00						0.00 1.16				0.00 0.00	10.95	73.33	99.42	116.52	170.30	371	825 825	CONC	0.11	26.5	476.0801	0.8906	0.4959	0.780																									
530 534			0.00 3.22						0.00 1.16				0.00 0.00	11.45	71.66	97.12	113.81	166.33	363	825 825	CONC	0.11	117.0	476.0801	0.8906	2.1895	0.762																									
Contribution From Centerline6 - 06, Pipe 533 - 534			2.67						0.00				0.00		12.72																																					
534 537 0.11 0.80 0.24 6.14			0.00 0.00						0.00 1.16				0.00 0.00	13.64	65.18	88.24	103.36	150.97	520	900 900	CONC	0.15	48.5	701.1305	1.1021	0.7334	0.742																									
To Centerline13 - 13, Pipe 537 - 538			6.14						0.00				1.16		0.00	14.37																																				
<b>Centerline13 - 13</b>																																																				
Contribution From Centerline14 - 14, Pipe 534 - 537			6.14						0.00				1.16		0.00	14.37																																				
Contribution From Centerline1 - 01, Pipe 536 - 537			0.00						0.87				0.00		0.00	12.10																																				
537 538 0.28 0.67 0.52 6.66			0.00 0.06	0.67	0.11 0.98				0.00 1.16				0.00 0.00																																							
538 543 0.25 0.67 0.47 7.13			0.00 0.98						0.00 1.16				0.00 0.00	14.37	63.29	85.65	100.31	146.50	622	975 975	CONC	0.15	83.0	867.9562	1.1625	1.1899	0.716																									
Contribution From Centerline8 - 08, Pipe 542 - 543			1.92						0.00				0.00		0.00	15.56	60.48	81.79	95.77	139.84	622	975 975	CONC	0.15	69.0	867.9562	1.1625	0.9892	0.717																							
543 528 0.05 0.67 0.09 9.14			0.00 0.98						0.00 1.16				0.00 0.00	16.55	58.34	78.86	92.33	134.80	717	1050 1050	CONC	0.11	29.0	905.6791	1.0459	0.4621	0.792																									
Contribution From Centerline12 - 12, Pipe 548 - 528			3.24						0.09				0.00		0.00	17.17																																				
528 HW9			0.00 12.38						0.00 1.07				0.00 1.16		0.00 0.00	17.17	57.08	77.15	90.32	131.84	894	1050 1050	CONC	0.20	4.5	1221.2174	1.4103	0.0532	0.732																							
Definitions:																																																				
Q = 2.78 AIR, where	Notes:																																																			
Q = Peak Flow in Litres per second (L/s)	1) Ottawa Rainfall-Intensity Curve																																																			
A = Areas in hectares (ha)	2) Min. Velocity = 0.80 m/s																																																			
I = Rainfall Intensity (mm/h)																																																				
R = Runoff Coefficient																																																				
Designed: A.S. PROJECT: Barrhaven Conservancy East Phase 5																																																				
Checked: W.L./V.W. LOCATION: City of Ottawa																																																				
Dwg. Reference: File Ref: Date: Sheet No. 01 Dec 2022 SHEET 3 OF 3																																																				





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Montréal, QC  
Québec, QC

March 08, 2021

Project Number: 1474

David Schaeffer Engineering Ltd  
120 Iber Road, Unit 103  
Ottawa, Ontario  
K2S 1E9

**Attention:** Steve Pichette, P.Eng.

**Subject:** Review of Quantity Control Requirement for Jock River-Reach One

---

## Introduction

Phase 2 of the Barrhaven Conservancy Development (aka Conservancy East) is located in Barrhaven, Ontario, north of the Jock River, south of the Fraser Clarke Creek and east of the Foster Creek. The proposed development is approximately 59.26 ha that will primarily comprise of single and townhouse residential lots. As a part of the City of Ottawa's review of the proposed development draft plan of Phase 2 of the Barrhaven Conservancy Development, submitted in December 2020, it is proposed that flood quantity control measures will not need to be implemented as a part of this development. This assumption is based on the work completed by Stantec in June 2007 in the "Jock River Reach One Subwatershed Study" which concluded that for future developments within Reach 1 of the Jock River: "No quantity control storage is required for flood control purposes as the hydrograph from the subwatershed will peak before the upstream peak in the Jock River" and that "No erosion control storage is required to maintain the predevelopment in-stream erosion condition". Although this study did not consider the future development of the Barrhaven Conservancy Lands, and as such the modelling completed by Stantec has been updated by JFSA to reflect these changes. The following memo outlines data sources, assessed scenarios, assumptions, and conclusions of this independent Jock River Reach One study.

It is noted that RVCA is currently engaging in a formal update/review of the Jock River Reach One Subwatershed Study, with the findings of this study having the potential to affect the above-noted design criteria. While that study is underway J.F. Sabourin and Associates Inc. (JFSA) has completed an independent Jock River - Reach One study to re-assess/confirm that the assumptions presented in the original 2007 study by Stantec are still valid, as any changes to this conclusion could greatly impact the current BCDC Phase 2 development plan.

## Background Data

The following outlines all the model and data sources used in this analysis:

- "*Jock River Floodplain Mapping Report*", (2005 - PSR Group Ltd. & JFSA)
- "*Jock River Reach One Subwatershed Study Final Report*", (2007 – Stantec)
- "*Corrigan Stormwater Management Facility Stormwater Management Report and Design Brief*", (2010 - IBI Group)
- "*Citi Gate, Highway 416 Employment Lands, Servicing Study and Stormwater Management Report (O'Keefe SWM)*", (2012 – Novatech)
- "*Foster Stormwater Management Facility, Environmental Study Report*", (2013 - CH2MHill)
- "*Todd Pond Model Keeper Analysis (Re-Assessment of Existing System Capacity)*", (2015 – JFSA)

- “*CitiGate 416 Corporate Campus Detailed Servicing and Stormwater Management Report (Phase 1)*”, (2015 – Novatech)
- “*Kennedy-Burnett Stormwater Management Facility Retrofit, Detailed Design Report*”, (2020 – Novatech)
- “*Half Moon Bay South / Addendum to April 2015 Todd Pond Model Keeper Analysis, Re-Assessment of Existing System Capacity Report*” (2020 - JFSA).

## Model Development/Scenarios

The following section outlines the various hydrologic model scenarios developed as a part of this work, with a brief description of the data sources used for each scenario and how they have been incorporated into the existing Jock River subwatershed hydrologic model.

### Model 1 - Jock River Floodplain Model – JFSA, 2005

This hydrologic model was developed as a part of the floodplain mapping study of the Jock River completed in 2005. The hydrologic model of the Jock River was developed by JFSA using SWMHYMO, with independent models developed to simulate both summer and spring events. Both models were calibrated to field measured flows, recorded at the Water Survey Canada Flow Gauge at Moodie Drive. These models function as the basis for which all future models (both by JFSA and others) have been built on. Refer to Figure 1 (JFSA, 2005) for an overview of the subcatchments for reach one in this model, with full SWMHYMO input and summary files provided in Attachment A.

### Model 2 – Jock River Reach One Model – Stantec, 2007

The hydrologic analysis completed by Stantec in 2007 built upon the JFSA 2005 floodplain mapping modelling. As a part of the Stantec work, the lower reach of the Jock River (3,176 ha) which was represented as a single subcatchment in the 2005 study was subdivided into thirteen (13) subcatchments to better delineate the drainage areas to the various tributaries (O’Keefe, Fraser, Foster, Todd, Corrigan and Clarke) and to also provide a better representation of the existing development areas (Kennedy Burnett, Chapman Mills, Jockvale and Hearts Desire). The remaining natural/undeveloped areas within the Jock River corridor were subdivided into three smaller (3) sub-catchments. Refer to Figure 2 (Stantec, 2007) for an overview of the subcatchments for reach one in this model, with full SWMHYMO input and summary files provided in Attachment B.

As mentioned above from this study, it was concluded that developments located in the lower reaches of the Jock River do not require any quantity control storage for flood control purposes as the hydrograph from the subwatershed will peak before the upstream peak in the Jock River and that no erosion control storage is required to maintain the pre-development in-stream erosion conditions.

### Model 3 – Jock River Reach One Model Update – JFSA, 2021

As a part of the study outlined in this report, the 2007 Stantec SWMHYMO model of the Jock River was updated to reflect (as best as possible with the available information) proposed, approved and potential future developments, since the 2007 study.

At the time of the 2007 study, it was assumed that the floodplain of reach one of the Jock River (from Highway 416 to Greenbank Road) would not be filled and developed. Furthermore, the assumptions that were made in 2007 for the total imperviousness of future developments are not reflective of the actual constructed conditions observed in 2021; for example, the total impervious area for the Todd drainage area was assumed to be 43% in the 2007 study, while based on latest aerial photography it appears that the imperviousness for this area is closer to 58.5%). Additionally, SWM quantity controls were implemented in some tributaries within Reach One (e.g., O'Keefe, Foster and Kennedy-Burnett) to respect the hydraulic capacity of the local watercourses or other existing hydraulic constraints.

As outlined in the Background Data section of this memo, data from various reports and studies were collected and used to update Stantec's 2007 model, to best reflect existing conditions and known approved and planned development projects. As such, the thirteen (13) subcatchments of the 2007 Stantec model have been further discretized into one hundred ten (110) subcatchments, with numerous additional major system storage, SWM Ponds, and channel routing commands added. This updated existing condition model is reflective of current 2021 conditions, which assumes that the lower Jock River floodplain is undeveloped. It should also be noted that only subcatchments downstream of Highway 416 have been updated as a part of this analysis. Updates to other catchments of the Jock River further upstream, such as the Monahan Drain, Hobbs Creek, King Creek, and development areas in Richmond, where additional new information may be available, have not been included in the model updates at this time. Refer to Figure 3 for an overview of the subcatchments for reach one in this model, with full SWMHYMO input and summary files been provided in Attachment C, detailed schematics of the subcatchments updated as a part of this study have been provided in Attachment F.

Note that Novatech's PCSWMM model of the Kennedy-Burnett area was used to create a detailed SWMHYMO model of the same area. In creating this SWMHYMO model it was found that the 100-year peak outflows from the Kennedy Burnett facility were 1.4 times higher than that reported in the Novatech PCSWMM model. While it is expected that different modelling software will produce slightly different results, this difference is significant and should be investigated further; although it is unlikely that this difference is expected to change the fundamental conclusions of this analysis.

#### **Model 4A & 4B – Jock River Reach One Future Conditions (without and with quantity SWM controls) – JFSA, 2021**

Two additional models (4A and 4B) were created (which built on model 3) to evaluate the impacts of developing portions of the lower Jock River floodplain (from Highway 416 to Greenbank Road). These lands make up approximately 156 ha and would include BCDC and other properties on the south side of the Jock River. Model 4A assumes that these lands would be developed without any SWM quantity controls and Model 4B assumes that the lands would be developed with SWM Post to Pre-development quantity controls. Refer to Figure 4 for an overview of the subcatchments for reach one in these models, with full SWMHYMO input and summary files for scenarios 4A and 4B provided in Attachment D & E, respectively.

## Results

All hydrologic models were run using a 24 hours SCS storm for the 2-to-100-year events. Note that this analysis focuses on this particular rainfall event as for developed areas the summer rainfall events are more critical than the spring rainfall plus snowmelt conditions. Hence, only the summer peak flows have been summarized and compared for the various scenarios below, as the flow contributions from the developments in the lower Jock River under the spring rainfall + snowmelt event are negligible compared to the flows upstream from the greater Jock River. It is further noted that the same design storms were used in all models.

Peak flows at key locations along Reach One of the Jock River have been extracted from the various hydrologic models and provided in the following section. As a part of this analysis, 5 key locations on the Jock River have been selected to compare the simulated peak flows and are as follows: Highway 416, Borrisokane Road, Greenbank Road, Jockvale Road and the Jock River's confluence with the Rideau River. Note that for the older models (JFSA 2005 & Stantec 2007) results have only been provided at some locations, as these original models were not discretized to this higher level of detail. Additionally, the Stantec 2007 model did not assess flows on the Jock River for the 10- and 50-year events at any locations.

**Table 1: Comparison of Summer Peak Flows (m<sup>3</sup>/s) at Highway 416 (52483.00 ha)**

Scenario	Return Period					
	2-Year	5- Year	10-Year	25-Year	50-Year	100-Year
Model 1: 2005 Floodplain Study	45.676	66.292	82.076	104.643	122.469	141.415
Model 2: Stantec 2007 Reach One Analysis	45.789	66.413	n/a	104.834	n/a	141.853
Model 3: Updated Model 2 to current/ approved conditions	46.294	67.222	83.235	106.109	124.249	143.580
Model 4A: Model 3 with BCDC & others w/o SWM	46.294	67.222	83.235	106.109	124.249	143.580
Model 4B: Model 3 with BCDC & others with SWM	46.294	67.222	83.235	106.109	124.249	143.580

From Table 1 above it is seen that the peak flows on the Jock River at Highway 416 for Models 3, 4A and 4B are higher than in Models 1 and 2. This is because the computational time step in the updated models was reduced from 5 - 10 minutes to 1 minute. This change was necessary to provide stable results in the various models, especially with the additional ROUTE CHANNEL commands that have been added to the updated models. There were no other changes made to the models upstream of Highway 416.

**Table 2: Comparison of Summer Peak Flows (m<sup>3</sup>/s) at Borrisokane Road (53577.82 ha)**

Scenario	Return Period					
	2-Year	5- Year	10-Year	25-Year	50-Year	100-Year
Model 1: 2005 Floodplain Study	n/a	n/a	n/a	n/a	n/a	n/a
Model 2: Stantec 2007 Reach One Analysis	46.817	68.124	n/a	107.402	n/a	144.892
Model 3: Updated Model 2 to current/ approved conditions	47.379	69.117	85.613	108.988	127.740	147.849
Model 4A: Model 3 with BCDC & others w/o SWM	47.426	68.998	85.561	109.064	127.650	147.535
Model 4B: Model 3 with BCDC & others with SWM	47.599	69.319	85.870	109.449	128.055	147.939

From Table 2 it is seen that the peak flows on the Jock River at Borrisokane are generally lower in model 4A (developed without SWM controls) than under existing conditions (Model 3). The inclusion of SWM controls for these future developments results in the peak flows increasing from existing conditions for all return periods at this location. Note that the increase in flows at this location between the Stantec model (model 2) and the JFSA existing conditions model (model 3) again is due to the greater discretization of subcatchments at Borrisokane Road in the JFSA model. For example, in the Stantec model, the subcatchment that represents the currently undeveloped lands along the Jock River is represented as a single subcatchment (S-1). Where the JFSA updated model represents these lands as 14 individual subcatchments, all discharging to their respective locations within the Jock River (e.g. O'Keefe Creek, Foster Creek & Borrisokane Road).

**Table 3: Comparison of Summer Peak Flows (m<sup>3</sup>/s) at Greenbank Road (54717.80 ha)**

Scenario	Return Period					
	2-Year	5- Year	10-Year	25-Year	50-Year	100-Year
Model 1: 2005 Floodplain Study	n/a	n/a	n/a	n/a	n/a	n/a
Model 2: Stantec 2007 Reach One Analysis	49.195	71.220	n/a	111.172	n/a	149.236
Model 3: Updated Model 2 to current/ approved conditions	49.055	70.826	86.895	110.282	128.564	147.488
Model 4A: Model 3 with BCDC & others w/o SWM	48.599	69.773	85.389	103.842	126.050	144.531
Model 4B: Model 3 with BCDC & others with SWM	48.982	70.171	85.928	103.651	126.537	144.894

From Table 3 it is seen that peak flows on the Jock River at Greenbank Road are the lowest without SWM controls in place (Model 4A). With SWM controls in place, the peak flows are lower than the existing conditions, but not as low as when SWM controls are not implemented. Note that the JFSA existing conditions model (model 3) is presenting peak flows lower than the Stantec model (model 2) at this location, again this is due to the greater discretization in the JFSA model as discussed above.

**Table 4: Comparison of Summer Peak Flows (m<sup>3</sup>/s) at Jockvale Road (55476.26 ha)**

Scenario	Return Period					
	2-Year	5- Year	10-Year	25-Year	50-Year	100-Year
Model 1: 2005 Floodplain Study	n/a	n/a	n/a	n/a	n/a	n/a
Model 2: Stantec 2007 Reach One Analysis	49.870	72.143	n/a	112.074	n/a	150.033
Model 3: Updated Model 2 to current/ approved conditions	49.619	72.224	88.294	111.989	130.865	149.819
Model 4A: Model 3 with BCDC & others w/o SWM	49.482	71.017	86.165	105.082	128.174	146.840
Model 4B: Model 3 with BCDC & others with SWM	49.606	71.408	86.690	104.765	128.229	147.027

From Table 4 is seen that the peak flows at Jockvale Road are generally at their lowest without SWM controls in place, and that either implementing or not implementing SWM controls for future developments results in peak flows at this location being less than existing conditions.

**Table 5: Comparison of Summer Peak Flows (m<sup>3</sup>/s) at Outlet of Jock River (55579.20 ha)**

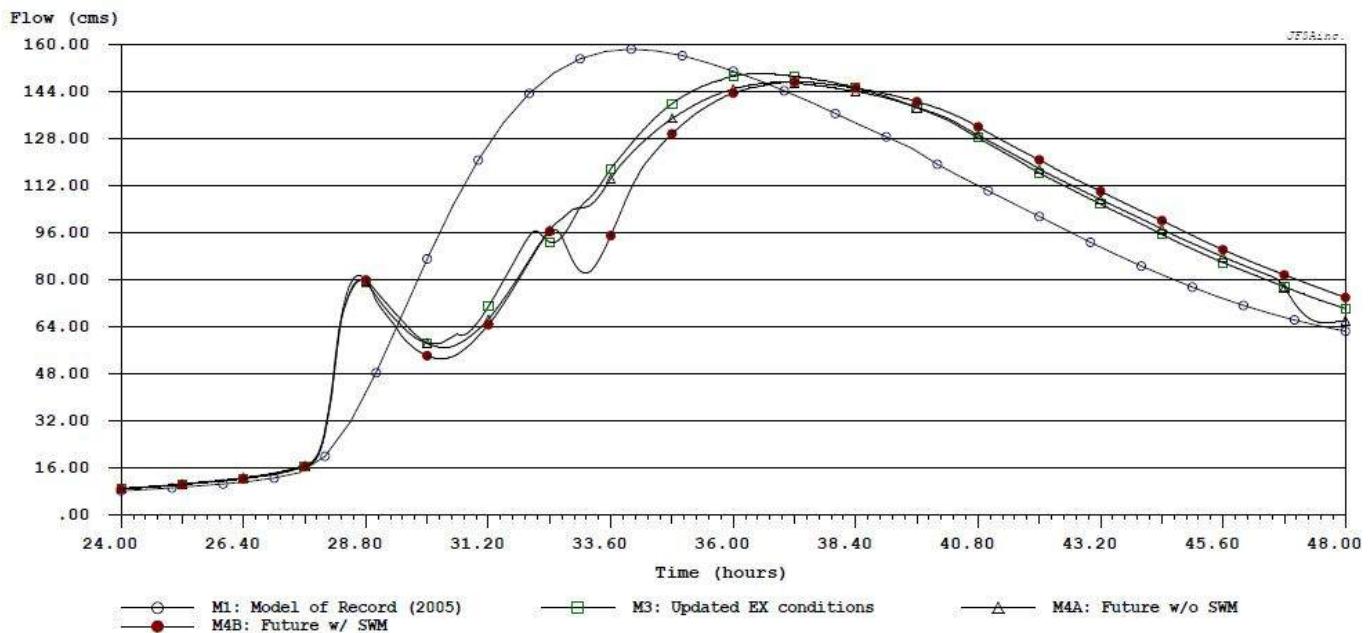
Scenario	Return Period					
	2-Year	5- Year	10-Year	25-Year	50-Year	100-Year
Model 1: 2005 Floodplain Study	49.16	72.08	89.96	115.84	136.46	158.42
Model 2: Stantec 2007 Reach One Analysis	50.78	73.65	n/a	113.97	n/a	157.69
Model 3: Updated Model 2 to current/ approved conditions	49.72	72.36	88.45	112.2	131.12	150.12
Model 4A: Model 3 with BCDC & others w/o SWM	49.58	71.17	86.35	105.27	128.42	147.10
Model 4B: Model 3 with BCDC & others with SWM	49.70	71.54	86.85	104.96	128.45	147.28

From Table 5 it is seen that the peak flows on the Jock River at the confluence with the Rideau River are generally at their lowest without SWM controls in place, and that either implementing or not implementing SWM controls for future developments results in peak flows at this location to be less than existing conditions.

## Discussion

Although not initially obvious, the reason that future urban developments within Reach One of the Jock River are decreasing peak flows on the Jock River is because developing land not only affects the peak of the hydrograph but also the overall shape. Figure A below provides a comparison of the simulated hydrographs at the Jock River's confluence with the Rideau River from the various model scenarios. During any rainfall event, the runoff from the existing and future developments within Reach One will have already peaked and decayed before the peak flows arrive at this location from the upstream drainage area. For the 100-Year SCS storm, the peak from the development in Reach One can be seen in the figure below at around 28 hours, while the peak flow on the Jock River from the upstream drainage areas occurs at around 36-37 hours, this is approximately a 9-hour difference in timing. As such, implementing SWM measures for developments in the lower portions of the Jock River will decrease peak flows from the development, but would also prolong the period of time during which they discharge into the Jock River, thus coinciding with flows from the greater Jock River, ultimately resulting in potential increases in peak flows on the Jock River. This is seen in the figure below with the future condition with SWM controls (Model 4B - Red Circles) having a higher flow in the tail than future conditions without SWM controls (Model 4A – Black Triangles). Note that the difference between Model 1 and all other scenarios is simply due to further discretization of subcatchments within Reach One.

Figure A: Comparison of simulated 100 yr Jock River hydrographs at the confluence with the Rideau River



### Hydrograph Statistics:

Legend	Filename & Comment	Time Step (min)	Drainage Area (ha)	Peak Flow (cms)	Time to Peak (hrs)	Runoff Volume (mm)	Duration of flow (hrs)	Average flow (cms)	
○	M1: Model of Record (2005)	30.00	55659.00	158.420	34.000	14.52	8.082E+06	24.000	93.538
□	M3: Updated EX conditions	1.00	55579.20	150.120	36.533	14.24	7.914E+06	24.000	91.603
△	M4A: Future w/o SWM	1.00	55579.20	147.102	36.917	14.12	7.848E+06	24.000	90.831
●	M4B: Future w/ SWM	1.00	55579.19	147.276	37.250	14.03	7.798E+06	24.000	90.252

## Conclusion

The hydrologic model developed as a part of the Jock River Reach One Subwatershed Study (Stantec 2007) has been updated to provide additional refinements in the lower reaches of the Jock River (downstream of Highway 416) and assumes the development of lands that were previously not considered in the 2007 analysis (e.g. Barrhaven Conservancy). Future development condition models were created with and without SWM controls assumed, and the peak flows extracted from these models at key locations along the lower Jock River. From this analysis, it was found that with these additional developments in the lower Jock River peak flows are generally less than existing conditions without SWM controls in place. Implementing SWM controls for these developments has also been found to generally decrease peak flows on the Jock River, but not at all locations and not to the same degree as without SWM controls. Ultimately these findings are consistent with the fundamental conclusions drawn in Stantec's 2007 Jock River Reach One study, which initially determined that for future developments within Reach One of the Jock River "No quantity control storage is required for flood control purposes as the hydrograph from the subwatershed will peak before the upstream peak in the Jock River" and that "No erosion control storage is required to maintain the pre-development in-stream erosion condition". Based on the results of the updated analysis outlined in this memo, it can confirm that the fundamental conclusions drawn in Stantec's 2007 for developments in reach one of the Jock River remain valid.

Yours truly,  
**J.F Sabourin and Associates Inc.**



Jonathon Burnett, P.Eng  
 Water Resources Engineer

cc: J.F Sabourin, M.Eng, P.Eng  
 Director of Water Resources Projects



## Figures

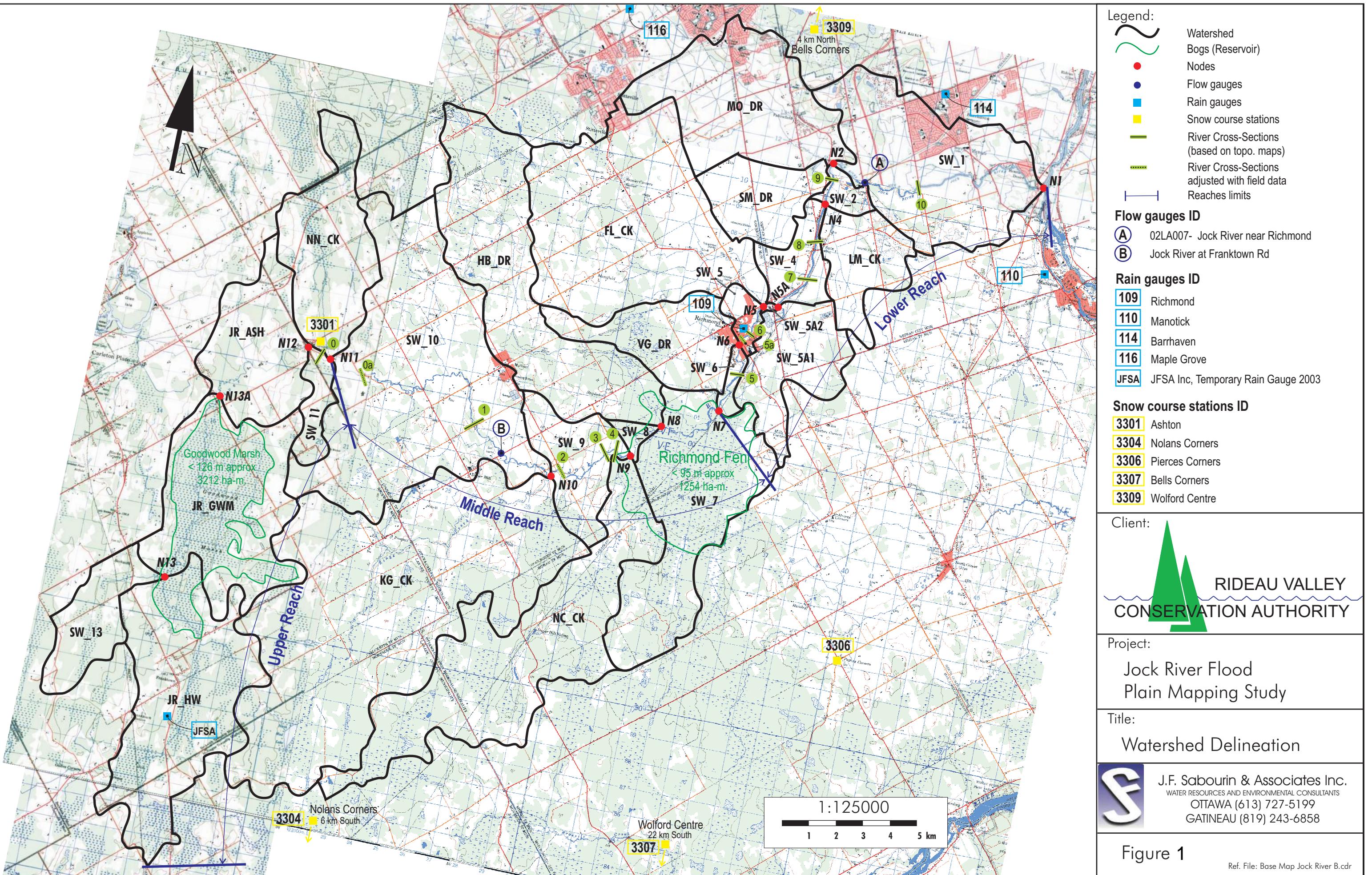
- Figure 1: Model 1 – Jock River Floodplain Model – JFSA, 2005
- Figure 2: Model 2 – Jock River Reach One Model – Stantec, 2007
- Figure 3: Model 3 – Jock River Reach One Model Update - JFSA, 2021
- Figure 4: Model 4A & 4B – Jock River Reach One Future Conditions - JFSA, 2021

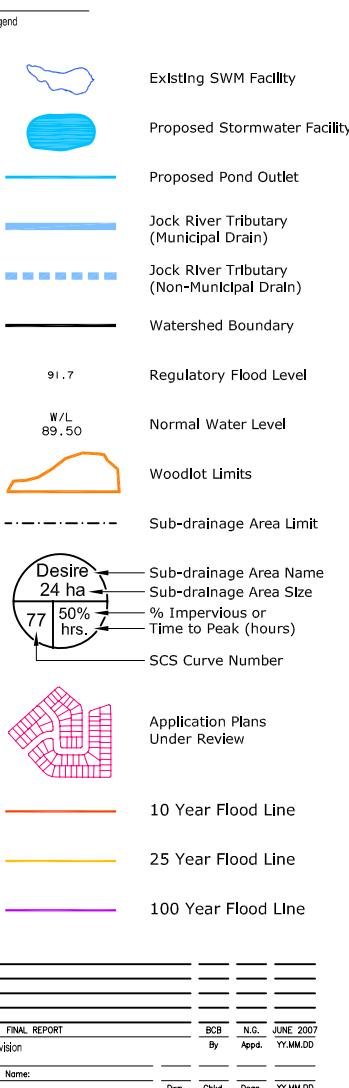
## Tables

- Table 1: Summer Peak Flows at Highway 416
- Table 2: Summer Peak Flows at Borrisokane Road.
- Table 3: Summer Peak Flows at Greenbank Road
- Table 4: Summer Peak Flows at Jockvale Road
- Table 5: Summer Peak Flows at Outlet of Jock River

## Attachments

- Attachment A: Model 1 - SWMHYMO Input & Summary files
- Attachment B: Model 2 - SWMHYMO Input & Summary files
- Attachment C: Model 3 - SWMHYMO Input & Summary files
- Attachment D: Model 4A - SWMHYMO Input & Summary files
- Attachment E: Model 4B - SWMHYMO Input & Summary files
- Attachment F: Updated Subcatchment Schematics & Tables



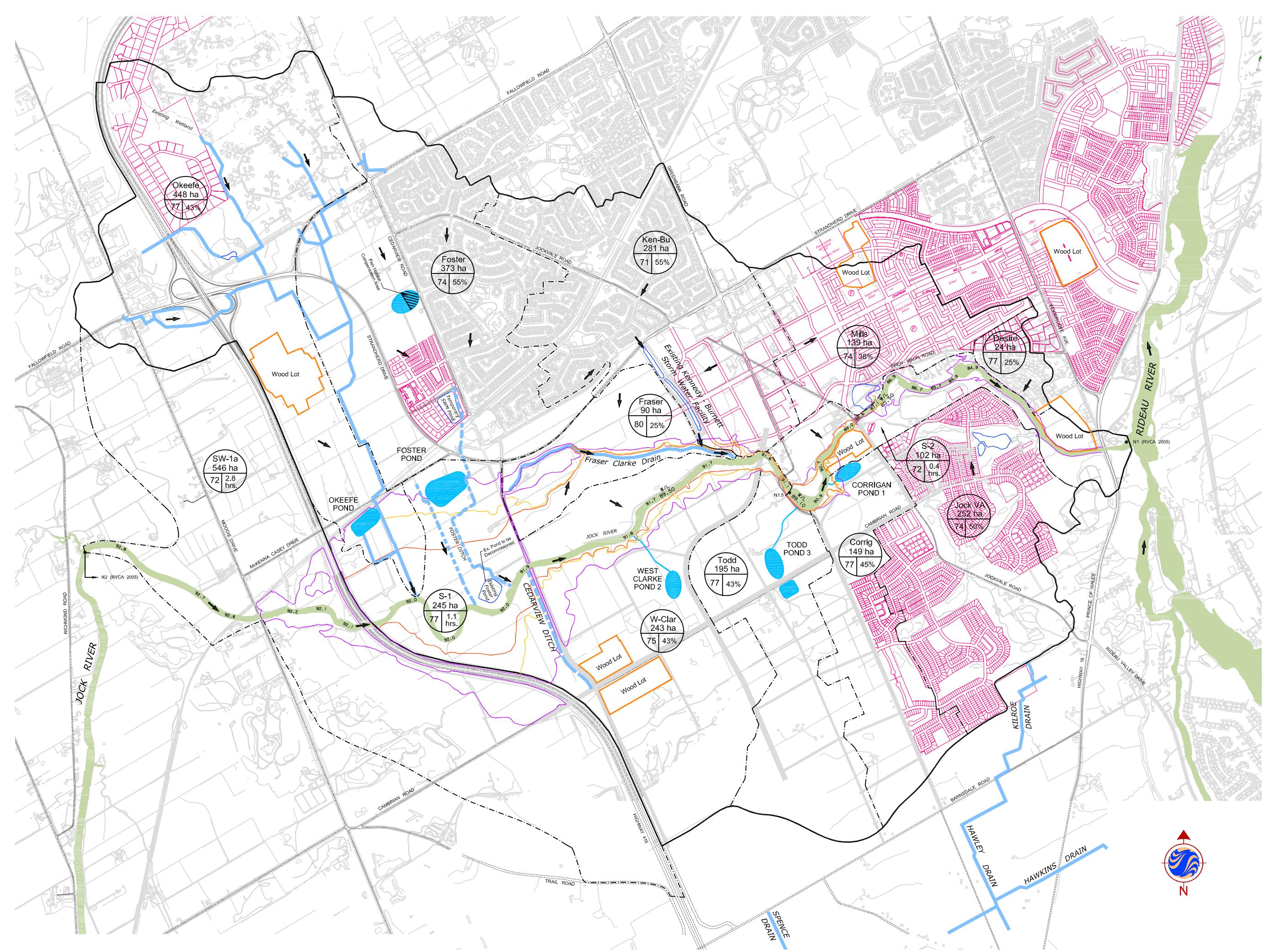


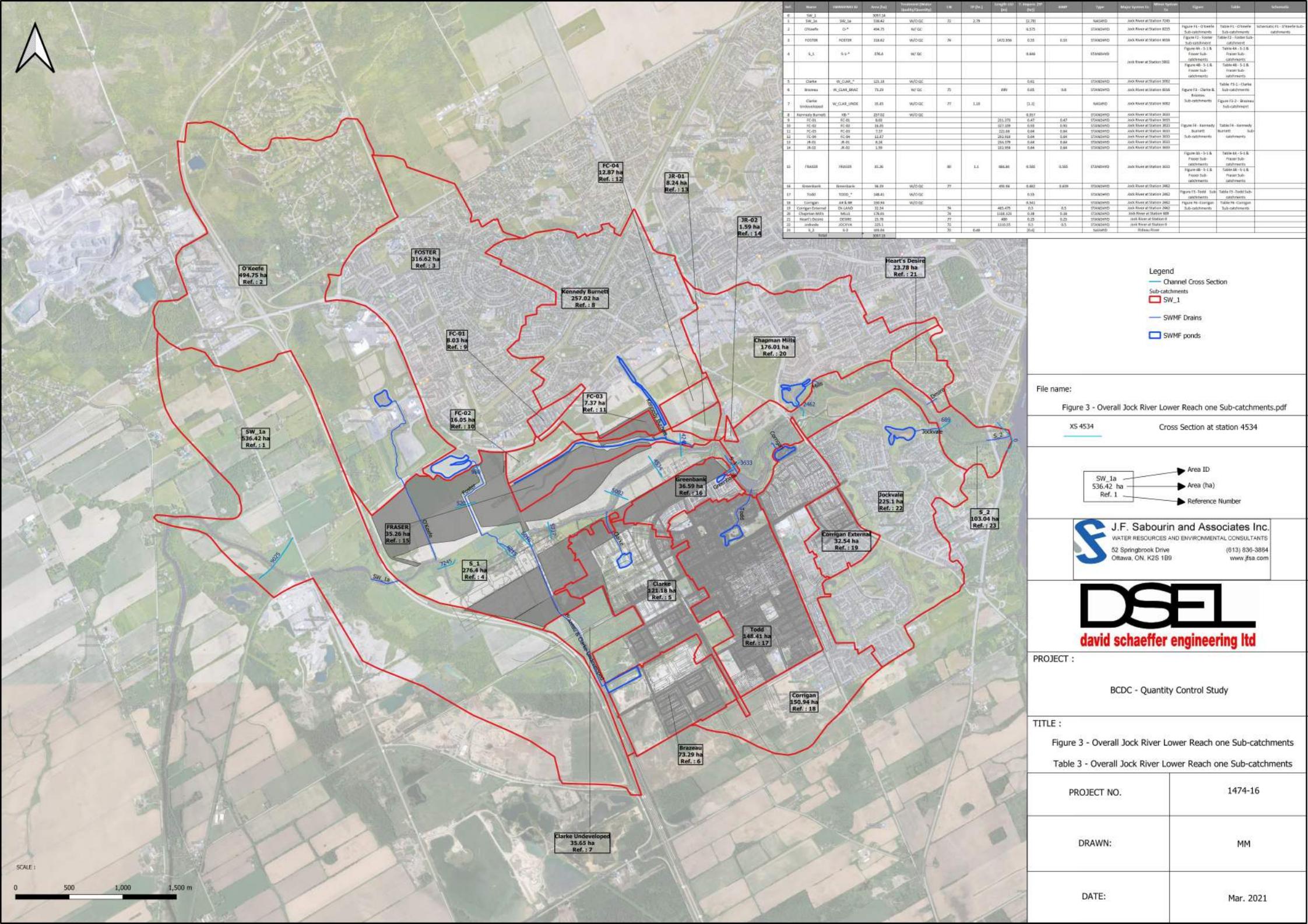
**JOCK RIVER REACH ONE  
SUB-WATERSHED STUDY**  
Ottawa ON Canada

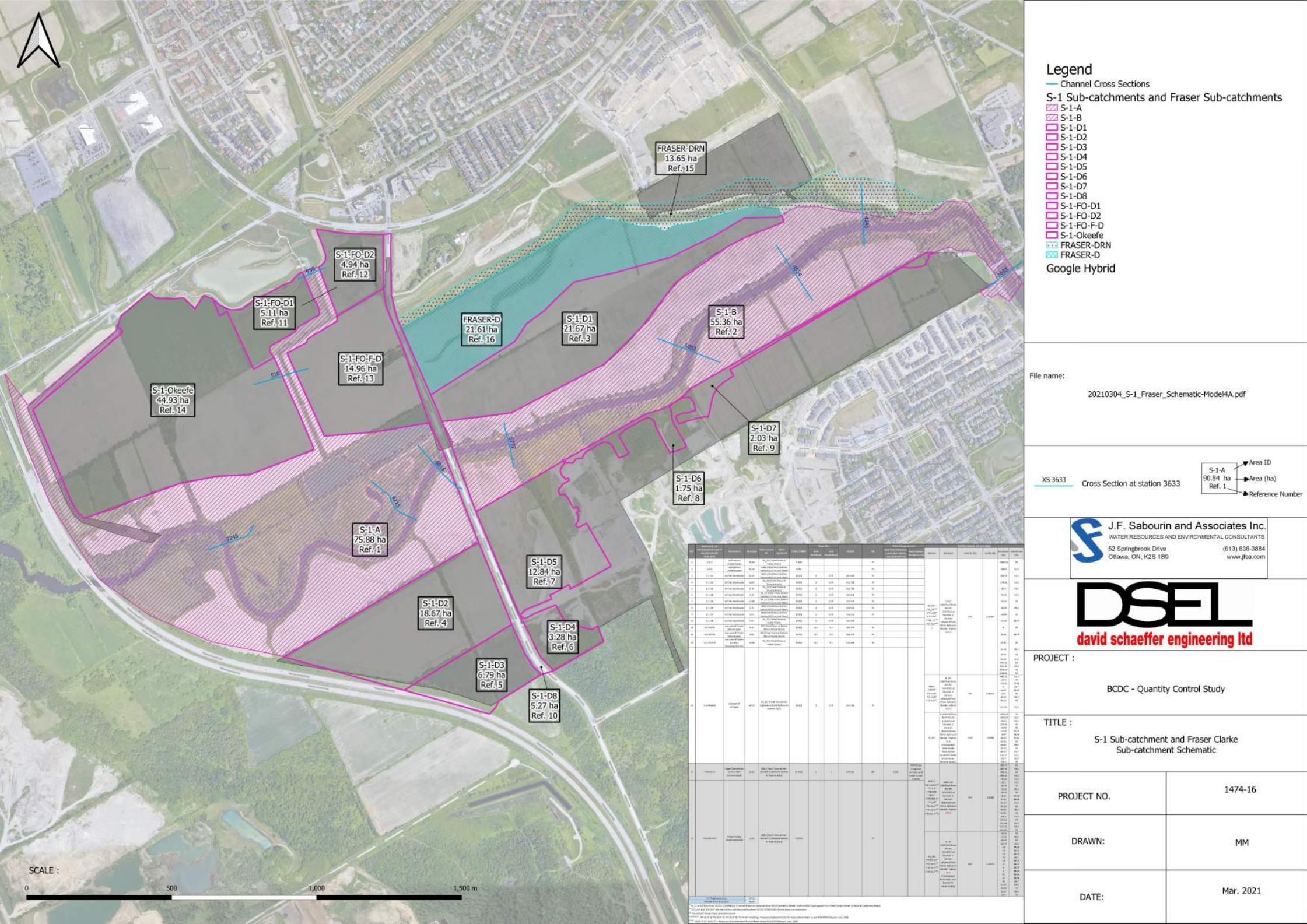
**Title**  
**PROPOSED CONDITIONS  
HYDROLOGIC MODEL  
DRAINAGE BOUNDARIES**

Project No. 60400414      Scale 0 100 200 300 500m  
 Drawing No. Sheet 1 Revision

Figure 2      1 of 1      1











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# Attachment A

Model 1 – Jock River Floodplain Model

JFSA, 2005

SWMHYMO Input & Summary files

```

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2      *#*****SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
3      *#*****SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
4      *#*****SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
5      *# Project Name: [Jock River]    Project Number: [411-02]
6      *# Date        : 06-06-2003
7      *# Modeler     : [JoF]
8      *# Company     : JFSAinc.
9      *# License #   : 2549237
10     *#*****SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
11     *# CALIBRATION OF SUMMER MODEL PARAMETERS
12     *# USING CONTINUOUS SIMULATIONS
13     *# Rainfall data from JFSA raingauge installed at site + other gauges by the City
14     *# Use data collected from May 1st to July 14, 2003
15     *
16     * Calibrated parameters for Summer 2003 data: APII=50, APIK=0.85, CN=varies,
17     *                                              SK=0.01, InterEventTime=12,
18     *                                              GWResk=0.96, VHydCond=0.055
19     *
20     *# -----
21     *
22     *START          TZERO=[2003.0501], METOUT=[2], NSTORM=[1], NRUN=[001]
23     *                  ["XAVG0315.STM"] average storm data a 15 minute time step
24     *                  The above rainf file is an average of the JFSA gauge data
25     *                  with the City of Ottawa rainfall data collected during
26     *                  the same period.
27     *% 2 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
28     START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[2]
29     *%                  ["C24SC002.stm"] <--storm filename, one per line for NSTORM time
30     *%
31     *%
32     READ STORM      STORM_FILENAME=[ "storm.001" ]
33     *%
34     MODIFY STORM     ICASEms=[1], NSHIFT=[96],
35     *                  RedFACT=[1],
36     *%
37     COMPUTE API      APII=[50], APIK=[.85]/day
38     *%
39     *%
40     *#
41     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
42     *# of 1.32
43     *%
44     CONTINUOUS NASHYD NHYD=[ "JR_HW" ], DT=[30]min, AREA=[3680](ha),
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46     *                  N=[3.0], TP=[7.13]hrs,
47     *                  Continuous simulation parameters:
48     *                  IaRECper=[4](hrs),
49     *                  SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
50     *                  InterEventTime=[12](hrs)
51     *                  Baseflow simulation parameters:
52     *                  BaseFlowOption=[1],
53     *                  InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
54     *                  VHydCond=[0.055](mm/hr), END=-1
55     *%
56     *#
57     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
58     *# of 1.32
59     *%
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63     *                  Continuous simulation parameters:
64     *                  IaRECper=[4](hrs),
65     *                  SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
66     *                  InterEventTime=[12](hrs)

```

```

67 Baseflow simulation parameters:
68 BaseFlowOption=[1] ,
69 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
70 VHydCond=[0.055](mm/hr), END=-1
71 *%-----|-----|
72 *#
73 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
74 *# of 1.80
75 *%-----|-----|
76 CONTINUOUS NASHYD NHYD= ["JR_GWM"], DT=[30]min, AREA=[3074](ha),
77 DWF=[0](cms), CN/C=[55], IA=[2.5](mm),
78 N=[3], TP=[11.33]hrs,
79 Continuous simulation parameters:
80 IaRECper=[4](hrs),
81 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
82 InterEventTime=[12](hrs)
83 Baseflow simulation parameters:
84 BaseFlowOption=[1] ,
85 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
86 VHydCond=[0.055](mm/hr), END=-1
87 *%-----|-----|
88 CONTINUOUS NASHYD NHYD= ["JR_ASH"], DT=[30]min, AREA=[1781](ha),
89 DWF=[0](cms), CN/C=[72], IA=[2.5](mm),
90 N=[3.0], TP=[3.91]hrs,
91 Continuous simulation parameters:
92 IaRECper=[4](hrs),
93 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
94 InterEventTime=[12](hrs)
95 Baseflow simulation parameters:
96 BaseFlowOption=[1] ,
97 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
98 VHydCond=[0.055](mm/hr), END=-1
99 *%-----|-----|
100 CONTINUOUS NASHYD NHYD= ["SW_11"], DT=[30]min, AREA=[500](ha),
101 DWF=[0](cms), CN/C=[66], IA=[2.5](mm),
102 N=[3.0], TP=[1.24]hrs,
103 Continuous simulation parameters:
104 IaRECper=[4](hrs),
105 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
106 InterEventTime=[12](hrs)
107 Baseflow simulation parameters:
108 BaseFlowOption=[1] ,
109 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
110 VHydCond=[0.055](mm/hr), END=-1
111 *%-----|-----|
112 *#
113 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
114 *# of 1.80
115 *%-----|-----|
116 CONTINUOUS NASHYD NHYD= ["NN_CK"], DT=[30]min, AREA=[1917](ha),
117 DWF=[0](cms), CN/C=[66], IA=[2.5](mm),
118 N=[3.0], TP=[5.29]hrs,
119 Continuous simulation parameters:
120 IaRECper=[4](hrs),
121 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
122 InterEventTime=[12](hrs)
123 Baseflow simulation parameters:
124 BaseFlowOption=[1] ,
125 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
126 VHydCond=[0.055](mm/hr), END=-1
127 *%-----|-----|
128 *#
129 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
130 *# of 1.52
131 *%-----|-----|
132 CONTINUOUS NASHYD NHYD= ["SW_10"], DT=[30]min, AREA=[5666](ha),

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133 DWF=[0](cms), CN/C=[72], IA=[2.5](mm),
134 N=[3.0], TP=[8.00]hrs,
135 Continuous simulation parameters:
136 IaRECper=[4](hrs),
137 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
138 InterEventTime=[12](hrs)
139 Baseflow simulation parameters:
140 BaseFlowOption=[1],
141 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
142 VHydCond=[0.055](mm/hr), END=-1
143 *%-----|-----|
144 *#
145 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
146 *# of 1.75
147 *%-----|-----|
148 CONTINUOUS NASHYD NHYD=[ "KG_CK" ], DT=[30]min, AREA=[8376](ha),
149 DWF=[0](cms), CN/C=[66], IA=[2.5](mm),
150 N=[3.0], TP=[11.66]hrs,
151 Continuous simulation parameters:
152 IaRECper=[4](hrs),
153 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
154 InterEventTime=[12](hrs)
155 Baseflow simulation parameters:
156 BaseFlowOption=[1],
157 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
158 VHydCond=[0.055](mm/hr), END=-1
159 *%-----|-----|
160 *#
161 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
162 *# of 1.68
163 *%-----|-----|
164 CONTINUOUS NASHYD NHYD=[ "SW_9" ], DT=[30]min, AREA=[1132](ha),
165 DWF=[0](cms), CN/C=[70], IA=[2.5](mm),
166 N=[3.0], TP=[2.51]hrs,
167 Continuous simulation parameters:
168 IaRECper=[4](hrs),
169 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
170 InterEventTime=[12](hrs)
171 Baseflow simulation parameters:
172 BaseFlowOption=[1],
173 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
174 VHydCond=[0.055](mm/hr), END=-1
175 *%-----|-----|
176 *#
177 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
178 *# of 1.82
179 *%-----|-----|
180 CONTINUOUS NASHYD NHYD=[ "NC_CK" ], DT=[30]min, AREA=[4464](ha),
181 DWF=[0](cms), CN/C=[62], IA=[2.5](mm),
182 N=[3.0], TP=[11.32]hrs,
183 Continuous simulation parameters:
184 IaRECper=[4](hrs),
185 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
186 InterEventTime=[12](hrs)
187 Baseflow simulation parameters:
188 BaseFlowOption=[1],
189 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
190 VHydCond=[0.055](mm/hr), END=-1
191 *%-----|-----|
192 *#
193 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
194 *# of 1.80
195 *%-----|-----|
196 CONTINUOUS NASHYD NHYD=[ "SW_8" ], DT=[30]min, AREA=[131](ha),
197 DWF=[0](cms), CN/C=[63], IA=[2.5](mm),
198 N=[3.0], TP=[0.90]hrs,

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199      Continuous simulation parameters:
200      IaRECper=[4](hrs),
201      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
202      InterEventTime=[12](hrs)
203      Baseflow simulation parameters:
204      BaseFlowOption=[1] ,
205      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
206      VHydCond=[0.055](mm/hr), END=-1
207      *%-----|-----|
208      *#
209      *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
210      *# of 1.65
211      *%-----|-----|
212      CONTINUOUS NASHYD      NHYD=[ "HB_DR" ], DT=[30]min, AREA=[3854](ha),
213      DWF=[0](cms), CN/C=[66], IA=[2.5](mm),
214      N=[3.0], TP=[8.42]hrs,
215      Continuous simulation parameters:
216      IaRECper=[4](hrs),
217      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
218      InterEventTime=[12](hrs)
219      Baseflow simulation parameters:
220      BaseFlowOption=[1] ,
221      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
222      VHydCond=[0.055](mm/hr), END=-1
223      *%-----|-----|
224      *#
225      *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
226      *# of 1.82
227      *%-----|-----|
228      CONTINUOUS NASHYD      NHYD=[ "SW_7" ], DT=[30]min, AREA=[3197](ha),
229      DWF=[0](cms), CN/C=[57], IA=[2.5](mm),
230      N=[3.0], TP=[6.65]hrs,
231      Continuous simulation parameters:
232      IaRECper=[4](hrs),
233      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
234      InterEventTime=[12](hrs)
235      Baseflow simulation parameters:
236      BaseFlowOption=[1] ,
237      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
238      VHydCond=[0.055](mm/hr), END=-1
239      *%-----|-----|
240      *#
241      *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
242      *# of 1.75
243      *%-----|-----|
244      CONTINUOUS NASHYD      NHYD=[ "SW_6" ], DT=[30]min, AREA=[165](ha),
245      DWF=[0](cms), CN/C=[67], IA=[2.5](mm),
246      N=[3.0], TP=[4.18]hrs,
247      Continuous simulation parameters:
248      IaRECper=[4](hrs),
249      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
250      InterEventTime=[12](hrs)
251      Baseflow simulation parameters:
252      BaseFlowOption=[1] ,
253      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
254      VHydCond=[0.055](mm/hr), END=-1
255      *%-----|-----|
256      *#
257      *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
258      *# of 1.67
259      *%-----|-----|
260      CONTINUOUS NASHYD      NHYD=[ "VG_DR" ], DT=[30]min, AREA=[1332](ha),
261      DWF=[0](cms), CN/C=[72], IA=[2.5](mm),
262      N=[3.0], TP=[5.95]hrs,
263      Continuous simulation parameters:
264      IaRECper=[4](hrs),

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265           SMIN=[-1](mm),   SMAX=[-1](mm),   SK=[0.010]/(mm),
266           InterEventTime=[12](hrs)
267           Baseflow simulation parameters:
268           BaseFlowOption=[1] ,
269           InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
270           VHydCond=[0.055](mm/hr),    END=-1
271
272 *%-----| CONTINUOUS NASHYD |-----|
273           NHYD= [ "SW_5" ], DT=[30]min, AREA=[224](ha),
274           DWF=[0](cms),   CN/C=[77],  IA=[2.5](mm),
275           N=[3.0],  TP=[0.75]hrs,
276           Continuous simulation parameters:
277           IaRECper=[4](hrs),
278           SMIN=[-1](mm),   SMAX=[-1](mm),   SK=[0.010]/(mm),
279           InterEventTime=[12](hrs)
280           Baseflow simulation parameters:
281           BaseFlowOption=[1] ,
282           InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
283           VHydCond=[0.055](mm/hr),    END=-1
284
285 *#-----| CONTINUOUS NASHYD |-----|
286 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
287 *# of 1.20
288
289 *%-----| CONTINUOUS NASHYD |-----|
290           NHYD= [ "FL_CK" ], DT=[30]min, AREA=[4945](ha),
291           DWF=[0](cms),   CN/C=[74],  IA=[2.5](mm),
292           N=[3.0],  TP=[4.45]hrs,
293           Continuous simulation parameters:
294           IaRECper=[4](hrs),
295           SMIN=[-1](mm),   SMAX=[-1](mm),   SK=[0.010]/(mm),
296           InterEventTime=[12](hrs)
297           Baseflow simulation parameters:
298           BaseFlowOption=[1] ,
299           InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
300           VHydCond=[0.055](mm/hr),    END=-1
301
302 *%-----| CONTINUOUS NASHYD |-----|
303           NHYD= [ "SW_5A2" ], DT=[30]min, AREA=[20](ha),
304           DWF=[0](cms),   CN/C=[81],  IA=[2.5](mm),
305           N=[3.0],  TP=[0.62]hrs,
306           Continuous simulation parameters:
307           IaRECper=[4](hrs),
308           SMIN=[-1](mm),   SMAX=[-1](mm),   SK=[0.010]/(mm),
309           InterEventTime=[12](hrs)
310           Baseflow simulation parameters:
311           BaseFlowOption=[1] ,
312           InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
313           VHydCond=[0.055](mm/hr),    END=-1
314
315 *#-----| CONTINUOUS NASHYD |-----|
316 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
317 *# of 1.61
318
319 *%-----| CONTINUOUS NASHYD |-----|
320           NHYD= [ "SW_5A1" ], DT=[30]min, AREA=[1412](ha),
321           DWF=[0](cms),   CN/C=[75],  IA=[2.5](mm),
322           N=[3.0],  TP=[8.00]hrs,
323           Continuous simulation parameters:
324           IaRECper=[4](hrs),
325           SMIN=[-1](mm),   SMAX=[-1](mm),   SK=[0.010]/(mm),
326           InterEventTime=[12](hrs)
327           Baseflow simulation parameters:
328           BaseFlowOption=[1] ,
329           InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
330           VHydCond=[0.055](mm/hr),    END=-1
331
332 *%-----| CONTINUOUS NASHYD |-----|
333           NHYD= [ "SW_4" ], DT=[30]min, AREA=[585](ha),
334           DWF=[0](cms),   CN/C=[81],  IA=[2.5](mm),
335           N=[3.0],  TP=[1.75]hrs,

```

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331           Continuous simulation parameters:
332           IaRECper=[4](hrs),
333           SMIN=[-1](mm),   SMAX=[-1](mm),   SK=[0.010]/(mm),
334           InterEventTime=[12](hrs)
335           Baseflow simulation parameters:
336           BaseFlowOption=[1] ,
337           InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
338           VHydCond=[0.055](mm/hr),   END=-1
339
340 *%-----| CONTINUOUS NASHYD
341           NHYD= ["LM_CK"], DT=[30]min, AREA=[1021](ha),
342           DWF=[0](cms),   CN/C=[80],  IA=[2.5](mm),
343           N=[3.0],  TP=[2.46]hrs,
344           Continuous simulation parameters:
345           IaRECper=[4](hrs),
346           SMIN=[-1](mm),   SMAX=[-1](mm),   SK=[0.010]/(mm),
347           InterEventTime=[12](hrs)
348           Baseflow simulation parameters:
349           BaseFlowOption=[1] ,
350           InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
351           VHydCond=[0.055](mm/hr),   END=-1
352
353 *%-----| CONTINUOUS NASHYD
354           NHYD= ["SW_2"], DT=[30]min, AREA=[177](ha),
355           DWF=[0](cms),   CN/C=[77],  IA=[2.5](mm),
356           N=[3.0],  TP=[0.75]hrs,
357           Continuous simulation parameters:
358           IaRECper=[4](hrs),
359           SMIN=[-1](mm),   SMAX=[-1](mm),   SK=[0.010]/(mm),
360           InterEventTime=[12](hrs)
361           Baseflow simulation parameters:
362           BaseFlowOption=[1] ,
363           InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
364
365 *%-----| CONTINUOUS NASHYD
366           NHYD= ["SM_DR"], DT=[30]min, AREA=[1122](ha),
367           DWF=[0](cms),   CN/C=[81],  IA=[2.5](mm),
368           N=[3.0],  TP=[3.25]hrs,
369           Continuous simulation parameters:
370           IaRECper=[4](hrs),
371           SMIN=[-1](mm),   SMAX=[-1](mm),   SK=[0.010]/(mm),
372           InterEventTime=[12](hrs)
373           Baseflow simulation parameters:
374           BaseFlowOption=[1] ,
375           InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
376
377 *%-----| CONTINUOUS NASHYD
378           NHYD= ["MO_DR"], DT=[30]min, AREA=[2737](ha),
379           DWF=[0](cms),   CN/C=[76],  IA=[2.5](mm),
380           N=[3.0],  TP=[3.03]hrs,
381           Continuous simulation parameters:
382           IaRECper=[4](hrs),
383           SMIN=[-1](mm),   SMAX=[-1](mm),   SK=[0.010]/(mm),
384           InterEventTime=[12](hrs)
385           Baseflow simulation parameters:
386           BaseFlowOption=[1] ,
387           InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
388
389 *%-----| CONTINUOUS NASHYD
390           NHYD= ["SW_1"], DT=[30]min, AREA=[3176](ha),
391           DWF=[0](cms),   CN/C=[78],  IA=[2.5](mm),
392           N=[3.0],  TP=[3.56]hrs,
393           Continuous simulation parameters:
394           IaRECper=[4](hrs),
395           SMIN=[-1](mm),   SMAX=[-1](mm),   SK=[0.010]/(mm),
396           InterEventTime=[12](hrs)
397           Baseflow simulation parameters:
398           BaseFlowOption=[1] ,

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397           InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
398           VHydCond=[0.055](mm/hr), END=-1
399 *%-----|-----|
400 *#
401 *# Routing hydrographs
402 *#
403 *# Starting with the addition of Jock River Headwater and Subwatershed 13
404 *#
405 ADD HYD          NHYDsum=[ "S_N13" ], NHYDs to add=[ "JR_HW"+"SW_13" ]
406 *%-----|-----|
407 *#
408 *# Sum of hydrographs from Node 13 routed to Node 13A
409 *# (Approximated cross-section - see cross-section 258)
410 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
411 *#
412 ROUTE CHANNEL      NHYDout=[ "N13A" ] ,NHYDin=[ "S_N13" ],
413             RDT=[30](min),
414             CHLNGTH=[9074](m), CHSLOPE=[0.0220](%),
415             FPSLOPE=[0.0220](%),
416             SECNUM=[1.0], NSEG=[1]
417             ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
418             ( DISTANCE (m), ELEVATION (m)=
419                 [-40, 132.5]
420                 [-30, 132]
421                 [-25, 131.5]
422                 [-13, 130]
423                 [-8, 127.00]
424                 [-7, 126.50]
425                 [-6, 126]
426                 [-5.5, 125.50]
427                 [0, 123.75]
428                 [4.5, 125.50]
429                 [6, 126]
430                 [7.5, 126.5]
431                 [9, 127]
432                 [10, 127.5]
433                 [11.5, 128.0]
434                 [15.5, 129.5]
435 *%-----|-----|
436 *#
437 *# Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
438 *#
439 ADD HYD          NHYDsum=[ "SN13A" ], NHYDs to add=[ "N13A"+"JR_GWM" ]
440 *%-----|-----|
441 *#
442 *# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
443 *#
444 ROUTE RESERVOIR   NHYDout=[ "RES_GM" ] ,NHYDin=[ "SN13A" ],
445             RDT=[30](min),
446             TABLE of ( OUTFLOW-STORAGE ) values
447             (cms) - (ha-m)
448             [ 0.0 , 0.0 ]
449             [1.991, 2.144    ]
450             [2.693, 39.826   ]
451             [3.509, 81.697   ]
452             [4.578, 318.774   ]
453             [5.647, 594.947   ]
454             [7.109, 910.219   ]
455             [8.616, 1264.589   ]
456             [10.371, 1658.057   ]
457             [12.402, 2090.622   ]
458             [22.056, 3462.487   ]
459             [ -1 , -1 ] (max twenty pts)
460             NHYDovf=[ " " ] ,
461 *%-----|-----|
462 *#

```

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463  SAVE HYD          NHYD=[ "RES_GM" ] , # OF PCYCLES=[ -1 ] , ICASEsh=[ -1 ]
464
465          HYD_FILENAME=[ "H_ESGM" ]
466          HYD_COMMENT=[ "Outflow from Res GM" ]
467 *%-----|-----|
468 *# Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
469 *# (Approximated cross-section - see cross-section 258)
470 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
471 ROUTE CHANNEL      NHYDout=[ "N12" ] , NHYDin=[ "RES_GM" ] ,
472          RDT=[ 30 ](min) ,
473          CHLGTH=[ 5926 ](m) , CHSLOPE=[ 0.0759 ](%) ,
474          FPSLOPE=[ 0.0759 ](%) ,
475          SECNUM=[ 1.0 ] , NSEG=[ 1 ]
476          ( SEGROUGH, SEGDIST (m) )=[ 0.04, 15.5 ] NSEG times
477          ( DISTANCE (m) , ELEVATION (m) )=
478              [-40, 132.5]
479              [-30, 132]
480              [-25, 131.5]
481              [-13, 130]
482              [-8, 127.00]
483              [-7, 126.50]
484              [-6, 126]
485              [-5.5, 125.50]
486              [0, 123.75]
487              [4.5, 125.50]
488              [6, 126]
489              [7.5, 126.5]
490              [9, 127]
491              [10, 127.5]
492              [11.5, 128.00]
493              [15.5, 129.5]
494 *%-----|-----|
495 *#
496 *# Addition of Subwatershed Jock River at Ashton to Node 12
497 *#
498 ADD HYD           NHYDsum=[ "S_N12" ] , NHYDs to add=[ "N12" + "JR_ASH" ]
499 SAVE HYD          NHYD=[ "S_N12" ] , # OF PCYCLES=[ -1 ] , ICASEsh=[ -1 ]
500          HYD_FILENAME=[ "H_SN12" ]
501          HYD_COMMENT=[ "flow at S_N12 near Ashton" ]
502 *%-----|-----|
503 *#
504 *# Sum of hydrographs from Node 12 routed to Node 11
505 *# (Approximated cross-section - see cross-section 258)
506 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
507 ROUTE CHANNEL      NHYDout=[ "N11" ] , NHYDin=[ "S_N12" ] ,
508          RDT=[ 30 ](min) ,
509          CHLGTH=[ 972 ](m) , CHSLOPE=[ 0.0514 ](%) ,
510          FPSLOPE=[ 0.0514 ](%) ,
511          SECNUM=[ 1.0 ] , NSEG=[ 1 ]
512          ( SEGROUGH, SEGDIST (m) )=[ 0.04, 15.5 ] NSEG times
513          ( DISTANCE (m) , ELEVATION (m) )=
514              [-40, 132.5]
515              [-30, 132]
516              [-25, 131.5]
517              [-13, 130]
518              [-8, 127.00]
519              [-7, 126.50]
520              [-6, 126]
521              [-5.5, 125.50]
522              [0, 123.75]
523              [4.5, 125.50]
524              [6, 126]
525              [7.5, 126.5]
526              [9, 127]
527              [10, 127.5]
528              [11.5, 128.00]
529              [15.5, 129.5]

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```

529 *-----|-----|
530 *#
531 *# Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
532 *#
533 ROUTE CHANNEL      NHYDout=[ "Dum11" ] , NHYDin=[ "S_N12" ] ,
534          RDT=[ 30 ](min),
535          CHLNGTH=[ 972 ](m),   CHSLOPE=[ 0.054 ](%),
536          FPSLOPE=[ 0.054 ](%),
537          SECNUM=[ 1.0 ],       NSEG=[ 1 ]
538          ( SEGROUGH, SEGDIST (m) )=[ 0.04, 15.5 ] NSEG times
539          ( DISTANCE (m), ELEVATION (m) )=
540          [ -40, 132.5 ]
541          [ -30, 132 ]
542          [ -25, 131.5 ]
543          [ -13, 130 ]
544          [ -8, 127.00 ]
545          [ -7, 126.50 ]
546          [ -6, 126 ]
547          [ -5.5, 125.50 ]
548          [ 0, 123.75 ]
549          [ 4.5, 125.50 ]
550          [ 6, 126 ]
551          [ 7.5, 126.5 ]
552          [ 9, 127 ]
553          [ 10, 127.5 ]
554          [ 11.5, 128.00 ]
555          [ 15.5, 129.5 ]
556 *-----|-----|
557 *#
558 *# Addition of Subwatershed 11 and No Name Creek to Node 11
559 *#
560 ADD HYD           NHYDsum=[ "S_N11" ], NHYDs to add=[ "Dum11"+ "SW_11" + "NN_CK" ]
561 *-----|-----|
562 *#
563 *# Sum of hydrographs from Node 11 routed to Node 10
564 *# Section 1
565 *#
566 ROUTE CHANNEL      NHYDout=[ "N10" ] , NHYDin=[ "S_N11" ] ,
567          RDT=[ 30 ](min),
568          CHLNGTH=[ 14028 ](m),   CHSLOPE=[ 0.1568 ](%),
569          FPSLOPE=[ 0.1568 ](%),
570          SECNUM=[ 1.0 ],       NSEG=[ 5 ]
571          ( SEGROUGH, SEGDIST (m) )=
572          [ 0.04,-52.82
573          0.1,-6.47
574          -0.05,6.47
575          0.1,45.36
576          0.04,423.88 ] NSEG times
577          ( DISTANCE (m), ELEVATION (m) )=
578          [ -226.24 ,112.50 ]
579          [ -167.50 ,111.50 ]
580          [ -106.81 ,111.00 ]
581          [ -92.37 ,110.00 ]
582          [ -52.82 ,109.00 ]
583          [ -24.90 ,109.00 ]
584          [ -17.02, 108.50 ]
585          [ -6.47, 108.00 ]
586          [ 6.47, 108.00 ]
587          [ 15.67, 108.50 ]
588          [ 18.95, 109.00 ]
589          [ 45.36, 109.50 ]
590          [ 120.79, 110.00 ]
591          [ 145.72, 111.00 ]
592          [ 181.56, 111.50 ]
593          [ 423.88, 112.50 ]
594 *-----|-----|

```



```

661          ( DISTANCE (m) , ELEVATION (m))=
662              [-201.19,100.50]
663              [-135.21, 100.00]
664              [-94.83, 99.50]
665              [-67.05, 99.00]
666              [-17.99, 98.50]
667              [-16.02, 98.00]
668              [-13.95, 97.50]
669              [13.95, 97.50]
670              [15.64, 98.00]
671              [17.31, 98.50]
672              [162.02, 98.50]
673              [172.89 ,99.00]
674              [314.38, 99.00]
675              [343.78, 99.50]
676              [365.67, 100.00]
677              [376.68, 100.00 ]
678              [393.11, 99.50]
679              [404.97, 99.50]
680              [431.70, 100.00]
681              [456.58, 100.50 ]
682 *%-----|-----|-----|
683 *#
684 *# Addition of Subwatershed 8 and Hobb's Drain to Node 8
685 *#
686 ADD HYD           NHYDsum=[ "S_N8" ] , NHYDs to add=[ "N8 "+"SW_8 "+"HB_DR" ]
687 *%-----|-----|-----|
688 *#
689 *# Sum of hydrographs from Node 8 routed to Node 7
690 *# Section 4
691 *#
692 ROUTE CHANNEL      NHYDout=[ "N7" ] ,NHYDin=[ "S_N8" ] ,
693             RDT=[30](min),
694             CHLGTH=[3750](m),   CHSLOPE=[0.0533](%),
695                           FPSLOPE=[0.0533](%),
696             SECNUM=[1.0] ,          NSEG=[3]
697             ( SEGROUGH, SEGDIST (m))=
698                 [0.12,-18.11
699                  -0.07,17.22
700                  0.12,590.05] NSEG times
701             ( DISTANCE (m) , ELEVATION (m))=
702                 [-433.21, 102.00]
703                 [-425.34, 101.50]
704                 [-377.56, 101.50]
705                 [-366.23, 101.00]
706                 [-202.60, 100.50]
707                 [-96.25, 99.50]
708                 [-68.36 99.00]
709                 [-18.11, 98.50]
710                 [-13.81, 97.50]
711                 [13.81, 97.50]
712                 [17.22, 98.50]
713                 [161.95, 98.50]
714                 [173.11, 99.00]
715                 [314.05, 99.00]
716                 [365.52, 100.00]
717                 [404.70, 99.50]
718                 [476.74, 100.50]
719                 [502.31, 101.00]
720                 [584.69, 101.00]
721                 [585.79, 101.00]
722                 [590.05, 102.00]
723 *%-----|-----|-----|
724 *#
725 *# Addition of Subwatershed 7 to Node 7
726 *#

```

```

727 ADD HYD           NHYDsum=[ "S_N7" ] , NHYDs to add=[ "N7" +"SW_7" ]
728 *%
729 SAVE HYD          NHYD=[ "S_N7" ] , # OF PCYCLES=[ -1 ] , ICASEsh=[ -1 ]
730             HYD_FILENAME=[ "H_SN7" ]
731             HYD_COMMENT=[ "flow at S_N7: N7 + SW_7" ]
732 *%
733 *# Insertion of a reservoir to simulate the effects of the Richmond Fen.
734 *# Storage area and volumes were estimated from available topo maps.
735 *# Release rate from fen was assumed to be controlled by the downstream
736 *# river cross-section for summer conditions. It is was assumed that for up to
737 *# 0.75 m of water, the main channel of the river provided the storage. Above
738 *# this depth, the wetland starts to signigicantly store water.
739 *#
740 ROUTE RESERVOIR   NHYDout=[ "RES_RF" ] , NHYDin=[ "S_N7" ] ,
741             RDT=[ 30 ](min),
742                 TABLE of ( OUTFLOW-STORAGE ) values
743                     (cms) - (ha-m)
744                 TABLE of ( OUTFLOW-STORAGE ) values
745                     (cms) - (ha-m)
746                     [ 0.0 , 0.0 ]
747                     [ 0.9051 , 2.40 ]
748                     [ 2.907 , 4.13 ]
749                     [ 9.744 , 9.18 ]
750                     [ 20.304 , 14.96 ]
751                     [ 34.167 , 310.21 ]
752                     [ 74.993 , 605.46 ]
753                     [ 104.876 , 900.71 ]
754                     [ 140.56 , 2892.00 ]
755                     [ 225.00 , 3615.63 ]
756                     [ -1 , -1 ] (max twenty pts)
757             NHYDovf=[ " " ] ,
758 *%
759 SAVE HYD          NHYD=[ "RES_RF" ] , # OF PCYCLES=[ -1 ] , ICASEsh=[ -1 ]
760             HYD_FILENAME=[ "H_ResRF" ]
761             HYD_COMMENT=[ "outflow of Richmond Fen" ]
762 *%
763 *#
764 *# Sum of hydrographs from Node 7 routed to Node 6
765 *# Section 5
766 *#
767 ROUTE CHANNEL      NHYDout=[ "N6" ] , NHYDin=[ "RES_RF" ] ,
768             RDT=[ 30 ](min),
769             CHLGH= [ 3056 ](m) , CHSLOPE=[ 0.0818 ](%),
770                     FPSLOPE=[ 0.0818 ](%),
771             SECNUM=[ 1.0 ] , NSEG=[ 5 ]
772             ( SEGRROUGH , SEGDIST (m))=
773                 [ 0.025 , -70.8
774                 0.1 , -23.9
775                 -0.05 , 23.9
776                 0.06 , 39.8
777                 0.05 , 96.3 ] NSEG times
778             ( DISTANCE (m) , ELEVATION (m))=
779                 [ -100.8 , 97.00 ]
780                 [ -70.8 , 96.50 ]
781                 [ -52.0 , 96.00 ]
782                 [ -35.1 , 95.50 ]
783                 [ -30.6 , 95.00 ]
784                 [ -23.9 , 94.54 ]
785                 [ 23.9 , 94.54 ]
786                 [ 39.8 , 95.00 ]
787                 [ 50.4 , 95.50 ]
788                 [ 93.5 , 96.00 ]
789                 [ 94.9 , 96.50 ]
790                 [ 96.3 , 97.00 ]
791 *%
792 *#

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793 *# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
794 *#
795 ADD HYD           NHYDsum=[ "S_N6" ] , NHYDs to add= [ "N6" +"SW_6" +"VG_DR" ]
796 *%-----|-----|
797 *#
798 *# Sum of hydrographs from Node 6 routed to Node 5
799 *# Section 6
800 *#
801 ROUTE CHANNEL      NHYDout=[ "N5" ] , NHYDin=[ "S_N6" ] ,
802                         RDT=[ 30 ](min) ,
803                         CHLGTH=[ 1852 ](m) , CHSLOPE=[ 0.0540 ](%) ,
804                                         FPSLOPE=[ 0.0540 ](%) ,
805                         SECNUM=[ 1.0 ] , NSEG=[ 3 ]
806                         ( SEGROUGH, SEGDIST (m))=
807                             [ 0.035, -131.59
808                                 -0.045, 48.96
809                                     0.1, 239.04] NSEG times
810                         ( DISTANCE (m) , ELEVATION (m))=
811                             [ -686.30, 94.50]
812                             [ -675.70, 94.00]
813                             [ -492.52, 93.00]
814                             [ -467.28, 94.00]
815                             [ -131.59, 94.00]
816                             [ -92.79, 92.50]
817                             [ -18.06, 91.00]
818                             [ 18.06, 91.00]
819                             [ 43.47, 92.50]
820                             [ 48.96, 94.00]
821                             [ 177.43, 94.00]
822                             [ 239.04, 94.50]
823 *%-----|-----|
824 *#
825 *# Addition of Subwatershed 5 and Flowing Creek to Node 5
826 *#
827 ADD HYD           NHYDsum=[ "S_N5" ] , NHYDs to add= [ "N5" +"SW_5" +"FL_CK" ]
828 *%-----|-----|
829 *#
830 *# Sum of hydrographs from Node 5 routed to Node 5A
831 *# Section 7
832 *#
833 ROUTE CHANNEL      NHYDout=[ "N5A" ] , NHYDin=[ "S_N5" ] ,
834                         RDT=[ 30 ](min) ,
835                         CHLGTH=[ 556 ](m) , CHSLOPE=[ 0.0900 ](%) ,
836                                         FPSLOPE=[ 0.0900 ](%) ,
837                         SECNUM=[ 1.0 ] , NSEG=[ 4 ]
838                         ( SEGROUGH, SEGDIST (m))=
839                             [ 0.04, -41.5
840                                 0.1, -14.0
841                                     -0.045, 14.0
842                                         0.1, 41.1] NSEG times
843                         ( DISTANCE (m) , ELEVATION (m))=
844                             [ -275.8, 93.00]
845                             [ -248.6, 92.50]
846                             [ -237.0, 92.00]
847                             [ -219.3, 91.50]
848                             [ -202.1, 91.50]
849                             [ -186.0, 92.00]
850                             [ -129.2, 92.00]
851                             [ -117.6, 91.50]
852                             [ -100.6, 91.00]
853                             [ -41.5, 91.00]
854                             [ -20.0, 91.00]
855                             [ -14.0, 90.54]
856                             [ 14.0, 90.54]
857                             [ 15.3, 91.00]
858                             [ 17.3, 91.50]

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```

859                               [ 38.4,  92.00]
860                               [ 39.8,  92.50]
861                               [ 41.1,  93.00]
862 *%-----|-----|
863 *#
864 *# Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
865 *#
866 ADD HYD          NHYDsum=[ "S_N5A" ] , NHYDs to add=[ "N5A"+"SW_5A2"+"SW_5A1" ]
867 *%-----|-----|
868 *#
869 *# Sum of hydrographs from Node 5A routed to Node 4
870 *# Section 8
871 *#
872 ROUTE CHANNEL      NHYDout=[ "N4" ] , NHYDin=[ "S_N5A" ] ,
873             RDT=[ 30 ](min),
874             CHLGTH=[ 4630 ](m),   CHSLOPE=[ 0.0432 ](%),
875                               FPSLOPE=[ 0.0432 ](%),
876             SECNUM=[ 1.0 ],        NSEG=[ 3 ]
877             ( SEGROUGH, SEGDIST (m))=
878                 [ 0.05,-28.2
879                 -0.035,28.2
880                 0.05,173.1] NSEG times
881             ( DISTANCE (m), ELEVATION (m))=
882                 [ -38.9, 92.00]
883                 [ -35.8, 91.50]
884                 [ -33.3, 91.00]
885                 [ -28.2, 90.50]
886                 [ -15.0, 87.48]
887                 [ -5.0, 88.34]
888                 [ 5.0, 86.20]
889                 [ 15.0, 88.55]
890                 [ 28.2, 90.50]
891                 [ 29.7, 91.00]
892                 [ 46.5, 91.00]
893                 [ 127.8, 91.00]
894                 [ 148.7, 91.50]
895                 [ 173.1, 92.00]
896 *%-----|-----|
897 *#
898 *# Addition of Subwatershed 4 and Leamy Creek to Node 4
899 *#
900 ADD HYD          NHYDsum=[ "S_N4" ] , NHYDs to add=[ "N4"+"SW_4"+"LM_CK" ]
901 SAVE HYD          NHYD=[ "S_N4" ] , # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
902             HYD_COMMENT=[ "flow at S_N4" ]
903 *%-----|-----|
904 *#
905 *# Sum of hydrographs from Node 4 routed to Node 2
906 *# Section 9
907 *#
908 ROUTE CHANNEL      NHYDout=[ "N2" ] , NHYDin=[ "S_N4" ] ,
909             RDT=[ 30 ](min),
910             CHLGTH=[ 1667 ](m),   CHSLOPE=[ 0.0600 ](%),
911                               FPSLOPE=[ 0.0600 ](%),
912             SECNUM=[ 1.0 ],        NSEG=[ 4 ]
913             ( SEGROUGH, SEGDIST (m))=
914                 [ 0.1,-28.0
915                 -0.04,28.4
916                 0.06,31.7
917                 0.04,80.2] NSEG times
918             ( DISTANCE (m), ELEVATION (m))=
919                 [ -36.3, 92.00]
920                 [ -32.6, 91.50]
921                 [ -30.2, 91.00]
922                 [ -28.0, 90.45]
923                 [ -15.0, 87.48]
924                 [ -5.0, 88.34]

```

```

925 [5.0, 86.20]
926 [15.0, 88.55]
927 [28.0, 90.45]
928 [28.4, 90.50]
929 [30.4, 91.00]
930 [31.7, 91.50]
931 [80.2, 92.00]
932 *%-----|-----|
933 *#
934 *# Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2
935 *#
936 ADD HYD NHYDsum=[ "S_N2" ], NHYDs to add=[ "N2"+"SW_2"+"SM_DR"+"MO_DR" ]
937 *%-----|-----|
938 SAVE HYD NHYD=[ "S_N2" ], # OF PCYCLES=[-1], ICASEsh=[-1]
939 HYD_FILENAME=[ "H_SN2" ]
940 HYD_COMMENT=[ "flow at S_N2 Jock River Gauge at Moodie Dr." ]
941 *%-----|-----|
942 *#
943 *# Sum of hydrographs from Node 2 routed to Node 1
944 *# Section 10
945 *#
946 ROUTE CHANNEL NHYDout=[ "N1" ] ,NHYDin=[ "S_N2" ] ,
947 RDT=[30](min),
948 CHLGTH=[10046](m), CHSLOPE=[0.0498](%),
949 FPSLOPE=[0.0498](%),
950 SECNUM=[1.0], NSEG=[5]
951 ( SEGROUGH, SEGDIST (m))=
952 [0.04,-27.6
953 0.06,-15.0
954 -0.045,15.0
955 0.06,25.4
956 0.04,122.6] NSEG times
957 ( DISTANCE (m), ELEVATION (m))=
958 [-87.0, 91.50]
959 [-32.4, 91.00]
960 [-27.6, 90.50]
961 [-25.0, 90.00]
962 [-22.9, 89.57]
963 [-15.0, 86.20]
964 [-5.0, 84.83]
965 [5.0, 84.83]
966 [15.0, 88.11]
967 [22.9, 89.57]
968 [25.4, 90.00]
969 [27.9, 90.50]
970 [38.0, 91.00]
971 [112.5, 91.00]
972 [114.3, 90.50]
973 [115.1, 90.26]
974 [116.3, 90.50]
975 [119.0, 91.00]
976 [121.0, 91.50]
977 [122.6, 92.00]
978 *%-----|-----|
979 *#
980 *# Addition of Subwatershed 1 to Node 1
981 *#
982 ADD HYD NHYDsum=[ "N1" ], NHYDs to add=[ "N1"+"SW_1" ]
983 SAVE HYD NHYD=[ "N1" ], # OF PCYCLES=[-1], ICASEsh=[1]
984 HYD_COMMENT=[ "total outflow of Jock River" ]
985 *%-----|-----|
986 #####5 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
987 *% 5 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
988 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[5]
989 *% [ "C24SC005.stm" ] <--storm filename, one per line for NSTORM time
990 *%-----|-----|

```

```
991 *% 10 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
992 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[10]
993 *%
994 *%-----|-----|-----|-----|-----|-----|
995 *% 25 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
996 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[25]
997 *%
998 *%-----|-----|-----|-----|-----|
999 *% 50 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
1000 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[50]
1001 *%
1002 *%-----|-----|-----|-----|-----|
1003 *% 100 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
1004 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
1005 *%
1006 FINISH
1007
```

00001+ =====

00002+ =====

00003+ SSSSS W W M M H H Y Y M M 000 222 000 11 5555 =====

00004+ S W W N M M M H H Y Y M M 0 0 2 0 0 0 11 5 . . . . .

00005+ SSSSS W W M M M H H Y Y M M 0 0 2 0 0 0 11 555 FEB 2015

00006+ S W W M M H H Y M M 000 222 0 0 0 11 555 FEB 2015

00007+ SSSSS W W M M H H Y M M 000 2 0 0 0 11 5 . . . . .

00008+ StormWater Management Hydrologic Model 222 000 11 455 =====

00009+ =====

00010+ =====

00011+ \*\*\*\*\* SWHMHYMO Ver. 5.600 \*\*\*

00012+ \*\*\*\*\* A single event and continuous hydrologic simulation model

00013+ \*\*\*\*\* based on the SWHM model and its successors

00014+ \*\*\*\*\* OTNHYMO-83 and CTHHYMO-89. \*\*\*

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00023+ \*\*\*\*\* Licensed user: JFSAinc. Ottawa SERIAL#=2549237 \*\*\*\*

00024+ =====

00025+ =====

00026+ =====

00027+ =====

00028+ =====

00029+ \*\*\*\*\* PROGRAM ARRAY DIMENSIONS \*\*\*\*\*

00030+ \*\*\*\*\* Maximum value of ID numbers : 11 \*\*\*\*\*

00031+ \*\*\*\*\* Max. number of rainfall points: 105408 \*\*\*\*\*

00032+ \*\*\*\*\* Max. number of output points: 105408 \*\*\*\*\*

00033+ \*\*\*\*\*

00034+ =====

00035+ =====

00036+ \*\*\*\*\* S U M M A R Y O U T P U T \*\*\*\*\*

00037+ \*\*\*\*\*

00038+ \*\*\*\*\* RUN DATE: 2021-02-22 TIME: 15:43:08 RUN COUNT: 001996

00039+ \*\*\*\*\*

00040+ \* Input file: T:\PROJ\1474-16\Design\20201026\QuantityControl\Analysis\SWMHYMO\SMR\Model\summer.\*

00041+ \* Output file: T:\PROJ\1474-16\Design\20201026\QuantityControl\Analysis\SWMHYMO\SMR\Model\summer.\*

00042+ \* Summary file: T:\PROJ\1474-16\Design\20201026\QuantityControl\Analysis\SWMHYMO\SMR\Model\summer.\*

00043+ \* sum

00044+ \* User comments:

00045+ \* 2:

00046+ \* 3:

00047+ \* 4:

00048+ \* 5:

00049+ \* 6:

00050+ \* 7:

00051+ \* 8:

00052+ \* 9:

00053+ \* 10:

00054+ \* SWMHYMO Ver.5.02/Jan 2001 <BETA> / INPUT DATA FILE

00055+ \* Project Name: [Rock River] Project Number: (411-02)

00056+ \* Date: 06-06-2003

00057+ \* Modeler: [JFSAinc]

00058+ \* Company: [JFSAinc]

00059+ \* License #: 2549237

00060+ =====

00061+ # CALIBRATION OF SUMMER MODEL PARAMETERS

00062+ # USING CONTINUOUS SIMULATIONS

00063+ # Rainfall data from gauges installed at site + other gauges by the City

00064+ # Rainfall data recorded from May 1st to July 14, 2003

00065+ #

00066+ \*\* END OF RUN : 1

00067+ =====

00068+ =====

00069+ =====

00070+ =====

00071+ =====

00072+ =====

00073+ =====

00074+ =====

00075+ RINN=COMMAND#

00076+ R0021:CO0001:0001

00077+ START

00078+ [\*TZERO = 2.00 hrs on 01

00079+ [\*TMAX = 24.00 hrs on 01

00080+ [\*NSTORM= 1 ]

00081+ [\*NRUN = 0002 ]

00082+ =====

00083+ # SWMHYMO Ver.5.02/Jan 2001 <BETA> / INPUT DATA FILE

00084+ \* Project Name: [Rock River] Project Number: (411-02)

00085+ \* Date: 06-06-2003

00086+ \* Modeler: [JFSAinc]

00087+ \* Company: [JFSAinc]

00088+ \* License #: 2549237

00089+ # CALIBRATION OF SUMMER MODEL PARAMETERS

00090+ # USING CONTINUOUS SIMULATIONS

00091+ # Rainfall data from gauges installed at site + other gauges by the City

00092+ # Rainfall data recorded from May 1st to July 14, 2003

00093+ #

00094+ =====

00095+ # SWMHYMO Ver.5.02/Jan 2001 <BETA> / INPUT DATA FILE

00096+ \* Project Name: [Rock River] Project Number: (411-02)

00097+ \* Date: 06-06-2003

00098+ \* Modeler: [JFSAinc]

00099+ \* Company: [JFSAinc]

00100+ \* License #: 2549237

00101+ #

00102+ # CALIBRATION OF SUMMER MODEL PARAMETERS

00103+ # USING CONTINUOUS SIMULATIONS

00104+ # Rainfall data from gauges installed at site + other gauges by the City

00105+ # Rainfall data recorded from May 1st to July 14, 2003

00106+ #

00107+ =====

00108+ # READ STORM

00109+ # Filename = storm.001

00110+ # Subwatershed file for 24 hours 1-2 sams pour Ottawa CDA

00111+ # [SUT=10.000000 24.00.PPTD= 45.51]

00112+ R0021:CO0005:0001

00113+ #

00114+ # [RFACT= 1.00:TSHFT= 960.00 min]

00115+ # [SUT=10.00:SOUR= 40.00:PPTD= 45.51]

00116+ R0021:CO0005:0002

00117+ # COMPUTE API

00118+ # [APIMin= 50.00: APIMax= 8500: APIdxt= 9989]

00119+ # [APIMin= 80.12: APIdxt= 56.74: APImax= 44.87]

00120+ #

00121+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00122+ # of 1.62

00123+ R0021:CO0005:0003

00124+ # CONTINUOUS HSMHDY . . . . .

00125+ # [CN= 64.00: NO\_3: 0.00: TP= 45.51]

00126+ # [TaEBC= 4.00: SMIN= 57.05: SMAX=380.10: SK= .010]

00127+ # [InterEventTime= 12.00]

00128+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00129+ # of 1.80

00130+ R0021:CO0005:0004

00131+ # CONTINUOUS HSMHDY . . . . .

00132+ # [CN= 55.00: NO\_3: 0.00: TP= 11.33]

00133+ # [TaEBC= 4.00: SMIN= 59.75: SMAX=554.96: SK= .010]

00134+ # [InterEventTime= 12.00]

00135+ R0021:CO0008:0001

00136+ # CONTINUOUS HSMHDY . . . . .

00137+ # [CN= 66.00: NO\_3: 0.00: TP= 24.00]

00138+ # [TaEBC= 4.00: SMIN= 62.00: SMAX=350.79: SK= .010]

00139+ # [InterEventTime= 12.00]

00140+ R0021:CO0008:0002

00141+ # CONTINUOUS HSMHDY . . . . .

00142+ # [CN= 66.00: NO\_3: 0.00: TP= 24.00]

00143+ # [TaEBC= 4.00: SMIN= 62.00: SMAX=350.79: SK= .010]

00144+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00145+ # of 1.80

00146+ R0021:CO0008:0003

00147+ # CONTINUOUS HSMHDY . . . . .

00148+ # [CN= 66.00: NO\_3: 0.00: TP= 5.29]

00149+ # [TaEBC= 4.00: SMIN= 61.00: SMAX=61.61]

00150+ # [InterEventTime= 12.00]

00151+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00152+ # of 1.52

00153+ R0021:CO0011:0001

00154+ # CONTINUOUS HSMHDY . . . . .

00155+ # [CN= 66.00: NO\_3: 0.00: TP= 10.93]

00156+ # [TaEBC= 4.00: SMIN= 66.00: SMAX=350.79: SK= .000]

00157+ # [InterEventTime= 12.00]

00158+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00159+ # of 1.80

00160+ R0021:CO0011:0002

00161+ # CONTINUOUS HSMHDY . . . . .

00162+ # [CN= 66.00: NO\_3: 0.00: TP= 8.00]

00163+ # [TaEBC= 4.00: SMIN= 39.75: SMAX=264.99: SK= .010]

00164+ # [InterEventTime= 12.00]

00165+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00166+ # of 1.80

00167+ R0021:CO0011:0003

00168+ # CONTINUOUS HSMHDY . . . . .

00169+ # [CN= 66.00: NO\_3: 0.00: TP= 11.33]

00170+ # [TaEBC= 4.00: SMIN= 61.00: SMAX=412.66: SK= .010]

00171+ # [InterEventTime= 12.00]

00172+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00173+ # of 1.80

00174+ R0021:CO0015:0001

00175+ # CONTINUOUS HSMHDY . . . . .

00176+ # [CN= 66.00: NO\_3: 0.00: TP= 11.33]

00177+ # [TaEBC= 4.00: SMIN= 61.00: SMAX=350.79: SK= .000]

00178+ # [InterEventTime= 12.00]

00179+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00180+ # of 1.80

00181+ R0021:CO0015:0002

00182+ # CONTINUOUS HSMHDY . . . . .

00183+ # [CN= 66.00: NO\_3: 0.00: TP= 11.33]

00184+ # [TaEBC= 4.00: SMIN= 61.00: SMAX=350.79: SK= .000]

00185+ # [InterEventTime= 12.00]

00186+ R0021:CO0015:0003

00187+ # CONTINUOUS HSMHDY . . . . .

00188+ # [CN= 66.00: NO\_3: 0.00: TP= 11.33]

00189+ # [TaEBC= 4.00: SMIN= 61.00: SMAX=350.79: SK= .000]

00190+ # [InterEventTime= 12.00]

00191+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00192+ # of 1.62

00193+ R0021:CO0015:0004

00194+ # CONTINUOUS HSMHDY . . . . .

00195+ # [CN= 66.00: NO\_3: 0.00: TP= 11.33]

00196+ # [TaEBC= 4.00: SMIN= 61.00: SMAX=412.66: SK= .010]

00197+ # [InterEventTime= 12.00]

00198+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00199+ # of 1.80

00200+ R0021:CO0015:0005

00201+ # CONTINUOUS HSMHDY . . . . .

00202+ # [CN= 66.00: NO\_3: 0.00: TP= 11.33]

00203+ # [TaEBC= 4.00: SMIN= 61.00: SMAX=350.79: SK= .000]

00204+ # [InterEventTime= 12.00]

00205+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00206+ # of 1.67

00207+ R0021:CO0015:0006

00208+ # CONTINUOUS HSMHDY . . . . .

00209+ # [CN= 66.00: NO\_3: 0.00: TP= 11.33]

00210+ # [TaEBC= 4.00: SMIN= 61.00: SMAX=350.79: SK= .000]

00211+ # [InterEventTime= 12.00]

00212+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00213+ # of 1.65

00214+ R0021:CO0015:0007

00215+ # CONTINUOUS HSMHDY . . . . .

00216+ # [CN= 66.00: NO\_3: 0.00: TP= 11.33]

00217+ # [TaEBC= 4.00: SMIN= 61.00: SMAX=350.79: SK= .000]

00218+ # [InterEventTime= 12.00]

00219+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00220+ # of 1.75

00221+ R0021:CO0015:0008

00222+ # CONTINUOUS HSMHDY . . . . .

00223+ # [CN= 67.00: NO\_3: 0.00: TP= 11.33]

00224+ # [TaEBC= 4.00: SMIN= 61.00: SMAX=336.97: SK= .010]

00225+ # [InterEventTime= 12.00]

00226+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00227+ # of 1.67

00228+ R0021:CO0015:0009

00229+ # CONTINUOUS HSMHDY . . . . .

00230+ # [CN= 67.00: NO\_3: 0.00: TP= 11.33]

00231+ # [TaEBC= 4.00: SMIN= 61.00: SMAX=264.99: SK= .010]

00232+ # [InterEventTime= 12.00]

00233+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00234+ # of 1.65

00235+ R0021:CO0015:0010

00236+ # CONTINUOUS HSMHDY . . . . .

00237+ # [CN= 67.00: NO\_3: 0.00: TP= 11.33]

00238+ # [TaEBC= 4.00: SMIN= 61.00: SMAX=207.66: SK= .010]

00239+ # [InterEventTime= 12.00]

00240+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00241+ # of 1.61

00242+ R0021:CO0015:0011

00243+ # CONTINUOUS HSMHDY . . . . .

00244+ # [CN= 67.00: NO\_3: 0.00: TP= 11.33]

00245+ # [TaEBC= 4.00: SMIN= 61.00: SMAX=244.49: SK= .010]

00246+ # [InterEventTime= 12.00]

00247+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00248+ # of 1.61

00249+ R0021:CO0015:0012

00250+ # CONTINUOUS HSMHDY . . . . .

00251+ # [CN= 67.00: NO\_3: 0.00: TP= 11.33]

00252+ # [TaEBC= 4.00: SMIN= 25.21: SMAX=168.09: SK= .010]

00253+ # [InterEventTime= 12.00]

00254+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00255+ # of 1.65

00256+ R0021:CO0015:0013

00257+ # CONTINUOUS HSMHDY . . . . .

00258+ # [CN= 68.00: NO\_3: 0.00: TP= 2.46]

00259+ # [TaEBC= 4.00: SMIN= 1.00: SMAX=175.80: SK= .010]

00260+ # [InterEventTime= 12.00]

00261+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00262+ # of 1.61

00263+ R0021:CO0022:0001

00264+ # CONTINUOUS HSMHDY . . . . .

00265+ # [CN= 68.00: NO\_3: 0.00: TP= 1.00]

00266+ # [TaEBC= 4.00: SMIN= 33.81: SMAX=225.43: SK= .010]

00267+ # [InterEventTime= 12.00]

00268+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00269+ # of 1.61

00270+ R0021:CO0022:0002

00271+ # CONTINUOUS HSMHDY . . . . .

00272+ # [CN= 68.00: NO\_3: 0.00: TP= 1.00]

00273+ # [TaEBC= 4.00: SMIN= 33.81: SMAX=207.66: SK= .010]

00274+ # [InterEventTime= 12.00]

00275+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00276+ # of 1.65

00277+ R0021:CO0022:0003

00278+ # CONTINUOUS HSMHDY . . . . .

00279+ # [CN= 68.00: NO\_3: 0.00: TP= 1.00]

00280+ # [TaEBC= 4.00: SMIN= 29.88: SMAX=199.22: SK= .010]

00281+ # [InterEventTime= 12.00]

00282+ # Routing hydrographs

00283+ # Sum of hydrographs from Node 13 routed to Node 12

00284+ # Starting with the addition of Jock River Headwater and Subwatershed 13

00285+ ADD HYD

00286+ # [CN= 68.00: NO\_3: 0.00: TP= 1.00]

00287+ SUM

00288+ # Sum of hydrographs from Node 13 routed to Node 12

00289+ # (Approximated cross-section - see cross-section 258)

00290+ # Use n=0.04 for summer conditions and n=0.025 for spring conditions

00291+ #

00292+ R0021:CO0031:0001

00293+ # DTMn-ID:HMYD . . . . .

00294+ # ROUTE CHANNEL > .30\_0.0128.M13

00295+ # [CN= 69.00: NO\_3: 0.00: TP= 3.03]

00296+ # [TaEBC= 4.00: SMIN= 3.03: SMAX=216.39: SK= .010]

00297+ # [InterEventTime= 12.00]

00298+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00299+ # of 1.61

00300+ R0021:CO0032:0001

00301+ # DTMn-ID:HMYD . . . . .

00302+ ADD HYD

00303+ # [CN= 70.00: NO\_3: 0.00: TP= 3.03]

00304+ # [TaEBC= 4.00: SMIN= 3.03: SMAX=168.09: SK= .010]

00305+ # [InterEventTime= 12.00]

00306+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00307+ # of 1.61

00308+ R0021:CO0032:0002

00309+ # DTMn-ID:HMYD . . . . .

00310+ # ROUTE RESERVOIR > .30\_0.0128.M13

00311+ # [CN= 70.00: NO\_3: 0.00: TP= 3.03]

00312+ # [TaEBC= 4.00: SMIN= 3.03: SMAX=176.39: SK= .010]

00313+ # [InterEventTime= 12.00]

00314+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00315+ # of 1.61

00316+ R0021:CO0034:0001

00317+ # DTMn-ID:HMYD . . . . .

00318+ # (Approximated cross-section - see cross-section 258)

00319+ # Use n=0.04 for summer conditions and n=0.025 for spring conditions

00320+ #

00321+ # DTMn-ID:HMYD . . . . .

00322+ # ROUTE CHANNEL > .30\_0.0128.M13

00323+ # [CN= 70.00: NO\_3: 0.00: TP= 3.03]

00324+ # [TaEBC= 4.00: SMIN= 3.03: SMAX=176.39: SK= .010]

00325+ # [InterEventTime= 12.00]

00326+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00327+ # of 1.61

00328+ R0021:CO0034:0002

00329+ # DTMn-ID:HMYD . . . . .

00330+ # ROUTE CHANNEL > .30\_0.0128.M13

00331+ # [CN= 70.00: NO\_3: 0.00: TP= 3.03]

00332+ # [TaEBC= 4.00: SMIN= 3.03: SMAX=176.39: SK= .010]

00333+ # [InterEventTime= 12.00]

00334+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00335+ # of 1.61

00336+ R0021:CO0034:0003

00337+ # DTMn-ID:HMYD . . . . .

00338+ # (Approximated cross-section - see cross-section 258)

00339+ # Use n=0.04 for summer conditions and n=0.025 for spring conditions

00340+ #

00341+ # DTMn-ID:HMYD . . . . .

00342+ # ROUTE CHANNEL > .30\_0.0128.M12

00343+ # [CN= 70.00: NO\_3: 0.00: TP= 3.03]

00344+ # [TaEBC= 4.00: SMIN= 3.03: SMAX=176.39: SK= .010]

00345+ # [InterEventTime= 12.00]

00346+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00347+ # of 1.61

00348+ R0021:CO0034:0004

00349+ # DTMn-ID:HMYD . . . . .

00350+ # ROUTE CHANNEL > .30\_0.0128.M11

00351+ # [CN= 70.00: NO\_3: 0.00: TP= 3.03]

00352+ # [TaEBC= 4.00: SMIN= 3.03: SMAX=176.39: SK= .010]

00353+ # [InterEventTime= 12.00]

00354+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00355+ # of 1.61

00356+ R0021:CO0040:0001

00357+ # DTMn-ID:HMYD . . . . .

00358+ ADD HYD

00359+ # [CN= 70.00: NO\_3: 0.00: TP= 3.03]

00360+ # [TaEBC= 4.00: SMIN= 3.03: SMAX=176.39: SK= .010]

00361+ # [InterEventTime= 12.00]

00362+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00363+ # of 1.61

00364+ R0021:CO0040:0002

00365+ # DTMn-ID:HMYD . . . . .

00366+ # ROUTE CHANNEL > .30\_0.0128.M11

00367+ # [RD7-30.00] out- .30\_0.0128.M11

00368+ # [CN= 70.00: NO\_3: 0.00: TP= 3.03]

00369+ # [TaEBC= 4.00: SMIN= 3.03: SMAX=176.39: SK= .010]

00370+ # [InterEventTime= 12.00]

00371+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00372+ # of 1.61

00373+ R0021:CO0042:0001

00374+ # DTMn-ID:HMYD . . . . .

00375+ # (Approximated cross-section - see cross-section 258)

00376+ # Use n=0.04 for summer conditions and n=0.025 for spring conditions

00377+ #

00378+ # DTMn-ID:HMYD . . . . .

00379+ # ROUTE CHANNEL > .30\_0.0128.M10

00380+ # [CN= 70.00: NO\_3: 0.00: TP= 3.03]

00381+ # [TaEBC= 4.00: SMIN= 3.03: SMAX=176.39: SK= .010]

00382+ # [InterEventTime= 12.00]

00383+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00384+ # of 1.61

00385+ R0021:CO0042:0002

00386+ # DTMn-ID:HMYD . . . . .

00387+ # ROUTE CHANNEL > .30\_0.0128.M10

00388+ # [CN= 70.00: NO\_3: 0.00: TP= 3.03]

00389+ # [TaEBC= 4.00: SMIN= 3.03: SMAX=176.39: SK= .010]

00390+ # [InterEventTime= 12.00]

00391+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00392+ # of 1.61

00393+ R0021:CO0042:0003

00394+ # DTMn-ID:HMYD . . . . .

00395+ # (Approximated cross-section - see cross-section 258)

00396+ # Use n=0.04 for summer conditions and n=0.025 for spring conditions

00397+ #

00398+ # DTMn-ID:HMYD . . . . .

00399+ # ROUTE CHANNEL > .30\_0.0128.M10

00400+ # [CN= 70.00: NO\_3: 0.00: TP= 3.03]

00401+ # [TaEBC= 4.00: SMIN= 3.03: SMAX=176.39: SK= .010]

00402+ # [InterEventTime= 12.00]

00403+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

00404+ # of 1.61

00405+ R0021:CO0042:0004

00406+ # DTMn-ID:HMYD . . . . .

00407+ # ROUTE CHANNEL > .30\_0.0128.M10

00408+ # [CN= 70.00: NO\_3: 0.00: TP= 3.03]

00409+ # [TaEBC= 4.00: SMIN= 3.03: SMAX=176.39: SK= .010]

00410+ # [InterEventTime= 12.00]

0041

00375+ + 30.0 02:SM\_10 5666.00 10.936 No\_date 38:00 13.91 n/a .000  
 00376+ SUM+ 30.0 01:S\_N10 17889.00 15.098 No\_date 38:30 12.16 n/a .000  
 00377+ \* 30.0 01:S\_N10 17889.00 15.098 No\_date 38:30 12.16 n/a .000  
 00378+ SAVE HYD  
 00379+ frame :H\_SNU  
 00380+ remark:flow at S\_JN10: N10 + SW\_10  
 00381+ # Addition of Kings Creek to S\_N10  
 00382+  
 00383+ # Sum of hydrographs from Node 10 routed to Node 9  
 00384+ Section 2  
 00385+  
 00386+ R0021:CO0045- Dtnin-ID:NHYD---AREaba-QPEAKcms-TpeakDate\_bh:mm---RVmn-R.C.--DWFcms  
 00387+ ADD HYD  
 00388+ \* 30.0 02:SM\_10 17889.00 15.098 No\_date 38:30 12.16 n/a .000  
 00389+ SUM+ 30.0 01:S\_N10A 25985.00 29.422 No\_date 39:30 12.09 n/a .000  
 00390+  
 00391+ # Sum of hydrographs from Node 10 routed to Node 9  
 00392+  
 00393+ ROUTE CHANNEL -> 30.0 02:S\_N10A 25985.00 29.622 No\_date 39:30 12.09 n/a .000  
 00394+ [ROT=30.001] out= 30.0 01:N9 25985.00 28.881 No\_date 39:30 12.09 n/a .000  
 00395+ [Vmax=.591,Imax=1.193]  
 00396+ #  
 00397+ # Addition of Subwatershed 9 and Nichols Creek to Node 9  
 00398+  
 00399+ R0021:CO0046- Dtnin-ID:NHYD---AREaba-QPEAKcms-TpeakDate\_bh:mm---RVmn-R.C.--DWFcms  
 00400+ ADD HYD  
 00401+ \* 30.0 02:SM\_9 1132.00 4.365 No\_date 38:30 13.32 n/a .000  
 00402+ \* 30.0 02:NC\_CK 4464.00 5.312 No\_date 38:30 10.96 n/a .000  
 00403+ SUM+ 30.0 01:S\_N9 31561.00 35.488 No\_date 39:30 11.98 n/a .000  
 00404+ #  
 00405+ # Sum of hydrographs from Node 9 routed to Node 8  
 00406+ Section 3  
 00407+  
 00408+ R0021:CO0047- Dtnin-ID:NHYD---AREaba-QPEAKcms-TpeakDate\_bh:mm---RVmn-R.C.--DWFcms  
 00409+ ROUTE CHANNEL -> 30.0 02:S\_N10A 31561.00 35.488 No\_date 38:30 11.98 n/a .000  
 00410+ [ROT=30.001] out= 30.0 01:N9 31561.00 33.301 No\_date 40:00 11.98 n/a .000  
 00411+ [L/S/n=.2269 / .088/.045]  
 00412+ [Vmax=.420,Imax=1.270]  
 00413+ #  
 00414+ # Addition of Subwatershed 8 and Hobbs's Drain to Node 8  
 00415+  
 00416+ R0021:CO0048- Dtnin-ID:NHYD---AREaba-QPEAKcms-TpeakDate\_bh:mm---RVmn-R.C.--DWFcms  
 00417+ ADD HYD  
 00418+ \* 30.0 02:SM\_8 131.00 1.702 No\_date 28:30 11.98 n/a .000  
 00419+ \* 30.0 02:DH\_DR 3854.00 6.083 No\_date 38:30 11.98 n/a .000  
 00420+ SUM+ 30.0 01:S\_N8 35464.00 39.356 No\_date 39:30 11.98 n/a .000  
 00421+ #  
 00422+ # Sum of hydrographs from Node 8 routed to Node 7  
 00423+ # Section 4  
 00424+  
 00425+ R0021:CO0049- Dtnin-ID:NHYD---AREaba-QPEAKcms-TpeakDate\_bh:mm---RVmn-R.C.--DWFcms  
 00426+ ROUTE CHANNEL -> 30.0 02:S\_N8 35464.00 39.356 No\_date 39:30 11.98 n/a .000  
 00427+ [ROT=30.001] out= 30.0 01:N8 35464.00 32.170 No\_date 44:00 11.97 n/a .000  
 00428+ [L/S/n=.3750 / .053/.070]  
 00429+ [Vmax=.209,Imax=1.635]  
 00430+ #  
 00431+ # Addition of Subwatershed 7 to Node 7  
 00432+  
 00433+ R0021:CO0050- Dtnin-ID:NHYD---AREaba-QPEAKcms-TpeakDate\_bh:mm---RVmn-R.C.--DWFcms  
 00434+ ADD HYD  
 00435+ \* 30.0 02:N7 35456.00 32.170 No\_date 44:00 11.97 n/a .000  
 00436+ \* 30.0 02:SM\_7 131.00 1.702 No\_date 28:30 11.98 n/a .000  
 00437+ SUM+ 30.0 01:S\_N7 38743.00 34.345 No\_date 43:00 11.97 n/a .000  
 00438+ SAVE HYD  
 00439+ frame :H\_SNU  
 00440+ remark:flow at S\_N7: N7 SW\_10  
 00441+ #  
 00442+ # Inflow from S\_N7 was used to simulate the effects of the Richmond Pen.  
 00443+ # Storage area and volumes were estimated from available topo maps.  
 00444+ # Release rate from flow was assumed to be controlled by the downstream  
 00445+ # storage area. A peak reduction factor of 0.7 was applied for up to  
 00446+ # 0.7% of water, the main channel of the river provided the storage. Above  
 00447+ # this depth, the wetland starts to significantly store water.  
 00448+  
 00449+ R0021:CO0052- Dtnin-ID:NHYD---AREaba-QPEAKcms-TpeakDate\_bh:mm---RVmn-R.C.--DWFcms  
 00450+ ROUTE RESERVOIR -> 30.0 02:S\_N7 38743.00 34.345 No\_date 43:00 11.97 n/a .000  
 00451+ [MWS=Closed,7399E-02 m3]  
 00452+ R0021:CO0053- Dtnin-ID:NHYD---AREaba-QPEAKcms-TpeakDate\_bh:mm---RVmn-R.C.--DWFcms  
 00453+ SAVE HYD  
 00454+ frame :H\_SNU  
 00455+ remark:flow at S\_N7: N7 SW\_10  
 00456+ #  
 00457+ # Sum of hydrographs from Node 7 routed to Node 6  
 00458+ # Section 5  
 00459+  
 00460+ R0021:CO0054- Dtnin-ID:NHYD---AREaba-QPEAKcms-TpeakDate\_bh:mm---RVmn-R.C.--DWFcms  
 00461+ ROUTE CHANNEL -> 30.0 02:S\_N6 38743.00 23.075 No\_date 54:30 11.79 n/a .000  
 00462+ [ROT=30.001] out= 30.0 01:N6 38743.00 23.052 No\_date 54:00 11.79 n/a .000  
 00463+ [L/S/n=.3056 / .082/.024]  
 00464+ [Vmax=.431,Imax=.805]  
 00465+ #  
 00466+ # Addition of Subwatershed 6 and Van Gaal Drain to Node 6  
 00467+  
 00468+ R0021:CO0055- Dtnin-ID:NHYD---AREaba-QPEAKcms-TpeakDate\_bh:mm---RVmn-R.C.--DWFcms  
 00469+ ADD HYD  
 00470+ \* 30.0 02:N6 38743.00 23.052 No\_date 54:00 11.79 n/a .000  
 00471+ \* 30.0 02:SM\_6 165.00 4.092 No\_date 38:30 12.01 n/a .000  
 00472+ SUM+ 30.0 01:S\_N6 40240.01 23.225 No\_date 39:30 11.87 n/a .000  
 00473+ #  
 00474+ # Sum of hydrographs from Node 6 routed to Node 5  
 00475+ # Section 6  
 00476+  
 00477+ R0021:CO0056- Dtnin-ID:NHYD---AREaba-QPEAKcms-TpeakDate\_bh:mm---RVmn-R.C.--DWFcms  
 00478+ ROUTE CHANNEL -> 30.0 02:S\_N5 40240.01 23.225 No\_date 39:30 11.87 n/a .000  
 00479+ [ROT=30.001] out= 30.0 01:N5 40240.01 23.171 No\_date 55:00 11.87 n/a .000  
 00480+ [L/S/n=.1852 / .054/.036]  
 00481+ [Vmax=.378,Imax=.915]  
 00482+ #  
 00483+ # Addition of Subwatershed 5 and Flowing Creek to Node 5  
 00484+  
 00485+ R0021:CO0057- Dtnin-ID:NHYD---AREaba-QPEAKcms-TpeakDate\_bh:mm---RVmn-R.C.--DWFcms  
 00486+ ADD HYD  
 00487+ \* 30.0 02:N5 40240.01 23.171 No\_date 55:00 11.87 n/a .000  
 00488+ \* 30.0 02:SM\_5 224.00 2.527 No\_date 28:30 15.88 n/a .000  
 00489+ SUM+ 30.0 01:S\_N5 44549.01 14.579 No\_date 35:00 14.54 n/a .000  
 00490+ #  
 00491+ # Sum of hydrographs from Node 5 routed to Node 4  
 00492+ # Section 7  
 00493+  
 00494+ R0021:CO0058- Dtnin-ID:NHYD---AREaba-QPEAKcms-TpeakDate\_bh:mm---RVmn-R.C.--DWFcms  
 00495+ ADD HYD  
 00496+ \* 30.0 02:N4 44549.01 32.922 No\_date 37:00 12.18 n/a .000  
 00497+ \* 30.0 02:SM\_5 287.00 2.082 No\_date 28:30 17.76 n/a .000  
 00498+ SUM+ 30.0 01:S\_N4 45409.01 35.939 No\_date 37:00 12.27 n/a .000  
 00499+ #  
 00500+ # Sum of hydrographs from Node 4 routed to Node 3  
 00501+ # Section 8  
 00502+ R0021:CO0059- Dtnin-ID:NHYD---AREaba-QPEAKcms-TpeakDate\_bh:mm---RVmn-R.C.--DWFcms  
 00503+ ADD HYD  
 00504+ \* 30.0 02:N3A 45409.01 32.922 No\_date 37:00 12.18 n/a .000  
 00505+ \* 30.0 02:SM\_5A 1412.00 3.007 No\_date 38:00 15.19 n/a .000  
 00506+ SUM+ 30.0 01:S\_N3A 46841.01 35.939 No\_date 37:00 12.27 n/a .000  
 00507+ #  
 00508+ # Sum of hydrographs from Node 3 routed to Node 4  
 00509+ # Section 9  
 00510+  
 00511+ R0021:CO0060- Dtnin-ID:NHYD---AREaba-QPEAKcms-TpeakDate\_bh:mm---RVmn-R.C.--DWFcms  
 00512+ ROUTE CHANNEL -> 30.0 02:S\_N3A 46841.01 35.939 No\_date 37:00 12.27 n/a .000  
 00513+ [ROT=30.001] out= 30.0 01:N4 46841.01 35.066 No\_date 39:00 12.27 n/a .000  
 00514+ [L/S/n=.4630 / .043/.036]  
 00515+ [Vmax=.693,Imax=2.838]  
 00516+ #  
 00517+ # Addition of Subwatershed 3 and Subwatershed 3A to Node 3A  
 00518+  
 00519+ R0021:CO0061- Dtnin-ID:NHYD---AREaba-QPEAKcms-TpeakDate\_bh:mm---RVmn-R.C.--DWFcms  
 00520+ ADD HYD  
 00521+ \* 30.0 02:N3A 46841.01 35.066 No\_date 37:00 12.27 n/a .000  
 00522+ \* 30.0 02:SM\_4 585.00 4.232 No\_date 29:30 17.76 n/a .000  
 00523+ SUM+ 30.0 01:S\_N3A 48447.00 37.399 No\_date 38:30 12.44 n/a .000  
 00524+ R0021:CO0062- Dtnin-ID:NHYD---AREaba-QPEAKcms-TpeakDate\_bh:mm---RVmn-R.C.--DWFcms  
 00525+ SAVE HYD  
 00526+ frame :H\_SNU  
 00527+ remark:flow at S\_N4  
 00528+ # Sum of hydrographs from Node 4 routed to Node 2  
 00529+ # Section 10  
 00530+  
 00531+ R0021:CO0063- Dtnin-ID:NHYD---AREaba-QPEAKcms-TpeakDate\_bh:mm---RVmn-R.C.--DWFcms  
 00532+ ROUTE CHANNEL -> 30.0 02:S\_N4 48447.00 37.399 No\_date 38:30 12.44 n/a .000  
 00533+ [ROT=30.001] out= 30.0 01:N2 48447.00 37.299 No\_date 39:00 12.44 n/a .000  
 00534+ [L/S/n=.7414 / .050/.041]  
 00535+ [Vmax=.7414,Imax=2.841]  
 00536+ #  
 00537+ # Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2  
 00538+  
 00539+ R0021:CO0064- Dtnin-ID:NHYD---AREaba-QPEAKcms-TpeakDate\_bh:mm---RVmn-R.C.--DWFcms  
 00540+ ADD HYD  
 00541+ \* 30.0 02:N2 48447.00 37.299 No\_date 38:00 13.44 n/a .000  
 00542+ \* 30.0 02:SM\_2 177.00 1.996 No\_date 28:30 15.88 n/a .000  
 00543+ \* 30.0 02:SM\_5B 122.00 5.267 No\_date 30:30 17.36 n/a .000  
 00544+ SUM+ 30.0 01:S\_N2 52483.00 45.676 No\_date 33:30 12.73 n/a .000  
 00545+ #  
 00546+ R0021:CO0065- Dtnin-ID:NHYD---AREaba-QPEAKcms-TpeakDate\_bh:mm---RVmn-R.C.--DWFcms  
 00547+ SAVE HYD  
 00548+ frame :H\_SNU  
 00549+ remark:flow at S\_N2 Jock River Gauge at Moodie Dr.  
 00550+ #  
 00551+ # Sum of hydrographs from Node 2 routed to Node 1  
 00552+ # Section 10  
 00553+  
 00554+ R0021:CO0066- Dtnin-ID:NHYD---AREaba-QPEAKcms-TpeakDate\_bh:mm---RVmn-R.C.--DWFcms  
 00555+ ROUTE CHANNEL -> 30.0 02:S\_N2 52483.00 45.676 No\_date 33:30 12.73 n/a .000  
 00556+ [ROT=30.001] out= 30.0 01:N1 52483.00 42.605 No\_date 39:30 12.73 n/a .000  
 00557+ [L/S/n=.10046 / .050/.040]  
 00558+ [Vmax=.767,Imax=2.662]  
 00559+ #  
 00560+ # Addition of Subwatershed 1 to Node 1  
 00561+ #

00749+ CONTINUOUS NASHYD 30.0 01:SMW\_2 1412.00 4.515 No\_date 37:30 21.96 .384 .000

00750+ [CN= 4.00:SMIN 3.00: Tp: 1.01] 30.0 01:SMW\_2A51 226.43: SKw .010]

00752+ [InterEventTime= 12.00]

00753+ R0005:CD0024-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00754+ CONTINUOUS NASHYD 30.0 01:SMW\_2 585.00 6.551 No\_date 28:30 25.59 .446 .000

00755+ [CN= 81.0: NO. 3:00: Tp: 1.75] 30.0 01:SMW\_2 1.75

00756+ [InterEventTime= 12.00]

00757+ R0005:CD0025-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00758+ CONTINUOUS NASHYD 30.0 01:SMW\_2 177.00 3.149 No\_date 28:30 22.94 .402 .000

00759+ [CN= 81.0: NO. 3:00: Tp: 1.46] 30.0 01:SMW\_2 1.46

00760+ [InterEventTime= 12.00]

00761+ R0005:CD0026-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00762+ CONTINUOUS NASHYD 30.0 01:SMW\_2 177.00 3.149 No\_date 30:30 25.04 .438 .000

00763+ [CN= 81.0: NO. 3:00: Tp: 1.75] 30.0 01:SMW\_2 1.75

00764+ CONTINUOUS NASHYD 30.0 01:SMW\_2 177.00 3.149 No\_date 28:30 22.94 .402 .000

00765+ [CN= 81.0: NO. 3:00: Tp: 1.46] 30.0 01:SMW\_2 1.46

00766+ [InterEventTime= 12.00]

00767+ R0005:CD0027-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00768+ CONTINUOUS NASHYD 30.0 01:SMW\_2 112.00 8.043 No\_date 31:30 25.59 .446 .000

00769+ [CN= 81.0: NO. 3:00: Tp: 3.25] 30.0 01:SMW\_2 3.25

00770+ [InterEventTime= 12.00]

00771+ R0005:CD0028-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00772+ CONTINUOUS NASHYD 30.0 01:SMW\_2 273.00 17.548 No\_date 31:30 22.44 .393 .000

00773+ [CN= 76.0: NO. 3:00: Tp: 3.03] 30.0 01:SMW\_2 3.03

00774+ CONTINUOUS NASHYD 30.0 01:SMW\_2 317.00 19.206 No\_date 32:00 23.45 .411 .000

00775+ [CN= 81.0: NO. 3:00: Tp: 1.75] 30.0 01:SMW\_2 1.75

00776+ [InterEventTime= 12.00]

00777+ R0005:CD0029-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00778+ CONTINUOUS NASHYD 30.0 01:SMW\_2 112.00 8.043 No\_date 31:30 25.59 .446 .000

00779+ [CN= 81.0: NO. 3:00: Tp: 3.25] 30.0 01:SMW\_2 3.25

00780+ [InterEventTime= 12.00]

00781+ R0005:CD0030-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00782+ CONTINUOUS NASHYD 30.0 01:SMW\_2 112.00 8.043 No\_date 31:30 25.59 .446 .000

00783+ [CN= 81.0: NO. 3:00: Tp: 1.75] 30.0 01:SMW\_2 1.75

00784+ [InterEventTime= 12.00]

00785+ # Starting with the addition of Jock River Headwater and Subwatershed 13

00786+ R0005:CD0031-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00787+ ADD HYD 30.0 02:JR\_HYD 3680.00 5.169 No\_date 37:00 16.38 n/a .000

00788+ SUM+ 30.0 02:SMW\_13 971.00 3.350 No\_date 32:30 15.27 n/a .000

00789+ SUM- 30.0 01:SIN13 4651.00 11.688 No\_date 38:30 16.15 n/a .000

00790+ #

00791+ # Sum of hydrographs from Node 13 routed to Node 13A

00792+ # (Approximated cross-section see cross-section 288)

00793+ R0005:CD0032-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00794+ ROUTE RESERVOIR-> 30.0 02:SMW\_13 4651.00 11.688 No\_date 35:30 16.15 n/a .000

00795+ [ROT:30.001] out-> 30.0 01:RES13A 4651.00 9.343 No\_date 39:30 16.15 n/a .000

00796+ [L/S/nr: 9074. /.022/.040]

00797+ [Vmax=.475:Dmax=.2992]

00798+ #

00799+ # Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A

00800+ R0005:CD0033-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00801+ ADD HYD 30.0 02:JR\_HYD 3680.00 5.169 No\_date 37:00 16.38 n/a .000

00802+ SUM+ 30.0 02:SMW\_13 971.00 3.350 No\_date 32:30 15.27 n/a .000

00803+ SUM- 30.0 01:SIN13A 7725.00 13.855 No\_date 39:30 14.97 n/a .000

00804+ # Insertion of a reservoir to simulate the effects of the Goodwood Marsh

00805+ R0005:CD0034-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00806+ ROUTE CHANNEL-> 30.0 02:SMW\_13 4651.00 11.688 No\_date 39:30 14.97 n/a .000

00807+ [ROT:30.001] out-> 30.0 01:RES13A 4651.00 9.343 No\_date 39:30 14.97 n/a .000

00808+ [L/S/nr: 556. /.009/.040]

00809+ [Vmax=.464:Dmax=.1057]

00810+ #

00811+ # Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A

00812+ R0005:CD0035-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00813+ ROUTE CHANNEL-> 30.0 02:SMW\_13 7725.00 13.855 No\_date 39:30 14.97 n/a .000

00814+ [ROT:30.001] out-> 30.0 01:RES13 7725.00 3.124 No\_date 58:00 14.97 n/a .000

00815+ [L/S/nr: 9074. /.022/.040]

00816+ [Vmax=.825:Dmax=1.424]

00817+ R0005:CD0036-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00818+ ADD HYD 30.0 02:JR\_HYD 7725.00 3.124 No\_date 58:00 14.97 n/a .000

00819+ # Outflow from Reservoir Goodwood Marsh routed from Node 13A to Node 12

00820+ # (Approximated cross-section - see cross-section 258)

00821+ Use n=0.04 for summer conditions and n=0.025 for spring conditions

00822+ R0005:CD0037-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00823+ ROUTE CHANNEL-> 30.0 02:RES13M 7725.00 3.124 No\_date 58:00 14.97 n/a .000

00824+ [ROT:30.001] out-> 30.0 01:RES13M 7725.00 3.124 No\_date 58:00 14.97 n/a .000

00825+ [L/S/nr: 556. /.009/.040]

00826+ [Vmax=.755:Dmax=3.105]

00827+ #

00828+ # Addition of Subwatershed Jock River at Ashton to Node 12

00829+ R0005:CD0038-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00830+ ADD HYD 30.0 02:N12 7725.00 1.114 No\_date 32:30 14.97 n/a .000

00831+ SUM+ 30.0 02:SMW\_12 1781.00 8.382 No\_date 32:30 14.97 n/a .000

00832+ SUM- 30.0 01:SIN12 981.00 10.361 No\_date 32:30 15.93 n/a .000

00833+ SAVE HYD 30.0 02:N12 9506.00 10.361 No\_date 32:30 15.93 n/a .000

00834+ frameflow\_at\_S112 near Ashton

00835+ #

00836+ # Sum of hydrographs from Node 12 routed to Node 11

00837+ # (Approximated cross-section - see cross-section 258)

00838+ R0005:CD0039-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00839+ ROUTE CHANNEL-> 30.0 02:SMW\_12 9506.00 10.361 No\_date 32:30 15.93 n/a .000

00840+ [ROT:30.001] out-> 30.0 01:N11 9506.00 10.228 No\_date 33:00 15.93 n/a .000

00841+ [L/S/nr: 972. /.051/.040]

00842+ [Vmax=.645:Dmax=2.392]

00843+ #

00844+ # Addition of Subwatershed Jock River at Ashton to Node 11

00845+ R0005:CD0040-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00846+ ADD HYD 30.0 02:N12 7725.00 1.114 No\_date 32:30 14.97 n/a .000

00847+ SUM+ 30.0 02:SMW\_12 1781.00 8.382 No\_date 32:30 14.97 n/a .000

00848+ SUM- 30.0 01:N11 9506.00 10.228 No\_date 33:00 15.93 n/a .000

00849+ #

00850+ # Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248

00851+ R0005:CD0041-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00852+ ROUTE CHANNEL-> 30.0 02:SMW\_12 9506.00 10.361 No\_date 32:30 15.93 n/a .000

00853+ [ROT:30.001] out-> 30.0 01:N11 9506.00 10.228 No\_date 33:00 15.93 n/a .000

00854+ [L/S/nr: 972. /.051/.040]

00855+ [Vmax=.645:Dmax=2.417]

00856+ #

00857+ # Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248

00858+ R0005:CD0042-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00859+ ADD HYD 30.0 02:N11 11923.00 11.896 No\_date 38:30 16.18 n/a .000

00860+ SUM+ 30.0 02:SMW\_11 1788.00 26.338 No\_date 38:30 17.44 n/a .000

00861+ SUM- 30.0 01:N11 11923.00 17.312 No\_date 38:30 16.18 n/a .000

00862+ #

00863+ # Sum of hydrographs from Node 11 routed to Node 10

00864+ R0005:CD0043-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00865+ ADD HYD 30.0 02:N10 11923.00 17.312 No\_date 38:30 16.18 n/a .000

00866+ #

00867+ # Addition of Subwatershed 11 and Nn Name Creek to Node 11

00868+ R0005:CD0044-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00869+ ROUTE CHANNEL-> 30.0 02:SIN11 11923.00 17.312 No\_date 38:30 16.18 n/a .000

00870+ [ROT:30.001] out-> 30.0 01:SIN11 11923.00 11.896 No\_date 38:30 16.18 n/a .000

00871+ [L/S/nr: 14028. /.157/.040]

00872+ [Vmax=.462:Dmax=1.078]

00873+ #

00874+ # Addition of Subwatershed 10 to Node 10

00875+ R0005:CD0045-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00876+ ADD HYD 30.0 02:N10 11923.00 11.896 No\_date 38:30 16.18 n/a .000

00877+ SUM+ 30.0 02:SMW\_10 1788.00 26.338 No\_date 38:30 17.44 n/a .000

00878+ SUM- 30.0 01:N10 11923.00 17.312 No\_date 38:30 16.18 n/a .000

00879+ #

00880+ # Sum of hydrographs from Node 10 routed to Node 9

00881+ R0005:CD0046-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00882+ ADD HYD 30.0 02:N9 11923.00 11.896 No\_date 38:30 16.18 n/a .000

00883+ SUM+ 30.0 02:SMW\_9 1788.00 26.338 No\_date 38:30 17.44 n/a .000

00884+ SUM- 30.0 01:N9 11923.00 17.312 No\_date 38:30 16.18 n/a .000

00885+ #

00886+ # Sum of hydrographs from Node 10 routed to Node 9

00887+ R0005:CD0047-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00888+ ADD HYD 30.0 02:N9 11923.00 11.896 No\_date 38:30 17.35 n/a .000

00889+ SUM+ 30.0 02:SMW\_9 1788.00 43.586 No\_date 38:30 17.35 n/a .000

00890+ SUM- 30.0 01:N9 11923.00 17.312 No\_date 38:30 17.35 n/a .000

00891+ #

00892+ # Sum of hydrographs from Node 10 routed to Node 9

00893+ R0005:CD0048-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00894+ ADD HYD 30.0 02:N9 2985.00 42.441 No\_date 39:30 17.35 n/a .000

00895+ SUM+ 30.0 02:SMW\_9 1132.00 6.854 No\_date 30:30 19.22 n/a .000

00896+ SUM- 30.0 01:N9 3156.00 44.285 No\_date 39:30 15.63 n/a .000

00897+ SUM+ 30.0 01:SIN9 3156.00 52.068 No\_date 39:30 17.17 n/a .000

00898+ #

00899+ # Sum of hydrographs from Node 9 routed to Node 8

00900+ R0005:CD0049-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00901+ ADD HYD 30.0 02:N8 3156.00 45.431 No\_date 40:00 17.17 n/a .000

00902+ SUM+ 30.0 02:SMW\_8 131.00 1.239 No\_date 28:30 16.00 n/a .000

00903+ SUM- 30.0 01:N8 3584.00 48.436 No\_date 40:00 17.17 n/a .000

00904+ #

00905+ # Sum of hydrographs from Node 8 routed to Node 7

00906+ R0005:CD0050-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00907+ ADD HYD 30.0 02:N7 3156.00 45.431 No\_date 40:00 17.17 n/a .000

00908+ SUM+ 30.0 02:SMW\_7 131.00 1.239 No\_date 28:30 16.00 n/a .000

00909+ SUM- 30.0 01:N7 3584.00 46.889 No\_date 40:00 17.17 n/a .000

00910+ #

00911+ # Addition of Subwatershed 8 and Hobbs's Drain to Node 8

00912+ R0005:CD0051-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00913+ ADD HYD 30.0 02:N8 3156.00 45.431 No\_date 40:00 17.17 n/a .000

00914+ SUM+ 30.0 02:SMW\_8 131.00 1.239 No\_date 28:30 16.00 n/a .000

00915+ SUM- 30.0 01:N8 3584.00 46.889 No\_date 40:00 17.17 n/a .000

00916+ #

00917+ # Addition of Subwatershed 8 and Hobbs's Drain to Node 8

00918+ R0005:CD0048-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00919+ ADD HYD 30.0 02:N8 3156.00 45.431 No\_date 40:00 17.17 n/a .000

00920+ SUM+ 30.0 02:SMW\_8 131.00 1.239 No\_date 28:30 16.00 n/a .000

00921+ SUM- 30.0 01:N8 3584.00 46.889 No\_date 40:00 17.17 n/a .000

00922+ #

00923+ # Addition of Subwatershed 8 and Hobbs's Drain to Node 8

00924+ R0005:CD0049-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00925+ ADD HYD 30.0 02:N8 3156.00 45.431 No\_date 40:00 17.17 n/a .000

00926+ SUM+ 30.0 02:SMW\_8 131.00 1.239 No\_date 28:30 16.00 n/a .000

00927+ SUM- 30.0 01:N8 3584.00 46.889 No\_date 40:00 17.17 n/a .000

00928+ #

00929+ # Addition of Subwatershed 8 and Hobbs's Drain to Node 8

00930+ R0005:CD0048-----DtnID:NHYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:---RvNm-R.C.---DFWfcm

00931+ ADD HYD 30.0 02:N8 3156.00 45.431 No\_date 40:00 17.17 n/a .000

00932+ SUM+ 30.0 02:SMW\_8 131.00 1.239 No\_date 28:30 16.00 n/a .000

00933+ SUM- 30.0 01:N8 3584.00 46.889 No\_date 40:00 17.17 n/a .000

00934+ #

00935+ # Addition of Subwatershed 8 to Node 7



04497# SUM- 30.0 01:S\_N8 45409.01 50,940 No\_date 34:30 21.53 n/a .000  
 04498# # Sum of hydrographs from Node 5 routed to Node 5A  
 04499# Section 9  
 05102# R010:000059 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05103# ROUTE CHANNEL > 30.0 02:S\_N8 45409.01 50,940 No\_date 34:30 21.53 n/a .000  
 05104# [RD7=30.00] out-> 30.0 01:N8A 45409.01 50,883 No\_date 35:00 21.53 n/a .000  
 05105# [/S/nv .556/. .090/.040] .000  
 05106# [/S/nv .484/.Maxx 1.127]  
 05107#  
 05108# # Addition of Subwatershed SA1 and Subwatershed SA2 to Node 5A  
 05109# Section 8  
 05110# R010:000059 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05111# ADD HYD 30.0 02:N8 45409.01 50,883 No\_date 35:00 21.53 n/a .000  
 05112# \* 30.0 02:N8 1200 11.574 No\_date 35:00 21.53 n/a .000  
 05113# \* 30.0 02:N8\_SA1 1412.00 5,651 No\_date 37:30 27.03 n/a .000  
 05114# SUM- 30.0 01:S\_N8A 46841.01 56,195 No\_date 35:00 21.70 n/a .000  
 05115#  
 05116# # Sum of hydrographs from Node 8A routed to Node 4  
 05117# Section 8  
 05118# R010:000060 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05119# ROUTE CHANNEL > 30.0 02:S\_N8A 46841.01 56,195 No\_date 35:00 21.70 n/a .000  
 05120# [RD7=30.00] out-> 30.0 01:N8A 46841.01 54,050 No\_date 36:30 21.70 n/a .000  
 05121# [/S/nv .430/.043/.035] .000  
 05122# [/S/nv .430/.043/.035] .000  
 05123# [/S/nv .430/.043/.035] .000  
 05124# [/S/nv .430/.043/.035] .000  
 05125# # Addition of Subwatershed 4 and Leamy Creek to Node 4  
 05126# Section 9  
 05127# R010:000061 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05128# ADD HYD 30.0 02:N8 46841.01 54,050 No\_date 36:30 21.70 n/a .000  
 05129# \* 30.0 02:N8 1200 11.574 No\_date 36:30 21.70 n/a .000  
 05130# \* 30.0 02:N8\_CK 1212.00 8,241 No\_date 36:30 23.69 n/a .000  
 05131# SUM- 30.0 01:S\_N8A 46847.00 59,486 No\_date 36:00 22.01 n/a .000  
 05132#  
 05133# R010:000062 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05134# SAVE HYD 30.0 01:S\_N8A 46847.00 59,486 No\_date 36:00 22.01 n/a .000  
 05135# frame=S\_N4.0010  
 05136# remark:flow at S\_N4  
 05137# # Sum of hydrographs from Node 4 routed to Node 2  
 05138# Section 9  
 05139# R010:000063 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05140# ADD HYD 30.0 02:N8 48447.00 59,486 No\_date 36:00 22.01 n/a .000  
 05141# \* 30.0 02:N8 1200 11.574 No\_date 36:00 22.01 n/a .000  
 05142# [RD7=30.00] out-> 30.0 01:N8 48447.00 59,486 No\_date 36:00 22.01 n/a .000  
 05143# [/S/nv .667/.060/.060] .000  
 05144# [/S/nv .667/.060/.060] .000  
 05145# [/S/nv .667/.060/.060] .000  
 05146# # Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2  
 05147# Section 9  
 05148# R010:000064 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05149# ADD HYD 30.0 02:N8 48447.00 59,486 No\_date 36:00 22.01 n/a .000  
 05150# \* 30.0 02:N8 1200 11.574 No\_date 36:00 22.01 n/a .000  
 05151# \* 30.0 02:N8\_DR 1212.00 10,121 No\_date 31:30 31.34 n/a .000  
 05152# \* 30.0 02:MR\_DR 2737.00 22.263 No\_date 31:30 27.61 n/a .000  
 05153# SUM- 30.0 01:S\_N8A 52483.00 82,076 No\_date 33:00 22.52 n/a .000  
 05154# R010:000065 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05155# SAVE HYD 30.0 01:S\_N8A 52483.00 82,076 No\_date 33:00 22.52 n/a .000  
 05156# frame=S\_N4.0010  
 05157# remark:flow at S\_N2 Jock River Gauge at Moodie Dr.  
 05158# # Sum of hydrographs from Node 2 routed to Node 1  
 05159# Section 10  
 05160# R010:000066 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05161# ADD HYD 30.0 02:N8 52483.00 82,076 No\_date 33:00 22.52 n/a .000  
 05162# \* 30.0 02:N8 1200 11.574 No\_date 33:00 22.52 n/a .000  
 05163# [/S/nv .524/.350/.250] .000  
 05164# [/S/nv .524/.350/.250] .000  
 05165# [/S/nv .524/.350/.250] .000  
 05166# [/S/nv .524/.350/.250] .000  
 05167# # Addition of Subwatershed 1 to Node 1  
 05168# Section 10  
 05169# R010:000067 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05170# ADD HYD 30.0 02:N8 52483.00 72,984 No\_date 36:30 22.52 n/a .000  
 05171# \* 30.0 02:N8 1200 11.574 No\_date 36:30 22.52 n/a .000  
 05172# \* 30.0 02:SMN\_1 3176.00 24,273 No\_date 32:00 28.81 n/a .000  
 05173# \* 30.0 02:SMN 5585.00 24,295 No\_date 34:30 22.88 n/a .000  
 05174# \* 30.0 02:MR 52483.00 82,076 No\_date 33:00 22.52 n/a .000  
 05175# SUM- 30.0 01:N8 55659.00 89,515 No\_date 34:30 22.88 n/a .000  
 05176# frame=NL\_0010  
 05177# remark:total outflow of Jock River  
 05178# \*\*\* END OF RUN : 24  
 05179# \*\*\*\*\*  
 05180# \*\*\*\*\*  
 05181# \*\*\*\*\*  
 05182# \*\*\*\*\*  
 05183# \*\*\*\*\*  
 05184# \*\*\*\*\*  
 05185# \*\*\*\*\*  
 05186# \*\*\*\*\*  
 05187# RUNI:COMMAND#  
 05188# R010:0001  
 05189# START  
 05190# [TZER0 = 1.00 hrs on 1/1/2001] .000  
 05191# [TZR1 = 1.00 hrs on 1/1/2001, 2 metric output] .000  
 05192# [INSTRM = 1] .000  
 05193# [INRUM = 0025] .000  
 05194# [INRUM = 0025] .000  
 05195# SWMMVNO Ver:5.02/Jan 2001 [BETA] / INPUT DATA FILE  
 05196# Project Name : Jock River Project Number : (411-02)  
 05197# Modeler : [User Name:  
 05198# Date : 06-06-2003  
 05199# Modeler : [User Name:  
 05200# License #: 2549237  
 05201# License #: 2549237  
 05202# CALIBRATION OF SUMMER MODEL PARAMETERS  
 05203# USING CONTINUOUS SIMULATIONS  
 05204# \*\*\*\*\*  
 05205# Rainfall data from JFSS rainfall installed at site + other gauges by the City  
 05206# \*\*\*\* last collected from May let to July 14, 2003  
 05207# \*\*\*\*\*  
 05208# \*\*\*\*\*  
 05209# READ STORM  
 05210# Filename = storm.001  
 05211# Comment : Pluie sur le 24 bres 1-25 ans pour Ottawa CDA  
 05212# [RD7=30.00] out-> 30.0 01:N8 30,749.00 24,050 PTOT07 74.59]  
 05213# \*\*\*\*\*  
 05214# R010:000068 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05215# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05216# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05217# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05218# [/S/nv .554/.999/.999] .000  
 05219# [/S/nv .554/.999/.999] .000  
 05220# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05221# Section 12  
 05222# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05223# Section 12  
 05224# R020:000005 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05225# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05226# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05227# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05228# [/S/nv .554/.999/.999] .000  
 05229# [/S/nv .554/.999/.999] .000  
 05230# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05231# Section 12  
 05232# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05233# Section 12  
 05234# R020:000006 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05235# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05236# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05237# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05238# [/S/nv .554/.999/.999] .000  
 05239# [/S/nv .554/.999/.999] .000  
 05240# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05241# Section 12  
 05242# R020:000005 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05243# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05244# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05245# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05246# [/S/nv .554/.999/.999] .000  
 05247# [/S/nv .554/.999/.999] .000  
 05248# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05249# Section 12  
 05250# R020:000006 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05251# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05252# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05253# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05254# [/S/nv .554/.999/.999] .000  
 05255# [/S/nv .554/.999/.999] .000  
 05256# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05257# Section 12  
 05258# R020:000007 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05259# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05260# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05261# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05262# [/S/nv .554/.999/.999] .000  
 05263# [/S/nv .554/.999/.999] .000  
 05264# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05265# Section 12  
 05266# R020:000008 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05267# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05268# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05269# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05270# [/S/nv .554/.999/.999] .000  
 05271# [/S/nv .554/.999/.999] .000  
 05272# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05273# Section 12  
 05274# R020:000009 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05275# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05276# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05277# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05278# [/S/nv .554/.999/.999] .000  
 05279# [/S/nv .554/.999/.999] .000  
 05280# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05281# Section 12  
 05282# R020:000010 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05283# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05284# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05285# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05286# [/S/nv .554/.999/.999] .000  
 05287# [/S/nv .554/.999/.999] .000  
 05288# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05289# Section 12  
 05290# R020:000011 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05291# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05292# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05293# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05294# [/S/nv .554/.999/.999] .000  
 05295# [/S/nv .554/.999/.999] .000  
 05296# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05297# Section 12  
 05298# R020:000012 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05299# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05300# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05301# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05302# [/S/nv .554/.999/.999] .000  
 05303# [/S/nv .554/.999/.999] .000  
 05304# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05305# Section 12  
 05306# R020:000013 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05307# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05308# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05309# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05310# [/S/nv .554/.999/.999] .000  
 05311# [/S/nv .554/.999/.999] .000  
 05312# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05313# Section 12  
 05314# R020:000014 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05315# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05316# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05317# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05318# [/S/nv .554/.999/.999] .000  
 05319# [/S/nv .554/.999/.999] .000  
 05320# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05321# Section 12  
 05322# R020:000015 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05323# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05324# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05325# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05326# [/S/nv .554/.999/.999] .000  
 05327# [/S/nv .554/.999/.999] .000  
 05328# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05329# Section 12  
 05330# R020:000016 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05331# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05332# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05333# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05334# [/S/nv .554/.999/.999] .000  
 05335# [/S/nv .554/.999/.999] .000  
 05336# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05337# Section 12  
 05338# R020:000017 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05339# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05340# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05341# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05342# [/S/nv .554/.999/.999] .000  
 05343# [/S/nv .554/.999/.999] .000  
 05344# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05345# Section 12  
 05346# R020:000018 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05347# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05348# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05349# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05350# [/S/nv .554/.999/.999] .000  
 05351# [/S/nv .554/.999/.999] .000  
 05352# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05353# Section 12  
 05354# R020:000019 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05355# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05356# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05357# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05358# [/S/nv .554/.999/.999] .000  
 05359# [/S/nv .554/.999/.999] .000  
 05360# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05361# Section 12  
 05362# R020:000020 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05363# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05364# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05365# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05366# [/S/nv .554/.999/.999] .000  
 05367# [/S/nv .554/.999/.999] .000  
 05368# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05369# Section 12  
 05370# R020:000021 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05371# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05372# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05373# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05374# [/S/nv .554/.999/.999] .000  
 05375# [/S/nv .554/.999/.999] .000  
 05376# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05377# Section 12  
 05378# R020:000022 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05379# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05380# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05381# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05382# [/S/nv .554/.999/.999] .000  
 05383# [/S/nv .554/.999/.999] .000  
 05384# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05385# Section 12  
 05386# R020:000023 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05387# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05388# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05389# [RD7=4.00] out-> 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05390# [/S/nv .554/.999/.999] .000  
 05391# [/S/nv .554/.999/.999] .000  
 05392# The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 05393# Section 12  
 05394# R020:000024 -> DTMN-ID:NHYSW...-AREBha-QPEAKcms-TpeakDate\_hh:mm-->RVm-R.C.--DWFcms  
 05395# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05396# CONTINUOUS\_NASHWD 30.0 01:S\_N8 3680.00 15,104 No\_date 36:30 25.77 .346 .000  
 05397# [RD7=4.00] out-> 30.0

01871+ + 30.0 02:NH\_NK 1917.00 10.139 No\_date 34:00 26.99 n/a .000  
 01872+ SUM\_ 30.0 01:S\_N11 11923.00 27.440 No\_date 33:00 25.40 n/a .000  
 01873+ # Sum of hydrographs from Node 11 routed to Node 10  
 01874+ # Section 1  
 01875+ # Addition of Subwatershed 10 to Node 10  
 01876+ ROUTE CHANNEL -> 30.0 02:NH\_NYD -> AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 01877+ [ROUTE:30.001.out-> 30.0 02:NH\_NYD ]  
 01878+ [L/S/nr:14028. / .157. /040] 11923.00 17.756 No\_date 40:00 25.40 n/a .000  
 01879+ [Vmax=.463\*Dmax= 1.320]  
 01880+ #  
 01881+ # Addition of Subwatershed 10 to Node 10  
 01882+ ROUTE CHANNEL -> 30.0 02:NH\_NYD -> AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 01883+ ADD HYD + 30.0 02:NH\_NYD 11923.00 27.440 No\_date 33:00 25.40 n/a .000  
 01884+ [ROUTE:30.001.out-> 30.0 02:NH\_NYD ]  
 01885+ [L/S/nr:14028. / .157. /040] 11923.00 17.756 No\_date 40:00 25.40 n/a .000  
 01886+ [Vmax=.463\*Dmax= 1.320]  
 01887+ #  
 01888+ # Addition of Subwatershed 1 to Node 1  
 01889+ ROUTE CHANNEL -> 30.0 02:NH\_NYD -> AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 01890+ ADD HYD + 30.0 02:NH\_NYD 11923.00 27.440 No\_date 33:00 25.40 n/a .000  
 01891+ [ROUTE:30.001.out-> 30.0 02:NH\_NYD ]  
 01892+ [L/S/nr:14028. / .157. /040] 11923.00 17.756 No\_date 40:00 25.40 n/a .000  
 01893+ [Vmax=.463\*Dmax= 1.320]  
 01894+ #  
 01895+ # Addition of King Creek to S\_3\_MIO  
 01896+ ROUTE CHANNEL -> 30.0 02:NH\_NYD -> AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 01897+ ADD HYD + 30.0 02:NH\_NYD 11923.00 27.440 No\_date 33:00 25.40 n/a .000  
 01898+ [ROUTE:30.001.out-> 30.0 02:NH\_NYD ]  
 01899+ [L/S/nr:14028. / .157. /040] 11923.00 17.756 No\_date 40:00 25.40 n/a .000  
 01900+ [Vmax=.463\*Dmax= 1.320]  
 01901+ #  
 01902+ # Section 2  
 01903+ #  
 01904+ # RO025:CO0045-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 01905+ [ROUTE CHANNEL -> 30.0 02:S\_N10A ]  
 01906+ [ROUTE:30.001.out-> 30.0 02:S\_N10A ]  
 01907+ [L/S/nr: 3982. / .075. /040] 29565.00 66.824 No\_date 39:30 27.24 n/a .000  
 01908+ [Vmax=.713\*Dmax= 1.864]  
 01909+ #  
 01910+ # Addition of Subwatershed 9 and Nichols Creek to Node 9  
 01911+ # Section 3  
 01912+ #  
 01913+ # Sum of hydrographs from Node 10 routed to Node 9  
 01914+ #  
 01915+ # Section 4  
 01916+ #  
 01917+ # Sum of hydrographs from Node 9 routed to Node 8  
 01918+ #  
 01919+ # Section 3  
 01920+ #  
 01921+ # RO025:CO0047-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 01922+ [ROUTE CHANNEL -> 30.0 02:S\_N10B ]  
 01923+ [ROUTE:30.001.out-> 30.0 02:S\_N10B ]  
 01924+ [L/S/nr: 2269. / .088. /045] 31561.00 77.115 No\_date 40:00 26.97 n/a .000  
 01925+ [Vmax=.362\*Dmax= 1.727]  
 01926+ #  
 01927+ # Addition of Subwatershed 8 and Hobbs's Drain to Node 8  
 01928+ #  
 01929+ # RO025:CO0048-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 01930+ ADD HYD + 30.0 02:NH\_NYD 31561.00 66.905 No\_date 39:30 27.24 n/a .000  
 01931+ [ROUTE:30.001.out-> 30.0 02:NH\_NYD ]  
 01932+ [L/S/nr: 3982. / .075. /040] 29565.00 66.905 No\_date 39:30 27.24 n/a .000  
 01933+ #  
 01934+ # Sum of hydrographs from Node 8 routed to Node 7  
 01935+ #  
 01936+ # Section 4  
 01937+ #  
 01938+ # RO025:CO0049-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 01939+ [ROUTE CHANNEL -> 30.0 02:S\_N8 ]  
 01940+ [ROUTE:30.001.out-> 30.0 02:S\_N8 ]  
 01941+ [L/S/nr: 2269. / .088. /045] 35546.00 91.271 No\_date 39:30 26.96 n/a .000  
 01942+ #  
 01943+ # Addition of Subwatershed 7 to Node 7  
 01944+ #  
 01945+ # RO025:CO0050-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 01946+ ADD HYD + 30.0 02:NH\_NYD 35546.00 76.196 No\_date 40:00 26.96 n/a .000  
 01947+ [ROUTE:30.001.out-> 30.0 02:NH\_NYD ]  
 01948+ [L/S/nr: 2269. / .088. /045] 35546.00 91.271 No\_date 39:30 26.96 n/a .000  
 01949+ #  
 01950+ # Section 5  
 01951+ #  
 01952+ # Insertion of flow at S\_N7: N7 = S\_M7  
 01953+ # Storage area and volume were estimated from available topo maps  
 01954+ # River flow was assumed to be controlled by the downstream  
 01955+ # river cross-section for summer conditions. It was assumed that up to  
 01956+ # 0.75% of water, the main channel of the river provided the storage.  
 01957+ # Above this value, the wetland area controlled the storage.  
 01958+ #  
 01959+ # Name : H\_S7N7  
 01960+ #  
 01961+ # Insertion of a reservoir to simulate the effects of the Richmond Pen.  
 01962+ # Storage area and volume were estimated from available topo maps  
 01963+ # River flow was assumed to be controlled by the downstream  
 01964+ # river cross-section for summer conditions. It was assumed that up to  
 01965+ # 0.75% of water, the main channel of the river provided the storage.  
 01966+ # Above this value, the wetland area controlled the storage.  
 01967+ #  
 01968+ # RO025:CO0051-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 01969+ SAVE HYD + 30.0 01:S\_N7 38743.00 84.011 No\_date 44:00 26.53 n/a .000  
 01970+ #  
 01971+ # Section 6  
 01972+ #  
 01973+ # RO025:CO0054-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 01974+ [ROUTE CHANNEL -> 30.0 02:S\_NF ]  
 01975+ [ROUTE:30.001.out-> 30.0 02:S\_NF ]  
 01976+ [L/S/nr: 556. / .050. /040] 38743.00 40.725 No\_date 60:30 26.53 n/a .000  
 01977+ [Vmax=.510\*Dmax= 1.101]  
 01978+ #  
 01979+ # Addition of Subwatershed 6 and Van Gaal Drain to Node 6  
 01980+ #  
 01981+ # RO025:CO0055-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 01982+ ADD HYD + 30.0 02:NH\_NYD 38743.00 40.725 No\_date 60:30 26.53 n/a .000  
 01983+ [ROUTE:30.001.out-> 30.0 02:NH\_NYD ]  
 01984+ [L/S/nr: 1852. / .060. /045] 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 01985+ #  
 01986+ # Section 6  
 01987+ #  
 01988+ # RO025:CO0056-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 01989+ ADD HYD + 30.0 02:NH\_NYD 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 01990+ [ROUTE:30.001.out-> 30.0 02:NH\_NYD ]  
 01991+ [L/S/nr: 1852. / .060. /045] 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 01992+ #  
 01993+ # Addition of Subwatershed 5 and Flowing Creek to Node 5  
 01994+ #  
 01995+ # RO025:CO0057-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 01996+ ADD HYD + 30.0 02:NH\_NYD 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 01997+ [ROUTE:30.001.out-> 30.0 02:NH\_NYD ]  
 01998+ [L/S/nr: 1852. / .060. /045] 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 01999+ #  
 02000+ # Section 7  
 02001+ #  
 02002+ # RO025:CO0058-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02003+ ADD HYD + 30.0 02:NH\_NYD 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02004+ [ROUTE:30.001.out-> 30.0 02:NH\_NYD ]  
 02005+ [L/S/nr: 556. / .050. /040] 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02006+ #  
 02007+ # Addition of Subwatershed 6 and Van Gaal Drain to Node 6  
 02008+ #  
 02009+ # RO025:CO0059-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02010+ ADD HYD + 30.0 02:NH\_NYD 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02011+ [ROUTE:30.001.out-> 30.0 02:NH\_NYD ]  
 02012+ [L/S/nr: 4630. / .043. /036] 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02013+ #  
 02014+ # Addition of Subwatershed 4 and Leamy Creek to Node 4  
 02015+ #  
 02016+ # RO025:CO0060-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02017+ ADD HYD + 30.0 02:NH\_NYD 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02018+ [ROUTE:30.001.out-> 30.0 02:NH\_NYD ]  
 02019+ [L/S/nr: 4630. / .043. /036] 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02020+ #  
 02021+ # Addition of Subwatershed SAL and Subwatershed SA2 to Node 5A  
 02022+ #  
 02023+ # RO025:CO0061-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02024+ ADD HYD + 30.0 02:NH\_NYD 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02025+ [ROUTE:30.001.out-> 30.0 02:NH\_NYD ]  
 02026+ [L/S/nr: 4630. / .043. /036] 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02027+ #  
 02028+ # Sum of hydrographs from Node 5A routed to Node 4  
 02029+ #  
 02030+ # Section 8  
 02031+ #  
 02032+ # RO025:CO0062-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02033+ ADD HYD + 30.0 02:NH\_NYD 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02034+ [ROUTE:30.001.out-> 30.0 02:NH\_NYD ]  
 02035+ [L/S/nr: 4630. / .043. /036] 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02036+ #  
 02037+ # Addition of Subwatershed 4 and Leamy Creek to Node 4  
 02038+ #  
 02039+ # RO025:CO0063-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02040+ ADD HYD + 30.0 02:NH\_NYD 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02041+ [ROUTE:30.001.out-> 30.0 02:NH\_NYD ]  
 02042+ [L/S/nr: 4630. / .043. /036] 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02043+ #  
 02044+ # Sum of hydrographs from Node 4 routed to Node 2  
 02045+ #  
 02046+ # Section 9  
 02047+ #  
 02048+ # RO025:CO0064-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02049+ ADD HYD + 30.0 02:NH\_NYD 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02050+ [ROUTE:30.001.out-> 30.0 02:NH\_NYD ]  
 02051+ [L/S/nr: 1667. / .060. /040] 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02052+ #  
 02053+ # Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2  
 02054+ #  
 02055+ # RO025:CO0064-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02056+ ADD HYD + 30.0 02:NH\_NYD 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02057+ [ROUTE:30.001.out-> 30.0 02:NH\_NYD ]  
 02058+ [L/S/nr: 1667. / .060. /040] 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02059+ #  
 02060+ # Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2  
 02061+ #  
 02062+ # RO025:CO0065-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02063+ ADD HYD + 30.0 02:NH\_NYD 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02064+ [ROUTE:30.001.out-> 30.0 02:NH\_NYD ]  
 02065+ [L/S/nr: 1667. / .060. /040] 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02066+ #  
 02067+ # Addition of Subwatershed 1 to Node 1  
 02068+ #  
 02069+ # RO025:CO0066-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02070+ ADD HYD + 30.0 02:NH\_NYD 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02071+ [ROUTE:30.001.out-> 30.0 02:NH\_NYD ]  
 02072+ [L/S/nr: 1667. / .060. /040] 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02073+ #  
 02074+ # Addition of Subwatershed 1 to Node 1  
 02075+ #  
 02076+ # RO025:CO0067-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02077+ ADD HYD + 30.0 02:NH\_NYD 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02078+ [ROUTE:30.001.out-> 30.0 02:NH\_NYD ]  
 02079+ [L/S/nr: 1667. / .060. /040] 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02080+ #  
 02081+ # remark:flow at S\_N2 Jock River Gauge at Moodie Dr.  
 02082+ #  
 02083+ # Section 10  
 02084+ #  
 02085+ # RO025:CO0068-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02086+ ADD HYD + 30.0 02:NH\_NYD 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02087+ [ROUTE:30.001.out-> 30.0 02:NH\_NYD ]  
 02088+ [L/S/nr: 1667. / .060. /040] 40420.01 40.549 No\_date 61:30 26.53 n/a .000  
 02089+ #  
 02090+ #  
 02091+ # RUNS:COMMANDS  
 02092+ # R0505:CO0001-----START-----TZERO= 0.00 hrs on 0 0  
 02093+ # R0505:CO0001-----END-----[TZERO= 0.00 hrs on 0 0]  
 02094+ #  
 02095+ # SWMMVNO Ver:5.20/3/2001 <BETA> / INPUT DATA FILE  
 02096+ #  
 02097+ # Project Name: [Jock River] Project Number: [411-02]  
 02098+ #  
 02099+ #  
 02100+ #  
 02101+ #  
 02102+ #  
 02103+ #  
 02104+ #  
 02105+ #  
 02106+ # CALIBRATION OF SUMMER MODEL PARAMETERS  
 02107+ #  
 02108+ # CONTINUOUS SIMULATIONS  
 02109+ #  
 02110+ # Data from SWMM gauges installed at site + other gauges by the City  
 02111+ #  
 02112+ # RD0505:CO0002-----READ STORM  
 02113+ #  
 02114+ # READ STORM  
 02115+ #  
 02116+ # File name : storm.001  
 02117+ #  
 02118+ #  
 02119+ # [SDT=1.00:00:00] [DPT= 24.00:PDT= 81.51]  
 02120+ #  
 02121+ #  
 02122+ # COMPUTE API  
 02123+ # [APInit= 0.00:00:00] [APIdv= 0.00:00:00] [APIdk= 0.998]  
 02124+ # [APInav=13.33:00:00] [APIavg= 67.14: APImin= 44.87]  
 02125+ #  
 02126+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02127+ #  
 02128+ # RO0505:CO0005-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02129+ #  
 02130+ # CONTINUOUS NASHY 30.0 01:NH\_NYD 3680.00 17.963 No\_date 36:30 30.30 372 .000  
 02131+ # [IN: 64.00: 1.00: 00] [EM: 4.00: 5.00: 00] [SMAX=380.32: SKW= .010]  
 02132+ #  
 02133+ # [InterEventTime= 12.00]  
 02134+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02135+ #  
 02136+ # RO0505:CO0006-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02137+ #  
 02138+ # CONTINUOUS NASHY 30.0 01:NH\_NYD 37.00:Tp= 3.761  
 02139+ # [IN: 61.00: 1.00: 00] [EM: 3.00: 4.00: 00] [SMAX=430.01: SKW= .010]  
 02140+ #  
 02141+ # [InterEventTime= 12.00]  
 02142+ #  
 02143+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02144+ #  
 02145+ # RO0505:CO0007-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02146+ #  
 02147+ # CONTINUOUS NASHY 30.0 01:NH\_NYD 37.00:Tp= 11.33  
 02148+ # [IN: 64.00: 1.00: 00] [EM: 3.00: 4.00: 00] [SMAX=430.96: SKW= .010]  
 02149+ #  
 02150+ # [InterEventTime= 12.00]  
 02151+ #  
 02152+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02153+ #  
 02154+ # RO0505:CO0008-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02155+ #  
 02156+ # CONTINUOUS NASHY 30.0 01:NH\_NYD 37.00:Tp= 11.33  
 02157+ # [IN: 64.00: 1.00: 00] [EM: 3.00: 4.00: 00] [SMAX=430.97: SKW= .010]  
 02158+ #  
 02159+ # [InterEventTime= 12.00]  
 02160+ #  
 02161+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02162+ #  
 02163+ # RO0505:CO0009-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02164+ #  
 02165+ # CONTINUOUS NASHY 30.0 01:NH\_NYD 37.00:Tp= 5.291  
 02166+ # [IN: 64.00: 1.00: 00] [EM: 3.00: 4.00: 00] [SMAX=430.98: SKW= .010]  
 02167+ #  
 02168+ # [InterEventTime= 12.00]  
 02169+ #  
 02170+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02171+ #  
 02172+ # RO0505:CO0010-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02173+ #  
 02174+ # CONTINUOUS NASHY 30.0 01:NH\_NYD 37.00:Tp= 8.001  
 02175+ # [IN: 64.00: 1.00: 00] [EM: 3.00: 4.00: 00] [SMAX=430.99: SKW= .010]  
 02176+ #  
 02177+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02178+ #  
 02179+ # RO0505:CO0012-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02180+ #  
 02181+ # CONTINUOUS NASHY 30.0 01:NH\_NYD 37.00:Tp= 8.001  
 02182+ # [IN: 64.00: 1.00: 00] [EM: 3.00: 4.00: 00] [SMAX=430.99: SKW= .010]  
 02183+ #  
 02184+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02185+ #  
 02186+ # RO0505:CO0013-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02187+ #  
 02188+ # CONTINUOUS NASHY 30.0 01:NH\_NYD 37.00:Tp= 8.001  
 02189+ # [IN: 64.00: 1.00: 00] [EM: 3.00: 4.00: 00] [SMAX=430.99: SKW= .010]  
 02190+ #  
 02191+ # [InterEventTime= 12.00]  
 02192+ #  
 02193+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02194+ #  
 02195+ # RO0505:CO0014-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02196+ #  
 02197+ # CONTINUOUS NASHY 30.0 01:NH\_NYD 37.00:Tp= 8.001  
 02198+ # [IN: 64.00: 1.00: 00] [EM: 3.00: 4.00: 00] [SMAX=430.99: SKW= .010]  
 02199+ #  
 02200+ # [InterEventTime= 12.00]  
 02201+ #  
 02202+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02203+ #  
 02204+ # RO0505:CO0015-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02205+ #  
 02206+ # CONTINUOUS NASHY 30.0 01:NH\_NYD 37.00:Tp= 8.001  
 02207+ # [IN: 64.00: 1.00: 00] [EM: 3.00: 4.00: 00] [SMAX=430.99: SKW= .010]  
 02208+ #  
 02209+ # [InterEventTime= 12.00]  
 02210+ #  
 02211+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02212+ #  
 02213+ # RO0505:CO0016-----Dtnin-ID:NYD-----AREaha-QPEAKcms-Tpeakdate\_bh:mm:- ->RVm-R.C. ---DWFcms  
 02214+ #  
 02215+ # CONTINUOUS NASHY 30.0 01:NH\_NYD 37.00:Tp= 8.001  
 02216+ # [IN: 64.00: 1.00: 00] [EM: 3.00: 4.00: 00] [SMAX=430.99: SKW= .010]  
 02217+ #  
 02218+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02219+ #  
 02220+ # RO0505:CO00

02245# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)

02246# # of 1.61

02247# R0505:000201-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02248# CONTINUOUS NASHYD -> 30.0 01:FLC\_CW 4945.00 43.824 No\_date 33:00 38.35 .470 .000

02249# [Tdt=74.00] [Pdt=45.00] [Ipd=1.00] [Dmax=244.49] [Skw=.010]

02250# [InterEventtime= 12.00]

02251# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)

02252# R0505:000202-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02253# CONTINUOUS NASHYD -> 30.0 01:SW\_5A2 20.00 .873 No\_date 28:30 45.57 .559 .000

02254# [Cn=81.01 No: 3.00: Tp=.62] [Ipd=.00] [Dmax=.00] [Skw=.010]

02255# [InterEventtime= 12.00]

02256# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)

02257# R0505:000203-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02258# CONTINUOUS NASHYD -> 30.0 01:SW\_5A1 1412.00 8.537 No\_date 37:30 39.99 .490 .000

02259# [Ipd=80.01 No: 3.00: Tp= 8.00] [Ipd=.00] [Dmax=.00] [Skw=.010]

02260# [InterEventtime= 12.00]

02261# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)

02262# R0505:000204-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02263# CONTINUOUS NASHYD -> 30.0 01:SW\_4 585.00 12.658 No\_date 29:30 45.57 .559 .000

02264# [Ipd=80.01 No: 3.00: Tp=.62] [Ipd=.00] [Dmax=.00] [Skw=.010]

02265# [InterEventtime= 12.00]

02266# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)

02267# R0505:000205-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02268# CONTINUOUS NASHYD -> 30.0 01:IMC\_W 1021.00 16.828 No\_date 30:30 44.74 .549 .000

02269# [Cn= 80.01 No: 3.00: Tp= 2.46] [Ipd=.00] [Dmax=.00] [Skw=.010]

02270# [InterEventtime= 12.00]

02271# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)

02272# R0505:000206-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02273# CONTINUOUS NASHYD -> 30.0 01:IMC\_W 177.00 6.279 No\_date 28:30 41.48 .309 .000

02274# [Cn= 77.01 No: 3.00: Tp=.75] [Ipd=.00] [Dmax=.00] [Skw=.010]

02275# [Ipd=80.01 No: 3.00: Tp=207.66] [Skw=.010]

02276# [InterEventtime= 12.00]

02277# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)

02278# R0505:000207-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02279# CONTINUOUS NASHYD -> 30.0 01:IMC\_W 1122.00 15.311 No\_date 31:30 45.57 .559 .000

02280# [Ipd=80.01 No: 3.00: Tp= 2.46] [Ipd=.00] [Dmax=.00] [Skw=.010]

02281# [InterEventtime= 12.00]

02282# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)

02283# R0505:000208-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02284# CONTINUOUS NASHYD -> 30.0 01:MO\_D 2737.00 34.329 No\_date 31:00 40.69 .499 .000

02285# [Cn= 76.01 No: 3.00: Tp= 3.03] [Ipd=.00] [Dmax=.00] [Skw=.010]

02286# [InterEventtime= 12.00]

02287# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)

02288# R0505:000209-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02289# CONTINUOUS NASHYD -> 30.0 01:MO\_D 3176.00 37.086 No\_date 32:00 42.26 .519 .000

02290# [Cn= 78.01 No: 3.00: Tp= 3.56] [Ipd=.00] [Dmax=.00] [Skw=.010]

02291# [InterEventtime= 12.00]

02292# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)

02293# R0505:000210-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02294# CONTINUOUS NASHYD -> 30.0 01:SW\_5 2737.00 34.329 No\_date 31:00 40.69 .499 .000

02295# [Cn= 77.01 No: 3.00: Tp=.75] [Ipd=.00] [Dmax=.00] [Skw=.010]

02296# [InterEventtime= 12.00]

02297# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)

02298# R0505:000211-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02299# Starting with the addition of Jock River Headwater and Subwatershed 13

02300# [ROUTE CHANNEL -> 30.0 01:SW\_5A1 1122.00 15.311 No\_date 31:30 45.57 .559 .000]

02301# ADD HVD 30.0 02:JR\_HW 3680.00 17.963 No\_date 36:30 30.30 n/a .000

02302# [ROUTE CHANNEL -> 30.0 01:SW\_5A1 3680.00 17.963 No\_date 36:30 29.75 n/a .000]

02303# SMM+ 30.0 01:SW\_5A1 4651.00 23.037 No\_date 36:30 29.87 n/a .000

02304# # Sum of hydrographs from Node 13 routed to Node 6

02305# # Approximated cross-section - see cross-section 258

02306# # Use no.0 for summer conditions and no.025 for spring conditions

02307# # Use no.0 for winter conditions and no.025 for fall conditions

02308# R0505:00031-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02309# ROUTE CHANNEL -> 30.0 02:S\_N13 4651.00 23.017 No\_date 35:00 29.87 n/a .000

02310# [ROUTE CHANNEL -> 30.0 02:S\_N13 4651.00 23.017 No\_date 35:00 29.87 n/a .000]

02311# [ROUTE CHANNEL -> 30.0 02:S\_N13 4651.00 18.758 No\_date 38:30 29.87 n/a .000]

02312# [L/B/nr 9074. / .022/.040] [Vmax=.571 Dmax= 3.883]

02313# [Vmax=.571 Dmax= 3.883]

02314# # Routing hydrographs

02315# # Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A

02316# # Starting with the addition of Jock River Headwater and Subwatershed 13

02317# R0505:00032-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02318# ADD HVD 30.0 02:N13A 4651.00 18.758 No\_date 38:30 29.87 n/a .000

02319# [ROUTE CHANNEL -> 30.0 02:N13A 3674.00 8.540 No\_date 39:30 29.75 n/a .000]

02320# SMM+ 30.0 01:N13A 7725.00 27.242 No\_date 39:30 27.65 n/a .000

02321# # Insertion of a reservoir to simulate the effects of the Goodwood Marsh

02322# # Insertion of a reservoir to simulate the effects of the Goodwood Marsh

02323# R0505:00033-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02324# ROUTE CHANNEL -> 30.0 01:N13A 7725.00 27.242 No\_date 39:30 27.65 n/a .000

02325# SMM+ 30.0 01:N13A 7725.00 3.797 No\_date 62:30 27.65 n/a .000

02326# # Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A

02327# # Starting with the addition of Jock River Headwater and Subwatershed 13

02328# R0505:00034-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02329# ROUTE CHANNEL -> 30.0 01:N13A 7725.00 3.797 No\_date 62:30 27.65 n/a .000

02330# SMM+ 30.0 01:N13A 7725.00 7.784 No\_date 65:00 27.65 n/a .000

02331# [L/B/nr .5926 / .076/.040]

02332# [Vmax=.556 Dmax= 1.539]

02333# # Addition of Subwatershed Jock River at Ashton to Node 12

02334# R0505:00035-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02335# ROUTE CHANNEL -> 30.0 02:RS\_GM 7725.00 3.794 No\_date 65:00 27.65 n/a .000

02336# SMM+ 30.0 02:RS\_GM 7725.00 3.794 No\_date 65:00 27.65 n/a .000

02337# # Insertion of a reservoir to simulate the effects of Ashton

02338# R0505:00036-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02339# frame H\_RSNN 30.0 01:RS\_GM 7725.00 3.794 No\_date 62:30 27.65 n/a .000

02340# # Routing hydrographs

02341# # Addition of Subwatershed Jock River at Ashton to Node 12

02342# R0505:00037-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02343# ADD HVD 30.0 02:NL2 7725.00 3.794 No\_date 65:00 27.65 n/a .000

02344# [ROUTE CHANNEL -> 30.0 02:NL2 7725.00 3.794 No\_date 65:00 27.65 n/a .000]

02345# SMM+ 30.0 01:NL2 9506.00 18.583 No\_date 32:30 29.37 n/a .000

02346# # Addition of Subwatershed 5 and Ashton to Node 12

02347# R0505:00038-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02348# ROUTE CHANNEL -> 30.0 02:S\_N13 9506.00 18.583 No\_date 32:30 29.37 n/a .000

02349# SMM+ 30.0 01:S\_N13 9506.00 18.279 No\_date 32:30 29.37 n/a .000

02350# # Sum of hydrographs from Node 5 routed to Node 5A

02351# # Insertion of a reservoir to simulate the effects of the Ashton

02352# R0505:00039-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02353# frame H\_RSNN 30.0 01:RS\_GM 7725.00 3.794 No\_date 62:30 27.65 n/a .000

02354# # Routing hydrographs from Node 5A routed to Node 5

02355# # Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A

02356# R0505:00040-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02357# ADD HVD 30.0 02:N13A 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02358# [ROUTE CHANNEL -> 30.0 02:N13A 4549.01 70.588 No\_date 34:30 32.16 n/a .000]

02359# SMM+ 30.0 01:N13A 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02360# # Sum of hydrographs from Node 5A routed to Node 5

02361# # Insertion of a reservoir to simulate the effects of the Ashton

02362# R0505:00041-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02363# frame H\_RSNN 30.0 01:RS\_GM 7725.00 3.794 No\_date 62:30 27.65 n/a .000

02364# # Routing hydrographs from Node 5A1 and 5A2 to Node 5A

02365# # Addition of Subwatershed 5A1 and 5A2 to Node 5A

02366# R0505:00042-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02367# ADD HVD 30.0 02:N13A 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02368# [ROUTE CHANNEL -> 30.0 02:N13A 4549.01 70.588 No\_date 34:30 32.16 n/a .000]

02369# SMM+ 30.0 01:N13A 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02370# # Sum of hydrographs from Node 5A1 and 5A2 to Node 5A

02371# # Insertion of a reservoir to simulate the effects of the Ashton

02372# R0505:00043-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02373# ADD HVD 30.0 02:N13A 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02374# [ROUTE CHANNEL -> 30.0 02:N13A 4549.01 70.588 No\_date 34:30 32.16 n/a .000]

02375# SMM+ 30.0 01:N13A 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02376# # Addition of Subwatershed 5 and Ashton to Node 4

02377# R0505:00044-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02378# ADD HVD 30.0 02:NL2 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02379# [ROUTE CHANNEL -> 30.0 02:NL2 4549.01 70.588 No\_date 34:30 32.16 n/a .000]

02380# SMM+ 30.0 01:NL2 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02381# # Sum of hydrographs from Node 4 routed to Node 2

02382# # Insertion of a reservoir to simulate the effects of the Ashton

02383# R0505:00045-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02384# ADD HVD 30.0 02:RS\_GM 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02385# [ROUTE CHANNEL -> 30.0 02:RS\_GM 4549.01 70.588 No\_date 34:30 32.16 n/a .000]

02386# SMM+ 30.0 01:RS\_GM 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02387# # Sum of hydrographs from Node 2 to Node 2

02388# # Insertion of a reservoir to simulate the effects of the Ashton

02389# R0505:00046-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02390# ADD HVD 30.0 02:NL2 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02391# [ROUTE CHANNEL -> 30.0 02:NL2 4549.01 70.588 No\_date 34:30 32.16 n/a .000]

02392# SMM+ 30.0 01:NL2 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02393# # Sum of hydrographs from Node 2 to Node 2

02394# # Insertion of a reservoir to simulate the effects of the Ashton

02395# R0505:00047-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02396# ADD HVD 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02397# [ROUTE CHANNEL -> 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000]

02398# SMM+ 30.0 01:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02399# # Sum of hydrographs from Node 2 to Node 2

02400# # Insertion of a reservoir to simulate the effects of the Ashton

02401# R0505:00048-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02402# ADD HVD 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02403# [ROUTE CHANNEL -> 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000]

02404# SMM+ 30.0 01:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02405# # Sum of hydrographs from Node 2 to Node 2

02406# # Insertion of a reservoir to simulate the effects of the Ashton

02407# R0505:00049-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02408# ADD HVD 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02409# [ROUTE CHANNEL -> 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000]

02410# SMM+ 30.0 01:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02411# # Sum of hydrographs from Node 2 to Node 2

02412# # Insertion of a reservoir to simulate the effects of the Ashton

02413# R0505:00050-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02414# ADD HVD 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02415# [ROUTE CHANNEL -> 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000]

02416# SMM+ 30.0 01:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02417# # Sum of hydrographs from Node 2 to Node 2

02418# # Insertion of a reservoir to simulate the effects of the Ashton

02419# R0505:00051-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02420# ADD HVD 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02421# [ROUTE CHANNEL -> 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000]

02422# SMM+ 30.0 01:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02423# # Sum of hydrographs from Node 2 to Node 2

02424# # Insertion of a reservoir to simulate the effects of the Ashton

02425# R0505:00052-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02426# ADD HVD 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02427# [ROUTE CHANNEL -> 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000]

02428# SMM+ 30.0 01:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02429# # Sum of hydrographs from Node 2 to Node 2

02430# # Insertion of a reservoir to simulate the effects of the Ashton

02431# R0505:00053-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02432# ADD HVD 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02433# [ROUTE CHANNEL -> 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000]

02434# SMM+ 30.0 01:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02435# # Sum of hydrographs from Node 2 to Node 2

02436# # Insertion of a reservoir to simulate the effects of the Ashton

02437# R0505:00054-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02438# ADD HVD 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02439# [ROUTE CHANNEL -> 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000]

02440# SMM+ 30.0 01:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02441# # Sum of hydrographs from Node 2 to Node 2

02442# # Insertion of a reservoir to simulate the effects of the Ashton

02443# R0505:00055-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02444# ADD HVD 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02445# [ROUTE CHANNEL -> 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000]

02446# SMM+ 30.0 01:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02447# # Sum of hydrographs from Node 2 to Node 2

02448# # Insertion of a reservoir to simulate the effects of the Ashton

02449# R0505:00056-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02450# ADD HVD 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02451# [ROUTE CHANNEL -> 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000]

02452# SMM+ 30.0 01:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02453# # Sum of hydrographs from Node 2 to Node 2

02454# # Insertion of a reservoir to simulate the effects of the Ashton

02455# R0505:00057-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02456# ADD HVD 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02457# [ROUTE CHANNEL -> 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000]

02458# SMM+ 30.0 01:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02459# # Sum of hydrographs from Node 2 to Node 2

02460# # Insertion of a reservoir to simulate the effects of the Ashton

02461# R0505:00058-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02462# ADD HVD 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02463# [ROUTE CHANNEL -> 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000]

02464# SMM+ 30.0 01:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02465# # Sum of hydrographs from Node 2 to Node 2

02466# # Insertion of a reservoir to simulate the effects of the Ashton

02467# R0505:00059-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02468# ADD HVD 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02469# [ROUTE CHANNEL -> 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000]

02470# SMM+ 30.0 01:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02471# # Sum of hydrographs from Node 2 to Node 2

02472# # Insertion of a reservoir to simulate the effects of the Ashton

02473# R0505:00060-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02474# ADD HVD 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02475# [ROUTE CHANNEL -> 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000]

02476# SMM+ 30.0 01:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02477# # Sum of hydrographs from Node 2 to Node 2

02478# # Insertion of a reservoir to simulate the effects of the Ashton

02479# R0505:00061-----Dtnin:ID:NHYD-----ARAhA-QPEAKcms-TpeakDate\_bh:mm:--RvNm-R.C.--DWFcms

02480# ADD HVD 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02481# [ROUTE CHANNEL -> 30.0 02:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000]

02482# SMM+ 30.0 01:NL1 4549.01 70.588 No\_date 34:30 32.16 n/a .000

02483# # Sum of hydrographs from Node 2 to Node 2

02484# #

02619: Comment + plus RCS de 24 hrs 1:100 ans pour Ottawa CDA  
02620: [SDT=1.00:00:00]-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
02621: R1010:00003:-->CONTINUOUS\_NASHVY...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
02622: [IARBC4: 1.00:00:00]-->TSHTFNT\_960.00\_min [ ]  
02623: [SDT=10.00:00:00]-->ROUTE CHANNEL...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
02624: R1010:00004:-->COMPUTE API  
02625: [APMin1= 50.00: AD1kdyv...= 8500: APIdkyv...= 9989]  
[APMin2=119.84: ADlavg...= 69.19: APMin4= 44.87]  
02626: #  
02627: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
02628: [APMin1= 50.00: AD1kdyv...= 8500: APIdkyv...= 9989]  
[APMin2=119.84: ADlavg...= 69.19: APMin4= 44.87]  
02629: #  
02630: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
02631: R1010:00005:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
02632: CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3680.00 21.054 No\_Date 36:30 35.15 .397 .000  
02633: [IARBC4: 0.00: SMID\_57.05: SMAX=380.32: SK\_ .010]  
02634: #  
02635: [InterEventTime: 12.00]  
02636: #  
02637: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
02638: [APMin1= 50.00: AD1kdyv...= 8500: APIdkyv...= 9989]  
[APMin2=119.84: ADlavg...= 69.19: APMin4= 44.87]  
02639: #  
02640: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
02641: R1010:00006:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
02642: CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3680.00 21.054 No\_Date 36:30 35.15 .397 .000  
02643: [CN\_60.00: N\_ 3.00: Tp\_3.761]  
02644: #  
02645: [InterEventTime: 12.00]  
02646: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
02647: #  
02648: R1010:00007:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3680.00 21.054 No\_Date 36:30 35.15 .397 .000  
02649: [CN\_55.00: N\_ 3.00: Tp\_11.33]  
02650: [CN\_60.00: N\_ 3.00: Tp\_4.00]  
02651: [IARBC4: 0.00: SMID\_83.24: SMAX=554.96: SK\_ .010]  
02652: #  
02653: R1010:00008:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_ASH 1781.00 19.356 No\_Date 32:30 42.46 .479 .000  
02654: [CN\_60.00: N\_ 3.00: Tp\_3.91]  
02655: [CN\_60.00: N\_ 3.00: Tp\_1.33]  
02656: [IARBC4: 0.00: SMID\_59.75: SMAX=264.99: SK\_ .010]  
02657: #  
02658: R1010:00009:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:SW\_11 500.00 10.499 No\_Date 29:00 36.74 .415 .000  
02659: [CN\_60.00: N\_ 3.00: Tp\_2.41]  
02660: [IARBC4: 0.00: SMID\_52.62: SMAX=350.79: SK\_ .010]  
02661: #  
02662: [InterEventTime: 12.00]  
02663: #  
02664: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
02665: #  
02666: R1010:00010:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:NC\_KX 1537.00 14.197 No\_Date 34:00 35.74 .415 .000  
02667: [CN\_60.00: N\_ 3.00: Tp\_5.29]  
02668: [IARBC4: 0.00: SMID\_52.62: SMAX=350.79: SK\_ .010]  
02669: #  
02670: [InterEventTime: 12.00]  
02671: #  
02672: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
02673: #  
02674: R1010:00011:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 5666.00 36.360 No\_Date 37:30 42.46 .479 .000  
02675: [CN\_72.00: N\_ 3.00: Tp\_8.00]  
02676: [IARBC4: 0.00: SMID\_39.75: SMAX=264.99: SK\_ .010]  
02677: #  
02678: [InterEventTime: 12.00]  
02679: #  
02680: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
02681: #  
02682: R1010:00012:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 8376.00 34.456 No\_Date 39:30 36.74 .415 .000  
02683: [CN\_70.00: N\_ 3.00: Tp\_2.51]  
02684: [IARBC4: 0.00: SMID\_52.62: SMAX=287.10: SK\_ .010]  
02685: #  
02686: [InterEventTime: 12.00]  
02687: #  
02688: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
02689: #  
02690: R1010:00013:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 1132.00 16.257 No\_Date 30:30 40.80 .461 .000  
02691: [CN\_70.00: N\_ 3.00: Tp\_1.66]  
02692: [IARBC4: 0.00: SMID\_52.62: SMAX=287.10: SK\_ .010]  
02693: #  
02694: [InterEventTime: 12.00]  
02695: #  
02696: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
02697: #  
02698: R1010:00014:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 4464.00 17.270 No\_Date 39:30 33.59 .379 .000  
02699: [CN\_62.00: N\_ 3.00: Tp\_11.33]  
02700: [IARBC4: 0.00: SMID\_52.62: SMAX=412.66: SK\_ .010]  
02701: #  
02702: [InterEventTime: 12.00]  
02703: #  
02704: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
02705: #  
02706: R1010:00015:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3854.00 20.590 No\_Date 38:00 36.74 .415 .000  
02707: [CN\_57.00: N\_ 3.00: Tp\_8.42]  
02708: [IARBC4: 0.00: SMID\_52.62: SMAX=350.79: SK\_ .010]  
02709: #  
02710: [InterEventTime: 12.00]  
02711: #  
02712: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
02713: #  
02714: R1010:00016:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 1392.00 16.027 No\_Date 36:00 29.76 .336 .000  
02715: [CN\_60.00: N\_ 3.00: Tp\_1.66]  
02716: [IARBC4: 0.00: SMID\_52.62: SMAX=287.10: SK\_ .010]  
02717: #  
02718: [InterEventTime: 12.00]  
02719: #  
02720: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
02721: #  
02722: R1010:00017:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3197.00 16.027 No\_Date 36:00 29.76 .336 .000  
02723: [CN\_60.00: N\_ 3.00: Tp\_6.65]  
02724: [IARBC4: 0.00: SMID\_50.55: SMAX=336.97: SK\_ .010]  
02725: #  
02726: [InterEventTime: 12.00]  
02727: #  
02728: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
02729: #  
02730: R1010:00018:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 165.00 1.462 No\_Date 33:00 37.54 .424 .000  
02731: [CN\_67.00: N\_ 3.00: Tp\_4.18]  
02732: [IARBC4: 0.00: SMID\_50.55: SMAX=396.11: SK\_ .010]  
02733: #  
02734: [InterEventTime: 12.00]  
02735: #  
02736: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
02737: #  
02738: R1010:00019:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 1332.00 10.635 No\_Date 35:00 42.46 .479 .000  
02739: [CN\_57.00: N\_ 3.00: Tp\_6.65]  
02740: [IARBC4: 0.00: SMID\_52.62: SMAX=508.81: SK\_ .010]  
02741: #  
02742: [InterEventTime: 12.00]  
02743: #  
02744: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
02745: #  
02746: R1010:00020:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 322.00 9.294 No\_Date 28:30 47.59 .537 .000  
02747: [CN\_57.00: N\_ 3.00: Tp\_7.51]  
02748: [IARBC4: 0.00: SMID\_52.62: SMAX=207.66: SK\_ .010]  
02749: #  
02750: [InterEventTime: 12.00]  
02751: #  
02752: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
02753: #  
02754: R1010:00021:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 1332.00 9.444 No\_Date 30:30 44.15 .498 .000  
02755: [CN\_74.00: N\_ 3.00: Tp\_4.45]  
02756: [IARBC4: 0.00: SMID\_56.67: SMAX=244.49: SK\_ .010]  
02757: #  
02758: R1010:00022:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 20.00 1.014 No\_Date 28:30 52.03 .587 .000  
02759: [CN\_60.00: N\_ 3.00: Tp\_6.65]  
02760: [IARBC4: 0.00: SMID\_52.62: SMAX=168.09: SK\_ .010]  
02761: #  
02762: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
02763: #  
02764: R1010:00023:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 1412.00 9.884 No\_Date 37:30 45.85 .518 .000  
02765: [CN\_60.00: N\_ 3.00: Tp\_4.45]  
02766: [IARBC4: 0.00: SMID\_33.81: SMAX=225.43: SK\_ .010]  
02767: #  
02768: [InterEventTime: 12.00]  
02769: R1010:00024:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 177.00 7.344 No\_Date 28:30 47.59 .537 .000  
02770: [CN\_60.00: N\_ 3.00: Tp\_7.51]  
02771: #  
02772: R1010:00025:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 1122.00 17.710 No\_Date 31:30 52.03 .587 .000  
02773: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02774: [IARBC4: 0.00: SMID\_21: SMAX=168.09: SK\_ .010]  
02775: #  
02776: [InterEventTime: 12.00]  
02777: #  
02778: R1010:00026:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 1021.00 19.515 No\_Date 30:30 51.13 .577 .000  
02779: [CN\_76.00: N\_ 3.00: Tp\_3.03]  
02780: [IARBC4: 0.00: SMID\_46.32: SMAX=216.39: SK\_ .010]  
02781: #  
02782: R1010:00027:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 317.00 43.079 No\_Date 32:00 48.46 .547 .000  
02783: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02784: [IARBC4: 0.00: SMID\_29.88: SMAX=199.22: SK\_ .010]  
02785: #  
02786: [InterEventTime: 12.00]  
02787: #  
02788: R1010:00028:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 2737.00 40.026 No\_Date 31:00 46.72 .527 .000  
02789: [CN\_76.00: N\_ 3.00: Tp\_3.03]  
02790: #  
02791: R1010:00029:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3680.00 21.054 No\_Date 36:30 35.15 .518 .000  
02792: [AQR\_HY...= 1.00:00:00]  
02793: # Starting with the addition of Jock River Headwater and Subwatershed 13

02794: R1010:00030:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02795: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02796: [IARBC4: 0.00: SMID\_29.88: SMAX=199.22: SK\_ .010]  
02797: #  
02798: R1010:00031:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02799: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02800: # Routing hydrographs

02801: # Starting with the addition of Jock River Headwater and Subwatershed 13

02802: R1010:00032:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3680.00 21.054 No\_Date 36:30 35.15 .518 .000  
02803: [AQR\_HY...= 1.00:00:00]  
02804: # Starting with the addition of Jock River Headwater and Subwatershed 13

02805: R1010:00033:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02806: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02807: #  
02808: R1010:00034:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02809: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02810: #  
02811: R1010:00035:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02812: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02813: #  
02814: R1010:00036:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02815: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02816: #  
02817: R1010:00037:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02818: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02819: #  
02820: R1010:00038:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02821: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02822: #  
02823: R1010:00039:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02824: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02825: #  
02826: R1010:00040:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02827: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02828: #  
02829: R1010:00041:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02830: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02831: #  
02832: R1010:00042:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02833: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02834: #  
02835: R1010:00043:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02836: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02837: #  
02838: R1010:00044:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02839: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02840: #  
02841: R1010:00045:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02842: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02843: #  
02844: R1010:00046:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02845: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02846: #  
02847: R1010:00047:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02848: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02849: #  
02850: R1010:00048:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02851: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02852: #  
02853: R1010:00049:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02854: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02855: #  
02856: R1010:00050:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02857: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02858: #  
02859: R1010:00051:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02860: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02861: #  
02862: R1010:00052:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02863: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02864: #  
02865: R1010:00053:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02866: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02867: #  
02868: R1010:00054:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02869: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02870: #  
02871: R1010:00055:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02872: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02873: #  
02874: R1010:00056:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02875: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02876: #  
02877: R1010:00057:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02878: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02879: #  
02880: R1010:00058:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02881: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02882: #  
02883: R1010:00059:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
02884: [CN\_81.00: N\_ 3.00: Tp\_12.00]  
02885: #  
02886: R1010:00060:-->DTRIN-ID:NHYW...-->AREBha-QPakcms-TpeakDate\_hh:mm-->RvNm-R.C...--DWFcm5  
CONTINUOUS\_NASHVY...-->30.01:01:JR\_KW 3176.00 43.079 No\_Date 32:00 48.46 .547 .000  
028

```

02993> # Sum of hydrographs from Node 6 routed to Node 5
02994> # Section 5
02995> # Dtnin-ID:NHYD-----ARRAha-QPEAKcms-Tpeakdate_bh:mm:---RVm=R.C.---DWFcms
02996> ROUTE CHANNEL -> 30.0 02:S.NS 40240.01 60.497 No_date 59:30 36.31 n/a .000
02997> [ROT=30.00] out-> 30.0 01:NS 40240.01 60.383 No_date 59:30 36.31 n/a .000
02998> [L/S/nr 160. / .084/.040]
02999> [Vmax=.430 Dmax=.141]
03000> # (Vmax=.430 Dmax=.141)
03002> #
03004> # Addition of Subwatershed 5 and Flowing Creek to Node 5
03005> # Dtnin-ID:NHYD-----ARRAha-QPEAKcms-Tpeakdate_bh:mm:---RVm=R.C.---DWFcms
03006> ADD HYD 40240.01 60.493 No_date 59:30 36.17 n/a .000
03007> + 30.0 02:SM_5 224.00 12.294 No_date 28:30 47.59 n/a .000
03008> + 30.0 02:FL_CK 4945.00 51.121 No_date 33:00 44.15 n/a .000
03009> SUM 30.0 01:S.NS 45409.01 79.891 No_date 34:00 37.22 n/a .000
03010> #
03011> # Sum of hydrographs from Node 5 routed to Node 5A
03012> # Section 7
03013> #
03014> # Dtnin-ID:NHYD-----ARRAha-QPEAKcms-Tpeakdate_bh:mm:---RVm=R.C.---DWFcms
03015> ROUTE CHANNEL -> 30.0 02:S.NS 45409.01 79.891 No_date 34:00 37.22 n/a .000
03016> [ROT=30.00] out-> 30.0 01:NSA 45409.01 79.833 No_date 34:00 37.22 n/a .000
03017> [L/S/nr .556. / .050/.040]
03018> [Vmax=.544 Dmax=1.346]
03019> #
03020> # Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
03021> #
03022> # Dtnin-ID:NHYD-----ARRAha-QPEAKcms-Tpeakdate_bh:mm:---RVm=R.C.---DWFcms
03023> ADD HYD 30.0 02:NSA 45409.01 79.815 No_date 34:00 37.22 n/a .000
03024> + 30.0 02:SM_5A2 20.00 1.020 No_date 34:00 37.22 n/a .000
03025> + 30.0 02:SM_5A 1412.00 9.884 No_date 37:30 45.85 n/a .000
03026> SUM 30.0 01:S.NSA 46841.01 88.619 No_date 34:30 37.48 n/a .000
03027> #
03028> # Sum of hydrographs from Node 5A routed to Node 4
03029> # Section 8
03030> #
03031> # Dtnin-ID:NHYD-----ARRAha-QPEAKcms-Tpeakdate_bh:mm:---RVm=R.C.---DWFcms
03032> ROUTE CHANNEL -> 30.0 02:S.NSA 46841.01 88.619 No_date 34:30 37.48 n/a .000
03033> [ROT=30.00] out-> 30.0 01:SM_3A4 46841.01 88.595 No_date 34:30 37.48 n/a .000
03034> [L/S/nr .4630. / .043/.036]
03035> [Vmax=.401 Dmax=3.849]
03036> #
03037> # Addition of Subwatershed 4 and Leamy Creek to Node 4
03038> #
03039> # Dtnin-ID:NHYD-----ARRAha-QPEAKcms-Tpeakdate_bh:mm:---RVm=R.C.---DWFcms
03040> ADD HYD 30.0 02:SM_4 46841.01 84.955 No_date 36:00 37.48 n/a .000
03041> + 30.0 02:SM_4 585.00 14.684 No_date 29:30 52.03 n/a .000
03042> + 30.0 02:FL_CK 1202.00 20.000 No_date 30:00 46.72 n/a .000
03043> SUM 30.0 01:S.N4 48447.00 69.694 No_date 34:30 37.95 n/a .000
03044> # Dtnin-ID:NHYD-----ARRAha-QPEAKcms-Tpeakdate_bh:mm:---RVm=R.C.---DWFcms
03045> SAVE HYD 30.0 01:S.N4 48447.00 95.694 No_date 34:30 37.95 n/a .000
03046> name : S_N4_0100
03047> remark:flow at S_N4
03048> #
03049> # Sum of hydrographs from Node 4 routed to Node 2
03050> # Section 9
03051> #
03052> # Dtnin-ID:NHYD-----ARRAha-QPEAKcms-Tpeakdate_bh:mm:---RVm=R.C.---DWFcms
03053> ROUTE CHANNEL -> 30.0 02:S.N4 48447.00 95.694 No_date 34:30 37.95 n/a .000
03054> [ROT=30.00] out-> 30.0 01:SM_3 48447.00 95.382 No_date 35:00 37.95 n/a .000
03055> [L/S/nr 1667. / .060/.040]
03056> [Vmax=.3942 Dmax=3.915]
03057> #
03058> # Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2
03059> #
03060> # Dtnin-ID:NHYD-----ARRAha-QPEAKcms-Tpeakdate_bh:mm:---RVm=R.C.---DWFcms
03061> ADD HYD 30.0 02:NZ2 48447.00 95.342 No_date 35:00 37.95 n/a .000
03062> + 30.0 02:SM_3 177.00 1.000 No_date 35:00 37.95 n/a .000
03063> + 30.0 02:SM_DR 1122.00 17.710 No_date 31:30 52.03 n/a .000
03064> + 30.0 02:MD_DR 2737.00 40.026 No_date 31:00 46.72 n/a .000
03065> SUM 30.0 01:S.N2 52483.00 141.415 No_date 32:30 38.74 n/a .000
03066> # Dtnin-ID:NHYD-----ARRAha-QPEAKcms-Tpeakdate_bh:mm:---RVm=R.C.---DWFcms
03067> SAVE HYD 30.0 01:S.N2 52483.00 141.415 No_date 32:30 38.74 n/a .000
03068> name : M_HNZ2
03069> remark:flow at S_M2 Jock River Gauge at Moodie Dr.
03070> #
03071> # Sum of hydrographs from Node 2 routed to Node 1
03072> # Section 10
03073> #
03074> # Dtnin-ID:NHYD-----ARRAha-QPEAKcms-Tpeakdate_bh:mm:---RVm=R.C.---DWFcms
03075> ROUTE CHANNEL -> 30.0 02:S.N2 52483.00 141.415 No_date 32:30 38.74 n/a .000
03076> [ROT=30.00] out-> 30.0 01:H1 52483.00 124.304 No_date 35:00 38.74 n/a .000
03077> [L/S/nr .4100. / .050/.040]
03078> [Vmax=1.091 Dmax=4.553]
03079> #
03080> # Addition of Subwatershed 1 to Node 1
03081> #
03082> # Dtnin-ID:NHYD-----ARRAha-QPEAKcms-Tpeakdate_bh:mm:---RVm=R.C.---DWFcms
03083> ADD HYD 30.0 02:N1 52483.00 124.304 No_date 35:00 38.74 n/a .000
03084> + 30.0 02:SM_1 3176.00 43.079 No_date 32:00 48.46 n/a .000
03085> SUM 30.0 01:H1 55659.00 158.420 No_date 35:00 38.74 n/a .000
03086> # Dtnin-ID:NHYD-----ARRAha-QPEAKcms-Tpeakdate_bh:mm:---RVm=R.C.---DWFcms
03087> SAVE HYD 30.0 01:H1 55659.00 158.420 No_date 34:00 39.29 n/a .000
03088> name : H1_O1H
03089> remark:total outflow of Jock River
03090> #####=====
03091> # Dtnin-ID:NHYD-----ARRAha-QPEAKcms-Tpeakdate_bh:mm:---RVm=R.C.---DWFcms
03092> ROUTE CHANNEL -> 30.0 02:S.N2 55659.00 158.420 No_date 34:00 39.29 n/a .000
03093> FINISH
03094> #
03095> ****WARNING: / ERRORS / NOTES
03096> #
03097> R0021:C00015 CONTINUOUS NASHYD
03098> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03099> R0021:C00020 CONTINUOUS NASHYD
03100> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03101> R0021:C00022 CONTINUOUS NASHYD
03102> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03103> R0021:C00024 CONTINUOUS NASHYD
03104> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03105> R0021:C00015 CONTINUOUS NASHYD
03106> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03107> R0021:C00020 CONTINUOUS NASHYD
03108> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03109> R0021:C00024 CONTINUOUS NASHYD
03110> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03111> R0021:C00015 CONTINUOUS NASHYD
03112> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03113> R0021:C00020 CONTINUOUS NASHYD
03114> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03115> R0021:C00024 CONTINUOUS NASHYD
03116> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03117> R0021:C00015 CONTINUOUS NASHYD
03118> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03119> R0021:C00020 CONTINUOUS NASHYD
03120> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03121> R0021:C00024 CONTINUOUS NASHYD
03122> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03123> R0021:C00015 CONTINUOUS NASHYD
03124> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03125> R0021:C00020 CONTINUOUS NASHYD
03126> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03127> R0021:C00024 CONTINUOUS NASHYD
03128> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03129> R0021:C00015 CONTINUOUS NASHYD
03130> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03131> R0021:C00020 CONTINUOUS NASHYD
03132> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03133> R0021:C00024 CONTINUOUS NASHYD
03134> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03135> R0021:C00015 CONTINUOUS NASHYD
03136> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03137> R0101:C00015 CONTINUOUS NASHYD
03138> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03139> R0101:C00020 CONTINUOUS NASHYD
03140> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03141> R0101:C00024 CONTINUOUS NASHYD
03142> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03143> R0101:C00015 CONTINUOUS NASHYD
03144> *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03145> Simulation ended on 2021-02-22 at 15:43:22
03146> =====

```



Ottawa. ON  
Paris. ON  
Gatineau. QC  
Montréal. QC  
Québec. QC

# Attachment B

Model 2 – Jock River Reach One Model

Stantec, 2007

SWMHYMO Input & Summary files

```

1   2      Metric units
2   *#*****
3   *# Project Name: [Jock River Reach 1 SubWatershed Study]Project #: [160400414]
4   *# Date       : October 2006
5   *# Modeller    : [Navin Gautam/ Original by Ana M Paerez]
6   *# Company     : Stantec.
7   *# License #   : 3824306
8   *#*****
9   START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[002]
10  *%              [ "C24SC002.stm" ] <--storm filename, one per line for NSTORM time
11  *#-----|-----|
12  READ STORM      STORM_FILENAME=[ "storm.001" ]
13  *%-----|-----|
14  MODIFY STORM    ICASEms=[1], NSHIFT=[96],
15                  RedFACT=[1],
16  *%-----|-----|
17  DEFAULT VALUES  ICASEdv=[1], read and print values
18                  DEFVAL_FILENAME=[ "MODIFIED.VAL" ]
19  COMPUTE API     APII=[50], APIK=[.85]/day
20  *#*****
21  *#
22  *#          JOCK RIVER REACH 1 SUBWATERSHED STUDY DISCRETIZED MODEL
23  *#          PROPOSED CONDITIONS DESIGN STORM MODEL (SUMMER)
24  *#
25  *# Version: Draft Final Report, October 2006
26  *# Revision History
27  *# -Draft Interim Condition Report, Nov. 2005
28  *#*****
29  *# Assumptions
30  *# - All catchments are assumed to be developed except S-1, S-2, and SW-1a
31  *# - SWM facilities are modeled
32  *# - Rating curves were estimated based on existing reports and modeling for the
33  *# proposed SWM facilities
34  *# - The rating curve for the existing Kennedy Burnett SWM Facility was obtained from
35  *# the Urban Runoff Treatment in the Kennedy Burnett Settling Pond (URTKBP)- Regional
36  *# Municipality of Ottawa Carleton, March 1983
37  *# - River routing modeled
38  *# - River cross sections obtained from RVCA's HEC-RAS hydraulic model
39  *#-----|-----|
40  *# Parameters
41  *# - Design Storms: 2,5,10,25,50 & 100yr events: 24hr SCS (DT=10min)-model comparison
42  *# - Impervious area weighted based on: rural subdivision @20%, urban @55%
43  *# - NRCS(SCS) CN based on landuse (airphoto) and soil type (base mapping)
44  *# - Time to peak using Uplands Method
45  *#-----|-----|
46  *#*****
47  *#Read hydrograph upstream of N2 from RVCA Jock R. floodrisk watershed modeling
48  *#*****
49  READ HYD         ID=[ 1 ], NYHD=[ "S_N2" ],
50                  HYD_FILENAME=[ "H-S_N2" ]
51  *%-----|-----|
52  *#
53  *# Hydrograph from Node 2 routed to Node 416
54  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 9025
55  *#
56  ROUTE CHANNEL    IDout=[4], NYHD=[ "N_416" ] ,IDin=[1] ,
57                  RDT=[10](min),
58                  CHLGTH=[2327](m), CHSLOPE=[0.0498](%),
59                  FPSLOPE=[0.0498](%),
60                  SECNUM=[1.0], NSEG=[3]
61                  ( SEGROUGH, SEGDIST (m))=
62                  [0.075,-23.96
63                  -0.055,23.96
64                  0.075,157.38] NSEG times
65                  ( DISTANCE (m), ELEVATION (m))=
66                  [-336.97,93.5]

```

```

67 [-318.85,93]
68 [-259,92.5]
69 [-133.18,92]
70 [-33.17,92]
71 [-27.21,92]
72 [-26.14,91.5]
73 [-24.99,91]
74 [-23.96,90.5]
75 [-14.33,88.26]
76 [-0.68,88.12]
77 [14.33,88.26]
78 [23.96,90.5]
79 [32.12,91]
80 [43.74,91.5]
81 [57.09,92]
82 [73.53,92.5]
83 [108.27,93]
84 [125.88,93.5]
85 [144.81,94]
86 [157.38,94.5]
87 *%-----|-----|
88 *#*****
89 *# Catchment SW-1a
90 *# - Portion of RVCA catchment SW_1 outside of Reach 1 subwatershed
91 *# - Undeveloped agricultural land
92 *#*****
93 CONTINUOUS NASHYD ID=[2], NHYD=["SW_1a"], DT=[5]min, AREA=[546](ha),
94 DWF=[0](cms), CN/C=[72], IA=[4.67](mm),
95 N=[3], TP=[2.79]hrs,
96 Continuous simulation parameters:
97 IaRECper=[4](hrs),
98 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
99 InterEventTime=[12](hrs)
100 Baseflow simulation parameters:
101 BaseFlowOption=[1],
102 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
103 VHydCond=[0.055](mm/hr), END=-1
104 *%-----|-----|
105 ADD HYD IDsum=[ 3 ], NHYD=["SN_416"], IDs to add=[4,2]
106 *%-----|-----|
107 SAVE HYD ID=[ 3 ], # OF PCYCLES=[-1], ICASEsh=[1]
108 HYD_COMMENT=["Total Flows at Highway 416"]
109 *%-----|-----|
110 *#
111 *# Hydrograph from Node 416 routed to Node at Okeefe drain
112 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 7245
113 *#
114 ROUTE CHANNEL IDout=[1], NHYD=[ "N_OK" ] ,IDin=[3] ,
115 RDT=[5](min),
116 CHLGTH=[497](m), CHSLOPE=[0.3018](%),
117 FPSLOPE=[0.3018](%),
118 SECNUM=[1.0], NSEG=[3]
119 ( SEGROUGH, SEGDIST (m))=
120 [0.075,-19.40
121 -0.055,19.40
122 0.075,377.02] NSEG times
123 ( DISTANCE (m), ELEVATION (m))=
124 [-1062.81, 93.00]
125 [-1061.41, 92.50]
126 [-945.91, 92.00]
127 [-783.64, 91.50]
128 [-136.74, 91.00]
129 [-134.06, 91.00]
130 [-128.97, 91.00]
131 [-86.04, 91.00]
132 [-20.86, 91.00]

```

```

133 [-20.18, 90.50]
134 [-19.40, 90.00]
135 [-11.68, 86.89]
136 [0.00, 86.10]
137 [12.09, 86.81]
138 [19.40, 90.00]
139 [34.68, 90.50]
140 [60.56, 91.00]
141 [170.14, 91.00]
142 [175.05, 90.50]
143 [180.29, 90.00]
144 [193.41, 90.00]
145 [195.98, 90.50]
146 [377.02, 92.50]
147 *%-----|-----|
148 *#*****
149 *#      Catchment OKEEFE
150 *#      - To O'Keefe drain (north of the Jock)
151 *#      - Developed with assumed 43% imp.
152 *#*****
153 CONTINUOUS STANDHYD ID=[2], NHYD=["OKEEFE"], DT=[5](min), AREA=[448](ha),
154 XIMP=[0.43], TIMP=[0.43], DWF=[0](cms), LOSS=[2],
155 SCS curve number CN=[77],
156 Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
157 LGP=[40](m), MNP=[0.25], SCP=[0](min),
158 Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
159 LGI=[1728](m), MNI=[0.013], SCI=[0](min),
160 Continuous simulation parameters:
161 IaRECper=[4](hrs), IaREClmp=[4](hrs),
162 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
163 InterEventTime=[18](hrs), END=-1
164
165 *#*****
166 *#      Okeefe Pond
167 *#      - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
168 *#      and a ratio of the catchment area to the West Clarke pond rating curve
169 *#      from the MSS for the next coordinates
170 *#*****
171 ROUTE RESERVOIR IDout=[4], NHYD=["P_OKE"], IDin=[2],
172 RDT=[5](min),
173             TABLE of ( OUTFLOW-STORAGE ) values
174             (cms) - (ha-m)
175             [ 0.0 , 0.0 ]
176             [ 0.20 , 1.72 ]
177             [ -1 , -1 ] (max twenty pts)
178 IDovf=[9], NHYDovf=["ok-OVF"]
179
180 *%-----|-----|
181 ADD HYD IDsum=[ 3 ], NHYD=["SN_OK"], IDs to add=[1,4,9]
182 *%-----|-----|
183 SAVE HYD ID=[ 3 ], # OF PCYCLES=[-1], ICASEsh=[1]
184             HYD_COMMENT=["Total Flows at Okeefe Drain"]
185 *%-----|-----|
186 *#
187 *# Hydrograph from Node Okeefe routed to Node at Foster Drain
188 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
189 *#
190 ROUTE CHANNEL IDout=[1], NHYD=["N_FO"] ,IDin=[3] ,
191 RDT=[5](min),
192 CHLGTH=[1183](m), CHSLOPE=[0.0761](%),
193             FPSLOPE=[0.0761](%),
194 SECNUM=[1.0] , NSEG=[3]
195             ( SEGROUGH, SEGDIST (m))=
196             [0.050,-33.89
197             -0.035,31.59
198             0.050,854.54] NSEG times

```

```

199      ( DISTANCE (m), ELEVATION (m) )=
200      [-1075.50, 93.00]
201      [-1070.59, 92.50]
202      [-1003.21, 92.00]
203      [-1001.67, 92.00]
204      [-986.64, 92.00]
205      [-816.61, 91.50]
206      [-797.29, 91.00]
207      [-794.18, 91.00]
208      [-775.41, 91.50]
209      [-702.63, 91.50]
210      [-546.19, 91.50]
211      [-529.54, 91.50]
212      [-323.44, 91.00]
213      [-320.71, 91.00]
214      [-183.59, 91.00]
215      [-182.54, 90.50]
216      [-181.36, 90.00]
217      [-177.37, 90.00]
218      [-87.70, 90.00]
219      [-33.89, 90.00]
220      [-18.52, 86.88]
221      [0.00, 85.20]
222      [16.20, 86.83]
223      [31.59, 90.00]
224      [33.03, 90.50]
225      [34.41, 91.00]
226      [34.99, 91.00]
227      [72.19, 91.00]
228      [208.76, 91.50]
229      [846.25, 92.00]
230      [854.54, 94.00]
231 *%-----|-----|
232 *#*****#
233 *#      Catchment FOSTER
234 *#      - To Foster ditch (north of the Jock)
235 *#      - Partially developed (medium density); remaining agricultural
236 *#*****#
237 CONTINUOUS STANDHYD ID=[2], NHYD=[ "FOSTER" ], DT=[5]min, AREA=[373](ha),
238 XIMP=[0.55], TIMP=[0.55], DWF=[0](cms), LOSS=[2],
239 SCS curve number CN=[74],
240 Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
241 LGP=[40](m), MNP=[0.25], SCP=[0](min),
242 Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
243 LGI=[1577](m), MNI=[0.013], SCI=[0](min),
244 Continuous simulation parameters:
245 IARECper=[4](hrs), IARECimp=[4](hrs),
246 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
247 InterEventTime=[18](hrs), END=-1
248
249 *#*****#
250 *#      Foster Pond
251 *#      - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
252 *#      and a ratio of the catchment area to the West Clarke pond rating curve
253 *#      from the MSS for the next coordinates
254 *#*****#
255 ROUTE RESERVOIR IDout=[4], NHYD=[ "P_FOS" ], IDin=[2],
256 RDT=[5](min),
257 TABLE of ( OUTFLOW-STORAGE ) values
258             (cms) - (ha-m)
259             [ 0.0 , 0.0 ]
260             [ 0.20 , 1.72 ]
261             [ -1 , -1 ] (max twenty pts)
262             IDovf=[9], NHYDovf=[ "FO-OVF" ]
263 *%-----|-----|
264 ADD HYD IDsum=[ 3 ], NHYD=[ "SN_FO" ], IDs to add=[1,4,9]

```

```

265 *%-----|-----|
266 SAVE HYD           ID=[ 3 ] ,    # OF PCYCLES=[-1] ,  ICASEsh=[1]
267             HYD_COMMENT=[ "Total Flows at Foster Drain" ]
268 *%-----|-----|
269 *#
270 *# Hydrograph from Node Foster routed to Node at Cedarview Road
271 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6016
272 *#
273 ROUTE CHANNEL      IDout=[1] ,  NHYD=[ "N_CE" ] , IDin=[3] ,
274             RDT=[5](min),
275             CHLGTH=[159](m) ,  CHSLOPE=[0.0818](%) ,
276                                         FPSLOPE=[0.0818](%) ,
277             SECNUM=[1.0] ,          NSEG=[3]
278             ( SEGROUGH, SEGDIST (m))=
279                 [0.050,-15.46
280                   -0.035,26.55
281                     0.050,1299.52] NSEG times
282             ( DISTANCE (m), ELEVATION (m))=
283                 [-891.38, 93.00]
284                 [-882.49, 93.00]
285                 [-880.92, 92.50]
286                 [-879.37, 92.00]
287                 [-877.72, 91.50]
288                 [-876.10, 91.00]
289                 [-873.23, 91.00]
290                 [-871.82, 91.50]
291                 [-870.40, 92.00]
292                 [-803.44, 92.00]
293                 [-645.23, 91.50]
294                 [-391.20, 91.50]
295                 [-91.00, 91.50]
296                 [-85.52, 91.50]
297                 [-15.46, 89.40]
298                 [-9.79, 89.31]
299                 [-3.22, 86.24]
300                 [3.22, 85.07]
301                 [10.96, 85.79]
302                 [16.44, 86.49]
303                 [26.55, 89.45]
304                 [29.03, 90.27]
305                 [35.76, 90.67]
306                 [36.67, 91.00]
307                 [108.08, 91.00]
308                 [109.82, 90.50]
309                 [112.04, 90.50]
310                 [114.62, 91.00]
311                 [116.76, 91.50]
312                 [118.42, 92.00]
313                 [449.53, 92.50]
314                 [571.98, 92.50]
315                 [1093.81, 93.50]
316                 [1150.48, 94.00]
317                 [1299.52, 95.00]
318 *%-----|-----|
319 *#*****#
320 *#      Catchment S-1
321 *#      - To Jock River (north and south of Jock)
322 *#      - Primarily agricultural fields; portion of sand quarry
323 *#*****#
324 CONTINUOUS NASHYD ID=[2] ,  NHYD=[ "S-1" ] ,  DT=[5]min, AREA=[245](ha) ,
325             DWF=[0](cms) ,  CN/C=[77] ,  IA=[4.67](mm) ,
326             N=[3] ,  TP=[1.10]hrs,
327             Continuous simulation parameters:
328             IaRECper=[4](hrs),
329             SMIN=[-1](mm) ,  SMAX=[-1](mm) ,  SK=[0.010]/(mm) ,
330             InterEventTime=[12](hrs)

```

```

331                                Baseflow simulation parameters:
332                                BaseFlowOption=[1] ,
333                                InitGWResVol=[ 50 ](mm) , GWResK=[ 0.96 ](mm/day/mm)
334                                VHydCond=[ 0.055 ](mm/hr) , END=-1
335
336 *%----- | -----
337 ADD HYD          IDsum=[ 3 ] , NHYD=[ "SN_CE" ] , IDs to add=[1,2]
338 *%----- | -----
339 SAVE HYD          ID=[ 3 ] , # OF PCYCLES=[-1] , ICASEsh=[1]
340                      HYD_COMMENT=[ "Total Flows at Cedarview Road" ]
341 *%----- | -----
342 *#
343 *# Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain
344 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5002
345 *#
346 ROUTE CHANNEL      IDout=[1] , NHYD=[ "N_WC" ] , IDin=[3] ,
347                      RDT=[5](min),
348                      CHLNGTH=[825](m) , CHSLOPE=[0.01](%) ,
349                                         FPSLOPE=[0.01](%) ,
350                      SECNUM=[1.0] , NSEG=[3]
351                      ( SEGRROUGH , SEGDIST (m))=
352                         [0.050,-37.5
353                           -0.035,37.50
354                           0.050,1367.08] NSEG times
355                      ( DISTANCE (m) , ELEVATION (m))=
356                         [-1095.18, 94.00]
357                         [-1091.79, 93.50]
358                         [-1088.95, 93.00]
359                         [-1086.77, 93.00]
360                         [-1069.38, 93.00]
361                         [-1063.14, 93.00]
362                         [-1017.52, 93.00]
363                         [-899.70, 93.00]
364                         [-877.78, 93.00]
365                         [-859.62, 92.50]
366                         [-803.18, 93.00]
367                         [-789.92, 92.00]
368                         [-37.50, 90.00]
369                         [-19.61, 87.04]
370                         [0.00, 85.70]
371                         [14.87, 86.93]
372                         [37.50, 90.00]
373                         [38.54, 90.50]
374                         [42.23, 91]
375                         [157.05,91.50]
376                         [161.44, 91.50]
377                         [236.48, 93.00]
378                         [385.47, 92.50]
379                         [390.78, 92.50]
380                         [863.80, 93.00]
381                         [866.13, 93.00]
382                         [990.85, 92.50]
383                         [991.82, 92.50]
384                         [993.04, 93.00]
385                         [994.81, 93.50]
386                         [1005.36, 93.00]
387                         [1190.52, 93.00]
388                         [1267.97, 93.50]
389                         [1318.99, 94.00]
390                         [1367.08, 94.50]
391 *%----- | -----
392 *#***** Catchment W_CLAR
393 *#      - To West Clarke Drain (south of the Jock)
394 *#      - Subdivision with 43% imp. as per Barrhaven South MSS
395 *#*****
```



```

463      *#      - Medium density residential subdivision
464      *#*****
465 CONTINUOUS STANDHYD ID=[2], NHYD=["KEN_BU"], DT=[5]min, AREA=[281](ha),
466          XIMP=[0.55], TIMP=[0.55], DWF=[0](cms), LOSS=[2],
467          SCS curve number CN=[71],
468          Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
469          LGP=[40](m), MNP=[0.25], SCP=[0](min),
470          Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
471          LGI=[1369](m), MNI=[0.013], SCI=[0](min),
472          Continuous simulation parameters:
473          IaRECper=[4](hrs), IaRECImp=[4](hrs),
474          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
475          InterEventTime=[18](hrs), END=-1
476      *%-----|-----|
477      *#*****
478 *# Existing Kennedy-Burnett SWM Facility
479 *# - Rating curve obtained from URTKBP
480 *# - Tributary Drainage Area to Pond = 160 ha
481      *#*****
482 ROUTE RESERVOIR IDout=[5], NHYD=["KEN_P"], IDin=[2],
483          RDT=[5](min),
484          TABLE of ( OUTFLOW-STORAGE ) values
485          (cms) - (ha-m)
486          [ 0.0 , 0.0 ]
487          [ 0.13 , 0.26 ]
488          [ 0.43 , 0.56 ]
489          [ 0.67 , 0.90 ]
490          [ 0.86 , 1.32 ]
491          [ 1.01 , 1.79 ]
492          [ 1.15 , 2.33 ]
493          [ -1 , -1 ] (max twenty pts)
494          IDovf=[6], NHYDovf=["KEN-OV"]
495      *%-----|-----|
496      *#*****
497 *# Catchment FRASER
498 *# - To Fraser-Clarke drain (north of the Jock)
499 *# - Developed land with assumed 43% imp.
500      *#*****
501 CONTINUOUS STANDHYD ID=[7], NHYD=["FRASER"], DT=[5]min, AREA=[90](ha),
502          XIMP=[0.25], TIMP=[0.25], DWF=[0](cms), LOSS=[2],
503          SCS curve number CN=[80],
504          Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
505          LGP=[40](m), MNP=[0.25], SCP=[0](min),
506          Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
507          LGI=[775](m), MNI=[0.013], SCI=[0](min),
508          Continuous simulation parameters:
509          IaRECper=[4](hrs), IaRECImp=[4](hrs),
510          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
511          InterEventTime=[18](hrs), END=-1
512
513      *%-----|-----|
514 ROUTE RESERVOIR IDout=[8], NHYD=["MS_P2"], IDin=[7],
515          RDT=[5](min),
516          TABLE of ( OUTFLOW-STORAGE ) values
517          (cms) - (ha-m)
518          [ 0.0 , 0.0 ]
519          [ 0.04 , 0.36 ]
520          [ -1 , -1 ] (max twenty pts)
521          IDovf=[9], NHYDovf=["P2-OVF"]
522      *%-----|-----|
523 ADD HYD IDsum=[ 4 ], NHYD=["SN_KB"], IDs to add=[5,6,8,9,1]
524      *%-----|-----|
525 SAVE HYD ID=[4], # OF PCYCLES=[-1], ICASEsh=[1]
526          HYD_COMMENT=["Total Flows at Ken-Burnett Outlet"]
527      *%-----|-----|
528      *# Hydrograph from Node Kennedy - Burnett Drain to Node Todd Drain

```

```

529 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 3633
530 *#
531 ROUTE CHANNEL IDout=[1], NHYD=[ "N_TO" ] ,IDin=[4] ,
532 RDT=[5](min),
533 CHLGTH=[650](m), CHSLOPE=[0.0498](%),
534 FPSLOPE=[0.0498](%),
535 SECNUM=[1.0], NSEG=[3]
536 ( SEGROUGH, SEGDIST (m))=
537 [0.050,-23.74
538 -0.035,23.74
539 0.050,74.7] NSEG times
540 ( DISTANCE (m), ELEVATION (m))=
541 [-74.18, 92.5]
542 [-65.96, 92]
543 [-54.17, 91.5]
544 [-29.24, 91]
545 [-27.41, 90.5]
546 [-25.64, 90]
547 [-23.74, 89.5]
548 [-22,89. 26]
549 [-20, 88.51]
550 [-19, 88.32]
551 [-15, 88.1]
552 [-10, 88.11]
553 [-5, 88.17]
554 [0, 88.27]
555 [5, 88.19]
556 [10, 88.06]
557 [15, 88.48]
558 [16, 88.7]
559 [23.74, 89.5]
560 [24.68, 90]
561 [25.57, 90.5]
562 [26.5, 91]
563 [47.55, 91]
564 [74.7, 92.5]
565 *%-----|-----|-----|-----|
566
567 *#*****
568 *# Catchment TODD
569 *# - To Todd Drain (south of the Jock)
570 *# - Subdivision with 43% imp. as per Barrhaven South MSS
571 *#*****
572 CONTINUOUS STANDHYD ID=[3], NHYD=[ "TODD" ], DT=[5]min, AREA=[195](ha),
573 XIMP=[0.43], TIMP=[0.43], DWF=[0](cms), LOSS=[2],
574 SCS curve number CN=[77],
575 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
576 LGP=[40](m), MNP=[0.25], SCP=[0](min),
577 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
578 LGI=[1140](m), MNI=[0.013], SCI=[0](min),
579 Continuous simulation parameters:
580 IaRECper=[4](hrs), IaRECImp=[4](hrs),
581 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
582 InterEventTime=[18](hrs), END=-1
583
584 *#*****
585 *# Todd Pond 3
586 *# - Rating curve obtained from Barrhaven South MSS modeling
587 *# - Tributary Drainage Area to MSS Pond 3 = 193 ha
588 *#*****
589 ROUTE RESERVOIR IDout=[2], NHYD=[ "MS_P3" ], IDin=[3],
590 RDT=[5](min),
591 TABLE of ( OUTFLOW-STORAGE ) values
592 (cms) - (ha-m)
593 [ 0.0 , 0.0 ]
594 [ 0.08 , 0.78 ]

```

```

595                               [ -1 , -1 ] (max twenty pts)
596                               IDovf=[9], NHYDovf=["P3-OVF"]
597 *%-----|-----|
598 ADD HYD           IDsum=[10], NHYD= ["SN_TO"], IDs to add=[1,2,9]
599 *%-----|-----|
600 SAVE HYD          ID=[ 10 ], # OF PCYCLES=[-1], ICASEsh=[1]
601                   HYD_COMMENT=[ "Total Flows at Todd Drain"]
602 *%-----|-----|
603 *#
604 *# Hydrograph from Todd Drain routed to Corrigan Drain
605 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
606 *#
607 ROUTE CHANNEL      IDout=[1], NHYD=[ "N_TO" ] ,IDin=[10] ,
608                   RDT=[5](min),
609                   CHLGTH=[280](m), CHSLOPE=[ 0.033](%),
610                   FPSLOPE=[ 0.033](%),
611                   SECNUM=[1.0], NSEG=[3]
612                   ( SEGROUGH, SEGDIST (m))=
613                   [0.075,-17.72
614                   -0.045,17.72
615                   0.075,80.62] NSEG times
616                   ( DISTANCE (m), ELEVATION (m))=
617                   [-83.32, 90.00]
618                   [-81.36, 89.50]
619                   [-79.12, 89.00]
620                   [-76.13, 88.50]
621                   [-20.46, 88.00]
622                   [-19.36, 87.50]
623                   [-18.51, 87.00]
624                   [-17.72, 86.50]
625                   [-11.95, 85.24]
626                   [-0.11, 85.12]
627                   [11.49, 85.20]
628                   [17.72, 86.50]
629                   [19.74, 87.00]
630                   [21.22, 87.50]
631                   [22.68, 88.00]
632                   [24.28, 88.50]
633                   [26.79, 89.00]
634                   [71.98, 90.00]
635                   [80.62, 90.50]
636 *%-----|-----|
637 *#*****
638 *# Catchment CORRIG
639 *# - To Corrigan Drain (south of the Jock)
640 *# - Primarily Developed (medium density)
641 *#*****
642 CONTINUOUS STANDHYD ID=[2], NHYD=[ "CORRIG" ], DT=[5]min, AREA=[149](ha),
643                   XIMP=[ 0.45 ], TIMP=[ 0.45 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
644                   SCS curve number CN=[ 77 ],
645                   Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
646                   LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
647                   Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
648                   LGI=[ 997 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
649                   Continuous simulation parameters:
650                   IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
651                   SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
652                   InterEventTime=[ 18 ](hrs), END=-1
653
654 *%-----|-----|
655 *#*****
656 *# Corrigan Pond 1
657 *# - Rating curve obtained from Barrhaven South MSS modeling
658 *# - Tributary Drainage Area to MSS Pond 1 = 145 ha
659 *#*****
660 ROUTE RESERVOIR    IDout=[5], NHYD=[ "MS_P1" ], IDin=[ 2 ],

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```

661          RDT=[5](min),
662                  TABLE of ( OUTFLOW-STORAGE ) values
663                      (cms) - (ha-m)
664                      [ 0.0 , 0.0 ]
665                      [ 0.06 , 0.58 ]
666                      [ -1 , -1 ] (max twenty pts)
667          IDovf=[4], NHYDovf=["P1-OVF"]
668 *%-----|-----|
669 ADD HYD          IDsum=[ 3 ], NHYD=[ "SN_CO" ], IDs to add=[1,4,5]
670 *%-----|-----|
671 SAVE HYD          ID=[ 3 ], # OF PCYCLES=[-1], ICASEsh=[1]
672          HYD_COMMENT=[ "Total Flows at Corrigan Drain" ]
673 *%-----|-----|
674 *#
675 *# Hydrograph from Corrigan Drain routed to Jockvale Road
676 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
677 *#
678 ROUTE CHANNEL      IDout=[1], NHYD=[ "N_MI" ] ,IDin=[3] ,
679          RDT=[5](min),
680          CHLGTH=[580](m), CHSLOPE=[0.4448](%),
681                      FPSLOPE=[0.4448](%),
682          SECNUM=[1.0], NSEG=[3]
683          ( SEGROUGH, SEGDIST (m))=
684              [0.075,-17.72
685              -0.045,17.72
686              0.075,80.62] NSEG times
687          ( DISTANCE (m), ELEVATION (m))=
688              [-83.32, 90.00]
689              [-81.36, 89.50]
690              [-79.12, 89.00]
691              [-76.13, 88.50]
692              [-20.46, 88.00]
693              [-19.36, 87.50]
694              [-18.51, 87.00]
695              [-17.72, 86.50]
696              [-11.95, 85.24]
697              [-0.11, 85.12]
698              [11.49, 85.20]
699              [17.72, 86.50]
700              [19.74, 87.00]
701              [21.22, 87.50]
702              [22.68, 88.00]
703              [24.28, 88.50]
704              [26.79, 89.00]
705              [71.98, 90.00]
706              [80.62, 90.50]
707 *%-----|-----|
708 *#*****
709 *#      Catchment MILLS
710 *#      - To SWM Facility north of the Jock
711 *#      - Primarily residential development
712 *#*****
713 CONTINUOUS STANDHYD ID=[2], NHYD=[ "MILLS" ], DT=[5]min, AREA=[139](ha),
714          XIMP=[0.38], TIMP=[0.38], DWF=[0](cms), LOSS=[2],
715          SCS curve number CN=[74],
716          Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
717          LGP=[40](m), MNP=[0.25], SCP=[0](min),
718          Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
719          LGI=[963](m), MNI=[0.013], SCI=[0](min),
720          Continuous simulation parameters:
721          IaRECper=[4](hrs), IaRECImp=[4](hrs),
722          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
723          InterEventTime=[18](hrs), END=-1
724
725 *%-----|-----|
726 *#*****

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```

727 *#      Chapman Mills SWM Pond
728 *#      - Rating curve obtained from CCL hydraulic modeling
729 *#*****
730 ROUTE RESERVOIR      IDout=[5],    NHYD=["MILL_P"],   IDin=[2],
731                           RDT=[5](min),
732                               TABLE of ( OUTFLOW-STORAGE ) values
733                               (cms) - (ha-m)
734                               [ 0.0 , 0.0 ]
735                               [ 0.01 , 0.01]
736                               [ 0.05 , 0.06]
737                               [ 0.09 , 0.11]
738                               [ 0.13 , 0.15]
739                               [ 0.18 , 0.19]
740                               [ 0.28 , 0.28]
741                               [ 0.37 , 0.34]
742                               [ 0.45 , 0.40]
743                               [ 0.51 , 0.44]
744                               [ 0.56 , 0.47]
745                               [ 0.64 , 0.52]
746                               [ 0.76 , 0.59]
747                               [ 0.86 , 0.65]
748                               [ 1.09 , 0.78]
749                               [ 1.44 , 0.96]
750                               [ 3.18 , 1.84]
751                               [ 4.05 , 2.31]
752                               [ -1 , -1 ] (max twenty pts)
753 IDovf=[4], NHYDovf=["MIL-OV"]
754 *%-----|-----|
755 ADD HYD      IDsum=[ 3 ], NHYD=["SN_MI"], IDs to add=[1,4,5]
756 *%-----|-----|
757 SAVE HYD      ID=[ 3 ], # OF PCYCLES=[-1], ICASEsh=[1]
758             HYD_COMMENT=[ "Total Flows at Jockvale Road" ]
759 *%-----|-----|
760 *#
761 *# Hydrograph from Jockvale Road routed to Heart's Desire
762 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 689
763 *#
764 ROUTE CHANNEL      IDout=[1], NHYD=[ "N_DE" ] ,IDin=[3] ,
765                           RDT=[5](min),
766                           CHLGTH=[1962](m), CHSLOPE=[0.2227](%),
767                                         FPSLOPE=[0.2227](%),
768                           SECNUM=[1.0], NSEG=[3]
769                           ( SEGROUGH, SEGDIST (m))=
770                               [0.075,-17.56
771                               -0.045,18.27
772                               0.075,67.59] NSEG times
773                           ( DISTANCE (m), ELEVATION (m))=
774                               [-111.59, 88.00]
775                               [-102.58, 87.50]
776                               [-96.20, 87.00]
777                               [-90.04, 86.50]
778                               [-84.02, 86.00]
779                               [-77.54, 85.50]
780                               [-54.07, 85.00]
781                               [-39.43, 84.50]
782                               [-28.30, 84.00]
783                               [-24.12, 83.50]
784                               [-22.30, 83.00]
785                               [-20.55, 82.50]
786                               [-17.56, 82.00]
787                               [-12.63, 81.22]
788                               [-0.11, 80.75]
789                               [11.55, 81.22]
790                               [18.27, 82.00]
791                               [19.82, 82.50]
792                               [22.48, 83.00]

```

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793 [27.90, 83.50]
794 [29.31, 84.00]
795 [30.81, 84.50]
796 [32.51, 85.00]
797 [34.24, 85.50]
798 [36.34, 86.00]
799 [41.65, 86.50]
800 [62.64, 87.00]
801 [65.14, 87.50]
802 [67.59, 88.00]
803 *%-----|-----|-----|-----|-----|-----|-----|-----|
804 *#*****
805 *#      Catchment DESIRE
806 *#      - To Jock River (north of the Jock)
807 *#      - Rural-estate subdivision (Heart's Desire Community)
808 *#*****
809 CONTINUOUS STANDHYD ID=[2], NHYD=["DESIRE"], DT=[5]min, AREA=[24](ha),
810 XIMP=[0.25], TIMP=[0.25], DWF=[0](cms), LOSS=[2],
811 SCS curve number CN=[77],
812 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
813 LGP=[40](m), MNP=[0.25], SCP=[0](min),
814 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
815 LGI=[400](m), MNI=[0.013], SCI=[0](min),
816 Continuous simulation parameters:
817 IaRECper=[4](hrs), IaRECImp=[4](hrs),
818 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
819 InterEventTime=[18](hrs), END=-1
820
821 *%-----|-----|-----|-----|-----|-----|-----|-----|
822 *#*****
823 *#      Catchment JOCKVA
824 *#      - To Jockvale SWM Facility
825 *#      - Residential development & golf course
826 *#*****
827 CONTINUOUS STANDHYD ID=[3], NHYD=["JOCKVA"], DT=[5]min, AREA=[252](ha),
828 XIMP=[0.50], TIMP=[0.50], DWF=[0](cms), LOSS=[2],
829 SCS curve number CN=[74],
830 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
831 LGP=[40](m), MNP=[0.25], SCP=[0](min),
832 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
833 LGI=[1296](m), MNI=[0.013], SCI=[0](min),
834 Continuous simulation parameters:
835 IaRECper=[4](hrs), IaRECImp=[4](hrs),
836 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
837 InterEventTime=[18](hrs), END=-1
838
839 *%-----|-----|-----|-----|-----|-----|-----|-----|
840 *#*****
841 *#      Jockvale SWM Facility
842 *#      - Rating curve obtained from Jockvale Servicing Study (CCL 1999)
843 *#*****
844 ROUTE RESERVOIR IDout=[5], NHYD=["JOCK_P"], IDin=[3],
845 RDT=[5](min),
846             TABLE of ( OUTFLOW-STORAGE ) values
847             (cms) - (ha-m)
848             [ 0.0 , 0.0 ]
849             [ 0.27 , 0.03]
850             [ 0.28 , 0.55]
851             [ 0.29 , 1.14]
852             [ 0.30 , 1.80]
853             [ 0.31 , 2.32]
854             [ 1.12 , 2.87]
855             [ 2.92 , 3.45]
856             [ 4.64 , 4.07]
857             [ 6.69 , 4.72]
858             [ 9.02 , 5.39]

```

```

859 [ 11.62 , 6.10]
860 [ 14.42 , 6.85]
861 [ 17.45 , 7.62]
862 [ 20.69 , 8.44]
863 [ 24.08 , 9.28]
864 [ 27.68 , 10.17]
865 [ -1 , -1 ] (max twenty pts)
866 IDovf=[ 4 ], NHYDovf= ["JO-OVF"]
867 *%-----|-----|
868 ADD HYD IDsum=[ 3 ], NHYD= ["SN_DE" ], IDs to add=[1,2,4,5]
869 *%-----|-----|
870 SAVE HYD ID=[ 3 ], # OF PCYCLES=[-1], ICASEsh=[1]
871 HYD_COMMENT= ["Total Flows at Heart's Desire"]
872 *%-----|-----|
873 *#
874 *# Hydrograph from Heart's Desire routed to Rideau River
875 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 0
876 *#
877 ROUTE CHANNEL IDout=[ 1 ], NHYD= ["N1" ] , IDin=[ 3 ] ,
878 RDT=[ 5 ](min),
879 CHLGHt=[ 563 ](m), CHSLOPE=[ 0.9668 ](%),
880 FPSLOPE=[ 0.9668 ](%),
881 SECNUM=[ 1.0 ], NSEG=[ 3 ]
882 ( SEGRROUGH, SEGDIST (m))=
883 [ 0.075,-30.20
884 -0.045,30.20
885 0.075,168.81] NSEG times
886 ( DISTANCE (m), ELEVATION (m))=
887 [-170.17, 86.00]
888 [-164.75, 85.50]
889 [-158.08, 85.00]
890 [-113.12, 82.00]
891 [-98.46, 81.50]
892 [-92.24, 81.00]
893 [-86.88, 80.50]
894 [-81.54, 80.00]
895 [-74.36, 79.50]
896 [-63.54, 79.00]
897 [-39.23, 78.50]
898 [-34.51, 78.00]
899 [-33.01, 77.50]
900 [-30.20, 77.00]
901 [-13.42, 76.18]
902 [-1.14, 76.09]
903 [17.06, 76.18]
904 [30.20, 77.00]
905 [32.95, 77.50]
906 [34.06, 78.00]
907 [35.11, 78.50]
908 [36.32, 79.00]
909 [37.74, 79.50]
910 [48.48, 81.50]
911 [49.25, 82.00]
912 [55.61, 84.50]
913 [57.09, 85.00]
914 [59.51, 85.50]
915 [64.34, 86.00]
916 [66.30, 86.00]
917 [76.71, 86.50]
918 [101.83, 86.50]
919 [119.73, 87.00]
920 [142.04, 87.50]
921 [168.81, 88.00]
922 *%-----|-----|
923 *#***** Catchment S-2

```

```

925 *#      - To Jock River (north and south)
926 *#      - Undeveloped floodplain and river
927 *#*****
928 CONTINUOUS NASHYD      ID=[ 2 ], NHYD=[ "S-2" ], DT=[ 5 ]min, AREA=[ 102 ](ha),
929                               DWF=[ 0 ](cms), CN/C=[ 72 ], IA=[ 4.67 ](mm),
930                               N=[ 3 ], TP=[ 0.40 ]hrs,
931                               Continuous simulation parameters:
932                               IaRECper=[ 4 ](hrs),
933                               SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
934                               InterEventTime=[ 12 ](hrs)
935                               Baseflow simulation parameters:
936                               BaseFlowOption=[ 1 ],
937                               InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
938                               VHydCond=[ 0.055 ](mm/hr), END=-1
939
940 *%-----|-----|
941 ADD HYD          IDsum=[ 3 ], NHYD=[ "SN_N1" ], IDs to add=[ 1, 2 ]
942 *%-----|-----|
943 SAVE HYD          ID=[ 3 ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
944                               HYD_COMMENT=[ "Total Flows at Rideau River" ]
945 *%-----|-----|
946 *% 5 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
947 START             TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 005 ]
948 *%                  [ "C24SC005.stm" ] <--storm filename, one per line for NSTORM time
949 *%-----|-----|
950 *% 10 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
951 *%START           TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 010 ]
952 *%                  [ "C24SC010.stm" ] <--storm filename, one per line for NSTORM time
953 *%-----|-----|
954 *% 25 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
955 START             TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 025 ]
956 *%                  [ "C24SC025.stm" ] <--storm filename, one per line for NSTORM time
957 *%-----|-----|
958 *% 50 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
959 *%START           TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 050 ]
960 *%                  [ "C24SC050.stm" ] <--storm filename, one per line for NSTORM time
961 *%-----|-----|
962 *% 100 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
963 START             TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 100 ]
964 *%                  [ "C24SC100.stm" ] <--storm filename, one per line for NSTORM time
965 *%-----|-----|
966
967 ##########
968 FINISH
969
970
971
972
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0001-----+
0002-----+
0003-----+ SSSSS W W M M B H Y Y N M M O O O 999 999 =====
0004-----+ SSSSS W W M M M M HHHHH Y Y N M M O O # # 9 9 9 Ver5 Beta
0005-----+ SSSSS W W M M H H Y M M O O 9999 9999 =====
0006-----+ S W M M H H Y M M O O 9999 9999 =====
0007-----+ SSSSS W W M M H H Y M M O O 9 9 9 # 3783815
0008-----+
0009-----+ StormWater Management HYdrologic Model 999 999 =====
0010-----+
0011-----+
0012-----+ SWMMV6 Ver 5 Beta *-----+
0013-----+ A single event and continuous hydrology simulation model
0014-----+ based on the principles of HDMO and its successors
0015-----+ GTRWMO-83 and OTTWWMO-85
0016-----+
0017-----+ Distributed by: J.F. Sabourin and Associates Inc.
0018-----+ Ottawa, Ontario: (613) 727-5198
0019-----+ Guelph, Ontario: (519) 243-6888
0020-----+ E-Mail: swmmsoft@jfs.com
0021-----+
0022-----+
0023-----+ Licensed user: Stanton - Ottawa 601
0024-----+ SERIAL# :3783815
0025-----+
0026-----+
0027-----+
0028-----+
0029-----+ ***** PROGRAM ARRAY DIMENSIONS *****
0030-----+ Max. number of basins: 1000
0031-----+ Max. number of rainfall points: 52750
0032-----+ Max. number of flow points: 52750
0033-----+
0034-----+
0035-----+ *** DESCRIPTION SUMMARY TABLE HEADERS (units depend on METOUT in START) ***
0036-----+
0037-----+ ID: Hydrograph Identification numbers, (3-10).
0038-----+ IDN: Hydrograph reference numbers, (6 digits or characters).
0039-----+ AREA: Area of the catchment area (sq km or sq mi).
0040-----+ QPEAK: Peak flow of simulated hydrograph, (ft3/sec) or (m3/sec).
0041-----+ Tpeakdate_hh:mm: The date and time of the peak flow.
0042-----+ R.C.: Runoff Coefficient of simulated hydrograph (ratio).
0043-----+ Iimp: see WARNING or NOTE message printed at end of run.
0044-----+ ERMS: Error message printed at end of run.
0045-----+
0046-----+
0047-----+
0048-----+
0049-----+
0050-----+
0051-----+ S W M M & R Y D O T P U T
0052-----+
0053-----+
0054-----+ DATE: 2006-11-15 TIME: 14:33:15 RUN COUNTER: 000132
0055-----+
0056-----+ Input filename: C:\Navin\OCTBVE-1\CONTIN-1\SMR_POST\INR_POST.dat
0057-----+ Output filename: C:\Navin\OCTBVE-1\CONTIN-1\SMR_POST\INR_POST.out
0058-----+ Summary filename: C:\Navin\OCTBVE-1\CONTIN-1\SMR_POST\INR_POST.sum
0059-----+ Summary commands:
0060-----+
0061-----+ 1:
0062-----+ 2:
0063-----+
0064-----+
0065-----+
0066-----+
0067-----+
0068-----+ Project Name: [Jock River Reach 1 Subwatershed Study]Project #: [160400414]
0069-----+ October 2006
0070-----+ Modeler: [Navin Gautam/ Original by Ana M Paerer]
0071-----+ Company: [Stantec]
0072-----+ Address: [3824306]
0073-----+
0074-----+ *** END OF RUN : 1
0075-----+
0076-----+
0077-----+
0078-----+
0079-----+
0080-----+
0081-----+
0082-----+ RUS:GARDNER
0083-----+ O2D:001-
0084-----+ START .00 hrs [0]
0085-----+ (TZERO = 2 hr [1=imperial, 2=metric output])
0086-----+ (INSTRM = 1)
0087-----+ (NRUN = 2)
0088-----+
0089-----+ # Project Name: [Jock River Reach 1 Subwatershed Study]Project #: [160400414]
0090-----+ Date: [October 2006]
0091-----+ Modeler: [Navin Gautam/ Original by Ana M Paerer]
0092-----+ Company: [Stantec]
0093-----+ Address: [3824306]
0094-----+
0095-----+ -----
0096-----+
0097-----+ 002:0002-----+
0098-----+ File name = storm.001
0099-----+ Comment = Plus SCS de 24 hrs 1:2 et pour Ottawa CDA
0100-----+ (TZERO = 2 hr [1=imperial, 2=metric output])
0101-----+ (INSTRM = 1)
0102-----+ (NRUN = 2)
0103-----+ MDCFY STORM
0104-----+ (TZERO = 2 hr [1=imperial, 2=metric output])
0105-----+ (TSHRT = 960.00 min)
0106-----+ (SDT=10.001$DTR= 40.00$PTD= 45.51)
0107-----+
0108-----+ 002:0004-----+
0109-----+ File name = C:\Navin\OCTBVE-1\CONTIN-1\SMR_POST\MODIFIED.VAL
0110-----+ IASCDv = 1 (read and print daily)
0111-----+ PFILETYPE = FILETYPE [see City of Ottawa Sewer Design Guideline]
0112-----+ HORTON's infiltration equation parameters [C0=0.14 /hr] [F= .00 mm]
0113-----+ Parameters for PREVIOUS surfaces in STANDHYD:
0114-----+ (Iapeq = 4.67 min [L=0.40 m] [MWD=.25])
0115-----+ (Iapmin = 0.00 min [L=0.40 m] [MWD=.25])
0116-----+ (Iapmax = 0.00 min [L=0.40 m] [MWD=.25])
0117-----+ (Iimp = 1.57 min [CLI= 1.50] [MHD=.03])
0118-----+ Parameters used in NASHYD:
0119-----+ (Iimp = 1.57 min [CLI= 1.50] [MHD=.03])
0120-----+ 002:0005-----+
0121-----+ COMPUTER AIDED DESIGN [CADD] = 1
0122-----+ APIDkdy = 50.12 APIDkdx = 8500 APIDkdm = .9988
0123-----+ APIMax = 80.12 APIavge = 66.74 APImin = 44.87
0124-----+
0125-----+ JOCK RIVER REACH 1 SUBWATERSHED STUDY DISCRETIZED MODEL
0126-----+ PROPOSED CONDITIONS DESIGN STORM MODEL (SUMMER)
0127-----+
0128-----+ Version: Draft Final Report, October 2006
0129-----+ Author: [Navin Gautam]
0130-----+ Draft Initial Condition Report, Nov. 2005
0131-----+
0132-----+ -----
0133-----+ Assumption:
0134-----+ All components are assumed to be developed except S-1, S-2, and SW-1a
0135-----+ SW facilities are modeled
0136-----+ Rainfall is estimated based on existing reports and modeling for the
0137-----+ proposed SW facilities
0138-----+ The rating curve for the existing Kennedy Burnett SMW Facility was obtained
0139-----+ from the design report in the Kennedy Burnett Settling Pond (KUBSP)- R
0140-----+ Municipality of Ottawa-Carleton, March 1983
0141-----+ River routing modeled
0142-----+ River cross sections obtained from RVCA's HEC-RAS hydraulic model
0143-----+
0144-----+ Parameters:
0145-----+ (Iimp = 1.57 min [CLI= 1.50] [MHD=.03])
0146-----+ (Iapeq = 4.67 min [L=0.40 m] [MWD=.25])
0147-----+ (NRCS/SCS CN based on landuse (airphoto) and soil type (base mapping)
0148-----+ Time to peak using Uplands Method
0149-----+
0150-----+ -----
0151-----+ Parameters used in NASHYD:
0152-----+ (Iimp = 1.57 min [CLI= 1.50] [MHD=.03])
0153-----+ File name = C:\Navin\OCTBVE-1\CONTIN-1\SMR_POST\INR_POST.sum
0154-----+ Comment = N2
0155-----+ -----
0156-----+ Hydrograph from Node 2 routed to Node 416
0157-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 9025
0158-----+
0159-----+ 002:0006-----+ ID:NHVD----+--AREA---+QPEAK:Tpeakdate_hh:mm---+R.V.-R.C.-
0160-----+ ROUTE CHANNEL --> 01:LN_02 52483.01 45.789 No_date 33:50 12.75 n/a
0161-----+ (ROUTE = 0) cut&join 01:LN_02 52483.01 44.971 36:30 12.75 n/a
0162-----+ (LN/S= .2377 , .050/.055)
0163-----+ (Vmax=.575$chm=.2199)
0164-----+
0165-----+ Catchment SW-1a
0166-----+ Portion of RVCA catchment SW-1 outside of Reach 1 subwatershed
0167-----+ (SW-1a is primarily agricultural land)
0168-----+
0169-----+ 002:0007-----+ ID:NHVD----+--AREA---+QPEAK:Tpeakdate_hh:mm---+R.V.-R.C.-
0170-----+ CONTINUOUS STANDHYD 240W.Lia 546.00 1.994 No_date 31:20 13.01 286
0171-----+ (CN = 72.90% N = 3.00)
0172-----+ (T = 2.91% 5.00)
0173-----+ (InterEventTime= 12.00)
0174-----+ (Iapeq = 4.67 min [CLI= 1.50] [MHD=.03])
0175-----+ (APIMax = 80.12 APIDkdy = 8500 APIDkdm = .9988)
0176-----+ (APIMin = 44.87 APIDkdx = 66.74)
0177-----+
0178-----+ 002:0008-----+ ID:NHVD----+--AREA---+QPEAK:Tpeakdate_hh:mm---+R.V.-R.C.-
0179-----+ ADD HVD 04:LN_416 52483.01 44.971 No_date 36:30 12.75 n/a
0180-----+ 04:LN_416 52483.01 45.789 No_date 31:20 13.01 n/a
0181-----+ (ROUTE = 0) cut&join 04:LN_416 52483.01 44.971 36:30 12.75 n/a
0182-----+ (LN/S= .2377 , .050/.055)
0183-----+ (Vmax=.575$chm=.2199)
0184-----+
0185-----+ Catchment SW-1a
0186-----+ Portion of RVCA catchment SW-1 outside of Reach 1 subwatershed
0187-----+ (SW-1a is primarily agricultural land)
0188-----+
0189-----+ 002:0009-----+ ID:NHVD----+--AREA---+QPEAK:Tpeakdate_hh:mm---+R.V.-R.C.-
0190-----+ CONTINUOUS STANDHYD 240W.Lia 546.00 1.994 No_date 31:20 13.01 286
0191-----+ (CN = 72.90% N = 3.00)
0192-----+ (T = 2.91% 5.00)
0193-----+ (InterEventTime= 12.00)
0194-----+ (Iapeq = 4.67 min [CLI= 1.50] [MHD=.03])
0195-----+ (APIMax = 80.12 APIDkdy = 8500 APIDkdm = .9988)
0196-----+ (APIMin = 44.87 APIDkdx = 66.74)
0197-----+
0198-----+ 002:0010-----+ ID:NHVD----+--AREA---+QPEAK:Tpeakdate_hh:mm---+R.V.-R.C.-
0199-----+ CONTINUOUS STANDHYD 240W.Lia 546.00 1.994 No_date 31:20 13.01 286
0200-----+ (CN = 72.90% N = 3.00)
0201-----+ (T = 2.91% 5.00)
0202-----+ (InterEventTime= 12.00)
0203-----+ (Iapeq = 4.67 min [CLI= 1.50] [MHD=.03])
0204-----+ (APIMax = 80.12 APIDkdy = 8500 APIDkdm = .9988)
0205-----+ (APIMin = 44.87 APIDkdx = 66.74)
0206-----+
0207-----+ -----
0208-----+ Rating curve obtained assuming 403s/ha in 24 hours for quality control
0209-----+ and a ratio of the catchment area to the West Clarke pond rating curve
0210-----+
0211-----+ -----
0212-----+ Catchment KEEFE
0213-----+ To Jockeys drain (north of the Jock)
0214-----+ Depth to water assumed 43% imp
0215-----+
0216-----+ -----
0217-----+ Catchments KEEFE
0218-----+ To Jockeys drain (north of the Jock)
0219-----+ Depth to water assumed 43% imp
0220-----+
0221-----+ -----
0222-----+ Catchments KEEFE
0223-----+ To Jockeys drain (north of the Jock)
0224-----+ Depth to water assumed 43% imp
0225-----+
0226-----+ -----
0227-----+ Catchments KEEFE
0228-----+ To Jockeys drain (north of the Jock)
0229-----+ Depth to water assumed 43% imp
0230-----+
0231-----+ -----
0232-----+ Catchments KEEFE
0233-----+ To Jockeys drain (north of the Jock)
0234-----+ Depth to water assumed 43% imp
0235-----+
0236-----+ -----
0237-----+ Catchment POSTER
0238-----+ To Foster Drain (north of the Jock)
0239-----+ Partially developed (medium density); remaining agricultural
0240-----+
0241-----+ -----
0242-----+ CONTINUOUS STANDHYD 02:POSTER
0243-----+ (XIMP=.55$TIME=.43)
0244-----+ (ROUTE = 0) cut&join 04:PK_OKE
0245-----+ overflow <on> 09:OF_DVF 331.54 13.458 No_date 28:15 25.18 n/a
0246-----+ (ROUTE = 0) cut&join 04:PK_OKE 116.46 .200 No_date 27:45 25.18 n/a
0247-----+ (ROUTE = 0) cut&join 04:PK_OKE 116.46 .200 No_date 28:20 25.18 n/a
0248-----+
0249-----+ 002:0014-----+ ID:NHVD----+--AREA---+QPEAK:Tpeakdate_hh:mm---+R.V.-R.C.-
0250-----+ CONTINUOUS STANDHYD 02:POSTER
0251-----+ (XIMP=.55$TIME=.43)
0252-----+ (ROUTE = 0) cut&join 04:PK_OKE
0253-----+ overflow <on> 09:OF_DVF 331.54 13.458 No_date 28:20 25.18 n/a
0254-----+ (ROUTE = 0) cut&join 04:PK_OKE 116.46 .200 No_date 28:20 25.18 n/a
0255-----+
0256-----+ 002:0015-----+ ID:NHVD----+--AREA---+QPEAK:Tpeakdate_hh:mm---+R.V.-R.C.-
0257-----+ CONTINUOUS STANDHYD 02:POSTER
0258-----+ (XIMP=.55$TIME=.43)
0259-----+ (ROUTE = 0) cut&join 04:PK_OKE
0260-----+ overflow <on> 09:OF_DVF 331.54 13.458 No_date 28:20 25.18 n/a
0261-----+ (ROUTE = 0) cut&join 04:PK_OKE 116.46 .200 No_date 27:45 25.18 n/a
0262-----+ (ROUTE = 0) cut&join 04:PK_OKE 116.46 .200 No_date 28:20 25.18 n/a
0263-----+
0264-----+ 002:0016-----+ ID:NHVD----+--AREA---+QPEAK:Tpeakdate_hh:mm---+R.V.-R.C.-
0265-----+ CONTINUOUS STANDHYD 02:POSTER
0266-----+ (XIMP=.55$TIME=.43)
0267-----+ (ROUTE = 0) cut&join 04:PK_OKE
0268-----+ overflow <on> 09:OF_DVF 331.54 13.458 No_date 28:20 25.18 n/a
0269-----+ (ROUTE = 0) cut&join 04:PK_OKE 116.46 .200 No_date 27:45 25.18 n/a
0270-----+ (ROUTE = 0) cut&join 04:PK_OKE 116.46 .200 No_date 28:20 25.18 n/a
0271-----+
0272-----+ -----
0273-----+ Catchments KEEFE
0274-----+ To Foster Drain (north of the Jock)
0275-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0276-----+
0277-----+ -----
0278-----+ Catchments KEEFE
0279-----+ To Foster Drain (north of the Jock)
0280-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0281-----+
0282-----+ -----
0283-----+ Catchments KEEFE
0284-----+ To Foster Drain (north of the Jock)
0285-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0286-----+
0287-----+ -----
0288-----+ Catchments KEEFE
0289-----+ To Foster Drain (north of the Jock)
0290-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0291-----+
0292-----+ -----
0293-----+ Catchments KEEFE
0294-----+ To Foster Drain (north of the Jock)
0295-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0296-----+
0297-----+ -----
0298-----+ Catchments KEEFE
0299-----+ To Foster Drain (north of the Jock)
0300-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0301-----+
0302-----+ -----
0303-----+ Catchments KEEFE
0304-----+ To Foster Drain (north of the Jock)
0305-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0306-----+
0307-----+ -----
0308-----+ Catchments KEEFE
0309-----+ To Foster Drain (north of the Jock)
0310-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0311-----+
0312-----+ -----
0313-----+ Catchments KEEFE
0314-----+ To Foster Drain (north of the Jock)
0315-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0316-----+
0317-----+ -----
0318-----+ Catchments KEEFE
0319-----+ To Foster Drain (north of the Jock)
0320-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0321-----+
0322-----+ -----
0323-----+ Catchments KEEFE
0324-----+ To Foster Drain (north of the Jock)
0325-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0326-----+
0327-----+ -----
0328-----+ Catchments KEEFE
0329-----+ To Foster Drain (north of the Jock)
0330-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0331-----+
0332-----+ -----
0333-----+ Catchments KEEFE
0334-----+ To Foster Drain (north of the Jock)
0335-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0336-----+
0337-----+ -----
0338-----+ Catchments KEEFE
0339-----+ To Foster Drain (north of the Jock)
0340-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0341-----+
0342-----+ -----
0343-----+ Catchments KEEFE
0344-----+ To Foster Drain (north of the Jock)
0345-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0346-----+
0347-----+ -----
0348-----+ Catchments KEEFE
0349-----+ To Foster Drain (north of the Jock)
0350-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0351-----+
0352-----+ -----
0353-----+ Catchments KEEFE
0354-----+ To Foster Drain (north of the Jock)
0355-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0356-----+
0357-----+ -----
0358-----+ Catchments KEEFE
0359-----+ To Foster Drain (north of the Jock)
0360-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0361-----+
0362-----+ -----
0363-----+ Catchments KEEFE
0364-----+ To Foster Drain (north of the Jock)
0365-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0366-----+
0367-----+ -----
0368-----+ Catchments KEEFE
0369-----+ To Foster Drain (north of the Jock)
0370-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0371-----+
0372-----+ -----
0373-----+ Catchments KEEFE
0374-----+ To Foster Drain (north of the Jock)
0375-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0376-----+
0377-----+ -----
0378-----+ Catchments KEEFE
0379-----+ To Foster Drain (north of the Jock)
0380-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0381-----+
0382-----+ -----
0383-----+ Catchments KEEFE
0384-----+ To Foster Drain (north of the Jock)
0385-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0386-----+
0387-----+ -----
0388-----+ Catchments KEEFE
0389-----+ To Foster Drain (north of the Jock)
0390-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0391-----+
0392-----+ -----
0393-----+ Catchments KEEFE
0394-----+ To Foster Drain (north of the Jock)
0395-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0396-----+
0397-----+ -----
0398-----+ Catchments KEEFE
0399-----+ To Foster Drain (north of the Jock)
0400-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0401-----+
0402-----+ -----
0403-----+ Catchments KEEFE
0404-----+ To Foster Drain (north of the Jock)
0405-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0406-----+
0407-----+ -----
0408-----+ Catchments KEEFE
0409-----+ To Foster Drain (north of the Jock)
0410-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0411-----+
0412-----+ -----
0413-----+ Catchments KEEFE
0414-----+ To Foster Drain (north of the Jock)
0415-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0416-----+
0417-----+ -----
0418-----+ Catchments KEEFE
0419-----+ To Foster Drain (north of the Jock)
0420-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0421-----+
0422-----+ -----
0423-----+ Catchments KEEFE
0424-----+ To Foster Drain (north of the Jock)
0425-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0426-----+
0427-----+ -----
0428-----+ Catchments KEEFE
0429-----+ To Foster Drain (north of the Jock)
0430-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0431-----+
0432-----+ -----
0433-----+ Catchments KEEFE
0434-----+ To Foster Drain (north of the Jock)
0435-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0436-----+
0437-----+ -----
0438-----+ Catchments KEEFE
0439-----+ To Foster Drain (north of the Jock)
0440-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0441-----+
0442-----+ -----
0443-----+ Catchments KEEFE
0444-----+ To Foster Drain (north of the Jock)
0445-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0446-----+
0447-----+ -----
0448-----+ Catchments KEEFE
0449-----+ To Foster Drain (north of the Jock)
0450-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0451-----+
0452-----+ -----
0453-----+ Catchments KEEFE
0454-----+ To Foster Drain (north of the Jock)
0455-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0456-----+
0457-----+ -----
0458-----+ Catchments KEEFE
0459-----+ To Foster Drain (north of the Jock)
0460-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0461-----+
0462-----+ -----
0463-----+ Catchments KEEFE
0464-----+ To Foster Drain (north of the Jock)
0465-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0466-----+
0467-----+ -----
0468-----+ Catchments KEEFE
0469-----+ To Foster Drain (north of the Jock)
0470-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0471-----+
0472-----+ -----
0473-----+ Catchments KEEFE
0474-----+ To Foster Drain (north of the Jock)
0475-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0476-----+
0477-----+ -----
0478-----+ Catchments KEEFE
0479-----+ To Foster Drain (north of the Jock)
0480-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0481-----+
0482-----+ -----
0483-----+ Catchments KEEFE
0484-----+ To Foster Drain (north of the Jock)
0485-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0486-----+
0487-----+ -----
0488-----+ Catchments KEEFE
0489-----+ To Foster Drain (north of the Jock)
0490-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0491-----+
0492-----+ -----
0493-----+ Catchments KEEFE
0494-----+ To Foster Drain (north of the Jock)
0495-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0496-----+
0497-----+ -----
0498-----+ Catchments KEEFE
0499-----+ To Foster Drain (north of the Jock)
0500-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0501-----+
0502-----+ -----
0503-----+ Catchments KEEFE
0504-----+ To Foster Drain (north of the Jock)
0505-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0506-----+
0507-----+ -----
0508-----+ Catchments KEEFE
0509-----+ To Foster Drain (north of the Jock)
0510-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0511-----+
0512-----+ -----
0513-----+ Catchments KEEFE
0514-----+ To Foster Drain (north of the Jock)
0515-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0516-----+
0517-----+ -----
0518-----+ Catchments KEEFE
0519-----+ To Foster Drain (north of the Jock)
0520-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0521-----+
0522-----+ -----
0523-----+ Catchments KEEFE
0524-----+ To Foster Drain (north of the Jock)
0525-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0526-----+
0527-----+ -----
0528-----+ Catchments KEEFE
0529-----+ To Foster Drain (north of the Jock)
0530-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0531-----+
0532-----+ -----
0533-----+ Catchments KEEFE
0534-----+ To Foster Drain (north of the Jock)
0535-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0536-----+
0537-----+ -----
0538-----+ Catchments KEEFE
0539-----+ To Foster Drain (north of the Jock)
0540-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0541-----+
0542-----+ -----
0543-----+ Catchments KEEFE
0544-----+ To Foster Drain (north of the Jock)
0545-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0546-----+
0547-----+ -----
0548-----+ Catchments KEEFE
0549-----+ To Foster Drain (north of the Jock)
0550-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0551-----+
0552-----+ -----
0553-----+ Catchments KEEFE
0554-----+ To Foster Drain (north of the Jock)
0555-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0556-----+
0557-----+ -----
0558-----+ Catchments KEEFE
0559-----+ To Foster Drain (north of the Jock)
0560-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0561-----+
0562-----+ -----
0563-----+ Catchments KEEFE
0564-----+ To Foster Drain (north of the Jock)
0565-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0566-----+
0567-----+ -----
0568-----+ Catchments KEEFE
0569-----+ To Foster Drain (north of the Jock)
0570-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0571-----+
0572-----+ -----
0573-----+ Catchments KEEFE
0574-----+ To Foster Drain (north of the Jock)
0575-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0576-----+
0577-----+ -----
0578-----+ Catchments KEEFE
0579-----+ To Foster Drain (north of the Jock)
0580-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0581-----+
0582-----+ -----
0583-----+ Catchments KEEFE
0584-----+ To Foster Drain (north of the Jock)
0585-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0586-----+
0587-----+ -----
0588-----+ Catchments KEEFE
0589-----+ To Foster Drain (north of the Jock)
0590-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0591-----+
0592-----+ -----
0593-----+ Catchments KEEFE
0594-----+ To Foster Drain (north of the Jock)
0595-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0596-----+
0597-----+ -----
0598-----+ Catchments KEEFE
0599-----+ To Foster Drain (north of the Jock)
0600-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0601-----+
0602-----+ -----
0603-----+ Catchments KEEFE
0604-----+ To Foster Drain (north of the Jock)
0605-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0606-----+
0607-----+ -----
0608-----+ Catchments KEEFE
0609-----+ To Foster Drain (north of the Jock)
0610-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0611-----+
0612-----+ -----
0613-----+ Catchments KEEFE
0614-----+ To Foster Drain (north of the Jock)
0615-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0616-----+
0617-----+ -----
0618-----+ Catchments KEEFE
0619-----+ To Foster Drain (north of the Jock)
0620-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0621-----+
0622-----+ -----
0623-----+ Catchments KEEFE
0624-----+ To Foster Drain (north of the Jock)
0625-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0626-----+
0627-----+ -----
0628-----+ Catchments KEEFE
0629-----+ To Foster Drain (north of the Jock)
0630-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0631-----+
0632-----+ -----
0633-----+ Catchments KEEFE
0634-----+ To Foster Drain (north of the Jock)
0635-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0636-----+
0637-----+ -----
0638-----+ Catchments KEEFE
0639-----+ To Foster Drain (north of the Jock)
0640-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0641-----+
0642-----+ -----
0643-----+ Catchments KEEFE
0644-----+ To Foster Drain (north of the Jock)
0645-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0646-----+
0647-----+ -----
0648-----+ Catchments KEEFE
0649-----+ To Foster Drain (north of the Jock)
0650-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0651-----+
0652-----+ -----
0653-----+ Catchments KEEFE
0654-----+ To Foster Drain (north of the Jock)
0655-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0656-----+
0657-----+ -----
0658-----+ Catchments KEEFE
0659-----+ To Foster Drain (north of the Jock)
0660-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0661-----+
0662-----+ -----
0663-----+ Catchments KEEFE
0664-----+ To Foster Drain (north of the Jock)
0665-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0666-----+
0667-----+ -----
0668-----+ Catchments KEEFE
0669-----+ To Foster Drain (north of the Jock)
0670-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0671-----+
0672-----+ -----
0673-----+ Catchments KEEFE
0674-----+ To Foster Drain (north of the Jock)
0675-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0676-----+
0677-----+ -----
0678-----+ Catchments KEEFE
0679-----+ To Foster Drain (north of the Jock)
0680-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0681-----+
0682-----+ -----
0683-----+ Catchments KEEFE
0684-----+ To Foster Drain (north of the Jock)
0685-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0686-----+
0687-----+ -----
0688-----+ Catchments KEEFE
0689-----+ To Foster Drain (north of the Jock)
0690-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0691-----+
0692-----+ -----
0693-----+ Catchments KEEFE
0694-----+ To Foster Drain (north of the Jock)
0695-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0696-----+
0697-----+ -----
0698-----+ Catchments KEEFE
0699-----+ To Foster Drain (north of the Jock)
0700-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0701-----+
0702-----+ -----
0703-----+ Catchments KEEFE
0704-----+ To Foster Drain (north of the Jock)
0705-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0706-----+
0707-----+ -----
0708-----+ Catchments KEEFE
0709-----+ To Foster Drain (north of the Jock)
0710-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0711-----+
0712-----+ -----
0713-----+ Catchments KEEFE
0714-----+ To Foster Drain (north of the Jock)
0715-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0716-----+
0717-----+ -----
0718-----+ Catchments KEEFE
0719-----+ To Foster Drain (north of the Jock)
0720-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0721-----+
0722-----+ -----
0723-----+ Catchments KEEFE
0724-----+ To Foster Drain (north of the Jock)
0725-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0726-----+
0727-----+ -----
0728-----+ Catchments KEEFE
0729-----+ To Foster Drain (north of the Jock)
0730-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0731-----+
0732-----+ -----
0733-----+ Catchments KEEFE
0734-----+ To Foster Drain (north of the Jock)
0735-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0736-----+
0737-----+ -----
0738-----+ Catchments KEEFE
0739-----+ To Foster Drain (north of the Jock)
0740-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0741-----+
0742-----+ -----
0743-----+ Catchments KEEFE
0744-----+ To Foster Drain (north of the Jock)
0745-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0746-----+
0747-----+ -----
0748-----+ Catchments KEEFE
0749-----+ To Foster Drain (north of the Jock)
0750-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0751-----+
0752-----+ -----
0753-----+ Catchments KEEFE
0754-----+ To Foster Drain (north of the Jock)
0755-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0756-----+
0757-----+ -----
0758-----+ Catchments KEEFE
0759-----+ To Foster Drain (north of the Jock)
0760-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0761-----+
0762-----+ -----
0763-----+ Catchments KEEFE
0764-----+ To Foster Drain (north of the Jock)
0765-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0766-----+
0767-----+ -----
0768-----+ Catchments KEEFE
0769-----+ To Foster Drain (north of the Jock)
0770-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0771-----+
0772-----+ -----
0773-----+ Catchments KEEFE
0774-----+ To Foster Drain (north of the Jock)
0775-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0776-----+
0777-----+ -----
0778-----+ Catchments KEEFE
0779-----+ To Foster Drain (north of the Jock)
0780-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0781-----+
0782-----+ -----
0783-----+ Catchments KEEFE
0784-----+ To Foster Drain (north of the Jock)
0785-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0786-----+
0787-----+ -----
0788-----+ Catchments KEEFE
0789-----+ To Foster Drain (north of the Jock)
0790-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0791-----+
0792-----+ -----
0793-----+ Catchments KEEFE
0794-----+ To Foster Drain (north of the Jock)
0795-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0796-----+
0797-----+ -----
0798-----+ Catchments KEEFE
0799-----+ To Foster Drain (north of the Jock)
0800-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
0801-----+
0802-----+ -----
0803-----+ Catchments KEEFE
0804-----+ To Foster Drain (north of the Jock)
0805-----+ Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
080
```

00375+ 002:0033----- ID:NHDY--- AREA--- QPEAK-TpeakDate\_hh:mm--- R.V.-R.C.-  
00376+ CONINUOUS STANDHYD07:FRASE 90.00 2.860 No\_date 28/05 20.31 .446  
00377+ [XIMP= 25:TIME=.25] .00  
00378+ [LOSS= 2 :CN= 80.0] .00  
00379+ [Pervious area: Iaper= 4.67:SLDP=1.00:LGP= 40:NHD= 250:SCP= .0] .00  
00380+ [Impervious area: IaImp= 1.57:SLD1=1.00:LGI= 775:NHH= .013:SCI= .0] .00  
00381+ [iakECLimp= 4.00: iakRECP= 4.00]  
00382+ [ROUTE CHANNEL= 26.32: SMAN= 500: LWD= 50]  
00383+ 002:0034----- ID:NHDY--- AREA--- QPEAK-TpeakDate\_hh:mm--- R.V.-R.C.-  
00384+ ROUTE RESERVOIR > 07:FRASE 90.00 2.860 No\_date 28/05 20.31 n/a  
00385+ [MDT = 5.00] cut< 01:MS\_P2 28.48 0.00 No\_date 28/05 20.31 n/a  
00386+ overflow <> 09:k-OVF 2.793 No\_date 28/05 20.31 n/a  
00387+ [McDsClded.. 3600B=00, TotOvVnl= 1250F=01, N-Ovf= 2, Tothurf= 13, hrs]  
00388+ ADD HYD  
00389+ 05:KEM\_P 208.71 1.150 No\_date 28/10 28.17 n/a  
00390+ \* 06:KEM-OD 72.21 12.623 No\_date 28/10 28.17 n/a  
00391+ \* 07:FRASE 90.00 2.860 No\_date 28/10 28.17 n/a  
00392+ \* 09:P2-OVF 61.52 2.793 No\_date 28/05 20.31 n/a  
00393+ \* 01\_N\_KB 54338.02 48.099 No\_date 36/15 13.045 n/a  
00394+ [G7.. 5.001 SUM 10:SN\_MI 54338.02 48.099 No\_date 36/15 13.045 n/a  
00395+ [LOSS= 2 :CN= 80.0] .00  
00396+ 002:0036----- ID:NHDY--- AREA--- QPEAK-TpeakDate\_hh:mm--- R.V.-R.C.-  
00397+ SAVE HVD  
00398+ frame :C:\Navin\Octobe\1\CONTIN-1\SMR\_POST\H-SN.KB.002  
00399+ remark:Total Flows at Ken-Burnett Outlet  
00400+ Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
00401+ 002:0037----- ID:NHDY--- AREA--- QPEAK-TpeakDate\_hh:mm--- R.V.-R.C.-  
00402+ CONINUOUS STANDHYD08:TOOD 195.00 6.304 No\_date 28/05 25.18 .553  
00403+ [XIMP= 43:TIME=.43] .00  
00404+ [ROUTE CHANNEL= 26.32: SMAN= 500: LWD= 50]  
00405+ [Pervious area: Iaper= 4.67:SLDP=1.00:LGP= 40:NHD= 250:SCP= .0] .00  
00406+ [Impervious area: IaImp= 1.57:SLD1=1.00:LGI= 1140:NHH= .013:SCI= .0] .00  
00407+ [iakECLimp= 4.00: iakRECP= 4.00]  
00408+ # Catchment TOOD  
00409+ \* To Jock River (south of the Jock)  
00410+ # Subdivision with 43% imp. per Barrhaven South M5S  
00411+ \*\*\*\*\*  
00412+ 002:0038----- ID:NHDY--- AREA--- QPEAK-TpeakDate\_hh:mm--- R.V.-R.C.-  
00413+ CONINUOUS STANDHYD03:TOOD 195.00 6.304 No\_date 28/05 25.18 .553  
00414+ [XIMP= 43:TIME=.43] .00  
00415+ [ROUTE CHANNEL= 26.32: SMAN= 500: LWD= 50]  
00416+ [Pervious area: Iaper= 4.67:SLDP=1.00:LGP= 40:NHD= 250:SCP= .0] .00  
00417+ [Impervious area: IaImp= 1.57:SLD1=1.00:LGI= 1140:NHH= .013:SCI= .0] .00  
00418+ [iakECLimp= 4.00: iakRECP= 4.00]  
00419+ [SMIN= 31.15: SMAX=207.66: SK= .010]  
00420+ \*\*\*\*\*  
00421+ # Todd Pond  
00422+ # - Rating curve obtained from Barrhaven South M5S modeling  
00423+ # - Tributary Drainage Area to M5S Pond 3 = 193 ha  
00424+ # - Rating curve obtained from Barrhaven South M5S modeling  
00425+ 002:0039----- ID:NHDY--- AREA--- QPEAK-TpeakDate\_hh:mm--- R.V.-R.C.-  
00426+ CONINUOUS STANDHYD03:TOOD 195.00 6.304 No\_date 28/05 25.18 .553  
00427+ [ROUTE CHANNEL= 26.32: SMAN= 500: LWD= 50]  
00428+ overflow <> 09:P3-OVF 45.22 8.086 No\_date 28/10 25.18 n/a  
00429+ [McDsClded.. 7798B=00, TotOvVnl= 1250F=01, N-Ovf= 2, Tothurf= 13, hrs]  
00430+ 002:0040----- ID:NHDY--- AREA--- QPEAK-TpeakDate\_hh:mm--- R.V.-R.C.-  
00431+ ADD HYD  
00432+ 01\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00433+ \* 02\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00434+ \* 03\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00435+ \* 04\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00436+ \* 05\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00437+ \* 06\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00438+ \* 07\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00439+ \* 08\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00440+ \* 09\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00441+ \* 10\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00442+ \* 11\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00443+ \* 12\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00444+ \* 13\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00445+ \* 14\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00446+ \* 15\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00447+ \* 16\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00448+ \* 17\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00449+ \* 18\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00450+ \* 19\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00451+ \* 20\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00452+ \* 21\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00453+ \* 22\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00454+ \* 23\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00455+ \* 24\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00456+ \* 25\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00457+ \* 26\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00458+ \* 27\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00459+ \* 28\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00460+ \* 29\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00461+ \* 30\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00462+ \* 31\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00463+ \* 32\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00464+ \* 33\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00465+ \* 34\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00466+ \* 35\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00467+ \* 36\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00468+ \* 37\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00469+ \* 38\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00470+ \* 39\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00471+ \* 40\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00472+ \* 41\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00473+ \* 42\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00474+ \* 43\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00475+ \* 44\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00476+ \* 45\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00477+ \* 46\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00478+ \* 47\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00479+ \* 48\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00480+ \* 49\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00481+ \* 50\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00482+ \* 51\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00483+ \* 52\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00484+ \* 53\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00485+ \* 54\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00486+ \* 55\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00487+ \* 56\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00488+ \* 57\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00489+ \* 58\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00490+ \* 59\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00491+ \* 60\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00492+ \* 61\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00493+ \* 62\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00494+ \* 63\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00495+ \* 64\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00496+ \* 65\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00497+ \* 66\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00498+ \* 67\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00499+ \* 68\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00500+ \* 69\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00501+ \* 70\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00502+ \* 71\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00503+ \* 72\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00504+ \* 73\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00505+ \* 74\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00506+ \* 75\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00507+ \* 76\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00508+ \* 77\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00509+ \* 78\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00510+ \* 79\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00511+ \* 80\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00512+ \* 81\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00513+ \* 82\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00514+ \* 83\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00515+ \* 84\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00516+ \* 85\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00517+ \* 86\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00518+ \* 87\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00519+ \* 88\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00520+ \* 89\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00521+ \* 90\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00522+ \* 91\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00523+ \* 92\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00524+ \* 93\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00525+ \* 94\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00526+ \* 95\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00527+ \* 96\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00528+ \* 97\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00529+ \* 98\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00530+ \* 99\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00531+ \* 100\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00532+ \* 101\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00533+ \* 102\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00534+ \* 103\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00535+ \* 104\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00536+ \* 105\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00537+ \* 106\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00538+ \* 107\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00539+ \* 108\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00540+ \* 109\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00541+ \* 110\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00542+ \* 111\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00543+ \* 112\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00544+ \* 113\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00545+ \* 114\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00546+ \* 115\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00547+ \* 116\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00548+ \* 117\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00549+ \* 118\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00550+ \* 119\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00551+ \* 120\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00552+ \* 121\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00553+ \* 122\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00554+ \* 123\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00555+ \* 124\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00556+ \* 125\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00557+ \* 126\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00558+ \* 127\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00559+ \* 128\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00560+ \* 129\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00561+ \* 130\_N\_TO 54709.01 49.001 No\_date 36/15 13.11 n/a  
00562+ overflow <> 04:JO-OVF 0.00 0.00 No\_date 0:00 .00 n/a  
00563+ [McDsClded.. 2128=00, TotOvFvl= 400000, N-Ovf= 2, Tothurf= 13, hrs]  
00564+ ADD HYD  
00565+ 01\_N\_TO 55192.02 49.452 No\_date 37/30 13.21 n/a  
00566+ \* 02\_N\_TO 55192.02 49.452 No\_date 37/30 19.26 n/a  
00567+ \* 03\_N\_TO 55192.02 49.452 No\_date 37/30 0.00 n/a  
00568+ \* 04\_N\_TO 55192.02 49.452 No\_date 37/30 2.252 No\_date 29/10 26.85 n/a  
00569+ \* 05\_N\_TO 55192.02 49.452 No\_date 37/30 13.21 n/a  
00570+ [LOSS= 5.001] SDM 55468.01 49.870 No\_date 37/20 13.28 n/a  
00571+ SAVE HVD  
00572+ frame :C:\Navin\Octobe\1\CONTIN-1\SMR\_POST\H-SN.DE.002  
00573+ remark:Total Flows at Heart's Desire  
00574+ # Hydrograph from Heart's Desire routed to Rideau River  
00575+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 0  
00576+ # Catchment JOCK  
00577+ # To Jock River (north and south)  
00578+ # - Undeveloped floodplain and river  
00579+ \*\*\*\*\*  
00580+ 002:0058----- ID:NHDY--- AREA--- QPEAK-TpeakDate\_hh:mm--- R.V.-R.C.-  
00581+ CONTINUOUS NASHD 028=2 102.00 1.359 No\_date 28/20 13.01 .286  
00582+ [ROUTE CHANNEL = 028=2 102.00 1.359 No\_date 28/20 13.01 .286]  
00583+ [LOSS= 5.001] SDM 55468.01 49.870 No\_date 37/25 13.28 n/a  
00584+ \*\*\*\*\*  
00585+ 002:0059----- ID:NHDY--- AREA--- QPEAK-TpeakDate\_hh:mm--- R.V.-R.C.-  
00586+ CONTINUOUS NASHD 028=2 102.00 1.359 No\_date 28/20 13.01 .286  
00587+ [ROUTE CHANNEL = 028=2 102.00 1.359 No\_date 28/20 13.01 .286]  
00588+ [LOSS= 5.001] SDM 55468.01 49.870 No\_date 37/25 13.28 n/a  
00589+ \*\*\*\*\*  
00590+ 002:0060----- ID:NHDY--- AREA--- QPEAK-TpeakDate\_hh:mm--- R.V.-R.C.-  
00591+ CONTINUOUS NASHD 028=2 102.00 1.359 No\_date 28/20 13.01 .286  
00592+ [ROUTE CHANNEL = 028=2 102.00 1.359 No\_date 28/20 13.01 .286]  
00593+ [LOSS= 5.001] SDM 55468.01 49.870 No\_date 37/25 13.28 n/a  
00594+ \*\*\*\*\*  
00595+ 002:0061----- ID:NHDY--- AREA--- QPEAK-TpeakDate\_hh:mm--- R.V.-R.C.-  
00596+ CONTINUOUS NASHD 028=2 102.00 1.359 No\_date 28/20 13.01 .286  
00597+ [ROUTE CHANNEL = 028=2 102.00 1.359 No\_date 28/20 13.01 .286]  
00598+ [LOSS= 5.001] SDM 55468.01 49.870 No\_date 37/25 13.28 n/a  
00599+ \*\*\*\*\*  
00600+ 002:0062----- ID:NHDY--- AREA--- QPEAK-TpeakDate\_hh:mm--- R.V.-R.C.-  
00601+ CONTINUOUS NASHD 028=2 102.00 1.359 No\_date 28/20 13.01 .286  
00602+ [ROUTE CHANNEL = 028=2 102.00 1.359 No\_date 28/20 13.01 .286]  
00603+ [LOSS= 5.001] SDM 55468.01 49.870 No\_date 37/25 13.28 n/a  
00604+ \*\*\*\*\*  
00605+ 002:0063----- ID:NHDY--- AREA--- QPEAK-TpeakDate\_hh:mm--- R.V.-R.C.-  
00606+ CONTINUOUS STANDHYD02:MILLS 139.00 5.455 No\_date 28/05 22.75 n/a  
00607+ [ROUTE RESERVOIR > 02:MILLS 139.00 1.782 No\_date 28/05 22.75 n/a]  
00608+ [LOSS= 2 :CN= 77.0] .00  
00609+ [Pervious area: Iaper= 4.67:SLDP=1.00:LGP= 40:NHD= 250:SCP= .0] .00  
00610+ [Impervious area: IaImp= 1.57:SLD1=1.00:LGI= 963:NHH= .013:SCI= .0] .00  
00611+ ADD HYD  
00612+ 04:MIL-OD 139.00 5.455 No\_date 0:00 ..00  
00613+ \* 05:MIL-OVF 139.00 5.455 No\_date 27/25 25.84 n/a  
00614+ overflow <> 09:k-OVF 28.00 25.84 No\_date 28/10 25.84 n/a  
00615+ ADD HYD  
00616+ 01\_N\_M 54904.01 49.134 No\_date 36/45 13.16 n/a  
00617+ \* 02\_N\_M 54904.01 49.134 No\_date 36/45 13.16 n/a  
00618+ \* 03\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00619+ \* 04\_N\_M 55053.02 49.312 No\_date 0:00 ..00  
00620+ \* 05\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00621+ \* 06\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00622+ \* 07\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00623+ \* 08\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00624+ \* 09\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00625+ \* 10\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00626+ \* 11\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00627+ \* 12\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00628+ \* 13\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00629+ \* 14\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00630+ \* 15\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00631+ \* 16\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00632+ \* 17\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00633+ \* 18\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00634+ \* 19\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00635+ \* 20\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00636+ \* 21\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00637+ \* 22\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00638+ \* 23\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00639+ \* 24\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00640+ \* 25\_N\_M 55053.02 49.312 No\_date 36/45 13.16 n/a  
00641+ \* 26\_N\_M 55053.02 49.312 No\_date 36/45 13.

007495 # - On Jock 08:00 359.8T 18.63z No\_date 28:20 34.02 n/a  
 007500 [DT= 5.00] SUM- 03:SN\_CK 53477.01 68.19z No\_date 34:05 18.44 n/a  
 007510 005:0013-----ID:NHDY---ARA---OPEAK-TpeakDate\_hh:mm---R.V.-R.C.-  
 007520 CONTINUOUS STANDBYS1:01:ROUTE 005:0013:00:LOGD- 75.5M 68.19z No\_date 34:05 18.44 n/a  
 007530 frame :c:\Navin\OCBTEC-1\CONTIN-1\SMW\_POSTV\SN\_TO\_005  
 007540 remark: Total Flows at Okeefe Drain  
 007550 # Hydrograph from Node Okeefe routed to Node at Foster Drain  
 007570 # Channel X-Section obtained from RVCA Hydraulic Model - Station 6215  
 007580 005:0014-----ID:NHDY---ARA---OPEAK-TpeakDate\_hh:mm---R.V.-R.C.-  
 007590 ROUTE CHANNEL > 03:SN\_CK 53477.01 68.19z No\_date 34:05 18.44 n/a  
 007600 [DT= 5.00] SUM- 03:SN\_CK 53477.01 68.12z No\_date 34:20 18.44 n/a  
 007610 [L/S/n= 1.83z .076/.035]  
 007630 [Vmax: 1.826;dmag: .015]  
 007640 # Catchment Okeefe  
 007650 # - To Foster ditch (north of the Jock)  
 007660 # - Developed land with assumed 43% imp.  
 007670 # - Subdivision with 43% imp. as per Barrenhaven South NBS  
 007680 005:0015-----ID:NHDY---ARA---OPEAK-TpeakDate\_hh:mm---R.V.-R.C.-  
 007690 CONTINUOUS STANDBYS1:POSTER 373.00 26.65z No\_date 28:10 37.71 660  
 007700 [XIMP=.5;TIMP=.55]  
 007720 [LOSS= 2 :74.00z]  
 007730 [Previous area: Iaper: 4.67:SLPP-.55:LOGD- 40. :NND-.250:SCP-.0]  
 007740 [Impervious area: Ialmp: 1.57:SLD1-.55:LOG1=1577.:NNI=.013:SCI=.0]  
 007750 [IaReClmp: 4.00: IaReCper: 4.00]  
 007760 [IaReCmp: 4.00: IaReCper: 4.00]  
 007770 \*\*\*\*\*  
 007780 # Foster Pond  
 007790 # - Rating curve obtained assuming 4m3/ha in 24 hours for quality control  
 007800 # - Ratio of the catchment area to the West Clarke pond rating curve  
 007810 from the NBS for the next coordinates  
 007820 \*\*\*\*\*  
 007830 005:0018-----ID:NHDY---ARA---OPEAK-TpeakDate\_hh:mm---R.V.-R.C.-  
 007840 ROUTE CHANNEL > 03:SN\_CK 53477.01 20.65z No\_date 28:10 37.71 n/a  
 007850 [DT= 5.00] out< 01:NC\_CE 53477.01 20.65z No\_date 28:15 37.71 n/a  
 007860 overflow < 09:PO-OPV 293.39 20.19z No\_date 28:15 37.71 n/a  
 007870 [ROUTE CHANNEL > 1720.00z TotDvVol=1.100E+01.00:OpV= 2 ,TotThruRof= 14. hrs]  
 007880 \*\*\*\*\*  
 007890 ADD HYD  
 007900 [G1\_M\_P0 53477.01 68.12z No\_date 34:20 18.44 n/a  
 007910 \* [G1\_M\_P1 53477.01 68.12z No\_date 28:45 37.71 n/a  
 007920 \* [G1\_M\_P2 53477.01 68.12z No\_date 34:20 18.57 n/a  
 007930 \*\*\*\*\*  
 007940 [DT= 5.00] SUM- 03:SN\_CK 53850.01 68.97z No\_date 34:20 18.57 n/a  
 007950 frame :c:\Navin\OCBTEC-1\CONTIN-1\SMW\_POSTV\SN\_TO\_005  
 007960 remark: Total Flows at Foster Drain  
 007970 #  
 007980 # Hydrograph from Node Foster routed to Node at Cedarview Road  
 007990 # Channel X-Section obtained from RVCA Hydraulic Model - Station 6016  
 008000 005:0019-----ID:NHDY---ARA---OPEAK-TpeakDate\_hh:mm---R.V.-R.C.-  
 008010 ROUTE CHANNEL > 03:SN\_CK 53880.01 68.97z No\_date 34:20 18.57 n/a  
 008020 [DT= 5.00] out< 01:NC\_CE 53880.01 68.97z No\_date 34:20 18.57 n/a  
 008030 [L/S/n= 159. /082/.035]  
 008040 \*\*\*\*\*  
 008050 \*\*\*\*\*  
 008060 \*\*\*\*\*  
 008070 # Catchment S-1  
 008080 # - Residential (north and south of Jock)  
 008090 # - Primarily agricultural fields; portion of sand quarry  
 008100 \*\*\*\*\*  
 008110 005:0020-----ID:NHDY---ARA---OPEAK-TpeakDate\_hh:mm---R.V.-R.C.-  
 008120 CONTINUOUS NASHWD 02:8- 240.00 3.163 No\_date 29:10 21.69 386  
 008130 [CN= 77.00 :N= 3.00]  
 008140 [ROUTE CHANNEL > 03:SN\_CK 53880.01 68.97z No\_date 34:15 18.67 n/a  
 008150 [IaReD= 4.00: SMMN: 31.15: SNMX: 207.66 :SK= .010]  
 008160 [IaReCmp: 4.00: IaReCper: 4.00]  
 008170 [IaReCmp: 4.00: IaReCper: 4.00]  
 008180 \*\*\*\*\*  
 008190 ADD HYD  
 008200 [G1\_M\_P0 53850.01 68.97z No\_date 34:20 18.57 n/a  
 008210 \* [G1\_M\_P1 53850.01 3.163 No\_date 29:10 21.69 n/a  
 008220 \* [G1\_M\_P2 53850.01 68.97z No\_date 34:15 18.67 n/a  
 008230 \*\*\*\*\*  
 008240 SAVE HYD  
 008250 [c:\Navin\OCBTEC-1\CONTIN-1\SMW\_POSTV\SN\_TO\_005  
 008260 remark: Total Flows at Cedarview Road  
 008270 #  
 008280 # Hydrograph from Node Cedarview Road routed to Node at West Clarke Brain  
 008290 # Channel X-Section obtained from RVCA Hydraulic Model - Station 5002  
 008300 005:0021-----ID:NHDY---ARA---OPEAK-TpeakDate\_hh:mm---R.V.-R.C.-  
 008310 ROUTE CHANNEL > 03:SN\_CK 54095.01 69.51z No\_date 34:15 18.58 n/a  
 008320 [DT= 5.00] SUM- 03:SN\_CK 54095.01 69.49z No\_date 34:25 18.58 n/a  
 008330 \*\*\*\*\*  
 008340 \*\*\*\*\*  
 008350 # Catchment W\_CLAR  
 008360 # - West Clarke Brain (south of the Jock)  
 008370 # Subdivision with 43% imp. as per Barrenhaven South NBS  
 008380 # - Residential development  
 008390 005:0022-----ID:NHDY---ARA---OPEAK-TpeakDate\_hh:mm---R.V.-R.C.-  
 008400 ROUTE CHANNEL > 03:SN\_CK 54095.01 69.51z No\_date 34:15 18.58 n/a  
 008410 [ROUTE CHANNEL > 03:SN\_CK 54095.01 69.49z No\_date 34:25 18.58 n/a  
 008420 [L/S/n= 825. /045/.035]  
 008430 \*\*\*\*\*  
 008440 [Vmax: 1.282;dmag: .001]  
 008450 \*\*\*\*\*  
 008460 # West Clarke Pond 2  
 008470 # - Residential developed from Barrenhaven South NBS modeling  
 008480 # - Tributary Drainage Area to MSS Pond 2 = 241 ha  
 008490 \*\*\*\*\*  
 008500 005:0023-----ID:NHDY---ARA---OPEAK-TpeakDate\_hh:mm---R.V.-R.C.-  
 008510 ROUTE CHANNEL > 03:SN\_CK 54095.01 69.51z No\_date 34:15 18.58 n/a  
 008520 [ROUTE CHANNEL > 03:SN\_CK 54095.01 69.49z No\_date 34:25 18.58 n/a  
 008530 \*\*\*\*\*  
 008540 \*\*\*\*\*  
 008550 # Catchment W\_CLAR  
 008560 # - West Clarke Brain (south of the Jock)  
 008570 # Subdivision with 43% imp. as per Barrenhaven South NBS  
 008580 005:0024-----ID:NHDY---ARA---OPEAK-TpeakDate\_hh:mm---R.V.-R.C.-  
 008590 ROUTE CHANNEL > 03:SN\_CK 54095.01 69.51z No\_date 34:15 18.58 n/a  
 008600 [ROUTE CHANNEL > 03:SN\_CK 54095.01 69.49z No\_date 34:25 18.58 n/a  
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 008620 005:0025-----ID:NHDY---ARA---OPEAK-TpeakDate\_hh:mm---R.V.-R.C.-  
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01123 ADD HWD 01:NI 55469.00 72.141 No\_date 36:20 18.97 n/a  
 01124 ADD HWD 02:S-2 102.00 2.237 No\_date 28:20 18.99 n/a  
 01125 ADD HWD 03:SN\_1M 55570.00 72.311 No\_date 36:20 18.97 n/a  
 005:064-  
 01126 SAW HWD 03:SN\_1M 55570.00 72.311 No\_date 36:20 18.97 n/a  
 01127 frame :C:\Navin\Octobre\1\CONTIN\1\BMR\_POST\N-SN\_N1.005  
 01128 \* Total Flow at Rideau River  
 01129 \*\*\* END OF RUN 24  
 01130  
 01131 RUM:COMMANDS  
 01132 # C:\2005\001...  
 01133 \* TZERO = .00 hrs on [0]  
 01142 # METROT= 2 (Imperial, 2-metric output)  
 01143 # NSTDM= 1  
 01144 # NODIM= 25  
 01145 \*\*\*  
 01146 Project Name: Jock River Reach 1 Subwatershed Study|Project #: (160400414)  
 01147 # Author: [Navin Gautam/ Original by Ana M Perez]  
 01148 # Modeler: [Starmap]  
 01149 # Company: [Starmap]  
 01150 # User ID: [824306]  
 01151 \*\*\*  
 01152 \*\*\*  
 01153 # C:\2005\002...  
 01154 READ STORM  
 01155 # Read Storms.storm.001  
 01156 Comment = Plusie SCS for 24 hours 1:25 am point Ottawa CDA  
 01157 [STD=10.00] SDR= 24.00[PDT= 74.39]  
 025:0002-  
 01158 MODIFY STORM  
 01159 # [PFACT= 1.00]TSHFT= 96.00 min  
 01160 # [SDR= 10.00] SDR= 10.00[PDT= 74.39]  
 01162 # C:\2005\004...  
 01163 DEFAULT VALUES  
 01164 # Parameters used in (Navin\Octobre\1\CONTIN\1\BMR\_POST\MODIFIED.VAL)  
 01165 ICASDv2 = 1 (read and print data)  
 01166 Filetitle= File comment: [2005 City of Ottawa Sewer Design Guideline]  
 01167 # Parameters used in (Navin\Octobre\1\CONTIN\1\BMR\_POST\STANDARD.COMMAND FOR OTTAWA)  
 01168 Horton's infiltration equation parameters:  
 01169 # [Fw= 76.20 mm/hr] [FCw= 13.20 mm/hr] [FW= 4.14 /hr] [FW= .00 mm]  
 01170 # [Pw= 1.00 mm hr] [PW= 1.00 mm hr] [Pfw= 1.00 mm hr]  
 01171 # [Iaper= 4.67 mm] [LGP= 40.00 m] [MNP=.250]  
 01172 # Parameters for IMPERVIOUS surfaces in STANDARDYD:  
 01173 # [IN= 1.00] [LDP= 1.00] [LGP= 1.00] [MNP=.013]  
 01174 # Parameters used in NASHYD:  
 01175 # [In= .25 mm] [N= 3.00]  
 025:0003-  
 01176 COMPUTE API  
 01177 # [APini= 5.00] [APDp0= 8500.00] [APhd= .8989]  
 01178 # [APd0= 1.76] [APdr= 55.03] [APdm= 44.87]  
 01180 \*\*\*  
 01183 # JOCK RIVER REACH 1 SUBWATERSHED STUDY DISCRETIZED MODEL  
 01184 # PROPOSED CONDITIONS DESIGN STORM MODEL (SUMMER)  
 01185 # Version: Draft Final Report, October 2006  
 01186 # Revision History  
 01187 # Draft Internal Condition Report, Nov. 2005  
 01188 \*\*\*  
 01189 # Assumptions  
 01190 # - All catchments are assumed to be developed except S-1, S-2, and SW-1a  
 01191 # - Catchments are modeled  
 01192 # - Rating curves were estimated based on existing reports and modeling for the  
 01193 # proposed conditions.  
 01194 # - The proposed outlet for the existing Kennedy Burnett Settling Pond (URKTP)- R  
 01195 # - The Urban Runoff Treatment in the Kennedy Burnett Settling Pond (URKTP)- R  
 01196 # - Municipality of Ottawa Carleton, March 1983  
 01197 # - Rivers cross sections obtained from RVCA's HEC-RAS hydraulic model  
 01198 # - River cross sections obtained from RVCA's HEC-RAS hydraulic model  
 01199 # -  
 01200 # Design Storms: 1.5, 10, 25, 50, 50 60y events: 24hr SCS (DT=10min) model comp  
 01201 # with 100% impervious area, rural subdivision, 20% urban wss  
 01202 # (NRCS/SCS) CN based on landuse (airphoto) and soil type (base mapping)  
 01204 # - Time to peak using Uplands Method  
 01205 #  
 025:0004-  
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01487# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462

01488#

01489# 025:0042-----> ID:NHVD----> AREA---QPEAK-TpeakDate\_hh:mm---R.V.-R.C.-

01490# \* ROUTE CHANNEL > 01\_SN\_TD 54904.01 111.061 No\_date 35:00 29.29 n/a

01491# \* [ROUTE 5.00] cut<- 01\_SN\_TD 54904.01 110.730 No\_date 35:20 29.29 n/a

01492# [L/S/nr . . . . . / .053/.045]

01493# [Vmax=.717:Dmax= 3.588]

01494# \*\*\*\*\*

01495# \* Catchment CORDIO

01496# \* To Corriagan Drain (south of the Jock)

01497# \* Primarily Developed (medium density)

01498# \*\*\*\*\*

01499# 025:0043-----> ID:NHVD----> AREA---QPEAK-TpeakDate\_hh:mm---R.V.-R.C.-

01500# \* CONTINUOUS STANDHYDRO CORRIAN

01501# [KIND= 45:TIMEP=.45]

01502# [LOGS= 2 :CIN 77.0]

01503# [Pervious area: IAlmp= 4.67:SLDP=1.00:LDP= 40.:NMP=.250:SCP= .0]

01504# [Impervious area: IAlmp= 1.57:SLDP=1.00:LGI= 997.:MMI=.013:SCI= .0]

01505# [iAbECimp= 4.00: iAbECper= 4.00]

01506# [iAbECimp= 11.15:Dmax= 4.00]

01507# \*\*\*\*\*

01508# \* Corriagan Pond

01509# \* Total Flows obtained from Barrhaven South MNS modeling

01510# \* Tributary Drainage Area to MSS Pond 1 = 145 ha

01511# \*\*\*\*\*

01512# 025:0044-----> ID:NHVD----> AREA---QPEAK-TpeakDate\_hh:mm---R.V.-R.C.-

01513# \* ROUTE RESERVOIR > 02\_CORRIAN 149.00 14.272 No\_date 28:05 49.32 n/a

01514# [ROUTE 5.00] cut<- 05\_MS\_P1 20.01 .060 No\_date 25:15 49.32 n/a

01515# [ROUTE 5.00] cut<- 05\_MS\_P2 14.272 No\_date 25:15 49.32 n/a

01516# [MSgtColseed=.5798E+00, TotCvFv1=.6362E+01, N-Ovr= . . . . . , TotDurOvf=.15, hrs]

01517# 025:0045-----> ID:NHVD----> AREA---QPEAK-TpeakDate\_hh:mm---R.V.-R.C.-

01518# ADD HYD

01519# \* [ROUTE 5.00] SUM 149.00 14.272 No\_date 28:05 49.32 n/a

01520# + 04\_P1\_OVR 128.99 14.115 No\_date 28:05 49.32 n/a

01521# \*\*\*\*\*

01522# 025:0046-----> ID:NHVD----> AREA---QPEAK-TpeakDate\_hh:mm---R.V.-R.C.-

01523# \* ROUTE RESERVOIR > 02\_CORRIAN 149.00 14.272 No\_date 28:05 49.32 n/a

01524# [ROUTE 5.00] cut<- 05\_MS\_P1 20.01 .060 No\_date 25:15 49.32 n/a

01525# [ROUTE 5.00] cut<- 05\_MS\_P2 14.272 No\_date 25:15 49.32 n/a

01526# [MSgtColseed=.5798E+00, TotCvFv1=.6362E+01, N-Ovr= . . . . . , TotDurOvf=.15, hrs]

01527# 025:0047-----> ID:NHVD----> AREA---QPEAK-TpeakDate\_hh:mm---R.V.-R.C.-

01528# \* CONTINUOUS STANDHYDRO CORRIAN

01529# [KIND= 45:TIMEP=.45]

01530# [LOGS= 2 :CIN 77.0]

01531# [Pervious area: IAlmp= 4.67:SLDP=1.00:LDP= 40.:NMP=.250:SCP= .0]

01532# [Impervious area: IAlmp= 1.57:SLDP=1.00:LGI= 997.:MMI=.013:SCI= .0]

01533# [iAbECimp= 4.00: iAbECper= 4.00]

01534# [iAbECimp= 11.15:Dmax= 4.00]

01535# \*\*\*\*\*

01536# \* Hydrograph from Corriagan Drain routed to Jockvale Road

01537# \* Channel X-Section obtained from RVCA Hydraulic Model - Station 2462

01538# \*\*\*\*\*

01539# 025:0048-----> ID:NHVD----> AREA---QPEAK-TpeakDate\_hh:mm---R.V.-R.C.-

01540# \* CONTINUOUS STANDHYDRO CATCHMENT MILLS

01541# [KIND= 38:TIMEP=.38]

01542# [LOGS= 2 :CIN 74.0]

01543# [Pervious area: IAlmp= 4.67:SLDP=1.00:LDP= 40.:NMP=.250:SCP= .0]

01544# [Impervious area: IAlmp= 1.57:SLDP=1.00:LGI= 963.:MMI=.013:SCI= .0]

01545# [iAbECimp= 4.00: iAbECper= 4.00]

01546# [iAbECimp= 11.15:Dmax= 4.00]

01547# \*\*\*\*\*

01548# \* Catchment MILLS

01549# \* To SWN Facility north of the Jock

01550# \* Primarily rural/agricultural

01551# \*\*\*\*\*

01552# 025:0049-----> ID:NHVD----> AREA---QPEAK-TpeakDate\_hh:mm---R.V.-R.C.-

01553# \* CONTINUOUS STANDHYDRO CATCHMENT MILLS

01554# [ROUTE 5.00] SUM 139.00 111.193 No\_date 35:20 29.35 n/a

01555# [ROUTE 5.00] cut<- 03\_SN\_CO 55053.01 111.193 No\_date 35:20 29.35 n/a

01556# overflow <= 04\_MIL\_OV .00 .000 No\_date 0:00 .000 n/a

01557# [MSgtColseed=.12708E+01, TotCvFv1=.2151E+02, N-Ovr= . . . . . , TotDurOvf=.15, hrs]

01558# 025:0050-----> ID:NHVD----> AREA---QPEAK-TpeakDate\_hh:mm---R.V.-R.C.-

01559# ADD HYD

01560# \* [ROUTE 5.00] SUM 139.00 111.193 No\_date 35:20 29.35 n/a

01561# + 04\_MIL\_OV 139.00 111.193 No\_date 35:20 29.35 n/a

01562# [ROUTE 5.00] cut<- 05\_MILL\_P 139.00 3.765 No\_date 28:40 44.62 n/a

01563# [ROUTE 5.00] cut<- 05\_MILL\_P 139.00 3.765 No\_date 28:40 44.62 n/a

01564# overflow <= 04\_MIL\_OV .00 .000 No\_date 0:00 .000 n/a

01565# [MSgtColseed=.12708E+01, TotCvFv1=.2151E+02, N-Ovr= . . . . . , TotDurOvf=.15, hrs]

01566# 025:0051-----> ID:NHVD----> AREA---QPEAK-TpeakDate\_hh:mm---R.V.-R.C.-

01567# ADD HYD

01568# \* [ROUTE 5.00] SUM 139.00 111.193 No\_date 35:20 29.35 n/a

01569# + 04\_MIL\_OV 139.00 111.193 No\_date 35:20 29.35 n/a

01570# \*\*\*\*\*

01571# 025:0052-----> ID:NHVD----> AREA---QPEAK-TpeakDate\_hh:mm---R.V.-R.C.-

01572# \* CONTINUOUS STANDHYDRO CATCHMENT SWAN

01573# [ROUTE 5.00] SUM 139.00 111.193 No\_date 35:20 29.35 n/a

01574# name: C:\Navin\Octobe\1\CONTIN-1\SME\_POSTW-SN.MI.025

01575# \*\*\*\*\*

01576# \* Hydrograph from Jockvale Road routed to Heart's Desire

01577# \* Channel X-Section obtained from RVCA Hydraulic Model - Station 698

01578# \*\*\*\*\*

01579# 025:0053-----> ID:NHVD----> AREA---QPEAK-TpeakDate\_hh:mm---R.V.-R.C.-

01580# \* CONTINUOUS STANDHYDRO CATCHMENT SWAN

01581# [ROUTE 5.00] cut<- 01\_SN\_M2 55192.01 111.193 No\_date 35:25 29.38 n/a

01582# [ROUTE 5.00] cut<- 01\_SN\_M2 55192.01 111.196 No\_date 36:05 29.38 n/a

01583# [ROUTE 5.00] cut<- 01\_SN\_M2 55192.01 111.196 No\_date 36:05 29.38 n/a

01584# [ROUTE 5.00] cut<- 01\_SN\_M2 55192.01 111.196 No\_date 36:05 29.38 n/a

01585# \*\*\*\*\*

01586# \* Catchment SWAN

01587# \* To Jockvale SWN Facility

01588# \* Residential and some golf course

01589# \*\*\*\*\*

01590# 025:0054-----> ID:NHVD----> AREA---QPEAK-TpeakDate\_hh:mm---R.V.-R.C.-

01591# \* CONTINUOUS STANDHYDRO2:DESIRE

01592# [KIND= 25:TIMEP=.25]

01593# [LOGS= 2 :CIN 77.0]

01594# [Pervious area: IAlmp= 4.67:SLDP=1.00:LDP= 40.:NMP=.250:SCP= .0]

01595# [Impervious area: IAlmp= 1.57:SLDP=1.00:LGI= 997.:MMI=.013:SCI= .0]

01596# [iAbECimp= 4.00: iAbECper= 4.00]

01597# [iAbECimp= 11.15:Dmax= 207.66: SK= .010]

01598# \*\*\*\*\*

01599# \* Catchment JOCKVA

01600# \* To Jockvale SWN Facility

01601# \* Residential and some golf course

01602# \*\*\*\*\*

01603# 025:0055-----> ID:NHVD----> AREA---QPEAK-TpeakDate\_hh:mm---R.V.-R.C.-

01604# \* CONTINUOUS STANDHYDRO:JOCKVA

01605# [ROUTE 5.00] cut<- 01\_SN\_M2 252.00 22.732 No\_date 28:05 50.68 n/a

01606# [ROUTE 5.00] cut<- 01\_SN\_M2 252.00 22.732 No\_date 28:05 50.68 n/a

01607# [ROUTE 5.00] cut<- 01\_SN\_M2 252.00 22.732 No\_date 28:40 50.08 n/a

01608# overflow <= 04\_JO\_OV .00 .000 No\_date 0:00 .000 n/a

01609# [MSgtColseed=.5185E+01, TotCvFv1=.005E+02, N-Ovr= . . . . . , TotDurOvf=.15, hrs]

01610# 025:0056-----> ID:NHVD----> AREA---QPEAK-TpeakDate\_hh:mm---R.V.-R.C.-

01611# ADD HYD

01612# \* [ROUTE 5.00] SUM 252.00 22.732 No\_date 28:40 50.08 n/a

01613# + 04\_JO\_OV 252.00 22.732 No\_date 28:40 50.08 n/a

01614# [ROUTE 5.00] cut<- 01\_SN\_M2 252.00 22.732 No\_date 28:40 50.08 n/a

01615# [ROUTE 5.00] cut<- 01\_SN\_M2 252.00 22.732 No\_date 28:40 50.08 n/a

01616# overflow <= 04\_JO\_OV .00 .000 No\_date 0:00 .000 n/a

01617# [MSgtColseed=.5185E+01, TotCvFv1=.005E+02, N-Ovr= . . . . . , TotDurOvf=.15, hrs]

01618# 025:0057-----> ID:NHVD----> AREA---QPEAK-TpeakDate\_hh:mm---R.V.-R.C.-

01619# \* CONTINUOUS STANDHYDRO:JOCKVA

01620# [ROUTE 5.00] cut<- 01\_SN\_M2 252.00 22.732 No\_date 28:40 50.08 n/a

01621# [ROUTE 5.00] cut<- 01\_SN\_M2 252.00 22.732 No\_date 28:40 50.08 n/a

01622# [ROUTE 5.00] cut<- 01\_SN\_M2 252.00 22.732 No\_date 28:40 50.08 n/a

01623# [ROUTE 5.00] cut<- 01\_SN\_M2 252.00 22.732 No\_date 28:40 50.08 n/a

01624# [ROUTE 5.00] cut<- 01\_SN\_M2 252.00 22.732 No\_date 28:40 50.08 n/a

01625# [ROUTE 5.00] cut<- 01\_SN\_M2 252.00 22.732 No\_date 28:40 50.08 n/a

01626# [ROUTE 5.00] cut<- 01\_SN\_M2 252.00 22.732 No\_date 28:40 50.08 n/a

01627# [ROUTE 5.00] cut<- 01\_SN\_M2 252.00 22.732 No\_date 28:40 50.08 n/a

01628# [ROUTE 5.00] cut<- 01\_SN\_M2 252.00 22.732 No\_date 28:40 50.08 n/a

01629# \*\*\*\*\*

01630# \* Hydrograph from Heart's Desire routed to Rideau River

01631# \* Channel X-Section obtained from RVCA Hydraulic Model - Station 0

01632# \*\*\*\*\*

01633# 025:0058-----> ID:NHVD----> AREA---QPEAK-TpeakDate\_hh:mm---R.V.-R.C.-

01634# \* CONTINUOUS STANDHYDRO:HEARTS

01635# [ROUTE 5.00] cut<- 01\_SN\_M2 252.00 22.732 No\_date 28:40 50.08 n/a

01636# [ROUTE 5.00] cut<- 01\_SN\_M2 252.00 22.732 No\_date 28:40 50.08 n/a

01637# [ROUTE 5.00] cut<- 01\_SN\_M2 252.00 22.732 No\_date 28:40 50.08 n/a

01638# [ROUTE 5.00] cut<- 01\_SN\_M2 252.00 22.732 No\_date 28:40 50.08 n/a

01639# [ROUTE 5.00] cut<- 01\_SN\_M2 252.00 22.732 No\_date 28:40 50.08 n/a

01640# \*\*\*\*\*

01641# \* Catchment Jock River (north and south)

01642# \* Residential and some golf course

01643# \*\*\*\*\*

01644# 025:0059-----> ID:NHVD----> AREA---QPEAK-TpeakDate\_hh:mm---R.V.-R.C.-

01645# \* CONTINUOUS STANDHYDRO:CLARKE

01646# [ROUTE 5.00] cut<- 01\_SN\_M2 102.00 3.924 No\_date 28:20 30.12 .405

01647# [ROUTE 5.00] cut<- 01\_SN\_M2 102.00 3.924 No\_date 28:20 30.12 .405

01648# [ROUTE 5.00] cut<- 01\_SN\_M2 102.00 3.924 No\_date 28:20 30.12 .405

01649# [ROUTE 5.00] cut<- 01\_SN\_M2 102.00 3.924 No\_date 28:20 30.12 .405

01650# 025:0060-----> ID:NHVD----> AREA---QPEAK-TpeakDate\_hh:mm---R.V.-R.C.-

01651# ADD HYD

01652# \* [ROUTE 5.00] SUM 102.00 3.924 No\_date 28:20 30.12 .405

01653# + 04\_P1\_OVR 102.00 3.924 No\_date 28:20 30.12 .405

01654# [ROUTE 5.00] cut<- 01\_SN\_M2 102.00 3.924 No\_date 28:20 30.12 .405

01655# [ROUTE 5.00] cut<- 01\_SN\_M2 102.00 3.924 No\_date 28:20 30.12 .405

01656# [ROUTE 5.00] cut<- 01\_SN\_M2 102.00 3.924 No\_date 28:20 30.12 .405

01657# [ROUTE 5.00] cut<- 01\_SN\_M2 102.00 3.924 No\_date 28:20 30.12 .405

01658# [ROUTE 5.00] cut<- 01\_SN\_M2 102.00 3.924 No\_date 28:20 30.12 .405

01659# [ROUTE 5.00] cut<- 01\_SN\_M2 102.00 3.924 No\_date 28:20 30.12 .405

01660# \*\*\*\*\*

01661# \* END OF RUN 99

01662# \*\*\*\*\*

01663# RUN:COMMAND#

01664# START

01665# [METOUT= 2 .00 hrs on 0]

01666# [NSTORM= 1 ]

01667# [NODATA= 1 ]

01668# \*\*\*\*\*

01669# Date Project Name: Rock River Reach 1 Subwatershed Study|Project #: 160400414

01670# Date: October 2004

01671# Modeler : Navin Gautam/ Original by Ana M Paerez

01672# Compiler : Stacitec

01673# Version #: 1.82206

01674# \*\*\*\*\*

01675# READ STORM

01676# Filename = storm.001

01677# \*\*\*\*\*

01678# Comment = Pluie SCS de 24 heures pour Ottawa CDA

01679# [EDP=15.00:EDS= 24.00:PCT= 88.57]

01680# 100:0003-----> ID:NHVD----> AREA---QPEAK-TpeakDate\_hh:mm---R.V.-R.C.-

01681# MODIFY STORM

01682# [RPT= 0.00:TSR= 0.00:TFR= 86.00 mil]

01683# [EDP= 10.00:EDS= 40.00:PCT= 88.57]

01684# \*\*\*\*\*

01685# Parameters used in STANDHYD

01686# Norton's infiltration equation parameters:

01687# [LOGS= 2 :CIN 77.0]

01688# Parameters for PREVIOUS surfaces in STANDHYD

01689# [IAlmp= 4.67 mil] [LDP=40.00 m] [NMW=.250]

01690# Parameters for SURFACE surfaces in STANDHYD

01691# [IAlmp= 1.57 mil] [CLL= 1.5-] [PMT= .013]

01692# Parameters used in NASHYD

01693# [LOGS= 2 :CIN 77.0]

01694# ICADEdv = 1 (read and print data)

01695# Filetitle = C:\Navin\Octobe\1\CONTIN-1\SME\_POSTW\MODIFIED.VAL

01696# Parameters used in Ottawa Sewer Design Guideline

01697# Norton's infiltration equation parameters:

01698# [LOGS= 2 :CIN 77.0]

01699# Parameters for PREVIOUS surfaces in STANDHYD

01700# [IAlmp= 4.67 mil] [LDP=40.00 m] [NMW=.250]

01701# Parameters for SURFACE surfaces in STANDHYD

01702# Parameters used in NASHYD

01703# [LOGS= 2 :CIN 77.0]

01704# \*\*\*\*\*

01705# COMPUTE API

01706# [ROUTE 5.00] cut<- 01\_SN\_M2 102.00 3.924 No\_date 28:20 30.12 .405

01707# [ROUTE 5.00] cut<- 01\_SN\_M2 102.00 3.924 No\_date 28:20 30.12 .405

01708# \*\*\*\*\*

01709# \* JOCK RIVER REACH 1 SUBWATERSHED STUDY DISCRETIZED MODEL

01710# \* PROPOSED CONDITIONS DESIGN MODEL (SUMMER)

01711# \*\*\*\*\*

01712# Version: Draft Final Report, October 2006

01713# Revision History:

01714# \* Draft Final Report, November 2005

01715# \* Aspirations

01716# \* All developments are assumed to be developed except S-1, S-2, and SW-1a

01717# \* SNW facilities are modeled

01718# \* Rating curves were estimated based on existing reports and modeling for the proposed new sewer facility

01719# \* The rating curve for the existing Kennedy Burnett SNW Facility was obtained

01720# \* The Urban Runoff Treatment in the Kennedy Burnett Settling Pond (URTBSP) - R

01721# \* Manual for the Treatment of Stormwater, March 1983

01722# \* River routing modeled

01723# \* River cross sections obtained from RVCA's HEC-RAS hydraulic model

01724# \*\*\*\*\*

01725# Parameters

01726# Design Storm: 2.10, 25.30, 30.00, 33.30, 37.50, 41.80, 46.00, 50.00, 54.00, 58.00, 62.00, 66.00, 70.00, 74.00, 78.00, 82.00, 86.00, 90.00, 94.00, 98.00, 102.00, 106.00, 110.00, 114.00, 118.00, 122.00, 126.00, 130.00, 134.00, 138.00, 142.00, 146.00, 150.00, 154.00, 158.00, 162.00, 166.00, 170.00, 174.00, 178.00, 182.00, 186.00, 190.00, 194.00, 198.00, 202.00, 206.00, 210.00, 214.00, 218.00, 222.00, 226.00, 230.00, 234.00, 238.00, 242.00, 246.00, 250.00, 254.00, 258.00, 262.00, 266.00, 270.00, 274.00, 278.00, 282.00, 286.00, 290.00, 294.00, 298.00, 302.00, 306.00, 310.00, 314.00, 318.00, 322.00, 326.00, 330.00, 334.00, 338.00, 342.00, 346.00, 350.00, 354.00, 358.00, 362.00, 366.00, 370.00, 374.00, 378.00, 382.00, 386.00, 390.00, 394.00, 398.00, 402.00, 406.00, 410.00, 414.00, 418.00, 422.00, 426.00, 430.00, 434.00, 438.00, 442.00, 446.00, 450.00, 454.00, 458.00, 462.00, 466.00, 470.00, 474.00, 478.00, 482.00, 486.00, 490.00, 494.00, 498.00, 502.00, 506.00, 510.00, 514.00, 518.00, 522.00, 526.00, 530.00, 534.00, 538.00, 542.00, 546.00, 550.00, 554.00, 558.00, 562.00, 566.00, 570.00, 574.00, 578.00, 582.00, 586.00, 590.00, 594.00, 598.00, 602.00, 606.00, 610.00, 614.00, 618.00, 622.00, 626.00, 630.00, 634.00, 638.00, 642.00, 646.00, 650.00, 654.00, 658.00, 662.00, 666.00, 670.00, 674.00, 678.00, 682.00, 686.00, 690.00, 694.00, 698.00, 702.00, 706.00, 710.00, 714.00, 718.00, 722.00, 726.00, 730.00, 734.00, 738.00, 742.00, 746.00, 750.00, 754.00, 758.00, 762.00, 766.00, 770.00, 774.00, 778.00, 782.00, 786.00, 790.00, 794.00, 798.00, 802.00, 806.00, 810.00, 814.00, 818.00, 822.00, 826.00, 830.00, 834.00, 838.00, 842.00, 846.00, 850.00, 854.00, 858.00, 862.00, 866.00, 870.00, 874.00, 878.00, 882.00, 886.00, 890.00, 894.00, 898.00, 902.00, 906.00, 910.00, 914.00, 918.00, 922.00, 926.00, 930.00, 934.00, 938.00, 942.00, 946.00, 950.00, 954.00, 958.00, 962.00, 966.00, 970.00, 974.00, 978.00, 982.00, 986.00, 990.00, 994.00, 998.00, 1002.00, 1006.00, 1010.00, 1014.00, 1018.00, 1022.00, 1026.00, 1030.00, 1034.00, 1038.00, 1042.00, 1046.00, 1050.00, 1054.00, 1058.00, 1062.00, 1066.00, 1070.00, 1074.00, 1078.00, 1082.00, 1086.00, 1090.00, 1094.00, 1098.00, 1102.00, 1106.00, 1110.00, 1114.00, 1118.00, 1122.00, 1126.00, 1130.00, 1134.00, 1138.00, 1142.00, 1146.00, 1150.00, 1154.00, 1158.00, 1162.00, 1166.00, 1170.00, 1174.00, 1178.00, 1182.00, 1186.00, 1190.00, 1194.00, 1198.00, 1202.00, 1206.00, 1210.00, 1214.00, 1218.00, 1222.00, 1226.00, 1230.00, 1234.00, 1238.00, 1242.00, 1246.00, 1250.00, 1254.00, 1258.00, 1262.00, 1266.00, 1270.00, 1274.00, 1278.00, 1282.00, 1286.00, 1290.00, 1294.00, 1298.00, 1302.00, 1306.00, 1310.00, 1314.00, 1318.00, 1322.00, 1326.00, 1330.00, 1334.00, 1338.00, 1342.00, 1346.00, 1350.00, 1354.00, 1358.00, 1362.00, 1366.00, 1370.00, 1374.00, 1378.00, 1382.00, 1386.00, 1390.00, 1394.00, 1398.00, 1402.00, 1406.00, 1410.00, 1414.00, 1418.00, 1422.00, 1426.00, 1430.00, 1434.00, 1438.00, 1442.00, 1446.00, 1450.00, 1454.00, 1458.00, 1462.00, 1466.00, 1470.00, 1474.00, 1478.00, 1482.00, 1486.00, 1490.00, 1494.00, 1498.00, 1502.00, 15



# Attachment C

Model 3 – Jock River Reach One Update

JFSA, 2021

SWMHYMO Input & Summary files

