

MONTGOMERY SISAM ARCHITECTS INC.

Orleans Long Term Care Facility Functional Servicing Report

City of Ottawa

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November 2021 – 21-2647

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November 2021 – 21-2647

Introduction

1.0

1.1

2.0

2.1

Dillon Consulting Limited (Dillon) was retained by Montgomery Sisam Architects Inc. to develop a functional servicing strategy for the undeveloped property fronting Famille-Laporte Avenue, located at 1161 Old Montreal Road in the City of Ottawa. This document outlines the servicing strategy including supporting studies and related information for the transportation, sanitary, stormwater management, and water main servicing for the site.

The total area of the entire site is approximately 2.01 Ha. The Developer is planning on severing the property into two separate development lots. The proposed Long Term Care development site is approximately 1.22 Ha, and the remaining undeveloped lands area are approximately 0.79 Ha. The overall site is presently zoned RI5 Rural Institutional and currently consists of a vacant/grassed field. The proposed Long Term Care Facility development will be located on the southern portion of the site within the limits of the vacant field.

Reference Documents

The following documents and drawings were referenced when completing this study:

- City of Ottawa- Sewer Design Guidelines (Ottawa, 2012)
- City of Ottawa GIS Interactive Mapping (Ottawa)
- Design Guidelines for Sewage Works (MOE, 2008)

Transportation Servicing

Existing Conditions

There is no existing access to the proposed development. The property is bounded on the north limit, east limit, and south limit by residential homes.

Proposed Roadways 2.2

The proposed access points to this development will be from Famille-Laporte Avenue at the west limit of the site. Staff, visitors, EMS, services and deliveries will access the site via Famille-Laporte Avenue. The site layout is shown in Appendix A. The pavement structure of the proposed internal roads will be consistent with geotechnical recommendations and the City's Development Manual. A Traffic Impact Study (TIS) is required for this project and is currently underway.



Sanitary Servicing

Existing Conditions 3.1

3.0

Currently, there is an existing 200 mm diameter sanitary sewer located underneath Famille-Laporte Avenue, which is located west of the proposed development. The existing sanitary sewer heads northwards, ultimately discharges to the City of Ottawa Robert O. Pickard Environmental Centre treatment plant.

Design Criteria 3.2

The following sanitary sewer design criteria for this property are outlined in Table 1. The design criteria was established by the City of Ottawa's Design Guidelines (2012).

Table 1: Sanitary Sewer Design Criteria

Criteria	City of Ottawa's Design Guidelines (2012)
Hydraulic Sewer Sizing	Manning's Equation
Minimum Sewer Size (mm)	135 mm diameter
Minimum Cover Depth (m)	2.0
Manning's Roughness Coefficient 'n'	0.013
Velocity: Minimum (m/s) Maximum (m/s)	0.60 3.00
Hydraulic Losses Across Manholes: • Straight Run (m) • 45 degree turn of less (m) • Greater than 45 degree turn to 90 degree turn (m)	Grade of Sewer 0.03 0.06
Infiltration Allowance/Peak Extraneous Flow	0.28 L/Ha/s
Peaking Factor	Based on Harmon Formula
Population Densities For Facility:	224 Bed Facility Assumed 30 Staff Members Total Population = 254 ppl
Average Daily Sewage	50,000 L/Gross Ha/Day [Per City Sewer Guidelines for Institutional Lands] 350 L/Cap/Day [Residential Average Flow]
Sewer Surcharging	Maximum hydraulic grade line



Proposed Servicing

3.3

Refer to the attached Appendix A which illustrates the proposed sanitary servicing layout. The sanitary servicing for the proposed development is as follows:

- All sanitary flows from within the proposed development will be conveyed via local sanitary sewers.
- It is proposed that the local sanitary sewer will outlet to the existing Private Drain Connection Manhole located at the Famille-Laporte Avenue right-of-way limit. The existing PDC sewer is 200mm in diameter, connects to an existing sanitary manhole within the Famille-Laporte right-of-way, and drains northerly via an existing 250mm diameter sewer.

