



Site Servicing and Stormwater Management Report Hazeldean Crossing

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Project Name
Hazeldean Crossing

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Hazeldean Crossing Inc.

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Table of Contents

1	Introduction	1
2	Geotechnical Considerations	4
3	Deviations	4
4	Watermain Servicing.....	4
4.1	Methodology.....	4
4.2	Design Criteria.....	4
4.3	Fire Flow Requirements.....	6
4.4	Boundary Conditions	7
4.5	Proposed Servicing and Calculations.....	8
4.5.1	Watermain Design	8
4.5.2	Modelling Scenarios.....	8
4.6	Simulation Results.....	8
4.6.1	Modelling Results.....	8
4.7	Review of Hydrant Spacing.....	10
5	Sanitary Sewer Design	10
5.1	Offsite Sanitary Sewer Analysis	11
6	Stormwater Management	13
6.1	Pre-Development Conditions	13
6.1.1	Estimation of Time of Concentration.....	13
6.1.2	Runoff Coefficients.....	13
6.1.3	Pre-Development Peak Flows.....	14
6.2	Calculation of Allowable Release Rate.....	15
6.3	Post-Development Conditions.....	16
6.4	Design Criteria.....	16
6.4.1	Minor System Design Criteria.....	16
6.4.2	Major System Design Criteria.....	16
6.5	Runoff Coefficients	16
6.6	Minor System (Storm Sewer) Design	17
6.6.1	Allowance for Foundation Drainage.....	17
6.7	Stormwater Management Modelling.....	17
6.7.1	Hydrologic/Hydraulic Analysis	18
6.7.2	Subcatchment Parameters.....	18
6.7.3	Storage Node Parameters for Underground Chambers	19
6.7.4	Storage Node Parameters for Surface Ponding Areas (Offsite).....	20
6.7.5	Outlet Node Parameters	20
6.7.6	Inlet Control at Flow-By Conditions	21
6.8	Dual Drainage Modelling.....	21
6.9	Storm Events Modelled.....	22
6.9.1	Modelling Results.....	22
6.9.2	Underground Storage.....	23

6.10	Hydraulics	24
6.10.1	Hydraulic Grade Line Analysis	24
6.10.2	Offsite Inlet Control Devices.....	24
6.11	Quality Control Measures	25
6.12	Water Balance.....	25
7	Erosion and Sediment Control.....	27
8	Conclusions	28

List of Tables

Table 4-1: Summary of Fire Flow Requirements for All Buildings	7
Table 4-2: Summary of Results of Scenario 1A for Peak Hour	8
Table 4-3: Summary of Results of Scenario 1B for Peak Hour	9
Table 4-4: Summary Results of Scenario 2B for Maximum Day Plus Fire Flow.....	9
Table 6-1: Summary of Pre-Development Average Runoff Coefficients – Pre-Development.....	14
Table 6-2: Summary of Pre-Development Peak Flows	15
Table 6-1: Summary of Average Runoff Coefficients – Post Development.....	17
Table 6-3: General Subcatchment Parameters	18
Table 6-4: Post-Development Subcatchment Parameters	19
Table 6-5: Volumes of Underground Chambers	19
Table 6-6: Storage Node Parameters for Underground Chambers	19
Table 6-8: Outlet (ICD) Node Parameters	20
Table 6-9: Rating Curves for Surface Catchbasin with Mountable Curb & Gutter in Flow-By Condition (3% cross fall, 2% slope).....	21
Table 6-8: Peak Flows at Outfalls	23
Table 6-9: Comparison of Pre-Development and Post-Development Peak Flows	23
Table 6-10: Summary of Storage Based on Modelling Results	23
Table 6-11: Design Parameters Used for Oil Grit Separator Sizing.....	25
Table B1: Water Demand Chart.....	B
Table B2: Fire Flow Contribution Based on Hydrant Spacing	B
Table B3: Fire Flow Requirements based on FUS, 1999 – Block 1.....	B
Table B4: Fire Flow Requirements based on FUS, 1999 – Block 2.....	B
Table B5: Fire Flow Requirements based on FUS, 1999 – Block 3.....	B
Table B6: Fire Flow Requirements based on FUS, 1999 – Block 4.....	B
Table B7: Fire Flow Requirements based on FUS, 1999 – Block 5.....	B
Table B8: Fire Flow Requirements based on FUS, 1999 – Block 6.....	B
Table B9: Fire Flow Requirements based on FUS, 1999 – Block 7.....	B
Table B10: Fire Flow Requirements based on FUS, 1999 – Block 8.....	B
Table B11: Fire Flow Requirements based on FUS, 1999 – Block 9.....	B
Table B12: Fire Flow Requirements based on FUS, 1999 – Block 10.....	B
Table B13: Fire Flow Requirements based on FUS, 1999 – Block 11.....	B
Table B14: Fire Flow Requirements based on FUS, 1999 – Block 12.....	B
Table D1: Sanitary Sewer Calculation Sheet.....	D

Table E1: Estimation of Catchment Time of Concentration (Pre-Development)	E
Table E2: Estimation of Peak Flows (Pre-Development) Using Calculated Time of Concentrations	E
Table E3: Estimation of Allowable Peak Flows (Based on 5-yr Pre-Development Rates and Max C-0.50 and Tc=10mins).....	E
Table E4: Average Runoff Coefficient (Post-Development).....	E
Table E5: Summary of Post Development Peak Flows (Uncontrolled and Controlled).....	E
Table E6: Summary of Post Development Storage	E
Table E7: Storage Volumes for 2-yr, 5-yr, 100-yr Storms Based on Modified Rational Method (Site 1).....	E
Table E8: Storage Volumes for 2-yr, 5-yr, 100-yr Storms Based on Modified Rational Method (Site 2).....	E
Table E9: MC-3500 Site Calculator for Chambers 1 (Site 1).....	E
Table E10: MC-3500 Site Calculator for Chambers 2 (Site 2).....	E
Table E11: MC-3500 Cumulative Storage Vs Depth Table (Site 1).....	E
Table E12: MC-3500 Cumulative Storage Vs Depth Table (Site 2).....	E
Table E13: 2-year Storm Sewer Calculation Sheet.....	E
Table E14: Major System (street segment) Characteristics	E
Table E15: Surface Ponding Area-Depth (total 3 pages).....	E

List of Figures

Figure 1 – Representation of Rating Curves for Modelling of Storage at Ponding Locations	20
Figure 2 - Model Schematic Illustrating Subcatchments, Links, Nodes, Outlets (ICDs)	22
Figure 3 – 100-year HGL (Main Storm Sewer).....	24
Figure A1: Site Location Plan	A
Figure A2: Water Distribution Plan.....	A
Figure A3: Water Demand Allocation Plan	A
Figure A4: Fire Hydrant Location Plan	A
Figure A5: Exposure Distances (FUS)	A
Figure A6: Sanitary Drainage Area Plan – Onsite Sewers.....	A
Figure A7: Sanitary Drainage Area Plan - Offsite Sewers.....	A
Figure A8: Pre-Development Drainage Area Plan.....	A
Figure A9: Inlet Control Devices (ICDs) in offsite Catch Basins	A
Drawing C400: Post Development Storm Drainage Plan.....	A

List of Appendices

- Appendix A – Figures
- Appendix B – Water Servicing Design Tables
- Appendix C – WaterGems Output Tables
- Appendix D – Sanitary Sewer Design Tables
- Appendix E – Stormwater Design Tables
- Appendix F – Stormceptor Sizing
- Appendix G – PCSWMM Data
- Appendix H – Correspondence
- Appendix I – Manufacturer Information
- Appendix J – Background Information
- Appendix K – Drawings
- Appendix L – Checklist

1 Introduction

1.1 Site Description and Proposed Development

Hazeldean Crossing Inc. retained EXP Services Inc. (EXP) to prepare a site servicing and stormwater management report for a proposed residential infill development.

The 0.9641-hectare development site is situated at the corner of Hazeldean Road and Victor Street in the City of Ottawa, Ontario as shown on Figure A1 in Appendix A. The site is within Ward 6 or Stittsville Ward.

The proposed site development consists of two (2) property parcels located in Lots 25 and 26, Concession 11, Geographic Township of Goulbourn, City of Ottawa. The following describes the two properties:

- 5924 Hazeldean Road. PIN 04462-0476, Part of Lot 26, on Registered Plan 4R-7332
- 5938 Hazeldean Road. PIN 04462-0475, Parts 1 & 2 on Registered Plan 4R-10078

The proposed development will be comprised of 76 stacked townhome units, and 10 traditional townhomes. Access to the properties will be from a single access off Victor Street. A copy of the topographic survey and the proposed site plan are provided in Appendix J.

This report will discuss the adequacy of the adjacent municipal storm sewers, sanitary sewers and watermains to convey the storm runoff, sewage flows and provide the water demands that will result from the proposed development. This report provides a design brief for submission, along with the engineering drawings, for City approval.

1.2 Background Documents

Various design guidelines were referred to in preparing the current report including:

- Sewer Design Guidelines, Second Edition, Document SDG002, October 2012, City of Ottawa including:
 - Technical Bulletin ISDTB-2012-4 (20 June 2012)
 - Technical Bulletin ISDTB-2014-01 (05 February 2014)
 - Technical Bulletin PIEDTB-2016-01 (September 6, 2016)
 - Technical Bulletin ISDTB-2018-01 (21 March 2018)
 - Technical Bulletin ISDTB-2018-04 (27 June 2018)
- Ottawa Design Guidelines – Water Distribution, July 2010 (WDG001), including:
 - Technical Bulletin ISDTB-2014-02 (May 27, 2014)
 - Technical Bulletin ISTB-2018-02 (21 March 2018)
- Stormwater Management Planning and Design Manual, Ontario Ministry of the Environment and Climate Change, March 2003 (SMPDM).

- Design Guidelines for Drinking-Water Systems, Ontario Ministry of the Environment and Climate Change, 2008 (GDWS).
- Fire Underwriters Survey, Water Supply for Public Fire Protection (FUS), 1999.
- Ontario Building Code 2012 (OBC), Ministry of Municipal Affairs and Housing.
- Ontario Ministry of Transportation (MTO) Drainage Manual, 1995-1997.

1.3 Existing Infrastructure

For the purpose of this report, reference is made to the two properties as: Site #1 and Site #2. The following summarizes the areas of each.

- Site # 1 (eastern) at 5924 Hazeldean Road. Area 0.4995 hectares.
- Site # 2 (western) at 5938 Hazeldean Road. Area 0.4646 hectares.

Site # 1 is a vacant parcel located at the corner of Victor and Hazeldean Road. The site appears to have never been developed based on City of Ottawa aerial images to as far back as 1976. The overall topography of Site # 1 is directed in a northerly direction and ranges from elevation ±115.0m to ±112.75m. The exiting ground cover within this property consists of grass with some mature trees along the eastern boundary of the property.

Site #2 contains a gas station and service garage that is abandoned and will be demolished for the redevelopment of the site. The following summarizes the onsite and offsite existing utilities:

Within Site #1

- 450mm storm sewer and catchbasin stubbed just inside property (off Victor Street)
- 150mm watermain c/w Valve & Valve Box stubbed just inside property (off Victor Street)
- 200mm sanitary sewer and manhole stubbed just inside property (off Victor Street)

Within Site #2

- The services for the former gas station will need to be abandon prior to demolition.

On Victor Street Along Frontage of Site #1

- 375mm storm sewers
- 250mm sanitary sewer
- 200mm watermain
- Underground Bell & Rogers
- 50mm Enbridge Gas main
- Overhead and underground Hydro
- Underground Streetlighting

On Hazeldean Road Along Frontage of Site #1 & Site @2

- 525mm & 2400mmx1800mm storm sewer
- 300mm & 450mm sanitary sewers
- 305mm & 762mm watermains
- Bell / Hydro / Telecom Ottawa/ Traffic. Status to be confirmed with the utility providers
- Underground 150mm & 300mm Gas

- Underground Bell & Rogers
- Underground Traffic plant
- Underground Streetlighting

The as-built drawings for both Victor Street and Hazeldean Road were obtained from the City Vault, and are included in Appendix I for reference.

1.4 Consultation and Permits

A pre-consultation meeting was held between Hazeldean Crossing Inc. and the City on November 8, 2018. This meeting outlined the submission requirements and provided information to assist with the development proposal.

For the onsite stormwater system, generally an ECA would be required for any stormwater management facilities. Stormwater Management (or SWM) Facilities are defined by any stormwater works used for the treatment, retention, infiltration or control of stormwater. However, an Approval Exemption under Ontario Regulation 525/98 can be applied. Under Section 3 of O'Reg 525/98, Section 53 (1) and (3) do not apply to the alteration, extension, replacement or a change to a stormwater management facility that 1) is designed to service one lot or parcel of land, b) discharges into a storm sewer that is not a combined sewer, c) does not service industrial land or a structure located on industrial land, and finally d) is not located on industrial land. If the property parcels noted in Section 1.1 are merged into one property parcel, this would satisfy the Approval Exemptions under O'Reg 525/98, and not require a stormwater ECA. Therefore, the ECA application should apply to the onsite storm and sanitary sewers only.

A small section of new sanitary sewer on Victor Street will be required to service the townhomes fronting the municipal street. In this case an ECA will be required for the municipal sewage works, which are owned by the City of Ottawa. This ECA will be filled under the Transfer of Review (ToR) process.

Prior to City signoff on the infrastructure design a pre-consultation meeting will be held with the local MECP, to confirm ECA requirements.

The proposed site is located within the Mississippi Valley Conservation Authority (MVCA) jurisdiction, therefore signoff from the MVCA will be required prior to Site Plan approval. The MVCA has been contacted to discuss the stormwater management quality control requirements.

2 Geotechnical Considerations

A geotechnical investigation was completed by EXP and was prepared to establish the subsurface and groundwater conditions and to provide recommendations related to excavation, foundation design, backfilling requirements, site grading, pipe bedding, pavement structure.

Within Site # 1 a thin layer of topsoil ranging from 0.0m to 0.9m is underlaid by bedrock. Some areas of the site have rock exposed at the surface. It appears that the overburden on most of the site has been removed.

Within Site # 2, thicker amounts of overburden ranging between 0.8 and 3.6m existing sand/till backfill.

Eleven boreholes were drilled. Within Site # 1 the groundwater table is expected at between 2.1 metres and 3.9 metres below existing grade. For site # 2 the groundwater table is expected at between 1.5 metres and 3.0 metres. A summary of the groundwater table elevations, as taken from the geotechnical report are illustrated on the grading plan.

A maximum grade raise requirement of 2.0m was established for the site. The recommended pavement structure was established at: 40mm + 50mm of asphalt, 150mm granular "A" and a maximum 400mm depth of Granular "B".

3 Deviations

There are no noted deviations from the City Design Standards (SDG002).

4 Watermain Servicing

4.1 Methodology

The water service for the proposed site is designed in accordance with the City Design Guidelines (July 2010). The following steps indicate the basic methodology that was used in the hydraulic analysis:

- Estimated water demands under average day, maximum day and peak hour conditions. As the total site population was below 500, residential peaking factors were interpolated based on MOE Table 3-3.
- Estimated the required fire flow (RFF) for each building block based on the Fire Underwriters Survey (FUS).
- Obtained hydraulic boundary conditions (HGL) from the City, based on the above water demands and required fire flows.
- Boundary condition data and water demands were used to estimate the pressure at the proposed site, and this was compared to the City's of Ottawa's design criteria.

4.2 Design Criteria

We estimated the domestic water demands as shown below, using parameters from the WDG001 as follows:

Pressure Zone

Proposed site located in zone = 3W

Number of Units

Stacked townhomes	=	76
Traditional townhomes	=	10

Densities

2-bedroom units (persons per unit)	=	2.1
Townhomes	=	3.7

Residential Populations

76, 2-bedroom units (@ 2.1 persons per unit)	=	159.6
10, Townhomes (@ 2.7 persons per unit)	=	<u>27.0</u>
	=	186.6

Demand Rates

Average Residential Demands (L/person/day) = 350

Peaking Factors

Max Day Residential Peaking Factor (as per MOE Table 3-3)	=	4.58 x avg. day
Peak Hour Residential Peaking Factor (as per MOE Table 3-3)	=	6.91 x avg. day

Watermain Design

C factor (200 mm – 300 mm)	=	110
Minimum Allowable Pressure	=	275 kPa (40 psi)
Maximum Allowable Pressure	=	690 kPa (100 psi)
Minimum Static Pressure (Under Fire Flow Conditions)	=	140 kPa (20 psi)

Residential Water Demands

Average Residential Demands
 $186.6 \text{ persons} \times 350 \text{ L/person/day} \times (1/86,400 \text{ sec/day})$ = 0.76 L/sec

Total Water Demands

Avg Day Demands =	=	0.76 L/sec
Maximum Day Demands = 0.76×4.58	=	3.46 L/sec
Peak Hour Demands = 0.76×6.91	=	5.22 L/sec

The average day, maximum day, and peak hourly demands for the proposed site at 5924 Hazeldean are 0.76 L/sec 3.46 L/sec, 5.22 L/sec, respectively. Please note that the maximum day and peak hour factors, noted above, were determined based on MOECC GDWS Table 3-3 as the population of the proposed development is less than 500 persons.

This requirement is noted in Section 4.2.8 of the City's WDG001. Detailed calculations of the domestic water demands are provided in Table B1 in Appendix B. The distribution of demands (or allocation) is illustrated in Figure A3.

4.3 Fire Flow Requirements

Water for fire protection will be available utilizing the proposed fire hydrants located along the adjacent roadways: Victor Street, and Hazeldean Road. The required fire flows for the proposed site were calculated based on typical values as established by the Fire Underwriters Survey 1999 (FUS).

The following equation from the Fire Underwriters document "Water Supply for Public Fire Protection", 1991, was used for calculation of the on-site supply rates required to be supplied by the hydrants:

$$F = 200 * C * \sqrt{A}$$

where

- F = Required Fire flow in Litres per minute
- C = Coefficient related to type of Construction
- A = Total Floor Area in square metres

A reduction for low hazard occupancy of -15% for residential dwellings, and an increase for fire area exposure of was used. Calculations of the Required Fire Flows (RFF), based on the FUS Method, for each residential block is provided in Appendix B.

The following details the fire flow requirements for the most critical residential block (Block 4).

Type of Construction	=	Wood Framed Construction
Coeff Related to Construction	=	1.5
Basement (more than 50% above ground)	=	310 m ²
1 st to 3 rd Floor Area	=	310 m ²
Number of Floors	=	4
Fire Flow Requirement, FF	=	200 * 1.5 * \sqrt{A}
	=	200 * 1.5 * $\sqrt{(4 \times 310m^2)}$
	=	11,620 L/min or 12,000 L/min (rounded up)
Occupancy Class	=	Limited Combustible
Occupancy Charge	=	-15%
Fire Flow Requirement, FF (with reduction due to occupancy)	=	12,000 *-15%
	=	-1,200 L/min
	=	10,200 L/min
Reductions due to Sprinklers	=	No reduction.
Charges Due to Exposures	=	sum for all sides
	=	18% + 8% + 5% + 12% = 43%
Required Fire Flow (RFF)	=	10,200 L/min + 4,386 L/min
	=	14,586 L/min
	=	15,000 L/min (rounded to closest 1,000) = 250 L/sec

The following table summarizes the required fire flows for all buildings, which include the reductions, and/or increases due to occupancy, sprinklers systems and exposures. These fire flows have been calculated based on the FUS method and the City of Ottawa Water Distribution Guidelines (WDG001), and the latest Technical Bulletin.

Table 4-1: Summary of Fire Flow Requirements for All Buildings

Block	Description	¹No of Storeys	Fire Flow, (L/min)	²Type of Constr. Coeff, C	³Reduction Due to Occupancy (%)	⁴Total Increase from Exposures	⁵,⁶Req's Fire Flow	
							(L/min)	(L/sec)
1	Townhomes	2+	11,000	1.5	-15%	45%	14,000	233
2	Stacked townhomes	3+	9,000	1.5	-15%	49%	11,000	183
3	Stacked townhomes	3+	7,000	1.5	-15%	40%	8,000	133
4	Stacked townhomes	3+	12,000	1.5	-15%	43%	15,000	250
5	Stacked townhomes	3+	9,000	1.5	-15%	67%	13,000	217
6	Stacked townhomes	3+	7,000	1.5	-15%	52%	9,000	150
7	Stacked townhomes	3+	9,000	1.5	-15%	48%	11,000	183
8	Stacked townhomes	3+	9,000	1.5	-15%	51%	12,000	200
9	Stacked townhomes	3+	7,000	1.5	-15%	51%	9,000	150
10	Stacked townhomes	3+	9,000	1.5	-15%	62%	12,000	200
11	Stacked townhomes	3+	9,000	1.5	-15%	36%	10,000	167
12	Stacked townhomes	3+	7,000	1.5	-15%	25%	7,000	117

1 - If basements are included (<50% below grade) then denoted as +.
 2 - Types of constructions: 0.8 for non-combustible, 1.0 for ordinary construction, 1.5 for wood frame construction.
 3 - Reductions due to Occupancy are -25% for non-combustible or -15% for limited combustible.
 4 - Increase due to exposures were calculated based on FUS and technical bulletin ISTB-2018-02.
 5 - Required Fire Flows are rounded to nearest 1,000 L/min.

4.4 Boundary Conditions

Hydraulic Grade Line (HGL) boundary conditions were obtained from the City for design purposes. A copy of the correspondence received from the City is provided in Appendix F. Boundary conditions at three (3) connection locations were requested from the City. Connections # 1 & 3 were used for modelling as it represents the closest junction to the boundary conditions. The following hydraulic grade line (HGL) boundary condition was provided:

- | | | |
|-------------------------|-------------------|-------------------|
| • Demand Condition | HGL Connection #1 | HGL Connection #3 |
| • Maximum = | 160.9 m | 160.8 m |
| • Max Day + Fire Flow = | 135.4 m | 158.3 m |
| • Peak Hour = | 157.2 m | 157.3 m |

The above noted HGL's are based on a ground elevation of approximately 114.0 m and 114.3 m at boundary conditions #1 and #3 respectively. This results in a system water pressure of 43.2 m (or 61.4 psi) and 43.0m (or 61.2 psi) at the connection points during peak hour conditions.

4.5 Proposed Servicing and Calculations

4.5.1 Watermain Design

Since the average day demands of 65.3 m³ per day exceed 50 m³ per day, two separate watermain connections for the site will be necessary as per Section 4.31 of the WDG001.

4.5.2 Modelling Scenarios

A total of five (4) scenarios were analyzed. The performance of the proposed water distribution system within the development was analyzed under each scenario. The following summarizes the modelling scenarios that were analyzed. Please refer to Figure A2 in Appendix A which illustrates the water distribution layout.

- Scenario 1A Peak Hour (using connection #1)
- Scenario 1B Peak Hour (using connection #3)
- Scenario 2A Max Day Plus Fire Flow (using connection #1)
- Scenario 2B Max Day Plus Fire Flow (using connection #3)

4.6 Simulation Results

4.6.1 Modelling Results

The results of the WaterCAD modelling under maximum day plus fire flow and peak hourly conditions are summarized in Table 4-2 and Table 4-3 below for Scenarios 1 and 2. These results are based on a hydraulic boundary condition on Victor Street where the private watermain connect to the municipal 200mm diameter watermain. The complete results for all scenarios are provided in Appendix C.

Table 4-2: Summary of Results of Scenario 1A for Peak Hour

Junction	Elevation (m)	Demand (L/s)	Hydraulic Grade (m)	Pressure (psi)
J-1	114.36	0.38	157.20	60.8
J-2	114.00	0.00	157.20	61.3
J-3	114.00	0.62	157.20	61.3
J-4	113.95	1.17	157.19	61.4
J-5	114.36	0.00	157.20	60.8
J-6	114.50	1.76	157.19	60.6
J-7	114.32	0.82	157.19	60.9
J-8	113.90	0.00	157.19	61.5
J-9	115.45	0.47	156.84	58.8
J-10	113.20	0.00	157.20	62.5
J-12	114.00	0.00	157.20	61.3

Table 4-3: Summary of Results of Scenario 1B for Peak Hour

Junction	Elevation (m)	Demand (L/s)	Hydraulic Grade (m)	Pressure (psi)
J-1	114.36	0.38	157.30	60.9
J-2	114.00	0.00	157.29	61.5
J-3	114.00	0.62	157.29	61.5
J-4	113.95	1.17	157.29	61.5
J-5	114.36	0.00	157.30	61.0
J-6	114.50	1.76	157.30	60.7
J-7	114.32	0.82	157.29	61.0
J-8	113.90	0.00	157.29	61.6
J-9	115.45	0.47	156.95	58.9
J-10	113.20	0.00	157.30	62.6
J-12	114.00	0.00	157.30	61.5

The calculated minimum and maximum working pressures anticipated within the development range from 58 psi to 62.6 psi under peak hour conditions. This meet the minimum 40 psi as per City of Ottawa Guidelines. Table 4-4 below provides the results of scenarios 2 under maximum day plus fire flow conditions. It should be noted that for Scenario 2A, onsite fire hydrants H-1, and H-2 were only able to provide 171 and 201 L/sec. This scenario was used to confirm if a single watermain feed from connection #1 (Victor Street / Denham Way) would be able to deliver appropriate fire flows. It was determined that a feed from Hazeldean Rd (Connection #3) would be necessary. Complete fire flow results are provided in Appendix C.

Table 4-4: Summary Results of Scenario 2B for Maximum Day Plus Fire Flow

Hydrant Node	Fire Flow Required (L/sec)	Total Flow Available Based on Model Results (L/sec)	Satisfies Fire Flow Constraints?
H-1	250	>250	Yes
H-2	250	>250	Yes
H-3	250	>250	Yes

Under Maximum Day + Fire Flow conditions the available fire flows are in excess of the required fire flows (RFF) at all junctions, and therefore meeting the City of Ottawa watermain design criteria. Additional information on the available fire flows from each hydrant based on the City's Technical Bulletin 2018-02 is provided Table B2 of Appendix B, and the proceeding section.

4.7 Review of Hydrant Spacing

A review of the hydrant spacing was completed to ensure compliance with Appendix I of Technical Bulletin ISTB-2018-02. As per Section 3 of Appendix I all hydrants within 150 metres were reviewed to assess the total possible contribution of flow from these contributing hydrants. For each hydrant the distance to the proposed site was determined to arrive at the contribution of fire flow from each. All hydrants are expected to be of Class AA as per Section 5.1 of Appendix I.

Table B2 in Appendix C summarizes all fire hydrants within a 150m distance from the proposed site. For each hydrant the straight-line distance, distance measured along a fire route or roadway, whether its location is accessible, and its contribution to the required fire flow. Figure A4 in Appendix A illustrates the hydrant locations in proximity to the site. Only the hydrants that are accessible, as per Appendix I of ISTB-2018-02, were used.

For the critical Block 4, the total available contribution of flow from all hydrants was estimated as 15,200 L/min, which exceeds the required fire flow of 15,000 L/min as identified in Appendix I of Technical Bulletin ISTB-2018-02. All other Blocks will also receive enough fire flow contribution from the newly proposed and existing surrounding hydrants. Three onsite fire hydrants will be necessary to meet the require fire flows based on the City's guidelines.

5 Sanitary Sewer Design

The sanitary sewer system is designed based on a population flow and an area-based infiltration allowance. The flows were calculated using City sewer design guidelines (SDG002) as follows:

Area

Gross site area	=	0.9641 ha
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Number of Units

2-bedroom units	=	76
Townhomes	=	10

Densities

2-bedroom units (persons per unit)	=	2.1
Townhomes (persons per unit)	=	2.7

Residential Populations

76, 2-bedroom units (@ 2.1 persons per unit)	=	159.6
10, Townhomes (@ 2.7 persons per unit)	=	27.0
	=	186.6

Residential Peaking Factor

Peak Factor = $1 + 14 / (4 + (P/1000)^{0.5}) * K$, where $K = 0.8$	=	
Peak Factor = $1 + 14 / (4 + (186.6/1000)^{0.5}) * 0.8$	=	3.53

Domestic Sewage Flow

Average Domestic Flow ($186.6 \times 280 \text{ L/cap/day} \times (1/86,400 \text{ sec/day})$)	=	0.605 L/sec
Peak Domestic Flow (3.53×0.605)	=	2.13 L/sec

Infiltration

Infiltration Allowance	=	0.33 L/ha/sec
Infiltration Flow (0.9641 ha x 0.33 L/ha/sec)	=	0.32 L/sec

Total Peak Sewage Flow

Peak Sanitary Flow = 2.13 + 0.32	=	2.45 L/sec
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The estimated peak sanitary flow rate from the proposed development at is **2.45 L/sec** based on City Design Guidelines.

The proposed development will have a sanitary sewer connection to the existing 250mm sanitary sewer on Victor Street. The proposed connection point is just south of the location of Manhole MHSA9001. It is proposed that the location of MHSA9001 will be adjusted slightly to accommodate the sanitary sewer from the site. The 200mm sanitary sewer through the site is proposed with a minimum 0.35% slope, having a capacity of 19.7 L/sec based on Manning's Equation under full flow conditions.

5.1 Offsite Sanitary Sewer Analysis

The proposed sanitary sewer within the development site will discharge to a 250mm sanitary sewer on Victor Street. An analysis of the existing sanitary infrastructure was conducted to determine the capacity of the existing system and determine if the existing infrastructure could handle the anticipated additional flows to the overall system due to the new development proposed at 5924 Hazeldean.

Existing Conditions

Area	=	12.113 hectares
Residential Density for Townhome	=	2.7 person/unit
Residential Density for 2-bedroom apartment	=	2.1 person/unit
Residential Density for Single home	=	3.4 person/unit
Residential Density for Semi-detached home	=	3.4 person/unit
Average Residential Flow Allowance	=	280 L/per/day
Residential Peaking Factor	=	Harmon Formula
Commercial Flow Allowance	=	28,000 L/ha/fay
Commercial Peaking Factor	=	1.5

To confirm adequate capacity is available in the downstream system a review of the as-constructed conditions was completed and the peak sewage rates were re-calculated based on current City Guidelines.

Figure A4 in Appendix A illustrates the off-site sanitary sewers and tributary drainage area. It consists of only residential homes. Using the City's urban site GIS layer, it was determined that there is approximately 12.113 hectares (250 homes) of residential lands tributary to the outlet sewer (sanitary manhole # 09013). The proposed development at 5924 Hazeldean Road will contain 76 2-bedroom suites, and 10 townhomes. The sewage flows, based on current City Guidelines, were re-calculated as follows:

Townhomes	=	10
2-bedroom apartment	=	76
Single home	=	158
Semi-detached home	=	6
10-Townhomes x 2.7 person/unit	=	27 persons
76-2 Bedroom apartments x 2.1 person/unit	=	159.6 persons
158-Residential Density for Single Home x 3.4 person/unit	=	537.2 persons
6-Residential Density for Single Home x 2.7 person/unit	=	16.2 persons
Residential Population = 27 + 159.6 + 537.2 + 16.2	=	740 persons

Residential Sewage Flow

Residential Flow Allowance	=	280 L/person/day
Correction Factor, K	=	0.8
Peak Factor = $1 + (14 / (4 + (P/1000)^{0.5})) * K$	=	
Peak Factor = $1 + (14 / (4 + (740/1000)^{0.5})) * 0.8$	=	
Peak Factor = $1 + (2.88) * 0.8$	=	3.30
Avg. Domestic Flow = $740 \times 280 \text{ L/person/day} \times (1/86,400 \text{ sec/day})$	=	2.398 L/sec
Peak Domestic Flow = $2.398 \text{ L/sec} \times 3.30$	=	7.91 L/sec

Extraneous Flows

Total Area	=	12.113 hectares
Extraneous Flow Allowance	=	0.33 L/ha/sec
Extraneous Flows = (0.33×12.113)	=	4.0 L/sec

Total Sewage Flow

Total Sanitary Flow (at last manhole from design sheet)	=	12.20 L/sec
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The calculated peak sewage flows under full build-out conditions within the existing system is calculated to be 12.20 L/sec including the proposed development at 5294 Hazeldean. It should be noted that the residential sanitary flow allowance is now 280 L/person/day as per Technical Bulletin ISTB-2018-01, and therefore the existing infrastructure is conservatively designed in accordance with today's standard guidelines.

The maximum percent (%) full capacity within with sanitary sewer system was determinized to be 36% between sewer runs 09012 and 09013, two sewer sections downstream of the proposed sewer connection from site. Existing sanitary sewer invert elevation data was taken from the City's website. It can be concluded that the existing sanitary sewer system can support the proposed development.

6 Stormwater Management

6.1 Pre-Development Conditions

6.1.1 Estimation of Time of Concentration

The time of concentration for the pre-development subcatchments were determined using both the Airport Method (Federal Aviation Administration), and the Bransby-Williams Method. The Airport Formula is suited well for undisturbed land and is typically used for drainage areas with a runoff coefficient of less than 0.40. The Bansby-Williams Method applies more for catchments with a runoff coefficient greater than 0.40.

From the MTO Drainage Manual the Airport Formula and the Bansby-Williams Methods used are as follows:

$$T_c = 3.26 * (1.1 - C) * L^{0.5} / S_w^{0.33} \quad \text{Federal Aviation Method (Airport Method)}$$

$$T_c = 0.057 * L / (S_w^{0.2} * A^{0.1}) \quad \text{Bansby-Williams Method}$$

where:

Tc	=	Time of Concentration (minutes)
C	=	Runoff Coefficient
S _w	=	Watershed Slope (%)
L	=	Watershed Length (m)

The watershed length and slope that were used were determined by using the topographic survey and the 85/10 Slope Method. Detailed calculations for each catchment are provided in Table E1 of Appendix E for reference.

The calculation of the tie of concentrations were used simply for comparison with standards design values only. The use of short time of concentrations will result in higher peak flows. General practice would be to use a consistent time of concentration of 10 minutes under pre and post development conditions.

6.1.2 Runoff Coefficients

Runoff coefficients used for pre-development conditions were based on actual areas. Runoff coefficients for impervious surfaces (roofs, asphalt, and concrete) were taken as 0.90, whereas those for pervious surfaces (grass/landscaping) were taken as 0.20. Average runoff coefficients for all catchments (both pre-development and post-development) were calculated using PCSWMM's area weighting routine.

This modelling software has a GIS engine which allows for catchment (or polygon) definition including attributes. The runoff coefficients for all catchments were area weighted to derive at average runoff coefficients based on hard surfaces (concrete or asphalt) having an imperviousness of 100%, soft surfaces (landscaping surfaces) having a zero percent imperviousness. The conversion from an imperviousness percent to a runoff coefficient was taken as $C = (\text{IMP} * 0.70) / 100 + 0.20$, with the imperviousness (IMP) as a percentage. Additional information is provided in Appendix E.

The pre-development and post-development average runoff coefficients for each site property is summarized in the following table.

Table 6-1: Summary of Pre-Development Average Runoff Coefficients – Pre-Development

Location	Area (hectares)	Imperviousness (%)	Avg. Runoff Coefficient (C_{AVG})
Site 1 (east)	0.4995	0	0.20
Site 2 (west)	0.4645	48.4	0.54
Total or average	0.9640	22.8	0.36

6.1.3 Pre-Development Peak Flows

The combined 0.9642-hectare sites are currently vacant, with the exception of a small former gas station building within the western property. From the existing ground elevations shown on the grading plan, there are two overland flow routes which discharge runoff to both Hazeldean Road and Victor Street.

Pre-development subcatchments are derived from PCSWMM using the watershed Delineation Tool. Subcatchments tributary to each OUTFALL were delineated into PRE_S01, PRE_S02 and PRE_S03 as shown FIGURE A8. The pre-development runoff coefficient for the entire development site was determined to be 0.36. From Figure A8, a small portion of the runoff from the site is directed northerly to catchbasins on Hazeldean Road, whereas the majority is easterly directed to Victor Street.

The time of concentration for each pre-development subcatchment was determined to range from 1.2 to 5.1 minutes. However, since the time of concentration under post-development was set at standard 10min as per City Guidelines, the allowable discharge release rates from the site were established using the peak flows derived with a standard time of concentration of 10 minutes. Using the lower calculated time of concentrations under pre-development conditions would artificially raise the peak flows.

For comparison, the pre-development peak flows, based on a calculated time of concentration were determined for the 2-year, 5-year and 100-year storms using the Rational Method. Detailed calculations for each drainage area (or catchment) is provided in Appendix E.

$$Q_{PRE} = 2.78 C I A$$

where:

Q_{PRE}	=	Peak Discharge (L/sec)
C	=	Runoff Coefficient (increase by 25% for 100-year)
I	=	Average Rainfall Intensity for return period (mm/hr)
	=	$732.951 / (T_c + 6.199)^{0.810}$ (2-year)
	=	$998.071 / (T_c + 6.053)^{0.814}$ (5-year)
	=	$1735.688 / (T_c + 6.014)^{0.820}$ (100-year)
T_c	=	Time of concentration (mins)
A	=	Drainage Area (hectares)

Table E2 summarizes the pre-development peak flows based on a calculated time of concentration, determined using either the Airport Formula or the Bransby Williams formula. Table 6-2 below summarizes these pre-development peak flows tributary to the storm sewers on Hazeldean Road and Victor Street.

Table 6-2: Summary of Pre-Development Peak Flows

Return Period Storm	Peak Flow to Victor Street Storm Sewers (L/sec)	Peak Flow to Hazeldean Road Storm Sewers (L/sec)	Total Peak Flows (L/sec)
2-year	76.6	46.1	122.7
5-year	104.9	63.1	168.0
100-year	226.1	135.8	361.9

6.2 Calculation of Allowable Release Rate

As previously mentioned, the allowable discharge release rates from the site were established using the peak flows derived with a standard time of concentration of 10 minutes as per City Guidelines. The allowable release rates from the proposed site were estimated using the Rational Formula are follows:

$$Q_{ALL} = 2.78 C_{AVG} I_T A$$

where:

- Q_{ALL} = Peak Allowable Discharge (L/sec)
- C_{AVG} = Average Runoff Coefficient (25% increase for 100-yr storm)
- I_T = Average Rainfall Intensity (mm/h) for Return Period
- A = Drainage Area (hectares)

Based on the consultation with the City of Ottawa, the post-development flows are to be controlled to the 5-year pre-development rate for all storms up to the 100-year event. Using a time of concentration (T_c) of 10 minutes and a maximum runoff coefficient of 0.50 or the pre-development value. The allowable release rates from the site were determined for the 2-year, and 5-year storms as follows:

To Victor Street

$$\begin{aligned} Q_{2ALL} &= 2.78 (0.28) (I_{2-year}) (0.7828 \text{ ha}) \\ &= 2.78 (0.28) (732.951/(10+6.199)^{0.810}) (0.7828 \text{ ha}) &= 46.7 \text{ L/sec} \\ Q_{5ALL} &= 2.78 (0.28) (I_{5-year}) (0.7828 \text{ ha}) \\ &= 2.78 (0.28) (998.071/(10+6.035)^{0.814}) (0.7828 \text{ ha}) &= 63.5 \text{ L/sec} \\ &\text{*Further reduced based on modelling of downstream storm} &= \textcolor{red}{50.0 \text{ L/sec}} \end{aligned}$$

To Hazeldean Road

$$\begin{aligned} Q_{2ALL} &= 2.78 (0.50) (I_{2-year}) (0.1814 \text{ ha}) \\ &= 2.78 (0.50) (732.951/(10+6.199)^{0.810}) (0.1814 \text{ ha}) &= 19.4 \text{ L/sec} \\ Q_{5ALL} &= 2.78 (0.50) (I_{5-year}) (0.1814 \text{ ha}) \\ &= 2.78 (0.50) (998.071/(10+6.035)^{0.814}) (0.1814 \text{ ha}) &= 26.3 \text{ L/sec} \end{aligned}$$

Therefore, the allowable release rate from the proposed site is will be 50 L/sec. This 50 L/sec represents the minor system (or piped) flow to the storm sewer on Victor Street. In addition, the allowable discharge rate to the storm sewers on Hazeldean Road is 26.3 L/sec, however this will only include overland flows that discharge northerly on the roadway.

6.3 Post-Development Conditions

6.4 Design Criteria

We designed the stormwater system in conformance with the latest version of the City of Ottawa Design Guidelines (October 2012). Section 5 "Storm and Combined Sewer Design" and Section 8 "Stormwater Management". A summary of the design criteria that relates to this design report is listed below.

6.4.1 Minor System Design Criteria

- The storm sewer was sized based on the Rational Method and Manning's Equation under free flow conditions for the 2-year storm using a 10-minute inlet time.
- Since a detailed site plan was available for the site, including building footprints, calculations of the average runoff coefficients for each drainage area was completed. Average runoff coefficients were calculated for each inlet drainage area.
- Minimum sewer slopes to be based on minimum velocities for storm sewers of 0.80 m/sec.

6.4.2 Major System Design Criteria

- The major system has been designed to accommodate on-site detention with sufficient capacity to attenuate the 100-year design storm. On-site storage is calculated based on the 100-year design storm with on-site detention storage provided in underground storage chambers.
- On site storage is provided and calculated for up to the 100-year design storm. There is no surface ponding proposed on the ground surface for up to the 100-year event.
- Calculation of the 100-year storage requirements was completed based on a dynamic stormwater model completed with PCSWMM.
- Overland flow routes are provided.
- The vertical distance from the spill elevation on the street and the ground elevation at the buildings is at least 150mm.
- The emergency overflow spill elevation is at least 30 cm below the lowest building opening.

6.5 Runoff Coefficients

Runoff coefficients were derived the same way under post development conditions. Average runoff coefficients for all catchments were calculated using PCSWMM's area weighting routine. The runoff coefficients for all catchments were area weighted to derive at average runoff coefficients based on hard surfaces (concrete or asphalt) having an imperviousness of 100%, soft surfaces (landscaping surfaces) having a zero percent imperviousness. Again, the conversion from an imperviousness percent to a runoff coefficient was taken as $C = (\text{IMP} * 0.70) / 100 + 0.20$, with the imperviousness (IMP) as a percentage.

The average runoff coefficients for both pre-development and post-development conditions were calculated. Under both conditions, the runoff coefficients for each subcatchment and site boundaries were determined. The runoff coefficients for pre-development and post-development catchments are provided in Appendix E.

The post-development average runoff coefficients for each site property is summarized in the following table.

Table 6-3: Summary of Average Runoff Coefficients – Post-Development

Location	Area (hectares)	Imperviousness (%)	Avg Runoff Coefficient (C_{AVG})
Site 1 (east)	0.4995	76.2	0.70
Site 2 (west)	0.4645	66.1	0.67
Totals	0.9640	71.4	0.70

6.6 Minor System (Storm Sewer) Design

A storm drainage plan is illustrated on drawing C400 located in Appendix A. A total ten (10) subcatchments (or drainage areas) within the development site are shown on this drawing with average runoff coefficients calculated for each drainage area.

Average runoff coefficients were calculated for all drainage areas for sizing of the storm sewers. A starting inlet times of 10 minutes were used for uppermost storm sewers. Design sheets for the 2-year sizing of the storm sewer system is included for reference in Appendix E.

Under the 2-year storm event adequate capacity is provided within the storm sewer system.

6.6.1 Allowance for Foundation Drainage

Foundation drainage was also considered based on City of Ottawa guidelines, that each foundation is assumed to drain at 0.45 L/sec. Therefore, the assumed foundation drainage was calculated as shown below and incorporated in the PCSWMM modeling as a constant inflow in addition to the flow resulting from rainfall events.

Number of foundations	= 12
Constant flow per foundation	= 0.45 L/sec
Assumed Foundation Flow	= $12 \times 0.45\text{L/sec}$
	= 5.4 L/sec

Therefore, a constant 5.4 L/sec will be taken into consideration for designing the storm sewer.

6.7 Stormwater Management Modelling

As a result of the City of Ottawa's previous submission review it was necessary to complete a full dual drainage stormwater model which would include the downstream storm sewer system. The previous design submission only accounted for the onsite storm sewer system within the subject property, however after discussions with the City of Ottawa staff, it was necessary to expand the stormwater (SWM) model all the way to Poole Creek, which is approx. 650m downstream of the site.

A dynamic stormwater model was used for this analysis, with all minor and major system components being included in the PCSWMM model, including inlet control devices (ICDs) in catchbasins and storage for underground chambers. Rating curves were developed for ICD's based on manufacturers specifications.

6.7.1 Hydrologic/Hydraulic Analysis

PCSWMM was used to create a dual drainage hydrologic/hydraulic model of the storm sewer system. The model accounts for both the minor system (storm sewer) and the major system (roads). Catchbasins were modelled in either a flow-by condition or in a ponding condition. For catchbasins in flow-by conditions inlet capture curves were developed based on the type of curbs used (mountable curb in this case), and the inlet type (surface inlet catchbasins in this case). Ponding areas were modelled as storage nodes with surface ponding represented by area-depth curves above the inlet control devices (ICDs) located at the outlet pipe invert. Calculations of runoff was completed based on the PCSWMM's EPA SWM 5 engine. Catchment parameters were taken from City of Ottawa's SDG002 Design parameters. The following design parameters and assumptions are noted as follows:

- Infiltration losses based on Horton Equation as per City of Ottawa SDG002.
- Impervious and pervious depression storage as per City of Ottawa SDG002.
- 5-year, 3-hour Chicago storm used to review minor system design based on Rational Method.
- 100-year, 3-hour Chicago storm used assess impact of major event and determine peak flows and depth of runoff.
- Runoff coefficient for all subcatchments were determined using area weighting routine and based on actual hard and soft surface areas. Runoff coefficients were calculated from the impervious levels using the relationship $C = (\text{IMP} \times 0.7) + 0.20$.
- Subcatchment areas were derived tributary to each surface inlet (catchbasin).
- Subcatchment widths are equal to the subcatchment area divided by the overland flow path length. As per City Guidelines, the subcatchment width is equal to $2 \times$ length for two-sided catchments.
- The volume of surface ponding at low-points were calculated using the prism-formula ($V=1/3*A*H$).

6.7.2 Subcatchment Parameters

Drawing C400 illustrate the post-development storm drainage system. Flow path lengths for each subcatchment was determined based on the average overland flow path length, with the catchment width being the area/length. Subcatchment slopes were set at 1%. The following table below summarizes the general subcatchment parameters used:

Table 6-4: General Subcatchment Parameters

Parameter	PCSWMM Parameter	Value
Infiltration Loss Method		Horton
Maximum Infiltration Rate	Max. Infil. Rate	76 mm/hr
Minimum Infiltration Rate	Min. Infil. Rate	13.2 mm/hr
Decay Constant (1/hr)	Decay Constant	4.14
Manning N (Impervious)	N Impev	0.013
Manning N (Pervious)	N Perv	0.40
Depression Storage – Pervious Surfaces	Dstore Imperv	1.57 mm
Depression Storage – Impervious Surfaces	Dstore Perv	4.67 mm
Zero Percent Impervious	Zero Imper	10% & 20%
Subcatchment Slopes	Slope	0.5% - 2%

The table below presents the individual onsite subcatchment parameters that were developed and used in the PCSWMM model. A complete list of subcatchments, including offsite subcatchments is included in Appendix G.

Table 6-5: Post-Development Subcatchment Parameters

Name	Outlet	Area (ha)	Width (m)	Flow Path Length (m)	Slope (%)	IMP (%)	Cavg
S01	CB06	0.1752	58	30.2	1	80.668	0.76
S02	CB01	0.1483	51.7	28.7	1	88.226	0.82
S03	CB01	0.0178	80.9	2.2	1	14.522	0.3
S04	CB03	0.2001	70.2	28.5	1	79.11	0.75
S05	218	0.1264	53.1	23.8	1	73.958	0.72
S06	CBT03	0.0617	52.3	11.8	1	35.843	0.45
S07	CBE01	0.0415	54.6	7.6	1	37.942	0.47
S08_1	CBT14	0.0405	57.8	7	1	59.421	0.62
S08_2	CBE04	0.0548	78.2	7	1	54.842	0.58
S09	IN103407	0.0806	94.8	8.5	1	71.197	0.7

6.7.3 Storage Node Parameters for Underground Chambers

The modelling of underground storage components in the PCSWMM was achieved using area-depth curves. Since PCSWMM uses an area-depth functional curve for determining storage, an equivalent area based on the number of chambers and endcaps was derived to obtain the total volume at the various storage depths. The following table summarizes the number of chambers and endcaps used at each location. The volumes within each underground chamber locations were based on storage-depth data provided by the Manufacturer. Additional information on the number of chambers is provided in Appendix E.

Table 6-6: Volumes of Underground Chambers

Name	Number of Chambers	Number of Endcaps	Total Volume (m ³)
CHAMBERS-1 (east)	28	8	152.5
CHAMBERS-2 (west)	28	10	155.2

Table 6-6 below summarizes the storage nodes used in the PCSWMM model, the associated invert and rim elevations, the curves type and name, the type of storage and the number of inlets.

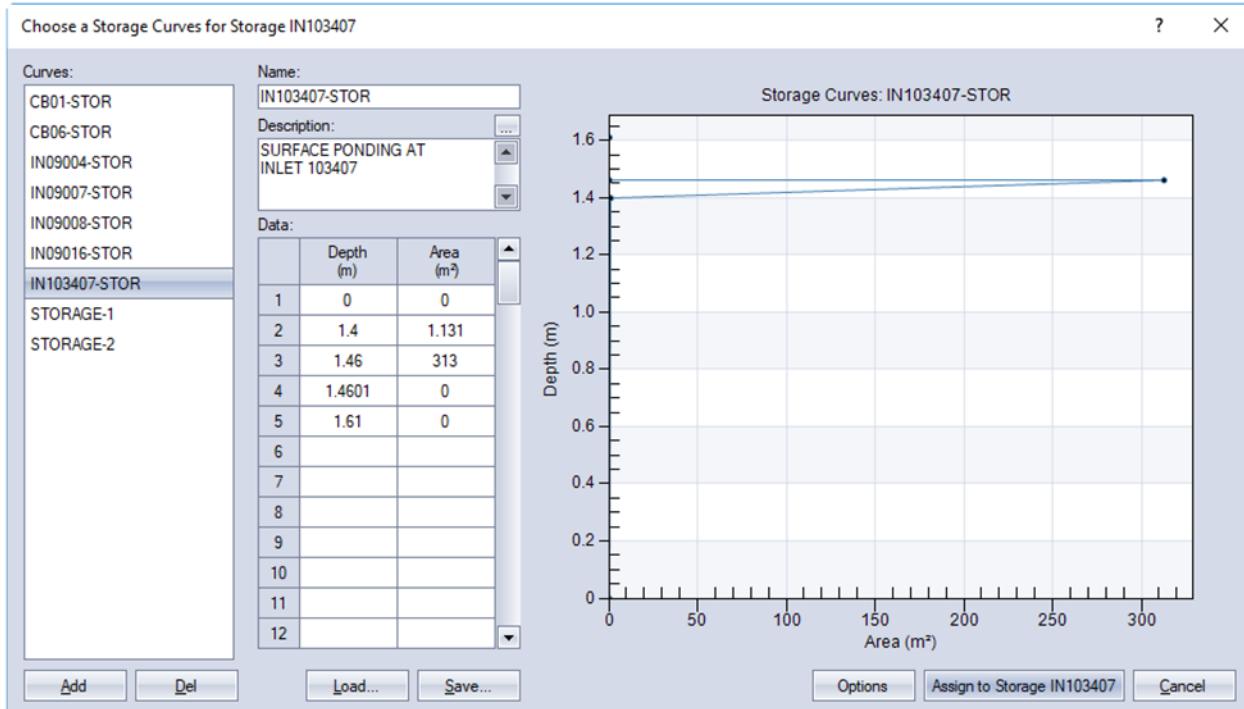
Table 6-7: Storage Node Parameters for Underground Chambers

Name	Invert Elev. (m)	Rim Elev. (m)	Depth (m)	Storage Curve	Curve Name	TYPE
CHAMBERS-1	111.516	114.1	2.58	TABULAR	STORAGE-1	STORAGE CHAMBERS
CHAMBERS-2	112.296	114.5	2.20	TABULAR	STORAGE-2	STORAGE CHAMBERS

6.7.4 Storage Node Parameters for Surface Ponding Areas (Offsite)

At ponding locations, the storage nodes were defined based on the depth to the ICD. At all locations the depth from the top of grate to the outlet pipe is 1.4m, therefore the storage of stormwater will only occur starting at a 1.4m depth. The storage rating curves at each catchbasin was modeled like the illustration in the figure below. There are a total of ten (10) ponding areas, four onsite and six (6) offsite.

Figure 1 – Representation of Rating Curves for Modelling of Storage at Ponding Locations



6.7.5 Outlet Node Parameters

In PCSWMM, OUTLETS are flow control devices used to control the outflow from storage units. OUTLETS are defined using rating curves, that relate head versus discharge. OUTLETS are represented by a link connecting two nodes. In this analysis OUTLETS were used to model ICDs located downstream of the underground chambers. Rating curves for IPEX Tempest inlet control devices is provided for reference in Appendix H. The proceeding table below summarizes the inlet control devices used in the catchbasin or manholes.

Table 6-8: Outlet (ICD) Node Parameters for Chambers

Name	Outlet Node	Type	Inlet Elev. (m)	Rating Curve	Curve Name	100-yr Flow (L/s)
212-ICD	216	ICD	111.42	TABULAR/DEPTH	IPEX-MHF-TYPEA	21.32
215-ICD	205	ICD	112.24	TABULAR/DEPTH	IPEX-MHF-TYPEA	24.49

6.7.6 Inlet Control at Flow-By Conditions

The flow-by capture curves are used when an inlet is not located in a ponding area. In this case only a portion of the overland flow is captured, while the remaining flow continues downstream (bypassed). Although the City of Ottawa does not specifically provide rating curves for catchbasins under flow-by conditions, they do provide gutter flow rate curves for either barrier curbs (SC1.1 or OPSD600.110) or mountable curb and gutter (SC1.3 or OPSD 600.020).

The gutter flow rates are provided at longitudinal road slopes of 2%, 4%, 6%, and 8% for flow spreads ranging between 0m to 3m. Along with the gutter flow rates, the inlet capacities of the surface inlets are provided at various spreads.

The inlet capacities of the curb inlet catchbasins were derived from Appendix 7-A.14 through 7-A.17. These pages provide the capture rates (Q_c) of the inlets at various approach flows (Q_t). Both rating curves for surface type inlets and curb-inlet type catchbasins were based on a roadway with a 3.0% cross fall and longitudinal slopes of 2%. The following Table 6-6 below summarizes the rating curves used for the curb inlet catchbasins in a flow-by condition.

The following Table 6-9 below summarizes the rating curves used for the surface catchbasins with a curb & gutter type curb in a flow-by condition.

Table 6-9: Rating Curves for Surface Catchbasin with Mountable Curb & Gutter in Flow-By Condition (3% cross fall, 2% slope)

Approach Flow (L/sec)	Total Spread, T (m)	Depth of Flow at Gutter (m)	Inlet Capture Rate (L/sec)
0	0.000	0.006	0
5	0.818	0.026	7
10	1.064	0.033	12
50	1.954	0.060	15
100	2.535	0.078	34
125	2.757	0.084	47
150	2.952	0.090	51
200	3.128	0.095	54
250	3.289	0.100	55

Tables E14 in Appendix E provides additional information on the development of the rating curves for the catchbasin in flow-by conditions. This exercise was completed since PCSWMM does not have the ability to provide Approach Flow versus Capture Flow at flow-by conditions. PCSWMM requires a depth versus captured flow rate instead.

6.8 Dual Drainage Modelling

The Figure below, captured from the PCSWMM model demonstrates the object connectivity. The subcatchment are illustrated as white polygons, with their area number, area in hectares and percent imperviousness labelled. The yellow lines and yellow circles represent the storm sewer system and manholes, with purple lines representing the OUTLET links (or ICDs). Catch basins storage nodes are shown as green squares.



Figure 2 - Model Schematic Illustrating Subcatchments, Links, Nodes, Outlets (ICDs)

6.9 Storm Events Modelled

Seven (7) storm events were modelled as follows: 3-hour 2-year Chicago storm (timestep 10 mins)

- 3-hour 2-year Chicago storm (timestep 10 mins)
- 3-hour 5-year Chicago storm (timestep 10 mins)
- 3-hour 100-year Chicago storm (timestep 10 mins)
- 3-hour 100-year + 20% Chicago storm (timestep 10 mins)
- Historical storms occurring July 1, 1979, Aug 4, 1988, August 08, 1996

6.9.1 Modelling Results

The following summarizes the results of various storm events to ensure the design criteria is met. This includes the following:

- Peak flows for all storms up to the 100-year event shall meet the allowable rate of 50 L/sec to the storm sewer on Victor Street based on City of Ottawa requirements
- Hydraulic grade line in all storm sewers to be 300mm below the USF elevation of adjacent residential units.

The following table summarizes the modelling results for all storm events.

Table 6-10: Peak Flows at Outfalls

Storm Event	Max. Flow (L/sec) to Victor Street		
	Uncontrolled Overland Flow (see note 1)	Minor System Controlled Flows (see note 2)	Total
Chicago_3h_2yr	12.7	32.8	45.4
Chicago_3h_5yr	20.3	38.1	58.4
Chicago_3h_100yr	38.2	50.5	88.7
Historic_Jul1-79	46.4	52.8	99.2
Chicago_3h_100yr + 20%	22.9	52.5	75.5
Historic_Aug4-88	33.7	51.3	85.0
Historic_Aug8-96	24.6	42.6	67.1

Notes
 1-Overland Flows from subcatchment S09. Discharges to ROW and captured by twin DCBs in ponding condition
 2-Minor System Capture Rate to not exceed 50 L/sec in 100-yr event. Conduit C10. Includes 5.4 L/sec of constant inflow from foundations

Table 6-11: Comparison of Pre-Development and Post-Development Peak Flows

Return Period Storm	Total Peak Flow (L/sec)	
	Pre-Dev	Post-Dev
2-year	122.7	45.4
5-year	168.0	58.4
100-year	361.9	88.7

6.9.2 Underground Storage

The total storage occurring during all storm events is presented in the table below. These results are based on the maximum volumes occurring in each PCSWMM STORAGE node.

Table 6-12: Summary of Storage Based on Modelling Results

Storm Event	Storage Location				Total Storage (m3)	
	Chambers - 1		Chambers - 2			
	Volume (m ³)	Depth (m)	Volume (m ³)	Depth (m)		
Chicago_3h_2yr	41	111.96	54	112.88	95	
Chicago_3h_5yr	60	112.18	80	113.16	140	
Chicago_3h_100yr	118	112.81	155	114.08	273	
Chicago_3h_100yr + 20%	148	113.14	155	114.36	303	
Historic_Jul1-79	142	113.08	155	114.17	297	
Historic_Aug4-88	125	112.89	155	114.28	280	
Historic_Aug8-96	76	112.35	114	113.52	190	

6.10 Hydraulics

6.10.1 Hydraulic Grade Line Analysis

The HGL was plotted from PCSWMM for the 2-year, 5-year, 100-year, 100-year + 20% and the three Historical Storm events. A profile through the complete storm sewer systems is shown below in Figure 3 below. It is shown that during the 100-yr event the maximum water surface elevations remain within the storm sewer system and does not surcharge.

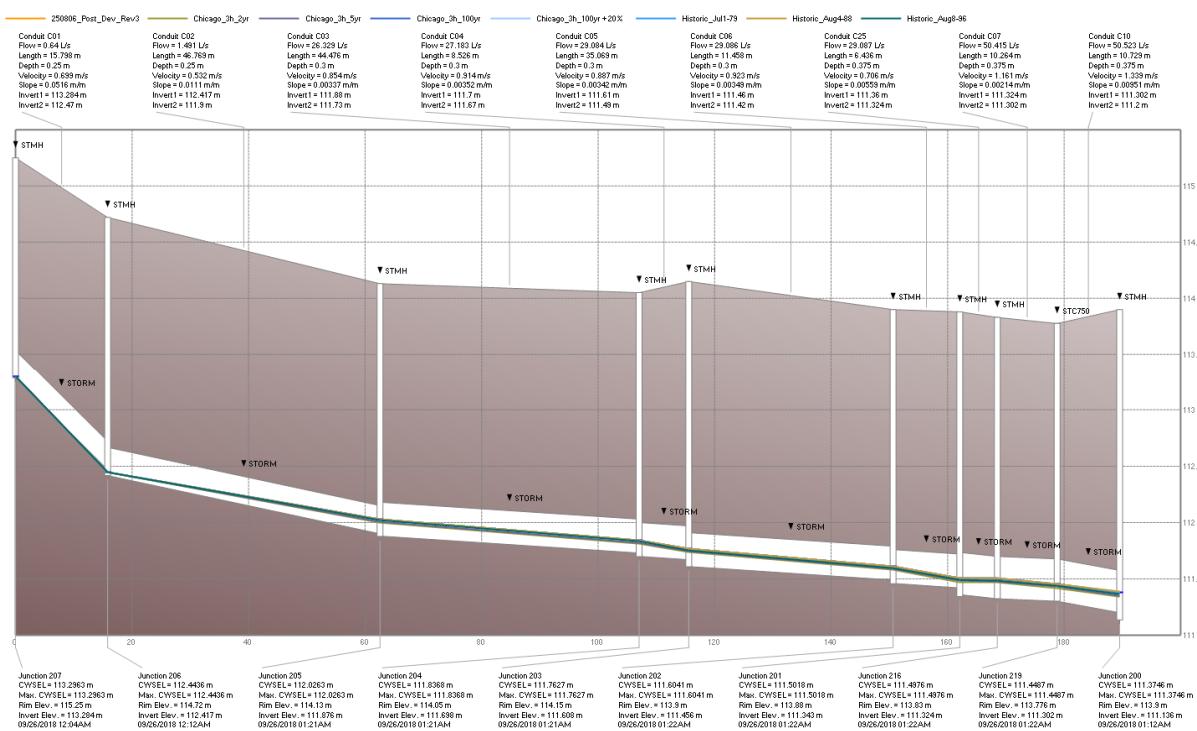


Figure 3 – 100-year HGL (Main Storm Sewer)

The 100-year HGL within both the onsite storm sewers and the offsite storm sewers are shown in the PCSWMM report provided in Appendix G.

From the 100-yr profiles it appears that minor surcharging in the 100-year event will occur in on Victor Street and Savage Drive, with slightly higher surcharging on Denham Way. This can be attributed to the larger rear yard areas contributing runoff to the storm sewer on Denham in relation to Victor St.

6.10.2 Offsite Inlet Control Devices

For modelling the offsite storm system, inlet control devices (ICDs) were used in all roadway CBs. For the rear yards catchbasins 200mm diameter leads at 1% were used. All ICDs were modeled as IPLEX Type A for 20 L/sec at 1.2m head. A complete list of OUTLETS used in the model please refer to the PCSWMM

report in Appendix G. Please refer to Figure A9 in Appendix A which identifies the ICD types modelled in the downstream storm system.

6.11 Quality Control Measures

It was established at the pre-consultation meeting with the City of Ottawa that the Water Quality (WQ) objective for the site is 80% TSS removal.

As a total suspended solids (TSS) removal efficiency of 80% is required, it is proposed to provide an oil grit separator for quality control. The following summarizes the design parameters used in the sizing of the Stormceptor manhole:

Table 6-13: Design Parameters Used for Oil Grit Separator Sizing

Parameter	Value Used	
Drainage Area	0.866 hectares	
Imperviousness	71.3 %	
TSS Removal Requirements	80 %	
Runoff Volume Capture	85%	
Particle distribution	fine	
	Flow (m ³ /s)	Storage (ha.m)
Flow attenuation upstream of OG separator	0.00000	0.00000
	0.02760	0.00945
	0.03290	0.01400
	0.04520	0.02734

Output from the PCSWMM for Stormceptor program is provided in Appendix F for reference. A Stormceptor model EF6 is necessary to meet the required TSS removal of 80%. The EF6 will provide an approximate TSS removal of 82%.

The Stormceptor Manhole is located within the subject property. It is identified as OGS on the drawings and manhole 219 in the PCSWMM model.

6.12 Water Balance

A review of the water balance method, as noted in section 3.2.3 of the MECP's SMPDM was completed to estimate the anticipated change in infiltration that will occur as a result of development of the subject property.

From Table 3.1 of the Ministry's SMPDM the total yearly pre-development and post-development infiltration amounts were estimated based on the site area and corresponding percent pervious. Using an infiltration allowance of 276 mm for fine sand within urban lawns (Table 3.1), the following infiltration amounts were estimated as follows:

- total yearly infiltration (pre-development) = 276 mm x 0.9641 ha x 77.2% = 2,054 m³
- total yearly infiltration (post-development) = 276 mm x 0.9641 ha x 28.6% = 761 m³

Discussion with the MVCA has indicated that an infiltration target of 104 mm/year is desired for the site. Based on the area of the site and a yearly infiltration target of 104 mm/year, the infiltration requirement would be: $104 \text{ mm/year} \times 0.9641 = 1,002.7 \text{ m}^3$.

From above the total yearly infiltration under post-development conditions is estimated at 761 m^3 , therefore additional infiltration practises of 241.7 m^3 is proposed to provide the additional volume storage.

In order to assist with infiltration, additional onsite servicing methods such as dry swales c/w perforated pipes and perforated underground chambers are proposed. The following briefly summarizes the infiltration practises proposed:

- $(195.4 + 201.3) = 396.7 \text{ m}^2$ footprint area of the StormTech Chambers. These chambers are 1.14m in high arch pipes having open bottoms to promote infiltration.
- 210m of 250mm perforates pipes and swales in rear-yard swales. (1.2m wide, 0.15m Gran A)

The subject site contains shallow bedrock depths which is not favourable for infiltration practises. As a result of the need for rock blasting of services, it is proposed (and necessary) to over-blast below the bottom of the infiltration trenches. Therefore, an additional 0.6m of over-blasting depth is proposed. The following summarizes the total estimated volumes that will be available based on a minimum void ratio of 0.40.

- Infiltration volume below chambers = $396.7 \text{ m}^2 \times (0.23\text{m} + 0.6\text{m}) \times 0.40 = 131.7 \text{ m}^3$
- Infiltration volume below swales = $210\text{m} \times 1.2\text{m} \times (0.15\text{m} + 0.6\text{m}) \times 0.40 = 75.6 \text{ m}^3$
 $= 207.3 \text{ m}^3$

Using these additional features, the revised infiltration rate would be $761 \text{ m}^3 + 207.3 \text{ m}^3$ or 968.3 m^3 . This is the yearly infiltration rate that is expected. Based on the site area this would result in a unit rate of 100.4 mm/hectare per year. This rate would be just 3.6 mm/year short of the target.

Additionally, a review of other areas in the City of Ottawa where runoff volume reduction is necessary was undertaken to determine if the onsite infiltration could meet other similar standards. For areas within the Pinecrest Creek watershed a volume reduction of the 10mm storm is required for erosion control. Under post-development conditions with an area of 0.9641 ha, 71.4% level of imperviousness (28.6% pervious), the estimated volume required for volume control (or infiltration of 10mm storm) is:

- Impervious Area x (10mm – IAimperv) + Pervious Area x (10mm - IAperv)
- $0.9641 \text{ ha} \times 71.4\% \times (10\text{mm} - 1.57\text{mm}) + 0.9641 \times 28.6\% \times (10\text{mm} - 4.67\text{mm})$
- $5.80 \text{ ha.mm} + 1.47 \text{ ha.mm} = 72.7 \text{ m}^3$

Based on Pinecrest Creek watershed criteria of 10mm retention for infiltration, the proposed site servicing would provide approximately 142.2 m^3 , which would exceed the infiltration volume requirement of 72.7 m^3 .

7 Erosion and Sediment Control

During all construction activities, erosion and sedimentation shall be controlled by the following techniques:

- Filter cloth shall be installed between the frame and cover of all adjacent catch basins and catch basin manhole structures. The filter cloth shall consist of a filter bag that is placed within the catchbasin, just beneath the lid. These Siltsacks shall be Geo-Synthetics or equivalent. Installation details are provided on the Erosion and Sediment Control Plan.
- Light duty silt fencing will be used to control runoff around the construction area. Silt fencing locations are identified on the site grading and erosion control plan.
- Visual inspection shall be completed daily on sediment control barriers and any damage repaired immediately. Care will be taken to prevent damage during construction operations.
- In some cases barriers may be removed temporarily to accommodate the construction operations. The affected barriers will be reinstated at night when construction is completed.
- Sediment control devices will be cleaned of accumulated silt as required. The deposits will be disposed of as per the requirements of the contract.
- During the course of construction, if the engineer believes that additional prevention methods are required to control erosion and sedimentation, the contractor will install additional silt fences or other methods as required to the satisfaction of the engineer.
- Construction and maintenance requirements for erosion and sediment controls are to comply with Ontario Provincial Standard Specification (OPSS) OPSS 805 and City specifications.

8 Conclusions

This report addresses site servicing and stormwater runoff from the proposed development located at the 5924 Hazeldean Road in the City of Ottawa. The proposed 0.964-hectare development by Hazeldean Crossing Inc. consists of 12 residential blocks, which is comprised of 76 stacked town homes, and 10 traditional back to back town homes.

The following summarizes the servicing requirements for the site:

- For the water, the estimated peak hour pressures ranged from 58 psi to 62.6 psi. This meet the City of Ottawa's minimum pressure requirement of 40 psi. Therefore, the existing municipal watermains along Victor Street and Hazeldean Road have adequate capacity to service the proposed site for both domestic and fire protection.
- The estimated fire flow requirement of 250 L/sec was completed based on the FUS. A review of the total combined flow from hydrants within a 150m distance from the site was completed to confirm that adequate fire flows are available.
- The site will be serviced by a 200mm diameter PVC watermain. The watermain will be connected at two separate locations, one on Victor Street, and one on Hazeldean Road. The use of two connections is required as the water demand is greater than 50 m³/day as noted in Section 4.3.1 of the City's Water Distribution Guidelines.
- An estimated peak sewage flow of 2.3 L/sec for the site and 12.2 L/sec for the system, based on City Guidelines. An onsite 200mm sewer will be installed with a minimum slope of 0.35% having a full flow capacity of 19.7 L/sec.
- A review of the offsite sanitary system was completed to confirm that adequate capacity is available based on the proposed uses onsite. It was determined that adequate reserve capacity is available in the downstream sewer system to service the proposed development. A total peak sewage flow of 1.2 L/sec was estimated, with a maximum percent of capacity used of 36%.
- The allowable rate is based on the 5-yr predevelopment peak flow using the lower of C=0.50 or the pre-development rate. The allowable rate was estimated at 63.5 L/sec, however a lower rate of 50 L/sec was established by the City of Ottawa. The 50 L/sec represents the allowable minor system release rate (piped flow) from the subject property to the storm sewer on Victor Street.
- To meet the stormwater requirements, underground chambers will be used which will have a single outlet manhole and flow control devices (ICDs). IPEX Type A ICDs will be used to control outflows from CHAMBERS-1 (within MH215) to 24.1 L/sec at 1.77m head, and to 21.2 L/sec at 1.39m head from CHAMBERS-2 (within MH212). The total 100-year storage volume for the site was estimated at 271.3 m³ using the Modified Rational Method. The actual combined volume occurring within the underground chambers during the 100-year event is 273.4 m³. Based on Manufacturers' specifications, and the number of chambers selected the total combined volume available in the chambers would be 307.7 m³.
- The total combined 2-year, 5-year and 100-year peak flows from the site (including uncontrolled overland flow) was estimated at 45.4 L/sec, 58.4 L/sec, and 88.7 L/sec respectively. The piped 100-year flow from the proposed property is ±50 L/sec.

Appendix A – Figures

Figure A1: Site Location Plan

Figure A2: Water Distribution Plan

Figure A3: Water Demand Allocation Plan

Figure A4: Fire Hydrant Location Plan

Figure A5: Exposure Distances (FUS)

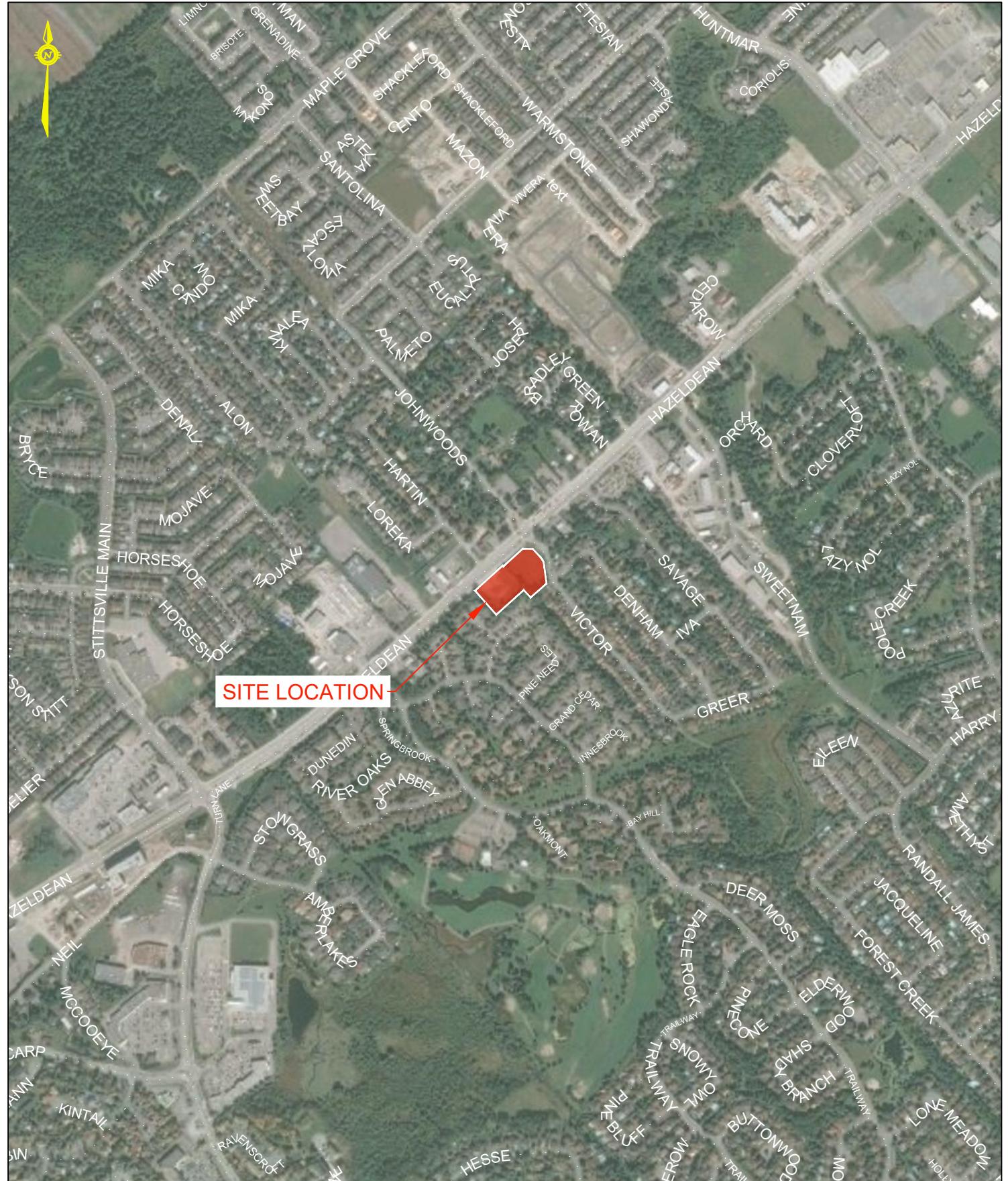
Figure A6: Sanitary Drainage Area Plan – Onsite Sewers

Figure A7: Sanitary Drainage Area Plan - Offsite Sewers

Figure A8: Pre-Development Drainage Area Plan

Figure A9: Inlet Control Devices (ICDs) in offsite Catch Basins

Drawing C400: Post Development Storm Drainage Plan



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100-2650 Queensview Drive
Ottawa, ON K2B 8H6

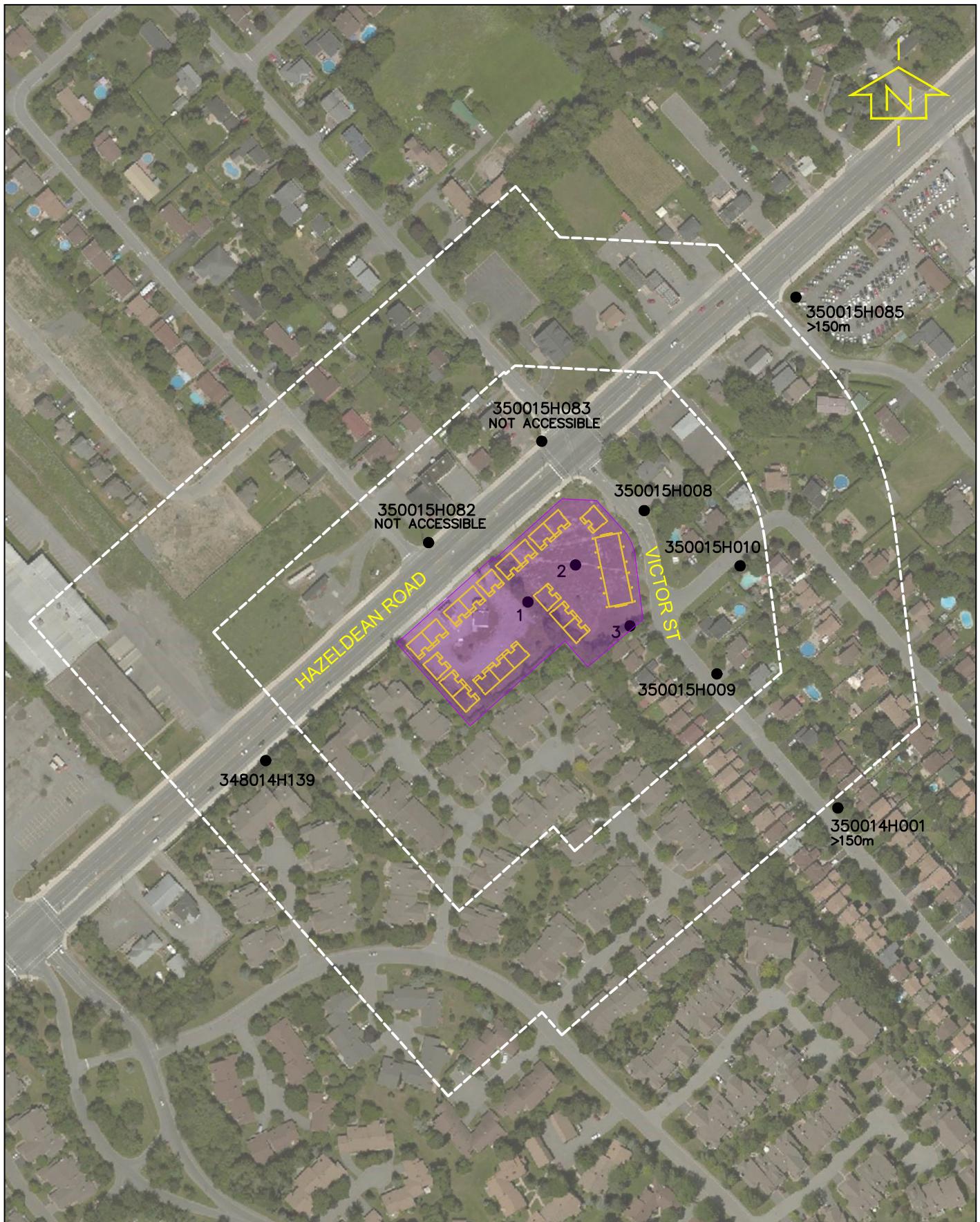
www.exp.com



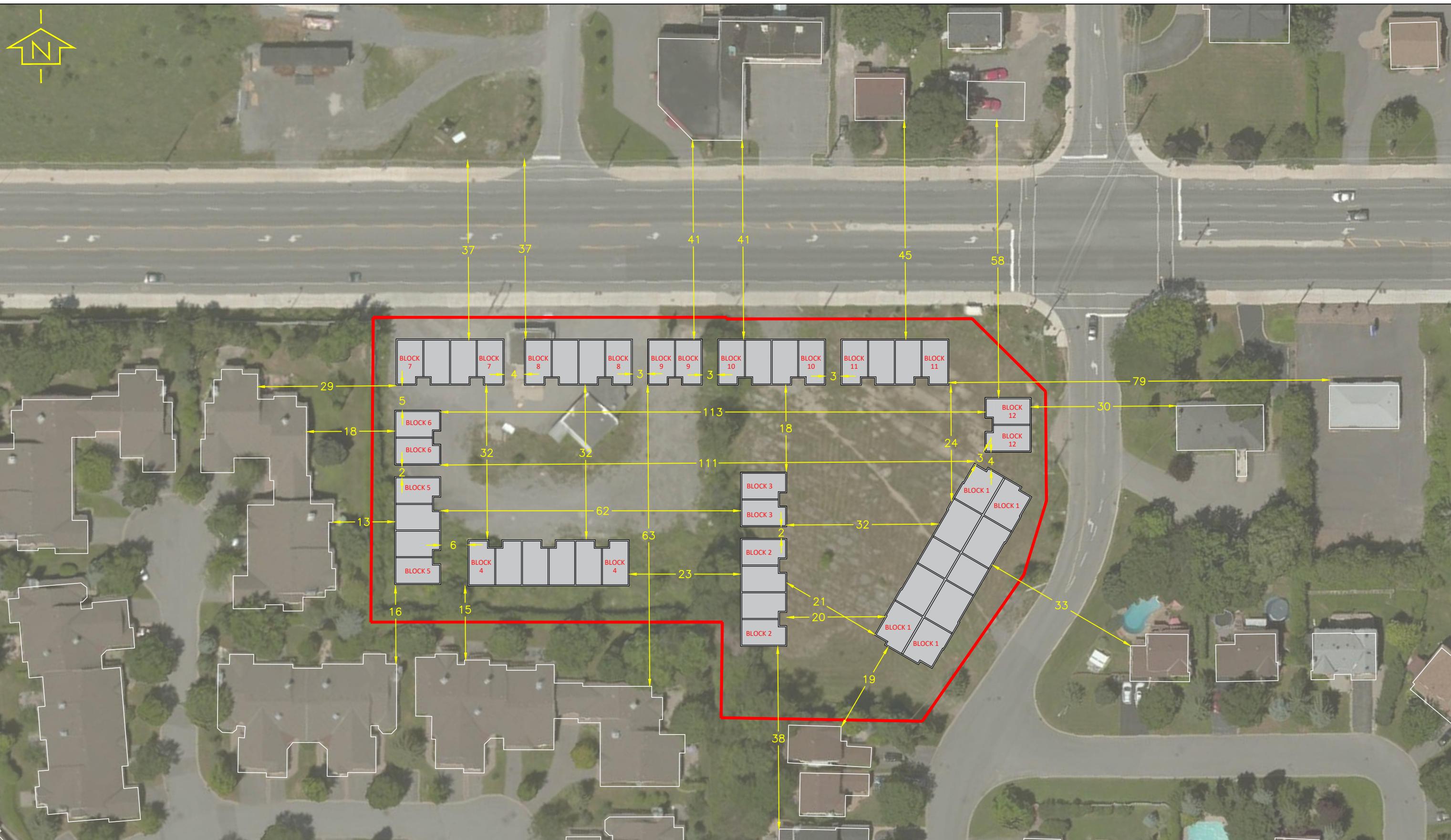
DESIGN	MZG	HAZELDEAN CROSSING 5924 HAZELDEAN ROAD	SCALE
DRAWN	MZG		1:10000
DATE	NOV 2019	SITE LOCATION	SKETCH NO
FILE NO	250806	PLAN	FIG A1