```

1      20      Metric units / ID numbers OFF
2      *#*****SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
3      *#*****SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
4      *#*****SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
5      *# Project Name: [Jock River]      Project Number: [1474-16]
6      *# Date        : 04-03-2021
7      *# Modeler     : [M.M.]
8      *# Company     : JFSAinc.
9      *# License #   : 2549237
10     *#*****SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
11     *# CALIBRATION OF SUMMER MODEL PARAMETERS
12     *# USING CONTINUOUS SIMULATIONS
13     *# Rainfall data from JFSA raingauge installed at site + other gauges by the City
14     *# Use data collected from May 1st to July 14, 2003
15     *# 2020-11-30 change TMJSTO in COMPUTE DUALHYD (TMJSTO = 0.1 instead of 0.0001)
16     *# 2020-12-01 correct pond curve values
17     *# 2020-12-01 change W_CLAR_BRAZ XIMP to 0.55, SLPI=[0.5](%) (impervious slope), and
18     LGI up to 700m
19     *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 2462 (NHYDout=["N_TO"]
20     ,NHYDin=["SN_TO"]) from 0.033 % (as per Stantec Report 2007) to 0.05 % so the model
21     will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELS
22     aren't well suited to really flat slopes.
23     *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHYDout=["N_WC"]
24     ,NHYDin=["SN_CE"]) from 0.01 % (as per Stantec Report 2007) to 0.0255 % so the model
25     will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELS
26     aren't well suited to really flat slopes.
27     *
28     * Calibrated parameters for Summer 2003 data: APII=50, APIK=0.85, CN=varies,
29     *                                              SK=0.01, InterEventTime=12,
30     *                                              GWResk=0.96, VHydCond=0.055
31     *
32     *# -----
33     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
34     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
35     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
36     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
37     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
38     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
39     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
40     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
41     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
42     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
43     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
44     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
45     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
46     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
47     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
48     *#
49     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
50     *# of 1.32
51     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
52     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
53     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
54     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
55     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
56     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
57     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
58     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
59     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|

```

```

60          BaseFlowOption=[1] ,
61          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
62          VHydCond=[0.055](mm/hr), END=-1
63 *%-----+-----+
64 *#
65 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
66 *# of 1.32
67 *%-----+-----|
68 CONTINUOUS NASHYD      NHYD=[ "SW_13" ], DT=[1]min, AREA=[971](ha),
69          DWF=[0](cms), CN/C=[61], IA=[2.5](mm),
70          N=[3.0], TP=[3.76]hrs,
71          Continuous simulation parameters:
72          IaRECper=[4](hrs),
73          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
74          InterEventTime=[12](hrs)
75          Baseflow simulation parameters:
76          BaseFlowOption=[1] ,
77          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
78          VHydCond=[0.055](mm/hr), END=-1
79 *%-----+-----|
80 *#
81 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
82 *# of 1.80
83 *%-----+-----|
84 CONTINUOUS NASHYD      NHYD=[ "JR_GWM" ], DT=[1]min, AREA=[3074](ha),
85          DWF=[0](cms), CN/C=[55], IA=[2.5](mm),
86          N=[3], TP=[11.33]hrs,
87          Continuous simulation parameters:
88          IaRECper=[4](hrs),
89          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
90          InterEventTime=[12](hrs)
91          Baseflow simulation parameters:
92          BaseFlowOption=[1] ,
93          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
94          VHydCond=[0.055](mm/hr), END=-1
95 *%-----+-----|
96 CONTINUOUS NASHYD      NHYD=[ "JR_ASH" ], DT=[1]min, AREA=[1781](ha),
97          DWF=[0](cms), CN/C=[72], IA=[2.5](mm),
98          N=[3.0], TP=[3.91]hrs,
99          Continuous simulation parameters:
100         IaRECper=[4](hrs),
101         SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
102         InterEventTime=[12](hrs)
103         Baseflow simulation parameters:
104         BaseFlowOption=[1] ,
105         InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
106         VHydCond=[0.055](mm/hr), END=-1
107 *%-----+-----|
108 CONTINUOUS NASHYD      NHYD=[ "SW_11" ], DT=[1]min, AREA=[500](ha),
109          DWF=[0](cms), CN/C=[66], IA=[2.5](mm),
110          N=[3.0], TP=[1.24]hrs,
111          Continuous simulation parameters:
112          IaRECper=[4](hrs),
113          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
114          InterEventTime=[12](hrs)
115          Baseflow simulation parameters:
116          BaseFlowOption=[1] ,
117          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
118          VHydCond=[0.055](mm/hr), END=-1
119 *%-----+-----|
120 *#
121 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
122 *# of 1.80
123 *%-----+-----|
124 CONTINUOUS NASHYD      NHYD=[ "NN_CK" ], DT=[1]min, AREA=[1917](ha),
125          DWF=[0](cms), CN/C=[66], IA=[2.5](mm),

```

```

126      N=[3.0], TP=[5.29]hrs,
127      Continuous simulation parameters:
128      IaRECper=[4](hrs),
129      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
130      InterEventTime=[12](hrs)
131      Baseflow simulation parameters:
132      BaseFlowOption=[1] ,
133      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
134      VHydCond=[0.055](mm/hr), END=-1
135      *%-----|-----|
136      *#
137      *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
138      *# of 1.52
139      *%-----|-----|
140      CONTINUOUS NASHYD      NHYD=[ "SW_10" ], DT=[1]min, AREA=[5666](ha),
141      DWF=[0](cms), CN/C=[72], IA=[2.5](mm),
142      N=[3.0], TP=[8.00]hrs,
143      Continuous simulation parameters:
144      IaRECper=[4](hrs),
145      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
146      InterEventTime=[12](hrs)
147      Baseflow simulation parameters:
148      BaseFlowOption=[1] ,
149      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
150      VHydCond=[0.055](mm/hr), END=-1
151      *%-----|-----|
152      *#
153      *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
154      *# of 1.75
155      *%-----|-----|
156      CONTINUOUS NASHYD      NHYD=[ "KG_CK" ], DT=[1]min, AREA=[8376](ha),
157      DWF=[0](cms), CN/C=[66], IA=[2.5](mm),
158      N=[3.0], TP=[11.66]hrs,
159      Continuous simulation parameters:
160      IaRECper=[4](hrs),
161      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
162      InterEventTime=[12](hrs)
163      Baseflow simulation parameters:
164      BaseFlowOption=[1] ,
165      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
166      VHydCond=[0.055](mm/hr), END=-1
167      *%-----|-----|
168      *#
169      *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
170      *# of 1.68
171      *%-----|-----|
172      CONTINUOUS NASHYD      NHYD=[ "SW_9" ], DT=[1]min, AREA=[1132](ha),
173      DWF=[0](cms), CN/C=[70], IA=[2.5](mm),
174      N=[3.0], TP=[2.51]hrs,
175      Continuous simulation parameters:
176      IaRECper=[4](hrs),
177      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
178      InterEventTime=[12](hrs)
179      Baseflow simulation parameters:
180      BaseFlowOption=[1] ,
181      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
182      VHydCond=[0.055](mm/hr), END=-1
183      *%-----|-----|
184      *#
185      *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
186      *# of 1.82
187      *%-----|-----|
188      CONTINUOUS NASHYD      NHYD=[ "NC_CK" ], DT=[1]min, AREA=[4464](ha),
189      DWF=[0](cms), CN/C=[62], IA=[2.5](mm),
190      N=[3.0], TP=[11.32]hrs,
191      Continuous simulation parameters:

```

```

192
193     IaRECper=[4](hrs),
194     SMIN=[-1](mm),   SMAX=[-1](mm),  SK=[0.010]/(mm),
195     InterEventTime=[12](hrs)
196     Baseflow simulation parameters:
197     BaseFlowOption=[1] ,
198     InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
199     VHydCond=[0.055](mm/hr),    END=-1
200
201 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
202 *# of 1.80
203
204 CONTINUOUS NASHYD      NHYD=[ "SW_8" ], DT=[1]min, AREA=[131](ha),
205     DWF=[0](cms),  CN/C=[63],  IA=[2.5](mm),
206     N=[3.0],  TP=[0.90]hrs,
207     Continuous simulation parameters:
208     IaRECper=[4](hrs),
209     SMIN=[-1](mm),   SMAX=[-1](mm),  SK=[0.010]/(mm),
210     InterEventTime=[12](hrs)
211     Baseflow simulation parameters:
212     BaseFlowOption=[1] ,
213     InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
214     VHydCond=[0.055](mm/hr),    END=-1
215
216 *#
217 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
218 *# of 1.65
219
220 CONTINUOUS NASHYD      NHYD=[ "HB_DR" ], DT=[1]min, AREA=[3854](ha),
221     DWF=[0](cms),  CN/C=[66],  IA=[2.5](mm),
222     N=[3.0],  TP=[8.42]hrs,
223     Continuous simulation parameters:
224     IaRECper=[4](hrs),
225     SMIN=[-1](mm),   SMAX=[-1](mm),  SK=[0.010]/(mm),
226     InterEventTime=[12](hrs)
227     Baseflow simulation parameters:
228     BaseFlowOption=[1] ,
229     InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
230     VHydCond=[0.055](mm/hr),    END=-1
231
232 *#
233 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
234 *# of 1.82
235
236 CONTINUOUS NASHYD      NHYD=[ "SW_7" ], DT=[1]min, AREA=[3197](ha),
237     DWF=[0](cms),  CN/C=[57],  IA=[2.5](mm),
238     N=[3.0],  TP=[6.65]hrs,
239     Continuous simulation parameters:
240     IaRECper=[4](hrs),
241     SMIN=[-1](mm),   SMAX=[-1](mm),  SK=[0.010]/(mm),
242     InterEventTime=[12](hrs)
243     Baseflow simulation parameters:
244     BaseFlowOption=[1] ,
245     InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
246     VHydCond=[0.055](mm/hr),    END=-1
247
248 *#
249 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
250 *# of 1.75
251
252 CONTINUOUS NASHYD      NHYD=[ "SW_6" ], DT=[1]min, AREA=[165](ha),
253     DWF=[0](cms),  CN/C=[67],  IA=[2.5](mm),
254     N=[3.0],  TP=[4.18]hrs,
255     Continuous simulation parameters:
256     IaRECper=[4](hrs),
257     SMIN=[-1](mm),   SMAX=[-1](mm),  SK=[0.010]/(mm),

```

```

258
259
260
261
262
263 *%-----|-----|
264 *#
265 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
266 *# of 1.67
267 *%-----|-----|
268 CONTINUOUS NASHYD NHYD= ["VG_DR"], DT=[1]min, AREA=[1332](ha),
269 DWF=[0](cms), CN/C=[72], IA=[2.5](mm),
270 N=[3.0], TP=[5.95]hrs,
271 Continuous simulation parameters:
272 IaRECper=[4](hrs),
273 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
274 InterEventTime=[12](hrs)
275 Baseflow simulation parameters:
276 BaseFlowOption=[1],
277 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
278 VHydCond=[0.055](mm/hr), END=-1
279 *%-----|-----|
280 CONTINUOUS NASHYD NHYD= ["SW_5"], DT=[1]min, AREA=[224](ha),
281 DWF=[0](cms), CN/C=[77], IA=[2.5](mm),
282 N=[3.0], TP=[0.75]hrs,
283 Continuous simulation parameters:
284 IaRECper=[4](hrs),
285 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
286 InterEventTime=[12](hrs)
287 Baseflow simulation parameters:
288 BaseFlowOption=[1],
289 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
290 VHydCond=[0.055](mm/hr), END=-1
291 *%-----|-----|
292 *#
293 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
294 *# of 1.20
295 *%-----|-----|
296 CONTINUOUS NASHYD NHYD= ["FL_CK"], DT=[1]min, AREA=[4945](ha),
297 DWF=[0](cms), CN/C=[74], IA=[2.5](mm),
298 N=[3.0], TP=[4.45]hrs,
299 Continuous simulation parameters:
300 IaRECper=[4](hrs),
301 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
302 InterEventTime=[12](hrs)
303 Baseflow simulation parameters:
304 BaseFlowOption=[1],
305 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
306 VHydCond=[0.055](mm/hr), END=-1
307 *%-----|-----|
308 CONTINUOUS NASHYD NHYD= ["SW_5A2"], DT=[1]min, AREA=[20](ha),
309 DWF=[0](cms), CN/C=[81], IA=[2.5](mm),
310 N=[3.0], TP=[0.62]hrs,
311 Continuous simulation parameters:
312 IaRECper=[4](hrs),
313 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
314 InterEventTime=[12](hrs)
315 Baseflow simulation parameters:
316 BaseFlowOption=[1],
317 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
318 VHydCond=[0.055](mm/hr), END=-1
319 *%-----|-----|
320 *#
321 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
322 *# of 1.61
323 *%-----|-----|

```

```

324 CONTINUOUS NASHYD NHYD=[ "SW_5A1" ], DT=[1]min, AREA=[1412](ha),
325 DWF=[0](cms), CN/C=[75], IA=[2.5](mm),
326 N=[3.0], TP=[8.00]hrs,
327 Continuous simulation parameters:
328 IaRECper=[4](hrs),
329 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
330 InterEventTime=[12](hrs)
331 Baseflow simulation parameters:
332 BaseFlowOption=[1],
333 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
334 VHydCond=[0.055](mm/hr), END=-1
335 *%
336 CONTINUOUS NASHYD NHYD=[ "SW_4" ], DT=[1]min, AREA=[585](ha),
337 DWF=[0](cms), CN/C=[81], IA=[2.5](mm),
338 N=[3.0], TP=[1.75]hrs,
339 Continuous simulation parameters:
340 IaRECper=[4](hrs),
341 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
342 InterEventTime=[12](hrs)
343 Baseflow simulation parameters:
344 BaseFlowOption=[1],
345 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
346 VHydCond=[0.055](mm/hr), END=-1
347 *%
348 CONTINUOUS NASHYD NHYD=[ "LM_CK" ], DT=[1]min, AREA=[1021](ha),
349 DWF=[0](cms), CN/C=[80], IA=[2.5](mm),
350 N=[3.0], TP=[2.46]hrs,
351 Continuous simulation parameters:
352 IaRECper=[4](hrs),
353 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
354 InterEventTime=[12](hrs)
355 Baseflow simulation parameters:
356 BaseFlowOption=[1],
357 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
358 VHydCond=[0.055](mm/hr), END=-1
359 *%
360 CONTINUOUS NASHYD NHYD=[ "SW_2" ], DT=[1]min, AREA=[177](ha),
361 DWF=[0](cms), CN/C=[77], IA=[2.5](mm),
362 N=[3.0], TP=[0.75]hrs,
363 Continuous simulation parameters:
364 IaRECper=[4](hrs),
365 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
366 InterEventTime=[12](hrs)
367 Baseflow simulation parameters:
368 BaseFlowOption=[1],
369 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
370 VHydCond=[0.055](mm/hr), END=-1
371 *%
372 CONTINUOUS NASHYD NHYD=[ "SM_DR" ], DT=[1]min, AREA=[1122](ha),
373 DWF=[0](cms), CN/C=[81], IA=[2.5](mm),
374 N=[3.0], TP=[3.25]hrs,
375 Continuous simulation parameters:
376 IaRECper=[4](hrs),
377 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
378 InterEventTime=[12](hrs)
379 Baseflow simulation parameters:
380 BaseFlowOption=[1],
381 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
382 VHydCond=[0.055](mm/hr), END=-1
383 *%
384 CONTINUOUS NASHYD NHYD=[ "MO_DR" ], DT=[1]min, AREA=[2737](ha),
385 DWF=[0](cms), CN/C=[76], IA=[2.5](mm),
386 N=[3.0], TP=[3.03]hrs,
387 Continuous simulation parameters:
388 IaRECper=[4](hrs),
389 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),

```

```

390
391     InterEventTime=[12](hrs)
392     Baseflow simulation parameters:
393     BaseFlowOption=[1] ,
394     InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
395     VHydCond=[0.055](mm/hr), END=-1
396 *%-----|-----
397 *      -JFSA 2020 replaced SW_1 with a detailed model from Stantec Report 2007
398 *CONTINUOUS NASHYD   NHYD=[ "SW_1"], DT=[1]min, AREA=[3176](ha),
399 *          DWF=[0](cms), CN/C=[78], IA=[2.5](mm),
400 *          N=[3.0], TP=[3.56]hrs,
401 *          Continuous simulation parameters:
402 *          IaRECper=[4](hrs),
403 *          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
404 *          InterEventTime=[12](hrs)
405 *          Baseflow simulation parameters:
406 *          BaseFlowOption=[1] ,
407 *          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
408 *          VHydCond=[0.055](mm/hr), END=-1
409 *%-----|-----
410 *#
411 *# Routing hydrographs
412 *# Starting with the addition of Jock River Headwater and Subwatershed 13
413 *#
414 ADD HYD           NHYDsum=[ "S_N13"], NHYDs to add=[ "JR_HW"+"SW_13"]
415 *%-----|-----
416 *#
417 *# Sum of hydrographs from Node 13 routed to Node 13A
418 *# (Approximated cross-section - see cross-section 258)
419 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
420 *#
421 ROUTE CHANNEL      NHYDout=[ "N13A"] ,NHYDin=[ "S_N13"],
422             RDT=[1](min),
423             CHLGTH=[ 9074](m), CHSLOPE=[0.0220](%), FPSLOPE=[0.0220](%),
424             SECNUM=[1.0], NSEG=[1]
425             ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
426             ( DISTANCE (m), ELEVATION (m))=
427                 [-40, 132.5]
428                 [-30, 132]
429                 [-25, 131.5]
430                 [-13, 130]
431                 [-8, 127.00]
432                 [-7, 126.50]
433                 [-6, 126]
434                 [-5.5, 125.50]
435                 [0, 123.75]
436                 [4.5, 125.50]
437                 [6, 126]
438                 [7.5, 126.5]
439                 [9, 127]
440                 [10, 127.5]
441                 [11.5, 128.0]
442                 [15.5, 129.5]
443
444 *%-----|-----
445 *#
446 *# Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
447 *#
448 ADD HYD           NHYDsum=[ "SN13A"], NHYDs to add=[ "N13A"+"JR_GWM"]
449 *%-----|-----
450 *#
451 *# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
452 *#
453 ROUTE RESERVOIR    NHYDout=[ "RES_GM"] ,NHYDin=[ "SN13A"],
454             RDT=[1](min),
455             TABLE of ( OUTFLOW-STORAGE ) values

```

```

456          (cms) - (ha-m)
457          [ 0.0 , 0.0 ]
458          [1.991, 2.144 ]
459          [2.693, 39.826 ]
460          [3.509, 81.697 ]
461          [4.578, 318.774 ]
462          [5.647, 594.947 ]
463          [7.109, 910.219 ]
464          [8.616, 1264.589 ]
465          [10.371, 1658.057 ]
466          [12.402, 2090.622 ]
467          [22.056, 3462.487 ]
468          [ -1 , -1 ] (max twenty pts)
469      NHYDovf=[ " " ] ,
470 *%-----|-----|
471 *#
472 SAVE HYD          NHYD=[ "RES_GM" ], # OF PCYCLES=[-1], ICASEsh=[-1]
473          HYD_FILENAME=[ "H_ESGM" ]
474          HYD_COMMENT=[ "Outflow from Res GM" ]
475 *%-----|-----|
476 *# Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
477 *# (Approximated cross-section - see cross-section 258)
478 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
479 ROUTE CHANNEL      NHYDout=[ "N12" ] ,NHYDin=[ "RES_GM" ] ,
480          RDT=[1](min),
481          CHLGTH=[5926](m), CHSLOPE=[0.0759](%), FPSLOPE=[0.0759](%),
482          SECNUM=[1.0], NSEG=[1]
483          ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
484          ( DISTANCE (m), ELEVATION (m))=
485          [-40, 132.5]
486          [-30, 132]
487          [-25, 131.5]
488          [-13, 130]
489          [-8, 127.00]
490          [-7, 126.50]
491          [-6, 126]
492          [-5.5, 125.50]
493          [0, 123.75]
494          [4.5, 125.50]
495          [6, 126]
496          [7.5, 126.5]
497          [9, 127]
498          [10, 127.5]
499          [11.5, 128.00]
500          [15.5, 129.5]
501
502 *%-----|-----|
503 *#
504 *# Addition of Subwatershed Jock River at Ashton to Node 12
505 *#
506 ADD HYD          NHYDsum=[ "S_N12" ], NHYDs to add=[ "N12"+"JR_ASH" ]
507 SAVE HYD          NHYD=[ "S_N12" ], # OF PCYCLES=[-1], ICASEsh=[-1]
508          HYD_FILENAME=[ "H_SN12" ]
509          HYD_COMMENT=[ "flow at S_N12 near Ashton" ]
510 *%-----|-----|
511 *#
512 *# Sum of hydrographs from Node 12 routed to Node 11
513 *# (Approximated cross-section - see cross-section 258)
514 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
515 *ROUTE CHANNEL      NHYDout=[ "N11" ] ,NHYDin=[ "S_N12" ] ,
516          *
517          RDT=[1](min),
518          *
519          CHLGTH=[972](m), CHSLOPE=[0.0514](%), FPSLOPE=[0.0514](%),
520          *
521          SECNUM=[1.0], NSEG=[1]
522          ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
523          ( DISTANCE (m), ELEVATION (m))=

```

```

522 * [-40, 132.5]
523 * [-30, 132]
524 * [-25, 131.5]
525 * [-13, 130]
526 * [-8, 127.00]
527 * [-7, 126.50]
528 * [-6, 126]
529 * [-5.5, 125.50]
530 * [0, 123.75]
531 * [4.5, 125.50]
532 * [6, 126]
533 * [7.5, 126.5]
534 * [9, 127]
535 * [10, 127.5]
536 * [11.5, 128.00]
537 * [15.5, 129.5]
538 *%-----|-----|-----|
539 *#
540 *# Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
541 *#
542 ROUTE CHANNEL      NHYDout=[ "Dum11" ] ,NHYDin=[ "S_N12" ] ,
543 RDT=[1](min),
544 CHLGTH=[972](m),   CHSLOPE=[0.054](%),
545                                     FPSLOPE=[0.054](%),
546 SECNUM=[1.0],       NSEG=[1]
547 ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
548 ( DISTANCE (m), ELEVATION (m))=
549          [-40, 132.5]
550          [-30, 132]
551          [-25, 131.5]
552          [-13, 130]
553          [-8, 127.00]
554          [-7, 126.50]
555          [-6, 126]
556          [-5.5, 125.50]
557          [0, 123.75]
558          [4.5, 125.50]
559          [6, 126]
560          [7.5, 126.5]
561          [9, 127]
562          [10, 127.5]
563          [11.5, 128.00]
564          [15.5, 129.5]
565 *%-----|-----|-----|
566 *#
567 *# Addition of Subwatershed 11 and No Name Creek to Node 11
568 *#
569 ADD HYD           NHYDsum= [ "S_N11" ], NHYDs to add=[ "Dum11"+ "SW_11" + "NN_CK" ]
570 *%-----|-----|-----|
571 *#
572 *# Sum of hydrographs from Node 11 routed to Node 10
573 *# Section 1
574 *#
575 ROUTE CHANNEL      NHYDout=[ "N10" ] ,NHYDin=[ "S_N11" ] ,
576 RDT=[1](min),
577 CHLGTH=[14028](m),   CHSLOPE=[0.1568](%),
578                                     FPSLOPE=[0.1568](%),
579 SECNUM=[1.0],       NSEG=[5]
580 ( SEGROUGH, SEGDIST (m))=
581          [0.04,-52.82
582          0.1,-6.47
583          -0.05,6.47
584          0.1,45.36
585          0.04,423.88] NSEG times
586 ( DISTANCE (m), ELEVATION (m))=
587          [-226.24 ,112.50]

```

```

588 [-167.50 ,111.50]
589 [-106.81 ,111.00]
590 [-92.37 ,110.00]
591 [-52.82 ,109.00]
592 [-24.90, 109.00]
593 [-17.02, 108.50]
594 [-6.47, 108.00]
595 [6.47, 108.00]
596 [15.67, 108.50]
597 [18.95, 109.00]
598 [45.36, 109.50]
599 [120.79, 110.00]
600 [145.72, 111.00]
601 [181.56, 111.50]
602 [423.88, 112.50]

603 *%-----|-----|
604 *#
605 *# Addition of Subwatershed 10 to Node 10
606 *#
607 ADD HYD      NHYDsum=[ "S_N10" ], NHYDs to add=[ "N10"+"SW_10" ]
608 *%-----|-----|
609 SAVE HYD      NHYD=[ "S_N10" ], # OF PCYCLES=[ -1 ], ICASEsh=[ -1 ]
610          HYD_FILENAME=[ "H_SN10" ]
611          HYD_COMMENT=[ "flow at S_N10: N10 + SW_10" ]
612 *%-----|-----|
613 *# Addition of Kings Creek to S_N10
614 *#
615 ADD HYD      NHYDsum=[ "S_N10A" ], NHYDs to add=[ "S_N10"+"KG_CK" ]
616 *%-----|-----|
617 *#
618 *# Sum of hydrographs from Node 10 routed to Node 9
619 *# Section 2
620 *#
621 ROUTE CHANNEL      NHYDout=[ "N9" ] ,NHYDin=[ "S_N10A" ] ,
622          RDT=[ 1 ](min),
623          CHLGTH=[ 3982 ](m), CHSLOPE=[ 0.0753 ](%),
624          FPSLOPE=[ 0.0753 ](%),
625          SECNUM=[ 1.0 ], NSEG=[ 4 ]
626          ( SEGROUGH, SEGDIST (m))=
627          [ 0.04,-30.27
628          0.05,-18.42
629          -0.05,18.42
630          0.04,131.58] NSEG times
631          ( DISTANCE (m), ELEVATION (m))=
632          [-446.74, 106.00]
633          [-415.68, 105.50]
634          [-285.40, 105.00]
635          [-173.77, 104.50]
636          [-144.95, 104.00]
637          [-111.18, 103.50]
638          [-94.06, 103.00]
639          [-71.02, 102.50]
640          [-30.27, 102.00]
641          [-19.33, 100.00]
642          [-18.42, 99.50]
643          [18.42, 99.50]
644          [20.77, 100.00]
645          [27.93, 101.00]
646          [52.29, 101.00]
647          [68.80, 101.50]
648          [79.66, 103.00]
649          [91.50, 103.50]
650          [131.58, 104.00]

651 *%-----|-----|
652 *#
653 *# Addition of Subwatershed 9 and Nichols Creek to Node 9

```

```

654 *#
655 ADD HYD NHYDsum=[ "S_N9" ] , NHYDs to add=[ "N9 "+"SW_9 "+"NC_CK" ]
656 *%-----|-----|
657 *#
658 *# Sum of hydrographs from Node 9 routed to Node 8
659 *# Section 3
660 *#
661 ROUTE CHANNEL NHYDout=[ "N8" ] , NHYDin=[ "S_N9" ] ,
662 RDT=[1](min),
663 CHLGTH=[2269](m), CHSLOPE=[0.0882](%),
664 FPSLOPE=[0.0882](%),
665 SECNUM=[1.0], NSEG=[3]
666 ( SEGROUGH, SEGDIST (m))=
667 [0.1,-17.99
668 -0.045,17.31
669 0.1,456.58] NSEG times
670 ( DISTANCE (m), ELEVATION (m))=
671 [-201.19,100.50]
672 [-135.21, 100.00]
673 [-94.83, 99.50]
674 [-67.05, 99.00]
675 [-17.99, 98.50]
676 [-16.02, 98.00]
677 [-13.95, 97.50]
678 [13.95, 97.50]
679 [15.64, 98.00]
680 [17.31, 98.50]
681 [162.02, 98.50]
682 [172.89 ,99.00]
683 [314.38, 99.00]
684 [343.78, 99.50]
685 [365.67, 100.00]
686 [376.68, 100.00 ]
687 [393.11, 99.50]
688 [404.97, 99.50]
689 [431.70, 100.00]
690 [456.58, 100.50 ]
691 *%-----|-----|
692 *#
693 *# Addition of Subwatershed 8 and Hobb's Drain to Node 8
694 *#
695 ADD HYD NHYDsum=[ "S_N8" ] , NHYDs to add=[ "N8 "+"SW_8 "+"HB_DR" ]
696 *%-----|-----|
697 *#
698 *# Sum of hydrographs from Node 8 routed to Node 7
699 *# Section 4
700 *#
701 ROUTE CHANNEL NHYDout=[ "N7" ] , NHYDin=[ "S_N8" ],
702 RDT=[1](min),
703 CHLGTH=[3750](m), CHSLOPE=[0.0533](%),
704 FPSLOPE=[0.0533](%),
705 SECNUM=[1.0], NSEG=[3]
706 ( SEGROUGH, SEGDIST (m))=
707 [0.12,-18.11
708 -0.07,17.22
709 0.12,590.05] NSEG times
710 ( DISTANCE (m), ELEVATION (m))=
711 [-433.21, 102.00]
712 [-425.34, 101.50]
713 [-377.56, 101.50]
714 [-366.23, 101.00]
715 [-202.60, 100.50]
716 [-96.25, 99.50]
717 [-68.36 99.00]
718 [-18.11, 98.50]
719 [-13.81, 97.50]

```

```

720 [13.81, 97.50]
721 [17.22, 98.50]
722 [161.95, 98.50]
723 [173.11, 99.00]
724 [314.05, 99.00]
725 [365.52, 100.00]
726 [404.70, 99.50]
727 [476.74, 100.50]
728 [502.31, 101.00]
729 [584.69, 101.00]
730 [585.79, 101.00]
731 [590.05, 102.00]

732 *%-----|-----|
733 *#
734 *# Addition of Subwatershed 7 to Node 7
735 *#
736 ADD HYD      NHYDsum= [ "S_N7" ] , NHYDs to add= [ "N7" + "SW_7" ]
737 *%-----|-----|
738 SAVE HYD      NHYD= [ "S_N7" ] , # OF PCYCLES= [ -1 ] , ICASEsh= [ -1 ]
739          HYD_FILENAME= [ "H_SN7" ]
740          HYD_COMMENT= [ "flow at S_N7: N7 + SW_7" ]
741 *%-----|-----|
742 *# Insertion of a reservoir to simulate the effects of the Richmond Fen.
743 *# Storage area and volumes were estimated from available topo maps.
744 *# Release rate from fen was assumed to be controlled by the downstream
745 *# river cross-section for summer conditions. It is was assumed that for up to
746 *# 0.75 m of water, the main channel of the river provided the storage. Above
747 *# this depth, the wetland starts to signigicantly store water.
748 *#
749 ROUTE RESERVOIR   NHYDout= [ "RES_RF" ] , NHYDin= [ "S_N7" ] ,
750          RDT= [ 1 ] (min),
751          TABLE of ( OUTFLOW-STORAGE ) values
752          (cms) - (ha-m)
753          TABLE of ( OUTFLOW-STORAGE ) values
754          (cms) - (ha-m)
755          [ 0.0 , 0.0 ]
756          [ 0.9051 , 2.40 ]
757          [ 2.907 , 4.13 ]
758          [ 9.744 , 9.18 ]
759          [ 20.304 , 14.96 ]
760          [ 34.167 , 310.21 ]
761          [ 74.993 , 605.46 ]
762          [ 104.876 , 900.71 ]
763          [ 140.56 , 2892.00 ]
764          [ 225.00 , 3615.63 ]
765          [ -1 , -1 ] (max twenty pts)
766          NHYDovf= [ " " ] ,
767 *%-----|-----|
768 SAVE HYD      NHYD= [ "RES_RF" ] , # OF PCYCLES= [ -1 ] , ICASEsh= [ -1 ]
769          HYD_FILENAME= [ "H_ResRF" ]
770          HYD_COMMENT= [ "outflow of Richmond Fen" ]
771 *%-----|-----|
772 *#
773 *# Sum of hydrographs from Node 7 routed to Node 6
774 *# Section 5
775 *#
776 ROUTE CHANNEL    NHYDout= [ "N6" ] , NHYDin= [ "RES_RF" ] ,
777          RDT= [ 1 ] (min),
778          CHLGTH= [ 3056 ] (m) , CHSLOPE= [ 0.0818 ] ( % ) ,
779          FPSLOPE= [ 0.0818 ] ( % ) ,
780          SECNUM= [ 1.0 ] , NSEG= [ 5 ]
781          ( SEGROUGH , SEGDIST (m) )=
782          [ 0.025 , -70.8
783          0.1 , -23.9
784          -0.05 , 23.9
785          0.06 , 39.8

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```

786          0.05,96.3] NSEG times
787  ( DISTANCE (m), ELEVATION (m))=
788          [-100.8, 97.00]
789          [-70.8, 96.50]
790          [-52.0, 96.00]
791          [-35.1, 95.50]
792          [-30.6, 95.00]
793          [-23.9, 94.54]
794          [23.9, 94.54]
795          [39.8, 95.00]
796          [50.4, 95.50]
797          [93.5, 96.00]
798          [94.9, 96.50]
799          [96.3, 97.00]
800 *%-----|-----|
801 *#
802 *# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
803 *#
804 ADD HYD      NHYDsum=[ "S_N6" ] , NHYDs to add=[ "N6"+"SW_6"+"VG_DR" ]
805 *%-----|-----|
806 *#
807 *# Sum of hydrographs from Node 6 routed to Node 5
808 *# Section 6
809 *#
810 ROUTE CHANNEL      NHYDout=[ "N5" ] ,NHYDin=[ "S_N6" ] ,
811          RDT=[1](min),
812          CHLGTH=[1852](m),   CHSLOPE=[0.0540](%),
813          FPSLOPE=[0.0540](%),
814          SECNUM=[1.0],       NSEG=[3]
815          ( SEGROUGH, SEGDIST (m))=
816          [0.035,-131.59
817          -0.045,48.96
818          0.1,239.04] NSEG times
819          ( DISTANCE (m), ELEVATION (m))=
820          [-686.30, 94.50]
821          [-675.70, 94.00]
822          [-492.52, 93.00]
823          [-467.28, 94.00]
824          [-131.59, 94.00]
825          [-92.79, 92.50]
826          [-18.06, 91.00]
827          [18.06, 91.00]
828          [43.47, 92.50]
829          [48.96, 94.00]
830          [177.43, 94.00]
831          [239.04,94.50]
832 *%-----|-----|
833 *#
834 *# Addition of Subwatershed 5 and Flowing Creek to Node 5
835 *#
836 ADD HYD      NHYDsum=[ "S_N5" ] , NHYDs to add=[ "N5"+"SW_5"+"FL_CK" ]
837 *%-----|-----|
838 *#
839 *# Sum of hydrographs from Node 5 routed to Node 5A
840 *# Section 7
841 *#
842 ROUTE CHANNEL      NHYDout=[ "N5A" ] ,NHYDin=[ "S_N5" ] ,
843          RDT=[1](min),
844          CHLGTH=[556](m),   CHSLOPE=[0.0900](%),
845          FPSLOPE=[0.0900](%),
846          SECNUM=[1.0],       NSEG=[4]
847          ( SEGROUGH, SEGDIST (m))=
848          [0.04,-41.5
849          0.1,-14.0
850          -0.045,14.0
851          0.1,41.1] NSEG times

```

```

852          ( DISTANCE (m) , ELEVATION (m))=
853                      [-275.8, 93.00]
854                      [-248.6, 92.50]
855                      [-237.0, 92.00]
856                      [-219.3, 91.50]
857                      [-202.1, 91.50]
858                      [-186.0, 92.00]
859                      [-129.2, 92.00]
860                      [-117.6, 91.50]
861                      [-100.6, 91.00]
862                      [-41.5, 91.00]
863                      [-20.0, 91.00]
864                      [-14.0, 90.54]
865                      [14.0, 90.54]
866                      [15.3, 91.00]
867                      [17.3, 91.50]
868                      [38.4, 92.00]
869                      [39.8, 92.50]
870                      [41.1, 93.00]
871 *%-----|-----|
872 *#
873 *# Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
874 *#
875 ADD HYD           NHYDsum=[ "S_N5A" ] , NHYDs to add=[ "N5A"+"SW_5A2"+"SW_5A1" ]
876 *%-----|-----|
877 *#
878 *# Sum of hydrographs from Node 5A routed to Node 4
879 *# Section 8
880 *#
881 ROUTE CHANNEL      NHYDout=[ "N4" ] , NHYDin=[ "S_N5A" ] ,
882             RDT=[1](min),
883             CHLGTH=[4630](m),   CHSLOPE=[0.0432](%),
884                               FPSLOPE=[0.0432](%),
885             SECNUM=[1.0],        NSEG=[3]
886             ( SEGRROUGH, SEGDIST (m))=
887                 [0.05,-28.2
888                 -0.035,28.2
889                 0.05,173.1] NSEG times
890             ( DISTANCE (m) , ELEVATION (m))=
891                         [-38.9, 92.00]
892                         [-35.8, 91.50]
893                         [-33.3, 91.00]
894                         [-28.2, 90.50]
895                         [-15.0, 87.48]
896                         [-5.0, 88.34]
897                         [5.0, 86.20]
898                         [15.0, 88.55]
899                         [28.2, 90.50]
900                         [29.7, 91.00]
901                         [46.5, 91.00]
902                         [127.8, 91.00]
903                         [148.7, 91.50]
904                         [173.1, 92.00]
905 *%-----|-----|
906 *#
907 *# Addition of Subwatershed 4 and Leamy Creek to Node 4
908 *#
909 ADD HYD           NHYDsum=[ "S_N4" ] , NHYDs to add=[ "N4"+"SW_4"+"LM_CK" ]
910 SAVE HYD          NHYD=[ "S_N4" ] , # OF PCYCLES=[-1], ICASEsh=[1]
911             HYD_COMMENT=[ "flow at S_N4" ]
912 *%-----|-----|
913 *#
914 *# Sum of hydrographs from Node 4 routed to Node 2
915 *# Section 9
916 *#
917 ROUTE CHANNEL      NHYDout=[ "N2" ] , NHYDin=[ "S_N4" ] ,

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918 RDT=[1](min),
919 CHLGTH=[1667](m), CHSLOPE=[0.0600](%),
920                                     FPSLOPE=[0.0600](%),
921 SECNUM=[1.0], NSEG=[4]
922 ( SEGROUGH, SEGDIST (m))=
923     [0.1,-28.0
924     -0.04,28.4
925     0.06,31.7
926     0.04,80.2] NSEG times
927 ( DISTANCE (m), ELEVATION (m))=
928     [-36.3, 92.00]
929     [-32.6, 91.50]
930     [-30.2, 91.00]
931     [-28.0, 90.45]
932     [-15.0, 87.48]
933     [-5.0, 88.34]
934     [5.0, 86.20]
935     [15.0, 88.55]
936     [28.0, 90.45]
937     [28.4, 90.50]
938     [30.4, 91.00]
939     [31.7, 91.50]
940     [80.2, 92.00]
941 *%-----|-----|
942 *#
943 *# Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2
944 *#
945 ADD HYD          NHYDsum= [ "S_N2" ], NHYDs to add= [ "N2"+ "SW_2"+ "SM_DR"+ "MO_DR" ]
946 *%-----|-----|
947 SAVE HYD          NHYD= [ "S_N2" ], # OF PCYCLES=[-1], ICASEsh=[-1]
948          HYD_FILENAME=[ "H_SN2" ]
949          HYD_COMMENT=[ "flow at S_N2 Jock River Gauge at Moodie Dr." ]
950 *%-----|-----|
951 *#
952 *# Sum of hydrographs from Node 2 routed to Node 1
953 *# Section 10
954 *#
955 *#***** ****
956 *%READ HYD          NHYD= [ "S_N2" ],
957 *%          HYD_FILENAME=[ "H-S_N2" ]
958 *%-----|-----|
959 *#
960 *# Hydrograph from Node 2 routed to Node 416
961 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 9025
962 *#
963 ROUTE CHANNEL      NHYDout=[ "N_416" ] , NHYDin=[ "S_N2" ] ,
964          RDT=[1](min),
965          CHLGTH=[2327](m), CHSLOPE=[0.0498](%),
966                                     FPSLOPE=[0.0498](%),
967          SECNUM=[1.0], NSEG=[3]
968 ( SEGROUGH, SEGDIST (m))=
969     [0.075,-23.96
970     -0.055,23.96
971     0.075,157.38] NSEG times
972 ( DISTANCE (m), ELEVATION (m))=
973     [-336.97,93.5]
974     [-318.85,93]
975     [-259,92.5]
976     [-133.18,92]
977     [-33.17,92]
978     [-27.21,92]
979     [-26.14,91.5]
980     [-24.99,91]
981     [-23.96,90.5]
982     [-14.33,88.26]
983     [-0.68,88.12]

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984 [14.33,88.26]
985 [23.96,90.5]
986 [32.12,91]
987 [43.74,91.5]
988 [57.09,92]
989 [73.53,92.5]
990 [108.27,93]
991 [125.88,93.5]
992 [144.81,94]
993 [157.38,94.5]
994 *%-----|-----|
995 *#***** Catchment SW-1a
996 *# - Portion of RVCA catchment SW_1 outside of Reach 1 subwatershed
997 *# - Undeveloped agricultural land
998 *#***** -----
999
1000 CONTINUOUS NASHYD NHYD=[ "SW_1a" ], DT=[1]min, AREA=[ 536.42 ](ha),
1001 DWF=[ 0 ](cms), CN/C=[ 72 ], IA=[ 4.67 ](mm),
1002 N=[ 3 ], TP=[ 2.79 ]hrs,
1003 Continuous simulation parameters:
1004 IaRECper=[ 4 ](hrs),
1005 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1006 InterEventTime=[ 12 ](hrs)
1007 Baseflow simulation parameters:
1008 BaseFlowOption=[ 1 ],
1009 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
1010 VHdCond=[ 0.055 ](mm/hr), END=-1
1011 *%-----|-----|
1012 * -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
before station 7245 on Jock River
1013 *CONTINUOUS STANDHYD NHYD=[ "S-1-Okeefe" ], DT=[1](min), AREA=[ 44.93 ](ha), XIMP=[ 0.65 ],
1014 TIMP=[ 0.65 ], DWF=[ 0 ](cms),
1015 * LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
1016 IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%),
1017 * LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min), Impervious surfaces:
1018 IAimp=[ 1.57 ](mm), SLPI=[ 0.75 ](%),
1019 * LGI=[ 547.296 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1020 * Continuous simulation parameters:
1021 * IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
1022 * SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1023 * InterEventTime=[ 12 ](hrs), END=-1
1024 *%-----|-----|
1025 CONTINUOUS NASHYD NHYD=[ "S-1-Okeefe" ], DT=[1]min, AREA=[ 44.93 ](ha),
1026 DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
1027 N=[ 3 ], TP=[ 1.049 ]hrs,
1028 Continuous simulation parameters:
1029 IaRECper=[ 4 ](hrs),
1030 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1031 InterEventTime=[ 12 ](hrs)
1032 Baseflow simulation parameters:
1033 BaseFlowOption=[ 1 ],
1034 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
1035 VHdCond=[ 0.055 ](mm/hr), END=-1
1036 *%-----|-----|
1037 *COMPUTE DUALHYD NHYDin=[ "S-1-Okeefe" ], CINLET=[ 4.796 ](cms), NINLET=[ 1 ],
1038 * MajNHYD=[ "S-1-OkMJ" ]
1039 * MinNHYD=[ "S-1-OkMN" ]
1040 * TMJSTO=[ 99999999 ](cu-m)
1041 *%-----|-----|
1042 *ADD HYD NHYDsum=[ "S-1-Oks" ], NHYDs to add=[ "S-1-OkMJ"+ "S-1-OkMN" ]
1043 *%-----|-----|
1044 *ROUTE RESERVOIR NHYDout=[ "S-1-OkSR" ], NHYDin=[ "S-1-Oks" ],
1045 * RDT=[ 1 ](min),
* TABLE of ( OUTFLOW-STORAGE ) values
* (cms) - (ha-m)
* [ 0.0 , 0.0 ]

```

```

1046 * [ 0.5370, 1.7917 ]
1047 *
1048 * [ -1 , -1 ] (max twenty pts)
1049 * NYDovf= [ "S-1-OkSovf" ]
1050 ADD HYD NYDsSum= [ "SN_416" ], NYDs to add= [ "N_416"+ "SW_1a"+ "S-1-Okeefe" ]
1051 SAVE HYD NYHYD= [ "SN_416" ], # OF PCYCLES=[-1], ICASEsh=[1]
1052 HYD_COMMENT= [ "Total Flows at Highway 416" ]
1053
1054
1055 *
1056 *# Hydrograph from Node 416 routed to Node at Okeefe drain
1057 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 7245
1058 *
1059 ROUTE CHANNEL NYDout= [ "N_OK" ] , NYDin= [ "SN_416" ] ,
1060 RDT=[1](min),
1061 CHLGTH=[497](m), CHSLOPE=[0.3018](%),
1062 FPSLOPE=[0.3018](%),
1063 SECNUM=[1.0], NSEG=[3]
1064 ( SEGROUGH, SEGDIST (m))=
1065 [0.075,-19.40
1066 -0.055,19.40
1067 0.075,377.02] NSEG times
1068 ( DISTANCE (m), ELEVATION (m))=
1069 [-1061.41, 92.50]
1070 [-945.91, 92.00]
1071 [-783.64, 91.50]
1072 [-136.74, 91.00]
1073 [-86.04, 91.00]
1074 [-20.86, 91.00]
1075 [-20.18, 90.50]
1076 [-19.40, 90.00]
1077 [-11.68, 86.89]
1078 [0.00, 86.10]
1079 [12.09, 86.81]
1080 [19.40, 90.00]
1081 [34.68, 90.50]
1082 [60.56, 91.00]
1083 [170.14, 91.00]
1084 [175.05, 90.50]
1085 [180.29, 90.00]
1086 [193.41, 90.00]
1087 [195.98, 90.50]
1088 [377.02, 92.50]
1089
1090 *#####
1091 *# Catchment OKEEFE
1092 *# - To O'Keefe drain (north of the Jock)
1093 *# - Developed with assumed 43% imp.
1094 *# - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area
513.02 HA)
1095 *# - 2020-11-20 Okeefe detailed model was added as per the NOVATECH SWMHMO model
(Citi-Gate 2014).
1096
1097 *POST DEVELOPMENT CONDITIONS
1098
1099 *#####
1100 CONTINUOUS NASHYD NYHD= [ "O-1" ], DT=[1]min, AREA=[63.72](ha),
1101 DWF=[0](cms), CN/C=[61], IA=[6.2](mm), N=[3], TP=[.9]hrs,
1102 Continuous simulation parameters:
1103 IaRECper=[4](hrs),
1104 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1105 InterEventTime=[12](hrs)
1106 Baseflow simulation parameters:
1107 BaseFlowOption=[1],
1108 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1109 VHydCond=[0.055](mm/hr), END=-1

```

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1110 *%-----|-----|
1111 *ROUTE FLOW THROUGH AREA 0-2
1112 ROUTE CHANNEL      NHYDout=[ "O-1R" ], NHYDin=[ "O-1" ], RDT=[ 1 ](min),
1113 CHLNGTH=[ 960 ](m), CHSLOPE=[ 0.63 ](%), FPSLOPE=[ 0.63 ](%),
1114 SECNUM=[ 1 ], NSEG=[ 3 ]
1115 ( SEGROUGH, SEGDIST (m) )=[ 0.06, 4 -.043, 6 0.06, 10 ] NSEG times
1116 ( DISTANCE (m), ELEVATION (m) )=[ 0.00, 2.0 ]
1117 [ 0.0, 2.0 ]
1118 [ 4.0, 0.0 ]
1119 [ 6.0, 0.0 ]
1120 [ 10.0, 2.0 ]
1121 *%
1122 CONTINUOUS NASHYD  NHYD=[ "O-2" ], DT=[ 1 ]min, AREA=[ 28.61 ](ha),
1123 DWF=[ 0 ](cms), CN/C=[ 57 ], IA=[ 5.2 ](mm), N=[ 3 ], TP=[ 1.1 ]hrs,
1124 Continuous simulation parameters:
1125 IaRECper=[ 4 ](hrs),
1126 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1127 InterEventTime=[ 12 ](hrs)
1128 Baseflow simulation parameters:
1129 BaseFlowOption=[ 1 ],
1130 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
1131 VHydCond=[ 0.055 ](mm/hr), END=-1
1132 *%
1133 CONTINUOUS NASHYD  NHYD=[ "O-4" ], DT=[ 1 ]min, AREA=[ 46.94 ](ha),
1134 DWF=[ 0 ](cms), CN/C=[ 49 ], IA=[ 9.2 ](mm), N=[ 3 ], TP=[ 0.9 ]hrs,
1135 Continuous simulation parameters:
1136 IaRECper=[ 4 ](hrs),
1137 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1138 InterEventTime=[ 12 ](hrs)
1139 Baseflow simulation parameters:
1140 BaseFlowOption=[ 1 ],
1141 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
1142 VHydCond=[ 0.055 ](mm/hr), END=-1
1143 *%
1144 *TOTAL EXTERNAL FLOW NORTH OF O'KEEFE CT. CROSSING
1145 ADD HYD          NHYDsum=[ "OKF-N" ], NHYDs to add=[ "O-1R"+ "O-2" + "O-4" ]
1146 *%
1147 *ROUTE FLOW THROUGH AREA O-6
1148 ROUTE CHANNEL    ROUTE CHANNEL NHYDout=[ "OKF-NR" ], NHYDin=[ "OKF-N" ], RDT=[ 1 ](min),
1149 CHLNGTH=[ 210 ](m), CHSLOPE=[ .81 ](%), FPSLOPE=[ .81 ](%),
1150 SECNUM=[ 1 ], NSEG=[ 3 ]
1151 ( SEGROUGH, SEGDIST (m) )=[ 0.043, 22.43 -.043, 25.07
1152 0.043, 45.54 ] NSEG times
1153 ( DISTANCE (m), ELEVATION (m) )=[ 0.00, 3.73 ]
1154 ( 14.62, 1.56 )
1155 ( 18.41, 1.44 )
1156 ( 22.43, 0.00 )
1157 ( 25.07, 0.70 )
1158 ( 29.10, 1.79 )
1159 ( 33.73, 2.71 )
1160 ( 45.54, 3.58 )
1161 *%
1162 CONTINUOUS NASHYD NHYD=[ "O-6" ], DT=[ 1 ]min, AREA=[ 16.46 ](ha),
1163 DWF=[ 0 ](cms), CN/C=[ 43 ], IA=[ 9.2 ](mm), N=[ 3 ], TP=[ 0.7 ]hrs,
1164 Continuous simulation parameters:
1165 IaRECper=[ 4 ](hrs),
1166 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1167 InterEventTime=[ 12 ](hrs)
1168 Baseflow simulation parameters:
1169 BaseFlowOption=[ 1 ],
1170 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
1171 VHydCond=[ 0.055 ](mm/hr), END=-1
1172 *%
1173 CONTINUOUS STANDHYD NHYD=[ "O-3" ], DT=[ 1 ](min), AREA=[ 39.67 ](ha), XIMP=[ 0.15 ],
1174 TIMP=[ 0.30 ], DWF=[ 0 ](cms),

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1174 LOSS=[2], SCS curve number CN=[50], Pervious surfaces:
1175 IAper=[4.67](mm), SLPP=[0.32](%),
1176 LGP=[440](m), MNP=[0.035], SCP=[0](min), Impervious surfaces:
1177 IAimp=[1.57](mm), SLPI=[0.32](%),
1178 LGI=[1880](m), MNI=[0.013], SCI=[0](min),
1179 Continuous simulation parameters:
1180 IaRECper=[4](hrs), IaRECImp=[4](hrs),
1181 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1182 InterEventTime=[12](hrs), END=-1
1183 *%-----|-----|
1184 CONTINUOUS STANDHYD NHYD=[ "O-5" ], DT=[1](min), AREA=[60.63](ha), XIMP=[0.13],
1185 TIMP=[0.26], DWF=[0](cms),
1186 LOSS=[2], SCS curve number CN=[61],
1187 Previous surfaces: IAper=[4.67](mm), SLPP=[1.38](%),
1188 LGP=[550](m), MNP=[0.035], SCP=[0](min), Impervious surfaces:
1189 IAimp=[1.57](mm), SLPI=[1.38](%),
1190 LGI=[1450](m), MNI=[0.013], SCI=[0](min),
1191 Continuous simulation parameters:
1192 IaRECper=[4](hrs), IaRECImp=[4](hrs),
1193 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1194 InterEventTime=[12](hrs), END=-1
1195 *%-----|-----|
1196 *TOTAL EXTERNAL FLOWS WEST OF THE SITE AND NORTH OF O'KEEFE CRT
1197 *%-----|-----|
1198 ADD HYD NHYDsum=[ "PT1" ], NHYDs to add=[ "OKF-NR "+"O-3 "+"O-5 "+"O-6" ]
1199 *%-----|-----|
1200 CONTINUOUS NASHYD NHYD=[ "O-7" ], DT=[1]min, AREA=[5.28](ha),
1201 DWF=[0](cms), CN/C=[54], IA=[7.5](mm), N=[3], TP=[0.6]hrs,
1202 Continuous simulation parameters:
1203 IaRECper=[4](hrs),
1204 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1205 InterEventTime=[12](hrs)
1206 Baseflow simulation parameters:
1207 BaseFlowOption=[1] ,
1208 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1209 VHydCond=[0.055](mm/hr), END=-1
1210 *%-----|-----|
1211 *ANALYSIS POINT 1 - TOTAL FLOW NORTH OF FALLOWFIELD DR. AND O'KEEFE CRT.
1212 ADD HYD NHYDsum=[ "FF" ], NHYDs to add=[ "PT1"+ "O-7" ]
1213 *%-----|-----|
1214 *ROUTE FLOW through O'Keefe Drain 1
1215 ROUTE CHANNEL NHYDout=[ "DRAIN1" ], NHYDin=[ "FF" ], RDT=[1](min),
1216 CHLNGTH=[302]{m}, CHSLOPE=[1.00](%), FPSLOPE=[1.00](%),
1217 SECNUM=[1], NSEG=[3]
1218 ( SEGRROUGH, SEGDIST (m))=[0.07,13.45 -0.043,16.55 0.07,30.00] NSEG
1219 times
1220 ( DISTANCE (m), ELEVATION (m))=[0.00, 1.70]
1221 (3.45, 0.60)
1222 (13.45, 0.50)
1223 (14.45, 0.00)
1224 (15.55, 0.00)
1225 (16.55, 0.50)
1226 (26.55, 0.60)
1227 (30.00, 1.70)
1228 *%-----|-----|
1229 CONTINUOUS NASHYD NHYD=[ "D1" ], DT=[1]min, AREA=[1.17](ha),
1230 DWF=[0](cms), CN/C=[84], IA=[9.0](mm), N=[3], TP=[0.28]hrs,
1231 Continuous simulation parameters:
1232 IaRECper=[4](hrs),
1233 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1234 InterEventTime=[12](hrs)
1235 Baseflow simulation parameters:
1236 BaseFlowOption=[1] ,
1237 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1238 VHydCond=[0.055](mm/hr), END=-1
1239 *%-----|-----|

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1235  CONTINUOUS STANDHYD NHYD=[ "A1" ], DT=[1]min, AREA=[ 2.50 ](ha), XIMP=[ 0.68 ], TIMP=[ 0.85 ],
1236  DWF=[ 0 ](cms), LOSS=[ 1 ]:
1237      Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
1238      F=[ 0.00 ](mm),
1239      Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%), LGP=[ 50 ](m),
1240      MNP=[ 0.250 ], SCP=[ 0 ](min),
1241      Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%),
1242      LGI=[ 223.607 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1243      Continuous simulation parameters:
1244      IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
1245      END=-1
1246  *%-----|-----|
1247  ROUTE RESERVOIR NHYDout=[ "A1-STR" ], NHYDin=[ "A1" ], RDT=[ 1 ](min),
1248      TABLE of ( OUTFLOW-STORAGE ) values
1249      (cms) - (ha-m)
1250      [ 0.000 , 0.000 ]
1251      [ 0.035 , 0.038 ]
1252      [ 0.072 , 0.051 ]
1253      [ 0.100 , 0.059 ]
1254      [ 0.125 , 0.070 ]
1255      [ 0.160 , 0.074 ]
1256      [ 0.185 , 0.081 ]
1257      [ -1 , -1 ] (max twenty pts)
1258      NHYDovf=[ "A1-OVF" ]
1259  *%-----|-----|
1260  CONTINUOUS STANDHYD NHYD=[ "ST-2" ], DT=[1]min, AREA=[ 0.59 ](ha), XIMP=[ 0.46 ],
1261  TIMP=[ 0.57 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
1262      Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
1263      F=[ 0.00 ](mm),
1264      Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%), LGP=[ 50 ](m),
1265      MNP=[ 0.250 ], SCP=[ 0 ](min),
1266      Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%),
1267      LGI=[ 108.628 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1268      Continuous simulation parameters:
1269      IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
1270      END=-1
1271  *%-----|-----|
1272  *%-----|-----|
1273  *TOTAL FLOW NORTH OF STRANDHERD DR. (EAST BRANCH) CROSSING
1274  *%-----|-----|
1275  CONTINUOUS NASHYD NHYD=[ "O-8" ], DT=[1]min, AREA=[ 60.55 ](ha),
1276  DWF=[ 0 ](cms), CN/C=[ 69 ], IA=[ 4.0 ](mm), N=[ 3 ], TP=[ 1.0 ]hrs,
1277  Continuous simulation parameters:
1278  IaRECper=[ 4 ](hrs),
1279  SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1280  InterEventTime=[ 12 ](hrs)
1281  Baseflow simulation parameters:
1282  BaseFlowOption=[ 1 ],
1283  InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
1284  VHdCond=[ 0.055 ](mm/hr), END=-1
1285  *%-----|-----|
1286  ROUTE PIPE PTYPE=[ 2 ]rect, NHYDout=[ "O8PIPE" ], RNUMBER=[ 1 ], PWIDTH=[ 1800 ](mm),
1287  PHEIGHT=[ 1200 ](mm), PLNGTH=[ 335.1 ](m),
1288  PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m), NHYDin=[ "O-8" ], RDT=[ 1 ](min)
1289  *%-----|-----|
1290  *%-----|-----|
ADD HYD NHYDsum=[ "ST2-IN" ], NHYDs to

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add=[ "DRAIN1" +"D1" +"A1-STR" +"A1-OVF" +"ST2STR" +"ST2OVF" +"O8PIPE" ]
*%-----|-----|
1290
1291 CONTINUOUS STANDHYD NHYD=[ "A7" ], DT=[1]min, AREA=[ 3.51 ](ha), XIMP=[ 0.68 ], TIMP=[ 0.85 ],
1292 DWF=[ 0 ](cms), LOSS=[ 1 ]:
1293             Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
1294             F=[ 0.00 ](mm),
1295             Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%), LGP=[ 50 ](m),
1296             MNP=[ 0.250 ], SCP=[ 0 ](min),
1297             Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%),
1298             LGI=[ 264.953 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1299             Continuous simulation parameters:
1300             IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
1301             END=-1
1302 *%-----|-----|
1303 ROUTE RESERVOIR NHYDout=[ "A7-STR" ], NHYDin=[ "A7" ], RDT=[ 1 ](min),
1304             TABLE of ( OUTFLOW-STORAGE ) values
1305             (cms) - (ha-m)
1306             [ 0.000 , 0.000 ]
1307             [ 0.049 , 0.054 ]
1308             [ 0.102 , 0.072 ]
1309             [ 0.140 , 0.082 ]
1310             [ 0.175 , 0.099 ]
1311             [ 0.225 , 0.105 ]
1312             [ 0.260 , 0.114 ]
1313             [ -1 , -1 ] (max twenty pts)
1314             NHYDovf=[ "A7-OVF" ]
1315 *%-----|-----|
1316 CONTINUOUS STANDHYD NHYD=[ "ST-3" ], DT=[1]min, AREA=[ 0.71 ](ha), XIMP=[ 0.46 ],
1317 TIMP=[ 0.57 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
1318             Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
1319             F=[ 0.00 ](mm),
1320             Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%), LGP=[ 50 ](m),
1321             MNP=[ 0.250 ], SCP=[ 0 ](min),
1322             Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%),
1323             LGI=[ 119.164 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1324             Continuous simulation parameters:
1325             IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
1326             END=-1
1327 *%-----|-----|
1328 ROUTE RESERVOIR NHYDout=[ "ST3STR" ], NHYDin=[ "ST-3" ], RDT=[ 1 ](min),
1329             TABLE of ( OUTFLOW-STORAGE ) values
1330             (cms) - (ha-m)
1331             [ 0.000 , 0.0000 ]
1332             [ 0.063 , 0.0010 ]
1333             [ 0.064 , 0.0094 ]
1334             [ -1 , -1 ] (max twenty pts)
1335             NHYDovf=[ "ST3OVF" ]
1336 *%-----|-----|
1337 *ANALYSIS POINT 2 - TOTAL FLOW AT OUTLET OF STREET 2/3 INTERSECTION
1338 *%-----|-----|
1339 ADD HYD NHYDsum=[ "PT2ST3" ], NHYDs to
1340 add=[ "ST2-IN" +"A7-STR" +"A7-OVF" +"ST3STR" +"ST3OVF" ]
1341 *%-----|-----|
1342 *ROUTE FLOW through O'Keefe Drain 2
1343 ROUTE CHANNEL NHYDout=[ "DRAIN2" ], NHYDin=[ "PT2ST3" ], RDT=[ 1 ](min),
1344             CHLGTH=[ 592 ]{m}, CHSLOPE=[ .23 ](%), FPSLOPE=[ .23 ](%),
1345             SECNUM=[ 1 ], NSEG=[ 3 ]
1346             ( SEGROUGH, SEGDIST (m))=[ 0.07, 12.60 -0.043, 17.40 0.07, 30.00 ] NSEG
1347             times
1348             ( DISTANCE (m), ELEVATION (m))=[ 0.00, 1.70 ]
1349             ( 2.60, 0.95 )
1350             ( 12.60, 0.75 )
1351             ( 14.10, 0.00 )
1352             ( 15.90, 0.00 )
1353             ( 17.40, 0.75 )
1354             ( 27.40, 0.95 )

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1343 (30.00, 1.70)
1344 *%-----|-----|
1345 CONTINUOUS NASHYD NYHD=[ "D2" ], DT=[1]min, AREA=[ 2.28 ](ha), DWF=[ 0 ](cms), CN/C=[ 84 ],
1346 IA=[ 9.0 ](mm),
1347 N=[ 3 ], TP=[ 0.99 ]hrs,
1348 Continuous simulation parameters:
1349 IaRECper=[ 4 ](hrs),
1350 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1351 InterEventTime=[ 12 ](hrs)
1352 Baseflow simulation parameters:
1353 BaseFlowOption=[ 1 ],
1354 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
1355 VHydCond=[ 0.055 ](mm/hr), END=-1
1356 *%-----|-----|
1357 CONTINUOUS STANDHYD NYHD=[ "A17" ], DT=[1]min, AREA=[ 12.04 ](ha), XIMP=[ 0.68 ],
1358 TIMP=[ 0.85 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
1359 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
1360 F=[ 0.00 ](mm),
1361 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%), LGP=[ 50 ](m),
1362 MNP=[ 0.250 ], SCP=[ 0 ](min),
1363 Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%),
1364 LGI=[ 490.714 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1365 Continuous simulation parameters:
1366 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
1367 END=-1
1368 *%-----|-----|
1369 ROUTE RESERVOIR NYHDout=[ "A17STR" ], NYHDin=[ "A17" ], RDT=[ 1 ](min),
1370 TABLE of ( OUTFLOW-STORAGE ) values
1371 (cms) - (ha-m)
1372 [ 0.000 , 0.000 ]
1373 [ 0.169 , 0.185 ]
1374 [ 0.349 , 0.248 ]
1375 [ 0.482 , 0.283 ]
1376 [ 0.602 , 0.338 ]
1377 [ 0.771 , 0.359 ]
1378 [ 0.891 , 0.391 ]
1379 [ -1 , -1 ] (max twenty pts)
1380 NYHDovf=[ "A17OVF" ]
1381 *%-----|-----|
1382 CONTINUOUS STANDHYD NYHD=[ "ST-4" ], DT=[1]min, AREA=[ 0.35 ](ha), XIMP=[ 0.46 ],
1383 TIMP=[ 0.57 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
1384 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
1385 F=[ 0.00 ](mm),
1386 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%), LGP=[ 50 ](m),
1387 MNP=[ 0.250 ], SCP=[ 0 ](min),
1388 Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%), LGI=[ 83.666 ](m),
1389 MNI=[ 0.013 ], SCI=[ 0 ](min),
1390 Continuous simulation parameters:
1391 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
1392 END=-1
1393 *%-----|-----|
1394 ROUTE RESERVOIR NYHDout=[ "ST4STR" ], NYHDin=[ "ST-4" ], RDT=[ 1 ](min),
1395 TABLE of ( OUTFLOW-STORAGE ) values
1396 (cms) - (ha-m)
1397 [ 0.000 , 0.0000 ]
1398 [ 0.031 , 0.0010 ]
1399 [ 0.032 , 0.0050 ]
1400 [ -1 , -1 ] (max twenty pts)
1401 NYHDovf=[ "ST4OVF" ]
1402 *%-----|-----|
1403 CONTINUOUS STANDHYD NYHD=[ "A18" ], DT=[1]min, AREA=[ 5.30 ](ha), XIMP=[ 0.68 ], TIMP=[ 0.85 ],
1404 DWF=[ 0 ](cms), LOSS=[ 1 ]:
1405 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
1406 F=[ 0.00 ](mm),
1407 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%), LGP=[ 50 ](m),
1408 MNP=[ 0.250 ], SCP=[ 0 ](min),

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1452 [ 0.048 , 0.052 ]
1453 [ 0.099 , 0.070 ]
1454 [ 0.136 , 0.080 ]
1455 [ 0.170 , 0.096 ]
1456 [ 0.218 , 0.102 ]
1457 [ 0.252 , 0.111 ]
1458 [ -1 , -1 ] (max twenty pts)
1459 NHYDovf=[ "C1-OVF" ]

1460 *%
1461 CONTINUOUS STANDHYD NHYD=[ "ST-5" ], DT=[1]min, AREA=[0.45](ha), XIMP=[0.46],
1462 TIMP=[0.57], DWF=[0](cms), LOSS=[1]:
1463 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1464 F=[0.00](mm),
1465 Previous areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1466 MNP=[0.250], SCP=[0](min),
1467 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[94.868](m),
1468 MNI=[0.013], SCI=[0](min),
1469 Continuous simulation parameters:
1470 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
1471 END=-1

1472 *%
1473 ROUTE RESERVOIR NHYDout=[ "ST5STR" ], NHYDin=[ "ST-5" ], RDT=[1](min),
1474 TABLE of ( OUTFLOW-STORAGE ) values
1475 (cms) - (ha-m)
1476 [ 0.000 , 0.0000 ]
1477 [ 0.040 , 0.0010 ]
1478 [ 0.041 , 0.0062 ]
1479 [ -1 , -1 ] (max twenty pts)
1480 NHYDovf=[ "ST5OVF" ]

1481 *%
1482 ADD HYD NHYDsum=[ "ST5-E" ], NHYDs to
1483 add=[ "DRAIN3 "+"D3 "+"C1-STR "+"C1-OVF "+"ST5STR "+"ST5OVF" ]
1484 *%
1485 CONTINUOUS STANDHYD NHYD=[ "STRAND" ], DT=[1](min), AREA=[7.59](ha),
1486 XIMP=[0.64], TIMP=[0.85], DWF=[0](cms), LOSS=[1]:
1487 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1488 F=[0.00](mm),
1489 Previous areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[40](m),
1490 MNP=[0.250], SCP=[0](min),
1491 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[1230](m),
1492 MNI=[0.013], SCI=[0](min),
1493 Continuous simulation parameters:
1494 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
1495 END=-1

1496 *%
1497 ROUTE RESERVOIR NHYDout=[ "S-POND" ], NHYDin=[ "STRAND" ], RDT=[1](min),
1498 TABLE of ( OUTFLOW-STORAGE ) values
1499 (cms) - (ha-m)
1500 [ 0.000 , 0.000 ]
1501 [ 0.033 , 0.188 ]
1502 [ 0.057 , 0.253 ]
1503 [ 0.104 , 0.287 ]
1504 [ 0.160 , 0.336 ]
1505 [ 0.340 , 0.346 ]
1506 [ 0.471 , 0.360 ]
1507 [ 0.824 , 0.390 ]
1508 [ -1 , -1 ] (max twenty pts)
1509 NHYDovf=[ "S-OVF" ]

1510 *%
1511 ADD HYD NHYDsum=[ "SSAOUT" ], NHYDs to add=[ "ST5-E "+"S-POND "+"S-OVF" ]
1512 *%
1513 SAVE HYD NHYD=[ "SSAOUT" ], # OF PCYCLES=[5], ICASESh=[1]
1514 HYD_COMMENT=[ "SSAOUT" ]

1515 *%
1516 CONTINUOUS STANDHYD NHYD=[ "Area-A" ], DT=[1]min, AREA=[66.75](ha), XIMP=[0.64],
1517 TIMP=[0.80], DWF=[0](cms), LOSS=[1]:

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1507 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1508 F=[0.00](mm),
1509 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1510 MNP=[0.250], SCP=[0](min),
1511 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[1155.422](m), MNI=[0.013], SCI=[0](min),
1512 Continuous simulation parameters:
1513 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
1514 END=-1
1515 *%-----|-----|
1516 SAVE HYD NHYD=[ "Area-A" ], # OF PCYCLES=[1], ICASEsh=[1]
1517 HYD_COMMENT=[ "SMWF-A Inflow" ]
1518 *%-----|-----|
1519 ROUTE RESERVOIR NHYDout=[ "SMWF-A" ], NHYDin=[ "Area-A" ], RDT=[1](min),
1520 TABLE of ( OUTFLOW-STORAGE ) values
1521 (cms) - (ha-m)
1522 [ 0.000 , 0.000 ]
1523 [ 0.103 , 1.077 ]
1524 [ 0.128 , 1.749 ]
1525 [ 0.382 , 2.282 ]
1526 [ 0.703 , 2.582 ]
1527 [ 1.256 , 2.978 ]
1528 [ 1.567 , 3.202 ]
1529 [ 1.955 , 3.493 ]
1530 [ 2.100 , 3.600 ]
1531 [ -1 , -1 ] (max twenty pts)
1532 NHYDovf=[ "SWMAOV" ]
1533 *%-----|-----|
1534 SAVE HYD NHYD=[ "SMWF-A" ], # OF PCYCLES=[1], ICASEsh=[1]
1535 HYD_COMMENT=[ "SMWF-A Outflow" ]
1536 *%-----|-----|
1537 *ANALYSIS POINT 4 - TOTAL FLOW AT OUTLET OF STREET 5
1538 ADD HYD NHYDsum=[ "PT4ST5" ], NHYDs to add=[ "SSAOUT"+ "SMWF-A" + "SWMAOV" ]
1539 *%-----|-----|
1540 CONTINUOUS STANDHYD NHYD=[ "C6" ], DT=[1]min, AREA=[1.87](ha), XIMP=[0.68], TIMP=[0.85],
1541 DWF=[0](cms), LOSS=[1]:
1542 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1543 F=[0.00](mm),
1544 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1545 MNP=[0.250], SCP=[0](min),
1546 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[193.391](m), MNI=[0.013], SCI=[0](min),
1547 Continuous simulation parameters:
1548 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
1549 END=-1
1550 *%-----|-----|
1551 ROUTE RESERVOIR NHYDout=[ "C6-STR" ], NHYDin=[ "C6" ], RDT=[1](min),
1552 TABLE of ( OUTFLOW-STORAGE ) values
1553 (cms) - (ha-m)
1554 [ 0.000 , 0.000 ]
1555 [ 0.026 , 0.029 ]
1556 [ 0.054 , 0.038 ]
1557 [ 0.075 , 0.044 ]
1558 [ 0.093 , 0.052 ]
1559 [ 0.120 , 0.056 ]
1560 [ 0.138 , 0.061 ]
1561 [ -1 , -1 ] (max twenty pts)
1562 NHYDovf=[ "C6-OVF" ]
1563 *%-----|-----|
1564 CONTINUOUS STANDHYD NHYD=[ "C7" ], DT=[1]min, AREA=[1.62](ha), XIMP=[0.68], TIMP=[0.85],
1565 DWF=[0](cms), LOSS=[1]:
1566 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1567 F=[0.00](mm),
1568 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1569 MNP=[0.250], SCP=[0](min),

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1617
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1621
1622 *%-----|-----|
1623 CONTINUOUS STANDHYD NHYD= [ "Area-B" ], DT=[1]min, AREA=[ 24.04 ](ha), XIMP=[ 0.62 ],
1624 TIMP=[ 0.77 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
1625 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
1626 F=[ 0.00 ](mm),
1627 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 1.4 ](%), LGP=[ 50 ](m),
1628 MNP=[ 0.250 ], SCP=[ 0 ](min),
1629 Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 1.4 ](%),
1630 LGI=[ 693.397 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1631 Continuous simulation parameters:
1632 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
1633 END=-1
1634 *%-----|-----|
1635 ROUTE RESERVOIR NHYDout=[ "SWMF-B" ], NHYDin=[ "Area-B" ], RDT=[ 1 ](min),
1636 TABLE of ( OUTFLOW-STORAGE ) values
1637 ( cms ) - ( ha-m )
1638 [ 0.000 , 0.000 ]
1639 [ 0.025 , 0.090 ]
1640 [ 0.175 , 0.510 ]
1641 [ 0.350 , 0.710 ]
1642 [ 0.495 , 0.820 ]
1643 [ 0.648 , 0.980 ]
1644 [ 0.965 , 1.045 ]
1645 [ 1.072 , 1.140 ]
1646 [ -1 , -1 ] (max twenty pts)
1647 NHYDovf=[ "SWMBOVF" ]
1648 *%-----|-----|
1649 ADD HYD NHYDsum=[ "D4-EX" ], NHYDs to add=[ "DRAIN4" + "D4" + "SWMF-B" + "SWMBOVF" ]
1650 *%-----|-----|
1651 *ROUTE FLOW THROUGH O'Keefe Drain 5
1652 * JFSA: Nov. 2020, added en points to close X-Section
1653 ROUTE CHANNEL NHYDout=[ "DRAIN5" ], NHYDin=[ "D4-EX" ], RDT=[ 1 ](min),
1654 CHLGTH=[ 413.0 ](m), CHSLOPE=[ 0.16 ](%), FPSLOPE=[ 0.16 ](%),
1655 SECNUM=[ 1 ], NSEG=[ 3 ]
1656 ( SEROUGH, SEGDIST (m))=[ 0.043, 12.29 -0.033, 17.97
1657 0.043, 32.84 ] NSEG times
1658 ( DISTANCE (m), ELEVATION (m))=(-0.01, 2.50)
1659 [ 0.00, 1.41 ]
1660 [ 6.13, 0.97 ]
1661 [ 12.29, 0.89 ]
1662 [ 15.71, 0.00 ]
1663 [ 17.97, 0.39 ]
1664 [ 23.04, 0.35 ]
1665 [ 32.83, 0.96 ]
1666 ( 32.84, 2.50 )
1667 *%-----|-----|
1668 CONTINUOUS NASHYD NHYD=[ "D5" ], DT=[ 1 ]min, AREA=[ 1.90 ](ha),
1669 DWF=[ 0 ](cms), CN/C=[ 86 ], IA=[ 8.7 ](mm), N=[ 3 ], TP=[ 0.69 ]hrs,
1670 Continuous simulation parameters:
1671 IaRECper=[ 4 ](hrs),
1672 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1673 InterEventTime=[ 12 ](hrs)
1674 Baseflow simulation parameters:
1675 BaseFlowOption=[ 1 ],
1676 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
1677 VHydCond=[ 0.055 ](mm/hr), END=-1
1678 *%-----|-----|
1679 *EXTERNAL FLOWS SOUTHEAST OF THE SITE NORTH OF McKENNA CASEY DR.
1680 CONTINUOUS NASHYD NHYD=[ "O-13SDF" ], DT=[ 1 ]min, AREA=[ 9.74 ](ha),
1681 DWF=[ 0 ](cms), CN/C=[ 81 ], IA=[ 4.0 ](mm), N=[ 3 ], TP=[ .43 ]hrs,
1682 Continuous simulation parameters:

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1678 IaRECper=[4](hrs),
1679 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1680 InterEventTime=[12](hrs)
1681 Baseflow simulation parameters:
1682 BaseFlowOption=[1],
1683 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1684 VHydCond=[0.055](mm/hr), END=-1
1685 *%-----|-----|
1686 *SNOW DISPOSAL FACILITY
1687 *PARAMETERS BASED ON ROBINSON 2006 MODEL
1688 ROUTE RESERVOIR NHYDout=[ "SDF" ], NHYDin=[ "O-13SDF" ], RDT=[1](min),
1689 TABLE of ( OUTFLOW-STORAGE ) values
1690 (cms) - (ha-m)
1691 [0.000,0.000]
1692 [0.150,0.600]
1693 (0.200,1.500)
1694 [-1, -1] (max twenty pts)
1695 NHYDovf=[ "OVFSDF" ]
1696 *%-----|-----|
1697 *ANALYSIS POINT 6 - McKenna Casey Dr.
1698 *%-----|-----|
1699 ADD HYD NHYDsum=[ "PT6MC" ], NHYDs to add=[ "DRAIN5"+"D5"+"SDF" ]
1700 *%-----|-----|
1701 CONTINUOUS NASHYD NHYD=[ "O-15" ], DT=[1]min, AREA=[10.67](ha),
1702 DWF=[0](cms), CN/C=[82], IA=[7.5](mm), N=[3], TP=[0.30]hrs,
1703 Continuous simulation parameters:
1704 IaRECper=[4](hrs),
1705 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1706 InterEventTime=[12](hrs)
1707 Baseflow simulation parameters:
1708 BaseFlowOption=[1],
1709 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1710 VHydCond=[0.055](mm/hr), END=-1
1711 *%-----|-----|
1712 *TOTAL FLOW NORTH OF McKENNA CASEY DR.
1713 ADD HYD NHYDsum=[ "M-C" ], NHYDs to add=[ "PT6MC"+"O-15" ]
1714 *%-----|-----|
1715 *ROUTE FLOW THROUGH AREA O-14
1716 * JFSA: Nov. 2020, added end points to close X-section
1717 ROUTE CHANNEL NHYDout=[ "O-14Ch" ], NHYDin=[ "M-C" ], RDT=[1](min),
1718 CHLNGTH=[845.3](m), CHSLOPE=[0.10](%), FPSLOPE=[0.10](%),
1719 SECNUM=[1], NSEG=[3]
1720 ( SEGROUGH, SEGDIST (m))=[0.06,15.00 -0.033,18.04 0.06,31.85] NSEG
times
1721 ( DISTANCE (m), ELEVATION (m))=[-0.01, 2.5
1722 (0.00, 1.53]
1723 (5.56, 1.47)
1724 (9.21, 1.45)
1725 (12.45, 1.53)
1726 (13.70, 1.50)
1727 (15.00, 0.69)
1728 (15.34, 0.00)
1729 (16.51, 0.05)
1730 (17.30, 0.17)
1731 (18.04, 0.74)
1732 (19.29, 1.32)
1733 (22.73, 1.47)
1734 (31.84, 1.41)
1735 (31.85, 2.50)
1736 *%-----|-----|
1737 *% -Change O-14 from NASHYD to STANDHYD, name it "S-1-Okeefe" and add it to S-1
subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
1738 *% -JFSA 2021-02-16, add detailed subcatchment drainage area for each subcatchment
in Corrigan sub-catchment. After adding part of O-14 to S_1 sub-catchment so O-14
becomes 5 ha instead of 30.02 ha and TP becomes 0.133 (5*0.8/30.02) instead of 0.8
1739 CONTINUOUS NASHYD NHYD=[ "O-14" ], DT=[1]min, AREA=[5](ha),

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1740 DWF=[0](cms), CN/C=[82], IA=[7.5](mm), N=[3], TP=[0.133]hrs,
1741 Continuous simulation parameters:
1742 IaRECper=[4](hrs),
1743 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1744 InterEventTime=[12](hrs)
1745 Baseflow simulation parameters:
1746 BaseFlowOption=[1],
1747 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1748 VHydCond=[0.055](mm/hr), END=-1
1749 *
1750 *%-----| -----
1751 *ANALYSIS POINT 7 - JOCK RIVER
1752 * 2020-12-01 To Foster Drain
1753 * 2020-12-01 replace ("PT7JR") by ("OKEEFE")
1754 *%-----| -----
1755 ADD HYD      NHYDsum=[ "OKEEFE" ], NHYDs to add=["O-14Ch"+ "O-14"]
1756 *%-----| -----
1757 *CONTINUOUS STANDHYD NHYD=[ "OKEEFE" ], DT=[1](min), AREA=[448](ha),
1758 *           XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
1759 *           SCS curve number CN=[77],
1760 *           Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
1761 *           LGP=[40](m), MNP=[0.25], SCP=[0](min),
1762 *           Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
1763 *           LGI=[1728](m), MNI=[0.013], SCI=[0](min),
1764 *           Continuous simulation parameters:
1765 *           IaRECper=[4](hrs), IaRECimp=[4](hrs),
1766 *           SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1767 *           InterEventTime=[18](hrs), END=-1
1768 *#*****=====
1769 *# Okeefe Pond
1770 *# - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1771 *# and a ratio of the catchment area to the West Clarke pond rating curve
1772 *# from the MSS for the next coordinates
1773 *#*****
1774 *ROUTE RESERVOIR   NHYDout=[ "P_OKE" ], NHYDin=[ "OKEEFE" ],
1775 *           RDT=[1](min),
1776 *           TABLE of ( OUTFLOW-STORAGE ) values
1777 *           (cms) - (ha-m)
1778 *           [ 0.0 , 0.0]
1779 *           [ 14.13 , 13.0]
1780 *           [ -1 , -1 ] (maximum one hundred pairs of points)
1781 *           NHYDovf=[ "ok-OVF" ],
1782 *%-----| -----
1783 * -JFSA 2021-02-25 "S-1-D2" and "S-1-D3" are part of S-1 sub-catchment. They are
1784 moved to drain before station 6215 on Jock River
1785 *CONTINUOUS STANDHYD NHYD=[ "S-1-D2" ], DT=[1](min), AREA=[18.67](ha), XIMP=[0.65],
1786 *           LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
1787 *           IAper=[4.67](mm), SLPP=[2.0](%),
1788 *           LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
1789 *           IAimp=[1.57](mm), SLPI=[0.75](%),
1790 *           LGI=[352.798](m), MNI=[0.013], SCI=[0](min),
1791 *           IaRECper=[4](hrs), IaRECimp=[4](hrs),
1792 *           SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1793 *           InterEventTime=[12](hrs), END=-1
1794 *%-----| -----
1795 *CONTINUOUS NASHYD  NHYD=[ "S-1-D2" ], DT=[1]min, AREA=[18.67](ha),
1796 *           DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
1797 *           N=[3], TP=[1.120]hrs,
1798 Continuous simulation parameters:
1799 *           IaRECper=[4](hrs),
1800 *           SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
Baseflow simulation parameters:

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BaseFlowOption=[1] ,
InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
VHydCond=[0.055](mm/hr), END=-1
*%-----|-----|
*COMPUTE DUALHYD
*
NHYDin=[ "S-1-D2" ], CINLET=[ 2.062 ](cms), NINLET=[ 1 ],
MajNHYD=[ "S-1-D2J" ]
*
MinNHYD=[ "S-1-D2N" ]
*
TMJSTO=[ 99999999 ](cu-m)
*%-----|-----|
*ADD HYD
NHYDsum=[ "S-1-D2S" ], NYHDS to add=[ "S-1-D2J" +"S-1-D2N" ]
*%-----|-----|
*ROUTE RESERVOIR
NHYDout=[ "S-1-D2R" ] ,NYHdin=[ "S-1-D2S" ] ,
RDT=[1](min),
*
TABLE of ( OUTFLOW-STORAGE ) values
(cms) - (ha-m)
[ 0.0 , 0.0 ]
[ 0.2231, 0.7445 ]
[ -1 , -1 ] (max twenty pts)
NYHDovf=[ "S-1-D2Rovf" ]
*%-----|-----|
*CONTINUOUS STANDHYD
NHYD=[ "S-1-D3" ], DT=[1](min), AREA=[ 6.79 ](ha), XIMP=[ 0.65 ],
TIMP=[ 0.65 ], DWF=[ 0 ](cms),
*
LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%),
*
LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min), Impervious surfaces:
IAimp=[ 1.57 ](mm), SLPI=[ 0.75 ](%),
*
LGI=[ 212.760 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
*
Continuous simulation parameters:
IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
InterEventTime=[ 12 ](hrs), END=-1
*%-----|-----|
CONTINUOUS NASHYD
NHYD=[ "S-1-D3" ], DT=[1]min, AREA=[ 6.79 ](ha),
DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
N=[ 3 ], TP=[ 1.281 ]hrs,
Continuous simulation parameters:
IaRECper=[ 4 ](hrs),
SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
InterEventTime=[ 12 ](hrs)
Baseflow simulation parameters:
BaseFlowOption=[ 1 ],
InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
VHydCond=[ 0.055 ](mm/hr), END=-1
*%-----|-----|
*COMPUTE DUALHYD
NHYDin=[ "S-1-D3" ], CINLET=[ 0.719 ](cms), NINLET=[ 1 ],
MajNHYD=[ "S-1-D3J" ]
*
MinNHYD=[ "S-1-D3N" ]
*
TMJSTO=[ 99999999 ](cu-m)
*%-----|-----|
*ADD HYD
NHYDsum=[ "S-1-D3S" ], NYHDS to add=[ "S-1-D3J" +"S-1-D3N" ]
*%-----|-----|
*ROUTE RESERVOIR
NHYDout=[ "S-1-D3R" ] ,NYHdin=[ "S-1-D3S" ] ,
RDT=[1](min),
*
TABLE of ( OUTFLOW-STORAGE ) values
(cms) - (ha-m)
[ 0.0 , 0.0 ]
[ 0.0811, 0.2708 ]
[ -1 , -1 ] (max twenty pts)
NYHDovf=[ "S-1-D3Rovf" ]
*%-----|-----|
ADD HYD
NYHDsum=[ "SN_OK" ], NYHDS to add=[ "N_OK" +"OKEEFE" +"S-1-D2" +"S-1-D3" ]
*%-----|-----|
SAVE HYD
NHYD=[ "SN_OK" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
HYD_COMMENT=[ "Total Flows at Okeefe Drain" ]
*%-----|-----|
*#

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1864 *# Hydrograph from Node Okeefe routed to Node at Foster Drain
1865 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
1866 *#
1867 ROUTE CHANNEL      NHYDout=[ "N_FO" ] , NHYDin=[ "SN_OK" ] ,
1868           RDT=[1](min),
1869           CHLGH= [1183](m),   CHSLOPE=[ 0.0761](%),
1870                           FPSLOPE=[ 0.0761](%),
1871           SECNUM=[ 1.0],       NSEG=[ 3]
1872           ( SEGROUGH, SEGDIST (m))=
1873             [ 0.050, -33.89
1874               -0.035, 31.59
1875                 0.050, 34.41] NSEG times
1876           ( DISTANCE (m), ELEVATION (m))=
1877             [-794.18, 91.00]
1878             [-775.41, 91.50]
1879             [-702.63, 91.50]
1880             [-546.19, 91.50]
1881             [-529.54, 91.50]
1882             [-323.44, 91.00]
1883             [-320.71, 91.00]
1884             [-183.59, 91.00]
1885             [-182.54, 90.50]
1886             [-181.36, 90.00]
1887             [-177.37, 90.00]
1888             [-87.70, 90.00]
1889             [-33.89, 90.00]
1890             [-18.52, 86.88]
1891             [ 0.00, 85.20]
1892             [16.20, 86.83]
1893             [31.59, 90.00]
1894             [33.03, 90.50]
1895             [34.41, 91.00]
1896 *%-----|-----|-----|-----|-----|-----|-----|-----|-----|
1897 *#*****
1898 *#      Catchment FOSTER
1899 *#      - To Foster ditch (north of the Jock)
1900 *#      - Partially developed (medium density); remaining agricultural
1901 *#      - 2020-12-01 JFSA Foster area is 332 as per Foster SWMF Environmental Study
Report, CH2MHILL, Aug 2013.
1902 *#      - 2020-12-01 decrease Foster drainage area from (373 HA) to (307.98 HA) after
increasing Okeefe drainage area to (513.02 HA) so the total drainage area remains the
same
1903 *#      - 2021-02-12 update Foster area to 325.44 ha as measured from QGIS
1904 *#*****
1905 CONTINUOUS STANDHYD NHYD=[ "FOSTER" ], DT=[1]min, AREA=[ 325.44](ha),
1906           XIMP=[ 0.55], TIMP=[ 0.55], DWF=[ 0](cms), LOSS=[ 2],
1907           SCS curve number CN=[ 74],
1908           Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 0.5](%),
1909             LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
1910           Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 0.5](%),
1911             LGI=[ 1472.956](m), MNI=[ 0.013], SCI=[ 0](min),
1912           Continuous simulation parameters:
1913             IaRECper=[ 4](hrs), IaRECimp=[ 4](hrs),
1914             SMIN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1915             InterEventTime=[ 18](hrs), END=-1
1916 *#*****
1917 *#      Foster Pond
1918 *#      - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1919 *#      and a ratio of the catchment area to the West Clarke pond rating curve
1920 *#      from the MSS for the next coordinates
1921 *#*****
1922 ROUTE RESERVOIR      NHYDout=[ "P_FOS" ],   NHYDin=[ "FOSTER" ],
1923           RDT=[1](min),
1924           TABLE of ( OUTFLOW-STORAGE ) values
1925                         (cms) - (ha-m)
1926                         [ 0.0 , 0.0 ]

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1927 [      10.34 , 10]
1928 [      -1 , -1 ] (max twenty pts)
1929 NHYDovf=[ "FO-OVF" ]
1930 *%-----|-----|
1931 ADD HYD NHYDsum=[ "FOSTER-OUT" ], NHYDs to add=[ "P_FOS"+"FO-OVF" ]
1932 *%-----|-----|
1933 *#*****|-----|
1934 * -Brazeau area from P 1800-19 =[71.751], change to 63.59 ha based on GIS measurements
1935 * -JFSA, 2021-01-19 update "W_CLAR_BRAZ" to 73.29 ha based on GIS measurements
1936 * -JFSA, 2021-01-22 Brazeau ("MS_P10"+"P10-OVF")brazeau pond discharges directly
to the jock river through a road side ditch on the west side of Borrisokane road
(station 6016)
1937 CONTINUOUS STANDHYD NHYD=[ "W_CLAR_BRAZ" ], DT=[1]min, AREA=[73.29](ha),
1938 XIMP=[0.6], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
1939 SCS curve number CN=[77],
1940 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
1941 LGP=[40](m), MNP=[0.25], SCP=[0](min),
1942 Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
1943 LGI=[699.00](m), MNI=[0.013], SCI=[0](min),
1944 Continuous simulation parameters:
1945 IaRECper=[4](hrs), IaRECImp=[4](hrs),
1946 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1947 InterEventTime=[18](hrs), END=-1
1948 *%-----|-----|
1949 * 2020-12-01 correct pond curve values
1950 ROUTE RESERVOIR NHYDout=[ "MS_P10" ], NHYDin=[ "W_CLAR_BRAZ" ],
1951 RDT=[1](min),
1952 TABLE of ( OUTFLOW-STORAGE ) values
1953 (cms) - (ha-m)
1954 [      0.0 , 0.0 ]
1955 [     0.068 , 0.001 ]
1956 [     0.271 , 0.022 ]
1957 [     0.379 , 0.051 ]
1958 [     0.48 , 0.091 ]
1959 [     0.853 , 0.341 ]
1960 [     1.005 , 0.61 ]
1961 [     1.128 , 1.231 ]
1962 [     1.155 , 1.592 ]
1963 [     1.194 , 1.876 ]
1964 [     1.2 , 1.921 ]
1965 [     1.259 , 2.369 ]
1966 [     1.3 , 2.665 ]
1967 [     1.349 , 2.813 ]
1968 [      -1 , -1 ] (max twenty pts)
1969 NHYDovf=[ "P10-OVF" ]
1970 *%-----|-----|
1971 * -JFSA 2021-02-26 "S-1-FO-D2" is a part of S-1 sub-catchment. It is moved to drain
before station 980 on Foster Drain
1972 *CONTINUOUS STANDHYD NHYD=[ "S-1-FO-D2" ], DT=[1]min, AREA=[4.94](ha),
1973 * XIMP=[0.55], TIMP=[0.55], DWF=[0](cms), LOSS=[2],
1974 * SCS curve number CN=[74],
1975 * Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
1976 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
1977 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
1978 * LGI=[181.475](m), MNI=[0.013], SCI=[0](min),
1979 * Continuous simulation parameters:
1980 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
1981 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1982 * InterEventTime=[18](hrs), END=-1
1983 *%-----|-----|
1984 CONTINUOUS NASHYD NHYD=[ "S-1-FO-D2" ], DT=[1]min, AREA=[4.94](ha),
1985 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
1986 N=[3], TP=[1.10]hrs,
1987 Continuous simulation parameters:
1988 IaRECper=[4](hrs),
1989 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),

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1990           InterEventTime=[12](hrs)
1991           Baseflow simulation parameters:
1992           BaseFlowOption=[1] ,
1993           InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1994           VHydCond=[0.055](mm/hr), END=-1
1995 *%-----|-----|
1996 *COMPUTE DUALHYD      NHYDin=[ "S-1-FO-D2" ], CINLET=[ 0.508 ](cms), NINLET=[ 1 ],
1997 *
1998 *
1999 *
2000 *
2001 *ADD HYD               NHYDsum=[ "S-1-FO-D2S" ], NHYDs to add=[ "S-1-FO-D2J"+"S-1-FO-D2N" ]
2002 *%-----|-----|
2003 *ROUTE RESERVOIR     NHYDout=[ "S-1-FO-D2R" ] ,NHYDin=[ "S-1-FO-D2S" ] ,
2004 *
2005 *                      TABLE of ( OUTFLOW-STORAGE ) values
2006 *
2007 *                         [ 0.0      , 0.0   ]
2008 *                         [ 0.0590, 0.1970 ]
2009 *                         [      -1 ,      -1   ] (max twenty pts)
2010 *                         NHYDovf=[ "S-1FOD2ovf" ]
2011 *%-----|-----|
2012 ADD HYD                NHYDsum=[ "980" ], NHYDs to add=[ "FOSTER-OUT"+"S-1-FO-D2" ]
2013 *%-----|-----|
2014 SAVE HYD               NHYD=[ "980" ], # OF PCYCLES=[-1], ICASEsh=[1]
2015                      HYD_COMMENT=[ "Total Flows at Station 980 on Foster Drain" ]
2016 *%-----|-----|
2017 *#
2018 *# Hydrograph from Node Foster SWM (Station 980)to Node at station 520
2019 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 980
2020 *#
2021 ROUTE CHANNEL          NHYDout=[ "980-out" ] ,NHYDin=[ "980" ] ,
2022 RDT=[1](min),
2023 CHLGTH=[460](m), CHSLOPE=[0.04348](%), FPSLOPE=[0.04348](%),
2024 SECNUM=[1.0], NSEG=[3]
2025 ( SEGROUGH, SEGDIST (m))=
2026     [0.050,45.90
2027     -0.035,53.30
2028     0.050,100] NSEG times
2029 ( DISTANCE (m), ELEVATION (m))=
2030 [0, 91.75 ]
2031 [42.4, 92.18 ]
2032 [43.5, 92.16 ]
2033 [44.1, 92.1 ]
2034 [44.6, 92 ]
2035 [44.8, 91.86 ]
2036 [45.9, 91.04 ]
2037 [46.4, 90.65 ]
2038 [46.8, 90.36 ]
2039 [47.9, 90.32 ]
2040 [48.7, 90.35 ]
2041 [50.7, 90.33 ]
2042 [52.2, 90.38 ]
2043 [52.5, 90.59 ]
2044 [53.3, 91.28 ]
2045 [54, 91.83 ]
2046 [54.3, 92 ]
2047 [54.8, 92.08 ]
2048 [55.4, 92.12 ]
2049 [100, 91.84 ]
2050
2051 *%-----|-----|
2052 * -JFSA 2021-02-26 "S-1-FO-D1" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2053 *CONTINUOUS STANDHYD NHYD=[ "S-1-FO-D1" ], DT=[1]min, AREA=[ 5.11 ](ha),
2054 *                      XIMP=[ 0.65 ], TIMP=[ 0.65 ], DWF=[ 0 ](cms), LOSS=[ 2 ],

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2055 *
2056 * SCS curve number CN=[74],
2057 * Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[40](m),
2058 * MNP=[0.25], SCP=[0](min), Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2059 * LGI=[184.572](m), MNI=[0.013], SCI=[0](min),
2060 * Continuous simulation parameters:
2061 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
2062 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2063 * InterEventTime=[18](hrs), END=-1
2064 *%
2065 CONTINUOUS NASHYD NHYD=[ "S-1-FO-D1" ], DT=[1]min, AREA=[5.11](ha),
2066 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2067 N=[3], TP=[1.10]hrs,
2068 Continuous simulation parameters:
2069 IaRECper=[4](hrs),
2070 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2071 InterEventTime=[12](hrs)
2072 Baseflow simulation parameters:
2073 BaseFlowOption=[1] ,
2074 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2075 VHdCond=[0.055](mm/hr), END=-1
2076 *%
2077 *COMPUTE DUALHYD NHYDin=[ "S-1-FO-D1" ], CINLET=[0.605](cms), NINLET=[1],
2078 * MajNHYD=[ "S-1-FO-D1J" ]
2079 * MinNHYD=[ "S-1-FO-D1N" ]
2080 * TMJSTO=[99999999](cu-m)
2081 *%
2082 *ADD HYD NHYDsum=[ "S-1-FO-D1S" ], NHYDs to add=[ "S-1-FO-D1N"+ "S-1-FO-D1J" ]
2083 *%
2084 *ROUTE RESERVOIR NHYDout=[ "S-1-FO-D1R" ] ,NHYDin=[ "S-1-FO-D1S" ] ,
2085 * RDT=[1](min),
2086 * TABLE of ( OUTFLOW-STORAGE ) values
2087 * (cms) - (ha-m)
2088 * [ 0.0 , 0.0 ]
2089 * [ 0.0611, 0.2038 ]
2090 * [ -1 , -1 ] (max twenty pts)
2091 * NHYDovf=[ "S-1FOD1ovf" ]
2092 *%
2093 *ADD HYD NHYDsum=[ "520" ], NHYDs to add=[ "980-out"+ "S-1-FO-D1" ]
2094 *%
2095 *SAVE HYD NHYD=[ "520" ], # OF PCYCLES=[-1], ICASEsh=[1]
2096 HYD_COMMENT=[ "Total Flows at Station 520 on Foster Drain" ]
2097 *%
2098 *# Hydrograph from Node at Station 520 (Foster Drain) to Node at station 6016 (Jock
River)
2099 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 520
2100 *#
2101 *ROUTE CHANNEL NHYDout=[ "520-out" ] ,NHYDin=[ "520" ] ,
2102 RDT=[1](min),
2103 CHLGTH=[860](m), CHSLOPE=[0.5872](%),
2104 FPSLOPE=[0.5872](%),
2105 SECNUM=[1.0], NSEG=[3]
2106 ( SEGROUGH, SEGDIST (m))=
2107 [0.050,45.90
2108 -0.035,54.3
2109 0.050,100.1097] NSEG times
2110 ( DISTANCE (m), ELEVATION (m))=
2111 [0, 91.26 ]
2112 [44.9, 91.46 ]
2113 [45.1, 91.37 ]
2114 [45.9, 90.84 ]
2115 [47, 90.32 ]
2116 [47.5, 90.22 ]
2117 [48, 90.17 ]
2118 [50.7, 90.19 ]
2119 [51.5, 90.17 ]

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2120 [52.2, 90.13 ]
2121 [52.7, 90.12 ]
2122 [53.3, 90.14 ]
2123 [53.5, 90.31 ]
2124 [53.9, 90.59 ]
2125 [54.3, 90.87 ]
2126 [54.7, 91.04 ]
2127 [55.3, 91.24 ]
2128 [55.5, 91.26 ]
2129 [63.7, 91.37 ]
2130 [100.1097, 91.43 ]
2131 *%-----|-----|
2132 * -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2133 *CONTINUOUS STANDHYD NHYD=[ "S-1-FO-F-D" ], DT=[1]min, AREA=[14.96](ha),
2134 * XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2135 * SCS curve number CN=[74],
2136 * Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2137 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
2138 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2139 * LGI=[315.806](m), MNI=[0.013], SCI=[0](min),
2140 * Continuous simulation parameters:
2141 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
2142 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2143 * InterEventTime=[18](hrs), END=-1
2144 *%-----|-----|
2145 CONTINUOUS NASHYD NHYD=[ "S-1-FO-F-D" ], DT=[1]min, AREA=[14.96](ha),
2146 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2147 N=[3], TP=[1.007]hrs,
2148 Continuous simulation parameters:
2149 IaRECper=[4](hrs),
2150 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2151 InterEventTime=[12](hrs)
2152 Baseflow simulation parameters:
2153 BaseFlowOption=[1],
2154 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2155 VHydCond=[0.055](mm/hr), END=-1
2156 *%-----|-----|
2157 *COMPUTE DUALHYD NHYDin=[ "S-1-FO-F-D" ], CINLET=[1.749](cms), NINLET=[1],
2158 * MajNHYD=[ "S-1FO-F-DJ" ]
2159 * MinNHYD=[ "S-1FO-F-DN" ]
2160 * TMJSTO=[ 9999999 ](cu-m)
2161 *%-----|-----|
2162 *ADD HYD NHYDsum=[ "S-1FO-F-DS" ], NHYDs to add=[ "S-1FO-F-DJ"+ "S-1FO-F-DN" ]
2163 *%-----|-----|
2164 *ROUTE RESERVOIR NHYDout=[ "S-1FO-F-DR" ], NHYDin=[ "S-1FO-F-DS" ],
2165 * RDT=[1](min),
2166 * TABLE of ( OUTFLOW-STORAGE ) values
2167 * (cms) - (ha-m)
2168 * [ 0.0 , 0.0 ]
2169 * [ 0.1788, 0.5966 ]
2170 * [ -1 , -1 ] (max twenty pts)
2171 * NHYDovf=[ "S-1FoFDovf" ]
2172 *%-----|-----|
2173 * -JFSA 2021-02-26 "S-1-D8" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2174 * -JFSA 2021-03-02 "S-1-D8" is Borrisokane Rd. so it will remain STANDHYD in all
scenarios
2175 CONTINUOUS STANDHYD NHYD=[ "S-1-D8" ], DT=[1](min), AREA=[5.27](ha), XIMP=[0.65],
2176 TIMP=[0.65], DWF=[0](cms),
LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
IAper=[4.67](mm), SLPP=[2.0](%),
LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
LGI=[187.439](m), MNI=[0.013], SCI=[0](min),
Continuous simulation parameters:

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2180 IaRECper=[4](hrs), IaRECImp=[4](hrs),
2181 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2182 InterEventTime=[12](hrs), END=-1
2183 *%-----|-----|
2184 * This is a road so it is always STANDHYD
2185 *CONTINUOUS NASHYD NHYD=[ "S-1-D8" ], DT=[1]min, AREA=[ 5.27 ](ha),
2186 * DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
2187 * N=[ 3 ], TP=[ 1.10 ]hrs,
2188 * Continuous simulation parameters:
2189 * IaRECper=[ 4 ](hrs),
2190 * SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2191 * InterEventTime=[ 12 ](hrs)
2192 * Baseflow simulation parameters:
2193 * BaseFlowOption=[ 1 ],
2194 * InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2195 * VHydCond=[ 0.055 ](mm/hr), END=-1
2196 *%-----|-----|
2197 *COMPUTE DUALHYD NHYDin=[ "S-1-D8" ], CINLET=[ 2.279 ](cms), NINLET=[ 1 ],
2198 * MajNHYD=[ "S-1-D8J" ]

2200 *
2201 * TMJSTO=[ 9999999 ](cu-m)
2202 *%-----|-----|
2203 *ADD HYD NHYDsum=[ "S-1-D8S" ], NHYDs to add=[ "S-1-D8J" +"S-1-D8N" ]
2204 *%-----|-----|
2205 *ADD HYD NHYDsum=[ "S-1-D" ], NHYDs to add=[ "S-1-Okeefe" +"S-1" +"S-1-Fost" ]
2206 *%-----|-----|
2207 *COMPUTE DUALHYD NHYDin=[ "S-1-D" ], CINLET=[ 11.616 ](cms), NINLET=[ 1 ],
2208 * MajNHYD=[ "S-1-D-MJ" ]
2209 * MinNHYD=[ "S-1-D-MN" ]
2210 * TMJSTO=[ 5974 ](cu-m)
2211 *%-----|-----|
2212 *ADD HYD NHYDsum=[ "S-1-DEV" ], NHYDs to add=[ "S-1-D-MJ" +"S-1-D-MN" ]
2213 *%-----|-----|
2214 *ROUTE RESERVOIR NHYDout=[ "S-1-D8R" ], NHYDin=[ "S-1-D8S" ],
2215 * RDT=[ 1 ](min),
2216 * TABLE of ( OUTFLOW-STORAGE ) values
2217 * (cms) - (ha-m)
2218 * [ 0.0 , 0.0 ]
2219 * [ 0.0630, 0.2102 ]
2220 * [ -1 , -1 ] (max twenty pts)
2221 * NHYDovf=[ "S-1-D8Rovf" ]
2222 * -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2223 *CONTINUOUS NASHYD NHYD=[ "S-1-A" ], DT=[1]min, AREA=[ 75.88 ](ha),
2224 DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
2225 N=[ 3 ], TP=[ 0.619 ]hrs,
2226 Continuous simulation parameters:
2227 IaRECper=[ 4 ](hrs),
2228 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2229 InterEventTime=[ 12 ](hrs)
2230 Baseflow simulation parameters:
2231 BaseFlowOption=[ 1 ],
2232 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2233 VHydCond=[ 0.055 ](mm/hr), END=-1
2234 *%-----|-----|
2235 * -JFSA, 2021-01-22 "W_CLAR_UNDE" (west of Clarke sub-catchment) discharges
directly to the jock river through a road side ditch on the west side of Borrisokane
road (station 6016)
2236 *CONTINUOUS NASHYD NHYD=[ "W_CLAR_UNDE" ], DT=[1]min, AREA=[ 35.65 ](ha),
2237 DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
2238 N=[ 3 ], TP=[ 1.10 ]hrs,
2239 Continuous simulation parameters:
2240 IaRECper=[ 4 ](hrs),
2241 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2242 InterEventTime=[ 12 ](hrs)

```

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2243                               Baseflow simulation parameters:
2244                               BaseFlowOption=[1] ,
2245                               InitGWResVol=[ 50 ](mm) , GWResK=[ 0.96 ](mm/day/mm)
2246                               VHydCond=[ 0.055 ](mm/hr) , END=-1
2247 *%-----|-----|
2248 ADD HYD          NHYDsum=[ "SN_FO" ] , NHYDs to
2249 add=[ "N_FO"+"520-out"+"MS_P10"+"P10-OVF"+"W_CLAR_UNDE"+"S-1-FO-F-D"+"S-1-D8"+"S-1-A" ]
2250 *%-----|-----|
2251 SAVE HYD          NHYD=[ "SN_FO" ] , # OF PCYCLES=[ -1 ] , ICASEsh=[ 1 ]
2252                      HYD_COMMENT=[ "Total Flows at Foster Drain" ]
2253 *%-----|-----|
2254 *# Hydrograph from Node Foster routed to Node at Cedarview Road
2255 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6016
2256 *#
2257 ROUTE CHANNEL      NHYDout=[ "N_CE" ] , NHYDin=[ "SN_FO" ] ,
2258                      RDT=[ 1 ](min),
2259                      CHLGTH=[ 159 ](m) , CHSLOPE=[ 0.0818 ](%) ,
2260                      FPSLOPE=[ 0.0818 ](%) ,
2261                      SECNUM=[ 1.0 ] , NSEG=[ 3 ]
2262                      ( SEGROUGH , SEGDIST (m))=
2263                      [ 0.050,-15.46
2264                      -0.035,26.55
2265                      0.050,116.76 ] NSEG times
2266                      ( DISTANCE (m) , ELEVATION (m))=
2267                      [-645.23, 91.50]
2268                      [-391.20, 91.50]
2269                      [-91.00, 91.50]
2270                      [-85.52, 91.50]
2271                      [-15.46, 89.40]
2272                      [-9.79, 89.31]
2273                      [-3.22, 86.24]
2274                      [3.22, 85.07]
2275                      [10.96, 85.79]
2276                      [16.44, 86.49]
2277                      [26.55, 89.45]
2278                      [29.03, 90.27]
2279                      [35.76, 90.67]
2280                      [36.67, 91.00]
2281                      [108.08, 91.00]
2282                      [109.82, 90.50]
2283                      [112.04, 90.50]
2284                      [114.62, 91.00]
2285                      [116.76, 91.50]
2286 *%-----|-----|
2287 *#***** Catchment S-1
2288 *# - To Jock River (north and south of Jock)
2289 *# - Primarily agricultural fields; portion of sand quarry
2290 *%-----|-----|
2291 *% -2020-12-17 "S-1-Undev" and "S-1-Fost" was a part of Foster drain, they are below
the foster pond. Now they are added to S-1 subcatchment based on Project 1474-BCDC,
JFSA, Nov. 2020
2292 *% -2020-12-17 Change O-14 (it was part of Okeefe drain) to "S-1-Okeefe" and add it
to S-1 subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
2293 *% -2020-12-17 Add "S-1-BCDC" as NASHYD
2294 *% -2020-12-17 all other S-1 subcatchment as STANDHYD with DUALHYD and ROUTE RESERVOIR
2295 *%-----|-----|
2296 *#***** Catchment S-1
2297 * -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2298 *CONTINUOUS NASHYD   NHYD=[ "S-1-A" ] , DT=[ 1 ]min, AREA=[ 75.88 ](ha) ,
2299 *                      DWF=[ 0 ](cms) , CN/C=[ 77 ] , IA=[ 4.67 ](mm) ,
2300 *                      N=[ 3 ] , TP=[ 0.619 ]hrs ,
2301 *                      Continuous simulation parameters:
2302 *                      IaRECPer=[ 4 ](hrs) ,
2303 *                      SMIN=[ -1 ](mm) , SMAX=[ -1 ](mm) , SK=[ 0.010 ]/(mm) ,

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2304 *
2305 *
2306 *
2307 *
2308 *
2309 *%-----| -----
2310 CONTINUOUS NASHYD
2311 NHYD= ["S-1-B"], DT=[1]min, AREA=[55.36](ha),
2312 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2313 N=[3], TP=[0.451]hrs,
2314 Continuous simulation parameters:
2315 IaRECper=[4](hrs),
2316 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2317 InterEventTime=[12](hrs)
2318 Baseflow simulation parameters:
2319 BaseFlowOption=[1],
2320 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2321 VHydCond=[0.055](mm/hr), END=-1
2322 *%-----| -----
2323 *# - JFSA 2021-02-24 change the name from S-1-BCDC to S-1-A and S-1-B. Change their
2324 TP values based on the new areas compared to the old ones.
2325 *CONTINUOUS NASHYD NHYD= ["S-1-BCDC"], DT=[1]min, AREA=[134.9](ha),
2326 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2327 * N=[3], TP=[1.10]hrs,
2328 * Continuous simulation parameters:
2329 * IaRECper=[4](hrs),
2330 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2331 * InterEventTime=[12](hrs)
2332 * Baseflow simulation parameters:
2333 * BaseFlowOption=[1],
2334 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2335 * VHydCond=[0.055](mm/hr), END=-1
2336 *%-----| -----
2337 *# - JFSA 2021-02-24 "S-1-BCDC-1" and "S-1-BCDC-2" are not existing anymore.
2338 "S-1-BCDC-1" is part of "S-1-FO-D2" and "S-1-BCDC-2" is part of "S-1-D2" and "S-1-D3"
2339 *CONTINUOUS NASHYD NHYD= ["S-1-BCDC-1"], DT=[1]min, AREA=[0.3](ha),
2340 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2341 * N=[3], TP=[1.10]hrs,
2342 * Continuous simulation parameters:
2343 * IaRECper=[4](hrs),
2344 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2345 * InterEventTime=[12](hrs)
2346 * Baseflow simulation parameters:
2347 * BaseFlowOption=[1],
2348 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2349 * VHydCond=[0.055](mm/hr), END=-1
2350 *%-----| -----
2351 *CONTINUOUS NASHYD NHYD= ["S-1-BCDC-2"], DT=[1]min, AREA=[1.3](ha),
2352 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2353 * N=[3], TP=[1.10]hrs,
2354 * Continuous simulation parameters:
2355 * IaRECper=[4](hrs),
2356 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2357 * InterEventTime=[12](hrs)
2358 * Baseflow simulation parameters:
2359 * BaseFlowOption=[1],
2360 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2361 * VHydCond=[0.055](mm/hr), END=-1
2362 *%-----| -----
2363 *# - JFSA 2021-01-19, after adding Greenbank pond, "S-1-BCDC-3" is not existing
2364 anymore
2365 *CONTINUOUS NASHYD NHYD= ["S-1-BCDC-3"], DT=[1]min, AREA=[3.9](ha),
2366 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2367 * N=[3], TP=[1.10]hrs,
2368 * Continuous simulation parameters:
2369 * IaRECper=[4](hrs),
2370 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),

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2367 *
2368 *           InterEventTime=[12](hrs)
2369 *           Baseflow simulation parameters:
2370 *           BaseFlowOption=[1] ,
2371 *           InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2372 *           VHydCond=[0.055](mm/hr), END=-1
2373 *%-----|-----|
2373 * -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
before station 7245 on Jock River
2374 *CONTINUOUS STANDHYD NHYD=["S-1-Okeefe"], DT=[1](min), AREA=[44.93](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
2375 *           LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
IAper=[4.67](mm), SLPP=[2.0](%),
2376 *           LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
2377 *           LGI=[547.296](m), MNI=[0.013], SCI=[0](min),
2378 *           Continuous simulation parameters:
2379 *           IaRECper=[4](hrs), IaRECimp=[4](hrs),
2380 *           SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2381 *           InterEventTime=[12](hrs), END=-1
2382 *%-----|-----|
2383 *COMPUTE DUALHYD NHYDin=[ "S-1-Okeefe" ], CINLET=[ 4.796 ](cms), NINLET=[ 1 ],
2384 *           MajNHYD=[ "S-1-OkMJ" ]
2385 *           MinNHYD=[ "S-1-OkMN" ]
2386 *           TMJSTO=[ 9999999 ](cu-m)
2387 *%-----|-----|
2388 *ADD HYD NHYDsum=[ "S-1-Oks" ], NHYDs to add=[ "S-1-OkMJ"+"S-1-OkMN" ]
2389 *%-----|-----|
2390 *ROUTE RESERVOIR NHYDout=[ "S-1-OkSR" ] ,NHYDin=[ "S-1-Oks" ] ,
RDT=[1](min),
2391 *           TABLE of ( OUTFLOW-STORAGE ) values
2392 *           (cms) - (ha-m)
2393 *           [ 0.0      , 0.0   ]
2394 *           [ 0.5370 , 1.7917 ]
2395 *           [     -1  ,    -1    ] (max twenty pts)
2396 *           NHYDovf=[ "S-1-OkSovf" ]
2397 *%-----|-----|
2398 *CONTINUOUS NASHYD NHYD=[ "S-1-Okeefe" ], DT=[1]min, AREA=[ 44.93 ](ha),
2399 *           DWF=[0](cms), CN/C=[77], IA=[ 4.67 ](mm),
2400 *           N=[ 3 ], TP=[ 1.049 ]hrs,
2401 *           Continuous simulation parameters:
2402 *           IaRECper=[ 4 ](hrs),
2403 *           SMIN=[-1](mm), SMAX=[-1](mm), SK=[ 0.010 ]/(mm),
2404 *           InterEventTime=[12](hrs)
2405 *           Baseflow simulation parameters:
2406 *           BaseFlowOption=[ 1 ] ,
2407 *           InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2408 *           VHydCond=[ 0.055 ](mm/hr), END=-1
2409 *%-----|-----|
2410 * -JFSA 2021-02-26 "S-1-FO-D1" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2411 *CONTINUOUS STANDHYD NHYD=[ "S-1-FO-D1" ], DT=[1]min, AREA=[ 5.11 ](ha),
2412 *           XIMP=[ 0.65 ], TIMP=[ 0.65 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
2413 *           SCS curve number CN=[ 74 ],
2414 *           Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%),
2415 *           LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
2416 *           Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%),
2417 *           LGI=[ 184.572 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
2418 *           Continuous simulation parameters:
2419 *           IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
2420 *           SMIN=[-1](mm), SMAX=[-1](mm), SK=[ 0.010 ]/(mm),
2421 *           InterEventTime=[ 18 ](hrs), END=-1
2422 *%-----|-----|
2423 *COMPUTE DUALHYD NHYDin=[ "S-1-FO-D1" ], CINLET=[ 0.605 ](cms), NINLET=[ 1 ],
2424 *           MajNHYD=[ "S-1-FO-D1J" ]
2425 *           MinNHYD=[ "S-1-FO-D1N" ]
2426 *           TMJSTO=[ 9999999 ](cu-m)

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2428 *----- | -----
2429 *ADD HYD NHYDsum= [ "S-1-FO-D1S" ] , NHYDs to add= [ "S-1-FO-D1N"+"S-1-FO-D1J" ]
2430 *----- |
2431 *ROUTE RESERVOIR NHYDout=[ "S-1-FO-D1R" ] , NHYDin=[ "S-1-FO-D1S" ] ,
2432 * RDT=[1](min),
2433 * TABLE of ( OUTFLOW-STORAGE ) values
2434 * (cms) - (ha-m)
2435 * [ 0.0 , 0.0 ]
2436 * [ 0.0611, 0.2038 ]
2437 * [ -1 , -1 ] (max twenty pts)
2438 * NHYDovf=[ "S-1FOD1ovf" ]
2439 *----- |
2440 *CONTINUOUS NASHYD NHYD=[ "S-1-FO-D1" ], DT=[1]min, AREA=[ 5.11 ](ha),
2441 * DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
2442 * N=[ 3 ], TP=[ 1.10 ]hrs,
2443 * Continuous simulation parameters:
2444 * IaRECper=[ 4 ](hrs),
2445 * SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2446 * InterEventTime=[ 12 ](hrs)
2447 * Baseflow simulation parameters:
2448 * BaseFlowOption=[ 1 ],
2449 * InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2450 * VHydCond=[ 0.055 ](mm/hr), END=-1
2451 *----- |
2452 * -JFSA 2021-02-26 "S-1-FO-D2" is a part of S-1 sub-catchment. It is moved to drain
before station 980 on Foster Drain
2453 *CONTINUOUS STANDHYD NHYD=[ "S-1-FO-D2" ], DT=[1]min, AREA=[ 4.94 ](ha),
2454 * XIMP=[ 0.55 ], TIMP=[ 0.55 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
2455 * SCS curve number CN=[ 74 ],
2456 * Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%),
2457 * LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
2458 * Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%),
2459 * LGI=[ 181.475 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
2460 * Continuous simulation parameters:
2461 * IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
2462 * SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2463 * InterEventTime=[ 18 ](hrs), END=-1
2464 *----- |
2465 *CONTINUOUS NASHYD NHYD=[ "S-1-FO-D2" ], DT=[1]min, AREA=[ 4.94 ](ha),
2466 * DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
2467 * N=[ 3 ], TP=[ 1.10 ]hrs,
2468 * Continuous simulation parameters:
2469 * IaRECper=[ 4 ](hrs),
2470 * SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2471 * InterEventTime=[ 12 ](hrs)
2472 * Baseflow simulation parameters:
2473 * BaseFlowOption=[ 1 ],
2474 * InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2475 * VHydCond=[ 0.055 ](mm/hr), END=-1
2476 *----- |
2477 *COMPUTE DUALHYD NHYDin=[ "S-1-FO-D2" ], CINLET=[ 0.508 ](cms), NINLET=[ 1 ],
2478 * MajNHYD=[ "S-1-FO-D2J" ]
2479 * MinNHYD=[ "S-1-FO-D2N" ]
2480 * TMJSTO=[ 9999999 ](cu-m)
2481 *----- |
2482 *ADD HYD NHYDsum=[ "S-1-FO-D2S" ], NHYDs to add= [ "S-1-FO-D2J"+"S-1-FO-D2N" ]
2483 *----- |
2484 *ROUTE RESERVOIR NHYDout=[ "S-1-FO-D2R" ] , NHYDin=[ "S-1-FO-D2S" ] ,
2485 * RDT=[1](min),
2486 * TABLE of ( OUTFLOW-STORAGE ) values
2487 * (cms) - (ha-m)
2488 * [ 0.0 , 0.0 ]
2489 * [ 0.0590, 0.1970 ]
2490 * [ -1 , -1 ] (max twenty pts)
2491 * NHYDovf=[ "S-1FOD2ovf" ]
2492 *----- |

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2493 * -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
2494 before station 6016 on Jock River
2495 *CONTINUOUS STANDHYD NHYD=[ "S-1-FO-F-D" ], DT=[1]min, AREA=[14.96](ha),
2496 * XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2497 * SCS curve number CN=[74],
2498 * Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2499 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
2500 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2501 * LGI=[315.806](m), MNI=[0.013], SCI=[0](min),
2502 * Continuous simulation parameters:
2503 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
2504 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2505 * InterEventTime=[18](hrs), END=-1
2506 *%-----|-----|
2507 *CONTINUOUS NASHYD NHYD=[ "S-1-FO-F-D" ], DT=[1]min, AREA=[14.96](ha),
2508 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2509 * N=[3], TP=[1.007]hrs,
2510 * Continuous simulation parameters:
2511 * IaRECper=[4](hrs),
2512 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2513 * InterEventTime=[12](hrs)
2514 * Baseflow simulation parameters:
2515 * BaseFlowOption=[1],
2516 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2517 * VHdCond=[0.055](mm/hr), END=-1
2518 *%-----|-----|
2519 *COMPUTE DUALHYD NHYDin=[ "S-1-FO-F-D" ], CINLET=[1.749](cms), NINLET=[1],
2520 * MajNHYD=[ "S-1FO-F-DJ" ]
2521 * MinNHYD=[ "S-1FO-F-DN" ]
2522 * TMJSTO=[ 9999999 ](cu-m)
2523 *%-----|-----|
2524 *ADD HYD NHYDsum=[ "S-1FO-F-DS" ], NHYDs to add=[ "S-1FO-F-DJ"+"S-1FO-F-DN" ]
2525 *%-----|-----|
2526 *ROUTE RESERVOIR NHYDout=[ "S-1FO-F-DR" ], NHYDin=[ "S-1FO-F-DS" ],
2527 * RDT=[1](min),
2528 * TABLE of ( OUTFLOW-STORAGE ) values
2529 * (cms) - (ha-m)
2530 * [ 0.0 , 0.0 ]
2531 * [ 0.1788, 0.5966 ]
2532 * [ -1 , -1 ] (max twenty pts)
2533 * NHYDovf=[ "S-1FoFDovf" ]
2534 *%-----|-----|
2535 *CONTINUOUS STANDHYD NHYD=[ "S-1-D1" ], DT=[1](min), AREA=[21.67](ha), XIMP=[0.65],
2536 * TIMP=[0.65], DWF=[0](cms),
2537 * LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
2538 * IAper=[4.67](mm), SLPP=[2.0](%),
2539 * LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
2540 * IAimp=[1.57](mm), SLPI=[0.75](%),
2541 * LGI=[380.088](m), MNI=[0.013], SCI=[0](min),
2542 * Continuous simulation parameters:
2543 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
2544 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2545 * InterEventTime=[12](hrs), END=-1
2546 *%-----|-----|
2547 *CONTINUOUS NASHYD NHYD=[ "S-1-D1" ], DT=[1]min, AREA=[21.67](ha),
2548 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2549 * N=[3], TP=[1.066]hrs,
2550 * Continuous simulation parameters:
2551 * IaRECper=[4](hrs),
2552 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2553 * InterEventTime=[12](hrs)
2554 * Baseflow simulation parameters:
2555 * BaseFlowOption=[1],
2556 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2557 * VHdCond=[0.055](mm/hr), END=-1
2558 *%-----|-----|

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2555 *COMPUTE DUALHYD      NHYDin=[ "S-1-D1" ], CINLET=[ 2.482 ](cms), NINLET=[ 1 ],
2556 *
2557 *
2558 *          MajNHYD=[ "S-1-D1J" ]
2559 *          MinNHYD=[ "S-1-D1N" ]
2560 *          TMJSTO=[ 9999999 ](cu-m)
2561 *%-----|-----|
2560 *ADD HYD             NHYDsum=[ "S-1-D1S" ], NHYDs to add=[ "S-1-D1J"+"S-1-D1N" ]
2561 *%-----|-----|
2562 *ROUTE RESERVOIR    NHYDout=[ "S-1-D1R" ] ,NHYDin=[ "S-1-D1S" ] ,
2563 *          RDT=[ 1 ](min),
2564 *          TABLE of ( OUTFLOW-STORAGE ) values
2565 *          (cms) - (ha-m)
2566 *          [ 0.0      , 0.0   ]
2567 *          [ 0.2590 , 0.8642 ]
2568 *          [      -1 ,      -1   ] (max twenty pts)
2569 *          NHYDovf=[ "S-1-D1Rovf" ]
2570 *%-----|-----|
2571 *      -JFSA 2021-02-25 "S-1-D2" and "S-1-D3" are part of S-1 sub-catchment. They are
2572 moved to drain before station 6215 on Jock River
2572 *CONTINUOUS STANDHYD NHYD=[ "S-1-D2" ], DT=[ 1 ](min), AREA=[ 18.67 ](ha), XIMP=[ 0.65 ],
2573 TIMP=[ 0.65 ], DWF=[ 0 ](cms),
2573 *          LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
2574 IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%),
2574 *          LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min), Impervious surfaces:
2575 IAimp=[ 1.57 ](mm), SLPI=[ 0.75 ](%),
2575 *          LGI=[ 352.798 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
2576 *          Continuous simulation parameters:
2577 *          IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
2578 *          SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2579 *          InterEventTime=[ 12 ](hrs), END=-1
2580 *%-----|-----|
2581 *CONTINUOUS NASHYD    NHYD=[ "S-1-D2" ], DT=[ 1 ]min, AREA=[ 18.67 ](ha),
2582 *          DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
2583 *          N=[ 3 ], TP=[ 1.120 ]hrs,
2584 *          Continuous simulation parameters:
2585 *          IaRECper=[ 4 ](hrs),
2586 *          SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2587 *          InterEventTime=[ 12 ](hrs)
2588 *          Baseflow simulation parameters:
2589 *          BaseFlowOption=[ 1 ],
2590 *          InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2591 *          VHdCond=[ 0.055 ](mm/hr), END=-1
2592 *%-----|-----|
2593 *COMPUTE DUALHYD      NHYDin=[ "S-1-D2" ], CINLET=[ 2.062 ](cms), NINLET=[ 1 ],
2594 *          MajNHYD=[ "S-1-D2J" ]
2595 *          MinNHYD=[ "S-1-D2N" ]
2596 *          TMJSTO=[ 9999999 ](cu-m)
2597 *%-----|-----|
2598 *ADD HYD              NHYDsum=[ "S-1-D2S" ], NHYDs to add=[ "S-1-D2J"+"S-1-D2N" ]
2599 *%-----|-----|
2600 *ROUTE RESERVOIR     NHYDout=[ "S-1-D2R" ] ,NHYDin=[ "S-1-D2S" ] ,
2601 *          RDT=[ 1 ](min),
2602 *          TABLE of ( OUTFLOW-STORAGE ) values
2603 *          (cms) - (ha-m)
2604 *          [ 0.0      , 0.0   ]
2605 *          [ 0.2231 , 0.7445 ]
2606 *          [      -1 ,      -1   ] (max twenty pts)
2607 *          NHYDovf=[ "S-1-D2Rovf" ]
2608 *%-----|-----|
2609 *CONTINUOUS STANDHYD NHYD=[ "S-1-D3" ], DT=[ 1 ](min), AREA=[ 6.79 ](ha), XIMP=[ 0.65 ],
2610 TIMP=[ 0.65 ], DWF=[ 0 ](cms),
2610 *          LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
2611 IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%),
2611 *          LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min), Impervious surfaces:
2612 IAimp=[ 1.57 ](mm), SLPI=[ 0.75 ](%),
2612 *          LGI=[ 212.760 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
2613 *          Continuous simulation parameters:

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2614 *
2615 *
2616 *
2617 *%-----|-----|-----|-----|-----|-----|-----|-----|-----|
2618 *CONTINUOUS NASHYD NHYD=[ "S-1-D3" ], DT=[1]min, AREA=[6.79](ha),
2619 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2620 * N=[3], TP=[1.281]hrs,
2621 * Continuous simulation parameters:
2622 * IaRECper=[4](hrs),
2623 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2624 * InterEventTime=[12](hrs)
2625 * Baseflow simulation parameters:
2626 * BaseFlowOption=[1],
2627 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2628 * VHdCond=[0.055](mm/hr), END=-1
2629 *%-----|-----|-----|-----|-----|-----|-----|-----|-----|
2630 *COMPUTE DUALHYD NHYDin=[ "S-1-D3" ], CINLET=[0.719](cms), NINLET=[1],
2631 * MajNHYD=[ "S-1-D3J" ]
2632 * MinNHYD=[ "S-1-D3N" ]
2633 * TMJSTO=[9999999](cu-m)
2634 *%-----|-----|-----|-----|-----|-----|-----|-----|-----|
2635 *ADD HYD NHYDsum=[ "S-1-D3S" ], NYHDS to add=[ "S-1-D3J" + "S-1-D3N" ]
2636 *%-----|-----|-----|-----|-----|-----|-----|-----|-----|
2637 *ROUTE RESERVOIR NYDout=[ "S-1-D3R" ], NYDin=[ "S-1-D3S" ],
2638 * RDT=[1](min),
2639 * TABLE of ( OUTFLOW-STORAGE ) values
2640 * (cms) - (ha-m)
2641 * [ 0.0 , 0.0 ]
2642 * [ 0.0811, 0.2708 ]
2643 * [ -1 , -1 ] (max twenty pts)
2644 * NYDovf=[ "S-1-D3Rovf" ]
2645 *%-----|-----|-----|-----|-----|-----|-----|-----|-----|
2646 *CONTINUOUS STANDHYD NYD=[ "S-1-D4" ], DT=[1](min), AREA=[3.28](ha), XIMP=[0.65],
2647 * TIMP=[0.65], DWF=[0](cms),
2648 * LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
2649 * IAperv=[4.67](mm), SLPP=[2.0](%),
2650 * LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
2651 * IAimp=[1.57](mm), SLPI=[0.75](%),
2652 * LGI=[147.874](m), MNI=[0.013], SCI=[0](min),
2653 * Continuous simulation parameters:
2654 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
2655 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2656 * InterEventTime=[12](hrs), END=-1
2657 *%-----|-----|-----|-----|-----|-----|-----|-----|-----|
2658 *CONTINUOUS NASHYD NYD=[ "S-1-D4" ], DT=[1]min, AREA=[3.28](ha),
2659 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2660 * N=[3], TP=[1.10]hrs,
2661 * Continuous simulation parameters:
2662 * IaRECper=[4](hrs),
2663 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2664 * InterEventTime=[12](hrs)
2665 * Baseflow simulation parameters:
2666 * BaseFlowOption=[1],
2667 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2668 * VHdCond=[0.055](mm/hr), END=-1
2669 *%-----|-----|-----|-----|-----|-----|-----|-----|-----|
2670 *COMPUTE DUALHYD NYDin=[ "S-1-D4" ], CINLET=[0.373](cms), NINLET=[1],
2671 * MajNHYD=[ "S-1-D4J" ]
2672 * MinNHYD=[ "S-1-D4N" ]
2673 * TMJSTO=[9999999](cu-m)
2674 *%-----|-----|-----|-----|-----|-----|-----|-----|-----|
2675 *ADD HYD NYDsum=[ "S-1-D4S" ], NYHDS to add=[ "S-1-D4J" + "S-1-D4N" ]
2676 *%-----|-----|-----|-----|-----|-----|-----|-----|-----|
2677 *ROUTE RESERVOIR NYDout=[ "S-1-D4R" ], NYDin=[ "S-1-D4S" ],
2678 * RDT=[1](min),
2679 * TABLE of ( OUTFLOW-STORAGE ) values

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2677 *                               (cms) - (ha-m)
2678 *                               [ 0.0      , 0.0 ]
2679 *                               [ 0.0392, 0.1308 ]
2680 *                               [     -1 ,   -1     ] (max twenty pts)
2681 *                               NHYDovf=[ "S-1-D4Rovf" ]
2682 *%-----|-----|
2683 *CONTINUOUS STANDHYD NHYD=[ "S-1-D5" ], DT=[1](min), AREA=[12.84](ha), XIMP=[0.65],
2684 TIMP=[0.65], DWF=[0](cms),
2685 *
2686 *                               LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min), Impervious surfaces:
2687 *                               IAimp=[ 1.57 ](mm), SLPI=[ 0.75 ](%),
2688 *                               LGI=[ 292.57 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
2689 *                               Continuous simulation parameters:
2690 *                               IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
2691 *                               SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2692 *                               InterEventTime=[ 12 ](hrs), END=-1
2693 *%-----|-----|
2694 *CONTINUOUS NASHYD NHYD=[ "S-1-D5" ], DT=[1]min, AREA=[12.84](ha),
2695 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2696 N=[3], TP=[1.10]hrs,
2697 Continuous simulation parameters:
2698 IaRECper=[ 4 ](hrs),
2699 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2700 InterEventTime=[ 12 ](hrs)
2701 Baseflow simulation parameters:
2702 BaseFlowOption=[ 1 ] ,
2703 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2704 VHydCond=[ 0.055 ](mm/hr), END=-1
2705 *%-----|-----|
2706 *COMPUTE DUALHYD NHYDin=[ "S-1-D5" ], CINLET=[ 1.395 ](cms), NINLET=[ 1 ],
2707 *                               MajNHYD=[ "S-1-D5J" ]
2708 *                               MinNHYD=[ "S-1-D5N" ]
2709 *                               TMJSTO=[ 9999999 ](cu-m)
2710 *%-----|-----|
2711 *ADD HYD NHYDsum=[ "S-1-D5S" ], NHYDs to add=[ "S-1-D5J" +"S-1-D5N" ]
2712 *%-----|-----|
2713 *ROUTE RESERVOIR NHYDout=[ "S-1-D5R" ] ,NHYDin=[ "S-1-D5S" ] ,
2714 *                               RDT=[ 1 ](min),
2715 *                               TABLE of ( OUTFLOW-STORAGE ) values
2716 *                               (cms) - (ha-m)
2717 *                               [ 0.0      , 0.0 ]
2718 *                               [     -1 ,   -1     ] (max twenty pts)
2719 *                               NHYDovf=[ "S-1-D5Rovf" ]
2720 *%-----|-----|
2721 *CONTINUOUS STANDHYD NHYD=[ "S-1-D6" ], DT=[1](min), AREA=[1.75](ha), XIMP=[0.65],
2722 TIMP=[0.65], DWF=[0](cms),
2723 *                               LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
2724 *                               IApert=[ 4.67 ](mm), SLPP=[ 2.0 ](%),
2725 *                               LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min), Impervious surfaces:
2726 *                               IAimp=[ 1.57 ](mm), SLPI=[ 0.75 ](%),
2727 *                               LGI=[ 108.01 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
2728 *                               Continuous simulation parameters:
2729 *                               IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
2730 *                               SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2731 *                               InterEventTime=[ 12 ](hrs), END=-1
2732 *%-----|-----|
2733 *CONTINUOUS NASHYD NHYD=[ "S-1-D6" ], DT=[1]min, AREA=[1.75](ha),
2734 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2735 N=[3], TP=[1.10]hrs,
2736 Continuous simulation parameters:
2737 IaRECper=[ 4 ](hrs),
2738 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2739 InterEventTime=[ 12 ](hrs)
2740 Baseflow simulation parameters:

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2737 BaseFlowOption=[1] ,
2738 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2739 VHydCond=[0.055](mm/hr), END=-1
2740 *%-----|-----|
2741 *COMPUTE DUALHYD NHYDin=[ "S-1-D6" ], CINLET=[ 0.218 ](cms), NINLET=[ 1 ],
2742 *
2743 *
2744 * MajNHYD=[ "S-1-D6J" ]
2745 * MinNHYD=[ "S-1-D6N" ]
2746 * TMJSTO=[ 99999999 ](cu-m)
2747 *%-----|-----|
2748 *ADD HYD NHYDsum=[ "S-1-D6S" ], NHYDs to add=[ "S-1-D6J"+"S-1-D6N" ]
2749 *%-----|-----|
2750 *ROUTE RESERVOIR NHYDout=[ "S-1-D6R" ], NHYDin=[ "S-1-D6S" ],
2751 * RDT=[ 1 ](min),
2752 * TABLE of ( OUTFLOW-STORAGE ) values
2753 * (cms) - (ha-m)
2754 * [ 0.0 , 0.0 ]
2755 * [ 0.0209, 0.0698 ]
2756 * [ -1 , -1 ] (max twenty pts)
2757 * NHYDovf=[ "S-1-D6Rovf" ]
2758 *%-----|-----|
2759 *CONTINUOUS STANDHYD NHYD=[ "S-1-D7" ], DT=[ 1 ](min), AREA=[ 2.03 ](ha), XIMP=[ 0.65 ],
2760 * TIMP=[ 0.65 ], DWF=[ 0 ](cms),
2761 * LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
2762 * IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%),
2763 *
2764 * LGI=[ 116.33 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
2765 * Continuous simulation parameters:
2766 * IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
2767 * SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2768 * InterEventTime=[ 12 ](hrs), END=-1
2769 *%-----|-----|
2770 *CONTINUOUS NASHYD NHYD=[ "S-1-D7" ], DT=[ 1 ]min, AREA=[ 2.03 ](ha),
2771 * DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
2772 * N=[ 3 ], TP=[ 1.10 ]hrs,
2773 * Continuous simulation parameters:
2774 * IaRECper=[ 4 ](hrs),
2775 * SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2776 * InterEventTime=[ 12 ](hrs)
2777 * Baseflow simulation parameters:
2778 * BaseFlowOption=[ 1 ],
2779 * InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2780 * VHydCond=[ 0.055 ](mm/hr), END=-1
2781 *%-----|-----|
2782 *COMPUTE DUALHYD NHYDin=[ "S-1-D7" ], CINLET=[ 2.279 ](cms), NINLET=[ 1 ],
2783 * MajNHYD=[ "S-1-D7J" ]
2784 * MinNHYD=[ "S-1-D7N" ]
2785 * TMJSTO=[ 99999999 ](cu-m)
2786 *%-----|-----|
2787 *ADD HYD NHYDsum=[ "S-1-D7S" ], NHYDs to add=[ "S-1-D7J"+"S-1-D7N" ]
2788 *%-----|-----|
2789 *ROUTE RESERVOIR NHYDout=[ "S-1-D7R" ], NHYDin=[ "S-1-D7S" ],
2790 * RDT=[ 1 ](min),
2791 * TABLE of ( OUTFLOW-STORAGE ) values
2792 * (cms) - (ha-m)
2793 * [ 0.0 , 0.0 ]
2794 * [ 0.0243, 0.0810 ]
2795 * [ -1 , -1 ] (max twenty pts)
2796 * NHYDovf=[ "S-1-D8Rovf" ]
2797 *%-----|-----|
2798 * -JFSA 2021-02-26 "S-1-D8" is a part of S-1 sub-catchment. It is moved to drain
2799 before station 6016 on Jock River
2800 *CONTINUOUS STANDHYD NHYD=[ "S-1-D8" ], DT=[ 1 ](min), AREA=[ 5.27 ](ha), XIMP=[ 0.65 ],
2801 * TIMP=[ 0.65 ], DWF=[ 0 ](cms),
2802 * LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
2803 * IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%),

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2797 * LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
2798 IAimp=[1.57](mm), SLPI=[0.75](%),
2799 * LGI=[187.439](m), MNI=[0.013], SCI=[0](min),
2800 * Continuous simulation parameters:
2801 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
2802 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2803 * InterEventTime=[12](hrs), END=-1
2804 *%----- | -----
2805 *CONTINUOUS NASHYD NHYD=[ "S-1-D8" ], DT=[1]min, AREA=[5.27](ha),
2806 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2807 * N=[3], TP=[1.10]hrs,
2808 * Continuous simulation parameters:
2809 * IaRECper=[4](hrs),
2810 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2811 * InterEventTime=[12](hrs)
2812 * Baseflow simulation parameters:
2813 * BaseFlowOption=[1],
2814 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2815 * VHydCond=[0.055](mm/hr), END=-1
2816 *%----- | -----
2817 *COMPUTE DUALHYD NHYDin=[ "S-1-D8" ], CINLET=[2.279](cms), NINLET=[1],
2818 * MajNHYD=[ "S-1-D8J" ]
2819 * MinNHYD=[ "S-1-D8N" ]
2820 * TMJSTO=[ 9999999 ](cu-m)
2821 *%----- | -----
2822 *ADD HYD NHYDsum=[ "S-1-D8S" ], NHYDs to add=[ "S-1-D8J"+ "S-1-D8N" ]
2823 *%----- | -----
2824 *ADD HYD NHYDsum=[ "S-1-D" ], NHYDs to add=[ "S-1-Okeefe"+ "S-1"+ "S-1-Fost" ]
2825 *%----- | -----
2826 *COMPUTE DUALHYD NHYDin=[ "S-1-D" ], CINLET=[11.616](cms), NINLET=[1],
2827 * MajNHYD=[ "S-1-D-MJ" ]
2828 * MinNHYD=[ "S-1-D-MN" ]
2829 * TMJSTO=[ 5974 ](cu-m)
2830 *%----- | -----
2831 *ADD HYD NHYDsum=[ "S-1-DEV" ], NHYDs to add=[ "S-1-D-MJ"+ "S-1-D-MN" ]
2832 *%----- | -----
2833 *ROUTE RESERVOIR NHYDout=[ "S-1-D8R" ], NHYDin=[ "S-1-D8S" ],
2834 * RDT=[1](min),
2835 * TABLE of ( OUTFLOW-STORAGE ) values
2836 * (cms) - (ha-m)
2837 * [ 0.0 , 0.0 ]
2838 * [ 0.0630 , 0.2102 ]
2839 * [ -1 , -1 ] (max twenty pts)
2840 * NHYDovf=[ "S-1-D8Rovf" ]
2841 *%----- | -----
2842 * -JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
2843 * (W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
2844 *# Catchment W_CLAR
2845 *# - To West Clarke Drain (south of the Jock)
2846 *# - Subdivision with 43% imp. as per Barrhaven South MSS
2847 *# - 2020-11-30 update CLARKE Tributary Drainage Area to = 121 ha based on
2848 *# P598(04)-11
2849 *# - 2020-11-30 split CLARKE Drainage Area to MAJOR and ALL
2850 *# ****
2851 *CONTINUOUS STANDHYD NHYD=[ "W_CLAR_MJ" ], DT=[1]min, AREA=[1.772](ha),
2852 XIMP=[0.46], TIMP=[0.59], DWF=[0](cms), LOSS=[2],
2853 SCS curve number CN=[77],
2854 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
2855 LGP=[40](m), MNP=[0.25], SCP=[0](min),
2856 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
2857 LGI=[109](m), MNI=[0.013], SCI=[0](min),
2858 Continuous simulation parameters:
2859 IaRECper=[4](hrs), IaRECImp=[4](hrs),
2860 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2861 InterEventTime=[18](hrs), END=-1

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2860 *%-----|-----|
2861 *COMPUTE DUALHYD      NHYDin= [ "W_CLAR_MJ" ] , CINLET=[ 0.213 ](cms) , NINLET=[ 1 ] ,
2862 *          MajNHYD= [ "W_CLAR_MJj" ]
2863 *          MinNHYD= [ "W_CLAR_MJn" ]
2864 *          TMJSTO=[ 0.1 ](cu-m)
2865 *%-----|-----|
2866 *# 5-Year + 12% Capture
2867 ROUTE RESERVOIR      NHYDout= [ "W_CLAR_MJn" ] , NHYDin= [ "W_CLAR_MJ" ] ,
2868 RDT=[ 1 ](min),
2869           TABLE of ( OUTFLOW-STORAGE ) values
2870           (cms) - (ha-m)
2871           [ 0.0 , 0.0 ]
2872           [ 0.213 , 0.0001 ]
2873           [ -1 , -1 ] (max twenty pts)
2874           NHYDovf= [ "W_CLAR_MJj" ] ,
2875 *%-----|-----|
2876 *      -Clarke_All area from P 598(04)-11 = 120.207 ha, change to 127.298 ha based on
2877 GIS measurements,
2878 *      -JFSA, 2021-01-19 update W_CLAR_ALL to (121.17-1.772=119.398) ha based on GIS
2879 measurements W_CLAR is 121.17 ha and W_CLAR_MJ is 1.772 ha
2880 CONTINUOUS STANDHYD NHYD= [ "W_CLAR_ALL" ] , DT=[ 1 ]min, AREA=[ 119.398 ](ha) ,
2881 XIMP=[ 0.60 ] , TIMP=[ 0.65 ] , DWF=[ 0 ](cms) , LOSS=[ 2 ] ,
2882 SCS curve number CN=[ 77 ] ,
2883 Previous surfaces: IAper=[ 4.67 ](mm) , SLPP=[ 1 ](%) ,
2884 LGP=[ 40 ](m) , MNP=[ 0.25 ] , SCP=[ 0 ](min) ,
2885 Impervious surfaces: IAimp=[ 1.57 ](mm) , SLPI=[ 1 ](%) ,
2886 LGI=[ 892.18 ](m) , MNI=[ 0.013 ] , SCI=[ 0 ](min) ,
2887 Continuous simulation parameters:
2888 IaRECper=[ 4 ](hrs) , IaRECImp=[ 4 ](hrs) ,
2889 SMIN=[ -1 ](mm) , SMAX=[ -1 ](mm) , SK=[ 0.010 ]/(mm) ,
2890 InterEventTime=[ 18 ](hrs) , END=-1
2891 *%-----|-----|
2892 ADD HYD      NHYDs[ "W_CLAR" ] , NHYDs to add= [ "W_CLAR_ALL"+ "W_CLAR_MJj" ]
2893 *%-----|-----|
2894 SAVE HYD      NHYD= [ "W_CLAR" ] , # OF PCYCLES=[ -1 ] , ICASEsh=[ 1 ]
2895           HYD_COMMENT=[ "Total Flows to West Clarke" ]
2896 *#*****#
2897 *#      West Clarke Pond 2
2898 *#      - Rating curve obtained from Barrhaven South MSS modeling
2899 *#      - Tributary Drainage Area to MSS Pond 2 = 241 ha
2900 *#*****#
2901 ROUTE RESERVOIR      NHYDout= [ "MS_P2" ] , NHYDin= [ "W_CLAR" ] ,
2902 RDT=[ 1 ](min),
2903           TABLE of ( OUTFLOW-STORAGE ) values
2904           (cms) - (ha-m)
2905           [ 0.0 , 0.0 ]
2906           [ 0.128 , 0.161 ]
2907           [ 0.138 , 0.409 ]
2908           [ 0.148 , 0.68 ]
2909           [ 0.227 , 0.931 ]
2910           [ 0.354 , 1.223 ]
2911           [ 0.505 , 1.52 ]
2912           [ 0.666 , 1.821 ]
2913           [ 0.831 , 2.123 ]
2914           [ 0.995 , 2.434 ]
2915           [ 1.069 , 2.583 ]
2916           [ 1.51 , 2.647 ]
2917           [ 4.904 , 2.861 ]
2918           [ 13.048 , 3.188 ]
2919           [ 23.745 , 3.523 ]
2920           [ 36.474 , 3.871 ]
2921           [ 45.938 , 4.127 ]
2922           [ 61.652 , 4.539 ]
2923           [ -1 , -1 ] (max twenty pts)
2924           NHYDovf= [ "P2-OVF" ]
2925 *%-----|-----|

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2924 ****
2925 *      -JFSA, 2021-01-22 "W_CLAR_UNDE" (west of Clarke sub-catchment) discharges
2926 directly to the jock river through a road side ditch on the west side of Borrisokane
2927 road (station 6016)
2928 *CONTINUOUS NASHYD   NHYD=[ "W_CLAR_UNDE" ], DT=[1]min, AREA=[35.65](ha),
2929 *                                DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2930 *                                N=[3], TP=[1.10]hrs,
2931 *                                Continuous simulation parameters:
2932 *                                IaRECper=[4](hrs),
2933 *                                SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2934 *                                InterEventTime=[12](hrs)
2935 *                                Baseflow simulation parameters:
2936 *                                BaseFlowOption=[1],
2937 *                                InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2938 *                                VHdCond=[0.055](mm/hr), END=-1
2939 *%
2940 ADD HYD          NHYDssum=[ "SN_CE" ], NHYDs to add=[ "N_CE" +
2941 *                                +"S-1-D4" +"S-1-D5" +"MS_P2" +"P2-OVF" ]
2942 *%
2943 SAVE HYD         NHYD=[ "SN_CE" ], # OF PCYCLES=[-1], ICASEsh=[1]
2944 *                                HYD_COMMENT=[ "Total Flows before Station 5737 on Jock River" ]
2945 *%
2946 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5737
2947 *# JFSA 2021-02-25 add station 5737 before station 5002. Station 5737 was extracted
2948 from the HEC-RAS model
2949 T:\PROJ\1474-16\Design\20201026-QuantityControlAnalysis\HEC-RAS\JockLidar2005
2950 *# JFSA 2021-03-02 change the slope to 0.1% instead of 0.0175 to stabilize the model
2951 ROUTE CHANNEL    NHYDout=[ "5737" ] ,NHYDin=[ "SN_CE" ],
2952 *                                RDT=[1](min),
2953 *                                CHLGTH=[270](m), CHSLOPE=[0.0175](%),
2954 *                                FPSLOPE=[0.0175](%),
2955 *                                SECNUM=[1.0], NSEG=[3]
2956 *                                ( SEGROUGH, SEGDIST (m))=
2957 *                                [0.050,-24.04
2958 *                                -0.035,23.92
2959 *                                0.050,1130.8] NSEG times
2960 *                                ( DISTANCE (m), ELEVATION (m))=
2961 *                                [-1060.52, 94 ]
2962 *                                [-268.6, 91.5 ]
2963 *                                [-259.43, 91.5 ]
2964 *                                [-179.48, 91.5 ]
2965 *                                [-67.9, 91.5 ]
2966 *                                [-59.21, 91.5 ]
2967 *                                [-33.19, 91 ]
2968 *                                [-26.08, 90.5 ]
2969 *                                [-24.04, 90 ]
2970 *                                [-13.14, 86.77 ]
2971 *                                [0, 85 ]
2972 *                                [14.68, 86.74 ]
2973 *                                [23.92, 90 ]
2974 *                                [25.78, 90.5 ]
2975 *                                [31.91, 91 ]
2976 *                                [91.95, 91.5 ]
2977 *                                [772.15, 92 ]
2978 *                                [961.49, 92.5 ]
2979 *                                [1044.69, 93 ]
2980 *                                [1130.8, 95 ]
2981 *%
2982 ADD HYD          NHYDssum=[ "5002" ], NHYDs to add=[ "5737" +
2983 *                                +"S-1-D1" +"S-1-D6" +"S-1-D7" ]
2984 *%
2985 SAVE HYD         NHYD=[ "5002" ], # OF PCYCLES=[-1], ICASEsh=[1]
2986 *                                HYD_COMMENT=[ "Total Flows before Station 5002 on Jock River" ]
2987 *%
2988 *# Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain
2989 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5002

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2986 *# JFSA 2021-02-19 Change the slope from 0.01 % (as per Stantec Report 2007) to 0.0255
% so the model will be more stable and give reasonable results. It is justifiable as
ROUTE CHANNELs aren't well suited to really flat slopes.
2987 *# JFSA 2021-02-19 Change to three ROUTE CHANNEL with length 275 m each instead of one
with 825 m length so the model will be more stable
2988 *# JFSA 2021-02-26 change the length of 5002 route channel from 825 m to 736 m. That is
because of adding station 5737 between station 6016 and station 5002. Then the length
from station 5737 to station 5002 is 736 m. Change the slope from 0.0255 % to 0.09511 %
2989 *
2990 ROUTE CHANNEL      NHYDout=[ "N_WCa" ] ,NHYDin=[ "5002" ] ,
2991             RDT=[1](min),
2992             CHLGTH=[245.33333](m),   CHSLOPE=[0.09511](%),
2993                                         FPSLOPE=[0.09511](%),
2994             SECNUM=[1.0],           NSEG=[3]
2995             ( SEGROUGH, SEGDIST (m))=
2996                 [0.050,-37.5
2997                 -0.035,37.50
2998                 0.050,157.05] NSEG times
2999             ( DISTANCE (m), ELEVATION (m))=
3000             [-601.81, 91.5]
3001             [-37.50, 90.00]
3002             [-19.61, 87.04]
3003             [0.00, 85.70]
3004             [14.87, 86.93]
3005             [37.50, 90.00]
3006             [38.54, 90.50]
3007             [42.23, 91]
3008             [157.05,91.50]
3009             *
3010             [161.44, 91.50]
3011             *
3012             [236.48, 93.00]
3013             *
3014 ROUTE CHANNEL      NHYDout=[ "N_WCb" ] ,NHYDin=[ "N_WCa" ] ,
3015             RDT=[1](min),
3016             CHLGTH=[245.33333](m),   CHSLOPE=[0.09511](%),
3017                                         FPSLOPE=[0.09511](%),
3018             SECNUM=[1.0],           NSEG=[3]
3019             ( SEGROUGH, SEGDIST (m))=
3020                 [0.050,-37.5
3021                 -0.035,37.50
3022                 0.050,157.05] NSEG times
3023             ( DISTANCE (m), ELEVATION (m))=
3024             [-601.81, 91.5]
3025             [-37.50, 90.00]
3026             [-19.61, 87.04]
3027             [0.00, 85.70]
3028             [14.87, 86.93]
3029             [37.50, 90.00]
3030             [38.54, 90.50]
3031             [42.23, 91]
3032             [157.05,91.50]
3033             *
3034 ROUTE CHANNEL      NHYDout=[ "N_WC" ] ,NHYDin=[ "N_WCb" ] ,
3035             RDT=[1](min),
3036             CHLGTH=[245.33333](m),   CHSLOPE=[0.09511](%),
3037                                         FPSLOPE=[0.09511](%),
3038             SECNUM=[1.0],           NSEG=[3]
3039             ( SEGROUGH, SEGDIST (m))=
3040                 [0.050,-37.5
3041                 -0.035,37.50
3042                 0.050,157.05] NSEG times
3043             ( DISTANCE (m), ELEVATION (m))=
3044             [-601.81, 91.5]
3045             [-37.50, 90.00]
3046             [-19.61, 87.04]

```

```

3047 [0.00, 85.70]
3048 [14.87, 86.93]
3049 [37.50, 90.00]
3050 [38.54, 90.50]
3051 [42.23, 91]
3052 [157.05, 91.50]
3053 *#####
3054 * -JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
3055 (W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
3056 *ADD HYD NHYDsum=[ "SN_WC" ], NHYDs to
3057 add=[ "MS_P2" +"P2-OVF" +"N_WC" +"W_CLAR_UNDE" ]
3058 *%-----|-----|
3059 *SAVE HYD NHYD=[ "SN_WC" ], # OF PCYCLES=[-1], ICASEsh=[1]
3060 * HYD_COMMENT=[ "Total Flows at West Clarke Pond Outlet" ]
3061 *# Hydrograph from Node West Clarke routed to Node at Kennedy - Burnett Drain
3062 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4534
3063 *#
3064 ROUTE CHANNEL NHYDout=[ "N_KB" ] , NHYDin=[ "N_WC" ] ,
3065 RDT=[1](min),
3066 CHLGTH=[1020](m), CHSLOPE=[0.0498](%),
3067 FPSLOPE=[0.0498](%),
3068 SECNUM=[1.0], NSEG=[3]
3069 ( SEGROUGH, SEGDIST (m))=
3070 [0.050,-23.63
3071 -0.035,23.63
3072 0.050,728.3] NSEG times
3073 ( DISTANCE (m), ELEVATION (m))=
3074 [-1082.01,94]
3075 [-1028.17,92.5]
3076 [-992.3,93.5]
3077 [-279.34,90]
3078 [-23.63,90]
3079 [-13.45,87.13]
3080 [-0.07,86.24]
3081 [10.54,87.15]
3082 [23.63,90]
3083 [24.86,90.5]
3084 [26.72,91]
3085 [45.07,91.5]
3086 [128.17,91.5]
3087 [270.7,92.5]
3088 [728.3,95]
3089 *%-----|-----|
3090 *#####
3091 *# Catchment KEN_BU
3092 *# - To Kennedy-Burnett SWM Facility
3093 *# - Outlets to Fraser-Clarke drain (north of the Jock)
3094 *# - Medium density residential subdivision
3095 *# - Add Kennedy Burnett model (Convert PCSWMM from NOVATECH June, 2020 to SWMHYMO)
3096 *CONTINUOUS STANDHYD NHYD=[ "KEN_BU" ], DT=[1]min, AREA=[281](ha),
3097 * XIMP=[0.55], TIMP=[0.55], DWF=[0](cms), LOSS=[2],
3098 * SCS curve number CN=[71],
3099 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3100 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3101 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3102 * LGI=[1369](m), MNI=[0.013], SCI=[0](min),
3103 * Continuous simulation parameters:
3104 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
3105 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3106 * InterEventTime=[18](hrs), END=-1
3107 *%-----|-----|
3108 *#####
3109 *# Existing Kennedy-Burnett SWM Facility
3110 *# - Rating curve obtained from URTKBP

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3111 *#      - Tributary Drainage Area to Pond = 160 ha
3112 *#*****
3113 *ROUTE RESERVOIR      NHYDout=[ "KEN_P" ],   NHYDin=[ "KEN_BU" ],
3114 *                    RDT=[1](min),
3115 *                                TABLE of ( OUTFLOW-STORAGE ) values
3116 *                                (cms) - (ha-m)
3117 *                                [ 0.0 , 0.0 ]
3118 *                                [ 0.13 , 0.26 ]
3119 *                                [ 0.43 , 0.56 ]
3120 *                                [ 0.67 , 0.90 ]
3121 *                                [ 0.86 , 1.32 ]
3122 *                                [ 1.01 , 1.79 ]
3123 *                                [ 1.15 , 2.33 ]
3124 *                                [ -1 , -1 ] (max twenty pts)
3125 *                                NHYDovf=[ "KEN-OV" ]
3126 *%-----|-----|
3127 *      -JFSA, 2021-01-19 update all KEN_BU areas based on GIS measurements
3128 CONTINUOUS STANDHYD NHYD=[ "KB-01A" ], DT=[1]min, AREA=[40.82](ha), XIMP=[0.097],
3129 TIMP=[0.4], DWF=[0](cms), LOSS=[1]:
3130             Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3131             F=[0.00](mm),
3132             Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[40](m),
3133             MNP=[0.250], SCP=[0](min),
3134             Impervious areas: IAimp=[0.785](mm), SLPI=[0.5](%), LGI=[521.664](m),
3135             MNI=[0.013], SCI=[0](min),
3136             Continuous simulation parameters:
3137             IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
3138             END=-1
3139 *%-----|-----|
3140 COMPUTE DUALHYD NHYDin=[ "KB-01A" ], CINLET=[ 3.6 ](cms), NINLET=[ 1 ],
3141 MajNHYD=[ "KB-01A-MJ" ]
3142 MinNHYD=[ "KB-01A-MN" ]
3143 TMJSTO=[ 4995 ](cu-m)
3144 *%-----|-----|
3145 ADD HYD NHYDsum=[ "KB-01A-S" ], NHYDs to add=[ "KB-01A-MJ" +"KB-01A-MN" ]
3146 *%-----|-----|
3147 CONTINUOUS STANDHYD NHYD=[ "KB-01B" ], DT=[1]min, AREA=[31.1](ha), XIMP=[0.1875],
3148 TIMP=[0.375], DWF=[0](cms), LOSS=[1]:
3149             Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3150             F=[0.00](mm),
3151             Pervious areas: IAper=[4.67](mm), SLPP=[0.42](%), LGP=[40](m),
3152             MNP=[0.250], SCP=[0](min),
3153             Impervious areas: IAimp=[0.785](mm), SLPI=[0.42](%), LGI=[455.339](m),
3154             MNI=[0.013], SCI=[0](min),
3155             Continuous simulation parameters:
3156             IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
3157             END=-1
3158 *%-----|-----|
3159 COMPUTE DUALHYD NHYDin=[ "KB-01B" ], CINLET=[ 1.585 ](cms), NINLET=[ 1 ],
3160 MajNHYD=[ "KB-01B-MJ" ]
3161 MinNHYD=[ "KB-01B-MN" ]
3162 TMJSTO=[ 6075 ](cu-m)
3163 *%-----|-----|
3164 ADD HYD NHYDsum=[ "KB-01B-S" ], NHYDs to add=[ "KB-01B-MJ" +"KB-01B-MN" ]
3165 *%-----|-----|
3166 CONTINUOUS STANDHYD NHYD=[ "KB-01C" ], DT=[1]min, AREA=[13.78](ha), XIMP=[0.2045],
3167 TIMP=[0.409], DWF=[0](cms), LOSS=[1]:
3168             Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3169             F=[0.00](mm),
3170             Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3171             MNP=[0.250], SCP=[0](min),
3172             Impervious areas: IAimp=[0.785](mm), SLPI=[0.5](%), LGI=[303.095](m),
3173             MNI=[0.013], SCI=[0](min),
3174             Continuous simulation parameters:
3175             IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
3176             END=-1

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3162 *%
3163 COMPUTE DUALHYD      NHYDin=[ "KB-01C" ], CINLET=[1.35](cms), NINLET=[1],
3164                               MajNHYD=[ "KB-01C-MJ" ]
3165                               MinNHYD=[ "KB-01C-MN" ]
3166                               TMJSTO=[1880](cu-m)
3167 *%
3168 ADD HYD               NHYDsum=[ "KB-01C-S" ], NHYDs to add=[ "KB-01C-MJ" +"KB-01C-MN" ]
3169 *%
3170 CONTINUOUS STANDHYD   NHYD=[ "KB-03" ], DT=[1]min, AREA=[84.78](ha), XIMP=[0.197],
3171 TIMP=[0.394], DWF=[0](cms), LOSS=[1]:
3172                               Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3173                               F=[0.00](mm),
3174                               Previous areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3175                               MNP=[0.250], SCP=[0](min),
3176                               Impervious areas: IAimp=[0.785](mm), SLPI=[0.63](%),
3177                               LGI=[751.798](m), MNI=[0.013], SCI=[0](min),
3178                               Continuous simulation parameters:
3179                               IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
3180 END=-1
3181 *%
3182 COMPUTE DUALHYD       NHYDin=[ "KB-03" ], CINLET=[5.27](cms), NINLET=[1],
3183                               MajNHYD=[ "KB-03-MJ" ]
3184                               MinNHYD=[ "KB-03-MN" ]
3185                               TMJSTO=[15500](cu-m)
3186 *%
3187 ADD HYD               NHYDsum=[ "KB-03-S" ], NHYDs to add=[ "KB-03-MJ" +"KB-03-MN" ]
3188 *%
3189 CONTINUOUS STANDHYD   NHYD=[ "KB-04" ], DT=[1]min, AREA=[6.95](ha), XIMP=[0.85],
3190 TIMP=[0.85], DWF=[0](cms), LOSS=[1]:
3191                               Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3192                               F=[0.00](mm),
3193                               Previous areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3194                               MNP=[0.250], SCP=[0](min),
3195                               Impervious areas: IAimp=[0.942](mm), SLPI=[0.5](%),
3196                               LGI=[215.252](m), MNI=[0.013], SCI=[0](min),
3197                               Continuous simulation parameters:
3198                               IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
3199 END=-1
3200 *%
3201 COMPUTE DUALHYD       NHYDin=[ "KB-04" ], CINLET=[0.503](cms), NINLET=[1],
3202                               MajNHYD=[ "KB-04-MJ" ]
3203                               MinNHYD=[ "KB-04-MN" ]
3204                               TMJSTO=[1972](cu-m)
3205 *%
3206 ADD HYD               NHYDsum=[ "KB-04-S" ], NHYDs to add=[ "KB-04-MJ" +"KB-04-MN" ]
3207 *%
3208 CONTINUOUS STANDHYD   NHYD=[ "KB-05" ], DT=[1]min, AREA=[5.19](ha), XIMP=[0.93],
3209 TIMP=[0.93], DWF=[0](cms), LOSS=[1]:
3210                               Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3211                               F=[0.00](mm),
3212                               Previous areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3213                               MNP=[0.250], SCP=[0](min),
3214                               Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
3215                               LGI=[186.011](m), MNI=[0.013], SCI=[0](min),
3216                               Continuous simulation parameters:
3217                               IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
3218 END=-1
3219 *%
3220 *%
3221 CONTINUOUS STANDHYD   NHYD=[ "KB-06" ], DT=[1]min, AREA=[12.93](ha), XIMP=[0.873],
3222 TIMP=[0.873], DWF=[0](cms), LOSS=[1]:
3223                               Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3224                               F=[0.00](mm),
3225                               Previous areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3226                               MNP=[0.250], SCP=[0](min),
3227                               Impervious areas: IAimp=[0.942](mm), SLPI=[4.75](%),

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3210 LGI=[293.598](m), MNI=[0.013], SCI=[0](min),
3211 Continuous simulation parameters:
3212 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
3213 END=-1
3214 *%-----|-----|
3215 COMPUTE DUALHYD NHYDin=[ "KB-06" ], CINLET=[ 2.262 ](cms), NINLET=[ 1 ],
3216 MajNHYD=[ "KB-06-MJ" ]
3217 MinNHYD=[ "KB-06-MN" ]
3218 TMJSTO=[1950](cu-m)
3219 *%-----|-----|
3220 ADD HYD NHYDsum=[ "KB-06-S" ], NHYDs to add=[ "KB-06-MJ" +"KB-06-MN" ]
3221 *%-----|-----|
3222 CONTINUOUS STANDHYD NHYD=[ "KB-11" ], DT=[1]min, AREA=[ 4.03 ](ha), XIMP=[ 0.675 ],
3223 TIMP=[ 0.675 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3224 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3225 F=[ 0.00 ](mm),
3226 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3227 MNP=[ 0.250 ], SCP=[ 0 ](min),
3228 Impervious areas: IAimp=[ 0.785 ](mm), SLPI=[ 2.0 ](%),
3229 LGI=[ 163.911 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3230 Continuous simulation parameters:
3231 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3232 END=-1
3233 *%-----|-----|
3234 COMPUTE DUALHYD NHYDin=[ "KB-11" ], CINLET=[ 0.5773 ](cms), NINLET=[ 1 ],
3235 MajNHYD=[ "KB-11-MJ" ]
3236 MinNHYD=[ "KB-11-MN" ]
3237 TMJSTO=[ 597 ](cu-m)
3238 *%-----|-----|
3239 ADD HYD NHYDsum=[ "KB-11-S" ], NHYDs to add=[ "KB-11-MJ" +"KB-11-MN" ]
3240 *%-----|-----|
3241 CONTINUOUS STANDHYD NHYD=[ "S1" ], DT=[1]min, AREA=[ 4.99 ](ha), XIMP=[ 0.93 ],
3242 TIMP=[ 0.93 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3243 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3244 F=[ 0.00 ](mm),
3245 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3246 MNP=[ 0.250 ], SCP=[ 0 ](min),
3247 Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 2.0 ](%),
3248 LGI=[ 182.392 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3249 Continuous simulation parameters:
3250 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3251 END=-1
3252 *%-----|-----|
3253 *%-----|-----|
3254 ADD HYD NHYDsum=[ "KB-P1" ], NHYDs to
3255 add=[ "KB-01A-S" +"KB-01B-S" +"KB-01C-S" +"KB-03-S" +"KB-04-S" +"KB-05" +"KB-06-S" +"KB-11-S" +"KB
3256 -15 " +"S1" ]
3257 *%-----|-----|
3258 ROUTE RESERVOIR NHYDout=[ "KB-P1R" ], NHYDin=[ "KB-P1" ],
3259 RDT=[ 1 ](min),
3260 TABLE of ( OUTFLOW-STORAGE ) values
3261 (cms) - (ha-m)
3262 [ 0.0 , 0.0 ]
3263 [ 0.076, 0.003 ]

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3257 [0.088,0.006]
3258 [0.136,0.011]
3259 [0.301,0.017]
3260 [0.454,0.027]
3261 [0.631,0.041]
3262 [1.173,0.068]
3263 [1.91,0.111]
3264 [4.847,0.231]
3265 [9.813,0.436]
3266 [12.134,0.617]
3267 [12.438,0.732]
3268 [12.424,0.811]
3269 [12.425,0.894]
3270 [-1,-1] (max twenty pts)
3271 NHYDovf=[ "KB-Plovf" ]
3272 *%-----|-----|
3273 ADD HYD NHYDsum=[ "KB-Pond1" ], NHYDs to add=[ "KB-P1R"+"KB-Plovf" ]
3274 *%-----|-----|
3275 SAVE HYD NHYD=[ "KB-Pond1" ], # OF PCYCLES=[-1], ICASEsh=[1]
3276 HYD_COMMENT=[ "Total Flows at KB first pond" ]
3277 *%-----|-----|
3278 CONTINUOUS STANDHYD NHYD=[ "KB-07" ], DT=[1]min, AREA=[10.86](ha), XIMP=[0.86],
3279 TEMP=[0.86], DWF=[0](cms), LOSS=[1]:
3280 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3281 F=[0.00](mm),
3282 Previous areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3283 MNP=[0.250], SCP=[0](min),
3284 Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%),
3285 LGI=[269.072](m), MNI=[0.013], SCI=[0](min),
3286 Continuous simulation parameters:
3287 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
3288 END=-1
3289 *%-----|-----|
3290 COMPUTE DUALHYD NHYDin=[ "KB-07" ], CINLET=[2.094](cms), NINLET=[1],
3291 MajNHYD=[ "KB-07-MJ" ]
3292 MinNHYD=[ "KB-07-MN" ]
3293 TMJSTO=[1378](cu-m)
3294 *%-----|-----|
3295 ADD HYD NHYDsum=[ "KB-07-S" ], NHYDs to add=[ "KB-07-MJ"+"KB-07-MN" ]
3296 *%-----|-----|
3297 CONTINUOUS STANDHYD NHYD=[ "KB-08" ], DT=[1]min, AREA=[6.61](ha), XIMP=[0.64],
3298 TEMP=[0.64], DWF=[0](cms), LOSS=[1]:
3299 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3300 F=[0.00](mm),
3301 Previous areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3302 MNP=[0.250], SCP=[0](min),
3303 Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%),
3304 LGI=[209.921](m), MNI=[0.013], SCI=[0](min),
3305 Continuous simulation parameters:
3306 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
3307 END=-1
3308 *%-----|-----|
3309 COMPUTE DUALHYD NHYDin=[ "KB-08" ], CINLET=[1.058](cms), NINLET=[1],
3310 MajNHYD=[ "KB-08-MJ" ]
3311 MinNHYD=[ "KB-08-MN" ]
3312 TMJSTO=[787](cu-m)
3313 *%-----|-----|
3314 ADD HYD NHYDsum=[ "KB-08-S" ], NHYDs to add=[ "KB-08-MJ"+"KB-08-MN" ]
3315 *%-----|-----|
3316 CONTINUOUS STANDHYD NHYD=[ "KB-09" ], DT=[1]min, AREA=[2.6](ha), XIMP=[0.86],
3317 TEMP=[0.86], DWF=[0](cms), LOSS=[1]:
3318 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3319 F=[0.00](mm),
3320 Previous areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3321 MNP=[0.250], SCP=[0](min),
3322 Impervious areas: IAimp=[1.57](mm), SLPI=[2.0](%),

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3310 LGI=[131.656](m), MNI=[0.013], SCI=[0](min),
3311 Continuous simulation parameters:
3312 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
3313 END=-1
3314 *%-----|-----|
3315 *%-----|-----|
3316 CONTINUOUS STANDHYD NHYD=[ "KB-10_1" ], DT=[1]min, AREA=[ 2.37 ](ha), XIMP=[ 0.86 ],
3317 TIMP=[ 0.86 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3318 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3319 F=[ 0.00 ](mm),
3320 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3321 MNP=[ 0.250 ], SCP=[ 0 ](min),
3322 Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 2.0 ](%),
3323 LGI=[ 125.698 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3324 Continuous simulation parameters:
3325 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3326 END=-1
3327 *%-----|-----|
3328 *%-----|-----|
3329 CONTINUOUS STANDHYD NHYD=[ "KB-10_2" ], DT=[1]min, AREA=[ 1.14 ](ha), XIMP=[ 0.86 ],
3330 TIMP=[ 0.86 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3331 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3332 F=[ 0.00 ](mm),
3333 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3334 MNP=[ 0.250 ], SCP=[ 0 ](min),
3335 Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 2.0 ](%), LGI=[ 87.178 ](m),
3336 MNI=[ 0.013 ], SCI=[ 0 ](min),
3337 Continuous simulation parameters:
3338 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3339 END=-1
3340 *%-----|-----|
3341 COMPUTE DUALHYD NHYDin=[ "KB-12" ], CINLET=[ 0.8665 ](cms), NINLET=[ 1 ],
3342 MajNHYD=[ "KB-12-MJ" ]
3343 MinNHYD=[ "KB-12-MN" ]
3344 TMJSTO=[ 632 ](cu-m)
3345 *%-----|-----|
3346 ADD HYD NHYDsum=[ "KB-12-S" ], NHYDs to add=[ "KB-12-MJ" +"KB-12-MN" ]
3347 *%-----|-----|
3348 CONTINUOUS STANDHYD NHYD=[ "KB-13" ], DT=[1]min, AREA=[ 10.19 ](ha), XIMP=[ 0.64 ],
3349 TIMP=[ 0.64 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3350 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3351 F=[ 0.00 ](mm),
3352 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3353 MNP=[ 0.250 ], SCP=[ 0 ](min),
3354 Impervious areas: IAimp=[ 0.785 ](mm), SLPI=[ 2.0 ](%),
3355 LGI=[ 260.640 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3356 Continuous simulation parameters:
3357 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3358 END=-1
3359 *%-----|-----|
3360 COMPUTE DUALHYD NHYDin=[ "KB-13" ], CINLET=[ 1.722 ](cms), NINLET=[ 1 ],
3361 MajNHYD=[ "KB-13-MJ" ]
3362 MinNHYD=[ "KB-13-MN" ]
3363 TMJSTO=[ 1077 ](cu-m)

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3354 *%
3355 ADD HYD NHYDsum= [ "KB-13-S" ], NHYDs to add= [ "KB-13-MJ" +"KB-13-MN" ]
3356 *%
3357 CONTINUOUS STANDHYD NHYD=[ "KB-14" ], DT=[1]min, AREA=[ 5.47 ](ha), XIMP=[ 0.64 ],
3358 TIMP=[ 0.64 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3359 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3360 F=[ 0.00 ](mm),
3361 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3362 MNP=[ 0.250 ], SCP=[ 0 ](min),
3363 Impervious areas: IAimp=[ 0.785 ](mm), SLPI=[ 2.0 ](%),
3364 LGI=[ 190.962 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3365 Continuous simulation parameters:
3366 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3367 END=-1
3368 *%
3369 COMPUTE DUALHYD NHYDin=[ "KB-14" ], CINLET=[ 0.8734 ](cms), NINLET=[ 1 ],
3370 MajNHYD=[ "KB-14-MJ" ]
3371 MinNHYD=[ "KB-14-MN" ]
3372 TMJSTO=[ 631 ](cu-m)
3373 *%
3374 ADD HYD NHYDsum= [ "KB-14-S" ], NHYDs to add= [ "KB-14-MJ" +"KB-14-MN" ]
3375 *%
3376 *%
3377 CONTINUOUS STANDHYD NHYD=[ "KB-16_2" ], DT=[1]min, AREA=[ 3.42 ](ha), XIMP=[ 0.71 ],
3378 TIMP=[ 0.71 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3379 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3380 F=[ 0.00 ](mm),
3381 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3382 MNP=[ 0.250 ], SCP=[ 0 ](min),
3383 Impervious areas: IAimp=[ 0.157 ](mm), SLPI=[ 0.3 ](%),
3384 LGI=[ 150.997 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3385 Continuous simulation parameters:
3386 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3387 END=-1
3388 *%
3389 ADD HYD NHYDsum= [ "KB-P2" ], NHYDs to
3390 add= [ "KB-Pond1" +"KB-07-S" +"KB-08-S" +"KB-09" +"KB-10_1" +"KB-10_2" +"KB-12-S" +"KB-13-S" +"KB-1
3391 4-S" +"KB-16_2" ]
3392 *%
3393 ROUTE RESERVOIR NHYDout=[ "KB-P2R" ], NHYDin=[ "KB-P2" ],
3394 RDT=[ 1 ](min),
3395 TABLE of ( OUTFLOW-STORAGE ) values
3396 (cms) - (ha-m)
3397 [ 0.0 , 0.0 ]
3398 [ 0.053 , 0.005 ]
3399 [ 0.132 , 0.009 ]
3400 [ 0.269 , 0.014 ]
3401 [ 0.455 , 0.023 ]
3402 [ 0.699 , 0.037 ]
3403 [ 0.947 , 0.056 ]
3404 [ 1.853 , 0.09 ]
3405 [ 2.712 , 0.146 ]
3406 [ 6.626 , 0.287 ]
3407 [ 11.228 , 0.515 ]
3408 [ 14.885 , 0.738 ]
3409 [ 16.473 , 0.893 ]
3410 [ 17.311 , 0.998 ]
3411 [ 17.633 , 1.063 ]
3412 [ 17.634 , 1.112 ]
3413 [ -1 , -1 ] (max twenty pts)
3414 NHYDovf=[ "KB-P2ovf" ]
3415 *%
3416 ADD HYD NHYDsum= [ "KB-Pond2" ], NHYDs to add= [ "KB-P2R" +"KB-P2ovf" ]
3417 *%
3418 SAVE HYD NHYD=[ "KB-Pond2" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
3419 HYD_COMMENT=[ "Total Flows at KB second pond" ]

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3408 *%
3409 CONTINUOUS STANDHYD NHYD=[ "KB-16_1" ], DT=[1]min, AREA=[ 2.8 ](ha), XIMP=[ 0.75 ],
3410 TIMP=[ 0.75 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3411 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3412 F=[ 0.00 ](mm),
3413 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3414 MNP=[ 0.250 ], SCP=[ 0 ](min),
3415 Impervious areas: IAimp=[ 0.157 ](mm), SLPI=[ 0.3 ](%),
3416 LGI=[ 136.626 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3417 Continuous simulation parameters:
3418 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3419 END=-1
3420 *%
3421 ADD HYD NHYDsum=[ "KB-P3" ], NHYDs to add=[ "KB-Pond2" + "KB-16_1" ]
3422 *%
3423 *%
3424 * One inflow node from pond 3 is added to the model (ROUTE RESERVOIR)
3425 * Another inflow node from right side of pond 3 is not added to the model
3426 ROUTE RESERVOIR NHYDout=[ "KB-P3R" ], NHYDin=[ "KB-P3" ],
3427 RDT=[ 1 ](min),
3428 TABLE of ( OUTFLOW-STORAGE ) values
3429 (cms) - (ha-m)
3430 [ 0.0 , 0.0 ]
3431 [ 0.051, 0.002 ]
3432 [ 0.048, 0.003 ]
3433 [ 0.057, 0.029 ]
3434 [ 0.089, 0.045 ]
3435 [ 0.133, 0.069 ]
3436 [ 0.199, 0.106 ]
3437 [ 0.321, 0.172 ]
3438 [ 1.029, 0.306 ]
3439 [ 4.036, 0.527 ]
3440 [ 8.332, 0.761 ]
3441 [ 11.727, 0.941 ]
3442 [ 14.125, 1.067 ]
3443 [ 15.675, 1.149 ]
3444 [ 16.555, 1.196 ]
3445 [ 16.911, 1.214 ]
3446 [ -1 , -1 ] (max twenty pts)
3447 NHYDovf=[ "KB-P3ovf" ]
3448 *%
3449 ADD HYD NHYDsum=[ "KB-Pond3" ], NHYDs to add=[ "KB-P3R" + "KB-P3ovf" ]
3450 *%
3451 SAVE HYD NHYD= [ "KB-Pond3" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
3452 HYD_COMMENT=[ "Total Flows at KB third pond" ]
3453 *# **** EXISTING / PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118080), SWM
3454 Modeling Approach, NOVATECH Report June, 2020)
3455 *# - TO FRASER-CLARKE DRAIN
3456 *# ****
3457 CONTINUOUS STANDHYD NHYD=[ "FC-01" ], DT=[1]min, AREA=[ 8.03 ](ha), XIMP=[ 0.47 ],
3458 TIMP=[ 0.47 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3459 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3460 F=[ 0.00 ](mm),
3461 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3462 MNP=[ 0.250 ], SCP=[ 0 ](min),
3463 Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 1.0 ](%),
3464 LGI=[ 231.373 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3465 Continuous simulation parameters:
3466 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3467 END=-1
3468 *%
3469 COMPUTE DUALHYD NHYDin=[ "FC-01" ], CINLET=[ 0.756 ](cms), NINLET=[ 1 ],
3470 MajNHYD=[ "FC-01-MJ" ]
3471 MinNHYD=[ "FC-01-MN" ]

```

```

3463
3464
3465 *%-----| TMJSTO=[ 714](cu-m)
3466 ADD HYD | NHYDsum=[ "FC-01-S"], NHYDs to add=[ "FC-01-MJ"+"FC-01-MN"]
3467 *%-----| CONTINUOUS STANDHYD NHYD=[ "FC-02"], DT=[1]min, AREA=[16.05](ha), XIMP=[ 0.93],
3468 TEMP=[ 0.93], DWF=[ 0](cms), LOSS=[ 1]:
3469 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3470 F=[ 0.00](mm),
3471 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3472 MNP=[ 0.250], SCP=[ 0](min),
3473 Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 1.0](%), LGI=[ 327.109](m),
3474 MNI=[ 0.013], SCI=[ 0](min),
3475 Continuous simulation parameters:
3476 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3477 END=-1
3478 *%-----| COMPUTE DUALHYD NHYDin=[ "FC-02"], CINLET=[ 1.159](cms), NINLET=[ 1],
3479 MajNHYD=[ "FC-02-MJ"]
3480 MinNHYD=[ "FC-02-MN"]
3481 TMJSTO=[ 2385](cu-m)
3482 *%-----| ADD HYD NHYDsum=[ "FC-02-S"], NHYDs to add=[ "FC-02-MJ"+"FC-02-MN"]
3483 *%-----| CONTINUOUS STANDHYD NHYD=[ "FC-03"], DT=[1]min, AREA=[ 7.37](ha), XIMP=[ 0.64],
3484 TEMP=[ 0.64], DWF=[ 0](cms), LOSS=[ 1]:
3485 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3486 F=[ 0.00](mm),
3487 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3488 MNP=[ 0.250], SCP=[ 0](min),
3489 Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 1.0](%), LGI=[ 221.660](m),
3490 MNI=[ 0.013], SCI=[ 0](min),
3491 Continuous simulation parameters:
3492 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3493 END=-1
3494 *%-----| COMPUTE DUALHYD NHYDin=[ "FC-03"], CINLET=[ 0.358](cms), NINLET=[ 1],
3495 MajNHYD=[ "FC-03-MJ"]
3496 MinNHYD=[ "FC-03-MN"]
3497 TMJSTO=[ 1131](cu-m)
3498 *%-----| ADD HYD NHYDsum=[ "FC-03-S"], NHYDs to add=[ "FC-03-MJ"+"FC-03-MN"]
3499 *%-----| CONTINUOUS STANDHYD NHYD=[ "FC-04"], DT=[1]min, AREA=[ 12.87](ha), XIMP=[ 0.64],
3500 TEMP=[ 0.64], DWF=[ 0](cms), LOSS=[ 1]:
3501 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3502 F=[ 0.00](mm),
3503 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3504 MNP=[ 0.250], SCP=[ 0](min),
3505 Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 1.0](%), LGI=[ 292.916](m),
3506 MNI=[ 0.013], SCI=[ 0](min),
3507 Continuous simulation parameters:
3508 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3509 END=-1
3510 *%-----| COMPUTE DUALHYD NHYDin=[ "FC-04"], CINLET=[ 0.741](cms), NINLET=[ 1],
3511 MajNHYD=[ "FC-04-MJ"]
3512 MinNHYD=[ "FC-04-MN"]
3513 TMJSTO=[ 1794](cu-m)
3514 *%-----| ADD HYD NHYDsum=[ "FC-04-S"], NHYDs to add=[ "FC-04-MJ"+"FC-04-MN"]
3515 *%-----| **** PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118080), SWM Modeling
3516 Approach, NOVATECH Report June, 2020)
3517 *#      - TO JOCK RIVER
3518 *# ****

```

```

3513 CONTINUOUS STANDHYD NHYD=[ "JR-01" ], DT=[1]min, AREA=[ 8.24 ](ha), XIMP=[ 0.64 ],
3514 TIMP=[ 0.64 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3515     Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3516     F=[ 0.00 ](mm),
3517     Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3518     MNP=[ 0.250 ], SCP=[ 0 ](min),
3519     Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 1.0 ](%),
3520     LGI=[ 234.379 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3521     Continuous simulation parameters:
3522     IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3523     END=-1
3524 *%-----|-----|
3525 COMPUTE DUALHYD NHYDin=[ "JR-01" ], CINLET=[ 0.563 ](cms), NINLET=[ 1 ],
3526     MajNHYD=[ "JR-01-MJ" ]
3527     MinNHYD=[ "JR-01-MN" ]
3528     TMJSTO=[ 1040 ](cu-m)
3529 *%-----|-----|
3530 ADD HYD NHYDsum=[ "JR-01-S" ], NHYDs to add=[ "JR-01-MJ" + "JR-01-MN" ]
3531 *%-----|-----|
3532 CONTINUOUS STANDHYD NHYD=[ "JR-02" ], DT=[1]min, AREA=[ 1.59 ](ha), XIMP=[ 0.64 ],
3533 TIMP=[ 0.64 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3534     Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3535     F=[ 0.00 ](mm),
3536     Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3537     MNP=[ 0.250 ], SCP=[ 0 ](min),
3538     Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 1.0 ](%),
3539     LGI=[ 102.956 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3540     Continuous simulation parameters:
3541     IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3542     END=-1
3543 *%-----|-----|
3544 COMPUTE DUALHYD NHYDin=[ "JR-02" ], CINLET=[ 0.153 ](cms), NINLET=[ 1 ],
3545     MajNHYD=[ "JR-02-MJ" ]
3546     MinNHYD=[ "JR-02-MN" ]
3547     TMJSTO=[ 153 ](cu-m)
3548 *%-----|-----|
3549 ADD HYD NHYDsum=[ "JR-02-S" ], NHYDs to add=[ "JR-02-MJ" + "JR-02-MN" ]
3550 *%-----|-----|
3551 *#*****|-----|
3552 *#   Catchment FRASER
3553 *#   - To Fraser-Clarke drain (north of the Jock)
3554 *#   - Developed land with assumed 43% imp.
3555 *#   - 2020-12-17 Change Fraser area to be 35.1 as measured from QGIS
3556 *#   - 2020-12-17 All Fraser is undeveloped (Nashyd)
3557 *#*****|-----|
3558 CONTINUOUS NASHYD NHYD=[ "FRASER-DRN" ], DT=[1]min, AREA=[ 13.65 ](ha),
3559     DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
3560     N=[ 3 ], TP=[ 0.4258 ]hrs,
3561     Continuous simulation parameters:
3562     IaRECper=[ 4 ](hrs),
3563     SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
3564     InterEventTime=[ 12 ](hrs)
3565     Baseflow simulation parameters:
3566     BaseFlowOption=[ 1 ],
3567     InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
3568     VHdCond=[ 0.055 ](mm/hr), END=-1
3569 *%-----|-----|
3570 *CONTINUOUS STANDHYD NHYD=[ "FRASER-D" ], DT=[1]min, AREA=[ 21.61 ](ha),
3571 *     XIMP=[ 0.585 ], TIMP=[ 0.585 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
3572 *     SCS curve number CN=[ 80 ],
3573 *     Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
3574 *             LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
3575 *     Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
3576 *             LGI=[ 379.561 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3577 *     Continuous simulation parameters:
3578 *     IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),

```

```

3569 *
3570 *
3571 *%
3572 CONTINUOUS NASHYD
3573 |-----| NYHD= [ "FRASER-D" ], DT=[1]min, AREA=[ 21.61 ](ha),
3574 |-----| DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
3575 |-----| N=[ 3 ], TP=[ 0.674 ]hrs,
3576 |-----| Continuous simulation parameters:
3577 |-----| IaRECper=[ 4 ](hrs),
3578 |-----| SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
3579 |-----| InterEventTime=[ 12 ](hrs)
3580 |-----| Baseflow simulation parameters:
3581 |-----| BaseFlowOption=[ 1 ],
3582 |-----| InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
3583 |-----| VHydCond=[ 0.055 ](mm/hr), END=-1
3584 *%
3585 *COMPUTE DUALHYD
3586 |-----| NYHDin= [ "FRASER-D" ], CINLET=[ 3.545 ](cms), NINLET=[ 1 ],
3587 |-----| MajNHYD= [ "FRASER-J" ]
3588 |-----| MinNHYD= [ "FRASER-N" ]
3589 |-----| TMJSTO=[ 9999999 ](cu-m)
3590 *%
3591 *ADD HYD
3592 |-----| NYHDsum= [ "FRASER-S" ], NYHDs to add= [ "FRASER-J" + "FRASER-N" ]
3593 *%
3594 *ROUTE RESERVOIR
3595 |-----| NYHDout= [ "MS_P20" ], NYHDin= [ "FRASER" ],
3596 |-----| RDT=[ 1 ](min),
3597 |-----| TABLE of ( OUTFLOW-STORAGE ) values
3598 |-----| ( cms ) - ( ha-m )
3599 |-----| [ 0.0 , 0.0 ]
3600 |-----| [ 0.04 , 0.36 ]
3601 |-----| [ -1 , -1 ] ( max twenty pts )
3602 |-----| NYHDovf= [ "P20-OVF" ]
3603 *%
3604 *ADD HYD
3605 |-----| NYHDsum= [ "4241" ], NYHDs to
3606 |-----| add= [ "KB-Pond3" + "S-1-B" + "FRASER-DRN" + "FRASER-D" + "N_KB" + "FC-01-S" + "FC-02-S" + "FC-03-S" ]
3607 *%
3608 *SAVE HYD
3609 |-----| NYHD= [ "4241" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
3610 |-----| HYD_COMMENT= [ "Total Flows at Ken-Burnett Outlet" ]
3611 *%
3612 *# Hydrograph from Node Ken-Burnett to station 3633
3613 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4241
3614 *#
3615 *ROUTE CHANNEL
3616 |-----| NYHDout= [ "4241-out" ], NYHDin= [ "4241" ], RDT=[ 1 ](min),
3617 |-----| CHLGTH=[ 294 ](m), CHSLOPE=[ 0.1088 ](%), FPSLOPE=[ 0.1088 ](%),
3618 |-----| SECNUM=[ 1.0 ], NSEG=[ 3 ]
3619 |-----| ( SEGROUGH, SEGDIST (m) )=[ 0.05, -20.12
3620 |-----| -0.035, 45.26
3621 |-----| 0.05, 403.84 ] NSEG times
3622 |-----| ( DISTANCE (m), ELEVATION (m) )=[ ]
3623 |-----| [ -909.72, 95 ]
3624 |-----| [ -907.09, 94.5 ]
3625 |-----| [ -904.65, 94 ]
3626 |-----| [ -902.26, 93.5 ]
3627 |-----| [ -44.51, 91.5 ]
3628 |-----| [ -25.1, 91.5 ]
3629 |-----| [ -20.98, 91 ]
3630 |-----| [ -20.61, 90.5 ]
3631 |-----| [ -20.12, 90 ]
3632 |-----| [ -6.13, 87.26 ]
3633 |-----| [ 17.51, 86.56 ]
3634 |-----| [ 31.37, 87.2 ]
3635 |-----| [ 45.26, 90 ]
3636 |-----| [ 50.41, 90.5 ]
3637 |-----| [ 63.06, 91 ]
3638 |-----| [ 134.5, 91.5 ]
3639 |-----| [ 190.63, 92 ]
3640 |-----| [ 251.98, 92.5 ]
3641 |-----| [ 321.32, 93.5 ]

```

```

3634 [403.84, 95 ]
3635 *%
3636 ADD HYD NHYDsum= [ "SN_KB" ], NHYDs to
add=[ "4241-out "+ "FC-04-S" +"JR-01-S" +"JR-02-S" ]
3637 *%
3638 SAVE HYD NHYD=[ "SN_KB" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
HYD_COMMENT=[ "Total Flows before Station 3633" ]
3639 *%
3640 *# Hydrograph from Station 3633 to Node Todd
3641 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 3633
3642 *# JFSA 2021-02-26 change the channel length (at station 3633) from 650m to 608m and
3643 change the slope from 0.0498% to 0.24671%. That is because of adding station 4241
between station 4534 and station 3633
3644 *#
3645 ROUTE CHANNEL NHYDout=[ "N_TO" ], NHYDin=[ "SN_KB" ], RDT=[ 1 ](min),
3646 CHLGTH=[ 608 ](m), CHSLOPE=[ 0.24671 ](%), FPSLOPE=[ 0.24671 ](%),
3647 SECNUM=[ 1.0 ], NSEG=[ 3 ]
3648 ( SEGRROUGH, SEGDIST (m))=[ 0.05, -23.74
3649 -0.035, 23.74
3650 0.05, 26.50 ] NSEG times
3651 ( DISTANCE (m), ELEVATION (m))= []
3652 -29.24, 91.0
3653 -27.41, 90.5
3654 -25.64, 90
3655 -23.74, 89.5
3656 -22, 89.26
3657 -20, 88.51
3658 -19, 88.32
3659 -15, 88.1
3660 -10, 88.11
3661 -5, 88.17
3662 0, 88.27
3663 5, 88.19
3664 10, 88.06
3665 15, 88.48
3666 16, 88.7
3667 23.74, 89.5
3668 24.68, 90
3669 25.57, 90.5
3670 26.50, 91.0
3671 *
3672 *
3673 *
3674 *
3675 *
3676 *
3677 *
3678 *
3679 *
3680 *
3681 *
3682 *
3683 *
3684 *
3685 *
3686 *
3687 *
3688 *
3689 *%
3690 *#*****
3691 *# Catchment Greenbank
3692 *# - To Greenbank Drain (south of the Jock)
3693 *# - JFSA 2021-01-18 add Greenbank pond as per JFSA, P598(06)-15, June 2016
3694 *# - JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GIS measurements
3695 *#*****
3696 CONTINUOUS STANDHYD NHYD=[ "Greenbank" ], DT=[ 1 ]min, AREA=[ 36.6 ](ha),

```

```

XIMP=[ 0.639], TIMP=[ 0.682], DWF=[ 0](cms), LOSS=[ 2],
SCS curve number CN=[ 77],
Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
LGI=[ 493.96](m), MNI=[ 0.013], SCI=[ 0](min),
Continuous simulation parameters:
IaRECper=[ 4](hrs), IaRECimp=[ 4](hrs),
SMIN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
InterEventTime=[ 18](hrs), END=-1

```

\* % -----

```
NHYDout=[ "GreenB_MN" ] , NYHdin=[ "Greenbank" ]  
RDT=[ 1 ](min),
```

TABLE of ( OUTFLOW-STORAGE ) values  
(cms) - (ha-m)

```
[ 0.0 , 0.0
[ 0.033 , 0.084 ]
[ 0.039 , 0.201 ]
[ 0.113 , 0.292 ]
[ 0.237 , 0.386 ]
[ 0.382 , 0.484 ]
[ 0.539 , 0.585 ]
[ 0.7 , 0.692 ]
[ 0.86 , 0.804 ]
[ 4.684 , 0.922 ]
[ 11.539 , 1.052 ]
[ 20.867 , 1.168 ]
[ 103.616 , 1.974 ]
[ -1 , -1 ]
```

NHYDovf=[ "GreenB\_MJ" ] ,

\* % -----

NHXRdum = ["GreenB"], NHXRdum\_to\_add = ["N\_TO", "GreenB\_M1", "GreenB\_MN"]

### **ADD AND**

```
NHYD= ["GreenB"],    # OF PCYCLES=[-1],  ICASEsh=[1]
HYD COMMENT=["Total Flows at Greenbank Drain"]
```

\* % -----

\*\*\*\*\*

## \*# Catchment TODD

\*# - To Todd Drain (south of the Jock,  
\*\* Subdivision with 438 lots as now

\*# - Subdivision with 45% imp. as per Baithnavaen South MSS  
\*# - 2020-11-30 increase imp. based on B598(04)-11

\*# - 2020-11-30 update TODD Tributary Drainage Area

P598 (04)-11

\*# - 2020-11-30 split TODD Drainage Area to MAJOR, MINOR, POND and ALL

~~^# - JFSA 2021-01-19 add "TODD\_MNI" as part of Clarke("W\_CLR\_MJ") and remove it from Todd~~

\*CONTINUOUS STANDBYD NYHD=[1,TODD\_MINI"], DI=[1]MIN, AREA=[1.1772](ha),  
 \*XIMP=[0.53], TIMP=[0.53], DWE=[0.1](cm/s), LOSS=[2]

\* XIMR-[0.35], TMR-[0.37], DWF-[0] (CMS), LOSS-[2]  
SCS curve number CN=[77]

\* Pervious surfaces: IApel

\* LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),

\* Impervious surfaces: IAimp=[1.57] (mm), SLPi=[1]

LGI=[108.689](m), MNI=[0.013], SCI=[0](min)

\* Continuous simulation parameters  
LaBEGper-[4](hrs) LaBEGimp-[4]

\*  
TARCEP1=[1] (HIS) ; TARCEP1=[1] (HIS)  
SMIN=[-1] (mm) ; SMAX=[-1] (mm) ; SK=[0]

\* InterEventTime=[ 18 ](hrs), END=-1

\* % - - - - - | - - - - -

**CONTINUOUS STANDHYD** NHYD=[ "TODD\_MN2" ], DT=[ 1 ]min, AREA=[ 2.1 ](ha),

XIMP=[0.53], TIMP=[0.57], DWF=[0] (cms), LOSS=[0],  
 SGS NUMBER NUMBER CN=[77]

SCS Curve Number CN-[77], Previous surfaces, TApex-[4.67] (mm), STPP-[1] (%)

$$LGP = [40] \text{ (m)} , MNP = [0, 25] , SCP = [0] \text{ (min)} .$$

```

3761 LGI=[118.322](m), MNI=[0.013], SCI=[0](min),
3762 Continuous simulation parameters:
3763 IaRECper=[4](hrs), IaRECImp=[4](hrs),
3764 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3765 InterEventTime=[18](hrs), END=-1
3766 *%-----|-----|
3767 CONTINUOUS STANDHYD NHYD=[ "TODD_MN3" ], DT=[1]min, AREA=[0.117](ha),
3768 XIMP=[0.53], TIMP=[0.57], DWF=[0](cms), LOSS=[2],
3769 SCS curve number CN=[77],
3770 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3771 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3772 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3773 LGI=[27.928](m), MNI=[0.013], SCI=[0](min),
3774 Continuous simulation parameters:
3775 IaRECper=[4](hrs), IaRECImp=[4](hrs),
3776 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3777 InterEventTime=[18](hrs), END=-1
3778 *%-----|-----|
3779 CONTINUOUS STANDHYD NHYD=[ "TODD_MJ" ], DT=[1]min, AREA=[30.230](ha),
3780 XIMP=[0.52], TIMP=[0.64], DWF=[0](cms), LOSS=[2],
3781 SCS curve number CN=[77],
3782 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3783 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3784 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3785 LGI=[448.925](m), MNI=[0.013], SCI=[0](min),
3786 Continuous simulation parameters:
3787 IaRECper=[4](hrs), IaRECImp=[4](hrs),
3788 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3789 InterEventTime=[18](hrs), END=-1
3790 *%-----|-----|
3791 * -JFSA, 2021-01-19 update "TODD_ALL" area from 108.741 ha to 112.908 ha based on
3792 GIS measurements (148.41-30.23-0.117-2.1-3.055=112.908 ha)
3793 CONTINUOUS STANDHYD NHYD=[ "TODD_ALL" ], DT=[1]min, AREA=[112.908](ha),
3794 XIMP=[0.52], TIMP=[0.57], DWF=[0](cms), LOSS=[2],
3795 SCS curve number CN=[77],
3796 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3797 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3798 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3799 LGI=[867.594](m), MNI=[0.013], SCI=[0](min),
3800 Continuous simulation parameters:
3801 IaRECper=[4](hrs), IaRECImp=[4](hrs),
3802 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3803 InterEventTime=[18](hrs), END=-1
3804 *%-----|-----|
3805 CONTINUOUS STANDHYD NHYD=[ "TODD_P" ], DT=[1]min, AREA=[3.055](ha),
3806 XIMP=[0.63], TIMP=[0.63], DWF=[0](cms), LOSS=[2],
3807 SCS curve number CN=[77],
3808 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3809 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3810 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3811 LGI=[142.712](m), MNI=[0.013], SCI=[0](min),
3812 Continuous simulation parameters:
3813 IaRECper=[4](hrs), IaRECImp=[4](hrs),
3814 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3815 InterEventTime=[18](hrs), END=-1
3816 *%-----|-----|
3817 * -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"
and its parameters remain the same.
3818 *CONTINUOUS STANDHYD NHYD=[ "TODD_DEVL" ], DT=[1]min, AREA=[15.87](ha),
3819 *
3820 *
3821 *
3822 *
3823 *

```

```

3824 * LGI=[325.27](m), MNI=[0.013], SCI=[0](min),
3825 *
3826 * Continuous simulation parameters:
3827 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
3828 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3829 * InterEventTime=[18](hrs), END=-1
3830 *%-----|-----|
3830 * -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
3830 is called "corr2" and its parameters remain the same.
3831 *CONTINUOUS NASHYD NHYD=[ "TODD_UnD" ], DT=[1]min, AREA=[12.47](ha),
3832 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
3833 * N=[3], TP=[1.10]hrs,
3834 * Continuous simulation parameters:
3835 * IaRECper=[4](hrs),
3836 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3837 * InterEventTime=[12](hrs)
3838 * Baseflow simulation parameters:
3839 * BaseFlowOption=[1],
3840 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
3841 * VHdCond=[0.055](mm/hr), END=-1
3842 *%-----|-----|
3843 *# 5-Year + 12% Capture
3844 *COMPUTE DUALHYD NHYDin=[ "TODD_MJ" ], CINLET=[3.314](cms), NINLET=[1],
3845 * MajNHYD=[ "TODD_MJj" ]
3846 * MinNHYD=[ "TODD_MJn" ]
3847 * TMJSTO=[0.1](cu-m)
3848 ROUTE RESERVOIR NHYDout=[ "TODD_MJn" ] ,NHYDin=[ "TODD_MJ" ] ,
3849 RDT=[1](min),
3850 * TABLE of ( OUTFLOW-STORAGE ) values
3851 * (cms) - (ha-m)
3852 * [ 0.0 , 0.0 ]
3853 * [ 3.314 , 0.0001 ]
3854 * [ -1 , -1 ] (max twenty pts)
3855 * NHYDovf=[ "TODD_MJj" ] ,
3856 *%-----|-----|
3856 *# 5-Year + 12% Capture
3857 *COMPUTE DUALHYD NHYDin=[ "TODD_MN1" ], CINLET=[0.227](cms), NINLET=[1],
3858 * MajNHYD=[ "TODD_MN1j" ]
3859 * MinNHYD=[ "TODD_MN1n" ]
3860 * TMJSTO=[0.1](cu-m)
3861 *ROUTE RESERVOIR NHYDout=[ "TODD_MN1n" ] ,NHYDin=[ "TODD_MN1" ] ,
3862 RDT=[1](min),
3863 * TABLE of ( OUTFLOW-STORAGE ) values
3864 * (cms) - (ha-m)
3865 * [ 0.0 , 0.0 ]
3866 * [ 0.227 , 0.0001 ]
3867 * [ -1 , -1 ] (max twenty pts)
3868 * NHYDovf=[ "TODD_MN1j" ] ,
3869 *%-----|-----|
3870 *COMPUTE DUALHYD NHYDin=[ "TODD_MN2" ], CINLET=[0.268](cms), NINLET=[1],
3871 * MajNHYD=[ "TODD_MN2j" ]
3872 * MinNHYD=[ "TODD_MN2n" ]
3873 * TMJSTO=[0.1](cu-m)
3874 *ROUTE RESERVOIR NHYDout=[ "TODD_MN2n" ] ,NHYDin=[ "TODD_MN2" ] ,
3875 RDT=[1](min),
3876 * TABLE of ( OUTFLOW-STORAGE ) values
3877 * (cms) - (ha-m)
3878 * [ 0.0 , 0.0 ]
3879 * [ 0.268 , 0.0001 ]
3880 * [ -1 , -1 ] (max twenty pts)
3881 * NHYDovf=[ "TODD_MN2j" ] ,
3882 *%-----|-----|
3883 *COMPUTE DUALHYD NHYDin=[ "TODD_MN3" ], CINLET=[0.016](cms), NINLET=[1],
3884 * MajNHYD=[ "TODD_MN3j" ]
3885 * MinNHYD=[ "TODD_MN3n" ]
3886 * TMJSTO=[0.1](cu-m)
3887 *ROUTE RESERVOIR NHYDout=[ "TODD_MN3n" ] ,NHYDin=[ "TODD_MN3" ] ,

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3889      RDT=[1](min),
3890          TABLE of ( OUTFLOW-STORAGE ) values
3891              (cms) - (ha-m)
3892              [ 0.0 , 0.0 ]
3893              [ 0.016 , 0.0001 ]
3894              [ -1 , -1 ] (max twenty pts)
3895      NHYDovf= [ "TODD_MN3j" ] ,
3896 *%-----|-----|
3897 * -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
3898 major system from A2 can be added to Todd
CONTINUOUS STANDHYD NHYD= [ "A2" ], DT=[1]min, AREA=[25.5](ha),
3899 XIMP=[0.42], TIMP=[0.52], DWF=[0](cms), LOSS=[2],
3900 SCS curve number CN=[75],
3901 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%) ,
3902 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3903 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%) ,
3904 LGI=[566](m), MNI=[0.013], SCI=[0](min),
3905 Continuous simulation parameters:
3906 IaRECper=[4](hrs), IaRECImp=[4](hrs),
3907 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3908 InterEventTime=[18](hrs), END=-1
3909 *%-----|-----|
3910 COMPUTE DUALHYD NHYDin= [ "A2" ], CINLET=[1.818](cms), NINLET=[1],
3911 MajNHYD= [ "A2-MJ" ]
3912 MinNHYD= [ "A2-MN" ]
3913 TMJSTO=[924](cu-m)
3914 *%-----|-----|
3915 ADD HYD NHYDsum= [ "TODD" ], NHYDs to
add=[ "TODD_MN2n "+ "TODD_MN3n "+ "TODD_MJj "+ "TODD_P "+ "TODD_ALL "+ "W_CLAR_MJn" ]
3916 *%-----|-----|
3917 SAVE HYD NHYD= [ "TODD" ], # OF PCYCLES=[-1], ICASEsh=[1]
3918 HYD_COMMENT=[ "Total Flows at Todd Drain" ]
3919 *%-----|-----|
3920 *#*****#
3921 *# Todd Pond 3
3922 *# - Rating curve obtained from Barrhaven South MSS modeling
3923 *# - stantec 2007, Tributary Drainage Area to MSS Pond 3 = 193 ha
3924 *#*****#
3925 ROUTE RESERVOIR NHYDout= [ "MS_P3" ], NHYDin= [ "TODD" ],
3926 RDT=[1](min),
3927     TABLE of ( OUTFLOW-STORAGE ) values
3928         (cms) - (ha-m)
3929         [ 0.0 , 0.0 ]
3930         [ 0.014 , 0.155 ]
3931         [ 0.048 , 0.394 ]
3932         [ 0.061 , 0.56 ]
3933         [ 0.08 , 0.909 ]
3934         [ 0.088 , 1.089 ]
3935         [ 0.109 , 1.652 ]
3936         [ 0.118 , 1.952 ]
3937         [ 0.122 , 2.099 ]
3938         [ 1.972 , 2.269 ]
3939         [ 9.135 , 2.598 ]
3940         [ 15.608 , 2.826 ]
3941         [ 19.256 , 2.942 ]
3942         [ 27.282 , 3.181 ]
3943         [ 40.957 , 3.55 ]
3944         [ 56.372 , 3.929 ]
3945         [ 73.349 , 4.317 ]
3946         [ 85.469 , 4.579 ]
3947         [ 104.771 , 4.977 ]
3948         [ -1 , -1 ] (max twenty pts)
3949     NHYDovf= [ "P3-OVF" ]
3950 *%-----|-----|
3951 ADD HYD NHYDsum= [ "SN_TO" ], NHYDs to
add=[ "GreenB "+ "MS_P3 "+ "P3-OVF "+ "TODD_MN2j "+ "A2-MJ" ]

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3952 *%
3953 SAVE HYD          NHYD=[ "SN_TO" ] ,   # OF PCYCLES=[-1] ,  ICASEsh=[1]
3954           HYD_COMMENT=[ "Total Flows at Todd Drain" ]
3955 *%
3956 *#
3957 *# Hydrograph from Todd Drain routed to Corrigan Drain
3958 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
3959 *# 2021-02-19 Change the slope from 0.033 % (as per Stantec Report 2007) to 0.05 % so
3960 the model will be more stable and give reasonable results. It is justifiable as ROUTE
3961 CHANNELS aren't well suited to really flat slopes.
3962 *
3963 ROUTE CHANNEL      NHYDout=[ "N_TO" ] , NHYDin=[ "SN_TO" ] ,
3964           RDT=[1](min),
3965           CHLGTH=[ 280 ](m),   CHSLOPE=[ 0.05 ](%),
3966           FPSLOPE=[ 0.05 ](%),
3967           SECNUM=[ 1.0 ],      NSEG=[ 3 ]
3968           ( SEGROUGH, SEGDIST (m))=
3969           [ 0.075,-17.72
3970             -0.045,17.72
3971               0.075,80.62 ] NSEG times
3972           ( DISTANCE (m), ELEVATION (m))=
3973           [-83.32, 90.00]
3974           [-81.36, 89.50]
3975           [-79.12, 89.00]
3976           [-76.13, 88.50]
3977           [-20.46, 88.00]
3978           [-19.36, 87.50]
3979           [-18.51, 87.00]
3980           [-17.72, 86.50]
3981           [-11.95, 85.24]
3982           [-0.11, 85.12]
3983           [11.49, 85.20]
3984           [17.72, 86.50]
3985           [19.74, 87.00]
3986           [21.22, 87.50]
3987           [22.68, 88.00]
3988           [24.28, 88.50]
3989           [26.79, 89.00]
3990           [71.98, 90.00]
3991           [80.62, 90.50]
3992 *%
3993 SAVE HYD          NHYD=[ "N_TO" ] ,   # OF PCYCLES=[-1] ,  ICASEsh=[1]
3994           HYD_COMMENT=[ "Total inflows at Station 2462" ]
3995 *#####
3996 *# Catchment CORRIG
3997 *# - To Corrigan Drain (south of the Jock)
3998 *# - Primarily Developed (medium density)
3999 *# - JFSA JAN 2021, add Corrigan subcatchments as per IBI, July 2008
4000 *#####
4001 ROUTE RESERVOIR    NHYDout=[ "MS_P1" ] ,  NHYDin=[ "CORRIG" ] ,
4002           *
4003           RDT=[1](min),
4004           *
4005           TABLE of ( OUTFLOW-STORAGE ) values
4006           (cms) - (ha-m)
4007           [
4008             0.0 , 0.0 ]
4009           [
4010             0.06 , 0.58 ]
4011           [
4012             -1 , -1 ] (max twenty pts)
4013           *
4014           NHYDovf=[ "P1-OVF" ]
4015 *%
4016 *ADD HYD            NHYDsum=[ "SN_CO" ] ,  NHYDs to add=[ "N_TO"+"P1-OVF"+"MS_P1" ]
4017 *%
4018 *SAVE HYD           NHYD=[ "SN_CO" ] ,   # OF PCYCLES=[-1] ,  ICASEsh=[1]
4019           *
4020           HYD_COMMENT=[ "Total Flows at Corrigan Drain" ]
4021 *%
4022 *      -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
4023 drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"

```



```

4071 *           Continuous simulation parameters:
4072 *
4073 *           IaRECper=[4](hrs),
4074 *           SMIN=[-1](mm),   SMAX=[-1](mm),   SK=[0.010]/(mm),
4075 *           InterEventTime=[12](hrs)
4076 *           Baseflow simulation parameters:
4077 *           BaseFlowOption=[1] ,
4078 *           InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
4079 *           VHydCond=[0.055](mm/hr),   END=-1
4080 *%-----|-----|
4081 CONTINUOUS NASHYD NHYD= [ "B1" ], DT=[1]min, AREA=[2.77](ha),
4082 DWF=[0](cms),  CN/C=[56],  IA=[2.5](mm),
4083 N=[3.0],  TP=[0.23]hrs,
4084 Continuous simulation parameters:
4085 IaRECper=[4](hrs),
4086 SMIN=[-1](mm),   SMAX=[-1](mm),   SK=[0.010]/(mm),
4087 InterEventTime=[12](hrs)
4088 Baseflow simulation parameters:
4089 BaseFlowOption=[1] ,
4090 InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
4091 VHydCond=[0.055](mm/hr),   END=-1
4092 *%-----|-----|
4093 CONTINUOUS STANDHYD NHYD= [ "A4" ], DT=[1]min, AREA=[1.27](ha),
4094 XIMP=[0.65],  TIMP=[0.65],  DWF=[0](cms),  LOSS=[2],
4095 SCS curve number CN=[75],
4096 Pervious surfaces: IAper=[4.67](mm),  SLPP=[1](%),
4097 LGP=[40](m),  MNP=[0.25],  SCP=[0](min),
4098 Impervious surfaces: IAimp=[1.57](mm),  SLPI=[1](%),
4099 LGI=[253](m),  MNI=[0.013],  SCI=[0](min),
4100 Continuous simulation parameters:
4101 IaRECper=[4](hrs),  IaRECimp=[4](hrs),
4102 SMIN=[-1](mm),   SMAX=[-1](mm),   SK=[0.010]/(mm),
4103 InterEventTime=[18](hrs),   END=-1
4104 *%-----|-----|
4105 COMPUTE DUALHYD NHYDin=[ "A4" ], CINLET=[0.405](cms), NINLET=[1],
4106 MajNHYD=[ "A4-MJ" ]
4107 MinNHYD=[ "A4-MN" ]
4108 TMJSTO=[68](cu-m)
4109 *%-----|-----|
4110 ADD HYD NHYDsum=[ "MH101" ], NHYDs to
4111 add=[ "A1-MJ"+"A1-MN"+"corr1-MJ"+"corr1-MN"+"corr2"+"B1"+"A4-MN" ]
4112 *%-----|-----|
4113 SAVE HYD NHYD=[ "MH101" ], # OF PCYCLES=[-1], ICASEsh=[1]
4114 HYD_COMMENT=[ "Total Flows at MH101" ]
4115 *%-----|-----|
4116 ROUTE PIPE PTYPE=[1]circ, NHYDout=[ "101-102" ], RNUMBER=[1.0], PDIAM=[1050](mm),
4117 PLNGTH=[368](m), PROUGH=[0.013], PSLOPE=[0.0054](m/m),
4118 NHYDin=[ "MH101" ], RDT=[1]
4119 *%-----|-----|
4120 * -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
4121 major system from A2 can be added to Todd
4122 *CONTINUOUS STANDHYD NHYD=[ "A2" ], DT=[1]min, AREA=[25.5](ha),
4123 *           XIMP=[0.42],  TIMP=[0.52],  DWF=[0](cms),  LOSS=[2],
4124 *           SCS curve number CN=[75],
4125 *           Pervious surfaces: IAper=[4.67](mm),  SLPP=[1](%),
4126 *           LGP=[40](m),  MNP=[0.25],  SCP=[0](min),
4127 *           Impervious surfaces: IAimp=[1.57](mm),  SLPI=[1](%),
4128 *           LGI=[566](m),  MNI=[0.013],  SCI=[0](min),
4129 *           Continuous simulation parameters:
4130 *           IaRECper=[4](hrs),  IaRECimp=[4](hrs),
4131 *           SMIN=[-1](mm),   SMAX=[-1](mm),   SK=[0.010]/(mm),
4132 *           InterEventTime=[18](hrs),   END=-1
4133 *%-----|-----|
4134 *COMPUTE DUALHYD NHYDin=[ "A2" ], CINLET=[1.818](cms), NINLET=[1],
4135 * MajNHYD=[ "A2-MJ" ]
4136 * MinNHYD=[ "A2-MN" ]
4137 * TMJSTO=[924](cu-m)

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4134 *%
4135 ADD HYD NHYDsum= [ "MH102" ], NHYDs to add= [ "A2-MN"+ "101-102" ]
4136 *%
4137 SAVE HYD NHYD= [ "MH102" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4138 HYD_COMMENT=[ "Total Flows at MH102" ]
4139 *%
4140 CONTINUOUS STANDHYD NHYD= [ "A5" ], DT=[ 1 ]min, AREA=[ 1.6 ](ha),
4141 XIMP=[ 0.71 ], TIMP=[ 0.71 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4142 SCS curve number CN=[ 75 ],
4143 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4144 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4145 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4146 LGI=[ 300 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4147 Continuous simulation parameters:
4148 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4149 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4150 InterEventTime=[ 18 ](hrs), END=-1
4151 *%
4152 ADD HYD NHYDsum= [ "A5T" ], NHYDs to add= [ "A4-MJ"+ "A5" ]
4153 *%
4154 COMPUTE DUALHYD NHYDin= [ "A5T" ], CINLET=[ 0.357 ](cms), NINLET=[ 1 ],
4155 MajNHYD= [ "A5-MJ" ]
4156 MinNHYD= [ "A5-MN" ]
4157 TMJSTO=[ 60 ](cu-m)
4158 *%
4159 * -JFSA Jan. 2021, A3 is a part of Todd so it is removed
4160 * -JFSA Jan. 2021, "A2-MJ" added to "Todd"
4161 *CONTINUOUS STANDHYD NHYD= [ "A3" ], DT=[ 1 ]min, AREA=[ 18.4 ](ha),
4162 * XIMP=[ 0.58 ], TIMP=[ 0.65 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4163 * SCS curve number CN=[ 75 ],
4164 * Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4165 * LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4166 * Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4167 * LGI=[ 450 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4168 * Continuous simulation parameters:
4169 * IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4170 * SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4171 * InterEventTime=[ 18 ](hrs), END=-1
4172 *%
4173 *ADD HYD NHYDsum= [ "A3-A2MJ" ], NHYDs to add= [ "A2-MJ"+ "A3" ]
4174 *%
4175 *COMPUTE DUALHYD NHYDin= [ "A3-A2MJ" ], CINLET=[ 2.208 ](cms), NINLET=[ 1 ],
4176 * MajNHYD= [ "A3R-MJ" ]
4177 * MinNHYD= [ "A3R-MN" ]
4178 * TMJSTO=[ 908 ](cu-m)
4179 *%
4180 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout= [ "102-103" ], RNUMBER=[ 1.0 ], PDIAM=[ 1500 ](mm),
4181 PLNGTH=[ 504 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0028 ](m/m),
4182 NHYDin= [ "MH102" ], RDT=[ 1 ]
4183 *%
4184 ADD HYD NHYDsum= [ "MH103" ], NHYDs to add= [ "102-103"+ "A5-MN" ]
4185 *%
4186 SAVE HYD NHYD= [ "MH103" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4187 HYD_COMMENT=[ "Total Flows at MH103" ]
4188 *%
4189 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout= [ "103-104" ], RNUMBER=[ 1.0 ], PDIAM=[ 1650 ](mm),
4190 PLNGTH=[ 438 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0046 ](m/m),
4191 NHYDin= [ "MH103" ], RDT=[ 1 ]
4192 *%
4193 CONTINUOUS STANDHYD NHYD= [ "A6" ], DT=[ 1 ]min, AREA=[ 1.56 ](ha),
4194 XIMP=[ 0.71 ], TIMP=[ 0.71 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4195 SCS curve number CN=[ 75 ],
4196 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4197 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
LGI=[ 280 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),

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```

4198 Continuous simulation parameters:
4199 IaRECper=[4](hrs), IaRECimp=[4](hrs),
4200 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4201 InterEventTime=[18](hrs), END=-1
4202 *%-----|-----|
4203 ADD HYD NHYDsum=[ "A6T" ], NHYDs to add=[ "A5-MJ "+"A6" ]
4204 *%-----|-----|
4205 COMPUTE DUALHYD NHYDin=[ "A6T" ], CINLET=[ 0.357 ](cms), NINLET=[ 1 ],
4206 MajNHYD=[ "A6-MJ" ]
4207 MinNHYD=[ "A6-MN" ]
4208 TMJSTO=[ 60 ](cu-m)
4209 *%-----|-----|
4210 * -JFSA Jan. 2021, A7-corrig is a part of Todd so it is removed
4211 *CONTINUOUS STANDHYD NHYD=[ "A7-corrig" ], DT=[1]min, AREA=[ 11.8 ](ha),
4212 * XIMP=[ 0.41 ], TIMP=[ 0.54 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4213 * SCS curve number CN=[ 75 ],
4214 * Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4215 * LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4216 * Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4217 * LGI=[ 438 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4218 * Continuous simulation parameters:
4219 * IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
4220 * SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4221 * InterEventTime=[ 18 ](hrs), END=-1
4222 *%-----|-----|
4223 *ADD HYD NHYDsum=[ "A7-A3RMJ" ], NHYDs to add=[ "A3R-MJ "+"A7-corrig" ]
4224 *%-----|-----|
4225 *COMPUTE DUALHYD NHYDin=[ "A7-A3RMJ" ], CINLET=[ 1.003 ](cms), NINLET=[ 1 ],
4226 * MajNHYD=[ "A7R-MJ" ]
4227 * MinNHYD=[ "A7R-MN" ]
4228 * TMJSTO=[ 496 ](cu-m)
4229 *%-----|-----|
4230 ADD HYD NHYDsum=[ "MH104" ], NHYDs to add=[ "A6-MN "+"103-104 "+"TODD_MJn" ]
4231 *%-----|-----|
4232 SAVE HYD NHYD=[ "MH104" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4233 HYD_COMMENT=[ "Total Flows at MH104" ]
4234 *%-----|-----|
4235 CONTINUOUS STANDHYD NHYD=[ "B2" ], DT=[ 1 ]min, AREA=[ 12.31 ](ha),
4236 XIMP=[ 0.41 ], TIMP=[ 0.54 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4237 SCS curve number CN=[ 75 ],
4238 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4239 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4240 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4241 LGI=[ 417 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4242 Continuous simulation parameters:
4243 IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
4244 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4245 InterEventTime=[ 18 ](hrs), END=-1
4246 *%-----|-----|
4247 COMPUTE DUALHYD NHYDin=[ "B2" ], CINLET=[ 1.029 ](cms), NINLET=[ 1 ],
4248 MajNHYD=[ "B2-MJ" ]
4249 MinNHYD=[ "B2-MN" ]
4250 TMJSTO=[ 508 ](cu-m)
4251 *%-----|-----|
4252 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout=[ "315-333" ], RNUMBER=[ 1.0 ], PDIAM=[ 1200 ](mm),
4253 PLNGTH=[ 254 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m),
4254 NHYDin=[ "B2-MN" ], RDT=[ 1 ]
4255 *%-----|-----|
4256 CONTINUOUS STANDHYD NHYD=[ "B3" ], DT=[ 1 ]min, AREA=[ 5.59 ](ha),
4257 XIMP=[ 0.41 ], TIMP=[ 0.54 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4258 SCS curve number CN=[ 75 ],
4259 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4260 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4261 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4262 LGI=[ 345 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4263 Continuous simulation parameters:

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4263
4264
4265
4266 *%-----| IaRECper=[4](hrs), IaRECImp=[4](hrs),
4267 COMPUTE DUALHYD | SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4268 | InterEventTime=[18](hrs), END=-1
4269
4270
4271 *%-----| NYHDin=[ "B3" ], CINLET=[ 0.459 ](cms), NINLET=[ 1 ],
4272 ADD HYD | MajNHYD=[ "B3-MJ" ]
4273 | MinNHYD=[ "B3-MN" ]
4274 | TMJSTO=[ 227 ](cu-m)
4275
4276 *%-----| NYHDsum=[ "MH333" ], NYHDs to add=[ "B3-MN" + "315-333" ]
4277 SAVE HYD | NYHD=[ "MH333" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4278 | HYD_COMMENT=[ "Total Flows at MH333" ]
4279
4280 *%-----| ROUTE PIPE PTYPE=[ 1 ]circ, NYHDout=[ "333-335" ], RNUMBER=[ 1.0 ], PDIAM=[ 1200 ](mm),
4281 | PLNGTH=[ 251 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m),
4282 | NYHDin=[ "MH333" ], RDT=[ 1 ]
4283
4284 *%-----| ROUTE PIPE PTYPE=[ 1 ]circ, NYHDout=[ "335-338" ], RNUMBER=[ 1.0 ], PDIAM=[ 1200 ](mm),
4285 | PLNGTH=[ 185 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m),
4286 CONTINUOUS STANDHYD | NYHDin=[ "333-335" ], RDT=[ 1 ]
4287 | NYHD=[ "B4" ], DT=[ 1 ]min, AREA=[ 7.6 ](ha),
4288 | XIMP=[ 0.41 ], TIMP=[ 0.54 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4289 | SCS curve number CN=[ 75 ],
4290 | Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4291 | LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4292 | Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4293 | LGI=[ 388 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4294 | Continuous simulation parameters:
4295 | IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4296 | SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4297 | InterEventTime=[ 18 ](hrs), END=-1
4298
4299 *%-----| COMPUTE DUALHYD NYHDin=[ "B4" ], CINLET=[ 0.655 ](cms), NINLET=[ 1 ],
4300 | MajNHYD=[ "B4-MJ" ]
4301 | MinNHYD=[ "B4-MN" ]
4302 | TMJSTO=[ 323 ](cu-m)
4303
4304 *%-----| ADD HYD NYHDsum=[ "MH340" ], NYHDs to add=[ "338-340" + "B4-MN" ]
4305
4306 *%-----| SAVE HYD NYHD=[ "MH340" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4307 | HYD_COMMENT=[ "Total Flows at MH340" ]
4308
4309 *%-----| ROUTE PIPE PTYPE=[ 1 ]circ, NYHDout=[ "340-104" ], RNUMBER=[ 1.0 ], PDIAM=[ 1650 ](mm),
4310 | PLNGTH=[ 240 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0015 ](m/m),
4311 | NYHDin=[ "MH340" ], RDT=[ 1 ]
4312
4313 *%-----| ADD HYD NYHDsum=[ "MH104T" ], NYHDs to add=[ "340-104" + "MH104" ]
4314
4315 *%-----| ROUTE PIPE PTYPE=[ 2 ]rect, NYHDout=[ "104-105" ], RNUMBER=[ 1.0 ],
4316 by PHEIGHT=[ 2100 ](mm),
4317 | PLNGTH=[ 380 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m),
4318 | NYHDin=[ "MH104T" ], RDT=[ 1 ]
4319
4320 *%-----| CONTINUOUS STANDHYD NYHD=[ "B5" ], DT=[ 1 ]min, AREA=[ 2.2 ](ha),
4321 | XIMP=[ 0.57 ], TIMP=[ 0.57 ], DWF=[ 0 ](cms), LOSS=[ 2 ],

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        LGI=[187](m), MNI=[0.013], SCI=[0](min),
Continuous simulation parameters:
IaRECper=[4](hrs), IaRECImp=[4](hrs),
SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
InterEventTime=[18](hrs), END=-1
*%-----|-----|
COMPUTE DUALHYD NHYDin=[ "B5" ], CINLET=[0.260](cms), NINLET=[1],
MajNHYD=[ "B5-MJ" ]
MinNHYD=[ "B5-MN" ]
TMJSTO=[250](cu-m)
*%-----|-----|
CONTINUOUS STANDHYD NHYD=[ "A8" ], DT=[1]min, AREA=[0.96](ha),
XIMP=[0.71], TIMP=[0.71], DWF=[0](cms), LOSS=[2],
SCS curve number CN=[75],
Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
LGP=[40](m), MNP=[0.25], SCP=[0](min),
Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
LGI=[186](m), MNI=[0.013], SCI=[0](min),
Continuous simulation parameters:
IaRECper=[4](hrs), IaRECImp=[4](hrs),
SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
InterEventTime=[18](hrs), END=-1
*%-----|-----|
ADD HYD NHYDsum=[ "A8T" ], NHYDs to add=[ "A6-MJ" +"A8" ]
*%-----|-----|
COMPUTE DUALHYD NHYDin=[ "A8T" ], CINLET=[0.238](cms), NINLET=[1],
MajNHYD=[ "A8-MJ" ]
MinNHYD=[ "A8-MN" ]
TMJSTO=[40](cu-m)
*%-----|-----|
ADD HYD NHYDsum=[ "MH105" ], NHYDs to
add=[ "104-105" +"B5-MN" +"A8-MN" +"TODD_MN3j" ]
*%-----|-----|
SAVE HYD NHYD=[ "MH105" ], # OF PCYCLES=[-1], ICASEsh=[1]
HYD_COMMENT=[ "Total Flows at MH105" ]
*%-----|-----|
DIVERT HYD NHYDin=[ "A8-MJ" ] NIDout=[2]max five,
outflow hydrographs (NHYDs)=[ "A8-MJ-JR" "A8-MJ-B6" ]
flow distribution table: (modify as necessary)
Note: all flows are in (cms)
    QIDI + QIDII = QTOTAL
    [ 0 + 0 = 0 ]
    [ 50 + 50 = 100 ] end
*%-----|-----|
DIVERT HYD NHYDin=[ "MH105" ] NIDout=[2]max five,
outflow hydrographs (NHYDs)=[ "MH105-JR" "MH105-B6" ]
flow distribution table: (modify as necessary)
Note: all flows are in (cms)
    QIDI + QIDII = QTOTAL
    [ 0 + 0 = 0 ]
    [ 0 + 3.0 = 3.0 ]
    [ 96.9+ 3.1 = 100 ] end
*%-----|-----|
CONTINUOUS STANDHYD NHYD=[ "B7" ], DT=[1]min, AREA=[7.19](ha),
XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
SCS curve number CN=[75],
Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
LGP=[40](m), MNP=[0.25], SCP=[0](min),
Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
LGI=[211](m), MNI=[0.013], SCI=[0](min),
Continuous simulation parameters:
IaRECper=[4](hrs), IaRECImp=[4](hrs),
SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
InterEventTime=[18](hrs), END=-1

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4385 *%
4386 ADD HYD NHYDsum= [ "B7-B4MJ" ], NHYDs to add=[ "B4-MJ"+"B7" ]
4387 *%
4388 COMPUTE DUALHYD NHYDin=[ "B7-B4MJ" ], CINLET=[ 0.629 ](cms), NINLET=[ 1 ],
4389 MajNHYD=[ "B7R-MJ" ]
4390 MinNHYD=[ "B7R-MN" ]
4391 TMJSTO=[ 311 ](cu-m)
4392 *%
4393 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout=[ "360-106A" ], RNUMBER=[ 1.0 ], PDIAM=[ 1050 ](mm),
4394 PLNGTH=[ 167 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m),
4395 NHYDin=[ "B7R-MN" ], RDT=[ 1 ]
4396 *%
4397 * -JFSA 2021-01-19 change B6 to be developed as per geoottawa website and apply the
4398 parameters of A7, the nearest sub-catchment to B6, LGI is calculated based on B6 area
4399 CONTINUOUS STANDHYD NHYD=[ "B6" ], DT=[ 1 ]min, AREA=[ 3.29 ](ha),
4400 XIMP=[ 0.41 ], TIMP=[ 0.54 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4401 SCS curve number CN=[ 75 ],
4402 Previous surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4403 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4404 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4405 LGI=[ 148.099 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4406 Continuous simulation parameters:
4407 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4408 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4409 InterEventTime=[ 18 ](hrs), END=-1
4410 *%
4411 * -JFSA 2021-01-25 add B1 DUALHYD as per Corrigan Report, IBI Group, 2008
4412 COMPUTE DUALHYD NHYDin=[ "B6" ], CINLET=[ 0.064 ](cms), NINLET=[ 1 ],
4413 MajNHYD=[ "B6-MJ" ]
4414 MinNHYD=[ "B6-MN" ]
4415 TMJSTO=[ 5484 ](cu-m)
4416 *%
4417 *CONTINUOUS NASHYD NHYD=[ "B6" ], DT=[ 1 ]min, AREA=[ 3.29 ](ha),
4418 * DWF=[ 0 ](cms), CN/C=[ 75 ], IA=[ 2.5 ](mm),
4419 * N=[ 3.0 ], TP=[ 0.36 ]hrs,
4420 * Continuous simulation parameters:
4421 * IaRECper=[ 4 ](hrs),
4422 * SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4423 * InterEventTime=[ 12 ](hrs)
4424 * Baseflow simulation parameters:
4425 * BaseFlowOption=[ 1 ],
4426 * InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
4427 * VHdCond=[ 0.055 ](mm/hr), END=-1
4428 *%
4429 *% -EX-LAND is external land. It is a part of JOCKVA sub-catchment as per Corrigan
4430 Report, IBI Group, 2008
4431 CONTINUOUS STANDHYD NHYD=[ "EX-LAND" ], DT=[ 1 ]min, AREA=[ 32.5 ](ha),
4432 XIMP=[ 0.50 ], TIMP=[ 0.50 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4433 SCS curve number CN=[ 74 ],
4434 Previous surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4435 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4436 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4437 LGI=[ 465.475 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4438 Continuous simulation parameters:
4439 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4440 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4441 InterEventTime=[ 18 ](hrs), END=-1
4442 *%
4443 COMPUTE DUALHYD NHYDin=[ "EX-LAND" ], CINLET=[ 2.275 ](cms), NINLET=[ 1 ],
4444 MajNHYD=[ "EX-LAND-MJ" ]
4445 MinNHYD=[ "EX-LAND-MN" ]
4446 TMJSTO=[ 1365 ](cu-m)
4447 *%
4448 ADD HYD NHYDsum=[ "B6-B7ExMJ" ], NHYDs to
4449 add=[ "B7R-MJ"+"EX-LAND-MJ"+"B5-MJ"+"B6-MJ"+"B6-MN"+"A8-MJ-B6" ]
4450 *%

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4447 COMPUTE DUALHYD      NHYDin=[ "B6-B7ExMJ" ], CINLET=[ 0.064 ](cms), NINLET=[ 1 ],
4448 MajNHYD=[ "B6R-MJ" ]
4449 MinNHYD=[ "B6R-MN" ]
4450 TMJSTO=[ 5484 ](cu-m)
4451 *%
4452 ROUTE PIPE          PTYPE=[ 1 ]circ, NHYDout=[ "105-106A" ], RNUMBER=[ 1.0 ], PDIAM=[ 1800 ](mm),
4453 PLNGTH=[ 208 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m),
4454 NHYDin=[ "MH105-B6" ], RDT=[ 1 ]
4455 *%
4456 ADD HYD              NHYDsum=[ "MH106A" ], NHYDs to
4457 add=[ "360-106A"+ "105-106A"+ "B6R-MN"+ "B6R-MJ" ]
4458 *%
4459 SAVE HYD             NHYD=[ "MH106A" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4460 HYD_COMMENT=[ "Total Flows at MH106A" ]
4461 *%
4462 ROUTE PIPE          PTYPE=[ 1 ]circ, NHYDout=[ "106A-106" ], RNUMBER=[ 1.0 ], PDIAM=[ 1800 ](mm),
4463 PLNGTH=[ 190 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m),
4464 NHYDin=[ "MH106A" ], RDT=[ 1 ]
4465 *%
4466 CONTINUOUS STANDHYD NHYD=[ "A9" ], DT=[ 1 ]min, AREA=[ 2.44 ](ha),
4467 XIMP=[ 0.71 ], TIMP=[ 0.71 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4468 SCS curve number CN=[ 75 ],
4469 Previous surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4470 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4471 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4472 LGI=[ 262 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4473 Continuous simulation parameters:
4474 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4475 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4476 InterEventTime=[ 18 ](hrs), END=-1
4477 *%
4478 COMPUTE DUALHYD      NHYDin=[ "A9" ], CINLET=[ 0.547 ](cms), NINLET=[ 1 ],
4479 MajNHYD=[ "A9-MJ" ]
4480 MinNHYD=[ "A9-MN" ]
4481 TMJSTO=[ 0 ](cu-m)
4482 *%
4483 ADD HYD              NHYDsum=[ "MH106" ], NHYDs to add=[ "106A-106"+ "A9-MN" ]
4484 *%
4485 SAVE HYD             NHYD=[ "MH106" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4486 HYD_COMMENT=[ "Total Flows at MH106" ]
4487 *%
4488 -JFSA 2021-01-12 THE MANHOLE MH107 is called MH118/107 in Corrigan Report, IBI
4489 Group, July 2008
4490 *%
4491 ROUTE PIPE          PTYPE=[ 1 ]circ, NHYDout=[ "106-107" ], RNUMBER=[ 1.0 ], PDIAM=[ 1800 ](mm),
4492 PLNGTH=[ 122.5 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m),
4493 NHYDin=[ "MH106" ], RDT=[ 1 ]
4494 *%
4495 CONTINUOUS STANDHYD NHYD=[ "A10" ], DT=[ 1 ]min, AREA=[ 4.14 ](ha),
4496 XIMP=[ 0.35 ], TIMP=[ 0.47 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4497 SCS curve number CN=[ 75 ],
4498 Previous surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4499 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4500 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4501 LGI=[ 183 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4502 Continuous simulation parameters:
4503 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4504 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4505 InterEventTime=[ 18 ](hrs), END=-1
4506 *%
4507 COMPUTE DUALHYD      NHYDin=[ "A10" ], CINLET=[ 0.310 ](cms), NINLET=[ 1 ],
4508 MajNHYD=[ "A10-MJ" ]
4509 MinNHYD=[ "A10-MN" ]

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4507 TMJSTO=[ 228 ](cu-m)
4508 *%
4509 CONTINUOUS STANDHYD NHYD=[ "A11" ], DT=[ 1 ]min, AREA=[ 10.61 ](ha),
4510 XIMP=[ 0.53 ], TIMP=[ 0.62 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4511 SCS curve number CN=[ 75 ],
4512 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4513 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4514 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4515 LGI=[ 379 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4516 Continuous simulation parameters:
4517 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4518 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4519 InterEventTime=[ 18 ](hrs), END=-1
4520 *%
4521 COMPUTE DUALHYD NHYDin=[ "A11" ], CINLET=[ 0.993 ](cms), NINLET=[ 1 ],
4522 MajNHYD=[ "A11-MJ" ]
4523 MinNHYD=[ "A11-MN" ]
4524 TMJSTO=[ 556 ](cu-m)
4525 *%
4526 ADD HYD NHYDsum=[ "MH107" ], NHYDs to add=[ "106-107" + "A10-MN" + "A11-MN" ]
4527 *%
4528 SAVE HYD NHYD=[ "MH107" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4529 HYD_COMMENT=[ "Total Flows at MH107" ]
4530 *%
4531 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout=[ "107-119" ], RNUMBER=[ 1.0 ], PDIAM=[ 1800 ](mm),
4532 PLNGTH=[ 114 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0012 ](m/m),
4533 NHYDin=[ "MH107" ], RDT=[ 1 ]
4534 *% -JFSA 2021-01-12 THE MANHOLE MH108 is called MH120/108 in Corrigan Report, IBI
4535 Group, July 2008
4536 *%
4537 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout=[ "119-108" ], RNUMBER=[ 1.0 ], PDIAM=[ 1800 ](mm),
4538 PLNGTH=[ 65.8 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0012 ](m/m),
4539 NHYDin=[ "107-119" ], RDT=[ 1 ]
4540 *%
4541 CONTINUOUS STANDHYD NHYD=[ "A12" ], DT=[ 1 ]min, AREA=[ 12.29 ](ha),
4542 XIMP=[ 0.41 ], TIMP=[ 0.54 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4543 SCS curve number CN=[ 75 ],
4544 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4545 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4546 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4547 LGI=[ 183 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4548 Continuous simulation parameters:
4549 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4550 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4551 InterEventTime=[ 18 ](hrs), END=-1
4552 *%
4553 COMPUTE DUALHYD NHYDin=[ "A12" ], CINLET=[ 1.029 ](cms), NINLET=[ 1 ],
4554 MajNHYD=[ "A12-MJ" ]
4555 MinNHYD=[ "A12-MN" ]
4556 TMJSTO=[ 672 ](cu-m)
4557 *%
4558 CONTINUOUS STANDHYD NHYD=[ "A13" ], DT=[ 1 ]min, AREA=[ 2.59 ](ha),
4559 XIMP=[ 0.71 ], TIMP=[ 0.71 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4560 SCS curve number CN=[ 75 ],
4561 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4562 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4563 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4564 LGI=[ 379 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4565 Continuous simulation parameters:
4566 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4567 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4568 InterEventTime=[ 18 ](hrs), END=-1
4569 *%
4570 COMPUTE DUALHYD NHYDin=[ "A13" ], CINLET=[ 0.571 ](cms), NINLET=[ 1 ],
4571 MajNHYD=[ "A13-MJ" ]

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4570 MinNHYD=[ "A13-MN" ]
4571 TMJSTO=[ 0 ](cu-m)
4572 *%-----|-----|
4573 * -JFSA 2021-01-22 add the Corrigan pond area ("Pond-Block")
4574 CONTINUOUS STANDHYD NHYD=[ "Pond-Block" ], DT=[ 1 ]min, AREA=[ 2.94 ](ha),
4575 XIMP=[ 0.415 ], TIMP=[ 0.415 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4576 SCS curve number CN=[ 75 ],
4577 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4578 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4579 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4580 LGI=[ 183 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4581 Continuous simulation parameters:
4582 IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
4583 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4584 InterEventTime=[ 18 ](hrs), END=-1
4585 *%-----|-----|
4586 ADD HYD NHYDs[ "MH108" ], NHYDs to add=[ "119-108" +"A13-MN" +"A12-MN" ]
4587 *%-----|-----|
4588 SAVE HYD NHYD=[ "MH108" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4589 HYD_COMMENT=[ "Total Flows at MH108" ]
4590 *%-----|-----|
4591 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout=[ "108-116" ], RNUMBER=[ 1.0 ], PDIAM=[ 1800 ](mm),
4592 PLNGTH=[ 76.6 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0013 ](m/m),
4593 NHYDin=[ "MH108" ], RDT=[ 1 ]
4594 *%-----|-----|
4594 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout=[ "116-corrig" ], RNUMBER=[ 1.0 ],
4595 PDIAM=[ 1800 ](mm),
4596 PLNGTH=[ 79.5 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0013 ](m/m),
4597 NHYDin=[ "108-116" ], RDT=[ 1 ]
4598 *%-----|-----|
4598 ADD HYD NHYDs[ "Corrigan" ], NHYDs to add=[ "116-corrig" +"Pond-Block" ]
4599 *%-----|-----|
4600 SAVE HYD NHYD=[ "Corrigan" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4601 HYD_COMMENT=[ "Total Flows at Corrigan Pond" ]
4602 *%-----|-----|
4602 ROUTE RESERVOIR NHYDout=[ "Co-P" ], NHYDin=[ "Corrigan" ],
4603 RDT=[ 1 ](min),
4604 TABLE of ( OUTFLOW-STORAGE ) values
4605 (cms) - (ha-m)
4606 [ 0.0 , 0.0 ]
4607 [ 0.015 , 0.04118 ]
4608 [ 0.030 , 0.08297 ]
4609 [ 0.045 , 0.12537 ]
4610 [ 0.060 , 0.16837 ]
4611 [ 0.075 , 0.21199 ]
4612 [ 0.090 , 0.27545 ]
4613 [ 0.105 , 0.34650 ]
4614 [ 0.120 , 0.42049 ]
4615 [ 0.135 , 0.50188 ]
4616 [ 0.186 , 0.60307 ]
4617 [ 2.110 , 0.79083 ]
4618 [ 5.874 , 1.00271 ]
4619 [ 11.395 , 1.29643 ]
4620 [ 18.770 , 1.62054 ]
4621 [ 28.143 , 1.97516 ]
4622 [ -1 , -1 ] (max twenty pts)
4623 NHYDovf=[ "Co-P-OVF" ]
4624 *%-----|-----|
4625 ADD HYD NHYDs[ "corrige" ], NHYDs to
4626 add=[ "Co-P-OVF" +"Co-P" +"N_TO" +"MH105-JR" +"A8-MJ-JR" +"A9-MJ" +"A10-MJ" +"A11-MJ" +"A12-MJ" +"A
4627 13-MJ" ]
4628 *%-----|-----|
4628 SAVE HYD NHYD=[ "corrige" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4629 HYD_COMMENT=[ "Total Flows at Corrigan Pond" ]
4630 *#*****#

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4631 *#      Corrigan Pond 1
4632 *#      - Rating curve obtained from Barrhaven South MSS modeling
4633 *#      - Tributary Drainage Area to MSS Pond 1 = 145 ha
4634 *#####
4635 *ROUTE RESERVOIR      NHYDout=[ "MS_P1" ],   NHYDin=[ "CORRIG" ],
4636 *          RDT=[1](min),
4637 *          TABLE of ( OUTFLOW-STORAGE ) values
4638 *          (cms) - (ha-m)
4639 *          [    0.0 ,  0.0 ]
4640 *          [    0.06 , 0.58]
4641 *          [     -1 ,   -1 ] (max twenty pts)
4642 *          NHYDovf= [ "P1-OVF" ]
4643 *%-----|-----|
4644 *ADD HYD      NHYDsum=[ "SN_CO" ],  NHYDs to add=[ "N_TO"+"P1-OVF"+"MS_P1" ]
4645 *%-----|-----|
4646 *SAVE HYD      NHYD=[ "SN_CO" ],    # OF PCYCLES=[-1],  ICASEsh=[1]
4647 *          HYD_COMMENT=[ "Total Flows at Corrigan Drain" ]
4648 *%-----|-----|
4649 *#
4650 *# Hydrograph from Corrigan Drain routed to Jockvale Road
4651 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
4652 *#
4653 ROUTE CHANNEL      NHYDout=[ "N_MI" ] ,NHYDin=[ "corrige" ] ,
4654 *          RDT=[1](min),
4655 *          CHLGTH=[580](m),   CHSLOPE=[0.4448](%),
4656 *          FPSLOPE=[0.4448](%),
4657 *          SECNUM=[1.0],      NSEG=[3]
4658 *          ( SEGROUGH, SEGDIST (m))=
4659 *          [0.075,-17.72
4660 *          -0.045,17.72
4661 *          0.075,80.62] NSEG times
4662 *          ( DISTANCE (m), ELEVATION (m))=
4663 *          [-83.32, 90.00]
4664 *          [-81.36, 89.50]
4665 *          [-79.12, 89.00]
4666 *          [-76.13, 88.50]
4667 *          [-20.46, 88.00]
4668 *          [-19.36, 87.50]
4669 *          [-18.51, 87.00]
4670 *          [-17.72, 86.50]
4671 *          [-11.95, 85.24]
4672 *          [-0.11, 85.12]
4673 *          [11.49, 85.20]
4674 *          [17.72, 86.50]
4675 *          [19.74, 87.00]
4676 *          [21.22, 87.50]
4677 *          [22.68, 88.00]
4678 *          [24.28, 88.50]
4679 *          [26.79, 89.00]
4680 *          [71.98, 90.00]
4681 *          [80.62, 90.50]
4682 *%-----|-----|
4683 *#####
4684 *#      Catchment MILLS
4685 *#      - To SWM Facility north of the Jock
4686 *#      - Primarily residential development
4687 *#####
4688 CONTINUOUS STANDHYD NHYD=[ "MILLS" ], DT=[1]min, AREA=[175.99](ha),
4689 *          XIMP=[0.38], TIMP=[0.38], DWF=[0](cms), LOSS=[2],
4690 *          SCS curve number CN=[74],
4691 *          Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4692 *          LGP=[40](m), MNP=[0.25], SCP=[0](min),
4693 *          Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4694 *          LGI=[1118.123](m), MNI=[0.013], SCI=[0](min),
4695 *          Continuous simulation parameters:
4696 *          IaRECper=[4](hrs),  IaRECImp=[4](hrs),

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4697           SMIN=[-1](mm),   SMAX=[-1](mm),   SK=[0.010]/(mm),
4698           InterEventTime=[18](hrs),      END=-1
4699 *%-----|-----|-----|-----|-----|-----|-----|-----|-----|
4700 *#*****|-----|-----|-----|-----|-----|-----|-----|-----|
4701 *#     Chapman Mills SWM Pond
4702 *#     - Rating curve obtained from CCL hydraulic modeling
4703 *#*****|-----|-----|-----|-----|-----|-----|-----|-----|
4704 ROUTE RESERVOIR    NHYDout=[ "MILL_P" ],   NHYDin=[ "MILLS" ],
4705          RDT=[1](min),
4706          TABLE of ( OUTFLOW-STORAGE ) values
4707          (cms) - (ha-m)
4708          [ 0.0 , 0.0 ]
4709          [ 0.01 , 0.01]
4710          [ 0.05 , 0.06]
4711          [ 0.09 , 0.11]
4712          [ 0.13 , 0.15]
4713          [ 0.18 , 0.19]
4714          [ 0.28 , 0.28]
4715          [ 0.37 , 0.34]
4716          [ 0.45 , 0.40]
4717          [ 0.51 , 0.44]
4718          [ 0.56 , 0.47]
4719          [ 0.64 , 0.52]
4720          [ 0.76 , 0.59]
4721          [ 0.86 , 0.65]
4722          [ 1.09 , 0.78]
4723          [ 1.44 , 0.96]
4724          [ 3.18 , 1.84]
4725          [ 4.05 , 2.31]
4726          [ -1 , -1 ] (max twenty pts)
4727          NHYDovf=[ "MIL-OV" ]
4728 *%-----|-----|-----|-----|-----|-----|-----|-----|-----|
4729 ADD HYD          NHYDsum=[ "SN_MI" ],   NHYDs to add=[ "N_MI"+"MIL-OV"+"MILL_P" ]
4730 *%-----|-----|-----|-----|-----|-----|-----|-----|-----|
4731 SAVE HYD         NHYD=[ "SN_MI" ],   # OF PCYCLES=[-1],   ICASEsh=[1]
4732          HYD_COMMENT=[ "Total Flows at Jockvale Road" ]
4733 *%-----|-----|-----|-----|-----|-----|-----|-----|-----|
4734 *#
4735 *# Hydrograph from Jockvale Road routed to Heart's Desire
4736 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 689
4737 *#
4738 ROUTE CHANNEL      NHYDout=[ "N_DE" ] ,NHYDin=[ "SN_MI" ] ,
4739          RDT=[1](min),
4740          CHLGTH=[1962](m),   CHSLOPE=[0.2227](%),   FPSLOPE=[0.2227](%),
4741          SECNUM=[1.0],      NSEG=[3]
4742          ( SEGRROUGH, SEGDIST (m))=
4743          [0.075,-17.56
4744          -0.045,18.27
4745          0.075,32.51] NSEG times
4746          ( DISTANCE (m), ELEVATION (m))=
4747          [-54.07, 85.00]
4748          [-39.43, 84.50]
4749          [-28.30, 84.00]
4750          [-24.12, 83.50]
4751          [-22.30, 83.00]
4752          [-20.55, 82.50]
4753          [-17.56, 82.00]
4754          [-12.63, 81.22]
4755          [-0.11, 80.75]
4756          [11.55, 81.22]
4757          [18.27, 82.00]
4758          [19.82, 82.50]
4759          [22.48, 83.00]
4760          [27.90, 83.50]
4761          [29.31, 84.00]

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4763 [30.81, 84.50]
4764 [32.51, 85.00]
4765 *%-----|-----|-----|-----|-----|-----|-----|-----|
4766 *#*****|-----|-----|-----|-----|-----|-----|-----|-----|
4767 *#     Catchment DESIRE
4768 *#     - To Jock River (north of the Jock)
4769 *#     - Rural-estate subdivision (Heart's Desire Community)
4770 *#*****|-----|-----|-----|-----|-----|-----|-----|-----|
4771 CONTINUOUS STANDHYD NHYD=[ "DESIRE" ], DT=[1]min, AREA=[ 23.78 ](ha),
4772 XIMP=[ 0.25 ], TIMP=[ 0.25 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4773 SCS curve number CN=[ 77 ],
4774 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4775 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4776 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4777 LGI=[ 400 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4778 Continuous simulation parameters:
4779 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4780 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4781 InterEventTime=[ 18 ](hrs), END=-1
4782 *%-----|-----|-----|-----|-----|-----|-----|-----|
4783 *#*****|-----|-----|-----|-----|-----|-----|-----|-----|
4784 *#     Catchment JOCKVA
4785 *#     - To Jockvale SWM Facility
4786 *#     - Residential development & golf course
4787 *#     - JFSA 2021-01-11 update JOCKVA after updating CORRIG as per IBI GROUP, July 2008.
4788 *#     JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two
4789 areas JOCKVA and EX-LAND 32.5 ha as per IBI GROUP, July 2008.
4790 *#*****|-----|-----|-----|-----|-----|-----|-----|-----|
4791 CONTINUOUS STANDHYD NHYD=[ "JOCKVA" ], DT=[1]min, AREA=[ 225.13 ](ha),
4792 XIMP=[ 0.50 ], TIMP=[ 0.50 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4793 SCS curve number CN=[ 74 ],
4794 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4795 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4796 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4797 LGI=[ 1310.55 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4798 Continuous simulation parameters:
4799 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4800 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4801 InterEventTime=[ 18 ](hrs), END=-1
4802 *%-----|-----|-----|-----|-----|-----|-----|-----|
4803 ADD HYD NHYDsum=[ "JOCKVA-TO" ], NHYDs to
4804 add=[ "EX-LAND-MN" + "JOCKVA" + "B2-MJ" + "B3-MJ" ]
4805 *%-----|-----|-----|-----|-----|-----|-----|-----|
4806 SAVE HYD NHYD=[ "JOCKVA-TO" ], # OF PCYCLES=[ -1 ], ICASESh=[ 1 ]
4807 HYD_COMMENT=[ "Total Flows at KB first pond" ]
4808 *%-----|-----|-----|-----|-----|-----|-----|-----|
4809 *#     Jockvale SWM Facility
4810 *#     - Rating curve obtained from Jockvale Servicing Study (CCL 1999)
4811 *#*****|-----|-----|-----|-----|-----|-----|-----|-----|
4812 ROUTE RESERVOIR NHYDout=[ "JOCK_P" ], NHYDin=[ "JOCKVA-TO" ],
4813 RDT=[ 1 ](min),
4814             TABLE of ( OUTFLOW-STORAGE ) values
4815             (cms) - (ha-m)
4816             [ 0.0 , 0.0 ]
4817             [ 0.27 , 0.03 ]
4818             [ 0.28 , 0.55 ]
4819             [ 0.29 , 1.14 ]
4820             [ 0.30 , 1.80 ]
4821             [ 0.31 , 2.32 ]
4822             [ 1.12 , 2.87 ]
4823             [ 2.92 , 3.45 ]
4824             [ 4.64 , 4.07 ]
4825             [ 6.69 , 4.72 ]
4826             [ 9.02 , 5.39 ]
4827             [ 11.62 , 6.10 ]

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4827 [ 14.42 , 6.85]
4828 [ 17.45 , 7.62]
4829 [ 20.69 , 8.44]
4830 [ 24.08 , 9.28]
4831 [ 27.68 , 10.17]
4832 [ -1 , -1 ] (max twenty pts)
4833 NHYDovf=[ "JO-OVF" ]
4834 *%-----|-----|
4835 ADD HYD NHYDsum=[ "SN_DE" ] , NHYDs to add=[ "N_DE"+"DESIRE"+"JO-OVF"+"JOCK_P" ]
4836 *%-----|-----|
4837 SAVE HYD NHYD=[ "SN_DE" ] , # OF PCYCLES=[-1] , ICASEsh=[1]
4838 HYD_COMMENT=[ "Total Flows at Heart's Desire" ]
4839 *%-----|-----|
4840 *#
4841 *# Hydrograph from Heart's Desire routed to Rideau River
4842 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 0
4843 *#
4844 ROUTE CHANNEL NHYDout=[ "N1" ] , NHYDin=[ "SN_DE" ] ,
4845 RDT=[1](min),
4846 CHLGTH=[563](m), CHSLOPE=[0.9668](%),
4847 FPSLOPE=[0.9668](%),
4848 SECNUM=[1.0], NSEG=[3]
4849 ( SEGROUGH, SEGDIST (m))=
4850 [0.075,-30.20
4851 -0.045,30.20
4852 0.075,48.48] NSEG times
4853 ( DISTANCE (m), ELEVATION (m))=
4854 [-98.46, 81.50]
4855 [-92.24, 81.00]
4856 [-86.88, 80.50]
4857 [-81.54, 80.00]
4858 [-74.36, 79.50]
4859 [-63.54, 79.00]
4860 [-39.23, 78.50]
4861 [-34.51, 78.00]
4862 [-33.01, 77.50]
4863 [-30.20, 77.00]
4864 [-13.42, 76.18]
4865 [-1.14, 76.09]
4866 [17.06, 76.18]
4867 [30.20, 77.00]
4868 [32.95, 77.50]
4869 [34.06, 78.00]
4870 [35.11, 78.50]
4871 [36.32, 79.00]
4872 [37.74, 79.50]
4873 [48.48, 81.50]
4874 *%-----|-----|
4875 *#*****|-----|
4876 *# Catchment S-2
4877 *# - To Jock River (north and south)
4878 *# - Undeveloped floodplain and river
4879 *#*****|-----|
4880 CONTINUOUS NASHYD NHYD=[ "S-2" ] , DT=[1]min, AREA=[102.94](ha) ,
4881 DWF=[0](cms), CN/C=[72], IA=[4.67](mm),
4882 N=[3], TP=[0.40]hrs,
4883 Continuous simulation parameters:
4884 IaRECper=[4](hrs),
4885 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4886 InterEventTime=[12](hrs)
4887 Baseflow simulation parameters:
4888 BaseFlowOption=[1],
4889 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4890 VHydCond=[0.055](mm/hr), END=-1
4891 *%-----|-----|
4892 ADD HYD NHYDsum=[ "SN_N1" ] , NHYDs to add=[ "N1"+"S-2" ]

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4893 *%-----|-----|
4894 SAVE HYD          NHYD=[ "SN_N1" ],      # OF PCYCLES=[-1],  ICASEsh=[1]
4895           HYD_COMMENT=[ "Total Flows at Rideau River" ]
4896 *%-----|-----|
4897 *##########
4898 *% 5 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4899 START            TZERO=[0.0],   METOUT=[2],   NSTORM=[1],   NRUN=[5]
4900           [%C24SC005.stm"] <--storm filename, one per line for NSTORM time
4901 *%-----|-----|
4902 *% 10 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4903 START            TZERO=[0.0],   METOUT=[2],   NSTORM=[1],   NRUN=[10]
4904           [%C24SC010.stm"] <--storm filename, one per line for NSTORM time
4905 *%-----|-----|
4906 *% 25 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4907 START            TZERO=[0.0],   METOUT=[2],   NSTORM=[1],   NRUN=[25]
4908           [%C24SC025.stm"] <--storm filename, one per line for NSTORM time
4909 *%-----|-----|
4910 *% 50 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4911 START            TZERO=[0.0],   METOUT=[2],   NSTORM=[1],   NRUN=[50]
4912           [%C24SC050.stm"] <--storm filename, one per line for NSTORM time
4913 *%-----|-----|
4914 *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4915 *START            TZERO=[0.0],   METOUT=[2],   NSTORM=[1],   NRUN=[100]
4916           [%100YC3H.STM"] <--storm filename, one per line for NSTORM time
4917 *%-----|-----|
4918 *% 100 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4919 START            TZERO=[0.0],   METOUT=[2],   NSTORM=[1],   NRUN=[100]
4920           [%C24SC100.stm"] <--storm filename, one per line for NSTORM time
4921 *%-----|-----|
4922 *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4923 *START            TZERO=[0.0],   METOUT=[2],   NSTORM=[1],   NRUN=[100]
4924           [%C24SC100.stm"] <--storm filename, one per line for NSTORM time
4925 *START            TZERO=[0.0],   METOUT=[2],   NSTORM=[1],   NRUN=[101]
4926           [%A24SC100.stm"] <--storm filename, one per line for NSTORM time
4927 *START            TZERO=[0.0],   METOUT=[2],   NSTORM=[1],   NRUN=[102]
4928           [%A24SC100_60.stm"] <--storm filename, one per line for NSTORM time
4929 FINISH
4930

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00001> \*\*\*\*  
00002> SSSSS W W M M H H Y Y M M 000 222 000 11 5555 \*\*\*\*\*  
00004> S W W N M M H H Y Y M M 0 0 2 0 0 11 5 Ver: 6.600  
00005> SSSSS W W M M H H Y Y M M 000 222 0 0 11 555 FEB 2015  
00007> SSSSS W W M M H H Y M M 000 222 0 0 11 5 \* 000  
00008> Stormwater Management Hydrologic Model 222 000 11 455 \*\*\*\*\*  
00010>  
00012> \*\*\*\*\* SWMMHYD Version 5.600 \*\*\*  
00013> \* A single event and continuous hydrologic simulation model  
00014> \* based on the SWMM model and its successors  
00015> \* CTHNHYD-83 and CTHNHYD-89.  
00016> \*  
00017> \* Distributed by: J. Fabre & Associates Inc.  
00018> \* Ottawa, Ontario: (613) 836-3884  
00019> \* Gatineau, Quebec: (819) 243-6858  
00020> \* E-mail: jfainc@jfainc.ca  
00021> \*  
00022>  
00024> \* Licensed user: JFSAinc.  
00025> \* Ottawa SERIAL# 2549237 \*\*\*\*\*  
00027>  
00028> \*\*\*\*\* PROGRAM ARRAY DIMENSIONS \*\*\*\*\*  
00029> \* Maximum value for ID numbers : 11 \*\*\*\*\*  
00030> \* Max. number of rainfall points: 105408 \*\*\*\*\*  
00031> \* Max. number of nodes: 105408 \*\*\*\*\*  
00032> \*  
00033> \*  
00034>  
00035> \* S U M M A R Y O U T P U T \*  
00036> \*  
00037> \* RUN DATE: 2021-03-04 TIME: 11:49:14 RUN COUNT: 02082 \*  
00038> \*  
00039> \* Input file: T:\R\ON\1474-16\Design\20210126\QuantityControlAnalysis\SWMMHYD\SMR-Model\updated\\*  
00040> \* Output file: T:\R\ON\1474-16\Design\20210126\QuantityControlAnalysis\SWMMHYD\SMR-Model\updated\\*  
00041> \* Summary file: T:\R\ON\1474-16\Design\20210126\QuantityControlAnalysis\SWMMHYD\SMR-Model\updated\\*  
00042> \* 3\SWMM\_S\_1-Fr-Nash.sum  
00043> \* User comments:  
00044> \* 2:  
00045> \* 3:  
00046>  
00047> \*  
00048> \*  
00049> \*  
00051>  
00052>  
00053> # SWMMHYD Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE  
00054> #  
00055> # Project Name: [Rock River] Project Number: [1474-16]  
00056> # Date : 04-03-2021  
00057> # Modeler : [JFSAinc]  
00058> # Company : [JFSAinc]  
00059> # License #: 1549237  
00060>  
00062> # CALIBRATION OF SUMMER MODEL PARAMETERS  
00063> # USING CONTINUOUS SIMULATIONS  
00064> # Rainfall data from JFSA rain gauge installed at site + other gauges by the City  
00065> # Use data collected from May 1st to July 14, 2003  
00066> # 2020-11-30 change TMNSTO to COMPUTE DUALYD (TMNSTO = 0.1 instead of 0.0001)  
00067> # 2020-12-12 change W\_CLAR\_BXAP to 0.55, SLP1=(0.5%) (imperious slope), and LGI up to 700m  
00068> # 2021-02-19 Change the slope for ROUTE CHANNEL Station 2442 (NHYDout["N\_TO"], NHYDin["SN\_TO"]) from 0.033 % (as per S  
00069> # 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHYDout["N\_MC"], NHYDin["SN\_CE"]) from 0.01 % (as per S  
00070> #  
00071> # END OF RUN : 1  
00072> \*\* END OF RUN :  
00073>  
00074> #  
00075> #  
00076> #  
00077> #  
00078> #  
00079> #  
00080> RUNS=COMMAND#  
00081> R0021:CO0001--  
00082> #  
00083> # [TZERO = 0.00 hrs on 0] #  
00084> # [METOUT = 2 (1=imperial, 2=metric output)] #  
00085> # [NRUN = 0000] #  
00086> # [NRUN = 0000] #  
00087> #  
00088> # SWMMHYD Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE  
00089> #  
00090> # Project Name: [Rock River] Project Number: [1474-16]  
00091> # Date : 04-03-2021  
00092> # Modeler : [JFSAinc]  
00093> # Company : [JFSAinc]  
00094> # License #: 1549237  
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00376+ #  
00376+ R0021:00039-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00377+ ADD HYD  
00378+ + 1.0 021SW\_11 8506.00 7.379 No\_date 33:12 11.20 n/a .000  
00379+ + 1.0 021SW\_11 500.00 2.720 No\_date 29:22 11.98 n/a .000  
00380+ SUM+ 1.0 021SW\_11 9197.00 4.042 No\_date 34:34 11.98 n/a .000  
00381+ SML+ 1.0 018.S.M11 11923.00 12.077 No\_date 33:14 11.96 n/a .000  
00382+ # Sum of hydrographs from Node 11 routed to Node 10  
00383+ # Section 1  
00384+ #  
00384+ R0021:00040-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00385+ ROUTE CHANNEL -> 1.0 021S.XM1 11923.00 12.077 No\_date 33:14 11.36 n/a .000  
00386+ [ROT= 1.00] out+ 1.0 01N10 11923.00 8.276 No\_date 39:46 11.36 n/a .000  
00387+ [L/S/n=.14628/. .157/.040]  
00388+ [Vmax=.462 Dmax=.888]  
00389+ #  
00390+ # Addition of Subwatershed 10 to Node 10  
00391+ #  
00392+ R0021:00041-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00393+ ADD HYD  
00394+ + 1.0 021SW\_10 11923.00 8.276 No\_date 39:46 11.36 n/a .000  
00395+ SUM+ 1.0 018.S.M10 17889.00 15.451 No\_date 38:31 12.19 n/a .000  
00396+ SAVE HYD  
00397+ fname : H\_SMX10  
00398+ # Addition of Kings Creek to S\_M10  
00399+ #  
00400+ R0021:00043-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00401+ ADD HYD  
00402+ + 1.0 021X.S10 17889.00 19.451 No\_date 38:31 12.19 n/a .000  
00403+ SUM+ 1.0 021KG\_CK 8376.00 11.072 No\_date 39:59 11.98 n/a .000  
00404+ SML+ 1.0 018.S.M10A 25968.00 30.328 No\_date 39:58 12.12 n/a .000  
00405+ #  
00406+ # Sum of hydrographs from Node 10 routed to Node 9  
00407+ # Section 2  
00408+ #  
00409+ R0021:00044-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00410+ ROUTE CHANNEL -> 1.0 021S.XM10 25968.00 30.328 No\_date 39:58 12.11 n/a .000  
00411+ [ROT= 1.00] out+ 1.0 01N10 25968.00 29.579 No\_date 39:58 12.12 n/a .000  
00412+ [L/S/n=.3982/. .057/.040]  
00413+ [Vmax=.595 Dmax=.1208]  
00414+ #  
00415+ # Addition of Subwatershed 9 and Nichols Creek to Node 9  
00416+ #  
00417+ #  
00418+ R0021:00045-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00419+ ADD HYD  
00420+ + 1.0 021H\_N 25968.00 29.579 No\_date 39:58 12.12 n/a .000  
00421+ + 1.0 021H\_N 1132.00 1.000 No\_date 39:58 12.12 n/a .000  
00422+ SUM+ 1.0 021NC\_CK 4464.00 5.504 No\_date 39:59 10.98 n/a .000  
00423+ SML+ 1.0 018.S.M10A 31561.00 36.313 No\_date 39:59 12.00 n/a .000  
00424+ #  
00425+ # Sum of hydrographs from Node 9 routed to Node 8  
00426+ # Section 3  
00427+ #  
00428+ R0021:00046-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00429+ ROUTE CHANNEL -> 1.0 021S.N10 31561.00 36.313 No\_date 39:59 12.00 n/a .000  
00430+ [ROT= 1.00] out+ 1.0 01N10 31561.00 34.173 No\_date 39:59 12.00 n/a .000  
00431+ [L/S/n=.2269/. .088/.048]  
00432+ [Vmax=.418 Dmax=.1281]  
00433+ #  
00434+ # Addition of Subwatershed 8 and Hobbs's Drain to Node 8  
00435+ #  
00436+ R0021:00047-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00437+ ADD HYD  
00438+ + 1.0 021H\_N 31561.00 34.173 No\_date 39:59 12.00 n/a .000  
00439+ + 1.0 021H\_N 3854.00 6.242 No\_date 38:46 11.98 n/a .000  
00440+ SUM+ 1.0 018.S.M10A 35846.00 40.474 No\_date 39:59 12.00 n/a .000  
00441+ #  
00442+ # Sum of hydrographs from Node 8 routed to Node 7  
00443+ # Section 4  
00444+ #  
00445+ R0021:00048-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00446+ ROUTE CHANNEL -> 1.0 021S.N8 35846.00 40.474 No\_date 39:59 12.00 n/a .000  
00447+ [ROT= 1.00] out+ 1.0 01N10 35846.00 32.891 No\_date 44:30 12.00 n/a .000  
00448+ [L/S/n=.3750/. .053/.070]  
00449+ [Vmax=.208 Dmax=.1651]  
00450+ #  
00451+ # Addition of Subwatershed 7 to Node 7  
00452+ #  
00453+ R0021:00049-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00454+ ADD HYD  
00455+ + 1.0 021H\_N 35846.00 32.891 No\_date 44:30 12.00 n/a .000  
00456+ + 1.0 021SW\_7 3197.00 4.651 No\_date 36:31 9.85 n/a .000  
00457+ SUM+ 1.0 018.S.M8 38544.00 32.891 No\_date 44:30 12.00 n/a .000  
00458+ SAVE HYD  
00459+ fname : H\_LNNT  
00460+ #  
00461+ # Function of a resistor to simulate the effects of the Richland Pen.  
00462+ # Store the flow volumes as estimated from available topo maps.  
00463+ # Release rate for pen was assumed to be controlled by the downstream  
00464+ # river cross-section for summer conditions. It was assumed that for up to  
00465+ # 10% of the flow in the river would be stored in the storage. Above  
00466+ # this depth, the wetlands start to significantly store water.  
00467+ #  
00468+ R0021:00051-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00469+ ROUTE RESERVOIR --> 1.0 021RES\_RF 38743.00 35.071 No\_date 43:33 11.82 n/a .000  
00470+ [McGCodes-.001802-.001802]  
00471+ #  
00472+ R0021:00052-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00473+ SML+ 1.0 018.S.MF 38743.00 23.265 No\_date 55:09 11.82 n/a .000  
00474+ #  
00475+ #  
00476+ #  
00477+ # Sum of hydrographs from Node 7 routed to Node 6  
00478+ # Section 5  
00479+ #  
00480+ R0021:00053-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00481+ ROUTE CHANNEL -> 1.0 021RES\_RF 38743.00 23.265 No\_date 55:09 11.82 n/a .000  
00482+ [ROT= 1.00] out+ 1.0 01N10 38743.00 23.228 No\_date 55:09 11.82 n/a .000  
00483+ [L/S/n=.3056/. .082/.028]  
00484+ [Vmax=.432 Dmax=.808]  
00485+ #  
00486+ # Addition of Subwatershed 6 and Van Gaal Drain to Node 6  
00487+ #  
00488+ R0021:00054-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00489+ ADD HYD  
00490+ + 1.0 021S.N6 38743.00 23.228 No\_date 54:58 11.82 n/a .000  
00491+ + 1.0 021SW\_6 165.00 .413 No\_date 33:07 12.24 n/a .000  
00492+ SUM+ 1.0 018.S.M6 38743.00 23.228 No\_date 54:58 11.82 n/a .000  
00493+ SML+ 1.0 018.S.M6 40240.01 23.318 No\_date 54:59 11.89 n/a .000  
00494+ #  
00495+ # Sum of hydrographs from Node 6 routed to Node 5  
00496+ # Section 6  
00497+ #  
00498+ R0021:00055-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00499+ ROUTE CHANNEL -> 1.0 021S.N6 40240.01 23.318 No\_date 54:58 11.82 n/a .000  
00500+ [ROT= 1.00] out+ 1.0 01N10 40240.01 23.285 No\_date 54:58 11.89 n/a .000  
00501+ [Vmax=.378 Dmax=.917]  
00502+ #  
00503+ # Addition of Subwatershed 5 and Flowing Creek to Node 5  
00504+ #  
00505+ R0021:00056-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00506+ ADD HYD  
00507+ + 1.0 021S.N5 40240.01 23.285 No\_date 54:59 11.82 n/a .000  
00508+ + 1.0 021SW\_5 224.00 2.597 No\_date 28:45 15.91 n/a .000  
00509+ + 1.0 021FL\_CK 4945.00 14.839 No\_date 33:25 14.57 n/a .000  
00510+ SUM+ 1.0 018.S.M5 40409.01 53.166 No\_date 37:08 12.30 n/a .000  
00511+ #  
00512+ # Sum of hydrographs from Node 5 routed to Node 5A  
00513+ # Section 7  
00514+ #  
00515+ R0021:00057-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00516+ ROUTE CHANNEL -> 1.0 021S.N5 45409.01 33.185 No\_date 37:08 12.20 n/a .000  
00517+ [ROT= 1.00] out+ 1.0 01N10 45409.01 33.135 No\_date 37:08 12.20 n/a .000  
00518+ [L/S/n=.0907/. .0907/.040]  
00519+ [Vmax=.443 Dmax=.897]  
00520+ #  
00521+ # Addition of Subwatershed 5A and Subwatershed 5A2 to Node 5A  
00522+ #  
00523+ R0021:00058-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00524+ ADD HYD  
00525+ + 1.0 021SW\_5A 20.00 .399 No\_date 28:36 17.79 n/a .000  
00526+ + 1.0 021SW\_5A1 1412.00 3.090 No\_date 38:04 15.22 n/a .000  
00527+ SUM+ 1.0 018.S.M5A 46841.01 36.236 No\_date 37:26 12.30 n/a .000  
00528+ #  
00529+ # Sum of hydrographs from Node 5A routed to Node 4  
00530+ # Section 8  
00531+ #  
00532+ R0021:00059-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00533+ ROUTE CHANNEL -> 1.0 021S.N5A 46841.01 36.236 No\_date 37:26 12.30 n/a .000  
00534+ [ROT= 1.00] out+ 1.0 01N10 46841.01 35.288 No\_date 39:22 12.30 n/a .000  
00535+ [L/S/n=.4630/. .043/.035]  
00536+ [Vmax=.495 Dmax=.2844]  
00537+ #  
00538+ # Addition of Subwatershed 4 and Leamy Creek to Node 4  
00539+ #  
00540+ R0021:00060-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00541+ ADD HYD  
00542+ + 1.0 021N10 46841.01 35.288 No\_date 39:22 12.30 n/a .000  
00543+ + 1.0 021SW\_4 1021.00 5.747 No\_date 30:50 17.39 n/a .000  
00544+ + 1.0 021NC\_CK 48447.00 37.581 No\_date 38:11 12.47 n/a .000  
00545+ SUM+ 1.0 018.S.M4 48447.00 37.581 No\_date 38:11 12.47 n/a .000  
00546+ SAVE HYD  
00547+ fname : S.M4.0002  
00548+ #  
00549+ # Sum of hydrographs from Node 4 routed to Node 2  
00550+ # Section 9  
00551+ #  
00552+ R0021:00061-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00553+ ROUTE CHANNEL -> 1.0 021S.N4 48447.00 37.581 No\_date 38:13 12.47 n/a .000  
00554+ [ROT= 1.00] out+ 1.0 01N2 48447.00 37.455 No\_date 38:49 12.47 n/a .000  
00555+ [L/S/n=.1667/. .060/.040]  
00556+ [Vmax=.715 Dmax=.2844]  
00557+ #  
00558+ # Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2  
00559+ #  
00560+ R0021:00063-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00561+ ADD HYD  
00562+ + 1.0 021N2 48447.00 37.455 No\_date 38:49 12.47 n/a .000  
00563+ #  
00564+ # Sum of hydrographs from Node 2 routed to Node 1  
00565+ # Section 10  
00566+ #  
00567+ R0021:00040-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00568+ ROUTE CHANNEL -> 1.0 021S.XM1 11923.00 12.077 No\_date 33:14 11.36 n/a .000  
00569+ [ROT= 1.00] out+ 1.0 01N10 11923.00 8.276 No\_date 39:46 11.36 n/a .000  
00570+ [L/S/n=.14628/. .157/.040]  
00571+ [Vmax=.462 Dmax=.888]  
00572+ #  
00573+ # Addition of Subwatershed 10 to Node 10  
00574+ #  
00575+ R0021:00041-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00576+ ADD HYD  
00577+ + 1.0 021SW\_10 11923.00 8.276 No\_date 39:46 11.36 n/a .000  
00578+ + 1.0 021NC\_CW 5666.00 11.228 No\_date 38:07 35:19 13.94 n/a .000  
00579+ SUM+ 1.0 018.S.M10 17889.00 15.451 No\_date 38:31 12.19 n/a .000  
00580+ SAVE HYD  
00581+ fname : H\_SMX10  
00582+ #  
00583+ # Addition of Kings Creek to S\_M10  
00584+ #  
00585+ R0021:00043-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00586+ ADD HYD  
00587+ + 1.0 021X.S10 17889.00 19.451 No\_date 38:31 12.19 n/a .000  
00588+ + 1.0 021KG\_CK 8376.00 11.072 No\_date 39:59 11.98 n/a .000  
00589+ SUM+ 1.0 018.S.M10A 25968.00 30.328 No\_date 39:58 12.12 n/a .000  
00590+ SAVE HYD  
00591+ fname : S.M10A.0002  
00592+ #  
00593+ # Addition of Nichols Creek to Node 9  
00594+ #  
00595+ R0021:00044-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00596+ ADD HYD  
00597+ + 1.0 021S.XM10 25968.00 30.328 No\_date 39:58 12.11 n/a .000  
00598+ + 1.0 021NC\_CW 5666.00 11.228 No\_date 38:07 35:19 13.94 n/a .000  
00599+ SUM+ 1.0 018.S.M10 17889.00 15.451 No\_date 38:31 12.19 n/a .000  
00600+ SAVE HYD  
00601+ fname : H\_SMX10  
00602+ #  
00603+ # Addition of Kings Creek to S\_M10  
00604+ #  
00605+ R0021:00045-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00606+ ADD HYD  
00607+ + 1.0 021H\_N 25968.00 29.579 No\_date 39:58 12.12 n/a .000  
00608+ + 1.0 021H\_N 1132.00 1.000 No\_date 39:58 12.12 n/a .000  
00609+ SUM+ 1.0 021NC\_CW 4464.00 5.504 No\_date 39:59 10.98 n/a .000  
00610+ SML+ 1.0 018.S.M10A 31561.00 36.313 No\_date 39:59 12.00 n/a .000  
00611+ #  
00612+ R0021:00046-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00613+ ADD HYD  
00614+ + 1.0 021S.XM10 31561.00 36.313 No\_date 39:59 12.00 n/a .000  
00615+ + 1.0 021NC\_CW 4464.00 5.504 No\_date 39:59 10.98 n/a .000  
00616+ SUM+ 1.0 018.S.M10A 35846.00 40.474 No\_date 39:59 12.00 n/a .000  
00617+ #  
00618+ # Catchment\_OKEFEE  
00619+ # Developed with assigned 43% imp.  
00620+ # - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current sheet (Area 513.02 HA)  
00621+ # - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current sheet (Area 513.02 HA)  
00622+ #  
00623+ # CONTINUOUS\_NASHYD -> 1.0 010-1<Okeefe> 1.0 010-1<Okeefe>  
00624+ #  
00625+ R0021:00047-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00626+ ADD HYD  
00627+ + 1.0 021-01-10 34.173 No\_date 39:59 12.00 n/a .000  
00628+ + 1.0 021-01-10 65.72 .305 No\_date 35:12 12.76 n/a .000  
00629+ + 1.0 021-01-10 65.72 .305 No\_date 35:12 12.76 n/a .000  
00630+ + 1.0 021-01-10 65.72 .305 No\_date 35:12 12.76 n/a .000  
00631+ #  
00632+ R0021:00048-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00633+ ADD HYD  
00634+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00635+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00636+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00637+ #  
00638+ R0021:00049-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00639+ ADD HYD  
00640+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00641+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00642+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00643+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00644+ R0021:00050-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00645+ ADD HYD  
00646+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00647+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00648+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00649+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00650+ #  
00651+ R0021:00051-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00652+ ADD HYD  
00653+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00654+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00655+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00656+ #  
00657+ R0021:00052-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00658+ ADD HYD  
00659+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00660+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00661+ #  
00662+ R0021:00053-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00663+ ADD HYD  
00664+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00665+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00666+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00667+ R0021:00054-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00668+ ADD HYD  
00669+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00670+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00671+ #  
00672+ R0021:00055-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00673+ ADD HYD  
00674+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00675+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00676+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00677+ #  
00678+ R0021:00056-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00679+ ADD HYD  
00680+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00681+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00682+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00683+ #  
00684+ R0021:00057-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00685+ ADD HYD  
00686+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00687+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00688+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00689+ #  
00690+ R0021:00058-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00691+ ADD HYD  
00692+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00693+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00694+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00695+ #  
00696+ R0021:00059-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00697+ ADD HYD  
00698+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00699+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00700+ #  
00701+ R0021:00060-----Dtnin-ID:NHYD-----ARAAha-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms  
00702+ ADD HYD  
00703+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00704+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00705+ + 1.0 021-01-10 65.72 .272 No\_date 29:10 9.62 n/a .000  
00706+ #