The sanitary sewer functional design sheets are provided in Appendix B. Criteria used in flow calculation is listed in Table 1.

The future detailed design of the sanitary sewer and service is to be consistent with the requirements of the City of Ottawa and the Ministry of Environment, Conservation and Parks (MECP).



Stormwater Servicing

Background Information 4.1

The proposed development is of approximately 1.21 Ha and is zoned RI5 Rural Institutional, currently consists of a vacant field. The City of Ottawa has previously installed a storm sewer stub for the proposed development at this location. There is an existing 1200 mm diameter municipal storm sewer within the Famille-Laporte Avenue right-of-way along east side of the road heading northwards, which outlets to the Ruisseau Cardinal Creek and ultimately discharges to the Ottawa River.

Design Criteria 4.2

4.0

The following storm sewer design criteria for this property are outlined in Table 2. The design criteria were established by the City of Ottawa's Design Guidelines (2012).

Storm Sewer Design Criteria Table 2:

Criteria	City of Ottawa's Design Guidelines (2012)
Hydraulic Sewer Sizing	Rational Method / Mannings Equation
Sewer Sizing Rainfall Event	5 year storm event
Minimum Cover Depth (m)	2
Manning's Roughness Coefficient 'n'	0.013
Velocity:	0.80 3.0
Roof Downspouts	May be connected directly to underground sewer system network or directed to surface
Rooftop Storage	Permitted (maximum 0.3m depth)
Inlet Times: • Institutional	15 minute maximum
Runoff Coefficients: • Paved and Roof Surfaces • Landscaped/Open Space	Calculated per Site Conditions 0.90 0.20
Sewer Surcharging	 No surface ponding during 5 year storm event 100 year Hydraulic Grade Line 0.3m below building footing
Stormwater Storage Requirements	 Storage of 100 year storm event Outlet rate to be confirmed through consultation with City



Criteria	City of Ottawa's Design Guidelines (2012)
Water Quality Treatment	Required per Rideau Valley Conservation Authority (RVCA)

Proposed Servicing 4.3

It is proposed that the site's stormwater outlet to the existing 1200 mm diameter storm sewer that is currently located within the Famille-Laporte Avenue right-of-way, located west of the site.

Refer to Appendix A for the proposed servicing. The stormwater servicing for the proposed development is as follows:

- The proposed site, and paved area will be serviced through a new storm sewer network constructed within the site.
- Onsite detention will be provided in accordance with City of Ottawa and Rideau Valley Conservation Authority Design Guidelines. Pre-consultation with the City is required, but in general the site storm outlet rate is to be restricted to the pre-development outlet rates for the 2, 5 and 100 year storm events.
- The site will be graded to allow for overland flow to be captured onsite and directed to the storm sewer network. Rain events in excess of the 100 year event will spill over the site entrances and drain overland within the existing City road network.

Refer to Appendix B for the sanitary sewer and storm sewer design and Appendix C for the Stormwater Management Calculations.



Watermain Servicing

Existing Conditions 5.1

5.0

An existing 400 mm diameter watermain is located within the Famille-Laporte Avenue right-of-way, located in the west boulevard. The site currently does not have any service connections.

Proposed Servicing 5.2

Please refer to the attached Appendix A which illustrates the proposed watermain servicing. The watermain servicing for the proposed development is as follows:

- The new building will be serviced by a new 150 mm diameter domestic watermain connected to the existing main on Famille-Laporte Avenue. The building service lines are split prior to entering the building into a 100mm diameter domestic service, and a 150mm diameter fire service. A backflow preventer will be installed inside the building mechanical room.
- Two (2) new fire hydrants and 150 mm diameter leads are proposed for the site. One is located in the south parking area to be in close proximity to the building FDC connection, the second is located in the north boulevard. Both fire hydrants will be connected to the existing main on Famille-Laporte
- All water crossings of Famille-Laporte Avenue will be completed via directional drill, with no open cuts to the roadway.

Fire hydrant flow testing has been completed for this development. Refer to Appendix D for the fire hydrant flow testing result.