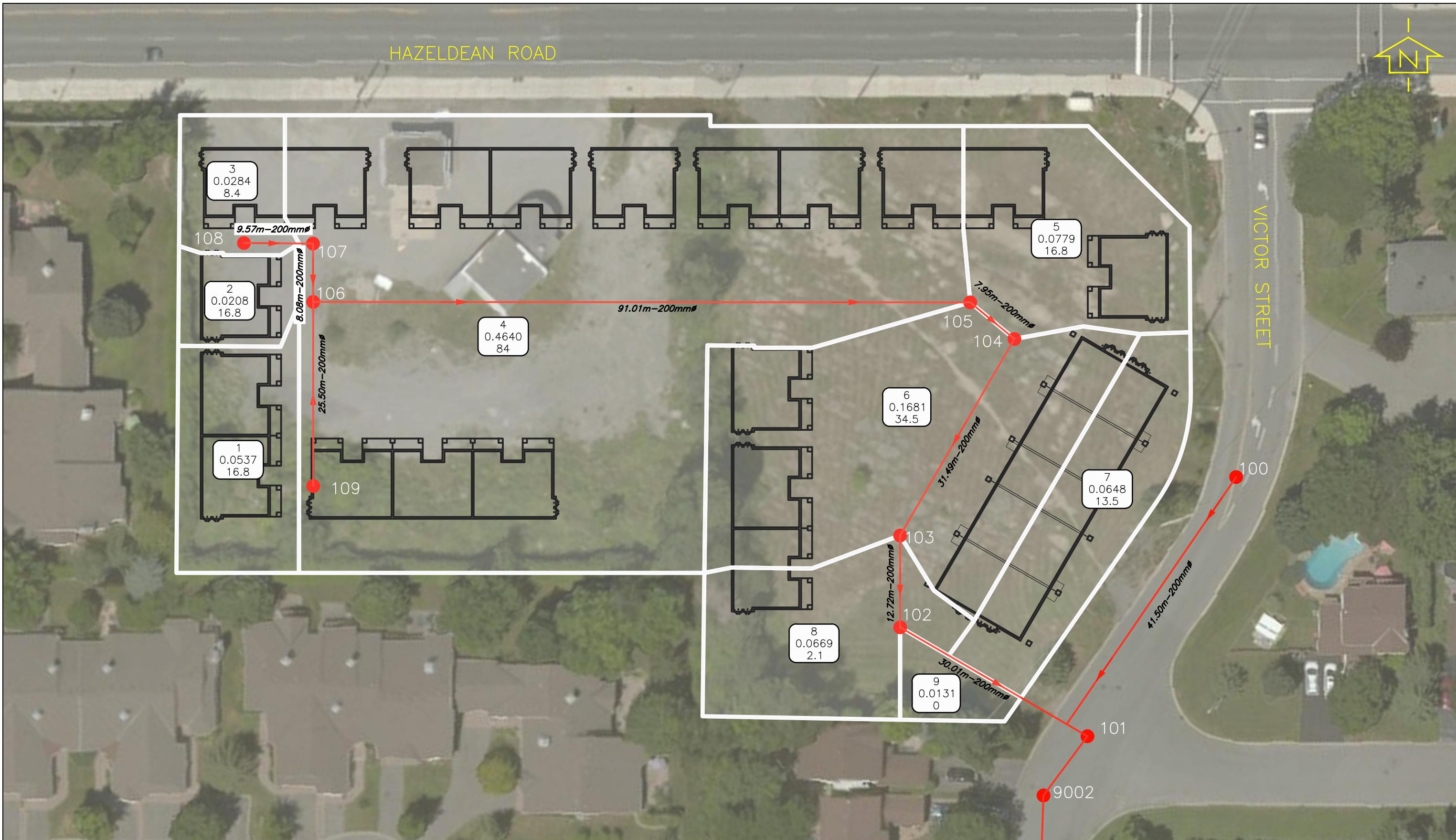


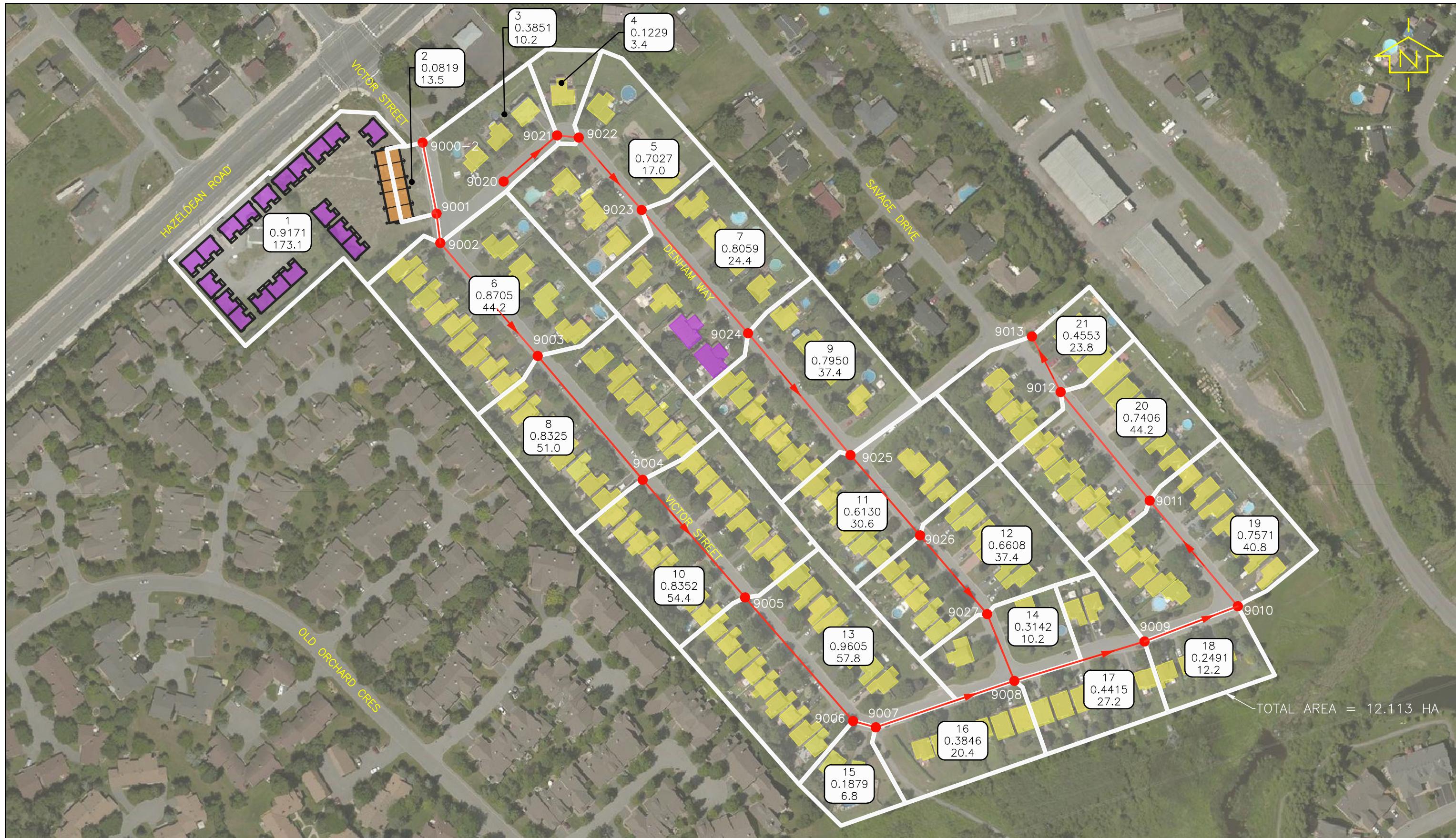


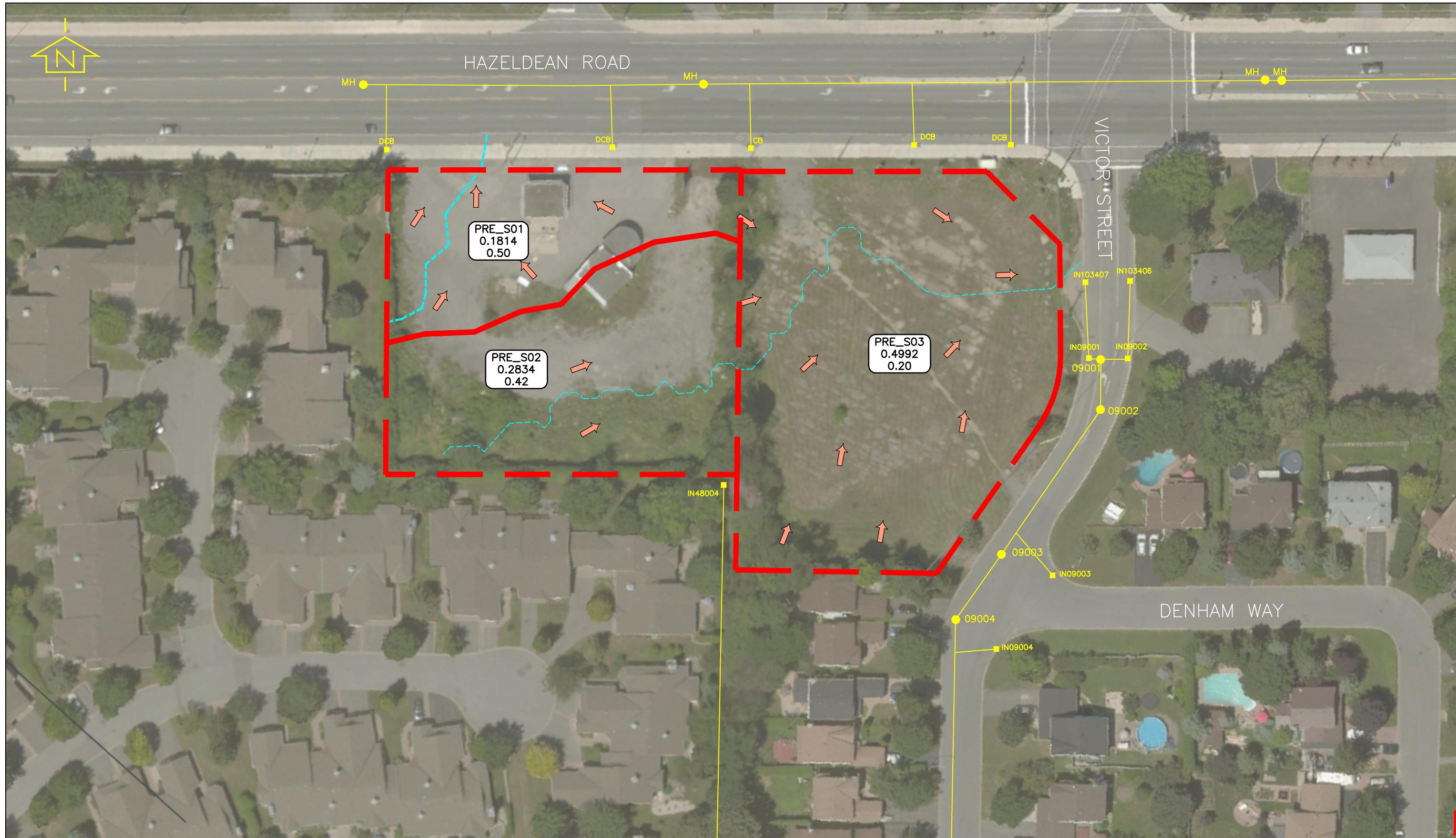


exp Services Inc. 100-2650 Queensview Drive Ottawa, ON K2B 8H6 www.exp.com		DESIGN JLF DRAWN SAB DATE NOV 2019 FILE NO 250806	HAZELDEAN CROSSING 5924 HAZELDEAN ROAD HYDRANT LOCATION PLAN	SCALE 1: 3000 SKETCH NO FIG A4
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 OVERLAND FLOW DIRECTION
----- OVERLAND FLOW PATH

PRE_S01	AREA NUMBER
0.1814	AREA (HECTARES)
0.50	POPULATION

HAZELDEAN CROSSING
5924 HAZELDEAN ROAD

PRE-DEVELOPMENT CATCHMENTS

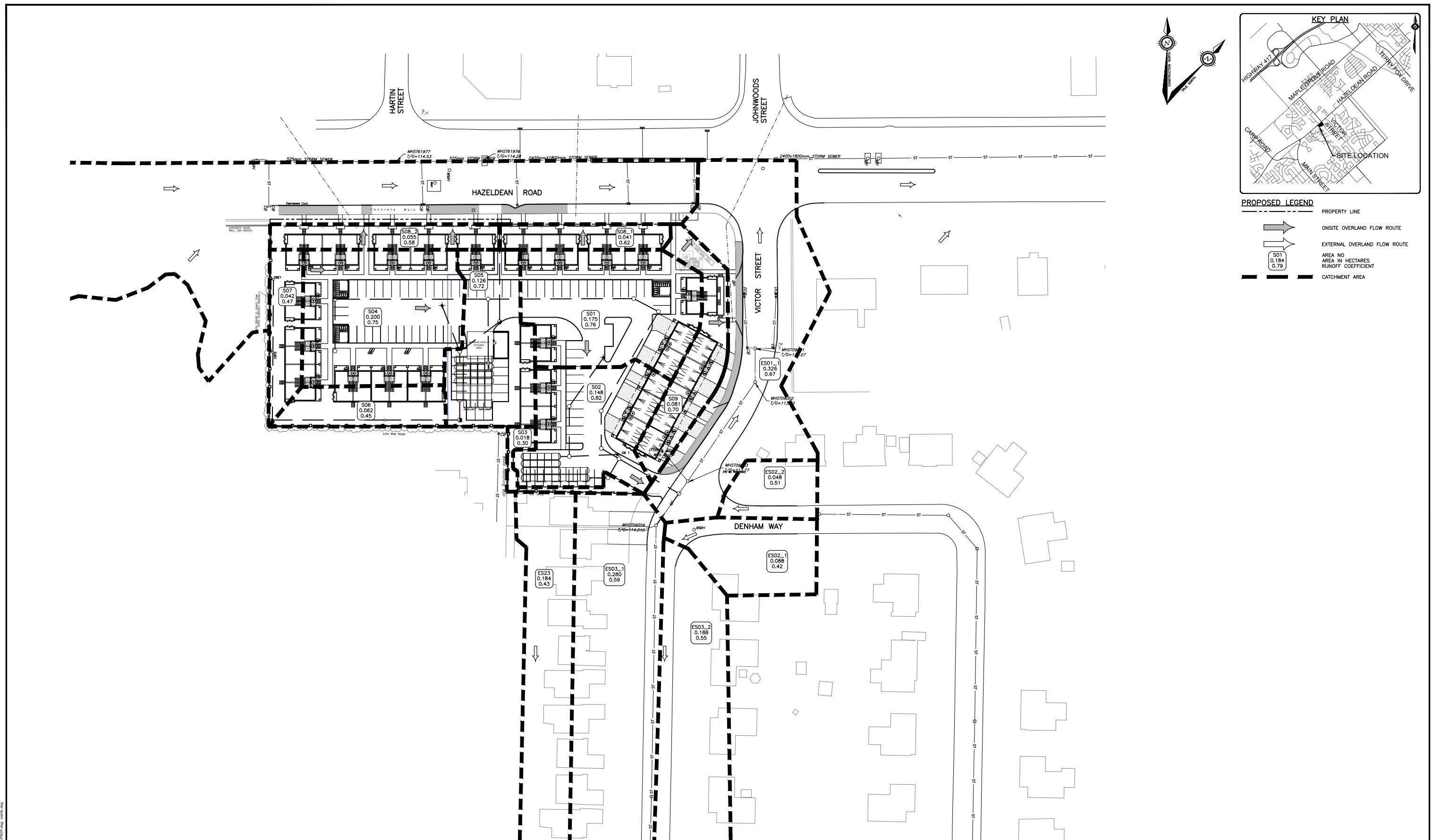
SCALE
1:750

FIGURE NO

FIG A8



FIGURE A9 - INLET CONTROL DEVICES (ICDs) IN OFFSITE CATCHBASINS



CAUTION
LOCATION OF ALL POLE LINES,
CONDUITS, WATERMAINS, SEWERS AND OTHER
UNDERGROUND AND OVERGROUND UTILITIES
AND STRUCTURES IS NOT NECESSARILY
SHOWN ON THE CONTRACT DRAWINGS, AND
WHERE SHOWN, THE ACCURACY OF THE
LOCATION OF SUCH UTILITIES AND
STRUCTURES IS NOT GUARANTEED. BEFORE
STARTING WORK, DETERMINE THE EXACT
LOCATION OF ALL SUCH UTILITIES AND
STRUCTURES AND ASSUME ALL LIABILITY FOR
DAMAGE TO THEM.

REV	REVISION DESCRIPTION	DATE	BY APPD	REV	REVISION DESCRIPTION	DATE	BY APPD
3	REVISED AS PER CITY COMMENTS	01/11/19	SAB BMT				
2	ISSUED FOR SITE PLAN APPROVAL	21/05/19	SAB BMT				
1	ISSUED FOR REVIEW	18/04/19	AO BMT				

SCALE
0 5m 10m 25m
HORIZONTAL 1:500

DESIGNED BY

REVIEWED BY

CLIENT

HAZELDEAN CROSSING INC.
5921 KILSPINDIE RIDGE
OTTAWA, ON.



BASEPLAN

SAB

DESIGN

JLF

CHECKED

BMT

CAD

SAB

PROJECT MANAGER

BMT

APPROVED

BMT

PROJECT NO.
OTT-00250806-B0
SURVEY
FSI
DATE
APRIL 2019

HAZELDEAN CROSSING TOWNS
5924 HAZELDEAN ROAD
OTTAWA, ONTARIO.

POST-DEVELOPMENT STORM
DRAINAGE PLAN

DRAWING NO.

C400

007-12-19-0089

#18003

Appendix B – Water Servicing Design Tables

Table B1: Water Demand Chart

Table B2: Fire Flow Contribution Based on Hydrant Spacing

Table B3: Fire Flow Requirements based on FUS, 1999 – Block 1

Table B4: Fire Flow Requirements based on FUS, 1999 – Block 2

Table B5: Fire Flow Requirements based on FUS, 1999 – Block 3

Table B6: Fire Flow Requirements based on FUS, 1999 – Block 4

Table B7: Fire Flow Requirements based on FUS, 1999 – Block 5

Table B8: Fire Flow Requirements based on FUS, 1999 – Block 6

Table B9: Fire Flow Requirements based on FUS, 1999 – Block 7

Table B10: Fire Flow Requirements based on FUS, 1999 – Block 8

Table B11: Fire Flow Requirements based on FUS, 1999 – Block 9

Table B12: Fire Flow Requirements based on FUS, 1999 – Block 10

Table B13: Fire Flow Requirements based on FUS, 1999 – Block 11

Table B14: Fire Flow Requirements based on FUS, 1999 – Block 12

TABLE B1: Water Demand Chart



Location:	5924 Hazeldean Road														
Project No:	OTT-00250806														
Designed by:	M. Ghadban														
Checked By:	J.Fitzpatrick														
Date Revised:	Nov 2019														
Water Consumption															
Residential =	350 L/cap/day														
Proposed Buildings	No. of Units								Total Persons (pop)	Demands in (L/sec)					
	Singles/Semis/Towns			Apartments						Average Demand (L/day)	Maximum Demand (L/day)	Peak Hourly Demand (L/day)	Avg Day (L/s)	Max Day (L/s)	Peak Hour (L/s)
	Single Family	Semi-Detached	Duplex	Townhome	Bachelor	1 Bedroom	2 Bedroom	4 Bedroom							
J-1			5						13.5	4,725	21,654	32,659	0.05	0.25	0.38
J-3			2		8				22.2	7,770	35,608	53,706	0.09	0.41	0.62
J-4			3		16				41.7	14,595	66,886	100,881	0.17	0.77	1.17
J-5															
J-6					30				63.0	22,050	101,051	152,410	0.26	1.17	1.76
J-7					14				29.4	10,290	47,157	71,124	0.12	0.55	0.82
J-8															
J-9					8				16.8	5,880	26,947	40,643	0.07	0.31	0.47
J-10															
Totals =			10		76				186.6	65,310	299,303	451,423	0.76	3.46	5.22

FROM MOECC TABLE 3-3 (Peaking Factors for Water Systems Servicing Fewer Than 500 persons

Dwelling Units Serviced	Equivalent Population	Night Min Factor	Maximum Day Factor	Peak Hour Factor
10	30	0.10	9.50	14.30
50	150	0.10	4.90	7.40
100	300	0.20	3.60	5.40
150	450	0.30	3.00	4.50
167	500	0.40	2.90	4.30



TABLE B2: FIRE FLOW CONTRIBUTIONS BASED ON HYDRANT SPACING

TABLE B3
FIRE FLOW REQUIREMENTS BASED ON FIRE UNDERWRITERS SURVEY(FUS) 1999

LOCATION: **Block 1**



An estimate of the Fire Flow required for a given fire area may be estimated by:

$$F = 220 * C * \text{SQRT}(A)$$

where:

F = required fire flow in litres per minute

A = total floor area in m² (including all storeys, but excluding basements at least 50% below grade)

C = coefficient related to the type of construction

Task	Options	Multiplier	Input				Value Used	Fire Flow Total (L/min)
Choose Building Frame (C)	Wood Frame	1.5	Wood Frame				1.5	
	Ordinary Construction	1						
	Non-combustible Construction	0.8						
	Fire Resistive Construction	0.6						
Input Building Floor Areas (A)			Area	% Used	Area Used		1150.0 m ²	
	Floor 3	0	100%	0				
	Floor 2	575	100%	575				
	Floor 1 (Ground Floor Commercial)	575	100%	575				
	Basement (At least 50% below grade, not included)	0	100%	0				
Fire Flow (F)	$F = 220 * C * \text{SQRT}(A)$							11,191
Fire Flow (F)	Rounded to nearest 1,000							11,000

Reductions/Increases Due to Factors Effecting Burning

Task	Options	Multiplier	Input					Value Used	Fire Flow Change (L/min)	Fire Flow Total (L/min)
Choose Combustibility of Building Contents	Non-combustible	-25%	Limited Combustible					-15%	-1,650	9,350
	Limited Combustible	-15%								
	Combustible	0%								
	Free Burning	15%								
	Rapid Burning	25%								
Choose Reduction Due to Sprinkler System	Adequate Sprinkler Conforms to NFPA13	-30%	No Sprinkler					0%	0	9,350
	No Sprinkler	0%								
	Standard Water Supply for Fire Department Hose Line and for Sprinkler System	-10%	Not Standard Water Supply or Unavailable					0%	0	9,350
	Not Standard Water Supply or Unavailable	0%								
	Fully Supervised Sprinkler System	-10%	Not Fully Supervised or N/A					0%	0	9,350
	Not Fully Supervised or N/A	0%								
Choose Structure Exposure Distance	Exposures	Separation Dist (m)	Cond	Separation Condition	Exposed Wall type	Length (m)	No of Storeys	Lenth-height Factor	Sub-Condition	Charge (%)
	Side 1 (west)	32	5	30.1 to 45	Type A	41	4	164	5E	5%
	Side 2 (east)	33	5	30.1 to 45	Type A	15	2	30	5A	5%
	Side 3 (north)	3	1	0 to 3	Type A	11	4	44	1B	23%
	Side 4 (south)	19	3	10.1 to 20	Type A	14	4	30	3A	12%
Obtain Required Fire Flow	Total Required Fire Flow, Rounded to the Nearest 1,000 L/min =									14,000
	Total Required Fire Flow, L/s =									233
	Can the Total Fire Flow be Capped at 10,000 L/min (167 L/sec) based on "TECHNICAL BULLETIN ISTB-2018-02", (yes/no) =									No
Total Required Fire Flow (RFF). If RFF < 167 use RFF (L/sec) =										233

Exposure Charges for Exposing Walls of Wood Frame Construction (from Table G5)

- Type A Wood-Frame or non-combustible
- Type B Ordinary or fire-resistive with unprotected openings
- Type C Ordinary or fire-resistive with semi-protected openings
- Type D Ordinary or fire-resistive with blank wall

Conditions for Separation

Separation Dist Condition

0m to 3m	1
3.1m to 10m	2
10.1m to 20m	3
20.1m to 30m	4
30.1m to 45m	5
> 45.1m	6

TABLE B4
FIRE FLOW REQUIREMENTS BASED ON FIRE UNDERWRITERS SURVEY(FUS) 1999

LOCATION: **Block 2**



An estimate of the Fire Flow required for a given fire area may be estimated by:

$$F = 220 * C * \text{SQRT}(A)$$

where:

F = required fire flow in litres per minute

A = total floor area in m² (including all storeys, but excluding basements at least 50% below grade)

C = coefficient related to the type of construction

Task	Options	Multiplier	Input				Value Used	Fire Flow Total (L/min)
Choose Building Frame (C)	Wood Frame	1.5	Wood Frame				1.5	
	Ordinary Construction	1						
	Non-combustible Construction	0.8						
	Fire Resistive Construction	0.6						
Input Building Floor Areas (A)			Area	% Used	Area Used		828.0 m ²	
	Floor 3	207	100%	207				
	Floor 2	207	100%	207				
	Floor 1 (Ground Floor Commercial)	207	100%	207				
	Basement (At least 50% below grade, not included)	207	100%	207				
Fire Flow (F)	$F = 220 * C * \text{SQRT}(A)$							9,496
Fire Flow (F)	Rounded to nearest 1,000							9,000

Reductions/Increases Due to Factors Effecting Burning

Task	Options	Multiplier	Input					Value Used	Fire Flow Change (L/min)	Fire Flow Total (L/min)			
Choose Combustibility of Building Contents	Non-combustible	-25%	Limited Combustible					-15%	-1,350	7,650			
	Limited Combustible	-15%											
	Combustible	0%											
	Free Burning	15%											
	Rapid Burning	25%											
Choose Reduction Due to Sprinkler System	Adequate Sprinkler Conforms to NFPA13	-30%	No Sprinkler					0%	0	7,650			
	No Sprinkler	0%											
	Standard Water Supply for Fire Department Hose Line and for Sprinkler System	-10%	Not Standard Water Supply or Unavailable					0%	0	7,650			
	Not Standard Water Supply or Unavailable	0%											
	Fully Supervised Sprinkler System	-10%	Not Fully Supervised or N/A					0%	0	7,650			
	Not Fully Supervised or N/A	0%											
Choose Structure Exposure Distance	Exposures	Separation Dist (m)	Cond	Separation Condition	Exposed Wall type	Length (m)	No of Storeys	Lenth-height Factor	Sub-Condition	Charge (%)	Total Charge (%)	Total Exposure Charge (L/min)	
	Side 1 (west)	25	4	20.1 to 30	Type A	10	4	40	4B	8%	49%	3,749	11,399
	Side 2 (east)	20	3	10.1 to 20	Type A	22	2	44	3B	13%			
	Side 3 (north)	2	1	0 to 3	Type A	10	4	40	1B	23%			
	Side 4 (south)	38	5	30.1 to 45	Type A	1	2	30	5A	5%			
Obtain Required Fire Flow	Total Required Fire Flow, Rounded to the Nearest 1,000 L/min =										11,000		
	Total Required Fire Flow, L/s =										183		
	Can the Total Fire Flow be Capped at 10,000 L/min (167 L/sec) based on "TECHNICAL BULLETIN ISTB-2018-02", (yes/no) =										No		
	Total Required Fire Flow (RFF). If RFF < 167 use RFF (L/sec) =										183		

Exposure Charges for Exposing Walls of Wood Frame Construction (from Table G5)

- Type A Wood-Frame or non-combustible
- Type B Ordinary or fire-resistive with unprotected openings
- Type C Ordinary or fire-resistive with semi-protected openings
- Type D Ordinary or fire-resistive with blank wall

Conditions for Separation

Separation Dist	Condition
0m to 3m	1
3.1m to 10m	2
10.1m to 20m	3
20.1m to 30m	4
30.1m to 45m	5
> 45.1m	6

TABLE B5
FIRE FLOW REQUIREMENTS BASED ON FIRE UNDERWRITERS SURVEY(FUS) 1999

LOCATION: **Block 3**



An estimate of the Fire Flow required for a given fire area may be estimated by:

$$F = 220 * C * \text{SQRT}(A)$$

where:

F = required fire flow in litres per minute

A = total floor area in m² (including all storeys, but excluding basements at least 50% below grade)

C = coefficient related to the type of construction

Task	Options	Multiplier	Input				Value Used	Fire Flow Total (L/min)
Choose Building Frame (C)	Wood Frame	1.5	Wood Frame				1.5	
	Ordinary Construction	1						
	Non-combustible Construction	0.8						
	Fire Resistive Construction	0.6						
Input Building Floor Areas (A)			Area	% Used	Area Used		420.0 m ²	
	Floor 3	105	100%	105				
	Floor 2	105	100%	105				
	Floor 1 (Ground Floor Commercial)	105	100%	105				
	Basement (At least 50% below grade, not included)	105	100%	105				
Fire Flow (F)	$F = 220 * C * \text{SQRT}(A)$							6,763
Fire Flow (F)	Rounded to nearest 1,000							7,000

Reductions/Increases Due to Factors Effecting Burning

Task	Options	Multiplier	Input					Value Used	Fire Flow Change (L/min)	Fire Flow Total (L/min)			
Choose Combustibility of Building Contents	Non-combustible	-25%	Limited Combustible					-15%	-1,050	5,950			
	Limited Combustible	-15%											
	Combustible	0%											
	Free Burning	15%											
	Rapid Burning	25%											
Choose Reduction Due to Sprinkler System	Adequate Sprinkler Conforms to NFPA13	-30%	No Sprinkler					0%	0	5,950			
	No Sprinkler	0%											
	Standard Water Supply for Fire Department Hose Line and for Sprinkler System	-10%	Not Standard Water Supply or Unavailable					0%	0	5,950			
	Not Standard Water Supply or Unavailable	0%											
	Fully Supervised Sprinkler System	-10%	Not Fully Supervised or N/A					0%	0	5,950			
	Not Fully Supervised or N/A	0%											
Choose Structure Exposure Distance	Exposures	Separation Dist (m)	Cond	Separation Condition	Exposed Wall type	Length (m)	No of Storeys	Lenth-height Factor	Sub-Condition	Charge (%)	Total Charge (%)	Total Exposure Charge (L/min)	
	Side 1 (west)	64	6	> 45.1	Type A	11	4	44	6	0%	40%	2,380	8,330
	Side 2 (east)	32	5	30.1 to 45	Type A	11	4	44	5B	5%			
	Side 3 (north)	18	3	10.1 to 20	Type A	10	4	40	3B	13%			
	Side 4 (south)	2	1	0 to 3	Type A	10	4	30	1A	22%			
Obtain Required Fire Flow	Total Required Fire Flow, Rounded to the Nearest 1,000 L/min =										8,000		
	Total Required Fire Flow, L/s =										133		
	Can the Total Fire Flow be Capped at 10,000 L/min (167 L/sec) based on "TECHNICAL BULLETIN ISTB-2018-02", (yes/no) =										No		
	Total Required Fire Flow (RFF). If RFF < 167 use RFF (L/sec) =										133		

Exposure Charges for Exposing Walls of Wood Frame Construction (from Table G5)

- Type A Wood-Frame or non-combustible
- Type B Ordinary or fire-resistive with unprotected openings
- Type C Ordinary or fire-resistive with semi-protected openings
- Type D Ordinary or fire-resistive with blank wall

Conditions for Separation

Separation Dist	Condition
0m to 3m	1
3.1m to 10m	2
10.1m to 20m	3
20.1m to 30m	4
30.1m to 45m	5
> 45.1m	6

TABLE B6
FIRE FLOW REQUIREMENTS BASED ON FIRE UNDERWRITERS SURVEY(FUS) 1999

LOCATION: **Block 4**



An estimate of the Fire Flow required for a given fire area may be estimated by:

$$F = 220 * C * \text{SQRT}(A)$$

where:

F = required fire flow in litres per minute

A = total floor area in m² (including all storeys, but excluding basements at least 50% below grade)

C = coefficient related to the type of construction

Task	Options	Multiplier	Input				Value Used	Fire Flow Total (L/min)
Choose Building Frame (C)	Wood Frame	1.5	Wood Frame				1.5	
	Ordinary Construction	1						
	Non-combustible Construction	0.8						
	Fire Resistive Construction	0.6						
Input Building Floor Areas (A)			Area	% Used	Area Used		1240.0 m ²	
	Floor 3	310	100%	310				
	Floor 2	310	100%	310				
	Floor 1 (Ground Floor Commercial)	310	100%	310				
	Basement (At least 50% below grade, not included)	310	100%	310				
Fire Flow (F)	$F = 220 * C * \text{SQRT}(A)$							11,620
Fire Flow (F)	Rounded to nearest 1,000							12,000

Reductions/Increases Due to Factors Effecting Burning

Task	Options	Multiplier	Input					Value Used	Fire Flow Change (L/min)	Fire Flow Total (L/min)
Choose Combustibility of Building Contents	Non-combustible	-25%	Limited Combustible					-15%	-1,800	10,200
	Limited Combustible	-15%								
	Combustible	0%								
	Free Burning	15%								
	Rapid Burning	25%								
Choose Reduction Due to Sprinkler System	Adequate Sprinkler Conforms to NFPA13	-30%	No Sprinkler					0%	0	10,200
	No Sprinkler	0%								
	Standard Water Supply for Fire Department Hose Line and for Sprinkler System	-10%	Not Standard Water Supply or Unavailable					0%	0	10,200
	Not Standard Water Supply or Unavailable	0%								
	Fully Supervised Sprinkler System	-10%								
	Not Fully Supervised or N/A	0%	Not Fully Supervised or N/A					0%	0	10,200
Choose Structure Exposure Distance	Exposures	Separation Dist (m)	Cond	Separation Condition	Exposed Wall type	Length (m)	No of Storeys	Lenth-height Factor	Sub-Condition	Charge (%)
	Side 1 (west)	6	2	3.1 to 10	Type A	10	4	40	2B	18%
	Side 2 (east)	25	4	20.1 to 30	Type A	10	4	40	4B	8%
	Side 3 (north)	32	5	30.1 to 45	Type A	29	4	116	5D	5%
	Side 4 (south)	15	3	10.1 to 20	Type A	34	2	30	3A	12%
Obtain Required Fire Flow	Total Required Fire Flow, Rounded to the Nearest 1,000 L/min =									15,000
	Total Required Fire Flow, L/s =									250
	Can the Total Fire Flow be Capped at 10,000 L/min (167 L/sec) based on "TECHNICAL BULLETIN ISTB-2018-02", (yes/no) =									No
Total Required Fire Flow (RFF). If RFF < 167 use RFF (L/sec) =										250

Exposure Charges for Exposing Walls of Wood Frame Construction (from Table G5)

- Type A Wood-Frame or non-combustible
- Type B Ordinary or fire-resistive with unprotected openings
- Type C Ordinary or fire-resistive with semi-protected openings
- Type D Ordinary or fire-resistive with blank wall

Conditions for Separation

Separation Dist Condition

0m to 3m	1
3.1m to 10m	2
10.1m to 20m	3
20.1m to 30m	4
30.1m to 45m	5
> 45.1m	6

TABLE B7
FIRE FLOW REQUIREMENTS BASED ON FIRE UNDERWRITERS SURVEY(FUS) 1999

LOCATION: **Block 5**



An estimate of the Fire Flow required for a given fire area may be estimated by:

$$F = 220 * C * \text{SQRT}(A)$$

where:

F = required fire flow in litres per minute

A = total floor area in m² (including all storeys, but excluding basements at least 50% below grade)

C = coefficient related to the type of construction

Task	Options	Multiplier	Input				Value Used	Fire Flow Total (L/min)
Choose Building Frame (C)	Wood Frame	1.5	Wood Frame				1.5	
	Ordinary Construction	1						
	Non-combustible Construction	0.8						
	Fire Resistive Construction	0.6						
Input Building Floor Areas (A)			Area	% Used	Area Used		828.0 m ²	
	Floor 3	207	100%	207				
	Floor 2	207	100%	207				
	Floor 1 (Ground Floor Commercial)	207	100%	207				
	Basement (At least 50% below grade, not included)	207	100%	207				
Fire Flow (F)	$F = 220 * C * \text{SQRT}(A)$							9,496
Fire Flow (F)	Rounded to nearest 1,000							9,000

Reductions/Increases Due to Factors Effecting Burning

Task	Options	Multiplier	Input					Value Used	Fire Flow Change (L/min)	Fire Flow Total (L/min)
Choose Combustibility of Building Contents	Non-combustible	-25%	Limited Combustible					-15%	-1,350	7,650
	Limited Combustible	-15%								
	Combustible	0%								
	Free Burning	15%								
	Rapid Burning	25%								
Choose Reduction Due to Sprinkler System	Adequate Sprinkler Conforms to NFPA13	-30%	No Sprinkler					0%	0	7,650
	No Sprinkler	0%								
	Standard Water Supply for Fire Department Hose Line and for Sprinkler System	-10%	Not Standard Water Supply or Unavailable					0%	0	7,650
	Not Standard Water Supply or Unavailable	0%								
	Fully Supervised Sprinkler System	-10%								
	Not Fully Supervised or N/A	0%	Not Fully Supervised or N/A					0%	0	7,650
Choose Structure Exposure Distance	Exposures	Separation Dist (m)	Cond	Separation Condition	Exposed Wall type	Length (m)	No of Storeys	Lenth-height Factor	Sub-Condition	Charge (%)
	Side 1 (west)	11	3	10.1 to 20	Type A	22	2	44	3B	13%
	Side 2 (east)	6	2	3.1 to 10	Type A	22	4	88	2C	19%
	Side 3 (north)	2	1	0 to 3	Type A	10	4	40	1B	23%
	Side 4 (south)	16	3	10.1 to 20	Type A	6	2	30	3A	12%
Obtain Required Fire Flow	Total Required Fire Flow, Rounded to the Nearest 1,000 L/min =									13,000
	Total Required Fire Flow, L/s =									217
	Can the Total Fire Flow be Capped at 10,000 L/min (167 L/sec) based on "TECHNICAL BULLETIN ISTB-2018-02", (yes/no) =									No
	Total Required Fire Flow (RFF). If RFF < 167 use RFF (L/sec) =									217

Exposure Charges for Exposing Walls of Wood Frame Construction (from Table G5)

- Type A Wood-Frame or non-combustible
- Type B Ordinary or fire-resistive with unprotected openings
- Type C Ordinary or fire-resistive with semi-protected openings
- Type D Ordinary or fire-resistive with blank wall

Conditions for Separation

Separation Dist Condition

0m to 3m	1
3.1m to 10m	2
10.1m to 20m	3
20.1m to 30m	4
30.1m to 45m	5
> 45.1m	6

TABLE B8
FIRE FLOW REQUIREMENTS BASED ON FIRE UNDERWRITERS SURVEY(FUS) 1999

LOCATION: **Block 6**



An estimate of the Fire Flow required for a given fire area may be estimated by:

$$F = 220 * C * \text{SQRT}(A)$$

where:

F = required fire flow in litres per minute

A = total floor area in m² (including all storeys, but excluding basements at least 50% below grade)

C = coefficient related to the type of construction

Task	Options	Multiplier	Input				Value Used	Fire Flow Total (L/min)
Choose Building Frame (C)	Wood Frame	1.5	Wood Frame				1.5	
	Ordinary Construction	1						
	Non-combustible Construction	0.8						
	Fire Resistive Construction	0.6						
Input Building Floor Areas (A)			Area	% Used	Area Used		436.0 m ²	
	Floor 3	109	100%	109				
	Floor 2	109	100%	109				
	Floor 1 (Ground Floor Commercial)	109	100%	109				
	Basement (At least 50% below grade, not included)	109	100%	109				
Fire Flow (F)	$F = 220 * C * \text{SQRT}(A)$							6,891
Fire Flow (F)	Rounded to nearest 1,000							7,000

Reductions/Increases Due to Factors Effecting Burning

Task	Options	Multiplier	Input					Value Used	Fire Flow Change (L/min)	Fire Flow Total (L/min)
Choose Combustibility of Building Contents	Non-combustible	-25%	Limited Combustible					-15%	-1,050	5,950
	Limited Combustible	-15%								
	Combustible	0%								
	Free Burning	15%								
	Rapid Burning	25%								
Choose Reduction Due to Sprinkler System	Adequate Sprinkler Conforms to NFPA13	-30%	No Sprinkler					0%	0	5,950
	No Sprinkler	0%								
	Standard Water Supply for Fire Department Hose Line and for Sprinkler System	-10%	Not Standard Water Supply or Unavailable					0%	0	5,950
	Not Standard Water Supply or Unavailable	0%								
	Fully Supervised Sprinkler System	-10%								
	Not Fully Supervised or N/A	0%	Not Fully Supervised or N/A					0%	0	5,950
Choose Structure Exposure Distance	Exposures	Separation Dist (m)	Cond	Separation Condition	Exposed Wall type	Length (m)	No of Storeys	Lenth-height Factor	Sub-Condition	Charge (%)
	Side 1 (west)	17	3	10.1 to 20	Type A	11	2	22	3A	12%
	Side 2 (east)	112	6	> 45.1	Type A	11	4	44	6	0%
	Side 3 (north)	6	2	3.1 to 10	Type A	10	4	40	2B	18%
	Side 4 (south)	2	1	0 to 3	Type A	10	4	30	1A	22%
Obtain Required Fire Flow	Total Required Fire Flow, Rounded to the Nearest 1,000 L/min =									9,000
	Total Required Fire Flow, L/s =									150
	Can the Total Fire Flow be Capped at 10,000 L/min (167 L/sec) based on "TECHNICAL BULLETIN ISTB-2018-02", (yes/no) =									No
	Total Required Fire Flow (RFF). If RFF < 167 use RFF (L/sec) =									150

Exposure Charges for Exposing Walls of Wood Frame Construction (from Table G5)

- Type A Wood-Frame or non-combustible
- Type B Ordinary or fire-resistive with unprotected openings
- Type C Ordinary or fire-resistive with semi-protected openings
- Type D Ordinary or fire-resistive with blank wall

Conditions for Separation

Separation Dist Condition

0m to 3m	1
3.1m to 10m	2
10.1m to 20m	3
20.1m to 30m	4
30.1m to 45m	5
> 45.1m	6

TABLE B9
FIRE FLOW REQUIREMENTS BASED ON FIRE UNDERWRITERS SURVEY(FUS) 1999

LOCATION: **Block 7**



An estimate of the Fire Flow required for a given fire area may be estimated by:

$$F = 220 * C * \text{SQRT}(A)$$

where:

F = required fire flow in litres per minute

A = total floor area in m² (including all storeys, but excluding basements at least 50% below grade)

C = coefficient related to the type of construction

Task	Options	Multiplier	Input				Value Used	Fire Flow Total (L/min)
Choose Building Frame (C)	Wood Frame	1.5	Wood Frame				1.5	
	Ordinary Construction	1						
	Non-combustible Construction	0.8						
	Fire Resistive Construction	0.6						
Input Building Floor Areas (A)			Area	% Used	Area Used		828.0 m ²	
	Floor 3	207	100%	207				
	Floor 2	207	100%	207				
	Floor 1 (Ground Floor Commercial)	207	100%	207				
	Basement (At least 50% below grade, not included)	207	100%	207				
Fire Flow (F)	$F = 220 * C * \text{SQRT}(A)$							9,496
Fire Flow (F)	Rounded to nearest 1,000							9,000

Reductions/Increases Due to Factors Effecting Burning

Task	Options	Multiplier	Input					Value Used	Fire Flow Change (L/min)	Fire Flow Total (L/min)
Choose Combustibility of Building Contents	Non-combustible	-25%	Limited Combustible					-15%	-1,350	7,650
	Limited Combustible	-15%								
	Combustible	0%								
	Free Burning	15%								
	Rapid Burning	25%								
Choose Reduction Due to Sprinkler System	Adequate Sprinkler Conforms to NFPA13	-30%	No Sprinkler					0%	0	7,650
	No Sprinkler	0%								
	Standard Water Supply for Fire Department Hose Line and for Sprinkler System	-10%	Not Standard Water Supply or Unavailable					0%	0	7,650
	Not Standard Water Supply or Unavailable	0%								
	Fully Supervised Sprinkler System	-10%								
	Not Fully Supervised or N/A	0%	Not Fully Supervised or N/A					0%	0	7,650
Choose Structure Exposure Distance	Exposures	Separation Dist (m)	Cond	Separation Condition	Exposed Wall type	Length (m)	No of Storeys	Lenth-height Factor	Sub-Condition	Charge (%)
	Side 1 (west)	27	4	20.1 to 30	Type A	3	2	6	4A	8%
	Side 2 (east)	6	2	3.1 to 10	Type A	10	4	40	2B	18%
	Side 3 (north)	37	5	30.1 to 45	Type A	22	1	22	5A	5%
	Side 4 (south)	6	2	3.1 to 10	Type A	16	4	30	2A	17%
Obtain Required Fire Flow	Total Required Fire Flow, Rounded to the Nearest 1,000 L/min =									11,000
	Total Required Fire Flow, L/s =									183
	Can the Total Fire Flow be Capped at 10,000 L/min (167 L/sec) based on "TECHNICAL BULLETIN ISTB-2018-02", (yes/no) =									No
Total Required Fire Flow (RFF). If RFF < 167 use RFF (L/sec) =										183

Exposure Charges for Exposing Walls of Wood Frame Construction (from Table G5)

- Type A Wood-Frame or non-combustible
- Type B Ordinary or fire-resistive with unprotected openings
- Type C Ordinary or fire-resistive with semi-protected openings
- Type D Ordinary or fire-resistive with blank wall

Conditions for Separation

Separation Dist Condition

0m to 3m	1
3.1m to 10m	2
10.1m to 20m	3
20.1m to 30m	4
30.1m to 45m	5
> 45.1m	6

TABLE B10
FIRE FLOW REQUIREMENTS BASED ON FIRE UNDERWRITERS SURVEY(FUS) 1999

LOCATION: **Block 8**



An estimate of the Fire Flow required for a given fire area may be estimated by:

$$F = 220 * C * \text{SQRT}(A)$$

where:

F = required fire flow in litres per minute

A = total floor area in m² (including all storeys, but excluding basements at least 50% below grade)

C = coefficient related to the type of construction

Task	Options	Multiplier	Input				Value Used	Fire Flow Total (L/min)
Choose Building Frame (C)	Wood Frame	1.5	Wood Frame				1.5	
	Ordinary Construction	1						
	Non-combustible Construction	0.8						
	Fire Resistive Construction	0.6						
Input Building Floor Areas (A)			Area	% Used	Area Used		828.0 m ²	
	Floor 3	207	100%	207				
	Floor 2	207	100%	207				
	Floor 1 (Ground Floor Commercial)	207	100%	207				
	Basement (At least 50% below grade, not included)	207	100%	207				
Fire Flow (F)	$F = 220 * C * \text{SQRT}(A)$							9,496
Fire Flow (F)	Rounded to nearest 1,000							9,000

Reductions/Increases Due to Factors Effecting Burning

Task	Options	Multiplier	Input					Value Used	Fire Flow Change (L/min)	Fire Flow Total (L/min)
Choose Combustibility of Building Contents	Non-combustible	-25%	Limited Combustible					-15%	-1,350	7,650
	Limited Combustible	-15%								
	Combustible	0%								
	Free Burning	15%								
	Rapid Burning	25%								
Choose Reduction Due to Sprinkler System	Adequate Sprinkler Conforms to NFPA13	-30%	No Sprinkler					0%	0	7,650
	No Sprinkler	0%								
	Standard Water Supply for Fire Department Hose Line and for Sprinkler System	-10%	Not Standard Water Supply or Unavailable					0%	0	7,650
	Not Standard Water Supply or Unavailable	0%								
	Fully Supervised Sprinkler System	-10%								
	Not Fully Supervised or N/A	0%	Not Fully Supervised or N/A					0%	0	7,650
Choose Structure Exposure Distance	Exposures	Separation Dist (m)	Cond	Separation Condition	Exposed Wall type	Length (m)	No of Storeys	Lenth-height Factor	Sub-Condition	Charge (%)
	Side 1 (west)	6	2	3.1 to 10	Type A	10	4	40	2B	18%
	Side 2 (east)	3	1	0 to 3	Type A	10	4	40	1B	23%
	Side 3 (north)	37	5	30.1 to 45	Type A	7	1	7	5A	5%
	Side 4 (south)	32	5	30.1 to 45	Type A	20	4	30	5A	5%
Obtain Required Fire Flow	Total Required Fire Flow, Rounded to the Nearest 1,000 L/min =									12,000
	Total Required Fire Flow, L/s =									200
	Can the Total Fire Flow be Capped at 10,000 L/min (167 L/sec) based on "TECHNICAL BULLETIN ISTB-2018-02", (yes/no) =									No
	Total Required Fire Flow (RFF). If RFF < 167 use RFF (L/sec) =									200

Exposure Charges for Exposing Walls of Wood Frame Construction (from Table G5)

- Type A Wood-Frame or non-combustible
- Type B Ordinary or fire-resistive with unprotected openings
- Type C Ordinary or fire-resistive with semi-protected openings
- Type D Ordinary or fire-resistive with blank wall

Conditions for Separation

Separation Dist Condition

0m to 3m	1
3.1m to 10m	2
10.1m to 20m	3
20.1m to 30m	4
30.1m to 45m	5
> 45.1m	6

TABLE B11
FIRE FLOW REQUIREMENTS BASED ON FIRE UNDERWRITERS SURVEY(FUS) 1999

LOCATION: **Block 9**



An estimate of the Fire Flow required for a given fire area may be estimated by:

$$F = 220 * C * \text{SQRT}(A)$$

where:

F = required fire flow in litres per minute

A = total floor area in m² (including all storeys, but excluding basements at least 50% below grade)

C = coefficient related to the type of construction

Task	Options	Multiplier	Input				Value Used	Fire Flow Total (L/min)
Choose Building Frame (C)	Wood Frame	1.5	Wood Frame				1.5	
	Ordinary Construction	1						
	Non-combustible Construction	0.8						
	Fire Resistive Construction	0.6						
Input Building Floor Areas (A)			Area	% Used	Area Used		420.0 m ²	
	Floor 3	105	100%	105				
	Floor 2	105	100%	105				
	Floor 1 (Ground Floor Commercial)	105	100%	105				
	Basement (At least 50% below grade, not included)	105	100%	105				
Fire Flow (F)	$F = 220 * C * \text{SQRT}(A)$							6,763
Fire Flow (F)	Rounded to nearest 1,000							7,000

Reductions/Increases Due to Factors Effecting Burning

Task	Options	Multiplier	Input					Value Used	Fire Flow Change (L/min)	Fire Flow Total (L/min)
Choose Combustibility of Building Contents	Non-combustible	-25%	Limited Combustible					-15%	-1,050	5,950
	Limited Combustible	-15%								
	Combustible	0%								
	Free Burning	15%								
	Rapid Burning	25%								
Choose Reduction Due to Sprinkler System	Adequate Sprinkler Conforms to NFPA13	-30%	No Sprinkler					0%	0	5,950
	No Sprinkler	0%								
	Standard Water Supply for Fire Department Hose Line and for Sprinkler System	-10%	Not Standard Water Supply or Unavailable					0%	0	5,950
	Not Standard Water Supply or Unavailable	0%								
	Fully Supervised Sprinkler System	-10%								
	Not Fully Supervised or N/A	0%	Not Fully Supervised or N/A					0%	0	5,950
Choose Structure Exposure Distance	Exposures	Separation Dist (m)	Cond	Separation Condition	Exposed Wall type	Length (m)	No of Storeys	Lenth-height Factor	Sub-Condition	Charge (%)
	Side 1 (west)	3	1	0 to 3	Type A	10	4	40	1B	23%
	Side 2 (east)	3	1	0 to 3	Type A	10	4	40	1B	23%
	Side 3 (north)	41	5	30.1 to 45	Type A	8	2	16	5A	5%
	Side 4 (south)	63	6	> 45.1	Type A	8	4	30	6	0%
Obtain Required Fire Flow	Total Required Fire Flow, Rounded to the Nearest 1,000 L/min =									9,000
	Total Required Fire Flow, L/s =									150
	Can the Total Fire Flow be Capped at 10,000 L/min (167 L/sec) based on "TECHNICAL BULLETIN ISTB-2018-02", (yes/no) =									No
	Total Required Fire Flow (RFF). If RFF < 167 use RFF (L/sec) =									150

Exposure Charges for Exposing Walls of Wood Frame Construction (from Table G5)

- Type A Wood-Frame or non-combustible
- Type B Ordinary or fire-resistive with unprotected openings
- Type C Ordinary or fire-resistive with semi-protected openings
- Type D Ordinary or fire-resistive with blank wall

Conditions for Separation

Separation Dist Condition

0m to 3m	1
3.1m to 10m	2
10.1m to 20m	3
20.1m to 30m	4
30.1m to 45m	5
> 45.1m	6

TABLE B12
FIRE FLOW REQUIREMENTS BASED ON FIRE UNDERWRITERS SURVEY(FUS) 1999

LOCATION: **Block 10**



An estimate of the Fire Flow required for a given fire area may be estimated by:

$$F = 220 * C * \text{SQRT}(A)$$

where:

F = required fire flow in litres per minute

A = total floor area in m² (including all storeys, but excluding basements at least 50% below grade)

C = coefficient related to the type of construction

Task	Options	Multiplier	Input				Value Used	Fire Flow Total (L/min)
Choose Building Frame (C)	Wood Frame	1.5	Wood Frame				1.5	
	Ordinary Construction	1						
	Non-combustible Construction	0.8						
	Fire Resistive Construction	0.6						
Input Building Floor Areas (A)			Area	% Used	Area Used		828.0 m ²	
	Floor 3	207	100%	207				
	Floor 2	207	100%	207				
	Floor 1 (Ground Floor Commercial)	207	100%	207				
	Basement (At least 50% below grade, not included)	207	100%	207				
Fire Flow (F)	$F = 220 * C * \text{SQRT}(A)$							9,496
Fire Flow (F)	Rounded to nearest 1,000							9,000

Reductions/Increases Due to Factors Effecting Burning

Task	Options	Multiplier	Input					Value Used	Fire Flow Change (L/min)	Fire Flow Total (L/min)
Choose Combustibility of Building Contents	Non-combustible	-25%	Limited Combustible					-15%	-1,350	7,650
	Limited Combustible	-15%								
	Combustible	0%								
	Free Burning	15%								
	Rapid Burning	25%								
Choose Reduction Due to Sprinkler System	Adequate Sprinkler Conforms to NFPA13	-30%	No Sprinkler					0%	0	7,650
	No Sprinkler	0%								
	Standard Water Supply for Fire Department Hose Line and for Sprinkler System	-10%	Not Standard Water Supply or Unavailable					0%	0	7,650
	Not Standard Water Supply or Unavailable	0%								
	Fully Supervised Sprinkler System	-10%								
	Not Fully Supervised or N/A	0%	Not Fully Supervised or N/A					0%	0	7,650
Choose Structure Exposure Distance	Exposures	Separation Dist (m)	Cond	Separation Condition	Exposed Wall type	Length (m)	No of Storeys	Lenth-height Factor	Sub-Condition	Charge (%)
	Side 1 (west)	3	1	0 to 3	Type A	10	4	40	1B	23%
	Side 2 (east)	3	1	0 to 3	Type A	1	4	4	1A	22%
	Side 3 (north)	45	5	30.1 to 45	Type A	10	2	20	5A	5%
	Side 4 (south)	18	3	10.1 to 20	Type A	22	4	30	3A	12%
Obtain Required Fire Flow	Total Required Fire Flow, Rounded to the Nearest 1,000 L/min =									12,000
	Total Required Fire Flow, L/s =									200
	Can the Total Fire Flow be Capped at 10,000 L/min (167 L/sec) based on "TECHNICAL BULLETIN ISTB-2018-02", (yes/no) =									No
	Total Required Fire Flow (RFF). If RFF < 167 use RFF (L/sec) =									200

Exposure Charges for Exposing Walls of Wood Frame Construction (from Table G5)

- Type A Wood-Frame or non-combustible
- Type B Ordinary or fire-resistive with unprotected openings
- Type C Ordinary or fire-resistive with semi-protected openings
- Type D Ordinary or fire-resistive with blank wall

Conditions for Separation

Separation Dist Condition

0m to 3m	1
3.1m to 10m	2
10.1m to 20m	3
20.1m to 30m	4
30.1m to 45m	5
> 45.1m	6

TABLE B13
FIRE FLOW REQUIREMENTS BASED ON FIRE UNDERWRITERS SURVEY(FUS) 1999

LOCATION: **Block 11**



An estimate of the Fire Flow required for a given fire area may be estimated by:

$$F = 220 * C * \text{SQRT}(A)$$

where:

F = required fire flow in litres per minute

A = total floor area in m² (including all storeys, but excluding basements at least 50% below grade)

C = coefficient related to the type of construction

Task	Options	Multiplier	Input				Value Used	Fire Flow Total (L/min)
Choose Building Frame (C)	Wood Frame	1.5	Wood Frame				1.5	
	Ordinary Construction	1						
	Non-combustible Construction	0.8						
	Fire Resistive Construction	0.6						
Input Building Floor Areas (A)			Area	% Used	Area Used		828.0 m ²	
	Floor 3	207	100%	207				
	Floor 2	207	100%	207				
	Floor 1 (Ground Floor Commercial)	207	100%	207				
	Basement (At least 50% below grade, not included)	207	100%	207				
Fire Flow (F)	$F = 220 * C * \text{SQRT}(A)$							9,496
Fire Flow (F)	Rounded to nearest 1,000							9,000

Reductions/Increases Due to Factors Effecting Burning

Task	Options	Multiplier	Input					Value Used	Fire Flow Change (L/min)	Fire Flow Total (L/min)
Choose Combustibility of Building Contents	Non-combustible	-25%	Limited Combustible					-15%	-1,350	7,650
	Limited Combustible	-15%								
	Combustible	0%								
	Free Burning	15%								
	Rapid Burning	25%								
Choose Reduction Due to Sprinkler System	Adequate Sprinkler Conforms to NFPA13	-30%	No Sprinkler					0%	0	7,650
	No Sprinkler	0%								
	Standard Water Supply for Fire Department Hose Line and for Sprinkler System	-10%	Not Standard Water Supply or Unavailable					0%	0	7,650
	Not Standard Water Supply or Unavailable	0%								
	Fully Supervised Sprinkler System	-10%								
	Not Fully Supervised or N/A	0%	Not Fully Supervised or N/A					0%	0	7,650
Choose Structure Exposure Distance	Exposures	Separation Dist (m)	Cond	Separation Condition	Exposed Wall type	Length (m)	No of Storeys	Lenth-height Factor	Sub-Condition	Charge (%)
	Side 1 (west)	3	1	0 to 3	Type A	10	4	40	1B	23%
	Side 2 (east)	79	6	> 45.1	Type A	22	2	44	6	0%
	Side 3 (north)	45	5	30.1 to 45	Type A	1	2	2	5A	5%
	Side 4 (south)	24	4	20.1 to 30	Type A	10	4	30	4A	8%
Obtain Required Fire Flow	Total Required Fire Flow, Rounded to the Nearest 1,000 L/min =									10,000
	Total Required Fire Flow, L/s =									167
	Can the Total Fire Flow be Capped at 10,000 L/min (167 L/sec) based on "TECHNICAL BULLETIN ISTB-2018-02", (yes/no) =									No
Total Required Fire Flow (RFF). If RFF < 167 use RFF (L/sec) =										167

Exposure Charges for Exposing Walls of Wood Frame Construction (from Table G5)

- Type A Wood-Frame or non-combustible
- Type B Ordinary or fire-resistive with unprotected openings
- Type C Ordinary or fire-resistive with semi-protected openings
- Type D Ordinary or fire-resistive with blank wall

Conditions for Separation

Separation Dist Condition

0m to 3m	1
3.1m to 10m	2
10.1m to 20m	3
20.1m to 30m	4
30.1m to 45m	5
> 45.1m	6

TABLE B14
FIRE FLOW REQUIREMENTS BASED ON FIRE UNDERWRITERS SURVEY(FUS) 1999

LOCATION: **Block 12**



An estimate of the Fire Flow required for a given fire area may be estimated by:

$$F = 220 * C * \text{SQRT}(A)$$

where:

F = required fire flow in litres per minute

A = total floor area in m² (including all storeys, but excluding basements at least 50% below grade)

C = coefficient related to the type of construction

Task	Options	Multiplier	Input				Value Used	Fire Flow Total (L/min)
Choose Building Frame (C)	Wood Frame	1.5	Wood Frame				1.5	
	Ordinary Construction	1						
	Non-combustible Construction	0.8						
	Fire Resistive Construction	0.6						
Input Building Floor Areas (A)			Area	% Used	Area Used		420.0 m ²	
	Floor 3	105	100%	105				
	Floor 2	105	100%	105				
	Floor 1 (Ground Floor Commercial)	105	100%	105				
	Basement (At least 50% below grade, not included)	105	100%	105				
Fire Flow (F)	$F = 220 * C * \text{SQRT}(A)$							6,763
Fire Flow (F)	Rounded to nearest 1,000							7,000

Reductions/Increases Due to Factors Effecting Burning

Task	Options	Multiplier	Input					Value Used	Fire Flow Change (L/min)	Fire Flow Total (L/min)
Choose Combustibility of Building Contents	Non-combustible	-25%	Limited Combustible					-15%	-1,050	5,950
	Limited Combustible	-15%								
	Combustible	0%								
	Free Burning	15%								
	Rapid Burning	25%								
Choose Reduction Due to Sprinkler System	Adequate Sprinkler Conforms to NFPA13	-30%	No Sprinkler					0%	0	5,950
	No Sprinkler	0%								
	Standard Water Supply for Fire Department Hose Line and for Sprinkler System	-10%	Not Standard Water Supply or Unavailable					0%	0	5,950
	Not Standard Water Supply or Unavailable	0%								
	Fully Supervised Sprinkler System	-10%								
	Not Fully Supervised or N/A	0%	Not Fully Supervised or N/A					0%	0	5,950
Choose Structure Exposure Distance	Exposures	Separation Dist (m)	Cond	Separation Condition	Exposed Wall type	Length (m)	No of Storeys	Lenth-height Factor	Sub-Condition	Charge (%)
	Side 1 (west)	115	6	> 45.1	Type A	5	4	20	6	0%
	Side 2 (east)	30	4	20.1 to 30	Type A	9	4	36	4B	8%
	Side 3 (north)	58	6	> 45.1	Type A	8	2	16	6	0%
	Side 4 (south)	4	2	3.1 to 10	Type A	10	4	30	2A	17%
Obtain Required Fire Flow	Total Required Fire Flow, Rounded to the Nearest 1,000 L/min =									7,000
	Total Required Fire Flow, L/s =									117
	Can the Total Fire Flow be Capped at 10,000 L/min (167 L/sec) based on "TECHNICAL BULLETIN ISTB-2018-02", (yes/no) =									No
	Total Required Fire Flow (RFF). If RFF < 167 use RFF (L/sec) =									117

Exposure Charges for Exposing Walls of Wood Frame Construction (from Table G5)

- Type A Wood-Frame or non-combustible
- Type B Ordinary or fire-resistive with unprotected openings
- Type C Ordinary or fire-resistive with semi-protected openings
- Type D Ordinary or fire-resistive with blank wall

Conditions for Separation

Separation Dist	Condition
0m to 3m	1
3.1m to 10m	2
10.1m to 20m	3
20.1m to 30m	4
30.1m to 45m	5
> 45.1m	6

Appendix C – WaterGems Output Tables

- Scenario 1 Result Tables (Peak Hour)
 - Junction Table
 - Pipe Table
 - Reservoir Table
- Scenario 2 Result Tables (Max Day Plus Fire Flow - 10,000 L/min)
 - Junction Table
 - Pipe Table
 - Reservoir Table
 - Fire Flow Report

5924 & 5938 Hazeldean Road
PEAK HOUR - HGL AT CONNECTION #1 (VICTOR / DENHAM)
Junction Table - Time: 0.00 hours

Label	Elevation (m)	Demand (L/s)	Hydraulic Grade (m)	Pressure (psi)
J-1	114.36	0.38	157.20	60.8
J-2	114.00	0.00	157.20	61.3
J-3	114.00	0.62	157.20	61.3
J-4	113.95	1.17	157.19	61.4
J-5	114.36	0.00	157.20	60.8
J-6	114.50	1.76	157.19	60.6
J-7	114.32	0.82	157.19	60.9
J-8	113.90	0.00	157.19	61.5
J-9	115.45	0.47	156.84	58.8
J-10	113.20	0.00	157.20	62.5

Pipe Table - Time: 0.00 hours

Label	Start Node	Stop Node	Length (Scaled) (m)	Diameter (mm)	Hazen-William s C	Flow (L/s)	Hydraulic Grade (L/s)	Hydraulic Grade (Stop) (m)	Velocity (m/s)	Headloss Gradient (m/m)
P-2	J-2	J-3	15	204.0	110.0	2.94	157.20	157.20	0.09	0.000
P-3	J-3	J-8	23	204.0	110.0	2.32	157.19	157.20	0.07	0.000
P-4	J-8	J-4	9	204.0	110.0	2.32	157.19	157.19	0.07	0.000
P-5	J-4	J-7	39	204.0	110.0	1.15	157.19	157.19	0.04	0.000
P-6	J-7	J-6	43	204.0	110.0	0.33	157.19	157.19	0.01	0.000
P-7	J-6	J-5	42	204.0	110.0	-1.90	157.20	157.19	0.06	0.000
P-8	J-9	J-6	29	38.0	100.0	-0.47	157.19	156.84	0.41	0.012
P-9	J-1	J-10	114	204.0	110.0	1.90	157.20	157.20	0.06	0.000
P-10	J-10	J-5	124	297.0	110.0	1.90	157.20	157.20	0.03	0.000
P-11	R-1	J-1	20	600.0	130.0	5.22	157.20	157.20	0.02	0.000
P-12	J-8	H-2	3	155.0	100.0	0.00	157.19	157.19	0.00	0.000
P-13	H-1	J-7	4	155.0	100.0	0.00	157.19	157.19	0.00	0.000

Reservoir Table - Time: 0.00 hours

ID	Label	Zone	Flow (Out net) (L/s)	Hydraulic Grade (m)
55	R-1	<None>	5.22	157.20

5924 & 5938 Hazeldean Road
MAX DAY PLUS FIREFLOW - HGL AT CONNECTION #1 (VICTOR / DENHAM)

Junction Table - Time: 0.00 hours

Label	Elevation (m)	Demand (L/s)	Hydraulic Grade (m)	Pressure (psi)
J-1	114.36	0.25	135.40	29.9
J-2	114.00	0.00	135.40	30.4
J-3	114.00	0.41	135.40	30.4
J-4	113.95	0.77	135.40	30.4
J-5	114.36	0.00	135.40	29.9
J-6	114.50	1.17	135.40	29.7
J-7	114.32	0.55	135.40	29.9
J-8	113.90	0.00	135.40	30.5
J-9	115.45	0.31	135.24	28.1
J-10	113.20	0.00	135.40	31.5

Pipe Table - Time: 0.00 hours

Label	Start Node	Stop Node	Length (Scaled) (m)	Diameter (mm)	Hazen-William s C	Flow (L/s)	Hydraulic Grade (Stop) (m)	Hydraulic Grade (Start) (m)	Velocity (m/s)	Headloss Gradient (m/m)
P-2	J-2	J-3	15	204.0	110.0	1.95	135.40	135.40	0.06	0.000
P-3	J-3	J-8	23	204.0	110.0	1.54	135.40	135.40	0.05	0.000
P-4	J-8	J-4	9	204.0	110.0	1.54	135.40	135.40	0.05	0.000
P-5	J-4	J-7	39	204.0	110.0	0.77	135.40	135.40	0.02	0.000
P-6	J-7	J-6	43	204.0	110.0	0.22	135.40	135.40	0.01	0.000
P-7	J-6	J-5	42	204.0	110.0	-1.26	135.40	135.40	0.04	0.000
P-8	J-9	J-6	29	38.0	100.0	-0.31	135.40	135.24	0.27	0.006
P-9	J-1	J-10	114	204.0	110.0	1.26	135.40	135.40	0.04	0.000
P-10	J-10	J-5	124	297.0	110.0	1.26	135.40	135.40	0.02	0.000
P-11	R-1	J-1	20	600.0	130.0	3.46	135.40	135.40	0.01	0.000
P-12	J-8	H-2	3	155.0	100.0	0.00	135.40	135.40	0.00	0.000
P-13	H-1	J-7	4	155.0	100.0	0.00	135.40	135.40	0.00	0.000

Reservoir Table - Time: 0.00 hours

ID	Label	Zone	Flow (Out net) (L/s)	Hydraulic Grade (m)
55	R-1	<None>	3.46	135.40

5924 & 5938 Hazeldean Road
MAX DAY PLUS FIREFLOW - HGL AT CONNECTION #1 (VICTOR /
DENHAM)

Fire Flow Report - Time: 0.00 hours

Label	Fire Flow (Needed) (L/s)	Flow (Total Needed) (L/s)	Fire Flow (Available) (L/s)	Flow (Total Available) (L/s)	Pressure (Calculated Residual) (psi)	Satisfies Fire Flow Constraints?
H-1	0.00	250.00	170.90	170.90	178.7	False
H-2	0.00	250.00	200.85	200.85	178.1	False
J-1	0.00	250.25	300.00	300.25	29.8	True
J-2	0.00	250.00	260.32	260.32	20.0	True
J-3	0.00	250.41	226.66	227.07	20.0	False
J-4	0.00	250.77	193.31	194.08	20.0	False
J-5	0.00	250.00	168.12	168.12	20.0	False
J-6	0.00	251.17	147.53	148.70	21.6	False
J-7	0.00	250.55	170.90	171.45	20.0	False
J-8	0.00	250.00	200.85	200.85	20.0	False
J-9	0.00	(N/A)	(N/A)	(N/A)	(N/A)	(N/A)
J-10	0.00	250.00	181.80	181.80	20.7	False

5924 & 5938 Hazeldean Road

PEAK HOUR - HGL AT CONNECTION #3 (HAZELDEAN)

Junction Table - Time: 0.00 hours

Label	Elevation (m)	Demand (L/s)	Hydraulic Grade (m)	Pressure (psi)
J-1	114.36	0.38	157.30	60.9
J-2	114.00	0.00	157.29	61.5
J-3	114.00	0.62	157.29	61.5
J-4	113.95	1.17	157.29	61.5
J-5	114.36	0.00	157.30	61.0
J-6	114.50	1.76	157.30	60.7
J-7	114.32	0.82	157.29	61.0
J-8	113.90	0.00	157.29	61.6
J-9	115.45	0.47	156.95	58.9
J-10	113.20	0.00	157.30	62.6

Pipe Table - Time: 0.00 hours

Label	Start Node	Stop Node	Length (Scaled) (m)	Diameter (mm)	Hazen-William s C	Flow (L/s)	Hydraulic Grade (Stop) (m)	Hydraulic Grade (Start) (m)	Velocity (m/s)	Headloss Gradient (m/m)
P-2	J-2	J-3	15	204.0	110.0	1.37	157.29	157.29	0.04	0.000
P-3	J-3	J-8	23	204.0	110.0	0.75	157.29	157.29	0.02	0.000
P-4	J-8	J-4	9	204.0	110.0	0.75	157.29	157.29	0.02	0.000
P-5	J-4	J-7	39	204.0	110.0	-0.42	157.29	157.29	0.01	0.000
P-6	J-7	J-6	43	204.0	110.0	-1.24	157.30	157.29	0.04	0.000
P-7	J-6	J-5	42	204.0	110.0	-3.47	157.30	157.30	0.11	0.000
P-8	J-9	J-6	29	38.0	100.0	-0.47	157.30	156.95	0.41	0.012
P-9	J-1	J-10	114	204.0	110.0	-1.75	157.30	157.30	0.05	0.000
P-10	J-10	J-5	124	297.0	110.0	-1.75	157.30	157.30	0.03	0.000
P-11	R-1	J-1	20	600.0	130.0	(N/A)	(N/A)	(N/A)	(N/A)	(N/A)
P-12	J-8	H-2	3	155.0	100.0	0.00	157.29	157.29	0.00	0.000
P-13	H-1	J-7	4	155.0	100.0	0.00	157.29	157.29	0.00	0.000

Reservoir Table - Time: 0.00 hours

ID	Label	Zone	Flow (Out net) (L/s)	Hydraulic Grade (m)
55	R-1	<None>	(N/A)	(N/A)

5924 & 5938 Hazeldean Road
MAX DAY PLUS FIREFLOW - HGL AT CONNECTION #3 (HAZELDEAN)
Junction Table - Time: 0.00 hours

Label	Elevation (m)	Demand (L/s)	Hydraulic Grade (m)	Pressure (psi)
J-1	114.36	0.25	158.30	62.4
J-2	114.00	0.00	158.30	62.9
J-3	114.00	0.41	158.30	62.9
J-4	113.95	0.77	158.30	62.9
J-5	114.36	0.00	158.30	62.4
J-6	114.50	1.17	158.30	62.2
J-7	114.32	0.55	158.30	62.4
J-8	113.90	0.00	158.30	63.0
J-9	115.45	0.31	158.14	60.6
J-10	113.20	0.00	158.30	64.0

Pipe Table - Time: 0.00 hours

Label	Start Node	Stop Node	Length (Scaled) (m)	Diameter (mm)	Hazen-William s C	Flow (L/s)	Hydraulic Grade (Stop) (m)	Hydraulic Grade (Start) (m)	Velocity (m/s)	Headloss Gradient (m/m)
P-2	J-2	J-3	15	204.0	110.0	0.91	158.30	158.30	0.03	0.000
P-3	J-3	J-8	23	204.0	110.0	0.50	158.30	158.30	0.02	0.000
P-4	J-8	J-4	9	204.0	110.0	0.50	158.30	158.30	0.02	0.000
P-5	J-4	J-7	39	204.0	110.0	-0.27	158.30	158.30	0.01	0.000
P-6	J-7	J-6	43	204.0	110.0	-0.82	158.30	158.30	0.03	0.000
P-7	J-6	J-5	42	204.0	110.0	-2.30	158.30	158.30	0.07	0.000
P-8	J-9	J-6	29	38.0	100.0	-0.31	158.30	158.14	0.27	0.006
P-9	J-1	J-10	114	204.0	110.0	-1.16	158.30	158.30	0.04	0.000
P-10	J-10	J-5	124	297.0	110.0	-1.16	158.30	158.30	0.02	0.000
P-11	R-1	J-1	20	600.0	130.0	(N/A)	(N/A)	(N/A)	(N/A)	(N/A)
P-12	J-8	H-2	3	155.0	100.0	0.00	158.30	158.30	0.00	0.000
P-13	H-1	J-7	4	155.0	100.0	0.00	158.30	158.30	0.00	0.000

Reservoir Table - Time: 0.00 hours

ID	Label	Zone	Flow (Out net) (L/s)	Hydraulic Grade (m)
55	R-1	<None>	(N/A)	(N/A)

5924 & 5938 Hazeldean Road
MAX DAY PLUS FIREFLOW - HGL AT CONNECTION #3 (HAZELDEAN)
Fire Flow Report - Time: 0.00 hours

Label	Fire Flow (Needed) (L/s)	Flow (Total Needed) (L/s)	Fire Flow (Available) (L/s)	Flow (Total Available) (L/s)	Pressure (Calculated Residual) (psi)	Satisfies Fire Flow Constraints?
H-1	0.00	250.00	300.00	300.00	191.0	True
H-2	0.00	250.00	300.00	300.00	188.8	True
J-1	0.00	250.25	300.00	300.25	33.9	True
J-2	0.00	250.00	300.00	300.00	33.3	True
J-3	0.00	250.41	300.00	300.41	33.5	True
J-4	0.00	250.77	300.00	300.77	35.0	True
J-5	0.00	250.00	300.00	300.00	62.3	True
J-6	0.00	251.17	300.00	301.17	46.9	True
J-7	0.00	250.55	300.00	300.55	38.8	True
J-8	0.00	250.00	300.00	300.00	34.5	True
J-9	0.00	(N/A)	(N/A)	(N/A)	(N/A)	(N/A)
J-10	0.00	250.00	300.00	300.00	55.4	True

Appendix D – Sanitary Sewer Design Tables

Table D1: Sanitary Sewer Calculation Sheet

Table D1: SANITARY SEWER CALCULATION SHEET

LOCATION				RESIDENTIAL AREAS AND POPULATIONS												COMMERCIAL		INDUSTRIAL		INfiltration		SEWER DATA												
Street	U/S MH	D/S MH	Area #	Area (ha)		NUMBER OF UNITS						POPULATION		Peak Factor	AREA (ha)		Peak Flow (L/sec)	AREA (ha)		Peak Factor (per)	AREA (Ha)	ACCU AREA (Ha)	AREA (ha)		INFILT FLOW (L/s)	TOTAL FLOW (L/s)	Nom Dia (mm)	Actual Dia (mm)	Slope (%)	Length (m)	Capacity (L/sec)	Q/Q _{CAP} (%)	Full Velocity (m/s)	
				INDIV	ACCUM	Singles	Semis	Towns	1-Bed Apt.	2-Bed Apt.	3-Bed Apt.	4-Bed Apt.	INDIV	ACCU	INDIV	ACCU	INDIV	ACCU	INDIV	ACCU														
Victor	SANMH110	SANMH101	7	0.0648	0.0648			5					13.5	13.5	3.72	0.16							0.065	0.0648	0.02	0.18	200	201.20	0.65	41.50	26.9	1%	0.98	
Private	SANMH109	SANMH106	1	0.0537	0.0537					8				16.8	16.8	3.71	0.20							0.054	0.0537	0.02	0.22	200	201.20	4.28	25.50	68.9	0%	2.51
	SANMH108	SANMH107	3	0.0284	0.0284					4				8.4	8.4	3.74	0.10							0.028	0.0284	0.01	0.11	200	201.20	1.88	9.57	45.7	0%	1.66
	SANMH107	SANMH106	2	0.0208	0.0492					4				8.4	16.8	3.71	0.20							0.021	0.0492	0.02	0.22	200	201.20	2.10	8.08	48.3	0%	1.76
	SANMH106	SANMH105	4	0.4640	0.5669					40				84	117.6	3.58	1.36							0.464	0.5669	0.19	1.55	200	201.20	0.60	91.01	25.8	6%	0.94
	SANMH105	SANMH104	5	0.0779	0.6448					8				16.8	134.4	3.56	1.55							0.078	0.6448	0.21	1.76	200	201.20	0.35	7.95	19.7	9%	0.72
	SANMH104	SANMH103	6	0.1681	0.8129			5		10				34.5	168.9	3.54	1.94							0.168	0.8129	0.27	2.21	200	201.20	0.35	31.49	19.7	11%	0.72
	SANMH103	SANMH102	8	0.0669	0.8798					2				4.2	173.1	3.54	1.99							0.067	0.8798	0.29	2.28	200	201.20	0.35	12.72	19.7	12%	0.72
	SANMH102	SANMH101	9	0.0131	0.8929									173.1	3.54	1.99								0.013	0.8929	0.29	2.28	200	201.20	0.35	26.68	19.7	12%	0.72
Victor	SANMH101	SANMH100			0.9577								186.6	3.53	2.13								0.9577	0.32	2.45	250	251.46	0.35	3.26	35.7	7%	0.72		
	SANMH100	MHSA09002			0.9171	1.8748							186.6	3.53	2.13								0.917	1.8748	0.62	2.75	250	251.46	0.55	10.00	44.7	6%	0.90	
	MHSA09002	MHSA09003	6	0.8705	2.7453	13							44.2	230.8	3.50	2.62							0.871	2.7453	0.91	3.52	250	251.46	0.62	82.90	47.4	7%	0.95	
	MHSA09003	MHSA09004	8	0.8325	3.5778	15							51	281.8	3.47	3.17							0.833	3.5778	1.18	4.35	250	251.46	0.40	90.10	38.2	11%	0.77	
	MHSA09004	MHSA09005	10	0.8352	4.4130	16							54.4	336.2	3.45	3.76							0.835	4.4130	1.46	5.22	250	251.46	0.47	86.60	41.6	13%	0.83	
	MHSA09005	MHSA09006	13	0.9605	5.3735	17							57.8	394	3.42	4.37							0.961	5.3735	1.77	6.14	250	251.46	0.42	91.20	39.0	16%	0.78	
	MHSA09006	MHSA09007	15	0.1879	5.5614	2							6.8	400.8	3.42	4.44							0.188	5.5614	1.84	6.28	250	251.46	0.15	13.10	23.6	27%	0.47	
	MHSA09007	MHSA09008	16	0.3846	5.9460	6							20.4	421.2	3.41	4.65							0.385	5.9460	1.96	6.62	250	251.46	0.42	81.20	39.1	17%	0.79	
Denham	MHSA09020	MHSA09021	3	0.3851	0.3851	3							10.2	10.2	3.73	0.12							0.385	0.3851	0.13	0.25	250	251.46	0.41	39.20	38.6	1%	0.78	
	MHSA09021	MHSA09022	4	0.1229	0.5080	1							3.4	13.6	3.72	0.16							0.123	0.5080	0.17	0.33	250	251.46	1.07	12.10	62.6	1%	1.26	
	MHSA09022	MHSA09023	5	0.7027	1.2107	5							17	30.6	3.68	0.36							0.703	1.2107	0.40	0.76	250	251.46	1.03	53.20	61.4	1%	1.23	
	MHSA09023	MHSA09024	7	0.8059	2.0166	4	4						24.4	55	3.64	0.65							0.806	2.0166	0.67	1.31	250	251.46	0.40	90.50	38.1	3%	0.77	
	MHSA09024	MHSA09025	9	0.7950	2.8116	11							37.4	92.4	3.60	1.08							0.795	2.8116	0.93	2.01	250	251.46	0.41	88.40	38.5	5%	0.77	
	MHSA09025	MHSA09026	11	0.6130	3.4246	9							30.6	123	3.57	1.42							0.613	3.4246	1.13	2.55	250	251.46	0.41	59.00	38.5	7%	0.77	
	MHSA09026	MHSA09027	12	0.6608</																														

Appendix E – Stormwater Design Tables

Table E1: Estimation of Catchment Time of Concentration (Pre-Development)

Table E2: Estimation of Peak Flows (Pre-Development) Using Calculated Time of Concentrations

Table E3: Estimation of Allowable Peak Flows (Based on 5-yr Pre-Development Rates and Max C-0.50 and Tc=10mins)

Table E4: Average Runoff Coefficient (Post-Development)

Table E5: Summary of Post Development Peak Flows (Uncontrolled and Controlled)

Table E6: Summary of Post Development Storage

Table E7: Storage Volumes for 2-yr, 5-yr, 100-yr Storms Based on Modified Rational Method (Site 1)

Table E8: Storage Volumes for 2-yr, 5-yr, 100-yr Storms Based on Modified Rational Method (Site 2)

Table E9: MC-3500 Site Calculator for Chambers 1 (Site 1)

Table E10: MC-3500 Site Calculator for Chambers 2 (Site 2)

Table E11: MC-3500 Cumulative Storage Vs Depth Table (Site 1)

Table E12: MC-3500 Cumulative Storage Vs Depth Table (Site 2)

Table E13: 2-year Storm Sewer Calculation Sheet

Table E14: Major System (street segment) Characteristics

Table E15: Surface Ponding Area-Depth (total 3 pages)

TABLE E1: ESTIMATION OF CATCHMENT TIME OF CONCENTRATION (PRE-DEVELOPMENT CONDITIONS)

Catchment No.	Area (ha)	Outlet Location	High Elev (m)	Low Elev (m)	Flow Path Length (m)	Indiv Slope	Avg. C	Time of Conc. Tc	Description
PRE_S02	0.2835	Victor	114.6	114.3	20.0	1.5	0.42	1.19	See Note 1
PRE_S03	0.4993	Victor	114.0	113.0	75.0	1.3	0.20	5.06	See Note 1
PRE_S01	0.1814	Hazeldean	116.0	115.5	41.0	1.2	0.73	2.66	See Note 2
Totals	0.9642								

Notes

1) For Catchments with Runoff Coefficient less than C=0.40, Time of Concentration Based on Federal Aviation Formula (Airport Method), from MTO Drainage Manual Equation 8.16, where: $T_c = 3.26 * (1.1 - C) * L^{0.5} / S_w^{0.33}$

2) For Catchments with Runoff Coefficient greater than C=0.40, Time of Concentration Based on Bransby Williams Equation, from MTO Drainage Manual Equation 8.15, where: $T_c = 0.057 * L / (S_w^{0.2} * A^{0.1})$

TABLE E2: ESTIMATION OF PEAK FLOWS (PRE-DEVELOPMENT CONDITIONS) USING CALCULATED TIME OF CONCENTRATIONS

Catchment No.	Area (ha)	Outlet Location	Time of Conc, Tc (min)	Storm = 2 yr			Storm = 5 yr			Storm = 100 yr		
				I ₂ (mm/hr)	Cavg	Q _{5PRE} (L/sec)	I ₅ (mm/hr)	Cavg	Q _{5PRE} (L/sec)	I ₁₀₀ (mm/hr)	Cavg	Q _{100PRE} (L/sec)
PRE_S02	0.2835	Victor	1.19	145.01	0.42	48.0	199.10	0.42	65.9	343.67	0.53	142.2
PRE_S03	0.4993	Victor	5.06	103.16	0.20	28.6	140.60	0.20	39.0	241.71	0.25	83.9
PRE_S01	0.1814	Hazeldean	2.66	125.18	0.73	46.1	171.28	0.73	63.1	295.09	0.91	135.8
Totals	0.9642				122.7			168.0			361.9	

Notes

1) Intensity, I = $732.951 / (T_c + 6.199)^{0.810}$ (2-year, City of Ottawa)

2) Intensity, I = $998.071 / (T_c + 6.035)^{0.814}$ (5-year, City of Ottawa)

3) Intensity, I = $1735.688 / (T_c + 6.014)^{0.820}$ (100-year, City of Ottawa)

4) Cavg for 100-year is increased by 25% to a maximum of 1.0

TABLE E3: ESTIMATION OF ALLOWABLE PEAK FLOWS (Based on 5 year Pre-Development Rates and Max C=0.50 & Tc=10mins)

Catchment No.	Area (ha)	Outlet Location	Time of Conc, Tc (min)	Storm = 2 yr			Storm = 5 yr		
				I ₂ (mm/hr)	Cavg	Q _{ALLOW} (L/sec)	I ₅ (mm/hr)	Cavg	Q _{ALLOW} (L/sec)
PRE_S02	0.2835	Victor	10	76.81	0.42	25.4	104.29	0.42	34.5
PRE_S03	0.4993	Victor	10	76.81	0.20	21.3	104.29	0.20	29.0
Total to Victor St				0.28		46.7			
PRE_S01	0.1814	Hazeldean	10	76.81	0.50	19.4	104.29	0.50	26.3
Total to Hazeldean Rd				19.4					26.3
Total to Both =				66.1					89.8

<-- Allowable Minor System Discharge Rate of 50 L/sec Used as per City

<-- Max C = 0.50 Used to establish allowable peak flow

Notes

- 1) Allowable Capture Rates are based on meeting pre-development peak flows for all storms up to 100-year event. Allowable runoff coefficient to meet pre-development Cavg or $C = 0.50$ (maximum)
 2) Time of Concentration (T_c) is based on the standard 10 minutes as per City Guidelines. The higher time of 10 minutes was used as it results in lower (more stringent) peak runoff rate used to establish allowable discharge rates.

TABLE E4: AVERAGE RUNOFF COEFFICIENTS (Post-Development)

Runoff Coefficients		$C_{ASPH/CONC} =$	<u>0.90</u>	$C_{ROOF} =$	<u>0.90</u>	$C_{GRASS} =$	<u>0.20</u>			
Area No.	Asphalt & Conc Areas (m^2)	$A * C_{ASPH}$	Roof Areas (m^2)	$A * C_{ROOF}$	Grassed Areas (m^2)	$A * C_{GRASS}$	Sum AC	Total Area (m^2)	C_{AVG} (see note)	Comment
S01							1331.5	1752	0.76	Surface Areas
S02							1216.1	1483	0.82	Surface Areas
S03							53.4	178	0.3	Surface Areas
S04							1500.8	2001	0.75	Surface Areas
S05							910.1	1264	0.72	Surface Areas
S06							277.7	617	0.45	Surface Areas
S07							195.1	415	0.47	Surface Areas
S08_1							251.1	405	0.62	Surface Areas
S08_2							317.8	548	0.58	Surface Areas
S09							564.2	806	0.7	Surface Areas
Totals							6617.7	9,469	0.70	

TABLE E5: SUMMARY OF POST-DEVELOPMENT PEAK FLOWS (Uncontrolled and Controlled)

TABLE E6: SUMMARY OF POST DEVELOPMENT STORAGE

Area No.	Area (ha)	Release Rate (L/s)			Storage Required (m ³)				Storage Provided (m ³)				Control Method	
		2-yr	5-yr	100-yr	2-yr (MRM)	5-yr (MRM)	100-yr (MRM)	100-yr (PCSWMM)	Roof	Surface Ponding	UG Chambers	UG CB/MHs	Total	
S01	0.1752	13.2	15.6	21.2	29.4	42.7	112.4	118.2		152.5		152.5	ICD - TEMPEST MHF TYPE A (Downstream of Chambers 1)	
S02	0.1483													
S03	0.0178													
S04	0.2001													
S05	0.1264													
S06	0.0617													
S07	0.0415													
S08_1	0.0405													
S08_2	0.0548													
S09	0.0806													
Totals (all)=	0.947	27.6	32.9	45.2	72.8	104.7	271.3	273.4	0.0	0.0	307.7	0.0	307.7	

Notes

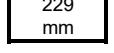
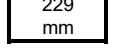
1) Storage Required Based on the Modified Rational Method (MRM) for the release rates noted.