02619+ overflow <= 1.0 03:TOO-OVF .00 .000 No\_date 0:00 .00 n/a .000  
 02620+ [Wet=0.2med .3334=0.00] \*3 m3 .000 No\_date 0:00 n/a .000  
 02621+ R0022:00304-----Dtnin-ID:NHND-----ARAbh-QPEAKms-TpeakDate\_hh:mm:---RVMn-B.C.--DWFcms  
 02622+ ADD HYD + 1.0 02:NHDE 55194.85 49.262 No\_date 38:53 13.16 n/a .000  
 02623+ \* 1.0 02:NHDE 23 .000 No\_date 38:53 19.75 n/a .000  
 02624+ \* 1.0 02:NHDE 00 .000 No\_date 38:53 26.00 n/a .000  
 02625+ \* 1.0 02:JOCK\_P 257.63 2,560 No\_date 29:05 26.85 n/a .000  
 02626+ \* 1.0 02:JOCK 585.00 1,619 No\_date 29:05 13.23 n/a .000  
 02627+ R0022:00347-----Dtnin-ID:NHND-----ARAbh-QPEAKms-TpeakDate\_hh:mm:---RVMn-B.C.--DWFcms  
 02628+ SAVE HYD 1.0 01:NHDE 55476.26 49.619 No\_date 38:49 13.23 n/a .000  
 02629+ frame: SN\_LDE\_0002  
 02630+ remap:Total Flows at Heart's Desire  
 02631+ # Hydrograph from Heart's Desire routed to Rideau River  
 02632+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 0  
 02633+ #  
 02634+ R0022:00348-----Dtnin-ID:NHND-----ARAbh-QPEAKms-TpeakDate\_hh:mm:---RVMn-B.C.--DWFcms  
 02635+ ROUTE CHANNEL -> 1.0 02:NHDE 55476.26 49.619 No\_date 38:49 13.23 n/a .000  
 02636+ [ROT: 1.001 out] 1.0 01:NH 55476.26 49.617 No\_date 38:54 13.23 n/a .000  
 02637+ [ROT: 1.001 in] 1.0 01:NH 55476.26 49.617 No\_date 38:54 13.23 n/a .000  
 02638+ [Vmax: 1,490] [max: 1,801]  
 02639+ \*\*\*\*\*  
 02640+ R0022:00349-----Dtnin-ID:NHND-----ARAbh-QPEAKms-TpeakDate\_hh:mm:---RVMn-B.C.--DWFcms  
 02641+ CONTINUOUS NASHYD 1.0 01:8-2 102.94 1.373 No\_date 28:20 13.01 .286 .000  
 02642+ \* 1.0 01:8-2 102.94 1.373 No\_date 28:20 13.01 n/a .000  
 02643+ \* - To Jock River (north and south)  
 02644+ # - Undeveloped floodplain and river  
 02645+ R0022:00349-----Dtnin-ID:NHND-----ARAbh-QPEAKms-TpeakDate\_hh:mm:---RVMn-B.C.--DWFcms  
 02646+ CONTINUOUS NASHYD 1.0 01:8-2 102.94 1.373 No\_date 28:20 13.01 .286 .000  
 02647+ [ROT: 1.001 out] 1.0 01:NH 55476.26 49.619 No\_date 38:49 13.23 n/a .000  
 02648+ [ROT: 1.001 in] 1.0 01:NH 55476.26 49.617 No\_date 38:54 13.23 n/a .000  
 02649+ R0022:00400-----Dtnin-ID:NHND-----ARAbh-QPEAKms-TpeakDate\_hh:mm:---RVMn-B.C.--DWFcms  
 02650+ ADD HYD 1.0 02:NH 55476.26 49.617 No\_date 38:54 13.23 n/a .000  
 02651+ ADD HYD 1.0 02:NH 55476.26 49.617 No\_date 38:54 13.23 n/a .000  
 02652+ \* 1.0 02:NH 102.94 1.373 No\_date 28:20 13.01 n/a .000  
 02653+ \* 1.0 02:NH 55476.26 49.617 No\_date 38:54 13.23 n/a .000  
 02654+ R0022:00401-----Dtnin-ID:NHND-----ARAbh-QPEAKms-TpeakDate\_hh:mm:---RVMn-B.C.--DWFcms  
 02655+ SAVE HYD 1.0 01:NH 55476.26 49.617 No\_date 38:54 13.23 n/a .000  
 02656+ frame: SN\_LDE\_0002  
 02657+ remap:Total Flows at Rideau River  
 02658+ \*\*\*\*\*  
 02659+ \*\*\* END OF RUN : 4  
 02660+  
 02661+ \*\*\*\*\*  
 02662+ #  
 02663+ #  
 02664+ #  
 02665+ #  
 02666+ # BNNI:COMMANDS  
 02667+ R0022:00001-----  
 02668+ START  
 02669+ [METCOUT = 2.00 hrs on 0]  
 02670+ [NETCOUT = 1]  
 02671+ [NISTROM = 1]  
 02672+ #  
 02673+ #\*\*\*\*\*  
 02674+ # SWMMHYD Ver:5.02/Jan 2001 <Beta> / INPUT DATA FILE  
 02675+ # Project Name: [Jock River] Project Number: [1474-16]  
 02676+ # Date : 04-03-2021  
 02677+ # Author : [JFSAinc]  
 02678+ # Company : [JFSAinc]  
 02679+ # License : [254923]  
 02680+ #  
 02681+ # CALIBRATION OF SUMMER MODEL PARAMETERS  
 02682+ USING CONTINUOUS SIMULATIONS  
 02683+ #  
 02684+ #  
 02685+ #  
 02686+ #  
 02687+ #  
 02688+ #  
 02689+ #  
 02690+ #  
 02691+ #  
 02692+ #  
 02693+ # R0022:0002-----  
 02694+ #  
 02695+ # filename = storm.001  
 02696+ # Comment + Plus ECS 0.24 for 24 hrs 1:8 ans pour Ottawa CDA  
 02697+ #  
 02698+ R0022:0003-----  
 02699+ # MODIFY STORM  
 02700+ #  
 02701+ # [ROT:10.00:SOEUR 96.00 min] [ROT:4.00:PTOT 57.12]  
 02702+ R0022:0004-----  
 02703+ #  
 02704+ #  
 02705+ #  
 02706+ #  
 02707+ #  
 02708+ #  
 02709+ #  
 02710+ #  
 02711+ #  
 02712+ #  
 02713+ # [TAinc: 1.57 mm] [CLin: 1.50] [MNin: 0.013]  
 02714+ # Parameters used in the calibration exercise in Ota  
 02715+ # [tainc: 4.67 mm] [mnin: 0.03]  
 02716+ #  
 02717+ # Average monthly Pan Evaporation data in (mm)  
 02718+ # JFM FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC  
 02719+ # 000 000 000 000 000 000 000 000 000 000 000 000 .000  
 02720+ # Average monthly Potential Evapotranspiration in (mm)  
 02721+ # JFM FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC  
 02722+ # 000 000 000 000 000 000 000 000 000 000 000 000 .000  
 02723+ R0022:0005-----  
 02724+ #  
 02725+ # [APIn1= 50.00: APIday= .8500: APIdtr= .9989]  
 02726+ # [APInax= 90.83: APday= 60.09: APIdns= 44.87]  
 02727+ #  
 02728+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02729+ # 1.0 12:1.02 1.0 01:NH 371.00 3.405 No\_date 32:36 15.29 .266 .000  
 02730+ #  
 02731+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02732+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02733+ #  
 02734+ # [ROT:12.00]  
 02735+ #  
 02736+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02737+ R0022:0007-----  
 02738+ #  
 02739+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02740+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02741+ #  
 02742+ #  
 02743+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02744+ # 1.0 12:1.02 1.0 01:NH 371.00 3.405 No\_date 32:36 15.29 .266 .000  
 02745+ #  
 02746+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02747+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02748+ #  
 02749+ # [ROT:12.00]  
 02750+ #  
 02751+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02752+ R0022:0008-----  
 02753+ #  
 02754+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02755+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02756+ #  
 02757+ # [ROT:12.00]  
 02758+ #  
 02759+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02760+ R0022:0009-----  
 02761+ #  
 02762+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02763+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02764+ #  
 02765+ # [ROT:12.00]  
 02766+ #  
 02767+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02768+ R0022:0010-----  
 02769+ #  
 02770+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02771+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02772+ #  
 02773+ # [ROT:12.00]  
 02774+ #  
 02775+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02776+ R0022:0011-----  
 02777+ #  
 02778+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02779+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02780+ #  
 02781+ # [ROT:12.00]  
 02782+ #  
 02783+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02784+ R0022:0012-----  
 02785+ #  
 02786+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02787+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02788+ #  
 02789+ # [ROT:12.00]  
 02790+ #  
 02791+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02792+ R0022:0013-----  
 02793+ #  
 02794+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02795+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02796+ #  
 02797+ # [ROT:12.00]  
 02798+ #  
 02799+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02800+ R0022:0014-----  
 02801+ #  
 02802+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02803+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02804+ #  
 02805+ # [ROT:12.00]  
 02806+ #  
 02807+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02808+ R0022:0015-----  
 02809+ #  
 02810+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02811+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02812+ #  
 02813+ # [ROT:12.00]  
 02814+ #  
 02815+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02816+ R0022:0016-----  
 02817+ #  
 02818+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02819+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02820+ #  
 02821+ # [ROT:12.00]  
 02822+ #  
 02823+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02824+ R0022:0017-----  
 02825+ #  
 02826+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02827+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02828+ #  
 02829+ # [ROT:12.00]  
 02830+ #  
 02831+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02832+ R0022:0018-----  
 02833+ #  
 02834+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02835+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02836+ #  
 02837+ # [ROT:12.00]  
 02838+ #  
 02839+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02840+ R0022:0019-----  
 02841+ #  
 02842+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02843+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02844+ #  
 02845+ # [ROT:12.00]  
 02846+ #  
 02847+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02848+ R0022:0020-----  
 02849+ #  
 02850+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02851+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02852+ #  
 02853+ # [ROT:12.00]  
 02854+ #  
 02855+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02856+ R0022:0021-----  
 02857+ #  
 02858+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02859+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02860+ #  
 02861+ # [ROT:12.00]  
 02862+ #  
 02863+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02864+ R0022:0022-----  
 02865+ #  
 02866+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02867+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02868+ #  
 02869+ # [ROT:12.00]  
 02870+ #  
 02871+ R0022:0023-----  
 02872+ #  
 02873+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02874+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02875+ #  
 02876+ # [ROT:12.00]  
 02877+ #  
 02878+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02879+ R0022:0024-----  
 02880+ #  
 02881+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02882+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02883+ #  
 02884+ # [ROT:12.00]  
 02885+ #  
 02886+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02887+ R0022:0025-----  
 02888+ #  
 02889+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02890+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02891+ #  
 02892+ # Routing hydrographs  
 02893+ # Starting with the addition of Jock River Headwater and Subwatershed 13  
 02894+ #  
 02895+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 02896+ R0022:0026-----  
 02897+ #  
 02898+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02899+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02900+ #  
 02901+ # [ROT:12.00]  
 02902+ #  
 02903+ # Approximated cross-section - see cross-section 289  
 02904+ #  
 02905+ R0022:0027-----  
 02906+ #  
 02907+ # [CN: 61.00 N: 3.00: Tp: 3.76]  
 02908+ # [taec: 4.00: SHIN: 64.50: SMAX:430.01: SK: .010]  
 02909+ #  
 02910+ # [ROT:12.00]  
 02911+ # Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A  
 02912+ #  
 02913+ #  
 02914+ #  
 02915+ #  
 02916+ #  
 02917+ #  
 02918+ # Insertion of a reservoir to simulate the effect of the Goodwood Marsh  
 02919+ #  
 02920+ R0022:0028-----  
 02921+ #  
 02922+ # ROUTE RESERVOIR --> 1.0 02:SNM\_13  
 02923+ #  
 02924+ #  
 02925+ #  
 02926+ #  
 02927+ #  
 02928+ #  
 02929+ # Output/flow from Reservoir Goodwood Marsh routed from Node 13A to Node 12  
 02930+ #  
 02931+ #  
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 02934+ #  
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02993+ SUM+ 1.0 01:S\_N10A 25965.00 44.722 No\_date 39:35 17.37 n/a .000  
 02994+ # Sum of hydrographs from Node 10 routed to Node 9  
 02995+ # Section 2  
 02996+ R0005:00044-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 02997+ ROUTE CHANNEL -> 1.0 02:S\_N10A 25965.00 44.722 No\_date 39:35 17.37 n/a .000  
 02998+ [ROT: 1.001 out-< 1.0 01:S\_N10A 25965.00 43.534 No\_date 39:35 17.37 n/a .000  
 02999+ [L/S/nr .3982 /-.075/.046]  
 03000+ [Vmax=.664\*Dmax 1.502]  
 03001+ \*\*\*\*\*  
 03002+ # Addition of Subwatershed 9 and Nichols Creek to Node 9  
 03003+ R0005:00045-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03004+ ADD HYD 1.0 02:N19Y 29695.00 43.534 No\_date 39:59 17.37 n/a .000  
 03005+ # Section 3  
 03006+ R0005:00046-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03007+ ROUTE CHANNEL -> 1.0 02:S\_N9 1132.00 6.963 No\_date 39:59 17.20 n/a .000  
 03008+ [ROT: 1.001 out-< 1.0 01:N9 1136.00 6.963 No\_date 28:57 17.20 n/a .000  
 03009+ [L/S/nr .0885 /-.0885/.046]  
 03010+ [Vmax=.370\*Dmax 1.520]  
 03011+ \*\*\*\*\*  
 03012+ # Addition of Subwatershed 8 and Hobbs's Drain to Node 8  
 03013+ R0005:00047-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03014+ ADD HYD 1.0 02:N19Y 31561.00 53.366 No\_date 39:59 17.20 n/a .000  
 03015+ # Section 4  
 03016+ R0005:00048-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03017+ ROUTE CHANNEL -> 1.0 02:S\_N8 131.00 1.298 No\_date 28:57 17.20 n/a .000  
 03018+ [ROT: 1.001 out-< 1.0 01:N8 135.00 1.298 No\_date 45:08 17.20 n/a .000  
 03019+ [L/S/nr .3750 /-.050/.070]  
 03020+ [Vmax=.208\*Dmax 1.855]  
 03021+ \*\*\*\*\*  
 03022+ # Addition of Subwatershed 8 and Hobbs's Drain to Node 8  
 03023+ R0005:00049-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03024+ ADD HYD 1.0 02:N19Y 31561.00 49.404 No\_date 39:59 17.20 n/a .000  
 03025+ # Section 5  
 03026+ R0005:00050-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03027+ SAVE HYD 1.0 01:S18N 35544.00 56.845 No\_date 39:59 17.19 n/a .000  
 03028+ # Sum of hydrographs from Node 8 routed to Node 7  
 03029+ # Section 6  
 03030+ R0005:00049-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03031+ ADD HYD 1.0 02:N19Y 31561.00 48.129 No\_date 39:59 17.19 n/a .000  
 03032+ # Section 7  
 03033+ R0005:00051-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03034+ # Insertion of a reservoir to simulate the effects of the Richmond Pen.  
 03035+ # Storage areas and volumes were estimated from available topo maps.  
 03036+ # It was assumed that up to 0.75 m of water could be stored.  
 03037+ # river cross-section for summer conditions. It was assumed that for up to  
 03038+ # 0.75 m of water, the main channel of the river provided the storage. Above  
 03039+ # this depth, the wetlands start to significantly store water.  
 03040+ # Section 8  
 03041+ R0005:00051-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03042+ ADD HYD 1.0 02:N19Y 31561.00 48.129 No\_date 39:59 17.19 n/a .000  
 03043+ # Section 9  
 03044+ R0005:00050-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03045+ SAVE HYD 1.0 01:S18N 38743.00 51.398 No\_date 44:14 16.92 n/a .000  
 03046+ # name :H\_NResRF  
 03047+ # Inflow to the reservoir at S-N7: NT = SW  
 03048+ # Insertion of a reservoir to simulate the effects of the Richmond Pen.  
 03049+ # Storage areas and volumes were estimated from available topo maps.  
 03050+ # It was assumed that up to 0.75 m of water could be stored.  
 03051+ # river cross-section for summer conditions. It was assumed that for up to  
 03052+ # 0.75 m of water, the main channel of the river provided the storage. Above  
 03053+ # this depth, the wetlands start to significantly store water.  
 03054+ # Section 10  
 03055+ R0005:00051-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03056+ # Section 11  
 03057+ R0005:00051-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03058+ # Section 12  
 03059+ R0005:00051-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03060+ SAVE HYD 1.0 01:S18N 38743.00 27.976 No\_date 59:12 16.92 n/a .000  
 03061+ # name :H\_NResRF  
 03062+ # Inflow to the reservoir at S-N7: NT = SW  
 03063+ # Section 13  
 03064+ # Sum of hydrographs from Node 7 routed to Node 6  
 03065+ # Section 14  
 03066+ R0005:00051-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03067+ # Section 15  
 03068+ R0005:00051-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03069+ # Section 16  
 03070+ [ROT: 1.001 out-< 1.0 01:N6 38743.00 27.976 No\_date 60:29 16.92 n/a .000  
 03071+ [L/S/nr .3056 /-.082/.025]  
 03072+ [Vmax=.465\*Dmax .895]  
 03073+ \*\*\*\*\*  
 03074+ # Addition of Subwatershed 6 and Van Gaal Drain to Node 6  
 03075+ R0005:00054-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03076+ ADD HYD 1.0 02:N19Y 38743.00 27.976 No\_date 60:29 16.92 n/a .000  
 03077+ # Section 17  
 03078+ + 1.0 02:SW\_5 132.00 1.298 No\_date 35:19 20.12 n/a .000  
 03079+ + 1.0 02:VO\_DNR 1332.00 4.803 No\_date 35:19 20.12 n/a .000  
 03080+ SUM+ 1.0 01:S18N 40240.01 27.944 No\_date 60:26 17.03 n/a .000  
 03081+ # Sum of hydrographs from Node 6 routed to Node 5  
 03082+ # Section 6  
 03083+ R0005:00055-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03084+ # Section 7  
 03085+ R0005:00055-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03086+ # Section 8  
 03087+ R0005:00056-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03088+ # Section 9  
 03089+ R0005:00056-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03090+ # Addition of Subwatershed 5 and Flowing Creek to Node 5  
 03091+ R0005:00051-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03092+ # Section 10  
 03093+ R0005:00051-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03094+ # Section 11  
 03095+ R0005:00051-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03096+ # Section 12  
 03097+ R0005:00051-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03098+ # Sum of hydrographs from Node 5 routed to Node 4  
 03099+ # Section 7  
 03100+ R0005:00057-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03101+ # Section 8  
 03102+ ROUTE CHANNEL -> 1.0 02:S\_N8 45409.01 45.566 No\_date 35:28 17.49 n/a .000  
 03103+ [ROT: 1.001 out-< 1.0 01:N8 45409.01 45.490 No\_date 35:17 17.49 n/a .000  
 03104+ [L/S/nr .556 /-.090/.040]  
 03105+ [Vmax=.465\*Dmax 1.060]  
 03106+ \*\*\*\*\*  
 03107+ # Addition of Subwatershed 5A1 and Subwatershed SA2 to Node 5A  
 03108+ R0005:00058-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03109+ ADD HYD 1.0 02:N19Y 45409.01 43.490 No\_date 35:27 17.49 n/a .000  
 03110+ # Section 9  
 03111+ + 1.0 02:SW\_5 20.00 4.483 No\_date 28:36 25.62 n/a .000  
 03112+ + 1.0 02:VO\_DNR 120.00 4.648 No\_date 35:28 21.59 n/a .000  
 03113+ SUM+ 1.0 01:N8A 46841.01 47.976 No\_date 35:28 17.49 n/a .000  
 03114+ # Sum of hydrographs from Node 5A routed to Node 4  
 03115+ # Section 8  
 03116+ R0005:00059-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03117+ # Section 9  
 03118+ ROUTE CHANNEL -> 1.0 02:S\_N8A 46841.01 47.976 No\_date 35:18 17.63 n/a .000  
 03119+ [ROT: 1.001 out-< 1.0 01:N8A 46841.01 47.976 No\_date 37:26 17.63 n/a .000  
 03120+ [L/S/nr .4665 /-.043/.025]  
 03121+ [Vmax=.756\*Dmax 3.116]  
 03122+ \*\*\*\*\*  
 03123+ # Addition of Subwatershed 4 and Leamy Creek to Node 4  
 03124+ R0005:00060-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03125+ ADD HYD 1.0 02:N19Y 46841.01 46.217 No\_date 37:26 17.63 n/a .000  
 03126+ # Section 10  
 03127+ R0005:00061-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03128+ # Section 11  
 03129+ R0005:00061-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03130+ # Section 12  
 03131+ R0005:00061-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03132+ # Section 13  
 03133+ # name :S\_N4\_2005  
 03134+ remark:flow at S\_N4  
 03135+ # Sum of hydrographs from Node 4 routed to Node 2  
 03136+ # Section 9  
 03137+ R0005:00062-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03138+ # Section 10  
 03139+ R0005:00062-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03140+ # Section 11  
 03141+ ROUTE CHANNEL -> 1.0 02:S\_N8 48447.00 50.308 No\_date 36:47 17.89 n/a .000  
 03142+ [ROT: 1.001 out-< 1.0 01:N8 48447.00 50.193 No\_date 37:08 17.89 n/a .000  
 03143+ [L/S/nr .1667 /-.060/.040]  
 03144+ [Vmax=.781\*Dmax 3.131]  
 03145+ \*\*\*\*\*  
 03146+ # Addition of Subwatershed 2 and Monohan Drain and Smith Drain to Node 2  
 03147+ R0005:00063-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03148+ ADD HYD 1.0 02:N19Y 48447.00 50.131 No\_date 37:08 17.89 n/a .000  
 03149+ # Section 9  
 03150+ + 1.0 02:SW\_5 177.00 3.240 No\_date 28:45 22.97 n/a .000  
 03151+ + 1.0 02:VO\_DNR 2737.00 17.859 No\_date 31:23 22.47 n/a .000  
 03152+ SUM+ 1.0 01:N8A 52483.00 67.222 No\_date 33:17 18.31 n/a .000  
 03153+ # Sum of hydrographs from Node 2 routed to Node 1  
 03154+ # Section 10  
 03155+ R0005:00064-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03156+ ADD HYD 1.0 01:S18N 52483.00 67.222 No\_date 33:17 18.31 n/a .000  
 03157+ # Sum of hydrographs from Node 2 routed to Node 1  
 03158+ # Section 11  
 03159+ R0005:00065-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03160+ # Section 12  
 03161+ # Hydrograph from Node 2 routed to Node 1  
 03162+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 9025  
 03163+ R0005:00065-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03164+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 7245  
 03165+ R0005:00065-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03166+ # Catchment SW\_1 outside of Reach 1 subwatershed  
 03167+ # - Undeveloped agricultural land  
 03168+ R0005:00065-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03169+ # Section 13  
 03170+ CONTINUOUS\_NASHYD 1.0 01:S18N14 536.42 3.032 No\_date 31:18 19.00 .333 .000  
 03171+ [CIN 72.01 N 3.00: Tp: 2.79]  
 03172+ [IAEBC 4.00: SMIN= 39.75: SMAX=246.99: SK= .010]

03180+ [InterEventTime: 12.00]  
 03181+ R0005:00067-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03182+ CONTINUOUS\_NASHYD 1.0 01:O1-1:Okeefe 44.93 .602 No\_date 29:08 21.69 .380 .000  
 03183+ [CIN 77.01 N 3.00: Tp: 1.05]  
 03184+ [IAEBC 4.00: SMIN= 39.75: SMAX=207.66: SK= .010]  
 03185+ R0005:00068-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03186+ ADD HYD 1.0 02:N19Y 52483.00 67.222 No\_date 31:18 19.00 .333 .000  
 03187+ + 1.0 02:S18N14 536.42 3.032 No\_date 31:18 19.00 .333 .000  
 03188+ [IAEBC 4.00: SMIN= 39.75: SMAX=246.99: SK= .010]  
 03189+ remark:Total Flows at Highway 416  
 03190+ # Hydrograph from Node 416 routed to Node at Okefe drain  
 03191+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 7245  
 03192+ SAVE HYD 1.0 01:S18N14 536.42 3.032 No\_date 34:06 18.32 .32 .000  
 03193+ [IAEBC 4.00: SMIN= 39.75: SMAX=246.99: SK= .010]  
 03194+ remark:Total Flows at Highway 416  
 03195+ # Hydrograph from Node 416 routed to Node at Okefe drain  
 03196+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 7245  
 03197+ [IAEBC 4.00: SMIN= 39.75: SMAX=246.99: SK= .010]  
 03198+ # Developed with assumed 4%  
 03199+ # 2020-11-20 Okefe detailed model was added as per the NOVATECH SWMM model (Citi-Gate 2014).  
 03200+ R0005:00069-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03201+ ADD HYD 1.0 02:N19Y 53064.36 67.933 No\_date 34:06 18.32 .32 .000  
 03202+ [ROT: 1.001 out-< 1.0 01:N19OK 53064.36 67.890 No\_date 34:06 18.32 .32 .000  
 03203+ [L/S/nr .335: 0.252]  
 03204+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 7245  
 03205+ [IAEBC 4.00: SMIN= 39.75: SMAX=246.99: SK= .010]  
 03206+ # To O'Keefe drain (north of the Jock)  
 03207+ # Developed with assumed 4%  
 03208+ # CONTINUOUS\_NASHYD 1.0 01:O1-1:Okeefe 63.72 .514 No\_date 28:19 13.88 .243 .000  
 03209+ [CIN 61.01 N 3.00: Tp: 90]  
 03210+ [IAEBC 4.00: SMIN= 39.75: SMAX=246.99: SK= .010]  
 03211+ R0005:00070-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03212+ CONTINUOUS\_NASHYD 1.0 01:O1-1:Okeefe 63.72 .514 No\_date 28:19 13.88 .243 .000  
 03213+ [CIN 61.01 N 3.00: Tp: 90]  
 03214+ [IAEBC 4.00: SMIN= 39.75: SMAX=246.99: SK= .010]  
 03215+ [InterEventTime: 12.00]  
 03216+ R0005:00071-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03217+ CONTINUOUS\_NASHYD 1.0 01:O1-1:Okeefe 63.72 .514 No\_date 28:19 13.88 .243 .000  
 03218+ [ROT: 1.001 out-< 1.0 01:O1-1:Okeefe 63.72 .470 No\_date 29:19 13.88 .243 .000  
 03219+ [L/S/nr .960: .630/.043]  
 03220+ R0005:00073-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03221+ CONTINUOUS\_NASHYD 1.0 01:O1-1:Okeefe 63.72 .514 No\_date 28:19 13.88 .243 .000  
 03222+ [CIN 61.01 N 3.00: Tp: 90]  
 03223+ [IAEBC 4.00: SMIN= 39.75: SMAX=508.81: SK= .010]  
 03224+ [IAEBC 4.00: SMIN= 76.32: SMAX=508.81: SK= .010]  
 03225+ R0005:00074-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03226+ CONTINUOUS\_NASHYD 1.0 01:O1-1:Okeefe 64.94 .222 No\_date 29:01 9.87 .173 .000  
 03227+ CONTINUOUS\_NASHYD 1.0 01:O1-1:Okeefe 64.94 .222 No\_date 29:01 9.87 .173 .000  
 03228+ [IAEBC 4.00: SMIN= 39.75: SMAX=87.25: SK= .010]  
 03229+ [InterEventTime: 12.00]  
 03230+ R0005:00075-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03231+ CONTINUOUS\_NASHYD 1.0 01:O1-1:Okeefe 64.94 .222 No\_date 29:01 9.87 .173 .000  
 03232+ ADD HYD 1.0 02:O1-1:Okeefe 64.94 .222 No\_date 29:01 9.87 .173 .000  
 03233+ # Section 10  
 03234+ R0005:00076-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03235+ CONTINUOUS\_NASHYD 1.0 01:O1-1:Okeefe 64.94 .222 No\_date 29:01 9.87 .173 .000  
 03236+ [ROT: 1.001 out-< 1.0 01:O1-1:Okeefe 64.94 .222 No\_date 29:17 10.15 .227 .000  
 03237+ [L/S/nr .210: 1.00/.041]  
 03238+ R0005:00077-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03239+ CONTINUOUS\_NASHYD 1.0 01:O1-1:Okeefe 64.94 .222 No\_date 29:17 10.15 .227 .000  
 03240+ [ROT: 1.001 out-< 1.0 01:O1-1:Okeefe 64.94 .222 No\_date 29:17 10.15 .227 .000  
 03241+ [L/S/nr .210: 1.00/.041]  
 03242+ R0005:00078-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03243+ CONTINUOUS\_NASHYD 1.0 01:O1-1:Okeefe 64.94 .222 No\_date 29:17 10.15 .227 .000  
 03244+ [ROT: 1.001 out-< 1.0 01:O1-1:Okeefe 64.94 .222 No\_date 29:17 10.15 .227 .000  
 03245+ [L/S/nr .210: 1.00/.041]  
 03246+ R0005:00079-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03247+ CONTINUOUS\_NASHYD 1.0 01:O1-1:Okeefe 64.94 .222 No\_date 29:17 10.15 .227 .000  
 03248+ [ROT: 1.001 out-< 1.0 01:O1-1:Okeefe 64.94 .222 No\_date 29:17 10.15 .227 .000  
 03249+ [L/S/nr .210: 1.00/.041]  
 03250+ R0005:00080-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03251+ ADD HYD 1.0 02:N19Y 65.03 67.933 No\_date 29:17 12.46 .000 .000  
 03252+ # Section 11  
 03253+ R0005:00081-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03254+ CONTINUOUS\_NASHYD 1.0 01:O1-1:Okeefe 65.03 67.933 No\_date 29:17 12.46 .000 .000  
 03255+ [IAEBC 4.00: SMIN= 39.75: SMAX=140.62: SK= .010]  
 03256+ [InterEventTime: 12.00]  
 03257+ R0005:00082-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03258+ CONTINUOUS\_NASHYD 1.0 01:O1-1:Okeefe 65.03 67.933 No\_date 29:17 12.46 .000 .000  
 03259+ [IAEBC 4.00: SMIN= 39.75: SMAX=140.62: SK= .010]  
 03260+ [InterEventTime: 12.00]  
 03261+ R0005:00083-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03262+ CONTINUOUS\_NASHYD 1.0 01:O1-1:Okeefe 65.03 67.933 No\_date 29:17 12.46 .000 .000  
 03263+ [IAEBC 4.00: SMIN= 39.75: SMAX=140.62: SK= .010]  
 03264+ [InterEventTime: 12.00]  
 03265+ R0005:00084-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03266+ CONTINUOUS\_NASHYD 1.0 01:O1-1:Okeefe 65.03 67.933 No\_date 29:17 12.46 .000 .000  
 03267+ [IAEBC 4.00: SMIN= 39.75: SMAX=140.62: SK= .010]  
 03268+ [InterEventTime: 12.00]  
 03269+ R0005:00085-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03270+ CONTINUOUS\_NASHYD 1.0 01:O1-1:Okeefe 65.03 67.933 No\_date 29:17 12.46 .000 .000  
 03271+ [IAEBC 4.00: SMIN= 39.75: SMAX=140.62: SK= .010]  
 03272+ [InterEventTime: 12.00]  
 03273+ R0005:00086-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03274+ CONTINUOUS\_NASHYD 1.0 01:O1-1:Okeefe 65.03 67.933 No\_date 29:17 12.46 .000 .000  
 03275+ [IAEBC 4.00: SMIN= 39.75: SMAX=140.62: SK= .010]  
 03276+ [InterEventTime: 12.00]  
 03277+ R0005:00087-----Dtnin:ID:NHYD---ARAEba-QPEAKcms-TpeakDate\_bh:mm---RvNm-R.C.---DWFcms  
 03278+ CONTINUOUS\_NASHYD 1.0 01:O1-1:Okeefe 65.03 67.933 No\_date 29:17 12.46 .000 .000  
 03279+ [IAEBC 4.00: SMIN= 39.75: SMAX=140.62: SK= .010]  
 03



03741+ remark:Total Flows at Station 520 on Foster Drain  
 03742+ # Hydrograph from Node at Station 520 (Foster Drain) to Node at Station 6016 (Jock River)  
 03743+ # Channel X-Section obtained from RVE Hydraulic Model - Station 520  
 03744+ # DTMn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03745+ ROUTE CHANNEL > 1.0 02:520 out-> 1.0 01:520-out 335.49 5.129 No\_date 29:14 37.23 n/a .000  
 03747+ [L/S/nr .270/.018/.035] .000  
 03748+ [L/S/nr .245/.095/.035] .000  
 03749+ [L/S/nr .245/.095/.035] .000  
 03750+ R0005:CO0162-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03751+ CONTINUOUS STANDHYD 1.0 01:8-1> 5.27 .654 No\_date 28:00 42.00 .735 .000  
 03752+ [L/S/nr .270/.018/.035] .000  
 03753+ [iabErc 4.001 SMIN 31.15: SMAX=207.66: SKw .010]  
 03754+ [InterEventTime: 12.00] .000  
 03755+ R0005:CO0163-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03756+ CONTINUOUS STANDHYD 1.0 01:8-1> 5.27 .654 No\_date 28:00 42.00 .735 .000  
 03757+ [L/S/nr .270/.018/.035] .000  
 03758+ [iabErc 4.001 SMIN 31.15: SMAX=207.66: SKw .010]  
 03759+ [Previous area: Iaper 4.67:SLPP=2.00:LGD= 40.:MNP=.250:SCP=.0]  
 03760+ [iabErc 4.001 SMIN 31.15: SMAX=207.66: SKw .010]  
 03761+ [iabEclmp 4.001 iabErc 4.001]  
 03762+ [SMIN .31: SMAX=225.43: SKw .010]  
 03763+ R0005:CO0164-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03764+ CONTINUOUS STANDHYD 1.0 01:8-1> 75.88 1.479 No\_date 28:07 21.69 .380 .000  
 03765+ [CN .77.01: NO .30: Tp .62] .000  
 03766+ [iabErc 4.001 SMIN 31.15: SMAX=207.66: SKw .010]  
 03767+ [InterEventTime: 12.00] .000  
 03768+ R0005:CO0165-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03769+ CONTINUOUS STANDHYD 1.0 01:8-1> 39.65 .462 No\_date 29:11 21.69 .380 .000  
 03770+ [CN .77.01: NO .30: Tp .11] .000  
 03771+ [iabErc 4.001 SMIN 31.15: SMAX=207.66: SKw .010]  
 03772+ [iabEclmp 4.001 iabErc 4.001]  
 03773+ R0005:CO0166-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03774+ ADD HYD 1.0 02:R\_NP 53577.82 69.117 No\_date 34:07 18.36 n/a .000  
 03775+ [CN .77.01: NO .30: Tp .11] .000  
 03776+ 1.0 02:MSP\_D10 73.29 1.101 No\_date 28:06 25.46 42.2 n/a .000  
 03777+ 1.0 02:P10\_VN 0.00 .000 No\_date 0:00 0:00 n/a .000  
 03778+ [CN .77.01: NO .30: Tp .11] .000  
 03779+ 1.0 02:S1-PO-1D 14.96 .206 No\_date 29:05 21.69 n/a .000  
 03780+ 1.0 02:S1-PO-1D 14.96 .206 No\_date 28:06 24.02 n/a .000  
 03781+ 1.0 02:S1-PO-1D 14.96 .206 No\_date 28:06 24.02 n/a .000  
 03782+ 1.0 01:SNM\_P 54118.36 71.824 No\_date 33:59 18.52 n/a .000  
 03783+ R0005:CO0167-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03784+ SAVE HYD 1.0 01:SNM\_P 54118.36 71.824 No\_date 33:59 18.52 n/a .000  
 03785+ fname: SN\_FO\_0005  
 03786+ remark:Total Flows at Foster Drain  
 03787+ # Hydrograph from Node at Station 520 (Foster Drain) to Node at Cedarview Road  
 03788+ # Channel X-Section obtained from RVE Hydraulic Model - Station 6016  
 03789+ # R0005:CO0168-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03790+ ROUTE CHANNEL > 1.0 01:SNM\_P 54118.36 71.824 No\_date 33:59 18.52 n/a .000  
 03791+ [NO .30: Tp .11] .000  
 03792+ [CN .77.01: NO .30: Tp .11] .000  
 03793+ [iabErc 4.001 SMIN 31.15: SMAX=207.66: SKw .010]  
 03794+ [Previous area: Iaper 4.67:SLPP=2.00:LGD= 40.:MNP=.250:SCP=.0]  
 03795+ [iabEclmp 4.001 iabErc 4.001]  
 03796+ # Catchment KEN\_BU  
 03797+ - To Jock River (north and south of Jock)  
 03798+ [iabErc 4.001 SMIN 31.15: SMAX=207.66: SKw .010]  
 03799+ [Previous area: Iaper 4.67:SLPP=2.00:LGD= 40.:MNP=.250:SCP=.0]  
 03800+ R0005:CO0169-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03801+ CONTINUOUS STANDHYD 1.0 01:8-1> 95.30 1.342 No\_date 28:24 21.69 .380 .000  
 03802+ [CN .77.01: NO .30: Tp .45] .000  
 03803+ [iabErc 4.001 SMIN 31.15: SMAX=207.66: SKw .010]  
 03804+ [iabErc 4.001 SMIN 31.15: SMAX=207.66: SKw .010]  
 03805+ # JFSA 2021-02-24 change the name from S-1-BDC to S-1-A-BDC & Change their TP values based on the new areas  
 03806+ # S-1-BDC & S-1-BDC' & S-1-BDC'' are not existing anymore. 'S-1-BDC'' is part of 'S-1-PO-D2' and  
 03807+ # S-1-BDC & S-1-BDC' are part of 'S-1-PO-D1'.  
 03808+ R0005:CO0170-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03809+ CONTINUOUS STANDHYD 1.0 01:8-1> 21.67 .287 No\_date 29:09 21.69 .380 .000  
 03810+ [iabErc 4.001 SMIN 31.15: SMAX=207.66: SKw .010]  
 03811+ [iabErc 4.001 SMIN 31.15: SMAX=207.66: SKw .010]  
 03812+ [InterEventTime: 12.00] .000  
 03813+ R0005:CO0171-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03814+ CONTINUOUS STANDHYD 1.0 01:8-1> 3.28 .042 No\_date 29:11 21.69 .380 .000  
 03815+ [CN .77.01: NO .30: Tp .11] .000  
 03816+ [iabErc 4.001 SMIN 31.15: SMAX=207.66: SKw .010]  
 03817+ [InterEventTime: 12.00] .000  
 03818+ R0005:CO0172-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03819+ CONTINUOUS STANDHYD 1.0 01:8-1> 12.84 .166 No\_date 29:11 21.69 .380 .000  
 03820+ [CN .77.01: NO .30: Tp .11] .000  
 03821+ [iabErc 4.001 SMIN 31.15: SMAX=207.66: SKw .010]  
 03822+ [iabErc 4.001 SMIN 31.15: SMAX=207.66: SKw .010]  
 03823+ R0005:CO0173-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03824+ CONTINUOUS STANDHYD 1.0 01:8-1> 1.75 .023 No\_date 29:11 21.69 .380 .000  
 03825+ [CN .77.01: NO .30: Tp .11] .000  
 03826+ [iabErc 4.001 SMIN 31.15: SMAX=207.66: SKw .010]  
 03827+ [InterEventTime: 12.00] .000  
 03828+ R0005:CO0174-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03829+ CONTINUOUS STANDHYD 1.0 01:8-1> 2.03 .026 No\_date 29:11 21.69 .380 .000  
 03830+ [CN .77.01: NO .30: Tp .11] .000  
 03831+ [iabErc 4.001 SMIN 31.15: SMAX=207.66: SKw .010]  
 03832+ [InterEventTime: 12.00] .000  
 03833+ # Catchment W\_CHEM  
 03834+ - To West Clarkie Drain (south of the Jock)  
 03835+ # Subdivision with 43% imp. from Barrhaven South MNS  
 03836+ # - 2022-11-30 update CLARIS Tributary Drainage Area to = 121 ha based on P5984(0)-11  
 03837+ # R0005:CO0175-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03838+ R0005:CO0176-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03839+ CONTINUOUS STANDHYD 1.0 01:8-1> 2.03 .026 No\_date 29:11 21.69 .380 .000  
 03840+ [CN .77.01: NO .30: Tp .11] .000  
 03841+ [iabErc 4.001 SMIN 31.15: SMAX=207.66: SKw .010]  
 03842+ [InterEventTime: 12.00] .000  
 03843+ R0005:CO0177-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03844+ CONTINUOUS STANDHYD 1.0 01:8-1> 1.75 .023 No\_date 29:11 21.69 .380 .000  
 03845+ [CN .77.01: NO .30: Tp .11] .000  
 03846+ [iabErc 4.001 SMIN 31.15: SMAX=207.66: SKw .010]  
 03847+ [InterEventTime: 12.00] .000  
 03848+ R0005:CO0178-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03849+ ROUTE RESERVOIR > 1.0 02:CLAR\_M2 1.77 .192 No\_date 28:00 37.36 n/a .000  
 03850+ out < 1.0 01:CLAR\_M2 1.77 .192 No\_date 28:00 37.36 n/a .000  
 03851+ overland < 1.0 01:CLAR\_M2 1.77 .192 No\_date 28:00 37.36 n/a .000  
 03852+ [MSzCMod=.916E-04 m3 , TotVolVn=.000E+00 m3 , N\_Ovdr= 0, TotTurvfn= 0, hrs]= .000  
 03853+ R0005:CO0179-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03854+ R0005:CO0180-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03855+ [LGSN .60: TIMEW .65] .000  
 03856+ [iabErc 4.001: iabErc 4.001] .000  
 03857+ R0005:CO0181-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03858+ CONTINUOUS STANDHYD 1.0 01:8-1> 1.77 .192 No\_date 28:00 37.36 .654 .000  
 03859+ [XMP .46:TIMEW .59] .000  
 03860+ R0005:CO0182-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03861+ [iabErc 4.001: iabErc 4.001] .000  
 03862+ R0005:CO0183-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03863+ [iabErc 4.001: iabErc 4.001] .000  
 03864+ [iabErc 4.001: iabErc 4.001] .000  
 03865+ R0005:CO0184-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03866+ [iabErc 4.001: iabErc 4.001] .000  
 03867+ R0005:CO0185-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03868+ SAVE HYD 1.0 01:CLAR\_M2 159.40 10.597 No\_date 28:05 41.21 .722 .000  
 03869+ [CN .77.01: NO .30: Tp .11] .000  
 03870+ R0005:CO0186-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03871+ [iabErc 4.001: iabErc 4.001] .000  
 03872+ R0005:CO0187-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03873+ [iabErc 4.001: iabErc 4.001] .000  
 03874+ R0005:CO0188-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03875+ [iabErc 4.001: iabErc 4.001] .000  
 03876+ R0005:CO0189-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03877+ [iabErc 4.001: iabErc 4.001] .000  
 03878+ R0005:CO0190-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03879+ [iabErc 4.001: iabErc 4.001] .000  
 03880+ R0005:CO0191-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03881+ [iabErc 4.001: iabErc 4.001] .000  
 03882+ R0005:CO0192-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03883+ [iabErc 4.001: iabErc 4.001] .000  
 03884+ R0005:CO0193-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03885+ [iabErc 4.001: iabErc 4.001] .000  
 03886+ R0005:CO0194-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03887+ [iabErc 4.001: iabErc 4.001] .000  
 03888+ R0005:CO0195-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03889+ [iabErc 4.001: iabErc 4.001] .000  
 03890+ R0005:CO0196-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03891+ [iabErc 4.001: iabErc 4.001] .000  
 03892+ R0005:CO0197-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03893+ [iabErc 4.001: iabErc 4.001] .000  
 03894+ R0005:CO0198-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03895+ [iabErc 4.001: iabErc 4.001] .000  
 03896+ R0005:CO0199-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03897+ [iabErc 4.001: iabErc 4.001] .000  
 03898+ R0005:CO0200-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03899+ [iabErc 4.001: iabErc 4.001] .000  
 03900+ R0005:CO0201-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03901+ [iabErc 4.001: iabErc 4.001] .000  
 03902+ R0005:CO0202-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03903+ [iabErc 4.001: iabErc 4.001] .000  
 03904+ R0005:CO0203-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03905+ [iabErc 4.001: iabErc 4.001] .000  
 03906+ R0005:CO0204-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03907+ [iabErc 4.001: iabErc 4.001] .000  
 03908+ R0005:CO0205-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03909+ [iabErc 4.001: iabErc 4.001] .000  
 03910+ R0005:CO0206-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03911+ [iabErc 4.001: iabErc 4.001] .000  
 03912+ R0005:CO0207-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03913+ [iabErc 4.001: iabErc 4.001] .000  
 03914+ R0005:CO0208-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03915+ [iabErc 4.001: iabErc 4.001] .000  
 03916+ R0005:CO0209-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03917+ [iabErc 4.001: iabErc 4.001] .000  
 03918+ R0005:CO0210-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03919+ [iabErc 4.001: iabErc 4.001] .000  
 03920+ R0005:CO0211-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03921+ [iabErc 4.001: iabErc 4.001] .000  
 03922+ R0005:CO0212-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03923+ [iabErc 4.001: iabErc 4.001] .000  
 03924+ R0005:CO0213-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03925+ [iabErc 4.001: iabErc 4.001] .000  
 03926+ R0005:CO0214-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03927+ [iabErc 4.001: iabErc 4.001] .000  
 03928+ R0005:CO0215-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03929+ [iabErc 4.001: iabErc 4.001] .000  
 03930+ R0005:CO0216-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03931+ [iabErc 4.001: iabErc 4.001] .000  
 03932+ R0005:CO0217-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03933+ [iabErc 4.001: iabErc 4.001] .000  
 03934+ R0005:CO0218-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03935+ [iabErc 4.001: iabErc 4.001] .000  
 03936+ R0005:CO0219-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03937+ [iabErc 4.001: iabErc 4.001] .000  
 03938+ R0005:CO0220-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03939+ [iabErc 4.001: iabErc 4.001] .000  
 03940+ R0005:CO0221-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03941+ [iabErc 4.001: iabErc 4.001] .000  
 03942+ R0005:CO0222-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03943+ [iabErc 4.001: iabErc 4.001] .000  
 03944+ R0005:CO0223-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03945+ [iabErc 4.001: iabErc 4.001] .000  
 03946+ R0005:CO0224-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03947+ [iabErc 4.001: iabErc 4.001] .000  
 03948+ R0005:CO0225-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03949+ [iabErc 4.001: iabErc 4.001] .000  
 03950+ R0005:CO0226-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03951+ [iabErc 4.001: iabErc 4.001] .000  
 03952+ R0005:CO0227-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03953+ [iabErc 4.001: iabErc 4.001] .000  
 03954+ R0005:CO0228-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03955+ [iabErc 4.001: iabErc 4.001] .000  
 03956+ R0005:CO0229-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03957+ [iabErc 4.001: iabErc 4.001] .000  
 03958+ R0005:CO0230-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03959+ [iabErc 4.001: iabErc 4.001] .000  
 03960+ R0005:CO0231-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03961+ [iabErc 4.001: iabErc 4.001] .000  
 03962+ R0005:CO0232-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03963+ [iabErc 4.001: iabErc 4.001] .000  
 03964+ R0005:CO0233-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03965+ [iabErc 4.001: iabErc 4.001] .000  
 03966+ R0005:CO0234-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03967+ [iabErc 4.001: iabErc 4.001] .000  
 03968+ R0005:CO0235-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03969+ [iabErc 4.001: iabErc 4.001] .000  
 03970+ R0005:CO0236-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03971+ [iabErc 4.001: iabErc 4.001] .000  
 03972+ R0005:CO0237-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03973+ [iabErc 4.001: iabErc 4.001] .000  
 03974+ R0005:CO0238-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03975+ [iabErc 4.001: iabErc 4.001] .000  
 03976+ R0005:CO0239-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03977+ [iabErc 4.001: iabErc 4.001] .000  
 03978+ R0005:CO0240-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03979+ [iabErc 4.001: iabErc 4.001] .000  
 03980+ R0005:CO0241-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03981+ [iabErc 4.001: iabErc 4.001] .000  
 03982+ R0005:CO0242-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03983+ [iabErc 4.001: iabErc 4.001] .000  
 03984+ R0005:CO0243-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03985+ [iabErc 4.001: iabErc 4.001] .000  
 03986+ R0005:CO0244-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03987+ [iabErc 4.001: iabErc 4.001] .000  
 03988+ R0005:CO0245-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03989+ [iabErc 4.001: iabErc 4.001] .000  
 03990+ R0005:CO0246-----DTin-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm-->Rvn=R.C.--DFWcm  
 03991+ [iabErc 4.001: iabErc 4.001] .000  
 03992+ R0005:CO0247-----DTin-ID:NHYD----ARAhA-QPE







05237# R0005:CO0400-----Dtnin-ID:NHYD-----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05238# ADD HYD 1.0 02:NM\_1 5549.24 72.207 No\_date 36:46 18.89 n/a .000  
 05239# + 1.0 01:NM\_1 102.54 72.207 No\_date 36:46 18.89 n/a .000  
 05240# SUM-----1.0 01:NM\_NI 5579.20 72.356 No\_date 36:46 18.89 n/a .000  
 05241# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05242# SAVE HYD 1.0 01:NM\_NI 5579.20 72.356 No\_date 36:46 18.89 n/a .000  
 05243# fname :SN\_NI\_0005  
 05244# location : Rideau River  
 05245# =====# END OF RUN : 9  
 05246# \*\*\*\*\*  
 05247# \*\*\*\*\*  
 05248# \*\*\*\*\*  
 05249# \*\*\*\*\*  
 05250# \*\*\*\*\*  
 05251# \*\*\*\*\*  
 05252# \*\*\*\*\*  
 05253# \*\*\*\*\*  
 05254# RUNS=COMMAND#  
 05255# R0010:CO0001-----  
 05256# STORM-----  
 05257# [TZERO = .00 hrs on 0]  
 05258# [METCOUT = 2 (Imperial, 2-metric output)]  
 05259# [NRUN = 0014]  
 05260# \*\*\*\*\*  
 05261# \*\*\*\*\*  
 05262# \*\*\*\*\*  
 05263# \*\*\*\*\*  
 05264# # Project Name: [Rock River] Project Number: [1474-16]  
 05265# \*\*\*\*\*  
 05266# # Modeler : [H.M.]  
 05267# # Company : JFSAinc.  
 05268# \*\*\*\*\*  
 05269# \*\*\*\*\*  
 05270# # CALIBRATION OF SUMMER MODEL PARAMETERS  
 05271# \*\*\*\*\*  
 05272# Rainfall data from JFSA rain gauge installed at site + other gauges by the City  
 05273# # Use data collected from May 1st to July 14, 2003  
 05274# \*\*\*\*\*  
 05275# 2020-12-01 correct pond curve values  
 05276# 2020-12-01 change W\_CLAR\_BAS\_KIM to 0.85 (SM2+(0.5)\*1) (impermeable slope), and LZR up to 700m  
 05277# 2020-12-01 change W\_CLAR\_BAS\_KIM to 0.85 (SM2+(0.5)\*1) (impermeable slope), and LZR up to 700m  
 05278# 2021-02-19 change the slope for SOUTH CHANNEL Station 5002 (NHYDout=[\*SN\_C2\*]), NHYDin=[\*SN\_C2\*]) from 0.033 % (as per S  
 05279# R0010:CO0002-----  
 05280# READING STORM  
 05281# Filename = storm.001  
 05282# \*\*\*\*\*  
 05283# \*\*\*\*\*  
 05284# \*\*\*\*\*  
 05285# [STW+10.00:SOUR= 24.00:PTOT= 64.69]  
 05286# R0010:CO0003-----  
 05287# [RFACFT=.1.00:TSHFTP=.960.00:min]  
 05288# [RFACFT=.00:THDT=.40:PTOTP=.64.69]  
 05289# R0010:CO0004-----  
 05290# DEFAULT VALUES  
 05291# ICAE901:1 (read and print data)  
 05292# \*\*\*\*\*  
 05293# FileTitle: File comment [Based on various calibration exercises in Ontario and the USA, and the design of the model in the DESIGN STANDARD COR  
 05294# \*\*\*\*\*  
 05295# Horton's infiltration equation parameters:  
 05296# [Fw=.76.20 mm/hr] [Fw=.15.20 mm hr] [Dcav=.4.14 hr] [Fw=.00 mm]  
 05297# [Pd=.00 mm] [Pd=.00 mm] [Pd=.00 mm] [Pd=.00 mm]  
 05298# [Apers=.4.67 mm] [Ldg=.50.00 mm] [Mdp=.250]  
 05299# Parameters for IMPERVIOUS surfaces in STANDHYD:  
 0530# [Infil=.0000000000.00] [MMT=.013]  
 05301# Parameters used in NASHYD:  
 05302# [ia=.4.67 mm] [In=.3.00]  
 05303# Average daily precipitation data in (mm):  
 05304# JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC  
 05305# .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00  
 05306# .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00  
 05307# .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00  
 05308# .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00  
 05309# R0010:CO0005-----  
 05310# COMPUTE API  
 05311# [APINit=.50.01: APIEnd=.8500: APIKdt=.9989]  
 05312# [APINext=.97.01: APIAvg=.62.29: APISlope=.44.87]  
 05313# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
 05314# \*\*\*\*\*  
 05315# CONTINUOUS NASHYD 1.0 01:SW\_13 3680.00 11.879 No\_date 36:59 20.23 .313 .000  
 05316# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05317# -----CONTINUOUS NASHYD 1.0 01:SW\_13 3680.00 11.879 No\_date 36:59 20.23 .313 .000  
 05318# [TaEBC=.4.00: SMIN=.57.05: SMAZ=.380.32: SK=.010]  
 05319# [InterEventTime= 12.00]  
 05320# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
 05321# \*\*\*\*\*  
 05322# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
 05323# \*\*\*\*\*  
 05324# R0010:CO0007-----  
 05325# CONTINUOUS NASHYD 1.0 01:SW\_13 971.00 4.365 No\_date 32:35 18.83 .291 .000  
 05326# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05327# [CN=.61.00: NO=.3.00:Tp=.37.61]  
 05328# [TaEBC=.4.00: SMIN=.59.75: SMAZ=.430.01: SK=.010]  
 05329# [InterEventTime= 12.00]  
 05330# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
 05331# \*\*\*\*\*  
 05332# R0010:CO0008-----  
 05333# CONTINUOUS NASHYD 1.0 01:SW\_13 1781.00 10.839 No\_date 32:42 24.81 .388 .000  
 05334# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05335# [TaEBC=.4.00: SMIN=.79.75: SMAZ=.264.99: SK=.010]  
 05336# [InterEventTime= 12.00]  
 05337# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
 05338# \*\*\*\*\*  
 05339# R0010:CO0009-----  
 05340# CONTINUOUS NASHYD 1.0 01:SW\_13 500.00 5.639 No\_date 29:22 21.19 .328 .000  
 05341# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05342# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05343# [TaEBC=.4.00: SMIN=.52.62: SMAZ=.350.79: SK=.010]  
 05344# [InterEventTime= 12.00]  
 05345# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
 05346# \*\*\*\*\*  
 05347# R0010:CO0010-----  
 05348# CONTINUOUS NASHYD 1.0 01:SW\_13 500.00 5.639 No\_date 29:22 21.19 .328 .000  
 05349# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05350# [TaEBC=.4.00: SMIN=.52.62: SMAZ=.350.79: SK=.010]  
 05351# [InterEventTime= 12.00]  
 05352# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
 05353# \*\*\*\*\*  
 05354# R0010:CO0011-----  
 05355# CONTINUOUS NASHYD 1.0 01:SW\_13 1917.00 7.897 No\_date 34:28 21.19 .328 .000  
 05356# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05357# [TaEBC=.4.00: SMIN=.59.75: SMAZ=.264.99: SK=.010]  
 05358# [InterEventTime= 12.00]  
 05359# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
 05360# \*\*\*\*\*  
 05361# R0010:CO0012-----  
 05362# CONTINUOUS NASHYD 1.0 01:SW\_13 5666.00 21.295 No\_date 37:58 24.81 .388 .000  
 05363# [TaEBC=.4.00: SMIN=.59.75: SMAZ=.264.99: SK=.010]  
 05364# [CN=.72.00: NO=.3.00:Tp=.8.00]  
 05365# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05366# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05367# [TaEBC=.4.00: SMIN=.59.75: SMAZ=.264.99: SK=.010]  
 05368# [InterEventTime= 12.00]  
 05369# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
 05370# \*\*\*\*\*  
 05371# R0010:CO0013-----  
 05372# CONTINUOUS NASHYD 1.0 01:SW\_13 8376.00 20.398 No\_date 39:59 21.19 .328 .000  
 05373# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05374# [TaEBC=.4.00: SMIN=.59.75: SMAZ=.264.99: SK=.010]  
 05375# [InterEventTime= 12.00]  
 05376# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
 05377# \*\*\*\*\*  
 05378# R0010:CO0014-----  
 05379# CONTINUOUS NASHYD 1.0 01:SW\_13 3854.00 11.811 No\_date 38:37 21.19 .328 .000  
 05380# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05381# [TaEBC=.4.00: SMIN=.59.75: SMAZ=.264.99: SK=.010]  
 05382# [InterEventTime= 12.00]  
 05383# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
 05384# \*\*\*\*\*  
 05385# R0010:CO0015-----  
 05386# CONTINUOUS NASHYD 1.0 01:SW\_13 131.00 1.689 No\_date 28:57 19.76 .305 .000  
 05387# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05388# [TaEBC=.4.00: SMIN=.59.75: SMAZ=.264.99: SK=.010]  
 05389# [CN=.63.00: NO=.3.00:Tp=.90]  
 05390# [TaEBC=.4.00: SMIN=.59.75: SMAZ=.264.99: SK=.010]  
 05391# [CN=.64.00: NO=.3.00:Tp=.65.11]  
 05392# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05393# [TaEBC=.4.00: SMIN=.59.42: SMAZ=.396.11: SK=.010]  
 05394# [InterEventTime= 12.00]  
 05395# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
 05396# \*\*\*\*\*  
 05397# R0010:CO0016-----  
 05398# CONTINUOUS NASHYD 1.0 01:SW\_13 133.00 1.689 No\_date 28:57 19.76 .305 .000  
 05399# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05400# [TaEBC=.4.00: SMIN=.59.75: SMAZ=.264.99: SK=.010]  
 05401# [TaEBC=.4.00: SMIN=.52.62: SMAZ=.350.79: SK=.010]  
 05402# [InterEventTime= 12.00]  
 05403# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
 05404# \*\*\*\*\*  
 05405# R0010:CO0017-----  
 05406# CONTINUOUS NASHYD 1.0 01:SW\_7 3197.00 8.899 No\_date 36:26 17.07 .264 .000  
 05407# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05408# [CN=.67.00: NO=.3.00:Tp=.4.18]  
 05409# [TaEBC=.4.00: SMIN=.50.55: SMAZ=.336.97: SK=.010]  
 05410# [CN=.67.00: NO=.3.00:Tp=.6.65]  
 05411# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
 05412# \*\*\*\*\*  
 05413# R0010:CO0018-----  
 05414# CONTINUOUS NASHYD 1.0 01:SW\_6 165.00 .818 No\_date 33:04 21.69 .335 .000  
 05415# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05416# [TaEBC=.4.00: SMIN=.50.81: SMAZ=.508.81: SK=.010]  
 05417# [InterEventTime= 12.00]  
 05418# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
 05419# \*\*\*\*\*  
 05420# R0010:CO0019-----  
 05421# CONTINUOUS NASHYD 1.0 01:VG\_DR 1332.00 6.069 No\_date 35:17 24.81 .388 .000  
 05422# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05423# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05424# [CN=.72.00: NO=.3.00:Tp=.5.95]  
 05425# [TaEBC=.4.00: SMIN=.50.75: SMAZ=.264.99: SK=.010]  
 05426# [CN=.72.00: NO=.3.00:Tp=.5.95]  
 05427# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05428# [TaEBC=.4.00: SMIN=.50.75: SMAZ=.264.99: SK=.010]  
 05429# [CN=.72.00: NO=.3.00:Tp=.5.95]  
 05430# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05431# [TaEBC=.4.00: SMIN=.50.75: SMAZ=.264.99: SK=.010]  
 05432# [CN=.72.00: NO=.3.00:Tp=.5.95]  
 05433# # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
 05434# \*\*\*\*\*  
 05435# R0010:CO0020-----  
 05436# CONTINUOUS NASHYD 1.0 01:FLC\_C 4945.00 28.945 No\_date 33:21 25.91 .401 .000  
 05437# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05438# [TaEBC=.4.00: SMIN=.36.67: SMAZ=.244.49: SK=.010]  
 05439# [CN=.72.00: NO=.3.00:Tp=.5.95]  
 05440# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05441# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05442# [CN=.81.00: NO=.3.00:Tp=.62]  
 05443# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05444# [TaEBC=.4.00: SMIN=.25.21: SMAZ=.168.09: SK=.010]  
 05445# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05446# [TaEBC=.4.00: SMIN=.25.21: SMAZ=.168.09: SK=.010]  
 05447# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05448# [TaEBC=.4.00: SMIN=.25.21: SMAZ=.168.09: SK=.010]  
 05449# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05450# [CN=.81.00: NO=.3.00:Tp=.8.00]  
 05451# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05452# [TaEBC=.4.00: SMIN=.33.81: SMAZ=.225.43: SK=.010]  
 05453# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05454# [TaEBC=.4.00: SMIN=.33.81: SMAZ=.225.43: SK=.010]  
 05455# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05456# [TaEBC=.4.00: SMIN=.25.21: SMAZ=.168.09: SK=.010]  
 05457# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05458# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05459# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05460# [CN=.80.00: NO=.3.00:Tp=.2.46]  
 05461# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05462# [TaEBC=.4.00: SMIN=.25.21: SMAZ=.167.50: SK=.010]  
 05463# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05464# [TaEBC=.4.00: SMIN=.25.21: SMAZ=.167.50: SK=.010]  
 05465# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05466# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05467# [TaEBC=.4.00: SMIN=.25.21: SMAZ=.167.50: SK=.010]  
 05468# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05469# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05470# [TaEBC=.4.00: SMIN=.25.21: SMAZ=.168.09: SK=.010]  
 05471# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05472# [TaEBC=.4.00: SMIN=.25.21: SMAZ=.168.09: SK=.010]  
 05473# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05474# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05475# [TaEBC=.4.00: SMIN=.25.21: SMAZ=.168.09: SK=.010]  
 05476# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05477# [TaEBC=.4.00: SMIN=.25.21: SMAZ=.168.09: SK=.010]  
 05478# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05479# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05480# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05481# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05482# -----Starting with the addition of Rock River Headwater and Subwatershed 13  
 05483# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05484# -----ADD HYD 1.0 01:NM\_1 102.00 5.817 No\_date 37:54 27.06 .418 .000  
 05485# -----CONTINUOUS NASHYD 1.0 01:LM\_C 1021.00 11.195 No\_date 30:48 30.72 .475 .000  
 05486# -----SUM-----1.0 01:NM\_1 1021.00 11.195 No\_date 30:48 30.72 .475 .000  
 05487# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05488# -----Sum of hydrographs from Node 13 routed to Node 13A  
 05489# -----[Approximated cross-section - see cross-section 258]  
 05490# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05491# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05492# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05493# -----ROUTE CHANNEL => 1.0 02:NM\_1 7275.00 17.918 No\_date 39:59 18.46 n/a .000  
 05494# -----ROUTE RESERVOIR => 1.0 02:NM\_1 7275.00 17.918 No\_date 39:59 18.46 n/a .000  
 05495# -----ROUTE CHANNEL => 1.0 02:NM\_1 7275.00 17.918 No\_date 39:59 18.46 n/a .000  
 05496# -----ROUTE RESERVOIR => 1.0 02:NM\_1 7275.00 17.918 No\_date 39:59 18.46 n/a .000  
 05497# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05498# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05499# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05500# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05501# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05502# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05503# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05504# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05505# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05506# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05507# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05508# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05509# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05510# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05511# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05512# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05513# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05514# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05515# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05516# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05517# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05518# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05519# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05520# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05521# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05522# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05523# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05524# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05525# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05526# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05527# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05528# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05529# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05530# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05531# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05532# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05533# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05534# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05535# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05536# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05537# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05538# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05539# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05540# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05541# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05542# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05543# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05544# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05545# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05546# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05547# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05548# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05549# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05550# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05551# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05552# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05553# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05554# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05555# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05556# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05557# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05558# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05559# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05560# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05561# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05562# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05563# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05564# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05565# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05566# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05567# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05568# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm-B.C.---DFWcmns  
 05569# -----ARBAha-QPEAKcms-TpeakDate\_hh:mm:---RVm

05611+ ADD HYD 1.0 02:NB 31561.00 61.483 No\_date 39:57 21.20 n/a .000  
 05612+ \* 1.0 02:SW\_6 133.00 1.689 No\_date 28:51 19.76 n/a .000  
 05613+ \* 1.0 02:SW\_6 31562.00 61.483 No\_date 39:57 21.20 n/a .000  
 05614+ SUM+ 1.0 01:SNS 35546.00 73.344 No\_date 39:57 21.19 n/a .000  
 05615+ # Sum of hydrographs from Node 8 routed to Node 7  
 05616+ # Section 4  
 05617+ R0101:000449-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05618+ ROUTE CHANNEL -> 1.0 02:SW\_8 35546.00 73.344 No\_date 39:57 21.19 n/a .000  
 05619+ [ROT: 1.00] out-> 1.0 01:SNS 35546.00 61.416 No\_date 48:01 21.19 n/a .000  
 05620+ [/S/n .1750/. .053/.078] .  
 05621+ [Vmax=.218:Imax=.1987]  
 05622+ # Catchment NASHYD  
 05623+ # Addition of Subwatershed 7 to Node 7  
 05624+ # Section 4  
 05625+ R0101:000449-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05626+ ADD HYD 1.0 02:NT 35546.00 61.416 No\_date 45:01 21.19 n/a .000  
 05627+ \* 1.0 02:SW\_7 3197.00 8.899 No\_date 36:26 17.07 n/a .000  
 05628+ SUM+ 1.0 01:SNS 35546.00 61.416 No\_date 45:01 21.19 n/a .000  
 05629+ # Sum of hydrographs from Node 7 routed to Node 6  
 05630+ R0101:000500-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05631+ SAVE HYD 1.0 01:SNS 38743.00 65.819 No\_date 44:06 20.85 n/a .000  
 05632+ # Catchment NASHYD  
 05633+ # Insertion of a reservoir to simulate the effects of the Subcatchment.  
 05634+ # Streamflow was controlled by the reservoir available atop map.  
 05635+ # Release rate from fens was assumed to be controlled by the downstream  
 05636+ # river cross-section for summer conditions. It was assumed that up to  
 05637+ # 10% of the flow from the fens would be diverted to riverbank storage. Above  
 05638+ # this depth, the wetlands start to significantly store water.  
 05639+ # this depth, the wetlands start to significantly store water.  
 05640+ # depth, the wetlands start to significantly store water.  
 05641+ R0101:000511-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05642+ ROUTE RESERVOIR -> 1.0 02:SW\_7 38743.00 65.819 No\_date 44:06 20.85 n/a .000  
 05643+ [ROT: 1.00] out-> 1.0 01:SNS\_RP 38743.00 31.796 No\_date 60:32 20.85 n/a .000  
 05644+ [/S/n .4630/. .0428/.01] .  
 05645+ [Vmax=.477:Imax=.960]  
 05646+ # Catchment NASHYD  
 05647+ # Addition of Subwatershed 6 to Vaal Grain Drain to Node 6  
 05648+ # Section 5  
 05649+ R0101:000513-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05650+ ROUTE CHANNEL -> 1.0 02:RSPF 38743.00 31.796 No\_date 60:32 20.85 n/a .000  
 05651+ [ROT: 1.00] out-> 1.0 01:SNS\_RP 38743.00 31.796 No\_date 60:32 20.85 n/a .000  
 05652+ [/S/n .4630/. .0428/.01] .  
 05653+ [Vmax=.477:Imax=.960]  
 05654+ # Catchment NASHYD  
 05655+ # Addition of Subwatershed 6 and Vaal Grain Drain to Node 6  
 05656+ R0101:000514-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05657+ ADD HYD 1.0 02:NB 38743.00 31.796 No\_date 60:32 20.85 n/a .000  
 05658+ \* 1.0 02:SW\_6 165.00 .838 No\_date 33:04 21.69 n/a .000  
 05659+ \* 1.0 02:VGD\_6 1332.00 6.069 No\_date 35:17 24.81 n/a .000  
 05660+ SUM+ 1.0 01:SNS 40245.01 31.797 No\_date 62:00 20.99 n/a .000  
 05661+ # Sum of hydrographs from Node 6 routed to Node 5  
 05662+ # Section 5  
 05663+ R0101:000555-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05664+ ROUTE CHANNEL -> 1.0 02:RSPF 38743.00 31.796 No\_date 62:00 20.99 n/a .000  
 05665+ [ROT: 1.00] out-> 1.0 01:SNS 38743.00 31.737 No\_date 62:48 20.99 n/a .000  
 05666+ [/S/n .4630/. .0428/.01] .  
 05667+ [Vmax=.477:Imax=.960]  
 05668+ # Catchment NASHYD  
 05669+ # Addition of Subwatershed 5 and Flowing Creek to Node 5  
 05670+ R0101:000556-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05671+ ADD HYD 1.0 02:NB 40240.01 31.713 No\_date 62:48 20.99 n/a .000  
 05672+ \* 1.0 02:SW\_5 224.00 5.246 No\_date 28:45 28.24 n/a .000  
 05673+ \* 1.0 02:FPLC\_5 4945.00 28.945 No\_date 33:21 25.91 n/a .000  
 05674+ SUM+ 1.0 01:SNS 45409.01 51.448 No\_date 34:54 21.56 n/a .000  
 05675+ # Sum of hydrographs from Node 5 routed to Node 4  
 05676+ # Section 4  
 05677+ R0101:000557-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05678+ ADD HYD 1.0 02:NB 45409.01 51.448 No\_date 34:54 21.56 n/a .000  
 05679+ \* 1.0 02:SW\_5 26.00 1.01 No\_date 28:36 21.93 n/a .000  
 05680+ [/S/n .556/. .054/.038] .  
 05681+ [Vmax=.477:Imax=.1089]  
 05682+ # Catchment NASHYD  
 05683+ # Addition of Subwatershed 5 and Flowing Creek to Node 5  
 05684+ R0101:000558-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05685+ ADD HYD 1.0 02:NB 45409.01 51.448 No\_date 34:54 21.56 n/a .000  
 05686+ \* 1.0 02:SW\_5 51.312 No\_date 34:54 21.56 n/a .000  
 05687+ [/S/n .4630/. .0428/.01] .  
 05688+ [Vmax=.477:Imax=.1089]  
 05689+ # Catchment NASHYD  
 05690+ # Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A  
 05691+ R0101:000559-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05692+ ADD HYD 1.0 02:NB 45409.01 51.312 No\_date 34:54 21.56 n/a .000  
 05693+ \* 1.0 02:SW\_5A1 26.00 1.01 No\_date 34:54 21.56 n/a .000  
 05694+ [/S/n .556/. .054/.040] .  
 05695+ [Vmax=.477:Imax=.1151]  
 05696+ # Catchment NASHYD  
 05697+ # Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A  
 05698+ R0101:000560-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05699+ ADD HYD 1.0 02:NB 45409.01 51.312 No\_date 34:54 21.56 n/a .000  
 05700+ \* 1.0 02:SW\_5A1 1412.00 5.827 No\_date 37:54 27.06 n/a .000  
 05701+ SUM+ 1.0 01:SNS 46841.01 56.788 No\_date 35:22 21.73 n/a .000  
 05702+ # Sum of hydrographs from Node 5 routed to Node 4  
 05703+ # Section 4  
 05704+ R0101:000559-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05705+ ROUTE CHANNEL -> 1.0 02:SNS 46841.01 56.788 No\_date 35:22 21.73 n/a .000  
 05706+ [ROT: 1.00] out-> 1.0 01:SNS 46841.01 56.543 No\_date 38:56 21.73 n/a .000  
 05707+ [/S/n .4630/. .0428/.01] .  
 05708+ [Vmax=.477:Imax=.3295]  
 05709+ # Catchment NASHYD  
 05710+ # Addition of Subwatershed 4 and Leamy Creek to Node 4  
 05711+ R0101:000560-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05712+ ADD HYD 1.0 02:NB 46841.01 54.543 No\_date 38:56 21.73 n/a .000  
 05713+ \* 1.0 02:SW\_4 17.00 1.01 No\_date 38:56 21.73 n/a .000  
 05714+ \* 1.0 02:IN\_4 122.00 10.275 No\_date 38:48 30.72 n/a .000  
 05715+ \* 1.0 02:IN\_4 122.00 11.195 No\_date 38:48 30.72 n/a .000  
 05716+ SUM+ 1.0 01:SNS 48447.00 59.934 No\_date 38:56 22.03 n/a .000  
 05717+ R0101:000561-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05718+ ADD HYD 1.0 02:NB 48447.00 59.934 No\_date 38:56 22.03 n/a .000  
 05719+ frame: S\_N4\_0010  
 05720+ remark:flow at S\_N4  
 05721+ # Catchment NASHYD  
 05722+ # Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2  
 05723+ # Section 4  
 05724+ R0101:000559-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05725+ ADD HYD 1.0 02:NB 48447.00 59.699 No\_date 38:56 22.03 n/a .000  
 05726+ \* 1.0 02:SW\_2 17.00 1.01 No\_date 38:56 22.03 n/a .000  
 05727+ [/S/n .4630/. .0428/.01] .  
 05728+ [Vmax=.477:Imax=.3295]  
 05729+ # Catchment NASHYD  
 05730+ # Addition of Subwatershed 4 and Leamy Creek to Node 4  
 05731+ R0101:000560-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05732+ ADD HYD 1.0 02:NB 48447.00 59.934 No\_date 38:56 22.03 n/a .000  
 05733+ \* 1.0 02:SW\_2 17.00 1.01 No\_date 38:56 22.03 n/a .000  
 05734+ SUM+ 1.0 01:SNS 52481.00 83.235 No\_date 33:15 22.55 n/a .000  
 05735+ frame: S\_H2N2  
 05736+ remark:flow at S\_N2 Rock Jock River Gauge at Moodie Dr.  
 05737+ # Sum of hydrograph from Node 2 routed to Node 1  
 05738+ # Section 10
 05739+ # Hydrograph from Node 2 routed to Node 4  
 05740+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 9025  
 05741+ # Catchment NASHYD  
 05742+ # - Portion of RVCA catchment SW\_1 outside of Reach 1 subwatershed  
 05743+ # - Undeveloped agricultural land  
 05744+ # - Catchment NASHYD  
 05745+ # - Portion of RVCA catchment SW\_1 outside of Reach 1 subwatershed  
 05746+ R0101:000566-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05747+ CONTINUOUS NASHYD 1.0 01:SW\_1M 536.42 3.888 No\_date 31:17 23.57 3.644 .000  
 05748+ [/S/n .4630/. .0428/.01] .  
 05749+ [Vmax=.477:Imax=.4949]  
 05750+ # Catchment NASHYD  
 05751+ # - Portion of RVCA catchment SW\_1 outside of Reach 1 subwatershed  
 05752+ # - Catchment NASHYD  
 05753+ # - Portion of RVCA catchment SW\_1 outside of Reach 1 subwatershed  
 05754+ R0101:000566-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05755+ CONTINUOUS NASHYD 1.0 01:SW\_1K 44.93 .778 No\_date 29:07 26.85 .415 .000  
 05756+ [/S/n .4630/. .0428/.01] .  
 05757+ [Vmax=.477:Imax=.4949]  
 05758+ # Catchment NASHYD  
 05759+ # - Portion of RVCA catchment SW\_1 outside of Reach 1 subwatershed  
 05760+ # - Catchment NASHYD  
 05761+ # - Portion of RVCA catchment SW\_1 outside of Reach 1 subwatershed  
 05762+ # - Catchment NASHYD  
 05763+ # - Portion of RVCA catchment SW\_1 outside of Reach 1 subwatershed  
 05764+ R0101:000566-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05765+ CONTINUOUS NASHYD 1.0 01:SW\_1K 44.93 .778 No\_date 29:07 26.85 .415 .000  
 05766+ [/S/n .4630/. .0428/.01] .  
 05767+ [Vmax=.477:Imax=.4949]  
 05768+ # Catchment NASHYD  
 05769+ # - Portion of RVCA catchment SW\_1 outside of Reach 1 subwatershed  
 05770+ # - Catchment NASHYD  
 05771+ # - Portion of RVCA catchment SW\_1 outside of Reach 1 subwatershed  
 05772+ # Catchment NASHYD  
 05773+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 7245  
 05774+ # Hydrograph from Node 4 routed to Node 4 at Highway 416  
 05775+ ADD HYD 1.0 02:IN\_416 52481.00 81.216 No\_date 34:18 22.55 n/a .000  
 05776+ \* 1.0 02:IN\_416 536.42 3.888 No\_date 31:17 23.57 n/a .000  
 05777+ SUM+ 1.0 01:SNS 53064.36 84.151 No\_date 29:07 26.85 n/a .000  
 05778+ R0101:000569-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05779+ CONTINUOUS NASHYD 1.0 01:IN\_416 44.93 .778 No\_date 31:41 22.55 n/a .000  
 05780+ [/S/n .4630/. .0428/.01] .  
 05781+ [Vmax=.477:Imax=.4949]  
 05782+ # Catchment NASHYD  
 05783+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 7245  
 05784+ # Hydrograph from Node 4 routed to Node 4 at Highway 416  
 05785+ ADD HYD 1.0 02:IN\_416 53064.36 84.151 No\_date 34:18 22.55 n/a .000  
 05786+ \* 1.0 02:IN\_416 536.42 3.888 No\_date 34:18 22.55 n/a .000  
 05787+ SUM+ 1.0 01:SNS 53064.36 84.151 No\_date 34:18 22.55 n/a .000  
 05788+ R0101:000570-----Dtnin:ID:NHYD-----ARAHa-QPEAKcms-Tpeakdate\_bh:mm:---RVm-R.C.--DWFcms  
 05789+ CONTINUOUS NASHYD 1.0 01:IN\_416 44.93 .778 No\_date 29:07 26.85 .415 .000  
 05790+ [/S/n .4630/. .0428/.01] .  
 05791+ [Vmax=.477:Imax=.4949]  
 05792+ # Catchment NASHYD  
 05793+ # - To O'keefe drain (node 018 of the Jock)  
 05794+ # - Downstream with O'keefe model (Area 513.02 HA) instead of current O'keefe (Area 513.02 HA)  
 05795+ # 2012-10-20 O'keefe detailed model was added as per the NOVATECH SWMMO model (Citi-Gate 2014).  
 05796+ # 2012-10-20 O'keefe detailed model was added as per the NOVATECH SWMMO model (Citi-Gate 2014).  
 05797+ #



06359+ [InterEventTime= 12.00] ...  
 06360+ R0010:CO0166----> Dtnin-ID:NHYD--- ADD HVD ...  
 06361+ ADD HVD ...  
 06362+ + 1.0 02N.FO 53577.82 85.413 No\_date 34:07 22.40 n/a .000  
 06363+ + 1.0 02S-2Q-out 335.49 5.972 No\_date 29:28 26.45 n/a .000  
 06364+ + 1.0 02S-1Q-OPV 73.97 1.158 No\_date 29:00 47.94 n/a .000  
 06365+ + 1.0 02P-OPV .00 1.02E-01 No\_date 29:00 .000  
 06366+ + 1.0 02W-CLAR\_UND 35.65 .596 No\_date 29:11 26.85 n/a .000  
 06367+ + 1.0 02S-1-PO-FD 14.56 .267 No\_date 28:00 .000  
 06368+ + 1.0 02S-1-A 5.72 .709 No\_date 28:00 48.43 n/a .000  
 06369+ \* 1.0 02S-1-A 78.86 1.915 No\_date 28:16 26.85 n/a .000  
 06370+ SMM+ 1.0 01N.MC 54118.36 89.156 No\_date 33:42 22.78 n/a .000  
 06371+ SAVV HYD 1.0 01N.FO 54118.36 89.156 No\_date 33:42 22.78 n/a .000  
 06372+ frame: SN\_FO\_0010  
 06373+ # remark:Total Flows at Foster Drain  
 06374+ # Hydrograph from Node Foster routed to Node at Cedarview Road  
 06375+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 6016  
 06376+ #  
 06377+ R0010:CO0168----> Dtnin-ID:NHYD--- ADD HVD ...  
 06378+ \* [S0T: 1.00] out+ 1.0 01N.CE 54118.36 89.156 No\_date 33:42 22.78 n/a .000  
 06379+ [L8/n= .159/.082/.036]  
 06380+ [Imperious area: Iaper= 4.67SLPP+ .50LGI+ 522.MNI+ .013:SCI+ .01]  
 06381+ #  
 06382+ \*\*\*\*\*  
 06383+ # Catchment S-1  
 06384+ # - Tributary Area (north and south of Jack)  
 06385+ # - Primarily agricultural fields; portion of sand quarry  
 06386+ R0010:CO0169----> Dtnin-ID:NHYD--- ADD HVD ...  
 06387+ CONTINUOUS\_NASHYD 1.0 01S-1-B 55.36 1.740 No\_date 28:24 26.85 .415 .000  
 06388+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06389+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06390+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06391+ [InterEventTime= 12.00] ...  
 06392+ # - JFSA 2021-02-24 change the names from S-1-BDCD to S-1-A and S-1-B. Change their TP values based on the pattern of "S-1-PO-02" and "S-1-PO-03" which are the names of the two subcatchments.  
 06393+ # - JFSA 2021-01-19, after adding Greenbank pond, "S-1-BDCD-3" is not existing anymore  
 06394+ R0010:CO0170----> Dtnin-ID:NHYD--- ADD HVD ...  
 06395+ CONTINUOUS\_NASHYD 1.0 01S-1-B 55.36 1.740 No\_date 29:08 26.85 .415 .000  
 06396+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06397+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06398+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06399+ [InterEventTime= 12.00] ...  
 06400+ R0010:CO0171----> Dtnin-ID:NHYD--- ADD HVD ...  
 06401+ CONTINUOUS\_NASHYD 1.0 01S-1-B 4.38 .055 No\_date 29:11 26.85 .415 .000  
 06402+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06403+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06404+ [InterEventTime= 12.00] ...  
 06405+ R0010:CO0172----> Dtnin-ID:NHYD--- ADD HVD ...  
 06406+ CONTINUOUS\_NASHYD 1.0 01S-1-B 12.84 .215 No\_date 29:11 26.85 .415 .000  
 06407+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06408+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06409+ [InterEventTime= 12.00] ...  
 06410+ R0010:CO0173----> Dtnin-ID:NHYD--- ADD HVD ...  
 06411+ CONTINUOUS\_NASHYD 1.0 01S-1-B 1.75 .029 No\_date 29:11 26.85 .415 .000  
 06412+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06413+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06414+ [InterEventTime= 12.00] ...  
 06415+ R0010:CO0174----> Dtnin-ID:NHYD--- ADD HVD ...  
 06416+ CONTINUOUS\_NASHYD 1.0 01S-1-B 4.38 .055 No\_date 29:11 26.85 .415 .000  
 06417+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06418+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06419+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06420+ # Catchment W\_CLAR  
 06421+ # - To West Clarke Drain (south of the Jock)  
 06422+ # - Tributary Area to North Branch of Barhaven South MMS  
 06423+ # - 2020-11-30 update CLARKE Tributary Drainage Area to a 121 ha based on P598(04)-11  
 06424+ # - 2020-11-30 split Clarke Drainage Area to MAJNA and ALB  
 06425+ #  
 06426+ #  
 06427+ R0010:CO0175----> Dtnin-ID:NHYD--- ADD HVD ...  
 06428+ CONTINUOUS\_NASHYD 1.0 01W.CLAR\_MJ 1.77 .229 No\_date 28:00 43.97 .680 .000  
 06429+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06430+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06431+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06432+ [iEcImp= 4.00! IaRcOper= 4.00!] ...  
 06433+ [SMIN= 31.15! SMAX= 207.66! SK= 010]  
 06434+ # 5 Years to 120 ha  
 06435+ R0010:CO0176----> Dtnin-ID:NHYD--- ADD HVD ...  
 06436+ ROUTE\_RESERVE--> 1.0 02W.CLAR\_MJ 1.77 .229 No\_date 28:00 43.97 n/a .000  
 06437+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06438+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06439+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06440+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06441+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06442+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06443+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06444+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06445+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06446+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06447+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06448+ R0010:CO0177----> Dtnin-ID:NHYD--- ADD HVD ...  
 06449+ ADD HVD ...  
 06450+ ADD HVD ...  
 06451+ SMM+ 1.0 01W.CLAR\_MJ 1.77 .229 No\_date 28:00 43.97 n/a .000  
 06452+ R0010:CO0179----> Dtnin-ID:NHYD--- ADD HVD ...  
 06453+ SAVV HYD 1.0 01W.CLAR\_MJ 1.77 .229 No\_date 28:00 43.97 n/a .000  
 06454+ frame: SNC\_CEO\_0010  
 06455+ remark:Total Flows before Station 573 on Rock River  
 06456+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 573  
 06457+ #  
 06458+ # Tributary Drainage Area to MSS Pond 2 = 241 ha  
 06459+ #  
 06460+ R0010:CO0180----> Dtnin-ID:NHYD--- ADD HVD ...  
 06461+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06462+ ROUTE\_RESERVOIR--> 1.0 01W.SCE 119.40 12.497 No\_date 28:05 47.94 n/a .000  
 06463+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06464+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06465+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06466+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06467+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06468+ R0010:CO0178----> Dtnin-ID:NHYD--- ADD HVD ...  
 06469+ ADD HVD ...  
 06470+ ADD HVD ...  
 06471+ SMM+ 1.0 01W.SCE 119.40 12.497 No\_date 28:05 47.94 n/a .000  
 06472+ R0010:CO0179----> Dtnin-ID:NHYD--- ADD HVD ...  
 06473+ SMM+ 1.0 01W.SCE 119.40 12.497 No\_date 28:05 47.94 n/a .000  
 06474+ R0010:CO0182----> Dtnin-ID:NHYD--- ADD HVD ...  
 06475+ SAVV HYD 1.0 01W.SCE 119.40 12.497 No\_date 28:05 47.94 n/a .000  
 06476+ frame: SNC\_CEO\_0010  
 06477+ remark:Total Flows before Station 573 on Rock River  
 06478+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 573  
 06479+ #  
 06480+ # JFSA 2021-02-25 add station 573 before Station 5002. Station 573 was extracted from the HEC-RAS model T:\\PROJ\\1474-1  
 06481+ # JFSA 2021-03-02 change the slope to 0.1 instead of 0.0175 to stabilize the model  
 06482+ #  
 06483+ \* [ROT: 1.00] out+ 1.0 01W.SCE 54253.88 89.884 No\_date 33:43 22.84 n/a .000  
 06484+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06485+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06486+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06487+ R0010:CO0184----> Dtnin-ID:NHYD--- ADD HVD ...  
 06488+ ADD HVD ...  
 06489+ ADD HVD ...  
 06490+ SMM+ 1.0 01W.SCE 54253.88 89.884 No\_date 33:43 22.84 n/a .000  
 06491+ R0010:CO0185----> Dtnin-ID:NHYD--- ADD HVD ...  
 06492+ SMM+ 1.0 01W.SCE 54279.34 86.671 No\_date 35:45 22.84 n/a .000  
 06493+ R0010:CO0186----> Dtnin-ID:NHYD--- ADD HVD ...  
 06494+ R0010:CO0187----> Dtnin-ID:NHYD--- ADD HVD ...  
 06495+ ADD HVD ...  
 06496+ ADD HVD ...  
 06497+ ADD HVD ...  
 06498+ ADD HVD ...  
 06499+ ADD HVD ...  
 06500+ R0010:CO0188----> Dtnin-ID:NHYD--- ADD HVD ...  
 06501+ R0010:CO0189----> Dtnin-ID:NHYD--- ADD HVD ...  
 06502+ ROUTE CHANNEL--> 1.0 02S-1-POV 54279.34 86.671 No\_date 35:45 22.84 n/a .000  
 06503+ \* [ROT: 1.00] out+ 1.0 01N.MCA 54279.34 86.671 No\_date 35:45 22.84 n/a .000  
 06504+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06505+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06506+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06507+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06508+ \* [ROT: 1.00] out+ 1.0 01N.MCD 54279.34 86.651 No\_date 35:51 22.84 n/a .000  
 06509+ [CN= 77.0! N= 245/.055/.035] ...  
 06510+ [CN= 77.0! N= 245/.055/.035] ...  
 06511+ R0010:CO0188----> Dtnin-ID:NHYD--- ADD HVD ...  
 06512+ ROUTE CHANNEL--> 1.0 02W.NCM 54279.34 86.651 No\_date 35:51 22.84 n/a .000  
 06513+ \* [ROT: 1.00] out+ 1.0 01N.MCD 54279.34 86.651 No\_date 35:51 22.84 n/a .000  
 06514+ [CN= 77.0! N= 245/.055/.035] ...  
 06515+ [CN= 77.0! N= 245/.055/.035] ...  
 06516+ [CN= 77.0! N= 245/.055/.035] ...  
 06517+ # Hydrograph from Node West Clarke to Node at Kennedy - Burnett Drain  
 06518+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 4534  
 06519+ #  
 06520+ R0010:CO0189----> Dtnin-ID:NHYD--- ADD HVD ...  
 06521+ ROUTE CHANNEL--> 1.0 02W.NMC 54279.34 86.639 No\_date 35:58 22.84 n/a .000  
 06522+ \* [ROT: 1.00] out+ 1.0 01N.MCB 54279.34 86.222 No\_date 36:19 22.84 n/a .000  
 06523+ [CN= 77.0! N= 1020/.050/.036] ...  
 06524+ [CN= 77.0! N= 1020/.050/.036] ...  
 06525+ R0010:CO0190----> Dtnin-ID:NHYD--- ADD HVD ...  
 06526+ CONTINUOUS\_STANDHYD 1.0 01E.KLAR 54118.36 89.070 No\_date 33:43 22.78 n/a .000  
 06527+ frame: SNC\_CEO\_0010  
 06528+ remark:Total Flows from Barhaven South MMS modeling  
 06529+ #  
 06530+ # Tributary Drainage Area to MSS Pond 2 = 241 ha  
 06531+ #  
 06532+ R0010:CO0180----> Dtnin-ID:NHYD--- ADD HVD ...  
 06533+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06534+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06535+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06536+ [CN= 77.0! N= 3.00! TP= .45!] ...  
 06537+ R0010:CO0181----> Dtnin-ID:NHYD--- ADD HVD ...  
 06538+ ADD HVD ...  
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07107> R0101:CG0584-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
CONTINUOUS STANDHY 1.0 01A2 25.50 2,388 No\_date 28:03 40.97 .633 .000  
07108> XMPN= 42;TIME= 52 [Previous area: Iaper 4.67:SLPP=1.00:LGP= 40:NWP= 250:SCP= .0]  
07109> [Previous area: Iaper 1.57:SLU=1.00:LGI= 566:MMI= 013:SCI= .0]  
07110> [iReCImp= 4.00: IaReCper= 4.00] [MMI= 33.81: SMAX=225.43: SK= 010]  
07111> R0101:CG0584-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
COMPUTE DUALHYD 1.0 01A2 25.50 2,388 No\_date 28:03 40.97 n/a .000  
07112> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:03 40.97 n/a .000  
07113> Minor System / 1.0 03A2-MN 25.50 1,818 No\_date 27:57 40.97 n/a .000  
07114> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07115> R0101:CG0584-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07116> COMPUTE DUALHYD 1.0 01A2 25.50 2,388 No\_date 28:03 40.97 n/a .000  
07117> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:03 40.97 n/a .000  
07118> Minor System / 1.0 03A2-MN 25.50 1,818 No\_date 27:57 40.97 n/a .000  
07119> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07120> R0101:CG0584-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07121> ADD HYD + 1.0 02TODD\_MZN 25.50 .268 No\_date 27:58 44.92 n/a .000  
07122> + 1.0 02TODD\_MJN 1.10 .016 No\_date 28:00 44.92 n/a .000  
07123> + 1.0 02TODD\_MJN 0 .01 .000 No\_date 28:00 44.92 n/a .000  
07124> + 1.0 02TODD\_ALL 3.00 .451 No\_date 28:00 45.23 n/a .000  
07125> + 1.0 02TODD\_ALL 112.93 10.943 No\_date 28:00 45.77 n/a .000  
07126> SUM= 1.0 01TODD 120.03 11.699 No\_date 28:03 44.79 n/a .000  
07127> SUM= 1.0 01TODD 120.03 11.699 No\_date 28:03 44.79 n/a .000  
07128> R0101:CG0584-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07129> COMPUTE DUALHYD 1.0 01A2 25.50 2,388 No\_date 28:03 40.97 n/a .000  
07130> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:03 40.97 n/a .000  
07131> Minor System / 1.0 03A2-MN 25.50 1,818 No\_date 27:57 40.97 n/a .000  
07132> SUM= 1.0 01TODD 120.03 11.699 No\_date 28:03 44.79 n/a .000  
07133> R0101:CG0584-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07134> # Total Pond 3 - Rating curve obtained from Heschhaven South M5S modeling  
07135> # Rating curve obtained from Heschhaven South M5S modeling  
07136> R0101:CG0584-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
ROUTE RESERVOIR 1.0 01SMN\_P0 120.03 6.151 No\_date 28:20 44.79 n/a .000  
07137> out < 1.0 01SMN\_P0 120.03 6.151 No\_date 28:20 44.79 n/a .000  
07138> overl < 1.0 01P19-OVF 05 .000 No\_date 28:00 44.92 n/a .000  
07139> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07140> R0101:CG0584-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07141> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07142> R0101:CG0584-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07143> ADD HYD 1.0 021GreenB 54717.74 86.895 No\_date 36:17 22.95 n/a .000  
07144> + 1.0 021GreenB 120.00 1.640 No\_date 28:00 44.92 n/a .000  
07145> + 1.0 021P3-OVF .000 No\_date 28:00 44.92 n/a .000  
07146> + 1.0 021TODD\_MZJ 0 .011 No\_date 28:00 44.92 n/a .000  
07147> + 1.0 021TODD\_MZJ 0 .00 .000 No\_date 28:00 44.92 n/a .000  
07148> SUM= 1.0 01SMN\_T 54837.79 87.200 No\_date 36:18 23.00 n/a .000  
07149> R0101:CG0584-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07150> SAVE HYD 1.0 01SMN\_T 54837.79 87.200 No\_date 36:16 23.00 n/a .000  
07151> fname: SN\_TO\_0010  
07152> remark:Total Flows at Todd Drain  
07153> #  
07154> # Hydrograph from Todd Drain routed to Corrigan Drain  
07155> # Rating curve obtained from Heschhaven South M5S hydrologic Model - Station 2462  
07156> #  
07157> R0101:CG0291-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07158> R0101:CG0291-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07159> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07160> [L8/n= 280. / .050 / .045] [MMI= 33.81: SMAX=225.43: SK= 010]  
07161> R0101:CG0291-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07162> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07163> R0101:CG0291-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07164> SAVE HYD 1.0 01N\_HTO 54837.79 87.112 No\_date 36:28 23.00 n/a .000  
07165> fname: SN\_TO\_0010  
07166> remark:Total Flows at Todd Drain  
07167> #  
07168> # Corrigan Drain (south of the Jock)  
07169> # Primarily Developed (medium density)  
07170> #  
07171> R0101:CG0293-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07172> R0101:CG0293-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07173> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07174> R0101:CG0293-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07175> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07176> R0101:CG0293-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07177> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07178> [iReCImp= 4.00: IaReCper= 4.00] [MMI= 33.81: SMAX=225.43: SK= 010]  
07179> R0101:CG0294-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07180> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07181> COMPUTE DUALHYD 1.0 01A1corr 2.87 2.113 No\_date 28:01 48.23 n/a .000  
07182> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:01 48.23 n/a .000  
07183> Minor System / 1.0 03A1corr-MN 1.87 1.818 No\_date 28:08 49.38 n/a .000  
07184> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07185> R0101:CG0294-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07186> COMPUTING NASHYD 1.0 01A1corr 12.47 .109 No\_date 29:11 26.85 .415 .000  
07187> [CN= 77.0 / NO 3.00 TP= 1.0] [MM= 63.11: SMAX=207.56: SK= 010]  
07188> [InterEventTime= 12.00] [MM= 63.11: SMAX=207.56: SK= 010]  
07189> R0101:CG0294-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07190> [InterEventTime= 12.00] [MM= 63.11: SMAX=207.56: SK= 010]  
07191> COMPUTE DUALHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07192> [XMPN= 42;TIME= 52] [MMI= 33.81: SMAX=225.43: SK= 010]  
07193> [L8/n= 2 CN= 75.0] [MMI= 33.81: SMAX=225.43: SK= 010]  
07194> [iReCImp= 4.00: IaReCper= 4.00] [MMI= 33.81: SMAX=225.43: SK= 010]  
07195> [iReCImp= 4.00: IaReCper= 4.00] [MMI= 33.81: SMAX=225.43: SK= 010]  
07196> R0101:CG0294-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07197> COMPUTING NASHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07198> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:02 40.97 n/a .000  
07199> Minor System / 1.0 03A1corr-MN 1.87 1.818 No\_date 28:08 49.38 n/a .000  
07200> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07201> R0101:CG0294-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07202> COMPUTING DUALHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07203> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:02 40.97 n/a .000  
07204> Minor System / 1.0 03A1corr-MN 1.87 1.818 No\_date 28:08 49.38 n/a .000  
07205> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07206> R0101:CG0294-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07207> COMPUTING DUALHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07208> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:02 40.97 n/a .000  
07209> Minor System / 1.0 03A1corr-MN 1.87 1.818 No\_date 28:08 49.38 n/a .000  
07210> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07211> R0101:CG0294-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07212> COMPUTING DUALHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07213> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:02 40.97 n/a .000  
07214> Minor System / 1.0 03A1corr-MN 1.87 1.818 No\_date 28:08 49.38 n/a .000  
07215> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07216> R0101:CG0300-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07217> COMPUTE DUALHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07218> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:02 40.97 n/a .000  
07219> Minor System / 1.0 03A1corr-MN 1.87 1.818 No\_date 28:08 49.38 n/a .000  
07220> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07221> R0101:CG0301-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07222> ADD HYD + 1.0 021A1-MN 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07223> + 1.0 021corr-MN 0 .000 No\_date 0:00 0/n/a .000  
07224> + 1.0 021corr-MN 0 .00 .000 No\_date 0:00 0/n/a .000  
07225> + 1.0 021corr-MN 0 .00 .000 No\_date 0:00 0/n/a .000  
07226> + 1.0 021corr-MN 1.87 1.818 No\_date 28:08 49.38 n/a .000  
07227> + 1.0 021B1 2.77 .072 No\_date 28:09 16.64 n/a .000  
07228> + 1.0 021A2-MN 2.77 .072 No\_date 28:09 16.64 n/a .000  
07229> + 1.0 021A2-MN 1.87 1.818 No\_date 28:08 49.38 n/a .000  
07230> SUM= 1.0 01SMN\_T 73.63 5.480 No\_date 28:03 39.39 n/a .000  
07231> R0101:CG0301-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07232> SAVE HYD 1.0 01MHN101 48.13 1.734 No\_date 28:02 38.56 n/a .000  
07233> fname: SN\_TO\_0010  
07234> R0101:CG0303-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07235> COMPUTE DUALHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07236> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07237> [L8/n= 204.000 Dmns= 1.098] [MMI= 33.81: SMAX=225.43: SK= 010]  
07238> R0101:CG0303-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07239> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07240> R0101:CG0304-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07241> COMPUTE DUALHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07242> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:02 40.97 n/a .000  
07243> Minor System / 1.0 03A1corr-MN 1.87 1.818 No\_date 28:08 49.38 n/a .000  
07244> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07245> R0101:CG0304-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07246> COMPUTE DUALHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07247> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:02 40.97 n/a .000  
07248> Minor System / 1.0 03A1corr-MN 1.87 1.818 No\_date 28:08 49.38 n/a .000  
07249> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07250> R0101:CG0304-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07251> COMPUTE DUALHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07252> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:02 40.97 n/a .000  
07253> Minor System / 1.0 03A1corr-MN 1.87 1.818 No\_date 28:08 49.38 n/a .000  
07254> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07255> R0101:CG0304-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07256> COMPUTE DUALHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07257> ADD HYD 1.0 02A4-MN 0 .00 .000 No\_date 0:00 0/n/a .000  
07258> + 1.0 021A1-MN 1.87 1.818 No\_date 28:02 40.97 n/a .000  
07259> SUM= 1.0 01A1corr 1.87 1.818 No\_date 28:01 51.11 n/a .000  
07260> R0101:CG0305-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07261> COMPUTE DUALHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07262> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:02 40.97 n/a .000  
07263> Minor System / 1.0 03A1corr-MN 1.87 1.818 No\_date 28:08 49.38 n/a .000  
07264> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07265> R0101:CG0305-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07266> ROUTE PIPE --> 1.0 021MHN102 73.63 5.480 No\_date 28:03 39.39 n/a .000  
07267> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07268> [L8/n= 204.000 Dmns= 1.098] [MMI= 33.81: SMAX=225.43: SK= 010]  
07269> R0101:CG0305-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07270> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07271> R0101:CG0310-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07272> COMPUTE DUALHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07273> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:02 40.97 n/a .000  
07274> Minor System / 1.0 03A1corr-MN 1.87 1.818 No\_date 28:08 49.38 n/a .000  
07275> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07276> R0101:CG0310-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07277> COMPUTING DUALHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07278> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:02 40.97 n/a .000  
07279> Minor System / 1.0 03A1corr-MN 1.87 1.818 No\_date 28:08 49.38 n/a .000  
07280> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07281> R0101:CG0310-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07282> COMPUTE DUALHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07283> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:02 40.97 n/a .000  
07284> Minor System / 1.0 03A1corr-MN 1.87 1.818 No\_date 28:08 49.38 n/a .000  
07285> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07286> R0101:CG0310-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07287> COMPUTE DUALHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07288> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:02 40.97 n/a .000  
07289> Minor System / 1.0 03A1corr-MN 1.87 1.818 No\_date 28:08 49.38 n/a .000  
07290> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07291> R0101:CG0310-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07292> COMPUTE DUALHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07293> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:02 40.97 n/a .000  
07294> Minor System / 1.0 03A1corr-MN 1.87 1.818 No\_date 28:08 49.38 n/a .000  
07295> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07296> R0101:CG0311-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07297> COMPUTE DUALHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07298> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:02 40.97 n/a .000  
07299> Minor System / 1.0 03A1corr-MN 1.87 1.818 No\_date 28:08 49.38 n/a .000  
07300> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07301> R0101:CG0311-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07302> COMPUTE DUALHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07303> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:02 40.97 n/a .000  
07304> Minor System / 1.0 03A1corr-MN 1.87 1.818 No\_date 28:08 49.38 n/a .000  
07305> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07306> R0101:CG0311-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07307> COMPUTE DUALHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07308> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:02 40.97 n/a .000  
07309> Minor System / 1.0 03A1corr-MN 1.87 1.818 No\_date 28:08 49.38 n/a .000  
07310> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07311> R0101:CG0311-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07312> COMPUTE DUALHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07313> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:02 40.97 n/a .000  
07314> Minor System / 1.0 03A1corr-MN 1.87 1.818 No\_date 28:08 49.38 n/a .000  
07315> [MMjySto=.8936E+03 TotCovYel=.0000E+00 N-Dwf= 0. TotDurOvf=.0hrs] [SK= 000]  
07316> R0101:CG0311-----Dtnin-ID:NHYD-----AReAh-aQPEAKcms-TpeakData\_hh:mm:--RvNm-R.C.--DWFcms  
07317> COMPUTE DUALHYD 1.0 01A1corr 15.75 1.640 No\_date 28:02 40.97 n/a .000  
07318> Major System / 1.0 02A4-MN 0 .00 .000 No\_date 28:02 40.97 n/a .000<br

[JFSAinc.]

07855 # Line-0002 # 254923  
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07856 # CALIBRATION OF SUMMER MODEL PARAMETERS  
07857 # USING CONTINUOUS SIMULATIONS  
07858 # Rainfall data from JRA rainfall installed at site + other gauges by the City  
07859 # Data collected from July 1 to July 14, 2003  
07860 # 2020-11-30 change TMSTO in COMPUTE DAILYRD (TMSTO = 0.1 instead of 0.0001)  
07861 # 2020-12-01 removed some values  
07862 # 2020-12-01 removed some values  
07863 # 2021-01-01 removed some values  
07864 # 2021-02-19 Change the slope for ROUTE CHANNEL Station 2462 ([NHDout=“N\_TD”], [NHDin=“SN\_TO”]) from 0.033 % (as per S  
07865 # 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 ([NHDout=“N\_WC”], [NHDin=“SN\_CK”]) from 0.01 % (as per S  
07866 # 2021-02-19 Change the slope for ROUTE CHANNEL Station 5138 ([NHDout=“N\_WC”], [NHDin=“SN\_CE”]) from 0.01 % (as per S  
07867 # RO225:C00022-----  
07868 # File name = storm.001  
07869 # Comment = Pluie SCS de 24 hres 1:25 ans pour Ottawa CDA  
07870 # [CN= 75.01 : N: 3.00 : Tp: 8.00] [Lm: 24.00 : Ptot: 74.39]  
07872 # RO225:C0003-----  
07873 # MODIFY STORM  
07874 # [CN= 75.01 : N: 3.00 : Tp: 8.00] [Lm: 24.00 : Ptot: 74.39]  
07875 # [Sdt=10.00:Sourc= 40.00:Ptot= 74.39]  
07876 # RO225:C0004-----  
07877 # File name = T:\\PROJ\\1474-16\\Design\\20201026-QuantityControlAnalysis\\SWMMH00\\SWM-Model\\updated3\\CitiGate.DEF  
07878 # Horton's infiltration equation parameters:  
07879 # Parameters for PREVIOUS surfaces in STANDHYD:  
07880 # FileTitle= “SWMMH00”  
07881 # THE FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDHYD COM  
07882 # Horton's infiltration equation parameters:  
07883 # Parameters for PREVIOUS surfaces in STANDHYD:  
07884 # FileTitle= “SWMMH00”  
07885 # [Taper= 4.67 mm] [LGW=50.00 mm] [MND= .250]  
07886 # [DMD=0.0000000000000000] [DWD=0.0000000000000000]  
07887 # [TAImp= 1.57 mm] [CLW= 1.50] [MWH= .013]  
07888 # Parameters used in NASHYD:  
07889 # [APimax= 60.000 : APIday= 8500 : APIkt= 9988]  
07890 # Average monthly Pan Evaporation data in (mm):  
07891 # JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC  
07892 # [CN= 60.00 : N: 3.00 : Tp: 3.61] [Lm: 24.00 : Ptot: 74.39]  
07893 # Average monthly Potential Evapotranspiration in (mm):  
07894 # JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC  
07895 # [CN= 60.00 : N: 3.00 : Tp: 3.61] [Lm: 24.00 : Ptot: 74.39]  
07896 # RO225:C0005-----  
07897 # COMPUTE API  
07898 # [APimax= 60.000 : APIday= 8500 : APIkt= 9988]  
07899 # File name = storm.001  
07900 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
07901 # of 1.32  
07902 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
07903 # of 1.32  
07904 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 3680.00 15.500 No\_date 36:57 23.80 3447 .000  
07905 # [CN= 64.01 : N: 3.00 : Tp: 7.13]  
07906 # [TaEBC= 4.00 : SMIN= 57.05 : SMAX=380.32 : SKw= .010]  
07907 # [InterEventTime= 12.00]  
07908 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
07909 # of 1.32  
07910 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 3680.00 15.500 No\_date 36:57 23.80 3447 .000  
07911 # [CN= 64.01 : N: 3.00 : Tp: 7.13]  
07912 # [TaEBC= 4.00 : SMIN= 57.05 : SMAX=380.32 : SKw= .010]  
07913 # [InterEventTime= 12.00]  
07914 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
07915 # of 1.32  
07916 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 3680.00 15.500 No\_date 36:57 23.80 3447 .000  
07917 # [CN= 64.01 : N: 3.00 : Tp: 3.91]  
07918 # [TaEBC= 4.00 : SMIN= 57.05 : SMAX=264.99 : SKw= .010]  
07919 # [InterEventTime= 12.00]  
07920 # RO225:C0008-----  
07921 # CONTINUOUS NASHYD: 1.0 01:JR\_GWM 3074.00 7.521 No\_date 39:59 20.65 278 .000  
07922 # [CN= 64.01 : N: 3.00 : Tp: 3.91]  
07923 # [TaEBC= 4.00 : SMIN= 58.24 : SMAX=554.96 : SKw= .010]  
07924 # [InterEventTime= 12.00]  
07925 # RO225:C0009-----  
07926 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 1781.00 14.166 No\_date 32:40 31.90 423 .000  
07927 # [CN= 72.0 : N: 3.00 : Tp: 3.91]  
07928 # [TaEBC= 4.00 : SMIN= 58.24 : SMAX=264.99 : SKw= .010]  
07929 # [InterEventTime= 12.00]  
07930 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
07931 # of 1.32  
07932 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 1781.00 14.166 No\_date 32:40 31.90 423 .000  
07933 # [CN= 72.0 : N: 3.00 : Tp: 3.91]  
07934 # [TaEBC= 4.00 : SMIN= 58.24 : SMAX=264.99 : SKw= .010]  
07935 # [InterEventTime= 12.00]  
07936 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
07937 # of 1.32  
07938 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 1917.00 10.351 No\_date 34:27 27.01 .363 .000  
07939 # [CN= 64.01 : N: 3.00 : Tp: 3.91]  
07940 # [TaEBC= 4.00 : SMIN= 52.62 : SMAX=350.79 : SKw= .010]  
07941 # [InterEventTime= 12.00]  
07942 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
07943 # of 1.32  
07944 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 1917.00 10.351 No\_date 34:27 27.01 .363 .000  
07945 # [CN= 64.01 : N: 3.00 : Tp: 3.91]  
07946 # [TaEBC= 4.00 : SMIN= 52.62 : SMAX=350.79 : SKw= .010]  
07947 # [InterEventTime= 12.00]  
07948 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
07949 # of 1.32  
07950 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 1917.00 10.351 No\_date 34:27 27.01 .363 .000  
07951 # [CN= 64.01 : N: 3.00 : Tp: 3.91]  
07952 # [TaEBC= 4.00 : SMIN= 52.62 : SMAX=350.79 : SKw= .010]  
07953 # [InterEventTime= 12.00]  
07954 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
07955 # of 1.32  
07956 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 1917.00 10.351 No\_date 34:27 27.01 .363 .000  
07957 # [CN= 64.01 : N: 3.00 : Tp: 3.91]  
07958 # [TaEBC= 4.00 : SMIN= 52.62 : SMAX=350.79 : SKw= .010]  
07959 # [InterEventTime= 12.00]  
07960 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
07961 # of 1.68  
07962 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 1132.00 11.792 No\_date 30:54 30.18 .406 .000  
07963 # [CN= 70.70 : N: 3.00 : Tp: 2.51]  
07964 # [TaEBC= 4.00 : SMIN= 43.07 : SMAX=287.10 : SKw= .010]  
07965 # [InterEventTime= 12.00]  
07966 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
07967 # of 1.68  
07968 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 1132.00 11.792 No\_date 30:54 30.18 .406 .000  
07969 # [CN= 70.70 : N: 3.00 : Tp: 2.51]  
07970 # [TaEBC= 4.00 : SMIN= 43.07 : SMAX=287.10 : SKw= .010]  
07971 # [InterEventTime= 12.00]  
07972 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
07973 # of 1.68  
07974 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 1132.00 11.792 No\_date 30:54 30.18 .406 .000  
07975 # [CN= 70.70 : N: 3.00 : Tp: 2.51]  
07976 # [TaEBC= 4.00 : SMIN= 43.07 : SMAX=287.10 : SKw= .010]  
07977 # [InterEventTime= 12.00]  
07978 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
07979 # of 1.68  
07980 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 3884.00 15.333 No\_date 38:34 27.01 .363 .000  
07981 # [CN= 66.01 : N: 3.00 : Tp: 8.42]  
07982 # [TaEBC= 4.00 : SMIN= 52.62 : SMAX=350.79 : SKw= .010]  
07983 # [InterEventTime= 12.00]  
07984 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
07985 # of 1.65  
07986 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 3884.00 15.333 No\_date 38:34 27.01 .363 .000  
07987 # [CN= 66.01 : N: 3.00 : Tp: 8.42]  
07988 # [TaEBC= 4.00 : SMIN= 52.62 : SMAX=350.79 : SKw= .010]  
07989 # [InterEventTime= 12.00]  
07990 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
07991 # of 1.68  
07992 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 3884.00 15.333 No\_date 38:34 27.01 .363 .000  
07993 # [CN= 66.01 : N: 3.00 : Tp: 8.42]  
07994 # [TaEBC= 4.00 : SMIN= 52.62 : SMAX=350.79 : SKw= .010]  
07995 # [InterEventTime= 12.00]  
07996 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
07997 # of 1.68  
07998 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 3884.00 15.333 No\_date 38:34 27.01 .363 .000  
07999 # [CN= 66.01 : N: 3.00 : Tp: 8.42]  
08000 # [TaEBC= 4.00 : SMIN= 52.62 : SMAX=350.79 : SKw= .010]  
08001 # [InterEventTime= 12.00]  
08002 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
08003 # of 1.67  
08004 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 3884.00 15.333 No\_date 38:34 27.01 .363 .000  
08005 # [CN= 66.01 : N: 3.00 : Tp: 8.42]  
08006 # [TaEBC= 4.00 : SMIN= 52.62 : SMAX=350.79 : SKw= .010]  
08007 # [InterEventTime= 12.00]  
08008 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
08009 # of 1.67  
08010 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 1332.00 7.882 No\_date 35:14 31.90 423 .000  
08011 # [CN= 72.0 : N: 3.00 : Tp: 5.91]  
08012 # [TaEBC= 4.00 : SMIN= 52.62 : SMAX=264.99 : SKw= .010]  
08013 # [InterEventTime= 12.00]  
08014 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 165.00 1.076 No\_date 33:03 27.61 .371 .000  
08015 # [CN= 66.01 : N: 3.00 : Tp: 6.18]  
08016 # [TaEBC= 4.00 : SMIN= 50.55 : SMAX=336.97 : SKw= .010]  
08017 # [InterEventTime= 12.00]  
08018 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
08019 # of 1.67  
08020 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 165.00 1.076 No\_date 33:03 27.61 .371 .000  
08021 # [CN= 66.01 : N: 3.00 : Tp: 6.18]  
08022 # [TaEBC= 4.00 : SMIN= 50.55 : SMAX=336.97 : SKw= .010]  
08023 # [InterEventTime= 12.00]  
08024 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
08025 # of 1.67  
08026 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 224.00 6.892 No\_date 28:45 39.36 .479 .000  
08027 # [CN= 77.01 : N: 3.00 : Tp: 7.51]  
08028 # [TaEBC= 4.00 : SMIN= 31.15 : SMAX=207.66 : SKw= .010]  
08029 # [InterEventTime= 12.00]  
08030 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
08031 # of 1.67  
08032 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 224.00 6.892 No\_date 28:45 39.36 .479 .000  
08033 # [CN= 77.01 : N: 3.00 : Tp: 7.51]  
08034 # [TaEBC= 4.00 : SMIN= 31.15 : SMAX=207.66 : SKw= .010]  
08035 # [InterEventTime= 12.00]  
08036 # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
08037 # of 1.67  
08038 # CONTINUOUS NASHYD: 1.0 01:JR\_NASH 585.00 10.942 No\_date 29:56 39.36 .529 .000  
08039 # [CN= 75.01 : N: 3.00 : Tp: 8.00]  
08040 # [TaEBC= 4.00 : SMIN= 31.15 : SMAX=225.43 : SKw= .010]  
08041 # [InterEventTime= 12.00]  
08042 # [CN= 81.0 : N: 3.00 : Tp: 1.75]  
08043 # [TaEBC= 4.00 : SMIN= 21.5 : SMAX=168.09 : SKw= .010]  
08044 # [InterEventTime= 12.00]  
08045 # [CN= 81.0 : N: 3.00 : Tp: 1.75]  
08046 # [TaEBC= 4.00 : SMIN= 21.5 : SMAX=175.60 : SKw= .010]  
08047 # [InterEventTime= 12.00]  
08048 # [CN= 81.0 : N: 3.00 : Tp: 1.75]  
08049 # [TaEBC= 4.00 : SMIN= 21.5 : SMAX=207.66 : SKw= .010]  
08050 # CONTINUOUS NASHYD: 1.0 01:SM\_2W  
08051 # [CN= 81.0 : N: 3.00 : Tp: 1.75]  
08052 # [TaEBC= 4.00 : SMIN= 21.5 : SMAX=168.09 : SKw= .010]  
08053 # [InterEventTime= 12.00]  
08054 # [CN= 81.0 : N: 3.00 : Tp: 1.75]  
08055 # [TaEBC= 4.00 : SMIN= 21.5 : SMAX=207.66 : SKw= .010]  
08056 # CONTINUOUS NASHYD: 1.0 01:SM\_2W  
08057 # [CN= 81.0 : N: 3.00 : Tp: 3.25]  
08058 # [TaEBC= 4.00 : SMIN= 21.5 : SMAX=168.09 : SKw= .010]  
08059 # [InterEventTime= 12.00]  
08060 # [CN= 81.0 : N: 3.00 : Tp: 3.25]  
08061 # [TaEBC= 4.00 : SMIN= 21.5 : SMAX=216.39 : SKw= .010]  
08062 # [CN= 76.70 : N: 3.00 : Tp: 3.03]  
08063 # [TaEBC= 4.00 : SMIN= 21.5 : SMAX=216.39 : SKw= .010]  
08064 # [InterEventTime= 12.00]  
08065 # Starting with the addition of Jock River Headwater and Subwatershed 13  
08066 # Starting with the addition of Jock River Headwater and Subwatershed 13  
08067 # Starting with the addition of Jock River Headwater and Subwatershed 13  
08068 # Starting with the addition of Jock River Headwater and Subwatershed 13  
08069 # Starting with the addition of Jock River Headwater and Subwatershed 13  
08070 # RO225:C00030-----  
08071 # ADD HYD  
08072 # ADD HYD  
08073 # ADD HYD  
08074 # ADD HYD  
08075 # Sum of hydrographs from Node 13 routed to Node 12  
08076 # Use n=0.04 for summer conditions and n=0.025 for spring conditions  
08077 # Use n=0.04 for summer conditions and n=0.025 for spring conditions  
08078 # Use n=0.04 for summer conditions and n=0.025 for spring conditions  
08079 # RO225:C00031-----  
08080 # ROUTE CHANNEL > 1.0 02:SR\_N13  
08081 # [RDt= 1.00 : out<- 1.0 01:SM13  
08082 # [RDt= 1.00 : out<- 1.0 01:SM13  
08083 # [RDt= 1.00 : out<- 1.0 01:SM13  
08084 # [RDt= 1.00 : out<- 1.0 01:SM13  
08085 # [RDt= 1.00 : out<- 1.0 01:SM13  
08086 # [RDt= 1.00 : out<- 1.0 01:SM13  
08087 # [RDt= 1.00 : out<- 1.0 01:SM13  
08088 # [RDt= 1.00 : out<- 1.0 01:SM13  
08089 # [RDt= 1.00 : out<- 1.0 01:SM13  
08090 # [RDt= 1.00 : out<- 1.0 01:SM13  
08091 # [RDt= 1.00 : out<- 1.0 01:SM13  
08092 # Insertion of a reservoir to simulate the effects of the Goodwood Marsh  
08093 # RO225:C00033-----  
08094 # ADD HYD  
08095 # ROUTE RESERVOIR > 1.0 02:SM13  
08096 # [RDt= 1.00 : out<- 1.0 01:SM13  
08097 # [RDt= 1.00 : out<- 1.0 01:SM13  
08098 # [RDt= 1.00 : out<- 1.0 01:SM13  
08099 # [RDt= 1.00 : out<- 1.0 01:SM13  
08100 # [RDt= 1.00 : out<- 1.0 01:SM13  
08101 # [RDt= 1.00 : out<- 1.0 01:SM13  
08102 # [RDt= 1.00 : out<- 1.0 01:SM13  
08103 # [RDt= 1.00 : out<- 1.0 01:SM13  
08104 # [RDt= 1.00 : out<- 1.0 01:SM13  
08105 # [RDt= 1.00 : out<- 1.0 01:SM13  
08106 # [RDt= 1.00 : out<- 1.0 01:SM13  
08107 # [RDt= 1.00 : out<- 1.0 01:SM13  
08108 # [RDt= 1.00 : out<- 1.0 01:SM13  
08109 # [RDt= 1.00 : out<- 1.0 01:SM13  
08110 # [RDt= 1.00 : out<- 1.0 01:SM13  
08111 # [RDt= 1.00 : out<- 1.0 01:SM13  
08112 # Addition of Subwatershed Jock River at Goodwood Marsh to Node 12  
08113 # Addition of Subwatershed Jock River at Ashtons to Node 12  
08114 # RO225:C00036-----  
08115 # ADD HYD  
08116 # ADD HYD  
08117 # ADD HYD  
08118 # ADD HYD  
08119 # ADD HYD  
08120 # ADD HYD  
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08219 # ADD HYD  
08220 # ADD HYD  
08221 # ADD HYD  
08222 # ADD HYD  
08223 # Storage area and volume were estimated from available topo maps.  
08224 # Release rate from fan was assumed to be controlled by the downstream river cross-section and fan width. It was assumed that for up to 20% of the water, the main channel of the river provided the storage. Above 20% of the water, the wetland starts to significantly store water.  
08225 # The depth, the wetland starts to significantly store water.

08229+ R025:00051-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08230+ ROUTE CHANNEL >> 1.0 02\$S\_NP 38743.00 86.331 No\_date 44:08 26.55 n/a .000  
 08231+ [ROUTE 1.001 out-> 1.0 01\$RES\_NP 38743.00 42.032 No\_date 60:05 26.55 n/a .000  
 08232+ [MscdUsed..3671E-03 m3] .000  
 08233+ R025:00052-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08234+ SAVE HYD .000  
 08235+ name :ResRef  
 08236+ remark:outflow of Richmond Fen  
 08237+ #  
 08238+ # Sum of hydrographs from Node 7 routed to Node 6  
 08239+ # Section 5  
 08240+ #  
 08241+ R025:00053-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08242+ ROUTE CHANNEL >> 1.0 02\$S\_NP 38743.00 42.032 No\_date 60:05 26.55 n/a .000  
 08243+ [ROUTE 1.001 out-> 1.0 01\$RES\_NP 38743.00 41.826 No\_date 61:26 26.55 n/a .000  
 08244+ [L/S/n .3056 / .082 /.025] .000  
 08245+ [Vmax.. .514\*Imax..1.120] .000  
 08246+ #  
 08247+ # Addition of Subwatershed 6 and Van Gaal Drain to Node 6  
 08248+ #  
 08249+ R025:00054-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08250+ ADD HYD 1.0 02\$N 38743.00 41.826 No\_date 61:26 26.55 n/a .000  
 08251+ + 1.0 02\$W\_52 22.04 6.882 No\_date 28:45 35.66 n/a .000  
 08252+ 1.0 02\$V\_02\_Dr 1332.00 7.892 No\_date 35:14 31.50 n/a .000  
 08253+ SUM: 1.0 01\$S\_N 40240.01 41.832 No\_date 61:26 26.72 n/a .000  
 08254+ #  
 08255+ # Sum of hydrographs from Node 6 routed to Node 5  
 08256+ # Section 6  
 08257+ #  
 08258+ R025:00055-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08259+ ROUTE CHANNEL >> 1.0 02\$S\_N 40240.01 41.832 No\_date 61:20 26.72 n/a .000  
 08260+ [ROUTE 1.001 out-> 1.0 01\$RES\_NP 40240.01 41.717 No\_date 62:14 26.72 n/a .000  
 08261+ [L/S/n .1852 / .054 /.038] .000  
 08262+ [Vmax.. .444\*Imax..1.222] .000  
 08263+ #  
 08264+ # Addition of Subwatershed 5 and Flowing Creek to Node 5  
 08265+ #  
 08266+ R025:00056-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08267+ ADD HYD 1.0 02\$N 40240.01 41.717 No\_date 62:14 26.72 n/a .000  
 08268+ + 1.0 02\$W\_52 22.04 6.882 No\_date 28:45 35.66 n/a .000  
 08269+ 1.0 02\$V\_02\_Dr 4340.00 10.248 No\_date 31:45 33.84 n/a .000  
 08270+ SUM: 1.0 01\$S\_N 40549.01 62.634 No\_date 34:27 27.43 n/a .000  
 08271+ #  
 08272+ # Sum of hydrographs from Node 5 routed to Node 4  
 08273+ # Section 7  
 08274+ #  
 08275+ R025:00057-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08276+ ROUTE CHANNEL >> 1.0 02\$S\_N 45409.01 62.634 No\_date 34:27 27.43 n/a .000  
 08277+ [ROUTE 1.001 out-> 1.0 01\$RES\_NP 45409.01 62.487 No\_date 34:43 27.43 n/a .000  
 08278+ [L/S/n .044 / .044 /.038] .000  
 08279+ [Vmax.. .511\*Imax..1.222] .000  
 08280+ #  
 08281+ # Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A  
 08282+ #  
 08283+ R025:00058-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08284+ ADD HYD 1.0 02\$N 45409.01 62.487 No\_date 34:43 27.43 n/a .000  
 08285+ + 1.0 02\$W\_52 20.00 .798 No\_date 28:35 35.36 n/a .000  
 08286+ 1.0 02\$V\_02\_Dr 1412.00 1.480 No\_date 31:45 33.84 n/a .000  
 08287+ SUM: 1.0 01\$S\_N 46844.01 69.394 No\_date 35:01 27.84 n/a .000  
 08288+ #  
 08289+ # Sum of hydrographs from Node 5A routed to Node 4  
 08290+ # Section 8  
 08291+ #  
 08292+ R025:00059-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08293+ ROUTE CHANNEL >> 1.0 02\$S\_N 46841.01 69.334 No\_date 35:01 27.64 n/a .000  
 08294+ [ROUTE 1.001 out-> 1.0 01\$RES\_NP 46841.01 66.496 No\_date 36:27 27.64 n/a .000  
 08295+ [L/S/n .044 / .044 /.038] .000  
 08296+ [Vmax.. .840\*Imax..3.530] .000  
 08297+ #  
 08298+ # Addition of Subwatershed 4 and Leamy Creek to Node 4  
 08299+ #  
 08300+ R025:00060-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08301+ ADD HYD 1.0 02\$N 46841.01 66.496 No\_date 36:27 27.64 n/a .000  
 08302+ + 1.0 02\$W\_52 58.00 10.942 No\_date 29:56 39.36 n/a .000  
 08303+ 1.0 02\$V\_02\_Dr 1202.00 14.476 No\_date 30:46 38.60 n/a .000  
 08304+ SUM: 1.0 01\$S\_N 52483.00 106.109 No\_date 33:07 28.64 n/a .000  
 08305+ SAVE HYD 1.0 01\$S\_N 52483.00 106.109 No\_date 33:07 28.64 n/a .000  
 08306+ #  
 08307+ #> S\_N4 0025  
 08308+ remark:flow at S\_N4  
 08309+ #  
 08310+ # Sum of hydrographs from Node 4 routed to Node 2  
 08311+ # Section 9  
 08312+ #  
 08313+ R025:00062-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08314+ ROUTE CHANNEL >> 1.0 02\$S\_N 48447.00 73.819 No\_date 35:41 28.02 n/a .000  
 08315+ [ROUTE 1.001 out-> 1.0 01\$RES\_NP 48447.00 73.485 No\_date 35:42 28.02 n/a .000  
 08316+ [L/S/n .1647 / .050 /.050] .000  
 08317+ [Vmax.. .754\*Imax..3.570] .000  
 08318+ #  
 08319+ # Addition of Subwatershed 2 with Monchan Drain and Smith Drain to Node 2  
 08320+ #  
 08321+ R025:00063-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08322+ ADD HYD 1.0 02\$N 48447.00 73.485 No\_date 35:42 28.02 n/a .000  
 08323+ + 1.0 02\$W\_52 177.00 5.438 No\_date 28:45 35.66 n/a .000  
 08324+ 1.0 02\$V\_02\_Dr 118.00 1.229 No\_date 31:45 39.55 n/a .000  
 08325+ SUM: 1.0 01\$S\_N 53420.00 106.109 No\_date 33:07 28.64 n/a .000  
 08326+ SAVE HYD 1.0 01\$S\_N 53420.00 106.109 No\_date 33:07 28.64 n/a .000  
 08327+ #  
 08328+ #> S\_N2 0025  
 08329+ remark:flow at S\_N2 Jock River Gauge at Moodie Dr.  
 08330+ #  
 08331+ # Sum of hydrographs from Node 2 routed to Node 1  
 08332+ # Section 10  
 08333+ #  
 08334+ #  
 08335+ # Hydrograph from Node 2 routed to Node 1  
 08336+ #> S\_N2 0025  
 08337+ # Channel X-Section obtained from Rvca Hydraulic Model - Station 9025  
 08338+ #  
 08339+ R025:00065-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08340+ ROUTE CHANNEL >> 1.0 02\$S\_N 52483.00 106.109 No\_date 33:07 28.64 n/a .000  
 08341+ [ROUTE 1.001 out-> 1.0 01\$RES\_NP 52483.00 103.294 No\_date 34:03 28.64 n/a .000  
 08342+ [L/S/n .2327 / .050 /.050] .000  
 08343+ [Vmax.. .754\*Imax..3.570] .000  
 08344+ #  
 08345+ # Catchment SW\_1a  
 08346+ # Portion of Rvca catchment SW\_1 outside of Reach 1 subwatershed  
 08347+ #> S\_N2 0025  
 08348+ #  
 08349+ #\*\*\*\*\*  
 08350+ R025:00066-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08351+ CONTINUOUS\_NASHYD 1.0 01\$S\_N 430.00 1.012\*10^4 No\_date 29:07 34.14 .4599 .000  
 08352+ [TaREC 4.001 SMIN..19.75\* SMAX..264.99 / SKA ..010] .000  
 08353+ [ROUTE 1.001 out-> 1.0 01\$RES\_NP 430.00 1.012\*10^4 No\_date 29:07 34.14 .4599 .000  
 08354+ [L/S/n .1647 / .050 /.050] .000  
 08355+ R025:00067-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08356+ CONTINUOUS\_NASHYD 1.0 01\$S\_N 44.93 1.029 No\_date 29:07 34.14 .4599 .000  
 08357+ [TaREC 4.001 SMIN..31.15\* SMAX..207.66 / SKA ..010] .000  
 08358+ [ROUTE 1.001 out-> 1.0 01\$RES\_NP 44.93 1.029 No\_date 29:07 34.14 .4599 .000  
 08359+ [L/S/n .71 / .050 /.050] .000  
 08360+ #  
 08361+ R025:00068-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08362+ ADD HYD 1.0 02\$N 45248.00 103.294 No\_date 34:03 28.64 n/a .000  
 08363+ + 1.0 02\$W\_52 334.00 5.524 No\_date 31:16 39.13 n/a .000  
 08364+ 1.0 02\$V\_02\_Dr 44.43 1.029 No\_date 32:16 39.13 n/a .000  
 08365+ SUM: 1.0 01\$S\_N 53064.36 107.224 No\_date 33:26 28.66 n/a .000  
 08366+ SAVE HYD 1.0 01\$S\_N 53064.36 107.224 No\_date 33:26 28.66 n/a .000  
 08367+ #  
 08368+ #> S\_N14 0025  
 08369+ #  
 08370+ # Hydrograph from Node 6 routed to Node at Okeefe drain  
 08371+ # Channel X-Section obtained from Rvca Hydraulic Model - Station 7245  
 08372+ #  
 08373+ R025:00070-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08374+ ROUTE CHANNEL >> 1.0 02\$S\_N 53064.36 107.224 No\_date 33:26 28.66 n/a .000  
 08375+ [ROUTE 1.001 out-> 1.0 01\$RES\_NP 53064.36 107.100 No\_date 33:50 28.66 n/a .000  
 08376+ [L/S/n .497 / .302 /.055] .000  
 08377+ #  
 08378+ # Catchment OKEFE  
 08379+ #> S\_N2 0025 (north of the Jock)  
 08380+ # Developed with assumed 43% imp.  
 08381+ #> S\_N2 0025 (north of the Jock)  
 08382+ # 2020-12-01 add Okeefe model (Area 513.02 HA instead of current Okeefe Area 513.02 HA) for the parameter smothing model (clt1.Gage 2014).  
 08383+ #> S\_N2 0025 (north of the Jock)  
 08384+ #\*\*\*\*\*  
 08385+ R025:00071-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08386+ [CN ..57.01 N ..3.00 Tp ..90] .000  
 08387+ [TaREC 4.001 SMIN..44.50\* SMAX..340.01 / SKA ..010] .000  
 08388+ [ROUTE 1.001 out-> 1.0 01\$RES\_NP 44.50 340.01 No\_date 29:07 34.14 .4599 .000  
 08389+ [L/S/n .2327 / .050 /.050] .000  
 08390+ R025:00072-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08391+ ROUTE CHANNEL >> 1.0 02\$O\_10 63.72 .937 No\_date 28:58 22.21 n/a .000  
 08392+ [ROUTE 1.001 out-> 1.0 01\$RES\_NP 63.72 .877 No\_date 29:15 22.21 n/a .000  
 08393+ [L/S/n .960 / .630 /.043] .000  
 08394+ [Vmax.. .829\*Imax..3.98] .000  
 08395+ #  
 08396+ R025:00073-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08397+ CONTINUOUS\_NASHYD 1.0 01\$O\_10 28.61 .330 No\_date 29:13 20.55 .276 .000  
 08398+ [CN ..57.01 N ..3.00 Tp ..1.10] .000  
 08399+ [TaREC 4.001 SMIN..44.50\* SMAX..508.81 / SKA ..010] .000  
 08400+ R025:00074-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08401+ CONTINUOUS\_NASHYD 1.0 01\$O\_10 44.94 .426 No\_date 29:00 15.62 n/a .000  
 08402+ [CN ..49.01 N ..3.00 Tp ..90] .000  
 08403+ [TaREC 4.001 SMIN..59.15\* SMAX..697.25 / SKA ..010] .000  
 08404+ [ROUTE 1.001 out-> 1.0 01\$RES\_NP 59.15 697.25 No\_date 29:14 19.65 n/a .000  
 08405+ R025:00075-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08406+ ADD HYD 1.0 02\$O\_10 46.94 .426 No\_date 29:00 15.62 n/a .000  
 08407+ + 1.0 02\$O\_4 26.61 .330 No\_date 29:13 20.55 .276 .000  
 08408+ 1.0 02\$O\_10 13.98 1.623 No\_date 29:11 19.65 n/a .000  
 08409+ SUM: 1.0 01\$O\_10 40420.01 41.832 No\_date 61:26 26.72 n/a .000  
 08410+ R025:00076-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms  
 08411+ ROUTE CHANNEL >> 1.0 02\$O\_10 139.27 1.623 No\_date 29:11 19.65 n/a .000  
 08412+ [ROUTE 1.001 out-> 1.0 01\$RES\_NP 139.27 1.620 No\_date 29:14 19.65 n/a .000  
 08413+ [L/S/n ..210 / .810 /.043] .000  
 08414+ [Vmax.. .998\*Imax.. .685] .000  
 08415+ R025:00077-----> Dtnin-ID:NHYD----> ARRAha-QPEAKcms-Tpeakdate\_bh:mm---->Rvmm-R.C.---DWFcms

08603+ CONTINUOUS STANDHYD 1.0 01:C1 3.41 .618 No\_date 28:01 58.43 .785 .000

08604+ [XMP= .618] TIME=.85 DTMN-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08605+ [Previous parameters: Po: 76.20[PC= 13.20[DCAV=14: Fe .00] .000

08606+ [Previous areas: Iaper: 4.67[SLPP=.50:LGP= 50.:MNP=.250:SCP=.0] .000

08607+ [Impervious areas: Iaper: 1.57[LGP= 50.:LGI= 261.:MMI=.013:SCI=.0] .000

08608+ [Inflow: 4.00: ID:MMI=.013:SCI=.0] .000

08609+ ROG25:C00109- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08610+ ROUTE RESERVOIR- > 1.0 01:C1 3.41 .618 No\_date 28:01 58.43 .785 .000

08611+ out <= 1.0 01:SDP-STE 3.41 .618 No\_date 28:23 58.43 .785 .000

08612+ overflow <= 1.0 03:CL-OVF .05 .000 No\_date 0:00 58.43 .785 .000

08613+ [MscCited=.2458e-01 m3\_TotVol=.00008 m3\_N-Ovf= 0 TotBurfv=.0 hrs] .000

08614+ ROG25:C00110- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08615+ CONTINUOUS STANDHYD 1.0 01:ST-5 .45 .071 No\_date 28:00 45.54 .612 .000

08616+ [XMP=.612] TIME=.85 DTMN-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08617+ [Morton parameters: Po: 76.20[PC= 13.20[DCAV=14: Fe .00] .000

08618+ [Previous areas: Iaper: 4.67[SLPP=.50:LGP= 50.:MNP=.250:SCP=.0] .000

08619+ [Impervious areas: Iaper: 1.57[LGP= 50.:LGI= 1230.:MMI=.013:SCI=.0] .000

08620+ [Inflow: 4.00: ID:MMI=.013:SCI=.0] .000

08621+ ROG25:C00111- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08622+ ROUTE RESERVOIR- > 1.0 01:ST-5 .45 .071 No\_date 28:00 45.54 .612 .000

08623+ out <= 1.0 01:STSSDE 3.45 .040 No\_date 28:07 45.54 .612 .000

08624+ overflow <= 1.0 03:CL-OVF .05 .000 No\_date 0:00 45.54 .612 .000

08625+ [MscCited=.2458e-01 m3\_TotVol=.00008 m3\_N-Ovf= 0 TotBurfv=.0 hrs] .000

08626+ ROG25:C00112- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08627+ ADD HYD 1.0 02:DRAINS 350.31 .511 No\_date 28:13 58.43 .785 .000

08628+ out <= 1.0 01:SDP-STE 3.41 .159 No\_date 28:23 58.43 .785 .000

08629+ + 1.0 02:C1-STR 3.41 .159 No\_date 28:23 58.43 .785 .000

08630+ + 1.0 02:C1-OVF .05 .000 No\_date 0:00 58.43 .785 .000

08631+ out <= 1.0 03:CL-OVF .05 .000 No\_date 0:00 58.43 .785 .000

08632+ + 1.0 02:STOVSF .05 .000 No\_date 0:00 58.43 .785 .000

08633+ SUM\_ 1.0 01:ST-5 356.68 5.480 No\_date 29:11 58.43 .785 .000

08634+ ROG25:C00113- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08635+ CONTINUOUS STANDHYD 1.0 01:ST-5 .79 .918 No\_date 28:10 57.02 .767 .000

08636+ [XMP=.767] TIME=.85 DTMN-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08637+ [Previous areas: Iaper: 4.67[SLPP=.50:LGP= 50.:MNP=.250:SCP=.0] .000

08638+ [Impervious areas: Iaper: 1.57[LGP= 50.:LGI= 1230.:MMI=.013:SCI=.0] .000

08639+ [Inflow: 4.00: ID:MMI=.013:SCI=.0] .000

08640+ ROG25:C00114- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08641+ ROUTE RESERVOIR- > 1.0 02:ST-5 7.59 .918 No\_date 28:10 57.02 .767 .000

08642+ out <= 1.0 01:SDP-STE 7.59 .918 No\_date 28:10 57.02 .767 .000

08643+ overflow <= 1.0 03:CL-OVF .05 .000 No\_date 0:00 57.02 .767 .000

08644+ out <= 1.0 03:OVS .05 .000 No\_date 0:00 57.02 .767 .000

08645+ [MscCited=.2915e-01 m3\_TotVol=.00008 m3\_N-Ovf= 0 TotBurfv=.0 hrs] .000

08646+ ROG25:C00115- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08647+ ADD HYD 1.0 02:ST-5 8.66 5.480 No\_date 29:11 26.21 .611 .000

08648+ out <= 1.0 02:POD-STE 7.58 .918 No\_date 29:10 57.02 .767 .000

08649+ out <= 1.0 01:SDAOD 364.27 5.589 No\_date 29:11 26.85 .611 .000

08650+ SUM\_ 1.0 01:SSAOAD 364.27 5.589 No\_date 29:11 26.85 .611 .000

08651+ ROG25:C00116- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08652+ ADD HYD 1.0 01:SSAOAD 364.27 5.589 No\_date 29:11 26.85 .611 .000

08653+ fname:SSAOAD\_0025

08654+ [Inflow: 5.18e-01 m3\_TotVol=.00008 m3\_N-Ovf= 0] .000

08655+ ROG25:C00117- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08656+ [Horton parameters: Po: 76.20[PC= 13.20[DCAV=14: Fe .00] .000

08657+ [Morton parameters: Po: 76.20[PC= 13.20[DCAV=14: Fe .00] .000

08658+ [Previous areas: Iaper: 4.67[SLPP=.50:LGP= 50.:MNP=.250:SCP=.0] .000

08659+ [Impervious areas: Iaper: 1.57[LGP= 50.:LGI= 1230.:MMI=.013:SCI=.0] .000

08660+ [Inflow: 4.00: ID:MMI=.013:SCI=.0] .000

08661+ ROG25:C00118- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08662+ ADD HYD 1.0 02:ST-5 7.59 .918 No\_date 28:09 56.06 .754 .000

08663+ fname:SSAOAD\_A\_0025

08664+ remark:SSAOAD\_A inflow

08665+ ROG25:C00119- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08666+ ROUTE RESERVOIR- > 1.0 02:A1Area 66.75 .788 No\_date 28:09 56.06 .754 .000

08667+ out <= 1.0 01:SMFPA 66.75 .788 No\_date 29:28 56.05 .754 .000

08668+ overflow <= 1.0 03:CL-OVF .05 .000 No\_date 0:00 56.05 .754 .000

08669+ [MscCited=.2443e-01 m3\_TotVol=.00008 m3\_N-Ovf= 0 TotBurfv=.0 hrs] .000

08670+ ROG25:C00120- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08671+ ROG25:C00121- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08672+ ADD HYD 1.0 01:A1Area 66.75 .788 No\_date 29:28 56.05 .754 .000

08673+ fname:SSAOAD\_A\_0025

08674+ remark:SSAOAD\_A Outflow

08675+ ROG25:C00122- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08676+ ADD HYD 1.0 02:SSAOAD 364.27 5.589 No\_date 29:11 26.85 .611 .000

08677+ out <= 1.0 01:SMFPA 66.75 .788 No\_date 29:28 56.05 .754 .000

08678+ overflow <= 1.0 03:CL-OVF .05 .000 No\_date 0:00 56.05 .754 .000

08679+ [MscCited=.2443e-01 m3\_TotVol=.00008 m3\_N-Ovf= 0 TotBurfv=.0 hrs] .000

08680+ ROG25:C00123- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08681+ CONTINUOUS STANDHYD 1.0 01:CE-5 .45 .085 No\_date 28:34 58.43 .785 .000

08682+ [XMP=.687] TIME=.85 [Vmax=.475] Dmax=.1440

08683+ [Horton parameters: Po: 76.20[PC= 13.20[DCAV=14: Fe .00] .000

08684+ [Morton parameters: Po: 76.20[PC= 13.20[DCAV=14: Fe .00] .000

08685+ [Previous areas: Iaper: 4.67[SLPP=.50:LGP= 50.:MNP=.250:SCP=.0] .000

08686+ [Impervious areas: Iaper: 1.57[LGP= 50.:LGI= 1230.:MMI=.013:SCI=.0] .000

08687+ [Inflow: 4.00: ID:MMI=.013:SCI=.0] .000

08688+ ROG25:C00124- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08689+ ADD HYD 1.0 02:ST-5 7.59 .918 No\_date 28:09 56.06 .754 .000

08690+ out <= 1.0 01:SDP-STE 7.59 .918 No\_date 28:09 56.06 .754 .000

08691+ overflow <= 1.0 03:CL-OVF .05 .000 No\_date 0:00 56.06 .754 .000

08692+ [MscCited=.2443e-01 m3\_TotVol=.00008 m3\_N-Ovf= 0 TotBurfv=.0 hrs] .000

08693+ ROG25:C00125- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08694+ CONTINUOUS STANDHYD 1.0 01:W1\_CLAR\_BRA 73.29 8.076 No\_date 28:09 52.35 .704 .000

08695+ [XMP=.607] TIME=.65 [Vmax=.475] Dmax=.1440

08696+ ROG25:C00126- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08697+ ADD HYD 1.0 02:POD-STE 325.44 7.246 No\_date 29:04 52.35 .704 .000

08698+ out <= 1.0 01:POF-STE 325.44 7.246 No\_date 29:04 52.35 .704 .000

08699+ overflow <= 1.0 03:POF-STE 325.44 7.246 No\_date 29:04 52.35 .704 .000

08700+ [MscCited=.1688e-01 m3\_TotVol=.00008 m3\_N-Ovf= 0 TotBurfv=.0 hrs] .000

08701+ ROG25:C00127- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08702+ ADD HYD 1.0 02:POD-STE 325.44 7.246 No\_date 29:04 52.35 .704 .000

08703+ out <= 1.0 01:POF-STE 325.44 7.246 No\_date 29:04 52.35 .704 .000

08704+ overflow <= 1.0 03:POF-STE 325.44 7.246 No\_date 29:04 52.35 .704 .000

08705+ [MscCited=.1688e-01 m3\_TotVol=.00008 m3\_N-Ovf= 0 TotBurfv=.0 hrs] .000

08706+ ROG25:C00128- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08707+ ADD HYD 1.0 02:POD-STE 325.44 7.246 No\_date 29:04 52.35 .704 .000

08708+ out <= 1.0 01:POF-STE 325.44 7.246 No\_date 29:04 52.35 .704 .000

08709+ overflow <= 1.0 03:POF-STE 325.44 7.246 No\_date 29:04 52.35 .704 .000

08710+ [MscCited=.1688e-01 m3\_TotVol=.00008 m3\_N-Ovf= 0 TotBurfv=.0 hrs] .000

08711+ ROG25:C00127- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08712+ ROUTE RESERVOIR- > 1.0 02:ST-6 .41 .065 No\_date 28:00 45.54 .611 .000

08713+ out <= 1.0 01:SDP-STE 4.01 .065 No\_date 28:00 45.54 .611 .000

08714+ overflow <= 1.0 03:CL-OVF .05 .000 No\_date 0:00 45.54 .611 .000

08715+ [MscCited=.4331e-01 m3\_TotVol=.00008 m3\_N-Ovf= 0 TotBurfv=.0 hrs] .000

08716+ ROG25:C00128- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08717+ ADD HYD 1.0 02:POD-STE 433.02 6.356 No\_date 29:13 31.37 .600 .000

08718+ out <= 1.0 01:POF-STE 1.87 .394 No\_date 28:01 58.43 .611 .000

08719+ out <= 1.0 01:CE-STE 1.87 .394 No\_date 28:01 58.43 .611 .000

08720+ overflow <= 1.0 03:CE-STE 1.87 .394 No\_date 28:01 58.43 .611 .000

08721+ + 1.0 02:CT-OVF .05 .000 No\_date 0:00 58.43 .611 .000

08722+ out <= 1.0 01:CT-OVF .05 .000 No\_date 0:00 58.43 .611 .000

08723+ overflow <= 1.0 03:CT-OVF .05 .000 No\_date 0:00 58.43 .611 .000

08724+ [MscCited=.4331e-01 m3\_TotVol=.00008 m3\_N-Ovf= 0 TotBurfv=.0 hrs] .000

08725+ ROG25:C00129- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08726+ ROUTE CHANNEL- > 1.0 02:PS7EST 434.92 6.464 No\_date 29:12 31.66 .610 .000

08727+ out <= 1.0 01:CE-STE 434.92 6.464 No\_date 29:12 31.66 .610 .000

08728+ overflow <= 1.0 03:CE-STE 434.92 6.464 No\_date 29:12 31.66 .610 .000

08729+ [MscCited=.4331e-01 m3\_TotVol=.00008 m3\_N-Ovf= 0 TotBurfv=.0 hrs] .000

08730+ ROG25:C00130- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08731+ ADD HYD 1.0 02:POD-STE 434.92 6.464 No\_date 29:12 31.66 .610 .000

08732+ out <= 1.0 01:POF-STE 434.92 6.464 No\_date 29:12 31.66 .610 .000

08733+ overflow <= 1.0 03:POF-STE 434.92 6.464 No\_date 29:12 31.66 .610 .000

08734+ [MscCited=.4331e-01 m3\_TotVol=.00008 m3\_N-Ovf= 0 TotBurfv=.0 hrs] .000

08735+ ROG25:C00131- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08736+ CONTINUOUS STANDHYD 1.0 01:A1 1.73 .092 No\_date 28:34 43.34 .583 .000

08737+ [XMP=.88.01 N .00D Tp=.60] .000

08738+ ROG25:C00132- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08739+ ADD HYD 1.0 02:POD-STE 434.92 6.464 No\_date 29:13 31.37 .600 .000

08740+ out <= 1.0 01:POF-STE 434.92 6.464 No\_date 29:13 31.37 .600 .000

08741+ overflow <= 1.0 03:POF-STE 434.92 6.464 No\_date 29:13 31.37 .600 .000

08742+ [MscCited=.4331e-01 m3\_TotVol=.00008 m3\_N-Ovf= 0 TotBurfv=.0 hrs] .000

08743+ ROG25:C00133- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08744+ ROUTE RESERVOIR- > 1.0 01:A2Area 24.04 .516 No\_date 28:03 54.85 .611 .000

08745+ out <= 1.0 01:SMFPA 24.04 .492 No\_date 28:04 54.85 .611 .000

08746+ overflow <= 1.0 03:CL-OVF .05 .000 No\_date 0:00 54.85 .611 .000

08747+ [MscCited=.1788e-01 m3\_TotVol=.00008 m3\_N-Ovf= 0 TotBurfv=.0 hrs] .000

08748+ ROG25:C00134- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08749+ ADD HYD 1.0 02:POD-STE 434.92 6.464 No\_date 29:13 31.37 .600 .000

08750+ out <= 1.0 01:POF-STE 434.92 6.464 No\_date 29:13 31.37 .600 .000

08751+ overflow <= 1.0 03:POF-STE 434.92 6.464 No\_date 29:13 31.37 .600 .000

08752+ [MscCited=.1788e-01 m3\_TotVol=.00008 m3\_N-Ovf= 0 TotBurfv=.0 hrs] .000

08753+ ROG25:C00135- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08754+ CONTINUOUS STANDHYD 1.0 01:D5 1.90 .075 No\_date 28:41 40.67 .547 .000

08755+ [XMP=.4.00 SMN=.17.43 SMAX=.116.21 SK=.010] .000

08756+ ROG25:C00136- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08757+ CONTINUOUS NASHYD 1.0 01:01-13SFDP 9.74 .487 No\_date 28:22 38.23 .514 .000

08758+ [XMP=.81.00 N .00D Tp=.43] .000

08759+ ROG25:C00137- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08760+ ROUTE RESERVOIR- > 1.0 01:10:13SFDP 9.74 .487 No\_date 28:22 38.23 .514 .000

08761+ out <= 1.0 01:SDP-STE 9.74 .052 No\_date 31:01 38.23 .514 .000

08762+ overflow <= 1.0 03:VFSDFP .05 .000 No\_date 0:00 38.23 .514 .000

08763+ [MscCited=.2458e-01 m3\_TotVol=.00008 m3\_N-Ovf= 0 TotBurfv=.0 hrs] .000

08764+ ROG25:C00138- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08765+ CONTINUOUS NASHYD 1.0 01:01-13SFDP 9.74 .487 No\_date 28:23 38.23 .514 .000

08766+ [XMP=.81.00 N .00D Tp=.43] .000

08767+ ROG25:C00139- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08768+ CONTINUOUS STANDHYD 1.0 01:01-13SFDP 9.74 .487 No\_date 28:23 38.23 .514 .000

08769+ [XMP=.81.00 N .00D Tp=.43] .000

08770+ ROG25:C00140- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08771+ ADD HYD 1.0 02:DRAINS 460.69 6.598 No\_date 29:35 32.86 .610 .000

08772+ out <= 1.0 01:SDP-STE 460.69 6.598 No\_date 29:35 32.86 .610 .000

08773+ overflow <= 1.0 03:CL-OVF .05 .000 No\_date 0:00 32.86 .610 .000

08774+ [MscCited=.2458e-01 m3\_TotVol=.00008 m3\_N-Ovf= 0 TotBurfv=.0 hrs] .000

08775+ ROG25:C00141- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08776+ CONTINUOUS NASHYD 1.0 01:01-14CH 460.69 6.598 No\_date 29:34 33.09 .610 .000

08777+ [XMP=.4.00 SMN=.17.43 SMAX=.153.94 SK=.010] .000

08778+ ROG25:C00142- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08779+ ADD HYD 1.0 02:M- 483.00 6.790 No\_date 29:34 33.09 .610 .000

08780+ out <= 1.0 01:01-14CH 483.00 6.790 No\_date 29:35 33.09 .610 .000

08781+ [XMP=.4.00 SMN=.17.43 SMAX=.153.94 SK=.010] .000

08782+ [XMP=.618] TIME=.12.00 DTMN-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08783+ ADD HYD 1.0 02:POD-STE 472.33 6.689 No\_date 29:35 33.09 .610 .000

08784+ out <= 1.0 01:POF-STE 10.67 .688 No\_date 29:35 37.06 .610 .000

08785+ overflow <= 1.0 03:POF-STE 10.67 .688 No\_date 0:00 37.06 .610 .000

08786+ [MscCited=.2458e-01 m3\_TotVol=.00008 m3\_N-Ovf= 0 TotBurfv=.0 hrs] .000

08787+ ROG25:C00141- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08788+ ROUTE CHANNEL- > 1.0 02:M- 483.00 6.790 No\_date 29:34 33.09 .610 .000

08789+ [XMP=.4.00 SMN=.17.43 SMAX=.153.94 SK=.010] .000

08790+ [XMP=.618] TIME=.12.00 DTMN-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08791+ ADD HYD 1.0 02:HWD 483.00 6.790 No\_date 29:35 33.09 .610 .000

08792+ out <= 1.0 01:01-14CH 483.00 6.790 No\_date 29:36 33.09 .610 .000

08793+ CONTINUOUS NASHYD 1.0 01:01-14CH 483.00 6.790 No\_date 29:36 33.09 .610 .000

08794+ [XMP=.618] TIME=.12.00 DTMN-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08795+ ADD HYD 1.0 02:HWD 483.00 6.790 No\_date 29:37 33.09 .610 .000

08796+ out <= 1.0 01:01-14CH 483.00 6.790 No\_date 29:38 33.09 .610 .000

08797+ overflow <= 1.0 03:01-14CH 483.00 6.790 No\_date 0:00 33.09 .610 .000

08798+ [MscCited=.2458e-01 m3\_TotVol=.00008 m3\_N-Ovf= 0 TotBurfv=.0 hrs] .000

08799+ ROG25:C00140- :>Dtmn-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn=R.C.--DWFcms

08800+ ADD HYD 1.0 02:DRAINS 483.00 6.790 No\_date 29:39 33.09 .610 .000

08801+ out <= 1.0 01:SDP-STE 483.00 6.790 No\_date 29:40 33.09 .610 .000

08802+ [XMP=.618] TIME=.12.00 DTMN-ID:NHYD- :>ARAH-A-PEAKcms-TpeakDate\_hh:mm-->Rvn



09351+ CONTINUOUS STANDHYD 1. 01:01-KB-13 10.19 1.930 No\_date 28:00 53.97 .726 .000

09352+ [XIMP=7-TIMEP=.64] Dtnin-ID:NHYD-  
[Horton parameters: Fo= 76.20Pc\*13.20(DCAY4.14: Fe\_00) ]  
[Previous areas: Iaper: 4.67\*SLPP2.0:00Ldg\* 40.:MNP\* .250:SCP\* .0] .000

09353+ [Impervious areas: IaImpg: 1.57\*SL1+1.00:Ldg1. 79\*1.00:Ldg1. 261. NMN\*.013:SCI\* .0]

09354+ Minor System \ 1. 03:01-KB-13-MN\* 10.19 1.722 No\_date 27:57 53.98 n/a .000

09355+ [WjSysSto-.4703E+02 TotoFvVol1.000E+00-N-Ovf\* 0. hrs]

09356+ Dtnin-ID:C00231----- Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09357+ ROG25:CO0231----- Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09358+ COMPUTE DUALHYD 1. 01:01-KB-13 10.19 1.930 No\_date 28:00 53.97 .726 .000

09359+ Minor System / 1. 02:01-KB-13-MN\* 10.19 1.722 No\_date 27:57 53.98 n/a .000

09360+ ADD HYD Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09361+ ADD HYD 1. 02:01-KB-13-MN\* 10.19 1.722 No\_date 27:57 53.98 n/a .000

09362+ ROG25:CO0231----- Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09363+ ADD HYD 1. 02:01-KB-13-MN\* 10.19 1.722 No\_date 27:57 53.98 n/a .000

09364+ SUM+ 1. 01:01-KB-13 10.19 1.722 No\_date 27:57 53.98 n/a .000

09365+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09366+ ROG25:CO0231----- Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09367+ [XIMP=64:TIMEP=.64]  
[Horton parameters: Fo= 76.20Pc\*13.20(DCAY4.14: Fe\_00) ]  
[Previous areas: Iaper: 4.67\*SLPP2.0:00Ldg\* 40.:MNP\* .250:SCP\* .0]

09368+ [Impervious areas: IaImpg: 1.57\*SL1+1.00:Ldg1. 191. NMN\*.013:SCI\* .0]

09369+ [iakEcmp: 4.00: IaRECPer\_ 1.00]

09370+ ROG25:CO0231----- Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09371+ COMPUTE DUALHYD 1. 01:01-KB-14 5.47 1.075 No\_date 28:00 53.97 n/a .000

09372+ Minor System / 1. 02:01-KB-14-MN\* 5.47 1.075 No\_date 28:00 53.97 n/a .000

09373+ ADD HYD 1. 02:01-KB-14-MN\* 5.47 1.075 No\_date 28:00 53.97 n/a .000

09374+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09375+ ADD HYD 1. 02:01-KB-14-MN\* 5.47 1.075 No\_date 28:00 53.97 n/a .000

09376+ SUM+ 1. 01:01-KB-14 5.47 1.075 No\_date 28:00 53.97 n/a .000

09377+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09378+ ROG25:CO0235----- Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09379+ ADD HYD 1. 02:01-KB-14-MN\* 5.47 1.075 No\_date 28:00 53.97 n/a .000

09380+ SUM+ 1. 01:01-KB-14-MN\* 5.47 1.075 No\_date 27:55 54.32 n/a .000

09381+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09382+ ROG25:CO0236----- Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09383+ CONTINUOUS STANDHYD 1. 01:01-KB-16\_2 3.42 .649 No\_date 28:01 58.24 .783 .000

09384+ [XIMP=7-TIMEP=.71]  
[Horton parameters: Fo= 76.20Pc\*13.20(DCAY4.14: Fe\_00) ]  
[Previous areas: Iaper: 4.67\*SLPP2.0:00Ldg\* 40.:MNP\* .250:SCP\* .0]

09385+ [Impervious areas: IaImpg: 1.57\*SL1+1.00:Ldg1. 191. NMN\*.013:SCI\* .0]

09386+ [iakEcmp: 4.00: IaRECPer\_ 1.00]

09387+ ROG25:CO0237----- Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09388+ COMPUTE DUALHYD 1. 01:01-KB-14 5.47 1.075 No\_date 28:00 53.97 n/a .000

09389+ Minor System / 1. 02:01-KB-14-MN\* 5.47 1.075 No\_date 28:00 53.97 n/a .000

09390+ ADD HYD 1. 02:01-KB-14-MN\* 5.47 1.075 No\_date 28:00 53.97 n/a .000

09391+ SUM+ 1. 01:01-KB-14 5.47 1.075 No\_date 27:55 54.32 n/a .000

09392+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09393+ ADD HYD 1. 02:01-KB-10\_2 1.14 .266 No\_date 28:00 65.30 n/a .000

09394+ SUM+ 1. 01:02-KB-12 1.14 .266 No\_date 28:00 65.30 n/a .000

09395+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09396+ ADD HYD 1. 01:02-KB-12 1.14 .266 No\_date 28:00 65.30 n/a .000

09397+ SUM+ 1. 01:02-KB-12 1.14 .266 No\_date 27:55 65.30 n/a .000

09398+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09399+ ADD HYD 1. 01:02-KB-14 5.47 .873 No\_date 27:55 54.32 n/a .000

09400+ SUM+ 1. 01:02-KB-14 5.47 .873 No\_date 27:55 54.32 n/a .000

09401+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09402+ ROUTE RESERVOIR < 1. 01:01-KB-20 1.14 .266 No\_date 28:00 65.30 n/a .000

09403+ out < 1. 01:01-KB-20 1.14 .266 No\_date 28:00 65.30 n/a .000

09404+ overflow < 1. 01:01-KB-20 1.14 .266 No\_date 28:00 65.30 n/a .000

09405+ [ModelSpecd=.9758E+02 TotoFvVol1.000E+00-N-Ovf\* 0. hrs]

09406+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09407+ ADD HYD 1. 02:01-KB-20 254.24 17.12 No\_date 28:11 42.08 n/a .000

09408+ SUM+ 1. 01:01-KB-20 254.24 17.12 No\_date 28:11 42.08 n/a .000

09409+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09410+ ADD HYD 1. 01:01-KB-20 254.24 17.12 No\_date 28:11 42.08 n/a .000

09411+ SUM+ 1. 01:01-KB-20 254.24 17.12 No\_date 28:11 42.08 n/a .000

09412+ KB-Pond2.0025  
rtotal:Total Flows at KB second pond

09413+ rtotal:Total Flows at KB third pond

09414+ rtotal:Total Flows at KB fourth pond

09415+ rtotal:Total Flows at KB fifth pond

09416+ rtotal:Total Flows at KB sixth pond

09417+ rtotal:Total Flows at KB seventh pond

09418+ rtotal:Total Flows at KB eighth pond

09419+ rtotal:Total Flows at KB ninth pond

09420+ rtotal:Total Flows at KB tenth pond

09421+ rtotal:Total Flows at KB eleventh pond

09422+ ADD HYD 1. 02:01-KB-Pond2 254.24 17.12 No\_date 28:11 42.08 n/a .000

09423+ Minor System / 1. 02:01-KB-Pond2 254.24 17.12 No\_date 28:11 42.08 n/a .000

09424+ SUM+ 1. 01:01-KB-Pond2 254.24 17.12 No\_date 28:11 42.08 n/a .000

09425+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09426+ ROUTE RESERVOIR < 1. 01:01-KB-Pond2 1.14 .266 No\_date 28:11 42.08 n/a .000

09427+ out < 1. 01:01-KB-Pond2 1.14 .266 No\_date 28:11 42.08 n/a .000

09428+ overflow < 1. 01:01-KB-Pond2 1.14 .266 No\_date 28:10 42.28 n/a .000

09429+ [ModelSpecd=.9758E+02 TotoFvVol1.000E+00-N-Ovf\* 0. hrs]

09430+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09431+ ADD HYD 1. 02:01-KB-Pond2 1.14 .266 No\_date 28:10 42.28 n/a .000

09432+ SUM+ 1. 01:01-KB-Pond2 1.14 .266 No\_date 28:10 42.28 n/a .000

09433+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09434+ ADD HYD 1. 01:01-KB-Pond2 257.04 17.344 No\_date 28:10 42.28 n/a .000

09435+ SUM+ 1. 01:01-KB-Pond2 257.04 17.344 No\_date 28:10 42.28 n/a .000

09436+ frame KB-Pond2.0025  
rtotal:Total Flows at KB third pond

09437+ rtotal:Total Flows at KB fourth pond

09438+ rtotal:Total Flows at KB fifth pond

09439+ EXISTING PROPOSED Subcatchments (Kennedy-Burnett SWN Facility (118080), SWN Modeling Approach, NOVATECH Report June, 2020 )  
+ PRAEGER-CLARKE DRAIN

09440+ \*\*\*\*\*

09441+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09442+ ROG25:CO0246----- Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09443+ Minor System / 1. 01:01-KB-FO-01 8.03 1.288 No\_date 28:01 44.33 .596 .000

09444+ [XIMP=47:TIMEP=.47]  
[Horton parameters: Fo= 4.67\*SLPP2.0:00Ldg\* 40.:MNP\* .250:SCP\* .0]

09445+ [Previous areas: Iaper: 4.67\*SLPP2.0:00Ldg\* 40.:MNP\* .250:SCP\* .0]

09446+ [Impervious areas: IaImpg: 1.61\*SL1+1.00:Ldg1. 30:Ldg1. 137. NMN\*.013:SCI\* .0]

09447+ [iakEcmp: 4.00: IaRECPer\_ 1.00]

09448+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09449+ COMPUTE DUALHYD 1. 01:01-KB-FO-01 8.03 1.288 No\_date 28:01 44.33 n/a .000

09450+ Minor System / 1. 02:01-KB-FO-01 8.03 1.288 No\_date 28:01 44.33 n/a .000

09451+ ADD HYD 1. 02:01-KB-FO-01 8.03 1.288 No\_date 27:55 44.33 n/a .000

09452+ SUM+ 1. 01:02-KB-FO-01 8.03 1.288 No\_date 27:55 44.33 n/a .000

09453+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09454+ COMPUTE DUALHYD 1. 01:01-KB-FO-01 8.03 1.288 No\_date 28:00 44.33 n/a .000

09455+ Minor System / 1. 02:01-KB-FO-01 8.03 1.288 No\_date 28:00 44.33 n/a .000

09456+ ADD HYD 1. 02:01-KB-FO-01 8.03 1.288 No\_date 28:00 44.33 n/a .000

09457+ SUM+ 1. 01:01-KB-FO-01 8.03 1.288 No\_date 27:55 44.33 n/a .000

09458+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09459+ CONTINUOUS STANDHYD 1. 01:01-KB-FO-02 16.05 3.498 No\_date 28:01 28.00 69.00 .928 .000

09460+ [XIMP=93:TIMEP=.93]  
[Horton parameters: Fo= 76.20Pc\*13.20(DCAY4.14: Fe\_00) ]

09461+ [Previous areas: Iaper: 4.67\*SLPP2.0:00Ldg\* 40.:MNP\* .250:SCP\* .0]

09462+ [Impervious areas: IaImpg: 1.57\*SL1+1.00:Ldg1. 327. NMN\*.013:SCI\* .0]

09463+ [iakEcmp: 4.00: IaRECPer\_ 1.00]

09464+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09465+ COMPUTE DUALHYD 1. 01:01-KB-FO-02 16.05 3.498 No\_date 28:00 69.00 n/a .000

09466+ Minor System / 1. 02:01-KB-FO-02 16.05 3.498 No\_date 28:00 69.00 n/a .000

09467+ SUM+ 1. 01:02-KB-FO-02 16.05 3.498 No\_date 28:00 69.00 n/a .000

09468+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09469+ CONTINUOUS STANDHYD 1. 01:01-KB-FO-02 16.05 3.498 No\_date 28:00 69.00 n/a .000

09470+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09471+ ADD HYD 1. 02:01-KB-FO-02-MN\* 16.05 1.599 No\_date 27:44 51.60 n/a .000

09472+ SUM+ 1. 01:02-KB-FO-02-MN\* 16.05 1.599 No\_date 27:44 51.60 n/a .000

09473+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09474+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09475+ CONTINUOUS STANDHYD 1. 01:01-KB-FO-02 16.05 3.498 No\_date 28:00 69.00 n/a .000

09476+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09477+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09478+ [Previous areas: Iaper: 4.67\*SLPP2.0:00Ldg\* 40.:MNP\* .250:SCP\* .0]

09479+ [Impervious areas: IaImpg: 1.57\*SL1+1.00:Ldg1. 222. NMN\*.013:SCI\* .0]

09480+ [iakEcmp: 4.00: IaRECPer\_ 1.00]

09481+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09482+ COMPUTE DUALHYD 1. 01:01-KB-FO-02 16.05 3.498 No\_date 28:00 69.00 n/a .000

09483+ Minor System / 1. 02:01-KB-FO-02 16.05 3.498 No\_date 28:00 69.00 n/a .000

09484+ SUM+ 1. 01:02-KB-FO-02 16.05 3.498 No\_date 28:00 69.00 n/a .000

09485+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09486+ ROG25:CO0248----- Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09487+ ADD HYD 1. 02:01-KB-FO-02 16.05 3.498 No\_date 27:45 51.60 n/a .000

09488+ SUM+ 1. 01:02-KB-FO-02 16.05 3.498 No\_date 27:45 51.60 n/a .000

09489+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09490+ CONTINUOUS STANDHYD 1. 01:01-KB-FO-02 16.05 3.498 No\_date 28:00 53.47 .719 .000

09491+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09492+ ADD HYD 1. 02:01-KB-FO-02 16.05 3.498 No\_date 27:45 53.47 n/a .000

09493+ Minor System / 1. 02:01-KB-FO-02 16.05 3.498 No\_date 27:45 53.47 n/a .000

09494+ SUM+ 1. 01:02-KB-FO-02 16.05 3.498 No\_date 27:45 53.47 n/a .000

09495+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09496+ COMPUTE DUALHYD 1. 01:01-KB-FO-02 16.05 3.498 No\_date 28:00 53.47 n/a .000

09497+ Minor System / 1. 02:01-KB-FO-02 16.05 3.498 No\_date 28:00 53.47 n/a .000

09498+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09499+ COMPUTE DUALHYD 1. 01:01-KB-FO-02 16.05 3.498 No\_date 28:01 53.47 n/a .000

09500+ Minor System / 1. 02:01-KB-FO-02 16.05 3.498 No\_date 28:01 53.47 n/a .000

09501+ [WjSysSto-.1887E+04 TotoFvVol1.000E+00-N-Ovf\* 0. hrs]

09502+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09503+ ADD HYD 1. 02:01-KB-FO-02 16.05 3.498 No\_date 28:00 53.47 n/a .000

09504+ Minor System / 1. 02:01-KB-FO-02 16.05 3.498 No\_date 28:00 53.47 n/a .000

09505+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09506+ \*\*\*\*\*  
# PROPOSED Subcatchments (Kennedy-Burnett SWN Facility (118080), SWN Modeling Approach, NOVATECH Report June, 2020 )  
+ PRAEGER-CLARKE DRAIN

09507+ \*\*\*\*\*

09508+ \*\*\*\*\*

09509+ \*\*\*\*\*

09510+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09511+ CONTINUOUS STANDHYD 1. 01:01-JR-01 16.05 1.515 No\_date 28:00 53.47 .719 .000

09512+ [XIMP=64:TIMEP=.64]  
[Horton parameters: Fo= 76.20Pc\*13.20(DCAY4.14: Fe\_00) ]

09513+ [Previous areas: Iaper: 4.67\*SLPP2.0:00Ldg\* 40.:MNP\* .250:SCP\* .0]

09514+ [Impervious areas: IaImpg: 1.57\*SL1+1.00:Ldg1. 103. NMN\*.013:SCI\* .0]

09515+ [iakEcmp: 4.00: IaRECPer\_ 1.00]

09516+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09517+ COMPUTE DUALHYD 1. 01:01-JR-01 16.05 1.515 No\_date 28:00 53.47 .719 .000

09518+ Minor System / 1. 02:01-JR-01 16.05 1.515 No\_date 28:00 53.47 n/a .000

09519+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09520+ ROG25:CO0260----- Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09521+ ADD HYD 1. 02:01-JR-01 16.05 1.515 No\_date 27:45 53.47 n/a .000

09522+ Minor System / 1. 02:01-JR-01 16.05 1.515 No\_date 27:45 53.47 n/a .000

09523+ SUM+ 1. 01:02-JR-01 16.05 1.515 No\_date 27:45 53.47 n/a .000

09524+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09525+ Minor System / 1. 01:02-JR-01 16.05 1.515 No\_date 27:45 53.47 n/a .000

09526+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09527+ CONTINUOUS STANDHYD 1. 01:01-JR-02 1.59 .316 No\_date 28:00 53.47 .719 .000

09528+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09529+ [WjSysSto-.7433E+03 TotoFvVol1.000E+00-N-Ovf\* 0. hrs]

09530+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09531+ Minor System / 1. 01:02-JR-02-MN\* 1.59 .316 No\_date 27:45 53.47 n/a .000

09532+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09533+ Minor System / 1. 02:01-JR-02-MN\* 1.59 .316 No\_date 27:45 53.47 n/a .000

09534+ Dtnin-ID:NHYD-  
[ARAH-A-OPENKcms-TpeakDate\_hh:mm--RVMn-R.C.--DWFcms .000]

09535+ \*\*\*\*\*  
# PROPOSED Subcatchments (Kennedy-Burnett SWN Facility (118080), SWN Modeling Approach, NOVATECH Report June, 2020 )  
+ PRAEGER-CLARKE DRAIN

09536+ \*\*\*\*\*

09537+ \*\*\*\*\*

09538+ \*\*\*\*\*

09539+ \*\*\*\*\*

09540+ \*\*\*\*\*

09541+ \*\*\*\*\*

09542+ \*\*\*\*\*

09543+ \*\*\*\*\*

09544+ \*\*\*\*\*

09545+ \*\*\*\*\*

09546+ \*\*\*\*\*

09547+ \*\*\*\*\*

09548+ \*\*\*\*\*

09549+ \*\*\*\*\*

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09600+ \*\*\*\*\*

09601+ \*\*\*\*\*

09602+ \*\*\*\*\*

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09619+ \*\*\*\*\*

09620+ \*\*\*\*\*

09621+ \*\*\*\*\*

09622+ \*\*\*\*\*

09623+ \*\*\*\*\*

09624+ \*\*\*\*\*

09625+ \*\*\*\*\*

09626+ \*\*\*\*\*

09627+ \*\*\*\*\*

09628+ \*\*\*\*\*

09629+ \*\*\*\*\*

09630+ \*\*\*\*\*

09631+ \*\*\*\*\*

09632+ \*\*\*\*\*

09633+ \*\*\*\*\*

09634+ \*\*\*\*\*

09635+ \*\*\*\*\*

09636+ \*\*\*\*\*

09637+ \*\*\*\*\*

09638+ \*\*\*\*\*

09639+ \*\*\*\*\*

09640+ \*\*\*\*\*

09641+ \*\*\*\*\*

096

09725- ROUTE RESERVOIR -> 1. 02:TODD 120.62 14.962 No\_date 28:03 53.48 n/a .000  
 09726- out <- 1. 01:MS\_P3 120.62 9.717 No\_date 28:14 53.48 n/a .000  
 09727- overfl <- 1. 01:MS\_P3 120.62 9.717 No\_date 28:14 53.48 n/a .000  
 09728- [Msc:Used=, 26191=0 m<sub>3</sub>, TotDurOfv= 0.hrs] .000  
 09729- R0215:CH0289-  
 09730- ADD HYD 1. 02:GreenB 5471.79 110.282 No\_date 28:07 29.14 n/a .000  
 09731- + 1. 02:MS\_P3 120.62 9.717 No\_date 28:14 53.48 n/a .000  
 09732- + 1. 02:TODD 120.62 9.717 No\_date 28:07 29.14 n/a .000  
 09733- + 1. 02:TODD\_MN2 0.04 967.00 No\_date 28:00 53.48 n/a .000  
 09734- SMM+ 1. 02:TODD 120.62 9.717 No\_date 28:00 53.48 n/a .000  
 09735- [Vmax=.905,Imax=.3258]  
 09736- R0215:CO0290-  
 09737- SAVW HYD 1. 01:SM\_INTO 54838.44 110.670 No\_date 36:07 29.14 n/a .000  
 09738- frame: SM\_INTO 0025  
 09739- remark:Total Flows at Todd Drain  
 09740- # Hydrograph from Todd drain routed to Corrigan Brain  
 09741- # Channel X-Section obtained from FVCA Hydraulic Model, Station 2462  
 09742- # Channel K-Section obtained from FVCA Hydraulic Model, Station 2462  
 09743- # 2021-02-19 Change the slope from 0.033 % (as per Staement Report) to 0.05 % so the model will be more stable and g  
 09744- R0215:CH0291-  
 09745- ROUTE CHANNEL -> 1. 01:SM\_INTO 54838.44 110.461 No\_date 36:21 29.14 n/a .000  
 09746- \* [R07-1.00] out- > 1. 01:SM\_INTO 54838.44 110.461 No\_date 36:21 29.14 n/a .000  
 09747- [Vmax=.905,Imax=.3258]  
 09748- R0215:CO0292-  
 09749- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09750- SMM+ 1. 01:INTO 54838.44 110.461 No\_date 36:21 29.14 n/a .000  
 09751- frame: IN\_TO\_0025  
 09752- remark:Total inflows at Station 2462  
 09753- R0215:CH0293-  
 09754- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09755- # Catchment CORRIG (node of the jock)  
 09756- # Dtnin:ID:NHYD- (medium density)  
 09757- # - FJRA JAN 2021, add Corrigan subcatchments as per IBI, July 2008  
 09758- \*  
 09759- R0215:CO0294-  
 09760- CONTINUOUS STANDYD 1. 01:Corrig 15.87 2.535 No\_date 28:01 57.01 .766 .000  
 09761- COMPUTE DUALHYD 1. 01:Corrig 15.87 2.535 No\_date 28:01 57.01 .766 .000  
 09762- Major System / 1. 01:Corrig 15.87 2.535 No\_date 28:01 57.01 .766 .000  
 09763- [XING= 63:TIME= 63]  
 09764- [Previous area: Iaper: 4.67:SLPP=1.00:LGP= 40.:MNP=.250:SCP=.0]  
 09765- [Impervious area: Iaper: 1.57:SLP1=1.00:LGP= 325.:MNP=.013:SCI=.0]  
 09766- [Vmax=.905,Imax=.3258]  
 09767- [SMIN= 31.15: SMAX=207.66: SKO=.010]  
 09768- R0215:CO0295-  
 09769- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09770- CONTINUOUS STANDYD 1. 01:Corrig 15.87 2.535 No\_date 28:01 57.01 .766 .000  
 09771- COMPUTE DUALHYD 1. 01:Corrig 15.87 2.535 No\_date 28:01 57.01 .766 .000  
 09772- R0215:CO0295-  
 09773- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09774- CONTINUOUS STANDYD 1. 01:Corrig 12.47 .276 No\_date 29:10 34.14 .459 .000  
 09775- COMPUTE DUALHYD 12.47 .276 No\_date 29:10 34.14 .459 .000  
 09776- [XING= 77.01: TIME= 12.00]  
 09777- R0215:CO0296-  
 09778- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09779- CONTINUOUS STANDYD 1. 01:Corrig 15.75 2.022 No\_date 28:01 49.44 .665 .000  
 09780- COMPUTE DUALHYD 1. 01:Corrig 15.75 2.022 No\_date 28:01 49.44 .665 .000  
 09781- [Previous area: Iaper: 4.67:SLPP=1.00:LGP= 40.:MNP=.250:SCP=.0]  
 09782- [Impervious area: Iaper: 1.57:SLP1=1.00:LGP= 325.:MNP=.013:SCI=.0]  
 09783- [Vmax=.905,Imax=.3258]  
 09784- [SMIN= 33.81: SMAX=225.43: SKO=.010]  
 09785- R0215:CO0297-  
 09786- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09787- COMPUTE DUALHYD 1. 01:Corrig 15.75 2.022 No\_date 28:01 49.44 .665 .000  
 09788- Major System / 1. 01:Corrig 15.75 2.022 No\_date 28:01 49.44 .665 .000  
 09789- [XING= 42:TIME= 12.00]  
 09790- R0215:CO0298-  
 09791- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09792- CONTINUOUS STANDYD 1. 01:Corrig 2.77 .097 No\_date 28:09 21.19 .285 .000  
 09793- [XING= 56.01: TIME= 2.77]  
 09794- [XING= 4.00: SMIN=.79.69: SMAX=513.24: SKO=.010]  
 09795- R0215:CO0299-  
 09796- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09797- CONTINUOUS STANDYD 1. 01:Corrig 1.27 .212 No\_date 28:01 57.38 .771 .000  
 09798- [XING= 57.38: TIME= 1.27]  
 09799- [Losses = 2 : CN= 75.0]  
 09800- [Previous area: Iaper: 4.67:SLPP=1.00:LGP= 40.:MNP=.250:SCP=.0]  
 09801- [Impervious area: Iaper: 1.57:SLP1=1.00:LGP= 253.:MNP=.013:SCI=.0]  
 09802- [Vmax=.905,Imax=.3258]  
 09803- R0215:CO0300-  
 09804- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09805- COMPUTE DUALHYD 1. 01:Corrig 1.27 .212 No\_date 28:01 57.38 .771 .000  
 09806- Major System / 1. 01:Corrig 1.27 .212 No\_date 28:01 57.38 .771 .000  
 09807- [XING= 57.38: TIME= 1.27]  
 09808- R0215:CO0301-  
 09809- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09810- ADD HYD 1. 01:Corrig 1.27 .212 No\_date 28:01 57.38 .771 .000  
 09811- + 1. 02:MS\_P3 1.27 .212 No\_date 28:01 57.38 .771 .000  
 09812- + 1. 02:TODD 1.27 .212 No\_date 28:01 57.38 .771 .000  
 09813- + 1. 02:TODD\_MN2 0.04 967.00 No\_date 28:00 53.48 n/a .000  
 09814- SMM+ 1. 02:TODD 1.27 .212 No\_date 28:00 53.48 n/a .000  
 09815- [Vmax=.905,Imax=.3258]  
 09816- R0215:CO0302-  
 09817- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09818- CONTINUOUS STANDYD 1. 01:Corrig 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09819- frame: MH02\_0025  
 09820- remark:Total Flows at MH01  
 09821- R0215:CO0303-  
 09822- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09823- ROUTE PIPE -> 1. 02:MH0101 48.13 3.979 No\_date 28:02 46.72 n/a .000  
 09824- \* [L/n= .368, A/n= .540, C/n= .013]  
 09825- [Vmax= 3.34: Imax=.1.144]  
 09826- [Losses = 0.05: Dnus= 1.00]  
 09827- R0215:CO0304-  
 09828- ADD HYD 1. 02:MH0101 25.02 1.818 No\_date 27:54 49.64 n/a .000  
 09829- + 1. 02:MS\_P3 1.02:MH0101 25.02 1.818 No\_date 27:54 49.64 n/a .000  
 09830- + 1. 02:TODD 1.02:MH0101 25.02 1.818 No\_date 27:54 49.64 n/a .000  
 09831- SMM+ 1. 02:MH0101 25.02 1.818 No\_date 27:54 49.64 n/a .000  
 09832- [XING= 33.81: SMAX=225.43: SKO=.010]  
 09833- R0215:CO0305-  
 09834- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09835- COMPUTE DUALHYD 1. 01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09836- Major System / 1. 01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09837- [XING= 57.38: TIME= 1.01]  
 09838- R0215:CO0306-  
 09839- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09840- COMPUTE DUALHYD 1. 01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09841- Major System / 1. 01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09842- [XING= 33.81: SMAX=225.43: SKO=.010]  
 09843- R0215:CO0307-  
 09844- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09845- ADD HYD 1. 01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09846- + 1. 02:MS\_P3 1.01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09847- + 1. 02:TODD 1.01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09848- SMM+ 1. 02:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09849- [Vmax=.905,Imax=.3258]  
 09850- R0215:CO0308-  
 09851- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09852- CONTINUOUS STANDYD 1. 01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09853- [XING= 71:TIME= 71]  
 09854- R0215:CO0309-  
 09855- ADD HYD 1. 01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09856- + 1. 02:MS\_P3 1.01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09857- + 1. 02:TODD 1.01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09858- SMM+ 1. 02:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09859- [Vmax=.905,Imax=.3258]  
 09860- R0215:CO0310-  
 09861- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09862- COMPUTE DUALHYD 1. 01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09863- Major System / 1. 01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09864- [XING= 33.81: SMAX=225.43: SKO=.010]  
 09865- R0215:CO0311-  
 09866- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09867- COMPUTE DUALHYD 1. 01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09868- Major System / 1. 01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09869- [XING= 33.81: SMAX=225.43: SKO=.010]  
 09870- R0215:CO0312-  
 09871- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09872- COMPUTE DUALHYD 1. 01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09873- Major System / 1. 01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09874- [XING= 71:TIME= 71]  
 09875- R0215:CO0313-  
 09876- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09877- COMPUTE DUALHYD 1. 01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09878- Major System / 1. 01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09879- [XING= 33.81: SMAX=225.43: SKO=.010]  
 09880- R0215:CO0314-  
 09881- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09882- ADD HYD 1. 02:MS\_P3 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09883- + 1. 02:TODD 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09884- SMM+ 1. 02:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09885- [Vmax=.905,Imax=.3258]  
 09886- R0215:CO0315-  
 09887- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09888- COMPUTE DUALHYD 1. 01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09889- Major System / 1. 01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09890- [XING= 33.81: SMAX=225.43: SKO=.010]  
 09891- R0215:CO0316-  
 09892- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09893- COMPUTE DUALHYD 1. 01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09894- Major System / 1. 01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09895- [XING= 33.81: SMAX=225.43: SKO=.010]  
 09896- R0215:CO0317-  
 09897- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09898- COMPUTE DUALHYD 1. 01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09899- Major System / 1. 01:MH0102 73.63 5.771 No\_date 28:05 47.73 n/a .000  
 09900- [XING= 33.81: SMAX=225.43: SKO=.010]  
 09901- R0215:CO0318-  
 09902- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09903- CONTINUOUS STANDYD 1. 01:B2-MN 12.31 1.521 No\_date 28:02 49.75 .669 .000  
 09904- [Losses = 2 : CN= 75.0]  
 09905- R0215:CO0319-  
 09906- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09907- COMPUTE DUALHYD 1. 01:B2-MN 12.31 1.521 No\_date 28:02 49.75 .669 .000  
 09908- Major System / 1. 01:B2-MN 12.31 1.521 No\_date 28:02 49.75 .669 .000  
 09909- [XING= 33.81: SMAX=225.43: SKO=.010]  
 09910- R0215:CO0320-  
 09911- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09912- ROUTE PIPE -> 1. 02:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09913- [Previous area: Iaper: 4.67:SLPP=1.00:LGP= 40.:MNP=.250:SCP=.0]  
 09914- [Impervious area: Iaper: 1.57:SLP1=1.00:LGP= 345.:MNP=.013:SCI=.0]  
 09915- [Vmax= 1.22:Imax=.838]  
 09916- R0215:CO0321-  
 09917- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09918- CONTINUOUS STANDYD 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09919- [Previous area: Iaper: 4.67:SLPP=1.00:LGP= 40.:MNP=.250:SCP=.0]  
 09920- [Impervious area: Iaper: 1.57:SLP1=1.00:LGP= 345.:MNP=.013:SCI=.0]  
 09921- [Vmax= 1.22:Imax=.838]  
 09922- R0215:CO0322-  
 09923- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09924- COMPUTE DUALHYD 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09925- Major System / 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09926- [XING= 41:TIME= 25.43: SKO=.010]  
 09927- R0215:CO0323-  
 09928- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09929- COMPUTE DUALHYD 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09930- Major System / 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09931- [XING= 41:TIME= 25.43: SKO=.010]  
 09932- R0215:CO0324-  
 09933- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09934- COMPUTE DUALHYD 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09935- Major System / 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09936- [XING= 41:TIME= 25.43: SKO=.010]  
 09937- R0215:CO0325-  
 09938- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09939- COMPUTE DUALHYD 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09940- Major System / 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09941- [XING= 41:TIME= 25.43: SKO=.010]  
 09942- R0215:CO0326-  
 09943- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09944- COMPUTE DUALHYD 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09945- Major System / 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09946- [XING= 41:TIME= 25.43: SKO=.010]  
 09947- R0215:CO0327-  
 09948- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09949- COMPUTE DUALHYD 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09950- Major System / 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09951- [XING= 41:TIME= 25.43: SKO=.010]  
 09952- R0215:CO0328-  
 09953- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09954- COMPUTE DUALHYD 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09955- Major System / 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09956- [XING= 41:TIME= 25.43: SKO=.010]  
 09957- R0215:CO0329-  
 09958- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09959- COMPUTE DUALHYD 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09960- Major System / 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09961- [XING= 41:TIME= 25.43: SKO=.010]  
 09962- R0215:CO0330-  
 09963- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09964- COMPUTE DUALHYD 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09965- Major System / 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09966- [XING= 41:TIME= 25.43: SKO=.010]  
 09967- R0215:CO0331-  
 09968- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09969- COMPUTE DUALHYD 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09970- Major System / 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09971- [XING= 41:TIME= 25.43: SKO=.010]  
 09972- R0215:CO0332-  
 09973- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09974- COMPUTE DUALHYD 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09975- Major System / 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09976- [XING= 41:TIME= 25.43: SKO=.010]  
 09977- R0215:CO0333-  
 09978- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09979- COMPUTE DUALHYD 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09980- Major System / 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09981- [XING= 41:TIME= 25.43: SKO=.010]  
 09982- R0215:CO0334-  
 09983- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09984- COMPUTE DUALHYD 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09985- Major System / 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09986- [XING= 41:TIME= 25.43: SKO=.010]  
 09987- R0215:CO0335-  
 09988- Dtnin:ID:NHYD- ARRAha-QPEAKcms-Tpeakdate\_hh:mm-->RVm-R.C.--DWFcms  
 09989- COMPUTE DUALHYD 1. 01:B2-MN 12.31 1.0213 No\_date 27:55 49.85 .669 .000  
 09



10473+ Parameters for IMPERVIOUS surfaces in STANDHYD:  
 10474+ [IAImp= 1.0, em= 0.0, k= 1.50] [MN1= 013]  
 10475+ [IA= 0.0, k= 0.0, kmax= 0.0]  
 10476+ [Ia= 4.67 mm] [N= 3.00]  
 10477+ Average monthly Pan Evaporation data in (mm)  
 10478+ JUN FEB MAR MAY JUN JUL AUG SEP OCT NOV DEC  
 10479+ .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00  
 10480+ Average monthly Potential Evapotranspiration in (mm)  
 10481+ JUN FEB MAR MAY JUN JUL AUG SEP OCT NOV DEC  
 10482+ .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00  
 RO505:0005-----  
 10483+ COMPUTE API  
 10484+ [APIni= 50.00: APIEnd= .8500: APIKdr= .9999]  
 10485+ [APImax=13.33: APIavg= 67.14 APImin= 44.87]  
 10487+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 10488+ [CN= 61.0: N= 3.00: Tp= 3.76]  
 10489+ RO505:0006-----  
 10490+ CONTINUOUS NASHYD 1.0 01:JK\_HW 3680.00 18.440 No\_date 36:55 30.33 .372 .000  
 10491+ [IaREC= 4.00: SMIN= 37.05: SMAX=380.32: SK= .010]  
 10492+ [InterEventTime= 12.00]  
 10493+ [IaREC= 4.00: SMIN= 39.75: SMAX=380.32: SK= .010]  
 10494+ [InterEventTime= 12.00]  
 10495+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 10496+ [CN= 61.0: N= 3.00: Tp= 3.76]  
 10497+ RO505:0007-----  
 10498+ CONTINUOUS NASHYD 1.0 01:SW\_13 971.00 6.937 No\_date 32:34 28.27 .347 .000  
 10499+ [CN= 55.01: N= 3.00: Tp= 11.33]  
 10500+ [IaREC= 4.00: SMIN= 32.24: SMAX=544.96: SK= .010]  
 10501+ [InterEventTime= 12.00]  
 10502+ [InterEventTime= 12.00]  
 10503+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 10504+ of 1.80  
 10505+ RO505:0008-----  
 10506+ CONTINUOUS NASHYD 1.0 01:JK\_HW 3674.00 8.912 No\_date 39:59 24.31 .298 .000  
 10507+ [CN= 61.0: N= 3.00: Tp= 3.76]  
 10508+ [IaREC= 4.00: SMIN= 39.75: SMAX=284.99: SK= .010]  
 10509+ [InterEventTime= 12.00]  
 10510+ [IaREC= 4.00: SMIN= 39.75: SMAX=284.99: SK= .010]  
 10511+ RO505:0009-----  
 10512+ CONTINUOUS NASHYD 1.0 01:JK\_HW 1781.00 16.834 No\_date 32:39 36.85 .452 .000  
 10513+ [CN= 61.0: N= 3.00: Tp= 3.76]  
 10514+ [IaREC= 4.00: SMIN= 39.75: SMAX=284.99: SK= .010]  
 10515+ [InterEventTime= 12.00]  
 10516+ [IaREC= 4.00: SMIN= 39.75: SMAX=284.99: SK= .010]  
 10517+ [InterEventTime= 12.00]  
 10518+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 10519+ [CN= 61.0: N= 3.00: Tp= 3.76]  
 10520+ RO505:0010-----  
 10521+ CONTINUOUS NASHYD 1.0 01:JK\_HW 500.00 9.061 No\_date 29:21 31.73 .389 .000  
 10522+ [CN= 66.0: N= 3.00: Tp= 2.24]  
 10523+ [IaREC= 4.00: SMIN= 39.75: SMAX=350.79: SK= .010]  
 10524+ [InterEventTime= 12.00]  
 10525+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 10526+ of 1.80  
 10527+ RO505:0011-----  
 10528+ CONTINUOUS NASHYD 1.0 01:NC\_NCK 1917.00 12.342 No\_date 34:26 31.73 .389 .000  
 10529+ [CN= 66.0: N= 3.00: Tp= 5.29]  
 10530+ [IaREC= 4.00: SMIN= 52.62: SMAX=350.79: SK= .010]  
 10531+ [InterEventTime= 12.00]  
 10532+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 10533+ of 1.80  
 10534+ RO505:0012-----  
 10535+ CONTINUOUS NASHYD 1.0 01:NC\_NCK 5668.00 32.402 No\_date 37:52 36.85 .452 .000  
 10536+ [CN= 72.0: N= 3.00: Tp= 8.00]  
 10537+ [IaREC= 4.00: SMIN= 39.75: SMAX=284.99: SK= .010]  
 10538+ [InterEventTime= 12.00]  
 10539+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 10540+ of 1.80  
 10541+ RO505:0013-----  
 10542+ CONTINUOUS NASHYD 1.0 01:JK\_CK 8376.00 31.024 No\_date 39:59 31.73 .389 .000  
 10543+ [CN= 70.0: N= 3.00: Tp= 2.51]  
 10544+ [IaREC= 4.00: SMIN= 39.75: SMAX=287.10: SK= .010]  
 10545+ [InterEventTime= 12.00]  
 10546+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 10547+ of 1.80  
 10548+ RO505:0014-----  
 10549+ CONTINUOUS NASHYD 1.0 01:JK\_CK 4464.00 15.472 No\_date 39:59 28.95 .355 .000  
 10550+ [CN= 62.0: N= 3.00: Tp= 11.33]  
 10551+ [IaREC= 4.00: SMIN= 61.90: SMAX=412.66: SK= .010]  
 10552+ [InterEventTime= 12.00]  
 10553+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 10554+ of 1.80  
 10555+ RO505:0015-----  
 10556+ CONTINUOUS NASHYD 1.0 01:JK\_CK 131.00 2.740 No\_date 28:57 29.64 .364 .000  
 10557+ [CN= 63.0: N= 3.00: Tp= 1.00]  
 10558+ [IaREC= 4.00: SMIN= 59.42: SMAX=396.11: SK= .010]  
 10559+ [InterEventTime= 12.00]  
 10560+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 10561+ of 1.80  
 10562+ RO505:0016-----  
 10563+ CONTINUOUS NASHYD 1.0 01:JK\_CK 131.00 1.285 No\_date 33:02 32.44 .398 .000  
 10564+ [CN= 67.0: N= 3.00: Tp= 4.18]  
 10565+ [IaREC= 4.00: SMIN= 50.55: SMAX=336.37: SK= .010]  
 10566+ [InterEventTime= 12.00]  
 10567+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 10568+ of 1.75  
 10569+ RO505:0017-----  
 10570+ CONTINUOUS NASHYD 1.0 01:JK\_CK 3197.00 13.937 No\_date 36:23 25.61 .314 .000  
 10571+ [CN= 57.0: N= 3.00: Tp= 6.65]  
 10572+ [IaREC= 4.00: SMIN= 39.75: SMAX=284.99: SK= .010]  
 10573+ [InterEventTime= 12.00]  
 10574+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 10575+ of 1.75  
 10576+ RO505:0018-----  
 10577+ CONTINUOUS NASHYD 1.0 01:JK\_CK 3854.00 18.180 No\_date 38:32 31.73 .389 .000  
 10578+ [CN= 70.0: N= 3.00: Tp= 4.41]  
 10579+ [IaREC= 4.00: SMIN= 52.62: SMAX=350.79: SK= .010]  
 10580+ [InterEventTime= 12.00]  
 10581+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 10582+ of 1.75  
 10583+ RO505:0019-----  
 10584+ CONTINUOUS NASHYD 1.0 01:JK\_CK 224.00 8.187 No\_date 28:45 41.51 .509 .000  
 10585+ [CN= 67.0: N= 3.00: Tp= 7.57]  
 10586+ [IaREC= 4.00: SMIN= 50.55: SMAX=207.66: SK= .010]  
 10587+ [InterEventTime= 12.00]  
 10588+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 10589+ of 1.75  
 10590+ RO505:0020-----  
 10591+ CONTINUOUS NASHYD 1.0 01:JK\_CK 3197.00 9.332 No\_date 35:12 36.85 .452 .000  
 10592+ [CN= 57.0: N= 3.00: Tp= 6.65]  
 10593+ [IaREC= 4.00: SMIN= 39.75: SMAX=284.99: SK= .010]  
 10594+ [InterEventTime= 12.00]  
 10595+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 10596+ of 1.75  
 10597+ RO505:0021-----  
 10598+ CONTINUOUS NASHYD 1.0 01:JK\_CK 132.00 9.332 No\_date 35:12 36.85 .452 .000  
 10599+ [CN= 67.0: N= 3.00: Tp= 6.65]  
 10600+ [IaREC= 4.00: SMIN= 39.75: SMAX=284.99: SK= .010]  
 10601+ [InterEventTime= 12.00]  
 10602+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 10603+ of 1.75  
 10604+ RO505:0022-----  
 10605+ CONTINUOUS NASHYD 1.0 01:JK\_CK 4945.00 44.623 No\_date 33:18 38.37 .473 .000  
 10606+ [CN= 74.0: N= 3.00: Tp= 4.45]  
 10607+ [IaREC= 4.00: SMIN= 44.62: SMAX=244.49: SK= .010]  
 10608+ [InterEventTime= 12.00]  
 10609+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 10610+ of 1.75  
 10611+ RO505:0023-----  
 10612+ CONTINUOUS NASHYD 1.0 01:JK\_CK 4945.00 20.00 0.943 No\_date 28:35 45.60 .560 .000  
 10613+ [CN= 81.0: N= 3.00: Tp= 6.61]  
 10614+ [IaREC= 4.00: SMIN= 25.21: SMAX=168.09: SK= .010]  
 10615+ [InterEventTime= 12.00]  
 10616+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 10617+ of 1.75  
 10618+ RO505:0024-----  
 10619+ CONTINUOUS NASHYD 1.0 01:JK\_CK 585.00 12.896 No\_date 29:55 45.60 .560 .000  
 10620+ [CN= 81.0: N= 3.00: Tp= 7.57]  
 10621+ [IaREC= 4.00: SMIN= 33.81: SMAX=225.43: SK= .010]  
 10622+ [InterEventTime= 12.00]  
 10623+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 10624+ of 1.75  
 10625+ RO505:0025-----  
 10626+ CONTINUOUS NASHYD 1.0 01:JK\_CK 1021.00 17.059 No\_date 30:46 44.77 .549 .000  
 10627+ [CN= 80.0: N= 3.00: Tp= 2.46]  
 10628+ [IaREC= 4.00: SMIN= 26.12: SMAX=175.50: SK= .010]  
 10629+ [InterEventTime= 12.00]  
 10630+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 10631+ of 1.75  
 10632+ RO505:0026-----  
 10633+ CONTINUOUS NASHYD 1.0 01:JK\_CK 177.00 6.469 No\_date 28:45 41.51 .509 .000  
 10634+ [CN= 71.0: N= 3.00: Tp= 1.00]  
 10635+ [IaREC= 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]  
 10636+ [InterEventTime= 12.00]  
 10637+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
 10638+ of 1.75  
 10639+ RO505:0027-----  
 10640+ CONTINUOUS NASHYD 1.0 01:JK\_CK 2373.00 34.946 No\_date 31:29 40.72 .500 .000  
 10641+ [CN= 76.0: N= 3.00: Tp= 3.03]  
 10642+ [IaREC= 4.00: SMIN= 44.62: SMAX=216.39: SK= .010]  
 10643+ [InterEventTime= 12.00]  
 10644+ # Routing hydrographs  
 10645+ # Starting with the addition of Rock River Headwater and Subwatershed 13  
 10646+ ADD HYD  
 10647+ RO505:0028-----  
 10648+ ADD HYD  
 10649+ ADD HYD  
 10650+ ADD HYD  
 10651+ ADD HYD  
 10652+ ADD HYD  
 10653+ ADD HYD  
 10654+ ADD HYD  
 10655+ ADD HYD  
 10656+ ADD HYD  
 10657+ RO505:0029-----  
 10658+ ADD HYD  
 10659+ ADD HYD

10660+ SUM# 1.0 01:SW\_N13 4651.00 23.559 No\_date 35:24 29.90 n/a .000  
 10661+ E  
 10662+ # Sum of hydrographs from Node 13 routed to Node 13A  
 10663+ # (Approximated cross-section - see cross-section 258)  
 10664+ ADD HYD  
 10665+ ROUTE CHANNEL > 1.0 02:IN13A 4651.00 19.136 No\_date 39:06 29.90 n/a .000  
 10666+ RO505:0030-----  
 10667+ ADD HYD  
 10668+ OUTLET > 1.0 01:IN13A 4651.00 18.856 No\_date 39:06 29.90 n/a .000  
 10669+ [L/n= 9074 ./ .022 .040]  
 10670+ [Vmax= .574 Dmax= 3.920]  
 10671+ # Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A  
 10672+ # Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A  
 10673+ ADD HYD  
 10674+ RO505:0032-----  
 10675+ ADD HYD  
 10676+ ROUTE CHANNEL > 1.0 02:IN13A 725.00 21.519 No\_date 34:19 27.68 n/a .000  
 10677+ SUM# out < 1.0 02:IN13A 725.00 21.519 No\_date 61:35 27.67 n/a .000  
 10678+ # Insertion of a reservoir to simulate the effects of the Goodwood Marsh  
 10679+ ADD HYD  
 10680+ RO505:0033-----  
 10681+ ADD HYD  
 10682+ ROUTE CHANNEL > 1.0 02:IN13A 725.00 21.519 No\_date 34:19 27.68 n/a .000  
 10683+ OUTLET > 1.0 01:IN13A 725.00 18.857 No\_date 61:35 27.67 n/a .000  
 10684+ [MGSCode= 1.4818e-03 m3]  
 10685+ # Addition of Subwatershed Jock River at Ashton to Node 12  
 10686+ RO505:0034-----  
 10687+ ADD HYD  
 10688+ OUTLET > 1.0 02:IN13A 725.00 18.857 No\_date 61:35 27.67 n/a .000  
 10689+ [L/n= 1.926 ./ .036 .040]  
 10690+ [ROUTE CHANNEL > 1.0 02:IN13A 725.00 18.857 No\_date 61:35 27.67 n/a .000]  
 10691+ [ROUTE 1.00 out< 1.0 01:IN12A 725.00 18.857 No\_date 61:35 27.67 n/a .000  
 10692+ # Use n=0.04 for summer conditions and n=0.025 for spring conditions  
 10693+ ADD HYD  
 10694+ RO505:0035-----  
 10695+ ADD HYD  
 10696+ OUTLET > 1.0 02:IN12A 9506.00 18.867 No\_date 32:42 29.99 n/a .000  
 10697+ [L/n= 927 ./ .034 .040]  
 10698+ [Vmax= .556 Dmax= 1.541]  
 10699+ # Addition of Subwatershed Jock River at Ashton to Node 12  
 10700+ ADD HYD  
 10701+ RO505:0036-----  
 10702+ ADD HYD  
 10703+ ADD HYD  
 10704+ OUTLET > 1.0 01:IN12A 9506.00 18.867 No\_date 32:42 29.99 n/a .000  
 10705+ # Addition of Subwatershed 11 and No Name Creek to Node 11  
 10706+ ADD HYD  
 10707+ RO505:0037-----  
 10708+ ADD HYD  
 10709+ # Sum of hydrographs from Node 12 routed to Node 11  
 10710+ # (Approximated cross-section - see cross-section 258)  
 10711+ # Use n=0.04 for summer conditions and n=0.025 for spring conditions  
 10712+ # Addition of Subwatershed 11 and No Name Creek to Node 11  
 10713+ # Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248  
 10714+ ADD HYD  
 10715+ RO505:0038-----  
 10716+ ADD HYD  
 10717+ RO505:0039-----  
 10718+ ADD HYD  
 10719+ RO505:0040-----  
 10720+ ADD HYD  
 10721+ ADD HYD  
 10722+ # Addition of Subwatershed 11 and No Name Creek to Node 11  
 10723+ ADD HYD  
 10724+ RO505:0041-----  
 10725+ ADD HYD  
 10726+ ADD HYD  
 10727+ ADD HYD  
 10728+ ADD HYD  
 10729+ ADD HYD  
 10730+ # Sum of hydrographs from Node 11 routed to Node 10  
 10731+ # Section 1  
 10732+ ADD HYD  
 10733+ RO505:0040-----  
 10734+ ADD HYD  
 10735+ ADD HYD  
 10736+ ADD HYD  
 10737+ ADD HYD  
 10738+ ADD HYD  
 10739+ # Addition of Subwatershed 11 and No Name Creek to Node 10  
 10740+ ADD HYD  
 10741+ RO505:0041-----  
 10742+ ADD HYD  
 10743+ ADD HYD  
 10744+ ADD HYD  
 10745+ ADD HYD  
 10746+ ADD HYD  
 10747+ ADD HYD  
 10748+ ADD HYD  
 10749+ ADD HYD  
 10750+ # Addition of King's Creek to S\_N10  
 10751+ RO505:0042-----  
 10752+ ADD HYD  
 10753+ ADD HYD  
 10754+ ADD HYD  
 10755+ ADD HYD  
 10756+ ADD HYD  
 10757+ ADD HYD  
 10758+ # Sum of hydrographs from Node 10 routed to Node 9  
 10759+ # Section 2  
 10760+ ADD HYD  
 10761+ RO505:0044-----  
 10762+ ROUTE CHANNEL > 1.0 02:IN12\_N11 11923.00 32.851 No\_date 33:00 29.87 n/a .000  
 10763+ [ROUTE 1.00 out< 1.0 01:IN12\_N11 11923.00 20.490 No\_date 40:02 29.87 n/a .000  
 10764+ [ROUTE CHANNEL > 1.0 02:IN12\_N11 11923.00 32.851 No\_date 33:00 29.87 n/a .000  
 10765+ # Addition of Subwatershed 10 and Dummy section 248  
 10766+ ADD HYD  
 10767+ RO505:0045-----  
 10768+ ADD HYD  
 10769+ ADD HYD  
 10770+ ADD HYD  
 10771+ ADD HYD  
 10772+ ADD HYD  
 10773+ # Sum of hydrographs from Node 9 routed to Node 8  
 10774+ # Section 3  
 10775+ ADD HYD  
 10776+ RO505:0046-----  
 10777+ ADD HYD  
 10778+ ADD HYD  
 10779+ ADD HYD  
 10780+ ADD HYD  
 10781+ ADD HYD  
 10782+ ADD HYD  
 10783+ ADD HYD  
 10784+ ADD HYD  
 10785+ ADD HYD  
 10786+ ADD HYD  
 10787+ ADD HYD  
 10788+ ADD HYD  
 10789+ # Addition of Subwatershed 9 and Nichols Creek to Node 9  
 10790+ ADD HYD  
 10791+ RO505:0047-----  
 10792+ ADD HYD  
 10793+ ADD HYD  
 10794+ ADD HYD  
 10795+ ADD HYD  
 10796+ ADD HYD  
 10797+ ADD HYD  
 10798+ ADD HYD  
 10799+ ADD HYD  
 10800+ ADD HYD  
 10801+ RO505:0049-----  
 10802+ ADD HYD  
 10803+ ADD HYD  
 10804+ ADD HYD  
 10805+ ADD HYD  
 10806+ ADD HYD  
 10807+ ADD HYD  
 10808+ ADD HYD  
 10809+ ADD HYD  
 10810+ ADD HYD  
 10811+ ADD HYD  
 10812+ ADD HYD  
 10813+ ADD HYD  
 10814+ ADD HYD  
 10815+ ADD HYD  
 10816+ RO505:0051-----  
 10817+ ADD HYD  
 10818+ ADD HYD  
 10819+ ADD HYD  
 10820+ ADD HYD  
 10821+ ADD HYD  
 10822+ ADD HYD  
 10823+ ADD HYD  
 10824+ ADD HYD  
 10825+ ADD HYD  
 10826+ ADD HYD  
 10827+ RO505:0052-----  
 10828+ ADD HYD  
 10829+ ADD HYD  
 10830+ ADD HYD  
 10831+ ADD HYD  
 10832+ ADD HYD  
 10833+ ADD HYD  
 10834+ ADD HYD  
 10835+ ADD HYD  
 10836+ RO505:0054-----  
 10837+ ADD HYD  
 10838+ ADD HYD  
 10839+ ADD HYD  
 10840+ ADD HYD  
 10841+ ADD HYD  
 10842+ ADD HYD  
 10843+ ADD HYD  
 10844+ ADD HYD  
 10845+ ADD HYD  
 10846+ ADD HYD



11221+ R0505:CO011----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
CONTINUOUS STANDYD 1.0 01:STRAND 7.59 1.038 No\_date 28:09 62.95 .772 .000  
11222+ [XMP= 64:TIME\_4S]-----  
11223+ [Horton parameters: Fo= 76.20FC= 13.20DCN4\*14: Fc=.00]  
11224+ [Previous areas: Taper: 4.67SLPP= 50:LDPG= 40:NHWD= 250:SCP= .01]  
11225+ [Impervious areas: Taper: 1.57SLPP= 50:LDPG= 50:NHWD= 120:SCP= .01]  
11226+ [iabEClipm= 4.00: iabRcp= 4.00]  
11227+ [MacStCaled= 84940+m3, TctovfVol= 0.00000+m3, N-Ofr= 0, TotBurrfv= 0, hrs]  
11228+ ROUTE RESERVOIR > 1.0 02:STANDYD 1.53 1.038 No\_date 28:09 62.95 n/a .000  
11229+ out < 1.0 01:S-POND 7.59 .137 No\_date 29:13 62.95 n/a .000  
11230+ overlwp < 1.0 01:S-POND 7.59 .137 No\_date 29:13 62.95 n/a .000  
11231+ [MacStCaled= 1158900 m3, TctovfVol= 0.00000 m3, N-Ofr= 0, TotBurrfv= 0, hrs]  
11232+ ADD HYD 1.0 01:HYD 1.53 1.038 No\_date 28:09 62.95 n/a .000  
11233+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11234+ [XMP= 64:TIME\_80]-----  
11235+ [Horton parameters: Fo= 76.20FC= 13.20DCN4\*14: Fc=.00]  
11236+ [Previous areas: Taper: 4.67SLPP= 50:LDPG= 40:NHWD= 250:SCP= .01]  
11237+ [Impervious areas: Taper: 1.57SLPP= 50:LDPG= 50:NHWD= 120:SCP= .01]  
11238+ [iabEClipm= 4.00: iabRcp= 4.00]  
11239+ SAVE HYD 1.0 01:SSA007 364.27 6.711 No\_date 28:09 31.19 n/a .000  
11240+ remark// SSA007.0050  
11241+ remark//  
11242+ R0505:CO0117----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
CONTINUOUS STANDYD 1.0 01:Area-A 66.75 8.917 No\_date 28:08 61.83 .759 .000  
11243+ [XMP= 64:TIME\_80]-----  
11244+ [Horton parameters: Fo= 76.20FC= 13.20DCN4\*14: Fc=.00]  
11245+ [Previous areas: Taper: 4.67SLPP= 50:LDPG= 40:NHWD= 250:SCP= .01]  
11246+ [Impervious areas: Taper: 1.57SLPP= 50:LDPG= 50:NHWD= 120:SCP= .01]  
11247+ [iabEClipm= 4.00: iabRcp= 4.00]  
11248+ R0505:CO0116----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11249+ CONTINUOUS STANDYD 1.0 01:Area-A 66.75 8.917 No\_date 28:08 61.83 n/a .000  
11250+ SAVE HYD 1.0 01:Area-A 66.75 8.917 No\_date 28:08 61.83 n/a .000  
11251+ frame: Area\_A.04.050  
11252+ frame: Area\_A.050  
11253+ R0505:CO0119----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11254+ ROUTE RESERVOIR > 1.0 02:Area-A 66.75 8.917 No\_date 28:08 61.83 n/a .000  
11255+ out < 1.0 01:S-POUN 66.75 .000 No\_date 28:08 61.83 n/a .000  
11256+ overlwp < 1.0 01:S-POUN 66.75 .000 No\_date 28:08 61.83 n/a .000  
11257+ [MacStCaled= 204540+m3, TctovfVol= 0.00000+m3, N-Ofr= 0, TotBurrfv= 0, hrs]  
11258+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11259+ SAVE HYD 1.0 01:SSM007-A 66.75 1.070 No\_date 29:16 61.83 n/a .000  
11260+ frame: SMMF\_A.050  
11261+ frame: SMMF\_A.050  
11262+ R0505:CO0211----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11263+ ADD HYD 1.0 02:SSA007-A 66.75 6.711 No\_date 28:08 61.83 n/a .000  
11264+ [XMP= 64:TIME\_80]-----  
11265+ overlwp < 1.0 01:S-POUN 66.75 .000 No\_date 28:08 61.83 n/a .000  
11266+ SUM 1.0 02:SSM007-A .000 No\_date 28:08 61.83 n/a .000  
11267+ R0505:CO0212----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11268+ CONTINUOUS STANDYD 1.0 01:ICE 1.87 .395 No\_date 28:01 64.42 .790 .000  
11269+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11270+ ADD HYD 1.0 02:SSA007-A 66.75 6.711 No\_date 28:01 64.42 n/a .000  
11271+ [XMP= 64:TIME\_80]-----  
11272+ [Previous areas: Taper: 4.67SLPP= 50:LDPG= 40:NHWD= 250:SCP= .01]  
11273+ [Impervious areas: Taper: 1.57SLPP= 50:LDPG= 50:NHWD= 120:SCP= .01]  
11274+ [iabEClipm= 4.00: iabRcp= 4.00]  
11275+ ROUTE RESERVOIR > 1.0 01:ICE-NHYD 1.87 .395 No\_date 28:01 64.42 n/a .000  
11276+ out < 1.0 01:ICE-NHYD 1.87 .110 No\_date 28:18 64.42 n/a .000  
11277+ overlwp < 1.0 03:CE-OVW .000 No\_date 28:18 64.42 n/a .000  
11278+ [MacStCaled= 545240+m3, TctovfVol= 0.00000+m3, N-Ofr= 0, TotBurrfv= 0, hrs]  
11279+ R0505:CO0214----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11280+ CONTINUOUS STANDYD 1.0 01:ICE 1.62 .347 No\_date 28:00 64.42 .790 .000  
11281+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11282+ [Horton parameters: Fo= 76.20FC= 13.20DCN4\*14: Fc=.00]  
11283+ [Previous areas: Taper: 4.67SLPP= 50:LDPG= 40:NHWD= 250:SCP= .01]  
11284+ [Impervious areas: Taper: 1.57SLPP= 50:LDPG= 50:NHWD= 120:SCP= .01]  
11285+ [iabEClipm= 4.00: iabRcp= 4.00]  
11286+ R0505:CO0215----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11287+ ROUTE RESERVOIR > 1.0 01:ICE-NHYD 1.62 .347 No\_date 28:00 64.42 n/a .000  
11288+ out < 1.0 01:ICE-NHYD 1.62 .096 No\_date 28:17 64.42 n/a .000  
11289+ overlwp < 1.0 03:ICE-OVW .000 No\_date 28:17 64.42 n/a .000  
11290+ [MacStCaled= 545240+m3, TctovfVol= 0.00000+m3, N-Ofr= 0, TotBurrfv= 0, hrs]  
11291+ R0505:CO0216----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11292+ CONTINUOUS STANDYD 1.0 01:IST 676 .073 No\_date 28:00 50.67 .622 .000  
11293+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11294+ [Horton parameters: Fo= 76.20FC= 13.20DCN4\*14: Fc=.00]  
11295+ [Previous areas: Taper: 4.67SLPP= 50:LDPG= 40:NHWD= 250:SCP= .01]  
11296+ [Impervious areas: Taper: 1.57SLPP= 50:LDPG= 50:NHWD= 120:SCP= .01]  
11297+ [iabEClipm= 4.00: iabRcp= 4.00]  
11298+ R0505:CO0217----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11299+ ROUTE RESERVOIR > 1.0 01:ICE-NHYD 1.62 .347 No\_date 28:00 50.67 n/a .000  
11300+ out < 1.0 01:ICE-NHYD 1.62 .096 No\_date 28:10 50.67 n/a .000  
11301+ overlwp < 1.0 03:ICE-OVW .000 No\_date 28:10 50.67 n/a .000  
11302+ [MacStCaled= 545240+m3, TctovfVol= 0.00000+m3, N-Ofr= 0, TotBurrfv= 0, hrs]  
11303+ R0505:CO0218----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11304+ ADD HYD 1.0 02:PT49TS 431.02 7.776 No\_date 29:10 35.93 n/a .000  
11305+ [XMP= 64:TIME\_80]-----  
11306+ overlwp < 1.0 02:PT49TS .000 No\_date 29:10 35.93 n/a .000  
11307+ 1.0 02:CT2-STR 1.62 .096 No\_date 28:17 64.42 n/a .000  
11308+ 1.0 02:CT2-STR 1.62 .096 No\_date 28:17 64.42 n/a .000  
11309+ 1.0 02:ST67ST 41 .021 No\_date 28:10 50.67 n/a .000  
11310+ 1.0 02:ST67ST 41 .021 No\_date 28:10 50.67 n/a .000  
11311+ SUM 1.0 02:ST67ST 43.92 7.904 No\_date 28:19 36.17 n/a .000  
11312+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11313+ ROUTE CHANNEL >> 1.0 02:PT58TS 43.92 7.904 No\_date 28:19 36.17 n/a .000  
11314+ [BOT= 1.0] out < 1.0 02:PT58TS 43.92 7.904 No\_date 28:20 36.17 n/a .000  
11315+ [L/nr= 160/.../003]-----  
11316+ [Wmax= .499:Imax= 1.531]  
11317+ R0505:CO0219----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11318+ CONTINUOUS STANDYD 1.0 01:ID 1.73 .097 No\_date 28:34 50.14 .615 .000  
11319+ [XMP= 64:TIME\_80]-----  
11320+ [InterEventTime: 12.00]  
11321+ R0505:CO0220----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11322+ CONTINUOUS STANDYD 1.0 01:Area-B 24.04 4.418 No\_date 28:02 60.51 .742 .000  
11323+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11324+ [XMP= 64:TIME\_77]-----  
11325+ [Horton parameters: Fo= 76.20FC= 13.20DCN4\*14: Fc=.00]  
11326+ [Previous areas: Taper: 4.67SLPP= 50:LDPG= 40:NHWD= 250:SCP= .01]  
11327+ [Impervious areas: Taper: 1.57SLPP= 50:LDPG= 50:NHWD= 120:SCP= .01]  
11328+ [iabEClipm= 4.00: iabRcp= 4.00]  
11329+ R0505:CO0227----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11330+ CONTINUOUS STANDYD 1.0 01:Area-B 24.04 4.418 No\_date 28:02 60.51 .742 .000  
11331+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11332+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11333+ ROUTE CHANNEL > 1.0 02:CE-NHYD 24.04 4.418 No\_date 28:02 60.51 .742 .000  
11334+ out < 1.0 02:CE-NHYD 24.04 4.418 No\_date 28:17 60.51 .742 .000  
11335+ overlwp < 1.0 02:CE-NHYD 24.04 4.418 No\_date 28:17 60.51 .742 .000  
11336+ ADD HYD 1.0 02:CE-NHYD 24.04 4.418 No\_date 28:17 60.51 .742 .000  
11337+ + 1.0 02:CE-NHYD 24.04 4.418 No\_date 28:17 60.51 .742 .000  
11338+ SUM 1.0 02:CE-NHYD 24.04 4.418 No\_date 28:17 60.51 .742 .000  
11339+ R0505:CO0234----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11340+ [XMP= 64:TIME\_80]-----  
11341+ [InterEventTime: 12.00]  
11342+ R0505:CO0235----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11343+ CONTINUOUS STANDYD 1.0 01:Area-B 9.74 .578 No\_date 28:21 44.42 .545 .000  
11344+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11345+ CONTINUOUS STANDYD 1.0 01:Area-B 9.74 .578 No\_date 28:21 44.42 .545 .000  
11346+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11347+ [CN= 86.01 N 3.00 P= .691]  
11348+ [iabEClipm= 4.00: iabRcp= 4.00]  
11349+ R0505:CO0236----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11350+ CONTINUOUS STANDYD 1.0 01:Area-B 9.74 .578 No\_date 28:20 44.42 .545 .000  
11351+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11352+ [CN= 81.01 N 3.00 P= .431]  
11353+ [iabEClipm= 4.00: iabRcp= 4.00]  
11354+ R0505:CO0237----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11355+ CONTINUOUS STANDYD 1.0 01:Area-B 9.74 .578 No\_date 28:21 44.42 .545 .000  
11356+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11357+ [CN= 86.01 N 3.00 P= .431]  
11358+ [iabEClipm= 4.00: iabRcp= 4.00]  
11359+ R0505:CO0238----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11360+ CONTINUOUS STANDYD 1.0 01:Area-B 9.74 .578 No\_date 28:20 44.42 .545 .000  
11361+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11362+ [CN= 82.01 N 3.00 P= .341]  
11363+ [iabEClipm= 4.00: iabRcp= 4.00]  
11364+ R0505:CO0239----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11365+ CONTINUOUS STANDYD 1.0 01:Area-B 9.74 .578 No\_date 28:21 44.42 .545 .000  
11366+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11367+ [CN= 82.01 N 3.00 P= .341]  
11368+ [iabEClipm= 4.00: iabRcp= 4.00]  
11369+ R0505:CO0240----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11370+ CONTINUOUS STANDYD 1.0 01:Area-B 9.74 .578 No\_date 28:21 44.42 .545 .000  
11371+ ADD HYD 1.0 02:PT60 47.33 8.151 No\_date 29:27 37.68 n/a .000  
11372+ [XMP= 64:TIME\_80]-----  
11373+ overlwp < 1.0 02:PT60 47.33 8.151 No\_date 29:27 37.68 n/a .000  
11374+ SUM 1.0 01:M-C 483.00 8.151 No\_date 29:27 36.78 n/a .000  
11375+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11376+ [CN= 86.01 N 3.00 P= .120]  
11377+ [iabEClipm= 4.00: iabRcp= 4.00]  
11378+ R0505:CO0241----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11379+ CONTINUOUS STANDYD 1.0 01:Area-B 5.00 .616 No\_date 28:04 43.28 .531 .000  
11380+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11381+ [CN= 86.01 N 3.00 P= .120]  
11382+ [iabEClipm= 4.00: iabRcp= 4.00]  
11383+ R0505:CO0242----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11384+ CONTINUOUS STANDYD 1.0 01:Area-B 5.00 .616 No\_date 28:04 43.28 .531 .000  
11385+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11386+ [CN= 86.01 N 3.00 P= .120]  
11387+ [iabEClipm= 4.00: iabRcp= 4.00]  
11388+ R0505:CO0243----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11389+ CONTINUOUS STANDYD 1.0 01:Area-B 5.00 .616 No\_date 28:04 43.28 .531 .000  
11390+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11391+ [CN= 86.01 N 3.00 P= .120]  
11392+ [iabEClipm= 4.00: iabRcp= 4.00]  
11393+ R0505:CO0244----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11394+ CONTINUOUS STANDYD 1.0 01:S-1-D 6.79 .161 No\_date 29:23 39.91 .490 .000  
11395+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11396+ [CN= 77.01 N 3.00 P= .028]  
11397+ [iabEClipm= 4.00: iabRcp= 4.00]  
11398+ R0505:CO0245----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11399+ CONTINUOUS STANDYD 1.0 01:S-1-D 6.79 .161 No\_date 29:23 39.91 .490 .000  
11400+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11401+ [CN= 77.01 N 3.00 P= .028]  
11402+ [iabEClipm= 4.00: iabRcp= 4.00]  
11403+ R0505:CO0246----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11404+ CONTINUOUS STANDYD 1.0 01:S-1-D 6.79 .161 No\_date 29:23 39.91 .490 .000  
11405+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11406+ [CN= 77.01 N 3.00 P= .028]  
11407+ [iabEClipm= 4.00: iabRcp= 4.00]  
11408+ R0505:CO0247----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11409+ CONTINUOUS STANDYD 1.0 01:S-1-D 6.79 .161 No\_date 29:23 39.91 .490 .000  
11410+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11411+ [CN= 77.01 N 3.00 P= .028]  
11412+ [iabEClipm= 4.00: iabRcp= 4.00]  
11413+ R0505:CO0248----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11414+ CONTINUOUS STANDYD 1.0 01:S-1-D 6.79 .161 No\_date 29:23 39.91 .490 .000  
11415+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11416+ [CN= 77.01 N 3.00 P= .028]  
11417+ [iabEClipm= 4.00: iabRcp= 4.00]  
11418+ R0505:CO0249----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11419+ CONTINUOUS STANDYD 1.0 01:S-1-D 6.79 .161 No\_date 29:23 39.91 .490 .000  
11420+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11421+ [CN= 77.01 N 3.00 P= .028]  
11422+ [iabEClipm= 4.00: iabRcp= 4.00]  
11423+ R0505:CO0250----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11424+ CONTINUOUS STANDYD 1.0 01:S-1-D 6.79 .161 No\_date 29:23 39.91 .490 .000  
11425+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11426+ [CN= 77.01 N 3.00 P= .028]  
11427+ [iabEClipm= 4.00: iabRcp= 4.00]  
11428+ R0505:CO0251----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11429+ CONTINUOUS STANDYD 1.0 01:S-1-D 6.79 .161 No\_date 29:23 39.91 .490 .000  
11430+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11431+ [CN= 77.01 N 3.00 P= .028]  
11432+ [iabEClipm= 4.00: iabRcp= 4.00]  
11433+ R0505:CO0252----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11434+ CONTINUOUS STANDYD 1.0 01:S-1-D 6.79 .161 No\_date 29:23 39.91 .490 .000  
11435+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11436+ [CN= 77.01 N 3.00 P= .028]  
11437+ [iabEClipm= 4.00: iabRcp= 4.00]  
11438+ R0505:CO0253----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11439+ CONTINUOUS STANDYD 1.0 01:S-1-D 6.79 .161 No\_date 29:23 39.91 .490 .000  
11440+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11441+ [CN= 77.01 N 3.00 P= .028]  
11442+ [iabEClipm= 4.00: iabRcp= 4.00]  
11443+ R0505:CO0254----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11444+ CONTINUOUS STANDYD 1.0 01:S-1-D 6.79 .161 No\_date 29:23 39.91 .490 .000  
11445+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11446+ [CN= 77.01 N 3.00 P= .028]  
11447+ [iabEClipm= 4.00: iabRcp= 4.00]  
11448+ R0505:CO0255----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11449+ CONTINUOUS STANDYD 1.0 01:S-1-D 6.79 .161 No\_date 29:23 39.91 .490 .000  
11450+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11451+ [CN= 77.01 N 3.00 P= .028]  
11452+ [iabEClipm= 4.00: iabRcp= 4.00]  
11453+ R0505:CO0256----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11454+ CONTINUOUS STANDYD 1.0 01:S-1-D 6.79 .161 No\_date 29:23 39.91 .490 .000  
11455+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11456+ [CN= 77.01 N 3.00 P= .028]  
11457+ [iabEClipm= 4.00: iabRcp= 4.00]  
11458+ R0505:CO0257----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11459+ CONTINUOUS STANDYD 1.0 01:S-1-D 6.79 .161 No\_date 29:23 39.91 .490 .000  
11460+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11461+ [CN= 77.01 N 3.00 P= .028]  
11462+ [iabEClipm= 4.00: iabRcp= 4.00]  
11463+ R0505:CO0258----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11464+ CONTINUOUS STANDYD 1.0 01:S-1-D 6.79 .161 No\_date 29:23 39.91 .490 .000  
11465+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11466+ [CN= 77.01 N 3.00 P= .028]  
11467+ [iabEClipm= 4.00: iabRcp= 4.00]  
11468+ R0505:CO0259----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11469+ CONTINUOUS STANDYD 1.0 01:S-1-D 6.79 .161 No\_date 29:23 39.91 .490 .000  
11470+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11471+ [CN= 77.01 N 3.00 P= .028]  
11472+ [iabEClipm= 4.00: iabRcp= 4.00]  
11473+ R0505:CO0260----- Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11474+ CONTINUOUS STANDYD 1.0 01:S-1-D 6.79 .161 No\_date 29:23 39.91 .490 .000  
11475+ Dtnin-ID:NHYD---ARAAha-QPEAKms-TpeakDate\_hh:mm---Rvnm-R.C.---DFFcms  
11476+ [CN= 77.01 N 3.00 P= .028]<

11595+ # - C-Way Clarke Drain (south of the Jock)  
 11596+ # - Subdivision with 43% impervious surface  
 11597+ # - 2020-11-03 split CLARKE Drainage Area to MAJOR and ALL  
 11598+ # - 2020-11-03 split CLARKE Drainage Area to MAJOR and ALL  
 11599+ # - [MjSysSto..1210E-04..TotDvFv01..0000E-00..N-Ovfr..0..TotDurOvf..0..hrs]  
 11600+ RO5050:CO0075- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11601+ CONTINUOUS STANDHYD 1.0 01:W\_CLAR\_MJ 1.77 .319 No\_date 28:00 59.44 .729 .000  
 11602+ [XIMP-61:TIME-59] 1.0 01:W\_CLAR\_MJ 1.77 .319 No\_date 28:00 59.44 .729 .000  
 11603+ [Limpervous area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11604+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11605+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11606+ [Major System / 1.0 01:K01-BIN-MJ 1.77 .319 No\_date 28:00 59.44 .729 .000  
 11607+ [Minor System \ 1.0 03:K01-BIN-MJ 1.77 .319 No\_date 28:00 59.44 .729 .000  
 11608+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11609+ RO5050:CO0176- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11610+ ROUTE RESERVOIN --> 1.0 02:W\_CLAR\_MJ 1.77 .319 No\_date 28:00 59.44 n/a .000  
 11611+ [Pervious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11612+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11613+ [Major System / 1.0 01:W\_CLAR\_MJ] .00 .102 No\_date 28:01 59.44 n/a .000  
 11614+ [Minor System \ 1.0 03:W\_CLAR\_MJ] .00 .102 No\_date 28:01 59.44 n/a .000  
 11615+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11616+ S-5-1000-100 Capture  
 11617+ [XIMP-61:TIME-65]  
 11618+ [C-Way Clarke Drain (south of the Jock)]  
 11619+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11620+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11621+ [Major System / 1.0 01:W\_CLAR\_MJ 1.77 .319 No\_date 28:00 59.44 .729 .000  
 11622+ [Minor System \ 1.0 03:W\_CLAR\_MJ 1.77 .319 No\_date 28:00 59.44 .729 .000  
 11623+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11624+ ADD HYD  
 11625+ RO5050:CO0178- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11626+ ROUTE RESERVOIN --> 1.0 02:W\_CLAR\_MJ 119.49 17.370 No\_date 28:04 63.49 n/a .000  
 11627+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11628+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11629+ [Major System / 1.0 01:W\_CLAR\_MJ] .00 .102 No\_date 28:04 63.49 n/a .000  
 11630+ [Minor System \ 1.0 03:W\_CLAR\_MJ] .00 .102 No\_date 28:04 63.49 n/a .000  
 11631+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11632+ [XIMP-61:TIME-65]  
 11633+ # West Clarke Pond 2  
 11634+ # - Bathtub Pond obtained from Barrenhaven South MESS modeling  
 11635+ # - Tributary Drainage Area to MSS Model  
 11636+ # - [XIMP-61:TIME-65]  
 11637+ ROUTE RESERVOIN --> 1.0 02:W\_CLAR\_MJ 119.49 17.371 No\_date 28:04 63.49 n/a .000  
 11638+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11639+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11640+ [Major System / 1.0 01:W\_CLAR\_MJ 119.49 17.371 No\_date 28:04 63.49 n/a .000  
 11641+ [Minor System \ 1.0 03:W\_CLAR\_MJ 119.49 17.371 No\_date 28:04 63.49 n/a .000  
 11642+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11643+ ADD HYD  
 11644+ RO5050:CO0179- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11645+ ROUTE RESERVOIN --> 1.0 01:W\_CLAR\_MJ 119.49 17.371 No\_date 28:04 63.49 n/a .000  
 11646+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11647+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11648+ [Major System / 1.0 01:W\_CLAR\_MJ 119.49 17.371 No\_date 28:04 63.49 n/a .000  
 11649+ [Minor System \ 1.0 03:W\_CLAR\_MJ 119.49 17.371 No\_date 28:04 63.49 n/a .000  
 11650+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11651+ SAVE HYD  
 11652+ frame: SNC\_CEO\_0050  
 11653+ remark:Total Flows before Station 5737 on Jock River  
 11654+ # JFSA 2021-02-13 add station 5737 before station 5002. Station 5737 was extracted from the HEC-RAS model T:PROJ1,1474-1  
 11655+ # JFSA 2021-03-02 change the slope to 0.1 instead of 0.0175 to stabilize the model  
 11656+ RO5050:CO0180- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11657+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54253.99 133.524 No\_date 33:22 39.90 n/a .000  
 11658+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11659+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11660+ [Major System / 1.0 01:W\_CLAR\_MJ 54253.99 127.938 No\_date 33:32 39.90 n/a .000  
 11661+ [Minor System \ 1.0 03:W\_CLAR\_MJ 54253.99 127.938 No\_date 33:32 39.90 n/a .000  
 11662+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11663+ ADD HYD  
 11664+ RO5050:CO0181- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11665+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54279.41 128.023 No\_date 35:32 33.90 n/a .000  
 11666+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11667+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11668+ frame: 5002.0050  
 11669+ remark:Total Flows before Station 5002 on Jock River  
 11670+ # Hydrograph from Nod West Clarke  
 11671+ # Channel X-Section obtained from Rvca Hydraulic Model - Station 5002  
 11672+ # JFSA 2021-02-19 Change the slope from 0.01 to 0.01 (as per Station Report 2002) to 0.055 so the model will be more stable  
 11673+ # Instead of adding station 5737 before station 5002, we instead of adding station 5737 before station 5002  
 11674+ # JFSA 2021-02-26 change the length of 5002 route channel from 825 m to 736 m. That is because of adding station 5737 before station 5002  
 11675+ RO5050:CO0186- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11676+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54279.41 128.023 No\_date 35:32 33.90 n/a .000  
 11677+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11678+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11679+ [Major System / 1.0 01:W\_CLAR\_MJ 54279.41 127.998 No\_date 35:39 33.90 n/a .000  
 11680+ [Minor System \ 1.0 03:W\_CLAR\_MJ 54279.41 127.998 No\_date 35:39 33.90 n/a .000  
 11681+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11682+ ADD HYD  
 11683+ RO5050:CO0187- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11684+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54279.41 127.998 No\_date 35:39 33.90 n/a .000  
 11685+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11686+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11687+ [Major System / 1.0 01:W\_CLAR\_MJ 54279.41 127.998 No\_date 35:39 33.90 n/a .000  
 11688+ [Minor System \ 1.0 03:W\_CLAR\_MJ 54279.41 127.998 No\_date 35:39 33.90 n/a .000  
 11689+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11690+ RO5050:CO0188- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11691+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54279.41 127.975 No\_date 35:46 33.90 n/a .000  
 11692+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11693+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11694+ [Major System / 1.0 01:W\_CLAR\_MJ 54279.41 127.975 No\_date 35:46 33.90 n/a .000  
 11695+ [Minor System \ 1.0 03:W\_CLAR\_MJ 54279.41 127.975 No\_date 35:46 33.90 n/a .000  
 11696+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11697+ ADD HYD  
 11698+ RO5050:CO0189- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11699+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54279.41 127.982 No\_date 36:14 33.90 n/a .000  
 11700+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11701+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11702+ # Hydrograph from Nod West Clarke routed to Node at Kennedy - Burnett Drain  
 11703+ # Channel X-Section obtained from Rvca Hydraulic Model - Station 4534  
 11704+ # - Kennedy-Burnett SWM Facility  
 11705+ # - Residential subdivision (north of the Jock)  
 11706+ # Existing Kennedy-Burnett SWM Facility  
 11707+ # - Rating curve obtained from URTBEP  
 11708+ # - 100 ha  
 11709+ # Existing Kennedy-Burnett SWM Facility  
 11710+ RO5050:CO0190- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11711+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11712+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11713+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11714+ [Major System / 1.0 01:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11715+ [Minor System \ 1.0 03:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11716+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11717+ ADD HYD  
 11718+ RO5050:CO0191- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11719+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11720+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11721+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11722+ [Major System / 1.0 01:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11723+ [Minor System \ 1.0 03:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11724+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11725+ RO5050:CO0192- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11726+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11727+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11728+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11729+ [Major System / 1.0 01:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11730+ [Minor System \ 1.0 03:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11731+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11732+ ADD HYD  
 11733+ RO5050:CO0193- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11734+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11735+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11736+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11737+ [Major System / 1.0 01:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11738+ [Minor System \ 1.0 03:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11739+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11740+ RO5050:CO0194- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11741+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11742+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11743+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11744+ [Major System / 1.0 01:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11745+ [Minor System \ 1.0 03:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11746+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11747+ ADD HYD  
 11748+ RO5050:CO0195- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11749+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11750+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11751+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11752+ [Major System / 1.0 01:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11753+ [Minor System \ 1.0 03:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11754+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11755+ RO5050:CO0196- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11756+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11757+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11758+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11759+ [Major System / 1.0 01:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11760+ [Minor System \ 1.0 03:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11761+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11762+ RO5050:CO0197- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11763+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11764+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11765+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11766+ [Major System / 1.0 01:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11767+ [Minor System \ 1.0 03:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11768+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11769+ RO5050:CO0198- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11770+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11771+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11772+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11773+ [Major System / 1.0 01:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11774+ [Minor System \ 1.0 03:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11775+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11776+ RO5050:CO0199- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11777+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11778+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11779+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11780+ [Major System / 1.0 01:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11781+ [Minor System \ 1.0 03:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11782+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11783+ RO5050:CO0200- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11784+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11785+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11786+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11787+ [Major System / 1.0 01:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11788+ [Minor System \ 1.0 03:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11789+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11790+ RO5050:CO0201- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11791+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11792+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11793+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11794+ [Major System / 1.0 01:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11795+ [Minor System \ 1.0 03:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11796+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11797+ RO5050:CO0202- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11798+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11799+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11800+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11801+ [Major System / 1.0 01:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11802+ [Minor System \ 1.0 03:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11803+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11804+ RO5050:CO0203- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11805+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11806+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11807+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11808+ [Major System / 1.0 01:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11809+ [Minor System \ 1.0 03:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11810+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11811+ RO5050:CO0204- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11812+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11813+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11814+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11815+ [Major System / 1.0 01:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11816+ [Minor System \ 1.0 03:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11817+ [SMIN..31..15..SMAX..207..66..SKR..010]  
 11818+ RO5050:CO0205- Dtnin:ID:NHDY---AREAh-QPEAKms-TpeakDate\_bh:mm---RVm-R.C.--DWFcms  
 11819+ ROUTE CHANNEL --> 1.0 02:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14 33.90 n/a .000  
 11820+ [Pervious area: Iaper: 4.67:SLPP:1.00:LGPd 40.:NMD-..250:SCP+ ..0]  
 11821+ [Imperious area: Iaper: 1.57:SLPP:1.00:LGPd 892.:NM1..013:SCI+ ..0]  
 11822+ [Major System / 1.0 01:W\_CLAR\_MJ 54279.41 128.023 No\_date 36:14

11959- ROSS05:00234- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 11970- CONTINUOUS STANDNDY 1.0 01:KEB-16\_2 3.42 .724 No\_date 28:01 64.30 .789 .000  
 11971- [Xm0= 71,TIMW=.71] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 11973- [Pervious area: Iaper: 4.67SLPP+0.02LDG+ 40.-NPW-.250SCP+.0] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 11974- [Impervious area: IaIpm: 16.1SLP+ .30.LGD1 .151.-NMW-.013:SCI-.01] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 11975- [Interpretaion: 4.00:ICRPcpr- 1.00] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 11976- ROSS05:00237- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 11977- ADD HYD 1.0 02:KEB-Pond- 206.72 18.01 No\_date 28:02 42.53 n/a .000  
 11978- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 11979- \* 1.0 02:KEB-08-8 6.61 1.058 No\_date 27:53 60.05 n/a .000  
 11980- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 11981- \* 1.0 02:KEB-10-1 1.37 .295 No\_date 28:00 71.90 n/a .000  
 11982- \* 1.0 02:KEB-10-2 1.14 .295 No\_date 28:00 71.90 n/a .000  
 11983- \* 1.0 02:KEB-12-9 1.86 .867 No\_date 28:09 68.93 n/a .000  
 11984- \* 1.0 02:KEB-13-9 1.81 .867 No\_date 28:09 68.93 n/a .000  
 11985- \* 1.0 02:KEB-14-9 5.47 .873 No\_date 27:53 60.02 n/a .000  
 11986- \* 1.0 02:KEB-16-2 1.42 .724 No\_date 28:01 64.30 n/a .000  
 11987- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 11988- ROSS05:00238- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 11989- ROUTE RESERVOIR< 1.0 02:KEB-P2- 254.24 26.339 No\_date 28:02 46.87 n/a .000  
 11990- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 11991- overflow << 1.0 03:KEB-P20v- 1.14 .5 267 No\_date 28:09 46.87 n/a .000  
 11992- [MxSto:0001-11098-3 m\_ TotoVolV01\_5351E-01\_5\_m\_N-Ofw- 1. TotDurOrf\_ 0.hrs] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 11993- ROSS05:00239- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 11994- ADD HYD 1.0 02:KEB-P2R- 253.10 17.634 No\_date 28:09 46.87 n/a .000  
 11995- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 11996- \* 1.0 02:KEB-P2v- 254.24 26.339 No\_date 28:09 46.87 n/a .000  
 11997- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 11998- SAVE HYD 1.0 01:KEB-Pond- 254.24 22.891 No\_date 28:09 46.87 n/a .000  
 11999- remark>Total Flows at Ks second pond  
 12000- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12001- ROSS05:00241- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12002- COMPUTE DLYHLDY< 1.0 01:KEB-16\_3 2.80 .624 No\_date 28:00 66.65 .818 .000  
 12003- [Xm0= 75,TIMW=.75] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12004- [Horton parameters: Fe: 76.207Cm: 13.20.DCAY4.14; Fc : 0.01] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12005- [Impervious area: IaIpm: 16.1SLP+ .30.LGD1 .151.-NMW-.013:SCI-.01] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12007- [iaICRPcpr: 4.00:ICRPcpr- 1.00] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12008- ROSS05:00242- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12009- ADD HYD 1.0 02:KEB-Pond- 254.24 22.891 No\_date 28:09 46.87 n/a .000  
 12010- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12011- \* 1.0 02:KEB-1\_1 2.80 .624 No\_date 28:00 66.65 .818 .000  
 12012- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12013- ROUTE RESERVOIR< 1.0 02:KEB-P3- 257.04 23.147 No\_date 28:09 47.08 n/a .000  
 12014- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12015- overflow << 1.0 03:KEB-P3v- 247.64 22.286 No\_date 28:10 47.08 n/a .000  
 12016- [MxSto:0001-11098-3 m\_ TotoVolV01\_1168E-02\_5\_m\_N-Ofw- 1. TotDurOrf\_ 23.hrs] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12017- ROSS05:00244- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12018- ADD HYD 1.0 02:KEB-P2R- 253.90 .051 No\_date 17:13 47.07 n/a .000  
 12019- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12020- \* 1.0 02:KEB-P2v- 247.64 22.286 No\_date 28:10 47.08 n/a .000  
 12021- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12022- SAVE HYD 1.0 01:KEB-Pond- 257.04 22.337 No\_date 28:10 47.08 n/a .000  
 12023- remark>Total Flows at Ks third pond  
 12025- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12027- # \*\*\*\*\* PROPOSED Subcatchments (Kennedy-Burnett SWN Facility (118080), SWM Modeling Approach, NOVATECH Report Ju  
 12028- # \*\*\*\*\* PROPOSED Subcatchments (Kennedy-Burnett SWN Facility (118080), SWM Modeling Approach, NOVATECH Report Ju  
 12029- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12030- CONTINUOUS STANDNDY 1.0 01:FCF-01 8.03 1.483 No\_date 28:01 49.52 .608 .000  
 12031- [Xm0= 47,TIMW=.47] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12032- [Pervious area: Iaper: 4.67SLPP+0.02LDG+ 40.-NPW-.250SCP+.0] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12034- [Impervious area: IaIpm: 1.57SLP+1.00.LGD1 .231.-NMW-.013:SCI-.01] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12035- [Interpretaion: 4.00:ICRPcpr- 1.00] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12036- ROSS05:00247- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12037- COMPUTE DLYHLDY< 1.0 01:FCF-01 8.03 1.483 No\_date 28:01 49.52 n/a .000  
 12038- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12039- Minor System << 1.0 03:FCF-01-MJ 8.03 .756 No\_date 28:12 49.91 n/a .000  
 12040- [MjSto:0001-4662E-03\_TotoVolV01\_0000E-00\_0000E-00] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12041- ROSS05:00248- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12042- ADD HYD 1.0 02:FCF-01-MJ 8.03 .000 No\_date 0:00 0:00 n/a .000  
 12043- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12044- \* 1.0 02:FCF-01-MJ 8.03 .000 No\_date 0:00 0:00 n/a .000  
 12045- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12046- CONTINUOUS STANDNDY 1.0 01:FCF-02 16.05 1.831 No\_date 28:00 75.92 .931 .000  
 12047- [Horton parameters: Fe: 76.207Cm: 13.20.DCAY4.14; Fc : 0.01] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12049- [Pervious area: Iaper: 4.67SLPP+0.02LDG+ 40.-NPW-.250SCP+.0] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12050- [Impervious area: IaIpm: 1.57SLP+1.00.LGD1 .231.-NMW-.013:SCI-.01] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12051- [Interpretaion: 4.00:ICRPcpr- 1.00] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12052- ROSS05:00250- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12053- COMPUTE DLYHLDY< 1.0 01:FCF-01 8.03 1.483 No\_date 28:01 49.52 n/a .000  
 12054- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12055- Major System << 1.0 02:FCF-02-MJ 16.05 1.159 No\_date 27:51 75.94 n/a .000  
 12056- Minor System << 1.0 03:FCF-02-MJ 16.05 1.159 No\_date 27:51 75.94 n/a .000  
 12057- ROSS05:00251- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12058- ADD HYD 1.0 02:FCF-02-MJ 16.05 1.159 No\_date 27:51 75.94 n/a .000  
 12059- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12060- \* 1.0 02:FCF-02-MJ 16.05 1.159 No\_date 27:51 75.94 n/a .000  
 12061- ROSS05:00252- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12062- COMPUTE DLYHLDY< 1.0 01:FCF-02 7.37 1.540 No\_date 28:00 59.28 .727 .000  
 12063- [Xm0= 64,TIMW=.64] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12064- [Horton parameters: Fe: 76.207Cm: 13.20.DCAY4.14; Fc : 0.01] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12065- [Impervious area: IaIpm: 1.57SLP+1.00.LGD1 .231.-NMW-.013:SCI-.01] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12067- [Interpretaion: 4.00:ICRPcpr- 1.00] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12068- ROSS05:00253- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12069- COMPUTE DLYHLDY< 1.0 01:FCF-03 7.37 1.540 No\_date 28:00 59.28 n/a .000  
 12070- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12071- Minor System << 1.0 02:FCF-03-MJ 8.03 .000 No\_date 0:00 0:00 n/a .000  
 12072- [MjSto:0001-1131E04\_TotoVolV01\_1375E-02\_N-Ofw- 1. TotDurOrf\_ 0.hrs] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12073- ROSS05:00254- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12074- ADD HYD 1.0 02:FCF-03-MJ 8.03 .000 No\_date 0:00 0:00 n/a .000  
 12075- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12076- \* 1.0 02:FCF-03-MJ 8.03 .000 No\_date 0:00 0:00 n/a .000  
 12077- ROSS05:00255- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12078- CONTINUOUS STANDNDY 1.0 01:FCF-04 12.87 2.587 No\_date 28:01 59.28 .727 .000  
 12079- [Xm0= 64,TIMW=.64] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12080- [Pervious area: Iaper: 4.67SLPP+0.02LDG+ 40.-NPW-.250SCP+.0] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12081- [Impervious area: IaIpm: 1.57SLP+1.00.LGD1 .231.-NMW-.013:SCI-.01] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12082- [Interpretaion: 4.00:ICRPcpr- 1.00] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12083- ROSS05:00256- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12084- # PROPOSED Subcatchments (Kennedy-Burnett SWN Facility (118080), SWM Modeling Approach, NOVATECH Report June, 2020)  
 12085- # \*\*\*\*\* PROPOSED Subcatchments (Kennedy-Burnett SWN Facility (118080), SWM Modeling Approach, NOVATECH Report June, 2020)  
 12086- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12087- COMPUTE DLYHLDY< 1.0 01:FCF-04 8.24 1.714 No\_date 28:00 59.28 n/a .000  
 12088- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12089- Minor System << 1.0 02:FCF-04-MJ 8.24 .741 No\_date 27:44 59.54 n/a .000  
 12090- [MjSto:0001-5643E03\_TotoVolV01\_0000E-00\_0000E-00] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12091- ROSS05:00257- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12092- ADD HYD 1.0 02:FCF-04-MJ 8.24 .741 No\_date 27:44 59.54 n/a .000  
 12093- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12094- \* 1.0 02:FCF-04-MJ 8.24 .741 No\_date 27:44 59.54 n/a .000  
 12095- ROSS05:00258- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12096- COMPUTE DLYHLDY< 1.0 01:FCF-05 8.24 1.540 No\_date 28:00 59.28 .727 .000  
 12097- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12098- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12099- Minor System << 1.0 02:FCF-05-MJ 8.24 .563 No\_date 27:44 59.48 n/a .000  
 12100- [MjSto:0001-00260\_TotoVolV01\_62E-02\_N-Ofw- 1. TotDurOrf\_ 0.hrs] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12101- ROSS05:00260- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12102- ADD HYD 1.0 02:FCF-05-MJ 8.24 .563 No\_date 27:44 59.48 n/a .000  
 12103- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12104- \* 1.0 02:FCF-05-MJ 8.24 .563 No\_date 27:44 59.48 n/a .000  
 12105- ROSS05:00261- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12106- COMPUTE DLYHLDY< 1.0 01:FCF-06 8.24 1.540 No\_date 28:00 59.28 .727 .000  
 12107- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12108- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12109- Minor System << 1.0 02:FCF-06-MJ 8.24 .563 No\_date 27:44 59.48 n/a .000  
 12110- [MjSto:0001-00261\_TotoVolV01\_62E-02\_N-Ofw- 1. TotDurOrf\_ 0.hrs] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12111- ROSS05:00262- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12112- ADD HYD 1.0 02:FCF-06-MJ 8.24 .563 No\_date 27:44 59.48 n/a .000  
 12113- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12114- \* 1.0 02:FCF-06-MJ 8.24 .563 No\_date 27:44 59.48 n/a .000  
 12115- ROSS05:00263- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12116- COMPUTE DLYHLDY< 1.0 01:FCF-07 8.24 1.540 No\_date 28:00 59.28 .727 .000  
 12117- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12118- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12119- Minor System << 1.0 02:FCF-07-MJ 8.24 .563 No\_date 27:44 59.48 n/a .000  
 12120- [MjSto:0001-00262\_TotoVolV01\_62E-02\_N-Ofw- 1. TotDurOrf\_ 0.hrs] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12121- ROSS05:00264- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12122- ADD HYD 1.0 02:FCF-07-MJ 8.24 .563 No\_date 27:44 59.48 n/a .000  
 12123- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12124- \* 1.0 02:FCF-07-MJ 8.24 .563 No\_date 27:44 59.48 n/a .000  
 12125- ROSS05:00265- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12126- COMPUTE DLYHLDY< 1.0 01:FCF-08 8.24 1.540 No\_date 28:00 59.28 .727 .000  
 12127- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12128- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12129- Minor System << 1.0 02:FCF-08-MJ 8.24 .563 No\_date 27:44 59.48 n/a .000  
 12130- [MjSto:0001-00263\_TotoVolV01\_62E-02\_N-Ofw- 1. TotDurOrf\_ 0.hrs] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12131- ROSS05:00266- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12132- ADD HYD 1.0 02:FCF-08-MJ 8.24 .563 No\_date 27:44 59.48 n/a .000  
 12133- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12134- \* 1.0 02:FCF-08-MJ 8.24 .563 No\_date 27:44 59.48 n/a .000  
 12135- ROSS05:00267- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12136- COMPUTE DLYHLDY< 1.0 01:FCF-09 8.24 1.540 No\_date 28:00 59.28 .727 .000  
 12137- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12138- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12139- Minor System << 1.0 02:FCF-09-MJ 8.24 .563 No\_date 27:44 59.48 n/a .000  
 12140- [MjSto:0001-00264\_TotoVolV01\_62E-02\_N-Ofw- 1. TotDurOrf\_ 0.hrs] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12141- ROSS05:00268- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12142- COMPUTE DLYHLDY< 1.0 01:FRAS-01 21.61 .816 No\_date 28:40 39.91 .490 .000  
 12143- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12144- Minor System << 1.0 02:FRAS-01 21.61 .816 No\_date 28:40 39.91 .490 .000  
 12145- [MjSto:0001-00265\_TotoVolV01\_62E-02\_N-Ofw- 1. TotDurOrf\_ 0.hrs] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12146- ROSS05:00269- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12147- ADD HYD 1.0 02:KEB-Pond- 257.04 22.337 No\_date 28:10 47.08 n/a .000  
 12148- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12149- \* 1.0 02:KEB-1-8 55.36 2.770 No\_date 28:23 39.91 n/a .000  
 12150- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12151- \* 1.0 02:KEFASER-D 21.61 .816 No\_date 28:40 39.91 n/a .000  
 12152- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12153- Minor System << 1.0 02:KEFASER-D 21.61 .816 No\_date 28:40 39.91 n/a .000  
 12154- [MjSto:0001-00266\_TotoVolV01\_62E-02\_N-Ofw- 1. TotDurOrf\_ 0.hrs] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12155- ROSS05:00270- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12156- ADD HYD 1.0 02:KEFASER-D 21.61 .816 No\_date 28:40 39.91 n/a .000  
 12157- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12158- \* 1.0 02:KEFASER-D 21.61 .816 No\_date 28:40 39.91 n/a .000  
 12159- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12160- Minor System << 1.0 02:KEFASER-D 21.61 .816 No\_date 28:40 39.91 n/a .000  
 12161- [MjSto:0001-00267\_TotoVolV01\_62E-02\_N-Ofw- 1. TotDurOrf\_ 0.hrs] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12162- ROSS05:00271- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12163- ADD HYD 1.0 02:KEFASER-D 21.61 .816 No\_date 28:40 39.91 n/a .000  
 12164- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12165- \* 1.0 02:KEFASER-D 21.61 .816 No\_date 28:40 39.91 n/a .000  
 12166- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12167- Minor System << 1.0 02:KEFASER-D 21.61 .816 No\_date 28:40 39.91 n/a .000  
 12168- [MjSto:0001-00268\_TotoVolV01\_62E-02\_N-Ofw- 1. TotDurOrf\_ 0.hrs] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12169- ROSS05:00272- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12170- ADD HYD 1.0 02:KEFASER-D 21.61 .816 No\_date 28:40 39.91 n/a .000  
 12171- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12172- \* 1.0 02:KEFASER-D 21.61 .816 No\_date 28:40 39.91 n/a .000  
 12173- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12174- Minor System << 1.0 02:KEFASER-D 21.61 .816 No\_date 28:40 39.91 n/a .000  
 12175- [MjSto:0001-00269\_TotoVolV01\_62E-02\_N-Ofw- 1. TotDurOrf\_ 0.hrs] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12176- ROSS05:00273- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12177- ADD HYD 1.0 02:KEFASER-D 21.61 .816 No\_date 28:40 39.91 n/a .000  
 12178- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12179- \* 1.0 02:KEFASER-D 21.61 .816 No\_date 28:40 39.91 n/a .000  
 12180- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12181- Minor System << 1.0 02:KEFASER-D 21.61 .816 No\_date 28:40 39.91 n/a .000  
 12182- [MjSto:0001-00270\_TotoVolV01\_62E-02\_N-Ofw- 1. TotDurOrf\_ 0.hrs] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12183- ROSS05:00274- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12184- ADD HYD 1.0 02:KEFASER-D 21.61 .816 No\_date 28:40 39.91 n/a .000  
 12185- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12186- \* 1.0 02:KEFASER-D 21.61 .816 No\_date 28:40 39.91 n/a .000  
 12187- \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12188- Minor System << 1.0 02:KEFASER-D 21.61 .816 No\_date 28:40 39.91 n/a .000  
 12189- [MjSto:0001-00271\_TotoVolV01\_62E-02\_N-Ofw- 1. TotDurOrf\_ 0.hrs] \* DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12190- ROSS05:00275- DT\$in:ID-NHDY- AREABA-QPEAKms-TpeakDate\_hh:mm:- RVNm-R.C. -- DWFcms  
 12191- ADD HYD 1.0 02:KEFASER-D 21.61 .816 No\_date 28:40 39.91 n/a



12717+ [Impervious area: IAImp- 1.57:SLP1=1.00:LGI+ 262:MNI+ .013:SCI+ .0] 12718+ [IAIM- 4.00: IAImp- 1.00] 12719+ [SM- 1.00: 33.81: SMAX225.43: SK- .010] 12720+ R0505:CO0359-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12721+ COMPUTE DUALHYD 1.0 01:A1-MJ .00 .000 No\_date 28:00 .000 12722+ Minor System \ 1.0 03:A1-MJ .24 .481 No\_date 28:00 66.69 n/a .000 12723+ Minor System \ 1.0 03:A1-MJ .24 .481 No\_date 28:00 66.69 n/a .000 12724+ R0505:CO0360-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12725+ ADD HYD \* 1.0 02:106A-106 106 106 1.702 No\_date 27:53 56.53 n/a .000 12726+ ADD HYD \* 1.0 02:A1-MJ 2.44 .481 No\_date 28:00 66.69 n/a .000 12727+ SMW \* 1.0 01:M108 111.94 4.177 No\_date 28:00 56.81 n/a .000 12728+ R0505:CO0361-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12729+ SAVE HYD 1.0 01:M108 111.94 4.177 No\_date 28:00 56.81 n/a .000 12730+ R0505:CO0362-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12731+ remark>Total Flows at MH106 12732+ R0505:CO0362-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12733+ [ROUTE 1.000 out<--> 1.0 01:M106 111.94 4.177 No\_date 28:00 56.81 n/a .000 12734+ \* [SDT= 1.00] out<--> 1.0 01:M106 111.94 4.177 No\_date 28:00 56.81 n/a .000 12735+ [L8/n= 123, .100/.013] 12736+ [Vmax= 2.080:Imax= 2.001] 12737+ [Din= 1.80:Dused= 1.98] 12738+ R0505:CO0363-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12739+ [ROUTE 1.000 out<--> 1.0 01:A10 4.14 .602 No\_date 28:01 53.20 .655 .000 12740+ [(XMD= 35:TIME=.47] 12741+ [LOGS= 2 :CIN= 75.0] 12742+ [ROUTE 1.000 out<--> 1.0 01:A10 4.14 .602 No\_date 28:01 53.20 .655 .000 12743+ [Impervious area: IAImp- 1.57:SLP1=1.00:LGI+ 183:MNI+ .013:SCI+ .0] 12744+ [IAIM- 4.00: IAEComp- 4.00] 12745+ [SM- 1.00: 33.81: SMAX225.43: SK- .010] 12746+ R0505:CO0364-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12747+ COMPUTE DUALHYD 1.0 01:A10 4.14 .602 No\_date 28:01 53.20 .655 .000 12748+ Minor System \ 1.0 01:A10 4.14 .330 No\_date 27:50 53.25 n/a .000 12749+ Minor System \ 1.0 01:A10 4.14 .330 No\_date 27:50 53.25 n/a .000 12750+ R0505:CO0365-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12751+ CONTINUOUS STANDYD 1.0 01:A1 106 106 1.720 No\_date 28:00 60.69 .745 .000 12752+ [XMD= 53:TIME=.62] 12753+ [ROUTE 1.000 out<--> 1.0 01:A1 106 106 1.720 No\_date 28:00 60.69 .745 .000 12754+ [Impervious area: IAImp- 4.67:SLP1=1.00:LGI+ 40:MNP-.250:SCP+ .0] 12755+ [Impervious area: IAImp- 4.67:SLP1=1.00:LGI+ 379:MNI+ .013:SCI+ .0] 12756+ [ROUTE 1.000 out<--> 1.0 01:A1 106 106 1.720 No\_date 28:00 60.69 .745 .000 12757+ [SMIN= 33.81: SMAX=225.43: SK- .010] 12758+ R0505:CO0366-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12759+ COMPUTE DUALHYD 1.0 01:A1 106 106 1.720 No\_date 28:00 60.69 .745 .000 12760+ Minor System \ 1.0 02:A1-MJ .00 .000 No\_date 0:00 .00 n/a .000 12761+ Major System / 1.0 02:A1-MJ .00 .000 No\_date 0:00 .00 n/a .000 12762+ Minor System / 1.0 02:A1-MJ .00 .000 No\_date 0:00 .00 n/a .000 12763+ R0505:CO0367-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12764+ ADD HYD \* 1.0 02:106E-107 111.94 4.129 No\_date 28:00 56.81 n/a .000 12765+ ADD HYD \* 1.0 02:106E-107 111.94 4.129 No\_date 28:00 56.81 n/a .000 12766+ ADD HYD \* 1.0 02:106E-107 111.94 4.129 No\_date 28:00 56.81 n/a .000 12767+ ADD HYD \* 1.0 02:A1-MJ .61 .993 No\_date 27:52 60.86 n/a .000 12768+ SMW \* 1.0 02:A1-MJ .61 .993 No\_date 27:52 60.86 n/a .000 12769+ R0505:CO0368-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12770+ SAVE HYD 1.0 01:M107 126.69 5.432 No\_date 28:00 57.03 n/a .000 12771+ R0505:CO0369-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12772+ remark>Total Flows at MH107 12773+ R0505:CO0369-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12774+ [ROUTE 1.000 out<--> 1.0 01:M107 126.69 5.432 No\_date 28:00 57.03 n/a .000 12775+ \* [SDT= 1.00] out<--> 1.0 01:M107 126.69 5.345 No\_date 28:00 57.03 n/a .000 12776+ [L8/n= 114, .120/.013] 12777+ [Vmax= 2.080:Dused= 2.02] 12778+ R0505:CO0370-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12779+ [ROUTE 1.000 out<--> 1.0 01:M107 126.69 5.345 No\_date 28:00 57.03 n/a .000 12780+ [SMIN= 33.81: SMAX=225.43: SK- .010] 12781+ R0505:CO0371-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12782+ [ROUTE 1.000 out<--> 1.0 01:A1 12.29 1.938 No\_date 28:01 56.26 n/a .000 12783+ [Impervious area: IAImp- 4.67:SLP1=1.00:LGI+ 40:MNP-.250:SCP+ .0] 12784+ [ROUTE 1.000 out<--> 1.0 01:A1 12.29 1.029 No\_date 27:50 56.44 n/a .000 12785+ [SMIN= 33.81: SMAX=225.43: SK- .010] 12786+ R0505:CO0372-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12787+ COMPUTE DUALHYD 1.0 01:A1 12.29 1.938 No\_date 28:01 56.26 n/a .000 12788+ Minor System \ 1.0 01:A1 12.29 1.029 No\_date 27:50 56.44 n/a .000 12789+ R0505:CO0373-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12790+ CONTINUOUS STANDYD 1.0 01:A1 12.29 1.938 No\_date 28:01 56.26 n/a .000 12791+ [XMD= 41:TIME=.54] 12792+ R0505:CO0372-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12793+ [ROUTE 1.000 out<--> 1.0 01:A1 12.29 1.938 No\_date 28:01 56.26 n/a .000 12794+ [Impervious area: IAImp- 4.67:SLP1=1.00:LGI+ 183:MNI+ .013:SCI+ .0] 12795+ [IAIM- 4.00: IAEComp- 4.00] 12796+ [SM- 1.00: 33.81: SMAX225.43: SK- .010] 12797+ R0505:CO0372-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12798+ COMPUTE DUALHYD 1.0 01:A1 12.29 1.938 No\_date 28:01 56.26 n/a .000 12799+ Minor System \ 1.0 01:A1 12.29 1.938 No\_date 28:01 56.26 n/a .000 12800+ R0505:CO0374-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12801+ CONTINUOUS STANDYD 1.0 01:Pond-Block 2.94 .430 No\_date 28:00 53.21 .653 .000 12802+ [XMD= 71:TIME=.71] 12803+ [ROUTE 1.000 out<--> 1.0 01:Pond-Block 2.94 .430 No\_date 28:00 53.21 .653 .000 12804+ [Impervious area: IAImp- 4.67:SLP1=1.00:LGI+ 40:MNP-.250:SCP+ .0] 12805+ [ROUTE 1.000 out<--> 1.0 01:Pond-Block 2.94 .430 No\_date 28:00 53.21 .653 .000 12806+ COMPUTE DUALHYD 1.0 01:A1 2.53 .487 No\_date 28:01 66.69 n/a .000 12807+ Minor System \ 1.0 02:A1-MJ .00 .000 No\_date 0:00 .00 n/a .000 12808+ Minor System \ 1.0 02:A1-MJ .00 .000 No\_date 0:00 .00 n/a .000 12809+ R0505:CO0375-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12810+ CONTINUOUS STANDYD 1.0 01:Pond-Block 2.94 .487 No\_date 28:00 53.21 .653 .000 12811+ [XMD= 41:TIME=.54] 12812+ R0505:CO0375-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12813+ [ROUTE 1.000 out<--> 1.0 01:Pond-Block 2.94 .487 No\_date 28:00 53.21 .653 .000 12814+ [Impervious area: IAImp- 4.67:SLP1=1.00:LGI+ 40:MNP-.250:SCP+ .0] 12815+ [ROUTE 1.000 out<--> 1.0 01:Pond-Block 2.94 .487 No\_date 28:00 53.21 .653 .000 12816+ [SMIN= 33.81: SMAX=225.43: SK- .010] 12817+ R0505:CO0377-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12818+ ADD HYD \* 1.0 02:A1-MJ .23 .534 No\_date 28:01 57.03 n/a .000 12819+ ADD HYD \* 1.0 02:A1-MJ .23 .534 No\_date 28:01 57.03 n/a .000 12820+ ADD HYD \* 1.0 02:A1-MJ .23 .534 No\_date 28:01 57.03 n/a .000 12821+ ADD HYD \* 1.0 02:A1-MJ .23 .534 No\_date 28:01 57.03 n/a .000 12822+ SMW \* 1.0 01:M108 141.57 6.850 No\_date 28:01 57.16 n/a .000 12823+ R0505:CO0377-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12824+ ADD HYD \* 1.0 02:A1-MJ .00 .000 No\_date 28:01 57.16 n/a .000 12825+ name:MMH08\_0050 12826+ remark>Total Flows at MH108 12827+ R0505:CO0378-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12828+ ROUTE PIPE <--> 1.0 02:A1-MJ 141.57 6.850 No\_date 28:01 57.16 n/a .000 12829+ \* [ROUTE 1.000 out<--> 1.0 01:108-119 141.57 6.810 No\_date 28:02 57.16 n/a .000 12830+ [ROUTE 1.000 out<--> 1.0 01:108-119 141.57 6.810 No\_date 28:02 57.16 n/a .000 12831+ [Vmax= 2.104:Dmax= 1.784] 12832+ [Din= 1.80:Dused= 2.17] 12833+ R0505:CO0381-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12834+ SAVE HYD 1.0 01:M108 141.57 7.185 No\_date 28:02 57.08 n/a .000 12835+ name:Corrigan\_0050 12836+ remark:HVD\_COMMENT [Total Flows at Corrigan Pond] 12837+ R0505:CO0382-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12838+ ROUTE RESERVOIR <--> 1.0 01:C0rri- 141.57 1.185 No\_date 28:02 57.08 n/a .000 12839+ out <--> 1.0 01:C0rri- 141.57 6.335 No\_date 28:26 57.08 n/a .000 12840+ [ROUTE 1.000 out<--> 1.0 01:C0rri- 141.57 6.335 No\_date 28:26 57.08 n/a .000 12841+ ADD HYD 1.0 02:1116-corrig 141.57 6.771 No\_date 28:02 57.16 n/a .000 12842+ ADD HYD 1.0 02:1116-corrig 141.57 6.771 No\_date 28:02 57.16 n/a .000 12843+ ADD HYD 1.0 02:1116-corrig 141.57 6.771 No\_date 28:02 57.16 n/a .000 12844+ R0505:CO0384-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12845+ ROUTE PIPE <--> 1.0 02:108-116 141.57 6.810 No\_date 28:02 57.16 n/a .000 12846+ ADD HYD 1.0 02:108-116 141.57 6.810 No\_date 28:02 57.16 n/a .000 12847+ ADD HYD 1.0 02:108-116 141.57 6.810 No\_date 28:02 57.16 n/a .000 12848+ R0505:CO0385-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12849+ ADD HYD 1.0 02:108-116 141.57 6.810 No\_date 28:02 57.16 n/a .000 12850+ ADD HYD 1.0 02:108-116 141.57 6.810 No\_date 28:02 57.16 n/a .000 12851+ name:MMH108\_0050 12852+ remark>Total Flows at MMH108 12853+ R0505:CO0386-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12854+ ROUTE PIPE <--> 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12855+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12856+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12857+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12858+ R0505:CO0387-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12859+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12860+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12861+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12862+ R0505:CO0388-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12863+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12864+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12865+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12866+ R0505:CO0389-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12867+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12868+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12869+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12870+ R0505:CO0389-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12871+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12872+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12873+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12874+ R0505:CO0390-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12875+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12876+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12877+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12878+ R0505:CO0391-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12879+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12880+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12881+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12882+ R0505:CO0392-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12883+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12884+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12885+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12886+ R0505:CO0393-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12887+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12888+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12889+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12890+ R0505:CO0394-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12891+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12892+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12893+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12894+ R0505:CO0395-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12895+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12896+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12897+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12898+ R0505:CO0396-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12899+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12900+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12901+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12902+ R0505:CO0397-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12903+ ADD HYD 1.0 02:108-118 141.57 6.810 No\_date 28:02 57.16 n/a .000 12904+ frame:SN\_M1\_050 12905+ R0505:CO0398-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12906+ \*\* END OF RUN : 99 12907+ R0505:CO0399-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12908+ R0505:CO0400-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12909+ CONTINUOUS STANDYD 1.0 01:S2-2 10.294 4.795 No\_date 28:20 35.39 n/a .000 12910+ R0505:CO0400-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12911+ R0505:CO0401-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12912+ R0505:CO0402-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12913+ R0505:CO0403-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12914+ R0505:CO0404-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12915+ R0505:CO0405-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12916+ R0505:CO0406-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12917+ R0505:CO0407-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12918+ R0505:CO0408-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12919+ R0505:CO0409-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12920+ R0505:CO0410-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12921+ R0505:CO0411-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12922+ R0505:CO0404-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12923+ R0505:CO0405-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12924+ R0505:CO0406-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12925+ R0505:CO0407-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12926+ R0505:CO0408-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12927+ R0505:CO0409-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12928+ R0505:CO0410-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12929+ R0505:CO0411-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12930+ R0505:CO0412-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12931+ R0505:CO0413-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12932+ R0505:CO0414-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12933+ R0505:CO0415-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12934+ R0505:CO0416-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12935+ R0505:CO0417-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12936+ R0505:CO0418-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12937+ R0505:CO0419-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12938+ R0505:CO0420-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12939+ R0505:CO0421-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12940+ R0505:CO0422-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12941+ R0505:CO0423-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12942+ R0505:CO0424-----Dtnin:ID:NHYD-----ARBAh-QPEAKcms-TpeakDate\_bh:mm:---RVM-R.C.---DWFcms 12943+ R0

13097+ # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
13098+ # of 1.5  
13099+ R0100:00008-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13094+ CONTINUOUS\_NASHYD 1.0 01:JR\_GWM 3074.00 10.428 No\_date 39:59 28.29 .319 .000  
13095+ [TnEC= 4.00: SMIN= 13.24: SMAX=544.96: SKw .010]  
13097+ [InterEventtime= 12.00]  
13098+ R0100:00009-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13099+ CONTINUOUS\_NASHYD 1.0 01:JR\_GWM 1781.00 19.495 No\_date 32:38 42.49 .480 .000  
13100+ [CN= 72.01 N: 3.00: Tp: 3.91]  
13101+ [TnEC= 4.00: SMIN= 7.95: SMAX=264.99: SKw .010]  
13102+ [InterEventtime= 12.00]  
13103+ R0100:00010-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13094+ CONTINUOUS\_NASHYD 1.0 01:IN12\_11 500.00 10.735 No\_date 29:21 36.76 .415 .000  
13095+ [CN= 66.01 N: 3.00: Tp: 2.24]  
13096+ [TnEC= 4.00: SMIN= 52.62: SMAX=350.79: SKw .010]  
13097+ [InterEventtime= 12.00]  
13108+ # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
13109+ # of 1.5  
13110+ R0100:00011-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13111+ CONTINUOUS\_NASHYD 1.0 01:INN\_CK 1917.00 14.496 No\_date 34:24 36.76 .415 .000  
13112+ [TnEC= 4.00: SMIN= 12.00: SMAX=350.79: SKw .010]  
13113+ [InterEventtime= 12.00]  
13117+ # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
13118+ # of 1.5  
13119+ R0100:00012-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13120+ CONTINUOUS\_NASHYD 1.0 01:IN10\_10 5666.00 37.663 No\_date 37:48 42.49 .480 .000  
13121+ [CN= 72.01 N: 3.00: Tp: 8.00]  
13122+ [TnEC= 4.00: SMIN= 13.24: SMAX=264.99: SKw .010]  
13123+ [InterEventtime= 12.00]  
13124+ # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
13125+ # of 1.5  
13126+ R0100:00013-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13127+ CONTINUOUS\_NASHYD 1.0 01:IN10\_10 8376.00 36.118 No\_date 39:59 36.76 .415 .000  
13128+ [CN= 66.01 N: 3.00: Tp: 11.66]  
13129+ [TnEC= 4.00: SMIN= 52.62: SMAX=350.79: SKw .010]  
13130+ [InterEventtime= 12.00]  
13132+ # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
13133+ # of 1.5  
13134+ R0100:00014-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13135+ CONTINUOUS\_NASHYD 1.0 01:SW\_9 1132.00 16.501 No\_date 30:52 40.82 .461 .000  
13136+ [TnEC= 4.00: SMIN= 43.07: SMAX=287.10: SKw .010]  
13137+ [InterEventtime= 12.00]  
13141+ # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
13142+ # of 1.5  
13143+ R0100:00015-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13144+ CONTINUOUS\_NASHYD 1.0 01:INN\_CK 4464.00 18.060 No\_date 39:59 33.61 .380 .000  
13145+ [TnEC= 4.00: SMIN= 12.00: SMAX=350.79: SKw .010]  
13146+ [InterEventtime= 12.00]  
13147+ # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
13148+ # of 1.5  
13149+ R0100:00016-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13150+ CONTINUOUS\_NASHYD 1.0 01:INN\_CK 133.00 3.259 No\_date 28:57 34.39 .388 .000  
13152+ [CN= 63.0 N: 3.00: Tp: .80]  
13153+ [TnEC= 4.00: SMIN= 12.02: SMAX=396.11: SKw .010]  
13154+ [InterEventtime= 12.00]  
13156+ # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
13157+ # of 1.5  
13158+ R0100:00017-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13159+ CONTINUOUS\_NASHYD 1.0 01:INN\_CK 3197.00 16.421 No\_date 36:21 29.79 .336 .000  
13160+ [TnEC= 4.00: SMIN= 12.00: SMAX=350.79: SKw .010]  
13161+ [InterEventtime= 12.00]  
13164+ # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
13165+ # of 1.5  
13166+ R0100:00018-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13167+ CONTINUOUS\_NASHYD 1.0 01:INN\_CK 3197.00 21.238 No\_date 36:28 36.76 .415 .000  
13168+ [TnEC= 4.00: SMIN= 52.62: SMAX=350.79: SKw .010]  
13169+ [InterEventtime= 12.00]  
13173+ # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
13174+ # of 1.5  
13175+ R0100:00019-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13176+ CONTINUOUS\_NASHYD 1.0 01:INN\_CK 165.00 1.511 No\_date 33:01 37.57 .424 .000  
13177+ [CN= 67.0 N: 3.00: Tp: 4.18]  
13178+ [TnEC= 4.00: SMIN= 12.00: SMAX=336.97: SKw .010]  
13179+ [InterEventtime= 12.00]  
13180+ # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
13181+ # of 1.5  
13182+ R0100:00020-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13183+ CONTINUOUS\_NASHYD 1.0 01:INN\_CK 1332.00 10.882 No\_date 35:10 42.49 .480 .000  
13185+ [CN= 72.01 N: 3.00: Tp: 5.95]  
13186+ [TnEC= 4.00: SMIN= 7.95: SMAX=264.99: SKw .010]  
13187+ [InterEventtime= 12.00]  
13188+ R0100:00021-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13189+ CONTINUOUS\_NASHYD 1.0 01:INN\_CK 224.00 9.576 No\_date 28:44 47.62 .538 .000  
13190+ [CN= 77.0 N: 3.00: Tp: 7.51]  
13191+ [TnEC= 4.00: SMIN= 31.15: SMAX=207.66: SKw .010]  
13192+ [InterEventtime= 12.00]  
13193+ # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
13194+ # of 1.5  
13195+ R0100:00022-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13196+ CONTINUOUS\_NASHYD 1.0 01:INN\_CK 1412.00 15.184 No\_date 37:44 45.88 .518 .000  
13197+ [CN= 75.0 N: 3.00: Tp: 8.00]  
13198+ [TnEC= 4.00: SMIN= 14.46: SMAX=244.9: SKw .010]  
13199+ [InterEventtime= 12.00]  
13200+ # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
13201+ # of 1.5  
13202+ R0100:00023-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13203+ CONTINUOUS\_NASHYD 1.0 01:INN\_CK 20.00 1.097 No\_date 28:35 52.06 .588 .000  
13204+ [CN= 81.0 N: 3.00: Tp: .62]  
13205+ [TnEC= 4.00: SMIN= 12.00: SMAX=211. SMAX=168.09: SKw .010]  
13206+ [InterEventtime= 12.00]  
13208+ # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
13209+ # of 1.5  
13210+ R0100:00024-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13211+ CONTINUOUS\_NASHYD 1.0 01:INN\_CK 4945.00 52.058 No\_date 33:16 44.17 .499 .000  
13212+ [TnEC= 4.00: SMIN= 12.00: SMAX=211. SMAX=175.50: SKw .010]  
13213+ [InterEventtime= 12.00]  
13214+ # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
13215+ # of 1.5  
13216+ R0100:00025-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13217+ CONTINUOUS\_NASHYD 1.0 01:INN\_CK 585.00 14.993 No\_date 29:55 52.06 .588 .000  
13218+ [TnEC= 4.00: SMIN= 21.25: SMAX=168.09: SKw .010]  
13219+ [InterEventtime= 12.00]  
13220+ # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
13221+ # of 1.5  
13222+ R0100:00026-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13223+ CONTINUOUS\_NASHYD 1.0 01:INN\_CK 1021.00 19.782 No\_date 30:45 51.16 .578 .000  
13224+ [TnEC= 4.00: SMIN= 50.00: Tp: 2.46]  
13225+ [TnEC= 4.00: SMIN= 175.50: SKw .010]  
13226+ [InterEventtime= 12.00]  
13227+ # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
13228+ # of 1.5  
13229+ R0100:00027-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13230+ CONTINUOUS\_NASHYD 1.0 01:INN\_CK 1412.00 15.184 No\_date 37:44 45.88 .518 .000  
13231+ [CN= 75.0 N: 3.00: Tp: 5.95]  
13232+ [TnEC= 4.00: SMIN= 14.46: SMAX=244.9: SKw .010]  
13233+ [InterEventtime= 12.00]  
13234+ # The Tp was modified according to a Peak Reduction factor (NTO-Chart B2-4)  
13235+ # of 1.5  
13236+ R0100:00028-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13237+ CONTINUOUS\_NASHYD 1.0 01:INN\_CK 2737.00 40.730 No\_date 31:28 46.75 .528 .000  
13238+ [TnEC= 4.00: SMIN= 12.00: SMAX=207.66: SKw .010]  
13239+ [InterEventtime= 12.00]  
13240+ # Starting with the addition of Jock River Headwater and Subwatershed 13  
13241+ # Starting with the addition of Jock River Headwater and Subwatershed 13  
13242+ R0100:00030-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13243+ ADD HYD 1.0 01:INN\_CK 4945.00 52.058 No\_date 32:35 36.76 .415 .000  
13244+ [TnEC= 4.00: SMIN= 12.00: SMAX=211. SMAX=175.50: SKw .010]  
13245+ [InterEventtime= 12.00]  
13246+ R0100:00031-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13247+ ADD HYD 1.0 01:INN\_CK 4651.00 27.660 No\_date 35:21 34.69 n/a .000  
13248+ # Sum of hydrographs from Node 13 routed to Node 13a  
13249+ # (Appended cross-section - see cross-section 28)  
13250+ # Use n=0.04 for summer conditions and n=0.025 for spring conditions  
13251+ R0100:00032-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13252+ ROUTE CHANNEL > 1.0 01:INN\_CK 4651.00 27.660 No\_date 35:21 34.69 n/a .000  
13253+ [L/S=nw .022/.040]  
13254+ [Vmax=.7586:Emax=.1876]  
13258+ # Addition of Subwatershed 13 and Subwatershed 13a  
13259+ ROUTE RESERVOIR > 1.0 01:INN\_CK 7725.00 3.950 No\_date 62:26 32.14 n/a .000  
13260+ [MtdCoSed=.1796e+03 m3]  
13261+ R0100:00033-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13262+ ADD HYD 1.0 01:INN\_CK 4651.00 22.598 No\_date 38:56 34.69 n/a .000  
13263+ [L/S=nw .022/.040]  
13264+ [Vmax=.7586:Emax=.1876]  
13265+ # Addition of Subwatershed 13 and Subwatershed 13a  
13266+ ROUTE CHANNEL > 1.0 01:INN\_CK 4651.00 22.598 No\_date 38:56 34.69 n/a .000  
13267+ [L/S=nw .022/.040]  
13268+ [Vmax=.7586:Emax=.1876]  
13269+ # Addition of Subwatershed 13 and Subwatershed 13a  
13270+ ROUTE CHANNEL > 1.0 01:INN\_CK 7725.00 3.950 No\_date 62:26 32.14 n/a .000  
13271+ [MtdCoSed=.1796e+03 m3]  
13272+ R0100:00034-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13273+ ADD HYD 1.0 01:INN\_CK 7725.00 3.950 No\_date 62:26 32.14 n/a .000  
13274+ [L/S=nw .022/.040]  
13275+ [Vmax=.7586:Emax=.1876]  
13276+ # Addition of Subwatershed 13 and Subwatershed 13a  
13277+ [L/S=nw .022/.040]  
13278+ [Vmax=.7586:Emax=.1876]  
13279+ # Insertion of a reservoir to simulate the effects of the Goodwood Marsh  
13280+ R0100:00035-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13281+ ROUTE CHANNEL > 1.0 01:INN\_CK 7725.00 3.947 No\_date 64:43 32.14 n/a .000  
13282+ [L/S=nw .022/.040]  
13283+ [Vmax=.7586:Emax=.1876]  
13284+ # Addition of Subwatershed Jock River at Ashton to Node 12  
13285+ # Sum of hydrographs from Node 12 routed to Node 12  
13286+ # (Appended cross-section - see cross-section 28)  
13287+ # Use n=0.04 for summer conditions and n=0.025 for spring conditions  
13288+ # Sum of hydrographs from Node 12 routed to Node 11  
13289+ # (Appended cross-section - see cross-section 28)  
13290+ # Addition of Subwatershed Jock River at Ashton to Node 11  
13291+ ROUTE CHANNEL > 1.0 01:INN\_CK 7725.00 3.947 No\_date 64:43 32.14 n/a .000  
13292+ ADD HYD 1.0 02:INN12 7725.00 21.745 No\_date 32:41 34.08 n/a .000  
13293+ [L/S=nw .022/.040]  
13294+ [Vmax=.7586:Emax=.1876]  
13295+ # remark:flow at S\_N12 near Ashton  
13296+ # Sum of hydrographs from Node 12 routed to Node 11  
13297+ # (Sum of hydrographs from Node 12 routed to Node 11  
13298+ # (Appended cross-section - see cross-section 28)  
13299+ # Use n=0.04 for summer conditions and n=0.025 for spring conditions  
13300+ # Addition of Subwatershed Jock River at Ashton to Node 11  
13301+ # Sum of hydrographs from Node 12 routed to Node 11  
13302+ # (Appended cross-section - see cross-section 28)  
13303+ R0100:00036-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13304+ ROUTE CHANNEL > 1.0 01:INN\_CK 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13305+ [RDW 1.00] out< 1.0 01:Dm11 9506.00 21.522 No\_date 32:57 34.08 n/a .000  
13306+ [L/S=nw .022/.040]  
13307+ [Vmax=.7586:Emax=.1876]  
13308+ # Addition of Subwatershed 11 and No Name Creek to Node 11  
13309+ R0100:00037-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13310+ ROUTE CHANNEL > 1.0 01:INN\_CK 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13311+ ADD HYD 1.0 02:INN12 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13312+ [L/S=nw .022/.040]  
13313+ [Vmax=.7586:Emax=.1876]  
13314+ # Addition of Subwatershed 11 and No Name Creek to Node 11  
13315+ R0100:00038-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13316+ ROUTE CHANNEL > 1.0 01:INN\_CK 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13317+ ADD HYD 1.0 02:INN12 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13318+ [L/S=nw .022/.040]  
13319+ [Vmax=.7586:Emax=.1876]  
13320+ # Addition of Subwatershed 11 and No Name Creek to Node 11  
13321+ R0100:00039-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13322+ ROUTE CHANNEL > 1.0 01:INN\_CK 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13323+ ADD HYD 1.0 02:INN12 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13324+ [L/S=nw .022/.040]  
13325+ [Vmax=.7586:Emax=.1876]  
13326+ # Addition of Subwatershed 11 and No Name Creek to Node 11  
13327+ R0100:00040-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13328+ ROUTE CHANNEL > 1.0 01:INN\_CK 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13329+ ADD HYD 1.0 02:INN12 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13330+ [L/S=nw .022/.040]  
13331+ [Vmax=.7586:Emax=.1876]  
13332+ # Addition of Subwatershed 11 and No Name Creek to Node 11  
13333+ R0100:00041-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13334+ ROUTE CHANNEL > 1.0 01:INN\_CK 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13335+ ADD HYD 1.0 02:INN12 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13336+ # Sum of hydrographs from Node 11 routed to Node 10  
13337+ R0100:00042-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13338+ ROUTE CHANNEL > 1.0 01:INN\_CK 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13339+ ADD HYD 1.0 02:INN12 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13340+ [L/S=nw .022/.040]  
13341+ [Vmax=.7586:Emax=.1876]  
13342+ # Addition of Subwatershed 11 and No Name Creek to Node 10  
13343+ R0100:00043-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13344+ ROUTE CHANNEL > 1.0 01:INN\_CK 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13345+ ADD HYD 1.0 02:INN12 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13346+ [L/S=nw .022/.040]  
13347+ [Vmax=.7586:Emax=.1876]  
13348+ # Addition of Subwatershed 11 and No Name Creek to Node 10  
13349+ R0100:00044-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13350+ ROUTE CHANNEL > 1.0 01:INN\_CK 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13351+ ADD HYD 1.0 02:INN12 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13352+ # Addition of Subwatershed 11 and Nichols Creek to Node 9  
13353+ R0100:00045-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13354+ ROUTE CHANNEL > 1.0 01:INN\_CK 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13355+ ADD HYD 1.0 02:INN12 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13356+ [L/S=nw .022/.040]  
13357+ [Vmax=.7586:Emax=.1876]  
13358+ # Addition of Subwatershed 11 and Nichols Creek to Node 9  
13359+ R0100:00046-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13360+ ROUTE CHANNEL > 1.0 01:INN\_CK 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13361+ ADD HYD 1.0 02:INN12 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13362+ [L/S=nw .022/.040]  
13363+ [Vmax=.7586:Emax=.1876]  
13364+ # Addition of Subwatershed 11 and Nichols Creek to Node 9  
13365+ R0100:00047-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13366+ ROUTE CHANNEL > 1.0 01:INN\_CK 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13367+ ADD HYD 1.0 02:INN12 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13368+ [L/S=nw .022/.040]  
13369+ [Vmax=.7586:Emax=.1876]  
13370+ # Insertion of a reservoir to simulate the effects of the Goodwood Marsh  
13371+ R0100:00048-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13372+ ROUTE CHANNEL > 1.0 01:INN\_CK 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13373+ ADD HYD 1.0 02:INN12 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13374+ [L/S=nw .022/.040]  
13375+ [Vmax=.7586:Emax=.1876]  
13376+ # Addition of Subwatershed 11 and Subwatershed 5 and Flowing Creek to Node 6  
13377+ R0100:00049-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13378+ ROUTE CHANNEL > 1.0 01:INN\_CK 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13379+ ADD HYD 1.0 02:INN12 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13380+ [L/S=nw .022/.040]  
13381+ [Vmax=.7586:Emax=.1876]  
13382+ # Addition of Subwatershed 11 and Subwatershed 5 and Flowing Creek to Node 6  
13383+ R0100:00050-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13384+ ROUTE CHANNEL > 1.0 01:INN\_CK 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13385+ ADD HYD 1.0 02:INN12 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13386+ [L/S=nw .022/.040]  
13387+ [Vmax=.7586:Emax=.1876]  
13388+ # Addition of Subwatershed 11 and Subwatershed 5 and Flowing Creek to Node 6  
13389+ R0100:00051-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13390+ ROUTE CHANNEL > 1.0 01:INN\_CK 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13391+ ADD HYD 1.0 02:INN12 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13392+ [L/S=nw .022/.040]  
13393+ [Vmax=.7586:Emax=.1876]  
13394+ # Addition of Subwatershed 11 and Subwatershed 5 and Flowing Creek to Node 6  
13395+ R0100:00052-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13396+ ROUTE CHANNEL > 1.0 01:INN\_CK 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13397+ ADD HYD 1.0 02:INN12 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13398+ [L/S=nw .022/.040]  
13399+ [Vmax=.7586:Emax=.1876]  
13400+ # Addition of Subwatershed 11 and Subwatershed 5 and Flowing Creek to Node 6  
13401+ R0100:00053-----Dtnin-ID:NHYD---ARRAha-QPEAKcms-TpeakDate\_bh:mm---RVm=R..C...--DFCms  
13402+ ROUTE CHANNEL > 1.0 01:INN\_CK 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13403+ ADD HYD 1.0 02:INN12 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
13404+ [L/S=nw .022/.040]  
13405+ [Vmax=.7586:Emax=.1876]  
13406+ # Addition of Subwatershed 11 and Subwatershed 5 and Flowing Creek to Node 6  
13407+ R01

13465+ #

13466+ R0100:CO0058-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13467+ ROUTE CHANNEL -> 1. 0 02S\_NSA 46841.01 85.756 No\_date 34:18 37.51 n/a .000

13468+ [ROT: 1.001\*] 1. 0 01N4A 46841.01 85.943 No\_date 36:10 37.51 n/a .000

13469+ [L/S/nr\_ 4630 .. /043..035] .000

13470+ [Vmax\_ .504 Dmax\_ 3.864]

13471+ #

13472+ # Addition of Subwatershed 4 and Leamy Creek to Node 4

13473+ #

13474+ R0100:CO0060-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13475+ ADD HYD + 1. 0 02SM\_1 46841.01 85.756 No\_date 34:18 37.51 n/a .000

13476+ 1. 0 02SM\_2 585.00 14.933 No\_date 29:55 52.67 n/a .000

13477+ 1. 0 021M\_CW 1021.00 19.782 No\_date 30:145 51.16 n/a .000

13478+ 1. 0 021M\_S 80M.. 1. 0 01S\_N 48447.00 96.618 No\_date 35:12 37.97 n/a .000

13479+ R0100:CO0061-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13480+ SAVE HYD 1. 0 01S\_N 48447.00 96.618 No\_date 35:12 37.97 n/a .000

13481+ fname: S\_N4\_0100

13482+ remark:f1ow at S\_N4

13483+ #

13484+ # Sum of hydrographs from Node 4 routed to Node 2

13485+ R0100:CO0062-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13486+ ADD HYD + 1. 0 02S\_N 48447.00 96.618 No\_date 35:12 37.97 n/a .000

13487+ ROUTE CHANNEL -> 1. 0 021S\_N 48447.00 96.618 No\_date 35:12 37.97 n/a .000

13488+ [ROT: 1.001\*] 1. 0 01N2 48447.00 96.322 No\_date 35:13 37.97 n/a .000

13489+ [L/S/nr\_ 4630 .. /043..035] .000

13490+ [Vmax\_ .944 Dmax\_ 3.928]

13491+ #

13492+ # Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2

13493+ #

13494+ R0100:CO0063-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13495+ ADD HYD + 1. 0 02N1 48447.00 96.322 No\_date 38:13 37.97 n/a .000

13496+ 1. 0 02SM\_2 7.567 7.567 No\_date 28:44 47.62 n/a .000

13497+ 1. 0 021M\_DR 1122.00 17.981 No\_date 31:142 52.06 n/a .000

13498+ 1. 0 021M\_S 80M.. 1. 0 01S\_N 52483.00 143.580 No\_date 32:59 38.76 n/a .000

13499+ R0100:CO0064-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13500+ SAVE HYD 1. 0 01S\_N 52483.00 143.580 No\_date 32:59 38.76 n/a .000

13501+ fname: H\_EN2

13502+ remark:f1ow at S\_M2 Jock River Gauge at Moodie Dr.