The detailed design of the watermain service are to be consistent with the requirements of the City of Ottawa and will be coordinated during the detailed design process.



Utilities

Gas 6.1

6.0

Existing natural gas infrastructure is located along the Famille-Laporte Avenue right-of-way, located west of the site. There is no existing natural gas service currently servicing the proposed site. During detailed design, future conversation on loading will be required with Enbridge.

Telecommunications 6.2

The existing site is not currently serviced by telecommunications. It is anticipated that existing telecommunications infrastructure exists within the Famille-Laporte Avenue right-of-way, located west of the site. Detailed design, additional consultation will be held with utility owner to confirm internal servicing requirements.

Hydro 6.3

Existing hydro infrastructure is buried along the east side of the Famille-Laporte Avenue right-of-way. There is no existing hydro currently servicing the proposed site. During detailed design, future conversation on loading will be required with the hydro provider.



Conclusion

7.0

The review of the adjacent services have been found to be sufficient for the proposed development. The design of the proposed internal services will be finalized during detailed design.

Yours sincerely,

DILLON CONSULTING LIMITED

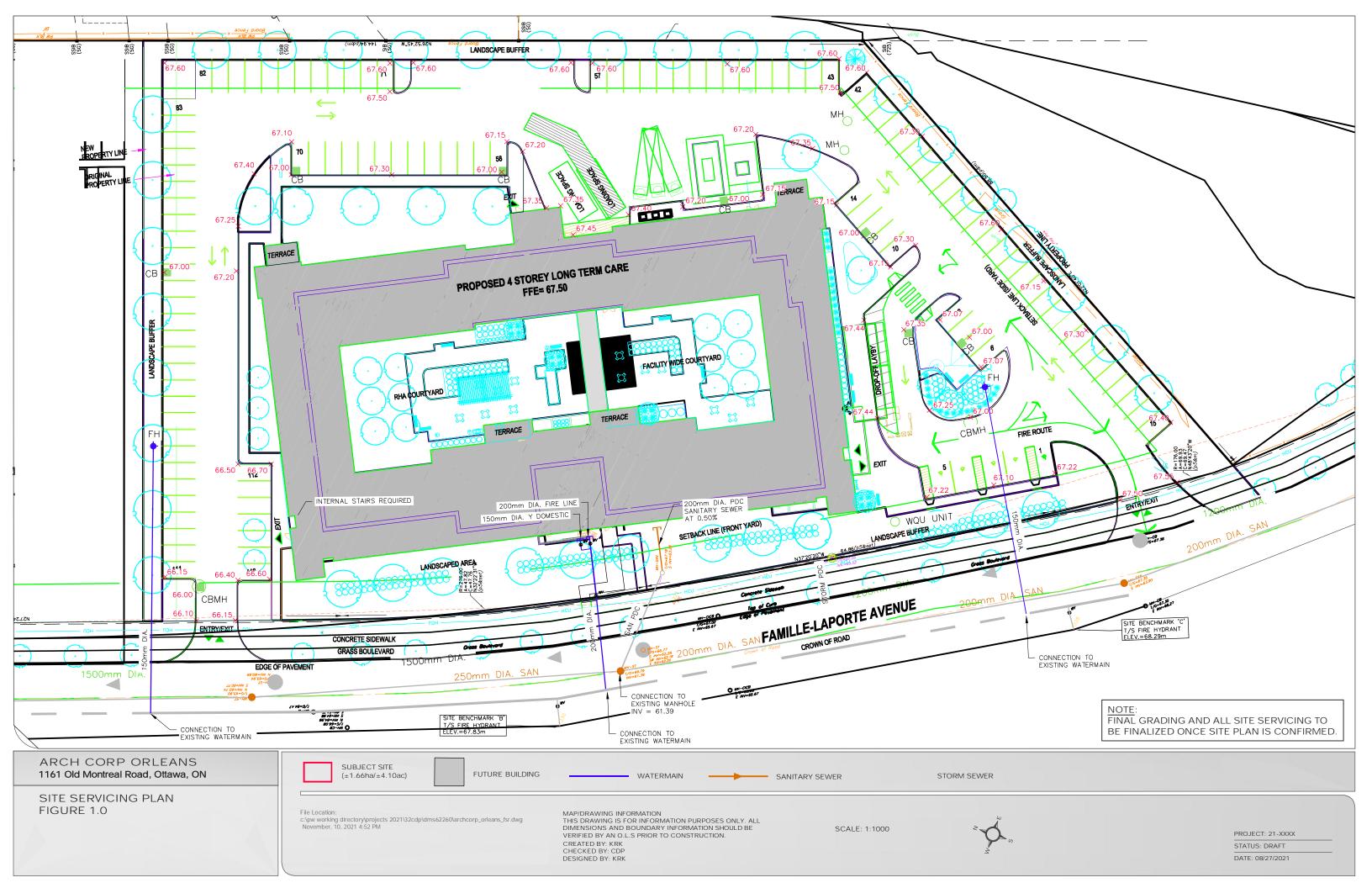
Chris Patten, P.Eng. Project Manager



Appendix A

Functional Servicing Plan





Appendix B

Sanitary Sewer and Storm Sewer Design Sheets



ORLEANS LONG TERM CARE FACILITY - CITY OF OTTAWA SANITARY SEWER DESIGN SHEET

Project Name: 0		LTC													Outlet Ir	vert Elevation=	60.740								
Project No: 21-4	4926				g Factor was de Irmon Formula	- Y	(Y or N)	Residential Ave	erage Daily Flow=	350	L/Cap.D					Mannings 'n'=	0.013		Basemen	t Floor Elevation =	0.000	Ground El	levation at Outlet =	66.790	
City of Ottawa				Va	From a Table lue from table=			Peak E	extraneous Flow=	0.280	L/Ha.S					Total Area=	1.220		Hvdraulic (or Grade Line Cover =	2.00		HGL at Outlet =	61.590	
	cation					Flow Charac								Sew	er Design/Pro				.,,		Cover			Hydraulic Grade Line)
ROAD/STN	LOC	CATION	INDIVID						PEAK DESIGN				Wall												1
	MH	MH	POP	AREA (ha.)	POP AREA (ha.)	FACTOR M	Q(p) (L/s)	FLOW Q(i) (L/s)	FLOW Q(d) (L/s)	CAPACITY (L/s)	LENGTH (m)	PIPE DIA. (mm)	Thickness (mm)			LOWER INVERT (m)	FALL (m)	VELOCITY (m/s)	DROP IN LOWER MANHOLE (m)	Ground Elevation Upper MH	Cover @ Up MH (m)			HGL Elev vs. Grnd Elev @ Up MH	HGL Elev v Obvert @ Up