Table E7 - Storage Volumes for 2-year, 5-Year and 100-Year Storms

Area No: Chamber 1 (east)															
$C_{AVG} = 0.76$ (2-yr)															
$C_{AVG} = 0.76$ (5-yr)															
$C_{AVG} = 0.95$ (100-yr, Max 1.0)															
Time Interval = 2.00 (mins)															
Drainage Area = 0.3413 (hectares)															
Duration (min)	Release Rate = <u>13.2</u> (L/sec) Return Period = <u>2</u> (years) IDF Parameters, A = <u>732.951</u> , B = <u>0.810</u> ($I = A/(T_c+C)$, C = <u>6.199</u>)					Release Rate = <u>15.6</u> (L/sec) Return Period = <u>5</u> (years) IDF Parameters, A = <u>998.071</u> , B = <u>0.814</u> ($I = A/(T_c+C)$, C = <u>6.053</u>)					Release Rate = <u>21.2</u> (L/sec) Return Period = <u>100</u> (years) IDF Parameters, A = <u>1735.688</u> , B = <u>0.820</u> ($I = A/(T_c+C)$, C = <u>6.014</u>)				
	Rainfall Intensity, I (mm/hr)	Peak Flow (L/sec)	Release Rate (L/sec)	Storage Rate (L/sec)	Storage (m³)	Rainfall Intensity, I (mm/hr)	Peak Flow (L/sec)	Release Rate (L/sec)	Storage Rate (L/sec)	Storage (m³)	Rainfall Intensity, I (mm/hr)	Peak Flow (L/sec)	Release Rate (L/sec)	Storage Rate (L/sec)	Storage (m³)
0	167.2	120.9	13.18	107.7	0.00	230.5	166.7	15.600	151.1	0.00	398.6	360.3	21.160	339.1	0.00
2	133.3	96.4	13.18	83.2	9.99	182.7	132.1	15.600	116.5	13.98	315.0	284.7	21.160	263.6	31.63
4	111.7	80.8	13.18	67.6	16.22	152.5	110.3	15.600	94.7	22.72	262.4	237.2	21.160	216.0	51.84
6	96.6	69.9	13.18	56.7	20.41	131.6	95.1	15.600	79.5	28.63	226.0	204.3	21.160	183.1	65.92
8	85.5	61.8	13.18	48.6	23.33	116.1	84.0	15.600	68.4	32.81	199.2	180.0	21.160	158.9	76.27
10	76.8	55.5	13.18	42.4	25.41	104.2	75.3	15.600	59.7	35.84	178.6	161.4	21.160	140.2	84.14
12	69.9	50.5	13.18	37.4	26.90	94.7	68.5	15.600	52.9	38.07	162.1	146.5	21.160	125.4	90.28
14	64.2	46.4	13.18	33.3	27.94	86.9	62.9	15.600	47.3	39.70	148.7	134.4	21.160	113.3	95.14
16	59.5	43.0	13.18	29.8	28.65	80.5	58.2	15.600	42.6	40.88	137.5	124.3	21.160	103.2	99.04
18	55.5	40.1	13.18	26.9	29.10	75.0	54.2	15.600	38.6	41.70	128.1	115.8	21.160	94.6	102.17
20	52.0	37.6	13.18	24.4	29.33	70.3	50.8	15.600	35.2	42.24	120.0	108.4	21.160	87.3	104.71
22	49.0	35.4	13.18	22.3	29.39	66.1	47.8	15.600	32.2	42.54	112.9	102.0	21.160	80.9	106.74
24	46.4	33.5	13.18	20.4	29.31	62.5	45.2	15.600	29.6	42.65	106.7	96.4	21.160	75.3	108.37
26	44.0	31.8	13.18	18.7	29.10	59.3	42.9	15.600	27.3	42.60	101.2	91.5	21.160	70.3	109.65
28	41.9	30.3	13.18	17.1	28.79	56.5	40.8	15.600	25.2	42.42	96.3	87.0	21.160	65.9	110.64
30	40.0	29.0	13.18	15.8	28.39	53.9	39.0	15.600	23.4	42.11	91.9	83.0	21.160	61.9	111.37
32	38.3	27.7	13.18	14.5	27.92	51.6	37.3	15.600	21.7	41.70	87.9	79.4	21.160	58.3	111.89
34	36.8	26.6	13.18	13.4	27.37	49.5	35.8	15.600	20.2	41.19	84.3	76.2	21.160	55.0	112.21
36	35.4	25.6	13.18	12.4	26.77	47.6	34.4	15.600	18.8	40.61	81.0	73.2	21.160	52.0	112.36
38	34.1	24.6	13.18	11.5	26.11	45.8	33.1	15.600	17.5	39.96	77.9	70.4	21.160	49.3	112.36
40	32.9	23.8	13.18	10.6	25.40	44.2	31.9	15.600	16.3	39.24	75.1	67.9	21.160	46.8	112.22
Max = 29.39														42.65	112.36

Table E7 - Storage Volumes for 2-year, 5-Year and 100-Year Storms

Area No: Chamber 2 (west)															
$C_{AVG} = 0.66$ (2-yr)															
$C_{AVG} = 0.66$ (5-yr)															
$C_{AVG} = 0.82$ (100-yr, Max 1.0)															
Time Interval = 3.00 (mins)															
Drainage Area = 0.5250 (hectares)															
Duration (min)	Release Rate = <u>14.4</u> (L/sec)				Release Rate = <u>17.3</u> (L/sec)				Release Rate = <u>24.0</u> (L/sec)						
	Return Period = <u>2</u> (years)				Return Period = <u>5</u> (years)				Return Period = <u>100</u> (years)						
	IDF Parameters, A = <u>732.951</u> , B = <u>0.810</u> ($I = A/(T_c+C)$, C = <u>6.199</u>)				IDF Parameters, A = <u>998.071</u> , B = <u>0.814</u> ($I = A/(T_c+C)$, C = <u>6.053</u>)				IDF Parameters, A = <u>1735.688</u> , B = <u>0.820</u> ($I = A/(T_c+C)$, C = <u>6.014</u>)						
Rainfall Intensity, I (mm/hr)	Peak Flow (L/sec)	Release Rate (L/sec)	Storage Rate (L/sec)	Storage (m³)	Rainfall Intensity, I (mm/hr)	Peak Flow (L/sec)	Release Rate (L/sec)	Storage Rate (L/sec)	Storage (m³)	Rainfall Intensity, I (mm/hr)	Peak Flow (L/sec)	Release Rate (L/sec)	Storage Rate (L/sec)	Storage (m³)	
0	167.2	160.5	14.40	146.1	0.00	230.5	221.2	17.270	203.9	0.00	398.6	478.2	24.010	454.2	0.00
3	121.5	116.6	14.40	102.2	18.39	166.1	159.4	17.270	142.1	25.58	286.0	343.2	24.010	319.2	57.45
6	96.6	92.8	14.40	78.4	28.21	131.6	126.3	17.270	109.0	39.24	226.0	271.2	24.010	247.1	88.97
9	80.9	77.6	14.40	63.2	34.14	109.8	105.4	17.270	88.1	47.58	188.3	225.9	24.010	201.8	109.00
12	69.9	67.1	14.40	52.7	37.93	94.7	90.9	17.270	73.6	53.00	162.1	194.5	24.010	170.5	122.76
15	61.8	59.3	14.40	44.9	40.40	83.6	80.2	17.270	62.9	56.63	142.9	171.4	24.010	147.4	132.68
18	55.5	53.3	14.40	38.9	41.97	75.0	72.0	17.270	54.7	59.06	128.1	153.7	24.010	129.7	140.03
21	50.5	48.4	14.40	34.0	42.90	68.1	65.4	17.270	48.1	60.63	116.3	139.5	24.010	115.5	145.55
24	46.4	44.5	14.40	30.1	43.36	62.5	60.0	17.270	42.8	61.57	106.7	128.0	24.010	104.0	149.72
27	43.0	41.2	14.40	26.8	43.45	57.9	55.6	17.270	38.3	62.02	98.7	118.4	24.010	94.4	152.86
30	40.0	38.4	14.40	24.0	43.26	53.9	51.8	17.270	34.5	62.08	91.9	110.2	24.010	86.2	155.17
33	37.5	36.0	14.40	21.6	42.83	50.5	48.5	17.270	31.2	61.83	86.0	103.2	24.010	79.2	156.83
36	35.4	33.9	14.40	19.5	42.21	47.6	45.7	17.270	28.4	61.33	81.0	97.1	24.010	73.1	157.95
39	33.5	32.1	14.40	17.7	41.43	45.0	43.2	17.270	25.9	60.61	76.5	91.8	24.010	67.8	158.61
42	31.8	30.5	14.40	16.1	40.52	42.7	41.0	17.270	23.7	59.71	72.6	87.1	24.010	63.1	158.89
45	30.2	29.0	14.40	14.6	39.48	40.6	39.0	17.270	21.7	58.66	69.1	82.8	24.010	58.8	158.85
48	28.9	27.7	14.40	13.3	38.35	38.8	37.2	17.270	20.0	57.47	65.9	79.0	24.010	55.0	158.51
51	27.6	26.5	14.40	12.1	37.12	37.1	35.6	17.270	18.4	56.16	63.0	75.6	24.010	51.6	157.93
54	26.5	25.5	14.40	11.1	35.82	35.6	34.2	17.270	16.9	54.75	60.4	72.5	24.010	48.5	157.14
57	25.5	24.5	14.40	10.1	34.45	34.2	32.8	17.270	15.6	53.24	58.1	69.7	24.010	45.7	156.14
60	24.6	23.6	14.40	9.2	33.01	32.9	31.6	17.270	14.3	51.66	55.9	67.1	24.010	43.0	154.98
Max =				43.45					62.08					158.89	

			Project Information: Project Name: 5294 Hazeldean Chambers Location: 5294 Hazeldean Chambers Date: 10/5/2019 Engineer: J Fitzpatrick StormTech RPM: V Sharma		
MC-3500 Site Calculator			Chambers-1		
System Requirements			System Sizing		
Units Required Storage Volume Stone Porosity (Industry Standard = 40%) Stone Above Chambers (305 mm min.) Stone Foundation Depth (229 mm min.) Average Cover over Chambers (610 mm min.) Bed size controlled by WIDTH or LENGTH? Limiting WIDTH or LENGTH dimension			Metric 150 cubic meters 40 % 305 mm 229 mm 610 mm WIDTH 12 meters		
Storage Volume per Chamber Storage Volume per End Cap			Number of Chambers Required Number of End Caps Required Bed Size (including perimeter stone) Stone Required (including perimeter stone) Volume of Excavation Non-woven Filter Fabric Required (20% Safety Factor) Length of Isolator Row Non-woven Isolator Row Fabric (20% Safety Factor) Woven Isolator Row Fabric (20% Safety Factor) Installed Storage Volume		
Controlled by Width (Rows)					
Maximum Width = 12 meters 3 rows of 6 chambers 2 row of 5 chambers					
Maximum Length = 14.5 meters Maximum Width = 11.0 meters					

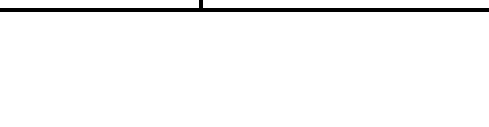
			Project Information: Project Name: 5294 Hazeldean Chambers Location: 5294 Hazeldean Chambers Date: 10/5/2019 Engineer: J Fitzpatrick StormTech RPM: V Sharma		
MC-3500 Site Calculator			Chambers-2		
System Requirements			System Sizing		
Units Required Storage Volume Stone Porosity (Industry Standard = 40%) Stone Above Chambers (305 mm min.) Stone Foundation Depth (229 mm min.) Average Cover over Chambers (610 mm min.) Bed size controlled by WIDTH or LENGTH? Limiting WIDTH or LENGTH dimension			Metric 155.2 cubic meters 40 % 305 mm 229 mm 610 mm LENGTH 13 meters		
Storage Volume per Chamber Storage Volume per End Cap			Number of Chambers Required Number of End Caps Required Bed Size (including perimeter stone) Stone Required (including perimeter stone) Volume of Excavation Non-woven Filter Fabric Required (20% Safety Factor) Length of Isolator Row Non-woven Isolator Row Fabric (20% Safety Factor) Woven Isolator Row Fabric (20% Safety Factor) Installed Storage Volume		
Controlled by Length			29 each 12 each 157 square meters 277 metric tonnes 311 cubic meters 478 square meters 12.3 meters 59 square meters 74 square meters 159 cubic meters		
Maximum Length = 5 rows of 5 chambers 1 row of 4 chambers			 610 mm		
Maximum Length = Maximum Width =			 305 mm		
			 229 mm		

TABLE E11 - MC-3500 CUMULATIVE STORAGE BY DEPTH TABLE (SITE 1 - EAST)

Length per Chamber, From Manufacturer (m)	2.184	No Chamber Req'd	28
End Cap Length, From Manufacturer (m)	0.673	No End Caps Req'd	8
L = Total Length of Chambers (m)			
Bottom Width of Chambers, From Manufacturer (m)	1.803		
Dsit form Chamber to Edge of Trench (m)	0.305		
Bottom Width of Trench Width + 2 x dist to edge, W (m)	2.403		
Total Trench Length (actual) Including End Caps =	75.60		
Maximum Trench Volume (m^3)	152.5		

Water Depth (in)	Water Depth (m)	Total Storage Volume Per Chamber (m^3)	Volume Per End Cap (m^3)	Total Storage Volume in Trench (m^3)
0	0.000	0.000	0.000	0.000
1	0.025	0.048	0.016	1.472
2	0.051	0.097	0.032	2.972
3	0.076	0.145	0.048	4.444
4	0.102	0.194	0.064	5.944
5	0.127	0.242	0.081	7.424
6	0.152	0.291	0.097	8.924
7	0.178	0.339	0.113	10.396
8	0.203	0.388	0.129	11.896
9	0.229	0.436	0.145	13.368
10	0.254	0.484	0.172	16.608
11	0.279	0.532	0.199	19.848
12	0.305	0.579	0.225	23.052
13	0.330	0.866	0.252	26.264
14	0.356	0.973	0.278	29.468
15	0.381	1.079	0.305	32.652
16	0.406	1.184	0.331	35.800
17	0.432	1.290	0.357	38.976
18	0.457	1.395	0.383	42.124
19	0.483	1.499	0.409	45.244
20	0.508	1.603	0.434	48.356
21	0.533	1.706	0.460	51.448
22	0.559	1.809	0.485	54.532
23	0.584	1.911	0.510	57.588
24	0.610	2.013	0.539	60.576
25	0.635	2.114	0.559	63.664
26	0.660	2.214	0.583	66.656
27	0.686	2.314	0.607	69.648
28	0.711	2.416	0.631	72.696
29	0.737	2.511	0.655	75.548
30	0.762	2.608	0.678	78.448
31	0.787	2.705	0.701	81.348
32	0.813	2.800	0.723	84.184
33	0.838	2.895	0.745	87.020
34	0.864	2.989	0.767	89.828
35	0.889	3.081	0.788	92.572
36	0.914	3.173	0.809	95.316
37	0.940	3.263	0.830	98.004
38	0.965	3.352	0.850	100.656
39	0.991	3.440	0.871	103.288
40	1.016	3.526	0.890	105.848
41	1.041	3.611	0.910	108.388
42	1.067	3.694	0.929	110.864
43	1.092	3.775	0.948	113.284
44	1.118	3.855	0.966	115.668
45	1.143	3.932	0.985	117.976
46	1.168	4.007	1.003	120.220
47	1.194	4.080	1.020	122.400
48	1.219	4.150	1.037	124.496
49	1.245	4.216	1.054	126.480
50	1.270	4.276	1.071	128.296
51	1.295	4.331	1.088	129.972
52	1.321	4.385	1.104	131.612
53	1.346	4.436	1.120	133.168
54	1.372	4.486	1.136	134.696
55	1.397	4.534	1.152	136.168
56	1.422	4.583	1.169	137.676
57	1.448	4.631	1.185	139.148
58	1.473	4.680	1.201	140.648
59	1.499	4.728	1.217	142.120
60	1.524	4.777	1.233	143.620
61	1.549	4.825	1.249	145.092
62	1.575	4.874	1.265	146.592
63	1.600	4.922	1.281	148.064
64	1.626	4.971	1.298	149.572
65	1.651	5.019	1.314	151.044
66	1.676	5.068	1.330	152.544

Sorted in Ascending Order		Sorted in Ascending Order			
Water Depth (in)	Water Depth (m)	Total Storage Volume in Trench (m3)	Water Depth (in)	Water Depth (m)	Total Storage Volume in Trench (m3)
0	0.000	0.000	66	1.676	152.54
1	0.025	1.472	65	1.651	151.04
2	0.051	2.972	64	1.626	149.59
3	0.076	4.444	63	1.600	148.06
4	0.102	5.944	62	1.575	146.59
5	0.127	7.424	61	1.549	145.09
6	0.152	8.924	60	1.524	143.62
7	0.178	10.396	59	1.499	142.12
8	0.203	11.896	58	1.473	140.65
9	0.229	13.368	57	1.448	139.15
10	0.254	16.608	56	1.422	137.68
11	0.279	19.848	55	1.397	136.17
12	0.305	23.052	54	1.372	134.70
13	0.330	26.264	53	1.346	133.17
14	0.356	29.468	52	1.321	131.61
15	0.381	32.652	51	1.295	129.97
16	0.406	35.800	50	1.270	128.30
17	0.432	38.976	49	1.245	126.48
18	0.457	42.124	48	1.219	124.50
19	0.483	45.244	47	1.194	122.40
20	0.508	48.356	46	1.168	120.22
21	0.533	51.448	45	1.143	117.98
22	0.559	54.532	44	1.118	115.67
23	0.584	57.588	43	1.092	113.28
24	0.610	60.670	42	1.067	110.86
25	0.635	63.664	41	1.041	108.39
26	0.660	66.656	40	1.016	105.85
27	0.686	69.648	39	0.991	103.29
28	0.711	72.696	38	0.965	100.66
29	0.737	75.548	37	0.940	98.00
30	0.762	78.448	36	0.914	95.32
31	0.787	81.348	35	0.889	92.57
32	0.813	84.184	34	0.864	89.83
33	0.838	87.020	33	0.838	87.02
34	0.864	89.828	32	0.813	84.18
35	0.889	92.572	31	0.787	81.35
36	0.914	95.310	30	0.762	78.45
37	0.940	98.004	29	0.737	75.55
38	0.965	100.656	28	0.711	72.70
39	0.991	103.288	27	0.686	69.65
40	1.016	105.848	26	0.660	66.66
41	1.041	108.388	25	0.635	63.66
42	1.067	110.864	24	0.610	60.68
43	1.092	113.284	23	0.584	57.59
44	1.118	115.668	22	0.559	54.53
45	1.143	117.976	21	0.533	51.45
46	1.168	120.220	20	0.508	48.36
47	1.194	122.400	19	0.483	45.24
48	1.219	124.490	18	0.457	42.12
49	1.245	126.480	17	0.432	38.98
50	1.270	128.296	16	0.406	35.80
51	1.295	129.972	15	0.381	32.65
52	1.321	131.612	14	0.356	29.47
53	1.346	133.168	13	0.330	26.26
54	1.372	134.696	12	0.305	23.05
55	1.397	136.168	11	0.279	19.85
56	1.422	137.676	10	0.254	16.61
57	1.448	139.148	9	0.229	13.37
58	1.473	140.648	8	0.203	11.90
59	1.499	142.120	7	0.178	10.40
60	1.524	143.620	6	0.152	8.92
61	1.549	145.092	5	0.127	7.42
62	1.575	146.592	4	0.102	5.94
63	1.600	148.064	3	0.076	4.44
64	1.626	149.572	2	0.051	2.97
65	1.651	151.044	1	0.025	1.47
66	1.676	152.544	0	0.000	0.00

TABLE E12 - MC-3500 CUMULATIVE STORAGE BY DEPTH TABLE (SITE 2 - WEST)

Length per Chamber, From Manufacturer (m)	2.184	No Chamber Req'd	28
End Cap Length, From Manufacturer (m)	0.673	No End Caps Req'd	10
L = Total Length of Chambers (m)			
Bottom Width of Chambers, From Manufacturer (m)	1.803		
Dsit form Chamber to Edge of Trench (m)	0.305		
Bottom Width of Trench Width + 2 x dist to edge, W (m)	2.403		
Total Trench Length (actual) Including End Caps =	75.60		
Maximum Trench Volume (m^3)	155.2		

Water Depth (in)	Water Depth (m)	Total Storage Volume Per Chamber (m^3)	Volume Per End Cap (m^3)	Total Storage Volume in Trench (m^3)
0	0.000	0.000	0.000	0.000
1	0.025	0.048	0.016	1.504
2	0.051	0.097	0.032	3.036
3	0.076	0.145	0.048	4.340
4	0.102	0.194	0.064	6.072
5	0.127	0.242	0.081	7.586
6	0.152	0.291	0.097	9.118
7	0.178	0.339	0.113	10.622
8	0.203	0.388	0.129	12.154
9	0.229	0.436	0.145	13.658
10	0.254	0.544	0.172	16.952
11	0.279	0.652	0.199	20.246
12	0.305	0.759	0.225	23.502
13	0.330	0.866	0.252	26.768
14	0.356	0.973	0.278	30.024
15	0.381	1.079	0.305	33.262
16	0.406	1.184	0.331	36.462
17	0.432	1.290	0.357	39.690
18	0.457	1.395	0.383	42.890
19	0.483	1.499	0.409	46.062
20	0.508	1.603	0.434	49.224
21	0.533	1.706	0.460	52.368
22	0.559	1.809	0.485	55.502
23	0.584	1.911	0.510	58.608
24	0.610	2.013	0.539	61.754
25	0.635	2.114	0.559	64.782
26	0.660	2.214	0.583	67.822
27	0.686	2.314	0.607	70.862
28	0.711	2.416	0.631	73.958
29	0.737	2.511	0.655	76.858
30	0.762	2.608	0.678	79.804
31	0.787	2.705	0.701	82.750
32	0.813	2.800	0.723	85.630
33	0.838	2.895	0.745	88.510
34	0.864	2.989	0.767	91.362
35	0.889	3.081	0.788	94.148
36	0.914	3.173	0.809	96.934
37	0.940	3.263	0.830	99.664
38	0.965	3.352	0.850	102.356
39	0.991	3.440	0.871	105.030
40	1.016	3.526	0.890	107.628
41	1.041	3.611	0.910	110.208
42	1.067	3.694	0.929	112.722
43	1.092	3.775	0.948	115.180
44	1.118	3.855	0.966	117.600
45	1.143	3.932	0.985	119.946
46	1.168	4.007	1.003	122.226
47	1.194	4.080	1.020	124.440
48	1.219	4.150	1.037	126.570
49	1.245	4.216	1.054	128.588
50	1.270	4.276	1.071	130.438
51	1.295	4.331	1.088	132.148
52	1.321	4.385	1.104	133.820
53	1.346	4.436	1.120	135.408
54	1.372	4.486	1.136	136.968
55	1.397	4.534	1.152	138.472
56	1.422	4.583	1.169	140.014
57	1.448	4.631	1.185	141.518
58	1.473	4.680	1.201	143.050
59	1.499	4.728	1.217	144.554
60	1.524	4.777	1.233	146.086
61	1.549	4.825	1.249	147.590
62	1.575	4.874	1.265	149.122
63	1.600	4.922	1.281	150.626
64	1.626	4.971	1.298	152.168
65	1.651	5.019	1.314	153.672
66	1.676	5.068	1.330	155.204

Water Depth (in)	Water Depth (m)	Sorted in Ascending Order	
		Total Storage Volume in Trench (m3)	Total Storage Volume in Trench (m3)
0	0.000	0.000	155.20
1	0.025	1.504	153.67
2	0.051	3.036	152.17
3	0.076	4.340	150.63
4	0.102	6.072	149.12
5	0.127	7.586	147.59
6	0.152	9.118	146.09
7	0.178	10.622	144.55
8	0.203	12.154	143.05
9	0.229	13.658	141.52
10	0.254	15.952	140.01
11	0.279	20.246	138.47
12	0.305	23.502	136.97
13	0.330	26.768	135.41
14	0.356	30.024	133.82
15	0.381	33.262	132.15
16	0.406	36.462	130.44
17	0.432	39.690	128.59
18	0.457	42.890	126.57
19	0.483	46.062	124.44
20	0.508	49.224	122.23
21	0.533	52.368	119.95
22	0.559	55.502	117.60
23	0.584	58.608	115.18
24	0.610	61.754	112.72
25	0.635	64.782	110.21
26	0.660	67.822	107.63
27	0.686	70.862	105.03
28	0.711	73.958	102.36
29	0.737	76.858	99.66
30	0.762	79.804	96.93
31	0.787	82.750	94.15
32	0.813	85.630	91.36
33	0.838	88.510	88.51
34	0.864	91.362	85.63
35	0.889	94.148	82.75
36	0.914	96.934	79.80
37	0.940	99.664	76.86
38	0.965	102.356	73.96
39	0.991	105.030	70.86
40	1.016	107.626	67.82
41	1.041	110.206	64.78
42	1.067	112.722	61.75
43	1.092	115.180	58.61
44	1.118	117.600	55.50
45	1.143	119.946	52.37
46	1.168	122.220	49.22
47	1.194	124.440	46.06
48	1.219	126.570	42.89
49	1.245	128.588	39.69
50	1.270	130.436	36.46
51	1.295	132.146	33.26
52	1.321	133.820	30.02
53	1.346	135.408	26.77
54	1.372	136.968	23.50
55	1.397	138.472	20.25
56	1.422	140.014	16.95
57	1.448	141.516	13.66
58	1.473	143.050	12.15
59	1.499	144.554	10.62
60	1.524	146.086	9.12
61	1.549	147.590	7.59
62	1.575	149.122	6.07
63	1.600	150.626	4.54
64	1.626	152.168	3.04
65	1.651	153.672	1.50
66	1.676	155.204	0.00

TABLE E14: MAJOR SYSTEM (STREET SEGMENT) CHARACTERISTICS

ROAD AND CURB DATA (For Gutter Grades Up to 8% and Lane Crossfalls Up to 6%)		
Asphalt width, W_A (m) =	4.100	From EOP to CL
Total Road Width, W_R (m) =	4.250	Includes gutter
Lane crossfall, S_x (m/m) =	0.030	3.0%
Gutter Grade, S_G (m/m) =	0.010	1.0%
Curb Type =	R-20	Mountable Curb and Gutter (Former Goulbourn)
Inlet Type =	S19	Heavy Duty Fish Type (Round Cover)
Curb height, H_C (m) =	0.075	
Total curb height, H_T (m) =	0.350	
Curb top width, W_C (m) =	0.200	
Curb bottom width, W (m) =	0.350	
Gutter width, W_G (m) =	0.150	
Gutter slope, S_G (m/m) =	0.040	$S_G = D_G / W_G$
Gutter depth, D_G (m) =	0.006	
Mannings, N =	0.013	
Max Spread, T_{MAX} (m) =	2.200	Max Permitted Spread = 1/2 Asphalt width, $W_A + W_G$
Max Spread on Asphalt, T_{SMAX} (m) =	2.050	Max Permitted Spread Over Asphalt = 1/2 Asphalt width
Max Depth at EOP, D_{SMAX} (m) =	0.062	Based on 1/2 Lane Width
Max depth over gutter, D_{MAX} (m) =	0.068	$D_{MAX} = D_{SMAX} + D_G$

Overland Gutter and Roadway Flow Based on Road & Curb Type									
Street Flow, (L/sec)	Assumed Spread (T)	Spread on Asphalt, $T_s = T - W_g$	$D_s = T_s * S_x$	$D = D_s + D_g$	Road and Gutter Flows (m^3/sec)				
					$Q_{(A+C)}$	$Q_{(C)}$	$Q_{(A)}$	$Q_{(B)}$	$Q_{(A+B)}$
0	0.000	0.000	0.000	0.006	0.0001	0.0000	0.0001	0.0000	0.09
5	0.818	0.668	0.020	0.026	0.0043	0.0021	0.0022	0.0028	5.00
10	1.064	0.914	0.027	0.033	0.0084	0.0049	0.0034	0.0066	10.00
50	1.954	1.804	0.054	0.060	0.0399	0.0302	0.0098	0.0402	50.00
100	2.535	2.385	0.072	0.078	0.0788	0.0636	0.0152	0.0848	100.00
125	2.757	2.607	0.078	0.084	0.0981	0.0806	0.0176	0.1074	125.00
150	2.952	2.802	0.084	0.090	0.1174	0.0977	0.0197	0.1303	150.00
175	3.128	2.978	0.089	0.095	0.1367	0.1149	0.0218	0.1532	175.00
200	3.289	3.139	0.094	0.100	0.1559	0.1322	0.0237	0.1763	200.00

*Note: Re-iterate to get Street Flow Equal to $Q_{(A+B)}$ (use Goal Seek Function)

INLET CAPACITY, APPROACH FLOW & SPREAD BASED ON					
Lane Crossfall = 0.030 m/m					
Gutter Grade = 0.010 m/m					
Street Flow (L/sec)	Total Spread, T (m)	Spread on Asphalt, T_s (metres)	Depth of Flow at Gutter (m)	Inlet Capture Rate (m^3/sec)	Inlet Capture Rate (L/sec)
0	0.000	0.000	0.006	0.000	0
5	0.818	0.668	0.026	0.007	7
10	1.064	0.914	0.033	0.012	12
50	1.954	1.804	0.060	0.015	15
100	2.535	2.385	0.078	0.034	34
125	2.757	2.607	0.084	0.047	47
150	2.952	2.802	0.090	0.051	51
175	3.128	2.978	0.095	0.054	54
200	3.289	3.139	0.100	0.055	55

Note: The Total Spread (T), includes Gutter width, (W_g) plus spread on lane, (T_s) for curb & gutter type curbs

Ponding Information	
Ponding Area (trap low) No:	SP01
Structure / Inlet No:	CB1
Structre / Inlet Type	Catcbasin
Include Structure Storage (yes/no)	Yes
Structure Shape (rect / round)	Rect
Structure Length or DIA (mm)	600
Structure Width (mm)	600
Max. Ponding Area (m2) =	269
Max. Ponding Elev at Spill (m):	114.00
Min. Ponding Elev (Lid Elev) (m):	113.80
Max. Prism Volume (m3)	17.93
Depth to Inv below ground (m)	1.400
Allowance for Overland Flow (m)	0.150
Ponding Rim Elevation (m)	114.15
Inv Elev of Storage Node (m)	112.40
Max Ponding Depth (m) =	0.200

Storage Function for Modelling			
Head / Depth (m)	Area (m2)	Incr Vol (m3)	Tot Vol (m3)
0.0000	0.0000	0.00	0.00
1.4000	0.3600	13.49	13.49
1.6000	269	17.93	31.42
1.6001	0	0.00	31.42
1.7500	0	0.00	31.42

Copy to PCSWMM (depth / area)

No. of Inlets = 1 catchbasin

Ponding Information	
Ponding Area (trap low) No:	SP02
Structure / Inlet No:	CB06
Structre / Inlet Type	Catcbasin
Include Structure Storage (yes/no)	Yes
Structure Shape (rect / round)	Rect
Structure Length or DIA (mm)	600
Structure Width (mm)	600
Max. Ponding Area (m2) =	101
Max. Ponding Elev at Spill (m):	114.00
Min. Ponding Elev (Lid Elev) (m):	113.90
Max. Prism Volume (m3)	3.37
Depth to Inv below ground (m)	1.400
Allowance for Overland Flow (m)	0.150
Ponding Rim Elevation (m)	114.15
Inv Elev of Storage Node (m)	112.50
Max Ponding Depth (m) =	0.100

Storage Function for Modelling			
Head / Depth (m)	Area (m2)	Incr Vol (m3)	Tot Vol (m3)
0.0000	0.0000	0.00	0.00
1.4000	0.3600	13.50	13.50
1.5000	101	3.37	16.87
1.5001	0	0.00	16.87
1.6500	0	0.00	16.87

Copy to PCSWMM (depth / area)

No. of Inlets = 1 catchbasin

Ponding Information	
Ponding Area (trap low) No:	SP03
Structure / Inlet No:	CBMH218
Structre / Inlet Type	Manhole
Include Structure Storage (yes/no)	Yes
Structure Shape (rect / round)	Round
Structure Length or DIA (mm)	1200
Structure Width (mm)	
Max. Ponding Area (m2) =	173
Max. Ponding Elev at Spill (m):	114.20
Min. Ponding Elev (Lid Elev) (m):	114.00
Max. Prism Volume (m3)	11.53
Depth to Inv below ground (m)	1.400
Allowance for Overland Flow (m)	0.150
Ponding Rim Elevation (m)	114.35
Inv Elev of Storage Node (m)	112.60
Max Ponding Depth (m) =	0.200

Storage Function for Modelling			
Head / Depth (m)	Area (m2)	Incr Vol (m3)	Tot Vol (m3)
0.0000	0.0000	0.00	0.00
1.4000	1.1310	1.58	1.58
1.6000	173	11.53	13.12
1.6001	0	0.00	13.12
1.7500	0	0.00	13.12

Copy to PCSWMM (depth / area)

No. of Inlets = 1 catchbasin

Ponding Information	
Ponding Area (trap low) No:	SP04
Structure / Inlet No:	CB03
Structre / Inlet Type	Catcbasin
Include Structure Storage (yes/no)	Yes
Structure Shape (rect / round)	Rect
Structure Length or DIA (mm)	600
Structure Width (mm)	600
Max. Ponding Area (m2) =	63
Max. Ponding Elev at Spill (m):	114.35
Min. Ponding Elev (Lid Elev) (m):	114.25
Max. Prism Volume (m3)	2.10
Depth to Inv below ground (m)	0.150
Allowance for Overland Flow (m)	0.150
Ponding Rim Elevation (m)	114.50
Inv Elev of Storage Node (m)	114.10
Max Ponding Depth (m) =	0.100

Storage Function for Modelling			
Head / Depth (m)	Area (m2)	Incr Vol (m3)	Tot Vol (m3)
0.0000	0.0000	0.00	0.00
0.1500	0.3600	0.05	0.05
0.2500	63	2.10	2.15
0.2501	0	0.00	2.15
0.4000	0	0.00	2.15

Copy to PCSWMM (depth / area)

No. of Inlets = 1 catchbasin

Ponding Information	
Ponding Area (trap low) No:	SP05
Structure / Inlet No:	IN103407
Structre / Inlet Type	Catcbasin
Include Structure Storage (yes/no)	Yes
Structure Shape (rect / round)	Round
Structure Length or DIA (mm)	1200
Structure Width (mm)	600
Max. Ponding Area (m2) =	313
Max. Ponding Elev at Spill (m):	113.10
Min. Ponding Elev (Lid Elev) (m):	113.04
Max. Prism Volume (m3)	6.26
Depth to Inv below ground (m)	1.400
Allowance for Overland Flow (m)	0.150
Ponding Rim Elevation (m)	113.25
Inv Elev of Storage Node (m)	111.64
Max Ponding Depth (m) =	0.060

Storage Function for Modelling			
Head / Depth (m)	Area (m2)	Incr Vol (m3)	Tot Vol (m3)
0.0000	0.0000	0.00	0.00
1.4000	1.1310	1.583362697	1.58
1.4600	313	6.26	7.84
1.4601	0	0.00	7.84
1.6100	0	0.00	7.84

Copy to PCSWMM (depth / area)

No. of Inlets = 1 catchbasin

Ponding Information	
Ponding Area (trap low) No:	SP06A, SP06B
Structure / Inlet No:	IN09007, IN09008
Structre / Inlet Type	Catcbasin
Include Structure Storage (yes/no)	Yes
Structure Shape (rect / round)	Rect
Structure Length or DIA (mm)	600
Structure Width (mm)	600
Max. Ponding Area (m2) =	173
Max. Ponding Elev at Spill (m):	112.98
Min. Ponding Elev (Lid Elev) (m):	112.88
Max. Prism Volume (m3)	5.77
Depth to Inv below ground (m)	1.400
Allowance for Overland Flow (m)	0.150
Ponding Rim Elevation (m)	113.13
Inv Elev of Storage Node (m)	111.48
Max Ponding Depth (m) =	0.100

Storage Function for Modelling			
Head / Depth (m)	Area (m2)	Incr Vol (m3)	Tot Vol (m3)
0.0000	0.0000	0.00	0.00
1.4000	0.3600	0.50	0.50
1.5000	173	5.77	6.27
1.5001	0	0.00	6.27
1.6500	0	0.00	6.27

Copy to PCSWMM (depth / area)

No. of Inlets = 2 catchbasin

Ponding Information	
Ponding Area (trap low) No:	SP07
Structure / Inlet No:	IN09004
Structre / Inlet Type	Catcbasin
Include Structure Storage (yes/no)	Yes
Structure Shape (rect / round)	Rect
Structure Length or DIA (mm)	600
Structure Width (mm)	600
Max. Ponding Area (m2) =	18
Max. Ponding Elev at Spill (m):	113.90
Min. Ponding Elev (Lid Elev) (m):	113.83
Max. Prism Volume (m3)	0.42
Depth to Inv below ground (m)	1.400
Allowance for Overland Flow (m)	0.150
Ponding Rim Elevation (m)	114.05
Inv Elev of Storage Node (m)	112.43
Max Ponding Depth (m) =	0.070

Storage Function for Modelling			
Head / Depth (m)	Area (m2)	Incr Vol (m3)	Tot Vol (m3)
0.0000	0.0000	0.00	0.00
1.4000	0.3600	0.50	0.50
1.4700	18	0.42	0.92
1.4701	0	0.00	0.92
1.6200	0	0.00	0.92

Copy to PCSWMM (depth / area)

No. of Inlets = 1 catchbasin

Ponding Information	
Ponding Area (trap low) No:	SP08
Structure / Inlet No:	IN09016
Structre / Inlet Type	Catcbasin
Include Structure Storage (yes/no)	Yes
Structure Shape (rect / round)	Rect
Structure Length or DIA (mm)	600
Structure Width (mm)	600
Max. Ponding Area (m2) =	41
Max. Ponding Elev at Spill (m):	111.30
Min. Ponding Elev (Lid Elev) (m):	111.00
Max. Prism Volume (m3)	4.10
Depth to Inv below ground (m)	1.660
Allowance for Overland Flow (m)	0.150
Ponding Rim Elevation (m)	111.45
Inv Elev of Storage Node (m)	109.34
Max Ponding Depth (m) =	0.300

Storage Function for Modelling			
Head / Depth (m)	Area (m2)	Incr Vol (m3)	Tot Vol (m3)
0.0000	0.0000	0.00	0.00
1.6600	0.3600	0.60	0.60
1.9600	41	4.10	4.70
1.9601	0	0.00	4.70
2.1100	0	0.00	4.70

Copy to PCSWMM (depth / area)

No. of Inlets = 1 catchbasin

Ponding Information	
Ponding Area (trap low) No:	SP09
Structure / Inlet No:	MHST09012
Structre / Inlet Type	Manhole
Include Structure Storage (yes/no)	Yes
Structure Shape (rect / round)	Round
Structure Length or DIA (mm)	1200
Structure Width (mm)	
Max. Ponding Area (m2) =	44
Max. Ponding Elev at Spill (m):	111.30
Min. Ponding Elev (Lid Elev) (m):	111.00
Max. Prism Volume (m3)	4.40
Depth to Inv below ground (m)	3.510
Allowance for Overland Flow (m)	0.150
Ponding Rim Elevation (m)	111.45
Inv Elev of Storage Node (m)	107.49
Max Ponding Depth (m) =	0.300

Storage Function for Modelling			
Head / Depth (m)	Area (m2)	Incr Vol (m3)	Tot Vol (m3)
0.0000	0.0000	0.00	0.00
3.5100	1.1310	3.97	3.97
3.8100	44	4.40	8.37
3.8101	0	0.00	8.37
3.9600	0	0.00	8.37
Copy to PCSWMM (depth / area)			

No. of Inlets = 1 manhole



Ponding Information	
Ponding Area (trap low) No:	SP10
Structure / Inlet No:	AD23
Structre / Inlet Type	Catcbasin
Include Structure Storage (yes/no)	Yes
Structure Shape (rect / round)	Rect
Structure Length or DIA (mm)	600
Structure Width (mm)	600
Max. Ponding Area (m2) =	2927
Max. Ponding Elev at Spill (m):	111.50
Min. Ponding Elev (Lid Elev) (m):	111.20
Max. Prism Volume (m3)	292.70
Depth to Inv below ground (m)	0.150
Allowance for Overland Flow (m)	0.150
Ponding Rim Elevation (m)	111.65
Inv Elev of Storage Node (m)	111.05
Max Ponding Depth (m) =	0.300

Storage Function for Modelling			
Head / Depth (m)	Area (m2)	Incr Vol (m3)	Tot Vol (m3)
0.0000	0.0000	0.00	0.00
0.1500	0.3600	0.05	0.05
0.4500	2927	292.70	292.75
0.4501	0	0.00	292.75
0.6000	0	0.00	292.75
Copy to PCSWMM (depth / area)			

No. of Inlets = 6 catchbasins

*exp Services Inc
Hazeldean Crossing Inc.
5924 Hazeldean Road
OTT-00250806-B0
January 22, 2020*

Appendix F – Stormceptor Sizing

Detailed Report from PCSWMM for Stormceptor

Product Sheet

Standard Model Detail

Stormceptor® EF Sizing Report

ESTIMATED NET ANNUAL SEDIMENT (TSS) LOAD REDUCTION STORMCEPTOR®			
Province:	Ontario	Project Name:	5924 Hazeldean
City:	Ottawa	Project Number:	20329
Nearest Rainfall Station:	OTTAWA MACDONALD-CARTIER INT'L AP	Designer Name:	Kent Campbell
NCDC Rainfall Station Id:	6000	Designer Company:	Forterra Pipe & Products
Years of Rainfall Data:	37	Designer Email/Phone:	kent.campbell@forterrabp.com
Site Name:	EF	EOR Name:	Moe Ghadban
Drainage Area (ha):	0.87	EOR Company:	EXP
% Imperviousness:	71.30	EOR Email/Phone:	
Runoff Coefficient 'c': 0.72		Net Annual Sediment (TSS) Load Reduction Sizing Summary	
Particle Size Distribution:	Fine	Stormceptor Model	TSS Removal Provided (%)
Target TSS Removal (%):	80.0	EF4	75
Require Hydrocarbon Spill Capture?	No	EF6	82
Upstream Flow Control?	No	EF8	86
Required Water Quality Runoff Volume Capture (%):	85.00	EF10	89
Estimated Water Quality Flow Rate (L/s):	16.17	EF12	90
Peak Conveyance (maximum) Flow Rate (L/s):	50.30		
Site Sediment Transport Rate (kg/ha/yr):			
Recommended Stormceptor EF Model: EF6 Estimated Net Annual Sediment (TSS) Load Reduction (%): 82 Water Quality Runoff Volume Capture (%): > 90			

Stormceptor® EF Sizing Report**THIRD-PARTY TESTING AND VERIFICATION**

► **Stormceptor® EF and Stormceptor® EFO** are the latest evolutions in the Stormceptor® oil-grit separator (OGS) technology series, and are designed to remove a wide variety of pollutants from stormwater and snowmelt runoff. These technologies have been third-party tested in accordance with the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators** and performance has been third-party verified in accordance with the ISO 14034 Environmental Technology Verification (ETV) protocol.

PERFORMANCE

► **Stormceptor® EF and EFO** remove stormwater pollutants through gravity separation and floatation, and feature a patent-pending design that generates positive removal of total suspended solids (TSS) throughout each storm event, including high-intensity storms. Captured pollutants include sediment, free oils, and sediment-bound pollutants such as nutrients, heavy metals, and petroleum hydrocarbons. Stormceptor is sized to remove a high level of TSS from the frequent rainfall events that contribute the vast majority of annual runoff volume and pollutant load. The technology incorporates an internal bypass to convey excessive stormwater flows from high-intensity storms through the device without resuspension and washout (scour) of previously captured pollutants. Proper routine maintenance ensures high pollutant removal performance and protection of downstream waterways.

PARTICLE SIZE DISTRIBUTION (PSD)

► The **Canadian ETV PSD** shown in the table below was used, or in part, for this sizing. This is the identical PSD that is referenced in the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators** for both sediment removal testing and scour testing. The Canadian ETV PSD contains a wide range of particle sizes in the sand and silt fractions, and is considered reasonably representative of the particle size fractions found in typical urban stormwater runoff.

Particle Size (μm)	Percent Less Than	Particle Size Fraction (μm)	Percent
1000	100	500-1000	5
500	95	250-500	5
250	90	150-250	15
150	75	100-150	15
100	60	75-100	10
75	50	50-75	5
50	45	20-50	10
20	35	8-20	15
8	20	5-8	10
5	10	2-5	5
2	5	<2	5



Stormceptor® EF Sizing Report

Rainfall Intensity (mm / hr)	Percent Rainfall Volume (%)	Cumulative Rainfall Volume (%)	Flow Rate (L/s)	Flow Rate (L/min)	Surface Loading Rate (L/min/m²)	Removal Efficiency (%)	Incremental Removal (%)	Cumulative Removal (%)
1	51.3	51.3	1.76	106.0	40.0	93	47.7	47.7
2	8.7	60.0	3.52	211.0	80.0	89	7.7	55.5
3	5.8	65.8	5.28	317.0	120.0	85	4.9	60.4
4	4.6	70.4	7.04	422.0	161.0	80	3.7	64.1
5	4.2	74.6	8.80	528.0	201.0	76	3.2	67.3
6	3.2	77.8	10.56	634.0	241.0	72	2.3	69.6
7	2.6	80.4	12.32	739.0	281.0	69	1.8	71.4
8	2.4	82.8	14.08	845.0	321.0	65	1.6	72.9
9	1.9	84.7	15.84	951.0	361.0	62	1.2	74.1
10	1.6	86.3	17.60	1056.0	402.0	58	0.9	75.0
11	1.3	87.6	19.36	1162.0	442.0	58	0.7	75.8
12	1.1	88.7	21.12	1267.0	482.0	57	0.6	76.4
13	1.3	90.0	22.88	1373.0	522.0	57	0.7	77.1
14	1.1	91.1	24.64	1479.0	562.0	56	0.6	77.8
15	0.6	91.7	26.40	1584.0	602.0	56	0.3	78.1
16	0.8	92.5	28.16	1690.0	643.0	56	0.4	78.5
17	0.7	93.2	29.92	1795.0	683.0	56	0.4	78.9
18	0.5	93.7	31.68	1901.0	723.0	55	0.3	79.2
19	0.6	94.3	33.44	2007.0	763.0	55	0.3	79.5
20	0.5	94.8	35.21	2112.0	803.0	55	0.3	79.8
21	0.2	95.0	36.97	2218.0	843.0	55	0.1	79.9
22	0.4	95.4	38.73	2324.0	883.0	55	0.2	80.1
23	0.5	95.9	40.49	2429.0	924.0	54	0.3	80.4
24	0.4	96.3	42.25	2535.0	964.0	54	0.2	80.6
25	0.1	96.4	44.01	2640.0	1004.0	54	0.1	80.7



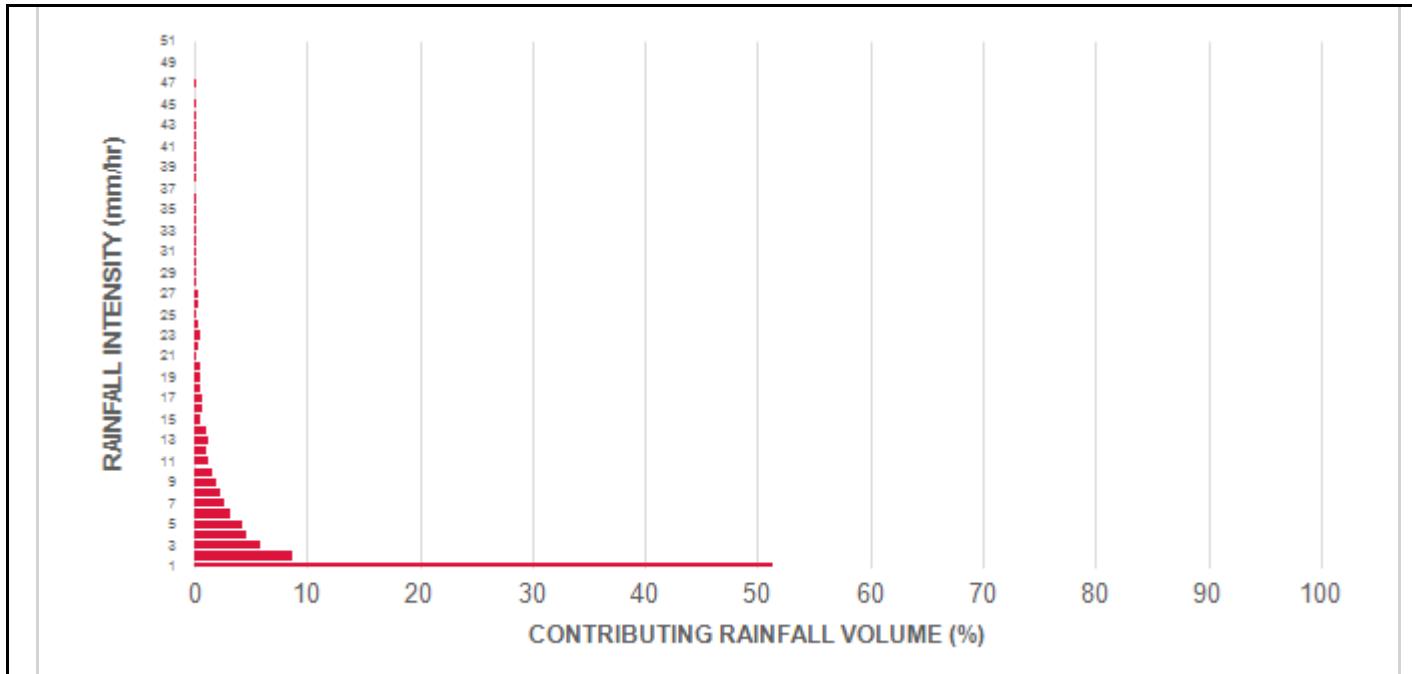
Stormceptor® EF Sizing Report

Rainfall Intensity (mm / hr)	Percent Rainfall Volume (%)	Cumulative Rainfall Volume (%)	Flow Rate (L/s)	Flow Rate (L/min)	Surface Loading Rate (L/min/m²)	Removal Efficiency (%)	Incremental Removal (%)	Cumulative Removal (%)
26	0.3	96.7	45.77	2746.0	1044.0	55	0.2	80.8
27	0.4	97.1	47.53	2852.0	1084.0	55	0.2	81.1
28	0.2	97.3	49.29	2957.0	1124.0	56	0.1	81.2
29	0.2	97.5	51.05	3063.0	1165.0	56	0.1	81.3
30	0.2	97.7	52.81	3168.0	1205.0	57	0.1	81.4
31	0.1	97.8	54.57	3274.0	1245.0	57	0.1	81.5
32	0.2	98.0	56.33	3380.0	1285.0	58	0.1	81.6
33	0.1	98.1	58.09	3485.0	1325.0	58	0.1	81.6
34	0.1	98.2	59.85	3591.0	1365.0	59	0.1	81.7
35	0.1	98.3	61.61	3697.0	1406.0	59	0.1	81.7
36	0.2	98.5	63.37	3802.0	1446.0	57	0.1	81.9
37	0.0	98.5	65.13	3908.0	1486.0	56	0.0	81.9
38	0.1	98.6	66.89	4013.0	1526.0	54	0.1	81.9
39	0.1	98.7	68.65	4119.0	1566.0	53	0.1	82.0
40	0.1	98.8	70.41	4225.0	1606.0	52	0.1	82.0
41	0.1	98.9	72.17	4330.0	1646.0	50	0.1	82.1
42	0.1	99.0	73.93	4436.0	1687.0	49	0.0	82.1
43	0.2	99.2	75.69	4541.0	1727.0	48	0.1	82.2
44	0.1	99.3	77.45	4647.0	1767.0	47	0.0	82.3
45	0.1	99.4	79.21	4753.0	1807.0	46	0.0	82.3
46	0.0	99.4	80.97	4858.0	1847.0	45	0.0	82.3
47	0.1	99.5	82.73	4964.0	1887.0	44	0.0	82.4
48	0.0	99.5	84.49	5070.0	1928.0	43	0.0	82.4
49	0.0	99.5	86.25	5175.0	1968.0	42	0.0	82.4
50	0.0	99.5	88.01	5281.0	2008.0	41	0.0	82.4
Estimated Net Annual Sediment (TSS) Load Reduction =							82 %	

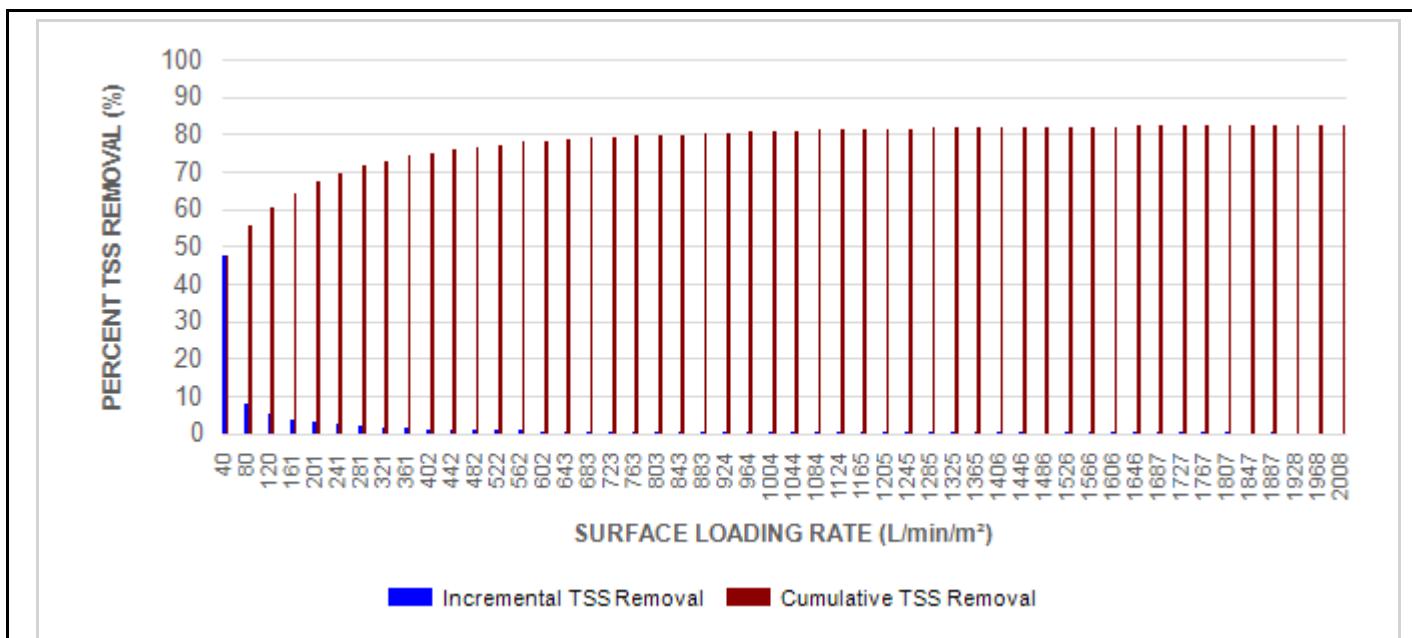


Stormceptor® EF Sizing Report

RAINFALL DATA FROM OTTAWA MACDONALD-CARTIER INT'L AP RAINFALL STATION



INCREMENTAL AND CUMULATIVE TSS REMOVAL FOR THE RECOMMENDED STORMCEPTOR® MODEL



Stormceptor® EF Sizing Report

Maximum Pipe Diameter / Peak Conveyance

Stormceptor EF / EFO	Model Diameter		Min Angle Inlet / Outlet Pipes	Max Inlet Pipe Diameter		Max Outlet Pipe Diameter		Peak Conveyance Flow Rate	
	(m)	(ft)		(mm)	(in)	(mm)	(in)	(L/s)	(cfs)
EF4 / EFO4	1.2	4	90	609	24	609	24	425	15
EF6 / EFO6	1.8	6	90	914	36	914	36	990	35
EF8 / EFO8	2.4	8	90	1219	48	1219	48	1700	60
EF10 / EFO10	3.0	10	90	1828	72	1828	72	2830	100
EF12 / EFO12	3.6	12	90	1828	72	1828	72	2830	100

SCOUR PREVENTION AND ONLINE CONFIGURATION

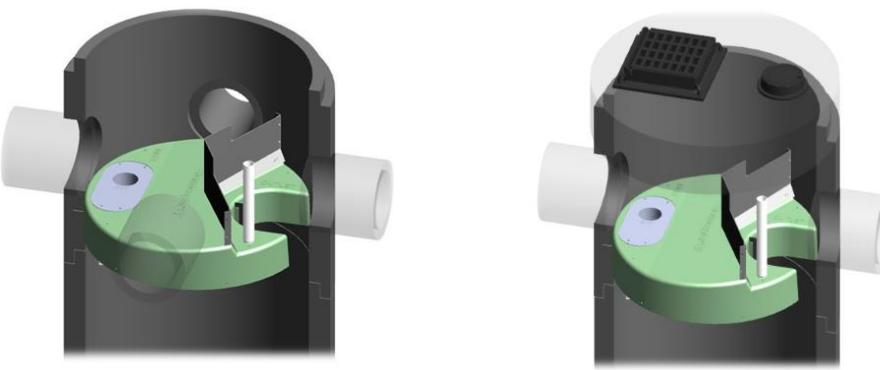
► Stormceptor® EF and EFO feature an internal bypass and superior scour prevention technology that have been demonstrated in third-party testing according to the scour testing provisions of the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators**, and the exceptional scour test performance has been third-party verified in accordance with the ISO 14034 ETV protocol. As a result, Stormceptor EF and EFO are approved for online installation, eliminating the need for costly additional bypass structures, piping, and installation expense.

DESIGN FLEXIBILITY

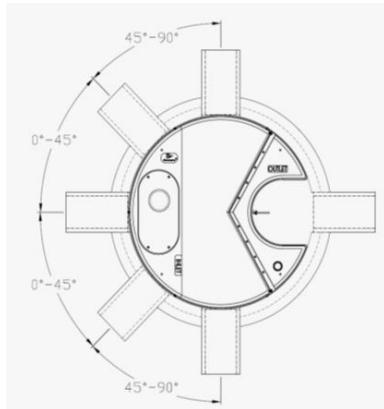
► Stormceptor® EF and EFO offers design flexibility in one simplified platform, accepting stormwater flow from a single inlet pipe or multiple inlet pipes, and/or surface runoff through an inlet grate. The device can also serve as a junction structure, accommodate a 90-degree inlet-to-outlet bend angle, and can be modified to ensure performance in submerged conditions.

OIL CAPTURE AND RETENTION

► While Stormceptor® EF will capture and retain oil from dry weather spills and low intensity runoff, Stormceptor® EFO has demonstrated superior oil capture and greater than 99% oil retention in third-party testing according to the light liquid re-entrainment testing provisions of the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators**. Stormceptor EFO is recommended for sites where oil capture and retention is a requirement.



Stormceptor® EF Sizing Report



INLET-TO-OUTLET DROP

Elevation differential between inlet and outlet pipe inverts is dictated by the angle at which the inlet pipe(s) enters the unit.

0° - 45° : The inlet pipe is 1-inch (25mm) higher than the outlet pipe.

45° - 90° : The inlet pipe is 2-inches (50mm) higher than the outlet pipe.

HEAD LOSS

The head loss through Stormceptor EF is similar to that of a 60-degree bend structure. The applicable K value for calculating minor losses through the unit is 1.1. For submerged conditions the applicable K value is 3.0.

Pollutant Capacity

Stormceptor EF / EFO	Model Diameter		Depth (Outlet Pipe Invert to Sump Floor)		Oil Volume		Recommended Sediment Maintenance Depth *		Maximum Sediment Volume * (ft³)		Maximum Sediment Mass **	
	(m)	(ft)	(m)	(ft)	(L)	(Gal)	(mm)	(in)	(L)	(ft³)	(kg)	(lb)
EF4 / EFO4	1.2	4	1.52	5.0	197	52	203	8	1190	42	1904	5250
EF6 / EFO6	1.8	6	1.93	6.3	348	92	305	12	3470	123	5552	15375
EF8 / EFO8	2.4	8	2.59	8.5	545	144	610	24	8780	310	14048	38750
EF10 / EFO10	3.0	10	3.25	10.7	874	231	610	24	17790	628	28464	78500
EF12 / EFO12	3.6	12	3.89	12.8	1219	322	610	24	31220	1103	49952	137875

*Increased sump depth may be added to increase sediment storage capacity

** Average density of wet packed sediment in sump = 1.6 kg/L (100 lb/ft³)

Feature	Benefit	Feature Appeals To
Patent-pending enhanced flow treatment and scour prevention technology	Superior, verified third-party performance	Regulator, Specifying & Design Engineer
Third-party verified light liquid capture and retention for EFO version	Proven performance for fuel/oil hotspot locations	Regulator, Specifying & Design Engineer, Site Owner
Functions as bend, junction or inlet structure	Design flexibility	Specifying & Design Engineer
Minimal drop between inlet and outlet	Site installation ease	Contractor
Large diameter outlet riser for inspection and maintenance	Easy maintenance access from grade	Maintenance Contractor & Site Owner

STANDARD STORMCEPTOR EF/EFO DRAWINGS

For standard details, please visit <http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef>

STANDARD STORMCEPTOR EF/EFO SPECIFICATION

For specifications, please visit <http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef>



Stormceptor® EF Sizing Report

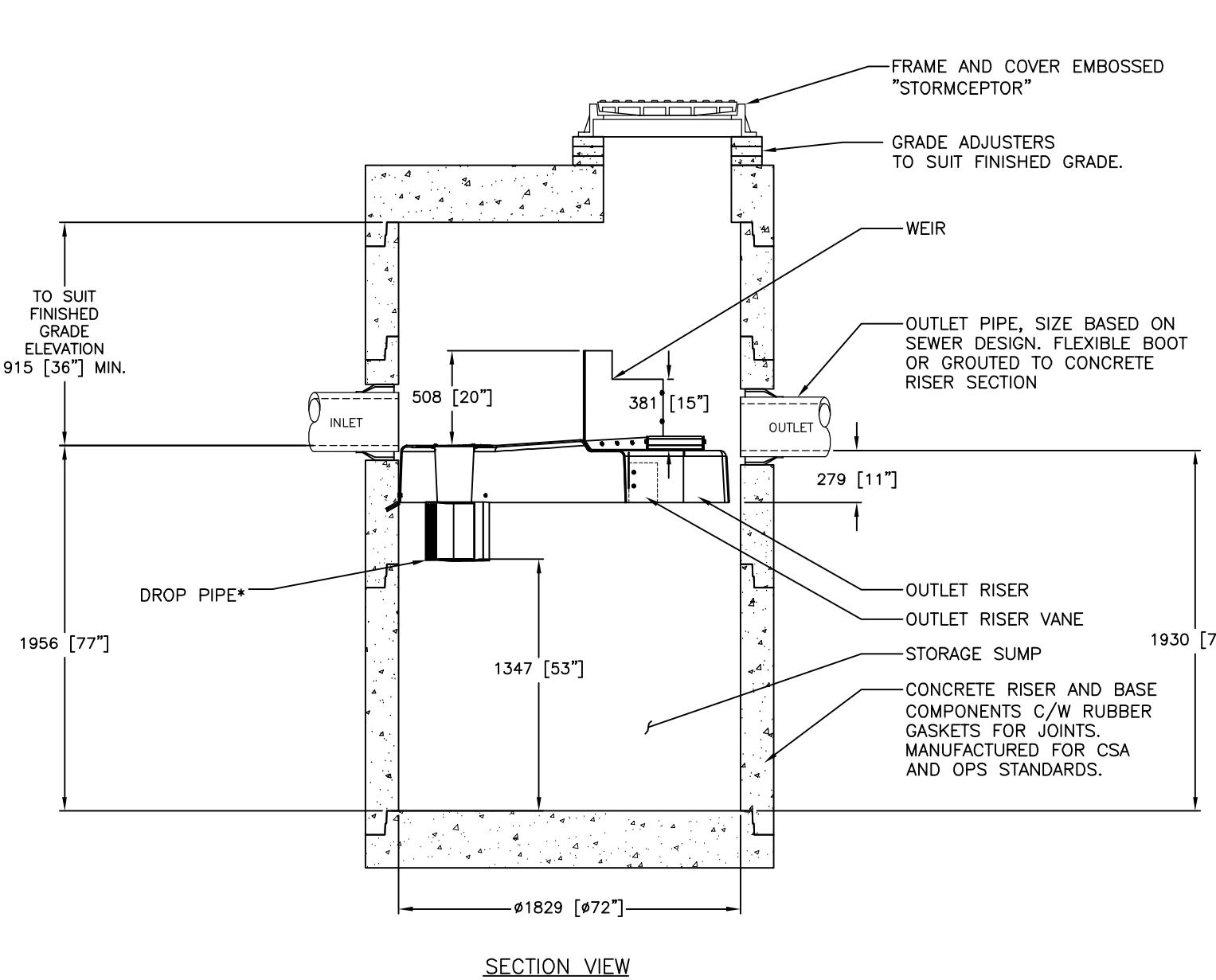
Table of TSS Removal vs Surface Loading Rate Based on Third-Party Test Results
Stormceptor® EF

SLR (L/min/m ²)	TSS % REMOVAL						
1	70	660	46	1320	48	1980	35
30	70	690	46	1350	48	2010	34
60	67	720	45	1380	49	2040	34
90	63	750	45	1410	49	2070	33
120	61	780	45	1440	48	2100	33
150	58	810	45	1470	47	2130	32
180	56	840	45	1500	46	2160	32
210	54	870	45	1530	45	2190	31
240	53	900	45	1560	44	2220	31
270	52	930	44	1590	43	2250	30
300	51	960	44	1620	42	2280	30
330	50	990	44	1650	42	2310	30
360	49	1020	44	1680	41	2340	29
390	48	1050	45	1710	40	2370	29
420	48	1080	45	1740	39	2400	29
450	48	1110	45	1770	39	2430	28
480	47	1140	46	1800	38	2460	28
510	47	1170	46	1830	37	2490	28
540	47	1200	47	1860	37	2520	27
570	46	1230	47	1890	36	2550	27
600	46	1260	47	1920	36	2580	27
630	46	1290	48	1950	35		



DRAWING NOT TO BE USED FOR CONSTRUCTION

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GENERAL NOTES:

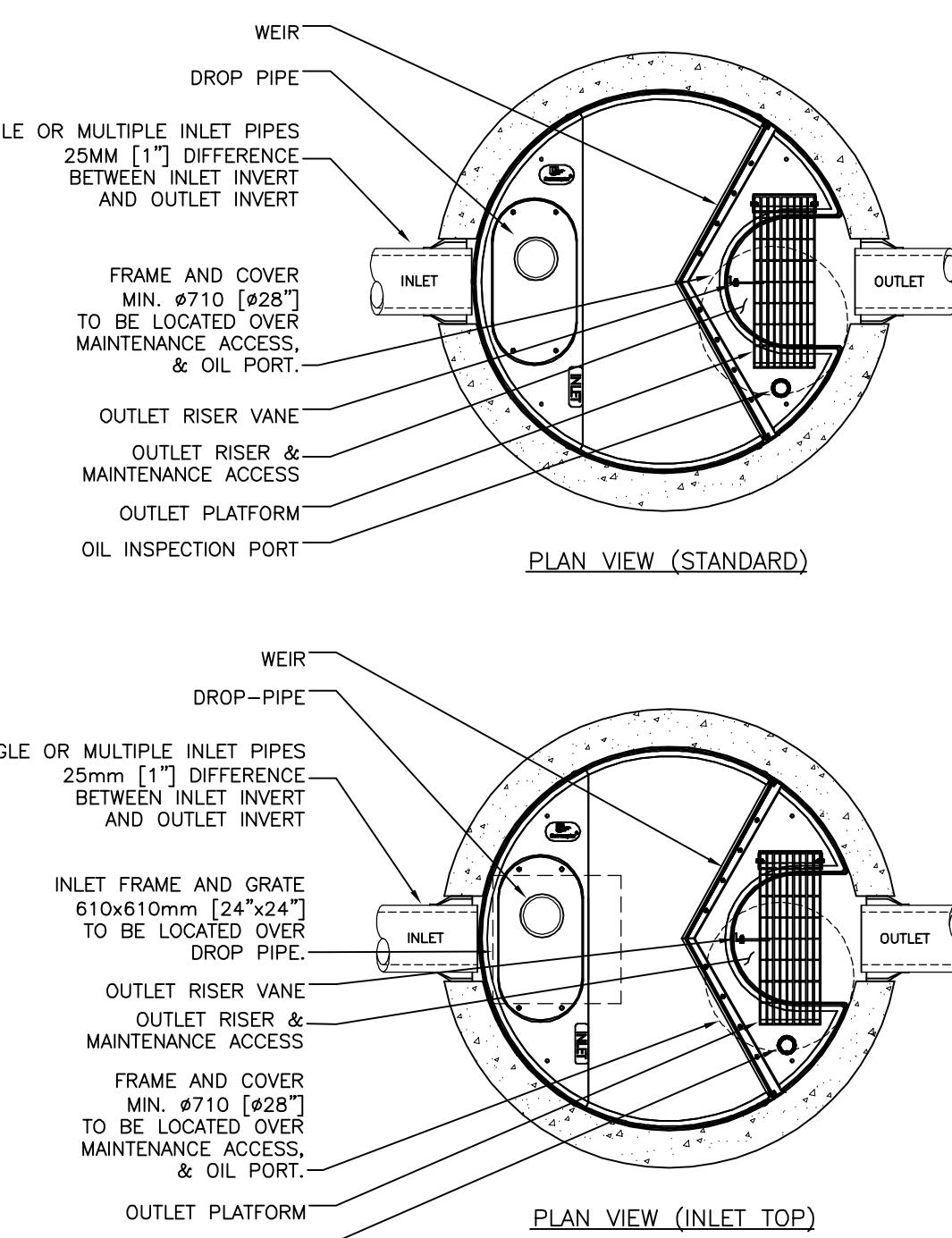
* MAXIMUM SURFACE LOADING RATE (SLR) INTO LOWER CHAMBER THROUGH DROP PIPE IS 1135 L/min/m² (27.9 gpm/ft²) FOR STORMCEPTOR EF6 AND 535 L/min/m² (13.1 gpm/ft²) FOR STORMCEPTOR EFO6 (OIL CAPTURE CONFIGURATION).

1. ALL DIMENSIONS INDICATED ARE IN MILLIMETERS (INCHES) UNLESS OTHERWISE SPECIFIED.
 2. STORMCEPTOR STRUCTURE INLET AND OUTLET PIPE SIZE AND ORIENTATION SHOWN FOR INFORMATIONAL PURPOSES ONLY.
 3. UNLESS OTHERWISE NOTED, BYPASS INFRASTRUCTURE, SUCH AS ALL UPSTREAM DIVERSION STRUCTURES, CONNECTING STRUCTURES, OR PIPE CONDUITS CONNECTING TO COMPLETE THE STORMCEPTOR SYSTEM SHALL BE PROVIDED AND ADDRESSED SEPARATELY.
 4. DRAWING FOR INFORMATION PURPOSES ONLY. REFER TO ENGINEER'S SITE/UTILITY PLAN FOR STRUCTURE ORIENTATION.
 5. NO PRODUCT SUBSTITUTIONS SHALL BE ACCEPTED UNLESS SUBMITTED 10 DAYS PRIOR TO PROJECT BID DATE, OR AS DIRECTED BY THE ENGINEER OF RECORD.

FOR SITE SPECIFIC DRAWINGS PLEASE CONTACT YOUR LOCAL STORMCEPTOR REPRESENTATIVE. SITE SPECIFIC DRAWINGS ARE BASED ON THE BEST AVAILABLE INFORMATION AT THE TIME. SOME FIELD REVISIONS TO THE SYSTEM LOCATION OR CONNECTION PIPING MAY BE NECESSARY BASED ON AVAILABLE SPACE OR SITE CONFIGURATION REVISIONS. ELEVATIONS SHOULD BE MAINTAINED EXCEPT WHERE NOTED ON BYPASS STRUCTURE (IF REQUIRED).

STANDARD DETAIL

NOT FOR CONSTRUCTION



SITE SPECIFIC DATA REQUIREMENTS

STORMCEPTOR MODEL		EF6											
STRUCTURE ID		*											
WATER QUALITY FLOW RATE (L/s)		*											
PEAK FLOW RATE (L/s)		*											
RETURN PERIOD OF PEAK FLOW (yrs)		*											
DRAINAGE AREA (HA)		*											
DRAINAGE AREA IMPERVIOUSNESS (%)		*											
PIPE DATA:	I.E.	MAT'L	DIA	SLOPE %	HGL								
INLET #1	*	*	*	*	*								
INLET #2	*	*	*	*	*								
OUTLET	*	*	*	*	*								
PER ENGINEER OF RECORD													
 <p>407 FAIRVIEW DRIVE, WHITBY, ON N9A 5G1, CANADA TOLL FREE: 1-866-468-5801 TELE: 905-669-5801 FAX: 905-669-5802 E-MAIL: info@imbrilis.com WEBSITE: www.imbrilis.com</p>													
<p>DATE: 5/26/2017</p> <table border="1"> <tr> <td>DESIGNED: JSK</td> <td>DRAWN: JSK</td> </tr> <tr> <td>CHECKED: BSF</td> <td>APPROVED: SP</td> </tr> <tr> <td>PROJECT No.: EF6</td> <td>SEQUENCE No.: *</td> </tr> <tr> <td colspan="2">SHEET: 1 OF 1</td> </tr> </table>						DESIGNED: JSK	DRAWN: JSK	CHECKED: BSF	APPROVED: SP	PROJECT No.: EF6	SEQUENCE No.: *	SHEET: 1 OF 1	
DESIGNED: JSK	DRAWN: JSK												
CHECKED: BSF	APPROVED: SP												
PROJECT No.: EF6	SEQUENCE No.: *												
SHEET: 1 OF 1													

* PER ENGINEER OF RECORD

Stormceptor® EF

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Appendix G – PCSWMM Data

Input File (Details) for 100-yr 3hr Chicago Storm

Output File (Status) for 100-yr 3hr Chicago Storm

PCSWMM Report Files

[TITLE]
Updated PCSWMM Model to Include offsite Storm Sewer Analysis
Full Dual Drainage Model
J Fitzpatrick
Nov 1, 2019
{Jason Fitzpatrick - 2019.10.25} IN09006-MAJ

[OPTIONS]
;Options Value
;-----
FLOW_UNITS LPS
INFILTRATION HORTON
FLOW_ROUTING DYNWAVE
LINK_OFFSETS ELEVATION
MIN_SLOPE 0
ALLOW_PONDING NO
SKIP_STEADY_STATE NO
START_DATE 09/26/2018
START_TIME 00:00:00
REPORT_START_DATE 09/26/2018
REPORT_START_TIME 00:00:00
END_DATE 09/26/2018
END_TIME 06:00:00
SWEEP_START 01/01
SWEEP_END 12/31
DRY_DAYS 0
REPORT_STEP 00:01:00
WET_STEP 00:01:00
DRY_STEP 00:01:00
ROUTING_STEP 5
INERTIAL_DAMPING PARTIAL
NORMAL_FLOW_LIMITED BOTH
FORCE_MAIN_EQUATION H-W
VARIABLE_STEP 0.75
LENGTHENING_STEP 0
MIN_SURFAREA 1.167
MAX_TRIALS 8
HEAD_TOLERANCE 0.0015
SYS_FLOW_TOL 5
LAT_FLOW_TOL 5
MINIMUM_STEP 0.5
THREADS 2

[EVAPORATION]
;Type Parameters
;-----
CONSTANT 0.0
DRY_ONLY NO

[RAINGAGES]
;; Rain Time Snow Data
;; Name Type Intrvl Catch Source

;-----
Chicago_3h_100yr INTENSITY 0:10 1.0 TIMESERIES Chicago_3h_100yr
Chicago_3h_2year INTENSITY 0:10 1.0 TIMESERIES Chicago_3h_2yr
Chicago_3h_5year INTENSITY 0:10 1.0 TIMESERIES Chicago_3h_5year

[SUBCATCHMENTS]
; ;Name Raingage Outlet Total Pcnt. Pcnt. Curb Snow
; ;Name Raingage Outlet Area Imperv Width Slope Length Pack
;-----
;OFFSITE
ES01_1 Chicago_3h_100yr IN103407 0.3255 67.777 57 1.5 0
;OFFSITE
ES02_1 Chicago_3h_100yr IN09004-MAJ 0.0884 31.285 48.8 1 0
;OFFSITE
ES02_2 Chicago_3h_100yr IN09003-MAJ 0.0477 44.983 36.7 1 0
;OFFSITE
ES03_1 Chicago_3h_100yr IN09005-MAJ 0.2801 55.552 132.1 1 0
;OFFSITE
ES03_2 Chicago_3h_100yr IN09006-MAJ 0.1878 50.126 114.5 1 0
;OFFSITE
ES04_1 Chicago_3h_100yr IN09008 0.2099 59.961 98.1 0.5 0
;OFFSITE
ES04_2 Chicago_3h_100yr IN09007 0.1951 55.139 98 0.5 0
;OFFSITE
ES05_1 Chicago_3h_100yr IN09009-MAJ 0.1906 52.183 91.6 0.5 0
;OFFSITE
ES05_2 Chicago_3h_100yr IN09010-MAJ 0.1843 54.377 89.9 0.5 0
;OFFSITE
ES06_1 Chicago_3h_100yr IN09011-MAJ 0.2778 59.044 134.9 0.5 0
;OFFSITE
ES06_2 Chicago_3h_100yr IN09012-MAJ 0.2407 55.203 123.4 0.5 0
;OFFSITE
ES07 Chicago_3h_100yr IN09013-MAJ 0.2147 55.576 96.7 0.5 0
;OFFSITE
ES08_1 Chicago_3h_100yr IN09022-MAJ 0.1217 44.675 85.1 0.5 0
;OFFSITE
ES08_2 Chicago_3h_100yr IN09023-MAJ 0.0863 29.627 47.2 0.5 0
;OFFSITE
ES09_1 Chicago_3h_100yr IN09024-MAJ 0.1738 53.85 96.6 0.5 0
;OFFSITE
ES09_2 Chicago_3h_100yr IN09025-MAJ 0.1796 40.275 125.6 0.5 0
;OFFSITE
ES10_1 Chicago_3h_100yr IN09026-MAJ 0.2118 50.248 108.1 0.5 0
;OFFSITE
ES10_2 Chicago_3h_100yr IN09027-MAJ 0.1837 48.55 110 0.5 0
;OFFSITE
ES11_1 Chicago_3h_100yr IN09029-MAJ 0.1845 55.004 88.3 0.5 0
;OFFSITE
ES11_2 Chicago_3h_100yr IN09028-MAJ 0.126 44.553 71.2 0.5 0
;OFFSITE
ES12_1 Chicago_3h_100yr MHST09022 0.1929 56.58 92.7 0.5 0
;OFFSITE
ES12_2 Chicago_3h_100yr IN09031-MAJ 0.1553 55.364 77.3 0.5 0

;OFFSITE							
ES13_1	Chicago_3h_100yr MHST09023	0.1559	56.354	69.9	0.5	0	
;OFFSITE							
ES13_2	Chicago_3h_100yr MHST09023	0.1672	53.557	85.3	0.5	0	
;OFFSITE							
ES14_1	Chicago_3h_100yr IN09014-MAJ	0.1317	42.85	97.6	0.5	0	
;OFFSITE							
ES14_2	Chicago_3h_100yr IN09015-MAJ	0.181	60.093	88.7	0.5	0	
;OFFSITE							
ES15_1	Chicago_3h_100yr IN09016	0.0733	37.055	75.6	0.5	0	
;OFFSITE							
ES15_2	Chicago_3h_100yr MHST09012	0.1226	57.086	70.5	0.5	0	
;OFFSITE							
ES16_1	Chicago_3h_100yr IN09034-MAJ	0.1	35.738	107.5	1.5	0	
;OFFSITE							
ES16_2	Chicago_3h_100yr IN09035-MAJ	0.1733	26.876	100.2	1.5	0	
;OFFSITE							
ES17	Chicago_3h_100yr IN09034-MAJ	0.135	41.718	78.5	2	0	
;OFFSITE							
ES18	Chicago_3h_100yr IN09021-MAJ	0.2378	40.757	93.3	2	0	
;OFFSITE							
ES19	Chicago_3h_100yr IN09019-MAJ	0.0992	63.062	46.4	0.5	0	
;OFFSITE							
ES20	Chicago_3h_100yr IN09020-MAJ	0.0692	33.177	32.3	0.5	0	
;OFFSITE							
ES21_1	Chicago_3h_100yr IN09018-MAJ	0.0791	58.867	36.8	0.5	0	
;OFFSITE							
ES21_3	Chicago_3h_100yr IN09020-MAJ	0.129	42.562	60.8	0.5	0	
;OFFSITE							
ES21_4	Chicago_3h_100yr IN09019-MAJ	0.1398	62.819	60.3	0.5	0	
;OFFSITE							
ES21_5	Chicago_3h_100yr IN09017-MAJ	0.0865	54.717	36.2	0.5	0	
;OFFSITE							
ES22_1	Chicago_3h_100yr IN09016	0.1847	62.634	74.8	0.5	0	
;OFFSITE							
ES22_2	Chicago_3h_100yr MHST09012	0.218	55.462	100.5	0.5	0	
;OFFSITE							
ES23	Chicago_3h_100yr IN45587	0.1837	32.553	22.5	1	0	
;OFFSITE							
ES24	Chicago_3h_100yr IN45588	0.0806	27.007	15.8	1	0	
;OFFSITE							
ES25	Chicago_3h_100yr IN45589	0.1875	27.249	16.6	1	0	
;OFFSITE							
ES26	Chicago_3h_100yr IN45590	0.1086	32.212	17.7	1	0	
;OFFSITE							
ES27	Chicago_3h_100yr IN45575	0.3696	13.466	52.4	1	0	
;OFFSITE							
ES28	Chicago_3h_100yr IN45570	0.3422	21.796	50.1	1	0	
;OFFSITE							
ES29	Chicago_3h_100yr IN45569	0.3256	26.731	46	1	0	
;OFFSITE							
ES30	Chicago_3h_100yr IN45572	0.2289	28.571	47.4	1	0	
;OFFSITE							

ES31	Chicago_3h_100yr IN45577	0.1922	24.966	48.3	1	0		
;OFFSITE								
ES32	Chicago_3h_100yr IN07998	0.7854	19.912	57.1	1	0		
;OFFSITE								
ES33	Chicago_3h_100yr IN45573	0.1591	31.774	51.3	1	0		
;OFFSITE								
ES34	Chicago_3h_100yr IN45574	0.4099	10.084	54.3	1	0		
;OFFSITE								
ES35	Chicago_3h_100yr IN45566	0.967	14.685	66.5	1	0		
;OFFSITE								
ES36	Chicago_3h_100yr IN09032-MAJ	0.215	32.12	113.8	0.5	0		
;ONSITE								
S01	Chicago_3h_100yr CB06	0.1752	80.668	58	1	0		
;ONSITE								
S02	Chicago_3h_100yr CB01	0.1483	88.226	51.7	1	0		
;ONSITE								
S03	Chicago_3h_100yr CB01	0.0178	14.522	80.9	1	0		
;ONSITE								
S04	Chicago_3h_100yr CB03	0.2001	79.11	70.2	1	0		
;ONSITE								
S05	Chicago_3h_100yr 218	0.1264	73.958	53.1	1	0		
;ONSITE								
S06	Chicago_3h_100yr CBT03	0.0617	35.843	52.3	1	0		
;ONSITE								
S07	Chicago_3h_100yr CBE01	0.0415	37.942	54.6	1	0		
;ONSITE								
S08_1	Chicago_3h_100yr CBT14	0.0405	59.421	57.857	1	0		
;ONSITE								
S08_2	Chicago_3h_100yr CBE04	0.0548	54.842	78.286	1	0		
;ONSITE								
S09	Chicago_3h_100yr IN103407	0.0806	71.197	94.8	1	0		
[SUBAREAS]								
;Subcatchment	N-Imperv	N-Perv	S-Imperv	S-Perv	PctZero	RouteTo	PctRouted	
ES01_1	0.011	0.25	1.57	4.67	10	OUTLET		
ES02_1	0.011	0.25	1.57	4.67	10	OUTLET		
ES02_2	0.011	0.25	1.57	4.67	10	OUTLET		
ES03_1	0.011	0.25	1.57	4.67	10	OUTLET		
ES03_2	0.011	0.25	1.57	4.67	10	OUTLET		
ES04_1	0.011	0.25	1.57	4.67	10	OUTLET		
ES04_2	0.011	0.25	1.57	4.67	10	OUTLET		
ES05_1	0.011	0.25	1.57	4.67	10	OUTLET		
ES05_2	0.011	0.25	1.57	4.67	10	OUTLET		
ES06_1	0.011	0.25	1.57	4.67	10	OUTLET		
ES06_2	0.011	0.25	1.57	4.67	10	OUTLET		
ES07	0.011	0.25	1.57	4.67	10	OUTLET		
ES08_1	0.011	0.25	1.57	4.67	10	OUTLET		
ES08_2	0.011	0.25	1.57	4.67	10	OUTLET		
ES09_1	0.011	0.25	1.57	4.67	10	OUTLET		
ES09_2	0.011	0.25	1.57	4.67	10	OUTLET		
ES10_1	0.011	0.25	1.57	4.67	10	OUTLET		
ES10_2	0.011	0.25	1.57	4.67	10	OUTLET		