13503+ #

13504+ # Sum of hydrographs from Node 2 routed to Node 1

13505+ R0100:CO0065-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13506+ # Section 10

13507+ #

13508+ #

13509+ #

13510+ # Hydrograph from Node 2 routed to Node 416

13512+ # Channel X-Section obtained from RvCA Hydraulic Model - Station 9025

13513+ #

13514+ R0100:CO0065-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13515+ ROUTE CHANNEL -> 1. 0 02S\_N 2 52483.00 143.580 No\_date 32:159 38.76 n/a .000

13516+ [ROT: 1.001\*] 1. 0 01N4A 52483.00 139.298 No\_date 33:145 38.76 n/a .000

13517+ [L/S/nr\_ 2327 .. /050..065] .000

13518+ [Vmax\_ .801 Dmax\_ 3.814]

13519+ #

13520+ # Catchment SW\_1a

13521+ # - Portion of RVCA catchment SW\_1 outside of Reach 1 subwatershed

13522+ #

13523+ #

13524+ R0100:CO0066-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13525+ CONTINOUS\_NASHYD 1. 0 01O1-A 52483.00 139.298 No\_date 31:14 40.95 .462 .000

13526+ [ROT: 1.001\*] 1. 0 01N4A 52483.00 139.298 No\_date 31:14 40.95 .462 .000

13527+ [TaREC\_ 4.00 SINM\_ 39.75 SMAX\_264..99 SK\_ .010]

13528+ R0100:CO0067-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13529+ CONTINUOUS\_NASHYD 1. 0 01O1-A 49.93 1. 44N 29:06 45.95 .519 .000

13530+ [TaREC\_ 4.00 SINM\_ 1.15 SMAX\_207..66 SK\_ .010]

13531+ [TaREC\_ 4.00 SINM\_ 1.15 SMAX\_207..66 SK\_ .010]

13532+ [TaREC\_ 4.00 SINM\_ 1.15 SMAX\_207..66 SK\_ .010]

13533+ [InterEventTime\_ 12.00]

13534+ R0100:CO0068-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13535+ ADD HYD 1. 0 02N1 52483.00 139.298 No\_date 33:45 38.76 n/a .000

13536+ 1. 0 02SM\_1 536.42 7.274 No\_date 31:14 40.95 n/a .000

13537+ 1. 0 021M\_DR 1. 0 01N4A 53643.00 143.580 No\_date 32:59 38.76 n/a .000

13538+ SUM\_ 1. 0 01N4A 53643.00 143.580 No\_date 33:31 38.79 n/a .000

13539+ R0100:CO0069-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13540+ SAVE HYD 1. 0 01N4A 53643.00 143.580 No\_date 33:31 38.79 n/a .000

13541+ fname: SN\_41N\_0100

13542+ remark: Total Flows at Highway 416

13543+ #

13544+ # Hydrograph from Node 416 routed to Node at Koekefdrain

13545+ # Channel X-Section obtained from RvCA Hydraulic Model - Station 7245

13546+ #

13547+ R0100:CO0070-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13548+ ROUTE CHANNEL -> 1. 0 02S\_N 416 53064.36 145.020 No\_date 33:31 38.76 n/a .000

13549+ [ROT: 1.001\*] 1. 0 01N4A 53064.36 144.944 No\_date 33:32 38.79 n/a .000

13550+ [L/S/nr\_ 497 .. /302..058] .000

13551+ [Vmax\_ 1.728 Dmax\_ 3.267]

13552+ #

13553+ # Catchment OKERFE

13554+ # - S\_OKEERFE (north of the Jock)

13555+ # Depth assumed as 43m imp.

13556+ # - 202-12-01 add Okeeffe model (Area 513.02 HA) instead of current Okeeffe (Area 513.02 HA)

13557+ # - 202-12-01 add Okeeffe model (Area 513.02 HA) instead of current Okeeffe (Area 513.02 HA)

13558+ #

13559+ R0100:CO0071-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13560+ CONTINUOUS\_NASHYD 1. 0 01O1 63.72 1. 380 No\_date 28:58 30.74 .347 .000

13561+ [ROT: 1.001\*] 1. 0 01N4A 63.72 1. 380 No\_date 28:58 30.74 .347 .000

13562+ [TaREC\_ 4.00 SINM\_ 64.50 SMAX\_430..01 SK\_ .010]

13563+ [InterEventTime\_ 12.00]

13564+ R0100:CO0074-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13565+ ROUTE CHANNEL -> 1. 0 02O1-O 63.72 1. 380 No\_date 28:58 30.74 n/a .000

13566+ [ROT: 1.001\*] 1. 0 01N4A 63.72 1. 380 No\_date 29:13 30.74 n/a .000

13567+ [L/S/nr\_ 960 .. /630..043] .000

13568+ [Vmax\_ .926 Dmax\_ .493]

13569+ R0100:CO0075-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13570+ CONTINUOUS\_NASHYD 1. 0 01O1-2 28.61 .485 No\_date 29:13 28.38 .320 .000

13571+ [Cn\_ 57.70 N\_ 3.00 Tp\_ 1.10]

13572+ [TaREC\_ 4.00 SINM\_ 57.70 SMAX\_808..81 SK\_ .010]

13573+ [InterEventTime\_ 12.00]

13574+ R0100:CO0074-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13575+ ROUTE CHANNEL -> 1. 0 02O1-O 63.72 1. 380 No\_date 28:58 30.74 n/a .000

13576+ [ROT: 1.001\*] 1. 0 01N4A 63.72 1. 380 No\_date 29:13 30.74 n/a .000

13577+ [L/S/nr\_ 960 .. /630..043] .000

13578+ [Vmax\_ .926 Dmax\_ .493]

13579+ R0100:CO0075-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13580+ ADD HYD 1. 0 02O1-O 63.72 1. 380 No\_date 29:13 30.74 n/a .000

13581+ 1. 0 02SM\_1 39.67 1. 454 No\_date 28:58 30.74 .347 .000

13582+ 1. 0 021O-2 46.94 .650 No\_date 28:59 21.79 n/a .000

13583+ SUM\_ 1. 0 01O1 46.94 .650 No\_date 28:59 21.79 n/a .000

13584+ R0100:CO0076-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13585+ ROUTE CHANNEL -> 1. 0 02O1-N 63.72 1. 380 No\_date 28:58 30.74 n/a .000

13586+ [ROT: 1.001\*] 1. 0 01N4A 63.72 1. 380 No\_date 29:13 30.74 n/a .000

13587+ [L/S/nr\_ 960 .. /630..043] .000

13588+ [Vmax\_ .926 Dmax\_ .493]

13589+ R0100:CO0077-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13590+ CONTINUOUS\_NASHYD 1. 0 01O1-6 36.46 .220 No\_date 28:45 18.67 .211 .000

13591+ [Cn\_ 43.01 N\_ 3.00 Tp\_ .70]

13592+ [TaREC\_ 4.01 SINM\_ 43.01 SMAX\_697..25 SK\_ .010]

13593+ [InterEventTime\_ 12.00]

13594+ R0100:CO0078-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13595+ CONTINUOUS\_NASHYD 1. 0 01O1-5 39.67 1. 454 No\_date 28:21 32.90 .375 .000

13596+ [KIND\_ 15..TIME\_ 1.00]

13597+ [L/S/nr\_ 2 .. /CNM\_ 50.00] .000

13598+ [TaREC\_ 4.00 SINM\_ 46.77 SMAX\_500..01 SK\_ .010]

13599+ [InterEventTime\_ 12.00]

13600+ R0100:CO0079-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13601+ [TaREC\_ 4.00 SINM\_ 49.77 SMAX\_667..25 SK\_ .010]

13602+ R0100:CO0078-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13603+ CONTINUOUS\_NASHYD 1. 0 01O1-5 60.63 3. 669 No\_date 28:10 38.00 .429 .000

13604+ [KIND\_ 13..TIME\_ 1.00]

13605+ [SMID\_ 64.50 SMAX\_430..01 SK\_ .010]

13606+ [TaREC\_ 4.00 SINM\_ 64.50 SMAX\_500..01 SK\_ .010]

13607+ [TaREC\_ 4.00 SINM\_ 64.50 SMAX\_500..01 SK\_ .010]

13608+ [TaREC\_ 4.00 SINM\_ 64.50 SMAX\_500..01 SK\_ .010]

13609+ [TaREC\_ 4.00 SINM\_ 64.50 SMAX\_500..01 SK\_ .010]

13610+ R0100:CO0080-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13611+ ADD HYD 1. 0 02O1-N 39.67 1. 454 No\_date 28:21 32.90 n/a .000

13612+ 1. 0 02SM\_1 60.63 .220 No\_date 28:21 32.90 n/a .000

13613+ 1. 0 021O-6 16.46 .220 No\_date 28:45 18.67 n/a .000

13614+ SUM\_ 1. 0 01P1 256.05 5. 930 No\_date 28:19 30.11 n/a .000

13615+ R0100:CO0081-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13616+ CONTINUOUS\_NASHYD 1. 0 01O1-7 8.28 .117 No\_date 28:37 25.18 .284 .000

13617+ [Cn\_ 54.00 N\_ 3.00 Tp\_ .60]

13618+ [TaREC\_ 4.00 SINM\_ 54.00 SMAX\_500..07 SK\_ .010]

13619+ [InterEventTime\_ 12.00]

13620+ R0100:CO0082-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13621+ ADD HYD 1. 0 02O1-N 19.27 2. 423 No\_date 29:12 27.24 n/a .000

13622+ 1. 0 02SM\_1 29.08 .117 No\_date 28:19 30.11 n/a .000

13623+ 1. 0 021O-7 5.28 .117 No\_date 28:37 25.16 n/a .000

13624+ SUM\_ 1. 0 01P1 261.38 6. 038 No\_date 28:19 30.06 n/a .000

13625+ R0100:CO0083-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13626+ ROUTE CHANNEL -> 1. 0 02O1-F 261.31 6. 038 No\_date 28:19 30.01 n/a .000

13627+ [ROT: 1.001\*] 1. 0 01DRAIN 261.31 5. 843 No\_date 28:12 30.01 n/a .000

13628+ [TaREC\_ 4.00 SINM\_ 84.00 SMAX\_84..00 SK\_ .010]

13629+ [TaREC\_ 4.00 SINM\_ 84.00 SMAX\_84..00 SK\_ .010]

13630+ [TaREC\_ 4.00 SINM\_ 84.00 SMAX\_84..00 SK\_ .010]

13631+ [TaREC\_ 4.00 SINM\_ 84.00 SMAX\_84..00 SK\_ .010]

13632+ [TaREC\_ 4.00 SINM\_ 84.00 SMAX\_84..00 SK\_ .010]

13633+ [TaREC\_ 4.00 SINM\_ 84.00 SMAX\_84..00 SK\_ .010]

13634+ [TaREC\_ 4.00 SINM\_ 84.00 SMAX\_84..00 SK\_ .010]

13635+ R0100:CO0085-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13636+ CONTINUOUS\_NASHYD 1. 0 01A1 2.50 .572 No\_date 28:01 70.42 n/a .000

13637+ [Horton parameters: Po\_ 76.20 Fpc\_ 13.20 DCNv4..14: F\_ .001]

13638+ [TaREC\_ 4.00 SINM\_ 76.20 SMAX\_84..00 SK\_ .010]

13639+ [TaREC\_ 4.00 SINM\_ 76.20 SMAX\_84..00 SK\_ .010]

13640+ [TaREC\_ 4.00 SINM\_ 76.20 SMAX\_84..00 SK\_ .010]

13641+ [TaREC\_ 4.00 SINM\_ 76.20 SMAX\_84..00 SK\_ .010]

13642+ R0100:CO0086-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13643+ ROUTE RESERVOIR -> 1. 0 02AI-STR 2.50 .173 No\_date 28:17 70.42 n/a .000

13644+ [TaREC\_ 4.00 SINM\_ 76.20 SMAX\_84..00 SK\_ .010]

13645+ [TaREC\_ 4.00 SINM\_ 76.20 SMAX\_84..00 SK\_ .010]

13646+ [McGColleod\_ 77465..01 m3 TotVolVol\_ 0.000 m3 N-Ovfr\_ 0. hrufr\_ 0. hrs]

13647+ R0100:CO0087-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13648+ CONTINUOUS\_NASHYD 1. 0 01ST-2 .59 .115 No\_date 28:00 55.76 .630 .000

13649+ [KIND\_ 46..TIME\_ 57]

13650+ [Horton parameters: Po\_ 76.20 Fpc\_ 13.20 DCNv4..14: F\_ .001]

13651+ [TaREC\_ 4.00 SINM\_ 76.20 SMAX\_84..00 SK\_ .010]

13652+ R0100:CO0088-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13653+ ADD HYD 1. 0 02O1-N 19.27 2. 423 No\_date 29:12 27.24 n/a .000

13654+ 1. 0 02SM\_1 29.08 .117 No\_date 28:19 30.11 n/a .000

13655+ 1. 0 021O-6 16.46 .220 No\_date 28:45 18.67 n/a .000

13656+ SUM\_ 1. 0 01P1 256.05 5. 930 No\_date 28:19 30.11 n/a .000

13657+ R0100:CO0089-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13658+ CONTINUOUS\_NASHYD 1. 0 01O1-7 8.28 .117 No\_date 28:37 25.18 .284 .000

13659+ [Cn\_ 54.00 N\_ 3.00 Tp\_ .60]

13660+ [TaREC\_ 4.00 SINM\_ 54.00 SMAX\_500..07 SK\_ .010]

13661+ [TaREC\_ 4.00 SINM\_ 54.00 SMAX\_500..07 SK\_ .010]

13662+ [TaREC\_ 4.00 SINM\_ 54.00 SMAX\_500..07 SK\_ .010]

13663+ [TaREC\_ 4.00 SINM\_ 54.00 SMAX\_500..07 SK\_ .010]

13664+ [TaREC\_ 4.00 SINM\_ 54.00 SMAX\_500..07 SK\_ .010]

13665+ [TaREC\_ 4.00 SINM\_ 54.00 SMAX\_500..07 SK\_ .010]

13666+ R0100:CO0090-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13667+ ADD HYD 1. 0 02O1-N 19.27 2. 423 No\_date 29:12 27.24 n/a .000

13668+ 1. 0 02SM\_1 29.08 .117 No\_date 28:19 30.11 n/a .000

13669+ 1. 0 021O-6 16.46 .220 No\_date 28:45 18.67 n/a .000

13670+ SUM\_ 1. 0 01P1 256.05 5. 930 No\_date 28:19 30.11 n/a .000

13671+ R0100:CO0091-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13672+ CONTINUOUS\_NASHYD 1. 0 01O1-8 2.50 .572 No\_date 28:01 70.42 n/a .000

13673+ [Cn\_ 66.01 N\_ 3.00 Tp\_ .73]

13674+ [TaREC\_ 4.00 SINM\_ 66.01 SMAX\_66..21 SK\_ .010]

13675+ [TaREC\_ 4.00 SINM\_ 66.01 SMAX\_66..21 SK\_ .010]

13676+ [TaREC\_ 4.00 SINM\_ 66.01 SMAX\_66..21 SK\_ .010]

13677+ R0100:CO0092-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13678+ CONTINUOUS\_NASHYD 1. 0 01O1-8 2.50 .572 No\_date 28:01 70.42 n/a .000

13679+ [Cn\_ 66.01 N\_ 3.00 Tp\_ .73]

13680+ [TaREC\_ 4.00 SINM\_ 66.01 SMAX\_66..21 SK\_ .010]

13681+ [TaREC\_ 4.00 SINM\_ 66.01 SMAX\_66..21 SK\_ .010]

13682+ R0100:CO0093-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13683+ ADD HYD 1. 0 02O1-N 19.27 2. 423 No\_date 29:12 27.24 n/a .000

13684+ 1. 0 02SM\_1 29.08 .117 No\_date 28:19 30.11 n/a .000

13685+ 1. 0 021O-6 16.46 .220 No\_date 28:45 18.67 n/a .000

13686+ SUM\_ 1. 0 01P1 256.05 5. 930 No\_date 28:19 30.11 n/a .000

13687+ R0100:CO0094-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13688+ CONTINUOUS\_NASHYD 1. 0 01O1-9 2.50 .572 No\_date 28:01 70.42 n/a .000

13689+ [Cn\_ 66.01 N\_ 3.00 Tp\_ .73]

13690+ [TaREC\_ 4.00 SINM\_ 66.01 SMAX\_66..21 SK\_ .010]

13691+ [TaREC\_ 4.00 SINM\_ 66.01 SMAX\_66..21 SK\_ .010]

13692+ R0100:CO0095-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13693+ ADD HYD 1. 0 02O1-N 19.27 2. 423 No\_date 29:12 27.24 n/a .000

13694+ 1. 0 02SM\_1 29.08 .117 No\_date 28:19 30.11 n/a .000

13695+ 1. 0 021O-6 16.46 .220 No\_date 28:45 18.67 n/a .000

13696+ SUM\_ 1. 0 01P1 256.05 5. 930 No\_date 28:19 30.11 n/a .000

13697+ R0100:CO0096-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13698+ CONTINUOUS\_NASHYD 1. 0 01O1-10 2.50 .572 No\_date 28:01 70.42 n/a .000

13699+ [Cn\_ 66.01 N\_ 3.00 Tp\_ .73]

13700+ [TaREC\_ 4.00 SINM\_ 66.01 SMAX\_66..21 SK\_ .010]

13701+ [TaREC\_ 4.00 SINM\_ 66.01 SMAX\_66..21 SK\_ .010]

13702+ R0100:CO0097-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13703+ ADD HYD 1. 0 02O1-N 19.27 2. 423 No\_date 29:12 27.24 n/a .000

13704+ 1. 0 02SM\_1 29.08 .117 No\_date 28:19 30.11 n/a .000

13705+ 1. 0 021O-6 16.46 .220 No\_date 28:45 18.67 n/a .000

13706+ SUM\_ 1. 0 01P1 256.05 5. 930 No\_date 28:19 30.11 n/a .000

13707+ R0100:CO0098-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13708+ CONTINUOUS\_NASHYD 1. 0 01O1-11 2.50 .572 No\_date 28:01 70.42 n/a .000

13709+ [Cn\_ 66.01 N\_ 3.00 Tp\_ .73]

13710+ [TaREC\_ 4.00 SINM\_ 66.01 SMAX\_66..21 SK\_ .010]

13711+ [TaREC\_ 4.00 SINM\_ 66.01 SMAX\_66..21 SK\_ .010]

13712+ R0100:CO0099-----Dtnin:ID:HYND-----ARAAh-QPEAKcms-TpeakDate\_bh:---RvNm-R.C.---DFWfms

13713+ ADD HYD 1.

13839+ remark:SMWF-A Inflow  
 13840+ R0100:CO0119- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13841+ ROUTE RESERVOIR -> 1. 0 02:AREAS-  
 13842+ out < 1. 0 01:SMWF-A 66.75 . 5,345 . No\_date 28:08 67.64 n/a .000  
 13843+ overlaid < 1. 0 01:SMWF-A 66.75 . 1,357 . No\_date 29:10 67.64 n/a .000  
 13844+ [MastCoWed\_30518-E01 m3\_TotDrvVol\_0.000E+00 m3\_N-Ovr- 0 .TotDrvVol< 0 .hrs]<  
 13845+ R0100:CO0120- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13846+ SAVV HYD 1. 0 01:SMWF-A 66.75 . 1,357 . No\_date 29:10 67.64 n/a .000  
 13847+ fwm:SMWF-A 0.100  
 13848+ remark:SMWF-A Outflow  
 13849+ R0100:CO0121- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13850+ ADD HYD + 1. 0 02:SMWF-A 66.75 . 1,357 . No\_date 29:10 67.64 n/a .000  
 13851+ overlaid < 1. 0 01:SMWF-A 66.75 . 1,357 . No\_date 29:10 67.64 n/a .000  
 13852+ SUM- 1. 0 01:PTP457C 431.09 . 9,279 . No\_date 29:07 40.92 n/a .000  
 13853+ [INP: 1. 0 01:PTP457C 431.09 . 9,279 . No\_date 29:07 40.92 n/a .000  
 13854+ R0100:CO0122- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13855+ CONTINUOUS STANDYD 1. 0 01:C6-  
 13856+ [XINP= 687:TIME= .85]  
 13857+ [Horton parameters: Po= 76.20; C= 1.3; LD=0.00; Tp= 1.14; F= .00] .000  
 13858+ [INP: 1. 0 01:PTP457C 431.09 . 9,279 . No\_date 29:07 40.92 n/a .000  
 13859+ [Impervious area: IAImp= 1. 571:SLD1=.50:LGD1 193.:MMI=.013:SCI=.01]  
 13860+ [iAEcImp= 4.00: iARECper= 4.00]  
 13861+ R0100:CO0123- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13862+ ROUTE RESERVOIR -> 1. 0 02:C6-  
 13863+ out < 1. 0 01:CT-STR 1.87 . 381 . No\_date 28:01 70.42 n/a .000  
 13864+ overlaid < 1. 0 01:CT-STR 1.87 . 381 . No\_date 28:01 70.42 n/a .000  
 13865+ [MastCoWed\_50454-E01 m3\_TotDrvVol\_0.000E+00 m3\_N-Ovr- 0 .TotDrvVol< 0 .hrs]<  
 13866+ R0100:CO0124- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13867+ SAVV HYD 1. 0 01:CT-STR 1.87 . 381 . No\_date 28:00 70.42 .795 .000  
 13868+ [XINP= 687:TIME= .85]  
 13869+ [Horton parameters: Po= 76.20; C= 1.3; LD=0.00; Tp= 1.14; F= .00] .000  
 13870+ [INP: 1. 0 01:PTP457C 431.09 . 9,279 . No\_date 28:00 70.42 n/a .000  
 13871+ [Impervious area: IAImp= 1. 571:SLD1=.50:LGD1 180.:MMI=.013:SCI=.01]  
 13872+ [iAEcImp= 4.00: iARECper= 4.00]  
 13873+ R0100:CO0125- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13874+ ROUTE RESERVOIR -> 1. 0 02:CT-  
 13875+ out < 1. 0 01:CT-STR 1.62 . 381 . No\_date 28:00 55.78 n/a .000  
 13876+ overlaid < 1. 0 01:CT-STR 1.62 . 381 . No\_date 28:00 55.78 n/a .000  
 13877+ [MastCoWed\_50366-E01 m3\_TotDrvVol\_0.000E+00 m3\_N-Ovr- 0 .TotDrvVol< 0 .hrs]<  
 13878+ R0100:CO0126- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13879+ CONTINUOUS STANDYD 1. 0 01:C6-  
 13880+ [XINP= 46:TIME= .57]  
 13881+ [Horton parameters: Po= 76.20; C= 1.3; LD=0.00; Tp= 1.14; F= .00] .000  
 13882+ [INP: 1. 0 01:PTP457C 431.09 . 9,279 . No\_date 28:00 55.78 n/a .000  
 13883+ [Impervious area: IAImp= 1. 571:SLD1=.50:LGD1 91.:MMI=.013:SCI=.01]  
 13884+ [iAEcImp= 4.00: iARECper= 4.00]  
 13885+ R0100:CO0127- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13886+ ROUTE RESERVOIR -> 1. 0 02:ST-  
 13887+ out < 1. 0 01:CT-STR 1.62 . 381 . No\_date 28:00 40.97 n/a .000  
 13888+ overlaid < 1. 0 01:CT-STR 1.62 . 381 . No\_date 28:00 40.97 n/a .000  
 13889+ [MastCoWed\_33787-E02 m3\_TotDrvVol\_0.000E+00 m3\_N-Ovr- 0 .TotDrvVol< 0 .hrs]<  
 13890+ R0100:CO0128- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13891+ ADD HYD + 1. 0 02:PT457C 433.01 . 9,279 . No\_date 29:07 40.97 n/a .000  
 13892+ overlaid < 1. 0 02:CT-STR 1.87 . 129 . No\_date 28:16 70.42 n/a .000  
 13893+ overlaid < 1. 0 02:CT-STR 1.87 . 129 . No\_date 28:16 70.42 n/a .000  
 13894+ overlaid < 1. 0 02:CT-STR 1.62 . 112 . No\_date 28:16 70.42 n/a .000  
 13895+ overlaid < 1. 0 02:CT-STR 1.62 . 112 . No\_date 28:16 55.78 n/a .000  
 13896+ overlaid < 1. 0 02:CT-STR 1.62 . 112 . No\_date 28:16 55.78 n/a .000  
 13897+ overlaid < 1. 0 02:ST650W 1.00 . 0 . No\_date 0:00 0:n/a .000  
 13898+ SUM- 1. 0 01:PT575C 434.92 . 9,426 . No\_date 29:06 40.97 n/a .000  
 13899+ R0100:CO0129- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13900+ ROUTE CHANNEL -> 1. 0 02:PT575C 434.92 . 9,426 . No\_date 29:06 40.97 n/a .000  
 13901+ [RDW= 1. 00] out-> 1. 0 01:DRAIN5 434.92 . 9,426 . No\_date 29:16 40.97 n/a .000  
 13902+ [INP: 1. 0 01:DRAIN5 434.92 . 9,426 . No\_date 29:16 40.97 n/a .000  
 13903+ [Vmax=.507:Dmax=.1619]  
 13904+ R0100:CO0130- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13905+ CONTINUOUS STANDYD 1. 0 01:CT-  
 13906+ [INP: 88.01:Tp=.57]:[Po=.60]  
 13907+ [iAEc 4.00: SMIN= 14.94: SMAK= 99.61: SK=.010]  
 13908+ [INP: 1. 0 01:PTP457C 434.92 . 9,426 . No\_date 28:33 57.07 .644 .000  
 13909+ R0100:CO0131- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13910+ CONTINUOUS STANDYD 1. 0 01:Area-B 24.04 . 4,871 . No\_date 28:02 66.17 .747 .000  
 13911+ [INP: 1. 0 01:Area-B 24.04 . 4,871 . No\_date 28:02 66.17 .747 .000  
 13912+ [Horton parameters: Po= 76.20; C= 1.3; LD=0.00; Tp= 1.14; F= .00] .000  
 13913+ [Pervious area: IAImp= 4.67:SLP9=1.40:LDP9=.50:HNG=.250:SCP=.01]  
 13914+ [iAEcImp= 4.00: iARECper= 4.00]  
 13915+ R0100:CO0132- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13916+ CONTINUOUS STANDYD 1. 0 01:Area-B 24.04 . 4,871 . No\_date 28:02 66.17 .747 .000  
 13917+ ROUTE RESERVOIR -> 1. 0 02:DRAIN5 434.92 . 9,426 . No\_date 28:26 66.17 n/a .000  
 13918+ overlaid < 1. 0 01:SMWF-B 24.04 . 641 . No\_date 28:41 66.17 n/a .000  
 13919+ overlaid < 1. 0 01:SMWF-B 24.04 . 641 . No\_date 28:41 66.17 n/a .000  
 13920+ overlaid < 1. 0 01:SMWF-B 24.04 . 641 . No\_date 28:41 66.17 n/a .000  
 13921+ R0100:CO0133- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13922+ ADD HYD + 1. 0 02:DRAIN5 434.92 . 9,426 . No\_date 28:26 40.97 n/a .000  
 13923+ overlaid < 1. 0 02:DRAIN5 434.92 . 9,426 . No\_date 28:26 40.97 n/a .000  
 13924+ overlaid < 1. 0 02:SMWF-B 24.04 . 641 . No\_date 28:41 66.17 n/a .000  
 13925+ overlaid < 1. 0 02:SMWF-B 24.04 . 641 . No\_date 28:41 66.17 n/a .000  
 13926+ overlaid < 1. 0 02:SMWF-B 24.04 . 641 . No\_date 28:41 66.17 n/a .000  
 13927+ R0100:CO0141- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13928+ ROUTE CHANNEL -> 1. 0 02:D4-EX 460.69 . 9,722 . No\_date 29:15 42.35 n/a .000  
 13929+ [RDW= 1. 00] out-> 1. 0 01:DRAIN5 460.69 . 9,722 . No\_date 29:15 42.35 n/a .000  
 13930+ [INP: 88.01:Tp=.57]:[Po=.60]  
 13931+ [Vmax=.703:Dmax=.0383]  
 13932+ R0100:CO0142- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13933+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 28:13 49.72 .565 .000  
 13934+ overlaid < 1. 0 01:0SFDF 9.74 . .705 . No\_date 30:50 50.83 n/a .000  
 13935+ overlaid < 1. 0 01:0SFDF 9.74 . .705 . No\_date 30:50 50.83 n/a .000  
 13936+ R0100:CO0143- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13937+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 28:13 49.72 .565 .000  
 13938+ [INP: 88.01:Tp=.57]:[Po=.60]  
 13939+ [iAEc 4.00: SMIN= 31.15: SMAK= 135.94: SK=.010]  
 13940+ R0100:CO0144- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13941+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 28:13 49.72 .565 .000  
 13942+ ADD HYD + 1. 0 02:DRAIN5 434.92 . 9,426 . No\_date 28:26 42.35 n/a .000  
 13943+ overlaid < 1. 0 02:DRAIN5 434.92 . 9,426 . No\_date 28:26 42.35 n/a .000  
 13944+ overlaid < 1. 0 02:DRAIN5 434.92 . 9,426 . No\_date 28:26 42.35 n/a .000  
 13945+ overlaid < 1. 0 02:DRAIN5 434.92 . 9,426 . No\_date 28:26 42.35 n/a .000  
 13946+ R0100:CO0145- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13947+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 28:13 49.72 .565 .000  
 13948+ [INP: 88.01:Tp=.57]:[Po=.60]  
 13949+ [iAEc 4.00: SMIN= 31.15: SMAK= 135.94: SK=.010]  
 13950+ R0100:CO0146- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13951+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 28:13 49.72 .565 .000  
 13952+ ADD HYD + 1. 0 02:DRAIN5 434.92 . 9,426 . No\_date 28:26 42.35 n/a .000  
 13953+ overlaid < 1. 0 02:DRAIN5 434.92 . 9,426 . No\_date 28:26 42.35 n/a .000  
 13954+ overlaid < 1. 0 02:DRAIN5 434.92 . 9,426 . No\_date 28:26 42.35 n/a .000  
 13955+ R0100:CO0147- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13956+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 28:13 49.72 .565 .000  
 13957+ [INP: 88.01:Tp=.57]:[Po=.60]  
 13958+ [iAEc 4.00: SMIN= 31.15: SMAK= 135.94: SK=.010]  
 13959+ R0100:CO0148- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13960+ ROUTE CHANNEL -> 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:31 38.83 n/a .000  
 13961+ [RDW= 1. 00] out-> 1. 0 01:SMWF 53577.82 . 147.990 . No\_date 33:31 38.83 n/a .000  
 13962+ [INP: 88.01:Tp=.57]:[Po=.60]  
 13963+ [iAEc 4.00: SMIN= 31.15: SMAK= 135.94: SK=.010]  
 13964+ R0100:CO0149- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13965+ [INP: 88.01:Tp=.57]:[Po=.60]  
 13966+ R0100:CO0150- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13967+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 28:10 65.13 .735 .000  
 13968+ ADD HYD + 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 28:10 65.13 .735 .000  
 13969+ [INP: 88.01:Tp=.57]:[Po=.60]  
 13970+ [iAEc 4.00: SMIN= 31.15: SMAK= 135.94: SK=.010]  
 13971+ R0100:CO0143- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13972+ ADD HYD + 1. 0 02:DRAIN5 481.03 . 8,844 . No\_date 28:26 42.73 n/a .000  
 13973+ overlaid < 1. 0 02:DRAIN5 481.03 . 8,844 . No\_date 28:26 42.73 n/a .000  
 13974+ R0100:CO0144- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13975+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 28:13 49.72 .565 .000  
 13976+ [INP: 88.01:Tp=.57]:[Po=.60]  
 13977+ [iAEc 4.00: SMIN= 31.15: SMAK= 135.94: SK=.010]  
 13978+ R0100:CO0145- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13979+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 28:13 49.72 .565 .000  
 13980+ [INP: 88.01:Tp=.57]:[Po=.60]  
 13981+ [iAEc 4.00: SMIN= 31.15: SMAK= 135.94: SK=.010]  
 13982+ R0100:CO0146- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13983+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 28:13 49.72 .565 .000  
 13984+ ADD HYD + 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:31 38.83 n/a .000  
 13985+ overlaid < 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:31 38.83 n/a .000  
 13986+ R0100:CO0147- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13987+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 33:31 38.83 n/a .000  
 13988+ [INP: 88.01:Tp=.57]:[Po=.60]  
 13989+ [iAEc 4.00: SMIN= 31.15: SMAK= 135.94: SK=.010]  
 13990+ R0100:CO0148- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13991+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 33:31 38.83 n/a .000  
 13992+ ADD HYD + 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 13993+ overlaid < 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 13994+ R0100:CO0149- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13995+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 33:32 38.79 n/a .000  
 13996+ ADD HYD + 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 13997+ overlaid < 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 13998+ R0100:CO0150- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 13999+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 33:32 38.79 n/a .000  
 14000+ [INP: 88.01:Tp=.57]:[Po=.60]  
 14001+ [iAEc 4.00: SMIN= 31.15: SMAK= 135.94: SK=.010]  
 14002+ R0100:CO0149- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 14003+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 33:32 38.79 n/a .000  
 14004+ ADD HYD + 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 14005+ overlaid < 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 14006+ R0100:CO0150- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 14007+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 33:32 38.79 n/a .000  
 14008+ ADD HYD + 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 14009+ overlaid < 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 14010+ R0100:CO0149- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 14011+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 33:32 38.79 n/a .000  
 14012+ ADD HYD + 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 14013+ overlaid < 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 14014+ R0100:CO0150- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 14015+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 33:32 38.79 n/a .000  
 14016+ ADD HYD + 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 14017+ overlaid < 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 14018+ R0100:CO0149- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 14019+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 33:32 38.79 n/a .000  
 14020+ ADD HYD + 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 14021+ overlaid < 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 14022+ R0100:CO0150- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 14023+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 33:32 38.79 n/a .000  
 14024+ ADD HYD + 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 14025+ overlaid < 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 14026+ R0100:CO0149- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 14027+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 33:32 38.79 n/a .000  
 14028+ ADD HYD + 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 14029+ overlaid < 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 14030+ R0100:CO0150- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 14031+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 33:32 38.79 n/a .000  
 14032+ ADD HYD + 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 14033+ overlaid < 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 14034+ R0100:CO0149- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 14035+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 33:32 38.79 n/a .000  
 14036+ ADD HYD + 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 14037+ overlaid < 1. 0 02:DRAIN5 53577.82 . 147.990 . No\_date 33:32 38.79 n/a .000  
 14038+ R0100:CO0150- > Dtnin:ID:HYND- > ARRAha-QPEAKcms-Tpeakdate\_bh:mm:->RVm-R.C.--DWFcms  
 14039+ CONTINUOUS STANDYD 1. 0 01:0-15 10.67 . 488.00 . No\_date 33:

14213+ R0100:CO0179-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14214+ \* frame:W\_CLAR\_0100 1.0 01W\_CLAR 119.48 19.657 No\_date 28:04 70.22 n/a .000  
14215+ remark:Total Flows to West Clarke  
14216+ \*  
14217+ # West Clarke Pond 2  
14218+ # Rating curve obtained from Barbwiren Soma MES modeling  
14219+ # Tillary Dam  
14220+ # [ModelID: 10000000000000000000000000000000] 24  
14221+ \*  
14222+ R0100:CO0180-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14223+ \* ROUTE RESERVATION < 1.0 01SN\_C2 119.48 13.064 No\_date 28:13 70.22 n/a .000  
14224+ \* out <= 1.0 03P2-OVF .05 .000 No\_date 0:00 .00 n/a .000  
14225+ \* overflow <= 1.0 03P2-OVF .05 .000 No\_date 0:00 .00 n/a .000  
14226+ \* [ModelID: 10000000000000000000000000000000] 24  
14227+ \*  
14228+ R0100:CO0181-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14229+ ADD HYD 1.0 02K8-1-1 54118 15.375 No\_date 28:00 67.54 n/a .000  
14230+ + 1.0 02S1-1-D4 5.28 .102 No\_date 29:10 45.95 n/a .000  
14231+ + 1.0 02S1-1-D4 12.84 .399 No\_date 29:10 45.95 n/a .000  
14232+ + 1.0 02S1-1-D4 119.48 13.064 No\_date 28:13 70.22 n/a .000  
14233+ + 1.0 02P2-OVF .05 .000 No\_date 0:00 .00 n/a .000  
14234+ SUM+ 1.0 01SN\_C2 5253.95 154.467 No\_date 33:33 39.12 n/a .000  
14235+ \* R0100:CO0182-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14236+ \* ROUTE CHANNEL < 1.0 01SN\_C2 5253.95 154.467 No\_date 33:33 39.12 n/a .000  
14237+ \* out <= 1.0 01SN\_C2 5253.95 154.467 No\_date 33:33 39.12 n/a .000  
14238+ \* overflow <= 1.0 01SN\_C2 5253.95 154.467 No\_date 33:33 39.12 n/a .000  
14239+ SAVE HYD 1.0 01SN\_C2 5253.95 154.467 No\_date 33:33 39.12 n/a .000  
14240+ \* frame: SN\_C2 0100  
14241+ \*  
14242+ R0100:CO0183-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14243+ \* ROUTE CHANNEL < 1.0 01SN\_C2 5253.95 154.467 No\_date 33:33 39.12 n/a .000  
14244+ \* out <= 1.0 01SN\_C2 5253.95 154.467 No\_date 33:33 39.12 n/a .000  
14245+ \* overflow <= 1.0 01SN\_C2 5253.95 154.467 No\_date 33:33 39.12 n/a .000  
14246+ \* [L/S\_nu: 270. / .018/.036]  
14247+ \*  
14248+ R0100:CO0184-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14249+ ADD HYD 1.0 02P5737 5253.95 147.337 No\_date 35:29 39.12 n/a .000  
14250+ + 1.0 02S1-1-D4 21.67 .689 No\_date 29:07 45.95 n/a .000  
14251+ + 1.0 02S1-1-D4 1.04 .100 No\_date 29:07 45.95 n/a .000  
14252+ + 1.0 02S1-1-D7 2.03 .063 No\_date 29:10 45.95 n/a .000  
14253+ SUM+ 1.0 01SN\_C2 5249.41 147.438 No\_date 35:20 39.12 n/a .000  
14254+ \* R0100:CO0185-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14255+ SAVE HYD 1.0 01S502 5249.41 147.438 No\_date 35:20 39.12 n/a .000  
14256+ \* frame: 502.01.0100  
14257+ \* Hydrograph from Node Cedarview Road to Node at West Clarke Drain  
14258+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 5737  
14259+ # JFSA 2021-02-25 add station 5737 before station 5002. Station 5737 was extracted from the HEC-RAS model T:\PROJ\1474-1  
14260+ # RVEA 2021-02-25 change the length of 5002 route channel from 82m to 786 m. That is because of adding station 5737 is before station 5002.  
14261+ \* R0100:CO0186-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14262+ \* ROUTE CHANNEL < 1.0 02P5002 5249.41 147.438 No\_date 35:20 39.12 n/a .000  
14263+ \* out <= 1.0 02P5002 5249.41 147.438 No\_date 35:20 39.12 n/a .000  
14264+ \* overflow <= 1.0 02P5002 5249.41 147.438 No\_date 35:20 39.12 n/a .000  
14265+ \* [L/S\_nu: 245. / .095/.036]  
14266+ \*  
14267+ R0100:CO0187-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14268+ \* ROUTE CHANNEL > 1.0 02N\_NMC 5249.41 147.396 No\_date 35:29 39.13 n/a .000  
14269+ \* [ROT: 1.00] out < 1.0 01N\_NMC 5249.41 147.399 No\_date 35:35 39.13 n/a .000  
14270+ \* [ROT: 1.00] out < 1.0 01N\_NMC 5249.41 147.399 No\_date 35:35 39.13 n/a .000  
14271+ \* [Vmax: 1.325] [max: 3.172]  
14272+ R0100:CO0188-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14273+ \* ROUTE CHANNEL < 1.0 02P5002 5249.41 147.396 No\_date 35:25 39.13 n/a .000  
14274+ \* out <= 1.0 02P5002 5249.41 147.396 No\_date 35:25 39.13 n/a .000  
14275+ \* overflow <= 1.0 02P5002 5249.41 147.396 No\_date 35:25 39.13 n/a .000  
14276+ \* [L/S\_nu: 245. / .095/.036]  
14277+ \*  
14278+ \* Hydrograph from Node West Clarke routed to Node at Kennedy - Burnett Drain  
14279+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 4534  
14280+ \*  
14281+ R0100:CO0189-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14282+ \* ROUTE CHANNEL < 1.0 02P5002 5249.41 147.396 No\_date 35:20 39.12 n/a .000  
14283+ \* [ROT: 1.00] out < 1.0 01N\_NKB 5249.41 146.607 No\_date 35:56 39.13 n/a .000  
14284+ \* [ROT: 1.00] out < 1.0 01N\_NKB 5249.41 146.607 No\_date 35:56 39.13 n/a .000  
14285+ \*  
14286+ \*  
14287+ \* Catchment KEN\_BU  
14288+ \* Outlets to Fraser-Clarke drain (north of the Jock)  
14289+ \* Medium density residential subdivision  
14290+ \* Existing Kennedy-Burnett SWM Facility  
14291+ \* Tributary Drainage Area to Pond = 160 ha  
14292+ \*  
14293+ R0100:CO0190-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14294+ CONTINUOUS STANDHYD 1.0 01K8-1-1 40.82 5.490 No\_date 28:09 36.71 .415 .000  
14295+ [XPM: 20-TIME: 40]  
14296+ \* (Horton parameters) Po: 76.20Pc 13.20DCAY4:14 Fc .00  
14297+ \* [Pervious areas: Iaper: 4.67SLPPw .50:LGP: 40. :NWP: 250:SCP: .0]  
14298+ \* [Impervious areas: Iaper: 79SLPPw .50:LGP: 522. :NWP: 013:SCI: .0]  
14299+ \* [MjSysSto: 1.774E+00] ToCovFv01...0000E+00 N-Ovf 0. TotTurrovf .hrs  
14300+ Minor System / 1.0 03K8-1-1 40.82 .000 No\_date 0:00 .00 n/a .000  
14301+ \* R0100:CO0191-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14302+ \* [ROT: 1.00] out < 1.0 01N\_NMC 40.82 5.490 No\_date 28:04 36.91 n/a .000  
14303+ \* [ROT: 1.00] out < 1.0 01N\_NMC 40.82 5.490 No\_date 28:04 36.91 n/a .000  
14304+ R0100:CO0192-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14305+ \* CONTINUOUS STANDHYD 1.0 01K8-1-1 31.19 4.072 No\_date 28:06 40.61 .458 .000  
14306+ [XPM: 19-TIME: 38]  
14307+ \* (Horton parameters) Po: 76.20Pc 13.20DCAY4:14 Fc .00  
14308+ \* [Pervious areas: Iaper: 4.67SLPPw .50:LGP: 40. :NWP: 250:SCP: .0]  
14309+ \* [Impervious areas: Iaper: 79SLPPw .50:LGP: 455. :NWP: 013:SCI: .0]  
14310+ R0100:CO0193-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14311+ \* CONTINUOUS STANDHYD 1.0 01K8-1-1 31.19 4.072 No\_date 28:06 40.61 .458 .000  
14312+ [XPM: 20-TIME: 40]  
14313+ \* (Horton parameters) Po: 76.20Pc 13.20DCAY4:14 Fc .00  
14314+ \* [Pervious areas: Iaper: 4.67SLPPw .50:LGP: 40. :NWP: 250:SCP: .0]  
14315+ \* [Impervious areas: Iaper: 79SLPPw .50:LGP: 522. :NWP: 013:SCI: .0]  
14316+ R0100:CO0194-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14317+ \* CONTINUOUS STANDHYD 1.0 01K8-1-1 31.19 4.072 No\_date 28:06 40.61 .458 .000  
14318+ [XPM: 20-TIME: 40]  
14319+ \* (Horton parameters) Po: 76.20Pc 13.20DCAY4:14 Fc .00  
14320+ \* [Pervious areas: Iaper: 4.67SLPPw .50:LGP: 40. :NWP: 250:SCP: .0]  
14321+ \* COMPUTE DUALHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 n/a .000  
14322+ Minor System / 1.0 02K8-1-1 40.82 5.490 No\_date 28:06 36.71 .415 .000  
14323+ \* R0100:CO0195-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14324+ \* CONTINUOUS STANDHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 .458 .000  
14325+ [XPM: 20-TIME: 40]  
14326+ \* (Horton parameters) Po: 76.20Pc 13.20DCAY4:14 Fc .00  
14327+ \* [Pervious areas: Iaper: 4.67SLPPw .50:LGP: 40. :NWP: 250:SCP: .0]  
14328+ \* [Impervious areas: Iaper: 79SLPPw .50:LGP: 522. :NWP: 013:SCI: .0]  
14329+ R0100:CO0196-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14330+ \* CONTINUOUS STANDHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 .458 .000  
14331+ [XPM: 20-TIME: 40]  
14332+ \* (Horton parameters) Po: 76.20Pc 13.20DCAY4:14 Fc .00  
14333+ \* [Pervious areas: Iaper: 4.67SLPPw .50:LGP: 40. :NWP: 250:SCP: .0]  
14334+ \* [Impervious areas: Iaper: 79SLPPw .50:LGP: 522. :NWP: 013:SCI: .0]  
14335+ R0100:CO0197-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14336+ \* CONTINUOUS STANDHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 .458 .000  
14337+ [XPM: 20-TIME: 40]  
14338+ \* (Horton parameters) Po: 76.20Pc 13.20DCAY4:14 Fc .00  
14339+ \* [Pervious areas: Iaper: 4.67SLPPw .50:LGP: 40. :NWP: 250:SCP: .0]  
14340+ \* [Impervious areas: Iaper: 79SLPPw .50:LGP: 522. :NWP: 013:SCI: .0]  
14341+ R0100:CO0198-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14342+ \* ADD HYD 1.0 02K8-1-1 40.82 .000 No\_date 0:00 .00 n/a .000  
14343+ \* R0100:CO0199-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14344+ \* COMPUTE DUALHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 n/a .000  
14345+ Minor System / 1.0 02K8-1-1 40.82 5.490 No\_date 28:06 36.71 .415 .000  
14346+ \* R0100:CO0200-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14347+ \* CONTINUOUS STANDHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 .458 .000  
14348+ [XPM: 20-TIME: 40]  
14349+ \* (Horton parameters) Po: 76.20Pc 13.20DCAY4:14 Fc .00  
14350+ \* [Pervious areas: Iaper: 4.67SLPPw .50:LGP: 40. :NWP: 250:SCP: .0]  
14351+ \* [Impervious areas: Iaper: 79SLPPw .50:LGP: 522. :NWP: 013:SCI: .0]  
14352+ R0100:CO0201-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14353+ \* COMPUTE DUALHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 n/a .000  
14354+ Minor System / 1.0 02K8-1-1 40.82 5.490 No\_date 28:06 36.71 .415 .000  
14355+ \* R0100:CO0202-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14356+ \* CONTINUOUS STANDHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 .458 .000  
14357+ [XPM: 20-TIME: 40]  
14358+ \* (Horton parameters) Po: 76.20Pc 13.20DCAY4:14 Fc .00  
14359+ \* [Pervious areas: Iaper: 4.67SLPPw .50:LGP: 40. :NWP: 250:SCP: .0]  
14360+ \* [Impervious areas: Iaper: 79SLPPw .50:LGP: 522. :NWP: 013:SCI: .0]  
14361+ R0100:CO0203-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14362+ \* CONTINUOUS STANDHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 .458 .000  
14363+ [XPM: 20-TIME: 40]  
14364+ \* (Horton parameters) Po: 76.20Pc 13.20DCAY4:14 Fc .00  
14365+ \* [Pervious areas: Iaper: 4.67SLPPw .50:LGP: 40. :NWP: 250:SCP: .0]  
14366+ \* [Impervious areas: Iaper: 79SLPPw .50:LGP: 522. :NWP: 013:SCI: .0]  
14367+ R0100:CO0204-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14368+ \* COMPUTE DUALHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 n/a .000  
14369+ Minor System / 1.0 02K8-1-1 40.82 5.490 No\_date 28:06 36.71 .415 .000  
14370+ \* R0100:CO0205-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14371+ \* CONTINUOUS STANDHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 .458 .000  
14372+ [XPM: 20-TIME: 40]  
14373+ \* (Horton parameters) Po: 76.20Pc 13.20DCAY4:14 Fc .00  
14374+ \* [Pervious areas: Iaper: 4.67SLPPw .50:LGP: 40. :NWP: 250:SCP: .0]  
14375+ \* [Impervious areas: Iaper: 79SLPPw .50:LGP: 522. :NWP: 013:SCI: .0]  
14376+ R0100:CO0206-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14377+ \* CONTINUOUS STANDHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 .458 .000  
14378+ [XPM: 20-TIME: 40]  
14379+ \* (Horton parameters) Po: 76.20Pc 13.20DCAY4:14 Fc .00  
14380+ \* [Pervious areas: Iaper: 4.67SLPPw .50:LGP: 40. :NWP: 250:SCP: .0]  
14381+ \* [Impervious areas: Iaper: 79SLPPw .50:LGP: 522. :NWP: 013:SCI: .0]  
14382+ R0100:CO0207-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14383+ \* COMPUTE DUALHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 n/a .000  
14384+ Minor System / 1.0 02K8-1-1 40.82 5.490 No\_date 28:06 36.71 .415 .000  
14385+ \* R0100:CO0208-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14386+ \* CONTINUOUS STANDHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 .458 .000  
14387+ [XPM: 20-TIME: 40]  
14388+ \* (Horton parameters) Po: 76.20Pc 13.20DCAY4:14 Fc .00  
14389+ \* [Pervious areas: Iaper: 4.67SLPPw .50:LGP: 40. :NWP: 250:SCP: .0]  
14390+ \* [Impervious areas: Iaper: 79SLPPw .50:LGP: 522. :NWP: 013:SCI: .0]  
14391+ R0100:CO0209-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14392+ \* COMPUTE DUALHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 n/a .000  
14393+ Minor System / 1.0 02K8-1-1 40.82 5.490 No\_date 28:06 36.71 .415 .000  
14394+ \* R0100:CO0210-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14395+ \* CONTINUOUS STANDHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 .458 .000  
14396+ [XPM: 20-TIME: 40]  
14397+ \* (Horton parameters) Po: 76.20Pc 13.20DCAY4:14 Fc .00  
14398+ \* [Pervious areas: Iaper: 4.67SLPPw .50:LGP: 40. :NWP: 250:SCP: .0]  
14399+ \* [Impervious areas: Iaper: 79SLPPw .50:LGP: 522. :NWP: 013:SCI: .0]  
14400+ R0100:CO0211-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14401+ \* COMPUTE DUALHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 n/a .000  
14402+ Minor System / 1.0 02K8-1-1 40.82 5.490 No\_date 28:06 36.71 .415 .000  
14403+ \* R0100:CO0212-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14404+ \* CONTINUOUS STANDHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 .458 .000  
14405+ [XPM: 20-TIME: 40]  
14406+ \* (Horton parameters) Po: 76.20Pc 13.20DCAY4:14 Fc .00  
14407+ \* [Pervious areas: Iaper: 4.67SLPPw .50:LGP: 40. :NWP: 250:SCP: .0]  
14408+ \* [Impervious areas: Iaper: 79SLPPw .50:LGP: 522. :NWP: 013:SCI: .0]  
14409+ R0100:CO0213-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14410+ \* COMPUTE DUALHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 n/a .000  
14411+ Minor System / 1.0 02K8-1-1 40.82 5.490 No\_date 28:06 36.71 .415 .000  
14412+ \* R0100:CO0214-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14413+ \* CONTINUOUS STANDHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 .458 .000  
14414+ [XPM: 20-TIME: 40]  
14415+ \* (Horton parameters) Po: 76.20Pc 13.20DCAY4:14 Fc .00  
14416+ \* [Pervious areas: Iaper: 4.67SLPPw .50:LGP: 40. :NWP: 250:SCP: .0]  
14417+ \* [Impervious areas: Iaper: 79SLPPw .50:LGP: 522. :NWP: 013:SCI: .0]  
14418+ R0100:CO0215-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14419+ \* COMPUTE DUALHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 n/a .000  
14420+ Minor System / 1.0 02K8-1-1 40.82 5.490 No\_date 28:06 36.71 .415 .000  
14421+ \* R0100:CO0216-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14422+ \* CONTINUOUS STANDHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 .458 .000  
14423+ [XPM: 20-TIME: 40]  
14424+ \* (Horton parameters) Po: 76.20Pc 13.20DCAY4:14 Fc .00  
14425+ \* [Pervious areas: Iaper: 4.67SLPPw .50:LGP: 40. :NWP: 250:SCP: .0]  
14426+ \* [Impervious areas: Iaper: 79SLPPw .50:LGP: 522. :NWP: 013:SCI: .0]  
14427+ R0100:CO0217-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14428+ \* COMPUTE DUALHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 n/a .000  
14429+ Minor System / 1.0 02K8-1-1 40.82 5.490 No\_date 28:06 36.71 .415 .000  
14430+ \* R0100:CO0218-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14431+ \* CONTINUOUS STANDHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 .458 .000  
14432+ [XPM: 20-TIME: 40]  
14433+ \* (Horton parameters) Po: 76.20Pc 13.20DCAY4:14 Fc .00  
14434+ \* [Pervious areas: Iaper: 4.67SLPPw .50:LGP: 40. :NWP: 250:SCP: .0]  
14435+ \* [Impervious areas: Iaper: 79SLPPw .50:LGP: 522. :NWP: 013:SCI: .0]  
14436+ R0100:CO0219-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14437+ \* COMPUTE DUALHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 n/a .000  
14438+ Minor System / 1.0 02K8-1-1 40.82 5.490 No\_date 28:06 36.71 .415 .000  
14439+ \* R0100:CO0220-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14440+ \* CONTINUOUS STANDHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 .458 .000  
14441+ [XPM: 20-TIME: 40]  
14442+ \* (Horton parameters) Po: 76.20Pc 13.20DCAY4:14 Fc .00  
14443+ \* [Pervious areas: Iaper: 4.67SLPPw .50:LGP: 40. :NWP: 250:SCP: .0]  
14444+ \* [Impervious areas: Iaper: 79SLPPw .50:LGP: 522. :NWP: 013:SCI: .0]  
14445+ R0100:CO0221-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14446+ \* COMPUTE DUALHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 n/a .000  
14447+ Minor System / 1.0 02K8-1-1 40.82 5.490 No\_date 28:06 36.71 .415 .000  
14448+ \* R0100:CO0222-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14449+ \* CONTINUOUS STANDHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 .458 .000  
14450+ [XPM: 20-TIME: 40]  
14451+ \* (Horton parameters) Po: 76.20Pc 13.20DCAY4:14 Fc .00  
14452+ \* [Pervious areas: Iaper: 4.67SLPPw .50:LGP: 40. :NWP: 250:SCP: .0]  
14453+ \* [Impervious areas: Iaper: 79SLPPw .50:LGP: 522. :NWP: 013:SCI: .0]  
14454+ R0100:CO0223-----Dtnin-ID:NHYD----AREaha-QPEAKcms-TpeakDate\_bh:mm---RVMn-R.C.---DFWfms  
14455+ \* COMPUTE DUALHYD 1.0 01K8-1-1 31.10 4.072 No\_date 28:06 40.61 n/a .000  
14456+





15335+ Major System / 1.0 02:A10-MJ .08 .218 No\_date 28:05 59.73 n/a .000

15336+ Major System / 1.0 03:A12-MJ 4.08 .218 No\_date 27:41 60.02 n/a .000

15337+ [M360+ 2,280E-03] 1.0 01:A11 5334Z:02: M360+ 1.0 TotDpfrv= 1.0 hrs

15338+ R1010:CO365:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15339+ COMPUTE\_SUNTIME: 42

15340+ [L0Sg= 2 : CN= 75.0] .00

15341+ [Previous areas: Iaper: 4.67:SLPP1:0.0:LDP= 40.:NWP= .250:SCP= .0]

15342+ [Previous areas: Iaper: 1.57:SLP1:1.00:LGI= 379.:MMI= .013:SCI= .0]

15343+ [iArECimp= 4.00: iArECPer= 4.00]

15344+ [iArECimp= 33.81: SMAX=225.43: SK= .010]

15345+ R1010:CO366:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15346+ COMPUTE\_DUALHYD 1.0 01:A11 10.61 1.941 No\_date 28:01 67.38 n/a .000

15347+ Major System / 1.0 02:A10-MJ 1.0 01:A11 1.941 No\_date 28:01 67.38 n/a .000

15348+ Major System / 1.0 03:A12-MJ 10.45 .993 No\_date 28:34 67.69 n/a .000

15349+ Minor System / 1.0 01:ME107 124.74 5.482 No\_date 28:02 63.62 n/a .000

15350+ [M360+ 5660E+03] TotDvYr=1090K:03 N-Owf= 1. TotDpfrv= 0. hrs]

15351+ R1010:CO367:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15352+ ADD HYD 1.0 02:10E-107 110.24 4.179 No\_date 28:02 63.36 n/a .000

15353+ \* + 1.0 02:A10-MJ 4.08 .310 No\_date 27:48 60.02 n/a .000

15354+ \* + 1.0 02:A12-MJ 10.45 .310 No\_date 27:48 60.02 n/a .000

15355+ SUM: 1.0 01:ME107 124.74 5.482 No\_date 28:02 63.62 n/a .000

15356+ R1010:CO368:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15357+ frame: MH07\_0100 124.74 5.482 No\_date 28:02 63.62 n/a .000

15358+ remark>Total Flows at MH010

15359+ R1010:CO369:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15360+ ROUTE PIPE > 1.0 02:ME107 124.74 5.482 No\_date 28:02 63.62 n/a .000

15361+ \* [ROUTE 1.00] 1.0 01:107-119 124.74 5.468 No\_date 28:04 63.62 n/a .000

15362+ [Vmax= 1.932:Dmax= 1.664]

15363+ [Din= 1.80:Dused= 2.03]

15364+ R1010:CO370:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15365+ ROUTE PIPE > 1.0 02:107-119 124.74 5.468 No\_date 28:04 63.62 n/a .000

15366+ \* [ROUTE 1.00] 1.0 01:119-108 124.74 5.480 No\_date 28:05 63.62 n/a .000

15367+ [Vmax= 1.932:Dmax= 1.664]

15368+ [Din= 1.80:Dused= 2.03]

15369+ R1010:CO371:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15370+ CONTINUOUS STANDYD 1.0 01:A13 12.29 2.213 No\_date 28:01 62.88 .710 .000

15371+ [XMP= 41:TINH= 54]

15372+ [Previous areas: Iaper: 4.67:SLPP1:0.0:LGI= 1.57:MMI= 1.00:LGI= 183.:MMI= .013:SCI= .0]

15373+ [Impervious areas: Iaper: 4.67:SLPP1:0.0:LGI= 1.57:MMI= 1.00:LGI= 183.:MMI= .013:SCI= .0]

15374+ [Vmax= 1.932:Dmax= 1.664]

15375+ [SMIN= 33.81: SMAX=225.43: SK= .010]

15376+ R1010:CO372:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15377+ COMPUTE\_DUALHYD 1.0 01:A12 2.513 No\_date 28:01 62.88 n/a .000

15378+ Major System / 1.0 02:A10-MJ .21 .599 No\_date 28:05 62.88 n/a .000

15379+ Minor System / 1.0 03:A12-MJ .20 .599 No\_date 27:41 63.11 n/a .000

15380+ Minor System / 1.0 01:ME107 2.59 .540 No\_date 28:01 73.40 n/a .000

15381+ R1010:CO373:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15382+ CONTINUOUS STANDYD 1.0 01:A13 2.50 .540 No\_date 28:01 62.88 .710 .000

15383+ [XMP= 41:TINH= 54]

15384+ R1010:CO374:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15385+ COMPUTE\_DUALHYD 1.0 01:A12 2.50 .540 No\_date 28:01 73.40 n/a .000

15386+ Major System / 1.0 02:A10-MJ .20 .599 No\_date 28:05 62.88 n/a .000

15387+ Minor System / 1.0 03:A12-MJ .20 .599 No\_date 27:41 63.11 n/a .000

15388+ Minor System / 1.0 01:ME107 2.50 .540 No\_date 28:01 73.40 n/a .000

15389+ R1010:CO375:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15390+ COMPUTE\_DUALHYD 1.0 01:A12 2.94 .490 No\_date 28:00 59.56 .673 .000

15391+ [L0Sg= 2 : CN= 75.0] .00

15392+ [Previous areas: Iaper: 4.67:SLPP1:0.0:LDP= 40.:NWP= .250:SCP= .0]

15393+ [Previous areas: Iaper: 1.57:SLP1:1.00:LGI= 379.:MMI= .013:SCI= .0]

15394+ [iArECimp= 4.00: iArECPer= 4.00]

15395+ [iArECimp= 33.81: SMAX=225.43: SK= .010]

15396+ R1010:CO376:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15397+ COMPUTE\_DUALHYD 1.0 01:A12 2.513 No\_date 28:01 62.88 n/a .000

15398+ Major System / 1.0 02:A10-MJ .21 .599 No\_date 28:05 62.88 n/a .000

15399+ Minor System / 1.0 03:A12-MJ .20 .599 No\_date 27:41 63.11 n/a .000

15400+ Minor System / 1.0 01:ME107 2.59 .540 No\_date 28:01 73.40 n/a .000

15401+ R1010:CO377:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15402+ ADD HYD 1.0 02:119-108 124.74 5.480 No\_date 28:05 63.62 n/a .000

15403+ \* + 1.0 02:A12-MJ 12.06 1.029 No\_date 27:48 63.11 n/a .000

15404+ \* + 1.0 02:A12-MJ 12.06 1.029 No\_date 27:48 63.11 n/a .000

15405+ SUM: 1.0 01:ME108 139.38 6.998 No\_date 28:03 63.75 n/a .000

15406+ R1010:CO378:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15407+ SAVE HYD 1.0 01:ME108 139.38 6.996 No\_date 28:03 63.75 n/a .000

15408+ frame: MH08\_0100

15409+ remark>Total Flows at MH010

15410+ R1010:CO378:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15411+ COMPUTE\_DUALHYD 1.0 01:A12 2.513 No\_date 28:01 62.88 n/a .000

15412+ Major System / 1.0 02:A10-MJ .21 .599 No\_date 28:05 62.88 n/a .000

15413+ Minor System / 1.0 03:A12-MJ .20 .599 No\_date 27:41 63.11 n/a .000

15414+ Minor System / 1.0 01:ME107 2.59 .540 No\_date 28:01 73.40 n/a .000

15415+ R1010:CO379:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15416+ ROUTE PIPE > 1.0 02:108-116 139.38 6.987 No\_date 28:04 63.75 n/a .000

15417+ \* [ROUTE 1.00] 1.0 01:108-116-corrig 139.38 6.949 No\_date 28:06 63.75 n/a .000

15418+ [L/S/n= 80. /130. /013]

15419+ [Vmax= 2.115:Dmax= 1.797]

15420+ R1010:CO380:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15421+ ADD HYD 1.0 02:119-108 139.38 6.985 No\_date 28:04 63.75 n/a .000

15422+ \* + 1.0 02:A12-MJ 12.06 1.029 No\_date 27:48 63.11 n/a .000

15423+ \* + 1.0 02:A12-MJ 12.06 1.029 No\_date 27:48 63.11 n/a .000

15424+ \* + 1.0 02:A12-MJ 12.06 1.029 No\_date 27:48 63.11 n/a .000

15425+ SUM: 1.0 01:ME108 139.38 6.986 No\_date 28:04 63.75 n/a .000

15426+ R1010:CO380:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15427+ ADD HYD 1.0 02:119-108 139.38 6.985 No\_date 28:04 63.75 n/a .000

15428+ \* + 1.0 02:A12-MJ 12.06 1.029 No\_date 27:48 63.11 n/a .000

15429+ \* + 1.0 02:A12-MJ 12.06 1.029 No\_date 27:48 63.11 n/a .000

15430+ SUM: 1.0 01:ME108 139.38 6.986 No\_date 28:04 63.75 n/a .000

15431+ frame: Corrigan\_0100

15432+ remark:RTD-HD\_Corriagan\_0100 (Total Flows at Corrigan Pond)

15433+ R1010:CO381:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15434+ ROUTE RESERVOIR > 1.0 02:ME108 142.32 7.300 No\_date 28:04 63.67 n/a .000

15435+ [ROUTE 1.00] 1.0 01:ME108 142.32 7.300 No\_date 28:04 63.67 n/a .000

15436+ overflow > 1.0 03:C0-P-OVF .00 .000 No\_date 0.00 0.00 n/a .000

15437+ [iArECimp= 1.044E+00 m3\_TotDvVol= 0.00E+00 m3\_O\_TotDpfrv= 0. hrs]

15438+ [M360+used=.1044E+00 m3\_TotDvVol= 0.00E+00 m3\_O\_TotDpfrv= 0. hrs]

15439+ R1010:CO381:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15440+ ADD HYD 1.0 02:C0-P-OVF .00 .000 No\_date 0.00 0.00 n/a .000

15441+ \* + 1.0 02:C0-P-OVF 142.32 7.300 No\_date 28:04 63.67 n/a .000

15442+ \* + 1.0 02:C0-P-OVF 142.32 7.300 No\_date 28:04 63.67 n/a .000

15443+ \* + 1.0 02:C0-P-OVF 142.32 7.300 No\_date 28:04 63.67 n/a .000

15444+ \* + 1.0 02:C0-P-OVF 142.32 7.300 No\_date 28:04 63.67 n/a .000

15445+ \* + 1.0 02:C0-P-OVF 142.32 7.300 No\_date 28:04 63.67 n/a .000

15446+ \* + 1.0 02:C0-P-OVF 142.32 7.300 No\_date 28:04 63.67 n/a .000

15447+ \* + 1.0 02:A10-MJ .16 .564 No\_date 28:05 59.73 n/a .000

15448+ \* + 1.0 02:A10-MJ .16 .564 No\_date 28:05 59.73 n/a .000

15449+ \* + 1.0 02:A10-MJ .16 .564 No\_date 28:05 59.73 n/a .000

15450+ \* + 1.0 02:A13-ML .00 .000 No\_date 0.00 0.00 n/a .000

15451+ \* + 1.0 02:A13-ML .00 .000 No\_date 0.00 0.00 n/a .000

15452+ SUM: 1.0 01:ME108 5520.08 146.408 No\_date 36:18 39.35 n/a .000

15453+ R1010:CO384:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15454+ SAVE HYD 1.0 01:corr1g 5520.08 146.408 No\_date 36:18 39.39 n/a .000

15455+ frame: corr1g\_0100

15456+ remark:Total Flows at Corrigan Pond

15457+ R1010:CO384:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15458+ COMPUTE\_DUALHYD 1.0 01:A12 142.32 7.300 No\_date 28:04 63.67 n/a .000

15459+ Major System / 1.0 02:A10-MJ .21 .599 No\_date 28:05 62.88 n/a .000

15460+ Minor System / 1.0 03:A12-MJ .20 .599 No\_date 27:41 63.11 n/a .000

15461+ Minor System / 1.0 01:ME107 2.59 .540 No\_date 28:01 73.40 n/a .000

15462+ R1010:CO385:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15463+ COMPUTE\_DUALHYD 1.0 01:A12 142.32 7.300 No\_date 28:04 63.67 n/a .000

15464+ Major System / 1.0 02:A10-MJ .21 .599 No\_date 28:05 62.88 n/a .000

15465+ Minor System / 1.0 03:A12-MJ .20 .599 No\_date 27:41 63.11 n/a .000

15466+ Minor System / 1.0 01:ME107 2.59 .540 No\_date 28:01 73.40 n/a .000

15467+ R1010:CO385:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15468+ frame: SNN\_M1\_0100

15469+ remark:Total Flows at Jock Vale Road

15470+ R1010:CO386:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15471+ # Corriagan Mills - To Jock River (north of the Jock) - Primary residential development

15472+ R1010:CO387:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15473+ frame: SNN\_M1\_0100

15474+ R1010:CO387:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15475+ COMPUTE\_STANDYD 1.0 01:ME108 178.39 20.390 No\_date 28:06 58.87 642 .000

15476+ [XMP= 38:TINH= .38]

15477+ [Previous areas: Iaper: 4.67:SLPP1:0.0:LDP= 40.:NWP= .250:SCP= .0]

15478+ [Previous areas: Iaper: 1.57:SLP1:1.00:LGI= 1118.:MMI= .013:SCI= .0]

15479+ [iArECimp= 4.00: iArECPer= 4.00]

15480+ [iArECimp= 33.81: SMAX=225.43: SK= .010]

15481+ R1010:CO388:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15482+ COMPUTE\_DUALHYD 1.0 01:A12 178.39 20.390 No\_date 28:06 58.87 642 .000

15483+ Major System / 1.0 02:A10-MJ .21 .599 No\_date 28:07 62.88 n/a .000

15484+ Minor System / 1.0 03:A12-MJ .20 .599 No\_date 27:41 63.11 n/a .000

15485+ Minor System / 1.0 01:ME107 2.59 .540 No\_date 28:01 73.40 n/a .000

15486+ R1010:CO389:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15487+ ROUTE RESERVOIR > 1.0 02:ME108 178.39 20.390 No\_date 28:06 58.87 n/a .000

15488+ \* + 1.0 02:ME108 178.39 20.390 No\_date 28:06 58.87 n/a .000

15489+ \* + 1.0 02:ME108 178.39 20.390 No\_date 28:06 58.87 n/a .000

15490+ [M360+used=.178.39 m3\_TotDvVol= 0.00E+00 m3\_O\_TotDpfrv= 0. hrs]

15491+ R1010:CO388:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15492+ ADD HYD 1.0 02:10E-107 178.39 20.390 No\_date 28:06 58.87 n/a .000

15493+ \* + 1.0 02:A10-MJ 178.39 20.390 No\_date 28:06 58.87 n/a .000

15494+ \* + 1.0 02:A12-MJ 178.39 20.390 No\_date 28:06 58.87 n/a .000

15495+ \* + 1.0 02:A12-MJ 178.39 20.390 No\_date 28:06 58.87 n/a .000

15496+ \* + 1.0 02:A12-MJ 178.39 20.390 No\_date 28:06 58.87 n/a .000

15497+ \* + 1.0 02:A12-MJ 178.39 20.390 No\_date 28:06 58.87 n/a .000

15498+ \* + 1.0 02:A12-MJ 178.39 20.390 No\_date 28:06 58.87 n/a .000

15499+ \* + 1.0 02:A12-MJ 178.39 20.390 No\_date 28:06 58.87 n/a .000

15500+ \* + 1.0 02:A12-MJ 178.39 20.390 No\_date 28:06 58.87 n/a .000

15501+ \* + 1.0 02:A12-MJ 178.39 20.390 No\_date 28:06 58.87 n/a .000

15502+ \* + 1.0 02:A12-MJ 178.39 20.390 No\_date 28:06 58.87 n/a .000

15503+ \* + 1.0 02:A12-MJ 178.39 20.390 No\_date 28:06 58.87 n/a .000

15504+ \* + 1.0 02:A12-MJ 178.39 20.390 No\_date 28:06 58.87 n/a .000

15505+ \* + 1.0 02:A12-MJ 178.39 20.390 No\_date 28:06 58.87 n/a .000

15506+ \* + 1.0 02:A12-MJ 178.39 20.390 No\_date 28:06 58.87 n/a .000

15507+ \* + 1.0 02:A12-MJ 178.39 20.390 No\_date 28:06 58.87 n/a .000

15508+ \* + 1.0 02:A12-MJ 178.39 20.390 No\_date 28:06 58.87 n/a .000

15509+ \* + 1.0 02:A12-MJ 178.39 20.390 No\_date 28:06 58.87 n/a .000

15510+ \* + 1.0 02:A12-MJ 178.39 20.390 No\_date 28:06 58.87 n/a .000

15511+ \* + 1.0 02:A12-MJ 178.39 20.390 No\_date 28:06 58.87 n/a .000

15512+ \* + 1.0 02:A12-MJ 178.39 20.390 No\_date 28:06 58.87 n/a .000

15513+ \* + 1.0 02:A12-MJ 178.39 20.390 No\_date 28:06 58.87 n/a .000

15514+ R1010:CO391:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15515+ COMPUTE\_STANDYD 1.0 01:DESIREE 23.78 3.004 No\_date 28:03 53.11 .600 .000

15516+ [XMP= 25:TINH= .25]

15517+ [L0Sg= 2 : CN= 77.0]

15518+ [Previous areas: Iaper: 4.67:SLPP1:0.0:LDP= 40.:NWP= .250:SCP= .0]

15519+ [Previous areas: Iaper: 1.57:SLP1:1.00:LGI= 400.:MMI= .013:SCI= .0]

15520+ [iArECimp= 4.00: iArECPer= 4.00]

15521+ [iArECimp= 33.81: SMAX=207.68: SK= .010]

15522+ # Catchment JOCKVA

15523+ # Hydrograph from Jock Vale Road to Heart's Desire

15524+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 689

15525+ R1010:CO390:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15526+ ROUTE CHANNEL > 1.0 02:SM\_M 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15527+ \* + 1.0 02:SM\_M 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15528+ [Vmax= 1.650:Dmax= 2.683]

15529+ \* + 1.0 02:SM\_M 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15530+ \* + 1.0 02:SM\_M 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15531+ \* + 1.0 02:SM\_M 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15532+ \* + 1.0 02:SM\_M 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15533+ \* + 1.0 02:SM\_M 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15534+ \* + 1.0 02:SM\_M 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15535+ \* + 1.0 02:SM\_M 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15536+ \* + 1.0 02:SM\_M 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15537+ \* + 1.0 02:SM\_M 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15538+ \* + 1.0 02:SM\_M 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15539+ \* + 1.0 02:SM\_M 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15540+ \* + 1.0 02:SM\_M 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15541+ R1010:CO398:-----Dtnin-ID:NHVD----ARAHa-QPEAKms-Tpeakdate\_bh:mm---RVM-R.C.---DFWfmc

15542+ ADD HYD 1.0 02:10E-107 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15543+ \* + 1.0 02:10E-107 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15544+ \* + 1.0 02:10E-107 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15545+ \* + 1.0 02:10E-107 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15546+ \* + 1.0 02:10E-107 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15547+ \* + 1.0 02:10E-107 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15548+ \* + 1.0 02:10E-107 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15549+ \* + 1.0 02:10E-107 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15550+ \* + 1.0 02:10E-107 55196.07 149.100 No\_date 36:20 39.44 n/a .000

15551+ \* + 1.0 02:10E-107 55196.07 149.100 No\_date 36:20 39.44 n/a

```

15709> ** WARNING: New pipe size used for routing.
15710> RO050:CO0170 ROUTE PIPE   ->
15711> ** WARNING: New pipe size used for routing.
15712> RO050:CO0378 ROUTE PIPE   ->
15713> ** WARNING: New pipe size used for routing.
15714> RO050:CO0379 ROUTE PIPE   ->
15715> ** WARNING: New pipe size used for routing.
15716> RO100:CO0003 ROUTE PIPE   ->
15717> ** WARNING: New pipe size used for routing.
15718> RO100:CO0009 ROUTE PIPE   ->
15719> ** WARNING: New pipe size used for routing.
15720> RO100:CO0025 ROUTE PIPE   ->
15721> ** WARNING: New pipe size used for routing.
15722> RO100:CO0026 ROUTE PIPE   ->
15723> ** WARNING: New pipe size used for routing.
15724> RO100:CO0034 ROUTE PIPE   ->
15725> ** WARNING: New pipe size used for routing.
15726> RO100:CO0342 DIVERT RVD  ->
15727> ** NOTE: Inflow hyd. is dry and cannot be diverted.
15728> ** WARNING: New pipe size used for routing.
15729> ** WARNING: New pipe size used for routing.
15730> RO100:CO0362 ROUTE PIPE   ->
15731> ** WARNING: New pipe size used for routing.
15732> RO100:CO0369 ROUTE PIPE   ->
15733> ** WARNING: New pipe size used for routing.
15734> ** WARNING: New pipe size used for routing.
15735> ** WARNING: New pipe size used for routing.
15736> RO100:CO0378 ROUTE PIPE   ->
15737> ** WARNING: New pipe size used for routing.
15738> RO100:CO0379 ROUTE PIPE   ->
15739> ** WARNING: New pipe size used for routing.
15740> ** WARNING: New pipe size used for routing at 153:36
15741> ****
15742>
15743>

```

# Attachment D

Model 4A – Jock River Reach One Future Conditions – Without SWM controls

JFSA, 2021

SWMHYMO Input & Summary files

```

1      20      Metric units / ID numbers OFF
2      *#*****SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
3      *#*****SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
4      *#*****SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
5      *# Project Name: [Jock River]      Project Number: [1474-16]
6      *# Date        : 04-03-2021
7      *# Modeler     : [M.M.]
8      *# Company     : JFSAinc.
9      *# License #   : 2549237
10     *#*****SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
11     *# CALIBRATION OF SUMMER MODEL PARAMETERS
12     *# USING CONTINUOUS SIMULATIONS
13     *# Rainfall data from JFSA raingauge installed at site + other gauges by the City
14     *# Use data collected from May 1st to July 14, 2003
15     *# 2020-11-30 change TMJSTO in COMPUTE DUALHYD (TMJSTO = 0.1 instead of 0.0001)
16     *# 2020-12-01 correct pond curve values
17     *# 2020-12-01 change W_CLAR_BRAZ XIMP to 0.55, SLPI=[0.5](%) (impervious slope), and
18     LGI up to 700m
19     *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 2462 (NHYDout=["N_TO"]
20     ,NHYDin=["SN_TO"]) from 0.033 % (as per Stantec Report 2007) to 0.05 % so the model
21     will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELS
22     aren't well suited to really flat slopes.
23     *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHYDout=["N_WC"]
24     ,NHYDin=["SN_CE"]) from 0.01 % (as per Stantec Report 2007) to 0.0255 % so the model
25     will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELS
26     aren't well suited to really flat slopes.
27     *
28     * Calibrated parameters for Summer 2003 data: APII=50, APIK=0.85, CN=varies,
29     *                                              SK=0.01, InterEventTime=12,
30     *                                              GWResk=0.96, VHydCond=0.055
31     *
32     *# -----
33     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
34     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
35     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
36     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
37     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
38     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
39     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
40     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
41     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
42     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
43     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
44     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
45     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
46     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
47     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
48     *#
49     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
50     *# of 1.32
51     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
52     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
53     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
54     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
55     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
56     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
57     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
58     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
59     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|

```

```

60          BaseFlowOption=[1] ,
61          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
62          VHydCond=[0.055](mm/hr), END=-1
63 *%-----+-----+
64 *#
65 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
66 *# of 1.32
67 *%-----+-----|
68 CONTINUOUS NASHYD      NHYD=[ "SW_13" ], DT=[1]min, AREA=[971](ha),
69          DWF=[0](cms), CN/C=[61], IA=[2.5](mm),
70          N=[3.0], TP=[3.76]hrs,
71          Continuous simulation parameters:
72          IaRECper=[4](hrs),
73          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
74          InterEventTime=[12](hrs)
75          Baseflow simulation parameters:
76          BaseFlowOption=[1] ,
77          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
78          VHydCond=[0.055](mm/hr), END=-1
79 *%-----+-----|
80 *#
81 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
82 *# of 1.80
83 *%-----+-----|
84 CONTINUOUS NASHYD      NHYD=[ "JR_GWM" ], DT=[1]min, AREA=[3074](ha),
85          DWF=[0](cms), CN/C=[55], IA=[2.5](mm),
86          N=[3], TP=[11.33]hrs,
87          Continuous simulation parameters:
88          IaRECper=[4](hrs),
89          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
90          InterEventTime=[12](hrs)
91          Baseflow simulation parameters:
92          BaseFlowOption=[1] ,
93          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
94          VHydCond=[0.055](mm/hr), END=-1
95 *%-----+-----|
96 CONTINUOUS NASHYD      NHYD=[ "JR_ASH" ], DT=[1]min, AREA=[1781](ha),
97          DWF=[0](cms), CN/C=[72], IA=[2.5](mm),
98          N=[3.0], TP=[3.91]hrs,
99          Continuous simulation parameters:
100         IaRECper=[4](hrs),
101         SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
102         InterEventTime=[12](hrs)
103         Baseflow simulation parameters:
104         BaseFlowOption=[1] ,
105         InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
106         VHydCond=[0.055](mm/hr), END=-1
107 *%-----+-----|
108 CONTINUOUS NASHYD      NHYD=[ "SW_11" ], DT=[1]min, AREA=[500](ha),
109          DWF=[0](cms), CN/C=[66], IA=[2.5](mm),
110          N=[3.0], TP=[1.24]hrs,
111          Continuous simulation parameters:
112          IaRECper=[4](hrs),
113          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
114          InterEventTime=[12](hrs)
115          Baseflow simulation parameters:
116          BaseFlowOption=[1] ,
117          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
118          VHydCond=[0.055](mm/hr), END=-1
119 *%-----+-----|
120 *#
121 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
122 *# of 1.80
123 *%-----+-----|
124 CONTINUOUS NASHYD      NHYD=[ "NN_CK" ], DT=[1]min, AREA=[1917](ha),
125          DWF=[0](cms), CN/C=[66], IA=[2.5](mm),

```

```

126      N=[3.0], TP=[5.29]hrs,
127      Continuous simulation parameters:
128      IaRECper=[4](hrs),
129      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
130      InterEventTime=[12](hrs)
131      Baseflow simulation parameters:
132      BaseFlowOption=[1] ,
133      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
134      VHydCond=[0.055](mm/hr), END=-1
135      *%-----|-----|
136      *#
137      *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
138      *# of 1.52
139      *%-----|-----|
140      CONTINUOUS NASHYD      NHYD=[ "SW_10" ], DT=[1]min, AREA=[5666](ha),
141      DWF=[0](cms), CN/C=[72], IA=[2.5](mm),
142      N=[3.0], TP=[8.00]hrs,
143      Continuous simulation parameters:
144      IaRECper=[4](hrs),
145      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
146      InterEventTime=[12](hrs)
147      Baseflow simulation parameters:
148      BaseFlowOption=[1] ,
149      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
150      VHydCond=[0.055](mm/hr), END=-1
151      *%-----|-----|
152      *#
153      *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
154      *# of 1.75
155      *%-----|-----|
156      CONTINUOUS NASHYD      NHYD=[ "KG_CK" ], DT=[1]min, AREA=[8376](ha),
157      DWF=[0](cms), CN/C=[66], IA=[2.5](mm),
158      N=[3.0], TP=[11.66]hrs,
159      Continuous simulation parameters:
160      IaRECper=[4](hrs),
161      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
162      InterEventTime=[12](hrs)
163      Baseflow simulation parameters:
164      BaseFlowOption=[1] ,
165      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
166      VHydCond=[0.055](mm/hr), END=-1
167      *%-----|-----|
168      *#
169      *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
170      *# of 1.68
171      *%-----|-----|
172      CONTINUOUS NASHYD      NHYD=[ "SW_9" ], DT=[1]min, AREA=[1132](ha),
173      DWF=[0](cms), CN/C=[70], IA=[2.5](mm),
174      N=[3.0], TP=[2.51]hrs,
175      Continuous simulation parameters:
176      IaRECper=[4](hrs),
177      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
178      InterEventTime=[12](hrs)
179      Baseflow simulation parameters:
180      BaseFlowOption=[1] ,
181      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
182      VHydCond=[0.055](mm/hr), END=-1
183      *%-----|-----|
184      *#
185      *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
186      *# of 1.82
187      *%-----|-----|
188      CONTINUOUS NASHYD      NHYD=[ "NC_CK" ], DT=[1]min, AREA=[4464](ha),
189      DWF=[0](cms), CN/C=[62], IA=[2.5](mm),
190      N=[3.0], TP=[11.32]hrs,
191      Continuous simulation parameters:

```

```

192
193     IaRECper=[4](hrs),
194     SMIN=[-1](mm),   SMAX=[-1](mm),  SK=[0.010]/(mm),
195     InterEventTime=[12](hrs)
196     Baseflow simulation parameters:
197     BaseFlowOption=[1] ,
198     InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
199     VHydCond=[0.055](mm/hr),    END=-1
200
201 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
202 *# of 1.80
203
204 CONTINUOUS NASHYD      NHYD=[ "SW_8" ], DT=[1]min, AREA=[131](ha),
205     DWF=[0](cms),  CN/C=[63],  IA=[2.5](mm),
206     N=[3.0],  TP=[0.90]hrs,
207     Continuous simulation parameters:
208     IaRECper=[4](hrs),
209     SMIN=[-1](mm),   SMAX=[-1](mm),  SK=[0.010]/(mm),
210     InterEventTime=[12](hrs)
211     Baseflow simulation parameters:
212     BaseFlowOption=[1] ,
213     InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
214     VHydCond=[0.055](mm/hr),    END=-1
215
216 *#
217 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
218 *# of 1.65
219
220 CONTINUOUS NASHYD      NHYD=[ "HB_DR" ], DT=[1]min, AREA=[3854](ha),
221     DWF=[0](cms),  CN/C=[66],  IA=[2.5](mm),
222     N=[3.0],  TP=[8.42]hrs,
223     Continuous simulation parameters:
224     IaRECper=[4](hrs),
225     SMIN=[-1](mm),   SMAX=[-1](mm),  SK=[0.010]/(mm),
226     InterEventTime=[12](hrs)
227     Baseflow simulation parameters:
228     BaseFlowOption=[1] ,
229     InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
230     VHydCond=[0.055](mm/hr),    END=-1
231
232 *#
233 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
234 *# of 1.82
235
236 CONTINUOUS NASHYD      NHYD=[ "SW_7" ], DT=[1]min, AREA=[3197](ha),
237     DWF=[0](cms),  CN/C=[57],  IA=[2.5](mm),
238     N=[3.0],  TP=[6.65]hrs,
239     Continuous simulation parameters:
240     IaRECper=[4](hrs),
241     SMIN=[-1](mm),   SMAX=[-1](mm),  SK=[0.010]/(mm),
242     InterEventTime=[12](hrs)
243     Baseflow simulation parameters:
244     BaseFlowOption=[1] ,
245     InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
246     VHydCond=[0.055](mm/hr),    END=-1
247
248 *#
249 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
250 *# of 1.75
251
252 CONTINUOUS NASHYD      NHYD=[ "SW_6" ], DT=[1]min, AREA=[165](ha),
253     DWF=[0](cms),  CN/C=[67],  IA=[2.5](mm),
254     N=[3.0],  TP=[4.18]hrs,
255     Continuous simulation parameters:
256     IaRECper=[4](hrs),
257     SMIN=[-1](mm),   SMAX=[-1](mm),  SK=[0.010]/(mm),

```

```

258
259
260
261
262
263 *%-----|-----|
264 *#
265 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
266 *# of 1.67
267 *%-----|-----|
268 CONTINUOUS NASHYD NHYD= ["VG_DR"], DT=[1]min, AREA=[1332](ha),
269 DWF=[0](cms), CN/C=[72], IA=[2.5](mm),
270 N=[3.0], TP=[5.95]hrs,
271 Continuous simulation parameters:
272 IaRECper=[4](hrs),
273 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
274 InterEventTime=[12](hrs)
275 Baseflow simulation parameters:
276 BaseFlowOption=[1],
277 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
278 VHydCond=[0.055](mm/hr), END=-1
279 *%-----|-----|
280 CONTINUOUS NASHYD NHYD= ["SW_5"], DT=[1]min, AREA=[224](ha),
281 DWF=[0](cms), CN/C=[77], IA=[2.5](mm),
282 N=[3.0], TP=[0.75]hrs,
283 Continuous simulation parameters:
284 IaRECper=[4](hrs),
285 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
286 InterEventTime=[12](hrs)
287 Baseflow simulation parameters:
288 BaseFlowOption=[1],
289 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
290 VHydCond=[0.055](mm/hr), END=-1
291 *%-----|-----|
292 *#
293 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
294 *# of 1.20
295 *%-----|-----|
296 CONTINUOUS NASHYD NHYD= ["FL_CK"], DT=[1]min, AREA=[4945](ha),
297 DWF=[0](cms), CN/C=[74], IA=[2.5](mm),
298 N=[3.0], TP=[4.45]hrs,
299 Continuous simulation parameters:
300 IaRECper=[4](hrs),
301 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
302 InterEventTime=[12](hrs)
303 Baseflow simulation parameters:
304 BaseFlowOption=[1],
305 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
306 VHydCond=[0.055](mm/hr), END=-1
307 *%-----|-----|
308 CONTINUOUS NASHYD NHYD= ["SW_5A2"], DT=[1]min, AREA=[20](ha),
309 DWF=[0](cms), CN/C=[81], IA=[2.5](mm),
310 N=[3.0], TP=[0.62]hrs,
311 Continuous simulation parameters:
312 IaRECper=[4](hrs),
313 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
314 InterEventTime=[12](hrs)
315 Baseflow simulation parameters:
316 BaseFlowOption=[1],
317 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
318 VHydCond=[0.055](mm/hr), END=-1
319 *%-----|-----|
320 *#
321 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
322 *# of 1.61
323 *%-----|-----|

```

```

324 CONTINUOUS NASHYD NHYD=[ "SW_5A1" ], DT=[1]min, AREA=[1412](ha),
325 DWF=[0](cms), CN/C=[75], IA=[2.5](mm),
326 N=[3.0], TP=[8.00]hrs,
327 Continuous simulation parameters:
328 IaRECper=[4](hrs),
329 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
330 InterEventTime=[12](hrs)
331 Baseflow simulation parameters:
332 BaseFlowOption=[1],
333 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
334 VHydCond=[0.055](mm/hr), END=-1
335 *%
336 CONTINUOUS NASHYD NHYD=[ "SW_4" ], DT=[1]min, AREA=[585](ha),
337 DWF=[0](cms), CN/C=[81], IA=[2.5](mm),
338 N=[3.0], TP=[1.75]hrs,
339 Continuous simulation parameters:
340 IaRECper=[4](hrs),
341 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
342 InterEventTime=[12](hrs)
343 Baseflow simulation parameters:
344 BaseFlowOption=[1],
345 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
346 VHydCond=[0.055](mm/hr), END=-1
347 *%
348 CONTINUOUS NASHYD NHYD=[ "LM_CK" ], DT=[1]min, AREA=[1021](ha),
349 DWF=[0](cms), CN/C=[80], IA=[2.5](mm),
350 N=[3.0], TP=[2.46]hrs,
351 Continuous simulation parameters:
352 IaRECper=[4](hrs),
353 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
354 InterEventTime=[12](hrs)
355 Baseflow simulation parameters:
356 BaseFlowOption=[1],
357 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
358 VHydCond=[0.055](mm/hr), END=-1
359 *%
360 CONTINUOUS NASHYD NHYD=[ "SW_2" ], DT=[1]min, AREA=[177](ha),
361 DWF=[0](cms), CN/C=[77], IA=[2.5](mm),
362 N=[3.0], TP=[0.75]hrs,
363 Continuous simulation parameters:
364 IaRECper=[4](hrs),
365 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
366 InterEventTime=[12](hrs)
367 Baseflow simulation parameters:
368 BaseFlowOption=[1],
369 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
370 VHydCond=[0.055](mm/hr), END=-1
371 *%
372 CONTINUOUS NASHYD NHYD=[ "SM_DR" ], DT=[1]min, AREA=[1122](ha),
373 DWF=[0](cms), CN/C=[81], IA=[2.5](mm),
374 N=[3.0], TP=[3.25]hrs,
375 Continuous simulation parameters:
376 IaRECper=[4](hrs),
377 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
378 InterEventTime=[12](hrs)
379 Baseflow simulation parameters:
380 BaseFlowOption=[1],
381 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
382 VHydCond=[0.055](mm/hr), END=-1
383 *%
384 CONTINUOUS NASHYD NHYD=[ "MO_DR" ], DT=[1]min, AREA=[2737](ha),
385 DWF=[0](cms), CN/C=[76], IA=[2.5](mm),
386 N=[3.0], TP=[3.03]hrs,
387 Continuous simulation parameters:
388 IaRECper=[4](hrs),
389 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),

```

```

390
391     InterEventTime=[12](hrs)
392     Baseflow simulation parameters:
393     BaseFlowOption=[1] ,
394     InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
395     VHydCond=[0.055](mm/hr), END=-1
396 *%-----|-----
397 *      -JFSA 2020 replaced SW_1 with a detailed model from Stantec Report 2007
398 *CONTINUOUS NASHYD   NHYD=[ "SW_1"], DT=[1]min, AREA=[3176](ha),
399 *          DWF=[0](cms), CN/C=[78], IA=[2.5](mm),
400 *          N=[3.0], TP=[3.56]hrs,
401 *          Continuous simulation parameters:
402 *          IaRECper=[4](hrs),
403 *          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
404 *          InterEventTime=[12](hrs)
405 *          Baseflow simulation parameters:
406 *          BaseFlowOption=[1] ,
407 *          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
408 *          VHydCond=[0.055](mm/hr), END=-1
409 *%-----|-----
410 *#
411 *# Routing hydrographs
412 *# Starting with the addition of Jock River Headwater and Subwatershed 13
413 *#
414 ADD HYD           NHYDsum=[ "S_N13"], NHYDs to add=[ "JR_HW"+"SW_13"]
415 *%-----|-----
416 *#
417 *# Sum of hydrographs from Node 13 routed to Node 13A
418 *# (Approximated cross-section - see cross-section 258)
419 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
420 *#
421 ROUTE CHANNEL      NHYDout=[ "N13A"] ,NHYDin=[ "S_N13"],
422             RDT=[1](min),
423             CHLGTH=[ 9074](m), CHSLOPE=[0.0220](%),
424             FPSLOPE=[0.0220](%),
425             SECNUM=[1.0], NSEG=[1]
426             ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
427             ( DISTANCE (m), ELEVATION (m))=
428                 [-40, 132.5]
429                 [-30, 132]
430                 [-25, 131.5]
431                 [-13, 130]
432                 [-8, 127.00]
433                 [-7, 126.50]
434                 [-6, 126]
435                 [-5.5, 125.50]
436                 [0, 123.75]
437                 [4.5, 125.50]
438                 [6, 126]
439                 [7.5, 126.5]
440                 [9, 127]
441                 [10, 127.5]
442                 [11.5, 128.0]
443                 [15.5, 129.5]
444 *%-----|-----
445 *#
446 *# Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
447 *#
448 ADD HYD           NHYDsum=[ "SN13A"], NHYDs to add=[ "N13A"+"JR_GWM"]
449 *%-----|-----
450 *#
451 *# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
452 *#
453 ROUTE RESERVOIR    NHYDout=[ "RES_GM"] ,NHYDin=[ "SN13A"],
454             RDT=[1](min),
455             TABLE of ( OUTFLOW-STORAGE ) values

```

```

456          (cms) - (ha-m)
457          [ 0.0 , 0.0 ]
458          [1.991, 2.144 ]
459          [2.693, 39.826 ]
460          [3.509, 81.697 ]
461          [4.578, 318.774 ]
462          [5.647, 594.947 ]
463          [7.109, 910.219 ]
464          [8.616, 1264.589 ]
465          [10.371, 1658.057 ]
466          [12.402, 2090.622 ]
467          [22.056, 3462.487 ]
468          [ -1 , -1 ] (max twenty pts)
469      NHYDovf=[ " " ] ,
470 *%-----|-----|
471 *#
472 SAVE HYD          NHYD=[ "RES_GM" ], # OF PCYCLES=[-1], ICASEsh=[-1]
473          HYD_FILENAME=[ "H_ESGM" ]
474          HYD_COMMENT=[ "Outflow from Res GM" ]
475 *%-----|-----|
476 *# Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
477 *# (Approximated cross-section - see cross-section 258)
478 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
479 ROUTE CHANNEL      NHYDout=[ "N12" ] ,NHYDin=[ "RES_GM" ] ,
480          RDT=[1](min),
481          CHLGTH=[5926](m), CHSLOPE=[0.0759](%), FPSLOPE=[0.0759](%),
482          SECNUM=[1.0], NSEG=[1]
483          ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
484          ( DISTANCE (m), ELEVATION (m))=
485          [-40, 132.5]
486          [-30, 132]
487          [-25, 131.5]
488          [-13, 130]
489          [-8, 127.00]
490          [-7, 126.50]
491          [-6, 126]
492          [-5.5, 125.50]
493          [0, 123.75]
494          [4.5, 125.50]
495          [6, 126]
496          [7.5, 126.5]
497          [9, 127]
498          [10, 127.5]
499          [11.5, 128.00]
500          [15.5, 129.5]
501
502 *%-----|-----|
503 *#
504 *# Addition of Subwatershed Jock River at Ashton to Node 12
505 *#
506 ADD HYD          NHYDsum=[ "S_N12" ], NHYDs to add=[ "N12"+"JR_ASH" ]
507 SAVE HYD          NHYD=[ "S_N12" ], # OF PCYCLES=[-1], ICASEsh=[-1]
508          HYD_FILENAME=[ "H_SN12" ]
509          HYD_COMMENT=[ "flow at S_N12 near Ashton" ]
510 *%-----|-----|
511 *#
512 *# Sum of hydrographs from Node 12 routed to Node 11
513 *# (Approximated cross-section - see cross-section 258)
514 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
515 ROUTE CHANNEL      NHYDout=[ "N11" ] ,NHYDin=[ "S_N12" ] ,
516          *
517          RDT=[1](min),
518          *
519          CHLGTH=[972](m), CHSLOPE=[0.0514](%), FPSLOPE=[0.0514](%),
520          *
521          SECNUM=[1.0], NSEG=[1]
522          ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
523          ( DISTANCE (m), ELEVATION (m))=

```

```

522 * [-40, 132.5]
523 * [-30, 132]
524 * [-25, 131.5]
525 * [-13, 130]
526 * [-8, 127.00]
527 * [-7, 126.50]
528 * [-6, 126]
529 * [-5.5, 125.50]
530 * [0, 123.75]
531 * [4.5, 125.50]
532 * [6, 126]
533 * [7.5, 126.5]
534 * [9, 127]
535 * [10, 127.5]
536 * [11.5, 128.00]
537 * [15.5, 129.5]
538 *%-----|-----|-----|
539 *#
540 *# Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
541 *#
542 ROUTE CHANNEL      NHYDout=[ "Dum11" ] ,NHYDin=[ "S_N12" ] ,
543 RDT=[1](min),
544 CHLGTH=[972](m),   CHSLOPE=[0.054](%),
545                                     FPSLOPE=[0.054](%),
546 SECNUM=[1.0],       NSEG=[1]
547 ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
548 ( DISTANCE (m), ELEVATION (m))=
549          [-40, 132.5]
550          [-30, 132]
551          [-25, 131.5]
552          [-13, 130]
553          [-8, 127.00]
554          [-7, 126.50]
555          [-6, 126]
556          [-5.5, 125.50]
557          [0, 123.75]
558          [4.5, 125.50]
559          [6, 126]
560          [7.5, 126.5]
561          [9, 127]
562          [10, 127.5]
563          [11.5, 128.00]
564          [15.5, 129.5]
565 *%-----|-----|-----|
566 *#
567 *# Addition of Subwatershed 11 and No Name Creek to Node 11
568 *#
569 ADD HYD           NHYDsum= [ "S_N11" ], NHYDs to add=[ "Dum11"+ "SW_11" + "NN_CK" ]
570 *%-----|-----|-----|
571 *#
572 *# Sum of hydrographs from Node 11 routed to Node 10
573 *# Section 1
574 *#
575 ROUTE CHANNEL      NHYDout=[ "N10" ] ,NHYDin=[ "S_N11" ] ,
576 RDT=[1](min),
577 CHLGTH=[14028](m),   CHSLOPE=[0.1568](%),
578                                     FPSLOPE=[0.1568](%),
579 SECNUM=[1.0],       NSEG=[5]
580 ( SEGROUGH, SEGDIST (m))=
581          [0.04,-52.82
582          0.1,-6.47
583          -0.05,6.47
584          0.1,45.36
585          0.04,423.88] NSEG times
586 ( DISTANCE (m), ELEVATION (m))=
587          [-226.24 ,112.50]

```

```

588 [-167.50 ,111.50]
589 [-106.81 ,111.00]
590 [-92.37 ,110.00]
591 [-52.82 ,109.00]
592 [-24.90, 109.00]
593 [-17.02, 108.50]
594 [-6.47, 108.00]
595 [6.47, 108.00]
596 [15.67, 108.50]
597 [18.95, 109.00]
598 [45.36, 109.50]
599 [120.79, 110.00]
600 [145.72, 111.00]
601 [181.56, 111.50]
602 [423.88, 112.50]

603 *%-----|-----|
604 *#
605 *# Addition of Subwatershed 10 to Node 10
606 *#
607 ADD HYD      NHYDsum=[ "S_N10" ], NHYDs to add=[ "N10"+"SW_10" ]
608 *%-----|-----|
609 SAVE HYD      NHYD=[ "S_N10" ], # OF PCYCLES=[ -1 ], ICASEsh=[ -1 ]
610          HYD_FILENAME=[ "H_SN10" ]
611          HYD_COMMENT=[ "flow at S_N10: N10 + SW_10" ]
612 *%-----|-----|
613 *# Addition of Kings Creek to S_N10
614 *#
615 ADD HYD      NHYDsum=[ "S_N10A" ], NHYDs to add=[ "S_N10"+"KG_CK" ]
616 *%-----|-----|
617 *#
618 *# Sum of hydrographs from Node 10 routed to Node 9
619 *# Section 2
620 *#
621 ROUTE CHANNEL      NHYDout=[ "N9" ] ,NHYDin=[ "S_N10A" ] ,
622          RDT=[ 1 ](min),
623          CHLGTH=[ 3982 ](m), CHSLOPE=[ 0.0753 ](%),
624          FPSLOPE=[ 0.0753 ](%),
625          SECNUM=[ 1.0 ], NSEG=[ 4 ]
626          ( SEGROUGH, SEGDIST (m))=
627          [ 0.04,-30.27
628          0.05,-18.42
629          -0.05,18.42
630          0.04,131.58 ] NSEG times
631          ( DISTANCE (m), ELEVATION (m))=
632          [-446.74, 106.00]
633          [-415.68, 105.50]
634          [-285.40, 105.00]
635          [-173.77, 104.50]
636          [-144.95, 104.00]
637          [-111.18, 103.50]
638          [-94.06, 103.00]
639          [-71.02, 102.50]
640          [-30.27, 102.00]
641          [-19.33, 100.00]
642          [-18.42, 99.50]
643          [18.42, 99.50]
644          [20.77, 100.00]
645          [27.93, 101.00]
646          [52.29, 101.00]
647          [68.80, 101.50]
648          [79.66, 103.00]
649          [91.50, 103.50]
650          [131.58, 104.00]

651 *%-----|-----|
652 *#
653 *# Addition of Subwatershed 9 and Nichols Creek to Node 9

```

```

654 *#
655 ADD HYD NHYDsum=[ "S_N9" ] , NHYDs to add=[ "N9 "+"SW_9 "+"NC_CK" ]
656 *%-----|-----|
657 *#
658 *# Sum of hydrographs from Node 9 routed to Node 8
659 *# Section 3
660 *#
661 ROUTE CHANNEL NHYDout=[ "N8" ] , NHYDin=[ "S_N9" ] ,
662 RDT=[1](min),
663 CHLGTH=[2269](m), CHSLOPE=[0.0882](%),
664 FPSLOPE=[0.0882](%),
665 SECNUM=[1.0], NSEG=[3]
666 ( SEGROUGH, SEGDIST (m))=
667 [0.1,-17.99
668 -0.045,17.31
669 0.1,456.58] NSEG times
670 ( DISTANCE (m), ELEVATION (m))=
671 [-201.19,100.50]
672 [-135.21, 100.00]
673 [-94.83, 99.50]
674 [-67.05, 99.00]
675 [-17.99, 98.50]
676 [-16.02, 98.00]
677 [-13.95, 97.50]
678 [13.95, 97.50]
679 [15.64, 98.00]
680 [17.31, 98.50]
681 [162.02, 98.50]
682 [172.89 ,99.00]
683 [314.38, 99.00]
684 [343.78, 99.50]
685 [365.67, 100.00]
686 [376.68, 100.00 ]
687 [393.11, 99.50]
688 [404.97, 99.50]
689 [431.70, 100.00]
690 [456.58, 100.50 ]
691 *%-----|-----|
692 *#
693 *# Addition of Subwatershed 8 and Hobb's Drain to Node 8
694 *#
695 ADD HYD NHYDsum=[ "S_N8" ] , NHYDs to add=[ "N8 "+"SW_8 "+"HB_DR" ]
696 *%-----|-----|
697 *#
698 *# Sum of hydrographs from Node 8 routed to Node 7
699 *# Section 4
700 *#
701 ROUTE CHANNEL NHYDout=[ "N7" ] , NHYDin=[ "S_N8" ],
702 RDT=[1](min),
703 CHLGTH=[3750](m), CHSLOPE=[0.0533](%),
704 FPSLOPE=[0.0533](%),
705 SECNUM=[1.0], NSEG=[3]
706 ( SEGROUGH, SEGDIST (m))=
707 [0.12,-18.11
708 -0.07,17.22
709 0.12,590.05] NSEG times
710 ( DISTANCE (m), ELEVATION (m))=
711 [-433.21, 102.00]
712 [-425.34, 101.50]
713 [-377.56, 101.50]
714 [-366.23, 101.00]
715 [-202.60, 100.50]
716 [-96.25, 99.50]
717 [-68.36 99.00]
718 [-18.11, 98.50]
719 [-13.81, 97.50]

```

```

720 [13.81, 97.50]
721 [17.22, 98.50]
722 [161.95, 98.50]
723 [173.11, 99.00]
724 [314.05, 99.00]
725 [365.52, 100.00]
726 [404.70, 99.50]
727 [476.74, 100.50]
728 [502.31, 101.00]
729 [584.69, 101.00]
730 [585.79, 101.00]
731 [590.05, 102.00]
732 *%-----|-----|
733 *#
734 *# Addition of Subwatershed 7 to Node 7
735 *#
736 ADD HYD      NHYDsum=[ "S_N7" ], NHYDs to add=[ "N7" +"SW_7" ]
737 *%-----|-----|
738 SAVE HYD      NHYD=[ "S_N7" ], # OF PCYCLES=[-1], ICASEsh=[-1]
739          HYD_FILENAME=[ "H_SN7" ]
740          HYD_COMMENT=[ "flow at S_N7: N7 + SW_7" ]
741 *%-----|-----|
742 *# Insertion of a reservoir to simulate the effects of the Richmond Fen.
743 *# Storage area and volumes were estimated from available topo maps.
744 *# Release rate from fen was assumed to be controlled by the downstream
745 *# river cross-section for summer conditions. It is was assumed that for up to
746 *# 0.75 m of water, the main channel of the river provided the storage. Above
747 *# this depth, the wetland starts to signigicantly store water.
748 *#
749 ROUTE RESERVOIR   NHYDout=[ "RES_RF" ] ,NHYDin=[ "S_N7" ] ,
750          RDT=[1](min),
751          TABLE of ( OUTFLOW-STORAGE ) values
752          (cms) - (ha-m)
753          TABLE of ( OUTFLOW-STORAGE ) values
754          (cms) - (ha-m)
755          [ 0.0 , 0.0 ]
756          [ 0.9051, 2.40]
757          [ 2.907, 4.13]
758          [ 9.744, 9.18]
759          [ 20.304, 14.96]
760          [ 34.167, 310.21]
761          [ 74.993, 605.46]
762          [ 104.876, 900.71]
763          [ 140.56, 2892.00]
764          [ 225.00, 3615.63]
765          [ -1 , -1 ] (max twenty pts)
766          NHYDovf=[ " " ] ,
767 *%-----|-----|
768 SAVE HYD      NHYD=[ "RES_RF" ], # OF PCYCLES=[-1], ICASEsh=[-1]
769          HYD_FILENAME=[ "H_ResRF" ]
770          HYD_COMMENT=[ "outflow of Richmond Fen" ]
771 *%-----|-----|
772 *#
773 *# Sum of hydrographs from Node 7 routed to Node 6
774 *# Section 5
775 *#
776 ROUTE CHANNEL    NHYDout=[ "N6" ] ,NHYDin=[ "RES_RF" ] ,
777          RDT=[1](min),
778          CHLGTH=[3056](m), CHSLOPE=[0.0818](%), FPSLOPE=[0.0818](%),
779          SECNUM=[1.0] , NSEG=[5]
780          ( SEGROUGH, SEGDIST (m))=
781          [ 0.025,-70.8
782          0.1,-23.9
783          -0.05,23.9
784          0.06,39.8

```

```

786          0.05,96.3] NSEG times
787  ( DISTANCE (m), ELEVATION (m))=
788          [-100.8, 97.00]
789          [-70.8, 96.50]
790          [-52.0, 96.00]
791          [-35.1, 95.50]
792          [-30.6, 95.00]
793          [-23.9, 94.54]
794          [23.9, 94.54]
795          [39.8, 95.00]
796          [50.4, 95.50]
797          [93.5, 96.00]
798          [94.9, 96.50]
799          [96.3, 97.00]
800 *%-----|-----|
801 *#
802 *# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
803 *#
804 ADD HYD      NHYDsum=[ "S_N6" ] , NHYDs to add=[ "N6"+"SW_6"+"VG_DR" ]
805 *%-----|-----|
806 *#
807 *# Sum of hydrographs from Node 6 routed to Node 5
808 *# Section 6
809 *#
810 ROUTE CHANNEL      NHYDout=[ "N5" ] ,NHYDin=[ "S_N6" ] ,
811          RDT=[1](min),
812          CHLGTH=[1852](m),   CHSLOPE=[0.0540](%),
813          FPSLOPE=[0.0540](%),
814          SECNUM=[1.0],       NSEG=[3]
815          ( SEGROUGH, SEGDIST (m))=
816          [0.035,-131.59
817          -0.045,48.96
818          0.1,239.04] NSEG times
819          ( DISTANCE (m), ELEVATION (m))=
820          [-686.30, 94.50]
821          [-675.70, 94.00]
822          [-492.52, 93.00]
823          [-467.28, 94.00]
824          [-131.59, 94.00]
825          [-92.79, 92.50]
826          [-18.06, 91.00]
827          [18.06, 91.00]
828          [43.47, 92.50]
829          [48.96, 94.00]
830          [177.43, 94.00]
831          [239.04,94.50]
832 *%-----|-----|
833 *#
834 *# Addition of Subwatershed 5 and Flowing Creek to Node 5
835 *#
836 ADD HYD      NHYDsum=[ "S_N5" ] , NHYDs to add=[ "N5"+"SW_5"+"FL_CK" ]
837 *%-----|-----|
838 *#
839 *# Sum of hydrographs from Node 5 routed to Node 5A
840 *# Section 7
841 *#
842 ROUTE CHANNEL      NHYDout=[ "N5A" ] ,NHYDin=[ "S_N5" ] ,
843          RDT=[1](min),
844          CHLGTH=[556](m),   CHSLOPE=[0.0900](%),
845          FPSLOPE=[0.0900](%),
846          SECNUM=[1.0],       NSEG=[4]
847          ( SEGROUGH, SEGDIST (m))=
848          [0.04,-41.5
849          0.1,-14.0
850          -0.045,14.0
851          0.1,41.1] NSEG times

```

```

852          ( DISTANCE (m) , ELEVATION (m))=
853                      [-275.8, 93.00]
854                      [-248.6, 92.50]
855                      [-237.0, 92.00]
856                      [-219.3, 91.50]
857                      [-202.1, 91.50]
858                      [-186.0, 92.00]
859                      [-129.2, 92.00]
860                      [-117.6, 91.50]
861                      [-100.6, 91.00]
862                      [-41.5, 91.00]
863                      [-20.0, 91.00]
864                      [-14.0, 90.54]
865                      [14.0, 90.54]
866                      [15.3, 91.00]
867                      [17.3, 91.50]
868                      [38.4, 92.00]
869                      [39.8, 92.50]
870                      [41.1, 93.00]
871 *%-----|-----|
872 *#
873 *# Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
874 *#
875 ADD HYD           NHYDsum=[ "S_N5A" ] , NHYDs to add=[ "N5A"+"SW_5A2"+"SW_5A1" ]
876 *%-----|-----|
877 *#
878 *# Sum of hydrographs from Node 5A routed to Node 4
879 *# Section 8
880 *#
881 ROUTE CHANNEL      NHYDout=[ "N4" ] , NHYDin=[ "S_N5A" ] ,
882             RDT=[1](min),
883             CHLGTH=[4630](m),   CHSLOPE=[0.0432](%),
884                               FPSLOPE=[0.0432](%),
885             SECNUM=[1.0],        NSEG=[3]
886             ( SEGRROUGH, SEGDIST (m))=
887                 [0.05,-28.2
888                 -0.035,28.2
889                 0.05,173.1] NSEG times
890             ( DISTANCE (m) , ELEVATION (m))=
891                         [-38.9, 92.00]
892                         [-35.8, 91.50]
893                         [-33.3, 91.00]
894                         [-28.2, 90.50]
895                         [-15.0, 87.48]
896                         [-5.0, 88.34]
897                         [5.0, 86.20]
898                         [15.0, 88.55]
899                         [28.2, 90.50]
900                         [29.7, 91.00]
901                         [46.5, 91.00]
902                         [127.8, 91.00]
903                         [148.7, 91.50]
904                         [173.1, 92.00]
905 *%-----|-----|
906 *#
907 *# Addition of Subwatershed 4 and Leamy Creek to Node 4
908 *#
909 ADD HYD           NHYDsum=[ "S_N4" ] , NHYDs to add=[ "N4"+"SW_4"+"LM_CK" ]
910 SAVE HYD          NHYD=[ "S_N4" ] , # OF PCYCLES=[-1], ICASEsh=[1]
911             HYD_COMMENT=[ "flow at S_N4" ]
912 *%-----|-----|
913 *#
914 *# Sum of hydrographs from Node 4 routed to Node 2
915 *# Section 9
916 *#
917 ROUTE CHANNEL      NHYDout=[ "N2" ] , NHYDin=[ "S_N4" ] ,

```

```

918 RDT=[1](min),
919 CHLGTH=[1667](m), CHSLOPE=[0.0600](%),
920                                     FPSLOPE=[0.0600](%),
921 SECNUM=[1.0], NSEG=[4]
922 ( SEGROUGH, SEGDIST (m))=
923     [0.1,-28.0
924     -0.04,28.4
925     0.06,31.7
926     0.04,80.2] NSEG times
927 ( DISTANCE (m), ELEVATION (m))=
928     [-36.3, 92.00]
929     [-32.6, 91.50]
930     [-30.2, 91.00]
931     [-28.0, 90.45]
932     [-15.0, 87.48]
933     [-5.0, 88.34]
934     [5.0, 86.20]
935     [15.0, 88.55]
936     [28.0, 90.45]
937     [28.4, 90.50]
938     [30.4, 91.00]
939     [31.7, 91.50]
940     [80.2, 92.00]
941 *%-----|-----|
942 *#
943 *# Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2
944 *#
945 ADD HYD          NHYDsum= [ "S_N2" ], NHYDs to add= [ "N2"+ "SW_2"+ "SM_DR"+ "MO_DR" ]
946 *%-----|-----|
947 SAVE HYD          NHYD= [ "S_N2" ], # OF PCYCLES=[-1], ICASEsh=[-1]
948          HYD_FILENAME=[ "H_SN2" ]
949          HYD_COMMENT=[ "flow at S_N2 Jock River Gauge at Moodie Dr." ]
950 *%-----|-----|
951 *#
952 *# Sum of hydrographs from Node 2 routed to Node 1
953 *# Section 10
954 *#
955 *#***** ****
956 *%READ HYD          NHYD= [ "S_N2" ],
957 *%          HYD_FILENAME=[ "H-S_N2" ]
958 *%-----|-----|
959 *#
960 *# Hydrograph from Node 2 routed to Node 416
961 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 9025
962 *#
963 ROUTE CHANNEL      NHYDout=[ "N_416" ] , NHYDin=[ "S_N2" ] ,
964          RDT=[1](min),
965          CHLGTH=[2327](m), CHSLOPE=[0.0498](%),
966                                     FPSLOPE=[0.0498](%),
967          SECNUM=[1.0], NSEG=[3]
968 ( SEGROUGH, SEGDIST (m))=
969     [0.075,-23.96
970     -0.055,23.96
971     0.075,157.38] NSEG times
972 ( DISTANCE (m), ELEVATION (m))=
973     [-336.97,93.5]
974     [-318.85,93]
975     [-259,92.5]
976     [-133.18,92]
977     [-33.17,92]
978     [-27.21,92]
979     [-26.14,91.5]
980     [-24.99,91]
981     [-23.96,90.5]
982     [-14.33,88.26]
983     [-0.68,88.12]

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984 [14.33,88.26]
985 [23.96,90.5]
986 [32.12,91]
987 [43.74,91.5]
988 [57.09,92]
989 [73.53,92.5]
990 [108.27,93]
991 [125.88,93.5]
992 [144.81,94]
993 [157.38,94.5]
994 *%-----|-----|-----|-----|
995 *#*****|-----|-----|-----|-----|
996 *#      Catchment SW-1a
997 *#      - Portion of RVCA catchment SW_1 outside of Reach 1 subwatershed
998 *#      - Undeveloped agricultural land
999 *#*****|-----|-----|-----|-----|
1000 CONTINUOUS NASHYD NHYD=[ "SW_1a" ], DT=[1]min, AREA=[536.42](ha),
1001 DWF=[0](cms), CN/C=[72], IA=[4.67](mm),
1002 N=[3], TP=[2.79]hrs,
1003 Continuous simulation parameters:
1004 IaRECper=[4](hrs),
1005 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1006 InterEventTime=[12](hrs)
1007 Baseflow simulation parameters:
1008 BaseFlowOption=[1],
1009 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1010 VHydCond=[0.055](mm/hr), END=-1
1011 *%-----|-----|-----|-----|
1012 *      -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
1013 before station 7245 on Jock River
1014 CONTINUOUS STANDHYD NHYD=[ "S-1-Okeefe" ], DT=[1](min), AREA=[44.93](ha), XIMP=[0.65],
1015 TIMP=[0.65], DWF=[0](cms),
1016 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
1017 IAper=[4.67](mm), SLPP=[2.0](%),
1018 LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
1019 IAimp=[1.57](mm), SLPI=[0.75](%),
1020 LGI=[547.296](m), MNI=[0.013], SCI=[0](min),
1021 Continuous simulation parameters:
1022 IaRECper=[4](hrs), IaRECImp=[4](hrs),
1023 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1024 InterEventTime=[12](hrs), END=-1
1025 *%-----|-----|-----|-----|
1026 *COMPUTE DUALHYD NHYDin=[ "S-1-Okeefe" ], CINLET=[ 4.796 ](cms), NINLET=[1],
1027 * MajNHYD=[ "S-1-OkMJ" ]
1028 * MinNHYD=[ "S-1-OkMN" ]
1029 * TMJSTO=[ 9999999 ](cu-m)
1030 *%-----|-----|-----|-----|
1031 *ADD HYD NHYDsum=[ "S-1-OkS" ], NHYDs to add=[ "S-1-OkMJ" + "S-1-OkMN" ]
1032 *%-----|-----|-----|-----|
1033 *ROUTE RESERVOIR NHYDout=[ "S-1-OkSR" ], NHYDin=[ "S-1-OkS" ],
1034 * RDT=[1](min),
1035 *          TABLE of ( OUTFLOW-STORAGE ) values
1036 *          (cms) - (ha-m)
1037 *          [ 0.0 , 0.0 ]
1038 *          [ 0.5370 , 1.7917 ]
1039 *          [ -1 , -1 ] (max twenty pts)
1040 *          NHYDovf=[ "S-1-OkSovf" ]
1041 *%-----|-----|-----|-----|
1042 ADD HYD NHYDsum=[ "SN_416" ], NHYDs to add=[ "N_416" + "SW_1a" + "S-1-Okeefe" ]
1043 *%-----|-----|-----|-----|
1044 SAVE HYD NHYD=[ "SN_416" ], # OF PCYCLES=[-1], ICASEsh=[1]
1045 *          HYD_COMMENT=[ "Total Flows at Highway 416" ]
1046 *%-----|-----|-----|-----|
1047 *#
1048 *# Hydrograph from Node 416 routed to Node at Okeefe drain
1049 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 7245

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1046 *#
1047 ROUTE CHANNEL      NHYDout=[ "N_OK" ] , NHYDin=[ "SN_416" ] ,
1048                               RDT=[ 1 ](min),
1049                               CHLGTH=[ 497 ](m),   CHSLOPE=[ 0.3018 ](%),
1050                               FPSLOPE=[ 0.3018 ](%),
1051                               SECNUM=[ 1.0 ],        NSEG=[ 3 ]
1052                               ( SEGROUGH, SEGDIST (m))=
1053                               [ 0.075,-19.40
1054                               -0.055,19.40
1055                               0.075,377.02] NSEG times
1056                               ( DISTANCE (m), ELEVATION (m))=
1057                               [-1061.41, 92.50]
1058                               [-945.91, 92.00]
1059                               [-783.64, 91.50]
1060                               [-136.74, 91.00]
1061                               [-86.04, 91.00]
1062                               [-20.86, 91.00]
1063                               [-20.18, 90.50]
1064                               [-19.40, 90.00]
1065                               [-11.68, 86.89]
1066                               [ 0.00, 86.10]
1067                               [12.09, 86.81]
1068                               [19.40, 90.00]
1069                               [34.68, 90.50]
1070                               [60.56, 91.00]
1071                               [170.14, 91.00]
1072                               [175.05, 90.50]
1073                               [180.29, 90.00]
1074                               [193.41, 90.00]
1075                               [195.98, 90.50]
1076                               [377.02, 92.50]
1077 *%-----|-----|
1078 *#*****
1079 *#      Catchment OKEEFE
1080 *#      - To O'Keefe drain (north of the Jock)
1081 *#      - Developed with assumed 43% imp.
1082 *#      - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area
1083 *#      - 2020-11-20 Okeefe detailed model was added as per the NOVATECH SWMHMO model
1084 *#      (Citi-Gate 2014).
1085 *#-----|-----|
1086 *POST DEVELOPMENT CONDITIONS
1087 *%-----|-----|
1088 *#*****
1089 CONTINUOUS NASHYD      NHYD=[ "O-1" ], DT=[ 1 ]min, AREA=[ 63.72 ](ha),
1090                               DWF=[ 0 ](cms), CN/C=[ 61 ], IA=[ 6.2 ](mm), N=[ 3 ], TP=[ .9 ]hrs,
1091                               Continuous simulation parameters:
1092                               IaRECper=[ 4 ](hrs),
1093                               SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1094                               InterEventTime=[ 12 ](hrs)
1095                               Baseflow simulation parameters:
1096                               BaseFlowOption=[ 1 ],
1097                               InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
1098                               VHdCond=[ 0.055 ](mm/hr), END=-1
1099 *%-----|-----|
1100 *ROUTE FLOW THROUGH AREA 0-2
1101 ROUTE CHANNEL      NHYDout=[ "O-1R" ], NHYDin=[ "O-1" ], RDT=[ 1 ](min),
1102                               CHLGTH=[ 960 ](m), CHSLOPE=[ 0.63 ](%), FPSLOPE=[ 0.63 ](%),
1103                               SECNUM=[ 1 ], NSEG=[ 3 ]
1104                               ( SEGROUGH, SEGDIST (m))=[ 0.06, 4 -.043, 6 0.06, 10 ] NSEG times
1105                               ( DISTANCE (m), ELEVATION (m))=[ 0.00, 2.0 ]
1106                               [ 0.0, 2.0 ]
1107                               [ 4.0, 0.0 ]
1108                               [ 6.0, 0.0 ]
1109                               [ 10.0, 2.0 ]

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1109 *%
1110 CONTINUOUS NASHYD NYHD=[ "O-2" ], DT=[1]min, AREA=[ 28.61 ](ha),
1111 DWF=[ 0 ](cms), CN/C=[ 57 ], IA=[ 5.2 ](mm), N=[ 3 ], TP=[ 1.1 ]hrs,
1112 Continuous simulation parameters:
1113 IaRECper=[ 4 ](hrs),
1114 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1115 InterEventTime=[ 12 ](hrs)
1116 Baseflow simulation parameters:
1117 BaseFlowOption=[ 1 ],
1118 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
1119 VHdCond=[ 0.055 ](mm/hr), END=-1
1120 *%
1121 CONTINUOUS NASHYD NYHD=[ "O-4" ], DT=[1]min, AREA=[ 46.94 ](ha),
1122 DWF=[ 0 ](cms), CN/C=[ 49 ], IA=[ 9.2 ](mm), N=[ 3 ], TP=[ 0.9 ]hrs,
1123 Continuous simulation parameters:
1124 IaRECper=[ 4 ](hrs),
1125 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1126 InterEventTime=[ 12 ](hrs)
1127 Baseflow simulation parameters:
1128 BaseFlowOption=[ 1 ],
1129 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
1130 VHdCond=[ 0.055 ](mm/hr), END=-1
1131 *%
1132 *TOTAL EXTERNAL FLOW NORTH OF O'KEEFE CT. CROSSING
1133 ADD HYD NYHDsum=[ "OKF-N" ], NYHDs to add=[ "O-1R"+ "O-2" + "O-4" ]
1134 *%
1135 *ROUTE FLOW THROUGH AREA O-6
1136 ROUTE CHANNEL ROUTE CHANNEL NYHDout=[ "OKF-NR" ], NYDin=[ "OKF-N" ], RDT=[ 1 ](min),
1137 CHLGTH=[ 210 ](m), CHSLOPE=[ .81 ](%), FPSLOPE=[ .81 ](%),
1138 SECNUM=[ 1 ], NSEG=[ 3 ]
1139 ( SEGROUGH, SEGDIST (m) )=[ 0.043, 22.43 -0.043, 25.07
1140 0.043, 45.54 ] NSEG times
1141 ( DISTANCE (m), ELEVATION (m) )=[ 0.00, 3.73 ]
1142 ( 14.62, 1.56 )
1143 ( 18.41, 1.44 )
1144 ( 22.43, 0.00 )
1145 ( 25.07, 0.70 )
1146 ( 29.10, 1.79 )
1147 ( 33.73, 2.71 )
1148 ( 45.54, 3.58 )
1149 *%
1150 CONTINUOUS NASHYD NYHD=[ "O-6" ], DT=[1]min, AREA=[ 16.46 ](ha),
1151 DWF=[ 0 ](cms), CN/C=[ 43 ], IA=[ 9.2 ](mm), N=[ 3 ], TP=[ 0.7 ]hrs,
1152 Continuous simulation parameters:
1153 IaRECper=[ 4 ](hrs),
1154 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1155 InterEventTime=[ 12 ](hrs)
1156 Baseflow simulation parameters:
1157 BaseFlowOption=[ 1 ],
1158 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
1159 VHdCond=[ 0.055 ](mm/hr), END=-1
1160 *%
1161 CONTINUOUS STANDHYD NYHD=[ "O-3" ], DT=[1](min), AREA=[ 39.67 ](ha), XIMP=[ 0.15 ],
1162 TIMP=[ 0.30 ], DWF=[ 0 ](cms),
1163 LOSS=[ 2 ], SCS curve number CN=[ 50 ], Pervious surfaces:
1164 IAper=[ 4.67 ](mm), SLPP=[ 0.32 ](%),
1165 LGP=[ 440 ](m), MNP=[ 0.035 ], SCP=[ 0 ](min), Impervious surfaces:
1166 IAimp=[ 1.57 ](mm), SLPI=[ 0.32 ](%),
1167 LGI=[ 1880 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1168 Continuous simulation parameters:
1169 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
1170 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1171 InterEventTime=[ 12 ](hrs), END=-1
1172 *%
1173 CONTINUOUS STANDHYD NYHD=[ "O-5" ], DT=[1](min), AREA=[ 60.63 ](ha), XIMP=[ 0.13 ],
1174 TIMP=[ 0.26 ], DWF=[ 0 ](cms),

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1171 LOSS=[2], SCS curve number CN=[61],
1172 Previous surfaces: IAper=[4.67](mm), SLPP=[1.38](%),
1173 LGP=[550](m), MNP=[0.035], SCP=[0](min), Impervious surfaces:
1174 IAimp=[1.57](mm), SLPI=[1.38](%),
1175 LGI=[1450](m), MNI=[0.013], SCI=[0](min),
1176 Continuous simulation parameters:
1177 IaRECper=[4](hrs), IaRECImp=[4](hrs),
1178 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1179 InterEventTime=[12](hrs), END=-1
1180 *%-----|-----|
1181 *TOTAL EXTERNAL FLOWS WEST OF THE SITE AND NORTH OF O'KEEFE CRT
1182 *%-----|-----|
1183 ADD HYD NHYDsum=[ "PT1" ], NHYDs to add=[ "OKF-NR "+"O-3 "+"O-5 "+"O-6" ]
1184 *%-----|-----|
1185 CONTINUOUS NASHYD NHYD=[ "O-7" ], DT=[1]min, AREA=[5.28](ha),
1186 DWF=[0](cms), CN/C=[54], IA=[7.5](mm), N=[3], TP=[0.6]hrs,
1187 Continuous simulation parameters:
1188 IaRECper=[4](hrs),
1189 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1190 InterEventTime=[12](hrs)
1191 Baseflow simulation parameters:
1192 BaseFlowOption=[1] ,
1193 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1194 VHydCond=[0.055](mm/hr), END=-1
1195 *%-----|-----|
1196 *ANALYSIS POINT 1 - TOTAL FLOW NORTH OF FALLOWFIELD DR. AND O'KEEFE CRT.
1197 ADD HYD NHYDsum=[ "FF" ], NHYDs to add=[ "PT1"+"O-7" ]
1198 *%-----|-----|
1199 ROUTE CHANNEL NHYDout=[ "DRAIN1" ], NHYDin=[ "FF" ], RDT=[1](min),
1200 CHLGT=[302]{m}, CHSLOPE=[1.00](%), FPSLOPE=[1.00](%),
1201 SECNUM=[1], NSEG=[3]
1202 ( SEGRROUGH, SEGDIST (m))=[0.07,13.45 -0.043,16.55 0.07,30.00] NSEG
times
1203 ( DISTANCE (m), ELEVATION (m))=[0.00, 1.70]
1204 (3.45, 0.60)
1205 (13.45, 0.50)
1206 (14.45, 0.00)
1207 (15.55, 0.00)
1208 (16.55, 0.50)
1209 (26.55, 0.60)
1210 (30.00, 1.70)
1211 *%-----|-----|
1212 CONTINUOUS NASHYD NHYD=[ "D1" ], DT=[1]min, AREA=[1.17](ha),
1213 DWF=[0](cms), CN/C=[84], IA=[9.0](mm), N=[3], TP=[0.28]hrs,
1214 Continuous simulation parameters:
1215 IaRECper=[4](hrs),
1216 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1217 InterEventTime=[12](hrs)
1218 Baseflow simulation parameters:
1219 BaseFlowOption=[1] ,
1220 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1221 VHydCond=[0.055](mm/hr), END=-1
1222 *%-----|-----|
1223 CONTINUOUS STANDHYD NHYD=[ "A1" ], DT=[1]min, AREA=[2.50](ha), XIMP=[0.68], TIMP=[0.85],
1224 DWF=[0](cms), LOSS=[1]:
Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1225 F=[0.00](mm),
Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1226 MNP=[0.250], SCP=[0](min),
Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
1227 LGI=[223.607](m), MNI=[0.013], SCI=[0](min),
Continuous simulation parameters:
1228 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
1229 END=-1
1230 *%-----|-----|

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1230 ROUTE RESERVOIR      NHYDout=[ "A1-STR" ], NHYDin=[ "A1" ], RDT=[1](min),
1231                                     TABLE of ( OUTFLOW-STORAGE ) values
1232                                     (cms) - (ha-m)
1233                                     [ 0.000 , 0.000 ]
1234                                     [ 0.035 , 0.038 ]
1235                                     [ 0.072 , 0.051 ]
1236                                     [ 0.100 , 0.059 ]
1237                                     [ 0.125 , 0.070 ]
1238                                     [ 0.160 , 0.074 ]
1239                                     [ 0.185 , 0.081 ]
1240                                     [ -1 , -1 ] (max twenty pts)
1241                                     NHYDovf=[ "A1-OVF" ]
1242 *%
1243 CONTINUOUS STANDHYD  NHYD=[ "ST-2" ], DT=[1]min, AREA=[ 0.59 ](ha), XIMP=[ 0.46 ],
1244 TIMP=[ 0.57 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
1245                                     Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
1246                                     F=[ 0.00 ](mm),
1247                                     Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%), LGP=[ 50 ](m),
1248                                     MNP=[ 0.250 ], SCP=[ 0 ](min),
1249                                     Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%),
1250                                     LGI=[ 108.628 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1251                                     Continuous simulation parameters:
1252                                     IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
1253                                     END=-1
1254 *%
1255 ROUTE RESERVOIR      NHYDout=[ "ST2STR" ], NHYDin=[ "ST-2" ], RDT=[1](min),
1256                                     TABLE of ( OUTFLOW-STORAGE ) values
1257                                     (cms) - (ha-m)
1258                                     [ 0.000 , 0.0000 ]
1259                                     [ 0.052 , 0.0010 ]
1260                                     [ 0.053 , 0.0080 ]
1261                                     [ -1 , -1 ] (max twenty pts)
1262                                     NHYDovf=[ "ST2OVF" ]
1263 *%
1264 *%
1265 *% TOTAL FLOW NORTH OF STRANDHERD DR. (EAST BRANCH) CROSSING
1266 *%
1267 CONTINUOUS NASHYD    NHYD=[ "O-8" ], DT=[1]min, AREA=[ 60.55 ](ha),
1268 DWF=[ 0 ](cms), CN/C=[ 69 ], IA=[ 4.0 ](mm), N=[ 3 ], TP=[ 1.0 ]hrs,
1269 Continuous simulation parameters:
1270 IaRECper=[ 4 ](hrs),
1271 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1272 InterEventTime=[ 12 ](hrs)
1273 Baseflow simulation parameters:
1274 BaseFlowOption=[ 1 ],
1275 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
1276 VHydCond=[ 0.055 ](mm/hr), END=-1
1277 *%
1278 ROUTE PIPE            PTYPE=[ 2 ]rect, NHYDout=[ "O8PIPE" ], RNUMBER=[ 1 ], PWIDTH=[ 1800 ](mm),
1279 PHEIGHT=[ 1200 ](mm), PLNGTH=[ 335.1 ](m),
1280 PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m), NHYDin=[ "O-8" ], RDT=[1](min)
1281 *%
1282 *%
1283 ADD HYD                NHYDsum=[ "ST2-IN" ], NHYDs to
1284 add=[ "DRAIN1 "+"D1 "+"A1-STR "+"A1-OVF "+"ST2STR "+"ST2OVF "+"O8PIPE" ]
1285 *%
1286 CONTINUOUS STANDHYD  NHYD=[ "A7" ], DT=[1]min, AREA=[ 3.51 ](ha), XIMP=[ 0.68 ], TIMP=[ 0.85 ],
1287 DWF=[ 0 ](cms), LOSS=[ 1 ]:
1288                                     Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
1289                                     F=[ 0.00 ](mm),
1290                                     Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%), LGP=[ 50 ](m),
1291                                     MNP=[ 0.250 ], SCP=[ 0 ](min),
1292                                     Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%),
1293                                     LGI=[ 264.953 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1294                                     Continuous simulation parameters:
1295                                     IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),

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1285      END=-1
1286 *%-----|-----|-----|-----|-----|-----|-----|
1286 ROUTE RESERVOIR      NHYDout= [ "A7-STR" ] , NHYDin= [ "A7" ] , RDT=[1](min),
1287          TABLE of ( OUTFLOW-STORAGE ) values
1288              (cms) - (ha-m)
1289              [ 0.000 , 0.000 ]
1290              [ 0.049 , 0.054 ]
1291              [ 0.102 , 0.072 ]
1292              [ 0.140 , 0.082 ]
1293              [ 0.175 , 0.099 ]
1294              [ 0.225 , 0.105 ]
1295              [ 0.260 , 0.114 ]
1296              [ -1 , -1 ] (max twenty pts)
1297          NHYDovf= [ "A7-OVF" ]
1298 *%-----|-----|-----|-----|-----|-----|-----|
1299 CONTINUOUS STANDHYD      NHYD= [ "ST-3" ] , DT=[1]min, AREA=[0.71](ha), XIMP=[0.46],
1300    TIMP=[0.57], DWF=[0](cms), LOSS=[1]:
1300        Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1301        F=[0.00](mm),
1301        Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1302        MNP=[0.250], SCP=[0](min),
1302        Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[119.164](m), MNI=[0.013], SCI=[0](min),
1303        Continuous simulation parameters:
1304        IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
1304        END=-1
1305 *%-----|-----|-----|-----|-----|-----|-----|
1306 ROUTE RESERVOIR      NHYDout= [ "ST3STR" ] , NHYDin= [ "ST-3" ] , RDT=[1](min),
1307          TABLE of ( OUTFLOW-STORAGE ) values
1308              (cms) - (ha-m)
1309              [ 0.000 , 0.0000 ]
1310              [ 0.063 , 0.0010 ]
1311              [ 0.064 , 0.0094 ]
1312              [ -1 , -1 ] (max twenty pts)
1313          NHYDovf= [ "ST3OVF" ]
1314 *%-----|-----|-----|-----|-----|-----|-----|
1315 *ANALYSIS POINT 2 - TOTAL FLOW AT OUTLET OF STREET 2/3 INTERSECTION
1316 *%-----|-----|-----|-----|-----|-----|-----|
1317 ADD HYD      NHYDsum= [ "PT2ST3" ] , NHYDs to
1317 add= [ "ST2-IN"+ "A7-STR"+ "A7-OVF"+ "ST3STR"+ "ST3OVF" ]
1318 *%-----|-----|-----|-----|-----|-----|-----|
1319 *ROUTE FLOW through O'Keefe Drain 2
1320 ROUTE CHANNEL      NHYDout= [ "DRAIN2" ] , NHYDin= [ "PT2ST3" ] , RDT=[1](min),
1321 CHLGTH=[592]{m}, CHSLOPE=[.23](%), FPSLOPE=[.23](%),
1322 SECNUM=[1], NSEG=[3]
1323 ( SEGROUGH, SEGDIST (m))=[0.07,12.60 -0.043,17.40 0.07,30.00] NSEG
1323 times
1324 ( DISTANCE (m), ELEVATION (m))=[0.00, 1.70]
1325 (2.60, 0.95)
1326 (12.60, 0.75)
1327 (14.10, 0.00)
1328 (15.90, 0.00)
1329 (17.40, 0.75)
1330 (27.40, 0.95)
1331 (30.00, 1.70)
1332 *%-----|-----|-----|-----|-----|-----|-----|
1333 CONTINUOUS NASHYD      NHYD= [ "D2" ] , DT=[1]min, AREA=[2.28](ha), DWF=[0](cms), CN/C=[84],
1333 IA=[9.0](mm),
1334 N=[3], TP=[0.99]hrs,
1335 Continuous simulation parameters:
1336 IaRECper=[4](hrs),
1337 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1338 InterEventTime=[12](hrs)
1339 Baseflow simulation parameters:
1340 BaseFlowOption=[1] ,
1341 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)

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1342          VHydCond=[ 0.055 ](mm/hr) ,      END=-1
1343 *%-----|-----|
1344 CONTINUOUS STANDHYD NHYD=[ "A17" ] , DT=[ 1 ]min, AREA=[ 12.04 ](ha) , XIMP=[ 0.68 ] ,
1345      TIMP=[ 0.85 ] , DWF=[ 0 ](cms) , LOSS=[ 1 ]:
1346          Horton: Fo=[ 76.20 ](mm/hr) , Fc=[ 13.20 ](mm/hr) , DCAY=[ 4.14 ](/hr) ,
1347          F=[ 0.00 ](mm) ,
1348          Pervious areas: IAper=[ 4.67 ](mm) , SLPP=[ 0.5 ](%) , LGP=[ 50 ](m) ,
1349          MNP=[ 0.250 ] , SCP=[ 0 ](min) ,
1350          Impervious areas: IAimp=[ 1.57 ](mm) , SLPI=[ 0.5 ](%) ,
1351          LGI=[ 490.714 ](m) , MNI=[ 0.013 ] , SCI=[ 0 ](min) ,
1352          Continuous simulation parameters:
1353          IaRECper=[ 4 ](hrs) , IaRECImp=[ 4 ](hrs) , InterEventTime=[ 12 ](hrs) ,
1354          END=-1
1355 *%-----|-----|
1356 ROUTE RESERVOIR      NHYDout=[ "A17STR" ] , NHYDin=[ "A17" ] , RDT=[ 1 ](min) ,
1357          TABLE of ( OUTFLOW-STORAGE ) values
1358          (cms) - (ha-m)
1359          [ 0.000 , 0.000 ]
1360          [ 0.169 , 0.185 ]
1361          [ 0.349 , 0.248 ]
1362          [ 0.482 , 0.283 ]
1363          [ 0.602 , 0.338 ]
1364          [ 0.771 , 0.359 ]
1365          [ 0.891 , 0.391 ]
1366          [ -1 , -1 ] (max twenty pts)
1367          NHYDovf=[ "A17OVF" ]
1368 *%-----|-----|
1369 CONTINUOUS STANDHYD NHYD=[ "ST-4" ] , DT=[ 1 ]min, AREA=[ 0.35 ](ha) , XIMP=[ 0.46 ] ,
1370      TIMP=[ 0.57 ] , DWF=[ 0 ](cms) , LOSS=[ 1 ]:
1371          Horton: Fo=[ 76.20 ](mm/hr) , Fc=[ 13.20 ](mm/hr) , DCAY=[ 4.14 ](/hr) ,
1372          F=[ 0.00 ](mm) ,
1373          Pervious areas: IAper=[ 4.67 ](mm) , SLPP=[ 0.5 ](%) , LGP=[ 50 ](m) ,
1374          MNP=[ 0.250 ] , SCP=[ 0 ](min) ,
1375          Impervious areas: IAimp=[ 1.57 ](mm) , SLPI=[ 0.5 ](%) , LGI=[ 83.666 ](m) ,
1376          MNI=[ 0.013 ] , SCI=[ 0 ](min) ,
1377          Continuous simulation parameters:
1378          IaRECper=[ 4 ](hrs) , IaRECImp=[ 4 ](hrs) , InterEventTime=[ 12 ](hrs) ,
1379          END=-1
1380 *%-----|-----|
1381 ROUTE RESERVOIR      NHYDout=[ "ST4STR" ] , NHYDin=[ "ST-4" ] , RDT=[ 1 ](min) ,
1382          TABLE of ( OUTFLOW-STORAGE ) values
1383          (cms) - (ha-m)
1384          [ 0.000 , 0.0000 ]
1385          [ 0.031 , 0.0010 ]
1386          [ 0.032 , 0.0050 ]
1387          [ -1 , -1 ] (max twenty pts)
1388          NHYDovf=[ "ST4OVF" ]
1389 *%-----|-----|
1390 CONTINUOUS STANDHYD NHYD=[ "A18" ] , DT=[ 1 ]min, AREA=[ 5.30 ](ha) , XIMP=[ 0.68 ] , TIMP=[ 0.85 ] ,
1391      DWF=[ 0 ](cms) , LOSS=[ 1 ]:
1392          Horton: Fo=[ 76.20 ](mm/hr) , Fc=[ 13.20 ](mm/hr) , DCAY=[ 4.14 ](/hr) ,
1393          F=[ 0.00 ](mm) ,
1394          Pervious areas: IAper=[ 4.67 ](mm) , SLPP=[ 0.5 ](%) , LGP=[ 50 ](m) ,
1395          MNP=[ 0.250 ] , SCP=[ 0 ](min) ,
1396          Impervious areas: IAimp=[ 1.57 ](mm) , SLPI=[ 0.5 ](%) ,
1397          LGI=[ 325.576 ](m) , MNI=[ 0.013 ] , SCI=[ 0 ](min) ,
1398          Continuous simulation parameters:
1399          IaRECper=[ 4 ](hrs) , IaRECImp=[ 4 ](hrs) , InterEventTime=[ 12 ](hrs) ,
1400          END=-1
1401 *%-----|-----|
1402 ROUTE RESERVOIR      NHYDout=[ "A18STR" ] , NHYDin=[ "A18" ] , RDT=[ 1 ](min) ,
1403          TABLE of ( OUTFLOW-STORAGE ) values
1404          (cms) - (ha-m)
1405          [ 0.000 , 0.000 ]
1406          [ 0.074 , 0.082 ]
1407          [ 0.154 , 0.109 ]

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1393 [ 0.212 , 0.125 ]
1394 [ 0.265 , 0.149 ]
1395 [ 0.339 , 0.158 ]
1396 [ 0.392 , 0.172 ]
1397 [ -1 , -1 ] (max twenty pts)
1398 NHYDovf=[ "A18OVF" ]

1399 *%----- |-----|
1400 *ANALYSIS POINT 3 - TOTAL FLOW AT OUTLET OF STREET 4
1401 *%----- |-----|
1402 ADD HYD NHYDsum=[ "PT3ST4" ], NHYDs to
1403 add=[ "DRAIN2"+ "D2" + "A17STR" + "A17OVF" + "ST4STR" + "ST4OVF" + "A18STR" + "A18OVF" ]
1404 *%----- |-----|
1405 *ROUTE FLOW through O'Keefe Drain 3
1406 ROUTE CHANNEL NHYDout=[ "DRAIN3" ], NHYDin=[ "PT3ST4" ], RDT=[ 1 ](min),
1407 CHLGTH=[ 525 ]{m}, CHSLOPE=[ .23 ](%), FPSLOPE=[ .23 ](%),
1408 SECNUM=[ 1 ], NSEG=[ 3 ]
1409 ( SEGROUGH, SEGDIST (m) )=[ 0.07, 12.50 -0.043, 17.50 0.07, 30.00 ] NSEG
1410 times
1411 ( DISTANCE (m), ELEVATION (m) )=[ 0.00, 1.70 ]
1412 ( 2.50, 1.00 )
1413 ( 12.50, 0.80 )
1414 ( 14.10, 0.00 )
1415 ( 15.90, 0.00 )
1416 ( 17.50, 0.80 )
1417 ( 27.50, 1.00 )
1418 ( 30.00, 1.70 )

1418 *%----- |-----|
1419 CONTINUOUS NASHYD NHYD=[ "D3" ], DT=[ 1 ]min, AREA=[ 2.51 ](ha),
1420 DWF=[ 0 ](cms), CN/C=[ 86 ], IA=[ 8.7 ](mm), N=[ 3 ], TP=[ 0.73 ]hrs,
1421 Continuous simulation parameters:
1422 IaRECper=[ 4 ](hrs),
1423 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1424 InterEventTime=[ 12 ](hrs)
1425 Baseflow simulation parameters:
1426 BaseFlowOption=[ 1 ],
1427 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
1428 VHydCond=[ 0.055 ](mm/hr), END=-1

1428 *%----- |-----|
1429 CONTINUOUS STANDHYD NHYD=[ "C1" ], DT=[ 1 ]min, AREA=[ 3.41 ](ha), XIMP=[ 0.68 ], TIMP=[ 0.85 ],
1430 DWF=[ 0 ](cms), LOSS=[ 1 ]:
1431 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
1432 F=[ 0.00 ](mm),
1433 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%), LGP=[ 50 ](m),
1434 MNP=[ 0.250 ], SCP=[ 0 ](min),
1435 Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%),
1436 LGI=[ 261.151 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1437 Continuous simulation parameters:
1438 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
1439 END=-1

1439 *%----- |-----|
1440 ROUTE RESERVOIR NHYDout=[ "C1-STR" ], NHYDin=[ "C1" ], RDT=[ 1 ](min),
1441 TABLE of ( OUTFLOW-STORAGE ) values
1442 (cms) - (ha-m)
1443 [ 0.000 , 0.000 ]
1444 [ 0.048 , 0.052 ]
1445 [ 0.099 , 0.070 ]
1446 [ 0.136 , 0.080 ]
1447 [ 0.170 , 0.096 ]
1448 [ 0.218 , 0.102 ]
1449 [ 0.252 , 0.111 ]
1450 [ -1 , -1 ] (max twenty pts)
1451 NHYDovf=[ "C1-OVF" ]

1451 *%----- |-----|
1452 CONTINUOUS STANDHYD NHYD=[ "ST-5" ], DT=[ 1 ]min, AREA=[ 0.45 ](ha), XIMP=[ 0.46 ],
1453 TIMP=[ 0.57 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
1454 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),

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1451 F=[0.00](mm),
1452 Previous areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1453 MNP=[0.250], SCP=[0](min),
1454 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[94.868](m),
1455 MNI=[0.013], SCI=[0](min),
1456 Continuous simulation parameters:
1457 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
1458 END=-1
1459 *%-----|-----|
1460 ROUTE RESERVOIR
1461 NHYDout=[ "ST5STR" ], NHYDin=[ "ST-5" ], RDT=[1](min),
1462 TABLE of ( OUTFLOW-STORAGE ) values
1463 (cms) - (ha-m)
1464 [ 0.000 , 0.0000 ]
1465 [ 0.040 , 0.0010 ]
1466 [ 0.041 , 0.0062 ]
1467 [ -1 , -1 ] (max twenty pts)
1468 NHYDovf=[ "ST5OVF" ]
1469 *%-----|-----|
1470 ADD HYD NHYDsum=[ "ST5-E" ], NHYDs to
1471 add=[ "DRAIN3"+ "D3"+ "C1-STR"+ "C1-OVF"+ "ST5STR"+ "ST5OVF" ]
1472 *%-----|-----|
1473 CONTINUOUS STANDHYD NHYD=[ "STRAND" ], DT=[1](min), AREA=[7.59](ha),
1474 XIMP=[0.64], TIMP=[0.85], DWF=[0](cms), LOSS=[1]:
1475 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1476 F=[0.00](mm),
1477 Previous areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[40](m),
1478 MNP=[0.250], SCP=[0](min),
1479 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[1230](m),
1480 MNI=[0.013], SCI=[0](min),
1481 Continuous simulation parameters:
1482 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
1483 END=-1
1484 *%-----|-----|
1485 ROUTE RESERVOIR NHYDout=[ "S-POND" ], NHYDin=[ "STRAND" ], RDT=[1](min),
1486 TABLE of ( OUTFLOW-STORAGE ) values
1487 (cms) - (ha-m)
1488 [ 0.000 , 0.000 ]
1489 [ 0.033 , 0.188 ]
1490 [ 0.057 , 0.253 ]
1491 [ 0.104 , 0.287 ]
1492 [ 0.160 , 0.336 ]
1493 [ 0.340 , 0.346 ]
1494 [ 0.471 , 0.360 ]
1495 [ 0.824 , 0.390 ]
1496 [ -1 , -1 ] (max twenty pts)
1497 NHYDovf=[ "S-OVF" ]
1498 *%-----|-----|
1499 ADD HYD NHYDsum=[ "SSAOUT" ], NHYDs to add=[ "ST5-E"+ "S-POND"+ "S-OVF" ]
1500 *%-----|-----|
1501 SAVE HYD NHYD=[ "SSAOUT" ], # OF PCYCLES=[5], ICASESh=[1]
1502 HYD_COMMENT=[ "SSAOUT" ]
1503 *%-----|-----|
1504 CONTINUOUS STANDHYD NHYD=[ "Area-A" ], DT=[1]min, AREA=[66.75](ha), XIMP=[0.64],
1505 TIMP=[0.80], DWF=[0](cms), LOSS=[1]:
1506 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1507 F=[0.00](mm),
1508 Previous areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1509 MNP=[0.250], SCP=[0](min),
1510 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[1155.422](m),
1511 MNI=[0.013], SCI=[0](min),
1512 Continuous simulation parameters:
1513 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
1514 END=-1
1515 *%-----|-----|
1516 SAVE HYD NHYD=[ "Area-A" ], # OF PCYCLES=[1], ICASESh=[1]
1517 HYD_COMMENT=[ "SMWF-A Inflow" ]

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1503 *%
1504 ROUTE RESERVOIR | NYHDout=[ "SWMF-A" ], NYHDin=[ "Area-A" ], RDT=[1](min),
1505 | TABLE of ( OUTFLOW-STORAGE ) values
1506 | (cms) - (ha-m)
1507 | [ 0.000 , 0.000 ]
1508 | [ 0.103 , 1.077 ]
1509 | [ 0.128 , 1.749 ]
1510 | [ 0.382 , 2.282 ]
1511 | [ 0.703 , 2.582 ]
1512 | [ 1.256 , 2.978 ]
1513 | [ 1.567 , 3.202 ]
1514 | [ 1.955 , 3.493 ]
1515 | [ 2.100 , 3.600 ]
1516 | [ -1 , -1 ] (max twenty pts)
1517 | NYHDovf=[ "SWMAOV" ]
1518 *%
1519 SAVE HYD | NYHD= [ "SWMF-A" ], # OF PCYCLES=[1], ICASEsh=[1]
1520 | HYD_COMMENT= [ "SMWF-A Outflow" ]
1521 *%
1522 *ANALYSIS POINT 4 - TOTAL FLOW AT OUTLET OF STREET 5
1523 *%
1524 ADD HYD | NYHDsum=[ "PT4ST5" ], NYHDs to add=[ "SSAOUT"+ "SWMF-A" +"SWMAOV" ]
1525 *%
1526 CONTINUOUS STANDHYD NYHD= [ "C6" ], DT=[1]min, AREA=[1.87](ha), XIMP=[0.68], TIMP=[0.85],
1527 DWF=[0](cms), LOSS=[1]:
1528 | Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1529 | F=[0.00](mm),
1530 | Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1531 | MNP=[0.250], SCP=[0](min),
1532 | Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
1533 | LGI=[193.391](m), MNI=[0.013], SCI=[0](min),
1534 | Continuous simulation parameters:
1535 | IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
1536 | END=-1
1537 *%
1538 ROUTE RESERVOIR | NYHDout=[ "C6-STR" ], NYHDin=[ "C6" ], RDT=[1](min),
1539 | TABLE of ( OUTFLOW-STORAGE ) values
1540 | (cms) - (ha-m)
1541 | [ 0.000 , 0.000 ]
1542 | [ 0.026 , 0.029 ]
1543 | [ 0.054 , 0.038 ]
1544 | [ 0.075 , 0.044 ]
1545 | [ 0.093 , 0.052 ]
1546 | [ 0.120 , 0.056 ]
1547 | [ 0.138 , 0.061 ]
1548 | [ -1 , -1 ] (max twenty pts)
1549 | NYHDovf=[ "C6-OVF" ]
1550 *%
1551 CONTINUOUS STANDHYD NYHD= [ "C7" ], DT=[1]min, AREA=[1.62](ha), XIMP=[0.68], TIMP=[0.85],
1552 DWF=[0](cms), LOSS=[1]:
1553 | Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1554 | F=[0.00](mm),
1555 | Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1556 | MNP=[0.250], SCP=[0](min),
1557 | Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
1558 | LGI=[180.000](m), MNI=[0.013], SCI=[0](min),
| Continuous simulation parameters:
| IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
| END=-1
1559 *%
1560 ROUTE RESERVOIR | NYHDout=[ "C7-STR" ], NYHDin=[ "C7" ], RDT=[1](min),
1561 | TABLE of ( OUTFLOW-STORAGE ) values
1562 | (cms) - (ha-m)
1563 | [ 0.000 , 0.000 ]
1564 | [ 0.023 , 0.025 ]
1565 | [ 0.047 , 0.033 ]

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1559 [ 0.065 , 0.038 ]
1560 [ 0.081 , 0.045 ]
1561 [ 0.104 , 0.048 ]
1562 [ 0.120 , 0.053 ]
1563 [ -1 , -1 ] (max twenty pts)
1564 NHYDovf=[ "C7-OVF" ]
1565 *%-----|-----|
1566 CONTINUOUS STANDHYD NHYD=[ "ST-6" ], DT=[1]min, AREA=[0.41](ha), XIMP=[0.46], TIMP=[0.57],
1567 DWF=[0](cms), LOSS=[1]:
1568 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1569 F=[0.00](mm),
1570 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1571 MNP=[0.250], SCP=[0](min),
1572 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[90.554](m),
1573 MNI=[0.013], SCI=[0](min),
1574 Continuous simulation parameters:
1575 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
1576 END=-1
1577 *%-----|-----|
1578 ROUTE RESERVOIR NHYDout=[ "ST6STR" ], NHYDin=[ "ST-6" ], RDT=[1](min),
1579 TABLE of ( OUTFLOW-STORAGE ) values
1580 (cms) - (ha-m)
1581 [ 0.000 , 0.0000 ]
1582 [ 0.036 , 0.0010 ]
1583 [ 0.037 , 0.0058 ]
1584 [ -1 , -1 ] (max twenty pts)
1585 NHYDovf=[ "ST6OVF" ]
1586 *%-----|-----|
1587 *ANALYSIS POINT 5 - TOTAL FLOW AT OUTLET OF STREET 6
1588 *%-----|-----|
1589 ADD HYD NHYDsum=[ "PT5ST6" ], NHYDs to
1590 add=[ "PT4ST5" +"C6-STR" +"C6-OVF" +"C7-STR" +"C7-OVF" +"ST6STR" +"ST6OVF" ]
1591 *%-----|-----|
1592 *ROUTE FLOW through O'Keefe Drain 4
1593 ROUTE CHANNEL NHYDout=[ "DRAIN4" ], NHYDin=[ "PT5ST6" ], RDT=[1](min),
1594 CHLGTH=[324]{m}, CHSLOPE=[.10](%), FPSLOPE=[.10](%),
1595 SECNUM=[1], NSEG=[3]
1596 ( SEROUGH, SEGDIST (m))=[0.07,12.00 -0.043,18.00 0.07,30.00] NSEG
1597 times
1598 ( DISTANCE (m), ELEVATION (m))=[0.00, 2.00]
1599 (2.00, 1.20)
1600 (12.00, 1.00)
1601 (14.00, 0.00)
1602 (16.00, 0.00)
1603 (18.00, 1.00)
1604 (28.00, 1.20)
1605 (30.00, 2.00)
1606 *%-----|-----|
1607 CONTINUOUS NASHYD NHYD=[ "D4" ], DT=[1]min, AREA=[1.73](ha), DWF=[0](cms), CN/C=[88],
1608 IA=[8.4](mm),
1609 N=[3], TP=[0.60]hrs,
1610 Continuous simulation parameters:
1611 IaRECper=[4](hrs),
1612 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1613 InterEventTime=[12](hrs)
1614 Baseflow simulation parameters:
1615 BaseFlowOption=[1] ,
1616 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1617 VHydCond=[0.055](mm/hr), END=-1
1618 *%-----|-----|
1619 CONTINUOUS STANDHYD NHYD=[ "Area-B" ], DT=[1]min, AREA=[24.04](ha), XIMP=[0.62],
1620 TIMP=[0.77], DWF=[0](cms), LOSS=[1]:
1621 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1622 F=[0.00](mm),
1623 Pervious areas: IAper=[4.67](mm), SLPP=[1.4](%), LGP=[50](m),
1624 MNP=[0.250], SCP=[0](min),

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1614 Impervious areas: IAimp=[1.57](mm), SLPI=[1.4](%),  

1615 LGI=[693.397](m), MNI=[0.013], SCI=[0](min),  

1616 Continuous simulation parameters:  

1617 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),  

1618 END=-1  

1619 *%-----|  

1620 ROUTE RESERVOIR NHYDout=[ "SWMF-B" ], NHYDin=[ "Area-B" ], RDT=[1](min),  

1621 TABLE of ( OUTFLOW-STORAGE ) values  

1622 (cms) - (ha-m)  

1623 [ 0.000 , 0.000 ]  

1624 [ 0.025 , 0.090 ]  

1625 [ 0.175 , 0.510 ]  

1626 [ 0.350 , 0.710 ]  

1627 [ 0.495 , 0.820 ]  

1628 [ 0.648 , 0.980 ]  

1629 [ 0.965 , 1.045 ]  

1630 [ 1.072 , 1.140 ]  

1631 [ -1 , -1 ] (max twenty pts)  

1632 NHYDovf=[ "SWMBOVF" ]  

1633 *%-----|  

1634 ADD HYD NHYDsum=[ "D4-EX" ], NHYDs to add=[ "DRAIN4"+ "D4" + "SWMF-B" + "SWMBOVF" ]  

1635 *%-----|  

1636 *ROUTE FLOW THROUGH O'Keefe Drain 5  

1637 * JFSA: Nov. 2020, added en points to close X-Section  

1638 ROUTE CHANNEL NHYDout=[ "DRAIN5" ], NHYDin=[ "D4-EX" ], RDT=[1](min),  

1639 CHLNGTH=[413.0](m), CHSLOPE=[0.16](%), FPSLOPE=[0.16](%),  

1640 SECNUM=[1], NSEG=[3]  

1641 ( SEROUGH, SEGDIST (m))=[0.043,12.29 -0.033,17.97  

1642 0.043,32.84] NSEG times  

1643 ( DISTANCE (m), ELEVATION (m))=(-0.01, 2.50)  

1644 [0.00, 1.41]  

1645 [6.13, 0.97]  

1646 [12.29, 0.89]  

1647 [15.71, 0.00]  

1648 [17.97, 0.39]  

1649 [23.04, 0.35]  

1650 [32.83, 0.96]  

1651 (32.84, 2.50)  

1652 *%-----|  

1653 CONTINUOUS NASHYD NHYD=[ "D5" ], DT=[1]min, AREA=[1.90](ha),  

1654 DWF=[0](cms), CN/C=[86], IA=[8.7](mm), N=[3], TP=[0.69]hrs,  

1655 Continuous simulation parameters:  

1656 IaRECper=[4](hrs),  

1657 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),  

1658 InterEventTime=[12](hrs)  

1659 Baseflow simulation parameters:  

1660 BaseFlowOption=[1],  

1661 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)  

1662 VHdyCond=[0.055](mm/hr), END=-1  

1663 *%-----|  

1664 *EXTERNAL FLOWS SOUTHEAST OF THE SITE NORTH OF McKENNA CASEY DR.  

1665 CONTINUOUS NASHYD NHYD=[ "O-13SDF" ], DT=[1]min, AREA=[9.74](ha),  

1666 DWF=[0](cms), CN/C=[81], IA=[4.0](mm), N=[3], TP=[.43]hrs,  

1667 Continuous simulation parameters:  

1668 IaRECper=[4](hrs),  

1669 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),  

1670 InterEventTime=[12](hrs)  

1671 Baseflow simulation parameters:  

1672 BaseFlowOption=[1],  

1673 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)  

1674 VHdyCond=[0.055](mm/hr), END=-1  

1675 *%-----|  

1676 *SNOW DISPOSAL FACILITY  

1677 *PARAMETERS BASED ON ROBINSON 2006 MODEL  

1678 ROUTE RESERVOIR NHYDout=[ "SDF" ], NHYDin=[ "O-13SDF" ], RDT=[1](min),  

1679 TABLE of ( OUTFLOW-STORAGE ) values

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1678          (cms) - (ha-m)
1679          [0.000,0.000]
1680          [0.150,0.600]
1681          (0.200,1.500)
1682          [ -1 , -1 ] (max twenty pts)
1683          NHYDovf=[ "OVFSDF" ]
1684 *%----- | -----
1685 *ANALYSIS POINT 6 - McKenna Casey Dr.
1686 *%----- | -----
1687 ADD HYD      NHYDsum=[ "PT6MC" ], NHYDs to add=[ "DRAIN5"+"D5"+"SDF" ]
1688 *%----- | -----
1689 CONTINUOUS NASHYD NHYD=[ "O-15" ], DT=[1]min, AREA=[10.67](ha),
1690 DWF=[0](cms), CN/C=[82], IA=[7.5](mm), N=[3], TP=[0.30]hrs,
1691 Continuous simulation parameters:
1692 IaRECper=[4](hrs),
1693 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1694 InterEventTime=[12](hrs)
1695 Baseflow simulation parameters:
1696 BaseFlowOption=[1] ,
1697 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1698 VHydCond=[0.055](mm/hr), END=-1
1699 *%----- | -----
1700 *TOTAL FLOW NORTH OF McKENNA CASEY DR.
1701 ADD HYD      NHYDsum=[ "M-C" ], NHYDs to add=[ "PT6MC"+"O-15" ]
1702 *%----- | -----
1703 *ROUTE FLOW THROUGH AREA O-14
1704 * JFSA: Nov. 2020, added end points to close X-section
1705 ROUTE CHANNEL NHYDout=[ "O-14Ch" ], NHYDin=[ "M-C" ], RDT=[1](min),
1706 CHLGTH=[845.3](m), CHSLOPE=[0.10](%), FPSLOPE=[0.10](%),
1707 SECNUM=[1], NSEG=[3]
1708 ( SEGRROUGH, SEGDIST (m) )=[0.06,15.00 -0.033,18.04 0.06,31.85] NSEG
times
1709 ( DISTANCE (m), ELEVATION (m) )=[-0.01, 2.5
1710 (0.00, 1.53]
1711 (5.56, 1.47)
1712 (9.21, 1.45)
1713 (12.45, 1.53)
1714 (13.70, 1.50)
1715 (15.00, 0.69)
1716 (15.34, 0.00)
1717 (16.51, 0.05)
1718 (17.30, 0.17)
1719 (18.04, 0.74)
1720 (19.29, 1.32)
1721 (22.73, 1.47)
1722 (31.84, 1.41)
1723 (31.85, 2.50)
1724 *%----- | -----
1725 *% -Change O-14 from NASHYD to STANDHYD, name it "S-1-Okeefe" and add it to S-1
1726 subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
1727 *% -JFSA 2021-02-16, add detailed subcatchment drainage area for each subcatchment
1728 in Corrigan sub-catchment. After adding part of O-14 to S_1 sub-catchment so O-14
1729 becomes 5 ha instead of 30.02 ha and TP becomes 0.133 (5*0.8/30.02) instead of 0.8
1730 CONTINUOUS NASHYD NHYD=[ "O-14" ], DT=[1]min, AREA=[5](ha),
1731 DWF=[0](cms), CN/C=[82], IA=[7.5](mm), N=[3], TP=[0.133]hrs,
1732 Continuous simulation parameters:
1733 IaRECper=[4](hrs),
1734 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1735 InterEventTime=[12](hrs)
1736 Baseflow simulation parameters:
1737 BaseFlowOption=[1] ,
1738 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1739 VHydCond=[0.055](mm/hr), END=-1
1740 *
1741 *%----- | -----
1742 *ANALYSIS POINT 7 - JOCK RIVER

```

```

* 2020-12-01 To Foster Drain
* 2020-12-01 replace ("PT7JR") by ("OKEEFE")
*%-----|-----|
1743 ADD HYD           NHYDsum=[ "OKEEFE" ], NHYDs to add=[ "O-14Ch"+"O-14" ]
1744 *%-----|-----|
1745 *CONTINUOUS STANDHYD NHYD=[ "OKEEFE" ], DT=[1](min), AREA=[ 448 ](ha),
1746 *
1747 *           XIMP=[ 0.65 ], TIMP=[ 0.65 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
1748 *           SCS curve number CN=[ 77 ],
1749 *           Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%),
1750 *           LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
1751 *           Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%),
1752 *           LGI=[ 1728 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1753 *           Continuous simulation parameters:
1754 *           IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
1755 *           SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1756 *           InterEventTime=[ 18 ](hrs), END=-1
1757 *#*****|-----|
1758 *#     Okeefe Pond
1759 *#     - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1760 *#     and a ratio of the catchment area to the West Clarke pond rating curve
1761 *#     from the MSS for the next coordinates
1762 *#*****|-----|
1763 *ROUTE RESERVOIR   NHYDout=[ "P_OKE" ], NHYDin=[ "OKEEFE" ],
1764 *           RDT=[1](min),
1765 *           TABLE of ( OUTFLOW-STORAGE ) values
1766 *           (cms) - (ha-m)
1767 *           [    0.0 ,  0.0 ]
1768 *           [  14.13 , 13.0 ]
1769 *           [    -1 ,   -1 ] (maximum one hundred pairs of points)
1770 *           NHYDovf=[ "ok-OVF" ],
1771 *%-----|-----|
1772 *     -JFSA 2021-02-25 "S-1-D2" and "S-1-D3" are part of S-1 sub-catchment. They are
1773 *     moved to drain before station 6215 on Jock River
1774 CONTINUOUS STANDHYD NHYD=[ "S-1-D2" ], DT=[1](min), AREA=[ 18.67 ](ha), XIMP=[ 0.65 ],
1775 *           TIMP=[ 0.65 ], DWF=[ 0 ](cms),
1776 *           LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
1777 *           IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%),
1778 *           LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min), Impervious surfaces:
1779 *           IAimp=[ 1.57 ](mm), SLPI=[ 0.75 ](%),
1780 *           LGI=[ 352.798 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1781 *           Continuous simulation parameters:
1782 *           IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
1783 *           SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1784 *           InterEventTime=[ 12 ](hrs), END=-1
1785 *%-----|-----|
1786 *CONTINUOUS NASHYD  NHYD=[ "S-1-D2" ], DT=[1]min, AREA=[ 18.67 ](ha),
1787 *           DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
1788 *           N=[ 3 ], TP=[ 1.120 ]hrs,
1789 *           Continuous simulation parameters:
1790 *           IaRECper=[ 4 ](hrs),
1791 *           SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1792 *           InterEventTime=[ 12 ](hrs)
1793 *           Baseflow simulation parameters:
1794 *           BaseFlowOption=[ 1 ],
1795 *           InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
1796 *           VHydCond=[ 0.055 ](mm/hr), END=-1
1797 *%-----|-----|
1798 *COMPUTE DUALHYD   NHYDin=[ "S-1-D2" ], CINLET=[ 2.062 ](cms), NINLET=[ 1 ],
1799 *           MajNHYD=[ "S-1-D2J" ]
1800 *           MinNHYD=[ "S-1-D2N" ]
1801 *           TMJSTO=[ 99999999 ](cu-m)
1802 *%-----|-----|
1803 *ADD HYD           NHYDsum=[ "S-1-D2S" ], NHYDs to add=[ "S-1-D2J"+"S-1-D2N" ]
1804 *%-----|-----|
1805 *ROUTE RESERVOIR   NHYDout=[ "S-1-D2R" ], NHYDin=[ "S-1-D2S" ],

```

```

1801 * RDT=[1](min),
1802 * TABLE of ( OUTFLOW-STORAGE ) values
1803 * (cms) - (ha-m)
1804 * [ 0.0 , 0.0 ]
1805 * [ 0.2231, 0.7445 ]
1806 * [ -1 , -1 ] (max twenty pts)
1807 * NYHDovf= [ "S-1-D2Rovf" ]
1808 *%-----|-----|
1809 CONTINUOUS STANDHYD NYHD= [ "S-1-D3" ], DT=[1](min), AREA=[ 6.79 ](ha), XIMP=[ 0.65 ],
1810 TIMP=[ 0.65 ], DWF=[ 0 ](cms),
1811 LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
1812 IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%),
1813 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min), Impervious surfaces:
1814 IAimp=[ 1.57 ](mm), SLPI=[ 0.75 ](%),
1815 LGI=[ 212.760 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1816 Continuous simulation parameters:
1817 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
1818 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1819 InterEventTime=[ 12 ](hrs), END=-1
1820 *%-----|-----|
1821 *CONTINUOUS NASHYD NYHD= [ "S-1-D3" ], DT=[ 1 ]min, AREA=[ 6.79 ](ha),
1822 DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
1823 N=[ 3 ], TP=[ 1.281 ]hrs,
1824 Continuous simulation parameters:
1825 IaRECper=[ 4 ](hrs),
1826 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1827 InterEventTime=[ 12 ](hrs)
1828 Baseflow simulation parameters:
1829 BaseFlowOption=[ 1 ],
1830 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
1831 VHdCond=[ 0.055 ](mm/hr), END=-1
1832 *%-----|-----|
1833 *COMPUTE DUALHYD NYHDin= [ "S-1-D3" ], CINLET=[ 0.719 ](cms), NINLET=[ 1 ],
1834 MajNHYD= [ "S-1-D3J" ]
1835 MinNHYD= [ "S-1-D3N" ]
1836 TMJSTO=[ 9999999 ](cu-m)
1837 *%-----|-----|
1838 *ADD HYD NYHDsum= [ "S-1-D3S" ], NYHDs to add= [ "S-1-D3J" + "S-1-D3N" ]
1839 *%-----|-----|
1840 *ROUTE RESERVOIR NYHDout= [ "S-1-D3R" ], NYHDin= [ "S-1-D3S" ],
1841 RDT=[ 1 ](min),
1842 TABLE of ( OUTFLOW-STORAGE ) values
1843 (cms) - (ha-m)
1844 [ 0.0 , 0.0 ]
1845 [ 0.0811, 0.2708 ]
1846 [ -1 , -1 ] (max twenty pts)
1847 NYHDovf= [ "S-1-D3Rovf" ]
1848 *%-----|-----|
1849 ADD HYD NYHDsum= [ "SN_OK" ], NYHDs to add= [ "N_OK" + "OKEEFE" + "S-1-D2" + "S-1-D3" ]
1850 *%-----|-----|
1851 SAVE HYD NYHD= [ "SN_OK" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
1852 HYD_COMMENT= [ "Total Flows at Okeefe Drain" ]
1853 *# Hydrograph from Node Okeefe routed to Node at Foster Drain
1854 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
1855 *#
1856 ROUTE CHANNEL NYHDout= [ "N_FO" ], NYHDin= [ "SN_OK" ],
1857 RDT=[ 1 ](min),
1858 CHLGTH=[ 1183 ](m), CHSLOPE=[ 0.0761 ](%),
1859 FPSLOPE=[ 0.0761 ](%),
1860 SECNUM=[ 1.0 ], NSEG=[ 3 ]
1861 ( SEGROUGH, SEGDIST (m) )=
1862 [ 0.050, -33.89
1863 -0.035, 31.59
0.050, 34.41 ] NSEG times

```

```

1864 ( DISTANCE (m) , ELEVATION (m))=
1865 [-794.18, 91.00]
1866 [-775.41, 91.50]
1867 [-702.63, 91.50]
1868 [-546.19, 91.50]
1869 [-529.54, 91.50]
1870 [-323.44, 91.00]
1871 [-320.71, 91.00]
1872 [-183.59, 91.00]
1873 [-182.54, 90.50]
1874 [-181.36, 90.00]
1875 [-177.37, 90.00]
1876 [-87.70, 90.00]
1877 [-33.89, 90.00]
1878 [-18.52, 86.88]
1879 [0.00, 85.20]
1880 [16.20, 86.83]
1881 [31.59, 90.00]
1882 [33.03, 90.50]
1883 [34.41, 91.00]
1884 *%-----|-----|
1885 *#*****
1886 *# Catchment FOSTER
1887 *# - To Foster ditch (north of the Jock)
1888 *# - Partially developed (medium density); remaining agricultural
1889 *# - 2020-12-01 JFSA Foster area is 332 as per Foster SWMF Environmental Study
Report, CH2MHILL, Aug 2013.
1890 *# - 2020-12-01 decrease Foster drainage area from (373 HA) to (307.98 HA) after
increasing Okeefe drainage area to (513.02 HA) so the total drainage area remains the
same
1891 *# - 2021-02-12 update Foster area to 325.44 ha as measured from QGIS
1892 *#*****
1893 CONTINUOUS STANDHYD NHYD=[ "FOSTER" ], DT=[1]min, AREA=[ 325.44](ha),
1894 XIMP=[ 0.55 ], TIMP=[ 0.55 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
1895 SCS curve number CN=[ 74 ],
1896 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%),
1897 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
1898 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%),
1899 LGI=[ 1472.956 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1900 Continuous simulation parameters:
1901 IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
1902 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1903 InterEventTime=[ 18 ](hrs), END=-1
1904 *#*****
1905 *# Foster Pond
1906 *# - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1907 *# and a ratio of the catchment area to the West Clarke pond rating curve
1908 *# from the MSS for the next coordinates
1909 *#*****
1910 ROUTE RESERVOIR NHYDout=[ "P_FOS" ], NHYDin=[ "FOSTER" ],
1911 RDT=[ 1 ](min),
1912 TABLE of ( OUTFLOW-STORAGE ) values
1913 (cms) - (ha-m)
1914 [ 0.0 , 0.0 ]
1915 [ 10.34 , 10 ]
1916 [ -1 , -1 ] (max twenty pts)
1917 NHYDovf=[ "FO-OVF" ]
1918 *%-----|-----|
1919 ADD HYD NHYDsum=[ "FOSTER-OUT" ], NHYDs to add=[ "P_FOS "+"FO-OVF" ]
1920 *%-----|-----|
1921 *#*****
1922 * -Brazeau area from P 1800-19 =[ 71.751 ], change to 63.59 ha based on GIS measurements
1923 * -JFSA, 2021-01-19 update "W_CLAR_BRAZ" to 73.29 ha based on GIS measurements
1924 * -JFSA, 2021-01-22 Brazeau ("MS_P10"+"P10-OVF")brazeau pond discharges directly
to the jock river through a road side ditch on the west side of Borrisokane road
(station 6016)

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```

1925 CONTINUOUS STANDHYD NHYD= [ "W_CLAR_BRAZ" ], DT=[1]min, AREA=[ 73.29 ](ha),
1926 XIMP=[ 0.6 ], TIMP=[ 0.65 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
1927 SCS curve number CN=[ 77 ],
1928 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
1929 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
1930 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%),
1931 LGI=[ 699.00 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1932 Continuous simulation parameters:
1933 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
1934 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1935 InterEventTime=[ 18 ](hrs), END=-1
1936 *%-----|-----|
1937 * 2020-12-01 correct pond curve values
1938 ROUTE RESERVOIR NHYDout=[ "MS_P10" ], NHYDin=[ "W_CLAR_BRAZ" ],
1939 RDT=[ 1 ](min),
1940 TABLE of ( OUTFLOW-STORAGE ) values
1941 (cms) - (ha-m)
1942 [ 0.0 , 0.0 ]
1943 [ 0.068 , 0.001 ]
1944 [ 0.271 , 0.022 ]
1945 [ 0.379 , 0.051 ]
1946 [ 0.48 , 0.091 ]
1947 [ 0.853 , 0.341 ]
1948 [ 1.005 , 0.61 ]
1949 [ 1.128 , 1.231 ]
1950 [ 1.155 , 1.592 ]
1951 [ 1.194 , 1.876 ]
1952 [ 1.2 , 1.921 ]
1953 [ 1.259 , 2.369 ]
1954 [ 1.3 , 2.665 ]
1955 [ 1.349 , 2.813 ]
1956 [ -1 , -1 ] (max twenty pts)
1957 NHYDovf=[ "P10-OVF" ]
1958 *%-----|-----|
1959 * -JFSA 2021-02-26 "S-1-FO-D2" is a part of S-1 sub-catchment. It is moved to drain
before station 980 on Foster Drain
1960 CONTINUOUS STANDHYD NHYD=[ "S-1-FO-D2" ], DT=[1]min, AREA=[ 4.94 ](ha),
1961 XIMP=[ 0.55 ], TIMP=[ 0.55 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
1962 SCS curve number CN=[ 74 ],
1963 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%),
1964 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
1965 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%),
1966 LGI=[ 181.475 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1967 Continuous simulation parameters:
1968 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
1969 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1970 InterEventTime=[ 18 ](hrs), END=-1
1971 *%-----|-----|
1972 *CONTINUOUS NASHYD NHYD=[ "S-1-FO-D2" ], DT=[1]min, AREA=[ 4.94 ](ha),
1973 * DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
1974 * N=[ 3 ], TP=[ 1.10 ]hrs,
1975 * Continuous simulation parameters:
1976 * IaRECper=[ 4 ](hrs),
1977 * SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1978 * InterEventTime=[ 12 ](hrs)
1979 * Baseflow simulation parameters:
1980 * BaseFlowOption=[ 1 ],
1981 * InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
1982 * VHdCond=[ 0.055 ](mm/hr), END=-1
1983 *%-----|-----|
1984 *COMPUTE DUALHYD NHYDin=[ "S-1-FO-D2" ], CINLET=[ 0.508 ](cms), NINLET=[ 1 ],
1985 * MajNHYD=[ "S-1-FO-D2J" ]
1986 * MinNHYD=[ "S-1-FO-D2N" ]
1987 * TMJSTO=[ 9999999 ](cu-m)
1988 *%-----|-----|
1989 *ADD HYD NHYDsum=[ "S-1-FO-D2S" ], NHYDs to add=[ "S-1-FO-D2J" + "S-1-FO-D2N" ]

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1990 *%-----|-----|
1991 *ROUTE RESERVOIR      NHYDout=[ "S-1-FO-D2R" ] , NHYDin=[ "S-1-FO-D2S" ] ,
1992 *          RDT=[1](min),
1993 *          TABLE of ( OUTFLOW-STORAGE ) values
1994 *          (cms) - (ha-m)
1995 *          [ 0.0      , 0.0   ]
1996 *          [ 0.0590 , 0.1970 ]
1997 *          [    -1   ,   -1    ] (max twenty pts)
1998 *          NHYDovf=[ "S-1FOD2ovf" ]
1999 *%-----|-----|
2000 ADD HYD      NHYDsum=[ "980" ], NHYDs to add=[ "FOSTER-OUT"+"S-1-FO-D2" ]
2001 *%-----|-----|
2002 SAVE HYD      NHYD=[ "980" ], # OF PCYCLES=[-1], ICASEsh=[1]
2003          HYD_COMMENT=[ "Total Flows at Station 980 on Foster Drain" ]
2004 *%-----|-----|
2005 *#
2006 *# Hydrograph from Node Foster SWM (Station 980)to Node at station 520
2007 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 980
2008 *#
2009 ROUTE CHANNEL      NHYDout=[ "980-out" ] , NHYDin=[ "980" ] ,
2010          RDT=[1](min),
2011          CHLGTH=[460](m), CHSLOPE=[0.04348](%), FPSLOPE=[0.04348](%),
2012          SECNUM=[1.0], NSEG=[3]
2013          ( SEGROUGH, SEGDIST (m))=
2014          [0.050,45.90
2015          -0.035,53.30
2016          0.050,100] NSEG times
2017          ( DISTANCE (m), ELEVATION (m))=
2018          [0, 91.75 ]
2019          [42.4, 92.18 ]
2020          [43.5, 92.16 ]
2021          [44.1, 92.1 ]
2022          [44.6, 92 ]
2023          [44.8, 91.86 ]
2024          [45.9, 91.04 ]
2025          [46.4, 90.65 ]
2026          [46.8, 90.36 ]
2027          [47.9, 90.32 ]
2028          [48.7, 90.35 ]
2029          [50.7, 90.33 ]
2030          [52.2, 90.38 ]
2031          [52.5, 90.59 ]
2032          [53.3, 91.28 ]
2033          [54, 91.83 ]
2034          [54.3, 92 ]
2035          [54.8, 92.08 ]
2036          [55.4, 92.12 ]
2037          [100, 91.84 ]
2038
2039 *%-----|-----|
2040 * -JFSA 2021-02-26 "S-1-FO-D1" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2041 CONTINUOUS STANDHYD NHYD=[ "S-1-FO-D1" ], DT=[1]min, AREA=[5.11](ha),
2042          XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2043          SCS curve number CN=[74],
2044          Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2045          LGP=[40](m), MNP=[0.25], SCP=[0](min),
2046          Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2047          LGI=[184.572](m), MNI=[0.013], SCI=[0](min),
2048          Continuous simulation parameters:
2049          IaRECper=[4](hrs), IaRECImp=[4](hrs),
2050          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2051          InterEventTime=[18](hrs), END=-1
2052 *%-----|-----|
2053 *COMPUTE DUALHYD      NHYDin=[ "S-1-FO-D1" ], CINLET=[0.605](cms), NINLET=[1],
2054          MajNHYD=[ "S-1-FO-D1J" ]

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```

2055 * MinNHYD= [ "S-1-FO-D1N" ]
2056 *
2057 *-----| TMJSTO=[ 9999999 ](cu-m)
2058 *ADD HYD NHYDsum= [ "S-1-FO-D1S" ], NHYDs to add= [ "S-1-FO-D1N"+"S-1-FO-D1J" ]
2059 *-----|
2060 *ROUTE RESERVOIR NHYDout= [ "S-1-FO-D1R" ] , NHYDin= [ "S-1-FO-D1S" ] ,
2061 * RDT=[1](min),
2062 * TABLE of ( OUTFLOW-STORAGE ) values
2063 * (cms) - (ha-m)
2064 * [ 0.0 , 0.0 ]
2065 * [ 0.0611, 0.2038 ]
2066 * [ -1 , -1 ] (max twenty pts)
2067 * NHYDovf= [ "S-1FOD1ovf" ]
2068 *-----|
2069 ADD HYD NHYDsum= [ "520" ], NHYDs to add= [ "980-out"+"S-1-FO-D1" ]
2070 *-----|
2071 SAVE HYD NHYD= [ "520" ], # OF PCYCLES=[-1], ICASEsh=[1]
2072 HYD_COMMENT= [ "Total Flows at Sation 520 on Foster Drain" ]
2073 *-----|
2074 *# Hydrograph from Node at Station 520 (Foster Drain) to Node at station 6016 (Jock
River)
2075 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 520
2076 *#
2077 ROUTE CHANNEL NHYDout= [ "520-out" ] , NHYDin= [ "520" ] ,
2078 RDT=[1](min),
2079 CHLGTH=[860](m), CHSLOPE=[ 0.5872 ](%),
2080 FPSLOPE=[ 0.5872 ](%),
2081 SECNUM=[ 1.0 ], NSEG=[ 3 ]
2082 ( SEGROUGH, SEGDIST (m))=
2083 [ 0.050, 45.90
2084 -0.035, 54.3
2085 0.050, 100.1097 ] NSEG times
2086 ( DISTANCE (m), ELEVATION (m))=
2087 [ 0, 91.26 ]
2088 [ 44.9, 91.46 ]
2089 [ 45.1, 91.37 ]
2090 [ 45.9, 90.84 ]
2091 [ 47, 90.32 ]
2092 [ 47.5, 90.22 ]
2093 [ 48, 90.17 ]
2094 [ 50.7, 90.19 ]
2095 [ 51.5, 90.17 ]
2096 [ 52.2, 90.13 ]
2097 [ 52.7, 90.12 ]
2098 [ 53.3, 90.14 ]
2099 [ 53.5, 90.31 ]
2100 [ 53.9, 90.59 ]
2101 [ 54.3, 90.87 ]
2102 [ 54.7, 91.04 ]
2103 [ 55.3, 91.24 ]
2104 [ 55.5, 91.26 ]
2105 [ 63.7, 91.37 ]
2106 [ 100.1097, 91.43 ]
2107 *-----|
2108 * -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2109 CONTINUOUS STANDHYD NHYD= [ "S-1-FO-F-D" ], DT=[1]min, AREA=[14.96](ha),
2110 XIMP=[ 0.65 ], TIMP=[ 0.65 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
2111 SCS curve number CN=[ 74 ],
2112 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%),
2113 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
2114 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%),
2115 LGI=[ 315.806 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
2116 Continuous simulation parameters:
2117 IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
2118 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),

```

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2119           InterEventTime=[18](hrs),      END=-1
2120 *%-----|-----|
2121 *CONTINUOUS NASHYD  NHYD=[ "S-1-FO-F-D" ], DT=[1]min, AREA=[14.96](ha),
2122 *
2123 *
2124 *          DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2125 *          N=[3], TP=[1.007]hrs,
2126 *          Continuous simulation parameters:
2127 *          IaRECper=[4](hrs),
2128 *          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2129 *          InterEventTime=[12](hrs)
2130 *          Baseflow simulation parameters:
2131 *          BaseFlowOption=[1],
2132 *          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2133 *          VHydCond=[0.055](mm/hr), END=-1
2134 *%-----|-----|
2135 *COMPUTE DUALHYD  NHYDin=[ "S-1-FO-F-D" ], CINLET=[1.749](cms), NINLET=[1],
2136 *          MajNHYD=[ "S-1FO-F-DJ" ]
2137 *          MinNHYD=[ "S-1FO-F-DN" ]
2138 *          TMJSTO=[ 9999999 ](cu-m)
2139 *%-----|-----|
2140 *ADD HYD          NHYDsum=[ "S-1FO-F-DS" ], NHYDs to add=[ "S-1FO-F-DJ"+"S-1FO-F-DN" ]
2141 *%-----|-----|
2142 *ROUTE RESERVOIR NHYDout=[ "S-1FO-F-DR" ], NHYDin=[ "S-1FO-F-DS" ],
2143 *          RDT=[1](min),
2144 *          TABLE of ( OUTFLOW-STORAGE ) values
2145 *          (cms) - (ha-m)
2146 *          [ 0.0 , 0.0 ]
2147 *          [ 0.1788, 0.5966 ]
2148 *          [ -1 , -1 ] (max twenty pts)
2149 *          NHYDovf=[ "S-1FoFDovf" ]
2150 * -JFSA 2021-02-26 "S-1-D8" is a part of S-1 sub-catchment. It is moved to drain
2151 * before station 6016 on Jock River
2152 *CONTINUOUS STANDHYD NHYD=[ "S-1-D8" ], DT=[1]min, AREA=[5.27](ha), XIMP=[0.325],
2153 *TIMP=[0.65], DWF=[0](cms), LOSS=[1]:
2154 *          Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
2155 *          F=[0.00](mm),
2156 *          Previous areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
2157 *          MNP=[0.250], SCP=[0](min),
2158 *          Impervious areas: IAimp=[0.785](mm), SLPI=[0.75](%),
2159 *          LGI=[187.439](m), MNI=[0.013], SCI=[0](min),
2160 *          Continuous simulation parameters:
2161 *          IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
2162 *          END=-1
2163 *%-----|-----|
2164 *CONTINUOUS NASHYD  NHYD=[ "S-1-D8" ], DT=[1]min, AREA=[5.27](ha),
2165 *          DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2166 *          N=[3], TP=[1.10]hrs,
2167 *          Continuous simulation parameters:
2168 *          IaRECper=[4](hrs),
2169 *          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2170 *          InterEventTime=[12](hrs)
2171 *          Baseflow simulation parameters:
2172 *          BaseFlowOption=[1],
2173 *          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2174 *          VHydCond=[0.055](mm/hr), END=-1
2175 *%-----|-----|
2176 *COMPUTE DUALHYD  NHYDin=[ "S-1-D8" ], CINLET=[2.279](cms), NINLET=[1],
2177 *          MajNHYD=[ "S-1-D8J" ]
2178 *          MinNHYD=[ "S-1-D8N" ]
2179 *          TMJSTO=[ 9999999 ](cu-m)
2180 *%-----|-----|
2181 *ADD HYD          NHYDsum=[ "S-1-D8S" ], NHYDs to add=[ "S-1-D8J"+"S-1-D8N" ]
2182 *%-----|-----|
2183 *ADD HYD          NHYDsum=[ "S-1-D" ], NHYDs to add=[ "S-1-Okeefe"+"S-1"+"S-1-Fost" ]
2184 *%-----|-----|
2185 *COMPUTE DUALHYD  NHYDin=[ "S-1-D" ], CINLET=[11.616](cms), NINLET=[1],

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2179 * MajNHYD=[ "S-1-D-MJ" ]
2180 * MinNHYD=[ "S-1-D-MN" ]
2181 * TMJSTO=[ 5974 ](cu-m)
2182 *%-----|-----|
2183 *ADD HYD NHYDsum=[ "S-1-DEV" ], NHYDs to add=[ "S-1-D-MJ" +"S-1-D-MN" ]
2184 *%-----|-----|
2185 *ROUTE RESERVOIR NHYDout=[ "S-1-D8R" ] , NHYDin=[ "S-1-D8S" ] ,
2186 * RDT=[1](min),
2187 * TABLE of ( OUTFLOW-STORAGE ) values
2188 * (cms) - (ha-m)
2189 * [ 0.0 , 0.0 ]
2190 * [ 0.0630, 0.2102 ]
2191 * [ -1 , -1 ] (max twenty pts)
2192 * NHYDovf=[ "S-1-D8Rovf" ]
2193 *%-----|-----|
2194 * -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2195 CONTINUOUS NASHYD NHYD=[ "S-1-A" ], DT=[1]min, AREA=[ 75.88 ](ha),
2196 DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
2197 N=[ 3 ], TP=[ 0.619 ]hrs,
2198 Continuous simulation parameters:
2199 IaRECper=[ 4 ](hrs),
2200 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2201 InterEventTime=[ 12 ](hrs)
2202 Baseflow simulation parameters:
2203 BaseFlowOption=[ 1 ],
2204 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2205 VHydCond=[ 0.055 ](mm/hr), END=-1
2206 *%-----|-----|
2207 * -JFSA, 2021-01-22 "W_CLAR_UNDE" (west of Clarke sub-catchment) discharges
directly to the jock river through a road side ditch on the west side of Borrisokane
road (station 6016)
2208 CONTINUOUS NASHYD NHYD=[ "W_CLAR_UNDE" ], DT=[1]min, AREA=[ 35.65 ](ha),
2209 DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
2210 N=[ 3 ], TP=[ 1.10 ]hrs,
2211 Continuous simulation parameters:
2212 IaRECper=[ 4 ](hrs),
2213 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2214 InterEventTime=[ 12 ](hrs)
2215 Baseflow simulation parameters:
2216 BaseFlowOption=[ 1 ],
2217 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2218 VHydCond=[ 0.055 ](mm/hr), END=-1
2219 *%-----|-----|
2220 ADD HYD NHYDsum=[ "SN_FO" ], NHYDs to
add=[ "N_FO" +"520-out" +"MS_P10" +"P10-OVF" +"W_CLAR_UNDE" +"S-1-FO-F-D" +"S-1-D8" +"S-1-A" ]
2221 *%-----|-----|
2222 SAVE HYD NHYD=[ "SN_FO" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
2223 HYD_COMMENT=[ "Total Flows at Foster Drain" ]
2224 *%-----|-----|
2225 *# Hydrograph from Node Foster routed to Node at Cedarview Road
2226 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6016
2227 *#
2228 ROUTE CHANNEL NHYDout=[ "N_CE" ] , NHYDin=[ "SN_FO" ] ,
2229 RDT=[ 1 ](min),
2230 CHLGH= [ 159 ](m), CHSLOPE=[ 0.0818 ](%),
2231 FPSLOPE=[ 0.0818 ](%),
2232 SECNUM=[ 1.0 ], NSEG=[ 3 ]
2233 ( SEGROUGH, SEGDIST (m))=
2234 [ 0.050,-15.46
2235 -0.035,26.55
2236 0.050,116.76 ] NSEG times
2237 ( DISTANCE (m), ELEVATION (m))=
2238 [ -645.23, 91.50 ]
2239 [ -391.20, 91.50 ]
2240 [ -91.00, 91.50 ]

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2241 [-85.52, 91.50]
2242 [-15.46, 89.40]
2243 [-9.79, 89.31]
2244 [-3.22, 86.24]
2245 [3.22, 85.07]
2246 [10.96, 85.79]
2247 [16.44, 86.49]
2248 [26.55, 89.45]
2249 [29.03, 90.27]
2250 [35.76, 90.67]
2251 [36.67, 91.00]
2252 [108.08, 91.00]
2253 [109.82, 90.50]
2254 [112.04, 90.50]
2255 [114.62, 91.00]
2256 [116.76, 91.50]
2257 *%-----|-----|
2258 *#*****
2259 *# Catchment S-1
2260 *# - To Jock River (north and south of Jock)
2261 *# - Primarily agricultural fields; portion of sand quarry
2262 *%-----|-----|
2263 *% -2020-12-17 "S-1-Undeveloped" and "S-1-Fost" was a part of Foster drain, they are below
the foster pond. Now they are added to S-1 subcatchment based on Project 1474-BCDC,
JFSA, Nov. 2020
2264 *% -2020-12-17 Change O-14 (it was part of Okeefe drain) to "S-1-Okeefe" and add it
to S-1 subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
2265 *% -2020-12-17 Add "S-1-BCDC" as NASHYD
2266 *% -2020-12-17 all other S-1 subcatchment as STANDHYD with DUALHYD and ROUTE RESERVOIR
2267 *%-----|-----|
2268 *#*****
2269 * -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2270 *CONTINUOUS NASHYD NYHD=[ "S-1-A" ], DT=[1]min, AREA=[ 75.88 ](ha),
2271 * DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
2272 * N=[ 3 ], TP=[ 0.619 ]hrs,
2273 * Continuous simulation parameters:
2274 * IaRECper=[ 4 ](hrs),
2275 * SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2276 * InterEventTime=[ 12 ](hrs)
2277 * Baseflow simulation parameters:
2278 * BaseFlowOption=[ 1 ],
2279 * InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2280 * VHdCond=[ 0.055 ](mm/hr), END=-1
2281 *%-----|-----|
2282 CONTINUOUS NASHYD NYHD=[ "S-1-B" ], DT=[1]min, AREA=[ 55.36 ](ha),
2283 DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
2284 N=[ 3 ], TP=[ 0.451 ]hrs,
2285 Continuous simulation parameters:
2286 IaRECper=[ 4 ](hrs),
2287 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2288 InterEventTime=[ 12 ](hrs)
2289 Baseflow simulation parameters:
2290 BaseFlowOption=[ 1 ],
2291 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2292 VHdCond=[ 0.055 ](mm/hr), END=-1
2293 *%-----|-----|
2294 *# - JFSA 2021-02-24 change the name from S-1-BCDC to S-1-A and S-1-B. Change their
TP values based on the new areas compared to the old ones.
2295 *CONTINUOUS NASHYD NYHD=[ "S-1-BCDC" ], DT=[1]min, AREA=[ 134.9 ](ha),
2296 * DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
2297 * N=[ 3 ], TP=[ 1.10 ]hrs,
2298 * Continuous simulation parameters:
2299 * IaRECper=[ 4 ](hrs),
2300 * SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2301 * InterEventTime=[ 12 ](hrs)

```

```

2302 *
2303 * Baseflow simulation parameters:
2304 * BaseFlowOption=[1] ,
2305 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2306 * VHydCond=[0.055](mm/hr), END=-1
2307 *%-----|-----|
2308 *# - JFSA 2021-02-24 "S-1-BCDC-1" and "S-1-BCDC-2" are not existing anymore.
2309 *S-1-BCDC-1" is part of "S-1-FO-D2" and "S-1-BCDC-2" is part of "S-1-D2" and "S-1-D3"
2310 *CONTINUOUS NASHYD NHYD=[ "S-1-BCDC-1"], DT=[1]min, AREA=[0.3](ha),
2311 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2312 * N=[3], TP=[1.10]hrs,
2313 * Continuous simulation parameters:
2314 * IaRECper=[4](hrs),
2315 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2316 * InterEventTime=[12](hrs)
2317 * Baseflow simulation parameters:
2318 * BaseFlowOption=[1] ,
2319 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2320 * VHydCond=[0.055](mm/hr), END=-1
2321 *%-----|-----|
2322 *CONTINUOUS NASHYD NHYD=[ "S-1-BCDC-2"], DT=[1]min, AREA=[1.3](ha),
2323 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2324 * N=[3], TP=[1.10]hrs,
2325 * Continuous simulation parameters:
2326 * IaRECper=[4](hrs),
2327 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2328 * InterEventTime=[12](hrs)
2329 * Baseflow simulation parameters:
2330 * BaseFlowOption=[1] ,
2331 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2332 * VHydCond=[0.055](mm/hr), END=-1
2333 *%-----|-----|
2334 *# - JFSA 2021-01-19, after adding Greenbank pond, "S-1-BCDC-3" is not existing
2335 anymore
2336 *CONTINUOUS NASHYD NHYD=[ "S-1-BCDC-3"], DT=[1]min, AREA=[3.9](ha),
2337 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2338 * N=[3], TP=[1.10]hrs,
2339 * Continuous simulation parameters:
2340 * IaRECper=[4](hrs),
2341 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2342 * InterEventTime=[12](hrs)
2343 * Baseflow simulation parameters:
2344 * BaseFlowOption=[1] ,
2345 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2346 * VHydCond=[0.055](mm/hr), END=-1
2347 *%-----|-----|
2348 * -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
2349 before station 7245 on Jock River
2350 *CONTINUOUS STANDHYD NHYD=[ "S-1-Okeefe"], DT=[1](min), AREA=[44.93](ha), XIMP=[0.65],
2351 * TIMP=[0.65], DWF=[0](cms),
2352 * LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
2353 * IApert=[4.67](mm), SLPP=[2.0](%), LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
2354 * IAimp=[1.57](mm), SLPI=[0.75](%), LGI=[547.296](m), MNI=[0.013], SCI=[0](min),
2355 * Continuous simulation parameters:
2356 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
2357 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2358 * InterEventTime=[12](hrs), END=-1
2359 *%-----|-----|
2360 *COMPUTE DUALHYD NHYDin=[ "S-1-Okeefe"], CINLET=[ 4.796](cms), NINLET=[1],
2361 * MajNHYD=[ "S-1-OkMJ"]
2362 * MinNHYD=[ "S-1-OkMN"]
2363 * TMJSTO=[ 9999999](cu-m)
2364 *%-----|-----|
2365 *ADD HYD NHYDsum=[ "S-1-OkS"], NHYDs to add=[ "S-1-OkMJ" + "S-1-OkMN"]
2366 *%-----|-----|

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2362 *ROUTE RESERVOIR      NHYDout=[ "S-1-OkSR" ] , NHYDin=[ "S-1-OkS" ] ,
2363 *
2364 *                                RDT=[1](min),
2365 *                                TABLE of ( OUTFLOW-STORAGE ) values
2366 *                                         (cms) - (ha-m)
2367 *                                         [ 0.0      , 0.0   ]
2368 *                                         [ 0.5370 , 1.7917 ]
2369 *                                         [     -1  ,    -1    ] (max twenty pts)
2370 *                                NHYDovf=[ "S-1-OkSovf" ]
2371 *%-----|-----|
2372 *CONTINUOUS NASHYD      NHYD=[ "S-1-Okeeefe" ], DT=[1]min, AREA=[44.93](ha),
2373 *                                DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2374 *                                N=[3], TP=[1.049]hrs,
2375 *                                Continuous simulation parameters:
2376 *                                IaRECper=[4](hrs),
2377 *                                SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2378 *                                InterEventTime=[12](hrs)
2379 *                                Baseflow simulation parameters:
2380 *                                BaseFlowOption=[1],
2381 *                                InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2382 *                                VHydCond=[0.055](mm/hr), END=-1
2383 *%-----|-----|
2384 *      -JFSA 2021-02-26 "S-1-FO-D1" is a part of S-1 sub-catchment. It is moved to drain
2385 before station 520 on Foster Drain
2386 *CONTINUOUS STANDHYD NHYD=[ "S-1-FO-D1" ], DT=[1]min, AREA=[5.11](ha),
2387 *                                XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2388 *                                SCS curve number CN=[74],
2389 *                                Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2390 *                                LGP=[40](m), MNP=[0.25], SCP=[0](min),
2391 *                                Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2392 *                                LGI=[184.572](m), MNI=[0.013], SCI=[0](min),
2393 *                                Continuous simulation parameters:
2394 *                                IaRECper=[4](hrs), IaRECimp=[4](hrs),
2395 *                                SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2396 *                                InterEventTime=[18](hrs), END=-1
2397 *%-----|-----|
2398 *COMPUTE DUALHYD      NHYDin=[ "S-1-FO-D1" ], CINLET=[ 0.605](cms), NINLET=[1],
2399 *                                MajNHYD=[ "S-1-FO-D1J" ]
2400 *                                MinNHYD=[ "S-1-FO-D1N" ]
2401 *                                TMJSTO=[ 99999999 ](cu-m)
2402 *%-----|-----|
2403 *ADD HYD               NHYDsum=[ "S-1-FO-D1S" ], NHYDs to add=[ "S-1-FO-D1N"+"S-1-FO-D1J" ]
2404 *%-----|-----|
2405 *ROUTE RESERVOIR      NHYDout=[ "S-1-FO-D1R" ] , NHYDin=[ "S-1-FO-D1S" ],
2406 *                                RDT=[1](min),
2407 *                                TABLE of ( OUTFLOW-STORAGE ) values
2408 *                                         (cms) - (ha-m)
2409 *                                         [ 0.0      , 0.0   ]
2410 *                                         [ 0.0611 , 0.2038 ]
2411 *                                         [     -1  ,    -1    ] (max twenty pts)
2412 *                                NHYDovf=[ "S-1FOD1ovf" ]
2413 *%-----|-----|
2414 *CONTINUOUS NASHYD      NHYD=[ "S-1-FO-D1" ], DT=[1]min, AREA=[5.11](ha),
2415 *                                DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2416 *                                N=[3], TP=[1.10]hrs,
2417 *                                Continuous simulation parameters:
2418 *                                IaRECper=[4](hrs),
2419 *                                SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2420 *                                InterEventTime=[12](hrs)
2421 *                                Baseflow simulation parameters:
2422 *                                BaseFlowOption=[1],
2423 *                                InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2424 *                                VHydCond=[0.055](mm/hr), END=-1
2425 *%-----|-----|
2426 *      -JFSA 2021-02-26 "S-1-FO-D2" is a part of S-1 sub-catchment. It is moved to drain
2427 before station 980 on Foster Drain
2428 *CONTINUOUS STANDHYD NHYD=[ "S-1-FO-D2" ], DT=[1]min, AREA=[4.94](ha),

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2426 *
2427 *
2428 *
2429 *
2430 *
2431 *
2432 *
2433 *
2434 *
2435 *
2436 *%-----| -----
2437 *CONTINUOUS NASHYD   NHYD=[ "S-1-FO-D2" ], DT=[1]min, AREA=[ 4.94 ](ha),
2438 *          DWF=[0](cms), CN/C=[77], IA=[ 4.67 ](mm),
2439 *          N=[ 3 ], TP=[1.10]hrs,
2440 *          Continuous simulation parameters:
2441 *          IaRECper=[4](hrs), IaRECimp=[4](hrs),
2442 *          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2443 *          InterEventTime=[18](hrs), END=-1
2444 *%-----| -----
2445 *COMPUTE DUALHYD    NHYDin=[ "S-1-FO-D2" ], CINLET=[ 0.508 ](cms), NINLET=[1],
2446 *          MajNHYD=[ "S-1-FO-D2J" ]
2447 *          MinNHYD=[ "S-1-FO-D2N" ]
2448 *          TMJSTO=[ 9999999 ](cu-m)
2449 *%-----| -----
2450 *ADD HYD             NHYDsum=[ "S-1-FO-D2S" ], NHYDs to add=[ "S-1-FO-D2J"+"S-1-FO-D2N" ]
2451 *%-----| -----
2452 *ROUTE RESERVOIR   NHYDout=[ "S-1-FO-D2R" ] ,NHYDin=[ "S-1-FO-D2S" ],
2453 *          RDT=[1](min),
2454 *          TABLE of ( OUTFLOW-STORAGE ) values
2455 *          (cms) - (ha-m)
2456 *          [ 0.0      , 0.0      ]
2457 *          [ 0.0590  , 0.1970  ]
2458 *          [     -1  ,     -1  ] (max twenty pts)
2459 *          NHYDovf=[ "S-1FOD2ovf" ]
2460 *%-----| -----
2461 *      -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
2462 before station 6016 on Jock River
2463 *CONTINUOUS STANDHYD NHYD=[ "S-1-FO-F-D" ], DT=[1]min, AREA=[14.96](ha),
2464 *          XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2465 *          SCS curve number CN=[74],
2466 *          Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2467 *          LGP=[40](m), MNP=[0.25], SCP=[0](min),
2468 *          Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2469 *          LGI=[315.806](m), MNI=[0.013], SCI=[0](min),
2470 *          Continuous simulation parameters:
2471 *          IaRECper=[4](hrs), IaRECimp=[4](hrs),
2472 *          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2473 *          InterEventTime=[18](hrs), END=-1
2474 *%-----| -----
2475 *CONTINUOUS NASHYD   NHYD=[ "S-1-FO-F-D" ], DT=[1]min, AREA=[14.96](ha),
2476 *          DWF=[0](cms), CN/C=[77], IA=[ 4.67 ](mm),
2477 *          N=[ 3 ], TP=[1.007]hrs,
2478 *          Continuous simulation parameters:
2479 *          IaRECper=[4](hrs),
2480 *          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2481 *          InterEventTime=[12](hrs)
2482 *          Baseflow simulation parameters:
2483 *          BaseFlowOption=[1],
2484 *          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2485 *          VHydCond=[0.055](mm/hr), END=-1
2486 *%-----| -----
2487 *COMPUTE DUALHYD    NHYDin=[ "S-1-FO-F-D" ], CINLET=[1.749](cms), NINLET=[1],

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2491 *
2492 * MajNHYD=[ "S-1FO-F-DJ" ]
2493 * MinNHYD=[ "S-1FO-F-DN" ]
2494 * TMJSTO=[ 99999999 ](cu-m)
2495 *%-----|-----|-----|-----|-----|-----|-----|-----|
2495 *ADD HYD NHYDsum=[ "S-1FO-F-DS" ], NHYDs to add=[ "S-1FO-F-DJ"+"S-1FO-F-DN" ]
2496 *%-----|-----|-----|-----|-----|-----|-----|-----|
2497 *ROUTE RESERVOIR NHYDout=[ "S-1FO-F-DR" ] , NHYDin=[ "S-1FO-F-DS" ] ,
2498 * RDT=[1](min),
2499 * TABLE of ( OUTFLOW-STORAGE ) values
2500 * (cms) - (ha-m)
2501 * [ 0.0 , 0.0 ]
2502 * [ 0.1788, 0.5966 ]
2503 * [ -1 , -1 ] (max twenty pts)
2504 * NHYDovf=[ "S-1FOFDovf" ]
2505 *%-----|-----|-----|-----|-----|-----|-----|-----|
2506 *CONTINUOUS STANDHYD NHYD=[ "S-1-D1" ], DT=[1](min), AREA=[21.67](ha), XIMP=[0.65],
2506 * TIMP=[0.65], DWF=[0](cms),
2507 * LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
2507 * IAper=[4.67](mm), SLPP=[2.0](%),
2508 * LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
2508 * IAimp=[1.57](mm), SLPI=[0.75](%),
2509 * LGI=[380.088](m), MNI=[0.013], SCI=[0](min),
2510 * Continuous simulation parameters:
2511 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
2512 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2513 * InterEventTime=[12](hrs), END=-1
2514 *%-----|-----|-----|-----|-----|-----|-----|-----|
2515 *CONTINUOUS NASHYD NHYD=[ "S-1-D1" ], DT=[1]min, AREA=[21.67](ha),
2516 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2517 * N=[3], TP=[1.066]hrs,
2518 * Continuous simulation parameters:
2519 * IaRECper=[4](hrs),
2520 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2521 * InterEventTime=[12](hrs)
2522 * Baseflow simulation parameters:
2523 * BaseFlowOption=[1],
2524 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2525 * VHydCond=[0.055](mm/hr), END=-1
2526 *%-----|-----|-----|-----|-----|-----|-----|-----|
2527 *COMPUTE DUALHYD NHYDin=[ "S-1-D1" ], CINLET=[ 2.482 ](cms), NINLET=[1],
2528 * MajNHYD=[ "S-1-D1J" ]
2529 * MinNHYD=[ "S-1-D1N" ]
2530 * TMJSTO=[ 99999999 ](cu-m)
2531 *%-----|-----|-----|-----|-----|-----|-----|-----|
2532 *ADD HYD NHYDsum=[ "S-1-D1S" ], NHYDs to add=[ "S-1-D1J"+"S-1-D1N" ]
2533 *%-----|-----|-----|-----|-----|-----|-----|-----|
2534 *ROUTE RESERVOIR NHYDout=[ "S-1-D1R" ] , NHYDin=[ "S-1-D1S" ] ,
2535 * RDT=[1](min),
2536 * TABLE of ( OUTFLOW-STORAGE ) values
2537 * (cms) - (ha-m)
2538 * [ 0.0 , 0.0 ]
2539 * [ 0.2590, 0.8642 ]
2540 * [ -1 , -1 ] (max twenty pts)
2541 * NHYDovf=[ "S-1-D1Rovf" ]
2542 *%-----|-----|-----|-----|-----|-----|-----|-----|
2543 * -JFSA 2021-02-25 "S-1-D2" and "S-1-D3" are part of S-1 sub-catchment. They are
2543 moved to drain before station 6215 on Jock River
2544 *CONTINUOUS STANDHYD NHYD=[ "S-1-D2" ], DT=[1](min), AREA=[18.67](ha), XIMP=[0.65],
2544 * TIMP=[0.65], DWF=[0](cms),
2545 * LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
2545 * IAper=[4.67](mm), SLPP=[2.0](%),
2546 * LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
2546 * IAimp=[1.57](mm), SLPI=[0.75](%),
2547 * LGI=[352.798](m), MNI=[0.013], SCI=[0](min),
2548 * Continuous simulation parameters:
2548 * IaRECper=[4](hrs), IaRECImp=[4](hrs),

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2550 *           SMIN=[-1](mm),   SMAX=[-1](mm),   SK=[0.010]/(mm),
2551 *           InterEventTime=[12](hrs),      END=-1
2552 *%-----|-----|
2553 *CONTINUOUS NASHYD  NHYD=[ "S-1-D2" ], DT=[1]min, AREA=[18.67](ha),
2554 *           DWF=[0](cms), CN/C=[77],   IA=[ 4.67 ](mm),
2555 *           N=[ 3 ], TP=[1.120 ]hrs,
2556 *           Continuous simulation parameters:
2557 *           IaRECper=[ 4 ](hrs),
2558 *           SMIN=[-1](mm),   SMAX=[-1](mm),   SK=[0.010]/(mm),
2559 *           InterEventTime=[12](hrs)
2560 *           Baseflow simulation parameters:
2561 *           BaseFlowOption=[ 1 ],
2562 *           InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2563 *           VHydCond=[ 0.055 ](mm/hr),    END=-1
2564 *%-----|-----|
2565 *COMPUTE DUALHYD  NHYDin=[ "S-1-D2" ], CINLET=[ 2.062 ](cms), NINLET=[ 1 ],
2566 *           MajNHYD=[ "S-1-D2J" ]
2567 *           MinNHYD=[ "S-1-D2N" ]
2568 *           TMJSTO=[ 9999999 ](cu-m)
2569 *%-----|-----|
2570 *ADD HYD          NHYDsum=[ "S-1-D2S" ], NHYDs to add=[ "S-1-D2J" +"S-1-D2N" ]
2571 *%-----|-----|
2572 *ROUTE RESERVOIR NHYDout=[ "S-1-D2R" ], NHYDin=[ "S-1-D2S" ],
2573 *           RDT=[ 1 ](min),
2574 *           TABLE of ( OUTFLOW-STORAGE ) values
2575 *           (cms) - (ha-m)
2576 *           [ 0.0      , 0.0      ]
2577 *           [ 0.2231, 0.7445 ]
2578 *           [     -1   ,     -1   ] (max twenty pts)
2579 *           NHYDovf=[ "S-1-D2Rovf" ]
2580 *%-----|-----|
2581 *CONTINUOUS STANDHYD NHYD=[ "S-1-D3" ], DT=[1](min), AREA=[ 6.79 ](ha), XIMP=[ 0.65 ],
2582 *           TIMP=[ 0.65 ], DWF=[ 0 ](cms),
2583 *           LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
2584 *           IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%),
2585 *           LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min), Impervious surfaces:
2586 *           IAimp=[ 1.57 ](mm), SLPI=[ 0.75 ](%),
2587 *           LGI=[ 212.760 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
2588 *           Continuous simulation parameters:
2589 *           IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
2590 *           SMIN=[-1](mm),   SMAX=[-1](mm),   SK=[0.010]/(mm),
2591 *           InterEventTime=[12](hrs),      END=-1
2592 *%-----|-----|
2593 *CONTINUOUS NASHYD  NHYD=[ "S-1-D3" ], DT=[1]min, AREA=[ 6.79 ](ha),
2594 *           DWF=[ 0 ](cms), CN/C=[ 77 ],   IA=[ 4.67 ](mm),
2595 *           N=[ 3 ], TP=[1.281 ]hrs,
2596 *           Continuous simulation parameters:
2597 *           IaRECper=[ 4 ](hrs),
2598 *           SMIN=[-1](mm),   SMAX=[-1](mm),   SK=[0.010]/(mm),
2599 *           InterEventTime=[12](hrs)
2600 *           Baseflow simulation parameters:
2601 *           BaseFlowOption=[ 1 ],
2602 *           InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2603 *           VHydCond=[ 0.055 ](mm/hr),    END=-1
2604 *%-----|-----|
2605 *COMPUTE DUALHYD  NHYDin=[ "S-1-D3" ], CINLET=[ 0.719 ](cms), NINLET=[ 1 ],
2606 *           MajNHYD=[ "S-1-D3J" ]
2607 *           MinNHYD=[ "S-1-D3N" ]
2608 *           TMJSTO=[ 9999999 ](cu-m)
2609 *%-----|-----|
2610 *ADD HYD          NHYDsum=[ "S-1-D3S" ], NHYDs to add=[ "S-1-D3J" +"S-1-D3N" ]
2611 *%-----|-----|
2612 *ROUTE RESERVOIR NHYDout=[ "S-1-D3R" ], NHYDin=[ "S-1-D3S" ],
2613 *           RDT=[ 1 ](min),
2614 *           TABLE of ( OUTFLOW-STORAGE ) values
2615 *           (cms) - (ha-m)

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2613 * [ 0.0      , 0.0 ]
2614 *
2615 * [ 0.0811, 0.2708 ]
2616 * [      -1 , -1      ] (max twenty pts)
2617 *%
2618 CONTINUOUS STANDHYD NHYD=[ "S-1-D3Rovf" ]
2619 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
2620 IAper=[4.67](mm), SLPP=[2.0](%),
2621 LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
2622 IAimp=[1.57](mm), SLPI=[0.75](%),
2623 LGI=[147.874](m), MNI=[0.013], SCI=[0](min),
2624 Continuous simulation parameters:
2625 IaRECper=[4](hrs), IaRECImp=[4](hrs),
2626 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2627 InterEventTime=[12](hrs), END=-1
2628 *%
2629 *CONTINUOUS NASHYD NHYD=[ "S-1-D4" ], DT=[1]min, AREA=[3.28](ha),
2630 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2631 N=[3], TP=[1.10]hrs,
2632 Continuous simulation parameters:
2633 IaRECper=[4](hrs),
2634 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2635 InterEventTime=[12](hrs)
2636 Baseflow simulation parameters:
2637 BaseFlowOption=[1],
2638 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2639 VHydCond=[0.055](mm/hr), END=-1
2640 *%
2641 *COMPUTE DUALHYD NHYDin=[ "S-1-D4" ], CINLET=[0.373](cms), NINLET=[1],
2642 MajNHYD=[ "S-1-D4J" ]
2643 MinNHYD=[ "S-1-D4N" ]
2644 TMJSTO=[9999999](cu-m)
2645 *%
2646 *ADD HYD NHYDsum=[ "S-1-D4S" ], NHYDs to add=[ "S-1-D4J" +"S-1-D4N" ]
2647 *%
2648 *ROUTE RESERVOIR NHYDout=[ "S-1-D4R" ], NHYDin=[ "S-1-D4S" ],
2649 RDT=[1](min),
2650 TABLE of ( OUTFLOW-STORAGE ) values
2651 (cms) - (ha-m)
2652 [ 0.0      , 0.0 ]
2653 [ 0.0392, 0.1308 ]
2654 [      -1 , -1      ] (max twenty pts)
2655 *%
2656 *CONTINUOUS STANDHYD NHYD=[ "S-1-D5" ], DT=[1](min), AREA=[12.84](ha), XIMP=[0.65],
2657 TIMP=[0.65], DWF=[0](cms),
2658 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
2659 IAper=[4.67](mm), SLPP=[2.0](%),
2660 LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
2661 IAimp=[1.57](mm), SLPI=[0.75](%),
2662 LGI=[292.57](m), MNI=[0.013], SCI=[0](min),
2663 Continuous simulation parameters:
2664 IaRECper=[4](hrs), IaRECImp=[4](hrs),
2665 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2666 InterEventTime=[12](hrs), END=-1
2667 *%
2668 *CONTINUOUS NASHYD NHYD=[ "S-1-D5" ], DT=[1]min, AREA=[12.84](ha),
2669 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2670 N=[3], TP=[1.10]hrs,
2671 Continuous simulation parameters:
2672 IaRECper=[4](hrs),
2673 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2674 InterEventTime=[12](hrs)
2675 Baseflow simulation parameters:
2676 BaseFlowOption=[1],

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2673 *
2674 *
2675 *%
2676 *COMPUTE DUALHYD | NHYDin=[ "S-1-D5" ], CINLET=[ 1.395 ](cms), NINLET=[ 1 ],
2677 * MajNHYD=[ "S-1-D5J" ]
2678 * MinNHYD=[ "S-1-D5N" ]
2679 * TMJSTO=[ 9999999 ](cu-m)
2680 *%
2681 *ADD HYD | NHYDsum=[ "S-1-D5S" ], NHYDs to add=[ "S-1-D5J"+"S-1-D5N" ]
2682 *%
2683 *ROUTE RESERVOIR | NHYDout=[ "S-1-D5R" ] ,NHYDin=[ "S-1-D5S" ] ,
2684 * RDT=[ 1 ](min),
2685 * TABLE of ( OUTFLOW-STORAGE ) values
2686 * (cms) - (ha-m)
2687 * [ 0.0 , 0.0 ]
2688 * [ 0.1535, 0.5120 ]
2689 * [ -1 , -1 ] (max twenty pts)
2690 * NHYDovf=[ "S-1-D5Rovf" ]
2691 *%
2692 CONTINUOUS STANDHYD | NHYD=[ "S-1-D6" ], DT=[ 1 ](min), AREA=[ 1.75 ](ha), XIMP=[ 0.65 ],
2693 TIMP=[ 0.65 ], DWF=[ 0 ](cms),
2694 LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
2695 IApel=[ 4.67 ](mm), SLPP=[ 2.0 ](%),
2696 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min), Impervious surfaces:
2697 IAimp=[ 1.57 ](mm), SLPI=[ 0.75 ](%),
2698 LGI=[ 108.01 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
2699 Continuous simulation parameters:
2700 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
2701 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2702 InterEventTime=[ 12 ](hrs), END=-1
2703 *%
2704 *CONTINUOUS NASHYD | NHYD=[ "S-1-D6" ], DT=[ 1 ]min, AREA=[ 1.75 ](ha),
2705 * DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
2706 * N=[ 3 ], TP=[ 1.10 ]hrs,
2707 * Continuous simulation parameters:
2708 * IaRECper=[ 4 ](hrs),
2709 * SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2710 * InterEventTime=[ 12 ](hrs)
2711 * Baseflow simulation parameters:
2712 * BaseFlowOption=[ 1 ],
2713 * InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2714 * VHydCond=[ 0.055 ](mm/hr), END=-1
2715 *%
2716 *COMPUTE DUALHYD | NHYDin=[ "S-1-D6" ], CINLET=[ 0.218 ](cms), NINLET=[ 1 ],
2717 * MajNHYD=[ "S-1-D6J" ]
2718 * MinNHYD=[ "S-1-D6N" ]
2719 * TMJSTO=[ 9999999 ](cu-m)
2720 *%
2721 *ADD HYD | NHYDsum=[ "S-1-D6S" ], NHYDs to add=[ "S-1-D6J"+"S-1-D6N" ]
2722 *%
2723 *ROUTE RESERVOIR | NHYDout=[ "S-1-D6R" ] ,NHYDin=[ "S-1-D6S" ] ,
2724 * RDT=[ 1 ](min),
2725 * TABLE of ( OUTFLOW-STORAGE ) values
2726 * (cms) - (ha-m)
2727 * [ 0.0 , 0.0 ]
2728 * [ 0.0209, 0.0698 ]
2729 * [ -1 , -1 ] (max twenty pts)
2730 * NHYDovf=[ "S-1-D6Rovf" ]
2731 *%
2732 CONTINUOUS STANDHYD | NHYD=[ "S-1-D7" ], DT=[ 1 ](min), AREA=[ 2.03 ](ha), XIMP=[ 0.65 ],
2733 TIMP=[ 0.65 ], DWF=[ 0 ](cms),
2734 LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
2735 IApel=[ 4.67 ](mm), SLPP=[ 2.0 ](%),
2736 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min), Impervious surfaces:
2737 IAimp=[ 1.57 ](mm), SLPI=[ 0.75 ](%),
2738 LGI=[ 116.33 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),

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2733           Continuous simulation parameters:
2734           IaRECper=[4](hrs), IaRECImp=[4](hrs),
2735           SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2736           InterEventTime=[12](hrs), END=-1
2737 *%----- | -----
2738 *CONTINUOUS NASHYD   NHYD=[ "S-1-D7" ], DT=[1]min, AREA=[ 2.03 ](ha),
2739 *
2740 *          DWF=[0](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
2741 *          N=[ 3 ], TP=[ 1.10 ]hrs,
2742 *          Continuous simulation parameters:
2743 *          IaRECper=[4](hrs),
2744 *          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2745 *          InterEventTime=[12](hrs)
2746 *          Baseflow simulation parameters:
2747 *          BaseFlowOption=[1],
2748 *          InitGWResVol=[50](mm), GWResK=[ 0.96 ](mm/day/mm)
2749 *          VHdCond=[ 0.055 ](mm/hr), END=-1
2750 *%----- | -----
2751 *COMPUTE DUALHYD   NHYDin=[ "S-1-D7" ], CINLET=[ 2.279 ](cms), NINLET=[ 1 ],
2752 *
2753 *          MajNHYD=[ "S-1-D7J" ]
2754 *          MinNHYD=[ "S-1-D7N" ]
2755 *          TMJSTO=[ 99999999 ](cu-m)
2756 *%----- | -----
2757 *ADD HYD           NHYDsum=[ "S-1-D7S" ], NYHDs to add=[ "S-1-D7J"+"S-1-D7N" ]
2758 *%----- | -----
2759 *ROUTE RESERVOIR  NHYDout=[ "S-1-D7R" ], NHYDin=[ "S-1-D7S" ],
2760 *          RDT=[ 1 ](min),
2761 *          TABLE of ( OUTFLOW-STORAGE ) values
2762 *          (cms) - (ha-m)
2763 *          [ 0.0 , 0.0 ]
2764 *          [ 0.0243, 0.0810 ]
2765 *          [ -1 , -1 ] (max twenty pts)
2766 *          NYHDovf=[ "S-1-D8Rovf" ]
2767 *%----- | -----
2768 *      -JFSA 2021-02-26 "S-1-D8" is a part of S-1 sub-catchment. It is moved to drain
2769 before station 6016 on Jock River
2770 *CONTINUOUS STANDHYD NHYD=[ "S-1-D8" ], DT=[1](min), AREA=[ 5.27 ](ha), XIMP=[ 0.65 ],
2771 *          TIMP=[ 0.65 ], DWF=[ 0 ](cms),
2772 *          LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
2773 *          IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%),
2774 *          LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min), Impervious surfaces:
2775 *          IAimp=[ 1.57 ](mm), SLPI=[ 0.75 ](%),
2776 *          LGI=[ 187.439 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
2777 *          Continuous simulation parameters:
2778 *          IaRECper=[4](hrs), IaRECImp=[4](hrs),
2779 *          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2780 *          InterEventTime=[12](hrs), END=-1
2781 *%----- | -----
2782 *CONTINUOUS NASHYD   NHYD=[ "S-1-D8" ], DT=[1]min, AREA=[ 5.27 ](ha),
2783 *
2784 *          DWF=[0](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
2785 *          N=[ 3 ], TP=[ 1.10 ]hrs,
2786 *          Continuous simulation parameters:
2787 *          IaRECper=[4](hrs),
2788 *          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2789 *          InterEventTime=[12](hrs)
2790 *          Baseflow simulation parameters:
2791 *          BaseFlowOption=[1],
2792 *          InitGWResVol=[50](mm), GWResK=[ 0.96 ](mm/day/mm)
2793 *          VHdCond=[ 0.055 ](mm/hr), END=-1
2794 *%----- | -----

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2795 *ADD HYD           NHYDsum=[ "S-1-D" ], NHYDs to add=[ "S-1-Okeefe"+"S-1"+"S-1-Fost" ]
2796 *%-----|-----|
2797 *COMPUTE DUALHYD NHYDin=[ "S-1-D" ], CINLET=[11.616](cms), NINLET=[1],
2798 *
2799 *          MajNHYD=[ "S-1-D-MJ" ]
2800 *          MinNHYD=[ "S-1-D-MN" ]
2801 *          TMJSTO=[ 5974 ](cu-m)
2802 *%-----|-----|
2803 *ADD HYD           NHYDsum=[ "S-1-DEV" ], NHYDs to add=[ "S-1-D-MJ"+"S-1-D-MN" ]
2804 *%-----|-----|
2805 *ROUTE RESERVOIR NHYDout=[ "S-1-D8R" ] , NHYDin=[ "S-1-D8S" ] ,
2806 *          RDT=[1](min),
2807 *          TABLE of ( OUTFLOW-STORAGE ) values
2808 *          (cms) - (ha-m)
2809 *          [ 0.0      , 0.0   ]
2810 *          [ 0.0630 , 0.2102 ]
2811 *          [     -1 ,     -1   ] (max twenty pts)
2812 *          NHYDovf=[ "S-1-D8Rovf" ]
2813 *%-----|-----|
2814 *          -JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
2815 *          (W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
2816 *#    Catchment W_CLAR
2817 *#    - To West Clarke Drain (south of the Jock)
2818 *#    - Subdivision with 43% imp. as per Barrhaven South MSS
2819 *#    - 2020-11-30 update CLARKE Tributary Drainage Area to = 121 ha based on
2820 *#          P598(04)-11
2821 *#          - 2020-11-30 split CLARKE Drainage Area to MAJOR and ALL
2822 *#***** ****
2823 CONTINUOUS STANDHYD NHYD=[ "W_CLAR_MJ" ], DT=[1]min, AREA=[1.772](ha),
2824 *          XIMP=[0.46], TIMP=[0.59], DWF=[0](cms), LOSS=[2],
2825 *          SCS curve number CN=[77],
2826 *          Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
2827 *          LGP=[40](m), MNP=[0.25], SCP=[0](min),
2828 *          Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
2829 *          LGI=[109](m), MNI=[0.013], SCI=[0](min),
2830 *          Continuous simulation parameters:
2831 *          IaRECper=[4](hrs), IaRECImp=[4](hrs),
2832 *          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2833 *          InterEventTime=[18](hrs), END=-1
2834 *%-----|-----|
2835 *COMPUTE DUALHYD NHYDin=[ "W_CLAR_MJ" ], CINLET=[0.213](cms), NINLET=[1],
2836 *          MajNHYD=[ "W_CLAR_MJj" ]
2837 *          MinNHYD=[ "W_CLAR_MJn" ]
2838 *          TMJSTO=[0.1](cu-m)
2839 *# 5-Year + 12% Capture
2840 ROUTE RESERVOIR NHYDout=[ "W_CLAR_MJn" ] , NHYDin=[ "W_CLAR_MJ" ] ,
2841 *          RDT=[1](min),
2842 *          TABLE of ( OUTFLOW-STORAGE ) values
2843 *          (cms) - (ha-m)
2844 *          [ 0.0      , 0.0   ]
2845 *          [ 0.213  , 0.0001 ]
2846 *          [     -1 ,     -1   ] (max twenty pts)
2847 *          NHYDovf=[ "W_CLAR_MJj" ] ,
2848 *          -Clarke_All area from P 598(04)-11 = 120.207 ha, change to 127.298 ha based on
2849 *          GIS measurements,
2850 *          -JFSA, 2021-01-19 update W_CLAR_ALL to (121.17-1.772=119.398) ha based on GIS
2851 *          measurements W_CLAR is 121.17 ha and W_CLAR_MJ is 1.772 ha
2852 CONTINUOUS STANDHYD NHYD=[ "W_CLAR_ALL" ], DT=[1]min, AREA=[119.398](ha),
2853 *          XIMP=[0.60], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2854 *          SCS curve number CN=[77],
2855 *          Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
2856 *          LGP=[40](m), MNP=[0.25], SCP=[0](min),
          Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
          LGI=[892.18](m), MNI=[0.013], SCI=[0](min),

```

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2857 Continuous simulation parameters:
2858 IaRECper=[4](hrs), IaRECImp=[4](hrs),
2859 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2860 InterEventTime=[18](hrs), END=-1
2861 *%-----|-----|
2862 ADD HYD NHYDsum=[ "W_CLAR" ], NHYDs to add=[ "W_CLAR_ALL"+"W_CLAR_MJj" ]
2863 *%-----|-----|
2864 SAVE HYD NHYD=[ "W_CLAR" ], # OF PCYCLES=[-1], ICASEsh=[1]
2865 HYD_COMMENT=[ "Total Flows to West Clarke" ]
2866 *#*****#
2867 *# West Clarke Pond 2
2868 *# - Rating curve obtained from Barrhaven South MSS modeling
2869 *# - Tributary Drainage Area to MSS Pond 2 = 241 ha
2870 *#*****#
2871 ROUTE RESERVOIR NHYDout=[ "MS_P2" ], NHYDin=[ "W_CLAR" ],
2872 RDT=[1](min),
2873 TABLE of ( OUTFLOW-STORAGE ) values
2874 (cms) - (ha-m)
2875 [ 0.0 , 0.0 ]
2876 [ 0.128 , 0.161 ]
2877 [ 0.138 , 0.409 ]
2878 [ 0.148 , 0.68 ]
2879 [ 0.227 , 0.931 ]
2880 [ 0.354 , 1.223 ]
2881 [ 0.505 , 1.52 ]
2882 [ 0.666 , 1.821 ]
2883 [ 0.831 , 2.123 ]
2884 [ 0.995 , 2.434 ]
2885 [ 1.069 , 2.583 ]
2886 [ 1.51 , 2.647 ]
2887 [ 4.904 , 2.861 ]
2888 [ 13.048 , 3.188 ]
2889 [ 23.745 , 3.523 ]
2890 [ 36.474 , 3.871 ]
2891 [ 45.938 , 4.127 ]
2892 [ 61.652 , 4.539 ]
2893 [ -1 , -1 ] (max twenty pts)
2894 NHYDovf=[ "P2-OVF" ]
2895 *%-----|-----|
2896 *#*****#
2897 * -JFSA, 2021-01-22 "W_CLAR_UNDE" (west of Clarke sub-catchment) discharges
2898 directly to the jock river through a road side ditch on the west side of Borrisokane
2899 road (station 6016)
2900 *CONTINUOUS NASHYD NHYD=[ "W_CLAR_UNDE" ], DT=[1]min, AREA=[35.65](ha),
2901 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2902 * N=[3], TP=[1.10]hrs,
2903 * Continuous simulation parameters:
2904 * IaRECper=[4](hrs),
2905 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2906 * InterEventTime=[12](hrs)
2907 * Baseflow simulation parameters:
2908 * BaseFlowOption=[1],
2909 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2910 * VHydCond=[0.055](mm/hr), END=-1
2911 *%-----|-----|
2912 ADD HYD NHYDsum=[ "SN_CE" ], NHYDs to
2913 add=[ "N_CE "+ "S-1-D4 "+ "S-1-D5 "+ "MS_P2 "+ "P2-OVF" ]
2914 *%-----|-----|
2915 SAVE HYD NHYD=[ "SN_CE" ], # OF PCYCLES=[-1], ICASEsh=[1]
2916 HYD_COMMENT=[ "Total Flows before Station 5737 on Jock River" ]
2917 *%-----|-----|
2918 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5737
2919 *# 2021-02-25 add station 5737 before station 5002. Station 5737 was extracted from the
2920 HEC-RAS model
2921 T:\PROJ\1474-16\Design\20201026-QuantityControlAnalysis\HEC-RAS\JockLidar2005
2922 *# JFSA 2021-03-02 change the slope to 0.0175% instead of 0.02593 to stabilize the model

```



```

2979 * [161.44, 91.50]
2980 * [236.48, 93.00]
2981 * [385.47, 92.50]
2982 * [390.78, 92.50]
2983 *%-----|-----|
2984 ROUTE CHANNEL      NHYDout=[ "N_WCb" ] ,NHYDin=[ "N_WCa" ] ,
2985 RDT=[1](min),
2986 CHLGTH=[ 245.33333](m),   CHSLOPE=[ 0.09511](%),
2987                                     FPSLOPE=[ 0.09511](%),
2988 SECNUM=[ 1.0],           NSEG=[ 3]
2989 ( SEGRROUGH, SEGDIST (m))=
2990     [ 0.050,-37.5
2991     -0.035,37.50
2992     0.050,157.05] NSEG times
2993 ( DISTANCE (m), ELEVATION (m))=
2994     [-601.81, 91.5]
2995     [-37.50, 90.00]
2996     [-19.61, 87.04]
2997     [ 0.00, 85.70]
2998     [14.87, 86.93]
2999     [37.50, 90.00]
3000     [38.54, 90.50]
3001     [42.23, 91]
3002     [157.05,91.50]
3003 *%-----|-----|
3004 ROUTE CHANNEL      NHYDout=[ "N_WC" ] ,NHYDin=[ "N_WCb" ] ,
3005 RDT=[1](min),
3006 CHLGTH=[ 245.33333](m),   CHSLOPE=[ 0.09511](%),
3007                                     FPSLOPE=[ 0.09511](%),
3008 SECNUM=[ 1.0],           NSEG=[ 3]
3009 ( SEGRROUGH, SEGDIST (m))=
3010     [ 0.050,-37.5
3011     -0.035,37.50
3012     0.050,157.05] NSEG times
3013 ( DISTANCE (m), ELEVATION (m))=
3014     [-601.81, 91.5]
3015     [-37.50, 90.00]
3016     [-19.61, 87.04]
3017     [ 0.00, 85.70]
3018     [14.87, 86.93]
3019     [37.50, 90.00]
3020     [38.54, 90.50]
3021     [42.23, 91]
3022     [157.05,91.50]
3023 *#*****|-----|
3024 *      -JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
3025 (W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
3026 *ADD HYD          NHYDsum=[ "SN_WC" ], NHYDs to
3027 add=[ "MS_P2"+ "P2-OVF"+ "N_WC"+ "W_CLAR_UNDE" ]
3028 *%-----|-----|
3029 *SAVE HYD          NHYD=[ "SN_WC" ], # OF PCYCLES=[-1], ICASEsh=[1]
3030 *                  HYD_COMMENT=[ "Total Flows at West Clarke Pond Outlet" ]
3031 *%-----|-----|
3032 *# Hydrograph from Node West Clarke routed to Node at Kennedy - Burnett Drain
3033 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4534
3034 *#
3035 ROUTE CHANNEL      NHYDout=[ "N_KB" ] ,NHYDin=[ "N_WC" ] ,
3036 RDT=[1](min),
3037 CHLGTH=[ 1020](m),   CHSLOPE=[ 0.0498](%),
3038                                     FPSLOPE=[ 0.0498](%),
3039 SECNUM=[ 1.0],           NSEG=[ 3]
3040 ( SEGRROUGH, SEGDIST (m))=
3041     [ 0.050,-23.63
3042     -0.035,23.63
3043     0.050,728.3] NSEG times
3044 ( DISTANCE (m), ELEVATION (m))=

```

```

3043 [-1082.01,94]
3044 [-1028.17,92.5]
3045 [-992.3,93.5]
3046 [-279.34,90]
3047 [-23.63,90]
3048 [-13.45,87.13]
3049 [-0.07,86.24]
3050 [10.54,87.15]
3051 [23.63,90]
3052 [24.86,90.5]
3053 [26.72,91]
3054 [45.07,91.5]
3055 [128.17,91.5]
3056 [270.7,92.5]
3057 [728.3,95]
3058 *%-----|-----|
3059 *#*****
3060 *# Catchment KEN_BU
3061 *# - To Kennedy-Burnett SWM Facility
3062 *# - Outlets to Fraser-Clarke drain (north of the Jock)
3063 *# - Medium density residential subdivision
3064 * - Add Kennedy Burnett model (Convert PCSWMM from NOVATECH June, 2020 to SWMHYMO)
3065 *#*****
3066 *CONTINUOUS STANDHYD NHYD=[ "KEN_BU" ], DT=[1]min, AREA=[ 281 ](ha),
3067 * XIMP=[ 0.55 ], TIMP=[ 0.55 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
3068 * SCS curve number CN=[ 71 ],
3069 * Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
3070 * LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
3071 * Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
3072 * LGI=[ 1369 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3073 * Continuous simulation parameters:
3074 * IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
3075 * SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
3076 * InterEventTime=[ 18 ](hrs), END=-1
3077 *%-----|-----|
3078 *#*****
3079 *# Existing Kennedy-Burnett SWM Facility
3080 *# - Rating curve obtained from URTKBP
3081 *# - Tributary Drainage Area to Pond = 160 ha
3082 *#*****
3083 *ROUTE RESERVOIR      NHYDout=[ "KEN_P" ], NHYDin=[ "KEN_BU" ],
3084 * RDT=[ 1 ](min),
3085 * TABLE of ( OUTFLOW-STORAGE ) values
3086 * ( cms ) - ( ha-m )
3087 * [ 0.0 , 0.0 ]
3088 * [ 0.13 , 0.26 ]
3089 * [ 0.43 , 0.56 ]
3090 * [ 0.67 , 0.90 ]
3091 * [ 0.86 , 1.32 ]
3092 * [ 1.01 , 1.79 ]
3093 * [ 1.15 , 2.33 ]
3094 * [ -1 , -1 ] (max twenty pts)
3095 * NHYDovf=[ "KEN-OV" ]
3096 *%-----|-----|
3097 * -JFSA, 2021-01-19 update all KEN_BU areas based on GIS measurements
3098 CONTINUOUS STANDHYD NHYD=[ "KB-01A" ], DT=[1]min, AREA=[ 40.82 ](ha), XIMP=[ 0.097 ],
3099 * TIMP=[ 0.4 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3100 * Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3101 * F=[ 0.00 ](mm),
3102 * Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%), LGP=[ 40 ](m),
3103 * MNP=[ 0.250 ], SCP=[ 0 ](min),
3104 * Impervious areas: IAimp=[ 0.785 ](mm), SLPI=[ 0.5 ](%),
3105 * LGI=[ 521.664 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3106 * Continuous simulation parameters:
3107 * IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3108 * END=-1

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3104 *%
3105 COMPUTE DUALHYD NHYDin=[ "KB-01A" ], CINLET=[ 3.6 ](cms), NINLET=[ 1 ],
3106 MajNHYD=[ "KB-01A-MJ" ]
3107 MinNHYD=[ "KB-01A-MN" ]
3108 TMJSTO=[ 4995 ](cu-m)
3109 *%
3110 ADD HYD NHYDsum=[ "KB-01A-S" ], NHYDs to add=[ "KB-01A-MJ" +"KB-01A-MN" ]
3111 *%
3112 CONTINUOUS STANDHYD NHYD=[ "KB-01B" ], DT=[ 1 ]min, AREA=[ 31.1 ](ha), XIMP=[ 0.1875 ],
3113 TIMP=[ 0.375 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3114 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3115 F=[ 0.00 ](mm),
3116 Previous areas: IAper=[ 4.67 ](mm), SLPP=[ 0.42 ](%), LGP=[ 40 ](m),
3117 MNP=[ 0.250 ], SCP=[ 0 ](min),
3118 Impervious areas: IAimp=[ 0.785 ](mm), SLPI=[ 0.42 ](%),
3119 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3120 MGI=[ 455.339 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3121 Continuous simulation parameters:
3122 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3123 END=-1
3124 *%
3125 COMPUTE DUALHYD NHYDin=[ "KB-01B" ], CINLET=[ 1.585 ](cms), NINLET=[ 1 ],
3126 MajNHYD=[ "KB-01B-MJ" ]
3127 MinNHYD=[ "KB-01B-MN" ]
3128 TMJSTO=[ 6075 ](cu-m)
3129 *%
3130 ADD HYD NHYDsum=[ "KB-01B-S" ], NHYDs to add=[ "KB-01B-MJ" +"KB-01B-MN" ]
3131 *%
3132 CONTINUOUS STANDHYD NHYD=[ "KB-01C" ], DT=[ 1 ]min, AREA=[ 13.78 ](ha), XIMP=[ 0.2045 ],
3133 TIMP=[ 0.409 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3134 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3135 F=[ 0.00 ](mm),
3136 Previous areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3137 MNP=[ 0.250 ], SCP=[ 0 ](min),
3138 Impervious areas: IAimp=[ 0.785 ](mm), SLPI=[ 0.5 ](%),
3139 MGI=[ 303.095 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3140 Continuous simulation parameters:
3141 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3142 END=-1
3143 *%
3144 COMPUTE DUALHYD NHYDin=[ "KB-01C" ], CINLET=[ 1.35 ](cms), NINLET=[ 1 ],
3145 MajNHYD=[ "KB-01C-MJ" ]
3146 MinNHYD=[ "KB-01C-MN" ]
3147 TMJSTO=[ 1880 ](cu-m)
3148 *%
3149 ADD HYD NHYDsum=[ "KB-01C-S" ], NHYDs to add=[ "KB-01C-MJ" +"KB-01C-MN" ]
3150 *%
3151 CONTINUOUS STANDHYD NHYD=[ "KB-03" ], DT=[ 1 ]min, AREA=[ 84.78 ](ha), XIMP=[ 0.197 ],
3152 TIMP=[ 0.394 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3153 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3154 F=[ 0.00 ](mm),
3155 Previous areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3156 MNP=[ 0.250 ], SCP=[ 0 ](min),
3157 Impervious areas: IAimp=[ 0.785 ](mm), SLPI=[ 0.63 ](%),
3158 MGI=[ 751.798 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3159 Continuous simulation parameters:
3160 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3161 END=-1
3162 *%
3163 COMPUTE DUALHYD NHYDin=[ "KB-03" ], CINLET=[ 5.27 ](cms), NINLET=[ 1 ],
3164 MajNHYD=[ "KB-03-MJ" ]
3165 MinNHYD=[ "KB-03-MN" ]
3166 TMJSTO=[ 15500 ](cu-m)
3167 *%
3168 ADD HYD NHYDsum=[ "KB-03-S" ], NHYDs to add=[ "KB-03-MJ" +"KB-03-MN" ]
3169 *%
3170 CONTINUOUS STANDHYD NHYD=[ "KB-04" ], DT=[ 1 ]min, AREA=[ 6.95 ](ha), XIMP=[ 0.85 ],

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3155    TIMP=[0.85], DWF=[0](cms), LOSS=[1]:
3156        Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3157        F=[0.00](mm),
3158        Previous areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3159        MNP=[0.250], SCP=[0](min),
3160        Impervious areas: IAimp=[0.942](mm), SLPI=[0.5](%),
3161        LGI=[215.252](m), MNI=[0.013], SCI=[0](min),
3162        Continuous simulation parameters:
3163        IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
3164        END=-1
3165    *%
3166    COMPUTE DUALHYD NHYDin=[ "KB-04" ], CINLET=[ 0.503 ](cms), NINLET=[ 1 ],
3167        MajNHYD=[ "KB-04-MJ" ]
3168        MinNHYD=[ "KB-04-MN" ]
3169        TMJSTO=[1972](cu-m)
3170    *%
3171    ADD HYD NHYDsum=[ "KB-04-S" ], NHYDs to add=[ "KB-04-MJ"+"KB-04-MN" ]
3172    *%
3173    CONTINUOUS STANDHYD NHYD=[ "KB-05" ], DT=[1]min, AREA=[5.19](ha), XIMP=[ 0.93 ],
3174    TIMP=[0.93], DWF=[0](cms), LOSS=[1]:
3175        Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3176        F=[0.00](mm),
3177        Previous areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3178        MNP=[0.250], SCP=[0](min),
3179        Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
3180        LGI=[186.011](m), MNI=[0.013], SCI=[0](min),
3181        Continuous simulation parameters:
3182        IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
3183        END=-1
3184    *%
3185    COMPUTE DUALHYD NHYDin=[ "KB-06" ], CINLET=[ 2.262 ](cms), NINLET=[ 1 ],
3186        MajNHYD=[ "KB-06-MJ" ]
3187        MinNHYD=[ "KB-06-MN" ]
3188        TMJSTO=[1950](cu-m)
3189    *%
3190    ADD HYD NHYDsum=[ "KB-06-S" ], NHYDs to add=[ "KB-06-MJ"+"KB-06-MN" ]
3191    *%
3192    CONTINUOUS STANDHYD NHYD=[ "KB-11" ], DT=[1]min, AREA=[4.03](ha), XIMP=[ 0.675 ],
3193    TIMP=[0.675], DWF=[0](cms), LOSS=[1]:
3194        Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3195        F=[0.00](mm),
3196        Previous areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3197        MNP=[0.250], SCP=[0](min),
3198        Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%),
3199        LGI=[163.911](m), MNI=[0.013], SCI=[0](min),
3200        Continuous simulation parameters:
3201        IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
3202        END=-1
3203    *%
3204    COMPUTE DUALHYD NHYDin=[ "KB-11" ], CINLET=[ 0.5773 ](cms), NINLET=[ 1 ],
3205        MajNHYD=[ "KB-11-MJ" ]
3206        MinNHYD=[ "KB-11-MN" ]
3207        TMJSTO=[597](cu-m)

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3201 *%
3202 ADD HYD NHYDsum= [ "KB-11-S" ], NHYDs to add= [ "KB-11-MJ" +"KB-11-MN" ]
3203 *%
3204 CONTINUOUS STANDHYD NHYD= [ "S1" ], DT=[1]min, AREA=[ 4.99 ](ha), XIMP=[ 0.93 ], TIMP=[ 0.93 ],
3205 DWF=[ 0 ](cms), LOSS=[ 1 ]:
3206 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3207 F=[ 0.00 ](mm),
3208 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3209 MNP=[ 0.250 ], SCP=[ 0 ](min),
3210 Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 2.0 ](%),
3211 LGI=[ 182.392 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3212 Continuous simulation parameters:
3213 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3214 END=-1
3215 *%
3216 CONTINUOUS STANDHYD NHYD= [ "KB-15" ], DT=[1]min, AREA=[ 2.15 ](ha), XIMP=[ 0.79 ],
3217 TIMP=[ 0.79 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3218 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3219 F=[ 0.00 ](mm),
3220 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3221 MNP=[ 0.250 ], SCP=[ 0 ](min),
3222 Impervious areas: IAimp=[ 0.157 ](mm), SLPI=[ 0.3 ](%),
3223 LGI=[ 119.722 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3224 Continuous simulation parameters:
3225 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3226 END=-1
3227 *%
3228 *%
3229 ADD HYD NHYDsum= [ "KB-P1" ], NHYDs to
3230 add= [ "KB-01A-S" +"KB-01B-S" +"KB-01C-S" +"KB-03-S" +"KB-04-S" +"KB-05" +"KB-06-S" +"KB-11-S" +"KB
3231 -15 " +"S1" ]
3232 *%
3233 ROUTE RESERVOIR NHYDout= [ "KB-P1R" ], NHYDin= [ "KB-P1" ],
3234 RDT=[ 1 ](min),
3235 TABLE of ( OUTFLOW-STORAGE ) values
3236 ( cms ) - ( ha-m )
3237 [ 0.0 , 0.0 ]
3238 [ 0.076 , 0.003 ]
3239 [ 0.088 , 0.006 ]
3240 [ 0.136 , 0.011 ]
3241 [ 0.301 , 0.017 ]
3242 [ 0.454 , 0.027 ]
3243 [ 0.631 , 0.041 ]
3244 [ 1.173 , 0.068 ]
3245 [ 1.91 , 0.111 ]
3246 [ 4.847 , 0.231 ]
3247 [ 9.813 , 0.436 ]
3248 [ 12.134 , 0.617 ]
3249 [ 12.438 , 0.732 ]
3250 [ 12.424 , 0.811 ]
3251 [ 12.425 , 0.894 ]
3252 [ -1 , -1 ] (max twenty pts)
3253 NHYDovf= [ "KB-P1ovf" ]
3254 *%
3255 ADD HYD NHYDsum= [ "KB-Pond1" ], NHYDs to add= [ "KB-P1R" +"KB-P1ovf" ]
3256 *%
3257 SAVE HYD NHYD= [ "KB-Pond1" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
3258 HYD_COMMENT= [ "Total Flows at KB first pond" ]
3259 *%
3260 CONTINUOUS STANDHYD NHYD= [ "KB-07" ], DT=[1]min, AREA=[ 10.86 ](ha), XIMP=[ 0.86 ],
3261 TIMP=[ 0.86 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3262 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3263 F=[ 0.00 ](mm),
3264 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3265 MNP=[ 0.250 ], SCP=[ 0 ](min),
3266 Impervious areas: IAimp=[ 0.785 ](mm), SLPI=[ 2.0 ](%),

```

```

3252 LGI=[269.072](m), MNI=[0.013], SCI=[0](min),
3253 Continuous simulation parameters:
3254 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
3255 END=-1
3256 *%-----|-----|
3257 COMPUTE DUALHYD NHYDin=[ "KB-07" ], CINLET=[ 2.094 ](cms), NINLET=[ 1 ],
3258 MajNHYD=[ "KB-07-MJ" ]
3259 MinNHYD=[ "KB-07-MN" ]
3260 TMJSTO=[ 1378 ](cu-m)
3261 *%-----|-----|
3262 ADD HYD NHYDsum=[ "KB-07-S" ], NHYDs to add=[ "KB-07-MJ" +"KB-07-MN" ]
3263 *%-----|-----|
3264 CONTINUOUS STANDHYD NHYD=[ "KB-08" ], DT=[ 1 ]min, AREA=[ 6.61 ](ha), XIMP=[ 0.64 ],
3265 TIMP=[ 0.64 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3266 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3267 F=[ 0.00 ](mm),
3268 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3269 MNP=[ 0.250 ], SCP=[ 0 ](min),
3270 Impervious areas: IAimp=[ 0.785 ](mm), SLPI=[ 2.0 ](%),
3271 LGI=[ 209.921 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3272 Continuous simulation parameters:
3273 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3274 END=-1
3275 *%-----|-----|
3276 COMPUTE DUALHYD NHYDin=[ "KB-08" ], CINLET=[ 1.058 ](cms), NINLET=[ 1 ],
3277 MajNHYD=[ "KB-08-MJ" ]
3278 MinNHYD=[ "KB-08-MN" ]
3279 TMJSTO=[ 787 ](cu-m)
3280 *%-----|-----|
3281 ADD HYD NHYDsum=[ "KB-08-S" ], NHYDs to add=[ "KB-08-MJ" +"KB-08-MN" ]
3282 *%-----|-----|
3283 CONTINUOUS STANDHYD NHYD=[ "KB-09" ], DT=[ 1 ]min, AREA=[ 2.6 ](ha), XIMP=[ 0.86 ],
3284 TIMP=[ 0.86 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3285 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3286 F=[ 0.00 ](mm),
3287 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3288 MNP=[ 0.250 ], SCP=[ 0 ](min),
3289 Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 2.0 ](%),
3290 LGI=[ 131.656 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3291 Continuous simulation parameters:
3292 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3293 END=-1
3294 *%-----|-----|
3295 CONTINUOUS STANDHYD NHYD=[ "KB-10_1" ], DT=[ 1 ]min, AREA=[ 2.37 ](ha), XIMP=[ 0.86 ],
3296 TIMP=[ 0.86 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3297 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3298 F=[ 0.00 ](mm),
3299 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3300 MNP=[ 0.250 ], SCP=[ 0 ](min),
3301 Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 2.0 ](%),
3302 LGI=[ 125.698 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3303 Continuous simulation parameters:
3304 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3305 END=-1
3306 *%-----|-----|
3307 CONTINUOUS STANDHYD NHYD=[ "KB-10_2" ], DT=[ 1 ]min, AREA=[ 1.14 ](ha), XIMP=[ 0.86 ],
3308 TIMP=[ 0.86 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3309 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3310 F=[ 0.00 ](mm),
3311 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3312 MNP=[ 0.250 ], SCP=[ 0 ](min),
3313 Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 2.0 ](%), LGI=[ 87.178 ](m),
3314 MNI=[ 0.013 ], SCI=[ 0 ](min),
3315 Continuous simulation parameters:
3316 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),

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3297      END=-1
3298      *%
3299      *%
3300      CONTINUOUS STANDHYD NHYD=[ "KB-12" ], DT=[1]min, AREA=[ 4.86 ](ha), XIMP=[ 0.79 ],
3301      TIMP=[ 0.79 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3302          Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3303          F=[ 0.00 ](mm),
3304          Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3305          MNP=[ 0.250 ], SCP=[ 0 ](min),
3306          Impervious areas: IAimp=[ 1.099 ](mm), SLPI=[ 2.0 ](%),
3307          LGI=[ 180.000 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3308          Continuous simulation parameters:
3309          IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3310          END=-1
3311      *%
3312      COMPUTE DUALHYD NHYDin=[ "KB-12" ], CINLET=[ 0.8665 ](cms), NINLET=[ 1 ],
3313      MajNHYD=[ "KB-12-MJ" ]
3314      MinNHYD=[ "KB-12-MN" ]
3315      TMJSTO=[ 632 ](cu-m)
3316      *%
3317      ADD HYD NHYDsum=[ "KB-12-S" ], NHYDs to add=[ "KB-12-MJ" + "KB-12-MN" ]
3318      *%
3319      CONTINUOUS STANDHYD NHYD=[ "KB-13" ], DT=[1]min, AREA=[ 10.19 ](ha), XIMP=[ 0.64 ],
3320      TIMP=[ 0.64 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3321          Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3322          F=[ 0.00 ](mm),
3323          Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3324          MNP=[ 0.250 ], SCP=[ 0 ](min),
3325          Impervious areas: IAimp=[ 0.785 ](mm), SLPI=[ 2.0 ](%),
3326          LGI=[ 260.640 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3327          Continuous simulation parameters:
3328          IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3329          END=-1
3330      *%
3331      COMPUTE DUALHYD NHYDin=[ "KB-13" ], CINLET=[ 1.722 ](cms), NINLET=[ 1 ],
3332      MajNHYD=[ "KB-13-MJ" ]
3333      MinNHYD=[ "KB-13-MN" ]
3334      TMJSTO=[ 1077 ](cu-m)
3335      *%
3336      ADD HYD NHYDsum=[ "KB-13-S" ], NHYDs to add=[ "KB-13-MJ" + "KB-13-MN" ]
3337      *%
3338      CONTINUOUS STANDHYD NHYD=[ "KB-14" ], DT=[1]min, AREA=[ 5.47 ](ha), XIMP=[ 0.64 ],
3339      TIMP=[ 0.64 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3340          Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3341          F=[ 0.00 ](mm),
3342          Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3343          MNP=[ 0.250 ], SCP=[ 0 ](min),
3344          Impervious areas: IAimp=[ 0.785 ](mm), SLPI=[ 2.0 ](%),
3345          LGI=[ 190.962 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3346          Continuous simulation parameters:
3347          IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3348          END=-1
3349      *%
3350      COMPUTE DUALHYD NHYDin=[ "KB-14" ], CINLET=[ 0.8734 ](cms), NINLET=[ 1 ],
3351      MajNHYD=[ "KB-14-MJ" ]
3352      MinNHYD=[ "KB-14-MN" ]
3353      TMJSTO=[ 631 ](cu-m)
3354      *%
3355      ADD HYD NHYDsum=[ "KB-14-S" ], NHYDs to add=[ "KB-14-MJ" + "KB-14-MN" ]
3356      *%
3357      *%
3358      CONTINUOUS STANDHYD NHYD=[ "KB-16_2" ], DT=[1]min, AREA=[ 3.42 ](ha), XIMP=[ 0.71 ],
3359      TIMP=[ 0.71 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3360          Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3361          F=[ 0.00 ](mm),
3362          Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3363          MNP=[ 0.250 ], SCP=[ 0 ](min),
3364          Impervious areas: IAimp=[ 1.099 ](mm), SLPI=[ 2.0 ](%),
3365          LGI=[ 180.000 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3366          Continuous simulation parameters:
3367          IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3368          END=-1
3369      *%

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3345 MNP=[0.250], SCP=[0](min),
3346 Impervious areas: IAimp=[0.157](mm), SLPI=[0.3](%),
3347 LGI=[150.997](m), MNI=[0.013], SCI=[0](min),
3348 Continuous simulation parameters:
3349 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
3350 END=-1
3351 *%-----|-----|
3352 ADD HYD NHYDsum=[ "KB-P2" ], NHYDs to
3353 add=[ "KB-Pond1 "+"KB-07-S "+"KB-08-S "+"KB-09 "+"KB-10_1 "+"KB-10_2 "+"KB-12-S "+"KB-13-S "+"KB-1
3354 4-S "+"KB-16_2" ]
3355 *%-----|-----|
3356 ROUTE RESERVOIR NHYDout=[ "KB-P2R" ], NHYDin=[ "KB-P2" ],
3357 RDT=[1](min),
3358 TABLE of ( OUTFLOW-STORAGE ) values
3359 (cms) - (ha-m)
3360 [ 0.0 , 0.0 ]
3361 [ 0.053,0.005]
3362 [ 0.132,0.009]
3363 [ 0.269,0.014]
3364 [ 0.455,0.023]
3365 [ 0.699,0.037]
3366 [ 0.947,0.056]
3367 [ 1.853,0.09]
3368 [ 2.712,0.146]
3369 [ 6.626,0.287]
3370 [ 11.228,0.515]
3371 [ 14.885,0.738]
3372 [ 16.473,0.893]
3373 [ 17.311,0.998]
3374 [ 17.633,1.063]
3375 [ 17.634,1.112]
3376 [ -1 , -1 ] (max twenty pts)
3377 NHYDovf=[ "KB-P2ovf" ]
3378 *%-----|-----|
3379 ADD HYD NHYDsum=[ "KB-Pond2" ], NHYDs to add=[ "KB-P2R "+"KB-P2ovf" ]
3380 *%-----|-----|
3381 SAVE HYD NHYD=[ "KB-Pond2" ], # OF PCYCLES=[-1], ICASEsh=[1]
3382 HYD_COMMENT=[ "Total Flows at KB second pond" ]
3383 *%-----|-----|
3384 CONTINUOUS STANDHYD NHYD=[ "KB-16_1" ], DT=[1]min, AREA=[2.8](ha), XIMP=[0.75],
3385 TIMP=[0.75], DWF=[0](cms), LOSS=[1]:
3386 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3387 F=[0.00](mm),
3388 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3389 MNP=[0.250], SCP=[0](min),
3390 Impervious areas: IAimp=[0.157](mm), SLPI=[0.3](%),
3391 LGI=[136.626](m), MNI=[0.013], SCI=[0](min),
3392 Continuous simulation parameters:
3393 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
3394 END=-1
3395 *%-----|-----|
3396 ADD HYD NHYDsum=[ "KB-P3" ], NHYDs to add=[ "KB-Pond2 "+"KB-16_1" ]
3397 *%-----|-----|
3398 *%-----|-----|
3399 * One inflow node from pond 3 is added to the model (ROUTE RESERVOIR)
3400 * Another inflow node from right side of pond 3 is not added to the model
3401 ROUTE RESERVOIR NHYDout=[ "KB-P3R" ], NHYDin=[ "KB-P3" ],
3402 RDT=[1](min),
3403 TABLE of ( OUTFLOW-STORAGE ) values
3404 (cms) - (ha-m)
3405 [ 0.0 , 0.0 ]
3406 [ 0.051,0.002]
3407 [ 0.048,0.003]
3408 [ 0.057,0.029]
3409 [ 0.089,0.045]
3410 [ 0.133,0.069]

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3401 [0.199,0.106]
3402 [0.321,0.172]
3403 [1.029,0.306]
3404 [4.036,0.527]
3405 [8.332,0.761]
3406 [11.727,0.941]
3407 [14.125,1.067]
3408 [15.675,1.149]
3409 [16.555,1.196]
3410 [16.911,1.214]
3411 [-1, -1] (max twenty pts)
3412 NHYDovf= ["KB-P3ovf"]
3413 *%
3414 ADD HYD NHYDsum= ["KB-Pond3"], NHYDs to add= ["KB-P3R"+ "KB-P3ovf"]
3415 *%
3416 SAVE HYD NHYD= ["KB-Pond3"], # OF PCYCLES=[-1], ICASEsh=[1]
3417 HYD_COMMENT= ["Total Flows at KB third pond"]
3418 *%
3419 *#*****
3420 *# EXISTING / PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118080), SWM
Modeling Approach, NOVATECH Report June, 2020)
3421 *# - TO FRASER-CLARKE DRAIN
3422 *#*****
3423 CONTINUOUS STANDHYD NHYD= ["FC-01"], DT=[1]min, AREA=[8.03](ha), XIMP=[0.47],
TIMP=[0.47], DWF=[0](cms), LOSS=[1]:
3424 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3425 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3426 Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%), LGI=[231.373](m),
MNI=[0.013], SCI=[0](min),
3427 Continuous simulation parameters:
3428 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3429 *%
3430 COMPUTE DUALHYD NHYDin= ["FC-01"], CINLET=[0.756](cms), NINLET=[1],
3431 MajNHYD= ["FC-01-MJ"]
3432 MinNHYD= ["FC-01-MN"]
3433 TMJSTO=[714](cu-m)
3434 *%
3435 ADD HYD NHYDsum= ["FC-01-S"], NHYDs to add= ["FC-01-MJ"+ "FC-01-MN"]
3436 *%
3437 CONTINUOUS STANDHYD NHYD= ["FC-02"], DT=[1]min, AREA=[16.05](ha), XIMP=[0.93],
TIMP=[0.93], DWF=[0](cms), LOSS=[1]:
3438 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3439 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3440 Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%), LGI=[327.109](m),
MNI=[0.013], SCI=[0](min),
3441 Continuous simulation parameters:
3442 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3443 *%
3444 COMPUTE DUALHYD NHYDin= ["FC-02"], CINLET=[1.159](cms), NINLET=[1],
3445 MajNHYD= ["FC-02-MJ"]
3446 MinNHYD= ["FC-02-MN"]
3447 TMJSTO=[2385](cu-m)
3448 *%
3449 ADD HYD NHYDsum= ["FC-02-S"], NHYDs to add= ["FC-02-MJ"+ "FC-02-MN"]
3450 *%
3451 CONTINUOUS STANDHYD NHYD= ["FC-03"], DT=[1]min, AREA=[7.37](ha), XIMP=[0.64],
TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3452 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3453 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),

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3454 MNP=[0.250], SCP=[0](min),
3455 Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
3456 LGI=[221.660](m), MNI=[0.013], SCI=[0](min),
3457 Continuous simulation parameters:
3458 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
3459 END=-1
3460
3461 *%-----|-----|
3462 COMPUTE DUALHYD NHYDin=[ "FC-03" ], CINLET=[ 0.358 ](cms), NINLET=[ 1 ],
3463 MajNHYD=[ "FC-03-MJ" ]
3464 MinNHYD=[ "FC-03-MN" ]
3465 TMJSTO=[ 1131 ](cu-m)
3466 *%-----|-----|
3467 ADD HYD NHYDsum=[ "FC-03-S" ], NHYDs to add=[ "FC-03-MJ" +"FC-03-MN" ]
3468 *%-----|-----|
3469 CONTINUOUS STANDHYD NHYD=[ "FC-04" ], DT=[ 1 ]min, AREA=[ 12.87 ](ha), XIMP=[ 0.64 ],
3470 TIMP=[ 0.64 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3471 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3472 F=[ 0.00 ](mm),
3473 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3474 MNP=[ 0.250 ], SCP=[ 0 ](min),
3475 Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 1.0 ](%),
3476 LGI=[ 292.916 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3477 Continuous simulation parameters:
3478 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3479 END=-1
3480 *%-----|-----|
3481 COMPUTE DUALHYD NHYDin=[ "FC-04" ], CINLET=[ 0.741 ](cms), NINLET=[ 1 ],
3482 MajNHYD=[ "FC-04-MJ" ]
3483 MinNHYD=[ "FC-04-MN" ]
3484 TMJSTO=[ 1794 ](cu-m)
3485 *%-----|-----|
3486 ADD HYD NHYDsum=[ "FC-04-S" ], NHYDs to add=[ "FC-04-MJ" +"FC-04-MN" ]
3487 *%-----|-----|
3488 *#***** PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118080), SWM Modeling
3489 Approach, NOVATECH Report June, 2020)
3490 *# - TO JOCK RIVER
3491 *#*****|-----|
3492 CONTINUOUS STANDHYD NHYD=[ "JR-01" ], DT=[ 1 ]min, AREA=[ 8.24 ](ha), XIMP=[ 0.64 ],
3493 TIMP=[ 0.64 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3494 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3495 F=[ 0.00 ](mm),
3496 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3497 MNP=[ 0.250 ], SCP=[ 0 ](min),
3498 Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 1.0 ](%),
3499 LGI=[ 234.379 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3500 Continuous simulation parameters:
3501 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3502 END=-1
3503 *%-----|-----|
3504 COMPUTE DUALHYD NHYDin=[ "JR-01" ], CINLET=[ 0.563 ](cms), NINLET=[ 1 ],
3505 MajNHYD=[ "JR-01-MJ" ]
3506 MinNHYD=[ "JR-01-MN" ]
3507 TMJSTO=[ 1040 ](cu-m)
3508 *%-----|-----|
3509 ADD HYD NHYDsum=[ "JR-01-S" ], NHYDs to add=[ "JR-01-MJ" +"JR-01-MN" ]
3510 *%-----|-----|
3511 CONTINUOUS STANDHYD NHYD=[ "JR-02" ], DT=[ 1 ]min, AREA=[ 1.59 ](ha), XIMP=[ 0.64 ],
3512 TIMP=[ 0.64 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3513 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3514 F=[ 0.00 ](mm),
3515 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3516 MNP=[ 0.250 ], SCP=[ 0 ](min),
3517 Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 1.0 ](%),
3518 LGI=[ 102.956 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3519 Continuous simulation parameters:

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3502                                     IaRECper=[4](hrs),  IaRECImp=[4](hrs),  InterEventTime=[12](hrs),
3503                                     END=-1
3504 *%-----| NHYDin=[ "JR-02" ],  CINLET=[ 0.153 ](cms),  NINLET=[ 1 ],
3504 COMPUTE DUALHYD   MajNHYD=[ "JR-02-MJ" ]
3505   MinNHYD=[ "JR-02-MN" ]
3506   TMJSTO=[ 153 ](cu-m)
3508 *%-----| ADD HYD          NHYDsum=[ "JR-02-S" ],  NHYDs to add=[ "JR-02-MJ" +"JR-02-MN" ]
3509 *%-----| ***** ****
3511 *#***** Catchment FRASER
3512   - To Fraser-Clarke drain (north of the Jock)
3513   - Developed land with assumed 43% imp.
3514   - 2020-12-17 Change Fraser area to be 35.1 as measured from QGIS
3515   - 2020-12-17 All Fraser is undeveloped (Nashyd)
3516 *#***** ****
3517 *#***** CONTINUOUS NASHYD  NHYD=[ "FRASER-DRN" ],  DT=[ 1 ]min,  AREA=[ 13.65 ](ha),
3518   DWF=[ 0 ](cms),  CN/C=[ 77 ],  IA=[ 4.67 ](mm),
3519   N=[ 3 ],  TP=[ 0.4258 ]hrs,
3520   Continuous simulation parameters:
3521     IaRECper=[ 4 ](hrs),
3522     SMIN=[ -1 ](mm),  SMAX=[ -1 ](mm),  SK=[ 0.010 ]/(mm),
3523     InterEventTime=[ 12 ](hrs)
3524   Baseflow simulation parameters:
3525     BaseFlowOption=[ 1 ],
3526     InitGWResVol=[ 50 ](mm),  GWResK=[ 0.96 ](mm/day/mm)
3527     VHdCond=[ 0.055 ](mm/hr),  END=-1
3528 *
3529 *
3530 *#***** CONTINUOUS STANDHYD NHYD=[ "FRASER-D" ],  DT=[ 1 ]min,  AREA=[ 21.61 ](ha),
3531   XIMP=[ 0.585 ],  TIMP=[ 0.585 ],  DWF=[ 0 ](cms),  LOSS=[ 2 ],
3532   SCS curve number CN=[ 80 ],
3533   Pervious surfaces:  IApert=[ 4.67 ](mm),  SLPP=[ 1 ](%),
3534     LGP=[ 40 ](m),  MNP=[ 0.25 ],  SCP=[ 0 ](min),
3535   Impervious surfaces:  IAimp=[ 1.57 ](mm),  SLPI=[ 1 ](%),
3536     LGI=[ 379.561 ](m),  MNI=[ 0.013 ],  SCI=[ 0 ](min),
3537   Continuous simulation parameters:
3538     IaRECper=[ 4 ](hrs),  IaRECImp=[ 4 ](hrs),
3539     SMIN=[ -1 ](mm),  SMAX=[ -1 ](mm),  SK=[ 0.010 ]/(mm),
3540     InterEventTime=[ 18 ](hrs),  END=-1
3541 *%-----| COMPUTE DUALHYD  NHYDin=[ "FRASER-D" ],  CINLET=[ 2.281 ](cms),  NINLET=[ 1 ],
3542   MajNHYD=[ "FRASER-J" ]
3543   MinNHYD=[ "FRASER-N" ]
3544   TMJSTO=[ 99999999 ](cu-m)
3545 *%-----| ADD HYD          NHYDsum=[ "FRASER-S" ],  NHYDs to add=[ "FRASER-J" +"FRASER-N" ]
3546 *%-----| ROUTE RESERVOIR NHYDout=[ "MS_P20" ],  NHYDin=[ "FRASER" ],
3547   RDT=[ 1 ](min),
3548   *
3549   *           TABLE of ( OUTFLOW-STORAGE ) values
3550   *           (cms) - (ha-m)
3551   *           [    0.0 ,  0.0 ]
3552   *           [    0.04 ,  0.36 ]
3553   *           [    -1 ,  -1 ] (max twenty pts)
3554   *
3555   *           NHYDovf=[ "P20-OVF" ]
3556   *
3557 *%-----| ADD HYD          NHYDsum=[ "4241" ],  NHYDs to
3558   add=[ "KB-Pond3" +"S-1-B" +"FRASER-DRN" +"FRASER-S" +"N_KB" +"FC-01-S" +"FC-02-S" +"FC-03-S" ]
3559 *%-----| SAVE HYD          NHYD=[ "4241" ],  # OF PCYCLES=[ -1 ],  ICASEsh=[ 1 ]
3560   HYD_COMMENT=[ "Total Flows at Ken-Burnett Outlet" ]
3561   *
3562   *
3563   *# Hydrograph from Node Ken-Burnett to station 3633
3564   *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4241
3565   *

```

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3566 ROUTE CHANNEL      NHYDout=[ "4241-out" ], NHYDin=[ "4241" ], RDT=[1](min),
3567 CHLGTH=[ 294 ](m), CHSLOPE=[ 0.1088 ](%), FPSLOPE=[ 0.1088 ](%),
3568 SECNUM=[ 1.0 ], NSEG=[ 3 ]
3569 ( SEGROUGH, SEGDIST (m) )=[ 0.05, -20.12
3570           -0.035, 45.26
3571           0.05, 403.84 ] NSEG times
3572 ( DISTANCE (m), ELEVATION (m) )=[ ]
3573 [-909.72, 95 ]
3574 [-907.09, 94.5 ]
3575 [-904.65, 94 ]
3576 [-902.26, 93.5 ]
3577 [-44.51, 91.5 ]
3578 [-25.1, 91.5 ]
3579 [-20.98, 91 ]
3580 [-20.61, 90.5 ]
3581 [-20.12, 90 ]
3582 [-6.13, 87.26 ]
3583 [17.51, 86.56 ]
3584 [31.37, 87.2 ]
3585 [45.26, 90 ]
3586 [50.41, 90.5 ]
3587 [63.06, 91 ]
3588 [134.5, 91.5 ]
3589 [190.63, 92 ]
3590 [251.98, 92.5 ]
3591 [321.32, 93.5 ]
3592 [403.84, 95 ]
3593 *%-----|-----|
3594 ADD HYD      NHYDsSum= [ "SN_KB" ], NHYDs to
3595 add= [ "4241-out "+ "FC-04-S" + "JR-01-S" + "JR-02-S" ]
3596 *%-----|-----|
3597 SAVE HYD      NHYD= [ "SN_KB" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
3598          HYD_COMMENT= [ "Total Flows before Station 3633" ]
3599 *%-----|-----|
3600 *# Hydrograph from Station 3633 to Node Todd
3601 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 3633
3602 *# JFSA 2021-02-26 change the channel length (at station 3633) from 650m to 608m and
3603 *# change the slope from 0.0498% to 0.24671%. That is because of adding station 4241
3604 *# between station 4534 and station 3633
3605 *#
3606 ROUTE CHANNEL      NHYDout=[ "N_TO" ], NHYDin=[ "SN_KB" ], RDT=[1](min),
3607 CHLGTH=[ 608 ](m), CHSLOPE=[ 0.24671 ](%), FPSLOPE=[ 0.24671 ](%),
3608 SECNUM=[ 1.0 ], NSEG=[ 3 ]
3609 ( SEGROUGH, SEGDIST (m) )=[ 0.05, -23.74
3610           -0.035, 23.74
3611           0.05, 26.50 ] NSEG times
3612 ( DISTANCE (m), ELEVATION (m) )=[ ]
3613 -29.24, 91.0
3614 -27.41, 90.5
3615 -25.64, 90
3616 -23.74, 89.5
3617 -22, 89.26
3618 -20, 88.51
3619 -19, 88.32
3620 -15, 88.1
3621 -10, 88.11
3622 -5, 88.17
3623 0, 88.27
3624 5, 88.19
3625 10, 88.06
3626 15, 88.48
3627 16, 88.7
3628 23.74, 89.5
3629 24.68, 90
3630 25.57, 90.5
3631 26.50, 91.0

```

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3629 *
3630 *
3631 *
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3640 *
3641 *
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3644 *
3645 *
3646 *
3647 *%-----|-----|
3648 *#*****
3649 *#      Catchment Greenbank
3650 *#      - To Greenbank Drain (south of the Jock)
3651 *#      - JFSA 2021-01-18 add Greenbank pond as per JFSA, P598(06)-15, June 2016
3652 *#      - JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GIS measurements
3653 *#*****
3654 CONTINUOUS STANDHYD NHYD=[ "Greenbank" ], DT=[1]min, AREA=[36.6](ha),
3655           XIMP=[0.639], TIMP=[0.682], DWF=[0](cms), LOSS=[2],
3656           SCS curve number CN=[77],
3657           Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3658           LGP=[40](m), MNP=[0.25], SCP=[0](min),
3659           Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3660           LGI=[493.96](m), MNI=[0.013], SCI=[0](min),
3661           Continuous simulation parameters:
3662           IaRECper=[4](hrs), IaRECImp=[4](hrs),
3663           SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3664           InterEventTime=[18](hrs), END=-1
3665 *%-----|-----|
3666 ROUTE RESERVOIR NHYDout=[ "GreenB_MN" ] ,NHYDin=[ "Greenbank" ] ,
3667           RDT=[1](min),
3668           TABLE of ( OUTFLOW-STORAGE ) values
3669           (cms) - (ha-m)
3670           [ 0.0 , 0.0 ]
3671           [ 0.033 , 0.084 ]
3672           [ 0.039 , 0.201 ]
3673           [ 0.113 , 0.292 ]
3674           [ 0.237 , 0.386 ]
3675           [ 0.382 , 0.484 ]
3676           [ 0.539 , 0.585 ]
3677           [ 0.7 , 0.692 ]
3678           [ 0.86 , 0.804 ]
3679           [ 4.684 , 0.922 ]
3680           [ 11.539 , 1.052 ]
3681           [ 20.867 , 1.168 ]
3682           [ 103.616 , 1.974 ]
3683           [ -1 , -1 ] (max twenty pts)
3684           NHYDovf=[ "GreenB_MJ" ] ,
3685 *%-----|-----|
3686 *%-----|-----|
3687 ADD HYD NHYDsum=[ "GreenB" ], NHYDs to add=[ "N_TO"+ "GreenB_MJ"+ "GreenB_MN" ]
3688 *%-----|-----|
3689 SAVE HYD NHYD=[ "GreenB" ], # OF PCYCLES=[-1], ICASEsh=[1]
3690           HYD_COMMENT=[ "Total Flows at Greenbank Drain" ]
3691 *%-----|-----|
3692 *#*****
3693 *#      Catchment TODD
3694 *#      - To Todd Drain (south of the Jock)

```

```

3695 *#      - Subdivision with 43% imp. as per Barrhaven South MSS
3696 *#      - 2020-11-30 increase imp. based on P598(04)-11
3697 *#      - 2020-11-30 update TODD Tributary Drainage Area to = 146.015 ha based on
P598(04)-11
3698 *#      - 2020-11-30 split TODD Drainage Area to MAJOR, MINOR, POND and ALL
3699 *#*****
3700 *#      - JFSA 2021-01-19 add "TODD_MN1" as part of Clarke("W_CLAR_MJ") and remove it
from Todd
3701 *CONTINUOUS STANDHYD NHYD=[ "TODD_MN1" ], DT=[1]min, AREA=[1.772](ha),
3702 *          XIMP=[ 0.53 ], TIMP=[ 0.57 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
3703 *          SCS curve number CN=[ 77 ],
3704 *          Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
3705 *          LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
3706 *          Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
3707 *          LGI=[ 108.689 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3708 *          Continuous simulation parameters:
3709 *          IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
3710 *          SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
3711 *          InterEventTime=[ 18 ](hrs), END=-1
3712 *%
3713 CONTINUOUS STANDHYD NHYD=[ "TODD_MN2" ], DT=[1]min, AREA=[ 2.1 ](ha),
3714 *          XIMP=[ 0.53 ], TIMP=[ 0.57 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
3715 *          SCS curve number CN=[ 77 ],
3716 *          Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
3717 *          LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
3718 *          Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
3719 *          LGI=[ 118.322 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3720 *          Continuous simulation parameters:
3721 *          IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
3722 *          SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
3723 *          InterEventTime=[ 18 ](hrs), END=-1
3724 *%
3725 CONTINUOUS STANDHYD NHYD=[ "TODD_MN3" ], DT=[1]min, AREA=[ 0.117 ](ha),
3726 *          XIMP=[ 0.53 ], TIMP=[ 0.57 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
3727 *          SCS curve number CN=[ 77 ],
3728 *          Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
3729 *          LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
3730 *          Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
3731 *          LGI=[ 27.928 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3732 *          Continuous simulation parameters:
3733 *          IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
3734 *          SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
3735 *          InterEventTime=[ 18 ](hrs), END=-1
3736 *%
3737 CONTINUOUS STANDHYD NHYD=[ "TODD_MJ" ], DT=[1]min, AREA=[ 30.230 ](ha),
3738 *          XIMP=[ 0.52 ], TIMP=[ 0.64 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
3739 *          SCS curve number CN=[ 77 ],
3740 *          Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
3741 *          LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
3742 *          Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
3743 *          LGI=[ 448.925 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3744 *          Continuous simulation parameters:
3745 *          IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
3746 *          SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
3747 *          InterEventTime=[ 18 ](hrs), END=-1
3748 *%
3749 *      -JFSA, 2021-01-19 update "TODD_ALL" area from 108.741 ha to 112.908 ha based on
GIS measurements (148.41-30.23-0.117-2.1-3.055=112.908 ha)
3750 CONTINUOUS STANDHYD NHYD=[ "TODD_ALL" ], DT=[1]min, AREA=[ 112.908 ](ha),
3751 *          XIMP=[ 0.52 ], TIMP=[ 0.57 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
3752 *          SCS curve number CN=[ 77 ],
3753 *          Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
3754 *          LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
3755 *          Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
3756 *          LGI=[ 867.594 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3757 *          Continuous simulation parameters:

```

```

3758
3759
3760
3761 *%-----|-----|-----|-----|-----|-----|-----|
3762 CONTINUOUS STANDHYD NHYD=[ "TODD_P" ], DT=[1]min, AREA=[3.055](ha),
3763 XIMP=[0.63], TIMP=[0.63], DWF=[0](cms), LOSS=[2],
3764 SCS curve number CN=[77],
3765 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3766 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3767 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3768 LGI=[142.712](m), MNI=[0.013], SCI=[0](min),
3769 Continuous simulation parameters:
3770 IARECper=[4](hrs), IaRECimp=[4](hrs),
3771 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3772 InterEventTime=[18](hrs), END=-1
3773 *%-----|-----|-----|-----|-----|-----|-----|
3774 *%-----|-----|-----|-----|-----|-----|-----|
3775 * -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"
and its parameters remain the same.
3776 *CONTINUOUS STANDHYD NHYD=[ "TODD_DEVL" ], DT=[1]min, AREA=[15.87](ha),
3777 *
3778 *
3779 *
3780 *
3781 *
3782 *
3783 *
3784 *
3785 *
3786 *
3787 *%-----|-----|-----|-----|-----|-----|-----|
3788 * -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
is called "corr2" and its parameters remain the same.
3789 *CONTINUOUS NASHYD NHYD=[ "TODD_UnD" ], DT=[1]min, AREA=[12.47](ha),
3790 *
3791 *
3792 *
3793 *
3794 *
3795 *
3796 *
3797 *
3798 *
3799 *
3800 *# 5-Year + 12% Capture
3801 *COMPUTE DUALHYD NHYDin=[ "TODD_MJ" ], CINLET=[3.314](cms), NINLET=[1],
3802 *
3803 MajNHYD=[ "TODD_MJj" ]
3804 *
3805 MinNHYD=[ "TODD_MJn" ]
3806 TMJSTO=[0.1](cu-m)
3807 ROUTE RESERVOIR NHYDout=[ "TODD_MJn" ] , NHYDin=[ "TODD_MJ" ] ,
3808 RDT=[1](min),
3809 TABLE of ( OUTFLOW-STORAGE ) values
3810 (cms) - (ha-m)
3811 [ 0.0 , 0.0 ]
3812 [ 3.314 , 0.0001 ]
3813 [ -1 , -1 ] (max twenty pts)
3814 NHYDovf=[ "TODD_MJj" ] ,
3815 *# 5-Year + 12% Capture
3816 *COMPUTE DUALHYD NHYDin=[ "TODD_MN1" ], CINLET=[0.227](cms), NINLET=[1],
3817 *
3818 MajNHYD=[ "TODD_MN1j" ]
3819 MinNHYD=[ "TODD_MN1n" ]
3820 *ROUTE RESERVOIR NHYDout=[ "TODD_MN1n" ] , NHYDin=[ "TODD_MN1" ] ,

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3821 * RDT=[1](min),
3822 * TABLE of ( OUTFLOW-STORAGE ) values
3823 * (cms) - (ha-m)
3824 * [ 0.0 , 0.0 ]
3825 * [ 0.227 , 0.0001 ]
3826 * [ -1 , -1 ] (max twenty pts)
3827 * NHYDovf= [ "TODD_MN1j" ] ,
3828 *%-----|-----|
3829 *COMPUTE DUALHYD NHYDin= [ "TODD_MN2" ], CINLET=[0.268](cms), NINLET=[1],
3830 * MajNHYD= [ "TODD_MN2j" ]
3831 * MinNHYD= [ "TODD_MN2n" ]
3832 * TMJSTO=[0.1](cu-m)
3833 ROUTE RESERVOIR NHYDout= [ "TODD_MN2n" ] , NHYDin= [ "TODD_MN2" ] ,
3834 RDT=[1](min),
3835 TABLE of ( OUTFLOW-STORAGE ) values
3836 (cms) - (ha-m)
3837 [ 0.0 , 0.0 ]
3838 [ 0.268 , 0.0001 ]
3839 [ -1 , -1 ] (max twenty pts)
3840 NHYDovf= [ "TODD_MN2j" ] ,
3841 *%-----|-----|
3842 *COMPUTE DUALHYD NHYDin= [ "TODD_MN3" ], CINLET=[0.016](cms), NINLET=[1],
3843 * MajNHYD= [ "TODD_MN3j" ]
3844 * MinNHYD= [ "TODD_MN3n" ]
3845 * TMJSTO=[0.1](cu-m)
3846 ROUTE RESERVOIR NHYDout= [ "TODD_MN3n" ] , NHYDin= [ "TODD_MN3" ] ,
3847 RDT=[1](min),
3848 TABLE of ( OUTFLOW-STORAGE ) values
3849 (cms) - (ha-m)
3850 [ 0.0 , 0.0 ]
3851 [ 0.016 , 0.0001 ]
3852 [ -1 , -1 ] (max twenty pts)
3853 NHYDovf= [ "TODD_MN3j" ] ,
3854 *%-----|-----|
3855 * -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
major system from A2 can be added to Todd
3856 CONTINUOUS STANDHYD NHYD= [ "A2" ], DT=[1]min, AREA=[25.5](ha),
3857 XIMP=[0.42], TIMP=[0.52], DWF=[0](cms), LOSS=[2],
3858 SCS curve number CN=[75],
3859 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3860 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3861 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3862 LGI=[566](m), MNI=[0.013], SCI=[0](min),
3863 Continuous simulation parameters:
3864 IaRECper=[4](hrs), IaRECImp=[4](hrs),
3865 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3866 InterEventTime=[18](hrs), END=-1
3867 *%-----|-----|
3868 COMPUTE DUALHYD NHYDin= [ "A2" ], CINLET=[1.818](cms), NINLET=[1],
3869 MajNHYD= [ "A2-MJ" ]
3870 MinNHYD= [ "A2-MN" ]
3871 TMJSTO=[924](cu-m)
3872 *%-----|-----|
3873 ADD HYD NHYDsum= [ "TODD" ], NHYDs to
add= [ "TODD_MN2n" + "TODD_MN3n" + "TODD_MJj" + "TODD_P" + "TODD_ALL" + "W_CLAR_MJn" ]
3874 *%-----|-----|
3875 SAVE HYD NHYD= [ "TODD" ], # OF PCYCLES=[-1], ICASEsh=[1]
HYD_COMMENT= [ "Total Flows at Todd Drain" ]
3876 *%-----|-----|
3877 *#*****#
3878 *# Todd Pond 3
3879 *# - Rating curve obtained from Barrhaven South MSS modeling
3880 *# - stantec 2007, Tributary Drainage Area to MSS Pond 3 = 193 ha
3881 *#*****#
3882 ROUTE RESERVOIR NHYDout= [ "MS_P3" ], NHYDin= [ "TODD" ],
3883 RDT=[1](min),
3884

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3885 TABLE of ( OUTFLOW-STORAGE ) values
3886           (cms) - (ha-m)
3887           [ 0.0 , 0.0 ]
3888           [ 0.014 , 0.155 ]
3889           [ 0.048 , 0.394 ]
3890           [ 0.061 , 0.56 ]
3891           [ 0.08 , 0.909 ]
3892           [ 0.088 , 1.089 ]
3893           [ 0.109 , 1.652 ]
3894           [ 0.118 , 1.952 ]
3895           [ 0.122 , 2.099 ]
3896           [ 1.972 , 2.269 ]
3897           [ 9.135 , 2.598 ]
3898           [ 15.608 , 2.826 ]
3899           [ 19.256 , 2.942 ]
3900           [ 27.282 , 3.181 ]
3901           [ 40.957 , 3.55 ]
3902           [ 56.372 , 3.929 ]
3903           [ 73.349 , 4.317 ]
3904           [ 85.469 , 4.579 ]
3905           [ 104.771 , 4.977 ]
3906           [ -1 , -1 ] (max twenty pts)
3907
3908 *%-----|-----|
3909 ADD HYD          NHYDsum= [ "SN_TO" ] , NHYDs to
3910 add=[ "GreenB" +"MS_P3" +"P3-OVF" +"TODD_MN2j" +"A2-MJ" ]
3911 *%-----|-----|
3912 SAVE HYD          NHYD= [ "SN_TO" ] , # OF PCYCLES=[-1] , ICASEsh=[1]
3913                         HYD_COMMENT=[ "Total Flows at Todd Drain" ]
3914 *%-----|-----|
3915 *# Hydrograph from Todd Drain routed to Corrigan Drain
3916 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
3917 *# 2021-02-19 Change the slope from 0.033 % (as per Stantec Report 2007) to 0.05 % so
3918 the model will be more stable and give reasonable results. It is justifiable as ROUTE
3919 CHANNELs aren't well suited to really flat slopes.
3920 *
3921 ROUTE CHANNEL      NHYDout= [ "N_TO" ] , NHYDin= [ "SN_TO" ] ,
3922             RDT=[1](min),
3923             CHLGTH=[280](m), CHSLOPE=[0.05](%),
3924                         FPSLOPE=[0.05](%),
3925             SECNUM=[1.0], NSEG=[3]
3926             ( SEGROUGH, SEGDIST (m))=
3927                 [0.075,-17.72
3928                   -0.045,17.72
3929                     0.075,80.62] NSEG times
3930             ( DISTANCE (m), ELEVATION (m))=
3931                 [-83.32, 90.00]
3932                 [-81.36, 89.50]
3933                 [-79.12, 89.00]
3934                 [-76.13, 88.50]
3935                 [-20.46, 88.00]
3936                 [-19.36, 87.50]
3937                 [-18.51, 87.00]
3938                 [-17.72, 86.50]
3939                 [-11.95, 85.24]
3940                 [-0.11, 85.12]
3941                 [11.49, 85.20]
3942                 [17.72, 86.50]
3943                 [19.74, 87.00]
3944                 [21.22, 87.50]
3945                 [22.68, 88.00]
3946                 [24.28, 88.50]
3947                 [26.79, 89.00]
3948                 [71.98, 90.00]
3949                 [80.62, 90.50]

```

```

3948 *%-----|-----|
3949 SAVE HYD          NHYD=[ "N_TO" ],    # OF PCYCLES=[-1],  ICASEsh=[1]
3950             HYD_COMMENT=[ "Total inflows at Station 2462" ]
3951 *%-----|-----|
3952 *#*****|-----|
3953 *#   Catchment CORRIG
3954 *#   - To Corrigan Drain (south of the Jock)
3955 *#   - Primarily Developed (medium density)
3956 *#   - JFSA JAN 2021, add Corrigan subcatchments as per IBI, July 2008
3957 *#*****|-----|
3958 ROUTE RESERVOIR  NHYDout=[ "MS_P1" ],  NHYDin=[ "CORRIG" ],
3959 *
3960 *           RDT=[1](min),
3961 *           TABLE of ( OUTFLOW-STORAGE ) values
3962 *           (cms) - (ha-m)
3963 *           [ 0.0 , 0.0 ]
3964 *           [ 0.06 , 0.58 ]
3965 *           [ -1 , -1 ] (max twenty pts)
3966 *           NHYDovf=[ "P1-OVF" ]
3967 *%-----|-----|
3968 ADD HYD          NHYDsum=[ "SN_CO" ],  NHYDs to add=[ "N_TO"+"P1-OVF"+"MS_P1" ]
3969 *%-----|-----|
3970 SAVE HYD          NHYD=[ "SN_CO" ],    # OF PCYCLES=[-1],  ICASEsh=[1]
3971 *           HYD_COMMENT=[ "Total Flows at Corrigan Drain" ]
3972 *%-----|-----|
3973 *           -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
3974 drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"
3975 and its parameters remain the same.
3976 CONTINUOUS STANDHYD NHYD=[ "corr1" ], DT=[1]min, AREA=[15.87](ha),
3977             XIMP=[0.63], TIMP=[0.63], DWF=[0](cms), LOSS=[2],
3978             SCS curve number CN=[77],
3979             Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3980             LGP=[40](m), MNP=[0.25], SCP=[0](min),
3981             Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3982             LGI=[325.27](m), MNI=[0.013], SCI=[0](min),
3983             Continuous simulation parameters:
3984             IaRECper=[4](hrs), IaRECImp=[4](hrs),
3985             SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3986             InterEventTime=[18](hrs), END=-1
3987 *%-----|-----|
3988 *           -JFSA 2021-02-23 add DUALHYD for "corr1". "corr1" DUALHYD Parameters are the
3989 same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to "corr1".
3990 *           At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for
3991 A1-Corrig
3992 COMPUTE DUALHYD  NHYDin=[ "corr1" ], CINLET=[1.818](cms), NINLET=[1],
3993             MajNHYD=[ "corr1-MJ" ]
3994             MinNHYD=[ "corr1-MN" ]
3995             TMJSTO=[924](cu-m)
3996 *%-----|-----|
3997 *           -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
3998 is called "corr2" and its parameters remain the same.
3999 CONTINUOUS NASHYD NHYD=[ "corr2" ], DT=[1]min, AREA=[12.47](ha),
4000             DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
4001             N=[3], TP=[1.10]hrs,
4002             Continuous simulation parameters:
4003             IaRECper=[4](hrs),
4004             SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4005             InterEventTime=[12](hrs)
4006             Baseflow simulation parameters:
4007             BaseFlowOption=[1] ,
4008             InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4009             VHdydCond=[0.055](mm/hr), END=-1
4010 *%-----|-----|
4011 *           -JFSA 2021-01-19 change A1-Corrig to be developed as per geoottawa website and
4012 apply the parameters of A2, the nearest sub-catchment to A1-Corrig, LGI is calculated
4013 based on A1-Corrig area
4014 *           -JFSA 2021-01-19 update all Corrigan areas based on GIS measurements, and keep

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LGI as it is from Corrigan Report, IBI Group, 2008 because LGI calculated is less than LGI from the Corrigan Report

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4018 \*  
4019 \* -JFSA 2021-01-25 add DUALHYD for A1-Corrig. A1-Corrig DUALHYD Parameters are the same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to A1-Corrig.  
4020 \* At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for A1-Corrig  
4021 **COMPUTE DUALHYD** NHYDin=[ "A1-Corrig" ], CINLET=[ 1.818 ](cms), NINLET=[ 1 ],  
4022 MajNHYD=[ "A1-MJ" ]  
4023 MinNHYD=[ "A1-MN" ]  
4024 TMJSTO=[ 924 ](cu-m)  
4025 \*%-----|-----|  
4026 \*CONTINUOUS NASHYD NHYD=[ "A1-Corrig" ], DT=[ 1 ]min, AREA=[ 15.75 ](ha),  
4027 \* DWF=[ 0 ](cms), CN/C=[ 66 ], IA=[ 2.5 ](mm),  
4028 \* N=[ 3.0 ], TP=[ 0.36 ]hrs,  
4029 \* Continuous simulation parameters:  
4030 \* IaRECper=[ 4 ](hrs),  
4031 \* SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),  
4032 \* InterEventTime=[ 12 ](hrs)  
4033 \* Baseflow simulation parameters:  
4034 \* BaseFlowOption=[ 1 ],  
4035 \* InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)  
4036 \* VHdCond=[ 0.055 ](mm/hr), END=-1  
4037 \*%-----|-----|  
4038 **CONTINUOUS NASHYD** NHYD=[ "B1" ], DT=[ 1 ]min, AREA=[ 2.77 ](ha),  
4039 DWF=[ 0 ](cms), CN/C=[ 56 ], IA=[ 2.5 ](mm),  
4040 N=[ 3.0 ], TP=[ 0.23 ]hrs,  
4041 Continuous simulation parameters:  
4042 IaRECper=[ 4 ](hrs),  
4043 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),  
4044 InterEventTime=[ 12 ](hrs)  
4045 Baseflow simulation parameters:  
4046 BaseFlowOption=[ 1 ],  
4047 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)  
4048 VHdCond=[ 0.055 ](mm/hr), END=-1  
4049 \*%-----|-----|  
4050 **CONTINUOUS STANDHYD** NHYD=[ "A4" ], DT=[ 1 ]min, AREA=[ 1.27 ](ha),  
4051 XIMP=[ 0.65 ], TIMP=[ 0.65 ], DWF=[ 0 ](cms), LOSS=[ 2 ],  
4052 SCS curve number CN=[ 75 ],  
4053 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),  
4054 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),  
4055 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),  
4056 LGI=[ 253 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),  
4057 Continuous simulation parameters:  
4058 IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),  
4059 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),  
4060 InterEventTime=[ 18 ](hrs), END=-1  
4061 \*%-----|-----|  
4062 **COMPUTE DUALHYD** NHYDin=[ "A4" ], CINLET=[ 0.405 ](cms), NINLET=[ 1 ],  
4063 MajNHYD=[ "A4-MJ" ]  
4064 MinNHYD=[ "A4-MN" ]  
4065 TMJSTO=[ 68 ](cu-m)  
4066 \*%-----|-----|  
4067 **ADD HYD** NHYDsum=[ "MH101" ], NHYDs to  
add=[ "A1-MJ" +"A1-MN" +"corr1-MJ" +"corr1-MN" +"corr2" +"B1" +"A4-MN" ]

