

MEMORANDUM

DATE: MAY 15, 2020 CITY FILE NUMBER:

TO: MARK FRASER

FROM: JAZMINE GAUTHIER

RE: 225 SCHOLASTIC AVENUE – GREYSTONE VILLAGE

DESCHATELETS BUILDING: SITE SERVICING AND STORMWATER

MANAGEMENT MEMORANDUM

CC: JOHN RIDDELL

ATTACHED: 120055A-GP: GENERAL PLAN OF SERVICES

120055A-STM: STORMWATER MANAGEMENT PLAN

EXCERPTS OF FIRE FLOW CALCS FROM SUBDIVISION REPORT EXCERPTS OF STORMWATER CRITERIA FROM SUBDIVISION REPORT

EXCERPTS OF SANITARY FROM SUBDIVISION REPORT

(120055A)

This memo is to support a zoning by-law amendment for the property and is supplementary to the MSS: "Greystone Village - 175 Main Street: Site Servicing, Stormwater Management, Noise, Erosion and Sediment Control Brief (Phase 2 and 3), R-2017-089", dated May 26, 2017 to provide specifics related to the Greystone Village Deschâtelets Building which is part of the overall Greystone Village subdivision development.

The proposed development is located at 225 Scholastic Avenue in Old Ottawa East, east of Deschâtelets Avenue, south of des Oblats Avenue, west of Scholastic Avenue and north of Deschâtelets Avenue within the City of Ottawa. The existing property is currently occupied by the existing Deschâtelets building. The proposed re-development of this portion of the site will consist of re-developing the building to include a school/daycare and in the future, possibly a community centre and residential units. Also, in future phases, the plan is to add a future gym building and future parking lot.

The Deschâtelets area subject site is approximately 0.2594 ha in area, the future gym area subject site is approximately 0.1084 ha in area and the future parking area subject site is approximately 0.0858 ha in area. The development will have frontage on the fire route that run through the park block to the west. In future phases, it will have a two-way vehicular access to the parking lot site located on des Oblats Avenue.

This site servicing and stormwater management memorandum will outline how the site will be serviced with sanitary, storm and watermain; and will demonstrate that adequate municipal capacity is available within the proposed infrastructure to service the development.



Sanitary

The proposed redevelopment of the existing 4-storey building between des Oblats Avenue/ Scholastic Avenue/Deschâtelets Avenue will be serviced by a 200mm dia. sanitary service that connects to the existing 250mm dia. sanitary sewer on Scholastic Avenue.

The ultimate outlet is the existing 1350mm Rideau River Interceptor trunk sewer that runs parallel to the Rideau River on the eastern portion of the overall site.

The re-development will consist of school with 401 students, 40 staff and 45 occupants of the daycare; possible 38 residential units; possible 155-person community centre. Also, there is the possible future gym building that would add 363 persons, therefore:

It should be noted that the MSS accounted for 350L/c/d, but this memo will consider 280L/c/d as per the technical bulletin.

Deschâtelets Building

 Q_{SAN} = (401 students x 90 L/cap/day) + (40 staff x 75 L/cap/day) + (45 daycare x 75 L/cap/day) + (38 units x 1.8 persons/unit x 280 L/cap/day) + (155 persons x 75 L/cap/day) + (363 gym x 36 L/cap/day) = 86,310 L/day

Average Sanitary Flow = 86,310 L/day = 0.999 L/sec

Peak Sanitary Flow = 3.221 L/sec (with PF =
$$1 + \left(\frac{14}{4 + \left(\frac{1072.4}{1000}\right)^{1/2}}\right) * 0.8 = 3.224$$
)

Extraneous flow = $0.33 \text{ L/sec/ha} \times 0.4536 \text{ ha} = 0.1497 \text{ L/sec}$

Therefore,

Total Site Average Sanitary Flow to Deschâtelets Ave = 1.15 L/sec (with extraneous flows)

Total Site Peak Sanitary Flow to Deschâtelets Ave = 3.37 L/sec (with PF and extraneous flows)

The proposed development population estimates and sanitary flows accounted for in the "Greystone Village - 175 Main Street: Site Servicing, Stormwater Management, Noise, Erosion and Sediment Control Brief (Phase 2 and 3)" are based on the City of Ottawa Sewer Design Guidelines.



Stormwater

The site has an overall slope towards the Rideau River to the East. Storm runoff from the majority of the site is conveyed overland towards the Rideau River.

The proposed redevelopment of the existing 4-storey building between des Oblats Avenue/ Scholastic Avenue/Deschâtelets Avenue will be serviced by a 200mm dia. storm service that connects to the existing 375mm dia. storm sewer on Scholastic Avenue.

The ultimate outlet is the Rideau River on the eastern portion of the overall site.

As discussed in the "Greystone Village - 175 Main Street: Site Servicing, Stormwater Management, Noise, Erosion and Sediment Control Brief (Phase 2 and 3)", water quality control will be provided within the subdivision's storm sewer system with Vortech type structures and water quantity control is not required, other than for the roof, since the sewers are ultimately discharging directly to the Rideau River, provided the outlets are designed with suitable erosion protection measures. **The roof is to be controlled to 80L/s/ha.**

The roof of the Deschâtelets building will have uncontrolled roof drains directed to the stormwater tank and be controlled to 80L/s/ha before it outlets to the service. The roof of the future gym will be controlled by a combination of controlled roof drains and a stormwater tank and be controlled to 80L/s/ha before it outlets to the service. The flows will be pump controlled at 12.42L/s and 5.08L/s respectively to Scholastic Avenue and possibly des Oblats Avenue (c/w back-up pump and emergency battery backup). The emergency overflow from the tank will be at the surface.

The site will be graded such that flows in excess of the 100-year storm event will be conveyed overland to des Oblats Avenue. Scholastic Avenue, as well as Deschâtelets Avenue.

Erosion and sediment control measures will be implemented during all phases of construction and inspected regularly.



Watermain

The proposed redevelopment of the existing 4-storey building between des Oblats Avenue/ Scholastic Avenue/Deschâtelets Avenue will be serviced by two 150mm dia. water services that connects to the existing 250mm dia. watermains on des Oblats Avenue and Scholastic Avenue.

It should be noted that both services will need to be interconnected for redundancy at the entry into the building.

The existing 250mm dia. watermains on Deschâtelets Avenue, Scholastic Avenue and des Oblats Avenue are looped from the existing 200mm dia. watermain on Clegg Street to the new 400mm dia. watermain on Main Street.

Estimated domestic water demands for the development are roughly the same as the proposed development sanitary flows listed above. Therefore:

Average Day Demand = 0.999 L/s

Maximum Day Demand = 0.999 L/s * 2.5 = 2.50 L/s

Maximum Hourly Demand = 2.50 L/s * 2.2 = 5.50 L/s

The hydraulic analysis performed for the overall site as per the "Greystone Village - 175 Main Street: Site Servicing, Stormwater Management, Noise, Erosion and Sediment Control Brief (Phase 2 and 3)" demonstrates that the system will work for domestic water as well as fire demand.