ORLEANS LTCF STORM SEWER DESIGN SHEET

Project Name: Orleans LTCF Project Number: 21-2647

BLDG STORAGE 0.43

0.82

0.97

0.97 10.0 0.17

Intensity Option # 1

1) Intensity (i) = $a/(t+b)^c$ 2) Intensity (i) = a^*t^b 3) Insert Intensity

10.00

178.56

172.99

46.38

1.48

11

Manning's n = 0.013

														IV	anning s n =	0.013										
Based on City of Ott	1:100 Year S awa	torm Event					a= b= c=		a= b=		i=			Tota	ıl Area (ha)=	1.21	Outlet Inve	ert Elevation=	65.5	520	Ground Elev	ation @ Outlet =	67.25	High	Water Level at Outlet=	-
	Location															Sewer Design	ı / Profile						Cover		Hydraulio	Grade Line
Road /Station	From s MH	To MH	Area (ha)	Run. Coef.	2.78AC	Accum. 2.78AC	T of In (min)	T of F (min)	T of Conc. (min)	Intensity (mm/hr)	Exp. Flow (L/s)	Capacity (L/s)	Velocity (m/s)	Wall Thickness (mm)	Length (m)	Pipe Dia. (mm)	Slope (%)	Invert Up MH	Invert Low MH	Fall (m)	Drop Across Low MH (m)		Cover @ Up MH (m)	Cover @ Low MH (m)	HGL Elevation at Upstream MH	HGL Elev vs. Grnd Elev @ Up MH
	MH1	MH2	0.04	0.82	0.08	0.08	10.0	0.40	10.00	178.56	14.25	162.54	1.02	11	24.6	450	0.33	65.94	65.86	0.08		67.150	0.75	1.08	66.39	Okay
	MH2	MH3	0.08	0.82	0.18	0.26	10.0	0.66	10.40	174.97	45.87	161.28	1.01	11	40.0	450	0.32	65.86	65.73	0.13	0.040	67.400	1.08	1.11	66.31	Okay
	MH3	STORAGE		0.82	0.23	0.49	10.0	0.03	11.06	169.43	82.65	201.60	1.27	100	2.5	450	0.50	65.69	65.68	0.01		67.300	1.06	1.27	66.14	Okay
	STORAG		0.10	0.82	0.23	0.72	10.0	0.07	11.09	169.16	121.09	127.50	0.80	100	3.3	450	0.20	65.68	65.67	0.01		67.500	1.27	1.20	66.13	Okay
	MH4 WQU	WQU OUTLET	0.00	0.82 0.82		0.72 0.72	10.0 10.0	1.31 0.23	11.16 12.47	168.61 158.73	120.69 113.62	127.50 127.50	0.80 0.80	100 100	63.1 11.3	450 450	0.20 0.20	65.67 65.54	65.54 65.52	0.13 0.02		67.420 67.450	1.20 1.36	1.36 1.18	66.12 65.99	Okay Okay
		00.22.	0.00	0.02		0.12	.0.0	0.20		100110		.=	0.00			.00	0.20	00.0	0002	0.02		311.00			00.00	o.a,
	CBMH5	MH6	0.26	0.82	0.59	0.59	10.0	0.89	10.00	178.56	105.83	161.28	1.01	100	54.1	450	0.32	65.92	65.75	0.17	0.060	67.000	0.53	1.12	66.37	Okay
	MH6	STORAGE		0.82	0.00	0.59	10.0	0.08	10.89	170.82	101.28	161.28	1.01	100	4.7	450	0.32	65.69	65.68	0.02	0.000	67.420	1.18	1.27	66.14	Okay
	CBMH7	MH8	0.11	0.82	0.25	0.25	10.0	0.45	10.00	178.56	44.78	54.70	0.77	11	20.8	300	0.32	65.75	65.69	0.07		66.300	65.92	-0.31	0.37	Okay
	MH8	MH9	0.05	0.82	0.10	0.35	10.0	1.38	10.00	178.56	62.50	127.50	0.80	100	66.5	450	0.20	65.69	65.56	0.13		66.600	65.92	-0.55	0.58	Okay
	MH9	OUTLET	0.05	0.82	0.11	0.48	10.0	0.39	12.71	157.10	75.41	127.50	0.80	100	18.7	450	0.20	65.56	65.52	0.04		67.300	1.19	1.18	66.01	Okay

15.0

200

2.00

65.975

65.675 0.30

67.500

1.31

1.61

From Mech. Engineer

70.30

Appendix C

Stormwater Management Report





Stormwater Management Calculations	Project:	Perth LTCF	No.:	212317	
Rational Method Calculations	Ву:	SZ	Date:	11/19/2021	Page:
	Checked:	JVM	Scenario:	Existing	1

Calculation of existing runoff rate is undertaken using the Rational Method:

Q = CIA / 360

Where: Q = Peak flow rate (litres/second)

C = Runoff coefficient

I = Rainfall intensity (mm/hour) A = Catchment area (hectares)

Project Area, A 1

Composite Runoff Coefficient

Existing Site

1.22

Land Use

hectares

Composite Runoff Coefficient

Soil type

С

0.35

0.35

Agg Maps

-	Silty Clay	נ
	_	

Time of Concentration												
	Up EL	Down EL	Length	Slope	Area	C	Min Inlet					
Method	(m)	(m)	(m)	(%)	(ha)	С	Time (min)					
	69.5	66.25	140	2.32	1.22	0.35	10					
Bransby Williams	ansby Williams											
Airport	•											