```

4068 *%
4069 SAVE HYD NHYD=[ "MH101" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4070 HYD_COMMENT=[ "Total Flows at MH101" ]
4071 *%
4072 ROUTE PIPE PTTYPE=[ 1 ]circ, NHYDout=[ "101-102" ], RNUMBER=[ 1.0 ], PDIAM=[ 1050 ](mm),
4073 PLNGTH=[ 368 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0054 ](m/m),
4074 NHYDin=[ "MH101" ], RDT=[ 1 ]
4075 *%
4076 * -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
4077 major system from A2 can be added to Todd
4078 *CONTINUOUS STANDHYD NHYD=[ "A2" ], DT=[ 1 ]min, AREA=[ 25.5 ](ha),
4079 * XIMP=[ 0.42 ], TIMP=[ 0.52 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4080 * SCS curve number CN=[ 75 ],
4081 * Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4082 * LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4083 * Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4084 * LGI=[ 566 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4085 * Continuous simulation parameters:
4086 * IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
4087 * SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4088 * InterEventTime=[ 18 ](hrs), END=-1
4089 *%
4090 *COMPUTE DUALHYD NHYDin=[ "A2" ], CINLET=[ 1.818 ](cms), NINLET=[ 1 ],
4091 * MajNHYD=[ "A2-MJ" ]
4092 * MinNHYD=[ "A2-MN" ]
4093 * TMJSTO=[ 924 ](cu-m)
4094 *%
4095 ADD HYD NHYDssum[ "MH102" ], NHYDs to add=[ "A2-MN"+ "101-102" ]
4096 *%
4097 SAVE HYD NHYD=[ "MH102" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4098 HYD_COMMENT=[ "Total Flows at MH102" ]
4099 *%
4100 *CONTINUOUS STANDHYD NHYD=[ "A5" ], DT=[ 1 ]min, AREA=[ 1.6 ](ha),
4101 * XIMP=[ 0.71 ], TIMP=[ 0.71 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4102 * SCS curve number CN=[ 75 ],
4103 * Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4104 * LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4105 * Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4106 * LGI=[ 300 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4107 * Continuous simulation parameters:
4108 * IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
4109 * SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4110 * InterEventTime=[ 18 ](hrs), END=-1
4111 *%
4112 ADD HYD NHYDssum[ "A5T" ], NHYDs to add=[ "A4-MJ"+ "A5" ]
4113 *%
4114 COMPUTE DUALHYD NHYDin=[ "A5T" ], CINLET=[ 0.357 ](cms), NINLET=[ 1 ],
4115 * MajNHYD=[ "A5-MJ" ]
4116 * MinNHYD=[ "A5-MN" ]
4117 * TMJSTO=[ 60 ](cu-m)
4118 *%
4119 * -JFSA Jan. 2021, A3 is a part of Todd so it is removed
4120 * -JFSA Jan. 2021, "A2-MJ" added to "Todd"
4121 *CONTINUOUS STANDHYD NHYD=[ "A3" ], DT=[ 1 ]min, AREA=[ 18.4 ](ha),
4122 * XIMP=[ 0.58 ], TIMP=[ 0.65 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4123 * SCS curve number CN=[ 75 ],
4124 * Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4125 * LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4126 * Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4127 * LGI=[ 450 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4128 * Continuous simulation parameters:
4129 * IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
4130 * SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4131 * InterEventTime=[ 18 ](hrs), END=-1
4132 *%
4133 *ADD HYD NHYDssum[ "A3-A2MJ" ], NHYDs to add=[ "A2-MJ"+ "A3" ]

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4132 *%-----|-----|
4133 *COMPUTE DUALHYD NHYDin=[ "A3-A2MJ" ], CINLET=[ 2.208 ](cms), NINLET=[ 1 ],
4134 * MajNHYD=[ "A3R-MJ" ]
4135 * MinNHYD=[ "A3R-MN" ]
4136 * TMJSTO=[ 908 ](cu-m)
4137 *%-----|-----|
4138 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout=[ "102-103" ], RNUMBER=[ 1.0 ], PDIAM=[ 1500 ](mm),
4139 PLNGTH=[ 504 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0028 ](m/m),
4140 NHYDin=[ "MH102" ], RDT=[ 1 ]
4141 *%-----|-----|
4142 ADD HYD NHYDsum=[ "MH103" ], NHYDs to add=[ "102-103" +"A5-MN" ]
4143 *%-----|-----|
4144 SAVE HYD NHYD=[ "MH103" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4145 HYD_COMMENT=[ "Total Flows at MH103" ]
4146 *%-----|-----|
4147 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout=[ "103-104" ], RNUMBER=[ 1.0 ], PDIAM=[ 1650 ](mm),
4148 PLNGTH=[ 438 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0046 ](m/m),
4149 NHYDin=[ "MH103" ], RDT=[ 1 ]
4150 *%-----|-----|
4151 CONTINUOUS STANDHYD NHYD=[ "A6" ], DT=[ 1 ]min, AREA=[ 1.56 ](ha),
4152 XIMP=[ 0.71 ], TIMP=[ 0.71 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4153 SCS curve number CN=[ 75 ],
4154 Previous surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4155 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4156 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4157 LGI=[ 280 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4158 Continuous simulation parameters:
4159 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4160 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4161 InterEventTime=[ 18 ](hrs), END=-1
4162 *%-----|-----|
4163 ADD HYD NHYDsum=[ "A6T" ], NHYDs to add=[ "A5-MJ" +"A6" ]
4164 *%-----|-----|
4165 COMPUTE DUALHYD NHYDin=[ "A6T" ], CINLET=[ 0.357 ](cms), NINLET=[ 1 ],
4166 MajNHYD=[ "A6-MJ" ]
4167 MinNHYD=[ "A6-MN" ]
4168 TMJSTO=[ 60 ](cu-m)
4169 * -JFSA Jan. 2021, A7-corrig is a part of Todd so it is removed
4170 *CONTINUOUS STANDHYD NHYD=[ "A7-corrig" ], DT=[ 1 ]min, AREA=[ 11.8 ](ha),
4171 * XIMP=[ 0.41 ], TIMP=[ 0.54 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4172 * SCS curve number CN=[ 75 ],
4173 * Previous surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4174 * LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4175 * Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4176 * LGI=[ 438 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4177 * Continuous simulation parameters:
4178 * IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4179 * SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4180 * InterEventTime=[ 18 ](hrs), END=-1
4181 *%-----|-----|
4182 *ADD HYD NHYDsum=[ "A7-A3RMJ" ], NHYDs to add=[ "A3R-MJ" +"A7-corrig" ]
4183 *%-----|-----|
4184 *COMPUTE DUALHYD NHYDin=[ "A7-A3RMJ" ], CINLET=[ 1.003 ](cms), NINLET=[ 1 ],
4185 * MajNHYD=[ "A7R-MJ" ]
4186 * MinNHYD=[ "A7R-MN" ]
4187 * TMJSTO=[ 496 ](cu-m)
4188 *%-----|-----|
4189 ADD HYD NHYDsum=[ "MH104" ], NHYDs to add=[ "A6-MN" +"103-104" +"TODD_MJn" ]
4190 *%-----|-----|
4191 SAVE HYD NHYD=[ "MH104" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4192 HYD_COMMENT=[ "Total Flows at MH104" ]
4193 *%-----|-----|
4194 CONTINUOUS STANDHYD NHYD=[ "B2" ], DT=[ 1 ]min, AREA=[ 12.31 ](ha),
4195 XIMP=[ 0.41 ], TIMP=[ 0.54 ], DWF=[ 0 ](cms), LOSS=[ 2 ],

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4196 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),  

4197 LGP=[40](m), MNP=[0.25], SCP=[0](min),  

4198 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),  

4199 LGI=[417](m), MNI=[0.013], SCI=[0](min),  

4200 Continuous simulation parameters:  

4201 IARECper=[4](hrs), IARECimp=[4](hrs),  

4202 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),  

4203 InterEventTime=[18](hrs), END=-1  

4204 *%-----|  

4205 COMPUTE DUALHYD NHYDin=[ "B2" ], CINLET=[1.029](cms), NINLET=[1],  

4206 MajNHYD=[ "B2-MJ" ]  

4207 MinNHYD=[ "B2-MN" ]  

4208 TMJSTO=[ 508 ](cu-m)  

4209 *%-----|  

4210 ROUTE PIPE PTYPE=[1]circ, NHYDout=[ "315-333" ], RNUMBER=[1.0], PDIAM=[1200](mm),  

4211 PLNGTH=[ 254 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m),  

4212 NHYDin=[ "B2-MN" ], RDT=[ 1 ]  

4213 *%-----|  

4214 CONTINUOUS STANDHYD NHYD=[ "B3" ], DT=[ 1 ]min, AREA=[ 5.59 ](ha),  

4215 XIMP=[ 0.41 ], TIMP=[ 0.54 ], DWF=[ 0 ](cms), LOSS=[ 2 ],  

4216 SCS curve number CN=[ 75 ],  

4217 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),  

4218 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),  

4219 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),  

4220 LGI=[ 345 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),  

4221 Continuous simulation parameters:  

4222 IARECper=[ 4 ](hrs), IARECimp=[ 4 ](hrs),  

4223 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),  

4224 InterEventTime=[ 18 ](hrs), END=-1  

4225 *%-----|  

4226 COMPUTE DUALHYD NHYDin=[ "B3" ], CINLET=[ 0.459 ](cms), NINLET=[ 1 ],  

4227 MajNHYD=[ "B3-MJ" ]  

4228 MinNHYD=[ "B3-MN" ]  

4229 TMJSTO=[ 227 ](cu-m)  

4230 *%-----|  

4231 ADD HYD NHYDsum=[ "MH333" ], NHYDs to add=[ "B3-MN"+ "315-333" ]  

4232 *%-----|  

4233 SAVE HYD NHYD=[ "MH333" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]  

4234 HYD_COMMENT=[ "Total Flows at MH333" ]  

4235 *%-----|  

4236 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout=[ "333-335" ], RNUMBER=[ 1.0 ], PDIAM=[ 1200 ](mm),  

4237 PLNGTH=[ 251 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m),  

4238 NHYDin=[ "MH333" ], RDT=[ 1 ]  

4239 *%-----|  

4240 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout=[ "335-338" ], RNUMBER=[ 1.0 ], PDIAM=[ 1200 ](mm),  

4241 PLNGTH=[ 185 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m),  

4242 NHYDin=[ "333-335" ], RDT=[ 1 ]  

4243 *%-----|  

4244 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout=[ "338-340" ], RNUMBER=[ 1.0 ], PDIAM=[ 1350 ](mm),  

4245 PLNGTH=[ 233 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m),  

4246 NHYDin=[ "335-338" ], RDT=[ 1 ]  

4247 *%-----|  

4248 CONTINUOUS STANDHYD NHYD=[ "B4" ], DT=[ 1 ]min, AREA=[ 7.6 ](ha),  

4249 XIMP=[ 0.41 ], TIMP=[ 0.54 ], DWF=[ 0 ](cms), LOSS=[ 2 ],  

4250 SCS curve number CN=[ 75 ],  

4251 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),  

4252 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),  

4253 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),  

4254 LGI=[ 388 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),  

4255 Continuous simulation parameters:  

4256 IARECper=[ 4 ](hrs), IARECimp=[ 4 ](hrs),  

4257 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),  

4258 InterEventTime=[ 18 ](hrs), END=-1  

4259 *%-----|  

4260 COMPUTE DUALHYD NHYDin=[ "B4" ], CINLET=[ 0.655 ](cms), NINLET=[ 1 ],  

4261 MajNHYD=[ "B4-MJ" ]

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4258 MinNHYD=[ "B4-MN" ]
4259 TMJSTO=[ 323 ](cu-m)
4260 *%
4261 ADD HYD NHYDs[ "MH340" ], NHYDs to add=[ "338-340"+"B4-MN" ]
4262 *%
4263 SAVE HYD NHYD=[ "MH340" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4264 HYD_COMMENT=[ "Total Flows at MH340" ]
4265 *%
4266 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout=[ "340-104" ], RNUMBER=[ 1.0 ], PDIAM=[ 1650 ](mm),
4267 PLNGTH=[ 240 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0015 ](m/m),
4268 NHYDin=[ "MH340" ], RDT=[ 1 ]
4269 *%
4270 ADD HYD NHYDs[ "MH104T" ], NHYDs to add=[ "340-104"+"MH104" ]
4271 *%
4272 ROUTE PIPE PTYPE=[ 2 ]rect, NHYDout=[ "104-105" ], RNUMBER=[ 1.0 ],
4273 PWIDTH=[ 2400 ](mm) by PHEIGHT=[ 2100 ](mm),
4274 PLNGTH=[ 380 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m),
4275 NHYDin=[ "MH104T" ], RDT=[ 1 ]
4276 *%
4277 CONTINUOUS STANDHYD NHYD=[ "B5" ], DT=[ 1 ]min, AREA=[ 2.2 ](ha),
4278 XIMP=[ 0.57 ], TIMP=[ 0.57 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4279 SCS curve number CN=[ 75 ],
4280 Previous surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4281 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4282 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4283 LGI=[ 187 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4284 Continuous simulation parameters:
4285 IARECper=[ 4 ](hrs), IARECimp=[ 4 ](hrs),
4286 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4287 InterEventTime=[ 18 ](hrs), END=-1
4288 *%
4289 COMPUTE DUALHYD NHYDin=[ "B5" ], CINLET=[ 0.260 ](cms), NINLET=[ 1 ],
4290 MajNHYD=[ "B5-MJ" ]
4291 MinNHYD=[ "B5-MN" ]
4292 TMJSTO=[ 250 ](cu-m)
4293 *%
4294 CONTINUOUS STANDHYD NHYD=[ "A8" ], DT=[ 1 ]min, AREA=[ 0.96 ](ha),
4295 XIMP=[ 0.71 ], TIMP=[ 0.71 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4296 SCS curve number CN=[ 75 ],
4297 Previous surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4298 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4299 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4300 LGI=[ 186 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4301 Continuous simulation parameters:
4302 IARECper=[ 4 ](hrs), IARECimp=[ 4 ](hrs),
4303 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4304 InterEventTime=[ 18 ](hrs), END=-1
4305 *%
4306 ADD HYD NHYDs[ "A8T" ], NHYDs to add=[ "A6-MJ"+"A8" ]
4307 *%
4308 COMPUTE DUALHYD NHYDin=[ "A8T" ], CINLET=[ 0.238 ](cms), NINLET=[ 1 ],
4309 MajNHYD=[ "A8-MJ" ]
4310 MinNHYD=[ "A8-MN" ]
4311 TMJSTO=[ 40 ](cu-m)
4312 *%
4313 ADD HYD NHYDs[ "MH105" ], NHYDs to
4314 add=[ "104-105"+"B5-MN"+"A8-MN"+"TODD_MN3j" ]
4315 *%
4316 SAVE HYD NHYD=[ "MH105" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4317 HYD_COMMENT=[ "Total Flows at MH105" ]
4318 *%
4319 DIVERT HYD NHYDin=[ "A8-MJ" ] NIDout=[ 2 ]max five,
4320 outflow hydrographs (NHYDs)=["A8-MJ-JR" "A8-MJ-B6"]
4321 flow distribution table: (modify as necessary)
4322 Note: all flows are in (cms)

```

```

4319          QIDi + QIDii = QTOTAL
4320          [ 0 + 0 = 0 ]
4321          [ 50 + 50 = 100 ] end
4322 *%-----|-----|
4323 DIVERT HYD      NHYDin=[ "MH105" ] NIDout=[ 2 ]max five,
4324          outflow hydrographs (NHYDs)=["MH105-JR" "MH105-B6"]
4325          flow distribution table: (modify as necessary)
4326          Note: all flows are in (cms)
4327          QIDi + QIDii = QTOTAL
4328          [ 0 + 0 = 0 ]
4329          [ 0 + 3.0 = 3.0 ]
4330          [ 96.9+ 3.1 = 100 ] end
4331 *%-----|-----|
4332 CONTINUOUS STANDHYD NHYD=[ "B7" ], DT=[ 1 ]min, AREA=[ 7.19 ](ha),
4333          XIMP=[ 0.41 ], TIMP=[ 0.54 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4334          SCS curve number CN=[ 75 ],
4335          Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4336          LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4337          Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4338          LGI=[ 211 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4339          Continuous simulation parameters:
4340          IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4341          SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4342          InterEventTime=[ 18 ](hrs), END=-1
4343 *%-----|-----|
4344 ADD HYD      NHYDsum=[ "B7-B4MJ" ], NHYDs to add=[ "B4-MJ" +"B7" ]
4345 *%-----|-----|
4346 COMPUTE DUALHYD NHYDin=[ "B7-B4MJ" ], CINLET=[ 0.629 ](cms), NINLET=[ 1 ],
4347          MajNHYD=[ "B7R-MJ" ]
4348          MinNHYD=[ "B7R-MN" ]
4349          TMJSTO=[ 311 ](cu-m)
4350 *%-----|-----|
4351 ROUTE PIPE    PTYPE=[ 1 ]circ, NHYDout=[ "360-106A" ], RNUMBER=[ 1.0 ], PDIAm=[ 1050 ](mm),
4352          PLNGTH=[ 167 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m),
4353          NHYDin=[ "B7R-MN" ], RDT=[ 1 ]
4354 *%-----|-----|
4355 *      -JFSA 2021-01-19 change B6 to be developed as per geoottawa website and apply the
4356 parameters of A7, the nearest sub-catchment to B6, LGI is calculated based on B6 area
4357 CONTINUOUS STANDHYD NHYD=[ "B6" ], DT=[ 1 ]min, AREA=[ 3.29 ](ha),
4358          XIMP=[ 0.41 ], TIMP=[ 0.54 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4359          SCS curve number CN=[ 75 ],
4360          Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4361          LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4362          Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4363          LGI=[ 148.099 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4364          Continuous simulation parameters:
4365          IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4366          SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4367          InterEventTime=[ 18 ](hrs), END=-1
4368 *%-----|-----|
4369 *      -JFSA 2021-01-25 add B1 DUALHYD as per Corrigan Report, IBI Group, 2008
4370 COMPUTE DUALHYD NHYDin=[ "B6" ], CINLET=[ 0.064 ](cms), NINLET=[ 1 ],
4371          MajNHYD=[ "B6-MJ" ]
4372          MinNHYD=[ "B6-MN" ]
4373          TMJSTO=[ 5484 ](cu-m)
4374 *%-----|-----|
4375 *CONTINUOUS NASHYD NHYD=[ "B6" ], DT=[ 1 ]min, AREA=[ 3.29 ](ha),
4376          DWF=[ 0 ](cms), CN/C=[ 75 ], IA=[ 2.5 ](mm),
4377          N=[ 3.0 ], TP=[ 0.36 ]hrs,
4378          Continuous simulation parameters:
4379          IaRECper=[ 4 ](hrs),
4380          SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4381          InterEventTime=[ 12 ](hrs)
4382          Baseflow simulation parameters:

```

```

4381 *
4382 *
4383 *
4384 *-----|-----|
4385 *% -EX-LAND is external land. It is a part of JOCKVA sub-catchment as per Corrigan
Report, IBI Group, 2008
4386 CONTINUOUS STANDHYD NHYD=[ "EX-LAND" ], DT=[ 1 ]min, AREA=[ 32.5 ](ha),
4387 XIMP=[ 0.50 ], TIMP=[ 0.50 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4388 SCS curve number CN=[ 74 ],
4389 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4390 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4391 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4392 LGI=[ 465.475 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4393 Continuous simulation parameters:
4394 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4395 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4396 InterEventTime=[ 18 ](hrs), END=-1
4397 *%
4398 COMPUTE DUALHYD NHYDin=[ "EX-LAND" ], CINLET=[ 2.275 ](cms), NINLET=[ 1 ],
4399 MajNHYD=[ "EX-LAND-MJ" ]
4400 MinNHYD=[ "EX-LAND-MN" ]
4401 TMJSTO=[ 1365 ](cu-m)
4402 *%
4403 ADD HYD NHYDsum=[ "B6-B7ExMJ" ], NHYDs to
add=[ "B7R-MJ" +"EX-LAND-MJ" +"B5-MJ" +"B6-MJ" +"B6-MN" +"A8-MJ-B6" ]
4404 *%
4405 COMPUTE DUALHYD NHYDin=[ "B6-B7ExMJ" ], CINLET=[ 0.064 ](cms), NINLET=[ 1 ],
4406 MajNHYD=[ "B6R-MJ" ]
4407 MinNHYD=[ "B6R-MN" ]
4408 TMJSTO=[ 5484 ](cu-m)
4409 *%
4410 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout=[ "105-106A" ], RNUMBER=[ 1.0 ], PDIAM=[ 1800 ](mm),
4411 PLNGTH=[ 208 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m),
4412 NHYDin=[ "MH105-B6" ], RDT=[ 1 ]
4413 *%
4414 ADD HYD NHYDsum=[ "MH106A" ], NHYDs to
add=[ "360-106A" +"105-106A" +"B6R-MN" +"B6R-MJ" ]
4415 *%
4416 SAVE HYD NHYD=[ "MH106A" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4417 HYD_COMMENT=[ "Total Flows at MH106A" ]
4418 *% -JFSA 2021-01-12 THE MANHOLE MH106 is called MH117/106 in Corrigan Report, IBI
Group, July 2008
4419 *%
4420 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout=[ "106A-106" ], RNUMBER=[ 1.0 ], PDIAM=[ 1800 ](mm),
4421 PLNGTH=[ 190 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m),
4422 NHYDin=[ "MH106A" ], RDT=[ 1 ]
4423 *%
4424 CONTINUOUS STANDHYD NHYD=[ "A9" ], DT=[ 1 ]min, AREA=[ 2.44 ](ha),
4425 XIMP=[ 0.71 ], TIMP=[ 0.71 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4426 SCS curve number CN=[ 75 ],
4427 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4428 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4429 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4430 LGI=[ 262 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4431 Continuous simulation parameters:
4432 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4433 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4434 InterEventTime=[ 18 ](hrs), END=-1
4435 *%
4436 COMPUTE DUALHYD NHYDin=[ "A9" ], CINLET=[ 0.547 ](cms), NINLET=[ 1 ],
4437 MajNHYD=[ "A9-MJ" ]
4438 MinNHYD=[ "A9-MN" ]
4439 TMJSTO=[ 0 ](cu-m)
4440 *%
4441 ADD HYD NHYDsum=[ "MH106" ], NHYDs to add=[ "106A-106" +"A9-MN" ]

```

```

4441 *%
4442 SAVE HYD NHYD=[ "MH106" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4443 HYD_COMMENT=[ "Total Flows at MH106" ]
4444 *%
4445 *% -JFSA 2021-01-12 THE MANHOLE MH107 is called MH118/107 in Corrigan Report, IBI
4446 Group, July 2008
4447 *%
4448 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout=[ "106-107" ], RNUMBER=[ 1.0 ], PDIAM=[ 1800 ](mm),
4449 PLNGTH=[ 122.5 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m),
4450 NHYDin=[ "MH106" ], RDT=[ 1 ]
4451 *%
4452 CONTINUOUS STANDHYD NHYD=[ "A10" ], DT=[ 1 ]min, AREA=[ 4.14 ](ha),
4453 XIMP=[ 0.35 ], TIMP=[ 0.47 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4454 SCS curve number CN=[ 75 ],
4455 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4456 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4457 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4458 LGI=[ 183 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4459 Continuous simulation parameters:
4460 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4461 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4462 InterEventTime=[ 18 ](hrs), END=-1
4463 *%
4464 COMPUTE DUALHYD NHYDin=[ "A10" ], CINLET=[ 0.310 ](cms), NINLET=[ 1 ],
4465 MajNHYD=[ "A10-MJ" ]
4466 MinNHYD=[ "A10-MN" ]
4467 TMJSTO=[ 228 ](cu-m)
4468 *%
4469 CONTINUOUS STANDHYD NHYD=[ "A11" ], DT=[ 1 ]min, AREA=[ 10.61 ](ha),
4470 XIMP=[ 0.53 ], TIMP=[ 0.62 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4471 SCS curve number CN=[ 75 ],
4472 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4473 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4474 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4475 LGI=[ 379 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4476 Continuous simulation parameters:
4477 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4478 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4479 InterEventTime=[ 18 ](hrs), END=-1
4480 *%
4481 COMPUTE DUALHYD NHYDin=[ "A11" ], CINLET=[ 0.993 ](cms), NINLET=[ 1 ],
4482 MajNHYD=[ "A11-MJ" ]
4483 MinNHYD=[ "A11-MN" ]
4484 TMJSTO=[ 556 ](cu-m)
4485 *%
4486 ADD HYD NHYDsum=[ "MH107" ], NHYDs to add=[ "106-107" + "A10-MN" + "A11-MN" ]
4487 *%
4488 SAVE HYD NHYD=[ "MH107" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4489 HYD_COMMENT=[ "Total Flows at MH107" ]
4490 *%
4491 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout=[ "107-119" ], RNUMBER=[ 1.0 ], PDIAM=[ 1800 ](mm),
4492 PLNGTH=[ 114 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0012 ](m/m),
4493 NHYDin=[ "MH107" ], RDT=[ 1 ]
4494 *%
4495 *% -JFSA 2021-01-12 THE MANHOLE MH108 is called MH120/108 in Corrigan Report, IBI
4496 Group, July 2008
4497 *%
4498 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout=[ "119-108" ], RNUMBER=[ 1.0 ], PDIAM=[ 1800 ](mm),
4499 PLNGTH=[ 65.8 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0012 ](m/m),
4500 NHYDin=[ "107-119" ], RDT=[ 1 ]
4501 *%
4502 CONTINUOUS STANDHYD NHYD=[ "A12" ], DT=[ 1 ]min, AREA=[ 12.29 ](ha),
4503 XIMP=[ 0.41 ], TIMP=[ 0.54 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4504 SCS curve number CN=[ 75 ],
4505 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4506 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),

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4502
4503 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),  

4504 LGI=[183](m), MNI=[0.013], SCI=[0](min),  

4505 Continuous simulation parameters:  

4506 IaRECper=[4](hrs), IaRECImp=[4](hrs),  

4507 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),  

4508 InterEventTime=[18](hrs), END=-1
4509 *%-----|  

4510 COMPUTE DUALHYD NHYDin=[ "A12" ], CINLET=[1.029](cms), NINLET=[1],  

4511 MajNHYD=[ "A12-MJ" ]  

4512 MinNHYD=[ "A12-MN" ]  

4513 TMJSTO=[672](cu-m)
4514 *%-----|  

4515 CONTINUOUS STANDHYD NHYD=[ "A13" ], DT=[1]min, AREA=[2.59](ha),  

4516 XIMP=[0.71], TIMP=[0.71], DWF=[0](cms), LOSS=[2],  

4517 SCS curve number CN=[75],  

4518 Pervious surfaces: IApel=[4.67](mm), SLPP=[1](%),  

4519 LGP=[40](m), MNP=[0.25], SCP=[0](min),  

4520 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),  

4521 LGI=[379](m), MNI=[0.013], SCI=[0](min),  

4522 Continuous simulation parameters:  

4523 IaRECper=[4](hrs), IaRECImp=[4](hrs),  

4524 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),  

4525 InterEventTime=[18](hrs), END=-1
4526 *%-----|  

4527 COMPUTE DUALHYD NHYDin=[ "A13" ], CINLET=[0.571](cms), NINLET=[1],  

4528 MajNHYD=[ "A13-MJ" ]  

4529 MinNHYD=[ "A13-MN" ]  

4530 TMJSTO=[0](cu-m)
4531 * -JFSA 2021-01-22 add the Corrigan pond area ("Pond-Block")
4532 CONTINUOUS STANDHYD NHYD=[ "Pond-Block" ], DT=[1]min, AREA=[2.94](ha),  

4533 XIMP=[0.415], TIMP=[0.415], DWF=[0](cms), LOSS=[2],  

4534 SCS curve number CN=[75],  

4535 Pervious surfaces: IApel=[4.67](mm), SLPP=[1](%),  

4536 LGP=[40](m), MNP=[0.25], SCP=[0](min),  

4537 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),  

4538 LGI=[183](m), MNI=[0.013], SCI=[0](min),  

4539 Continuous simulation parameters:  

4540 IaRECper=[4](hrs), IaRECImp=[4](hrs),  

4541 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),  

4542 InterEventTime=[18](hrs), END=-1
4543 *%-----|  

4544 ADD HYD NHYDsum=[ "MH108" ], NHYDs to add=[ "119-108"+ "A13-MN"+ "A12-MN" ]
4545 *%-----|  

4546 SAVE HYD NHYD=[ "MH108" ], # OF PCYCLES=[-1], ICASEsh=[1]  

4547 HYD_COMMENT=[ "Total Flows at MH108" ]
4548 *%-----|  

4549 ROUTE PIPE PTTYPE=[1]circ, NHYDout=[ "108-116" ], RNUMBER=[1.0], PDIAM=[1800](mm),  

4550 PLNGTH=[76.6](m), PROUGH=[0.013], PSLOPE=[0.0013](m/m),  

4551 NHYDin=[ "MH108" ], RDT=[1]
4552 *%-----|  

4553 ROUTE PIPE PTTYPE=[1]circ, NHYDout=[ "116-corrig" ], RNUMBER=[1.0],  

4554 PDIAM=[1800](mm),  

4555 PLNGTH=[79.5](m), PROUGH=[0.013], PSLOPE=[0.0013](m/m),  

4556 NHYDin=[ "108-116" ], RDT=[1]
4557 *%-----|  

4558 ADD HYD NHYDsum=[ "Corrigan" ], NHYDs to add=[ "116-corrig"+ "Pond-Block" ]
4559 *%-----|  

4560 SAVE HYD NHYD=[ "Corrigan" ], # OF PCYCLES=[-1], ICASEsh=[1]  

4561 HYD_COMMENT=[ "Total Flows at Corrigan Pond" ]
4562 *%-----|  

4563 ROUTE RESERVOIR NHYDout=[ "Co-P" ], NHYDin=[ "Corrigan" ],  

4564 RDT=[1](min),
        TABLE of ( OUTFLOW-STORAGE ) values  

          (cms) - (ha-m)  

          [ 0.0 , 0.0 ]

```

```

4565 [ 0.015 , 0.04118]
4566 [ 0.030 , 0.08297]
4567 [ 0.045 , 0.12537]
4568 [ 0.060 , 0.16837]
4569 [ 0.075 , 0.21199]
4570 [ 0.090 , 0.27545]
4571 [ 0.105 , 0.34650]
4572 [ 0.120 , 0.42049]
4573 [ 0.135 , 0.50188]
4574 [ 0.186 , 0.60307]
4575 [ 2.110 , 0.79083]
4576 [ 5.874 , 1.00271]
4577 [ 11.395 , 1.29643]
4578 [ 18.770 , 1.62054]
4579 [ 28.143 , 1.97516]
4580 [ -1 , -1 ] (max twenty pts)
4581 NHYDovf=[ "Co-P-OVF" ]
4582 *%-----|-----|
4583 ADD HYD NHYDsum=[ "corrig" ], NHYDs to
add= [ "Co-P-OVF" + "Co-P" + "N_TO" + "MH105-JR" + "A8-MJ-JR" + "A9-MJ" + "A10-MJ" + "A11-MJ" + "A12-MJ" + "A13-MJ" ]
4584 *%-----|-----|
4585 SAVE HYD NHYD=[ "corrig" ], # OF PCYCLES=[-1], ICASEsh=[1]
HYD_COMMENT=[ "Total Flows at Corrigan Pond" ]
4586 *%-----|-----|
4587 *#*****|-----|
4588 *#*****|-----|
4589 *# Corrigan Pond 1
4590 *# - Rating curve obtained from Barrhaven South MSS modeling
4591 *# - Tributary Drainage Area to MSS Pond 1 = 145 ha
4592 *#*****|-----|
4593 *ROUTE RESERVOIR NHYDout=[ "MS_P1" ], NHYDin=[ "CORRIG" ],
4594 * RDT=[1](min),
4595 * TABLE of ( OUTFLOW-STORAGE ) values
4596 * (cms) - (ha-m)
4597 * [ 0.0 , 0.0 ]
4598 * [ 0.06 , 0.58 ]
4599 * [ -1 , -1 ] (max twenty pts)
4600 * NHYDovf=[ "P1-OVF" ]
4601 *%-----|-----|
4602 *ADD HYD NHYDsum=[ "SN_CO" ], NHYDs to add=[ "N_TO" + "P1-OVF" + "MS_P1" ]
4603 *%-----|-----|
4604 *SAVE HYD NHYD=[ "SN_CO" ], # OF PCYCLES=[-1], ICASEsh=[1]
4605 * HYD_COMMENT=[ "Total Flows at Corrigan Drain" ]
4606 *%-----|-----|
4607 *#
4608 *# Hydrograph from Corrigan Drain routed to Jockvale Road
4609 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
4610 *#
4611 ROUTE CHANNEL NHYDout=[ "N_MI" ] , NHYDin=[ "corrig" ] ,
4612 RDT=[1](min),
4613 CHLGTH=[ 580 ](m), CHSLOPE=[ 0.4448 ](%),
4614 FPSLOPE=[ 0.4448 ](%),
4615 SECNUM=[ 1.0 ], NSEG=[ 3 ]
4616 ( SEGROUGH, SEGDIST (m))=
4617 [ 0.075, -17.72
4618 -0.045, 17.72
4619 0.075, 80.62 ] NSEG times
4620 ( DISTANCE (m), ELEVATION (m))=
4621 [ -83.32, 90.00 ]
4622 [ -81.36, 89.50 ]
4623 [ -79.12, 89.00 ]
4624 [ -76.13, 88.50 ]
4625 [ -20.46, 88.00 ]
4626 [ -19.36, 87.50 ]
4627 [ -18.51, 87.00 ]
4628 [ -17.72, 86.50 ]

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```

4629      [-11.95, 85.24]
4630      [-0.11, 85.12]
4631      [11.49, 85.20]
4632      [17.72, 86.50]
4633      [19.74, 87.00]
4634      [21.22, 87.50]
4635      [22.68, 88.00]
4636      [24.28, 88.50]
4637      [26.79, 89.00]
4638      [71.98, 90.00]
4639      [80.62, 90.50]

4640 *%-----|-----|
4641 *#*****
4642 *#      Catchment MILLS
4643 *#      - To SWM Facility north of the Jock
4644 *#      - Primarily residential development
4645 *#*****
4646 CONTINUOUS STANDHYD NHYD=[ "MILLS" ], DT=[1]min, AREA=[175.99](ha),
4647           XIMP=[0.38], TIMP=[0.38], DWF=[0](cms), LOSS=[2],
4648           SCS curve number CN=[74],
4649           Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4650           LGP=[40](m), MNP=[0.25], SCP=[0](min),
4651           Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4652           LGI=[1118.123](m), MNI=[0.013], SCI=[0](min),
4653           Continuous simulation parameters:
4654           IaRECper=[4](hrs), IaRECImp=[4](hrs),
4655           SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4656           InterEventTime=[18](hrs), END=-1

4657 *%-----|-----|
4658 *#*****
4659 *#      Chapman Mills SWM Pond
4660 *#      - Rating curve obtained from CCL hydraulic modeling
4661 *#*****
4662 ROUTE RESERVOIR      NHYDout=[ "MILL_P" ], NHYDin=[ "MILLS" ],
4663           RDT=[1](min),
4664           TABLE of ( OUTFLOW-STORAGE ) values
4665           (cms) - (ha-m)
4666           [ 0.0 , 0.0 ]
4667           [ 0.01 , 0.01 ]
4668           [ 0.05 , 0.06 ]
4669           [ 0.09 , 0.11 ]
4670           [ 0.13 , 0.15 ]
4671           [ 0.18 , 0.19 ]
4672           [ 0.28 , 0.28 ]
4673           [ 0.37 , 0.34 ]
4674           [ 0.45 , 0.40 ]
4675           [ 0.51 , 0.44 ]
4676           [ 0.56 , 0.47 ]
4677           [ 0.64 , 0.52 ]
4678           [ 0.76 , 0.59 ]
4679           [ 0.86 , 0.65 ]
4680           [ 1.09 , 0.78 ]
4681           [ 1.44 , 0.96 ]
4682           [ 3.18 , 1.84 ]
4683           [ 4.05 , 2.31 ]
4684           [ -1 , -1 ] (max twenty pts)
4685           NHYDovf=[ "MIL-OV" ]

4686 *%-----|-----|
4687 ADD HYD      NHYDsum=[ "SN_MI" ], NHYDs to add=[ "N_MI "+ "MIL-OV" "+ "MILL_P" ]
4688 *%-----|-----|
4689 SAVE HYD      NHYD=[ "SN_MI" ], # OF PCYCLES=[-1], ICASEsh=[1]
4690           HYD_COMMENT=[ "Total Flows at Jockvale Road" ]
4691 *%-----|-----|
4692 *#
4693 *# Hydrograph from Jockvale Road routed to Heart's Desire
4694 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 689

```

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4695 *#
4696 ROUTE CHANNEL      NHYDout=[ "N_DE" ] , NHYDin=[ "SN_MI" ] ,
4697 RDT=[1](min),
4698 CHLGTH=[1962](m),   CHSLOPE=[0.2227](%),   FPSLOPE=[0.2227](%),
4699 SECNUM=[1.0],       NSEG=[3]
4700 ( SEGRROUGH, SEGDIST (m))=
4701     [0.075,-17.56
4702     -0.045,18.27
4703     0.075,32.51] NSEG times
4704 ( DISTANCE (m), ELEVATION (m))=
4705 [-54.07, 85.00]
4706 [-39.43, 84.50]
4707 [-28.30, 84.00]
4708 [-24.12, 83.50]
4709 [-22.30, 83.00]
4710 [-20.55, 82.50]
4711 [-17.56, 82.00]
4712 [-12.63, 81.22]
4713 [-0.11, 80.75]
4714 [11.55, 81.22]
4715 [18.27, 82.00]
4716 [19.82, 82.50]
4717 [22.48, 83.00]
4718 [27.90, 83.50]
4719 [29.31, 84.00]
4720 [30.81, 84.50]
4721 [32.51, 85.00]
4722
4723 *%-----|-----|
4724 *#*****
4725 *#      Catchment DESIRE
4726 *#      - To Jock River (north of the Jock)
4727 *#      - Rural-estate subdivision (Heart's Desire Community)
4728 *#*****
4729 CONTINUOUS STANDHYD NHYD=[ "DESIRE" ], DT=[1]min, AREA=[ 23.78 ](ha),
4730 XIMP=[ 0.25 ], TIMP=[ 0.25 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4731 SCS curve number CN=[ 77 ],
4732 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4733 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4734 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4735 LGI=[ 400 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4736 Continuous simulation parameters:
4737 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4738 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4739 InterEventTime=[ 18 ](hrs), END=-1
4740 *%-----|-----|
4741 *#*****
4742 *#      Catchment JOCKVA
4743 *#      - To Jockvale SWM Facility
4744 *#      - Residential development & golf course
4745 *#      - JFSA 2021-01-11 update JOCKVA after updating CORRIG as per IBI GROUP, July 2008.
4746 *#      JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two
4747 areas JOCKVA and EX-LAND 32.5 ha as per IBI GROUP, July 2008.
4748 *#*****
4749 CONTINUOUS STANDHYD NHYD=[ "JOCKVA" ], DT=[1]min, AREA=[ 225.13 ](ha),
4750 XIMP=[ 0.50 ], TIMP=[ 0.50 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4751 SCS curve number CN=[ 74 ],
4752 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4753 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4754 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4755 LGI=[ 1310.55 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4756 Continuous simulation parameters:
4757 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4758 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4759 InterEventTime=[ 18 ](hrs), END=-1
4760 *%-----|-----|

```

```

4760          ADD HYD          NHYDsum=[ "JOCKVA-TO" ] , NHYDs to
4761          add=[ "EX-LAND-MN"+"JOCKVA"+ "B2-MJ" +"B3-MJ" ]
4762          *%-----|-----|
4763          SAVE HYD          NHYD=[ "JOCKVA-TO" ] , # OF PCYCLES=[-1] , ICASEsh=[1]
4764          HYD_COMMENT=[ "Total Flows at KB first pond" ]
4765          *%-----|-----|
4766          **#      Jockvale SWM Facility
4767          **# - Rating curve obtained from Jockvale Servicing Study (CCL 1999)
4768          **#-----|
4769          ROUTE RESERVOIR    NHYDout=[ "JOCK_P" ] , NHYDin=[ "JOCKVA-TO" ],
4770          RDT=[1](min),
4771          TABLE of ( OUTFLOW-STORAGE ) values
4772          (cms) - (ha-m)
4773          [ 0.0 , 0.0 ]
4774          [ 0.27 , 0.03 ]
4775          [ 0.28 , 0.55 ]
4776          [ 0.29 , 1.14 ]
4777          [ 0.30 , 1.80 ]
4778          [ 0.31 , 2.32 ]
4779          [ 1.12 , 2.87 ]
4780          [ 2.92 , 3.45 ]
4781          [ 4.64 , 4.07 ]
4782          [ 6.69 , 4.72 ]
4783          [ 9.02 , 5.39 ]
4784          [ 11.62 , 6.10 ]
4785          [ 14.42 , 6.85 ]
4786          [ 17.45 , 7.62 ]
4787          [ 20.69 , 8.44 ]
4788          [ 24.08 , 9.28 ]
4789          [ 27.68 , 10.17 ]
4790          [ -1 , -1 ] (max twenty pts)
4791          NHYDovf=[ "JO-OVF" ]
4792          *%-----|-----|
4793          ADD HYD          NHYDsum=[ "SN_DE" ] , NHYDs to add=[ "N_DE"+"DESIRE"+"JO-OVF"+"JOCK_P" ]
4794          *%-----|-----|
4795          SAVE HYD          NHYD=[ "SN_DE" ] , # OF PCYCLES=[-1] , ICASEsh=[1]
4796          HYD_COMMENT=[ "Total Flows at Heart's Desire" ]
4797          *%-----|-----|
4798          **#
4799          **# Hydrograph from Heart's Desire routed to Rideau River
4800          **# Channel X-Section obtained from RVCA Hydraulic Model - Station 0
4801          **#
4802          ROUTE CHANNEL    NHYDout=[ "N1" ] , NHYDin=[ "SN_DE" ] ,
4803          RDT=[1](min),
4804          CHLGTH=[563](m), CHSLOPE=[0.9668](%) ,
4805          FPSLOPE=[0.9668](%) ,
4806          SECNUM=[1.0] , NSEG=[3]
4807          ( SEGROUGH, SEGDIST (m))=
4808          [0.075,-30.20
4809          -0.045,30.20
4810          0.075,48.48] NSEG times
4811          ( DISTANCE (m) , ELEVATION (m))=
4812          [-98.46, 81.50]
4813          [-92.24, 81.00]
4814          [-86.88, 80.50]
4815          [-81.54, 80.00]
4816          [-74.36, 79.50]
4817          [-63.54, 79.00]
4818          [-39.23, 78.50]
4819          [-34.51, 78.00]
4820          [-33.01, 77.50]
4821          [-30.20, 77.00]
4822          [-13.42, 76.18]
4823          [-1.14, 76.09]
4824          [17.06, 76.18]

```

```

4825 [30.20, 77.00]
4826 [32.95, 77.50]
4827 [34.06, 78.00]
4828 [35.11, 78.50]
4829 [36.32, 79.00]
4830 [37.74, 79.50]
4831 [48.48, 81.50]
4832 *%-----|-----|
4833 *#*****|-----|
4834 *#      Catchment S-2
4835 *#      - To Jock River (north and south)
4836 *#      - Undeveloped floodplain and river
4837 *#*****|-----|
4838 CONTINUOUS NASHYD   NHYD=[ "S-2" ], DT=[1]min, AREA=[102.94](ha),
4839           DWF=[0](cms), CN/C=[72], IA=[4.67](mm),
4840           N=[3], TP=[0.40]hrs,
4841           Continuous simulation parameters:
4842           IaRECper=[4](hrs),
4843           SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4844           InterEventTime=[12](hrs)
4845           Baseflow simulation parameters:
4846           BaseFlowOption=[1],
4847           InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4848           VHydCond=[0.055](mm/hr), END=-1
4849 *%-----|-----|
4850 ADD HYD          NHYDsum= [ "SN_N1" ], NHYDs to add=[ "N1 "+"S-2" ]
4851 *%-----|-----|
4852 SAVE HYD          NHYD=[ "SN_N1" ], # OF PCYCLES=[-1], ICASEsh=[1]
4853           HYD_COMMENT=[ "Total Flows at Rideau River" ]
4854 *%-----|-----|
4855 #####|-----|
4856 *% 5 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4857 START             TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[5]
4858           [ "C24SC005.stm" ] <--storm filename, one per line for NSTORM time
4859 *%-----|-----|
4860 *% 10 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4861 START             TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[10]
4862           [ "C24SC010.stm" ] <--storm filename, one per line for NSTORM time
4863 *%-----|-----|
4864 *% 25 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4865 START             TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[25]
4866           [ "C24SC025.stm" ] <--storm filename, one per line for NSTORM time
4867 *%-----|-----|
4868 *% 50 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4869 START             TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[50]
4870           [ "C24SC050.stm" ] <--storm filename, one per line for NSTORM time
4871 *%-----|-----|
4872 *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4873 START             TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4874           [ "100YC3H.STM" ] <--storm filename, one per line for NSTORM time
4875 *%-----|-----|
4876 *% 100 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4877 START             TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4878           [ "C24SC100.stm" ] <--storm filename, one per line for NSTORM time
4879 *%-----|-----|
4880 *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4881 START             TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4882           [ "C24SC100.stm" ] <--storm filename, one per line for NSTORM time
4883 *START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[101]
4884           [ "A24SC100.stm" ] <--storm filename, one per line for NSTORM time
4885 *START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[102]
4886           [ "A24SC100_60.stm" ] <--storm filename, one per line for NSTORM time
4887 FINISH
4888

```

00001> \*\*\*\*  
00002> SSSSS W W M M H H Y Y M M 000 222 000 11 5555 \*\*\*\*\*  
00004> S W W N M M H H Y Y M M 0 0 2 0 0 11 5 Ver: 6.600  
00005> SSSSS W W M M H H Y Y M M 000 222 0 0 11 555 FEB 2015  
00007> SSSSS W W M M H H Y M M 000 222 0 0 11 5 \* 000  
00008> Stormwater Management Hydrologic Model 222 000 11 455 \*\*\*\*\*  
00010>  
00012> \*\*\*\*\* SWMMHYD Ver. 5.600 \*\*\*  
00013> \* A single event and continuous hydrologic simulation model  
00014> \* based on the SWMM model and its successors  
00015> \* CTHNHYD-83 and CTHNHYD-89.  
00016> \*  
00017> \* Distributed by: J. Fabre & Associates Inc.  
00018> \* Ottawa, Ontario: (613) 836-3884  
00019> \* Gatineau, Quebec: (819) 243-6858  
00020> \* E-mail: jfainc@jfainc.ca  
00021> \*  
00022>  
00024> \* Licensed user: JFSAinc.  
00025> \* Ottawa SERIAL# 2549237 \*\*\*\*\*  
00027>  
00028> \*\*\*\*\* PROGRAM ARRAY DIMENSIONS \*\*\*\*\*  
00029> \* Maximum value for ID numbers : 11 \*\*\*\*\*  
00030> \* Max. number of rainfall points: 105408 \*\*\*\*\*  
00031> \* Max. number of nodes: 105408 \*\*\*\*\*  
00032> \*  
00033> \*  
00034>  
00035> \* S U M M A R Y O U T P U T \*  
00036> \*  
00037> \* RUN DATE: 2021-03-04 TIME: 11:54:16 RUN COUNT: 02083 \*  
00038> \*  
00039> \* Input file: T:\R\ON\1474-16\Design\20210126\QuantityControlAnalysis\SWMMHYD\SMR-Model\updated\\*  
00040> \* Output file: T:\R\ON\1474-1.5-Fr\_SD.out  
00041> \* Summary file: T:\R\ON\1474-1.5-Fr\_SD.sum  
00042> \* 3\SWMM\_S-1\_S-Fr\_SD.sum  
00043> \* User comments:  
00044> \* 2:  
00045> \* 3:  
00046>  
00051>  
00052>  
00053> # SWMMHYD Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE  
00054> #  
00055> # Project Name: [Rock River] Project Number: [1474-16]  
00056> # Date : 04-03-2021  
00057> # Modeler : JFSAinc.  
00058> # Company : JFSAinc.  
00059> # License #: 1549237  
00060> #  
00062> # CALIBRATION OF SUMMER MODEL PARAMETERS  
00063> # USING CONTINUOUS SIMULATIONS  
00064> # Rainfall data from JFSA rain gauge installed at site + other gauges by the City  
00065> # Use data collected from May 1st to July 14, 2003  
00066> # 2020-11-30 change TMNSTO to COMPUTE DUALYD (TMNSTO = 0.1 instead of 0.0001)  
00067> # 2020-12-12 change W\_CLAR\_BXAP to 0.55, SLP1=[0.5%] (imperious slope), and LGI up to 700m  
00068> # 2021-02-19 Change the slope for ROUTE CHANNEL Station 2442 (NHYDout=[\*TO\*], NHYDin=[\*SN\_TO\*]) from 0.033 % (as per S  
00069> # 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHYDout=[\*MC\*], NHYDin=[\*SN\_CE\*]) from 0.01 % (as per S  
00070> # 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHYDout=[\*AC\*], NHYDin=[\*SN\_AC\*]) from 0.01 % (as per S  
00071> #  
00072> \*\* END OF RUN : 1  
00073>  
00074> #  
00075> # RUNS=COMMAND#  
00076> R0021:CO0001-----  
00077> #  
00078> # [TZERO = 0.00 hrs on 0] [METOUT = 2 (1=imperial, 2=metric output)]  
00079> # [NRUN = 0000] [NRUN = 1]  
00080> #  
00081> # SWMMHYD Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE  
00082> #  
00083> # Project Name: [Rock River] Project Number: [1474-16]  
00084> # Date : 04-03-2021  
00085> # Modeler : [M.W.]  
00086> # Company : [JFSAinc.]  
00087> # License #: 1549237  
00088> #  
00089> # EQUILIBRATION OF SUMMER PARAMETERS  
00090> #  
00091> # USING CONTINUOUS SIMULATIONS  
00092> # Rainfall data from JFSA rain gauge installed at site + other gauges by the City  
00093> # Use data collected from May 1st to July 14, 2003  
00094> # 2020-12-12 correct pond curve values  
00095> # 2021-02-19 Change the slope for ROUTE CHANNEL Station 2442 (NHYDout=[\*TO\*], NHYDin=[\*SN\_TO\*]) from 0.033 % (as per S  
00096> # 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHYDout=[\*MC\*], NHYDin=[\*SN\_CE\*]) from 0.01 % (as per S  
00097> # 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHYDout=[\*AC\*], NHYDin=[\*SN\_AC\*]) from 0.01 % (as per S  
00098> #  
00099> #  
00100> # RUNS=COMMAND#  
00101> R0022:CO0001-----  
00102> #  
00103> # [TZERO = 0.00 hrs on 0] [METOUT = 2 (1=imperial, 2=metric output)]  
00104> # [NRUN = 0000] [NRUN = 1]  
00105> #  
00106> #  
00107> # RESTART-  
00108> # File comment: [Based on various calibration exercises in Onta  
00109> # File comment: [Based on various calibration exercises in the DESIGN STANDYD COM  
00110> # Horton's infiltration equation parameters:  
00111> # [Flow = 76.20 mm/hr] [Fc=13.20 mm/hr] [DCav= 4.14 hr] [F= .00 mm]  
00112> # [P=0.00 mm] [S=0.00 mm] [L=0.00 mm] [K=0.00 mm]  
00113> # [Aper= 4.67 mm] [LGP=50.00 mm] [MDW= .250]  
00114> # Parameters for IMPERVIOUS surfaces in STANDYD:  
00115> # [Infiltration = 0.00 mm] [C=0.00 mm] [K=0.00 mm] [M=0.013] [N=0.013]  
00116> # Parameters used in NASHYD:  
00117> # [In= 4.67 mm] [N= 3.00]  
00118> # Average precipitation and infiltration data in (mm)  
00119> # JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC  
00120> # 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
00121> # Horton's infiltration equation parameters:  
00122> # [Flow = 76.20 mm/hr] [Fc=13.20 mm hr] [DCav= 4.14 hr] [F= .00 mm]  
00123> # [P=0.00 mm] [S=0.00 mm] [L=0.00 mm] [K=0.00 mm]  
00124> # [Aper= 4.67 mm] [LGP=50.00 mm] [MDW= .250]  
00125> # Parameters for IMPERVIOUS surfaces in STANDYD:  
00126> # [Infiltration = 0.00 mm] [C=0.00 mm] [K=0.00 mm] [M=0.013] [N=0.013]  
00127> # Parameters used in NASHYD:  
00128> # [In= 4.67 mm] [N= 3.00]  
00129> # Average precipitation and infiltration data in (mm)  
00130> # JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC  
00131> # 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
00132> # Average monthly Potential Evapotranspiration in (mm)  
00133> # JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC  
00134> # 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
00135> #  
00136> # COMPUTE API:  
00137> # [ApIn= 5.00 mm] [ApRdly= .8580; ApRdtr= 9988]  
00138> # [ApAvg= 80.12; ApAvgv= 56.74; ApRmin= 44.67]  
00139> #  
00140> # TheTp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00141> # of 1.32  
00142> R0023:CO0006-----  
00143> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00144> # CONTINUOUS:NASHYD 1.0 01SNW\_13 3680.00 6.204 No\_date 37:06 11.47 .252 .000  
00145> # [iAEc= 4.00 SMIN= 57.05 SMAX=380.32] SK= .010  
00146> # [InterEventTime= 12.00]  
00147> # TheTp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00148> # of 1.32  
00149> R0023:CO0007-----  
00150> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00151> # CONTINUOUS:NASHYD 1.0 01SNW\_13 971.00 2.187 No\_date 32:37 10.75 .236 .000  
00152> # [iAEc= 4.00 SMIN= 44.50 SMAX=430.01] SK= .010  
00153> # [InterEventTime= 12.00]  
00154> #  
00155> # TheTp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00156> # of 1.80  
00157> R0023:CO0008-----  
00158> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00159> # CONTINUOUS:NASHYD 1.0 01SNW\_13 3074.00 3.218 No\_date 39:59 9.43 .207 .000  
00160> # [iAEc= 4.00 SMIN= 37.00 SMAX=101.31] SK= .010  
00161> # [InterEventTime= 12.00]  
00162> #  
00163> R0023:CO0009-----  
00164> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00165> # CONTINUOUS:NASHYD 1.0 01SNW\_13 1781.00 5.504 No\_date 32:45 13.94 .306 .000  
00166> # [iAEc= 4.00 SMIN= 39.75 SMAX=264.99] SK= .010  
00167> #  
00168> R0023:CO0100-----  
00169> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00170> # CONTINUOUS:NASHYD 1.0 01SNW\_13 1917.00 4.042 No\_date 34:34 11.98 .263 .000  
00171> # [iAEc= 4.00 SMIN= 52.62 SMAX=350.79] SK= .010  
00172> # [InterEventTime= 12.00]  
00173> #  
00174> # TheTp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00175> # of 1.32  
00176> R0023:CO0101-----  
00177> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00178> # CONTINUOUS:NASHYD 1.0 01SNW\_13 9666.00 11.228 No\_date 38:07 13.94 .306 .000  
00179> # [iAEc= 4.00 SMIN= 39.75 SMAX=264.99] SK= .010  
00180> #  
00181> # TheTp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00182> # of 1.52  
00183> R0023:CO0112-----  
00184> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00185> # CONTINUOUS:NASHYD 1.0 01SNW\_13 8666.00 11.228 No\_date 38:07 11.98 .263 .000  
00186> # [iAEc= 4.00 SMIN= 39.75 SMAX=350.79] SK= .010  
00187> #  
00188> # InterEventTime= 12.00  
00189> # TheTp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00190> # of 1.75  
00191> R0023:CO0113-----  
00192> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00193> # CONTINUOUS:NASHYD 1.0 01SNW\_13 1132.00 4.434 No\_date 30:56 13.35 .293 .000  
00194> # [iAEc= 4.00 SMIN= 52.62 SMAX=350.79] SK= .010  
00195> # [InterEventTime= 12.00]  
00196> #  
00197> # TheTp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00198> # of 1.80  
00199> R0023:CO0114-----  
00200> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00201> # CONTINUOUS:NASHYD 1.0 01SNW\_13 8376.00 11.072 No\_date 39:59 11.98 .263 .000  
00202> # [iAEc= 4.00 SMIN= 52.62 SMAX=350.79] SK= .010  
00203> # [InterEventTime= 12.00]  
00204> #  
00205> # TheTp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00206> # of 1.80  
00207> R0023:CO0115-----  
00208> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00209> # CONTINUOUS:NASHYD 1.0 01SNW\_13 4464.00 5.504 No\_date 39:59 10.98 .241 .000  
00210> # [iAEc= 4.00 SMIN= 52.62 SMAX=350.79] SK= .010  
00211> # [InterEventTime= 12.00]  
00212> #  
00213> # TheTp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00214> # of 1.80  
00215> R0023:CO0116-----  
00216> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00217> # CONTINUOUS:NASHYD 1.0 01SNW\_13 131.00 .805 No\_date 28:57 11.22 .247 .000  
00218> # [iAEc= 4.00 SMIN= 52.62 SMAX=350.79] SK= .010  
00219> # [InterEventTime= 12.00]  
00220> #  
00221> # TheTp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00222> # of 1.65  
00223> R0023:CO0117-----  
00224> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00225> # CONTINUOUS:NASHYD 1.0 01SNW\_13 3884.00 6.242 No\_date 38:46 11.98 .263 .000  
00226> # [iAEc= 4.00 SMIN= 52.62 SMAX=350.79] SK= .010  
00227> # [InterEventTime= 12.00]  
00228> #  
00229> # TheTp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00230> # of 1.80  
00231> R0023:CO0118-----  
00232> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00233> # CONTINUOUS:NASHYD 1.0 01SNW\_13 3197.00 3.148 No\_date 35:23 13.94 .306 .000  
00234> # [iAEc= 4.00 SMIN= 52.62 SMAX=350.79] SK= .010  
00235> # [InterEventTime= 12.00]  
00236> #  
00237> # TheTp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00238> # of 1.65  
00239> R0023:CO0119-----  
00240> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00241> # CONTINUOUS:NASHYD 1.0 01SNW\_13 165.00 .413 No\_date 33:07 12.24 .269 .000  
00242> # [iAEc= 4.00 SMIN= 52.62 SMAX=350.79] SK= .010  
00243> # [InterEventTime= 12.00]  
00244> #  
00245> # TheTp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00246> # of 1.67  
00247> R0023:CO0120-----  
00248> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00249> # CONTINUOUS:NASHYD 1.0 01SNW\_13 1322.00 3.148 No\_date 35:23 13.94 .306 .000  
00250> # [iAEc= 72.01 S MIN: 0.00 Tp: 5.95] SK= .010  
00251> # [InterEventTime= 12.00]  
00252> #  
00253> R0023:CO0121-----  
00254> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00255> # CONTINUOUS:NASHYD 1.0 01SNW\_13 224.00 3.156 No\_date 28:45 15.91 .350 .000  
00256> # [iAEc= 4.00 SMIN= 31.15 SMAX=207.66] SK= .010  
00257> # [InterEventTime= 12.00]  
00258> #  
00259> # TheTp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00260> # of 1.67  
00261> R0023:CO0122-----  
00262> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00263> # CONTINUOUS:NASHYD 1.0 01SNW\_13 165.00 .413 No\_date 33:25 14.57 .320 .000  
00264> # [iAEc= 72.01 S MIN: 0.00 Tp: 5.95] SK= .010  
00265> # [InterEventTime= 12.00]  
00266> #  
00267> R0023:CO0123-----  
00268> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00269> # CONTINUOUS:NASHYD 1.0 01SNW\_13 20.00 .309 No\_date 28:36 17.79 .391 .000  
00270> # [iAEc= 4.00 SMIN= 6.67 SMAX=168.09] SK= .010  
00271> # [InterEventTime= 12.00]  
00272> #  
00273> # TheTp was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00274> # of 1.61  
00275> R0023:CO0124-----  
00276> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00277> # CONTINUOUS:NASHYD 1.0 01SNW\_13 1412.00 3.090 No\_date 38:04 15.22 .334 .000  
00278> # [iAEc= 4.00 SMIN= 25.21 SMAX=244.49] SK= .010  
00279> # [InterEventTime= 12.00]  
00280> #  
00281> R0023:CO0125-----  
00282> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00283> # CONTINUOUS:NASHYD 1.0 01SNW\_13 1021.00 5.747 No\_date 30:50 17.39 .382 .000  
00284> # [iAEc= 4.00 SMIN= 25.21 SMAX=244.49] SK= .010  
00285> # [InterEventTime= 12.00]  
00286> #  
00287> R0023:CO0126-----  
00288> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00289> # CONTINUOUS:NASHYD 1.0 01SNW\_13 585.00 4.325 No\_date 29:58 17.79 .391 .000  
00290> # [iAEc= 81.01 S MIN: 0.00 Tp: 7.51] SK= .010  
00291> # [iAEc= 4.00 SMIN= 25.21 SMAX=168.09] SK= .010  
00292> # [InterEventTime= 12.00]  
00293> #  
00294> R0023:CO0127-----  
00295> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00296> # CONTINUOUS:NASHYD 1.0 01SNW\_13 1122.00 5.337 No\_date 31:00 17.79 .391 .000  
00297> # [iAEc= 4.00 SMIN= 25.21 SMAX=168.09] SK= .010  
00298> # [InterEventTime= 12.00]  
00299> #  
00300> R0023:CO0129-----  
00301> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00302> # CONTINUOUS:NASHYD 1.0 01SNW\_13 1021.00 5.747 No\_date 30:50 17.39 .342 .000  
00303> # [iAEc= 74.00 S MIN: 0.00 Tp: 7.51] SK= .010  
00304> # [InterEventTime= 12.00]  
00305> #  
00306> R0023:CO0130-----  
00307> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00308> # CONTINUOUS:NASHYD 1.0 01SNW\_13 7273.00 9.475 No\_date 39:59 10.57 n/a .000  
00309> # [iAEc= 4.00 SMIN= 25.21 SMAX=215.50] SK= .010  
00310> # [InterEventTime= 12.00]  
00311> #  
00312> R0023:CO0131-----  
00313> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00314> # Insertion of a reservoir to simulate the effects of the Goodwood Marsh  
00315> # [iAEc= 61.00 S MIN: 0.00 Tp: 7.51] SK= .010  
00316> # [InterEventTime= 12.00]  
00317> #  
00318> R0023:CO0132-----  
00319> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00320> # ROUTE RESERVOIR --> 1.0 02:IR\_NSM13 7725.00 9.475 No\_date 39:59 10.57 n/a .000  
00321> # [iAEc= 61.00 S MIN: 0.00 Tp: 7.51] SK= .010  
00322> # [InterEventTime= 12.00]  
00323> #  
00324> R0023:CO0133-----  
00325> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00326> # ROUTE RESERVOIR --> 1.0 02:IR\_NSM13 7725.00 9.475 No\_date 39:59 10.57 n/a .000  
00327> # [iAEc= 61.00 S MIN: 0.00 Tp: 7.51] SK= .010  
00328> # [InterEventTime= 12.00]  
00329> #  
00330> R0023:CO0134-----  
00331> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00332> # ROUTE CHANNEL --> 1.0 02:IR\_ASH 7725.00 2.619 No\_date 55:07 10.57 n/a .000  
00333> # [iAEc= 61.00 S MIN: 0.00 Tp: 7.51] SK= .010  
00334> # [InterEventTime= 12.00]  
00335> #  
00336> R0023:CO0135-----  
00337> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00338> # SAVE HYD 1.0 01:SNM12 9506.00 7.458 No\_date 32:50 11.20 n/a .000  
00339> # frame\_B\_SN12  
00340> # remark\_Outflow from Node 12 to Node 13  
00341> # [iAEc= 61.00 S MIN: 0.00 Tp: 7.51] SK= .010  
00342> # [InterEventTime= 12.00]  
00343> #  
00344> # Use n=0.04 for summer conditions and n=0.025 for spring conditions  
00345> # [iAEc= 61.00 S MIN: 0.00 Tp: 7.51] SK= .010  
00346> # [InterEventTime= 12.00]  
00347> #  
00348> R0023:CO0136-----  
00349> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00350> # [iAEc= 61.00 S MIN: 0.00 Tp: 7.51] SK= .010  
00351> # [InterEventTime= 12.00]  
00352> #  
00353> R0023:CO0137-----  
00354> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00355> # [iAEc= 61.00 S MIN: 0.00 Tp: 7.51] SK= .010  
00356> # [InterEventTime= 12.00]  
00357> #  
00358> R0023:CO0138-----  
00359> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00360> # [iAEc= 61.00 S MIN: 0.00 Tp: 7.51] SK= .010  
00361> # [InterEventTime= 12.00]  
00362> #  
00363> R0023:CO0139-----  
00364> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00365> # [iAEc= 61.00 S MIN: 0.00 Tp: 7.51] SK= .010  
00366> # [InterEventTime= 12.00]  
00367> #  
00368> R0023:CO0140-----  
00369> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00370> # [iAEc= 61.00 S MIN: 0.00 Tp: 7.51] SK= .010  
00371> # [InterEventTime= 12.00]  
00372> #  
00373> R0023:CO0141-----  
00374> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00375> # [iAEc= 61.00 S MIN: 0.00 Tp: 7.51] SK= .010  
00376> # [InterEventTime= 12.00]  
00377> #  
00378> R0023:CO0142-----  
00379> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--DWFcms  
00380> # [iAEc= 61.00 S MIN: 0.00 Tp: 7.51] SK= .010  
00381> # [InterEventTime= 12.00]  
00382> #  
00383> R0023:CO0143-----  
00384> # DYNIN:ID=NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVNm-R.C.--D

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00375* # 00020:000039 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00377* ADD HVD
00378*   + 1.0 02:02:00:1 9560.00 7.379 No.Date 33:12 11.20 n/a .000
00379*   + 1.0 02:02:00:1 9560.00 7.379 No.Date 33:12 11.20 n/a .000
00380*   SUM: 1.0 01:08:1_N11 11923.00 12.077 No.Date 33:14 11.36 n/a .000
00382* # Sum of hydrographs from Node 11 routed to Node 10
00383* # Section 1
00384* # 00020:000040 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00385* ADD HVD
00386*   + [RDtv 1.00] cut-> 1.0 02:08:1_N11 11923.00 12.077 No.Date 33:14 11.36 n/a .000
00387*   [L/S(n=1428*) / .057, .040]
00388*   [Vmax=.462*Dmax=.886]
00389* # 00020:000041 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00390* ADD HVD
00391*   + [RDtv 1.00] cut-> 1.0 02:08:1_N10 11923.00 8.276 No.Date 39:46 11.36 n/a .000
00392*   [L/S(n=1428*) / .157, .040]
00393* # 00020:000042 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00394* ADD HVD
00395*   + 1.0 02:02:00:1 11923.00 1.276 No.Date 39:46 11.36 n/a .000
00396*   SUM: 1.0 01:08:1_N10 17589.00 15.228 No.Date 39:47 11.36 n/a .000
00397* # 00020:000043 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00398* ADD HVD
00399*   + 1.0 02:02:00:1 11923.00 19.451 No.Date 38:31 12.19 n/a .000
00400*   remark:flow at S_N10_N10 = N10 + SW_10
00401* # 00020:000044 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00402* ADD HVD
00403*   + [RDtv 1.00] cut-> 1.0 02:08:1_N10 25965.00 30.328 No.Date 39:58 12.15 n/a .000
00404*   [L/S(n= 3982*) / .075, .040]
00405*   [Vmax=.595*Dmax=.208]
00406* # 00020:000045 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00407* ADD HVD
00408*   + 1.0 02:02:00:1 25965.00 19.451 No.Date 39:58 12.15 n/a .000
00409* # Sum of hydrographs from Node 10 routed to Node 9
00410* # Section 2
00411* # 00020:000046 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00412* ADD HVD
00413*   + 1.0 02:02:00:1 25965.00 30.328 No.Date 39:58 12.15 n/a .000
00414*   [RDtv 1.00] cut-> 1.0 02:08:1_N10 25965.00 29.579 No.Date 39:59 12.12 n/a .000
00415*   [L/S(n= 3982*) / .075, .040]
00416*   [Vmax=.595*Dmax=.208]
00417* # Addition of Subwatershed 9 and Nicholls Creek to Node 9
00418* # 00020:000047 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00419* ADD HVD
00420*   + 1.0 02:02:00:1 25965.00 29.579 No.Date 39:59 12.12 n/a .000
00421*   SUM: 1.0 02:08:1_N10 1132.00 4.334 No.Date 30:16 13.35 n/a .000
00422*   SUM: 1.0 02:08:1_N10 1132.00 4.334 No.Date 30:16 13.35 n/a .000
00423*   SUM: 1.0 01:08:1_N10 31561.00 36.313 No.Date 39:59 12.00 n/a .000
00424* # Sum of hydrographs from Node 9 routed to Node 8
00425* # Section 3
00426* # 00020:000048 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00427* ADD HVD
00428*   + 1.0 02:02:00:1 31561.00 36.313 No.Date 39:59 12.00 n/a .000
00429*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 31561.00 34.173 No.Date 39:59 12.00 n/a .000
00430*   [L/S(n= 3750*) / .057, .040]
00431*   [Vmax=.418*Dmax=.128]
00432*   [Vmax=.418*Dmax=.128]
00433* # 00020:000049 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00434* ADD HVD
00435*   + 1.0 02:02:00:1 31561.00 36.313 No.Date 39:59 12.00 n/a .000
00436*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 31561.00 34.173 No.Date 39:59 12.00 n/a .000
00437*   [L/S(n= 3750*) / .057, .040]
00438*   [Vmax=.418*Dmax=.128]
00439* # Addition of Subwatershed 9 and Hobbs's Drain to Node 8
00440* # 00020:000050 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00441* ADD HVD
00442*   + 1.0 02:02:00:1 31561.00 36.313 No.Date 39:59 12.00 n/a .000
00443*   SUM: 1.0 02:08:1_N10 31561.00 40.474 No.Date 39:59 12.00 n/a .000
00444* # Sum of hydrographs from Node 8 routed to Node 7
00445* # Section 4
00446* # 00020:000051 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00447* ADD HVD
00448*   + 1.0 02:02:00:1 31561.00 40.474 No.Date 39:59 12.00 n/a .000
00449*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 31561.00 40.474 No.Date 39:59 12.00 n/a .000
00450*   [L/S(n= 3750*) / .057, .040]
00451*   [Vmax=.418*Dmax=.128]
00452* # Addition of Subwatershed 7 to Node 7
00453* # 00020:000052 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00454* ADD HVD
00455*   + 1.0 02:02:00:1 31561.00 40.474 No.Date 39:59 12.00 n/a .000
00456*   SUM: 1.0 01:08:1_N10 38743.00 36.311 No.Date 43:31 11.82 n/a .000
00457* # 00020:000053 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00458* ADD HVD
00459*   + 1.0 02:02:00:1 38743.00 36.311 No.Date 43:31 11.82 n/a .000
00460*   SUM: 1.0 01:08:1_N10 38743.00 40.474 No.Date 43:31 11.82 n/a .000
00461* # Insertion of a reservoir to simulate the effects of the Richmond Pen.
00462* # Storage area and volumes were estimated from available topo maps.
00463* # The reservoir was assumed to be 100% full at the start of the simulation.
00464* # river cross-section for summer conditions.
00465* # It was assumed that for up to this depth, the wetland starts to significantly store water.
00466* # 0.75 m of water, the main channel of the river provided the storage. Above
00467* # this depth, the wetland starts to significantly store water.
00468* # 00020:000054 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00469* ADD HVD
00470*   + 1.0 02:02:00:1 38743.00 40.474 No.Date 43:31 11.82 n/a .000
00471*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 38743.00 23.265 No.Date 55:09 11.82 n/a .000
00472*   [L/S(n= 3056*) / .082, .025]
00473*   [Vmax=.432*Dmax=.808]
00474* # 00020:000055 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00475* ADD HVD
00476*   + 1.0 02:02:00:1 38743.00 23.265 No.Date 55:09 11.82 n/a .000
00477* # Sum of hydrographs from Node 7 routed to Node 6
00478* # Section 5
00479* # 00020:000056 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00480* ADD HVD
00481*   + 1.0 02:02:00:1 38743.00 23.265 No.Date 55:09 11.82 n/a .000
00482*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 38743.00 23.268 No.Date 56:18 11.82 n/a .000
00483*   [L/S(n= 3056*) / .082, .025]
00484*   [Vmax=.432*Dmax=.808]
00485* # 00020:000057 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00486* ADD HVD
00487*   + 1.0 02:02:00:1 38743.00 23.265 No.Date 56:18 11.82 n/a .000
00488*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 38743.00 23.268 No.Date 56:18 11.82 n/a .000
00489*   [L/S(n= 3056*) / .082, .025]
00490*   [Vmax=.432*Dmax=.808]
00491* # 00020:000058 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00492* ADD HVD
00493*   + 1.0 02:02:00:1 38743.00 23.268 No.Date 56:18 11.82 n/a .000
00494*   SUM: 1.0 01:08:1_N10 40240.01 23.318 No.Date 56:18 11.89 n/a .000
00495* # Sum of hydrographs from Node 6 routed to Node 5
00496* # Section 6
00497* # 00020:000059 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00498* ADD HVD
00499*   + 1.0 02:02:00:1 40240.01 23.318 No.Date 56:18 11.89 n/a .000
00500*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.325 No.Date 56:19 11.89 n/a .000
00501*   [L/S(n= 1852*) / .044, .035]
00502* # 00020:000060 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00503* ADD HVD
00504*   + 1.0 02:02:00:1 40240.01 23.325 No.Date 56:19 11.89 n/a .000
00505*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.328 No.Date 56:20 11.89 n/a .000
00506*   [L/S(n= 1852*) / .044, .035]
00507* # 00020:000061 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00508* ADD HVD
00509*   + 1.0 02:02:00:1 40240.01 23.328 No.Date 56:20 11.89 n/a .000
00510*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.331 No.Date 56:21 11.89 n/a .000
00511* # Sum of hydrographs from Node 5 routed to Node 4
00512* # Section 7
00513* # 00020:000062 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00514* ADD HVD
00515*   + 1.0 02:02:00:1 40240.01 23.331 No.Date 56:21 11.89 n/a .000
00516*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.338 No.Date 56:22 11.89 n/a .000
00517*   [L/S(n= 1852*) / .044, .035]
00518*   [Vmax=.443*Dmax=.937]
00519* # 00020:000063 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00520* ADD HVD
00521*   + 1.0 02:02:00:1 40240.01 23.338 No.Date 56:22 11.89 n/a .000
00522*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.341 No.Date 56:23 11.89 n/a .000
00523*   [L/S(n= 1852*) / .044, .035]
00524*   [Vmax=.443*Dmax=.937]
00525* # 00020:000064 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00526* ADD HVD
00527*   + 1.0 02:02:00:1 40240.01 23.341 No.Date 56:23 11.89 n/a .000
00528*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.344 No.Date 56:24 11.89 n/a .000
00529*   [L/S(n= 1852*) / .044, .035]
00530* # 00020:000065 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00531* ADD HVD
00532*   + 1.0 02:02:00:1 40240.01 23.344 No.Date 56:24 11.89 n/a .000
00533*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.347 No.Date 56:25 11.89 n/a .000
00534*   [L/S(n= 1852*) / .044, .035]
00535*   [Vmax=.443*Dmax=.937]
00536* # 00020:000066 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00537* ADD HVD
00538*   + 1.0 02:02:00:1 40240.01 23.347 No.Date 56:25 11.89 n/a .000
00539*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.350 No.Date 56:26 11.89 n/a .000
00540*   [L/S(n= 1852*) / .044, .035]
00541*   [Vmax=.443*Dmax=.937]
00542* # 00020:000067 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00543* ADD HVD
00544*   + 1.0 02:02:00:1 40240.01 23.350 No.Date 56:26 11.89 n/a .000
00545*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.353 No.Date 56:27 11.89 n/a .000
00546*   [L/S(n= 1852*) / .044, .035]
00547*   [Vmax=.443*Dmax=.937]
00548* # 00020:000068 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00549* ADD HVD
00550*   + 1.0 02:02:00:1 40240.01 23.353 No.Date 56:27 11.89 n/a .000
00551*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.356 No.Date 56:28 11.89 n/a .000
00552*   [L/S(n= 1852*) / .044, .035]
00553*   [Vmax=.443*Dmax=.937]
00554* # 00020:000069 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00555* ADD HVD
00556*   + 1.0 02:02:00:1 40240.01 23.356 No.Date 56:28 11.89 n/a .000
00557*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.359 No.Date 56:29 11.89 n/a .000
00558*   [L/S(n= 1852*) / .044, .035]
00559*   [Vmax=.443*Dmax=.937]
00560* # 00020:000070 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00561* ADD HVD
00562*   + 1.0 02:02:00:1 40240.01 23.359 No.Date 56:29 11.89 n/a .000
00563*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.362 No.Date 56:30 11.89 n/a .000
00564*   [L/S(n= 1852*) / .044, .035]
00565*   [Vmax=.443*Dmax=.937]
00566* # 00020:000071 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00567* ADD HVD
00568*   + 1.0 02:02:00:1 40240.01 23.362 No.Date 56:30 11.89 n/a .000
00569*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.365 No.Date 56:31 11.89 n/a .000
00570*   [L/S(n= 1852*) / .044, .035]
00571*   [Vmax=.443*Dmax=.937]
00572* # 00020:000072 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00573* ADD HVD
00574*   + 1.0 02:02:00:1 40240.01 23.365 No.Date 56:31 11.89 n/a .000
00575*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.368 No.Date 56:32 11.89 n/a .000
00576*   [L/S(n= 1852*) / .044, .035]
00577*   [Vmax=.443*Dmax=.937]
00578* # 00020:000073 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00579* ADD HVD
00580*   + 1.0 02:02:00:1 40240.01 23.368 No.Date 56:32 11.89 n/a .000
00581*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.371 No.Date 56:33 11.89 n/a .000
00582*   [L/S(n= 1852*) / .044, .035]
00583*   [Vmax=.443*Dmax=.937]
00584* # 00020:000074 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00585* ADD HVD
00586*   + 1.0 02:02:00:1 40240.01 23.371 No.Date 56:33 11.89 n/a .000
00587*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.374 No.Date 56:34 11.89 n/a .000
00588*   [L/S(n= 1852*) / .044, .035]
00589*   [Vmax=.443*Dmax=.937]
00590* # 00020:000075 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00591* ADD HVD
00592*   + 1.0 02:02:00:1 40240.01 23.374 No.Date 56:34 11.89 n/a .000
00593*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.377 No.Date 56:35 11.89 n/a .000
00594*   [L/S(n= 1852*) / .044, .035]
00595*   [Vmax=.443*Dmax=.937]
00596* # 00020:000076 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00597* ADD HVD
00598*   + 1.0 02:02:00:1 40240.01 23.377 No.Date 56:35 11.89 n/a .000
00599*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.380 No.Date 56:36 11.89 n/a .000
00600*   [L/S(n= 1852*) / .044, .035]
00601*   [Vmax=.443*Dmax=.937]
00602* # 00020:000077 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00603* ADD HVD
00604*   + 1.0 02:02:00:1 40240.01 23.380 No.Date 56:36 11.89 n/a .000
00605*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.383 No.Date 56:37 11.89 n/a .000
00606*   [L/S(n= 1852*) / .044, .035]
00607*   [Vmax=.443*Dmax=.937]
00608* # 00020:000078 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00609* ADD HVD
00610*   + 1.0 02:02:00:1 40240.01 23.383 No.Date 56:37 11.89 n/a .000
00611*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.386 No.Date 56:38 11.89 n/a .000
00612*   [L/S(n= 1852*) / .044, .035]
00613*   [Vmax=.443*Dmax=.937]
00614* # 00020:000079 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00615* ADD HVD
00616*   + 1.0 02:02:00:1 40240.01 23.386 No.Date 56:38 11.89 n/a .000
00617*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.389 No.Date 56:39 11.89 n/a .000
00618*   [L/S(n= 1852*) / .044, .035]
00619*   [Vmax=.443*Dmax=.937]
00620* # 00020:000080 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00621* ADD HVD
00622*   + 1.0 02:02:00:1 40240.01 23.389 No.Date 56:39 11.89 n/a .000
00623*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.392 No.Date 56:40 11.89 n/a .000
00624*   [L/S(n= 1852*) / .044, .035]
00625*   [Vmax=.443*Dmax=.937]
00626* # 00020:000081 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00627* ADD HVD
00628*   + 1.0 02:02:00:1 40240.01 23.392 No.Date 56:40 11.89 n/a .000
00629*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.395 No.Date 56:41 11.89 n/a .000
00630*   [L/S(n= 1852*) / .044, .035]
00631*   [Vmax=.443*Dmax=.937]
00632* # 00020:000082 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00633* ADD HVD
00634*   + 1.0 02:02:00:1 40240.01 23.395 No.Date 56:41 11.89 n/a .000
00635*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.398 No.Date 56:42 11.89 n/a .000
00636*   [L/S(n= 1852*) / .044, .035]
00637*   [Vmax=.443*Dmax=.937]
00638* # 00020:000083 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00639* ADD HVD
00640*   + 1.0 02:02:00:1 40240.01 23.398 No.Date 56:42 11.89 n/a .000
00641*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.401 No.Date 56:43 11.89 n/a .000
00642*   [L/S(n= 1852*) / .044, .035]
00643*   [Vmax=.443*Dmax=.937]
00644* # 00020:000084 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00645* ADD HVD
00646*   + 1.0 02:02:00:1 40240.01 23.401 No.Date 56:43 11.89 n/a .000
00647*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.404 No.Date 56:44 11.89 n/a .000
00648*   [L/S(n= 1852*) / .044, .035]
00649*   [Vmax=.443*Dmax=.937]
00650* # 00020:000085 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00651* ADD HVD
00652*   + 1.0 02:02:00:1 40240.01 23.404 No.Date 56:44 11.89 n/a .000
00653*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.407 No.Date 56:45 11.89 n/a .000
00654*   [L/S(n= 1852*) / .044, .035]
00655*   [Vmax=.443*Dmax=.937]
00656* # 00020:000086 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00657* ADD HVD
00658*   + 1.0 02:02:00:1 40240.01 23.407 No.Date 56:45 11.89 n/a .000
00659*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.410 No.Date 56:46 11.89 n/a .000
00660*   [L/S(n= 1852*) / .044, .035]
00661*   [Vmax=.443*Dmax=.937]
00662* # 00020:000087 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00663* ADD HVD
00664*   + 1.0 02:02:00:1 40240.01 23.410 No.Date 56:46 11.89 n/a .000
00665*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.413 No.Date 56:47 11.89 n/a .000
00666*   [L/S(n= 1852*) / .044, .035]
00667*   [Vmax=.443*Dmax=.937]
00668* # 00020:000088 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00669* ADD HVD
00670*   + 1.0 02:02:00:1 40240.01 23.413 No.Date 56:47 11.89 n/a .000
00671*   [RDtv 1.00] cut-> 1.0 01:08:1_N10 40240.01 23.416 No.Date 56:48 11.89 n/a .000
00672*   [L/S(n= 1852*) / .044, .035]
00673*   [Vmax=.443*Dmax=.937]
00674* # 00020:000089 -> DTMN-ID:NHNDY -> AREBAA-QPEAKcms-TpeakDate_hh:mm--> RVNm-R.C.--DWFcms
00675* ADD HVD
00676*   + 1.0 02:02:00:1 
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01123+ [SMIN= 31.15 : SMAX=207.66 : SK\_ .010 ]

01124+ R0022:CO0153-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-B.C.---DWFcms

01125+ ROUTE RESERVOIR <-> 1.0 02W-CLAR\_BRA 73.29 4,584 No\_date 28:07 31.34 n/a .000

01126+ outflow <-> 1.0 01MS\_PLO\_PWD 73.29 1,033 No\_date 28:50 31.34 n/a .000

01127+ overlfow <-> 1.0 03W-CLAR\_M3 73.29 1,000 No\_date 0:00 31.34 n/a .000

01128+ [Modifd-6675e-0 : m3\_TotDvVol-.000000 : m3\_N-DvF- 0. TotDurDvF- 0 hrs]

01129+ R0022:CO0154-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01130+ CONTINUOUS STANDYD 1.0 01S-1-P0-D2 4.94 .383 No\_date 28:01 31.34 .628 .000

01131+ [XIMP= 55:TIME=.65]

01132+ [LOSS= 2 : CN= 74.0 ]

01133+ [Pervious area: Apers= 4.67:SLPP= .50:LGP= 40 :MNP= .250:SCP= .0 ]

01134+ [Impervious area: AIimp= 1.57:SLP1= .50:LGI= 181 :MMI=.013:SCI= .0 ]

01135+ [iAEClipm= 4.00: iAERepers= 4.00]

01136+ [iAEClipm= 36.67 :SMAX=207.66 :SK\_ .010 ]

01137+ R0022:CO0155-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01138+ ADD HYD 1.0 02 019800-02 325.44 3,894 No\_date 29:12 28.56 n/a .000

01139+ \* SUM 1.0 01 9800-02 320.38 3,925 No\_date 29:11 28.56 n/a .000

01140+ ROUTE CHANNEL >> 1.0 01 9800-02 320.38 3,801 No\_date 29:11 28.56 n/a .000

01141+ R0022:CO0156-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01142+ SAVE HYD 320.38 3,925 No\_date 29:11 28.56 n/a .000

01143+ frame= 980.002

01144+ remark= Total Flows at Station 980 on Foster Drain

01145+ # Hydrograph from Node Foster SWM Station 980 to Node at station 520

01146+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 980

01147+ # Impervious area: Apers= 4.67:SLPP= .50:LGP= 40 :MNP= .250:SCP= .0 ]

01148+ [Pervious area: Apers= 1.57:SLP1= .50:LGI= 181 :MMI=.013:SCI= .0 ]

01149+ R0022:CO0157-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01150+ ROUTE CHANNEL >> 1.0 02 019800-02 320.38 3,925 No\_date 29:11 28.56 n/a .000

01151+ [L/S=ln .460 : .043 : .038 ]

01152+ [Vmax= .544 :IMax= 1.093 ]

01153+ [SMIN= 36.67 :SMAX=244.49 :SK\_ .010 ]

01154+ R0022:CO0158-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01155+ CONTINUOUS STANDYD 1.0 01S-1-P0-D1 5.11 .460 No\_date 28:01 31.38 .703 .000

01156+ [XIMP= 65:TIME=.65]

01157+ [LOSS= 2 : CN= 74.0 ]

01158+ [Pervious area: Apers= 4.67:SLPP= .50:LGP= 40 :MNP= .250:SCP= .0 ]

01159+ [Impervious area: AIimp= 1.57:SLP1= .50:LGI= 181 :MMI=.013:SCI= .0 ]

01160+ [iAEClipm= 36.67 :SMAX=244.49 :SK\_ .010 ]

01161+ R0022:CO0159-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01162+ ADD HYD 1.0 02 019800-02 320.38 3,891 No\_date 29:21 28.56 n/a .000

01163+ \* SUM 1.0 01 5120-02 335.48 3,832 No\_date 29:21 28.56 n/a .000

01164+ R0022:CO0160-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01165+ SAVE HYD 1.0 01 5120-02 335.49 3,832 No\_date 29:21 28.62 n/a .000

01166+ frame= 520.002

01167+ remark= Total Flows at Station 520 on Foster Drain

01168+ # Hydrograph from Node at Station 520 (Foster Drain) to Node at station 6016 (Jock River)

01169+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 520

01170+ # Impervious area: Apers= 4.67:SLPP= .50:LGP= 40 :MNP= .250:SCP= .0 ]

01171+ [Pervious area: Apers= 1.57:SLP1= .50:LGI= 181 :MMI=.013:SCI= .0 ]

01172+ [L/S=ln .860 : .587 : .035 ]

01173+ [Vmax= .544 :IMax= 1.093 ]

01174+ R0022:CO0162-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01175+ CONTINUOUS STANDYD 1.0 01S-1-P0-F-D 14.96 1,215 No\_date 28:02 31.38 .703 .000

01176+ [XIMP= 65:TIME=.65]

01177+ [LOSS= 2 : CN= 74.0 ]

01178+ [Pervious area: Apers= 4.67:SLPP= .50:LGP= 40 :MNP= .250:SCP= .0 ]

01179+ [Impervious area: AIimp= 1.57:SLP1= .50:LGI= 181 :MMI=.013:SCI= .0 ]

01180+ [iAEClipm= 4.00: iAERepers= 4.00]

01181+ [SMIN= 36.67 :SMAX=244.49 :SK\_ .010 ]

01182+ R0022:CO0163-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01183+ CONTINUOUS STANDYD 1.0 01S-1-P0-F-D 8.27 .475 No\_date 28:02 23.32 .512 .000

01184+ [XIMP= 65:TIME=.65]

01185+ [LOSS= 2 : CN= 74.0 ]

01186+ [Pervious area: Apers= 4.67:SLPP= .50:LGP= 40 :MNP= .250:SCP= .0 ]

01187+ [Impervious area: AIimp= 1.57:SLP1= .50:LGI= 181 :MMI=.013:SCI= .0 ]

01188+ [iAEClipm= 4.00: iAERepers= 4.00]

01189+ [SMIN= 36.67 :SMAX=244.49 :SK\_ .010 ]

01190+ R0022:CO0164-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01191+ CONTINUOUS STANDYD 1.0 01S-1-P0-F-D 75.84 .912 No\_date 28:37 14.83 .326 .000

01192+ [XIMP= 65:TIME=.65]

01193+ [LOSS= 2 : CN= 74.0 ]

01194+ [Pervious area: Apers= 4.67:SLPP= .50:LGP= 40 :MNP= .250:SCP= .0 ]

01195+ [Impervious area: AIimp= 1.57:SLP1= .50:LGI= 181 :MMI=.013:SCI= .0 ]

01196+ [iAEClipm= 4.00: iAERepers= 4.00]

01197+ [SMIN= 31.05 :SMAX=207.66 :SK\_ .010 ]

01198+ R0022:CO0165-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01199+ CONTINUOUS STANDYD 1.0 01W-CLAR\_UND 35.65 .286 No\_date 29:12 14.83 .326 .000

01200+ [CN= 77.0 : NO 3.00 :Tp= 1.0 ]

01201+ [XIMP= 65:TIME=.65]

01202+ [INTERVENTIME= 12.00 ]

01203+ R0022:CO0166-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01204+ ADD HYD 1.0 02 019800-02 520.70 4,587 No\_date 28:35 12.82 .510 .000

01205+ \* SUM 1.0 02 5120-02 335.49 3,792 No\_date 29:34 28.62 n/a .000

01206+ 1.0 02 M2MS\_PWD 73.29 1,033 No\_date 28:50 31.34 n/a .000

01207+ 1.0 02 019800-02 320.38 3,891 No\_date 29:21 28.56 n/a .000

01208+ 1.0 02 01W-CLAR\_UND 35.65 .286 No\_date 29:12 14.83 n/a .000

01209+ 1.0 02 018-1-P0-D1 14.96 1,215 No\_date 28:01 31.38 n/a .000

01210+ 1.0 02 018-1-P0-F-D 14.96 1,215 No\_date 28:01 31.38 n/a .000

01211+ 1.0 02 019800-02 320.38 3,891 No\_date 29:37 14.83 n/a .000

01212+ 1.0 02 01W-CLAR\_UND 57.88 1,414 No\_date 28:42 12.95 n/a .000

01213+ R0022:CO0167-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01214+ SAVE HYD 1.0 01 5120-02 5418.36 49.014 No\_date 34:32 12.96 n/a .000

01215+ frame= 520.002

01216+ remark= Total Flows at Foster Drain

01217+ # Hydrograph from Node Foster routed to Node at Cedarview Road

01218+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 6016

01219+ # Impervious area: Apers= 4.67:SLPP= .50:LGP= 40 :MNP= .250:SCP= .0 ]

01220+ [Pervious area: AIimp= 1.57:SLP1= .75:LGI= 187 :MMI=.013:SCI= .0 ]

01221+ [L/S=ln .159 : .082 : .035 ]

01222+ [Vmax= .544 :IMax= 1.093 ]

01223+ R0022:CO0168-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01224+ CONTINUOUS STANDYD 1.0 01S-1-P0-F-D 12.00 .100 No\_date 28:37 14.83 .326 .000

01225+ [XIMP= 65:TIME=.65]

01226+ [LOSS= 2 : CN= 74.0 ]

01227+ [Pervious area: Apers= 4.67:SLPP= .50:LGP= 40 :MNP= .250:SCP= .0 ]

01228+ [Primarily agricultural fields: portion of sand quarry

01229+ R0022:CO0169-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01230+ CONTINUOUS STANDYD 1.0 01S-1-B 55.36 .849 No\_date 28:24 14.83 .326 .000

01231+ [XIMP= 4.00 : SMIN= 31.05 :SMAX=207.66 :SK\_ .010 ]

01232+ [INTERVENTIME= 12.00 ]

01233+ R0022:CO0170-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01234+ CONTINUOUS STANDYD 1.0 01W-CLAR\_UND 35.65 .286 No\_date 29:12 14.83 .326 .000

01235+ [XIMP= 4.00 : SMIN= 31.05 :SMAX=207.66 :SK\_ .010 ]

01236+ R0022:CO0171-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01237+ CONTINUOUS STANDYD 1.0 01S-1-B 3.26 .322 No\_date 28:00 32.20 .707 .000

01238+ [INTERVENTIME= 12.00 ]

01239+ R0022:CO0172-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01240+ CONTINUOUS STANDYD 1.0 01S-1-P0-D 27.01 1,867 No\_date 28:02 32.20 .707 .000

01241+ [XIMP= 65:TIME=.65]

01242+ [LOSS= 2 : CN= 74.0 ]

01243+ [Pervious area: Apers= 4.67:SLPP= .50:LGP= 40 :MNP= .250:SCP= .0 ]

01244+ [iAEClipm= 4.00 : iAERepers= 4.00]

01245+ [iAEClipm= 31.81 :SMAX=225.43 :SK\_ .010 ]

01246+ R0022:CO0173-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01247+ CONTINUOUS STANDYD 1.0 01S-1-P0-D 1.75 .176 No\_date 28:00 32.20 .707 .000

01248+ [XIMP= 65:TIME=.65]

01249+ [LOSS= 2 : CN= 75.0 ]

01250+ [Pervious area: Apers= 4.67:SLPP= .50:LGP= 40 :MNP= .250:SCP= .0 ]

01251+ [iAEClipm= 4.00 : iAERepers= 4.00]

01252+ [iAEClipm= 33.81 :SMAX=225.43 :SK\_ .010 ]

01253+ R0022:CO0174-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01254+ CONTINUOUS STANDYD 1.0 01S-1-P0-D 2.03 .204 No\_date 28:00 32.20 .707 .000

01255+ [XIMP= 65:TIME=.65]

01256+ [LOSS= 2 : CN= 75.0 ]

01257+ [Pervious area: Apers= 4.67:SLPP= .50:LGP= 40 :MNP= .250:SCP= .0 ]

01258+ [iAEClipm= 4.00 : iAERepers= 4.00]

01259+ [iAEClipm= 33.81 :SMAX=225.43 :SK\_ .010 ]

01260+ R0022:CO0175-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01261+ CONTINUOUS STANDYD 1.0 01W-CLAR\_M3 17.77 .141 No\_date 28:00 27.78 .610 .000

01262+ [XIMP= 4.00 : SMIN= 31.15 :SMAX=207.66 :SK\_ .010 ]

01263+ [INTERVENTIME= 12.00 ]

01264+ R0022:CO0176-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01265+ ROUTE RESERVOIR >-> 1.0 02W-CLAR\_M3 1.77 .141 No\_date 28:00 27.78 n/a .000

01266+ overflow <-> 1.0 03W-CLAR\_M3 .00 .000 No\_date 0:00 0 n/a .000

01267+ [Modifd-6675e-0 : m3\_TotDvVol-.000000 : m3\_N-DvF- 0. TotDurDvF- 0 hrs]

01268+ R0022:CO0177-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01269+ CONTINUOUS STANDYD 1.0 01W-CLAR\_ALL 119.40 7.746 No\_date 28:06 31.31 .689 .000

01270+ [XIMP= 4.00 : iAERepers= 4.00]

01271+ [iAEClipm= 31.15 :SMAX=207.66 :SK\_ .010 ]

01272+ R0022:CO0178-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01273+ CONTINUOUS STANDYD 1.0 01W-CLAR\_M3 1.77 .141 No\_date 28:00 27.78 n/a .000

01274+ [XIMP= 4.00 : SMIN= 31.15 :SMAX=207.66 :SK\_ .010 ]

01275+ [INTERVENTIME= 12.00 ]

01276+ R0022:CO0179-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01277+ CONTINUOUS STANDYD 1.0 01W-CLAR\_M3 1.77 .141 No\_date 28:00 27.78 n/a .000

01278+ [XIMP= 4.00 : iAERepers= 4.00]

01279+ # To West Clarke Drain (south of the Jock)

01280+ # 20-10-11 update to clarify drainage Area to a 121 ha based on P598(04)-11

01281+ # 20-10-11 update to split Clarke Tributary drainage Area to MAJOR and MINOR

01282+ # 20-11-01 update to clarify drainage Area to MAJOR and MINOR

01283+ R0022:CO0179-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01284+ CONTINUOUS STANDYD 1.0 01W-CLAR\_M3 1.77 .141 No\_date 28:00 27.78 .610 .000

01285+ [XIMP= 4.00 : iAERepers= 4.00]

01286+ [iAEClipm= 31.15 :SMAX=207.66 :SK\_ .010 ]

01287+ R0022:CO0180-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01288+ CONTINUOUS STANDYD 1.0 01W-CLAR\_M3 1.77 .141 No\_date 28:00 27.78 n/a .000

01289+ [XIMP= 4.00 : iAERepers= 4.00]

01290+ [iAEClipm= 31.15 :SMAX=207.66 :SK\_ .010 ]

01291+ R0022:CO0181-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01292+ CONTINUOUS STANDYD 1.0 01W-CLAR\_M3 1.77 .141 No\_date 28:00 27.78 n/a .000

01293+ [XIMP= 4.00 : iAERepers= 4.00]

01294+ [iAEClipm= 31.15 :SMAX=207.66 :SK\_ .010 ]

01295+ R0022:CO0182-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01296+ CONTINUOUS STANDYD 1.0 01W-CLAR\_M3 1.77 .141 No\_date 28:00 27.78 n/a .000

01297+ [XIMP= 4.00 : iAERepers= 4.00]

01298+ [iAEClipm= 31.15 :SMAX=207.66 :SK\_ .010 ]

01299+ R0022:CO0183-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01300+ CONTINUOUS STANDYD 1.0 01W-CLAR\_M3 1.77 .141 No\_date 28:00 27.78 n/a .000

01301+ [XIMP= 4.00 : iAERepers= 4.00]

01302+ [iAEClipm= 31.15 :SMAX=207.66 :SK\_ .010 ]

01303+ R0022:CO0184-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01304+ CONTINUOUS STANDYD 1.0 01W-CLAR\_M3 1.77 .141 No\_date 28:00 27.78 n/a .000

01305+ [XIMP= 4.00 : iAERepers= 4.00]

01306+ [iAEClipm= 31.15 :SMAX=207.66 :SK\_ .010 ]

01307+ ADD HYD 1.0 02W-CLAR\_M3 .00 .000 No\_date 0:00 0 n/a .000

01308+ \* 1.0 02W-CLAR\_M3 .00 .000 No\_date 0:00 0 n/a .000

01309+ SUM 1.0 01W-CLAR\_M3 119.40 7.746 No\_date 28:06 31.34 n/a .000

01310+ frame= 980.002

01311+ remark= Total Flows at Station 980 on Foster Drain

01312+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 980

01313+ R0022:CO0157-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01314+ ROUTE CHANNEL >> 1.0 02 019800-02 325.44 3,894 No\_date 29:12 28.56 n/a .000

01315+ [L/S=ln .460 : .043 : .038 ]

01316+ [Vmax= .544 :IMax= 1.093 ]

01317+ R0022:CO0158-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01318+ CONTINUOUS STANDYD 1.0 01S-1-P0-D1 5.11 .460 No\_date 28:01 31.34 .628 .000

01319+ [XIMP= 65:TIME=.65]

01320+ [LOSS= 2 : CN= 74.0 ]

01321+ [Pervious area: Apers= 4.67:SLPP= .50:LGP= 40 :MNP= .250:SCP= .0 ]

01322+ [Impervious area: AIimp= 1.57:SLP1= .50:LGI= 181 :MMI=.013:SCI= .0 ]

01323+ R0022:CO0159-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01324+ ADD HYD 1.0 02 019800-02 325.44 3,894 No\_date 29:12 28.56 n/a .000

01325+ \* SUM 1.0 01 5120-02 335.49 3,832 No\_date 29:21 28.62 n/a .000

01326+ ROUTE CHANNEL >> 1.0 02 019800-02 335.49 3,832 No\_date 29:21 28.62 n/a .000

01327+ [L/S=ln .460 : .043 : .038 ]

01328+ [Vmax= .544 :IMax= 1.093 ]

01329+ R0022:CO0160-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01330+ CONTINUOUS STANDYD 1.0 01S-1-P0-D1 5.11 .460 No\_date 28:01 31.34 .628 .000

01331+ [XIMP= 65:TIME=.65]

01332+ [LOSS= 2 : CN= 74.0 ]

01333+ [Pervious area: Apers= 4.67:SLPP= .50:LGP= 40 :MNP= .250:SCP= .0 ]

01334+ [Impervious area: AIimp= 1.57:SLP1= .50:LGI= 181 :MMI=.013:SCI= .0 ]

01335+ R0022:CO0161-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01336+ CONTINUOUS STANDYD 1.0 01S-1-P0-D1 5.11 .460 No\_date 28:01 31.34 .628 .000

01337+ [XIMP= 65:TIME=.65]

01338+ [LOSS= 2 : CN= 74.0 ]

01339+ [Pervious area: Apers= 4.67:SLPP= .50:LGP= 40 :MNP= .250:SCP= .0 ]

01340+ [Impervious area: AIimp= 1.57:SLP1= .50:LGI= 181 :MMI=.013:SCI= .0 ]

01341+ R0022:CO0162-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01342+ CONTINUOUS STANDYD 1.0 01S-1-P0-D1 5.11 .460 No\_date 28:01 31.34 .628 .000

01343+ [XIMP= 65:TIME=.65]

01344+ [LOSS= 2 : CN= 74.0 ]

01345+ [Pervious area: Apers= 4.67:SLPP= .50:LGP= 40 :MNP= .250:SCP= .0 ]

01346+ [Impervious area: AIimp= 1.57:SLP1= .50:LGI= 181 :MMI=.013:SCI= .0 ]

01347+ R0022:CO0163-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01348+ CONTINUOUS STANDYD 1.0 01S-1-P0-D1 5.11 .460 No\_date 28:01 31.34 .628 .000

01349+ [XIMP= 65:TIME=.65]

01350+ [LOSS= 2 : CN= 74.0 ]

01351+ [Pervious area: Apers= 4.67:SLPP= .50:LGP= 40 :MNP= .250:SCP= .0 ]

01352+ [Impervious area: AIimp= 1.57:SLP1= .50:LGI= 181 :MMI=.013:SCI= .0 ]

01353+ R0022:CO0164-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01354+ CONTINUOUS STANDYD 1.0 01S-1-P0-D1 5.11 .460 No\_date 28:01 31.34 .628 .000

01355+ [XIMP= 65:TIME=.65]

01356+ [LOSS= 2 : CN= 74.0 ]

01357+ [Pervious area: Apers= 4.67:SLPP= .50:LGP= 40 :MNP= .250:SCP= .0 ]

01358+ [Impervious area: AIimp= 1.57:SLP1= .50:LGI= 181 :MMI=.013:SCI= .0 ]

01359+ R0022:CO0165-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01360+ CONTINUOUS STANDYD 1.0 01S-1-P0-D1 5.11 .460 No\_date 28:01 31.34 .628 .000

01361+ [XIMP= 65:TIME=.65]

01362+ [LOSS= 2 : CN= 74.0 ]

01363+ [Pervious area: Apers= 4.67:SLPP= .50:LGP= 40 :MNP= .250:SCP= .0 ]

01364+ [Impervious area: AIimp= 1.57:SLP1= .50:LGI= 181 :MMI=.013:SCI= .0 ]

01365+ R0022:CO0166-----> Dtnin:ID:NHYD---> AREAh-APEAKcms-TpeakDate\_bh:mm:---Rvms-R.C.---DWFcms

01366+ CONTINUOUS STANDYD 1.0 01S-

This file contains a large amount of hydrological data and model parameters for various basins across the state of New Mexico. The data includes precipitation, streamflow, and model outputs for different subwatersheds and basins. The file is organized into sections for different basins and subwatersheds, with specific parameters and data points listed for each.



02245+ [iaEClipm- 4.00: IaREOpers- 4.00]  
 02246+ [SMIN- 33.81: SMAX-22.43: SK- .010]  
 02247+ R0022:003134-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02248+ COMPUTE DUALHYD | 1.0 01:BA-MJ .76 .459 No\_date 28:02 25 .66 n/a .000  
 02249+ Major System / | 1.0 01:BA-MJ .00 .000 No\_date 0:00 0 n/a .000  
 02250+ Minor System \ | 1.0 01:BA-MJ .76 .459 No\_date 28:02 25 .66 n/a .000  
 02251+ [MjSysSto\_00000-00, TotCovFvl-00000-00, N-Ovfl- 0, TotDurOvf-.hrs] .0  
 02252+ R0022:003132-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02253+ ADD HYD \* | 1.0 01:BA-MJ .76 .459 No\_date 28:02 25 .66 n/a .000  
 02254+ \* | 1.0 02:BA-MJ .76 .459 No\_date 28:02 25 .66 n/a .000  
 02255+ SUM- | 1.0 01:BA-MJ .30 .124 No\_date 28:02 25 .66 n/a .000  
 02256+ R0022:00333-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02257+ SAVE HYD \* | 1.0 01:MH340 .25 .50 1.234 No\_date 28:05 25 .66 n/a .000  
 02258+ \* | 1.0 01:MH340 .25 .50 1.234 No\_date 28:05 25 .66 n/a .000  
 02259+ remark:Total Flows at MH340 .0  
 02260+ R0022:00334-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02261+ R0022:00334-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02262+ [S0Tz: 1.00] out-\* | 1.0 01:MH340 .25 .50 1.234 No\_date 28:07 25 .66 n/a .000  
 02263+ [\*] [L/S/nr: 240, .150/.013] .0  
 02264+ [Vmax: 1.482 Dmax: 1.685] .0  
 02265+ Dtnin: 1.685 Dmax: 1.685 .0  
 02266+ R0022:00335-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02267+ ADD HYD .0  
 02268+ \* | 1.0 02:MH104 .107 .02 5.765 No\_date 28:05 26 .32 n/a .000  
 02269+ SUM- | 1.0 01:MH104 .132 .52 6.925 No\_date 28:05 26 .19 n/a .000  
 02270+ R0022:00336-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02271+ ROUTE PIPE --> | 1.0 02:MH104 .132 .52 6.925 No\_date 28:05 26 .19 n/a .000  
 02272+ [\*] [ROTz: 1.00] out-\* | 1.0 01:104-105 .132 .52 6.452 No\_date 28:06 26 .19 n/a .000  
 02273+ [\*] [L/S/nr: 114, .120/.013] .0  
 02274+ [Vmax: 1.871 Dmax: 1.542] .0  
 02275+ [HGTn: 2.10 DWTn: 2.40] .0  
 02276+ R0022:00337-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02277+ CONTINUOUS STANDHYD | 1.0 01:BS .2.20 .187 No\_date 28:00 29 .51 .648 .000  
 02278+ [\*] [XIND: 57,TIMD: 57] .0  
 02279+ [Imperialv area: IaPep: 4.67:SLPP1-00:LDPg: 40.:MNP: .250:SCP: .0] .0  
 02280+ [Imperialv area: IaPep: 4.67:SLPP1-00:LDPg: 186.:MH1-.013:SCI: .0] .0  
 02281+ [Previous area: IaPep: 4.67:SLPP1-00:LDPg: 40.:MNP: .250:SCP: .0] .0  
 02282+ [Imperialv area: IaPep: 4.67:SLPP1-00:LDPg: 186.:MH1-.013:SCI: .0] .0  
 02283+ [SMIN- 33.81: SMAX-22.43: SK- .010] .0  
 02284+ R0022:00338-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02285+ COMPUTE DUALHYD | 1.0 01:BS-MJ .2.20 .187 No\_date 28:00 29 .51 .648 .000  
 02286+ Major System / | 1.0 01:BS-MJ .00 .000 No\_date 0:00 0 n/a .000  
 02287+ Minor System \ | 1.0 01:BS-MJ .2.20 .187 No\_date 28:00 29 .51 .648 .000  
 02288+ [MjSysSto\_00000-00, TotCovFvl-00000-00, N-Ovfl- 0, TotDurOvf-.hrs] .0  
 02289+ R0022:00339-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02290+ CONTINUOUS STANDHYD | 1.0 01:BS .2.20 .187 No\_date 28:00 29 .51 .648 .000  
 02291+ [\*] [L/S/nr: 2 CNW: 75.0] .0  
 02292+ [Previous area: IaPep: 4.67:SLPP1-00:LDPg: 40.:MNP: .250:SCP: .0] .0  
 02293+ [Imperialv area: IaPep: 4.67:SLPP1-00:LDPg: 186.:MH1-.013:SCI: .0] .0  
 02294+ [iaEClipm- 4.00: IaREOpers- 4.00] .0  
 02295+ [SMIN- 33.81: SMAX-22.43: SK- .010] .0  
 02296+ R0022:00340-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02297+ ADD HYD .0  
 02298+ \* | 1.0 02:BA-MJ .00 .000 No\_date 0:00 0 n/a .000  
 02299+ \* | 1.0 01:AB-MJ .00 .000 No\_date 28:00 24 .31 n/a .000  
 02300+ SUM- | 1.0 01:AB-MJ .00 .000 No\_date 28:00 24 .31 n/a .000  
 02301+ R0022:00341-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02302+ COMPUTE DUALHYD | 1.0 01:AB-MJ .00 .000 No\_date 28:00 24 .31 n/a .000  
 02303+ Major System / | 1.0 01:AB-MJ .00 .000 No\_date 28:00 24 .31 n/a .000  
 02304+ Minor System \ | 1.0 01:AB-MJ .00 .000 No\_date 28:00 24 .31 n/a .000  
 02305+ [MjSysSto\_00000-00, TotCovFvl-00000-00, N-Ovfl- 0, TotDurOvf-.hrs] .0  
 02306+ R0022:00342-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02307+ ADD HYD .0  
 02308+ \* | 1.0 02:104-105 .132 .52 6.452 No\_date 28:05 26 .19 n/a .000  
 02309+ \* | 1.0 01:104-105 .132 .52 6.452 No\_date 28:05 26 .19 n/a .000  
 02310+ \* | 1.0 02:TOD2\_MN3j .00 .000 No\_date 0:00 0 n/a .000  
 02311+ \* | 1.0 01:TOD2\_MN3j .00 .000 No\_date 28:00 24 .31 n/a .000  
 02312+ R0022:00343-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02313+ SAVE HYD .0  
 02314+ \* | 1.0 01:MH105 .135 .66 6.624 No\_date 28:05 26 .30 n/a .000  
 02315+ remark:Total Flows at MH105 .0  
 02316+ R0022:00344-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02317+ \* DIVERT \* | 1.0 01:AB-MJ .00 .000 No\_date 0:00 0 n/a .000  
 02318+ diverted <= | 1.0 02:AB-MJ .00 .000 No\_date 0:00 0 n/a .000  
 02319+ diverted <= | 1.0 01:03:AB-MJ-B6 .00 .000 No\_date 0:00 0 n/a .000  
 02320+ R0022:00345-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02321+ DIVERT HVMV --> | 1.0 01:MH105 .135 .68 6.624 No\_date 28:05 26 .30 n/a .000  
 02322+ diverted <= | 1.0 02:MH105 .16.59 3.620 No\_date 28:05 26 .30 n/a .000  
 02323+ diverted <= | 1.0 01:104-105 .132 .52 6.452 No\_date 28:05 26 .30 n/a .000  
 02324+ R0022:00346-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02325+ CONTINUOUS STANDHYD | 1.0 01:BT .7.19 .479 No\_date 28:01 25 .66 .564 .000  
 02326+ [\*] [L/S/nr: 1.45/.013] .0  
 02327+ [\*] [L/S/nr: 2 CNW: 75.0] .0  
 02328+ [Previous area: IaPep: 4.67:SLPP1-00:LDPg: 40.:MNP: .250:SCP: .0] .0  
 02329+ [Imperialv area: IaPep: 4.67:SLPP1-00:LDPg: 211.:MH1-.013:SCI: .0] .0  
 02330+ [iaEClipm- 4.00: IaREOpers- 4.00] .0  
 02331+ [\*] [L/S/nr: 33.81: SMAX-22.43: SK- .010] .0  
 02332+ R0022:00347-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02333+ ADD HYD .0  
 02334+ \* | 1.0 02:BT .7.19 .479 No\_date 28:01 25 .66 .564 .000  
 02335+ \* | 1.0 01:BT .7.19 .479 No\_date 28:01 25 .66 .564 .000  
 02336+ SUM- | 1.0 01:BT .7.19 .479 No\_date 28:01 25 .66 .564 .000  
 02337+ R0022:00348-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02338+ COMPUTE DUALHYD | 1.0 01:BT .7.19 .479 No\_date 28:01 25 .66 .564 .000  
 02339+ Major System / | 1.0 01:BT .00 .000 No\_date 0:00 0 n/a .000  
 02340+ Minor System \ | 1.0 01:BT .00 .000 No\_date 0:00 0 n/a .000  
 02341+ [MjSysSto\_00000-00, TotCovFvl-00000-00, N-Ovfl- 0, TotDurOvf-.hrs] .0  
 02342+ R0022:00349-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02343+ ADD HYD .0  
 02344+ \* | 1.0 02:BT .7.19 .479 No\_date 28:01 25 .66 .564 .000  
 02345+ \* | 1.0 01:BT .7.19 .479 No\_date 28:01 25 .66 .564 .000  
 02346+ SUM- | 1.0 01:BT .7.19 .479 No\_date 28:01 25 .66 .564 .000  
 02347+ R0022:00350-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02348+ CONTINUOUS STANDHYD | 1.0 01:BT .7.19 .479 No\_date 28:01 25 .66 .564 .000  
 02349+ [\*] [L/S/nr: 1.45/.013] .0  
 02350+ [\*] [L/S/nr: 2 CNW: 75.0] .0  
 02351+ [Previous area: IaPep: 4.67:SLPP1-00:LDPg: 40.:MNP: .250:SCP: .0] .0  
 02352+ [Imperialv area: IaPep: 4.67:SLPP1-00:LDPg: 211.:MH1-.013:SCI: .0] .0  
 02353+ [iaEClipm- 4.00: IaREOpers- 4.00] .0  
 02354+ [\*] [L/S/nr: 33.81: SMAX-22.43: SK- .010] .0  
 02355+ R0022:00351-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02356+ COMPUTE DUALHYD | 1.0 01:BT .7.19 .479 No\_date 28:00 25 .66 .564 .000  
 02357+ Major System / | 1.0 01:BT .00 .000 No\_date 0:00 0 n/a .000  
 02358+ Minor System \ | 1.0 01:BT .00 .000 No\_date 0:00 0 n/a .000  
 02359+ [MjSysSto\_00000-00, TotCovFvl-00000-00, N-Ovfl- 0, TotDurOvf-.hrs] .0  
 02360+ R0022:00352-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02361+ CONTINUOUS STANDHYD | 1.0 01:EX-LAND .32 .50 2.093 No\_date 28:02 26 .85 .590 .000  
 02362+ [\*] [XIND: 57,TIMD: 57] .0  
 02363+ [\*] [L/S/nr: 2 CNW: 75.0] .0  
 02364+ [Previous area: IaPep: 4.67:SLPP1-00:LDPg: 40.:MNP: .250:SCP: .0] .0  
 02365+ [Imperialv area: IaPep: 4.67:SLPP1-00:LDPg: 186.:MH1-.013:SCI: .0] .0  
 02366+ [iaEClipm- 4.00: IaREOpers- 4.00] .0  
 02367+ [\*] [L/S/nr: 33.81: SMAX-22.43: SK- .010] .0  
 02368+ R0022:00353-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02369+ COMPUTE DUALHYD | 1.0 01:EX-LAND .32 .50 .29 .093 No\_date 28:00 25 .66 n/a .000  
 02370+ Major System / | 1.0 01:EX-LAND .00 .000 No\_date 0:00 0 n/a .000  
 02371+ Minor System \ | 1.0 01:EX-LAND .32 .50 .29 .093 No\_date 28:02 26 .85 n/a .000  
 02372+ [MjSysSto\_00000-00, TotCovFvl-00000-00, N-Ovfl- 0, TotDurOvf-.hrs] .0  
 02373+ R0022:00354-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02374+ ADD HYD .0  
 02375+ \* | 1.0 02:BT .7.19 .479 No\_date 28:00 25 .66 n/a .000  
 02376+ \* | 1.0 01:BT .7.19 .479 No\_date 28:00 25 .66 n/a .000  
 02377+ \* | 1.0 02:BE-MJ .00 .000 No\_date 0:00 0 n/a .000  
 02378+ \* | 1.0 01:BE-MJ .00 .000 No\_date 0:00 0 n/a .000  
 02379+ SUM- | 1.0 01:BE-MJ .00 .000 No\_date 27:43 25 .67 n/a .000  
 02380+ R0022:00355-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02381+ COMPUTE DUALHYD | 1.0 01:BE-MJ .3.20 .064 No\_date 27:43 25 .67 n/a .000  
 02382+ Major System / | 1.0 01:BE-MJ .00 .000 No\_date 0:00 0 n/a .000  
 02383+ Minor System \ | 1.0 01:BE-MJ .3.20 .064 No\_date 27:43 25 .67 n/a .000  
 02384+ [MjSysSto\_00000-00, TotCovFvl-00000-00, N-Ovfl- 0, TotDurOvf-.hrs] .0  
 02385+ R0022:00356-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02386+ R0022:00357-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02387+ [\*] [L/S/nr: 208, .100/.013] .0  
 02388+ [\*] [L/S/nr: 109-104-106A .119 .09 3.054 No\_date 28:08 26 .35 n/a .000  
 02389+ [\*] [L/S/nr: 208, .100/.013] .0  
 02390+ [\*] [L/S/nr: 109-104-106A .119 .09 3.056 No\_date 28:08 26 .35 n/a .000  
 02391+ [\*] [L/S/nr: 109-104-106A .120 .57 3.466 No\_date 28:03 26 .25 n/a .000  
 02392+ R0022:00358-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02393+ ADD HYD .0  
 02394+ \* | 1.0 01:MH108A .120 .57 3.466 No\_date 28:03 26 .25 n/a .000  
 02395+ \* | 1.0 01:MH108A .120 .57 3.466 No\_date 28:03 26 .25 n/a .000  
 02396+ SUM- | 1.0 01:MH108A .120 .57 3.466 No\_date 28:03 26 .25 n/a .000  
 02397+ R0022:00359-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02398+ CONTINUOUS STANDHYD | 1.0 01:MH108A .2.44 .240 No\_date 28:01 34 .21 .752 .000  
 02399+ [\*] [XIND: 71,TIMD: 71] .0  
 02400+ [\*] [L/S/nr: 123, .100/.013] .0  
 02401+ remark:Total Flows at MH108 .0  
 02402+ R0022:00360-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02403+ ROUTE PIPE --> | 1.0 02:MH108A .129 .57 3.466 No\_date 28:03 26 .25 n/a .000  
 02404+ [\*] [ROTz: 1.00] out-\* | 1.0 01:104-106A .129 .57 3.466 No\_date 28:04 26 .25 n/a .000  
 02405+ [\*] [L/S/nr: 109-104-106A .129 .57 3.466 No\_date 28:04 26 .25 n/a .000  
 02406+ [\*] [L/S/nr: 109-104-106A .129 .57 3.466 No\_date 28:04 26 .25 n/a .000  
 02407+ [\*] [L/S/nr: 109-104-106A .129 .57 3.466 No\_date 28:04 26 .25 n/a .000  
 02408+ [\*] [L/S/nr: 109-104-106A .129 .57 3.466 No\_date 28:04 26 .25 n/a .000  
 02409+ [\*] [L/S/nr: 109-104-106A .129 .57 3.466 No\_date 28:04 26 .25 n/a .000  
 02410+ [\*] [L/S/nr: 109-104-106A .129 .57 3.466 No\_date 28:04 26 .25 n/a .000  
 02411+ [\*] [L/S/nr: 109-104-106A .129 .57 3.466 No\_date 28:04 26 .25 n/a .000  
 02412+ [\*] [L/S/nr: 109-104-106A .129 .57 3.466 No\_date 28:04 26 .25 n/a .000  
 02413+ [\*] [L/S/nr: 109-104-106A .129 .57 3.466 No\_date 28:04 26 .25 n/a .000  
 02414+ [\*] [L/S/nr: 109-104-106A .129 .57 3.466 No\_date 28:04 26 .25 n/a .000  
 02415+ [\*] [L/S/nr: 109-104-106A .129 .57 3.466 No\_date 28:04 26 .25 n/a .000  
 02416+ R0022:00361-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02417+ COMPUTE DUALHYD | 1.0 01:MH108A .2.44 .240 No\_date 28:03 26 .25 n/a .000  
 02418+ Major System / | 1.0 01:MH108A .00 .000 No\_date 0:00 0 n/a .000  
 02419+ Minor System \ | 1.0 01:MH108A .2.44 .240 No\_date 28:03 26 .25 n/a .000  
 02420+ R0022:00362-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02421+ ADD HYD .0  
 02422+ \* | 1.0 02:MH108A .129 .57 3.466 No\_date 28:03 26 .25 n/a .000  
 02423+ \* | 1.0 01:MH108A .129 .57 3.466 No\_date 28:03 26 .25 n/a .000  
 02424+ SUM- | 1.0 01:MH108A .129 .57 3.466 No\_date 28:03 26 .25 n/a .000  
 02425+ R0022:00363-----Dtnin-ID:NHYD---ARArh-QPEAKcms-TpeakDate\_bh:mm--->Rvnm-R.C.--DWFcms  
 02426+ [\*] [ROTz: 1.00] out-\* | 1.0 01:MH108A .129 .57 3.466 No\_date 28:04 26 .25 n/a .000  
 02427+ [\*] [L/S/nr: 123, .100/.013] .0  
 02428+ [\*] [L/S/nr: 123, .100/.013] .0  
 02429+ [\*] [L/S/nr: 123, .100/.013] .0  
 02430+ [\*] [L/S/nr: 123, .100/.013] .0  
 02431+ [\*] [L/S/nr: 123, .100/.013] .0



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02993* # Sum of hydrographs from Node 12 routed to Node 11
02994* # (Approximated cross-section - see cross-section 288)
02995* # Use n=0.04 for summer conditions and n=0.328 for spring conditions
02996* # Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
02997* # Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
02998* R0005:00038-----Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
02999* ROUTE CHANNEL: > 1.0 0218_S.N11 9506.00 10.383 No_date 33:07 15.96 n/a .000
03000* [ROT( 1.001) out-< 1.0 0181_N11 9506.00 10.383 No_date 33:07 15.96 n/a .000
03001* [L/S/nm .972 / .054/.040]
03002* [Vmax=.648*Imax.2.406]
03003* #
03004* # Addition of Subwatershed 11 and Name Creek to Node 11
03005* # Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03006* ROUTE CHANNEL: > 1.0 0218_S.N11 9506.00 10.383 No_date 33:07 15.96 n/a .000
03007* [ROT( 1.001) out-< 1.0 0181_N11 9506.00 10.383 No_date 33:07 15.96 n/a .000
03008* [L/S/nm14028 / .157/.040]
03009* [Vmax=.461*Imax.1.087]
03010* #
03011* SUM: 1.0 0181_N11 11923.00 17.560 No_date 33:09 16.21 n/a .000
03012* #
03013* # Sum of hydrographs from Node 11 routed to Node 10
03014* # Section 1
03015* #
03016* R0005:00040-----Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03017* ROUTE CHANNEL: > 1.0 0218_S.N11 11923.00 17.560 No_date 33:09 16.21 n/a .000
03018* [ROT( 1.001) out-< 1.0 0181_N11 11923.00 12.006 No_date 33:09 16.21 n/a .000
03019* [L/S/nm14028 / .157/.040]
03020* [Vmax=.461*Imax.1.087]
03021* #
03022* # Addition of Subwatershed 10 to Node 10
03023* # Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03024* ADD HYD 1.0 0218_N10 11923.00 12.006 No_date 38:17 16.21 n/a .000
03025* +
03026* [ROT( 1.001) out-< 1.0 0181_N10 11923.00 12.006 No_date 38:17 16.21 n/a .000
03027* [SM: 1.0 0181_N10 17589.00 28.927 No_date 38:09 17.47 n/a .000
03028* #
03029* # Addition of Kings Creek to S_N10
03030* frame: H_RestDef
03031* remark:flow at S_N10: N10_S_W10
03032* #
03033* # Addition of Nichols Creek to S_N10
03034* R0005:00043-----Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03035* ADD HYD 1.0 0218_N10 25965.00 28.927 No_date 39:15 17.47 n/a .000
03036* +
03037* [ROT( 1.001) out-< 1.0 0181_N10 25965.00 28.927 No_date 39:15 17.47 n/a .000
03038* [L/S/nm3992 / .075/.040]
03039* [Vmax=.644*Imax.1.502]
03040* #
03041* # Addition of Subwatershed 9 and Nichols Creek to Node 9
03042* R0005:00044-----Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03043* ADD HYD 1.0 0218_N9 25965.00 43.534 No_date 39:59 17.37 n/a .000
03044* +
03045* [ROT( 1.001) out-< 1.0 0181_N9 25965.00 43.534 No_date 39:59 17.37 n/a .000
03046* [L/S/nm3992 / .075/.040]
03047* [Vmax=.644*Imax.1.502]
03048* #
03049* # Addition of Subwatershed 9 and Nichols Creek to Node 9
03050* R0005:00045-----Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03051* ADD HYD 1.0 0218_N9 25965.00 43.534 No_date 39:59 17.37 n/a .000
03052* +
03053* [ROT( 1.001) out-< 1.0 0181_N9 25965.00 43.534 No_date 39:59 17.37 n/a .000
03054* [SM: 1.0 0181_N9 31585.00 53.368 No_date 39:59 17.37 n/a .000
03055* #
03056* # Sum of hydrographs from Node 9 routed to Node 8
03057* # Section 3
03058* #
03059* R0005:00046-----Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03060* ADD HYD 1.0 0218_N8 31561.00 53.366 No_date 39:59 17.37 n/a .000
03061* +
03062* [ROT( 1.001) out-< 1.0 0181_N8 31561.00 49.404 No_date 39:59 17.20 n/a .000
03063* [SM: 1.0 0181_N8 31561.00 49.404 No_date 39:59 17.20 n/a .000
03064* #
03065* # Addition of Subwatershed 8 and Hobbs's Drain to Node 8
03066* R0005:00047-----Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03067* ADD HYD 1.0 0218_N8 31561.00 49.404 No_date 39:59 17.20 n/a .000
03068* +
03069* [ROT( 1.001) out-< 1.0 0181_N8 31561.00 49.404 No_date 39:59 17.20 n/a .000
03070* [SM: 1.0 0181_N8 31561.00 49.404 No_date 39:59 17.20 n/a .000
03071* #
03072* # Sum of hydrographs from Node 8 routed to Node 7
03073* # Section 4
03074* #
03075* R0005:00048-----Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03076* ROUTE CHANNEL: > 1.0 0218_S.N8 35546.00 58.845 No_date 38:59 17.19 n/a .000
03077* [ROT( 1.001) out-< 1.0 0181_N8 35546.00 48.127 No_date 45:08 17.19 n/a .000
03078* [L/S/nm3750 / .053/.070]
03079* [Vmax=.308*Imax.1.853]
03080* #
03081* # Addition of Subwatershed 7 to Node 7
03082* R0005:00049-----Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03083* ADD HYD 1.0 0218_N7 35546.00 48.127 No_date 38:59 17.19 n/a .000
03084* +
03085* [ROT( 1.001) out-< 1.0 0181_N7 35546.00 48.127 No_date 38:59 17.19 n/a .000
03086* [SM: 1.0 0181_N7 38743.00 51.395 No_date 44:14 16.92 n/a .000
03087* +
03088* [ROT( 1.001) out-< 1.0 0181_N7 38743.00 51.395 No_date 44:14 16.92 n/a .000
03089* frame: H_RestDef
03090* remark:flow at S_N7: NT_S7 - SW7
03091* #
03092* # Inclusion of a reservoir to simulate the effects of the Richmond Pen.
03093* # Storage area and volumes were estimated from available topo maps
03094* # and flow rates from the USGS streamflow database
03095* # river cross-sections for summer conditions. It was assumed that up to
03096* # 0.75 m of water, the main channel of the river provided the storage. Above
03097* # this depth, the wetland starts to significantly store water.
03098* R0005:00051-----Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03099* ROUTE CHANNEL: > 1.0 0218_S.N7 38743.00 27.976 No_date 59:12 16.92 n/a .000
03100* [ROT( 1.001) out-< 1.0 0181_N7 38743.00 27.976 No_date 59:12 16.92 n/a .000
03101* [SM: 1.0 0181_N7 38743.00 27.976 No_date 59:12 16.92 n/a .000
03102* [MgSt:0.0001-17848-03 m3]
03103* R0005:00052-----Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03104* SAVE HYD 1.0 0181_N7 38743.00 27.976 No_date 59:12 16.92 n/a .000
03105* frame: H_RestDef
03106* remark:outflow of Richmond Pen
03107* #
03108* # Sum of hydrographs from Node 7 routed to Node 6
03109* # Section 5
03110* #
03111* R0005:00053-----Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03112* ROUTE CHANNEL: > 1.0 0218_S.N7 38743.00 27.976 No_date 60:01 16.92 n/a .000
03113* [ROT( 1.001) out-< 1.0 0181_N7 38743.00 27.976 No_date 60:01 16.92 n/a .000
03114* [SM: 1.0 0181_N7 40240.01 27.993 No_date 60:01 16.92 n/a .000
03115* #
03116* # Addition of Subwatershed 6 and Van Gaal Drain to Node 6
03117* R0005:00054-----Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03118* ADD HYD 1.0 0218_N6 40240.01 27.993 No_date 60:01 16.92 n/a .000
03119* +
03120* [ROT( 1.001) out-< 1.0 0181_N6 40240.01 27.993 No_date 60:01 16.92 n/a .000
03121* [SM: 1.0 0181_N6 40240.01 27.993 No_date 60:01 16.92 n/a .000
03122* #
03123* # Sum of hydrographs from Node 6 routed to Node 5
03124* #
03125* # Section 6
03126* #
03127* R0005:00055-----Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03128* ROUTE CHANNEL: > 1.0 0218_S.N5 40240.01 27.994 No_date 60:06 17.03 n/a .000
03129* [ROT( 1.001) out-< 1.0 0181_N5 40240.01 27.994 No_date 60:06 17.03 n/a .000
03130* [SM: 1.0 0181_N5 40240.01 27.992 No_date 60:06 17.03 n/a .000
03131* [L/S/nm1852 / .054/.034]
03132* [Vmax=.756*Imax.3.116]
03133* #
03134* # Addition of Subwatershed 5 and Flowing Creek to Node 5
03135* R0005:00056-----Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03136* ADD HYD 1.0 0218_N5 40240.01 27.992 No_date 60:07 17.03 n/a .000
03137* +
03138* [ROT( 1.001) out-< 1.0 0181_N5 40240.01 27.992 No_date 60:07 17.03 n/a .000
03139* [SM: 1.0 0181_N5 40240.01 27.992 No_date 60:07 17.03 n/a .000
03140* #
03141* # Sum of hydrographs from Node 5 routed to Node 4
03142* #
03143* # Section 7
03144* #
03145* R0005:00057-----Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03146* ADD HYD 1.0 0218_N5 40240.01 27.992 No_date 35:28 17.49 n/a .000
03147* +
03148* [ROT( 1.001) out-< 1.0 0181_N5 40240.01 27.992 No_date 35:28 17.49 n/a .000
03149* [L/S/nm .556 / .050/.040]
03150* [Vmax=.465*Imax.1.060]
03151* #
03152* # Addition of Subwatershed 5A and Subwatershed 5A to Node 5A
03153* R0005:00058-----Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03154* ADD HYD 1.0 0218_N5A 40493.01 43.490 No_date 35:47 17.49 n/a .000
03155* +
03156* [ROT( 1.001) out-< 1.0 0181_N5A 40493.01 43.490 No_date 35:47 17.49 n/a .000
03157* [SM: 1.0 0181_N5A 40493.01 43.490 No_date 35:47 17.49 n/a .000
03158* #
03159* # Sum of hydrographs from Node 5A routed to Node 4
03160* #
03161* # Section 8
03162* #
03163* R0005:00059-----Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03164* ROUTE CHANNEL: > 1.0 0218_S.N5A 40493.01 43.490 No_date 35:58 17.63 n/a .000
03165* [ROT( 1.001) out-< 1.0 0181_N5A 40493.01 43.490 No_date 35:58 17.63 n/a .000
03166* [SM: 1.0 0181_N5A 40493.01 43.490 No_date 35:58 17.63 n/a .000
03167* [L/S/nm .756 / .054/.043]
03168* [Vmax=.756*Imax.3.116]
03169* #
03170* # Addition of Subwatershed 4 and Leamy Creek to Node 4
03171* R0005:00060-----Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03172* ADD HYD 1.0 0218_N4 40493.01 43.490 No_date 37:06 17.63 n/a .000
03173* +
03174* [ROT( 1.001) out-< 1.0 0181_N4 40493.01 43.490 No_date 37:06 17.63 n/a .000
03175* [SM: 1.0 0181_N4 40493.01 43.490 No_date 37:06 17.63 n/a .000
03176* [L/S/nm .972 / .054/.040]
03177* [Vmax=.648*Imax.2.406]
03178* #
03179* # Addition of Subwatershed 11 and Name Creek to Node 11
03180* # (Approximated cross-section - see cross-section 288)
03181* # Use n=0.04 for summer conditions and n=0.328 for spring conditions
03182* # Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
03183* # Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03184* ROUTE CHANNEL: > 1.0 0218_S.N11 40493.01 43.490 No_date 37:06 17.63 n/a .000
03185* [ROT( 1.001) out-< 1.0 0181_N11 40493.01 43.490 No_date 37:06 17.63 n/a .000
03186* [L/S/nm14028 / .157/.040]
03187* [Vmax=.461*Imax.1.087]
03188* #
03189* # Addition of Subwatershed 2 with Monohan drain and Smith drain to Node 2
03190* # (Approximated cross-section - see cross-section 288)
03191* # Use n=0.04 for summer conditions and n=0.328 for spring conditions
03192* # Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
03193* # Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03194* ADD HYD 1.0 0218_N11 40493.01 43.490 No_date 37:06 17.63 n/a .000
03195* +
03196* [ROT( 1.001) out-< 1.0 0181_N11 40493.01 43.490 No_date 37:06 17.63 n/a .000
03197* [SM: 1.0 0181_N11 40493.01 43.490 No_date 37:06 17.63 n/a .000
03198* [L/S/nm .972 / .054/.040]
03199* [Vmax=.648*Imax.2.406]
03200* #
03201* # Addition of Subwatershed 2 with Monohan drain and Smith drain to Node 2
03202* # (Approximated cross-section - see cross-section 288)
03203* # Sum of hydrographs from Node 2 routed to Node 1
03204* #
03205* # Section 10
03206* #
03207* # Hydrograph from Node 2 routed to Node 11
03208* # Channel X-Section obtained from RVEA Hydraulic Model - Station 9025
03209* R0005:00039-----Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03210* ROUTE CHANNEL: > 1.0 0218_S.N11 40493.01 43.490 No_date 37:06 17.63 n/a .000
03211* [ROT( 1.001) out-< 1.0 0181_N11 40493.01 43.490 No_date 37:06 17.63 n/a .000
03212* [SM: 1.0 0181_N11 40493.01 43.490 No_date 37:06 17.63 n/a .000
03213* [L/S/nm .972 / .054/.040]
03214* [Vmax=.461*Imax.1.087]
03215* #
03216* # Catchment SW_1
03217* # Portion of the catchment SW_1 outside of Reach 1 subwatershed
03218* # Undeveloped agricultural land
03219* R0005:00040-----Dtnin-ID:NYHD--->ARAHa-QPEAKcms-TpeakDate_hh:mm---RvNm-R.C.--DWFcms
03220* CONTINUOUS_NASHRD 1.0 0181_N11 40493.01 43.490 No_date 37:06 17.63 n/a .000
03221* [CONTINUOUS_NASHRD 1.0 0181_N11 40493.01 3.012 No_date 29:03 42.00 .755 .000
03222* [CONTINUOUS_NASHRD 1.0 0181_N11 40493.01 3.012 No_date 29:03 19.00 .333 .000
03223* [CONTINUOUS_NASHRD 1.0 0181_N11 40493.01 3.012 No_date 31:18 19.00 .333 .000
03224* [INTERVENTIONTIME 12.00]
03225* # Catchment SW_1a
03226* # Catchment SW_1a
03227* # To O'Keefe drain (north of the Jock)
03228* # Developed with assumed 4% Imp.
03229* # Catchment SW_1a (area: 4.67*SLPP*2.0*LDG = 40.4MM* .250*SCP* .0)
03230* [IMPERVIOUS area: TAIPEC 1.57*SLPP*2.0*LDG = 75.5LGI *5.7LGI *54.7MM* .013*SC1* .0]
03231* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK1* .0]
03232* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK2* .0]
03233* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK3* .0]
03234* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK4* .0]
03235* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK5* .0]
03236* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK6* .0]
03237* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK7* .0]
03238* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK8* .0]
03239* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK9* .0]
03240* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK10* .0]
03241* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK11* .0]
03242* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK12* .0]
03243* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK13* .0]
03244* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK14* .0]
03245* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK15* .0]
03246* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK16* .0]
03247* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK17* .0]
03248* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK18* .0]
03249* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK19* .0]
03250* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK20* .0]
03251* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK21* .0]
03252* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK22* .0]
03253* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK23* .0]
03254* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK24* .0]
03255* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK25* .0]
03256* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK26* .0]
03257* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK27* .0]
03258* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK28* .0]
03259* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK29* .0]
03260* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK30* .0]
03261* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK31* .0]
03262* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK32* .0]
03263* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK33* .0]
03264* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK34* .0]
03265* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK35* .0]
03266* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK36* .0]
03267* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK37* .0]
03268* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK38* .0]
03269* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK39* .0]
03270* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK40* .0]
03271* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK41* .0]
03272* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK42* .0]
03273* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK43* .0]
03274* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK44* .0]
03275* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK45* .0]
03276* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK46* .0]
03277* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK47* .0]
03278* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK48* .0]
03279* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK49* .0]
03280* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK50* .0]
03281* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK51* .0]
03282* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *54.7MM* .010*SK52* .0]
03283* [IMPERVIOUS area: TAIPEC 4.00*SLPP*2.0*LDG = 33.8LGI *4.0LGI *5
```







04489+ #

04471+ # Dtnin-ID:HYNDY -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04483+ # ROUTE CHANNEL -> 1. 0. 021 4241 -> 54658..44 65.643 No\_date 36:38 18.70 n/a .000

04492+ # [ROT: 1.00] out-> 1. 0. 014241-out 54658..44 65.650 No\_date 36:38 18.70 n/a .000

04493+ # [L/S:n/- 394] -> 1. 0. 014241-out 54658..44 65.650 No\_date 36:38 18.70 n/a .000

04494+ # [SNIN: 31.15 SMAX:207.66 SK: 0100] -> 1. 0. 014241-out 54658..44 65.650 No\_date 36:38 18.70 n/a .000

04495+ # ADD HYD 1. 0. 021 4241-out 54658..44 65.650 No\_date 36:38 18.70 n/a .000

04497+ + 1. 0. 021 4241-out 54658..44 65.650 No\_date 36:38 18.70 n/a .000

04498+ + 1. 0. 021 4241-out 54658..44 65.650 No\_date 36:38 18.70 n/a .000

04499+ + 1. 0. 021 4241-out 54658..44 65.650 No\_date 36:38 18.70 n/a .000

04500+ SUM\_ 1. 0. 01 SNK\_XR 54681..13 69.678 No\_date 36:38 18.71 n/a .000

04501+ RO005:CO0271-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04502+ SAVE HYD 1. 0. 01 SNK\_XR 54681..13 69.678 No\_date 36:38 18.71 n/a .000

04503+ frame :SNK\_XR\_0005 remark:HVD\_COMMENT['Total Flows before Station 3633']

04504+ # Hydrograph from Corrigan Branch (south of the Jock)

04505+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633

04507+ # JFSA 2021-02-26 change the channel length (at station 3633) from 65m to 60m and change the slope from 0.0498 to 0.2

04508+ # [ROT: 1.00] out-> 1. 0. 01 SNK\_XR 54681..13 69.678 No\_date 36:38 18.71 n/a .000

04509+ # [L/S:n/- 247. /036] -> 1. 0. 01 SNK\_XR 54681..13 69.666 No\_date 36:51 18.71 n/a .000

04512+ # [Vmax: 1.446 Dmax: 1.371] \*\*\*\*\*

04515+ # Catchment Greenbank

04516+ # - To Greenbank Drain (mouth of the Jock)

04517+ # - From Greenbank Drain (mouth of the Jock) pond as per JFSA\_P598(04)-15, June 2016

04518+ # - JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GIS measurements

04519+ # \*\*\*\*\*

04520+ RO005:CO0272-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04521+ CONTINUOUS STANDHYD 1. 0. 01 Greenbank 36.60 3.925 No\_date 28:02 42.59 .745 .000

04522+ # [XPM: 64-TIMEP: 68] \*\*\*\*\*

04523+ # [ROT: 1.00] out-> 1. 0. 01 Greenbank 36.60 3.925 No\_date 28:02 42.59 .745 .000

04524+ # [Previous area: Iaper: 4.67:SLDP:1.00:LGD: 40.:MNP: .250:SCP: .0] \*\*\*\*\*

04525+ # [Impervious area: Iaper: 1.57:SLDP:1.00:LGD: 494.:MMI: .013:SCI: .0] \*\*\*\*\*

04526+ # [SNIN: 31.15 SMAX:207.66 SK: 0100] \*\*\*\*\*

04527+ # ROUTE RESERVOIR -> 1. 0. 01 Greenbank 36.60 3.925 No\_date 28:02 42.59 .745 .000

04528+ out <- 1. 0. 01 Greenbank 36.60 .811 No\_date 28:35 42.58 n/a .000

04530+ overlaid 1. 0. 01 Greenbank 36.60 .000 No\_date 0:00 0:00 n/a .000

04531+ [Motsclsed: 8651E-00 m3, TotCorVol: 0.000E+00 m3, N-Ovr: 0.000 m3, TotDurv: 0. hrs]

04533+ RO005:CO0276-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04534+ ADD HYD 1. 0. 021 4241-out 54681..13 69.666 No\_date 36:51 18.71 n/a .000

04535+ # [ROT: 1.00] out-> 1. 0. 01 Greenbank 36.60 .811 No\_date 28:35 42.58 n/a .000

04536+ SUM\_ 1. 0. 01 Greenbank 54717..73 69.773 No\_date 36:51 18.71 n/a .000

04537+ RO005:CO0277-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04538+ SAVE HYD 1. 0. 01 Greenbank 54717..73 69.773 No\_date 36:51 18.73 n/a .000

04539+ frame :Greenbank\_0008 remark:Total Flows at Greenbank Drain

04542+ \*\*\*\*\*

04543+ # Catchment Greenbank

04544+ # - To Todd brain (mouth of the Jock)

04545+ # - Subdivision with 43% imp. as per Barrhaven South MNS

04546+ # - [ROT: 1.00] out-> 1. 0. 01 Todd\_MN 2.10 .000 No\_date 28:00 38.39 .672 .000

04547+ # 2020-11-30 UPDATE TODD Tributary Drainage Area to = 146.05 ha based on P598(04)-11

04548+ # - 2020-11-30 update TODD Drainage Area to MAJOR, MINOR, FOND and ALL

04549+ # - [ROT: 1.00] out-> 1. 0. 01 Todd\_MN 2.10 .000 No\_date 28:00 38.39 .672 .000

04550+ # [JFSA 2021-01-19 add "DOD\_MN" as part of Clarke("W\_CLAR\_MN") and remove it from Todd

04551+ # \*\*\*\*\*

04552+ RO005:CO0278-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04553+ CONTINUOUS STANDHYD 1. 0. 01 TODD\_MN 2.10 .000 No\_date 28:00 38.41 .672 .000

04554+ # [XPM: 53-TIMEP: 57] \*\*\*\*\*

04555+ # [ROT: 2 CN: 77.0] \*\*\*\*\*

04556+ # [Previous area: Iaper: 4.67:SLDP:1.00:LGD: 40.:MNP: .250:SCP: .0] \*\*\*\*\*

04557+ # [Impervious area: Iaper: 1.57:SLDP:1.00:LGD: 118.:MMI: .013:SCI: .0] \*\*\*\*\*

04558+ # [IaECimp: 4.00: IaRepCper: 4.00] \*\*\*\*\*

04559+ # [SNIN: 31.15 SMAX:207.66 SK: 0100] \*\*\*\*\*

04560+ RO005:CO0279-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04561+ CONTINUOUS STANDHYD 1. 0. 01 TODD\_MN .12 .014 No\_date 28:00 38.39 .672 .000

04562+ # [ROT: 1.00] out-> 1. 0. 01 TODD\_MN .12 .014 No\_date 28:00 38.39 .672 .000

04563+ # [LGS: 2 CN: 77.0] \*\*\*\*\*

04564+ # [Previous area: Iaper: 4.67:SLDP:1.00:LGD: 40.:MNP: .250:SCP: .0] \*\*\*\*\*

04565+ # [Impervious area: Iaper: 1.57:SLDP:1.00:LGD: 118.:MMI: .013:SCI: .0] \*\*\*\*\*

04566+ # [IaECimp: 4.00: IaRepCper: 4.00] \*\*\*\*\*

04567+ # [SNIN: 31.15 SMAX:207.66 SK: 0100] \*\*\*\*\*

04568+ RO005:CO0280-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04569+ CONTINUOUS STANDHYD 1. 0. 01 TODD\_MN .30..23 2.959 No\_date 28:02 39.47 .691 .000

04570+ # [XPM: 52-TIMEP: 64] \*\*\*\*\*

04571+ # [ROT: 1.00] out-> 1. 0. 01 TODD\_MN .30..23 2.959 No\_date 28:00 38.41 .690 .000

04572+ # [Previous area: Iaper: 4.67:SLDP:1.00:LGD: 40.:MNP: .250:SCP: .0] \*\*\*\*\*

04573+ # [Impervious area: Iaper: 1.57:SLDP:1.00:LGD: 149.:MMI: .013:SCI: .0] \*\*\*\*\*

04574+ # [IaECimp: 4.00: IaRepCper: 4.00] \*\*\*\*\*

04575+ # [SNIN: 31.15 SMAX:207.66 SK: 0100] \*\*\*\*\*

04576+ RO005:CO0281-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04577+ CONTINUOUS STANDHYD 1. 0. 01 TODD\_MN .12 .014 No\_date 28:00 38.39 .669 .000

04578+ # [XPM: 52 CN: 77.0] \*\*\*\*\*

04579+ # [Previous area: Iaper: 4.67:SLDP:1.00:LGD: 40.:MNP: .250:SCP: .0] \*\*\*\*\*

04580+ # [Impervious area: Iaper: 1.57:SLDP:1.00:LGD: 143.:MMI: .013:SCI: .0] \*\*\*\*\*

04581+ # [IaECimp: 4.00: IaRepCper: 4.00] \*\*\*\*\*

04582+ # [SNIN: 31.15 SMAX:207.66 SK: 0100] \*\*\*\*\*

04583+ RO005:CO0282-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04584+ CONTINUOUS STANDHYD 1. 0. 01 TODD\_MN .30..05 .398 No\_date 28:00 41.58 .728 .000

04585+ # [ROT: 1.00] out-> 1. 0. 01 TODD\_MN .30..05 .398 No\_date 28:00 41.58 .728 .000

04586+ # [LGS: 2 CN: 77.0] \*\*\*\*\*

04587+ # [Previous area: Iaper: 4.67:SLDP:1.00:LGD: 40.:MNP: .250:SCP: .0] \*\*\*\*\*

04588+ # [Impervious area: Iaper: 1.57:SLDP:1.00:LGD: 143.:MMI: .013:SCI: .0] \*\*\*\*\*

04589+ # [IaECimp: 4.00: IaRepCper: 4.00] \*\*\*\*\*

04590+ # [SNIN: 31.15 SMAX:207.66 SK: 0100] \*\*\*\*\*

04591+ # 5 Year+ 12% Capture

04592+ RO005:CO0283-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04593+ CONTINUOUS STANDHYD 1. 0. 01 TODD\_P 3.00 .398 No\_date 28:00 41.58 .728 .000

04594+ # [XPM: 63-TIMEP: 65] \*\*\*\*\*

04595+ # [ROT: 1.00] out-> 1. 0. 01 TODD\_P 3.00 .398 No\_date 28:00 41.58 .728 .000

04596+ # [LGS: 2 CN: 77.0] \*\*\*\*\*

04597+ # [Previous area: Iaper: 4.67:SLDP:1.00:LGD: 40.:MNP: .250:SCP: .0] \*\*\*\*\*

04598+ # [Impervious area: Iaper: 1.57:SLDP:1.00:LGD: 143.:MMI: .013:SCI: .0] \*\*\*\*\*

04599+ # [IaECimp: 4.00: IaRepCper: 4.00] \*\*\*\*\*

04600+ # [SNIN: 31.15 SMAX:207.66 SK: 0100] \*\*\*\*\*

04601+ RO005:CO0284-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04602+ ROUTE RESERVOIR -> 1. 0. 021 T0DD\_MH 2.10 .238 No\_date 28:00 38.41 n/a .000

04603+ overlaid 1. 0. 021 T0DD\_MH 2.10 .000 No\_date 0:00 0:00 n/a .000

04604+ [Motsclsed: 8651E-00 m3, TotCorVol: 0.000E+00 m3, N-Ovr: 0.000 m3, TotDurv: 0. hrs]

04605+ RO005:CO0285-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04606+ ROUTE RESERVOIR -> 1. 0. 021 T0DD\_MH .12 .014 No\_date 28:00 38.39 n/a .000

04607+ overlaid 1. 0. 021 T0DD\_MH .12 .014 No\_date 28:00 38.39 n/a .000

04608+ overlaid 1. 0. 021 T0DD\_MH .00 .000 No\_date 0:00 0:00 n/a .000

04609+ [Motsclsed: 8651E-00 m3, TotCorVol: 0.000E+00 m3, N-Ovr: 0.000 m3, TotDurv: 0. hrs]

04610+ RO005:CO0286-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04611+ CONTINUOUS STANDHYD 1. 0. 01 T0DD\_MH .25..52 1.991 No\_date 28:00 34.46 .697 .000

04612+ # [XPM: 42-TIMEP: 52] \*\*\*\*\*

04613+ # [ROT: 1.00] out-> 1. 0. 01 T0DD\_MH .25..52 1.991 No\_date 28:00 34.46 .697 .000

04614+ # [LGS: 2 CN: 77.0] \*\*\*\*\*

04615+ # [Previous area: Iaper: 4.67:SLDP:1.00:LGD: 40.:MNP: .250:SCP: .0] \*\*\*\*\*

04616+ # [Impervious area: Iaper: 1.57:SLDP:1.00:LGD: 366.:MMI: .013:SCI: .0] \*\*\*\*\*

04617+ # [IaECimp: 4.00: IaRepCper: 4.00] \*\*\*\*\*

04618+ # [SNIN: 33.81 SMAX:225.43 SK: 0100] \*\*\*\*\*

04619+ RO005:CO0287-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04620+ CONTINUOUS STANDHYD 1. 0. 01 T0DD\_MH .25..52 1.991 No\_date 28:00 34.46 .697 .000

04621+ ADD HYD 1. 0. 021 4241-out 54658..44 65.643 No\_date 36:38 18.70 n/a .000

04622+ # [ROT: 1.00] out-> 1. 0. 01 T0DD\_MH .25..52 1.991 No\_date 28:00 34.46 .697 .000

04623+ # [LGS: 2 CN: 77.0] \*\*\*\*\*

04624+ # [Previous area: Iaper: 4.67:SLDP:1.00:LGD: 40.:MNP: .250:SCP: .0] \*\*\*\*\*

04625+ # [Impervious area: Iaper: 1.57:SLDP:1.00:LGD: 366.:MMI: .013:SCI: .0] \*\*\*\*\*

04626+ # [IaECimp: 4.00: IaRepCper: 4.00] \*\*\*\*\*

04627+ # [SNIN: 33.81 SMAX:225.43 SK: 0100] \*\*\*\*\*

04628+ RO005:CO0288-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04629+ CONTINUOUS STANDHYD 1. 0. 01 T0DD\_MH .25..52 1.991 No\_date 28:00 34.46 .697 .000

04630+ # [XPM: 41-TIMEP: 54] \*\*\*\*\*

04631+ # [ROT: 1.00] out-> 1. 0. 01 T0DD\_MH .25..52 1.991 No\_date 28:00 34.46 .697 .000

04632+ # [LGS: 2 CN: 77.0] \*\*\*\*\*

04633+ # [Previous area: Iaper: 4.67:SLDP:1.00:LGD: 40.:MNP: .250:SCP: .0] \*\*\*\*\*

04634+ # [Impervious area: Iaper: 1.57:SLDP:1.00:LGD: 366.:MMI: .013:SCI: .0] \*\*\*\*\*

04635+ # [IaECimp: 4.00: IaRepCper: 4.00] \*\*\*\*\*

04636+ # [SNIN: 33.81 SMAX:225.43 SK: 0100] \*\*\*\*\*

04637+ RO005:CO0289-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04638+ CONTINUOUS STANDHYD 1. 0. 01 T0DD\_MH .25..52 1.991 No\_date 28:00 34.46 .697 .000

04639+ # [XPM: 41-TIMEP: 54] \*\*\*\*\*

04640+ # [ROT: 1.00] out-> 1. 0. 01 T0DD\_MH .25..52 1.991 No\_date 28:00 34.46 .697 .000

04641+ # [LGS: 2 CN: 77.0] \*\*\*\*\*

04642+ # [Previous area: Iaper: 4.67:SLDP:1.00:LGD: 40.:MNP: .250:SCP: .0] \*\*\*\*\*

04643+ # [Impervious area: Iaper: 1.57:SLDP:1.00:LGD: 366.:MMI: .013:SCI: .0] \*\*\*\*\*

04644+ # [IaECimp: 4.00: IaRepCper: 4.00] \*\*\*\*\*

04645+ # [SNIN: 33.81 SMAX:225.43 SK: 0100] \*\*\*\*\*

04646+ RO005:CO0290-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04647+ CONTINUOUS STANDHYD 1. 0. 01 T0DD\_MH .25..52 1.991 No\_date 28:00 34.46 .697 .000

04648+ # [XPM: 41-TIMEP: 54] \*\*\*\*\*

04649+ # [ROT: 1.00] out-> 1. 0. 01 T0DD\_MH .25..52 1.991 No\_date 28:00 34.46 .697 .000

04650+ # [LGS: 2 CN: 77.0] \*\*\*\*\*

04651+ # [Previous area: Iaper: 4.67:SLDP:1.00:LGD: 40.:MNP: .250:SCP: .0] \*\*\*\*\*

04652+ # [Impervious area: Iaper: 1.57:SLDP:1.00:LGD: 366.:MMI: .013:SCI: .0] \*\*\*\*\*

04653+ # [IaECimp: 4.00: IaRepCper: 4.00] \*\*\*\*\*

04654+ # [SNIN: 33.81 SMAX:225.43 SK: 0100] \*\*\*\*\*

04655+ RO005:CO0291-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04656+ CONTINUOUS STANDHYD 1. 0. 01 T0DD\_MH .25..52 1.991 No\_date 28:00 34.46 .697 .000

04657+ # [XPM: 41-TIMEP: 54] \*\*\*\*\*

04658+ # [ROT: 1.00] out-> 1. 0. 01 T0DD\_MH .25..52 1.991 No\_date 28:00 34.46 .697 .000

04659+ # [LGS: 2 CN: 77.0] \*\*\*\*\*

04660+ # [Previous area: Iaper: 4.67:SLDP:1.00:LGD: 40.:MNP: .250:SCP: .0] \*\*\*\*\*

04661+ # [Impervious area: Iaper: 1.57:SLDP:1.00:LGD: 366.:MMI: .013:SCI: .0] \*\*\*\*\*

04662+ # [IaECimp: 4.00: IaRepCper: 4.00] \*\*\*\*\*

04663+ # [SNIN: 33.81 SMAX:225.43 SK: 0100] \*\*\*\*\*

04664+ RO005:CO0292-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04665+ CONTINUOUS STANDHYD 1. 0. 01 T0DD\_MH .25..52 1.991 No\_date 28:00 34.46 .697 .000

04666+ # [XPM: 41-TIMEP: 54] \*\*\*\*\*

04667+ # [ROT: 1.00] out-> 1. 0. 01 T0DD\_MH .25..52 1.991 No\_date 28:00 34.46 .697 .000

04668+ # [LGS: 2 CN: 77.0] \*\*\*\*\*

04669+ # [Previous area: Iaper: 4.67:SLDP:1.00:LGD: 40.:MNP: .250:SCP: .0] \*\*\*\*\*

04670+ # [Impervious area: Iaper: 1.57:SLDP:1.00:LGD: 366.:MMI: .013:SCI: .0] \*\*\*\*\*

04671+ # [IaECimp: 4.00: IaRepCper: 4.00] \*\*\*\*\*

04672+ # [SNIN: 33.81 SMAX:225.43 SK: 0100] \*\*\*\*\*

04673+ RO005:CO0293-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04674+ CONTINUOUS STANDHYD 1. 0. 01 T0DD\_MH .25..52 1.991 No\_date 28:00 34.46 .697 .000

04675+ # [XPM: 41-TIMEP: 54] \*\*\*\*\*

04676+ # [ROT: 1.00] out-> 1. 0. 01 T0DD\_MH .25..52 1.991 No\_date 28:00 34.46 .697 .000

04677+ # [LGS: 2 CN: 77.0] \*\*\*\*\*

04678+ # [Previous area: Iaper: 4.67:SLDP:1.00:LGD: 40.:MNP: .250:SCP: .0] \*\*\*\*\*

04679+ # [Impervious area: Iaper: 1.57:SLDP:1.00:LGD: 366.:MMI: .013:SCI: .0] \*\*\*\*\*

04680+ # [IaECimp: 4.00: IaRepCper: 4.00] \*\*\*\*\*

04681+ # [SNIN: 33.81 SMAX:225.43 SK: 0100] \*\*\*\*\*

04682+ RO005:CO0294-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04683+ CONTINUOUS STANDHYD 1. 0. 01 T0DD\_MH .25..52 1.991 No\_date 28:00 34.46 .697 .000

04684+ # [XPM: 41-TIMEP: 54] \*\*\*\*\*

04685+ # [ROT: 1.00] out-> 1. 0. 01 T0DD\_MH .25..52 1.991 No\_date 28:00 34.46 .697 .000

04686+ # [LGS: 2 CN: 77.0] \*\*\*\*\*

04687+ # [Previous area: Iaper: 4.67:SLDP:1.00:LGD: 40.:MNP: .250:SCP: .0] \*\*\*\*\*

04688+ # [Impervious area: Iaper: 1.57:SLDP:1.00:LGD: 366.:MMI: .013:SCI: .0] \*\*\*\*\*

04689+ # [IaECimp: 4.00: IaRepCper: 4.00] \*\*\*\*\*

04690+ # [SNIN: 33.81 SMAX:225.43 SK: 0100] \*\*\*\*\*

04691+ RO005:CO0295-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04692+ CONTINUOUS STANDHYD 1. 0. 01 T0DD .25..52 1.991 No\_date 28:00 34.46 .697 .000

04693+ # [XPM: 41-TIMEP: 54] \*\*\*\*\*

04694+ # [ROT: 1.00] out-> 1. 0. 01 T0DD .25..52 1.991 No\_date 28:00 34.46 .697 .000

04695+ # [LGS: 2 CN: 77.0] \*\*\*\*\*

04696+ # [Previous area: Iaper: 4.67:SLDP:1.00:LGD: 40.:MNP: .250:SCP: .0] \*\*\*\*\*

04697+ # [Impervious area: Iaper: 1.57:SLDP:1.00:LGD: 366.:MMI: .013:SCI: .0] \*\*\*\*\*

04698+ # [IaECimp: 4.00: IaRepCper: 4.00] \*\*\*\*\*

04699+ # [SNIN: 33.81 SMAX:225.43 SK: 0100] \*\*\*\*\*

04700+ RO005:CO0296-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04701+ CONTINUOUS STANDHYD 1. 0. 01 T0DD .25..52 1.991 No\_date 28:00 34.46 .697 .000

04702+ # [XPM: 41-TIMEP: 54] \*\*\*\*\*

04703+ # [ROT: 1.00] out-> 1. 0. 01 T0DD .25..52 1.991 No\_date 28:00 34.46 .697 .000

04704+ # [LGS: 2 CN: 77.0] \*\*\*\*\*

04705+ # [Previous area: Iaper: 4.67:SLDP:1.00:LGD: 40.:MNP: .250:SCP: .0] \*\*\*\*\*

04706+ # [Impervious area: Iaper: 1.57:SLDP:1.00:LGD: 366.:MMI: .013:SCI: .0] \*\*\*\*\*

04707+ # [IaECimp: 4.00: IaRepCper: 4.00] \*\*\*\*\*

04708+ # [SNIN: 33.81 SMAX:225.43 SK: 0100] \*\*\*\*\*

04709+ RO005:CO0297-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04710+ CONTINUOUS STANDHYD 1. 0. 01 T0DD .25..52 1.991 No\_date 28:00 34.46 .697 .000

04711+ # [XPM: 41-TIMEP: 54] \*\*\*\*\*

04712+ # [ROT: 1.00] out-> 1. 0. 01 T0DD .25..52 1.991 No\_date 28:00 34.46 .697 .000

04713+ # [LGS: 2 CN: 77.0] \*\*\*\*\*

04714+ # [Previous area: Iaper: 4.67:SLDP:1.00:LGD: 40.:MNP: .250:SCP: .0] \*\*\*\*\*

04715+ # [Impervious area: Iaper: 1.57:SLDP:1.00:LGD: 366.:MMI: .013:SCI: .0] \*\*\*\*\*

04716+ # [IaECimp: 4.00: IaRepCper: 4.00] \*\*\*\*\*

04717+ # [SNIN: 33.81 SMAX:225.43 SK: 0100] \*\*\*\*\*

04718+ RO005:CO0298-72 -> Dtnin-ID:HYNDY -> ARBaha-QPEAKcms-TpeakDate\_bh:m:-> RVmn-R.C. ---DWFcms

04719+ CONTINUOUS STANDHYD 1. 0. 01 T0DD .25..52 1.991 No\_date 28:00 34.46 .697 .000

04720+ # [XPM: 41-TIMEP: 54] \*\*\*\*\*

04721+ # [ROT: 1.00] out-> 1. 0. 01 T0DD .25..52 1.991 No\_date 28:00 34.46 .697 .000

04722+ # [LGS: 2 CN: 77.0] \*\*\*\*\*

04723+ # [Previous area: Iaper: 4.67:SLDP:1.0

[...]

05237\* SAVE HYD :SN\_M1\_0005 55194.85 70.602 No\_date 37:03 18.87 n/a .000

05240\* # Hydrograph from Total Flows at Jock Vale Road

05242\* # Channel X-Section obtained from EYCA Hydrologic Model - Station 689

05243\* R0055-C00192-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05244\* ROUTE CHANNEL --> 1.0 02 SN\_M1 55194.85 70.602 No\_date 37:03 18.87 n/a .000

05245\* [ROT= 1.00] out-> 1.0 01\_N\_DE 55194.85 70.452 No\_date 37:20 18.87 n/a .000

05246\* [L/S/nr= 1.00 / 22.00] [SMIN= 55.00 / DMAX= 1.891]

05247\* [InterEventTime= 12.00]

05248\* # The Tp was modified according to a peak Reduction factor (MTO-Chart B2-4)

05249\* # of 1.80

05250\* # Catchment JOCKVA

05251\* # To Jock River (north of the Jock)

05252\* # Rural-estate subdivision (Heart's Desire Community)

05253\* R0055-C00193-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05254\* CONTINUOUS STANDHYD 1.0 01:DESH 23.78 1.359 No\_date 28:03 27.22 4.77 .000

05255\* [LNG= -28.10] [LAT= 45.22]

05256\* [LGS= 2 CN= 77.0]

05257\* [Previous areas: Japer: 4.67 SLPW=1.00:LGW= 40 :NMW= 250:SCP= .0]

05258\* [Previous areas: Japer: 4.67 SLPW=1.00:LGW= 40 :NMW= 250:SCP= .0]

05259\* [SMM= 31.15 :SMAX= 207.66: SK= .010]

05260\* [iabECLmp= 4.00: iarePcrp= 4.00]

05261\* [InterEventTime= 12.00]

05262\* # Catchment JOCKVA

05263\* # To Jock River SWM Facility

05264\* # Reservoir Total Flow from golf course

05265\* # JFSR 2021-01-11 issue JOCKVA after updating CORRIG as per IBI GROUP, July 2008.

05266\* # JFSR area becomes 225.13 ha instead of 225.10, JOCKVA separated into two areas JOCKVA and EX-LAND 32.5 ha as per IBI GROUP, July 2008.

05267\* R0055-C00194-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05268\* CONTINUOUS STANDHYD 1.0 01:JOCKVA 225.13 14.675 No\_date 28:09 35.73 .626 .000

05269\* [LNG= -72.01] [LAT= 45.22]

05270\* [LGS= 2 CN= 74.0]

05271\* [Previous areas: Japer: 4.67 SLPW=1.00:LGW= 40 :NMW= 250:SCP= .0]

05272\* [Previous areas: Japer: 4.67 SLPW=1.00:LGW= 40 :NMW= 250:SCP= .0]

05273\* [SMM= 31.15 :SMAX= 207.66: SK= .010]

05274\* [iabECLmp= 4.00: iarePcrp= 4.00]

05275\* [InterEventTime= 12.00]

05276\* [SMM= 36.67 :SMAX= 244.49: SK= .010]

05277\* R0055-C00195-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05278\* ADD HYD 1.0 02 EX-LAND\_MN 32.50 2.275 No\_date 27:57 35.73 n/a .000

05279\* + 1.0 02 JOCKVA 225.13 14.675 No\_date 28:09 35.73 n/a .000

05280\* + 1.0 02 SN\_MN 32.50 2.275 No\_date 28:09 35.73 n/a .000

05281\* + 1.0 02 BS-MN .00 .000 No\_date 0:00 .00 n/a .000

05282\* SUM 1.0 01 JOCKVA\_TO 257.63 16.950 No\_date 28:09 35.73 n/a .000

05283\* R0055-C00196-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05284\* SAVE HYD 1.0 01 JOCKVA 257.63 16.950 No\_date 28:09 35.73 n/a .000

05285\* fname :JOCKVA\_TO.DAT

05286\* remark:Total Flows at KB first pond

05287\* # D-Reservoir

05288\* # Rating curve obtained from Jockvalle Servicing Study (CC1, 1998)

05289\* R0055-C00197-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05290\* ROUTE RESERVOIR --> 1.0 02 JOCKVA 257.63 16.950 No\_date 28:09 35.73 n/a .000

05291\* out <- 1.0 01 JOCK\_P 257.63 4.781 No\_date 28:48 35.73 n/a .000

05292\* [LGS= 2 CN= 74.0]

05293\* [iabECLmp= 4.00: iarePcrp= 4.00]

05294\* [InterEventTime= 12.00]

05295\* R0055-C00198-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05296\* ADD HYD 1.0 02 SN\_MN 32.50 2.275 No\_date 27:57 35.73 n/a .000

05297\* + 1.0 02 DESH 25.18 1.359 No\_date 28:03 27.22 n/a .000

05298\* + 1.0 02 JOC-DV 0:00 .000 No\_date 0:00 .00 n/a .000

05299\* + 1.0 02 JOC-OP 0:00 .000 No\_date 0:00 .00 n/a .000

05300\* + 1.0 02 SN-OP 257.63 16.950 No\_date 28:09 35.73 n/a .000

05301\* SUM 1.0 01 SN\_MN 55476.26 71.017 No\_date 37:17 18.95 n/a .000

05302\* R0055-C00199-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05303\* SAVE HYD 1.0 01 SN\_MN 55476.26 71.017 No\_date 37:17 18.95 n/a .000

05304\* fname :SN\_M1\_0005

05305\* remark:Total Flows at Heart's Desire

05306\* # D-Reservoir

05307\* # Hydrograph from Heart's Desire routed to Rideau River

05308\* # Channel X-Section obtained from EYCA Hydrologic Model - Station 0

05309\* R0055-C00200-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05310\* ROUTE CHANNEL --> 1.0 02 SN\_MN 55476.26 71.017 No\_date 37:17 18.95 n/a .000

05311\* ADD HYD 1.0 02 SN\_MN 55476.26 71.029 No\_date 37:08 18.95 n/a .000

05312\* [L/S/nr= 563.1 / .967 / .045]

05313\* [Vmax= 1.676 :DMax= .955]

05314\* # Catchment S-2

05315\* # To Jock River (north and south)

05316\* # Reservoir floodplain and river

05317\* # D-Reservoir

05318\* R0055-C00201-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05319\* CONTINUOUS NASHYD 1.0 01:DESH 102.94 2.262 No\_date 28:20 18.95 .333 .000

05320\* [CN= 72.01 :SMIN= 3.00 :TP= 40]

05321\* [iabECA 4.00 :SMIN= 75 :TP= 224.99: SK= .010]

05322\* [InterEventTime= 12.00]

05323\* R0055-C00202-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05324\* ADD HYD 1.0 02 SN\_MN 55476.26 71.017 No\_date 27:58 18.95 n/a .000

05325\* + 1.0 02 DESH 102.94 2.262 No\_date 28:20 18.95 n/a .000

05326\* + 1.0 02 SN-OP 55476.26 71.017 No\_date 37:08 18.95 n/a .000

05327\* SUM 1.0 01 SN\_MN 55476.26 71.168 No\_date 27:08 18.95 n/a .000

05328\* R0055-C00203-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05329\* SAVE HYD 1.0 01 SN\_MN 55476.26 71.168 No\_date 27:08 18.95 n/a .000

05330\* fname :SN\_M1\_0005

05331\* remark:Total Flows at Rideau River

05332\* #####END RUN : 9

05335\* \*\* END RUN :

05336\* \*\*\*\*\*

05337\* R0055-C00204-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05338\* ADD HYD 1.0 02 SN\_MN 55476.26 71.168 No\_date 27:08 18.95 n/a .000

05339\* [InterEventTime= 12.00]

05340\* R0055-C00205-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05341\* ADD HYD 1.0 02 SN\_MN 55476.26 71.168 No\_date 27:08 18.95 n/a .000

05342\* R0055-C00206-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05343\* ADD HYD 1.0 02 SN\_MN 55476.26 71.168 No\_date 27:08 18.95 n/a .000

05344\* R0055-C00207-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05345\* ADD HYD 1.0 02 SN\_MN 55476.26 71.168 No\_date 27:08 18.95 n/a .000

05346\* R0055-C00208-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05347\* ADD HYD 1.0 02 SN\_MN 55476.26 71.168 No\_date 27:08 18.95 n/a .000

05348\* R0055-C00209-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05349\* ADD HYD 1.0 02 SN\_MN 55476.26 71.168 No\_date 27:08 18.95 n/a .000

05350\* R0055-C00210-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05351\* ADD HYD 1.0 02 SN\_MN 55476.26 71.168 No\_date 27:08 18.95 n/a .000

05352\* R0055-C00211-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05353\* ADD HYD 1.0 02 SN\_MN 55476.26 71.168 No\_date 27:08 18.95 n/a .000

05354\* R0055-C00212-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05355\* ADD HYD 1.0 02 SN\_MN 55476.26 71.168 No\_date 27:08 18.95 n/a .000

05356\* R0055-C00213-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05357\* ADD HYD 1.0 02 SN\_MN 55476.26 71.168 No\_date 27:08 18.95 n/a .000

05358\* R0055-C00214-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05359\* ADD HYD 1.0 02 SN\_MN 55476.26 71.168 No\_date 27:08 18.95 n/a .000

05360\* R0055-C00215-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05361\* ADD HYD 1.0 02 SN\_MN 55476.26 71.168 No\_date 27:08 18.95 n/a .000

05362\* R0055-C00216-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05363\* ADD HYD 1.0 02 SN\_MN 55476.26 71.168 No\_date 27:08 18.95 n/a .000

05364\* R0055-C00217-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05365\* ADD HYD 1.0 02 SN\_MN 55476.26 71.168 No\_date 27:08 18.95 n/a .000

05366\* R0055-C00218-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05367\* ADD HYD 1.0 02 SN\_MN 55476.26 71.168 No\_date 27:08 18.95 n/a .000

05368\* R0055-C00219-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05369\* ADD HYD 1.0 02 SN\_MN 55476.26 71.168 No\_date 27:08 18.95 n/a .000

05370\* R0055-C00220-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05371\* ADD HYD 1.0 02 SN\_MN 55476.26 71.168 No\_date 27:08 18.95 n/a .000

05372\* R0055-C00221-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05373\* ADD HYD 1.0 02 SN\_MN 55476.26 71.168 No\_date 27:08 18.95 n/a .000

05374\* MODIFY STORM

05375\* [RFAC= 1.00 :TSHFT= 960.00 min]

05376\* [RFAC= 1.00 :TSHFT= 240.00 min]

05377\* [RFAC= 1.00 :TSHFT= 40.00 min]

05378\* DEFAULT VALUES

05379\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5462 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05380\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5002 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05381\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5002 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05382\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5002 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05383\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5002 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05384\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5002 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05385\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5002 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05386\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5002 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05387\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5002 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05388\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5002 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05389\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5002 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05390\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5002 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05391\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5002 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05392\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5002 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05393\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5002 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05394\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5002 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05395\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5002 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05396\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5002 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05397\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5002 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05398\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5002 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05399\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5002 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05400\* Filename = JOCKVA\_2001-01-01-2020-12-01 Change the slope for ROUTE CHANNEL Station 5002 (RNDDout=1.5% TO 1.0%) (IMPROV=0.5%) (improvised slope) and LGR up to 70m

05401\* # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

05402\* # of 1.80

05403\* # Catchment JOCKVA

05404\* R0010-C00006-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05405\* CONTINUOUS NASHYD 1.0 01:JCK\_RW 3680.00 11.879 No\_date 36:59 20.23 .313 .000

05406\* [ROT= 1.00] [SMIN= 64.00 :LNG= 1.00 :LAT= 45.22]

05407\* [iabECA 4.00 :SMIN= 57.05 :SMAX= 380.32: SK= .010]

05408\* [InterEventTime= 12.00]

05409\* # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

05410\* # of 1.80

05411\* R0010-C00007-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05412\* CONTINUOUS NASHYD 1.0 01:W\_M13 971.00 4.365 No\_date 32:35 18.83 .291 .000

05413\* [ROT= 1.00] [SMIN= 64.50 :LNG= 430.01 :LAT= 44.87]

05414\* [InterEventTime= 12.00]

05415\* # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

05416\* # of 1.80

05417\* R0010-C00008-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05418\* CONTINUOUS NASHYD 1.0 01:CHW\_MW 3074.00 5.829 No\_date 39:59 16.22 .251 .000

05419\* [ROT= 1.00] [SMIN= 55.01 :LNG= 111.33]

05420\* R0010-C00009-----Dtnin-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm:--RVMn-R.C.--DWFcms

05421\* CONTINUOUS NASHYD 1.0 01:CHW\_GW 3074.00 5.829 No\_date 39:59 16.22 .251 .000

05422\* [ROT= 1.00] [SMIN= 55.01 :LNG= 111.33]

05423\* [iabECA 4.00 :SMIN= 83.24: SMAX= 554.96: SK= .010]

05424\* [InterEventTime= 12.00]

05425\* # Catchment Jock Vale

05426\* # Routing Outflow from Res GM

05427\* # Outflow from Res GM to Node 13A

05428\* # Approximated cross-section = cross-section 258

05429\* # Routing Outflow from Res GM to Node 13A

05430\* # Approximated cross-section = cross-section 258

05431\* # Routing Outflow from Res GM to Node 13A

05432\* # Approximated cross-section = cross-section 258

05433\* # Routing Outflow from Res GM to Node 13A

05434\* # Starting with the addition of Jock River Headwater and Subwatershed 13

05435\* # Routing Outflow from Res GM to Node 13A

05436\* # Approximated cross-section = cross-section 258

05437\* # Routing Outflow from Res GM to Node 13A

05438\* # Approximated cross-section = cross-section 258

05439\* # Routing Outflow from Res GM to Node 13A

05440\* # Approximated cross-section = cross-section 258

05441\* # Routing Outflow from Res GM to Node 13A

05442\* # Approximated cross-section = cross-section 258

05443\* # Routing Outflow from Res GM to Node 13A

05444\* # Starting with the addition of Jock River Headwater and Subwatershed 13

05445\* # Routing Outflow from Res GM to Node 13A

05446\* # Approximated cross-section = cross-section 258

05447\* # Routing Outflow from Res GM to Node 13A

05448\* # Approximated cross-section = cross-section 258

05449\* # Routing Outflow from Res GM to Node 13A

05450\* # Starting with the addition of Goodwood Marsh

05451\* # Routing Outflow from Res GM to Node 13A

05452\* # Approximated cross-section = cross-section 258

05453\* # Routing Outflow from Res GM to Node 13A

05454\* # Starting with the addition of Goodwood Marsh

05455\* # Routing Outflow from Res GM to Node 13A

05456\* # Approximated cross-section = cross-section 258

05457\* # Routing Outflow from Res GM to Node 13A

05458\* # Starting with the addition of Goodwood Marsh

05459\* # Routing Outflow from Res GM to Node 13A

05460\* # Approximated cross-section = cross-section 258

05461\* # Routing Outflow from Res GM to Node 13A

05462\* # Starting with the addition of Goodwood Marsh

05463\* # Routing Outflow from Res GM to Node 13A

05464\* # Approximated cross-section = cross-section 258

05465\* # Routing Outflow from Res GM to Node 13A

05466\* # Starting with the addition of Goodwood Marsh

05467\* # Routing Outflow from Res GM to Node 13A

05468\* # Approximated cross-section = cross-section 258

05469\* # Routing Outflow from Res GM to Node 13A

05470\* # Starting with the addition of Goodwood Marsh

05471\* # Routing Outflow from Res GM to Node 13A

05472\* # Approximated cross-section = cross-section 258

05473\* # Routing Outflow from Res GM to Node 13A

05474\* # Starting with the addition of Goodwood Marsh

05475\* # Routing Outflow from Res GM to Node 13A

05476\* # Approximated cross-section = cross-section 258

05477\* # Routing Outflow from Res GM to Node 13A

05478\* # Starting with the addition of Goodwood Marsh

05479\* # Routing Outflow from Res GM to Node 13A

05480\* # Approximated cross-section = cross-section 258

05481\* # Routing Outflow from Res GM to Node 13A

05482\* # Starting with the addition of Goodwood Marsh

05483\* # Routing Outflow from Res GM to Node 13A

05484\* # Approximated cross-section = cross-section 258

05485\* # Routing Outflow from Res GM to Node 13A

05486\* # Starting with the addition of Goodwood Marsh

05487\* # Routing Outflow from Res GM to Node 13A

05488\* # Approximated cross-section = cross-section 258

05489\* # Routing Outflow from Res GM to Node 13A

05490\* # Starting with the addition of Goodwood Marsh

05491\* # Routing Outflow from Res GM to Node 13A

05492\* # Approximated cross-section = cross-section 258

05493\* # Starting with the addition of Goodwood Marsh

05494\* # Routing Outflow from Res GM to Node 13A

05495\* # Approximated cross-section = cross-section 258

05496\* # Starting with the addition of Goodwood Marsh

05497\* # Routing Outflow from Res GM to Node 13A

05498\* # Approximated cross-section = cross-section 258

05499\* # Starting with the addition of Goodwood Marsh

05500\* # Routing Outflow from Res GM to Node 13A

05501\* # Approximated cross-section = cross-section 258

05502\* # Starting with the addition of Goodwood Marsh

05503\* # Routing Outflow from Res GM to Node 13A

05504\* # Approximated cross-section = cross-section 258

05505\* # Starting with the addition of Goodwood Marsh

05506\* # Routing Outflow from Res GM to Node 13A

05507\* # Approximated cross-section = cross-section 258

05508\* # Starting with the addition of Goodwood Marsh

05509\* # Routing Outflow from Res GM to Node 13A

05510\* # Approximated cross-section = cross-section 258

05511\* # Starting with the addition of Goodwood Marsh

05512\* # Routing Outflow from Res GM to Node 13A

05513\* # Approximated cross-section = cross-section 258

05514\* # Starting with the addition of Goodwood Marsh

05515\* # Routing Outflow from Res GM to Node 13A

05516\* # Approximated cross-section = cross-section 258

05517\* # Starting with the addition of Goodwood Marsh

05518\* # Routing Outflow from Res GM to Node 13A

05519\* # Approximated cross-section = cross-section 258

05520\* # Starting with the addition of Goodwood Marsh

05521\* # Routing Outflow from Res GM to Node 13A

05522\* # Approximated cross-section = cross-section 258

05523\* # Starting with the addition of Goodwood Marsh

05524\* # Routing Outflow from Res GM to Node 13A

05525\* # Approximated cross-section = cross-section

```

05611> [Vmax=.546:Dmax= 1.499]
05612> # Addition of Subwatershed Jock River at Ashton to Node 12
05613> ADD HYD
05614> DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05615> 1.0 02:NI2    7728.00  1.519 No_date 61:53 18.46 n/a .000
05616> + 1.0 02:JR_ASH 1781.00 10.839 No_date 32:42 24.81 n/a .000
05617>     SUM+ 1.0 01:S,N12 1834.00 10.834 No_date 32:42 18.46 n/a .000
05618> AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05619> SAVE HYD
05620> 1.0 01:S,N12 9506.00 12.834 No_date 32:45 19.65 n/a .000
05621> frame_R_SN12
05622> remark:flow at S,N12 near Ashton
05623> # Sum of hydrographs from Node 12 routed to Node 11
05624> # (Approximated cross-section - see cross-section 258)
05625> Use no-0.04 for summer conditions and no-0.025 for spring conditions
05626> # Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
05627> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05628> ROUTE CHANNEL -> 1.0 02:S,N12 9506.00 12.834 No_date 32:45 19.65 n/a .000
05629> + 1.0 02:SW_11 500.00 5.639 No_date 29:22 21.19 n/a .000
05630>     * 1.0 02:NNC_N 1917.00 7.897 No_date 34:28 21.19 n/a .000
05631>     SUM+ 1.0 01:S,N11 11923.00 21.813 No_date 33:05 19.96 n/a .000
05632> # [RDt= 1.00] out- 1.0 01:DM11 9506.00 12.710 No_date 33:02 19.65 n/a .000
05633> [L/S/n=.0583/.0583] [Vmax=.680:Dmax= 2.598]
05634> # Addition of Subwatershed 11 and No Name Creek to Node 11
05635> ADD HYD
05636> DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05637> 1.0 02:NI3    9506.00 12.710 No_date 33:02 19.65 n/a .000
05638> + 1.0 02:SW_11 500.00 5.639 No_date 29:22 21.19 n/a .000
05639>     * 1.0 02:NNC_N 1917.00 7.897 No_date 34:28 21.19 n/a .000
05640>     SUM+ 1.0 01:S,N11 11923.00 21.813 No_date 33:05 19.96 n/a .000
05641> # [RDt= 1.00] out- 1.0 01:NI10 11923.00 21.813 No_date 33:05 19.96 n/a .000
05642> [L/S/n=.14028/.1597/.040] [Vmax=.452:Dmax= 1.212]
05643> # Sum of hydrographs from Node 11 routed to Node 10
05644> # Addition of Subwatershed 10 and No Name Creek to Node 10
05645> ADD HYD
05646> DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05647> 1.0 02:NI4    9506.00 12.710 No_date 33:05 19.96 n/a .000
05648> + 1.0 02:SW_11 500.00 5.639 No_date 29:22 21.19 n/a .000
05649>     * 1.0 02:NNC_N 1917.00 7.897 No_date 34:28 21.19 n/a .000
05650>     SUM+ 1.0 01:S,N11 11923.00 21.813 No_date 33:05 19.96 n/a .000
05651> # [RDt= 1.00] out- 1.0 01:NI10 11923.00 21.813 No_date 33:05 19.96 n/a .000
05652> # Addition of Subwatershed 11 and No Name Creek to Node 11
05653> ADD HYD
05654> DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05655> 1.0 02:NI4    11923.00 14.761 No_date 39:58 19.56 n/a .000
05656> + 1.0 02:SW_11 500.00 12.710 No_date 33:02 19.65 n/a .000
05657>     SUM+ 1.0 01:S,N10 11923.00 21.813 No_date 33:05 19.96 n/a .000
05658> # [RDt= 1.00] out- 1.0 01:NI10 11923.00 21.813 No_date 33:05 19.96 n/a .000
05659> [L/S/n=.14028/.1597/.040] [Vmax=.452:Dmax= 1.212]
05660> # Sum of hydrographs from Node 11 routed to Node 10
05661> frame_R_SN12
05662> remark:flow at S,N10 NI10 = SW_10
05663> # Addition of Kings Creek to R,S10
05664> # Addition of Kings Creek to R,S10
05665> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05666> ADD HYD
05667> 1.0 02:S,N10 15789.00 35.808 No_date 38:35 21.52 n/a .000
05668> + 1.0 02:EK_S,N10 8376.00 20.398 No_date 39:59 21.19 n/a .000
05669>     SUM+ 1.0 01:S,N9 25965.00 55.807 No_date 39:59 21.41 n/a .000
05670> # [RDt= 1.00] out- 1.0 01:NI9 25965.00 55.807 No_date 39:59 21.41 n/a .000
05671> [Vmax=.682:Dmax= 1.696]
05672> # Section 2
05673> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05674> [RDt= 1.00] out- 1.0 02:S,N10 25965.00 55.807 No_date 39:59 21.41 n/a .000
05675> [RDt= 1.00] out- 1.0 01:NI9 25965.00 54.076 No_date 39:59 21.41 n/a .000
05676> [L/S/n=.3982/.075/.040] [Vmax=.682:Dmax= 1.696]
05677> # Sum of hydrographs from Node 10 routed to Node 9
05678> # Section 3
05679> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05680> ADD HYD
05681> DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05682> + 1.0 02:S,N10 25965.00 54.076 No_date 39:59 21.41 n/a .000
05683>     SUM+ 1.0 01:S,N9 31561.00 66.284 No_date 39:59 21.20 n/a .000
05684> # [RDt= 1.00] out- 1.0 01:NI9 31561.00 66.284 No_date 39:59 21.20 n/a .000
05685> # Sum of hydrographs from Node 9 routed to Node 8
05686> # Section 3
05687> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05688> ADD HYD
05689> DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05690> + 1.0 02:S,N10 31561.00 66.284 No_date 39:59 21.20 n/a .000
05691>     SUM+ 1.0 01:S,N9 31561.00 61.405 No_date 39:59 21.10 n/a .000
05692> [L/S/n=.2269/.088/.046] [Vmax=.363:Dmax= 1.619]
05693> # Addition of Subwatershed 8 and Hobbs's Drain to Node 8
05694> # Addition of Subwatershed 8 and Hobbs's Drain to Node 8
05695> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05696> ADD HYD
05697> DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05698> + 1.0 02:S,N10 31561.00 61.405 No_date 39:59 21.10 n/a .000
05699>     SUM+ 1.0 01:S,N9 31561.00 61.405 No_date 39:59 21.10 n/a .000
05700> # [RDt= 1.00] out- 1.0 01:NI9 31561.00 61.405 No_date 39:59 21.10 n/a .000
05701> [Vmax=.218:Dmax= 1.987]
05702> # Addition of Subwatershed 7 to Node 7
05703> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05704> ADD HYD
05705> DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05706> + 1.0 02:N17 3197.00 8.899 No_date 45:01 21.19 n/a .000
05707>     SUM+ 1.0 01:S,N7 3197.00 8.899 No_date 45:01 21.19 n/a .000
05708> # [RDt= 1.00] out- 1.0 01:NI7 3197.00 8.899 No_date 45:01 21.19 n/a .000
05709> # Sum of hydrographs from Node 8 routed to Node 7
05710> # Section 4
05711> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05712> ADD HYD
05713> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05714> [RDt= 1.00] out- 1.0 02:S,N8 35456.00 73.344 No_date 39:57 21.19 n/a .000
05715> [RDt= 1.00] out- 1.0 01:NI8 35456.00 73.344 No_date 39:57 21.19 n/a .000
05716> # Sum of hydrographs from Node 7 routed to Node 6
05717> # Section 4
05718> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05719> ADD HYD
05720> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05721> [RDt= 1.00] out- 1.0 02:S,N8 35456.00 73.344 No_date 39:57 21.19 n/a .000
05722> [RDt= 1.00] out- 1.0 01:NI8 35456.00 73.344 No_date 39:57 21.19 n/a .000
05723> # Insertion of a reservoir to simulate the effects of the Backbone Pen.
05724> # Streamflow was approximated from available topo maps.
05725> # Reaches rate from pen was assumed to be controlled by the downstream
05726> # river cross-section for summer conditions. It was assumed that for up to
05727> # 100% of the flow, the streamflow would be controlled by the storage. Above
05728> # this depth, the wetland starts to significantly store water.
05729> # [RDt= 1.00] out- 1.0 01:NI8 38743.00 65.819 No_date 44:06 20.85 n/a .000
05730> [Vmax=.477:Dmax= .960]
05731> # Sum of hydrographs from Node 7 routed to Node 6
05732> # Section 5
05733> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05734> ADD HYD
05735> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05736> [RDt= 1.00] out- 1.0 02:S,N8 38743.00 65.819 No_date 44:06 20.85 n/a .000
05737> [RDt= 1.00] out- 1.0 01:NI8 38743.00 65.819 No_date 44:06 20.85 n/a .000
05738> # Sum of hydrographs from Node 6 routed to Node 5
05739> # Section 6
05740> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05741> ADD HYD
05742> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05743> [RDt= 1.00] out- 1.0 02:S,N8 38743.00 65.819 No_date 44:06 20.85 n/a .000
05744> [RDt= 1.00] out- 1.0 01:NI8 38743.00 65.819 No_date 44:06 20.85 n/a .000
05745> [L/S/n=.3086/.082/.046] [Vmax=.477:Dmax= .960]
05746> # Sum of hydrographs from Node 5 routed to Node 4
05747> # Section 7
05748> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05749> ADD HYD
05750> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05751> [RDt= 1.00] out- 1.0 02:S,N8 38743.00 61.416 No_date 45:01 21.19 n/a .000
05752> [RDt= 1.00] out- 1.0 01:NI8 38743.00 61.416 No_date 45:01 21.19 n/a .000
05753> # Sum of hydrographs from Node 4 routed to Node 3
05754> # Section 6
05755> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05756> ADD HYD
05757> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05758> [RDt= 1.00] out- 1.0 02:S,N8 38743.00 61.416 No_date 45:01 21.19 n/a .000
05759> [RDt= 1.00] out- 1.0 01:NI8 38743.00 61.416 No_date 45:01 21.19 n/a .000
05760> # Sum of hydrographs from Node 3 routed to Node 2
05761> # Section 7
05762> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05763> ADD HYD
05764> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05765> [RDt= 1.00] out- 1.0 02:S,N8 40240.01 31.737 No_date 62:00 20.99 n/a .000
05766> [RDt= 1.00] out- 1.0 01:NI8 40240.01 31.737 No_date 62:00 20.99 n/a .000
05767> # Sum of hydrographs from Node 2 routed to Node 1
05768> # Section 8
05769> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05770> ADD HYD
05771> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05772> [RDt= 1.00] out- 1.0 02:S,N8 40240.01 31.737 No_date 62:00 20.99 n/a .000
05773> [RDt= 1.00] out- 1.0 01:NI8 40240.01 31.737 No_date 62:00 20.99 n/a .000
05774> # Sum of hydrographs from Node 1 routed to Node 0
05775> # Section 9
05776> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05777> ADD HYD
05778> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05779> [RDt= 1.00] out- 1.0 02:S,N8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05780> [RDt= 1.00] out- 1.0 01:NI8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05781> # Sum of hydrographs from Node 0 routed to Node -1
05782> # Section 10
05783> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05784> ADD HYD
05785> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05786> [RDt= 1.00] out- 1.0 02:S,N8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05787> [RDt= 1.00] out- 1.0 01:NI8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05788> # Sum of hydrographs from Node -1 routed to Node -2
05789> # Section 11
05790> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05791> ADD HYD
05792> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05793> [RDt= 1.00] out- 1.0 02:S,N8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05794> [RDt= 1.00] out- 1.0 01:NI8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05795> # Sum of hydrographs from Node -2 routed to Node -3
05796> # Section 12
05797> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05798> ADD HYD
05799> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05800> [RDt= 1.00] out- 1.0 02:S,N8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05801> [RDt= 1.00] out- 1.0 01:NI8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05802> # Sum of hydrographs from Node -3 routed to Node -4
05803> # Section 13
05804> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05805> ADD HYD
05806> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05807> [RDt= 1.00] out- 1.0 02:S,N8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05808> [RDt= 1.00] out- 1.0 01:NI8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05809> # Sum of hydrographs from Node -4 routed to Node -5
05810> # Section 14
05811> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05812> ADD HYD
05813> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05814> [RDt= 1.00] out- 1.0 02:S,N8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05815> [RDt= 1.00] out- 1.0 01:NI8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05816> # Sum of hydrographs from Node -5 routed to Node -6
05817> # Section 15
05818> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05819> ADD HYD
05820> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05821> [RDt= 1.00] out- 1.0 02:S,N8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05822> [RDt= 1.00] out- 1.0 01:NI8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05823> # Sum of hydrographs from Node -6 routed to Node -7
05824> # Section 16
05825> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05826> ADD HYD
05827> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05828> [RDt= 1.00] out- 1.0 02:S,N8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05829> [RDt= 1.00] out- 1.0 01:NI8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05830> # Sum of hydrographs from Node -7 routed to Node -8
05831> # Section 17
05832> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05833> ADD HYD
05834> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05835> [RDt= 1.00] out- 1.0 02:S,N8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05836> [RDt= 1.00] out- 1.0 01:NI8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05837> # Sum of hydrographs from Node -8 routed to Node -9
05838> # Section 18
05839> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05840> ADD HYD
05841> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05842> [RDt= 1.00] out- 1.0 02:S,N8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05843> [RDt= 1.00] out- 1.0 01:NI8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05844> # Sum of hydrographs from Node -9 routed to Node -10
05845> # Section 19
05846> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05847> ADD HYD
05848> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05849> [RDt= 1.00] out- 1.0 02:S,N8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05850> [RDt= 1.00] out- 1.0 01:NI8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05851> # Sum of hydrographs from Node -10 routed to Node -11
05852> # Section 20
05853> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05854> ADD HYD
05855> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05856> [RDt= 1.00] out- 1.0 02:S,N8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05857> [RDt= 1.00] out- 1.0 01:NI8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05858> # Sum of hydrographs from Node -11 routed to Node -12
05859> # Section 21
05860> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05861> ADD HYD
05862> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05863> [RDt= 1.00] out- 1.0 02:S,N8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05864> [RDt= 1.00] out- 1.0 01:NI8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05865> # Sum of hydrographs from Node -12 routed to Node -13
05866> # Section 22
05867> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05868> ADD HYD
05869> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05870> [RDt= 1.00] out- 1.0 02:S,N8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05871> [RDt= 1.00] out- 1.0 01:NI8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05872> # Sum of hydrographs from Node -13 routed to Node -14
05873> # Section 23
05874> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05875> ADD HYD
05876> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05877> [RDt= 1.00] out- 1.0 02:S,N8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05878> [RDt= 1.00] out- 1.0 01:NI8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05879> # Sum of hydrographs from Node -14 routed to Node -15
05880> # Section 24
05881> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05882> ADD HYD
05883> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05884> [RDt= 1.00] out- 1.0 02:S,N8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05885> [RDt= 1.00] out- 1.0 01:NI8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05886> # Sum of hydrographs from Node -15 routed to Node -16
05887> # Section 25
05888> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05889> ADD HYD
05890> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05891> [RDt= 1.00] out- 1.0 02:S,N8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05892> [RDt= 1.00] out- 1.0 01:NI8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05893> # Sum of hydrographs from Node -16 routed to Node -17
05894> # Section 26
05895> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05896> ADD HYD
05897> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05898> [RDt= 1.00] out- 1.0 02:S,N8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05899> [RDt= 1.00] out- 1.0 01:NI8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05900> # Sum of hydrographs from Node -17 routed to Node -18
05901> # Section 27
05902> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05903> ADD HYD
05904> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05905> [RDt= 1.00] out- 1.0 02:S,N8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05906> [RDt= 1.00] out- 1.0 01:NI8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05907> # Sum of hydrographs from Node -18 routed to Node -19
05908> # Section 28
05909> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05910> ADD HYD
05911> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05912> [RDt= 1.00] out- 1.0 02:S,N8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05913> [RDt= 1.00] out- 1.0 01:NI8 45401.01 51.312 No_date 35:12 21.56 n/a .000
05914> # Sum of hydrographs from Node -19 routed to Node -20
05915> # Section 29
05916> # DYN-ID:NHYD---AReAha-QPEAKcms-TpeakDate_bh:mm---RVm-R.C.--DWFcms
05917> ADD HYD
05918> # DYN-ID:NHYD---AReAha-Q
```

05985\* ROUTE RESERVOIR -> 1.0 02-ST-2 .59 .075 No\_date 28:00 38.69 n/a .000

05986\* [ROUTE RESERVOIR] 1.0 01-ST-7T .59 .052 No\_date 28:00 38.69 n/a .000

05987\* [overline] <- 1.0 02-ST-25DFN .00 .000 No\_date 28:00 38.69 n/a .000

05988\* [McStCUsed:18352-00 m3\_TotVolVol=.00000 m3\_N-Ovfr\_0\_TotDurfv= 0\_hrs]

05989\* D0101:CO0090-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

CONTINUOUS NASHYD 1.0 01-ST-2 .60 .057 No\_date 28:04 22.40 .346 .000

05990\* [CN# 69.01 Tp: 3.00 Tp: 1.001] .60 .057 No\_date 28:04 22.40 .346 .000

05991\* [IaRecEmpc: 4.00: IRPDR: 1.001] .60 .057 No\_date 28:04 22.40 .346 .000

05992\* [ROUTE RESERVOIR] 1.0 01-ST-2 .000 .000 No\_date 28:04 22.40 .346 .000

05993\* [XDM: 64-TIMW-.85] .60 .057 No\_date 28:04 22.40 .346 .000

05994\* R0101:CO0090-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

ROUTE RESERVOIR 1.0 02-ST-8 60.55 .087 No\_date 29:04 22.40 n/a .000

05995\* [ROUTE RESERVOIR] 1.0 01-ST-25DFN .00 .000 No\_date 29:04 22.40 n/a .000

05996\* [ROUTE 1.001 out] .00 .000 No\_date 29:04 22.40 n/a .000

05997\* [L/S/no: 335 / .100/.013] .00 .000 No\_date 29:04 22.40 n/a .000

05998\* [ROUTE 1.001 in] .00 .000 No\_date 29:04 22.40 n/a .000

05999\* [ROUTE 1.201WOTC] .00 .000 No\_date 29:04 22.40 n/a .000

06000\* R0101:CO0091-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

ADD HYD 1.0 02-ST-25AIN1 261.13 .072 No\_date 28:01 19.19 .000

06001\* + 1.0 02-D1 1.37 .058 No\_date 28:12 29.30 n/a .000

06002\* + 1.0 02-A1-ST-2 2.50 .098 No\_date 28:12 29.30 n/a .000

06003\* + 1.0 02-ST-2 1.00 .060 No\_date 28:12 29.30 n/a .000

06004\* + 1.0 02-ST25TR 2.59 .052 No\_date 28:05 38.69 n/a .000

06005\* + 1.0 02-ST 2 .59 .052 No\_date 28:05 38.69 n/a .000

06006\* + 1.0 02-ST 2 .00 .000 No\_date 28:05 38.69 n/a .000

06007\* + 1.0 02-ST 2 .00 .000 No\_date 28:05 38.69 n/a .000

06008\* SUM: 1.0 01-ST-2-IN 326.12 3.771 No\_date 28:40 18.45 .45 n/a .000

06009\* R0101:CO0092-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

CONTINUOUS NASHYD 1.0 01-ST-1 3.51 .598 No\_date 28:01 50.29 .777 .000

06010\* [XDM: 68-TIMW-.85] .598 No\_date 28:01 50.29 .777 .000

06011\* [Horton parameters] Po: 76.20Pc 13.20DcV4.14 Fc: .001

06012\* [Infiltration] 1.0 01-ST-2 60.55 .087 No\_date 28:01 50.29 .777 .000

06013\* [overline] <- 1.0 01-ST-2 60.55 .087 No\_date 28:01 50.29 .777 .000

06014\* [Impervious] area: IaImpg: 1.57SL1D+.50:LG112.265..MM1+.013:SCI+ .000

06015\* [IaRecEmpc: 4.00: IRPDR: 1.001] .00 .000 No\_date 28:01 50.29 .777 .000

06016\* R0101:CO0094-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

CONTINUOUS NASHYD 1.0 01-ST-1 .00 .000 No\_date 28:01 38.69 .598 .000

06017\* ROUTE RESERVOIR -> 1.0 02-ST-2 3.51 .538 No\_date 28:01 50.29 n/a .000

06018\* out <- 1.0 01-ST-2 3.51 .139 No\_date 28:01 50.29 n/a .000

06019\* overline <- 1.0 01-ST-2 3.51 .139 No\_date 28:01 50.29 n/a .000

06020\* [McStCUsed: .81676-01 m3\_TotVolVol=.00000 m3\_N-Ovfr\_0\_TotDurfv= 0\_hrs]

06021\* R0101:CO0094-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

CONTINUOUS NASHYD 1.0 01-ST-1 .00 .000 No\_date 28:01 38.69 .598 .000

06022\* [XDM: 46-TIMW-.57] .00 .000 No\_date 28:01 38.69 .598 .000

06023\* [Horton parameters] Po: 76.20Pc 13.20DcV4.14 Fc: .001

06024\* [Infiltration] 1.0 01-ST-2 60.55 .087 No\_date 28:01 50.29 .777 .000

06025\* [overline] <- 1.0 01-ST-2 60.55 .087 No\_date 28:01 50.29 .777 .000

06026\* [Impervious] area: IaImpg: 1.57SL1D+.50:LG112.119..MM1+.013:SCI+ .000

06027\* [IaRecEmpc: 4.00: IRPDR: 1.001] .00 .000 No\_date 28:01 50.29 .777 .000

06028\* R0101:CO0097-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

CONTINUOUS NASHYD 1.0 01-ST-1 .00 .000 No\_date 28:01 38.69 .598 .000

06029\* ROUTE RESERVOIR -> 1.0 02-ST-2 .71 .088 No\_date 28:00 38.69 n/a .000

06030\* out <- 1.0 01-ST-2 71.00 .088 No\_date 28:00 38.69 n/a .000

06031\* overline <- 1.0 01-ST-2 71.00 .088 No\_date 28:00 38.69 n/a .000

06032\* [McStCUsed: .18898-02 m3\_TotVolVol=.00000 m3\_N-Ovfr\_0\_TotDurfv= 0\_hrs]

06033\* R0101:CO0096-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

CONTINUOUS NASHYD 1.0 01-ST-1 .00 .000 No\_date 28:00 38.69 .598 .000

06034\* ADD HYD 1.0 02-ST-2-IN 59.41 .072 No\_date 28:01 25.50 n/a .000

06035\* + 1.0 02-A1-ST-2 1.51 .139 No\_date 28:01 25.50 n/a .000

06036\* + 1.0 02-ST-2 1.00 .060 No\_date 28:01 25.50 n/a .000

06037\* + 1.0 02-ST25TR .71 .063 No\_date 28:05 38.69 n/a .000

06038\* + 1.0 02-ST30V 2.00 .000 No\_date 0:00 0:n/a .000

06039\* SUM: 1.0 01-ST-2 336.00 3.914 No\_date 28:40 18.83 n/a .000

06040\* R0101:CO0097-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

CONTINUOUS NASHYD 1.0 01-ST-1 .00 .000 No\_date 28:00 38.69 .598 .000

06041\* ROUTE CHANNEL -> 1.0 02-ST25ST 330.34 3.914 No\_date 28:39 18.83 n/a .000

06042\* out <- 1.0 01-ST25ST 330.34 3.914 No\_date 28:39 18.83 n/a .000

06043\* [L/S/no: 592 / .230/.043] .00 .000 No\_date 28:39 18.83 n/a .000

06044\* [Vmax: .582-1Max: 1.002] .00 .000 No\_date 28:39 18.83 n/a .000

06045\* R0101:CO0098-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

CONTINUOUS NASHYD 1.0 01-ST-2 2.28 .046 No\_date 29:04 29.30 .453 .000

06046\* [CN# 84.01 N 3.00 Tp: .99] .00 .000 No\_date 29:04 29.30 .453 .000

06047\* [InterEventTime: 12.00] .00 .000 No\_date 29:04 29.30 .453 .000

06048\* R0101:CO0099-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

CONTINUOUS NASHYD 1.0 01-ST-1 .00 .000 No\_date 28:00 38.69 .598 .000

06049\* [XDM: 68-TIMW-.85] .00 .000 No\_date 28:00 38.69 .598 .000

06050\* [Horton parameters] Po: 76.20Pc 13.20DcV4.14 Fc: .001

06051\* [Infiltration] 1.0 01-ST-2 60.55 .087 No\_date 28:04 20.00 .50 .000

06052\* [overline] <- 1.0 01-ST-2 60.55 .087 No\_date 28:04 20.00 .50 .000

06053\* [Impervious] area: IaImpg: 1.57SL1D+.50:LG112.491..MM1+.013:SCI+ .000

06054\* [IaRecEmpc: 4.00: IRPDR: 1.001] .00 .000 No\_date 28:04 20.00 .50 .000

06055\* R0101:CO0100-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

CONTINUOUS NASHYD 1.0 01-ST-1 .00 .000 No\_date 28:04 20.00 .50 .000

06056\* [XDM: 46-TIMW-.57] .00 .000 No\_date 28:04 20.00 .50 .000

06057\* [Horton parameters] Po: 76.20Pc 13.20DcV4.14 Fc: .001

06058\* [Infiltration] 1.0 01-ST-2 60.55 .087 No\_date 28:04 20.00 .50 .000

06059\* [overline] <- 1.0 01-ST-2 60.55 .087 No\_date 28:04 20.00 .50 .000

06060\* [McStCUsed: .27180-01 m3\_TotVolVol=.00000 m3\_N-Ovfr\_0\_TotDurfv= 0\_hrs]

06061\* R0101:CO0101-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

CONTINUOUS NASHYD 1.0 01-ST-1 .00 .000 No\_date 28:00 38.69 .598 .000

06062\* [XDM: 68-TIMW-.85] .00 .000 No\_date 28:00 38.69 .598 .000

06063\* ROUTE RESERVOIR -> 1.0 02-ST-2 330.34 3.640 No\_date 29:01 25.50 n/a .000

06064\* out <- 1.0 01-ST-2 330.34 3.640 No\_date 29:01 25.50 n/a .000

06065\* overline <- 1.0 01-ST-2 330.34 3.640 No\_date 29:01 25.50 n/a .000

06066\* [McStCUsed: .18898-02 m3\_TotVolVol=.00000 m3\_N-Ovfr\_0\_TotDurfv= 0\_hrs]

06067\* R0101:CO0102-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

CONTINUOUS NASHYD 1.0 01-ST-1 .00 .000 No\_date 28:00 38.69 .598 .000

06068\* ROUTE RESERVOIR -> 1.0 02-A1ST 1.00 .000 No\_date 28:04 20.00 .50 .000

06069\* out <- 1.0 01-A1ST78 1.00 .000 No\_date 28:04 20.00 .50 .000

06070\* overline <- 1.0 01-A1ST78 1.00 .000 No\_date 28:04 20.00 .50 .000

06071\* [ROUTE RESERVOIR] 1.0 02-ST-4 .35 .046 No\_date 28:08 38.69 n/a .000

06072\* out <- 1.0 01-ST-2 35.00 .031 No\_date 28:08 38.69 n/a .000

06073\* overline <- 1.0 01-ST-2 35.00 .031 No\_date 28:08 38.69 n/a .000

06074\* [McStCUsed: .18898-02 m3\_TotVolVol=.00000 m3\_N-Ovfr\_0\_TotDurfv= 0\_hrs]

06075\* R0101:CO0103-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

CONTINUOUS NASHYD 1.0 01-ST-1 .00 .000 No\_date 28:00 38.69 .598 .000

06076\* [XDM: 68-TIMW-.85] .00 .000 No\_date 28:00 38.69 .598 .000

06077\* [Horton parameters] Po: 76.20Pc 13.20DcV4.14 Fc: .001

06078\* [Infiltration] 1.0 01-ST-2 60.55 .087 No\_date 28:04 20.00 .50 .000

06079\* [overline] <- 1.0 01-ST-2 60.55 .087 No\_date 28:04 20.00 .50 .000

06080\* [McStCUsed: .18898-02 m3\_TotVolVol=.00000 m3\_N-Ovfr\_0\_TotDurfv= 0\_hrs]

06081\* R0101:CO0104-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

CONTINUOUS NASHYD 1.0 01-ST-1 .00 .000 No\_date 28:00 38.69 .598 .000

06082\* ROUTE RESERVOIR -> 1.0 02-ST-2 330.34 3.640 No\_date 29:01 25.50 n/a .000

06083\* out <- 1.0 01-ST-2 330.34 3.640 No\_date 29:01 25.50 n/a .000

06084\* overline <- 1.0 01-ST-2 330.34 3.640 No\_date 29:01 25.50 n/a .000

06085\* [McStCUsed: .18898-02 m3\_TotVolVol=.00000 m3\_N-Ovfr\_0\_TotDurfv= 0\_hrs]

06086\* R0101:CO0106-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

CONTINUOUS NASHYD 1.0 01-ST-1 .00 .000 No\_date 28:00 38.69 .598 .000

06087\* [XDM: 68-TIMW-.85] .00 .000 No\_date 28:00 38.69 .598 .000

06088\* ROUTE RESERVOIR -> 1.0 02-ST-2 330.34 3.640 No\_date 29:01 25.50 n/a .000

06089\* out <- 1.0 01-ST-2 330.34 3.640 No\_date 29:01 25.50 n/a .000

06090\* overline <- 1.0 01-ST-2 330.34 3.640 No\_date 29:01 25.50 n/a .000

06091\* [ROUTE RESERVOIR] 1.0 02-ST45ST 330.34 .031 No\_date 28:08 38.69 n/a .000

06092\* out <- 1.0 01-ST45ST 330.34 .031 No\_date 28:08 38.69 n/a .000

06093\* overline <- 1.0 01-ST45ST 330.34 .031 No\_date 28:08 38.69 n/a .000

06094\* [ROUTE RESERVOIR] 1.0 02-A1ST9V 5.30 .206 No\_date 28:07 25.50 n/a .000

06095\* out <- 1.0 01-A1ST9V 5.30 .000 No\_date 0:00 0:n/a .000

06096\* overline <- 1.0 01-A1ST9V 5.30 .000 No\_date 0:00 0:n/a .000

06097\* [McStCUsed: .00166-01 m3\_TotVolVol=.00000 m3\_N-Ovfr\_0\_TotDurfv= 0\_hrs]

06098\* R0101:CO0107-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

CONTINUOUS NASHYD 1.0 01-ST-1 .00 .000 No\_date 28:00 38.69 .598 .000

06099\* [XDM: 68-TIMW-.85] .00 .000 No\_date 28:00 38.69 .598 .000

06100\* [Horton parameters] Po: 76.20Pc 13.20DcV4.14 Fc: .001

06101\* [Infiltration] 1.0 01-ST-2 60.55 .087 No\_date 28:04 20.00 .50 .000

06102\* [overline] <- 1.0 01-ST-2 60.55 .087 No\_date 28:04 20.00 .50 .000

06103\* [McStCUsed: .79308-01 m3\_TotVolVol=.00000 m3\_N-Ovfr\_0\_TotDurfv= 0\_hrs]

06104\* R0101:CO0108-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

CONTINUOUS NASHYD 1.0 01-ST-1 .00 .000 No\_date 28:00 38.69 .598 .000

06105\* [XDM: 68-TIMW-.85] .00 .000 No\_date 28:00 38.69 .598 .000

06106\* [Horton parameters] Po: 76.20Pc 13.20DcV4.14 Fc: .001

06107\* [Infiltration] 1.0 01-ST-2 60.55 .087 No\_date 28:04 20.00 .50 .000

06108\* [overline] <- 1.0 01-ST-2 60.55 .087 No\_date 28:04 20.00 .50 .000

06109\* [McStCUsed: .27180-01 m3\_TotVolVol=.00000 m3\_N-Ovfr\_0\_TotDurfv= 0\_hrs]

06110\* R0101:CO0109-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

CONTINUOUS NASHYD 1.0 01-ST-1 .00 .000 No\_date 28:00 38.69 .598 .000

06111\* [XDM: 68-TIMW-.85] .00 .000 No\_date 28:00 38.69 .598 .000

06112\* [ROUTE RESERVOIR] 1.0 02-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06113\* out <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06114\* overline <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06115\* [ROUTE RESERVOIR] 1.0 02-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06116\* out <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06117\* overline <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06118\* [ROUTE RESERVOIR] 1.0 02-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06119\* out <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06120\* overline <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06121\* [ROUTE RESERVOIR] 1.0 02-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06122\* out <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06123\* overline <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06124\* [ROUTE RESERVOIR] 1.0 02-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06125\* out <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06126\* overline <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06127\* [ROUTE RESERVOIR] 1.0 02-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06128\* out <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06129\* overline <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06130\* [ROUTE RESERVOIR] 1.0 02-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06131\* ADD HYD 1.0 02-ST5AIN1 350.31 .037 No\_date 29:17 20.48 n/a .000

06132\* + 1.0 02-ID1 2.51 .072 No\_date 28:44 32.13 .497 .000

06133\* + 1.0 02-ID5 2.24 .052 No\_date 28:44 32.13 .497 .000

06134\* + 1.0 02-ID7 3.14 .052 No\_date 28:44 32.13 .497 .000

06135\* + 1.0 02-ID9 1.00 .000 No\_date 0:00 0:n/a .000

06136\* + 1.0 02-A1ST2 5.30 .206 No\_date 28:07 25.50 n/a .000

06137\* SUM: 1.0 01-ST-5 356.60 4.191 No\_date 29:15 20.48 n/a .000

06138\* R0101:CO0110-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

CONTINUOUS NASHYD 1.0 01-ST-1 .00 .000 No\_date 28:00 38.69 .598 .000

06139\* [XDM: 68-TIMW-.85] .00 .000 No\_date 28:00 38.69 .598 .000

06140\* [Horton parameters] Po: 76.20Pc 13.20DcV4.14 Fc: .001

06141\* [Infiltration] 1.0 01-ST-2 60.55 .087 No\_date 28:04 20.00 .49 .000

06142\* [overline] <- 1.0 01-ST-2 60.55 .087 No\_date 28:04 20.00 .49 .000

06143\* [McStCUsed: 1.01315-01 m3\_TotVolVol=.00000 m3\_N-Ovfr\_0\_TotDurfv= 0\_hrs]

06144\* R0101:CO0111-----DtnID:INHYD---ARAhA-QPEAKms-Tpeakdate\_bh:mm:--Rvn-R.C.--DWFcms

CONTINUOUS NASHYD 1.0 01-ST-1 .00 .000 No\_date 28:00 38.69 .598 .000

06145\* [XDM: 68-TIMW-.85] .00 .000 No\_date 28:00 38.69 .598 .000

06146\* [ROUTE RESERVOIR] 1.0 02-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06147\* out <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06148\* overline <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06149\* [ROUTE RESERVOIR] 1.0 02-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06150\* out <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06151\* overline <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06152\* [ROUTE RESERVOIR] 1.0 02-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06153\* out <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06154\* overline <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06155\* [ROUTE RESERVOIR] 1.0 02-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06156\* out <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06157\* overline <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06158\* [ROUTE RESERVOIR] 1.0 02-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06159\* out <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06160\* overline <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06161\* [ROUTE RESERVOIR] 1.0 02-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06162\* out <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06163\* overline <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06164\* [ROUTE RESERVOIR] 1.0 02-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06165\* out <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06166\* overline <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06167\* [ROUTE RESERVOIR] 1.0 02-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06168\* out <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06169\* overline <- 1.0 01-ST-5 4.00 .058 No\_date 28:01 50.29 n/a .000

06170\* [ROUTE RES

[Impervious areas: IAimp= 4.00; IAICPerc = 4.00]

[SMIN= 26.77; SMAZ=244.49; SK= .010]

6363# # Foster Pond

- Rating curve obtained assuming 4m/s in 24 hours for quality control

- Rating curve basic of the catchment area to the West Clarke pond rating curve

6366# # from the MSS for the new coordinates

6367# \*\*\*\*\*

6368# R010:CO0150- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6369# ROUTE RESERVOIR -> 1.0 0.2 POFESTER-OUT 325.44 22.87 No\_Data 2813 43.99 n/a .000

6370# + 1.0 0.2 POF-OUT 325.44 6.03 No\_Data 2813 43.99 n/a .000

6371# overflow<-----+ 1.0 0.2 POF-OUT 325.44 6.03 No\_Data 0.00 43.99 n/a .000

6372# [MxModSet=.58628+01 m3, TotDvOfw=.00008 m3, N-Ovr= 0, TotDvOfw= 0.(hrs)]

6373# ADD HWD + 1.0 0.2 POF-OUT 325.44 6.03 No\_Data 2936 43.99 n/a .000

6374# SUM + 1.0 0.2 POF-OUT 325.44 6.03 No\_Data 0.00 43.99 n/a .000

6375# + 1.0 0.2 POF-OUT 325.44 6.03 No\_Data 2936 43.99 n/a .000

6376# \*\*\*\*\*

6377# R010:CO0152- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6378# CONTOUS STANDBY 1.0 0.1 SWP-FD 73.29 7.523 No\_Data 2815 47.94 .741 .000

[XIMP= 6.07; TIND=.65]

[LOSS: 2.0% IN: 77.0]

[Previous areas: IAimp= 4.67; SLDP=.01; LDG= 40. MNPD=.250; SCP= .01]

[IAICPerc = 4.00; IAICPerc = 4.00]

[SMIN= 31.15; SMAZ=207.66; SK= .010]

6381# ROUTE RESERVOIR -> 1.0 0.2 W2W\_CLAR\_BRA 73.29 7.523 No\_Data 2805 47.94 .741 .000

6382# [Previous areas: IAimp= 4.67; SLDP=.01; LDG= 40. MNPD=.250; SCP= .01]

[IAICPerc = 4.00; IAICPerc = 4.00]

[SMIN= 31.15; SMAZ=207.66; SK= .010]

[IAimpCng = 4.00; IAimpCng = 4.00]

6385# overflow<-----+ 1.0 0.2 POF-OUT 325.44 6.03 No\_Data 2813 43.99 n/a .000

6386# [MxModSet=.58628+01 m3, TotDvOfw=.00008 m3, N-Ovr= 0, TotDvOfw= 0.(hrs)]

6387# ADD HWD + 1.0 0.2 POF-OUT 325.44 6.03 No\_Data 2936 43.99 n/a .000

6388# SUM + 1.0 0.2 POF-OUT 325.44 6.03 No\_Data 0.00 43.99 n/a .000

6389# + 1.0 0.2 POF-OUT 325.44 6.03 No\_Data 2936 43.99 n/a .000

6390# \*\*\*\*\*

6391# R010:CO0153- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6392# CONTOUS STANDBY 1.0 0.1 SWP-FD 4.94 .594 No\_Data 2811 43.99 .690 .000

[XIMP= 5.57; TIND=.65]

[LOSS: 2.0% IN: 74.0]

[Previous areas: IAimp= 4.67; SLDP=.01; LDG= 40. MNPD=.250; SCP= .01]

[IAICPerc = 4.00; IAICPerc = 4.00]

[SMIN= 31.15; SMAZ=207.66; SK= .010]

6395# ROUTE RESERVOIR -> 1.0 0.2 W2W\_CLAR\_BRA 73.29 7.523 No\_Data 2805 47.94 .741 .000

6396# [Previous areas: IAimp= 1.57; SLDP=.10; LDG= 185. MNPD=.013; SCP= .01]

[IAICPerc = 4.00; IAICPerc = 4.00]

[SMIN= 31.15; SMAZ=207.66; SK= .010]

6399# R010:CO0155- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6400# ADD HWD + 1.0 0.2 POFESTER-OUT 325.44 6.03 No\_Data 2936 43.99 n/a .000

6401# SUM + 1.0 0.2 POF-OUT 325.44 6.03 No\_Data 0.00 43.99 n/a .000

6402# + 1.0 0.1 SWP-FD 330.38 6.115 No\_Data 2904 43.99 n/a .000

6403# \*\*\*\*\*

6404# R010:CO0156- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6405# SAVE HWD + 1.0 0.1 SWP-FD 330.38 6.115 No\_Data 2936 43.99 n/a .000

6406# fname : R080\_0010

6407# \*\*\*\*\*

6408# # Hydrograph from Node Foster Station 980 to Foster Drain

6409# # Channel X-Section obtained from RIVCA Hydraulic Model - Station 980

6410# \*\*\*\*\*

6411# R010:CO0157- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6412# CATCHMENT > 1.0 0.2 POFESTER-OUT 325.44 6.03 No\_Data 2936 43.99 n/a .000

[RDT=.001] out<-----+ 1.0 0.2 POF-OUT 325.44 6.03 No\_Data 0.00 43.99 n/a .000

[L/S=.400/. .400/.035]

[Vmax= 6.74; Dmax=1.981]

6414# \*\*\*\*\*

6415# R010:CO0158- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6416# CONTINUOUS STANDBY 1.0 0.18-S-PD-FD 5.11 .702 No\_Data 2800 48.24 .746 .000

6417# \*\*\*\*\*

6418# R010:CO0159- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6419# CONTOUS STANDBY 1.0 0.18-S-PD-FD 7.00 .702 No\_Data 2800 48.24 .746 .000

6420# \*\*\*\*\*

6421# Previous areas: IAimp= 4.67; SLDP=.50; LDG= 40. MNPD=.250; SCP= .01

[IAICPerc = 4.00; IAICPerc = 4.00]

[SMIN= 36.67; SMAZ=244.49; SK= .010]

6423# \*\*\*\*\*

6424# R010:CO0160- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6425# ADD HWD + 1.0 0.2 POFESTER-OUT 325.44 6.03 No\_Data 2936 43.99 n/a .000

6426# SUM + 1.0 0.1 SWP-FD 5.11 .702 No\_Data 2800 48.24 .746 .000

6427# \*\*\*\*\*

6428# R010:CO0161- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6429# SAVE HWD + 1.0 0.1 SWP-FD 335.49 5.966 No\_Data 2936 43.99 n/a .000

6430# \*\*\*\*\*

6431# fname : R080\_0010

6432# \*\*\*\*\*

6433# # Hydrograph from Station 520 on Foster Drain (Foster) to Node at station 6016 (Jock River)

6434# # Channel X-Section obtained from RIVCA Hydraulic Model - Station 520

6435# \*\*\*\*\*

6436# R010:CO0162- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6437# CATCHMENT > 1.0 0.2 POFESTER-OUT 325.44 6.03 No\_Data 2936 44.05 n/a .000

[RDT=.001] out<-----+ 1.0 0.2 POF-OUT 325.44 6.03 No\_Data 0.00 44.05 n/a .000

[L/S=.860/. .860/.035]

[Vmax= 1.391; Dmax=1.659]

6439# \*\*\*\*\*

6440# R010:CO0163- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6441# CONTINUOUS STANDBY 1.0 0.18-S-PD-FD 14.96 1.881 No\_Data 2802 48.24 .746 .000

6442# \*\*\*\*\*

6443# R010:CO0164- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6444# CONTOUS STANDBY 1.0 0.18-S-PD-FD 5.27 1.781 No\_Data 2800 43.99 n/a .000

6445# \*\*\*\*\*

6446# R010:CO0165- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6447# CONTINUOUS STANDBY 1.0 0.18-S-PD-FD 7.00 1.781 No\_Data 2800 43.99 n/a .000

6448# \*\*\*\*\*

6449# R010:CO0166- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6450# CONTOUS STANDBY 1.0 0.18-S-PD-FD 5.27 1.781 No\_Data 2800 43.99 n/a .000

6451# \*\*\*\*\*

6452# R010:CO0167- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6453# CONTOUS STANDBY 1.0 0.18-S-PD-FD 5.27 1.781 No\_Data 2800 43.99 n/a .000

6454# \*\*\*\*\*

6455# R010:CO0168- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6456# CONTOUS STANDBY 1.0 0.18-S-PD-FD 5.27 1.781 No\_Data 2800 43.99 n/a .000

6457# [CEN: 77.0; N: 0.0; E: 70. ; F: 62]

[InterEventTime= 12.00]

6458# \*\*\*\*\*

6459# R010:CO0169- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6460# CONTOUS STANDBY 1.0 0.1 SWP-FD 35.65 .596 No\_Data 2911 26.85 .415 .000

6461# \*\*\*\*\*

6462# R010:CO0170- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6463# CONTOUS STANDBY 1.0 0.1 SWP-FD 35.65 .596 No\_Data 2911 26.85 .415 .000

6464# \*\*\*\*\*

6465# R010:CO0166- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6466# ADD HWD + 1.0 0.2 POFESTER-OUT 325.44 6.03 No\_Data 2936 44.05 n/a .000

6467# SUM + 1.0 0.2 POF-OUT 325.44 6.03 No\_Data 0.00 44.05 n/a .000

6468# \*\*\*\*\*

6469# R010:CO0171- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6470# CONTOUS STANDBY 1.0 0.1 SWP-FD 5.27 1.781 No\_Data 2800 43.99 n/a .000

6471# \*\*\*\*\*

6472# R010:CO0172- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6473# CONTOUS STANDBY 1.0 0.1 SWP-FD 5.27 1.781 No\_Data 2800 43.99 n/a .000

6474# \*\*\*\*\*

6475# R010:CO0173- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6476# CONTOUS STANDBY 1.0 0.1 SWP-FD 5.27 1.781 No\_Data 2800 43.99 n/a .000

6477# \*\*\*\*\*

6478# R010:CO0174- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6479# CONTOUS STANDBY 1.0 0.1 SWP-FD 5.27 1.781 No\_Data 2800 43.99 n/a .000

6480# \*\*\*\*\*

6481# R010:CO0175- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6482# CONTOUS STANDBY 1.0 0.1 SWP-FD 5.27 1.781 No\_Data 2800 43.99 n/a .000

6483# \*\*\*\*\*

6484# R010:CO0176- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6485# CONTOUS STANDBY 1.0 0.1 SWP-FD 5.27 1.781 No\_Data 2800 43.99 n/a .000

6486# \*\*\*\*\*

6487# R010:CO0177- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6488# CONTOUS STANDBY 1.0 0.1 SWP-FD 5.27 1.781 No\_Data 2800 43.99 n/a .000

6489# \*\*\*\*\*

6490# R010:CO0178- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6491# CONTOUS STANDBY 1.0 0.1 SWP-FD 5.27 1.781 No\_Data 2800 43.99 n/a .000

6492# \*\*\*\*\*

6493# R010:CO0179- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6494# CONTOUS STANDBY 1.0 0.1 SWP-FD 5.27 1.781 No\_Data 2800 43.99 n/a .000

6495# \*\*\*\*\*

6496# R010:CO0180- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6497# CONTOUS STANDBY 1.0 0.1 SWP-FD 5.27 1.781 No\_Data 2800 43.99 n/a .000

6498# \*\*\*\*\*

6499# R010:CO0181- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6500# CONTOUS STANDBY 1.0 0.1 SWP-FD 5.27 1.781 No\_Data 2800 43.99 n/a .000

6501# \*\*\*\*\*

6502# R010:CO0182- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6503# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6504# \*\*\*\*\*

6505# R010:CO0183- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6506# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6507# \*\*\*\*\*

6508# R010:CO0184- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6509# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6510# \*\*\*\*\*

6511# R010:CO0185- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6512# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6513# \*\*\*\*\*

6514# R010:CO0186- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6515# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6516# \*\*\*\*\*

6517# R010:CO0187- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6518# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6519# \*\*\*\*\*

6520# R010:CO0188- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6521# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6522# \*\*\*\*\*

6523# R010:CO0189- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6524# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6525# \*\*\*\*\*

6526# R010:CO0190- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6527# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6528# \*\*\*\*\*

6529# R010:CO0191- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6530# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6531# \*\*\*\*\*

6532# R010:CO0192- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6533# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6534# \*\*\*\*\*

6535# R010:CO0193- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6536# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6537# \*\*\*\*\*

6538# R010:CO0194- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6539# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6540# \*\*\*\*\*

6541# R010:CO0195- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6542# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6543# \*\*\*\*\*

6544# R010:CO0196- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6545# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6546# \*\*\*\*\*

6547# R010:CO0197- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6548# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6549# \*\*\*\*\*

6550# R010:CO0198- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6551# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6552# \*\*\*\*\*

6553# R010:CO0199- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6554# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6555# \*\*\*\*\*

6556# R010:CO0200- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6557# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6558# \*\*\*\*\*

6559# R010:CO0201- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6560# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6561# \*\*\*\*\*

6562# R010:CO0202- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6563# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6564# \*\*\*\*\*

6565# R010:CO0203- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6566# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6567# \*\*\*\*\*

6568# R010:CO0204- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6569# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6570# \*\*\*\*\*

6571# R010:CO0205- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6572# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6573# \*\*\*\*\*

6574# R010:CO0206- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6575# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6576# \*\*\*\*\*

6577# R010:CO0207- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6578# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6579# \*\*\*\*\*

6580# R010:CO0208- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6581# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6582# \*\*\*\*\*

6583# R010:CO0209- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6584# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6585# \*\*\*\*\*

6586# R010:CO0210- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6587# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6588# \*\*\*\*\*

6589# R010:CO0211- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6590# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6591# \*\*\*\*\*

6592# R010:CO0212- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6593# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6594# \*\*\*\*\*

6595# R010:CO0213- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6596# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6597# \*\*\*\*\*

6598# R010:CO0214- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6599# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6600# \*\*\*\*\*

6601# R010:CO0215- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6602# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6603# \*\*\*\*\*

6604# R010:CO0216- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6605# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6606# \*\*\*\*\*

6607# R010:CO0217- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6608# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6609# \*\*\*\*\*

6610# R010:CO0218- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6611# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6612# \*\*\*\*\*

6613# R010:CO0219- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6614# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6615# \*\*\*\*\*

6616# R010:CO0220- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6617# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6618# \*\*\*\*\*

6619# R010:CO0221- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6620# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6621# \*\*\*\*\*

6622# R010:CO0222- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6623# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6624# \*\*\*\*\*

6625# R010:CO0223- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6626# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6627# \*\*\*\*\*

6628# R010:CO0224- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6629# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6630# \*\*\*\*\*

6631# R010:CO0225- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6632# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6633# \*\*\*\*\*

6634# R010:CO0226- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6635# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6636# \*\*\*\*\*

6637# R010:CO0227- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6638# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6639# \*\*\*\*\*

6640# R010:CO0228- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6641# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6642# \*\*\*\*\*

6643# R010:CO0229- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,hh:mm---RVmR-C.----DWFcms

6644# CONTOUS STANDBY 1.0 0.1 SWP-FD 21.67 2.814 No\_Data 2802 48.63 .752 .000

6645# \*\*\*\*\*

6646# R010:CO0230- > DtnIn:ID:NHDY--- AREAbh-QPEAKmcspkate,h



07107+ + 1. 0 02:FRASER-DRN 13.65 .447 No\_date 28:22 26.85 n/a .000  
 07108+ + 1. 0 02:FRASER-DRN 21.43 .281 No\_date 27:57 47.46 n/a .000  
 07109+ + 1. 0 02:FCP-01-S 54685.44 .851 No\_date 27:57 23.91 n/a .000  
 07110+ + 1. 0 02:FCP-01-S 8.03 .756 No\_date 27:57 23.91 n/a .000  
 07111+ + 1. 0 02:FCP-02-S 16.91 .159 No\_date 27:57 58.56 n/a .000  
 07112+ + 1. 0 02:FCP-02-S 7.37 .359 No\_date 27:57 23.91 n/a .000  
 07113+ SUM+ 1. 0 01:4241 54685.45 86.106 No\_date 35:57 22.98 n/a .000  
 07114+ ROUTE CHANNEL > 1. 0 02:4241 54685.45 86.106 No\_date 35:57 22.98 n/a .000  
 07115+ [ROUTE\_ID: 294... / .109/.036]  
 07116+ [Vmax: 1.173 Dmax: 2.018]  
 07117+ R0010:CO0268+ DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07118+ SAVE HYD  
 07119+ name : 4241\_0010  
 07120+ remark:Total flows at Ken-Burnett outlet  
 07121+ # Hydrograph from Ken-Burnett to station 3633  
 07122+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07123+ R0010:CO0270-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07124+ ROUTE CHANNEL > 1. 0 02:4241 54685.45 86.106 No\_date 35:57 22.98 n/a .000  
 07125+ [ROUTE\_ID: 294... / .109/.036]  
 07126+ [Vmax: 1.173 Dmax: 2.018]  
 07127+ R0010:CO0271-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07128+ ADD HYD  
 07129+ + 1. 0 02:4241 54685.45 86.076 No\_date 35:57 22.98 n/a .000  
 07130+ + 1. 0 01:SNK-XB 6.32 .161 No\_date 35:57 22.98 n/a .000  
 07131+ + 1. 0 02:JRN-02-S 1.59 .153 No\_date 27:51 46.12 n/a .000  
 07132+ SUM+ 1. 0 01:SNK-XB 54681.14 86.123 No\_date 35:57 22.99 n/a .000  
 07133+ R0010:CO0272-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07134+ SAVE HYD  
 07135+ name : SN\_XB\_0010  
 07136+ remark:Hydrograph from Station 3633 [Total Flow between Station 3633]  
 07137+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07138+ JFSA 2021-02-26 change the channel length (at station 3633) from 650m to 608m and change the slope from 0.0498t to 0.2  
 07139+ R0010:CO0273-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07140+ R0010:CO0274-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07141+ [ROUTE\_ID: 294... / .109/.036]  
 07142+ [ROUTE\_ID: 1. 001:OUT 1. 0 01:NIN\_TO 54685.44 86.255 No\_date 37:08 22.99 n/a .000  
 07143+ [L/S/nr: 608/ .247/.036]  
 07144+ [ROUTE\_ID: 294... / .109/.036]  
 07145+ # Catchment Greenbank  
 07146+ # - Todd Drain (south of the Jock)  
 07147+ # - FJSA 2021-01-18 add Greenbank pond as per JFSA\_P598(04)-15 June 2016  
 07148+ # - FJSA 2021-01-18 update area from 37.479 ha to 37.479 ha due to new measurements  
 07149+ # - Todd Drain (south of the Jock)  
 07150+ R0010:CO0274-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07151+ CONTIOUS STANDHY 1. 0 01:GREENB\_001 36.60 .462 No\_date 28:02 49.38 .763 .000  
 07152+ [ROUTE\_ID: 294... / .109/.036]  
 07153+ [LOSS: 2 CN: 77.0] .  
 07154+ [Previous area: Iaper: 4.67 SLPP=1.00 LDP= 40. NMNP= 250 SCP= .01]  
 07155+ [Impervious area: IAlmp: 1.57 SLIP=1.00 LGI= 494. NMNI= .013:SCI= .01]  
 07156+ R0010:CO0275-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07157+ ROUTE RESERVOIR > 1. 0 02:Greenbank 36.60 4.662 No\_date 28:02 49.38 n/a .000  
 07158+ [ROUTE\_ID: 294... / .109/.036]  
 07159+ overlap < 1. 0 03:GREENB\_MZ .000 No\_date 0:00 .000 n/a .000  
 07160+ [MStCoLdss=.8399e-00 m3 , m3 , TotDrvVol=.0000e+00 m3 , N-Ovr= .0 , TotDrvFr=.0 , hrs= .0]  
 07161+ R0010:CO0276-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07162+ ADD HYD  
 07163+ + 1. 0 02:GreenB\_MZ .000 No\_date 0:00 .000 n/a .000  
 07164+ + 1. 0 01:SNK-XB 36.60 .161 No\_date 28:02 49.38 n/a .000  
 07165+ + 1. 0 01:GREENB\_MZ .000 No\_date 0:00 .000 n/a .000  
 07166+ SUM+ 1. 0 01:GREENB\_MZ .000 No\_date 35:58 23.01 n/a .000  
 07167+ R0010:CO0277-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07168+ SAVE HYD  
 07169+ name : Greenb\_0010  
 07170+ remark:Total Flows at Greenbank Drain  
 07171+ R0010:CO0278-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07172+ # Catchment Todd  
 07173+ # - Todd Drain (south of the Jock)  
 07174+ # - FJSA 2021-01-18 add Greenbank South M5S  
 07175+ # - 2020-11-30 increase imp. based on P598(04)-11  
 07176+ # - 2020-11-30 update TODD Tributary Drainage Area to = 146.016 ha based on P598(04)-11  
 07177+ # - 2020-11-30 add Todd Pond as per JFSA\_P598(04)-11  
 07178+ # - 2020-11-30 add Todd Pond and All  
 07179+ R0010:CO0279-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07180+ # Todd Pond  
 07181+ # FJSA 2021-01-18 add "TODD\_MN" as part of Clarke("M\_CLA\_R\_M") and remove it from Todd Pond  
 07182+ # - Todd Pond and All  
 07183+ R0010:CO0279-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07184+ CONTIOUS STANDHY 1. 0 01:TODD\_MN 2.19 .482 No\_date 28:00 44.93 .694 .000  
 07185+ [ROUTE\_ID: 294... / .109/.036]  
 07186+ [LOSS: 2 CN: 77.0] .  
 07187+ [Previous area: Iaper: 4.67 SLPP=1.00 LDP= 40. NMNP= 250 SCP= .01]  
 07188+ [Impervious area: IAlmp: 1.57 SLIP=1.00 LGI= 118. NMNI= .013:SCI= .01]  
 07189+ [ROUTE\_ID: 294... / .109/.036]  
 07190+ R0010:CO0279-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07191+ CONTIOUS STANDHY 1. 0 01:TODD\_MN 12 .06 .491 No\_date 28:00 44.93 .694 .000  
 07192+ [XND: 53:TIMEP=.57]  
 07193+ [ROUTE\_ID: 294... / .109/.036]  
 07194+ [LOSS: 2 CN: 77.0] .  
 07195+ [Previous area: Iaper: 4.67 SLPP=1.00 LDP= 40. NMNP= 250 SCP= .01]  
 07196+ [Impervious area: IAlmp: 1.57 SLIP=1.00 LGI= 409. NMNI= .013:SCI= .01]  
 07197+ R0010:CO0280-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07198+ R0010:CO0280-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07199+ R0010:CO0280-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07200+ R0010:CO0280-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07201+ CONTIOUS STANDHY 1. 0 01:TODD\_MN 12 .06 .491 No\_date 28:00 44.93 .694 .000  
 07202+ [ROUTE\_ID: 294... / .109/.036]  
 07203+ [LOSS: 2 CN: 77.0] .  
 07204+ [Previous area: Iaper: 4.67 SLPP=1.00 LDP= 40. NMNP= 250 SCP= .01]  
 07205+ [Impervious area: IAlmp: 1.57 SLIP=1.00 LGI= 449. NMNI= .013:SCI= .01]  
 07206+ R0010:CO0281-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07207+ CONTIOUS STANDHY 1. 0 01:TODD\_MN 112.91 10.943 No\_date 28:05 44.71 .691 .000  
 07208+ [ROUTE\_ID: 294... / .109/.036]  
 07209+ [LOSS: 2 CN: 77.0] .  
 07210+ [Previous area: Iaper: 4.67 SLPP=1.00 LDP= 40. NMNP= 250 SCP= .01]  
 07211+ [Impervious area: IAlmp: 1.57 SLIP=1.00 LGI= 868. NMNI= .013:SCI= .01]  
 07212+ [ROUTE\_ID: 294... / .109/.036]  
 07213+ [Loss: 2 CN: 77.0] .  
 07214+ [ROUTE\_ID: 294... / .109/.036]  
 07215+ [Loss: 2 CN: 77.0] .  
 07216+ [XND: 63:TIMEP=.63]  
 07217+ [ROUTE\_ID: 294... / .109/.036]  
 07218+ [Previous area: Iaper: 4.67 SLPP=1.00 LDP= 40. NMNP= 250 SCP= .01]  
 07219+ [Impervious area: IAlmp: 1.57 SLIP=1.00 LGI= 143. NMNI= .013:SCI= .01]  
 07220+ R0010:CO0285-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07221+ # 5-Year + 12 Capture  
 07222+ R0010:CO0286-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07223+ ROUTE RESERVOIR > 1. 0 02:TODD\_MN 30.23 3.512 R0010:CO0286-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07224+ out < 1. 0 01:TODD\_MN 30.14 .314 No\_date 28:05 48.20 n/a .000  
 07225+ overlap < 1. 0 01:TODD\_MN 30.14 .314 No\_date 28:05 48.20 n/a .000  
 07226+ R0010:CO0286-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07227+ # 5-Year + 12 Capture  
 07228+ R0010:CO0286-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07229+ R0010:CO0286-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07230+ ROUTE RESERVOIR > 1. 0 02:TODD\_MN 2.10 .282 No\_date 28:00 44.92 n/a .000  
 07231+ out < 1. 0 01:TODD\_MN 2.10 .282 No\_date 27:58 47.94 n/a .000  
 07232+ overlap < 1. 0 01:TODD\_MN 2.10 .282 No\_date 27:58 47.94 n/a .000  
 07233+ [MStCoLdss=.1267e-03 m3 , m3 , TotDrvVol=.0000e+00 m3 , N-Ovr= .0 , TotDrvFr=.0 , hrs= .0]  
 07234+ R0010:CO0286-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07235+ CONTIOUS STANDHY 1. 0 01:TODD\_MN 2.10 .282 No\_date 28:00 44.92 n/a .000  
 07236+ [ROUTE\_ID: 294... / .109/.036]  
 07237+ [Loss: 2 CN: 77.0] .  
 07238+ [ROUTE\_ID: 294... / .109/.036]  
 07239+ R0010:CO0286-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07240+ overlap < 1. 0 01:TODD\_MN 2.10 .282 No\_date 28:00 44.92 n/a .000  
 07241+ [ROUTE\_ID: 294... / .109/.036]  
 07242+ [Loss: 2 CN: 75.0] .  
 07243+ [ROUTE\_ID: 294... / .109/.036]  
 07244+ [Loss: 2 CN: 75.0] .  
 07245+ [ROUTE\_ID: 294... / .109/.036]  
 07246+ [Loss: 2 CN: 75.0] .  
 07247+ R0010:CO0287-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07248+ COMPUTE DUALHY  
 07249+ 1. 0 01:AZ 25.0 .298 No\_date 28:03 40.97 n/a .000  
 07250+ 1. 0 01:AZ 25.0 .298 No\_date 28:03 40.97 n/a .000  
 07251+ 1. 0 01:AZ 25.0 .298 No\_date 28:03 40.97 n/a .000  
 07252+ 1. 0 01:AZ 25.0 .298 No\_date 28:03 40.97 n/a .000  
 07253+ 1. 0 01:AZ 25.0 .298 No\_date 28:03 40.97 n/a .000  
 07254+ ADD HYD  
 07255+ + 1. 0 02:TODD\_MN 12 .12 .016 No\_date 28:00 44.90 n/a .000  
 07256+ + 1. 0 02:TODD\_MN 12 .12 .016 No\_date 28:00 44.90 n/a .000  
 07257+ + 1. 0 02:TODD\_MN 12 .12 .016 No\_date 28:00 44.90 n/a .000  
 07258+ + 1. 0 02:TODD\_MN 12 .12 .016 No\_date 28:00 44.90 n/a .000  
 07259+ SUM+ 1. 0 01:TODD\_MN 120.0 .169 No\_date 28:03 44.79 n/a .000  
 07260+ R0010:CO0288-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07261+ ADD HYD  
 07262+ name : TODD\_0010  
 07263+ remark:Total Flows at Todd Drain  
 07264+ # Todd Pond 3  
 07265+ # - Rating curve obtained from Greenbank South M5S modeling  
 07266+ # - Catchment Todd Pond 3 area to Todd Pond 3 = 183 ha  
 07267+ R0010:CO0290-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07268+ ROUTE RESERVOIR > 1. 0 01:TODD\_MN 1.01:AZ 25.0 .000 No\_date 28:03 44.77 n/a .000  
 07269+ out < 1. 0 01:TODD\_MN 1.01:AZ 25.0 .000 No\_date 28:03 44.77 n/a .000  
 07270+ overlap < 1. 0 01:TODD\_MN 1.01:AZ 25.0 .000 No\_date 28:03 44.77 n/a .000  
 07271+ [ROUTE\_ID: 294... / .109/.036]  
 07272+ [Loss: 2 CN: 75.0] .  
 07273+ [ROUTE\_ID: 294... / .109/.036]  
 07274+ R0010:CO0291-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07275+ ADD HYD  
 07276+ + 1. 0 02:GREENB 120.0 .161 No\_date 28:20 44.77 n/a .000  
 07277+ + 1. 0 02:P2C\_OVF .000 No\_date 28:00 44.77 n/a .000  
 07278+ + 1. 0 02:TODD\_MN2 1.01:AZ 25.0 .000 No\_date 28:00 44.77 n/a .000  
 07279+ + 1. 0 02:TODD\_MN2 1.01:AZ 25.0 .000 No\_date 28:00 44.77 n/a .000  
 07280+ SUM+ 1. 0 01:SNK\_TO 54837.78 85.715 No\_date 35:58 23.06 n/a .000  
 07281+ R0010:CO0292-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07282+ SAVE HYD  
 07283+ name : SN\_TO\_0010  
 07284+ remark:Total Flows at Todd Drain  
 07285+ # Hydrograph from Todd drain routed to Corrigan Drain  
 07286+ # - Rating curve obtained from Corrigan Drain Model - Station 4241  
 07287+ # 2021-02-19 Change the slope from 0.031 % (as per Stateco Report 2007) to 0.05 % so the model will be more stable and g  
 07288+ R0010:CO0293-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07289+ R0010:CO0293-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07290+ [ROUTE\_ID: 294... / .109/.036]  
 07291+ [Loss: 2 CN: 280... / .050/.045]  
 07292+ [ROUTE\_ID: 294... / .109/.036]  
 07293+ [Loss: 2 CN: 280... / .050/.045]  
 07294+ R0010:CO0294-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07295+ ADD HYD  
 07296+ + 1. 0 02:FRASER-DRN 13.65 .447 No\_date 28:22 26.85 n/a .000  
 07297+ + 1. 0 02:FRASER-DRN 21.43 .281 No\_date 27:57 47.46 n/a .000  
 07298+ + 1. 0 02:FCP-01-S 8.03 .756 No\_date 27:57 23.91 n/a .000  
 07299+ + 1. 0 02:FCP-02-S 16.91 .159 No\_date 27:57 58.56 n/a .000  
 07300+ SUM+ 1. 0 01:4241 54685.45 86.106 No\_date 35:57 22.98 n/a .000  
 07301+ R0010:CO0295-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07302+ SAVE HYD  
 07303+ name : 4241\_0010  
 07304+ remark:Total Flows at Ken-Burnett outlet  
 07305+ # Hydrograph from Ken-Burnett to station 3633  
 07306+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07307+ R0010:CO0270-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07308+ ROUTE CHANNEL > 1. 0 02:4241 54685.45 86.106 No\_date 35:57 22.98 n/a .000  
 07309+ out < 1. 0 02:4241 54685.45 86.106 No\_date 35:57 22.98 n/a .000  
 07310+ [ROUTE\_ID: 294... / .109/.036]  
 07311+ # Catchment Greenbank  
 07312+ # - Todd Drain (south of the Jock)  
 07313+ # - FJSA 2021-01-18 add Greenbank pond as per JFSA\_P598(04)-15 June 2016  
 07314+ # - FJSA 2021-01-18 update area from 37.479 ha to 37.479 ha due to new measurements  
 07315+ # - Todd Drain (south of the Jock)  
 07316+ R0010:CO0272-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07317+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07318+ # 2021-02-26 change the channel length (at station 3633) from 650m to 608m and change the slope from 0.0498t to 0.2  
 07319+ R0010:CO0273-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07320+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07321+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07322+ R0010:CO0274-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07323+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07324+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07325+ R0010:CO0275-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07326+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07327+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07328+ R0010:CO0276-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07329+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07330+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07331+ R0010:CO0277-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07332+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07333+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07334+ R0010:CO0278-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07335+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07336+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07337+ R0010:CO0279-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07338+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07339+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07340+ R0010:CO0280-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07341+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07342+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07343+ R0010:CO0281-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07344+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07345+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07346+ R0010:CO0282-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07347+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07348+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07349+ R0010:CO0283-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07350+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07351+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07352+ R0010:CO0284-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07353+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07354+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07355+ R0010:CO0285-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07356+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07357+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07358+ R0010:CO0286-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07359+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07360+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07361+ R0010:CO0287-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07362+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07363+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07364+ R0010:CO0288-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07365+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07366+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07367+ R0010:CO0289-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07368+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07369+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07370+ R0010:CO0290-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07371+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07372+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07373+ R0010:CO0291-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07374+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07375+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07376+ R0010:CO0292-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07377+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07378+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07379+ R0010:CO0293-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07380+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07381+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07382+ R0010:CO0294-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07383+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07384+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07385+ R0010:CO0295-----DTMN-ID:NYHD---ARAHa-QPEAKms-TpeakDate\_hh:mm---RVMn-R.C. ---DWFcms  
 07386+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633  
 07387+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 4241  
 07388+ R00



78785+ # - Rating curve obtained from CCL hydraulic modeling

78786+ R0101:00389-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78787+ ROUTE RESERVOIR -> 1.0 02:MILLS\_P 175.99 12.212 No\_date 28:07 36.76 n/a .000

78788+ out 1.0 02:MILLS\_P 175.99 4.122 No\_date 28:03 36.76 n/a .000

78789+ overlap <= 0.01 SNM 1.0 01:SNM 1.0 01:SNM .00 .000

78790+ [MgSt:CoSed..:2298\_E-01 m<sup>3</sup>] TctovfVol..0000E+00 m<sup>3</sup> N-Ovf..0. TotDurOff..0. hrs]

78791+ R0101:00390-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78792+ ADD HYD 1.0 02:N\_MU .55018 .85 85.374 No\_date 37:18 23.16 n/a .000

78793+ ADD HYD 1.0 02:MIL-OV .00 .000 No\_date 0:00 .00 n/a .000

78794+ ADD HYD 1.0 02:MIL-OP 175.99 4.122 No\_date 28:03 36.76 n/a .000

78795+ SUM 1.0 01:SNM 55194.85 85.786 No\_date 37:17 23.16 n/a .000

78796+ R0101:00391-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78797+ SAVE HYD 1.0 01:SNM\_M 55194.85 85.786 No\_date 37:17 23.16 n/a .000

78798+ name :SNM\_0010

78799+ remark:Total Flows at Jockvale Road

78800+ #

78801+ # Hydrograph from Jockvale Road routed to Heart's Desire

78802+ # Channel X-Section obtained from RvVA Hydraulic Model - Station 689

78803+ R0101:00392-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78804+ [L/s/nr 1962 .. /223. /048] [Vmax= 1.390 Dmax= 2.066]

78805+ #

78806+ # Catchment DESIRE

78807+ # - To Jock River (north of the Dock)

78808+ # - To Jock River (Heart's Desire Community)

78809+ R0101:00393-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78810+ [XIM=.. 25:TIME=.. 28]

78811+ #

78812+ # Catchment JOCKVA

78813+ # - To Jock River (Facility)

78814+ # Residential development & golf course

78815+ # JFSA 201-01-11 update JOCKVA after updating CORRG as per IBI GROUP, July 2008.

78816+ [COS= 1.0 01:DESEIR 1.0 01:DESEIR 1.0 01:DESEIR 1.0 01:DESEIR]

78817+ R0101:00394-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78818+ [XIM=.. 25:TIME=.. 50]

78819+ #

78820+ [L/s/nr 1962 .. /223. /048] [Vmax= 1.390 Dmax= 2.066]

78821+ #

78822+ # Catchment STANDYD

78823+ # - To Jock River (74.40)

78824+ #

78825+ [Imperial= areas 1Aimp= 1.571 SLDI=1.00:LGI= 400:MMI= 0.013:SCI= .0]

78826+ [Imperial= areas 1Bimp= 1.571 SLDI=1.00:LGI= 1311:MMI= 0.013:SCI= .0]

78827+ [Imperial= areas 1Cimp= 1.571 SLDI=1.00:LGI= 1311:MMI= 0.013:SCI= .0]

78828+ R0101:00395-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78829+ ADD HYD 1.0 02:N\_MU .52318 .275 No\_date 27:55 40.79 n/a .000

78830+ ADD HYD 1.0 02:N\_MU .52313 17.470 No\_date 28:08 41.86 n/a .000

78831+ ADD HYD 1.0 02:B2-MU .00 .000 No\_date 0:00 .00 n/a .000

78832+ ADD HYD 1.0 02:B2-OP 175.99 4.122 No\_date 28:03 36.76 n/a .000

78833+ SUM 1.0 01:SNM\_TO 257.63 19.643 No\_date 28:08 41.88 n/a .000

78834+ R0101:00396-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78835+ SAVE HYD 1.0 01:SNM\_TO 257.63 19.945 No\_date 28:08 41.88 n/a .000

78836+ name :JOCKVA\_TO\_R01010

78837+ remark:Total Flows at KB first pond

78838+ #

78839+ # Jockvale SWM Facility

78840+ # - Rating curve obtained from Ottawa Sewerage Study (CCL 1986)

78841+ R0101:00397-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78842+ [L/s/nr 1962 .. /223. /048] [Vmax= 1.390 Dmax= 2.066]

78843+ #

78844+ [Imperial= areas 1Aimp= 1.571 SLDI=1.00:LGI= 400:MMI= 0.013:SCI= .0]

78845+ [Imperial= areas 1Bimp= 1.571 SLDI=1.00:LGI= 1311:MMI= 0.013:SCI= .0]

78846+ [Imperial= areas 1Cimp= 1.571 SLDI=1.00:LGI= 1311:MMI= 0.013:SCI= .0]

78847+ R0101:00398-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78848+ ADD HYD 1.0 02:N\_MU .55194 .85 85.515 No\_date 37:21 23.16 n/a .000

78849+ ADD HYD 1.0 02:DSEIR 23.75 1.694 No\_date 28:03 32.93 .000

78850+ ADD HYD 1.0 02:DSEIR 23.75 1.694 No\_date 28:03 32.93 .000

78851+ ADD HYD 1.0 02:JOCK\_P 257.63 19.643 No\_date 28:08 41.88 n/a .000

78852+ ADD HYD 1.0 02:JOCK\_P 257.63 19.945 No\_date 28:08 41.88 n/a .000

78853+ SUM 1.0 01:SNM\_DE 55476.26 86.165 No\_date 37:21 23.26 n/a .000

78854+ R0101:00399-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78855+ SAVE HYD 1.0 01:SNM\_DE 55476.26 86.165 No\_date 37:21 23.26 n/a .000

78856+ name :SNM\_0010

78857+ remark:Total Flows at Heart's Desire

78858+ #

78859+ # Hydrograph from Heart's Desire routed to Rideau River

78860+ # Channel X-Section obtained from RvVA Hydraulic Model - Station 0

78861+ R0101:00400-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78862+ ROUTE CHANNEL -> 1.0 02:SNM\_DE 55476.26 86.165 No\_date 37:21 23.26 n/a .000

78863+ [Imperial= areas 1Aimp= 1.001 SNM .. /0.001]

78864+ [Imperial= areas 1Bimp= 1.001 SNM .. /0.001]

78865+ [Imperial= areas 1Cimp= 1.001 SNM .. /0.001]

78866+ R0101:00403-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78867+ SAVE HYD 1.0 01:SNM .. /0.001

78868+ name :SNM\_0010

78869+ remark:Total Flows at Rideau River

78870+ #

78871+ # END OF RUN : 24

78872+ #

78873+ R0101:COMMAND#

78874+ R0252:00001-----

78875+ START [TZERO = 2.00 hrs on 01]

78876+ [TZERO = 2.00 hrs on 01-(imperial, 2metric output)]

78877+ [INSTRUM = 1]

78878+ [NRUNS = 0022 ]

78879+ R0101:00401-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78880+ [COS= 1.0 01:S-2 102.94 2.957 No\_date 28:20 23.57 .364 .000

78881+ [INTERVENTIME= 12:00]

78882+ R0101:00402-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78883+ ADD HYD 1.0 02:N\_MU .55476.26 86.183 No\_date 37:18 23.26 n/a .000

78884+ ADD HYD 1.0 02:N\_MU .55476.26 86.183 No\_date 37:18 23.26 n/a .000

78885+ SUM 1.0 01:SNM .. /0.001

78886+ R0101:00403-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78887+ SAVE HYD 1.0 01:SNM .. /0.001

78888+ name :SNM\_0010

78889+ remark:Total Flows at Rideau River

78890+ ##### END OF RUN : 24

78891+ #

78892+ #

78893+ R0101:00404-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78894+ [COS= 1.0 01:S-2 102.94 2.957 No\_date 28:20 23.57 .364 .000

78895+ [INTERVENTIME= 12:00]

78896+ R0101:00405-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78897+ ADD HYD 1.0 02:N\_MU .55476.26 86.183 No\_date 37:18 23.26 n/a .000

78898+ ADD HYD 1.0 02:N\_MU .55476.26 86.183 No\_date 37:18 23.26 n/a .000

78899+ SUM 1.0 01:SNM .. /0.001

78900+ R0101:00406-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78901+ FILENAME = T:\PROJ\1474-16\Design2010\01-QuantityControl\analysis\SMWMMY\SMW-Model\updated3\Cityate.DEF

78902+ ICASDEV = 1 (read and print data)

78903+ R0101:00407-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78904+ Rainfall data from RvVA rainfall gauge installed at site + other gauges by the City

78905+ Rainfall data from RvVA rainfall gauge installed at site + other gauges by the City

78906+ R0101:00408-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78907+ R0101:00409-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78908+ R0101:00410-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78909+ R0101:00411-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78910+ R0101:00412-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78911+ R0101:00413-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78912+ R0101:00414-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78913+ R0101:00415-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78914+ R0101:00416-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78915+ R0101:00417-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78916+ R0101:00418-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78917+ R0101:00419-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78918+ R0101:00420-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78919+ R0101:00421-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78920+ R0101:00422-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78921+ R0101:00423-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78922+ R0101:00424-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78923+ R0101:00425-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78924+ R0101:00426-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78925+ R0101:00427-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78926+ R0101:00428-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78927+ R0101:00429-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78928+ R0101:00430-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78929+ R0101:00431-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78930+ R0101:00432-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78931+ R0101:00433-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78932+ R0101:00434-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78933+ R0101:00435-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78934+ R0101:00436-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78935+ R0101:00437-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78936+ R0101:00438-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78937+ R0101:00439-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78938+ R0101:00440-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78939+ R0101:00441-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78940+ R0101:00442-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78941+ R0101:00443-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78942+ R0101:00444-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78943+ R0101:00445-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78944+ R0101:00446-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78945+ R0101:00447-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78946+ R0101:00448-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78947+ R0101:00449-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78948+ R0101:00450-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78949+ R0101:00451-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78950+ R0101:00452-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78951+ R0101:00453-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78952+ R0101:00454-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78953+ R0101:00455-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78954+ R0101:00456-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78955+ R0101:00457-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78956+ R0101:00458-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78957+ R0101:00459-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78958+ R0101:00460-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78959+ R0101:00461-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78960+ R0101:00462-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78961+ R0101:00463-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78962+ R0101:00464-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78963+ R0101:00465-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78964+ R0101:00466-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78965+ R0101:00467-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78966+ R0101:00468-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78967+ R0101:00469-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78968+ R0101:00470-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78969+ R0101:00471-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78970+ R0101:00472-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78971+ R0101:00473-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78972+ R0101:00474-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78973+ R0101:00475-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78974+ R0101:00476-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78975+ R0101:00477-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78976+ R0101:00478-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78977+ R0101:00479-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78978+ R0101:00480-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78979+ R0101:00481-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78980+ R0101:00482-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78981+ R0101:00483-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78982+ R0101:00484-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78983+ R0101:00485-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78984+ R0101:00486-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78985+ R0101:00487-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78986+ R0101:00488-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78987+ R0101:00489-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78988+ R0101:00490-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78989+ R0101:00491-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78990+ R0101:00492-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78991+ R0101:00493-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78992+ R0101:00494-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78993+ R0101:00495-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78994+ R0101:00496-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78995+ R0101:00497-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78996+ R0101:00498-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78997+ R0101:00499-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78998+ R0101:00500-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

78999+ R0252:00002-----

79000+ R0252:00003-----

79001+ FILENAME = T:\PROJ\1474-16\Design2010\01-QuantityControl\analysis\SMWMMY\SMW-Model\updated3\Cityate.DEF

79002+ ICASDEV = 1 (read and print data)

79003+ R0252:00004-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

79004+ Rainfall data from RvVA rainfall gauge installed at site + other gauges by the City

79005+ Rainfall data from RvVA rainfall gauge installed at site + other gauges by the City

79006+ R0252:00005-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

79007+ R0252:00006-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

79008+ R0252:00007-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

79009+ R0252:00008-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

79010+ R0252:00009-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

79011+ R0252:00010-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

79012+ R0252:00011-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

79013+ THE FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDYD COM

79014+ Horizontal infiltration evaporation parameters:

79015+ [Lg= 76.20 mm] [P= 0.55 mm] [T= 0.44 / hr] [F= .00 mm]

79016+ Parameters for PREVIOUS surfaces in STANDYD:

79017+ [Taper= 4.67 mm] [LG=50.00 m] [NWD= .250]

79018+ Average monthly Potential Evapotranspiration in (mm)

79019+ Parameters used in STANDYD:

79020+ [Lg= 1.57 mm] [CLL= 1.50] [NWD= .000]

79021+ Parameters used in NASHYD:

79022+ Average monthly Pan Evaporation data in (mm)

79023+ JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC

79024+ .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00

79025+ Average monthly Potential Evapotranspiration in (mm)

79026+ JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC

79027+ .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00

79028+ R0252:00005-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

79029+ [COS= 64.01 N 3.00: Tp= 7.13]

79030+ CONTINEXUS NASHYD 1.0 01:CR\_NH .. 3660.00 15.500 No\_date 36:57 25.80 .347 .000

79031+ [ImEBC 4.00: SMIN= 83.24: SMAX=54.96: SK= .010]

79032+ [INTERVENTIME= 12:00]

79033+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

79034+ # of 1.32

79035+ R0252:00006-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

79036+ [COS= 64.01 N 3.00: Tp= 7.13]

79037+ CONTINEXUS NASHYD 1.0 01:CR\_NH .. 3660.00 15.500 No\_date 36:57 25.80 .347 .000

79038+ [ImEBC 4.00: SMIN= 83.24: SMAX=54.96: SK= .010]

79039+ [INTERVENTIME= 12:00]

79040+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

79041+ # of 1.32

79042+ R0252:00007-----DRAIN-ID:NHYD---ARArha-QPEAKms-Tpeakdate\_bh:mm---Rvnm-R.C.--DWFcms

79043+ [COS= 64.01 N 3.00: Tp= 7.13]

79044+ CONTINEXUS NASHYD 1.0 01:CR\_NH .. 3660.00 15.500 No\_date 36:57 25.80 .347 .000

79045+ [ImEBC 4.00: SMIN= 83.24: SMAX=54.96: SK= .010]

79046+ [INTERVENTIME= 12:00]

79047+ # The Tp was modified according to a Peak Reduction factor (MTO-Chart B

08229+ [MStUsed-.119E+03 m3]

08230+ # Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08231+ SAVE HYD 1.0 01RES\_NM 7725.00 3.678 No\_date 60:27 23.52 n/a .000

08232+ frame H\_ResRM remark:outflow Goodwill Marsh, you flow from Node 13a to Node 12

08233+ # Output of Subwatershed 4 - see cross-section 288

08234+ # User n=0.04 for snowmelt correction and n=0.25 for spring conditions

08235+ ROG25:CO0035-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08236+ ROUTE CHANNEL > 1.0 02RES\_ON 7725.00 3.678 No\_date 60:27 23.52 n/a .000

08237+ [ROT: 1.001 out-] 1.0 01NS\_M12 7725.00 3.479 No\_date 60:09 23.52 n/a .000

08238+ [L/S/nr .5926 / .076 /.040] [Vmax=.552\*Imax(.524)]

08239+ #

08240+ # Addition of Subwatershed Rock River at Ashton to Node 12

08241+ ROG25:CO0036-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08242+ ADD HYD 1.0 02RES\_ON 7725.00 3.678 No\_date 60:27 23.52 n/a .000

08243+ frame H\_ResRM remark:outflow Goodwill Marsh, you flow from Node 13a to Node 12

08244+ # Output of Subwatershed 4 and Leamy Creek to Node 12

08245+ ROG25:CO0036-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08246+ ADD HYD 1.0 02RES\_ON 7725.00 3.678 No\_date 60:27 23.52 n/a .000

08247+ frame H\_ResRM remark:outflow Goodwill Marsh, you flow from Node 13a to Node 12

08248+ SUM----- 1.0 01S\_M12 9506.00 16.182 No\_date 32:43 25.02 n/a .000

08249+ ROG25:CO0037-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08250+ ROUTE CHANNEL > 1.0 01S\_M12 9506.00 16.182 No\_date 32:43 25.02 n/a .000

08251+ [ROT: 1.001 out-] 1.0 01S\_M12 9506.00 16.182 No\_date 32:43 25.02 n/a .000

08252+ frame H\_ResRM remark:flow to S\_12JN near Ashton

08253+ #

08254+ # Sum of hydrographs from Node 12 routed to Node 11

08255+ # (Approximated cross-section - see cross-section 258)

08256+ # User n=0.04 for summer conditions and n=0.25 for spring conditions

08257+ # Sum of hydrographs from Node 12 routed to Node 11 with Dumoni section 248

08258+ #

08259+ ROG25:CO0038-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08260+ ROUTE CHANNEL > 1.0 02S\_M12 9506.00 16.182 No\_date 32:43 25.02 n/a .000

08261+ [ROT: 1.001 out-] 1.0 02S\_M12 9506.00 16.182 No\_date 32:43 25.02 n/a .000

08262+ [L/S/nr .5926 / .054 /.040] [Vmax=.721\*Imax(2.847)]

08263+ #

08264+ # Addition of Subwatershed 11 and No Name Creek to Node 11

08265+ ROG25:CO0039-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08266+ ADD HYD 1.0 02S\_M12 9506.00 16.1007 No\_date 33:02 25.02 n/a .000

08267+ frame H\_ResRM remark:flow to S\_12JN near Ashton

08268+ #

08269+ ROG25:CO0040-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08270+ ROUTE CHANNEL > 1.0 02S\_M12 11923.00 27.908 No\_date 33:04 25.42 n/a .000

08271+ [ROT: 1.001 out-] 1.0 02S\_M12 11923.00 18.039 No\_date 40:01 25.42 n/a .000

08272+ [L/S/nr .142428 / .157 /.040] [Vmax=.644\*Imax(1.329)]

08273+ #

08274+ # Sum of hydrographs from Node 11 routed to Node 10

08275+ ROG25:CO0041-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08276+ ADD HYD 1.0 02S\_M12 11923.00 18.039 No\_date 40:01 25.42 n/a .000

08277+ frame H\_ResRM remark:flow to S\_12JN near Ashton

08278+ #

08279+ ROG25:CO0040-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08280+ ROUTE CHANNEL > 1.0 02S\_M12 11923.00 27.908 No\_date 33:04 25.42 n/a .000

08281+ [ROT: 1.001 out-] 1.0 02S\_M12 11923.00 18.039 No\_date 40:01 25.42 n/a .000

08282+ [Vmax=.644\*Imax(1.329)]

08283+ #

08284+ # Addition of Subwatershed 10 to Node 10

08285+ ROG25:CO0041-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08286+ ADD HYD 1.0 02S\_M12 11923.00 18.039 No\_date 40:01 25.42 n/a .000

08287+ frame H\_ResRM remark:flow to S\_12JN near Ashton

08288+ #

08289+ ROG25:CO0042-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08290+ ROUTE CHANNEL > 1.0 02S\_M12 11923.00 27.908 No\_date 33:04 25.42 n/a .000

08291+ [ROT: 1.001 out-] 1.0 02S\_M12 11923.00 18.039 No\_date 40:01 25.42 n/a .000

08292+ [Vmax=.644\*Imax(1.329)]

08293+ #

08294+ # Addition of Kings Creek to S\_10JN

08295+ ROG25:CO0043-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08296+ ADD HYD 1.0 02S\_M12 11758.00 45.026 No\_date 38:35 27.38 n/a .000

08297+ frame H\_ResRM remark:flow to S\_10JN

08298+ #

08299+ ROG25:CO0043-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08300+ ADD HYD 1.0 02S\_M12 11758.00 45.026 No\_date 38:35 27.38 n/a .000

08301+ frame H\_ResRM remark:flow to S\_10JN

08302+ # Sum of hydrographs from Node 10 routed to Node 9

08303+ ROG25:CO0044-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08304+ ADD HYD 1.0 02S\_M12 11758.00 45.026 No\_date 38:35 27.38 n/a .000

08305+ frame H\_ResRM remark:flow to S\_10JN

08306+ #

08307+ ROG25:CO0045-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08308+ ADD HYD 1.0 02S\_M12 11758.00 45.026 No\_date 38:35 27.38 n/a .000

08309+ frame H\_ResRM remark:flow to S\_10JN

08310+ #

08311+ # Addition of Subwatershed 9 and Nichols Creek to Node 9

08312+ ROG25:CO0045-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08313+ ADD HYD 1.0 02S\_M12 11758.00 45.026 No\_date 38:35 27.38 n/a .000

08314+ frame H\_ResRM remark:flow to S\_10JN

08315+ #

08316+ ROG25:CO0046-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08317+ ADD HYD 1.0 02S\_M12 11758.00 45.026 No\_date 38:35 27.38 n/a .000

08318+ frame H\_ResRM remark:flow to S\_10JN

08319+ #

08320+ ROG25:CO0046-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08321+ ADD HYD 1.0 02S\_M12 11758.00 45.026 No\_date 38:35 27.38 n/a .000

08322+ frame H\_ResRM remark:flow to S\_10JN

08323+ #

08324+ # Addition of Subwatershed 8 and Hobbs's Drain to Node 8

08325+ ROG25:CO0047-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08326+ ADD HYD 1.0 02S\_M12 31565.00 79.245 No\_date 39:59 26.99 n/a .000

08327+ frame H\_ResRM remark:flow to S\_10JN

08328+ #

08329+ ROG25:CO0048-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08330+ ROUTE CHANNEL > 1.0 02S\_M12 31565.00 84.584 No\_date 39:59 26.99 n/a .000

08331+ [ROT: 1.001 out-] 1.0 01NS 31561.00 79.245 No\_date 39:59 26.99 n/a .000

08332+ [L/S/nr .2269 / .088 /.045] [Vmax=.511\*Imax(1.743)]

08333+ #

08334+ # Addition of Subwatershed 8 and Hobbs's Drain to Node 8

08335+ ROG25:CO0049-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08336+ ADD HYD 1.0 02S\_M12 31565.00 84.584 No\_date 39:59 26.99 n/a .000

08337+ frame H\_ResRM remark:flow to S\_10JN

08338+ #

08339+ ROG25:CO0049-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08340+ ROUTE CHANNEL > 1.0 02S\_M12 35546.00 84.597 No\_date 39:59 26.99 n/a .000

08341+ [ROT: 1.001 out-] 1.0 01NS 35546.00 80.337 No\_date 45:08 26.99 n/a .000

08342+ [L/S/nr .3750 / .053 /.070] [Vmax=.226\*Imax(2.161)]

08343+ #

08344+ # Addition of Subwatershed 7 to Node 7

08345+ ROG25:CO0049-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08346+ ADD HYD 1.0 02HNT 35546.00 80.337 No\_date 45:08 26.98 n/a .000

08347+ frame H\_ResRM remark:flow to S\_7JN

08348+ #

08349+ ROG25:CO0049-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08350+ ADD HYD 1.0 02HNT 35546.00 80.337 No\_date 45:08 26.95 n/a .000

08351+ frame H\_ResRM remark:flow to S\_7JN

08352+ #

08353+ ROG25:CO0049-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08354+ ADD HYD 1.0 02HNT 35546.00 80.337 No\_date 45:08 26.95 n/a .000

08355+ frame H\_ResRM remark:flow to S\_7JN

08356+ #

08357+ ROG25:CO0051-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08358+ ADD HYD 1.0 02HNT 35546.00 80.337 No\_date 45:08 26.95 n/a .000

08359+ frame H\_ResRM remark:flow to S\_7JN

08360+ #

08361+ ROG25:CO0051-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08362+ ADD HYD 1.0 02HNT 35546.00 80.337 No\_date 45:08 26.95 n/a .000

08363+ frame H\_ResRM remark:flow to S\_7JN

08364+ #

08365+ ROG25:CO0051-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08366+ ADD HYD 1.0 02HNT 35546.00 80.337 No\_date 45:08 26.95 n/a .000

08367+ frame H\_ResRM remark:flow to S\_7JN

08368+ #

08369+ ROG25:CO0051-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08370+ ADD HYD 1.0 02HNT 35546.00 80.337 No\_date 45:08 26.95 n/a .000

08371+ frame H\_ResRM remark:flow to S\_7JN

08372+ #

08373+ ROG25:CO0053-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08374+ ROUTE CHANNEL > 1.0 02RES\_NF 38743.00 41.832 No\_date 61:20 26.55 n/a .000

08375+ [ROT: 1.001 out-] 1.0 01NS 38743.00 41.832 No\_date 61:20 26.55 n/a .000

08376+ [L/S/nr .3056 / .082 /.025] [Vmax=.514\*Imax(1.120)]

08377+ #

08378+ # Addition of Subwatershed 6 and Van Gaal Drain to Node 6

08379+ ROG25:CO0054-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08380+ ADD HYD 1.0 02RES\_NF 38743.00 41.832 No\_date 61:20 26.55 n/a .000

08381+ frame H\_ResRM remark:flow to S\_6JN

08382+ #

08383+ ROG25:CO0054-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08384+ ADD HYD 1.0 02RES\_NF 38743.00 41.832 No\_date 61:20 26.55 n/a .000

08385+ frame H\_ResRM remark:flow to S\_6JN

08386+ #

08387+ ROG25:CO0055-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08388+ ADD HYD 1.0 02RES\_NF 38743.00 41.832 No\_date 61:20 26.55 n/a .000

08389+ frame H\_ResRM remark:flow to S\_6JN

08390+ #

08391+ ROG25:CO0056-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08392+ ADD HYD 1.0 02RES\_NF 38743.00 41.832 No\_date 61:20 26.55 n/a .000

08393+ frame H\_ResRM remark:flow to S\_6JN

08394+ #

08395+ ROG25:CO0056-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08396+ ADD HYD 1.0 02RES\_NF 38743.00 41.832 No\_date 61:20 26.55 n/a .000

08397+ frame H\_ResRM remark:flow to S\_6JN

08398+ #

08399+ ROG25:CO0057-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08400+ ADD HYD 1.0 02RES\_NF 38743.00 41.832 No\_date 61:20 26.55 n/a .000

08401+ frame H\_ResRM remark:flow to S\_6JN

08402+ #

08403+ ROG25:CO0058-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08404+ ADD HYD 1.0 02RES\_NF 38743.00 41.832 No\_date 61:20 26.55 n/a .000

08405+ frame H\_ResRM remark:flow to S\_6JN

08406+ #

08407+ ROG25:CO0057-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08408+ ADD HYD 1.0 02RES\_NF 38743.00 41.832 No\_date 61:20 26.55 n/a .000

08409+ frame H\_ResRM remark:flow to S\_6JN

08410+ #

08411+ ROG25:CO0058-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms

08412+ ADD HYD 1.0 02RES\_NF 38743.00 41.832 No\_date 61:20 26.55 n/a .000

08413+ frame H\_ResRM remark:flow to S\_6JN

08414+ #

08415+ ROG25:CO0058-----Dmtn-ID:NHYD-----ARAHa-QPEAKcms-TpeakDate\_bb:mn---RvNm-R.C.---DWFcms





This block contains the configuration file for the RMAN backup and recovery process, detailing storage details, backup types, and various parameters.

09725+ [SMIN= 26.32 : SMAX=175.50: SK= .010] ...  
 09726+ R025:CO0264- Dtnin-ID:NHYD- ...  
 COMPUTE DUALND / 1.0 01:FRASER-D 21.61 1,258 No\_date 28:01 56.23 n/a .000  
 09728+ Major System / 1.0 02:FRASER-J .00 .000 No\_date 0:00 n/a .000  
 09729+ Minor System / 1.0 02:FRASER-J 21.61 2,281 No\_date 27:55 56.43 n/a .000  
 09730+ [MSysUsed=.47283+003- TotoFrVol=.0000- N-Ofr= 0. TotSurfrv=.0.]  
 09731+ R025:CO0265- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:FRASER-N ...  
 09732+ SUMM+ 1.0 01:FRASER-S 21.61 2,281 No\_date 27:55 56.43 n/a .000  
 09733+ ADD HYD 1.0 02:KBP-Pond- 257.04 17,344 No\_date 28:10 42.00 n/a .000  
 09734+ \* 1.0 02:FRASER-N 55.36 2,311 No\_date 28:23 34.14 n/a .000  
 09735+ \* 1.0 02:FRASER-N 55.36 2,311 No\_date 28:23 34.14 n/a .000  
 09736+ ADD HYD 1.0 02:KBP-Pond- 257.04 17,344 No\_date 28:10 42.00 n/a .000  
 09737+ \* 1.0 02:FRASER-N 55.36 2,311 No\_date 28:23 34.14 n/a .000  
 09738+ \* 1.0 02:FRASER-N 55.36 2,311 No\_date 28:23 34.14 n/a .000  
 09739+ \* 1.0 02:FRASER-S 21.61 2,281 No\_date 27:55 56.43 n/a .000  
 09740+ \* 1.0 02:KBP-Pond- 257.04 17,344 No\_date 28:10 42.00 n/a .000  
 09741+ \* 1.0 02:FRASER-N 55.36 2,311 No\_date 28:23 34.14 n/a .000  
 09742+ \* 1.0 02:FCP-02-8 16.09 1,159 No\_date 27:44 69.13 n/a .000  
 09743+ \* 1.0 02:FCP-03-8 .37 .358 No\_date 27:43 69.13 n/a .000  
 09744+ SAVE HYD 54681.18 103,751 No\_date 38:34 29.13 n/a .000  
 09745+ R025:CO0269- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:4241 54681.48 103,701 No\_date 38:36 29.12 n/a .000  
 09746+ SAVE HYD 1.0 01:4241 54681.48 103,701 No\_date 38:36 29.12 n/a .000  
 09747+ remark:H2O\_4241\_0025 ...  
 09748+ # Hydrograph from Ken-Burnett at Station 3633  
 09749+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 4241  
 09750+ # CONTINUOUS STANDBY 1.0 01:corsi1 ...  
 09751+ # Dtnin-ID:NHYD- ...  
 09752+ R025:CO0270- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:4241 54681.48 103,701 No\_date 38:36 29.11 n/a .000  
 09753+ \* [Rdtv= 1.00] out\* 1.0 01:4241-out\* 54681.48 103,716 No\_date 38:34 29.11 n/a .000  
 09754+ \* [L/S= .294-.109\*.036] ...  
 09755+ \* [Vmax= 1.675: Max= 1.657] ...  
 09756+ R025:CO0271- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:4241- 54681.48 103,751 No\_date 38:34 29.13 n/a .000  
 09757+ R025:CO0272- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:4241 54681.18 103,751 No\_date 38:34 29.13 n/a .000  
 09758+ SAVE HYD 54681.18 103,751 No\_date 38:34 29.13 n/a .000  
 09759+ remark:H2O\_54681\_0025 ...  
 09760+ # Hydrograph from Station 4633 - MSS Pond  
 09761+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 3633  
 09762+ # CONTINUOUS STANDBY 1.0 01:corsi1 ...  
 09763+ # Dtnin-ID:NHYD- ...  
 09764+ SAVE HYD 1.0 01:SKN\_0025 ...  
 09765+ # Hydrograph from Station 4633 - MSS Pond  
 09766+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 3633  
 09767+ # CONTINUOUS STANDBY 1.0 01:corsi1 ...  
 09768+ # Dtnin-ID:NHYD- ...  
 09769+ ROUTE CHANNEL -> 1.0 02:KBP-Pond- 54681.18 103,751 No\_date 38:34 29.13 n/a .000  
 09770+ \* [Rdtv= 1.00] out\* 1.0 01:INr\_TO 54681.18 103,755 No\_date 38:38 29.13 n/a .000  
 09771+ \* [L/S= .294-.109\*.036] ...  
 09772+ \* [Vmax= 1.675: Max= 1.657] ...  
 09773+ # Catchment CORIC  
 09774+ # To Greenbank Drain South of the Jock  
 09775+ # CONTINUOUS STANDBY 1.0 01:corsi1 ...  
 09776+ # Dtnin-ID:NHYD- ...  
 09777+ # To Greenbank  
 09778+ # - To Greenbank Drain South of the Jock  
 09779+ # - To Greenbank Drain South of the Jock per JFRA\_P598(04)-15, June 2016  
 09780+ # - JFRA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GIS measurements  
 09781+ \* [L/S= .294-.109\*.036] ...  
 09782+ R025:CO0273- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:4241- 54681.48 103,751 No\_date 38:34 29.13 n/a .000  
 09783+ CONTINUOUS STANDBY 1.0 01:GrenB\_MN 36.60 5,574 No\_date 28:02 59.33 n/a .000  
 09784+ \* [Ximp= .64: TIME=.68] ...  
 09785+ \* [Previous area: Iaper= 4.67:SLPP1=0.0:LGP= 40.:MNP=.250:SCP=.0] ...  
 09786+ \* [Imperialv area: Iaper= 4.57:SLPD1=1.00:LGP= 494.:MMI=.013:SCI=.0] ...  
 09787+ \* [Imperialv area: Iaper= 4.57:SLPD1=1.00:LGP= 494.:MMI=.013:SCI=.0] ...  
 09788+ \* [SMIN= 31.15 : SMAX=207.66: SK= .010] ...  
 09789+ R025:CO0275- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:4241- 54681.48 103,751 No\_date 38:34 29.13 n/a .000  
 09790+ ROUTE RESERVEIN <- 1.0 01:GreenB\_MN 36.60 5,574 No\_date 28:02 59.33 n/a .000  
 09791+ out <- 1.0 01:GreenB\_MN 36.60 5,574 No\_date 28:11 58.33 n/a .000  
 09792+ \* 1.0 01:GreenB\_MN 36.60 5,574 No\_date 28:11 58.33 n/a .000  
 09793+ \* 1.0 01:GreenB\_MN .00 .000 No\_date 0:00 n/a .000  
 09794+ \* [McStUsed=.81984-0000-] ...  
 09795+ R025:CO0276- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:NH2\_TO 54681.18 103,735 No\_date 38:18 29.13 n/a .000  
 09796+ \* 1.0 02:NH2\_TO 54681.18 103,735 No\_date 38:18 29.13 n/a .000  
 09797+ \* 1.0 02:NH2\_TO 54681.18 103,735 No\_date 38:18 29.13 n/a .000  
 09798+ \* 1.0 02:NH2\_TO 54681.18 103,735 No\_date 38:18 29.13 n/a .000  
 09799+ SUMM+ 1.0 01:GreenB\_MN 36.60 3,118 No\_date 28:11 58.33 n/a .000  
 09800+ R025:CO0277- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:4241- 54717.78 103,842 No\_date 38:38 29.15 n/a .000  
 09801+ SAVE HYD 54717.78 103,842 No\_date 38:38 29.15 n/a .000  
 09802+ frame: Grend\_0025 ...  
 09803+ \* [Total Flow= 1.0 at Greenbank Drain] ...  
 09804+ \* [ ] ...  
 09805+ # Catchment TOOD ...  
 09806+ # - Subdivision (south of the Jock)  
 09807+ # - Subdivision with 43% imp. as per Barrhaven South MSS  
 09808+ # 2021-11-30 increase imp. based on P598(04)-11  
 09809+ # 2021-01-19 update area to 146.01 ha based on P598(04)-11  
 09810+ # 2021-01-19 update area to 146.01 ha based on P598(04)-11  
 09811+ \* [Rdtv= 1.00] out\* 1.0 01:TODD\_MN1 ...  
 09812+ \* [SMIN= 31.15 : SMAX=207.66: SK= .010] ...  
 09813+ R025:CO0278- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09814+ \* [McStUsed=.81984-0000-] ...  
 09815+ R025:CO0279- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09816+ \* [McStUsed=.81984-0000-] ...  
 09817+ \* [L/S= .117E-03 : SMIN= 31.15 : SMAX=207.66: SK= .010] ...  
 09818+ R025:CO0282- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09819+ \* [McStUsed=.81984-0000-] ...  
 09820+ R025:CO0283- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09821+ \* [McStUsed=.81984-0000-] ...  
 09822+ CONTINUOUS STANDBY 1.0 01:TODD\_MN1 ...  
 09823+ \* [Ximp= .52: TIME=.57] ...  
 09824+ \* [Previous area: Iaper= 4.67:SLPP1=0.0:LGP= 40.:MNP=.250:SCP=.0] ...  
 09825+ \* [Imperialv area: Iaper= 4.57:SLPD1=1.00:LGP= 118.:MMI=.013:SCI=.0] ...  
 09826+ \* [Imperialv area: Iaper= 4.57:SLPD1=1.00:LGP= 118.:MMI=.013:SCI=.0] ...  
 09827+ \* [SMIN= 31.15 : SMAX=207.66: SK= .010] ...  
 09828+ R025:CO0284- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09829+ \* [McStUsed=.81984-0000-] ...  
 09830+ R025:CO0285- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09831+ \* [McStUsed=.81984-0000-] ...  
 09832+ CONTINUOUS STANDBY 1.0 01:TODD\_MN1 ...  
 09833+ \* [Ximp= .52: TIME=.57] ...  
 09834+ \* [Previous area: Iaper= 4.67:SLPP1=0.0:LGP= 40.:MNP=.250:SCP=.0] ...  
 09835+ \* [Imperialv area: Iaper= 4.57:SLPD1=1.00:LGP= 449.:MMI=.013:SCI=.0] ...  
 09836+ \* [Imperialv area: Iaper= 4.57:SLPD1=1.00:LGP= 449.:MMI=.013:SCI=.0] ...  
 09837+ R025:CO0281- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09838+ \* [McStUsed=.81984-0000-] ...  
 09839+ R025:CO0282- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09840+ \* [McStUsed=.81984-0000-] ...  
 09841+ \* [L/S= .2 : CN= 77.0] ...  
 09842+ \* [Previous area: Iaper= 4.67:SLPP1=0.0:LGP= 40.:MNP=.250:SCP=.0] ...  
 09843+ \* [Imperialv area: Iaper= 4.57:SLPD1=1.00:LGP= 118.:MMI=.013:SCI=.0] ...  
 09844+ R025:CO0283- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09845+ \* [McStUsed=.81984-0000-] ...  
 09846+ R025:CO0284- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09847+ \* [McStUsed=.81984-0000-] ...  
 09848+ R025:CO0285- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09849+ \* [McStUsed=.81984-0000-] ...  
 09850+ R025:CO0286- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09851+ \* [McStUsed=.81984-0000-] ...  
 09852+ # 5 Year - 12% Imp. ...  
 09853+ R025:CO0283- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09854+ \* [McStUsed=.81984-0000-] ...  
 09855+ R025:CO0284- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09856+ \* [McStUsed=.81984-0000-] ...  
 09857+ R025:CO0285- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09858+ \* [McStUsed=.81984-0000-] ...  
 09859+ R025:CO0286- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09860+ \* [McStUsed=.81984-0000-] ...  
 09861+ R025:CO0287- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09862+ \* [McStUsed=.81984-0000-] ...  
 09863+ R025:CO0288- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09864+ \* [McStUsed=.81984-0000-] ...  
 09865+ R025:CO0289- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09866+ \* [McStUsed=.81984-0000-] ...  
 09867+ R025:CO0281- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09868+ \* [McStUsed=.81984-0000-] ...  
 09869+ R025:CO0282- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09870+ \* [McStUsed=.81984-0000-] ...  
 09871+ R025:CO0283- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09872+ \* [McStUsed=.81984-0000-] ...  
 09873+ R025:CO0284- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09874+ \* [McStUsed=.81984-0000-] ...  
 09875+ R025:CO0285- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09876+ \* [McStUsed=.81984-0000-] ...  
 09877+ R025:CO0286- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09878+ \* [McStUsed=.81984-0000-] ...  
 09879+ R025:CO0287- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 01:TODD\_MN1 ...  
 09880+ \* [McStUsed=.81984-0000-] ...  
 09881+ Minor System / 1.0 02:CLAR\_MJ 25.50 1,818 No\_date 27:54 49.64 n/a .000  
 09882+ ROUTE RESERVEIN <- 1.0 02:CLAR\_MJ 25.50 1,818 No\_date 27:54 49.64 n/a .000  
 09883+ out <- 1.0 02:CLAR\_MJ 25.50 1,818 No\_date 27:54 49.64 n/a .000  
 09884+ \* 1.0 02:CLAR\_MJ .00 .000 No\_date 0:00 n/a .000  
 09885+ \* 1.0 02:CLAR\_MJ .00 .000 No\_date 0:00 n/a .000  
 09886+ Minor System / 1.0 02:CLAR\_MJ 25.50 1,818 No\_date 27:54 49.64 n/a .000  
 09887+ \* 1.0 02:CLAR\_MJ .00 .000 No\_date 0:00 n/a .000  
 09888+ \* 1.0 02:CLAR\_MJ .00 .000 No\_date 0:00 n/a .000  
 09889+ \* 1.0 02:CLAR\_MJ .00 .000 No\_date 0:00 n/a .000  
 09890+ Minor System / 1.0 02:TODD 120.62 14,962 No\_date 28:01 53.48 n/a .000  
 09891+ \* 1.0 02:TODD .00 .000 No\_date 0:00 n/a .000  
 09892+ SAVE HYD 1.0 01:TODD 120.62 14,962 No\_date 28:03 53.48 n/a .000  
 09893+ frame: TODD\_0025 ...  
 09894+ \* [Total Flow= 1.0 at Todd Drain] ...  
 09895+ # Todd\_0025 ...  
 09896+ # - Rating Curve obtained from Barrhaven South MSS modeling  
 09897+ # - started 2007, Tributary Drainage Area to MSS Pond 3 + 19.1 ha  
 09898+ # - 2021-01-19 update area to 19.1 ha based on P598(04)-11  
 09899+ R025:CO0291- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09900+ R025:CO0292- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09901+ R025:CO0293- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09902+ R025:CO0294- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09903+ R025:CO0295- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09904+ R025:CO0296- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09905+ R025:CO0297- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09906+ R025:CO0298- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09907+ R025:CO0299- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09908+ R025:CO0300- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09909+ R025:CO0301- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09910+ R025:CO0302- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09911+ R025:CO0303- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09912+ R025:CO0302- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09913+ R025:CO0303- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09914+ R025:CO0304- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09915+ R025:CO0305- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09916+ R025:CO0306- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09917+ R025:CO0307- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09918+ R025:CO0308- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09919+ R025:CO0309- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09920+ R025:CO0310- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09921+ R025:CO0311- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09922+ R025:CO0312- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09923+ R025:CO0313- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09924+ R025:CO0314- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09925+ R025:CO0315- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09926+ R025:CO0316- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09927+ R025:CO0317- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09928+ R025:CO0318- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09929+ R025:CO0319- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09930+ R025:CO0320- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09931+ R025:CO0321- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09932+ R025:CO0322- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09933+ R025:CO0323- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09934+ R025:CO0324- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09935+ R025:CO0325- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09936+ R025:CO0326- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09937+ R025:CO0327- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09938+ R025:CO0328- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09939+ R025:CO0329- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09940+ R025:CO0330- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09941+ R025:CO0331- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09942+ R025:CO0332- Dtnin-ID:NHYD- ...  
 ADD HYD 1.0 02:GreenB 54717.78 103,842 No\_date 38:38 29.13 n/a .000  
 09943+ R025:CO0333- Dtnin-ID:NHYD- ...



10473+ # - To SWM Facility north of the Jock  
10474+ # - Privately residential development  
10475+ # \*\*\*\*\*  
10476+ R025:C00388-----Dtnin:ID=NYHD----ARAAha-QPEAKcms-TpeakDate\_hh:mm:---Rvnm-R.C.---DWFcms  
CONTINUOUS STANDHYD 1.0 01:MILLS 175.99 15.275 No\_date 28:07 44.62 .600 .000  
10477+ # KINP= 38 TIMEP= 38  
10478+ # [Previous areas: Aper= 4.67;SLPP=1.08;LGP= 40;MNP=.250;SCP= .0]  
10479+ # [Impervious areas: Aper= 4.57;SLP1=1.00;LG1=1118;MM1=.013;SC1= .0]  
10480+ # [iAECIcmpe 4.00: iARECper= 4.00]  
10481+ # [iAECIcmpe 36.67:SMAX=244.49;SK= .010]  
10482+ # [iAECIcmpe 36.67:SMAX=244.49;SK= .010]  
10483+ # \*\*\*\*\*  
10484+ # Chapman Mills SWM Pond  
10485+ # - Rainfall curve obtained from CCL hydraulic modeling  
10486+ # \*\*\*\*\*  
10487+ R025:C00389-----Dtnin:ID=NYHD----ARAAha-QPEAKcms-TpeakDate\_hh:mm:---Rvnm-R.C.---DWFcms  
ROUT RESERVOIR 1.0 01:MILL\_P 175.99 15.275 No\_date 28:07 44.62 .600 .000  
10488+ # [out < 1.0 01:MILL\_P 162.60 4.050 No\_date 28:16 44.62 n/a .000  
10489+ # [overflow < 1.0 03:MILL\_OV 13.39 8.160 No\_date 28:16 44.62 n/a .000  
10490+ # [Modulus= 212000,Pol= 5.973,abs= 1.00,exp= 0.00]  
10491+ # \*\*\*\*\*  
10492+ R025:C00390-----Dtnin:ID=NYHD----ARAAha-QPEAKcms-TpeakDate\_hh:mm:---Rvnm-R.C.---DWFcms  
025:CONTINUOUS 1.0 01:SN\_M 55194.86 104.475 No\_date 38:54 29.33 n/a .000  
10493+ # \*\*\*\*\*  
10494+ ADD HYD 1.0 02:N\_M 55194.86 104.271 No\_date 38:54 29.28 n/a .000  
10495+ # \*\*\*\*\*  
10496+ # \*\*\*\*\*  
10497+ # \*\*\*\*\*  
10498+ # \*\*\*\*\*  
10499+ # \*\*\*\*\*  
10500+ # \*\*\*\*\*  
10501+ # \*\*\*\*\*  
10502+ # Hydrograph from Jockvale Road routed to Heart's Desire  
10503+ # Channel X-Section obtained from Rvna Hydraulic Model - Station 689  
10504+ # \*\*\*\*\*  
10505+ R025:C00392-----Dtnin:ID=NYHD----ARAAha-QPEAKcms-TpeakDate\_hh:mm:---Rvnm-R.C.---DWFcms  
025:CONTINUOUS 1.0 01:SN\_M 55194.86 104.475 No\_date 38:54 29.31 n/a .000  
10506+ # [RDT= 1.00] out< 1.0 01:N\_M 55194.86 104.438 No\_date 39:12 29.33 n/a .000  
10507+ # [L/s/n .1962/.223/.045]  
10508+ # \*\*\*\*\*  
10509+ # \*\*\*\*\*  
10510+ # \*\*\*\*\*  
10511+ # \*\*\*\*\*  
10512+ # Catchment DESIRE  
10513+ # - To Jockvale area (north of the Jock)  
10514+ # - Rural-estate in semi-developed (Heart's Desire Community)  
10515+ # \*\*\*\*\*  
10516+ R025:C00393-----Dtnin:ID=NYHD----ARAAha-QPEAKcms-TpeakDate\_hh:mm:---Rvnm-R.C.---DWFcms  
025:CONTINUOUS 1.0 01:DESIRE 23.78 2.161 No\_date 28:03 40.77 .548 .000  
10517+ # KINP= 28 TIMEP= 28  
10518+ # [Previous areas: Aper= 4.67;SLPP=1.00;LGP= 40;.MNP=.250;SCP= .0]  
10519+ # [Impervious areas: Aper= 4.57;SLP1=1.00;LG1=400;MM1=.013;SC1= .0]  
10520+ # [iAECIcmpe 4.00: iARECper= 4.00]  
10521+ # [iAECIcmpe 36.67:SMAX=244.49;SK= .010]  
10522+ # \*\*\*\*\*  
10523+ # \*\*\*\*\*  
10524+ # Catchment JOCKVA  
10525+ # - To Jockvale SWM Facility  
10526+ # - To Jock River (golf course)  
10527+ # - To Jock River (north of the Jock)  
10528+ # \*\*\*\*\*  
10529+ R025:C00394-----Dtnin:ID=NYHD----ARAAha-QPEAKcms-TpeakDate\_hh:mm:---Rvnm-R.C.---DWFcms  
025:CONTINUOUS STANDHYD 1.0 01:JOCKVA 225.13 21.797 No\_date 28:07 50.08 .673 .000  
10530+ # \*\*\*\*\*  
10531+ # \*\*\*\*\*  
10532+ # \*\*\*\*\*  
10533+ # \*\*\*\*\*  
10534+ # \*\*\*\*\*  
10535+ # \*\*\*\*\*  
10536+ # \*\*\*\*\*  
10537+ # \*\*\*\*\*  
10538+ # \*\*\*\*\*  
10539+ R025:C00395-----Dtnin:ID=NYHD----ARAAha-QPEAKcms-TpeakDate\_hh:mm:---Rvnm-R.C.---DWFcms  
025:CONTINUOUS 1.0 01:EX-LAND-MN 32.50 2.275 No\_date 27:52 50.26 n/a .000  
10540+ ADD HYD 1.0 02:EX-LAND-MN 225.13 21.797 No\_date 28:07 50.08 n/a .000  
10541+ # \*\*\*\*\*  
10542+ # \*\*\*\*\*  
10543+ # \*\*\*\*\*  
10544+ # \*\*\*\*\*  
10545+ # \*\*\*\*\*  
10546+ R025:C00396-----Dtnin:ID=NYHD----ARAAha-QPEAKcms-TpeakDate\_hh:mm:---Rvnm-R.C.---DWFcms  
025:CONTINUOUS 1.0 01:JOCKVA-TO 247.63 24.072 No\_date 28:07 50.10 n/a .000  
10547+ # \*\*\*\*\*  
10548+ # \*\*\*\*\*  
10549+ # \*\*\*\*\*  
10550+ # \*\*\*\*\*  
10551+ # \*\*\*\*\*  
10552+ # \*\*\*\*\*  
10553+ R025:C00397-----Dtnin:ID=NYHD----ARAAha-QPEAKcms-TpeakDate\_hh:mm:---Rvnm-R.C.---DWFcms  
025:CONTINUOUS 1.0 01:JOCKVA-TO 120.94 3.971 No\_date 28:20 30.11 .405 .000  
10554+ # \*\*\*\*\*  
10555+ # \*\*\*\*\*  
10556+ # \*\*\*\*\*  
10557+ # \*\*\*\*\*  
10558+ R025:C00398-----Dtnin:ID=NYHD----ARAAha-QPEAKcms-TpeakDate\_hh:mm:---Rvnm-R.C.---DWFcms  
025:CONTINUOUS 1.0 01:N\_M 257.63 9.145 No\_date 28:37 50.10 n/a .000  
10559+ # \*\*\*\*\*  
10560+ # \*\*\*\*\*  
10561+ # \*\*\*\*\*  
10562+ # \*\*\*\*\*  
10563+ # \*\*\*\*\*  
10564+ R025:C00399-----Dtnin:ID=NYHD----ARAAha-QPEAKcms-TpeakDate\_hh:mm:---Rvnm-R.C.---DWFcms  
025:CONTINUOUS 1.0 01:N\_M 257.63 24.072 No\_date 28:07 50.10 n/a .000  
10565+ # \*\*\*\*\*  
10566+ # \*\*\*\*\*  
10567+ # \*\*\*\*\*  
10568+ # \*\*\*\*\*  
10569+ # \*\*\*\*\*  
10570+ # \*\*\*\*\*  
10571+ # \*\*\*\*\*  
10572+ # \*\*\*\*\*  
10573+ # \*\*\*\*\*  
10574+ # \*\*\*\*\*  
10575+ # \*\*\*\*\*  
10576+ # \*\*\*\*\*  
10577+ # \*\*\*\*\*  
10578+ # \*\*\*\*\*  
10579+ # \*\*\*\*\*  
10580+ # \*\*\*\*\*  
10581+ # \*\*\*\*\*  
10582+ R025:C00401-----Dtnin:ID=NYHD----ARAAha-QPEAKcms-TpeakDate\_hh:mm:---Rvnm-R.C.---DWFcms  
025:CONTINUOUS 1.0 01:N\_M 120.94 3.971 No\_date 28:20 30.11 .405 .000  
10583+ # \*\*\*\*\*  
10584+ # \*\*\*\*\*  
10585+ # \*\*\*\*\*  
10586+ # \*\*\*\*\*  
10587+ R025:C00402-----Dtnin:ID=NYHD----ARAAha-QPEAKcms-TpeakDate\_hh:mm:---Rvnm-R.C.---DWFcms  
025:CONTINUOUS 1.0 01:N\_M 120.94 3.971 No\_date 28:20 30.11 .405 .000  
10588+ ADD HYD 1.0 02:N\_M 55194.86 104.438 No\_date 39:12 29.33 n/a .000  
10589+ # \*\*\*\*\*  
10590+ # \*\*\*\*\*  
10591+ # \*\*\*\*\*  
10592+ # \*\*\*\*\*  
10593+ # \*\*\*\*\*  
10594+ R025:C00403-----Dtnin:ID=NYHD----ARAAha-QPEAKcms-TpeakDate\_hh:mm:---Rvnm-R.C.---DWFcms  
025:CONTINUOUS 1.0 01:SN\_M 55194.27 105.274 No\_date 39:15 29.43 n/a .000  
10595+ # \*\*\*\*\*  
10596+ # \*\*\*\*\*  
10597+ # \*\*\*\*\*  
10598+ # \*\*\*\*\*  
10599+ # \*\*\*\*\*  
10600+ # \*\*\*\*\*  
10601+ # \*\*\*\*\*  
10602+ # \*\*\*\*\*  
10603+ # \*\*\*\*\*  
10604+ RINH:COMMANDS  
10605+ R050:COMMANDS-----  
10606+ # \*\*\*\*\*  
10607+ # \*\*\*\*\*  
10608+ # [METCUTS 2 (Imperial, 2-metric output)]  
10609+ # [HDFORM 1]  
10610+ # [INPUT = 0500 ]  
10611+ # \*\*\*\*\*  
10612+ # \*\*\*\*\*  
10613+ # \*\*\*\*\*  
10614+ # Project Name: [Jock River] Project Number: [1474-16]  
10615+ # \*\*\*\*\*  
10616+ # \*\*\*\*\*  
10617+ # Company : JFSAinc.  
10618+ # \*\*\*\*\*  
10619+ # \*\*\*\*\*  
10620+ # CALIBRATION OF SUMMER MODEL PARAMETERS  
10621+ # \*\*\*\*\*  
10622+ # Rainfall data from JFSA rainfall gauge installed at site + other gauges by the City  
10623+ # Data collection from May 1 to July 14, 2003  
10624+ # [L/s/n .853/.967/.045]  
10625+ # \*\*\*\*\*  
10626+ # \*\*\*\*\*  
10627+ # \*\*\*\*\*  
10628+ # \*\*\*\*\*  
10629+ # \*\*\*\*\*  
10630+ R050:COMMANDS-----  
10631+ # \*\*\*\*\*  
10632+ # REA STORM  
10633+ # Filename = storm.001  
10634+ # Contour file for 24 hours 1:160 ans pour Ottawa CDA  
10635+ # [SET=10.00]SOURC 24.00[POTD= 81.51]  
10636+ R050:COMMANDS-----  
10637+ # [PFACT= 1.00:TSHFT= 960.00 min]  
10638+ # [TSHFT= 10.00:SOURC= 40.00:POTD= 81.51]  
10639+ # \*\*\*\*\*  
10640+ # \*\*\*\*\*  
10641+ # \*\*\*\*\*  
10642+ # \*\*\*\*\*  
10643+ # \*\*\*\*\*  
10644+ # \*\*\*\*\*  
10645+ # \*\*\*\*\*  
10646+ # \*\*\*\*\*  
10647+ # \*\*\*\*\*  
10648+ # \*\*\*\*\*  
10649+ # \*\*\*\*\*  
10650+ # \*\*\*\*\*  
10651+ # \*\*\*\*\*  
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10660+ # \*\*\*\*\*  
10661+ # \*\*\*\*\*  
10662+ # \*\*\*\*\*  
10663+ # \*\*\*\*\*  
10664+ # \*\*\*\*\*  
10665+ # \*\*\*\*\*  
10666+ # \*\*\*\*\*  
10667+ # \*\*\*\*\*  
10668+ # \*\*\*\*\*  
10669+ # \*\*\*\*\*  
10670+ # \*\*\*\*\*  
10671+ # \*\*\*\*\*  
10672+ # The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
10673+ # \*\*\*\*\*  
10674+ R050:COMMANDS-----  
10675+ # \*\*\*\*\*  
10676+ # \*\*\*\*\*  
10677+ # \*\*\*\*\*  
10678+ # \*\*\*\*\*  
10679+ # \*\*\*\*\*  
10680+ # \*\*\*\*\*  
10681+ # \*\*\*\*\*  
10682+ # \*\*\*\*\*  
10683+ # \*\*\*\*\*  
10684+ # \*\*\*\*\*  
10685+ # \*\*\*\*\*  
10686+ # \*\*\*\*\*  
10687+ # \*\*\*\*\*  
10688+ # \*\*\*\*\*  
10689+ # \*\*\*\*\*  
10690+ # \*\*\*\*\*  
10691+ # \*\*\*\*\*  
10692+ R050:COMMANDS-----  
10693+ # \*\*\*\*\*  
10694+ # \*\*\*\*\*  
10695+ # \*\*\*\*\*  
10696+ # \*\*\*\*\*  
10697+ # \*\*\*\*\*  
10698+ # \*\*\*\*\*  
10699+ # \*\*\*\*\*  
10700+ # \*\*\*\*\*  
10701+ # \*\*\*\*\*  
10702+ # \*\*\*\*\*  
10703+ # \*\*\*\*\*  
10704+ # \*\*\*\*\*  
10705+ # \*\*\*\*\*  
10706+ # \*\*\*\*\*  
10707+ # \*\*\*\*\*  
10708+ # \*\*\*\*\*  
10709+ # \*\*\*\*\*  
10710+ # \*\*\*\*\*  
10711+ # \*\*\*\*\*  
10712+ # \*\*\*\*\*  
10713+ # \*\*\*\*\*  
10714+ # The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
10715+ # \*\*\*\*\*  
10716+ R050:COMMANDS-----  
10717+ # \*\*\*\*\*  
10718+ # \*\*\*\*\*  
10719+ # \*\*\*\*\*  
10720+ # \*\*\*\*\*  
10721+ # \*\*\*\*\*  
10722+ # The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
10723+ # \*\*\*\*\*  
10724+ R050:COMMANDS-----  
10725+ # \*\*\*\*\*  
10726+ # \*\*\*\*\*  
10727+ # \*\*\*\*\*  
10728+ # \*\*\*\*\*  
10729+ # \*\*\*\*\*  
10730+ # \*\*\*\*\*  
10731+ # \*\*\*\*\*  
10732+ # \*\*\*\*\*  
10733+ # \*\*\*\*\*  
10734+ # \*\*\*\*\*  
10735+ # \*\*\*\*\*  
10736+ # \*\*\*\*\*  
10737+ # \*\*\*\*\*  
10738+ # \*\*\*\*\*  
10739+ # \*\*\*\*\*  
10740+ R050:COMMANDS-----  
10741+ # \*\*\*\*\*  
10742+ # \*\*\*\*\*  
10743+ # \*\*\*\*\*  
10744+ # \*\*\*\*\*  
10745+ # \*\*\*\*\*  
10746+ # \*\*\*\*\*  
10747+ # \*\*\*\*\*  
10748+ # \*\*\*\*\*  
10749+ # \*\*\*\*\*  
10750+ # \*\*\*\*\*  
10751+ # \*\*\*\*\*  
10752+ # \*\*\*\*\*  
10753+ # \*\*\*\*\*  
10754+ # The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
10755+ # \*\*\*\*\*  
10756+ R050:COMMANDS-----  
10757+ # \*\*\*\*\*  
10758+ # \*\*\*\*\*  
10759+ # \*\*\*\*\*  
10760+ # \*\*\*\*\*  
10761+ # \*\*\*\*\*  
10762+ # The TP was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
10763+ # \*\*\*\*\*  
10764+ R050:COMMANDS-----  
10765+ # \*\*\*\*\*  
10766+ # \*\*\*\*\*  
10767+ # \*\*\*\*\*  
10768+ # \*\*\*\*\*  
10769+ # \*\*\*\*\*  
10770+ # \*\*\*\*\*  
10771+ # \*\*\*\*\*  
10772+ # \*\*\*\*\*  
10773+ # \*\*\*\*\*  
10774+ # \*\*\*\*\*  
10775+ # \*\*\*\*\*  
10776+ R050:COMMANDS-----  
10777+ # \*\*\*\*\*  
10778+ # \*\*\*\*\*  
10779+ # \*\*\*\*\*  
10780+ # \*\*\*\*\*  
10781+ # \*\*\*\*\*  
10782+ # \*\*\*\*\*  
10783+ # \*\*\*\*\*  
10784+ # \*\*\*\*\*  
10785+ # \*\*\*\*\*  
10786+ # \*\*\*\*\*  
10787+ # \*\*\*\*\*  
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10789+ # \*\*\*\*\*  
10790+ # \*\*\*\*\*  
10791+ # \*\*\*\*\*  
10792+ # \*\*\*\*\*  
10793+ # \*\*\*\*\*  
10794+ # \*\*\*\*\*  
10795+ # \*\*\*\*\*  
10796+ # \*\*\*\*\*  
10797+ # \*\*\*\*\*  
10798+ R050:COMMANDS-----  
10799+ # \*\*\*\*\*  
10800+ # \*\*\*\*\*  
10801+ # \*\*\*\*\*  
10802+ # \*\*\*\*\*  
10803+ # \*\*\*\*\*  
10804+ # \*\*\*\*\*  
10805+ # \*\*\*\*\*  
10806+ # \*\*\*\*\*  
10807+ # \*\*\*\*\*  
10808+ R050:COMMANDS-----  
10809+ # \*\*\*\*\*  
10810+ # \*\*\*\*\*  
10811+ # \*\*\*\*\*  
10812+ # \*\*\*\*\*  
10813+ R050:COMMANDS-----  
10814+ # \*\*\*\*\*  
10815+ # \*\*\*\*\*  
10816+ # \*\*\*\*\*  
10817+ # \*\*\*\*\*  
10818+ # \*\*\*\*\*  
10819+ # \*\*\*\*\*  
10820+ # \*\*\*\*\*  
10821+ # \*\*\*\*\*  
10822+ # \*\*\*\*\*  
10823+ R050:COMMANDS-----  
10824+ # \*\*\*\*\*  
10825+ # \*\*\*\*\*  
10826+ # \*\*\*\*\*  
10827+ # \*\*\*\*\*  
10828+ # Routing hydrographs  
10829+ # \*\*\*\*\*  
10830+ # \*\*\*\*\*  
10831+ # Starting with the addition of Jock River Headwater and Subwatershed 13  
10832+ # \*\*\*\*\*  
10833+ R050:COMMANDS-----  
10834+ # \*\*\*\*\*  
10835+ # \*\*\*\*\*  
10836+ # \*\*\*\*\*  
10837+ # \*\*\*\*\*  
10838+ # Sum of hydrographs from Node 13 routed to Node 13A  
10839+ # [Approximated cross-section - see cross-section 258]  
10840+ # n=0.04 for summer conditions and n=0.025 for spring conditions  
10841+ # \*\*\*\*\*  
10842+ R050:COMMANDS-----  
10843+ # \*\*\*\*\*  
10844+ # \*\*\*\*\*  
10845+ # \*\*\*\*\*  
10846+ # \*\*\*\*\*