Table 5.2: Hydraulic Model Results

| Operating Condition | Minimum Operating Pressure |
|------------------------------|----------------------------|
| Max Daily Demand + Fire Flow | Watermain |
| MD = 4.83 L/s | 293.91 kPa |
| FF= 286.45 L/s at node N6 | 42.63 psi |
| MD = 0.62 L/s | 319.51 kPa |
| FF= 167.00 L/s at node N7 | 46.34 psi |
| MD = 0.16 L/s | 300.48 kPa |
| FF= 286.45 L/s at node N8 | 43.58 psi |
| MD = 0.57 L/s | 257.71 kPa |
| FF= 219.97 L/s at node N12 | 37.38 psi |
| MD = 2.25 L/s | 211.01 kPa |
| FF= 300.24 L/s at node N15 | 30.60 psi |
| MD = 2.48 L/s | 238.19 kPa |
| FF= 300.24 L/s at node N21 | 34.55 psi |



| Peak Hour Demand | |
|-----------------------|--------------------------------------|
| PH = 48.86 L/s | 385.93 kPa (At Node 10) 55.97 psi |
| Maximum High Pressure | |
| MHP = node N25 | 551.91 kPa 80.05 psi |
| Maximum Time On Site | |
| MTS = node N30 | 38.3 hours |

The Deschâtelets Building has at least 3 hydrants within less than 75m, therefore at least 17,100L/min is available for fire flow. The calculated fire flow is 15,172L/min.



