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Project Number: 959(03)

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**Attention:** **Laura Maxwell, B.Sc., M.PI.**

**Subject:** **Cardinal Creek Village South –  
Preliminary Stormwater Management Plan and Stormwater  
Management Facility Design**

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## Introduction

As requested by your office, J.F. Sabourin and Associates (JFSA) has evaluated, based on the provided information as described below; (i) the adequacy of the proposed minor system with respect to hydraulic gradeline (HGL) analysis; and (ii) the storage required in the SWM facilities to meet quality and quantity control requirements for the proposed development at Cardinal Creek Village South.

The proposed Cardinal Creek Village South site has a development area of approximately 46.30 ha. 6.29 ha of the proposed development is tributary to Pond 1 and the stormwater management system for Cardinal Creek Phase 4. 38.08 ha of the site will discharge to Pond 2 which will provide quality control, erosion control and quantity control up to the 100-year level, before discharging to the south tributary of Cardinal Creek. 1.93 ha consisting primarily of rear yards will drain uncontrolled to the south tributary of Cardinal Creek. Refer to Figure 12 for the proposed drainage areas for the subject site.

## Stormwater Management Facility (Pond 2)

As noted above, SWM facility 2 will provide quality control for 38.08 ha of the site. Pond 2 also requires erosion control, provided based on the detention of the 25 mm storm runoff for a drawdown time of approximately 96 hours. The effectiveness of this erosion control was confirmed by a continuous erosion analysis, as documented in the June 2013 Cardinal Creek Village / Continuous Erosion Analysis memo.

Pond 2, discharging to the south tributary of Cardinal Creek, also requires 2- to 100-year post-to pre-development quantity control. Target release rates for Pond 2 were calculated based on existing flows simulated with AECOM's 2013 Cardinal Creek XPSWMM model for the 24-hour SCS Type II design storms, pro-rated by existing drainage area from the subject site to the south tributary. This source is appropriate as it supersedes the AECOM August 2009 "Greater Cardinal Creek Subwatershed Study - Existing Conditions" study.

The proposed drainage area to Pond 2 was simulated using SWMHYMO modelling software to assess its performance and ensure the design requirements were met. The SWMHYMO model and associated files are included in Attachment A.

A summary of the proposed SWM facility operating conditions are presented in Tables A-1 to A-5 of Attachment A, including a comparison of the existing and proposed conditions flows from the subject site to Cardinal Creek. All quantity control requirements were met by the proposed outlet controls, while still providing a 0.3 m freeboard between the maximum water level in the pond and the top of bank elevation, and a maximum 100-year active storage depth of 2.0 m.

Pond 2 is equipped with one sediment forebay connected to the main cell of the pond by a standard forebay berm. Refer to Attachment B for preliminary calculations for the required sediment forebay dimensions for this SWM facility. Pond 2 will also be equipped with a bottom-draw outlet pipe to reduce the temperatures of the outflow to Cardinal Creek.

### HGL Analysis

Preliminary hydraulic grade line calculations for the proposed Cardinal Creek development were completed using PCSWMM modelling software. Pipe data, storm sewer layout and Rational Method flows in the storm sewer are as provided by DSEL. The Rational Method flows were calculated based on the 2-, 5- or 10-year level of service requirements, and the 100-year flows in the hydraulic grade line calculations were estimated as 14% greater than the Rational Method flows, to account for the additional flows captured by catchbasin grates, lead pipes and/or inlet control devices under the higher surface water depths of the 100-year storm. The proposed storm sewer infrastructure data was extracted from DSEL's detailed drawings and incorporated into a PCSWMM model, and flows derived by DSEL's rational method calculations were then applied to each Maintenance Hole (MH) in the model as steady flows (using the baseflow option). Exit losses were applied to all storm sewer pipes in the system based on the angle of the downstream connection.

The maximum HGL obtained at each MH has been extracted and provided in Table C1 in Attachment C. In absence of USF elevations for the site, the maximum HGL was compared to elevations 1.90 m below the road elevation as an assumed USF elevation. This will be updated once the USF elevations are obtained at detailed design.

An average freeboard of 2.64 m from the top of MH was observed throughout the proposed development for the 100-year return period. With a minimum freeboard of 2.1m at MH\_63. As such it can be concluded that the proposed storm sewer infrastructure is sufficiently sized, to safely convey minor system flows from the development under various extreme conditions. The PCSWMM model and associated modelling files are included in Attachment C.

### Drainage Area to Cardinal Creek Village Phase 4

As noted above, a 6.29 ha area from the southern portion of Cardinal Creek Village is tributary to the north and is to be captured by the Phase 4 storm sewer and network and eventually drains to Pond 1. This area has an imperviousness of 75% according to Figure 12. As per the JFSA January 2020 SWM report for these lands, it was previously assumed that 11.84 ha at 33% imperviousness would drain to this location. While the previously assumed imperviousness is lower than the proposed imperviousness, the drainage area is substantially reduced and as such the previously assumed Area x Runoff Coefficient value (5.07) is higher than the proposed Area x Runoff Coefficient value (4.72), thus the receiving storm sewer and Pond 1 are adequately sized to handle the drainage from the area in question and no additional controls are required for these lands.

## Uncontrolled Drainage Area to Cardinal Creek South Tributary

As noted above, a 1.93 ha area of rear yards from Cardinal Creek Village South will drain uncontrolled to the southern tributary of Cardinal Creek. This area is to provide the southern tributary with clean runoff to mimic pre-development conditions. A full analysis of the peak flows to the tributary will be assessed at detailed design.

### Cox County Road Culvert

A 74.30 ha area has been identified as the drainage area to a 900 m concrete culvert underneath Cox Country Rd. A SWMHYMO model of the drainage area was built to simulate peak flows at the culvert in question to assess if the existing culvert's size is sufficient. A peak flow of 1.324 cms was established by the model for the 25-year design event; the required level of service for this road.

An HY-8 model was assembled to assess the conditions under the design event. Based on existing conditions, the 25-year water level was established as 88.46 m, which provides 0.81 m of freeboard for this event. The based on this analysis this crossing has sufficient capacity to convey 2.28 m<sup>3</sup>/s before overtopping, the 100 Year flow for this location is 1.904 m<sup>3</sup>/s, as such this culvert has greater than a 100-year level of service. See attachment D for the full analysis of this crossing

### Conclusion

The memorandum confirms the following design conditions:

- Pond 2 is sufficiently sized to meet the existing release rates and erosion control requirements.
- The preliminary HGL analysis confirms the proposed storm sewer network is sufficiently sized.
- The 6.29 ha drainage area to the north will be treated by Pond 1.
- The 1.93 ha uncontrolled rear yard area will discharge directly to the southern tributary of Cardinal Creek.
- The existing culvert at Cox County Rd is sufficiently sized.
- Pond 2's bottom-draw outlet pipe will reduce outflow temperatures to Cardinal Creek.

Yours truly,  
**J.F Sabourin and Associates Inc.**

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Cardinal Creek Village South –  
Preliminary Stormwater Management Plan and Stormwater Management Facility Design  
December 2021

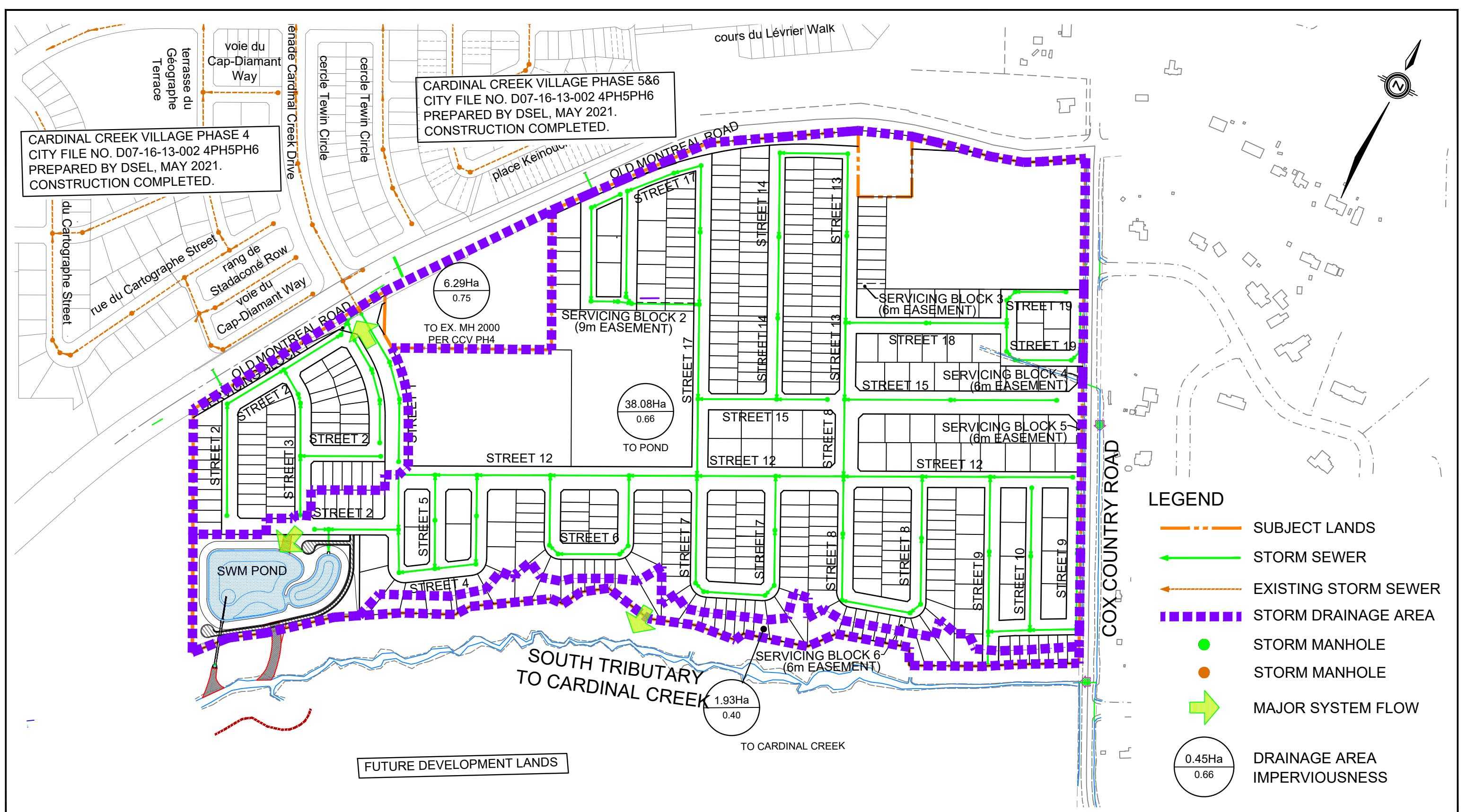


## Figures

Figure 12: Post-Development Drainage Area Plan (DSEL)

## Attachments

- Attachment A: Pond 2 Summary Tables and Modelling Files
- Attachment B: Pond 2 Forebay Calculations
- Attachment C: HGL Analysis Results and Modelling Files
- Attachment D: Cox Country Road Culvert Analysis





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# Attachment A

Pond 2 Summary Tables and Modelling Files

**Table A-1: Summary of Total Proposed Drainage Area**

To SWM Facility	Area (ha)	Imperv. (%)	Area x Imp.	Required Storage <sup>(1)</sup> (m <sup>3</sup> )		
				Perm. Pool	Qual. Control	Eros. Control
Pond 2	38.08	66	2513.3	6689	1523	5495

<sup>(1)</sup> Quality control and permanent pool requirements based on MOE guidelines for enhanced quality control for wet ponds.

Erosion control based on 25 mm storm runoff volume for Pond 2, confirmed by 2013 continuous erosion analysis.

**Table A-2: Simulated Release Rates and Volumes for Proposed SWM Facility 2 to South Tributary of Cardinal Creek <sup>(1)</sup>**

Pond Component	Existing Outflow (m <sup>3</sup> /s)	SWM Facility 2 (38.08 ha)		
		Pond Outflow (m <sup>3</sup> /s)	Pond Level (m)	Pond Storage (m <sup>3</sup> )
Permanent Pool <sup>(2)</sup>	N/A	N/A	82.50	12419
Extended Detention <sup>(2)</sup>	N/A	0.044	83.40	8282
2yr/24hr SCS	0.253	0.091	83.48	9132
5yr/24hr SCS	0.432	0.241	83.75	12010
10yr/24hr SCS	0.565	0.340	83.93	14030
25yr/24hr SCS	0.741	0.442	84.15	16620
50yr/24hr SCS	0.883	0.503	84.31	18620
100yr/24hr SCS	1.043	0.559	84.48	20780
July 1st, 1979	N/A	0.801	84.66	23060
August 4th, 1988	N/A	0.544	84.44	20150
August 8, 1996	N/A	0.511	84.34	18910

<sup>(1)</sup> Existing conditions flows as generated on subcatchments to south tributary as per Greater Cardinal Creek Subwatershed Study Existing Conditions XPSWMM hydrology model provided by AECOM on December 21, 2012, and pro-rated by drainage area (228.87 ha total, 31.20 ha through subject site). Post- to pre-development quantity control required for the 2- to 100-year design storms.

<sup>(2)</sup> Extended detention based on 25 mm storm runoff volume with a drawdown time of 96 hours. Volumes are active storage only for all components except the permanent pool.

**Table A-3: Extended Detention Parameters for SWM Facility 2**

Permanent Pool Parameters		Quality Orifice Parameters	
Area (C3)	8150.05 m <sup>2</sup>	Diameter	0.150 m
Volume	12418.64 m <sup>3</sup>	Area	0.018 m <sup>2</sup>
PP Elev	82.500 m	Invert	82.500 m
QC Elev	82.700 m	C <sub>o</sub>	0.62
h (m)	0.200 m		

- Notes:
- C3 is the intercept from the area-depth linear regression.
  - PP Elev indicates the elevation of the permanent pool.
  - QC Elev indicates the elevation of the storage volume required by MOE for quality control.
  - h is the maximum water elevation above the orifice (m).

**Table A-4: Extended Detention Drawdown Time for SWM Facility 2**

Elev. (m)	Active Storage			C2 (m <sup>2</sup> /m)	Drawdown Time (h)	Drawdown Time (days)	Flow (m <sup>3</sup> /s)	Demarkation Point
	V (m <sup>3</sup> )	A (m <sup>2</sup> )	depth (m)					
<b>82.50</b>	<b>0.00</b>	<b>8150.05</b>	<b>0.00</b>				<b>0.000</b>	PP Elev
82.60	826.69	8383.80	0.10	2337	29.74	1.24	0.009	
<b>82.70</b>	<b>1676.76</b>	<b>8617.55</b>	<b>0.20</b>	<b>2337</b>	<b>42.46</b>	<b>1.77</b>	<b>0.017</b>	QC Elev
82.80	2550.20	8851.29	0.30	2337	52.48	2.19	0.023	
82.90	3447.02	9085.04	0.40	2337	61.16	2.55	0.028	
83.00	4367.21	9318.79	0.50	2337	69.00	2.87	0.032	
83.10	5310.78	9552.53	0.60	2337	76.27	3.18	0.035	
83.20	6277.72	9786.28	0.70	2337	83.12	3.46	0.038	
83.30	7268.03	10020.03	0.80	2337	89.64	3.74	0.041	
<b>83.40</b>	<b>8281.72</b>	<b>10253.78</b>	<b>0.90</b>	<b>2337</b>	<b>95.92</b>	<b>4.00</b>	<b>0.044</b>	Ext. Det.
83.50	9318.79	10487.53	1.00	2337	101.99	4.25	0.047	

- Notes:
- C2 is the slope coefficient from the area-depth linear regression.
  - PP Elev indicates the elevation of the permanent pool.
  - QC Elev indicates the elevation of the storage volume required by MOE for quality control.
  - Ext. Det. indicates the elevation of extended detention provided based on the detention of the 25 mm storm for a 96 hour drawdown time.