ES11_1	0.011	0.25	1.57	4.67	10	OUTLET
ES11_2	0.011	0.25	1.57	4.67	10	OUTLET
ES12_1	0.011	0.25	1.57	4.67	10	OUTLET
ES12_2	0.011	0.25	1.57	4.67	10	OUTLET
ES13_1	0.011	0.25	1.57	4.67	10	OUTLET
ES13_2	0.011	0.25	1.57	4.67	10	OUTLET
ES14_1	0.011	0.25	1.57	4.67	10	OUTLET
ES14_2	0.011	0.25	1.57	4.67	10	OUTLET
ES15_1	0.011	0.25	1.57	4.67	10	OUTLET
ES15_2	0.011	0.25	1.57	4.67	10	OUTLET
ES16_1	0.011	0.25	1.57	4.67	10	OUTLET
ES16_2	0.011	0.25	1.57	4.67	10	OUTLET
ES17	0.011	0.25	1.57	4.67	10	OUTLET
ES18	0.011	0.25	1.57	4.67	10	OUTLET
ES19	0.011	0.25	1.57	4.67	10	OUTLET
ES20	0.011	0.25	1.57	4.67	10	OUTLET
ES21_1	0.011	0.25	1.57	4.67	10	OUTLET
ES21_3	0.011	0.25	1.57	4.67	10	OUTLET
ES21_4	0.011	0.25	1.57	4.67	10	OUTLET
ES21_5	0.011	0.25	1.57	4.67	10	OUTLET
ES22_1	0.011	0.25	1.57	4.67	10	OUTLET
ES22_2	0.011	0.25	1.57	4.67	10	OUTLET
ES23	0.011	0.25	1.57	4.67	10	OUTLET
ES24	0.011	0.25	1.57	4.67	10	OUTLET
ES25	0.011	0.25	1.57	4.67	10	OUTLET
ES26	0.011	0.25	1.57	4.67	10	OUTLET
ES27	0.011	0.25	1.57	4.67	10	OUTLET
ES28	0.011	0.25	1.57	4.67	10	OUTLET
ES29	0.011	0.25	1.57	4.67	10	OUTLET
ES30	0.011	0.25	1.57	4.67	10	OUTLET
ES31	0.011	0.25	1.57	4.67	10	OUTLET
ES32	0.011	0.25	1.57	4.67	10	OUTLET
ES33	0.011	0.25	1.57	4.67	10	OUTLET
ES34	0.011	0.25	1.57	4.67	10	OUTLET
ES35	0.011	0.25	1.57	4.67	10	OUTLET
ES36	0.011	0.25	1.57	4.67	10	OUTLET
S01	0.011	0.25	1.57	4.67	20	OUTLET
S02	0.011	0.25	1.57	4.67	20	OUTLET
S03	0.011	0.25	1.57	4.67	20	OUTLET
S04	0.011	0.25	1.57	4.67	20	OUTLET
S05	0.011	0.25	1.57	4.67	20	OUTLET
S06	0.011	0.25	1.57	4.67	20	OUTLET
S07	0.011	0.25	1.57	4.67	20	OUTLET
S08_1	0.011	0.25	1.57	4.67	20	OUTLET
S08_2	0.011	0.25	1.57	4.67	20	OUTLET
S09	0.011	0.25	1.57	4.67	20	OUTLET

[INFILTRATION]	;	Subcatchment	MaxRate	MinRate	Decay	DryTime	MaxInfil
;	-----						
ES01_1	76.2	13.2	4.14	7	0		
ES02_1	76.2	13.2	4.14	7	0		
ES02_2	76.2	13.2	4.14	7	0		

ES03_1	76.2	13.2	4.14	7	0
ES03_2	76.2	13.2	4.14	7	0
ES04_1	76.2	13.2	4.14	7	0
ES04_2	76.2	13.2	4.14	7	0
ES05_1	76.2	13.2	4.14	7	0
ES05_2	76.2	13.2	4.14	7	0
ES06_1	76.2	13.2	4.14	7	0
ES06_2	76.2	13.2	4.14	7	0
ES07	76.2	13.2	4.14	7	0
ES08_1	76.2	13.2	4.14	7	0
ES08_2	76.2	13.2	4.14	7	0
ES09_1	76.2	13.2	4.14	7	0
ES09_2	76.2	13.2	4.14	7	0
ES10_1	76.2	13.2	4.14	7	0
ES10_2	76.2	13.2	4.14	7	0
ES11_1	76.2	13.2	4.14	7	0
ES11_2	76.2	13.2	4.14	7	0
ES12_1	76.2	13.2	4.14	7	0
ES12_2	76.2	13.2	4.14	7	0
ES13_1	76.2	13.2	4.14	7	0
ES13_2	76.2	13.2	4.14	7	0
ES14_1	76.2	13.2	4.14	7	0
ES14_2	76.2	13.2	4.14	7	0
ES15_1	76.2	13.2	4.14	7	0
ES15_2	76.2	13.2	4.14	7	0
ES16_1	76.2	13.2	4.14	7	0
ES16_2	76.2	13.2	4.14	7	0
ES17	76.2	13.2	4.14	7	0
ES18	76.2	13.2	4.14	7	0
ES19	76.2	13.2	4.14	7	0
ES20	76.2	13.2	4.14	7	0
ES21_1	76.2	13.2	4.14	7	0
ES21_3	76.2	13.2	4.14	7	0
ES21_4	76.2	13.2	4.14	7	0
ES21_5	76.2	13.2	4.14	7	0
ES22_1	76.2	13.2	4.14	7	0
ES22_2	76.2	13.2	4.14	7	0
ES23	76.2	13.2	4.14	7	0
ES24	76.2	13.2	4.14	7	0
ES25	76.2	13.2	4.14	7	0
ES26	76.2	13.2	4.14	7	0
ES27	76.2	13.2	4.14	7	0
ES28	76.2	13.2	4.14	7	0
ES29	76.2	13.2	4.14	7	0
ES30	76.2	13.2	4.14	7	0
ES31	76.2	13.2	4.14	7	0
ES32	76.2	13.2	4.14	7	0
ES33	76.2	13.2	4.14	7	0
ES34	76.2	13.2	4.14	7	0
ES35	76.2	13.2	4.14	7	0
ES36	76.2	13.2	4.14	7	0
S01	76.2	13.2	4.14	7	0
S02	76.2	13.2	4.14	7	0

S03	76.2	13.2	4.14	7	0
S04	76.2	13.2	4.14	7	0
S05	76.2	13.2	4.14	7	0
S06	76.2	13.2	4.14	7	0
S07	76.2	13.2	4.14	7	0
S08_1	76.2	13.2	4.14	7	0
S08_2	76.2	13.2	4.14	7	0
S09	76.2	13.2	4.14	7	0

[JUNCTIONS]					
;;	Invert Elev.	Max. Depth	Init. Depth	Surcharge Depth	Ponded Area
200	111.136	2.764	0	0	0
201	111.343	2.537	0	0	0
202	111.456	2.444	0	0	0
203	111.608	2.542	0	0	0
204	111.698	2.352	0	0	0
205	111.876	2.254	0	0	0
206	112.417	2.303	0	0	0
207	113.284	1.966	0	0	0
208	112.565	1.935	0	0	0
210	112.16	2.12	0	0	0
211	111.81	2.24	0	0	0
212	111.42	2.7	0	0	0
213	112.824	1.496	0	0	0
215	112.24	2.26	0	0	0
216	111.324	2.506	0	0	0
217	113.462	1.498	0	0	0
218	112.736	1.264	0	0	0
219	111.302	2.474	0	0	0
CB03	113.104	1.146	0	0	0
CB05	114.004	1.056	0	0	0
CBE01	114.25	1.06	0	0	0
CBE04	113.9	1	0	0	0
CBT02	114.113	1.057	0	0	0
CBT03	113.784	1.056	0	0	0
CBT05	113.786	1.024	0	0	0
CBT06	113.68	1.04	0	0	0
CBT07	113.614	1.046	0	0	0
CBT08	113.516	1.164	0	0	0
CBT09	113.388	1.082	0	0	0
CBT10	113.276	1.074	0	0	0
CBT11	112.864	1.436	0	0	0
CBT12	112.886	1.394	0	0	0
CBT13	112.917	1.143	0	0	0
CBT14	112.945	1.075	0	0	0
INO7998	110.43	1.402	0	0	0
INO9003-MAJ	113.93	0.15	0	0	0
INO9004-MAJ	113.83	0.15	0	0	0
INO9005-MAJ	113.22	0.15	0	0	0
INO9006-MAJ	113.22	0.15	0	0	0
INO9009-MAJ	112.75	0.15	0	0	0

INO9010-MAJ	112.75	0.15	0	0	0
INO9011-MAJ	112.21	0.15	0	0	0
INO9012-MAJ	112.21	0.15	0	0	0
INO9013-MAJ	111.78	0.15	0	0	0
INO9014-MAJ	111.41	0.15	0	0	0
INO9015-MAJ	111.41	0.15	0	0	0
INO9017-MAJ	111.56	0.15	0	0	0
INO9018-MAJ	111.56	0.15	0	0	0
INO9019-MAJ	111.33	0.15	0	0	0
INO9020-MAJ	111.33	0.15	0	0	0
INO9021-MAJ	111	0.15	0	0	0
INO9022-MAJ	113.94	0.15	0	0	0
INO9023-MAJ	113.75	0.15	0	0	0
INO9024-MAJ	113.15	0.15	0	0	0
INO9025-MAJ	113.13	0.15	0	0	0
INO9026-MAJ	112.66	0.15	0	0	0
INO9027-MAJ	112.68	0.15	0	0	0
INO9028-MAJ	112.36	0.15	0	0	0
INO9029-MAJ	112.37	0.15	0	0	0
INO9030-MAJ	111.97	0.15	0	0	0
INO9031-MAJ	111.97	0.15	0	0	0
INO9032-MAJ	111.62	0.15	0	0	0
INO9033-MAJ	111.62	0.15	0	0	0
INO9034-MAJ	111.27	0.15	0	0	0
INO9035-MAJ	111.27	0.15	0	0	0
IN45566	109.82	1.395	0	0	0
;RYCB					
IN45569	111.61	1.397	0	0	0
IN45570	111.7	1.404	0	0	0
IN45572	111.51	1.402	0	0	0
IN45573	112.76	1.396	0	0	0
IN45574	111.3	0.3	0	0	0
IN45575	112.17	1.402	0	0	0
IN45577	111.28	1.402	0	0	0
IN45587	112.44	1.405	0	0	0
IN45588	112.52	1.402	0	0	0
IN45589	111.85	1.396	0	0	0
IN45590	111.58	1.402	0	0	0
J1	111.77	0.15	0	0	0
J2	111.2	0.15	0	0	0
MHST09001	111.29	1.851	0	0	0
MHST09002	111.25	1.966	0	0	0
MHST09003	111.15	2.686	0	0	0
MHST09004	111.02	3.007	0	0	0
MHST09005	110.43	3.073	0	0	0
MHST09006	110.07	2.864	0	0	0
MHST09007	109.61	3.224	0	0	0
MHST09008	109.27	3.155	0	0	0
MHST09009	109.21	3.069	0	0	0
MHST09010	108.65	3.324	0	0	0
MHST09011	108.29	3.382	0	0	0
MHST09013	108.16	3.426	0	0	0
MHST09014	108.38	3.116	0	0	0

MHST09015	108.53	3.268	0	0	0
MHST09016	110.98	3.202	0	0	0
MHST09017	110.75	3.348	0	0	0
MHST09018	110.66	3.211	0	0	0
MHST09019	110.38	2.899	0	0	0
MHST09020	109.94	2.991	0	0	0
MHST09021	109.05	3.481	0	0	0
MHST09022	108.93	3.336	0	0	0
MHST09023	108.79	3.014	0	0	0
MHST09024	108.86	2.531	0	0	0
[OUTFALLS]					
;;	Invert	Outfall	Stage/Table	Tide	
;;:Name	Elev.	Type	Time Series	Gate Route To	
OF-CREEK	107.5	FREE		NO	
OF-HAZELDEAN	112.83	FREE		NO	
[STORAGE]					
;;	Invert	Max.	Init.	Storage	Curve
;;:Name	Elev.	Depth	Depth	Curve	Params
;;					
CB01	112.4	1.4	0	TABULAR	CB01-STOR
CB06	112.5	1.4	0	TABULAR	CB06-STOR
CHAMBERS-1	111.516	2.584	0	TABULAR	STORAGE-1
CHAMBERS-2	112.296	2.204	0	TABULAR	STORAGE-2
IN09003	112.53	1.4	0	FUNCTIONAL	0 0
IN09004	112.43	1.55	0	TABULAR	IN09004-STOR
IN09005	111.82	1.4	0	FUNCTIONAL	0 0
IN09006	111.82	1.4	0	FUNCTIONAL	0 0
IN09007	111.58	1.55	0	TABULAR	IN09007-STOR
IN09008	111.58	1.55	0	TABULAR	IN09008-STOR
IN09009	111.35	1.4	0	FUNCTIONAL	0 0
IN09010	111.35	1.4	0	FUNCTIONAL	1000 0
IN09011	110.81	1.4	0	FUNCTIONAL	0 0
IN09012	110.81	1.4	0	FUNCTIONAL	0 0
IN09013	110.38	1.4	0	FUNCTIONAL	0 0
IN09014	110.01	1.4	0	FUNCTIONAL	0 0
IN09015	110.01	1.4	0	FUNCTIONAL	0 0
IN09016	109.85	1.55	0	TABULAR	IN09016-STOR
IN09017	110.16	1.4	0	FUNCTIONAL	0 0
IN09018	110.16	1.4	0	FUNCTIONAL	0 0
IN09019	109.93	1.4	0	FUNCTIONAL	0 0
IN09020	109.93	1.4	0	FUNCTIONAL	0 0
IN09021	109.6	1.4	0	FUNCTIONAL	0 0
IN09022	112.54	1.4	0	FUNCTIONAL	0 0
IN09023	112.35	1.4	0	FUNCTIONAL	0 0
IN09024	111.75	1.4	0	FUNCTIONAL	0 0
IN09025	111.73	1.4	0	FUNCTIONAL	0 0
IN09026	111.26	1.4	0	FUNCTIONAL	0 0
IN09027	111.28	1.4	0	FUNCTIONAL	0 0
IN09028	110.96	1.4	0	FUNCTIONAL	0 0
IN09029	110.97	1.4	0	FUNCTIONAL	0 0

IN09030	110.57	1.4	0	FUNCTIONAL	0 0	0.36	0	0
IN09031	110.57	1.4	0	FUNCTIONAL	0 0	0.36	0	0
IN09032	110.22	1.4	0	FUNCTIONAL	0 0	0.36	0	0
IN09033	110.22	1.4	0	FUNCTIONAL	0 0	0.36	0	0
IN09034	109.87	1.4	0	FUNCTIONAL	0 0	0.36	0	0
IN09035	109.87	1.4	0	FUNCTIONAL	0 0	0.36	0	0
IN103407	111.64	1.61	0	TABULAR	IN103407-STOR	0	0	0
MHST09012	107.61	3.518	0	FUNCTIONAL	0 0	1.13	0	0
[CONDUITS]								
;;	Inlet	Outlet		Manning	Inlet	Outlet	Init.	Max.
;;:Name	Node	Node	Length	N	Offset	Offset	Flow	Flow
;;								
C01	207	206	15.798	0.013	113	112.47	0	0
C02	206	205	46.769	0.013	112.3	112.02	0	0
C03	205	204	44.476	0.013	111.88	111.73	0	0
C04	204	203	8.526	0.013	111.7	111.67	0	0
C05	203	202	35.069	0.013	111.61	111.49	0	0
C06	202	201	11.458	0.013	111.46	111.42	0	0
C07	216	219	10.264	0.013	111.324	111.302	0	0
C08	CB03	208	14.991	0.01	113.104	112.565	0	0
C09	208	CHAMBERS-2	1.5	0.013	112.565	112.55	0	0
C1	IN45587	MHST09004	40	0.013	112.44	112.04	0	0
C10	219	200	10.729	0.013	111.302	111.2	0	0
C11	210	211	15.342	0.013	112.28	112.12	0	0
C12	CB01	211	16.041	0.013	112.4	112.19	0	0
C13	IN07998	MHST09011	10	0.013	110.43	110.33	0	0
C14	217	CHAMBERS-2	7.6	0.013	113.462	112.91	0	0
C15	CHAMBERS-1	212	23.7	0.013	111.72	111.68	0	0
C16	211	CHAMBERS-1	2.5	0.013	111.79	111.77	0	0
C17	CBE01	CBT02	22.237	0.013	114.25	114.113	0	0
C18	CBT02	CB05	22.237	0.013	114.113	114.004	0	0
C19	CB05	CBT03	35.089	0.013	114.004	113.784	0	0
C2	IN45588	MHST09005	116.338	0.013	112.52	112.02	0	0
C20	CBT03	217	22.884	0.013	113.784	113.51	0	0
C21	218	208	15.162	0.013	112.736	112.595	0	0
C22	IN45573	MHST09016	40	0.013	112.76	112.26	0	0
C23	CB06	210	11.287	0.013	112.5	112.31	0	0
C24	CHAMBERS-2	215	1.5	0.013	112.48	112.44	0	0
C25	201	216	6.436	0.013	111.356	111.32	0	0
C26	IN45574	MHST09017	40	0.013	111.3	111	0	0
C27	IN45566	MHST09024	10	0.013	109.82	109.72	0	0
C28	CBE04	CBT05	11.405	0.013	113.9	113.786	0	0
C29	CBT05	CBT06	10.537	0.013	113.786	113.68	0	0
C3	IN45589	MHST09007	40	0.013	111.85	111.45	0	0
C30	CBT06	CBT07	6.663	0.013	113.681	113.614	0	0
C31	CBT07	CBT08	9.787	0.013	113.614	113.516	0	0
C32	CBT08	CBT09	12.746	0.013	113.516	113.388	0	0
C33	CBT09	CBT10	11.17	0.013	113.388	113.276	0	0
C34	CBT10	213	3.295	0.013	113.276	113.243	0	0
C35	CBT11	213	3.295	0.013	112.874	112.864	0	0
C36	CBT12	CBT11	9.526	0.013	112.893	112.864	0	0
C37	CBT13	CBT12	12.745	0.013	112.925	112.886	0	0

C38	CBT14	CBT13	12.745	0.013	112.955	112.917	0	0
C39	IN103407	OF-HAZELDEAN	40.346	0.013	113.04	112.83	0	0
C4	IN45590	MHST09007	40	0.013	111.58	111.08	0	0
C40	213	218	29.265	0.013	112.824	112.736	0	0
C5	IN45575	MHST09019	40	0.013	112.17	111.77	0	0
C6	IN45570	MHST09020	40	0.013	111.7	111.3	0	0
C7	IN45569	MHST09021	40	0.013	111.61	111.41	0	0
C8	IN45572	MHST09021	40	0.013	111.51	111.11	0	0
C9	IN45577	MHST09022	40	0.013	111.28	110.88	0	0
C98	CHAMBERS-1	212	26.513	0.013	111.516	111.42	0	0
C99	CHAMBERS-2	215	28.637	0.013	112.296	112.27	0	0
OF1	IN09016	MHST09012	17.899	0.013	111.4	111.128	0	0
R01	IN09004-MAJ	IN09006-MAJ	92.678	0.013	113.83	113.22	0	0
R02	IN09006-MAJ	IN09007	79.588	0.013	113.22	113.13	0	0
R03	IN09005-MAJ	IN09008	79.205	0.013	113.22	112.98	0	0
R04	IN09007	IN09010-MAJ	71.554	0.013	113.13	112.75	0	0
R05	IN09008	IN09009-MAJ	72.205	0.013	112.98	112.75	0	0
R06	IN09010-MAJ	IN09012-MAJ	101.975	0.013	112.75	112.21	0	0
R07	IN09009-MAJ	IN09011-MAJ	106.231	0.013	112.75	112.21	0	0
R08	IN09012-MAJ	J1	98.186	0.013	112.21	111.77	0	0
R09	IN09033-MAJ	J1	13.729	0.013	111.62	111.77	0	0
R10	IN09032-MAJ	J1	24.181	0.013	0	111.62	0	0
R11	IN09011-MAJ	IN09013-MAJ	91.997	0.013	112.21	111.78	0	0
R12	IN09013-MAJ	IN09015-MAJ	71.755	0.013	111.78	111.41	0	0
R13	IN09015-MAJ	MHST09012	64.056	0.013	111.41	111.128	0	0
R14	IN09014-MAJ	IN09016	54.483	0.013	111.41	111.25	0	0
R15	J1	IN09014-MAJ	59.615	0.013	111.77	111.41	0	0
R16	IN09035-MAJ	J2	17.745	0.013	0	0	0	0
R17	IN09034-MAJ	J2	26.122	0.013	0	0	0	0
R18	IN09021-MAJ	IN09020-MAJ	30.532	0.013	0	0	0	0
R19	J2	IN09019-MAJ	27.476	0.013	0	0	0	0
R20	IN09020-MAJ	IN09018-MAJ	80.609	0.013	0	111.56	0	0
R21	IN09019-MAJ	IN09017-MAJ	81.078	0.013	0	111.56	0	0
R22	IN09018-MAJ	MHST09012	83.592	0.013	111.56	111.128	0	0
R23	IN09017-MAJ	IN09016	67.772	0.013	111.56	111.25	0	0
R24	IN09003-MAJ	IN103407	71.254	0.013	113.93	113.04	0	0
R25	IN09023-MAJ	IN09024-MAJ	81.428	0.013	113.75	113.15	0	0
R26	IN09022-MAJ	IN09025-MAJ	86.482	0.013	113.94	113.13	0	0
R27	IN09025-MAJ	IN09027-MAJ	86.008	0.013	113.13	112.68	0	0
R28	IN09024-MAJ	IN09026-MAJ	85.805	0.013	113.15	112.66	0	0
R29	IN09027-MAJ	IN09028-MAJ	61.833	0.013	112.68	112.36	0	0
R30	IN09026-MAJ	IN09029-MAJ	68.091	0.013	112.66	112.37	0	0
R31	IN09029-MAJ	IN09030-MAJ	72.254	0.013	112.37	111.97	0	0
R32	IN09028-MAJ	IN09034-MAJ	88.109	0.013	112.36	111.27	0	0
R33	IN09030-MAJ	IN09032-MAJ	67.283	0.013	111.97	111.62	0	0
R34	IN09031-MAJ	IN09033-MAJ	69.891	0.013	111.97	111.62	0	0
STM04620	MHST09014	MHST09013	76.347	0.013	108.38	108.22	0	0
STM04621	MHST09013	MHST09012	77.994	0.013	108.16	108	0	0
STM07857	MHST09005	MHST09006	90.117	0.013	110.43	110.07	0	0
STM07870	MHST09015	MHST09014	51.716	0.013	108.53	108.45	0	0
STM07871	MHST09012	OF-CREEK	44.59	0.013	107.61	107.5	0	0
STM07872	MHST09024	MHST09015	65.567	0.013	108.86	108.61	0	0
STM07873	MHST09009	MHST09010	81.53	0.013	109.21	108.93	0	0

STM07874	MHST09001	MHST09002	10.425	0.013	111.29	111.25	0	0
STM07875	MHST09006	MHST09007	89.989	0.013	110.07	109.71	0	0
STM07876	MHST09016	MHST09017	39.458	0.013	110.98	110.83	0	0
STM45150	MHST09017	MHST09018	13.481	0.013	110.75	110.7	0	0
STM45151	MHST09018	MHST09019	52.811	0.013	110.66	110.45	0	0
STM45152	MHST09019	MHST09020	90.099	0.013	110.38	110.02	0	0
STM45153	MHST09020	MHST09021	89.396	0.013	109.94	109.13	0	0
STM45154	MHST09021	MHST09022	58.932	0.013	109.05	108.93	0	0
STM45155	MHST09022	MHST09023	56.802	0.013	108.93	108.79	0	0
STM45156	MHST09023	MHST09010	41.513	0.013	108.79	108.66	0	0
STM45159	MHST09010	MHST09011	75.08	0.013	108.65	108.29	0	0
STM45160	MHST09011	MHST09012	58.178	0.013	108.29	107.99	0	0
STM45161	MHST09007	MHST09008	88.113	0.013	109.61	109.3	0	0
STM45162	MHST09008	MHST09009	12.683	0.013	109.27	109.25	0	0
STM45163	MHST09002	MHST09003	36.553	0.013	111.25	111.15	0	0
STM45164_1	MHST09003	200	4.698	0.013	111.15	111.136	0	0
STM45164_2	200	MHST09004	11.906	0.013	111.136	111.1	0	0
STM45165	MHST09004	MHST09005	82.915	0.013	111.02	110.51	0	0

[OUTLETS]								
;	Inlet Node	Outlet Node	Outflow Height	Outlet Type	Qcoeff/ QTable	Flap Qexpon	Gate	
;	;	;	;	;	;	;	;	;
212-ICD	212	216	111.42	TABULAR/DEPTH	IPEX-MHF-TYPEA			NO
215-ICD	215	205	111.24	TABULAR/DEPTH	IPEX-MHF-TYPEA			NO
IN09003-ICD	IN09003	MHST09003	112.53	TABULAR/DEPTH	IPEX-MHF-TYPEA			NO
IN09003-INC	IN09003-MAJ	IN09003	113.93	TABULAR/DEPTH	CB-INC-1%			NO
IN09004-ICD	IN09004	MHST09004	112.45	TABULAR/DEPTH	IPEX-MHF-TYPEA			NO
IN09004-INC	IN09004-MAJ	IN09004	113.83	TABULAR/DEPTH	CB-INC-1%			NO
IN09005-ICD	IN09005	MHST09005	111.82	TABULAR/DEPTH	IPEX-MHF-TYPEA			NO
IN09005-INC	IN09005-MAJ	IN09005	113.22	TABULAR/DEPTH	CB-INC-1%			NO
IN09006-ICD	IN09006	MHST09005	111.82	TABULAR/DEPTH	IPEX-MHF-TYPEA			NO
IN09006-INC	IN09006-MAJ	IN09006	113.22	TABULAR/DEPTH	CB-INC-1%			NO
IN09007-ICD	IN09007	MHST09006	111.58	TABULAR/DEPTH	IPEX-MHF-TYPEA			NO
IN09008-ICD	IN09008	MHST09006	111.58	TABULAR/DEPTH	IPEX-MHF-TYPEA			NO
IN09009-ICD	IN09009	MHST09007	111.35	TABULAR/DEPTH	IPEX-MHF-TYPEA			NO
IN09009-INC	IN09009-MAJ	IN09009	112.72	TABULAR/DEPTH	CB-INC-1%			NO
IN09010-ICD	IN09010	MHST09007	111.32	TABULAR/DEPTH	IPEX-MHF-TYPEA			NO
IN09010-INC	IN09010-MAJ	IN09010	112.75	TABULAR/DEPTH	CB-INC-1%			NO
IN09011-ICD	IN09011	MHST09008	110.87	TABULAR/DEPTH	IPEX-MHF-TYPEA			NO
IN09011-INC	IN09011-MAJ	IN09011	112.21	TABULAR/DEPTH	CB-INC-1%			NO
IN09012-ICD	IN09012	MHST09008	110.81	TABULAR/DEPTH	IPEX-MHF-TYPEA			NO
IN09012-INC	IN09012-MAJ	IN09012	112.21	TABULAR/DEPTH	CB-INC-1%			NO
IN09013-ICD	IN09013	MHST09010	110.38	TABULAR/DEPTH	IPEX-MHF-TYPEA			NO
IN09013-INC	IN09013-MAJ	IN09013	111.78	TABULAR/DEPTH	CB-INC-1%			NO
IN09014-ICD	IN09014	MHST09011	110.01	TABULAR/DEPTH	IPEX-MHF-TYPEA			NO
IN09014-INC	IN09014-MAJ	IN09014	111.41	TABULAR/DEPTH	CB-INC-1%			NO
IN09015-ICD	IN09015	MHST09011	110.01	TABULAR/DEPTH	IPEX-MHF-TYPEA			NO
IN09015-INC	IN09015-MAJ	IN09015	56.848	TABULAR/DEPTH	CB-INC-1%			NO
IN09016-ICD	IN09016	MHST09013	109.85	TABULAR/DEPTH	IPEX-MHF-TYPEA			NO
IN09017-ICD	IN09017	MHST09013	110.16	TABULAR/DEPTH	IPEX-MHF-TYPEA			NO
IN09017-INC	IN09017-MAJ	IN09017	111.56	TABULAR/DEPTH	CB-INC-1%			NO
IN09018-ICD	IN09018	MHST09013	110.16	TABULAR/DEPTH	IPEX-MHF-TYPEA			NO

INO9018-INC	INO9018-MAJ	INO9018	111.56	TABULAR/DEPTH	CB-INC-1%	NO
INO9019-ICD	INO9019	MHST09014	109.93	TABULAR/DEPTH	IPEX-MHF-TYPEA	NO
INO9019-INC	INO9019-MAJ	INO9019	111.33	TABULAR/DEPTH	CB-INC-1%	NO
INO9020-ICD	INO9020	MHST09014	109.93	TABULAR/DEPTH	IPEX-MHF-TYPEA	NO
INO9020-INC	INO9020-MAJ	INO9020	111.33	TABULAR/DEPTH	CB-INC-1%	NO
INO9021-ICD	INO9021	MHST09015	109.6	TABULAR/DEPTH	IPEX-MHF-TYPEB	NO
INO9021-INC	INO9021-MAJ	INO9021	111	TABULAR/DEPTH	CB-INC-1%	NO
INO9022-ICD	INO9022	MHST09017	112.54	TABULAR/DEPTH	IPEX-MHF-TYPEA	NO
INO9022-INC	INO9022-MAJ	INO9022	113.94	TABULAR/DEPTH	CB-INC-1%	NO
INO9023-ICD	INO9023	MHST09017	112.35	TABULAR/DEPTH	IPEX-MHF-TYPEA	NO
INO9023-INC	INO9023-MAJ	INO9023	113.75	TABULAR/DEPTH	CB-INC-1%	NO
INO9024-ICD	INO9024	MHST09019	111.75	TABULAR/DEPTH	IPEX-MHF-TYPEA	NO
INO9024-INC	INO9024-MAJ	INO9024	113.15	TABULAR/DEPTH	CB-INC-1%	NO
INO9025-ICD	INO9025	MHST09019	111.73	TABULAR/DEPTH	IPEX-MHF-TYPEA	NO
INO9025-INC	INO9025-MAJ	INO9025	113.13	TABULAR/DEPTH	CB-INC-1%	NO
INO9026-ICD	INO9026	MHST09020	111.26	TABULAR/DEPTH	IPEX-MHF-TYPEA	NO
INO9026-INC	INO9026-MAJ	INO9026	112.66	TABULAR/DEPTH	CB-INC-1%	NO
INO9027-ICD	INO9027	MHST09020	111.28	TABULAR/DEPTH	IPEX-MHF-TYPEA	NO
INO9027-INC	INO9027-MAJ	INO9027	112.68	TABULAR/DEPTH	CB-INC-1%	NO
INO9028-ICD	INO9028	MHST09021	110.96	TABULAR/DEPTH	IPEX-MHF-TYPEA	NO
INO9028-INC	INO9028-MAJ	INO9028	112.36	TABULAR/DEPTH	CB-INC-1%	NO
INO9029-ICD	INO9029	MHST09021	110.97	TABULAR/DEPTH	IPEX-MHF-TYPEA	NO
INO9029-INC	INO9029-MAJ	INO9029	112.37	TABULAR/DEPTH	CB-INC-1%	NO
INO9030-ICD	INO9030	MHST09022	110.57	TABULAR/DEPTH	IPEX-MHF-TYPEA	NO
INO9030-INC	INO9030-MAJ	INO9030	111.97	TABULAR/DEPTH	CB-INC-1%	NO
INO9031-ICD	INO9031	MHST09022	110.57	TABULAR/DEPTH	IPEX-MHF-TYPEA	NO
INO9031-INC	INO9031-MAJ	INO9031	111.97	TABULAR/DEPTH	CB-INC-1%	NO
INO9032-ICD	INO9032	MHST09023	110.22	TABULAR/DEPTH	IPEX-MHF-TYPEA	NO
INO9032-INC	INO9032-MAJ	INO9032	111.62	TABULAR/DEPTH	CB-INC-1%	NO
INO9033-ICD	INO9033	MHST09023	110.22	TABULAR/DEPTH	IPEX-MHF-TYPEA	NO
INO9033-INC	INO9033-MAJ	INO9033	111.62	TABULAR/DEPTH	CB-INC-1%	NO
INO9034-ICD	INO9034	MHST09024	109.87	TABULAR/DEPTH	IPEX-MHF-TYPEB	NO
INO9034-INC	INO9034-MAJ	INO9034	111.27	TABULAR/DEPTH	CB-INC-1%	NO
INO9035-ICD	INO9035	MHST09024	109.87	TABULAR/DEPTH	IPEX-MHF-TYPEB	NO
INO9035-INC	INO9035-MAJ	INO9035	111.27	TABULAR/DEPTH	CB-INC-1%	NO
IN103407-ICD	IN103407	MHST09001	111.64	TABULAR/DEPTH	IPEX-MHF-TYPEB	NO

[XSECTIONS]	;	Link	Shape	Geom1	Geom2	Geom3	Geom4	Barrels
;	;	C01	CIRCULAR	0.25	0	0	0	1
;	;	C02	CIRCULAR	0.25	0	0	0	1
;	;	C03	CIRCULAR	0.375	0	0	0	1
;	;	C04	CIRCULAR	0.375	0	0	0	1
;	;	C05	CIRCULAR	0.375	0	0	0	1
;	;	C06	CIRCULAR	0.375	0	0	0	1
;	;	C07	CIRCULAR	0.375	0	0	0	1
;	;	C08	CIRCULAR	0.3	0	0	0	1
;	;	C09	CIRCULAR	0.6	0	0	0	1
;	;	C1	CIRCULAR	0.2	0	0	0	1
;	;	C10	CIRCULAR	0.375	0	0	0	1
;	;	C11	CIRCULAR	0.3	0	0	0	1
;	;	C12	CIRCULAR	0.3	0	0	0	1

C13	CIRCULAR	0.2	0	0	0	0	1
C14	CIRCULAR	0.3	0	0	0	0	1
C15	CIRCULAR	0.375	0	0	0	0	1
C16	CIRCULAR	0.6	0	0	0	0	1
C17	CIRCULAR	0.25	0	0	0	0	1
C18	CIRCULAR	0.25	0	0	0	0	1
C19	CIRCULAR	0.25	0	0	0	0	1
C2	CIRCULAR	0.2	0	0	0	0	1
C20	CIRCULAR	0.25	0	0	0	0	1
C21	CIRCULAR	0.3	0	0	0	0	1
C22	CIRCULAR	0.2	0	0	0	0	1
C23	CIRCULAR	0.3	0	0	0	0	1
C24	CIRCULAR	0.375	0	0	0	0	1
C25	CIRCULAR	0.375	0	0	0	0	1
C26	CIRCULAR	0.2	0	0	0	0	1
C27	CIRCULAR	0.2	0	0	0	0	1
C28	CIRCULAR	0.25	0	0	0	0	1
C29	CIRCULAR	0.25	0	0	0	0	1
C3	CIRCULAR	0.2	0	0	0	0	1
C30	CIRCULAR	0.25	0	0	0	0	1
C31	CIRCULAR	0.25	0	0	0	0	1
C32	CIRCULAR	0.25	0	0	0	0	1
C33	CIRCULAR	0.25	0	0	0	0	1
C34	CIRCULAR	0.25	0	0	0	0	1
C35	CIRCULAR	0.25	0	0	0	0	1
C36	CIRCULAR	0.25	0	0	0	0	1
C37	CIRCULAR	0.25	0	0	0	0	1
C38	CIRCULAR	0.25	0	0	0	0	1
C39	TRAPEZOIDAL	0.3	1	3	3	3	1
C4	CIRCULAR	0.2	0	0	0	0	1
C40	CIRCULAR	0.3	0	0	0	0	1
C5	CIRCULAR	0.2	0	0	0	0	1
C6	CIRCULAR	0.2	0	0	0	0	1
C7	CIRCULAR	0.2	0	0	0	0	1
C8	CIRCULAR	0.2	0	0	0	0	1
C9	CIRCULAR	0.2	0	0	0	0	1
C98	CIRCULAR	0.1	0	0	0	0	1
C99	CIRCULAR	0.1	0	0	0	0	1
OF1	IRREGULAR	Half_Street_4.25m	0	0	0	0	1
R01	IRREGULAR	Half_Street_4.25m	0	0	0	0	1
R02	IRREGULAR	Half_Street_4.25m	0	0	0	0	1
R03	IRREGULAR	Half_Street_4.25m	0	0	0	0	1
R04	IRREGULAR	Half_Street_4.25m	0	0	0	0	1
R05	IRREGULAR	Half_Street_4.25m	0	0	0	0	1
R06	IRREGULAR	Half_Street_4.25m	0	0	0	0	1
R07	IRREGULAR	Half_Street_4.25m	0	0	0	0	1
R08	IRREGULAR	Half_Street_4.25m	0	0	0	0	1
R09	IRREGULAR	Half_Street_4.25m	0	0	0	0	1
R10	IRREGULAR	Half_Street_4.25m	0	0	0	0	1
R11	IRREGULAR	Half_Street_4.25m	0	0	0	0	1
R12	IRREGULAR	Half_Street_4.25m	0	0	0	0	1
R13	IRREGULAR	Half_Street_4.25m	0	0	0	0	1
R14	IRREGULAR	Half_Street_4.25m	0	0	0	0	1

R15	IRREGULAR	Half_Street_4.25m 0	0	0	1
R16	IRREGULAR	Half_Street_4.25m 0	0	0	1
R17	IRREGULAR	Half_Street_4.25m 0	0	0	1
R18	IRREGULAR	Half_Street_4.25m 0	0	0	1
R19	IRREGULAR	Half_Street_4.25m 0	0	0	1
R20	IRREGULAR	Half_Street_4.25m 0	0	0	1
R21	IRREGULAR	Half_Street_4.25m 0	0	0	1
R22	IRREGULAR	Half_Street_4.25m 0	0	0	1
R23	IRREGULAR	Half_Street_4.25m 0	0	0	1
R24	IRREGULAR	Half_Street_4.25m 0	0	0	1
R25	IRREGULAR	Half_Street_4.25m 0	0	0	1
R26	IRREGULAR	Half_Street_4.25m 0	0	0	1
R27	IRREGULAR	Half_Street_4.25m 0	0	0	1
R28	IRREGULAR	Half_Street_4.25m 0	0	0	1
R29	IRREGULAR	Half_Street_4.25m 0	0	0	1
R30	IRREGULAR	Half_Street_4.25m 0	0	0	1
R31	IRREGULAR	Half_Street_4.25m 0	0	0	1
R32	IRREGULAR	Half_Street_4.25m 0	0	0	1
R33	IRREGULAR	Half_Street_4.25m 0	0	0	1
R34	IRREGULAR	Half_Street_4.25m 0	0	0	1
STM04620	CIRCULAR	0.525	0	0	1
STM04621	CIRCULAR	0.6	0	0	1
STM07857	CIRCULAR	0.525	0	0	1
STM07870	CIRCULAR	0.45	0	0	1
STM07871	CIRCULAR	0.9	0	0	1
STM07872	CIRCULAR	0.375	0	0	1
STM07873	CIRCULAR	0.6	0	0	1
STM07874	CIRCULAR	0.375	0	0	1
STM07875	CIRCULAR	0.525	0	0	1
STM07876	CIRCULAR	0.3	0	0	1
STM45150	CIRCULAR	0.375	0	0	1
STM45151	CIRCULAR	0.375	0	0	1
STM45152	CIRCULAR	0.45	0	0	1
STM45153	CIRCULAR	0.525	0	0	1
STM45154	CIRCULAR	0.6	0	0	1
STM45155	CIRCULAR	0.6	0	0	1
STM45156	CIRCULAR	0.6	0	0	1
STM45159	CIRCULAR	0.75	0	0	1
STM45160	CIRCULAR	0.75	0	0	1
STM45161	CIRCULAR	0.6	0	0	1
STM45162	CIRCULAR	0.6	0	0	1
STM45163	CIRCULAR	0.375	0	0	1
STM45164_1	CIRCULAR	0.375	0	0	1
STM45164_2	CIRCULAR	0.375	0	0	1
STM45165	CIRCULAR	0.45	0	0	1

[TRANSECTS]

;Half street, width = 4.25m, curb = 0.075m , cross-slope = 0.03m/m, bank-slope = 0.03m/m, bank-height = 0.2m.
NC 0.03 0.03 0.013
X1 Half_Street_4.25m 4 0.0 4.25 0.0 0.0 0.0 0.0 0.0
GR 0.13 0 4.25 0.08 4.25 0.2 8.42

[LOSSES]
;Link Inlet Outlet Average Flap Gate SeepageRate

[INFLOWS]
;
;Node Parameter Time Series Param Units Scale Baseline Baseline

203 FLOW "" FLOW 1.0 1 1.91
204 FLOW "" FLOW 1.0 1 0.85
205 FLOW "" FLOW 1.0 1 0.85
206 FLOW "" FLOW 1.0 1 0.85
207 FLOW "" FLOW 1.0 1 0.64
[CURVES]
;Name Type X-Value Y-Value

;Inlet Capacity for Standard CB
;with mountable curb & gutter
;3% Crossfall & 1.0% Gutter Slope
;1% Gutter Grade
CB-INC-1% Rating 0.006 0
CB-INC-1% 0.026 7
CB-INC-1% 0.033 12
CB-INC-1% 0.06 15
CB-INC-1% 0.078 34
CB-INC-1% 0.084 47
CB-INC-1% 0.09 51
CB-INC-1% 0.095 54
CB-INC-1% 0.1 55
;Inlet Capacity for Standard CB
;with mountable curb & gutter
;3% Crossfall & 2.0% Gutter Slope
;Inlet Capacity for Standard CB
;with mountable curb & gutter
;3% Crossfall & 3.0% Gutter Slope
;IPEX TEMPEST MHF TYPE A
IPEX-MHF-TYPEA Rating 0 0
IPEX-MHF-TYPEA 0.2 8.088
IPEX-MHF-TYPEA 0.4 11.438
IPEX-MHF-TYPEA 0.6 14.008
IPEX-MHF-TYPEA 0.8 16.175
IPEX-MHF-TYPEA 1 18.085
IPEX-MHF-TYPEA 1.2 19.811
IPEX-MHF-TYPEA 1.4 21.398
IPEX-MHF-TYPEA 1.6 22.875
IPEX-MHF-TYPEA 1.8 24.263
IPEX-MHF-TYPEA 2 25.575
IPEX-MHF-TYPEA 2.2 26.824
IPEX-MHF-TYPEA 2.4 28.017
IPEX-MHF-TYPEA 2.6 29.16
IPEX-MHF-TYPEA 2.8 30.261

IPEX-MHF-TYPEA	3	31.323
IPEX-MHF-TYPEA	3.2	32.351
IPEX-MHF-TYPEA	3.4	33.346
IPEX-MHF-TYPEA	3.6	34.313
IPEX-MHF-TYPEA	3.8	35.253
; IPEX TEMPEST MHF TYPE B		
IPEX-MHF-TYPEB	Rating	0
IPEX-MHF-TYPEB	0.2	11.478
IPEX-MHF-TYPEB	0.4	16.233
IPEX-MHF-TYPEB	0.6	19.881
IPEX-MHF-TYPEB	0.8	22.957
IPEX-MHF-TYPEB	1	25.666
IPEX-MHF-TYPEB	1.2	28.116
IPEX-MHF-TYPEB	1.4	30.369
IPEX-MHF-TYPEB	1.6	32.466
IPEX-MHF-TYPEB	1.8	34.435
IPEX-MHF-TYPEB	2	36.298
IPEX-MHF-TYPEB	2.2	38.069
IPEX-MHF-TYPEB	2.4	39.762
IPEX-MHF-TYPEB	2.6	41.386
IPEX-MHF-TYPEB	2.8	42.948
IPEX-MHF-TYPEB	3	44.455
IPEX-MHF-TYPEB	3.2	45.913
IPEX-MHF-TYPEB	3.4	47.326
IPEX-MHF-TYPEB	3.6	48.698
IPEX-MHF-TYPEB	3.8	50.033
; IPEX TEMPEST MHF TYPE C		
IPEX-MHF-TYPEC	Rating	0
IPEX-MHF-TYPEC	0.2	14.965
IPEX-MHF-TYPEC	0.4	21.163
IPEX-MHF-TYPEC	0.6	25.92
IPEX-MHF-TYPEC	0.8	29.93
IPEX-MHF-TYPEC	1	33.462
IPEX-MHF-TYPEC	1.2	36.656
IPEX-MHF-TYPEC	1.4	39.593
IPEX-MHF-TYPEC	1.6	42.327
IPEX-MHF-TYPEC	1.8	44.895
IPEX-MHF-TYPEC	2	47.323
IPEX-MHF-TYPEC	2.2	49.633
IPEX-MHF-TYPEC	2.4	51.84
IPEX-MHF-TYPEC	2.6	53.957
IPEX-MHF-TYPEC	2.8	55.993
IPEX-MHF-TYPEC	3	57.959
IPEX-MHF-TYPEC	3.2	59.859
IPEX-MHF-TYPEC	3.4	61.702
IPEX-MHF-TYPEC	3.6	63.49
IPEX-MHF-TYPEC	3.8	65.23
; IPEX TEMPEST MHF TYPE D		
IPEX-MHF-TYPED	Rating	0
IPEX-MHF-TYPED	0.2	21.883

IPEX-MHF-TYPED	0.4	30.948
IPEX-MHF-TYPED	0.6	37.903
IPEX-MHF-TYPED	0.8	43.766
IPEX-MHF-TYPED	1	48.932
IPEX-MHF-TYPED	1.2	53.603
IPEX-MHF-TYPED	1.4	57.898
IPEX-MHF-TYPED	1.6	61.895
IPEX-MHF-TYPED	1.8	65.65
IPEX-MHF-TYPED	2	69.201
IPEX-MHF-TYPED	2.2	72.578
IPEX-MHF-TYPED	2.4	75.806
IPEX-MHF-TYPED	2.6	78.901
IPEX-MHF-TYPED	2.8	81.879
IPEX-MHF-TYPED	3	84.753
IPEX-MHF-TYPED	3.2	87.533
IPEX-MHF-TYPED	3.4	90.227
IPEX-MHF-TYPED	3.6	92.843
IPEX-MHF-TYPED	3.8	95.387
; IPEX TEMPEST MHF TYPE F		
IPEX-MHF-TYPEF	Rating	0
IPEX-MHF-TYPEF	0.2	28.951
IPEX-MHF-TYPEF	0.4	40.943
IPEX-MHF-TYPEF	0.6	50.145
IPEX-MHF-TYPEF	0.8	57.902
IPEX-MHF-TYPEF	1	64.737
IPEX-MHF-TYPEF	1.2	70.916
IPEX-MHF-TYPEF	1.4	76.598
IPEX-MHF-TYPEF	1.6	81.886
IPEX-MHF-TYPEF	1.8	86.854
IPEX-MHF-TYPEF	2	91.552
IPEX-MHF-TYPEF	2.2	96.02
IPEX-MHF-TYPEF	2.4	100.29
IPEX-MHF-TYPEF	2.6	104.385
IPEX-MHF-TYPEF	2.8	108.326
IPEX-MHF-TYPEF	3	112.128
IPEX-MHF-TYPEF	3.2	115.805
IPEX-MHF-TYPEF	3.4	119.369
IPEX-MHF-TYPEF	3.6	122.83
IPEX-MHF-TYPEF	3.8	126.195
; SURFACE PONDING		
; AT CB01		
CB01-STOR	Storage	0
CB01-STOR		1.4
CB01-STOR		1.6
CB01-STOR		1.6001
CB01-STOR		1.75
; SURFACE PONDING		
; AT CB06		
CB06-STOR	Storage	0
CB06-STOR		1.4

CB06-STOR	1.5	101
CB06-STOR	1.5001	0
CB06-STOR	1.65	0
;SURFACE PONDING AT		
;INLET IN09004		
IN09004-STOR	Storage	0 0
IN09004-STOR		1.4 0.36
IN09004-STOR		1.45 18
IN09004-STOR		1.4501 0
IN09004-STOR		1.6 0
;SURFACE POING AT		
;IN09007.		
;PONDING AREA # SP06A		
IN09007-STOR	Storage	0 0
IN09007-STOR		1.4 0.36
IN09007-STOR		1.5 173
IN09007-STOR		1.5001 0
IN09007-STOR		1.65 0
;SURFACE POING AT		
;IN09008.		
;PONDING AREA # SP06B		
IN09008-STOR	Storage	0 0
IN09008-STOR		1.4 0.36
IN09008-STOR		1.5 173
IN09008-STOR		1.5001 0
IN09008-STOR		1.65 0
;SURFACE PONDING AT		
;INLET 09016		
IN09016-STOR	Storage	0 0
IN09016-STOR		1.66 0.36
IN09016-STOR		1.96 41
IN09016-STOR		1.9601 0
IN09016-STOR		2.11 0
;SURFACE PONDING AT		
;INLET 103407		
IN103407-STOR	Storage	0 0
IN103407-STOR		1.4 1.131
IN103407-STOR		1.46 313
IN103407-STOR		1.4601 0
IN103407-STOR		1.61 0
;AREA-DEPTH FOR		
;MC-3500 CHAMBERS		
;22 chambers		
;10 end caps		
STORAGE-1	Storage	0 91
STORAGE-1		1.676 91
STORAGE-1		1.67601 0

STORAGE-1	3	0
;AREA-DEPTH FOR		
;MC-3500 CHAMBERS		
;22 chambers		
;10 end caps		
STORAGE-2	Storage	0 92.6
STORAGE-2		1.676 92.6
STORAGE-2		1.67601 0
STORAGE-2		3 0
[TIMESERIES]		
;Name Date Time Value		
;-----		
;Rainfall (mm/hr)		
Chicago_3h_100yr	09/26/2018 00:00:00	5.339
Chicago_3h_100yr	09/26/2018 00:10:00	6.376
Chicago_3h_100yr	09/26/2018 00:20:00	7.977
Chicago_3h_100yr	09/26/2018 00:30:00	10.797
Chicago_3h_100yr	09/26/2018 00:40:00	17.136
Chicago_3h_100yr	09/26/2018 00:50:00	44.676
Chicago_3h_100yr	09/26/2018 01:00:00	178.559
Chicago_3h_100yr	09/26/2018 01:10:00	51.056
Chicago_3h_100yr	09/26/2018 01:20:00	26.163
Chicago_3h_100yr	09/26/2018 01:30:00	17.571
Chicago_3h_100yr	09/26/2018 01:40:00	13.277
Chicago_3h_100yr	09/26/2018 01:50:00	10.712
Chicago_3h_100yr	09/26/2018 02:00:00	9.008
Chicago_3h_100yr	09/26/2018 02:10:00	7.793
Chicago_3h_100yr	09/26/2018 02:20:00	6.883
Chicago_3h_100yr	09/26/2018 02:30:00	6.174
Chicago_3h_100yr	09/26/2018 02:40:00	5.607
Chicago_3h_100yr	09/26/2018 02:50:00	5.142
Chicago_3h_100yr	09/26/2018 03:00:00	0
;Chicago design storm, a = 732.951, b = 6.199, c = 0.81, Duration = 180 minutes, r = 0.35, rain units = mm/hr.		
Chicago_3h_2yr	0:00	2.491
Chicago_3h_2yr	0:10	2.966
Chicago_3h_2yr	0:20	3.696
Chicago_3h_2yr	0:30	4.976
Chicago_3h_2yr	0:40	7.828
Chicago_3h_2yr	0:50	19.966
Chicago_3h_2yr	1:00	76.805
Chicago_3h_2yr	1:10	22.777
Chicago_3h_2yr	1:20	11.852
Chicago_3h_2yr	1:30	8.025
Chicago_3h_2yr	1:40	6.096
Chicago_3h_2yr	1:50	4.938
Chicago_3h_2yr	2:00	4.165
Chicago_3h_2yr	2:10	3.613
Chicago_3h_2yr	2:20	3.197
Chicago_3h_2yr	2:30	2.873
Chicago_3h_2yr	2:40	2.613

Chicago_3h_2yr	2:50	2.4
Chicago_3h_2yr	3:00	0
;Chicago design storm, a = 998.071, b = 6.053, c = 0.814, Duration = 180 minutes, r = 0.35, rain units = mm/hr.		
Chicago_3h_5year	0:00	3.256
Chicago_3h_5year	0:10	3.881
Chicago_3h_5year	0:20	4.844
Chicago_3h_5year	0:30	6.532
Chicago_3h_5year	0:40	10.308
Chicago_3h_5year	0:50	26.529
Chicago_3h_5year	1:00	104.193
Chicago_3h_5year	1:10	30.286
Chicago_3h_5year	1:20	15.655
Chicago_3h_5year	1:30	10.568
Chicago_3h_5year	1:40	8.013
Chicago_3h_5year	1:50	6.482
Chicago_3h_5year	2:00	5.462
Chicago_3h_5year	2:10	4.733
Chicago_3h_5year	2:20	4.186
Chicago_3h_5year	2:30	3.76
Chicago_3h_5year	2:40	3.418
Chicago_3h_5year	2:50	3.137
Chicago_3h_5year	3:00	0

[REPORT]
 INPUT YES
 CONTROLS NO
 SUBCATCHMENTS ALL
 NODES ALL
 LINKS ALL

[TAGS]

Node	200	STMH
Node	201	STMH
Node	202	STMH
Node	203	STMH
Node	204	STMH
Node	205	STMH
Node	206	STMH
Node	207	STMH
Node	208	STMH
Node	210	STMH
Node	211	STMH
Node	212	STMH
Node	213	STMH
Node	215	STMH
Node	216	STMH
Node	217	CBMH
Node	218	CBMH
Node	219	STC750
Node	CB03	CB
Node	CB05	CB
Node	CBE01	CBE

Node	CBE04	CBE
Node	CBT02	CBT
Node	CBT03	CBT
Node	CBT05	CBT
Node	CBT06	CBT
Node	CBT07	CBT
Node	CBT08	CBT
Node	CBT09	CBT
Node	CBT10	CBT
Node	CBT11	CBT
Node	CBT12	CBT
Node	CBT13	CBT
Node	CBT14	CBT
Node	IN07998	RYCB
Node	IN09003-MAJ	MAJOR
Node	IN09004-MAJ	MAJOR
Node	IN09005-MAJ	MAJOR
Node	IN09006-MAJ	MAJOR
Node	IN09009-MAJ	MAJOR
Node	IN09010-MAJ	MAJOR
Node	IN09011-MAJ	MAJOR
Node	IN09012-MAJ	MAJOR
Node	IN09013-MAJ	MAJOR
Node	IN09014-MAJ	MAJOR
Node	IN09015-MAJ	MAJOR
Node	IN09017-MAJ	MAJOR
Node	IN09018-MAJ	MAJOR
Node	IN09019-MAJ	MAJOR
Node	IN09020-MAJ	MAJOR
Node	IN09021-MAJ	MAJOR
Node	IN09022-MAJ	MAJOR
Node	IN09023-MAJ	MAJOR
Node	IN09024-MAJ	MAJOR
Node	IN09025-MAJ	MAJOR
Node	IN09026-MAJ	MAJOR
Node	IN09027-MAJ	MAJOR
Node	IN09028-MAJ	MAJOR
Node	IN09029-MAJ	MAJOR
Node	IN09030-MAJ	MAJOR
Node	IN09031-MAJ	MAJOR
Node	IN09032-MAJ	MAJOR
Node	IN09033-MAJ	MAJOR
Node	IN09034-MAJ	MAJOR
Node	IN09035-MAJ	MAJOR
Node	IN45566	RYCB
Node	IN45569	RYCB
Node	IN45570	RYCB
Node	IN45572	RYCB
Node	IN45573	RYCB
Node	IN45574	RYCB
Node	IN45575	RYCB
Node	IN45577	RYCB
Node	IN45587	RYCB

Node	IN45588	RYCB
Node	IN45589	RYCB
Node	IN45590	RYCB
Node	J1	MAJOR
Node	J2	MAJOR
Node	MHST09001	STMH
Node	MHST09002	STMH
Node	MHST09003	STMH
Node	MHST09004	STMH
Node	MHST09005	STMH
Node	MHST09006	STMH
Node	MHST09007	STMH
Node	MHST09008	STMH
Node	MHST09009	STMH
Node	MHST09010	STMH
Node	MHST09011	STMH
Node	MHST09013	STMH
Node	MHST09014	STMH
Node	MHST09015	STMH
Node	MHST09016	STMH
Node	MHST09017	STMH
Node	MHST09018	STMH
Node	MHST09019	STMH
Node	MHST09020	STMH
Node	MHST09021	STMH
Node	MHST09022	STMH
Node	MHST09023	STMH
Node	MHST09024	STMH
Node	CB01	CATCHBASIN
Node	CB06	CATCHBASIN
Node	CHAMBERS-1	STORAGE_CHAMBERS
Node	CHAMBERS-2	STORAGE_CHAMBERS
Node	IN09003	CATCHBASIN
Node	IN09004	CATCHBASIN
Node	IN09005	CATCHBASIN
Node	IN09006	CATCHBASIN
Node	IN09007	CATCHBASIN
Node	IN09008	CATCHBASIN
Node	IN09009	CATCHBASIN
Node	IN09010	CATCHBASIN
Node	IN09011	CATCHBASIN
Node	IN09012	CATCHBASIN
Node	IN09013	CATCHBASIN
Node	IN09014	CATCHBASIN
Node	IN09015	CATCHBASIN
Node	IN09016	CATCHBASIN
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Node	IN09018	CATCHBASIN
Node	IN09019	CATCHBASIN
Node	IN09020	CATCHBASIN
Node	IN09021	CATCHBASIN
Node	IN09022	CATCHBASIN
Node	IN09023	CATCHBASIN

Node	IN09024	CATCHBASIN
Node	IN09025	CATCHBASIN
Node	IN09026	CATCHBASIN
Node	IN09027	CATCHBASIN
Node	IN09028	CATCHBASIN
Node	IN09029	CATCHBASIN
Node	IN09030	CATCHBASIN
Node	IN09031	CATCHBASIN
Node	IN09032	CATCHBASIN
Node	IN09033	CATCHBASIN
Node	IN09034	CATCHBASIN
Node	IN09035	CATCHBASIN
Node	IN10_3407	DOUBLE_CATCHBASIN
Node	MHST09012	STMH
Link	C01	STORM
Link	C02	STORM
Link	C03	STORM
Link	C04	STORM
Link	C05	STORM
Link	C06	STORM
Link	C07	STORM
Link	C08	STORM
Link	C09	STORM
Link	C1	RYCB LEAD
Link	C10	STORM
Link	C11	STORM
Link	C12	STORM
Link	C13	RYCB LEAD
Link	C14	STORM
Link	C15	STORM
Link	C16	STORM
Link	C17	STORM
Link	C18	STORM
Link	C19	STORM
Link	C2	RYCB LEAD
Link	C20	STORM
Link	C21	STORM
Link	C22	RYCB LEAD
Link	C23	STORM
Link	C24	STORM
Link	C25	STORM
Link	C26	RYCB LEAD
Link	C27	RYCB LEAD
Link	C28	STORM
Link	C29	STORM
Link	C3	RYCB LEAD
Link	C30	STORM
Link	C31	STORM
Link	C32	STORM
Link	C33	STORM
Link	C34	STORM
Link	C35	STORM
Link	C36	STORM

Link	C37	STORM
Link	C38	STORM
Link	C39	MAJOR
Link	C4	RYCB LEAD
Link	C40	STORM
Link	C5	RYCB LEAD
Link	C6	RYCB LEAD
Link	C7	RYCB LEAD
Link	C8	RYCB LEAD
Link	C9	RYCB LEAD
Link	C98	SUBDRAIN
Link	C99	SUBDRAIN
Link	OF1	OVERFLOW-ROAD
Link	R01	MAJOR
Link	R02	MAJOR
Link	R03	MAJOR
Link	R04	MAJOR
Link	R05	MAJOR
Link	R06	MAJOR
Link	R07	MAJOR
Link	R08	MAJOR
Link	R09	MAJOR
Link	R10	MAJOR
Link	R11	MAJOR
Link	R12	MAJOR
Link	R13	MAJOR
Link	R14	MAJOR
Link	R15	MAJOR
Link	R16	MAJOR
Link	R17	MAJOR
Link	R18	MAJOR
Link	R19	MAJOR
Link	R20	MAJOR
Link	R21	MAJOR
Link	R22	MAJOR
Link	R23	MAJOR
Link	R24	MAJOR
Link	R25	MAJOR
Link	R26	MAJOR
Link	R27	MAJOR
Link	R28	MAJOR
Link	R29	MAJOR
Link	R30	MAJOR
Link	R31	MAJOR
Link	R32	MAJOR
Link	R33	MAJOR
Link	R34	MAJOR
Link	STM04620	STORM
Link	STM04621	STORM
Link	STM07857	STORM
Link	STM07870	STORM
Link	STM07871	STORM
Link	STM07872	STORM

Link	STM07873	STORM
Link	STM07874	STORM
Link	STM07875	STORM
Link	STM07876	STORM
Link	STM45150	STORM
Link	STM45151	STORM
Link	STM45152	STORM
Link	STM45153	STORM
Link	STM45154	STORM
Link	STM45155	STORM
Link	STM45156	STORM
Link	STM45159	STORM
Link	STM45160	STORM
Link	STM45161	STORM
Link	STM45162	STORM
Link	STM45163	STORM
Link	STM45164_1	STORM
Link	STM45164_2	STORM
Link	STM45165	STORM
Link	212-ICD	ICD
Link	215-ICD	ICD
Link	IN09003-ICD	ICD
Link	IN09003-INC	INC
Link	IN09004-ICD	ICD
Link	IN09004-INC	INC
Link	IN09005-ICD	ICD
Link	IN09005-INC	INC
Link	IN09006-ICD	ICD
Link	IN09006-INC	INC
Link	IN09007-ICD	ICD
Link	IN09008-ICD	ICD
Link	IN09009-ICD	ICD
Link	IN09009-INC	INC
Link	IN09010-ICD	ICD
Link	IN09010-INC	INC
Link	IN09011-ICD	ICD
Link	IN09011-INC	INC
Link	IN09012-ICD	ICD
Link	IN09012-INC	INC
Link	IN09013-ICD	ICD
Link	IN09013-INC	INC
Link	IN09014-ICD	ICD
Link	IN09014-INC	INC
Link	IN09015-ICD	ICD
Link	IN09015-INC	INC
Link	IN09016-ICD	ICD
Link	IN09017-ICD	ICD
Link	IN09017-INC	INC
Link	IN09018-ICD	ICD
Link	IN09018-INC	INC
Link	IN09019-ICD	ICD
Link	IN09019-INC	INC
Link	IN09020-ICD	ICD

Link IN09020-INC INC
 Link IN09021-ICD ICD
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 Link IN09033-ICD ICD
 Link IN09033-INC INC
 Link IN09034-ICD ICD
 Link IN09034-INC INC
 Link IN09035-ICD ICD
 Link IN09035-INC INC
 Link IN103407-ICD ICD

[MAP]
 DIMENSIONS 350056.306251781 5014976.29176218 350757.766320881 5015428.42071167
 UNITS Meters

[COORDINATES]
 ;;Node X-Coord Y-Coord
 ;-----
 200 350236.22 5015304.609
 201 350209.335 5015299.052
 202 350201.692 5015307.586
 203 350194.468 5015341.9
 204 350186.244 5015339.654
 205 350153.118 5015309.999
 206 350118.272 5015278.782
 207 350128.825 5015267
 208 350157.244 5015292.366
 210 350192.735 5015301.458
 211 350203.38 5015290.412
 212 350216.879 5015293.723
 213 350140.85 5015328.978

215	350161.778	5015300.394
216	350215.638	5015300.361
217	350171.983	5015275.934
218	350160.358	5015307.194
219	350225.718	5015302.427
CB03	350143.947	5015299.152
CB05	350129.074	5015236.82
CBE01	350099.944	5015270.421
CBE04	350091.977	5015285.221
CBT02	350114.509	5015253.621
CBT03	350155.089	5015260.363
CBT05	350100.476	5015292.825
CBT06	350108.325	5015299.854
CBT07	350113.289	5015304.298
CBT08	350120.579	5015310.827
CBT09	350130.074	5015319.329
CBT10	350138.395	5015326.78
CBT11	350143.305	5015331.176
CBT12	350150.4	5015337.53
CBT13	350159.895	5015346.032
CBT14	350169.389	5015354.533
IN07998	350621.425	5015080.81
IN09003-MAJ	350247.234	5015313.065
IN09004-MAJ	350248.311	5015293.655
IN09005-MAJ	350299.715	5015216.72
IN09006-MAJ	350305.672	5015221.82
IN09009-MAJ	350398.641	5015102.487
IN09010-MAJ	350404.597	5015107.853
IN09011-MAJ	350468.924	5015023.32
IN09012-MAJ	350471.593	5015031.288
IN09013-MAJ	350556.46	5015047.398
IN09014-MAJ	350621.898	5015074.916
IN09015-MAJ	350625.131	5015067.338
IN09017-MAJ	350626.792	5015150.775
IN09018-MAJ	350632.578	5015155.866
IN09019-MAJ	350574.34	5015212.475
IN09020-MAJ	350580.594	5015217.119
IN09021-MAJ	350562.587	5015240.618
IN09022-MAJ	350312.204	5015357.483
IN09023-MAJ	350310.292	5015349.062
IN09024-MAJ	350363.423	5015288.115
IN09025-MAJ	350369.697	5015293.42
IN09026-MAJ	350419.396	5015223.431
IN09027-MAJ	350425.329	5015228.659
IN09028-MAJ	350466.777	5015183.937
IN09029-MAJ	350463.571	5015172.282
IN09030-MAJ	350510.843	5015118.237
IN09031-MAJ	350517.004	5015122.947
IN09032-MAJ	350546.223	5015063.339
IN09033-MAJ	350553.825	5015064.965
IN09034-MAJ	350534.993	5015237.172
IN09035-MAJ	350538.935	5015231.292
IN45566	350496.323	5015216.908

IN45569	350432.152	5015141.063
IN45570	350384.539	5015198.238
IN45572	350467.839	5015101.558
IN45573	350264.776	5015373.712
IN45574	350326.162	5015397.08
IN45575	350336.094	5015254.524
IN45577	350496.079	5015068.346
IN45587	350257.173	5015210.155
IN45588	350312.141	5015145.597
IN45589	350381.132	5015064.396
IN45590	350423.244	5015015.609
J1	350564.843	5015058.534
J2	350555.207	5015232.098
MHST09001	350224.039	5015353.25
MHST09002	350230.972	5015345.475
MHST09003	350235.708	5015309.242
MHST09004	350237.701	5015292.778
MHST09005	350291.793	5015229.955
MHST09006	350349.966	5015161.147
MHST09007	350409.63	5015093.799
MHST09008	350467.085	5015027.014
MHST09009	350479.295	5015023.595
MHST09010	350556.479	5015049.846
MHST09011	350628.361	5015071.514
MHST09013	350633.137	5015150.737
MHST09014	350584.395	5015209.484
MHST09015	350553.203	5015250.719
MHST09016	350272.391	5015328.497
MHST09017	350302.028	5015354.551
MHST09018	350315.399	5015352.853
MHST09019	350350.045	5015313.01
MHST09020	350408.843	5015244.76
MHST09021	350467.282	5015177.128
MHST09022	350505.694	5015132.451
MHST09023	350541.908	5015088.705
MHST09024	350503.21	5015208.294
OF-CREEK	350725.882	5015078.087
OF-HAZELDEAN	350206.288	5015398.796
CB01	350215.017	5015301.442
CB06	350191.863	5015320.653
CHAMBERS-1	350199.465	5015282.365
CHAMBERS-2	350165.304	5015289.803
INO9003	350246.559	5015313.113
INO9004	350248.307	5015293.832
INO9005	350300.205	5015216.385
INO9006	350306.001	5015221.469
INO9007	350357.814	5015161.87
INO9008	350351.701	5015157.165
INO9009	350398.931	5015102.149
INO9010	350404.886	5015107.563
INO9011	350469.113	5015023.754
INO9012	350471.437	5015030.953
INO9013	350556.355	5015047.722

INO9014	350621.772	5015075.37
INO9015	350625.099	5015067.459
INO9016	350667.92	5015097.621
INO9017	350626.37	5015150.174
INO9018	350632.086	5015155.363
INO9019	350574.678	5015212.726
INO9020	350581.021	5015217.481
INO9021	350563.395	5015241.028
INO9022	350312.767	5015357.29
INO9023	350310.748	5015348.819
INO9024	350363.662	5015287.797
INO9025	350370.08	5015292.654
INO9026	350419.942	5015222.816
INO9027	350426.026	5015227.901
INO9028	350467.566	5015183.842
INO9029	350464.177	5015171.575
INO9030	350511.332	5015117.665
INO9031	350517.379	5015122.612
INO9032	350546.357	5015062.966
INO9033	350553.994	5015064.494
INO9034	350534.392	5015237.866
INO9035	350539.504	5015231.73
IN103407	350211.409	5015362.487
MHST09012	350683.196	5015090.945

[VERTICES]	X-Coord	Y-Coord
;		
;		
C09	350158.069	5015291.377
C09	350161.689	5015287.406
C09	350162.465	5015287.269
C09	350164.94	5015289.654
C1	350283.551	5015232.784
C1	350283.823	5015234.693
C1	350236.873	5015289.803
C13	350625.96	5015079.068
C14	350166.158	5015282.396
C14	350162.639	5015286.345
C14	350162.676	5015287.017
C14	350165.141	5015289.426
C15	350201.493	5015280.024
C15	350210.972	5015288.473
C16	350201.767	5015288.895
C16	350197.282	5015284.87
C2	350339.619	5015168.398
C2	350339.525	5015169.525
C2	350290.333	5015226.561
C2	350290.209	5015228.721
C22	350286.133	5015349.217
C22	350286.33	5015346.558
C22	350271.128	5015332.885
C22	350270.684	5015330.44
C24	350168.372	5015292.427

C24	350168.306	5015293.156
C24	350163.135	5015298.874
C26	350311.388	5015361.299
C26	350309.99	5015360.66
C26	350303.634	5015360.85
C26	350301.988	5015359.423
C3	350408.849	5015087.268
C3	350408.812	5015088.586
C3	350407.062	5015090.551
C3	350407.157	5015091.748
C39	350212.499	5015374.507
C39	350205.667	5015381.865
C39	350203.995	5015385.263
C39	350202.762	5015389.296
C39	350203.507	5015393.387
C4	350450.725	5015038.494
C4	350451.008	5015039.812
C4	350407.528	5015090.94
C4	350407.468	5015091.571
C4	350409.167	5015092.902
C5	350366.59	5015280.139
C5	350366.575	5015282.182
C5	350345.57	5015306.319
C5	350345.027	5015308.165
C6	350416.049	5015224.631
C6	350416.095	5015226.037
C6	350403.983	5015239.331
C6	350403.974	5015240.624
C7	350463.644	5015167.655
C7	350463.738	5015169.47
C7	350462.118	5015171.433
C7	350462.095	5015173.744
C7	350465.971	5015177.031
C8	350498.952	5015128.032
C8	350498.914	5015129.691
C8	350462.536	5015172.149
C8	350462.623	5015173.371
C9	350527.085	5015095.748
C9	350527.033	5015097.419
C9	350500.892	5015127.123
C9	350500.675	5015128.385
C98	350199.352	5015281.657
C98	350202.004	5015278.64
C98	350213.16	5015288.415
C98	350213.128	5015289.863
C98	350216.78	5015293.143
C99	350169.532	5015285.118
C99	350173.477	5015288.631
C99	350173.344	5015289.46
C99	350164.378	5015299.47
OF1	350668.269	5015097.373
OF1	350668.301	5015096.929
OF1	350668.318	5015096.23

OF1	350668.425	5015095.836
OF1	350668.712	5015095.22
OF1	350669.211	5015094.672
OF1	350675.211	5015092.864
R01	350248.297	5015293.371
R01	350248.314	5015292.432
R01	350248.549	5015291.416
R01	350248.891	5015289.736
R01	350249.708	5015287.81
R01	350250.612	5015286.497
R01	350252.16	5015284.45
R01	350256.394	5015279.434
R01	350305.531	5015222.39
R02	350306.03	5015221.796
R02	350306.69	5015221.058
R02	350357.668	5015162.212
R03	350299.744	5015216.685
R03	350300.129	5015216.201
R03	350300.728	5015215.875
R03	350351.146	5015157.312
R04	350358.015	5015161.811
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R04	350358.164	5015161.465
R05	350351.702	5015156.595
R06	350404.615	5015107.599
R06	350404.955	5015107.21
R06	350405.243	5015107.156
R06	350469.133	5015033.143
R06	350470.282	5015032.04
R07	350398.935	5015102.419
R07	350399.322	5015102.012
R07	350399.354	5015101.678
R07	350461.708	5015029.076
R07	350463.642	5015026.888
R07	350466.029	5015025.152
R07	350467.411	5015024.118
R08	350473.766	5015030.316
R08	350476.034	5015029.845
R08	350477.587	5015029.775
R08	350479.122	5015029.898
R08	350480.832	5015030.264
R09	350554.166	5015064.842
R09	350554.287	5015064.337
R09	350554.523	5015063.738
R09	350555.254	5015062.649
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R09	350557.044	5015060.784
R09	350558.118	5015060.038
R09	350559.207	5015059.427
R09	350560.416	5015059.024
R09	350561.654	5015058.755
R09	350563.026	5015058.696
R10	350546.105	5015063.079

R10	350546.335	5015062.506
R10	350546.603	5015061.591
R10	350547.217	5015059.642
R10	350547.911	5015058.2
R10	350549.006	5015056.411
R10	350549.887	5015055.744
R10	350551.249	5015055.423
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R10	350553.332	5015055.236
R10	350554.88	5015055.583
R10	350557.71	5015056.545
R10	350562.542	5015058.138
R11	350469.966	5015022.816
R11	350470.98	5015022.548
R11	350472.53	5015022.127
R11	350474.271	5015021.783
R11	350476.108	5015021.611
R11	350477.428	5015021.611
R11	350479.877	5015021.706
R11	350481.561	5015022.127
R11	350483.895	5015022.835
R11	350555.002	5015046.903
R12	350580.725	5015055.859
R12	350590.263	5015058.963
R12	350597.824	5015061.567
R12	350604.259	5015063.82
R12	350608.665	5015064.772
R12	350615.625	5015065.698
R12	350624.162	5015067.038
R12	350624.697	5015067.197
R12	350624.956	5015067.28
R13	350625.32	5015067.393
R13	350632.374	5015069.879
R13	350676.513	5015084.801
R13	350679.868	5015086.278
R13	350681.645	5015087.404
R13	350682.772	5015088.706
R13	350683.039	5015089.612
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R14	350668.145	5015096.072
R14	350668.08	5015097.033
R15	350577.563	5015063.065
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R15	350619.254	5015074.552
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R15	350621.372	5015075.034
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R16	350540.889	5015232.738
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R16	350544.733	5015234.103
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R16	350552.109	5015233.714
R16	350553.54	5015233.06
R17	350536.588	5015238.596
R17	350538.914	5015240.49
R17	350540.842	5015242.251
R17	350541.872	5015242.683
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R17	350546.942	5015238.226
R17	350550.271	5015235.089
R17	350552.81	5015233.93
R18	350563.457	5015239.733
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R18	350563.687	5015238.712
R18	350563.622	5015237.466
R18	350563.728	5015236.48
R18	350564.144	5015235.386
R18	350564.584	5015234.464
R18	350580.55	5015217.877
R19	350564.327	5015223.043
R19	350574.148	5015213.085
R20	350581.252	5015217.153
R20	350603.279	5015190.77
R20	350631.75	5015156.598
R21	350575.236	5015212.077
R21	350626.187	5015151.499
R22	350632.945	5015155.287
R22	350659.643	5015122.789
R22	350681.572	5015097.8
R22	350683.041	5015095.598
R22	350683.571	5015094.29
R22	350683.886	5015092.462
R22	350683.59	5015091.668
R23	350627.032	5015150.333
R23	350627.124	5015149.595
R23	350657.703	5015112.666
R23	350666.588	5015102.09
R23	350667.318	5015100.661
R23	350667.749	5015099.363
R23	350668.015	5015098.408
R24	350246.353	5015313.522
R24	350244.438	5015314.175

R24	350242.77	5015315.18
R24	350241.572	5015316.431
R24	350240.684	5015317.619
R24	350239.796	5015319.329
R24	350239.196	5015322.327
R24	350237.752	5015334.1
R24	350237.261	5015337.806
R24	350236.553	5015341.24
R24	350235.272	5015344.702
R24	350233.473	5015348.381
R24	350231.04	5015352.347
R24	350227.625	5015358.005
R24	350225.333	5015360.737
R24	350221.333	5015365.273
R25	350310.846	5015349.204
R25	350311.582	5015348.674
R25	350311.726	5015348.113
R25	350363.47	5015288.645
R26	350313.076	5015357.438
R26	350314.179	5015356.786
R26	350316.085	5015355.402
R26	350317.793	5015353.68
R26	350320.857	5015350.221
R27	350369.563	5015292.635
R27	350370.119	5015291.906
R27	350370.948	5015291.97
R28	350364.194	5015287.898
R28	350419.262	5015224.247
R29	350425.308	5015227.908
R29	350425.981	5015227.068
R29	350427.04	5015227.118
R29	350461.462	5015187.723
R29	350463.653	5015185.518
R29	350464.834	5015184.778
R30	350420.449	5015223.287
R30	350420.994	5015222.64
R30	350421.062	5015221.856
R30	350463.357	5015173.105
R31	350464.377	5015172.202
R31	350465.253	5015171.426
R31	350465.23	5015170.583
R31	350509.996	5015119.189
R32	350467.005	5015183.407
R32	350467.75	5015183.338
R32	350468.98	5015183.979
R32	350470.192	5015184.065
R32	350471.509	5015184.412
R32	350472.946	5015185.035
R32	350474.297	5015185.867
R32	350532.246	5015235.864
R32	350533.582	5015236.911
R33	350511.659	5015118.372
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R33	350511.864	5015116.953
R33	350530.125	5015096.133
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R33	350535.1	5015089.744
R33	350536.724	5015087.047
R33	350538.688	5015083.512
R33	350545.787	5015063.889
R33	350545.953	5015063.499
R34	350517.052	5015122.474
R34	350517.499	5015121.996
R34	350517.859	5015121.964
R34	350538.513	5015098.111
R34	350541.199	5015094.873
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R34	350544.89	5015088.321
R34	350546.622	5015084.43
R34	350553.561	5015066.376
R34	350553.987	5015065.349
INO9004-ICD	350241.872	5015289.056
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INO9005-ICD	350301.363	5015217.207
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INO9005-ICD	350291.485	5015228.24
INO9006-ICD	350303.415	5015221.919
INO9006-ICD	350295.551	5015231.269
INO9007-ICD	350357.307	5015161.501
INO9007-ICD	350356.552	5015161.675
INO9007-ICD	350355.012	5015163.4
INO9008-ICD	350352.003	5015157.431
INO9008-ICD	350351.955	5015157.804
INO9008-ICD	350349.676	5015160.321
INO9009-ICD	350400.3	5015102.355
INO9009-ICD	350407.391	5015093.864
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INO9010-ICD	350403.535	5015104.811
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INO9011-ICD	350467.421	5015024.755
INO9011-ICD	350466.698	5015025.785
INO9012-ICD	350469.993	5015030.36
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INO9014-ICD	350623.616	5015073.245
INO9014-ICD	350625.864	5015073.945
INO9015-ICD	350625.715	5015068.474
INO9015-ICD	350628.238	5015069.448
INO9016-ICD	350668.74	5015100.546
INO9016-ICD	350631.121	5015146.614
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INO9018-ICD	350631.741	5015154.008
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INO9019-ICD	350576.961	5015214.57
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IN09020-ICD	350580.829	5015215.599
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IN09021-ICD	350555.952	5015249.96
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IN09027-ICD	350423.725	5015228.795
IN09027-ICD	350410.488	5015244.156
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IN09030-ICD	350513.132	5015119.276
IN09030-ICD	350513.163	5015120.106
IN09030-ICD	350504.186	5015130.559
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IN09031-ICD	350506.582	5015132.521
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IN09032-ICD	350540.488	5015086.32
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IN09035-ICD	350535.193	5015231.94
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[POLYGONS]	;	Subcatchment	X-Coord	Y-Coord
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ES01_1		350249.833	5015306.976	
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ES01_1		350228.288	5015297.311	
ES01_1		350228.295	5015297.313	
ES01_1		350227.076	5015307.139	
ES01_1		350223.845	5015334.24	
ES01_1		350223.681	5015335.166	
ES01_1		350223.487	5015336.086	
ES01_1		350223.262	5015336.998	
ES01_1		350223.007	5015337.903	
ES01_1		350222.722	5015338.799	

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ES01_1	350222.063	5015340.56
ES01_1	350221.69	5015341.423
ES01_1	350221.289	5015342.273
ES01_1	350220.86	5015343.109
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ES01_1	350218.873	5015346.298
ES01_1	350218.312	5015347.052
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ES01_1	350201.662	5015365.502
ES01_1	350186.7	5015366.274
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ES01_1	350191.968	5015407.869
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ES01_1	350229.475	5015381.327
ES01_1	350237.544	5015349.952
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ES01_1	350261.014	5015340.444
ES01_1	350244.79	5015325.87
ES01_1	350246.596	5015314.238
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ES02_1	350268.01	5015291.14
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ES02_1	350241.854	5015291.481
ES02_1	350239.121	5015295.194
ES02_1	350249.833	5015306.976
ES02_1	350272.925	5015326.896
ES02_2	350244.79	5015325.87
ES02_2	350261.014	5015340.444
ES02_2	350272.925	5015326.896
ES02_2	350249.833	5015306.976
ES02_2	350246.596	5015314.238
ES02_2	350244.79	5015325.87
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ES03_1	350275.492	5015211.374
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ES03_2	350302.554	5015219.116
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ES03_2	350320.254	5015234.481
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ES04_2	350354.62	5015159.699
ES04_2	350302.554	5015219.116
ES04_2	350320.254	5015234.481
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ES04_2	350357.821	5015162.128
ES04_2	350354.62	5015159.699
ES05_1	350354.62	5015159.699
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ES05_2	350401.995	5015104.511
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ES06_2	350480.519	5015050.249
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ES07	350554.367	5015051.146
ES07	350562.689	5015027.23
ES07	350502.967	5015008.267
ES07	350489.816	5015018.728
ES07	350474.118	5015013.397
ES07	350468.867	5014996.843
ES07	350454.439	5015004.767
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ES07	350471.244	5015027.036
ES07	350473.652	5015026.496
ES07	350476.019	5015025.965
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ES08_2	350310.984	5015348.635
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ES10_1	350423.501	5015225.4
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ES10_1	350353.992	5015268.905
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ES10_1	350363.859	5015287.57
ES10_1	350367.301	5015290.193
ES10_2	350423.501	5015225.4
ES10_2	350367.301	5015290.193
ES10_2	350370.579	5015292.69
ES10_2	350383.043	5015303.573
ES10_2	350440.411	5015239.822
ES10_2	350426.223	5015227.675
ES10_2	350423.501	5015225.4
ES11_1	350423.501	5015225.4
ES11_1	350467.202	5015176.36
ES11_1	350466.293	5015170.651
ES11_1	350449.238	5015155.003
ES11_1	350404.004	5015209.097
ES11_1	350420.139	5015222.589
ES11_1	350423.501	5015225.4
ES11_2	350467.202	5015176.36
ES11_2	350423.501	5015225.4
ES11_2	350426.223	5015227.675
ES11_2	350440.411	5015239.822
ES11_2	350471.902	5015204.826
ES11_2	350467.202	5015176.36
ES12_1	350514.415	5015119.799
ES12_1	350511.529	5015117.439
ES12_1	350507.005	5015113.557
ES12_1	350494.422	5015100.968
ES12_1	350483.267	5015114.309
ES12_1	350449.238	5015155.003
ES12_1	350466.293	5015170.651
ES12_1	350467.202	5015176.36
ES12_1	350514.415	5015119.799
ES12_2	350514.415	5015119.799
ES12_2	350467.202	5015176.36
ES12_2	350500.572	5015174.972
ES12_2	350533.605	5015135.958
ES12_2	350517.576	5015122.386
ES12_2	350514.415	5015119.799
ES13_1	350541.96	5015086.344
ES13_1	350534.378	5015097.718
ES13_1	350514.415	5015119.799
ES13_1	350507.005	5015113.557
ES13_1	350511.529	5015117.439
ES13_1	350514.415	5015119.799
ES13_1	350534.378	5015097.718
ES13_2	350514.415	5015119.799
ES13_2	350517.576	5015122.386
ES13_2	350533.605	5015135.958
ES13_2	350560.92	5015103.697
ES13_2	350569.201	5015078.321
ES13_2	350554.648	5015064.422
ES13_2	350549.524	5015063.793
ES13_2	350541.96	5015086.344
ES13_2	350538.765	5015092.194
ES13_2	350534.378	5015097.718
ES14_1	350598.934	5015066.244
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ES14_1	350549.524	5015063.793
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ES14_1	350624.263	5015071.886
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ES14_1	350617.033	5015069.915
ES14_1	350614.301	5015069.403
ES14_1	350610.203	5015068.805
ES14_1	350606.618	5015068.037
ES14_1	350602.691	5015067.354
ES14_1	350598.934	5015066.244
ES14_2	350620.533	5015070.598
ES14_2	350624.263	5015071.886
ES14_2	350631.522	5015050.441
ES14_2	350562.689	5015027.23
ES14_2	350554.367	5015051.146
ES14_2	350554.334	5015051.239
ES14_2	350598.934	5015066.244
ES14_2	350602.691	5015067.354
ES14_2	350606.618	5015068.037
ES14_2	350610.203	5015068.805
ES14_2	350614.301	5015069.403
ES14_2	350617.033	5015069.915
ES14_2	350620.533	5015070.598
ES15_1	350667.353	5015085.75
ES15_1	350624.262	5015071.891
ES15_1	350621.472	5015080.131
ES15_1	350636.525	5015096.98

ES15_1	350667.555	5015095.113
ES15_1	350675.352	5015092.73
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ES15_2	350674.518	5015090.875
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ES15_2	350684.893	5015089.977
ES15_2	350676.012	5015072.254
ES15_2	350677.665	5015066.586
ES15_2	350633.769	5015051.181
ES15_2	350631.522	5015050.441
ES15_2	350624.262	5015071.891
ES15_2	350667.353	5015085.75
ES15_2	350672.479	5015088.064
ES15_2	350673.691	5015089.497
ES15_2	350674.518	5015090.875
ES16_1	350467.202	5015176.36
ES16_1	350471.902	5015204.826
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ES16_1	350516.816	5015231.613
ES16_1	350520.547	5015239.947
ES16_1	350533.326	5015238.736
ES16_1	350534.416	5015237.367
ES16_1	350537.166	5015234.378
ES16_1	350467.202	5015176.36
ES16_2	350467.202	5015176.36
ES16_2	350537.166	5015234.378
ES16_2	350543.352	5015228.647
ES16_2	350544.914	5015210.616
ES16_2	350500.572	5015174.972
ES16_2	350467.202	5015176.36
ES17	350503.081	5015293.23
ES17	350523.624	5015268.442
ES17	350539.907	5015250.846
ES17	350548.888	5015242.22
ES17	350537.166	5015234.378
ES17	350534.416	5015237.367
ES17	350533.326	5015238.736
ES17	350520.547	5015239.947
ES17	350486.567	5015280.036
ES17	350503.081	5015293.23
ES18	350579.975	5015251.855
ES18	350559.918	5015236.037
ES18	350548.888	5015242.22
ES18	350539.907	5015250.846
ES18	350523.624	5015268.442
ES18	350503.081	5015293.23
ES18	350524.877	5015311.721
ES18	350579.975	5015251.855
ES19	350537.166	5015234.378