Other Reference Documents

N/A

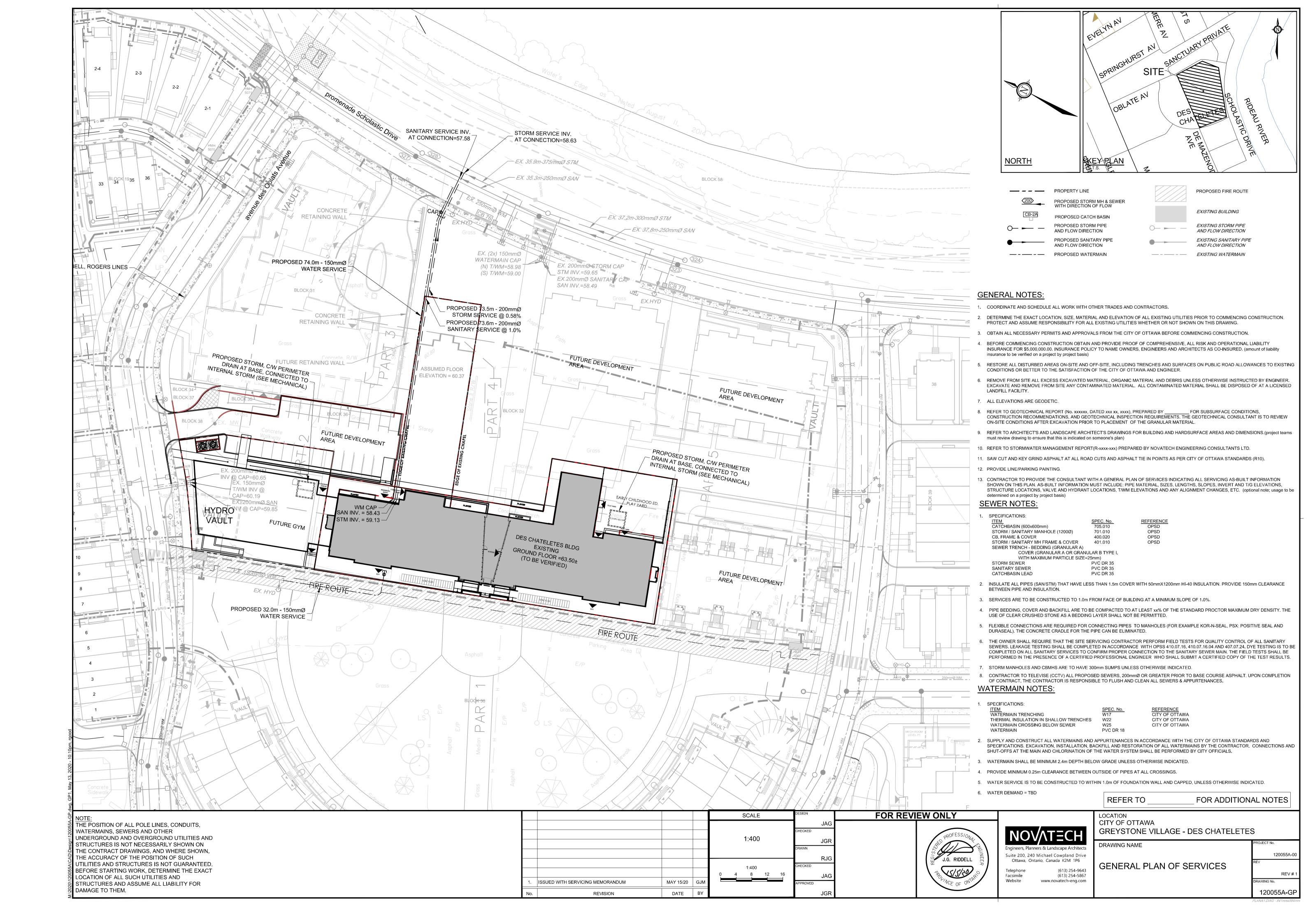
<u>LID</u>

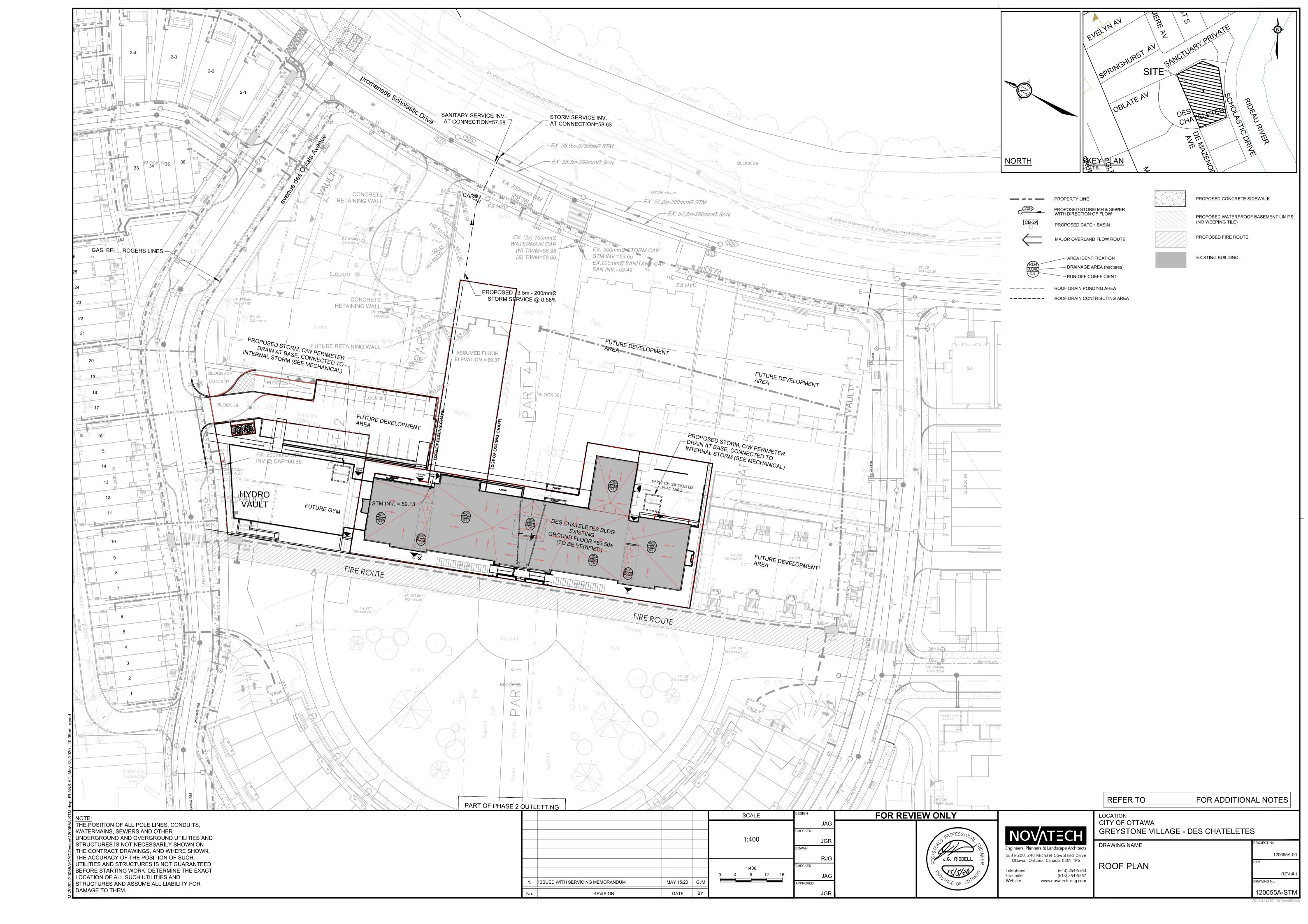
As mentioned in the MSS, LID features were to be considered at the lot level, but no specific LID features were suggested for the Deschâtelets block in the report "Greystone Village -175 Main Street - Potential Low Impact Development Opportunities" (Novatech, November 25th, 2015, R-2015-182). Due to site constraints LID features for this site (Deschâtelets) were deemed not feasible.

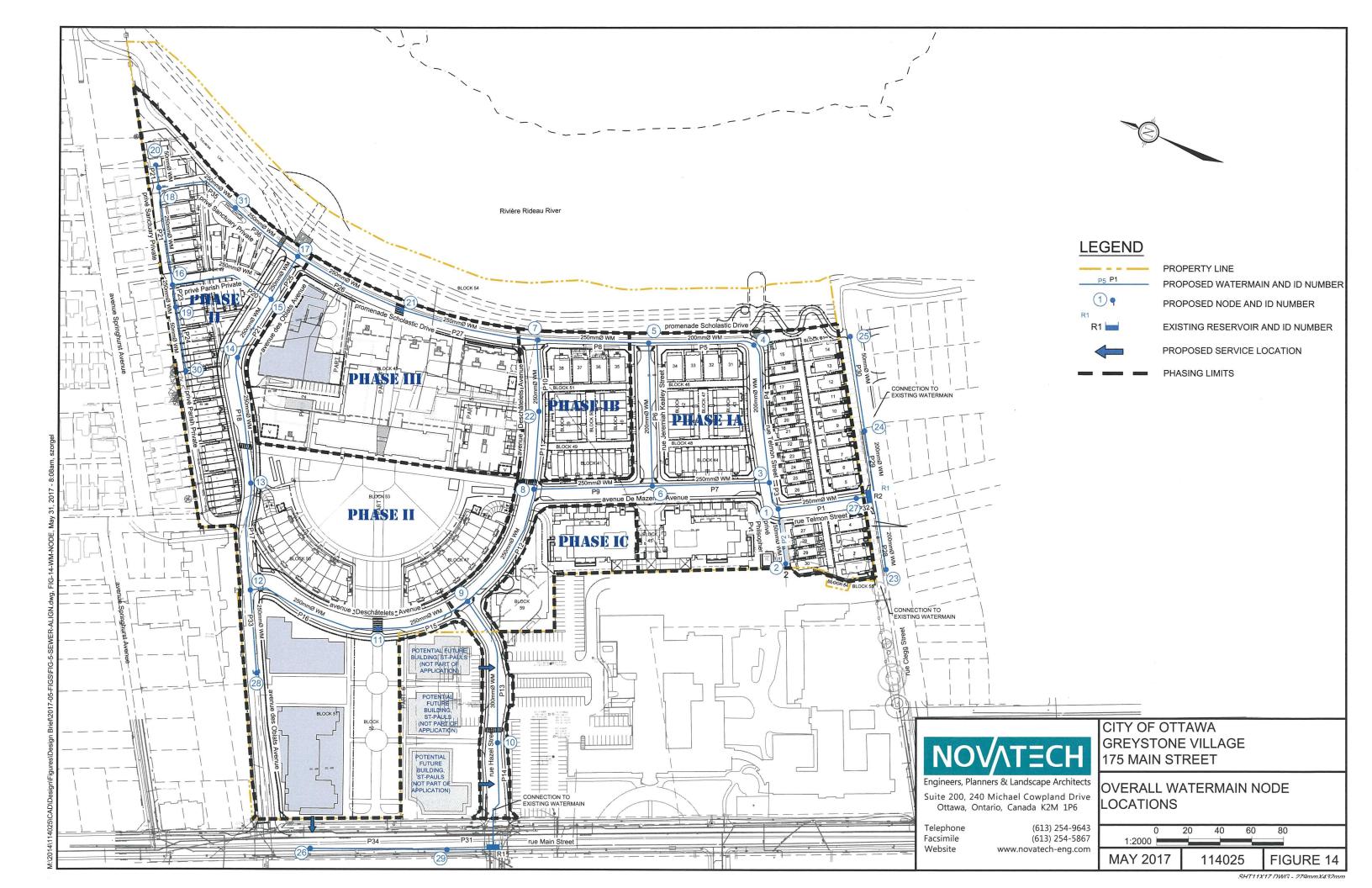
We submit the following and request your review and approval in order that we can receive site plan approval.