**Table A-5: Stage-Storage-Outflow Curve for SWM Facility 2**

			Quality Control 1		Quantity Control 1		Emergency Spillway		
			Vertical Orifice		Vertical Orifice		Broad Crested Weir		
Elevation	Active Sto.	Demarkation Points	Head	Outflow	Head	Outflow	L (m)	6.000	
(m)	(m <sup>3</sup> )		(m)	(m <sup>3</sup> /s)	(m)	(m <sup>3</sup> /s)			
<b>82.50</b>	<b>0</b>	PP Elev	<b>0.000</b>	<b>0.000</b>	<b>0.000</b>	<b>0.000</b>	<b>0.000</b>	<b>0.000</b>	<b>0.000</b>
82.60	827		0.100	0.009	0.000	0.000	0.000	0.000	0.009
<b>82.70</b>	<b>1677</b>	QC Elev	<b>0.200</b>	<b>0.017</b>	<b>0.000</b>	<b>0.000</b>	<b>0.000</b>	<b>0.000</b>	<b>0.017</b>
82.80	2550		0.300	0.023	0.000	0.000	0.000	0.000	0.023
82.90	3447		<b>0.400</b>	<b>0.028</b>	<b>0.000</b>	<b>0.000</b>	<b>0.000</b>	<b>0.000</b>	<b>0.028</b>
83.00	4367		0.500	0.032	0.000	0.000	0.000	0.000	0.032
83.10	5311		0.600	0.035	0.000	0.000	0.000	0.000	0.035
83.20	6278		0.700	0.038	0.000	0.000	0.000	0.000	0.038
83.30	7268		0.800	0.041	0.000	0.000	0.000	0.000	0.041
<b>83.40</b>	<b>8282</b>	Ext. Det.	<b>0.900</b>	<b>0.044</b>	<b>0.000</b>	<b>0.000</b>	<b>0.000</b>	<b>0.000</b>	<b>0.044</b>
83.50	9319		1.000	0.047	0.100	0.054	0.000	0.000	0.101
83.60	10379		1.100	0.049	0.200	0.108	0.000	0.000	0.157
83.70	11463		1.200	0.051	0.300	0.162	0.000	0.000	0.213
83.80	12570		1.300	0.054	0.400	0.216	0.000	0.000	0.269
83.90	13701		1.400	0.056	0.500	0.270	0.000	0.000	0.325
84.00	14855		1.500	0.058	0.600	0.319	0.000	0.000	0.377
84.10	16032		1.600	0.060	0.700	0.362	0.000	0.000	0.422
84.20	17233		1.700	0.062	0.800	0.400	0.000	0.000	0.462
84.30	18457		1.800	0.064	0.900	0.435	0.000	0.000	0.498
84.40	19704		1.900	0.066	1.000	0.467	0.000	0.000	0.533
84.50	20975		2.000	0.067	1.100	0.497	0.000	0.000	0.564
<b>84.60</b>	<b>22258</b>	Ovf Elev	<b>2.100</b>	<b>0.069</b>	<b>1.200</b>	<b>0.526</b>	<b>0.000</b>	<b>0.000</b>	<b>0.595</b>
84.70	23540		2.200	0.071	1.300	0.553	0.100	0.300	0.923
84.80	24823		2.300	0.072	1.400	0.578	0.200	0.848	1.499
									2.482

- Notes :
- PP Elev indicates the elevation of the permanent pool.
  - QC Elev indicates the elevation of the storage volume required by MOE for quality control.
  - Ext. Det. indicates the elevation of extended detention provided based on the detention of the 25 mm storm.
  - Ovf Elev indicates the elevation of the emergency overflow provided above the 100-year water level.

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00122 *-----[005YCH.stm]-->-storm filename, one per line for NSTORM time
00123 *-----[005YCH.stm]-->-storm filename, one per line for NSTORM time
00124 *-----[005YCH.stm]-->-storm filename, one per line for NSTORM time
00125 *-----[005YCH.stm]-->-storm filename, one per line for NSTORM time
00126 *-----[005YCH.stm]-->-storm filename, one per line for NSTORM time
00127 *-----[005YCH.stm]-->-storm filename, one per line for NSTORM time
00128 *-----[005YCH.stm]-->-storm filename, one per line for NSTORM time
00129 *-----[005YCH.stm]-->-storm filename, one per line for NSTORM time
00130 *-----[005YCH.stm]-->-storm filename, one per line for NSTORM time
00131 *-----[005YCH.stm]-->-storm filename, one per line for NSTORM time
00132 *-----[005YCH.stm]-->-storm filename, one per line for NSTORM time
00133 *-----[005YCH.stm]-->-storm filename, one per line for NSTORM time
00134 *-----[005YCH.stm]-->-storm filename, one per line for NSTORM time
00135 *-----[005YCH.stm]-->-storm filename, one per line for NSTORM time
00136 FINISH

```

```

00001+ ****
00002+ **** SWMM Version 5.02/Jan 2001 -BETA* / INPUT DATA FILE
00003+ **** SSSSS W W M M N H E Y Y M M O O O 222 000 11 5555 ****
00004+ **** S W W M M M H E Y Y M M M O O O 2 0 0 11 5 .500
00005+ **** SSSSS WWW M M M HHHHH Y Y M M M O O O 2 0 0 11 555 Ver 5.500
00006+ **** SSSSS W W M M H H Y M M M O O O 222 0 0 11 555 FBS 2015
00007+ **** SSSSS W W M M H H Y M M M O O O 2 0 0 11 5 .500
00008+ **** StormWater Management HYdrologic Model 222 000 11 555 2549237
00009+ ****
00010+ **** SWMM Version 1.500
00011+ **** A single event and continuous hydrologic simulation model
00012+ **** based on the principles of HMO and its successors
00013+ ****
00014+ **** Distributed by: J.F. Sabourin and Associates Inc.
00015+ **** 1000, Rue de la Montagne, Suite 200
00016+ **** Gatineau, Quebec, (819) 243-6858
00017+ **** E-Mail: swmymo@fma.ca
00018+ ****
00019+ **** Project Number: [959(03)]
00020+ **** File Name: [Cardinal Creek Village South]
00021+ ****
00022+ **** Licensed user: [*****]
00023+ **** Ottawa SERIAL#:[2549237]
00024+ ****
00025+ **** ***** PROGRAM ARRAY DIMENSIONS *****
00026+ **** Max. number of basins : 105408
00027+ **** Max. number of rainfall points : 105408
00028+ **** Max. number of flow points : 105408
00029+ ****
00030+ **** S U M M A R Y O U T P U T
00031+ ****
00032+ **** RUN DATE: 2021-12-16 TIME: 12:08:11 RUN COUNTER: 001514
00033+ ****
00034+ **** Input file: C:\Users\blidbette\Desktop\SWMM\SWM\CCVS_v01.vol
00035+ **** Output file: C:\Users\blidbette\Desktop\SWMM\SWM\CCVS_v01.out
00036+ **** Summary file: C:\Users\blidbette\Desktop\SWMM\SWM\CCVS_v01.sum
00037+ **** User comments:
00038+ 1:
00039+ 2:
00040+ 3:
00041+ ****
00042+ ****
00043+ ****
00044+ ****
00045+ ****
00046+ ****
00047+ ****
00048+ ****
00049+ ****
00050+ ****
00051+ **** SWMM Version 1.502/Jan 2001 -BETA* / INPUT DATA FILE
00052+ ****
00053+ **** Project Name: [Cardinal Creek Village South]
00054+ **** Project Number: [959(03)]
00055+ **** Date : [2021/12/10]
00056+ **** Modeler : [*****]
00057+ **** Company : [J.F. Sabourin and Associates]
00058+ **** License # : 2549237
00059+ ****
00060+ **** RINN:COMMAND#
00061+ **** R0001:CODE0001
00062+ ****
00063+ **** [TZERO = 0.00 hrs on 0]
00064+ **** [METOUT= 2 (Imperial, 2=metric output)]
00065+ **** [NRUN= 0000]
00066+ **** [NRUN= 0001]
00067+ **** R0001:CODE0002
00068+ ****
00069+ **** File name = storm.001
00070+ **** Comment = 20 MM Based on CHICAGO STORM 2 Year, 3 Hours
00071+ **** [SUT=10.00:SOUR= 3.00:PTOT= 35.00]
00072+ **** R0001:CODE0003
00073+ **** DEFAULT VALUES
00074+ ****
00075+ **** ICASEDV = 1 (read and print data)
00076+ **** FileTitle= File comment [Parameters for City of Ottawa Projects]
00077+ **** FileTitle= File comment [Parameters for CITY OF CHICAGO STORM IN THE DESIGN STANHDY COM]
00078+ **** Horton's Infiltration equation parameters:
00079+ **** [Fo=.76 .20 mm/hr] [Fo=.13 .20 mm hr] [DCvA= 4.14 hr] [Fa=.00 mm]
00080+ **** Parameters for IMPERVIOUS surfaces in STANHDY:
00081+ **** [Iapex= 4.67 mm] [LGP=.40 .00 mm] [NMW=.250]
00082+ **** Parameters for IMPERVIOUS surfaces in STANHDY:
00083+ **** [Iapex= 1.57 mm] [LGP=.50 .00 mm] [NMW=.100]
00084+ **** Parameters used in NASHY:
00085+ **** [Ia=.467 mm] [N=.300]
00086+ **** Average monthly Par Evaporation data in (mm):
00087+ **** JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00088+ **** .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00089+ **** Average monthly Potential Evapotranspiration in (mm):
00090+ **** JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00091+ **** .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00092+ ****
00093+ **** PROPOSED CONDITIONS
00094+ ****
00095+ **** File name = Cardinal Creek Village South Pond 2
00096+ ****
00097+ **** R0001:CODE0004:-----DtnID:NHYD----ARAAh-QPAKms-Tpeakdate_hh:mm:--RVm-R.C.--DWFcms
00098+ **** CALIBRATION-----1.0 01:CVCS 38.08 2.435 No_date 1:05 14.43 .757 .000
00099+ **** [XIND=.56:TIMP=.66]
00100+ **** [Horton parameters: Fo=.76 .20 Fc=.13 .20 DCvA=.14: Fa=.00]
00101+ **** [Impervious area: Iapex= 1.57 SLPI=.90 LGI=.504 NMW=.013:RCI=.0]
00102+ **** Estimated Pond Volumes for SWM Facility:
00103+ **** R0001:CODE0005:-----DtnID:NHYD----ARAAh-QPAKms-Tpeakdate_hh:mm:--RVm-R.C.--DWFcms
00104+ **** ROUTE RESERVOIR --> 1.0 02:CVCS 38.08 .2435 No_date 1:05 14.43 n/a .000
00105+ **** out <= 1.0 01:Pout 38.08 .035 No_date 1:16 14.43 n/a .000
00106+ **** overflow <= 1.0 01:Ovfl 38.08 .000 No_date 1:16 14.43 n/a .000
00107+ **** [MstCoLsEd=.5219E+00 m3, TotCovVol=.0000E+00 m3, N-Ovfl= 0, TotSurfOvfl= 0.hrs]
00108+ ****
00109+ ****
00110+ ****
00111+ **** ** END OF RUN : 1
00112+ ****
00113+ ****
00114+ ****
00115+ ****
00116+ ****
00117+ ****
00118+ **** RINN:COMMAND#
00119+ **** R0002:CODE0001
00120+ ****
00121+ **** [TZERO = 0.00 hrs on 0]
00122+ **** [METOUT= 2 (Imperial, 2=metric output)]
00123+ **** [NRUN= 0000]
00124+ **** [NRUN= 0001]
00125+ ****
00126+ **** # SWMM Version 1.502/Jan 2001 -BETA* / INPUT DATA FILE
00127+ ****
00128+ **** Project Name: [Cardinal Creek Village South]
00129+ **** Project Number: [959(03)]
00130+ **** Date : [2021/12/10]
00131+ **** Modeler : [*****]
00132+ **** Company : [J.F. Sabourin and Associates]
00133+ **** License # : 2549237
00134+ ****
00135+ **** R0002:CODE0002
00136+ ****
00137+ **** READ STORM
00138+ **** File name = storm.001
00139+ **** Comment = CHICAGO STORM 2 Year, 3 Hours
00140+ **** [SUT=10.00:SOUR= 3.00:PTOT= 31.86]
00141+ **** R0002:CODE0003
00142+ **** DEFAULT VALUES
00143+ **** File name = C:\Users\blidbette\Desktop\SWMM\SWM\Ottawa.vol
00144+ ****
00145+ **** FileTitle= File comment [Parameters for City of Ottawa Projects]
00146+ **** FileTitle= File comment [Parameters for CITY OF CHICAGO STORM IN THE DESIGN STANHDY COM]
00147+ **** Horton's Infiltration equation parameters:
00148+ **** [Fo=.76 .20 mm/hr] [Fo=.13 .20 mm hr] [DCvA= 4.14 hr] [Fa=.00 mm]
00149+ **** Parameters for PERVIOUS surfaces in STANHDY:
00150+ **** [Iapex= 4.67 mm] [LGP=.40 .00 mm] [NMW=.250]
00151+ **** Parameters for IMPERVIOUS surfaces in STANHDY:
00152+ **** [Iapex= 1.57 mm] [LGP=.50 .00 mm] [NMW=.013]
00153+ **** Parameters used in NASHY:
00154+ **** [Ia=.467 mm] [N=.300]
00155+ **** Average monthly Par Evaporation data in (mm):
00156+ **** JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00157+ **** .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00158+ **** Average monthly Potential Evapotranspiration in (mm):
00159+ **** JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00160+ **** .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00161+ ****
00162+ ****
00163+ **** Lumped drainage to Cardinal Creek Village South Pond 2
00164+ ****
00165+ **** R0002:CODE0004:-----DtnID:NHYD----ARAAh-QPAKms-Tpeakdate_hh:mm:--RVm-R.C.--DWFcms
00166+ **** CALIB 1.0 01:CVCS 38.08 3.438 No_date 1:04 19.77 .620 .000
00167+ **** [XIND=.56:TIMP=.66]
00168+ **** [Pervious area: Iapex= 4.67 SLPI=.90 LGI=.504 NMW=.013:RCI=.0]
00169+ **** ROUTE RESERVOIR --> 1.0 02:CVCS 38.08 .3438 No_date 1:16 19.77 n/a .000
00170+ **** out <= 1.0 01:Pout 38.08 .041 No_date 3:14 19.77 .000
00171+ **** overflow <= 1.0 01:Ovfl 38.08 .000 No_date 0:00 .00 n/a .000
00172+ **** [MstCoLsEd=.7205E+00 m3, TotCovVol=.0000E+00 m3, N-Ovfl= 0, TotSurfOvfl= 0.hrs]
00173+ ****
00174+ **** # STORMS
00175+ ****
00176+ ****
00177+ ****
00178+ ****
00179+ ****
00180+ ****
00181+ ****
00182+ ****
00183+ ****
00184+ ****
00185+ ****
00186+ ****
00187+ ****
00188+ **** RINN:COMMAND#
00189+ **** R0002:CODE0001