```

10847# # Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
10848# 
10849# 
10850# R050:00032-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
10851#   ADD HYD
10852#     + 1.0 02:R_SW_1 18.00 1.021 18.00 No_date 39:06 29.68 n/a .000
10853#     SUM+ 1.0 01:SN1A 3574.00 3.812 No_date 39:53 24.31 n/a .000
10854#   SUM+ 1.0 01:SN1A 7724.00 27.939 No_date 39:54 27.68 n/a .000
10855# 
10856# # Insertion of a reservoir to simulate the effects of the Goodwood Marsh
10857# 
10858# R050:00033-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
10859#   ROUTE RESERVOIR -> 1.0 01:RES_GM
10860#     out<= 1.0 01:RES_GM
10861#       [ModtCoed=.1481e-03 m3]
10862# 
10863# R050:00034-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
10864#   SUM+ 1.0 01:RES_GM
10865#   frame :H_RSEGGM
10866#   remark:Outflow from Res GM
10867# 
10868# # Outflow from the Goodwood Marsh routed from Node 13A to Node 12
10869# 
10870# # (Approximated cross-section - see cross-section 258)
10871# 
10872# ROUTE CHANNEL -> 1.0 02:RES_GM
10873#   [RDt= 1.001 out<- 1.0 01:IN12
10874#     7725.00 3.808 No_date 61:35 27.67 n/a .000
10875#   [L/S/n= .0782/.0782] [Vmax=.5561max= 1.541]
10876# 
10877# # Addition of Subwatershed Jock River at Ashton to Node 12
10878# 
10879# R050:00036-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
10880#   ADD HYD
10881#     + 1.0 02:JR_AN 7725.00 1.804 No_date 64:19 27.68 n/a .000
10882#     SUM+ 1.0 02:JR_AN 1781.00 16.834 No_date 32:39 36.85 n/a .000
10883#   SUM+ 1.0 01:S_N12 9506.00 18.867 No_date 32:42 29.39 n/a .000
10884# 
10885# R050:00037-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
10886#   SAVE HYD
10887#   frame :H_SN12
10888#   remark:flow to S_N12 near Ashton
10889# 
10890# # Sum of hydrographs from Node 12 routed to Node 11
10891# 
10892# # (Approximated cross-section - see cross-section 258)
10893# 
10894# # Use n=0.04 for sunditions and no=0.25 for spring conditions
10895# 
10896# # Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
10897# 
10898# R050:00038-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
10899#   ROUTE CHANNEL -> 1.0 02:JR_AN
10900#     [RDt= 1.001 out<- 1.0 01:Dum1
10901#     9506.00 18.867 No_date 32:42 29.39 n/a .000
10902#   [L/S/n= .972/.054/ .040]
10903#   [Vmax=.751 Dmax= 3.029]
10904# 
10905# # Addition of Subwatershed 11 and Name Creek to Node 11
10906# 
10907# R050:00039-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
10908#   ADD HYD
10909#     + 1.0 02:JR_AN 9506.00 18.867 No_date 32:42 29.39 n/a .000
10910#     SUM+ 1.0 02:SN11 500.00 9.061 No_date 29:21 33.73 n/a .000
10911#   SUM+ 1.0 02:NC_N 1917.00 12.342 No_date 34:26 31.73 n/a .000
10912#   SUM+ 1.0 01:S_N11 11923.00 32.851 No_date 33:00 29.87 n/a .000
10913# 
10914# # Sum of hydrographs from Node 11 routed to Node 10
10915# 
10916# # Section 1
10917# 
10918# R050:00040-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
10919#   ROUTE CHANNEL -> 1.0 02:S_N11
10920#     [RDt= 1.001 out<- 1.0 01:IN10
10921#     11923.00 32.851 No_date 40:02 29.87 n/a .000
10922#   [L/S/n=14028/.157/.042]
10923#   [Vmax=.474 Dmax= 1.423]
10924# 
10925# # Addition of Subwatershed 10 to Node 10
10926# 
10927# R050:00041-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
10928#   ADD HYD
10929#     + 1.0 02:JR_AN 11923.00 20.490 No_date 40:02 29.87 n/a .000
10930#     SUM+ 1.0 02:JR_AN 11923.00 20.490 No_date 40:02 29.87 n/a .000
10931# 
10932# # Sum of hydrographs from Node 10 routed to Node 9
10933# 
10934# # Section 1
10935# 
10936# R050:00044-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
10937#   ROUTE CHANNEL -> 1.0 02:S_N10
10938#     [RDt= 1.001 out<- 1.0 01:IN9
10939#     29865.00 82.746 No_date 39:45 31.99 n/a .000
10940#   [L/S/n= .0756/.0756]
10941#   [Vmax=.744 Dmax= 2.015]
10942# 
10943# # Addition of Subwatershed 9 and Nichols Creek to Node 9
10944# 
10945# R050:00045-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
10946#   ADD HYD
10947#     + 1.0 02:JR_AN 29865.00 82.746 No_date 39:45 31.99 n/a .000
10948#     SUM+ 1.0 02:JR_AN 29865.00 82.746 No_date 39:45 31.99 n/a .000
10949# 
10950# # Sum of hydrographs from Node 9 routed to Node 8
10951# 
10952# R050:00046-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
10953#   ROUTE CHANNEL -> 1.0 02:S_N9
10954#     [RDt= 1.001 out<- 1.0 01:IN8
10955#     31561.00 93.665 No_date 39:59 31.68 n/a .000
10956#   [L/S/n= .2269/.088/ .048]
10957#   [Vmax=.367 Dmax= 1.834]
10958# 
10959# # Addition of Subwatershed 8 and Hobbs's Drain to Node 8
10960# 
10961# R050:00047-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
10962#   ADD HYD
10963#     + 1.0 02:SN_8 31561.00 99.424 No_date 39:59 31.68 n/a .000
10964#     SUM+ 1.0 02:SN_8 31561.00 99.424 No_date 39:59 31.68 n/a .000
10965# 
10966# # Sum of hydrographs from Node 8 routed to Node 7
10967# 
10968# R050:00048-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
10969#   ROUTE CHANNEL -> 1.0 02:S_N7
10970#     [RDt= 1.001 out<- 1.0 01:IN7
10971#     35546.00 111.843 No_date 39:59 31.68 n/a .000
10972#   [L/S/n= .3982/.083/ .041]
10973#   [Vmax=.231 Dmax= 2.290]
10974# 
10975# # Addition of Subwatershed 7 to Node 7
10976# 
10977# R050:00049-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
10978#   ADD HYD
10979#     + 1.0 02:SN_7 3197.00 13.937 No_date 36:23 25.61 n/a .000
10980#     SUM+ 1.0 02:SN_7 38743.00 102.892 No_date 43:46 31.18 n/a .000
10981# 
10982# R050:00050-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
10983#   SAVE HYD
10984#   frame :H_SNT
10985#   remark:flow at S_N7: NT+ SW_7
10986# 
10987# # Insertion of a reservoir to simulate the effects of the Richmon Fen.
10988# It was assumed that the flow available to the reservoir
10989# Release rate from fen was assumed to be controlled by the downstream
10990# river cross-section for sunditions. It was assumed that for up to
10991# 10% of the water, the main channel of the river would store water.
10992# This is to prevent the river from significantly storing water.
10993# 
10994# # Sum of hydrographs from Node 7 routed to Node 6
10995# 
10996# R050:00051-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
10997#   ROUTE RESERVOIR -> 1.0 02:S_N7
10998#     out<= 1.0 01:RES_RF
10999#       [ModtCoed=.1481e-03 m3]
11000# 
11001# R050:00052-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
11002#   SUM+ 1.0 01:S_N7
11003#   frame :H_RSEFR
11004#   remark:outflow of Richmond Fen
11005# 
11006# R050:00053-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
11007#   ROUTE CHANNEL -> 1.0 02:S_N6
11008#     [RDt= 1.001 out<- 1.0 01:IN6
11009#     38743.00 51.784 No_date 60:27 31.18 n/a .000
11010#     SUM+ 1.0 01:S_N6 40240.01 51.784 No_date 60:27 31.18 n/a .000
11011# 
11012# # Addition of Subwatershed 6 and Van Gaal Drain to Node 6
11013# 
11014# R050:00054-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
11015#   ADD HYD
11016#     + 1.0 02:JR_AN 38743.00 51.784 No_date 60:27 31.18 n/a .000
11017#     SUM+ 1.0 02:VW_DR 1332.00 9.332 No_date 35:12 36.85 n/a .000
11018#     SUM+ 1.0 01:S_N6 40240.01 51.784 No_date 60:27 31.18 n/a .000
11019# 
11020# # Sum of hydrographs from Node 6 routed to Node 5
11021# 
11022# R050:00055-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
11023#   ADD HYD
11024#     + 1.0 02:SN_5 165.00 1.285 No_date 33:02 32.44 n/a .000
11025#     SUM+ 1.0 02:SN_5 1332.00 1.285 No_date 35:12 36.85 n/a .000
11026#     SUM+ 1.0 01:S_N5 40240.01 51.784 No_date 60:27 31.18 n/a .000
11027# 
11028# # Addition of Subwatershed 5 and Flowing Creek to Node 5
11029# 
11030# R050:00056-----Dtnin-ID:NHYD---AREAb-APEAKcms-TpeakDate_hh:mm---RVm=R.C.--DWFcms
11031#   ADD HYD
11032#     + 1.0 02:SN_5 224.00 1.187 No_date 28:45 41.51 n/a .000
11033#     SUM+ 1.0 02:FL_CK 4945.00 44.623 No_date 33:18 38.37 n/a .000
11034#   SUM+ 1.0 01:S_NS 45409.01 71.514 No_date 34:20 32.18 n/a .000

```



11595\* R0505:CO0147-----Dtnin:ID:NHYD-----ARAAh-QPEAKcms-Tpeakdate\_hh:mm:---RVmm-R.C.---DFWfms  
11596\* SWH HYD 1.0 01SWH\_0K 53577.82 128.036 No\_date 33:19 33.65 n/a .000  
11597\* fsum=1.0 SWH\_0K\_0050  
11598\* remark:Total Flows at Okeefe Drain

11600# Hydrograph from Node Okeefe routed to Node at Foster Drain

11601# Channel X-Section obtained from RVCA Hydraulic Model - Station 6215

11602# [ROUTE CHANNEL] -> 1.0 021\_SWH\_0K 53577.82 128.036 No\_date 33:19 33.65 n/a .000  
11603# [ROUTE CHANNEL] -> 1.0 01N\_FO 53577.82 127.650 No\_date 33:44 33.65 n/a .000  
11604# [ROUTE CHANNEL] -> 1.0 021\_SWH\_0K 53577.82 128.036 No\_date 33:19 33.65 n/a .000  
11605# [ROUTE CHANNEL] -> 1.0 01N\_FO 53577.82 127.650 No\_date 33:44 33.65 n/a .000  
11606# [L/b/m] 1.183.../.076.../.038...  
11607# [Vmax] 1.239...[max] 3.374  
11608# \*\*\*\*\*  
11609# Catchment POSTER  
11610# - To Foster ditch south of the poster  
11611# - The poster ditch area is 33.65 ha, remaining agricultural  
11612# 2020-12-01 JFSA Poster area is 33.65 as per Foster SWMP Environmental Study Report, CHMNHILL, Aug 2013.  
11613# - 2020-12-01 decrease Foster drainage area from (373 HA) to (307.98 HA) after increasing Okeefe drainage area to (5  
11614# 2020-12-01 Foster drainage area from (373 HA) to (307.98 HA) after increasing Okeefe drainage area to (5  
11615# \*\*\*\*\*  
11616# R0505:CO0149-----Dtnin:ID:NHYD-----ARAAh-QPEAKcms-Tpeakdate\_hh:mm:---RVmm-R.C.---DFWfms  
11617# SWH HYD 1.0 01-POSTER 5325.44 32.213 No\_date 28:11 58.65 .720 .000  
11618# [XINDP=.55,TIMP=.55]  
11619# [ROUTE CHANNEL] -> 1.0 021\_POSTER 5325.44 32.213 No\_date 28:11 58.65 .720 .000  
11620# [ROUTE CHANNEL] -> 1.0 01N\_POSTER 5325.44 32.213 No\_date 28:11 58.65 .720 .000  
11621# [Impervious area: IAlmp= 1.57SLP1.../.50LGI1473..MMI=.013:SCI=.0]  
11622# [iAECLmp= 4.00..IArECPer= 4.00]  
11623# [ROUTE CHANNEL] -> 1.0 021\_POSTER 5325.44 32.213 No\_date 28:11 58.65 .720 .000  
11624# \*\*\*\*\*  
11625# Foster Pond  
11626# A ratio of the catchment area to the West Clarke pond rating curve  
11627# & a ratio of the catchment area to the West Clarke pond rating curve  
11628# \* from the MSH for the next coordinates  
11629# \*\*\*\*\*  
11630# R0505:CO0150-----Dtnin:ID:NHYD-----ARAAh-QPEAKcms-Tpeakdate\_hh:mm:---RVmm-R.C.---DFWfms  
11631# ROUTE RESERVOIR -> 1.0 021\_POSTER 525.44 .32.213 No\_date 28:11 58.65 n/a .000  
11632# [ROUTE CHANNEL] -> 1.0 021\_POSTER 525.44 .32.213 No\_date 28:11 58.65 n/a .000  
11633# overflow< 1.0 031\_PFOV .00..000 No\_date 0:00 ..000 n/a ..000  
11634# [Mod\*coefs=.7887E+0..m3\_TotVol=250000..m3\_Bv=0..m3\_TotSurf=0..m3]  
11635# \*\*\*\*\*  
11636# ADD HYD 1.0 021\_P\_FOS 325.44 8.185 No\_date 29:03 58.69 n/a .000  
11637# \* 1.0 021\_P\_FOS 325.44 8.185 No\_date 29:03 58.69 n/a .000  
11638# SUM+ 1.0 021\_P\_FOS 325.44 8.185 No\_date 29:03 58.69 n/a .000  
11639# \*\*\*\*\*  
11640# R0505:CO0152-----Dtnin:ID:NHYD-----ARAAh-QPEAKcms-Tpeakdate\_hh:mm:---RVmm-R.C.---DFWfms  
11641# SWH HYD 1.0 01-CLAR\_BRA 73.29 10.442 No\_date 28:05 61.49 .779 .000  
11642# [XINDP=.60,TIMP=.65]  
11643# [ROUTE CHANNEL] -> 1.0 021\_CLAR\_BRA 73.29 10.442 No\_date 28:05 61.49 .779 .000  
11644# [ROUTE CHANNEL] -> 1.0 01N\_CLAR\_BRA 73.29 1.204 No\_date 29:03 61.49 n/a .000  
11645# [Impervious area: IAlmp= 1.57SLP1.../.50LGI1699..MMI=.013:SCI=.0]  
11646# [iAECLmp= 4.00..IArECPer= 4.00]  
11647# [ROUTE CHANNEL] -> 1.0 021\_CLAR\_BRA 73.29 1.204 No\_date 29:03 61.49 n/a .000  
11648# R0505:CO0153-----Dtnin:ID:NHYD-----ARAAh-QPEAKcms-Tpeakdate\_hh:mm:---RVmm-R.C.---DFWfms  
11649# ROUTE RESERVOIR -> 1.0 021\_POSTER 73.29 10.442 No\_date 28:05 61.49 n/a .000  
11650# overflow< 1.0 031\_PFOV .00..000 No\_date 0:00 ..000 n/a ..000  
11651# [Mod\*coefs=.1159E+0..m3\_TotVol=250000..m3\_Bv=0..m3\_TotSurf=0..m3]  
11652# \*\*\*\*\*  
11653# R0505:CO0154-----Dtnin:ID:NHYD-----ARAAh-QPEAKcms-Tpeakdate\_hh:mm:---RVmm-R.C.---DFWfms  
11654# CONTINUOUS STANDHY 1.0 01S1-1\_P-PO-2 4.94 ..000 No\_date 28:01 58.69 .720 .000  
11655# \*\*\*\*\*  
11656# R0505:CO0155-----Dtnin:ID:NHYD-----ARAAh-QPEAKcms-Tpeakdate\_hh:mm:---RVmm-R.C.---DFWfms  
11657# SWH HYD 1.0 01-CLAR\_BRA 73.29 1.204 No\_date 29:03 61.49 n/a .000  
11658# \*\*\*\*\*  
11659# R0505:CO0156-----Dtnin:ID:NHYD-----ARAAh-QPEAKcms-Tpeakdate\_hh:mm:---RVmm-R.C.---DFWfms  
11660# SWH HYD 1.0 01N\_980 330.38 8.232 No\_date 29:01 58.69 n/a .000  
11661# \*\*\*\*\*  
11662# R0505:CO0157-----Dtnin:ID:NHYD-----ARAAh-QPEAKcms-Tpeakdate\_hh:mm:---RVmm-R.C.---DFWfms  
11663# SWH HYD 1.0 01N\_980 330.38 7.857 No\_date 29:22 58.69 n/a .000  
11664# \*\*\*\*\*  
11665# R0505:CO0158-----Dtnin:ID:NHYD-----ARAAh-QPEAKcms-Tpeakdate\_hh:mm:---RVmm-R.C.---DFWfms  
11666# SWH HYD 1.0 01N\_980 330.38 7.857 No\_date 29:22 58.69 n/a .000  
11667# \*\*\*\*\*  
11668# R0505:CO0159-----Dtnin:ID:NHYD-----ARAAh-QPEAKcms-Tpeakdate\_hh:mm:---RVmm-R.C.---DFWfms  
11669# \*\*\*\*\*  
11670# Hydrograph from Node Foster SWM Station 9800 at Foster Drain at station 520  
11671# \* Channel X-Section obtained from RVCA Hydraulic Model - Station 9800  
11672# \*\*\*\*\*  
11673# R0505:CO0157-----Dtnin:ID:NHYD-----ARAAh-QPEAKcms-Tpeakdate\_hh:mm:---RVmm-R.C.---DFWfms  
11674# ROUTE CHANNEL -> 1.0 021\_N980 330.38 8.232 No\_date 29:01 58.69 n/a .000  
11675# [ROUTE 1.00] out< 1.0 01N\_980 330.38 7.857 No\_date 29:22 58.69 n/a .000  
11676# [ROUTE CHANNEL] -> 1.0 021\_N980 330.38 7.857 No\_date 29:22 58.69 n/a .000  
11677# [Impervious area: IAlmp= 1.57SLP1.../.50LGI181..MMI=.013:SCI=.0]  
11678# [iAECLmp= 4.00..IArECPer= 4.00]  
11679# [ROUTE CHANNEL] -> 1.0 021\_N980 330.38 7.857 No\_date 29:22 58.69 n/a .000  
11680# \*\*\*\*\*  
11681# ADD HYD 1.0 021\_N980 330.38 7.857 No\_date 29:22 58.69 n/a .000  
11682# \* 1.0 021\_N980 330.38 7.857 No\_date 29:22 58.69 n/a .000  
11683# SUM+ 1.0 021\_N980 330.38 7.857 No\_date 29:22 58.69 n/a .000  
11684# \*\*\*\*\*  
11685# R0505:CO0160-----Dtnin:ID:NHYD-----ARAAh-QPEAKcms-Tpeakdate\_hh:mm:---RVmm-R.C.---DFWfms  
11686# \*\*\*\*\*  
11687# ADD HYD 1.0 01N\_980 330.38 7.857 No\_date 29:22 58.69 n/a .000  
11688# \*\*\*\*\*  
11689# R0505:CO0161-----Dtnin:ID:NHYD-----ARAAh-QPEAKcms-Tpeakdate\_hh:mm:---RVmm-R.C.---DFWfms  
11690# \*\*\*\*\*  
11691# R0505:CO0162-----Dtnin:ID:NHYD-----ARAAh-QPEAKcms-Tpeakdate\_hh:mm:---RVmm-R.C.---DFWfms  
11692# \*\*\*\*\*  
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12343+ # \*\*\*\*\*

12344+ RO505:CO0264-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12345+ CONTINUOUS NASHYD 1.0 01:FRASER-SRN 13.45 .711 No\_date 28:22 39.91 1.490 .000

12346+ [CIN= 77.0 : Tp= .43] .01

12347+ [iaREC= 4.01 : SMIN= 15.0 : SMAX= 207.66 : SK= 010]

12348+ [Pervious area: IaIimp= 1.57 : SLI= 1.0 : LGI= .01]

12349+ RO505:CO0265-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12350+ CONTINUOUS NASHYD 1.0 01:FRASER-D 21.61 .688 No\_date 28:01 62.97 .773 .000

12351+ KIMP= 5A TIMEPD=.48

12352+ [LOSS= 2 : CIN= 80.0]

12353+ [Previous area: IaIimp= 4.67 : SLI= 1.00 : LGD= 40 : MNP= .250 : SCP= .0]

12354+ [Impervious area: IaIimp= 1.57 : SLI= 1.0 : LGI= .01]

12355+ [iaRECimp= 4.00 : iAREPper= 4.00]

12356+ [MjSys= 30.0 : Tp= .01]

12357+ [Loss= 26.32 : SMIN= 15.0 : SMAX= 207.66 : SK= 010]

12358+ RO505:CO0266-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12359+ COMPUTE DUALHYD 1.0 01:FRASER-D 21.61 .688 No\_date 28:01 62.97 .773 .000

12360+ [Previous area: IaIimp= 4.67 : SLI= 1.00 : LGD= 40 : MNP= .250 : SCP= .0]

12361+ [Impervious area: IaIimp= 1.57 : SLI= 1.0 : LGI= .01]

12362+ [MjSys= 30.0 : Tp= .01]

12363+ RO505:CO0267-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12364+ ADD HYD 1.0 01:FRASER-J .00 .000 No\_date 0:00 .00 n/a .000

12365+ [Loss= 2 : CIN= 80.0]

12366+ [Previous area: IaIimp= 4.67 : SLI= 1.00 : LGD= 40 : MNP= .250 : SCP= .0]

12367+ [Impervious area: IaIimp= 1.57 : SLI= 1.0 : LGI= .01]

12368+ RO505:CO0268-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12369+ COMPUTE DUALHYD 1.0 01:FRASER-D 21.61 .688 No\_date 28:01 62.97 .773 .000

12370+ [Previous area: IaIimp= 4.67 : SLI= 1.00 : LGD= 40 : MNP= .250 : SCP= .0]

12371+ [Impervious area: IaIimp= 1.57 : SLI= 1.0 : LGI= .01]

12372+ [MjSys= 30.0 : Tp= .01]

12373+ RO505:CO0269-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12374+ ADD HYD 1.0 01:FRASER-J .00 .000 No\_date 0:00 .00 n/a .000

12375+ [Loss= 2 : CIN= 80.0]

12376+ RO505:CO0269-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12377+ ADD HYD 1.0 01:FRASER-J .00 .000 No\_date 0:00 .00 n/a .000

12378+ RO505:CO0269-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12379+ frame= 4241\_0050

12380+ remark>Total Flows at Todd-Burnett outlet

12381+ # Hydrograph from Todd-Burnett to station 3633

12382+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 4241

12383+ RO505:CO0270-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12384+ ROUTE CHANNEL > 1.0 01:24241 54568.52 126.092 No\_date 36:02 34.06 n/a .000

12385+ [REC= 1.00 : Tp= .01 : LGI= .01]

12386+ [Loss= 24.0 : CIN= 80.0 : LGD= 40 : MNP= .250 : SCP= .0]

12387+ [Vmax= 1.329 : Dmax= 2.424]

12388+ RO505:CO0271-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12389+ ADD HYD 1.0 01:24241-out 54568.52 126.092 No\_date 36:02 34.06 n/a .000

12390+ [Loss= 2 : CIN= 80.0]

12391+ [Previous area: IaIimp= 4.67 : SLI= 1.00 : LGD= 40 : MNP= .250 : SCP= .0]

12392+ [Impervious area: IaIimp= 1.57 : SLI= 1.0 : LGI= .01]

12393+ RO505:CO0272-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12394+ SUMM 1.0 01:SNK\_XB 54681.21 126.145 No\_date 36:02 34.07 n/a .000

12395+ RO505:CO0272-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12396+ SAVE HYD 1.0 01:SNK\_XB 54681.21 126.145 No\_date 36:02 34.07 n/a .000

12397+ frame= SNK\_XB\_0050

12398+ remark>Total Flows before Station 3633

12399+ # Hydrograph from Station 3633 to Node Todd

12400+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 3633

12401+ # JFSA 2021-2-26 change the channel length (at Station 3633) from 80m to 60m and change the slope from 0.0498% to 0.2

12402+ RO505:CO0273-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12403+ RO505:CO0273-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12404+ [S0T= 1.00 : Tp= .01 : LGI= .01]

12405+ [Loss= 6.08 : .247 : 035]

12406+ [Previous area: IaIimp= 4.67 : SLI= 1.00 : LGD= 40 : MNP= .250 : SCP= .0]

12407+ # \*\*\*\*\*

12408+ # Catchment Greenbank

12409+ To Todd-Burnett (south of the Jock)

12410+ # - JFSA 2021-01-18 add Greenbank pond as per JFSA, P598(04)-15, June 2016

12411+ # - JFSA 2021-01-19 update area from 17.479 ha to 36.6 ha based on GIS measurements

12412+ # - JFSA 2021-01-19 add Greenbank pond as per JFSA, P598(04)-15, June 2016

12413+ RO505:CO0274-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12414+ CONTINUOUS STANDHYD 1.0 01:Greenbank 36.60 .628 No\_date 28:02 65.04 .798 .000

12415+ [Loss= 2 : CIN= 80.0]

12416+ [Previous area: IaIimp= 4.67 : SLI= 1.00 : LGD= 40 : MNP= .250 : SCP= .0]

12417+ [Impervious area: IaIimp= 1.57 : SLI= 1.0 : LGI= .01]

12418+ [iaRECimp= 4.00 : iAREPper= 4.00]

12419+ [SMIN= 31.15 : SMAX= 207.66 : SK= 010]

12420+ RO505:CO0275-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12421+ RO505:CO0275-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12422+ ROUTE RESERVOIR > 1.0 02:Greenbank 36.60 .628 No\_date 28:02 65.04 n/a .000

12423+ out <> 1.0 01:Greenbank 36.60 .417 No\_date 28:03 65.04 n/a .000

12424+ overflow <> 1.0 01:Greenbank 36.60 .176 No\_date 28:03 65.04 n/a .000

12425+ [MjSys= 96.03 : S0T= 0.005 : m3\_TotVol= 0.00005 : m3\_TotSurf= 0.0]

12426+ RO505:CO0276-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12427+ ADD HYD 1.0 02:Greenbank 36.60 .628 No\_date 28:02 65.04 n/a .000

12428+ [Loss= 2 : CIN= 80.0]

12429+ [Previous area: IaIimp= 4.67 : SLI= 1.00 : LGD= 40 : MNP= .250 : SCP= .0]

12430+ [Impervious area: IaIimp= 1.57 : SLI= 1.0 : LGI= .01]

12431+ RO505:CO0277-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12432+ RO505:CO0277-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12433+ RO505:CO0277-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12434+ RO505:CO0277-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12435+ frame= Greenbank\_0050

12436+ # \*\*\*\*\*

12437+ # Catchment Todd

12438+ # Subdivision with 43% imp. as per Barrhaven South M55

12439+ [Pervious area: IaIimp= 4.67 : SLI= 1.00 : LGD= 40 : MNP= .250 : SCP= .0]

12440+ [Loss= 2 : CIN= 80.0]

12441+ [Previous area: IaIimp= 1.57 : SLI= 1.0 : LGI= .01]

12442+ [iaRECimp= 4.00 : iAREPper= 4.00]

12443+ [SMIN= 31.15 : SMAX= 207.66 : SK= 010]

12444+ RO505:CO0278-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12445+ CONTINUOUS STANDHYD 1.0 01:TODD\_MND 2.10 .384 No\_date 28:02 60.20 .654 .798 .000

12446+ [XMP= 53.15 : TIMEPD=.57]

12447+ [Previous area: IaIimp= 4.67 : SLI= 1.00 : LGD= 40 : MNP= .250 : SCP= .0]

12448+ [Impervious area: IaIimp= 1.57 : SLI= 1.0 : LGI= .01]

12449+ [iaRECimp= 4.00 : iAREPper= 4.00]

12450+ [SMIN= 31.15 : SMAX= 207.66 : SK= 010]

12451+ RO505:CO0279-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12452+ RO505:CO0279-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12453+ RO505:CO0279-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12454+ RO505:CO0279-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12455+ frame= TODD\_MND\_0050

12456+ # \*\*\*\*\*

12457+ # Catchment Todd

12458+ # To Todd-Burnett (south of the Jock)

12459+ # - To Todd-Burnett (south of the Jock)

12460+ # - To Todd-Burnett (south of the Jock)

12461+ # - To Todd-Burnett (south of the Jock)

12462+ # - To Todd-Burnett (south of the Jock)

12463+ RO505:CO0279-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12464+ CONTINUOUS NASHYD 1.0 01:TODD\_MND 2.10 .384 No\_date 28:02 60.20 .654 .798 .000

12465+ [Loss= 2 : CIN= 80.0]

12466+ [Previous area: IaIimp= 4.67 : SLI= 1.00 : LGD= 40 : MNP= .250 : SCP= .0]

12467+ [Impervious area: IaIimp= 1.57 : SLI= 1.0 : LGI= .01]

12468+ [iaRECimp= 4.00 : iAREPper= 4.00]

12469+ [SMIN= 31.15 : SMAX= 207.66 : SK= 010]

12470+ RO505:CO0280-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12471+ RO505:CO0280-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12472+ ROUTE RESERVOIR > 1.0 01:TODD\_MND 2.10 .384 No\_date 28:02 60.20 .654 .798 .000

12473+ out <> 1.0 01:TODD\_MND 2.10 .384 No\_date 28:03 60.14 .738 .000

12474+ overflow <> 1.0 01:TODD\_MND 2.10 .384 No\_date 28:03 60.14 .738 .000

12475+ [MjSys= 96.03 : S0T= 0.005 : m3\_TotVol= 0.00005 : m3\_TotSurf= 0.0]

12476+ RO505:CO0281-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12477+ RO505:CO0281-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12478+ RO505:CO0281-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12479+ RO505:CO0281-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12480+ frame= TODD\_MND\_0050

12481+ # \*\*\*\*\*

12482+ # Catchment Todd

12483+ # Subdivision with 43% imp. as per Barrhaven South M55

12484+ [Pervious area: IaIimp= 4.67 : SLI= 1.00 : LGD= 40 : MNP= .250 : SCP= .0]

12485+ [Loss= 2 : CIN= 80.0]

12486+ [Previous area: IaIimp= 1.57 : SLI= 1.0 : LGI= .01]

12487+ [iaRECimp= 4.00 : iAREPper= 4.00]

12488+ [SMIN= 31.15 : SMAX= 207.66 : SK= 010]

12489+ RO505:CO0282-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12490+ RO505:CO0282-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12491+ RO505:CO0282-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12492+ RO505:CO0282-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12493+ RO505:CO0282-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12494+ RO505:CO0282-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12495+ frame= TODD\_MND\_0050

12496+ # \*\*\*\*\*

12497+ # Catchment Todd

12498+ # Subdivision with 43% imp. as per Barrhaven South M55

12499+ [Pervious area: IaIimp= 4.67 : SLI= 1.00 : LGD= 40 : MNP= .250 : SCP= .0]

12500+ [Loss= 2 : CIN= 80.0]

12501+ [Previous area: IaIimp= 1.57 : SLI= 1.0 : LGI= .01]

12502+ [iaRECimp= 4.00 : iAREPper= 4.00]

12503+ [SMIN= 31.15 : SMAX= 207.66 : SK= 010]

12504+ RO505:CO0283-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12505+ RO505:CO0283-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12506+ RO505:CO0283-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12507+ RO505:CO0283-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12508+ RO505:CO0283-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12509+ RO505:CO0283-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12510+ COMPUTE DUALHYD 1.0 01:2A2-MJ 25.50 .3441 No\_date 28:03 55.89 n/a .000

12511+ Major System / 1.0 01:2A2-MJ .64 .180 No\_date 28:07 55.89 n/a .000

12512+ Minor System / 1.0 01:2A2-MJ .00 .000 No\_date 28:07 55.89 n/a .000

12513+ [MjSys= 30.0 : Tp= .01]

12514+ RO505:CO0284-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12515+ RO505:CO0284-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12516+ RO505:CO0284-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12517+ RO505:CO0284-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12518+ RO505:CO0284-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12519+ RO505:CO0284-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12520+ RO505:CO0284-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12521+ RO505:CO0284-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12522+ RO505:CO0284-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12523+ RO505:CO0284-----Dtnin-ID:NHDY---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms

12524+ frame= TODD\_0050

12525+ remark>Total Flows at Todd-Dodd

12526+ # - Rating curve obtained from Barrhaven South M55 modeling

12527+ # - started 2007, Tributary Drainage Area to M55 Pond 3 = 193 ha

12717+ [MJSysSto-.4799E+03, TotDvVol=.0000E+00, N-Ovf= 0, TotDurOvf= 0-.hrs] -> ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12718+ R0505:003122-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12719+ COMPUTE\_DUALHY / 1.0 02:18-MN 15.31 1.029 No\_date 27:53 56.54 n/a .000

12720+ \* [RDV: 1.00] out-> 1.0 01:315-333 12.31 1.029 No\_date 28:33 56.54 n/a .000

12721+ [/S/n= 254, /000E+00] .00 .000 No\_date 0:00 56.54 n/a .000

12722+ [SNIN: 33.81 SMAX-225.43: SK= 010] .00 .000 No\_date 0:00 56.54 n/a .000

12723+ [Din: 1.20]Used= 1.20]

12724+ R0505:003123-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12725+ CONTINUOUS STANDHY 1.0 01:01B 5.53 .825 No\_date 28:01 56.26 690 .000

12726+ [\*XMPn: 41-TIMP=.54] .00 .000 No\_date 0:00 56.26 690 .000

12727+ [Previous area: Iaper: 4.67:SLPP=1.00:LDP= 40.-MNP=.250:SCP=.0] .00 .000 No\_date 0:00 56.26 690 .000

12728+ [Impervious area: Iainp: 1.57:SLPP=1.00:LDP= 345.-MNI=.013:SCIN=.0] .00 .000 No\_date 0:00 56.26 690 .000

12729+ [Snow: 33.81 SNMX-225.43: SK= 010] .00 .000 No\_date 0:00 56.26 690 .000

12730+ R0505:003124-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12731+ COMPUTE\_DUALHY / 1.0 02:18-MN 9.13 .825 No\_date 28:01 56.26 n/a .000

12732+ Major System / 1.0 02:18-MN .02 .083 No\_date 28:09 56.26 n/a .000

12733+ Minor System < 1.0 03:18-MN .57 .459 No\_date 27:52 56.26 n/a .000

12734+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.26 n/a .000

12735+ [SNIN: 33.81 SMAX-225.43: SK= 010] .00 .000 No\_date 0:00 56.26 n/a .000

12736+ R0505:003125-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12737+ ADD HYD 1.0 02:18-MN 5.57 .459 No\_date 27:52 56.26 n/a .000

12738+ [\*XMPn: 41-TIMP=.54] .00 .000 No\_date 0:00 56.26 n/a .000

12739+ [Previous area: Iaper: 4.67:SLPP=1.00:LDP= 40.-MNP=.250:SCP=.0] .00 .000 No\_date 0:00 56.26 n/a .000

12740+ SUM 1.0 01:ME333 17.88 1.488 No\_date 28:32 56.46 n/a .000

12741+ R0505:003126-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12742+ SAVE HYD 1.0 01:ME333 17.88 1.488 No\_date 28:32 56.46 n/a .000

12743+ fname :MH333\_0050 .00 .000 No\_date 0:00 56.46 n/a .000

12744+ remark:Total Flows at MH333 .00 .000 No\_date 0:00 56.46 n/a .000

12745+ R0505:003127-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12746+ ROUTE PIPE --> 1.0 02:ME333 17.88 1.488 No\_date 28:32 56.46 n/a .000

12747+ \* [RDV: 1.00] out-> 1.0 01:333-335 17.88 1.479 No\_date 28:19 56.46 n/a .000

12748+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.46 n/a .000

12749+ [Vmax: 1.302:Dmax: 1.057] .00 .000 No\_date 0:00 56.46 n/a .000

12750+ [Din: 1.20]Used= 1.29]

12751+ R0505:003128-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12752+ ROUTE PIPE --> 1.0 02:333-335 17.88 1.479 No\_date 28:19 56.46 n/a .000

12753+ \* [RDV: 1.00] out-> 1.0 01:333-338 17.88 1.478 No\_date 28:16 56.46 n/a .000

12754+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.46 n/a .000

12755+ [Vmax: 1.300:Dmax: 1.054] .00 .000 No\_date 0:00 56.46 n/a .000

12756+ [Din: 1.20]Used= 1.28]

12757+ R0505:003129-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12758+ ROUTE PIPE --> 1.0 02:333-338 17.88 1.478 No\_date 28:16 56.46 n/a .000

12759+ \* [RDV: 1.00] out-> 1.0 01:338-340 17.88 1.454 No\_date 28:18 56.46 n/a .000

12760+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.46 n/a .000

12761+ [Vmax: 1.330:Dmax: .979] .00 .000 No\_date 0:00 56.46 n/a .000

12762+ [Din: 1.35]Used= 1.35]

12763+ R0505:003130-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12764+ CONTINUOUS STANDHY 1.0 01:BA 7.60 1.094 No\_date 28:02 56.26 690 .000

12765+ [\*XMPn: 41-TIMP=.54] .00 .000 No\_date 0:00 56.26 690 .000

12766+ [Previous area: Iaper: 4.67:SLPP=1.00:LDP= 40.-MNP=.250:SCP=.0] .00 .000 No\_date 0:00 56.26 690 .000

12767+ SUM 1.0 01:ME333 17.88 1.479 No\_date 28:19 56.46 n/a .000

12768+ R0505:003131-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12769+ [SNIN: 33.81 SMAX-225.43: SK= 010] .00 .000 No\_date 0:00 56.46 n/a .000

12770+ SAVE HYD 1.0 01:ME333 17.88 1.479 No\_date 28:19 56.46 n/a .000

12771+ fname :MH340\_0050 .00 .000 No\_date 0:00 56.46 n/a .000

12772+ remark:Total Flows at MH340 .00 .000 No\_date 0:00 56.46 n/a .000

12773+ R0505:003132-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12774+ ADD HYD 1.0 01:BA 7.60 1.094 No\_date 28:02 56.26 n/a .000

12775+ [\*XMPn: 2780B+3, TotDvVol=.0000E+00, N-Ovf= 0, TotDurOvf= 0-.hrs] .00 .000 No\_date 0:00 56.26 700 .000

12776+ R0505:003132-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12777+ COMPUTE\_DUALHY / 1.0 02:18-MN 7.60 .655 No\_date 27:53 56.27 n/a .000

12778+ Major System / 1.0 02:18-MN .02 .083 No\_date 27:53 56.27 n/a .000

12779+ Minor System < 1.0 03:18-MN .57 .459 No\_date 27:53 56.27 n/a .000

12780+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.27 n/a .000

12781+ [SNIN: 33.81 SMAX-225.43: SK= 010] .00 .000 No\_date 0:00 56.27 n/a .000

12782+ R0505:003133-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12783+ COMPUTE\_DUALHY / 1.0 01:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12784+ Major System / 1.0 01:01A .02 .083 No\_date 28:02 56.27 n/a .000

12785+ Minor System < 1.0 02:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12786+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.27 n/a .000

12787+ [Vmax: 1.330:Dmax: .979] .00 .000 No\_date 0:00 56.27 n/a .000

12788+ R0505:003134-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12789+ ROUTE PIPE --> 1.0 02:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12790+ \* [RDV: 1.00] out-> 1.0 01:104-105 13.92 11.118 No\_date 28:10 56.46 n/a .000

12791+ [/S/n= 180, /000E+00] .00 .000 No\_date 0:00 56.46 n/a .000

12792+ fname :MH340\_0050 .00 .000 No\_date 0:00 56.46 n/a .000

12793+ remark:Total Flows at MH340 .00 .000 No\_date 0:00 56.46 n/a .000

12794+ R0505:003134-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12795+ ROUTE PIPE --> 1.0 02:01A 7.60 1.094 No\_date 28:18 56.46 n/a .000

12796+ \* [RDV: 1.00] out-> 1.0 01:104-104 23.48 2.090 No\_date 28:18 56.46 n/a .000

12797+ [/S/n= 210, /000E+00] .00 .000 No\_date 0:00 56.46 n/a .000

12798+ [Vmax: 1.723:Dmax: .918] .00 .000 No\_date 0:00 56.46 n/a .000

12799+ [Din: 1.35]Used= 1.35]

12800+ R0505:003135-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12801+ COMPUTE\_DUALHY / 1.0 02:18-MN 7.60 .655 No\_date 27:53 56.27 n/a .000

12802+ Major System / 1.0 02:18-MN .02 .083 No\_date 27:53 56.27 n/a .000

12803+ Minor System < 1.0 03:18-MN .57 .459 No\_date 27:53 56.27 n/a .000

12804+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.27 n/a .000

12805+ [SNIN: 33.81 SMAX-225.43: SK= 010] .00 .000 No\_date 0:00 56.27 n/a .000

12806+ R0505:003136-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12807+ COMPUTE\_DUALHY / 1.0 01:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12808+ Major System / 1.0 01:01A .02 .083 No\_date 28:02 56.27 n/a .000

12809+ Minor System < 1.0 02:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12810+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.27 n/a .000

12811+ [SNIN: 33.81 SMAX-225.43: SK= 010] .00 .000 No\_date 0:00 56.27 n/a .000

12812+ R0505:003137-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12813+ COMPUTE\_DUALHY / 1.0 01:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12814+ Major System / 1.0 01:01A .02 .083 No\_date 28:02 56.27 n/a .000

12815+ Minor System < 1.0 02:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12816+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.27 n/a .000

12817+ [Vmax: 1.307:Dmax: .918] .00 .000 No\_date 0:00 56.27 n/a .000

12818+ R0505:003138-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12819+ COMPUTE\_DUALHY / 1.0 01:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12820+ Major System / 1.0 01:01A .02 .083 No\_date 28:02 56.27 n/a .000

12821+ Minor System < 1.0 02:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12822+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.27 n/a .000

12823+ [Vmax: 1.307:Dmax: .918] .00 .000 No\_date 0:00 56.27 n/a .000

12824+ R0505:003139-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12825+ COMPUTE\_DUALHY / 1.0 01:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12826+ Major System / 1.0 01:01A .02 .083 No\_date 28:02 56.27 n/a .000

12827+ Minor System < 1.0 02:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12828+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.27 n/a .000

12829+ [Vmax: 1.307:Dmax: .918] .00 .000 No\_date 0:00 56.27 n/a .000

12830+ R0505:003140-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12831+ COMPUTE\_DUALHY / 1.0 01:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12832+ Major System / 1.0 01:01A .02 .083 No\_date 28:02 56.27 n/a .000

12833+ Minor System < 1.0 02:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12834+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.27 n/a .000

12835+ [Vmax: 1.307:Dmax: .918] .00 .000 No\_date 0:00 56.27 n/a .000

12836+ R0505:003141-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12837+ COMPUTE\_DUALHY / 1.0 01:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12838+ Major System / 1.0 01:01A .02 .083 No\_date 28:02 56.27 n/a .000

12839+ Minor System < 1.0 02:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12840+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.27 n/a .000

12841+ [Vmax: 1.307:Dmax: .918] .00 .000 No\_date 0:00 56.27 n/a .000

12842+ R0505:003142-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12843+ COMPUTE\_DUALHY / 1.0 01:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12844+ Major System / 1.0 01:01A .02 .083 No\_date 28:02 56.27 n/a .000

12845+ Minor System < 1.0 02:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12846+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.27 n/a .000

12847+ [Vmax: 1.307:Dmax: .918] .00 .000 No\_date 0:00 56.27 n/a .000

12848+ R0505:003143-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12849+ COMPUTE\_DUALHY / 1.0 01:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12850+ Major System / 1.0 01:01A .02 .083 No\_date 28:02 56.27 n/a .000

12851+ Minor System < 1.0 02:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12852+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.27 n/a .000

12853+ [Vmax: 1.307:Dmax: .918] .00 .000 No\_date 0:00 56.27 n/a .000

12854+ R0505:003144-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12855+ COMPUTE\_DUALHY / 1.0 01:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12856+ Major System / 1.0 01:01A .02 .083 No\_date 28:02 56.27 n/a .000

12857+ Minor System < 1.0 02:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12858+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.27 n/a .000

12859+ [Vmax: 1.307:Dmax: .918] .00 .000 No\_date 0:00 56.27 n/a .000

12860+ R0505:003145-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12861+ COMPUTE\_DUALHY / 1.0 01:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12862+ Major System / 1.0 01:01A .02 .083 No\_date 28:02 56.27 n/a .000

12863+ Minor System < 1.0 02:01A 7.60 1.094 No\_date 28:02 56.27 n/a .000

12864+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.27 n/a .000

12865+ [Vmax: 1.307:Dmax: .918] .00 .000 No\_date 0:00 56.27 n/a .000

12866+ R0505:003146-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12867+ \* [RDV: 1.00] out-> 1.0 01:360-106A 7.19 .629 No\_date 27:51 56.37 n/a .000

12868+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.37 n/a .000

12869+ [Vmax: 1.089:Dmax: .665] .00 .000 No\_date 0:00 56.37 n/a .000

12870+ [Din: 1.05]Used= 1.05]

12871+ R0505:003147-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12872+ CONTINUOUS STANDHY 1.0 01:01B 3.29 .535 No\_date 28:00 56.26 690 .000

12873+ [\*XMPn: 41-TIMP=.54] .00 .000 No\_date 0:00 56.26 690 .000

12874+ [Previous area: Iaper: 4.67:SLPP=1.00:LDP= 40.-MNP=.250:SCP=.0] .00 .000 No\_date 0:00 56.26 690 .000

12875+ [Impervious area: Iainp: 1.57:SLPP=1.00:LDP= 465.-MNI=.013:SCIN=.0] .00 .000 No\_date 0:00 56.26 690 .000

12876+ [Snow: 33.81 SMAX-225.43: SK= 010] .00 .000 No\_date 0:00 56.26 690 .000

12877+ R0505:003148-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12878+ COMPUTE\_DUALHY / 1.0 02:18-MN 7.19 1.124 No\_date 28:01 56.26 n/a .000

12879+ Major System / 1.0 02:18-MN .02 .083 No\_date 28:01 56.26 n/a .000

12880+ Minor System < 1.0 03:18-MN .57 .459 No\_date 27:51 56.27 n/a .000

12881+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.27 n/a .000

12882+ [Vmax: 1.307:Dmax: .918] .00 .000 No\_date 0:00 56.27 n/a .000

12883+ R0505:003149-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12884+ COMPUTE\_DUALHY / 1.0 02:18-MN 7.19 .629 No\_date 27:51 56.37 n/a .000

12885+ Major System / 1.0 02:18-MN .02 .083 No\_date 28:28 56.37 n/a .000

12886+ Minor System < 1.0 03:18-MN .57 .459 No\_date 27:51 56.37 n/a .000

12887+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.37 n/a .000

12888+ [Vmax: 1.307:Dmax: .918] .00 .000 No\_date 0:00 56.37 n/a .000

12889+ R0505:003150-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12890+ COMPUTE\_DUALHY / 1.0 02:18-MN 7.19 .629 No\_date 27:51 56.37 n/a .000

12891+ Major System / 1.0 02:18-MN .02 .083 No\_date 28:28 56.37 n/a .000

12892+ Minor System < 1.0 03:18-MN .57 .459 No\_date 27:51 56.37 n/a .000

12893+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.37 n/a .000

12894+ [Vmax: 1.307:Dmax: .918] .00 .000 No\_date 0:00 56.37 n/a .000

12895+ R0505:003151-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12896+ COMPUTE\_DUALHY / 1.0 02:18-MN 7.19 .629 No\_date 27:51 56.37 n/a .000

12897+ Major System / 1.0 02:18-MN .02 .083 No\_date 28:28 56.37 n/a .000

12898+ Minor System < 1.0 03:18-MN .57 .459 No\_date 27:51 56.37 n/a .000

12899+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.37 n/a .000

12900+ [Vmax: 1.307:Dmax: .918] .00 .000 No\_date 0:00 56.37 n/a .000

12901+ R0505:003152-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12902+ CONTINUOUS STANDHY 1.0 01:EX-LAND 32.50 4.637 No\_date 28:02 56.33 691 .000

12903+ [\*XMPn: 41-TIMP=.54] .00 .000 No\_date 0:00 56.33 691 .000

12904+ [Previous area: Iaper: 4.67:SLPP=1.00:LDP= 40.-MNP=.250:SCP=.0] .00 .000 No\_date 0:00 56.33 691 .000

12905+ [Impervious area: Iainp: 1.57:SLPP=1.00:LDP= 465.-MNI=.013:SCIN=.0] .00 .000 No\_date 0:00 56.33 691 .000

12906+ [Snow: 33.81 SMAX-225.43: SK= 010] .00 .000 No\_date 0:00 56.33 691 .000

12907+ R0505:003153-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->Rvn-R.C. -- DWFcms

12908+ COMPUTE\_DUALHY / 1.0 02:18-MN 7.19 .629 No\_date 27:51 56.33 n/a .000

12909+ Major System / 1.0 02:18-MN .02 .083 No\_date 28:28 56.33 n/a .000

12910+ Minor System < 1.0 03:18-MN .57 .459 No\_date 27:51 56.33 n/a .000

12911+ [/S/n= 120, /000E+00] .00 .000 No\_date 0:00 56.33 n/a .000

12912+ [Vmax: 1.307:Dmax: .918] .00 .000 No\_date 0:00 56.33 n/a .000

12913+ R0505:003154-----DtnID:ID-NHYD-----ARaha-QPEAKms-Tpeakdate\_hh:mm:- ->

13091# # - Tributary Drainage Area to MSS Pond 1 = 145 ha

13092# \*\*\*\*\*

13093# # Hydrograph from Corrigan Drain routed to Jockvale Road

13094# # Channel X-Section obtained from RVEA Hydraulic Model - Station 2462

13095# #

13097# RO050:00387-----Dtnin-ID:NHYD---AREAh-a-QPEAKms-TpeakDate\_hh:mm---RVnn-R.C.---DWFcms

13098# # Rainfall: 1.001 m/hour<----> 1.0 01:R.MJL 55015.59 126.908 No\_date 36:31 34.22 n/a .000

13099# [L/s/n\_ 580 / .445/.045]

13100# [Wmax\_ 2,065.1max\_ 1.983]

13101# \*\*\*\*\*

13102# # Catchment MILLIS

13103# # - To Jock River (north of the Jock)

13104# # - Primarily residential development

13105# #

13106# RO050:00388-----Dtnin-ID:NHYD---AREAh-a-QPEAKms-TpeakDate\_hh:mm---RVnn-R.C.---DWFcms

13107# CONTINUOUS STANDHYD 1.0 01:MILLS 175.99 17.756 No\_date 28:06 50.66 .622 .000

13108# [XING=..38:TIME=.38]

13109# \*\*\*\*\*

13110# # Imperious area: IaPex= 4.67;SLP1=0.00:LGP= 40.:NHP= .250:SCP= .0]

13111# [Imperious area: IaPex= 1.57;SLP1=1.00:LGP=1118.:NM1=.013:SCI= .0]

13112# [ROUTE 1.001 out<----> 1.0 01:R.MJL 55015.59 126.908 No\_date 36:31 34.22 n/a .000

13113# [Wmax\_ 2,065.1max\_ 1.983]

13114# \*\*\*\*\*

13115# # Catchment SMILLIS

13116# # - Channel X-Section obtained from CCL hydraulic modeling

13117# # - Rating curve obtained from CCL hydraulic modeling

13118# \*\*\*\*\*

13119# # Previous area: IaPex= 4.67;SLP1=0.00:LGP= 40.:NHP= .250:SCP= .0]

13120# ROUTE RESERVOIR -> 1. 0 02:MILLS 175.99 17.756 No\_date 28:06 50.66 n/a .000

13121# out <----> 1. 0 01:MILLS\_P 22.12 12.440 No\_date 28:11 50.66 n/a .000

13122# [ROUTE 1.001 out<----> 1. 0 01:MILLS\_P 22.12 12.440 No\_date 28:11 50.66 n/a .000

13123# [ROUTE 1.001 out<----> 1. 0 01:MILLS\_P 22.12 12.440 No\_date 28:11 50.66 n/a .000

13124# [MSTOutCode], 21310-E01 m3, TotVolV1..1121K-E01 m3, N-Ovf= 2, TotHovFv= 1.hrs

13125# ADD HYD 55015.59 126.908 No\_date 28:06 50.66 .622 .000

13126# \*\*\*\*\*

13127# # To Jock River (north of the Jock)

13128# # - Residential development (Heart's Desire Community)

13129# #

13130# RO050:00391-----Dtnin-ID:NHYD---AREAh-a-QPEAKms-TpeakDate\_hh:mm---RVnn-R.C.---DWFcms

13131# [ROUTE 1.001 out<----> 1. 0 01:SN\_MJL 55195.59 127.533 No\_date 36:30 34.27 n/a .000

13132# [ROUTE 1.001 out<----> 1. 0 01:SN\_MJL 55195.59 127.533 No\_date 36:30 34.27 n/a .000

13133# [Wmax\_ 1.877.1max\_ 2.490]

13134# \*\*\*\*\*

13135# # Catchment DESIRE

13136# # - To Jock River (north of the Jock)

13137# # - Residential development (Heart's Desire Community)

13138# \*\*\*\*\*

13139# # Previous area: IaPex= 4.67;SLP1=0.00:LGP= 40.:NHP= .250:SCP= .0]

13140# [Imperious area: IaPex= 1.57;SLP1=1.00:LGP= 400.:NM1=.013:SCI= .0]

13141# [iabECM= 4.00: IaRECPer= 4.00]

13142# \*\*\*\*\*

13143# # Catchment JOCKVA

13144# # - To Jock River (north of the Jock)

13145# # - Residential development & golf course

13146# # JFRA 2021-01-11 update JOCKVA to include updating CORRIS as per IRI GROUP, July 2008.

13147# \*\*\*\*\*

13148# # Previous area: IaPex= 4.67;SLP1=0.00:LGP= 40.:NHP= .250:SCP= .0]

13149# [LGS0= 2 :CIN= 77.0]

13150# \*\*\*\*\*

13151# # Previous area: IaPex= 4.67;SLP1=0.00:LGP= 40.:NHP= .250:SCP= .0]

13152# [Imperious area: IaPex= 1.57;SLP1=1.00:LGP= 400.:NM1=.013:SCI= .0]

13153# [iabECM= 4.00: IaRECPer= 4.00]

13154# \*\*\*\*\*

13155# # Catchment JOKCKVA

13156# # - To Jock River (north of the Jock)

13157# # - Residential development & golf course

13158# \*\*\*\*\*

13159# # Previous area: IaPex= 4.67;SLP1=0.00:LGP= 40.:NHP= .250:SCP= .0]

13160# [ROUTE 1.001 out<----> 1. 0 01:JOCKVA 22.13 25.293 No\_date 28:07 56.33 .691 .000

13161# \*\*\*\*\*

13162# RO050:00394-----Dtnin-ID:NHYD---AREAh-a-QPEAKms-TpeakDate\_hh:mm---RVnn-R.C.---DWFcms

13163# CONTINUOUS STANDHYD 1.0 01:JOCKVA 32.13 25.293 No\_date 28:07 56.33 .691 .000

13164# [XING=..50:TIME=.50]

13165# \*\*\*\*\*

13166# # Previous area: IaPex= 4.67;SLP1=0.00:LGP= 40.:NHP= .250:SCP= .0]

13167# [Imperious area: IaPex= 1.57;SLP1=1.00:LGP= 400.:NM1=.013:SCI= .0]

13168# [iabECM= 4.00: IaRECPer= 4.00]

13169# \*\*\*\*\*

13170# RO050:00395-----Dtnin-ID:NHYD---AREAh-a-QPEAKms-TpeakDate\_hh:mm---RVnn-R.C.---DWFcms

13171# ADD HYD 1. 0 02:EX-LAND\_MN 31.74 2. 275 No\_date 27:49 56.55 n/a .000

13172# out <----> 1. 0 02:EX-LAND\_MN .000 .000 No\_date 28:07 56.33 .691 .000

13173# [ROUTE 1.001 out<----> 1. 0 02:EX-LAND\_MN .000 .000 No\_date 28:07 56.33 .691 .000

13174# [ROUTE 1.001 out<----> 1. 0 02:EX-LAND\_MN .000 .000 No\_date 28:07 56.33 .691 .000

13175# [ROUTE 1.001 out<----> 1. 0 02:EX-LAND\_MN .000 .000 No\_date 28:07 56.33 .691 .000

13176# RO050:00396-----Dtnin-ID:NHYD---AREAh-a-QPEAKms-TpeakDate\_hh:mm---RVnn-R.C.---DWFcms

13177# \*\*\*\*\*

13178# name: JOCKVA-TO.0500

13179# remark:Total Flows at KB first pond

13180# \*\*\*\*\*

13181# # Jockvale SNM Facility

13182# # - Rating curve obtained from Jockvale Service Study (CC 1999)

13183# \*\*\*\*\*

13184# RO050:00397-----Dtnin-ID:NHYD---AREAh-a-QPEAKms-TpeakDate\_hh:mm---RVnn-R.C.---DWFcms

13185# ROUTE RESERVOIR -> 1. 0 02:JOCKVA-TO 256.89 27.528 No\_date 28:07 56.36 n/a .000

13186# out <----> 1. 0 02:JOCKVA-TO 256.89 10.991 No\_date 28:07 56.36 n/a .000

13187# [ROUTE 1.001 out<----> 1. 0 02:JOCKVA-TO 256.89 10.991 No\_date 28:07 56.36 n/a .000

13188# [MSTOutCode], 59280-E01 m3, TotVolV1..0.0, N-Ovf= 0, TotHovFv= 0.hrs

13189# \*\*\*\*\*

13190# ADD HYD 1. 0 02:D\_NDE 55195.59 127.235 No\_date 28:43 34.27 n/a .000

13191# out <----> 1. 0 02:D\_NDE 23.78 2.563 No\_date 28:07 46.85 n/a .000

13192# [ROUTE 1.001 out<----> 1. 0 02:D\_NDE 23.78 2.563 No\_date 28:07 46.85 n/a .000

13193# [ROUTE 1.001 out<----> 1. 0 02:JOCK\_P 256.89 10.991 No\_date 28:38 56.36 n/a .000

13194# SUM= 1. 0 01:SN\_HYD 55476.26 128.174 No\_date 36:42 34.38 n/a .000

13195# \*\*\*\*\*

13196# SAVE HYD 1. 0 01:SN\_DNE 55476.26 128.174 No\_date 36:42 34.38 n/a .000

13197# \*\*\*\*\*

13198# name: SN\_DE\_0500

13199# remark:Total Flows at Heart's Desire

13200# \*\*\*\*\*

13201# # Hydrograph from Heart's Desire routed to Rideau River

13202# # Channel X-Section obtained from RVEA Hydraulic Model - Station 0

13203# RO050:00400-----Dtnin-ID:NHYD---AREAh-a-QPEAKms-TpeakDate\_hh:mm---RVnn-R.C.---DWFcms

13204# ROUTE CHANNEL -> 1. 0 01:R.DES 55476.26 128.174 No\_date 36:42 34.38 n/a .000

13205# [ROUTE 1.001 out<----> 1. 0 01:R.DES 55476.26 128.174 No\_date 36:42 34.38 n/a .000

13206# [ROUTE 1.001 out<----> 1. 0 01:R.DES 55476.26 128.174 No\_date 36:45 34.38 n/a .000

13207# [ROUTE 1.001 out<----> 1. 0 01:R.DES 55476.26 128.174 No\_date 36:45 34.38 n/a .000

13208# \*\*\*\*\*

13209# # Catchment S-2

13210# # - To Jock River (north and south)

13211# # - Underdeveloped floodplain and river

13212# \*\*\*\*\*

13213# RO050:00401-----Dtnin-ID:NHYD---AREAh-a-QPEAKms-TpeakDate\_hh:mm---RVnn-R.C.---DWFcms

13214# CONTINUOUS NASHRD 1. 0 01:S-2 102.94 4.795 No\_date 28:20 35.39 .434 .000

13215# [CN= 72. 0: NM= 3.0: Tp= 40]

13216# [ROUTE 1.001 out<----> 1. 0 01:S-2 102.94 4.795 No\_date 28:20 35.39 .434 .000

13217# [InterEventTime= 12.00]

13218# RO050:00402-----Dtnin-ID:NHYD---AREAh-a-QPEAKms-TpeakDate\_hh:mm---RVnn-R.C.---DWFcms

13219# ADD HYD 1. 0 02:S-2 55476.26 128.160 No\_date 36:45 34.38 n/a .000

13220# out <----> 1. 0 02:S-2 102.94 4.795 No\_date 28:20 35.39 .434 .000

13221# [ROUTE 1.001 out<----> 1. 0 02:S-2 102.94 4.795 No\_date 28:20 35.39 .434 .000

13222# RO050:00403-----Dtnin-ID:NHYD---AREAh-a-QPEAKms-TpeakDate\_hh:mm---RVnn-R.C.---DWFcms

13223# SAVE HYD 1. 0 01:SN\_MJL 55579.20 128.417 No\_date 36:44 34.38 n/a .000

13224# \*\*\*\*\*

13225# remark:Total Flows at Rideau River

13226# \*\*\*\*\*

13227# \*\*\* END OF RUN : 99

13228# \*\*\*\*\*

13229# \*\*\*\*\*

13230# \*\*\*\*\*

13231# \*\*\*\*\*

13232# \*\*\*\*\*

13233# RNN:COMMAND

13234# \*\*\*\*\*

13235# START

13236# [TZRO = -1.00 hrs on 0]

13237# [ROUTE 1.001 out<----> 1. 0 01:R.DES 55476.26 128.174 No\_date 36:45 34.38 n/a .000]

13238# [NSTORM= 1 ]

13239# [NRUN= 0100 ]

13240# \*\*\*\*\*

13241# SWMMHY Ver=1.02/Jan 2001 <BETA> / INPUT DATA FILE

13242# \*\*\*\*\*

13243# # Using SWMMHY Parameters

13244# \*\*\*\*\*

13245# # USING CONTINUOUS NASHRD

13246# \*\*\*\*\*

13247# # Modelling : [N,W]

13248# # License # : 2549237

13249# \*\*\*\*\*

13250# \*\*\*\*\*

13251# \*\*\*\*\*

13252# \*\*\*\*\*

13253# \*\*\*\*\*

13254# \*\*\*\*\*

13255# \*\*\*\*\*

13256# \*\*\*\*\*

13257# \*\*\*\*\*

13258# \*\*\*\*\*

13259# \*\*\*\*\*

13260# \*\*\*\*\*

13261# \*\*\*\*\*

13262# READ STORM

13263# Filenam= P:\\PROJ\\1474-16\\Design\\20201026-QuantityControlAnalysis\\SWMMHY\\SMR-Model\\updated3\\CitiGate.DEF

13264# Comment = Plots SCS de 24 hres 1:100 ans pour Ottawa CDA

13265# [SDT=10.00:SDUR= 24.00:PTOT= 88.57]

13266# \*\*\*\*\*

13267# MODIFY STORM

13268# [PFAUT= 0.01:PFSUR= 40.00:PTOT= 88.57]

13269# \*\*\*\*\*

13270# RO050:0004-----

13271# \*\*\*\*\*

13272# DESTRUCT VALUE

13273# Filenam= P:\\PROJ\\1474-16\\Design\\20201026-QuantityControlAnalysis\\SWMMHY\\SMR-Model\\updated3\\CitiGate.DEF

13274# ICASERW = 1 (read and print data)

13275# Filetitle= file title for basic onvarious calibration exercises in Cntra

13276# THE FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDHYD COM

13277# Horton's infiltration equation parameters:

13278# [F=76.20 mm/hr] [FC=13.20 mm/hr] [DCATy= 4.14 / hr] [F= .00 mm]

13279# \*\*\*\*\*

13280# Parameters for PVERG surfaces in STANDHYD:

13281# [TaP= 16.67 TaL= 25.00 mm TaR= 25.00]

13282# Parameters for IMPERV surfaces in STANDHYD:

13283# [TaIimp= 1.57 mm] [CLL= 1.50] [MN1= .013]

13284# Parameters used in NASHRD:

13285# [Ta= 4.67 mm] [TaR= 3.00]

13286# Average monthly Pan Evaporation data in (mm)

13287# Average monthly Potential Evapotranspiration in (mm)

13288# [APIDay= .00 APIMin= .00 APIDay= .00 APIMin= .00]

13289# [APIDay= .00 APIMin= .00 APIDay= .00 APIMin= .00]

13290# RO101:CG0005-----Dtnin-ID:NHYD---AREAh-a-QPEAKms-TpeakDate\_hh:mm---RVnn-R.C.---DWFcms

13291# \*\*\*\*\*

13292# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13293# \*\*\*\*\*

13294# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13295# \*\*\*\*\*

13296# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13297# \*\*\*\*\*

13298# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13299# \*\*\*\*\*

13300# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13301# \*\*\*\*\*

13302# \*\*\*\*\*

13303# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13304# \*\*\*\*\*

13305# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13306# \*\*\*\*\*

13307# CONTINUOUS NASHRD 1. 0 01:JR\_HJD 3680.0 21.616 No\_date 36:52 35.18 .397 .000

13308# [CN= 64.0: NM= 3.00: Tp= 7.13]

13309# \*\*\*\*\*

13310# [InterEventTime= 12.00]

13311# \*\*\*\*\*

13312# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13313# \*\*\*\*\*

13314# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13315# \*\*\*\*\*

13316# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13317# \*\*\*\*\*

13318# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13319# \*\*\*\*\*

13320# CONTINUOUS NASHRD 1. 0 01:JR\_ASH 1781.0 19.695 No\_date 32:38 42.49 .480 .000

13321# [CN= 64.0: NM= 3.00: Tp= 3.91]

13322# [InterEventTime= 12.00]

13323# \*\*\*\*\*

13324# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13325# \*\*\*\*\*

13326# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13327# \*\*\*\*\*

13328# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13329# \*\*\*\*\*

13330# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13331# \*\*\*\*\*

13332# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13333# \*\*\*\*\*

13334# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13335# \*\*\*\*\*

13336# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13337# \*\*\*\*\*

13338# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13339# \*\*\*\*\*

13340# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13341# \*\*\*\*\*

13342# CONTINUOUS NASHRD 1. 0 01:JR\_CK 1917.0 14.496 No\_date 34:24 36.76 .415 .000

13343# [CN= 64.0: NM= 3.00: Tp= 5.29]

13344# [InterEventTime= 12.00]

13345# \*\*\*\*\*

13346# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13347# \*\*\*\*\*

13348# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13349# \*\*\*\*\*

13350# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13351# \*\*\*\*\*

13352# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13353# \*\*\*\*\*

13354# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13355# \*\*\*\*\*

13356# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13357# \*\*\*\*\*

13358# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13359# \*\*\*\*\*

13360# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13361# \*\*\*\*\*

13362# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13363# \*\*\*\*\*

13364# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13365# \*\*\*\*\*

13366# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13367# \*\*\*\*\*

13368# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13369# \*\*\*\*\*

13370# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13371# \*\*\*\*\*

13372# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13373# \*\*\*\*\*

13374# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13375# \*\*\*\*\*

13376# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13377# \*\*\*\*\*

13378# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13379# \*\*\*\*\*

13380# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13381# \*\*\*\*\*

13382# CONTINUOUS NASHRD 1. 0 01:JR\_SMR 1312.0 37.663 No\_date 37:48 42.49 .480 .000

13383# [CN= 64.0: NM= 3.00: Tp= 2.51]

13384# [InterEventTime= 12.00]

13385# \*\*\*\*\*

13386# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13387# \*\*\*\*\*

13388# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13389# \*\*\*\*\*

13390# CONTINUOUS NASHRD 1. 0 01:JR\_HJD 3854.00 21.238 No\_date 38:28 36.76 .415 .000

13391# [CN= 64.0: NM= 3.00: Tp= 8.42]

13392# \*\*\*\*\*

13393# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13394# \*\*\*\*\*

13395# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13396# \*\*\*\*\*

13397# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13398# \*\*\*\*\*

13399# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13400# \*\*\*\*\*

13401# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13402# \*\*\*\*\*

13403# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13404# \*\*\*\*\*

13405# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13406# \*\*\*\*\*

13407# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13408# \*\*\*\*\*

13409# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13410# \*\*\*\*\*

13411# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13412# \*\*\*\*\*

13413# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13414# \*\*\*\*\*

13415# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13416# \*\*\*\*\*

13417# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13418# \*\*\*\*\*

13419# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13420# \*\*\*\*\*

13421# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13422# \*\*\*\*\*

13423# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13424# \*\*\*\*\*

13425# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13426# \*\*\*\*\*

13427# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13428# \*\*\*\*\*

13429# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13430# \*\*\*\*\*

13431# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13432# \*\*\*\*\*

13433# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13434# \*\*\*\*\*

13435# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13436# \*\*\*\*\*

13437# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13438# \*\*\*\*\*

13439# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13440# \*\*\*\*\*

13441# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13442# \*\*\*\*\*

13443# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13444# \*\*\*\*\*

13445# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13446# \*\*\*\*\*

13447# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13448# \*\*\*\*\*

13449# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13450# \*\*\*\*\*

13451# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13452# \*\*\*\*\*

13453# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13454# \*\*\*\*\*

13455# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13456# \*\*\*\*\*

13457# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13458# \*\*\*\*\*

13459# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13460# \*\*\*\*\*

13461# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

13462# \*\*\*\*\*

13463# Starting with the addition of Jock River Headwater and Subwatershed 13

13464# RO101:CG0030-----Dtnin-ID:NHYD---AREAh-a-QPEAKms-TpeakDate\_hh:mm---RVnn-R.C.---DWFcms

13465+ ADD HYD 1.0 02:JR\_HW 3680.00 21.616 No\_date 36:52 35.18 n/a .000  
 13466+ \* 1.0 02:SW\_13 971.00 6.203 No\_date 32:33 32.84 n/a .000  
 13467+ SUM+ 1.0 01:RS\_13 4651.00 27.640 No\_date 35:21 34.69 n/a .000

13468+ # Sum of hydrographs from Node 13 routed to Node 14a  
 13469+ # (Approximated cross-section - see cross-section 258)  
 13470+ # Use n=0.04 for summer conditions and n=0.025 for spring conditions  
 13471+ #  
 13472+ #  
 13473+ # Approximated cross-section - see cross-section 258  
 13474+ ROUTE CHANNEL -> 1.0 02:S,N13 4651.00 27.660 No\_date 35:21 34.69 n/a .000  
 13475+ [ROT= 1.001 out- 1.0 01:N13A 4651.00 22.598 No\_date 38:06 34.69 n/a .000  
 13476+ [L/S/nv 9074.0 / .022/.049] [Vmax=.598 Dmax= 4.178]  
 13477+ [Vmax=.598 Dmax= 4.178]  
 13478+ # Addition of Subwatershed 5 and Flowing Creek to Node 5  
 13479+ #  
 13480+ # Addition of Subwatershed Jock River at Goodwood Marsh to Node 13a  
 13481+ #  
 13482+ ADD HYD 1.0 02:N13A 4651.00 22.598 No\_date 38:06 34.69 n/a .000  
 13483+ \* 1.0 02:JR\_GWH 3074.00 10.428 No\_date 39:59 28.29 n/a .000  
 13484+ SUM+ 1.0 01:N13A 7725.00 32.845 No\_date 39:44 32.14 n/a .000

13485+ # Insertion of a reservoir to simulate the effects of the Goodwood Marsh  
 13486+ #  
 13487+ # R0100:CO0031-----Dtnin-ID:NYRD-----AREAbn-QPEAKcms-TpeakDate\_bh:mm:---RVMn-R.C.---DWFcms  
 13488+ ROUTE RESERVOIR -> 1.0 02:N13A 7725.00 32.845 No\_date 38:44 32.14 n/a .000  
 13489+ [ROT= 1.001 out- 1.0 01:RES\_GWH 7725.00 3.980 No\_date 62:26 32.14 n/a .000

13490+ # [MstcOuted,17968<3 m3]  
 13491+ #  
 13492+ # R0100:CO0034-----Dtnin-ID:NYRD-----AREAbn-QPEAKcms-TpeakDate\_bh:mm:---RVMn-R.C.---DWFcms  
 13493+ SAVV HYD 1.0 01:RES\_GWH 7725.00 3.980 No\_date 62:26 32.14 n/a .000

13494+ frame H\_RSRR  
 13495+ remark:flow from Res GM  
 13496+ #  
 13497+ # Output of Reservoir Goodwood Marsh routed from Node 13a to Node 12  
 13498+ # (Approximated cross-section - see cross-section 258)  
 13499+ # Use n=0.04 for summer conditions and n=0.025 for spring conditions  
 13500+ #  
 13501+ # R0100:CO0035-----Dtnin-ID:NYRD-----AREAbn-QPEAKcms-TpeakDate\_bh:mm:---RVMn-R.C.---DWFcms  
 13502+ ROUTE CHANNEL -> 1.0 02:RES\_GWH 7725.00 3.980 No\_date 62:26 32.14 n/a .000  
 13503+ [ROT= 1.001 out- 1.0 01:N12 7725.00 3.947 No\_date 64:43 32.14 n/a .000

13504+ [L/S/nv .5926 / .076/.049] [Vmax=.560 Dmax= 1.560]  
 13505+ #  
 13506+ # Addition of Subwatershed Jock River at Ashton to Node 12  
 13507+ #  
 13508+ # R0100:CO0036-----Dtnin-ID:NYRD-----AREAbn-QPEAKcms-TpeakDate\_bh:mm:---RVMn-R.C.---DWFcms  
 13509+ ADD HYD 1.0 02:N12 7725.00 3.947 No\_date 64:43 32.14 n/a .000  
 13510+ \* 1.0 02:JR\_GWH 1781.00 19.695 No\_date 33:57 42.12 n/a .000  
 13511+ SUM+ 1.0 01:RS\_12 9506.00 21.745 No\_date 32:41 34.08 n/a .000

13512+ # [ROT= 1.001 out- 1.0 01:N12 9506.00 21.522 No\_date 32:57 34.08 n/a .000

13513+ [L/S/nv .972 / .054/.049] [Vmax=.777 Dmax= 3.194]  
 13514+ #  
 13515+ #  
 13516+ # Addition of Subwatershed 11 and Name Creek to Node 11  
 13517+ #  
 13518+ # (Approximated cross-section - see cross-section 258)  
 13519+ # Use n=0.04 for summer conditions and n=0.025 for spring conditions  
 13520+ #  
 13521+ # Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248  
 13522+ #  
 13523+ # R0100:CO0038-----Dtnin-ID:NYRD-----AREAbn-QPEAKcms-TpeakDate\_bh:mm:---RVMn-R.C.---DWFcms  
 13524+ ROUTE CHANNEL -> 1.0 02:S,N12 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
 13525+ [ROT= 1.001 out- 1.0 01:Dm1 9506.00 21.522 No\_date 32:57 34.08 n/a .000

13526+ [L/S/nv .972 / .054/.049] [Vmax=.777 Dmax= 3.194]  
 13527+ #  
 13528+ #  
 13529+ # Addition of Subwatershed 11 and Name Creek to Node 11  
 13530+ #  
 13531+ # R0100:CO0039-----Dtnin-ID:NYRD-----AREAbn-QPEAKcms-TpeakDate\_bh:mm:---RVMn-R.C.---DWFcms  
 13532+ ADD HYD 1.0 02:N12 9506.00 21.522 No\_date 32:57 34.08 n/a .000  
 13533+ \* 1.0 02:SW\_11 500.00 10.735 No\_date 29:21 36.76 n/a .000  
 13534+ SUM+ 1.0 01:RS\_11 1973.00 21.440 No\_date 38:06 34.62 n/a .000

13535+ SHM+ 1.0 01:S,N12 11923.00 38.138 No\_date 32:59 34.62 n/a .000

13536+ #  
 13537+ # Sum of hydrographs from Node 11 routed to Node 10  
 13538+ #  
 13539+ # R0100:CO0040-----Dtnin-ID:NYRD-----AREAbn-QPEAKcms-TpeakDate\_bh:mm:---RVMn-R.C.---DWFcms  
 13540+ ROUTE CHANNEL -> 1.0 02:S,N11 11923.00 38.138 No\_date 32:59 34.62 n/a .000  
 13541+ [ROT= 1.001 out- 1.0 01:N11 11923.00 23.609 No\_date 39:19 34.62 n/a .000

13542+ [L/S/nv .152 / .076/.049] [Vmax=.486 Dmax= 1.492]  
 13543+ #  
 13544+ frame H\_RSRR  
 13545+ remark:flow at S,N11 near Ashton  
 13546+ #  
 13547+ # Sum of hydrographs from Node 12 routed to Node 11  
 13548+ # (Approximated cross-section - see cross-section 258)  
 13549+ # Use n=0.04 for summer conditions and n=0.025 for spring conditions  
 13550+ #  
 13551+ # Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248  
 13552+ #  
 13553+ # R0100:CO0038-----Dtnin-ID:NYRD-----AREAbn-QPEAKcms-TpeakDate\_bh:mm:---RVMn-R.C.---DWFcms  
 13554+ ROUTE CHANNEL -> 1.0 02:S,N12 9506.00 21.745 No\_date 32:41 34.08 n/a .000  
 13555+ [ROT= 1.001 out- 1.0 01:Dm1 9506.00 21.522 No\_date 32:57 34.08 n/a .000

13556+ [L/S/nv .972 / .054/.049] [Vmax=.777 Dmax= 3.194]  
 13557+ #  
 13558+ #  
 13559+ # Addition of Subwatershed 11 and Name Creek to Node 11  
 13560+ #  
 13561+ # R0100:CO0043-----Dtnin-ID:NYRD-----AREAbn-QPEAKcms-TpeakDate\_bh:mm:---RVMn-R.C.---DWFcms  
 13562+ ADD HYD 1.0 02:N12 1789.00 61.058 No\_date 38:16 37.16 n/a .000  
 13563+ \* 1.0 02:SW\_12 8376.00 36.118 No\_date 39:06 35.76 n/a .000  
 13564+ SUM+ 1.0 01:RS\_12 25985.00 96.054 No\_date 39:40 37.03 n/a .000

13565+ #  
 13566+ # Sum of hydrographs from Node 10 routed to Node 9  
 13567+ #  
 13568+ # R0100:CO0044-----Dtnin-ID:NYRD-----AREAbn-QPEAKcms-TpeakDate\_bh:mm:---RVMn-R.C.---DWFcms  
 13569+ ADD HYD 1.0 02:N12 11921.00 23.609 No\_date 38:19 34.62 n/a .000  
 13570+ \* 1.0 02:SW\_12 5906.00 37.663 No\_date 37:48 42.49 n/a .000  
 13571+ SUM+ 1.0 01:RS\_12 17889.00 61.058 No\_date 38:16 37.16 n/a .000

13572+ #  
 13573+ # R0100:CO0042-----Dtnin-ID:NYRD-----AREAbn-QPEAKcms-TpeakDate\_bh:mm:---RVMn-R.C.---DWFcms  
 13574+ SAVV HYD 1.0 01:RS\_12 17889.00 61.058 No\_date 38:16 37.16 n/a .000

13575+ frame H\_RSRR  
 13576+ remark:flow at S,N10 1.0 01:SW\_10  
 13577+ #  
 13578+ # Addition of Kings Creek to S,N10  
 13579+ #  
 13580+ # R0100:CO0043-----Dtnin-ID:NYRD-----AREAbn-QPEAKcms-TpeakDate\_bh:mm:---RVMn-R.C.---DWFcms  
 13581+ ADD HYD 1.0 02:N10 17889.00 61.058 No\_date 38:16 37.16 n/a .000  
 13582+ \* 1.0 02:SW\_10 8376.00 36.118 No\_date 39:06 35.76 n/a .000  
 13583+ SUM+ 1.0 01:RS\_10 25985.00 96.054 No\_date 39:40 37.03 n/a .000

13584+ #  
 13585+ # Sum of hydrographs from Node 10 routed to Node 9  
 13586+ #  
 13587+ # Section 2  
 13588+ #  
 13589+ # R0100:CO0044-----Dtnin-ID:NYRD-----AREAbn-QPEAKcms-TpeakDate\_bh:mm:---RVMn-R.C.---DWFcms  
 13590+ ADD HYD 1.0 02:N10 11921.00 23.609 No\_date 38:19 34.62 n/a .000  
 13591+ \* 1.0 02:SW\_10 5906.00 37.663 No\_date 37:48 42.49 n/a .000  
 13592+ SUM+ 1.0 01:RS\_10 25985.00 96.054 No\_date 39:40 37.03 n/a .000

13593+ #  
 13594+ # Sum of hydrographs from Node 10 routed to Node 9  
 13595+ #  
 13596+ # R0100:CO0045-----Dtnin-ID:NYRD-----AREAbn-QPEAKcms-TpeakDate\_bh:mm:---RVMn-R.C.---DWFcms  
 13597+ ADD HYD 1.0 02:N10 32869.00 94.262 No\_date 39:59 37.03 n/a .000  
 13598+ \* 1.0 02:SW\_10 1132.00 16.501 No\_date 30:52 40.89 n/a .000  
 13599+ SUM+ 1.0 02:NCK\_C 4464.00 18.060 No\_date 39:59 33.61 n/a .000  
 13600+ SHM+ 1.0 01:S,N10 31561.00 115.681 No\_date 39:59 36.68 n/a .000

13601+ #  
 13602+ # Sum of hydrographs from Node 9 routed to Node 8  
 13603+ #  
 13604+ # R0100:CO0046-----Dtnin-ID:NYRD-----AREAbn-QPEAKcms-TpeakDate\_bh:mm:---RVMn-R.C.---DWFcms  
 13605+ ADD HYD 1.0 02:N10 31561.00 115.681 No\_date 39:59 36.68 n/a .000  
 13606+ \* 1.0 02:SW\_10 31561.00 109.393 No\_date 39:59 36.68 n/a .000

13607+ [ROT= 1.001 out- 1.0 01:N10 31561.00 109.393 No\_date 39:59 36.68 n/a .000

13608+ [L/S/nv .2269 / .082/.025] [Vmax=.775 Dmax= 2.151]  
 13609+ #  
 13610+ # Addition of Subwatershed 9 and Nichols Creek to Node 9  
 13611+ #  
 13612+ # R0100:CO0047-----Dtnin-ID:NYRD-----AREAbn-QPEAKcms-TpeakDate\_bh:mm:---RVMn-R.C.---DWFcms  
 13613+ ADD HYD 1.0 02:N10 31561.00 109.393 No\_date 39:59 36.68 n/a .000  
 13614+ \* 1.0 02:SW\_10 31561.00 109.393 No\_date 39:59 36.68 n/a .000  
 13615+ SUM+ 1.0 01:RS\_10 31561.00 111.942 No\_date 44:52 36.68 n/a .000

13616+ #  
 13617+ # Sum of hydrographs from Node 8 routed to Node 7  
 13618+ #  
 13619+ # R0100:CO0048-----Dtnin-ID:NYRD-----AREAbn-QPEAKcms-TpeakDate\_bh:mm:---RVMn-R.C.---DWFcms  
 13620+ ADD HYD 1.0 02:N10 35546.00 111.942 No\_date 44:52 36.68 n/a .000  
 13621+ \* 1.0 02:SW\_10 35546.00 111.942 No\_date 38:28 36.76 n/a .000

13622+ #  
 13623+ # Addition of Subwatershed 8 and Hobbs's Drain to Node 7  
 13624+ #  
 13625+ # R0100:CO0049-----Dtnin-ID:NYRD-----AREAbn-QPEAKcms-TpeakDate\_bh:mm:---RVMn-R.C.---DWFcms  
 13626+ ADD HYD 1.0 02:N10 35546.00 111.942 No\_date 44:52 36.68 n/a .000  
 13627+ \* 1.0 02:SW\_10 35546.00 111.942 No\_date 38:28 36.76 n/a .000

13628+ #  
 13629+ # Sum of hydrographs from Node 7 routed to Node 6  
 13630+ #  
 13631+ # R0100:CO0046-----Dtnin-ID:NYRD-----AREAbn-QPEAKcms-TpeakDate\_bh:mm:---RVMn-R.C.---DWFcms  
 13632+ ADD HYD 1.0 02:N10 35546.00 111.942 No\_date 44:52 36.68 n/a .000  
 13633+ \* 1.0 02:SW\_10 35546.00 111.942 No\_date 38:28 36.76 n/a .000  
 13634+ SUM+ 1.0 01:RS\_10 35546.00 120.740 No\_date 43:36 36.11 n/a .000

13635+ #  
 13636+ # Storage area and volumes were estimated from available topo maps.  
 13637+ # Release rate from flow was assumed to be controlled by the downstream  
 13638+ # reach. This is a conservative assumption since the storage is large enough for up to  
 13639+ # 0.75% of water, the main channel of the river provided the storage. Above  
 13640+ # this depth, the wetland starts to significantly store water.  
 13641+ # this depth, the wetland starts to significantly store water.  
 13642+ #  
 13643+ # R0100:CO0051-----Dtnin-ID:NYRD-----AREAbn-QPEAKcms-TpeakDate\_bh:mm:---RVMn-R.C.---DWFcms  
 13644+ ADD HYD 1.0 02:N10 38743.00 62.067 No\_date 59:46 36.11 n/a .000  
 13645+ \* 1.0 02:SW\_10 38743.00 62.067 No\_date 59:46 36.11 n/a .000  
 13646+ SUM+ 1.0 02:VRD\_DR 1320.00 10.382 No\_date 59:10 42.12 n/a .000

13647+ SHM+ 1.0 01:RES\_RF 40240.01 62.114 No\_date 59:39 36.33 n/a .000

13648+ #  
 13649+ # frame H\_RSRR  
 13650+ remark:outflow of Richmond Fen  
 13651+ #  
 13652+ # Sum of hydrographs from Node 7 routed to Node 6  
 13653+ #  
 13654+ # Section 5  
 13655+ #  
 13656+ # R0100:CO0053-----Dtnin-ID:NYRD-----AREAbn-QPEAKcms-TpeakDate\_bh:mm:---RVMn-R.C.---DWFcms  
 13657+ ADD HYD 1.0 02:N10 38743.00 62.351 No\_date 58:25 36.11 n/a .000  
 13658+ \* 1.0 02:VRD\_RF 38743.00 62.351 No\_date 58:25 36.11 n/a .000  
 13659+ SUM+ 1.0 02:VRD\_RF 38743.00 62.067 No\_date 59:46 36.11 n/a .000

13660+ #  
 13661+ # Sum of hydrographs from Node 6 routed to Node 5  
 13662+ #  
 13663+ # Section 6







14961\* Major System / 1.0 02:JR-02-MJ .02 .087 No\_date 28:03 64.85 n/a .000

14962\* Minor System / 0.0 03:JR-02-MJ 1.57 .028 No\_date 27:41 65.24 n/a .000

14963\* [MSysCdt...1303-E03...TocDvVol...1755-E02...Mfref...1...TotSurf...]

14964\* R0100:CO253+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

14965\* ADD HYD + 1.0 02:JR-02-MJ .07 .086 No\_date 28:04 64.85 n/a .000

14966\* + 1.0 01:JR-02-S 1.57 .153 No\_date 27:44 65.23 n/a .000

14967\* SUM+ 1.0 01:JR-02-S 1.59 .240 No\_date 28:03 65.23 n/a .000

14968\* # Catchment FRASER

14969\* # - To Fraser-Clarke drain (north of the Jock)

14970\* # - Debris flow will assumed no imp.

14971\* # - 2020-12-17 All Fraser is undeveloped (Nashy)

14972\* # - 2020-12-17 Fraser area to 35.1 as measured from QGIS

14973\* # - 2020-12-17 Fraser area to 35.1 as measured from QGIS

14974\* # - [iBEC... 4.00: SMIN... 31.15: SMAX...207.66: SK... 010]

14975\* [InterEventTime... 12.00]

14976\* R0100:CO266+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

14977\* CONTINUOUS STANDHYD 1.0 01:FRASER-DRN 13.65 .837 No\_date 28:21 45.95 .519 .000

14978\* [IMPERVIOUS areas: IaIimp... 1.57:SLP1+1.00:LGM... 40.:MNP...-250:SCP... .0]

14979\* [IMPERVIOUS areas: IaIimp... 1.57:SLP1+1.00:LGM... 380.:MNP...-013:SCI... .0]

14980\* [SMIN... 26.32: SMAX...175.50: SK... 010]

14981\* CONTINUOUS STANDHYD 1.0 01:FRASER-D 21.61 4.106 No\_date 28:01 69.71 .787 .000

14982\* [XIMP...58:TIMP...58]

14983\* [IMPERVIOUS areas: IaIimp... 1.57:SLP1+1.00:LGM... 40.:MNP...-250:SCP... .0]

14984\* [Previous areas: IaIimp... 4.67:SLP1+1.00:LGM... 40.:MNP...-250:SCP... .0]

14985\* [IMPERVIOUS areas: IaIimp... 1.57:SLP1+1.00:LGM... 380.:MNP...-013:SCI... .0]

14986\* [SMIN... 26.32: SMAX...175.50: SK... 010]

14987\* R0100:CO266+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

14988\* CONTINUOUS STANDHYD 1.0 01:FRASER-D 23.64 .4106 No\_date 28:01 69.71 n/a .000

14989\* [IMPERVIOUS areas: IaIimp... 1.57:SLP1+1.00:LGM... 40.:MNP...-250:SCP... .0]

14990\* Major System / 1.0 02:FRASER-J 21.61 .4006 No\_date 27:51 69.88 n/a .000

14991\* Minor System / 1.0 03:FRASER-J 21.61 .2810 No\_date 27:51 69.88 n/a .000

14992\* [SMIN... 26.32: SMAX...175.50: SK... 010]

14993\* R0100:CO267+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

14994\* ADD HYD 1.0 02:FRASER-J 0.00 .000 No\_date 0:00 0.00 n/a .000

14995\* + 1.0 02:FRASER-J 21.61 .2810 No\_date 27:51 69.88 n/a .000

14996\* SUM+ 1.0 02:FRASER-J 21.61 .2810 No\_date 27:51 69.88 n/a .000

14997\* R0100:CO268+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

14998\* ADD HYD 1.0 02:FRASER-J 0.00 .000 No\_date 0:00 0.00 n/a .000

14999\* + 1.0 02:FRASER-J 21.61 .2810 No\_date 27:51 69.88 n/a .000

15000\* SUM+ 1.0 02:FRASER-J 21.61 .2810 No\_date 27:51 69.88 n/a .000

15001\* + 1.0 02:N\_KB 54279.43 143.629 No\_date 36:32 39.19 n/a .000

15002\* + 1.0 02:FC-01-S 8.03 .756 No\_date 27:49 54.46 n/a .000

15003\* + 1.0 02:FC-01-S 8.03 .756 No\_date 27:49 54.46 n/a .000

15004\* SUM+ 1.0 02:FC-01-S 8.03 .756 No\_date 27:49 54.46 n/a .000

15005\* + 1.0 02:FC-03-S 7.37 1.019 No\_date 28:00 64.90 n/a .000

15006\* SUM+ 1.0 01:4241 54688.52 144.306 No\_date 36:29 39.28 n/a .000

15007\* R0100:CO269+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

15008\* SAVE HYD 1.0 01:4241 54689.52 144.306 No\_date 36:29 39.28 n/a .000

15009\* frame: 4401.D100

15010\* remark:Total Flows at Ken-Burnett Outlet

15011\* # Hydrograph from Node Ken-Burnett to station 3633

15012\* # Channel X-Section obtained from RVEA Hydraulic Model - Station 4241

15013\* # Channel X-Section obtained from RVEA Hydraulic Model - Station 3633

15014\* R0100:CO270+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

15015\* R0100:CO271+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

15016\* [SLOT... 1.001: 01:4241 54688.52 144.306 No\_date 36:29 39.28 n/a .000

15017\* [L/S... 009. / 099. /095. ]

15018\* R0100:CO272+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

15019\* R0100:CO273+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

15020\* ADD HYD 1.0 02:4241-out 54688.52 144.351 No\_date 36:25 39.28 n/a .000

15021\* + 1.0 02:4241-out 54688.52 144.351 No\_date 36:25 39.28 n/a .000

15022\* + 1.0 02:4241-out 8.24 1.034 No\_date 28:06 64.95 n/a .000

15023\* + 1.0 02:4241-out 8.24 1.034 No\_date 28:06 64.95 n/a .000

15024\* SUM+ 1.0 02:4241-out 8.24 1.034 No\_date 28:06 64.95 n/a .000

15025\* R0100:CO272+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

15026\* SAVE HYD 1.0 01:SK\_EB\_0100

15027\* remark:H2O\_COMMENT...[Total Flows before Station 3633]

15028\* # Hydrograph from Station 3633 to Node Todd

15029\* # Channel X-Section obtained from RVEA Hydraulic Model - Station 3633

15030\* # Channel X-Section obtained from RVEA Hydraulic Model - Station 3633

15031\* # JFSA 2021-02-26 change the channel length (at station 3633) from 650m to 608m and change the slope from 0.0498% to 0.2

15032\* R0100:CO273+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

15033\* ROUTE CHANNEL > 1.0 01:N\_KB 54681.21 144.394 No\_date 36:25 39.29 n/a .000

15034\* [ROUTE... 1.001: 01:N\_KB 54681.21 144.394 No\_date 36:25 39.29 n/a .000

15035\* [ROUTE... 1.001: 01:N\_KB 54681.21 144.394 No\_date 36:30 39.29 n/a .000

15036\* [ROUTE... 1.001: 01:N\_KB 54681.21 144.394 No\_date 36:30 39.29 n/a .000

15037\* [ROUTE... 1.001: 01:N\_KB 54681.21 144.394 No\_date 36:30 39.29 n/a .000

15038\* # Catchment Greenbank

15039\* # - To Greenbank Drain (south of the Jock)

15040\* # - JFSA 2021-01-28 add Greenbank pond and set JFSA\_P588046-15.. June 2016

15041\* # - 2020-10-10 increase imp. by 43% to 475 ha to 56.6 ha based on CIS measurements

15042\* R0100:CO274+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

15043\* R0100:CO275+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

15044\* CONTINUOUS STANDHYD 1.0 01:Greenbank 36.64 .7069 No\_date 28:01 71.80 .811 .000

15045\* [XIMP... 64:TIMP... 68]

15046\* [IMPERVIOUS areas: IaIimp... 4.67:SLP1+1.00:LGM... 40.:MNP...-250:SCP... .0]

15047\* [IMPERVIOUS areas: IaIimp... 1.57:SLP1+1.00:LGM... 40.:MNP...-250:SCP... .0]

15048\* [IMPERVIOUS areas: IaIimp... 1.57:SLP1+1.00:LGM... 40.:MNP...-250:SCP... .0]

15049\* [IMPERVIOUS areas: IaIimp... 1.57:SLP1+1.00:LGM... 40.:MNP...-250:SCP... .0]

15050\* [IMPERVIOUS areas: IaIimp... 1.57:SLP1+1.00:LGM... 40.:MNP...-250:SCP... .0]

15051\* R0100:CO276+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

15052\* R0100:CO277+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

15053\* ROUTE RESERVEPIPE > 1.0 02:4241 54681.21 144.394 No\_date 36:30 39.29 n/a .000

15054\* [ROUTE... 1.001: 02:4241 54681.21 144.394 No\_date 36:30 39.29 n/a .000

15055\* [ROUTE... 1.001: 02:4241 54681.21 144.394 No\_date 36:30 39.29 n/a .000

15056\* [ROUTE... 1.001: 02:4241 54681.21 144.394 No\_date 36:30 39.29 n/a .000

15057\* R0100:CO276+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

15058\* ADD HYD 1.0 02:N\_TO 54681.21 144.359 No\_date 36:30 39.29 n/a .000

15059\* + 1.0 02:N\_TO 54681.21 144.359 No\_date 36:30 39.29 n/a .000

15060\* + 1.0 02:N\_TO 54681.21 144.359 No\_date 36:30 39.29 n/a .000

15061\* SUM+ 1.0 01:GEMB 54717.82 144.533 No\_date 36:30 39.32 n/a .000

15062\* R0100:CO277+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

15063\* SAVE HYD 1.0 01:GEMB 54717.82 144.533 No\_date 36:30 39.32 n/a .000

15064\* frame: Greenbank

15065\* # Catchment Greenbank

15066\* # Catchment Greenbank

15067\* # Catchments Todd

15068\* # Subdivision with 43% imp. as per Barrhaven South MSS

15069\* # - 2020-10-10 increase imp. based on P5981041-11

15070\* # - 2020-10-30 split Todd Draining Area to MAJOR, MINOR, POND and ALL

15071\* # - 2020-10-30 split Todd Draining Area to MAJOR, MINOR, POND and ALL

15072\* # - 2020-10-30 split Todd Draining Area to MAJOR, MINOR, POND and ALL

15073\* # - 2020-10-30 split Todd Draining Area to MAJOR, MINOR, POND and ALL

15074\* # - 2020-10-30 split Todd Draining Area to MAJOR, MINOR, POND and ALL

15075\* R0100:CO278+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

15076\* CONTINUOUS STANDHYD 1.0 01:TODD\_MN2 2.10 .428 No\_date 28:00 66.78 .754 .000

15077\* [ROUTE... 2 :CNM... 77.0]

15078\* [ROUTE... 2 :CNM... 77.0]

15079\* [ROUTE... 2 :CNM... 77.0]

15080\* [ROUTE... 2 :CNM... 77.0]

15081\* [ROUTE... 2 :CNM... 77.0]

15082\* [ROUTE... 2 :CNM... 77.0]

15083\* [ROUTE... 2 :CNM... 77.0]

15084\* [ROUTE... 2 :CNM... 77.0]

15085\* [ROUTE... 2 :CNM... 77.0]

15086\* [ROUTE... 2 :CNM... 77.0]

15087\* R0100:CO279+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

15088\* CONTINUOUS STANDHYD 1.0 01:TODD\_MN2 2.10 .428 No\_date 28:00 66.78 .754 .000

15089\* [ROUTE... 2 :CNM... 77.0]

15090\* [ROUTE... 2 :CNM... 77.0]

15091\* [ROUTE... 2 :CNM... 77.0]

15092\* [ROUTE... 2 :CNM... 77.0]

15093\* [ROUTE... 2 :CNM... 77.0]

15094\* [ROUTE... 2 :CNM... 77.0]

15095\* [ROUTE... 2 :CNM... 77.0]

15096\* [ROUTE... 2 :CNM... 77.0]

15097\* R0100:CO282+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

15098\* CONTINUOUS STANDHYD 1.0 01:TODD\_PDR 3.06 .669 No\_date 28:00 70.28 .794 .000

15099\* [ROUTE... 2 :CNM... 77.0]

15100\* [ROUTE... 2 :CNM... 77.0]

15101\* [ROUTE... 2 :CNM... 77.0]

15102\* [ROUTE... 2 :CNM... 77.0]

15103\* [ROUTE... 2 :CNM... 77.0]

15104\* [ROUTE... 2 :CNM... 77.0]

15105\* [ROUTE... 2 :CNM... 77.0]

15106\* [ROUTE... 2 :CNM... 77.0]

15107\* R0100:CO283+ Dtnin-ID:NHYD---ARRAhs-QPEAKms-Tpeakdate\_bh:mm---RVMn-R.C.---DWFcms

15108\* CONTINUOUS STANDHYD 1.0 01:TODD\_PDR 30.23 5.210 No\_date 28:00 66.65 .775 .000

15109\* [ROUTE... 2 :CNM... 77.0]

15110\* [ROUTE... 2 :CNM... 77.0]

15111\* [ROUTE... 2 :CNM... 77.0]

15112\* [ROUTE... 2 :CNM... 77.0]

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15709+ + 1.0 02:AI-MJ .00 .000 No\_date 0:00 .00 n/a .000  
 15710+ + 1.0 02:AI-MJ .05 .218 No\_date 28:06 57.73 n/a .000  
 15711+ + 1.0 02:AI-MJ .15 .144 No\_date 28:06 57.73 n/a .000  
 15712+ + 1.0 02:AI-2-MJ .23 .599 No\_date 28:06 62.88 n/a .000  
 15713+ + 1.0 02:AI-2-MJ .00 .000 No\_date 28:06 62.88 n/a .000  
 15714+ SUM- 1.0 01:SN\_MJ .00 .000 No\_date 36:37 39.46 n/a .000  
 15715+ R0100:CO0186-----Dtnin-ID:NHNYD---ARAhA-QPEAKcms-TpeakDate\_bh:mm---RVMm-R.C.---DWFcms  
 15716+ SUM- 0.00 .000 No\_date 36:37 39.46 n/a .000  
 15717+ frame corr1c\_0100  
 15718+ remark:Total Flows at Corrigan Pond  
 15719+ # Corrigan Pond 1  
 15720+ # - Rating curve obtained from Barrhaven South MESS modeling  
 15721+ # Tributary Drainage Area to MSS Pond 1 = 140 ha  
 15722+ #\*\*\*\*\*  
 15723+ # Hydrograph from Corrigan Branch routed to Jockvale Road  
 15724+ # Channel X-Section obtained from Rvca Hydraulic Model - Station 2462  
 15725+ #\*\*\*\*\*  
 15726+ R0100:CO0187-----Dtnin-ID:NHNYD---ARAhA-QPEAKcms-TpeakDate\_bh:mm---RVMm-R.C.---DWFcms  
 15727+ ROUTE CHANNEL -> 1.0 02:corr1c .55020.08 145.505 No\_date 36:37 39.46 n/a .000  
 15728+ [RDT: 1.00] out<= 1.0 01:N\_MJ 55020.08 145.490 No\_date 36:40 39.46 n/a .000  
 15729+ [XPM: 2.170] Dmax( 2.124)  
 15730+ #\*\*\*\*\*  
 15731+ # Catchment DESIRE  
 15732+ # - To SWM Facility north of the Jock  
 15733+ # - Primarily residential development  
 15734+ #\*\*\*\*\*  
 15735+ R0100:CO0188-----Dtnin-ID:NHNYD---ARAhA-QPEAKcms-TpeakDate\_bh:mm---RVMm-R.C.---DWFcms  
 15736+ CONTINUOUS STANNDY 1.0 01:NMILLS 175.99 20.390 No\_date 28:06 56.87 .642 .000  
 15737+ [L005: 2 CN: 74.0]  
 15738+ [Previous area: Iaper: 4.67|SLDP1:1.00|LGP: 40.|NNP: .250|SCP: .0]  
 15739+ [Inflow: 1.0 01:JCKVA-TO .000 No\_date 28:06 56.87 n/a .000  
 15740+ [iabcECmp: 4.00|IaRcpers: 4.00]  
 15741+ [SMIN: 36.67|SMAX:244.49: SK: .010]  
 15742+ #\*\*\*\*\*  
 15743+ # Chapman Mills SWM Pond  
 15744+ # - Rating curve obtained from Rvca hydraulic modeling  
 15745+ #\*\*\*\*\*  
 15746+ R0100:CO0189-----Dtnin-ID:NHNYD---ARAhA-QPEAKcms-TpeakDate\_bh:mm---RVMm-R.C.---DWFcms  
 15747+ ROUTE RESERVOIR -> 1.0 02:MILLS .55020.08 145.505 No\_date 36:37 39.46 n/a .000  
 15748+ out <= 1.0 02:MILLS .55020.08 145.505 No\_date 28:06 56.87 n/a .000  
 15749+ overflow <= 1.0 03:MLV .29 .77 16.228 No\_date 28:08 56.87 n/a .000  
 15750+ [Mgt:0.25ed: .21310=> m3\_TotVol:1.6993|Iabc:0.0000|IabcECmp:0.0000|IabcRcpers:0.0000]  
 15751+ ADD HYD 1.0 02:N\_MJ .00 .000 No\_date 36:40 2.700 hr  
 15752+ Dtnin-ID:NHNYD---ARAhA-QPEAKcms-TpeakDate\_bh:mm---RVMm-R.C.---DWFcms  
 15753+ ADD NHD 1.0 02:N\_MJ .29 .77 16.228 No\_date 28:08 56.87 n/a .000  
 15754+ R0100:CO0190-----Dtnin-ID:NHNYD---ARAhA-QPEAKcms-TpeakDate\_bh:mm---RVMm-R.C.---DWFcms  
 15755+ [KIND:50|TIME: 50]  
 15756+ [Previous area: Iaper: 4.67|SLDP1:1.00|LGP: 40.|NNP: .250|SCP: .0]  
 15757+ [Inflow: 1.0 01:JCKVA-TO .000 No\_date 36:37 39.51 n/a .000  
 15758+ [L/S/nr: 1962 / .223/.045]  
 15759+ [iabcECmp: 4.00|IaRcpers: 4.00]  
 15760+ #\*\*\*\*\*  
 15761+ # Save HYD 1.0 01:SN\_MJ .55036.07 146.141 No\_date 36:39 39.51 n/a .000  
 15762+ frame :SN\_MJ\_0100  
 15763+ remark:Total Flows at Jockvale Road  
 15764+ #\*\*\*\*\*  
 15765+ # Hydrograph from Jockvale Road routed to Heart's Desire  
 15766+ # Channel X-section obtained from Rvca Hydraulic Model - Station 689  
 15767+ #\*\*\*\*\*  
 15768+ R0100:CO0192-----Dtnin-ID:NHNYD---ARAhA-QPEAKcms-TpeakDate\_bh:mm---RVMm-R.C.---DWFcms  
 15769+ ROUTE RESERVOIR -> 1.0 02:SN\_MJ .55036.07 146.141 No\_date 36:39 39.51 n/a .000  
 15770+ [RDT: 1.00] out<= 1.0 01:N\_MJ 55036.07 146.839 No\_date 36:54 39.51 n/a .000  
 15771+ [L/S/nr: 1962 / .223/.045]  
 15772+ [iabcECmp: 4.00|IaRcpers: 4.00]  
 15773+ #\*\*\*\*\*  
 15774+ # Catchment DESIRE  
 15775+ # - To Jockvale Road (north of the Jock)  
 15776+ # - Rural-estate subdivision (Heart's Desire Community)  
 15777+ #\*\*\*\*\*  
 15778+ R0100:CO0193-----Dtnin-ID:NHNYD---ARAhA-QPEAKcms-TpeakDate\_bh:mm---RVMm-R.C.---DWFcms  
 15779+ CONTINUOUS STANNDY 1.0 01:DESIRE 25.79 3.004 No\_date 28:03 93.11 .400 .000  
 15780+ [XPM: 25|TIME: 25]  
 15781+ [Previous area: Iaper: 4.67|SLDP1:1.00|LGP: 40.|NNP: .250|SCP: .0]  
 15782+ [Inflow: 1.0 01:JCKVA-TO .000 No\_date 28:03 93.11 n/a .000  
 15783+ [iabcECmp: 4.00|IaRcpers: 4.00]  
 15784+ [SMIN: 31.15|SMAX:207.66: SK: .010]  
 15785+ #\*\*\*\*\*  
 15786+ # Catchment JOCKVA  
 15787+ # - To Jockvale SWM Facility  
 15788+ # - Residential development, golf course  
 15789+ # - Residential development, golf course  
 15790+ # - Residential development, golf course after updating CORRIG as per IGI Group, July 2008  
 15791+ # - JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX-LAND 32.5 ha as per IGI Group, July 2008  
 15792+ #\*\*\*\*\*  
 15793+ R0100:CO0194-----Dtnin-ID:NHNYD---ARAhA-QPEAKcms-TpeakDate\_bh:mm---RVMm-R.C.---DWFcms  
 15794+ CONTINUOUS STANNDY 1.0 01:JOCKVA .225.13 28.623 No\_date 28:07 62.70 .708 .000  
 15795+ [KIND:50|TIME: 50]  
 15796+ [Previous area: Iaper: 4.67|SLDP1:1.00|LGP: 40.|NNP: .250|SCP: .0]  
 15797+ [Inflow: 1.0 01:JOCKVA-TO .000 No\_date 28:07 62.70 n/a .000  
 15798+ [iabcECmp: 4.00|IaRcpers: 4.00]  
 15799+ [SMIN: 36.67|SMAX:244.49: SK: .010]  
 15800+ #\*\*\*\*\*  
 15801+ R0100:CO0195-----Dtnin-ID:NHNYD---ARAhA-QPEAKcms-TpeakDate\_bh:mm---RVMm-R.C.---DWFcms  
 15802+ ADD HYD 1.0 02:EX-LAND\_NN .30 .73 2.275 No\_date 27:48 62.82 n/a .000  
 15803+ + 1.0 02:BI-MT .30 .820 No\_date 28:05 62.88 n/a .000  
 15804+ + 1.0 02:BI-MT .30 .149 No\_date 28:05 62.88 n/a .000  
 15805+ + 1.0 02:BI-MT .00 .000 No\_date 28:05 62.88 n/a .000  
 15806+ SUM- 1.0 01:JOCKVA-TO .256.41 31.850 No\_date 28:06 62.71 n/a .000  
 15807+ frame :JOCKVA-TO .256.41 31.850 No\_date 28:06 62.71 n/a .000  
 15808+ frame :HYD .256.41 31.850 No\_date 28:06 62.71 n/a .000  
 15809+ frame :NOH .256.41 31.850 No\_date 28:06 62.71 n/a .000  
 15810+ frame :NOH .256.41 31.850 No\_date 28:06 62.71 n/a .000  
 15811+ #\*\*\*\*\*  
 15812+ # Jockvale SWM Facility  
 15813+ # - Residential development from Jockvale Servicing Study (CCL 1988)  
 15814+ #\*\*\*\*\*  
 15815+ R0100:CO0197-----Dtnin-ID:NHNYD---ARAhA-QPEAKcms-TpeakDate\_bh:mm---RVMm-R.C.---DWFcms  
 15816+ ROUTE RESERVOIR -> 1.0 01:JOCKVA-TO .000 No\_date 28:07 62.70 n/a .000  
 15817+ out <= 1.0 01:JOCK\_P .256.41 12.890 No\_date 28:35 64.71 n/a .000  
 15818+ overflow <= 1.0 03:JOCK\_P .00 .000 No\_date 0:00 0:00 n/a .000  
 15819+ [Mgt:0.25ed: .64304=> m3\_TotVol:1.0000|m3\_Rcpers:0.0000|m3\_Ecmp:0.0000]  
 15820+ R0100:CO0198-----Dtnin-ID:NHNYD---ARAhA-QPEAKcms-TpeakDate\_bh:mm---RVMm-R.C.---DWFcms  
 15821+ ADD HYD 1.0 02:HDE .00 .000 No\_date 28:07 62.70 n/a .000  
 15822+ + 1.0 02:BI-MT .25 .149 No\_date 28:05 62.70 n/a .000  
 15823+ + 1.0 02:BI-MT .00 .000 No\_date 28:05 62.70 n/a .000  
 15824+ + 1.0 02:JOCK\_P .256.41 12.890 No\_date 28:35 64.71 n/a .000  
 15825+ + 1.0 02:JOCK\_P .00 .000 No\_date 28:35 64.71 n/a .000  
 15826+ SUM- 1.0 01:JOCKVA-TO .256.41 31.850 No\_date 28:06 62.71 n/a .000  
 15827+ frame :HYD .256.41 31.850 No\_date 28:06 62.71 n/a .000  
 15828+ frame :SN\_MJ\_0100 1.0 01:SN\_MJ .55076.46 146.840 No\_date 36:52 39.63 n/a .000  
 15829+ remark:Total Flows at Heart's Desire  
 15830+ #\*\*\*\*\*  
 15831+ # Hydrograph from Heart's Desire routed to Rideau River  
 15832+ # Channel X-section obtained from Rvca Hydraulic Model - Station 0  
 15833+ #\*\*\*\*\*  
 15834+ R0100:CO0400-----Dtnin-ID:NHNYD---ARAhA-QPEAKcms-TpeakDate\_bh:mm---RVMm-R.C.---DWFcms  
 15835+ ROUTE CHANNEL -> 1.0 02:SN\_DE .55476.26 146.840 No\_date 36:52 39.63 n/a .000  
 15836+ [RDT: 1.00] out<= 1.0 01:SN\_DE 55476.26 146.826 No\_date 36:55 39.63 n/a .000  
 15837+ [L/S/nr: 1962 / .967/.045]  
 15838+ [Vmax: 2.218] Dmax( 1.328)  
 15839+ #\*\*\*\*\*  
 15840+ # Catchment G-3  
 15841+ # - To Jock River (north and south)  
 15842+ # - Undeveloped land and river  
 15843+ #\*\*\*\*\*  
 15844+ R0100:CO0401-----Dtnin-ID:NHNYD---ARAhA-QPEAKcms-TpeakDate\_bh:mm---RVMm-R.C.---DWFcms  
 15845+ CONTINUOUS STANNDY 1.0 01:SN\_DE 102.94 5.685 No\_date 28:20 40.95 .462 .000  
 15846+ [CN: 72.01|N: 3.00|Tp: 40]  
 15847+ [iabcECmp: 4.00|SMIN: 39.75|SMAX:244.39: SK: .010]  
 15848+ [InterEventTime: 12.00]  
 15849+ R0100:CO0402-----Dtnin-ID:NHNYD---ARAhA-QPEAKcms-TpeakDate\_bh:mm---RVMm-R.C.---DWFcms  
 15850+ ADD HYD 1.0 02:NLI .55476.26 146.826 No\_date 36:55 39.63 n/a .000  
 15851+ + 1.0 02:BI-MT .10 .000 No\_date 28:05 59.73 n/a .000  
 15852+ SUM- 1.0 01:SN\_MJ .55579.20 147.102 No\_date 36:55 39.63 n/a .000  
 15853+ R0100:CO0403-----Dtnin-ID:NHNYD---ARAhA-QPEAKcms-TpeakDate\_bh:mm---RVMm-R.C.---DWFcms  
 15854+ SUM- 1.0 01:SN\_MJ .55579.20 147.102 No\_date 36:55 39.63 n/a .000  
 15855+ frame :SN\_MJ\_0100 .000 No\_date 36:55 39.63 n/a .000  
 15856+ remark:Total Flows at Rideau River  
 15857+ #\*\*\*\*\*  
 15858+ R0100:CO0002 FINISH  
 15859+ #\*\*\*\*\*  
 15860+ #\*\*\*\*\*  
 15861+ #\*\*\*\*\*  
 15862+ # WARNINGS / ERRORS / NOTES  
 15863+ #\*\*\*\*\*  
 15864+ R0002:CO0283 ROUTE RESERVOIR  
 15865+ \*\*\* WARNING: Inflow peak was not reduced! Check OUTFLOW/STORAGE table or reduce DT.  
 15866+ \*\*\* WARNING: New pipe size used for routing.  
 15867+ \*\*\* WARNING: New pipe size used for routing.  
 15868+ R0002:CO0311 ROUTE PIPE ->  
 15869+ \*\*\* WARNING: New pipe size used for routing.  
 15870+ R0002:CO0344 DIVERT HYD ->  
 15871+ \*\*\* NOTE: Inflow hyd. is dry and cannot be diverted.  
 15872+ \*\*\* WARNING: New pipe size used for routing.  
 15873+ \*\*\* WARNING: New pipe size used for routing.  
 15874+ R0002:CO0352 ROUTE PIPE ->  
 15875+ \*\*\* WARNING: New pipe size used for routing.  
 15876+ R0002:CO0359 ROUTE PIPE ->  
 15877+ \*\*\* WARNING: New pipe size used for routing.  
 15878+ R0002:CO0364 ROUTE PIPE ->  
 15879+ \*\*\* WARNING: New pipe size used for routing.  
 15880+ R0002:CO0371 ROUTE PIPE ->  
 15881+ \*\*\* WARNING: New pipe size used for routing.  
 15882+ R0002:CO0372 ROUTE PIPE ->  
 15883+ \*\*\* WARNING: New pipe size used for routing.  
 15884+ R0002:CO0378 ROUTE PIPE ->  
 15885+ \*\*\* WARNING: New pipe size used for routing.  
 15886+ R0002:CO0386 ROUTE PIPE ->  
 15887+ \*\*\* WARNING: New pipe size used for routing.  
 15888+ R0002:CO0387 ROUTE PIPE ->  
 15889+ \*\*\* WARNING: New pipe size used for routing.  
 15890+ R0002:CO0388 ROUTE PIPE ->  
 15891+ \*\*\* WARNING: New pipe size used for routing.  
 15892+ R0002:CO0389 ROUTE PIPE ->  
 15893+ \*\*\* WARNING: New pipe size used for routing.  
 15894+ R0002:CO0390 ROUTE PIPE ->  
 15895+ \*\*\* WARNING: New pipe size used for routing.  
 15896+ R0002:CO0391 ROUTE PIPE ->  
 15897+ \*\*\* WARNING: New pipe size used for routing.  
 15898+ R0002:CO0392 ROUTE PIPE ->  
 15899+ \*\*\* WARNING: New pipe size used for routing.  
 15900+ R0002:CO0393 ROUTE PIPE ->  
 15901+ \*\*\* WARNING: New pipe size used for routing.  
 15902+ R0002:CO0394 ROUTE PIPE ->  
 15903+ \*\*\* WARNING: New pipe size used for routing.  
 15904+ Simulation ended on 2021-03-04 at 13:57:06

# Attachment E

Model 4B – Jock River Reach One Future Conditions – With SWM controls

JFSA, 2021

SWMHYMO Input & Summary files

```

1      20      Metric units / ID numbers OFF
2      *#*****SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
3      *#*****SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
4      *#*****SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
5      *# Project Name: [Jock River]      Project Number: [1474-16]
6      *# Date        : 04-03-2021
7      *# Modeler     : [M.M.]
8      *# Company     : JFSAinc.
9      *# License #   : 2549237
10     *#*****SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
11     *# CALIBRATION OF SUMMER MODEL PARAMETERS
12     *# USING CONTINUOUS SIMULATIONS
13     *# Rainfall data from JFSA raingauge installed at site + other gauges by the City
14     *# Use data collected from May 1st to July 14, 2003
15     *# 2020-11-30 change TMJSTO in COMPUTE DUALHYD (TMJSTO = 0.1 instead of 0.0001)
16     *# 2020-12-01 correct pond curve values
17     *# 2020-12-01 change W_CLAR_BRAZ XIMP to 0.55, SLPI=[0.5](%) (impervious slope), and
18     LGI up to 700m
19     *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 2462 (NHYDout=["N_TO"]
20     ,NHYDin=["SN_TO"]) from 0.033 % (as per Stantec Report 2007) to 0.05 % so the model
21     will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELS
22     aren't well suited to really flat slopes.
23     *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHYDout=["N_WC"]
24     ,NHYDin=["SN_CE"]) from 0.01 % (as per Stantec Report 2007) to 0.0255 % so the model
25     will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELS
26     aren't well suited to really flat slopes.
27     *
28     * Calibrated parameters for Summer 2003 data: APII=50, APIK=0.85, CN=varies,
29     *                                              SK=0.01, InterEventTime=12,
30     *                                              GWResk=0.96, VHydCond=0.055
31     *
32     *# -----
33     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
34     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
35     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
36     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
37     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
38     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
39     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
40     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
41     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
42     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
43     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
44     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
45     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
46     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
47     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
48     *#
49     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
50     *# of 1.32
51     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
52     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
53     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
54     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
55     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
56     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
57     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
58     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
59     *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|

```

```

60          BaseFlowOption=[1] ,
61          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
62          VHydCond=[0.055](mm/hr), END=-1
63 *%-----+-----+
64 *#
65 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
66 *# of 1.32
67 *%-----+-----|
68 CONTINUOUS NASHYD      NHYD=[ "SW_13" ], DT=[1]min, AREA=[ 971 ](ha),
69          DWF=[ 0 ](cms), CN/C=[ 61 ], IA=[ 2.5 ](mm),
70          N=[ 3.0 ], TP=[ 3.76 ]hrs,
71          Continuous simulation parameters:
72          IaRECper=[ 4 ](hrs),
73          SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
74          InterEventTime=[ 12 ](hrs)
75          Baseflow simulation parameters:
76          BaseFlowOption=[ 1 ],
77          InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
78          VHydCond=[ 0.055 ](mm/hr), END=-1
79 *%-----+-----|
80 *#
81 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
82 *# of 1.80
83 *%-----+-----|
84 CONTINUOUS NASHYD      NHYD=[ "JR_GWM" ], DT=[1]min, AREA=[ 3074 ](ha),
85          DWF=[ 0 ](cms), CN/C=[ 55 ], IA=[ 2.5 ](mm),
86          N=[ 3 ], TP=[ 11.33 ]hrs,
87          Continuous simulation parameters:
88          IaRECper=[ 4 ](hrs),
89          SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
90          InterEventTime=[ 12 ](hrs)
91          Baseflow simulation parameters:
92          BaseFlowOption=[ 1 ],
93          InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
94          VHydCond=[ 0.055 ](mm/hr), END=-1
95 *%-----+-----|
96 CONTINUOUS NASHYD      NHYD=[ "JR_ASH" ], DT=[1]min, AREA=[ 1781 ](ha),
97          DWF=[ 0 ](cms), CN/C=[ 72 ], IA=[ 2.5 ](mm),
98          N=[ 3.0 ], TP=[ 3.91 ]hrs,
99          Continuous simulation parameters:
100         IaRECper=[ 4 ](hrs),
101         SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
102         InterEventTime=[ 12 ](hrs)
103         Baseflow simulation parameters:
104         BaseFlowOption=[ 1 ],
105         InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
106         VHydCond=[ 0.055 ](mm/hr), END=-1
107 *%-----+-----|
108 CONTINUOUS NASHYD      NHYD=[ "SW_11" ], DT=[1]min, AREA=[ 500 ](ha),
109          DWF=[ 0 ](cms), CN/C=[ 66 ], IA=[ 2.5 ](mm),
110          N=[ 3.0 ], TP=[ 1.24 ]hrs,
111          Continuous simulation parameters:
112          IaRECper=[ 4 ](hrs),
113          SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
114          InterEventTime=[ 12 ](hrs)
115          Baseflow simulation parameters:
116          BaseFlowOption=[ 1 ],
117          InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
118          VHydCond=[ 0.055 ](mm/hr), END=-1
119 *%-----+-----|
120 *#
121 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
122 *# of 1.80
123 *%-----+-----|
124 CONTINUOUS NASHYD      NHYD=[ "NN_CK" ], DT=[1]min, AREA=[ 1917 ](ha),
125          DWF=[ 0 ](cms), CN/C=[ 66 ], IA=[ 2.5 ](mm),

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```

126      N=[3.0], TP=[5.29]hrs,
127      Continuous simulation parameters:
128      IaRECper=[4](hrs),
129      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
130      InterEventTime=[12](hrs)
131      Baseflow simulation parameters:
132      BaseFlowOption=[1] ,
133      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
134      VHydCond=[0.055](mm/hr), END=-1
135      *%-----|-----|
136      *#
137      *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
138      *# of 1.52
139      *%-----|-----|
140      CONTINUOUS NASHYD      NHYD=[ "SW_10" ], DT=[1]min, AREA=[5666](ha),
141      DWF=[0](cms), CN/C=[72], IA=[2.5](mm),
142      N=[3.0], TP=[8.00]hrs,
143      Continuous simulation parameters:
144      IaRECper=[4](hrs),
145      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
146      InterEventTime=[12](hrs)
147      Baseflow simulation parameters:
148      BaseFlowOption=[1] ,
149      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
150      VHydCond=[0.055](mm/hr), END=-1
151      *%-----|-----|
152      *#
153      *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
154      *# of 1.75
155      *%-----|-----|
156      CONTINUOUS NASHYD      NHYD=[ "KG_CK" ], DT=[1]min, AREA=[8376](ha),
157      DWF=[0](cms), CN/C=[66], IA=[2.5](mm),
158      N=[3.0], TP=[11.66]hrs,
159      Continuous simulation parameters:
160      IaRECper=[4](hrs),
161      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
162      InterEventTime=[12](hrs)
163      Baseflow simulation parameters:
164      BaseFlowOption=[1] ,
165      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
166      VHydCond=[0.055](mm/hr), END=-1
167      *%-----|-----|
168      *#
169      *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
170      *# of 1.68
171      *%-----|-----|
172      CONTINUOUS NASHYD      NHYD=[ "SW_9" ], DT=[1]min, AREA=[1132](ha),
173      DWF=[0](cms), CN/C=[70], IA=[2.5](mm),
174      N=[3.0], TP=[2.51]hrs,
175      Continuous simulation parameters:
176      IaRECper=[4](hrs),
177      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
178      InterEventTime=[12](hrs)
179      Baseflow simulation parameters:
180      BaseFlowOption=[1] ,
181      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
182      VHydCond=[0.055](mm/hr), END=-1
183      *%-----|-----|
184      *#
185      *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
186      *# of 1.82
187      *%-----|-----|
188      CONTINUOUS NASHYD      NHYD=[ "NC_CK" ], DT=[1]min, AREA=[4464](ha),
189      DWF=[0](cms), CN/C=[62], IA=[2.5](mm),
190      N=[3.0], TP=[11.32]hrs,
191      Continuous simulation parameters:

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192
193     IaRECper=[4](hrs),
194     SMIN=[-1](mm),   SMAX=[-1](mm),  SK=[0.010]/(mm),
195     InterEventTime=[12](hrs)
196     Baseflow simulation parameters:
197     BaseFlowOption=[1] ,
198     InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
199     VHydCond=[0.055](mm/hr),    END=-1
200
201 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
202 *# of 1.80
203
204 CONTINUOUS NASHYD      NHYD=[ "SW_8" ], DT=[1]min, AREA=[131](ha),
205     DWF=[0](cms),  CN/C=[63],  IA=[2.5](mm),
206     N=[3.0],  TP=[0.90]hrs,
207     Continuous simulation parameters:
208     IaRECper=[4](hrs),
209     SMIN=[-1](mm),   SMAX=[-1](mm),  SK=[0.010]/(mm),
210     InterEventTime=[12](hrs)
211     Baseflow simulation parameters:
212     BaseFlowOption=[1] ,
213     InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
214     VHydCond=[0.055](mm/hr),    END=-1
215
216 *#
217 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
218 *# of 1.65
219
220 CONTINUOUS NASHYD      NHYD=[ "HB_DR" ], DT=[1]min, AREA=[3854](ha),
221     DWF=[0](cms),  CN/C=[66],  IA=[2.5](mm),
222     N=[3.0],  TP=[8.42]hrs,
223     Continuous simulation parameters:
224     IaRECper=[4](hrs),
225     SMIN=[-1](mm),   SMAX=[-1](mm),  SK=[0.010]/(mm),
226     InterEventTime=[12](hrs)
227     Baseflow simulation parameters:
228     BaseFlowOption=[1] ,
229     InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
230     VHydCond=[0.055](mm/hr),    END=-1
231
232 *#
233 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
234 *# of 1.82
235
236 CONTINUOUS NASHYD      NHYD=[ "SW_7" ], DT=[1]min, AREA=[3197](ha),
237     DWF=[0](cms),  CN/C=[57],  IA=[2.5](mm),
238     N=[3.0],  TP=[6.65]hrs,
239     Continuous simulation parameters:
240     IaRECper=[4](hrs),
241     SMIN=[-1](mm),   SMAX=[-1](mm),  SK=[0.010]/(mm),
242     InterEventTime=[12](hrs)
243     Baseflow simulation parameters:
244     BaseFlowOption=[1] ,
245     InitGWResVol=[50](mm),  GWResK=[0.96](mm/day/mm)
246     VHydCond=[0.055](mm/hr),    END=-1
247
248 *#
249 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
250 *# of 1.75
251
252 CONTINUOUS NASHYD      NHYD=[ "SW_6" ], DT=[1]min, AREA=[165](ha),
253     DWF=[0](cms),  CN/C=[67],  IA=[2.5](mm),
254     N=[3.0],  TP=[4.18]hrs,
255     Continuous simulation parameters:
256     IaRECper=[4](hrs),
257     SMIN=[-1](mm),   SMAX=[-1](mm),  SK=[0.010]/(mm),

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```

258
259
260
261
262
263 *%-----|-----|
264 *#
265 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
266 *# of 1.67
267 *%-----|-----|
268 CONTINUOUS NASHYD NHYD= ["VG_DR"], DT=[1]min, AREA=[1332](ha),
269 DWF=[0](cms), CN/C=[72], IA=[2.5](mm),
270 N=[3.0], TP=[5.95]hrs,
271 Continuous simulation parameters:
272 IaRECper=[4](hrs),
273 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
274 InterEventTime=[12](hrs)
275 Baseflow simulation parameters:
276 BaseFlowOption=[1],
277 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
278 VHydCond=[0.055](mm/hr), END=-1
279 *%-----|-----|
280 CONTINUOUS NASHYD NHYD= ["SW_5"], DT=[1]min, AREA=[224](ha),
281 DWF=[0](cms), CN/C=[77], IA=[2.5](mm),
282 N=[3.0], TP=[0.75]hrs,
283 Continuous simulation parameters:
284 IaRECper=[4](hrs),
285 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
286 InterEventTime=[12](hrs)
287 Baseflow simulation parameters:
288 BaseFlowOption=[1],
289 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
290 VHydCond=[0.055](mm/hr), END=-1
291 *%-----|-----|
292 *#
293 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
294 *# of 1.20
295 *%-----|-----|
296 CONTINUOUS NASHYD NHYD= ["FL_CK"], DT=[1]min, AREA=[4945](ha),
297 DWF=[0](cms), CN/C=[74], IA=[2.5](mm),
298 N=[3.0], TP=[4.45]hrs,
299 Continuous simulation parameters:
300 IaRECper=[4](hrs),
301 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
302 InterEventTime=[12](hrs)
303 Baseflow simulation parameters:
304 BaseFlowOption=[1],
305 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
306 VHydCond=[0.055](mm/hr), END=-1
307 *%-----|-----|
308 CONTINUOUS NASHYD NHYD= ["SW_5A2"], DT=[1]min, AREA=[20](ha),
309 DWF=[0](cms), CN/C=[81], IA=[2.5](mm),
310 N=[3.0], TP=[0.62]hrs,
311 Continuous simulation parameters:
312 IaRECper=[4](hrs),
313 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
314 InterEventTime=[12](hrs)
315 Baseflow simulation parameters:
316 BaseFlowOption=[1],
317 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
318 VHydCond=[0.055](mm/hr), END=-1
319 *%-----|-----|
320 *#
321 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
322 *# of 1.61
323 *%-----|-----|

```

```

324 CONTINUOUS NASHYD NHYD=[ "SW_5A1" ], DT=[1]min, AREA=[1412](ha),
325 DWF=[0](cms), CN/C=[75], IA=[2.5](mm),
326 N=[3.0], TP=[8.00]hrs,
327 Continuous simulation parameters:
328 IaRECper=[4](hrs),
329 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
330 InterEventTime=[12](hrs)
331 Baseflow simulation parameters:
332 BaseFlowOption=[1],
333 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
334 VHydCond=[0.055](mm/hr), END=-1
335 *%
336 CONTINUOUS NASHYD NHYD=[ "SW_4" ], DT=[1]min, AREA=[585](ha),
337 DWF=[0](cms), CN/C=[81], IA=[2.5](mm),
338 N=[3.0], TP=[1.75]hrs,
339 Continuous simulation parameters:
340 IaRECper=[4](hrs),
341 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
342 InterEventTime=[12](hrs)
343 Baseflow simulation parameters:
344 BaseFlowOption=[1],
345 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
346 VHydCond=[0.055](mm/hr), END=-1
347 *%
348 CONTINUOUS NASHYD NHYD=[ "LM_CK" ], DT=[1]min, AREA=[1021](ha),
349 DWF=[0](cms), CN/C=[80], IA=[2.5](mm),
350 N=[3.0], TP=[2.46]hrs,
351 Continuous simulation parameters:
352 IaRECper=[4](hrs),
353 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
354 InterEventTime=[12](hrs)
355 Baseflow simulation parameters:
356 BaseFlowOption=[1],
357 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
358 VHydCond=[0.055](mm/hr), END=-1
359 *%
360 CONTINUOUS NASHYD NHYD=[ "SW_2" ], DT=[1]min, AREA=[177](ha),
361 DWF=[0](cms), CN/C=[77], IA=[2.5](mm),
362 N=[3.0], TP=[0.75]hrs,
363 Continuous simulation parameters:
364 IaRECper=[4](hrs),
365 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
366 InterEventTime=[12](hrs)
367 Baseflow simulation parameters:
368 BaseFlowOption=[1],
369 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
370 VHydCond=[0.055](mm/hr), END=-1
371 *%
372 CONTINUOUS NASHYD NHYD=[ "SM_DR" ], DT=[1]min, AREA=[1122](ha),
373 DWF=[0](cms), CN/C=[81], IA=[2.5](mm),
374 N=[3.0], TP=[3.25]hrs,
375 Continuous simulation parameters:
376 IaRECper=[4](hrs),
377 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
378 InterEventTime=[12](hrs)
379 Baseflow simulation parameters:
380 BaseFlowOption=[1],
381 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
382 VHydCond=[0.055](mm/hr), END=-1
383 *%
384 CONTINUOUS NASHYD NHYD=[ "MO_DR" ], DT=[1]min, AREA=[2737](ha),
385 DWF=[0](cms), CN/C=[76], IA=[2.5](mm),
386 N=[3.0], TP=[3.03]hrs,
387 Continuous simulation parameters:
388 IaRECper=[4](hrs),
389 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),

```

```

390
391     InterEventTime=[12](hrs)
392     Baseflow simulation parameters:
393     BaseFlowOption=[1] ,
394     InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
395     VHydCond=[0.055](mm/hr), END=-1
396 *%-----|-----
397 *      -JFSA 2020 replaced SW_1 with a detailed model from Stantec Report 2007
398 *CONTINUOUS NASHYD   NHYD=[ "SW_1" ], DT=[1]min, AREA=[3176](ha),
399 *          DWF=[0](cms), CN/C=[78], IA=[2.5](mm),
400 *          N=[3.0], TP=[3.56]hrs,
401 *          Continuous simulation parameters:
402 *          IaRECper=[4](hrs),
403 *          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
404 *          InterEventTime=[12](hrs)
405 *          Baseflow simulation parameters:
406 *          BaseFlowOption=[1] ,
407 *          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
408 *          VHydCond=[0.055](mm/hr), END=-1
409 *%-----|-----
410 *#
411 *# Routing hydrographs
412 *# Starting with the addition of Jock River Headwater and Subwatershed 13
413 *#
414 ADD HYD           NHYDsum=[ "S_N13" ], NHYDs to add=[ "JR_HW"+"SW_13" ]
415 *%-----|-----
416 *#
417 *# Sum of hydrographs from Node 13 routed to Node 13A
418 *# (Approximated cross-section - see cross-section 258)
419 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
420 *#
421 ROUTE CHANNEL      NHYDout=[ "N13A" ] ,NHYDin=[ "S_N13" ],
422             RDT=[1](min),
423             CHLGTH=[ 9074 ](m), CHSLOPE=[ 0.0220 ](%),
424             FPSLOPE=[ 0.0220 ](%),
425             SECNUM=[ 1.0 ], NSEG=[ 1 ]
426             ( SEGROUGH, SEGDIST (m) )=[ 0.04, 15.5 ] NSEG times
427             ( DISTANCE (m), ELEVATION (m) )=
428                 [-40, 132.5]
429                 [-30, 132]
430                 [-25, 131.5]
431                 [-13, 130]
432                 [-8, 127.00]
433                 [-7, 126.50]
434                 [-6, 126]
435                 [-5.5, 125.50]
436                 [0, 123.75]
437                 [4.5, 125.50]
438                 [6, 126]
439                 [7.5, 126.5]
440                 [9, 127]
441                 [10, 127.5]
442                 [11.5, 128.0]
443                 [15.5, 129.5]
444 *%-----|-----
445 *#
446 *# Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
447 *#
448 ADD HYD           NHYDsum=[ "SN13A" ], NHYDs to add=[ "N13A"+"JR_GWM" ]
449 *%-----|-----
450 *#
451 *# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
452 *#
453 ROUTE RESERVOIR    NHYDout=[ "RES_GM" ] ,NHYDin=[ "SN13A" ],
454             RDT=[1](min),
455             TABLE of ( OUTFLOW-STORAGE ) values

```

```

456          (cms) - (ha-m)
457          [ 0.0 , 0.0 ]
458          [1.991, 2.144 ]
459          [2.693, 39.826 ]
460          [3.509, 81.697 ]
461          [4.578, 318.774 ]
462          [5.647, 594.947 ]
463          [7.109, 910.219 ]
464          [8.616, 1264.589 ]
465          [10.371, 1658.057 ]
466          [12.402, 2090.622 ]
467          [22.056, 3462.487 ]
468          [ -1 , -1 ] (max twenty pts)
469      NHYDovf=[ " " ] ,
470 *%-----|-----|
471 *#
472 SAVE HYD          NHYD=[ "RES_GM" ], # OF PCYCLES=[-1], ICASEsh=[-1]
473          HYD_FILENAME=[ "H_ESGM" ]
474          HYD_COMMENT=[ "Outflow from Res GM" ]
475 *%-----|-----|
476 *# Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
477 *# (Approximated cross-section - see cross-section 258)
478 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
479 ROUTE CHANNEL      NHYDout=[ "N12" ] ,NHYDin=[ "RES_GM" ] ,
480          RDT=[1](min),
481          CHLGTH=[5926](m), CHSLOPE=[0.0759](%), FPSLOPE=[0.0759](%),
482          SECNUM=[1.0], NSEG=[1]
483          ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
484          ( DISTANCE (m), ELEVATION (m))=
485          [-40, 132.5]
486          [-30, 132]
487          [-25, 131.5]
488          [-13, 130]
489          [-8, 127.00]
490          [-7, 126.50]
491          [-6, 126]
492          [-5.5, 125.50]
493          [0, 123.75]
494          [4.5, 125.50]
495          [6, 126]
496          [7.5, 126.5]
497          [9, 127]
498          [10, 127.5]
499          [11.5, 128.00]
500          [15.5, 129.5]
501
502 *%-----|-----|
503 *#
504 *# Addition of Subwatershed Jock River at Ashton to Node 12
505 *#
506 ADD HYD          NHYDsum=[ "S_N12" ], NHYDs to add=[ "N12"+"JR_ASH" ]
507 SAVE HYD          NHYD=[ "S_N12" ], # OF PCYCLES=[-1], ICASEsh=[-1]
508          HYD_FILENAME=[ "H_SN12" ]
509          HYD_COMMENT=[ "flow at S_N12 near Ashton" ]
510 *%-----|-----|
511 *#
512 *# Sum of hydrographs from Node 12 routed to Node 11
513 *# (Approximated cross-section - see cross-section 258)
514 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
515 *ROUTE CHANNEL      NHYDout=[ "N11" ] ,NHYDin=[ "S_N12" ] ,
516          *
517          RDT=[1](min),
518          *
519          CHLGTH=[972](m), CHSLOPE=[0.0514](%), FPSLOPE=[0.0514](%),
520          *
521          SECNUM=[1.0], NSEG=[1]
522          ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
523          ( DISTANCE (m), ELEVATION (m))=

```

```

522 * [-40, 132.5]
523 * [-30, 132]
524 * [-25, 131.5]
525 * [-13, 130]
526 * [-8, 127.00]
527 * [-7, 126.50]
528 * [-6, 126]
529 * [-5.5, 125.50]
530 * [0, 123.75]
531 * [4.5, 125.50]
532 * [6, 126]
533 * [7.5, 126.5]
534 * [9, 127]
535 * [10, 127.5]
536 * [11.5, 128.00]
537 * [15.5, 129.5]
538 *%-----|-----|-----|
539 *#
540 *# Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
541 *#
542 ROUTE CHANNEL      NHYDout=[ "Dum11" ] ,NHYDin=[ "S_N12" ] ,
543 RDT=[1](min),
544 CHLGTH=[972](m),   CHSLOPE=[0.054](%),
545                                     FPSLOPE=[0.054](%),
546 SECNUM=[1.0],       NSEG=[1]
547 ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
548 ( DISTANCE (m), ELEVATION (m))=
549          [-40, 132.5]
550          [-30, 132]
551          [-25, 131.5]
552          [-13, 130]
553          [-8, 127.00]
554          [-7, 126.50]
555          [-6, 126]
556          [-5.5, 125.50]
557          [0, 123.75]
558          [4.5, 125.50]
559          [6, 126]
560          [7.5, 126.5]
561          [9, 127]
562          [10, 127.5]
563          [11.5, 128.00]
564          [15.5, 129.5]
565 *%-----|-----|-----|
566 *#
567 *# Addition of Subwatershed 11 and No Name Creek to Node 11
568 *#
569 ADD HYD           NHYDsum= [ "S_N11" ], NHYDs to add=[ "Dum11"+ "SW_11" + "NN_CK" ]
570 *%-----|-----|-----|
571 *#
572 *# Sum of hydrographs from Node 11 routed to Node 10
573 *# Section 1
574 *#
575 ROUTE CHANNEL      NHYDout=[ "N10" ] ,NHYDin=[ "S_N11" ] ,
576 RDT=[1](min),
577 CHLGTH=[14028](m),   CHSLOPE=[0.1568](%),
578                                     FPSLOPE=[0.1568](%),
579 SECNUM=[1.0],       NSEG=[5]
580 ( SEGROUGH, SEGDIST (m))=
581          [0.04,-52.82
582          0.1,-6.47
583          -0.05,6.47
584          0.1,45.36
585          0.04,423.88] NSEG times
586 ( DISTANCE (m), ELEVATION (m))=
587          [-226.24 ,112.50]

```

```

588 [-167.50 ,111.50]
589 [-106.81 ,111.00]
590 [-92.37 ,110.00]
591 [-52.82 ,109.00]
592 [-24.90, 109.00]
593 [-17.02, 108.50]
594 [-6.47, 108.00]
595 [6.47, 108.00]
596 [15.67, 108.50]
597 [18.95, 109.00]
598 [45.36, 109.50]
599 [120.79, 110.00]
600 [145.72, 111.00]
601 [181.56, 111.50]
602 [423.88, 112.50]

603 *%-----|-----|
604 *#
605 *# Addition of Subwatershed 10 to Node 10
606 *#
607 ADD HYD      NHYDsum=[ "S_N10" ], NHYDs to add=[ "N10"+"SW_10" ]
608 *%-----|-----|
609 SAVE HYD      NHYD=[ "S_N10" ], # OF PCYCLES=[ -1 ], ICASEsh=[ -1 ]
610          HYD_FILENAME=[ "H_SN10" ]
611          HYD_COMMENT=[ "flow at S_N10: N10 + SW_10" ]
612 *%-----|-----|
613 *# Addition of Kings Creek to S_N10
614 *#
615 ADD HYD      NHYDsum=[ "S_N10A" ], NHYDs to add=[ "S_N10"+"KG_CK" ]
616 *%-----|-----|
617 *#
618 *# Sum of hydrographs from Node 10 routed to Node 9
619 *# Section 2
620 *#
621 ROUTE CHANNEL      NHYDout=[ "N9" ] ,NHYDin=[ "S_N10A" ] ,
622          RDT=[ 1 ](min),
623          CHLGTH=[ 3982 ](m), CHSLOPE=[ 0.0753 ](%),
624          FPSLOPE=[ 0.0753 ](%),
625          SECNUM=[ 1.0 ], NSEG=[ 4 ]
626          ( SEGROUGH, SEGDIST (m))=
627          [ 0.04,-30.27
628          0.05,-18.42
629          -0.05,18.42
630          0.04,131.58] NSEG times
631          ( DISTANCE (m), ELEVATION (m))=
632          [-446.74, 106.00]
633          [-415.68, 105.50]
634          [-285.40, 105.00]
635          [-173.77, 104.50]
636          [-144.95, 104.00]
637          [-111.18, 103.50]
638          [-94.06, 103.00]
639          [-71.02, 102.50]
640          [-30.27, 102.00]
641          [-19.33, 100.00]
642          [-18.42, 99.50]
643          [18.42, 99.50]
644          [20.77, 100.00]
645          [27.93, 101.00]
646          [52.29, 101.00]
647          [68.80, 101.50]
648          [79.66, 103.00]
649          [91.50, 103.50]
650          [131.58, 104.00]

651 *%-----|-----|
652 *#
653 *# Addition of Subwatershed 9 and Nichols Creek to Node 9

```

```

654 *#
655 ADD HYD NHYDsum=[ "S_N9" ] , NHYDs to add=[ "N9 "+"SW_9 "+"NC_CK" ]
656 *%-----|-----|
657 *#
658 *# Sum of hydrographs from Node 9 routed to Node 8
659 *# Section 3
660 *#
661 ROUTE CHANNEL NHYDout=[ "N8" ] , NHYDin=[ "S_N9" ] ,
662 RDT=[1](min),
663 CHLGTH=[2269](m), CHSLOPE=[0.0882](%),
664 FPSLOPE=[0.0882](%),
665 SECNUM=[1.0], NSEG=[3]
666 ( SEGROUGH, SEGDIST (m))=
667 [0.1,-17.99
668 -0.045,17.31
669 0.1,456.58] NSEG times
670 ( DISTANCE (m), ELEVATION (m))=
671 [-201.19,100.50]
672 [-135.21, 100.00]
673 [-94.83, 99.50]
674 [-67.05, 99.00]
675 [-17.99, 98.50]
676 [-16.02, 98.00]
677 [-13.95, 97.50]
678 [13.95, 97.50]
679 [15.64, 98.00]
680 [17.31, 98.50]
681 [162.02, 98.50]
682 [172.89 ,99.00]
683 [314.38, 99.00]
684 [343.78, 99.50]
685 [365.67, 100.00]
686 [376.68, 100.00 ]
687 [393.11, 99.50]
688 [404.97, 99.50]
689 [431.70, 100.00]
690 [456.58, 100.50 ]
691 *%-----|-----|
692 *#
693 *# Addition of Subwatershed 8 and Hobb's Drain to Node 8
694 *#
695 ADD HYD NHYDsum=[ "S_N8" ] , NHYDs to add=[ "N8 "+"SW_8 "+"HB_DR" ]
696 *%-----|-----|
697 *#
698 *# Sum of hydrographs from Node 8 routed to Node 7
699 *# Section 4
700 *#
701 ROUTE CHANNEL NHYDout=[ "N7" ] , NHYDin=[ "S_N8" ],
702 RDT=[1](min),
703 CHLGTH=[3750](m), CHSLOPE=[0.0533](%),
704 FPSLOPE=[0.0533](%),
705 SECNUM=[1.0], NSEG=[3]
706 ( SEGROUGH, SEGDIST (m))=
707 [0.12,-18.11
708 -0.07,17.22
709 0.12,590.05] NSEG times
710 ( DISTANCE (m), ELEVATION (m))=
711 [-433.21, 102.00]
712 [-425.34, 101.50]
713 [-377.56, 101.50]
714 [-366.23, 101.00]
715 [-202.60, 100.50]
716 [-96.25, 99.50]
717 [-68.36 99.00]
718 [-18.11, 98.50]
719 [-13.81, 97.50]

```

```

720 [13.81, 97.50]
721 [17.22, 98.50]
722 [161.95, 98.50]
723 [173.11, 99.00]
724 [314.05, 99.00]
725 [365.52, 100.00]
726 [404.70, 99.50]
727 [476.74, 100.50]
728 [502.31, 101.00]
729 [584.69, 101.00]
730 [585.79, 101.00]
731 [590.05, 102.00]

732 *%-----|-----|
733 *#
734 *# Addition of Subwatershed 7 to Node 7
735 *#
736 ADD HYD      NHYDsum= [ "S_N7" ] , NHYDs to add= [ "N7" + "SW_7" ]
737 *%-----|-----|
738 SAVE HYD      NHYD= [ "S_N7" ] , # OF PCYCLES= [ -1 ] , ICASEsh= [ -1 ]
739          HYD_FILENAME= [ "H_SN7" ]
740          HYD_COMMENT= [ "flow at S_N7: N7 + SW_7" ]
741 *%-----|-----|
742 *# Insertion of a reservoir to simulate the effects of the Richmond Fen.
743 *# Storage area and volumes were estimated from available topo maps.
744 *# Release rate from fen was assumed to be controlled by the downstream
745 *# river cross-section for summer conditions. It is was assumed that for up to
746 *# 0.75 m of water, the main channel of the river provided the storage. Above
747 *# this depth, the wetland starts to signigicantly store water.
748 *#
749 ROUTE RESERVOIR   NHYDout= [ "RES_RF" ] , NHYDin= [ "S_N7" ] ,
750          RDT= [ 1 ] (min),
751          TABLE of ( OUTFLOW-STORAGE ) values
752          (cms) - (ha-m)
753          TABLE of ( OUTFLOW-STORAGE ) values
754          (cms) - (ha-m)
755          [ 0.0 , 0.0 ]
756          [ 0.9051 , 2.40 ]
757          [ 2.907 , 4.13 ]
758          [ 9.744 , 9.18 ]
759          [ 20.304 , 14.96 ]
760          [ 34.167 , 310.21 ]
761          [ 74.993 , 605.46 ]
762          [ 104.876 , 900.71 ]
763          [ 140.56 , 2892.00 ]
764          [ 225.00 , 3615.63 ]
765          [ -1 , -1 ] (max twenty pts)
766          NHYDovf= [ " " ] ,
767 *%-----|-----|
768 SAVE HYD      NHYD= [ "RES_RF" ] , # OF PCYCLES= [ -1 ] , ICASEsh= [ -1 ]
769          HYD_FILENAME= [ "H_ResRF" ]
770          HYD_COMMENT= [ "outflow of Richmond Fen" ]
771 *%-----|-----|
772 *#
773 *# Sum of hydrographs from Node 7 routed to Node 6
774 *# Section 5
775 *#
776 ROUTE CHANNEL    NHYDout= [ "N6" ] , NHYDin= [ "RES_RF" ] ,
777          RDT= [ 1 ] (min),
778          CHLGTH= [ 3056 ] (m) , CHSLOPE= [ 0.0818 ] ( % ) ,
779          FPSLOPE= [ 0.0818 ] ( % ) ,
780          SECNUM= [ 1.0 ] , NSEG= [ 5 ]
781          ( SEGROUGH , SEGDIST (m) ) =
782          [ 0.025 , -70.8
783          0.1 , -23.9
784          -0.05 , 23.9
785          0.06 , 39.8

```

```

786          0.05,96.3] NSEG times
787  ( DISTANCE (m), ELEVATION (m))=
788          [-100.8, 97.00]
789          [-70.8, 96.50]
790          [-52.0, 96.00]
791          [-35.1, 95.50]
792          [-30.6, 95.00]
793          [-23.9, 94.54]
794          [23.9, 94.54]
795          [39.8, 95.00]
796          [50.4, 95.50]
797          [93.5, 96.00]
798          [94.9, 96.50]
799          [96.3, 97.00]
800 *%-----|-----|
801 *#
802 *# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
803 *#
804 ADD HYD      NHYDsum=[ "S_N6" ] , NHYDs to add=[ "N6"+"SW_6"+"VG_DR" ]
805 *%-----|-----|
806 *#
807 *# Sum of hydrographs from Node 6 routed to Node 5
808 *# Section 6
809 *#
810 ROUTE CHANNEL      NHYDout=[ "N5" ] ,NHYDin=[ "S_N6" ] ,
811          RDT=[1](min),
812          CHLGTH=[1852](m),   CHSLOPE=[0.0540](%),
813          FPSLOPE=[0.0540](%),
814          SECNUM=[1.0],       NSEG=[3]
815          ( SEGROUGH, SEGDIST (m))=
816          [0.035,-131.59
817          -0.045,48.96
818          0.1,239.04] NSEG times
819          ( DISTANCE (m), ELEVATION (m))=
820          [-686.30, 94.50]
821          [-675.70, 94.00]
822          [-492.52, 93.00]
823          [-467.28, 94.00]
824          [-131.59, 94.00]
825          [-92.79, 92.50]
826          [-18.06, 91.00]
827          [18.06, 91.00]
828          [43.47, 92.50]
829          [48.96, 94.00]
830          [177.43, 94.00]
831          [239.04,94.50]
832 *%-----|-----|
833 *#
834 *# Addition of Subwatershed 5 and Flowing Creek to Node 5
835 *#
836 ADD HYD      NHYDsum=[ "S_N5" ] , NHYDs to add=[ "N5"+"SW_5"+"FL_CK" ]
837 *%-----|-----|
838 *#
839 *# Sum of hydrographs from Node 5 routed to Node 5A
840 *# Section 7
841 *#
842 ROUTE CHANNEL      NHYDout=[ "N5A" ] ,NHYDin=[ "S_N5" ] ,
843          RDT=[1](min),
844          CHLGTH=[556](m),   CHSLOPE=[0.0900](%),
845          FPSLOPE=[0.0900](%),
846          SECNUM=[1.0],       NSEG=[4]
847          ( SEGROUGH, SEGDIST (m))=
848          [0.04,-41.5
849          0.1,-14.0
850          -0.045,14.0
851          0.1,41.1] NSEG times

```

```

852          ( DISTANCE (m) , ELEVATION (m))=
853                      [-275.8, 93.00]
854                      [-248.6, 92.50]
855                      [-237.0, 92.00]
856                      [-219.3, 91.50]
857                      [-202.1, 91.50]
858                      [-186.0, 92.00]
859                      [-129.2, 92.00]
860                      [-117.6, 91.50]
861                      [-100.6, 91.00]
862                      [-41.5, 91.00]
863                      [-20.0, 91.00]
864                      [-14.0, 90.54]
865                      [14.0, 90.54]
866                      [15.3, 91.00]
867                      [17.3, 91.50]
868                      [38.4, 92.00]
869                      [39.8, 92.50]
870                      [41.1, 93.00]
871 *%-----|-----|
872 *#
873 *# Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
874 *#
875 ADD HYD           NHYDsum=[ "S_N5A" ] , NHYDs to add=[ "N5A"+"SW_5A2"+"SW_5A1" ]
876 *%-----|-----|
877 *#
878 *# Sum of hydrographs from Node 5A routed to Node 4
879 *# Section 8
880 *#
881 ROUTE CHANNEL      NHYDout=[ "N4" ] , NHYDin=[ "S_N5A" ] ,
882             RDT=[1](min),
883             CHLGTH=[4630](m),   CHSLOPE=[0.0432](%),
884                               FPSLOPE=[0.0432](%),
885             SECNUM=[1.0],        NSEG=[3]
886             ( SEGRROUGH, SEGDIST (m))=
887                 [0.05,-28.2
888                 -0.035,28.2
889                 0.05,173.1] NSEG times
890             ( DISTANCE (m) , ELEVATION (m))=
891                         [-38.9, 92.00]
892                         [-35.8, 91.50]
893                         [-33.3, 91.00]
894                         [-28.2, 90.50]
895                         [-15.0, 87.48]
896                         [-5.0, 88.34]
897                         [5.0, 86.20]
898                         [15.0, 88.55]
899                         [28.2, 90.50]
900                         [29.7, 91.00]
901                         [46.5, 91.00]
902                         [127.8, 91.00]
903                         [148.7, 91.50]
904                         [173.1, 92.00]
905 *%-----|-----|
906 *#
907 *# Addition of Subwatershed 4 and Leamy Creek to Node 4
908 *#
909 ADD HYD           NHYDsum=[ "S_N4" ] , NHYDs to add=[ "N4"+"SW_4"+"LM_CK" ]
910 SAVE HYD          NHYD=[ "S_N4" ] , # OF PCYCLES=[-1], ICASEsh=[1]
911             HYD_COMMENT=[ "flow at S_N4" ]
912 *%-----|-----|
913 *#
914 *# Sum of hydrographs from Node 4 routed to Node 2
915 *# Section 9
916 *#
917 ROUTE CHANNEL      NHYDout=[ "N2" ] , NHYDin=[ "S_N4" ] ,

```

```

918 RDT=[1](min),
919 CHLGTH=[1667](m), CHSLOPE=[0.0600](%),
920                                     FPSLOPE=[0.0600](%),
921 SECNUM=[1.0], NSEG=[4]
922 ( SEGROUGH, SEGDIST (m))=
923     [0.1,-28.0
924     -0.04,28.4
925     0.06,31.7
926     0.04,80.2] NSEG times
927 ( DISTANCE (m), ELEVATION (m))=
928     [-36.3, 92.00]
929     [-32.6, 91.50]
930     [-30.2, 91.00]
931     [-28.0, 90.45]
932     [-15.0, 87.48]
933     [-5.0, 88.34]
934     [5.0, 86.20]
935     [15.0, 88.55]
936     [28.0, 90.45]
937     [28.4, 90.50]
938     [30.4, 91.00]
939     [31.7, 91.50]
940     [80.2, 92.00]
941 *%-----|-----|
942 *#
943 *# Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2
944 *#
945 ADD HYD          NHYDsum= [ "S_N2" ], NHYDs to add= [ "N2"+ "SW_2"+ "SM_DR"+ "MO_DR" ]
946 *%-----|-----|
947 SAVE HYD          NHYD= [ "S_N2" ], # OF PCYCLES=[-1], ICASEsh=[-1]
948          HYD_FILENAME=[ "H_SN2" ]
949          HYD_COMMENT=[ "flow at S_N2 Jock River Gauge at Moodie Dr." ]
950 *%-----|-----|
951 *#
952 *# Sum of hydrographs from Node 2 routed to Node 1
953 *# Section 10
954 *#
955 *#***** ****
956 *%READ HYD          NHYD= [ "S_N2" ],
957 *%          HYD_FILENAME=[ "H-S_N2" ]
958 *%-----|-----|
959 *#
960 *# Hydrograph from Node 2 routed to Node 416
961 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 9025
962 *#
963 ROUTE CHANNEL      NHYDout=[ "N_416" ] , NHYDin=[ "S_N2" ] ,
964          RDT=[1](min),
965          CHLGTH=[2327](m), CHSLOPE=[0.0498](%),
966                                     FPSLOPE=[0.0498](%),
967          SECNUM=[1.0], NSEG=[3]
968 ( SEGROUGH, SEGDIST (m))=
969     [0.075,-23.96
970     -0.055,23.96
971     0.075,157.38] NSEG times
972 ( DISTANCE (m), ELEVATION (m))=
973     [-336.97,93.5]
974     [-318.85,93]
975     [-259,92.5]
976     [-133.18,92]
977     [-33.17,92]
978     [-27.21,92]
979     [-26.14,91.5]
980     [-24.99,91]
981     [-23.96,90.5]
982     [-14.33,88.26]
983     [-0.68,88.12]

```



```

1045 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 7245
1046 *#
1047 ROUTE CHANNEL      NHYDout=[ "N_OK" ] , NHYDin=[ "SN_416" ] ,
1048                               RDT=[1](min),
1049                               CHLGTH=[497](m),   CHSLOPE=[0.3018](%),
1050                               FPSLOPE=[0.3018](%),
1051                               SECNUM=[1.0],       NSEG=[3]
1052                               ( SEGROUGH, SEGDIST (m))=
1053                               [0.075,-19.40
1054                               -0.055,19.40
1055                               0.075,377.02] NSEG times
1056                               ( DISTANCE (m), ELEVATION (m))=
1057                               [-1061.41, 92.50]
1058                               [-945.91, 92.00]
1059                               [-783.64, 91.50]
1060                               [-136.74, 91.00]
1061                               [-86.04, 91.00]
1062                               [-20.86, 91.00]
1063                               [-20.18, 90.50]
1064                               [-19.40, 90.00]
1065                               [-11.68, 86.89]
1066                               [0.00, 86.10]
1067                               [12.09, 86.81]
1068                               [19.40, 90.00]
1069                               [34.68, 90.50]
1070                               [60.56, 91.00]
1071                               [170.14, 91.00]
1072                               [175.05, 90.50]
1073                               [180.29, 90.00]
1074                               [193.41, 90.00]
1075                               [195.98, 90.50]
1076                               [377.02, 92.50]
1077 *%-----|-----|
1078 *#*****
1079 *#      Catchment OKEEFE
1080 *#      - To O'Keefe drain (north of the Jock)
1081 *#      - Developed with assumed 43% imp.
1082 *#      - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area
1083 *#      - 2020-11-20 Okeefe detailed model was added as per the NOVATECH SWMHMO model
(Citi-Gate 2014).
1084 *%-----|-----|
1085 *POST DEVELOPMENT CONDITIONS
1086 *%-----|-----|
1087 *#*****
1088 CONTINUOUS NASHYD      NHYD=[ "O-1" ], DT=[1]min, AREA=[63.72](ha),
1089                               DWF=[0](cms), CN/C=[61], IA=[6.2](mm), N=[3], TP=[.9]hrs,
1090                               Continuous simulation parameters:
1091                               IaRECper=[4](hrs),
1092                               SMIN=[-1](mm),   SMAX=[-1](mm), SK=[0.010]/(mm),
1093                               InterEventTime=[12](hrs)
1094                               Baseflow simulation parameters:
1095                               BaseFlowOption=[1] ,
1096                               InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1097                               VHydCond=[0.055](mm/hr), END=-1
1098 *%-----|-----|
1099 *ROUTE FLOW THROUGH AREA 0-2
1100 ROUTE CHANNEL      NHYDout=[ "O-1R" ], NHYDin=[ "O-1" ], RDT=[1](min),
1101                               CHLGTH=[960](m), CHSLOPE=[0.63](%), FPSLOPE=[0.63](%),
1102                               SECNUM=[1], NSEG=[3]
1103                               ( SEGROUGH, SEGDIST (m))=[0.06,4 -.043,6 0.06,10] NSEG times
1104                               ( DISTANCE (m), ELEVATION (m))=[0.00, 2.0]
1105                               [4.0, 0.0]
1106                               [6.0, 0.0]

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1171   TIMP=[0.26], DWF=[0](cms),
1172   LOSS=[2], SCS curve number CN=[61],
1173   Previous surfaces: IAper=[4.67](mm), SLPP=[1.38](%),
1174   LGP=[550](m), MNP=[0.035], SCP=[0](min), Impervious surfaces:
1175   IAimp=[1.57](mm), SLPI=[1.38](%),
1176   LGI=[1450](m), MNI=[0.013], SCI=[0](min),
1177   Continuous simulation parameters:
1178   IaRECper=[4](hrs), IaRECImp=[4](hrs),
1179   SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1180   InterEventTime=[12](hrs), END=-1
1181 *%-----|-----|
1182 *TOTAL EXTERNAL FLOWS WEST OF THE SITE AND NORTH OF O'KEEFE CRT
1183 *%-----|-----|
1184 ADD HYD      NHYDsum=[ "PT1" ], NHYDs to add=[ "OKF-NR" +"O-3" +"O-5" +"O-6" ]
1185 *%-----|-----|
1186 CONTINUOUS NASHYD NHYD=[ "O-7" ], DT=[1]min, AREA=[5.28](ha),
1187 DWF=[0](cms), CN/C=[54], IA=[7.5](mm), N=[3], TP=[0.6]hrs,
1188 Continuous simulation parameters:
1189 IaRECper=[4](hrs),
1190 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1191 InterEventTime=[12](hrs)
1192 Baseflow simulation parameters:
1193 BaseFlowOption=[1],
1194 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1195 VHydCond=[0.055](mm/hr), END=-1
1196 *%-----|-----|
1197 *ANALYSIS POINT 1 - TOTAL FLOW NORTH OF FALLOWFIELD DR. AND O'KEEFE CRT.
1198 ADD HYD      NHYDsum=[ "FF" ], NHYDs to add=[ "PT1" +"O-7" ]
1199 *%-----|-----|
1200 *ROUTE FLOW through O'Keefe Drain 1
1201 ROUTE CHANNEL NHYDout=[ "DRAIN1" ], NHYDin=[ "FF" ], RDT=[1](min),
1202 CHLGH= [302]{m}, CHSLOPE=[1.00](%), FPSLOPE=[1.00](%),
1203 SECNUM=[1], NSEG=[3]
1204 ( SEGROUGH, SEGDIST (m))=[0.07,13.45 -0.043,16.55 0.07,30.00] NSEG
1205 times
1206 ( DISTANCE (m), ELEVATION (m))=[0.00, 1.70]
1207 (3.45, 0.60)
1208 (13.45, 0.50)
1209 (14.45, 0.00)
1210 (15.55, 0.00)
1211 (16.55, 0.50)
1212 (26.55, 0.60)
1213 (30.00, 1.70)
1214 *%-----|-----|
1215 CONTINUOUS NASHYD NHYD=[ "D1" ], DT=[1]min, AREA=[1.17](ha),
1216 DWF=[0](cms), CN/C=[84], IA=[9.0](mm), N=[3], TP=[0.28]hrs,
1217 Continuous simulation parameters:
1218 IaRECper=[4](hrs),
1219 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1220 InterEventTime=[12](hrs)
1221 Baseflow simulation parameters:
1222 BaseFlowOption=[1],
1223 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1224 VHydCond=[0.055](mm/hr), END=-1
1225 *%-----|-----|
1226 CONTINUOUS STANDHYD NHYD=[ "A1" ], DT=[1]min, AREA=[2.50](ha), XIMP=[0.68], TIMP=[0.85],
1227 DWF=[0](cms), LOSS=[1]:
1228 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1229 F=[0.00](mm),
1230 Previous areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1231 MNP=[0.250], SCP=[0](min),
1232 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
1233 LGI=[223.607](m), MNI=[0.013], SCI=[0](min),
1234 Continuous simulation parameters:
1235 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
1236 END=-1

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1229 *%
1230 ROUTE RESERVOIR NHYDout= [ "A1-STR" ], NHYDin= [ "A1" ], RDT=[1](min),
1231 TABLE of ( OUTFLOW-STORAGE ) values
1232 (cms) - (ha-m)
1233 [ 0.000 , 0.000 ]
1234 [ 0.035 , 0.038 ]
1235 [ 0.072 , 0.051 ]
1236 [ 0.100 , 0.059 ]
1237 [ 0.125 , 0.070 ]
1238 [ 0.160 , 0.074 ]
1239 [ 0.185 , 0.081 ]
1240 [ -1 , -1 ] (max twenty pts)
1241 NHYDovf= [ "A1-OVF" ]
1242 *%
1243 CONTINUOUS STANDHYD NHYD= [ "ST-2" ], DT=[1]min, AREA=[0.59](ha), XIMP=[0.46],
1244 TIMP=[0.57], DWF=[0](cms), LOSS=[1]:
1245 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1246 F=[0.00](mm),
1247 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1248 MNP=[0.250], SCP=[0](min),
1249 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
1250 LGI=[108.628](m), MNI=[0.013], SCI=[0](min),
1251 Continuous simulation parameters:
1252 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
1253 END=-1
1254 *%
1255 ROUTE RESERVOIR NHYDout= [ "ST2STR" ], NHYDin= [ "ST-2" ], RDT=[1](min),
1256 TABLE of ( OUTFLOW-STORAGE ) values
1257 (cms) - (ha-m)
1258 [ 0.000 , 0.0000 ]
1259 [ 0.052 , 0.0010 ]
1260 [ 0.053 , 0.0080 ]
1261 [ -1 , -1 ] (max twenty pts)
1262 NHYDovf= [ "ST2OVF" ]
1263 *%
1264 *%
1265 *TOTAL FLOW NORTH OF STRANDHERD DR. (EAST BRANCH) CROSSING*
1266 *%
1267 CONTINUOUS NASHYD NHYD= [ "O-8" ], DT=[1]min, AREA=[60.55](ha),
1268 DWF=[0](cms), CN/C=[69], IA=[4.0](mm), N=[3], TP=[1.0]hrs,
1269 Continuous simulation parameters:
1270 IaRECper=[4](hrs),
1271 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1272 InterEventTime=[12](hrs)
1273 Baseflow simulation parameters:
1274 BaseFlowOption=[1],
1275 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1276 VHydCond=[0.055](mm/hr), END=-1
1277 *%
1278 ROUTE PIPE PTYPE=[2]rect, NHYDout= [ "O8PIPE" ], RNUMBER=[1], PWIDTH=[1800](mm),
1279 PHEIGHT=[1200](mm), PLNGTH=[335.1](m),
1280 PROUGH=[0.013], PSLOPE=[0.001](m/m), NHYDin= [ "O-8" ], RDT=[1](min)
1281 *%
1282 *%
1283 ADD HYD NHYDsum= [ "ST2-IN" ], NHYDs to
1284 add= [ "DRAIN1 "+"D1 "+"A1-STR "+"A1-OVF "+"ST2STR "+"ST2OVF "+"O8PIPE" ]
1285 *%
1286 CONTINUOUS STANDHYD NHYD= [ "A7" ], DT=[1]min, AREA=[3.51](ha), XIMP=[0.68], TIMP=[0.85],
1287 DWF=[0](cms), LOSS=[1]:
1288 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1289 F=[0.00](mm),
1290 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1291 MNP=[0.250], SCP=[0](min),
1292 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
1293 LGI=[264.953](m), MNI=[0.013], SCI=[0](min),
1294 Continuous simulation parameters:

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1284           IaRECper=[4](hrs),  IaRECImp=[4](hrs),  InterEventTime=[12](hrs),
1285           END=-1
1286 *%----- ROUTE RESERVOIR -----| NHYDout= [ "A7-STR" ], NHYDin= [ "A7" ], RDT=[1](min),
1287             TABLE of ( OUTFLOW-STORAGE ) values
1288               (cms) - (ha-m)
1289               [ 0.000 , 0.000 ]
1290               [ 0.049 , 0.054 ]
1291               [ 0.102 , 0.072 ]
1292               [ 0.140 , 0.082 ]
1293               [ 0.175 , 0.099 ]
1294               [ 0.225 , 0.105 ]
1295               [ 0.260 , 0.114 ]
1296               [ -1 , -1 ] (max twenty pts)
1297             NHYDovf= [ "A7-OVF" ]
1298 *%-----| CONTINUOUS STANDHYD -----| NHYD= [ "ST-3" ], DT=[1]min, AREA=[0.71](ha), XIMP=[0.46],
1299             TIMP=[0.57], DWF=[0](cms), LOSS=[1]:
1300               Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1301               F=[0.00](mm),
1302               Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1303               MNP=[0.250], SCP=[0](min),
1304               Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[119.164](m), MNI=[0.013], SCI=[0](min),
1305               Continuous simulation parameters:
1306             IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
1307             END=-1
1308 *%----- ROUTE RESERVOIR -----| NHYDout= [ "ST3STR" ], NHYDin= [ "ST-3" ], RDT=[1](min),
1309             TABLE of ( OUTFLOW-STORAGE ) values
1310               (cms) - (ha-m)
1311               [ 0.000 , 0.0000 ]
1312               [ 0.063 , 0.0010 ]
1313               [ 0.064 , 0.0094 ]
1314               [ -1 , -1 ] (max twenty pts)
1315             NHYDovf= [ "ST3OVF" ]
1316 *%-----| *ANALYSIS POINT 2 - TOTAL FLOW AT OUTLET OF STREET 2/3 INTERSECTION -----|
1317 ADD HYD      NHYDs[ "PT2ST3" ], NHYDs to
1318 add=[ "ST2-IN"+ "A7-STR" + "A7-OVF" + "ST3STR" + "ST3OVF" ]
1319 *%-----| *ROUTE FLOW through O'Keefe Drain 2 -----|
1320 ROUTE CHANNEL NHYDout= [ "DRAIN2" ], NHYDin= [ "PT2ST3" ], RDT=[1](min),
1321             CHLGTH=[592]{m}, CHSLOPE=[.23](%), FPSLOPE=[.23](%),
1322             SECNUM=[1], NSEG=[3]
1323             ( SEGROUGH, SEGDIST (m))=[0.07,12.60 -0.043,17.40 0.07,30.00] NSEG
1324             times
1325             ( DISTANCE (m), ELEVATION (m))=[0.00, 1.70]
1326             (2.60, 0.95)
1327             (12.60, 0.75)
1328             (14.10, 0.00)
1329             (15.90, 0.00)
1330             (17.40, 0.75)
1331             (27.40, 0.95)
1332             (30.00, 1.70)
1333 *%-----| CONTINUOUS NASHYD -----| NHYD= [ "D2" ], DT=[1]min, AREA=[2.28](ha), DWF=[0](cms), CN/C=[84],
1334             IA=[9.0](mm),
1335             N=[3], TP=[0.99]hrs,
1336             Continuous simulation parameters:
1337             IaRECper=[4](hrs),
1338             SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1339             InterEventTime=[12](hrs)
1340             Baseflow simulation parameters:
1341             BaseFlowOption=[1] ,

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1341           InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
1342           VHydCond=[ 0.055 ](mm/hr), END=-1
1343 *%-----|-----|
1344 CONTINUOUS STANDHYD NHYD=[ "A17" ], DT=[ 1 ]min, AREA=[ 12.04 ](ha), XIMP=[ 0.68 ],
1345   TIMP=[ 0.85 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
1346   Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
1347   F=[ 0.00 ](mm),
1348   Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%), LGP=[ 50 ](m),
1349   MNP=[ 0.250 ], SCP=[ 0 ](min),
1350   Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%),
1351   LGI=[ 490.714 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1352   Continuous simulation parameters:
1353   IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
1354   END=-1
1355 *%-----|-----|
1356 ROUTE RESERVOIR NHYDout=[ "A17STR" ], NHYDin=[ "A17" ], RDT=[ 1 ](min),
1357   TABLE of ( OUTFLOW-STORAGE ) values
1358   (cms) - (ha-m)
1359   [ 0.000 , 0.000 ]
1360   [ 0.169 , 0.185 ]
1361   [ 0.349 , 0.248 ]
1362   [ 0.482 , 0.283 ]
1363   [ 0.602 , 0.338 ]
1364   [ 0.771 , 0.359 ]
1365   [ 0.891 , 0.391 ]
1366   [ -1 , -1 ] (max twenty pts)
1367   NHYDovf=[ "A17OVF" ]
1368 *%-----|-----|
1369 CONTINUOUS STANDHYD NHYD=[ "ST-4" ], DT=[ 1 ]min, AREA=[ 0.35 ](ha), XIMP=[ 0.46 ],
1370   TIMP=[ 0.57 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
1371   Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
1372   F=[ 0.00 ](mm),
1373   Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%), LGP=[ 50 ](m),
1374   MNP=[ 0.250 ], SCP=[ 0 ](min),
1375   Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%), LGI=[ 83.666 ](m),
1376   MNI=[ 0.013 ], SCI=[ 0 ](min),
1377   Continuous simulation parameters:
1378   IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
1379   END=-1
1380 *%-----|-----|
1381 ROUTE RESERVOIR NHYDout=[ "ST4STR" ], NHYDin=[ "ST-4" ], RDT=[ 1 ](min),
1382   TABLE of ( OUTFLOW-STORAGE ) values
1383   (cms) - (ha-m)
1384   [ 0.000 , 0.0000 ]
1385   [ 0.031 , 0.0010 ]
1386   [ 0.032 , 0.0050 ]
1387   [ -1 , -1 ] (max twenty pts)
1388   NHYDovf=[ "ST4OVF" ]
1389 *%-----|-----|
1390 CONTINUOUS STANDHYD NHYD=[ "A18" ], DT=[ 1 ]min, AREA=[ 5.30 ](ha), XIMP=[ 0.68 ], TIMP=[ 0.85 ],
1391   DWF=[ 0 ](cms), LOSS=[ 1 ]:
1392   Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
1393   F=[ 0.00 ](mm),
1394   Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%), LGP=[ 50 ](m),
1395   MNP=[ 0.250 ], SCP=[ 0 ](min),
1396   Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%),
1397   LGI=[ 325.576 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1398   Continuous simulation parameters:
1399   IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
1400   END=-1
1401 *%-----|-----|
1402 ROUTE RESERVOIR NHYDout=[ "A18STR" ], NHYDin=[ "A18" ], RDT=[ 1 ](min),
1403   TABLE of ( OUTFLOW-STORAGE ) values
1404   (cms) - (ha-m)
1405   [ 0.000 , 0.000 ]
1406   [ 0.074 , 0.082 ]

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1392 [ 0.154 , 0.109 ]
1393 [ 0.212 , 0.125 ]
1394 [ 0.265 , 0.149 ]
1395 [ 0.339 , 0.158 ]
1396 [ 0.392 , 0.172 ]
1397 [ -1 , -1 ] (max twenty pts)
1398 NHYDovf=[ "A18OVF" ]
1399 *%-----|-----|
1400 *ANALYSIS POINT 3 - TOTAL FLOW AT OUTLET OF STREET 4
1401 *%-----|-----|
1402 ADD HYD NHYDsum=[ "PT3ST4" ], NHYDs to
1403 add=[ "DRAIN2"+ "D2"+ "A17STR"+ "A17OVF"+ "ST4STR"+ "ST4OVF"+ "A18STR"+ "A18OVF" ]
1404 *%-----|-----|
1405 *ROUTE FLOW through O'Keefe Drain 3
1406 ROUTE CHANNEL NHYDout=[ "DRAIN3" ], NHYDin=[ "PT3ST4" ], RDT=[ 1 ](min),
1407 CHLGTH=[ 525 ]{m}, CHSLOPE=[ .23 ](%), FPSLOPE=[ .23 ](%),
1408 SECNUM=[ 1 ], NSEG=[ 3 ]
1409 ( SEGRROUGH, SEGDIST (m) )=[ 0.07, 12.50 -0.043, 17.50 0.07, 30.00 ] NSEG
1410 times
1411 ( DISTANCE (m), ELEVATION (m) )=[ 0.00, 1.70 ]
1412 ( 2.50, 1.00 )
1413 ( 12.50, 0.80 )
1414 ( 14.10, 0.00 )
1415 ( 15.90, 0.00 )
1416 ( 17.50, 0.80 )
1417 ( 27.50, 1.00 )
1418 ( 30.00, 1.70 )
1419 *%-----|-----|
1420 CONTINUOUS NASHYD NHYD=[ "D3" ], DT=[ 1 ]min, AREA=[ 2.51 ](ha),
1421 DWF=[ 0 ](cms), CN/C=[ 86 ], IA=[ 8.7 ](mm), N=[ 3 ], TP=[ 0.73 ]hrs,
1422 Continuous simulation parameters:
1423 IaRECper=[ 4 ](hrs),
1424 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1425 InterEventTime=[ 12 ](hrs)
1426 Baseflow simulation parameters:
1427 BaseFlowOption=[ 1 ],
1428 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
1429 VHydCond=[ 0.055 ](mm/hr), END=-1
1430 *%-----|-----|
1431 CONTINUOUS STANDHYD NHYD=[ "C1" ], DT=[ 1 ]min, AREA=[ 3.41 ](ha), XIMP=[ 0.68 ], TIMP=[ 0.85 ],
1432 DWF=[ 0 ](cms), LOSS=[ 1 ]:
1433 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
1434 F=[ 0.00 ](mm),
1435 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%), LGP=[ 50 ](m),
1436 MNP=[ 0.250 ], SCP=[ 0 ](min),
1437 Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%),
1438 LGI=[ 261.151 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1439 Continuous simulation parameters:
1440 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
1441 END=-1
1442 *%-----|-----|
1443 ROUTE RESERVOIR NHYDout=[ "C1-STR" ], NHYDin=[ "C1" ], RDT=[ 1 ](min),
1444 TABLE of ( OUTFLOW-STORAGE ) values
1445 ( cms ) - ( ha-m )
1446 [ 0.000 , 0.000 ]
1447 [ 0.048 , 0.052 ]
1448 [ 0.099 , 0.070 ]
1449 [ 0.136 , 0.080 ]
1450 [ 0.170 , 0.096 ]
1451 [ 0.218 , 0.102 ]
1452 [ 0.252 , 0.111 ]
1453 [ -1 , -1 ] (max twenty pts)
1454 NHYDovf=[ "C1-OVF" ]
1455 *%-----|-----|
1456 CONTINUOUS STANDHYD NHYD=[ "ST-5" ], DT=[ 1 ]min, AREA=[ 0.45 ](ha), XIMP=[ 0.46 ],
1457 TIMP=[ 0.57 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:

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1450 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1451 F=[0.00](mm),
1452 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1453 MNP=[0.250], SCP=[0](min),
1454 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[94.868](m),
1455 MNI=[0.013], SCI=[0](min),
1456 Continuous simulation parameters:
1457 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
1458 END=-1
1459 *%-----|-----|
1460 ROUTE RESERVOIR NHYDout=[ "ST5STR" ], NHYDin=[ "ST-5" ], RDT=[1](min),
1461 TABLE of ( OUTFLOW-STORAGE ) values
1462 (cms) - (ha-m)
1463 [ 0.000 , 0.0000 ]
1464 [ 0.040 , 0.0010 ]
1465 [ 0.041 , 0.0062 ]
1466 [ -1 , -1 ] (max twenty pts)
1467 NHYDovf=[ "ST5OVF" ]
1468 *%-----|-----|
1469 ADD HYD NHYDsum=[ "ST5-E" ], NHYDs to
1470 add=[ "DRAIN3 "+ "D3 "+ "C1-STR "+ "C1-OVF "+ "ST5STR "+ "ST5OVF" ]
1471 *%-----|-----|
1472 CONTINUOUS STANDHYD NHYD=[ "STRAND" ], DT=[1](min), AREA=[ 7.59 ](ha),
1473 XIMP=[ 0.64 ], TIMP=[ 0.85 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
1474 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1475 F=[0.00](mm),
1476 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[40](m),
1477 MNP=[0.250], SCP=[0](min),
1478 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[1230](m),
1479 MNI=[0.013], SCI=[0](min),
1480 Continuous simulation parameters:
1481 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
1482 END=-1
1483 *%-----|-----|
1484 ROUTE RESERVOIR NHYDout=[ "S-POND" ], NHYDin=[ "STRAND" ], RDT=[1](min),
1485 TABLE of ( OUTFLOW-STORAGE ) values
1486 (cms) - (ha-m)
1487 [ 0.000 , 0.000 ]
1488 [ 0.033 , 0.188 ]
1489 [ 0.057 , 0.253 ]
1490 [ 0.104 , 0.287 ]
1491 [ 0.160 , 0.336 ]
1492 [ 0.340 , 0.346 ]
1493 [ 0.471 , 0.360 ]
1494 [ 0.824 , 0.390 ]
1495 [ -1 , -1 ] (max twenty pts)
1496 NHYDovf=[ "S-OVF" ]
1497 *%-----|-----|
1498 ADD HYD NHYDsum=[ "SSAOUT" ], NHYDs to add=[ "ST5-E "+ "S-POND "+ "S-OVF" ]
1499 *%-----|-----|
1500 SAVE HYD NHYD=[ "SSAOUT" ], # OF PCYCLES=[ 5 ], ICASEsh=[ 1 ]
1501 HYD_COMMENT=[ "SSAOUT" ]
1502 *%-----|-----|
1503 CONTINUOUS STANDHYD NHYD=[ "Area-A" ], DT=[1]min, AREA=[ 66.75 ](ha), XIMP=[ 0.64 ],
1504 TIMP=[ 0.80 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
1505 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1506 F=[0.00](mm),
1507 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1508 MNP=[0.250], SCP=[0](min),
1509 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[1155.422](m), MNI=[0.013], SCI=[0](min),
1510 Continuous simulation parameters:
1511 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
1512 END=-1
1513 *%-----|-----|
1514 SAVE HYD NHYD=[ "Area-A" ], # OF PCYCLES=[ 1 ], ICASEsh=[ 1 ]

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1502
1503 *%
1504 ROUTE RESERVOIR HYD_COMMENT=[ "SMWF-A Inflow" ]
1505 | NYHDout=[ "SMWF-A" ], NHYDin=[ "Area-A" ], RDT=[1](min),
1506 | TABLE of ( OUTFLOW-STORAGE ) values
1507 | (cms) - (ha-m)
1508 | [ 0.000 , 0.000 ]
1509 | [ 0.103 , 1.077 ]
1510 | [ 0.128 , 1.749 ]
1511 | [ 0.382 , 2.282 ]
1512 | [ 0.703 , 2.582 ]
1513 | [ 1.256 , 2.978 ]
1514 | [ 1.567 , 3.202 ]
1515 | [ 1.955 , 3.493 ]
1516 | [ 2.100 , 3.600 ]
1517 | [ -1 , -1 ] (max twenty pts)
1518 | NYHDovf=[ "SWMAOV" ]
1519 *%
1520 SAVE HYD NYHD=[ "SMWF-A" ], # OF PCYCLES=[1], ICASESh=[1]
1521 | HYD_COMMENT=[ "SMWF-A Outflow" ]
1522 *%
1523 *ANALYSIS POINT 4 - TOTAL FLOW AT OUTLET OF STREET 5
1524 *%
1525 ADD HYD NYHDSum=[ "PT4ST5" ], NYHDs to add=[ "SSAOUT"+ "SMWF-A" + "SWMAOV" ]
1526 *%
1527 CONTINUOUS STANDHYD NYHD=[ "C6" ], DT=[1]min, AREA=[1.87](ha), XIMP=[0.68], TIMP=[0.85],
1528 DWF=[0](cms), LOSS=[1]:
1529 | Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1530 | F=[0.00](mm),
1531 | Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1532 | MNP=[0.250], SCP=[0](min),
1533 | Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
1534 | LGI=[193.391](m), MNI=[0.013], SCI=[0](min),
1535 | Continuous simulation parameters:
1536 | IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
1537 | END=-1
1538 *%
1539 ROUTE RESERVOIR NYHDout=[ "C6-STR" ], NHYDin=[ "C6" ], RDT=[1](min),
1540 | TABLE of ( OUTFLOW-STORAGE ) values
1541 | (cms) - (ha-m)
1542 | [ 0.000 , 0.000 ]
1543 | [ 0.026 , 0.029 ]
1544 | [ 0.054 , 0.038 ]
1545 | [ 0.075 , 0.044 ]
1546 | [ 0.093 , 0.052 ]
1547 | [ 0.120 , 0.056 ]
1548 | [ 0.138 , 0.061 ]
1549 | [ -1 , -1 ] (max twenty pts)
1550 | NYHDovf=[ "C6-OVF" ]
1551 *%
1552 CONTINUOUS STANDHYD NYHD=[ "C7" ], DT=[1]min, AREA=[1.62](ha), XIMP=[0.68], TIMP=[0.85],
1553 DWF=[0](cms), LOSS=[1]:
1554 | Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1555 | F=[0.00](mm),
1556 | Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1557 | MNP=[0.250], SCP=[0](min),

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1558 [ 0.047 , 0.033 ]
1559 [ 0.065 , 0.038 ]
1560 [ 0.081 , 0.045 ]
1561 [ 0.104 , 0.048 ]
1562 [ 0.120 , 0.053 ]
1563 [ -1 , -1 ] (max twenty pts)
1564 NHYDovf= [ "C7-OVF" ]
1565 *%
1566 CONTINUOUS STANDHYD NHYD= [ "ST-6" ], DT=[1]min, AREA=[0.41](ha), XIMP=[0.46], TIMP=[0.57],
1567 DWF=[0](cms), LOSS=[1]:
1568 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1569 F=[0.00](mm),
1570 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1571 MNP=[0.250], SCP=[0](min),
1572 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[90.554](m),
1573 MNI=[0.013], SCI=[0](min),
1574 Continuous simulation parameters:
1575 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
1576 END=-1
1577 *%
1578 ROUTE RESERVOIR NHYDout= [ "ST6STR" ], NHYDin= [ "ST-6" ], RDT=[1](min),
1579 TABLE of ( OUTFLOW-STORAGE ) values
1580 (cms) - (ha-m)
1581 [ 0.000 , 0.0000 ]
1582 [ 0.036 , 0.0010 ]
1583 [ 0.037 , 0.0058 ]
1584 [ -1 , -1 ] (max twenty pts)
1585 NHYDovf= [ "ST6OVF" ]
1586 *%
1587 *ANALYSIS POINT 5 - TOTAL FLOW AT OUTLET OF STREET 6
1588 *%
1589 ADD HYD NHYDsum= [ "PT5ST6" ], NHYDs to
1590 add= [ "PT4ST5" + "C6-STR" + "C6-OVF" + "C7-STR" + "C7-OVF" + "ST6STR" + "ST6OVF" ]
1591 *%
1592 *ROUTE FLOW through O'Keefe Drain 4
1593 ROUTE CHANNEL NHYDout= [ "DRAIN4" ], NHYDin= [ "PT5ST6" ], RDT=[1](min),
1594 CHLGTH=[324]{m}, CHSLOPE=[.10](%), FPSLOPE=[.10](%),
1595 SECNUM=[1], NSEG=[3]
1596 ( SEGRROUGH, SEGDIST (m))=[0.07,12.00 -0.043,18.00 0.07,30.00] NSEG
1597 times
1598 ( DISTANCE (m), ELEVATION (m))=[0.00, 2.00]
1599 (2.00, 1.20)
1600 (12.00, 1.00)
1601 (14.00, 0.00)
1602 (16.00, 0.00)
1603 (18.00, 1.00)
1604 (28.00, 1.20)
1605 (30.00, 2.00)
1606 *%
1607 CONTINUOUS NASHYD NHYD= [ "D4" ], DT=[1]min, AREA=[1.73](ha), DWF=[0](cms), CN/C=[88],
1608 IA=[8.4](mm),
1609 N=[3], TP=[0.60]hrs,
1610 Continuous simulation parameters:
1611 IaRECper=[4](hrs),
1612 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1613 InterEventTime=[12](hrs)
1614 Baseflow simulation parameters:
1615 BaseFlowOption=[1] ,
1616 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1617 VHydCond=[0.055](mm/hr), END=-1
1618 *%
1619 CONTINUOUS STANDHYD NHYD= [ "Area-B" ], DT=[1]min, AREA=[24.04](ha), XIMP=[0.62],
1620 TIMP=[0.77], DWF=[0](cms), LOSS=[1]:
1621 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1622 F=[0.00](mm),
1623 Pervious areas: IAper=[4.67](mm), SLPP=[1.4](%), LGP=[50](m),

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1614 MNP=[0.250], SCP=[0](min),
1615 Impervious areas: IAimp=[1.57](mm), SLPI=[1.4](%),
1616 LGI=[693.397](m), MNI=[0.013], SCI=[0](min),
1617 Continuous simulation parameters:
1618 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
1619 END=-1
1620 *%-----|-----|
1621 ROUTE RESERVOIR NHYDout=[ "SWMF-B" ], NHYDin=[ "Area-B" ], RDT=[1](min),
1622 TABLE of ( OUTFLOW-STORAGE ) values
1623 (cms) - (ha-m)
1624 [ 0.000 , 0.000 ]
1625 [ 0.025 , 0.090 ]
1626 [ 0.175 , 0.510 ]
1627 [ 0.350 , 0.710 ]
1628 [ 0.495 , 0.820 ]
1629 [ 0.648 , 0.980 ]
1630 [ 0.965 , 1.045 ]
1631 [ 1.072 , 1.140 ]
1632 [ -1 , -1 ] (max twenty pts)
1633 NHYDovf=[ "SWMBOVF" ]
1634 *%-----|-----|
1635 ADD HYD NHYDsum=[ "D4-EX" ], NHYDs to add=[ "DRAIN4"+"D4"+"SWMF-B"+"SWMBOVF" ]
1636 *%-----|-----|
1637 *ROUTE FLOW THROUGH O'Keefe Drain 5
1638 * JFSA: Nov. 2020, added en points to close X-Section
1639 ROUTE CHANNEL NHYDout=[ "DRAIN5" ], NHYDin=[ "D4-EX" ], RDT=[1](min),
1640 CHLGTH=[413.0](m), CHSLOPE=[0.16](%), FPSLOPE=[0.16](%),
1641 SECNUM=[1], NSEG=[3]
1642 ( SEROUGH, SEGDIST (m))=[0.043,12.29 -0.033,17.97
1643 0.043,32.84] NSEG times
1644 ( DISTANCE (m), ELEVATION (m))=(-0.01, 2.50)
1645 [0.00, 1.41]
1646 [6.13, 0.97]
1647 [12.29, 0.89]
1648 [15.71, 0.00]
1649 [17.97, 0.39]
1650 [23.04, 0.35]
1651 [32.83, 0.96]
1652 (32.84, 2.50)
1653 *%-----|-----|
1654 CONTINUOUS NASHYD NHYD=[ "D5" ], DT=[1]min, AREA=[1.90](ha),
1655 DWF=[0](cms), CN/C=[86], IA=[8.7](mm), N=[3], TP=[0.69]hrs,
1656 Continuous simulation parameters:
1657 IaRECper=[4](hrs),
1658 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1659 InterEventTime=[12](hrs)
1660 Baseflow simulation parameters:
1661 BaseFlowOption=[1] ,
1662 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1663 VHydCond=[0.055](mm/hr), END=-1
1664 *%-----|-----|
1665 *EXTERNAL FLOWS SOUTHEAST OF THE SITE NORTH OF McKENNA CASEY DR.
1666 CONTINUOUS NASHYD NHYD=[ "O-13SDF" ], DT=[1]min, AREA=[9.74](ha),
1667 DWF=[0](cms), CN/C=[81], IA=[4.0](mm), N=[3], TP=[.43]hrs,
1668 Continuous simulation parameters:
1669 IaRECper=[4](hrs),
1670 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1671 InterEventTime=[12](hrs)
1672 Baseflow simulation parameters:
1673 BaseFlowOption=[1] ,
1674 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1675 VHydCond=[0.055](mm/hr), END=-1
1676 *%-----|-----|
1677 *SNOW DISPOSAL FACILITY
1678 *PARAMETERS BASED ON ROBINSON 2006 MODEL
1679 ROUTE RESERVOIR NHYDout=[ "SDF" ], NHYDin=[ "O-13SDF" ], RDT=[1](min),

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1677 TABLE of ( OUTFLOW-STORAGE ) values
1678 (cms) - (ha-m)
1679 [0.000,0.000]
1680 [0.150,0.600]
1681 (0.200,1.500)
1682 [-1 , -1 ] (max twenty pts)
1683 NHYDovf=[ "OVFSDF" ]
1684 *%-----|-----|
1685 *ANALYSIS POINT 6 - McKenna Casey Dr.
1686 *%-----|-----|
1687 ADD HYD NHYDsum=[ "PT6MC" ], NHYDs to add=[ "DRAIN5"+"D5"+"SDF" ]
1688 *%-----|-----|
1689 CONTINUOUS NASHYD NHYD=[ "O-15" ], DT=[1]min, AREA=[10.67](ha),
1690 DWF=[0](cms), CN/C=[82], IA=[7.5](mm), N=[3], TP=[0.30]hrs,
1691 Continuous simulation parameters:
1692 IaRECper=[4](hrs),
1693 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1694 InterEventTime=[12](hrs)
1695 Baseflow simulation parameters:
1696 BaseFlowOption=[1],
1697 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1698 VHydCond=[0.055](mm/hr), END=-1
1699 *%-----|-----|
1700 *TOTAL FLOW NORTH OF McKENNA CASEY DR.
1701 ADD HYD NHYDsum=[ "M-C" ], NHYDs to add=[ "PT6MC"+"O-15" ]
1702 *%-----|-----|
1703 *ROUTE FLOW THROUGH AREA O-14
1704 * JFSA: Nov. 2020, added end points to close X-section
1705 ROUTE CHANNEL NHYDout=[ "O-14Ch" ], NHYDin=[ "M-C" ], RDT=[1](min),
1706 CHLGH=845.3(m), CHSLOPE=[0.10](%), FPSLOPE=[0.10](%),
1707 SECNUM=[1], NSEG=[3]
1708 ( SEGROUGH, SEGDIST (m))=[0.06,15.00 -0.033,18.04 0.06,31.85] NSEG
times
1709 ( DISTANCE (m), ELEVATION (m))=[-0.01, 2.5
1710 (0.00, 1.53]
1711 (5.56, 1.47)
1712 (9.21, 1.45)
1713 (12.45, 1.53)
1714 (13.70, 1.50)
1715 (15.00, 0.69)
1716 (15.34, 0.00)
1717 (16.51, 0.05)
1718 (17.30, 0.17)
1719 (18.04, 0.74)
1720 (19.29, 1.32)
1721 (22.73, 1.47)
1722 (31.84, 1.41)
1723 (31.85, 2.50)
1724 *%-----|-----|
1725 *% -Change O-14 from NASHYD to STANDHYD, name it "S-1-Okeefe" and add it to S-1
subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
1726 *% -JFSA 2021-02-16, add detailed subcatchment drainage area for each subcatchment
in Corrigan sub-catchment. After adding part of O-14 to S_1 sub-catchment so O-14
becomes 5 ha instead of 30.02 ha and TP becomes 0.133 (5*0.8/30.02) instead of 0.8
1727 CONTINUOUS NASHYD NHYD=[ "O-14" ], DT=[1]min, AREA=[5](ha),
1728 DWF=[0](cms), CN/C=[82], IA=[7.5](mm), N=[3], TP=[0.133]hrs,
1729 Continuous simulation parameters:
1730 IaRECper=[4](hrs),
1731 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1732 InterEventTime=[12](hrs)
1733 Baseflow simulation parameters:
1734 BaseFlowOption=[1],
1735 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1736 VHydCond=[0.055](mm/hr), END=-1
1737 *
1738 *%-----|-----|

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1739 *ANALYSIS POINT 7 - JOCK RIVER
1740 * 2020-12-01 To Foster Drain
1741 * 2020-12-01 replace ("PT7JR") by ("OKEEFE")
1742 *%
1743 ADD HYD          NHYDsum=[ "OKEEFE" ], NHYDs to add=[ "O-14Ch"+"O-14" ]
1744 *%
1745 *CONTINUOUS STANDHYD NHYD=[ "OKEEFE" ], DT=[1](min), AREA=[ 448 ](ha),
1746 *           XIMP=[ 0.65 ], TIMP=[ 0.65 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
1747 *           SCS curve number CN=[ 77 ],
1748 *           Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%),
1749 *           LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
1750 *           Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%),
1751 *           LGI=[ 1728 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1752 *           Continuous simulation parameters:
1753 *           IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
1754 *           SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1755 *           InterEventTime=[ 18 ](hrs), END=-1
1756 *#*****
1757 *# Okeefe Pond
1758 *# - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1759 *# and a ratio of the catchment area to the West Clarke pond rating curve
1760 *# from the MSS for the next coordinates
1761 *#*****
1762 *ROUTE RESERVOIR      NHYDout=[ "P_OKE" ], NHYDin=[ "OKEEFE" ],
1763 *           RDT=[ 1 ](min),
1764 *           TABLE of ( OUTFLOW-STORAGE ) values
1765 *           (cms) - (ha-m)
1766 *           [ 0.0 , 0.0 ]
1767 *           [ 14.13 , 13.0 ]
1768 *           [ -1 , -1 ] (maximum one hundred pairs of points)
1769 *           NHYDovf=[ "ok-OVF" ],
1770 *%
1771 * -JFSA 2021-02-25 "S-1-D2" and "S-1-D3" are part of S-1 sub-catchment. They are
1772 moved to drain before station 6215 on Jock River
1773 CONTINUOUS STANDHYD NHYD=[ "S-1-D2" ], DT=[ 1 ](min), AREA=[ 18.67 ](ha), XIMP=[ 0.65 ],
1774 *           TIMP=[ 0.65 ], DWF=[ 0 ](cms),
1775 *           LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
1776 *           IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%),
1777 *           LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min), Impervious surfaces:
1778 *           IAimp=[ 1.57 ](mm), SLPI=[ 0.75 ](%),
1779 *           LGI=[ 352.798 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
1780 *           Continuous simulation parameters:
1781 *           IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
1782 *           SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1783 *           InterEventTime=[ 12 ](hrs), END=-1
1784 *%
1785 *CONTINUOUS NASHYD    NHYD=[ "S-1-D2" ], DT=[ 1 ]min, AREA=[ 18.67 ](ha),
1786 *           DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
1787 *           N=[ 3 ], TP=[ 1.120 ]hrs,
1788 *           Continuous simulation parameters:
1789 *           IaRECper=[ 4 ](hrs),
1790 *           SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
1791 *           InterEventTime=[ 12 ](hrs)
1792 *           Baseflow simulation parameters:
1793 *           BaseFlowOption=[ 1 ],
1794 *           InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
1795 *           VHdCond=[ 0.055 ](mm/hr), END=-1
1796 *%
1797 COMPUTE DUALHYD      NHYDin=[ "S-1-D2" ], CINLET=[ 2.097 ](cms), NINLET=[ 1 ],
1798 *           MajNHYD=[ "S-1-D2J" ]
1799 *           MinNHYD=[ "S-1-D2N" ]
1800 *           TMJSTO=[ 9999999 ](cu-m)
1801 *%
1802 ADD HYD              NHYDsum=[ "S-1-D2S" ], NHYDs to add=[ "S-1-D2J"+"S-1-D2N" ]
1803 *%

```

```

1800 ROUTE RESERVOIR      NHYDout=[ "S-1-D2R" ] ,NHYDin=[ "S-1-D2S" ] ,
1801                                         RDT=[1](min),
1802                                         TABLE of ( OUTFLOW-STORAGE ) values
1803                                         (cms) - (ha-m)
1804                                         [ 0.0 , 0.0 ]
1805                                         [ 0.2231, 0.7445 ]
1806                                         [ -1 , -1 ] (max twenty pts)
1807                                         NHYDovf=[ "S-1-D2Rovf" ]
1808 *%-----|-----|
1809 CONTINUOUS STANDHYD NHYD=[ "S-1-D3" ] , DT=[1](min), AREA=[6.79](ha), XIMP=[0.65],
1810 TIMP=[0.65], DWF=[0](cms),
1811                                         LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
1812                                         IAper=[4.67](mm), SLPP=[2.0](%),
1813                                         LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
1814                                         IAimp=[1.57](mm), SLPI=[0.75](%),
1815                                         LGI=[212.760](m), MNI=[0.013], SCI=[0](min),
1816                                         Continuous simulation parameters:
1817                                         IaRECper=[4](hrs), IaRECImp=[4](hrs),
1818                                         SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1819                                         InterEventTime=[12](hrs), END=-1
1820 *%-----|-----|
1821 *CONTINUOUS NASHYD   NHYD=[ "S-1-D3" ], DT=[1]min, AREA=[6.79](ha),
1822 *                                         DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
1823 *                                         N=[3], TP=[1.281]hrs,
1824 *                                         Continuous simulation parameters:
1825 *                                         IaRECper=[4](hrs),
1826 *                                         SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1827 *                                         InterEventTime=[12](hrs)
1828 *                                         Baseflow simulation parameters:
1829 *                                         BaseFlowOption=[1],
1830 *                                         InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1831 *                                         VHdCond=[0.055](mm/hr), END=-1
1832 *%-----|-----|
1833 COMPUTE DUALHYD      NHYDin=[ "S-1-D3" ], CINLET=[0.831](cms), NINLET=[1],
1834 MajNHYD=[ "S-1-D3J" ]
1835 MinNHYD=[ "S-1-D3N" ]
1836 TMJSTO=[9999999](cu-m)
1837 *%-----|-----|
1838 ADD HYD               NHYDs[ "S-1-D3S" ], NHYDs to add=[ "S-1-D3J"+ "S-1-D3N" ]
1839 *%-----|-----|
1840 ROUTE RESERVOIR      NHYDout=[ "S-1-D3R" ] ,NHYDin=[ "S-1-D3S" ] ,
1841 RDT=[1](min),
1842                                         TABLE of ( OUTFLOW-STORAGE ) values
1843                                         (cms) - (ha-m)
1844                                         [ 0.0 , 0.0 ]
1845                                         [ 0.0811, 0.2708 ]
1846                                         [ -1 , -1 ] (max twenty pts)
1847                                         NHYDovf=[ "S-1-D3Rovf" ]
1848 *%-----|-----|
1849 ADD HYD               NHYDs[ "SN_OK" ], NHYDs to
1850 add=[ "N_OK"+ "OKEEFE"+ "S-1-D2R"+ "S-1-D3R"+ "S-1-D2Rovf"+ "S-1-D3Rovf" ]
1851 *%-----|-----|
1852 SAVE HYD              NHYD=[ "SN_OK" ], # OF PCYCLES=[-1], ICASEsh=[1]
1853                                         HYD_COMMENT=[ "Total Flows at Okeefe Drain" ]
1854 *#-----|-----|
1855 *# Hydrograph from Node Okeefe routed to Node at Foster Drain
1856 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
1857 *#
1858 ROUTE CHANNEL          NHYDout=[ "N_FO" ] ,NHYDin=[ "SN_OK" ] ,
1859 RDT=[1](min),
1860 CHLGTH=[1183](m), CHSLOPE=[0.0761](%), FPSLOPE=[0.0761](%),
1861 SECNUM=[1.0], NSEG=[3]
1862 ( SEGROUGH, SEGDIST (m))=
1863 [0.050,-33.89]

```

```

1862          -0.035,31.59
1863          0.050,34.41] NSEG times
1864          ( DISTANCE (m), ELEVATION (m))=
1865          [-794.18, 91.00]
1866          [-775.41, 91.50]
1867          [-702.63, 91.50]
1868          [-546.19, 91.50]
1869          [-529.54, 91.50]
1870          [-323.44, 91.00]
1871          [-320.71, 91.00]
1872          [-183.59, 91.00]
1873          [-182.54, 90.50]
1874          [-181.36, 90.00]
1875          [-177.37, 90.00]
1876          [-87.70, 90.00]
1877          [-33.89, 90.00]
1878          [-18.52, 86.88]
1879          [0.00,85.20]
1880          [16.20, 86.83]
1881          [31.59, 90.00]
1882          [33.03, 90.50]
1883          [34.41, 91.00]
1884 *%-----|-----|
1885 *#*****
1886 *#      Catchment FOSTER
1887 *#      - To Foster ditch (north of the Jock)
1888 *#      - Partially developed (medium density); remaining agricultural
1889 *#      - 2020-12-01 JFSA Foster area is 332 as per Foster SWMF Environmental Study
Report, CH2MHILL, Aug 2013.
1890 *#      - 2020-12-01 decrease Foster drainage area from (373 HA) to (307.98 HA) after
increasing Okeefe drainage area to (513.02 HA) so the total drainage area remains the
same
1891 *#      - 2021-02-12 update Foster area to 325.44 ha as measured from QGIS
1892 *#*****
1893 CONTINUOUS STANDHYD NYHD=[ "FOSTER"], DT=[1]min, AREA=[ 325.44](ha),
1894 XIMP=[ 0.55], TIMP=[ 0.55], DWF=[ 0](cms), LOSS=[ 2],
1895 SCS curve number CN=[ 74],
1896 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 0.5](%),
1897 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
1898 Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 0.5](%),
1899 LGI=[ 1472.956](m), MNI=[ 0.013], SCI=[ 0](min),
1900 Continuous simulation parameters:
1901 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
1902 SMIN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1903 InterEventTime=[ 18](hrs), END=-1
1904 *#*****
1905 *#      Foster Pond
1906 *#      - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1907 *#      and a ratio of the catchment area to the West Clarke pond rating curve
1908 *#      from the MSS for the next coordinates
1909 *#*****
1910 ROUTE RESERVOIR NYHDout=[ "P_FOS"], NYHDin=[ "FOSTER"],
1911 RDT=[ 1](min),
1912          TABLE of ( OUTFLOW-STORAGE ) values
1913          (cms) - (ha-m)
1914          [ 0.0 , 0.0 ]
1915          [ 10.34 , 10 ]
1916          [ -1 , -1 ] (max twenty pts)
1917          NYDovf=[ "FO-OVF" ]
1918 *%-----|-----|
1919 ADD HYD          NYHDSum=[ "FOSTER-OUT" ], NYHDs to add=[ "P_FOS"+ "FO-OVF" ]
1920 *%-----|-----|
1921 *#*****
1922 *      -Brazeau area from P 1800-19 =[71.751], change to 63.59 ha based on GIS measurements
1923 *      -JFSA, 2021-01-19 update "W_CLAR_BRAZ" to 73.29 ha based on GIS measurements
1924 *      -JFSA, 2021-01-22 Brazeau ("MS_P10"+ "P10-OVF")brazeau pond discharges directly

```



```

1988 *%
1989 ADD HYD NHYDsum= [ "S-1-FO-D2S" ] , NHYDs to add=[ "S-1-FO-D2J"+"S-1-FO-D2N" ]
1990 *%
1991 ROUTE RESERVOIR NHYDout=[ "S-1-FO-D2R" ] ,NHYDin=[ "S-1-FO-D2S" ] ,
1992 RDT=[1](min),
1993 TABLE of ( OUTFLOW-STORAGE ) values
1994 (cms) - (ha-m)
1995 [ 0.0 , 0.0 ]
1996 [ 0.0590, 0.1970 ]
1997 [ -1 , -1 ] (max twenty pts)
1998 NHYDovf=[ "S-1FOD2ovf" ]
1999 *%
2000 ADD HYD NHYDsum= [ "980" ] , NHYDs to
add=[ "FOSTER-OUT"+"S-1-FO-D2R"+"S-1FOD2ovf" ]
2001 *%
2002 SAVE HYD NHYD= [ "980" ] , # OF PCYCLES=[-1], ICASEsh=[1]
2003 HYD_COMMENT=[ "Total Flows at Station 980 on Foster Drain" ]
2004 *%
2005 *#
2006 *# Hydrograph from Node Foster SWM (Station 980)to Node at station 520
2007 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 980
2008 *#
2009 ROUTE CHANNEL NHYDout=[ "980-out" ] ,NHYDin=[ "980" ] ,
2010 RDT=[1](min),
2011 CHLGTH=[460](m), CHSLOPE=[ 0.04348 ](%) ,
2012 FPSLOPE=[ 0.04348 ](%) ,
2013 SECNUM=[1.0] , NSEG=[3]
2014 ( SEGROUGH, SEGDIST (m))=
2015 [ 0.050, 45.90
2016 -0.035, 53.30
2017 0.050, 100 ] NSEG times
2018 ( DISTANCE (m), ELEVATION (m))=
2019 [ 0, 91.75 ]
2020 [ 42.4, 92.18 ]
2021 [ 43.5, 92.16 ]
2022 [ 44.1, 92.1 ]
2023 [ 44.6, 92 ]
2024 [ 44.8, 91.86 ]
2025 [ 45.9, 91.04 ]
2026 [ 46.4, 90.65 ]
2027 [ 46.8, 90.36 ]
2028 [ 47.9, 90.32 ]
2029 [ 48.7, 90.35 ]
2030 [ 50.7, 90.33 ]
2031 [ 52.2, 90.38 ]
2032 [ 52.5, 90.59 ]
2033 [ 53.3, 91.28 ]
2034 [ 54, 91.83 ]
2035 [ 54.3, 92 ]
2036 [ 54.8, 92.08 ]
2037 [ 55.4, 92.12 ]
2038 [ 100, 91.84 ]
2039 *%
2040 * -JFSA 2021-02-26 "S-1-FO-D1" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2041 CONTINUOUS STANDHYD NHYD=[ "S-1-FO-D1" ], DT=[1]min, AREA=[ 5.11 ](ha),
2042 XIMP=[ 0.65 ], TIMP=[ 0.65 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
2043 SCS curve number CN=[ 74 ],
2044 Previous surfaces: IApert=[ 4.67 ](mm), SLPP=[ 0.5 ](%) ,
2045 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
2046 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%) ,
2047 LGI=[ 184.572 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
2048 Continuous simulation parameters:
2049 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
2050 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2051 InterEventTime=[ 18 ](hrs), END=-1

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2052 *%
2053 COMPUTE DUALHYD      NHYDin=[ "S-1-FO-D1" ], CINLET=[ 0.605 ](cms), NINLET=[ 1 ],
2054                                         MajNHYD=[ "S-1-FO-D1J" ]
2055                                         MinNHYD=[ "S-1-FO-D1N" ]
2056                                         TMJSTO=[ 9999999 ](cu-m)
2057 *%
2058 ADD HYD               NHYDsum=[ "S-1-FO-D1S" ], NHYDs to add=[ "S-1-FO-D1N"+"S-1-FO-D1J" ]
2059 *%
2060 ROUTE RESERVOIR     NHYDout=[ "S-1-FO-D1R" ] ,NHYDin=[ "S-1-FO-D1S" ] ,
2061                                         RDT=[ 1 ](min),
2062                                         TABLE of ( OUTFLOW-STORAGE ) values
2063                                         (cms) - (ha-m)
2064                                         [ 0.0 , 0.0 ]
2065                                         [ 0.0611, 0.2038 ]
2066                                         [ -1 , -1 ] (max twenty pts)
2067                                         NHYDovf=[ "S-1FOD1ovf" ]
2068 *%
2069 ADD HYD               NHYDsum=[ "520" ], NHYDs to add=[ "980-out"+"S-1-FO-D1R"+"S-1FOD1ovf" ]
2070 *%
2071 SAVE HYD              NHYD=[ "520" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
2072                                         HYD_COMMENT=[ "Total Flows at Sation 520 on Foster Drain" ]
2073 *%
2074 *# Hydrograph from Node at Station 520 (Foster Drain) to Node at station 6016 (Jock
2075 River)
2076 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 520
2077 *#
2078 ROUTE CHANNEL          NHYDout=[ "520-out" ] ,NHYDin=[ "520" ] ,
2079                                         RDT=[ 1 ](min),
2080                                         CHLGTH=[ 860 ](m), CHSLOPE=[ 0.5872 ](%),
2081                                         FPSLOPE=[ 0.5872 ](%),
2082                                         SECNUM=[ 1.0 ], NSEG=[ 3 ]
2083                                         ( SEGROUGH, SEGDIST (m))=
2084                                         [ 0.050,45.90
2085                                         -0.035,54.3
2086                                         0.050,100.1097] NSEG times
2087                                         ( DISTANCE (m), ELEVATION (m))=
2088                                         [ 0, 91.26 ]
2089                                         [ 44.9, 91.46 ]
2090                                         [ 45.1, 91.37 ]
2091                                         [ 45.9, 90.84 ]
2092                                         [ 47, 90.32 ]
2093                                         [ 47.5, 90.22 ]
2094                                         [ 48, 90.17 ]
2095                                         [ 50.7, 90.19 ]
2096                                         [ 51.5, 90.17 ]
2097                                         [ 52.2, 90.13 ]
2098                                         [ 52.7, 90.12 ]
2099                                         [ 53.3, 90.14 ]
2100                                         [ 53.5, 90.31 ]
2101                                         [ 53.9, 90.59 ]
2102                                         [ 54.3, 90.87 ]
2103                                         [ 54.7, 91.04 ]
2104                                         [ 55.3, 91.24 ]
2105                                         [ 55.5, 91.26 ]
2106                                         [ 63.7, 91.37 ]
2107                                         [ 100.1097, 91.43 ]
2108 *%-----|-----|
2108 * -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2109 CONTINUOUS STANDHYD    NHYD=[ "S-1-FO-F-D" ], DT=[ 1 ]min, AREA=[ 14.96 ](ha),
2110                                         XIMP=[ 0.65 ], TIMP=[ 0.65 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
2111                                         SCS curve number CN=[ 74 ],
2112                                         Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 0.5 ](%),
2113                                         LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
2114                                         Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%),
2115                                         LGI=[ 315.806 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),

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2116           Continuous simulation parameters:
2117           IaRECper=[4](hrs), IaRECImp=[4](hrs),
2118           SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2119           InterEventTime=[18](hrs), END=-1
2120 *%----- | -----
2121 *CONTINUOUS NASHYD   NHYD=[ "S-1-FO-F-D" ], DT=[1]min, AREA=[14.96](ha),
2122 *          DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2123 *          N=[3], TP=[1.007]hrs,
2124 *          Continuous simulation parameters:
2125 *          IaRECper=[4](hrs),
2126 *          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2127 *          InterEventTime=[12](hrs)
2128 *          Baseflow simulation parameters:
2129 *          BaseFlowOption=[1],
2130 *          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2131 *          VHdCond=[0.055](mm/hr), END=-1
2132 *%----- | -----
2133 COMPUTE DUALHYD   NHYDin=[ "S-1-FO-F-D" ], CINLET=[1.615](cms), NINLET=[1],
2134 MajNHYD=[ "S-1FO-F-DJ" ]
2135 MinNHYD=[ "S-1FO-F-DN" ]
2136 TMJSTO=[99999999](cu-m)
2137 *%----- | -----
2138 ADD HYD      NHYDsum=[ "S-1FO-F-DS" ], NHYDs to add=[ "S-1FO-F-DJ" +"S-1FO-F-DN" ]
2139 *%----- | -----
2140 ROUTE RESERVOIR NHYDout=[ "S-1FO-F-DR" ] ,NHYDin=[ "S-1FO-F-DS" ],
2141 RDT=[1](min),
2142             TABLE of ( OUTFLOW-STORAGE ) values
2143             (cms) - (ha-m)
2144             [ 0.0 , 0.0 ]
2145             [ 0.1788, 0.5966 ]
2146             [ -1 , -1 ] (max twenty pts)
2147             NHYDovf=[ "S-1FoFDovf" ]
2148 *%----- | -----
2149 * -JFSA 2021-02-26 "S-1-D8" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2150 CONTINUOUS STANDHYD NHYD=[ "S-1-D8" ], DT=[1]min, AREA=[5.27](ha), XIMP=[0.325],
2151 TIMP=[0.65], DWF=[0](cms), LOSS=[1]:
2152             Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
2153             F=[0.00](mm),
2154             Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
2155             MNP=[0.250], SCP=[0](min),
2156             Impervious areas: IAimp=[0.785](mm), SLPI=[0.75](%),
2157             LGI=[187.439](m), MNI=[0.013], SCI=[0](min),
2158             Continuous simulation parameters:
2159             IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
2160             END=-1
2161 *%----- | -----
2162 *CONTINUOUS NASHYD   NHYD=[ "S-1-D8" ], DT=[1]min, AREA=[5.27](ha),
2163 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2164 N=[3], TP=[1.10]hrs,
2165 Continuous simulation parameters:
2166 IaRECper=[4](hrs),
2167 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2168 InterEventTime=[12](hrs)
2169 Baseflow simulation parameters:
2170 BaseFlowOption=[1],
2171 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2172 VHdCond=[0.055](mm/hr), END=-1
2173 *%----- | -----
2174 COMPUTE DUALHYD   NHYDin=[ "S-1-D8" ], CINLET=[0.672](cms), NINLET=[1],
2175 MajNHYD=[ "S-1-D8J" ]
2176 MinNHYD=[ "S-1-D8N" ]
2177 TMJSTO=[99999999](cu-m)
2178 *%----- | -----
2179 ADD HYD      NHYDsum=[ "S-1-D8S" ], NHYDs to add=[ "S-1-D8J" +"S-1-D8N" ]
2180 *%----- | -----

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2176 *ADD HYD           NHYDsum=[ "S-1-D" ], NHYDs to add=[ "S-1-Okeefe"+"S-1"+"S-1-Fost" ]
2177 *%
2178 *COMPUTE DUALHYD   NHYDin=[ "S-1-D" ], CINLET=[11.616](cms), NINLET=[1],
2179 *
2180 *                MajNHYD=[ "S-1-D-MJ" ]
2181 *                MinNHYD=[ "S-1-D-MN" ]
2182 *                TMJSTO=[ 5974 ](cu-m)
2183 *%
2184 *ADD HYD           NHYDsum=[ "S-1-DEV" ], NHYDs to add=[ "S-1-D-MJ"+"S-1-D-MN" ]
2185 *%
2186 ROUTE RESERVOIR   NHYDout=[ "S-1-D8R" ] , NHYDin=[ "S-1-D8S" ] ,
2187 RDT=[ 1 ](min),
2188             TABLE of ( OUTFLOW-STORAGE ) values
2189             (cms) - (ha-m)
2190             [ 0.0 , 0.0 ]
2191             [ 0.0630 , 0.2102 ]
2192             [ -1 , -1 ] (max twenty pts)
2193 NHYDovf=[ "S-1-D8Rovf" ]
2194 *%
2195 * -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
2196 before station 6016 on Jock River
2197 CONTINUOUS NASHYD  NHYD=[ "S-1-A" ], DT=[ 1 ]min, AREA=[ 75.88 ](ha),
2198 DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
2199 N=[ 3 ], TP=[ 0.619 ]hrs,
2200 Continuous simulation parameters:
2201 IaRECper=[ 4 ](hrs),
2202 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2203 InterEventTime=[ 12 ](hrs)
2204 Baseflow simulation parameters:
2205 BaseFlowOption=[ 1 ],
2206 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2207 VHydCond=[ 0.055 ](mm/hr), END=-1
2208 *%
2209 * -JFSA, 2021-01-22 "W_CLAR_UNDE" (west of Clarke sub-catchment) discharges
2210 directly to the jock river through a road side ditch on the west side of Borrisokane
2211 road (station 6016)
2212 CONTINUOUS NASHYD  NHYD=[ "W_CLAR_UNDE" ], DT=[ 1 ]min, AREA=[ 35.65 ](ha),
2213 DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
2214 N=[ 3 ], TP=[ 1.10 ]hrs,
2215 Continuous simulation parameters:
2216 IaRECper=[ 4 ](hrs),
2217 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2218 InterEventTime=[ 12 ](hrs)
2219 Baseflow simulation parameters:
2220 BaseFlowOption=[ 1 ],
2221 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2222 VHydCond=[ 0.055 ](mm/hr), END=-1
2223 *%
2224 ADD HYD            NHYDsum=[ "SN_FO" ], NHYDs to
2225 add=[ "N_FO"+"520-out"+"MS_P10"+"P10-OVF"+"W_CLAR_UNDE"+"S-1FoFDovf"+"S-1FO-F-DR"+"S-1-D8R"
2226 ovf+"S-1-D8R"+"S-1-A" ]
2227 *%
2228 SAVE HYD           NHYD=[ "SN_FO" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
2229             HYD_COMMENT=[ "Total Flows at Foster Drain" ]
2230 *%
2231 *# Hydrograph from Node Foster routed to Node at Cedarview Road
2232 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6016
2233 *#
2234 ROUTE CHANNEL       NHYDout=[ "N_CE" ] , NHYDin=[ "SN_FO" ] ,
2235 RDT=[ 1 ](min),
2236 CHLGTH=[ 159 ](m), CHSLOPE=[ 0.0818 ](%),
2237 FPSLOPE=[ 0.0818 ](%),
2238 SECNUM=[ 1.0 ], NSEG=[ 3 ]
2239 ( SEGROUGH, SEGDIST (m))=
2240     [ 0.050,-15.46
2241     -0.035,26.55
2242     0.050,116.76 ] NSEG times

```

```

2237      ( DISTANCE (m), ELEVATION (m) )=
2238      [-645.23, 91.50]
2239      [-391.20, 91.50]
2240      [-91.00, 91.50]
2241      [-85.52, 91.50]
2242      [-15.46, 89.40]
2243      [-9.79, 89.31]
2244      [-3.22, 86.24]
2245      [3.22, 85.07]
2246      [10.96, 85.79]
2247      [16.44, 86.49]
2248      [26.55, 89.45]
2249      [29.03, 90.27]
2250      [35.76, 90.67]
2251      [36.67, 91.00]
2252      [108.08, 91.00]
2253      [109.82, 90.50]
2254      [112.04, 90.50]
2255      [114.62, 91.00]
2256      [116.76, 91.50]
2257 *%-----+-----+-----+
2258 *#*****
2259 *#      Catchment S-1
2260 *#      - To Jock River (north and south of Jock)
2261 *#      - Primarily agricultural fields; portion of sand quarry
2262 *%-----+-----+
2263 *%      -2020-12-17 "S-1-Undeveloped" and "S-1-Fost" was a part of Foster drain, they are below
the foster pond. Now they are added to S-1 subcatchment based on Project 1474-BCDC,
JFSA, Nov. 2020
2264 *%      -2020-12-17 Change O-14 (it was part of Okeefe drain) to "S-1-Okeefe" and add it
to S-1 subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
2265 *%      -2020-12-17 Add "S-1-BCDC" as NASHYD
2266 *%      -2020-12-17 all other S-1 subcatchment as STANDHYD with DUALHYD and ROUTE RESERVOIR
2267 *%-----+-----+
2268 *#*****
2269 *      -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2270 *CONTINUOUS NASHYD    NHYD=[ "S-1-A" ], DT=[1]min, AREA=[ 75.88 ](ha),
2271 *                      DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
2272 *                      N=[ 3 ], TP=[ 0.619 ]hrs,
2273 *                      Continuous simulation parameters:
2274 *                      IaRECper=[ 4 ](hrs),
2275 *                      SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2276 *                      InterEventTime=[ 12 ](hrs)
2277 *                      Baseflow simulation parameters:
2278 *                      BaseFlowOption=[ 1 ],
2279 *                      InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2280 *                      VHydCond=[ 0.055 ](mm/hr), END=-1
2281 *%-----+-----+
2282 CONTINUOUS NASHYD    NHYD=[ "S-1-B" ], DT=[1]min, AREA=[ 55.36 ](ha),
2283 *                      DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
2284 *                      N=[ 3 ], TP=[ 0.451 ]hrs,
2285 *                      Continuous simulation parameters:
2286 *                      IaRECper=[ 4 ](hrs),
2287 *                      SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2288 *                      InterEventTime=[ 12 ](hrs)
2289 *                      Baseflow simulation parameters:
2290 *                      BaseFlowOption=[ 1 ],
2291 *                      InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2292 *                      VHydCond=[ 0.055 ](mm/hr), END=-1
2293 *%-----+-----+
2294 *#      - JFSA 2021-02-24 change the name from S-1-BCDC to S-1-A and S-1-B. Change their
TP values based on the new areas compared to the old ones.
2295 *CONTINUOUS NASHYD    NHYD=[ "S-1-BCDC" ], DT=[1]min, AREA=[ 134.9 ](ha),
2296 *                      DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
2297 *                      N=[ 3 ], TP=[ 1.10 ]hrs,

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2298 *
2299 * Continuous simulation parameters:
2300 * IaRECper=[4](hrs),
2301 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2302 * InterEventTime=[12](hrs)
2303 * Baseflow simulation parameters:
2304 * BaseFlowOption=[1] ,
2305 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2306 * VHydCond=[0.055](mm/hr), END=-1
2307 *%-----|-----|
2308 *# - JFSA 2021-02-24 "S-1-BCDC-1" and "S-1-BCDC-2" are not existing anymore.
2309 * "S-1-BCDC-1" is part of "S-1-FO-D2" and "S-1-BCDC-2" is part of "S-1-D2" and "S-1-D3"
2310 *CONTINUOUS NASHYD NHYD=[ "S-1-BCDC-1"], DT=[1]min, AREA=[0.3](ha),
2311 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2312 * N=[3], TP=[1.10]hrs,
2313 * Continuous simulation parameters:
2314 * IaRECper=[4](hrs),
2315 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2316 * InterEventTime=[12](hrs)
2317 * Baseflow simulation parameters:
2318 * BaseFlowOption=[1] ,
2319 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2320 * VHydCond=[0.055](mm/hr), END=-1
2321 *%-----|-----|
2322 *CONTINUOUS NASHYD NHYD=[ "S-1-BCDC-2"], DT=[1]min, AREA=[1.3](ha),
2323 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2324 * N=[3], TP=[1.10]hrs,
2325 * Continuous simulation parameters:
2326 * IaRECper=[4](hrs),
2327 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2328 * InterEventTime=[12](hrs)
2329 * Baseflow simulation parameters:
2330 * BaseFlowOption=[1] ,
2331 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2332 * VHydCond=[0.055](mm/hr), END=-1
2333 *%-----|-----|
2334 *# - JFSA 2021-01-19, after adding Greenbank pond, "S-1-BCDC-3" is not existing
2335 anymore
2336 *CONTINUOUS NASHYD NHYD=[ "S-1-BCDC-3"], DT=[1]min, AREA=[3.9](ha),
2337 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2338 * N=[3], TP=[1.10]hrs,
2339 * Continuous simulation parameters:
2340 * IaRECper=[4](hrs),
2341 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2342 * InterEventTime=[12](hrs)
2343 * Baseflow simulation parameters:
2344 * BaseFlowOption=[1] ,
2345 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2346 * VHydCond=[0.055](mm/hr), END=-1
2347 *%-----|-----|
2348 * -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
2349 before station 7245 on Jock River
2350 *CONTINUOUS STANDHYD NHYD=[ "S-1-Okeefe"], DT=[1](min), AREA=[44.93](ha), XIMP=[0.65],
2351 TIMP=[0.65], DWF=[0](cms),
2352 * LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
2353 IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
2354 IAimp=[1.57](mm), SLPI=[0.75](%), LGI=[547.296](m), MNI=[0.013], SCI=[0](min),
2355 * Continuous simulation parameters:
2356 * IaRECper=[4](hrs), IaREimp=[4](hrs),
2357 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2358 * InterEventTime=[12](hrs), END=-1
2359 *%-----|-----|
2360 *COMPUTE DUALHYD NHYDin=[ "S-1-Okeefe"], CINLET=[4.796](cms), NINLET=[1],
2361 * MajNHYD=[ "S-1-OkMJ"]
2362 * MinNHYD=[ "S-1-OkMN"]

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2358 *
2359 *-----|-----|-----|-----|-----|-----|-----|-----|
2360 *ADD HYD NHYDsum=[ "S-1-OkS" ] , NHYDs to add=[ "S-1-OkMJ"+ "S-1-OkMN" ]
2361 *-----|-----|-----|-----|-----|-----|-----|-----|
2362 *ROUTE RESERVOIR NHYDout=[ "S-1-OkSR" ] , NHYDin=[ "S-1-OkS" ] ,
2363 * RDT=[1](min) ,
2364 * TABLE of ( OUTFLOW-STORAGE ) values
2365 * (cms) - (ha-m)
2366 * [ 0.0 , 0.0 ]
2367 * [ 0.5370, 1.7917 ]
2368 * [ -1 , -1 ] (max twenty pts)
2369 * NHYDovf=[ "S-1-OkSovf" ]
2370 *-----|-----|-----|-----|-----|-----|-----|-----|
2371 *CONTINUOUS NASHYD NHYD=[ "S-1-Okeefe" ] , DT=[1]min, AREA=[ 44.93 ](ha) ,
2372 * DWF=[0](cms) , CN/C=[77] , IA=[ 4.67 ](mm) ,
2373 * N=[ 3 ] , TP=[ 1.049 ]hrs,
2374 * Continuous simulation parameters:
2375 * IaRECper=[ 4 ](hrs),
2376 * SMIN=[ -1 ](mm) , SMAX=[ -1 ](mm) , SK=[ 0.010 ]/(mm) ,
2377 * InterEventTime=[ 12 ](hrs)
2378 * Baseflow simulation parameters:
2379 * BaseFlowOption=[ 1 ] ,
2380 * InitGWResVol=[ 50 ](mm) , GWResK=[ 0.96 ](mm/day/mm)
2381 * VHdCond=[ 0.055 ](mm/hr) , END=-1
2382 *-----|-----|-----|-----|-----|-----|-----|-----|
2383 * -JFSA 2021-02-26 "S-1-FO-D1" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2384 *CONTINUOUS STANDHYD NHYD=[ "S-1-FO-D1" ] , DT=[1]min, AREA=[ 5.11 ](ha) ,
2385 * XIMP=[ 0.65 ] , TIMP=[ 0.65 ] , DWF=[ 0 ](cms) , LOSS=[ 2 ] ,
2386 * SCS curve number CN=[ 74 ] ,
2387 * Pervious surfaces: IAper=[ 4.67 ](mm) , SLPP=[ 0.5 ](%) ,
2388 * LGP=[ 40 ](m) , MNP=[ 0.25 ] , SCP=[ 0 ](min) ,
2389 * Impervious surfaces: IAimp=[ 1.57 ](mm) , SLPI=[ 0.5 ](%) ,
2390 * LGI=[ 184.572 ](m) , MNI=[ 0.013 ] , SCI=[ 0 ](min) ,
2391 * Continuous simulation parameters:
2392 * IaRECper=[ 4 ](hrs) , IaRECimp=[ 4 ](hrs) ,
2393 * SMIN=[ -1 ](mm) , SMAX=[ -1 ](mm) , SK=[ 0.010 ]/(mm) ,
2394 * InterEventTime=[ 18 ](hrs) , END=-1
2395 *-----|-----|-----|-----|-----|-----|-----|-----|
2396 *COMPUTE DUALHYD NHYDin=[ "S-1-FO-D1" ] , CINLET=[ 0.605 ](cms) , NINLET=[ 1 ] ,
2397 * MajNHYD=[ "S-1-FO-D1J" ]
2398 * MinNHYD=[ "S-1-FO-D1N" ]
2399 * TMJSTO=[ 99999999 ](cu-m)
2400 *-----|-----|-----|-----|-----|-----|-----|-----|
2401 *ADD HYD NHYDsum=[ "S-1-FO-D1S" ] , NHYDs to add=[ "S-1-FO-D1N"+ "S-1-FO-D1J" ]
2402 *-----|-----|-----|-----|-----|-----|-----|-----|
2403 *ROUTE RESERVOIR NHYDout=[ "S-1-FO-D1R" ] , NHYDin=[ "S-1-FO-D1S" ] ,
2404 * RDT=[1](min) ,
2405 * TABLE of ( OUTFLOW-STORAGE ) values
2406 * (cms) - (ha-m)
2407 * [ 0.0 , 0.0 ]
2408 * [ 0.0611, 0.2038 ]
2409 * [ -1 , -1 ] (max twenty pts)
2410 * NHYDovf=[ "S-1FOD1ovf" ]
2411 *-----|-----|-----|-----|-----|-----|-----|-----|
2412 *CONTINUOUS NASHYD NHYD=[ "S-1-FO-D1" ] , DT=[1]min, AREA=[ 5.11 ](ha) ,
2413 * DWF=[0](cms) , CN/C=[77] , IA=[ 4.67 ](mm) ,
2414 * N=[ 3 ] , TP=[ 1.10 ]hrs,
2415 * Continuous simulation parameters:
2416 * IaRECper=[ 4 ](hrs),
2417 * SMIN=[ -1 ](mm) , SMAX=[ -1 ](mm) , SK=[ 0.010 ]/(mm) ,
2418 * InterEventTime=[ 12 ](hrs)
2419 * Baseflow simulation parameters:
2420 * BaseFlowOption=[ 1 ] ,
2421 * InitGWResVol=[ 50 ](mm) , GWResK=[ 0.96 ](mm/day/mm)
2422 * VHdCond=[ 0.055 ](mm/hr) , END=-1

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2423 *-----|-----|
2424 * -JFSA 2021-02-26 "S-1-FO-D2" is a part of S-1 sub-catchment. It is moved to drain
2425 before station 980 on Foster Drain
2426 *CONTINUOUS STANDHYD NHYD=["S-1-FO-D2"], DT=[1]min, AREA=[4.94](ha),
2427 * XIMP=[0.55], TIMP=[0.55], DWF=[0](cms), LOSS=[2],
2428 * SCS curve number CN=[74],
2429 * Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2430 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
2431 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2432 * LGI=[181.475](m), MNI=[0.013], SCI=[0](min),
2433 * Continuous simulation parameters:
2434 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
2435 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2436 * InterEventTime=[18](hrs), END=-1
2437 *-----|-----|
2438 *CONTINUOUS NASHYD NHYD=["S-1-FO-D2"], DT=[1]min, AREA=[4.94](ha),
2439 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2440 * N=[3], TP=[1.10]hrs,
2441 * Continuous simulation parameters:
2442 * IaRECper=[4](hrs),
2443 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2444 * InterEventTime=[12](hrs)
2445 * Baseflow simulation parameters:
2446 * BaseFlowOption=[1],
2447 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2448 * VHdCond=[0.055](mm/hr), END=-1
2449 *-----|-----|
2450 *COMPUTE DUALHYD NHYDin=["S-1-FO-D2"], CINLET=[0.508](cms), NINLET=[1],
2451 * MajNHYD=["S-1-FO-D2J"]
2452 * MinNHYD=["S-1-FO-D2N"]
2453 * TMJSTO=[9999999](cu-m)
2454 *-----|-----|
2455 *ADD HYD NHYDsum=["S-1-FO-D2S"], NHYDs to add=["S-1-FO-D2J"+"S-1-FO-D2N"]
2456 *-----|-----|
2457 *ROUTE RESERVOIR NHYDout=["S-1-FO-D2R"], NHYDin=["S-1-FO-D2S"],
2458 * RDT=[1](min),
2459 * TABLE of ( OUTFLOW-STORAGE ) values
2460 * (cms) - (ha-m)
2461 * [ 0.0 , 0.0 ]
2462 * [ 0.0590, 0.1970 ]
2463 * [ -1 , -1 ] (max twenty pts)
2464 *-----|-----|
2465 * -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
2466 before station 6016 on Jock River
2467 *CONTINUOUS STANDHYD NHYD=["S-1-FO-F-D"], DT=[1]min, AREA=[14.96](ha),
2468 * XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2469 * SCS curve number CN=[74],
2470 * Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2471 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
2472 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2473 * LGI=[315.806](m), MNI=[0.013], SCI=[0](min),
2474 * Continuous simulation parameters:
2475 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
2476 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2477 * InterEventTime=[18](hrs), END=-1
2478 *-----|-----|
2479 *CONTINUOUS NASHYD NHYD=["S-1-FO-F-D"], DT=[1]min, AREA=[14.96](ha),
2480 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2481 * N=[3], TP=[1.007]hrs,
2482 * Continuous simulation parameters:
2483 * IaRECper=[4](hrs),
2484 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2485 * InterEventTime=[12](hrs)
2486 * Baseflow simulation parameters:
2487 * BaseFlowOption=[1],

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2487 *
2488 *
2489 *-----| InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2490 *-----| VHydCond=[0.055](mm/hr), END=-1
2491 *-----| NHYDin= [ "S-1-FO-F-D" ], CINLET=[ 1.749 ](cms), NINLET=[ 1 ],
2492 *-----| MajNHYD= [ "S-1FO-F-DJ" ]
2493 *-----| MinNHYD= [ "S-1FO-F-DN" ]
2494 *-----| TMJSTO=[ 9999999 ](cu-m)
2495 *-----| NHYDsum= [ "S-1FO-F-DS" ], NHYDs to add= [ "S-1FO-F-DJ" + "S-1FO-F-DN" ]
2496 *-----| NHYDout= [ "S-1FO-F-DR" ], NHYDin= [ "S-1FO-F-DS" ],
2497 *-----| RDT=[ 1 ](min),
2498 *-----| TABLE of ( OUTFLOW-STORAGE ) values
2499 *-----| (cms) - (ha-m)
2500 *-----| [ 0.0 , 0.0 ]
2501 *-----| [ 0.1788, 0.5966 ]
2502 *-----| [ -1 , -1 ] (max twenty pts)
2503 *-----| NHYDovf= [ "S-1FoFDovf" ]
2504 *-----|
2505 *-----| CONTINUOUS STANDHYD NHYD= [ "S-1-D1" ], DT=[ 1 ](min), AREA=[ 21.67 ](ha), XIMP=[ 0.65 ],
2506 *-----| TIMP=[ 0.65 ], DWF=[ 0 ](cms),
2507 *-----| LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
2508 *-----| IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%),
2509 *-----| LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min), Impervious surfaces:
2510 *-----| IAimp=[ 1.57 ](mm), SLPI=[ 0.75 ](%),
2511 *-----| LGI=[ 380.088 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
2512 *-----| Continuous simulation parameters:
2513 *-----| IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
2514 *-----| SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2515 *-----| InterEventTime=[ 12 ](hrs), END=-1
2516 *-----| NHYD= [ "S-1-D1" ], DT=[ 1 ]min, AREA=[ 21.67 ](ha),
2517 *-----| DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
2518 *-----| N=[ 3 ], TP=[ 1.066 ]hrs,
2519 *-----| Continuous simulation parameters:
2520 *-----| IaRECper=[ 4 ](hrs),
2521 *-----| SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2522 *-----| InterEventTime=[ 12 ](hrs)
2523 *-----| Baseflow simulation parameters:
2524 *-----| BaseFlowOption=[ 1 ],
2525 *-----| InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2526 *-----| VHydCond=[ 0.055 ](mm/hr), END=-1
2527 *-----| COMPUTE DUALHYD NHYDin= [ "S-1-D1" ], CINLET=[ 2.409 ](cms), NINLET=[ 1 ],
2528 *-----| MajNHYD= [ "S-1-D1J" ]
2529 *-----| MinNHYD= [ "S-1-D1N" ]
2530 *-----| TMJSTO=[ 9999999 ](cu-m)
2531 *-----|
2532 *-----| ADD HYD NHYDsum= [ "S-1-D1S" ], NHYDs to add= [ "S-1-D1J" + "S-1-D1N" ]
2533 *-----|
2534 *-----| NHYDout= [ "S-1-D1R" ], NHYDin= [ "S-1-D1S" ],
2535 *-----| RDT=[ 1 ](min),
2536 *-----| TABLE of ( OUTFLOW-STORAGE ) values
2537 *-----| (cms) - (ha-m)
2538 *-----| [ 0.0 , 0.0 ]
2539 *-----| [ 0.2590, 0.8642 ]
2540 *-----| [ -1 , -1 ] (max twenty pts)
2541 *-----| NHYDovf= [ "S-1-D1Rovf" ]
2542 *-----|
2543 *-----| -JFSA 2021-02-25 "S-1-D2" and "S-1-D3" are part of S-1 sub-catchment. They are
2544 moved to drain before station 6215 on Jock River
2545 *CONTINUOUS STANDHYD NHYD= [ "S-1-D2" ], DT=[ 1 ](min), AREA=[ 18.67 ](ha), XIMP=[ 0.65 ],
2546 *-----| TIMP=[ 0.65 ], DWF=[ 0 ](cms),
2547 *-----| LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
2548 *-----| IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%),
2549 *-----| LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min), Impervious surfaces:

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2547 IAimp=[1.57](mm), SLPI=[0.75](%),
2548 * LGI=[352.798](m), MNI=[0.013], SCI=[0](min),
2549 * Continuous simulation parameters:
2550 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
2551 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2552 * InterEventTime=[12](hrs), END=-1
2553 *%-----|-----|
2553 *CONTINUOUS NASHYD NHYD=[ "S-1-D2" ], DT=[1]min, AREA=[18.67](ha),
2554 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2555 * N=[3], TP=[1.120]hrs,
2556 * Continuous simulation parameters:
2557 * IaRECper=[4](hrs),
2558 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2559 * InterEventTime=[12](hrs)
2560 * Baseflow simulation parameters:
2561 * BaseFlowOption=[1],
2562 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2563 * VHydCond=[0.055](mm/hr), END=-1
2564 *%-----|-----|
2565 *COMPUTE DUALHYD NHYDin=[ "S-1-D2" ], CINLET=[2.062](cms), NINLET=[1],
2566 * MajNHYD=[ "S-1-D2J" ]
2567 * MinNHYD=[ "S-1-D2N" ]
2568 * TMJSTO=[9999999](cu-m)
2569 *%-----|-----|
2570 *ADD HYD NHYDsum=[ "S-1-D2S" ], NYHDs to add=[ "S-1-D2J" +"S-1-D2N" ]
2571 *%-----|-----|
2572 *ROUTE RESERVOIR NYHDout=[ "S-1-D2R" ] ,NYDin=[ "S-1-D2S" ],
2573 * RDT=[1](min),
2574 * TABLE of ( OUTFLOW-STORAGE ) values
2575 * (cms) - (ha-m)
2576 * [ 0.0 , 0.0 ]
2577 * [ 0.2231, 0.7445 ]
2578 * [ -1 , -1 ] (max twenty pts)
2579 * NYDovf=[ "S-1-D2Rovf" ]
2580 *%-----|-----|
2581 *CONTINUOUS STANDHYD NYHD=[ "S-1-D3" ], DT=[1](min), AREA=[6.79](ha), XIMP=[0.65],
2582 * TIMP=[0.65], DWF=[0](cms),
2583 * LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
2584 * IAper=[4.67](mm), SLPP=[2.0](%),
2585 * LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
2586 * IAimp=[1.57](mm), SLPI=[0.75](%),
2587 * LGI=[212.760](m), MNI=[0.013], SCI=[0](min),
2588 * Continuous simulation parameters:
2589 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
2590 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2591 * InterEventTime=[12](hrs), END=-1
2592 *%-----|-----|
2592 *CONTINUOUS NASHYD NHYD=[ "S-1-D3" ], DT=[1]min, AREA=[6.79](ha),
2593 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2594 * N=[3], TP=[1.281]hrs,
2595 * Continuous simulation parameters:
2596 * IaRECper=[4](hrs),
2597 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2598 * InterEventTime=[12](hrs)
2599 * Baseflow simulation parameters:
2600 * BaseFlowOption=[1],
2601 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2602 * VHydCond=[0.055](mm/hr), END=-1
2603 *%-----|-----|
2603 *COMPUTE DUALHYD NHYDin=[ "S-1-D3" ], CINLET=[0.719](cms), NINLET=[1],
2604 * MajNHYD=[ "S-1-D3J" ]
2605 * MinNHYD=[ "S-1-D3N" ]
2606 * TMJSTO=[9999999](cu-m)
2607 *%-----|-----|
2607 *ADD HYD NHYDsum=[ "S-1-D3S" ], NYHDs to add=[ "S-1-D3J" +"S-1-D3N" ]
2608 *%-----|-----|

```

```

2609 *ROUTE RESERVOIR      NHYDout=[ "S-1-D3R" ] ,NHYDin=[ "S-1-D3S" ] ,
2610 *
2611 *
2612 *          TABLE of ( OUTFLOW-STORAGE ) values
2613 *                                (cms) - (ha-m)
2614 *                                [ 0.0      , 0.0   ]
2615 *                                [ 0.0811 , 0.2708 ]
2616 *                                [      -1 ,      -1    ] (max twenty pts)
2617 *%
2618 CONTINUOUS STANDHYD  NHYD=[ "S-1-D4" ] , DT=[1](min), AREA=[3.28](ha), XIMP=[0.65],
2619 TIMP=[0.65], DWF=[0](cms),
2620 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
2621 IAper=[4.67](mm), SLPP=[2.0](%),
2622 LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
2623 IAimp=[1.57](mm), SLPI=[0.75](%),
2624 LGI=[147.874](m), MNI=[0.013], SCI=[0](min),
2625 Continuous simulation parameters:
2626 IaRECper=[4](hrs), IaRECImp=[4](hrs),
2627 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2628 InterEventTime=[12](hrs), END=-1
2629 *%
2630 *CONTINUOUS NASHYD   NHYD=[ "S-1-D4" ], DT=[1]min, AREA=[3.28](ha),
2631 *                      DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2632 *                      N=[3], TP=[1.10]hrs,
2633 *                      Continuous simulation parameters:
2634 *                      IaRECper=[4](hrs),
2635 *                      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2636 *                      InterEventTime=[12](hrs)
2637 *                      Baseflow simulation parameters:
2638 *                      BaseFlowOption=[1] ,
2639 *                      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2640 *                      VHdCond=[0.055](mm/hr), END=-1
2641 *%
2642 COMPUTE DUALHYD     NHYDin=[ "S-1-D4" ], CINLET=[0.421](cms), NINLET=[1],
2643 MajNHYD=[ "S-1-D4J" ]
2644 MinNHYD=[ "S-1-D4N" ]
2645 TMJSTO=[99999999](cu-m)
2646 *%
2647 ADD HYD              NHYDssum=[ "S-1-D4S" ], NHYDs to add=[ "S-1-D4J"+ "S-1-D4N" ]
2648 *%
2649 ROUTE RESERVOIR    NHYDout=[ "S-1-D4R" ] ,NHYDin=[ "S-1-D4S" ] ,
2650 RDT=[1](min),
2651 *          TABLE of ( OUTFLOW-STORAGE ) values
2652 *                                (cms) - (ha-m)
2653 *                                [ 0.0      , 0.0   ]
2654 *                                [ 0.0392 , 0.1308 ]
2655 *                                [      -1 ,      -1    ] (max twenty pts)
2656 *%
2657 CONTINUOUS STANDHYD NHYD=[ "S-1-D5" ] , DT=[1](min), AREA=[12.84](ha), XIMP=[0.65],
2658 TIMP=[0.65], DWF=[0](cms),
2659 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
2660 IAper=[4.67](mm), SLPP=[2.0](%),
2661 LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
2662 IAimp=[1.57](mm), SLPI=[0.75](%),
2663 LGI=[292.57](m), MNI=[0.013], SCI=[0](min),
2664 Continuous simulation parameters:
2665 IaRECper=[4](hrs), IaRECImp=[4](hrs),
2666 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2667 InterEventTime=[12](hrs), END=-1
2668 *%
2669 *CONTINUOUS NASHYD   NHYD=[ "S-1-D5" ], DT=[1]min, AREA=[12.84](ha),
2670 *                      DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2671 *                      N=[3], TP=[1.10]hrs,
2672 *                      Continuous simulation parameters:
2673 *                      IaRECper=[4](hrs),

```

```

2669 *
2670 *
2671 *
2672 *
2673 *
2674 *
2675 *%
2676 COMPUTE DUALHYD | NHYDin=[ "S-1-D5" ], CINLET=[1.5](cms), NINLET=[1],
2677 | MajNHYD=[ "S-1-D5J" ]
2678 | MinNHYD=[ "S-1-D5N" ]
2679 | TMJSTO=[ 9999999 ](cu-m)
2680 *%
2681 ADD HYD | NHYDsum=[ "S-1-D5S" ], NHYDs to add=[ "S-1-D5J" + "S-1-D5N" ]
2682 *%
2683 ROUTE RESERVOIR | NHYDout=[ "S-1-D5R" ], NHYDin=[ "S-1-D5S" ],
2684 | RDT=[1](min),
2685 | TABLE of ( OUTFLOW-STORAGE ) values
2686 | (cms) - (ha-m)
2687 | [ 0.0 , 0.0 ]
2688 | [ 0.1535 , 0.5120 ]
2689 | [ -1 , -1 ] (max twenty pts)
2690 | NHYDovf=[ "S-1-D5Rovf" ]
2691 *%
2692 CONTINUOUS STANDHYD | NHYD=[ "S-1-D6" ], DT=[1](min), AREA=[1.75](ha), XIMP=[0.65],
2693 | TIMP=[0.65], DWF=[0](cms),
2694 | LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
2695 | IAper=[4.67](mm), SLPP=[2.0](%),
2696 | LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
2697 | IAimp=[1.57](mm), SLPI=[0.75](%),
2698 | LGI=[108.01](m), MNI=[0.013], SCI=[0](min),
2699 | Continuous simulation parameters:
2700 | IaRECper=[4](hrs), IaRECImp=[4](hrs),
2701 | SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2702 | InterEventTime=[12](hrs), END=-1
2703 *%
2704 *CONTINUOUS NASHYD | NHYD=[ "S-1-D6" ], DT=[1]min, AREA=[1.75](ha),
2705 | DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2706 | N=[3], TP=[1.10]hrs,
2707 | Continuous simulation parameters:
2708 | IaRECper=[4](hrs),
2709 | SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2710 | InterEventTime=[12](hrs)
2711 | Baseflow simulation parameters:
2712 | BaseFlowOption=[1],
2713 | InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2714 | VHydCond=[0.055](mm/hr), END=-1
2715 *%
2716 COMPUTE DUALHYD | NHYDin=[ "S-1-D6" ], CINLET=[0.232](cms), NINLET=[1],
2717 | MajNHYD=[ "S-1-D6J" ]
2718 | MinNHYD=[ "S-1-D6N" ]
2719 | TMJSTO=[ 9999999 ](cu-m)
2720 *%
2721 ADD HYD | NHYDsum=[ "S-1-D6S" ], NHYDs to add=[ "S-1-D6J" + "S-1-D6N" ]
2722 *%
2723 ROUTE RESERVOIR | NHYDout=[ "S-1-D6R" ], NHYDin=[ "S-1-D6S" ],
2724 | RDT=[1](min),
2725 | TABLE of ( OUTFLOW-STORAGE ) values
2726 | (cms) - (ha-m)
2727 | [ 0.0 , 0.0 ]
2728 | [ 0.0209 , 0.0698 ]
2729 | [ -1 , -1 ] (max twenty pts)
2730 | NHYDovf=[ "S-1-D6Rovf" ]
2731 *%
2732 CONTINUOUS STANDHYD | NHYD=[ "S-1-D7" ], DT=[1](min), AREA=[2.03](ha), XIMP=[0.65],
2733 | TIMP=[0.65], DWF=[0](cms),
2734 | LOSS=[2], SCS curve number CN=[75], Pervious surfaces:

```



```

2791 *
2792 *-----|-----|-----|-----|-----|-----|-----|-----|-----|
2793 *ADD HYD          NHYDsum=[ "S-1-D8S" ],  NHYDs to add=[ "S-1-D8J"+"S-1-D8N" ]
2794 *-----|-----|-----|-----|-----|-----|-----|-----|-----|
2795 *ADD HYD          NHYDsum=[ "S-1-D" ],   NHYDs to add=[ "S-1-Okeefe"+"S-1"+"S-1-Fost" ]
2796 *-----|-----|-----|-----|-----|-----|-----|-----|-----|
2797 *COMPUTE DUALHYD NHYDin=[ "S-1-D" ],  CINLET=[11.616](cms), NINLET=[1],
2798 *           MajNHYD=[ "S-1-D-MJ" ]
2799 *           MinNHYD=[ "S-1-D-MN" ]
2800 *           TMJSTO=[5974](cu-m)
2801 *-----|-----|-----|-----|-----|-----|-----|-----|-----|
2802 *ADD HYD          NHYDsum=[ "S-1-DEV" ], NHYDs to add=[ "S-1-D-MJ"+"S-1-D-MN" ]
2803 *-----|-----|-----|-----|-----|-----|-----|-----|-----|
2804 *ROUTE RESERVOIR NHYDout=[ "S-1-D8R" ] , NHYDin=[ "S-1-D8S" ] ,
2805 *           RDT=[1](min),
2806 *           TABLE of ( OUTFLOW-STORAGE ) values
2807 *           (cms) - (ha-m)
2808 *           [ 0.0      , 0.0   ]
2809 *           [ 0.0630 , 0.2102 ]
2810 *           [      -1 ,      -1   ] (max twenty pts)
2811 *           NHYDovf=[ "S-1-D8Rovf" ]
2812 *-----|-----|-----|-----|-----|-----|-----|-----|-----|
2813 *-----|-----|-----|-----|-----|-----|-----|-----|-----|
2814 *      -JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
2815 *      (W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
2816 *#      Catchment W_CLAR
2817 *#      - To West Clarke Drain (south of the Jock)
2818 *#      - Subdivision with 43% imp. as per Barrhaven South MSS
2819 *#      - 2020-11-30 update CLARKE Tributary Drainage Area to = 121 ha based on
2820 *#      P598(04)-11
2821 *#      - 2020-11-30 split CLARKE Drainage Area to MAJOR and ALL
2822 *#*****
2823 CONTINUOUS STANDHYD NHYD=[ "W_CLAR_MJ" ], DT=[1]min, AREA=[1.772](ha),
2824 XIMP=[0.46], TIMP=[0.59], DWF=[0](cms), LOSS=[2],
2825 SCS curve number CN=[77],
2826 Previous surfaces: IAper=[4.67](mm), SLPP=[1](%),
2827 LGP=[40](m), MNP=[0.25], SCP=[0](min),
2828 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
2829 LGI=[109](m), MNI=[0.013], SCI=[0](min),
2830 Continuous simulation parameters:
2831 IaRECper=[4](hrs), IaRECImp=[4](hrs),
2832 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2833 InterEventTime=[18](hrs), END=-1
2834 *-----|-----|-----|-----|-----|-----|-----|-----|-----|
2835 *COMPUTE DUALHYD NHYDin=[ "W_CLAR_MJ" ], CINLET=[0.213](cms), NINLET=[1],
2836 *           MajNHYD=[ "W_CLAR_MJj" ]
2837 *           MinNHYD=[ "W_CLAR_MJn" ]
2838 *           TMJSTO=[0.1](cu-m)
2839 *-----|-----|-----|-----|-----|-----|-----|-----|-----|
2840 *# 5-Year + 12% Capture
2841 ROUTE RESERVOIR NHYDout=[ "W_CLAR_MJn" ] , NHYDin=[ "W_CLAR_MJ" ] ,
2842 RDT=[1](min),
2843 *           TABLE of ( OUTFLOW-STORAGE ) values
2844 *           (cms) - (ha-m)
2845 *           [ 0.0      , 0.0   ]
2846 *           [ 0.213   , 0.0001 ]
2847 *           [      -1 ,      -1   ] (max twenty pts)
2848 *           NHYDovf=[ "W_CLAR_MJj" ] ,
2849 *      -Clarke_All area from P 598(04)-11 = 120.207 ha, change to 127.298 ha based on
2850 *      GIS measurements,
2851 *      -JFSA, 2021-01-19 update W_CLAR_ALL to (121.17-1.772=119.398) ha based on GIS
2852 *      measurements W_CLAR is 121.17 ha and W_CLAR_MJ is 1.772 ha
2853 CONTINUOUS STANDHYD NHYD=[ "W_CLAR_ALL" ], DT=[1]min, AREA=[119.398](ha),
2854 XIMP=[0.60], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2855 SCS curve number CN=[77],

```



```

2916 *# 2021-02-25 add station 5737 before station 5002. Station 5737 was extracted from the
2917 HEC-RAS model
2918 T:\PROJ\1474-16\Design\20201026-QuantityControlAnalysis\HEC-RAS\JockLidar2005
2919 *# JFSA 2021-03-02 change the slope to 0.0175% instead of 0.02593 to stabilize the model
2920 ROUTE CHANNEL      NHYDout=[ "5737" ] , NHYDin=[ "SN_CE" ] ,
2921                         RDT=[1](min),
2922                         CHLNGTH=[ 270 ](m),   CHSLOPE=[ 0.0175 ](%),
2923                         FPSLOPE=[ 0.0175 ](%),
2924                         SECNUM=[ 1.0 ],           NSEG=[ 3 ]
2925                         ( SEGROUGH, SEGDIST (m))=
2926                         [ 0.050, -24.04
2927                         -0.035, 23.92
2928                         0.050, 1130.8 ] NSEG times
2929                         ( DISTANCE (m), ELEVATION (m))=
2930                         [ -1060.52, 94 ]
2931                         [ -268.6, 91.5 ]
2932                         [ -259.43, 91.5 ]
2933                         [ -179.48, 91.5 ]
2934                         [ -67.9, 91.5 ]
2935                         [ -59.21, 91.5 ]
2936                         [ -33.19, 91 ]
2937                         [ -26.08, 90.5 ]
2938                         [ -24.04, 90 ]
2939                         [ -13.14, 86.77 ]
2940                         [ 0, 85 ]
2941                         [ 14.68, 86.74 ]
2942                         [ 23.92, 90 ]
2943                         [ 25.78, 90.5 ]
2944                         [ 31.91, 91 ]
2945                         [ 91.95, 91.5 ]
2946                         [ 772.15, 92 ]
2947                         [ 961.49, 92.5 ]
2948                         [ 1044.69, 93 ]
2949                         [ 1130.8, 95 ]
2950 *%-----|-----|
2951 ADD HYD          NHYDsum= [ "5002" ], NHYDs to
2952 add=[ "5737"+ "S-1-D1R"+ "S-1-D6R"+ "S-1-D7R"+ "S-1-D1Rovf"+ "S-1-D6Rovf"+ "S-1-D7Rovf" ]
2953 *%-----|-----|
2954 SAVE HYD         NHYD= [ "5002" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
2955                         HYD_COMMENT=[ "Total Flows before Station 5002 on Jock River" ]
2956 *%-----|-----|
2957 *# Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain
2958 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5002
2959 *# JFSA 2021-02-19 Change the slope from 0.01 % (as per Stantec Report 2007) to 0.0255 %
2960 % so the model will be more stable and give reasonable results. It is justifiable as
2961 ROUTE CHANNELs aren't well suited to really flat slopes.
2962 *# JFSA 2021-02-19 Change to three ROUTE CHANNEL with length 275 m each instead of one
2963 with 825 m length so the model will be more stable
2964 *# JFSA 2021-02-26 change the length of 5002 route channel from 825 m to 736 m. That is
2965 because of adding station 5737 between station 6016 and station 5002. Then the length
2966 from station 5737 to station 5002 is 736 m. Change the slope from 0.0255 % to 0.09511 %
2967 *
2968 ROUTE CHANNEL      NHYDout=[ "N_WCa" ] , NHYDin=[ "5002" ] ,
2969                         RDT=[1](min),
2970                         CHLNGTH=[ 245.33333 ](m),   CHSLOPE=[ 0.09511 ](%),
2971                         FPSLOPE=[ 0.09511 ](%),
2972                         SECNUM=[ 1.0 ],           NSEG=[ 3 ]
2973                         ( SEGROUGH, SEGDIST (m))=
2974                         [ 0.050, -37.5
2975                         -0.035, 37.50
2976                         0.050, 157.05 ] NSEG times
2977                         ( DISTANCE (m), ELEVATION (m))=
2978                         [ -601.81, 91.5 ]
2979                         [ -37.50, 90.00 ]
2980                         [ -19.61, 87.04 ]
2981                         [ 0.00, 85.70 ]

```

```

2974 [14.87, 86.93]
2975 [37.50, 90.00]
2976 [38.54, 90.50]
2977 [42.23, 91]
2978 [157.05,91.50]
2979 *
2980 *
2981 *
2982 *
2983 *%-----|-----|-----|-----|
2984 ROUTE CHANNEL
2985 NHYDout=[ "N_WCb" ] ,NHYDin=[ "N_WCa" ] ,
2986 RDT=[1](min),
2987 CHLGTH=[245.33333](m), CHSLOPE=[0.09511](%),
2988 FPSLOPE=[0.09511](%),
2989 SECNUM=[1.0], NSEG=[3]
2990 ( SEGROUGH, SEGDIST (m))=
2991 [0.050,-37.5
2992 -0.035,37.50
2993 0.050,157.05] NSEG times
2994 ( DISTANCE (m), ELEVATION (m))=
2995 [-601.81, 91.5]
2996 [-37.50, 90.00]
2997 [-19.61, 87.04]
2998 [0.00, 85.70]
2999 [14.87, 86.93]
3000 [37.50, 90.00]
3001 [38.54, 90.50]
3002 [42.23, 91]
3003 [157.05,91.50]
3004 *%-----|-----|-----|-----|
3005 ROUTE CHANNEL
3006 NHYDout=[ "N_WC" ] ,NHYDin=[ "N_WCb" ] ,
3007 RDT=[1](min),
3008 CHLGTH=[245.33333](m), CHSLOPE=[0.09511](%),
3009 FPSLOPE=[0.09511](%),
3010 SECNUM=[1.0], NSEG=[3]
3011 ( SEGROUGH, SEGDIST (m))=
3012 [0.050,-37.5
3013 -0.035,37.50
3014 0.050,157.05] NSEG times
3015 ( DISTANCE (m), ELEVATION (m))=
3016 [-601.81, 91.5]
3017 [-37.50, 90.00]
3018 [-19.61, 87.04]
3019 [0.00, 85.70]
3020 [14.87, 86.93]
3021 [37.50, 90.00]
3022 [38.54, 90.50]
3023 [42.23, 91]
3024 [157.05,91.50]
3025 *#####
3026 * -JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
3027 (W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
3028 *ADD HYD NHYDsum=[ "SN_WC" ], NHYDs to
3029 add=[ "MS_P2"+"P2-OVF"+"N_WC"+"W_CLAR_UNDE" ]
3030 *%-----|-----|-----|-----|
3031 *SAVE HYD NHYD=[ "SN_WC" ], # OF PCYCLES=[-1], ICASEsh=[1]
3032 *
3033 * HYD_COMMENT=[ "Total Flows at West Clarke Pond Outlet" ]
3034 *# Hydrograph from Node West Clarke routed to Node at Kennedy - Burnett Drain
3035 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4534
3036 *#
3037 ROUTE CHANNEL
3038 NHYDout=[ "N_KB" ] ,NHYDin=[ "N_WC" ] ,
3039 RDT=[1](min),
3040 CHLGTH=[1020](m), CHSLOPE=[0.0498](%),
3041 FPSLOPE=[0.0498](%),
3042 SECNUM=[1.0], NSEG=[3]

```

```

3038      ( SEGROUGH, SEGDIST (m))=
3039          [0.050,-23.63
3040          -0.035,23.63
3041          0.050,728.3] NSEG times
3042      ( DISTANCE (m), ELEVATION (m))=
3043          [-1082.01,94]
3044          [-1028.17,92.5]
3045          [-992.3,93.5]
3046          [-279.34,90]
3047          [-23.63,90]
3048          [-13.45,87.13]
3049          [-0.07,86.24]
3050          [10.54,87.15]
3051          [23.63,90]
3052          [24.86,90.5]
3053          [26.72,91]
3054          [45.07,91.5]
3055          [128.17,91.5]
3056          [270.7,92.5]
3057          [728.3,95]
3058 *%----- | -----
3059 *#*****
3060 *#      Catchment KEN_BU
3061 *#      - To Kennedy-Burnett SWM Facility
3062 *#      - Outlets to Fraser-Clarke drain (north of the Jock)
3063 *#      - Medium density residential subdivision
3064 *#      - Add Kennedy Burnett model (Convert PCSWMM from NOVATECH June, 2020 to SWMHYMO)
3065 *#*****
3066 *CONTINUOUS STANDHYD NHYD=[ "KEN_BU" ], DT=[1]min, AREA=[281](ha),
3067 *          XIMP=[0.55], TIMP=[0.55], DWF=[0](cms), LOSS=[2],
3068 *          SCS curve number CN=[71],
3069 *          Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3070 *          LGP=[40](m), MNP=[0.25], SCP=[0](min),
3071 *          Impervious surfaces: IAimp=[1.57](mm), SLPi=[1](%),
3072 *          LGI=[1369](m), MNI=[0.013], SCI=[0](min),
3073 *          Continuous simulation parameters:
3074 *          IaRECper=[4](hrs), IaRECimp=[4](hrs),
3075 *          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3076 *          InterEventTime=[18](hrs), END=-1
3077 *%----- | -----
3078 *#*****
3079 *#      Existing Kennedy-Burnett SWM Facility
3080 *#      - Rating curve obtained from URTKBP
3081 *#      - Tributary Drainage Area to Pond = 160 ha
3082 *#*****
3083 *ROUTE RESERVOIR      NHYDout=[ "KEN_P" ], NHYDin=[ "KEN_BU" ],
3084 *          RDT=[1](min),
3085 *          TABLE of ( OUTFLOW-STORAGE ) values
3086 *          (cms) - (ha-m)
3087 *          [ 0.0 , 0.0 ]
3088 *          [ 0.13 , 0.26 ]
3089 *          [ 0.43 , 0.56 ]
3090 *          [ 0.67 , 0.90 ]
3091 *          [ 0.86 , 1.32 ]
3092 *          [ 1.01 , 1.79 ]
3093 *          [ 1.15 , 2.33 ]
3094 *          [ -1 , -1 ] (max twenty pts)
3095 *          NHYDovf=[ "KEN-OV" ]
3096 *%----- | -----
3097 *      -JFSA, 2021-01-19 update all KEN_BU areas based on GIS measurements
3098 CONTINUOUS STANDHYD NHYD=[ "KB-01A" ], DT=[1]min, AREA=[40.82](ha), XIMP=[0.097],
3099 *          TIMP=[0.4], DWF=[0](cms), LOSS=[1]:
3100 *          Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14]/(hr),
            F=[0.00](mm),
            Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[40](m),
            MNP=[0.250], SCP=[0](min),

```



```

3150 TMJSTO=[15500](cu-m)
3151 *%
3152 ADD HYD NHYDsum= [ "KB-03-S" ], NHYDs to add= [ "KB-03-MJ" +"KB-03-MN" ]
3153 *%
3154 CONTINUOUS STANDHYD NHYD= [ "KB-04" ], DT=[1]min, AREA=[ 6.95 ](ha), XIMP=[ 0.85 ],
3155 TIMP=[ 0.85 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3156 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3157 F=[ 0.00 ](mm),
3158 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3159 MNP=[ 0.250 ], SCP=[ 0 ](min),
3160 Impervious areas: IAimp=[ 0.942 ](mm), SLPI=[ 0.5 ](%),
3161 LGI=[ 215.252 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3162 Continuous simulation parameters:
3163 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3164 END=-1
3165 *%
3166 COMPUTE DUALHYD NHYDin= [ "KB-04" ], CINLET=[ 0.503 ](cms), NINLET=[ 1 ],
3167 MajNHYD= [ "KB-04-MJ" ]
3168 MinNHYD= [ "KB-04-MN" ]
3169 TMJSTO=[ 1972 ](cu-m)
3170 *%
3171 ADD HYD NHYDsum= [ "KB-04-S" ], NHYDs to add= [ "KB-04-MJ" +"KB-04-MN" ]
3172 *%
3173 CONTINUOUS STANDHYD NHYD= [ "KB-05" ], DT=[1]min, AREA=[ 5.19 ](ha), XIMP=[ 0.93 ],
3174 TIMP=[ 0.93 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3175 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3176 F=[ 0.00 ](mm),
3177 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3178 MNP=[ 0.250 ], SCP=[ 0 ](min),
3179 Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 0.5 ](%),
3180 LGI=[ 186.011 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3181 Continuous simulation parameters:
3182 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3183 END=-1
3184 *%
3185 COMPUTE DUALHYD NHYDin= [ "KB-06" ], CINLET=[ 2.262 ](cms), NINLET=[ 1 ],
3186 MajNHYD= [ "KB-06-MJ" ]
3187 MinNHYD= [ "KB-06-MN" ]
3188 TMJSTO=[ 1950 ](cu-m)
3189 *%
3190 ADD HYD NHYDsum= [ "KB-06-S" ], NHYDs to add= [ "KB-06-MJ" +"KB-06-MN" ]
3191 *%
3192 CONTINUOUS STANDHYD NHYD= [ "KB-11" ], DT=[1]min, AREA=[ 4.03 ](ha), XIMP=[ 0.675 ],
3193 TIMP=[ 0.675 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3194 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3195 F=[ 0.00 ](mm),
3196 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3197 MNP=[ 0.250 ], SCP=[ 0 ](min),
3198 Impervious areas: IAimp=[ 0.785 ](mm), SLPI=[ 2.0 ](%),
3199 LGI=[ 163.911 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3200 Continuous simulation parameters:
3201 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3202 END=-1

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3196 *%
3197 COMPUTE DUALHYD NHYDin=[ "KB-11" ], CINLET=[ 0.5773 ](cms), NINLET=[ 1 ],
3198 MajNHYD=[ "KB-11-MJ" ]
3199 MinNHYD=[ "KB-11-MN" ]
3200 TMJSTO=[ 597 ](cu-m)
3201 *%
3202 ADD HYD NHYDsum=[ "KB-11-S" ], NHYDs to add=[ "KB-11-MJ" +"KB-11-MN" ]
3203 *%
3204 CONTINUOUS STANDHYD NHYD=[ "S1" ], DT=[ 1 ]min, AREA=[ 4.99 ](ha), XIMP=[ 0.93 ],
3205 DWF=[ 0 ](cms), LOSS=[ 1 ]:
3206 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3207 F=[ 0.00 ](mm),
3208 Previous areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3209 MNP=[ 0.250 ], SCP=[ 0 ](min),
3210 Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 2.0 ](%),
3211 LGI=[ 182.392 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3212 Continuous simulation parameters:
3213 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3214 END=-1
3215 *%
3216 CONTINUOUS STANDHYD NHYD=[ "KB-15" ], DT=[ 1 ]min, AREA=[ 2.15 ](ha), XIMP=[ 0.79 ],
3217 TIMP=[ 0.79 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3218 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3219 F=[ 0.00 ](mm),
3220 Previous areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3221 MNP=[ 0.250 ], SCP=[ 0 ](min),
3222 Impervious areas: IAimp=[ 0.157 ](mm), SLPI=[ 0.3 ](%),
3223 LGI=[ 119.722 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3224 Continuous simulation parameters:
3225 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3226 END=-1
3227 *%
3228 *%
3229 ADD HYD NHYDsum=[ "KB-P1" ], NHYDs to
3230 add=[ "KB-01A-S" +"KB-01B-S" +"KB-01C-S" +"KB-03-S" +"KB-04-S" +"KB-05" +"KB-06-S" +"KB-11-S" +"KB
3231 -15" +"S1" ]
3232 *%
3233 ROUTE RESERVOIR NHYDout=[ "KB-P1R" ], NHYDin=[ "KB-P1" ],
3234 RDT=[ 1 ](min),
3235 TABLE of ( OUTFLOW-STORAGE ) values
3236 (cms) - (ha-m)
3237 [ 0.0 , 0.0 ]
3238 [ 0.076, 0.003 ]
3239 [ 0.088, 0.006 ]
3240 [ 0.136, 0.011 ]
3241 [ 0.301, 0.017 ]
3242 [ 0.454, 0.027 ]
3243 [ 0.631, 0.041 ]
3244 [ 1.173, 0.068 ]
3245 [ 1.91, 0.111 ]
3246 [ 4.847, 0.231 ]
3247 [ 9.813, 0.436 ]
3248 [ 12.134, 0.617 ]
3249 [ 12.438, 0.732 ]
3250 [ 12.424, 0.811 ]
3251 [ 12.425, 0.894 ]
3252 [ -1 , -1 ] (max twenty pts)
3253 NHYDovf=[ "KB-P1ovf" ]
3254 *%
3255 ADD HYD NHYDsum=[ "KB-Pond1" ], NHYDs to add=[ "KB-P1R" +"KB-P1ovf" ]
3256 *%
3257 SAVE HYD NHYD=[ "KB-Pond1" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
3258 HYD_COMMENT=[ "Total Flows at KB first pond" ]
3259 *%
3260 CONTINUOUS STANDHYD NHYD=[ "KB-07" ], DT=[ 1 ]min, AREA=[ 10.86 ](ha), XIMP=[ 0.86 ],
3261 TIMP=[ 0.86 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:

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Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%), LGI=[269.072](m), MNI=[0.013], SCI=[0](min),
Continuous simulation parameters:
IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
END=-1

NHYDin=[ "KB-07" ], CINLET=[ 2.094 ](cms), NINLET=[ 1 ],
MajNHYD=[ "KB-07-MJ" ]
MinNHYD=[ "KB-07-MN" ]
TMJSTO=[ 1378 ](cu-m)

NHYDsum= [ "KB-07-S" ], NYHDs to add=[ "KB-07-MJ" +"KB-07-MN" ]

NYHD=[ "KB-08" ], DT=[1]min, AREA=[ 6.61 ](ha), XIMP=[ 0.64 ],
](cms), LOSS=[1]:
Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%), LGI=[209.921](m), MNI=[0.013], SCI=[0](min),
Continuous simulation parameters:
IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
END=-1

NHYDin=[ "KB-08" ], CINLET=[ 1.058 ](cms), NINLET=[ 1 ],
MajNHYD=[ "KB-08-MJ" ]
MinNHYD=[ "KB-08-MN" ]
TMJSTO=[ 787 ](cu-m)

NHYDsum= [ "KB-08-S" ], NYHDs to add=[ "KB-08-MJ" +"KB-08-MN" ]

NYHD=[ "KB-09" ], DT=[1]min, AREA=[ 2.6 ](ha), XIMP=[ 0.86 ],
](cms), LOSS=[1]:
Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
Impervious areas: IAimp=[1.57](mm), SLPI=[2.0](%), LGI=[131.656](m), MNI=[0.013], SCI=[0](min),
Continuous simulation parameters:
IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
END=-1

NHYD=[ "KB-10_1" ], DT=[1]min, AREA=[ 2.37 ](ha), XIMP=[ 0.86 ],
](cms), LOSS=[1]:
Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
Impervious areas: IAimp=[1.57](mm), SLPI=[2.0](%), LGI=[125.698](m), MNI=[0.013], SCI=[0](min),
Continuous simulation parameters:
IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
END=-1

NHYD=[ "KB-10_2" ], DT=[1]min, AREA=[ 1.14 ](ha), XIMP=[ 0.86 ],
](cms), LOSS=[1]:
Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),

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3294 MNP=[0.250], SCP=[0](min),
3295 Impervious areas: IAimp=[1.57](mm), SLPI=[2.0](%), LGI=[87.178](m),
3296 MNI=[0.013], SCI=[0](min),
3297 Continuous simulation parameters:
3298 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
3299 END=-1
3299 *%-----|-----|
3300 *%-----|-----|
3300 CONTINUOUS STANDHYD NHYD=[ "KB-12" ], DT=[1]min, AREA=[ 4.86 ](ha), XIMP=[ 0.79 ],
3301 TIMP=[ 0.79 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3302 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3303 F=[ 0.00 ](mm),
3304 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3305 MNP=[ 0.250 ], SCP=[ 0 ](min),
3306 Impervious areas: IAimp=[ 1.099 ](mm), SLPI=[ 2.0 ](%),
3307 LGI=[ 180.000 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3308 Continuous simulation parameters:
3309 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3310 END=-1
3310 *%-----|-----|
3311 COMPUTE DUALHYD NHYDin=[ "KB-12" ], CINLET=[ 0.8665 ](cms), NINLET=[ 1 ],
3312 MajNHYD=[ "KB-12-MJ" ]
3313 MinNHYD=[ "KB-12-MN" ]
3313 TMJSTO=[ 632 ](cu-m)
3313 *%-----|-----|
3314 ADD HYD NHYDsum=[ "KB-12-S" ], NHYDs to add=[ "KB-12-MJ" +"KB-12-MN" ]
3315 *%-----|-----|
3316 CONTINUOUS STANDHYD NHYD=[ "KB-13" ], DT=[1]min, AREA=[ 10.19 ](ha), XIMP=[ 0.64 ],
3317 TIMP=[ 0.64 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3318 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3319 F=[ 0.00 ](mm),
3320 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3321 MNP=[ 0.250 ], SCP=[ 0 ](min),
3322 Impervious areas: IAimp=[ 0.785 ](mm), SLPI=[ 2.0 ](%),
3323 LGI=[ 260.640 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3324 Continuous simulation parameters:
3325 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3326 END=-1
3326 *%-----|-----|
3327 COMPUTE DUALHYD NHYDin=[ "KB-13" ], CINLET=[ 1.722 ](cms), NINLET=[ 1 ],
3328 MajNHYD=[ "KB-13-MJ" ]
3329 MinNHYD=[ "KB-13-MN" ]
3330 TMJSTO=[ 1077 ](cu-m)
3330 *%-----|-----|
3331 ADD HYD NHYDsum=[ "KB-13-S" ], NHYDs to add=[ "KB-13-MJ" +"KB-13-MN" ]
3332 *%-----|-----|
3333 CONTINUOUS STANDHYD NHYD=[ "KB-14" ], DT=[1]min, AREA=[ 5.47 ](ha), XIMP=[ 0.64 ],
3334 TIMP=[ 0.64 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3335 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3336 F=[ 0.00 ](mm),
3337 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3338 MNP=[ 0.250 ], SCP=[ 0 ](min),
3339 Impervious areas: IAimp=[ 0.785 ](mm), SLPI=[ 2.0 ](%),
3340 LGI=[ 190.962 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3341 Continuous simulation parameters:
3342 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3343 END=-1
3343 *%-----|-----|
3344 COMPUTE DUALHYD NHYDin=[ "KB-14" ], CINLET=[ 0.8734 ](cms), NINLET=[ 1 ],
3345 MajNHYD=[ "KB-14-MJ" ]
3346 MinNHYD=[ "KB-14-MN" ]
3347 TMJSTO=[ 631 ](cu-m)
3347 *%-----|-----|
3348 ADD HYD NHYDsum=[ "KB-14-S" ], NHYDs to add=[ "KB-14-MJ" +"KB-14-MN" ]
3349 *%-----|-----|
3350 *%-----|-----|

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3342 CONTINUOUS STANDHYD NHYD=[ "KB-16_2" ], DT=[1]min, AREA=[ 3.42 ](ha), XIMP=[ 0.71 ],
3343 TIMP=[ 0.71 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3344     Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3345     F=[ 0.00 ](mm),
3346     Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3347     MNP=[ 0.250 ], SCP=[ 0 ](min),
3348     Impervious areas: IAimp=[ 0.157 ](mm), SLPI=[ 0.3 ](%),
3349     LGI=[ 150.997 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3350     Continuous simulation parameters:
3351     IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3352     END=-1
3353 *%-----|-----|
3354 ADD HYD NHYDsum=[ "KB-P2" ], NHYDs to
3355 add=[ "KB-Pond1" +"KB-07-S" +"KB-08-S" +"KB-09" +"KB-10_1" +"KB-10_2" +"KB-12-S" +"KB-13-S" +"KB-1
3356 4-S" +"KB-16_2" ]
3357 *%-----|-----|
3358 ROUTE RESERVOIR NHYDout=[ "KB-P2R" ], NHYDin=[ "KB-P2" ],
3359 RDT=[ 1 ](min),
3360     TABLE of ( OUTFLOW-STORAGE ) values
3361     (cms) - (ha-m)
3362     [ 0.0 , 0.0 ]
3363     [ 0.053,0.005 ]
3364     [ 0.132,0.009 ]
3365     [ 0.269,0.014 ]
3366     [ 0.455,0.023 ]
3367     [ 0.699,0.037 ]
3368     [ 0.947,0.056 ]
3369     [ 1.853,0.09 ]
3370     [ 2.712,0.146 ]
3371     [ 6.626,0.287 ]
3372     [ 11.228,0.515 ]
3373     [ 14.885,0.738 ]
3374     [ 16.473,0.893 ]
3375     [ 17.311,0.998 ]
3376     [ 17.633,1.063 ]
3377     [ 17.634,1.112 ]
3378     [ -1 , -1 ] (max twenty pts)
3379     NHYDovf=[ "KB-P2ovf" ]
3380 *%-----|-----|
3381 ADD HYD NHYDsum=[ "KB-Pond2" ], NHYDs to add=[ "KB-P2R" +"KB-P2ovf" ]
3382 *%-----|-----|
3383 SAVE HYD NHYD=[ "KB-Pond2" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
3384     HYD_COMMENT=[ "Total Flows at KB second pond" ]
3385 *%-----|-----|
3386 CONTINUOUS STANDHYD NHYD=[ "KB-16_1" ], DT=[1]min, AREA=[ 2.8 ](ha), XIMP=[ 0.75 ],
3387 TIMP=[ 0.75 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3388     Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3389     F=[ 0.00 ](mm),
3390     Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3391     MNP=[ 0.250 ], SCP=[ 0 ](min),
3392     Impervious areas: IAimp=[ 0.157 ](mm), SLPI=[ 0.3 ](%),
3393     LGI=[ 136.626 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3394     Continuous simulation parameters:
3395     IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3396     END=-1
3397 *%-----|-----|
3398 ADD HYD NHYDsum=[ "KB-P3" ], NHYDs to add=[ "KB-Pond2" +"KB-16_1" ]
3399 *%-----|-----|
3400 *%-----|-----|
3401 * One inflow node from pond 3 is added to the model (ROUTE RESERVOIR)
3402 * Another inflow node from right side of pond 3 is not added to the model
3403 ROUTE RESERVOIR NHYDout=[ "KB-P3R" ], NHYDin=[ "KB-P3" ],
3404 RDT=[ 1 ](min),
3405     TABLE of ( OUTFLOW-STORAGE ) values
3406     (cms) - (ha-m)
3407     [ 0.0 , 0.0 ]

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3396 [0.051,0.002]
3397 [0.048,0.003]
3398 [0.057,0.029]
3399 [0.089,0.045]
3400 [0.133,0.069]
3401 [0.199,0.106]
3402 [0.321,0.172]
3403 [1.029,0.306]
3404 [4.036,0.527]
3405 [8.332,0.761]
3406 [11.727,0.941]
3407 [14.125,1.067]
3408 [15.675,1.149]
3409 [16.555,1.196]
3410 [16.911,1.214]
3411 [-1, -1] (max twenty pts)
3412 NHYDovf=[ "KB-P3ovf" ]
3413 *%-----|-----|
3414 ADD HYD NHYDsum=[ "KB-Pond3" ], NHYDs to add=[ "KB-P3R "+"KB-P3ovf" ]
3415 *%-----|-----|
3416 SAVE HYD NHYD=[ "KB-Pond3" ], # OF PCYCLES=[-1], ICASEsh=[1]
3417 HYD_COMMENT=[ "Total Flows at KB third pond" ]
3418 *%-----|-----|
3419 *#***** EXISTING / PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118080), SWM
3420 Modeling Approach, NOVATECH Report June, 2020)
3421 *# - TO FRASER-CLARKE DRAIN
3422 *#***** EXISTING / PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118080), SWM
3423 CONTINUOUS STANDHYD NHYD=[ "FC-01" ], DT=[1]min, AREA=[ 8.03 ](ha), XIMP=[ 0.47 ],
3424 TIMP=[ 0.47 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3425 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3426 F=[ 0.00 ](mm),
3427 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3428 MNP=[ 0.250 ], SCP=[ 0 ](min),
3429 Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 1.0 ](%),
3430 LGI=[ 231.373 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3431 Continuous simulation parameters:
3432 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3433 END=-1
3434 *%-----|-----|
3435 COMPUTE DUALHYD NHYDin=[ "FC-01" ], CINLET=[ 0.756 ](cms), NINLET=[ 1 ],
3436 MajNHYD=[ "FC-01-MJ" ]
3437 MinNHYD=[ "FC-01-MN" ]
3438 TMJSTO=[ 714 ](cu-m)
3439 *%-----|-----|
3440 ADD HYD NHYDsum=[ "FC-01-S" ], NHYDs to add=[ "FC-01-MJ "+"FC-01-MN" ]
3441 *%-----|-----|
3442 CONTINUOUS STANDHYD NHYD=[ "FC-02" ], DT=[1]min, AREA=[ 16.05 ](ha), XIMP=[ 0.93 ],
3443 TIMP=[ 0.93 ], DWF=[ 0 ](cms), LOSS=[ 1 ]:
3444 Horton: Fo=[ 76.20 ](mm/hr), Fc=[ 13.20 ](mm/hr), DCAY=[ 4.14 ](/hr),
3445 F=[ 0.00 ](mm),
3446 Pervious areas: IAper=[ 4.67 ](mm), SLPP=[ 2.0 ](%), LGP=[ 40 ](m),
3447 MNP=[ 0.250 ], SCP=[ 0 ](min),
3448 Impervious areas: IAimp=[ 1.57 ](mm), SLPI=[ 1.0 ](%),
3449 LGI=[ 327.109 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3450 Continuous simulation parameters:
3451 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs), InterEventTime=[ 12 ](hrs),
3452 END=-1
3453 *%-----|-----|
3454 COMPUTE DUALHYD NHYDin=[ "FC-02" ], CINLET=[ 1.159 ](cms), NINLET=[ 1 ],
3455 MajNHYD=[ "FC-02-MJ" ]
3456 MinNHYD=[ "FC-02-MN" ]
3457 TMJSTO=[ 2385 ](cu-m)
3458 *%-----|-----|
3459 ADD HYD NHYDsum=[ "FC-02-S" ], NHYDs to add=[ "FC-02-MJ "+"FC-02-MN" ]
3460 *%-----|-----|

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3499 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3500 MNP=[0.250], SCP=[0](min),
3501 Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%), LGI=[102.956](m), MNI=[0.013], SCI=[0](min),
3502 Continuous simulation parameters:
3503 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs), END=-1
3504 *%-----|-----|
3505 COMPUTE DUALHYD NHYDin=[ "JR-02" ], CINLET=[ 0.153 ](cms), NINLET=[ 1 ],
3506 MajNHYD=[ "JR-02-MJ" ]
3507 MinNHYD=[ "JR-02-MN" ]
3508 TMJSTO=[ 153 ](cu-m)
3509 *%-----|-----|
3510 ADD HYD NHYDsum=[ "JR-02-S" ], NYHDS to add=[ "JR-02-MJ" +"JR-02-MN" ]
3511 *%-----|-----|
3512 *#***** Catchment FRASER
3513 *# - To Fraser-Clarke drain (north of the Jock)
3514 *# - Developed land with assumed 43% imp.
3515 *# - 2020-12-17 Change Fraser area to be 35.1 as measured from QGIS
3516 *# - 2020-12-17 All Fraser is undeveloped (Nashyd)
3517 *#*****|-----|
3518 CONTINUOUS NASHYD NYHD=[ "FRASER-DRN" ], DT=[ 1 ]min, AREA=[ 13.65 ](ha),
3519 DWF=[ 0 ](cms), CN/C=[ 77 ], IA=[ 4.67 ](mm),
3520 N=[ 3 ], TP=[ 0.4258 ]hrs,
3521 Continuous simulation parameters:
3522 IaRECper=[ 4 ](hrs),
3523 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
3524 InterEventTime=[ 12 ](hrs)
3525 Baseflow simulation parameters:
3526 BaseFlowOption=[ 1 ],
3527 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
3528 VHydCond=[ 0.055 ](mm/hr), END=-1
3529 *
3530 CONTINUOUS STANDHYD NYHD=[ "FRASER-D" ], DT=[ 1 ]min, AREA=[ 21.61 ](ha),
3531 XIMP=[ 0.585 ], TIMP=[ 0.585 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
3532 SCS curve number CN=[ 80 ],
3533 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
3534 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
3535 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
3536 LGI=[ 379.561 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3537 Continuous simulation parameters:
3538 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
3539 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
3540 InterEventTime=[ 18 ](hrs), END=-1
3541 *%-----|-----|
3542 COMPUTE DUALHYD NHYDin=[ "FRASER-D" ], CINLET=[ 2.281 ](cms), NINLET=[ 1 ],
3543 MajNHYD=[ "FRASER-J" ]
3544 MinNHYD=[ "FRASER-N" ]
3545 TMJSTO=[ 9999999 ](cu-m)
3546 *%-----|-----|
3547 ADD HYD NYDsum=[ "FRASER-S" ], NYHDS to add=[ "FRASER-J" +"FRASER-N" ]
3548 *%-----|-----|
3549 *ROUTE RESERVOIR NYDout=[ "MS_P20" ], NYDin=[ "FRASER" ],
3550 * RDT=[ 1 ](min),
3551 * TABLE of ( OUTFLOW-STORAGE ) values
3552 * (cms) - (ha-m)
3553 * [ 0.0 , 0.0 ]
3554 * [ 0.04 , 0.36 ]
3555 * [ -1 , -1 ] (max twenty pts)
3556 * NYDovf=[ "P20-OVF" ]
3557 *%-----|-----|
3558 ADD HYD NYDsum=[ "4241" ], NYHDS to
3559 add=[ "KB-Pond3" +"S-1-B" +"FRASER-DRN" +"FRASER-S" +"N_KB" +"FC-01-S" +"FC-02-S" +"FC-03-S" ]
3560 SAVE HYD NYD=[ "4241" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]

```

```

3561 HYD_COMMENT=[ "Total Flows at Ken-Burnett Outlet" ]
3562 *%-----|-----|
3563 *# Hydrograph from Node Ken-Burnett to station 3633
3564 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4241
3565 *#
3566 ROUTE CHANNEL      NHYDout=[ "4241-out" ], NHYDin=[ "4241" ], RDT=[1](min),
3567 CHLGHTh=[294](m), CHSLOPE=[0.1088](%), FPSLOPE=[0.1088](%),
3568 SECNUM=[1.0], NSEG=[3]
3569 ( SEGROUGH, SEGDIST (m))=[0.05, -20.12
3570                               -0.035, 45.26
3571                               0.05, 403.84] NSEG times
3572 ( DISTANCE (m), ELEVATION (m))= []
3573 [-909.72, 95 ]
3574 [-907.09, 94.5 ]
3575 [-904.65, 94 ]
3576 [-902.26, 93.5 ]
3577 [-44.51, 91.5 ]
3578 [-25.1, 91.5 ]
3579 [-20.98, 91 ]
3580 [-20.61, 90.5 ]
3581 [-20.12, 90 ]
3582 [-6.13, 87.26 ]
3583 [17.51, 86.56 ]
3584 [31.37, 87.2 ]
3585 [45.26, 90 ]
3586 [50.41, 90.5 ]
3587 [63.06, 91 ]
3588 [134.5, 91.5 ]
3589 [190.63, 92 ]
3590 [251.98, 92.5 ]
3591 [321.32, 93.5 ]
3592 [403.84, 95 ]
3593 *%-----|-----|
3594 ADD HYD          NHYDsum=[ "SN_KB" ], NHYDs to
3595 add=[ "4241-out" +"FC-04-S" +"JR-01-S" +"JR-02-S" ]
3596 *%-----|-----|
3597 SAVE HYD         NHYD=[ "SN_KB" ], # OF PCYCLES=[-1], ICASEsh=[1]
3598                  HYD_COMMENT=[ "Total Flows before Station 3633" ]
3599 *%-----|-----|
3600 *# Hydrograph from Station 3633 to Node Todd
3601 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 3633
3602 *# JFSA 2021-02-26 change the channel length (at station 3633) from 650m to 608m and
3603   change the slope from 0.0498% to 0.24671%. That is because of adding station 4241
3604   between station 4534 and station 3633
3605 *#
3606 ROUTE CHANNEL      NHYDout=[ "N_TO" ], NHYDin=[ "SN_KB" ], RDT=[1](min),
3607 CHLGHTh=[608](m), CHSLOPE=[0.24671](%), FPSLOPE=[0.24671](%),
3608 SECNUM=[1.0], NSEG=[3]
3609 ( SEGROUGH, SEGDIST (m))=[0.05, -23.74
3610                               -0.035, 23.74
3611                               0.05, 26.50] NSEG times
3612 ( DISTANCE (m), ELEVATION (m))= []
3613 -29.24, 91.0
3614 -27.41, 90.5
3615 -25.64, 90
3616 -23.74, 89.5
3617 -22, 89.26
3618 -20, 88.51
3619 -19, 88.32
3620 -15, 88.1
3621 -10, 88.11
3622 -5, 88.17
3623 0, 88.27
3624 5, 88.19
3625 10, 88.06
3626 15, 88.48

```

```

3624          16, 88.7
3625          23.74, 89.5
3626          24.68, 90
3627          25.57, 90.5
3628          26.50, 91.0
3629          *
3630          *
3631          *
3632          *
3633          *
3634          *
3635          *
3636          *
3637          *
3638          *
3639          *
3640          *
3641          *
3642          *
3643          *
3644          *
3645          *
3646          *
3647          *
3648          *
3649          *# Catchment Greenbank
3650          *# - To Greenbank Drain (south of the Jock)
3651          *# - JFSA 2021-01-18 add Greenbank pond as per JFSA, P598(06)-15, June 2016
3652          *# - JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GIS measurements
3653          *#
3654 CONTINUOUS STANDHYD NHYD=[ "Greenbank" ], DT=[1]min, AREA=[36.6](ha),
3655          XIMP=[0.639], TIMP=[0.682], DWF=[0](cms), LOSS=[2],
3656          SCS curve number CN=[77],
3657          Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3658          LGP=[40](m), MNP=[0.25], SCP=[0](min),
3659          Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3660          LGI=[493.96](m), MNI=[0.013], SCI=[0](min),
3661          Continuous simulation parameters:
3662          IaRECper=[4](hrs), IaRECimp=[4](hrs),
3663          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3664          InterEventTime=[18](hrs), END=-1
3665          *
3666 ROUTE RESERVOIR
3667          NHYDout=[ "GreenB_MN" ] ,NHYDin=[ "Greenbank" ] ,
3668          RDT=[1](min),
3669          TABLE of ( OUTFLOW-STORAGE ) values
3670          (cms) - (ha-m)
3671          [ 0.0 , 0.0 ]
3672          [ 0.033 , 0.084 ]
3673          [ 0.039 , 0.201 ]
3674          [ 0.113 , 0.292 ]
3675          [ 0.237 , 0.386 ]
3676          [ 0.382 , 0.484 ]
3677          [ 0.539 , 0.585 ]
3678          [ 0.7 , 0.692 ]
3679          [ 0.86 , 0.804 ]
3680          [ 4.684 , 0.922 ]
3681          [ 11.539 , 1.052 ]
3682          [ 20.867 , 1.168 ]
3683          [ 103.616 , 1.974 ]
3684          [ -1 , -1 ] (max twenty pts)
3685          NHYDovf=[ "GreenB_MJ" ] ,
3686          *
3687 ADD HYD          NHYDsum=[ "GreenB" ], NHYDs to add=[ "N_TO" +"GreenB_MJ" +"GreenB_MN" ]
3688          *
3689 SAVE HYD          NHYD=[ "GreenB" ], # OF PCYCLES=[-1], ICASEsh=[1]

```

```

3690          HYD_COMMENT=[ "Total Flows at Greenbank Drain" ]
3691 *%-----|-----|
3692 *#***** Catchment TODD
3693 *#   - To Todd Drain (south of the Jock)
3694 *#   - Subdivision with 43% imp. as per Barrhaven South MSS
3695 *#   - 2020-11-30 increase imp. based on P598(04)-11
3696 *#   - 2020-11-30 update TODD Tributary Drainage Area to = 146.015 ha based on
3697 P598(04)-11
3698 *#   - 2020-11-30 split TODD Drainage Area to MAJOR, MINOR, POND and ALL
3699 *#*****|-----|
3700 *#   - JFSA 2021-01-19 add "TODD_MN1" as part of Clarke("W_CLAR_MJ") and remove it
from Todd
3701 *CONTINUOUS STANDHYD NYHD=[ "TODD_MN1" ], DT=[1]min, AREA=[1.772](ha),
3702 *                               XIMP=[0.53], TIMP=[0.57], DWF=[0](cms), LOSS=[2],
3703 *                               SCS curve number CN=[77],
3704 *                               Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3705 *                               LGP=[40](m), MNP=[0.25], SCP=[0](min),
3706 *                               Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3707 *                               LGI=[108.689](m), MNI=[0.013], SCI=[0](min),
3708 *                               Continuous simulation parameters:
3709 *                               IaRECper=[4](hrs), IaRECImp=[4](hrs),
3710 *                               SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3711 *                               InterEventTime=[18](hrs), END=-1
3712 *%-----|-----|
3713 CONTINUOUS STANDHYD NYHD=[ "TODD_MN2" ], DT=[1]min, AREA=[2.1](ha),
3714 XIMP=[0.53], TIMP=[0.57], DWF=[0](cms), LOSS=[2],
3715 SCS curve number CN=[77],
3716 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3717 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3718 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3719 LGI=[118.322](m), MNI=[0.013], SCI=[0](min),
3720 Continuous simulation parameters:
3721 IaRECper=[4](hrs), IaRECImp=[4](hrs),
3722 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3723 InterEventTime=[18](hrs), END=-1
3724 *%-----|-----|
3725 CONTINUOUS STANDHYD NYHD=[ "TODD_MN3" ], DT=[1]min, AREA=[0.117](ha),
3726 XIMP=[0.53], TIMP=[0.57], DWF=[0](cms), LOSS=[2],
3727 SCS curve number CN=[77],
3728 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3729 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3730 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3731 LGI=[27.928](m), MNI=[0.013], SCI=[0](min),
3732 Continuous simulation parameters:
3733 IaRECper=[4](hrs), IaRECImp=[4](hrs),
3734 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3735 InterEventTime=[18](hrs), END=-1
3736 *%-----|-----|
3737 CONTINUOUS STANDHYD NYHD=[ "TODD_MJ" ], DT=[1]min, AREA=[30.230](ha),
3738 XIMP=[0.52], TIMP=[0.64], DWF=[0](cms), LOSS=[2],
3739 SCS curve number CN=[77],
3740 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3741 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3742 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3743 LGI=[448.925](m), MNI=[0.013], SCI=[0](min),
3744 Continuous simulation parameters:
3745 IaRECper=[4](hrs), IaRECImp=[4](hrs),
3746 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3747 InterEventTime=[18](hrs), END=-1
3748 *%-----|-----|
3749 *      -JFSA, 2021-01-19 update "TODD_ALL" area from 108.741 ha to 112.908 ha based on
GIS measurements (148.41-30.23-0.117-2.1-3.055=112.908 ha)
3750 CONTINUOUS STANDHYD NYHD=[ "TODD_ALL" ], DT=[1]min, AREA=[112.908](ha),
3751 XIMP=[0.52], TIMP=[0.57], DWF=[0](cms), LOSS=[2],
3752 SCS curve number CN=[77],

```

```

Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),  

    LGP=[40](m), MNP=[0.25], SCP=[0](min),  

Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),  

    LGI=[867.594](m), MNI=[0.013], SCI=[0](min),
Continuous simulation parameters:  

IaRECper=[4](hrs), IaRECImp=[4](hrs),  

SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),  

InterEventTime=[18](hrs), END=-1
|-----|
NHYD= ["TODD_P"], DT=[1]min, AREA=[3.055](ha),  

XIMP=[0.63], TIMP=[0.63], DWF=[0](cms), LOSS=[2],  

SCS curve number CN=[77],  

Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),  

    LGP=[40](m), MNP=[0.25], SCP=[0](min),  

Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),  

    LGI=[142.712](m), MNI=[0.013], SCI=[0](min),
Continuous simulation parameters:  

IaRECper=[4](hrs), IaRECImp=[4](hrs),  

SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),  

InterEventTime=[18](hrs), END=-1
|-----|
|-----|
23 "TODD_DEVL" is part of the Corrigan sub-catchment because it  

SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"  

remain the same.  