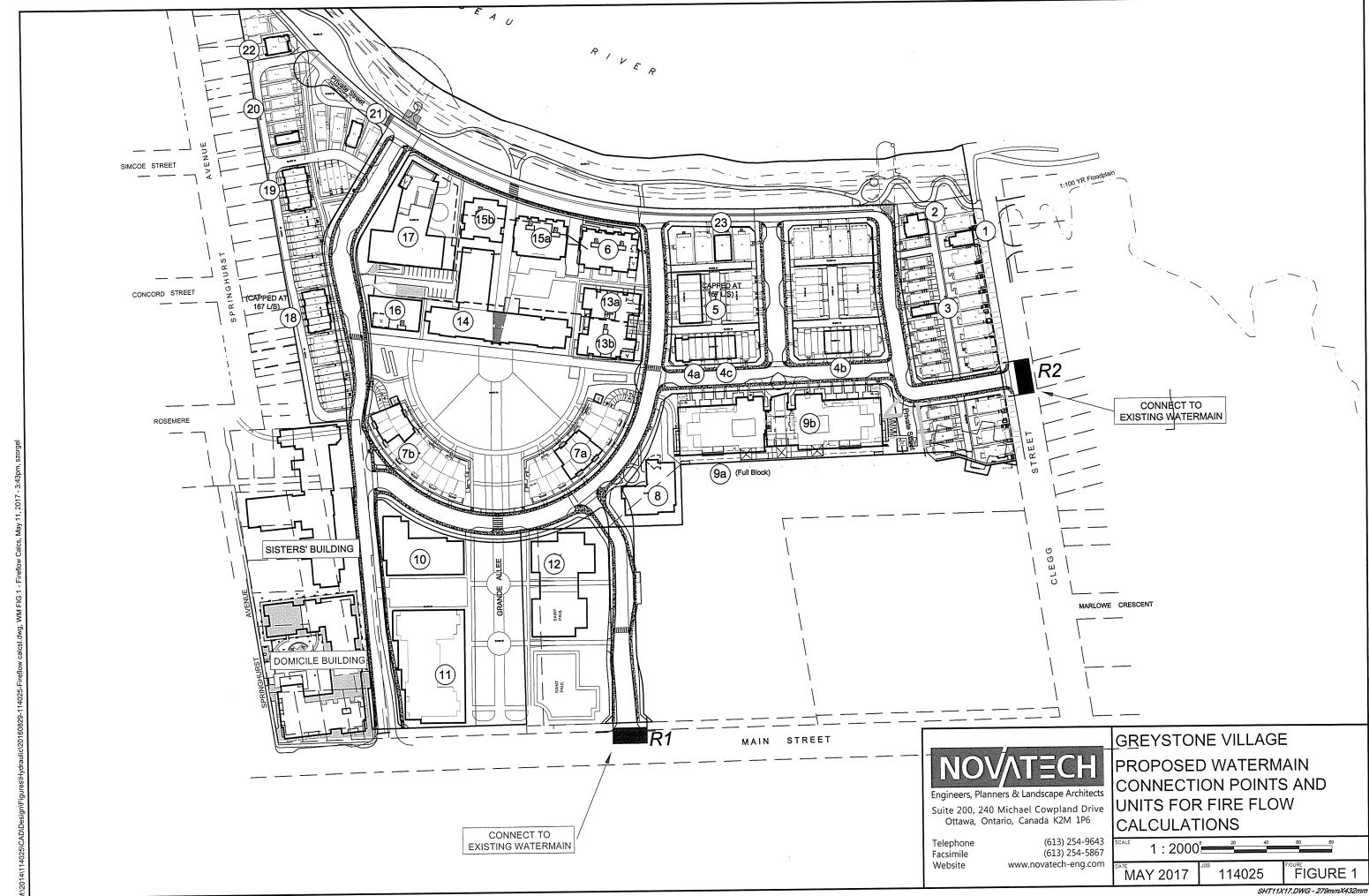
Thanks.











Fire Flow Calculations - Deschatelets Unit

As per Fire Underwriter's Survey Guidelines

PROJECT: Greystone Village - 175 Main St

DATE: May 10, 2017

JOB#: 114025

DESCHATELETS UNIT #14 - 4 storeys

| C | Coefficient related to type of construction | [yes/no] | | |
|-----|--|----------|------------------|---|
| | Wood frame | | 1.5 | |
| | Ordinary construction | | 1 | |
| | Non-combustible construction | yes | 0.8 | |
| | Fire resistive construction (< 2 hrs) | | 0.7 | |
| | Fire resistive construction (> 2 hrs) | | 0.6 | |
| | Interpolation (Using FUS Tables) | | | |
| А | Area of structure considered (m ²) | 8,500 | <==> | 91,493 ft² |
| | (All floors excluding Basement) | | l | THE RESIDENCE OF THE PROPERTY |
| F-a | Required fire flow (L/min) | | | |
| | $F = 220 \text{ C (A)}^{0.5}$ | | | 16,226 L/min |
| | ` ' | | | |
| | Occupancy hazard reduction of surcharge | [yes/no] | | |
| | Non-combustible | | - -25% | |
| | Limited combustible | yes | -15% | |
| | Combustible | - | 0% | |
| | Free burning | | 15% | |
| | Rapid burning | | 25% | 12 702 I /min (1) |
| | Sprinkler Reduction | | : | <u>13,792 L/min</u> (1) |
| | • Non-combustible - Fire Resistive (3) | yes | 50% | 6,896 L/min (2) |
| | Exposure surcharge (cumulative (%)) | [yes/no] | _ | |
| | 0 - 3 m | | 25% | |
| | 3.1 - 10 m | yes | 20% | 3 side 60% |
| | 10.1 - 20 m | | 15% | |
| | 20.1 - 30 m | | 10% | |
| | 30.1- 45 m | | 5% | |
| | | | Cumulati | ve Total 60% |
| | | | | 8,275 L/min |
| | Fire Wall Separation | | | |
| | Number of Party Walls * 1000 L/min | | | |
| | (As per City of Ottawa Standard) | | : | 8,275 L/min (3) |
| | REQUIRED FIRE FLOW [(1) - (2) + (3)] | | | 15,172 L/min |
| | (2,000 L/min < Fire Flow < 45,000 L/min) | | or | 252.86 L/s |
| | | | or | 3,340 IGPM |
| | BY: Steve Zorgel | | | |
| | DI. Sieve Zuigei | | | |
| | | | | |

3.0 STORMWATER MANAGEMENT

3.1 Existing Conditions

Existing development consists of the Deschâtelets Building, plus the parking and loading areas on the north, south, and east sides of the building. The remainder of the site consists of vacant land with some mature trees within and around the periphery. The Rideau River Nature Trail runs along the eastern limit of the site. Access is provided from Main Street by Oblate Avenue and the Grande Allée.

Topography and Drainage

The site has an overall slope towards the Rideau River to the East. While the south and west portions of the site are relatively flat, there is a ridge in the northeast portion of the site where the existing ground elevation drops by approximately 5m. There is also a relatively steep vegetated slope adjacent to the Rideau River, and a berm along the southern portion of the site adjacent to Clegg Street.

Storm runoff from the majority of the site is conveyed overland towards the Rideau River. There is also an existing outlet at the back of the existing Deschâtelets building that outlet's along the bank of the Rideau River, which will be abandoned/removed and the flows directed to the new proposed outlet. The southernmost portion of the site drains overland onto Clegg Street. There is also some external overland drainage from St. Paul University to be included in the storm system. Refer to **Figure 4** – Existing Storm Drainage Area Plan for details.

3.2 SWM Criteria

A small portion of the site will be tributary to the existing storm system on Main Street. The majority of the site will outlet directly to the Rideau River. The stormwater management criteria used in the design of the Greystone Village are presented below. They were developed in consultation with the City of Ottawa and the Rideau Valley Conservation Authority.

3.2.1 Water Quality Control

- Provide an Enhanced level of water quality control, corresponding to a long-term TSS removal rate of 80%% for lands draining to the Rideau River
- No water quality treatment is required for areas tributary to the existing storm sewer on Main Street.

3.2.2 Quantity Control

- Quantity control is not required for sewers discharging directly to the Rideau River, provided the outlets are designed with suitable erosion protection measures.
- Areas tributary to the Main Street storm sewer are to be controlled to either:
 - o the allowable release rate for the system (to be confirmed by City);
 - o to pre-development flow rates.