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00757+ R0125:00002-----
00758+ READ STORM
00759+   Filename = storm.001
00760+   Comment = 50 years SCS Type 2 Storm 24 Hours step 10 min, City of Ottawa
00761+   [SDT=10.00:SDUR= 24.00:PTOT= 86.89]
00762+ R0125:00003-----
00763+ DEFAULT VALUES
00764+   Filename = C:\Users\blidbette\Desktop\SWMHYMO\SWN\Ottawa.val
00765+   FileTitle= File comment: [Parameters for City of Ottawa Projects]
00766+   FileContent= File comment: [Parameters for City of Ottawa Projects]
00767+   THE FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDYD COM
00768+ Horton's infiltration equation parameters:
00769+   [F= 76.20 mm/hr] [DCAY= 4.14 hr] [F= .00 mm]
00770+   Parameters for PREVIOUS surfaces in STANDYD:
00771+   [Iaper= 4.67 mm] [LDP= 0.01 m] [N= .00]
00772+   Parameters for IMPERVIOUS surfaces in STANDYD:
00773+   [IAimp= 1.57 mm] [CLD= 1.50] [MNW= .013]
00774+   Parameters used in NASHYD:
00775+   [Ia= 4.67 mm] [N= 3.00]
00776+   Average monthly Pa Evaporation data in (mm)
00777+   JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00778+   .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00779+   Average monthly Potential Evapotranspiration in (mm)
00780+   JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00781+   .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00782+ ****
00783+ ****
00784+ ****
00785+ ****
00786+ ****
00787+ # Lumped drainage to Cardinal Creek Village South Pond 2
00788+ R0125:00004-----Dtnin-ID:NYND---ARAHb-OPAKms-Tpeakdate_hh:mm:--RVm=R.C.--DFWcm
00789+   CALIB STANDYD 1.0 01:CVCS 38.08 7.455 No_date 12:02 60.46 .696 .000
00790+   [XIND=.56:TIMEP=.66]
00791+   [Impervious area: Iaper= 4.67:SLDP=2.00:LDP= 40:NWP= .250:SCP= .0]
00792+   [Previous area: IAimp= 1.57:SLDP= .90:LDP= 504:MNW= .013:SCl= .0]
00793+   # Estimated Pond Volume for SWN Facility
00794+   R0125:00005-----Dtnin-ID:NYND---ARAHb-OPAKms-Tpeakdate_hh:mm:--RVm=R.C.--DFWcm
00795+   ROUTE RESERVOIR -> 1.0 02:CVCS 38.08 7.455 No_date 12:02 60.46 .696 .000
00796+   [MetOut= 0.01 m3 .TotVol= 0.000e+00 m3 .N-Ov= 0. TotSurf= 0.hrs]
00797+   [MetC-Sed=.162E+01 m3 .TotCVol=.0000e+00 m3 .N-Ov= 0. TotSurf= 0.hrs]
00798+   [Iaper= 4.67 mm] [LDP= 0.01 m] [NWP= .000]
00799+   # PROPOSED CONDITIONS
00800+   ****
00801+   ** END OF RUN : 149
00802+ ****
00803+ ****
00804+ ****
00805+ ****
00806+ ****
00807+ ****
00808+ ****
00809+ R0119:COMMAND#
00810+ R0119:00001-----
00811+   START
00812+   [TZERO = .00 hrs on 0]
00813+   [METOUT= 2 (Imperial, 2=metric output)]
00814+   [INSTORM= 1 ]
00815+   [IMWD= .000]
00816+   ****
00817+ # SWMHYMO Ver:5.02/Jan 2001 <Beta> / INPUT DATA FILE
00818+   ****
00819+   # Project Name : [Cardinal Creek Village South]
00820+   # Project Number: [559|031]
00821+   # Date : [2021/12/10]
00822+   # Modeler : [BL]
00823+   # Company : [J.F. Sabourin and Associates]
00824+   # License # : [2549237]
00825+   ****
00826+ R0119:00002-----
00827+ ****
00828+   Filename = storm.001
00829+   Comment = 50 years SCS Type 2 Storm 24 Hours step 10 min, City of Ottawa
00830+   [SDT=10.00:SDUR= 24.00:PTOT= 86.89]
00831+ R0119:00003-----
00832+ DEFAULT VALUES
00833+   FileTitle= File comment: [Parameters for City of Ottawa Projects]
00834+   FileContent= File comment: [Parameters for City of Ottawa Projects]
00835+   THE FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDYD COM
00836+   Horton's infiltration equation parameters:
00837+   [F= 76.20 mm/hr] [DCAY= 4.14 hr] [F= .00 mm]
00838+   Parameters for PREVIOUS surfaces in STANDYD:
00839+   [Iaper= 4.67 mm] [LDP= 0.01 m] [N= .00]
00840+   Parameters for IMPERVIOUS surfaces in STANDYD:
00841+   [IAimp= 1.57 mm] [CLD= 1.50] [MNW= .013]
00842+   Parameters used in NASHYD:
00843+   [Ia= 4.67 mm] [N= 3.00]
00844+   Average monthly Pa Evaporation data in (mm)
00845+   JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00846+   .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00847+   Average monthly Potential Evapotranspiration in (mm)
00848+   JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00849+   .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00850+   ****
00851+ ****
00852+ ****
00853+ ****
00854+ ****
00855+ ****
00856+ ****
00857+ R0979:COMMAND#
00858+   READ STORM
00859+   FileTitle= File comment: [Parameters for City of Ottawa Projects]
00860+   FileContent= File comment: [Parameters for City of Ottawa Projects]
00861+   THE FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDYD COM
00862+   Horton's infiltration equation parameters:
00863+   [F= 76.20 mm/hr] [DCAY= 4.14 hr] [F= .00 mm]
00864+   Parameters for PREVIOUS surfaces in STANDYD:
00865+   [Iaper= 4.67 mm] [LDP= 0.01 m] [N= .00]
00866+   Parameters for IMPERVIOUS surfaces in STANDYD:
00867+   [IAimp= 1.57 mm] [CLD= 1.50] [MNW= .013]
00868+   Parameters used in NASHYD:
00869+   [Ia= 4.67 mm] [N= 3.00]
00870+   Average monthly Pa Evaporation data in (mm)
00871+   JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00872+   .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00873+   Average monthly Potential Evapotranspiration in (mm)
00874+   JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00875+   .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00876+   ****
00877+ ****
00878+ ****
00879+ ****
00880+ ****
00881+ ****
00882+ ****
00883+ ****
00884+ ****
00885+ ****
00886+ ****
00887+ ****
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00932+ ****
00933+ ****
00934+ ****
00935+ ****
00936+ ****
00937+ ****
00938+ ****
00939+ ****
00940+ ****
00941+ ****
00942+ ****
00943+ ****
00944+ ****
00945+ ****
00946+ ****
00947+ RUN#:COMMAND#
00948+ R0979:COMMAND#
00949+   START
00950+   [TZERO = .00 hrs on 0]
00951+   [INSTORM= 2 (Imperial, 2=metric output)]
00952+   [INSTORM= 1 ]
00953+   [INRNU= .0979]
00954+   ****
00955+ ****
00956+ ****
00957+ R0979:COMMAND#
00958+   READ STORM
00959+   FileTitle= File comment: [Parameters for City of Ottawa Projects]
00960+   FileContent= File comment: [Parameters for City of Ottawa Projects]
00961+   THE FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDYD COM
00962+   Horton's infiltration equation parameters:
00963+   [F= 76.20 mm hr] [DCAY= 4.14 hr] [F= .00 mm]
00964+   Parameters for PREVIOUS surfaces in STANDYD:
00965+   [Iaper= 4.67 mm] [LDP= 0.01 m] [N= .00]
00966+   Parameters for IMPERVIOUS surfaces in STANDYD:
00967+   [IAimp= 1.57 mm] [CLD= 1.50] [MNW= .013]
00968+   Parameters used in NASHYD:
00969+   [Ia= 4.67 mm] [N= 3.00]
00970+   Average monthly Pa Evaporation data in (mm)
00971+   JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00972+   .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00973+   Average monthly Potential Evapotranspiration in (mm)
00974+   JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00975+   .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00976+   ****
00977+ ****
00978+ ****
00979+ ****
00980+ ****
00981+ ****
00982+ ****
00983+ ****
00984+ ****
00985+ ****
00986+ ****
00987+ ****
00988+ ****
00989+ ****
00990+ ****
00991+ ****
00992+ ****
00993+ ****
00994+ ****
00995+ ****
00996+ ****
00997+ ****
00998+ ****
00999+ ****
01000+ ****
01001+ R0979:COMMAND#
01002+   ROUTE RESERVOIR -> 1.0 01:CVCS 38.08 8.163 No_date 1:35 68.14 .811 .000
01003+   [MetOut= 1.0 01:Port 38.08 .801 No_date 2:23 68.14 n/a .000
01004+   [MetC-Sed=.162E+01 m3 .TotCVol=.0000e+00 m3 .N-Ov= 0. TotSurf= 0.hrs]
01005+   [MetC-Sed=.2018E+01 m3 .TotCVol=.0000e+00 m3 .N-Ov= 0. TotSurf= 0.hrs]
01006+   ****
01007+ ****
01008+   ** END OF RUN : 987
01009+ ****
01100+ ****
01101+ ****
01102+ ****
01103+ ****
01104+ ****
01105+ ****
01106+ ****
01107+ ****
01108+ ****
01109+ ****
01110+ ****
01111+ ****
01112+ ****
01113+ ****
01114+ ****
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01117+ ****
01118+ ****
01119+ ****
01120+ ****
01121+ ****
01122+ ****
01123+ ****
01124+ ****
01125+ ****
01126+ ****
01127+ ****
01128+ ****
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01130+ ****
01131+ ****
01132+ ****
01133+ ****
01134+ ****
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01136+ ****
01137+ ****
01138+ ****
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01140+ ****
01141+ ****
01142+ ****
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01146+ ****
01147+ ****
01148+ ****
01149+ ****
01150+ ****
01151+ ****
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01161+ ****
01162+ ****
01163+ ****
01164+ ****
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01166+ ****
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01169+ ****
01170+ ****
01171+ ****
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01173+ ****
01174+ ****
01175+ ****
01176+ ****
01177+ ****
01178+ ****
01179+ ****
01180+ ****
01181+ ****
01182+ ****
01183+ ****
01184+ ****
01185+ R0979:COMMAND#
01186+ R0996:COMMAND#
01187+   READ STORM
01188+   FileTitle= File comment: [Parameters for City of Ottawa Projects]
01189+   FileContent= File comment: [Parameters for City of Ottawa Projects]
01190+   THE FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDYD COM
01191+   Horton's infiltration equation parameters:
01192+   [F= 76.20 mm hr] [DCAY= 4.14 hr] [F= .00 mm]
01193+   Parameters for PREVIOUS surfaces in STANDYD:
01194+   [Iaper= 4.67 mm] [LDP= 0.01 m] [N= .00]
01195+   Parameters for IMPERVIOUS surfaces in STANDYD:
01196+   [IAimp= 1.57 mm] [CLD= 1.50] [MNW= .013]
01197+   Parameters used in NASHYD:
01198+   [Ia= 4.67 mm] [N= 3.00]
01199+   Average monthly Pa Evaporation data in (mm)
01200+   JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
01201+   .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
01202+   Average monthly Potential Evapotranspiration in (mm)
01203+   JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
01204+   .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
01205+   ****
01206+ ****
01207+ ****
01208+ ****
01209+ ****
01210+ ****
01211+ ****
01212+ ****
01213+ ****
01214+ ****
01215+ ****
01216+ ****
01217+ ****
01218+ ****
01219+ ****
01220+ ****
01221+ ****
01222+ ****
01223+ ****
01224+ ****
01225+ ****
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01135> [Previous area: Iaper 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP=.0]
01136> [Impervious area: IAlmp= 1.57:SLP1=.90:LGN= 504.:MNP=.013:SC1=.0]
01137> # Estimated Pond Volumes for Rain Facility
01138> DYN99:CD0005-----ARAhb-OPENKcms-TpeakDate_hb.m:---RVm=R.C.---DWFcms
01139> ROUTE RESERVOIR -> 1.0 01:CVS 38.08 6.695 No_date 1:31 58.25 n/a .000
01140> ROUTE OVERFLOW -> 1.0 01:Pout 38.08 .511 No_date 1:31 58.25 n/a .000
01141> overflow <= 1.0 03:Povf .05 .000 No_date 0:00 .00 n/a .000
01142> [MscTotalVol=.1891E+01 m3 TotCvVol=.0000E+00 m3 N-Ovf= 0. TotDurOvf=.0hrs]
01143> #####
01144> # STORM
01145> ##### END OF RUN ! 998
01146> ****
01147>
01148> ****
01149>
01150>
01151>
01152>
01153> RINN:COMMAND#
01154> RINN:CD0001-----
01155> START
01156> [TZERO = 0.00 hrs 0]
01157> [IMPERVIOUS = 2.00 (1=imperial, 2=metric output)]
01158> [NSTORM = 1]
01159> [NRUN = 0999]
01160> ****
01161> # SWMHYMO Ver5.01/Jan 2001 *BETTA* / INPUT DATA FILE
01162> # ****
01163> # Project Name: Cardinal Creek Village South
01164> # Project Number: (959103)
01165> # Date : (2021/12/10)
01166> # Compiler : 1
01167> # Company : J.F. Sabourin and Associates
01168> # License #: 2549237
01169> ****
01170> R0999:CD0002-----
01171> READ STORM
01172> File= storm.001
01173> Comment = CHICAGO STORM 100 Year, 3 Hours
01174> (EDT=18.00:SDUR= 3.00:PTOT= 86.00)
01175> ****
01176> R0999:CD0003-----DEFUALT VALUES
01177> Filename = C:\Users\willib\Documents\Desktop\SWMHYMO\SWM\Ottawa.val
01178> IPR=1000000 (read and print data)
01179> FileTitle= File comment [Parameters for City of Ottawa Projects]
01180> ****
01181> THE FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDYD COM
01182> Morton's infiltration parameters [F=1.20 mm/hr] [DCAY= 4.14 /hr] [Fz=.00 mm]
01183> Parameters for PERMEABLE surfaces in STANDYD:
01184> [IAlmp=.667 (LGP=.00 mm) [IAlmp=.250]