ES19	350548.888	5015242.22
ES19	350559.918	5015236.037
ES19	350578.255	5015215.022
ES19	350574.561	5015212.24
ES19	350571.935	5015206.644
ES19	350558.48	5015195.476
ES19	350544.914	5015210.616
ES19	350543.352	5015228.647
ES19	350537.166	5015234.378
ES20	350596.738	5015232.091
ES20	350586.069	5015221.104
ES20	350581.212	5015217.25
ES20	350578.255	5015215.022
ES20	350559.918	5015236.037
ES20	350579.975	5015251.855
ES20	350596.738	5015232.091
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ES21_1	350630.223	5015192.681
ES21_1	350650.406	5015168.925
ES21_1	350638.08	5015158.476
ES21_1	350632.805	5015155.859
ES21_1	350629.767	5015153.191
ES21_3	350610.824	5015175.978
ES21_3	350578.255	5015215.022
ES21_3	350581.212	5015217.25
ES21_3	350586.069	5015221.104
ES21_3	350596.738	5015232.091
ES21_3	350630.223	5015192.681
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ES21_4	350578.255	5015215.022
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ES21_4	350588.892	5015157.094
ES21_4	350558.48	5015195.476
ES21_4	350571.935	5015206.644
ES21_4	350574.561	5015212.24
ES21_4	350578.255	5015215.022
ES21_5	350610.825	5015175.979
ES21_5	350629.767	5015153.191
ES21_5	350626.273	5015150.337
ES21_5	350622.373	5015146.391
ES21_5	350607.248	5015134.276
ES21_5	350588.892	5015157.094
ES21_5	350610.825	5015175.979
ES22_1	350675.443	5015093.308
ES22_1	350675.307	5015092.744
ES22_1	350667.555	5015095.113
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ES22_1	350622.373	5015146.391
ES22_1	350626.273	5015150.337
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ES22_1	350669.773	5015104.421

ES22_1	350672.575	5015100.901
ES22_1	350674.465	5015097.447
ES22_1	350675.345	5015095.198
ES22_1	350675.443	5015093.308
ES22_2	350669.773	5015104.421
ES22_2	350629.767	5015153.191
ES22_2	350632.805	5015155.859
ES22_2	350638.08	5015158.476
ES22_2	350650.406	5015168.925
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ES22_2	350684.893	5015089.977
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ES22_2	350675.352	5015092.73
ES22_2	350675.307	5015092.744
ES22_2	350675.443	5015093.308
ES22_2	350675.345	5015095.198
ES22_2	350674.465	5015097.447
ES22_2	350672.575	5015100.901
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ES23	350275.492	5015211.374
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ES23	350208.517	5015261.122
ES23	350198.768	5015271.796
ES23	350212.793	5015283.918
ES23	350275.492	5015211.374
ES24	350312.067	5015144.703
ES24	350277.456	5015185.27
ES24	350289.035	5015195.296
ES24	350323.339	5015154.439
ES24	350312.067	5015144.703
ES25	350334.405	5015141.95
ES25	350382.489	5015087.882
ES25	350401.067	5015066.555
ES25	350388.3	5015055.525
ES25	350312.067	5015144.703
ES25	350323.339	5015154.439
ES25	350334.405	5015141.95
ES26	350442.724	5015018.336
ES26	350429.701	5015007.093
ES26	350388.3	5015055.525
ES26	350401.067	5015066.555
ES26	350442.724	5015018.336
ES27	350353.992	5015268.905
ES27	350317.719	5015237.254
ES27	350268.01	5015291.14
ES27	350288.081	5015309.656
ES27	350306.052	5015326.234
ES27	350353.992	5015268.905
ES28	350401.433	5015212.171
ES28	350367.692	5015183.082
ES29	350401.433	5015212.171
ES30	350449.238	5015155.003
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ES30	350421.526	5015120.994
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ES30	350449.238	5015155.003
ES31	350494.422	5015100.968
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ES31	350480.519	5015050.249
ES31	350450.609	5015086.116
ES31	350483.267	5015114.309
ES31	350494.422	5015100.968
ES32	350558.48	5015195.476
ES32	350607.248	5015134.276
ES32	350636.525	5015096.98
ES32	350621.472	5015080.131
ES32	350601.222	5015088.612
ES32	350569.201	5015078.321
ES32	350560.92	5015103.697
ES32	350500.572	5015174.972
ES32	350544.914	5015210.616
ES32	350558.48	5015195.476
ES33	350267.274	5015375.65
ES33	350280.493	5015360.842
ES33	350259.532	5015342.13
ES33	350237.544	5015349.952
ES33	350229.475	5015381.327
ES33	350246.554	5015396.89
ES33	350267.274	5015375.65
ES34	350341.416	5015396.087
ES34	350396.729	5015335.026
ES34	350384.909	5015319.835
ES34	350375.792	5015311.631
ES34	350319.242	5015374.474
ES34	350294.076	5015372.967
ES34	350280.493	5015360.842
ES34	350267.274	5015375.65
ES34	350289.432	5015395.43
ES34	350297.547	5015401.984
ES34	350341.416	5015396.087
ES35	350486.567	5015280.036
ES35	350520.547	5015239.947

ES35	350516.816	5015231.613
ES35	350490.656	5015208.217
ES35	350471.902	5015204.826
ES35	350440.411	5015239.822
ES35	350383.043	5015303.573
ES35	350375.792	5015311.631
ES35	350384.909	5015319.835
ES35	350396.729	5015335.026
ES35	350424.484	5015357.689
ES35	350486.567	5015280.036
ES36	350476.019	5015025.965
ES36	350471.244	5015027.036
ES36	350472.085	5015031.234
ES36	350481.422	5015052.285
ES36	350511.126	5015082.018
ES36	350521.632	5015066.116
ES36	350546.071	5015062.538
ES36	350549.524	5015063.793
ES36	350550.007	5015062.533
ES36	350554.367	5015051.146
ES36	350526.313	5015041.811
ES36	350502.826	5015033.836
ES36	350484.328	5015027.496
ES36	350480.482	5015026.197
ES36	350476.019	5015025.965
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S01	350177.65	5015304.164
S01	350168.942	5015313.701
S01	350165.549	5015311.05
S01	350150.342	5015327.786
S01	350169.972	5015345.351
S01	350182.595	5015356.647
S01	350196.599	5015359.286
S01	350204.273	5015350.909
S01	350207.291	5015346.328
S01	350209.118	5015337.455
S01	350200.93	5015335.569
S01	350198.855	5015326.267
S01	350197.439	5015321.911
S01	350193.582	5015318.297
S01	350184.844	5015310.363
S02	350200.93	5015335.569
S02	350209.118	5015337.455
S02	350215.262	5015309.144
S02	350227.076	5015307.139
S02	350228.288	5015297.311
S02	350215.081	5015294.443
S02	350214.891	5015293.867
S02	350217.754	5015290.668
S02	350198.158	5015273.127
S02	350194.923	5015276.741
S02	350194.429	5015276.768
S02	350194.17	5015276.536
S03	350193.252	5015276.587
S03	350194.429	5015276.768
S03	350194.923	5015276.741
S03	350198.158	5015273.127
S03	350217.754	5015290.668
S03	350214.891	5015293.867
S03	350215.081	5015294.443
S03	350228.295	5015297.318
S03	350196.633	5015269.95
S03	350183.588	5015284.926
S04	350155.738	5015284.72
S04	350159.373	5015280.428
S04	350126.935	5015251.392
S04	350100.074	5015282.781
S04	350136.045	5015314.992
S04	350140.179	5015310.41
S04	350144.135	5015309.53
S04	350157.317	5015293.332
S04	350153.453	5015289.791
S04	350155.738	5015284.72
S05	350140.179	5015310.41
S05	350136.045	5015314.992
S05	350150.342	5015327.795
S05	350165.549	5015311.059
S05	350168.941	5015313.711
S05	350189.982	5015290.669
S05	350168.345	5015271.31
S05	350162.87	5015277.22
S05	350161.176	5015279.124
S05	350160.952	5015278.924
S05	350159.502	5015280.544
S05	350159.373	5015280.428
S05	350155.738	5015284.72
S05	350153.453	5015289.791
S05	350157.317	5015293.332

S05	350144.135	5015309.53
S05	350140.179	5015310.41
S06	350126.935	5015251.392
S06	350159.502	5015280.544
S06	350160.952	5015278.924
S06	350161.176	5015279.124
S06	350162.87	5015277.22
S06	350168.345	5015271.301
S06	350129.089	5015236.177
S06	350126.935	5015251.392
S07	350100.074	5015282.781
S07	350126.935	5015251.392
S07	350129.089	5015236.177
S07	350093.341	5015276.753
S07	350100.074	5015282.781
S08_1	350145.703	5015323.624
S08_1	350140.479	5015329.438
S08_1	350179.362	5015364.268
S08_1	350182.364	5015361.059
S08_1	350182.743	5015356.675
S08_1	350182.595	5015356.647
S08_1	350148.071	5015325.743
S08_1	350145.703	5015323.624
S08_2	350140.479	5015329.438
S08_2	350145.703	5015323.624
S08_2	350093.341	5015276.753
S08_2	350088.191	5015282.599
S08_2	350140.479	5015329.438
S09	350182.743	5015356.675
S09	350182.364	5015361.059
S09	350179.362	5015364.268
S09	350181.891	5015366.534
S09	350201.662	5015365.507
S09	350217.048	5015348.568
S09	350217.665	5015347.856
S09	350218.257	5015347.124
S09	350218.823	5015346.372
S09	350219.362	5015345.6
S09	350219.874	5015344.81
S09	350220.359	5015344.003
S09	350220.815	5015343.179
S09	350221.242	5015342.34
S09	350221.639	5015341.486
S09	350222.007	5015340.619
S09	350222.344	5015339.74
S09	350222.65	5015338.85
S09	350222.925	5015337.95
S09	350223.169	5015337.04
S09	350223.381	5015336.123
S09	350223.56	5015335.199
S09	350223.708	5015334.269
S09	350227.076	5015307.139
S09	350215.262	5015309.144

S09	350207.291	5015346.328
S09	350204.273	5015350.909
S09	350196.599	5015359.286
S09	350182.743	5015356.675

[SYMBOLS]
;:Gage X-Coord Y-Coord
;-----
;
[PROFILES]
;:Name Links
;-----
"Node MHST09016 to Node OF-CREEK (Denham Way)" STM07876 STM45150 STM45151 STM45152 STM45153
"Node MHST09016 to Node OF-CREEK (Denham Way)" STM45154 STM45155 STM45156 STM45159 STM45160
"Node MHST09016 to Node OF-CREEK (Denham Way)" STM07871
"Node MHST09001 to Node OF-CREEK (Victor St)" STM07874 STM45163 STM45164_1 STM45164_2 STM45165
"Node MHST09001 to Node OF-CREEK (Victor St)" STM07857 STM07875 STM45161 STM45162 STM07873
"Node MHST09001 to Node OF-CREEK (Victor St)" STM45159 STM45160 STM07871
"Node MHST09024 to Node OF-CREEK (Savage Dr)" STM07872 STM07870 STM04620 STM04621 STM07871
"Node CBE04 to Node CBE15 (Perforated Pipes Along Hazeldean)" C28 C29 C30 C31 C32
"Node CBE04 to Node CBE15 (Perforated Pipes Along Hazeldean)" C33 C34 C35 C36 C37
"Node CBE04 to Node CBE15 (Perforated Pipes Along Hazeldean)" C38
"Node CBE04 to Node CBE15 (Perforated Pipes Along Hazeldean)" C38
"Node CBE01 to Node CHAMBERS-2 (Rear Perf Pipes)" C17 C18 C19 C20 C14
"Node CB03 to Node 205 (Through West Chambers 1)" C08 C09 C24 215-ICD
"Node 207 to Node 200 (Onsite Storm)" C01 C02 C03 C04 C05
"Node 207 to Node 200 (Onsite Storm)" C06 C25 C07 C10
"Node CB06 to Node 216 (Through East Chambers 1)" C23 C11 C16 C15 212-ICD
"Node CB01 to Node 216 (Through East Chambers 2)" C12 C16 C15 212-ICD

Updated PCSWMM Model to Include offsite Storm Sewer Analysis
 Full Dual Drainage Model
 J Fitzpatrick

WARNING 03: negative offset ignored for Link C01
 WARNING 03: negative offset ignored for Link C02
 WARNING 03: negative offset ignored for Link C16
 WARNING 03: negative offset ignored for Link C25
 WARNING 03: negative offset ignored for Link R10
 WARNING 03: negative offset ignored for Link R10
 WARNING 03: negative offset ignored for Link R16
 WARNING 03: negative offset ignored for Link R16
 WARNING 03: negative offset ignored for Link R17
 WARNING 03: negative offset ignored for Link R17
 WARNING 03: negative offset ignored for Link R18
 WARNING 03: negative offset ignored for Link R18
 WARNING 03: negative offset ignored for Link R19
 WARNING 03: negative offset ignored for Link R19
 WARNING 03: negative offset ignored for Link R20
 WARNING 03: negative offset ignored for Link R21
 WARNING 03: negative offset ignored for Link IN09009-INC
 WARNING 03: negative offset ignored for Link IN09010-ICD
 WARNING 03: negative offset ignored for Link IN09015-INC
 WARNING 02: maximum depth increased for Node IN09003-MAJ
 WARNING 02: maximum depth increased for Node IN09004-MAJ
 WARNING 02: maximum depth increased for Node IN09005-MAJ
 WARNING 02: maximum depth increased for Node IN09006-MAJ
 WARNING 02: maximum depth increased for Node IN09009-MAJ
 WARNING 02: maximum depth increased for Node IN09010-MAJ
 WARNING 02: maximum depth increased for Node IN09011-MAJ
 WARNING 02: maximum depth increased for Node IN09012-MAJ
 WARNING 02: maximum depth increased for Node IN09013-MAJ
 WARNING 02: maximum depth increased for Node IN09014-MAJ
 WARNING 02: maximum depth increased for Node IN09015-MAJ
 WARNING 02: maximum depth increased for Node IN09017-MAJ
 WARNING 02: maximum depth increased for Node IN09018-MAJ
 WARNING 02: maximum depth increased for Node IN09019-MAJ
 WARNING 02: maximum depth increased for Node IN09020-MAJ
 WARNING 02: maximum depth increased for Node IN09021-MAJ
 WARNING 02: maximum depth increased for Node IN09022-MAJ
 WARNING 02: maximum depth increased for Node IN09023-MAJ
 WARNING 02: maximum depth increased for Node IN09024-MAJ
 WARNING 02: maximum depth increased for Node IN09025-MAJ
 WARNING 02: maximum depth increased for Node IN09026-MAJ
 WARNING 02: maximum depth increased for Node IN09027-MAJ
 WARNING 02: maximum depth increased for Node IN09028-MAJ
 WARNING 02: maximum depth increased for Node IN09029-MAJ
 WARNING 02: maximum depth increased for Node IN09030-MAJ
 WARNING 02: maximum depth increased for Node IN09031-MAJ

WARNING 02: maximum depth increased for Node IN09032-MAJ
 WARNING 02: maximum depth increased for Node IN09033-MAJ
 WARNING 02: maximum depth increased for Node IN09034-MAJ
 WARNING 02: maximum depth increased for Node IN09035-MAJ
 WARNING 02: maximum depth increased for Node J1
 WARNING 02: maximum depth increased for Node J2

 Element Count

 Number of rain gages 3
 Number of subcatchments ... 64
 Number of nodes 143
 Number of links 177
 Number of pollutants 0
 Number of land uses 0

 Raingage Summary

Name	Data Source	Data Type	Recording Interval
Chicago_3h_100yr	Chicago_3h_100yr	INTENSITY	10 min.
Chicago_3h_2year	Chicago_3h_2yr	INTENSITY	10 min.
Chicago_3h_5year	Chicago_3h_5year	INTENSITY	10 min.

 Subcatchment Summary

Name	Area	Width	%Imperv	%Slope	Rain Gage	Outlet
ES01_1	0.33	57.00	67.78	1.5000	Chicago_3h_100yr	IN103407
ES02_1	0.09	48.80	31.29	1.0000	Chicago_3h_100yr	IN09004-MAJ
ES02_2	0.05	36.70	44.98	1.0000	Chicago_3h_100yr	IN09003-MAJ
ES03_1	0.28	132.10	55.55	1.0000	Chicago_3h_100yr	IN09005-MAJ
ES03_2	0.19	114.50	50.13	1.0000	Chicago_3h_100yr	IN09006-MAJ
ES04_1	0.21	98.10	59.96	0.5000	Chicago_3h_100yr	IN09008
ES04_2	0.20	98.00	55.14	0.5000	Chicago_3h_100yr	IN09007
ES05_1	0.19	91.60	52.18	0.5000	Chicago_3h_100yr	IN09009-MAJ
ES05_2	0.18	89.90	54.38	0.5000	Chicago_3h_100yr	IN09010-MAJ
ES06_1	0.28	134.90	59.04	0.5000	Chicago_3h_100yr	IN09011-MAJ
ES06_2	0.24	123.40	55.20	0.5000	Chicago_3h_100yr	IN09012-MAJ
ES07	0.21	96.70	55.58	0.5000	Chicago_3h_100yr	IN09013-MAJ
ES08_1	0.12	85.10	44.67	0.5000	Chicago_3h_100yr	IN09022-MAJ
ES08_2	0.09	47.20	29.63	0.5000	Chicago_3h_100yr	IN09023-MAJ
ES09_1	0.17	96.60	53.85	0.5000	Chicago_3h_100yr	IN09024-MAJ
ES09_2	0.18	125.60	40.27	0.5000	Chicago_3h_100yr	IN09025-MAJ
ES10_1	0.21	108.10	50.25	0.5000	Chicago_3h_100yr	IN09026-MAJ
ES10_2	0.18	110.00	48.55	0.5000	Chicago_3h_100yr	IN09027-MAJ
ES11_1	0.18	88.30	55.00	0.5000	Chicago_3h_100yr	IN09029-MAJ

ES11_2	0.13	71.20	44.55	0.5000	Chicago_3h_100yr	IN09028-MAJ
ES12_1	0.19	92.70	56.58	0.5000	Chicago_3h_100yr	MHST09022
ES12_2	0.16	77.30	55.36	0.5000	Chicago_3h_100yr	IN09031-MAJ
ES13_1	0.16	69.90	56.35	0.5000	Chicago_3h_100yr	MHST09023
ES13_2	0.17	85.30	53.56	0.5000	Chicago_3h_100yr	MHST09023
ES14_1	0.13	97.60	42.85	0.5000	Chicago_3h_100yr	IN09014-MAJ
ES14_2	0.18	88.70	60.09	0.5000	Chicago_3h_100yr	IN09015-MAJ
ES15_1	0.07	75.60	37.06	0.5000	Chicago_3h_100yr	IN09016
ES15_2	0.12	70.50	57.09	0.5000	Chicago_3h_100yr	MHST09012
ES16_1	0.10	107.50	35.74	1.5000	Chicago_3h_100yr	IN09034-MAJ
ES16_2	0.17	100.20	26.88	1.5000	Chicago_3h_100yr	IN09035-MAJ
ES17	0.14	78.50	41.72	2.0000	Chicago_3h_100yr	IN09034-MAJ
ES18	0.24	93.30	40.76	2.0000	Chicago_3h_100yr	IN09021-MAJ
ES19	0.10	46.40	63.06	0.5000	Chicago_3h_100yr	IN09019-MAJ
ES20	0.07	32.30	33.18	0.5000	Chicago_3h_100yr	IN09020-MAJ
ES21_1	0.08	36.80	58.87	0.5000	Chicago_3h_100yr	IN09018-MAJ
ES21_3	0.13	60.80	42.56	0.5000	Chicago_3h_100yr	IN09020-MAJ
ES21_4	0.14	60.30	62.82	0.5000	Chicago_3h_100yr	IN09019-MAJ
ES21_5	0.09	36.20	54.72	0.5000	Chicago_3h_100yr	IN09017-MAJ
ES22_1	0.18	74.80	62.63	0.5000	Chicago_3h_100yr	IN09016
ES22_2	0.22	100.50	55.46	0.5000	Chicago_3h_100yr	MHST09012
ES23	0.18	22.50	32.55	1.0000	Chicago_3h_100yr	IN45587
ES24	0.08	15.80	27.01	1.0000	Chicago_3h_100yr	IN45588
ES25	0.19	16.60	27.25	1.0000	Chicago_3h_100yr	IN45589
ES26	0.11	17.70	32.21	1.0000	Chicago_3h_100yr	IN45590
ES27	0.37	52.40	13.47	1.0000	Chicago_3h_100yr	IN45575
ES28	0.34	50.10	21.80	1.0000	Chicago_3h_100yr	IN45570
ES29	0.33	46.00	26.73	1.0000	Chicago_3h_100yr	IN45569
ES30	0.23	47.40	28.57	1.0000	Chicago_3h_100yr	IN45572
ES31	0.19	48.30	24.97	1.0000	Chicago_3h_100yr	IN45577
ES32	0.79	57.10	19.91	1.0000	Chicago_3h_100yr	IN07998
ES33	0.16	51.30	31.77	1.0000	Chicago_3h_100yr	IN45573
ES34	0.41	54.30	10.08	1.0000	Chicago_3h_100yr	IN45574
ES35	0.97	66.50	14.69	1.0000	Chicago_3h_100yr	IN45566
ES36	0.22	113.80	32.12	0.5000	Chicago_3h_100yr	IN09032-MAJ
S01	0.18	58.00	80.67	1.0000	Chicago_3h_100yr	CB06
S02	0.15	51.70	88.23	1.0000	Chicago_3h_100yr	CB01
S03	0.02	80.90	14.52	1.0000	Chicago_3h_100yr	CB01
S04	0.20	70.20	79.11	1.0000	Chicago_3h_100yr	CB03
S05	0.13	53.10	73.96	1.0000	Chicago_3h_100yr	218
S06	0.06	52.30	35.84	1.0000	Chicago_3h_100yr	CBT03
S07	0.04	54.60	37.94	1.0000	Chicago_3h_100yr	CBE01
S08_1	0.04	57.86	59.42	1.0000	Chicago_3h_100yr	CBT14
S08_2	0.05	78.29	54.84	1.0000	Chicago_3h_100yr	CBE04
S09	0.08	94.80	71.20	1.0000	Chicago_3h_100yr	IN103407

Node Summary

Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
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200	JUNCTION	111.14	2.76	0.0	
201	JUNCTION	111.34	2.54	0.0	
202	JUNCTION	111.46	2.44	0.0	
203	JUNCTION	111.61	2.54	0.0	Yes
204	JUNCTION	111.70	2.35	0.0	Yes
205	JUNCTION	111.88	2.25	0.0	Yes
206	JUNCTION	112.42	2.30	0.0	Yes
207	JUNCTION	113.28	1.97	0.0	Yes
208	JUNCTION	112.57	1.94	0.0	
210	JUNCTION	112.16	2.12	0.0	
211	JUNCTION	111.81	2.24	0.0	
212	JUNCTION	111.42	2.70	0.0	
213	JUNCTION	112.82	1.50	0.0	
215	JUNCTION	112.24	2.26	0.0	
216	JUNCTION	111.32	2.51	0.0	
217	JUNCTION	113.46	1.50	0.0	
218	JUNCTION	112.74	1.26	0.0	
219	JUNCTION	111.30	2.47	0.0	
CB03	JUNCTION	113.10	1.15	0.0	
CB05	JUNCTION	114.00	1.06	0.0	
CBE01	JUNCTION	114.25	1.06	0.0	
CBE04	JUNCTION	113.90	1.00	0.0	
CBT02	JUNCTION	114.11	1.06	0.0	
CBT03	JUNCTION	113.78	1.06	0.0	
CBT05	JUNCTION	113.79	1.02	0.0	
CBT06	JUNCTION	113.68	1.04	0.0	
CBT07	JUNCTION	113.61	1.05	0.0	
CBT08	JUNCTION	113.52	1.16	0.0	
CBT09	JUNCTION	113.39	1.08	0.0	
CBT10	JUNCTION	113.28	1.07	0.0	
CBT11	JUNCTION	112.86	1.44	0.0	
CBT12	JUNCTION	112.89	1.39	0.0	
CBT13	JUNCTION	112.92	1.14	0.0	
CBT14	JUNCTION	112.94	1.08	0.0	
IN07998	JUNCTION	110.43	1.40	0.0	
IN09003-MAJ	JUNCTION	113.93	0.20	0.0	
IN09004-MAJ	JUNCTION	113.83	0.20	0.0	
IN09005-MAJ	JUNCTION	113.22	0.20	0.0	
IN09006-MAJ	JUNCTION	113.22	0.20	0.0	
IN09009-MAJ	JUNCTION	112.75	0.20	0.0	
IN09010-MAJ	JUNCTION	112.75	0.20	0.0	
IN09011-MAJ	JUNCTION	112.21	0.20	0.0	
IN09012-MAJ	JUNCTION	112.21	0.20	0.0	
IN09013-MAJ	JUNCTION	111.78	0.20	0.0	
IN09014-MAJ	JUNCTION	111.41	0.20	0.0	
IN09015-MAJ	JUNCTION	111.41	0.20	0.0	
IN09017-MAJ	JUNCTION	111.56	0.20	0.0	
IN09018-MAJ	JUNCTION	111.56	0.20	0.0	
IN09019-MAJ	JUNCTION	111.33	0.20	0.0	
IN09020-MAJ	JUNCTION	111.33	0.20	0.0	
IN09021-MAJ	JUNCTION	111.00	0.20	0.0	
IN09022-MAJ	JUNCTION	113.94	0.20	0.0	
IN09023-MAJ	JUNCTION	113.75	0.20	0.0	

IN09024-MAJ	JUNCTION	113.15	0.20	0.0
IN09025-MAJ	JUNCTION	113.13	0.20	0.0
IN09026-MAJ	JUNCTION	112.66	0.20	0.0
IN09027-MAJ	JUNCTION	112.68	0.20	0.0
IN09028-MAJ	JUNCTION	112.36	0.20	0.0
IN09029-MAJ	JUNCTION	112.37	0.20	0.0
IN09030-MAJ	JUNCTION	111.97	0.20	0.0
IN09031-MAJ	JUNCTION	111.97	0.20	0.0
IN09032-MAJ	JUNCTION	111.62	0.20	0.0
IN09033-MAJ	JUNCTION	111.62	0.20	0.0
IN09034-MAJ	JUNCTION	111.27	0.20	0.0
IN09035-MAJ	JUNCTION	111.27	0.20	0.0
IN45566	JUNCTION	109.82	1.39	0.0
IN45569	JUNCTION	111.61	1.40	0.0
IN45570	JUNCTION	111.70	1.40	0.0
IN45572	JUNCTION	111.51	1.40	0.0
IN45573	JUNCTION	112.76	1.40	0.0
IN45574	JUNCTION	111.30	0.30	0.0
IN45575	JUNCTION	112.17	1.40	0.0
IN45577	JUNCTION	111.28	1.40	0.0
IN45587	JUNCTION	112.44	1.41	0.0
IN45588	JUNCTION	112.52	1.40	0.0
IN45589	JUNCTION	111.85	1.40	0.0
IN45590	JUNCTION	111.58	1.40	0.0
J1	JUNCTION	111.77	0.20	0.0
J2	JUNCTION	111.20	0.20	0.0
MHST09001	JUNCTION	111.29	1.85	0.0
MHST09002	JUNCTION	111.25	1.97	0.0
MHST09003	JUNCTION	111.15	2.69	0.0
MHST09004	JUNCTION	111.02	3.01	0.0
MHST09005	JUNCTION	110.43	3.07	0.0
MHST09006	JUNCTION	110.07	2.86	0.0
MHST09007	JUNCTION	109.61	3.22	0.0
MHST09008	JUNCTION	109.27	3.15	0.0
MHST09009	JUNCTION	109.21	3.07	0.0
MHST09010	JUNCTION	108.65	3.32	0.0
MHST09011	JUNCTION	108.29	3.38	0.0
MHST09013	JUNCTION	108.16	3.43	0.0
MHST09014	JUNCTION	108.38	3.12	0.0
MHST09015	JUNCTION	108.53	3.27	0.0
MHST09016	JUNCTION	110.98	3.20	0.0
MHST09017	JUNCTION	110.75	3.35	0.0
MHST09018	JUNCTION	110.66	3.21	0.0
MHST09019	JUNCTION	110.38	2.90	0.0
MHST09020	JUNCTION	109.94	2.99	0.0
MHST09021	JUNCTION	109.05	3.48	0.0
MHST09022	JUNCTION	108.93	3.34	0.0
MHST09023	JUNCTION	108.79	3.01	0.0
MHST09024	JUNCTION	108.86	2.53	0.0
OF-CREEK	OUTFALL	107.50	0.90	0.0
OF-HAZELDEAN	OUTFALL	112.83	0.30	0.0
CB01	STORAGE	112.40	1.40	0.0
CB06	STORAGE	112.50	1.40	0.0

CHAMBERS-1	STORAGE	111.52	2.58	0.0
CHAMBERS-2	STORAGE	112.30	2.20	0.0
IN09003	STORAGE	112.53	1.40	0.0
IN09004	STORAGE	112.43	1.55	0.0
IN09005	STORAGE	111.82	1.40	0.0
IN09006	STORAGE	111.82	1.40	0.0
IN09007	STORAGE	111.58	1.55	0.0
IN09008	STORAGE	111.58	1.55	0.0
IN09009	STORAGE	111.35	1.40	0.0
IN09010	STORAGE	111.35	1.40	0.0
IN09011	STORAGE	110.81	1.40	0.0
IN09012	STORAGE	110.81	1.40	0.0
IN09013	STORAGE	110.38	1.40	0.0
IN09014	STORAGE	110.01	1.40	0.0
IN09015	STORAGE	110.01	1.40	0.0
IN09016	STORAGE	109.85	1.55	0.0
IN09017	STORAGE	110.16	1.40	0.0
IN09018	STORAGE	110.16	1.40	0.0
IN09019	STORAGE	109.93	1.40	0.0
IN09020	STORAGE	109.93	1.40	0.0
IN09021	STORAGE	109.60	1.40	0.0
IN09022	STORAGE	112.54	1.40	0.0
IN09023	STORAGE	112.35	1.40	0.0
IN09024	STORAGE	111.75	1.40	0.0
IN09025	STORAGE	111.73	1.40	0.0
IN09026	STORAGE	111.26	1.40	0.0
IN09027	STORAGE	111.28	1.40	0.0
IN09028	STORAGE	110.96	1.40	0.0
IN09029	STORAGE	110.97	1.40	0.0
IN09030	STORAGE	110.57	1.40	0.0
IN09031	STORAGE	110.57	1.40	0.0
IN09032	STORAGE	110.22	1.40	0.0
IN09033	STORAGE	110.22	1.40	0.0
IN09034	STORAGE	109.87	1.40	0.0
IN09035	STORAGE	109.87	1.40	0.0
IN103407	STORAGE	111.64	1.61	0.0
MHST09012	STORAGE	107.61	3.52	0.0

Link Summary

Name	From Node	To Node	Type	Length	%Slope	Roughness
C01	207	206	CONDUIT	15.8	5.1594	0.0130
C02	206	205	CONDUIT	46.8	0.8489	0.0130
C03	205	204	CONDUIT	44.5	0.3373	0.0130
C04	204	203	CONDUIT	8.5	0.3519	0.0130
C05	203	202	CONDUIT	35.1	0.3422	0.0130
C06	202	201	CONDUIT	11.5	0.3491	0.0130
C07	216	219	CONDUIT	10.3	0.2143	0.0130
C08	CB03	208	CONDUIT	15.0	3.5978	0.0100
C09	208	CHAMBERS-2	CONDUIT	1.5	1.0001	0.0130

C1	IN45587	MHST09004	CONDUIT	40.0	1.0001	0.0130
C10	219	200	CONDUIT	10.7	0.9507	0.0130
C11	210	211	CONDUIT	15.3	1.0429	0.0130
C12	CB01	211	CONDUIT	16.0	1.3093	0.0130
C13	IN07998	MHST09011	CONDUIT	10.0	1.0001	0.0130
C14	217	CHAMBERS-2	CONDUIT	7.6	7.2824	0.0130
C15	CHAMBERS-1	212	CONDUIT	23.7	0.1688	0.0130
C16	211	CHAMBERS-1	CONDUIT	2.5	1.6002	0.0130
C17	CBE01	CBT02	CONDUIT	22.2	0.6161	0.0130
C18	CBT02	CB05	CONDUIT	22.2	0.4902	0.0130
C19	CB05	CBT03	CONDUIT	35.1	0.6270	0.0130
C2	IN45588	MHST09005	CONDUIT	116.3	0.4298	0.0130
C20	CBT03	217	CONDUIT	22.9	1.1974	0.0130
C21	218	208	CONDUIT	15.2	0.9300	0.0130
C22	IN45573	MHST09016	CONDUIT	40.0	1.2501	0.0130
C23	CB06	210	CONDUIT	11.3	1.6836	0.0130
C24	CHAMBERS-2	215	CONDUIT	1.5	2.6676	0.0130
C25	201	216	CONDUIT	6.4	0.4972	0.0130
C26	IN45574	MHST09017	CONDUIT	40.0	0.7500	0.0130
C27	IN45566	MHST09024	CONDUIT	10.0	1.0001	0.0130
C28	CBE04	CBT05	CONDUIT	11.4	0.9996	0.0130
C29	CBT05	CBT06	CONDUIT	10.5	1.0060	0.0130
C3	IN45589	MHST09007	CONDUIT	40.0	1.0001	0.0130
C30	CBT06	CBT07	CONDUIT	6.7	1.0056	0.0130
C31	CBT07	CBT08	CONDUIT	9.8	1.0014	0.0130
C32	CBT08	CBT09	CONDUIT	12.7	1.0043	0.0130
C33	CBT09	CBT10	CONDUIT	11.2	1.0027	0.0130
C34	CBT10	213	CONDUIT	3.3	1.0016	0.0130
C35	CBT11	213	CONDUIT	3.3	0.3035	0.0130
C36	CBT12	CBT11	CONDUIT	9.5	0.3044	0.0130
C37	CBT13	CBT12	CONDUIT	12.7	0.3060	0.0130
C38	CBT14	CBT13	CONDUIT	12.7	0.2982	0.0130
C39	IN103407	OF-HAZELDEAN	CONDUIT	40.3	0.5205	0.0130
C4	IN45590	MHST09007	CONDUIT	40.0	1.2501	0.0130
C40	213	218	CONDUIT	29.3	0.3007	0.0130
C5	IN45575	MHST09019	CONDUIT	40.0	1.0001	0.0130
C6	IN45570	MHST09020	CONDUIT	40.0	1.0001	0.0130
C7	IN45569	MHST09021	CONDUIT	40.0	0.5000	0.0130
C8	IN45572	MHST09021	CONDUIT	40.0	1.0001	0.0130
C9	IN45577	MHST09022	CONDUIT	40.0	1.0001	0.0130
C98	CHAMBERS-1	212	CONDUIT	26.5	0.3621	0.0130
C99	CHAMBERS-2	215	CONDUIT	28.6	0.0908	0.0130
OF1	IN09016	MHST09012	CONDUIT	17.9	1.5198	0.0130
R01	IN09044-MAJ	IN09006-MAJ	CONDUIT	92.7	0.6582	0.0130
R02	IN09006-MAJ	IN09007	CONDUIT	79.6	0.1131	0.0130
R03	IN09005-MAJ	IN09008	CONDUIT	79.2	0.3030	0.0130
R04	IN09007	IN09010-MAJ	CONDUIT	71.6	0.5311	0.0130
R05	IN09008	IN09009-MAJ	CONDUIT	72.2	0.3185	0.0130
R06	IN09010-MAJ	IN09012-MAJ	CONDUIT	102.0	0.5295	0.0130
R07	IN09009-MAJ	IN09011-MAJ	CONDUIT	106.2	0.5083	0.0130
R08	IN09012-MAJ	J1	CONDUIT	98.2	0.4481	0.0130
R09	IN09033-MAJ	J1	CONDUIT	13.7	-1.0926	0.0130
R10	IN09032-MAJ	J1	CONDUIT	24.2	-0.6203	0.0130

R11	IN09011-MAJ	IN09013-MAJ	CONDUIT	92.0	0.4674	0.0130
R12	IN09013-MAJ	IN09015-MAJ	CONDUIT	71.8	0.5157	0.0130
R13	IN09015-MAJ	MHST09012	CONDUIT	64.1	0.4402	0.0130
R14	IN09014-MAJ	IN09016	CONDUIT	54.5	0.2937	0.0130
R15	J1	IN09014-MAJ	CONDUIT	59.6	0.6039	0.0130
R16	IN09035-MAJ	J2	CONDUIT	17.7	0.3945	0.0130
R17	IN09034-MAJ	J2	CONDUIT	26.1	0.2680	0.0130
R18	IN09021-MAJ	IN09020-MAJ	CONDUIT	30.5	-1.0809	0.0130
R19	J2	IN09019-MAJ	CONDUIT	27.5	-0.4731	0.0130
R20	IN09020-MAJ	IN09018-MAJ	CONDUIT	80.6	-0.2853	0.0130
R21	IN09019-MAJ	IN09017-MAJ	CONDUIT	81.1	-0.2837	0.0130
R22	IN09018-MAJ	MHST09012	CONDUIT	83.6	0.5168	0.0130
R23	IN09017-MAJ	IN09016	CONDUIT	67.8	0.4574	0.0130
R24	IN09003-MAJ	IN103407	CONDUIT	71.3	1.2492	0.0130
R25	IN09023-MAJ	IN09024-MAJ	CONDUIT	81.4	0.7369	0.0130
R26	IN09022-MAJ	IN09025-MAJ	CONDUIT	86.5	0.9367	0.0130
R27	IN09025-MAJ	IN09027-MAJ	CONDUIT	86.0	0.5232	0.0130
R28	IN09024-MAJ	IN09026-MAJ	CONDUIT	85.8	0.5711	0.0130
R29	IN09027-MAJ	IN09028-MAJ	CONDUIT	61.8	0.5175	0.0130
R30	IN09026-MAJ	IN09029-MAJ	CONDUIT	68.1	0.4259	0.0130
R31	IN09029-MAJ	IN09030-MAJ	CONDUIT	72.3	0.5536	0.0130
R32	IN09028-MAJ	IN09034-MAJ	CONDUIT	88.1	1.2372	0.0130
R33	IN09030-MAJ	IN09032-MAJ	CONDUIT	67.3	0.5202	0.0130
R34	IN09031-MAJ	IN09033-MAJ	CONDUIT	69.9	0.5008	0.0130
STM04620	MHST09014	MHST09013	CONDUIT	76.3	0.2096	0.0130
STM04621	MHST09013	MHST09012	CONDUIT	78.0	0.2051	0.0130
STM07857	MHST09005	MHST09006	CONDUIT	90.1	0.3995	0.0130
STM07870	MHST09015	MHST09014	CONDUIT	51.7	0.1547	0.0130
STM07871	MHST09012	OF-CREEK	CONDUIT	44.6	0.2467	0.0130
STM07872	MHST09024	MHST09015	CONDUIT	65.6	0.3813	0.0130
STM07873	MHST09009	MHST09010	CONDUIT	81.5	0.3434	0.0130
STM07874	MHST09001	MHST09002	CONDUIT	10.4	0.3837	0.0130
STM07875	MHST09006	MHST09007	CONDUIT	90.0	0.4001	0.0130
STM07876	MHST09016	MHST09017	CONDUIT	39.5	0.3802	0.0130
STM45150	MHST09017	MHST09018	CONDUIT	13.5	0.3709	0.0130
STM45151	MHST09018	MHST09019	CONDUIT	52.8	0.3976	0.0130
STM45152	MHST09019	MHST09020	CONDUIT	90.1	0.3996	0.0130
STM45153	MHST09020	MHST09021	CONDUIT	89.4	0.9061	0.0130
STM45154	MHST09021	MHST09022	CONDUIT	58.9	0.2036	0.0130
STM45155	MHST09022	MHST09023	CONDUIT	56.8	0.2465	0.0130
STM45156	MHST09023	MHST09010	CONDUIT	41.5	0.3132	0.0130
STM45159	MHST09010	MHST09011	CONDUIT	75.1	0.4795	0.0130
STM45160	MHST09011	MHST09012	CONDUIT	58.2	0.5157	0.0130
STM45161	MHST09007	MHST09008	CONDUIT	88.1	0.3518	0.0130
STM45162	MHST09008	MHST09009	CONDUIT	12.7	0.1577	0.0130
STM45163	MHST09002	MHST09003	CONDUIT	36.6	0.2736	0.0130
STM45164_1	MHST09003	200	CONDUIT	4.7	0.2980	0.0130
STM45164_2	200	MHST09004	CONDUIT	11.9	0.3024	0.0130
STM45165	MHST09004	MHST09005	CONDUIT	82.9	0.6151	0.0130
212-ICD	212	216	OUTLET			
215-ICD	215	205	OUTLET			
IN09003-ICD	IN09003	MHST09003	OUTLET			
IN09003-INC	IN09003	IN09003	OUTLET			

IN09004-ICD	IN09004	MHST09004	OUTLET
IN09004-INC	IN09004-MAJ	IN09004	OUTLET
IN09005-ICD	IN09005	MHST09005	OUTLET
IN09005-INC	IN09005-MAJ	IN09005	OUTLET
IN09006-ICD	IN09006	MHST09005	OUTLET
IN09006-INC	IN09006-MAJ	IN09006	OUTLET
IN09007-ICD	IN09007	MHST09006	OUTLET
IN09008-ICD	IN09008	MHST09006	OUTLET
IN09009-ICD	IN09009	MHST09007	OUTLET
IN09009-INC	IN09009-MAJ	IN09009	OUTLET
IN09010-ICD	IN09010	MHST09007	OUTLET
IN09010-INC	IN09010-MAJ	IN09010	OUTLET
IN09011-ICD	IN09011	MHST09008	OUTLET
IN09011-INC	IN09011-MAJ	IN09011	OUTLET
IN09012-ICD	IN09012	MHST09008	OUTLET
IN09012-INC	IN09012-MAJ	IN09012	OUTLET
IN09013-ICD	IN09013	MHST09010	OUTLET
IN09013-INC	IN09013-MAJ	IN09013	OUTLET
IN09014-ICD	IN09014	MHST09011	OUTLET
IN09014-INC	IN09014-MAJ	IN09014	OUTLET
IN09015-ICD	IN09015	MHST09011	OUTLET
IN09015-INC	IN09015-MAJ	IN09015	OUTLET
IN09016-ICD	IN09016	MHST09013	OUTLET
IN09017-ICD	IN09017	MHST09013	OUTLET
IN09017-INC	IN09017-MAJ	IN09017	OUTLET
IN09018-ICD	IN09018	MHST09013	OUTLET
IN09018-INC	IN09018-MAJ	IN09018	OUTLET
IN09019-ICD	IN09019	MHST09014	OUTLET
IN09019-INC	IN09019-MAJ	IN09019	OUTLET
IN09020-ICD	IN09020	MHST09014	OUTLET
IN09020-INC	IN09020-MAJ	IN09020	OUTLET
IN09021-ICD	IN09021	MHST09015	OUTLET
IN09021-INC	IN09021-MAJ	IN09021	OUTLET
IN09022-ICD	IN09022	MHST09017	OUTLET
IN09022-INC	IN09022-MAJ	IN09022	OUTLET
IN09023-ICD	IN09023	MHST09017	OUTLET
IN09023-INC	IN09023-MAJ	IN09023	OUTLET
IN09024-ICD	IN09024	MHST09019	OUTLET
IN09024-INC	IN09024-MAJ	IN09024	OUTLET
IN09025-ICD	IN09025	MHST09019	OUTLET
IN09025-INC	IN09025-MAJ	IN09025	OUTLET
IN09026-ICD	IN09026	MHST09020	OUTLET
IN09026-INC	IN09026-MAJ	IN09026	OUTLET
IN09027-ICD	IN09027	MHST09020	OUTLET
IN09027-INC	IN09027-MAJ	IN09027	OUTLET
IN09028-ICD	IN09028	MHST09021	OUTLET
IN09028-INC	IN09028-MAJ	IN09028	OUTLET
IN09029-ICD	IN09029	MHST09021	OUTLET
IN09029-INC	IN09029-MAJ	IN09029	OUTLET
IN09030-ICD	IN09030	MHST09022	OUTLET
IN09030-INC	IN09030-MAJ	IN09030	OUTLET
IN09031-ICD	IN09031	MHST09022	OUTLET
IN09031-INC	IN09031-MAJ	IN09031	OUTLET

IN09032-ICD	IN09032	MHST09023	OUTLET
IN09032-INC	IN09032-MAJ	IN09032	OUTLET
IN09033-ICD	IN09033	MHST09023	OUTLET
IN09033-INC	IN09033-MAJ	IN09033	OUTLET
IN09034-ICD	IN09034	MHST09024	OUTLET
IN09034-INC	IN09034-MAJ	IN09034	OUTLET
IN09035-ICD	IN09035	MHST09024	OUTLET
IN09035-INC	IN09035-MAJ	IN09035	OUTLET
IN103407-ICD	IN103407	MHST09001	OUTLET

Cross Section Summary

Conduit	Shape	Full Depth	Full Area	Hyd. Rad.	Max. Width	No. of Barrels	Full Flow
C01	CIRCULAR	0.25	0.05	0.06	0.25	1	135.08
C02	CIRCULAR	0.25	0.05	0.06	0.25	1	54.79
C03	CIRCULAR	0.38	0.11	0.09	0.38	1	101.83
C04	CIRCULAR	0.38	0.11	0.09	0.38	1	104.01
C05	CIRCULAR	0.38	0.11	0.09	0.38	1	102.57
C06	CIRCULAR	0.38	0.11	0.09	0.38	1	103.60
C07	CIRCULAR	0.38	0.11	0.09	0.38	1	81.18
C08	CIRCULAR	0.30	0.07	0.07	0.30	1	238.46
C09	CIRCULAR	0.60	0.28	0.15	0.60	1	614.06
C1	CIRCULAR	0.20	0.03	0.05	0.20	1	32.80
C10	CIRCULAR	0.38	0.11	0.09	0.38	1	170.97
C11	CIRCULAR	0.30	0.07	0.07	0.30	1	98.76
C12	CIRCULAR	0.30	0.07	0.07	0.30	1	110.65
C13	CIRCULAR	0.20	0.03	0.05	0.20	1	32.80
C14	CIRCULAR	0.30	0.07	0.07	0.30	1	260.97
C15	CIRCULAR	0.38	0.11	0.09	0.38	1	72.03
C16	CIRCULAR	0.60	0.28	0.15	0.60	1	776.77
C17	CIRCULAR	0.25	0.05	0.06	0.25	1	46.68
C18	CIRCULAR	0.25	0.05	0.06	0.25	1	41.64
C19	CIRCULAR	0.25	0.05	0.06	0.25	1	47.09
C2	CIRCULAR	0.20	0.03	0.05	0.20	1	21.50
C20	CIRCULAR	0.25	0.05	0.06	0.25	1	65.08
C21	CIRCULAR	0.30	0.07	0.07	0.30	1	93.26
C22	CIRCULAR	0.20	0.03	0.05	0.20	1	36.67
C23	CIRCULAR	0.30	0.07	0.07	0.30	1	125.48
C24	CIRCULAR	0.38	0.11	0.09	0.38	1	286.38
C25	CIRCULAR	0.38	0.11	0.09	0.38	1	123.64
C26	CIRCULAR	0.20	0.03	0.05	0.20	1	28.41
C27	CIRCULAR	0.20	0.03	0.05	0.20	1	32.80
C28	CIRCULAR	0.25	0.05	0.06	0.25	1	59.46
C29	CIRCULAR	0.25	0.05	0.06	0.25	1	59.65
C3	CIRCULAR	0.20	0.03	0.05	0.20	1	32.80
C30	CIRCULAR	0.25	0.05	0.06	0.25	1	59.64
C31	CIRCULAR	0.25	0.05	0.06	0.25	1	59.51
C32	CIRCULAR	0.25	0.05	0.06	0.25	1	59.60
C33	CIRCULAR	0.25	0.05	0.06	0.25	1	59.55

C34	CIRCULAR	0.25	0.05	0.06	0.25	1	59.52
C35	CIRCULAR	0.25	0.05	0.06	0.25	1	32.76
C36	CIRCULAR	0.25	0.05	0.06	0.25	1	32.81
C37	CIRCULAR	0.25	0.05	0.06	0.25	1	32.90
C38	CIRCULAR	0.25	0.05	0.06	0.25	1	32.47
C39	TRAPEZOIDAL	0.30	0.57	0.20	2.80	1	1070.08
C4	CIRCULAR	0.20	0.03	0.05	0.20	1	36.67
C40	CIRCULAR	0.30	0.07	0.07	0.30	1	53.03
C5	CIRCULAR	0.20	0.03	0.05	0.20	1	32.80
C6	CIRCULAR	0.20	0.03	0.05	0.20	1	32.80
C7	CIRCULAR	0.20	0.03	0.05	0.20	1	23.19
C8	CIRCULAR	0.20	0.03	0.05	0.20	1	32.80
C9	CIRCULAR	0.20	0.03	0.05	0.20	1	32.80
C98	CIRCULAR	0.10	0.01	0.03	0.10	1	3.11
C99	CIRCULAR	0.10	0.01	0.03	0.10	1	1.56
OF1	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	1552.15
R01	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	1021.45
R02	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	423.38
R03	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	693.06
R04	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	917.52
R05	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	710.59
R06	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	916.20
R07	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	897.66
R08	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	842.83
R09	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	1316.06
R10	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	991.63
R11	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	860.77
R12	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	904.10
R13	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	835.38
R14	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	682.29
R15	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	978.40
R16	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	790.77
R17	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	651.76
R18	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	1308.97
R19	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	866.03
R20	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	672.53
R21	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	670.58
R22	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	905.11
R23	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	851.52
R24	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	1407.17
R25	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	1080.77
R26	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	1218.50
R27	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	910.70
R28	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	951.44
R29	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	905.74
R30	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	821.66
R31	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	936.79
R32	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	1400.42
R33	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	908.08
R34	Half_Street_4.25m	0.20	0.82	0.09	8.42	1	890.97
STM04620	CIRCULAR	0.53	0.22	0.13	0.53	1	196.89
STM04621	CIRCULAR	0.60	0.28	0.15	0.60	1	278.12
STM07857	CIRCULAR	0.53	0.22	0.13	0.53	1	271.84

STM07870	CIRCULAR	0.45	0.16	0.11	0.45	1	112.14
STM07871	CIRCULAR	0.90	0.64	0.23	0.90	1	899.20
STM07872	CIRCULAR	0.38	0.11	0.09	0.38	1	108.27
STM07873	CIRCULAR	0.60	0.28	0.15	0.60	1	359.85
STM07874	CIRCULAR	0.38	0.11	0.09	0.38	1	108.61
STM07875	CIRCULAR	0.53	0.22	0.13	0.53	1	272.03
STM07876	CIRCULAR	0.30	0.07	0.07	0.30	1	59.63
STM45150	CIRCULAR	0.38	0.11	0.09	0.38	1	106.78
STM45151	CIRCULAR	0.38	0.11	0.09	0.38	1	110.57
STM45152	CIRCULAR	0.45	0.16	0.11	0.45	1	180.23
STM45153	CIRCULAR	0.53	0.22	0.13	0.53	1	409.40
STM45154	CIRCULAR	0.60	0.28	0.15	0.60	1	277.09
STM45155	CIRCULAR	0.60	0.28	0.15	0.60	1	304.85
STM45156	CIRCULAR	0.60	0.28	0.15	0.60	1	343.62
STM45159	CIRCULAR	0.75	0.44	0.19	0.75	1	770.94
STM45160	CIRCULAR	0.75	0.44	0.19	0.75	1	799.49
STM45161	CIRCULAR	0.60	0.28	0.15	0.60	1	364.22
STM45162	CIRCULAR	0.60	0.28	0.15	0.60	1	243.84
STM45163	CIRCULAR	0.38	0.11	0.09	0.38	1	91.71
STM45164_1	CIRCULAR	0.38	0.11	0.09	0.38	1	95.72
STM45164_2	CIRCULAR	0.38	0.11	0.09	0.38	1	96.42
STM45165	CIRCULAR	0.45	0.16	0.11	0.45	1	223.62

Transect Summary

Transect Half_Street_4.25m

Area:

0.0003	0.0013	0.0029	0.0051	0.0079
0.0114	0.0156	0.0203	0.0257	0.0317
0.0384	0.0457	0.0536	0.0622	0.0714
0.0813	0.0917	0.1028	0.1146	0.1270
0.1403	0.1550	0.1710	0.1882	0.2068
0.2267	0.2479	0.2705	0.2943	0.3194
0.3459	0.3736	0.4026	0.4324	0.4628
0.4939	0.5256	0.5581	0.5912	0.6250
0.6594	0.6946	0.7304	0.7669	0.8041
0.8419	0.8804	0.9196	0.9595	1.0000

Hrad:

0.0218	0.0436	0.0655	0.0873	0.1091
0.1309	0.1528	0.1746	0.1964	0.2182
0.2401	0.2619	0.2837	0.3055	0.3273
0.3492	0.3710	0.3928	0.4146	0.4365
0.4574	0.4757	0.4920	0.5069	0.5206
0.5334	0.5457	0.5575	0.5690	0.5803
0.5915	0.6026	0.6221	0.6495	0.6761
0.7019	0.7270	0.7514	0.7751	0.7982
0.8207	0.8426	0.8639	0.8848	0.9051
0.9250	0.9444	0.9633	0.9819	1.0000

Width:

0.0155	0.0311	0.0466	0.0621	0.0777
0.0932	0.1087	0.1242	0.1398	0.1553
0.1708	0.1864	0.2019	0.2174	0.2330
0.2485	0.2640	0.2796	0.2951	0.3106
0.3427	0.3747	0.4067	0.4388	0.4708
0.5029	0.5349	0.5669	0.5990	0.6310
0.6630	0.6951	0.7194	0.7359	0.7524
0.7689	0.7854	0.8019	0.8184	0.8349
0.8514	0.8679	0.8844	0.9010	0.9175
0.9340	0.9505	0.9670	0.9835	1.0000

 NOTE: The summary statistics displayed in this report are
 based on results found at every computational time step,
 not just on results from each reporting time step.

 Analysis Options

Flow Units LPS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed NO

Water Quality NO

Infiltration Method HORTON

Flow Routing Method DYNWAVE

Starting Date 09/26/2018 00:00:00

Ending Date 09/26/2018 06:00:00

Antecedent Dry Days 0.0

Report Time Step 00:01:00

Wet Time Step 00:01:00

Dry Time Step 00:01:00

Routing Time Step 5.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 2

Head Tolerance 0.001500 m

Runoff Quantity Continuity	Volume	Depth
	hectare-m	mm
Total Precipitation	0.864	71.708
Evaporation Loss	0.000	0.000
Infiltration Loss	0.334	27.748
Surface Runoff	0.523	43.433
Final Storage	0.007	0.582

Continuity Error (%) -0.077

Flow Routing Continuity	Volume	Volume
	hectare-m	10^6 ltr
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.523	5.234
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.011	0.110
External Outflow	0.468	4.681
Flooding Loss	0.062	0.623
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.005	0.055
Continuity Error (%)	-0.278	

Highest Continuity Errors	Volume	Volume
	hectare-m	10^6 ltr
Node 208 (-3.09%)	0.000	0.000
Node J2 (2.79%)	0.523	5.234
Node CBT11 (-2.78%)	0.000	0.000
Node IN09030-MAJ (-2.01%)	0.000	0.000
Node IN09032-MAJ (1.67%)	0.000	0.000

Time-Step Critical Elements	Volume	Volume
	hectare-m	10^6 ltr
Link C25 (36.39%)	0.000	0.000
Link STM45164_1 (28.88%)	0.523	5.234
Link C09 (15.69%)	0.000	0.000
Link C24 (4.38%)	0.000	0.000
Link C35 (4.06%)	0.000	0.000

Highest Flow Instability Indexes	Volume	Volume
	hectare-m	10^6 ltr
Link C24 (22)	0.000	0.000
Link C09 (19)	0.523	5.234
Link C08 (9)	0.000	0.000
Link C14 (9)	0.000	0.000
Link C21 (8)	0.000	0.000

Routing Time Step Summary	Volume	Volume
	hectare-m	10^6 ltr
Total Precipitation	0.864	71.708
Evaporation Loss	0.000	0.000
Infiltration Loss	0.334	27.748
Surface Runoff	0.523	43.433
Final Storage	0.007	0.582

Minimum Time Step : 0.03 sec
 Average Time Step : 2.34 sec
 Maximum Time Step : 5.00 sec
 Percent in Steady State : 0.00
 Average Iterations per Step : 2.32
 Percent Not Converging : 2.88

 Subcatchment Runoff Summary

Subcatchment	Total Precip	Total Runon	Total Evap	Total Infil	Total Runoff	Total Runoff 10^6 ltr	Peak Runoff LPS	Runoff Coeff
	mm	mm	mm	mm	mm			
ES01_1	71.71	0.00	0.00	14.55	56.26	0.18	136.52	0.785
ES02_1	71.71	0.00	0.00	30.80	40.53	0.04	31.03	0.565
ES02_2	71.71	0.00	0.00	24.27	46.88	0.02	19.97	0.654
ES03_1	71.71	0.00	0.00	19.75	51.25	0.14	117.33	0.715
ES03_2	71.71	0.00	0.00	22.08	49.01	0.09	78.54	0.683
ES04_1	71.71	0.00	0.00	17.93	53.00	0.11	86.70	0.739
ES04_2	71.71	0.00	0.00	20.12	50.88	0.10	78.13	0.710
ES05_1	71.71	0.00	0.00	21.53	49.51	0.09	73.74	0.690
ES05_2	71.71	0.00	0.00	20.49	50.51	0.09	72.96	0.704
ES06_1	71.71	0.00	0.00	18.33	52.61	0.15	114.46	0.734
ES06_2	71.71	0.00	0.00	20.07	50.92	0.12	96.75	0.710
ES07	71.71	0.00	0.00	20.00	50.99	0.11	84.84	0.711
ES08_1	71.71	0.00	0.00	24.71	46.44	0.06	47.15	0.648
ES08_2	71.71	0.00	0.00	32.04	39.30	0.03	26.74	0.548
ES09_1	71.71	0.00	0.00	20.64	50.37	0.09	69.93	0.702
ES09_2	71.71	0.00	0.00	26.74	44.47	0.08	66.90	0.620
ES10_1	71.71	0.00	0.00	22.38	48.68	0.10	81.31	0.679
ES10_2	71.71	0.00	0.00	23.04	48.05	0.09	71.49	0.670
ES11_1	71.71	0.00	0.00	20.22	50.78	0.09	73.23	0.708
ES11_2	71.71	0.00	0.00	24.95	46.19	0.06	46.69	0.644
ES12_1	71.71	0.00	0.00	19.48	51.50	0.10	77.70	0.718
ES12_2	71.71	0.00	0.00	20.02	50.97	0.08	62.22	0.711
ES13_1	71.71	0.00	0.00	19.64	51.34	0.08	62.01	0.716
ES13_2	71.71	0.00	0.00	20.84	50.18	0.08	66.18	0.700
ES14_1	71.71	0.00	0.00	25.50	45.67	0.06	50.81	0.637
ES14_2	71.71	0.00	0.00	17.84	53.09	0.10	75.32	0.740
ES15_1	71.71	0.00	0.00	27.90	43.36	0.03	28.86	0.605
ES15_2	71.71	0.00	0.00	19.13	51.85	0.06	50.90	0.723
ES16_1	71.71	0.00	0.00	28.15	43.13	0.04	42.83	0.601
ES16_2	71.71	0.00	0.00	32.57	38.81	0.07	62.46	0.541
ES17	71.71	0.00	0.00	25.71	45.49	0.06	55.98	0.634
ES18	71.71	0.00	0.00	26.42	44.79	0.11	91.20	0.625
ES19	71.71	0.00	0.00	16.50	54.39	0.05	42.02	0.758
ES20	71.71	0.00	0.00	30.58	40.71	0.03	21.40	0.568
ES21_1	71.71	0.00	0.00	18.44	52.50	0.04	32.35	0.732
ES21_3	71.71	0.00	0.00	26.08	45.08	0.06	44.95	0.629

ES21_4	71.71	0.00	0.00	16.65	54.23	0.08	58.53	0.756
ES21_5	71.71	0.00	0.00	20.46	50.54	0.04	33.50	0.705
ES22_1	71.71	0.00	0.00	16.78	54.11	0.10	76.60	0.755
ES22_2	71.71	0.00	0.00	20.03	50.96	0.11	86.38	0.711
ES23	71.71	0.00	0.00	33.09	38.19	0.07	42.33	0.533
ES24	71.71	0.00	0.00	34.70	36.67	0.03	19.06	0.511
ES25	71.71	0.00	0.00	37.08	34.27	0.06	35.20	0.478
ES26	71.71	0.00	0.00	32.49	38.80	0.04	26.83	0.541
ES27	71.71	0.00	0.00	42.85	28.69	0.11	54.66	0.400
ES28	71.71	0.00	0.00	38.27	33.16	0.11	65.07	0.462
ES29	71.71	0.00	0.00	35.76	35.60	0.12	68.83	0.496
ES30	71.71	0.00	0.00	33.77	37.58	0.09	56.80	0.524
ES31	71.71	0.00	0.00	35.12	36.27	0.07	47.73	0.506
ES32	71.71	0.00	0.00	42.10	29.34	0.23	112.45	0.409
ES33	71.71	0.00	0.00	31.30	40.01	0.06	47.93	0.558
ES34	71.71	0.00	0.00	44.97	26.62	0.11	52.02	0.371
ES35	71.71	0.00	0.00	45.45	26.07	0.25	111.44	0.364
ES36	71.71	0.00	0.00	30.90	40.41	0.09	68.09	0.564
S01	71.71	0.00	0.00	8.49	62.27	0.11	82.83	0.868
S02	71.71	0.00	0.00	5.13	65.54	0.10	72.09	0.914
S03	71.71	0.00	0.00	37.08	34.57	0.01	7.78	0.482
S04	71.71	0.00	0.00	9.18	61.61	0.12	94.15	0.859
S05	71.71	0.00	0.00	11.46	59.40	0.08	58.55	0.828
S06	71.71	0.00	0.00	28.34	42.99	0.03	24.79	0.599
S07	71.71	0.00	0.00	27.17	44.14	0.02	17.94	0.616
S08_1	71.71	0.00	0.00	17.66	53.49	0.02	18.82	0.746
S08_2	71.71	0.00	0.00	19.67	51.45	0.03	25.18	0.717
S09	71.71	0.00	0.00	12.52	58.41	0.05	38.28	0.815

 Node Depth Summary

Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Occurrence days hr:min	Reported Max Depth Meters
200	JUNCTION	0.16	0.24	111.38	0 01:11	0.24
201	JUNCTION	0.12	0.16	111.50	0 01:21	0.16
202	JUNCTION	0.11	0.14	111.59	0 01:20	0.14
203	JUNCTION	0.11	0.14	111.75	0 01:20	0.14
204	JUNCTION	0.10	0.13	111.83	0 01:20	0.13
205	JUNCTION	0.10	0.14	112.01	0 01:19	0.14
206	JUNCTION	0.03	0.03	112.45	0 05:50	0.03
207	JUNCTION	0.01	0.01	113.30	0 00:11	0.01
208	JUNCTION	0.55	1.51	114.08	0 01:18	1.44
210	JUNCTION	0.25	0.65	112.81	0 01:30	0.65
211	JUNCTION	0.31	1.00	112.81	0 01:30	1.00
212	JUNCTION	0.55	1.39	112.81	0 01:30	1.39
213	JUNCTION	0.40	1.20	114.02	0 01:18	1.19
215	JUNCTION	0.81	1.84	114.08	0 01:18	1.76

216	JUNCTION	0.13	0.17	111.50	0	01:21	0.17
217	JUNCTION	0.12	0.68	114.14	0	01:18	0.54
218	JUNCTION	0.45	1.26	114.00	0	01:18	1.26
219	JUNCTION	0.10	0.15	111.45	0	01:21	0.15
CB03	JUNCTION	0.26	0.98	114.09	0	01:18	0.91
CB05	JUNCTION	0.02	0.11	114.11	0	01:10	0.11
CBE01	JUNCTION	0.02	0.11	114.36	0	01:10	0.11
CBE04	JUNCTION	0.03	0.13	114.03	0	01:19	0.13
CBT02	JUNCTION	0.02	0.11	114.23	0	01:10	0.11
CBT03	JUNCTION	0.05	0.78	114.57	0	01:18	0.24
CBT05	JUNCTION	0.05	0.24	114.03	0	01:19	0.24
CBT06	JUNCTION	0.07	0.43	114.11	0	01:16	0.34
CBT07	JUNCTION	0.08	0.47	114.08	0	01:16	0.41
CBT08	JUNCTION	0.11	0.53	114.05	0	01:16	0.50
CBT09	JUNCTION	0.15	0.64	114.03	0	01:16	0.62
CBT10	JUNCTION	0.19	0.75	114.02	0	01:18	0.73
CBT11	JUNCTION	0.38	1.16	114.02	0	01:18	1.15
CBT12	JUNCTION	0.37	1.14	114.02	0	01:18	1.13
CBT13	JUNCTION	0.35	1.14	114.06	0	01:06	1.10
CBT14	JUNCTION	0.34	1.08	114.02	0	01:06	1.07
IN07998	JUNCTION	0.15	1.28	111.71	0	01:10	1.28
IN09003-MAJ	JUNCTION	0.01	0.03	113.96	0	01:10	0.03
IN09004-MAJ	JUNCTION	0.01	0.04	113.87	0	01:10	0.04
IN09005-MAJ	JUNCTION	0.02	0.09	113.31	0	01:10	0.09
IN09006-MAJ	JUNCTION	0.02	0.09	113.31	0	01:10	0.09
IN09009-MAJ	JUNCTION	0.02	0.10	112.85	0	01:10	0.10
IN09010-MAJ	JUNCTION	0.02	0.07	112.82	0	01:10	0.07
IN09011-MAJ	JUNCTION	0.03	0.11	112.32	0	01:10	0.11
IN09012-MAJ	JUNCTION	0.02	0.10	112.31	0	01:10	0.09
IN09013-MAJ	JUNCTION	0.03	0.11	111.89	0	01:10	0.11
IN09014-MAJ	JUNCTION	0.02	0.07	111.48	0	01:10	0.07
IN09015-MAJ	JUNCTION	0.03	0.11	111.52	0	01:11	0.11
IN09017-MAJ	JUNCTION	0.01	0.04	111.60	0	01:10	0.04
IN09018-MAJ	JUNCTION	0.01	0.04	111.60	0	01:10	0.04
IN09019-MAJ	JUNCTION	0.02	0.08	111.41	0	01:10	0.08
IN09020-MAJ	JUNCTION	0.02	0.06	111.39	0	01:10	0.06
IN09021-MAJ	JUNCTION	0.04	0.20	111.20	0	01:06	0.20
IN09022-MAJ	JUNCTION	0.01	0.05	113.99	0	01:10	0.05
IN09023-MAJ	JUNCTION	0.01	0.04	113.79	0	01:10	0.04
IN09024-MAJ	JUNCTION	0.02	0.07	113.22	0	01:10	0.07
IN09025-MAJ	JUNCTION	0.02	0.08	113.21	0	01:10	0.08
IN09026-MAJ	JUNCTION	0.02	0.09	112.75	0	01:10	0.09
IN09027-MAJ	JUNCTION	0.02	0.09	112.77	0	01:10	0.09
IN09028-MAJ	JUNCTION	0.02	0.07	112.43	0	01:10	0.07
IN09029-MAJ	JUNCTION	0.02	0.09	112.46	0	01:10	0.09
IN09030-MAJ	JUNCTION	0.02	0.07	112.04	0	01:11	0.07
IN09031-MAJ	JUNCTION	0.02	0.07	112.04	0	01:10	0.07
IN09032-MAJ	JUNCTION	0.04	0.20	111.82	0	01:11	0.20
IN09033-MAJ	JUNCTION	0.02	0.11	111.73	0	01:11	0.11
IN09034-MAJ	JUNCTION	0.03	0.14	111.41	0	01:08	0.14
IN09035-MAJ	JUNCTION	0.03	0.13	111.40	0	01:07	0.13
IN45566	JUNCTION	0.16	1.27	111.09	0	01:10	1.26
IN45569	JUNCTION	0.15	1.40	113.01	0	01:01	1.40

IN45570	JUNCTION	0.10	1.40	113.10	0	01:03	1.38
IN45572	JUNCTION	0.07	1.40	112.91	0	01:05	0.96
IN45573	JUNCTION	0.04	1.40	114.16	0	01:08	0.51
IN45574	JUNCTION	0.06	0.30	111.60	0	01:06	0.30
IN45575	JUNCTION	0.07	1.40	113.57	0	01:07	0.87
IN45577	JUNCTION	0.05	1.40	112.68	0	01:07	0.66
IN45587	JUNCTION	0.05	0.92	113.36	0	01:08	0.42
IN45588	JUNCTION	0.03	0.14	112.66	0	01:10	0.14
IN45589	JUNCTION	0.04	0.17	112.02	0	01:10	0.17
IN45590	JUNCTION	0.03	0.13	111.71	0	01:10	0.13
J1	JUNCTION	0.01	0.05	111.82	0	01:10	0.05
J2	JUNCTION	0.10	0.20	111.40	0	01:07	0.20
MHST09001	JUNCTION	0.06	0.14	111.43	0	01:11	0.14
MHST09002	JUNCTION	0.07	0.16	111.41	0	01:12	0.16
MHST09003	JUNCTION	0.14	0.23	111.38	0	01:11	0.23
MHST09004	JUNCTION	0.14	0.25	111.27	0	01:10	0.25
MHST09005	JUNCTION	0.16	0.33	110.76	0	01:10	0.33
MHST09006	JUNCTION	0.18	0.38	110.45	0	01:12	0.38
MHST09007	JUNCTION	0.19	0.50	110.11	0	01:12	0.50
MHST09008	JUNCTION	0.22	1.01	110.28	0	01:10	0.69
MHST09009	JUNCTION	0.21	1.01	110.22	0	01:10	0.72
MHST09010	JUNCTION	0.27	1.18	109.83	0	01:10	1.03
MHST09011	JUNCTION	0.26	0.87	109.16	0	01:11	0.87
MHST09013	JUNCTION	0.15	0.59	108.75	0	01:10	0.59
MHST09014	JUNCTION	0.15	0.71	109.09	0	01:10	0.57
MHST09015	JUNCTION	0.15	0.73	109.26	0	01:10	0.63
MHST09016	JUNCTION	0.05	0.37	111.35	0	01:12	0.37
MHST09017	JUNCTION	0.08	0.62	111.37	0	01:10	0.56
MHST09018	JUNCTION	0.09	0.65	111.31	0	01:10	0.62
MHST09019	JUNCTION	0.12	0.79	111.17	0	01:12	0.79
MHST09020	JUNCTION	0.13	0.94	110.88	0	01:12	0.94
MHST09021	JUNCTION	0.25	1.56	110.61	0	01:10	1.56
MHST09022	JUNCTION	0.25	1.49	110.42	0	01:10	1.49
MHST09023	JUNCTION	0.24	1.39	110.18	0	01:10	1.28
MHST09024	JUNCTION	0.14	0.82	109.68	0	01:10	0.80
OF-CREEK	OUTFALL	0.27	0.74	108.24	0	01:10	0.74
OF-HAZELDEAN	OUTFALL	0.01	0.11	112.94	0	01:10	0.11
CB01	STORAGE	0.10	0.41	112.81	0	01:30	0.41
CB06	STORAGE	0.08	0.32	112.82	0	01:30	0.32
CHAMBERS-1	STORAGE	0.52	1.30	112.81	0	01:30	1.30
CHAMBERS-2	STORAGE	0.77	1.78	114.08	0	01:18	1.71
IN09003	STORAGE	0.04	0.35	112.88	0	01:10	0.34
IN09004	STORAGE	0.09	0.54	112.97	0	01:11	0.54
IN09005	STORAGE	0.27	1.40	113.22	0	01:03	1.40
IN09006	STORAGE	0.26	1.40	113.22	0	01:05	1.40
IN09007	STORAGE	0.41	1.55	113.13	0	01:04	1.55
IN09008	STORAGE	0.44	1.51	113.09	0	01:10	1.51
IN09009	STORAGE	0.24	1.40	112.75	0	01:05	1.40
IN09010	STORAGE	0.03	0.04	111.39	0	02:30	0.04
IN09011	STORAGE	0.36	1.40	112.21	0	01:03	1.40
IN09012	STORAGE	0.29	1.40	112.21	0	01:03	1.40
IN09013	STORAGE	0.31	1.40	111.78	0	01:03	1.40
IN09014	STORAGE	0.17	1.40	111.41	0	01:08	1.40

IN09015	STORAGE	0.31	1.40	111.41	0	01:03	1.40
IN09016	STORAGE	0.53	1.55	111.40	0	01:05	1.55
IN09017	STORAGE	0.07	0.50	110.66	0	01:11	0.50
IN09018	STORAGE	0.07	0.49	110.65	0	01:11	0.49
IN09019	STORAGE	0.28	1.40	111.33	0	01:04	1.40
IN09020	STORAGE	0.13	0.90	110.83	0	01:10	0.90
IN09021	STORAGE	0.31	1.40	111.00	0	01:01	1.40
IN09022	STORAGE	0.10	0.61	113.15	0	01:10	0.61
IN09023	STORAGE	0.06	0.48	112.83	0	01:11	0.48
IN09024	STORAGE	0.17	1.40	113.15	0	01:09	1.40
IN09025	STORAGE	0.18	1.40	113.13	0	01:07	1.40
IN09026	STORAGE	0.26	1.40	112.66	0	01:04	1.40
IN09027	STORAGE	0.24	1.40	112.68	0	01:05	1.40
IN09028	STORAGE	0.18	1.40	112.36	0	01:08	1.40
IN09029	STORAGE	0.28	1.40	112.37	0	01:03	1.40
IN09030	STORAGE	0.15	1.40	111.97	0	01:08	1.40
IN09031	STORAGE	0.15	1.21	111.78	0	01:10	1.18
IN09032	STORAGE	0.33	1.40	111.62	0	01:03	1.40
IN09033	STORAGE	0.22	1.40	111.62	0	01:05	1.40
IN09034	STORAGE	0.28	1.40	111.27	0	01:03	1.40
IN09035	STORAGE	0.27	1.40	111.27	0	01:03	1.40
IN103407	STORAGE	0.46	1.51	113.15	0	01:10	1.51
MHST09012	STORAGE	0.32	0.99	108.60	0	01:10	0.99

Node Inflow Summary

Node	Type	Maximum Lateral Inflow	Maximum Total Inflow	Time of Max Occurrence	Lateral Inflow Volume	Total Inflow Volume	Flow Balance Error
		LPS	LPS	days hr:min	10^6 ltr	10^6 ltr	Percent
200	JUNCTION	0.00	85.73	0 01:11	0	0.753	0.057
201	JUNCTION	0.00	29.12	0 01:21	0	0.391	0.033
202	JUNCTION	0.00	29.12	0 01:20	0	0.391	0.059
203	JUNCTION	1.91	29.13	0 01:20	0.0413	0.392	0.141
204	JUNCTION	0.85	27.22	0 01:19	0.0184	0.351	0.044
205	JUNCTION	0.85	26.85	0 01:18	0.0184	0.333	0.149
206	JUNCTION	0.85	1.49	0 05:14	0.0184	0.0322	0.535
207	JUNCTION	0.64	0.64	0 00:00	0.0138	0.0138	0.198
208	JUNCTION	0.00	186.81	0 01:10	0	0.239	-2.997
210	JUNCTION	0.00	84.12	0 01:09	0	0.109	0.200
211	JUNCTION	0.00	160.14	0 01:08	0	0.212	-0.868
212	JUNCTION	0.00	27.48	0 01:03	0	0.211	-0.161
213	JUNCTION	0.00	42.67	0 01:06	0	0.0519	-1.000
215	JUNCTION	0.00	93.81	0 01:02	0	0.282	-1.310
216	JUNCTION	0.00	50.40	0 01:30	0	0.602	0.033
217	JUNCTION	0.00	41.60	0 01:10	0	0.0448	-0.830
218	JUNCTION	58.55	93.40	0 01:09	0.0751	0.13	0.037
219	JUNCTION	0.00	50.41	0 01:33	0	0.601	0.017

CB03	JUNCTION	94.15	94.15	0 01:10	0.123	0.123	-0.141
CB05	JUNCTION	0.00	17.71	0 01:10	0	0.0184	-0.067
CBE01	JUNCTION	17.94	17.94	0 01:10	0.0183	0.0183	-0.014
CBE04	JUNCTION	25.18	25.18	0 01:10	0.0282	0.0282	-0.025
CBT02	JUNCTION	0.00	17.84	0 01:10	0	0.0183	-0.001
CBT03	JUNCTION	24.79	42.14	0 01:10	0.0265	0.045	0.684
CBT05	JUNCTION	0.00	25.15	0 01:10	0	0.0282	0.001
CBT06	JUNCTION	0.00	25.07	0 01:09	0	0.0282	-0.049
CBT07	JUNCTION	0.00	25.05	0 01:09	0	0.0282	-0.180
CBT08	JUNCTION	0.00	25.33	0 01:09	0	0.0283	-0.235
CBT09	JUNCTION	0.00	24.58	0 01:08	0	0.0284	-0.315
CBT10	JUNCTION	0.00	24.28	0 01:07	0	0.0284	-0.775
CBT11	JUNCTION	0.00	20.48	0 01:06	0	0.0228	-2.706
CBT12	JUNCTION	0.00	19.97	0 01:06	0	0.0224	-1.074
CBT13	JUNCTION	0.00	20.61	0 01:06	0	0.022	-0.967
CBT14	JUNCTION	18.82	18.82	0 01:10	0.0217	0.0217	-0.896
IN07998	JUNCTION	112.45	112.45	0 01:10	0.231	0.231	-0.007
IN09003-MAJ	JUNCTION	19.97	19.97	0 01:10	0.0224	0.0224	-0.357
IN09004-MAJ	JUNCTION	31.03	31.03	0 01:10	0.0358	0.0359	-0.241
IN09005-MAJ	JUNCTION	117.33	117.33	0 01:10	0.144	0.144	1.395
IN09006-MAJ	JUNCTION	78.54	93.44	0 01:10	0.0921	0.104	0.146
IN09009-MAJ	JUNCTION	73.74	187.18	0 01:10	0.0944	0.181	0.155
IN09010-MAJ	JUNCTION	72.96	72.96	0 01:10	0.0931	0.0932	-0.077
IN09011-MAJ	JUNCTION	114.46	225.08	0 01:10	0.146	0.249	-0.062
IN09012-MAJ	JUNCTION	96.75	141.99	0 01:10	0.123	0.166	-0.090
IN09013-MAJ	JUNCTION	84.84	226.01	0 01:10	0.11	0.252	-0.011
IN09014-MAJ	JUNCTION	50.81	72.61	0 01:10	0.0602	0.088	-1.032
IN09015-MAJ	JUNCTION	75.32	219.81	0 01:10	0.0961	0.246	0.054
IN09017-MAJ	JUNCTION	33.50	33.50	0 01:10	0.0437	0.0437	-1.318
IN09018-MAJ	JUNCTION	32.35	32.35	0 01:10	0.0415	0.0416	0.009
IN09019-MAJ	JUNCTION	100.55	108.47	0 01:10	0.13	0.138	-0.485
IN09020-MAJ	JUNCTION	66.35	73.76	0 01:10	0.0864	0.0938	-0.407
IN09021-MAJ	JUNCTION	91.20	143.06	0 01:10	0.107	0.157	0.247
IN09022-MAJ	JUNCTION	47.15	47.15	0 01:10	0.0565	0.0566	-0.211
IN09023-MAJ	JUNCTION	26.74	26.74	0 01:10	0.0339	0.0339	0.119
IN09024-MAJ	JUNCTION	69.93	81.77	0 01:10	0.0876	0.0987	-0.085
IN09025-MAJ	JUNCTION	66.90	97.82	0 01:10	0.0799	0.105	0.141
IN09026-MAJ	JUNCTION	81.31	131.93	0 01:10	0.103	0.151	0.074
IN09027-MAJ	JUNCTION	71.49	130.26	0 01:10	0.0883	0.141	-0.034
IN09028-MAJ	JUNCTION	46.69	121.78	0 01:10	0.0582	0.131	-0.504
IN09029-MAJ	JUNCTION	73.23	148.81	0 01:10	0.0937	0.17	-0.204
IN09030-MAJ	JUNCTION	0.00	90.68	0 01:10	0	0.089	-1.974
IN09031-MAJ	JUNCTION	62.22	62.22	0 01:10	0.0792	0.0792	-0.833
IN09032-MAJ	JUNCTION	68.09	143.50	0 01:10	0.0869	0.156	1.696
IN09033-MAJ	JUNCTION	0.00	68.99	0 01:10	0	0.0722	1.014
IN09034-MAJ	JUNCTION	98.80	183.88	0 01:10	0.105	0.19	0.386
IN09035-MAJ	JUNCTION	62.46	71.30	0 01:05	0.0673	0.126	-0.015
IN45566	JUNCTION	111.44	111.44	0 01:10	0.252	0.252	-0.007
IN45569	JUNCTION	68.83	68.83	0 01:10	0.116	0.116	-0.005
IN45570	JUNCTION	65.07	65.07	0 01:10	0.114	0.114	0.004
IN45572	JUNCTION	56.80	56.80	0 01:10	0.086	0.0861	0.009
IN45573	JUNCTION	47.93	47.93	0 01:10	0.0637	0.0637	0.010
IN45574	JUNCTION	52.02	52.02	0 01:10	0.109	0.109	-0.001

IN45575	JUNCTION	54.66	54.66	0	01:10	0.106	0.106	-0.007
IN45577	JUNCTION	47.73	47.73	0	01:10	0.0697	0.0698	0.060
IN45587	JUNCTION	42.33	42.33	0	01:10	0.0702	0.0702	0.018
IN45588	JUNCTION	19.06	19.06	0	01:10	0.0296	0.0296	0.005
IN45589	JUNCTION	35.20	35.20	0	01:10	0.0643	0.0643	0.002
IN45590	JUNCTION	26.83	26.83	0	01:10	0.0421	0.0422	0.002
J1	JUNCTION	0.00	78.66	0	01:10	0	0.082	-0.092
J2	JUNCTION	0.00	251.73	0	01:09	0	0.123	2.872
MHST09001	JUNCTION	0.00	31.48	0	01:10	0	0.138	-0.002
MHST09002	JUNCTION	0.00	31.45	0	01:08	0	0.138	-0.047
MHST09003	JUNCTION	0.00	41.63	0	01:10	0	0.152	0.220
MHST09004	JUNCTION	0.00	137.96	0	01:10	0	0.847	0.122
MHST09005	JUNCTION	0.00	194.93	0	01:10	0	1.01	0.072
MHST09006	JUNCTION	0.00	238.66	0	01:10	0	1.18	0.205
MHST09007	JUNCTION	0.00	310.49	0	01:10	0	1.37	-0.042
MHST09008	JUNCTION	0.00	349.36	0	01:10	0	1.52	0.122
MHST09009	JUNCTION	0.00	339.11	0	01:14	0	1.51	0.096
MHST09010	JUNCTION	0.00	940.46	0	01:10	0	3.1	-0.006
MHST09011	JUNCTION	0.00	1075.53	0	01:10	0	3.46	0.041
MHST09013	JUNCTION	0.00	275.22	0	01:10	0	0.801	-0.110
MHST09014	JUNCTION	0.00	232.02	0	01:10	0	0.641	0.091
MHST09015	JUNCTION	0.00	193.96	0	01:10	0	0.528	0.090
MHST09016	JUNCTION	0.00	47.91	0	01:10	0	0.0637	0.565
MHST09017	JUNCTION	0.00	108.31	0	01:10	0	0.222	-0.204
MHST09018	JUNCTION	0.00	105.71	0	01:09	0	0.222	0.211
MHST09019	JUNCTION	0.00	196.90	0	01:09	0	0.428	0.186
MHST09020	JUNCTION	0.00	280.41	0	01:08	0	0.664	-0.205
MHST09021	JUNCTION	0.00	363.25	0	01:13	0	0.98	0.081
MHST09022	JUNCTION	77.70	484.14	0	01:10	0.0994	1.23	0.004
MHST09023	JUNCTION	128.19	618.74	0	01:10	0.164	1.52	-0.006
MHST09024	JUNCTION	0.00	172.12	0	01:10	0	0.434	0.076
OF-CREEK	OUTFALL	0.00	1577.82	0	01:10	0	4.58	0.000
OF-HAZELDEAN	OUTFALL	0.00	148.26	0	01:10	0	0.101	0.000
CB01	STORAGE	79.88	79.88	0	01:10	0.103	0.103	0.341
CB06	STORAGE	82.83	82.83	0	01:10	0.109	0.109	0.201
CHAMBERS-1	STORAGE	0.00	159.67	0	01:08	0	0.214	0.122
CHAMBERS-2	STORAGE	0.00	227.73	0	01:10	0	0.293	0.444
IN09003	STORAGE	0.00	10.92	0	01:10	0	0.0146	0.002
IN09004	STORAGE	0.00	13.22	0	01:10	0	0.0237	0.099
IN09005	STORAGE	0.00	49.44	0	01:10	0	0.0802	-0.021
IN09006	STORAGE	0.00	50.88	0	01:10	0	0.0772	-0.021
IN09007	STORAGE	78.13	106.09	0	01:10	0.0993	0.126	-0.011
IN09008	STORAGE	86.70	151.31	0	01:10	0.111	0.173	-1.198
IN09009	STORAGE	0.00	54.70	0	01:10	0	0.0785	-0.028
IN09010	STORAGE	0.00	24.64	0	01:10	0	0.0498	0.005
IN09011	STORAGE	0.00	55.00	0	01:07	0	0.106	0.024
IN09012	STORAGE	0.00	54.05	0	01:10	0	0.0878	-0.023
IN09013	STORAGE	0.00	55.00	0	01:08	0	0.103	-0.018
IN09014	STORAGE	0.00	29.08	0	01:10	0	0.0488	-0.017
IN09015	STORAGE	0.00	55.00	0	01:08	0	0.103	-0.024
IN09016	STORAGE	105.46	154.75	0	01:10	0.132	0.182	0.771
IN09017	STORAGE	0.00	12.84	0	01:10	0	0.0262	0.001
IN09018	STORAGE	0.00	12.72	0	01:10	0	0.0248	0.000

IN09019	STORAGE	0.00	40.81	0	01:10	0	0.0766	-0.013
IN09020	STORAGE	0.00	18.91	0	01:10	0	0.0442	0.001
IN09021	STORAGE	0.00	55.00	0	01:02	0	0.13	-0.020
IN09022	STORAGE	0.00	14.32	0	01:10	0	0.0318	0.001
IN09023	STORAGE	0.00	12.72	0	01:10	0	0.0228	0.000
IN09024	STORAGE	0.00	26.78	0	01:10	0	0.0508	-0.000
IN09025	STORAGE	0.00	32.56	0	01:10	0	0.0522	-0.009
IN09026	STORAGE	0.00	49.26	0	01:10	0	0.0751	-0.020
IN09027	STORAGE	0.00	48.30	0	01:10	0	0.0684	-0.023
IN09028	STORAGE	0.00	30.80	0	01:10	0	0.0492	-0.010
IN09029	STORAGE	0.00	52.03	0	01:10	0	0.0811	-0.024
IN09030	STORAGE	0.00	30.79	0	01:11	0	0.0391	-0.011
IN09031	STORAGE	0.00	21.63	0	01:10	0	0.0449	0.001
IN09032	STORAGE	0.00	55.00	0	01:05	0	0.141	-0.016
IN09033	STORAGE	0.00	55.00	0	01:09	0	0.0714	-0.029
IN09034	STORAGE	0.00	55.00	0	01:04	0	0.131	-0.017
IN09035	STORAGE	0.00	55.00	0	01:05	0	0.124	-0.019
IN103407	STORAGE	174.80	183.35	0	01:10	0.23	0.238	0.040
MHST09012	STORAGE	137.28	1575.67	0	01:10	0.175	4.58	0.029

Node Surcharge Summary

Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Meters	Min. Depth Below Rim Meters
208	JUNCTION	2.39	0.913	0.422
210	JUNCTION	0.96	0.205	1.465
211	JUNCTION	1.24	0.323	1.237
212	JUNCTION	2.24	0.755	1.310
213	JUNCTION	1.74	0.527	0.300
215	JUNCTION	3.20	1.265	0.420
217	JUNCTION	1.06	0.379	0.819
218	JUNCTION	2.67	0.964	0.000
CB03	JUNCTION	1.93	0.681	0.165
CBT03	JUNCTION	0.01	0.534	0.272
CBT06	JUNCTION	0.56	0.178	0.611
CBT07	JUNCTION	0.79	0.220	0.576
CBT08	JUNCTION	1.09	0.282	0.632
CBT09	JUNCTION	1.40	0.391	0.441
CBT10	JUNCTION	1.66	0.496	0.328
CBT11	JUNCTION	2.49	0.897	0.279
CBT12	JUNCTION	2.44	0.882	0.255
CBT13	JUNCTION	2.38	0.885	0.000
CBT14	JUNCTION	2.32	0.815	0.000
IN07998	JUNCTION	0.59	1.085	0.117
IN09021-MAJ	JUNCTION	0.18	0.000	0.000
IN09032-MAJ	JUNCTION	0.09	0.000	0.000

IN45566	JUNCTION	0.71	1.065	0.130
IN45569	JUNCTION	0.41	1.197	0.000
IN45570	JUNCTION	0.29	1.204	0.000
IN45572	JUNCTION	0.12	1.202	0.000
IN45573	JUNCTION	0.04	1.196	0.000
IN45574	JUNCTION	0.31	0.100	0.000
IN45575	JUNCTION	0.23	1.202	0.000
IN45577	JUNCTION	0.06	1.202	0.000
IN45587	JUNCTION	0.05	0.716	0.489
J2	JUNCTION	0.17	0.000	0.000
MHST09008	JUNCTION	0.09	0.379	2.146
MHST09009	JUNCTION	0.10	0.368	2.061
MHST09010	JUNCTION	0.20	0.300	2.144
MHST09014	JUNCTION	0.02	0.189	2.402
MHST09015	JUNCTION	0.12	0.275	2.538
MHST09017	JUNCTION	0.09	0.167	2.731
MHST09018	JUNCTION	0.14	0.236	2.560
MHST09023	JUNCTION	0.38	0.787	1.627

Node Flooding Summary

Flooding refers to all water that overflows a node, whether it ponds or not.