3.2.3 Minor System (Storm Sewers)

Storm sewers are to be designed using the Rational Method for a 1:5 year return period;

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| STM MH ID | Street | Obvert Elevation | T/G Elevation | HGL Elevation | Stress Test HGL | Sur- charge | Clearance from T/G | Minimum Required USF |
|--------------|-------------------|---------------------|------------------|------------------|-----------------------|----------------|--------------------|----------------------------|
| | | (m) | (m) | (m) | (m) | (m) | (m) | (m) |
| MH230 | Philosopher Pvt. | 60.15 | 63.44 | 60.63 | 60.87 | 0.48 | 2.81 | 60.93 |
| MH238 | - | 59.04 | 62.56 | 58.86 | 58.93 | 0.00 | 3.70 | 59.16 |
| MH242 | - | 57.00 | 61.68 | 58.40 | 58.52 | 1.40 | 3.28 | 58.70 |
| MH246 | - | 60.22 | 64.28 | 60.69 | 60.92 | 0.47 | 3.59 | 60.99 |
| MH248 | Deschâtelets Ave. | 62.23 | 64.77 | 62.16 | 62.20 | 0.00 | 2.61 | 62.46 |
| MH250 | Hazel St. | 63.08 | 65.74 | 62.85 | 62.88 | 0.00 | 2.89 | 63.15 |
| MH300 | des Oblats Ave. | 62.74 | 64.86 | 62.53 | 62.54 | 0.00 | 2.33 | 62.83 |
| MH302 | des Oblats Ave. | 61.80 | 64.32 | 61.59 | 61.61 | 0.00 | 2.72 | 61.89 |
| MH304 | des Oblats Ave. | 61.26 | 63.44 | 61.07 | 61.08 | 0.00 | 2.37 | 61.37 |
| MH306 | des Oblats Ave. | 59.77 | 62.10 | 59.58 | 59.59 | 0.00 | 2.52 | 59.88 |
| MH308 | des Oblats Ave. | 59.05 | 61.62 | 58.85 | 59.01 | 0.00 | 2.77 | 59.15 |
| MH310 | des Oblats Ave. | 57.20 | 60.06 | 58.70 | 58.87 | 1.50 | 1.36 | 59.00 |
| MH312 | Parish Pvt. | 61.96 | 64.19 | 61.78 | 61.78 | 0.00 | 2.41 | 62.08 |
| MH314 | Parish Pvt. | 60.96 | 63.06 | 60.81 | 60.81 | 0.00 | 2.25 | 61.11 |
| MH316 | Parish Pvt. | 57.51 | 60.20 | 59.12 | 59.27 | 1.61 | 1.08 | 59.42 |
| MH318 | Parish Pvt. | 57.82 | 59.59 | 59.14 | 59.28 | 1.32 | 0.45 | 59.44 |
| MH320 | Parish Pvt. | 57.34 | 59.97 | 58.97 | 59.11 | 1.64 | 1.00 | 59.27 |
| MH322 | Parish Pvt. | 57.30 | 60.03 | 58.92 | 59.07 | 1.63 | 1.11 | 59.22 |
| MH324 | Scholastic Dr. | 60.95 | 62.79 | 60.75 | 60.75 | 0.00 | 2.04 | 61.05 |
| MH326 | Scholastic Dr. | 59.57 | 61.81 | 59.31 | 59.31 | 0.00 | 2.50 | 59.61 |
| MH328 | Scholastic Dr. | 58.40 | 60.43 | 59.13 | 59.36 | 0.73 | 1.30 | 59.43 |
| MH330 | Sanctuary Pvt. | 57.43 | 59.30 | 58.79 | 59.01 | 1.37 | 0.51 | 59.09 |
| MH332 | Sanctuary Pvt. | 57.28 | 59.20 | 58.78 | 59.01 | 1.50 | 0.41 | 59.08 |
| MH334 | des Oblats Ave. | 57.11 | 59.03 | 58.62 | 58.79 | 1.51 | 0.41 | 58.92 |
| MH336 | - | 56.80 | 58.81 | 58.29 | 58.39 | 1.49 | 0.52 | 58.59 |
| MH338 | - | 57.09 | 58.75 | 58.28 | 58.37 | 1.19 | 0.47 | 58.58 |
| MH340 | - | 56.76 | 58.33 | 58.12 | 58.17 | 1.36 | 0.21 | 58.42 |

3.6 Release Rates for Future Development

The following section provides general guidelines for release rates for future development. Any changes to the proposed land use that significantly differ from the assumptions used in this analysis (land use, imperviousness, storage, etc.) should be identified and discussed with the City as part of the individual Site Plan submissions.

3.6.1 Flat Roof Buildings

Runoff from flat-roof buildings connecting to the storm sewer is to be controlled to a maximum release rate of 80 L/s/ha (equivalent to one drain per 250m² of roof area with a capacity of 2 L/s). This release rate would apply to any land use being proposed for these sites, including parking lots and also applies to roof areas draining to Main Street.

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4.0 SANITARY SEWER SYSTEM

4.1 Proposed Sanitary Sewer System

It is proposed that the entirety of the development area will be serviced by 250mm gravity sewers, including a small portion on Clegg Street (in proximity to the outlet #1). The development area will ultimately outlet via two connections to the existing 1350mm Rideau River Interceptor trunk sewer that runs parallel to the Rideau River on the eastern portion of the site. Outlet #1 will connect east of Clegg Street and upstream of the existing manhole on the Rideau River Interceptor to an existing sewer using an offline proposed manhole and the existing 900mm combined sewer pipe. Outlet #2 will connect northeast of the existing building (175 Deschâtelets) and Oblats Avenue to an existing manhole using an offline proposed manhole. A portion of the existing sanitary sewer that currently services the existing building will be removed and replaced with 250mm gravity sewers that will connect to the proposed sanitary system. The buildings along Main Street will be serviced by the proposed 450mm dia. sanitary sewers (replacing existing 375/450mm dia. sanitary sewers) within Main Street. Refer to Figure 10 — Overall Proposed Sanitary Alignment for details, Figure 11 — Sanitary Outlet 1 Plan View and Figure 12 — Proposed Sanitary Outlet 2 Plan View for details on the Phase 1A/1B and the Phase 2/3 connection to the existing trunk sewer.