01185> Parameters for IMPERVIOUS surfaces in STANDYD:
01186> [IAlmp=.667 (LGP=.00 mm) [IAlmp=.250] [MNP=.013]
01187> Parameters used in NASHTD:
01188> [Ia=.67 mm] [H 3.00]
01189> Average rainfall intensity in precipitation data in (mm):
01190> JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
01191> .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
01192> JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
01193> .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
01194> JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
01195> .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
01196> #####
01197> # PROPOSED CONDITIONS
01198> #####
01199> # Rainfall Data for Rain Facility
01200> DYN99:CD0004-----ARAhb-OPENKcms-TpeakDate_hb.m:---RVm=R.C.---DWFcms
01201> CALIB:STANDYD 1.0 01:CVS 38.08 14.800 No_date 1:02 68.72 .799
01202> ****
01203> (Morton parameters: F= 76.20:Fc= 13.20:DCAY=4.14: Fz .00)
01204> [Previous area: Iaper 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP=.0]
01205> [Impervious area: IAlmp= 1.57:SLP1=.90:LGN= 504.:MNP=.013:SC1=.0]
01206> # Estimated Pond Volumes for RIN Facility
01207> DYN99:CD0005-----ARAhb-OPENKcms-TpeakDate_hb.m:---RVm=R.C.---DWFcms
01208> ROUTE RESERVOIR -> 1.0 01:CVS 38.08 14.800 No_date 1:02 68.71 n/a .000
01209> ROUTE OVERFLOW -> 1.0 01:Pout 38.08 .644 No_date 2:12 68.71 n/a .000
01210> overflow <= 1.0 03:Povf .05 .000 No_date 0:00 .00 n/a .000
01211> [MscTotalVol=.1891E+01 m3 TotCvVol=.0000E+00 m3 N-Ovf= 0. TotDurOvf=.0hrs]
01212> #####
01213> # STORM
01214> ****
01215> R0999:CD0002-----
01216> FINISH
01217> ****
01218> ****
01219> WARNING: ERRORS / NOTES
01220> -----
01221> Simulation ended on 2021-12-16 at 12:08:18
01222> ****

```



Ottawa. ON  
Paris. ON  
Gatineau. QC  
Montréal. QC  
Québec. QC

# Attachment B

## Pond 2 Forebay Calculations

## **CALCULATION SHEET B-1: FOREBAY SIZING FOR SWM FACILITY 2**

### **Cardinal Creek Village South SWM Facility 2 City of Ottawa Calculation of Forebay Size**

© DSEL

#### **Settling Criteria**

From the SWMP Manual, the required length for settling is as follows:

$$L_{\min} = \left( \frac{r Q_p}{V_s} \right)^{0.5}$$

where:       $r$  = length to width ratio, at the invert of the inlet pipe.  
 $Q_p$  = peak outflow during design quality storm  
 $V_s$  = settling velocity

Input:       $r = 0.33$       (assumed)  
 $Q_p = 0.044 \text{ m}^3/\text{s}$       (at elevation 82.7 m)  
 $V_s = 0.0003 \text{ m/s}$

$$L_{\min} = 6.99 \text{ m}$$

The peak flow rate from the pond during the quality storm is taken as the flow that would occur just below the quantity controls (refer to Attachment C)

#### **Dispersion Criteria**

From the SWMP Manual, the required length for dispersion is as follows:

$$L_{\min} = \frac{8Q}{d V_f}$$

where:       $Q$  = Inlet flowrate (10-Year, 24-Hour SCS Type II Storm)  
 $d$  = depth of permanent pool (forebay)  
 $V_f$  = desired final velocity

Input:       $Q = 6.089 \text{ m}^3/\text{s}$   
 $d = 2.5 \text{ m}$   
 $V_f = 0.5 \text{ m/s}$

$$L_{\min} = 38.97 \text{ m}$$

The minimum forebay length is determined by the larger of the settling or dispersion criteria.

**Minimum Length of Forebay Required                  38.97 m                  (at elevation 82.5 m)**

#### **Average Forebay Velocity**

From the SWMP Manual, the maximum allowable average velocity is 0.15 m/s:

$$V_{avg} = \frac{Q}{d W_{avg}}$$

where:       $Q$  = Inlet flowrate (10-Year, 24-Hour SCS Type II Storm)  
 $d$  = depth of pond during peak 10-year inflow (12h:00min)  
 $W_{avg}$  = average width of forebay

Input:       $Q = 6.089 \text{ m}^3/\text{s}$   
 $d = 3.93 \text{ m}$   
 $W_{avg} = 14 \text{ m}$       (minimum required)

$$V = 0.11 \text{ m/s}$$



Ottawa. ON  
Paris. ON  
Gatineau. QC  
Montréal. QC  
Québec. QC

# Attachment C

HGL Analysis Results and Modelling Files

**Table C1: Cardinal Creek Village South - Preliminary HGL Analysis**  
**100-Year Development Flows**

MH-ID	Invert Elevation	Top of MH (m)	Max HGL (m)	Freeboard (m)
1	87.36	90.16	87.77	2.39
2	86.96	90.05	87.67	2.38
3	86.73	89.93	87.60	2.33
5	87.14	90.09	87.72	2.37
6	86.97	89.98	87.69	2.29
7	86.55	89.86	87.55	2.31
8	87.00	89.80	87.41	2.39
9	86.26	89.80	87.41	2.39
10	86.10	89.67	87.32	2.35
11	87.30	90.17	87.50	2.67
13	85.86	89.54	87.15	2.39
14	86.67	89.62	87.26	2.36
15	86.45	89.52	87.18	2.34
16	85.56	89.43	87.05	2.38
17	88.40	91.20	88.60	2.60
18	88.20	91.16	88.42	2.74
19	88.00	91.15	88.36	2.79
20	87.84	91.06	88.31	2.75
21	87.79	91.04	88.28	2.76
22	87.87	91.19	88.57	2.62
23	87.70	91.08	88.45	2.63
24	87.63	91.06	88.40	2.66
25	87.20	90.99	88.22	2.77
26	87.00	90.76	88.11	2.65
27	93.09	95.96	93.29	2.67
28	89.24	92.84	89.55	3.29
29	86.71	90.59	87.90	2.69
30	87.86	90.96	88.25	2.71
31	87.36	90.57	88.11	2.46
32	86.44	90.02	87.68	2.34
33	86.62	89.60	87.24	2.36
34	86.39	89.50	87.18	2.32
36	86.16	89.39	87.08	2.31
37	85.13	89.30	86.96	2.34
38	87.05	90.00	87.32	2.68
39	86.89	89.91	87.10	2.81
40	84.67	89.18	86.68	2.50
41	87.27	90.07	87.66	2.41
43	86.93	90.02	87.65	2.37
45	86.66	89.86	87.54	2.32
46	86.57	89.80	87.51	2.29
47	88.61	91.56	88.82	2.74
48	87.75	90.79	88.25	2.54
49	87.00	90.09	87.83	2.26
50	86.74	89.80	87.54	2.26
52	86.38	89.78	87.50	2.28
53	88.41	91.45	88.60	2.85
54	86.05	89.72	87.32	2.40
55	92.86	95.72	93.06	2.66
57	89.15	92.43	89.42	3.01
58	86.94	90.51	87.64	2.87
59	87.10	89.98	87.50	2.48
60	86.63	89.89	87.43	2.46
61	85.76	89.51	87.12	2.39
62	86.23	89.92	86.99	2.93
63	85.81	88.80	86.70	2.10
64	85.55	88.78	86.67	2.11
65	84.30	88.60	86.49	2.11
66	85.69	88.64	86.33	2.31
67	83.92	88.49	86.25	2.24
68	85.72	88.63	86.32	2.31
69	85.49	88.52	86.19	2.33
70	85.22	88.50	86.14	2.36
71	83.68	88.36	86.06	2.30
72	85.67	88.55	85.91	2.64
73	83.46	88.23	85.86	2.37
74	85.68	88.49	85.83	2.66
75	83.32	88.16	85.74	2.42
76	83.16	88.12	85.33	2.79
77	85.44	88.47	85.74	2.73
79	85.27	88.40	85.69	2.71
81	85.13	88.34	85.61	2.73
82	82.94	88.26	84.88	3.38
83	84.20	87.00	84.39	2.61
84	82.69	87.03	84.35	2.68
86	81.61	85.91	81.82	4.09
87	76.57	80.28	77.60	2.68
89	81.44	84.32	81.67	2.65
90	84.05	86.85	84.16	2.69
91	80.53	84.28	80.73	3.55
92	78.24	81.31	78.46	2.85
93	77.50	80.76	77.89	2.87
94	76.27	80.37	77.44	2.93
95	76.02	81.13	77.27	3.86
96	81.57	84.37	81.67	2.70
97	79.99	83.08	80.13	2.95
98	79.26	82.10	79.45	2.65
99	78.43	81.16	78.73	2.43
101	75.94	80.94	77.22	3.72
102	85.07	88.06	85.18	2.88
103	81.89	85.07	82.02	3.05
104	78.02	82.97	78.55	4.42
105	75.89	80.68	77.05	3.63
			Min	2.10
			Max	4.42
			Average	2.64

Model Name: CCVS\_v01.inp

## EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

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Element Count
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Number of rain gages ..... 0
Number of subcatchments ... 0
Number of nodes ..... 95
Number of links ..... 100
Number of pollutants ..... 0
Number of land uses ..... 0

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Node Summary
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Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
MH-1	JUNCTION	87.36	2.80	0.0	Yes
MH-10	JUNCTION	86.10	3.57	0.0	Yes
MH-101	JUNCTION	75.94	5.00	0.0	
MH-102	JUNCTION	85.07	2.99	0.0	Yes
MH-103	JUNCTION	81.89	3.18	0.0	Yes
MH-104	JUNCTION	78.02	4.95	0.0	Yes
MH-105	JUNCTION	75.89	4.79	0.0	
MH-11	JUNCTION	87.29	2.88	0.0	Yes
MH-13	JUNCTION	85.86	3.68	0.0	Yes
MH-14	JUNCTION	86.67	2.95	0.0	Yes
MH-15	JUNCTION	86.45	3.07	0.0	Yes
MH-16	JUNCTION	85.56	3.87	0.0	
MH-17	JUNCTION	88.40	2.80	0.0	Yes
MH-18	JUNCTION	88.19	2.96	0.0	Yes
MH-19	JUNCTION	88.00	3.15	0.0	Yes
MH-2	JUNCTION	86.95	3.10	0.0	Yes
MH-20	JUNCTION	87.84	3.22	0.0	Yes
MH-21	JUNCTION	87.79	3.25	0.0	
MH-22	JUNCTION	87.87	3.32	0.0	Yes
MH-23	JUNCTION	87.69	3.38	0.0	Yes
MH-24	JUNCTION	87.63	3.43	0.0	
MH-25	JUNCTION	87.20	3.79	0.0	Yes
MH-26	JUNCTION	87.00	3.76	0.0	Yes
MH-27	JUNCTION	93.09	2.87	0.0	Yes
MH-28	JUNCTION	89.24	3.60	0.0	
MH-29	JUNCTION	86.71	3.88	0.0	
MH-3	JUNCTION	86.73	3.21	0.0	Yes
MH-30	JUNCTION	87.86	3.10	0.0	Yes
MH-31	JUNCTION	87.36	3.21	0.0	Yes
MH-32	JUNCTION	86.44	3.58	0.0	
MH-33	JUNCTION	86.62	2.98	0.0	Yes
MH-34	JUNCTION	86.39	3.11	0.0	Yes
MH-36	JUNCTION	86.16	3.23	0.0	Yes
MH-37	JUNCTION	85.13	4.17	0.0	
MH-38	JUNCTION	87.05	2.95	0.0	Yes

MH-39	JUNCTION	86.89	3.02	0.0	Yes
MH-40	JUNCTION	84.67	4.51	0.0	
MH-41	JUNCTION	87.27	2.80	0.0	Yes
MH-43	JUNCTION	86.92	3.10	0.0	Yes
MH-45	JUNCTION	86.66	3.21	0.0	
MH-46	JUNCTION	86.56	3.23	0.0	
MH-47	JUNCTION	88.61	2.95	0.0	Yes
MH-48	JUNCTION	87.75	3.04	0.0	Yes
MH-49	JUNCTION	87.00	3.09	0.0	Yes
MH-5	JUNCTION	87.14	2.95	0.0	Yes
MH-50	JUNCTION	86.74	3.06	0.0	
MH-52	JUNCTION	86.38	3.40	0.0	
MH-53	JUNCTION	88.41	3.04	0.0	Yes
MH-54	JUNCTION	86.05	3.67	0.0	Yes
MH-55	JUNCTION	92.86	2.86	0.0	Yes
MH-57	JUNCTION	89.15	3.28	0.0	Yes
MH-58	JUNCTION	86.94	3.57	0.0	Yes
MH-59	JUNCTION	87.10	2.88	0.0	Yes
MH-6	JUNCTION	86.97	3.01	0.0	Yes
MH-60	JUNCTION	86.63	3.26	0.0	Yes
MH-61	JUNCTION	85.75	3.75	0.0	
MH-62	JUNCTION	86.23	3.69	0.0	Yes
MH-63	JUNCTION	85.81	2.99	0.0	Yes
MH-64	JUNCTION	85.55	3.23	0.0	Yes
MH-65	JUNCTION	84.30	4.30	0.0	
MH-66	JUNCTION	85.69	2.96	0.0	Yes
MH-67	JUNCTION	83.92	4.57	0.0	Yes
MH-68	JUNCTION	85.72	2.91	0.0	Yes
MH-69	JUNCTION	85.49	3.04	0.0	Yes
MH-7	JUNCTION	86.55	3.31	0.0	Yes
MH-70	JUNCTION	85.22	3.28	0.0	Yes
MH-71	JUNCTION	83.68	4.68	0.0	
MH-72	JUNCTION	85.67	2.88	0.0	Yes
MH-73	JUNCTION	83.46	4.77	0.0	
MH-74	JUNCTION	85.68	2.81	0.0	Yes
MH-75	JUNCTION	83.32	4.84	0.0	
MH-76	JUNCTION	83.16	4.96	0.0	
MH-77	JUNCTION	85.44	3.04	0.0	Yes
MH-79	JUNCTION	85.27	3.13	0.0	Yes
MH-8	JUNCTION	87.00	2.80	0.0	Yes
MH-81	JUNCTION	85.13	3.21	0.0	Yes
MH-82	JUNCTION	82.94	5.32	0.0	
MH-83	JUNCTION	84.20	2.80	0.0	Yes
MH-84	JUNCTION	82.69	4.34	0.0	
MH-86	JUNCTION	81.61	4.30	0.0	Yes
MH-87	JUNCTION	76.57	3.71	1.0	Yes
MH-89	JUNCTION	81.44	2.88	0.0	Yes
MH-9	JUNCTION	86.26	3.54	0.0	Yes
MH-90	JUNCTION	84.05	2.80	0.0	Yes
MH-91	JUNCTION	80.53	3.75	0.0	Yes
MH-92	JUNCTION	78.24	3.07	0.0	Yes
MH-93	JUNCTION	77.50	3.26	0.0	Yes
MH-94	JUNCTION	76.27	4.10	1.0	
MH-95	JUNCTION	76.02	5.11	0.0	
MH-96	JUNCTION	81.57	2.80	0.0	Yes
MH-97	JUNCTION	79.99	3.09	0.0	Yes
MH-98	JUNCTION	79.26	2.84	0.0	Yes

MH-99	JUNCTION	78.43	2.73	0.0
MH-HW1	OUTFALL	82.62	1.65	0.0
OF1	OUTFALL	75.83	1.05	0.0

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Link Summary

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Name Slope	From Node	To Node	Type	Length	%
STM-101-105	MH-101	MH-105	CONDUIT	17.5	
0.3029	0.0130				
STM-10-13	MH-10	MH-13	CONDUIT	83.5	
0.2000	0.0130				
STM-102-103	MH-102	MH-103	CONDUIT	70.0	
4.0032	0.0130				
STM-103-104	MH-103	MH-104	CONDUIT	43.0	
4.0032	0.0130				
STM-104-105	MH-104	MH-105	CONDUIT	66.5	
1.2001	0.0130				
STM-105-OF1	MH-105	OF1	CONDUIT	20.0	
0.3000	0.0130				
STM-11-13	MH-11	MH-13	CONDUIT	92.5	
0.7006	0.0130				
STM-1-2	MH-1	MH-2	CONDUIT	73.0	
0.3507	0.0130				
STM-13-16	MH-13	MH-16	CONDUIT	76.0	
0.2000	0.0130				
STM-14-15	MH-14	MH-15	CONDUIT	74.0	
0.2000	0.0130				
STM-14-33	MH-14	MH-33	CONDUIT	15.5	
0.3484	0.0130				
STM-15-16	MH-15	MH-16	CONDUIT	68.5	
0.2496	0.0130				
STM-16-37	MH-16	MH-37	CONDUIT	88.0	
0.1500	0.0130				
STM-17-18	MH-17	MH-18	CONDUIT	50.5	
0.3505	0.0130				
STM-18-19	MH-18	MH-19	CONDUIT	13.5	
0.3482	0.0130				
STM-19-20	MH-19	MH-20	CONDUIT	63.0	
0.2000	0.0130				
STM-20-21	MH-20	MH-21	CONDUIT	13.5	
0.2000	0.0130				
STM-21-25	MH-21	MH-25	CONDUIT	31.5	
0.2000	0.0130				
STM-22-23	MH-22	MH-23	CONDUIT	56.5	
0.2496	0.0130				
STM-2-3	MH-2	MH-3	CONDUIT	85.0	
0.2000	0.0130				
STM-23-24	MH-23	MH-24	CONDUIT	13.5	
0.2519	0.0130				
STM-24-25	MH-24	MH-25	CONDUIT	25.5	
0.2510	0.0130				
STM-25-26	MH-25	MH-26	CONDUIT	90.0	
0.2000	0.0130				
STM-26-29	MH-26	MH-29	CONDUIT	90.0	
0.2000	0.0130				

STM-27-28	MH-27	MH-28	CONDUIT	92.0
3.4020	0.0130			
STM-27-55	MH-27	MH-55	CONDUIT	76.0
0.3500	0.0130			
STM-28-29	MH-28	MH-29	CONDUIT	97.0
1.6507	0.0130			
STM-29-32	MH-29	MH-32	CONDUIT	86.0
0.3000	0.0130			
STM-30-31	MH-30	MH-31	CONDUIT	118.5
0.3502	0.0130			
STM-31-32	MH-31	MH-32	CONDUIT	118.5
0.4498	0.0130			
STM-32-37	MH-32	MH-37	CONDUIT	86.0
0.7000	0.0130			
STM-33-34	MH-33	MH-34	CONDUIT	77.5