Area (m²)

12,232

12,232

Rainfall intensity calculated in accordance with Sault Ste. Marie IDF Parameters: (if only two parameters are provided, enter B as "0" and C as positive number)

 $I = \frac{A}{(B + t_c)^C}$

Where: A, B, and C = IDF Parameters From Local Municipality Guidelines

I = Rainfall intensity (mm/hour)

T = Time of concentration (hours)

Return Period (Years)	2	5	10	25	50	100
Α	732.951	998.071	1174.184	1402.884	1569.580	1735.688
В	6.199	6.053	6.014	6.018	6.014	6.014
С	0.810	0.814	0.816	0.819	0.820	0.820
T (mins) **	21.9	21.9	21.9	21.9	21.9	21.9
l (mm/hr)	49.1	66.3	77.6	91.8	102.3	113.2
Q (L/s)	58.5	78.9	92.3	109.2	121.8	134.7
Q (m ₃ /s)	0.058	0.079	0.092	0.109	0.122	0.135

ORIFICE PLATE SIZING	CALCUL	ATION
Orifice Coeficient (C) =	0.62	
Allowable Outflow (Q) =	2.05	cfs
Invert =	215.45	
100 Year HWL =	217.95	
Trial D =	0.600	feet
Head (h) =	2.2	
Actual D =	0.595	feet
Actual D =	7 4/32	inches
USE A	7.14	INCH ORIFICE
USE A		
	181.3	mm



Stormwater Management Calculations	Project:	Orleans LTCF	No.:	21-2647	
Storage Calculations	Ву:	SZ	Date:	11/19/2021	Page:
	Checked:	JVM	Scenario:	Proposed	2

Calculation of existing runoff rate is undertaken using the Rational Method:

Q = CIA / 360

Where: Q = Peak flow rate (litres/second)

C = Runoff coefficient

I = Rainfall intensity (mm/hour) A = Catchment area (hectares)

Project Area, A

1.22 hectares

Composite Runoff Coefficient				
Land Use	Area (m²)	С		
Building	3,034	0.90		
Asphalt Pavenment	4,630	0.90		
Rocks, Misc Landscape	1,211	0.80		
Grass	3,357	0.25		
Composite Runoff Coefficient	12,232	0.71		

Runoff Coefficient Adjustment:	25%
Design Runoff Coefficient:	0.89

Target Discharge (m ³ /s):	0.058
---------------------------------------	-------

Design Event

100-Year Storm - From Ottawa SWM Guidelines 2012

A =	1735.7	
B =	6.014	
C =	0.820	
Time Step =	5	n

(if only two paramters are provided, enter B as "0" and C as positive number)

Where: A, B, and C = IDF Parameters From MTO

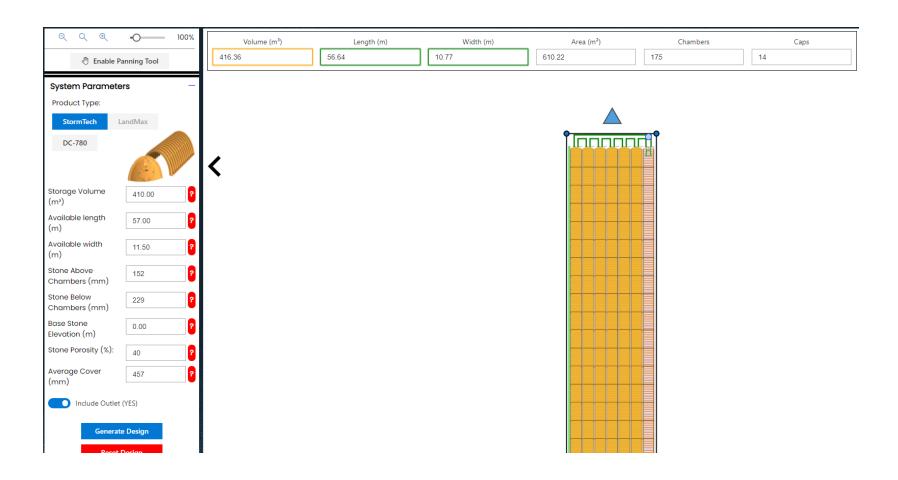
I = Rainfall intensity (mm/hour)
T = Time of concentration (hours)