4.2 Sanitary Design

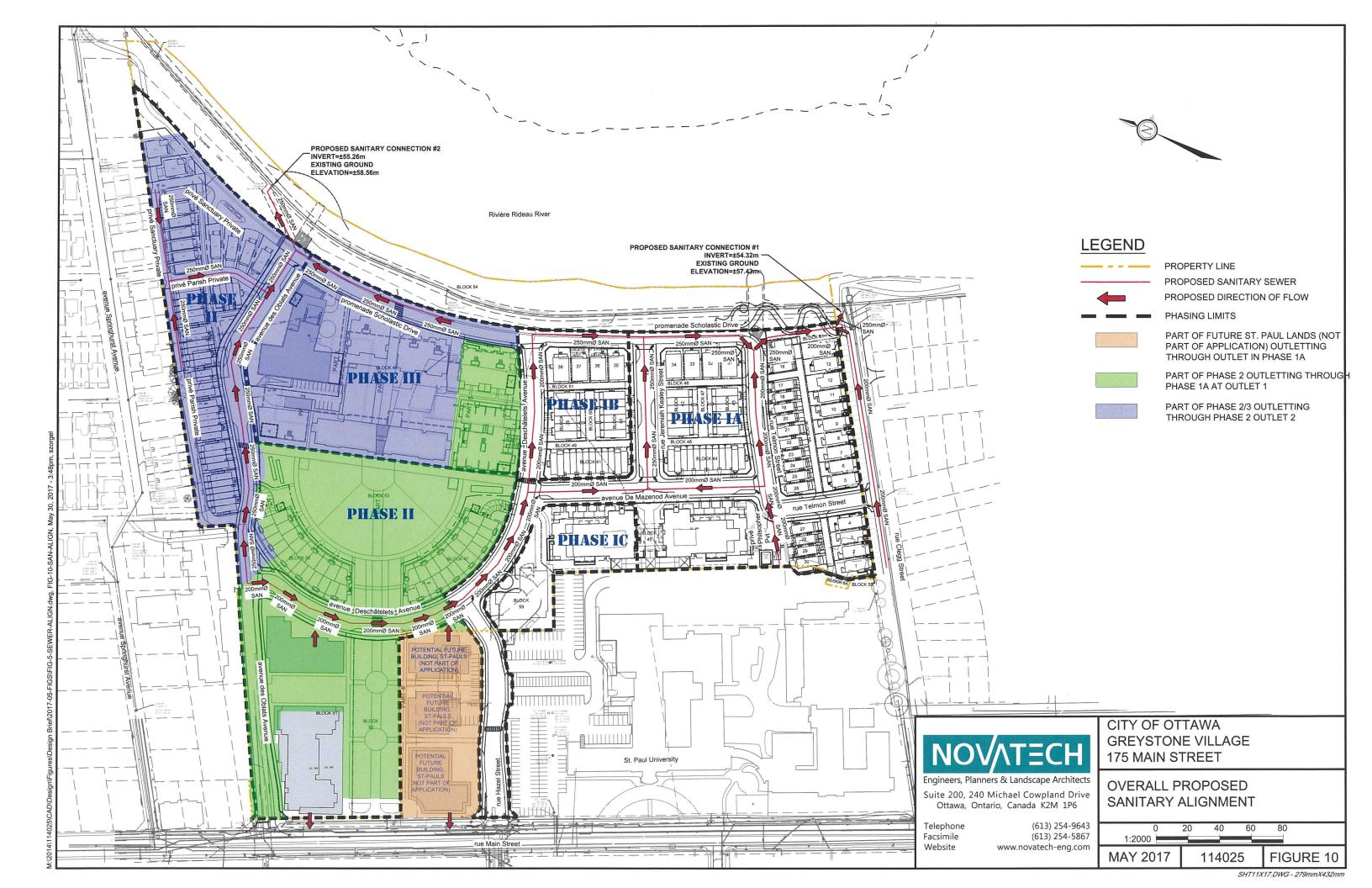
The design flows were calculated for the development using estimated populations based on design plans and composition of the townhouses/condo buildings and in accordance with the City of Ottawa Sewer Design Guidelines using the following design criteria:

- Residential Average Sewage Flow = 350 L/capita/day
- Residential Peaking Factor = Harmon Equation
- Max Peaking Factor = 4.0
- Infiltration Allowance = 0.28 L/s/ha
- Population Density:
 - o 3.4/unit (Singles)
 - o 2.7/unit (Towns)
 - o 2.1/unit (Apartment)
 - o 2.0/unit (School Residence)
 - o 1.4/unit (Retirement Residence)

The minimum size for sanitary sewers on the subject site is a 250mm diameter PVC pipe at a slope of 0.24%, which provides full-flow capacity of 30.39 L/s and will achieve the minimum cleansing velocity of 0.60 m/s.

Using the above criteria, the theoretical peak design flow from phase 1A and 1B (Outlet 1) was determined to be 24.03 L/s. The theoretical peak design flow from phase 2 and 3 (Outlet 2) was determined to be 10.72 L/s. The peak sanitary flows are summarized below in **Table 4.1**. Refer to **Appendix B** for Sanitary Design Sheets and to the Sanitary Drainage Areas Plans (Drawings **114025-SAN1**, **SAN2** and **SAN1-B**) for additional information.

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SANITARY SEWER DESIGN SHEET

Greystone Village - 175 Main Street - Phase 2 and 3 (Outlet 2)

Developer: Greystone Village Inc.



DESIGNED BY: SZ
CHECKED BY: JAG
DATE PREPARED: 18-Nov-16
DATE REVISED: 15-Mar-17
DATE REVISED: 26-May-17

114025

PROJECT #:

| LOCATIO | V | | | | | INDIVIDU | JAL | | | CUMULA | ATIVE | | | PEAK | PEAK | | | | PROPO | SED SEWE | R | | |
|-------------------|------------|----------|------|--------------|--------------------|-------------|--------------------------|---------------------------|---------------|---------------------------|----------------|---------------------|----------------------------------|---------|------------------------------------|---------------|-------------------|-----------------|-----------------|----------|-------------------|--------------------------------|----------------|
| STREET | FROM MH | TO MH | Area | Single Units | Townhouse Units | Condo Units | Retirement Home Units | Population (in 1000's) | AREA (ha.) | Population (in 1000's) | AREA (ha.) | PEAK FACTOR M | POPULATION FLOW Q(p) (L/s) | EXTRAN. | XTRAN. DESIGN OW Q(i) FLOW Q(d) | LENGTH (m) | PIPE SIZE (mm) | PIPE ID (mm) | TYPE OF PIPE | GRADE % | CAPACITY (L/s) | FULL FLOW VELOCITY (m/s) | Qpeak/ Qcap |
| | | | | | | | | | | | | | | | | | | | | | | | |
| OBLATS AVENUE | 301A | 301 | B1 | | | | | 0.000 | 0.04 | 0.000 | 0.040 | 4.0 | 0.00 | 0.01 | 0.01 | 18.5 | 250 | 254.00 | DR 35 | 5.25 | 142.1 | 2.81 | 0% |
| OBLATS AVENUE | 301 | 303 | B2 | | 3 | | | 0.008 | 0.12 | 0.008 | 0.160 | 4.0 | 0.13 | 0.04 | 0.18 | 27.9 | 250 | 254.00 | DR 35 | 2.30 | 94.1 | 1.86 | 0% |
| OBLATS AVENUE | 303 | 305 | В3 | | 7 | | | 0.019 | 0.15 | 0.027 | 0.310 | 4.0 | 0.44 | 0.09 | 0.52 | 32.4 | 250 | 254.00 | DR 35 | 3.33 | 113.2 | 2.23 | 0% |
| OBLATS AVENUE | 305 | 307 | B4 | L | 10 | 19 | | 0.067 | 0.33 | 0.094 | 0.640 | 4.0 | 1.52 | 0.18 | 1.70 | 44.9 | 250 | 254.00 | DR 35 | 3.34 | 113.4 | 2.24 | 2% |
| OBLATS AVENUE | 307 | 309 | B5 | | | | | 0.000 | 0.03 | 0.094 | 0.670 | 4.0 | 1.52 | 0.19 | 1.71 | 14.8 | 250 | 254.00 | DR 35 | 4.99 | 138.6 | 2.73 | 1% |
| OBLATS AVENUE | 309 | 311 | B6 | | | | | 0.000 | 0.09 | 0.094 | 0.760 | 4.0 | 1.52 | 0.21 | 1.73 | 36.7 | 250 | 254.00 | DR 35 | 3.81 | 121.1 | 2.39 | 1% |
| PARISH PRIVATE | 313 | 315 | B7 | | 12 | | | 0.032 | 0.14 | 0.032 | 0.140 | 4.0 | 0.53 | 0.04 | 0.56 | 56.5 | 250 | 254.00 | DR 35 | 3.24 | 111.7 | 2.20 | 1% |
| SANCTUARY PRIVATE | 317 | 315 | B8 | 9 | | | | 0.031 | 0.33 | 0.031 | 0.330 | 4.0 | 0.50 | 0.09 | 0.59 | 61.3 | 250 | 254.00 | DR 35 | 0.65 | 50.0 | 0.99 | 1% |
| SANCTUARY PRIVATE | 315 | 319 | B9 | 1 | 2 | | | 0.009 | 0.15 | 0.072 | 0.620 | 4.0 | 1.16 | 0.17 | 1.34 | 36.3 | 250 | 254.00 | DR 35 | 0.41 | 39.7 | 0.78 | 3% |
| SANCTUARY PRIVATE | 319 | 321 | B10 | 1 | 2 | | | 0.009 | 0.06 | 0.081 | 0.680 | 4.0 | 1.31 | 0.19 | 1.50 | 8.1 | 250 | 254.00 | DR 35 | 0.50 | 43.9 | 0.87 | 3% |
| SANCTUARY PRIVATE | 321 | 311 | B11 | 2 | | | | 0.007 | 0.09 | 0.087 | 0.770 | 4.0 | 1.42 | 0.22 | 1.63 | 22.4 | 250 | 254.00 | DR 35 | 0.40 | 39.2 | 0.77 | 4% |
| OBLATS AVENUE | 311 | 329 | B12 | | | | 141 | 0.197 | 0.41 | 0.379 | 1.940 | 4.0 | 6.14 | 0.54 | 6.68 | 32.9 | 250 | 254.00 | DR 35 | 0.42 | 40.2 | 0.79 | 17% |
| SCHOLASTIC DRIVE | 323 | 325 | B13 | | | 30 | 85 | 0.182 | 0.94 | 0.402 | 0.840 | 4.0 | 2.95 | 0.24 | 3.18 | 27.0 | 250 | 254.00 | DR 35 | 3,87 | 122.0 | 2.41 | 3% |
| SCHOLASTIC DRIVE | 325 | 327 | B13 | | | 30 | 00 | 0.162 | 0.84 | 0.182 | 0.840 0.890 | 4.0 | 3.97 | 0.24 | 4.22 | 37.8 35.3 | 250 250 | 254.00 | DR 35 | 3.32 | 113.0 | 2.23 | 4% |
| SCHOLASTIC DRIVE | 327 | 329 | B15 | | | 30 | | 0.000 | 0.05 | 0.245 | 0.890 | 4.0 | 3.97 | 0.25 | 4.22 | 36.7 | 250 | 254.00 | DR 35 | 3.88 | 122.2 | 2.23 | 3% |
| CONCLASTIC DITIVE | JEI | 323 | DIO | | | | | 0.000 | 0.04 | 0.243 | 0.830 | 4.0 | 3.51 | 0.20 | 4.23 | 30.7 | 250 | 204.00 | DI 33 | 3.00 | 122.2 | 2.41 | |
| OUTLET | 329 | 331 | | | | | | | | 0.624 | 2.870 | 3.9 | 9.91 | 0.80 | 10.72 | 41.0 | 250 | 254.00 | DR 35 | 0.41 | 39.7 | 0.78 | 27% |
| OUTLET | 331 | EXMH | | | | | | | | 0.624 | 2.870 | 3.9 | 9.91 | 0.80 | 10.72 | 5.3 | 250 | 254.00 | DR 35 | 0.38 | 38.2 | 0.75 | 28% |
| | | | | | | | | | | | | | | | | | | | | | | | |

Notes:

<u>Definitions:</u>

 1. Q(d) = Q(p) + Q(i)
 Q(d) = Design Flow (L/sec)

 2. Q(i) = 0.28 L/sec/ha
 Q(p) = Population Flow (L/sec)

 3. Q(p) = (PxqxM/86,400)
 Q(i) = Extraneous Flow (L/sec)

Population = 75 Persons/acre
Institutional Peaking factor = 1.5

P = Population (3.4 persons/single unit, 2.7 persons/townhouse, 2.1 persons/apartment, 1.4 persons/retirement residence)

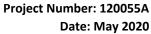
q = Average per capita flow = 350 L/cap/day - Residential

q = Average per gross ha. flow = 35000 L/gross ha/day - Light industrial

q = Average per gross ha. flow = 50000 L/gross ha/day - Commercial/Mixed use

M = Harmon Formula (maximum of 4.0)

Min pipe size 250mm @ min. slope 0.24%





| 4.1 General Content | Addressed (Y/N/NA) | Section | Comments |
|--|-----------------------|---------|--------------|
| Executive Summary (for larger reports only). | NA | | |
| Date and revision number of the report. | Υ | p.1 | |
| Location map and plan showing municipal address, | Υ | Durge | CD STM |
| boundary, and layout of proposed development. | Y | Dwgs | GP, STM |
| Plan showing the site and location of all existing services. | Υ | Dwg | GP |
| Development statistics, land use, density, adherence to | | | |
| zoning and official plan, and reference to applicable | Υ | Intro | |
| subwatershed and watershed plans that provide context | T | IIILIO | |
| to which individual developments must adhere. | | | |
| Summary of Pre-consultation Meetings with City and | N | | |
| other approval agencies. | IN | | |
| Reference and confirm conformance to higher level | | | |
| studies and reports (Master Servicing Studies, | | | |
| Environmental Assessments, Community Design Plans), | Υ | Memo | All sections |
| or in the case where it is not in conformance, the | | | |
| proponent must provide justification and develop a | | | |
| defendable design criteria. | | | |
| Statement of objectives and servicing criteria. | Υ | Memo | |
| Identification of existing and proposed infrastructure available in the immediate area. | Υ | Dwg | GP |
| Identification of Environmentally Significant Areas, watercourses and Municipal Drains potentially impacted by the proposed development (Reference can be made to the Natural Heritage Studies, if available). | NA | | |
| Concept level master grading plan to confirm existing and proposed grades in the development. This is required to confirm the feasibility of proposed stormwater management and drainage, soil removal and fill constraints, and potential impacts to neighboring properties. This is also required to confirm that the proposed grading will not impede existing major system flow paths. | Υ | Memo | |