0.2000	0.0130			
STM-34-36	MH-34	MH-36	CONDUIT	74.5
0.2000	0.0130			
STM-36-37	MH-36	MH-37	CONDUIT	64.5
0.1504	0.0130			
STM-37-7	MH-3	MH-7	CONDUIT	52.0
0.2000	0.0130			
STM-37-40	MH-37	MH-40	CONDUIT	76.0
0.4000	0.0130			
STM-38-39	MH-38	MH-39	CONDUIT	61.5
0.2000	0.0130			
STM-38-62	MH-38	MH-62	CONDUIT	15.0
0.5000	0.0130			
STM-39-40	MH-39	MH-40	CONDUIT	60.5
1.1505	0.0130			
STM-40-65	MH-40	MH-65	CONDUIT	88.0
0.2500	0.0130			
STM-41-43	MH-41	MH-43	CONDUIT	35.5
0.3493	0.0130			
STM-43-45	MH-43	MH-45	CONDUIT	105.0
0.2000	0.0130			
STM-45-46	MH-45	MH-46	CONDUIT	30.0
0.2000	0.0130			
STM-46-52	MH-46	MH-52	CONDUIT	15.5
0.2000	0.0130			
STM-47-48	MH-47	MH-48	CONDUIT	31.5
2.8520	0.0130			
STM-47-53	MH-47	MH-53	CONDUIT	74.5
0.2497	0.0130			
STM-48-49	MH-48	MH-49	CONDUIT	55.5
0.9009	0.0130			
STM-49-50	MH-49	MH-50	CONDUIT	118.5
0.2000	0.0130			
STM-50-52	MH-50	MH-52	CONDUIT	10.0
0.2000	0.0130			
STM-52-54	MH-52	MH-54	CONDUIT	75.5
0.1497	0.0130			
STM-53-54	MH-53	MH-54	CONDUIT	81.0
2.0510	0.0130			
STM-54-61	MH-54	MH-61	CONDUIT	105.5
0.2502	0.0130			
STM-55-57	MH-55	MH-57	CONDUIT	94.0
3.4521	0.0130			
STM-5-6	MH-5	MH-6	CONDUIT	76.5
0.2000	0.0130			



STM-14-15	CIRCULAR	0.45	0.16	0.11	0.45	1		STM-40-65	CIRCULAR	1.35	1.43	0.34	1.35	1
127.51							2668.87							
STM-14-33	CIRCULAR	0.30	0.07	0.07	0.30	1	STM-41-43	CIRCULAR	0.30	0.07	0.07	0.30	1	
57.08							57.15							
STM-15-16	CIRCULAR	0.53	0.22	0.13	0.53	1	STM-43-45	CIRCULAR	0.53	0.22	0.13	0.53	1	
214.89							192.34							
STM-16-37	CIRCULAR	0.90	0.64	0.23	0.90	1	STM-45-46	CIRCULAR	0.53	0.22	0.13	0.53	1	
701.17							192.34							
STM-17-18	CIRCULAR	0.30	0.07	0.07	0.30	1	STM-46-52	CIRCULAR	0.53	0.22	0.13	0.53	1	
57.25							192.34							
STM-18-19	CIRCULAR	0.30	0.07	0.07	0.30	1	STM-47-48	CIRCULAR	0.30	0.07	0.07	0.30	1	
57.06							163.32							
STM-19-20	CIRCULAR	0.45	0.16	0.11	0.45	1	STM-47-53	CIRCULAR	0.45	0.16	0.11	0.45	1	
127.51							142.47							
STM-20-21	CIRCULAR	0.45	0.16	0.11	0.45	1	STM-48-49	CIRCULAR	0.30	0.07	0.07	0.30	1	
127.51							91.79							
STM-21-25	CIRCULAR	0.45	0.16	0.11	0.45	1	STM-49-50	CIRCULAR	0.53	0.22	0.13	0.53	1	
127.51							192.34							
STM-22-23	CIRCULAR	0.82	0.53	0.21	0.82	1	STM-50-52	CIRCULAR	0.53	0.22	0.13	0.53	1	
717.13							192.34							
STM-2-3	CIRCULAR	0.45	0.16	0.11	0.45	1	STM-52-54	CIRCULAR	0.68	0.36	0.17	0.68	1	
127.51							325.22							
STM-23-24	CIRCULAR	0.82	0.53	0.21	0.82	1	STM-53-54	CIRCULAR	0.45	0.16	0.11	0.45	1	
720.42							408.34							
STM-24-25	CIRCULAR	0.82	0.53	0.21	0.82	1	STM-54-61	CIRCULAR	0.90	0.64	0.23	0.90	1	
719.17							905.64							
STM-25-26	CIRCULAR	0.97	0.75	0.24	0.97	1	STM-55-57	CIRCULAR	0.30	0.07	0.07	0.30	1	
1002.29							179.68							
STM-26-29	CIRCULAR	0.97	0.75	0.24	0.97	1	STM-5-6	CIRCULAR	0.45	0.16	0.11	0.45	1	
1002.29							127.51							
STM-27-28	CIRCULAR	0.38	0.11	0.09	0.38	1	STM-57-58	CIRCULAR	0.45	0.16	0.11	0.45	1	
323.41							377.27							
STM-27-55	CIRCULAR	0.30	0.07	0.07	0.30	1	STM-58-60	CIRCULAR	0.68	0.36	0.17	0.68	1	
57.21							420.78							
STM-28-29	CIRCULAR	0.45	0.16	0.11	0.45	1	STM-59-60	CIRCULAR	0.38	0.11	0.09	0.38	1	
366.33							96.04							
STM-29-32	CIRCULAR	0.97	0.75	0.24	0.97	1	STM-60-61	CIRCULAR	0.68	0.36	0.17	0.68	1	
1227.55							531.67							
STM-30-31	CIRCULAR	0.60	0.28	0.15	0.60	1	STM-61-65	CIRCULAR	0.90	0.64	0.23	0.90	1	
363.39							1402.36							
STM-31-32	CIRCULAR	0.68	0.36	0.17	0.68	1	STM-62-63	CIRCULAR	0.30	0.07	0.07	0.30	1	
563.79							68.38							
STM-32-37	CIRCULAR	0.97	0.75	0.24	0.97	1	STM-63-64	CIRCULAR	0.38	0.11	0.09	0.38	1	
1875.14							96.04							
STM-33-34	CIRCULAR	0.45	0.16	0.11	0.45	1	STM-64-65	CIRCULAR	0.60	0.28	0.15	0.60	1	
127.51							274.61							
STM-34-36	CIRCULAR	0.53	0.22	0.13	0.53	1	STM-65-67	CIRCULAR	1.50	1.77	0.38	1.50	1	
192.34							3872.02							
STM-36-37	CIRCULAR	0.60	0.28	0.15	0.60	1	STM-66-67	CIRCULAR	0.45	0.16	0.11	0.45	1	
238.13							127.51							
STM-3-7	CIRCULAR	0.45	0.16	0.11	0.45	1	STM-66-68	CIRCULAR	0.30	0.07	0.07	0.30	1	
127.51							57.06							
STM-37-40	CIRCULAR	1.20	1.13	0.30	1.20	1	STM-6-7	CIRCULAR	0.45	0.16	0.11	0.45	1	
2465.93							127.51							
STM-38-39	CIRCULAR	0.45	0.16	0.11	0.45	1	STM-67-71	CIRCULAR	1.65	2.14	0.41	1.65	1	
127.51							4557.51							
STM-38-62	CIRCULAR	0.30	0.07	0.07	0.30	1	STM-68-69	CIRCULAR	0.38	0.11	0.09	0.38	1	
68.38							96.04							
STM-39-40	CIRCULAR	0.45	0.16	0.11	0.45	1	STM-69-70	CIRCULAR	0.38	0.11	0.09	0.38	1	
305.83							96.04							

STM-70-71	CIRCULAR	0.60	0.28	0.15	0.60	1
237.82						
STM-71-73	CIRCULAR	1.65	2.14	0.41	1.65	1
4557.51						
STM-72-73	CIRCULAR	0.30	0.07	0.07	0.30	1
80.98						
STM-72-77	CIRCULAR	0.38	0.11	0.09	0.38	1
96.04						
STM-73-75	CIRCULAR	1.65	2.14	0.41	1.65	1
4567.19						
STM-74-75	CIRCULAR	0.30	0.07	0.07	0.30	1
78.03						
STM-74-79	CIRCULAR	0.30	0.07	0.07	0.30	1
57.21						
STM-75-76	CIRCULAR	1.65	2.14	0.41	1.65	1
4568.61						
STM-76-82	CIRCULAR	1.65	2.14	0.41	1.65	1
4561.21						
STM-77-79	CIRCULAR	0.45	0.16	0.11	0.45	1
127.51						
STM-7-9	CIRCULAR	0.53	0.22	0.13	0.53	1
235.99						
STM-79-81	CIRCULAR	0.53	0.22	0.13	0.53	1
192.34						
STM-81-82	CIRCULAR	0.53	0.22	0.13	0.53	1
183.10						
STM-82-84	CIRCULAR	1.65	2.14	0.41	1.65	1
4557.51						
STM-83-84	CIRCULAR	0.30	0.07	0.07	0.30	1
57.21						
STM-84-HW1	CIRCULAR	1.65	2.14	0.41	1.65	1
4573.19						
STM-86-87	CIRCULAR	0.38	0.11	0.09	0.38	1
330.49						
STM-87-94	CIRCULAR	0.97	0.75	0.24	0.97	1
1227.55						
STM-8-9	CIRCULAR	0.30	0.07	0.07	0.30	1
57.16						
STM-89-91	CIRCULAR	0.38	0.11	0.09	0.38	1
117.62						
STM-90-91	CIRCULAR	0.30	0.07	0.07	0.30	1
191.05						
STM-9-10	CIRCULAR	0.68	0.36	0.17	0.68	1
325.27						
STM-91-92	CIRCULAR	0.38	0.11	0.09	0.38	1
330.51						
STM-92-93	CIRCULAR	0.38	0.11	0.09	0.38	1
330.47						
STM-93-94	CIRCULAR	0.45	0.16	0.11	0.45	1
285.13						
STM-94-95	CIRCULAR	1.05	0.87	0.26	1.05	1
1495.77						
STM-95-101	CIRCULAR	1.05	0.87	0.26	1.05	1
1373.46						
STM-96-97	CIRCULAR	0.30	0.07	0.07	0.30	1
158.93						
STM-97-98	CIRCULAR	0.30	0.07	0.07	0.30	1
135.03						
STM-98-99	CIRCULAR	0.30	0.07	0.07	0.30	1
129.76						

STM-99-101	CIRCULAR	0.38	0.11	0.09	0.38	1
110.90						

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 NOTE: The summary statistics displayed in this report are  
 based on results found at every computational time step,  
 not just on results from each reporting time step.  
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\*\*\*\*\*  
 Analysis Options  
 \*\*\*\*\*  
 Flow Units ..... LPS  
 Process Models:  
 Rainfall/Runoff ..... NO  
 RDII ..... NO  
 Snowmelt ..... NO  
 Groundwater ..... NO  
 Flow Routing ..... YES  
 Ponding Allowed ..... NO  
 Water Quality ..... NO  
 Flow Routing Method ..... DYNWAVE  
 Surcharge Method ..... EXTRAN  
 Starting Date ..... 12/14/2021 00:00:00  
 Ending Date ..... 12/15/2021 00:00:00  
 Antecedent Dry Days ..... 0.0  
 Report Time Step ..... 00:01:00  
 Routing Time Step ..... 1.00 sec  
 Variable Time Step ..... YES  
 Maximum Trials ..... 8  
 Number of Threads ..... 6  
 Head Tolerance ..... 0.000100 m

\*\*\*\*\*  
 Flow Routing Continuity ..... Volume ..... Volume .....  
 hectare-m ..... 10^6 ltr .....  
 \*\*\*\*\*  
 Dry Weather Inflow ..... 0.000 ..... 0.000 .....  
 Wet Weather Inflow ..... 0.000 ..... 0.000 .....  
 Groundwater Inflow ..... 0.000 ..... 0.000 .....  
 RDII Inflow ..... 0.000 ..... 0.000 .....  
 External Inflow ..... 62.205 ..... 622.053 .....  
 External Outflow ..... 62.205 ..... 622.053 .....  
 Flooding Loss ..... 0.000 ..... 0.000 .....  
 Evaporation Loss ..... 0.000 ..... 0.000 .....  
 Exfiltration Loss ..... 0.000 ..... 0.000 .....  
 Initial Stored Volume ..... 0.265 ..... 2.653 .....  
 Final Stored Volume ..... 0.265 ..... 2.648 .....  
 Continuity Error (%) ..... 0.001 .....  
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 Time-Step Critical Elements  
 \*\*\*\*\*  
 None

Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days hr:min	Reported Max Depth Meters
MH-1	JUNCTION	0.41	0.41	87.77	0 17:16	0.41
MH-10	JUNCTION	1.22	1.22	87.32	0 09:45	1.22
MH-101	JUNCTION	1.27	1.27	77.22	0 16:42	1.27
MH-102	JUNCTION	0.10	0.10	85.18	0 00:15	0.10
MH-103	JUNCTION	0.13	0.13	82.02	0 00:00	0.13
MH-104	JUNCTION	0.53	0.53	78.55	0 00:00	0.53
MH-105	JUNCTION	1.16	1.16	77.05	0 23:46	1.16
MH-11	JUNCTION	0.21	0.21	87.50	0 02:26	0.21
MH-13	JUNCTION	1.29	1.29	87.15	0 19:41	1.29
MH-14	JUNCTION	0.59	0.59	87.26	0 01:51	0.59
MH-15	JUNCTION	0.73	0.73	87.18	0 00:45	0.73
MH-16	JUNCTION	1.49	1.49	87.05	0 23:23	1.49
MH-17	JUNCTION	0.19	0.19	88.60	0 04:24	0.19
MH-18	JUNCTION	0.23	0.23	88.42	0 08:47	0.23
MH-19	JUNCTION	0.36	0.36	88.36	0 08:46	0.36
MH-2	JUNCTION	0.71	0.71	87.67	0 12:50	0.71
MH-20	JUNCTION	0.47	0.47	88.31	0 08:46	0.47
MH-21	JUNCTION	0.50	0.50	88.28	0 08:45	0.50
MH-22	JUNCTION	0.71	0.71	88.57	0 08:46	0.71
MH-23	JUNCTION	0.76	0.76	88.45	0 08:46	0.76
MH-24	JUNCTION	0.77	0.77	88.40	0 08:46	0.77
MH-25	JUNCTION	1.02	1.02	88.22	0 08:45	1.02
MH-26	JUNCTION	1.11	1.11	88.11	0 22:43	1.11
MH-27	JUNCTION	0.20	0.20	93.29	0 00:00	0.20
MH-28	JUNCTION	0.30	0.30	89.55	0 00:00	0.30
MH-29	JUNCTION	1.18	1.18	87.90	0 19:38	1.18
MH-3	JUNCTION	0.88	0.88	87.60	0 01:49	0.88
MH-30	JUNCTION	0.40	0.40	88.25	0 08:47	0.40
MH-31	JUNCTION	0.75	0.75	88.11	0 23:23	0.75
MH-32	JUNCTION	1.24	1.24	87.68	0 19:14	1.24
MH-33	JUNCTION	0.63	0.63	87.24	0 20:08	0.63
MH-34	JUNCTION	0.80	0.80	87.18	0 17:12	0.80
MH-36	JUNCTION	0.92	0.92	87.08	0 06:59	0.92
MH-37	JUNCTION	1.84	1.84	86.96	0 20:26	1.84
MH-38	JUNCTION	0.27	0.27	87.32	0 00:02	0.27
MH-39	JUNCTION	0.21	0.21	87.10	0 00:00	0.21
MH-40	JUNCTION	2.01	2.01	86.68	0 11:03	2.01
MH-41	JUNCTION	0.39	0.39	87.66	0 23:26	0.39
MH-43	JUNCTION	0.73	0.73	87.65	0 15:23	0.73
MH-45	JUNCTION	0.88	0.88	87.54	0 23:13	0.88
MH-46	JUNCTION	0.94	0.95	87.51	0 11:08	0.95
MH-47	JUNCTION	0.21	0.21	88.82	0 00:01	0.21
MH-48	JUNCTION	0.50	0.50	88.25	0 11:37	0.50
MH-49	JUNCTION	0.83	0.83	87.83	0 15:28	0.83
MH-5	JUNCTION	0.58	0.58	87.72	0 17:54	0.58
MH-50	JUNCTION	0.81	0.81	87.54	0 22:04	0.81
MH-52	JUNCTION	1.11	1.11	87.50	0 02:29	1.11
MH-53	JUNCTION	0.19	0.19	88.60	0 00:00	0.19
MH-54	JUNCTION	1.27	1.27	87.32	0 23:53	1.27
MH-55	JUNCTION	0.20	0.20	93.06	0 00:23	0.20
MH-57	JUNCTION	0.26	0.26	89.42	0 00:00	0.26
MH-58	JUNCTION	0.70	0.70	87.64	0 13:22	0.70
MH-59	JUNCTION	0.39	0.39	87.50	0 05:56	0.39
MH-6	JUNCTION	0.72	0.72	87.69	0 07:43	0.72
MH-60	JUNCTION	0.80	0.80	87.43	0 07:22	0.80
MH-61	JUNCTION	1.36	1.36	87.12	0 23:51	1.36
MH-62	JUNCTION	0.76	0.76	86.99	0 20:31	0.76
MH-63	JUNCTION	0.88	0.89	86.70	0 06:31	0.88
MH-64	JUNCTION	1.12	1.12	86.67	0 06:06	1.12
MH-65	JUNCTION	2.19	2.19	86.49	0 09:09	2.19
MH-66	JUNCTION	0.65	0.65	86.33	0 20:14	0.65
MH-67	JUNCTION	2.33	2.33	86.25	0 12:33	2.33
MH-68	JUNCTION	0.60	0.60	86.32	0 19:19	0.60
MH-69	JUNCTION	0.70	0.70	86.19	0 18:22	0.70
MH-7	JUNCTION	1.01	1.01	87.55	0 00:06	1.01
MH-70	JUNCTION	0.92	0.92	86.14	0 08:44	0.92
MH-71	JUNCTION	2.37	2.37	86.06	0 14:36	2.37
MH-72	JUNCTION	0.24	0.24	85.91	0 14:58	0.24
MH-73	JUNCTION	2.40	2.40	85.86	0 17:21	2.40
MH-74	JUNCTION	0.15	0.15	85.83	0 10:26	0.15
MH-75	JUNCTION	2.42	2.42	85.74	0 20:53	2.42
MH-76	JUNCTION	2.18	2.18	85.33	0 08:23	2.18
MH-77	JUNCTION	0.31	0.31	85.74	0 11:39	0.31
MH-79	JUNCTION	0.42	0.42	85.69	0 11:35	0.42
MH-8	JUNCTION	0.41	0.41	87.41	0 10:46	0.41
MH-81	JUNCTION	0.48	0.48	85.61	0 11:35	0.48

MH-82	JUNCTION	1.93	1.93	84.88	0	11:19	1.93
MH-83	JUNCTION	0.20	0.20	84.39	0	09:39	0.20
MH-84	JUNCTION	1.66	1.66	84.35	0	17:32	1.66
MH-86	JUNCTION	0.21	0.21	81.82	0	00:17	0.21
MH-87	JUNCTION	1.03	1.03	77.60	0	01:13	1.03
MH-89	JUNCTION	0.23	0.23	81.67	0	00:00	0.23
MH-9	JUNCTION	1.15	1.15	87.41	0	05:06	1.15
MH-90	JUNCTION	0.11	0.11	84.16	0	00:03	0.11
MH-91	JUNCTION	0.20	0.20	80.73	0	00:00	0.20
MH-92	JUNCTION	0.22	0.22	78.46	0	00:00	0.22
MH-93	JUNCTION	0.39	0.39	77.89	0	00:01	0.39
MH-94	JUNCTION	1.17	1.17	77.44	0	11:11	1.17
MH-95	JUNCTION	1.25	1.25	77.27	0	15:36	1.25
MH-96	JUNCTION	0.10	0.10	81.67	0	00:00	0.10
MH-97	JUNCTION	0.14	0.14	80.13	0	00:00	0.14
MH-98	JUNCTION	0.19	0.19	79.45	0	00:00	0.19