Node	Hours Flooded	Maximum Rate LPS	Time of Max Occurrence days hr:min	Total Flood Volume 10^6 ltr	Maximum Ponded Depth Meters
218	0.25	49.99	0 01:19	0.014	0.000
CBT13	0.01	15.28	0 01:06	0.000	0.000
CBT14	0.01	8.00	0 01:06	0.000	0.000
IN09021-MAJ	0.17	87.93	0 01:10	0.026	0.000
IN09032-MAJ	0.09	65.01	0 01:11	0.008	0.000
IN45569	0.04	9.28	0 01:01	0.000	0.000
IN45570	0.01	3.03	0 01:03	0.000	0.000
IN45572	0.01	2.14	0 01:05	0.000	0.000
IN45573	0.01	3.13	0 01:08	0.000	0.000
IN45574	0.23	17.18	0 01:10	0.006	0.000
IN45575	0.01	2.75	0 01:07	0.000	0.000
IN45577	0.01	2.62	0 01:07	0.000	0.000
J2	0.16	251.66	0 01:09	0.057	0.000
IN09005	0.17	28.04	0 01:10	0.011	0.000
IN09006	0.24	29.48	0 01:10	0.013	0.000
IN09007	0.34	83.49	0 01:10	0.041	0.000
IN09009	0.27	33.30	0 01:10	0.019	0.000
IN09011	0.35	34.08	0 01:09	0.029	0.000
IN09012	0.23	32.65	0 01:10	0.017	0.000
IN09013	0.34	33.60	0 01:10	0.028	0.000
IN09014	0.07	7.68	0 01:10	0.001	0.000
IN09015	0.35	33.60	0 01:10	0.029	0.000

IN09016	0.39	132.12	0 01:10	0.070	0.000
IN09019	0.28	19.41	0 01:10	0.008	0.000
IN09021	0.41	24.63	0 01:06	0.036	0.000
IN09024	0.04	5.39	0 01:10	0.001	0.000
IN09025	0.08	11.16	0 01:10	0.002	0.000
IN09026	0.19	27.86	0 01:10	0.011	0.000
IN09027	0.17	26.90	0 01:10	0.009	0.000
IN09028	0.09	9.40	0 01:10	0.002	0.000
IN09029	0.23	30.63	0 01:10	0.015	0.000
IN09030	0.10	9.39	0 01:11	0.002	0.000
IN09032	0.56	33.60	0 01:10	0.065	0.000
IN09033	0.31	33.60	0 01:10	0.026	0.000
IN09034	0.44	24.63	0 01:06	0.037	0.000
IN09035	0.44	24.63	0 01:06	0.036	0.000

Storage Volume Summary

Storage Unit	Average Volume 1000 m3	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 m3	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow LPS
CB01	0.000	1	0	0	0.000	9	0 01:30	80.43
CB06	0.000	1	0	0	0.000	5	0 01:30	84.12
CHAMBERS-1	0.047	31	0	0	0.118	77	0 01:30	27.48
CHAMBERS-2	0.072	46	0	0	0.155	100	0 01:18	93.81
IN09003	0.000	3	0	0	0.000	25	0 01:10	10.52
IN09004	0.000	0	0	0	0.000	5	0 01:11	12.96
IN09005	0.000	20	0	0	0.001	100	0 01:03	21.40
IN09006	0.000	18	0	0	0.001	100	0 01:05	21.40
IN09007	0.002	17	0	0	0.009	100	0 01:04	22.51
IN09008	0.001	11	0	0	0.009	100	0 01:07	138.69
IN09009	0.000	17	0	0	0.001	100	0 01:05	21.40
IN09010	0.026	2	0	0	0.040	3	0 02:30	1.60
IN09011	0.000	26	0	0	0.001	100	0 01:03	20.92
IN09012	0.000	20	0	0	0.001	100	0 01:03	21.40
IN09013	0.000	22	0	0	0.001	100	0 01:03	21.40
IN09014	0.000	12	0	0	0.001	100	0 01:08	21.40
IN09015	0.000	22	0	0	0.001	100	0 01:03	21.40
IN09016	0.000	30	0	0	0.000	100	0 01:05	22.51
IN09017	0.000	5	0	0	0.000	36	0 01:11	12.70
IN09018	0.000	5	0	0	0.000	35	0 01:11	12.58
IN09019	0.000	20	0	0	0.001	100	0 01:04	21.40
IN09020	0.000	9	0	0	0.000	64	0 01:10	17.14
IN09021	0.000	22	0	0	0.001	100	0 01:01	30.37
IN09022	0.000	7	0	0	0.000	43	0 01:10	14.10
IN09023	0.000	4	0	0	0.000	34	0 01:11	12.46
IN09024	0.000	12	0	0	0.001	100	0 01:09	21.40
IN09025	0.000	13	0	0	0.001	100	0 01:07	21.40
IN09026	0.000	18	0	0	0.001	100	0 01:04	21.40

IN09027	0.000	17	0	0	0.001	100	0	01:05	21.40
IN09028	0.000	13	0	0	0.001	100	0	01:08	21.40
IN09029	0.000	20	0	0	0.001	100	0	01:03	21.40
IN09030	0.000	11	0	0	0.001	100	0	01:08	21.40
IN09031	0.000	11	0	0	0.000	86	0	01:10	19.88
IN09032	0.000	24	0	0	0.001	100	0	01:03	21.40
IN09033	0.000	15	0	0	0.001	100	0	01:05	21.40
IN09034	0.000	20	0	0	0.001	100	0	01:03	30.37
IN09035	0.000	20	0	0	0.001	100	0	01:03	30.37
IN103407	0.001	15	0	0	0.010	100	0	01:03	179.74
MHST09012	0.000	9	0	0	0.001	28	0	01:10	1577.82

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow LPS	Max Flow LPS	Total Volume 10^6 ltr
OF-CREEK	99.49	347.82	1577.82	4.581
OF-HAZELDEAN	25.30	48.89	148.26	0.101
System	62.40	396.71	1722.24	4.681

Link Flow Summary

Link	Type	Maximum Flow LPS	Time of Occurrence days hr:min	Maximum Veloc m/sec	Max/Full	Max/Full Depth
C01	CONDUIT	0.64	0 05:14	0.70	0.00	0.05
C02	CONDUIT	1.49	0 04:57	0.48	0.03	0.11
C03	CONDUIT	26.37	0 01:19	0.83	0.26	0.33
C04	CONDUIT	27.22	0 01:20	0.88	0.26	0.32
C05	CONDUIT	29.12	0 01:20	0.86	0.28	0.35
C06	CONDUIT	29.12	0 01:21	0.89	0.28	0.34
C07	CONDUIT	50.41	0 01:33	1.16	0.62	0.43
C08	CONDUIT	94.08	0 01:09	2.04	0.39	1.00
C09	CONDUIT	189.80	0 01:10	1.65	0.31	1.00
C1	CONDUIT	42.31	0 01:10	1.39	1.29	0.93
C10	CONDUIT	50.52	0 01:33	1.34	0.30	0.43
C11	CONDUIT	81.48	0 01:08	1.56	0.83	1.00
C12	CONDUIT	80.43	0 01:09	1.70	0.73	1.00
C13	CONDUIT	112.40	0 01:10	3.58	3.43	1.00
C14	CONDUIT	41.08	0 01:09	2.31	0.16	1.00
C15	CONDUIT	26.74	0 01:03	0.59	0.37	1.00

C16	CONDUIT	159.67	0 01:08	2.05	0.21	1.00
C17	CONDUIT	17.84	0 01:10	0.85	0.38	0.44
C18	CONDUIT	17.71	0 01:10	0.86	0.43	0.44
C19	CONDUIT	17.54	0 01:10	0.74	0.37	0.62
C2	CONDUIT	16.36	0 01:10	0.80	0.76	0.62
C20	CONDUIT	41.60	0 01:10	1.41	0.64	1.00
C21	CONDUIT	93.44	0 01:09	1.34	1.00	1.00
C22	CONDUIT	47.91	0 01:10	1.55	1.31	0.95
C23	CONDUIT	84.12	0 01:09	1.88	0.67	1.00
C24	CONDUIT	93.81	0 01:02	1.24	0.33	1.00
C25	CONDUIT	29.12	0 01:21	0.69	0.24	0.43
C26	CONDUIT	35.68	0 01:10	1.17	1.26	1.00
C27	CONDUIT	111.38	0 01:10	3.55	3.40	1.00
C28	CONDUIT	25.15	0 01:10	1.16	0.42	0.74
C29	CONDUIT	25.07	0 01:09	1.15	0.42	0.99
C3	CONDUIT	34.05	0 01:10	1.23	1.04	0.83
C30	CONDUIT	25.05	0 01:09	1.16	0.42	1.00
C31	CONDUIT	25.33	0 01:09	1.16	0.43	1.00
C32	CONDUIT	24.58	0 01:08	1.15	0.41	1.00
C33	CONDUIT	24.28	0 01:07	1.12	0.41	1.00
C34	CONDUIT	22.01	0 01:06	1.12	0.37	1.00
C35	CONDUIT	21.31	0 01:06	0.72	0.65	1.00
C36	CONDUIT	20.48	0 01:06	0.62	0.62	1.00
C37	CONDUIT	19.97	0 01:06	0.61	0.61	1.00
C38	CONDUIT	19.53	0 01:06	0.63	0.60	1.00
C39	CONDUIT	148.26	0 01:10	1.06	0.14	0.35
C4	CONDUIT	26.25	0 01:10	1.27	0.72	0.63
C40	CONDUIT	37.09	0 01:06	0.59	0.70	1.00
C5	CONDUIT	54.64	0 01:10	1.76	1.67	0.97
C6	CONDUIT	65.07	0 01:10	2.07	1.98	1.00
C7	CONDUIT	61.30	0 01:09	1.95	2.64	1.00
C8	CONDUIT	56.78	0 01:10	1.82	1.73	0.97
C9	CONDUIT	47.72	0 01:10	1.55	1.45	0.95
C98	CONDUIT	4.62	0 00:57	0.59	1.49	1.00
C99	CONDUIT	4.04	0 00:53	0.54	2.60	1.00
OF1	CHANNEL	0.00	0 00:00	0.00	0.00	0.00
R01	CHANNEL	15.17	0 01:10	0.21	0.01	0.33
R02	CHANNEL	28.70	0 01:10	0.32	0.07	0.37
R03	CHANNEL	64.78	0 01:10	0.48	0.09	0.49
R04	CHANNEL	0.00	0 00:00	0.00	0.00	0.17
R05	CHANNEL	116.49	0 01:10	0.62	0.16	0.52
R06	CHANNEL	45.38	0 01:10	0.41	0.05	0.41
R07	CHANNEL	115.27	0 01:10	0.62	0.13	0.52
R08	CHANNEL	78.66	0 01:10	0.89	0.09	0.37
R09	CHANNEL	30.55	0 01:10	0.38	0.02	0.40
R10	CHANNEL	23.02	0 01:10	0.17	0.02	0.63
R11	CHANNEL	147.91	0 01:10	0.70	0.17	0.55
R12	CHANNEL	153.55	0 01:10	0.73	0.17	0.55
R13	CHANNEL	142.47	0 01:11	0.68	0.17	0.55
R14	CHANNEL	39.55	0 01:10	0.24	0.06	0.56
R15	CHANNEL	22.71	0 01:10	0.40	0.02	0.31
R16	CHANNEL	38.02	0 01:26	0.18	0.05	0.83
R17	CHANNEL	171.10	0 01:09	0.30	0.26	0.85

R18	CHANNEL	52.12	0	01:10	0.24	0.04	0.66
R19	CHANNEL	65.77	0	01:10	0.21	0.08	0.70
R20	CHANNEL	7.47	0	01:10	0.17	0.01	0.26
R21	CHANNEL	8.00	0	01:10	0.13	0.01	0.30
R22	CHANNEL	9.73	0	01:10	0.40	0.01	0.19
R23	CHANNEL	10.16	0	01:10	0.23	0.01	0.48
R24	CHANNEL	8.57	0	01:10	0.28	0.01	0.34
R25	CHANNEL	12.06	0	01:10	0.24	0.01	0.28
R26	CHANNEL	31.07	0	01:10	0.45	0.03	0.33
R27	CHANNEL	59.35	0	01:10	0.55	0.07	0.41
R28	CHANNEL	50.90	0	01:10	0.50	0.05	0.40
R29	CHANNEL	76.14	0	01:10	0.72	0.08	0.40
R30	CHANNEL	76.18	0	01:10	0.57	0.09	0.45
R31	CHANNEL	90.68	0	01:10	0.82	0.10	0.42
R32	CHANNEL	86.08	0	01:10	0.48	0.06	0.53
R33	CHANNEL	55.79	0	01:11	0.29	0.06	0.69
R34	CHANNEL	39.46	0	01:10	0.57	0.04	0.42
STM04620	CONDUIT	227.48	0	01:10	1.17	1.16	1.00
STM04621	CONDUIT	276.26	0	01:11	1.27	0.99	0.99
STM07857	CONDUIT	193.96	0	01:10	1.26	0.71	0.67
STM07870	CONDUIT	193.95	0	01:10	1.23	1.73	1.00
STM07871	CONDUIT	1577.82	0	01:10	2.60	1.75	0.91
STM07872	CONDUIT	163.59	0	01:10	1.48	1.51	1.00
STM07873	CONDUIT	339.46	0	01:14	1.53	0.94	1.00
STM07874	CONDUIT	31.45	0	01:08	0.79	0.29	0.40
STM07875	CONDUIT	237.07	0	01:11	1.51	0.87	0.74
STM07876	CONDUIT	47.23	0	01:10	0.94	0.79	1.00
STM45150	CONDUIT	105.71	0	01:09	1.30	0.99	1.00
STM45151	CONDUIT	102.12	0	01:09	1.13	0.92	1.00
STM45152	CONDUIT	178.64	0	01:08	1.36	0.99	1.00
STM45153	CONDUIT	254.87	0	01:23	1.29	0.62	1.00
STM45154	CONDUIT	370.37	0	01:14	1.31	1.34	1.00
STM45155	CONDUIT	479.38	0	01:11	1.70	1.57	1.00
STM45156	CONDUIT	618.76	0	01:10	2.19	1.80	1.00
STM45159	CONDUIT	943.85	0	01:10	2.14	1.22	1.00
STM45160	CONDUIT	1060.10	0	01:11	2.49	1.33	0.92
STM45161	CONDUIT	307.04	0	01:10	1.41	0.84	0.92
STM45162	CONDUIT	339.11	0	01:14	1.58	1.39	1.00
STM45163	CONDUIT	31.43	0	01:08	0.70	0.34	0.51
STM45164_1	CONDUIT	41.17	0	01:10	0.67	0.43	0.62
STM45164_2	CONDUIT	85.74	0	01:11	1.23	0.89	0.60
STM45165	CONDUIT	135.79	0	01:10	1.47	0.61	0.56
212-ICD	DUMMY	21.32	0	01:30			
215-ICD	DUMMY	24.51	0	01:18			
IN09003-ICD	DUMMY	10.52	0	01:10			
IN09003-INC	DUMMY	10.92	0	01:10			
IN09004-ICD	DUMMY	12.96	0	01:11			
IN09004-INC	DUMMY	13.22	0	01:10			
IN09005-ICD	DUMMY	21.40	0	01:03			
IN09005-INC	DUMMY	49.44	0	01:10			
IN09006-ICD	DUMMY	21.40	0	01:05			
IN09006-INC	DUMMY	50.88	0	01:10			
IN09007-ICD	DUMMY	22.51	0	01:04			

IN09008-ICD	DUMMY	22.21	0	01:10			
IN09009-ICD	DUMMY	21.40	0	01:05			
IN09009-INC	DUMMY	54.70	0	01:10			
IN09010-ICD	DUMMY	1.60	0	02:30			
IN09010-INC	DUMMY	24.64	0	01:10			
IN09011-ICD	DUMMY	20.92	0	01:03			
IN09011-INC	DUMMY	55.00	0	01:07			
IN09012-ICD	DUMMY	21.40	0	01:03			
IN09012-INC	DUMMY	54.05	0	01:10			
IN09013-ICD	DUMMY	21.40	0	01:03			
IN09013-INC	DUMMY	55.00	0	01:08			
IN09014-ICD	DUMMY	21.40	0	01:08			
IN09014-INC	DUMMY	29.08	0	01:10			
IN09015-ICD	DUMMY	21.40	0	01:03			
IN09015-INC	DUMMY	55.00	0	01:08			
IN09016-ICD	DUMMY	22.51	0	01:05			
IN09017-ICD	DUMMY	12.70	0	01:11			
IN09017-INC	DUMMY	12.84	0	01:10			
IN09018-ICD	DUMMY	12.58	0	01:11			
IN09018-INC	DUMMY	12.72	0	01:10			
IN09019-ICD	DUMMY	21.40	0	01:04			
IN09019-INC	DUMMY	40.81	0	01:10			
IN09020-ICD	DUMMY	17.14	0	01:10			
IN09020-INC	DUMMY	18.91	0	01:10			
IN09021-ICD	DUMMY	30.37	0	01:01			
IN09021-INC	DUMMY	55.00	0	01:02			
IN09022-ICD	DUMMY	14.10	0	01:10			
IN09022-INC	DUMMY	14.32	0	01:10			
IN09023-ICD	DUMMY	12.46	0	01:11			
IN09023-INC	DUMMY	12.72	0	01:10			
IN09024-ICD	DUMMY	21.40	0	01:09			
IN09024-INC	DUMMY	26.78	0	01:10			
IN09025-ICD	DUMMY	21.40	0	01:07			
IN09025-INC	DUMMY	32.56	0	01:10			
IN09026-ICD	DUMMY	21.40	0	01:04			
IN09026-INC	DUMMY	49.26	0	01:10			
IN09027-ICD	DUMMY	21.40	0	01:05			
IN09027-INC	DUMMY	48.30	0	01:10			
IN09028-ICD	DUMMY	21.40	0	01:08			
IN09028-INC	DUMMY	30.80	0	01:10			
IN09029-ICD	DUMMY	21.40	0	01:04			
IN09029-INC	DUMMY	52.03	0	01:10			
IN09030-ICD	DUMMY	21.40	0	01:08			
IN09030-INC	DUMMY	30.79	0	01:11			
IN09031-ICD	DUMMY	19.88	0	01:10			
IN09031-INC	DUMMY	21.63	0	01:10			
IN09032-ICD	DUMMY	21.40	0	01:03			
IN09032-INC	DUMMY	55.00	0	01:05			
IN09033-ICD	DUMMY	21.40	0	01:05			
IN09033-INC	DUMMY	55.00	0	01:09			
IN09034-ICD	DUMMY	30.37	0	01:03			
IN09034-INC	DUMMY	55.00	0	01:04			
IN09035-ICD	DUMMY	30.37	0	01:03			

IN09035-INC	DUMMY	55.00	0	01:05
IN103407-ICD	DUMMY	31.48	0	01:10

Flow Classification Summary

Conduit	Adjusted Length	Fraction of Time in Flow Class									
		Dry	Dry	Up	Down	Sub	Sup	Up	Down	Norm	Inlet
Crit	Crit	Crit	Crit	Crit	Crit	Crit	Crit	Crit	Ltd	Ctrl	
C01	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	
C02	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	
C03	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	
C04	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	
C05	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	
C06	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	
C07	1.00	0.00	0.00	0.00	0.14	0.86	0.00	0.00	0.00	0.00	
C08	1.00	0.00	0.00	0.00	0.75	0.25	0.00	0.00	0.57	0.00	
C09	1.00	0.00	0.00	0.00	0.67	0.01	0.00	0.31	0.01	0.00	
C1	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	
C10	1.00	0.00	0.00	0.00	0.21	0.12	0.00	0.66	0.01	0.00	
C11	1.00	0.02	0.00	0.00	0.34	0.00	0.00	0.64	0.06	0.00	
C12	1.00	0.00	0.00	0.00	0.31	0.01	0.00	0.68	0.08	0.00	
C13	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	
C14	1.00	0.00	0.00	0.00	0.50	0.02	0.00	0.48	0.20	0.00	
C15	1.00	0.34	0.00	0.00	0.54	0.00	0.00	0.11	0.00	0.00	
C16	1.00	0.00	0.00	0.00	0.51	0.02	0.00	0.47	0.02	0.00	
C17	1.00	0.00	0.00	0.00	0.97	0.03	0.00	0.00	0.91	0.00	
C18	1.00	0.00	0.00	0.00	0.96	0.04	0.00	0.00	0.51	0.00	
C19	1.00	0.00	0.01	0.00	0.99	0.00	0.00	0.00	0.98	0.00	
C2	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	
C20	1.00	0.00	0.00	0.00	0.27	0.00	0.00	0.72	0.12	0.00	
C21	1.00	0.00	0.00	0.00	0.64	0.01	0.00	0.35	0.06	0.00	
C22	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	
C23	1.00	0.00	0.00	0.00	0.27	0.03	0.00	0.70	0.08	0.00	
C24	1.00	0.17	0.00	0.00	0.77	0.01	0.00	0.04	0.00	0.00	
C25	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00	
C26	1.00	0.00	0.00	0.00	0.03	0.00	0.00	0.97	0.00	0.00	
C27	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	
C28	1.00	0.00	0.00	0.00	0.58	0.42	0.00	0.00	0.51	0.00	
C29	1.00	0.00	0.14	0.00	0.49	0.36	0.00	0.00	0.77	0.00	
C3	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	
C30	1.00	0.01	0.00	0.00	0.65	0.34	0.00	0.00	0.65	0.00	
C31	1.00	0.01	0.00	0.00	0.68	0.31	0.00	0.00	0.58	0.00	
C32	1.00	0.01	0.00	0.00	0.72	0.27	0.00	0.00	0.57	0.00	
C33	1.00	0.01	0.00	0.00	0.74	0.25	0.00	0.00	0.50	0.00	
C34	1.00	0.02	0.00	0.00	0.38	0.00	0.00	0.60	0.01	0.00	
C35	1.00	0.03	0.00	0.00	0.56	0.00	0.00	0.41	0.00	0.00	
C36	1.00	0.02	0.00	0.00	0.98	0.00	0.00	0.00	0.43	0.00	
C37	1.00	0.01	0.00	0.00	0.98	0.00	0.00	0.00	0.45	0.00	

C38	1.00	0.01	0.00	0.00	0.99	0.00	0.00	0.00	0.48	0.00
C39	1.00	0.75	0.00	0.00	0.11	0.14	0.00	0.00	0.04	0.00
C4	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
C40	1.00	0.00	0.02	0.00	0.98	0.00	0.00	0.00	0.42	0.00
C5	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
C6	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
C7	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
C8	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
C9	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
C98	1.00	0.01	0.00	0.00	0.96	0.04	0.00	0.00	0.00	0.00
C99	1.00	0.01	0.00	0.00	0.82	0.00	0.00	0.17	0.00	0.00
OF1	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
R01	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.99	0.00
R02	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
R03	1.00	0.00	0.00	0.00	0.17	0.00	0.00	0.83	0.07	0.00
R04	1.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
R05	1.00	0.00	0.79	0.00	0.20	0.00	0.00	0.00	0.77	0.00
R06	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.99	0.00
R07	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.99	0.00
R08	1.00	0.00	0.00	0.00	0.50	0.50	0.00	0.00	0.00	0.00
R09	1.00	0.01	0.00	0.00	0.69	0.30	0.00	0.00	0.73	0.00
R10	1.00	0.00	0.01	0.00	0.99	0.00	0.00	0.00	0.94	0.00
R11	1.00	0.00	0.00	0.00	0.93	0.07	0.00	0.00	0.48	0.00
R12	1.00	0.00	0.00	0.00	0.91	0.09	0.00	0.00	0.58	0.00
R13	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
R14	1.00	0.00	0.00	0.00	0.27	0.00	0.00	0.73	0.16	0.00
R15	1.00	0.00	0.01	0.00	0.99	0.00	0.00	0.00	0.98	0.00
R16	1.00	0.00	0.00	0.00	0.99	0.01	0.00	0.00	0.11	0.00
R17	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.16	0.00
R18	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.99	0.00
R19	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.00	0.93	0.00
R20	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.99	0.00
R21	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.99	0.00
R22	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
R23	1.00	0.00	0.00	0.00	0.27	0.00	0.00	0.73	0.16	0.00
R24	1.00	0.00	0.00	0.00	0.18	0.01	0.00	0.80	0.08	0.00
R25	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.99	0.00
R26	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.00	0.97	0.00
R27	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.99	0.00
R28	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.99	0.00
R29	1.00	0.00	0.00	0.00	0.80	0.20	0.00	0.00	0.00	0.00
R30	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.75	0.00
R31	1.00	0.00	0.00	0.00	0.41	0.59	0.00	0.00	0.39	0.00
R32	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.99	0.00
R33	1.00	0.00	0.01	0.00	0.99	0.00	0.00	0.00	0.98	0.00
R34	1.00	0.00	0.00	0.00	0.85	0.15	0.00	0.00	0.56	0.00
STM04620	1.00	0.01	0.00	0.00	0.32	0.00	0.00	0.67	0.00	0.00
STM04621	1.00	0.00	0.00	0.00	0.15	0.00	0.00	0.85	0.00	0.00
STM07857	1.00	0.00	0.01	0.00	0.99	0.01	0.00	0.00	0.93	0.00
STM07870	1.00	0.01	0.00	0.00	0.18	0.00	0.00	0.81	0.00	0.00
STM07871	1.00	0.00	0.00	0.00	0.99	0.01	0.00	0.00	0.00	0.00
STM07872	1.00	0.00	0.00	0.00	0.20	0.00	0.00	0.79	0.00	0.00
STM07873	1.00	0.01	0.00	0.00	0.10	0.00	0.00	0.89	0.00	0.00

STM07874	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.70	0.00
STM07875	1.00	0.00	0.00	0.00	0.03	0.00	0.00	0.97	0.01	0.00
STM07876	1.00	0.00	0.00	0.00	0.18	0.00	0.00	0.81	0.04	0.00
STM45150	1.00	0.00	0.00	0.00	0.07	0.00	0.00	0.93	0.00	0.00
STM45151	1.00	0.01	0.00	0.00	0.15	0.00	0.00	0.85	0.02	0.00
STM45152	1.00	0.00	0.00	0.00	0.08	0.00	0.00	0.92	0.01	0.00
STM45153	1.00	0.00	0.00	0.00	0.19	0.18	0.00	0.63	0.13	0.00
STM45154	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.81	0.00
STM45155	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.85	0.00
STM45156	1.00	0.00	0.00	0.00	0.98	0.00	0.00	0.02	0.74	0.00
STM45159	1.00	0.00	0.00	0.00	0.36	0.64	0.00	0.00	0.41	0.00
STM45160	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
STM45161	1.00	0.00	0.00	0.00	0.50	0.00	0.00	0.50	0.03	0.00
STM45162	1.00	0.01	0.00	0.00	0.12	0.00	0.00	0.87	0.00	0.00
STM45163	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.46	0.00
STM45164_1	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
STM45164_2	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
STM45165	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00

Conduit Surcharge Summary

Conduit	Hours		Hours		Capacity		
	Both Ends	Full	Upstream	Dnstream	Above Full	Normal Flow	Limited
C08	1.93	1.93	3.08	0.01	0.01		
C09	2.39	2.39	2.42	0.01	0.01		
C1	0.01	0.05	0.01	0.10	0.01		
C11	1.03	1.03	1.41	0.01	0.01		
C12	0.66	0.66	1.24	0.01	0.01		
C13	0.25	0.59	0.25	0.69	0.25		
C14	1.06	1.06	2.30	0.01	0.01		
C15	2.16	2.16	2.24	0.01	0.01		
C16	1.43	1.43	1.53	0.01	0.01		
C19	0.01	0.01	0.01	0.01	0.01		
C20	0.01	0.01	1.07	0.01	0.01		
C21	2.67	2.67	3.00	0.01	0.01		
C22	0.01	0.04	0.01	0.07	0.01		
C23	0.24	0.24	0.96	0.01	0.01		
C24	3.10	3.10	3.20	0.01	0.01		
C26	0.09	0.31	0.09	0.37	0.06		
C27	0.33	0.71	0.33	0.82	0.33		
C29	0.01	0.01	0.56	0.01	0.01		
C3	0.01	0.01	0.01	0.02	0.01		
C30	0.56	0.56	0.79	0.01	0.01		
C31	0.79	0.79	1.09	0.01	0.01		
C32	1.09	1.09	1.40	0.01	0.01		
C33	1.40	1.40	1.66	0.01	0.01		
C34	1.66	1.66	1.74	0.01	0.01		

C35	2.49	2.49	2.50	0.01	0.01
C36	2.44	2.44	2.50	0.01	0.01
C37	2.38	2.38	2.45	0.01	0.01
C38	2.32	2.32	2.39	0.01	0.01
C40	2.49	2.49	2.67	0.01	0.01
C5	0.01	0.23	0.01	0.28	0.01
C6	0.02	0.29	0.02	0.33	0.02
C7	0.04	0.41	0.04	0.49	0.04
C8	0.01	0.12	0.01	0.18	0.01
C9	0.01	0.06	0.01	0.10	0.01
C98	3.62	4.18	3.62	1.44	0.69
C99	4.16	5.25	4.16	1.32	0.15
R10	0.01	0.01	0.09	0.01	0.01
R16	0.01	0.01	0.16	0.01	0.01
R17	0.01	0.01	0.16	0.01	0.01
R18	0.01	0.01	0.17	0.01	0.01
R19	0.01	0.01	0.16	0.01	0.01
R33	0.01	0.01	0.09	0.01	0.01
STM04620	0.01	0.02	0.01	0.17	0.01
STM04621	0.01	0.01	0.01	0.01	0.01
STM07870	0.03	0.14	0.03	0.52	0.03
STM07871	0.01	0.14	0.01	0.47	0.01
STM07872	0.12	0.30	0.12	0.48	0.12
STM07873	0.13	0.13	0.20	0.01	0.01
STM07876	0.06	0.06	0.13	0.01	0.01
STM45150	0.13	0.13	0.14	0.01	0.01
STM45151	0.16	0.16	0.21	0.01	0.01
STM45152	0.20	0.20	0.24	0.01	0.01
STM45153	0.24	0.24	0.38	0.01	0.01
STM45154	0.38	0.38	0.39	0.35	0.36
STM45155	0.38	0.39	0.38	0.42	0.38
STM45156	0.35	0.38	0.35	0.46	0.35
STM45159	0.23	0.27	0.23	0.34	0.23
STM45160	0.01	0.23	0.01	0.38	0.01
STM45161	0.01	0.01	0.09	0.01	0.01
STM45162	0.10	0.11	0.10	0.44	0.10

Analysis begun on: Fri Nov 01 14:46:54 2019
Analysis ended on: Fri Nov 01 14:46:56 2019
Total elapsed time: 00:00:02

PCSWMM Report

PCSWMM REPORT Model 250806_Post_Dev_Rev3.inp

exp Services Inc.
November 1, 2019

Table of Contents

Summaries

Summary 1: Subcatchment attributes	4
Summary 2: Storage attributes	6
Summary 3: Conduit attributes	6

Maps

Figure 1: SUBCATCHMENTS	8
Figure 2: CONDUITS	9
Figure 3: PONDING AREAS	10
Figure 4: OFFSITE STRUCTURES	11
Figure 5: ONSITE SYSTEM	12

Graphs

Figure 6: CONDUIT 10	13
Figure 7: LINK 212-ICD	14
Figure 8: LINK 215-ICD	15
Figure 9: CHAMBERS 1	16
Figure 10: CHAMBERS 2	17
Figure 11: STM07871 - MAIN OUTLET	18

Profiles

Figure 12: Node MHST09016 to Node OF-CREEK (Denham Way)	19
Figure 13: Node MHST09001 to Node OF-CREEK (Victor St)	20
Figure 14: Node MHST09024 to Node OF-CREEK (Savage Dr)	21
Figure 15: Node CBE04 to Node CBE15 (Perforated Pipes Along Hazeldean) ..	22

Table of Contents

Figure 16: Node CBE01 to Node CHAMBERS-2 (Rear Perf Pipes)	23
Figure 17: Node CB03 to Node 205 (Through West Chambers 1)	24
Figure 18: Node 207 to Node 200 (Onsite Storm)	25
Figure 19: Node CB06 to Node 216 (Through East Chambers 1)	26
Figure 20: Node CB01 to Node 216 (Through East Chambers 2)	27

Tables

Table 1: OUTFALL - SUMMARY	28
Table 2: JUNCTIONS - SUMMARY	28
Table 3: STORAGES - SUMMARY	31
Table 4A: CONDUITS - SUMMARY	32
Table 4B: CONDUITS - SUMMARY	35
Table 5: OUTLETS - SUMMARY	39
Table 6: SUBCATCHMENTS - SUMMARY	42
Table 7: Existing_Structures	44

Summary 1: Subcatchment attributes

Name	Chicago_3h_100yr	Chicago_3h_100yr + 20%	Chicago_3h_2yr	Chicago_3h_5yr	Historic_Aug4-88	Historic_Jul1-79
S01 - Peak Runoff (L/s)	82.67	100.76	30.40	44.35	72.47	50.26
S02 - Peak Runoff (L/s)	71.96	86.87	28.12	40.27	62.84	43.21
S03 - Peak Runoff (L/s)	7.77	9.62	0.89	3.36	6.99	4.66
S04 - Peak Runoff (L/s)	93.97	114.71	34.08	50.02	82.51	57.24
S05 - Peak Runoff (L/s)	58.44	71.70	20.19	30.29	51.52	35.81
S06 - Peak Runoff (L/s)	24.73	31.82	4.96	9.80	22.35	16.10
S07 - Peak Runoff (L/s)	17.89	22.48	3.61	7.55	15.86	11.13
S08_1 - Peak Runoff (L/s)	18.78	22.96	5.39	9.42	16.58	11.32
S08_2 - Peak Runoff (L/s)	25.13	30.84	6.76	12.23	22.18	15.20
S09 - Peak Runoff (L/s)	38.21	46.38	12.65	20.28	33.69	22.94
ES33 - Peak Runoff (L/s)	47.79	64.41	11.03	18.72	48.02	35.28
ES34 - Peak Runoff (L/s)	51.83	75.89	9.08	16.69	66.39	52.31
ES35 - Peak Runoff (L/s)	111.11	152.57	30.60	46.99	131.48	97.37
ES31 - Peak Runoff (L/s)	47.58	65.58	10.47	17.88	50.84	37.31
ES30 - Peak Runoff (L/s)	56.63	77.01	14.18	22.90	60.14	43.64
ES29 - Peak Runoff (L/s)	68.63	92.94	18.78	29.14	74.82	53.41
ES28 - Peak Runoff (L/s)	64.88	89.51	16.15	25.90	73.26	52.48
ES27 - Peak Runoff (L/s)	54.47	78.14	10.87	18.94	66.64	50.12
ES02_1 - Peak Runoff (L/s)	30.94	41.11	6.13	11.59	29.35	21.62
ES32 - Peak Runoff (L/s)	112.14	150.74	33.60	50.29	125.93	88.06
ES19 - Peak Runoff (L/s)	41.93	52.66	13.50	20.46	37.86	26.84
ES17 - Peak Runoff (L/s)	55.84	71.13	12.53	23.37	50.13	35.81
ES18 - Peak Runoff (L/s)	90.96	118.04	21.29	37.43	83.97	60.91
ES20 - Peak Runoff (L/s)	21.34	28.64	5.01	8.46	21.26	15.60
ES23 - Peak Runoff (L/s)	42.22	55.96	12.85	19.24	44.38	31.50
ES24 - Peak Runoff (L/s)	19.00	25.95	4.72	7.63	20.44	14.81
ES25 - Peak Runoff (L/s)	35.11	46.54	10.96	16.23	37.69	26.49

Summary 1: Subcatchment attributes (continued...)

Name	Chicago_3h_100yr	Chicago_3h_100yr + 20%	Chicago_3h_2yr	Chicago_3h_5yr	Historic_Aug4-88	Historic_Jul1-79
ES26 - Peak Runoff (L/s)	26.76	35.82	7.55	11.63	28.13	20.17
ES07 - Peak Runoff (L/s)	84.64	107.91	25.77	39.66	78.05	55.85
ES36 - Peak Runoff (L/s)	67.90	91.18	15.11	26.28	67.04	49.38
ES03_1 - Peak Runoff (L/s)	117.06	147.99	33.81	54.15	105.69	75.21
ES03_2 - Peak Runoff (L/s)	78.36	99.34	20.61	34.85	70.52	50.26
ES04_1 - Peak Runoff (L/s)	86.50	109.27	27.17	41.49	78.68	56.00
ES04_2 - Peak Runoff (L/s)	77.94	99.28	23.27	36.23	71.52	51.16
ES05_1 - Peak Runoff (L/s)	73.56	94.34	21.52	33.65	68.24	49.01
ES05_2 - Peak Runoff (L/s)	72.79	92.90	21.68	33.72	67.04	48.01
ES06_1 - Peak Runoff (L/s)	114.20	144.42	35.44	54.41	103.93	74.01
ES06_2 - Peak Runoff (L/s)	96.52	122.87	28.75	44.85	88.45	63.26
ES14_1 - Peak Runoff (L/s)	50.68	65.60	12.36	21.26	46.76	33.85
ES14_2 - Peak Runoff (L/s)	75.15	94.83	23.50	36.01	68.19	48.49
ES15_1 - Peak Runoff (L/s)	28.79	37.23	6.04	11.47	26.23	18.98
ES15_2 - Peak Runoff (L/s)	50.78	64.25	15.16	23.79	46.04	32.79
ES01_1 - Peak Runoff (L/s)	136.23	170.49	47.31	69.10	123.06	87.44
ES02_2 - Peak Runoff (L/s)	19.92	25.29	4.75	8.55	17.86	12.73
ES08_1 - Peak Runoff (L/s)	47.03	60.74	11.88	20.06	43.38	31.35
ES08_2 - Peak Runoff (L/s)	26.66	36.02	5.61	10.01	26.51	19.59
ES09_1 - Peak Runoff (L/s)	69.77	88.91	20.29	32.04	63.86	45.71
ES09_2 - Peak Runoff (L/s)	66.73	87.05	15.85	27.41	62.28	45.31
ES13_1 - Peak Runoff (L/s)	61.86	78.75	18.97	29.12	56.93	40.70
ES13_2 - Peak Runoff (L/s)	66.03	84.34	19.39	30.37	60.79	43.56
ES12_1 - Peak Runoff (L/s)	77.52	98.53	23.59	36.42	71.04	50.74
ES12_2 - Peak Runoff (L/s)	62.08	79.05	18.60	28.91	56.96	40.74
ES11_1 - Peak Runoff (L/s)	73.06	93.16	21.94	34.01	67.25	48.13
ES11_2 - Peak Runoff (L/s)	46.57	60.53	12.21	20.02	43.69	31.66

Summary 1: Subcatchment attributes (continued...)

Name	Chicago_3h_100yr	Chicago_3h_100yr + 20%	Chicago_3h_2yr	Chicago_3h_5yr	Historic_Aug4-88	Historic_Jul1-79
ES10_1 - Peak Runoff (L/s)	81.11	104.33	23.06	36.52	75.37	54.24
ES10_2 - Peak Runoff (L/s)	71.32	91.74	19.39	31.49	65.86	47.44
ES16_1 - Peak Runoff (L/s)	42.73	53.85	8.22	17.66	37.92	26.68
ES16_2 - Peak Runoff (L/s)	62.28	82.65	10.51	22.13	58.23	42.94
ES22_1 - Peak Runoff (L/s)	76.42	96.26	24.92	37.39	69.46	49.37
ES22_2 - Peak Runoff (L/s)	86.17	109.85	26.13	40.30	79.38	56.80
ES21_3 - Peak Runoff (L/s)	44.83	58.74	11.92	19.23	42.97	31.21
ES21_4 - Peak Runoff (L/s)	58.40	73.46	18.93	28.53	52.92	37.57
ES21_1 - Peak Runoff (L/s)	32.28	40.86	10.05	15.39	29.45	20.98
ES21_5 - Peak Runoff (L/s)	33.42	42.72	10.22	15.65	31.02	22.22

Summary 2: Storage attributes

Name	Chicago_3h_100yr	Chicago_3h_100yr + 20%	Chicago_3h_2yr	Chicago_3h_5yr	Historic_Aug4-88	Historic_Jul1-79
CHAMBERS-1 - Max. HGL (m)	112.81	113.14	111.96	112.18	112.89	113.08
CHAMBERS-1 - Max. Outflow (L/s)	27.30	24.61	19.80	23.09	21.95	23.24
CHAMBERS-1 - Max. Volume (1000 m ³)	0.118	0.148	0.041	0.060	0.125	0.142
CHAMBERS-2 - Max. HGL (m)	114.08	114.36	112.88	113.16	114.28	114.17
CHAMBERS-2 - Max. Outflow (L/s)	94.63	90.70	94.40	94.07	60.53	139.72
CHAMBERS-2 - Max. Volume (1000 m ³)	0.155	0.155	0.054	0.080	0.155	0.155

Summary 3: Conduit attributes

Name	Chicago_3h_100yr	Chicago_3h_100yr + 20%	Chicago_3h_2yr	Chicago_3h_5yr	Historic_Aug4-88	Historic_Jul1-79

Summary 3: Conduit attributes (continued...)

Name	Chicago_3h_100yr	Chicago_3h_100yr + 20%	Chicago_3h_2yr	Chicago_3h_5yr	Historic_Aug4-88	Historic_Jul1-79
C10 - Max. Flow (L/s)	50.50	52.84	32.76	38.13	51.45	52.53



Figure 1: SUBCATCHMENTS



Figure 2: CONDUITS

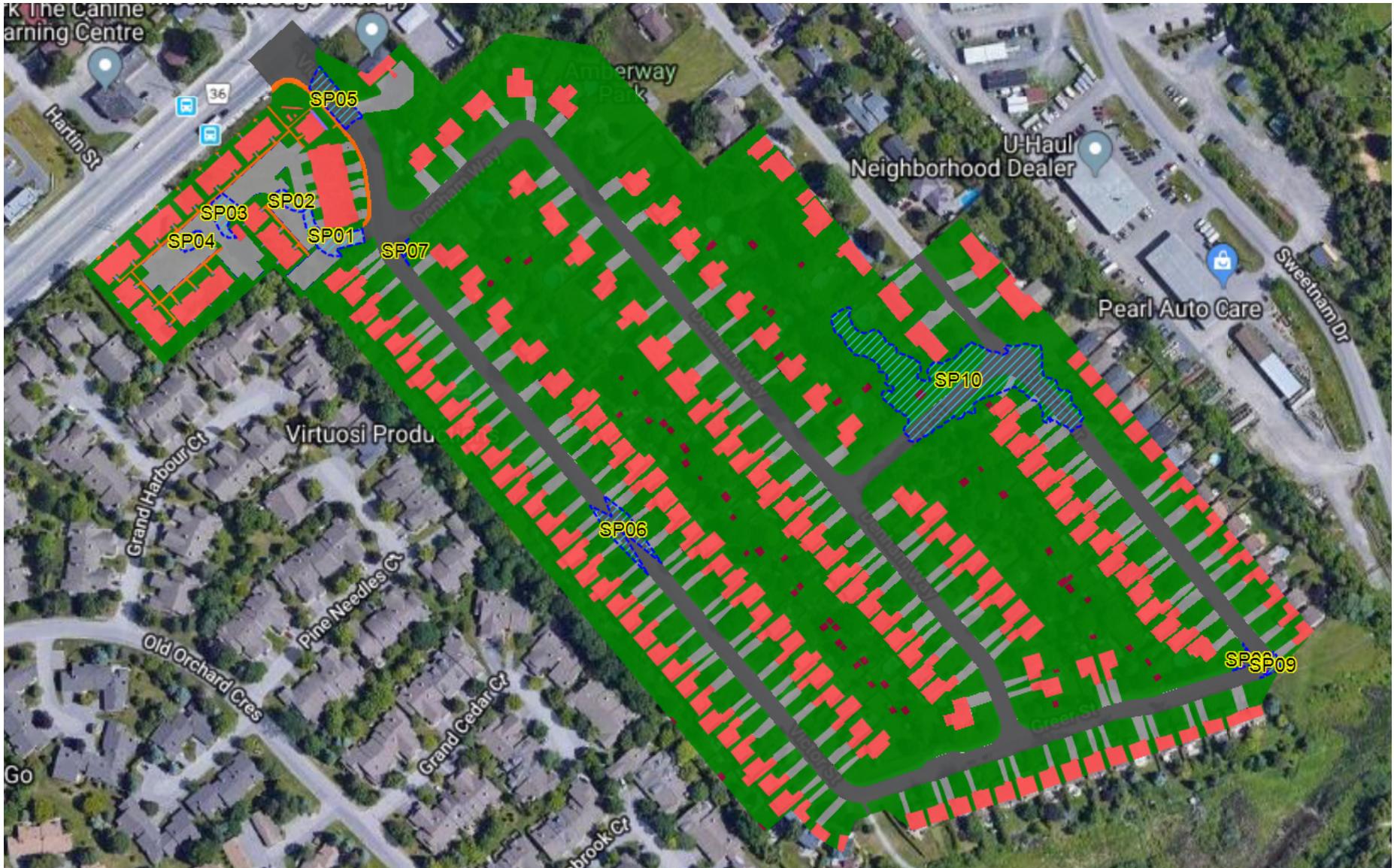


Figure 3: PONDING AREAS



Figure 4: OFFSITE STRUCTURES



Figure 5: ONSITE SYSTEM

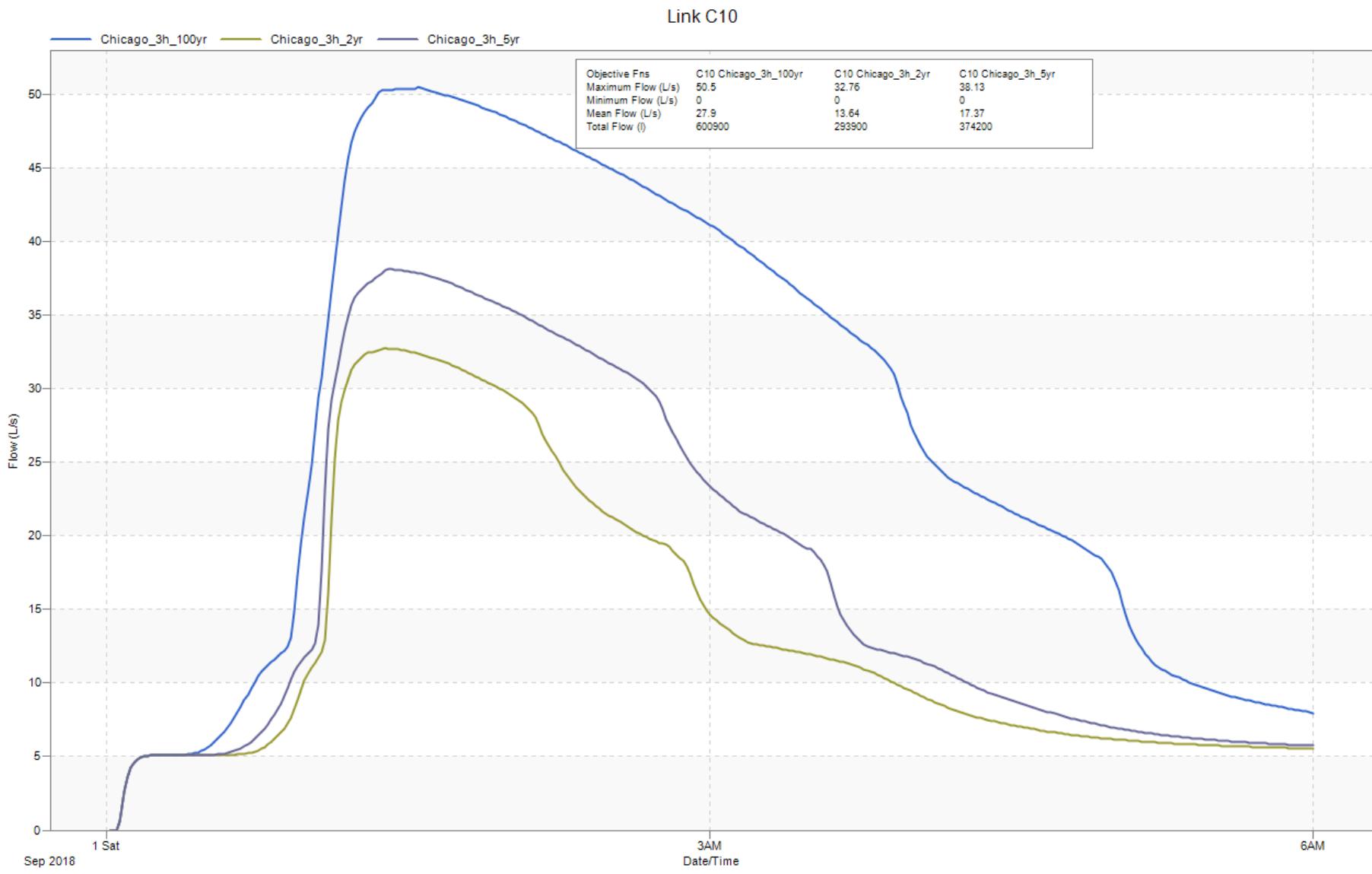


Figure 6: CONDUIT 10

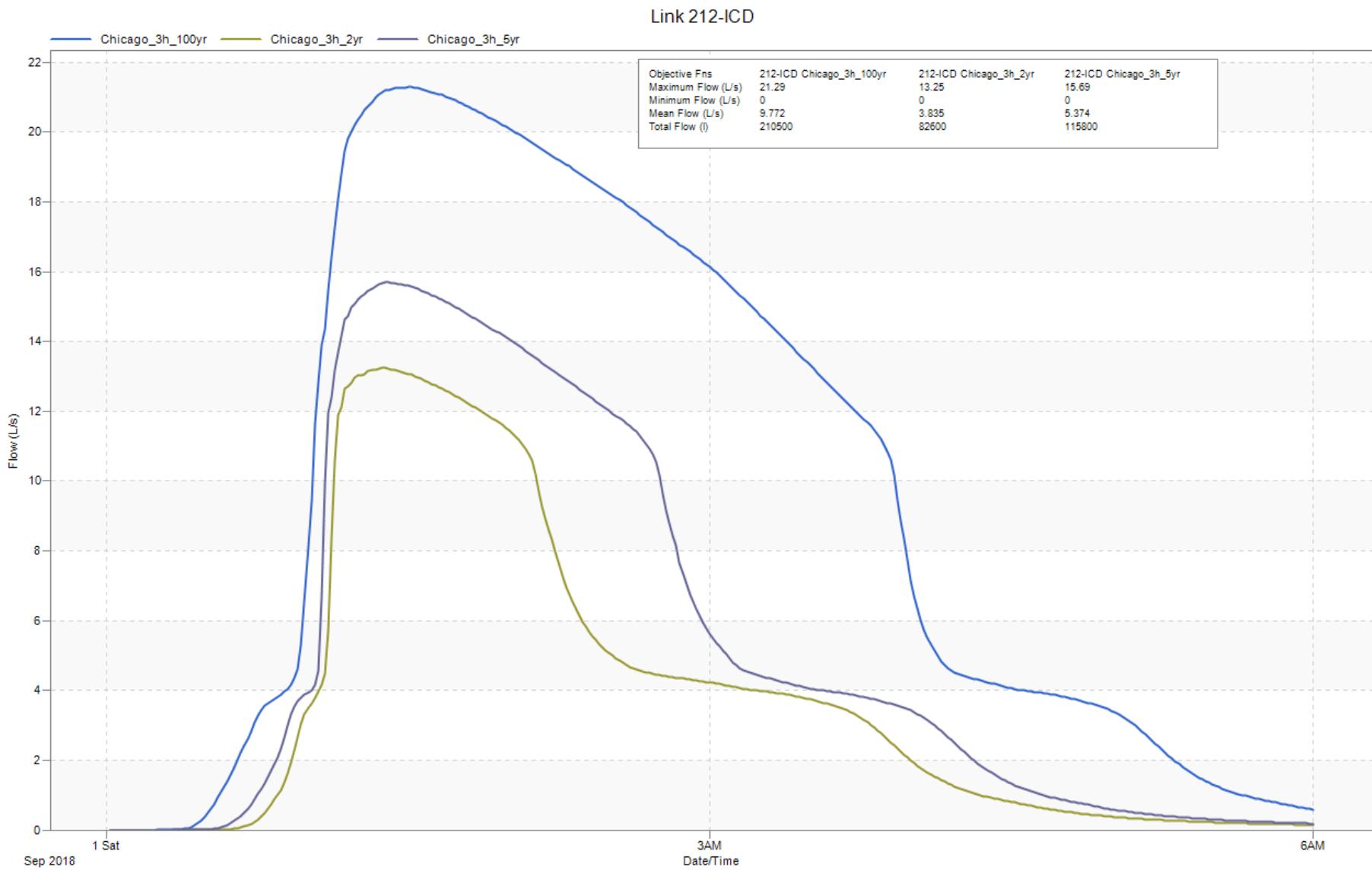


Figure 7: LINK 212-ICD

Link 215-ICD

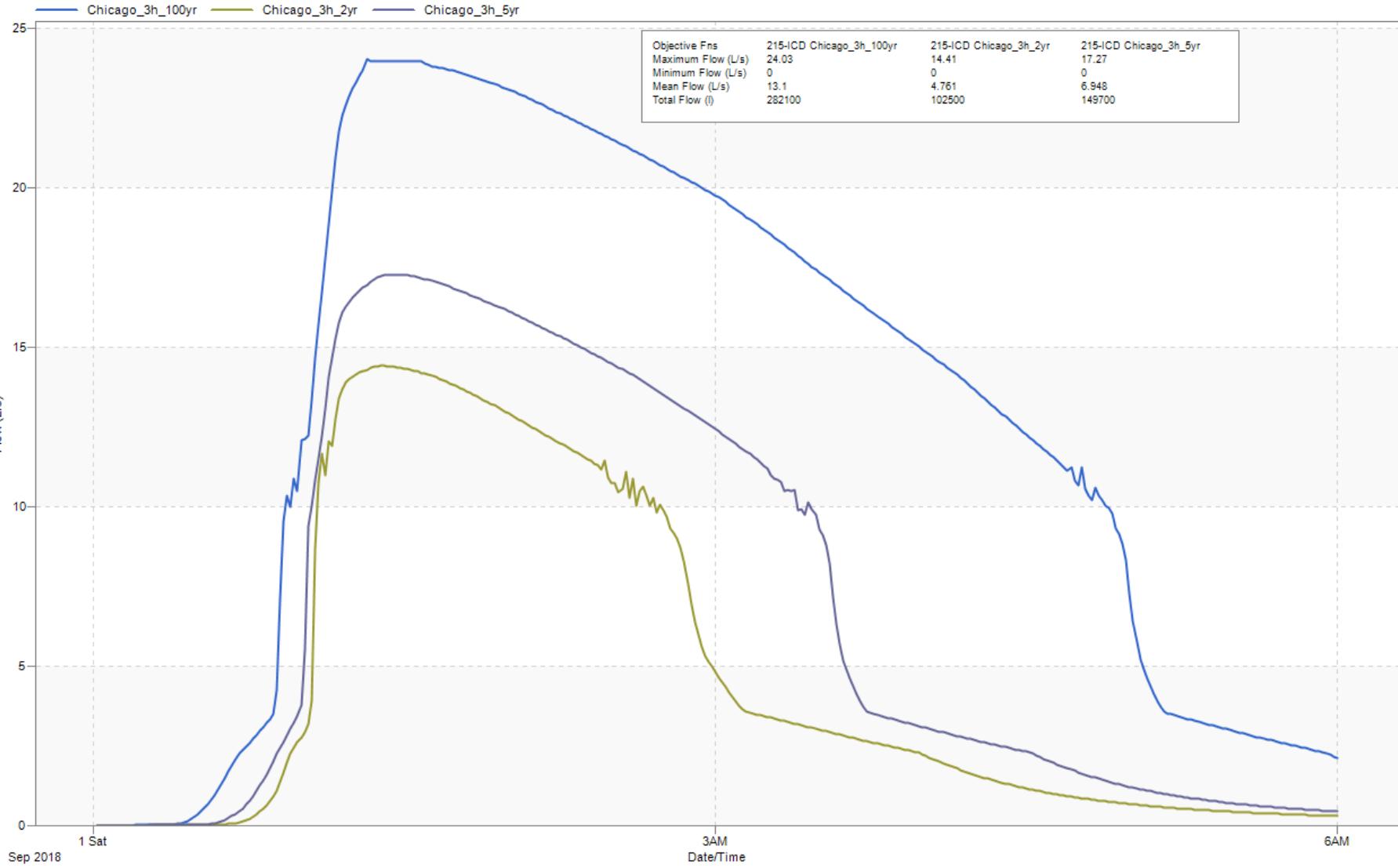


Figure 8: LINK 215-ICD

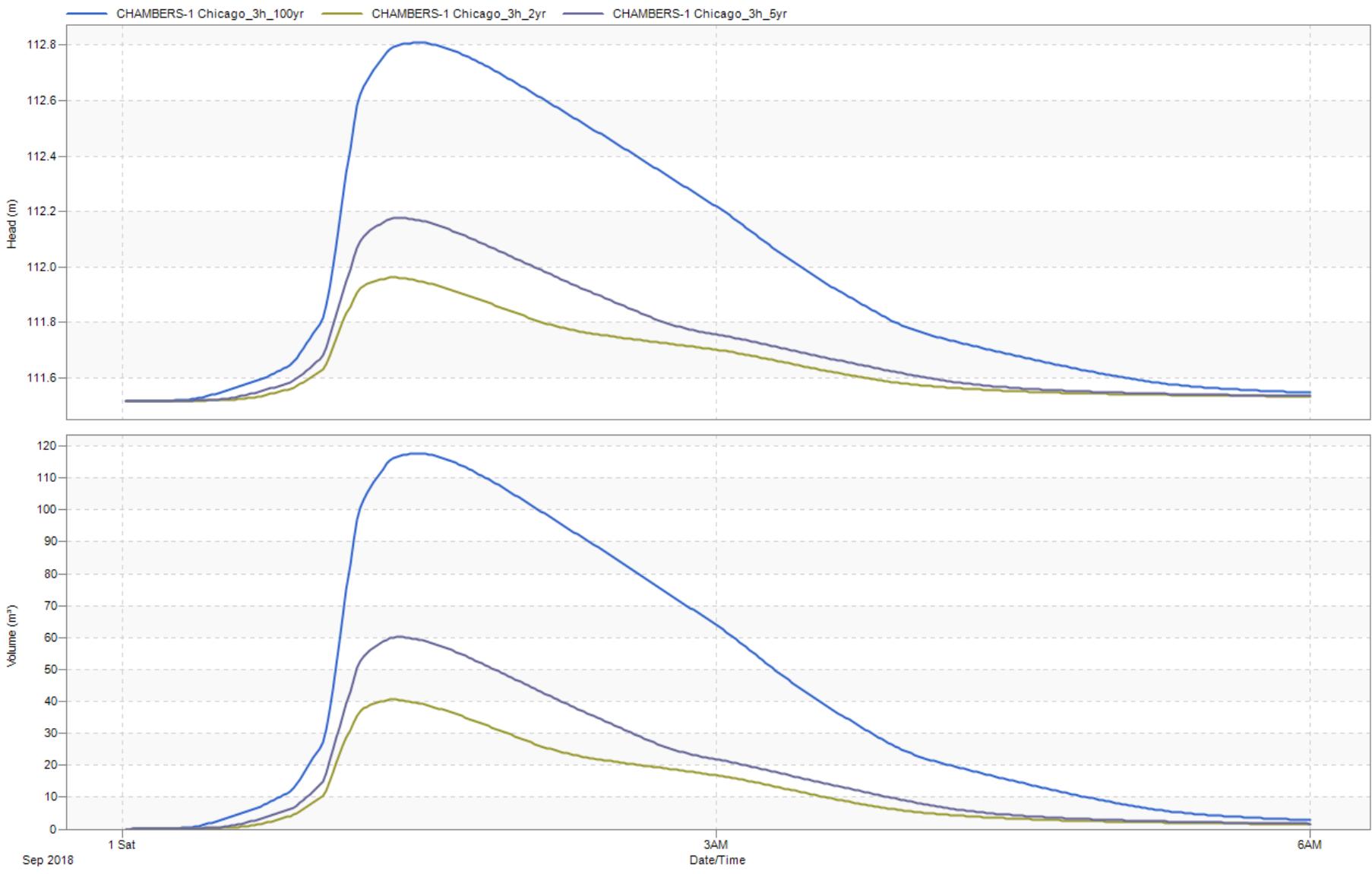


Figure 9: CHAMBERS 1

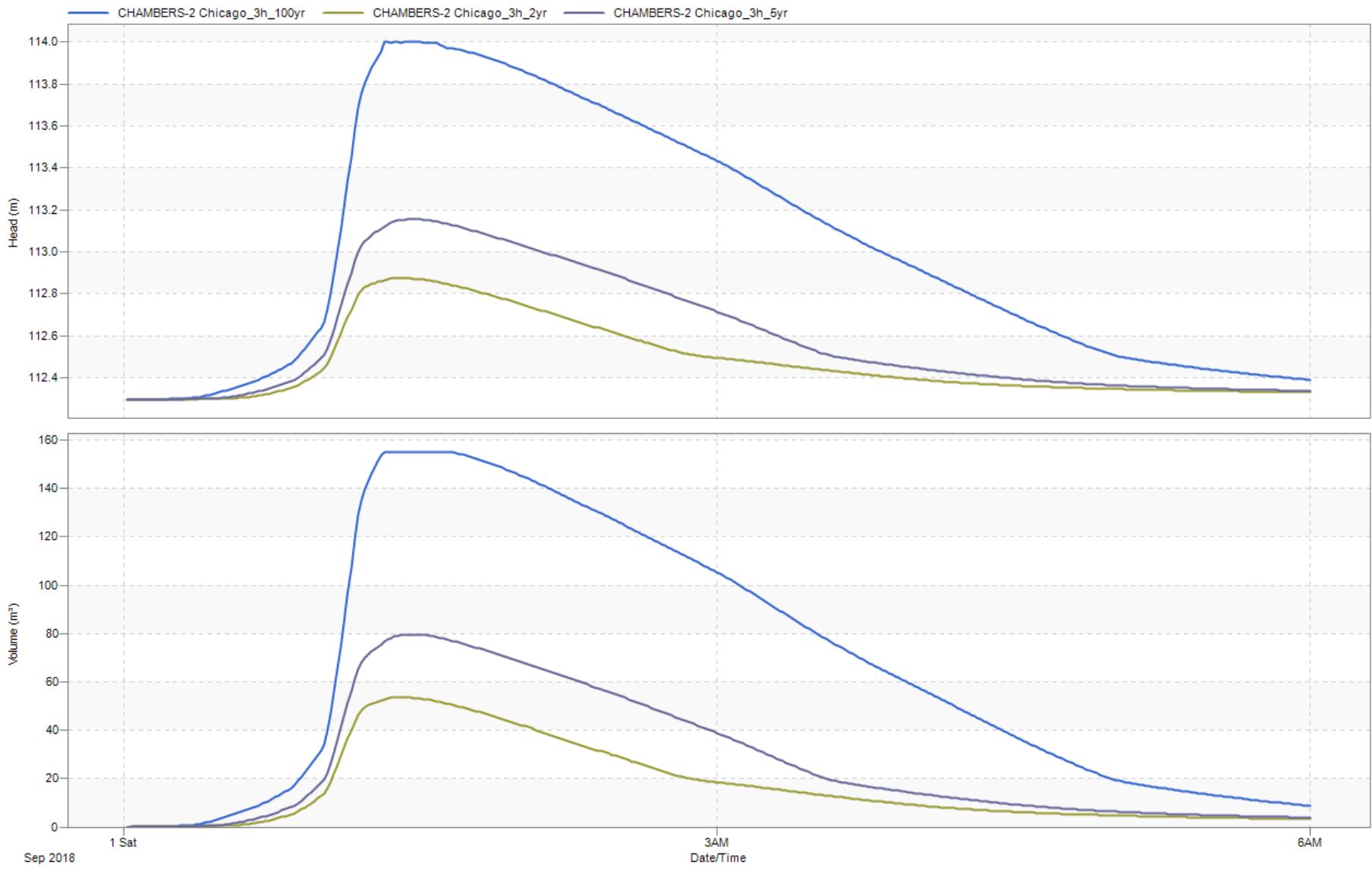


Figure 10: CHAMBERS 2

Link STM07871

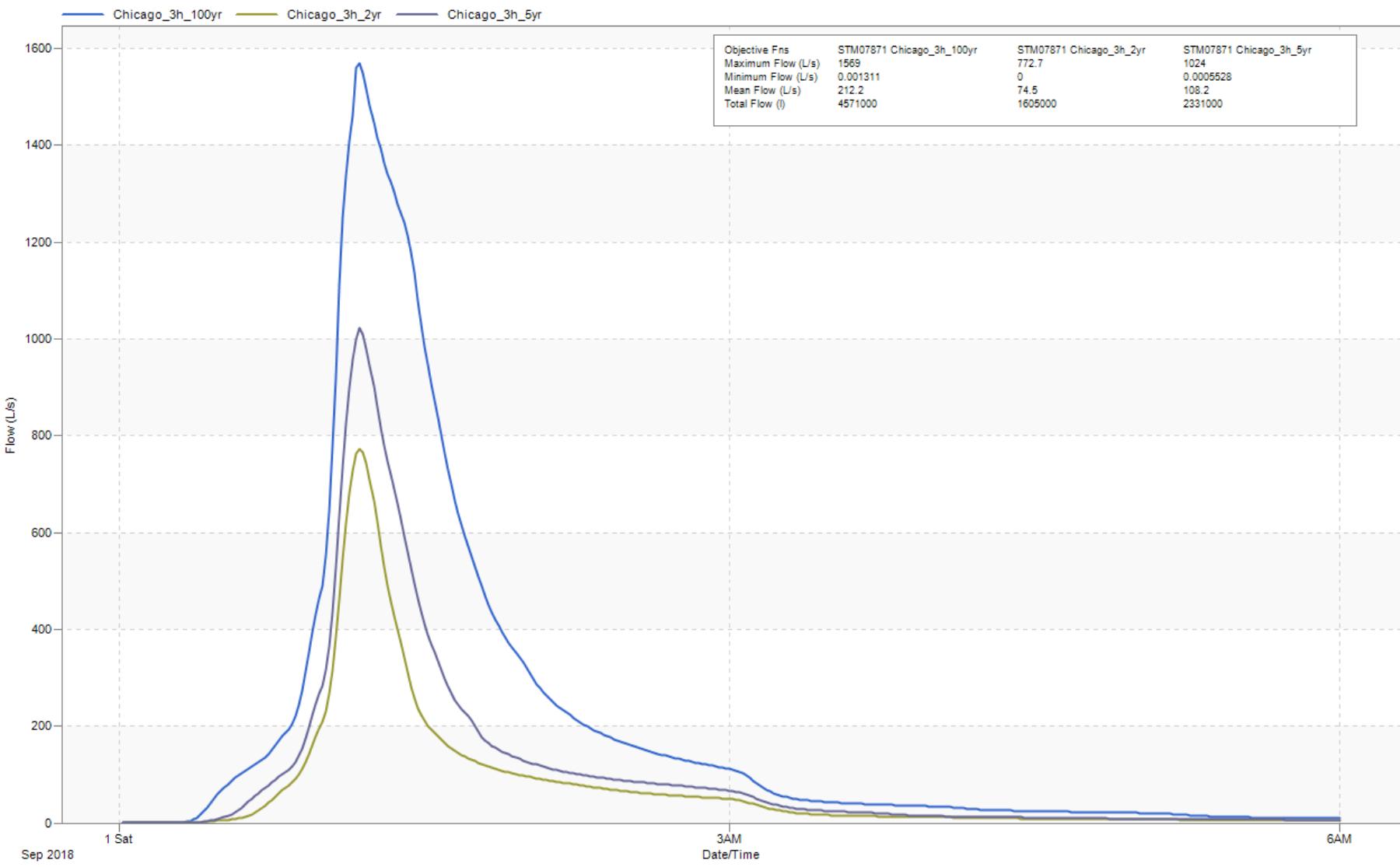


Figure 11: STM07871 - MAIN OUTLET

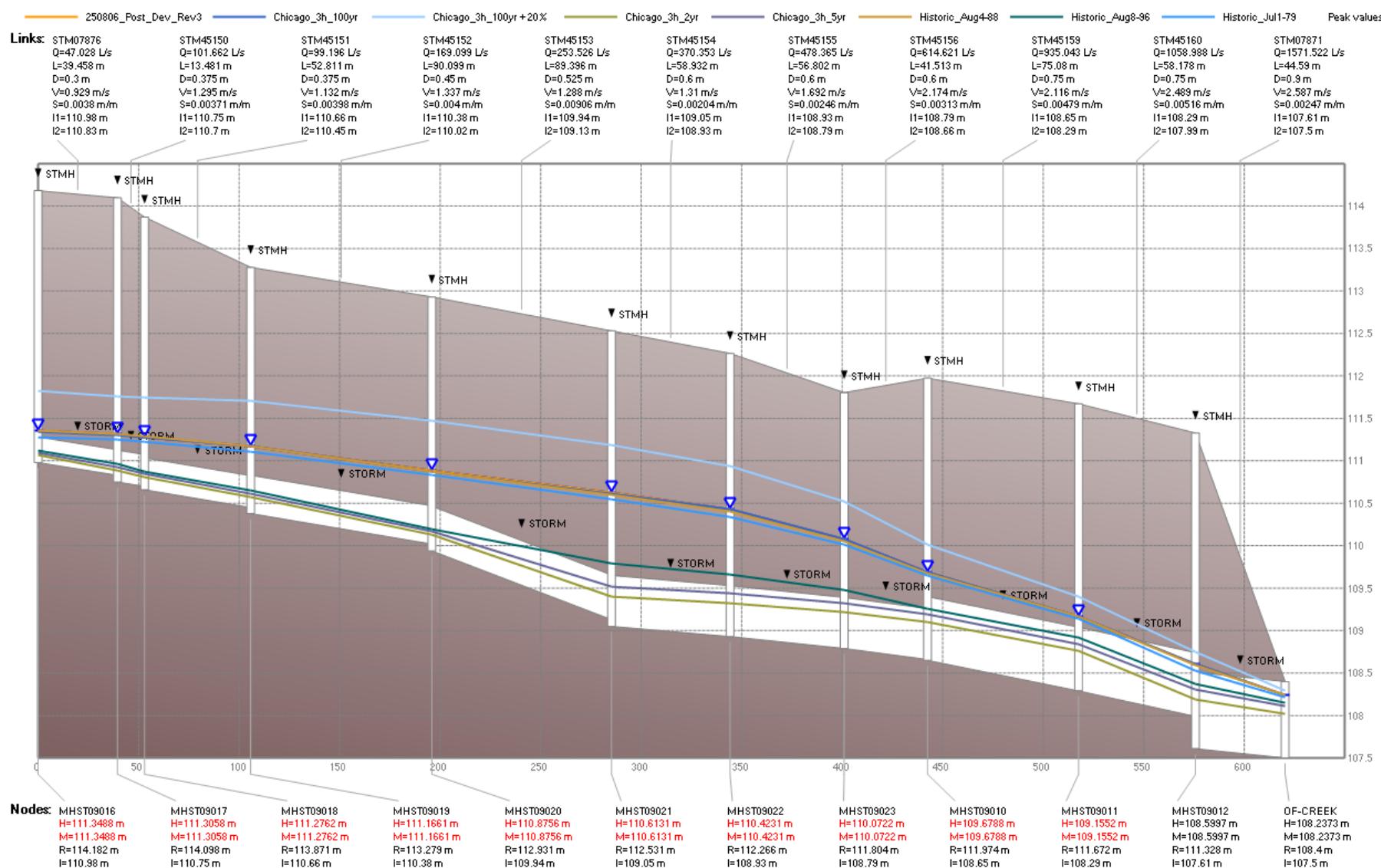


Figure 12: Node MHST09016 to Node OF-CREEK (Denham Way)

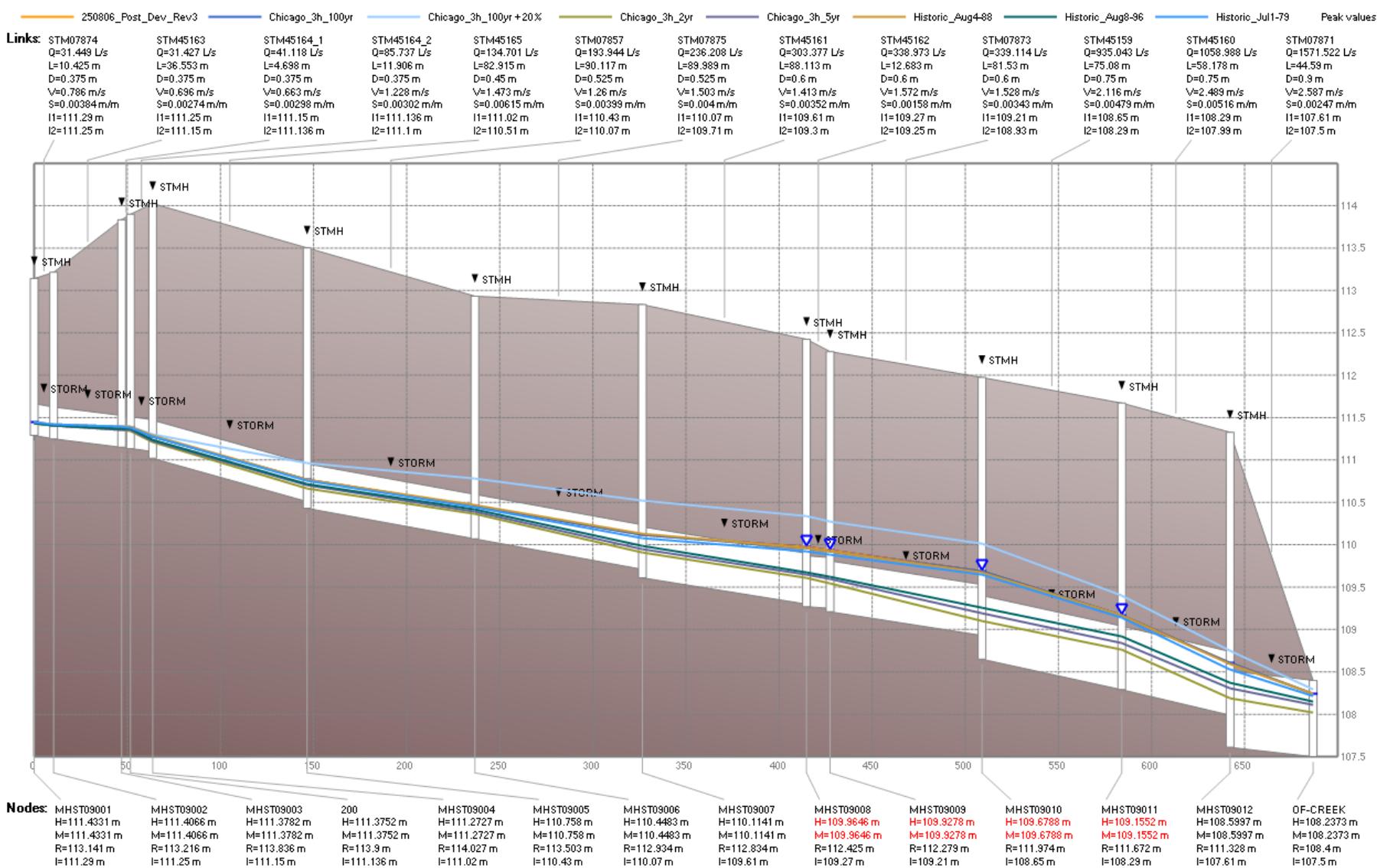


Figure 13: Node MHST09001 to Node OF-CREEK (Victor St)

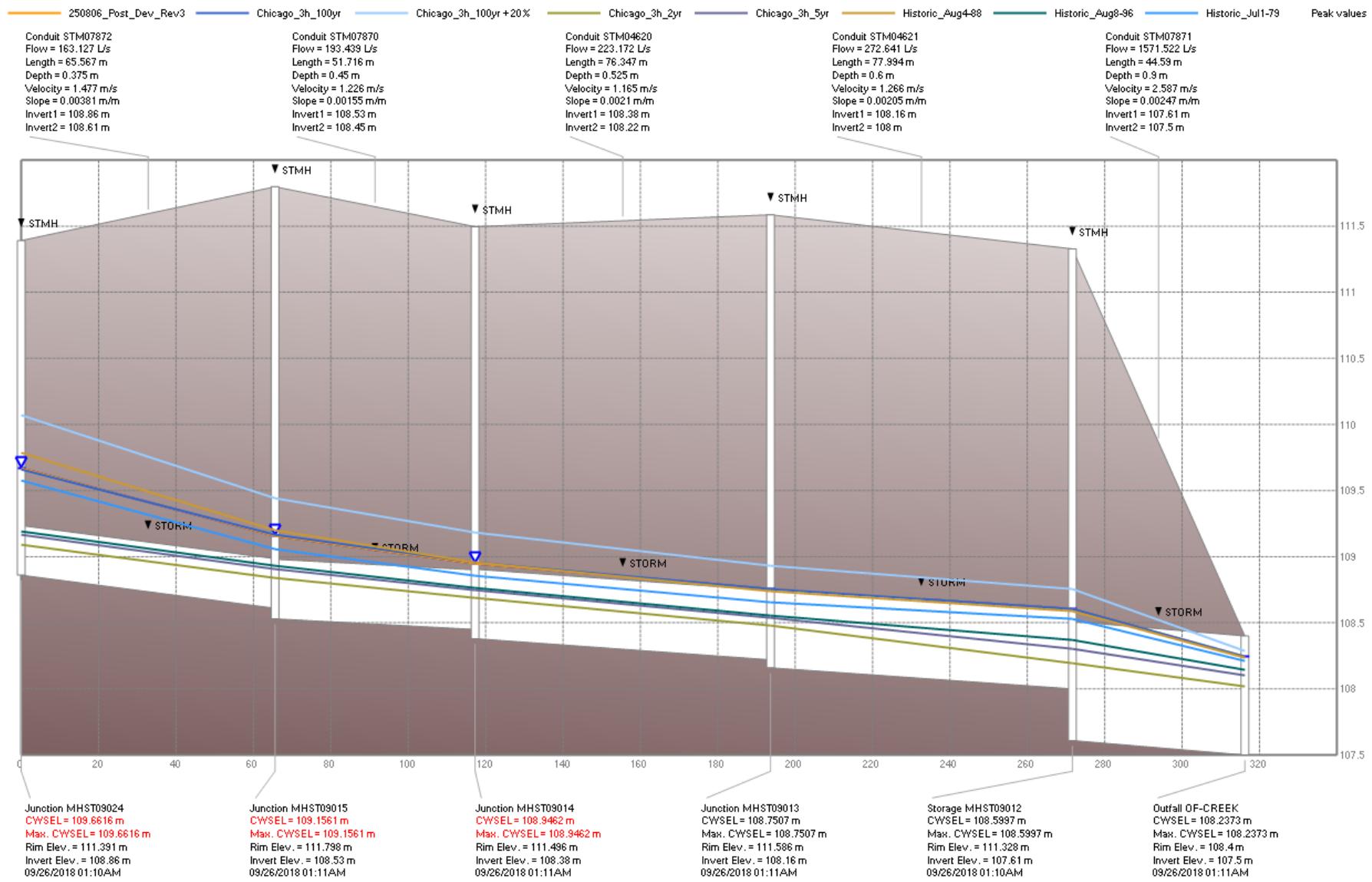


Figure 14: Node MHST09024 to Node OF-CREEK (Savage Dr)

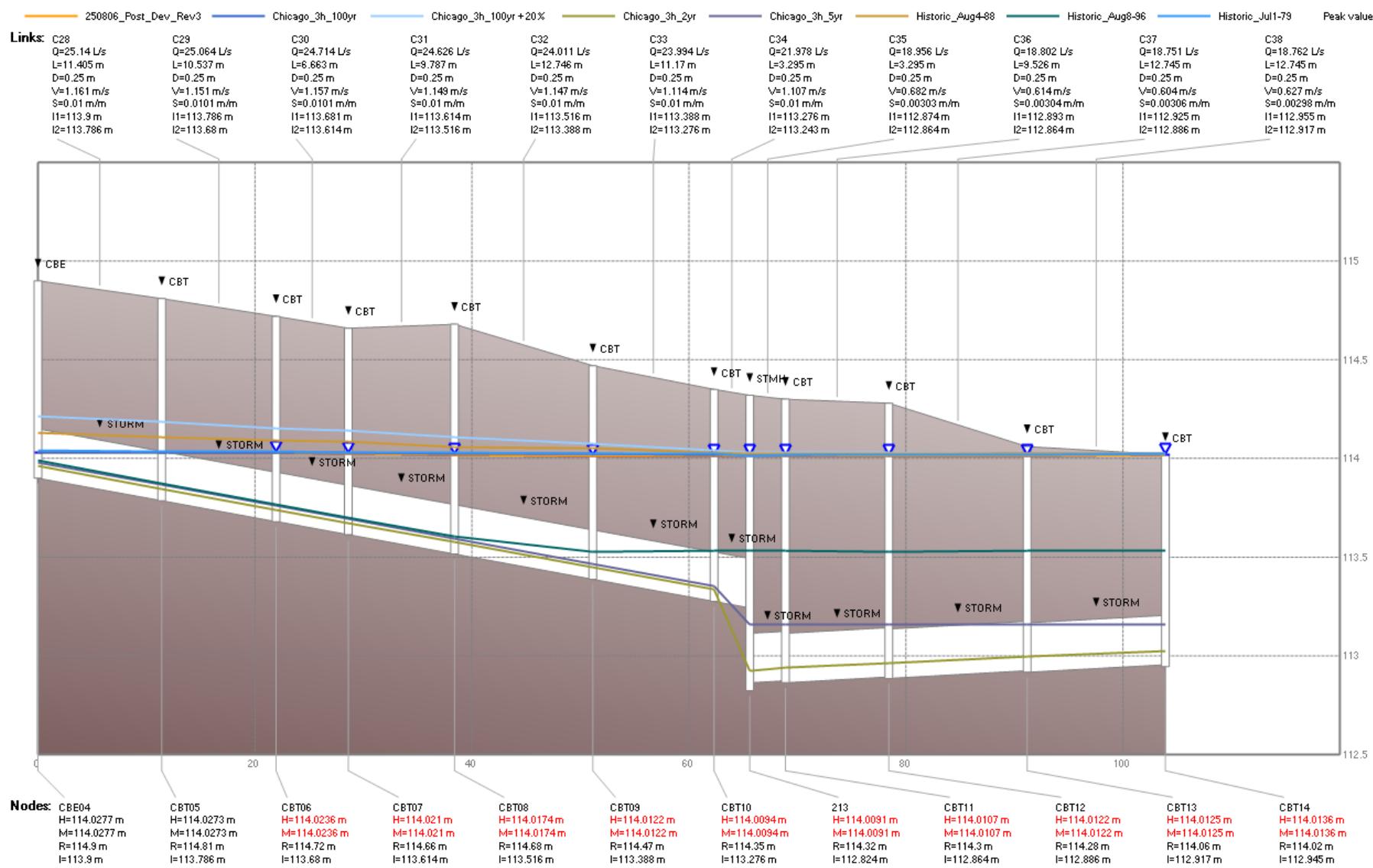


Figure 15: Node CBE04 to Node CBE15 (Perforated Pipes Along Hazeldean)