D NYHD= ["TODD_DEVL"], DT=[1]min, AREA=[15.87](ha),  

XIMP=[0.63], TIMP=[0.63], DWF=[0](cms), LOSS=[2],  

SCS curve number CN=[77],  

Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),  

    LGP=[40](m), MNP=[0.25], SCP=[0](min),  

Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),  

    LGI=[325.27](m), MNI=[0.013], SCI=[0](min),
Continuous simulation parameters:  

IaRECper=[4](hrs), IaRECImp=[4](hrs),  

SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),  

InterEventTime=[18](hrs), END=-1
|-----|
23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now  

nd its parameters remain the same.  

NYHD= ["TODD_UnD"], DT=[1]min, AREA=[12.47](ha),  

DWF=[0](cms), CN/C=[77], IA=[4.67](mm),  

N=[3], TP=[1.10]hrs,  

Continuous simulation parameters:  

IaRECper=[4](hrs),  

SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),  

InterEventTime=[12](hrs)
Baseflow simulation parameters:  

BaseFlowOption=[1],  

InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)  

VHydCond=[0.055](mm/hr), END=-1
|-----|
ture
NHYDin= ["TODD_MJ"], CINLET=[3.314](cms), NINLET=[1],  

MajNHYD= ["TODD_MJj"]  

MinNHYD= ["TODD_MJn"]  

TMJSTO=[0.1](cu-m)  

NHYDout= ["TODD_MJn"] , NYHDin= ["TODD_MJ"] ,  

RDT=[1](min),
    TABLE of ( OUTFLOW-STORAGE ) values
        (cms) - (ha-m)
        [      0.0 , 0.0      ]
        [ 3.314 , 0.0001   ]
        [      -1 , -1      ] (max twenty pts)
    NYHDovf= ["TODD_MJj"] ,
|-----|
ture

```

```

3816 *COMPUTE DUALHYD      NHYDin=[ "TODD_MN1" ], CINLET=[ 0.227 ](cms), NINLET=[1],
3817 *
3818 *
3819 *
3820 *ROUTE RESERVOIR    MajNHYD=[ "TODD_MN1j" ]
3821 *                         MinNHYD=[ "TODD_MN1n" ]
3822 *                         TMJSTO=[ 0.1 ](cu-m)
3823 *                         NHYDout=[ "TODD_MN1n" ] , NHYDin=[ "TODD_MN1" ] ,
3824 *                         RDT=[1](min),
3825 *                         TABLE of ( OUTFLOW-STORAGE ) values
3826 *                                         (cms) - (ha-m)
3827 *                                         [     0.0 , 0.0      ]
3828 *                                         [ 0.227 , 0.0001  ]
3829 *                                         [     -1 , -1       ] (max twenty pts)
3830 *                         NHYDovf=[ "TODD_MN1j" ] ,
3831 *%
3832 *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
3833 *COMPUTE DUALHYD      NHYDin=[ "TODD_MN2" ], CINLET=[ 0.268 ](cms), NINLET=[1],
3834 *                         MajNHYD=[ "TODD_MN2j" ]
3835 *                         MinNHYD=[ "TODD_MN2n" ]
3836 *                         TMJSTO=[ 0.1 ](cu-m)
3837 *ROUTE RESERVOIR      NHYDout=[ "TODD_MN2n" ] , NHYDin=[ "TODD_MN2" ] ,
3838 *                         RDT=[1](min),
3839 *                         TABLE of ( OUTFLOW-STORAGE ) values
3840 *                                         (cms) - (ha-m)
3841 *                                         [     0.0 , 0.0      ]
3842 *                                         [ 0.268 , 0.0001  ]
3843 *                                         [     -1 , -1       ] (max twenty pts)
3844 *                         NHYDovf=[ "TODD_MN2j" ] ,
3845 *%
3846 *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
3847 *COMPUTE DUALHYD      NHYDin=[ "TODD_MN3" ], CINLET=[ 0.016 ](cms), NINLET=[1],
3848 *                         MajNHYD=[ "TODD_MN3j" ]
3849 *                         MinNHYD=[ "TODD_MN3n" ]
3850 *                         TMJSTO=[ 0.1 ](cu-m)
3851 *ROUTE RESERVOIR      NHYDout=[ "TODD_MN3n" ] , NHYDin=[ "TODD_MN3" ] ,
3852 *                         RDT=[1](min),
3853 *                         TABLE of ( OUTFLOW-STORAGE ) values
3854 *                                         (cms) - (ha-m)
3855 *                                         [     0.0 , 0.0      ]
3856 *                                         [ 0.016 , 0.0001  ]
3857 *                                         [     -1 , -1       ] (max twenty pts)
3858 *                         NHYDovf=[ "TODD_MN3j" ] ,
3859 *%
3860 *-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
3861 *      -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
3862 major system from A2 can be added to Todd
3863 CONTINUOUS STANDHYD  NHYD=[ "A2" ], DT=[1]min, AREA=[ 25.5 ](ha),
3864 XIMP=[ 0.42 ], TIMP=[ 0.52 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
3865 SCS curve number CN=[ 75 ],
3866 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
3867 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
3868 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
3869 LGI=[ 566 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
3870 Continuous simulation parameters:
3871 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
3872 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
3873 InterEventTime=[ 18 ](hrs), END=-1
3874 *%
3875 COMPUTE DUALHYD      NHYDin=[ "A2" ], CINLET=[ 1.818 ](cms), NINLET=[1],
3876 MajNHYD=[ "A2-MJ" ]
3877 MinNHYD=[ "A2-MN" ]
3878 TMJSTO=[ 924 ](cu-m)
3879 *%
3880 ADD HYD              NHYDsum=[ "TODD" ], NHYDs to
3881 add=[ "TODD_MN2n" +"TODD_MN3n" +"TODD_MJj" +"TODD_P" +"TODD_ALL" +"W_CLAR_MJn" ]
3882 *%
3883 SAVE HYD             NHYD=[ "TODD" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
3884 HYD_COMMENT=[ "Total Flows at Todd Drain" ]
3885 *%
3886 *#*****#
3887 *# Todd Pond 3

```

```

3880 *#      - Rating curve obtained from Barrhaven South MSS modeling
3881 *#      - stantec 2007, Tributary Drainage Area to MSS Pond 3 = 193 ha
3882 *#*****
3883 ROUTE RESERVOIR      NHYDout=[ "MS_P3" ],   NHYDin=[ "TODD" ],
3884          RDT=[1](min),
3885          TABLE of ( OUTFLOW-STORAGE ) values
3886          (cms) - (ha-m)
3887          [ 0.0 , 0.0 ]
3888          [ 0.014 , 0.155 ]
3889          [ 0.048 , 0.394 ]
3890          [ 0.061 , 0.56 ]
3891          [ 0.08 , 0.909 ]
3892          [ 0.088 , 1.089 ]
3893          [ 0.109 , 1.652 ]
3894          [ 0.118 , 1.952 ]
3895          [ 0.122 , 2.099 ]
3896          [ 1.972 , 2.269 ]
3897          [ 9.135 , 2.598 ]
3898          [ 15.608 , 2.826 ]
3899          [ 19.256 , 2.942 ]
3900          [ 27.282 , 3.181 ]
3901          [ 40.957 , 3.55 ]
3902          [ 56.372 , 3.929 ]
3903          [ 73.349 , 4.317 ]
3904          [ 85.469 , 4.579 ]
3905          [ 104.771 , 4.977 ]
3906          [ -1 , -1 ] (max twenty pts)
3907          NHYDovf=[ "P3-OVF" ]
3908 *%-----|-----|
3909 ADD HYD      NHYDsum=[ "SN_TO" ], NHYDs to
3910 add=[ "GreenB"+"MS_P3"+"P3-OVF"+"TODD_MN2j"+"A2-MJ" ]
3911 *%-----|-----|
3912 SAVE HYD      NHYD=[ "SN_TO" ], # OF PCYCLES=[-1], ICASEsh=[1]
3913          HYD_COMMENT=[ "Total Flows at Todd Drain" ]
3914 *%-----|-----|
3915 *# Hydrograph from Todd Drain routed to Corrigan Drain
3916 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
3917 *# 2021-02-19 Change the slope from 0.033 % (as per Stantec Report 2007) to 0.05 % so
3918 the model will be more stable and give reasonable results. It is justifiable as ROUTE
3919 CHANNELs aren't well suited to really flat slopes.
3920 *
3921 ROUTE CHANNEL      NHYDout=[ "N_TO" ] ,NHYDin=[ "SN_TO" ] ,
3922          RDT=[1](min),
3923          CHLGTH=[280](m),   CHSLOPE=[0.05](%),
3924          FPSLOPE=[0.05](%),
3925          SECNUM=[1.0],      NSEG=[3]
3926          ( SEGROUGH, SEGDIST (m))=
3927          [0.075,-17.72
3928          -0.045,17.72
3929          0.075,80.62] NSEG times
3930          ( DISTANCE (m), ELEVATION (m))=
3931          [-83.32, 90.00]
3932          [-81.36, 89.50]
3933          [-79.12, 89.00]
3934          [-76.13, 88.50]
3935          [-20.46, 88.00]
3936          [-19.36, 87.50]
3937          [-18.51, 87.00]
3938          [-17.72, 86.50]
3939          [-11.95, 85.24]
3940          [-0.11, 85.12]
3941          [11.49, 85.20]
3942          [17.72, 86.50]
3943          [19.74, 87.00]
3944          [21.22, 87.50]

```

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3943 [22.68, 88.00]
3944 [24.28, 88.50]
3945 [26.79, 89.00]
3946 [71.98, 90.00]
3947 [80.62, 90.50]
3948 *%-----|-----|
3949 SAVE HYD NHYD=[ "N_TO" ], # OF PCYCLES=[-1], ICASEsh=[1]
3950 HYD_COMMENT=[ "Total inflows at Station 2462" ]
3951 *%-----|-----|
3952 *#*****|-----|
3953 *# Catchment CORRIG
3954 *# - To Corrigan Drain (south of the Jock)
3955 *# - Primarily Developed (medium density)
3956 *# - JFSA JAN 2021, add Corrigan subcatchments as per IBI, July 2008
3957 *#*****|-----|
3958 *ROUTE RESERVOIR NHYDout=[ "MS_P1" ], NHYDin=[ "CORRIG" ],
3959 *
3960 * TABLE of ( OUTFLOW-STORAGE ) values
3961 * (cms) - (ha-m)
3962 * [ 0.0 , 0.0 ]
3963 * [ 0.06 , 0.58 ]
3964 * [ -1 , -1 ] (max twenty pts)
3965 * NHYDovf=[ "P1-OVF" ]
3966 *%-----|-----|
3967 *ADD HYD NHYDsum=[ "SN_CO" ], NHYDs to add=[ "N_TO"+"P1-OVF"+"MS_P1" ]
3968 *%-----|-----|
3969 *SAVE HYD NHYD=[ "SN_CO" ], # OF PCYCLES=[-1], ICASEsh=[1]
3970 * HYD_COMMENT=[ "Total Flows at Corrigan Drain" ]
3971 *%-----|-----|
3972 * -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"
and its parameters remain the same.
3973 CONTINUOUS STANDHYD NHYD=[ "corr1" ], DT=[1]min, AREA=[15.87](ha),
3974 XIMP=[0.63], TIMP=[0.63], DWF=[0](cms), LOSS=[2],
3975 SCS curve number CN=[77],
3976 Previous surfaces: IAper=[4.67](mm), SLPP=[1](%),
3977 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3978 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3979 LGI=[325.27](m), MNI=[0.013], SCI=[0](min),
3980 Continuous simulation parameters:
3981 IaRECper=[4](hrs), IaRECImp=[4](hrs),
3982 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3983 InterEventTime=[18](hrs), END=-1
3984 *%-----|-----|
3985 * -JFSA 2021-02-23 add DUALHYD for "corr1". "corr1" DUALHYD Parameters are the
same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to "corr1".
3986 * At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for
A1-Corrig
3987 COMPUTE DUALHYD NHYDin=[ "corr1" ], CINLET=[1.818](cms), NINLET=[1],
3988 MajNHYD=[ "corr1-MJ" ]
3989 MinNHYD=[ "corr1-MN" ]
3990 TMJSTO=[924](cu-m)
3991 *%-----|-----|
3992 * -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
is called "corr2" and its parameters remain the same.
3993 CONTINUOUS NASHYD NHYD=[ "corr2" ], DT=[1]min, AREA=[12.47](ha),
3994 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
3995 N=[3], TP=[1.10]hrs,
3996 Continuous simulation parameters:
3997 IaRECper=[4](hrs),
3998 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3999 InterEventTime=[12](hrs)
4000 Baseflow simulation parameters:
4001 BaseFlowOption=[1],
4002 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4003 VHydCond=[0.055](mm/hr), END=-1

```

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4004 *-----|-----|
4005 *      -JFSA 2021-01-19 change A1-Corrig to be developed as per geoottawa website and
4006 apply the parameters of A2, the nearest sub-catchment to A1-Corrig, LGI is calculated
4007 based on A1-Corrig area
4008 *      -JFSA 2021-01-19 update all Corrigan areas based on GIS measurements, and keep
4009 LGI as it is from Corrigan Report, IBI Group, 2008 because LGI calculated is less than
4010 LGI from the Corrigan Report
4011 CONTINUOUS STANDHYD NHYD=[ "A1-Corrig" ], DT=[1]min, AREA=[15.75](ha),
4012 XIMP=[ 0.42 ], TIMP=[ 0.52 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4013 SCS curve number CN=[ 75 ],
4014 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4015 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4016 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4017 LGI=[ 324.037 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4018 Continuous simulation parameters:
4019 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4020 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4021 InterEventTime=[ 18 ](hrs), END=-1
4022 *
4023 *      -JFSA 2021-01-25 add DUALHYD for A1-Corrig. A1-Corrig DUALHYD Parameters are the
4024 same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to A1-Corrig.
4025 *      At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for
4026 A1-Corrig
4027 COMPUTE DUALHYD NHYDin=[ "A1-Corrig" ], CINLET=[ 1.818 ](cms), NINLET=[ 1 ],
4028 MajNHYD=[ "A1-MJ" ]
4029 MinNHYD=[ "A1-MN" ]
4030 TMJSTO=[ 924 ](cu-m)
4031 *-----|-----|
4032 *CONTINUOUS NASHYD NHYD=[ "A1-Corrig" ], DT=[1]min, AREA=[15.75](ha),
4033 *      DWF=[ 0 ](cms), CN/C=[ 66 ], IA=[ 2.5 ](mm),
4034 *      N=[ 3.0 ], TP=[ 0.36 ]hrs,
4035 *      Continuous simulation parameters:
4036 *      IaRECper=[ 4 ](hrs),
4037 *      SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4038 *      InterEventTime=[ 12 ](hrs)
4039 *      Baseflow simulation parameters:
4040 *      BaseFlowOption=[ 1 ],
4041 *      InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
4042 *      VHdCond=[ 0.055 ](mm/hr), END=-1
4043 *-----|-----|
4044 CONTINUOUS NASHYD NHYD=[ "B1" ], DT=[1]min, AREA=[ 2.77 ](ha),
4045 DWF=[ 0 ](cms), CN/C=[ 56 ], IA=[ 2.5 ](mm),
4046 N=[ 3.0 ], TP=[ 0.23 ]hrs,
4047 Continuous simulation parameters:
4048 IaRECper=[ 4 ](hrs),
4049 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4050 InterEventTime=[ 12 ](hrs)
4051 Baseflow simulation parameters:
4052 BaseFlowOption=[ 1 ],
4053 InitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
4054 VHdCond=[ 0.055 ](mm/hr), END=-1
4055 *-----|-----|
4056 CONTINUOUS STANDHYD NHYD=[ "A4" ], DT=[1]min, AREA=[ 1.27 ](ha),
4057 XIMP=[ 0.65 ], TIMP=[ 0.65 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4058 SCS curve number CN=[ 75 ],
4059 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4060 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4061 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4062 LGI=[ 253 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4063 Continuous simulation parameters:
4064 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4065 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4066 InterEventTime=[ 18 ](hrs), END=-1
4067 *-----|-----|
4068 COMPUTE DUALHYD NHYDin=[ "A4" ], CINLET=[ 0.405 ](cms), NINLET=[ 1 ],
4069 MajNHYD=[ "A4-MJ" ]

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4064 MinNHYD=[ "A4-MN" ]
4065 TMJSTO=[ 68 ](cu-m)
4066 *%
4067 ADD HYD NHYDsum=[ "MH101" ], NHYDs to
4068 add=[ "A1-MJ"+"A1-MN"+"corr1-MJ"+"corr1-MN"+"corr2"+"B1"+"A4-MN" ]
4069 *%
4070 SAVE HYD NHYD=[ "MH101" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4071 HYD_COMMENT=[ "Total Flows at MH101" ]
4072 *%
4073 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout=[ "101-102" ], RNUMBER=[ 1.0 ], PDIAM=[ 1050 ](mm),
4074 PLNGTH=[ 368 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0054 ](m/m),
4075 NHYDin=[ "MH101" ], RDT=[ 1 ]
4076 *%
4077 * -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
4078 major system from A2 can be added to Todd
4079 *CONTINUOUS STANDHYD NHYD=[ "A2" ], DT=[ 1 ]min, AREA=[ 25.5 ](ha),
4080 * XIMP=[ 0.42 ], TIMP=[ 0.52 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4081 * SCS curve number CN=[ 75 ],
4082 * Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4083 * LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4084 * Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4085 * LGI=[ 566 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4086 * Continuous simulation parameters:
4087 * IaRECper=[ 4 ](hrs), IaREComp=[ 4 ](hrs),
4088 * SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4089 * InterEventTime=[ 18 ](hrs), END=-1
4090 *%
4091 *COMPUTE DUALHYD NHYDin=[ "A2" ], CINLET=[ 1.818 ](cms), NINLET=[ 1 ],
4092 * MajNHYD=[ "A2-MJ" ]
4093 * MinNHYD=[ "A2-MN" ]
4094 * TMJSTO=[ 924 ](cu-m)
4095 *%
4096 ADD HYD NHYDsum=[ "MH102" ], NHYDs to add=[ "A2-MN"+"101-102" ]
4097 *%
4098 SAVE HYD NHYD=[ "MH102" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4099 HYD_COMMENT=[ "Total Flows at MH102" ]
4100 *%
4101 CONTINUOUS STANDHYD NHYD=[ "A5" ], DT=[ 1 ]min, AREA=[ 1.6 ](ha),
4102 XIMP=[ 0.71 ], TIMP=[ 0.71 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4103 SCS curve number CN=[ 75 ],
4104 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4105 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4106 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4107 LGI=[ 300 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4108 Continuous simulation parameters:
4109 IaRECper=[ 4 ](hrs), IaREComp=[ 4 ](hrs),
4110 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4111 InterEventTime=[ 18 ](hrs), END=-1
4112 *%
4113 ADD HYD NHYDsum=[ "A5T" ], NHYDs to add=[ "A4-MJ"+"A5" ]
4114 *%
4115 COMPUTE DUALHYD NHYDin=[ "A5T" ], CINLET=[ 0.357 ](cms), NINLET=[ 1 ],
4116 MajNHYD=[ "A5-MJ" ]
4117 MinNHYD=[ "A5-MN" ]
4118 TMJSTO=[ 60 ](cu-m)
4119 *%
4120 * -JFSA Jan. 2021, A3 is a part of Todd so it is removed
4121 * -JFSA Jan. 2021, "A2-MJ" added to "Todd"
4122 *CONTINUOUS STANDHYD NHYD=[ "A3" ], DT=[ 1 ]min, AREA=[ 18.4 ](ha),
4123 XIMP=[ 0.58 ], TIMP=[ 0.65 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4124 SCS curve number CN=[ 75 ],
4125 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4126 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4127 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4128 LGI=[ 450 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4129 Continuous simulation parameters:

```

```

4127 *
4128 *
4129 *
4130 *%
4131 *ADD HYD
4132 *%
4133 *COMPUTE DUALHYD
4134 *
4135 *
4136 *
4137 *%
4138 ROUTE PIPE
4139
4140 *%
4141 ADD HYD
4142 *%
4143 SAVE HYD
4144
4145 *%
4146 ROUTE PIPE
4147
4148 *%
4149 CONTINUOUS STANDHYD
4150 NYHD=[ "A6" ], DT=[1]min, AREA=[1.56](ha),
4151 XIMP=[0.71], TIMP=[0.71], DWF=[0](cms), LOSS=[2],
4152 SCS curve number CN=[75],
4153 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4154 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4155 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4156 LGI=[280](m), MNI=[0.013], SCI=[0](min),
4157 Continuous simulation parameters:
4158 IaRECper=[4](hrs), IaRECimp=[4](hrs),
4159 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4160 InterEventTime=[18](hrs), END=-1
4161 *%
4162 ADD HYD
4163 *%
4164 COMPUTE DUALHYD
4165 NYHDin=[ "A6T" ], CINLET=[0.357](cms), NINLET=[1],
4166 MajNHYD=[ "A6-MJ" ]
4167 MinNHYD=[ "A6-MN" ]
4168 TMJSTO=[ 60 ](cu-m)
4169 * -JFSA Jan. 2021, A7-corrig is a part of Todd so it is removed
4170 *CONTINUOUS STANDHYD
4171 NYHD=[ "A7-corrig" ], DT=[1]min, AREA=[11.8](ha),
4172 XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4173 SCS curve number CN=[75],
4174 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4175 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4176 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4177 LGI=[438](m), MNI=[0.013], SCI=[0](min),
4178 Continuous simulation parameters:
4179 IaRECper=[4](hrs), IaRECimp=[4](hrs),
4180 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4181 InterEventTime=[18](hrs), END=-1
4182 *%
4183 *ADD HYD
4184 *%
4185 *COMPUTE DUALHYD
4186 NYHDin=[ "A7-A3RMJ" ], CINLET=[1.003](cms), NINLET=[1],
4187 MajNHYD=[ "A7R-MJ" ]
4188 MinNHYD=[ "A7R-MN" ]
4189 TMJSTO=[ 496 ](cu-m)
4190 *%
4191 ADD HYD
4192 *%
4193 SAVE HYD

```

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4191 HYD_COMMENT=[ "Total Flows at MH104" ]
4192 *%
4193 CONTINUOUS STANDHYD NHYD=[ "B2" ], DT=[1]min, AREA=[12.31](ha),
4194 XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4195 SCS curve number CN=[75],
4196 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4197 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4198 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4199 LGI=[417](m), MNI=[0.013], SCI=[0](min),
4200 Continuous simulation parameters:
4201 IaRECper=[4](hrs), IaRECImp=[4](hrs),
4202 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4203 InterEventTime=[18](hrs), END=-1
4204 *%
4205 COMPUTE DUALHYD NHYDin=[ "B2" ], CINLET=[1.029](cms), NINLET=[1],
4206 MajNHYD=[ "B2-MJ" ]
4207 MinNHYD=[ "B2-MN" ]
4208 TMJSTO=[508](cu-m)
4209 *%
4210 ROUTE PIPE PTYPE=[1]circ, NHYDout=[ "315-333" ], RNUMBER=[1.0], PDIAM=[1200](mm),
4211 PLNGTH=[254](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
4212 NHYDin=[ "B2-MN" ], RDT=[1]
4213 *%
4214 CONTINUOUS STANDHYD NHYD=[ "B3" ], DT=[1]min, AREA=[5.59](ha),
4215 XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4216 SCS curve number CN=[75],
4217 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4218 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4219 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4220 LGI=[345](m), MNI=[0.013], SCI=[0](min),
4221 Continuous simulation parameters:
4222 IaRECper=[4](hrs), IaRECImp=[4](hrs),
4223 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4224 InterEventTime=[18](hrs), END=-1
4225 *%
4226 COMPUTE DUALHYD NHYDin=[ "B3" ], CINLET=[0.459](cms), NINLET=[1],
4227 MajNHYD=[ "B3-MJ" ]
4228 MinNHYD=[ "B3-MN" ]
4229 TMJSTO=[227](cu-m)
4230 *%
4231 ADD HYD NHYDsum=[ "MH333" ], NHYDs to add=[ "B3-MN" + "315-333" ]
4232 *%
4233 SAVE HYD NHYD=[ "MH333" ], # OF PCYCLES=[-1], ICASEsh=[1]
4234 HYD_COMMENT=[ "Total Flows at MH333" ]
4235 *%
4236 ROUTE PIPE PTYPE=[1]circ, NHYDout=[ "333-335" ], RNUMBER=[1.0], PDIAM=[1200](mm),
4237 PLNGTH=[251](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
4238 NHYDin=[ "MH333" ], RDT=[1]
4239 *%
4240 ROUTE PIPE PTYPE=[1]circ, NHYDout=[ "335-338" ], RNUMBER=[1.0], PDIAM=[1200](mm),
4241 PLNGTH=[185](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
4242 NHYDin=[ "333-335" ], RDT=[1]
4243 *%
4244 ROUTE PIPE PTYPE=[1]circ, NHYDout=[ "338-340" ], RNUMBER=[1.0], PDIAM=[1350](mm),
4245 PLNGTH=[233](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
4246 NHYDin=[ "335-338" ], RDT=[1]
4247 *%
4248 CONTINUOUS STANDHYD NHYD=[ "B4" ], DT=[1]min, AREA=[7.6](ha),
4249 XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4250 SCS curve number CN=[75],
4251 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4252 LGP=[40](m), MNP=[0.25], SCP=[0](min),
Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
LGI=[388](m), MNI=[0.013], SCI=[0](min),
Continuous simulation parameters:
IaRECper=[4](hrs), IaRECImp=[4](hrs),

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4253                               SMIN=[-1](mm),   SMAX=[-1](mm),   SK=[0.010]/(mm),
4254                               InterEventTime=[18](hrs),     END=-1
4255 *%
4256 COMPUTE DUALHYD      NHYDin=[ "B4" ], CINLET=[ 0.655 ](cms), NINLET=[ 1 ],
4257                               MajNHYD=[ "B4-MJ" ]
4258                               MinNHYD=[ "B4-MN" ]
4259                               TMJSTO=[ 323 ](cu-m)
4260 *%
4261 ADD HYD                NHYDsum=[ "MH340" ], NHYDs to add=[ "338-340" +"B4-MN" ]
4262 *%
4263 SAVE HYD               NHYD=[ "MH340" ],    # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4264                               HYD_COMMENT=[ "Total Flows at MH340" ]
4265 *%
4266 ROUTE PIPE             PTYPE=[ 1 ]circ, NHYDout=[ "340-104" ], RNUMBER=[ 1.0 ], PDIAM=[ 1650 ](mm),
4267                               PLNGTH=[ 240 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0015 ](m/m),
4268                               NHYDin=[ "MH340" ], RDT=[ 1 ]
4269 *%
4270 ADD HYD                NHYDsum=[ "MH104T" ], NHYDs to add=[ "340-104" +"MH104" ]
4271 *%
4272 ROUTE PIPE             PTYPE=[ 2 ]rect, NHYDout=[ "104-105" ], RNUMBER=[ 1.0 ],
4273                               PWIDTH=[ 2400 ](mm) by PHEIGHT=[ 2100 ](mm),
4274                               PLNGTH=[ 380 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m),
4275                               NHYDin=[ "MH104T" ], RDT=[ 1 ]
4276 *%
4277 CONTINUOUS STANDHYD    NHYD=[ "B5" ], DT=[ 1 ]min, AREA=[ 2.2 ](ha),
4278                               XIMP=[ 0.57 ], TIMP=[ 0.57 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4279                               SCS curve number CN=[ 75 ],
4280                               Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4281                               LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4282                               Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4283                               LGI=[ 187 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4284                               Continuous simulation parameters:
4285                               IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4286                               SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4287                               InterEventTime=[ 18 ](hrs), END=-1
4288 *%
4289 COMPUTE DUALHYD        NHYDin=[ "B5" ], CINLET=[ 0.260 ](cms), NINLET=[ 1 ],
4290                               MajNHYD=[ "B5-MJ" ]
4291                               MinNHYD=[ "B5-MN" ]
4292                               TMJSTO=[ 250 ](cu-m)
4293 *%
4294 CONTINUOUS STANDHYD    NHYD=[ "A8" ], DT=[ 1 ]min, AREA=[ 0.96 ](ha),
4295                               XIMP=[ 0.71 ], TIMP=[ 0.71 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4296                               SCS curve number CN=[ 75 ],
4297                               Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4298                               LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4299                               Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4300                               LGI=[ 186 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4301                               Continuous simulation parameters:
4302                               IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4303                               SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4304                               InterEventTime=[ 18 ](hrs), END=-1
4305 *%
4306 ADD HYD                NHYDsum=[ "A8T" ], NHYDs to add=[ "A6-MJ" +"A8" ]
4307 *%
4308 COMPUTE DUALHYD        NHYDin=[ "A8T" ], CINLET=[ 0.238 ](cms), NINLET=[ 1 ],
4309                               MajNHYD=[ "A8-MJ" ]
4310                               MinNHYD=[ "A8-MN" ]
4311                               TMJSTO=[ 40 ](cu-m)
4312 *%
4313 ADD HYD                NHYDsum=[ "MH105" ], NHYDs to
4314                               add=[ "104-105" +"B5-MN" +"A8-MN" +"TODD_MN3j" ]
4315 *%
4316 SAVE HYD               NHYD=[ "MH105" ],    # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4317                               HYD_COMMENT=[ "Total Flows at MH105" ]

```

```

4314 *%
4315 DIVERT HYD      NHYDin=[ "A8-MJ" ] NIDout=[ 2 ]max five,
4316 outflow hydrographs (NHYDs)=[ "A8-MJ-JR" "A8-MJ-B6" ]
4317 flow distribution table: (modify as necessary)
4318 Note: all flows are in (cms)
4319     QIDi + QIDii = QTOTAL
4320     [ 0 + 0 = 0 ] ]
4321     [ 50 + 50 = 100 ] end
4322 *%
4323 DIVERT HYD      NHYDin=[ "MH105" ] NIDout=[ 2 ]max five,
4324 outflow hydrographs (NHYDs)=[ "MH105-JR" "MH105-B6" ]
4325 flow distribution table: (modify as necessary)
4326 Note: all flows are in (cms)
4327     QIDi + QIDii = QTOTAL
4328     [ 0 + 0 = 0 ]
4329     [ 0 + 3.0 = 3.0 ]
4330     [ 96.9+ 3.1 = 100 ] end
4331 *%
4332 CONTINUOUS STANDHYD NHYD=[ "B7" ], DT=[ 1 ]min, AREA=[ 7.19 ](ha),
4333 XIMP=[ 0.41 ], TIMP=[ 0.54 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4334 SCS curve number CN=[ 75 ],
4335 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4336 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4337 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4338 LGI=[ 211 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4339 Continuous simulation parameters:
4340 IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
4341 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4342 InterEventTime=[ 18 ](hrs), END=-1
4343 *%
4344 ADD HYD          NHYDsum=[ "B7-B4MJ" ], NHYDs to add=[ "B4-MJ" "+" B7" ]
4345 *%
4346 COMPUTE DUALHYD NHYDin=[ "B7-B4MJ" ], CINLET=[ 0.629 ](cms), NINLET=[ 1 ],
4347 MajNHYD=[ "B7R-MJ" ]
4348 MinNHYD=[ "B7R-MN" ]
4349 TMJSTO=[ 311 ](cu-m)
4350 *%
4351 ROUTE PIPE       PTTYPE=[ 1 ]circ, NHYDout=[ "360-106A" ], RNUMBER=[ 1.0 ], PDIAM=[ 1050 ](mm),
4352 PLNGTH=[ 167 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m),
4353 NHYDin=[ "B7R-MN" ], RDT=[ 1 ]
4354 *%
4355 * -JFSA 2021-01-19 change B6 to be developed as per geoottawa website and apply the
4356 parameters of A7, the nearest sub-catchment to B6, LGI is calculated based on B6 area
4357 CONTINUOUS STANDHYD NHYD=[ "B6" ], DT=[ 1 ]min, AREA=[ 3.29 ](ha),
4358 XIMP=[ 0.41 ], TIMP=[ 0.54 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4359 SCS curve number CN=[ 75 ],
4360 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4361 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4362 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4363 LGI=[ 148.099 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4364 Continuous simulation parameters:
4365 IaRECper=[ 4 ](hrs), IaRECimp=[ 4 ](hrs),
4366 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4367 InterEventTime=[ 18 ](hrs), END=-1
4368 *%
4369 * -JFSA 2021-01-25 add B1 DUALHYD as per Corrigan Report, IBI Group, 2008
4370 COMPUTE DUALHYD NHYDin=[ "B6" ], CINLET=[ 0.064 ](cms), NINLET=[ 1 ],
4371 MajNHYD=[ "B6-MJ" ]
4372 MinNHYD=[ "B6-MN" ]
4373 TMJSTO=[ 5484 ](cu-m)
4374 *%
4375 *CONTINUOUS NASHYD NHYD=[ "B6" ], DT=[ 1 ]min, AREA=[ 3.29 ](ha),
4376 * DWF=[ 0 ](cms), CN/C=[ 75 ], IA=[ 2.5 ](mm),
4377 * N=[ 3.0 ], TP=[ 0.36 ]hrs,
```

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4376 *
4377 *
4378 *
4379 *
4380 *
4381 *
4382 *
4383 *
4384 *-----|-----|
4385 *% -EX-LAND is external land. It is a part of JOCKVA sub-catchment as per Corrigan
Report, IBI Group, 2008
4386 CONTINUOUS STANDHYD NHYD=[ "EX-LAND" ], DT=[1]min, AREA=[32.5](ha),
4387 XIMP=[0.50], TIMP=[0.50], DWF=[0](cms), LOSS=[2],
4388 SCS curve number CN=[74],
4389 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4390 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4391 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4392 LGI=[465.475](m), MNI=[0.013], SCI=[0](min),
4393 Continuous simulation parameters:
4394 IaRECper=[4](hrs), IaRECImp=[4](hrs),
4395 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4396 InterEventTime=[18](hrs), END=-1
4397 *%-----|-----|
4398 COMPUTE DUALHYD NHYDin=[ "EX-LAND" ], CINLET=[2.275](cms), NINLET=[1],
4399 MajNHYD=[ "EX-LAND-MJ" ]
4400 MinNHYD=[ "EX-LAND-MN" ]
4401 TMJSTO=[1365](cu-m)
4402 *%-----|-----|
4403 ADD HYD NHYDsum=[ "B6-B7ExMJ" ], NHYDs to
add=[ "B7R-MJ "+ "EX-LAND-MJ "+ "B5-MJ "+ "B6-MJ "+ "B6-MN "+ "A8-MJ-B6" ]
4404 *%-----|-----|
4405 COMPUTE DUALHYD NHYDin=[ "B6-B7ExMJ" ], CINLET=[0.064](cms), NINLET=[1],
4406 MajNHYD=[ "B6R-MJ" ]
4407 MinNHYD=[ "B6R-MN" ]
4408 TMJSTO=[5484](cu-m)
4409 *%-----|-----|
4410 ROUTE PIPE PTYPE=[1]circ, NHYDout=[ "105-106A" ], RNUMBER=[1.0], PDIAM=[1800](mm),
4411 PLNGTH=[208](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
4412 NHYDin=[ "MH105-B6" ], RDT=[1]
4413 *%-----|-----|
4414 ADD HYD NHYDsum=[ "MH106A" ], NHYDs to
add=[ "360-106A "+ "105-106A "+ "B6R-MN "+ "B6R-MJ" ]
4415 *%-----|-----|
4416 SAVE HYD NHYD=[ "MH106A" ], # OF PCYCLES=[-1], ICASEsh=[1]
4417 HYD_COMMENT=[ "Total Flows at MH106A" ]
4418 *% -JFSA 2021-01-12 THE MANHOLE MH106 is called MH117/106 in Corrigan Report, IBI
Group, July 2008
4419 *%
4420 ROUTE PIPE PTYPE=[1]circ, NHYDout=[ "106A-106" ], RNUMBER=[1.0], PDIAM=[1800](mm),
4421 PLNGTH=[190](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
4422 NHYDin=[ "MH106A" ], RDT=[1]
4423 *%-----|-----|
4424 CONTINUOUS STANDHYD NHYD=[ "A9" ], DT=[1]min, AREA=[2.44](ha),
4425 XIMP=[0.71], TIMP=[0.71], DWF=[0](cms), LOSS=[2],
4426 SCS curve number CN=[75],
4427 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4428 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4429 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4430 LGI=[262](m), MNI=[0.013], SCI=[0](min),
4431 Continuous simulation parameters:
4432 IaRECper=[4](hrs), IaRECImp=[4](hrs),
4433 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4434 InterEventTime=[18](hrs), END=-1
4435 *%-----|-----|
COMPUTE DUALHYD NHYDin=[ "A9" ], CINLET=[0.547](cms), NINLET=[1],

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4436
4437
4438
4439 *%-----|-----|
4440 ADD HYD NHYDsum=[ "MH106" ], NHYDs to add=[ "106A-106 "+"A9-MN" ]
4441 *%-----|-----|
4442 SAVE HYD NHYD=[ "MH106" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4443 HYD_COMMENT=[ "Total Flows at MH106" ]
4444 *%-----|-----|
4445 *% -JFSA 2021-01-12 THE MANHOLE MH107 is called MH118/107 in Corrigan Report, IBI
4446 Group, July 2008
4447 *%
4448 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout=[ "106-107" ], RNUMBER=[ 1.0 ], PDIAM=[ 1800 ](mm),
4449 PLNGTH=[ 122.5 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.001 ](m/m),
4450 NHYDin=[ "MH106" ], RDT=[ 1 ]
4451 *%-----|-----|
4452 CONTINUOUS STANDHYD NHYD=[ "A10" ], DT=[ 1 ]min, AREA=[ 4.14 ](ha),
4453 XIMP=[ 0.35 ], TIMP=[ 0.47 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4454 SCS curve number CN=[ 75 ],
4455 Previous surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4456 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4457 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4458 LGI=[ 183 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4459 Continuous simulation parameters:
4460 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4461 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4462 InterEventTime=[ 18 ](hrs), END=-1
4463 *%-----|-----|
4464 COMPUTE DUALHYD NHYDin=[ "A10" ], CINLET=[ 0.310 ](cms), NINLET=[ 1 ],
4465 MajNHYD=[ "A10-MJ" ]
4466 MinNHYD=[ "A10-MN" ]
4467 TMJSTO=[ 228 ](cu-m)
4468 *%-----|-----|
4469 CONTINUOUS STANDHYD NHYD=[ "A11" ], DT=[ 1 ]min, AREA=[ 10.61 ](ha),
4470 XIMP=[ 0.53 ], TIMP=[ 0.62 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4471 SCS curve number CN=[ 75 ],
4472 Previous surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4473 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4474 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4475 LGI=[ 379 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4476 Continuous simulation parameters:
4477 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4478 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4479 InterEventTime=[ 18 ](hrs), END=-1
4480 *%-----|-----|
4481 COMPUTE DUALHYD NHYDin=[ "A11" ], CINLET=[ 0.993 ](cms), NINLET=[ 1 ],
4482 MajNHYD=[ "A11-MJ" ]
4483 MinNHYD=[ "A11-MN" ]
4484 TMJSTO=[ 556 ](cu-m)
4485 *%-----|-----|
4486 ADD HYD NHYDsum=[ "MH107" ], NHYDs to add=[ "106-107 "+"A10-MN" "+"A11-MN" ]
4487 *%-----|-----|
4488 SAVE HYD NHYD=[ "MH107" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4489 HYD_COMMENT=[ "Total Flows at MH107" ]
4490 *%-----|-----|
4491 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout=[ "107-119" ], RNUMBER=[ 1.0 ], PDIAM=[ 1800 ](mm),
4492 PLNGTH=[ 114 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0012 ](m/m),
4493 NHYDin=[ "MH107" ], RDT=[ 1 ]
4494 *%-----|-----|
4495 *% -JFSA 2021-01-12 THE MANHOLE MH108 is called MH120/108 in Corrigan Report, IBI
4496 Group, July 2008
4497 *%
4498 ROUTE PIPE PTYPE=[ 1 ]circ, NHYDout=[ "119-108" ], RNUMBER=[ 1.0 ], PDIAM=[ 1800 ](mm),
4499 PLNGTH=[ 65.8 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0012 ](m/m),
4500 NHYDin=[ "107-119" ], RDT=[ 1 ]
4501 *%-----|-----|

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4497 CONTINUOUS STANDHYD NHYD=[ "A12" ], DT=[1]min, AREA=[12.29](ha),
4498 XIMP=[ 0.41 ], TIMP=[ 0.54 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4499 SCS curve number CN=[ 75 ],
4500 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4501 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4502 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4503 LGI=[ 183 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4504 Continuous simulation parameters:
4505 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4506 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4507 InterEventTime=[ 18 ](hrs), END=-1
4508 *%
4509 COMPUTE DUALHYD NHYDin=[ "A12" ], CINLET=[ 1.029 ](cms), NINLET=[ 1 ],
4510 MajNHYD=[ "A12-MJ" ]
4511 MinNHYD=[ "A12-MN" ]
4512 TMJSTO=[ 672 ](cu-m)
4513 *%
4514 CONTINUOUS STANDHYD NHYD=[ "A13" ], DT=[1]min, AREA=[2.59](ha),
4515 XIMP=[ 0.71 ], TIMP=[ 0.71 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4516 SCS curve number CN=[ 75 ],
4517 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4518 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4519 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4520 LGI=[ 379 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4521 Continuous simulation parameters:
4522 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4523 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4524 InterEventTime=[ 18 ](hrs), END=-1
4525 *%
4526 COMPUTE DUALHYD NHYDin=[ "A13" ], CINLET=[ 0.571 ](cms), NINLET=[ 1 ],
4527 MajNHYD=[ "A13-MJ" ]
4528 MinNHYD=[ "A13-MN" ]
4529 TMJSTO=[ 0 ](cu-m)
4530 *%
4531 * -JFSA 2021-01-22 add the Corrigan pond area ("Pond-Block")
4532 CONTINUOUS STANDHYD NHYD=[ "Pond-Block" ], DT=[1]min, AREA=[2.94](ha),
4533 XIMP=[ 0.415 ], TIMP=[ 0.415 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4534 SCS curve number CN=[ 75 ],
4535 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4536 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4537 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4538 LGI=[ 183 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4539 Continuous simulation parameters:
4540 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4541 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4542 InterEventTime=[ 18 ](hrs), END=-1
4543 *%
4544 ADD HYD NHYDsum=[ "MH108" ], NHYDs to add=[ "119-108"+ "A13-MN"+ "A12-MN" ]
4545 *%
4546 SAVE HYD NHYD=[ "MH108" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4547 HYD_COMMENT=[ "Total Flows at MH108" ]
4548 *%
4549 ROUTE PIPE PTTYPE=[ 1 ]circ, NHYDout=[ "108-116" ], RNUMBER=[ 1.0 ], PDIAM=[ 1800 ](mm),
4550 PLNGTH=[ 76.6 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0013 ](m/m),
4551 NHYDin=[ "MH108" ], RDT=[ 1 ]
4552 *%
4553 ROUTE PIPE PTTYPE=[ 1 ]circ, NHYDout=[ "116-corrig" ], RNUMBER=[ 1.0 ],
4554 PDIAM=[ 1800 ](mm),
4555 PLNGTH=[ 79.5 ](m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0013 ](m/m),
4556 NHYDin=[ "108-116" ], RDT=[ 1 ]
4557 *%
4558 ADD HYD NHYDsum=[ "Corrigan" ], NHYDs to add=[ "116-corrig"+ "Pond-Block" ]
4559 *%
4560 SAVE HYD NHYD=[ "Corrigan" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4561 HYD_COMMENT=[ "Total Flows at Corrigan Pond" ]
4562 *%

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4560 ROUTE RESERVOIR      NHYDout=[ "Co-P" ] ,   NHYDin=[ "Corrigan" ] ,
4561                                     RDT=[1](min),
4562                                         TABLE of ( OUTFLOW-STORAGE ) values
4563                                         (cms) - (ha-m)
4564                                         [ 0.0 , 0.0 ]
4565                                         [ 0.015 , 0.04118 ]
4566                                         [ 0.030 , 0.08297 ]
4567                                         [ 0.045 , 0.12537 ]
4568                                         [ 0.060 , 0.16837 ]
4569                                         [ 0.075 , 0.21199 ]
4570                                         [ 0.090 , 0.27545 ]
4571                                         [ 0.105 , 0.34650 ]
4572                                         [ 0.120 , 0.42049 ]
4573                                         [ 0.135 , 0.50188 ]
4574                                         [ 0.186 , 0.60307 ]
4575                                         [ 2.110 , 0.79083 ]
4576                                         [ 5.874 , 1.00271 ]
4577                                         [ 11.395 , 1.29643 ]
4578                                         [ 18.770 , 1.62054 ]
4579                                         [ 28.143 , 1.97516 ]
4580                                         [ -1 , -1 ] (max twenty pts)
4581 NHYDovf=[ "Co-P-OVF" ]
4582 *%----- | -----| -----
4583 ADD HYD          NHYDsum=[ "corrige" ], NHYDs to
add=[ "Co-P-OVF" + "Co-P" + "N_TO" + "MH105-JR" + "A8-MJ-JR" + "A9-MJ" + "A10-MJ" + "A11-MJ" + "A12-MJ" + "A13-MJ" ]
4584 *%----- | -----| -----
4585 SAVE HYD          NHYD=[ "corrige" ], # OF PCYCLES=[-1], ICASEsh=[1]
4586             HYD_COMMENT=[ "Total Flows at Corrigan Pond" ]
4587 *%----- | -----| -----
4588 *#*****#
4589 *#    Corrigan Pond 1
4590 *# - Rating curve obtained from Barrhaven South MSS modeling
4591 *# - Tributary Drainage Area to MSS Pond 1 = 145 ha
4592 *#*****#
4593 ROUTE RESERVOIR      NHYDout=[ "MS_P1" ] ,   NHYDin=[ "CORRIG" ] ,
4594 * RDT=[1](min),
4595 *                                         TABLE of ( OUTFLOW-STORAGE ) values
4596 *                                         (cms) - (ha-m)
4597 *                                         [ 0.0 , 0.0 ]
4598 *                                         [ 0.06 , 0.58 ]
4599 *                                         [ -1 , -1 ] (max twenty pts)
4600 * NHYDovf=[ "P1-OVF" ]
4601 *%----- | -----| -----
4602 *ADD HYD          NHYDsum=[ "SN_CO" ], NHYDs to add=[ "N_TO" + "P1-OVF" + "MS_P1" ]
4603 *%----- | -----| -----
4604 *SAVE HYD          NHYD=[ "SN_CO" ], # OF PCYCLES=[-1], ICASEsh=[1]
4605 *             HYD_COMMENT=[ "Total Flows at Corrigan Drain" ]
4606 *%----- | -----| -----
4607 *#
4608 *# Hydrograph from Corrigan Drain routed to Jockvale Road
4609 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
4610 *#
4611 ROUTE CHANNEL      NHYDout=[ "N_MI" ] , NHYDin=[ "corrige" ] ,
4612 RDT=[1](min),
4613 CHLGTH=[ 580 ](m), CHSLOPE=[ 0.4448 ](%),
4614                                     FPSLOPE=[ 0.4448 ](%),
4615 SECNUM=[ 1.0 ] , NSEG=[ 3 ]
4616 ( SEGRUGH, SEGDIST (m) )=
4617     [ 0.075,-17.72
4618     -0.045,17.72
4619     0.075,80.62 ] NSEG times
4620 ( DISTANCE (m), ELEVATION (m) )=
4621     [-83.32, 90.00]
4622     [-81.36, 89.50]
4623     [-79.12, 89.00]

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4624      [-76.13, 88.50]
4625      [-20.46, 88.00]
4626      [-19.36, 87.50]
4627      [-18.51, 87.00]
4628      [-17.72, 86.50]
4629      [-11.95, 85.24]
4630      [-0.11, 85.12]
4631      [11.49, 85.20]
4632      [17.72, 86.50]
4633      [19.74, 87.00]
4634      [21.22, 87.50]
4635      [22.68, 88.00]
4636      [24.28, 88.50]
4637      [26.79, 89.00]
4638      [71.98, 90.00]
4639      [80.62, 90.50]
4640 *%-----|-----|
4641 *#*****
4642 *#      Catchment MILLS
4643 *#      - To SWM Facility north of the Jock
4644 *#      - Primarily residential development
4645 *#*****
4646 CONTINUOUS STANDHYD NHYD=[ "MILLS" ], DT=[1]min, AREA=[175.99](ha),
4647 XIMP=[ 0.38 ], TIMP=[ 0.38 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4648 SCS curve number CN=[ 74 ],
4649 Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%),
4650 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4651 Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%),
4652 LGI=[ 1118.123 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4653 Continuous simulation parameters:
4654 IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4655 SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4656 InterEventTime=[ 18 ](hrs), END=-1
4657 *%-----|-----|
4658 *#*****
4659 *#      Chapman Mills SWM Pond
4660 *#      - Rating curve obtained from CCL hydraulic modeling
4661 *#*****
4662 ROUTE RESERVOIR      NHYDout=[ "MILL_P" ], NHYDin=[ "MILLS" ],
4663 RDT=[ 1 ](min),
4664          TABLE of ( OUTFLOW-STORAGE ) values
4665          (cms) - (ha-m)
4666          [ 0.0 , 0.0 ]
4667          [ 0.01 , 0.01 ]
4668          [ 0.05 , 0.06 ]
4669          [ 0.09 , 0.11 ]
4670          [ 0.13 , 0.15 ]
4671          [ 0.18 , 0.19 ]
4672          [ 0.28 , 0.28 ]
4673          [ 0.37 , 0.34 ]
4674          [ 0.45 , 0.40 ]
4675          [ 0.51 , 0.44 ]
4676          [ 0.56 , 0.47 ]
4677          [ 0.64 , 0.52 ]
4678          [ 0.76 , 0.59 ]
4679          [ 0.86 , 0.65 ]
4680          [ 1.09 , 0.78 ]
4681          [ 1.44 , 0.96 ]
4682          [ 3.18 , 1.84 ]
4683          [ 4.05 , 2.31 ]
4684          [ -1 , -1 ] (max twenty pts)
4685          NHYDovf=[ "MIL-OV" ]
4686 *%-----|-----|
4687 ADD HYD      NHYDs[ "SN_MI" ], NHYDs to add=[ "N_MI"+ "MIL-OV" + "MILL_P" ]
4688 *%-----|-----|
4689 SAVE HYD      NHYD=[ "SN_MI" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]

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```

4690                                HYD_COMMENT=[ "Total Flows at Jockvale Road" ]
4691 *%-----|-----|
4692 *#
4693 *# Hydrograph from Jockvale Road routed to Heart's Desire
4694 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 689
4695 *#
4696 ROUTE CHANNEL      NHYDout=[ "N_DE" ] , NHYDin=[ "SN_MI" ] ,
4697          RDT=[1](min),
4698          CHLGTH=[1962](m),   CHSLOPE=[ 0.2227 ](%) ,
4699          FPSLOPE=[ 0.2227 ](%) ,
4700          SECNUM=[ 1.0 ],           NSEG=[ 3 ]
4701          ( SEGROUGH, SEGDIST (m))=
4702          [ 0.075,-17.56
4703          -0.045,18.27
4704          0.075,32.51 ] NSEG times
4705          ( DISTANCE (m), ELEVATION (m))=
4706          [-54.07, 85.00]
4707          [-39.43, 84.50]
4708          [-28.30, 84.00]
4709          [-24.12, 83.50]
4710          [-22.30, 83.00]
4711          [-20.55, 82.50]
4712          [-17.56, 82.00]
4713          [-12.63, 81.22]
4714          [-0.11, 80.75]
4715          [11.55, 81.22]
4716          [18.27, 82.00]
4717          [19.82, 82.50]
4718          [22.48, 83.00]
4719          [27.90, 83.50]
4720          [29.31, 84.00]
4721          [30.81, 84.50]
4722          [32.51, 85.00]
4723 *%-----|-----|
4724 *#*****
4725 *#      Catchment DESIRE
4726 *#      - To Jock River (north of the Jock)
4727 *#      - Rural-estate subdivision (Heart's Desire Community)
4728 *#*****
4729 CONTINUOUS STANDHYD NHYD=[ "DESIRE" ], DT=[1]min, AREA=[ 23.78 ](ha),
4730          XIMP=[ 0.25 ], TIMP=[ 0.25 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4731          SCS curve number CN=[ 77 ],
4732          Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%) ,
4733          LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4734          Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%) ,
4735          LGI=[ 400 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),
4736          Continuous simulation parameters:
4737          IaRECper=[ 4 ](hrs), IaRECImp=[ 4 ](hrs),
4738          SMIN=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
4739          InterEventTime=[ 18 ](hrs), END=-1
4740 *%-----|-----|
4741 *#*****
4742 *#      Catchment JOCKVA
4743 *#      - To Jockvale SWM Facility
4744 *#      - Residential development & golf course
4745 *#      - JFSA 2021-01-11 update JOCKVA after updating CORRIG as per IBI GROUP, July 2008.
4746 *#      JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two
4747 areas JOCKVA and EX-LAND 32.5 ha as per IBI GROUP, July 2008.
4748 *#*****
4749 CONTINUOUS STANDHYD NHYD=[ "JOCKVA" ], DT=[1]min, AREA=[ 225.13 ](ha),
4750          XIMP=[ 0.50 ], TIMP=[ 0.50 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
4751          SCS curve number CN=[ 74 ],
4752          Pervious surfaces: IAper=[ 4.67 ](mm), SLPP=[ 1 ](%) ,
4753          LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](min),
4754          Impervious surfaces: IAimp=[ 1.57 ](mm), SLPI=[ 1 ](%) ,
4755          LGI=[ 1310.55 ](m), MNI=[ 0.013 ], SCI=[ 0 ](min),

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4755 Continuous simulation parameters:
4756 IaRECper=[4](hrs), IaRECImp=[4](hrs),
4757 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4758 InterEventTime=[18](hrs), END=-1
4759 *%
4760 ADD HYD NHYDsum=[ "JOCKVA-TO" ], NHYDs to
4761 add=[ "EX-LAND-MN" +"JOCKVA" +"B2-MJ" +"B3-MJ" ]
4762 *%
4763 SAVE HYD NHYD=[ "JOCKVA-TO" ], # OF PCYCLES=[-1], ICASEsh=[1]
4764 HYD_COMMENT=[ "Total Flows at KB first pond" ]
4765 *%
4766 *#***** Jockvale SWM Facility
4767 *# - Rating curve obtained from Jockvale Servicing Study (CCL 1999)
4768 *#*****
4769 ROUTE RESERVOIR NHYDout=[ "JOCK_P" ], NHYDin=[ "JOCKVA-TO" ],
4770 RDT=[1](min),
4771 TABLE of ( OUTFLOW-STORAGE ) values
4772 (cms) - (ha-m)
4773 [ 0.0 , 0.0 ]
4774 [ 0.27 , 0.03 ]
4775 [ 0.28 , 0.55 ]
4776 [ 0.29 , 1.14 ]
4777 [ 0.30 , 1.80 ]
4778 [ 0.31 , 2.32 ]
4779 [ 1.12 , 2.87 ]
4780 [ 2.92 , 3.45 ]
4781 [ 4.64 , 4.07 ]
4782 [ 6.69 , 4.72 ]
4783 [ 9.02 , 5.39 ]
4784 [ 11.62 , 6.10 ]
4785 [ 14.42 , 6.85 ]
4786 [ 17.45 , 7.62 ]
4787 [ 20.69 , 8.44 ]
4788 [ 24.08 , 9.28 ]
4789 [ 27.68 , 10.17 ]
4790 [ -1 , -1 ] (max twenty pts)
4791 NHYDovf=[ "JO-OVF" ]
4792 *%
4793 ADD HYD NHYDsum=[ "SN_DE" ], NHYDs to add=[ "N_DE" +"DESIRE" +"JO-OVF" +"JOCK_P" ]
4794 *%
4795 SAVE HYD NHYD=[ "SN_DE" ], # OF PCYCLES=[-1], ICASEsh=[1]
4796 HYD_COMMENT=[ "Total Flows at Heart's Desire" ]
4797 *%
4798 *#
4799 *# Hydrograph from Heart's Desire routed to Rideau River
4800 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 0
4801 *#
4802 ROUTE CHANNEL NHYDout=[ "N1" ] , NHYDin=[ "SN_DE" ] ,
4803 RDT=[1](min),
4804 CHLGTH=[563](m), CHSLOPE=[0.9668](%),
4805 FPSLOPE=[0.9668](%),
4806 SECNUM=[1.0], NSEG=[3]
4807 ( SEGROUGH, SEGDIST (m))=
4808 [0.075,-30.20
4809 -0.045,30.20
4810 0.075,48.48] NSEG times
4811 ( DISTANCE (m), ELEVATION (m))=
4812 [-98.46, 81.50]
4813 [-92.24, 81.00]
4814 [-86.88, 80.50]
4815 [-81.54, 80.00]
4816 [-74.36, 79.50]
4817 [-63.54, 79.00]
4818 [-39.23, 78.50]
4819 [-34.51, 78.00]

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4820 [-33.01, 77.50]
4821 [-30.20, 77.00]
4822 [-13.42, 76.18]
4823 [-1.14, 76.09]
4824 [17.06, 76.18]
4825 [30.20, 77.00]
4826 [32.95, 77.50]
4827 [34.06, 78.00]
4828 [35.11, 78.50]
4829 [36.32, 79.00]
4830 [37.74, 79.50]
4831 [48.48, 81.50]
4832 *%-----|-----|
4833 *#*****|-----|
4834 *#      Catchment S-2
4835 *#      - To Jock River (north and south)
4836 *#      - Undeveloped floodplain and river
4837 *#*****|-----|
4838 CONTINUOUS NASHYD    NHYD=[ "S-2" ], DT=[1]min, AREA=[102.94](ha),
4839           DWF=[0](cms), CN/C=[72], IA=[4.67](mm),
4840           N=[3], TP=[0.40]hrs,
4841           Continuous simulation parameters:
4842           IaRECper=[4](hrs),
4843           SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4844           InterEventTime=[12](hrs)
4845           Baseflow simulation parameters:
4846           BaseFlowOption=[1],
4847           InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4848           VHydCond=[0.055](mm/hr), END=-1
4849 *%-----|-----|
4850 ADD HYD          NHYDsum=[ "SN_N1" ], NHYDs to add=[ "N1 "+"S-2" ]
4851 *%-----|-----|
4852 SAVE HYD          NHYD=[ "SN_N1" ], # OF PCYCLES=[-1], ICASEsh=[1]
4853           HYD_COMMENT=[ "Total Flows at Rideau River" ]
4854 *%-----|-----|
4855 *#####|-----|
4856 *% 5 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4857 START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[5]
4858           [ "C24SC005.stm" ] <--storm filename, one per line for NSTORM time
4859 *%-----|-----|
4860 *% 10 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4861 START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[10]
4862           [ "C24SC010.stm" ] <--storm filename, one per line for NSTORM time
4863 *%-----|-----|
4864 *% 25 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4865 START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[25]
4866           [ "C24SC025.stm" ] <--storm filename, one per line for NSTORM time
4867 *%-----|-----|
4868 *% 50 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4869 START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[50]
4870           [ "C24SC050.stm" ] <--storm filename, one per line for NSTORM time
4871 *%-----|-----|
4872 *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4873 START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4874           [ "100YC3H.STM" ] <--storm filename, one per line for NSTORM time
4875 *%-----|-----|
4876 *% 100 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4877 START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4878           [ "C24SC100.stm" ] <--storm filename, one per line for NSTORM time
4879 *%-----|-----|
4880 *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4881 START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4882           [ "C24SC100.stm" ] <--storm filename, one per line for NSTORM time
4883 START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[101]
4884           [ "A24SC100.stm" ] <--storm filename, one per line for NSTORM time
4885 START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[102]

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[ "A24SC100\_60.stm" ] <--storm filename, one per line for NSTORM time

4886 \*%

4887 **FINISH**

4888

00001> \*\*\*\*  
00002> SSSSS W W M M H H Y Y M M 000 222 000 11 5555 \*\*\*\*\*  
00004> S W W N M M H H Y Y M M 0 0 2 0 0 11 5 Ver: 6.600  
00005> SSSSS W W M M H H Y Y M M 000 222 0 0 11 555 FEB 2015  
00007> SSSSS W W M M H H Y M M 000 222 0 0 11 5 \* 000  
00008> Stormwater Management Hydrologic Model 222 000 11 455 \*\*\*\*\*  
00010>  
00012> \*\*\*\*\* SWMMHYD Version 5.600 \*\*\*  
00013> \*\*\*\*\* A single event and continuous hydrologic simulation model  
00014> based on the SWMM model and its successors  
00015> CTHNHYD-83 and CTHNHYD-89.  
00016> \*\*\*\*\*  
00017> \*\*\*\*\* Distributed by: JFSA Inc.  
00018> Ottawa, Ontario: (613) 836-3884  
00019> Gatineau, Quebec: (819) 243-6858  
00020> Email: info@jfainc.ca  
00021> \*\*\*\*\*  
00022>  
00024> \*\*\*\*\* Licensed user: JFSAInc.  
00025> Ottawa SERIAL# 2549237 \*\*\*\*\*  
00027>  
00028> \*\*\*\*\* PROGRAM ARRAY DIMENSIONS \*\*\*\*\*  
00029> \*\*\*\*\* Maximum value for ID numbers : 11 \*\*\*\*\*  
00030> \*\*\*\*\* Max. number of rainfall points: 105408 \*\*\*\*\*  
00031> \*\*\*\*\* Max. number of nodes: 105408 \*\*\*\*\*  
00032> \*\*\*\*\*  
00033> \*\*\*\*\* S U M M A R Y O U T P U T \*\*\*\*\*  
00034>  
00035> \*\*\*\*\* RUN DATE: 2021-03-04 TIME: 11:57:49 RUN COUNT: 002084 \*\*\*\*\*  
00036> \*\*\*\*\*  
00037> \*\*\*\*\* Input file: T:\R\RN\1474-16\Design\20201026\QuantityControlAnalysis\SWMMHYD\SMR-Model\updated\SMR\_1.SMR \*\*\*\*\*  
00038> \*\*\*\*\* Output file: T:\R\RN\1474-16\Design\20201026\QuantityControlAnalysis\SWMMHYD\SMR-Model\updated\SMR\_1.SMR\_Fr.DS.out \*\*\*\*\*  
00039> \*\*\*\*\* Summary file: T:\R\RN\1474-16\Design\20201026\QuantityControlAnalysis\SWMMHYD\SMR-Model\updated\SMR\_1.SMR\_Fr.DS.sum \*\*\*\*\*  
00040> \*\*\*\*\* User comments:  
00041> \* 1:  
00042> \* 2:  
00043> \* 3:  
00044>  
00051>  
00053> # SWMMHYD Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE  
00054> #  
00055> # Project Name: [Rock River] Project Number: [1474-16]  
00056> # Date : 04-03-2021  
00057> # Modeler : [JFSAinc]  
00058> # Company : [JFSAinc]  
00059> # License #: [2549237]  
00060>  
00062> # CALIBRATION OF SUMMER MODEL PARAMETERS  
00063> # USING CONTINUOUS SIMULATIONS  
00064> # Rainfall data from JFSA rain gauge installed at site + other gauges by the City  
00065> # Use data collected from May 1st to July 14, 2003  
00066> # 2020-11-30 change TMSTO in COMPUTE DUALYD (TMSTO = 0.1 instead of 0.0001)  
00067> # 2020-12-01 change W\_CLAR\_BXAP KIMP to 0.55, SLP1=[0.5%] (imperious slope), and LGI up to 700m  
00068> # 2021-02-19 Change the slope for ROUTE CHANNEL Station 2442 (NHYDout["N\_TO"], NHYDin["SN\_TO"]) from 0.033 % (as per S<sup>2</sup>) to 0.031 % (as per St)  
00069> # 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHYDout["N\_MC"], NHYDin["SN\_CK"]) from 0.01 % (as per St)  
00070> # 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHYDout["N\_MC"], NHYDin["SN\_CK"]) from 0.01 % (as per St)  
00071> #  
00072> \*\* END OF RUN : 1  
00073>  
00074> #  
00075> #  
00076> #  
00077> #  
00078> #  
00079> #  
00080> RUNS=COMMAND#  
00081> R0021:CO0001-----  
00082> [TZERO = .00 hrs on 0]  
00083> [METOUT = 2 (1=imperial, 2=metric output)]  
00084> [NRUN = 0000]  
00085> #  
00086> # SWMMHYD Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE  
00087> #  
00088> # Project Name: [Rock River] Project Number: [1474-16]  
00089> # Date : 04-03-2021  
00090> # Modeler : [JFSAinc]  
00091> # Company : [JFSAinc]  
00092> # License #: [2549237]  
00093> #  
00094> # CALIBRATION OF SUMMER MODEL PARAMETERS  
00095> # USING CONTINUOUS SIMULATIONS  
00096> # Rainfall data from JFSA rain gauge installed at site + other gauges by the City  
00097> # Use data collected from May 1st to July 14, 2003  
00098> # 2020-12-01 change TMSTO in COMPUTE DUALYD (TMSTO = 0.1 instead of 0.0001)  
00099> # 2020-12-01 correct pond curve values  
00100> # 2021-02-19 Change the slope for ROUTE CHANNEL Station 2442 (NHYDout["N\_TO"], NHYDin["SN\_TO"]) from 0.033 % (as per S<sup>2</sup>) to 0.031 % (as per St)  
00101> # 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHYDout["N\_MC"], NHYDin["SN\_CK"]) from 0.01 % (as per St)  
00102> # 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHYDout["N\_MC"], NHYDin["SN\_CK"]) from 0.01 % (as per St)  
00103> #  
00104> R0021:CO0002-----  
00105> #  
00106> # READING FROM STORM#  
00107> #  
00108> #  
00109> # Comment : Plus RCS de 24 heures 1/2 ans pour Ottawa CDA  
00110> # [SDT=10.00:SOUR= 24.00:PTOT= 45.51]  
00111> R0022:CO0003-----  
00112> # MODIFY STORM  
00113> # [RFAC= 1.00:RSHFTP= 960, min= 0, max= 0]  
00114> # [RSHFTP= 40.00:PTOT= 45.51]  
00115> R0021:CO0004-----  
00116> # DEFAULT VALUES  
00117> #  
00118> # File comment: [Based on various calibration exercises in Onta  
00119> # File comment: [Based on various calibration exercises in Onta  
00120> # Horton's infiltration equation parameters:  
00121> # [Fw= 76.20 mm/hr] [Fc=13.20 mm/hr] [DCav= 4.14 hr] [Fw=.00 mm]  
00122> # [PIS= 1.00 mm] [LGI= 0.00 mm] [RNDW= .250]  
00123> # [Aper= 4.67 mm] [LGI= 50.00 mm] [RNDW= .250]  
00124> # Parameters for IMPERVIOUS surfaces in STANDHYD:  
00125> # [LGI= 0.00 mm] [RNDW= 0.00 mm] [RNDW= 0.013]  
00126> # Parameters used in NASHYD:  
00127> # [LGI= 4.67 mm] [N= 3.00]  
00128> # Average precipitation and infiltration data in (mm)  
00129> #  
00130> JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC  
00131> .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00  
00132> # Average monthly Potential Evapotranspiration in (mm)  
00133> JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC  
00134> .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00  
00135> R0021:CO0005-----  
00136> # COMPUTE API  
00137> # [ApIn1= 5.00: ApRIn1= 8580: ApRIdy= 9988]  
00138> # [ApIn2= 80.12: ApAvg= 56.74: ApInin= 44.67]  
00139> #  
00140> # The Ts was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00141> # of 1.32  
00142> R0021:CO0006-----  
00143> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00144> # CONTINUOUS:NASHYD 1.0 01:SW\_1M 3680.00 6.204 No\_date 37:06 11.47 .252 .000  
00145> # [iAEc= 4.00: SMIN= 57.05: SMAX=380.32: SK= .010]  
00146> #  
00147> # The Ts was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00148> # of 1.32  
00149> R0021:CO0007-----  
00150> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00151> # CONTINUOUS:NASHYD 1.0 01:SW\_1M 971.00 2.187 No\_date 32:37 10.75 .236 .000  
00152> # [iAEc= 4.00: SMIN= 44.96: SMAX=430.01: SK= .010]  
00153> #  
00154> # [InterEventTime= 12.00]  
00155> #  
00156> # The Ts was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00157> # of 1.80  
00158> R0021:CO0008-----  
00159> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00160> # CONTINUOUS:NASHYD 1.0 01:SW\_1M 3074.00 3.218 No\_date 39:59 9.43 .207 .000  
00161> # [CIN= 55.00: N= 3.00: Tp=11.33]  
00162> #  
00163> R0021:CO0009-----  
00164> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00165> # CONTINUOUS:NASHYD 1.0 01:SW\_1M 1781.00 5.504 No\_date 32:45 13.94 .306 .000  
00166> # [CIN= 72.01: N= 3.00: Tp= 3.91]  
00167> # [iAEc= 4.00: SMIN= 39.75: SMAX=264.99: SK= .010]  
00168> #  
00169> R0021:CO0010-----  
00170> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00171> # CONTINUOUS:NASHYD 1.0 01:SW\_1M 1917.00 4.042 No\_date 34:34 11.98 .263 .000  
00172> # [iAEc= 4.00: SMIN= 12.42: SMAX=350.79: SK= .010]  
00173> #  
00174> # The Ts was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00175> # of 1.52  
00176> R0021:CO0011-----  
00177> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00178> # CONTINUOUS:NASHYD 1.0 01:NN\_CW 8666.00 11.228 No\_date 38:07 13.94 .306 .000  
00179> # [iAEc= 72.01: N= 3.00: Tp= 8.00]  
00180> #  
00181> # [InterEventTime= 12.00]  
00182> #  
00183> # The Ts was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00184> # of 1.52  
00185> R0021:CO0012-----  
00186> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00187> # CONTINUOUS:NASHYD 1.0 01:SW\_1M 8376.00 11.072 No\_date 39:59 11.98 .263 .000  
00188> # [CIN= 66.0: N= 3.00: Tp=11.66]  
00189> # [iAEc= 4.00: SMIN= 12.00: SMAX=350.79: SK= .010]  
00190> #  
00191> # [InterEventTime= 12.00]  
00192> #  
00193> # The Ts was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00194> # of 1.68  
00195> R0021:CO0014-----  
00196> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00197> # CONTINUOUS:NASHYD 1.0 01:SW\_1M 1132.00 4.434 No\_date 30:56 13.35 .293 .000  
00198> # [CIN= 70.0: N= 3.00: Tp= 2.51]  
00199> # [iAEc= 4.00: SMIN= 43.07: SMAX=287.10: SK= .010]  
00200> #  
00201> # [InterEventTime= 12.00]  
00202> #  
00203> # The Ts was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00204> # of 1.80  
00205> R0021:CO0015-----  
00206> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00207> # CONTINUOUS:NASHYD 1.0 01:NN\_CW 4464.00 5.504 No\_date 39:59 10.98 .241 .000  
00208> # [CIN= 66.0: N= 3.00: Tp= 1.91]  
00209> # [iAEc= 4.00: SMIN= 61.90: SMAX=412.66: SK= .010]  
00210> #  
00211> # [InterEventTime= 12.00]  
00212> #  
00213> # The Ts was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00214> # of 1.80  
00215> R0021:CO0016-----  
00216> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00217> # CONTINUOUS:NASHYD 1.0 01:SW\_8 131.00 .805 No\_date 28:57 11.22 .247 .000  
00218> # [CIN= 61.0: N= 3.00: Tp= 7.91]  
00219> # [iAEc= 4.00: SMIN= 52.62: SMAX=350.79: SK= .010]  
00220> #  
00221> # [InterEventTime= 12.00]  
00222> #  
00223> # The Ts was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00224> # of 1.65  
00225> R0021:CO0017-----  
00226> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00227> # CONTINUOUS:NASHYD 1.0 01:SW\_DR 384.00 6.242 No\_date 38:46 11.98 .263 .000  
00228> # [CIN= 66.0: N= 3.00: Tp= 8.42]  
00229> # [iAEc= 4.00: SMIN= 55.95: SMAX=346.99: SK= .010]  
00230> #  
00231> # [InterEventTime= 12.00]  
00232> #  
00233> # The Ts was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00234> # of 1.80  
00235> R0021:CO0018-----  
00236> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00237> # CONTINUOUS:NASHYD 1.0 01:SW\_7 319.00 4.651 No\_date 36:31 9.85 .217 .000  
00238> # [CIN= 61.0: N= 3.00: Tp= 6.65]  
00239> # [iAEc= 4.00: SMIN= 76.32: SMAX=508.81: SK= .010]  
00240> #  
00241> # [InterEventTime= 12.00]  
00242> #  
00243> # The Ts was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00244> # of 1.80  
00245> R0021:CO0019-----  
00246> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00247> # CONTINUOUS:NASHYD 1.0 01:NN\_CW 319.00 3.148 No\_date 35:23 13.94 .306 .000  
00248> # [CIN= 72.0: N= 3.00: Tp= 5.95]  
00249> # [iAEc= 4.00: SMIN= 25.21: SMAX=244.49: SK= .010]  
00250> #  
00251> # [InterEventTime= 12.00]  
00252> #  
00253> R0021:CO0021-----  
00254> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00255> # CONTINUOUS:NASHYD 1.0 01:SW\_7 224.00 2.597 No\_date 28:45 15.91 .350 .000  
00256> # [CIN= 77.0: N= 3.00: Tp= 7.51]  
00257> # [iAEc= 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]  
00258> #  
00259> # [InterEventTime= 12.00]  
00260> #  
00261> # The Ts was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00262> # of 1.67  
00263> R0021:CO0022-----  
00264> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00265> # CONTINUOUS:NASHYD 1.0 01:SW\_6 165.00 .413 No\_date 33:07 12.24 .269 .000  
00266> # [CIN= 72.0: N= 3.00: Tp= 7.91]  
00267> # [iAEc= 4.00: SMIN= 55.95: SMAX=336.97: SK= .010]  
00268> #  
00269> # [InterEventTime= 12.00]  
00270> #  
00271> # The Ts was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00272> # of 1.61  
00273> R0021:CO0023-----  
00274> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00275> # CONTINUOUS:NASHYD 1.0 01:SW\_5A1 4945.00 14.839 No\_date 33:25 14.57 .320 .000  
00276> # [CIN= 74.0: N= 3.00: Tp= 6.00]  
00277> # [iAEc= 4.00: SMIN= 36.67: SMAX=244.49: SK= .010]  
00278> #  
00279> # [InterEventTime= 12.00]  
00280> #  
00281> R0021:CO0024-----  
00282> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00283> # CONTINUOUS:NASHYD 1.0 01:SW\_5A2 3132.00 3.148 No\_date 35:23 13.94 .306 .000  
00284> # [CIN= 75.0: N= 3.00: Tp= 5.95]  
00285> # [iAEc= 4.00: SMIN= 25.21: SMAX=264.99: SK= .010]  
00286> #  
00287> # [InterEventTime= 12.00]  
00288> #  
00289> R0021:CO0025-----  
00290> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00291> # CONTINUOUS:NASHYD 1.0 01:SW\_5A2 224.00 5.740 No\_date 32:07 12.24 .269 .000  
00292> # [CIN= 77.0: N= 3.00: Tp= 7.51]  
00293> # [iAEc= 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]  
00294> #  
00295> R0021:CO0026-----  
00296> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00297> # ADD HYD 1.0 01:NN\_DR 1412.00 3.090 No\_date 38:04 15.22 .334 .000  
00298> # [CIN= 74.0: N= 3.00: Tp= 6.00]  
00299> # [iAEc= 4.00: SMIN= 36.67: SMAX=244.49: SK= .010]  
00300> #  
00301> # [InterEventTime= 12.00]  
00302> #  
00303> R0021:CO0027-----  
00304> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00305> # CONTINUOUS:NASHYD 1.0 01:NN\_DR 1021.00 5.747 No\_date 30:50 17.39 .382 .000  
00306> # [CIN= 74.0: N= 3.00: Tp= 6.00]  
00307> # [iAEc= 4.00: SMIN= 25.21: SMAX=168.09: SK= .010]  
00308> #  
00309> # Starting with the addition of Jock River Headwater and Subwatershed 13  
00310> #  
00311> R0021:CO0028-----  
00312> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00313> # ADD HYD 1.0 01:DR 3689.00 5.204 No\_date 37:06 11.47 n/a .000  
00314> # [CIN= 74.0: N= 3.00: Tp= 6.00]  
00315> # [iAEc= 4.00: SMIN= 25.21: SMAX=168.09: SK= .010]  
00316> #  
00317> # [InterEventTime= 12.00]  
00318> #  
00319> R0021:CO0029-----  
00320> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00321> # ADD 1.0 01:DR 1.0 01:SW\_1M 3747.00 5.218 No\_date 32:37 10.75 n/a .000  
00322> # [CIN= 74.0: N= 3.00: Tp= 6.00]  
00323> # [iAEc= 4.00: SMIN= 25.21: SMAX=175.50: SK= .010]  
00324> #  
00325> R0021:CO0030-----  
00326> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00327> # SUM 1.0 01:NN\_13A 5651.00 4.325 No\_date 31:57 10.57 n/a .000  
00328> #  
00329> # Insertion of a reservoir to simulate the effects of the Goodwood Marsh  
00330> #  
00331> R0021:CO0031-----  
00332> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00333> # ROUTE RESERVOIR --> 1.0 01:SW\_13A 7725.00 9.475 No\_date 39:59 10.57 n/a .000  
00334> # [CIN= 74.0: N= 3.00: Tp= 6.00]  
00335> # [iAEc= 4.00: SMIN= 25.21: SMAX=175.50: SK= .010]  
00336> #  
00337> R0021:CO0034-----  
00338> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00339> # ROUTE CHANNEL --> 1.0 02:DR 3651.00 7.215 No\_date 32:45 13.94 n/a .000  
00340> # [CIN= 74.0: N= 3.00: Tp= 6.00]  
00341> # [iAEc= 4.00: SMIN= 25.21: SMAX=175.50: SK= .010]  
00342> #  
00343> # frame\_B\_SK12 remark\_outflow from Node 13 to Node 12  
00344> # [CIN= 74.0: N= 3.00: Tp= 6.00]  
00345> # Use n=0.04 for summer conditions and n=0.025 for spring conditions  
00346> #  
00347> R0021:CO0035-----  
00348> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00349> # ROUTE CHANNEL --> 1.0 02:DR 3651.00 7.215 No\_date 55:07 10.57 n/a .000  
00350> # [CIN= 74.0: N= 3.00: Tp= 6.00]  
00351> # [iAEc= 4.00: SMIN= 25.21: SMAX=175.50: SK= .010]  
00352> #  
00353> R0021:CO0036-----  
00354> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00355> # ADD 1.0 01:NN\_13M 7255.00 2.605 No\_date 58:08 10.57 n/a .000  
00356> #  
00357> R0021:CO0037-----  
00358> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00359> # SAVE HYD 1.0 01:SW\_1M 7255.00 2.609 No\_date 58:09 10.57 n/a .000  
00360> #  
00361> # frame\_B\_SK12 remark\_outflow from Node 13 to Node 12  
00362> # [CIN= 74.0: N= 3.00: Tp= 6.00]  
00363> # Use n=0.04 for summer conditions and n=0.025 for spring conditions  
00364> #  
00365> R0021:CO0038-----  
00366> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00367> # SUM of hydrographs from Node 12 routed to Node 11 to Dummy section 248  
00368> # [CIN= 74.0: N= 3.00: Tp= 6.00]  
00369> # [iAEc= 4.00: SMIN= 25.21: SMAX=264.99: SK= .010]  
00370> #  
00371> # [InterEventTime= 12.00]  
00372> #  
00373> # The Ts was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00374> # of 1.52  
00375> R0021:CO0010-----  
00376> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00377> # CONTINUOUS:NASHYD 1.0 01:NN\_CW 1917.00 4.042 No\_date 34:34 11.98 .263 .000  
00378> # [CIN= 66.0: N= 3.00: Tp= 6.00]  
00379> # [iAEc= 4.00: SMIN= 12.42: SMAX=350.79: SK= .010]  
00380> #  
00381> # [InterEventTime= 12.00]  
00382> #  
00383> # The Ts was modified according to a Peak Reduction factor (MTO-Chart B2-4)  
00384> # of 1.52  
00385> R0021:CO0011-----  
00386> # DYNIN-ID:NHYD---->ARAHa-QPEAKcms-TpeakDate\_hh:mm::--RVMn-R.C.--DWFcms  
00387> # CONTINUOUS:NASHYD 1.0 01:SW\_1M 8666.00 11.228 No\_date 38:07 13.94 .306 .000  
00388> # [CIN= 72.01: N= 3.00: Tp= 8.00]  
00389> # [iAEc= 4.00: SMIN= 39.75: SMAX=264.99: SK= .010]  
00390> #  
00391> # [InterEventTime= 12.00]  
00392> #  
003

00376+ # Dtnin-ID:HYND-----ARAbn-QPEAKms-Tpeakdate\_hh:mm:--RVMn-R.C.---DWFcms  
00377+ ADD HYD + 1.0 021SW\_11 8506.00 7.379 No\_date 33:12 11.20 n/a .000  
00378+ + 1.0 021SW\_11 500.00 2.720 No\_date 29:22 11.98 n/a .000  
00379+ + 1.0 021SW\_11 9197.00 4.042 No\_date 34:34 11.98 n/a .000  
00380+ SUM+ 1.0 018.N.311 11923.00 12.077 No\_date 33:14 11.96 n/a .000  
00381+ # Sum of hydrographs from Node 11 routed to Node 10  
00382+ # Section 1.  
00383+ #  
00384+ # Dtnin-ID:00040-----Dtnin-ID:HYND-----ARAbn-QPEAKms-Tpeakdate\_hh:mm:--RVMn-R.C.---DWFcms  
00385+ ROUTE CHANNEL -> 1.0 021.S.X11 11923.00 12.077 No\_date 33:14 11.96 n/a .000  
00386+ [ROT: 1.00] out-> 1.0 01N10 11923.00 8.276 No\_date 39:46 11.36 n/a .000  
00387+ [L/S/n=.14628/.1577/.040] [Vmax=.462 Dmax=.888]  
00388+ #  
00389+ # Addition of Subwatershed 10 to Node 10  
00390+ #  
00391+ # Dtnin-ID:00041-----Dtnin-ID:HYND-----ARAbn-QPEAKms-Tpeakdate\_hh:mm:--RVMn-R.C.---DWFcms  
00392+ ADD HYD + 1.0 021SW\_10 11923.00 8.276 No\_date 39:46 11.36 n/a .000  
00393+ + 1.0 021SW\_10 5666.00 11.228 No\_date 38:07 13.94 n/a .000  
00394+ SUM+ 1.0 018.N.310 17889.00 19.451 No\_date 38:31 12.19 n/a .000  
00395+ # SAVE HYD 1.0 018.N.310 17889.00 19.451 No\_date 38:31 12.19 n/a .000  
00396+ #  
00397+ # Sum of hydrographs from Node 10 routed to Node 9  
00398+ # Section 2.  
00399+ #  
00400+ # Dtnin-ID:00042-----Dtnin-ID:HYND-----ARAbn-QPEAKms-Tpeakdate\_hh:mm:--RVMn-R.C.---DWFcms  
00401+ ADD HYD 1.0 021S.X10 17889.00 19.451 No\_date 38:31 12.19 n/a .000  
00402+ + 1.0 021KCG\_XM 8376.00 11.072 No\_date 39:59 11.98 n/a .000  
00403+ SUM+ 1.0 018.N.310A 25966.00 30.328 No\_date 39:59 12.12 n/a .000  
00404+ #  
00405+ #  
00406+ #  
00407+ # Addition of Subwatershed 9 to Nichols Creek to Node 9  
00408+ #  
00409+ # Dtnin-ID:00045-----Dtnin-ID:HYND-----ARAbn-QPEAKms-Tpeakdate\_hh:mm:--RVMn-R.C.---DWFcms  
00410+ ADD HYD 1.0 021NS 25966.00 29.579 No\_date 39:59 12.12 n/a .000  
00411+ + 1.0 021NS 1132.00 1.000 No\_date 39:59 12.12 n/a .000  
00412+ + 1.0 021NC\_CW 4464.00 5.504 No\_date 39:59 10.98 n/a .000  
00413+ SUM+ 1.0 018.N.310 31561.00 36.313 No\_date 39:59 12.00 n/a .000  
00414+ #  
00415+ # Sum of hydrographs from Node 9 routed to Node 8  
00416+ # Section 3.  
00417+ #  
00418+ # Dtnin-ID:00046-----Dtnin-ID:HYND-----ARAbn-QPEAKms-Tpeakdate\_hh:mm:--RVMn-R.C.---DWFcms  
00419+ ADD HYD 1.0 021S.N.310 31561.00 36.313 No\_date 39:59 12.00 n/a .000  
00420+ + 1.0 021S.N.310 1.000 No\_date 39:59 12.00 n/a .000  
00421+ + 1.0 021NS 31561.00 34.173 No\_date 39:59 12.00 n/a .000  
00422+ [L/S/n=.2269/.088/.048] [Vmax=.418 Dmax=.1281]  
00423+ #  
00424+ #  
00425+ #  
00426+ #  
00427+ # Addition of Subwatershed 8 and Hobbs's Drain to Node 8  
00428+ #  
00429+ # Dtnin-ID:00047-----Dtnin-ID:HYND-----ARAbn-QPEAKms-Tpeakdate\_hh:mm:--RVMn-R.C.---DWFcms  
00430+ ADD HYD 1.0 021S.N.310 31561.00 36.313 No\_date 39:59 12.00 n/a .000  
00431+ + 1.0 021S.N.310 1.000 No\_date 39:59 12.00 n/a .000  
00432+ + 1.0 021NS 31561.00 34.173 No\_date 39:59 12.00 n/a .000  
00433+ [L/S/n=.3750/.053/.070] [Vmax=.208 Dmax=.1651]  
00434+ #  
00435+ #  
00436+ #  
00437+ #  
00438+ #  
00439+ #  
00440+ #  
00441+ #  
00442+ # Sum of hydrographs from Node 8 routed to Node 7  
00443+ # Section 4.  
00444+ #  
00445+ # Dtnin-ID:00048-----Dtnin-ID:HYND-----ARAbn-QPEAKms-Tpeakdate\_hh:mm:--RVMn-R.C.---DWFcms  
00446+ ADD HYD 1.0 021S.N.310 31561.00 34.173 No\_date 39:59 12.00 n/a .000  
00447+ + 1.0 021S.N.310 1.000 No\_date 39:59 12.00 n/a .000  
00448+ + 1.0 021NS 31561.00 32.891 No\_date 44:30 12.00 n/a .000  
00449+ [L/S/n=.3750/.053/.070] [Vmax=.208 Dmax=.1651]  
00450+ #  
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01487\* overflow < 1.0 03:2P-0WF .00 .000 No\_date 0:00 .00 n/a .000

[Morton-based\_208E+00] -> 1.0 03:2P-0WF .00 .000 No\_date 0:00 .00 n/a .000

01488\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01489\* ADD HYD

01490\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

+ 1.0 02:18-1-M4B .328 .019 No\_date 24:16 32.20 n/a .000

01491\* + 1.0 02:18-1-M4C .00 .000 No\_date 0:00 .00 n/a .000

01492\* + 1.0 02:18-1-M4D .00 .000 No\_date 0:00 .00 n/a .000

01493\* + 1.0 02:18-1-M4Bovf .12.84 .075 No\_date 29:23 32.20 n/a .000

01494\* + 1.0 02:18-1-M4Covf .00 .000 No\_date 0:00 .00 n/a .000

01495\* + 1.0 02:18-1-M4Dovf .00 .000 No\_date 0:00 .00 n/a .000

01496\* SUM+ 1.0 02:18-1-M4 .19.40 .816 No\_date 29:25 31.34 n/a .000

01497\* + 1.0 02:18-1-M4P2 .00 .000 No\_date 29:25 31.34 n/a .000

01498\* SUM+ 1.0 01:18-1-M4 .19.40 .816 No\_date 29:25 31.34 n/a .000

01499\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01500\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01501\* \*\*\*\*\* name :SNL\_CKE\_0002

01502\* # Channel X-Section obtained from RVEA Hydraulic Model - Station 5737

01503\* # Total Flows before Station 5737 on Rock River

01504\* # Channel X-Section obtained from RVEA Hydraulic Model - Station 5737

01505\* # 2021-02-25 add station 5737 before station 5002. Station 5737 was extracted from the HEC-RAS model T:\POBJ\1474-16\Dea

01506\* # JFS 2021-02-03 change the slope to 0.0175s instead of 0.0259s to stabilize the model

01507\* ROUTE CHANNEL --> 1.0 01:SNL\_CKE

01508\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01509\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01510\* \*\*\*\*\* name :SNL\_CKE\_0002

01511\* \*\*\*\*\* name :SNL\_CKE\_0002

01512\* remark:Total Flows before Station 5737 on Rock River

01513\* # Channel X-Section obtained from RVEA Hydraulic Model - Station 5737

01514\* # 2021-02-25 add station 5737 before station 5002. Station 5737 was extracted from the HEC-RAS model T:\POBJ\1474-16\Dea

01515\* # JFS 2021-02-03 change the slope to 0.0175s instead of 0.0259s to stabilize the model

01516\* ROUTE CHANNEL --> 1.0 01:SNL\_CKE

01517\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01518\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01519\* \*\*\*\*\* (RDT= 1.00) out- 1.0 01:5737 .54253 .89 48.535 No\_date 37:45 13.00 n/a .000

01520\* \*\*\*\*\* (Vmax=.611,Dmax= 3.459)

01521\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01522\* \*\*\*\*\* ADD HYD

01523\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

+ 1.0 02:18-1-M4B .21.67 .126 No\_date 29:27 32.20 n/a .000

01524\* + 1.0 02:18-1-M4B .1.75 .010 No\_date 29:14 32.20 n/a .000

01525\* + 1.0 02:18-1-M4C .20.00 .010 No\_date 29:14 32.20 n/a .000

01526\* + 1.0 02:18-1-M4D .00 .000 No\_date 0:00 .00 n/a .000

01527\* + 1.0 02:18-1-M4Bovf .00 .000 No\_date 0:00 .00 n/a .000

01528\* + 1.0 02:18-1-M4Covf .00 .000 No\_date 0:00 .00 n/a .000

01529\* SUM+ 1.0 01:5002 .54279 .33 48.627 No\_date 37:44 13.01 n/a .000

01530\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01531\* \*\*\*\*\* ADD RVD

01532\* \*\*\*\*\* name :S5002\_0002

01533\* remark:Total Flows before Station 5002. Rock River

01534\* # Channel X-Section obtained from RVEA Hydraulic Model - Station 5737

01535\* # Channel X-Section obtained from RVEA Hydraulic Model - Station 5002

01536\* # Hydrograph Total Flows before Station 5002. Road to Node at West Clarke Draw

01537\* # 2021-02-19 Change the slope from 0.01 s (per Man Stander Report 2007) to 0.0255 s so the model will be more stable

01538\* # JFS 2021-02-26 change the length of 5002 route channel from 825 m to 736 m. That is because of adding station 5737 to the model

01539\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01540\* \*\*\*\*\* ROUTE CHANNEL --> 1.0 01:SNL\_CKE

01541\* \*\*\*\*\* (RDT= 1.00) out- 1.0 01:MN\_CKE .54279 .33 48.688 No\_date 37:44 13.01 n/a .000

01542\* \*\*\*\*\* (Vmax=.648,Dmax= 2.423)

01543\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01544\* \*\*\*\*\* ROUTE CHANNEL --> 1.0 02:HN\_MCS .54279 .33 48.688 No\_date 37:20 13.01 n/a .000

01545\* \*\*\*\*\* (RDT= 1.00) out- 1.0 01:SLP1 .54279 .33 48.709 No\_date 37:36 13.01 n/a .000

01546\* \*\*\*\*\* (Vmax=.961,Dmax= .056)

01547\* \*\*\*\*\* (L8/rw .245 ./.056)

01548\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01549\* \*\*\*\*\* ROUTE CHANNEL --> 1.0 02:HN\_MCS .54279 .33 48.709 No\_date 37:36 13.01 n/a .000

01550\* \*\*\*\*\* (RDT= 1.00) out- 1.0 01:HN\_MCS .54279 .33 48.660 No\_date 36:26 13.01 n/a .000

01551\* \*\*\*\*\* (Vmax=.961,Dmax= .056)

01552\* \*\*\*\*\* (L8/rw .245 ./.056)

01553\* \*\*\*\*\* (Vmax=.961,Dmax= 2.011)

01554\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01555\* \*\*\*\*\* # Hydrograph from Node West Clarke route to Node at Kennedy - Burnett Drain

01556\* \*\*\*\*\* Channel X-Section obtained from RVEA Hydraulic Model - Station 4534

01557\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01558\* \*\*\*\*\* ROUTE CHANNEL --> 1.0 02:HN\_MCS .54279 .33 48.660 No\_date 36:26 13.01 n/a .000

01559\* \*\*\*\*\* (RDT= 1.00) out- 1.0 01:HN\_MCS .54279 .33 48.660 No\_date 36:26 13.01 n/a .000

01560\* \*\*\*\*\* (Vmax=.648,Dmax= 2.423)

01561\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01562\* \*\*\*\*\* (RDT= 1.00) out- 1.0 01:HN\_MCS .54279 .33 48.660 No\_date 36:26 13.01 n/a .000

01563\* \*\*\*\*\* (Vmax=.648,Dmax= 2.423)

01564\* # Catchment KEN\_BU

01565\* # To Kennedy-Burnett SWN Facility

01566\* # Catchment KEN\_BU (part of the basin (north of the Jock)

01567\* # Medium density residential subdivision

01568\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01569\* # Existing Kennedy-Burnett SWN Facility

01570\* # Rating curve obtained from RVEP

01571\* # 2021-02-26 change the length of 160 ha

01572\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01573\* \*\*\*\*\* CONTINOUS STANDYD 1.0 01:K8-1 .54279 .33 48.660 No\_date 28:08 13.01 n/a .000

01574\* \*\*\*\*\* (XIM=10-TIMEP=.40)

01575\* [Horton parameters] Po: 76.20:Pc-13.20:DCAY4:14. Fc .00

01576\* [Inverious area: IaImp=.79SLP1+.50:LGI=.522:MNI=.013:SCI=.01]

01577\* [iAEclmp: 4.00: iAEcpesr: 1.00]

01578\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01579\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01580\* Major System / .1.0 02:K8-1A-AZ .00 .000 No\_date 0:00 .00 n/a .000

01581\* Minor System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01582\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01583\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01584\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01585\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01586\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01587\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01588\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01589\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01590\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01591\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01592\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01593\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01594\* \*\*\*\*\* CONTINOUS STANDYD 1.0 01:K8-1 .54279 .33 48.660 No\_date 28:08 16.73 n/a .000

01595\* \*\*\*\*\* (XIM=10-TIMEP=.38)

01596\* [Horton parameters] Po: 76.20:Pc-13.20:DCAY4:14. Fc .00

01597\* [Inverious area: IaImp=.79SLP1+.50:LGI=.522:MNI=.013:SCI=.01]

01598\* [iAEclmp: 4.00: iAEcpesr: 1.00]

01599\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01600\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01601\* Major System / .1.0 02:K8-1A-AZ .00 .000 No\_date 0:00 .00 n/a .000

01602\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01603\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01604\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01605\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01606\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01607\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01608\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01609\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01610\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01611\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01612\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01613\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01614\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01615\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01616\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01617\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01618\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01619\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01620\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01621\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01622\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01623\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01624\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01625\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01626\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01627\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01628\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01629\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01630\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01631\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01632\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01633\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01634\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01635\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01636\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01637\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01638\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01639\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01640\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01641\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01642\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01643\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01644\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01645\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01646\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01647\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01648\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01649\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01650\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01651\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01652\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01653\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01654\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01655\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01656\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01657\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01658\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01659\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01660\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01661\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01662\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01663\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01664\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01665\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01666\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01667\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01668\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01669\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01670\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01671\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01672\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01673\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01674\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01675\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01676\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01677\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01678\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01679\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01680\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01681\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01682\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01683\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01684\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01685\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01686\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01687\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01688\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01689\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01690\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01691\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01692\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01693\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01694\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01695\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01696\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01697\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01698\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01699\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01700\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01701\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01702\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01703\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01704\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01705\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01706\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01707\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01708\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01709\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01710\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01711\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01712\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01713\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01714\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01715\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01716\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01717\* Minor System / .1.0 03:K8-1B-MN .31.10 .1.062 No\_date 28:08 16.73 n/a .000

01718\* [MjSysSto=.00000:TotOfV01=.00000:No\_Ovrl=.0. TotTurhovf=.0 hrs]

01719\* \*\*\*\*\* DTMN-ID:NHYD---ARAHa-QPEAKcms-Tpeakdate\_hh:mm::--RVM=R.C.--DWFcms

01720\* COMPUTER DUALHYS .1.0 01:K8-1A .00 .000 No\_date 0:00 .00 n/a .000

01721\* Major System / .1.0 02:K8-1B-MN .00 .000 No\_date 0:00 .00 n/a .000

01722\* Minor System / .1.0 03:K8-1

01871+ [IaREClipm- 4.00: IaREClipm- 4.00]

01872+ R0021:CO0078-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

01873+ 1.0 01:FR-2:Pond2 254.24 .5,330 No\_date 28:12 23.82 n/a .000

01874+ 1.0 01:FR-16\_1- 2.80 .293 No\_date 28:15 35.54 n/a .000

01875+ SUM- / 1.0 01:FR-16\_2- 25.21 104.99 No\_date 28:15 22.94 n/a .000

01876+ CONTINUOUS STANDYD -->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

01877+ ROUTE RESERVOIR -> 1.0 02:KE-P3 257.04 10.049 No\_date 28:11 22.96 n/a .000

01878+ [Previous area: IaIimp- 1.57 SLIP1+0.00LGd 28:11 22.96 n/a .000

01879+ overflow <- 1.0 01:KE-P4ovr 238.00 9.987 No\_date 18:01 22.96 n/a .000

01880+ [MjSysSto+, 2001E-03, TctOvFv01...000E+00, N-Ovr- 1. TotDurOvf+ 0. hrs] .000

01881+ ADD HYD \* 1.0 02:KE-P3ovr 238.50 9.997 No\_date 28:11 22.96 n/a .000

01882+ SUM- / 1.0 02:KE-P3ond 257.04 10.048 No\_date 28:11 22.96 n/a .000

01883+ SAVE HYD IaH\_Pond1 1.0 01:KE-Pond3 257.04 10.048 No\_date 28:11 22.96 n/a .000

01884+ # remark:Total Flows at KB thir pond

01885+ # EXPOSED PROPOSED Subcatchments (Kenney-Burnett SWN Facility (118080). SWN Modeling Approach, NOVATECH Report Ju

01886+ 1.0 01:FR-CLARE DRAIN

01887+ R0021:CO0080-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

01888+ 1.0 01:FR-CLARE DRAIN 8.03 .575 No\_date 28:01 23.89 .525 .000

01889+ CONTINUOUS STANDYD 1.0 01:FC-01 8.03 .575 No\_date 28:01 23.89 .525 .000

01890+ [XIMP- 47:TIME- 47]

01891+ Po: 76.20:FC-13.20:DCV4+14: F= .00

01892+ [Previous area: IaIimp- 4.67 SLIP1+0.00LGd 40.-NMP+-.250:SCP+ .0]

01893+ [Impervious area: IaIimp- 1.57 SLIP1+0.00LGd 231.-NMP-.013:SCI+ .0]

01894+ 4.00:FC-01 16.05 .159 No\_date 27:52 41.31 n/a .000

01895+ Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

01896+ COMPUTE DUALHYD 1.0 01:FC-01 8.03 .575 No\_date 28:01 23.89 n/a .000

01897+ ADD HYD 1.0 01:FC-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

01898+ SUM- / 1.0 01:FC-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

01899+ Minor System <- 1.0 01:FC-01-MJ 8.03 .575 No\_date 28:01 23.89 n/a .000

01900+ [KjND- 53:TIME- 64]

01901+ [Horton parameters: Po: 76.20:FC-13.20:DCV4+14: F= .00]

01902+ [Previous area: IaIimp- 4.67 SLIP1+0.00LGd 40.-NMP+-.250:SCP+ .0]

01903+ [Impervious area: IaIimp- 1.57 SLIP1+0.00LGd 327.-NMP-.013:SCI+ .0]

01904+ [IaREClipm- 4.00: IaREClipm- 4.00]

01905+ R0021:CO0084-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

01906+ 1.0 02:FC-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

01907+ ADD HYD 1.0 02:FC-01-MJ 8.03 .575 No\_date 28:01 23.89 n/a .000

01908+ SUM- / 1.0 02:FC-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

01909+ CONTINUOUS STANDYD 1.0 02:FC-01 16.05 1.938 No\_date 28:01 41.29 .907 .000

01910+ [KjND- 53:TIME- 64]

01911+ [Horton parameters: Po: 76.20:FC-13.20:DCV4+14: F= .00]

01912+ [Previous area: IaIimp- 4.67 SLIP1+0.00LGd 40.-NMP+-.250:SCP+ .0]

01913+ [Impervious area: IaIimp- 1.57 SLIP1+0.00LGd 231.-NMP-.013:SCI+ .0]

01914+ [IaREClipm- 4.00: IaREClipm- 4.00]

01915+ R0021:CO0085-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

01916+ 1.0 02:FC-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

01917+ COMPUTE DUALHYD 1.0 02:FC-02 8.03 .575 No\_date 28:01 23.89 n/a .000

01918+ Major System <- 1.0 02:FC-02-MJ 16.05 1.159 No\_date 27:52 41.31 n/a .000

01919+ Minor System <- 1.0 02:FC-02-MJ 16.05 1.159 No\_date 27:52 41.31 n/a .000

01920+ R0021:CO0086-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

01921+ 1.0 02:FC-02-MJ 0.00 .000 No\_date 0:00 0 n/a .000

01922+ CONTINUOUS STANDYD 1.0 02:FC-02 16.05 1.159 No\_date 27:52 41.31 n/a .000

01923+ [KjND- 53:TIME- 64]

01924+ [Horton parameters: Po: 76.20:FC-13.20:DCV4+14: F= .00]

01925+ [Previous area: IaIimp- 4.67 SLIP1+0.00LGd 40.-NMP+-.250:SCP+ .0]

01926+ [Impervious area: IaIimp- 1.57 SLIP1+0.00LGd 231.-NMP-.013:SCI+ .0]

01927+ [IaREClipm- 4.00: IaREClipm- 4.00]

01928+ R0021:CO0087-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

01929+ 1.0 02:FC-02-MJ 0.00 .000 No\_date 0:00 0 n/a .000

01930+ COMPUTE DUALHYD 1.0 02:FC-02 8.03 .575 No\_date 28:01 23.89 n/a .000

01931+ Major System <- 1.0 02:FC-02-MJ 16.05 1.159 No\_date 27:52 41.31 n/a .000

01932+ Minor System <- 1.0 02:FC-02-MJ 16.05 1.159 No\_date 27:52 41.31 n/a .000

01933+ R0021:CO0088-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

01934+ 1.0 02:FC-02-MJ 0.00 .000 No\_date 0:00 0 n/a .000

01935+ CONTINUOUS STANDYD 1.0 02:FC-02 16.05 1.159 No\_date 27:52 41.31 n/a .000

01936+ [KjND- 53:TIME- 64]

01937+ [Horton parameters: Po: 76.20:FC-13.20:DCV4+14: F= .00]

01938+ [Previous area: IaIimp- 4.67 SLIP1+0.00LGd 40.-NMP+-.250:SCP+ .0]

01939+ [Impervious area: IaIimp- 1.57 SLIP1+0.00LGd 231.-NMP-.013:SCI+ .0]

01940+ [IaREClipm- 4.00: IaREClipm- 4.00]

01941+ R0021:CO0089-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

01942+ CONTINUOUS STANDYD 1.0 01:FC-01 12.87 1.148 No\_date 28:01 30.32 .666 .000

01943+ [KjND- 53:TIME- 64]

01944+ [Horton parameters: Po: 76.20:FC-13.20:DCV4+14: F= .00]

01945+ [Previous area: IaIimp- 4.67 SLIP1+0.00LGd 40.-NMP+-.250:SCP+ .0]

01946+ [Impervious area: IaIimp- 1.57 SLIP1+0.00LGd 231.-NMP-.013:SCI+ .0]

01947+ [IaREClipm- 4.00: IaREClipm- 4.00]

01948+ R0021:CO0090-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

01949+ 1.0 01:FC-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

01950+ ADD HYD \* 1.0 01:FC-01-MJ 7.37 .398 No\_date 27:49 30.49 n/a .000

01951+ SUM- / 1.0 01:FC-01-MJ 7.37 .398 No\_date 27:49 30.49 n/a .000

01952+ R0021:CO0091-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

01953+ 1.0 01:FC-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

01954+ CONTINUOUS STANDYD 1.0 01:FC-01 12.87 1.148 No\_date 28:01 30.32 .666 .000

01955+ [KjND- 53:TIME- 64]

01956+ [Horton parameters: Po: 76.20:FC-13.20:DCV4+14: F= .00]

01957+ [Previous area: IaIimp- 4.67 SLIP1+0.00LGd 40.-NMP+-.250:SCP+ .0]

01958+ [Impervious area: IaIimp- 1.57 SLIP1+0.00LGd 231.-NMP-.013:SCI+ .0]

01959+ [IaREClipm- 4.00: IaREClipm- 4.00]

01960+ R0021:CO0092-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

01961+ 1.0 01:FC-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

01962+ CONTINUOUS STANDYD 1.0 01:FC-01 12.87 1.148 No\_date 28:01 30.32 .666 .000

01963+ [KjND- 53:TIME- 64]

01964+ [Horton parameters: Po: 76.20:FC-13.20:DCV4+14: F= .00]

01965+ [Previous area: IaIimp- 4.67 SLIP1+0.00LGd 40.-NMP+-.250:SCP+ .0]

01966+ [Impervious area: IaIimp- 1.57 SLIP1+0.00LGd 231.-NMP-.013:SCI+ .0]

01967+ [IaREClipm- 4.00: IaREClipm- 4.00]

01968+ R0021:CO0093-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

01969+ 1.0 01:FC-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

01970+ ADD HYD \* 1.0 01:FC-01-MJ 7.37 .398 No\_date 27:52 30.49 n/a .000

01971+ SUM- / 1.0 01:FC-01-MJ 7.37 .398 No\_date 27:52 30.49 n/a .000

01972+ R0021:CO0094-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

01973+ 1.0 01:FC-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

01974+ CONTINUOUS STANDYD 1.0 01:FR-01 12.87 1.148 No\_date 28:01 30.32 .666 .000

01975+ [KjND- 53:TIME- 64]

01976+ [Horton parameters: Po: 76.20:FC-13.20:DCV4+14: F= .00]

01977+ [Previous area: IaIimp- 4.67 SLIP1+0.00LGd 40.-NMP+-.250:SCP+ .0]

01978+ [Impervious area: IaIimp- 1.57 SLIP1+0.00LGd 231.-NMP-.013:SCI+ .0]

01979+ [IaREClipm- 4.00: IaREClipm- 4.00]

01980+ R0021:CO0095-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

01981+ 1.0 01:FR-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

01982+ CONTINUOUS STANDYD 1.0 01:FR-01 12.87 1.148 No\_date 28:01 30.32 .666 .000

01983+ [KjND- 53:TIME- 64]

01984+ [Horton parameters: Po: 76.20:FC-13.20:DCV4+14: F= .00]

01985+ [Previous area: IaIimp- 4.67 SLIP1+0.00LGd 40.-NMP+-.250:SCP+ .0]

01986+ [Impervious area: IaIimp- 1.57 SLIP1+0.00LGd 231.-NMP-.013:SCI+ .0]

01987+ [IaREClipm- 4.00: IaREClipm- 4.00]

01988+ R0021:CO0096-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

01989+ 1.0 01:FR-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

01990+ CONTINUOUS STANDYD 1.0 01:FR-01 12.87 1.148 No\_date 28:01 30.32 .666 .000

01991+ [KjND- 53:TIME- 64]

01992+ [Horton parameters: Po: 76.20:FC-13.20:DCV4+14: F= .00]

01993+ [Previous area: IaIimp- 4.67 SLIP1+0.00LGd 40.-NMP+-.250:SCP+ .0]

01994+ [Impervious area: IaIimp- 1.57 SLIP1+0.00LGd 231.-NMP-.013:SCI+ .0]

01995+ [IaREClipm- 4.00: IaREClipm- 4.00]

01996+ R0021:CO0097-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

01997+ 1.0 01:FR-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

01998+ CONTINUOUS STANDYD 1.0 01:FR-01 12.87 1.148 No\_date 28:01 30.32 .666 .000

01999+ [KjND- 53:TIME- 64]

02000+ [Horton parameters: Po: 76.20:FC-13.20:DCV4+14: F= .00]

02001+ [Previous area: IaIimp- 4.67 SLIP1+0.00LGd 40.-NMP+-.250:SCP+ .0]

02002+ [Impervious area: IaIimp- 1.57 SLIP1+0.00LGd 231.-NMP-.013:SCI+ .0]

02003+ [IaREClipm- 4.00: IaREClipm- 4.00]

02004+ R0021:CO0098-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

02005+ 1.0 01:FR-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

02006+ CONTINUOUS STANDYD 1.0 01:FR-01 12.87 1.148 No\_date 28:02 30.37 .678 .000

02007+ [KjND- 53:TIME- 64]

02008+ [Horton parameters: Po: 76.20:FC-13.20:DCV4+14: F= .00]

02009+ [Previous area: IaIimp- 4.67 SLIP1+0.00LGd 40.-NMP+-.250:SCP+ .0]

02010+ [Impervious area: IaIimp- 1.57 SLIP1+0.00LGd 231.-NMP-.013:SCI+ .0]

02011+ [IaREClipm- 4.00: IaREClipm- 4.00]

02012+ R0021:CO0099-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

02013+ 1.0 01:FR-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

02014+ CONTINUOUS STANDYD 1.0 01:FR-01 12.87 1.148 No\_date 28:02 30.37 .678 .000

02015+ [KjND- 53:TIME- 64]

02016+ [Horton parameters: Po: 76.20:FC-13.20:DCV4+14: F= .00]

02017+ [Previous area: IaIimp- 4.67 SLIP1+0.00LGd 40.-NMP+-.250:SCP+ .0]

02018+ [Impervious area: IaIimp- 1.57 SLIP1+0.00LGd 231.-NMP-.013:SCI+ .0]

02019+ [IaREClipm- 4.00: IaREClipm- 4.00]

02020+ R0021:CO0100-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

02021+ 1.0 01:FR-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

02022+ CONTINUOUS STANDYD 1.0 01:FR-01 12.87 1.148 No\_date 28:02 30.37 .678 .000

02023+ [KjND- 53:TIME- 64]

02024+ [Horton parameters: Po: 76.20:FC-13.20:DCV4+14: F= .00]

02025+ [Previous area: IaIimp- 4.67 SLIP1+0.00LGd 40.-NMP+-.250:SCP+ .0]

02026+ [Impervious area: IaIimp- 1.57 SLIP1+0.00LGd 231.-NMP-.013:SCI+ .0]

02027+ [IaREClipm- 4.00: IaREClipm- 4.00]

02028+ R0021:CO0101-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

02029+ 1.0 01:FR-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

02030+ CONTINUOUS STANDYD 1.0 01:FR-01 12.87 1.148 No\_date 28:02 30.37 .678 .000

02031+ [KjND- 53:TIME- 64]

02032+ [Horton parameters: Po: 76.20:FC-13.20:DCV4+14: F= .00]

02033+ [Previous area: IaIimp- 4.67 SLIP1+0.00LGd 40.-NMP+-.250:SCP+ .0]

02034+ [Impervious area: IaIimp- 1.57 SLIP1+0.00LGd 231.-NMP-.013:SCI+ .0]

02035+ [IaREClipm- 4.00: IaREClipm- 4.00]

02036+ R0021:CO0102-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

02037+ 1.0 01:FR-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

02038+ CONTINUOUS STANDYD 1.0 01:FR-01 12.87 1.148 No\_date 28:02 30.37 .678 .000

02039+ [KjND- 53:TIME- 64]

02040+ [Horton parameters: Po: 76.20:FC-13.20:DCV4+14: F= .00]

02041+ [Previous area: IaIimp- 4.67 SLIP1+0.00LGd 40.-NMP+-.250:SCP+ .0]

02042+ [Impervious area: IaIimp- 1.57 SLIP1+0.00LGd 231.-NMP-.013:SCI+ .0]

02043+ [IaREClipm- 4.00: IaREClipm- 4.00]

02044+ R0021:CO0103-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

02045+ 1.0 01:FR-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

02046+ COMPUTE DUALHYD 1.0 01:FR-01-MJ 25.50 1.427 No\_date 28:04 25.60 n/a .000

02047+ Major System <- 1.0 01:FR-01-MJ .00 .000 No\_date 0:00 0 n/a .000

02048+ Minor System <- 1.0 01:FR-01-MJ 25.50 1.427 No\_date 28:04 25.60 n/a .000

02049+ R0021:CO0104-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

02050+ 1.0 01:FR-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

02051+ CONTINUOUS STANDYD 1.0 01:FR-01 21.61 1.710 No\_date 28:02 30.87 .678 .000

02052+ [KjND- 53:TIME- 64]

02053+ [Horton parameters: Po: 76.20:FC-13.20:DCV4+14: F= .00]

02054+ [Previous area: IaIimp- 4.67 SLIP1+0.00LGd 40.-NMP+-.250:SCP+ .0]

02055+ [Impervious area: IaIimp- 1.57 SLIP1+0.00LGd 231.-NMP-.013:SCI+ .0]

02056+ [IaREClipm- 4.00: IaREClipm- 4.00]

02057+ R0021:CO0105-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

02058+ 1.0 01:FR-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

02059+ COMPUTE DUALHYD 1.0 01:FR-01-MJ 25.50 1.427 No\_date 28:04 25.60 n/a .000

02060+ Major System <- 1.0 01:FR-01-MJ .00 .000 No\_date 0:00 0 n/a .000

02061+ Minor System <- 1.0 01:FR-01-MJ 25.50 1.427 No\_date 28:04 25.60 n/a .000

02062+ R0021:CO0106-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

02063+ 1.0 01:FR-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

02064+ COMPUTE DUALHYD 1.0 01:FR-01-MJ 25.50 1.427 No\_date 28:04 25.60 n/a .000

02065+ Major System <- 1.0 01:FR-01-MJ .00 .000 No\_date 0:00 0 n/a .000

02066+ Minor System <- 1.0 01:FR-01-MJ 25.50 1.427 No\_date 28:04 25.60 n/a .000

02067+ R0021:CO0107-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

02068+ 1.0 01:FR-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

02069+ COMPUTE DUALHYD 1.0 01:FR-01-MJ 25.50 1.427 No\_date 28:04 25.60 n/a .000

02070+ Major System <- 1.0 01:FR-01-MJ .00 .000 No\_date 0:00 0 n/a .000

02071+ Minor System <- 1.0 01:FR-01-MJ 25.50 1.427 No\_date 28:04 25.60 n/a .000

02072+ R0021:CO0108-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

02073+ 1.0 01:FR-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

02074+ COMPUTE DUALHYD 1.0 01:FR-01-MJ 25.50 1.427 No\_date 28:04 25.60 n/a .000

02075+ Major System <- 1.0 01:FR-01-MJ .00 .000 No\_date 0:00 0 n/a .000

02076+ Minor System <- 1.0 01:FR-01-MJ 25.50 1.427 No\_date 28:04 25.60 n/a .000

02077+ R0021:CO0109-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

02078+ 1.0 01:FR-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

02079+ COMPUTE DUALHYD 1.0 01:FR-01-MJ 25.50 1.427 No\_date 28:04 25.60 n/a .000

02080+ Major System <- 1.0 01:FR-01-MJ .00 .000 No\_date 0:00 0 n/a .000

02081+ Minor System <- 1.0 01:FR-01-MJ 25.50 1.427 No\_date 28:04 25.60 n/a .000

02082+ R0021:CO0110-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

02083+ 1.0 01:FR-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

02084+ COMPUTE DUALHYD 1.0 01:FR-01-MJ 25.50 1.427 No\_date 28:04 25.60 n/a .000

02085+ Major System <- 1.0 01:FR-01-MJ .00 .000 No\_date 0:00 0 n/a .000

02086+ Minor System <- 1.0 01:FR-01-MJ 25.50 1.427 No\_date 28:04 25.60 n/a .000

02087+ R0021:CO0111-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

02088+ 1.0 01:FR-01-MJ 0.00 .000 No\_date 0:00 0 n/a .000

02089+ COMPUTE DUALHYD 1.0 01:FR-01-MJ 25.50 1.427 No\_date 28:04 25.60 n/a .000

02090+ Major System <- 1.0 01:FR-01-MJ .00 .000 No\_date 0:00 0 n/a .000

02091+ Minor System <- 1.0 01:FR-01-MJ 25.50 1.427 No\_date 28:04 25.60 n/a .000

02092+ R0021:CO0112-->Dtnin:ID-NHYD-->ARAHa-QPEAKcms-Tpeakdate\_bh:mm---RVmn-R.C.---DFWfms

02093+ 1.0 01:FR-01-MJ 0.00 .00



[...]





03741+ frame : SNMF-A.0005  
03742+ remarks:SNMF-A Outflow  
03743+ R0005:CO0124-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03744+ ADD HVD + 1.0 02:SSA00T 364.27 3.398 No\_date 29:13 17.68 n/a .000  
03745+ out < 1.0 02:SSA00T 66.28 2.288 No\_date 30:00 42.00 n/a .000  
03746+ overfl < 1.0 02:SSA00T 0.00 0.000 No\_date 0:00 .00 n/a .000  
03747+ SUM+ 1.0 01:PT40S 431.02 3.613 No\_date 29:19 21.45 n/a .000  
03748+ [MjySsCed.:3924E-03] Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03749+ CONTINUOUS STANDHYD 1.0 01:CTC 5.87 .260 No\_date 28:01 44.01 .776 .000  
03750+ [XIMP+:68:TIME+.85] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03751+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03752+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03753+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03754+ R0005:CO0124-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03755+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03756+ ROUTE RESERVOIR > 1.0 02:CTC 1.87 .266 No\_date 28:01 44.03 n/a .000  
03757+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03758+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03759+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03760+ R0005:CO0124-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03761+ ROUTE RESERVOIR > 1.0 02:CTC 1.62 .227 No\_date 28:01 44.03 n/a .000  
03762+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03763+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03764+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03765+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03766+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03767+ R0005:CO0124-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03768+ ROUTE RESERVOIR > 1.0 02:CTC 1.62 .227 No\_date 28:01 44.03 n/a .000  
03769+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03770+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03771+ [MjySsCed.:3924E-03] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03772+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03773+ CONTINUOUS STANDHYD 1.0 01:CTC 1.62 .227 No\_date 28:01 44.01 .776 .000  
03774+ [XIMP+:68:TIME+.85] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03775+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03776+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03777+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03778+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03779+ R0005:CO0130-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03780+ ROUTE RESERVOIR > 1.0 02:ST-6 45 .044 No\_date 28:01 33.25 n/a .000  
03781+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03782+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03783+ [MjySsCed.:1924E-03] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03784+ CONTINUOUS STANDHYD 1.0 01:ST-6 45 .044 No\_date 28:00 33.25 .582 .000  
03785+ [XIMP+:68:TIME+.85] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03786+ ADD HVD + 1.0 02:PT40S 1.87 .058 No\_date 28:26 44.03 n/a .000  
03787+ out < 1.0 02:PT40S 0.00 .000 No\_date 0:00 .00 n/a .000  
03788+ 1.0 02:CT-7 1.62 .050 No\_date 28:26 44.03 n/a .000  
03789+ 1.0 02:CT-7 0.44 .000 No\_date 0:00 .00 n/a .000  
03790+ 1.0 02:CT-7 0.45 .000 No\_date 0:00 .00 n/a .000  
03791+ 1.0 02:ST60WV 0.00 .000 No\_date 0:00 .00 n/a .000  
03792+ 80M+ 1.0 02:PT75T 416.00 3.684 No\_date 29:13 21.64 n/a .000  
03793+ R0005:CO0132-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03794+ ROUTE CHANNEL > 1.0 02:PT57S 434.92 3.684 No\_date 29:13 21.64 n/a .000  
03795+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03796+ [L/S/nr: 424 / .100/.043] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03797+ [Vmax: .480:Time: 2.18] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03798+ R0005:CO0133-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03799+ CONTINUOUS STANDHYD 1.0 01:ID-4 1.76 .049 No\_date 28:35 27.98 .499 .000  
03800+ [CN: 88.0: N 3.00: Tp: .60] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03801+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03802+ [InterEventTime: 12.00] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03803+ R0005:CO0134-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03804+ 1.0 01:Area-B 24.04 2.784 No\_date 28:00 40.98 .717 .000  
03805+ [XIMP+:68:TIME+.77] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03806+ [Horton parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03807+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03808+ [iREcE: 4.00: IapRecP: 4.00] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03809+ R0005:CO0135-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03810+ ROUTE RESERVOIR > 1.0 02:Area-B 24.04 2.784 No\_date 28:04 40.98 n/a .000  
03811+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03812+ out < 1.0 02:Area-B 24.04 2.784 No\_date 28:15 40.98 n/a .000  
03813+ overfl < 1.0 02:Area-B 24.04 2.784 No\_date 28:15 40.98 n/a .000  
03814+ [MjySsCed.:6777E-03] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03815+ ADD HVD + 1.0 02:PT40S 0.00 .000 No\_date 0:00 .00 n/a .000  
03816+ R0005:CO0136-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03817+ out < 1.0 02:PT40S 1.73 .049 No\_date 28:35 27.98 n/a .000  
03818+ 1.0 02:SM2WP 24.04 .278 No\_date 28:15 40.98 n/a .000  
03819+ 1.0 02:SM2WP 24.04 .278 No\_date 28:15 40.98 n/a .000  
03820+ SUM+ 1.0 01:ID-EX 460.60 3.861 No\_date 29:25 22.68 n/a .000  
03821+ R0005:CO0137-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03822+ ROUTE CHANNEL > 1.0 02:ID-1 38.00 No\_date 28:42 25.92 .454 .000  
03823+ [RD7: 1.00:01] < 1.0 01:DRAIN4 460.69 3.810 No\_date 29:44 22.68 n/a .000  
03824+ [RD7: 1.00:01] < 1.0 01:DRAIN4 460.69 3.810 No\_date 28:42 25.92 .454 .000  
03825+ CONTINUOUS STANDHYD 1.0 01:ID-1 1.90 .044 No\_date 28:42 25.92 .454 .000  
03826+ [CN: 88.0: N 3.00: Tp: .60] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03827+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03828+ [InterEventTime: 12.00] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03829+ R0005:CO0138-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03830+ CONTINUOUS STANDHYD 1.0 01:ID-1 9.74 .290 No\_date 28:22 24.64 .431 .000  
03831+ [CN: 88.0: N 3.00: Tp: .60] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03832+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03833+ [InterEventTime: 12.00] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03834+ R0005:CO0139-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03835+ CONTINUOUS STANDHYD 1.0 01:ID-1 10.67 .385 No\_date 28:13 23.43 .410 .000  
03836+ [CN: 88.0: N 3.00: Tp: .60] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03837+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03838+ [InterEventTime: 12.00] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03839+ R0005:CO0140-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03840+ CONTINUOUS STANDHYD 1.0 01:ID-1 9.74 .290 No\_date 28:22 24.64 n/a .000  
03841+ [CN: 88.0: N 3.00: Tp: .60] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03842+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03843+ ADD HVD + 1.0 02:ID-1 38.00 No\_date 28:42 25.92 n/a .000  
03844+ out < 1.0 02:ID-1 38.00 No\_date 28:42 25.92 n/a .000  
03845+ overfl < 1.0 02:ID-1 38.00 No\_date 28:42 25.92 n/a .000  
03846+ [MjySsCed.:1186E-03] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03847+ R0005:CO0142-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03848+ CONTINUOUS STANDHYD 1.0 01:ID-1 10.67 .385 No\_date 28:13 23.43 .410 .000  
03849+ [CN: 88.0: N 3.00: Tp: .60] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03850+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03851+ [InterEventTime: 12.00] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03852+ R0005:CO0143-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03853+ CONTINUOUS STANDHYD 1.0 01:ID-1 9.74 .290 No\_date 28:22 24.64 n/a .000  
03854+ [CN: 88.0: N 3.00: Tp: .60] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03855+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03856+ [InterEventTime: 12.00] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03857+ R0005:CO0144-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03858+ ADD HVD + 1.0 02:ID-1 38.00 No\_date 28:42 25.92 n/a .000  
03859+ out < 1.0 02:ID-1 38.00 No\_date 28:42 25.92 n/a .000  
03860+ overfl < 1.0 02:ID-1 38.00 No\_date 28:42 25.92 n/a .000  
03861+ [MjySsCed.:1186E-03] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03862+ R0005:CO0145-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03863+ CONTINUOUS STANDHYD 1.0 01:ID-1 8.79 .297 No\_date 28:02 22.71 n/a .000  
03864+ [CN: 88.0: N 3.00: Tp: .60] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03865+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03866+ [InterEventTime: 12.00] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03867+ R0005:CO0146-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03868+ ADD HVD + 1.0 02:ID-1 38.00 No\_date 28:04 22.71 n/a .000  
03869+ out < 1.0 02:ID-1 38.00 No\_date 28:04 22.71 n/a .000  
03870+ overfl < 1.0 02:ID-1 38.00 No\_date 28:04 22.71 n/a .000  
03871+ [MjySsCed.:4714E-03] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03872+ R0005:CO0151-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03873+ CONTINUOUS STANDHYD 1.0 01:ID-1 6.79 .831 No\_date 28:01 42.00 n/a .000  
03874+ [CN: 88.0: N 3.00: Tp: .60] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03875+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03876+ [InterEventTime: 12.00] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03877+ R0005:CO0152-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03878+ COMPUTE DUALHYD 1.0 01:ID-1 6.79 .831 No\_date 28:01 42.00 n/a .000  
03879+ Major System / 1.0 02:ID-1 38.00 No\_date 0:00 .00 n/a .000  
03880+ Minor System / 1.0 02:ID-1 38.00 No\_date 0:00 .00 n/a .000  
03881+ [MjySsCed.:1144E-03] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03882+ R0005:CO0153-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03883+ ROUTE RESERVOIR > 1.0 02:ID-1 38.00 No\_date 28:02 22.07 n/a .000  
03884+ out < 1.0 02:ID-1 38.00 No\_date 28:02 22.07 n/a .000  
03885+ overfl < 1.0 02:ID-1 38.00 No\_date 28:02 22.07 n/a .000  
03886+ [MjySsCed.:4714E-03] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03887+ R0005:CO0154-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03888+ CONTINUOUS STANDHYD 1.0 01:ID-1 6.79 .831 No\_date 28:01 42.00 n/a .000  
03889+ [CN: 88.0: N 3.00: Tp: .60] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03890+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03891+ [InterEventTime: 12.00] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03892+ R0005:CO0155-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03893+ CONTINUOUS STANDHYD 1.0 01:ID-1 6.79 .831 No\_date 28:01 42.00 n/a .000  
03894+ [CN: 88.0: N 3.00: Tp: .60] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03895+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03896+ [InterEventTime: 12.00] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03897+ R0005:CO0156-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03898+ CONTINUOUS STANDHYD 1.0 01:ID-1 6.79 .831 No\_date 28:01 42.00 n/a .000  
03899+ [CN: 88.0: N 3.00: Tp: .60] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03900+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03901+ [InterEventTime: 12.00] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03902+ R0005:CO0157-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03903+ CONTINUOUS STANDHYD 1.0 01:ID-1 6.79 .831 No\_date 28:01 42.00 n/a .000  
03904+ [CN: 88.0: N 3.00: Tp: .60] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03905+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03906+ [InterEventTime: 12.00] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03907+ R0005:CO0158-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03908+ CONTINUOUS STANDHYD 1.0 01:ID-1 6.79 .831 No\_date 28:01 42.00 n/a .000  
03909+ [CN: 88.0: N 3.00: Tp: .60] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03910+ [Previous parameters area: Iaper: 4.67:SLPP+:50:LGP: 50.NMP+:250:SCP+:0] .000  
03911+ ADD HVD + 1.0 02:ID-1 38.00 No\_date 0:00 .00 n/a .000  
03912+ out < 1.0 02:ID-1 38.00 No\_date 0:00 .00 n/a .000  
03913+ SUM+ 1.0 02:ID-1 38.00 No\_date 0:00 .00 n/a .000  
03914+ R0005:CO0154-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03915+ ROUTE RESERVOIR > 1.0 02:ID-1 38.00 No\_date 29:01 22.07 n/a .000  
03916+ out < 1.0 02:ID-1 38.00 No\_date 29:01 22.07 n/a .000  
03917+ overfl < 1.0 02:ID-1 38.00 No\_date 0:00 .00 n/a .000  
03918+ [MjySsCed.:1171E-03] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03919+ R0005:CO0155-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03920+ CONTINUOUS STANDHYD 1.0 01:ID-1 5364.36 68.074 No\_date 34:06 18.33 n/a .000  
03921+ [CN: 88.0: N 3.00: Tp: .60] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03922+ out < 1.0 02:ID-1 38.00 No\_date 34:06 18.33 n/a .000  
03923+ overfl < 1.0 02:ID-1 38.00 No\_date 34:06 18.33 n/a .000  
03924+ [MjySsCed.:1171E-03] Dtnin:ID:NHYD---Po: 76.20fPc: 13.20:DCAY:4.14: Fc\_001  
03925+ R0005:CO0156-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03926+ CONTINUOUS STANDHYD 1.0 01:ID-1 5377.82 69.530 No\_date 34:06 18.39 n/a .000  
03927+ R0005:CO0156-----Dtnin:ID:NHYD---AReAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcms  
03928+ SAVE HYD frame:SNMF-A.0005  
03929+ frame:SNMF-A.0005  
03930+ frame:SNMF-A.0005  
03931+ frame:SNMF-A.0005  
03932+ frame:SNMF-A.0005  
03933+ frame:SNMF-A.0005  
03934+ frame:SNMF-A.0005  
03935+ frame:SNMF-A.0005  
03936+ frame:SNMF-A.0005  
03937+ frame:SNMF-A.0005  
03938+ frame:SNMF-A.0005  
03939+ frame:SNMF-A.0005  
03940+ frame:SNMF-A.0005  
03941+ frame:SNMF-A.0005  
03942+ frame:SNMF-A.0005  
03943+ frame:SNMF-A.0005  
03944+ frame:SNMF-A.0005  
03945+ frame:SNMF-A.0005  
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03963+ frame:SNMF-A.0005  
03964+ frame:SNMF-A.0005  
03965+ frame:SNMF-A.0005  
03966+ frame:SNMF-A.0005  
03967+ frame:SNMF-A.0005  
03968+ frame:SNMF-A.0005  
03969+ frame:SNMF-A.0005  
03970+ frame:SNMF-A.0005  
03971+ frame:SNMF-A.0005  
03972+ frame:SNMF-A.0005  
03973+ frame:SNMF-A.0005  
03974+ frame:SNMF-A.0005  
03975+ frame:SNMF-A.0005  
03976+ frame:SNMF-A.0005  
03977+ frame:SNMF-A.0005  
03978+ frame:SNMF-A.0005  
03979+ frame:SNMF-A.0005  
03980+ frame:SNMF-A.0005  
03981+ frame:SNMF-A.0005  
03982+ frame:SNMF-A.0005  
03983+ frame:SNMF-A.0005<br

04115+ [IaRC4c: 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]  
 04116+ [InterEventTime= 12.00]  
 04117+ DROOS:CO00188-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04118+ ADD HVD  
 04119+ 1. 0 021-S\_FO 53377.82 69.319 No\_date 34:07 18.39 n/a .000  
 04120+ 1. 0 021-S\_PIO 335.42 6.023 No\_date 28:00 37.36 n/a .000  
 04121+ 1. 0 021-P10\_OVF 75.00 .000 No\_date 0:00 41.22 n/a .000  
 04122+ 1. 0 021-M\_WUD 35.65 .462 No\_date 28:00 21.69 n/a .000  
 04123+ 1. 0 021-M1\_P10Pnd 1.00 .000 No\_date 0:00 41.22 n/a .000  
 04124+ 1. 0 021-S1PFO\_FDR 14.96 .112 No\_date 29:32 41.69 n/a .000  
 04125+ 1. 0 021-S1-DBRovf 1.00 .000 No\_date 28:48 30.94 n/a .000  
 04126+ 1. 0 021-S1 5.27 .036 No\_date 28:48 30.94 n/a .000  
 04127+ 1. 0 021-S1-A 75.87 1.479 No\_date 28:37 21.69 n/a .000  
 04128+ SMD 1. 0 01W-CLAR\_MJ 54118.36 18.51 No\_date 34:07 18.39 n/a .000  
 04129+ RDOOS:CO00188-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04130+ SAVE HYD 1. 0 01W\_SPM\_FO 54118.36 72.161 No\_date 33:44 18.55 n/a .000  
 04131+ remark:Total Flows at Foster Drainage Node Foster from RVEA Hydraulic Model - Station 6016  
 04132+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 6016  
 04133+ # Catchment S-1  
 04134+ # Catchments S-1 (north and south of Jock)  
 04135+ # - Primarily agricultural fields; portion of sand quarry  
 04136+ RDOOS:CO00189-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04137+ CONTINUOUS STANDYD 1. 0 01S-1-B 55.36 1.342 No\_date 28:24 21.69 .380 .000  
 04138+ [CN= 77.0: N= 3.0: Tp= .45] [L/S= 159. / .082/.035]  
 04139+ # InterEventTime= 12.001  
 04140+ # - JFSA 2021-02-24 change the names from S-1-Boc to S-1-A and S-1-B. Change their TP values based on the new areas  
 04141+ # - S-1-Boc and S-1-Boc1 and S-1-Boc2 and S-1-Boc3 and S-1-Boc4 are not existing anymore. "S-1-Boc1" is part of "S-1-PO-02" and "S-1-Boc2" is part of "S-1-PO-03"  
 04142+ # JFSA 2021-01-19, after adding Greenbank pond "S-1-Boc3" is not existing anymore  
 04143+ RDOOS:CO00191-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04144+ CONTINUOUS STANDYD 1. 0 01S-1-B 21.67 2.409 No\_date 28:02 42.00 .735 .000  
 04145+ [XWD=.65:TIME=.65] [LGS= 2 CN=.75;]  
 04146+ # Previous areas: Iaper: 4.67:SLPP=2.0:LGDP 40.:MNP=.250:SCP=.0] [Imperious: 1.57:SLIP=.75:LGM= 380.:MNP=.013:SCI=.0]  
 04147+ iabEClipm: 4.00:IRaRCPper: 4.00: [IaRC4c: 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]  
 04148+ COMPUTE DUALHYP 1. 0 01S-1-B 21.67 2.409 No\_date 28:02 42.00 .000  
 04149+ Major System / 1. 0 01S-1-B 21.67 2.409 No\_date 28:02 42.00 .000  
 04150+ Minor System / 1. 0 01S-1-B 21.67 2.409 No\_date 28:02 42.00 .000  
 04151+ ROUTE RESERVOIR > 1. 0 01S-1-B 21.67 2.409 No\_date 28:02 42.00 .000  
 04152+ SMD 1. 0 01S-1-B 21.67 2.409 No\_date 28:02 42.00 .000  
 04153+ ROUTE RESERVOIR < 1. 0 01S-1-B 21.67 .164 No\_date 29:24 42.01 n/a .000  
 04154+ overflow < 1. 0 01S-1-B 21.67 .000 No\_date 0:00 42.00 n/a .000  
 04155+ [ModCustEd.: 547000.000000, m3\_TotDvVol=.000000, m3\_N-Ovfl=.000000]  
 04156+ RDOOS:CO00192-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04157+ CONTINUOUS STANDYD 1. 0 01S-1-B 3.28 42.01 No\_date 28:00 42.00 .735 .000  
 04158+ [LGS=.65:TIME=.65] [Iaper: 4.67:SLPP=2.0:LGDP 40.:MNP=.250:SCP=.0] [Imperious: 1.57:SLIP=.75:LGM= 380.:MNP=.013:SCI=.0]  
 04159+ iabEClipm: 4.00:IRaRCPper: 4.00: [IaRC4c: 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]  
 04160+ COMPUTE DUALHYP 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04161+ Major System / 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04162+ Minor System / 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04163+ ROUTE RESERVOIR > 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04164+ SMD 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04165+ ROUTE RESERVOIR < 1. 0 01S-1-B 3.28 .025 No\_date 29:15 42.01 n/a .000  
 04166+ overflow < 1. 0 01S-1-B 3.28 .025 No\_date 0:00 42.00 n/a .000  
 04167+ [ModCustEd.: 547000.000000, m3\_TotDvVol=.000000, m3\_N-Ovfl=.000000]  
 04168+ RDOOS:CO00193-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04169+ CONTINUOUS STANDYD 1. 0 01S-1-B 3.28 42.01 No\_date 28:00 42.00 .735 .000  
 04170+ [LGS=.65:TIME=.65] [Iaper: 4.67:SLPP=2.0:LGDP 40.:MNP=.250:SCP=.0] [Imperious: 1.57:SLIP=.75:LGM= 380.:MNP=.013:SCI=.0]  
 04171+ iabEClipm: 4.00:IRaRCPper: 4.00: [IaRC4c: 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]  
 04172+ RDOOS:CO00194-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04173+ ROUTE RESERVOIR > 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04174+ overflow < 1. 0 01S-1-B 3.28 .025 No\_date 0:00 42.00 n/a .000  
 04175+ [ModCustEd.: 547000.000000, m3\_TotDvVol=.000000, m3\_N-Ovfl=.000000]  
 04176+ RDOOS:CO00195-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04177+ CONTINUOUS STANDYD 1. 0 01S-1-B 3.28 42.01 No\_date 28:00 42.00 .735 .000  
 04178+ [LGS=.65:TIME=.65] [Iaper: 4.67:SLPP=2.0:LGDP 40.:MNP=.250:SCP=.0] [Imperious: 1.57:SLIP=.75:LGM= 380.:MNP=.013:SCI=.0]  
 04179+ iabEClipm: 4.00:IRaRCPper: 4.00: [IaRC4c: 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]  
 04180+ COMPUTE DUALHYP 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04181+ Major System / 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04182+ Minor System / 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04183+ ROUTE RESERVOIR > 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04184+ SMD 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04185+ ROUTE RESERVOIR < 1. 0 01S-1-B 3.28 .025 No\_date 29:15 42.01 n/a .000  
 04186+ overflow < 1. 0 01S-1-B 3.28 .025 No\_date 0:00 42.00 n/a .000  
 04187+ [ModCustEd.: 547000.000000, m3\_TotDvVol=.000000, m3\_N-Ovfl=.000000]  
 04188+ RDOOS:CO00196-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04189+ CONTINUOUS STANDYD 1. 0 01S-1-B 3.28 42.01 No\_date 28:00 42.00 .735 .000  
 04190+ [LGS=.65:TIME=.65] [Iaper: 4.67:SLPP=2.0:LGDP 40.:MNP=.250:SCP=.0] [Imperious: 1.57:SLIP=.75:LGM= 380.:MNP=.013:SCI=.0]  
 04191+ iabEClipm: 4.00:IRaRCPper: 4.00: [IaRC4c: 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]  
 04192+ RDOOS:CO00197-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04193+ COMPUTE DUALHYP 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04194+ Major System / 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04195+ Minor System / 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04196+ ROUTE RESERVOIR > 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04197+ SMD 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04198+ ROUTE RESERVOIR < 1. 0 01S-1-B 3.28 .025 No\_date 29:15 42.01 n/a .000  
 04199+ overflow < 1. 0 01S-1-B 3.28 .025 No\_date 0:00 42.00 n/a .000  
 04200+ [ModCustEd.: 547000.000000, m3\_TotDvVol=.000000, m3\_N-Ovfl=.000000]  
 04201+ RDOOS:CO00198-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04202+ CONTINUOUS STANDYD 1. 0 01S-1-B 3.28 42.01 No\_date 28:00 42.00 .735 .000  
 04203+ [LGS=.65:TIME=.65] [Iaper: 4.67:SLPP=2.0:LGDP 40.:MNP=.250:SCP=.0] [Imperious: 1.57:SLIP=.75:LGM= 380.:MNP=.013:SCI=.0]  
 04204+ iabEClipm: 4.00:IRaRCPper: 4.00: [IaRC4c: 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]  
 04205+ RDOOS:CO00199-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04206+ COMPUTE DUALHYP 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04207+ Major System / 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04208+ Minor System / 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04209+ ROUTE RESERVOIR > 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04210+ SMD 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04211+ ROUTE RESERVOIR < 1. 0 01S-1-B 3.28 .025 No\_date 29:15 42.01 n/a .000  
 04212+ overflow < 1. 0 01S-1-B 3.28 .025 No\_date 0:00 42.00 n/a .000  
 04213+ [ModCustEd.: 547000.000000, m3\_TotDvVol=.000000, m3\_N-Ovfl=.000000]  
 04214+ RDOOS:CO00200-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04215+ CONTINUOUS STANDYD 1. 0 01S-1-B 3.28 42.01 No\_date 28:00 42.00 .735 .000  
 04216+ [LGS=.65:TIME=.65] [Iaper: 4.67:SLPP=2.0:LGDP 40.:MNP=.250:SCP=.0] [Imperious: 1.57:SLIP=.75:LGM= 380.:MNP=.013:SCI=.0]  
 04217+ iabEClipm: 4.00:IRaRCPper: 4.00: [IaRC4c: 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]  
 04218+ RDOOS:CO00201-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04219+ COMPUTE DUALHYP 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04220+ Major System / 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04221+ Minor System / 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04222+ ROUTE RESERVOIR > 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04223+ SMD 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04224+ ROUTE RESERVOIR < 1. 0 01S-1-B 3.28 .025 No\_date 29:15 42.01 n/a .000  
 04225+ overflow < 1. 0 01S-1-B 3.28 .025 No\_date 0:00 42.00 n/a .000  
 04226+ [ModCustEd.: 547000.000000, m3\_TotDvVol=.000000, m3\_N-Ovfl=.000000]  
 04227+ RDOOS:CO00202-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04228+ CONTINUOUS STANDYD 1. 0 01S-1-B 3.28 42.01 No\_date 28:00 42.00 .735 .000  
 04229+ [LGS=.65:TIME=.65] [Iaper: 4.67:SLPP=2.0:LGDP 40.:MNP=.250:SCP=.0] [Imperious: 1.57:SLIP=.75:LGM= 380.:MNP=.013:SCI=.0]  
 04230+ iabEClipm: 4.00:IRaRCPper: 4.00: [IaRC4c: 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]  
 04231+ RDOOS:CO00203-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04232+ CONTINUOUS STANDYD 1. 0 01S-1-B 3.28 42.01 No\_date 28:00 42.00 .735 .000  
 04233+ [LGS=.65:TIME=.65] [Iaper: 4.67:SLPP=2.0:LGDP 40.:MNP=.250:SCP=.0] [Imperious: 1.57:SLIP=.75:LGM= 380.:MNP=.013:SCI=.0]  
 04234+ iabEClipm: 4.00:IRaRCPper: 4.00: [IaRC4c: 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]  
 04235+ RDOOS:CO00204-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04236+ COMPUTE DUALHYP 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04237+ Major System / 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04238+ Minor System / 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04239+ ROUTE RESERVOIR > 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04240+ SMD 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04241+ ROUTE RESERVOIR < 1. 0 01S-1-B 3.28 .025 No\_date 29:13 42.01 n/a .000  
 04242+ overflow < 1. 0 01S-1-B 3.28 .025 No\_date 0:00 42.00 n/a .000  
 04243+ [ModCustEd.: 547000.000000, m3\_TotDvVol=.000000, m3\_N-Ovfl=.000000]  
 04244+ RDOOS:CO00205-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04245+ CONTINUOUS STANDYD 1. 0 01S-1-B 3.28 42.01 No\_date 28:00 42.00 .735 .000  
 04246+ [LGS=.65:TIME=.65] [Iaper: 4.67:SLPP=2.0:LGDP 40.:MNP=.250:SCP=.0] [Imperious: 1.57:SLIP=.75:LGM= 380.:MNP=.013:SCI=.0]  
 04247+ iabEClipm: 4.00:IRaRCPper: 4.00: [IaRC4c: 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]  
 04248+ RDOOS:CO00206-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04249+ COMPUTE DUALHYP 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04250+ Major System / 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04251+ Minor System / 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04252+ ROUTE RESERVOIR > 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04253+ SMD 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04254+ ROUTE RESERVOIR < 1. 0 01S-1-B 3.28 .025 No\_date 29:14 42.01 n/a .000  
 04255+ overflow < 1. 0 01S-1-B 3.28 .025 No\_date 0:00 42.00 n/a .000  
 04256+ [ModCustEd.: 547000.000000, m3\_TotDvVol=.000000, m3\_N-Ovfl=.000000]  
 04257+ RDOOS:CO00207-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04258+ CONTINUOUS STANDYD 1. 0 01S-1-B 3.28 42.01 No\_date 28:00 42.00 .735 .000  
 04259+ [LGS=.65:TIME=.65] [Iaper: 4.67:SLPP=2.0:LGDP 40.:MNP=.250:SCP=.0] [Imperious: 1.57:SLIP=.75:LGM= 380.:MNP=.013:SCI=.0]  
 04260+ iabEClipm: 4.00:IRaRCPper: 4.00: [IaRC4c: 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]  
 04261+ RDOOS:CO00208-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04262+ CONTINUOUS STANDYD 1. 0 01S-1-B 3.28 42.01 No\_date 28:00 42.00 .735 .000  
 04263+ [LGS=.65:TIME=.65] [Iaper: 4.67:SLPP=2.0:LGDP 40.:MNP=.250:SCP=.0] [Imperious: 1.57:SLIP=.75:LGM= 380.:MNP=.013:SCI=.0]  
 04264+ iabEClipm: 4.00:IRaRCPper: 4.00: [IaRC4c: 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]  
 04265+ RDOOS:CO00209-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04266+ COMPUTE DUALHYP 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04267+ Major System / 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04268+ Minor System / 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04269+ ROUTE RESERVOIR > 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04270+ SMD 1. 0 01S-1-B 3.28 .421 No\_date 28:00 42.00 .000  
 04271+ ROUTE RESERVOIR < 1. 0 01S-1-B 3.28 .025 No\_date 29:15 42.01 n/a .000  
 04272+ overflow < 1. 0 01S-1-B 3.28 .025 No\_date 0:00 42.00 n/a .000  
 04273+ [ModCustEd.: 547000.000000, m3\_TotDvVol=.000000, m3\_N-Ovfl=.000000]  
 04274+ RDOOS:CO00210-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04275+ CONTINUOUS STANDYD 1. 0 01S-1-B 3.28 42.01 No\_date 28:00 42.00 .735 .000  
 04276+ [LGS=.65:TIME=.65] [Iaper: 4.67:SLPP=2.0:LGDP 40.:MNP=.250:SCP=.0] [Imperious: 1.57:SLIP=.75:LGM= 380.:MNP=.013:SCI=.0]  
 04277+ iabEClipm: 4.00:IRaRCPper: 4.00: [IaRC4c: 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]  
 04278+ RDOOS:CO00211-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04279+ CONTINUOUS STANDYD 1. 0 01W-CLAR\_MJ 3.77 .192 No\_date 28:00 37.36 .654 .000  
 04280+ ROUTE RESERVOIR > 1. 0 02W-CLAR\_MJ 3.77 .192 No\_date 28:00 37.36 .654 .000  
 04281+ overflow < 1. 0 02W-CLAR\_MJ .00 .000 No\_date 0:00 .00 n/a .000  
 04282+ [ModCustEd.: 91164.00, m3\_TotDvVol=.000000, m3\_N-Ovfl=.000000]  
 04283+ RDOOS:CO00212-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04284+ CONTINUOUS STANDYD 1. 0 01W-CLAR\_ALL 119.40 10.597 No\_date 28:05 41.22 .722 .000  
 04285+ [XWD=.65:TIME=.65] [Iaper: 4.67:SLPP=1.00:LGDP 40.:MNP=.250:SCP=.0] [Imperious: 1.57:SLIP=.75:LGM= 380.:MNP=.013:SCI=.0]  
 04286+ iabEClipm: 4.00:IRaRCPper: 4.00: [IaRC4c: 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]  
 04287+ RDOOS:CO00213-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04288+ COMPUTE DUALHYP 1. 0 01W-CLAR\_MJ 3.77 .192 No\_date 28:00 37.36 .654 .000  
 04289+ Major System / 1. 0 02W-CLAR\_MJ 3.77 .192 No\_date 28:00 37.36 .654 .000  
 04290+ Minor System / 1. 0 02W-CLAR\_MJ 3.77 .192 No\_date 28:00 37.36 .654 .000  
 04291+ ROUTE RESERVOIR > 1. 0 02W-CLAR\_MJ 3.77 .192 No\_date 28:00 37.36 .654 .000  
 04292+ overflow < 1. 0 02W-CLAR\_MJ .00 .000 No\_date 0:00 .00 n/a .000  
 04293+ [ModCustEd.: 91164.00, m3\_TotDvVol=.000000, m3\_N-Ovfl=.000000]  
 04294+ RDOOS:CO00214-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04295+ CONTINUOUS STANDYD 1. 0 01W-CLAR\_MJ 3.77 .192 No\_date 28:00 37.36 .654 .000  
 04296+ [LGS=.65:TIME=.65] [Iaper: 4.67:SLPP=2.0:LGDP 40.:MNP=.250:SCP=.0] [Imperious: 1.57:SLIP=.75:LGM= 380.:MNP=.013:SCI=.0]  
 04297+ iabEClipm: 4.00:IRaRCPper: 4.00: [IaRC4c: 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]  
 04298+ RDOOS:CO00215-----Dtnin:ID-NHYD---ARAhA-OPENKms-Tpeakdate\_bh:mm:--RVMn-R.C.--DWFcms  
 04299+ CONTINUOUS STANDYD 1. 0 01W-CLAR\_MJ 3.77 .192 No\_date 28:00 37.36 .654 .000  
 04300+ [XWD=.65:TIME=.65] [Iaper: 4.67:SLPP=2.0:LGDP 40.:MNP=.250:SCP=.0] [Imperious: 1.57:SLIP=.75:LGM= 380.:MNP=.013:SCI=.0]  
 04301+ iabEClipm: 4.00:IRaRCPper: 4.00: [IaRC4c: 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]  
 04302+ # To West Clarke Drain (south of the Jock)  
 04303+ # - To West Clarke Drain (south of the Jock)  
 04304+ # - 2020-11-30 update CLARKE Tributary Drainage Area to 121 ha based on P598(04)-11  
 04305+ # - 2020-11-30 update CLARKE Tributary Drainage Area to Major and ALL  
 04306+ # - 2020-11-30 update CLARKE Tributary Drainage Area to Major and ALL  
 04307+ # - 2020-11-30 update CLARKE Tributary Drainage Area to Major and ALL  
 04308+ # - 2020-11-30 update CLARKE Tributary Drainage Area to Major and ALL  
 04309+ # - 2020-11-30 update CLARKE Tributary Drainage Area to Major and ALL  
 04310+ # - 2020

[XINP...86-TIME=...68] \*CONTINUOUS STANDBY 1.0 01-KB-11 4.03 .584 No\_date 28:00 41.88 .733 .000

[44950...44959] [Horton parameters] :Fm= 76.20-Pc= 13.20-DCAV4=14; Fw= 00; ADD HYD / 1.0 01-KB-11-M 4.03 .584 No\_date 28:00 41.88 n/a .000

[44960...44969] [Impervious area] :IAlmp= 4.67-SLPD9+2.00-LDG= 40.-NMP= 250:SCP...[.]

[44970...44979] [Major System] / 1.0 01-KB-11-M 4.03 .584 No\_date 28:00 41.89 n/a .000

[44980...44989] [Minor System] \ 1.0 01-KB-11-M 4.03 .584 No\_date 28:00 41.89 n/a .000

[44990...44999] [MjSys2to...= 42277.00s; TotVolV0...= 00000K...N-Ovfr= 0, Totturbofr= 0.hrs]

[45000...45009] ROOS5-C0247+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[45010...45019] ADD HYD / 1.0 01-KB-11-M 4.03 .584 No\_date 28:00 41.89 n/a .000

[45020...45029] + 1.0 01-KB-11-M 4.03 .577 No\_date 28:00 41.89 n/a .000

[45030...45039] SUM+ 1.0 01-KB-11-S 4.03 .577 No\_date 28:00 41.89 n/a .000

[45040...45049] ROOS5-C0248+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[45050...45059] CONTINUOUS STANDBY 1.0 01-S18 4.99 .892 No\_date 28:00 52.49 .513 .000

[45060...45069] [XINP...93-TIME=...79] \*CONTINUOUS STANDBY 1.0 01-KB-15 2.15 .321 No\_date 28:00 47.49 .831 .000

[45070...45079] [Horton parameters] :Fm= 76.20-Pc= 13.20-DCAV4=14; Fw= 00;

[45080...45089] [Impervious area] :IAlpr= 4.67-SLPD9+2.00-LDG= 40.-NMP= 250:SCP...[.]

[45090...45099] [Infiltration area] :IAlmp= 4.57-SLPD14+0.00-LDG= 182.-NMP= 013:SCP...[.]

[45100...45109] [IaRCimp= 4.00; IaREPerp= 4.00];

[45110...45119] ROOS5-C0249+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[45120...45129] CONTINUOUS STANDBY 1.0 01-KB-15 2.15 .321 No\_date 28:00 47.49 .831 .000

[45130...45139] [XINP...93-TIME=...79] \*CONTINUOUS STANDBY 1.0 01-KB-15 2.15 .321 No\_date 28:00 47.49 .831 .000

[45140...45149] [Horton parameters] :Fm= 76.20-Pc= 13.20-DCAV4=14; Fw= 00;

[45150...45159] [Previous area] :IAlpr= 4.67-SLPD9+2.00-LDG= 40.-NMP= 250:SCP...[.]

[45160...45169] [Infiltration area] :IAlmp= 4.57-SLPD14+0.00-LDG= 182.-NMP= 013:SCP...[.]

[45170...45179] [IaRCimp= 4.00; IaREPerp= 4.00];

[45180...45189] ROOS5-C0250+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[45190...45199] COMPUTE DUALNDY / 1.0 01-KB-01B-8 31.10 .585 No\_date 28:14 20.08 n/a .000

[45200...45209] + 1.0 01-KB-01C-8 31.10 .585 No\_date 28:03 22.52 n/a .000

[45210...45219] + 1.0 01-KB-01D-8 31.10 .585 No\_date 28:05 23.43 n/a .000

[45220...45229] + 1.0 01-KB-01E-8 31.10 .585 No\_date 28:07 24.34 n/a .000

[45230...45239] + 1.0 01-KB-04B-8 6.99 .503 No\_date 27:48 49.78 n/a .000

[45240...45249] + 1.0 01-KB-04C-8 5.19 .855 No\_date 28:00 52.49 n/a .000

[45250...45259] + 1.0 01-KB-04D-8 5.19 .855 No\_date 28:02 52.49 n/a .000

[45260...45269] + 1.0 01-KB-04E-8 5.19 .855 No\_date 28:04 52.49 n/a .000

[45270...45279] + 1.0 01-KB-04F-8 2.15 .577 No\_date 28:06 47.49 n/a .000

[45280...45289] + 1.0 01-KB-04G-8 2.15 .577 No\_date 28:08 47.49 n/a .000

[45290...45299] SUM+ 1.0 01-KB-04H-8 206.72 14.564 No\_date 28:02 27.13 n/a .000

[45300...45309] ROOS5-C0251+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[45310...45319] ROUTE RESERVOIR out <> 1.0 01-KB-01P 206.72 11.746 No\_date 28:15 27.13 n/a .000

[45320...45329] + 1.0 01-KB-01P 206.72 11.746 No\_date 28:15 27.13 n/a .000

[45330...45339] overflow <> 1.0 01-KB-01P 206.72 11.746 No\_date 28:15 0.00 n/a .000

[45340...45349] [Mostly dry] / 1.0 01-KB-01P 206.72 11.746 No\_date 28:15 0.00 n/a .000

[45350...45359] ROOS5-C0252+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[45360...45369] ADD HYD / 1.0 01-KB-01P 206.72 11.746 No\_date 28:15 27.13 n/a .000

[45370...45379] remark\*Total Flows at KB first pond

[45380...45389] ROOS5-C0253+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[45390...45399] CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 50.11 .877 .000

[45400...45409] [XINP...86-TIME=...68] \*CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 50.11 .877 .000

[45410...45419] [Horton parameters] :Fm= 76.20-Pc= 13.20-DCAV4=14; Fw= 00;

[45420...45429] [Previous area] :IAlpr= 4.67-SLPD9+2.00-LDG= 40.-NMP= 250:SCP...[.]

[45430...45439] [Infiltration area] :IAlmp= 4.57-SLPD14+0.00-LDG= 182.-NMP= 013:SCP...[.]

[45440...45449] [IaRCimp= 4.00; IaREPerp= 4.00];

[45450...45459] ROOS5-C0254+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[45460...45469] COMPUTE DUALNDY / 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 50.11 n/a .000

[45470...45479] + 1.0 01-KB-01Q-7M 10.86 1.770 No\_date 28:00 50.11 n/a .000

[45480...45489] Minor System / 1.0 01-KB-03T-07M 10.86 1.770 No\_date 28:00 50.11 n/a .000

[45490...45499] [MjSys2to...= 00000K...N-Ovfr= 0, Totturbofr= 0.hrs]

[45500...45509] ROOS5-C0255+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[45510...45519] ADD HYD / 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 0.00 n/a .000

[45520...45529] + 1.0 01-KB-01Q-7M 10.86 1.770 No\_date 28:00 0.00 n/a .000

[45530...45539] SUM+ 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 0.00 n/a .000

[45540...45549] ROOS5-C0256+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[45550...45559] CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 0.00 n/a .000

[45560...45569] [XINP...86-TIME=...68] \*CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 0.00 n/a .000

[45570...45579] [Horton parameters] :Fm= 76.20-Pc= 13.20-DCAV4=14; Fw= 00;

[45580...45589] [Previous area] :IAlpr= 4.67-SLPD9+2.00-LDG= 40.-NMP= 250:SCP...[.]

[45590...45599] [Infiltration area] :IAlmp= 4.57-SLPD14+0.00-LDG= 182.-NMP= 013:SCP...[.]

[45600...45609] [IaRCimp= 4.00; IaREPerp= 4.00];

[45610...45619] ROOS5-C0257+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[45620...45629] COMPUTE DUALNDY / 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[45630...45639] + 1.0 01-KB-01Q-7M 10.86 1.770 No\_date 28:00 46.75 .818 .000

[45640...45649] Minor System / 1.0 01-KB-03T-07M 10.86 1.770 No\_date 28:00 46.75 .818 .000

[45650...45659] [MjSys2to...= 00000K...N-Ovfr= 0, Totturbofr= 0.hrs]

[45660...45669] ROOS5-C0258+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[45670...45679] CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[45680...45689] [XINP...79-TIME=...79] \*CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[45690...45699] [Horton parameters] :Fm= 76.20-Pc= 13.20-DCAV4=14; Fw= 00;

[45700...45709] [Previous area] :IAlpr= 4.67-SLPD9+2.00-LDG= 40.-NMP= 250:SCP...[.]

[45710...45719] [Infiltration area] :IAlmp= 4.57-SLPD14+0.00-LDG= 182.-NMP= 013:SCP...[.]

[45720...45729] [IaRCimp= 4.00; IaREPerp= 4.00];

[45730...45739] ROOS5-C0259+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[45740...45749] ADD HYD / 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[45750...45759] + 1.0 01-KB-01Q-7M 10.86 1.770 No\_date 28:00 46.75 .818 .000

[45760...45769] SUM+ 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[45770...45779] ROOS5-C0260+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[45780...45789] CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[45790...45799] [XINP...86-TIME=...68] \*CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[45800...45809] [Horton parameters] :Fm= 76.20-Pc= 13.20-DCAV4=14; Fw= 00;

[45810...45819] [Previous area] :IAlpr= 4.67-SLPD9+2.00-LDG= 40.-NMP= 250:SCP...[.]

[45820...45829] [Infiltration area] :IAlmp= 4.57-SLPD14+0.00-LDG= 182.-NMP= 013:SCP...[.]

[45830...45839] [IaRCimp= 4.00; IaREPerp= 4.00];

[45840...45849] ROOS5-C0261+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[45850...45859] COMPUTE DUALNDY / 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[45860...45869] + 1.0 01-KB-01Q-7M 10.86 1.770 No\_date 28:00 46.75 .818 .000

[45870...45879] Minor System / 1.0 01-KB-03T-07M 10.86 1.770 No\_date 28:00 46.75 .818 .000

[45880...45889] [MjSys2to...= 00000K...N-Ovfr= 0, Totturbofr= 0.hrs]

[45890...45899] ROOS5-C0262+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[45900...45909] CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[45910...45919] [XINP...86-TIME=...68] \*CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[45920...45929] [Horton parameters] :Fm= 76.20-Pc= 13.20-DCAV4=14; Fw= 00;

[45930...45939] [Previous area] :IAlpr= 4.67-SLPD9+2.00-LDG= 40.-NMP= 250:SCP...[.]

[45940...45949] [Infiltration area] :IAlmp= 4.57-SLPD14+0.00-LDG= 182.-NMP= 013:SCP...[.]

[45950...45959] [IaRCimp= 4.00; IaREPerp= 4.00];

[45960...45969] ROOS5-C0263+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[45970...45979] ADD HYD / 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[45980...45989] + 1.0 01-KB-01Q-7M 10.86 1.770 No\_date 28:00 46.75 .818 .000

[45990...45999] SUM+ 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46000...46009] ROOS5-C0264+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[46010...46019] CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46020...46029] [XINP...86-TIME=...68] \*CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46030...46039] [Horton parameters] :Fm= 76.20-Pc= 13.20-DCAV4=14; Fw= 00;

[46040...46049] [Previous area] :IAlpr= 4.67-SLPD9+2.00-LDG= 40.-NMP= 250:SCP...[.]

[46050...46059] [Infiltration area] :IAlmp= 4.57-SLPD14+0.00-LDG= 182.-NMP= 013:SCP...[.]

[46060...46069] [IaRCimp= 4.00; IaREPerp= 4.00];

[46070...46079] ROOS5-C0265+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[46080...46089] COMPUTE DUALNDY / 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46090...46099] + 1.0 01-KB-01Q-7M 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46100...46109] Minor System / 1.0 01-KB-03T-07M 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46110...46119] [MjSys2to...= 00000K...N-Ovfr= 0, Totturbofr= 0.hrs]

[46120...46129] ROOS5-C0266+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[46130...46139] CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46140...46149] [XINP...86-TIME=...68] \*CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46150...46159] [Horton parameters] :Fm= 76.20-Pc= 13.20-DCAV4=14; Fw= 00;

[46160...46169] [Previous area] :IAlpr= 4.67-SLPD9+2.00-LDG= 40.-NMP= 250:SCP...[.]

[46170...46179] [Infiltration area] :IAlmp= 4.57-SLPD14+0.00-LDG= 182.-NMP= 013:SCP...[.]

[46180...46189] [IaRCimp= 4.00; IaREPerp= 4.00];

[46190...46199] ROOS5-C0267+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[46200...46209] ADD HYD / 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46210...46219] + 1.0 01-KB-01Q-7M 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46220...46229] SUM+ 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46230...46239] ROOS5-C0268+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[46240...46249] CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46250...46259] [XINP...86-TIME=...68] \*CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46260...46269] [Horton parameters] :Fm= 76.20-Pc= 13.20-DCAV4=14; Fw= 00;

[46270...46279] [Previous area] :IAlpr= 4.67-SLPD9+2.00-LDG= 40.-NMP= 250:SCP...[.]

[46280...46289] [Infiltration area] :IAlmp= 4.57-SLPD14+0.00-LDG= 182.-NMP= 013:SCP...[.]

[46290...46299] [IaRCimp= 4.00; IaREPerp= 4.00];

[46300...46309] ROOS5-C0269+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[46310...46319] COMPUTE DUALNDY / 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46320...46329] + 1.0 01-KB-01Q-7M 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46330...46339] Minor System / 1.0 01-KB-03T-07M 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46340...46349] [MjSys2to...= 00000K...N-Ovfr= 0, Totturbofr= 0.hrs]

[46350...46359] ROOS5-C0270+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[46360...46369] CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46370...46379] [XINP...71-TIME=...71] \*CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46380...46389] [Horton parameters] :Fm= 76.20-Pc= 13.20-DCAV4=14; Fw= 00;

[46390...46399] [Previous area] :IAlpr= 4.67-SLPD9+2.00-LDG= 40.-NMP= 250:SCP...[.]

[46400...46409] [Infiltration area] :IAlmp= 4.57-SLPD14+0.00-LDG= 182.-NMP= 013:SCP...[.]

[46410...46419] [IaRCimp= 4.00; IaREPerp= 4.00];

[46420...46429] ROOS5-C0271+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[46430...46439] ADD HYD / 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46440...46449] + 1.0 01-KB-01Q-7M 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46450...46459] SUM+ 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46460...46469] ROOS5-C0272+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[46470...46479] CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46480...46489] [XINP...86-TIME=...68] \*CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46490...46499] [Horton parameters] :Fm= 76.20-Pc= 13.20-DCAV4=14; Fw= 00;

[46500...46509] [Previous area] :IAlpr= 4.67-SLPD9+2.00-LDG= 40.-NMP= 250:SCP...[.]

[46510...46519] [Infiltration area] :IAlmp= 4.57-SLPD14+0.00-LDG= 182.-NMP= 013:SCP...[.]

[46520...46529] [IaRCimp= 4.00; IaREPerp= 4.00];

[46530...46539] ROOS5-C0273+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[46540...46549] ADD HYD / 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46550...46559] + 1.0 01-KB-01Q-7M 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46560...46569] SUM+ 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46570...46579] ROOS5-C0274+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[46580...46589] COMPUTE DUALNDY / 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46590...46599] + 1.0 01-KB-01Q-7M 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46600...46609] Minor System / 1.0 01-KB-03T-07M 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46610...46619] [MjSys2to...= 00000K...N-Ovfr= 0, Totturbofr= 0.hrs]

[46620...46629] ROOS5-C0275+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[46630...46639] CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46640...46649] [XINP...71-TIME=...71] \*CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46650...46659] [Horton parameters] :Fm= 76.20-Pc= 13.20-DCAV4=14; Fw= 00;

[46660...46669] [Previous area] :IAlpr= 4.67-SLPD9+2.00-LDG= 40.-NMP= 250:SCP...[.]

[46670...46679] [Infiltration area] :IAlmp= 4.57-SLPD14+0.00-LDG= 182.-NMP= 013:SCP...[.]

[46680...46689] [IaRCimp= 4.00; IaREPerp= 4.00];

[46690...46699] ROOS5-C0276+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[46700...46709] ADD HYD / 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46710...46719] + 1.0 01-KB-01Q-7M 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46720...46729] SUM+ 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46730...46739] ROOS5-C0277+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[46740...46749] CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46750...46759] [XINP...86-TIME=...68] \*CONTINUOUS STANDBY 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46760...46769] [Horton parameters] :Fm= 76.20-Pc= 13.20-DCAV4=14; Fw= 00;

[46770...46779] [Previous area] :IAlpr= 4.67-SLPD9+2.00-LDG= 40.-NMP= 250:SCP...[.]

[46780...46789] [Infiltration area] :IAlmp= 4.57-SLPD14+0.00-LDG= 182.-NMP= 013:SCP...[.]

[46790...46799] [IaRCimp= 4.00; IaREPerp= 4.00];

[46800...46809] ROOS5-C0278+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[46810...46819] ADD HYD / 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46820...46829] + 1.0 01-KB-01Q-7M 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46830...46839] SUM+ 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46840...46849] ROOS5-C0279+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[46850...46859] COMPUTE DUALNDY / 1.0 01-KB-01P 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46860...46869] + 1.0 01-KB-01Q-7M 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46870...46879] Minor System / 1.0 01-KB-03T-07M 10.86 1.770 No\_date 28:00 46.75 .818 .000

[46880...46889] [MjSys2to...= 00000K...N-Ovfr= 0, Totturbofr= 0.hrs]

[46890...46899] ROOS5-C0280+/-DmIn-ID:NHND----AReAhs-QPEAKcms-TpeakDate\_bh:mm----RvNm-R.C...-DWFcms

[46900...46909



05237+ [SMIN= 33.81 : SMAX=225.43; SK= .010] ADD HYD \* 1.0 01B106-106 1.70 .638 No\_date 28:02 34.82 n/a .000

05238+ R0005:CO0167-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05239+ COMPUTE DUALHYD \* 1.0 01B106-106 1.70 .638 No\_date 28:02 34.82 n/a .000

05240+ Major System / 1.0 02B104-MJ 1.70 .638 No\_date 0:00 30 n/a .000

05241+ Minor System \ 1.0 03B104-MN 1.70 .638 No\_date 28:02 34.82 n/a .000

05242+ [MjySto=0.0000+0.0000+0.0000+0.0000+0.0000] Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05243+ R0005:CO0358-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05244+ ADD HYD \* 1.0 01B106-106 1.70 .638 No\_date 28:02 34.82 n/a .000

05245+ SMM+ 1.0 01B106-106 25.50 1.761 No\_date 28:05 34.83 n/a .000

05246+ SMM+ 1.0 01B106-106 25.50 1.761 No\_date 28:05 34.83 n/a .000

05247+ R0005:CO0169-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05248+ SAVE HYD \* 1.0 01B106-106 25.50 1.761 No\_date 28:05 34.83 n/a .000

05249+ fname:MH40\_0005

05250+ remark:Total Flows at MH40

05251+ R0005:CO0370-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05252+ ROUTE PIPE > 1.0 02B104-MJ 25.50 1.761 No\_date 28:05 34.83 n/a .000

05253+ [L/S/nw .240/.150/.013] [Vmax= 1.648:Dmax= 823] [Din= 1.85:Dused= 1.00]

05254+ [ROUTE 1.00] out< 1.0 02B104-MJ 25.50 1.698 No\_date 28:06 34.83 n/a .000

05255+ R0005:CO0371-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05256+ COMPUTE DUALHYD \* 1.0 01B106-106 1.70 .638 No\_date 28:06 34.83 n/a .000

05257+ R0005:CO0373-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05258+ ADD HYD \* 1.0 02B104-MJ 25.50 1.698 No\_date 28:06 34.83 n/a .000

05259+ SMM+ 1.0 01B106-106 1.70 .638 No\_date 28:06 34.83 n/a .000

05260+ SMM+ 1.0 01B106-106 1.70 .638 No\_date 28:06 34.83 n/a .000

05261+ R0005:CO0372-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05262+ ROUTE PIPE > 1.0 02B104-MJ 1.70 .638 No\_date 28:06 34.83 n/a .000

05263+ [ROUTE 1.00] out< 1.0 01B106-106 1.70 .638 No\_date 28:06 34.83 n/a .000

05264+ [L/S/nw .240/.150/.013] [Vmax= 1.648:Dmax= 823] [Din= 1.85:Dused= 1.00]

05265+ Minor System \ 1.0 03B104-MN 1.70 .638 No\_date 28:06 34.83 n/a .000

05266+ [MjySto= 2.20:DWfth= 2.52]

05267+ R0005:CO0373-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05268+ COMPUTE DUALHYD \* 1.0 01B106-106 2.20 .248 No\_date 28:06 38.90 .681 .000

05269+ [XIM= 57:TIMEP=.57]

05270+ [LOSS= 2 : CIN= 75.0] [ROUTE 1.00] out< 1.0 01B106-106 2.20 .248 No\_date 28:06 38.90 .681 .000

05271+ [Imprvns area: IaPer= 4.67:SLPP=1.00:LGP= 40.:MNP= 250:SCP= .0]

05272+ [Imprvns area: IaPer= 1.57:SLPP=1.00:LGP= 187.:MNP= 013:SCI= .0]

05273+ [iaECimp= 4.00:ID=MH107]

05274+ [ROUTE 1.00] out< 1.0 01B106-106 2.20 .248 No\_date 28:06 38.90 .681 .000

05275+ R0005:CO0374-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05276+ COMPUTE DUALHYD \* 1.0 01B106-106 2.20 .248 No\_date 28:06 38.90 .681 .000

05277+ Minor System \ 1.0 03B104-MN 2.20 .248 No\_date 28:06 38.90 .681 .000

05278+ Minor System \ 1.0 03B104-MN 2.20 .248 No\_date 28:06 38.90 .681 .000

05279+ R0005:CO0374-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05280+ Minor System \ 1.0 03B104-MN 2.20 .248 No\_date 28:06 38.90 .681 .000

05281+ CONTINUOUS STANDNYD 1.0 01AB .96 .130 No\_date 28:06 44.32 .776 .000

05282+ [XIM= 71:TIMEP=.71] [ROUTE 1.00] out< 1.0 01AB .96 .130 No\_date 28:06 44.32 .776 .000

05283+ [Imprvns area: IaPer= 1.57:SLPP=1.00:LGP= 186.:MNP= 013:SCI= .0]

05284+ [Imprvns area: IaPer= 4.67:SLPP=1.00:LGP= 40.:MNP= 250:SCP= .0]

05285+ [Imprvns area: IaPer= 1.57:SLPP=1.00:LGP= 186.:MNP= 013:SCI= .0]

05286+ [ROUTE 1.00] out< 1.0 01AB .96 .130 No\_date 28:06 44.32 .776 .000

05287+ [SMIN= 33.81 : SMAX=225.43; SK= .010]

05288+ R0005:CO0376-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05289+ ADD HYD \* 1.0 02B104-MJ .06 .000 No\_date 0:00 0:00 n/a .000

05290+ SMM+ 1.0 02B104-MJ .96 .130 No\_date 28:00 44.32 n/a .000

05291+ SMM+ 1.0 02B104-MJ .96 .130 No\_date 28:00 44.32 n/a .000

05292+ R0005:CO0377-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05293+ COMPUTE DUALHYD \* 1.0 01B106-106 .96 .130 No\_date 28:00 44.32 n/a .000

05294+ Minor System \ 1.0 03B104-MN .96 .130 No\_date 28:00 44.32 n/a .000

05295+ Minor System \ 1.0 03B104-MN .96 .130 No\_date 28:00 44.32 n/a .000

05296+ R0005:CO0378-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05297+ ADD HYD \* 1.0 02B104-105-106 1.70 .638 No\_date 28:06 35.27 n/a .000

05298+ SMM+ 1.0 02B104-105-106 2.20 .248 No\_date 28:06 38.90 n/a .000

05299+ SMM+ 1.0 02B104-105-106 2.20 .248 No\_date 28:06 38.90 n/a .000

05300+ SMM+ 1.0 02B104-105-106 2.20 .248 No\_date 28:06 38.90 n/a .000

05301+ SMM+ 1.0 02B104-105-106 2.20 .248 No\_date 28:06 38.90 n/a .000

05302+ SMM+ 1.0 01B106-106 1.70 .638 No\_date 28:05 35.39 n/a .000

05303+ R0005:CO0379-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05304+ SAVE HYD \* 1.0 01B106-106 1.70 .638 No\_date 28:05 35.39 n/a .000

05305+ fname:MH05\_0005

05306+ remark:Total Flows at MH05

05307+ R0005:CO0380-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05308+ \* DIVERT HYD > 1.0 01B106-106 1.00 .000 No\_date 0:00 0:00 n/a .000

05309+ diverted < 1.0 01B106-106 1.00 .000 No\_date 0:00 0:00 n/a .000

05310+ diverted < 1.0 03B105-BE 1.00 .000 No\_date 0:00 0:00 n/a .000

05311+ R0005:CO0381-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05312+ \* DIVERT HYD > 1.0 01B106-106 1.00 .000 No\_date 0:00 0:00 n/a .000

05313+ diverted < 1.0 02B105-106 25.70 6.058 No\_date 28:05 35.39 n/a .000

05314+ diverted < 1.0 02B105-106 110.61 3.005 No\_date 28:05 35.39 n/a .000

05315+ R0005:CO0382-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05316+ CONTINUOUS STANDNYD 1.0 01B106-106 1.70 .638 No\_date 28:01 34.82 .610 .000

05317+ [XIM= 41:TIMEP=.54]

05318+ [ROUTE 1.00] out< 1.0 01B106-106 1.70 .638 No\_date 28:01 34.82 .610 .000

05319+ [Imprvns area: IaPer= 4.67:SLPP=1.00:LGP= 40.:MNP= 250:SCP= .0]

05320+ [Imprvns area: IaPer= 1.57:SLPP=1.00:LGP= 211.:MNP= 013:SCI= .0]

05321+ [ROUTE 1.00] out< 1.0 01B106-106 1.70 .638 No\_date 28:01 34.82 .610 .000

05322+ [SMIN= 33.81 : SMAX=225.43; SK= .010]

05323+ R0005:CO0383-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05324+ ADD HYD \* 1.0 02B104-MJ .06 .000 No\_date 0:00 0:00 n/a .000

05325+ SMM+ 1.0 02B104-MJ 7.19 .661 No\_date 28:01 34.82 n/a .000

05326+ SMM+ 1.0 02B104-MJ 7.19 .661 No\_date 28:01 34.82 n/a .000

05327+ R0005:CO0384-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05328+ COMPUTE DUALHYD \* 1.0 01B106-106 7.19 .661 No\_date 28:01 34.82 n/a .000

05329+ Major System / 1.0 02B104-MJ 7.19 .661 No\_date 28:01 34.82 n/a .000

05330+ Major System / 1.0 02B104-MJ 7.19 .661 No\_date 28:01 34.82 n/a .000

05331+ Minor System \ 1.0 03B104-MN 7.19 .661 No\_date 28:01 34.82 n/a .000

05332+ Minor System \ 1.0 03B104-MN 7.19 .661 No\_date 28:01 34.82 n/a .000

05333+ R0005:CO0384-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05334+ ROUTE PIPE > 1.0 02B104-MJ 7.19 .661 No\_date 28:01 34.82 n/a .000

05335+ [ROUTE 1.00] out< 1.0 03B104-MN 7.19 .661 No\_date 28:01 34.82 n/a .000

05336+ [L/S/nw .100/.013/.013]

05337+ [ROUTE 1.00] out< 1.0 02B104-106A 7.19 .615 No\_date 28:05 34.89 n/a .000

05338+ [ROUTE 1.00] out< 1.0 02B104-106A 7.19 .615 No\_date 28:05 34.89 n/a .000

05339+ [ROUTE 1.00] out< 1.0 02B104-106A 7.19 .615 No\_date 28:05 34.89 n/a .000

05340+ R0005:CO0385-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05341+ COMPUTE DUALHYD \* 1.0 01B106-106 7.19 .615 No\_date 28:05 34.89 n/a .000

05342+ Minor System \ 1.0 03B104-MN 7.19 .615 No\_date 28:05 34.89 n/a .000

05343+ Minor System \ 1.0 03B104-MN 7.19 .615 No\_date 28:05 34.89 n/a .000

05344+ R0005:CO0386-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05345+ CONTINUOUS STANDNYD 1.0 01B106-106 7.19 .615 No\_date 28:05 34.89 n/a .000

05346+ [ROUTE 1.00] out< 1.0 01B106-106 7.19 .615 No\_date 28:05 34.89 n/a .000

05347+ [ROUTE 1.00] out< 1.0 01B106-106 7.19 .615 No\_date 28:05 34.89 n/a .000

05348+ [ROUTE 1.00] out< 1.0 01B106-106 7.19 .615 No\_date 28:05 34.89 n/a .000

05349+ [ROUTE 1.00] out< 1.0 01B106-106 7.19 .615 No\_date 28:05 34.89 n/a .000

05350+ R0005:CO0387-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05351+ COMPUTE DUALHYD \* 1.0 01B106-106 7.19 .615 No\_date 28:05 34.89 n/a .000

05352+ Minor System \ 1.0 03B104-MN 7.19 .615 No\_date 28:05 34.89 n/a .000

05353+ Minor System \ 1.0 03B104-MN 7.19 .615 No\_date 28:05 34.89 n/a .000

05354+ R0005:CO0388-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05355+ CONTINUOUS STANDNYD 1.0 01B106-106 7.19 .615 No\_date 28:05 34.89 n/a .000

05356+ [ROUTE 1.00] out< 1.0 01B106-106 7.19 .615 No\_date 28:05 34.89 n/a .000

05357+ [ROUTE 1.00] out< 1.0 01B106-106 7.19 .615 No\_date 28:05 34.89 n/a .000

05358+ [ROUTE 1.00] out< 1.0 01B106-106 7.19 .615 No\_date 28:05 34.89 n/a .000

05359+ R0005:CO0389-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05360+ COMPUTE DUALHYD \* 1.0 01B106-106 7.19 .615 No\_date 28:05 34.89 n/a .000

05361+ Minor System \ 1.0 03B104-MN 7.19 .615 No\_date 28:05 34.89 n/a .000

05362+ Minor System \ 1.0 03B104-MN 7.19 .615 No\_date 28:05 34.89 n/a .000

05363+ R0005:CO0390-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05364+ ADD HYD \* 1.0 02B104-106-106A 1.70 .638 No\_date 28:05 34.89 n/a .000

05365+ SMM+ 1.0 02B104-106-106A 1.70 .638 No\_date 28:05 34.89 n/a .000

05366+ SMM+ 1.0 02B104-106-106A 1.70 .638 No\_date 28:05 34.89 n/a .000

05367+ SMM+ 1.0 02B104-106-106A 1.70 .638 No\_date 28:05 34.89 n/a .000

05368+ R0005:CO0391-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05369+ COMPUTE DUALHYD \* 1.0 01B106-106 1.70 .638 No\_date 28:05 34.89 n/a .000

05370+ Minor System \ 1.0 03B104-MN 1.70 .638 No\_date 28:05 34.89 n/a .000

05371+ R0005:CO0392-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05372+ COMPUTE DUALHYD \* 1.0 01B106-106 1.70 .638 No\_date 28:05 34.89 n/a .000

05373+ Minor System \ 1.0 03B104-MN 1.70 .638 No\_date 28:05 34.89 n/a .000

05374+ Minor System \ 1.0 03B104-MN 1.70 .638 No\_date 28:05 34.89 n/a .000

05375+ Minor System \ 1.0 03B104-MN 1.70 .638 No\_date 28:05 34.89 n/a .000

05376+ R0005:CO0393-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05377+ Minor System \ 1.0 03B104-MN 1.70 .638 No\_date 28:05 34.89 n/a .000

05378+ ROUTE PIPE > 1.0 02B104-106-106A 110.61 3.005 No\_date 28:05 35.39 n/a .000

05379+ [ROUTE 1.00] out< 1.0 02B104-106-106A 110.61 3.005 No\_date 28:05 35.39 n/a .000

05380+ [ROUTE 1.00] out< 1.0 02B104-106-106A 110.61 3.005 No\_date 28:05 35.39 n/a .000

05381+ [ROUTE 1.00] out< 1.0 02B104-106-106A 110.61 3.005 No\_date 28:05 35.39 n/a .000

05382+ [ROUTE 1.00] out< 1.0 02B104-106-106A 110.61 3.005 No\_date 28:05 35.39 n/a .000

05383+ R0005:CO0394-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05384+ ADD HYD \* 1.0 01B106-106 1.21.05 3.682 No\_date 28:05 35.35 n/a .000

05385+ remark:Total Flows at MH106

05386+ R0005:CO0395-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05387+ Minor System \ 1.0 03B104-MN 1.21.05 3.682 No\_date 28:05 35.35 n/a .000

05388+ \* [ROUTE 1.00] out< 1.0 01B106-106 1.21.05 3.682 No\_date 28:05 35.35 n/a .000

05389+ [ROUTE 1.00] out< 1.0 01B106-106 1.21.05 3.682 No\_date 28:05 35.35 n/a .000

05390+ [ROUTE 1.00] out< 1.0 01B106-106 1.21.05 3.682 No\_date 28:05 35.35 n/a .000

05391+ R0005:CO0396-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05392+ Minor System \ 1.0 03B104-MN 1.21.05 3.682 No\_date 28:05 35.35 n/a .000

05393+ Minor System \ 1.0 03B104-MN 1.21.05 3.682 No\_date 28:05 35.35 n/a .000

05394+ R0005:CO0397-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05395+ Minor System \ 1.0 03B104-MN 1.21.05 3.682 No\_date 28:05 35.35 n/a .000

05396+ Minor System \ 1.0 03B104-MN 1.21.05 3.682 No\_date 28:05 35.35 n/a .000

05397+ Minor System \ 1.0 03B104-MN 1.21.05 3.682 No\_date 28:05 35.35 n/a .000

05398+ R0005:CO0398-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05399+ Minor System \ 1.0 03B104-MN 1.21.05 3.682 No\_date 28:05 35.35 n/a .000

05400+ Minor System \ 1.0 03B104-MN 1.21.05 3.682 No\_date 28:05 35.35 n/a .000

05401+ Minor System \ 1.0 03B104-MN 1.21.05 3.682 No\_date 28:05 35.35 n/a .000

05402+ Minor System \ 1.0 03B104-MN 1.21.05 3.682 No\_date 28:05 35.35 n/a .000

05403+ Minor System \ 1.0 03B104-MN 1.21.05 3.682 No\_date 28:05 35.35 n/a .000

05404+ Minor System \ 1.0 03B104-MN 1.21.05 3.682 No\_date 28:05 35.35 n/a .000

05405+ Minor System \ 1.0 03B104-MN 1.21.05 3.682 No\_date 28:05 35.35 n/a .000

05406+ Minor System \ 1.0 03B104-MN 1.21.05 3.682 No\_date 28:05 35.35 n/a .000

05407+ R0005:CO0397-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05408+ COMPUTE DUALHYD \* 1.0 01B106-106 1.21.05 3.682 No\_date 28:05 35.35 n/a .000

05409+ Minor System \ 1.0 03B104-MN 1.21.05 3.682 No\_date 28:05 35.35 n/a .000

05410+ Minor System \ 1.0 03B104-MN 1.21.05 3.682 No\_date 28:05 35.35 n/a .000

05411+ R0005:CO0398-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05412+ ADD HYD \* 1.0 02B104-106 121.05 3.682 No\_date 28:05 35.35 n/a .000

05413+ SMM+ 1.0 02B104-106 121.05 3.682 No\_date 28:05 35.35 n/a .000

05414+ SMM+ 1.0 02B104-106 121.05 3.682 No\_date 28:05 35.35 n/a .000

05415+ R0005:CO0394-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05416+ SMM+ 1.0 01B106-106 121.53 3.896 No\_date 28:05 35.52 n/a .000

05417+ R0005:CO0395-----Dtnin:ID=NHYD-----ARAhA-QPEAKms-Tpeakdate\_hh:mm:---RVM=R.C.---DFWfms

05418+ Minor System \ 1.0 03B104-MN 121.53 3.896 No\_date 28:05 35.52 n/a .000

05419+ Minor System \ 1.0 03B104-MN 121.53 3.896 No\_date 28:05 35.52 n/a .000

05420+ Minor System \ 1.0 03B104-MN 121.53 3.896 No\_date 28:05 35.52 n/a .000

05421+ Minor System \ 1.0 03B104-MN 121.53 3.896 No\_date 28:05 35.52 n/a .000

05422+ Minor System \ 1.0 03B104-MN 121.53 3.896 No\_date 28:05 35.52 n/a .000

05423+ Minor System \ 1.0 03B104-MN 121.53 3.896 No\_date 28:05 35.52 n/a .000

05424+ Minor System \ 1.0 03B104-MN 121.53 3.896 No\_date 28:05 35.52 n/a .000

05425+ Minor System \ 1.0 03B104-MN 121.53 3.896 No\_date 28:05 35.52 n/a .000

05426+ Minor System \ 1.0 03B104-MN 121.53 3.896 No\_date 28:05 35.52 n/a .000

05427+ Minor System \ 1.0 03B104-MN 121.53 3.896 No\_date 28:05 35.52 n/a .000

05428+ Minor System \ 1.0 03B104-MN 121.53 3.896 No\_date 28:05 35.52 n/a .000

05429+ Minor System \ 1.0 03B104-MN 121.53 3.896 No\_date 28:05 35.52 n/a .000

05430+ Minor System \ 1.0 03B104-MN 121.53 3.896 No\_date 28:05 35.52 n





06359+ R010:00091-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06360+ ROUTE RESERVOIR >> 1.0 02:ST7-2 .59 .075 No\_date 28:08 38.69 n/a .000  
 06361+ [Impervious area: Iaper 4.67:SLPP= .50:LGP= .250:SCP= .0] .000 .000 No\_date 0:00 .000  
 06362+ [overflow <= 1.0 03:ST20Vf .m3\_TotOfVol=.0000< m3\_Bvrf= .0 TotBvrf= .0 hrs] .000  
 06363+ [McSto:4386-1.0358e-03 .m3\_TotOfVol=.0000< m3\_Bvrf= .0 TotBvrf= .0 hrs] .000  
 06364+ R010:00092-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06365+ CONTINUOUS NASHYD 1.0 01:AT-8 60.55 .857 No\_date 28:04 22.40 n/a .000  
 06366+ [Taper 4.03:SMIN=249.82:SK= .010] .000 .000 No\_date 28:04 22.40 n/a .000  
 06367+ [InterEventTime= 12.00] .000 .000 No\_date 28:04 22.40 n/a .000  
 06368+ R010:00093-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06369+ ROUTE PIPE >> 1.0 02:O1-8 60.55 .857 No\_date 29:04 22.40 n/a .000  
 06370+ [RDT= 1.00] out< 1.0 01:OBPIPE 60.55 .852 No\_date 29:08 22.40 n/a .000  
 06371+ [Taper 4.03:SMIN=249.82:SK= .010] .000 .000 No\_date 29:08 22.40 n/a .000  
 06372+ [Vmax= 1.080:Dmax= .441] .000 .000 No\_date 29:08 22.40 n/a .000  
 06373+ [HGTW= 1.20:WHTW= 1.80] .000 .000 No\_date 29:08 22.40 n/a .000  
 06374+ R010:00094-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06375+ ADD HVD + 1.0 02:DRAIN 261.31 2.972 No\_date 28:31 17.14 n/a .000  
 06376+ [Taper 4.67:SLPP= .50:LGP= .250:SCP= .0] 1.17 .058 No\_date 28:12 29.30 n/a .000  
 06377+ [Impervious area: Iaper 4.67:SLPP= .50:LGP= .250:SCP= .0] 2.03 .058 No\_date 28:12 29.30 n/a .000  
 06378+ + 1.0 02:AI-37F .00 .000 No\_date 0:00 .000 n/a .000  
 06379+ + 1.0 02:AI-37F .00 .000 No\_date 0:00 .000 n/a .000  
 06380+ + 1.0 02:ST25T .59 .052 No\_date 28:05 38.69 n/a .000  
 06381+ [Taper 4.03:SMIN=249.82:SK= .010] .000 .000 No\_date 28:05 38.69 n/a .000  
 06382+ + 1.0 02:OBPIPE 60.55 .852 No\_date 29:08 22.40 n/a .000  
 06383+ SUM+ 1.0 02:ST-2N 326.12 3.771 No\_date 28:40 22.40 n/a .000  
 06384+ [Taper 4.03:SMIN=249.82:SK= .010] .000 .000 No\_date 28:40 22.40 n/a .000  
 06385+ CONTINUOUS STANDHYD 1.0 01:AT 3.51 .538 No\_date 28:01 50.29 .777 .000  
 06386+ [XIMP= .68:TIME= .85] .000 .000 No\_date 28:01 50.29 .777 .000  
 06387+ [InterEventTime= 12.00] .000 .000 No\_date 28:01 50.29 .777 .000  
 06388+ R010:00095-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06389+ ROUTE RESERVOIR >> 1.0 02:AT-7 3.51 .538 No\_date 28:01 50.29 n/a .000  
 06390+ [Impervious area: Iaper 4.67:SLPP= .50:LGP= .250:SCP= .0] 1.17 .058 No\_date 28:01 50.29 n/a .000  
 06391+ [Impervious area: Iaper 4.67:SLPP= .50:LGP= .250:SCP= .0] 2.03 .058 No\_date 28:01 50.29 n/a .000  
 06392+ [overflow <= 1.0 03:AT-07V 60.55 .852 No\_date 0:00 .000 n/a .000  
 06393+ [McSto:med=.167E-03 .m3\_TotOfVol=.0000< m3\_Bvrf= .0 TotBvrf= .0 hrs] .000  
 06394+ R010:00096-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06395+ CONTINUOUS STANDHYD 1.0 01:AT 3.51 .538 No\_date 28:01 50.29 .777 .000  
 06396+ [XIMP= .68:TIME= .85] .000 .000 No\_date 28:01 50.29 .777 .000  
 06397+ [InterEventTime= 12.00] .000 .000 No\_date 28:01 50.29 .777 .000  
 06398+ R010:00097-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06399+ ROUTE RESERVOIR >> 1.0 02:AT-7 3.51 .538 No\_date 28:01 50.29 n/a .000  
 06400+ [Impervious area: Iaper 4.67:SLPP= .50:LGP= .250:SCP= .0] 1.17 .058 No\_date 28:01 50.29 n/a .000  
 06401+ [Impervious area: Iaper 4.67:SLPP= .50:LGP= .250:SCP= .0] 2.03 .058 No\_date 28:01 50.29 n/a .000  
 06402+ [overflow <= 1.0 03:AT-07V 60.55 .852 No\_date 0:00 .000 n/a .000  
 06403+ R010:00098-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06404+ ROUTE RESERVOIR >> 1.0 02:AT-7 3.51 .538 No\_date 28:01 50.29 n/a .000  
 06405+ [Impervious area: Iaper 4.67:SLPP= .50:LGP= .250:SCP= .0] 1.17 .058 No\_date 28:01 50.29 n/a .000  
 06406+ [overflow <= 1.0 03:AT-07V 60.55 .852 No\_date 0:00 .000 n/a .000  
 06407+ [McSto:med=.167E-03 .m3\_TotOfVol=.0000< m3\_Bvrf= .0 TotBvrf= .0 hrs] .000  
 06408+ R010:00099-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06409+ ADD HVD + 1.0 02:ST-2N 326.12 3.771 No\_date 28:40 18.45 n/a .000  
 06410+ [Taper 4.03:SMIN=249.82:SK= .010] .000 .000 No\_date 28:40 18.45 n/a .000  
 06411+ + 1.0 02:AT-07F .00 .000 No\_date 0:00 .000 n/a .000  
 06412+ + 1.0 02:ST35T .72 .063 No\_date 28:05 38.69 n/a .000  
 06413+ + 1.0 02:OBPIPE .00 .000 No\_date 28:05 38.69 n/a .000  
 06414+ SUM+ 1.0 02:PT25T 330.34 3.914 No\_date 28:39 18.83 n/a .000  
 06415+ R010:00100-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06416+ [RDT= 1.00] out< 1.0 01:OBRAIN 330.34 3.940 No\_date 28:01 50.29 .777 .000  
 06417+ [L/S=n\_e .592 / .230 / 043] .000 .000 No\_date 28:01 50.29 .777 .000  
 06418+ [Impervious area: Iaper 4.67:SLPP= .50:LGP= .250:SCP= .0] .000 .000 No\_date 28:01 50.29 .777 .000  
 06419+ R010:00101-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06420+ CONTINUOUS NASHYD 1.0 01:ID 2.26 .046 No\_date 28:04 29.30 .453 .000  
 06421+ [Taper 4.03:SMIN=249.82:SK= .010] .000 .000 No\_date 28:04 29.30 .453 .000  
 06422+ [InterEventTime= 12.00] .000 .000 No\_date 28:04 29.30 .453 .000  
 06423+ R010:00102-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06424+ CONTINUOUS STANDHYD 1.0 01:AT 12.04 1.618 No\_date 28:04 50.29 .777 .000  
 06425+ [XIMP= .68:TIME= .85] .000 .000 No\_date 28:04 50.29 .777 .000  
 06426+ R010:00103-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06427+ [Taper 4.67:SLPP= .50:LGP= .250:SCP= .0] .000 .000 No\_date 28:04 50.29 .777 .000  
 06428+ [Impervious area: Iaper 4.67:SLPP= .50:LGP= .250:SCP= .0] .000 .000 No\_date 28:04 50.29 .777 .000  
 06429+ [overflow <= 1.0 03:AT-07V 60.55 .852 No\_date 0:00 .000 n/a .000  
 06430+ R010:00104-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06431+ CONTINUOUS NASHYD 1.0 01:ID 2.26 .046 No\_date 28:04 29.30 .453 .000  
 06432+ [Taper 4.03:SMIN=249.82:SK= .010] .000 .000 No\_date 28:04 29.30 .453 .000  
 06433+ [InterEventTime= 12.00] .000 .000 No\_date 28:04 29.30 .453 .000  
 06434+ R010:00105-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06435+ ROUTE RESERVOIR >> 1.0 02:AT-7 12.04 1.618 No\_date 28:04 50.29 n/a .000  
 06436+ [Impervious area: Iaper 4.67:SLPP= .50:LGP= .250:SCP= .0] 1.17 .058 No\_date 28:04 50.29 n/a .000  
 06437+ [overflow <= 1.0 03:AT-07V 60.55 .852 No\_date 0:00 .000 n/a .000  
 06438+ R010:00106-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06439+ CONTINUOUS STANDHYD 1.0 01:ST-7 .35 .046 No\_date 28:04 38.69 .598 .000  
 06440+ [XIMP= .68:TIME= .57] .000 .000 No\_date 28:04 38.69 .598 .000  
 06441+ R010:00107-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06442+ [Taper 4.67:SLPP= .50:LGP= .250:SCP= .0] .000 .000 No\_date 28:04 38.69 .598 .000  
 06443+ [Impervious area: Iaper 4.67:SLPP= .50:LGP= .250:SCP= .0] .000 .000 No\_date 28:04 38.69 .598 .000  
 06444+ R010:00108-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06445+ ROUTE RESERVOIR >> 1.0 02:ST-2N .35 .046 No\_date 28:04 38.69 n/a .000  
 06446+ [Impervious area: Iaper 4.67:SLPP= .50:LGP= .250:SCP= .0] 1.17 .058 No\_date 28:04 38.69 n/a .000  
 06447+ [overflow <= 1.0 03:ST40Vf .m3\_TotOfVol=.0000< m3\_Nvrf= .0 TotBvrf= .0 hrs] .000  
 06448+ R010:00109-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06449+ CONTINUOUS STANDHYD 1.0 01:ST-7 .35 .046 No\_date 28:04 38.69 .598 .000  
 06450+ [XIMP= .68:TIME= .57] .000 .000 No\_date 28:04 38.69 .598 .000  
 06451+ R010:00110-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06452+ CONTINUOUS NASHYD 1.0 01:AT 2.51 .072 No\_date 28:44 32.13 .497 .000  
 06453+ [Taper 4.67:SLPP= .50:LGP= .250:SCP= .0] .000 .000 No\_date 28:44 32.13 .497 .000  
 06454+ [Impervious area: Iaper 4.67:SLPP= .50:LGP= .250:SCP= .0] .000 .000 No\_date 28:44 32.13 .497 .000  
 06455+ R010:00101-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06456+ ROUTE RESERVOIR >> 1.0 02:AT-7 2.51 .072 No\_date 28:44 32.13 .497 .000  
 06457+ [Impervious area: Iaper 4.67:SLPP= .50:LGP= .250:SCP= .0] .000 .000 No\_date 28:44 32.13 .497 .000  
 06458+ [overflow <= 1.0 03:AT-07V 60.55 .852 No\_date 0:00 .000 n/a .000  
 06459+ R010:00112-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06460+ CONTINUOUS NASHYD 1.0 01:ID 2.26 .046 No\_date 28:04 29.30 .453 .000  
 06461+ [Taper 4.03:SMIN=249.82:SK= .010] .000 .000 No\_date 28:04 29.30 .453 .000  
 06462+ [InterEventTime= 12.00] .000 .000 No\_date 28:04 29.30 .453 .000  
 06463+ R010:00105-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06464+ CONTINUOUS NASHYD 1.0 01:ID 2.26 .046 No\_date 28:04 29.30 .453 .000  
 06465+ [Taper 4.03:SMIN=249.82:SK= .010] .000 .000 No\_date 28:04 29.30 .453 .000  
 06466+ R010:00106-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06467+ CONTINUOUS NASHYD 1.0 01:ID 2.26 .046 No\_date 28:04 29.30 .453 .000  
 06468+ [Taper 4.03:SMIN=249.82:SK= .010] .000 .000 No\_date 28:04 29.30 .453 .000  
 06469+ R010:00107-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06470+ CONTINUOUS NASHYD 1.0 01:ID 2.26 .046 No\_date 28:04 29.30 .453 .000  
 06471+ R010:00109-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06472+ ROUTE CHANNEL >> 1.0 02:ST-2N 350.31 4.213 No\_date 28:37 25.77 48 n/a .000  
 06473+ [Taper 4.03:SMIN=249.82:SK= .010] .000 .000 No\_date 28:37 25.77 48 n/a .000  
 06474+ R010:00110-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06475+ CONTINUOUS NASHYD 1.0 01:AT 350.31 4.213 No\_date 28:37 25.77 48 n/a .000  
 06476+ [Taper 4.03:SMIN=249.82:SK= .010] .000 .000 No\_date 28:37 25.77 48 n/a .000  
 06477+ R010:00111-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06478+ CONTINUOUS NASHYD 1.0 01:AT 350.31 4.213 No\_date 28:37 25.77 48 n/a .000  
 06479+ [Taper 4.03:SMIN=249.82:SK= .010] .000 .000 No\_date 28:37 25.77 48 n/a .000  
 06480+ R010:00112-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06481+ CONTINUOUS STANDHYD 1.0 01:CL 3.41 .523 No\_date 28:01 50.29 .777 .000  
 06482+ [Taper 4.03:SMIN=249.82:SK= .010] .000 .000 No\_date 28:01 50.29 .777 .000  
 06483+ R010:00108-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06484+ ADD HVD + 1.0 02:DRAIN 330.34 3.640 No\_date 29:01 18.83 n/a .000  
 06485+ [Taper 4.67:SLPP= .50:LGP= .250:SCP= .0] 1.17 .058 No\_date 28:27 50.29 n/a .000  
 06486+ [Impervious area: Iaper 4.67:SLPP= .50:LGP= .250:SCP= .0] 2.03 .058 No\_date 28:27 50.29 n/a .000  
 06487+ [overflow <= 1.0 03:OBPIPE 60.55 .852 No\_date 0:00 .000 n/a .000  
 06488+ R010:00112-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06489+ CONTINUOUS STANDHYD 1.0 01:ST-7 .45 .058 No\_date 28:00 38.69 .598 .000  
 06490+ [XIMP= .68:TIME= .57] .000 .000 No\_date 28:00 38.69 .598 .000  
 06491+ R010:00107-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06492+ CONTINUOUS NASHYD 1.0 01:ID 2.51 .072 No\_date 28:44 32.13 .497 .000  
 06493+ [Taper 4.67:SLPP= .50:LGP= .250:SCP= .0] .000 .000 No\_date 28:44 32.13 .497 .000  
 06494+ R010:00114-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06495+ ROUTE RESERVOIR >> 1.0 02:AT-7 2.51 .072 No\_date 28:44 32.13 .497 .000  
 06496+ [Impervious area: Iaper 4.67:SLPP= .50:LGP= .250:SCP= .0] .000 .000 No\_date 28:44 32.13 .497 .000  
 06497+ [overflow <= 1.0 03:AT-07V 60.55 .852 No\_date 0:00 .000 n/a .000  
 06498+ R010:00115-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06499+ CONTINUOUS NASHYD 1.0 01:AT 2.51 .072 No\_date 28:44 32.13 .497 .000  
 06500+ R010:00116-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06501+ CONTINUOUS NASHYD 1.0 01:AT 2.51 .072 No\_date 28:44 32.13 .497 .000  
 06502+ R010:00117-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06503+ CONTINUOUS NASHYD 1.0 01:AT 2.51 .072 No\_date 28:44 32.13 .497 .000  
 06504+ R010:00118-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06505+ CONTINUOUS NASHYD 1.0 01:AT 2.51 .072 No\_date 28:44 32.13 .497 .000  
 06506+ R010:00119-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06507+ CONTINUOUS NASHYD 1.0 01:AT 2.51 .072 No\_date 28:44 32.13 .497 .000  
 06508+ R010:00120-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06509+ CONTINUOUS NASHYD 1.0 01:AT 2.51 .072 No\_date 28:44 32.13 .497 .000  
 06510+ R010:00121-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06511+ CONTINUOUS NASHYD 1.0 01:AT 2.51 .072 No\_date 28:44 32.13 .497 .000  
 06512+ SUM+ 356.68 4.181 No\_date 29:15 20.87 n/a .000  
 06513+ [Taper 4.67:SLPP= .50:LGP= .250:SCP= .0] .000 .000 No\_date 29:15 20.87 n/a .000  
 06514+ CONTINUOUS NASHYD 1.0 01:ST-5 7.59 .058 No\_date 28:11 49.05 .798 .000  
 06515+ [XIMP= .68:TIME= .85] .000 .000 No\_date 28:11 49.05 .798 .000  
 06516+ R010:00122-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06517+ CONTINUOUS NASHYD 1.0 01:Area-A 66.75 6.470 No\_date 28:10 48.24 .746 .000  
 06518+ [Taper 4.67:SLPP= .50:LGP= .250:SCP= .0] .000 .000 No\_date 28:10 48.24 .746 .000  
 06519+ R010:00123-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06520+ R010:00124-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06521+ ROUTE RESERVOIR >> 1.0 02:ST-2N 7.59 .058 No\_date 28:11 49.05 n/a .000  
 06522+ [Impervious area: Iaper 4.67:SLPP= .50:LGP= .250:SCP= .0] .000 .000 No\_date 28:11 49.05 n/a .000  
 06523+ [overflow <= 1.0 03:OBPIPE 60.55 .852 No\_date 0:00 .000 n/a .000  
 06524+ R010:00125-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06525+ CONTINUOUS NASHYD 1.0 01:AT 7.59 .058 No\_date 28:11 49.05 n/a .000  
 06526+ R010:00126-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06527+ CONTINUOUS NASHYD 1.0 01:AT 7.59 .058 No\_date 28:11 49.05 n/a .000  
 06528+ R010:00127-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06529+ CONTINUOUS NASHYD 1.0 01:AT 7.59 .058 No\_date 28:11 49.05 n/a .000  
 06530+ R010:00128-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06531+ CONTINUOUS NASHYD 1.0 01:AT 7.59 .058 No\_date 28:11 49.05 n/a .000  
 06532+ R010:00129-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06533+ remark:SSAOUT\_0100 R010:00129-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06534+ CONTINUOUS NASHYD 1.0 01:Area-A 66.75 6.470 No\_date 28:10 48.24 .746 .000  
 06535+ [Taper 4.67:SLPP= .50:LGP= .250:SCP= .0] .000 .000 No\_date 28:10 48.24 .746 .000  
 06536+ R010:00130-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06537+ CONTINUOUS NASHYD 1.0 01:Area-A 66.75 6.470 No\_date 28:10 48.24 .746 .000  
 06538+ [Taper 4.67:SLPP= .50:LGP= .250:SCP= .0] .000 .000 No\_date 28:10 48.24 .746 .000  
 06539+ R010:00131-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06540+ CONTINUOUS NASHYD 1.0 01:Area-A 66.75 6.470 No\_date 28:10 48.24 .746 .000  
 06541+ R010:00132-----> Dtnin-ID:NHYD-----> AREAh-APEAKms-TpeakData\_hh:mm:-->RVn=R.C.-->DFWcmcs  
 06542+ CONTINUOUS NASHYD 1.0 01:Area-A 66.75 6.470 No\_date 28:10 48.24 .746 .000  
 065

06733+ + 1.0 02:S-1-D2R 18.67 .163 No\_date 29:23 48.63 n/a .000  
06734+ + 1.0 02:S-1-B3R 6.75 .060 No\_date 29:16 48.93 n/a .000  
06735+ + 1.0 02:S-1-B3R 0.00 .000 No\_date 0:00 n/a .000  
06736+ + 1.0 02:S-1-B3R 0.00 .000 No\_date 0:00 n/a .000  
06737+ + 1.0 01:SM-N 53577.82 86.110 No\_date 33:41 22.63 n/a .000  
06738+ R010:CO0156-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06739+ SAVE HYD 1.0 01:SM-N 53577.82 86.110 No\_date 33:41 22.63 n/a .000  
06740+ remark:Total Flows at 0 keefe Drain.  
06741+ remark:Total Flows at 0 keefe Drain.  
06742+ # Hydrograph from Node 0keefe routed to Node at Foster Drain  
06743+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 6215  
06744+ # DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06745+ ROUTE CHANNEL -> 1.0 02:S-1-DRB 53577.82 86.110 No\_date 33:41 22.63 n/a .000  
06746+ [ROT: 1.00] out< 1.0 01:SM-NFO 53577.82 86.110 No\_date 34:07 22.63 n/a .000  
06747+ [ROT: 1.00] out< 1.0 01:SM-NFO 53577.82 86.110 No\_date 34:07 22.63 n/a .000  
06748+ [Vmax= 1.104-Dmax: 2.868]  
06749+ \*\*\*\*\*  
06750+ \*\*\*\*\*  
06751+ \*\*\*\*\*  
06752+ \*\*\*\*\*  
06753+ # Catchment 8-1  
06754+ # To Foster ditch (north of the Jock)  
06755+ # - Partially developed (medium density) remaining agricultural  
06756+ # - 2020-12-01 decreasing Foster drainage area from (373 HA) to (307.98 HA) after increasing Koeefe drainage area to (5  
06757+ # - 2021-02-12 update Foster drainage area to 325.44 ha as measured from QGIS  
06758+ # - 2021-02-12 update Foster drainage area to 325.44 ha as measured from QGIS  
06759+ R010:CO0158-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06760+ CONTINUOUS STANDYND 1.0 01:POSTER 325.44 22.870 No\_date 28:13 43.99 .680 .000  
06761+ [ROT: 1.00] out< 1.0 01:SM-NFO 53577.82 86.110 No\_date 33:41 22.63 n/a .000  
06762+ [L00S= 2 CNM: 74.0]  
06763+ [Pervious area: Iaper: 4.67-SLPP= .50;LGP= 40.-NMP= .250;SCP= .0]  
06764+ [Impervious area: IAlmp= 1.57-SLPL= .50;LGI= 699.-NM1= .013;SCI= .0]  
06765+ [iakECimp: 4.00; iareCper: 4.00]  
06766+ [SMN= 36.67; SMAX=244.49; SK= .010]  
06767+ \*\*\*\*\*  
06768+ # Foster Pond  
06769+ # Rainfall measured assuming 400mm/ha in 24 hours for quality control  
06770+ # from the MSH for the next coordinates  
06771+ # from the MSH for the next coordinates  
06772+ R010:CO0159-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06773+ [ROT: 1.00] out< 1.0 01:POSTER 325.44 22.870 No\_date 28:13 43.99 .680 .000  
06774+ ROUTE RESERVOIR -> 1.0 02:POSTER 325.44 22.870 No\_date 28:13 43.99 .680 .000  
06775+ out< 1.0 01:PO-FDR 325.44 6.061 No\_date 29:06 43.99 .680 .000  
06776+ overlap <= 1.0 01:PO-FDR 325.44 6.061 No\_date 29:06 43.99 .680 .000  
06777+ [MgCoSed=.5682E-01 m3, TtotVol=.0000E+00 m3, N-Ovf= 0, TotDurfv= 0, hrs]=  
06778+ ADD HYD 1.0 02:PO-FDR 325.44 6.061 No\_date 29:06 43.99 .680 .000  
06779+ [ROT: 1.00] out< 1.0 02:PO-FDR 325.44 6.061 No\_date 29:06 43.99 .680 .000  
06780+ [SP= 0.00, No\_date 0:00 n/a .000]  
06781+ \*\*\*\*\*  
06782+ R010:CO0160-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06783+ CONFIRMATION STANDYND 1.0 01:W-CLAR-BRA 73.21 7.523 No\_date 28:05 47.94 .741 .000  
06784+ [XIMP= 55-TIMP= .55]  
06785+ [ROT: 1.00] out< 1.0 01:W-CLAR-BRA 73.21 7.523 No\_date 28:05 47.94 .741 .000  
06786+ [L00S= 2 CNM: 65]  
06787+ [Pervious area: Iaper: 4.67-SLPP= .50;LGP= 40.-NMP= .250;SCP= .0]  
06788+ [Impervious area: IAlmp= 1.57-SLPL= .50;LGI= 699.-NM1= .013;SCI= .0]  
06789+ [iakECimp: 4.00; iareCper: 4.00]  
06790+ [SMN= 31.15; SMAX=244.49; SK= .010]  
06791+ R010:CO0162-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06792+ ROUTE RESERVOIR -> 1.0 02:W-CLAR-BRA 73.29 7.523 No\_date 28:05 43.99 .n/a .000  
06793+ out< 1.0 01:PO-FDR 73.29 1.000 No\_date 29:06 47.94 .741 .000  
06794+ overlap <= 1.0 01:PO-FDR 73.29 1.000 No\_date 29:06 47.94 .741 .000  
06795+ [MgCoSed=.1341E+00 m3, TtotVol=.0000E+00 m3, N-Ovf= 0, TotDurfv= 0, hrs]=  
06796+ \*\*\*\*\*  
06797+ CONTINUOUS STANDYND 1.0 01:S-1-PO-D2 4.94 .594 No\_date 28:01 43.99 .469 .000  
06798+ [ROT: 1.00] out< 1.0 01:S-1-PO-D2 4.94 .594 No\_date 28:01 43.99 .469 .000  
06799+ [L00S= 2 CNM: 65]  
06800+ [Pervious area: Iaper: 4.67-SLPP= .50;LGP= 40.-NMP= .250;SCP= .0]  
06801+ [Impervious area: IAlmp= 1.57-SLPL= .50;LGI= 181.-NM1= .013;SCI= .0]  
06802+ [iakECimp: 4.00; iareCper: 4.00]  
06803+ [SMN= 36.67; SMAX=244.49; SK= .010]  
06804+ R010:CO0164-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06805+ CONFIRMATION STANDYND 1.0 01:POSTER 325.44 22.870 No\_date 28:01 43.99 .680 .000  
06806+ Major System / 1.0 02:S-1-PO-D2 4.94 .594 No\_date 28:01 43.99 .680 .000  
06807+ Minor System / 1.0 03:S-1-PO-D2 4.94 .598 No\_date 27:51 44.18 n/a .000  
06808+ [ROT: 1.00] out< 1.0 03:S-1-PO-D2 4.94 .598 No\_date 27:51 44.18 n/a .000  
06809+ R010:CO0165-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06810+ ADD HYD 1.0 01:S-1-PO-D2 4.94 .598 No\_date 27:51 44.18 n/a .000  
06811+ [ROT: 1.00] out< 1.0 01:S-1-PO-D2 4.94 .598 No\_date 27:51 44.18 n/a .000  
06812+ SUM+ 1.0 01:S-1-PO-D2 4.94 .598 No\_date 27:51 44.18 n/a .000  
06813+ R010:CO0166-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06814+ CONFIRMATION STANDYND 1.0 01:W-CLAR-BRA 73.21 7.523 No\_date 28:05 47.94 .741 .000  
06815+ [XIMP= 55-TIMP= .55]  
06816+ [ROT: 1.00] out< 1.0 01:W-CLAR-BRA 73.21 7.523 No\_date 28:05 47.94 .741 .000  
06817+ [L00S= 2 CNM: 65]  
06818+ [Pervious area: Iaper: 4.67-SLPP= .50;LGP= 40.-NMP= .250;SCP= .0]  
06819+ [Impervious area: IAlmp= 1.57-SLPL= .50;LGI= 699.-NM1= .013;SCI= .0]  
06820+ [iakECimp: 4.00; iareCper: 4.00]  
06821+ [SMN= 33.81; SMAX=244.49; SK= .010]  
06822+ \*\*\*\*\*  
06823+ R010:CO0167-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06824+ ROUTE RESERVOIR -> 1.0 02:W-CLAR-BRA 73.29 7.523 No\_date 28:05 43.99 .n/a .000  
06825+ out< 1.0 01:PO-FDR 73.29 1.000 No\_date 29:06 47.94 .741 .000  
06826+ overlap <= 1.0 01:PO-FDR 73.29 1.000 No\_date 29:06 47.94 .741 .000  
06827+ [MgCoSed=.1341E+00 m3, TtotVol=.0000E+00 m3, N-Ovf= 0, TotDurfv= 0, hrs]=  
06828+ \*\*\*\*\*  
06829+ CONTINUOUS STANDYND 1.0 01:S-1-PO-D2 4.94 .594 No\_date 28:01 43.99 .469 .000  
06830+ [ROT: 1.00] out< 1.0 01:S-1-PO-D2 4.94 .594 No\_date 28:01 43.99 .469 .000  
06831+ [L00S= 2 CNM: 65]  
06832+ [Pervious area: Iaper: 4.67-SLPP= .50;LGP= 40.-NMP= .250;SCP= .0]  
06833+ [Impervious area: IAlmp= 1.57-SLPL= .50;LGI= 181.-NM1= .013;SCI= .0]  
06834+ [iakECimp: 4.00; iareCper: 4.00]  
06835+ [SMN= 33.81; SMAX=244.49; SK= .010]  
06836+ \*\*\*\*\*  
06837+ R010:CO0168-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06838+ CONFIRMATION STANDYND 1.0 01:POSTER 325.44 22.870 No\_date 28:01 43.99 .680 .000  
06839+ Major System / 1.0 02:S-1-PO-D2 4.94 .594 No\_date 28:01 43.99 .680 .000  
06840+ Minor System / 1.0 03:S-1-PO-D2 4.94 .598 No\_date 27:51 44.18 n/a .000  
06841+ [ROT: 1.00] out< 1.0 03:S-1-PO-D2 4.94 .598 No\_date 27:51 44.18 n/a .000  
06842+ R010:CO0169-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06843+ ADD HYD 1.0 01:S-1-PO-D2 4.94 .598 No\_date 27:51 44.18 n/a .000  
06844+ [ROT: 1.00] out< 1.0 01:S-1-PO-D2 4.94 .598 No\_date 27:51 44.18 n/a .000  
06845+ ROUTE RESERVOIR -> 1.0 02:S-1-PO-D2 4.94 .598 No\_date 28:01 43.99 .680 .000  
06846+ out< 1.0 01:PO-FDR 4.94 .598 No\_date 29:06 47.94 .741 .000  
06847+ overlap <= 1.0 01:PO-FDR 4.94 .598 No\_date 29:06 47.94 .741 .000  
06848+ [MgCoSed=.1341E+00 m3, TtotVol=.0000E+00 m3, N-Ovf= 0, TotDurfv= 0, hrs]=  
06849+ \*\*\*\*\*  
06850+ R010:CO0170-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06851+ CONFIRMATION STANDYND 1.0 01:S-1-PO-D2 4.94 .594 No\_date 28:01 43.99 .469 .000  
06852+ [ROT: 1.00] out< 1.0 01:S-1-PO-D2 4.94 .594 No\_date 28:01 43.99 .469 .000  
06853+ [L00S= 2 CNM: 65]  
06854+ [Pervious area: Iaper: 4.67-SLPP= .50;LGP= 40.-NMP= .250;SCP= .0]  
06855+ [Impervious area: IAlmp= 1.57-SLPL= .50;LGI= 181.-NM1= .013;SCI= .0]  
06856+ [iakECimp: 4.00; iareCper: 4.00]  
06857+ [SMN= 33.81; SMAX=244.49; SK= .010]  
06858+ \*\*\*\*\*  
06859+ R010:CO0171-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06860+ COMPUTE DUALHYD / 1.0 01:S-1-PO-D1 5.11 .702 No\_date 28:00 48.24 .n/a .000  
06861+ out< 1.0 01:S-1-PO-D1 5.11 .702 No\_date 29:06 47.94 .741 .000  
06862+ overlap <= 1.0 01:S-1-PO-D1 5.11 .702 No\_date 29:06 47.94 .741 .000  
06863+ R010:CO0172-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06864+ ROUTE RESERVOIR -> 1.0 01:S-1-PO-D1 5.11 .605 No\_date 27:57 48.27 n/a .000  
06865+ out< 1.0 01:S-1-PO-D1 5.11 .605 No\_date 28:07 48.27 n/a .000  
06866+ overlap <= 1.0 01:S-1-PO-D1 5.11 .605 No\_date 28:07 48.27 n/a .000  
06867+ [MgCoSed=.1341E+00 m3, TtotVol=.0000E+00 m3, N-Ovf= 0, TotDurfv= 0, hrs]=  
06868+ \*\*\*\*\*  
06869+ R010:CO0173-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06870+ ROUTE RESERVOIR -> 1.0 02:S-1-PO-D1 5.11 .605 No\_date 27:57 48.27 n/a .000  
06871+ out< 1.0 01:PO-FDR 5.11 .605 No\_date 29:06 47.94 .741 .000  
06872+ overlap <= 1.0 01:PO-FDR 5.11 .605 No\_date 29:06 47.94 .741 .000  
06873+ [MgCoSed=.1341E+00 m3, TtotVol=.0000E+00 m3, N-Ovf= 0, TotDurfv= 0, hrs]=  
06874+ \*\*\*\*\*  
06875+ R010:CO0174-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06876+ ADD HYD 1.0 01:S-1-PO-D1 5.11 .605 No\_date 27:57 48.27 n/a .000  
06877+ [ROT: 1.00] out< 1.0 01:S-1-PO-D1 5.11 .605 No\_date 27:57 48.27 n/a .000  
06878+ [L00S= 2 CNM: 65]  
06879+ [Pervious area: Iaper: 4.67-SLPP= .50;LGP= 40.-NMP= .250;SCP= .0]  
06880+ [Impervious area: IAlmp= 1.57-SLPL= .50;LGI= 181.-NM1= .013;SCI= .0]  
06881+ [iakECimp: 4.00; iareCper: 4.00]  
06882+ [SMN= 33.81; SMAX=244.49; SK= .010]  
06883+ \*\*\*\*\*  
06884+ R010:CO0175-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06885+ CONFIRMATION STANDYND 1.0 01:POSTER 325.44 22.870 No\_date 28:00 48.24 .746 .000  
06886+ Major System / 1.0 02:S-1-PO-D1 5.11 .605 No\_date 28:00 48.24 .746 .000  
06887+ Minor System / 1.0 03:S-1-PO-D1 5.11 .605 No\_date 28:07 48.27 n/a .000  
06888+ [ROT: 1.00] out< 1.0 03:S-1-PO-D1 5.11 .605 No\_date 28:07 48.27 n/a .000  
06889+ R010:CO0176-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06890+ ADD HYD 1.0 01:S-1-PO-D1 5.11 .605 No\_date 27:57 48.27 n/a .000  
06891+ [ROT: 1.00] out< 1.0 01:S-1-PO-D1 5.11 .605 No\_date 27:57 48.27 n/a .000  
06892+ overlap <= 1.0 01:S-1-PO-D1 5.11 .605 No\_date 27:57 48.27 n/a .000  
06893+ [MgCoSed=.1341E+00 m3, TtotVol=.0000E+00 m3, N-Ovf= 0, TotDurfv= 0, hrs]=  
06894+ \*\*\*\*\*  
06895+ R010:CO0177-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06896+ CONFIRMATION STANDYND 1.0 01:POSTER 325.44 22.870 No\_date 28:00 48.24 .746 .000  
06897+ Major System / 1.0 02:S-1-PO-D1 5.11 .605 No\_date 28:00 48.24 .746 .000  
06898+ Minor System / 1.0 03:S-1-PO-D1 5.11 .605 No\_date 28:07 48.27 n/a .000  
06899+ [ROT: 1.00] out< 1.0 03:S-1-PO-D1 5.11 .605 No\_date 28:07 48.27 n/a .000  
06900+ R010:CO0178-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06901+ ADD HYD 1.0 01:S-1-PO-D1 5.11 .605 No\_date 27:57 48.27 n/a .000  
06902+ [ROT: 1.00] out< 1.0 01:S-1-PO-D1 5.11 .605 No\_date 27:57 48.27 n/a .000  
06903+ overlap <= 1.0 01:S-1-PO-D1 5.11 .605 No\_date 27:57 48.27 n/a .000  
06904+ [MgCoSed=.1341E+00 m3, TtotVol=.0000E+00 m3, N-Ovf= 0, TotDurfv= 0, hrs]=  
06905+ \*\*\*\*\*  
06906+ R010:CO0179-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06907+ CONFIRMATION STANDYND 1.0 01:POSTER 325.44 22.870 No\_date 28:00 48.24 .746 .000  
06908+ Major System / 1.0 02:S-1-PO-D1 5.11 .605 No\_date 28:00 48.24 .746 .000  
06909+ Minor System / 1.0 03:S-1-PO-D1 5.11 .605 No\_date 28:07 48.27 n/a .000  
06910+ [ROT: 1.00] out< 1.0 03:S-1-PO-D1 5.11 .605 No\_date 28:07 48.27 n/a .000  
06911+ R010:CO0180-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06912+ ADD HYD 1.0 01:S-1-PO-D1 5.11 .605 No\_date 27:57 48.27 n/a .000  
06913+ [ROT: 1.00] out< 1.0 01:S-1-PO-D1 5.11 .605 No\_date 27:57 48.27 n/a .000  
06914+ overlap <= 1.0 01:S-1-PO-D1 5.11 .605 No\_date 27:57 48.27 n/a .000  
06915+ [MgCoSed=.1341E+00 m3, TtotVol=.0000E+00 m3, N-Ovf= 0, TotDurfv= 0, hrs]=  
06916+ \*\*\*\*\*  
06917+ R010:CO0181-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06918+ CONTINUOUS STANDYND 1.0 01:S-1-PO-D1 5.27 .781 No\_date 28:01 45.83 .554 .000  
06919+ [ROT: 1.00] out< 1.0 01:S-1-PO-D1 5.27 .781 No\_date 28:01 45.83 .554 .000  
06920+ overlap <= 1.0 01:S-1-PO-D1 5.27 .781 No\_date 28:01 45.83 .554 .000  
06921+ [MgCoSed=.1341E+00 m3, TtotVol=.0000E+00 m3, N-Ovf= 0, TotDurfv= 0, hrs]=  
06922+ \*\*\*\*\*  
06923+ R010:CO0182-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06924+ CONFIRMATION STANDYND 1.0 01:POSTER 325.44 22.870 No\_date 28:00 48.24 .746 .000  
06925+ Major System / 1.0 02:S-1-DRB 5.27 .672 No\_date 27:58 45.92 n/a .000  
06926+ Minor System / 1.0 03:S-1-DRB 5.27 .672 No\_date 27:58 45.92 n/a .000  
06927+ [ROT: 1.00] out< 1.0 03:S-1-DRB 5.27 .672 No\_date 27:58 45.92 n/a .000  
06928+ overlap <= 1.0 03:S-1-DRB 5.27 .672 No\_date 27:58 45.92 n/a .000  
06929+ [MgCoSed=.1341E+00 m3, TtotVol=.0000E+00 m3, N-Ovf= 0, TotDurfv= 0, hrs]=  
06930+ \*\*\*\*\*  
06931+ R010:CO0183-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06932+ CONFIRMATION STANDYND 1.0 01:POSTER 325.44 22.870 No\_date 28:00 48.24 .746 .000  
06933+ Major System / 1.0 02:S-1-DRB 5.27 .672 No\_date 28:00 48.24 .746 .000  
06934+ Minor System / 1.0 03:S-1-DRB 5.27 .672 No\_date 28:07 45.92 n/a .000  
06935+ [ROT: 1.00] out< 1.0 03:S-1-DRB 5.27 .672 No\_date 28:07 45.92 n/a .000  
06936+ overlap <= 1.0 03:S-1-DRB 5.27 .672 No\_date 28:07 45.92 n/a .000  
06937+ [MgCoSed=.1341E+00 m3, TtotVol=.0000E+00 m3, N-Ovf= 0, TotDurfv= 0, hrs]=  
06938+ \*\*\*\*\*  
06939+ R010:CO0184-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06940+ CONFIRMATION STANDYND 1.0 01:POSTER 325.44 22.870 No\_date 28:00 48.24 .746 .000  
06941+ Major System / 1.0 02:S-1-DRB 5.27 .672 No\_date 28:00 48.24 .746 .000  
06942+ Minor System / 1.0 03:S-1-DRB 5.27 .672 No\_date 28:07 45.92 n/a .000  
06943+ [ROT: 1.00] out< 1.0 03:S-1-DRB 5.27 .672 No\_date 28:07 45.92 n/a .000  
06944+ overlap <= 1.0 03:S-1-DRB 5.27 .672 No\_date 28:07 45.92 n/a .000  
06945+ [MgCoSed=.1341E+00 m3, TtotVol=.0000E+00 m3, N-Ovf= 0, TotDurfv= 0, hrs]=  
06946+ \*\*\*\*\*  
06947+ R010:CO0185-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06948+ CONFIRMATION STANDYND 1.0 01:S-1-A 75.88 1.915 No\_date 28:36 26.85 .415 .000  
06949+ [ROT: 1.00] out< 1.0 01:S-1-A 75.88 1.915 No\_date 28:36 26.85 .415 .000  
06950+ overlap <= 1.0 01:S-1-A 75.88 1.915 No\_date 28:36 26.85 .415 .000  
06951+ [Morton parameters: F= 76.20F; 13.20DCNvY= 14; F= 0.00]  
06952+ [Pervious area: Iaper: 4.67-SLPP= .2.00-LGP= 40.-NMP= .250;SCP= .0]  
06953+ [Impervious area: IAlmp= 1.57-SLPL= .50;LGI= 181.-NM1= .013;SCI= .0]  
06954+ [iakECimp: 4.00; iareCper: 4.00]  
06955+ [SMN= 31.15; SMAX=244.49; SK= .010]  
06956+ \*\*\*\*\*  
06957+ R010:CO0186-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06958+ CONFIRMATION STANDYND 1.0 01:S-1-A 75.88 1.915 No\_date 28:36 26.85 .415 .000  
06959+ Major System / 1.0 02:S-1-DRB 5.27 .672 No\_date 28:36 26.85 .415 .000  
06960+ Minor System / 1.0 03:S-1-DRB 5.27 .672 No\_date 28:36 26.85 .415 .000  
06961+ [ROT: 1.00] out< 1.0 03:S-1-DRB 5.27 .672 No\_date 28:36 26.85 .415 .000  
06962+ overlap <= 1.0 03:S-1-DRB 5.27 .672 No\_date 28:36 26.85 .415 .000  
06963+ [MgCoSed=.1341E+00 m3, TtotVol=.0000E+00 m3, N-Ovf= 0, TotDurfv= 0, hrs]=  
06964+ \*\*\*\*\*  
06965+ R010:CO0187-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06966+ CONFIRMATION STANDYND 1.0 01:S-1-A 75.88 1.915 No\_date 28:36 26.85 .415 .000  
06967+ Major System / 1.0 02:S-1-DRB 5.27 .672 No\_date 28:36 26.85 .415 .000  
06968+ Minor System / 1.0 03:S-1-DRB 5.27 .672 No\_date 28:36 26.85 .415 .000  
06969+ [ROT: 1.00] out< 1.0 03:S-1-DRB 5.27 .672 No\_date 28:36 26.85 .415 .000  
06970+ overlap <= 1.0 03:S-1-DRB 5.27 .672 No\_date 28:36 26.85 .415 .000  
06971+ [MgCoSed=.1341E+00 m3, TtotVol=.0000E+00 m3, N-Ovf= 0, TotDurfv= 0, hrs]=  
06972+ \*\*\*\*\*  
06973+ R010:CO0188-----DtnIn-ID:NHYD----ARAhA-QPEAKms-Tpeakdate\_hh:mm---RvNm-R.C.---DWFcms  
06974+ CONFIRMATION STANDYND 1.0 01:S-1-A 75.88 1.915 No\_date 28:

07107+ R010:CO0215-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07108+ ADD HYD  
 07109+ fms ID:CLAR\_0110 1.0 01W\_CLAR 119.40 12.497 No\_date 28:05 47.94 n/a .000  
 07110+ remark:Total Flows to West Clark  
 07111+ \*  
 07112+ # West Clarke Pond 2  
 07113+ # Rating curve obtained from Barbwiren SoilNet MES modeling  
 07114+ # Tillary Dam  
 07115+ #  
 07116+ R010:CO0216-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07117+ ROUTE RESERVE > 1.0 01W\_CLAR 119.40 12.497 No\_date 28:05 47.94 n/a .000  
 07118+ out < 1.0 01W\_CLAR 119.40 12.497 No\_date 28:33 47.94 n/a .000  
 07119+ overflow < 1.0 03P2-OVW .00 .000 No\_date 0:00 .00 n/a .000  
 07120+ (Mechanics) 1.0 03P2-OVW .00 .000 No\_date 0:00 .00 n/a .000  
 07121+ #  
 07122+ R010:CO0217-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07123+ ADD HYD  
 07124+ 1.0 02S-1-01B 2.28 .029 No\_date 29:14 48.78 n/a .000  
 07125+ + 1.0 02S-1-01B 12.84 .113 No\_date 29:20 48.75 n/a .000  
 07126+ + 1.0 02S-1-01B 2.28 .029 No\_date 29:24 48.78 n/a .000  
 07127+ + 1.0 02S-1-01Bovf .00 .000 No\_date 0:00 .00 n/a .000  
 07128+ + 1.0 02MS\_P2 .00 .000 No\_date 28:33 47.94 n/a .000  
 07129+ + 1.0 01S-NC\_C 119.40 .199 No\_date 33:44 22.88 n/a .000  
 07130+ SUM+ 1.0 01S-NC 54253.89 90.199 No\_date 33:44 22.88 n/a .000  
 07131+ name: SN\_C,0010  
 07132+ remark: Total Flows before Station 577 on Rock River  
 07133+ # Channel X-Section obtained from HEC-RAS Model - Station 577  
 07134+ # Channel X-Section obtained from HEC-RAS Model - Station 577  
 07135+ # Channel X-Section obtained from HEC-RAS Model - Station 577  
 07136+ # 2021-02-25 add station 577 before station 5002. Station 577 was extracted from the HEC-RAS model T:\\PROJ\\1474-16\\Data\\HEC-RAS\\Station\\577.dwg  
 07137+ # JFSA 2021-03-02 change the slope to 0.0175s instead of 0.0259s to stabilize the model  
 07138+ R010:CO0218-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07139+ ROUTE CHANNEL > 1.0 01SN\_C 54253.89 90.199 No\_date 33:44 22.88 n/a .000  
 07140+ \* [ROT: 1.00] out: 1.0 01SN\_C 54253.89 85.563 No\_date 36:21 22.88 n/a .000  
 07141+ (Vmax: .730 Dmax: 4.478)  
 07142+ R010:CO0220-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07143+ ADD HYD  
 07144+ 1.0 02S-1-01B 25.81 .191 No\_date 36:21 22.88 n/a .000  
 07145+ + 1.0 02S-1-01B 21.67 .191 No\_date 29:23 48.83 n/a .000  
 07146+ + 1.0 02S-1-01B 1.75 .015 No\_date 29:11 48.89 n/a .000  
 07147+ + 1.0 02S-1-01B 2.03 .020 No\_date 29:24 48.83 n/a .000  
 07148+ + 1.0 02S-1-01Bovf .00 .000 No\_date 0:00 .00 n/a .000  
 07149+ + 1.0 02S-1-01Bovf .00 .000 No\_date 0:00 .00 n/a .000  
 07150+ + 1.0 02S-1-01Bovf .00 .000 No\_date 0:00 .00 n/a .000  
 07151+ SUM+ 1.0 01S-0502 54279.30 85.716 No\_date 36:21 22.88 n/a .000  
 07152+ R010:CO0221-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07153+ ADD HYD  
 07154+ 1.0 02S-1-01B 54251.89 85.563 No\_date 36:21 22.88 n/a .000  
 07155+ name: 5002\_0010  
 07156+ remark: Total Flows before Station 5002 on Rock River  
 07157+ # Hydrograph from Cedarview Road routed to Node at West Clarke Drain  
 07158+ # Channel X-Section obtained from HEC Hydraulic Model - Station 5002  
 07159+ # Hydrograph from Cedarview Road routed to Node at West Clarke Drain  
 07160+ # Channel X-Section obtained from HEC Hydraulic Model - Station 5002  
 07161+ # Hydrograph from Cedarview Road routed to Node at West Clarke Drain  
 07162+ # Channel X-Section obtained from HEC Hydraulic Model - Station 5002  
 07163+ # [ROT: 1.00] out: 1.0 01N-NC 54279.30 85.716 No\_date 36:21 22.88 n/a .000  
 07164+ (Vmax: 1.333 Dmax: 2.527)  
 07165+ R010:CO0222-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07166+ ROUTE RESERVE > 1.0 01N-NC 54279.30 85.716 No\_date 36:21 22.88 n/a .000  
 07167+ \* [ROT: 1.00] out: 1.0 01N-NC 54279.30 85.711 No\_date 36:25 22.89 n/a .000  
 07168+ (L/S/nr: 245/.055/.035)  
 07169+ R010:CO0223-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07170+ ROUTE CHANNEL > 1.0 01N-NC 54279.30 85.711 No\_date 36:25 22.89 n/a .000  
 07171+ \* [ROT: 1.00] out: 1.0 01N-NC 54279.30 85.718 No\_date 36:25 22.89 n/a .000  
 07172+ (L/S/nr: 245/.055/.035)  
 07173+ R010:CO0224-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07174+ ROUTE CHANNEL > 1.0 01N-NC 54279.30 85.718 No\_date 36:25 22.89 n/a .000  
 07175+ \* [ROT: 1.00] out: 1.0 01N-NC 54279.30 85.732 No\_date 36:17 22.89 n/a .000  
 07176+ (Vmax: 1.333 Dmax: 2.527)  
 07177+ # Hydrograph from Node West Clarke routed to Node at Kennedy - Burnett Drain  
 07178+ # Channel X-Section obtained from HEC Hydraulic Model - Station 4934  
 07179+ # Hydrograph from Kennedy-Burnett Canal  
 07180+ # Existing Kennedy-Burnett Canal Facility  
 07181+ # Rating curve obtained from TRIPKE  
 07182+ # [ROT: 1.00] out: 1.0 01N-NC 54279.30 85.736 No\_date 36:41 22.89 n/a .000  
 07183+ (L/S/nr: 1020/.050/.035)  
 07184+ (Vmax: 1.004 Dmax: 3.198)  
 07185+ R010:CO0225-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07186+ CATCHMENT\_KEN\_BU  
 07187+ # To Kennedy-Burnett Canal Facility  
 07188+ # Catchment Kennedy-Burnett Canal (north of the Jock)  
 07189+ # Medium density residential subdivision  
 07190+ #  
 07191+ # Existing Kennedy-Burnett Canal Facility  
 07192+ # Rating curve obtained from TRIPKE  
 07193+ # [ROT: 1.00] out: 1.0 01N-NC 54279.30 85.736 No\_date 36:41 22.89 n/a .000  
 07194+ (L/S/nr: 1020/.050/.035)  
 07195+ R010:CO0226-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07196+ CONTINUOUS STANDYD 1.0 01E-01A 40.82 7.138 No\_date 28:00 28:12 24.14 .379 .000  
 07197+ (XDM: 10/TIMW: 40)  
 07198+ [Horton parameters: Po: 76.20/TIMW: 13.20/DCAVY: 14. Fe: .00]  
 07199+ (Permeous area: Iaper: 4.67SLPP/2.00LDP/ 40. MNW: .250/SCP: .01)  
 07200+ (Impervious area: IaIempc: 4.00: iareoper: 1.00)  
 07201+ (Impervious area: IaIempc: 1.00: iareoper: 1.00)  
 07202+ R010:CO0227-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07203+ COMPUTE DUALHY 1.0 01K-01B 40.82 3.398 No\_date 28:12 24.14 n/a .000  
 07204+ Major System / 1.0 01K-01B-1 40.82 3.398 No\_date 28:12 24.14 n/a .000  
 07205+ Minor System / 1.0 01K-01B-1 31.10 1.580 No\_date 27:59 26.73 n/a .000  
 07206+ (MjSysSto: .6981E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07207+ ADD HYD  
 07208+ 1.0 02K-01B-1A 40.82 .000 No\_date 0:00 .00 n/a .000  
 07209+ \* 1.0 02K-01B-1A 40.82 3.398 No\_date 28:12 24.14 n/a .000  
 07210+ SUM+ 1.0 02K-01B-1A 40.82 3.398 No\_date 28:12 24.14 n/a .000  
 07211+ (MjSysSto: .6981E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07212+ R010:CO0229-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07213+ CONTINUOUS STANDYD 1.0 01E-01A 40.82 1.338 No\_date 28:00 28:00 28:12 24.14 .379 .000  
 07214+ (XDM: 10/TIMW: 40)  
 07215+ [Horton parameters: Po: 76.20/TIMW: 13.20/DCAVY: 14. Fe: .00]  
 07216+ (Permeous area: Iaper: 4.67SLPP/2.00LDP/ 40. MNW: .250/SCP: .01)  
 07217+ (Impervious area: IaIempc: 4.00: iareoper: 1.00)  
 07218+ R010:CO0230-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07219+ COMPUTE DUALHY 1.0 01K-01B 31.10 2.135 No\_date 28:00 28:00 26.73 n/a .000  
 07220+ Major System / 1.0 01K-01B-1 31.10 2.135 No\_date 28:00 28:00 26.73 n/a .000  
 07221+ Minor System / 1.0 01K-01B-1 31.10 1.580 No\_date 27:59 26.73 n/a .000  
 07222+ (MjSysSto: .8727E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07223+ R010:CO0231-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07224+ COMPUTE DUALHY 1.0 01K-01B 31.79 1.534 No\_date 28:00 28:00 26.73 n/a .000  
 07225+ Major System / 1.0 01K-01B-1 31.79 1.534 No\_date 28:00 28:00 26.73 n/a .000  
 07226+ Minor System / 1.0 01K-01B-1 31.79 1.530 No\_date 27:59 26.73 n/a .000  
 07227+ (MjSysSto: .6981E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07228+ R010:CO0232-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07229+ COMPUTE DUALHY 1.0 01K-01B 31.79 1.530 No\_date 28:00 28:00 26.73 n/a .000  
 07230+ Major System / 1.0 01K-01B-1 31.79 1.530 No\_date 28:00 28:00 26.73 n/a .000  
 07231+ Minor System / 1.0 01K-01B-1 31.79 1.530 No\_date 27:59 26.73 n/a .000  
 07232+ (MjSysSto: .6981E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07233+ R010:CO0233-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07234+ COMPUTE DUALHY 1.0 01K-01B 31.79 1.530 No\_date 28:00 28:00 26.73 n/a .000  
 07235+ Major System / 1.0 01K-01B-1 31.79 1.530 No\_date 28:00 28:00 26.73 n/a .000  
 07236+ Minor System / 1.0 01K-01B-1 31.79 1.530 No\_date 27:59 26.73 n/a .000  
 07237+ (MjSysSto: .6981E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07238+ R010:CO0234-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07239+ COMPUTE DUALHY 1.0 01K-01B 31.79 1.530 No\_date 28:00 28:00 26.73 n/a .000  
 07240+ Major System / 1.0 01K-01B-1 31.79 1.530 No\_date 28:00 28:00 26.73 n/a .000  
 07241+ Minor System / 1.0 01K-01B-1 31.79 1.530 No\_date 27:59 26.73 n/a .000  
 07242+ (MjSysSto: .6981E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07243+ R010:CO0235-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07244+ COMPUTE DUALHY 1.0 01K-01B 31.79 1.530 No\_date 28:00 28:00 26.73 n/a .000  
 07245+ CONTINUOUS STANDYD 1.0 01K-01B 40.82 7.685 No\_date 28:09 27.30 .422 .000  
 07246+ (XDM: 10/TIMW: 40)  
 07247+ [Horton parameters: Po: 76.20/TIMW: 13.20/DCAVY: 14. Fe: .00]  
 07248+ (Permeous area: Iaper: 4.67SLPP/2.00LDP/ 40. MNW: .250/SCP: .01)  
 07249+ (Impervious area: IaIempc: 4.00: iareoper: 1.00)  
 07250+ R010:CO0236-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07251+ COMPUTE DUALHY 1.0 01K-01B 40.82 7.685 No\_date 28:09 27.30 .422 .000  
 07252+ Major System / 1.0 01K-01B-1 40.82 7.685 No\_date 28:09 27.30 .422 .000  
 07253+ Minor System / 1.0 01K-01B-1 40.82 7.685 No\_date 27:59 27.30 .422 .000  
 07254+ (MjSysSto: .6981E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07255+ R010:CO0237-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07256+ COMPUTE DUALHY 1.0 01K-01B 40.82 7.685 No\_date 28:09 27.30 .422 .000  
 07257+ Major System / 1.0 01K-01B-1 40.82 7.685 No\_date 28:09 27.30 .422 .000  
 07258+ Minor System / 1.0 01K-01B-1 40.82 7.685 No\_date 27:59 27.30 .422 .000  
 07259+ (MjSysSto: .6981E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07260+ R010:CO0238-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07261+ COMPUTE DUALHY 1.0 01K-01B 40.82 7.685 No\_date 28:09 27.30 .422 .000  
 07262+ Major System / 1.0 01K-01B-1 40.82 7.685 No\_date 28:09 27.30 .422 .000  
 07263+ Minor System / 1.0 01K-01B-1 40.82 7.685 No\_date 27:59 27.30 .422 .000  
 07264+ (MjSysSto: .6981E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07265+ R010:CO0239-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07266+ COMPUTE DUALHY 1.0 01K-01B 40.82 7.685 No\_date 28:09 27.30 .422 .000  
 07267+ Major System / 1.0 01K-01B-1 40.82 7.685 No\_date 28:09 27.30 .422 .000  
 07268+ Minor System / 1.0 01K-01B-1 40.82 7.685 No\_date 27:59 27.30 .422 .000  
 07269+ (MjSysSto: .6981E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07270+ R010:CO0240-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07271+ COMPUTE DUALHY 1.0 01K-01B 40.82 7.685 No\_date 28:09 27.30 .422 .000  
 07272+ Major System / 1.0 01K-01B-1 40.82 7.685 No\_date 28:09 27.30 .422 .000  
 07273+ Minor System / 1.0 01K-01B-1 40.82 7.685 No\_date 27:59 27.30 .422 .000  
 07274+ (MjSysSto: .6981E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07275+ R010:CO0241-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07276+ COMPUTE DUALHY 1.0 01K-01B 40.82 7.685 No\_date 28:09 27.30 .422 .000  
 07277+ CONTINUOUS STANDYD 1.0 01K-01B 5.19 .983 No\_date 28:00 59.76 .924 .000  
 07278+ (XDM: 93/TIMW: 93)  
 07279+ [Horton parameters: Po: 76.20/TIMW: 13.20/DCAVY: 14. Fe: .00]  
 07280+ (Permeous area: Iaper: 4.67SLPP/2.00LDP/ 40. MNW: .250/SCP: .01)  
 07281+ (Impervious area: IaIempc: 4.00: iareoper: 1.00)  
 07282+ R010:CO0242-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07283+ COMPUTE DUALHY 1.0 01K-01B 5.19 .983 No\_date 28:00 59.76 .924 .000  
 07284+ Major System / 1.0 01K-01B-1 5.19 .983 No\_date 28:00 59.76 .924 .000  
 07285+ Minor System / 1.0 01K-01B-1 5.19 .983 No\_date 27:59 59.76 .924 .000  
 07286+ (MjSysSto: .6981E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07287+ R010:CO0243-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07288+ COMPUTE DUALHY 1.0 01K-01B 5.19 .983 No\_date 28:00 59.76 .924 .000  
 07289+ Major System / 1.0 01K-01B-1 5.19 .983 No\_date 28:00 59.76 .924 .000  
 07290+ Minor System / 1.0 01K-01B-1 5.19 .983 No\_date 27:59 59.76 .924 .000  
 07291+ (MjSysSto: .6981E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07292+ R010:CO0244-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07293+ COMPUTE DUALHY 1.0 01K-01B 5.19 .983 No\_date 28:00 59.76 .924 .000  
 07294+ Major System / 1.0 01K-01B-1 5.19 .983 No\_date 28:00 59.76 .924 .000  
 07295+ Minor System / 1.0 01K-01B-1 5.19 .983 No\_date 27:59 59.76 .924 .000  
 07296+ (MjSysSto: .6981E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07297+ R010:CO0245-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07298+ COMPUTE DUALHY 1.0 01K-01B 5.19 .983 No\_date 28:00 59.76 .924 .000  
 07299+ Major System / 1.0 01K-01B-1 5.19 .983 No\_date 28:00 59.76 .924 .000  
 07300+ Minor System / 1.0 01K-01B-1 5.19 .983 No\_date 27:59 59.76 .924 .000  
 07301+ (MjSysSto: .6981E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07302+ R010:CO0246-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07303+ COMPUTE DUALHY 1.0 01K-01B 5.19 .983 No\_date 28:00 59.76 .924 .000  
 07304+ Major System / 1.0 01K-01B-1 5.19 .983 No\_date 28:00 59.76 .924 .000  
 07305+ Minor System / 1.0 01K-01B-1 5.19 .983 No\_date 27:59 59.76 .924 .000  
 07306+ (MjSysSto: .6981E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07307+ R010:CO0247-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07308+ COMPUTE DUALHY 1.0 01K-01B 5.19 .983 No\_date 28:00 59.76 .924 .000  
 07309+ Major System / 1.0 01K-01B-1 5.19 .983 No\_date 28:00 59.76 .924 .000  
 07310+ Minor System / 1.0 01K-01B-1 5.19 .983 No\_date 27:59 59.76 .924 .000  
 07311+ (MjSysSto: .6981E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07312+ R010:CO0248-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07313+ COMPUTE DUALHY 1.0 01K-01B 5.19 .983 No\_date 28:00 59.76 .924 .000  
 07314+ Major System / 1.0 01K-01B-1 5.19 .983 No\_date 28:00 59.76 .924 .000  
 07315+ Minor System / 1.0 01K-01B-1 5.19 .983 No\_date 27:59 59.76 .924 .000  
 07316+ (MjSysSto: .6981E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07317+ R010:CO0249-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07318+ COMPUTE DUALHY 1.0 01K-01B 5.19 .983 No\_date 28:00 59.76 .924 .000  
 07319+ Major System / 1.0 01K-01B-1 5.19 .983 No\_date 28:00 59.76 .924 .000  
 07320+ Minor System / 1.0 01K-01B-1 5.19 .983 No\_date 27:59 59.76 .924 .000  
 07321+ (MjSysSto: .6981E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07322+ R010:CO0250-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07323+ COMPUTE DUALHY 1.0 01K-01B 5.19 .983 No\_date 28:00 59.76 .924 .000  
 07324+ Major System / 1.0 01K-01B-1 5.19 .983 No\_date 28:00 59.76 .924 .000  
 07325+ Minor System / 1.0 01K-01B-1 5.19 .983 No\_date 27:59 59.76 .924 .000  
 07326+ (MjSysSto: .6981E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07327+ R010:CO0251-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07328+ COMPUTE DUALHY 1.0 01K-01B 5.19 .983 No\_date 28:00 59.76 .924 .000  
 07329+ Major System / 1.0 01K-01B-1 5.19 .983 No\_date 28:00 59.76 .924 .000  
 07330+ Minor System / 1.0 01K-01B-1 5.19 .983 No\_date 27:59 59.76 .924 .000  
 07331+ (MjSysSto: .6981E-02, TotVolVnl: .0000E+00, N-Ovfl: 0, TotTurOvf: 0, hrs: 0)  
 07332+ R010:CO0252-----Dtnin-ID:NHYD---AREAh-aQPEAKms-TpeakDate\_bh:mm:---Rvnm-R.C.---DWFcms  
 07333+ COMPUTE DUALHY 1.0 01K-01B 5.19 .983 No\_date 28:00 59.76 .924 .