MH-99	JUNCTION	0.30	0.30	78.73	0	00:00	0.30
MH-HW1	OUTFALL	1.65	1.65	84.27	0	00:00	1.65
OF1	OUTFALL	1.05	1.05	76.88	0	00:00	1.05

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Node Inflow Summary
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Total	Flow	Maximum	Maximum	Lateral		
Inflow	Balance	Lateral	Total	Time of Max	Inflow	
Volume	Error	Inflow	Inflow	Occurrence	Volume	
Node ltr	Type	LPS	LPS	days hr:min	10^6 ltr	
					10^6	
MH-1 3.15	JUNCTION 0.000	36.41	36.41	0 00:00	3.15	
MH-10 27	JUNCTION 0.000	48.34	312.62	0 20:12	4.18	
MH-101 113	JUNCTION -0.000	0.00	1308.90	0 04:15	0	
MH-102 4.27	JUNCTION 0.000	49.40	49.40	0 00:00	4.27	
MH-103 6.27	JUNCTION -0.000	23.14	72.53	0 00:15	2	
MH-104 99.3	JUNCTION -0.000	1077.01	1149.54	0 00:00	93.1	
MH-105 212	JUNCTION 0.000	0.00	2458.41	0 04:39	0	
MH-11 7.58	JUNCTION 0.000	87.73	87.73	0 00:00	7.58	
MH-13 35.1	JUNCTION 0.000	5.88	406.22	0 13:25	0.508	
MH-14 10.3	JUNCTION -0.000	119.17	119.17	0 00:00	10.3	
MH-15 13.8	JUNCTION -0.000	67.97	160.14	0 12:30	5.87	

MH-16 48.9	-0.000	JUNCTION	0.00	566.34	0 17:50	0
MH-17 3.58	-0.000	JUNCTION	41.38	41.38	0 00:00	3.58
MH-18 4.22	0.000	JUNCTION	7.41	48.79	0 07:39	0.64
MH-19 7.11	0.000	JUNCTION	33.55	82.34	0 18:42	2.9
MH-2 5.99	-0.000	JUNCTION	32.90	69.32	0 01:41	2.84
MH-20 8.74	0.000	JUNCTION	18.78	101.12	0 18:42	1.62
MH-21 8.74	0.000	JUNCTION	0.00	101.12	0 18:42	0
MH-22 52.9	0.000	JUNCTION	612.05	612.05	0 00:00	52.9
MH-23 53.1	0.000	JUNCTION	2.04	614.09	0 09:40	0.177
MH-24 53.1	0.000	JUNCTION	0.00	614.09	0 18:41	0
MH-25 67.5	-0.000	JUNCTION	66.24	781.45	0 18:41	5.72
MH-26 72	0.000	JUNCTION	51.75	833.22	0 11:14	4.47
MH-27 17.4	-0.000	JUNCTION	201.93	201.93	0 00:00	17.4
MH-28 25.2	0.000	JUNCTION	105.35	292.05	0 00:00	9.1
MH-29 97.2	0.000	JUNCTION	0.00	1125.26	0 09:40	0
MH-3 7.52	-0.000	JUNCTION	17.68	87.00	0 03:47	1.53
MH-30 20.8	0.000	JUNCTION	240.26	240.26	0 00:00	20.8
MH-31 38	0.000	JUNCTION	199.54	439.81	0 04:03	17.2
MH-32 135	-0.000	JUNCTION	0.00	1565.07	0 16:38	0
MH-33 6.11	0.000	JUNCTION	43.76	70.80	0 03:34	3.78
MH-34 13.8	-0.000	JUNCTION	89.42	160.21	0 14:09	7.73
MH-36 18.5	-0.000	JUNCTION	53.96	214.16	0 21:31	4.66
MH-37 203	-0.000	JUNCTION	0.00	2345.55	0 22:49	0
MH-38 9.3	0.000	JUNCTION	107.59	107.59	0 00:00	9.3
MH-39 11.9	-0.000	JUNCTION	50.60	137.44	0 00:00	4.37
MH-40 215	0.000	JUNCTION	0.00	2482.99	0 16:05	0
MH-41 1	-0.000	JUNCTION	11.59	11.59	0 00:00	1
MH-43 11	0.000	JUNCTION	116.18	127.77	0 23:13	10
MH-45 11	-0.000	JUNCTION	0.00	127.77	0 08:27	0
MH-46 11	0.000	JUNCTION	0.00	127.78	0 21:51	0

MH-47		JUNCTION	122.48	122.48	0 00:00	10.6
10.6	0.000	JUNCTION	16.24	78.41	0 00:01	1.4
MH-48		JUNCTION	128.72	207.13	0 02:31	11.1
6.77	0.000	JUNCTION	56.28	56.28	0 00:00	4.86
MH-49	-0.000	JUNCTION	0.00	207.14	0 14:11	0
17.9	-0.000	JUNCTION	95.09	155.40	0 00:00	8.22
MH-50	0.000	JUNCTION	295.62	785.94	0 19:57	25.5
17.9	0.000	JUNCTION	120.62	135.86	0 00:00	10.4
MH-51		JUNCTION	109.41	245.27	0 00:23	9.45
21.2	-0.000	JUNCTION	96.04	341.31	0 00:00	8.3
MH-52	-0.000	JUNCTION	57.93	57.93	0 00:00	5.01
28.9	-0.000	JUNCTION	48.05	104.34	0 08:29	4.15
MH-53		JUNCTION	22.76	422.03	0 13:58	1.97
13.4	-0.000	JUNCTION	0.00	1207.95	0 22:43	0
MH-54	-0.000	JUNCTION	40.64	61.39	0 00:02	3.51
67.9	0.000	JUNCTION	9.21	70.62	0 04:28	0.796
MH-55		JUNCTION	138.20	208.82	0 07:09	11.9
11.7	0.000	JUNCTION	0.00	3899.71	0 01:46	0
MH-56	-0.000	JUNCTION	107.59	107.59	0 00:00	9.3
5.3	0.000	JUNCTION	296.71	4277.33	0 22:38	25.6
MH-57		JUNCTION	47.03	73.74	0 16:58	4.06
9.01	-0.000	JUNCTION	11.08	84.81	0 16:58	0.957
MH-58	-0.000	JUNCTION	1.15	192.49	0 07:09	0.0992
29.5	-0.000	JUNCTION	86.90	171.73	0 20:53	7.51
MH-59		JUNCTION	0.00	4449.03	0 12:19	0
5.01	0.000	JUNCTION	94.35	94.35	0 00:00	8.15
MH-60	-0.000	JUNCTION	0.00	4481.83	0 00:08	0
36.5	-0.000	JUNCTION	66.21	66.21	0 00:00	5.72
MH-61		JUNCTION	0.00	4520.72	0 08:19	0
104	-0.000	JUNCTION				
MH-62		JUNCTION				
5.3	0.000	JUNCTION				
MH-63		JUNCTION				
6.1	0.000	JUNCTION				
MH-64		JUNCTION				
18	-0.000	JUNCTION				
MH-65		JUNCTION				
337	-0.000	JUNCTION				
MH-66		JUNCTION				
9.3	-0.000	JUNCTION				
MH-67		JUNCTION				
370	-0.000	JUNCTION				
MH-68		JUNCTION				
6.37	0.000	JUNCTION				
MH-69		JUNCTION				
7.33	0.000	JUNCTION				
MH-70		JUNCTION				
16.6	0.000	JUNCTION				
MH-71	-0.000	JUNCTION				
384	0.000	JUNCTION				
MH-72		JUNCTION				
8.15	-0.000	JUNCTION				
MH-73		JUNCTION				
387	-0.000	JUNCTION				
MH-74		JUNCTION				
5.72	-0.000	JUNCTION				
MH-75		JUNCTION				
391	0.000	JUNCTION				

Node	Type	Hours Surcharged	Max. Height Above Crown Meters	Min. Depth Below Rim Meters
MH-76	JUNCTION	0.00	4520.65	0 14:30 0
391	JUNCTION	27.32	88.88	0 14:58 2.36
MH-77	JUNCTION	23.67	139.95	0 13:03 2.05
7.68	JUNCTION	8.28	8.28	0 00:00 0.715
MH-79	JUNCTION	50.98	190.93	0 11:35 4.4
12.1	JUNCTION	407	4711.55	0 07:17 0
MH-80	JUNCTION	29.79	29.79	0 00:00 2.57
0.715	JUNCTION	0.00	4741.30	0 11:19 0
MH-81	JUNCTION	201.93	201.93	0 00:00 17.4
16.5	JUNCTION	17.4	0.000	
MH-82	JUNCTION	796.60	998.53	0 00:03 68.8
407	JUNCTION	71.17	71.17	0 00:00 6.15
MH-83	JUNCTION	63.50	264.29	0 18:28 5.49
2.57	JUNCTION	4.72	0.000	
MH-84	JUNCTION	54.62	54.62	0 00:00 4.72
410	JUNCTION	55.22	181.01	0 00:00 4.77
MH-85	JUNCTION	14.07	195.08	0 00:00 1.22
17.4	JUNCTION	16.9	0.000	
MH-86	JUNCTION	22.31	217.40	0 00:00 1.93
86.3	JUNCTION	0.00	1215.95	0 00:49 0
MH-87	JUNCTION	0.00	1215.96	0 04:51 0
6.15	JUNCTION	3.43	-0.000	
MH-88	JUNCTION	22.08	61.80	0 00:00 1.91
15.6	JUNCTION	31.12	92.92	0 00:00 2.69
MH-89	JUNCTION	8.03	0.000	
16.9	JUNCTION	8.03	0.000	
MH-90	JUNCTION	0.00	92.92	0 00:00 0
105	JUNCTION	410	4741.30	0 11:19 0
MH-91	OUTFALL	0.00	2458.41	0 16:42 0
105	OUTFALL	212	0.000	
MH-92	JUNCTION	39.72	39.72	0 00:00 3.43
105	JUNCTION	5.34	-0.000	
MH-93	JUNCTION	8.03	0.000	
18.8	JUNCTION	4.03	0.000	
MH-94	JUNCTION	22.08	61.80	0 00:00 0
105	JUNCTION	31.12	92.92	0 00:00 0
MH-95	JUNCTION	8.03	0.000	
105	JUNCTION	8.03	0.000	
MH-96	JUNCTION	0.00	92.92	0 00:00 0
3.43	JUNCTION	410	4741.30	0 11:19 0
MH-97	JUNCTION	0.00	2458.41	0 16:42 0
5.34	JUNCTION	212	0.000	
MH-98	JUNCTION	39.72	39.72	0 00:00 0
8.03	JUNCTION	5.34	-0.000	
MH-99	JUNCTION	8.03	0.000	
8.03	JUNCTION	410	4741.30	0 11:19 0
MH-HW1	OUTFALL	0.00	2458.41	0 16:42 0
OF1	OUTFALL	212	0.000	
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Node Surcharge Summary				
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Surcharging occurs when water rises above the top of the highest conduit.				
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MH-1	JUNCTION	24.00	0.109	2.390
MH-10	JUNCTION	24.00	0.522	2.351
MH-13	JUNCTION	24.00	0.130	2.388
MH-14	JUNCTION	24.00	0.138	2.361
MH-15	JUNCTION	24.00	0.209	2.338
MH-16	JUNCTION	24.00	0.248	2.380
MH-2	JUNCTION	24.00	0.262	2.383
MH-21	JUNCTION	24.00	0.019	2.756
MH-26	JUNCTION	24.00	0.115	2.653
MH-3	JUNCTION	24.00	0.369	2.326
MH-31	JUNCTION	24.00	0.067	2.463
MH-32	JUNCTION	24.00	0.181	2.341
MH-33	JUNCTION	24.00	0.177	2.356
MH-34	JUNCTION	24.00	0.272	2.316
MH-36	JUNCTION	24.00	0.317	2.310
MH-37	JUNCTION	24.00	0.153	2.338
MH-40	JUNCTION	24.00	0.039	2.497
MH-41	JUNCTION	24.00	0.087	2.409
MH-43	JUNCTION	24.00	0.205	2.365
MH-45	JUNCTION	24.00	0.299	2.321
MH-46	JUNCTION	24.00	0.391	2.289
MH-48	JUNCTION	24.00	0.156	2.538
MH-49	JUNCTION	24.00	0.281	2.255
MH-5	JUNCTION	24.00	0.131	2.366
MH-50	JUNCTION	24.00	0.254	2.255
MH-52	JUNCTION	24.00	0.255	2.284
MH-54	JUNCTION	24.00	0.120	2.403
MH-59	JUNCTION	24.00	0.018	2.484
MH-6	JUNCTION	24.00	0.254	2.286
MH-60	JUNCTION	24.00	0.046	2.457
MH-61	JUNCTION	24.00	0.162	2.393
MH-63	JUNCTION	24.00	0.510	2.105
MH-64	JUNCTION	24.00	0.520	2.114
MH-65	JUNCTION	24.00	0.350	2.111
MH-66	JUNCTION	24.00	0.190	2.306
MH-67	JUNCTION	24.00	0.276	2.236
MH-68	JUNCTION	24.00	0.224	2.309
MH-69	JUNCTION	24.00	0.299	2.331
MH-7	JUNCTION	24.00	0.300	2.305
MH-70	JUNCTION	24.00	0.324	2.358
MH-71	JUNCTION	24.00	0.354	2.305
MH-73	JUNCTION	24.00	0.138	2.374
MH-75	JUNCTION	24.00	0.089	2.423
MH-76	JUNCTION	24.00	0.466	2.786
MH-8	JUNCTION	24.00	0.112	2.390
MH-87	JUNCTION	24.00	0.048	2.684
MH-9	JUNCTION	24.00	0.241	2.392
MH-95	JUNCTION	24.00	0.175	3.859

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Node Flooding Summary
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No nodes were flooded.

Outfall Loading Summary						
Outfall Node	Flow Freq Pcnt	Avg Flow LPS	Max Flow LPS	Total Volume 10^6 ltr	Max/ Full	Max/ Full
MH-HWL	100.00	4741.27	4741.30	409.646		
OF1	100.00	2458.39	2458.41	212.405		
System	100.00	7199.67	7199.70	622.051		

Link Flow Summary						
Link	Type	Maximum  Flow  LPS	Time of Occurrence days	Max/  Veloc  m/sec	Max/ Full Flow	Max/ Depth
STM-101-105	CONDUIT	1308.87	0 04:39	1.51	0.87	1.00
STM-10-13	CONDUIT	312.62	0 13:25	0.87	0.83	1.00
STM-102-103	CONDUIT	49.40	0 00:15	2.28	0.26	0.35
STM-103-104	CONDUIT	72.53	0 00:00	2.53	0.37	0.43
STM-104-105	CONDUIT	1149.54	0 00:00	3.20	0.73	0.64
STM-105-OF1	CONDUIT	2458.41	0 16:42	2.84	1.64	1.00
STM-11-13	CONDUIT	87.73	0 00:18	0.95	0.60	0.78
STM-1-2	CONDUIT	36.42	0 01:41	0.52	0.64	1.00
STM-13-16	CONDUIT	406.21	0 17:54	0.92	0.82	1.00
STM-14-15	CONDUIT	92.17	0 12:30	0.58	0.72	1.00
STM-14-33	CONDUIT	27.04	0 03:34	0.38	0.47	1.00
STM-15-16	CONDUIT	160.14	0 20:22	0.74	0.75	1.00
STM-16-37	CONDUIT	566.34	0 14:35	0.89	0.81	1.00
STM-17-18	CONDUIT	41.38	0 07:39	0.84	0.72	0.65
STM-18-19	CONDUIT	48.79	0 18:42	0.88	0.86	0.73
STM-19-20	CONDUIT	82.34	0 18:42	0.55	0.65	0.89
STM-20-21	CONDUIT	101.12	0 18:42	0.64	0.79	1.00
STM-21-25	CONDUIT	101.12	0 04:23	0.64	0.79	1.00
STM-22-23	CONDUIT	612.05	0 09:40	1.24	0.85	0.87
STM-2-3	CONDUIT	69.33	0 03:47	0.44	0.54	1.00
STM-23-24	CONDUIT	614.09	0 18:41	1.21	0.85	0.91
STM-24-25	CONDUIT	614.09	0 18:41	1.26	0.85	0.86
STM-25-26	CONDUIT	781.47	0 11:14	1.05	0.78	1.00
STM-26-29	CONDUIT	833.21	0 09:40	1.12	0.83	1.00
STM-27-28	CONDUIT	186.70	0 00:00	3.03	0.58	0.55
STM-27-55	CONDUIT	15.24	0 00:00	0.57	0.27	0.40
STM-28-29	CONDUIT	292.05	0 00:00	2.55	0.80	0.68
STM-29-32	CONDUIT	1125.27	0 21:41	1.51	0.92	1.00
STM-30-31	CONDUIT	240.27	0 04:03	0.96	0.66	0.83
STM-31-32	CONDUIT	439.81	0 17:50	1.23	0.78	1.00
STM-32-37	CONDUIT	1565.07	0 05:21	2.10	0.83	1.00
STM-33-34	CONDUIT	70.79	0 14:09	0.45	0.56	1.00

STM-34-36	CONDUIT	160.21	0	21:31	0.74	0.83	1.00
STM-36-37	CONDUIT	214.16	0	06:21	0.76	0.90	1.00
STM-3-7	CONDUIT	87.01	0	20:32	0.55	0.68	1.00
STM-37-40	CONDUIT	2345.56	0	16:05	2.07	0.95	1.00
STM-38-39	CONDUIT	86.84	0	00:00	1.03	0.68	0.52
STM-38-62	CONDUIT	20.75	0	00:02	0.83	0.30	0.38
STM-39-40	CONDUIT	137.44	0	00:00	1.10	0.45	0.74
STM-40-65	CONDUIT	2482.98	0	04:20	1.73	0.93	1.00
STM-41-43	CONDUIT	11.59	0	23:13	0.16	0.20	1.00
STM-43-45	CONDUIT	127.77	0	08:27	0.59	0.66	1.00
STM-45-46	CONDUIT	127.78	0	21:51	0.59	0.66	1.00
STM-46-52	CONDUIT	127.80	0	21:51	0.59	0.66	1.00
STM-47-48	CONDUIT	62.17	0	00:01	1.15	0.38	0.71
STM-47-53	CONDUIT	60.31	0	00:00	0.94	0.42	0.42
STM-48-49	CONDUIT	78.41	0	02:31	1.11	0.85	1.00
STM-49-50	CONDUIT	207.14	0	14:11	0.96	1.08	1.00
STM-50-52	CONDUIT	207.16	0	04:41	0.96	1.08	1.00
STM-52-54	CONDUIT	334.92	0	19:57	0.94	1.03	1.00
STM-53-54	CONDUIT	155.40	0	00:00	1.28	0.38	0.71
STM-54-61	CONDUIT	785.95	0	22:43	1.24	0.87	1.00
STM-55-57	CONDUIT	135.86	0	00:23	2.79	0.76	0.65
STM-5-6	CONDUIT	56.28	0	08:29	0.35	0.44	1.00
STM-57-58	CONDUIT	245.27	0	00:00	2.52	0.65	0.59
STM-58-60	CONDUIT	341.33	0	13:58	0.95	0.81	1.00
STM-59-60	CONDUIT	57.94	0	01:53	0.52	0.60	1.00
STM-60-61	CONDUIT	422.03	0	02:22	1.18	0.79	1.00
STM-61-65	CONDUIT	1207.95	0	16:41	1.90	0.86	1.00
STM-62-63	CONDUIT	61.40	0	04:28	0.87	0.90	1.00
STM-63-64	CONDUIT	70.62	0	07:09	0.64	0.74	1.00
STM-64-65	CONDUIT	208.82	0	18:15	0.74	0.76	1.00
STM-65-67	CONDUIT	3899.72	0	22:38	2.21	1.01	1.00
STM-66-67	CONDUIT	80.91	0	19:09	0.51	0.63	1.00
STM-66-68	CONDUIT	26.71	0	16:58	0.38	0.47	1.00
STM-6-7	CONDUIT	104.34	0	08:01	0.66	0.82	1.00
STM-67-71	CONDUIT	4277.34	0	12:19	2.00	0.94	1.00
STM-68-69	CONDUIT	73.73	0	16:58	0.67	0.77	1.00
STM-69-70	CONDUIT	84.83	0	20:53	0.77	0.88	1.00
STM-70-71	CONDUIT	171.71	0	13:28	0.61	0.72	1.00
STM-71-73	CONDUIT	4449.04	0	00:08	2.08	0.98	1.00
STM-72-73	CONDUIT	32.79	0	17:29	0.54	0.40	0.79
STM-72-77	CONDUIT	61.56	0	14:58	0.84	0.64	0.63