<i>1</i> _	A	
1 =	$\overline{(B+t_c)^C}$	

Event Duration (mins)	Rainfall Intensity (mm/hr)	Peak Runoff Rate (m3/s)	Total Inflow Volume (m3)	Total Outflow Volume (m3)	Required Storage Volume (m3)
10	178.56	0.54	324.1	35.1	289.0
15	142.89	0.43	389.0	52.6	336.4
20	119.95	0.36	435.4	70.2	365.2
25	103.85	0.31	471.2	87.7	383.5
30	91.87	0.28	500.2	105.3	394.9
35	82.58	0.25	524.6	122.8	401.8
40	75.15	0.23	545.6	140.4	405.2
45	69.05	0.21	564.0	157.9	406.1
50	63.95	0.19	580.4	175.5	404.9
55	59.62	0.18	595.2	193.0	402.2
60	55.89	0.17	608.71	210.6	398.13
65	52.65	0.16	621.1	228.1	393.0

Maximum Required Storage (m³)	Peak Duration
406.1	45

ADS STORMWATER DETENTION SIZING TOOL



Appendix D

Fire Hydrant Flow Testing Results



FLOW TEST REPORT Life & Fire Safety Ltd OFFICE REPORT: OTTAWA ON LOCATION: 1123 OLD MONTREAL RD ORLEANS ON. DATE OF FLOW TEST: JULY 27 2021 TIME OF FLOW TEST: 09:00 AM COMANY CONDUCTING TEST: Troy Life & Fire safety **CONDUCTED BY**: MICH LACHANCE WITNESSED BY: MICHEAL McLEESE W NOZZLE TYPE (HOSE MONSTER/PLAY PIPE): LITTLE HOSE MONSTER WATER MAIN SIZE (IF AVAILABLE): 16" **TORANT ELEVATION COMPARED TO BUILDING:** SAME ELEVATION AS BUILDING **HYDRANT FLOW DATA** STANDING PRESSURE (HYDR #1): 64PSI 1-1/8" 1-3/4" 2-1/2" SIZE OF OPENING: DISCHARGE COEFICIENT: 0.09 PITOT READING (HYDRANT #2): 29PSI FLOW USGPM: 564GPM RESIDUAL PRESSURE (HYDRANT#1): 59PSI

Google Maps Famille-Laporte Ave

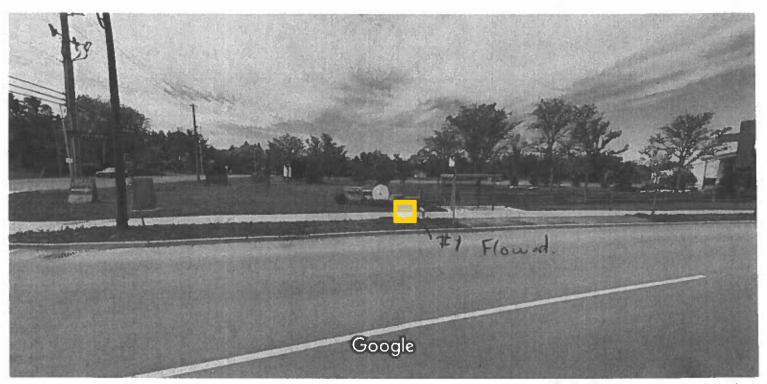


Image capture: Jun 2019

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Ottawa, Ontario

Google Google

7/27/2021

1128 Ch. Old Montréal Rd - Google Maps

Google Maps 1128 Ch. Old Montréal Rd



Imade capture: Jun 2019 @ 2021 Google