70481+ \* + 1.0 02:KB-P2ovz .00 .000 No\_date 0:00 .00 n/a .000  
 70482+ SUM\_ / 1.0 01:KB-Ponds .264 .24 15.083 No\_date 28:10 35.46 n/a .000  
 70483+ ADD HYD / 1.0 01:KB-Ponds .254 .24 15.083 No\_date 28:10 35.46 n/a .000  
 70484+ SAVE HYD  
 70485+ frame KB\_Ponds .00  
 70486+ remark:Total Flows at KB second pond  
 70487+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70488+ CONTINUOUS STANDYD 1.0 01:KB-16\_1 2.80 .465 No\_date 28:01 52.17 .806 .000  
 70489+ XINPMS-75:TIMEP\_75  
 70490+ [Horton parameters] Fo= 76.20FCPc\_13.20DCNv4\_14: Fw .001  
 70491+ [Previous area]: Taper: 4.67SLPP1-2.00LGPw\_40-.MNP-.250SCPw\_0.  
 70492+ [Infiltration area]: 54SLPP1-1.00LGPw\_37-.MNP-.013:SCIw\_0.  
 70493+ [iaEClipm] 4.00: iareCper .100  
 70494+ R0101:CO0277-----DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70495+ ADD HYD 1.0 02:KB-Ponds .254 .24 15.083 No\_date 28:10 35.46 n/a .000  
 70496+ ADD HYD + 1.0 02:KB-16\_1 2.80 .465 No\_date 28:01 52.17 n/a .000  
 70497+ SUM\_ / 1.0 01:KB-16\_1 2.80 .465 No\_date 28:01 52.17 n/a .000  
 70498+ R0101:CO0279-----DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70499+ ROUTE RESERVOIR 1.0 02:KB-P3 257.04 15.294 No\_date 28:09 35.64 n/a .000  
 70500+ ADD HYD / 1.0 01:KB-P3 257.04 15.294 No\_date 28:09 35.64 n/a .000  
 70501+ overlap < 1.0 03:KB-P2ovz 244.78 15.243 No\_date 28:09 35.64 n/a .000  
 70502+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70503+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70504+ ADD HYD 1.0 02:KB-P3 12.26 .051 No\_date 17:31 35.64 n/a .000  
 70505+ ADD HYD + 1.0 02:KB-P3 12.26 .051 No\_date 28:01 52.17 n/a .000  
 70506+ SUM\_ / 1.0 01:KB-16\_1 2.80 .465 No\_date 28:01 52.17 n/a .000  
 70507+ R0101:CO0281-----DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70508+ SAVE HYD 1.0 01:KB-P3 257.04 15.294 No\_date 28:09 35.64 n/a .000  
 70509+ frame KB\_Ponds .001  
 70510+ remark:Total Flows at KB third pond  
 70511+ \*\*\*\*\*  
 70512+ EXPROB Subcatchments (Kennedy-Burnett SWN Facility (118080), SWN Modeling Approach, NOVATECH Report Ju  
 70513+ \* To FRASER-CLARKE DRAIN  
 70514+ \*\*\*\*\*  
 70515+ R0101:CO0282-----DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70516+ CONTINUOUS STANDYD 1.0 01:FOC-01 8.03 1.049 No\_date 28:01 37.67 .582 .000  
 70517+ XINPMS-47:TIMEP\_47  
 70518+ [Horton parameters] Fo= 76.20FCPc\_13.20DCNv4\_14: Fw .001  
 70519+ [Previous area]: Taper: 4.67SLPP1-2.00LGPw\_40-.MNP-.250SCPw\_0.  
 70520+ [Infiltration area]: Infiltr: 1.57SLPP1-1.00LGPw\_231-.MNP-.013:SCIw\_0.  
 70521+ [iaEClipm] 4.00: iareCper .100  
 70522+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70523+ COMPUTE DUALHY 1.0 01:FOC-01 8.03 1.049 No\_date 28:01 37.67 n/a .000  
 70524+ ADD HYD / 1.0 01:FOC-01-MJ 8.03 .000 No\_date 0:00 n/a .000  
 70525+ Minor System \ 1.0 03:FOC-01-MJ 8.03 .000 No\_date 0:00 n/a .000  
 70526+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70527+ ADD HYD 1.0 02:FOC-01-MJ 8.03 .000 No\_date 0:00 n/a .000  
 70528+ ADD HYD + 1.0 02:FOC-01-MJ 8.03 .000 No\_date 0:00 n/a .000  
 70529+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70530+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70531+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70532+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70533+ [XINPMS-93:TIMEP\_93]  
 70534+ [Horton parameters] Fo= 76.20FCPc\_13.20DCNv4\_14: Fw .001  
 70535+ [Previous area]: Taper: 4.67SLPP1-2.00LGPw\_40-.MNP-.250SCPw\_0.  
 70536+ [Infiltration area]: Infiltr: 1.57SLPP1-0.00LGPw\_327-.MNP-.013:SCIw\_0.  
 70537+ [iaEClipm] 4.00: iareCper .100  
 70538+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70539+ COMPUTE DUALHY 1.0 01:FOC-01 16.05 2.930 No\_date 28:01 59.94 n/a .000  
 70540+ Major System / 1.0 02:FOC-02-MJ 16.05 2.930 No\_date 28:01 59.94 n/a .000  
 70541+ Minor System \ 1.0 03:FOC-02-MJ 16.05 2.930 No\_date 28:01 59.94 n/a .000  
 70542+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70543+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70544+ ADD HYD 1.0 02:FOC-02-MN 16.05 1.159 No\_date 27:46 59.94 n/a .000  
 70545+ ADD HYD + 1.0 02:FOC-02-MN 16.05 1.159 No\_date 27:46 59.94 n/a .000  
 70546+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70547+ CONTINUOUS STANDYD 1.0 01:FOC-02 7.37 1.130 No\_date 28:01 45.83 .708 .000  
 70548+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70549+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70550+ [Previous area]: Taper: 4.67SLPP1-2.00LGPw\_40-.MNP-.250SCPw\_0.  
 70551+ [Infiltration area]: Infiltr: 1.57SLPP1-0.01LGPw\_222-.MNP-.013:SCIw\_0.  
 70552+ [iaEClipm] 4.00: iareCper .100  
 70553+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70554+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70555+ COMPUTE DUALHY 1.0 01:FOC-02 7.37 1.130 No\_date 28:01 45.83 n/a .000  
 70556+ Major System / 1.0 02:FOC-03-MJ 16.05 1.159 No\_date 27:46 45.93 n/a .000  
 70557+ Minor System \ 1.0 03:FOC-03-MJ 16.05 1.159 No\_date 27:46 45.93 n/a .000  
 70558+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70559+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70560+ ADD HYD 1.0 02:FOC-03-MJ 16.05 .000 No\_date 0:00 n/a .000  
 70561+ ADD HYD + 1.0 02:FOC-03-MJ 16.05 .000 No\_date 0:00 n/a .000  
 70562+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70563+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70564+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70565+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70566+ ADD HYD 1.0 20:20FC-01 16.05 .000 No\_date 0:00 n/a .000  
 70567+ [Previous area]: Taper: 4.67SLPP1-2.00LGPw\_40-.MNP-.250SCPw\_0.  
 70568+ [Infiltration area]: Infiltr: 1.57SLPP1-0.00LGPw\_231-.MNP-.013:SCIw\_0.  
 70569+ [iaEClipm] 4.00: iareCper .100  
 70570+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70571+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70572+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70573+ ADD HYD 1.0 02:20FC-01 12.87 1.980 No\_date 28:01 45.83 .708 .000  
 70574+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70575+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70576+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70577+ ADD HYD 1.0 02:20FC-04 12.87 .737 .388 No\_date 27:45 45.93 n/a .000  
 70578+ ADD HYD + 1.0 01:FOC-04 12.87 .737 .388 No\_date 27:46 45.93 n/a .000  
 70579+ \*\*\*\*\*  
 70580+ # PROPOSED Subcatchments (Kennedy-Burnett SWN Facility (118080), SWN Modeling Approach, NOVATECH Report June, 2020)  
 70581+ \* To JOK DRAIN  
 70582+ \*\*\*\*\*  
 70583+ R0101:CO0294-----DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70584+ CONTINUOUS STANDYD 1.0 01:JK-01 8.24 1.257 No\_date 28:01 45.83 .708 .000  
 70585+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70586+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70587+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70588+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70589+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70590+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70591+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70592+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70593+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70594+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70595+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70596+ ADD HYD 1.0 02:JK-01-MJ 8.24 .000 No\_date 0:00 n/a .000  
 70597+ ADD HYD + 1.0 02:JK-01-MJ 8.24 .000 No\_date 0:00 n/a .000  
 70598+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70599+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70600+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70601+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70602+ [Horton parameters] Fo= 76.20FCPc\_13.20DCNv4\_14: Fw .001  
 70603+ [Previous area]: Taper: 4.67SLPP1-2.00LGPw\_40-.MNP-.250SCPw\_0.  
 70604+ [Infiltration area]: Infiltr: 1.57SLPP1-0.01LGPw\_103-.MNP-.013:SCIw\_0.  
 70605+ [iaEClipm] 4.00: iareCper .100  
 70606+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70607+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70608+ COMPUTE DUALHY 1.0 01:JK-02 .159 .264 No\_date 28:00 45.83 n/a .000  
 70609+ Major System / 1.0 02:JK-02-MJ .159 .000 No\_date 0:00 n/a .000  
 70610+ Minor System \ 1.0 03:JK-02-MJ .159 .563 No\_date 28:01 45.83 n/a .000  
 70611+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70612+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70613+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70614+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70615+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70616+ ADD HYD 1.0 02:JK-02-MJ .159 .563 No\_date 27:47 46.14 n/a .000  
 70617+ ADD HYD + 1.0 02:JK-02-MJ .159 .563 No\_date 27:48 46.14 n/a .000  
 70618+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70619+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70620+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70621+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70622+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70623+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70624+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70625+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70626+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70627+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70628+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70629+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70630+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70631+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70632+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70633+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70634+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70635+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70636+ COMPUTE DUALHY 23.61 .2700 No\_date 28:01 47.42 n/a .000  
 70637+ Major System / 1.0 02:FRASER-J .000 .000 No\_date 0:00 n/a .000  
 70638+ Minor System \ 1.0 03:FRASER-J .000 .000 No\_date 0:00 n/a .000  
 70639+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70640+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70641+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70642+ ADD HYD 21.61 .281 No\_date 27:57 47.46 n/a .000  
 70643+ ADD HYD + 1.0 02:FRASER-N 21.61 .281 No\_date 27:57 47.46 n/a .000  
 70644+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70645+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70646+ ADD HYD 1.0 02:FRASER-P 257.04 15.294 No\_date 28:09 35.64 n/a .000  
 70647+ ADD HYD + 1.0 02:FRASER-P 257.04 15.294 No\_date 28:09 35.64 n/a .000  
 70648+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70649+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70650+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70651+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70652+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70653+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70654+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70655+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70656+ frame 14241\_001  
 70657+ remark:Total Flows at Ken-Burnett outlet  
 70658+ frame KB\_Ponds .00  
 70659+ # Channel X-Section obtained from EVA Hydraulic Model - Station 4241  
 70660+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70661+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70662+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70663+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70664+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70665+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70666+ DTbin-ID:NHYD---ARAHa-QPEAKms-Tpeakdate\_bh:mm:--RvNm-R.C.--DWFcms  
 70667+ ADD HYD 1.0 02:4241-out 54658.45 85.856 No\_date 36:23 22.98 n/a .000  
 70668+ \*\*\*\*\*  
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08229+ remark:Total Flows at MH106  
 08300+ R0101:CD0040-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08301+ ROUTE PIPE / 1.0 02-MH106 119.82 1.592 No\_date 28:01 41.87 n/a .000  
 08302+ \* [ROT 1.00] out-> 1.0 01-106-107 119.82 3.962 No\_date 28:03 41.87 n/a .000  
 08303+ [L/S/nr. 122] 106.107 119.82 3.962 No\_date 28:03 41.87 n/a .000  
 08304+ [Vmax= 1.408\*Dmax 1.530]  
 08305+ [Din = 1.80\*Dused 1.86]  
 08306+ R0101:CD0040-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08307+ CONTINUOUS STANDHYD 1.0 01-A10 4.14 .416 No\_date 28:01 38.46 535 .000  
 08308+ [\*XIMP= 35\*TIME= .47]  
 08309+ # Corrigan Pond 2 C/NW  
 08310+ [Previous area: Japer= 4.67\*SLP1=0.00:LGP= 40.:NMN=.250:SCP=.01]  
 08311+ [Impervious area: JAimp= 1.57\*SLD1=1.00:LGI= 183.:MMI=.013:SCI=.01]  
 08312+ [SMIN= 33.81:SMAX=225.43: SK= .010]  
 08313+ [Din = 1.80\*Dused 1.86]  
 08314+ R0101:CD0042-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08315+ COMPUTE DUALHY / 1.0 02-A10-MJ .00 .000 No\_date 0:00 0:00 n/a .000  
 08316+ Major System < 1.0 02-A10-MJ 4.14 .310 No\_date 27:55 41.36 n/a .000  
 08317+ Minor System < 1.0 03-A10-1 4.14 .310 No\_date 27:55 41.36 n/a .000  
 08318+ [Din = 1.80\*Dused 1.86]  
 08319+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08320+ CONTINUOUS STANDHYD 1.0 01-A10 10.61 1.251 No\_date 28:01 45.36 .701 .000  
 08321+ [LGS= 2 C/N 75.0]  
 08322+ [Previous area: Japer= 4.67\*SLP1=0.00:LGP= 40.:NMN=.250:SCP=.01]  
 08323+ [Impervious area: JAimp= 1.57\*SLD1=1.00:LGI= 183.:MMI=.013:SCI=.01]  
 08324+ [SMIN= 33.81:SMAX=225.43: SK= .010]  
 08325+ [Din = 1.80\*Dused 1.86]  
 08326+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08327+ COMPUTE DUALHY / 1.0 01-A11 10.61 1.251 No\_date 28:01 45.36 .701 .000  
 08328+ Major System < 1.0 01-A11-MJ .00 .000 No\_date 0:00 0:00 n/a .000  
 08329+ Minor System < 1.0 02-A11-1 10.61 .998 No\_date 27:55 41.36 n/a .000  
 08330+ [Din = 1.80\*Dused 1.86]  
 08331+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08332+ CONTINUOUS STANDHYD 1.0 01-A12 12.29 1.385 No\_date 28:01 41.19 .637 .000  
 08333+ [LGS= 2 C/N 75.0]  
 08334+ [Previous area: Japer= 4.67\*SLP1=0.00:LGP= 40.:NMN=.250:SCP=.01]  
 08335+ [Impervious area: JAimp= 1.57\*SLD1=1.00:LGI= 183.:MMI=.013:SCI=.01]  
 08336+ [SMIN= 33.81:SMAX=225.43: SK= .010]  
 08337+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08338+ COMPUTE DUALHY / 1.0 02-A11-MJ .00 .000 No\_date 0:00 0:00 n/a .000  
 08339+ Major System < 1.0 02-A11-MJ 12.29 1.385 No\_date 27:55 41.19 .637 .000  
 08340+ Minor System < 1.0 03-A11-1 12.29 1.385 No\_date 27:55 41.19 .637 .000  
 08341+ [Din = 1.80\*Dused 1.86]  
 08342+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08343+ CONTINUOUS STANDHYD 1.0 01-A12 2.59 .368 No\_date 28:01 51.11 .790 .000  
 08344+ [LGS= 2 C/N 75.0]  
 08345+ [Previous area: Japer= 4.67\*SLP1=0.00:LGP= 40.:NMN=.250:SCP=.01]  
 08346+ [Impervious area: JAimp= 1.57\*SLD1=1.00:LGI= 183.:MMI=.013:SCI=.01]  
 08347+ [SMIN= 33.81:SMAX=225.43: SK= .010]  
 08348+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08349+ COMPUTE DUALHY / 1.0 02-A11-MJ .00 .000 No\_date 0:00 0:00 n/a .000  
 08350+ Major System < 1.0 02-A11-MJ 2.59 .368 No\_date 28:01 51.11 n/a .000  
 08351+ Minor System < 1.0 03-A11-1 2.59 .368 No\_date 27:55 41.19 n/a .000  
 08352+ [Din = 1.80\*Dused 2.00]  
 08353+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08354+ COMPUTE DUALHY / 1.0 02-A11-MJ .00 .000 No\_date 0:00 0:00 n/a .000  
 08355+ Major System < 1.0 02-A11-MJ 134.57 5.251 No\_date 28:05 42.04 n/a .000  
 08356+ Minor System < 1.0 03-A11-1 134.57 5.248 No\_date 28:06 42.04 n/a .000  
 08357+ [Din = 1.80\*Dused 2.00]  
 08358+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08359+ COMPUTE DUALHY / 1.0 02-A11-MJ .00 .000 No\_date 0:00 0:00 n/a .000  
 08360+ Major System < 1.0 02-A11-MJ 134.57 5.251 No\_date 28:05 42.04 n/a .000  
 08361+ Minor System < 1.0 03-A11-1 134.57 5.248 No\_date 28:06 42.04 n/a .000  
 08362+ [Din = 1.80\*Dused 2.00]  
 08363+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08364+ COMPUTE DUALHY / 1.0 02-A11-MJ .00 .000 No\_date 0:00 0:00 n/a .000  
 08365+ Major System < 1.0 02-A11-MJ 134.57 5.251 No\_date 28:05 42.04 n/a .000  
 08366+ Minor System < 1.0 03-A11-1 134.57 5.248 No\_date 28:06 42.04 n/a .000  
 08367+ [Din = 1.80\*Dused 2.00]  
 08368+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08369+ COMPUTE DUALHY / 1.0 02-A11-MJ .00 .000 No\_date 0:00 0:00 n/a .000  
 08370+ Major System < 1.0 02-A11-MJ 134.57 5.251 No\_date 28:05 42.04 n/a .000  
 08371+ Minor System < 1.0 03-A11-1 134.57 5.248 No\_date 28:06 42.04 n/a .000  
 08372+ [Din = 1.80\*Dused 2.00]  
 08373+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08374+ COMPUTE DUALHY / 1.0 02-A11-MJ .00 .000 No\_date 0:00 0:00 n/a .000  
 08375+ Major System < 1.0 02-A11-MJ 134.57 5.251 No\_date 28:05 42.04 n/a .000  
 08376+ Minor System < 1.0 03-A11-1 134.57 5.248 No\_date 28:06 42.04 n/a .000  
 08377+ [Din = 1.80\*Dused 2.00]  
 08378+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08379+ COMPUTE DUALHY / 1.0 02-A11-MJ .00 .000 No\_date 0:00 0:00 n/a .000  
 08380+ Major System < 1.0 02-A11-MJ 134.57 5.251 No\_date 28:05 42.04 n/a .000  
 08381+ Minor System < 1.0 03-A11-1 134.57 5.248 No\_date 28:06 42.04 n/a .000  
 08382+ [Din = 1.80\*Dused 2.00]  
 08383+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08384+ COMPUTE DUALHY / 1.0 02-A11-MJ .00 .000 No\_date 0:00 0:00 n/a .000  
 08385+ Major System < 1.0 02-A11-MJ 134.57 5.251 No\_date 28:05 42.04 n/a .000  
 08386+ Minor System < 1.0 03-A11-1 134.57 5.248 No\_date 28:06 42.04 n/a .000  
 08387+ [Din = 1.80\*Dused 2.00]  
 08388+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08389+ COMPUTE DUALHY / 1.0 02-A11-MJ .00 .000 No\_date 0:00 0:00 n/a .000  
 08390+ Major System < 1.0 02-A11-MJ 134.57 5.251 No\_date 28:05 42.04 n/a .000  
 08391+ Minor System < 1.0 03-A11-1 134.57 5.248 No\_date 28:06 42.04 n/a .000  
 08392+ [Din = 1.80\*Dused 2.00]  
 08393+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08394+ COMPUTE DUALHY / 1.0 02-A11-MJ .00 .000 No\_date 0:00 0:00 n/a .000  
 08395+ Major System < 1.0 02-A11-MJ 134.57 5.251 No\_date 28:05 42.04 n/a .000  
 08396+ Minor System < 1.0 03-A11-1 134.57 5.248 No\_date 28:06 42.04 n/a .000  
 08397+ [Din = 1.80\*Dused 2.00]  
 08398+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08399+ COMPUTE DUALHY / 1.0 02-A11-MJ .00 .000 No\_date 0:00 0:00 n/a .000  
 08400+ overlaid 1.0 03-A11-MJ .00 .000 No\_date 0:00 0:00 n/a .000  
 08401+ [M0304edc\_229890.m3,TotVol=0.000,m3,N-Ovrf=0,m3,TotSurf=0,nm,0,hz]  
 08402+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08403+ ADD HYD 1.0 02-H\_MJ 55108.86 85.828 No\_date 37:24 23.12 n/a .000  
 08404+ \* Rating curve obtained from CVM hydraulic modeling  
 08405+ [Vmax= 2.084\*Dmax 1.758]  
 08406+ [Din = 1.80\*Dused 1.86]  
 08407+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08408+ SAVV HYD 1.0 01-H\_Corri 55108.86 85.837 No\_date 37:21 23.12 n/a .000  
 08409+ name:Corri0010  
 08410+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08411+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08412+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08413+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08414+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08415+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08416+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08417+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08418+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08419+ [Vmax= 1.393\*Dmax 2.071]  
 08420+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08421+ # Catchment DESIRE  
 08422+ # - To Jock River (north of the Jock)  
 08423+ # Ruralized residential area in Desire Community  
 08424+ #  
 08425+ R0101:CD0044-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08426+ CONFIRM SPANNING 1.0 01-DESIRE 23.78 1.694 No\_date 28:03 32.93 .509 .000  
 08427+ [XIMP= 26\*TIME=.25]  
 08428+ [LOSS= 2 C/N 77.0]  
 08429+ [Impervious area: Japer= 4.67\*SLP1=0.00:LGP= 40.:NMN=.250:SCP=.01]  
 08430+ [Impervious area: JAimp= 1.57\*SLD1=1.00:LGI= 131.:MMI=.013:SCI=.01]  
 08431+ [iaECImp= 4.00: iareCper= 4.00]  
 08432+ [SMIN= 33.81:SMAX=225.43: SK= .010]  
 08433+ #  
 08434+ # Catchment JOCKVA  
 08435+ # - Residential development a golf course  
 08436+ #  
 08437+ # - JFSA 2011-11 update JOCKVA after updating CORRIG as per IBI GROUP, July 2008.  
 08438+ #  
 08439+ #  
 08440+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08441+ CONFIRM SPANNING 1.0 01-JOCKVA 228.13 17.670 No\_date 28:08 41.86 .647 .000  
 08442+ [XIMP= 50\*TIME=.50]  
 08443+ [LOSS= 2 C/N 74.0]  
 08444+ [Impervious area: Japer= 4.67\*SLP1=0.00:LGP= 40.:NMN=.250:SCP=.01]  
 08445+ [Impervious area: JAimp= 1.57\*SLD1=1.00:LGI=1311.:MMI=.013:SCI=.01]  
 08446+ [iaECImp= 4.00: iareCper= 4.00]  
 08447+ [SMIN= 33.81:SMAX=225.43: SK= .010]  
 08448+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08449+ ADD HYD 1.0 02-EXAND-MN 32.50 2.275 No\_date 27:15 41.93 n/a .000  
 08450+ \* Rating curve obtained from Jockva Servicing Study (CCL 1999)  
 08451+ [L/S/nr. 114] 120.00 1.592 No\_date 28:01 41.93 n/a .000  
 08452+ [L/S/nr. 114] 120.00 1.592 No\_date 28:01 41.93 n/a .000  
 08453+ [Vmax= 1.918\*Dmax 1.639]  
 08454+ [Din = 1.80\*Dused 2.00]  
 08455+ R0101:CD0046-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08456+ COMPUTE DUALHY / 1.0 01-A11 1.251 No\_date 28:01 45.36 .701 .000  
 08457+ remark:Total Flows at MH107  
 08458+ R0101:CD0046-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08459+ # Jockva SWN Facility  
 08460+ # - Rating curve obtained from Jockva Servicing Study (CCL 1999)  
 08461+ #  
 08462+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08463+ ROUTE RESERVOIR > 1.0 02-JOCKVA-TO 257.63 19.945 No\_date 28:08 41.88 .647 .000  
 08464+ [XIMP= 50\*TIME=.50]  
 08465+ [LOSS= 2 C/N 74.0]  
 08466+ overflow < 1.0 02-01-MJ 0:00 .000 No\_date 0:00 0:00 n/a .000  
 08467+ [L/S/nr. 114] 120.00 1.592 No\_date 28:01 41.88 .647 .000  
 08468+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08469+ ADD HYD 1.0 02-NDE 55194.86 86.067 No\_date 37:44 23.16 n/a .000  
 08470+ # Jockva SWN Facility TO 01-JOCKVA-TO 257.63 19.945 No\_date 28:08 41.88 .647 .000  
 08471+ #  
 08472+ SUM 1.0 01-SMK\_DE 55476.46 86.690 No\_date 37:37 23.26 n/a .000  
 08473+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08474+ SAVE HYD 1.0 01-SMK\_DE 55476.26 86.698 No\_date 37:44 23.26 n/a .000  
 08475+ name:SWN\_DE\_0010  
 08476+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08477+ # Hydrograph from Heart's Desire at Rideau River  
 08478+ # Hydrograph from Heart's Desire obtained from RIDEAU River  
 08479+ # Channel X-Section obtained from RIDEAU River  
 08480+ #  
 08481+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08482+ ROUTE CHANNEL > 1.0 01-DESIRE 55476.26 86.690 No\_date 37:37 23.26 n/a .000  
 08483+ [ROT 1.00] out-> 1.0 01-IN1 55476.26 86.683 No\_date 37:44 23.23 n/a .000  
 08484+ [L/S/nr. 56.5] 1.967 .045 .000 .000  
 08485+ [Vmax= 1.918\*Dmax 1.639]  
 08486+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08487+ COMPUTE DUALHY / 1.0 02-A11-MJ 2.59 .368 No\_date 28:01 51.11 n/a .000  
 08488+ Major System < 1.0 02-A11-MJ 2.59 .368 No\_date 28:01 51.11 n/a .000  
 08489+ Minor System < 1.0 03-A11-1 2.59 .368 No\_date 27:55 41.19 n/a .000  
 08490+ [Din = 1.80\*Dused 2.00]  
 08491+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08492+ CONTINUOUS NASHYD 1.0 01-SMK\_DE 2.942 2.957 No\_date 28:20 23.57 .364 .000  
 08493+ [Vmax= 1.918\*Dmax 1.639]  
 08494+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08495+ [InterEventTime= 12.00]  
 08496+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08497+ ADD HYD 1.0 02-IN1 55476.26 86.693 No\_date 37:44 23.23 n/a .000  
 08498+ \* Rating curve obtained from RIDEAU River  
 08499+ [L/S/nr. 77] 1.10 .013 [C/N 75.0]  
 08500+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08501+ [Vmax= 1.918\*Dmax 1.639]  
 08502+ name:SWN\_HYD\_0010  
 08503+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08504+ \*\* END OF RUN : 24  
 08505+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08506+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08507+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08508+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08509+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08510+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08511+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08512+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08513+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08514+ R0101:CD0043-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08515+ ICASED9 1 file (read and print data)  
 08516+ [TZERO = 0.00 hrs on 0]  
 08517+ [ROT 1.00] out-> 2 (1=Imperial, 2=metric output)  
 08518+ [INSTRM= 1]  
 08519+ [INSTRM= 0.02]  
 08520+ #  
 08521+ # SWNHYMO Ver1.05/Jan 2001 **BETA** / INPUT DATA FILE  
 08522+ # Project Name: Jockva01 Project Number: 1474-16  
 08523+ #  
 08524+ Date 04-03-2021  
 08525+ Model 1 [M.M.]  
 08526+ Units 1 [mm, sec]  
 08527+ License # 254927  
 08528+ #  
 08529+ # CALIBRATION OF SWMM MODEL PARAMETERS  
 08530+ name:CONTINUOUS SIMULATIONS  
 08531+ Rainfall data from Jockva rainfall installed at site + other gauges by the City  
 08532+ 2001-11-30 change TMST0 to 0.55, SLPI[0.5](8) (imperious slope), and LGI up to 70m  
 08533+ 2001-12-01 change TMST0 in COMPUTE ROUTE [TMST0 = 0.1 instead of 0.0001]  
 08534+ 2021-12-01 change point pending values to 0.55, SLPI[0.5](8) (imperious slope), and LGI up to 70m  
 08535+ 2021-12-01 change the slope for ROUTE CHANNEL Station 2462 [TMST0="1.ND", TMST0="1.NC"] from 0.033 % (as per S1) to 0.01 % (as per St)  
 08536+ 2021-12-01 change the slope for ROUTE CHANNEL Station 502 [TMST0="1.NC", TMST0="1.NC"] from 0.01 % (as per St) to 0.001 % (as per St)  
 08537+ 2021-12-01 change TMST0 in COMPUTE ROUTE [TMST0="1.ND", TMST0="1.NC"] from 0.033 % (as per S1) to 0.01 % (as per St)  
 08538+ 2021-12-01 change TMST0 in COMPUTE ROUTE [TMST0="1.ND", TMST0="1.NC"] from 0.033 % (as per S1) to 0.01 % (as per St)  
 08539+ R0205:CO0002-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08540+ R0205:CO0002-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08541+ R0205:CO0002-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08542+ R0205:CO0002-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08543+ R0205:CO0002-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08544+ R0205:CO0002-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08545+ M0304edc\_1.m3,TotVol=0.000,m3,MDkds=.9981  
 08546+ FileTitle="PROJ1474-16/design/20210210-QuantityControlAnalysis/SWNHYMO/SWN-Model\updated3/CitiGate.DEF"  
 08547+ FileTitle="CitiGate.DEF"  
 08548+ ICASED9 1 file (read and print data)  
 08549+ FileTitle="CitiGate.DEF"  
 08550+ R0205:CO0007-----> Dmin-ID:HYNDY---ARAHa-QPEAKcms-Tpeakdate\_bh:mm:--Rvnm-B.C.--DWFcms  
 08551+ CONFIRM SPANNING 1.0 01-SMK\_I3 971.00 5.778 No\_date 32:34 24.02 .323 .000  
 08552+ [L/S/nr. 1.0 01-SMK\_I3] 1.0 01-SMK\_I3 .00 .000 No\_date 0:00 0:00 n/a .000  
 08553+ [Vmax= 1.393\*Dmax



08977+ R025:CO0061-----Dtnin-ID:NHYD----AREAh-aQPEAKms-Peakdate\_hh:mm---Rvnm-R.C.---DWFcns  
08978+ SML HYD 1.0 01:S\_N4 48447.00 73.819 No\_date 35:41 28.02 n/a .000  
08979+ fsum=1.S\_N4.0025  
08980+ remark:flow at S\_N4  
08981+ # Sum of hydrographs from Node 4 routed to Node 2  
08982+ # Section 9  
08983+ #  
08984+ # ROUTE CHANNEL -> 1.0 02:S\_N4 48447.00 73.819 No\_date 35:41 28.02 n/a .000  
08985+ [ROUTE CHANNEL] 1.0 01:IN2 48447.00 73.485 No\_date 35:42 28.02 n/a .000  
08986+ [ROUTE CHANNEL] 1.0 01:IN2 48447.00 73.485 No\_date 35:42 28.02 n/a .000  
08987+ [L/S/n= 1667.1 / .060/.048]  
08988+ [Vmax=.874\*Imax 3.570]  
08989+ #  
08990+ # Addition of Subwatershed 2 with Monchan Drain and Smith Drain to Node 2  
08991+ #  
08992+ # ADD HYD 1.0 01:S\_N2 52483.00 106.109 No\_date 33:07 28.64 n/a .000  
08993+ name: H\_SN2  
08994+ remark:flow at S\_N2 Jock River Gauge at Moodie Dr.  
08995+ # Sum of hydrographs from Node 2 routed to Node 1  
08996+ # Section 10  
08997+ #  
08998+ #  
08999+ # Hydrograph from Node 2 routed to Node 416  
09000+ #  
09001+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 9025  
09002+ #  
09003+ # Dtnin-ID:NHYD----AREAh-aQPEAKms-Peakdate\_hh:mm---Rvnm-R.C.---DWFcns  
09004+ # ROUTE CHANNEL -> 1.0 02:S\_N2 52483.00 106.109 No\_date 33:07 28.64 n/a .000  
09005+ [ROUTE CHANNEL] 1.0 01:IN1 52483.00 103.234 No\_date 34:03 28.64 n/a .000  
09006+ [L/S/n= 2327.1 / .050/.058]  
09007+ [Vmax=.754\*Imax 3.305]  
09008+ #  
09009+ # Catchment SW-A  
09010+ # Portion of the catchment SW-1 outside of Reach 1 subwatershed  
09011+ # predominantly agricultural land  
09012+ #  
09013+ # CONTINUOUS NASHYD 1.0 01:S\_N2 536.42 5.184 No\_date 31:16 36.13 409 .000  
09014+ [CN= 72.01 N= 3.00 Tp= 2.79]  
09015+ [iaREc 4.01 SMIN=.751 SMAX=.2649; SK= .010]  
09016+ [ROUTE CHANNEL] 1.0 01:IN1 536.42 5.184 No\_date 31:16 36.13 409 .000  
09017+ [KIND= 65\*TIME=.65]  
09018+ [ROUTE CHANNEL] 1.0 01:S\_N2 44.93 6.507 No\_date 28:03 57.38 .771 .000  
09019+ [CN= 72.01 N= 3.00 Tp= 2.79]  
09020+ [iaREc 4.01 SMIN=.751 SMAX=.2649; SK= .010]  
09021+ [ROUTE CHANNEL] 1.0 01:S\_N2 44.93 6.507 No\_date 28:03 57.38 .771 .000  
09022+ [CONTINUOUS NASHYD 1.0 01:S\_N2 44.93 6.507 No\_date 28:03 57.38 .771 .000  
09023+ [CN= 72.01 N= 3.00 Tp= 2.79]  
09024+ [iaREc 4.01 SMIN=.751 SMAX=.2649; SK= .010]  
09025+ [ROUTE CHANNEL] 1.0 01:S\_N2 44.93 6.507 No\_date 28:03 57.38 .771 .000  
09026+ [CONTINUOUS NASHYD 1.0 01:S\_N2 44.93 6.507 No\_date 28:03 57.38 .771 .000  
09027+ R025:CO0067-----Dtnin-ID:NHYD----AREAh-aQPEAKms-Peakdate\_hh:mm---Rvnm-R.C.---DWFcns  
09028+ #  
09029+ #  
09030+ # COMPUTE DUALHYS 1.0 01:S\_1-Kf0000 44.93 6.507 No\_date 28:03 57.38 .771 .000  
09031+ [CN= 72.01 N= 3.00 Tp= 2.79]  
09032+ [Impervious area: IaImp= 1.57\*SL1+ .75\*LG1 547.1\*MMI-.013\*SCI+ .01]  
09033+ [iaREcImp= 4.00: 1aREcPerp= 4.00]  
09034+ [ROUTE CHANNEL] 1.0 01:S\_1-Kf0000 44.93 6.507 No\_date 28:03 57.38 .771 .000  
09035+ [R025:CO0068-----Dtnin-ID:NHYD----AREAh-aQPEAKms-Peakdate\_hh:mm---Rvnm-R.C.---DWFcns  
09036+ [ROUTE CHANNEL] 1.0 01:S\_1-Kf0000 44.93 6.507 No\_date 28:03 57.38 .771 .000  
09037+ [CN= 72.01 N= 3.00 Tp= 2.79]  
09038+ [iaREc 4.01 SMIN=.751 SMAX=.2649; SK= .010]  
09039+ [ROUTE CHANNEL] 1.0 01:S\_1-Kf0000 44.93 6.507 No\_date 28:03 57.38 .771 .000  
09040+ [CN= 72.01 N= 3.00 Tp= 2.79]  
09041+ ADD HYD 1.0 01:S\_1-Kf0000 44.93 6.507 No\_date 28:03 57.38 .771 .000  
09042+ #  
09043+ [ROUTE CHANNEL] 1.0 01:S\_1-Kf0000 44.93 6.507 No\_date 28:03 57.38 .771 .000  
09044+ R025:CO0070-----Dtnin-ID:NHYD----AREAh-aQPEAKms-Peakdate\_hh:mm---Rvnm-R.C.---DWFcns  
09045+ #  
09046+ #  
09047+ [ROUTE CHANNEL] 1.0 01:S\_1-Kf0000 44.93 6.507 No\_date 28:03 57.38 .771 .000  
09048+ [CN= 72.01 N= 3.00 Tp= 2.79]  
09049+ [ROUTE CHANNEL] 1.0 01:S\_1-Kf0000 44.93 6.507 No\_date 28:03 57.38 .771 .000  
09050+ R025:CO0071-----Dtnin-ID:NHYD----AREAh-aQPEAKms-Peakdate\_hh:mm---Rvnm-R.C.---DWFcns  
09051+ ADD HYD 1.0 01:S\_1-Kf0000 44.93 6.507 No\_date 28:03 57.38 .771 .000  
09052+ #  
09053+ [ROUTE CHANNEL] 1.0 01:S\_1-Kf0000 44.93 6.507 No\_date 28:03 57.38 .771 .000  
09054+ [CN= 72.01 N= 3.00 Tp= 2.79]  
09055+ SML HYD 1.0 01:S\_1-Kf0000 53064.36 107.436 No\_date 33:26 28.68 n/a .000  
09056+ #  
09057+ name: SH\_A146.0025  
09058+ remark:Total Flows at Highway 416 before Station 7245  
09059+ # Hydrograph from Node 416 routed to Node at Okere drain  
09060+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 7245  
09061+ #  
09062+ #  
09063+ # Dtnin-ID:NHYD----AREAh-aQPEAKms-Peakdate\_hh:mm---Rvnm-R.C.---DWFcns  
09064+ # ROUTE CHANNEL -> 1.0 02:S\_N1 53064.36 107.436 No\_date 33:26 28.68 n/a .000  
09065+ [ROUTE CHANNEL] 1.0 01:IN1 53064.36 107.360 No\_date 33:27 28.68 n/a .000  
09066+ [L/S/n= .497 / .050/.058]  
09067+ [Vmax=.998\*Imax 2.04]  
09068+ #  
09069+ # Catchment SW-A  
09070+ # To O'Keefe drain (north of the Jack)  
09071+ # Developed with assumed 43% imp.  
09072+ # - 3202-12-01 add Okere model (Area was added as per the NOVATEC SWNOHYD mode (Citi-Cate 2014).  
09073+ #  
09074+ #  
09075+ #  
09076+ # CONTINUOUS NASHYD 1.0 01:O-1 63.74 537 No\_date 28:58 22.31 .289 .000  
09077+ [CN= 61.01 N= 3.00 Tp= .901]  
09078+ [ROUTE CHANNEL] 1.0 01:IN1 63.74 537 No\_date 28:58 22.31 .289 .000  
09079+ [CN= 61.01 N= 3.00 Tp= .901]  
09080+ [ROUTE CHANNEL] 1.0 01:O-1R 63.74 .877 No\_date 29:15 28.68 n/a .000  
09081+ [ROUTE CHANNEL] 1.0 01:O-1R 63.74 .877 No\_date 29:15 28.68 n/a .000  
09082+ [ROUTE CHANNEL] 1.0 01:O-1R 63.74 .877 No\_date 29:15 28.68 n/a .000  
09083+ [CN= 49.01 N= 3.00 Tp= .901]  
09084+ [ROUTE CHANNEL] 1.0 01:O-1R 63.74 .877 No\_date 29:15 28.68 n/a .000  
09085+ [ROUTE CHANNEL] 1.0 01:O-1R 63.74 .877 No\_date 29:15 28.68 n/a .000  
09086+ [CN= 49.01 N= 3.00 Tp= .901]  
09087+ [ROUTE CHANNEL] 1.0 01:O-1R 63.74 .877 No\_date 29:15 28.68 n/a .000  
09088+ [CN= 49.01 N= 3.00 Tp= .901]  
09089+ [ROUTE CHANNEL] 1.0 01:O-1R 63.74 .877 No\_date 29:15 28.68 n/a .000  
09090+ [CN= 49.01 N= 3.00 Tp= .901]  
09091+ [ROUTE CHANNEL] 1.0 01:O-1R 63.74 .877 No\_date 29:15 28.68 n/a .000  
09092+ [CN= 49.01 N= 3.00 Tp= .901]  
09093+ [ROUTE CHANNEL] 1.0 01:O-1R 63.74 .877 No\_date 29:15 28.68 n/a .000  
09094+ [CN= 49.01 N= 3.00 Tp= .901]  
09095+ [ROUTE CHANNEL] 1.0 01:O-1R 63.74 .877 No\_date 29:15 28.68 n/a .000  
09096+ [CN= 49.01 N= 3.00 Tp= .901]  
09097+ [ROUTE CHANNEL] 1.0 01:O-1R 63.74 .877 No\_date 29:15 28.68 n/a .000  
09098+ [CN= 49.01 N= 3.00 Tp= .901]  
09099+ [ROUTE CHANNEL] 1.0 01:O-1R 63.74 .877 No\_date 29:15 28.68 n/a .000  
09100+ R025:CO0079-----Dtnin-ID:NHYD----AREAh-aQPEAKms-Peakdate\_hh:mm---Rvnm-R.C.---DWFcns  
09101+ #  
09102+ #  
09103+ #  
09104+ #  
09105+ #  
09106+ #  
09107+ #  
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09123+ #  
09124+ #  
09125+ #  
09126+ #  
09127+ ADD HYD 1.0 02:O-1 28.61 .330 No\_date 29:13 20.55 .276 .000  
09128+ #  
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09350+ #



09725+ ROUTE RESERVOIR -> 1.0 018-S-1-D8S 5.27 .672 No\_date 27:55 42.30 n/a .000

09726+ 1.0 018-1-08B 5.27 .050 No\_date 28:47 42.30 n/a .000

09727+ 1.0 018-1-08C 5.27 .050 No\_date 28:47 42.30 n/a .000

09728+ [MastCUsed: 11658E-00 m<sup>3</sup>, TotCovVol: 0.000E+00 m<sup>3</sup>, N-Ovfr: 0, TotTurvol: 0, hrs] .000

09729+ CONTINUOUS\_NASHYD -> ARRAha-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09730+ 1.0 018-1-08C 5.27 .250 No\_date 28:47 34.14 .459 .000

09731+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09732+ [iabECmp: 4.00 IABP: 31.15 SMAX:207.66 SKA: .010]

09733+ # To West Clarke Pond 12.001

09734+ ROG25:CO0186-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09735+ CONTINUOUS\_NASHYD -> 1.0 01W-CLAR\_LND 35.61 .789 No\_date 29:10 34.14 .459 .000

09736+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09737+ [iabECmp: 4.00 IABP: 31.15 SMAX:207.66 SKA: .010]

09738+ ROG25:CO0187-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09739+ ADD HYD + 1.0 02N\_FO 53577.82 108.449 No\_date 33:28 28.74 n/a .000

09740+ 1.0 02N-1-08C 53577.82 108.449 No\_date 33:28 28.74 n/a .000

09741+ 1.0 02N-1-08B 5.27 .050 No\_date 28:47 28.74 n/a .000

09742+ 1.0 02N-1-08C 5.27 1.168 No\_date 29:06 56.82 n/a .000

09743+ 1.0 02P-1DFOV 0.00 .000 No\_date 0:00 0.00 n/a .000

09744+ 1.0 02P-1DFOV 0.00 .000 No\_date 0:00 0.00 n/a .000

09745+ 1.0 02S-1-PDFov 0.00 .000 No\_date 0:00 0.00 n/a .000

09746+ 1.0 02S-1-POF-DR 14.96 .183 No\_date 29:30 56.95 n/a .000

09747+ 1.0 02S-1-POF-DR 14.96 .000 No\_date 29:30 56.95 n/a .000

09748+ 1.0 02S-1-DRB 5.27 .050 No\_date 28:47 42.30 n/a .000

09749+ 1.0 02S-1-DRB 5.27 75.88 .2541 No\_date 28:36 34.14 n/a .000

09750+ SUM -> 1.0 018-1-08C 54118.36 114.034 No\_date 33:32 28.94 n/a .000

09751+ ROG25:CO0188-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09752+ SAVE HYD 1.0 01SN\_FO 54118.36 114.198 No\_date 33:27 28.94 n/a .000

09753+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09754+ remark:Total Flows at Foster Drain

09755+ # Hydrograph from Node Foster routed to Node at Cedarview Road

09756+ # Channel X-Section obtained from Rvca Hydraulic Model - Station 6016

09757+ # Channel X-Section obtained from Rvca Hydraulic Model - Station 5737

09758+ ROG25:CO0189-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09759+ 1.0 018-1-08C 5111.36 114.198 No\_date 33:32 28.94 n/a .000

09760+ [RDT: 1.00 out-] 1.0 01N\_CNE 54118.36 114.034 No\_date 33:32 28.94 n/a .000

09761+ [L/S: /nvn: .159-.082/.035]

09762+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09763+ # Catchment 5-1

09764+ # Jock River (north and south of Jock)

09765+ # Primarily agricultural fields; portion of sand quarry

09766+ ROG25:CO0190-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09767+ CONTINUOUS\_NASHYD 1.0 018-1-B 55.36 2.311 No\_date 28:23 34.14 .459 .000

09768+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09769+ [Intervertintime: .12001]

09770+ # - JFSA 2021-02-24 change the name from S-1-B0C to S-1-A and S-1-B. Change their TP values based on the new areas

09771+ # - JFSA 2021-02-24 change the name from S-1-B0C to S-1-A and S-1-B. "S-1-B0C" & "S-1-B0C-1" are not existing anymore

09772+ # - JFSA 2021-01-19, after adding Greenbank pond, "S-1-B0C-1" is not existing anymore

09773+ ROG25:CO0191-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09774+ CONTINUOUS\_NASHYD 1.0 018-1-B 21.67 3.388 No\_date 28:01 57.38 .773 .000

09775+ [XMP: 65-TIM:65]

09776+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09777+ [Previous: area: Iaper: 4.67 SLPP:2.00:LGP: 40.-MNP: .250:SCP: .01]

09778+ [Imperial: area: IaImp: 1.57SLPP: .75:LGP: 380.-MNP: .013:SCI: .01]

09779+ [iabECmp: 33.81 SMAX:225.43 SK: .010]

09780+ ROG25:CO0192-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09781+ 1.0 02S-1-08C 21.67 .3185 No\_date 28:01 57.38 .773 .000

09782+ Major System / 1.0 02S-1-DAL .00 .000 No\_date 0:00 0.00 n/a .000

09783+ Minor System / 1.0 03S-1-DIN 21.67 2.409 No\_date 27:55 57.58 n/a .000

09784+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09785+ ROG25:CO0193-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09786+ ADD HYD + 1.0 02S-1-DIL 0.00 .000 No\_date 0:00 0.00 n/a .000

09787+ 1.0 02S-1-DIL 0.00 .000 No\_date 0:00 0.00 n/a .000

09788+ 1.0 02S-1-DR 21.67 2.409 No\_date 27:55 57.58 n/a .000

09789+ 1.0 018-1-08C 21.67 2.409 No\_date 27:55 57.58 n/a .000

09790+ SUM -> 1.0 018-1-08C 21.67 2.409 No\_date 27:55 57.58 n/a .000

09791+ ROG25:CO0194-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09792+ ROUTE RESERVOIR -> 1.0 018-1-08C 21.67 .225 No\_date 29:22 57.58 n/a .000

09793+ overflow <- 1.0 018-1-08C 0.00 .000 No\_date 0:00 0.00 n/a .000

09794+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09795+ ROG25:CO0195-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09796+ CONTINUOUS\_NASHYD 1.0 018-1-B 3.26 .581 No\_date 28:00 57.38 .773 .000

09797+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09798+ [Previous: area: Iaper: 4.67 SLPP:2.00:LGP: 40.-MNP: .250:SCP: .01]

09799+ [Imperial: area: IaImp: 1.57SLPP: .75:LGP: 380.-MNP: .013:SCI: .01]

09800+ [iabECmp: 33.81 SMAX:225.43 SK: .010]

09801+ ROG25:CO0196-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09802+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09803+ [Previous: area: Iaper: 1.57SLPP: .75:LGP: 148.-MNP: .013:SCI: .01]

09804+ [iabECmp: 4.00 IaREPPer: .000]

09805+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09806+ ROG25:CO0197-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09807+ COMPUTE DUALHY 1.0 01S-1-D4 3.28 .581 No\_date 28:00 57.38 n/a .000

09808+ Major System / 1.0 02S-1-08C 0.00 .000 No\_date 0:00 0.00 n/a .000

09809+ Minor System / 1.0 03S-1-08C 0.00 .000 No\_date 0:00 0.00 n/a .000

09810+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09811+ ROG25:CO0198-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09812+ ADD HYD + 1.0 01S-1-043 0.00 .000 No\_date 0:00 0.00 n/a .000

09813+ 1.0 01S-1-043 0.00 .000 No\_date 0:00 0.00 n/a .000

09814+ 1.0 01S-1-043 0.00 .000 No\_date 0:00 0.00 n/a .000

09815+ 1.0 01S-1-043 0.00 .000 No\_date 0:00 0.00 n/a .000

09816+ 1.0 01S-1-043 0.00 .000 No\_date 0:00 0.00 n/a .000

09817+ 1.0 01S-1-043 0.00 .000 No\_date 0:00 0.00 n/a .000

09818+ 1.0 01S-1-043 0.00 .000 No\_date 0:00 0.00 n/a .000

09819+ 1.0 01S-1-043 0.00 .000 No\_date 0:00 0.00 n/a .000

09820+ ROG25:CO0199-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09821+ CONTINUOUS\_NASHYD 1.0 01S-1-B 12.84 2.093 No\_date 28:01 57.38 .773 .000

09822+ [XMP: 65-TIM:65]

09823+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09824+ [Previous: area: Iaper: 4.67 SLPP:2.00:LGP: 40.-MNP: .250:SCP: .01]

09825+ [Imperial: area: IaImp: 1.57SLPP: .75:LGP: 293.-MNP: .013:SCI: .01]

09826+ [iabECmp: 4.00 IaREPPer: .000]

09827+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09828+ ROG25:CO0200-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09829+ 1.0 02S-1-08C 12.84 2.083 No\_date 28:01 57.38 .773 .000

09830+ Major System / 1.0 02S-1-08D 0.00 .000 No\_date 0:00 0.00 n/a .000

09831+ Minor System / 1.0 03S-1-08D 0.00 .000 No\_date 0:00 0.00 n/a .000

09832+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09833+ ROG25:CO0201-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09834+ ADD HYD + 1.0 02S-1-08C 0.00 .000 No\_date 0:00 0.00 n/a .000

09835+ 1.0 02S-1-08C 0.00 .000 No\_date 0:00 0.00 n/a .000

09836+ 1.0 02S-1-08C 0.00 .000 No\_date 0:00 0.00 n/a .000

09837+ 1.0 02S-1-08C 0.00 .000 No\_date 0:00 0.00 n/a .000

09838+ 1.0 02S-1-08C 0.00 .000 No\_date 0:00 0.00 n/a .000

09839+ 1.0 02S-1-08C 0.00 .000 No\_date 0:00 0.00 n/a .000

09840+ overflow <- 1.0 01S-1-08C 0.00 .000 No\_date 0:00 0.00 n/a .000

09841+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09842+ ROG25:CO0203-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09843+ CONTINUOUS\_NASHYD 1.0 01S-1-B 1.76 .319 No\_date 28:00 57.38 .771 .000

09844+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09845+ [Previous: area: Iaper: 4.67 SLPP:2.00:LGP: 40.-MNP: .250:SCP: .01]

09846+ [Imperial: area: IaImp: 1.57SLPP: .75:LGP: 148.-MNP: .013:SCI: .01]

09847+ [iabECmp: 4.00 IaREPPer: .000]

09848+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09849+ ROG25:CO0205-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09850+ COMPUTE DUALHY 1.0 01S-1-08C 1.76 .319 No\_date 28:00 57.38 .771 .000

09851+ Major System / 1.0 02S-1-08C 0.00 .000 No\_date 0:00 0.00 n/a .000

09852+ Minor System / 1.0 03S-1-08C 0.00 .000 No\_date 0:00 0.00 n/a .000

09853+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09854+ ROG25:CO0206-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09855+ 1.0 02S-1-08C 1.76 .232 No\_date 27:53 57.55 n/a .000

09856+ 1.0 02S-1-08C 1.76 .232 No\_date 27:53 57.55 n/a .000

09857+ 1.0 02S-1-08C 1.76 .232 No\_date 27:53 57.55 n/a .000

09858+ 1.0 02S-1-08C 1.76 .232 No\_date 27:53 57.55 n/a .000

09859+ 1.0 02S-1-08C 1.76 .232 No\_date 27:53 57.55 n/a .000

09860+ ROUTE RESERVOIR -> 1.0 02S-1-08C 1.76 .232 No\_date 27:53 57.55 n/a .000

09861+ overflow <- 1.0 01S-1-08C 0.00 .000 No\_date 0:00 0.00 n/a .000

09862+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09863+ ROG25:CO0207-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09864+ 1.0 02S-1-08C 1.76 .232 No\_date 27:53 57.55 n/a .000

09865+ 1.0 02S-1-08C 1.76 .232 No\_date 27:53 57.55 n/a .000

09866+ 1.0 02S-1-08C 1.76 .232 No\_date 27:53 57.55 n/a .000

09867+ 1.0 02S-1-08C 1.76 .232 No\_date 27:53 57.55 n/a .000

09868+ 1.0 02S-1-08C 1.76 .232 No\_date 27:53 57.55 n/a .000

09869+ 1.0 02S-1-08C 1.76 .232 No\_date 27:53 57.55 n/a .000

09870+ ROG25:CO0208-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09871+ 1.0 02S-1-08C 1.76 .232 No\_date 27:53 57.55 n/a .000

09872+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09873+ ROG25:CO0209-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09874+ 1.0 02S-1-08C 1.76 .232 No\_date 27:53 57.55 n/a .000

09875+ 1.0 02S-1-08C 1.76 .232 No\_date 27:53 57.55 n/a .000

09876+ 1.0 02S-1-08C 1.76 .232 No\_date 27:53 57.55 n/a .000

09877+ 1.0 02S-1-08C 1.76 .232 No\_date 27:53 57.55 n/a .000

09878+ ROG25:CO0210-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09879+ 1.0 02S-1-08C 1.76 .232 No\_date 27:53 57.55 n/a .000

09880+ 1.0 02S-1-08C 1.76 .232 No\_date 27:53 57.55 n/a .000

09881+ ROG25:CO0210-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09882+ 1.0 02S-1-08C 1.76 .232 No\_date 27:53 57.55 n/a .000

09883+ 1.0 02S-1-08C 1.76 .232 No\_date 27:53 57.55 n/a .000

09884+ overflow <- 1.0 01S-1-08C 0.00 .000 No\_date 0:00 0.00 n/a .000

09885+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09886+ # Catchment 5-1

09887+ # To West Clarke Pond 12.001 as per hydrograph South NS

09888+ # - 2020-11-30 update CLARKE Tributary drainage Area to = 121 ha based on PMS9804-11

09889+ # - 2020-11-30 split CLARKE drainage Area to MAJOR and A12

09890+ # - 2020-11-30 update CLARKE Tributary drainage Area to MAJOR and A12

09891+ ROG25:CO0211-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09892+ CONTINUOUS\_NASHYD 1.0 01W-CLAR\_MJ 1.77 .231 No\_date 28:00 58.78 .709 .000

09893+ overflow <- 1.0 03W-CLAR\_MJ 0.00 .000 No\_date 28:01 58.78 n/a .000

09894+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09895+ ROG25:CO0212-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09896+ CONTINUOUS\_NASHYD 1.0 01W-CLAR\_MJ 1.77 .231 No\_date 28:00 58.78 .709 .000

09897+ overflow <- 1.0 03W-CLAR\_MJ 0.00 .000 No\_date 28:01 58.78 n/a .000

09898+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09899+ ROG25:CO0213-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09900+ CONTINUOUS\_NASHYD 1.0 01W-CLAR\_ALL 119.40 15.305 No\_date 28:04 56.81 .764 .000

09901+ ROG25:CO0212-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09902+ ROUTE RESERVOIR -> 1.0 01W-CLAR\_MJ 1.77 .231 No\_date 28:00 58.78 .709 .000

09903+ overflow <- 1.0 03W-CLAR\_MJ 0.00 .000 No\_date 28:01 58.78 n/a .000

09904+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09905+ ROG25:CO0213-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09906+ CONTINUOUS\_NASHYD 1.0 01W-CLAR\_ALL 119.40 15.305 No\_date 28:04 56.81 .764 .000

09907+ CONTINUOUS\_NASHYD 1.0 01W-CLAR\_ALL 119.40 15.305 No\_date 28:04 56.81 .764 .000

09908+ frame:W-CLAR 12.001

09909+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09910+ ROG25:CO0214-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09911+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09912+ [iabECmp: 4.00 IaREPPer: .000]

09913+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09914+ ROG25:CO0215-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09915+ ADD HYD + 1.0 02S-1-08C 113.40 1.350 No\_date 27:57 33.51 n/a .000

09916+ 1.0 02S-1-08C 113.40 1.350 No\_date 27:57 33.51 n/a .000

09917+ 1.0 02S-1-08C 113.40 1.350 No\_date 27:57 33.51 n/a .000

09918+ 1.0 02S-1-08C 113.40 1.350 No\_date 27:57 33.51 n/a .000

09919+ 1.0 02S-1-08C 113.40 1.350 No\_date 27:57 33.51 n/a .000

09920+ 1.0 02S-1-08C 113.40 1.350 No\_date 27:57 33.51 n/a .000

09921+ frame:W-CLAR 12.001

09922+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09923+ ROG25:CO0216-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09924+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09925+ ROG25:CO0217-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09926+ CONTINUOUS\_NASHYD 1.0 01W-CLAR\_MJ 119.40 15.305 No\_date 28:04 56.81 .764 .000

09927+ overflow <- 1.0 03W-CLAR\_MJ 0.00 .000 No\_date 28:01 58.78 n/a .000

09928+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09929+ ROG25:CO0218-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09930+ CONTINUOUS\_NASHYD 1.0 01W-CLAR\_MJ 119.40 15.305 No\_date 28:04 56.81 .764 .000

09931+ overflow <- 1.0 03W-CLAR\_MJ 0.00 .000 No\_date 28:01 58.78 n/a .000

09932+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09933+ ROG25:CO0219-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09934+ CONTINUOUS\_NASHYD 1.0 01W-CLAR\_MJ 119.40 15.305 No\_date 28:04 56.81 .764 .000

09935+ overflow <- 1.0 03W-CLAR\_MJ 0.00 .000 No\_date 28:01 58.78 n/a .000

09936+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09937+ ROG25:CO0220-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09938+ CONTINUOUS\_NASHYD 1.0 01W-CLAR\_MJ 119.40 15.305 No\_date 28:04 56.81 .764 .000

09939+ overflow <- 1.0 03W-CLAR\_MJ 0.00 .000 No\_date 28:01 58.78 n/a .000

09940+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09941+ ROG25:CO0221-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09942+ CONTINUOUS\_NASHYD 1.0 01W-CLAR\_MJ 119.40 15.305 No\_date 28:04 56.81 .764 .000

09943+ overflow <- 1.0 03W-CLAR\_MJ 0.00 .000 No\_date 28:01 58.78 n/a .000

09944+ [CN: 77.01 No: 3.00 Tp: 1.62] .000

09945+ ROG25:CO0222-----Dtnin:ID:NHYD-----ARRAh-QPEAKcms-Tpeakdate\_hh:mm:->RVm-R.C.--DFWfms

09946+ CONTINUOUS\_NASHYD 1.0 01W-CLAR\_MJ 119.40 15.305 No\_date 28:04 56.81 .764 .000

09947+ overflow <- 1.0 03W-CLAR\_MJ 0.00 .000 No

10099+ [Impervious area: IAImp+ 94:SLD1+4.75:LG1+ 294:MNI+ 013:SCI+ .0] 10100+ [Bareimp+ 4.00: IAImp+ 0.00: .0] 10101+ RO25:CO0244-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10102+ COMPUTE DUALHYD / 1.0 01:KE-06 12.93 2.960 No\_date 28:00 66.54 n/a .000 10103+ Major System / 1.0 01:KE-06 12.93 2.242 No\_date 28:07 66.54 n/a .000 10104+ Minor System / 1.0 01:KE-06 12.93 2.242 No\_date 28:07 66.54 n/a .000 10105+ [MjyStcTo...\_2613+03, TotCovFvl+0000E+00, N-Ovrf+ 0, TotDurOvf+ 0,hrs] 10106+ RO25:CO0244-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10107+ CONTINUOUS STANDHYD / 1.0 01:KE-11 4.03 .817 No\_date 28:00 55.88 .751 .000 10108+ ADD HYD + 1.0 02:KE-06-MN 12.93 2.262 No\_date 28:07 66.58 n/a .000 10109+ SUM+ 1.0 02:KE-06-MN 12.93 2.262 No\_date 28:07 66.58 n/a .000 10110+ RO25:CO0245-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10111+ CONTINUOUS STANDHYD / 1.0 01:KE-11 4.03 .817 No\_date 28:00 55.88 .751 .000 10112+ [Morton parameters: Fo: 76, 20:Po: 13, 20:DCWY4+14: Fw\_ .00] 10113+ [Previous areas: Iaper: 4.67:SLP2+2.00:LGD+ 40:-MND+ 250:SCP+ .0] 10114+ [Impervious areas: IAImp+ 1.57:SLP1+2.00:LGD+ 164:MNI+ 013:SCI+ .0] 10115+ [Bareimp+ 4.00: IAImp+ 4.00] 10116+ RO25:CO0246-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10117+ COMPUTE DUALHYD / 1.0 01:KE-11-MJ .00 .000 No\_date 0:00 0:00 n/a .000 10118+ Major System / 1.0 01:KE-11-MJ .00 .000 No\_date 0:00 0:00 n/a .000 10119+ Minor System / 1.0 01:KE-11-MJ .00 .000 No\_date 0:00 0:00 n/a .000 10120+ [Morton parameters: Fo: 76, 20:Po: 13, 20:DCWY4+14: Fw\_ .00] 10121+ [Previous areas: Iaper: 4.67:SLP2+2.00:LGD+ 40:-MND+ 250:SCP+ .0] 10122+ RO25:CO0247-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10123+ ADD HYD + 1.0 02:KE-11-MJ .00 .000 No\_date 0:00 0:00 n/a .000 10124+ SUM+ 1.0 02:KE-11-MJ .00 .000 No\_date 0:00 0:00 n/a .000 10125+ [Morton parameters: Fo: 76, 20:Po: 13, 20:DCWY4+14: Fw\_ .00] 10126+ [Previous areas: Iaper: 4.67:SLP2+2.00:LGD+ 40:-MND+ 250:SCP+ .0] 10127+ [Impervious areas: IAImp+ 1.57:SLP1+2.00:LGD+ 182:MNI+ 013:SCI+ .0] 10128+ [Bareimp+ 4.00: IAImp+ 4.00] 10129+ RO25:CO0248-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10130+ CONTINUOUS STANDHYD / 1.0 01:KE-11 4.03 .817 No\_date 28:00 66.06 .928 .000 10131+ [XIMD+ 93:TIME+ .93] 10132+ [Morton parameters: Fo: 76, 20:Po: 13, 20:DCWY4+14: Fw\_ .00] 10133+ [Previous areas: Iaper: 4.67:SLP2+2.00:LGD+ 40:-MND+ 250:SCP+ .0] 10134+ [Impervious areas: IAImp+ 1.57:SLP1+2.00:LGD+ 182:MNI+ 013:SCI+ .0] 10135+ [Bareimp+ 4.00: IAImp+ 4.00] 10136+ RO25:CO0249-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10137+ CONTINUOUS STANDHYD / 1.0 01:KE-15 2.15 .447 No\_date 28:00 62.65 .842 .000 10138+ [XIMD+ 79:TIME+ .79] 10139+ [Morton parameters: Fo: 76, 20:Po: 13, 20:DCWY4+14: Fw\_ .00] 10140+ [Previous areas: Iaper: 4.67:SLP2+2.00:LGD+ 40:-MND+ 250:SCP+ .0] 10141+ [Impervious areas: IAImp+ 1.57:SLP1+2.00:LGD+ 182:MNI+ 013:SCI+ .0] 10142+ [Bareimp+ 4.00: IAImp+ 4.00] 10143+ RO25:CO0250-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10144+ ADD HYD + 1.0 02:KE-08-MN 40.82 3.600 No\_date 28:00 25.50 n/a .000 10145+ SUM+ 1.0 02:KE-08-MN 40.82 3.600 No\_date 28:00 25.50 n/a .000 10146+ [Morton parameters: Fo: 76, 20:Po: 13, 20:DCWY4+14: Fw\_ .00] 10147+ [Previous areas: Iaper: 4.67:SLP2+2.00:LGD+ 40:-MND+ 250:SCP+ .0] 10148+ [Impervious areas: IAImp+ 1.57:SLP1+2.00:LGD+ 182:MNI+ 013:SCI+ .0] 10149+ [Bareimp+ 4.00: IAImp+ 4.00] 10150+ RO25:CO0251-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10151+ ADD HYD + 1.0 01:KE-08-MN 206.72 17.555 No\_date 28:01 38.99 n/a .000 10152+ RO25:CO0251-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10153+ ROUTE RESERVOIR -----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10154+ overflow <= 1.0 01:KE-08-MN 201.26 12.438 No\_date 28:05 38.09 n/a .000 10155+ [Morton parameters: Fo: 76, 20:Po: 13, 20:DCWY4+14: Fw\_ .00] 10156+ [Previous areas: Iaper: 4.67:SLP2+2.00:LGD+ 40:-MND+ 250:SCP+ .0] 10157+ RO25:CO0252-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10158+ ADD HYD + 1.0 02:KE-08-MN 201.26 12.438 No\_date 28:05 38.09 n/a .000 10159+ SUM+ 1.0 02:KE-08-MN 201.26 12.438 No\_date 28:05 38.09 n/a .000 10160+ [Morton parameters: Fo: 76, 20:Po: 13, 20:DCWY4+14: Fw\_ .00] 10161+ [Previous areas: Iaper: 4.67:SLP2+2.00:LGD+ 40:-MND+ 250:SCP+ .0] 10162+ RO25:CO0253-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10163+ name: KI-Pond1\_0025 10.86 2.392 No\_date 28:00 65.97 .887 .000 10164+ remark: Total Flows at KI Pond first pond 10165+ overflow <= 1.0 01:KE-08-MN 201.26 12.438 No\_date 28:05 38.09 n/a .000 10166+ [XIMD+ 02:TIME+ .02] 10167+ [Morton parameters: Fo: 76, 20:Po: 13, 20:DCWY4+14: Fw\_ .00] 10168+ [Previous areas: Iaper: 4.67:SLP2+2.00:LGD+ 40:-MND+ 250:SCP+ .0] 10169+ [Impervious areas: IAImp+ 1.57:SLP1+2.00:LGD+ 269:MNI+ 013:SCI+ .0] 10170+ [Bareimp+ 4.00: IAImp+ 4.00] 10171+ RO25:CO0254-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10172+ RO25:CO0255-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10173+ COMPUTE DUALHYD / 1.0 01:KE-07 10.86 2.392 No\_date 28:00 66.57 n/a .000 10174+ Major System / 1.0 01:KE-07 10.86 2.094 No\_date 27:56 66.57 n/a .000 10175+ Minor System / 1.0 01:KE-07 10.86 2.094 No\_date 27:56 66.57 n/a .000 10176+ [MjyStcTo...\_7532+02, TotCovFvl+0000E+00, N-Ovrf+ 0, TotDurOvf+ 0,hrs] 10177+ RO25:CO0256-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10178+ ADD HYD + 1.0 02:KE-07-MN 10.86 .000 No\_date 0:00 0:00 n/a .000 10179+ SUM+ 1.0 02:KE-07-MN 10.86 .000 No\_date 0:00 0:00 n/a .000 10180+ [Morton parameters: Fo: 76, 20:Po: 13, 20:DCWY4+14: Fw\_ .00] 10181+ [Previous areas: Iaper: 4.67:SLP2+2.00:LGD+ 40:-MND+ 250:SCP+ .0] 10182+ RO25:CO0257-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10183+ CONTINUOUS STANDHYD / 1.0 01:KE-07 6.61 1.292 No\_date 28:00 53.97 n/a .000 10184+ [XIMD+ 64:TIME+ .64] 10185+ [Morton parameters: Fo: 76, 20:Po: 13, 20:DCWY4+14: Fw\_ .00] 10186+ [Previous areas: Iaper: 4.67:SLP2+2.00:LGD+ 40:-MND+ 250:SCP+ .0] 10187+ RO25:CO0258-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10188+ COMPUTE DUALHYD / 1.0 01:KE-08 6.61 1.292 No\_date 28:00 53.97 n/a .000 10189+ Major System / 1.0 01:KE-08 6.61 1.058 No\_date 27:55 54.34 n/a .000 10190+ Minor System / 1.0 01:KE-08 6.61 1.058 No\_date 27:55 54.34 n/a .000 10191+ [MjyStcTo...\_6182+02, TotCovFvl+0000E+00, N-Ovrf+ 0, TotDurOvf+ 0,hrs] 10192+ RO25:CO0259-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10193+ ADD HYD + 1.0 02:KE-08-MN 6.61 1.292 No\_date 28:00 53.97 n/a .000 10194+ RO25:CO0259-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10195+ COMPUTE DUALHYD / 1.0 01:KE-08 6.61 1.292 No\_date 28:00 53.97 n/a .000 10196+ Major System / 1.0 01:KE-08 6.61 1.058 No\_date 27:55 54.34 n/a .000 10197+ Minor System / 1.0 01:KE-08 6.61 1.058 No\_date 27:55 54.34 n/a .000 10198+ [MjyStcTo...\_6182+02, TotCovFvl+0000E+00, N-Ovrf+ 0, TotDurOvf+ 0,hrs] 10199+ RO25:CO0260-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10200+ CONTINUOUS STANDHYD / 1.0 01:KE-08 6.61 1.292 No\_date 28:00 53.97 n/a .000 10201+ [XIMD+ 86:TIME+ .86] 10202+ [Morton parameters: Fo: 76, 20:Po: 13, 20:DCWY4+14: Fw\_ .00] 10203+ [Previous areas: Iaper: 4.67:SLP2+2.00:LGD+ 40:-MND+ 250:SCP+ .0] 10204+ [Impervious areas: IAImp+ 1.57:SLP1+2.00:LGD+ 132:MNI+ 013:SCI+ .0] 10205+ [Bareimp+ 4.00: IAImp+ 4.00] 10206+ RO25:CO0261-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10207+ CONTINUOUS STANDHYD / 1.0 01:KE-08 2.37 .580 No\_date 28:00 65.30 .878 .000 10208+ [Morton parameters: Fo: 76, 20:Po: 13, 20:DCWY4+14: Fw\_ .00] 10209+ [Previous areas: Iaper: 4.67:SLP2+2.00:LGD+ 40:-MND+ 250:SCP+ .0] 10210+ [Bareimp+ 4.00: IAImp+ 4.00] 10211+ RO25:CO0262-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10212+ [MjyStcTo...\_7532+02, TotCovFvl+0000E+00, N-Ovrf+ 0, TotDurOvf+ 0,hrs] 10213+ RO25:CO0263-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10214+ COMPUTE DUALHYD / 1.0 01:KE-08 2.37 .580 No\_date 28:00 65.30 .878 .000 10215+ Major System / 1.0 01:KE-08 2.37 .580 No\_date 27:55 65.30 .878 .000 10216+ Minor System / 1.0 01:KE-08 2.37 .580 No\_date 27:55 65.30 .878 .000 10217+ [MjyStcTo...\_6182+02, TotCovFvl+0000E+00, N-Ovrf+ 0, TotDurOvf+ 0,hrs] 10218+ RO25:CO0264-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10219+ CONTINUOUS STANDHYD / 1.0 01:KE-08 4.86 .109 No\_date 28:00 55.97 n/a .000 10220+ [XIMD+ 79:TIME+ .79] 10221+ [Morton parameters: Fo: 76, 20:Po: 13, 20:DCWY4+14: Fw\_ .00] 10222+ [Previous areas: Iaper: 4.67:SLP2+2.00:LGD+ 40:-MND+ 250:SCP+ .0] 10223+ [Impervious areas: IAImp+ 1.57:SLP1+2.00:LGD+ 180:MNI+ 013:SCI+ .0] 10224+ [Bareimp+ 4.00: IAImp+ 4.00] 10225+ RO25:CO0265-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10226+ COMPUTE DUALHYD / 1.0 01:KE-08 4.86 1.059 No\_date 28:00 66.57 n/a .000 10227+ Major System / 1.0 01:KE-08 4.86 1.059 No\_date 27:56 66.57 n/a .000 10228+ Minor System / 1.0 01:KE-08 4.86 1.059 No\_date 27:56 66.57 n/a .000 10229+ [MjyStcTo...\_6182+02, TotCovFvl+0000E+00, N-Ovrf+ 0, TotDurOvf+ 0,hrs] 10230+ RO25:CO0266-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10231+ ADD HYD + 1.0 02:KE-08-MN 4.86 .000 No\_date 0:00 0:00 n/a .000 10232+ SUM+ 1.0 02:KE-08-MN 4.86 .000 No\_date 0:00 0:00 n/a .000 10233+ [Morton parameters: Fo: 76, 20:Po: 13, 20:DCWY4+14: Fw\_ .00] 10234+ [Previous areas: Iaper: 4.67:SLP2+2.00:LGD+ 40:-MND+ 250:SCP+ .0] 10235+ RO25:CO0267-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10236+ COMPUTE DUALHYD / 1.0 01:KE-08 4.86 .000 No\_date 0:00 0:00 n/a .000 10237+ Major System / 1.0 01:KE-08 4.86 .000 No\_date 0:00 0:00 n/a .000 10238+ Minor System / 1.0 01:KE-08 4.86 .000 No\_date 0:00 0:00 n/a .000 10239+ [MjyStcTo...\_6182+02, TotCovFvl+0000E+00, N-Ovrf+ 0, TotDurOvf+ 0,hrs] 10240+ RO25:CO0268-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10241+ COMPUTE DUALHYD / 1.0 01:KE-08 4.86 .000 No\_date 0:00 0:00 n/a .000 10242+ Major System / 1.0 01:KE-08 4.86 .000 No\_date 0:00 0:00 n/a .000 10243+ Minor System / 1.0 01:KE-08 4.86 .000 No\_date 0:00 0:00 n/a .000 10244+ [MjyStcTo...\_6182+02, TotCovFvl+0000E+00, N-Ovrf+ 0, TotDurOvf+ 0,hrs] 10245+ RO25:CO0269-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10246+ ADD HYD + 1.0 02:KE-08-MN 4.86 .000 No\_date 0:00 0:00 n/a .000 10247+ SUM+ 1.0 02:KE-08-MN 4.86 .000 No\_date 0:00 0:00 n/a .000 10248+ [Morton parameters: Fo: 76, 20:Po: 13, 20:DCWY4+14: Fw\_ .00] 10249+ [Previous areas: Iaper: 4.67:SLP2+2.00:LGD+ 40:-MND+ 250:SCP+ .0] 10250+ RO25:CO0270-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10251+ COMPUTE DUALHYD / 1.0 01:KE-08 4.86 1.059 No\_date 28:00 66.57 n/a .000 10252+ Major System / 1.0 01:KE-08 4.86 1.059 No\_date 27:56 66.57 n/a .000 10253+ Minor System / 1.0 01:KE-08 4.86 1.059 No\_date 27:56 66.57 n/a .000 10254+ [MjyStcTo...\_6182+02, TotCovFvl+0000E+00, N-Ovrf+ 0, TotDurOvf+ 0,hrs] 10255+ RO25:CO0271-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10256+ ADD HYD + 1.0 02:KE-08-MN 4.86 .000 No\_date 0:00 0:00 n/a .000 10257+ SUM+ 1.0 02:KE-08-MN 4.86 .000 No\_date 0:00 0:00 n/a .000 10258+ [Morton parameters: Fo: 76, 20:Po: 13, 20:DCWY4+14: Fw\_ .00] 10259+ [Previous areas: Iaper: 4.67:SLP2+2.00:LGD+ 40:-MND+ 250:SCP+ .0] 10260+ RO25:CO0272-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10261+ COMPUTE DUALHYD / 1.0 01:KE-08 4.86 1.059 No\_date 28:00 55.97 n/a .000 10262+ Major System / 1.0 01:KE-08 4.86 1.059 No\_date 27:55 55.97 n/a .000 10263+ Minor System / 1.0 01:KE-08 4.86 1.059 No\_date 27:55 55.97 n/a .000 10264+ [MjyStcTo...\_6182+02, TotCovFvl+0000E+00, N-Ovrf+ 0, TotDurOvf+ 0,hrs] 10265+ RO25:CO0273-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10266+ COMPUTE DUALHYD / 1.0 01:KE-08 4.86 1.059 No\_date 28:00 55.97 n/a .000 10267+ Major System / 1.0 01:KE-08 4.86 1.059 No\_date 27:55 55.97 n/a .000 10268+ Minor System / 1.0 01:KE-08 4.86 1.059 No\_date 27:55 55.97 n/a .000 10269+ [MjyStcTo...\_6182+02, TotCovFvl+0000E+00, N-Ovrf+ 0, TotDurOvf+ 0,hrs] 10270+ RO25:CO0274-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10271+ COMPUTE DUALHYD / 1.0 01:KE-08 4.86 1.059 No\_date 28:00 55.97 n/a .000 10272+ Major System / 1.0 01:KE-08 4.86 1.059 No\_date 27:55 55.97 n/a .000 10273+ Minor System / 1.0 01:KE-08 4.86 1.059 No\_date 27:55 55.97 n/a .000 10274+ [MjyStcTo...\_6182+02, TotCovFvl+0000E+00, N-Ovrf+ 0, TotDurOvf+ 0,hrs] 10275+ RO25:CO0275-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10276+ COMPUTE DUALHYD / 1.0 01:KE-08 4.86 1.059 No\_date 28:00 55.97 n/a .000 10277+ Major System / 1.0 01:KE-08 4.86 1.059 No\_date 27:55 55.97 n/a .000 10278+ Minor System / 1.0 01:KE-08 4.86 1.059 No\_date 27:55 55.97 n/a .000 10279+ [MjyStcTo...\_6182+02, TotCovFvl+0000E+00, N-Ovrf+ 0, TotDurOvf+ 0,hrs] 10280+ RO25:CO0276-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs 10281+ COMPUTE DUALHYD / 1.0 01:KE-08 4.86 1.059 No\_date 28:00 55.97 n/a .000 10282+ Major System / 1.0 01:KE-08 4.86 1.059 No\_date 27:55 55.97 n/a .000 10283+ Minor System / 1.0 01:KE-08 4.86 1.059 No\_date 27:55 55.97 n/a .000 10284+ [MjyStcTo...\_6182+02, TotCovFvl+0000E+00, N-Ovrf+ 0, TotDurOvf+ 0,hrs] 10285+ RO25:CO0277-----DTin-ID:NHYD-----ARAhA-QPEAKms-TpeakDate\_hh:mm:---Rvnn-R.C.---DFWcmcs

10473+ ROUTE CHANNEL > 1. 02:4241- 54658.44 103.518 No\_date 38:57 29.12 n/a .000

10474+ \* [ROUTE\_ID: 1.00] out > 1.01:4241-out 54658.44 103.664 No\_date 38:36 29.12 n/a .000

10475+ [L/Sm= 2.294 /...109.03m] [Vmax= 1.253\*Dmax: 2.209]

10476+ ROG25:CO3057----->Dtnin-ID:NHDY---ARAAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcmcs

10477+ ADD HVD + 1. 02:FC-04-S 12.87 .741 No\_date 27:45 53.74 n/a .000

10478+ \* 1. 02:FC-04-S 12.87 .741 No\_date 27:45 53.74 n/a .000

10479+ \* 1. 02:FC-04-S 12.87 .741 No\_date 27:45 53.74 n/a .000

10480+ \* 1. 02:FC-04-S 1.53 .153 No\_date 27:47 53.49 n/a .000

10481+ SMM+ 1. 01:SN\_KB\_X 54681.18 103.700 No\_date 38:36 29.13 n/a .000

10482+ SMM+ 1. 01:SN\_KB\_X 54681.18 103.700 No\_date 38:36 29.13 n/a .000

10483+ SAVV HYD 1. 01:SN\_KB\_X 54681.18 103.700 No\_date 38:36 29.13 n/a .000

10484+ name : SN\_KB\_0025

10485+ remark:Total inflows before Station 3633

10486+ # Hydrograph from Todd 3 (south of the Jock)

10487+ # Channel X-Section obtained from RVE Hydraulic Model - Station 3633

10488+ # JFSR 2021-02-26 change the channel length (at station 3633) from 450m to 60m and change the slope from 0.0498% to 0.2

10489+ ROG25:CO3091----->Dtnin-ID:NHDY---ARAAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcmcs

10490+ ROG25:CO3100----->Dtnin-ID:NHDY---ARAAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcmcs

10491+ [Sdtx: 1.00] out > 1. 01:NM\_TO 54681.18 103.546 No\_date 39:00 53.11 n/a .000

10492+ [L/S:n= .608 /... .247/.036]

10493+ \*\*\*\*\*

10494+ # Catchment Greenbank

10495+ # [ROUTE\_ID: 1.00] out > 1. 01:NM\_TO 54681.18 103.546 No\_date 39:00 53.11 n/a .000

10496+ \*\*\*\*\*

10497+ # Catchment Greenbank (south of the Jock)

10498+ # - JFSR 2021-01-18 add Greenbank pond as per JFSA, P598(06)-15, Jun 2016

10499+ # - JFSR 2021-01-18 update area from 37.479 ha to 36.6 ha based on GIS measurements

10500+ # - JFSR 2021-01-18 update area from 37.479 ha to 36.6 ha based on GIS measurements

10501+ ROG25:CO3110----->Dtnin-ID:NHDY---ARAAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcmcs

10502+ CONTINUOUS STANDHYD 1. 01:Greenbank 36.60 5.574 No\_date 28:02 58.33 .784 .000

10503+ [L/Sm= 2 CNm 77.0]

10504+ [Previous areas: Iaper: 4.67:SLPP:1.00:LGPd: 40.:MNP: .250:SCP: .0]

10505+ [ROUTE\_ID: 1.00] out > 1. 01:NM\_TO 54681.18 103.546 No\_date 39:00 53.11 n/a .000

10506+ [L/Sm= 31.15: SMAX=207.66: SK= .010]

10507+ [iabECimp: 4.00: IaRePercr: 4.00]

10508+ ROG25:CO3111----->Dtnin-ID:NHDY---ARAAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcmcs

10509+ ROUTE RESERVOIR > 1. 02:Greenbank 36.60 5.574 No\_date 28:02 58.33 .000

10510+ out < 1. 01:02:Greenbank 36.60 5.118 No\_date 28:01 58.33 .000

10511+ overlap < 1. 01:02:Greenbank 36.60 5.118 No\_date 28:01 58.33 .000

10512+ [MstcOuted: 87398-E 03 m3, TotVolV= .0000E+00 m3, N-Ovr= 0, TotSurfV= 0, hrs]

10513+ ROG25:CO3112----->Dtnin-ID:NHDY---ARAAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcmcs

10514+ ADD HVD + 1. 02:Greenbank\_MJ 54681.18 103.546 No\_date 39:00 53.11 n/a .000

10515+ [ROUTE\_ID: 1.00] out > 1. 02:Greenbank\_MJ 54681.18 103.546 No\_date 39:00 53.11 n/a .000

10516+ [L/Sm= 1.02:SMAX=207.66: SK= .010]

10517+ [iabECimp: 4.00: IaRePercr: 4.00]

10518+ [ROUTE\_ID: 1.00] out > 1. 01:02:Greenbank\_MJ 54717.79 103.651 No\_date 39:00 53.11 n/a .000

10519+ ROG25:CO3113----->Dtnin-ID:NHDY---ARAAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcmcs

10520+ remark:Total flows at Greenbank Drain

10521+ \*\*\*\*\*

10522+ # Catchment Todd 3

10523+ # - To Todd drain (area of the Jock)

10524+ # - JFSR 2021-01-18 add Todd 3 (area of the Jock) based on P598(04)-11

10525+ # - JFSR 2021-01-18 increase imp load by 41% per Barrenhill South MNS

10526+ # - JFSR 2021-01-18 update area from 146.015 ha based on P598(04)-11

10527+ \*\*\*\*\*

10528+ # - JFSR 2021-01-18 add "Todd\_NH1" as part of Clarke("N\_Clar\_M") and remove it from Todd

10529+ ROG25:CO3114----->Dtnin-ID:NHDY---ARAAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcmcs

10530+ CONTINUOUS STANDHYD 1. 01:TOGD\_MH2 2.10 .339 No\_date 28:00 58.33 .729 .000

10531+ [XIMP= .53:TIMEP=.57]

10532+ [ROUTE\_ID: 1.00] out > 1. 02:TOGD\_MH2 2.10 .339 No\_date 28:00 58.33 .729 .000

10533+ \*\*\*\*\*

10534+ # - JFSR 2021-01-18 add "Todd\_NH1" as part of Clarke("N\_Clar\_M") and remove it from Todd

10535+ CONTINUOUS STANDHYD 1. 01:TOGD\_MH2 2.10 .339 No\_date 28:00 58.33 .729 .000

10536+ [XIMP= .53:TIMEP=.57]

10537+ [Previous areas: Iaper: 4.67:SLPP:1.00:LGPd: 40.:MNP: .250:SCP: .0]

10538+ [Impervious areas: Iaper: 1.57:SLIP:1.00:LGPd: 118.:MNP: .013:SCI: .0]

10539+ [iabECimp: 4.00: IaRePercr: 4.00]

10540+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 54717.79 103.651 No\_date 39:00 53.11 n/a .000

10541+ ROG25:CO3115----->Dtnin-ID:NHDY---ARAAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcmcs

10542+ ADD HVD + 1. 01:02:TOGD\_MH2 54717.79 103.651 No\_date 39:00 53.11 n/a .000

10543+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 54717.79 103.651 No\_date 39:00 53.11 n/a .000

10544+ [L/Sm= 2 CNm 77.0]

10545+ [iabECimp: 4.00: IaRePercr: 4.00]

10546+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 54717.79 103.651 No\_date 39:00 53.11 n/a .000

10547+ [L/Sm= 31.15: SMAX=207.66: SK= .010]

10548+ ROG25:CO3116----->Dtnin-ID:NHDY---ARAAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcmcs

10549+ CONTINUOUS STANDHYD 1. 01:TOGD\_MH2 3.12 .000 No\_date 28:00 55.51 .729 .000

10550+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 30.23 4.269 No\_date 28:02 55.13 .741 .000

10551+ [L/Sm= 2 CNm 77.0]

10552+ [iabECimp: 4.00: IaRePercr: 4.00]

10553+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 30.23 4.269 No\_date 28:00 55.51 .729 .000

10554+ [L/Sm= 31.15: SMAX=207.66: SK= .010]

10555+ ROG25:CO3117----->Dtnin-ID:NHDY---ARAAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcmcs

10556+ CONTINUOUS STANDHYD 1. 01:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10557+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10558+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10559+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10560+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10561+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10562+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10563+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10564+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10565+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10566+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10567+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10568+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10569+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10570+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10571+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10572+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10573+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10574+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10575+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10576+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10577+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10578+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10579+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10580+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10581+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10582+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10583+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10584+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10585+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10586+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10587+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10588+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10589+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10590+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10591+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10592+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10593+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10594+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10595+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10596+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10597+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10598+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10599+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10600+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10601+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10602+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10603+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10604+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10605+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10606+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10607+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10608+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10609+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10610+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10611+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 28:00 55.51 .729 .000

10612+ ROG25:CO3122----->Dtnin-ID:NHDY---ARAAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcmcs

10613+ SMM+ 1. 01:01:SN\_TO 54838.44 103.908 No\_date 39:00 29.21 n/a .000

10614+ name : DTDN\_0205

10615+ remark:Total flows at Todd Drain

10616+ \*\*\*\*\*

10617+ # Todd Pond 3

10618+ # - Rating curve obtained from Barrenhill South MNS modeling

10619+ # - JFSR 2021-01-18 add Todd 3 (area of the Jock)

10620+ ROG25:CO3126----->Dtnin-ID:NHDY---ARAAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcmcs

10621+ ROUTE RESERVOIR > 1. 01:02:TOGD\_MH2 2.06 268 No\_date 27:54 53.60 n/a .000

10622+ overlap < 1. 01:02:TOGD\_MH2 2.06 268 No\_date 27:54 53.60 n/a .000

10623+ [MstcOuted: 8415-E 03 m3, TotVolV= .0000E+00 m3, N-Ovr= 0, TotSurfV= 0, hrs]

10624+ ROG25:CO321----->Dtnin-ID:NHDY---ARAAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcmcs

10625+ ROUTE RESERVOIR > 1. 01:02:TOGD\_MH2 2.10 .339 No\_date 27:53 53.58 n/a .000

10626+ out < 1. 01:02:TOGD\_MH2 .01 .016 No\_date 27:53 53.58 n/a .000

10627+ overlap < 1. 01:02:TOGD\_MH2 .01 .016 No\_date 27:53 53.58 n/a .000

10628+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 .01 .016 No\_date 27:53 53.58 n/a .000

10629+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 .01 .016 No\_date 27:53 53.58 n/a .000

10630+ [ROUTE\_ID: 1.00] out > 1. 01:02:TOGD\_MH2 .01 .016 No\_date 27:53 53.58 n/a .000

10631+ SMM+ 1. 01:01:SN\_TO 54838.44 103.908 No\_date 39:00 29.21 n/a .000

10632+ ROG25:CO3218----->Dtnin-ID:NHDY---ARAAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcmcs

10633+ SMM+ 1. 01:01:SN\_TO 54838.44 103.908 No\_date 39:00 29.21 n/a .000

10634+ name : SN\_TO\_0025

10635+ remark:Total inflows at Station 2462

10636+ \*\*\*\*\*

10637+ # Hydrograph from Todd drain routed to Corriag Drain

10638+ # - Primarily 2021, add Corriag subcatchments as per BSI, July 2008

10639+ ROG25:CO3229----->Dtnin-ID:NHDY---ARAAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcmcs

10640+ ROUTE CHANNEL > 1. 02:02:SN\_TO 54838.44 103.908 No\_date 39:00 29.21 n/a .000

10641+ ROUTE CHANNEL > 1. 02:02:SN\_TO 54838.44 103.668 No\_date 39:23 29.21 n/a .000

10642+ [L/S:n= .280 /... .050/.045]

10643+ [ROUTE\_ID: 1.00] out > 1. 01:02:SN\_TO 54838.44 103.908 No\_date 39:00 29.21 n/a .000

10644+ [ROUTE\_ID: 1.00] out > 1. 01:02:SN\_TO 54838.44 103.908 No\_date 39:00 29.21 n/a .000

10645+ [ROUTE\_ID: 1.00] out > 1. 01:02:SN\_TO 54838.44 103.908 No\_date 39:00 29.21 n/a .000

10646+ SMM+ 1. 01:01:SN\_TO 54838.44 103.908 No\_date 39:00 29.21 n/a .000

10647+ ADD HVD + 1. 02:02:SN\_TO 54838.44 103.668 No\_date 39:23 29.21 n/a .000

10648+ name : SN\_TO\_0025

10649+ remark:Total inflows at Station 2462

10650+ \*\*\*\*\*

10651+ # Corriag Drain (south of the Jock)

10652+ # - Primarily 2021, add Corriag subcatchments as per BSI, July 2008

10653+ ROG25:CO331----->Dtnin-ID:NHDY---ARAAh-QPEAKms-Tpeakdate\_hh:mm:--RvNm-R.C.--DWFcmcs

10654+ CONTINUOUS STANDHYD 1. 01:01:corri- 15.87 2.535 No\_date 28:01 57.01 .766 .000

10655+ [XIMP= .63:TIMEP=.63]

10656+ [L/Sm= 2 CNm 77.0]

10657+ [Previous areas: Iaper: 4.67:SLPP:1.00:LGPd: 40.:MNP: .250:SCP: .0]

10658+ [ROUTE\_ID: 1.00] out > 1. 01:01:corri- 15.87 2.535 No\_date 28:01 57.01 .766 .000

10659+ [ROUTE\_ID: 1.00] out > 1. 01:01:corri- 15.87 2.535 No\_date 28:01 57.01 .766 .000

10660+ [ROUTE\_ID: 1.00] out > 1. 01:01:corri- 15.87 2.535 No\_date 28:01 57.01 .766 .000

10661+ [ROUTE\_ID: 1.00] out > 1. 01:01:corri- 15.87 2.535 No\_date 28:01 57.01 .766 .000

10662+ [ROUTE\_ID: 1.00] out > 1. 01:01:corri- 15.87 2.535 No\_date 28:01 57.01 .766 .000

10663+ [ROUTE\_ID: 1.00] out > 1. 01:01:corri- 15.87 2.535 No\_date 28:01 57.01 .766 .000

10664+ [ROUTE\_ID: 1.00] out > 1. 01:01:corri- 15.87 2.535 No\_date 28:01 57.01 .766 .000

10665+ [ROUTE\_ID: 1.00] out > 1. 01:01:corri- 15.87 2.535 No\_date 28:01 57.01 .766 .000

10666+ [ROUTE\_ID: 1.00] out > 1. 01:01:corri- 15.87 2.535 No\_date 28:01 57.01 .766 .000

10667+ [ROUTE\_ID: 1.00] out > 1. 01:01:corri- 15.87 2.535 No\_date 28:01 57.01 .766 .000

10668+ [ROUTE\_ID: 1.00] out > 1. 01:01:corri- 15.87 2.535 No\_date 28:01 57.01 .766 .000

10669+ [ROUTE\_ID: 1.00] out > 1. 01:01:corri- 15.87 2.535 No\_date 28:01 57.01 .766 .000

10670+ [ROUTE\_ID: 1.00] out > 1. 01:01:corri- 15.87 2.535 No\_date 28:01 57.01 .766 .000

10671+ [ROUTE\_ID: 1.00] out > 1. 01:01:corri- 15.87 2.535 No\_date 28:01 57.01 .766 .000

10672+ [ROUTE\_ID: 1.00] out > 1. 01:01:corri- 15.87 2.535 No\_date 28:01 57.01 .766 .000

10673+ [ROUTE\_ID: 1.00] out > 1. 01:01:corri- 15.87 2.535 No\_date 28:01 57.01 .766 .000

10674+ [ROUTE\_ID: 1.00] out > 1. 01:01:corri- 15.87 2.535 No\_date 28:01 57.01 .766 .000</



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11222# remark:Total Flows at Jockvale Road
11223# Hydrograph from Jockvale Road routed to Heart's Desire
11224# Channel X-Section obtained from RVEA Hydraulic Model - Station 689
11225# 
11226# 80025/C04242-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11227# [ROUTE_ID: 0.0] outx > 1.0 0.01_NRE 55194.86 104.397 No_Date 39:28 29.33 n/a .000
11228# [ROUTE_ID: 0.0] outx > 1.0 0.01_NRE 55194.86 104.140 No_Date 39:48 29.33 n/a .000
11229# [L/S/n: 1962. / .223/.045]
11230# 
11231# *****#
11232# * Catchment DESIGN
11233# * - Residential area north of the Jock
11234# * - Rural-area subdivision (Heart's Desire Community)
11235# *****#
11236# 80025/C04243-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11237# CONTINUOUS STANHYD 1.0 01:DESEIRE 23.78 2.161 No_Date 28:03 40.77 .548 .000
11238# [XIMP: .25,TIMP:.05]
11239# *****#
11240# Previous area: Iapcr: 4.67:SLP1=1.00:LDP= 40..MNW=.250(SCP= .0]
11241# Impervious area: IaImp: 1.57:SLP1=1.00:LDP= 400..MNW=.013:SCI= .0]
11242# [SMMN: 31.15; SMX:207.66; SK: 010]
11243# 
11244# *****#
11245# * Catchment JOCKVA
11246# * To Jockvale SWN Facility
11247# * - Residential development & golf course update
11248# * - Residential area: 256 ha instead of 257.63 ha, JOCKVA separated into two areas JOCKVA and EX-LAND 32.5 ha as
11249# * - JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX-LAND 32.5 ha as
11250# *****#
11251# 80025/C04434-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11252# CONTINUOUS STANHYD 1.0 01:JOCKVA 225.13 21.797 No_Date 28:07 50.08 .673 .000
11253# [XIMP: .50,TIMP:.05]
11254# *****#
11255# Previous area: Iapcr: 4.67:SLP1=1.00:LDP= 40..MNW=.250(SCP= .0]
11256# Impervious area: IaImp: 1.57:SLP1=1.00:LDP= 400..MNW=.013:SCI= .0]
11257# [SMMN: 36.67; SMX:244.49; SK: 010]
11258# 
11259# 80025/C04431-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11260# ADD HYD 1.0 01:EX-LAND-NW 32.50 2.275 No_Date 27:52 50.26 n/a .000
11261# + 1.0 02:JOCKVA 225.13 21.797 No_Date 28:07 50.08 n/a .000
11262# + 1.0 02:JOC-B2-M2 .00 .000 No_Date 0:00 .00 n/a .000
11263# + 1.0 02:JOC-B2-SM .00 .000 No_Date 0:00 .00 n/a .000
11264# SUM 1.0 01:JOCKVA-TO 257.63 24.072 No_Date 28:07 50.10 n/a .000
11265# 
11266# 80025/C04432-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11267# SAVE HYD 1.0 01:JOCKVA-TO 257.63 24.072 No_Date 28:07 50.10 n/a .000
11268# 
11269# *****#
11270# remark:Total Flows at K1 first pond
11271# 
11272# * Rating Curve obtained from Jockvale Servicing Study (CDM 1989)
11273# *****#
11274# 80025/C04433-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11275# ROUTE RESERVOIR > 1.0 02:JN_NI 297.63 24.072 No_Date 39:48 50.10 n/a .000
11276# *****#
11277# overflow < 1.0 03:JO-OVF .00 .000 No_Date 0:00 .00 n/a .000
11278# *****#
11279# 80025/C04434-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11280# ADD HYD 1.0 02:JN_NI 55194.86 104.140 No_Date 39:45 29.33 n/a .000
11281# + 1.0 02:JN_NI 23.78 2.161 No_Date 28:03 40.77 .548 .000
11282# + 1.0 02:JO-OVF .00 .000 No_Date 0:00 .00 n/a .000
11283# + 1.0 02:JOCKVA 257.63 9.145 No_Date 28:07 50.10 n/a .000
11284# SUM 1.0 01:JN_NI 55194.86 104.140 No_Date 39:45 29.33 n/a .000
11285# 
11286# 80025/C04435-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11287# SAVE HYD 1.0 01:JN_NI 55194.86 104.140 No_Date 39:45 29.33 n/a .000
11288# 
11289# *****#
11290# remark:Total Flows at Heart's Desire
11291# 
11292# Channel X-Section obtained from RVEA Hydraulic Model - Station 0
11293# *****#
11294# 80025/C04436-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11295# ROUTE CHANNEL > 1.0 02:SN_NI 55476.27 104.765 No_Date 39:48 29.43 n/a .000
11296# [ROUTE_ID: 0.0] outx > 1.0 01:NI 55476.27 104.757 No_Date 39:48 29.43 n/a .000
11297# [Wmax: 1.941:Dmax: 1.134]
11298# *****#
11299# Catchment S-2
11300# - To Jock River (north and south)
11301# - Undeveloped floodplain and river
11302# *****#
11303# 80025/C04437-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11304# CONTINUOUS NASHYD 1.0 01:S-2 102.94 3.971 No_Date 28:20 30.13 .405 .000
11305# 
11306# 80025/C04438-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11307# ADD HYD 1.0 02:NI 55476.27 104.757 No_Date 39:48 29.43 n/a .000
11308# + 1.0 02:S-2 102.94 3.971 No_Date 28:20 30.13 n/a .000
11309# SUM 1.0 01:NI 55476.27 104.757 No_Date 39:48 29.43 n/a .000
11310# 
11311# 80025/C04439-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11312# SAVE HYD 1.0 01:SN_NI 55579.21 104.958 No_Date 39:48 29.43 n/a .000
11313# 
11314# *****#
11315# remark:Total Flows at Rideau River
11316# 
11317# END OF RUN - 48
11318# *****#
11319# *****#
11320# *****#
11321# *****#
11322# *****#
11323# *****#
11324# *****#
11325# *****#
11326# 80050/C0001-----START
11327# [ZERO .00 hrs on 0]
11328# [IMPERIAL .2 -(Imperial, metric output)]
11329# [NSTORM: 1]
11330# [NRUN: 0000]
11331# *****#
11332# SWHMYS Ver:15.2/Jan 2001 <BETA> / INPUT DATA FILE
11333# Project Name : [Jock River] Project Number: [1474-16]
11334# Date : 04-03-2021
11335# [ROUTE_ID: 0.0] outx > 1.0 01:NI 55476.27 104.757 No_Date 39:48 29.43 n/a .000
11336# [Wmax: 1.941:Dmax: 1.134]
11337# *****#
11338# *****#
11339# *****#
11340# *****#
11341# *****#
11342# *****#
11343# *****#
11344# *****#
11345# *****#
11346# *****#
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11358# *****#
11359# *****#
11360# *****#
11361# *****#
11362# *****#
11363# *****#
11364# *****#
11365# *****#
11366# *****#
11367# *****#
11368# *****#
11369# *****#
11370# *****#
11371# *****#
11372# *****#
11373# Average monthly Pan Evaporation data in (mm)
11374# JAN FEB MAR APR MAY JUN JUN AUG SEP OCT NOV DEC
11375# .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
11376# .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
11377# .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
11378# .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
11379# *****#
11380# *****#
11381# [APRIM: 24.000; DPKd: 8500; ADPKd: .9988]
11382# [APIMax:113.33; APDlyavg: 67.147; ADIMin: 44.87]
11383# *****#
11384# The Twp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
11385# + of 1.32
11386# 80050/C0004-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11387# CONTINUOUS NASHYD 1.0 01:JR_JN 3980.00 18.440 No_Date 39:55 30.33 .372 .000
11388# 
11389# *****#
11390# The Twp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
11391# + of 1.32
11392# 80050/C0005-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11393# CONTINUOUS NASHYD 1.0 01:JR_JN 971.00 6.937 No_Date 32:34 28.27 .347 .000
11394# 
11395# *****#
11396# [ROUTE_ID: 0.0] outx > 1.0 01:JR_JN 39.78 .000
11397# *****#
11398# [ROUTE_ID: 0.0] outx > 1.0 01:JR_JN 64.50:SMAX:430.01:SK: .010
11399# [L/S/n: 1962. / .223/.045]
11400# [InterEventtime: 12.00]
11401# 
11402# The Twp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
11403# + of 1.32
11404# 80050/C0006-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11405# CONTINUOUS NASHYD 1.0 01:JR_JN 8.912 No_Date 39:55 24.31 .298 .000
11406# 
11407# *****#
11408# CONTINUOUS NASHYD 1.0 01:JR_JN 1781.00 16.834 No_Date 32:39 36.85 .452 .000
11409# [CN: 72.0: N: 3.00: Tp: 3.91]
11410# [iAEC4: 4.00: SMIN: 39.75: SMAX:264.99: SK: 010]
11411# *****#
11412# 80050/C0010-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11413# CONTINUOUS NASHYD 1.0 01:SR_11 500.00 9.061 No_Date 29:21 31.73 .389 .000
11414# 
11415# [CN: 66.0: N: 3.00: Tp: 5.29]
11416# [iAEC4: 4.00: SMIN: 52.62: SMAX:350.79: SK: .010]
11417# [InterEventtime: 12.00]
11418# The Twp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
11419# + of 1.32
11420# 80050/C0011-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11421# CONTINUOUS NASHYD 1.0 01:SR_10 1917.00 12.342 No_Date 34:26 31.73 .389 .000
11422# 
11423# [CN: 66.0: N: 3.00: Tp: 5.29]
11424# [iAEC4: 4.00: SMIN: 52.62: SMAX:350.79: SK: .010]
11425# [InterEventtime: 12.00]
11426# The Twp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
11427# + of 1.52
11428# 80050/C0012-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11429# CONTINUOUS NASHYD 1.0 01:SR_10 5666.00 32.402 No_Date 33:52 36.85 .452 .000
11430# 
11431# [CN: 72.0: N: 3.00: Tp: 8.00]
11432# [iAEC4: 4.00: SMIN: 52.62: SMAX:350.79: SK: .010]
11433# [InterEventtime: 12.00]
11434# The Twp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
11435# + of 1.75
11436# 80050/C0013-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11437# CONTINUOUS NASHYD 1.0 01:CR_0K 8376.00 31.024 No_Date 39:59 31.73 .389 .000
11438# 
11439# [CN: 66.0: N: 3.00: Tp: 5.29]
11440# [iAEC4: 4.00: SMIN: 52.62: SMAX:350.79: SK: .010]
11441# [InterEventtime: 12.00]
11442# The Twp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
11443# + of 1.82
11444# 80050/C0014-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11445# CONTINUOUS NASHYD 1.0 01:CR_0K 1132.00 14.039 No_Date 30:53 35.35 .434 .000
11446# 
11447# [CN: 67.0: N: 3.00: Tp: 5.21]
11448# [iAEC4: 4.00: SMIN: 52.62: SMAX:287.10: SK: .010]
11449# [InterEventtime: 12.00]
11450# The Twp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
11451# + of 1.82
11452# 80050/C0015-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11453# CONTINUOUS NASHYD 1.0 01:CR_0K 4464.00 18.472 No_Date 39:59 28.95 .355 .000
11454# 
11455# [CN: 62.0: N: 3.00: Tp: 11.32]
11456# [iAEC4: 4.00: SMIN: 61.95: SMAX:412.66: SK: .010]
11457# [InterEventtime: 12.00]
11458# The Twp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
11459# + of 1.80
11460# 80050/C0016-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11461# CONTINUOUS NASHYD 1.0 01:CR_0K 131.00 2.740 No_Date 28:57 29.64 .364 .000
11462# 
11463# [CN: 67.0: N: 3.00: Tp: 5.21]
11464# [iAEC4: 4.00: SMIN: 59.42: SMAX:396.11: SK: .010]
11465# [InterEventtime: 12.00]
11466# The Twp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
11467# + of 1.82
11468# 80050/C0017-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11469# CONTINUOUS NASHYD 1.0 01:CR_0K 384.00 18.180 No_Date 38:32 31.73 .389 .000
11470# 
11471# [CN: 67.0: N: 3.00: Tp: 5.21]
11472# [iAEC4: 4.00: SMIN: 59.42: SMAX:396.11: SK: .010]
11473# [InterEventtime: 12.00]
11474# The Twp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
11475# + of 1.82
11476# 80050/C0018-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11477# CONTINUOUS NASHYD 1.0 01:CR_0K 3197.00 13.937 No_Date 36:23 25.61 .314 .000
11478# 
11479# [CN: 67.0: N: 3.00: Tp: 5.21]
11480# [iAEC4: 4.00: SMIN: 59.42: SMAX:508.81: SK: .010]
11481# [InterEventtime: 12.00]
11482# The Twp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
11483# + of 1.75
11484# 80050/C0019-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11485# CONTINUOUS NASHYD 1.0 01:CR_0K 165.00 1.285 No_Date 38:02 32.44 .398 .000
11486# 
11487# [CN: 67.0: N: 3.00: Tp: 4.18]
11488# [iAEC4: 4.00: SMIN: 50.55: SMAX:336.97: SK: .010]
11489# [InterEventtime: 12.00]
11490# The Twp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
11491# + of 1.82
11492# 80050/C0020-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11493# CONTINUOUS NASHYD 1.0 01:CR_0K 1332.00 9.332 No_Date 35:12 36.85 .452 .000
11494# 
11495# [CN: 67.0: N: 3.00: Tp: 5.21]
11496# [iAEC4: 4.00: SMIN: 39.75: SMAX:264.99: SK: .010]
11497# [InterEventtime: 12.00]
11498# The Twp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
11499# + of 1.75
11500# 80050/C0021-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11501# CONTINUOUS NASHYD 1.0 01:CR_0K 384.00 18.187 No_Date 28:45 41.51 .509 .000
11502# 
11503# [CN: 67.0: N: 3.00: Tp: 5.21]
11504# [iAEC4: 4.00: SMIN: 25.21: SMAX:207.66: SK: .010]
11505# [InterEventtime: 12.00]
11506# The Twp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
11507# + of 1.20
11508# 80050/C0022-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11509# CONTINUOUS NASHYD 1.0 01:CR_0K 224.00 8.187 No_Date 32:45 41.51 .509 .000
11510# 
11511# [CN: 67.0: N: 3.00: Tp: 4.18]
11512# [iAEC4: 4.00: SMIN: 50.55: SMAX:336.97: SK: .010]
11513# [InterEventtime: 12.00]
11514# The Twp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
11515# + of 1.20
11516# The Twp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
11517# + of 1.20
11518# 80050/C0024-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11519# CONTINUOUS NASHYD 1.0 01:WS_5A1 1412.00 8.794 No_Date 37:48 39.93 .490 .000
11520# 
11521# [CN: 74.0: N: 3.00: Tp: 4.45]
11522# [iAEC4: 4.00: SMIN: 36.67: SMAX:244.99: SK: .010]
11523# [InterEventtime: 12.00]
11524# 80050/C0025-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11525# CONTINUOUS NASHYD 1.0 01:WS_5A2 585.00 12.896 No_Date 29:55 45.60 .560 .000
11526# 
11527# [CN: 81.0: N: 3.00: Tp: 7.51]
11528# [iAEC4: 4.00: SMIN: 21.00: SMAX:168.09: SK: .010]
11529# [InterEventtime: 12.00]
11530# 80050/C0026-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11531# CONTINUOUS NASHYD 1.0 01:WS_5A3 1021.00 17.059 No_Date 30:46 44.77 .549 .000
11532# 
11533# [CN: 80.0: N: 3.00: Tp: 2.46]
11534# [iAEC4: 4.00: SMIN: 26.32: SMAX:175.50: SK: .010]
11535# [InterEventtime: 12.00]
11536# 80050/C0027-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11537# CONTINUOUS NASHYD 1.0 01:WS_5A2 177.00 6.469 No_Date 28:45 41.51 .509 .000
11538# 
11539# [CN: 80.0: N: 3.00: Tp: 2.46]
11540# [iAEC4: 4.00: SMIN: 31.15: SMAX:207.66: SK: .010]
11541# [InterEventtime: 12.00]
11542# The Twp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
11543# + of 1.20
11544# 80050/C0029-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11545# CONTINUOUS NASHYD 1.0 01:WS_5A2 273.00 34.946 No_Date 31:29 40.72 .500 .000
11546# 
11547# [CN: 74.0: N: 3.00: Tp: 3.03]
11548# [iAEC4: 4.00: SMIN: 32.46: SMAX:216.39: SK: .010]
11549# [InterEventtime: 12.00]
11550# The Twp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
11551# Starting with the addition of Jock River Headwater and Subwatershed 13
11552# 80050/C0030-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11553# CONTINUOUS NASHYD 1.0 01:JR_JN 1122.00 15.544 No_Date 31:43 45.40 .560 .000
11554# 
11555# [CN: 81.0: N: 3.00: Tp: 3.25]
11556# [iAEC4: 4.00: SMIN: 26.32: SMAX:168.09: SK: .010]
11557# [InterEventtime: 12.00]
11558# The following parameters were used in NASHYD
11559# [APXIM: 24.000; SMAX: 216.000]
11560# [n=0.04 for summer conditions and n=0.025 for spring conditions]
11561# [ROUTE CHANNEL: > 1.0 02:JR_N1]
11562# 80050/C0031-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11563# ROUTE CHANNEL: > 1.0 01:NI_N1A 4651.00 23.559 No_Date 35:24 29.90 n/a .000
11564# [ROUTE CHANNEL: > 1.0 02:JR_N1A 4651.00 19.136 No_Date 39:06 29.90 n/a .000
11565# [ROUTE CHANNEL: > 1.0 02:JR_N1A 4651.00 23.559 No_Date 35:24 29.90 n/a .000
11566# [ROUTE CHANNEL: > 1.0 02:JR_N1A 4651.00 23.559 No_Date 35:24 29.90 n/a .000
11567# [ROUTE CHANNEL: > 1.0 02:JR_N1A 4651.00 23.559 No_Date 35:24 29.90 n/a .000
11568# [ROUTE CHANNEL: > 1.0 02:JR_N1A 4651.00 23.559 No_Date 35:24 29.90 n/a .000
11569# [ROUTE CHANNEL: > 1.0 02:JR_N1A 4651.00 23.559 No_Date 35:24 29.90 n/a .000
11570# [ROUTE CHANNEL: > 1.0 02:JR_N1A 4651.00 19.336 No_Date 39:06 29.90 n/a .000
11571# [ROUTE CHANNEL: > 1.0 02:JR_N1A 4651.00 19.336 No_Date 39:06 29.90 n/a .000
11572# [ROUTE CHANNEL: > 1.0 02:JR_N1A 4651.00 19.336 No_Date 39:06 29.90 n/a .000
11573# [ROUTE CHANNEL: > 1.0 02:JR_N1A 4651.00 19.336 No_Date 39:06 29.90 n/a .000
11574# [ROUTE CHANNEL: > 1.0 02:JR_N1A 4651.00 19.336 No_Date 39:06 29.90 n/a .000
11575# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
11576# 80050/C0032-----DTrin-ID:NHDY---AREAbn_QPEAKcms-TpeakDate.bb:hh---RvNm-R.C.--DWFcms
11577# CONTINUOUS NASHYD 1.0 01:WS_5A1 725.00 27.399 No_Date 39:54 27.68 n/a .000
11578# ROUTE RESERVOIR > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11579# ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11580# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11581# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11582# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11583# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11584# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11585# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11586# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11587# Output of Reservoir Goodwood March routed from Node 13 to Node 12
11588# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11589# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11590# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11591# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11592# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11593# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11594# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11595# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11596# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11597# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11598# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11599# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11600# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11601# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11602# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11603# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11604# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11605# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11606# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11607# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11608# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No_Date 39:54 27.68 n/a .000
11609# [ROUTE CHANNEL: > 1.0 02:NI_N1A 725.00 27.399 No
```

11595+ # Addition of Subwatershed Jock River at Ashton to Node 12  
 11596+ #  
 11597+ R0505:00036-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11598+ ADD HYD 1. 0 021N12 7725.00 3.804 No\_date 64:19 27.68 n/a .000  
 11599+ \* 1. 0 021N12 1781.00 1.056 No\_date 64:19 27.68 n/a .000  
 11600+ SUM+ 1. 0 01S\_N12 15.847 No\_date 32:42 29.39 n/a .000  
 11601+ R0505:00037-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11602+ SUM+ 1. 0 01S\_N12 9506.00 18.867 No\_date 32:42 29.39 n/a .000  
 11603+ frame \_H\_SNN12  
 11604+ remark:flow at S\_M12 near Ashton  
 11605+ #  
 11606+ # Sum of hydrographs from Node 12 routed to Node 11  
 11607+ # (Approximated cross-section - see cross-section 258)  
 11608+ # Use n=0.04 for summer conditions and n=0.028 for spring conditions  
 11609+ #  
 11610+ # Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248  
 11611+ #  
 11612+ R0505:00038-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11613+ ROUTE CHANNEL > 1. 0 021S\_N12 9506.00 18.867 No\_date 32:42 29.39 n/a .000  
 11614+ \* 1. 0 021S\_N12 20.490 No\_date 32:42 29.39 n/a .000  
 11615+ [L/S/nr .972 +/- .054/.140] [Vmax=.751:Dmax=.329]  
 11616+ #  
 11617+ # Addition of Subwatershed 11 and No Name Creek to Node 11  
 11618+ #  
 11619+ R0505:00039-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11620+ ADD HYD 1. 0 021N11 9506.00 18.687 No\_date 32:59 29.39 n/a .000  
 11621+ \* 1. 0 021N11 5666.00 5.061 No\_date 32:59 29.39 n/a .000  
 11622+ SUM+ 1. 0 01S\_N11 12.346 No\_date 34:06 33.83 n/a .000  
 11623+ \* 1. 0 01S\_N11 11923.00 32.881 No\_date 33:00 29.87 n/a .000  
 11624+ #  
 11625+ # Sum of hydrographs from Node 11 routed to Node 10  
 11626+ # Section 1  
 11627+ R0505:00040-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11628+ ADD HYD 1. 0 021N10 11923.00 20.490 No\_date 40:02 29.87 n/a .000  
 11629+ \* 1. 0 021N10 5666.00 32.402 No\_date 37:52 36.85 n/a .000  
 11630+ SUM+ 1. 0 01S\_N10 17888.00 52.600 No\_date 38:19 32.15 n/a .000  
 11631+ frame \_H\_SNN10  
 11632+ remark:flow at S\_M10 N10\_SW\_10  
 11633+ # Addition of King's Creek to S\_M10  
 11634+ #  
 11635+ R0505:00043-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11636+ ADD HYD 1. 0 021N10 17889.00 52.600 No\_date 38:19 32.12 n/a .000  
 11637+ \* 1. 0 021N10 4876.00 31.024 No\_date 39:59 31.73 n/a .000  
 11638+ SUM+ 1. 0 01S\_N10 25985.00 82.746 No\_date 39:48 31.99 n/a .000  
 11639+ #  
 11640+ # Sum of hydrographs from Node 10 routed to Node 9  
 11641+ # Section 2  
 11642+ R0505:00044-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11643+ ADD HYD 1. 0 021N10 28665.00 80.380 No\_date 39:59 31.99 n/a .000  
 11644+ \* 1. 0 021N10 1132.00 14.039 No\_date 30:53 35.35 n/a .000  
 11645+ \* 1. 0 021N10 4464.00 15.472 No\_date 39:59 28.95 n/a .000  
 11646+ SUM+ 1. 0 01S\_N10 31561.00 99.424 No\_date 39:59 31.68 n/a .000  
 11647+ #  
 11648+ # Addition of Subwatershed 9 and Nichols Creek to Node 9  
 11649+ #  
 11650+ R0505:00045-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11651+ ADD HYD 1. 0 021N10 31561.00 99.424 No\_date 39:59 31.68 n/a .000  
 11652+ \* 1. 0 021N10 1132.00 14.039 No\_date 30:53 35.35 n/a .000  
 11653+ \* 1. 0 021N10 4464.00 15.472 No\_date 39:59 28.95 n/a .000  
 11654+ SUM+ 1. 0 01S\_N10 31561.00 99.424 No\_date 39:59 31.68 n/a .000  
 11655+ #  
 11656+ # Sum of hydrographs from Node 9 routed to Node 8  
 11657+ # Section 3  
 11658+ R0505:00046-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11659+ ROUTE CHANNEL > 1. 0 021S\_N10A 25965.00 82.746 No\_date 39:45 31.99 n/a .000  
 11660+ \* [RDt= 1.00] out< 1. 0 01N\_N9 25965.00 80.980 No\_date 39:59 31.99 n/a .000  
 11661+ [L/S/nr .389 +/- .075/.048] [Vmax=.441:Dmax=.2 015]  
 11662+ #  
 11663+ # Addition of Subwatershed 8 and Nichols Creek to Node 8  
 11664+ #  
 11665+ R0505:00047-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11666+ ADD HYD 1. 0 021N10 31561.00 99.424 No\_date 39:59 31.68 n/a .000  
 11667+ \* 1. 0 021N10 1132.00 14.039 No\_date 30:53 35.35 n/a .000  
 11668+ \* 1. 0 021N10 4464.00 15.472 No\_date 39:59 28.95 n/a .000  
 11669+ SUM+ 1. 0 01S\_N10 31561.00 99.424 No\_date 39:59 31.68 n/a .000  
 11670+ #  
 11671+ # Sum of hydrographs from Node 8 routed to Node 7  
 11672+ # Section 4  
 11673+ R0505:00048-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11674+ ROUTE CHANNEL > 1. 0 021S\_N10 35546.00 111.843 No\_date 39:59 31.68 n/a .000  
 11675+ \* [RDt= 1.00] out< 1. 0 01N\_N8 35546.00 95.475 No\_date 44:55 31.68 n/a .000  
 11676+ [L/S/nr .2269 / .053/.070] [Vmax=.537:Dmax=.2 290]  
 11677+ #  
 11678+ # Addition of Subwatershed 8 and Hobbs Drain to Node 8  
 11679+ #  
 11680+ R0505:00049-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11681+ ADD HYD 1. 0 021N10 35546.00 111.843 No\_date 39:59 31.68 n/a .000  
 11682+ \* 1. 0 021N10 1132.00 14.039 No\_date 30:53 35.35 n/a .000  
 11683+ \* 1. 0 021N10 4464.00 15.472 No\_date 39:59 28.95 n/a .000  
 11684+ SUM+ 1. 0 01S\_N10 35546.00 111.843 No\_date 39:59 31.68 n/a .000  
 11685+ #  
 11686+ # Sum of hydrographs from Node 8 routed to Node 7  
 11687+ # Section 5  
 11688+ R0505:00050-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11689+ ADD HYD 1. 0 021N10 38743.00 102.892 No\_date 43:46 31.18 n/a .000  
 11690+ \* 1. 0 021N10 56.00 1.748 No\_date 28:57 34.84 n/a .000  
 11691+ \* 1. 0 021N10 3894.00 16.180 No\_date 38:32 31.73 n/a .000  
 11692+ SUM+ 1. 0 01S\_N10 38743.00 102.892 No\_date 43:46 31.18 n/a .000  
 11693+ frame \_H\_SNN10  
 11694+ remark:flow at S\_M7: N7\_SW\_1  
 11695+ # In addition to flow, simulate the effects of the Richmond Fen.  
 11696+ # Storage area and storage release were assumed to be controlled by the downstream  
 11697+ # Release rate from fen was assumed to be controlled by the downstream  
 11698+ # storage area. This assumption was made because it was felt that for up to  
 11699+ # 0.75 m of water, the main channel of the river provided the storage. Above  
 11700+ # this depth, the wetland starts to significantly store water.  
 11701+ #  
 11702+ R0505:00051-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11703+ ADD HYD 1. 0 021N10 38743.00 102.892 No\_date 43:46 31.18 n/a .000  
 11704+ \* 1. 0 021N10 56.00 1.748 No\_date 28:57 34.84 n/a .000  
 11705+ \* 1. 0 021N10 3894.00 16.180 No\_date 38:32 31.73 n/a .000  
 11706+ SUM+ 1. 0 01S\_N10 38743.00 102.892 No\_date 43:46 31.18 n/a .000  
 11707+ frame \_H\_SNN10  
 11708+ #  
 11709+ # Addition of Subwatershed 7 to Node 7  
 11710+ #  
 11711+ R0505:00049-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11712+ ADD HYD 1. 0 021N10 38743.00 102.892 No\_date 43:46 31.18 n/a .000  
 11713+ \* 1. 0 021N10 56.00 1.748 No\_date 28:57 34.84 n/a .000  
 11714+ \* 1. 0 021N10 3894.00 16.180 No\_date 38:32 31.73 n/a .000  
 11715+ SUM+ 1. 0 01S\_N10 38743.00 102.892 No\_date 43:46 31.18 n/a .000  
 11716+ frame \_H\_SNN10  
 11717+ #  
 11718+ # Sum of hydrographs from Node 7 routed to Node 6  
 11719+ # Section 5  
 11720+ R0505:00052-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11721+ ADD HYD 1. 0 021N10 38743.00 102.892 No\_date 43:46 31.18 n/a .000  
 11722+ \* 1. 0 021N10 56.00 1.748 No\_date 28:57 34.84 n/a .000  
 11723+ \* 1. 0 021N10 3894.00 16.180 No\_date 38:32 31.73 n/a .000  
 11724+ SUM+ 1. 0 01S\_N10 38743.00 102.892 No\_date 43:46 31.18 n/a .000  
 11725+ frame \_H\_SNN10  
 11726+ #  
 11727+ # Addition of Subwatershed 6 and Gaal Drain to Node 6  
 11728+ #  
 11729+ R0505:00054-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11730+ ADD HYD 1. 0 021N10 38743.00 102.892 No\_date 43:46 31.18 n/a .000  
 11731+ \* 1. 0 021N10 56.00 1.748 No\_date 28:57 34.84 n/a .000  
 11732+ \* 1. 0 021N10 3894.00 16.180 No\_date 38:32 31.73 n/a .000  
 11733+ SUM+ 1. 0 01S\_N10 38743.00 102.892 No\_date 43:46 31.18 n/a .000  
 11734+ frame \_H\_SNN10  
 11735+ #  
 11736+ # Sum of hydrographs from Node 6 routed to Node 5  
 11737+ # Section 6  
 11738+ R0505:00055-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11739+ ADD HYD 1. 0 021N10 38743.00 102.892 No\_date 43:46 31.18 n/a .000  
 11740+ \* 1. 0 021N10 56.00 1.748 No\_date 28:57 34.84 n/a .000  
 11741+ \* 1. 0 021N10 3894.00 16.180 No\_date 38:32 31.73 n/a .000  
 11742+ SUM+ 1. 0 01S\_N10 38743.00 102.892 No\_date 43:46 31.18 n/a .000  
 11743+ frame \_H\_SNN10  
 11744+ #  
 11745+ R0505:00056-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11746+ ADD HYD 1. 0 021N10 40240.01 51.810 No\_date 60:20 31.37 n/a .000  
 11747+ \* 1. 0 021N10 224.00 8.187 No\_date 28:45 41.51 n/a .000  
 11748+ \* 1. 0 021N10 44.620 No\_date 30:48 38.31 n/a .000  
 11749+ SUM+ 1. 0 01S\_N10 45409.01 51.814 No\_date 34:20 32.18 n/a .000  
 11750+ frame \_H\_SNN10  
 11751+ #  
 11752+ # Sum of hydrographs from Node 5 routed to Node 4  
 11753+ # Section 7  
 11754+ R0505:00057-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11755+ ADD HYD 1. 0 021N10 45409.01 71.514 No\_date 34:20 32.18 n/a .000  
 11756+ \* 1. 0 021N10 20.00 .943 No\_date 28:35 45.60 n/a .000  
 11757+ SUM+ 1. 0 01S\_N10 45409.01 71.514 No\_date 34:20 32.18 n/a .000  
 11758+ frame \_H\_SNN10  
 11759+ #  
 11760+ # Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A  
 11761+ #  
 11762+ R0505:00058-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11763+ ADD HYD 1. 0 021NSA 45409.01 71.311 No\_date 34:15 32.18 n/a .000  
 11764+ \* 1. 0 021NSA 14.00 3.094 No\_date 28:35 38.31 n/a .000  
 11765+ SUM+ 1. 0 01S\_N5A 45409.01 71.314 No\_date 34:46 32.42 n/a .000  
 11766+ #  
 11767+ # Sum of hydrographs from Node 5 routed to Node 4  
 11768+ # Section 8  
 11769+ R0505:00059-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11770+ ROUTE CHANNEL > 1. 0 021S\_N5A 46841.01 79.247 No\_date 34:46 32.42 n/a .000  
 11771+ \* 1. 0 01NSA 46841.01 79.833 No\_date 36:02 32.42 n/a .000  
 11772+ #  
 11773+ # Addition of Subwatershed 4 and Leamy Creek to Node 4  
 11774+ #  
 11775+ R0505:00058-----Dtnin:ID:NHYD---->AREAbn-QPEAKcms-TpeakDate\_hh:mm:---RvNm-R.C.--DWFcms  
 11776+ ROUTE CHANNEL > 1. 0 021S\_N5A 46841.01 79.247 No\_date 34:46 32.42 n/a .000  
 11777+ \* 1. 0 01NSA 46841.01 79.833 No\_date 36:02 32.42 n/a .000  
 11778+ #  
 11779+ # Addition of Subwatershed 4 and Leamy Creek to Node 4

11969+ R0505:00089----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 11970+ ROUTE RESERVATION > 1. 0. 021A1 2.50 .517 No\_date 28:16 64.40 n/a .000  
 11971+ [Previous areas Iaper: 4.67SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 11972+ [Inferiorous areas IAlmp: 1.57SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 11973+ [Mortn params: 77424E-01 m3 TottvVol=00000..m3 No-Vol= 0. TotDurVrf= 0. hrs]  
 11974+ R0505:00090----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 11975+ CONTINUOUS STANDYD 1. 01 01ST-2 .59 .103 No\_date 28:00 50.67 .622 .000  
 11976+ [XMP= 64:TIME= .57]  
 11977+ [Previous areas Iaper: 4.671SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 11978+ [Inferiorous areas IAlmp: 1.571SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 11979+ R0505:00091----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 11980+ ROUTE RESERVATION > 1. 0. 021A1 2.50 .517 No\_date 28:16 64.40 n/a .000  
 11981+ [Previous areas Iaper: 4.671SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 11982+ [Inferiorous areas IAlmp: 1.571SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 11983+ [Route Pipe <= 1. 0. 01ST20W00..05 ..05 ..000 No\_date 0:00 .0/n/a .000  
 11984+ [Overflow <= 1. 0. 01ST20W00..05 ..05 ..000 No\_date 0:00 .0/n/a .000  
 11985+ [Mortn params: 3192E-01 m3 TottvVol=00000..m3 No-Vol= 0. TotDurVrf= 0. hrs]  
 11986+ R0505:00092----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 11987+ CONTINUOUS NASHYD 1. 01 01ST-8 60.55 1.383 No\_date 28:04 33.66 .413 .000  
 11988+ [XMP= 64:TIME= .85]  
 11989+ [IaECm= 4.00 SMM= 44.821 SMX=299.82: Ska .010]  
 11990+ [InterEventTime: 12.00]  
 11991+ R0505:00093----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 11992+ ROUTE PIPE > -> 1. 0. 021-0 8 60.55 1.383 No\_date 29:04 33.66 n/a .000  
 11993+ [RDT= 1.00] out-> 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 11994+ [Inferiorous areas IAlmp: 1.57SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 11995+ [Vmax= 1.244:Max= 617]  
 11996+ [HGT= 1.20:WDTH= 1.80]  
 11997+ R0505:00094----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 11998+ ADD HYD 1. 021DRAIN 261.31 4.883 No\_date 28:25 25.81 n/a .000  
 11999+ + 1. 0. 021D1 1.17 .094 No\_date 28:12 43.70 n/a .000  
 12000+ [Inferiorous areas IAlmp: 1.571SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12001+ + 1. 0. 021A1-OVF .000 No\_date 0:00 .0/n/a .000  
 12002+ + 1. 0. 021ST27P 59.50 .052 No\_date 28:11 50.67 n/a .000  
 12003+ [Inferiorous areas IAlmp: 1.571SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12004+ + 1. 0. 0208PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12005+ SUM- 1. 0. 021ST2N 126.12 6.061 No\_date 28:35 25.75 n/a .000  
 12006+ R0505:00095----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12007+ CONTINUOUS STANDYD 1. 01 01AT-7 .75 .123 No\_date 28:20 50.67 .622 .000  
 12008+ [XMP= 64:TIME= .85]  
 12009+ [Previous areas Iaper: 4.671SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12010+ [Inferiorous areas IAlmp: 1.571SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12011+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12012+ [Overflow <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12013+ R0505:00096----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12014+ ROUTE RESERVATION > 1. 0. 021A7 3.51 .704 No\_date 28:01 64.40 n/a .000  
 12015+ [Previous areas IAlmp: 1.571SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12016+ [Route Pipe <= 1. 0. 031AT-0W ..05 ..000 No\_date 0:00 .0/n/a .000  
 12017+ [Overflow <= 1. 0. 031AT-0W ..05 ..000 No\_date 0:00 .0/n/a .000  
 12018+ R0505:00097----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12019+ CONTINUOUS STANDYD 1. 01 01AT-3 .75 .123 No\_date 28:20 50.67 .622 .000  
 12020+ [XMP= 64:TIME= .85]  
 12021+ [Mortn parameters: Po: 76.201Pc 13.20DCX4/14: Fe .00]  
 12022+ [Previous areas Iaper: 4.671SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12023+ [Inferiorous areas IAlmp: 1.571SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12024+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12025+ R0505:00098----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12026+ ROUTE RESERVATION > 1. 0. 021A7 3.51 .704 No\_date 28:01 64.40 n/a .000  
 12027+ [Previous areas IAlmp: 1.571SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12028+ [Route Pipe <= 1. 0. 031AT-0W ..05 ..000 No\_date 0:00 .0/n/a .000  
 12029+ [Overflow <= 1. 0. 031AT-0W ..05 ..000 No\_date 0:00 .0/n/a .000  
 12030+ R0505:00099----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12031+ ADD HYD 1. 021DRAIN 326.12 6.061 No\_date 28:35 27.67 n/a .000  
 12032+ [Inferiorous areas IAlmp: 1.571SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12033+ + 1. 0. 021A1-OVF .000 No\_date 0:00 .0/n/a .000  
 12034+ + 1. 0. 021ST35P 76.03 .063 No\_date 28:11 50.67 n/a .000  
 12035+ [Inferiorous areas IAlmp: 1.571SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12036+ SUM- 1. 0. 021ST2N 330.34 6.299 No\_date 28:33 28.11 n/a .000  
 12037+ R0505:00100----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12038+ ROUTE CHANNEL > 1. 0. 021A1 2.50 .074 No\_date 29:02 43.70 .536 .000  
 12039+ [L/S/n= 592 / .230/.043]  
 12040+ [RDT= 1.00] out-> 1. 0. 01DRAINS 330.34 5.789 No\_date 28:58 28.11 n/a .000  
 12041+ [Inferiorous areas IAlmp: 1.571SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12042+ R0505:00101----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12043+ CONTINUOUS NASHYD 1. 01 01D 2.26 .074 No\_date 29:02 43.70 .536 .000  
 12044+ [XMP= 64:TIME= .05]  
 12045+ [IaECm= 4.00 SMM= 12.01 SMX=140.62: Ska .010]  
 12046+ [InterEventTime: 12.00]  
 12047+ R0505:00102----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12048+ CONTINUOUS STANDYD 1. 01 01A17 12.04 2.163 No\_date 28:03 64.42 .790 .000  
 12049+ [XMP= 64:TIME= .85]  
 12050+ [Previous areas Iaper: 4.671SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12051+ [Inferiorous areas IAlmp: 1.571SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12052+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12053+ [Overflow <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12054+ R0505:00103----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12055+ ROUTE RESERVATION > 1. 0. 021A1 12.04 2.163 No\_date 28:01 64.40 n/a .000  
 12056+ [Previous areas IAlmp: 1.571SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12057+ [Route Pipe <= 1. 0. 031AT-0W ..05 ..000 No\_date 0:00 .0/n/a .000  
 12058+ [Overflow <= 1. 0. 031AT-0W ..05 ..000 No\_date 0:00 .0/n/a .000  
 12059+ R0505:00104----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12060+ CONTINUOUS STANDYD 1. 01 01ST-4 5.30 .063 No\_date 28:00 50.67 .622 .000  
 12061+ [XMP= 64:TIME= .57]  
 12062+ [Previous areas Iaper: 4.671SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12063+ [Inferiorous areas IAlmp: 1.571SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12064+ R0505:00105----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12065+ ROUTE RESERVATION > 1. 0. 021A1 3.51 .704 No\_date 28:01 64.40 n/a .000  
 12066+ [Previous areas IAlmp: 1.571SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12067+ [Route Pipe <= 1. 0. 031AT-0W ..05 ..000 No\_date 0:00 .0/n/a .000  
 12068+ [Overflow <= 1. 0. 031AT-0W ..05 ..000 No\_date 0:00 .0/n/a .000  
 12069+ R0505:00106----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12070+ CONTINUOUS STANDYD 1. 01 01A18 5.30 .690 No\_date 28:01 64.42 .790 .000  
 12071+ [XMP= 64:TIME= .05]  
 12072+ R0505:00107----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12073+ [Route Channel <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12074+ [Mortn parameters: Po: 76.201Pc 13.20DCX4/14: Fe .00]  
 12075+ [Previous areas Iaper: 4.671SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12076+ [Inferiorous areas IAlmp: 1.571SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12077+ R0505:00108----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12078+ CONTINUOUS STANDYD 1. 01 01A18 2.51 .113 No\_date 28:43 47.27 .580 .000  
 12079+ [XMP= 64:TIME= .05]  
 12080+ [Route Pipe <= 1. 0. 01A18STP 5.30 ..028 ..000 No\_date 28:22 64.40 n/a .000  
 12081+ [Overflow <= 1. 0. 01A18STP 5.30 ..028 ..000 No\_date 28:22 64.40 n/a .000  
 12082+ R0505:00109----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12083+ ADD HYD 1. 0. 021A1 35 ..028 ..000 No\_date 28:10 50.67 .622 .000  
 12084+ [Inferiorous areas IAlmp: 1.571SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12085+ [Route Pipe <= 1. 0. 031AT-0W ..05 ..000 No\_date 0:00 .0/n/a .000  
 12086+ [Overflow <= 1. 0. 031AT-0W ..05 ..000 No\_date 0:00 .0/n/a .000  
 12087+ R0505:00110----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12088+ ADD HYD 1. 0. 021A1 35 ..028 ..000 No\_date 28:10 50.67 .622 .000  
 12089+ [Inferiorous areas IAlmp: 1.571SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12090+ [Route Pipe <= 1. 0. 031AT-0W ..05 ..000 No\_date 0:00 .0/n/a .000  
 12091+ R0505:00111----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12092+ CONTINUOUS STANDYD 1. 01 01A18 350.31 6.632 No\_date 28:55 30.03 n/a .000  
 12093+ [Route Channel <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12094+ [RDT= 1.00] out-> 1. 0. 01DRAINS 350.31 6.632 No\_date 28:55 30.03 n/a .000  
 12095+ [Inferiorous areas IAlmp: 1.571SLPP...50:LGD= 50..MNP= 250:SCP= .0]  
 12096+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12097+ R0505:00112----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12098+ CONTINUOUS STANDYD 1. 01 01C 3.41 ..690 No\_date 28:01 64.42 .790 .000  
 12099+ [XMP= 64:TIME= .05]  
 12100+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12101+ R0505:00113----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12102+ CONTINUOUS STANDYD 1. 01 01ST-5 45 ..079 No\_date 28:00 50.67 .622 .000  
 12103+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12104+ R0505:00114----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12105+ CONTINUOUS STANDYD 1. 01 01ST-2 3.41 ..194 No\_date 28:20 64.42 n/a .000  
 12106+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12107+ R0505:00115----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12108+ CONTINUOUS STANDYD 1. 01 01ST-2 3.41 ..194 No\_date 28:20 64.42 n/a .000  
 12109+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12110+ R0505:00116----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12111+ CONTINUOUS STANDYD 1. 01 01ST-2 3.41 ..194 No\_date 28:20 64.42 n/a .000  
 12112+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12113+ R0505:00117----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12114+ CONTINUOUS STANDYD 1. 01 01ST-2 3.41 ..194 No\_date 28:20 64.42 n/a .000  
 12115+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12116+ R0505:00118----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12117+ CONTINUOUS STANDYD 1. 01 01ST-2 3.41 ..194 No\_date 28:20 64.42 n/a .000  
 12118+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12119+ R0505:00119----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12120+ CONTINUOUS STANDYD 1. 01 01ST-2 3.41 ..194 No\_date 28:20 64.42 n/a .000  
 12121+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12122+ R0505:00120----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12123+ CONTINUOUS STANDYD 1. 01 01ST-2 3.41 ..194 No\_date 28:20 64.42 n/a .000  
 12124+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12125+ R0505:00121----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12126+ CONTINUOUS STANDYD 1. 01 01ST-2 3.41 ..194 No\_date 28:20 64.42 n/a .000  
 12127+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12128+ R0505:00122----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12129+ CONTINUOUS STANDYD 1. 01 01ST-2 3.41 ..194 No\_date 28:20 64.42 n/a .000  
 12130+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12131+ R0505:00123----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12132+ CONTINUOUS STANDYD 1. 01 01ST-2 3.41 ..194 No\_date 28:20 64.42 n/a .000  
 12133+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12134+ R0505:00124----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12135+ CONTINUOUS STANDYD 1. 01 01ST-2 3.41 ..194 No\_date 28:20 64.42 n/a .000  
 12136+ CONTINUOUS STANDYD 1. 01 01ST-2 3.41 ..194 No\_date 28:20 64.42 n/a .000  
 12137+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12138+ R0505:00125----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12139+ CONTINUOUS STANDYD 1. 01 01ST-2 3.41 ..194 No\_date 28:20 64.42 n/a .000  
 12140+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12141+ R0505:00126----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12142+ CONTINUOUS STANDYD 1. 01 01ST-2 3.41 ..194 No\_date 28:20 64.42 n/a .000  
 12143+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12144+ R0505:00127----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12145+ CONTINUOUS STANDYD 1. 01 01ST-2 3.41 ..194 No\_date 28:20 64.42 n/a .000  
 12146+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12147+ R0505:00128----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12148+ ADD HYD 1. 0. 021ST-E 356.68 6.575 No\_date 29:09 30.51 n/a .000  
 12149+ + 1. 0. 021ST-E 7.59 ..193 No\_date 29:03 62.94 n/a .000  
 12150+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12151+ R0505:00129----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12152+ CONTINUOUS STANDYD 1. 01 01ST-2 3.41 ..194 No\_date 28:09 31.19 n/a .000  
 12153+ [Route Pipe <= 1. 0. 0108PIPE 60.55 1.376 No\_date 29:07 33.66 n/a .000  
 12154+ R0505:00130----- Dtnin-ID:NHYD----- ARRAh-QPEAKcms-Tpeakdate\_bh:mm---RVm-B.C.---DFWcmcs  
 12155+ SAVE HYD 1. 0. 01SSAC0T 364.27 6.711 No\_date 29:09 31.19 n/a .000  
 12156+ name:SSAC0T.0050  
 12157+ remark:SSAC0T.0050





13091> + 1. 0 02:KB-12-S 4.86 .867 No\_date 28:09 69.93 n/a .000

13092> + 1. 0 02:KB-13-S 10.15 1.722 No\_date 27:10 60.04 n/a .000

13093> + 1. 0 02:KB-14-S 5.47 1.003 No\_date 28:03 60.04 n/a .000

13094> + 1. 0 02:KB-16-2 3.42 .724 No\_date 28:01 64.30 n/a .000

13095> + 1. 0 01:KB-17-2 24.84 26.339 No\_date 28:02 46.87 n/a .000

13096> + 1. 0 01:KB-18-2 1.14 1.003 No\_date 28:01 46.87 n/a .000

13097> ROUTE RESERVOIR > 1. 0 02:KB-P2 254.24 26.339 No\_date 28:02 46.87 n/a .000

13098> + 1. 0 01:KB-20cvt 1.14 1.003 No\_date 28:01 46.87 n/a .000

13099> + [MgStCelds..1109E-03 m3\_TotVolV..535E-01 m3\_N-Ovfr- 0. hrs] 1. TotTurvor[ 0. hrs]

13100> R0505:CO0274- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13101> ADD HVD + 1. 0 02:KB-P2 253.19 17.634 No\_date 28:09 46.87 n/a .000

13102> ADD HVD + 1. 0 02:KB-P2 253.19 17.634 No\_date 28:09 46.87 n/a .000

13103> + [Impervious area: IApmp ..16:SLP9 ..30:LGH ..137:NHI+ ..013:SCI+ ..0]

13104> R0505:CO0275- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13105> SAVE HYD + 1. 0 01:KB-Ponds 254.24 22.891 No\_date 28:09 46.87 n/a .000

13106> + [Hvd: KB-Pond2 ..00000 m3] 1. TotTurvor[ 0. hrs]

13107> R0505:CO0277- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13108> remark>Total Flows at KB second pond + 1. 0 01:KB-16-1 2.80 .624 No\_date 28:00 66.65 .818 .000

13109> R0505:CO0277- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13110> + [XIMP-75:TIMEP-.75] 1. 0 01:KB-16-1 2.80 .624 No\_date 28:00 66.65 .818 .000

13111> [XIMP-75:TIMEP-.75]

13112> [Horton parameters: Po= 76.20FC4- 13.20DCV4-14: Fc ..00]

13113> [Previous areas: IApmp ..16:SLP9 ..30:LGH ..137:NHI+ ..013:SCI+ ..0]

13114> [Impervious area: IApmp ..16:SLP9 ..30:LGH ..137:NHI+ ..013:SCI+ ..0]

13115> [IaECimp ..4:00: IaRCper ..4:00]

13116> R0505:CO0278- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13117> ADD HVD + 1. 0 02:KB-Ponds 254.24 22.891 No\_date 28:09 46.87 n/a .000

13118> ADD HVD + 1. 0 02:KB-16-1 2.80 .624 No\_date 28:08 66.65 n/a .000

13119> + [Impervious area: IApmp ..16:SLP9 ..30:LGH ..137:NHI+ ..013:SCI+ ..0]

13120> R0505:CO0279- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13121> ROUTE RESERVOIR > 1. 0 02:KB-P3 257.04 23.147 No\_date 28:09 47.08 n/a .000

13122> + 1. 0 01:KB-Ponds 257.04 23.147 No\_date 28:09 47.08 n/a .000

13123> + [overlap ..013:SCI+ ..0]

13124> + 1. 0 01:KB-P2ovz 247.64 22.286 No\_date 28:10 47.08 n/a .000

13125> + [MgStCelds..1109E-02 m3\_TotVolV..1166E-02 m3\_N-Ovfr- 0. hrs] 1. TotTurvor[ 0. hrs]

13126> R0505:CO0280- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13127> ADD HVD + 1. 0 02:KB-P2ovz 247.64 22.286 No\_date 28:10 47.08 n/a .000

13128> + [Impervious area: IApmp ..16:SLP9 ..30:LGH ..137:NHI+ ..013:SCI+ ..0]

13129> + [IaECimp ..4:00: IaRCper ..4:00]

13130> R0505:CO0281- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13131> SAVE HYD + 1. 0 01:KB-Ponds 257.04 22.337 No\_date 28:10 47.08 n/a .000

13132> + [IaECimp ..4:00: IaRCper ..4:00]

13133> remark>Total Flows at KB third pond +

13134> # EXISTING /SUBBATCHMENTS(Kennedy-Burnett SWN Facility (11080), SWN Modeling Approach, NOVATECH Report Ju

13135> # - FRASER-CLARK DRAIN

13136> R0505:CO0282- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13137> + [CONTINUOUS STANDHYD 1. 0 01:FC-01 8.03 1.493 No\_date 28:01 49.52 .608 .000

13138> [XIMP-47:TIMEP-.47]

13139> [Previous areas: IApmp ..4:67:SLP9 ..2:00:LGH ..40:NHP ..250:SCP ..0]

13140> [Impervious area: IApmp ..4:67:SLP9 ..2:00:LGH ..40:NHP ..250:SCP ..0]

13141> [IaECimp ..4:00: IaRCper ..4:00]

13142> R0505:CO0283- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13143> COMPUTE DUALHYD 1. 0 01:FC-01 8.03 1.493 No\_date 28:01 49.52 .608 .000

13144> Major System / 1. 0 02:FC-01-M 0.00 .000 No\_date 0:00 0/n/a .000

13145> Minor System / 1. 0 02:FC-01-M 0.00 .000 No\_date 0:00 0/n/a .000

13146> + [Major System / 1. 0 02:FC-01-M ..00 ..000 No\_date 0:00 0/n/a .000

13147> Minor System / 1. 0 03:FC-01-M 8.03 .756 No\_date 28:32 49.91 n/a .000

13148> + [Major System / 1. 0 03:FC-01-M ..00 ..000 No\_date 0:00 0/n/a .000

13149> R0505:CO0284- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13150> ADD HVD + 1. 0 02:FC-01-MJ 0.00 .000 No\_date 0:00 0/n/a .000

13151> + [Impervious area: IApmp ..1.57:SLP1 ..1:00:LGH ..40:NHP ..250:SCP ..0]

13152> + [IaECimp ..4:00: IaRCper ..4:00]

13153> R0505:CO0285- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13154> CONTINUOUS STANDHYD 1. 0 01:FC-01 16.05 3.891 No\_date 28:00 75.92 .931 .000

13155> [XIMP-93:TIMEP-.93]

13156> [Horton parameters: Po= 76.20FC4- 13.20DCV4-14: Fc ..00]

13157> [Previous areas: IApmp ..4:67:SLP9 ..2:00:LGH ..40:NHP ..250:SCP ..0]

13158> [Impervious area: IApmp ..1.57:SLP1 ..1:00:LGH ..327:NHI+ ..013:SCI+ ..0]

13159> + [IaECimp ..4:00: IaRCper ..4:00]

13160> R0505:CO0286- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13161> COMPUTE DUALHYD 1. 0 01:FC-01 16.05 3.891 No\_date 28:00 75.92 n/a .000

13162> Major System / 1. 0 02:FC-02-M 0.00 .000 No\_date 0:00 0/n/a .000

13163> Minor System / 1. 0 02:FC-02-M 0.00 .000 No\_date 0:00 0/n/a .000

13164> + [Major System / 1. 0 02:FC-02-M ..00 ..000 No\_date 0:00 0/n/a .000

13165> Minor System / 1. 0 03:FC-02-M 0.00 .000 No\_date 0:00 0/n/a .000

13166> + [Major System / 1. 0 03:FC-02-M ..00 ..000 No\_date 0:00 0/n/a .000

13167> Minor System / 1. 0 04:FC-02-M 0.00 .000 No\_date 0:00 0/n/a .000

13168> + [Major System / 1. 0 04:FC-02-M ..00 ..000 No\_date 0:00 0/n/a .000

13169> R0505:CO0288- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13170> CONTINUOUS STANDHYD 1. 0 01:FC-03 3.75 1.540 No\_date 28:00 59.23 .727 .000

13171> [XIMP-64:TIMEP-.64]

13172> [Horton parameters: Po= 76.20FC4- 13.20DCV4-14: Fc ..00]

13173> [Previous areas: IApmp ..4:67:SLP9 ..2:00:LGH ..40:NHP ..250:SCP ..0]

13174> [Impervious area: IApmp ..1.57:SLP1 ..1:00:LGH ..222:NHI+ ..013:SCI+ ..0]

13175> + [IaECimp ..4:00: IaRCper ..4:00]

13176> R0505:CO0289- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13177> COMPUTE DUALHYD 1. 0 01:FC-03 7.37 1.540 No\_date 28:00 59.28 n/a .000

13178> Major System / 1. 0 02:FC-03-M 0.00 .000 No\_date 0:00 0/n/a .000

13179> Minor System / 1. 0 03:FC-03-M 7.35 .727 No\_date 27:42 59.54 n/a .000

13180> + [Major System / 1. 0 03:FC-03-M ..00 ..000 No\_date 0:00 0/n/a .000

13181> Minor System / 1. 0 04:FC-03-M 0.00 .000 No\_date 0:00 0/n/a .000

13182> R0505:CO0290- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13183> COMPUTE DUALHYD 1. 0 01:FC-03 7.37 1.540 No\_date 28:00 59.28 .727 .000

13184> Major System / 1. 0 02:FC-03-M 0.00 .000 No\_date 0:00 0/n/a .000

13185> Minor System / 1. 0 03:FC-03-M 7.37 1.540 No\_date 28:00 59.28 .727 .000

13186> R0505:CO0291- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13187> COMPUTE DUALHYD 1. 0 01:FC-04 12.87 2.587 No\_date 28:01 59.51 n/a .000

13188> Major System / 1. 0 02:FC-04-M 0.00 .000 No\_date 0:00 0/n/a .000

13189> Minor System / 1. 0 03:FC-04-M 0.00 .000 No\_date 0:00 0/n/a .000

13190> + [Major System / 1. 0 02:FC-04-M ..00 ..000 No\_date 0:00 0/n/a .000

13191> Minor System / 1. 0 03:FC-04-M 0.00 .000 No\_date 0:00 0/n/a .000

13192> R0505:CO0292- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13193> COMPUTE DUALHYD 1. 0 01:FC-04 12.87 .530 No\_date 28:01 59.52 n/a .000

13194> Major System / 1. 0 02:FC-04-M 0.00 .000 No\_date 0:00 0/n/a .000

13195> Minor System / 1. 0 03:FC-04-M 0.00 .000 No\_date 0:00 0/n/a .000

13196> + [Major System / 1. 0 02:FC-04-M ..00 ..000 No\_date 0:00 0/n/a .000

13197> Minor System / 1. 0 03:FC-04-M 0.00 .000 No\_date 0:00 0/n/a .000

13198> R0505:CO0293- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13199> ADD HVD + 1. 0 02:FC-04-MJ 0.00 .000 No\_date 0:00 0/n/a .000

13200> + [Impervious area: IApmp ..1.57:SLP1 ..1:00:LGH ..40:NHP ..250:SCP ..0]

13201> + [IaECimp ..4:00: IaRCper ..4:00]

13202> # PROPOSED Subbatchments (Kennedy-Burnett SWN Facility (11080), SWN Modeling Approach, NOVATECH Report June, 2020)

13203> # TO JOCIE RIVER

13204> R0505:CO0294- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13205> CONTINUOUS STANDHYD 1. 0 01:JK-01 8.24 1.714 No\_date 28:00 59.28 .727 .000

13206> [Horton parameters: Po= 76.20FC4- 13.20DCV4-14: Fc ..00]

13207> [Previous areas: IApmp ..4:67:SLP9 ..2:00:LGH ..40:NHP ..250:SCP ..0]

13208> [Impervious area: IApmp ..1.57:SLP1 ..1:00:LGH ..103:NHI+ ..013:SCI+ ..0]

13209> + [IaECimp ..4:00: IaRCper ..4:00]

13210> R0505:CO0295- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13211> COMPUTE DUALHYD 1. 0 01:JK-02 12.87 2.587 No\_date 28:01 59.51 n/a .000

13212> Major System / 1. 0 02:JK-02-M 0.00 .000 No\_date 0:00 0/n/a .000

13213> Minor System / 1. 0 03:JK-02-M 0.00 .000 No\_date 0:00 0/n/a .000

13214> + [Major System / 1. 0 02:JK-02-M ..00 ..000 No\_date 0:00 0/n/a .000

13215> Minor System / 1. 0 03:JK-02-M 0.00 .000 No\_date 0:00 0/n/a .000

13216> R0505:CO0296- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13217> ADD HVD + 1. 0 01:JK-02-M 0.00 .000 No\_date 0:00 0/n/a .000

13218> + [Impervious area: IApmp ..1.57:SLP1 ..1:00:LGH ..27:44 59.54 n/a ..000]

13219> + [IaECimp ..4:00: IaRCper ..4:00]

13220> R0505:CO0297- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13221> COMPUTE DUALHYD 1. 0 01:JK-03 8.24 .563 No\_date 27:44 59.54 n/a ..000

13222> Major System / 1. 0 02:JK-03-M 0.00 .000 No\_date 0:00 0/n/a .000

13223> Minor System / 1. 0 03:JK-03-M 0.00 .000 No\_date 0:00 0/n/a .000

13224> + [Major System / 1. 0 02:JK-03-M ..00 ..000 No\_date 0:00 0/n/a .000

13225> Minor System / 1. 0 03:JK-03-M 0.00 .000 No\_date 0:00 0/n/a .000

13226> R0505:CO0298- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13227> COMPUTE DUALHYD 1. 0 01:JK-04 12.87 2.587 No\_date 28:01 59.55 n/a .000

13228> Major System / 1. 0 02:JK-04-M 0.00 .000 No\_date 0:00 0/n/a .000

13229> Minor System / 1. 0 03:JK-04-M 0.00 .000 No\_date 0:00 0/n/a .000

13230> + [Major System / 1. 0 02:JK-04-M ..00 ..000 No\_date 0:00 0/n/a .000

13231> Minor System / 1. 0 03:JK-04-M 0.00 .000 No\_date 0:00 0/n/a .000

13232> R0505:CO0299- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13233> COMPUTE DUALHYD 1. 0 01:JK-05 8.24 .563 No\_date 27:44 59.55 n/a ..000

13234> Major System / 1. 0 02:JK-05-M 0.00 .000 No\_date 0:00 0/n/a .000

13235> Minor System / 1. 0 03:JK-05-M 0.00 .000 No\_date 0:00 0/n/a .000

13236> + [Major System / 1. 0 02:JK-05-M ..00 ..000 No\_date 0:00 0/n/a .000

13237> Minor System / 1. 0 03:JK-05-M 0.00 .000 No\_date 0:00 0/n/a .000

13238> # Catchment FRASER

13239> # - Developed Fraser drain (north of the Jock).

13240> # - Developed Lethbridge with assumed 43% imp.

13241> # - 2020-12-17 Change Fraser area to 35.1 as measured from QGIS

13242> # - 2020-12-17 Change Lethbridge area to 35.1 as measured from QGIS

13243> # - Primary developed (medium density) - 2020-12-17

13244> R0505:CO0300- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13245> COMPUTE DUALHYD 1. 0 01:FR-01 13.65 1.711 No\_date 28:00 59.55 n/a .000

13246> Major System / 1. 0 02:FR-01-M 0.00 .000 No\_date 0:00 0/n/a .000

13247> Minor System / 1. 0 03:FR-01-M 0.00 .000 No\_date 0:00 0/n/a .000

13248> + [Major System / 1. 0 02:FR-01-M ..00 ..000 No\_date 0:00 0/n/a .000

13249> Minor System / 1. 0 03:FR-01-M 0.00 .000 No\_date 0:00 0/n/a .000

13250> R0505:CO0301- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13251> COMPUTE DUALHYD 1. 0 01:FR-02 12.61 3.688 No\_date 28:01 62.97 .773 .000

13252> Major System / 1. 0 02:FR-02-M 0.00 .000 No\_date 0:00 0/n/a .000

13253> Minor System / 1. 0 03:FR-02-M 0.00 .000 No\_date 0:00 0/n/a .000

13254> + [Major System / 1. 0 02:FR-02-M ..00 ..000 No\_date 0:00 0/n/a .000

13255> Minor System / 1. 0 03:FR-02-M 0.00 .000 No\_date 0:00 0/n/a .000

13256> R0505:CO0302- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13257> COMPUTE DUALHYD 1. 0 01:FR-03 21.61 2.281 No\_date 27:53 63.21 n/a ..000

13258> Major System / 1. 0 02:FR-03-M 0.00 .000 No\_date 0:00 0/n/a .000

13259> Minor System / 1. 0 03:FR-03-M 0.00 .000 No\_date 0:00 0/n/a .000

13260> + [Major System / 1. 0 02:FR-03-M ..00 ..000 No\_date 0:00 0/n/a .000

13261> Minor System / 1. 0 03:FR-03-M 0.00 .000 No\_date 0:00 0/n/a .000

13262> R0505:CO0303- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13263> COMPUTE DUALHYD 1. 0 01:FR-04 21.61 2.281 No\_date 27:53 63.21 n/a ..000

13264> Major System / 1. 0 02:FR-04-M 0.00 .000 No\_date 0:00 0/n/a .000

13265> Minor System / 1. 0 03:FR-04-M 0.00 .000 No\_date 0:00 0/n/a .000

13266> + [Major System / 1. 0 02:FR-04-M ..00 ..000 No\_date 0:00 0/n/a .000

13267> Minor System / 1. 0 03:FR-04-M 0.00 .000 No\_date 0:00 0/n/a .000

13268> R0505:CO0304- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13269> COMPUTE DUALHYD 1. 0 01:FR-05 25.04 22.337 No\_date 28:10 47.08 n/a ..000

13270> Major System / 1. 0 02:FR-05-M 0.00 .000 No\_date 0:00 0/n/a .000

13271> Minor System / 1. 0 03:FR-05-M 0.00 .000 No\_date 0:00 0/n/a .000

13272> + [Major System / 1. 0 02:FR-05-M ..00 ..000 No\_date 0:00 0/n/a .000

13273> Minor System / 1. 0 03:FR-05-M 0.00 .000 No\_date 0:00 0/n/a .000

13274> R0505:CO0305- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13275> COMPUTE DUALHYD 1. 0 01:FR-06 25.04 22.337 No\_date 28:10 47.08 n/a ..000

13276> Major System / 1. 0 02:FR-06-M 0.00 .000 No\_date 0:00 0/n/a .000

13277> Minor System / 1. 0 03:FR-06-M 0.00 .000 No\_date 0:00 0/n/a .000

13278> + [Major System / 1. 0 02:FR-06-M ..00 ..000 No\_date 0:00 0/n/a .000

13279> Minor System / 1. 0 03:FR-06-M 0.00 .000 No\_date 0:00 0/n/a .000

13280> R0505:CO0306- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13281> COMPUTE DUALHYD 1. 0 01:FR-07 25.04 22.337 No\_date 28:10 47.08 n/a ..000

13282> Major System / 1. 0 02:FR-07-M 0.00 .000 No\_date 0:00 0/n/a .000

13283> Minor System / 1. 0 03:FR-07-M 0.00 .000 No\_date 0:00 0/n/a .000

13284> + [Major System / 1. 0 02:FR-07-M ..00 ..000 No\_date 0:00 0/n/a .000

13285> Minor System / 1. 0 03:FR-07-M 0.00 .000 No\_date 0:00 0/n/a .000

13286> R0505:CO0307- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13287> COMPUTE DUALHYD 1. 0 01:FR-08 25.04 22.337 No\_date 28:10 47.08 n/a ..000

13288> Major System / 1. 0 02:FR-08-M 0.00 .000 No\_date 0:00 0/n/a .000

13289> Minor System / 1. 0 03:FR-08-M 0.00 .000 No\_date 0:00 0/n/a .000

13290> + [Major System / 1. 0 02:FR-08-M ..00 ..000 No\_date 0:00 0/n/a .000

13291> Minor System / 1. 0 03:FR-08-M 0.00 .000 No\_date 0:00 0/n/a .000

13292> R0505:CO0308- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13293> COMPUTE DUALHYD 1. 0 01:FR-09 25.04 22.337 No\_date 28:10 47.08 n/a ..000

13294> Major System / 1. 0 02:FR-09-M 0.00 .000 No\_date 0:00 0/n/a .000

13295> Minor System / 1. 0 03:FR-09-M 0.00 .000 No\_date 0:00 0/n/a .000

13296> + [Major System / 1. 0 02:FR-09-M ..00 ..000 No\_date 0:00 0/n/a .000

13297> Minor System / 1. 0 03:FR-09-M 0.00 .000 No\_date 0:00 0/n/a .000

13298> R0505:CO0309- DTRin-ID:NHYD-->ARArba-OPENKms-TpeakData\_hh:mm-->RvNm-R.C.--DWFcms

13299> COMPUTE DUALHYD 1. 0 01:FR-10 25.04 22.337 No\_date 28:10 47.08 n/a ..000

13300> Major System / 1. 0 02:FR-10-M 0.00 .000 No\_date 0:00 0/n/a .000

13301> Minor System / 1. 0 03:FR-10-M 0.00 .000 No\_date 0:00 0/n/a .000

13302> + [Major System / 1. 0 02:FR-10-M ..00 ..000 No\_date 0:00 0/n/a .000

13303> Minor System /

13465+ \*-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13466+ RO5050:C0031-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13467+ CONTINUOUS STANDHY 1.0 01 corrr 15..87 2..831 No\_date 28:01 63.61 .785 .000  
13468+ [XMD= 63-TIMP= 63]  
13469+ [LOSS= 2 CN= 75.0]  
13470+ [Previous area: Iaper= 4.67:SLPP=1.00:LGP= 40::MNP=.250:SCP= .0]  
13471+ [Impervious area: IaIimp= 1.57:SLP1=1.00:LGI= 325::MMI=.013:SCI= .0]  
13472+ [iaECLimp= 4.00:IaREPer= 4.00]  
13473+ [SINM= 33.81:SMAX=225.43: SK= 010]  
13474+ [Dtnin-ID:NH001-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13475+ COMPUTE DUALHY 1.0 01A1-MJ 19..75 2..830 No\_date 28:01 63.61 .785 .000  
13476+ Major System / 1.0 02A1-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13477+ Minor System \ 1.0 03A1-MJ 15..87 1..818 No\_date 28:19 63.67 n/a ..000  
13478+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13479+ RO5050:C0033-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13480+ CONTINUOUS NASHYD 1.0 01 corrr 12..47 ..330 No\_date 29:10 39.91 .490 ..000  
13481+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13482+ [iaEBC= 4.00:SMIN= 11.15:SMAX=207.66: SK= 010]  
13483+ [InterEventTime= 12.00]  
13484+ RO5050:C0034-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13485+ CONTINUOUS STANDHY 1.0 01A1-Corrig 15..75 2..330 No\_date 28:01 55.89 .686 ..000  
13486+ [XMD= 52-TIMP= 52]  
13487+ [ROUTE\_Pipe\_50m-TotDv= 0]  
13488+ [Previous area: Iaper= 4.67:SLPP=1.00:LGP= 40::MNP=.250:SCP= .0]  
13489+ [Impervious area: IaIimp= 1.57:SLP1=1.00:LGI= 324::MMI=.013:SCI= .0]  
13490+ [iaECLimp= 4.00:IaREPer= 4.00]  
13491+ [SINM= 33.81:SMAX=225.43: SK= 010]  
13492+ RO5050:C0035-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13493+ CONTINUOUS NASHYD 1.0 01B1 ..29 2..330 No\_date 28:01 55.89 .686 ..000  
13494+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13495+ RO5050:C0036-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13496+ CONTINUOUS STANDHY 1.0 01A1-Corrig 15..75 2..330 No\_date 28:01 55.89 .686 ..000  
13497+ [XMD= 63-TIMP= 63]  
13498+ [ROUTE\_Pipe\_50m-TotDv= 0]  
13499+ [Previous area: Iaper= 4.67:SLPP=1.00:LGP= 40::MNP=.250:SCP= .0]  
13500+ [Impervious area: IaIimp= 1.57:SLP1=1.00:LGI= 253::MMI=.013:SCI= .0]  
13501+ [iaECLimp= 4.00:IaREPer= 4.00]  
13502+ [SINM= 33.81:SMAX=225.43: SK= 010]  
13503+ CONTINUOUS STANDHY 1.0 01A1 ..27 ..299 No\_date 28:00 63.95 .785 ..000  
13504+ [XMD= 63-TIMP= 63]  
13505+ ADD HYD 1.0 02A1-MJ ..29 ..299 No\_date 28:00 63.95 .785 ..000  
13506+ COMPUTE DUALHY 1.0 01A1-MJ 15..75 2..330 No\_date 28:00 63.95 .785 ..000  
13507+ Major System / 1.0 02A1-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13508+ Minor System \ 1.0 03A1-MJ 15..75 1..818 No\_date 27:51 63.95 n/a ..000  
13509+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13510+ RO5050:C0038-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13511+ COMPUTE DUALHY 1.0 01A1-MJ 15..75 2..330 No\_date 28:00 63.95 .785 ..000  
13512+ Major System / 1.0 02A1-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13513+ Minor System \ 1.0 03A1-MJ 15..75 2..330 No\_date 28:00 63.95 .785 ..000  
13514+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13515+ RO5050:C0039-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13516+ ADD HYD 1.0 02A1-MJ ..29 ..299 No\_date 28:00 63.95 .785 ..000  
13517+ Major System / 1.0 02A1-MJ 15..75 1..818 No\_date 27:56 56.07 n/a ..000  
13518+ Minor System \ 1.0 03A1-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13519+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13520+ RO5050:C0040-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13521+ ADD HYD 1.0 02B1 ..27 ..119 No\_date 28:00 24.96 .n/a ..000  
13522+ [XMD= 52-TIMP= 52]  
13523+ SUM= 1.0 01M101 ..43 4..028 No\_date 28:02 52.81 ..n/a ..000  
13524+ RO5050:C0040-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13525+ ADD HYD 1.0 01M101 ..43 4..028 No\_date 28:02 52.81 ..n/a ..000  
13526+ frame: MH01.0050  
13527+ remark:Total Flows at MH01  
13528+ RO5050:C0041-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13529+ ROUTE PIPE --> 1.0 02A1-MJ 48..13 4..028 No\_date 28:02 52.81 ..n/a ..000  
13530+ [ROT= 1.00] out= 1.0 01 101-102 48..13 4..005 No\_date 28:03 52.81 ..n/a ..000  
13531+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13532+ [Vmax= 3.143:DMax= 1.119]  
13533+ [Din= 1.05:DMax= 1.16]  
13534+ RO5050:C0041-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13535+ ADD HYD 1.0 02A1-MJ 24..86 1..818 No\_date 28:03 56.08 ..n/a ..000  
13536+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13537+ SUM= 1.0 01M102 ..102 72..98 5..823 No\_date 28:03 53.93 ..n/a ..000  
13538+ RO5050:C0043-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13539+ ADD HYD 1.0 01M102 72..98 5..823 No\_date 28:03 53.93 ..n/a ..000  
13540+ frame: MH02.0050  
13541+ remark:Total Flows at MH02  
13542+ RO5050:C0044-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13543+ CONTINUOUS STANDHY 1.0 01A1 ..27 ..299 No\_date 28:00 63.95 .918 ..000  
13544+ [XMD= 71-TIMP= 71]  
13545+ [ROUTE\_Pipe\_50m-TotDv= 0]  
13546+ [Previous area: Iaper= 4.67:SLPP=1.00:LGP= 40::MNP=.250:SCP= .0]  
13547+ [Impervious area: IaIimp= 1.57:SLP1=1.00:LGI= 300::MMI=.013:SCI= .0]  
13548+ [iaECLimp= 4.00:IaREPer= 4.00]  
13549+ [SINM= 33.81:SMAX=225.43: SK= 010]  
13550+ RO5050:C0045-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13551+ ADD HYD 1.0 02A1-MJ ..29 ..299 No\_date 28:00 63.95 .918 ..000  
13552+ [XMD= 52-TIMP= 52]  
13553+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13554+ RO5050:C0046-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13555+ ADD HYD 1.0 02A1-MJ 24..86 1..818 No\_date 28:03 56.08 ..n/a ..000  
13556+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13557+ COMPUTE DUALHY 1.0 01A1-MT ..29 ..299 No\_date 28:00 63.95 .918 ..000  
13558+ Major System / 1.0 02A1-MT ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13559+ Minor System \ 1.0 03A1-MT ..00 ..000 No\_date 28:00 63.95 .918 ..000  
13560+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13561+ RO5050:C0047-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13562+ ADD HYD 1.0 02A1-MJ 72..99 5..823 No\_date 28:03 53.92 ..n/a ..000  
13563+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13564+ [SINM= 2.048:DMax= 1.433]  
13565+ RO5050:C0048-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13566+ ADD HYD 1.0 02A1-MJ 72..99 5..823 No\_date 28:03 53.92 ..n/a ..000  
13567+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13568+ RO5050:C0049-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13569+ ADD HYD 1.0 01M103 72..99 5..961 No\_date 28:03 54.19 ..n/a ..000  
13570+ frame: MH03.0050  
13571+ remark:Total Flows at MH03  
13572+ RO5050:C0050-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13573+ ROUTE PIPE --> 1.0 02A1-MJ 72..99 5..773 No\_date 28:14 53.97 ..n/a ..000  
13574+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13575+ RO5050:C0051-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13576+ ADD HYD 1.0 01M102 72..99 5..773 No\_date 28:14 53.97 ..n/a ..000  
13577+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13578+ RO5050:C0052-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13579+ ADD HYD 1.0 01M102 ..29 ..299 No\_date 28:03 53.92 ..n/a ..000  
13580+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13581+ RO5050:C0053-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13582+ ADD HYD 1.0 01M102 ..29 ..299 No\_date 28:03 53.92 ..n/a ..000  
13583+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13584+ RO5050:C0054-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13585+ ADD HYD 1.0 01M102 ..29 ..299 No\_date 28:03 53.92 ..n/a ..000  
13586+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13587+ RO5050:C0055-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13588+ ADD HYD 1.0 02A1-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13589+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13590+ RO5050:C0056-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13591+ COMPUTE DUALHY 1.0 01A1-MJ 1..56 ..306 No\_date 28:00 66.69 ..n/a ..000  
13592+ Major System / 1.0 02A1-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13593+ Minor System \ 1.0 03A1-MJ ..00 ..000 No\_date 28:00 66.69 ..n/a ..000  
13594+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13595+ RO5050:C0057-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13596+ CONTINUOUS STANDHY 1.0 01A1-A6 1..56 ..306 No\_date 28:00 66.69 ..n/a ..000  
13597+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13598+ [LOSS= 2 CN= 75.0]  
13599+ [Previous area: Iaper= 4.67:SLPP=1.00:LGP= 40::MNP=.250:SCP= .0]  
13600+ [Impervious area: IaIimp= 1.57:SLP1=1.00:LGI= 345::MMI=.013:SCI= .0]  
13601+ [iaECLimp= 4.00:IaREPer= 4.00]  
13602+ [SINM= 33.81:SMAX=225.43: SK= 010]  
13603+ frame: MH04.0050  
13604+ remark:Total Flows at MH04  
13605+ RO5050:C0058-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13606+ CONTINUOUS STANDHY 1.0 01B2 12..31 1..758 No\_date 28:02 56.26 ..n/a ..000  
13607+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13608+ RO5050:C0059-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13609+ ADD HYD 1.0 01M104 105..04 9..444 No\_date 28:04 56.49 ..n/a ..000  
13610+ RO5050:C0060-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13611+ ADD HYD 1.0 01M104 105..04 5..444 No\_date 28:04 56.49 ..n/a ..000  
13612+ frame: MH04.0050  
13613+ remark:Total Flows at MH04  
13614+ RO5050:C0061-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13615+ ADD HYD 1.0 01B2 ..29 ..299 No\_date 28:02 56.26 ..n/a ..000  
13616+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13617+ RO5050:C0062-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13618+ ADD HYD 1.0 01B2 ..29 ..299 No\_date 28:02 56.26 ..n/a ..000  
13619+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13620+ \* [ROT= 1.00] out= 1.0 01 315-333 12..31 1..029 No\_date 28:33 56.54 ..n/a ..000  
13621+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13622+ [SINM= 2.054:DMax= 1.403]  
13623+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13624+ RO5050:C0063-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13625+ ADD HYD 1.0 01B2 ..29 ..299 No\_date 28:02 56.26 ..n/a ..000  
13626+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13627+ RO5050:C0064-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13628+ CONTINUOUS STANDHY 1.0 01B2 ..29 ..299 No\_date 28:02 56.26 ..n/a ..000  
13629+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13630+ RO5050:C0065-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13631+ COMPUTE DUALHY 1.0 01B2-MJ 12..31 1..758 No\_date 28:02 56.26 ..n/a ..000  
13632+ Major System / 1.0 02B2-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13633+ Minor System \ 1.0 03B2-MJ ..00 ..000 No\_date 28:02 56.26 ..n/a ..000  
13634+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13635+ RO5050:C0066-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13636+ ADD HYD 1.0 02B2-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13637+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13638+ RO5050:C0067-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13639+ COMPUTE DUALHY 1.0 01B3 12..31 1..825 No\_date 28:01 56.26 ..n/a ..000  
13640+ Major System / 1.0 02B3-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13641+ Minor System \ 1.0 03B3-MJ ..00 ..000 No\_date 28:01 56.26 ..n/a ..000  
13642+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13643+ RO5050:C0068-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13644+ frame: MH05.0050  
13645+ remark:Total Flows at MH05  
13646+ RO5050:C0069-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13647+ CONTINUOUS STANDHY 1.0 01B3 ..29 ..299 No\_date 28:01 56.26 ..n/a ..000  
13648+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13649+ RO5050:C0070-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13650+ frame: MH05.0050  
13651+ RO5050:C0071-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13652+ ROUTE PIPE --> 1.0 02 333-335 12..31 1..029 No\_date 28:01 56.26 ..n/a ..000  
13653+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13654+ RO5050:C0072-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13655+ CONTINUOUS STANDHY 1.0 01B3 ..29 ..299 No\_date 28:01 56.26 ..n/a ..000  
13656+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13657+ RO5050:C0073-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13658+ ADD HYD 1.0 02B3-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13659+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13660+ RO5050:C0074-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13661+ COMPUTE DUALHY 1.0 01B4 12..31 1..825 No\_date 28:01 56.26 ..n/a ..000  
13662+ Major System / 1.0 02B4-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13663+ Minor System \ 1.0 03B4-MJ ..00 ..000 No\_date 28:01 56.26 ..n/a ..000  
13664+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13665+ RO5050:C0075-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13666+ ADD HYD 1.0 02B4-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13667+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13668+ RO5050:C0076-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13669+ COMPUTE DUALHY 1.0 01B5 12..31 1..825 No\_date 28:01 56.26 ..n/a ..000  
13670+ Major System / 1.0 02B5-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13671+ Minor System \ 1.0 03B5-MJ ..00 ..000 No\_date 28:01 56.26 ..n/a ..000  
13672+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13673+ RO5050:C0077-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13674+ ADD HYD 1.0 02B5-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13675+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13676+ RO5050:C0078-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13677+ COMPUTE DUALHY 1.0 01B6 12..31 1..825 No\_date 28:01 56.26 ..n/a ..000  
13678+ Major System / 1.0 02B6-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13679+ Minor System \ 1.0 03B6-MJ ..00 ..000 No\_date 28:01 56.26 ..n/a ..000  
13680+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13681+ RO5050:C0079-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13682+ ADD HYD 1.0 02B6-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13683+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13684+ RO5050:C0080-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13685+ COMPUTE DUALHY 1.0 01B7 12..31 1..825 No\_date 28:01 56.26 ..n/a ..000  
13686+ Major System / 1.0 02B7-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13687+ Minor System \ 1.0 03B7-MJ ..00 ..000 No\_date 28:01 56.26 ..n/a ..000  
13688+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13689+ RO5050:C0081-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13690+ ADD HYD 1.0 02B7-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13691+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13692+ RO5050:C0082-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13693+ COMPUTE DUALHY 1.0 01B8 12..31 1..825 No\_date 28:01 56.26 ..n/a ..000  
13694+ Major System / 1.0 02B8-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13695+ Minor System \ 1.0 03B8-MJ ..00 ..000 No\_date 28:01 56.26 ..n/a ..000  
13696+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13697+ RO5050:C0083-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13698+ ADD HYD 1.0 02B8-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13699+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13700+ RO5050:C0084-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13701+ COMPUTE DUALHY 1.0 01B9 12..31 1..825 No\_date 28:01 56.26 ..n/a ..000  
13702+ Major System / 1.0 02B9-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13703+ Minor System \ 1.0 03B9-MJ ..00 ..000 No\_date 28:01 56.26 ..n/a ..000  
13704+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf= 0 hrs]  
13705+ RO5050:C0085-----> Dtnin-ID:NH001-----AERAh-QPEAKms-TpeakDate\_hh:mm:--RvNm-R.C.--DWFcms  
13706+ ADD HYD 1.0 02B9-MJ ..00 ..000 No\_date 0:00 ..000 n/a ..000  
13707+ [ROUTE\_Pipe\_50m-TotDv=000000-00-NrOf= 0 TotDurOf

13839+ [SMIN= 33.81 : SMAX=225.43; SK= .010] 13840+ R0550:CO0419-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13841+ COMPUTE DUALHY 1.0 01:A11-A3 2.44 .491 No\_date 28:00 66.63 n/a .000 13842+ Major System / 1.0 02:A5-MJ .000 .000 No\_date 0:00 n/a .000 13843+ Minor System / 1.0 03:A12-MJ 1.0 .491 No\_date 28:00 66.63 n/a .000 13844+ R0550:CO0384-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13845+ ADD HYD 1.0 02:106A-106 109.50 3.702 No\_date 27:59 56.59 n/a .000 13846+ \* [XIMP= 38:TIME= .38] 1.0 01:M106 111.14 4.177 No\_date 28:00 56.81 n/a .000 13847+ SUMN= 1.0 01:M106 111.94 4.177 No\_date 28:00 56.81 n/a .000 13848+ R0550:CO0399-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13849+ frame:MMU06\_0050 1.0 01:M106 111.94 4.177 No\_date 28:00 56.81 n/a .000 13850+ remark:Total Flows at MMU06 13851+ frame:MMU06\_0050 1.0 01:M106 111.94 4.177 No\_date 28:00 56.81 n/a .000 13852+ R0550:CO0400-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13853+ \* [Previous areas: IaIimp= 4.67:SLPP=1.00:LGP= 40.:MNP=.250:SCP= .0] 13854+ \* [ROUTE 1.00] out<- 1.0 01:106-107 111.94 4.129 No\_date 28:00 56.81 n/a .000 13855+ [L/8/n= 1.01:106-107 111.94 4.129 No\_date 28:00 56.81 n/a .000 13856+ [Vmax= 1.685:Dmax= 1.558] 13857+ [Dini= 1.80:Dused= 1.98] 13858+ R0550:CO0401-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13859+ CONTINUOUS STANDHY 1.0 01:A10 4.14 .602 No\_date 28:01 53.26 .653 .000 13860+ \* [XIMP= 38:TIME= .47] 13861+ frame:CN-100 1.0 01:A10 4.14 .602 No\_date 28:01 53.26 .653 .000 13862+ \* [Previous areas: IaIimp= 1.57:SLPP=1.00:LGP= 183.:MNP=.013:SCI= .0] 13863+ [Imperial areas: IaIimp= 1.57:SLPP=1.00:LGP= 183.:MNP=.013:SCI= .0] 13864+ \* [ROUTE 1.00] out<- 1.0 01:106-107 111.94 4.129 No\_date 28:00 56.81 n/a .000 13865+ [L/8/n= 1.01:106-107 111.94 4.129 No\_date 28:00 56.81 n/a .000 13866+ [Vmax= 1.685:Dmax= 1.558] 13867+ [Dini= 1.80:Dused= 1.98] 13868+ R0550:CO0402-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13869+ CONTINUOUS STANDHY 1.0 01:A10 4.14 .602 No\_date 28:01 53.26 .653 .000 13870+ \* [XIMP= 38:TIME= .47] 13871+ frame:MMU06\_0050 1.0 01:M106 109.50 3.702 No\_date 27:59 56.59 n/a .000 13872+ CONTINUOUS STANDHY 1.0 01:A10 109.61 1.722 No\_date 28:02 60.69 .745 .000 13873+ \* [ROUTE 1.00] out<- 1.0 01:106-107 111.94 4.129 No\_date 28:02 60.69 .745 .000 13874+ [L/8/n= 2 : CN= 75.0] 13875+ \* [Previous areas: IaIimp= 4.67:SLPP=1.00:LGP= 40.:MNP=.250:SCP= .0] 13876+ \* [Imperial areas: IaIimp= 1.57:SLPP=1.00:LGP= 379.:MNP=.013:SCI= .0] 13877+ [IaECImp= 4.00: IaRECPer= 4.00] 13878+ [SMIN= 33.81 : SMAX=225.43; SK= .010] 13879+ R0550:CO0403-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13880+ COMPUTE DUALHY 1.0 01:A11 106.61 .602 No\_date 28:02 60.69 n/a .000 13881+ Major System / 1.0 02:A11-MJ .000 .000 No\_date 0:00 n/a .000 13882+ Minor System / 1.0 03:A12-MJ 1.0 .602 No\_date 27:50 53.25 n/a .000 13883+ \* [ROUTE 1.00] out<- 1.0 01:106-107 111.94 4.129 No\_date 28:00 56.81 n/a .000 13884+ [L/8/n= 1.01:106-107 111.94 4.129 No\_date 28:00 56.81 n/a .000 13885+ [Vmax= 1.685:Dmax= 1.558] 13886+ [Dini= 1.80:Dused= 1.98] 13887+ R0550:CO0404-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13888+ frame:MMU07\_0050 1.0 01:M107 126.61 5.432 No\_date 28:00 57.03 n/a .000 13889+ remark:Total Flows at MMU07 13890+ R0550:CO0405-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13891+ \* [ROUTE 1.00] out<- 1.0 01:106-107 126.69 5.345 No\_date 28:00 57.03 n/a .000 13892+ [L/8/n= 1.01:106-107 126.69 5.345 No\_date 28:00 57.03 n/a .000 13893+ [Vmax= 1.919:Dmax= 1.650] 13894+ [Dini= 1.80:Dused= 2.01] 13895+ R0550:CO0406-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13896+ CONTINUOUS STANDHY 1.0 01:A12 12.29 1.938 No\_date 28:01 56.26 .690 .000 13897+ \* [XIMP= 41:TIME= .54] 13898+ frame:CN-100 1.0 01:A12 12.29 1.938 No\_date 28:01 56.26 .690 .000 13899+ \* [Previous areas: IaIimp= 4.67:SLPP=1.00:LGP= 40.:MNP=.250:SCP= .0] 13900+ \* [Imperial areas: IaIimp= 1.57:SLPP=1.00:LGP= 183.:MNP=.013:SCI= .0] 13901+ [IaECImp= 4.00: IaRECPer= 4.00] 13902+ [SMIN= 33.81 : SMAX=225.43; SK= .010] 13903+ R0550:CO0407-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13904+ COMPUTE DUALHY 1.0 01:A11 12.29 1.938 No\_date 28:01 56.26 .690 .000 13905+ \* [ROUTE 1.00] out<- 1.0 01:106-107 126.69 5.344 No\_date 28:00 57.03 n/a .000 13906+ [L/8/n= 1.01:106-107 126.69 5.344 No\_date 28:00 57.03 n/a .000 13907+ [Vmax= 1.919:Dmax= 1.650] 13908+ R0550:CO0408-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13909+ CONTINUOUS STANDHY 1.0 01:A12 2.59 .487 No\_date 28:01 66.69 .818 .000 13910+ \* [ROUTE 1.00] out<- 1.0 01:106-107 126.69 5.344 No\_date 28:01 66.69 .818 .000 13911+ [L/8/n= 1.01:106-107 126.69 5.344 No\_date 28:01 66.69 .818 .000 13912+ [SMIN= 33.81 : SMAX=225.43; SK= .010] 13913+ R0550:CO0410-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13914+ COMPUTE DUALHY 1.0 01:A11 12.29 1.938 No\_date 28:01 56.26 .690 .000 13915+ \* [ROUTE 1.00] out<- 1.0 01:106-107 126.69 5.344 No\_date 28:00 57.03 n/a .000 13916+ [L/8/n= 1.01:106-107 126.69 5.344 No\_date 28:00 57.03 n/a .000 13917+ [Vmax= 1.919:Dmax= 1.650] 13918+ R0550:CO0411-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13919+ CONTINUOUS STANDHY 1.0 01:A12 2.59 .487 No\_date 28:01 66.69 .818 .000 13920+ \* [ROUTE 1.00] out<- 1.0 01:106-107 126.69 5.344 No\_date 28:01 66.69 .818 .000 13921+ [L/8/n= 2 : CN= 75.0] 13922+ \* [Previous areas: IaIimp= 4.67:SLPP=1.00:LGP= 40.:MNP=.250:SCP= .0] 13923+ \* [Imperial areas: IaIimp= 1.57:SLPP=1.00:LGP= 379.:MNP=.013:SCI= .0] 13924+ [IaECImp= 4.00: IaRECPer= 4.00] 13925+ [SMIN= 33.81 : SMAX=225.43; SK= .010] 13926+ R0550:CO0413-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13927+ COMPUTE DUALHY 1.0 01:A11 2.59 .487 No\_date 28:01 66.69 n/a .000 13928+ Major System / 1.0 02:A11-MJ .000 .000 No\_date 0:00 n/a .000 13929+ Minor System / 1.0 03:A12-MJ 1.0 .602 No\_date 27:50 53.25 n/a .000 13930+ \* [ROUTE 1.00] out<- 1.0 01:106-107 126.69 5.344 No\_date 28:00 57.03 n/a .000 13931+ [L/8/n= 1.01:106-107 126.69 5.344 No\_date 28:00 57.03 n/a .000 13932+ [Vmax= 1.919:Dmax= 1.650] 13933+ R0550:CO0414-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13934+ frame:CN-100 1.0 01:Pond-Block 2.94 .436 No\_date 28:00 53.21 .653 .000 13935+ \* [ROUTE 1.00] out<- 1.0 01:106-107 126.69 5.344 No\_date 28:00 57.03 n/a .000 13936+ [L/8/n= 2 : CN= 75.0] 13937+ \* [Previous areas: IaIimp= 4.67:SLPP=1.00:LGP= 40.:MNP=.250:SCP= .0] 13938+ \* [Imperial areas: IaIimp= 1.57:SLPP=1.00:LGP= 183.:MNP=.013:SCI= .0] 13939+ [IaECImp= 4.00: IaRECPer= 4.00] 13940+ [SMIN= 33.81 : SMAX=225.43; SK= .010] 13941+ R0550:CO0415-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13942+ frame:CN-100 1.0 01:Pond-Block 2.94 .436 No\_date 28:00 53.21 .653 .000 13943+ \* [ROUTE 1.00] out<- 1.0 01:106-107 126.69 5.344 No\_date 28:00 57.03 n/a .000 13944+ \* [ROUTE 1.00] out<- 1.0 01:106-108 141.57 6.850 No\_date 28:01 57.16 n/a .000 13945+ frame:MMU08\_0050 1.0 01:M108 141.57 6.850 No\_date 28:01 57.16 n/a .000 13946+ remark:Total Flows at MMU08 13947+ R0550:CO0416-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13948+ ROUTE PIPE > 1.0 02:M108 141.57 6.850 No\_date 28:01 57.16 n/a .000 13949+ \* [ROUTE 1.00] out<- 1.0 01:106-108 141.57 6.810 No\_date 28:02 57.16 n/a .000 13950+ [L/8/n= 77.0 : 130.0 : 013] 13951+ [Vmax= 2.104:Dmax= 1.784] 13952+ [ROUTE 1.00] out<- 1.0 01:106-108 141.57 6.810 No\_date 28:01 57.16 n/a .000 13953+ R0550:CO0417-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13954+ ROUTE PIPE > 1.0 02:108-108 141.57 6.810 No\_date 28:02 57.16 n/a .000 13955+ \* [ROUTE 1.00] out<- 1.0 01:106-108 141.57 6.771 No\_date 28:02 57.16 n/a .000 13956+ [L/8/n= 80.0 : 130.0 : 013] 13957+ [Vmax= 2.101:Dmax= 1.780] 13958+ R0550:CO0418-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13959+ frame:MMU08\_0050 1.0 01:M108 141.57 6.850 No\_date 28:01 57.16 n/a .000 13960+ remark:Total Flows at MMU08 13961+ R0550:CO0419-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13962+ frame:CN-100 1.0 01:Corriган 144.51 7.185 No\_date 28:02 57.08 n/a .000 13963+ ROUTE RESERVOIR > 1.0 02:Corriган 144.51 7.185 No\_date 28:02 57.08 n/a .000 13964+ \* [ROUTE 1.00] out<- 1.0 02:108-108 144.51 7.185 No\_date 28:02 57.08 n/a .000 13965+ [L/8/n= 80.0 : 130.0 : 013] 13966+ [Vmax= 2.085:Dmax= 1.784] 13967+ R0550:CO0420-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13968+ frame:Corriган\_0050 1.0 01:Corriган 144.51 7.185 No\_date 28:02 57.08 n/a .000 13969+ remark:HVD\_COMMENT [Total Flows at Corriган Pond] 13970+ R0550:CO0421-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13971+ frame:CN-100 1.0 01:Corriган 144.51 7.185 No\_date 28:02 57.08 n/a .000 13972+ R0550:CO0421-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13973+ ADD HYD + 1.0 02:Cori-P 144.51 6.335 No\_date 28:26 57.08 n/a .000 13974+ \* [ROUTE 1.00] out<- 1.0 02:108-108 144.51 6.335 No\_date 28:26 57.08 n/a .000 13975+ [L/8/n= 80.0 : 130.0 : 013] 13976+ [Vmax= 2.104:Dmax= 1.784] 13977+ R0550:CO0422-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13978+ frame:CN-100 1.0 01:Corriган 144.51 7.185 No\_date 28:02 57.08 n/a .000 13979+ \* [ROUTE 1.00] out<- 1.0 02:108-108 144.51 7.185 No\_date 28:02 57.08 n/a .000 13980+ [L/8/n= 80.0 : 130.0 : 013] 13981+ [Vmax= 2.066:Dmax= 1.982] 13982+ frame:CN-100 1.0 01:Corriган 144.51 7.185 No\_date 28:02 57.08 n/a .000 13983+ frame:Corriган\_0050 1.0 01:Corriган 144.51 7.185 No\_date 28:02 57.08 n/a .000 13984+ remark:HVD\_COMMENT [Total Flows at Corriган Pond] 13985+ R0550:CO0423-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 13986+ ROUTE CHANNEL > 1.0 02:Corriган 55019.59 127.077 No\_date 36:49 34.22 n/a .000 13987+ \* [ROUTE 1.00] out<- 1.0 01:Corriган 55019.59 127.062 No\_date 36:52 34.22 n/a .000 13988+ [L/8/n= 80.0 : 145.0 : 045] 13989+ [Vmax= 2.066:Dmax= 1.982] 13990+ frame:CN-100 1.0 01:Corriган 55019.59 127.077 No\_date 36:49 34.22 n/a .000 13991+ frame:Corriган\_0050 1.0 01:Corriган 55019.59 127.077 No\_date 36:49 34.22 n/a .000 13992+ frame:CN-100 1.0 01:Corriган 55019.59 127.077 No\_date 36:49 34.22 n/a .000 13993+ # Channel X-Section obtained from Riva Hydraulic Model - Station 2462 13994+ # Hydrograph from Corriган Drained route to Jockville Road 13995+ # Channel X-Section obtained from Riva Hydraulic Model - Station 2462 13996+ # Hydrograph from Corriган Drained route to Jockville Road 13997+ # Channel X-Section obtained from Riva Hydraulic Model - Station 2462 13998+ # Channel X-Section obtained from Riva Hydraulic Model - Station 2462 13999+ R0550:CO0423-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 14000+ ROUTE CHANNEL > 1.0 02:Corriган 55019.59 127.077 No\_date 36:49 34.22 n/a .000 14001+ \* [ROUTE 1.00] out<- 1.0 01:Corriган 55019.59 127.062 No\_date 36:52 34.22 n/a .000 14002+ [L/8/n= 77.0 : 130.0 : 013] 14003+ [Vmax= 2.104:Dmax= 1.784] 14004+ R0550:CO0424-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 14005+ ADD HYD + 1.0 02:M112 178.95 17.756 No\_date 28:06 50.66 .622 .000 14006+ \* [ROUTE 1.00] out<- 1.0 01:M112\_P 153.87 4.050 No\_date 28:11 50.66 n/a .000 14007+ [L/8/n= 80.0 : 145.0 : 045] 14008+ [Vmax= 2.066:Dmax= 1.982] 14009+ frame:CN-100 1.0 01:M112 178.95 17.756 No\_date 28:06 50.66 .622 .000 14010+ [L/8/n= 77.0 : 130.0 : 013] 14011+ [Vmax= 2.104:Dmax= 1.784] 14012+ \* [ROUTE 1.00] out<- 1.0 01:M112 153.87 4.050 No\_date 28:11 50.66 n/a .000 14013+ [L/8/n= 80.0 : 145.0 : 045] 14014+ [Vmax= 2.066:Dmax= 1.982] 14015+ frame:CN-100 1.0 01:M112 178.95 17.756 No\_date 28:06 50.66 .622 .000 14016+ # Catchment MILLS 14017+ # To SWM Facility north of the Jock 14018+ # Residential development 14019+ # Residential development 14020+ R0550:CO0424-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 14021+ frame:CN-100 1.0 01:M112 178.95 17.756 No\_date 28:06 50.66 .622 .000 14022+ \* [ROUTE 1.00] out<- 1.0 01:M112\_P 153.87 4.050 No\_date 28:11 50.66 n/a .000 14023+ [L/8/n= 80.0 : 145.0 : 045] 14024+ [Vmax= 2.066:Dmax= 1.982] 14025+ frame:CN-100 1.0 01:M112 178.95 17.756 No\_date 28:06 50.66 .622 .000 14026+ ADD HYD + 1.0 02:N\_M 55019.59 127.062 No\_date 36:52 34.22 n/a .000 14027+ frame:MMU06\_0050 1.0 01:N\_M 55019.59 127.062 No\_date 36:52 34.22 n/a .000 14028+ remark:Total Flows at Jockville Road 14029+ frame:MMU06\_0050 1.0 01:N\_M 55019.59 127.062 No\_date 36:52 34.22 n/a .000 14030+ # Catchment Jock 14031+ # Hydrograph from Jockville Road to Heart's Desire 14032+ # Channel X-Section obtained from Riva Hydraulic Model - Station 2462 14033+ # Hydrograph from Jockville Road to Heart's Desire 14034+ # Channel X-Section obtained from Riva Hydraulic Model - Station 2462 14035+ R0550:CO0425-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 14036+ ROUTE CHANNEL > 1.0 02:Jock 55019.59 127.062 No\_date 36:52 34.22 n/a .000 14037+ \* [ROUTE 1.00] out<- 1.0 01:Jock 55019.59 127.062 No\_date 36:53 34.22 n/a .000 14038+ [L/8/n= 77.0 : 130.0 : 013] 14039+ [Vmax= 2.104:Dmax= 1.784] 14040+ R0550:CO0426-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 14041+ frame:CN-100 1.0 01:Jock 55019.59 127.062 No\_date 36:52 34.22 n/a .000 14042+ \* [ROUTE 1.00] out<- 1.0 01:Jock 55019.59 127.062 No\_date 36:53 34.22 n/a .000 14043+ [L/8/n= 77.0 : 130.0 : 013] 14044+ [Vmax= 2.104:Dmax= 1.784] 14045+ R0550:CO0427-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 14046+ frame:CN-100 1.0 01:Jock 55019.59 127.062 No\_date 36:52 34.22 n/a .000 14047+ \* [ROUTE 1.00] out<- 1.0 01:Jock 55019.59 127.062 No\_date 36:53 34.22 n/a .000 14048+ [L/8/n= 77.0 : 130.0 : 013] 14049+ [Vmax= 2.104:Dmax= 1.784] 14050+ R0550:CO0428-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 14051+ frame:CN-100 1.0 01:Jock 55019.59 127.062 No\_date 36:52 34.22 n/a .000 14052+ \* [ROUTE 1.00] out<- 1.0 01:Jock 55019.59 127.062 No\_date 36:53 34.22 n/a .000 14053+ [L/8/n= 77.0 : 130.0 : 013] 14054+ [Vmax= 2.104:Dmax= 1.784] 14055+ R0550:CO0429-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 14056+ frame:CN-100 1.0 01:Jock 55019.59 127.062 No\_date 36:52 34.22 n/a .000 14057+ \* [ROUTE 1.00] out<- 1.0 01:Jock 55019.59 127.062 No\_date 36:53 34.22 n/a .000 14058+ [L/8/n= 77.0 : 130.0 : 013] 14059+ [Vmax= 2.104:Dmax= 1.784] 14060+ R0550:CO0430-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 14061+ frame:CN-100 1.0 01:Jock 55019.59 127.062 No\_date 36:52 34.22 n/a .000 14062+ \* [ROUTE 1.00] out<- 1.0 01:Jock 55019.59 127.062 No\_date 36:53 34.22 n/a .000 14063+ [L/8/n= 77.0 : 130.0 : 013] 14064+ [Vmax= 2.104:Dmax= 1.784] 14065+ R0550:CO0431-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 14066+ frame:CN-100 1.0 01:Jock 55019.59 127.062 No\_date 36:52 34.22 n/a .000 14067+ \* [ROUTE 1.00] out<- 1.0 01:Jock 55019.59 127.062 No\_date 36:53 34.22 n/a .000 14068+ [L/8/n= 77.0 : 130.0 : 013] 14069+ [Vmax= 2.104:Dmax= 1.784] 14070+ R0550:CO0432-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 14071+ frame:CN-100 1.0 01:Jock 55019.59 127.062 No\_date 36:52 34.22 n/a .000 14072+ \* [ROUTE 1.00] out<- 1.0 01:Jock 55019.59 127.062 No\_date 36:53 34.22 n/a .000 14073+ [L/8/n= 77.0 : 130.0 : 013] 14074+ [Vmax= 2.104:Dmax= 1.784] 14075+ R0550:CO0433-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 14076+ frame:CN-100 1.0 01:Jock 55019.59 127.062 No\_date 36:52 34.22 n/a .000 14077+ \* [ROUTE 1.00] out<- 1.0 01:Jock 55019.59 127.062 No\_date 36:53 34.22 n/a .000 14078+ [L/8/n= 77.0 : 130.0 : 013] 14079+ [Vmax= 2.104:Dmax= 1.784] 14080+ R0550:CO0434-----Dtnin-ID:NHYD---ARAhA-QPEAKcms-Tpeakdate\_hh:mm::--RvNm-B.C.--DWFcms 14081+ frame:CN-100 1.0 01:Jock 55019.59 127.062 No\_date 36:52 34.22 n/a .000 14082+ \* [ROUTE 1.00] out<- 1.0 01:Jock 55019.59 127.062 No\_date 36:53 34.22 n/a .000 14083+ [L/8/n= 77.0 : 130.0 : 013] 14084+ [Vmax= 2.104:Dmax= 1.784] 14085+ R0550











16083+ + 1. 02:FC-01-S 8.03 .756 No\_date 27:49 54.46 n/a .000  
 16084+ + 1. 02:FC-02-S 16.05 2.927 No\_date 26:05 82.87 n/a .000  
 16085+ + 1. 02:FC-03-S 1.37 .157 No\_date 26:05 82.87 n/a .000  
 16086+ SUM+ 1. 01:4241 54658.51 144.701 No\_date 36:48 39.28 n/a .000  
 16087+ RO100:CO005+ 1. 01:4241 ARAhA-QPEAKms-Tpeakdate\_bh:mm::--RvNm-R.C.--DWFcms  
 16088+ SAVE HYD 1. 01:4241 54658.51 144.701 No\_date 36:49 39.28 n/a .000  
 16089+ name :HYD 1. 01:4241 54658.51 144.701 No\_date 36:49 39.28 n/a .000  
 16090+ remark:Total Flows at Ken-Burnett outlet  
 16091+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 4241  
 16092+ # Dtnin-ID:NHNDY-  
 16093+ ROUTE CHANNEL -> 1. 02:4241 54658.51 144.701 No\_date 36:48 39.28 n/a .000  
 16094+ \* [ROUTE\_ID: 0000000000000000] 1. 02:4241-out 54658.51 144.744 No\_date 36:44 39.28 n/a .000  
 16095+ [L/S:n\_ 294.1 / .099/.098]  
 16096+ RO100:CO005+ 1. 02:4241 54658.51 144.744 No\_date 36:44 39.28 n/a .000  
 16097+ ADD HYD 1. 02:4241 54658.51 144.744 No\_date 36:44 39.28 n/a .000  
 16098+ [Vmax\_ 1.396 Dmax\_ 2.598]  
 16099+ RO100:CO005+ 1. 02:4241 54658.51 144.744 No\_date 36:44 39.28 n/a .000  
 16100+ ADD HYD 1. 02:4241 54658.51 144.744 No\_date 36:44 39.28 n/a .000  
 16101+ \* [ROUTE\_ID: 0000000000000000] 1. 02:4241-out 54658.51 144.744 No\_date 36:44 39.28 n/a .000  
 16102+ [L/S:n\_ 294.1 / .099/.098]  
 16103+ RO100:CO005+ 1. 02:4241 54658.51 144.744 No\_date 36:44 39.28 n/a .000  
 16104+ SAVE HYD 1. 01:SN\_XB 54681.20 144.787 No\_date 36:44 39.29 n/a .000  
 16105+ RO100:CO005+ 1. 01:SN\_XB 54681.20 144.787 No\_date 36:44 39.29 n/a .000  
 16106+ name :SN\_XB\_0100 1. 01:SN\_XB 54681.20 144.787 No\_date 36:44 39.29 n/a .000  
 16107+ # Hydrograph from Station 3633 to Node Todd  
 16108+ # Channel X-Section obtained from RVEA Hydraulic Model - Station 3633  
 16109+ # Dtnin-ID:NHNDY-  
 16110+ ROUTE CHANNEL -> 1. 02:4241 54658.51 144.744 No\_date 36:44 39.28 n/a .000  
 16111+ \* [ROUTE\_ID: 0000000000000000] 1. 02:4241-out 54658.51 144.744 No\_date 36:44 39.28 n/a .000  
 16112+ [L/S:n\_ 294.1 / .099/.098]  
 16113+ RO100:CO005+ 1. 02:4241 54658.51 144.744 No\_date 36:44 39.28 n/a .000  
 16114+ ADD HYD 1. 02:4241 54658.51 144.744 No\_date 36:44 39.28 n/a .000  
 16115+ [ROUTE\_ID: 0000000000000000] 1. 02:4241-out 54658.51 144.744 No\_date 36:44 39.28 n/a .000  
 16116+ [L/S:n\_ 294.1 / .099/.098]  
 16117+ RO100:CO005+ 1. 02:4241 54658.51 144.744 No\_date 36:44 39.28 n/a .000  
 16118+ # Catchment Greenbank  
 16119+ # Dtnin-ID:NHNDY-  
 16120+ ROUTE CHANNEL -> 1. 02:4241 54658.51 144.744 No\_date 36:44 39.28 n/a .000  
 16121+ \* [ROUTE\_ID: 0000000000000000] 1. 02:4241-out 54658.51 144.744 No\_date 36:44 39.28 n/a .000  
 16122+ [L/S:n\_ 294.1 / .099/.098]  
 16123+ RO100:CO005+ 1. 02:4241 54658.51 144.744 No\_date 36:44 39.28 n/a .000  
 16124+ [ROUTE\_ID: 0000000000000000] 1. 02:4241-out 54658.51 144.744 No\_date 36:44 39.28 n/a .000  
 16125+ CONTINUOUS STANDY 1. 01:01:GREENBANK 36.60 7.069 No\_date 28:01 71.80 .811 .000  
 16126+ [ROUTE\_ID: 0000000000000000] 1. 01:01:GREENBANK 36.60 7.069 No\_date 28:01 71.80 .811 .000  
 16127+ [L/S:n\_ 2 CN\_ 77.0]  
 16128+ [Previous] area: Iaper\_ 4.67:SLPP=1.00:LGP= 40.:MNP= 250:SCP= .01  
 16129+ [Imperious] area: IALimp\_ 1.57:SLIP=1.00:LGI= 44.1:MMI=.013:SCI= .01  
 16130+ [IaRCimp\_ 4.00:1aRCper\_ 4.00]  
 16131+ RO100:CO005+ 1. 02:4241 54658.51 144.744 No\_date 36:44 39.28 n/a .000  
 16132+ # Dtnin-ID:NHNDY-  
 16133+ ROUTE RESERVOIR --> 1. 02:01:Greenbank 36.60 7.069 No\_date 28:01 71.80 n/a .000  
 16134+ [ROUTE\_ID: 0000000000000000] 1. 02:01:Greenbank 36.60 7.069 No\_date 28:01 71.80 n/a .000  
 16135+ [overload < 0] 1. 02:01:Greenbank 36.60 7.069 No\_date 28:01 71.80 n/a .000  
 16136+ [MSCToCsed\_ 9351E000 m\_ 3, TotDurVol\_ 0.00000 m\_ N-Ovf\_ 0\_ TotDurOvf\_ 0\_.hrs]  
 16137+ RO100:CO005+ 1. 02:01:Greenbank 36.60 7.069 No\_date 28:01 71.80 n/a .000  
 16138+ ADD HYD 1. 02:01:TO\_N 54681.20 144.792 No\_date 36:45 39.29 n/a .000  
 16139+ \* 1. 02:01:GREENBANK .00 .000 No\_date 0:00 n/a .000  
 16140+ [ROUTE\_ID: 0000000000000000] 1. 02:01:GREENBANK .00 .000 No\_date 0:00 n/a .000  
 16141+ [SUM\_ 1.01:01:GREENBANK .00 .000 No\_date 0:00 n/a .000  
 16142+ RO100:CO005+ 1. 02:01:TO\_N 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16143+ \* 1. 02:01:GREENBANK .00 .000 No\_date 0:00 n/a .000  
 16144+ name :Greenbank\_0100 1. 02:01:GREENBANK .00 .000 No\_date 0:00 n/a .000  
 16145+ remark:Total Flows at Greenbank Drain  
 16146+ # Catchment Todd  
 16147+ # To Todd Drain (site of the catch)  
 16148+ # Dtnin-ID:NHNDY-  
 16149+ route: Todd with 41% imp., as per Barrhaven South MSS  
 16150+ \* 2020-11-10 increase imp. based on P598(04)-11  
 16151+ # 2020-11-10 update TDR Tributary drainage Area to = 146.616 ha based on P598(04)-11  
 16152+ [ROUTE\_ID: 0000000000000000] 1. 02:01:TO\_N 146.616 No\_date 28:01 71.80 .811 .000  
 16153+ CONTINUOUS STANDY 1. 01:01:TODD\_MN2 2.19 .428 No\_date 28:00 66.78 .754 .000  
 16154+ [ROUTE\_ID: 0000000000000000] 1. 01:01:TODD\_MN2 2.19 .428 No\_date 28:00 66.78 .754 .000  
 16155+ [XIMP\_ 53:TIMEP\_ 57]  
 16156+ [ROUTE\_ID: 0000000000000000] 1. 01:01:TODD\_MN2 2.19 .428 No\_date 28:00 66.78 .754 .000  
 16157+ [Previous] area: Iaper\_ 4.67:SLPP=1.00:LGP= 40.:MNP= 250:SCP= .01  
 16158+ [Imperious] area: IALimp\_ 1.57:SLIP=1.00:LGI= 118.1:MMI=.013:SCI= .01  
 16159+ [IaRCimp\_ 4.00:1aRCper\_ 4.00]  
 16160+ RO100:CO005+ 1. 01:01:TODD\_MN2 2.19 .428 No\_date 28:00 66.78 .754 .000  
 16161+ # Dtnin-ID:NHNDY-  
 16162+ RO100:CO005+ 1. 01:01:TODD\_MN2 2.19 .428 No\_date 28:00 66.78 .754 .000  
 16163+ CONTINUOUS STANDY 1. 01:01:TODD\_MN2 .1 .035 No\_date 28:00 66.78 .754 .000  
 16164+ [ROUTE\_ID: 0000000000000000] 1. 01:01:TODD\_MN2 .1 .035 No\_date 28:00 66.78 .754 .000  
 16165+ [XIMP\_ 53:TIMEP\_ 57]  
 16166+ [ROUTE\_ID: 0000000000000000] 1. 01:01:TODD\_MN2 .1 .035 No\_date 28:00 66.78 .754 .000  
 16167+ [Previous] area: Iaper\_ 4.67:SLPP=1.00:LGP= 40.:MNP= 250:SCP= .01  
 16168+ [Imperious] area: IALimp\_ 1.57:SLIP=1.00:LGI= 118.1:MMI=.013:SCI= .01  
 16169+ [IaRCimp\_ 4.00:1aRCper\_ 4.00]  
 16170+ RO100:CO005+ 1. 01:01:TODD\_MN2 .1 .035 No\_date 28:00 66.78 .754 .000  
 16171+ RO100:CO005+ 1. 01:01:TODD\_MN2 .1 .035 No\_date 28:00 66.78 .754 .000  
 16172+ CONTINUOUS STANDY 1. 01:01:TODD\_MN2 30.23 5.210 No\_date 28:02 68.65 .775 .000  
 16173+ [ROUTE\_ID: 0000000000000000] 1. 01:01:TODD\_MN2 30.23 5.210 No\_date 28:02 68.65 .775 .000  
 16174+ [XIMP\_ 53:TIMEP\_ 64]  
 16175+ [ROUTE\_ID: 0000000000000000] 1. 01:01:TODD\_MN2 30.23 5.210 No\_date 28:02 68.65 .775 .000  
 16176+ [Previous] area: Iaper\_ 4.67:SLPP=1.00:LGP= 40.:MNP= 250:SCP= .01  
 16177+ [Imperious] area: IALimp\_ 1.57:SLIP=1.00:LGI= 118.1:MMI=.013:SCI= .01  
 16178+ [IaRCimp\_ 4.00:1aRCper\_ 4.00]  
 16179+ RO100:CO005+ 1. 01:01:TODD\_MN2 30.23 5.210 No\_date 28:02 68.65 .775 .000  
 16180+ # Dtnin-ID:NHNDY-  
 16181+ RO100:CO005+ 1. 01:01:TODD\_MN2 30.23 5.210 No\_date 28:02 68.65 .775 .000  
 16182+ CONTINUOUS STANDY 1. 01:01:TODD\_MN2 112.91 17.286 No\_date 28:04 66.60 .752 .000  
 16183+ [ROUTE\_ID: 0000000000000000] 1. 01:01:TODD\_MN2 112.91 17.286 No\_date 28:04 66.60 .752 .000  
 16184+ [XIMP\_ 53:TIMEP\_ 77.0]  
 16185+ [Previous] area: Iaper\_ 4.67:SLPP=1.00:LGP= 40.:MNP= 250:SCP= .01  
 16186+ [Imperious] area: IALimp\_ 1.57:SLIP=1.00:LGI= 186.8:MMI=.013:SCI= .01  
 16187+ [IaRCimp\_ 4.00:1aRCper\_ 4.00]  
 16188+ RO100:CO005+ 1. 01:01:TODD\_MN2 112.91 17.286 No\_date 28:04 66.60 .752 .000  
 16189+ # Dtnin-ID:NHNDY-  
 16190+ RO100:CO005+ 1. 01:01:TODD\_MN2 112.91 17.286 No\_date 28:04 66.60 .752 .000  
 16191+ CONTINUOUS STANDY 1. 01:01:TODD\_MN2 .1 .035 No\_date 28:00 66.78 .754 .000  
 16192+ [ROUTE\_ID: 0000000000000000] 1. 01:01:TODD\_MN2 .1 .035 No\_date 28:00 66.78 .754 .000  
 16193+ [XIMP\_ 53:TIMEP\_ 52]  
 16194+ [ROUTE\_ID: 0000000000000000] 1. 01:01:TODD\_MN2 .1 .035 No\_date 28:00 66.78 .754 .000  
 16195+ [Previous] area: Iaper\_ 4.67:SLPP=1.00:LGP= 40.:MNP= 250:SCP= .01  
 16196+ [Imperious] area: IALimp\_ 1.57:SLIP=1.00:LGI= 143.1:MMI=.013:SCI= .01  
 16197+ [IaRCimp\_ 4.00:1aRCper\_ 4.00]  
 16198+ RO100:CO005+ 1. 01:01:TODD\_MN2 .1 .035 No\_date 28:00 66.78 .754 .000  
 16199+ # Dtnin-ID:NHNDY-  
 16200+ RO100:CO005+ 1. 01:01:TODD\_MN2 .1 .035 No\_date 28:00 66.78 .754 .000  
 16201+ # 5 Year + 12 Capture  
 16202+ RO100:CO005+ 1. 01:01:TODD\_MN2 2.10 .428 No\_date 28:00 66.78 .754 .000  
 16203+ ROUTE RESERVOIR --> 1. 01:02:TODD\_MN2 2.10 .428 No\_date 28:00 66.78 .754 .000  
 16204+ [ROUTE\_ID: 0000000000000000] 1. 01:02:TODD\_MN2 1.99 .268 No\_date 27:52 66.78 n/a .000  
 16205+ [overload < 0] 1. 01:02:TODD\_MN2 1.99 .268 No\_date 27:52 66.78 n/a .000  
 16206+ [MSCToCsed\_ 1204E-03 m\_ 3, TotDurVol\_ 0.00000 m\_ N-Ovf\_ 0\_ TotDurOvf\_ 0\_.hrs]  
 16207+ RO100:CO005+ 1. 01:02:TODD\_MN2 1.99 .268 No\_date 27:52 66.78 n/a .000  
 16208+ # Dtnin-ID:NHNDY-  
 16209+ RO100:CO005+ 1. 01:02:TODD\_MN2 1.99 .268 No\_date 27:52 66.78 n/a .000  
 16210+ CONTINUOUS STANDY 1. 01:02:TODD\_MN2 .1 .036 No\_date 27:52 66.78 n/a .000  
 16211+ [ROUTE\_ID: 0000000000000000] 1. 01:02:TODD\_MN2 .1 .036 No\_date 27:52 66.78 n/a .000  
 16212+ [XIMP\_ 53:TIMEP\_ 52]  
 16213+ [ROUTE\_ID: 0000000000000000] 1. 01:02:TODD\_MN2 .1 .036 No\_date 27:52 66.78 n/a .000  
 16214+ [Previous] area: Iaper\_ 4.67:SLPP=1.00:LGP= 40.:MNP= 250:SCP= .01  
 16215+ [Imperious] area: IALimp\_ 1.57:SLIP=1.00:LGI= 143.1:MMI=.013:SCI= .01  
 16216+ [IaRCimp\_ 4.00:1aRCper\_ 4.00]  
 16217+ RO100:CO005+ 1. 01:02:TODD\_MN2 .1 .036 No\_date 27:52 66.78 n/a .000  
 16218+ # Dtnin-ID:NHNDY-  
 16219+ RO100:CO005+ 1. 01:02:TODD\_MN2 .1 .036 No\_date 27:52 66.78 n/a .000  
 16220+ COMPUTE DUALHYD 1. 01:02:A1 25.50 3.894 No\_date 28:03 62.46 n/a .000  
 16221+ Major System / 1. 01:02:A1-MN 1.02 2.818 No\_date 28:03 62.46 n/a .000  
 16222+ Minor System / 1. 01:02:A1-MN 1.02 2.818 No\_date 28:03 62.46 n/a .000  
 16223+ Minor System / 1. 01:02:A1-MN 1.02 2.818 No\_date 28:03 62.46 n/a .000  
 16224+ Minor System / 1. 01:02:A1-MN 1.02 2.818 No\_date 28:03 62.46 n/a .000  
 16225+ SUM+ 1. 01:02:TODD\_MN2 121.36 15.844 No\_date 28:03 66.71 n/a .000  
 16226+ [ROUTE\_ID: 0000000000000000] 1. 01:02:TODD\_MN2 121.36 15.844 No\_date 28:03 66.71 n/a .000  
 16227+ [XIMP\_ 53:TIMEP\_ 52]  
 16228+ [ROUTE\_ID: 0000000000000000] 1. 01:02:TODD\_MN2 121.36 15.844 No\_date 28:03 66.71 n/a .000  
 16229+ [Previous] area: Iaper\_ 4.67:SLPP=1.00:LGP= 40.:MNP= 250:SCP= .01  
 16230+ [Imperious] area: IALimp\_ 1.57:SLIP=1.00:LGI= 143.1:MMI=.013:SCI= .01  
 16231+ [IaRCimp\_ 4.00:1aRCper\_ 4.00]  
 16232+ RO100:CO005+ 1. 01:02:TODD\_MN2 121.36 15.844 No\_date 28:03 66.71 n/a .000  
 16233+ # Dtnin-ID:NHNDY-  
 16234+ RO100:CO005+ 1. 01:02:TODD\_MN2 121.36 15.844 No\_date 28:03 66.71 n/a .000  
 16235+ CONTINUOUS STANDY 1. 01:02:TODD\_MN2 .1 .036 No\_date 28:03 66.71 n/a .000  
 16236+ [ROUTE\_ID: 0000000000000000] 1. 01:02:TODD\_MN2 .1 .036 No\_date 28:03 66.71 n/a .000  
 16237+ # Tod Pond 3  
 16238+ # - Rating curve obtained from Barrhaven South MSS model  
 16239+ route: Tod Pond 3 to Tod Pond 3 + 183 ha  
 16240+ # Dtnin-ID:NHNDY-  
 16241+ RO100:CO005+ 1. 01:02:TODD\_MN2 .1 .036 No\_date 28:03 66.71 n/a .000  
 16242+ RO100:CO005+ 1. 01:02:TODD\_MN2 .1 .036 No\_date 28:03 66.71 n/a .000  
 16243+ [ROUTE\_ID: 0000000000000000] 1. 01:02:TODD\_MN2 .1 .036 No\_date 28:03 66.71 n/a .000  
 16244+ [XIMP\_ 53:TIMEP\_ 050]  
 16245+ [ROUTE\_ID: 0000000000000000] 1. 01:02:TODD\_MN2 .1 .036 No\_date 28:03 66.71 n/a .000  
 16246+ [Previous] area: Iaper\_ 4.67:SLPP=1.00:LGP= 40.:MNP= 250:SCP= .01  
 16247+ [Imperious] area: IALimp\_ 1.57:SLIP=1.00:LGI= 143.1:MMI=.013:SCI= .01  
 16248+ [IaRCimp\_ 4.00:1aRCper\_ 4.00]  
 16249+ RO100:CO005+ 1. 01:02:TODD\_MN2 .1 .036 No\_date 28:03 66.71 n/a .000  
 16250+ ADD HYD 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16251+ \* [ROUTE\_ID: 0000000000000000] 1. 02:4241-out 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16252+ [L/S:n\_ 280.0 / .050/.045]  
 16253+ RO100:CO005+ 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16254+ SAVE HYD 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16255+ name :TOD\_POND\_0100 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16256+ remark:Total Flows at Toddrain  
 16257+ # Catchment Toddrain  
 16258+ # Dtnin-ID:NHNDY-  
 16259+ RO100:CO005+ 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16260+ ADD HYD 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16261+ \* [ROUTE\_ID: 0000000000000000] 1. 02:4241-out 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16262+ [L/S:n\_ 280.0 / .050/.045]  
 16263+ RO100:CO005+ 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16264+ # Dtnin-ID:NHNDY-  
 16265+ RO100:CO005+ 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16266+ SAVE HYD 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16267+ remark:Total Flows at Toddrain  
 16268+ # Hydrograph from Toddrain routed to Coughlin Park  
 16269+ route: Toddrain to Coughlin Park  
 16270+ # Dtnin-ID:NHNDY-  
 16271+ RO100:CO005+ 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16272+ [ROUTE\_ID: 0000000000000000] 1. 02:4241-out 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16273+ [L/S:n\_ 280.0 / .050/.045]  
 16274+ RO100:CO005+ 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16275+ # Dtnin-ID:NHNDY-  
 16276+ RO100:CO005+ 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16277+ ADD HYD 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16278+ \* [ROUTE\_ID: 0000000000000000] 1. 02:4241-out 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16279+ [L/S:n\_ 280.0 / .050/.045]  
 16280+ RO100:CO005+ 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16281+ # Dtnin-ID:NHNDY-  
 16282+ RO100:CO005+ 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16283+ ADD HYD 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16284+ \* [ROUTE\_ID: 0000000000000000] 1. 02:4241-out 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16285+ [L/S:n\_ 280.0 / .050/.045]  
 16286+ RO100:CO005+ 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16287+ # Dtnin-ID:NHNDY-  
 16288+ RO100:CO005+ 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16289+ ADD HYD 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16290+ \* [ROUTE\_ID: 0000000000000000] 1. 02:4241-out 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16291+ [L/S:n\_ 280.0 / .050/.045]  
 16292+ RO100:CO005+ 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16293+ # Dtnin-ID:NHNDY-  
 16294+ RO100:CO005+ 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16295+ ADD HYD 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16296+ \* [ROUTE\_ID: 0000000000000000] 1. 02:4241-out 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16297+ [L/S:n\_ 280.0 / .050/.045]  
 16298+ RO100:CO005+ 1. 02:4241 54717.80 144.894 No\_date 36:50 39.32 n/a .000  
 16299+ # Dtnin-ID:N



16831+ ROUTE RESERVOIR -> 1.0 02:MILLS 175.99 20.390 No\_date 28:06 56.87 n/a .000  
 16832+ [ROUTE] out <= 1.0 01:MILL\_P 146.23 10.050 No\_date 28:08 56.87 n/a .000  
 16833+ [ROUTE] overflw <= 1.0 01:MILL\_P 29.77 16.228 No\_date 28:08 56.87 n/a .000  
 16834+ [Metcalled...\_2180>01 m3\_TotCvVol... m3\_N-Ovf... 2. TotSurf= 1. hrs] ---DWFcms  
 16835+ R0100:C00426-----Dtnin-ID:HYDRO-  
 16836+ ADD HYD + 1.0 02:N\_MU 55220.07 145.768 No\_date 36:53 39.46 n/a .000  
 16837+ [ROUTE CHANNEL] -> 1.0 02:ML-OV 29.77 16.228 No\_date 28:08 56.87 n/a .000  
 16838+ [ROUTE CHANNEL] -> 1.0 02:SN\_MU 55196.05 146.399 No\_date 36:53 39.51 n/a .000  
 16839+ SUM... 1.0 01:SN\_MU 55196.05 146.399 No\_date 36:53 39.51 n/a .000  
 16840+ frame : SN\_MU\_0100 55196.05 146.399 No\_date 36:58 39.51 n/a .000  
 16841+ remark:Total Flows at Jockvale Road  
 16842+ [ROUTE CHANNEL] -> 1.0 01:SN\_MU  
 16843+ frame : SN\_MU\_0100  
 16844+ # Hydrograph from Jockvale Road routed to Heart's Desire  
 16845+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 689  
 16846+ # ROUTE CHANNEL -> 1.0 02:SN\_MU 55196.05 146.399 No\_date 36:58 39.51 n/a .000  
 16847+ [ROUTE CHANNEL] -> 1.0 01:SN\_MU 55196.05 146.071 No\_date 37:13 39.51 n/a .000  
 16848+ [XSEC#\_25:TIME...\_28] ---Dtnin-ID:HYDRO-  
 16849+ [ARBAh-OPENKms-TpeakDate\_bh:mm---RVMw-R.C.---DWFcms  
 16850+ ROUTE CHANNEL -> 1.0 01:SN\_MU 23.78 3.004 No\_date 28:03 53.11 .600  
 16851+ [L/S/nr\_1982 / .223/.048] ---  
 16852+ [(Max= 1.442)Max= 2.661]  
 16853+ \*\*\*\*\*  
 16854+ # Catchment DESIRE  
 16855+ # - To Jock River (north of the Rock)  
 16856+ # - Residential area (Heart's Desire Community)  
 16857+ \*\*\*\*\*  
 16858+ R0100:C00429-----Dtnin-ID:HYDRO-  
 16859+ [ARBAh-OPENKms-TpeakDate\_bh:mm---RVMw-R.C.---DWFcms  
 16860+ [ROUTE CHANNEL] -> 1.0 01:DESIRE 23.78 3.004 No\_date 28:03 53.11 .600  
 16861+ [LGS#\_2 C/Nr\_77.0] ---  
 16862+ [Imperialv. areas: IaImp= 4.67 SLDP1=1.00 LGP= 40. MNW= 250 SCP= .0]  
 16863+ [Imperialv. areas: IaImp= 1.57 SLDP1=1.00 LGP= 400. MNW= 0.013 SCI= .0]  
 16864+ [Imperialv. areas: IaImp= 4.00 IMRPer= 4.00]  
 16865+ [Imperialv. areas: IaImp= 15.00 SLDP1=1.00]  
 16866+ \*\*\*\*\*  
 16867+ # Catchment JOCKVA  
 16868+ # - Residential area / golf course  
 16869+ # - Residential area / golf course  
 16870+ # JFSA 2021-01-11 update JOCKVA after updating CORRG as per ISI GROUP, July 2008.  
 16871+ [ROUTE CHANNEL] -> 1.0 01:JOCKVA 257.63 No\_date 28:07 62.70 .708 .000  
 16872+ \*\*\*\*\*  
 16873+ R0100:C00430-----Dtnin-ID:HYDRO-  
 16874+ [ARBAh-OPENKms-TpeakDate\_bh:mm---RVMw-R.C.---DWFcms  
 16875+ CONTINUOUS STANHYD 1.0 01:JOCKVA 26.13 28.623 No\_date 28:07 62.70 .708 .000  
 16876+ [XIND...\_50:TIME...\_50] ---  
 16877+ [LGS#\_2 C/Nr\_77.0] ---  
 16878+ [Imperialv. areas: IaImp= 4.67 SLDP1=1.00 LGP= 40. MNW= 250 SCP= .0]  
 16879+ [Imperialv. areas: IaImp= 1.57 SLDP1=1.00 LGP= 1311. MNW= 0.013 SCI= .0]  
 16880+ [Imperialv. areas: IaImp= 4.00 IMRPer= 4.00]  
 16881+ [Imperialv. areas: IaImp= 55.67 SLDP1=1.00]  
 16882+ \*\*\*\*\*  
 16883+ R0100:C00431-----Dtnin-ID:HYDRO-  
 16884+ [ARBAh-OPENKms-TpeakDate\_bh:mm---RVMw-R.C.---DWFcms  
 16885+ ADD HYD + 1.0 02:JOCKVA 30.77 1.275 No\_date 27:48 60.48 n/a .000  
 16886+ [ROUTE CHANNEL] -> 1.0 02:JOCKVA 225.13 26.423 No\_date 28:07 62.70 n/a .000  
 16887+ [ROUTE CHANNEL] -> 1.0 02:B2-MU .36 .820 No\_date 28:05 62.88 n/a .000  
 16888+ [ROUTE CHANNEL] -> 1.0 02:B2-MU 1.4 .820 No\_date 28:05 62.88 n/a .000  
 16889+ SUM... 1.0 01:SN\_DE 256.41 31.850 No\_date 28:06 62.71 n/a .000  
 16890+ frame : SN\_DE\_0100 256.41 31.850 No\_date 28:06 62.71 n/a .000  
 16891+ [ARBAh-OPENKms-TpeakDate\_bh:mm---RVMw-R.C.---DWFcms  
 16892+ remark:Total Flows at TO\_1010  
 16893+ \*\*\*\*\*  
 16894+ # Jockvale SWM Facility  
 16895+ # - Rating curve obtained from Jockvale Servicing Study (CLL 1999)  
 16896+ # - Undeveloped floodplain and river  
 16897+ # - Residential area / golf course  
 16898+ R0100:C00433-----Dtnin-ID:HYDRO-  
 16899+ [ARBAh-OPENKms-TpeakDate\_bh:mm---RVMw-R.C.---DWFcms  
 16900+ ROUTE RESERVOIR -> 1.0 02:JOCKVA\_TO 256.41 31.850 No\_date 28:06 62.71 n/a .000  
 16901+ [ROUTE CHANNEL] -> 1.0 02:JOCKVA\_TO 256.41 31.850 No\_date 28:06 62.71 n/a .000  
 16902+ [ROUTE CHANNEL] -> 1.0 02:SN\_DE 256.41 31.850 No\_date 28:06 62.71 n/a .000  
 16903+ [ROUTE CHANNEL] -> 1.0 02:SN\_DE 256.41 31.850 No\_date 28:06 62.71 n/a .000  
 16904+ [ROUTE CHANNEL] -> 1.0 02:JOCK\_P 256.41 12.850 No\_date 28:35 62.71 n/a .000  
 16905+ SUM... 1.0 01:SN\_DE 55476.29 147.027 No\_date 37:12 39.63 n/a .000  
 16906+ frame : SN\_DE\_0100 55476.29 147.027 No\_date 37:12 39.63 n/a .000  
 16907+ SAVE HYD 1.0 01:SN\_DE 55476.29 147.027 No\_date 37:12 39.63 n/a .000  
 16908+ frame : SN\_DE\_0100  
 16909+ remark:Total Flows at Heart's Desire  
 16910+ # Hydrograph from Heart's Desire routed to Sidas River  
 16911+ # Channel X-Section obtained from RVCA Hydraulic Model - Station 0  
 16912+ R0100:C00436-----Dtnin-ID:HYDRO-  
 16913+ [ARBAh-OPENKms-TpeakDate\_bh:mm---RVMw-R.C.---DWFcms  
 16914+ ROUTE CHANNEL -> 1.0 02:SN\_DE 256.41 147.027 No\_date 37:12 39.63 n/a .000  
 16915+ [ROUTE CHANNEL] -> 1.0 01:NL 55476.29 147.014 No\_date 37:15 39.63 n/a .000  
 16916+ [ROUTE CHANNEL] -> 1.0 01:JOCK\_P 55476.29 147.014 No\_date 37:15 39.63 n/a .000  
 16917+ [L/S/nr\_1983 / .967/.048] ---  
 16918+ [L/S/nr\_2000 / .223/.048] ---  
 16919+ \*\*\*\*\*  
 16920+ # Catchment SIDA  
 16921+ # - To Jock River (north and south)  
 16922+ # - Undeveloped floodplain and river  
 16923+ # - Residential area / golf course  
 16924+ R0100:C00437-----Dtnin-ID:HYDRO-  
 16925+ CONTINUOUS WASHYD 1.0 01:S2 102.94 5.685 No\_date 28:20 40.98 .462 .000  
 16926+ [CN\_72 NO\_00: Tp\_00: 102.94 5.685] ---  
 16927+ [ROUTE CHANNEL] -> 1.0 04:SN\_DE 256.41 31.850 No\_date 28:20 40.98 .462 .000  
 16928+ [InterEventTime...\_12.00] ---  
 16929+ R0100:C00438-----Dtnin-ID:HYDRO-  
 16930+ [ARBAh-OPENKms-TpeakDate\_bh:mm---RVMw-R.C.---DWFcms  
 16931+ ADD HYD + 1.0 02:NL 55476.29 147.014 No\_date 37:15 39.63 n/a .000  
 16932+ [ROUTE CHANNEL] -> 1.0 02:NL 102.94 5.685 No\_date 28:20 40.98 n/a .000  
 16933+ [ROUTE CHANNEL] -> 1.0 01:NL 55476.29 147.014 No\_date 37:15 39.63 n/a .000  
 16934+ SAVE HYD 1.0 01:SN\_DE 55479.19 147.276 No\_date 37:15 39.63 n/a .000  
 16935+ frame : SN\_DE\_0100  
 16936+ remark:Total Flows at Ridaue River  
 16937+ #####  
 16938+ FINISH  
 16939+ -----  
 16940+ -----  
 16941+ -----  
 16942+ [WARNING / ERRORS / NOTES  
 16943+ -----  
 16944+ R0021:C00319 ROUTE RESERVOIR  
 16945+ \*\*\* WARNING: Inflow peak was not reduced! Check OUTFLOW/STORAGE table or reduce DT.  
 16946+ R0021:C00341 ROUTE PIPE ->  
 16947+ [ROUTE CHANNEL] -> 1.0 02:ROUTE PIPE used for routing.  
 16948+ R0021:C00347 ROUTE PIPE ->  
 16949+ \*\*\* WARNING: New pipe size used for routing.  
 16950+ R0021:C00407 ROUTE PIPE ->  
 16951+ \*\*\* NOTE: Inflow hyd. is dry and cannot be diverted.  
 16952+ R0021:C00400 ROUTE PIPE ->  
 16953+ \*\*\* WARNING: New pipe size used for routing.  
 16954+ R0021:C00407 ROUTE PIPE ->  
 16955+ \*\*\* WARNING: New pipe size used for routing.  
 16956+ R0021:C00416 ROUTE PIPE ->  
 16957+ \*\*\* WARNING: New pipe size used for routing.  
 16958+ R0021:C00416 ROUTE PIPE ->  
 16959+ \*\*\* WARNING: New pipe size used for routing.  
 16960+ R0021:C00417 ROUTE PIPE ->  
 16961+ \*\*\* WARNING: New pipe size used for routing.  
 16962+ R0021:C00417 ROUTE PIPE ->  
 16963+ \*\*\* WARNING: Inflow peak was not reduced! Check OUTFLOW/STORAGE table or reduce DT.  
 16964+ R0021:C00417 ROUTE PIPE ->  
 16965+ \*\*\* WARNING: New pipe size used for routing.  
 16966+ R0021:C00437 ROUTE PIPE ->  
 16967+ \*\*\* WARNING: New pipe size used for routing.  
 16968+ R0021:C00437 ROUTE PIPE ->  
 16969+ \*\*\* WARNING: New pipe size used for routing.  
 16970+ R0021:C00437 ROUTE PIPE ->  
 16971+ \*\*\* WARNING: New pipe size used for routing.  
 16972+ R0021:C00372 ROUTE PIPE ->  
 16973+ R0021:C00372 ROUTE PIPE ->  
 16974+ R0021:C00372 ROUTE PIPE ->  
 16975+ \*\*\* NOTE: Inflow hyd. is dry and cannot be diverted.  
 16976+ R0021:C00400 ROUTE PIPE ->  
 16977+ \*\*\* WARNING: New pipe size used for routing.  
 16978+ R0021:C00400 ROUTE PIPE ->  
 16979+ \*\*\* WARNING: New pipe size used for routing.  
 16980+ R0100:C00347 ROUTE PIPE ->  
 16981+ \*\*\* WARNING: New pipe size used for routing.  
 16982+ R0100:C00347 ROUTE PIPE ->  
 16983+ \*\*\* WARNING: New pipe size used for routing.  
 16984+ R0021:C00416 ROUTE PIPE ->  
 16985+ \*\*\* WARNING: New pipe size used for routing.  
 16986+ R0021:C00416 ROUTE PIPE ->  
 16987+ \*\*\* WARNING: New pipe size used for routing.  
 16988+ R0021:C00417 ROUTE PIPE ->  
 16989+ \*\*\* WARNING: New pipe size used for routing.  
 16990+ R0021:C00417 ROUTE PIPE ->  
 16991+ \*\*\* WARNING: New pipe size used for routing.  
 16992+ R0021:C00417 ROUTE PIPE ->  
 16993+ \*\*\* WARNING: New pipe size used for routing.  
 16994+ R0021:C00417 ROUTE PIPE ->  
 16995+ \*\*\* WARNING: New pipe size used for routing.  
 16996+ R0021:C00372 ROUTE PIPE ->  
 16997+ R0021:C00372 ROUTE PIPE ->  
 16998+ R0021:C00372 DIVERT HYD ->  
 16999+ \*\*\* NOTE: Inflow hyd. is dry and cannot be diverted.  
 17000+ R0021:C00372 ROUTE PIPE ->  
 17001+ \*\*\* WARNING: New pipe size used for routing.  
 17002+ R0100:C00400 ROUTE PIPE ->  
 17003+ \*\*\* WARNING: New pipe size used for routing.  
 17004+ R0100:C00407 ROUTE PIPE ->  
 17005+ \*\*\* WARNING: New pipe size used for routing.  
 17006+ R0100:C00407 ROUTE PIPE ->  
 17007+ \*\*\* WARNING: New pipe size used for routing.  
 17008+ R0100:C00408 ROUTE PIPE ->  
 17009+ \*\*\* WARNING: New pipe size used for routing.  
 17010+ R0100:C00417 ROUTE PIPE ->  
 17011+ \*\*\* WARNING: New pipe size used for routing.  
 17012+ R0241:C00341 ROUTE PIPE ->  
 17013+ \*\*\* WARNING: New pipe size used for routing.  
 17014+ R0241:C00347 ROUTE PIPE ->  
 17015+ \*\*\* WARNING: New pipe size used for routing.  
 17016+ R0242:C00363 ROUTE PIPE ->  
 17017+ \*\*\* WARNING: New pipe size used for routing.

# Attachment F

Updated Subcatchment Schematics & Tables

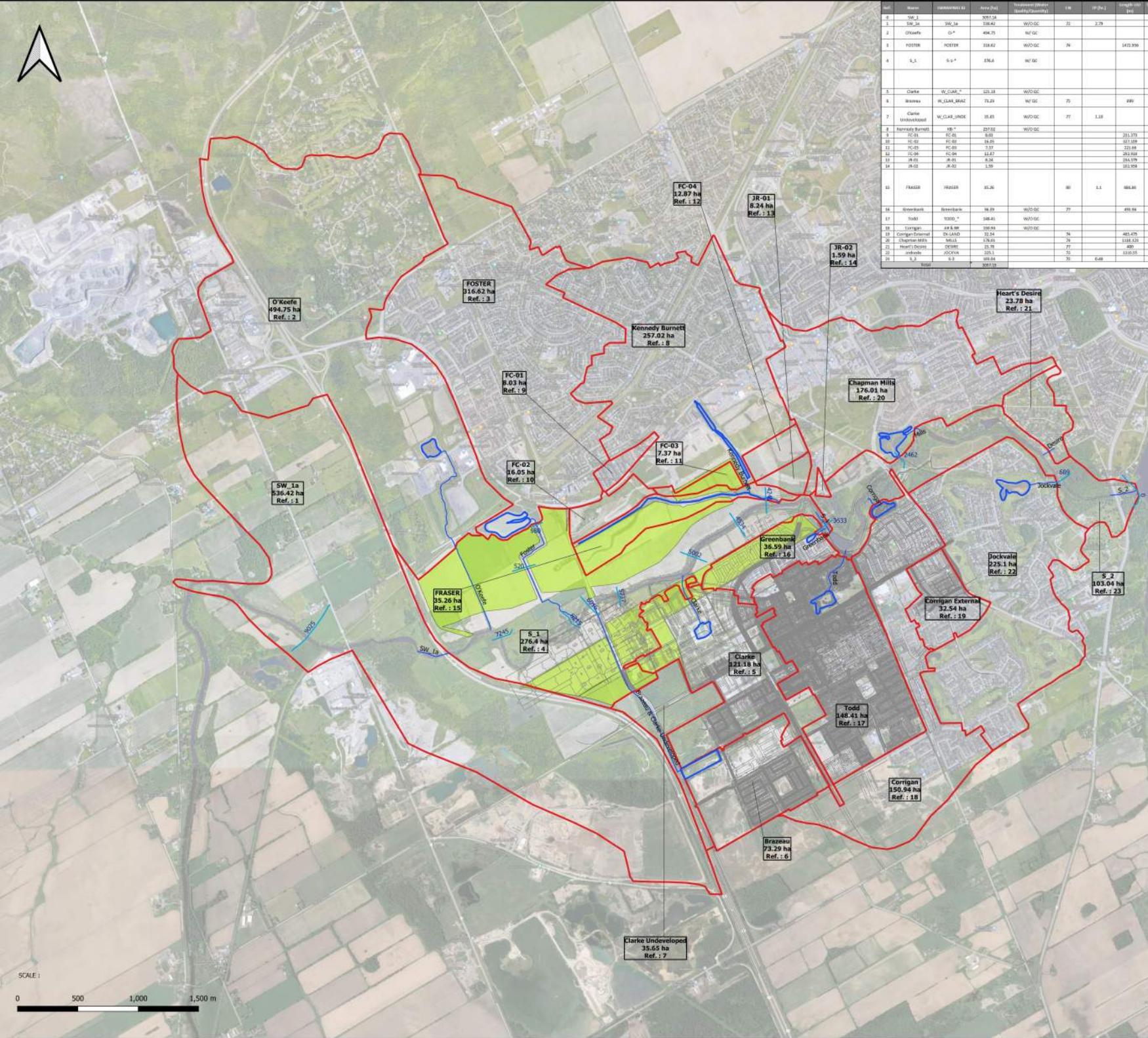


Figure 3 - Overall Jock River Lower Reach one Sub-catchments.pdf

SW\_1a              Area ID  
536.42 ha          Area (ha)  
Ref. 1              Reference Number

**J.F. Sabourin and Associates Inc.**  
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**DSEL**  
david schaeffer engineering ltd

PROJECT

BCDC - Quantity Control Study

**TITLE:**

Figure 3 - Overall Jock River Lower Reach one Sub-catchments

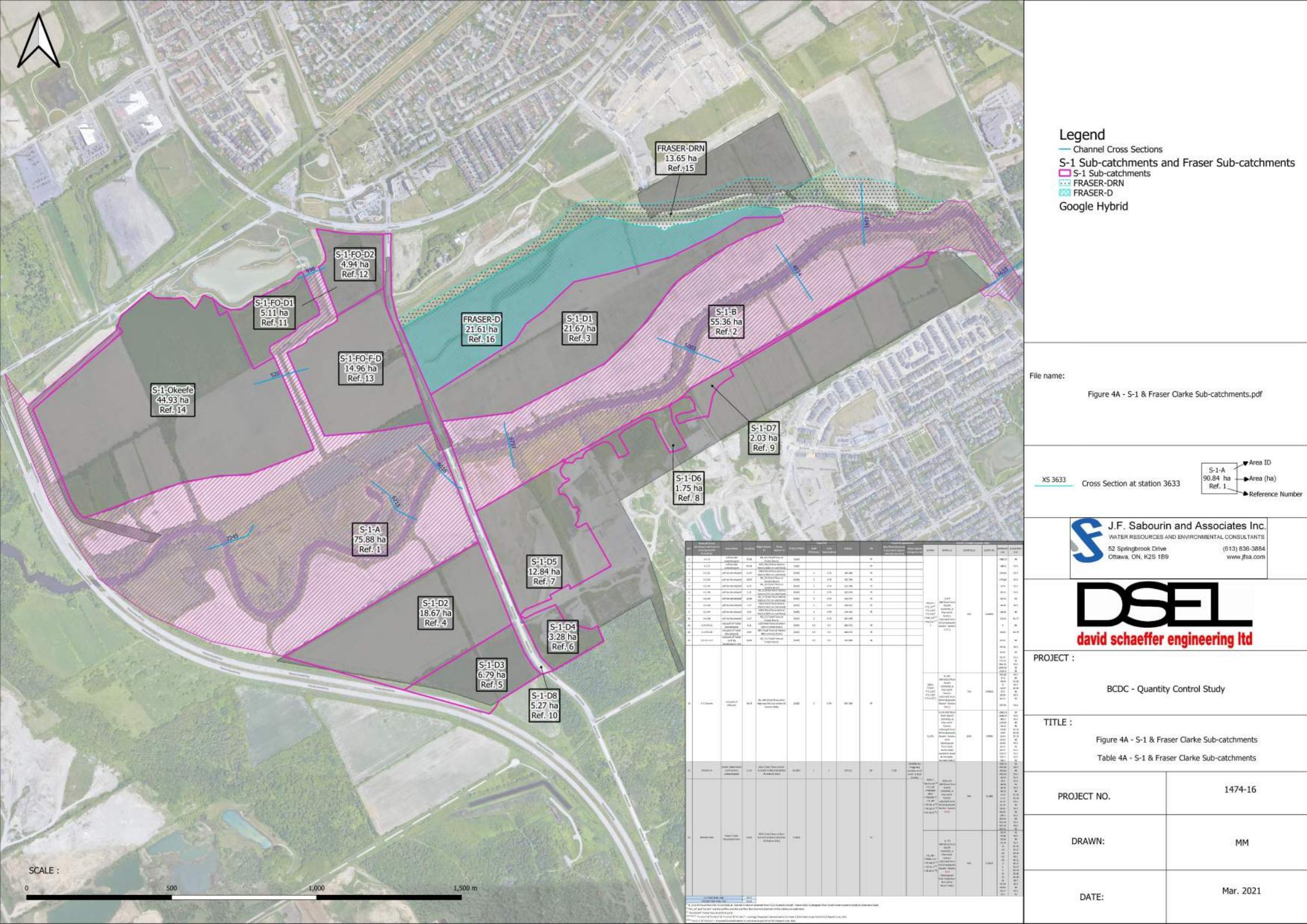
Table 3 - Overall Jock River Lower Reach one Sub-catchments

PROJECT NO. 1474-16

BRUNNEN

DATE: Mar. 2021





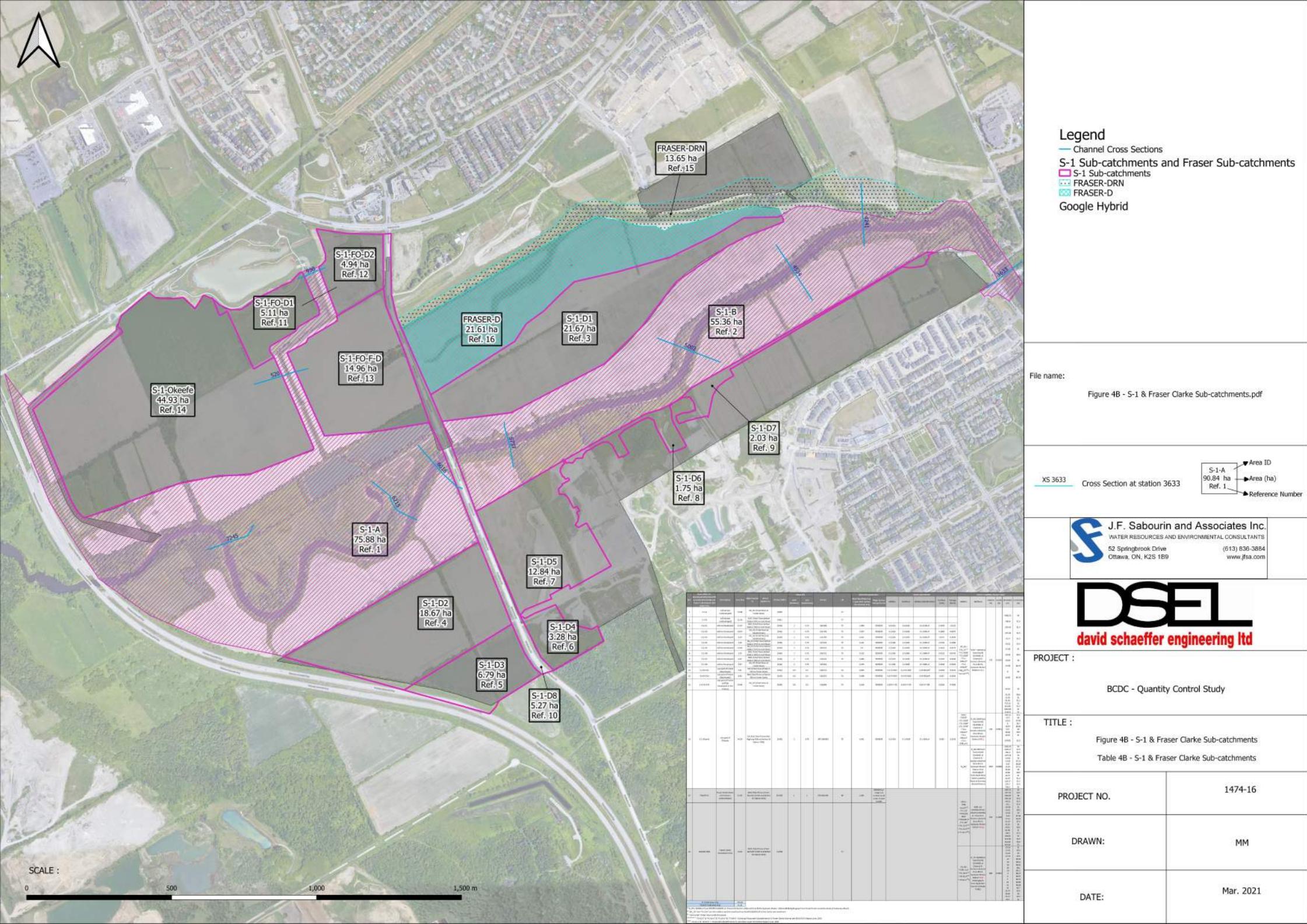
<sup>(1)</sup> N\_CE is NYHDot from ROUTE CHANNEL at Channel X-Section obtained from RVCA Hydraulic Model - Station 6016 (Hydrograph from Node Foster routed to Node at Cedarview Road)

<sup>(2)</sup> "MS\_P2" and "P2-OVF" are the outflow and the overflow from ROUTE RESERVOIR of the Clarke sub-catchment

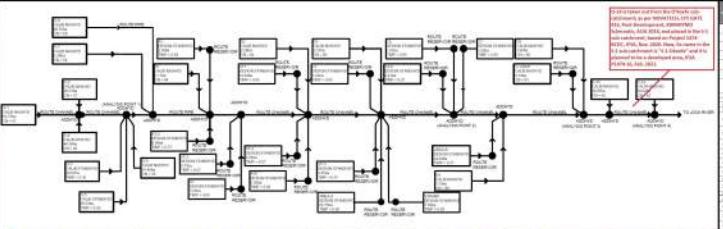
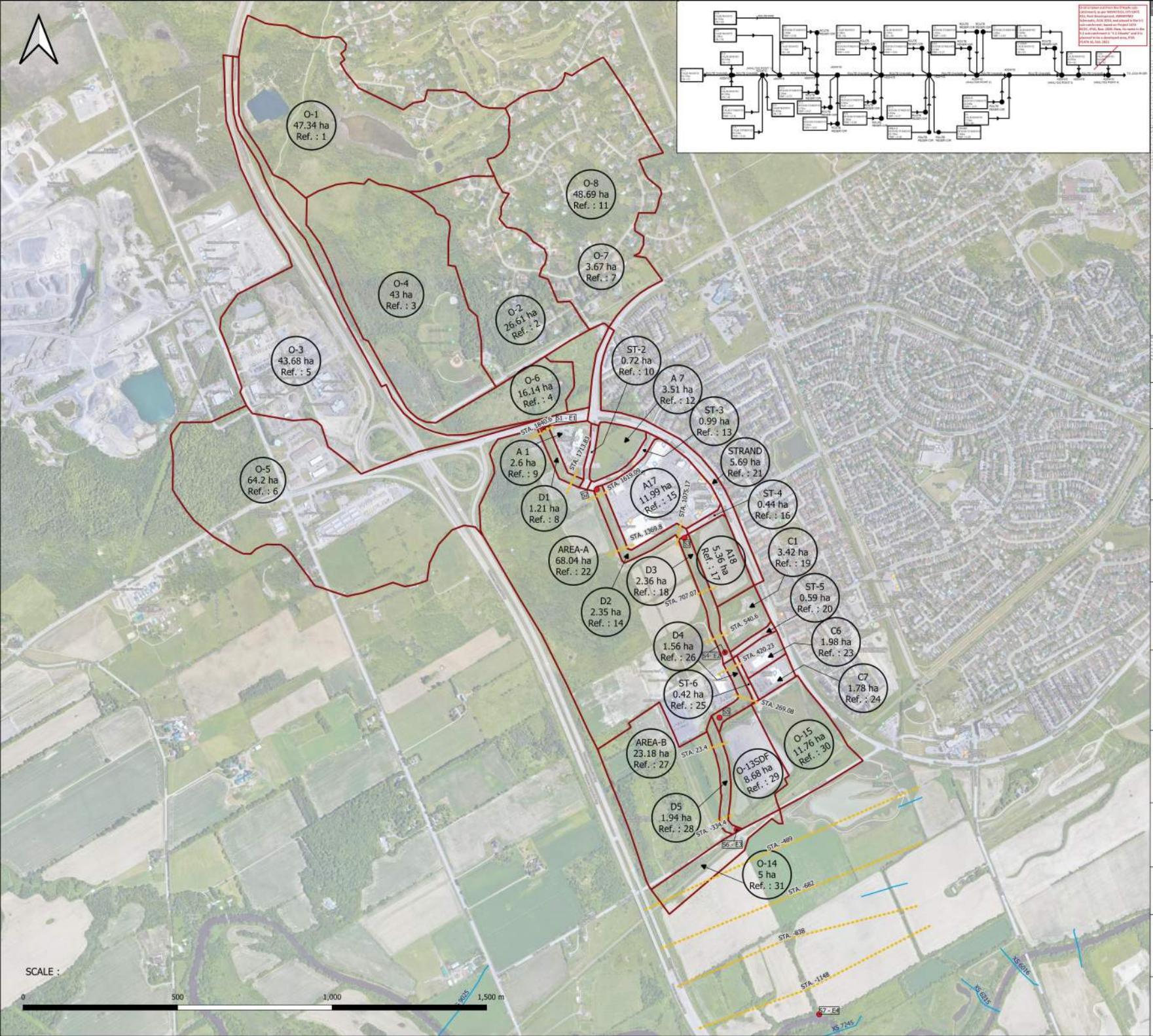
(3) "KB-Pond3" =Total Flows at KB third pond

(4 & 5 & 6 & 7) "FC-01-S" & "FC-02-S" & "FC-03-S" & "FC-04-S" = Existing / Proposed Subcatchments To Fraser Clarke Drain as per NOVATECH Report June, 2020

(8 & 9) "JR-01-S" & "JR-02-S" = Proposed Subcatchments To Jock River as per NOVATECH Report June, 2020



Ref.	Name ID (S-1 is developed with DUALHYD & ROUTE RESERVOIR and Fraser is developed with DUALHYD)	Description	Area (ha)	Major System To	Minor System To	TP (hr) [TIMP]	Slope (%)		LGI (m)	CN	DUALHYD parameters		ROUTE RESERVOIR					ROUTE CHANNEL (Station 5002)							
							SLPP (Pervious)	SLPI (Impervious)			Max Flow Rate(cms)- 5-year inlet capture rate (24-hour SCS)	Major System storage (cu-m)	NHYDin	NHYDout	NHYDovf (OVERFLOW)	Outflow (cms)	Storage (ha-m)	NHYDin	NHYDout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)		
1	S-1-A	will remain undeveloped	75.88	SN_FO (Total Flows at Foster Drain)		0.619			77											-1060.52	94				
2	S-1-B	will remain undeveloped	55.36	4241 (Total Flows before Station 4241)		0.451			77											-268.6	91.5				
3	S-1-D1	will be Developed	21.67	5002 (Total Flows before Station 5002)	[0.65]	2	0.75	380.088	75	2.409	9999999	S-1-D1S	S-1-D1R	S-1-D1Rovf	0.3033	1.0125				-259.43	91.5				
4	S-1-D2	will be Developed	18.67	SN_OK (Total Flows at O'keefe Drain)	[0.65]	2	0.75	352.798	75	2.097	9999999	S-1-D2S	S-1-D2R	S-1-D2Rovf	0.2485	0.8297				-179.48	91.5				
5	S-1-D3	will be Developed	6.79	SN_OK (Total Flows at O'keefe Drain)	[0.65]	2	0.75	212.760	75	0.831	9999999	S-1-D3S	S-1-D3R	S-1-D3Rovf	0.079	0.2639				-67.9	91.5				
6	S-1-D4	will be Developed	3.28	SN_CE (Total Flows before Station 5737)	[0.65]	2	0.75	147.874	75	0.421	9999999	S-1-D4S	S-1-D4R	S-1-D4Rovf	0.0392	0.1308				-59.21	91.5				
7	S-1-D5	will be Developed	12.84	SN_CE (Total Flows before Station 5737)	[0.65]	2	0.75	292.575	75	1.5	9999999	S-1-D5S	S-1-D5R	S-1-D5Rovf	0.1611	0.5377				-33.19	91				
8	S-1-D6	will be Developed	1.75	5002 (Total Flows before Station 5002)	[0.65]	2	0.75	108.012	75	0.232	9999999	S-1-D6S	S-1-D6R	S-1-D6Rovf	0.0222	0.0742				-26.08	90.5				
9	S-1-D7	will be Developed	2.03	5002 (Total Flows before Station 5002)	[0.65]	2	0.75	116.333	75	0.265	9999999	S-1-D7S	S-1-D7R	S-1-D7Rovf	0.2767	0.9238				-24.04	90				
10	S-1-D8	will be Developed	5.27	SN_FO (Total Flows at Foster Drain)	[0.65]	2	0.75	187.439		0.672	9999999	S-1-D8S	S-1-D8R	S-1-D8Rovf	0.0630	0.2102				-13.14	86.77				
11	S-1-FO-D1	was part of Foster (Developed)	5.11	520 (Total Flows at Sation 520 on Foster Drain)	[0.65]	0.5	0.5	184.572	74	0.605	9999999	S-1-FO-D1S	S-1-FO-D1R	S-1FOD1ovf	0.0693	0.2313				0	85				
12	S-1-FO-D2	was part of Foster (Developed)	4.94	980 (Total Flows at Station 980 on Foster Drain)	[0.55]	0.5	0.5	181.475	74	0.508	9999999	S-1-FO-D2S	S-1-FO-D2R	S-1FOD2ovf	0.067	0.2236				14.68	86.74				
13	S-1-FO-F-D	was part of Foster (will be Developed in the Future)	14.96	SN_FO (Total Flows at Foster Drain)	[0.65]	0.5	0.5	315.806	74	1.615	9999999	S-1FO-F-DS	S-1FO-F-DR	S-1FO-F-DR	0.2215	0.7396				23.92	90				
																			25.78	90.5					
																			31.91	91					
																			91.95	91.5					
																			772.15	92					
																			961.49	92.5					
																			1044.69	93					
																			1130.8	95					
14	S-1-Okeefe	was part of O'keefe	44.93	SN_416 (Total Flows after Highway 416 and before XS Station 7245)	[0.65]	2	0.75	547.296	75	4.591	9999999	S-1-OKs	S-1-OKSR	S-1-OkSovf	0.639	2.1333				5002= ["N_CE" <sup>(1)</sup> + "S-1-D1R" + "S-1-D5R" + "S-1-D7R" + "S-1-D1Rovf" + "S-1-D6Rovf" + "S-1-D5Rovf"]	N_WC (NHYDout from ROUTE CHANNEL at Channel X-Section obtained from RVCA Hydraulic Model - Station 5002 )	736	0.09511	-601.81	91.5
																			-37.5	90					
																			-19.61	87.04					
																			0	85.7					
																			14.87	86.93					
																			37.5	90					
																			38.54	90.5					
																			42.23	91					
																			157.05	91.5					
15	FRASER-D	Fraser Clarke Drain (will remain undeveloped)	21.61	4241 (Total Flows at Ken-Burnett Outlet and before XS Station 4241)	[0.585]	1	1	379.561	80	2.281	9999999 (an imaginary number so all water is kept Inside)								-909.72	95					
																			-907.09	94.5					
																			-904.65	94					
																			-902.26	93.5					
																			-44.51	91.5					
																			-25.1	91.5					
																			-20.98	91					
																			-20.61	90.5					
																			-20.12	90					
																			-6.13	87.26					
																			17.51	86.56					
																			31.37	87.2					
																			45.26	90					
																			50.41	90.5					
																			63.06	91					
																			134.5	91.5					
																			190.63	92					
																			251.98	92.5					
																			321.32	93.5					
																			403.84	95					
16	FRASER-DRN	Fraser Clarke Developed Area	13.65	4241 (Total Flows at Ken-Burnett Outlet and before XS Station 4241)	0.4258				77										-29.24	91					
		</																							



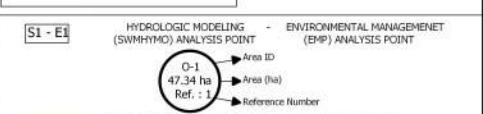
**File name:**

Figure F1 - O'Keefe Sub-catchments.pdf

## Legend

20210129-O'Keefe Sub-catchment Boundaries  
O'Keefe Sub-catchment Boundaries  
Google Hybrid

Boundaries X5 7245 Cross Section at station 7245



**DSEL**  
david schaeffer engineering ltd

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**PROJECT :**

BCDC - Quantity Control Study

**TITLE :** Figure F1 - O'Keefe Sub-catchments

Table E1 - O'Keefe Sub-catchments

#### Schematic F1 - O'Keefe Sub-catchments

1472

PROJECT NO.:

DRAWN: MM

Mar. 2021

Ref.	ID O'Keefe	Area (ha) (from Novatech Report AUG2014)	Area (ha) (from GIS- JFSA P1474-16-QC,JAN2021)	Major System To	Minor System To	T. Imperv. [TP (hr)]	XIMP	CN	Slope (%)	ROUTE RESERVOIR					ROUTE CHANNEL [ROUTE PIPE]					
										NHYdin	NHYDout	NHYDovf (OVERFLOW)	Outflow (cms)	Storage (ha-m)	NHYdin	NHYDout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)
1	O-1	63.72	47.34	OKF-N (NORTH OF	[0.9]			61									0	2		
2	O-2	28.61	26.61	OKF-N (NORTH OF	[1.1]			57								4	0			
3	O-4	46.94	43	OKF-N (NORTH OF	[0.9]			49								6	0			
4	O-6	16.46	16.14	PT1 <sup>(1)</sup> (WEST OF THE	[0.7]			43								10	2			
5	O-3	39.67	43.68	PT1 <sup>(1)</sup> (WEST OF THE	0.3	0.15	50	0.32								14.62	1.56			
6	O-5	60.63	64.2	PT1 <sup>(1)</sup> (WEST OF THE	0.26	0.13	61	1.38								18.41	1.44			
7	O-7	5.28	3.67	FF(TOTAL FLOW	[0.6]			54								22.43	0			
8	D1	1.17	1.21	ST2-IN <sup>(2)</sup>	[0.28]			84								25.07	0.7			
9	A1	2.5	2.6	ST2-IN <sup>(2)</sup>	0.85	0.68	Horton	0.5								29.1	1.79			
10	ST-2	0.59	0.72	ST2-IN <sup>(2)</sup>	0.57	0.46	Horton	0.5								33.73	2.71			
11	O-8	60.55	48.69	ST2-IN <sup>(2)</sup>	[1]			69								45.54	3.58			
12	A7	3.51	3.51	PT2ST3(TOTAL FLOW	0.85	0.68	Horton	0.5								3.45	0.6			
13	ST-3	0.71	0.99	PT2ST3(TOTAL FLOW	0.57	0.46	Horton	0.5								13.45	0.5			
14	D2	2.28	2.35	PT3ST4 (TOTAL FLOW	[0.99]			84								14.45	0			
15	A17	12.04	11.99	PT3ST4 (TOTAL FLOW	0.85	0.68	Horton	0.5								15.55	0			
16	ST-4	0.35	0.44	PT3ST4 (TOTAL FLOW	0.57	0.46	Horton	0.5								16.55	0.5			
17	A18	5.3	5.36	PT3ST4 (TOTAL FLOW	0.85	0.68	Horton	0.5								26.55	0.6			
18	D3	2.51	2.36	STS-E <sup>(5)</sup>	[0.73]			86								30	1.7			
19	C1	3.41	3.42	STS-E <sup>(5)</sup>	0.85	0.68	Horton	0.5								[Width= 1800 mm]	[Height= 1200 mm]			
20	ST-5	0.45	0.59	STS-E <sup>(5)</sup>	0.57	0.46	Horton	0.5								2.6	0.95			
21	STRAND	7.59	5.69	SSAOUT <sup>(4)</sup>	0.85	0.64	Horton	0.5								12.6	0.75			
22	AREA-A	68.04	68.04	PT4ST5 <sup>(3)</sup> (TOTAL	0.8	0.64	Horton	0.5								14.1	0			
23	C6	1.87	1.98	PT5ST6(TOTAL FLOW	0.85	0.68	Horton	0.5								15.9	0			
24	C7	1.62	1.78	PT5ST6(TOTAL FLOW	0.85	0.68	Horton	0.5								17.4	0.75			
25	ST-6	0.41	0.42	PT5ST6(TOTAL FLOW	0.57	0.46	Horton	0.5								27.4	0.95			
26	D4	1.73	1.56	D4-EX	[0.60]			88								30	1.7			
27	AREA-B	24.04	23.08	D4-EX	0.77	0.62	Horton	1.4												
28	D5	1.9	1.93	PT6MC <sup>(6)</sup> (McKenna	[0.69]			86												
29	O-13SDF	9.74	8.8	PT6MC <sup>(6)</sup> (McKenna	[0.43]			81												
30	O-15	10.67	11.76	M-C	[0.30]			82												
31	O-14	30.02	5	OKEEFE	[0.133]			82												
Total		514.31	458.91																	

<sup>(1)</sup> PT1=[OKF-N+"O-3"+"O-5"+"O-6"]

<sup>(2)</sup> ST2-IN=[DRAIN1+"D1"+A1-STR+A1-OVF+ST2STR+ST2OVF+O8PIPE]

<sup>(3)</sup> PT4ST5=[SSAOUT<sup>(4)</sup>+SWMF-A"+SWMAOV]

<sup>(4)</sup> SSAOUT=[ST5-E<sup>(5)</sup>+S-POND"+S-OVF"]

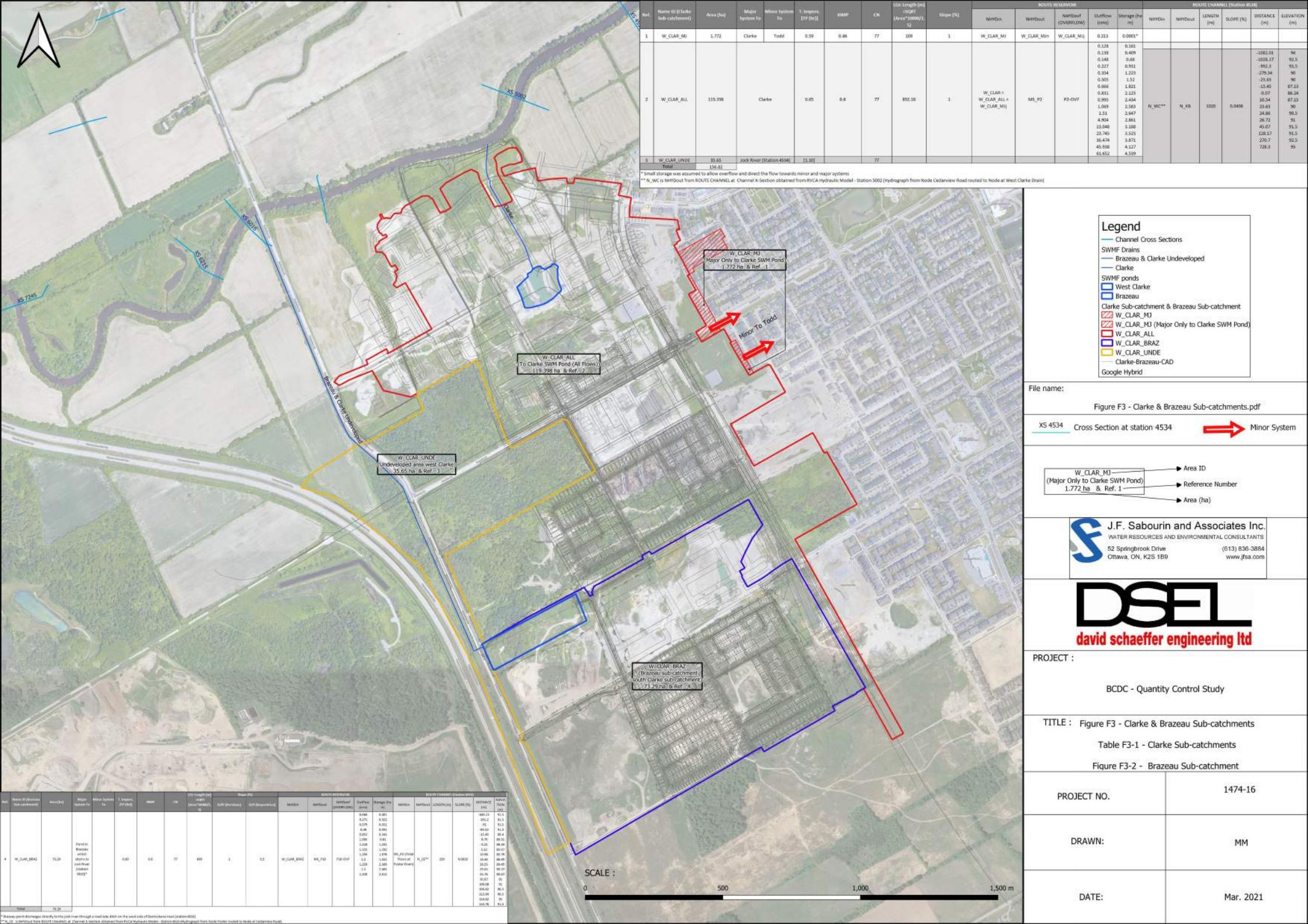
<sup>(5)</sup> ST5-E[DRAIN3"+D3"+C1-STR+C1-OVF+ST5STR+ST5OVF]

<sup>(6)</sup> PT6MC=[DRAINS5"+D5"+SDF]

Ref.	Name ID	Area (ha)	Major System ID	Minor System ID	T. Imperv.	KMP	CR	EGL Length (m)		Slope (%)		ROUTE RELIEF		ROUTE CHANNEL (Bottom Left)								
								<0.01 (Area < 0.0001 ha)	0.01-0.1 (Area 0.0001-0.01 ha)	SLOP (Horizontal)	SLOP (Vertical)	NWDir	NWDist	NWFlow (D/Overflow)	Surface (km)	Storage (ha m)	NWDir	NWDist	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)
3	FOSTER	325.44	FOSTER-CUT = ["P_FOSTER_OV"]	0.0001	0.33	0.55	78	3477.554011	0.5	0.5	0.5	FOSTER	P_FOS	EO-OVF	30.34	10	AS_EO (Total Flow at Foster Drain)	N_CSE	159	0.0018	-445.23	91.5
																				-391.2	91.5	
																				-41	91.5	
																				-48.53	91.5	
																				33.49	91.4	
																				-1.22	90.34	
																				1.22	90.34	
																				10.96	91.79	
																				10.44	90.49	
																				26.55	90.45	
																				29.03	90.27	
																				30.79	90.17	
																				56.47	91	
																				108.08	91	
																				109.82	90.5	
																				112.04	90.5	
																				114.42	91	
																				116.76	91.5	



Ref.	Name ID	Area (ha)	Major System To	Minor System To	T. Imperv.	XIMP	CN	LGI: Length (m) =SQRT (Area*10000/1.5)	Slope (%)		ROUTE RESERVOIR					ROUTE CHANNEL (Station 6016)					
									SLPP (Pervious)	SLPI (Impervious)	NHYDin	NHYDout	NHYDovf (OVERFLOW)	Outflow (cms)	Storage (ha-m)	NHYDin	NHYDout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)
1	FOSTER	325.44	FOSTER-OUT = ["P_FOS"+ "FO-OVF"]		0.55	0.55	74	1472.956211	0.5	0.5	FOSTER	P_FOS	FO-OVF	10.34	10	SN_FO (Total Flows at Foster Drain)	N_CE	159	0.0818	-645.23 -391.2 -91 -85.52 -15.46 -9.79 -3.22 3.22 10.96 16.44 26.55 29.03 35.76 36.67 108.08 109.82 112.04 114.62 116.76	91.5 91.5 91.5 91.5 89.4 89.31 86.24 85.07 85.79 86.49 89.45 90.27 90.67 91 91 90.5 90.5 91 91.5



Ref.	Name ID (Clarke Sub-catchment)	Area (ha)	Major System To	Minor System To	T. Imperv. [TP (hr)]	XIMP	CN	LGI: Length (m) =SQRT (Area*10000/1.5)	Slope (%)	ROUTE RESERVOIR					ROUTE CHANNEL (Station 4534)					
										NHYDin	NHYDout	NHYDovf (OVERFLOW)	Outflow (cms)	Storage (ha-m)	NHYDin	NHYDout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)
1	W_CLAR_MJ	1.772	Clarke	Todd	0.59	0.46	77	109	1	W_CLAR_MJ	W_CLAR_MJn	W_CLAR_MJj	0.213	0.0001*						
2	W_CLAR_ALL	119.398	Clarke	0.65	0.6	77	892.18	1	W_CLAR = W_CLAR_ALL + W_CLAR_MJj	MS_P2	P2-OVF	0.995 1.069 1.51 4.904 13.048 23.745 36.474 45.938 61.652	0.128 0.138 0.148 0.227 0.354 0.505 0.666 0.831 2.123	0.161 0.409 0.68 0.931 1.223 1.52 1.821 2.123 2.434	N_WC**	N_KB	1020	0.0498	-1082.01 -1028.17 -992.3 -279.34 -23.63 -13.45 -0.07 10.54 23.63 24.86 26.72 45.07 128.17 270.7 728.3	94 92.5 93.5 90 90 87.13 86.24 87.15 90 90.5 91 91.5 91.5 92.5 95
3	W_CLAR_UNDE	35.65	Jock River (Station	[1.10]		77														
	Total	156.82																		

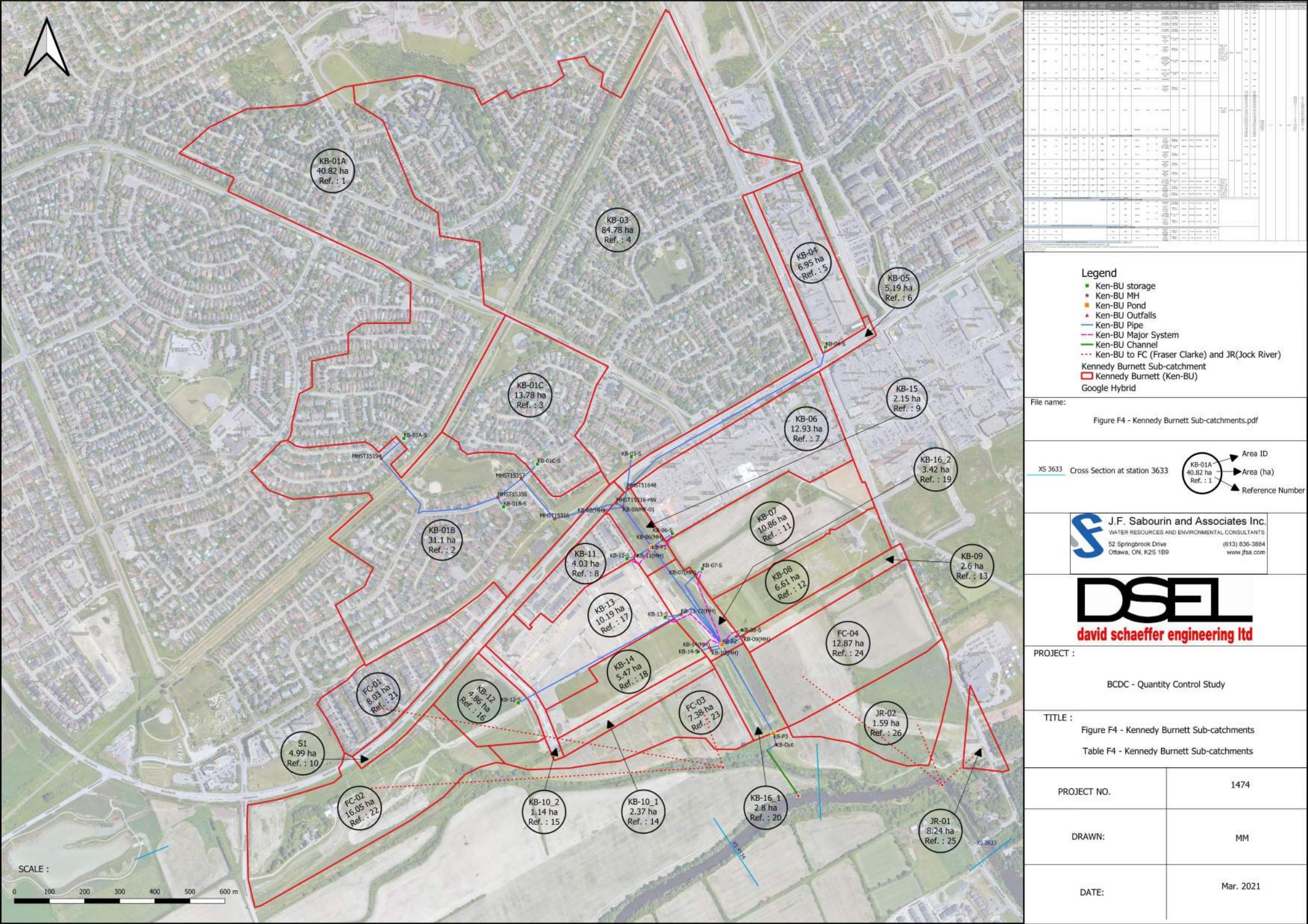
\* Small storage was assumed to allow overflow and direct the flow towards minor and major systems

\*\* N\_WC is NHYDout from ROUTE CHANNEL at Channel X-Section obtained from RVCA Hydraulic Model - Station 5002 (Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain)

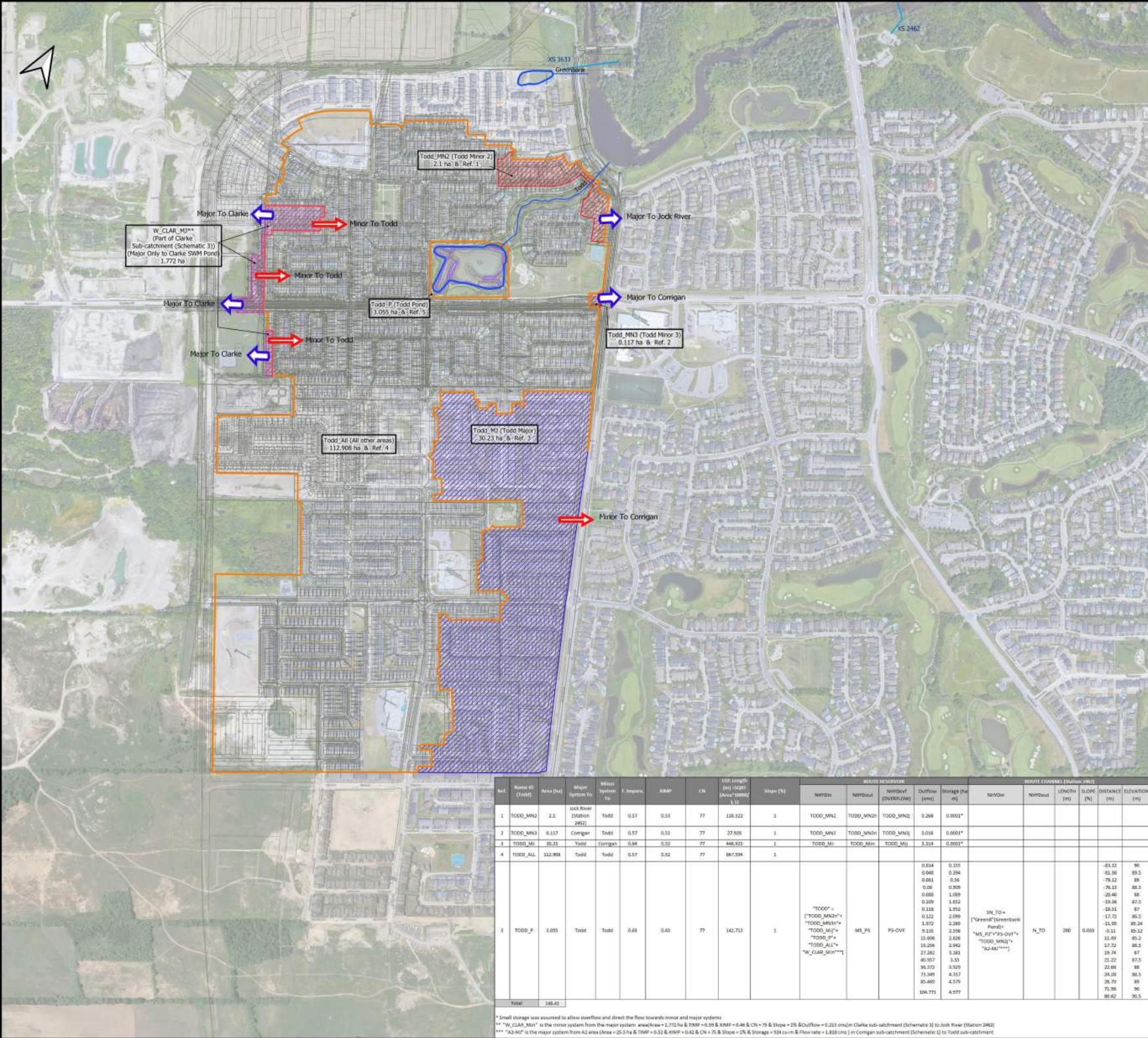
Ref.	ID (Brazeau Sub-catchment)	Area (ha)	Major System To	Minor System To	T. Imperv. [TP (hr)]	XIMP	CN	LGI: Length (m) =SQRT (Area*10000/1.5)	Slope (%)		ROUTE RESERVOIR					ROUTE CHANNEL (Station 6016)					
									SLPP (Pervious)	SLPI (Impervious)	NHYDin	NHYDout	NHYDovf (OVERFLOW)	Outflow (cms)	Storage (ha-m)	NHYDin	NHYDout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)
4	W_CLAR_BR AZ	73.29	Pond in Brazeau which drains to Jock River (station 6016)*		0.65	0.6	77	699	1	0.5	W_CLAR_BRAZ	MS_P10	P10-OVF	0.068 0.271 0.379 0.48 0.853 1.005 1.128 1.155 1.194 1.2 1.259 1.3 1.349	0.001 0.022 0.051 0.091 0.341 0.61 1.231 1.592 1.876 1.921 2.369 2.665 2.813	SN_FO (Total Flows at Foster Drain)	N_CE**	159	0.0818	-645.23 -391.2 -91 -85.52 -15.46 -9.79 -3.22 3.22 10.96 26.55 29.03 35.76 36.67 108.08 109.82 112.04 114.62 116.76	91.5 91.5 91.5 91.5 89.4 89.31 86.24 85.07 85.79 89.45 90.27 90.67 91 91 90.5 90.5 91 91.5
	Total	73.29																			

\* Brazeau pond discharges directly to the jock river through a road side ditch on the west side of Borrisokane road (station 6016)

\*\* N\_CE is NHYDout from ROUTE CHANNEL at Channel X-Section obtained from RVCA Hydraulic Model - Station 6016 (Hydrograph from Node Foster routed to Node at Cedarview Road)



Ref.	ID	KENNEDY-BURNETT	Area (ha)	Runoff Coef. <sup>(1)</sup>	Zero Imperv (%)	Slope <sup>(1)</sup> (%)	Equivalent Width <sup>(1)</sup> (m)	Flow Length <sup>(1)</sup> (m)	Percent Routed <sup>(1)</sup> (%) (Pervious)	TIMP <sup>(2)</sup>	XIMP <sup>(2)</sup>	LGI: Length (m) =SQRT (Area*10000/1.5)	SLPP (%)	SLPI <sup>(2)</sup> (%)	Minor System Criteria <sup>(1)</sup>	Major System Criteria <sup>(1)</sup>	Major and Minor System To	DUALHYD parameters				ROUTE RESERVOIR				ROUTE CHANNEL (Station 3633)					
																		Major System	Minor System	Max. Release Rate <sup>(2)</sup> (cms)	Storage <sup>(2)</sup> (m <sup>3</sup> )	NHYdin	NHYdout	NHYdovf (OVERFLOW)	Outflow (cms)	Storage (ha-m)	NHYdin	NHYdout	LENGTH (m)	SLOPE (%)	DISTANCE (m)
<b>Existing Subcatchments to KB-SWMF</b>																															
1	KB-01A	40.82	0.49	50%	0.97%	1879	220	76%	0.408	0.09792	521.664	0.5	0.5	10 L/s/inlet & 15 L/s/inlet ICDs to KB-SWMF	No MS flows to KB-SWMF	KB-01A-S	KB-01A-MJ	KB-01A-MN	3.6	4995	KB-P1 = ["KB-01A-S" + "KB-01B-S" + "KB-01C-S" + "KB-03-S" + "KB-04-S" + "KB-05" + "KB-06-S" + "KB-11-S" + "KB-15" + "S1"]	KB-P1R	KB-P1ovf	0.076	0.003	NHYdin	NHYdout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)
2	KB-01B	31.1	0.46	50%	0.42%	312	1000	50%	0.375	0.1875	455.339	0.42	0.42	10 L/s/inlet & 15 L/s/inlet ICDs to KB-SWMF	No MS flows to KB-SWMF	KB-01B-S	KB-01B-MJ	KB-01B-MN	1.585	6075											
3	KB-01C	13.78	0.49	50%	0.50%	403	335	50%	0.409	0.2045	303.095	2.0	0.5	10 L/s/inlet & 15 L/s/inlet ICDs to KB-SWMF	No MS flows to KB-SWMF	KB-01C-S	KB-01C-MJ	KB-01C-MN	1.35	1880											
4	KB-03	84.78	0.48	50%	0.63%	647	1300	50%	0.394	0.197	751.798	2.0	0.63	10 L/s/inlet & 15 L/s/inlet ICDs to KB-SWMF	No MS flows to KB-SWMF	KB-03-S	KB-03-MJ	KB-03-MN	5.27	15500											
5	KB-04	6.95	0.80	40%	0.50%	55	1265	100%	0.85	0.85	215.252	2.0	0.5	Controlled to 503 L/s (approx. 5-year inlet capture rate)	MS flows stored on-site	KB-04-S	KB-04-MJ	KB-04-MN	0.503	1972											
6	KB-05	5.19	0.65	0%	2.00%	51	1000	100%	0.93	0.93	186.011	2.0	0.50	10-year inlet capture rate for storm sewers	MS flows to KB-SWMF	KB-P1															
7	KB-06	12.93	0.81	40%	4.75%	217	600	100%	0.873	0.873	293.598	2.0	4.75	Controlled to Qcap (1350mm) 1,760 L/s (approx. 5-year inlet capture rate)	MS flows stored on-site	KB-06-S	KB-06-MJ	KB-06-MN	2.262	1950											
8	KB-11	4.03	0.67	50%	2.00%	116	350	100%	0.675	0.675	163.911	2.0	2.0	Controlled to 577 L/s (approx. 5-year inlet capture rate)	MS flows to KB-SWMF	KB-11-S	KB-11-MJ	KB-11-MN	0.577	597											
9	KB-15	2.15	0.90	90%	0.30%	476	45	100%	0.79	0.79	119.722	2.0	0.3	Uncontrolled	KB-P1																
10	S1	4.99	0.65	0	0.02	50	1000	1	0.93	0.93	182.3915203	2	2	10-year inlet capture rate for storm sewers	MS flows to KB-SWMF	KB-P1															
<b>Proposed Subcatchments to KB-SWMF</b>																															
11	KB-07	10.86	0.8	0.5	0.02	209	525	1	0.86	0.86	269.072	2.0	2.0	5-year inlet capture rate (3-hour Chicago)	MS flows to KB-SWMF	KB-07-S	KB-07-MJ	KB-07-MN	2.094	1378	KB-P3 = [KB-Pond2 <sup>(4)</sup> + KB-16_1]	KB-P3R	KB-P3ovf	0.051	0.002	N_TO	SN_KB (Total Flows before Station 3633)	650	0.0498	-29.24	91
12	KB-08	6.61	0.65	0.5	0.02	133	500	1	0.64	0.64	209.921	2.0	2.0	5-year inlet capture rate (3-hour Chicago)	MS flows to KB-SWMF	KB-08-S	KB-08-MJ	KB-08-MN	1.058	787											
13	KB-09	2.6	0.8	0	0.02	70	500	1	0.86	0.86	131.656	2.0	2.0	10-year inlet capture rate for storm sewers	MS flows to KB-SWMF	KB-P2															
14	KB-10_1	2.37	0.8	0	0.02	64	500	1	0.86	0.86	125.698	2.0	2.0	10-year inlet capture rate for storm sewers	MS flows to KB-SWMF	KB-P3															
15	KB-10_2	1.14	0.8	0	0.02	57	200	1	0.86	0.86	87.178	2.0	2.0	10-year inlet capture rate for storm sewers	MS flows to KB-SWMF	KB-P4															
16	KB-12	4.86	0.75	0.3	0.02	227	215	1	0.79	0.79	180.000	2.0	2.0	5-year inlet capture rate (3-hour Chicago)	MS flows to FC-Drain	KB-12-S	KB-12-MJ	KB-12-MN	0.8665	632											
17	KB-13	10.19	0.65	50%	2.00%	227	450	100%	0.64	0.64	260.640	2.0	2.0	5-year inlet capture rate (3-hour Chicago)	MS flows to KB-SWMF	KB-13-S	KB-13-MJ	KB-13-MN	1.722	1077											
18	KB-14	5.47	0.65	50%	2.00%	121	450	100%	0.64	0.64	190.962	2.0	2.0	5-year inlet capture rate (3-hour Chicago)	MS flows to KB-SWMF	KB-14-S	KB-14-MJ	KB-14-MN	0.8734	631											
Existing and Proposed Subcatchments Total Area to KB-SWMF (ha)										257.04																					
<b>EXISTING / PROPOSED SUBCATCHMENTS TO FRASER-CLARKE DRAIN</b>																															
21	FC-01	8.03	0.53						0.47	0.47	231.373	2.0	1.0	Controlled to 756 L/s	No MS flows to KB-SWMF	FC-01-S	FC-01-MJ	FC-01-MN	0.756	714											



**Legend**

- Channel Cross Sections
- SWMF Drains
- SWMF ponds
- Sub-catchments
- Todd
- Todd Minor
- Todd Major
- W\_CLAR\_Major
- Todd-Greenbank-CAD
- Google Hybrid

File name:

Figure F5 -Todd Sub-catchments.pdf

Major System

Minor System

XS 2462 Cross Section at station 2462

Area ID  
Todd\_P (Todd Pond)  
Reference Number  
Area (ha)

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**DSEL**  
**david schaeffer engineering ltd**

SCALE :

0 250 500 m

PROJECT :

BCDC - Quantity Control Study

TITLE :

Figure F5 -Todd Sub-catchments

Table F5 -Todd Sub-catchments

PROJECT NO.

1474-16

DRAWN:

MM

DATE:

Mar. 2021

Ref	Name ID (TSM)	Area (ha)	Major System To	Minor System To	T. Ingress	XMAP	CN	MFL Length (m) - Right Area*10000	Slope (%)	ROUTE RESERVOIR			ROUTE CHANNEL Station 2462							
										NHDin	NHDout	NHDout (OVERFLOW)	Outflow (cm)	Storage (m)	NHDin	NHDout	Length (%)	Slope (%)	Distance (m)	Elevation (m)
1	TODD_MN2	2.1	Jock River (Station 2462)	Todd	0.57	0.59	77	118.322	1	TODD_MN2	TODD_MN2	TODD_MN2	0.268	0.0001*						
2	TODD_MN3	0.117	Corriah	Todd	0.57	0.53	77	27.928	1	TODD_MN1	TODD_MN3	TODD_MN1	0.03	0.0001*						
3	TODD_MJ	30.23	Todd	Corriah	0.64	0.52	77	446.925	1	TODD_MJ	TODD_MJ	TODD_MJ	3.354	0.0001*						
4	TODD_ALL	112.908	Todd	Todd	0.57	0.52	77	887.594	1											
5	TODD_P	3.055	Total	Todd	0.63	0.63	77	142.712	1											
<b>Total:</b>		<b>148.41</b>																		

\* Small storage was assumed to allow overflow and direct the flow towards minor and major systems

\*\* W\_CLAR\_MN2 is the minor system from the major system. area(Area = 1.72 ha & CN = 7.8 Slope = 1% Aduflow = 0.213 cm/s) Clarke sub-catchment (Schematic 3) to Jock River (Station 2462)

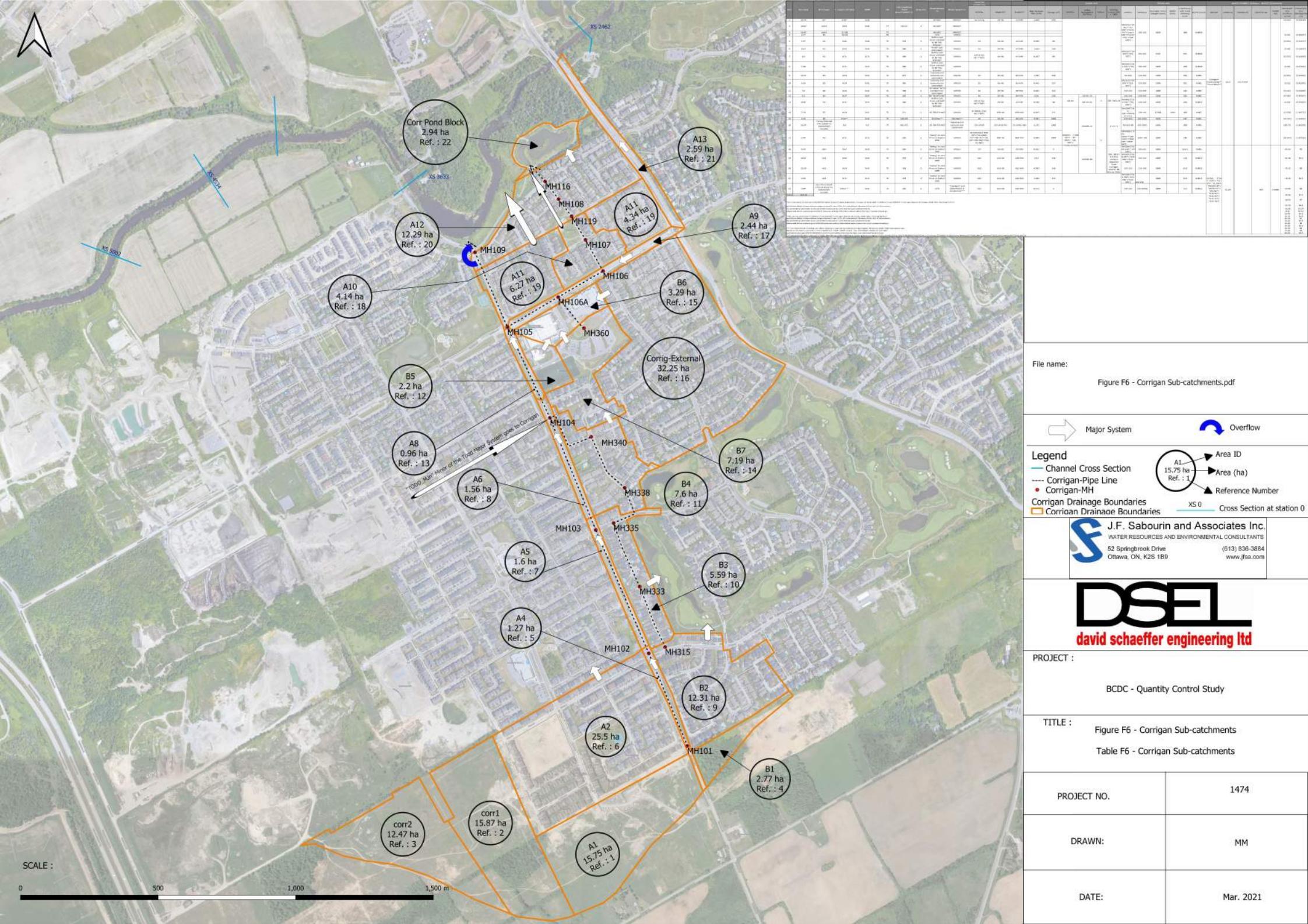
\*\*\* A2\_MJ2 is the major system from A2 area (Area = 25.6 ha & CN = 0.52 & XMAP = 0.4 & CN = 7.5 Slope = 1% Povrate = 1.0E+00) to Corriah sub-catchment (Schematic 3) to Todd sub-catchment

Ref.	Name ID (Todd)	Area (ha)	Major System To	Minor System To	T. Imperv.	XIMP	CN	LGI: Length (m) =SQRT (Area*10000/1.5)	Slope (%)	ROUTE RESERVOIR					ROUTE CHANNEL (Station 2462)					
										NHYDin	NHYDout	NHYDovf (OVERFLOW)	Outflow (cms)	Storage (ha-m)	NHYDin	NHYDout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)
1	TODD_MN2	2.1	Jock River (Station 2462)	Todd	0.57	0.53	77	118.322	1	TODD_MN2	TODD_MN2n	TODD_MN2j	0.268	0.0001*						
2	TODD_MN3	0.117	Corrigan	Todd	0.57	0.53	77	27.928	1	TODD_MN3	TODD_MN3n	TODD_MN3j	0.016	0.0001*						
3	TODD_MJ	30.23	Todd	Corrigan	0.64	0.52	77	448.925	1	TODD_MJ	TODD_MJn	TODD_MJj	3.314	0.0001*						
4	TODD_ALL	112.908	Todd	Todd	0.57	0.52	77	867.594	1											
5	TODD_P	3.055	Todd	Todd	0.63	0.63	77	142.712	1	"TODD" = ["TODD_MN2n"+ "TODD_MN3n"+ "TODD_MJj"+ "TODD_P"+ "TODD_ALL"+ "W_CLAR_MJn"]**]	MS_P3	P3-OVF	0.014 0.048 0.061 0.08 0.088 0.109 0.118 0.122 1.972 9.135 15.608 19.256 27.282 40.957 56.372 73.349 85.469 104.771	0.155 0.394 0.56 0.909 1.089 1.652 1.952 2.099 2.269 2.598 2.826 2.942 3.181 3.55 3.929 4.317 4.579 4.977	SN_TO = ["GreenB" (Greenbank Pond)+ "MS_P3"+P3-OVF"+ "TODD_MN2j"+ "A2-MJ"***]	N_TO	280	0.033	-83.32 -81.36 -79.12 -76.13 -20.46 -19.36 -18.51 -17.72 -11.95 -0.11 11.49 17.72 19.74 21.22 22.68 24.28 26.79 71.98 80.62	90 89.5 89 88.5 88 87.5 87 86.5 85.24 85.12 85.2 86.5 87 87.5 88 88.5 89 90 90.5
Total		148.41																		

\* Small storage was assumed to allow overflow and direct the flow towards minor and major systems

\*\* "W\_CLAR\_MJn" is the minor system from the major system area(Area = 1.772 ha & TIMP = 0.59 & XIMP = 0.46 & CN = 75 & Slope = 1% & Outflow = 0.213 cms)in Clarke sub-catchment (Schematic 3) to Jock River (Station 2462)

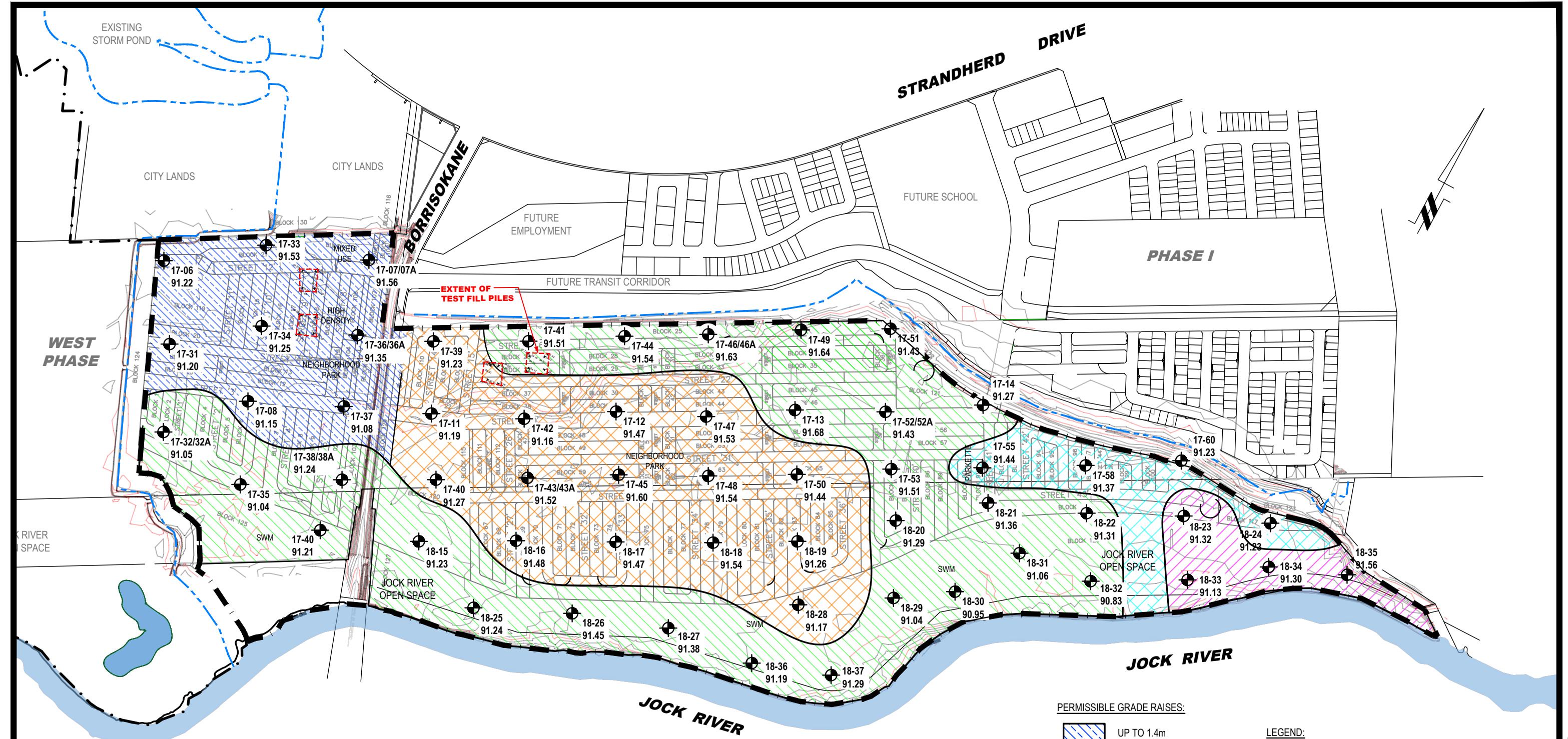
\*\*\* "A2-MJ" is the major system from A2 area (Area = 25.5 ha & TIMP = 0.52 & XIMP = 0.42 & CN = 75 & Slope = 1% & Storage = 924 cu-m & Flow rate = 1.818 cms ) in Corrigan sub-catchment (Schematic 1) to Todd sub-catchment



Ref.	Area (ha)	ID Corrigan	T. Imperv. [TP (hr)]	XIMP	CN	LGI: Length (m) =SQRT (Area*10000 /1.5)	Slope (%)	Major System To	Minor System To	DUALHYD parameters					DIVERT HYD				ROUTE PIPE					ROUTE CHANNEL (Station)					ROUTE RESERVOIR																				
										NHYDin	MajNHYD	MinNHYD	Max. Release Rate Rate (cms)	Storage (m <sup>3</sup> )	NHYDin	outflow hydrographs (NHYDs)	NIDout	QTOTAL (cms)= QIDi + QIDii	NHYDin	NHYDout	Diameter (mm) [Height (mm)]	Width (mm)	LENGTH (m) with 0.013 Manning Coef.	SLOPE (m/m)	NHYDin	NHYDout	[NHYDovf]	LENGTH (m)	SLOPE (%)	DISTANCE (m) [Outflow (cms)]	ELEVATION (m) [Storage (ha- m)]																		
1	15.75	A1*	0.52*	0.42				MH101*	MH101*	A1-Corrigan	A1-MJ	A1-MN	1.818	924	MH101= ["A1-MJ" +"A1-MN" +"corr1-MJ" +"corr1-MN" +"corr2-MJ" +"B1" +"A4-MN"]					101-102	1050	368	0.0054	Corrigan= ["116-corrig" + "Pond-Block"]	Co-P	Co-P-OVF	[0.15]	[0.04118]	[0.03]	[0.08297]																			
2	15.87	corr1	0.63	0.63	77	325.27	1	MH101*	MH101*																																								
3	12.47	corr2	[1.10]		77			MH101*	MH101*																																								
4	2.77	B1	[0.23]		56			N/A	MH101																																								
5	1.27	A4	0.65	0.65	75	253	1	Half to Jock River and Half to B6 "B6-B7ExMJ"	MH101	A4	A4-MJ	A4-MN	0.405	68																																			
6	25.5	A2	0.52	0.42	75	566	1	"Todd" sub-catchment	MH102	A2	A2-MJ	A2-MN	1.818	924																																			
7	1.6	A5	0.71	0.71	75	300	1	Half to Jock River and Half to B6 "B6-B7ExMJ"	MH103	A5T=[A4-MJ]+[A5]	A5-MJ	A5-MN	0.357	60																																			
8	1.56	A6	0.71	0.71	75	280	1	Half to Jock River and Half to B6 "B6-B7ExMJ"	MH104																																								
9	12.31	B2	0.54	0.41	75	417	1	"JOCKVA-TO" Jockvale sub-catchment	MH315	B2	B2-MJ	B2-MN	1.029	508																																			
10	5.59	B3	0.54	0.41	75	345	1	"JOCKVA-TO" Jockvale sub-catchment	MH333	B3	B3-MJ	B3-MN	0.459	227																																			
11	7.6	B4	0.54	0.41	75	388	1	"B7-B4MJ" B7 in Corrigan sub-catchment	MH340	B4	B5-MJ	B4-MN	0.655	323																																			
12	2.2	B5	0.57	0.57	75	187	1	B6 "B6-B7ExMJ"	MH105	B5	B5-MJ	B4-MN	0.26	250	A8-MJ	A8-MJ-JR	2	100 = 50 + 50																															
13	0.96	A8	0.71	0.71	75	186	1	Half to Jock River and Half to B6 "B6-B7ExMJ"	MH105	A8T=[A6-MJ]+[A8]	A8-MJ	A8-MN	0.238	40																																			
14	7.19	B7	0.54	0.41	75	211	1	B6 "B6-B7ExMJ"	MH360	B7-B4MJ=[B4-MJ]+[B7]	B7R-MJ	B7R-MN	0.629	311																																			
15	3.29	B6	0.54**	0.41	75	148.099	1	MH106A**	MH106A**	B6	B6-MJ	B6-MN	0.064	5484																																			
16	32.54	Corrig-External ("EX-LAND" in SWMHYMO model)	0.5	0.5	74	465.475	1	B6 "B6-B7ExMJ"	JOCKVA-TO	EX-LAND	EX-LAND-M	X-LAND-M	2.275	1365																																			
17	2.44	A9	0.71	0.71	75	262	1	"corrug" to Jock River at Station 2462	MH106	B6-B7ExMJ=[B7R-MJ]+[EX-LAND-M]+[B5-MJ]+[B6-MJ]+[B6-MN]+[A8-MJ-B6]	B6R-MJ	B6R-MN	0.064	5484	MH105= ["104-105" + "B5-MN" + "A8-MN" + "TODD_MN3J"]	MH105-JR	2	3 = 0 + 3																															
18	4.14	A10	0.47	0.35	75	183	1	"corrug" to Jock River at Station 2463	MH107	A9	A9-MJ	A9-MN	0.547	0																																			
19	10.61	A11	0.62	0.53	75	379	1	"corrug" to Jock River at Station 2464	MH107	A10	A10-MJ	A10-MN	0.31	228																																			
20	12.29	A12	0.54	0.41	75	183	1	"corrug" to Jock River at Station 2465	MH108	A11	A11-MJ	A11-MN	0.993	556																																			
21	2.59	A13	0.71	0.71	75	379	1	"corrug" to Jock River at Station 2466	MH108	A12	A12-MJ	A12-MN	1.02																																				

## **APPENDIX E**

## **GEOTECHNICAL**



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CAIVAN COMMUNITIES  
GEOTECHNICAL INVESTIGATION  
PROP. RESIDENTIAL DEVELOPMENT - CONSERVANCY LANDS EAST  
OTTAWA, ONTARIO  
Title: **PERMISSIBLE GRADE RAISE PLAN**

Scale: 1:6000	Date: 09/2019
Drawn by: MPG	Report No.: PG5036-1
Checked by: OC	
Approved by: DJG	
Revision No.: 2	

**PG5036-2**

re: **Road Grade Exceedance Review**

Proposed Residential Development - Conservancy Lands  
Borrisokane Road - Ottawa

to: Caivan Communities - **Mr. Hugo Lalonde** - [hugo.lalonde@caivan.com](mailto:hugo.lalonde@caivan.com)

David Schaeffer Engineering Ltd. - **Mr. Kevin Murphy** - [KMurphy@dsel.ca](mailto:KMurphy@dsel.ca)

date: March 8, 2021

file: PG5036-MEMO.10

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Paterson Group (Paterson) prepared the following memo to provide a geotechnical review of permissible grade raise exceedances of the proposed roadway grading at various locations throughout the aforementioned development. This memorandum should be read in conjunction with Paterson Group Report PG5036-1 Revision 1 dated February 3, 2021.

The following drawings prepared by David Schaeffer Engineering Ltd. were reviewed from a geotechnical perspective:

- Barrhaven Conservancy - Maximum Grade Raise Exceedance - Project No. 16-891
  - Drawing No. 6 and 7 - dated March 2021
- Latest road grading AutoCAD file - 891\_Grad\_PS\_Lowered\_Mar5-21

Based on the available drawings, it is understood that minor permissible grade raise exceedances occur within the proposed roadway grades at various locations throughout the subject development.

### Geotechnical Review

Based on our detailed review, the grading exceedances are considered acceptable from a geotechnical perspective and lightweight fill will not be required within the City of Ottawa right-of-way(s).

We trust that this information satisfies your immediate requirements.

**Paterson Group Inc.**



Owen Canton, E.I.T.

**Paterson Group Inc.**

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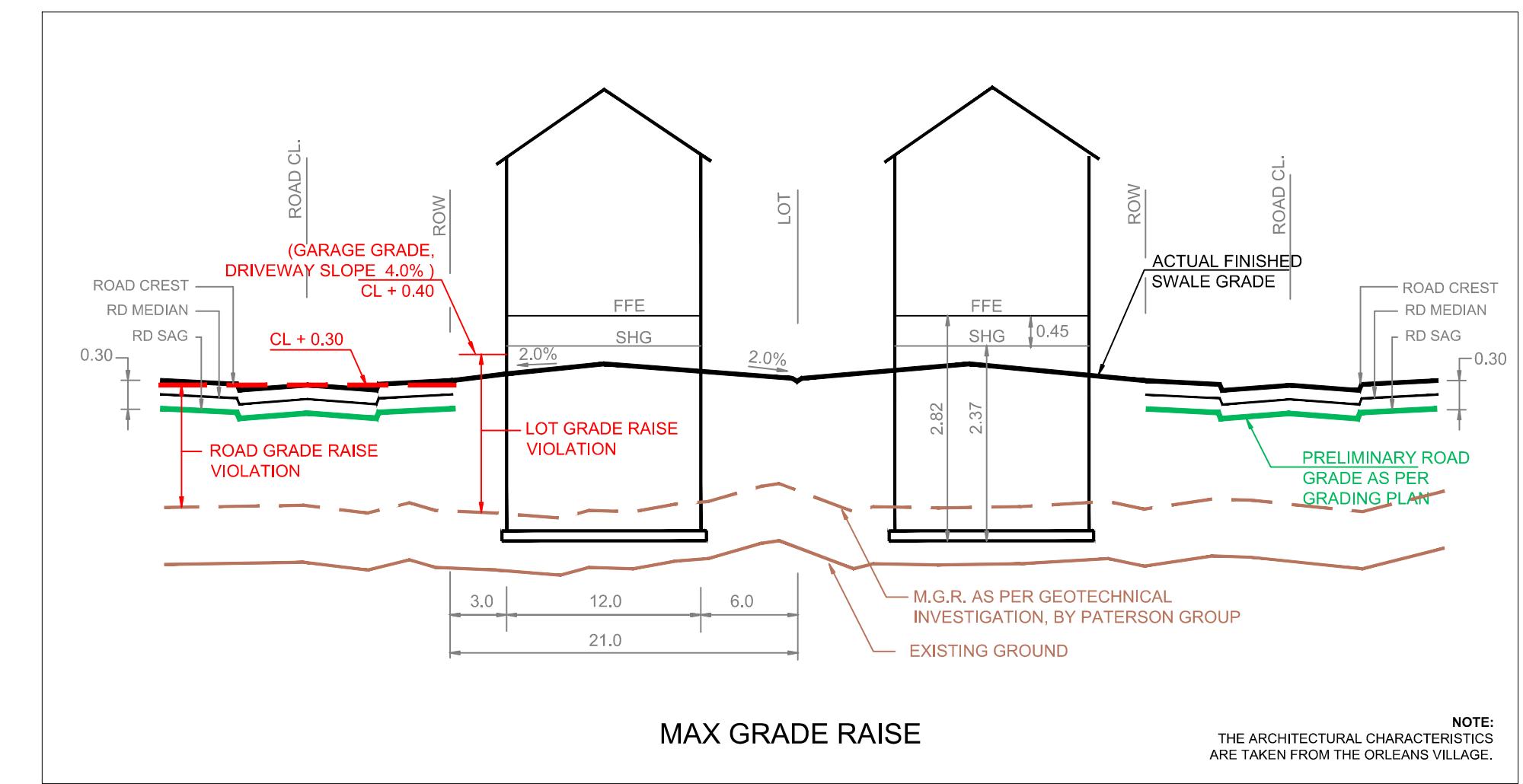
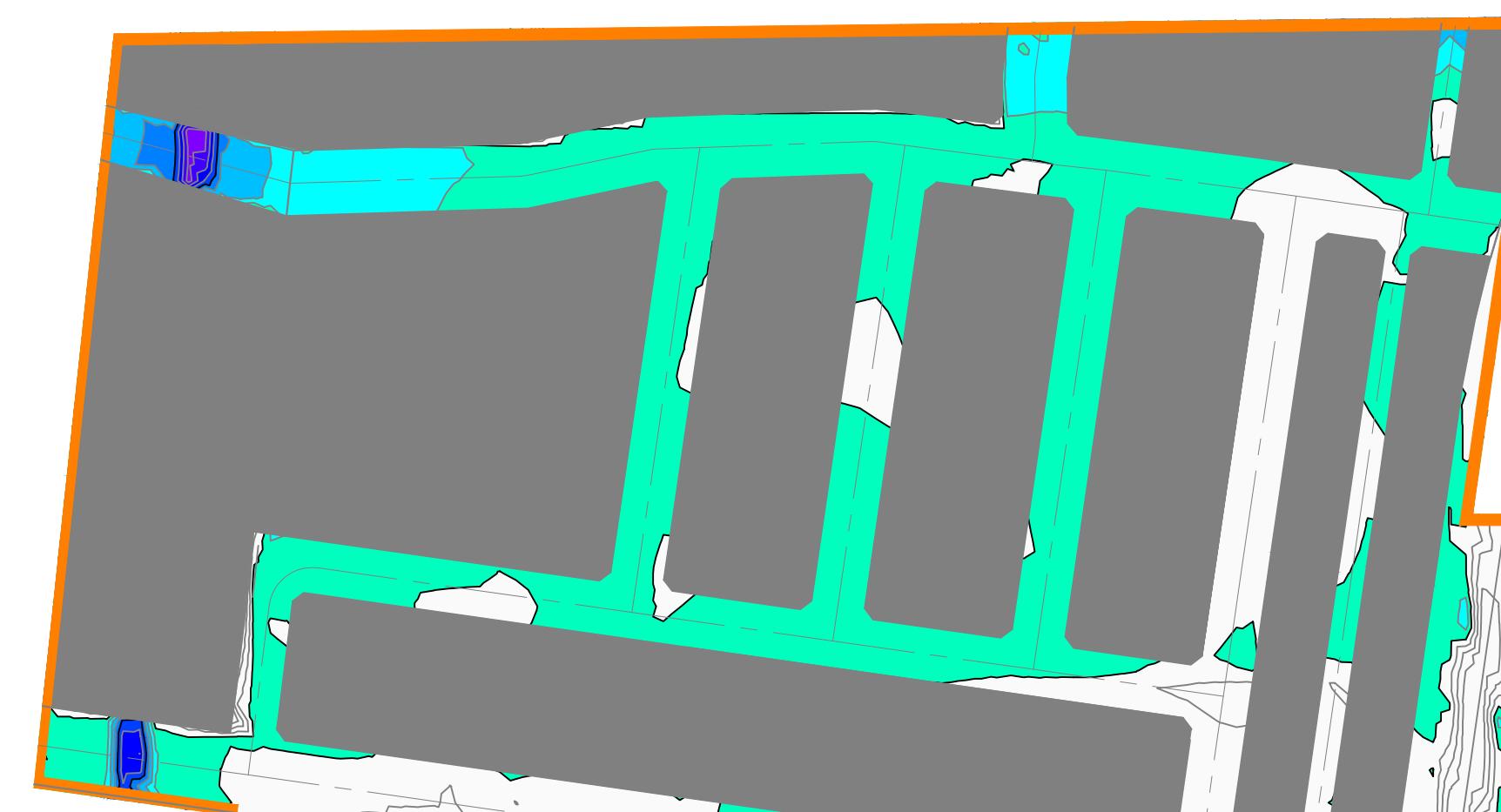


David J. Gilbert, P.Eng.

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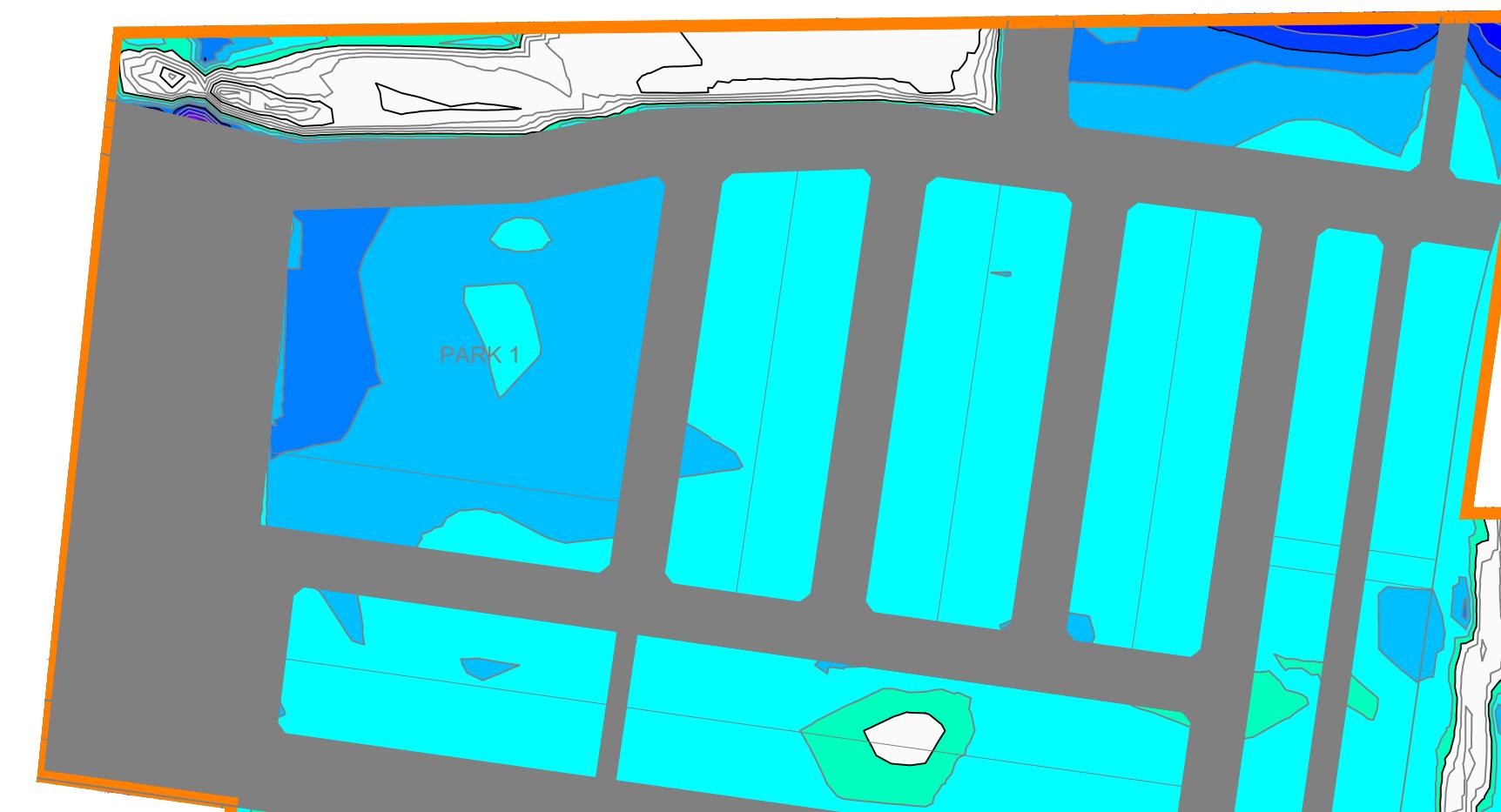
**St. Lawrence Office**  
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Kingston - Ontario - K7L 1H3  
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## MAXIMUM GRADE RAISE EXEEDANCE - ROADS



Elevations Table - ROADS		
Minimum Elevation	Maximum Elevation	Color
-2.29	0.00	
0.00	0.25	Green
0.25	0.50	Cyan
0.50	0.75	Blue
0.75	1.00	Dark Blue
1.00	1.25	Medium Blue
1.25	1.50	Dark Purple
1.50	1.75	Medium Purple
1.75	1.92	Purple

## MAXIMUM GRADE RAISE EXEEDANCE - LOTS

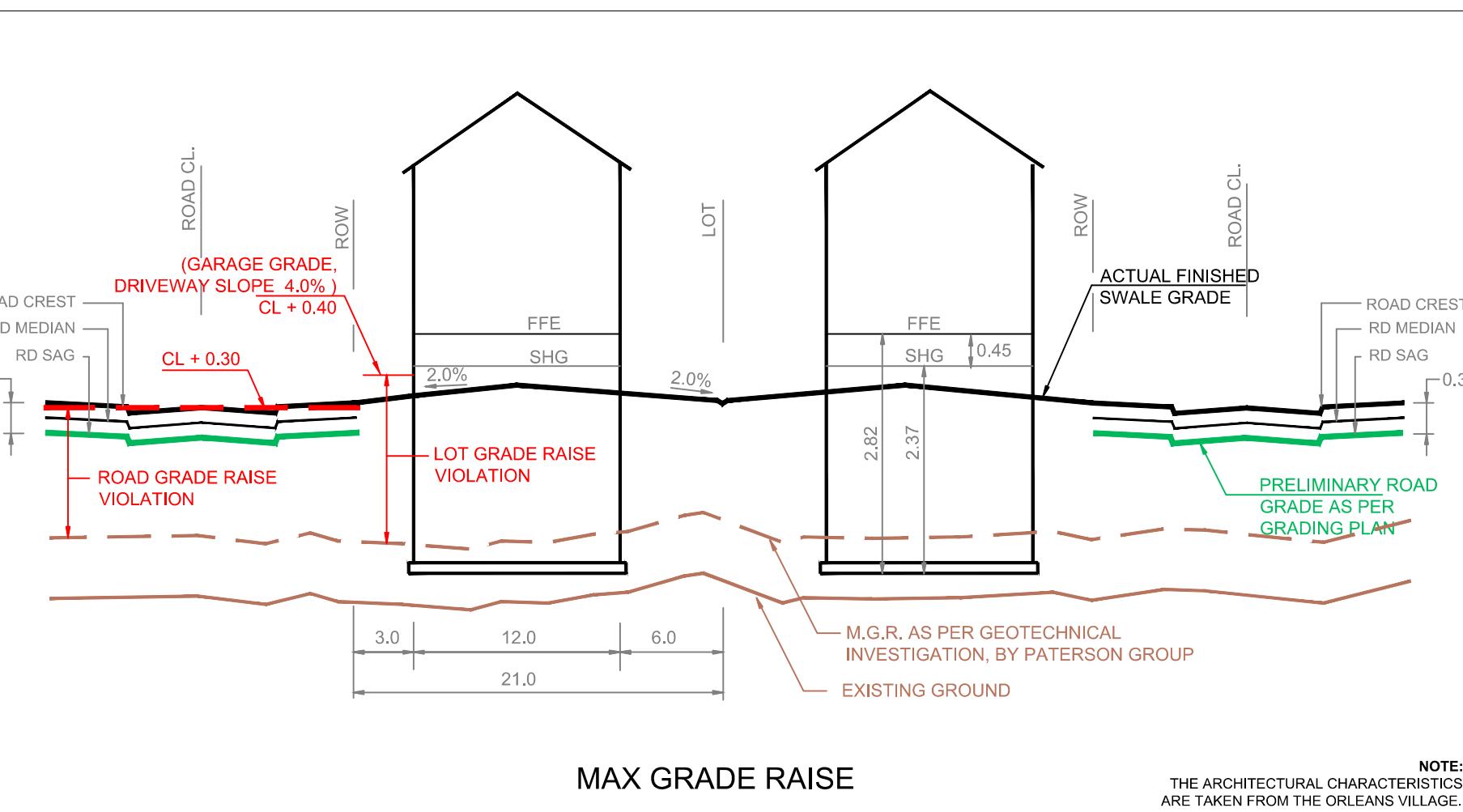


Elevations Table - LOTS		
Minimum Elevation	Maximum Elevation	Color
-2.32	0.00	
0.00	0.25	Green
0.25	0.50	Cyan
0.50	0.75	Blue
0.75	1.00	Dark Blue
1.00	1.25	Medium Blue
1.25	1.50	Dark Purple
1.50	1.75	Medium Purple
1.75	2.00	Purple
2.00	2.32	Dark Magenta

CONCEPTUAL GRADING PLAN: CONCEPTUAL GRADING PLAN DATED MARCH 2021

ORIGINAL GROUND: SURVEY DATED NOVEMBER 2019

MAXIMUM GRADE RAISE AS PER : GEOTECHNICAL INVESTIGATION,  
BY PATERSON GROUP  
DATED SEPTEMBER 27, 2019 -  
REVISED MAY 15, 2020



**NOTES:**

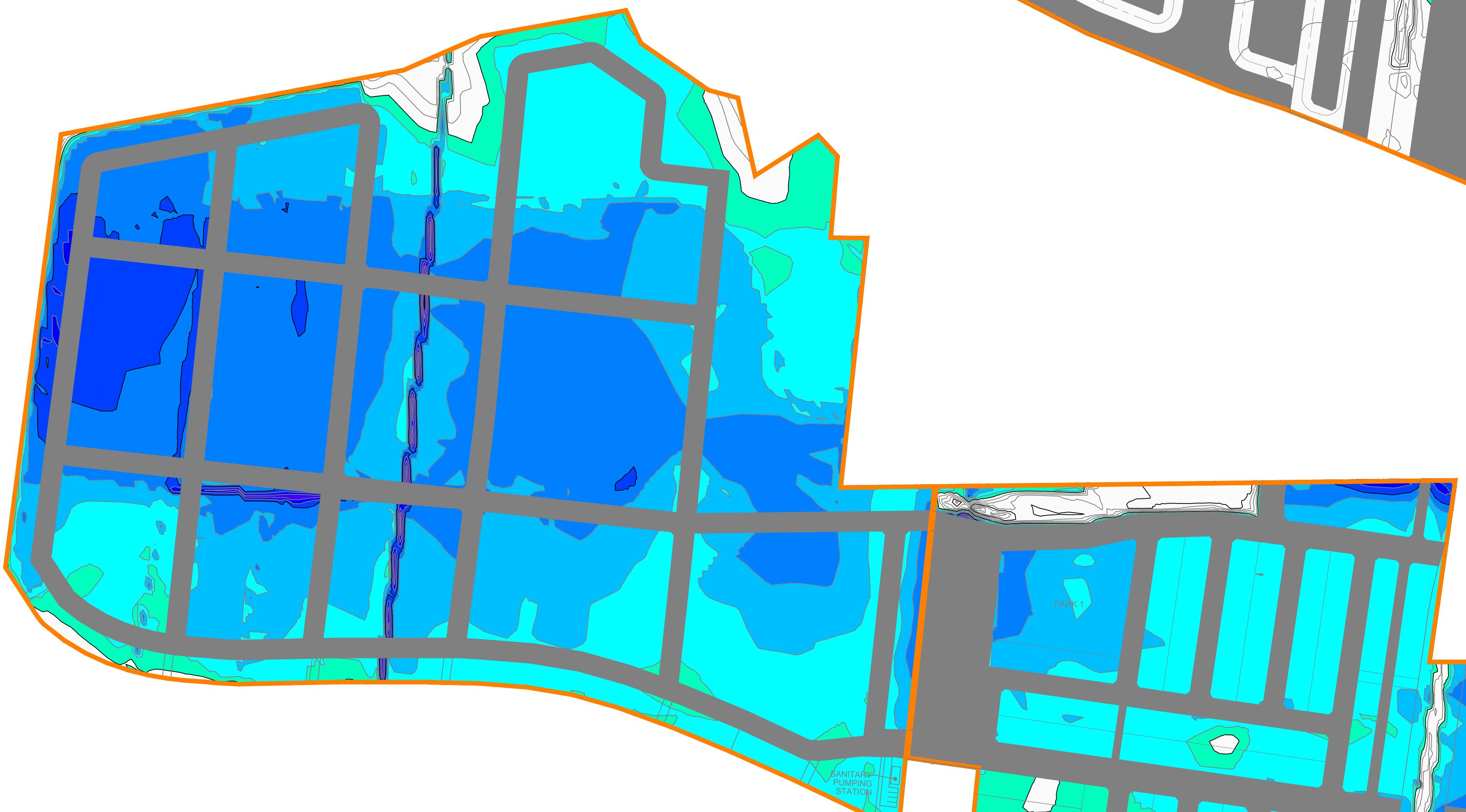
1. LOW FLOW CHANNEL ELEVATION TO BE VERIFIED IN THE FIELD AT ALL ROAD AND SEWER CROSSING LOCATIONS.
2. DETAILED DESIGN ROAD GRADES REPRESENT LOW POINTS. ACTUAL DESIGN GRADES WILL RISE AND FALL BY APPROXIMATELY 0.3m ABOVE THE TROUGH/SAG GRADES PRESENTED ON THIS PLAN.
3. EARTHWORKS VOLUMES ARE BASED ON THE MEDIAN ROAD GRADES, WHICH ARE ESTIMATED TO BE 0.09m HIGHER THAN THE TROUGH/SAG GRADES PRESENTED ON THIS PLAN.

EARTHWORKS DEPTHS AND VOLUMES ARE APPROXIMATE BASED ON USING ASSUMED MEDIAN VALUES FOR THE MANY VARIABLES THAT AFFECT EARTHWORKS. WHILE THE MAX DEPTH AND VOLUME ARE GENERALLY REFLECTIVE OF THE SITE CONDITIONS, THE ACTUAL DEPTH AND VOLUME AT ANY PARTICULAR LOCATION WILL VARY (UP OR DOWN) BASED ON THE LOCATION OF HIGH POINTS AND LOW POINTS IN THE ROAD AND ON THE LOTS.

THE SITE GRADING PLAN HAS BEEN PREPARED IN GENERAL CONFORMANCE WITH CITY OF OTTAWA DESIGN CRITERIA AND HISTORIC PRACTICES. THE GRADING PLAN HAS NOT BEEN REVIEWED BY CITY OF OTTAWA AND IS SUBJECT TO CHANGE FOLLOWING CITY REVIEW. ANY CHANGE IN THE GRADING PLAN WILL HAVE A CORRESPONDING CHANGE IN EARTHWORKS.

MAXIMUM GRADE RAISE EXCEEDANCE - ROADS

Elevations Table - ROADS		
Minimum Elevation	Maximum Elevation	Color
-2.29	0.00	
0.00	0.25	■
0.25	0.50	■
0.50	0.75	■
0.75	1.00	■
1.00	1.25	■
1.25	1.50	■
1.50	1.75	■
1.75	1.92	■



MAXIMUM GRADE RAISE EXCEEDANCE - LOTS

Elevations Table - LOTS		
Minimum Elevation	Maximum Elevation	Color
-1.89	0.00	
0.00	0.25	■
0.25	0.50	■
0.50	0.75	■
0.75	1.00	■
1.00	1.25	■
1.25	1.50	■
1.50	1.75	■
1.75	2.00	■
2.00	2.32	■

CONCEPTUAL GRADING PLAN: CONCEPTUAL GRADING PLAN DATED MARCH 2021

ORIGINAL GROUND: SURVEY DATED NOVEMBER 2019

MAXIMUM GRADE RAISE AS PER : GEOTECHNICAL INVESTIGATION, BY PATERSON GROUP  
DATED SEPTEMBER 27, 2019 - REVISED MAY 15, 2020