STM-73-75	CONDUIT	4481.92	0	08:19	2.10	0.98	1.00
STM-74-75	CONDUIT	38.81	0	05:20	0.68	0.50	0.75
STM-74-79	CONDUIT	27.40	0	10:26	0.66	0.48	0.57
STM-75-76	CONDUIT	4520.65	0	14:30	2.11	0.99	1.00
STM-76-82	CONDUIT	4520.63	0	07:17	2.11	0.99	1.00
STM-77-79	CONDUIT	88.88	0	14:59	0.71	0.70	0.73
STM-7-9	CONDUIT	192.51	0	18:28	0.89	0.82	1.00
STM-79-81	CONDUIT	139.95	0	11:35	0.75	0.73	0.81
STM-81-82	CONDUIT	190.93	0	11:35	1.11	1.04	0.74
STM-82-84	CONDUIT	4711.51	0	11:19	2.21	1.03	0.98
STM-83-84	CONDUIT	29.79	0	10:26	0.59	0.52	0.68
STM-84-HW1	CONDUIT	4741.30	0	11:19	2.22	1.04	1.00
STM-86-87	CONDUIT	201.93	0	00:03	2.18	0.61	0.78
STM-87-94	CONDUIT	998.55	0	00:49	1.34	0.81	1.00
STM-8-9	CONDUIT	8.29	0	18:35	0.12	0.14	1.00
STM-89-91	CONDUIT	71.17	0	00:00	1.10	0.61	0.57

STM-90-91	CONDUIT	54.62	0	00:03	2.33	0.29	0.37			
STM-9-10	CONDUIT	264.28	0	20:12	0.74	0.81	1.00			
STM-91-92	CONDUIT	181.01	0	00:00	3.04	0.55	0.53			
STM-92-93	CONDUIT	195.08	0	00:00	3.02	0.59	0.57			
STM-93-94	CONDUIT	217.40	0	00:01	1.68	0.76	0.76			
STM-94-95	CONDUIT	1215.96	0	04:51	1.40	0.81	1.00			
STM-95-101	CONDUIT	1215.98	0	04:15	1.40	0.89	1.00			
STM-96-97	CONDUIT	39.72	0	00:00	1.86	0.25	0.34			
STM-97-98	CONDUIT	61.80	0	00:00	1.79	0.46	0.49			
STM-98-99	CONDUIT	92.92	0	00:00	1.80	0.72	0.69			
STM-99-101	CONDUIT	92.92	0	00:01	1.13	0.84	0.70			
***** Flow Classification Summary *****										
-----										
----- Adjusted ----- Fraction of Time in Flow Class -----										
----- /Actual Up Down Sub Sup Up Down Norm -----										
Inlet	Conduit	Length	Dry	Dry	Dry	Crit	Crit	Crit	Crit	Ltd
Ctrl										
-----	STM-101-105	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-10-13	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-102-103	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00
0.00	STM-103-104	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00
0.00	STM-104-105	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00
0.00	STM-105-OF1	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-11-13	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00
0.00	STM-1-2	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-13-16	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-14-15	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-14-33	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-15-16	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-16-37	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-17-18	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-18-19	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-19-20	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00

STM-20-21	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
0.00	STM-21-25	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-22-23	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-2-3	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-23-24	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-24-25	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-25-26	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-26-29	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-27-28	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00
0.00	STM-27-55	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00
0.00	STM-28-29	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00
0.00	STM-29-32	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-30-31	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-31-32	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-32-37	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-33-34	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-34-36	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-36-37	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-3-7	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-37-40	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-38-39	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00
0.00	STM-38-62	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00
0.00	STM-39-40	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00
0.00	STM-40-65	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-41-43	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-43-45	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-45-46	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-46-52	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00	STM-47-48	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00
0.00	STM-47-53	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00

STM-75-76	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
0.00										
STM-76-82	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
0.00										
STM-77-79	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
0.00										
STM-7-9	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
0.00										
STM-79-81	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
0.00										
STM-81-82	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
0.00										
STM-82-84	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
0.00										
STM-83-84	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
0.00										
STM-84-HW1	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
0.00										
STM-86-87	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	1.00	0.00
0.00										
STM-87-94	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
0.00										
STM-8-9	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
0.00										
STM-89-91	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
0.00										
STM-90-91	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
0.00										
STM-9-10	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
0.00										
STM-91-92	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
0.00										
STM-92-93	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
0.00										
STM-93-94	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
0.00										
STM-94-95	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
0.00										
STM-95-101	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
0.00										
STM-96-97	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
0.00										
STM-97-98	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	1.00	0.00
0.00										
STM-98-99	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	1.00	0.00
0.00										
STM-99-101	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
0.00										
*****Conduit Surcharge Summary*****										
----- Hours Full ----- Hours Above Full Capacity										
Conduit		Both Ends	Upstream	Dnstream	Normal Flow	Limited				
-----										

STM-101-105	24.00	24.00	24.00	0.01	24.00
STM-10-13	24.00	24.00	24.00	0.01	14.93
STM-105-OF1	24.00	24.00	24.00	24.00	24.00
STM-11-13	0.01	0.01	24.00	0.01	0.01
STM-1-2	24.00	24.00	24.00	0.01	0.01
STM-13-16	24.00	24.00	24.00	0.01	0.01
STM-14-15	24.00	24.00	24.00	0.01	0.01
STM-14-33	24.00	24.00	24.00	0.01	0.01
STM-15-16	24.00	24.00	24.00	0.01	0.01
STM-16-37	24.00	24.00	24.00	0.01	0.01
STM-20-21	24.00	24.00	24.00	0.01	0.01
STM-21-25	24.00	24.00	24.00	0.01	24.00
STM-2-3	24.00	24.00	24.00	0.01	0.01
STM-25-26	24.00	24.00	24.00	0.01	0.01
STM-26-29	24.00	24.00	24.00	0.01	24.00
STM-29-32	24.00	24.00	24.00	0.01	0.01
STM-30-31	0.01	0.01	24.00	0.01	0.01
STM-31-32	24.00	24.00	24.00	0.01	0.01
STM-32-37	24.00	24.00	24.00	0.01	24.00
STM-33-34	24.00	24.00	24.00	0.01	0.01
STM-34-36	24.00	24.00	24.00	0.01	0.01
STM-36-37	24.00	24.00	24.00	0.01	24.00
STM-3-7	24.00	24.00	24.00	0.01	0.01
STM-37-40	24.00	24.00	24.00	0.01	0.01
STM-39-40	0.01	0.01	24.00	0.01	0.01
STM-40-65	24.00	24.00	24.00	0.01	0.01
STM-41-43	24.00	24.00	24.00	0.01	0.01
STM-43-45	24.00	24.00	24.00	0.01	0.01
STM-45-46	24.00	24.00	24.00	0.01	0.01
STM-46-52	24.00	24.00	24.00	0.01	0.01
STM-47-48	0.01	0.01	24.00	0.01	0.01
STM-48-49	24.00	24.00	24.00	0.01	0.01
STM-49-50	24.00	24.00	24.00	24.00	24.00
STM-50-52	24.00	24.00	24.00	24.00	24.00
STM-52-54	24.00	24.00	24.00	24.00	24.00
STM-53-54	0.01	0.01	24.00	0.01	0.01
STM-54-61	24.00	24.00	24.00	0.01	0.01
STM-5-6	24.00	24.00	24.00	0.01	0.01
STM-58-60	24.00	24.00	24.00	0.01	0.01
STM-59-60	24.00	24.00	24.00	0.01	0.01
STM-60-61	24.00	24.00	24.00	0.01	0.01
STM-61-65	24.00	24.00	24.00	0.01	24.00
STM-62-63	24.00	24.00	24.00	0.01	0.01
STM-63-64	24.00	24.00	24.00	0.01	0.01
STM-64-65	24.00	24.00	24.00	0.01	0.01
STM-65-67	24.00	24.00	24.00	24.00	24.00
STM-66-67	24.00	24.00	24.00	0.01	0.01
STM-66-68	24.00	24.00	24.00	0.01	0.01
STM-6-7	24.00	24.00	24.00	0.01	0.01
STM-67-71	24.00	24.00	24.00	0.01	0.01
STM-68-69	24.00	24.00	24.00	0.01	0.01
STM-69-70	24.00	24.00	24.00	0.01	24.00
STM-70-71	24.00	24.00	24.00	0.01	0.01
STM-71-73	24.00	24.00	24.00	0.01	0.01
STM-72-73	0.01	0.01	24.00	0.01	0.01
STM-73-75	24.00	24.00	24.00	0.01	13.07
STM-74-75	0.01	0.01	24.00	0.01	0.01

STM-75-76	24.00	24.00	24.00	0.01	24.00
STM-76-82	24.00	24.00	24.00	0.01	24.00
STM-7-9	24.00	24.00	24.00	0.01	24.00
STM-81-82	0.01	0.01	0.01	24.00	0.01
STM-82-84	0.01	24.00	0.01	24.00	0.01
STM-84-HW1	24.00	24.00	24.00	24.00	24.00
STM-86-87	0.01	0.01	24.00	0.01	0.01
STM-87-94	24.00	24.00	24.00	0.01	0.01
STM-8-9	24.00	24.00	24.00	0.01	0.01
STM-9-10	24.00	24.00	24.00	0.01	0.01
STM-94-95	24.00	24.00	24.00	0.01	0.01
STM-95-101	24.00	24.00	24.00	0.01	24.00

Analysis begun on: Tue Dec 14 16:02:14 2021

Analysis ended on: Tue Dec 14 16:02:24 2021

Total elapsed time: 00:00:10



Ottawa. ON  
Paris. ON  
Gatineau. QC  
Montréal. QC  
Québec. QC

# Attachment D

Cox Country Road Culvert Analysis

Area ID	Area (ha)	Soil Description	Soil Group	Land Use Description	CN	CN*	Tp (h)
eCCR	74.3	F1, G4, R3	B / BC / D	50% B = 70% Woods, 30% Farm; 40% BC = 15% Imp, 25% Woods, 60% Urban Lawn; 10% D = 15% Imp, 15% Woods, 70% Urban Lawn	71.525	61	1.29

As per Ontario Soil Map 58 and the MTO Manual:

Short ID	Soil Description	Soil Group
F1	Farmington, fine sandy loam or sandy loam or loam, good drainage	B
G4	Grenville, sandy loam or loam or silt loam, mix of good and imperfect drainage	BC
R1	Rideau, silty clay or clay, imperfect drainage	D
R3	Rideau, silty clay or clay, poor drainage	D
X1	Escarpment, marine clay or heavy clay	D
X3	Escarpment, limestone or dolomite or sandstone scarps	D

## Calculation of Time to Peak (Tp)

EXISTING CONDITIONS		
UNITS Metric	eCCR metric	
Area	(ha)	74.3
Hydrologic Soil Group <sup>1</sup>		B / BC / D
CN <sup>2</sup>		72
C (as per Rational Method) <sup>3</sup>		0.25
Length of Channel <sup>4</sup>	(m)	1997
Elevation of Channel Outlet	(m)	87.31
Elevation of Channel Headwater	(m)	111.5
Average Slope of Channel	(m/m)	0.0121
Time to Peak (=2/3 Tc)		
Kirpich	(min)	25
FAA	(min)	77
SCS	(min)	111
Brainby Williams	(min)	48
		1.29

### NOTES:

- 1- As per Ontario Soil Map
- 2- See CN C spreadsheet for detail
- 3- See CN C spreadsheet for detail
- 4- As measured on topographic map provided by DSEL



### Tc Equations applicability

Kirpich	Best for rural watersheds with slopes ranging from 3% to 10%
FAA	Best for flat drainage areas (was developed for air field drainage) but used frequently for urban watersheds
SCS	Best for Agricultural SW in general and urban SW < 2000 acres
BW	One of the best method for predicting Tc. Especially good for small culvert design

### Tc Equations and inputs

(imperial unless otherwise noted)

Result  
in      input L as

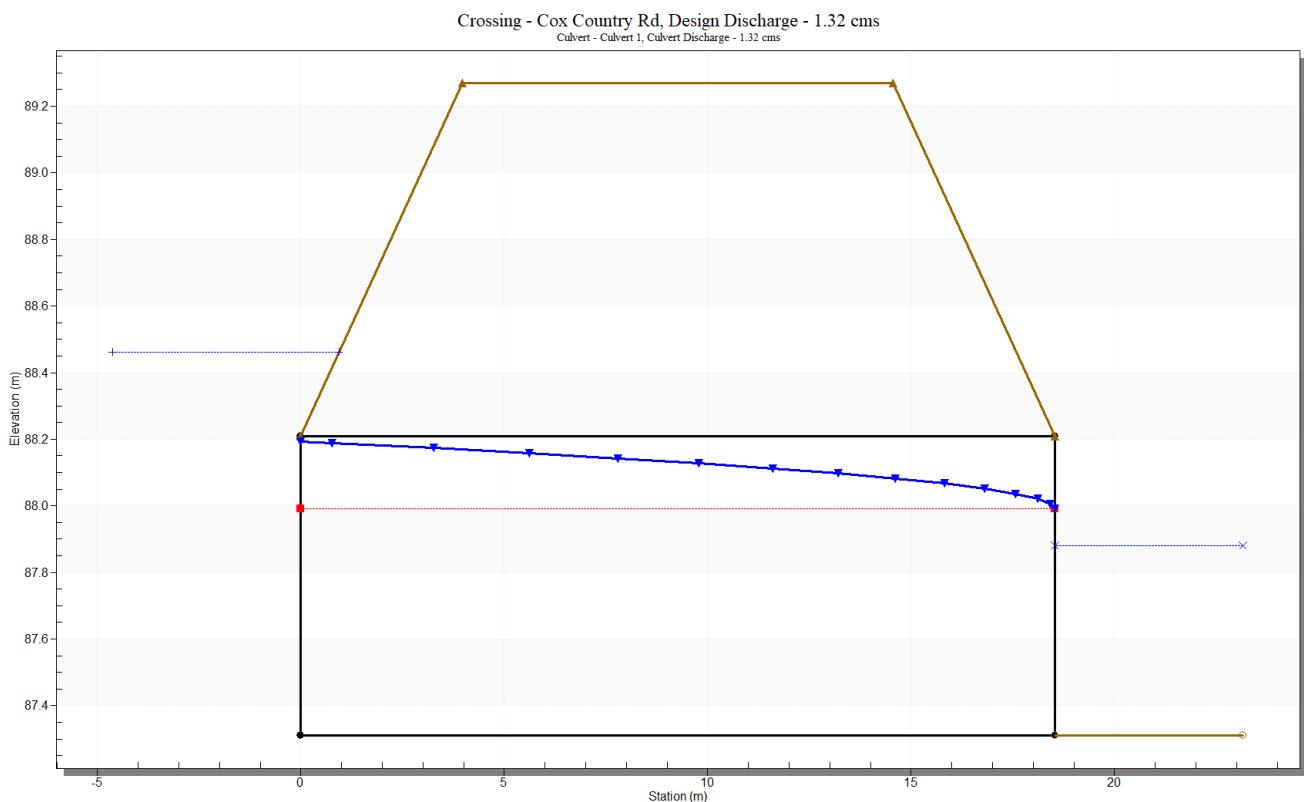
Kirpich	$Tc = 0.0078 L^{0.77} S^{-0.385}$	(min)	(ft)
FAA	$Tc = (1.8(1.1-C)L^{0.50}) / (S^{0.333})$	(min)	(ft)
SCS Lag	$Tc = (100L^{0.8}((1000/CN)-9)^{0.7} / (1900 S^{0.5}))$	(min)	(ft)
BW (metr)	$Tc = (0.605L) / (S^{0.2} A^{0.1})$	(hrs)	(km)

# HY-8 Analysis Results

## Crossing Summary Table

Culvert Crossing: Cox Country Rd

Headwater Elevation (m)	Total Discharge (cms)	Culvert 1 Discharge (cms)	Roadway Discharge (cms)	Iterations
87.31	0.00	0.00	0.00	1
87.63	0.13	0.13	0.00	1
87.76	0.26	0.26	0.00	1
87.87	0.40	0.40	0.00	1
87.96	0.53	0.53	0.00	1
88.05	0.66	0.66	0.00	1
88.13	0.79	0.79	0.00	1
88.21	0.93	0.93	0.00	1
88.29	1.06	1.06	0.00	1
88.37	1.19	1.19	0.00	1
88.46	1.32	1.32	0.00	1
89.27	2.28	2.28	0.00	Overtopping