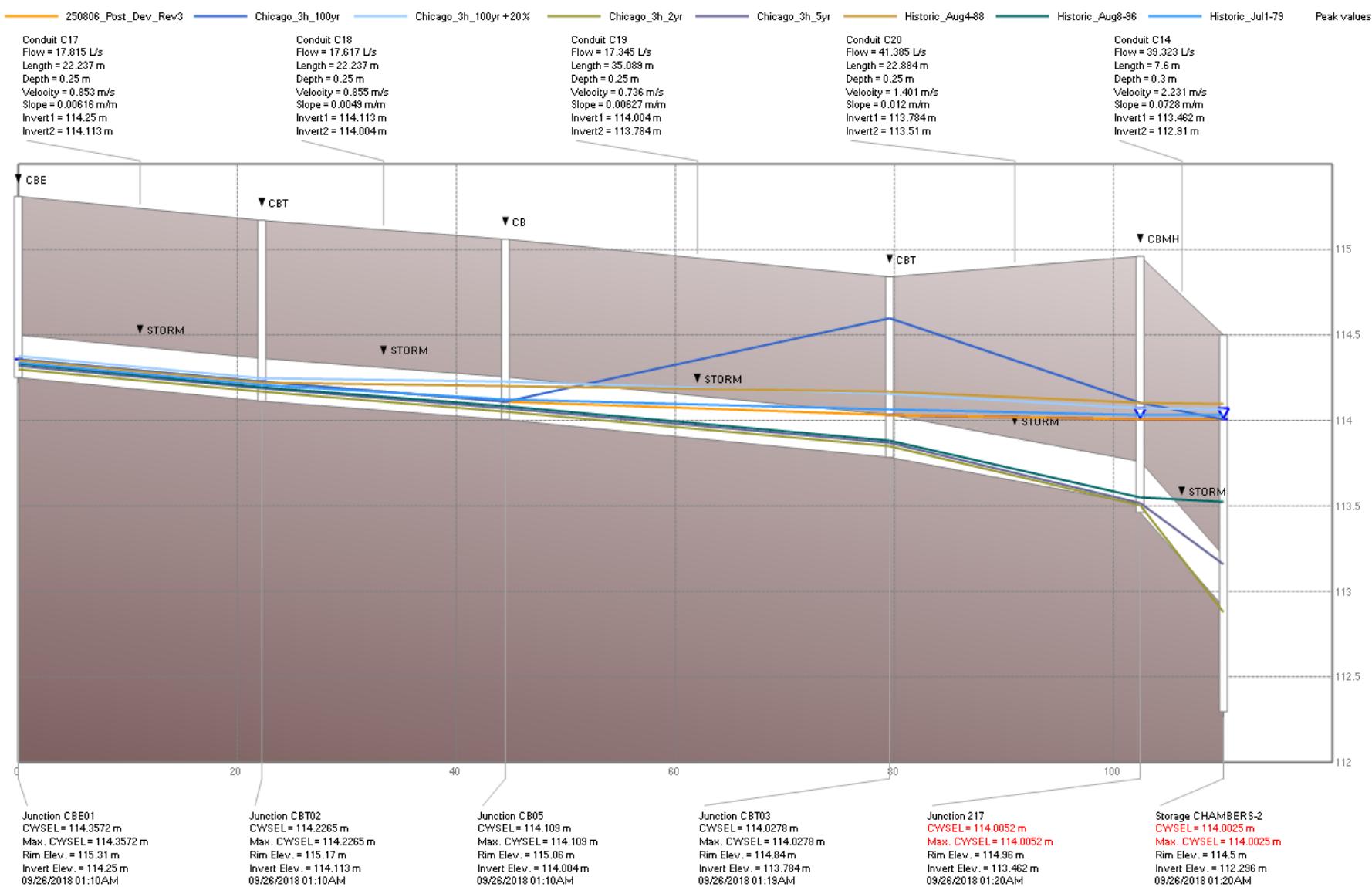


Figure 16: Node CBE01 to Node CHAMBERS-2 (Rear Perf Pipes)

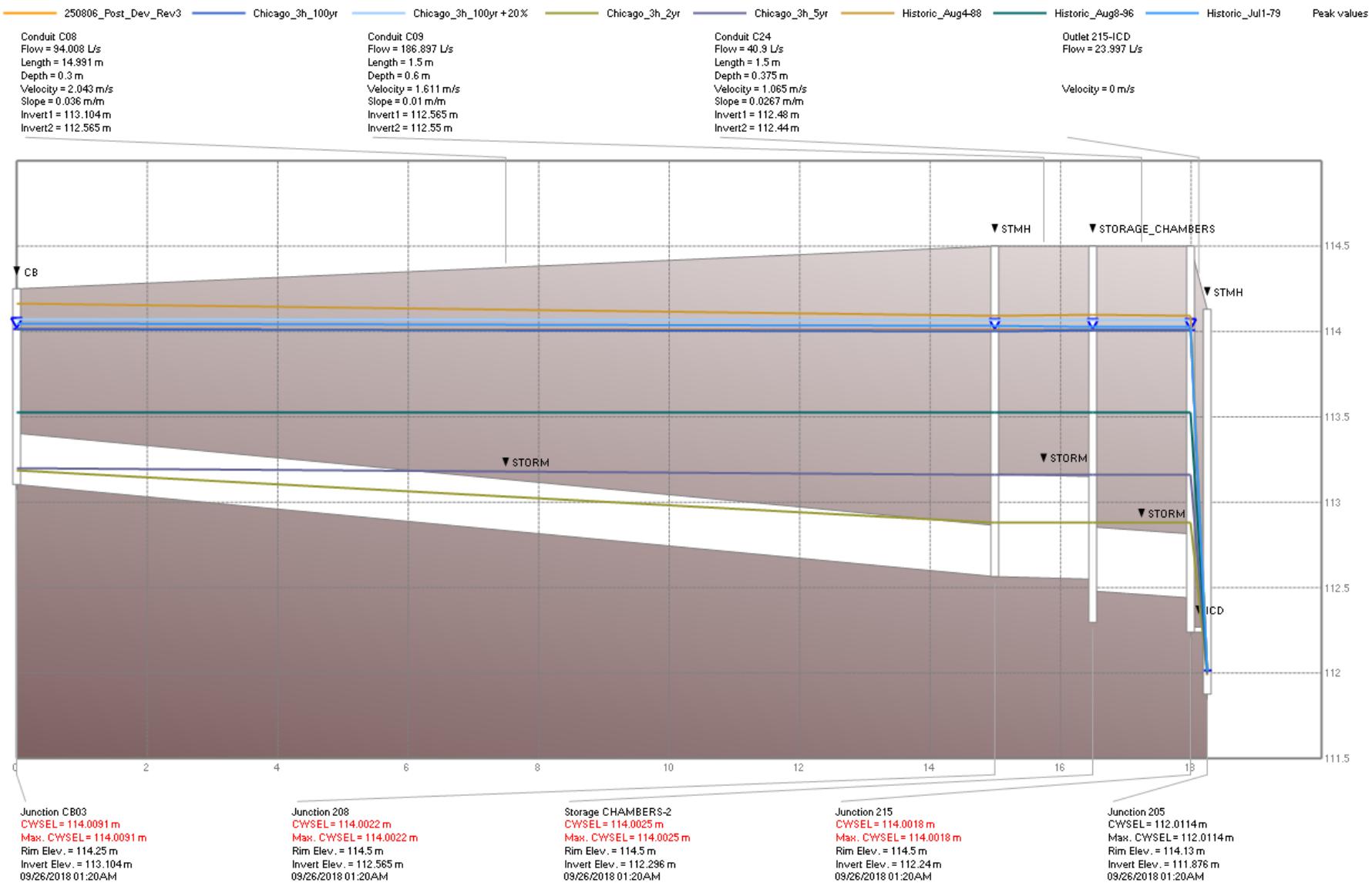


Figure 17: Node CB03 to Node 205 (Through West Chambers 1)

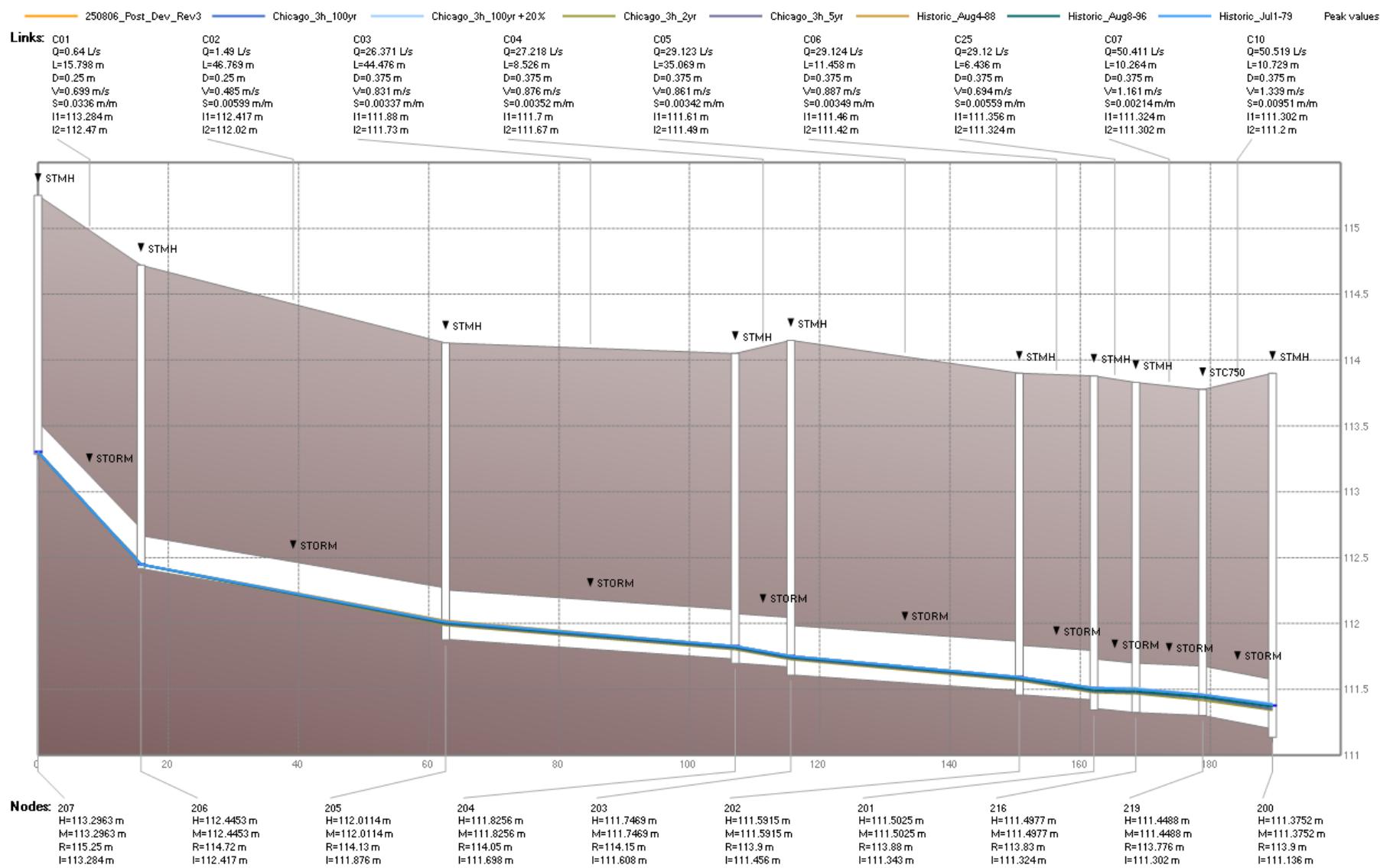


Figure 18: Node 207 to Node 200 (Onsite Storm)

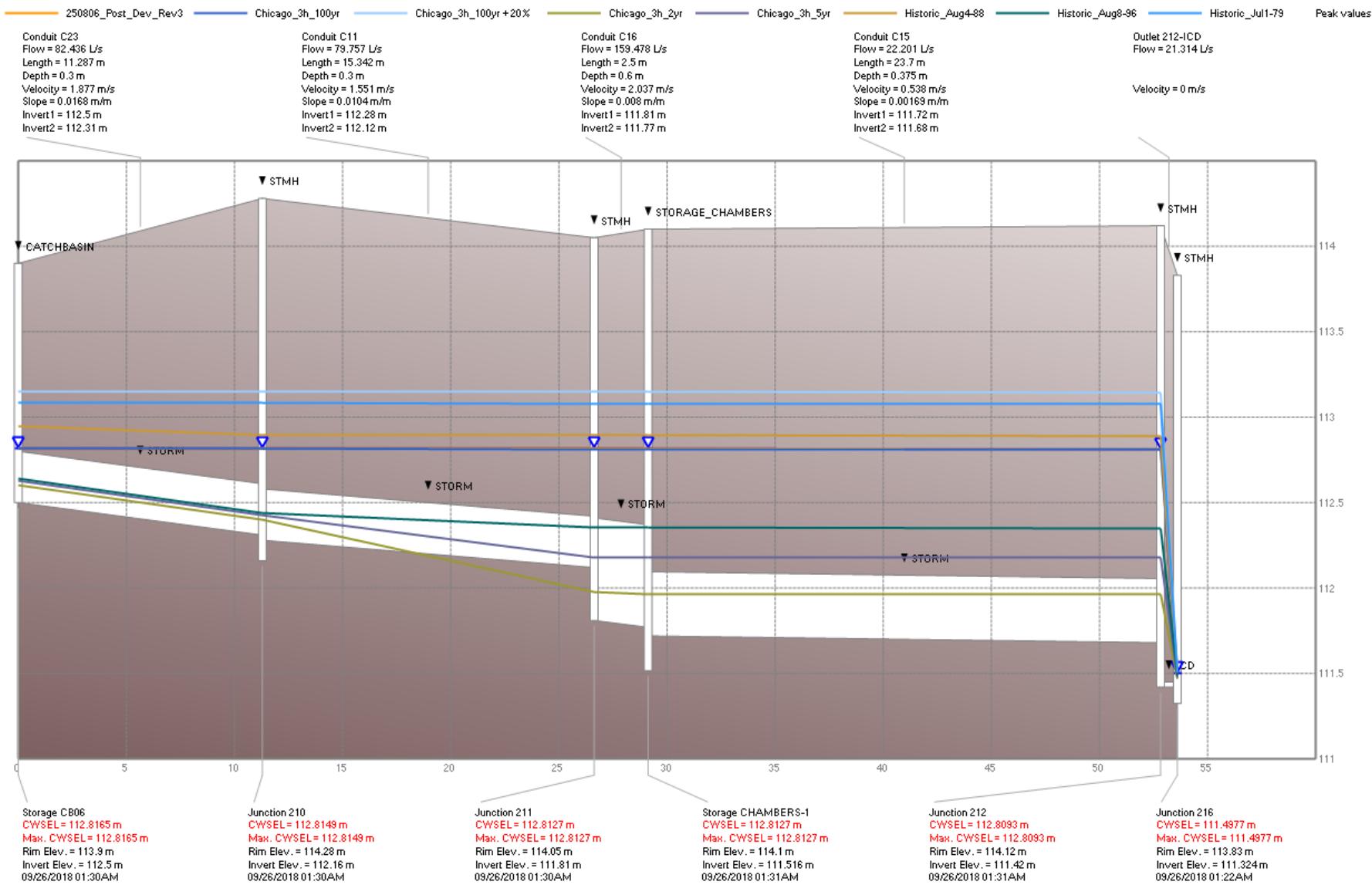


Figure 19: Node CB06 to Node 216 (Through East Chambers 1)

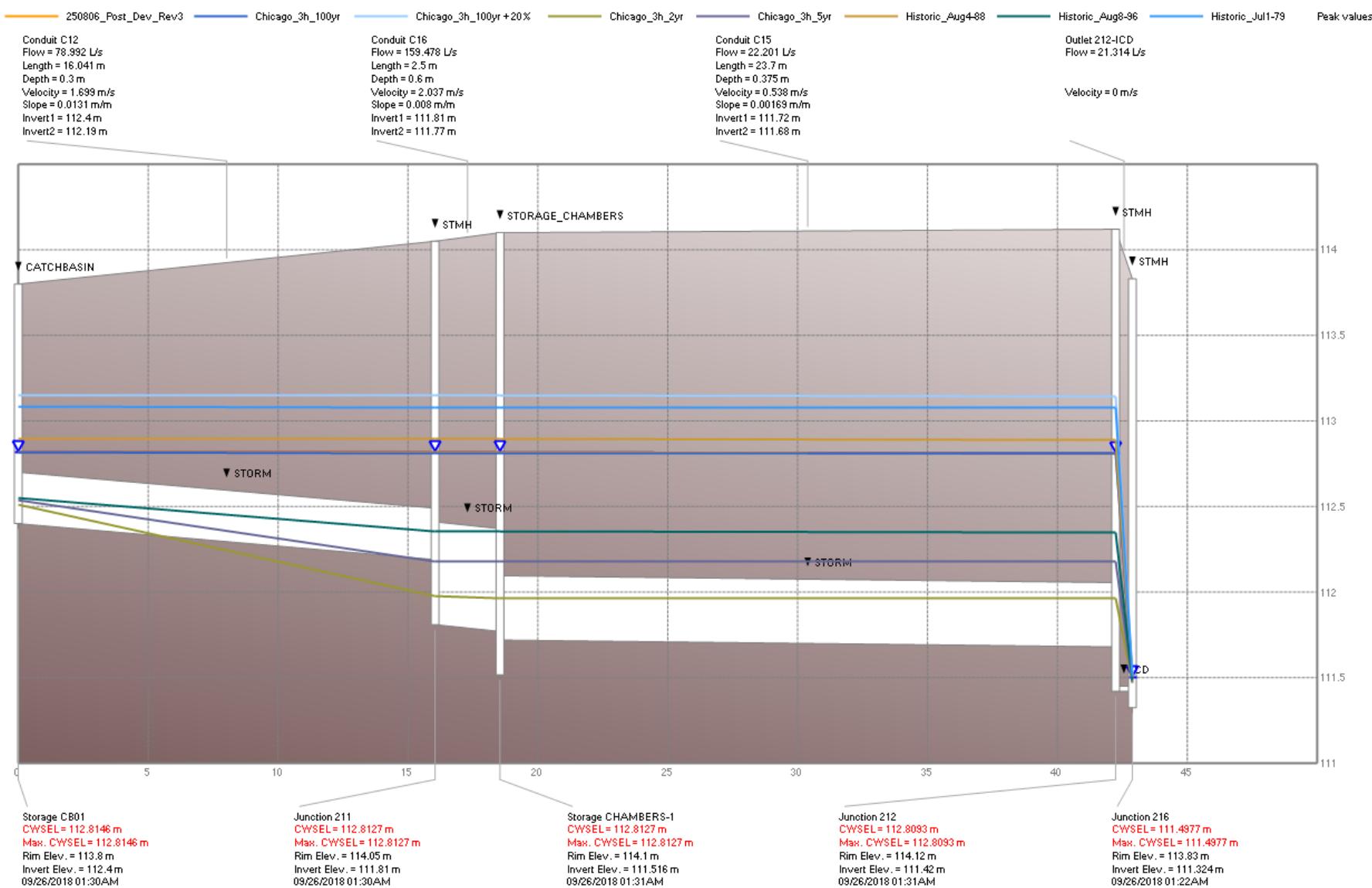


Figure 20: Node CB01 to Node 216 (Through East Chambers 2)

Table 1: OUTFALL - SUMMARY

Name	Inflows	Invert Elev. (m)	Rim Elev. (m)	Type	Max. Total Inflow (L/s)	Total inflow (ML)	Contributing Area (ha)	Contributing Imp. Area (ha)	Max. Unit Flow (L/s/ha)
OF-CREEK	NO	107.5	107.5	FREE	1577.82	4.58	12.044	5.025	131.008
OF-HAZELDEAN	NO	112.83	113.13	FREE	148.26	0.101	0.454	0.299	326.708

Table 2: JUNCTIONS - SUMMARY

Name	Tag	Invert Elev. (m)	Rim Elev. (m)	Max. HGL (m)
200	STMH	111.136	113.9	111.38
201	STMH	111.343	113.88	111.5
202	STMH	111.456	113.9	111.59
203	STMH	111.608	114.15	111.75
204	STMH	111.698	114.05	111.83
205	STMH	111.876	114.13	112.01
206	STMH	112.417	114.72	112.45
207	STMH	113.284	115.25	113.3
208	STMH	112.565	114.5	114.08
210	STMH	112.16	114.28	112.81
211	STMH	111.81	114.05	112.81
212	STMH	111.42	114.12	112.81
213	STMH	112.824	114.32	114.02
215	STMH	112.24	114.5	114.08
216	STMH	111.324	113.83	111.5
217	CBMH	113.462	114.96	114.14
218	CBMH	112.736	114	114
219	STC750	111.302	113.776	111.45
CB03	CB	113.104	114.25	114.09
CB05	CB	114.004	115.06	114.11
CBE01	CBE	114.25	115.31	114.36
CBE04	CBE	113.9	114.9	114.03
CBT02	CBT	114.113	115.17	114.23
CBT03	CBT	113.784	114.84	114.57
CBT05	CBT	113.786	114.81	114.03
CBT06	CBT	113.68	114.72	114.11
CBT07	CBT	113.614	114.66	114.08
CBT08	CBT	113.516	114.68	114.05
CBT09	CBT	113.388	114.47	114.03

Table 2: JUNCTIONS - SUMMARY (continued...)

Name	Tag	Invert Elev. (m)	Rim Elev. (m)	Max. HGL (m)
CBT10	CBT	113.276	114.35	114.02
CBT11	CBT	112.864	114.3	114.02
CBT12	CBT	112.886	114.28	114.02
CBT13	CBT	112.917	114.06	114.06
CBT14	CBT	112.945	114.02	114.02
IN07998	RYCB	110.43	111.832	111.71
IN09003-MAJ	MAJOR	113.93	114.08	113.96
IN09004-MAJ	MAJOR	113.83	113.98	113.87
IN09005-MAJ	MAJOR	113.22	113.37	113.31
IN09006-MAJ	MAJOR	113.22	113.37	113.31
IN09009-MAJ	MAJOR	112.75	112.9	112.85
IN09010-MAJ	MAJOR	112.75	112.9	112.82
IN09011-MAJ	MAJOR	112.21	112.36	112.32
IN09012-MAJ	MAJOR	112.21	112.36	112.31
IN09013-MAJ	MAJOR	111.78	111.93	111.89
IN09014-MAJ	MAJOR	111.41	111.56	111.48
IN09015-MAJ	MAJOR	111.41	111.56	111.52
IN09017-MAJ	MAJOR	111.56	111.71	111.6
IN09018-MAJ	MAJOR	111.56	111.71	111.6
IN09019-MAJ	MAJOR	111.33	111.48	111.41
IN09020-MAJ	MAJOR	111.33	111.48	111.39
IN09021-MAJ	MAJOR	111	111.15	111.2
IN09022-MAJ	MAJOR	113.94	114.09	113.99
IN09023-MAJ	MAJOR	113.75	113.9	113.79
IN09024-MAJ	MAJOR	113.15	113.3	113.22
IN09025-MAJ	MAJOR	113.13	113.28	113.21
IN09026-MAJ	MAJOR	112.66	112.81	112.75
IN09027-MAJ	MAJOR	112.68	112.83	112.77
IN09028-MAJ	MAJOR	112.36	112.51	112.43
IN09029-MAJ	MAJOR	112.37	112.52	112.46
IN09030-MAJ	MAJOR	111.97	112.12	112.04
IN09031-MAJ	MAJOR	111.97	112.12	112.04
IN09032-MAJ	MAJOR	111.62	111.77	111.82
IN09033-MAJ	MAJOR	111.62	111.77	111.73
IN09034-MAJ	MAJOR	111.27	111.42	111.41
IN09035-MAJ	MAJOR	111.27	111.42	111.4
IN45566	RYCB	109.82	111.215	111.09

Table 2: JUNCTIONS - SUMMARY (continued...)

Name	Tag	Invert Elev. (m)	Rim Elev. (m)	Max. HGL (m)
IN45569	RYCB	111.61	113.007	113.01
IN45570	RYCB	111.7	113.104	113.1
IN45572	RYCB	111.51	112.912	112.91
IN45573	RYCB	112.76	114.156	114.16
IN45574	RYCB	111.3	111.6	111.6
IN45575	RYCB	112.17	113.572	113.57
IN45577	RYCB	111.28	112.682	112.68
IN45587	RYCB	112.44	113.845	113.36
IN45588	RYCB	112.52	113.922	112.66
IN45589	RYCB	111.85	113.246	112.02
IN45590	RYCB	111.58	112.982	111.71
J1	MAJOR	111.77	111.92	111.82
J2	MAJOR	111.2	111.35	111.4
MHST09001	STMH	111.29	113.141	111.43
MHST09002	STMH	111.25	113.216	111.41
MHST09003	STMH	111.15	113.836	111.38
MHST09004	STMH	111.02	114.027	111.27
MHST09005	STMH	110.43	113.503	110.76
MHST09006	STMH	110.07	112.934	110.45
MHST09007	STMH	109.61	112.834	110.11
MHST09008	STMH	109.27	112.425	110.28
MHST09009	STMH	109.21	112.279	110.22
MHST09010	STMH	108.65	111.974	109.83
MHST09011	STMH	108.29	111.672	109.16
MHST09013	STMH	108.16	111.586	108.75
MHST09014	STMH	108.38	111.496	109.09
MHST09015	STMH	108.53	111.798	109.26
MHST09016	STMH	110.98	114.182	111.35
MHST09017	STMH	110.75	114.098	111.37
MHST09018	STMH	110.66	113.871	111.31
MHST09019	STMH	110.38	113.279	111.17
MHST09020	STMH	109.94	112.931	110.88
MHST09021	STMH	109.05	112.531	110.61
MHST09022	STMH	108.93	112.266	110.42
MHST09023	STMH	108.79	111.804	110.18
MHST09024	STMH	108.86	111.391	109.68

Table 3: STORAGES - SUMMARY

Name	Invert Elev. (m)	Rim Elev. (m)	Depth (m)	Storage Curve	Curve Name	Max. Depth (m)	Max. HGL (m)	Max. Total Inflow (L/s)	Max. Outflow (L/s)	CONDITON
CB01	112.4	113.8	1.4	TABULAR	CB01-STOR	0.41	112.81	79.88	80.43	PONDING
CB06	112.5	113.9	1.4	TABULAR	CB06-STOR	0.32	112.82	82.83	84.12	PONDING
CHAMBERS-1	111.516	114.1	2.584	TABULAR	STORAGE-1	1.3	112.81	159.67	27.48	UG STORAGE
CHAMBERS-2	112.296	114.5	2.204	TABULAR	STORAGE-2	1.78	114.08	227.73	93.81	UG STORAGE
IN09003	112.53	113.93	1.4	FUNCTIONAL		*	0.35	112.88	10.92	10.52
IN09004	112.43	113.98	1.55	TABULAR	IN09004-STOR	0.54	112.97	13.22	12.96	PONDING
IN09005	111.82	113.22	1.4	FUNCTIONAL		*	1.4	113.22	49.44	21.4
IN09006	111.82	113.22	1.4	FUNCTIONAL		*	1.4	113.22	50.88	21.4
IN09007	111.58	113.13	1.55	TABULAR	IN09007-STOR	1.55	113.13	106.09	22.51	PONDING
IN09008	111.58	113.13	1.55	TABULAR	IN09008-STOR	1.51	113.09	151.31	138.69	PONDING
IN09009	111.35	112.75	1.4	FUNCTIONAL		*	1.4	112.75	54.7	21.4
IN09010	111.35	112.75	1.4	FUNCTIONAL	IN09007-STOR	0.04	111.39	24.64	1.6	FLOW-BY
IN09011	110.81	112.21	1.4	FUNCTIONAL		*	1.4	112.21	55	20.92
IN09012	110.81	112.21	1.4	FUNCTIONAL		*	1.4	112.21	54.05	21.4
IN09013	110.38	111.78	1.4	FUNCTIONAL		*	1.4	111.78	55	21.4
IN09014	110.01	111.41	1.4	FUNCTIONAL		*	1.4	111.41	29.08	21.4
IN09015	110.01	111.41	1.4	FUNCTIONAL		*	1.4	111.41	55	21.4
IN09016	109.85	111.4	1.55	TABULAR	IN09016-STOR	1.55	111.4	154.75	22.51	PONDING
IN09017	110.16	111.56	1.4	FUNCTIONAL		*	0.5	110.66	12.84	12.7
IN09018	110.16	111.56	1.4	FUNCTIONAL		*	0.49	110.65	12.72	12.58
IN09019	109.93	111.33	1.4	FUNCTIONAL			1.4	111.33	40.81	21.4
IN09020	109.93	111.33	1.4	FUNCTIONAL			0.9	110.83	18.91	17.14
IN09021	109.6	111	1.4	FUNCTIONAL			1.4	111	55	30.37
IN09022	112.54	113.94	1.4	FUNCTIONAL		*	0.61	113.15	14.32	14.1
IN09023	112.35	113.75	1.4	FUNCTIONAL		*	0.48	112.83	12.72	12.46
IN09024	111.75	113.15	1.4	FUNCTIONAL		*	1.4	113.15	26.78	21.4
IN09025	111.73	113.13	1.4	FUNCTIONAL		*	1.4	113.13	32.56	21.4
IN09026	111.26	112.66	1.4	FUNCTIONAL		*	1.4	112.66	49.26	21.4
IN09027	111.28	112.68	1.4	FUNCTIONAL		*	1.4	112.68	48.3	21.4
IN09028	110.96	112.36	1.4	FUNCTIONAL		*	1.4	112.36	30.8	21.4
IN09029	110.97	112.37	1.4	FUNCTIONAL		*	1.4	112.37	52.03	21.4
IN09030	110.57	111.97	1.4	FUNCTIONAL		*	1.4	111.97	30.79	21.4
IN09031	110.57	111.97	1.4	FUNCTIONAL		*	1.21	111.78	21.63	19.88
IN09032	110.22	111.62	1.4	FUNCTIONAL		*	1.4	111.62	55	21.4
IN09033	110.22	111.62	1.4	FUNCTIONAL		*	1.4	111.62	55	21.4
IN09034	109.87	111.27	1.4	FUNCTIONAL			1.4	111.27	55	30.37
IN09035	109.87	111.27	1.4	FUNCTIONAL			1.4	111.27	55	30.37

Table 3: STORAGES - SUMMARY (continued...)

Name	Invert Elev. (m)	Rim Elev. (m)	Depth (m)	Storage Curve	Curve Name	Max. Depth (m)	Max. HGL (m)	Max. Total Inflow (L/s)	Max. Outflow (L/s)	CONDITON
IN103407	111.64	113.25	1.61	TABULAR	IN103407-STOR	1.51	113.15	183.35	179.74	PONDING
MHST09012	107.61	111.128	3.518	FUNCTIONAL	*	0.99	108.6	1575.67	1577.82	PONDING

Table 4A: CONDUITS - SUMMARY

Name	Inlet Node	Outlet Node	Tag	Length (m)	Roughness	Inlet Elev. (m)	Outlet Elev. (m)	Cross-Section
C01	207	206	STORM	15.798	0.013	113	112.47	CIRCULAR
C02	206	205	STORM	46.769	0.013	112.3	112.02	CIRCULAR
C03	205	204	STORM	44.476	0.013	111.88	111.73	CIRCULAR
C04	204	203	STORM	8.526	0.013	111.7	111.67	CIRCULAR
C05	203	202	STORM	35.069	0.013	111.61	111.49	CIRCULAR
C06	202	201	STORM	11.458	0.013	111.46	111.42	CIRCULAR
C07	216	219	STORM	10.264	0.013	111.324	111.302	CIRCULAR
C08	CB03	208	STORM	14.991	0.01	113.104	112.565	CIRCULAR
C09	208	CHAMBERS-2	STORM	1.5	0.013	112.565	112.55	CIRCULAR
C1	IN45587	MHST09004	RYCB_LEAD	40	0.013	112.44	112.04	CIRCULAR
C10	219	200	STORM	10.729	0.013	111.302	111.2	CIRCULAR
C11	210	211	STORM	15.342	0.013	112.28	112.12	CIRCULAR
C12	CB01	211	STORM	16.041	0.013	112.4	112.19	CIRCULAR
C13	IN07998	MHST09011	RYCB_LEAD	10	0.013	110.43	110.33	CIRCULAR
C14	217	CHAMBERS-2	STORM	7.6	0.013	113.462	112.91	CIRCULAR
C15	CHAMBERS-1	212	STORM	23.7	0.013	111.72	111.68	CIRCULAR
C16	211	CHAMBERS-1	STORM	2.5	0.013	111.79	111.77	CIRCULAR
C17	CBE01	CBT02	STORM	22.237	0.013	114.25	114.113	CIRCULAR
C18	CBT02	CB05	STORM	22.237	0.013	114.113	114.004	CIRCULAR
C19	CB05	CBT03	STORM	35.089	0.013	114.004	113.784	CIRCULAR
C2	IN45588	MHST09005	RYCB_LEAD	116.338	0.013	112.52	112.02	CIRCULAR
C20	CBT03	217	STORM	22.884	0.013	113.784	113.51	CIRCULAR
C21	218	208	STORM	15.162	0.013	112.736	112.595	CIRCULAR
C22	IN45573	MHST09016	RYCB_LEAD	40	0.013	112.76	112.26	CIRCULAR
C23	CB06	210	STORM	11.287	0.013	112.5	112.31	CIRCULAR
C24	CHAMBERS-2	215	STORM	1.5	0.013	112.48	112.44	CIRCULAR
C25	201	216	STORM	6.436	0.013	111.356	111.32	CIRCULAR
C26	IN45574	MHST09017	RYCB_LEAD	40	0.013	111.3	111	CIRCULAR
C27	IN45566	MHST09024	RYCB_LEAD	10	0.013	109.82	109.72	CIRCULAR

Table 4A: CONDUITS - SUMMARY (continued...)

Name	Inlet Node	Outlet Node	Tag	Length (m)	Roughness	Inlet Elev. (m)	Outlet Elev. (m)	Cross-Section
C28	CBE04	CBT05	STORM	11.405	0.013	113.9	113.786	CIRCULAR
C29	CBT05	CBT06	STORM	10.537	0.013	113.786	113.68	CIRCULAR
C3	IN45589	MHST09007	RYCB_LEAD	40	0.013	111.85	111.45	CIRCULAR
C30	CBT06	CBT07	STORM	6.663	0.013	113.681	113.614	CIRCULAR
C31	CBT07	CBT08	STORM	9.787	0.013	113.614	113.516	CIRCULAR
C32	CBT08	CBT09	STORM	12.746	0.013	113.516	113.388	CIRCULAR
C33	CBT09	CBT10	STORM	11.17	0.013	113.388	113.276	CIRCULAR
C34	CBT10	213	STORM	3.295	0.013	113.276	113.243	CIRCULAR
C35	CBT11	213	STORM	3.295	0.013	112.874	112.864	CIRCULAR
C36	CBT12	CBT11	STORM	9.526	0.013	112.893	112.864	CIRCULAR
C37	CBT13	CBT12	STORM	12.745	0.013	112.925	112.886	CIRCULAR
C38	CBT14	CBT13	STORM	12.745	0.013	112.955	112.917	CIRCULAR
C39	IN103407	OF-HAZELDEAN	MAJOR	40.346	0.013	113.04	112.83	TRAPEZOIDAL
C4	IN45590	MHST09007	RYCB_LEAD	40	0.013	111.58	111.08	CIRCULAR
C40	213	218	STORM	29.265	0.013	112.824	112.736	CIRCULAR
C5	IN45575	MHST09019	RYCB_LEAD	40	0.013	112.17	111.77	CIRCULAR
C6	IN45570	MHST09020	RYCB_LEAD	40	0.013	111.7	111.3	CIRCULAR
C7	IN45569	MHST09021	RYCB_LEAD	40	0.013	111.61	111.41	CIRCULAR
C8	IN45572	MHST09021	RYCB_LEAD	40	0.013	111.51	111.11	CIRCULAR
C9	IN45577	MHST09022	RYCB_LEAD	40	0.013	111.28	110.88	CIRCULAR
C98	CHAMBERS-1	212	SUBDRAIN	26.513	0.013	111.516	111.42	CIRCULAR
C99	CHAMBERS-2	215	SUBDRAIN	28.637	0.013	112.296	112.27	CIRCULAR
OF1	IN09016	MHST09012	OVERFLOW-ROAD	17.899	0.013	111.4	111.128	IRREGULAR
R01	IN09004-MAJ	IN09006-MAJ	MAJOR	92.678	0.013	113.83	113.22	IRREGULAR
R02	IN09006-MAJ	IN09007	MAJOR	79.588	0.013	113.22	113.13	IRREGULAR
R03	IN09005-MAJ	IN09008	MAJOR	79.205	0.013	113.22	112.98	IRREGULAR
R04	IN09007	IN09010-MAJ	MAJOR	71.554	0.013	113.13	112.75	IRREGULAR
R05	IN09008	IN09009-MAJ	MAJOR	72.205	0.013	112.98	112.75	IRREGULAR
R06	IN09010-MAJ	IN09012-MAJ	MAJOR	101.975	0.013	112.75	112.21	IRREGULAR
R07	IN09009-MAJ	IN09011-MAJ	MAJOR	106.231	0.013	112.75	112.21	IRREGULAR
R08	IN09012-MAJ	J1	MAJOR	98.186	0.013	112.21	111.77	IRREGULAR
R09	IN09033-MAJ	J1	MAJOR	13.729	0.013	111.62	111.77	IRREGULAR
R10	IN09032-MAJ	J1	MAJOR	24.181	0.013	0	111.62	IRREGULAR
R11	IN09011-MAJ	IN09013-MAJ	MAJOR	91.997	0.013	112.21	111.78	IRREGULAR
R12	IN09013-MAJ	IN09015-MAJ	MAJOR	71.755	0.013	111.78	111.41	IRREGULAR
R13	IN09015-MAJ	MHST09012	MAJOR	64.056	0.013	111.41	111.128	IRREGULAR
R14	IN09014-MAJ	IN09016	MAJOR	54.483	0.013	111.41	111.25	IRREGULAR

Table 4A: CONDUITS - SUMMARY (continued...)

Name	Inlet Node	Outlet Node	Tag	Length (m)	Roughness	Inlet Elev. (m)	Outlet Elev. (m)	Cross-Section
R15	J1	IN09014-MAJ	MAJOR	59.615	0.013	111.77	111.41	IRREGULAR
R16	IN09035-MAJ	J2	MAJOR	17.745	0.013	0	0	IRREGULAR
R17	IN09034-MAJ	J2	MAJOR	26.122	0.013	0	0	IRREGULAR
R18	IN09021-MAJ	IN09020-MAJ	MAJOR	30.532	0.013	0	0	IRREGULAR
R19	J2	IN09019-MAJ	MAJOR	27.476	0.013	0	0	IRREGULAR
R20	IN09020-MAJ	IN09018-MAJ	MAJOR	80.609	0.013	0	111.56	IRREGULAR
R21	IN09019-MAJ	IN09017-MAJ	MAJOR	81.078	0.013	0	111.56	IRREGULAR
R22	IN09018-MAJ	MHST09012	MAJOR	83.592	0.013	111.56	111.128	IRREGULAR
R23	IN09017-MAJ	IN09016	MAJOR	67.772	0.013	111.56	111.25	IRREGULAR
R24	IN09003-MAJ	IN103407	MAJOR	71.254	0.013	113.93	113.04	IRREGULAR
R25	IN09023-MAJ	IN09024-MAJ	MAJOR	81.428	0.013	113.75	113.15	IRREGULAR
R26	IN09022-MAJ	IN09025-MAJ	MAJOR	86.482	0.013	113.94	113.13	IRREGULAR
R27	IN09025-MAJ	IN09027-MAJ	MAJOR	86.008	0.013	113.13	112.68	IRREGULAR
R28	IN09024-MAJ	IN09026-MAJ	MAJOR	85.805	0.013	113.15	112.66	IRREGULAR
R29	IN09027-MAJ	IN09028-MAJ	MAJOR	61.833	0.013	112.68	112.36	IRREGULAR
R30	IN09026-MAJ	IN09029-MAJ	MAJOR	68.091	0.013	112.66	112.37	IRREGULAR
R31	IN09029-MAJ	IN09030-MAJ	MAJOR	72.254	0.013	112.37	111.97	IRREGULAR
R32	IN09028-MAJ	IN09034-MAJ	MAJOR	88.109	0.013	112.36	111.27	IRREGULAR
R33	IN09030-MAJ	IN09032-MAJ	MAJOR	67.283	0.013	111.97	111.62	IRREGULAR
R34	IN09031-MAJ	IN09033-MAJ	MAJOR	69.891	0.013	111.97	111.62	IRREGULAR
STM04620	MHST09014	MHST09013	STORM	76.347	0.013	108.38	108.22	CIRCULAR
STM04621	MHST09013	MHST09012	STORM	77.994	0.013	108.16	108	CIRCULAR
STM07857	MHST09005	MHST09006	STORM	90.117	0.013	110.43	110.07	CIRCULAR
STM07870	MHST09015	MHST09014	STORM	51.716	0.013	108.53	108.45	CIRCULAR
STM07871	MHST09012	OF-CREEK	STORM	44.59	0.013	107.61	107.5	CIRCULAR
STM07872	MHST09024	MHST09015	STORM	65.567	0.013	108.86	108.61	CIRCULAR
STM07873	MHST09009	MHST09010	STORM	81.53	0.013	109.21	108.93	CIRCULAR
STM07874	MHST09001	MHST09002	STORM	10.425	0.013	111.29	111.25	CIRCULAR
STM07875	MHST09006	MHST09007	STORM	89.989	0.013	110.07	109.71	CIRCULAR
STM07876	MHST09016	MHST09017	STORM	39.458	0.013	110.98	110.83	CIRCULAR
STM45150	MHST09017	MHST09018	STORM	13.481	0.013	110.75	110.7	CIRCULAR
STM45151	MHST09018	MHST09019	STORM	52.811	0.013	110.66	110.45	CIRCULAR
STM45152	MHST09019	MHST09020	STORM	90.099	0.013	110.38	110.02	CIRCULAR
STM45153	MHST09020	MHST09021	STORM	89.396	0.013	109.94	109.13	CIRCULAR
STM45154	MHST09021	MHST09022	STORM	58.932	0.013	109.05	108.93	CIRCULAR
STM45155	MHST09022	MHST09023	STORM	56.802	0.013	108.93	108.79	CIRCULAR
STM45156	MHST09023	MHST09010	STORM	41.513	0.013	108.79	108.66	CIRCULAR

Table 4A: CONDUITS - SUMMARY (continued...)

Name	Inlet Node	Outlet Node	Tag	Length (m)	Roughness	Inlet Elev. (m)	Outlet Elev. (m)	Cross-Section
STM45159	MHST09010	MHST09011	STORM	75.08	0.013	108.65	108.29	CIRCULAR
STM45160	MHST09011	MHST09012	STORM	58.178	0.013	108.29	107.99	CIRCULAR
STM45161	MHST09007	MHST09008	STORM	88.113	0.013	109.61	109.3	CIRCULAR
STM45162	MHST09008	MHST09009	STORM	12.683	0.013	109.27	109.25	CIRCULAR
STM45163	MHST09002	MHST09003	STORM	36.553	0.013	111.25	111.15	CIRCULAR
STM45164_1	MHST09003	200	STORM	4.698	0.013	111.15	111.136	CIRCULAR
STM45164_2	200	MHST09004	STORM	11.906	0.013	111.136	111.1	CIRCULAR
STM45165	MHST09004	MHST09005	STORM	82.915	0.013	111.02	110.51	CIRCULAR

Table 4B: CONDUITS - SUMMARY

Name	Geom1 (m)	Transect	Slope (m/m)	Max. Flow (L/s)	Max. Velocity (m/s)	Max/Full Flow	Max. Spread (m)
C01	0.25		0.03357	0.64	0.7	0	0
C02	0.25		0.00599	1.49	0.48	0.03	0
C03	0.375		0.00337	26.37	0.83	0.26	0
C04	0.375		0.00352	27.22	0.88	0.26	0
C05	0.375		0.00342	29.12	0.86	0.28	0
C06	0.375		0.00349	29.12	0.89	0.28	0
C07	0.375		0.00214	50.41	1.16	0.62	0
C08	0.3		0.03598	94.08	2.04	0.39	0
C09	0.6		0.01	189.8	1.65	0.31	0
C1	0.2		0.01	42.31	1.39	1.29	0
C10	0.375		0.00951	50.52	1.34	0.3	0
C11	0.3		0.01043	81.48	1.56	0.83	0
C12	0.3		0.01309	80.43	1.7	0.73	0
C13	0.2		0.01	112.4	3.58	3.43	0
C14	0.3		0.07282	41.08	2.31	0.16	0
C15	0.375		0.00169	26.74	0.59	0.37	0
C16	0.6		0.008	159.67	2.05	0.21	0
C17	0.25		0.00616	17.84	0.85	0.38	0
C18	0.25		0.0049	17.71	0.86	0.43	0
C19	0.25		0.00627	17.54	0.74	0.37	0
C2	0.2		0.0043	16.36	0.8	0.76	0
C20	0.25		0.01197	41.6	1.41	0.64	0
C21	0.3		0.0093	93.44	1.34	1	0
C22	0.2		0.0125	47.91	1.55	1.31	0

Table 4B: CONDUITS - SUMMARY (continued...)

Name	Geom1 (m)	Transect	Slope (m/m)	Max. Flow (L/s)	Max. Velocity (m/s)	Max/Full Flow	Max. Spread (m)
C23	0.3		0.01684	84.12	1.88	0.67	0
C24	0.375		0.02668	93.81	1.24	0.33	0
C25	0.375		0.00559	29.12	0.69	0.24	0
C26	0.2		0.0075	35.68	1.17	1.26	0
C27	0.2		0.01	111.38	3.55	3.4	0
C28	0.25		0.01	25.15	1.16	0.42	0
C29	0.25		0.01006	25.07	1.15	0.42	0
C3	0.2		0.01	34.05	1.23	1.04	0
C30	0.25		0.01006	25.05	1.16	0.42	0
C31	0.25		0.01001	25.33	1.16	0.43	0
C32	0.25		0.01004	24.58	1.15	0.41	0
C33	0.25		0.01003	24.28	1.12	0.41	0
C34	0.25		0.01002	22.01	1.12	0.37	0
C35	0.25		0.00303	21.31	0.72	0.65	0
C36	0.25		0.00304	20.48	0.62	0.62	0
C37	0.25		0.00306	19.97	0.61	0.61	0
C38	0.25		0.00298	19.53	0.63	0.6	0
C39	0.3		0.00521	148.26	1.06	0.14	0
C4	0.2		0.0125	26.25	1.27	0.72	0
C40	0.3		0.00301	37.09	0.59	0.7	0
C5	0.2		0.01	54.64	1.76	1.67	0
C6	0.2		0.01	65.07	2.07	1.98	0
C7	0.2		0.005	61.3	1.95	2.64	0
C8	0.2		0.01	56.78	1.82	1.73	0
C9	0.2		0.01	47.72	1.55	1.45	0
C98	0.1		0.00362	4.62	0.59	1.49	0
C99	0.1		0.00091	4.04	0.54	2.6	0
OF1	0	Half_Street_4.25m	0.0152	0	0	0	0
R01	0	Half_Street_4.25m	0.00658	15.17	0.21	0.01	2.158
R02	0	Half_Street_4.25m	0.00113	28.7	0.32	0.07	2.419
R03	0	Half_Street_4.25m	0.00303	64.78	0.48	0.09	3.829
R04	0	Half_Street_4.25m	0.00531	0	0	0	1.112
R05	0	Half_Street_4.25m	0.00319	116.49	0.62	0.16	4.234
R06	0	Half_Street_4.25m	0.0053	45.38	0.41	0.05	2.75
R07	0	Half_Street_4.25m	0.00508	115.27	0.62	0.13	4.234
R08	1	Half_Street_4.25m	0.00448	78.66	0.89	0.09	2.419
R09	1	Half_Street_4.25m	-0.01093	30.55	0.38	0.02	2.615

Table 4B: CONDUITS - SUMMARY (continued...)

Name	Geom1 (m)	Transect	Slope (m/m)	Max. Flow (L/s)	Max. Velocity (m/s)	Max/Full Flow	Max. Spread (m)
R10	1	Half_Street_4.25m	-999	23.02	0.17	0.02	5.718
R11	1	Half_Street_4.25m	0.00467	147.91	0.7	0.17	4.639
R12	1	Half_Street_4.25m	0.00516	153.55	0.73	0.17	4.639
R13	1	Half_Street_4.25m	0.0044	142.47	0.68	0.17	4.639
R14	1	Half_Street_4.25m	0.00294	39.55	0.24	0.06	4.774
R15	1	Half_Street_4.25m	0.00604	22.71	0.4	0.02	2.027
R16	1	Half_Street_4.25m	0	38.02	0.18	0.05	7.238
R17	1	Half_Street_4.25m	0	171.1	0.3	0.26	7.378
R18	1	Half_Street_4.25m	0	52.12	0.24	0.04	6.057
R19	1	Half_Street_4.25m	0	65.77	0.21	0.08	6.335
R20	1	Half_Street_4.25m	-999	7.47	0.17	0.01	1.7
R21	1	Half_Street_4.25m	-999	8	0.13	0.01	1.962
R22	1	Half_Street_4.25m	0.00517	9.73	0.4	0.01	1.242
R23	1	Half_Street_4.25m	0.00457	10.16	0.23	0.01	3.694
R24	1	Half_Street_4.25m	0.01249	8.57	0.28	0.01	2.223
R25	1	Half_Street_4.25m	0.00737	12.06	0.24	0.01	1.831
R26	1	Half_Street_4.25m	0.00937	31.07	0.45	0.03	2.158
R27	1	Half_Street_4.25m	0.00523	59.35	0.55	0.07	2.75
R28	1	Half_Street_4.25m	0.00571	50.9	0.5	0.05	2.615
R29	1	Half_Street_4.25m	0.00518	76.14	0.72	0.08	2.615
R30	1	Half_Street_4.25m	0.00426	76.18	0.57	0.09	3.29
R31	1	Half_Street_4.25m	0.00554	90.68	0.82	0.1	2.885
R32	1	Half_Street_4.25m	0.01237	86.08	0.48	0.06	4.369
R33	1	Half_Street_4.25m	0.0052	55.79	0.29	0.06	6.265
R34	1	Half_Street_4.25m	0.00501	39.46	0.57	0.04	2.885
STM04620	0.525		0.0021	227.48	1.17	1.16	0
STM04621	0.6		0.00205	276.26	1.27	0.99	0
STM07857	0.525		0.00399	193.96	1.26	0.71	0
STM07870	0.45		0.00155	193.95	1.23	1.73	0
STM07871	0.9		0.00247	1577.82	2.6	1.75	0
STM07872	0.375		0.00381	163.59	1.48	1.51	0
STM07873	0.6		0.00343	339.46	1.53	0.94	0
STM07874	0.375		0.00384	31.45	0.79	0.29	0
STM07875	0.525		0.004	237.07	1.51	0.87	0
STM07876	0.3		0.0038	47.23	0.94	0.79	0
STM45150	0.375		0.00371	105.71	1.3	0.99	0
STM45151	0.375		0.00398	102.12	1.13	0.92	0

Table 4B: CONDUITS - SUMMARY (continued...)

Name	Geom1 (m)	Transect	Slope (m/m)	Max. Flow (L/s)	Max. Velocity (m/s)	Max/Full Flow	Max. Spread (m)
STM45152	0.45		0.004	178.64	1.36	0.99	0
STM45153	0.525		0.00906	254.87	1.29	0.62	0
STM45154	0.6		0.00204	370.37	1.31	1.34	0
STM45155	0.6		0.00246	479.38	1.7	1.57	0
STM45156	0.6		0.00313	618.76	2.19	1.8	0
STM45159	0.75		0.00479	943.85	2.14	1.22	0
STM45160	0.75		0.00516	1060.1	2.49	1.33	0
STM45161	0.6		0.00352	307.04	1.41	0.84	0
STM45162	0.6		0.00158	339.11	1.58	1.39	0
STM45163	0.375		0.00274	31.43	0.7	0.34	0
STM45164_1	0.375		0.00298	41.17	0.67	0.43	0
STM45164_2	0.375		0.00302	85.74	1.23	0.89	0
STM45165	0.45		0.00615	135.79	1.47	0.61	0

Table 5: OUTLETS - SUMMARY

Name	Inlet Node	Outlet Node	Tag	Inlet Elev. (m)	Flap Gate	Rating Curve	Coefficient (m)	Exponent (m)	Curve Name	Max. Flow (L/s)
212-ICD	212	216	ICD	111.42	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	21.32
215-ICD	215	205	ICD	112.24	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	24.51
IN09003-ICD	IN09003	MHST09003	ICD	112.53	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	10.52
IN09003-INC	IN09003-MAJ	IN09003	INC	113.93	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	10.92
IN09004-ICD	IN09004	MHST09004	ICD	112.45	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	12.96
IN09004-INC	IN09004-MAJ	IN09004	INC	113.83	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	13.22
IN09005-ICD	IN09005	MHST09005	ICD	111.82	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	21.4
IN09005-INC	IN09005-MAJ	IN09005	INC	113.22	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	49.44
IN09006-ICD	IN09006	MHST09005	ICD	111.82	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	21.4
IN09006-INC	IN09006-MAJ	IN09006	INC	113.22	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	50.88
IN09007-ICD	IN09007	MHST09006	ICD	111.58	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	22.51
IN09008-ICD	IN09008	MHST09006	ICD	111.58	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	22.21
IN09009-ICD	IN09009	MHST09007	ICD	111.35	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	21.4
IN09009-INC	IN09009-MAJ	IN09009	INC	112.72	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	54.7
IN09010-ICD	IN09010	MHST09007	ICD	111.32	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	1.6
IN09010-INC	IN09010-MAJ	IN09010	INC	112.75	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	24.64
IN09011-ICD	IN09011	MHST09008	ICD	110.87	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	20.92
IN09011-INC	IN09011-MAJ	IN09011	INC	112.21	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	55
IN09012-ICD	IN09012	MHST09008	ICD	110.81	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	21.4
IN09012-INC	IN09012-MAJ	IN09012	INC	112.21	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	54.05
IN09013-ICD	IN09013	MHST09010	ICD	110.38	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	21.4
IN09013-INC	IN09013-MAJ	IN09013	INC	111.78	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	55
IN09014-ICD	IN09014	MHST09011	ICD	110.01	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	21.4
IN09014-INC	IN09014-MAJ	IN09014	INC	111.41	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	29.08
IN09015-ICD	IN09015	MHST09011	ICD	110.01	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	21.4
IN09015-INC	IN09015-MAJ	IN09015	INC	56.848	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	55
IN09016-ICD	IN09016	MHST09013	ICD	109.85	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	22.51

Table 5: OUTLETS - SUMMARY (continued...)

Name	Inlet Node	Outlet Node	Tag	Inlet Elev. (m)	Flap Gate	Rating Curve	Coefficient (m)	Exponent (m)	Curve Name	Max. Flow (L/s)
IN09017-ICD	IN09017	MHST09013	ICD	110.16	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	12.7
IN09017-INC	IN09017-MAJ	IN09017	INC	111.56	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	12.84
IN09018-ICD	IN09018	MHST09013	ICD	110.16	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	12.58
IN09018-INC	IN09018-MAJ	IN09018	INC	111.56	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	12.72
IN09019-ICD	IN09019	MHST09014	ICD	109.93	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	21.4
IN09019-INC	IN09019-MAJ	IN09019	INC	111.33	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	40.81
IN09020-ICD	IN09020	MHST09014	ICD	109.93	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	17.14
IN09020-INC	IN09020-MAJ	IN09020	INC	111.33	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	18.91
IN09021-ICD	IN09021	MHST09015	ICD	109.6	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEB	30.37
IN09021-INC	IN09021-MAJ	IN09021	INC	111	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	55
IN09022-ICD	IN09022	MHST09017	ICD	112.54	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	14.1
IN09022-INC	IN09022-MAJ	IN09022	INC	113.94	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	14.32
IN09023-ICD	IN09023	MHST09017	ICD	112.35	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	12.46
IN09023-INC	IN09023-MAJ	IN09023	INC	113.75	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	12.72
IN09024-ICD	IN09024	MHST09019	ICD	111.75	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	21.4
IN09024-INC	IN09024-MAJ	IN09024	INC	113.15	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	26.78
IN09025-ICD	IN09025	MHST09019	ICD	111.73	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	21.4
IN09025-INC	IN09025-MAJ	IN09025	INC	113.13	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	32.56
IN09026-ICD	IN09026	MHST09020	ICD	111.26	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	21.4
IN09026-INC	IN09026-MAJ	IN09026	INC	112.66	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	49.26
IN09027-ICD	IN09027	MHST09020	ICD	111.28	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	21.4
IN09027-INC	IN09027-MAJ	IN09027	INC	112.68	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	48.3
IN09028-ICD	IN09028	MHST09021	ICD	110.96	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	21.4
IN09028-INC	IN09028-MAJ	IN09028	INC	112.36	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	30.8
IN09029-ICD	IN09029	MHST09021	ICD	110.97	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	21.4
IN09029-INC	IN09029-MAJ	IN09029	INC	112.37	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	52.03
IN09030-ICD	IN09030	MHST09022	ICD	110.57	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	21.4

Table 5: OUTLETS - SUMMARY (continued...)

Name	Inlet Node	Outlet Node	Tag	Inlet Elev. (m)	Flap Gate	Rating Curve	Coefficient (m)	Exponent (m)	Curve Name	Max. Flow (L/s)
IN09030-INC	IN09030-MAJ	IN09030	INC	111.97	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	30.79
IN09031-ICD	IN09031	MHST09022	ICD	110.57	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	19.88
IN09031-INC	IN09031-MAJ	IN09031	INC	111.97	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	21.63
IN09032-ICD	IN09032	MHST09023	ICD	110.22	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	21.4
IN09032-INC	IN09032-MAJ	IN09032	INC	111.62	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	55
IN09033-ICD	IN09033	MHST09023	ICD	110.22	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEA	21.4
IN09033-INC	IN09033-MAJ	IN09033	INC	111.62	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	55
IN09034-ICD	IN09034	MHST09024	ICD	109.87	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEB	30.37
IN09034-INC	IN09034-MAJ	IN09034	INC	111.27	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	55
IN09035-ICD	IN09035	MHST09024	ICD	109.87	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEB	30.37
IN09035-INC	IN09035-MAJ	IN09035	INC	111.27	NO	TABULAR/DEPTH	10	0.5	CB-INC-1%	55
IN103407-ICD	IN103407	MHST09001	ICD	111.64	NO	TABULAR/DEPTH	10	0.5	IPEX-MHF-TYPEB	31.48

Table 6: SUBCATCHMENTS - SUMMARY

Name	Outlet	Area (ha)	Width (m)	Flow Length (m)	Slope (%)	Imperv. (%)	Peak Runoff (L/s)	CAVG
S03	CB01	0.0178	80.9	2.2	1	14.522	7.78	0.3
S06	CBT03	0.0617	52.3	11.8	1	35.843	24.79	0.45
S07	CBE01	0.0415	54.6	7.6	1	37.942	17.94	0.47
S02	CB01	0.1483	51.7	28.7	1	88.226	72.09	0.82
S04	CB03	0.2001	70.2	28.5	1	79.11	94.15	0.75
S05	218	0.1264	53.1	23.8	1	73.958	58.55	0.72
S01	CB06	0.1752	58	30.2	1	80.668	82.83	0.76
S09	IN103407	0.0806	94.8	8.5	1	71.197	38.28	0.7
ES33	IN45573	0.1591	51.3	31	1	31.774	47.93	0.42
ES34	IN45574	0.4099	54.3	75.5	1	10.084	52.02	0.27
ES35	IN45566	0.967	66.5	145.5	1	14.685	111.44	0.3
ES31	IN45577	0.1922	48.3	39.8	1	24.966	47.73	0.37
ES30	IN45572	0.2289	47.4	48.3	1	28.571	56.8	0.4
ES29	IN45569	0.3256	46	70.8	1	26.731	68.83	0.39
ES28	IN45570	0.3422	50.1	68.3	1	21.796	65.07	0.35
ES27	IN45575	0.3696	52.4	70.5	1	13.466	54.66	0.29
ES02_1	IN09004-MAJ	0.0884	48.8	18.1	1	31.285	31.03	0.42
ES32	IN07998	0.7854	57.1	137.6	1	19.912	112.45	0.34
ES19	IN09019-MAJ	0.0992	46.4	21.4	0.5	63.062	42.02	0.64
ES17	IN09034-MAJ	0.135	78.5	17.2	2	41.718	55.98	0.49
ES18	IN09021-MAJ	0.2378	93.3	25.5	2	40.757	91.2	0.49
ES20	IN09020-MAJ	0.0692	32.3	21.4	0.5	33.177	21.4	0.43
ES23	IN45587	0.1837	22.5	81.5	1	32.553	42.33	0.43
ES24	IN45588	0.0806	15.8	51.1	1	27.007	19.06	0.39
ES25	IN45589	0.1875	16.6	112.9	1	27.249	35.2	0.39
ES26	IN45590	0.1086	17.7	61.3	1	32.212	26.83	0.43
ES07	IN09013-MAJ	0.2147	96.7	22.2	0.5	55.576	84.84	0.59
ES36	IN09032-MAJ	0.215	113.8	18.9	0.5	32.12	68.09	0.42
ES03_1	IN09005-MAJ	0.2801	132.1	21.2	1	55.552	117.33	0.59
ES03_2	IN09006-MAJ	0.1878	114.5	16.4	1	50.126	78.54	0.55
ES04_1	IN09008	0.2099	98.1	21.4	0.5	59.961	86.7	0.62
ES04_2	IN09007	0.1951	98	19.9	0.5	55.139	78.13	0.59
ES05_1	IN09009-MAJ	0.1906	91.6	20.8	0.5	52.183	73.74	0.57
ES05_2	IN09010-MAJ	0.1843	89.9	20.5	0.5	54.377	72.96	0.58
ES06_1	IN09011-MAJ	0.2778	134.9	20.6	0.5	59.044	114.46	0.61
ES06_2	IN09012-MAJ	0.2407	123.4	19.5	0.5	55.203	96.75	0.59
ES14_1	IN09014-MAJ	0.1317	97.6	13.5	0.5	42.85	50.81	0.5

Table 6: SUBCATCHMENTS - SUMMARY (continued...)

Name	Outlet	Area (ha)	Width (m)	Flow Length (m)	Slope (%)	Imperv. (%)	Peak Runoff (L/s)	CAVG
ES14_2	IN09015-MAJ	0.181	88.7	20.4	0.5	60.093	75.32	0.62
ES15_1	IN09016	0.0733	75.6	9.7	0.5	37.055	28.86	0.46
ES15_2	MHST09012	0.1226	70.5	17.4	0.5	57.086	50.9	0.6
ES01_1	IN103407	0.3255	57	57.1	1.5	67.777	136.52	0.67
ES02_2	IN09003-MAJ	0.0477	36.7	13	1	44.983	19.97	0.51
ES08_1	IN09022-MAJ	0.1217	85.1	14.3	0.5	44.675	47.15	0.51
ES08_2	IN09023-MAJ	0.0863	47.2	18.3	0.5	29.627	26.74	0.41
ES09_1	IN09024-MAJ	0.1738	96.6	18	0.5	53.85	69.93	0.58
ES09_2	IN09025-MAJ	0.1796	125.6	14.3	0.5	40.275	66.9	0.48
ES13_1	MHST09023	0.1559	69.9	22.3	0.5	56.354	62.01	0.59
ES13_2	MHST09023	0.1672	85.3	19.6	0.5	53.557	66.18	0.57
ES12_1	MHST09022	0.1929	92.7	20.8	0.5	56.58	77.7	0.6
ES12_2	IN09031-MAJ	0.1553	77.3	20.1	0.5	55.364	62.22	0.59
ES11_1	IN09029-MAJ	0.1845	88.3	20.9	0.5	55.004	73.23	0.59
ES11_2	IN09028-MAJ	0.126	71.2	17.7	0.5	44.553	46.69	0.51
ES10_1	IN09026-MAJ	0.2118	108.1	19.6	0.5	50.248	81.31	0.55
ES10_2	IN09027-MAJ	0.1837	110	16.7	0.5	48.55	71.49	0.54
ES16_1	IN09034-MAJ	0.1	107.5	9.3	1.5	35.738	42.83	0.45
ES16_2	IN09035-MAJ	0.1733	100.2	17.3	1.5	26.876	62.46	0.39
ES22_1	IN09016	0.1847	74.8	24.7	0.5	62.634	76.6	0.64
ES22_2	MHST09012	0.218	100.5	21.7	0.5	55.462	86.38	0.59
ES21_3	IN09020-MAJ	0.129	60.8	21.2	0.5	42.562	44.95	0.5
ES21_4	IN09019-MAJ	0.1398	60.3	23.2	0.5	62.819	58.53	0.64
ES21_1	IN09018-MAJ	0.0791	36.8	21.5	0.5	58.867	32.35	0.61
ES21_5	IN09017-MAJ	0.0865	36.2	23.9	0.5	54.717	33.5	0.58
S08_1	CBT14	0.0405	57.857	7	1	59.421	18.82	0.62
S08_2	CBE04	0.0548	78.286	7	1	54.842	25.18	0.58

Table 7: Existing_Structures

NAME	TYPE	LID_ELEV	LID_SOURCE	RYCB_INV	GIS_LENGTH	GIS_AREA
IN07998	RYCB	111.832	CITY GIS	110.43	0	0
IN09001	Catch Basin	113.02	FMW Survey	111.62	0	0
IN09002	Catch Basin	113.02	FMW Survey	111.62	0	0
IN09003	Catch Basin	113.93	OMM grading plan	112.53	0	0
IN09004	Catch Basin	113.83	OMM grading plan	112.43	0	0
IN09005	Catch Basin	113.22	OMM grading plan	111.82	0	0
IN09006	Catch Basin	113.22	OMM grading plan	111.82	0	0
IN09007	Catch Basin	112.98	OMM grading plan	111.58	0	0
IN09008	Catch Basin	112.98	OMM grading plan	111.58	0	0
IN09009	Catch Basin	112.75	OMM Plan & Profile	111.35	0	0
IN09010	Catch Basin	112.75	OMM Plan & Profile	111.35	0	0
IN09011	Catch Basin	112.21	OMM Plan & Profile	110.81	0	0
IN09012	Catch Basin	112.21	OMM Plan & Profile	110.81	0	0
IN09013	Catch Basin	111.78	OMM Plan & Profile	110.38	0	0
IN09014	Catch Basin	111.41	OMM Plan & Profile	110.01	0	0
IN09015	Catch Basin	111.41	OMM Plan & Profile	110.01	0	0
IN09016	Catch Basin	111.25	OMM Plan & Profile	109.85	0	0
IN09017	Catch Basin	111.56	OMM Plan & Profile	110.16	0	0
IN09018	Catch Basin	111.56	OMM Plan & Profile	110.16	0	0
IN09019	Catch Basin	111.33	OMM Plan & Profile	109.93	0	0
IN09020	Catch Basin	111.33	OMM Plan & Profile	109.93	0	0
IN09021	Catch Basin	111	OMM Plan & Profile	109.6	0	0
IN09022	Catch Basin	113.94	OMM Plan & Profile	112.54	0	0
IN09023	Catch Basin	113.75	OMM Plan & Profile	112.35	0	0
IN09024	Catch Basin	113.15	OMM Plan & Profile	111.75	0	0
IN09025	Catch Basin	113.13	OMM Plan & Profile	111.73	0	0
IN09026	Catch Basin	112.66	OMM Plan & Profile	111.26	0	0
IN09027	Catch Basin	112.68	OMM Plan & Profile	111.28	0	0
IN09028	Catch Basin	112.36	OMM Plan & Profile	110.96	0	0
IN09029	Catch Basin	112.37	OMM Plan & Profile	110.97	0	0
IN09030	Catch Basin	111.97	OMM Plan & Profile	110.57	0	0
IN09031	Catch Basin	111.97	OMM Plan & Profile	110.57	0	0
IN09032	Catch Basin	111.62	OMM Plan & Profile	110.22	0	0
IN09033	Catch Basin	111.62	OMM Plan & Profile	110.22	0	0
IN09034	Catch Basin	111.27	OMM Plan & Profile	109.87	0	0
IN09035	Catch Basin	111.27	OMM Plan & Profile	109.87	0	0
IN103406	Double Catch Basin	112.95	FMW Survey	111.55	0	0
IN103407	Double Catch Basin	112.97	FMW Survey	111.57	0	0
IN45566	RYCB	111.215	CITY GIS	109.82	0	0

Table 7: Existing_Structures (continued...)

NAME	TYPE	LID_ELEV	LID_SOURCE	RYCB_INV	GIS_LENGTH	GIS_AREA
IN45569	RYCB	113.007	CITY GIS	111.61	0	0
IN45570	RYCB	113.104	CITY GIS	111.7	0	0
IN45572	RYCB	112.912	CITY GIS	111.51	0	0
IN45573	RYCB	114.156	CITY GIS	112.76	0	0
IN45574	RYCB	111.346	CITY GIS	109.95	0	0
IN45575	RYCB	113.572	CITY GIS	112.17	0	0
IN45577	RYCB	112.682	CITY GIS	111.28	0	0
IN45587	RYCB	113.845	CITY GIS	112.44	0	0
IN45588	RYCB	113.922	CITY GIS	112.52	0	0
IN45589	RYCB	113.246	CITY GIS	111.85	0	0
IN45590	RYCB	112.982	CITY GIS	111.58	0	0
MHST09001	Storm Manhole	113.141	DTM	111.74	0	0
MHST09002	Storm Manhole	113.216	DTM	111.82	0	0
MHST09003	Storm Manhole	113.836	DTM	112.44	0	0
MHST09004	Storm Manhole	114.027	DTM	112.63	0	0
MHST09005	Storm Manhole	113.503	DTM	112.1	0	0
MHST09006	Storm Manhole	112.934	DTM	111.53	0	0
MHST09007	Storm Manhole	112.834	DTM	111.43	0	0
MHST09008	Storm Manhole	112.425	DTM	111.02	0	0
MHST09009	Storm Manhole	112.279	DTM	110.88	0	0
MHST09010	Storm Manhole	111.974	DTM	110.57	0	0
MHST09011	Storm Manhole	111.672	DTM	110.27	0	0
MHST09012	Catch Basin Manhole	111.128	DTM	109.73	0	0
MHST09013	Storm Manhole	111.586	DTM	110.19	0	0
MHST09014	Storm Manhole	111.496	DTM	110.1	0	0
MHST09015	Storm Manhole	111.798	DTM	110.4	0	0
MHST09016	Storm Manhole	114.182	DTM	112.78	0	0
MHST09017	Storm Manhole	114.098	DTM	112.7	0	0
MHST09018	Storm Manhole	113.871	DTM	112.47	0	0
MHST09019	Storm Manhole	113.279	DTM	111.88	0	0
MHST09020	Storm Manhole	112.931	DTM	111.53	0	0
MHST09021	Storm Manhole	112.531	DTM	111.13	0	0
MHST09022	Storm Manhole	112.266	DTM	110.87	0	0
MHST09023	Storm Manhole	111.804	DTM	110.4	0	0
MHST09024	Storm Manhole	111.391	DTM	109.99	0	0

*exp Services Inc
Hazeldean Crossing Inc.
5924 Hazeldean Road
OTT-00250806-B0
January 22, 2020*

Appendix H – Correspondence

Correspondence from City of Ottawa

Jason Fitzpatrick

From: Kuruvilla, Santhosh <Santhosh.Kuruvilla@ottawa.ca>
Sent: Wednesday, October 9, 2019 7:40 AM
To: Jason Fitzpatrick
Cc: Bruce Thomas
Subject: RE: Hazeldean Crossing - 5924, 5938 Hazeldean Road
Attachments: 5924 Hazeldean Road _Boundary Conditions_8Oct2019.docx

Categories: RECEIVED - ACTION REQUIRED

Hi Jason,

Please find attached the boundary conditions for the subject application.

Thanks,

Santhosh

From: Jason Fitzpatrick <jason.fitzpatrick@exp.com>
Sent: October 03, 2019 9:28 AM
To: Kuruvilla, Santhosh <Santhosh.Kuruvilla@ottawa.ca>
Cc: Bruce Thomas <bruce.thomas@exp.com>
Subject: Hazeldean Crossing - 5924, 5938 Hazeldean Road

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ATTENTION : Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.

Hi Santosh,

We would appreciate if you could arrange for updated boundary conditions that we can use to revise our water model for the above noted project.

On our previous submission the boundary condition was based on a lower RFF of 10,000 L/min, whereas it should be based on a higher RFF of 250 L/sec (most critical block)

For reference , I've attached the previous boundary conditions that we received from Eric.

We would appreciate if Water Resources could provide Boundary Conditions at the same three locations, based on the higher RFF of 250 L/sec

The HGL boundary conditions based on the following information at your earliest convenience:

- Max Day Plus Fire flow : ~~167~~ **250** L/sec (most critical) + 3.5 L/sec = ~~170.5~~ **253.5** L/sec
- Peak Hour: 5.2 L/sec

Regards.



Jason Fitzpatrick, P.Eng.

EXP | Project Engineer

t : +1.613.688.1899 | m : +1.613.302.7441 | e : jason.fitzpatrick@exp.com

2650 Queensview Drive

Suite 100

Ottawa, ON K2B 8H6

CANADA

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'

Boundary Conditions for 5924 Hazeldean Road

Date Provided

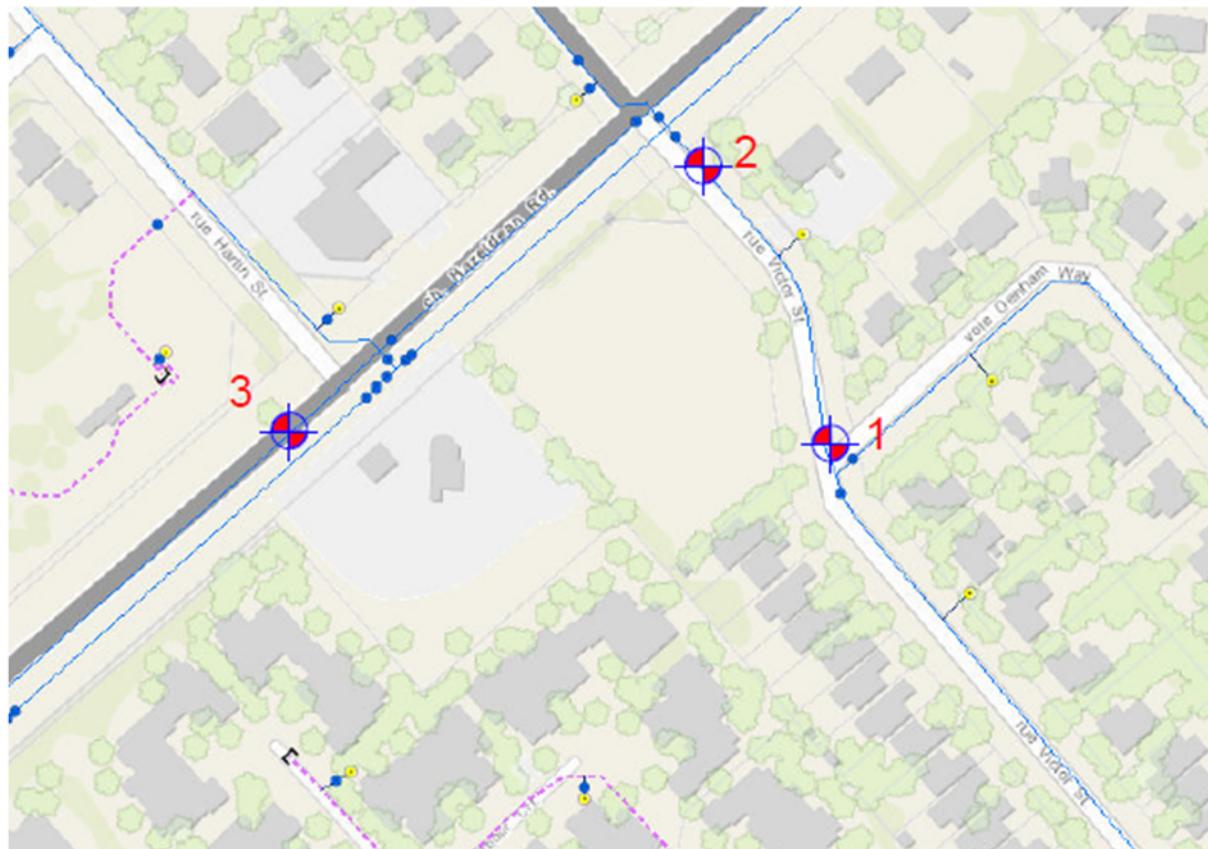
October-19

Scenario	Demand	
	L/min	L/s
Average Daily Demand	46	0.76
Maximum Daily Demand	210	3.5
Peak Hour	312	5.2
Fire Flow Demand #1	15000	250

of connections

3

Location:



Results:

Connection 1 - Victor Street and Denham Way

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	160.9	66.6
Peak Hour	157.2	61.4
Max Day plus Fire 1	135.4	30.4

¹ Ground Elevation = 114.0 m

Connection 2 - Victor Street

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	160.9	68.0
Peak Hour	157.3	62.9
Max Day plus Fire 1	154.1	58.4

¹ Ground Elevation = 113.0 m

Connection 3 - Hazeldean Road

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	160.8	66.2
Peak Hour	157.3	61.2
Max Day plus Fire 1	158.3	62.6

¹ Ground Elevation = 114.3 m

Notes:

1. Connection 3 to 762mm watermain on Hazeldean Road is not permitted.

Disclaimer

The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation. Fire Flow analysis is a reflection of available flow in the watermain; there may be additional restrictions that occur between the watermain and the hydrant that the model cannot take into account.

*exp Services Inc
Hazeldean Crossing Inc.
5924 Hazeldean Road
OTT-00250806-B0
January 22, 2020*

Appendix I – Manufacturer Information

IPEX Tempest Inlet Control Devices – Technical Manual

Stormtech MC-3500 Design Manual (Pages B16, B17)

Stormtech MC-3500 Cut Sheet

Volume III: TEMPEST™ INLET CONTROL DEVICES

Municipal Technical
Manual Series



SECOND EDITION

LMF (Low to Medium Flow) ICD

HF (High Flow) ICD

MHF (Medium to High Flow) ICD



IPEX

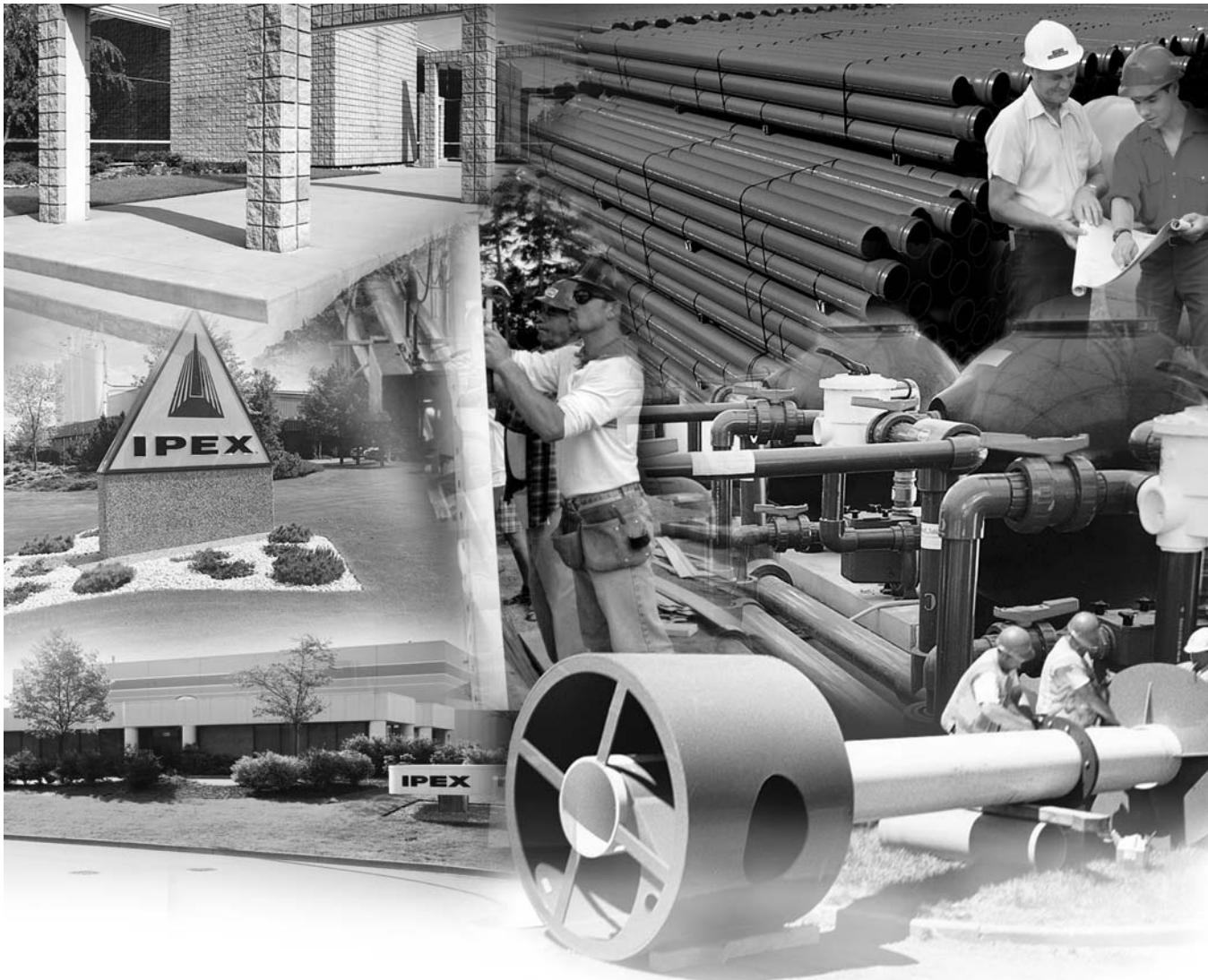
IPEX Tempest™ Inlet Control Devices

Municipal Technical Manual Series

Vol. I, 2nd Edition

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ABOUT IPEX

At IPEX, we have been manufacturing non-metallic pipe and fittings since 1951. We formulate our own compounds and maintain strict quality control during production. Our products are made available for customers thanks to a network of regional stocking locations throughout North America. We offer a wide variety of systems including complete lines of piping, fittings, valves and custom-fabricated items.

More importantly, we are committed to meeting our customers' needs. As a leader in the plastic piping industry, IPEX continually develops new products, modernizes manufacturing facilities and acquires innovative process technology. In addition, our staff take pride in their work, making available to customers their extensive thermoplastic knowledge and field experience. IPEX personnel are committed to improving the safety, reliability and performance of thermoplastic materials. We are involved in several standards committees and are members of and/or comply with the organizations listed on this page.

For specific details about any IPEX product, contact our customer service department.

CONTENTS

TEMPEST INLET CONTROL DEVICES Technical Manual

About IPEX

Section One: Product Information: TEMPEST Low, Medium Flow (LMF) ICD

Purpose	4
Product Description	4
Product Function	4
Product Construction	4
Product Applications	4
Chart 1: LMF 14 Preset Flow Curves	5
Chart 2: LMF Flow Vs. ICD Alternatives	5

Product Installation

Instructions to assemble a TEMPEST LMF ICD into a square catch basin:	6
Instructions to assemble a TEMPEST LMF ICD into a round catch basin:	6

Product Technical Specification

General	7
Materials	7
Dimensioning	7
Installation	7

Section Two: Product Information: TEMPEST High Flow (HF) & Medium, High Flow (MHF) ICD

Product Description	8
Product Function	8
Product Construction	8
Product Applications	8
Chart 3: HF & MHF Preset Flow Curves	9

Product Installation

Instructions to assemble a TEMPEST HF or MHF ICD into a square catch basin:	10
Instructions to assemble a TEMPEST HF or MHF ICD into a round catch basin:	10
Instructions to assemble a TEMPEST HF Sump into a square or round catch basin:	11

Product Technical Specification

General	11
Materials	11
Dimensioning	11
Installation	11

PRODUCT INFORMATION: TEMPEST LOW, MEDIUM FLOW (LMF) ICD

Purpose

To control the amount of storm water runoff entering a sewer system by allowing a specified flow volume out of a catch basin or manhole at a specified head. This approach conserves pipe capacity so that catch basins downstream do not become uncontrollably surcharged, which can lead to basement floods, flash floods and combined sewer overflows.

Product Description

Our LMF ICD is designed to accommodate catch basins or manholes with sewer outlet pipes 6" in diameter and larger. Any storm sewer larger than 12" may require custom modification. However, IPEX can custom build a TEMPEST device to accommodate virtually any storm sewer size.

Available in 14 preset flow curves, the LMF ICD has the ability to provide flow rates: 2lps – 17lps (31gpm – 270gpm)

Product Function

The LMF ICD vortex flow action allows the LMF ICD to provide a narrower flow curve using a larger orifice than a conventional orifice plate ICD, making it less likely to clog. When comparing flows at the same head level, the LMF ICD has the ability to restrict more flow than a conventional ICD during a rain event, preserving greater sewer capacity.

Product Construction

Constructed from durable PVC, the LMF ICD is light weight 8.9 Kg (19.7 lbs).