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| 4.1 General Content | Addressed (Y/N/NA) | Section | Comments |
|--|-----------------------|---------|-----------------------|
| Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts. | NA | | |
| Proposed phasing of the development, if applicable. | NA | | |
| Reference to geotechnical studies and recommendations concerning servicing. | Υ | Memo | |
| All preliminary and formal site plan submissions should have the following information: | | | |
| Metric scale | Υ | | All Drawings |
| North arrow (including construction North) | Υ | | All Drawings |
| Key plan | Υ | | All Drawings |
| Name and contact information of applicant and property owner | Υ | | Drawings/Design Brief |
| Property limits including bearings and dimensions | Υ | | Design Brief |
| Existing and proposed structures and parking areas | Υ | | All Drawings |
| Easements, road widening and rights-of-way | Υ | | All Drawings |
| Adjacent street names | Υ | | All Drawings |





| 4.2 Water | Addressed (Y/N/NA) | Section | Comments |
|---|-----------------------|---------|--------------|
| Confirm consistency with Master Servicing Study, if | Υ | Memo | |
| available. | Y | Memo | |
| Availability of public infrastructure to service proposed | V | Mama | |
| development. | Y | Memo | |
| Identification of system constraints. | Υ | Memo | |
| Identify boundary conditions. | Υ | Memo | And Appendix |
| Confirmation of adequate domestic supply and pressure. | Υ | Memo | And Appendix |
| Confirmation of adequate fire flow protection and confirmation that fire flow is calculated as per the Fire Underwriter's Survey. Output should show available fire flow at locations throughout the development. | Υ | Memo | And Appendix |
| Provide a check of high pressures. If pressure is found to be high, an assessment is required to confirm the application of pressure reducing valves. | Υ | Memo | And Appendix |
| Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defined phases of the project including the ultimate design. | Υ | Memo | |
| Address reliability requirements such as appropriate location of shut-off valves. | Υ | | GP |
| Check on the necessity of a pressure zone boundary modification. | NA | | |
| Reference to water supply analysis to show that major infrastructure is capable of delivering sufficient water for the proposed land use. This includes data that shows that the expected demands under average day, peak hour and fire flow conditions provide water within the required pressure range. | Υ | Memo | And Appendix |
| Description of the proposed water distribution network, including locations of proposed connections to the existing system, provisions for necessary looping, and appurtenances (valves, pressure reducing valves, valve chambers, and fire hydrants) including special metering provisions. | Υ | Memo | |
| Description of off-site required feedermains, booster pumping stations, and other water infrastructure that will be ultimately required to service proposed development, including financing, interim facilities, and timing of implementation. | NA | | |
| Confirmation that water demands are calculated based on the City of Ottawa Design Guidelines. | Y | Memo | |
| Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference. | Υ | | Appendix |



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| 4.3 Wastewater | Addressed (Y/N/NA) | Section | Comments |
|--|-----------------------|---------|----------|
| Summary of proposed design criteria (Note: Wet- weather flow criteria should not deviate from the City of | | | |
| Ottawa Sewer Design Guidelines. Monitored flow data from relatively new infrastructure cannot be used to justify capacity requirements for proposed | Y | Memo | |
| infrastructure). Confirm consistency with Master Servicing Study and/or justifications for deviations. | Υ | Memo | |
| Consideration of local conditions that may contribute to extraneous flows that are higher than the recommended flows in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers. | Υ | Memo | |
| Description of existing sanitary sewer available for discharge of wastewater from proposed development. | Y | Memo | |
| Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable) | Υ | Memo | |
| Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format. | NA | | |
| Description of proposed sewer network including sewers, pumping stations, and forcemains. | Υ | Memo | |
| Discussion of previously identified environmental constraints and impact on servicing (environmental constraints are related to limitations imposed on the development in order to preserve the physical condition of watercourses, vegetation, soil cover, as well as protecting against water quantity and quality). Pumping stations: impacts of proposed development on existing pumping stations or requirements for new | NA NA | | |
| pumping station to service development. Forcemain capacity in terms of operational redundancy, | NA | | |
| surge pressure and maximum flow velocity. Identification and implementation of the emergency overflow from sanitary pumping stations in relation to the hydraulic grade line to protect against basement flooding. | NA | | |
| Special considerations such as contamination, corrosive environment etc. | NA | | |





| 4.4 Stormwater | Addressed (Y/N/NA) | Section | Comments |
|--|-----------------------|---------|----------|
| Description of drainage outlets and downstream constraints including legality of outlet (i.e. municipal drain, right-of-way, watercourse, or private property). | Y | Memo | |
| Analysis of the available capacity in existing public infrastructure. | Υ | Memo | Appendix |
| A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns and proposed drainage patterns. | Υ | | GR, STM |
| Water quantity control objective (e.g. controlling post-development peak flows to pre-development level for storm events ranging from the 2 or 5 year event (dependent on the receiving sewer design) to 100 year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects. | Y | Memo | |
| Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements. | Υ | Memo | |
| Description of stormwater management concept with facility locations and descriptions with references and supporting information. | Υ | Memo | |
| Set-back from private sewage disposal systems. | NA | | |
| Watercourse and hazard lands setbacks. | Υ | | |
| Record of pre-consultation with the Ontario Ministry of Environment and the Conservation Authority that has jurisdiction on the affected watershed. | Υ | Memo | |
| Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists. | Υ | Memo | |
| Storage requirements (complete with calcs) and conveyance capacity for 5 yr and 100 yr events. | Υ | | Appendix |
| Identification of watercourse within the proposed development and how watercourses will be protected, or, if necessary, altered by the proposed development with applicable approvals. | Υ | Memo | |
| Calculate pre and post development peak flow rates including a description of existing site conditions and proposed impervious areas and drainage catchments in comparison to existing conditions. | Y | | Appendix |
| Any proposed diversion of drainage catchment areas from one outlet to another. | NA | | |



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| Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and SWM facilities. | Υ | Memo | And Appendix |
|--|---|------|--------------|
| If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post-development flows up to and including the 100-year return period storm event. | Υ | Memo | And Appendix |

| 4.4 Stormwater | Addressed (Y/N/NA) | Section | Comments |
|---|-----------------------|---------|----------|
| Identification of municipal drains and related approval requirements. | Υ | Memo | |
| Description of how the conveyance and storage capacity will be achieved for the development. | Y | Memo | |
| 100 year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading. | Y | | Appendix |
| Inclusion of hydraulic analysis including HGL elevations. | Υ | | Appendix |
| Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors. | Υ | Memo | |
| Identification of floodplains – proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions. | Υ | | |
| Identification of fill constrains related to floodplain and geotechnical investigation. | NA | | |





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| 4.5 Approval and Permit Requirements | Addressed (Y/N/NA) | Section | Comments |
|--|-----------------------|---------|----------|
| Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act. | Υ | Memo | |
| Application for Certificate of Approval (CofA) under the Ontario Water Resources Act. | NA | | |
| Changes to Municipal Drains. | NA | | |
| Other permits (National Capital Commission, Parks | | | |
| Canada, Public Works and Government Services Canada, | NA | | |
| Ministry of Transportation etc.) | | | |

| 4.6 Conclusion | Addressed (Y/N/NA) | Section | Comments |
|---|--------------------|---------|----------|
| Clearly stated conclusions and recommendations. | Υ | Memo | |
| Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency. | NA | | |
| All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario. | Υ | Memo | |