```

00001+ 20 * Metric units / ID Numbers OFI
00002+ 20 * NWS-NOHRP Version 0.52 Jan 2004 / INPUT DATA FILE
00003+ 20 * Project Name : [Cardinal Creek Village]
00004+ 20 * Project Number : [1234567890]
00005+ 20 * Date : 2021/07/07
00006+ 20 * Modeler : Laura Kripke, P.Eng.
00007+ 20 * Organization : [Kipp & Associates]
00008+ 20 * License # : 2582634
00011+ 20 * 25-Year - 3-hour Chicago Storm
00013+ START TZERO=[0.0], METOUT=[2], NNRUN=[025]
00014+ ["025YCH3.stm"] <- storm filename, one per line for NSTM0 time
00015+ ["025YCH3.stm"] <- storm filename, one per line for NSTM0 time
00016+ READ STORM STORM_FILENAME=[["storm_001"]]
00017+ ["025YCH3.stm"] <- storm filename, one per line for NSTM0 time
00018+ DEFAULT VALUES ICASDefd[1], read and print values
00019+ DEFVAL_FILNAMES=[["Ottawa_val.vsl"]]
00020+ FINISH
00021+ * CN to CN* based on Ontario Soil Map Nov. 1985 MTO Manual Chart H2-6A,
00022+ * Lidar data, May 2009 SWMFO USGS's Manual, air photos, assume good condition
00023+ * 25-Year - 3-hour Chicago Storm
00024+ * Ties to Peak = 2 / 3 of FA TC
00025+ ##### Existing Drainage from Subject Site to Ottawa River#####
00026+ * Existing Drainage from Subject Site to Ottawa River
00027+ DESIGN RASHD##### Design Rainfall = 25-Year, 3-hour Chicago Storm
00028+ * Existing Drainage from Subject Site to Ottawa River
00029+ DESIGN RASHD##### Design Rainfall = 25-Year, 3-hour Chicago Storm
00030+ * Existing Drainage from Subject Site to Ottawa River
00031+ DESIGN RASHD##### Design Rainfall = 25-Year, 3-hour Chicago Storm
00032+ * Existing Drainage from Subject Site to Ottawa River
00033+ * Existing Drainage from Subject Site to Ottawa River
00034+ * Existing Drainage from Subject Site to Ottawa River
00035+ * Existing Drainage from Subject Site to Ottawa River
00036+ * Existing Drainage from Subject Site to Ottawa River
00037+ * 25 Year - 3 hour Chicago Storm
00038+ * 25 Year - 3 hour Chicago Storm
00039+ * 25 Year - 3 hour Chicago Storm
00040+ * 25 Year - 3 hour Chicago Storm
00041+ * 25 Year - 3 hour Chicago Storm
00042+ * START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[001]
00043+ ["025YCH3.stm"] <- storm filename, one per line for NSTM0 time
00044+ ["025YCH3.stm"] <- storm filename, one per line for NSTM0 time
00045+ * 5-Year, 3-hour Chicago Storm
00046+ * START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[005]
00047+ ["025YCH3.stm"] <- storm filename, one per line for NSTM0 time
00048+ * 5-Year, 3-hour Chicago Storm
00049+ * START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[009]
00050+ * 5-Year, 3-hour Chicago Storm
00051+ * START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[010]
00052+ * 5-Year, 3-hour Chicago Storm
00053+ * 25-Year, 3-hour Chicago Storm
00054+ * START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[025]
00055+ ["025YCH3.stm"] <- storm filename, one per line for NSTM0 time
00056+ ["025YCH3.stm"] <- storm filename, one per line for NSTM0 time
00057+ * 50-Year, 3-hour Chicago Storm
00058+ * START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[050]
00059+ * 50-Year, 3-hour Chicago Storm
00060+ * 100-Year, 3-hour Chicago Storm
00061+ * START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[090]
00062+ START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[098]
00063+ * 100-Year, 3-hour Chicago Storm
00064+ * START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[100]
00065+ * 2-Year, 24-Hour SCS Storm
00066+ * START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[102]
00067+ ["SC240100X.stm"] <- storm filename, one per line for NSTM0 time
00068+ * 2-Year, 24-Hour SCS Storm
00069+ * START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[105]
00070+ ["SC24050X.stm"] <- storm filename, one per line for NSTM0 time
00071+ * 10-Year, 24-Hour SCS Storm
00072+ * START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[110]
00073+ ["SC24100X.stm"] <- storm filename, one per line for NSTM0 time
00074+ * 10-Year, 24-Hour SCS Storm
00075+ * START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[110]
00076+ ["SC24100X.stm"] <- storm filename, one per line for NSTM0 time
00077+ * 25-Year, 24-Hour SCS Storm
00078+ * START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[125]
00079+ ["SC24100X.stm"] <- storm filename, one per line for NSTM0 time
00080+ * 50-Year, 24-Hour SCS Storm
00081+ * START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[150]
00082+ * 100-Year, 24-Hour SCS Storm
00083+ * START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[150]
00084+ * 100-Year, 24-Hour SCS Storm
00085+ * START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[198]
00086+ START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[198]
00087+ ["SC24100X.stm"] <- storm filename, one per line for NSTM0 time
00088+ * 100-Year, 24-Hour SCS Storm
00089+ * JULY 1st, 1979 Storm - Ottawa International Airport
00090+ * START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[199]
00091+ ["19790701.stm"] <- storm filename, one per line for NSTM0 time
00092+ * August 4th, 1988 Ottawa International Airport
00093+ * START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[198]
00094+ * START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[198]
00095+ ["19880804.stm"] <- storm filename, one per line for NSTM0 time
00096+ * August 8th, 1996 Ottawa International Airport
00097+ * START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[199]
00098+ ["19960808.stm"] <- storm filename, one per line for NSTM0 time
00099+ * August 8th, 1996 Ottawa International Airport
00100+ * FINISH
00101+ * 100-Year, 3-hour Chicago Storm + 20'
00102+ * START TZERO=[0.0], METOUT=[2], NNRUN=[1], NNRUN=[199]
00103+ ["100YCH3.stm"] <- storm filename, one per line for NSTM0 time
00104+ * FINISH
00105+ * FINISH

```



```

00379> ****END OF RUN : 198
00380> ****
00381> ****
00382> ****
00383> ****
00384> ****
00385> ****
00386> ****
00387> ****
00388> RUNS:COMMAND#
00389> RO199:CO0001-----
00390> *****STORM*****
00391> [TZERO = 0.00 hrs on 0]
00392> [METOUT= 2 (Imperial, 2=metric output)]
00393> [DRAFT= 0]
00394> [NRUN= 0199]
00395> #*****INPUT DATA FILE*****
00396> SWMHYMO\202107\Jan 2021\SWTIA - INPUT DATA FILE
00397> #*****Project Name : [Cardinal Creek Village]
00398> # Project Number : [ ]
00399> # Date : 2021/07/07
00400> # Modeler : Laura Pipkins, P.Eng.
00401> # Organization : [Laurie Pipkin and Associates]
00402> # License # : 2582634
00403> #*****READ STORM*****
00404> RO199:CO0002-----
00405> READ STORM
00406> Filename = storm.001
00407> C:\Program Files\Storm SCS Type 2 Storm 24 Hours step 10 min, City of Ottawa
00408> [SET=10.00:SOUR= 24.00:PTOT= 106.73]
00409> RO199:CO0003-----
00410> *****STANDYD*****
00411> *****STANDYD VALUES*****
00412> [File name = T:\PROJ\959(02)-11\202001\Subm1\Design\SWMHYMO\202107 Pre-Dev\Ottawa.val]
00413> ICASEdy = 1 (read and print data)
00414> File = [ ] (read and print Parameters for City of Ottawa Projects)
00415> *****THE FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDYD COM*****
00416> *****Horton's 2 infiltration equation parameters:*****
00417> [Pc = 76.20 mm] [Pd = 10.00 mm] [Pf = 4.14 / hr] [Pe = .00 mm]
00418> *****Parameters for PREVIOUS surfaces in STANDYD:*****
00419> [TAper = 4.67 mm] [LGW=40.00 m] [RND= .250]
00420> [DPER= 0.00 mm] [LGW=40.00 m] [RND= .250]
00421> [IAimp = 1.57 mm] [CLv= 1.50] [WNL=.013]
00422> [Parameters used in NHDYD:]
00423> [Pc = 76.20 mm]
00424> Average monthly Pan Evaporation data in (mm)
00425> JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00426> .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00427> Average monthly Potential Evapotranspiration in (mm)
00428> JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00429> .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00430> # CN -> CN based Ontario Soil Map 58, Nov 1985 NTD Manual Chart H-6A,
00431> Lidar data, May 2008 SWMHYMO USER's Manual, air photos, assume good condition
00432> #
00433> # Time to Peak = 2/3 of FAA To
00434> #*****EXISTING CONDITIONS Drainage to South Tributary East of Cox County Road
00435> #*****SWTIA*****
00436> *****SWTIA*****
00437> [SWTIA=SWTIA from CO0001 to CO0002]
00438> RO199:CO0004-----DWin-ID=NHDYD---ARBA=QPEAKms-TpeakDate_h:mm---RVM=R.C.---DWFCms
00439> DESIGN_NASH= 1.0 01=eCCR 74.30 1.904 No_date 13:21 39.39 .369 .000
00440> DPER= 0.00 mm
00441> *****STORM*****
00442> # STORMS
00443> #*****RO199:CO0002*****
00444> RO199:CO0002-----
00445> FINISH
00446> -----
00447> ****
00448> ****
00449> ****
00450> Simulation ended on 2021-07-19 at 10:39:03
00451> ****
00452>

```