Product Applications

Will accommodate both square and round applications:

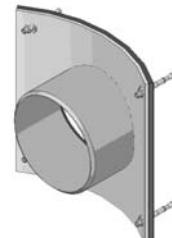


Square Application

Round Application

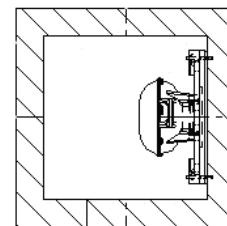


Universal
Mounting Plate



+

Spigot CB
Wall Plate



=

Universal
Mounting
Plate Hub
Adapter

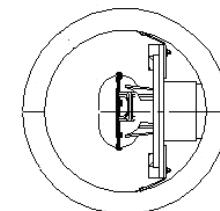
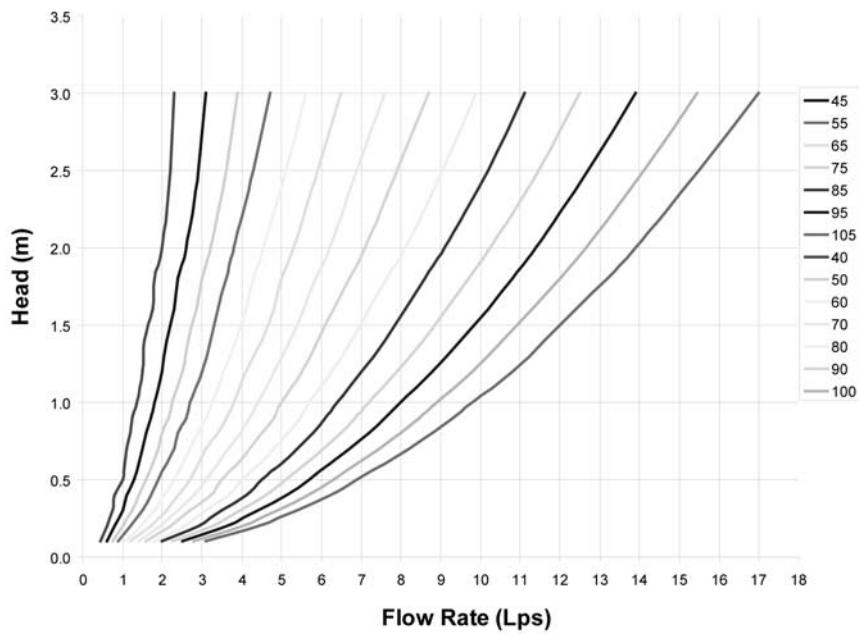
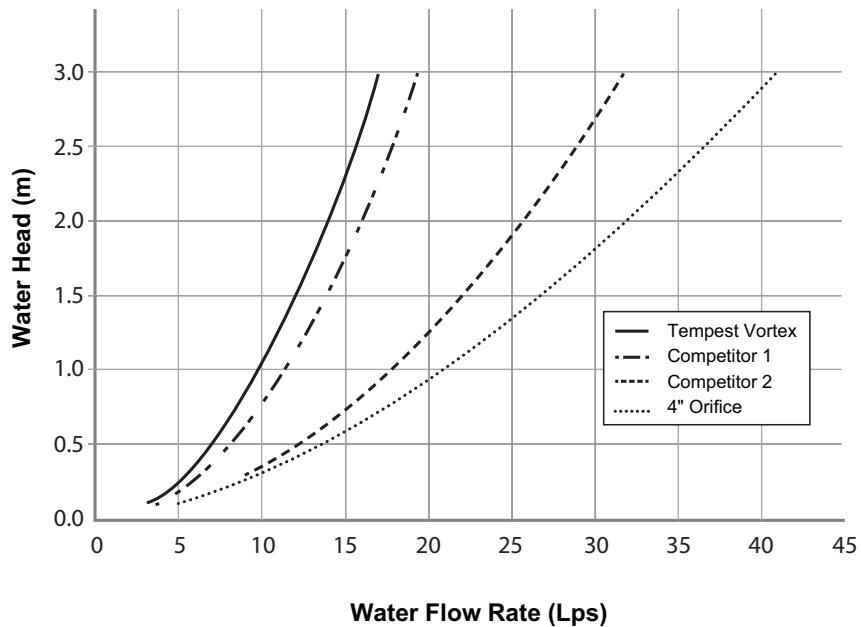


Chart 1: LMF 14 Preset Flow Curves**Chart 2: LMF Flow vs. ICD Alternatives**

PRODUCT INSTALLATION

Instructions to assemble a TEMPEST LMF ICD into a Square Catch Basin:

STEPS:

- Materials and tooling verification:
 - Tooling: impact drill, 3/8" concrete bit, torque wrench for 9/16" nut, hand hammer, level, and marker.
 - Material: (4) concrete anchor 3/8 x 3-1/2, (4) washers, (4) nuts, universal mounting plate, ICD device.
- Use the mounting wall plate to locate and mark the hole (4) pattern on the catch basin wall. You should use a level to ensure that the plate is at the horizontal.
- Use an impact drill with a 3/8" concrete bit to make the four holes at a minimum of 1-1/2" depth up to 2-1/2". Clean the concrete dust from the holes.
- Install the anchors (4) in the holes by using a hammer. Thread the nuts on the top of the anchors to protect the threads when you hit the anchors with the hammer. Remove the nuts from the ends of the anchors.
- Install the universal mounting plate on the anchors and screw the 4 nuts in place with a maximum torque of 40 N.m (30 lbf-ft). There should be no gap between the wall mounting plate and the catch basin wall.
- From the ground above using a reach bar, lower the ICD device by hooking the end of the reach bar to the handle of the ICD device. Align the triangular plate portion into the mounting wall plate. Push down the device to be sure it has centered in to the universal mounting plate and has created a seal.



WARNING

- Verify that the outlet pipe doesn't protrude into the catch basin. If it does, cut down the pipe flush to the catch basin wall.
- Call your IPEX representative for more information or if you have any questions about our products.

Instructions to assemble a TEMPEST LMF ICD into a Round Catch Basin:

STEPS:

- Materials and tooling verification:
 - Tooling: impact drill, 3/8" concrete bit, torque wrench for 9/16" nut, hand hammer, level and marker.
 - Material: (4) concrete anchor 3/8 x 3-1/2, (4) washers and (4) nuts, spigot CB wall plate, universal mounting plate hub adapter, ICD device.
- Use the spigot catch basin wall plate to locate and mark the hole (4) pattern on the catch basin wall. You should use a level to ensure that the plate is at the horizontal.
- Use an impact drill with a 3/8" concrete bit to make the four holes at a depth between 1-1/2" to 2-1/2". Clean the concrete dust from the holes.
- Install the anchors (4) in the holes by using a hammer. Thread the nuts on the top of the anchors to protect the threads when you hit the anchors with the hammer. Remove the nuts from the ends of the anchors.
- Install the CB spigot wall plate on the anchors and screw the 4 nuts in place with a maximum torque of 40 N.m (30 lbf-ft). There should be no gap between the spigot wall plate and the catch basin wall.
- Apply solvent cement on the hub of the universal mounting plate, hub adapter and the spigot of the CB wall plate, then slide the hub over the spigot. Make sure the universal mounting plate is at the horizontal and its hub is completely inserted onto the spigot. Normally, the corners of the universal mounting plate hub adapter should touch the catch basin wall.
- From ground above using a reach bar, lower the ICD device by hooking the end of the reach bar to the handle of the ICD device. Align the triangular plate portion into the mounting wall plate. Push down the device to be sure it has centered in to the mounting plate and has created a seal.



WARNING

- Verify that the outlet pipe doesn't protrude into the catch basin. If it does, cut back the pipe flush to the catch basin wall.
- The solvent cement which is used in this installation is to be approved for PVC.
- The solvent cement should not be used below 0°C (32°F) or in a high humidity environment. Refer to the IPEX solvent cement guide to confirm the required curing time or visit the IPEX Online Solvent Cement Training Course available at www.ipexinc.com.
- Call your IPEX representative for more information or if you have any questions about our products.

PRODUCT TECHNICAL SPECIFICATION

General

Inlet control devices (ICD's) are designed to provide flow control at a specified rate for a given water head level and also provide odour and floatable control. All ICD's will be IPEX Tempest or approved equal.

All devices shall be removable from a universal mounting plate. An operator from street level using only a T-bar with a hook will be able to retrieve the device while leaving the universal mounting plate secured to the catch basin wall face. The removal of the TEMPEST devices listed above must not require any unbolting or special manipulation or any special tools.

High Flow (HF) Sump devices will consist of a removable threaded cap which can be accessible from street level without entry into the catchbasin (CB). The removal of the threaded cap shall not require any special tools other than the operator's hand.

ICD's shall have no moving parts.

Materials

ICD's are to be manufactured from Polyvinyl Chloride (PVC) or Polyurethane material, designed to be durable enough to withstand multiple freeze-thaw cycles and exposure to harsh elements.

The inner ring seal will be manufactured using a Buna or Nitrile material with hardness between Duro 50 and Duro 70.

The wall seal is to be comprised of a 3/8" thick Neoprene Closed Cell Sponge gasket which is attached to the back of the wall plate.

All hardware will be made from 304 stainless steel.

Dimensioning

The Low Medium Flow (LMF), High Flow (HF) and the High Flow (HF) Sump shall allow for a minimum outlet pipe diameter of 200mm with a 600mm deep Catch Basin sump.

Installation

Contractor shall be responsible for securing, supporting and connecting the ICD's to the existing influent pipe and catchbasin/manhole structure as specified and designed by the Engineer.

PRODUCT INFORMATION: TEMPEST HF & MHF ICD

Product Description

Our HF, HF Sump and MHF ICD's are designed to accommodate catch basins or manholes with sewer outlet pipes 6" in diameter or larger. Any storm sewer larger than 12" may require custom modification. However, IPEX can custom build a TEMPEST device to accommodate virtually any storm sewer size.

Available in 5 preset flow curves, these ICDs have the ability to provide constant flow rates: 9lps (143 gpm) and greater

Product Function

TEMPEST HF (High Flow): designed to manage moderate to higher flows 15 L/s (240 gpm) or greater and prevent the propagation of odour and floatables. With this device, the cross-sectional area of the device is larger than the orifice diameter and has been designed to limit head losses. The HF ICD can also be ordered without flow control when only odour and floatable control is required.



TEMPEST HF (High Flow) Sump: The height of a sewer outlet pipe in a catch basin is not always conveniently located. At times it may be located very close to the catch basin floor, not providing enough sump for one of the other TEMPEST ICDs with universal back plate to be installed. In these applications, the HF Sump is offered. The HF Sump offers the same features and benefits as the HF ICD; however, is designed to raise the outlet in a square or round catch basin structure. When installed, the HF sump is fixed in place and not easily removed. Any required service to the device is performed through a clean-out located in the top of the device which can be often accessed from ground level.



TEMPEST MHF (Medium to High Flow):

The MHF plate or plug is designed to control flow rates 9 L/s (143 gpm) or greater. It is not designed to prevent the propagation of odour and floatables.

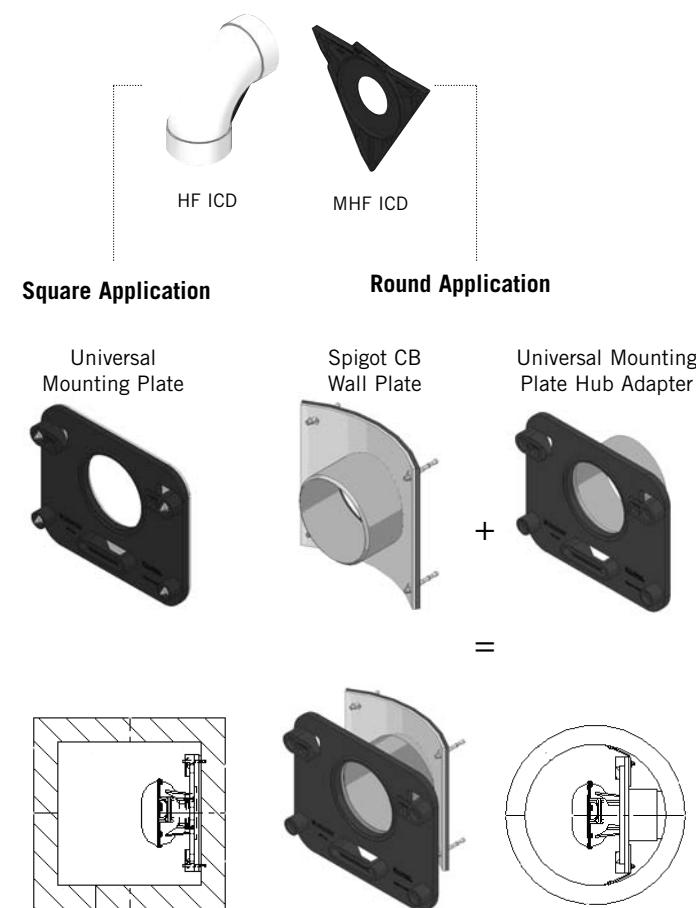


Product Construction

The HF, HF Sump and MHF ICDs are built to be light weight at a maximum weight of 6.8 Kg (14.6 lbs).

Product Applications

The HF and MHF ICD's are available to accommodate both square and round applications:



The HF Sump is available to accommodate low to no sump applications in both square and round catch basins:

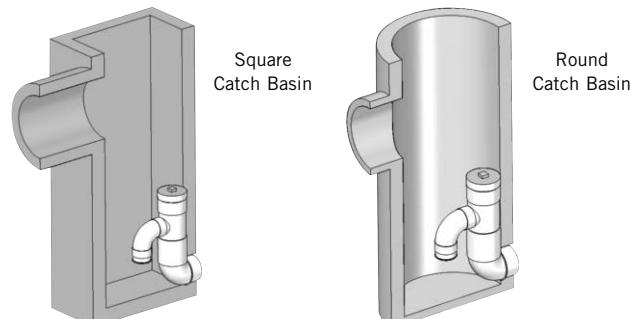
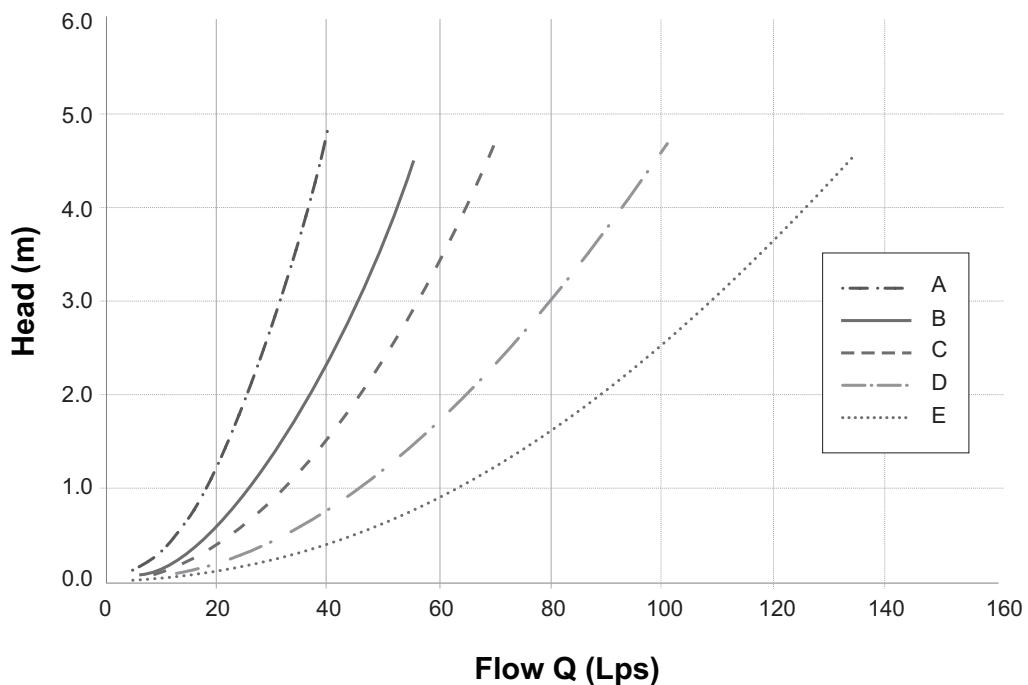


Chart 3: HF & MHF Preset Flow Curves



PRODUCT INSTALLATION

Instructions to assemble a TEMPEST HF or MHF ICD into a Square Catch Basin:

1. Materials and tooling verification:
 - Tooling: impact drill, 3/8" concrete bit, torque wrench for 9/16" nut, hand hammer, level, and marker.
 - Material: (4) concrete anchor 3/8 x 3-1/2, (4) washers, (4) nuts, universal mounting plate, ICD device
2. Use the mounting wall plate to locate and mark the hole (4) pattern on the catch basin wall. You should use a level to ensure that the plate is at the horizontal.
3. Use an impact drill with a 3/8" concrete bit to make the four holes at a minimum of 1-1/2" depth up to 2-1/2". Clean the concrete dust from the holes.
4. Install the anchors (4) in the holes by using a hammer. Thread the nuts on the top of the anchors to protect the threads when you hit the anchors with the hammer. Remove the nuts from the ends of the anchors.
5. Install the universal wall mounting plate on the anchors and screw the 4 nuts in place with a maximum torque of 40 N.m (30 lbf-ft). There should be no gap between the wall mounting plate and the catch basin wall.
6. From the ground above using a reach bar, lower the device by hooking the end of the reach bar to the handle of the ICD device. Align the triangular plate portion into the mounting wall plate. Push down the device to be sure it has centered in to the universal wall mounting plate and has created a seal.



WARNING

- Verify that the outlet pipe doesn't protrude into the catch basin. If it does, cut down the pipe flush to the catch basin wall.
- Call your IPEX representative for more information or if you have any questions about our products.

Instructions to assemble a TEMPEST HF or MHF ICD into a Round Catch Basin:

STEPS:

1. Materials and tooling verification.
- Tooling: impact drill, 3/8" concrete bit, torque wrench for 9/16" nut, hand hammer, level and marker.
- Material: (4) concrete anchor 3/8 x 3-1/2, (4) washers and (4) nuts, spigot CB wall plate, universal mounting plate hub adapter, ICD device.
2. Use the round catch basin spigot adaptor to locate and mark the hole (4) pattern on the catch basin wall. You should use a level to ensure that the plate is at the horizontal.
3. Use an impact drill with a 3/8" concrete bit to make the four holes at a depth between 1-1/2" to 2-1/2". Clean the concrete dust from the holes.
4. Install the anchors (4) in the holes by using a hammer. Thread the nuts on the top of the anchors to protect the threads when you hit the anchors with the hammer. Remove the nuts from the ends of the anchors.
5. Install the spigot CB wall plate on the anchors and screw the 4 nuts in place with a maximum torque of 40 N.m (30 lbf-ft). There should be no gap between the spigot CB wall plate and the catch basin wall.
6. Put solvent cement on the hub of the universal mounting plate, hub adapter and the spigot of the CB wall plate, then slide the hub over the spigot. Make sure the universal mounting plate is at the horizontal and its hub is completely inserted onto the spigot. Normally, the corners of the hub adapter should touch the catch basin wall.
7. From ground above using a reach bar, lower the device by hooking the end of the reach bar to the handle of the ICD device. Align the triangular plate portion into the mounting wall plate. Push down the device to be sure it has centered in to the wall mounting plate and has created a seal.



WARNING

- Verify that the outlet pipe doesn't protrude into the catch basin. If it does, cut down the pipe flush to the catch basin wall.
- The solvent cement which is used in this installation is to be approved for PVC.
- The solvent cement should not be used below 0°C (32°F) or in a high humidity environment. Refer to the IPEX solvent cement guide to confirm the required curing time or visit the IPEX Online Solvent Cement Training Course available at www.ipexinc.com.
- Call your IPEX representative for more information or if you have any questions about our products.

PRODUCT TECHNICAL SPECIFICATION

Instructions to assemble a TEMPEST HF Sump into a Square or Round Catch Basin:

STEPS:

1. Materials and tooling verification:
 - Tooling: impact drill, 3/8" concrete bit, torque wrench for 9/16" nut, hand hammer, level, mastic tape and metal strapping
 - Material: (2) concrete anchor 3/8 x 3-1/2, (2) washers, (2) nuts, HF Sump pieces (2).
2. Apply solvent cement to the spigot end of the top half of the sump. Apply solvent cement to the hub of the bottom half of the sump. Insert the spigot of the top half of the sump into the hub of the bottom half of the sump.
3. Install the 8" spigot of the device into the outlet pipe. Use the mastic tape to seal the device spigot into the outlet pipe. You should use a level to be sure that the fitting is standing at the vertical.
4. Use an impact drill with a 3/8" concrete bit to make a series of 2 holes along each side of the body throat. The depth of the hole should be between 1-1/2" to 2-1/2". Clean the concrete dust from the 2 holes.
5. Install the anchors (2) in the holes by using a hammer. Put the nuts on the top of the anchors to protect the threads when you hit the anchors. Remove the nuts from the ends of the anchors.
6. Cut the metal strapping to length and connect each end of the strapping to the anchors. Screw the nuts in place with a maximum torque of 40 N.m (30 lbf-ft). The device should be completely flush with the catch basin wall.



WARNING

- Verify that the outlet pipe doesn't protrude into the catch basin. If it does, cut down the pipe flush to the catch basin wall.
- The solvent cement which is used in this installation is to be approved for PVC.
- The solvent cement should not be used below 0°C (32°F) or in a high humidity environment. Refer to the IPEX solvent cement guide to confirm the required curing time or visit the IPEX Online Solvent Cement Training Course available at www.ipexinc.com.
- Call your IPEX representative for more information or if you have any questions about our products.

General

Inlet control devices (ICD's) are designed to provide flow control at a specified rate for a given water head level and also provide odour and floatable control where specified. All ICD's will be IPEX Tempest or approved equal.

All devices shall be removable from a universal mounting plate. An operator from street level using only a T-bar with a hook shall be able to retrieve the device while leaving the universal mounting plate secured to the catch basin wall face. The removal of the TEMPEST devices listed above shall not require any unbolting or special manipulation or any special tools.

High Flow (HF) Sump devices shall consist of a removable threaded cap which can be accessible from street level with out entry into the catchbasin (CB). The removal of the threaded cap shall not require any special tools other than the operator's hand.

ICD's shall have no moving parts.

TEMPEST
HF & MHF ICD

Materials

ICD's are to be manufactured from Polyvinyl Chloride (PVC) or Polyurethane material, designed to be durable enough to withstand multiple freeze-thaw cycles and exposure to harsh elements.

The inner ring seal will be manufactured using a Buna or Nitrile material with hardness between Duro 50 and Duro 70.

The wall seal is to be comprised of a 3/8" thick Neoprene Closed Cell Sponge gasket which is attached to the back of the wall plate.

All hardware will be made from 304 stainless steel.

Dimensioning

The Low Medium Flow (LMF), High Flow (HF) and the High Flow (HF) Sump shall allow for a minimum outlet pipe diameter of 200mm with a 600mm deep Catch Basin sump.

Installation

Contractor shall be responsible for securing, supporting and connecting the ICD's to the existing influent pipe and catchbasin/manhole structure as specified and designed by the Engineer.

SALES AND CUSTOMER SERVICE

Canadian Customers call IPEX Inc.

Toll free: (866) 473-9462

www.ipexinc.com

U.S. Customers call IPEX USA LLC

Toll free: (800) 463-9572

www.ipexamerica.com

About the IPEX Group of Companies

As leading suppliers of thermoplastic piping systems, the IPEX Group of Companies provides our customers with some of the largest and most comprehensive product lines. All IPEX products are backed by more than 50 years of experience. With state-of-the-art manufacturing facilities and distribution centers across North America, we have established a reputation for product innovation, quality, end-user focus and performance.

Markets served by IPEX group products are:

- Electrical systems
- Telecommunications and utility piping systems
- PVC, CPVC, PP, ABS, PEX, FR-PVDF and PE pipe and fittings
(1/4" to 48")
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- Municipal pressure and gravity piping systems
- Plumbing and mechanical piping systems
- PE Electrofusion systems for gas and water
- Industrial, plumbing and electrical cements
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A policy of ongoing product improvement is maintained. This may result in modifications of features and/or specifications without notice.

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5.0 Cumulative Storage Volumes



Tables 7 and 8 provide cumulative storage volumes for the MC-3500 chamber and end cap. These tables can be used to calculate the stage-storage relationship for the retention or detention system. Digital spreadsheets in which the number of chambers and end caps can be input for quick

cumulative storage calculations are available at www.stormtech.com. For assistance with site-specific calculations or input into routing software, contact the StormTech Technical Services Department.

TABLE 7 – MC-3500 Incremental Storage Volume Per Chamber

Assumes 40% stone porosity. Calculations are based upon a 9" (230 mm) stone base under the chambers, 12" (300 mm) of stone above chambers, and 9" (230 mm) of spacing between chambers.

Depth of Water in System Inches (mm)	Cumulative Chamber Storage ft ³ (m ³)	Total System Cumulative Storage ft ³ (m ³)
66 (1676)	0.00	178.96 (5.068)
65 (1651)	0.00	177.25 (5.019)
64 (1626)	0.00	175.54 (4.971)
63 (1600)	Stone	0.00
62 (1575)	Cover	0.00
61 (1549)	0.00	170.40 (4.825)
60 (1524)	0.00	168.69 (4.777)
59 (1499)	0.00	166.98 (4.728)
58 (1473)	0.00	165.27 (4.680)
57 (1448)	0.00	163.55 (4.631)
56 (1422)	0.00	161.84 (4.583)
55 (1397)	0.00	160.13 (4.534)
54 (1372)	109.95 (3.113)	158.42 (4.486)
53 (1346)	109.89 (3.112)	156.67 (4.436)
52 (1321)	109.69 (3.106)	154.84 (4.385)
51 (1295)	109.40 (3.098)	152.95 (4.331)
50 (1270)	109.00 (3.086)	151.00 (4.276)
49 (1245)	108.31 (3.067)	148.88 (4.216)
48 (1219)	107.28 (3.038)	146.55 (4.150)
47 (1194)	106.03 (3.003)	144.09 (4.080)
46 (1168)	104.61 (2.962)	141.52 (4.007)
45 (1143)	103.04 (2.918)	138.86 (3.932)
44 (1118)	101.33 (2.869)	136.13 (3.855)
43 (1092)	99.50 (2.818)	133.32 (3.775)
42 (1067)	97.56 (2.763)	130.44 (3.694)
41 (1041)	95.52 (2.705)	127.51 (3.611)
40 (1016)	93.39 (2.644)	124.51 (3.526)
39 (991)	91.16 (2.581)	121.47 (3.440)
38 (965)	88.86 (2.516)	118.37 (3.352)
37 (948)	86.47 (2.449)	115.23 (3.263)
36 (914)	84.01 (2.379)	112.04 (3.173)
35 (889)	81.49 (2.307)	108.81 (3.081)
34 (864)	78.89 (2.234)	105.54 (2.989)
33 (838)	76.24 (2.159)	102.24 (2.895)

Depth of Water in System Inches (mm)	Cumulative Chamber Storage ft ³ (m ³)	Total System Cumulative Storage ft ³ (m ³)
32 (813)	73.52 (2.082)	98.90 (2.800)
31 (787)	70.75 (2.003)	95.52 (2.705)
30 (762)	67.92 (1.923)	92.12 (2.608)
29 (737)	65.05 (1.842)	88.68 (2.511)
28 (711)	62.12 (1.759)	85.21 (2.413)
27 (686)	59.15 (1.675)	81.72 (2.314)
26 (660)	56.14 (1.590)	78.20 (2.214)
25 (635)	53.09 (1.503)	74.65 (2.114)
24 (610)	49.99 (1.416)	71.09 (2.013)
23 (584)	46.86 (1.327)	67.50 (1.911)
22 (559)	43.70 (1.237)	63.88 (1.809)
21 (533)	40.50 (1.147)	60.25 (1.706)
20 (508)	37.27 (1.055)	56.60 (1.603)
19 (483)	34.01 (0.963)	52.93 (1.499)
18 (457)	30.72 (0.870)	49.25 (1.395)
17 (432)	27.40 (0.776)	45.54 (1.290)
16 (406)	24.05 (0.681)	41.83 (1.184)
15 (381)	20.69 (0.586)	38.09 (1.079)
14 (356)	17.29 (0.490)	34.34 (0.973)
13 (330)	13.88 (0.393)	30.58 (0.866)
12 (305)	10.44 (0.296)	26.81 (0.759)
11 (279)	6.98 (0.198)	23.02 (0.652)
10 (254)	3.51 (0.099)	19.22 (0.544)
9 (229)	0.00	15.41 (0.436)
8 (203)	0.00	13.70 (0.388)
7 (178)	0.00	11.98 (0.339)
6 (152)	Stone	0.00
5 (127)	Foundation	0.00
4 (102)	0.00	6.85 (0.194)
3 (76)	0.00	5.14 (0.145)
2 (51)	0.00	3.42 (0.097)
1 (25)	0.00	1.71 (0.048)

NOTE: Add 1.71 ft³ (0.030 m³) of storage for each additional inch (25 mm) of stone foundation.
Contact StormTech for cumulative volume spreadsheets in digital format.

5.0 Cumulative Storage Volume

TABLE 8 – MC-3500 Incremental Storage Volume Per End Cap

Assumes 40% stone porosity. Calculations are based upon a 9" (230 mm) stone base under the chambers, 12" (300 mm) of stone above end caps, and 9" (230 mm) of spacing between end caps and 6" (150 mm) of stone perimeter.

Depth of Water in System Inches (mm)	Cumulative End Cap Storage ft ³ (m ³)	Total System Cumulative Storage ft ³ (m ³)
66 (1676)	0.00	46.96 (1.330)
65 (1651)	0.00	46.39 (1.314)
64 (1626)	0.00	45.82 (1.298)
63 (1600)	Stone	45.25 (1.281)
62 (1575)	Cover	44.68 (1.265)
61 (1549)		44.11 (1.249)
60 (1524)		43.54 (1.233)
59 (1499)		42.98 (1.217)
58 (1473)		42.41 (1.201)
57 (1448)		41.84 (1.185)
56 (1422)		41.27 (1.169)
55 (1397)	0.00	40.70 (1.152)
54 (1372)	15.64 (0.443)	40.13 (1.136)
53 (1346)	15.64 (0.443)	39.56 (1.120)
52 (1321)	15.63 (0.443)	38.99 (1.104)
51 (1295)	15.62 (0.442)	38.41 (1.088)
50 (1270)	15.60 (0.442)	37.83 (1.071)
49 (1245)	15.56 (0.441)	37.24 (1.054)
48 (1219)	15.51 (0.439)	36.64 (1.037)
47 (1194)	15.44 (0.437)	36.02 (1.020)
46 (1168)	15.35 (0.435)	35.40 (1.003)
45 (1143)	15.25 (0.432)	34.77 (0.985)
44 (1118)	15.13 (0.428)	34.13 (0.966)
43 (1092)	14.99 (0.424)	33.48 (0.948)
42 (1067)	14.83 (0.420)	32.81 (0.929)
41 (1041)	14.65 (0.415)	32.13 (0.910)
40 (1016)	14.45 (0.409)	31.45 (0.890)
39 (991)	14.24 (0.403)	30.75 (0.871)
38 (965)	14.00 (0.396)	30.03 (0.850)
37 (948)	13.74 (0.389)	29.31 (0.830)
36 (914)	13.47 (0.381)	28.58 (0.809)
35 (889)	13.18 (0.373)	27.84 (0.788)
34 (864)	12.86 (0.364)	27.08 (0.767)

Depth of Water in System Inches (mm)	Cumulative Chamber Storage ft ³ (m ³)	Total System Cumulative Storage ft ³ (m ³)
33 (838)	12.53 (0.355)	26.30 (0.745)
32 (813)	12.18 (0.345)	25.53 (0.723)
31 (787)	11.81 (0.335)	24.74 (0.701)
30 (762)	11.42 (0.323)	23.93 (0.678)
29 (737)	11.01 (0.312)	23.12 (0.655)
28 (711)	10.58 (0.300)	22.29 (0.631)
27 (686)	10.13 (0.287)	21.45 (0.607)
26 (660)	9.67 (0.274)	20.61 (0.583)
25 (635)	9.19 (0.260)	19.75 (0.559)
24 (610)	8.70 (0.246)	18.88 (0.559)
23 (584)	8.19 (0.232)	18.01 (0.510)
22 (559)	7.67 (0.217)	17.13 (0.485)
21 (533)	7.13 (0.202)	16.24 (0.460)
20 (508)	6.59 (0.187)	15.34 (0.434)
19 (483)	6.03 (0.171)	14.43 (0.409)
18 (457)	5.46 (0.155)	13.52 (0.383)
17 (432)	4.88 (0.138)	12.61 (0.357)
16 (406)	4.30 (0.122)	11.69 (0.331)
15 (381)	3.70 (0.105)	10.76 (0.305)
14 (356)	3.10 (0.088)	9.83 (0.278)
13 (330)	2.49 (0.071)	8.90 (0.252)
12 (305)	1.88 (0.053)	7.96 (0.225)
11 (279)	1.26 (0.036)	7.02 (0.199)
10 (254)	0.63 (0.018)	6.07 (0.172)
9 (229)	0.00	5.12 (0.145)
8 (203)	0.00	4.55 (0.129)
7 (178)	0.00	3.99 (0.113)
6 (152)	Stone	3.42 (0.097)
5 (127)	Foundation	2.85 (0.081)
4 (102)		2.28 (0.064)
3 (76)		1.71 (0.048)
2 (51)		1.14 (0.032)
1 (25)		0.56 (0.016)

NOTE: Add 0.56 ft³ (0.016 m³) of storage for each additional inch (25 mm) of stone foundation.
Contact StormTech for cumulative volume spreadsheets in digital format.

StormTech MC-3500 Chamber

Designed to meet the most stringent industry performance standards for superior structural integrity while providing designers with a cost-effective method to save valuable land and protect water resources. The StormTech system is designed primarily to be used under parking lots thus maximizing land usage for commercial and municipal applications.



StormTech MC-3500 Chamber (not to scale)

Nominal Chamber Specifications

Size (L x W x H)	90" (2286 mm) x 77" (1956 mm) x 45" (1143 mm)
Chamber Storage	109.9 ft³ (3.11 m³)
Min. Installed Storage*	178.9 ft³ (5.06 m³)
Weight	134 lbs (60.8 kg)

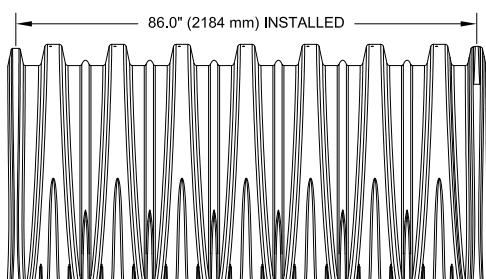
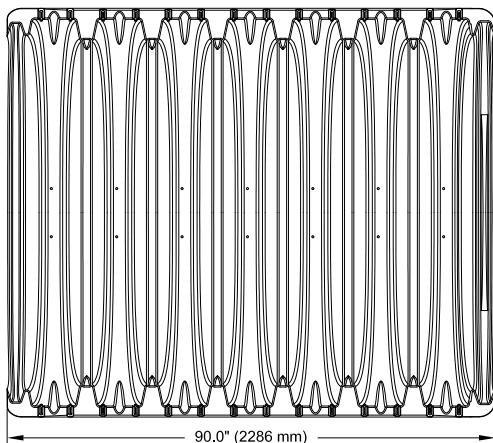
* This assumes a minimum of 12" (305 mm) of stone above, 9" (229 mm) of stone below chambers, 9" (229 mm) of row spacing, and 40% stone porosity.

Shipping

15 chambers/pallet

7 end caps/pallet

7 pallets/truck

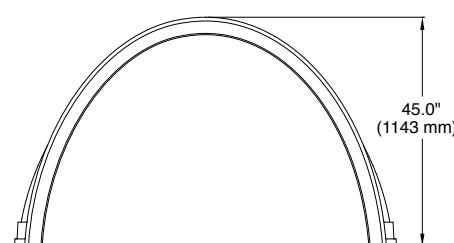
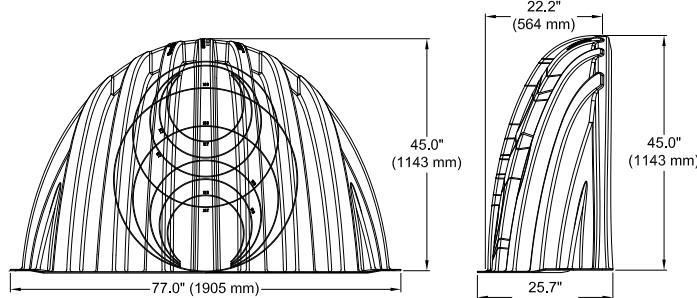


StormTech MC-3500 End Cap (not to scale)

Nominal End Cap Specifications

Size (L x W x H)	25.7" (653 mm) x 75" (1905 mm) x 45" (1143 mm)
End Cap Storage	14.9 ft³ (0.42 m³)
Min. Installed Storage*	46.0 ft³ (1.30 m³)
Weight	49 lbs (22.2 kg)

* This assumes a minimum of 12" (305mm) of stone above, 9" (229 mm) of stone below, 9" (229 mm) row spacing, 6" (152 mm) of stone perimeter, and 40% stone porosity.



Storage Volume Per Chamber/End Cap ft³ (m³)

	Bare Unit Storage ft ³ (m ³)	Chamber/End Cap and Stone Volume — Stone Foundation Depth in. (mm)			
		9 (229)	12 (305)	15 (381)	18 (457)
MC-3500 Chamber	109.9 (3.11)	178.9 (5.06)	184.0 (5.21)	189.2 (5.36)	194.3 (5.5)
MC-3500 End Cap	14.9 (0.42)	46.0 (1.33)	47.7 (1.35)	49.4 (1.40)	51.1 (1.45)

NOTE: Assumes 40% porosity for the stone plus the chamber/end cap volume. End Cap volume assumes 6" (152mm) stone perimeter.

Amount of Stone Per Chamber

	Stone Foundation Depth			
	9 in.	12 in.	15 in.	18 in.
MC-3500	9.1 (6.4)	9.7 (6.9)	10.4 (7.3)	11.1 (7.8)
End Cap	4.1 (2.9)	4.3 (3.0)	4.5 (3.2)	4.7 (3.3)
METRIC kg (m ³)	229 mm	305 mm	381 mm	457 mm
MC-3500	8220 (4.9)	8831 (5.3)	9443 (5.6)	10054 (6.0)
End Cap	3699 (2.2)	3900 (2.3)	4100 (2.4)	4301 (2.6)

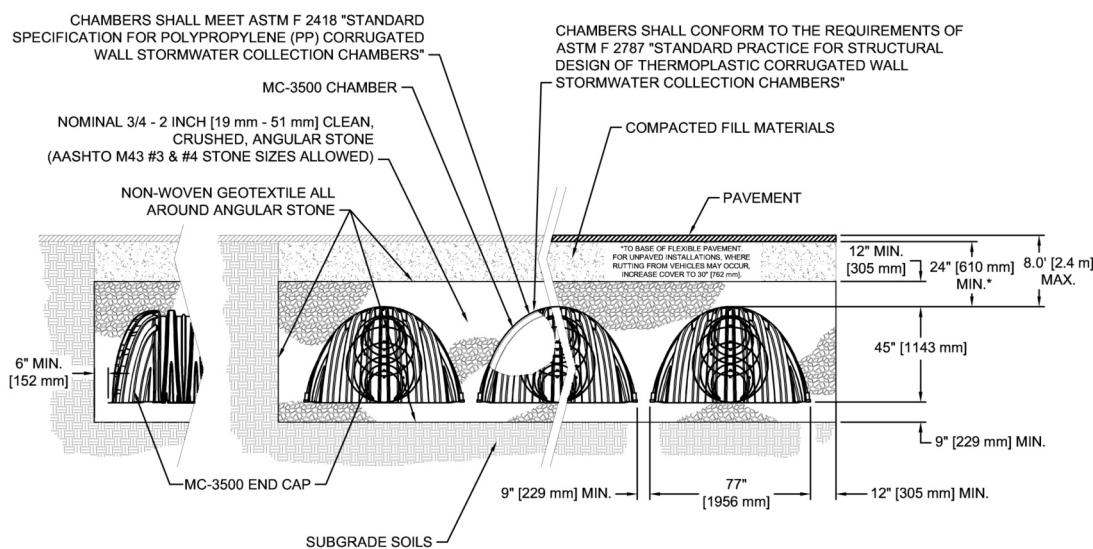
NOTE: Assumes 12" (305 mm) of stone above, and 9" (229 mm) row spacing, and 6" (152mm) of perimeter stone in front of end caps.

Volume of Excavation Per Chamber/End Cap in yd³ (m³)

	Stone Foundation Depth in. (mm)			
	9 (229)	12 (305)	15 (381)	18 (457)
MC-3500	12.4 (9.5)	12.8 (9.8)	13.3 (10.2)	13.8 (10.5)
End Cap	4.1 (3.1)	4.2 (3.2)	4.4 (3.3)	4.5 (3.5)

NOTE: Assumes 9" (229 mm) of separation between chamber rows, 6" (152 mm) of perimeter in front of end caps, and 24" (610 mm) of cover. The volume of excavation will vary as depth of cover increases.

General Cross Section



NOTES:

1. THIS CROSS SECTION PROVIDES GENERAL INFORMATION FOR THE MC-3500 CHAMBER. STORMTECH MC-3500 CHAMBERS MUST BE DESIGNED AND INSTALLED IN ACCORDANCE WITH THE MC-3500 DESIGN MANUAL AND MC-3500 CONSTRUCTION GUIDE.
2. PROPERLY INSTALLED MC-3500 CHAMBERS PROVIDE THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS FOR EARTH AND LIVE LOADS WITH CONSIDERATION FOR IMPACT AND MULTIPLE PRESENCES.
3. PERIMETER STONE MUST ALWAYS BE BROUGHT UP EVENLY WITH BACKFILL OF BED. PERIMETER STONE MUST EXTEND HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH STRAIGHT OR SLOPED SIDEWALLS.



A division of

70 Inwood Road, Suite 3 | Rocky Hill | Connecticut | 06067
860.529.8188 | 888.892.2694 | fax 866.328.8401 | fax 860-529-8040 | www.stormtech.com

ADS "Terms and Conditions of Sale" are available on the ADS website, www.ads-pipe.com.

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S150909 03/2014



Printed on recycled paper



Appendix J – Background Information

Plan & Profile – Victor Street, Oliver Mangione McCalla, Dwg 83-3638-1 to 6. (8.5x11 Reduction)

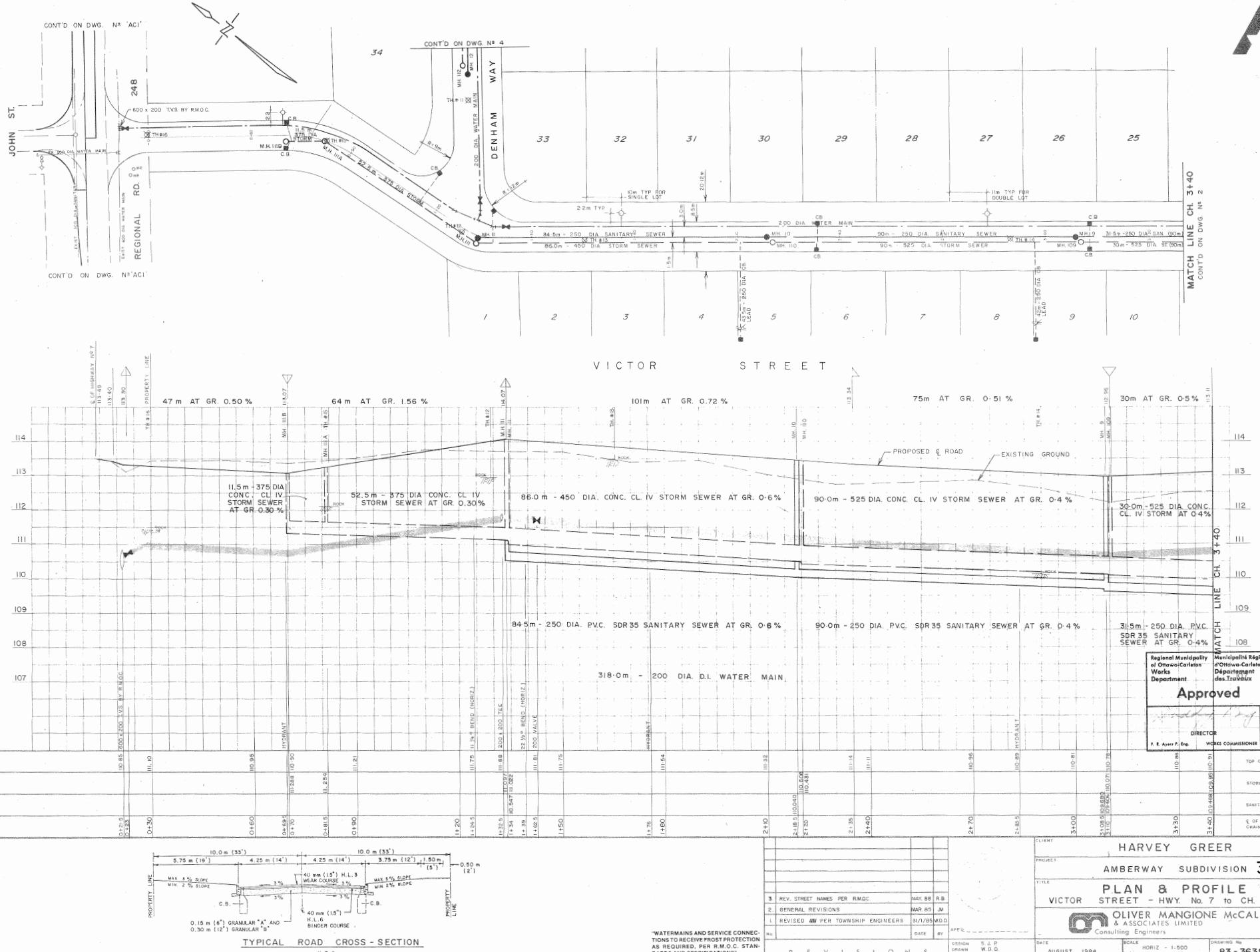
Grading Plan, Oliver Mangione McCalla, Dwg 83-3638-GR1. (8.5x11 Reduction)

Grade Control Plan, UMA, Dwg G1 (8.5x11 Reduction)

Savage Drive, Kostuch Eng. Dwg 5, 6, 8 (8.5x11 Reductions)

Site Services Plan – Amber Terrace, McIntosh Perry, Dwg C1.2. (8.5x11 Reduction)

Plan & Profile – Hazeldean Road Widening, McCormick Rankin. Dwg 022. (8.5x11 Reduction)



MATCH LINE CH. 3+40

Approved	
<i>[Signature]</i>	Date <i>[Signature]</i>

DIRECTOR
F. E. Ayers, P. Eng. **WORKS COMMISSIONER**

161

TOP OF WATER MAIN

156

STORM SEWER INVERT

888

SANITARY SEWER INVERT

END OF ROAD

CHAINAGE

WENGER

VEY GREER

NAME - SUBMISSION 3330-1

WAY SUBDIVISION 5230-1

8 BROUILLÉ

HWY. No. 3 to CH. 3 & 42

- HWY. No. 7 to CH. 3 + 40

R MANGIONE McCALLA
SOLICITED ATTORNEYS

U.S. STATES LIMITED
Ottawa

DRAWING No. 100-1000 REV. A

HORIZ - 1:500
VERT - 1:500

VERT. \geq 1.00

Signatures of the author and editor



REG. MUN. OF OTTAWA-CARLETON

ENGINEERING DIVISION

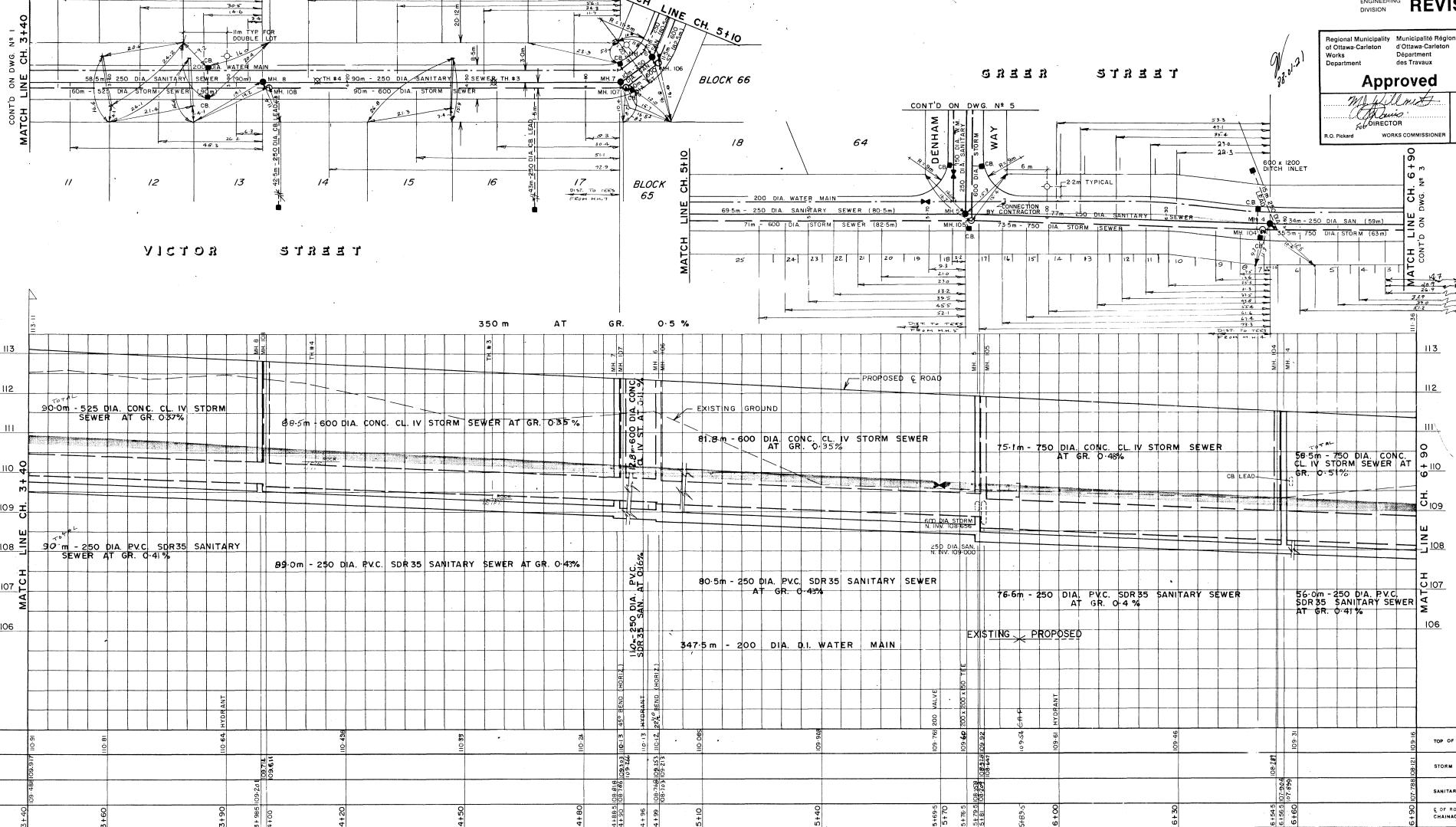
REVISED



Regional Municipality of Ottawa-Carleton
Works Department

[Signature]
Approved
R.O. Pickard
WATER WORKS

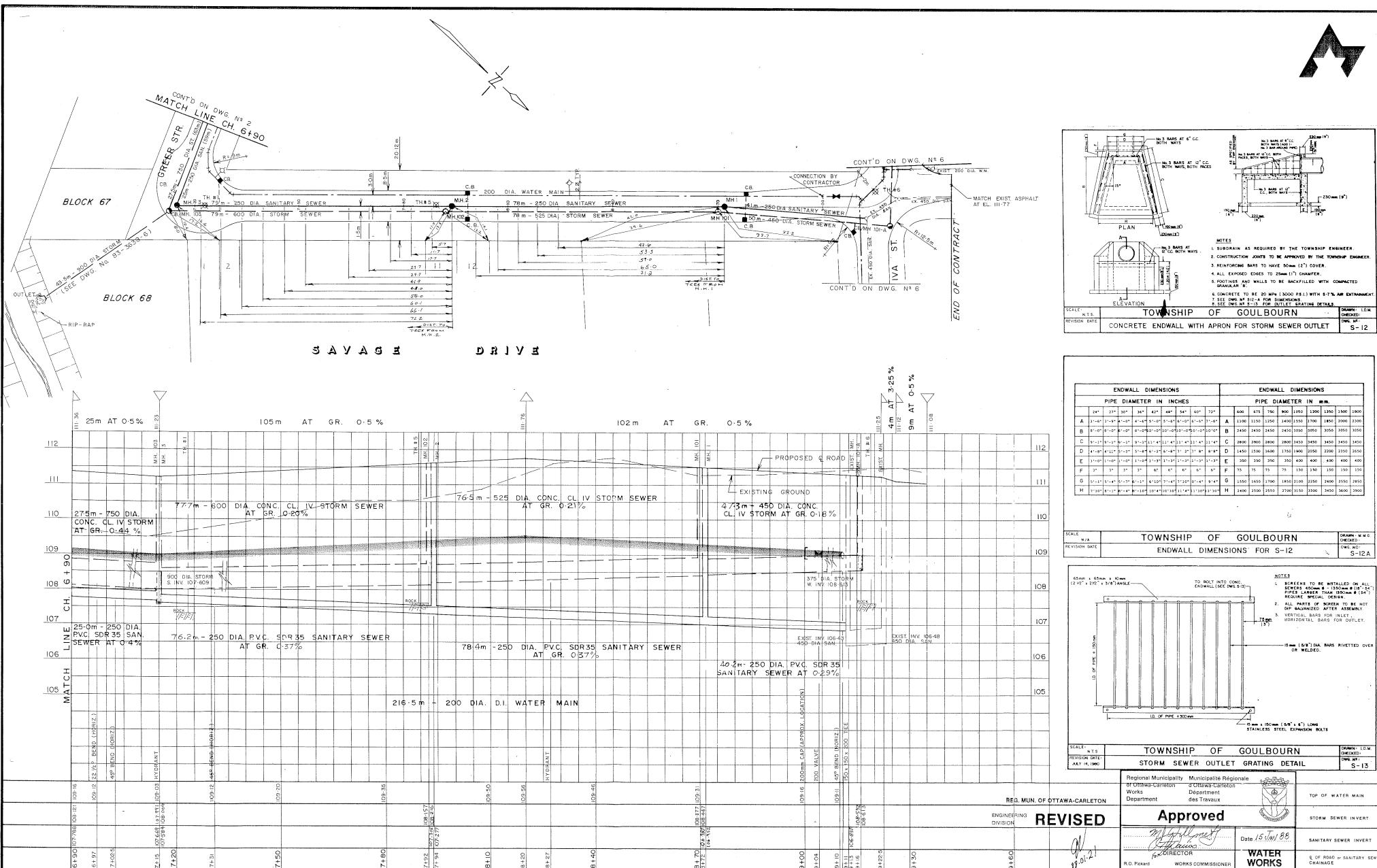
Date 15.Jul.88

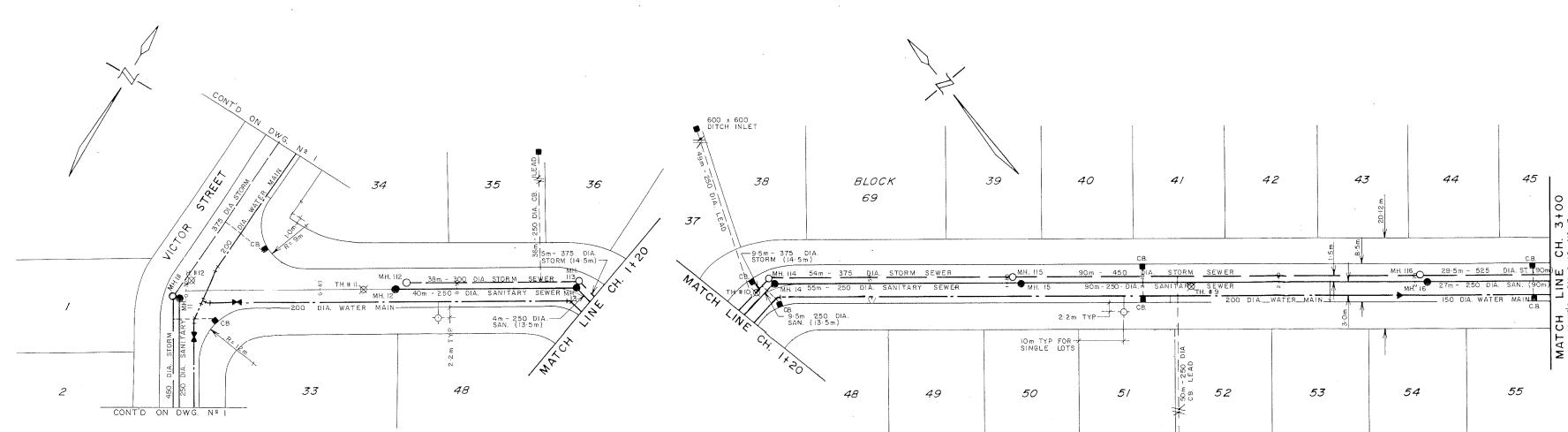


8. REV. PER R.M.O.C.	10/0/88 M.W.
7. STREET NAME CHANGE AS PER TWP	3/0/87 G.U.
6. A.S. ROUTE	1/2/87 E.S.
5. LOT NUMBERS REV AS PER DRAFT M-PLAN	3/9/85 M.J.M.
4. REV BLOCKLAND NUMBERS & DITCH INLET	1/6/85 W.D.D.
3. ADDED LOTS & CB TO BLOCKS 65 & 68	2/3/85 W.D.D.
2. GENERAL REVISIONS	MAR 85 J.M.
I. REV. AS PER TOWNSHIP ENGINEERS	3/1/85 W.D.D.
Re. APP'D	1/22/85 E.S.
DATE	10/0/88

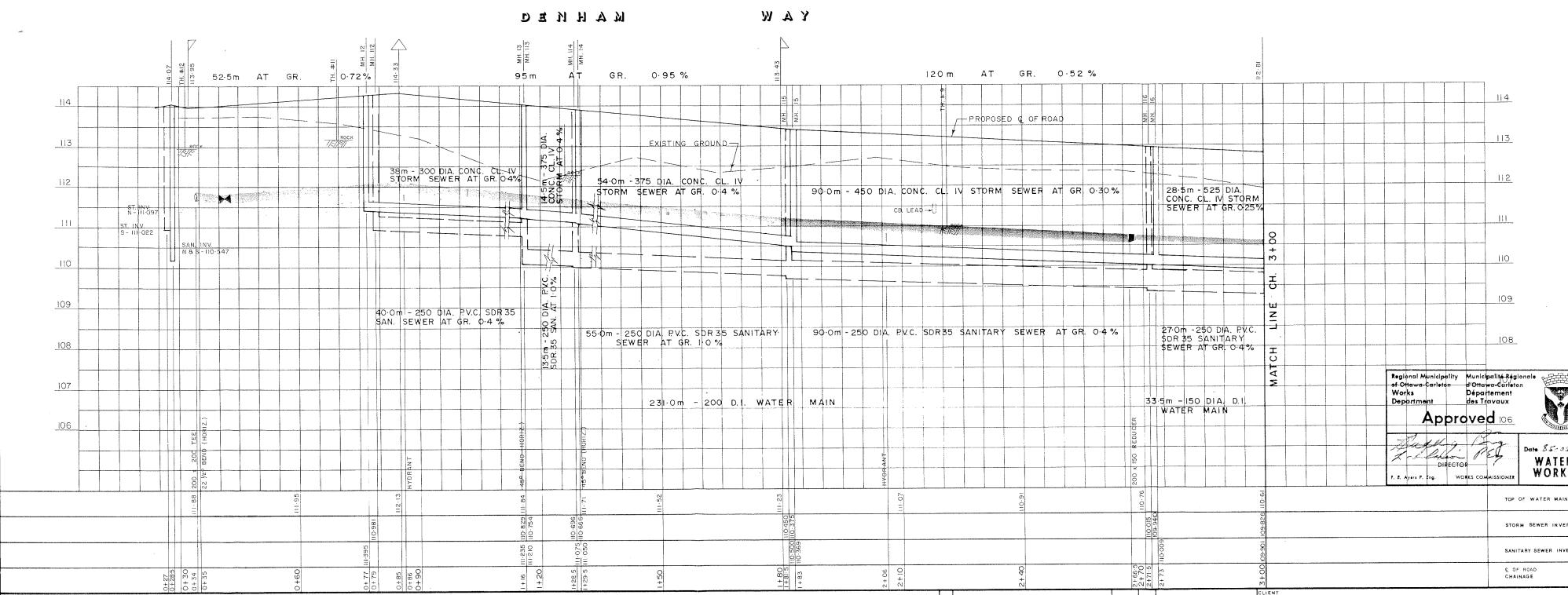
REVISIONS

CLIENT	HARVEY GREER 3230-2
PROJECT	AMBERWAY SUBDIVISION
TITLE	PLAN & PROFILE
VICTOR & GREER STR. - CH. 3+40 to CH. 6+90	
OLIVER MANGIONE McCALLA & ASSOCIATES LIMITED Consulting Engineers	Ottawa
DESIGN S.J.P. DRAWN W.D.D. CHECKED J.N.S.	DATE AUGUST, 1984
SCALE HORIZ. - 1:500 VERT. - 1:50	DRAWING NO. 83-3638-2
REV. 7	





MATCH LINE CH 3100
CONT'D ON DWG. N° 5



Regional Municipality of Ottawa-Carleton
Municipalité Régionale de l'Outaouais-Carleton
Works Department
Département des Travaux
Approved 106
F. E. Ayres P. Eng. WATER WORKS
Date 85-12-07
Signature

TOP OF WATER MAIN

STORM SEWER INVERT

SANITARY SEWER INVERT

E. OF ROAD CHANAGE

HARVEY GREER

AMBERWAY SUBDIVISION 3230-4

PLAN & PROFILE
DENHAM WAY - VICTOR ST to CH. 3 + 00

OLIVER MANGIONE McCALLA
& ASSOCIATES LIMITED
Consulting Engineers

Ottawa

3. REV. STREET NAMES PER R.M.O.C.	MAY 88 R.B.
2. GENERAL REVISIONS	MAR 85 M
1. REV. PER TOWNSHIP ENGINEERS	U/2/85 W.D.
No.	DATE BY APP'D.

R E V I S I O N S

DESIGN S. J. P.
DRAWN W. D.
CHECKED J. N. S.

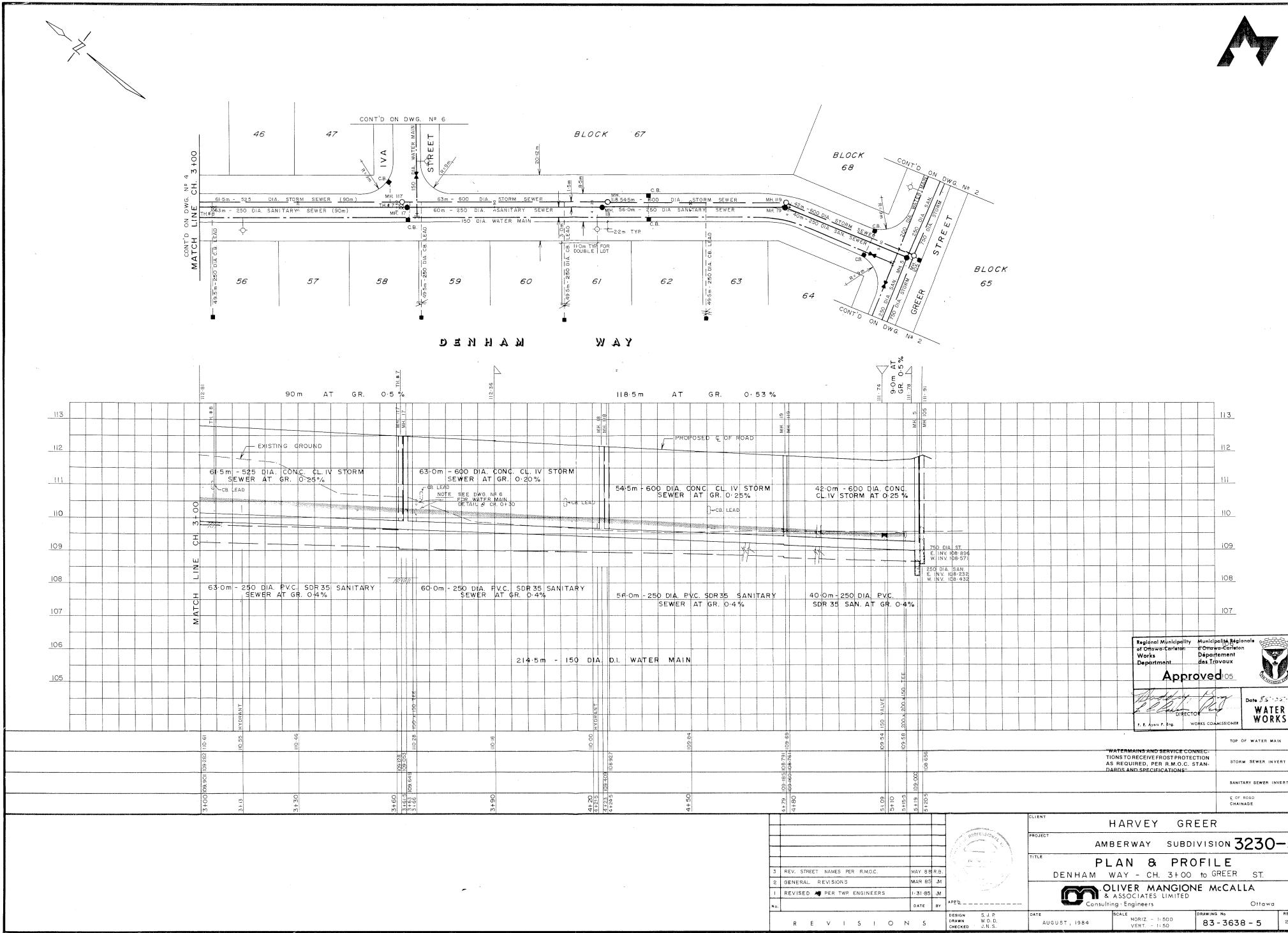
DATE AUGUST, 1984

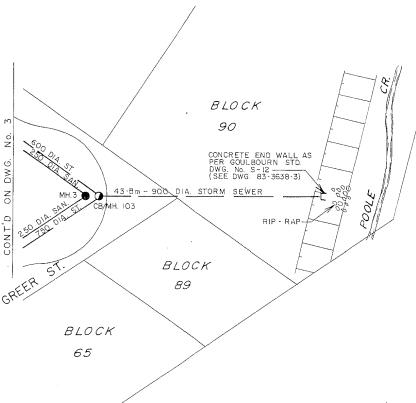
SCALE NORIZ - 1:500
VERT - 1:50

DRAWING NO. 83-3638-4

REV. 2

"WATERMAINS AND SERVICE CONNECTIONS TO RECEIVE FROST PROTECTION AS REQUIRED, PER R.M.O.C. STANDARDS AND SPECIFICATIONS"





CONTD ON DWG. NO. 3

4.5m

8.5m WIDE ROAD

3.06

CB TOP
III-00

150 mm DIA. WATERMAIN

70m x 3.75 DIA. STORM SEWER

CB TOP
III-00

CB TOP
III-00

3.06

WATER MAIN TO BE RAISED ABOVE
STORM SEWER & INSULATED
PER RMOC STD. W.3.23

MATCH EXISTING ASPHALT
AT ELEV. III-77

CONNECT TO EXISTING
BY CONTRACTOR

END OF CONTRACT

SAVAGE

LOCK

67

2.5m TYP

100 x 1200

TGH INLET

C.B.

SUS. DIA. STEM

150 DIA. W.M.

150 DIA. STEM

150 DIA. W.M.

150 DIA. STEM

150 DIA. W.M.

150 DIA. STEM

150 DIA. W.M.

CONT'D ON DWG. N° 5

WAY

DENHAM

47

CONT'D ON DWG. N° 5

VA STREET

TOP OF WATER MAIN
STORM SEWER INVERT
SANITARY SEWER INVERT
%

ER

VISION 3230-6

FILE
Y TO CH 1496
POOLE CREEK

McCALLA

Ottawa

DRAWING No. 84-3638-6 REV.

GRADE CONTROL REQUIREMENTS

N. T. S.

EXIST. HOUSE
 TOP OF HZ 206
 12/11/98

EXIST. HOUSE
 TOP OF HZ 206
 12/12/98

5.0 m DRAINAGE EASEMENT

This image shows an architectural drawing of a building footprint and foundation plan. The footprint is a rectangle divided into two sections: 'EXIST' (top) and 'NEW' (bottom). A north arrow points upwards. Foundation details include 'TYP 13-845' and 'TYP 13-846'. A dimension line indicates a width of 10'-0". The foundation plan shows 'GS TOP H2 945' and 'CB TOP H2 945'. A dimension line indicates a height of 11'-0". A note 'X (13-07)' is present. A large rectangular box at the bottom contains the text 'RECORD DRAWING' and 'DATE: 13/12/97'. A north arrow is also present in the bottom right corner.

This figure is a detailed site plan for the 'VICTOR' project, showing property boundaries, building footprints, and various utility and drainage easements. The plan includes labels for 'TH B' and 'TH C' roads, as well as specific elevations like 'ROCK ELEV 113-18' and '113-95'. A legend indicates '2.4m DRAINAGE EASEMENT (TYPICAL)'. The plan shows numerous buildings labeled with numbers such as 34, 33, 32, 31, 30, 29, 28, 27, 26, 25, 24, 23, and 22. It also shows several utility poles and associated labels like 'CB TOP HS-900' and 'CB TOP 113-95'. Elevation points are marked throughout the plan, including 'ROCK ELEV 113-18' at TH B and '113-95' at CB TOP HS-900. A legend indicates '2.4m DRAINAGE EASEMENT (TYPICAL)'.

NOTE

1. USE = FINISHED FIRST FL - 2'-8"
2. SEE SUBDIVISION AGREEMENT FOR PARK DEVELOPMENT.

LEGEND

- EXISTING ELEVATION
- PROPOSED ELEVATION
- PROPOSED FINISHED FIRST FLOOR ELEVATION
- ✖ PROPOSED ROAD ELEVATION
- PROPOSED CATCH BASIN
- ☒ TEST HOLE
- ◆ PROPOSED STREET LIGHT
- ▲ BUILT GRADE FLOOR ELEVATION

No.	RECORD DRAWING	STREET NAME CHANGE AS PER TWP	LOT NUMBERS REV.AS PER DRAFT M-PLAN	REV. BLOCK NUMBER & ADDED ST. LIGHTS	ADDED BYPASS & ACCESS LANE HWY. 7	REV AS PER TOWNSHIP ENGINEERS	APPROVED
6	12/2/87 J.G.						
5		10/10/87 G.U.					
4			3/9/85 W.D.M.				
3				7/6/85 W.D.D.			
2					WAD2056 M		
1						4/2/85 W.D.D.	

CLIENT HARVEY GREER
PROJECT AMBERWAY SUBDIVISION
TITLE GRADING PLAN
OLIVER MANGIONE McCALLA Consulting Engineers
 Ottawa, Ontario

GRADE CONTROL-TYPICAL FRONT AND REAR LOT DRAINAGE

N. T. S.

NOTE

- NOTE**

1. USE = FINISHED FIRST FL - 2-84
2. SEE SUBDIVISION AGREEMENT
FOR PARK DEVELOPMENT.

14-53 EXISTING ELEVATION
14-53 PROPOSED ELEVATION

LEGEND

- EXISTING ELEVATION
02/2012 ELEVATION
PROPOSED ELEVATION

PROPOSED FINISHED FIRST FLOOR ELEVATION

PROPOSED ROAD ELEVATION

PROPOSED CATCH BASIN

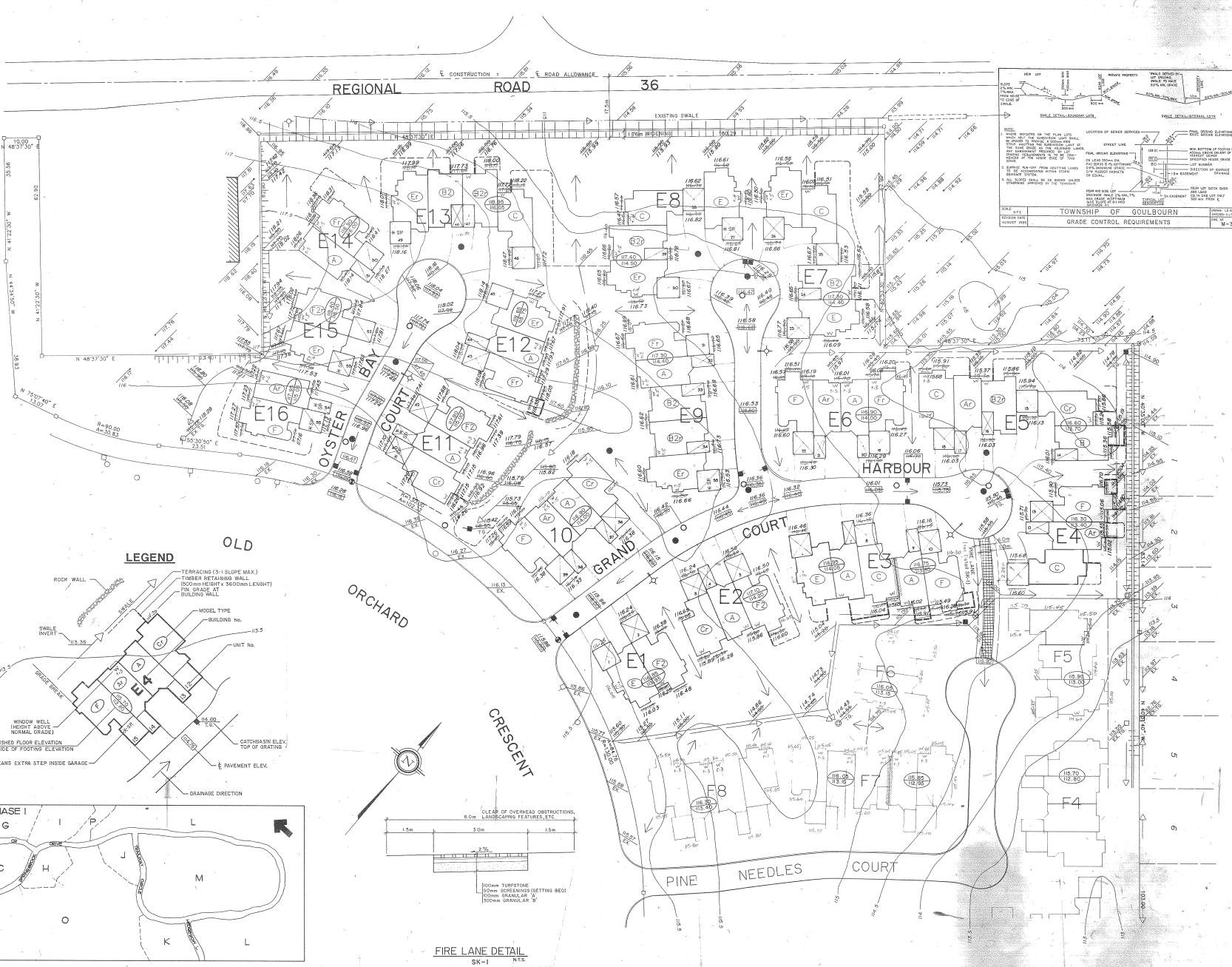
TEST HOLE

PROPOSED STREET LIGHT

RS BUILT GARAGE FLOOR ELEVATION

6	RECORD DRAWINGS	12/14/87	G-4
5	STREET NAME CHANGE AS PER TWP	10/10/87	G.U.
4	LOT NUMBERS REV.AS PER DRAFT M-PLAN	3/9/85	M.M.
	REV. BLOCK NUMBER & ADDED ST LIGHTS	10/6/85	W.D.
2	ADDED BYPASS & ACCESS LANE HWY. 7	10/25/85	S.M.
1	REV AS PER TOWNSHIP ENGINEERS	4/2/85	W.D.
No.		DATE	APPROVED
	R E V I S I O N S	DESIGN DRAWN	

CLIENT	HARVEY GREER	
PROJECT	AMBERWAY SUBDIVISION	
TITLE	GRADING PLAN	
 OLIVER MANGIONE MCCALL Consulting Engineers		Ottawa, Ontario
DATE	SEPTEMBER 1984	SCALE 1:5000
		DRAWING NO. 7-737



RECORD DRAWING

GRADING ELEVATIONS

AS BUILT ELEVATIONS
TAKEN ON NOV. 29/90
REVISED T.H. BLOCKS E5-5 E15 AND CURB A
TH. BLOCK E6
CODED FIRE LANE & DETAIL SK-1
ISSUED FOR APPROVAL
revision

uma UMA Engineering Ltd.
Engineers & Planners

[View all posts by admin](#) | [View all posts in category](#)

AMBERWOOD VILLAGE

NCC GRA
Gradin
ID #9

#350

014
RB
Amber

R CO
wood v

File
RT
age pr

#62

date: JANUARY 1989 scale:

R.G.V. 5772-003
checked drug no. 1

— ZERO

10. The following table gives the number of hours per week spent by students in various activities.

NCC #35

1

File #6

62

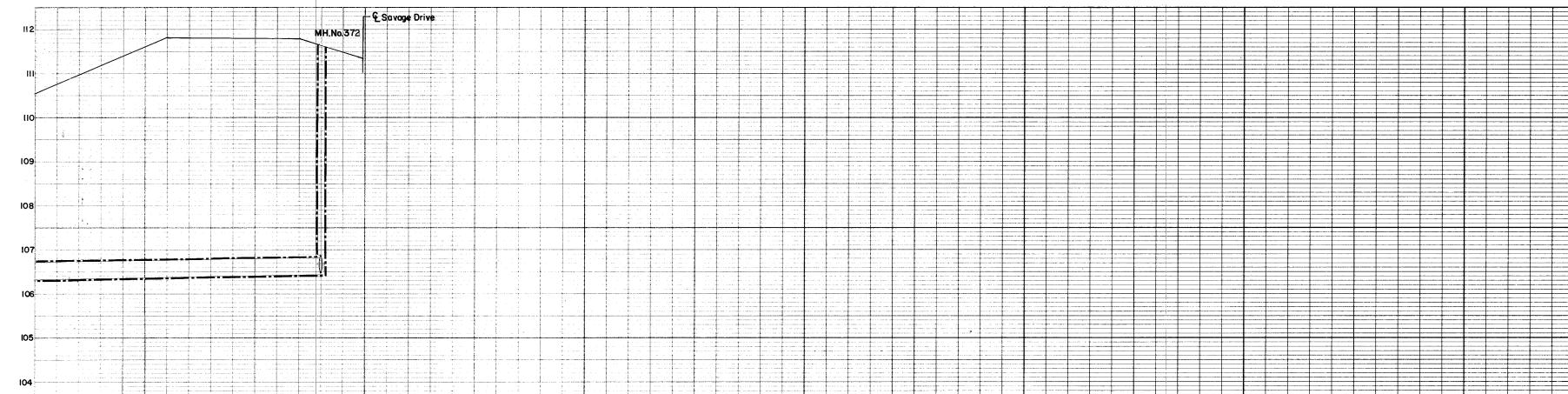
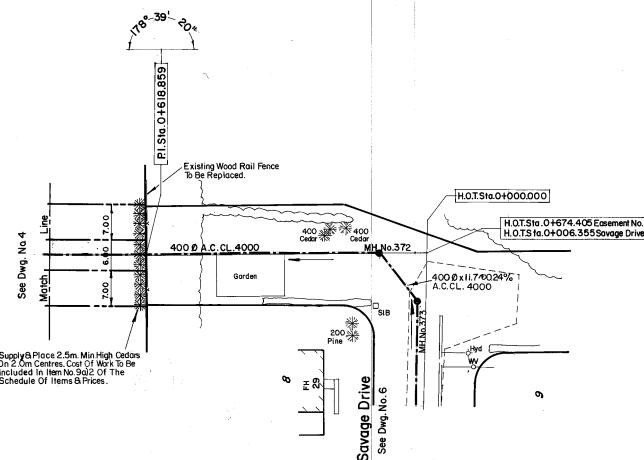
100

METRIC

G0-245

All Dimensions Are In Millimetres And/Or Metres
Unless Shown Otherwise.

All Underground Utilities Are Approximate. Contractor
Is Required To Notify The Utility Before Excavating.



AS BUILT

EXISTING GRADE	I1150	III180	III1800	III1350									EXISTING GRADE
WATER MAIN TOP OF PIPE ELEVATION													WATER MAIN TOP OF PIPE ELEVATION
SANITARY SEWER INVERT ELEVATION	400 0	X 119.8	± 0.20%	116.476									SANITARY SEWER INVERT ELEVATION
STORM SEWER INVERT ELEVATION													STORM SEWER INVERT ELEVATION
CHAINAGE	O+600	O+625	O+550	+665.027	O+7350								CHAINAGE

Scale (Metric): 0 5 10 20m HORIZONTAL
0 0.5 1 2m VERTICAL

Design D.M. CHKD M.J.H.
DRAWN CHKD
E.C. D.M.
APPROVED
W.R. No. 949

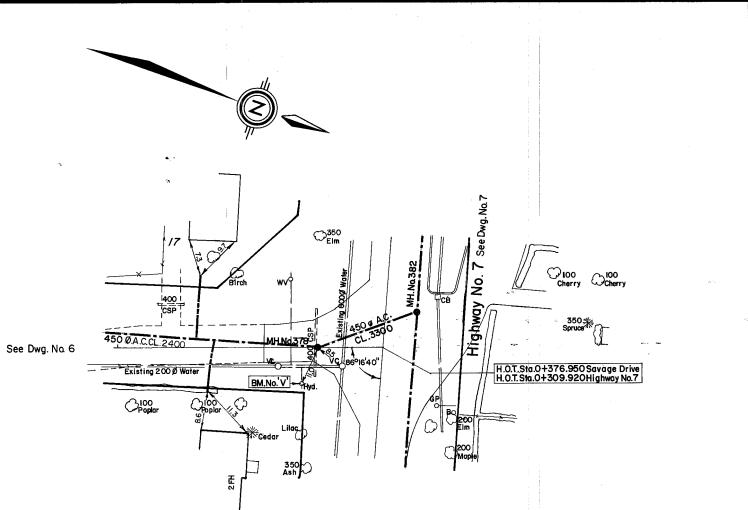
KOSTUCH ENGINEERING LIMITED
CONSULTING ENGINEERS
BROCKVILLE • OTTAWA • BELLEVILLE • CORNWALL

Ministry Of The Environment
Sewage Works Project No. 1-0127
Township Of Goulbourn
Stittsville Sanitary Sewers

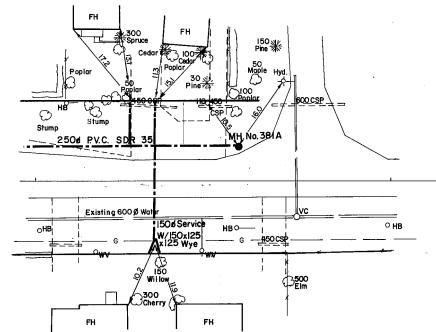
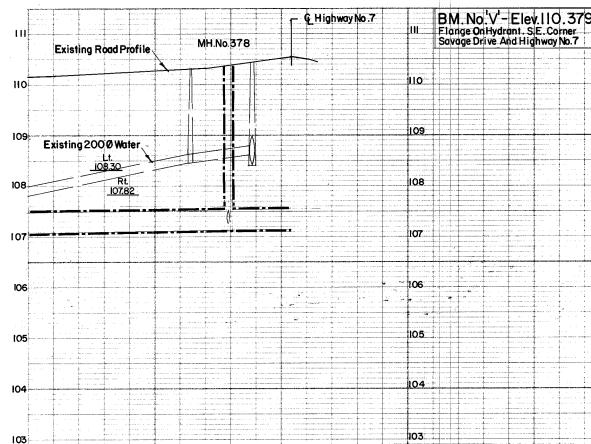
EASEMENT No. 6
STA. O+600 to STA. O+675

DATE DRAWN
MAY 1, 1978
CONT. NO.
6
DRAWING NO.
5
REV. NO.
-

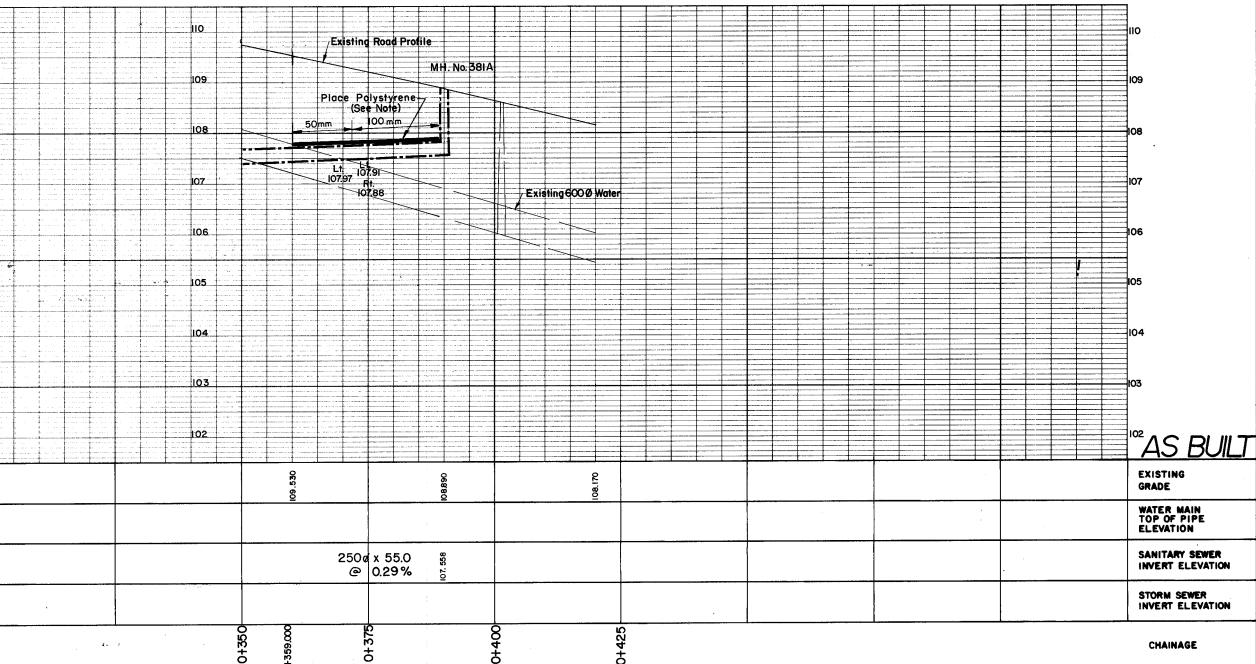
G0-245



SAVAGE DRIVE



HIGHWAY No.7



T.Mc	Feb 18/82	AS BUILT	
1	EC 22 [initials]	MH 381A ADDED	
No.	BY	DATE	REVISION

SCALE (METRIC)			DESIGN	CHKD
5	10	20m	D.M.	M.J
HORIZONTAL			E.C.	CHKD
0.5	1	2m	APPROVED	
VERTICAL			W. R. No.	949



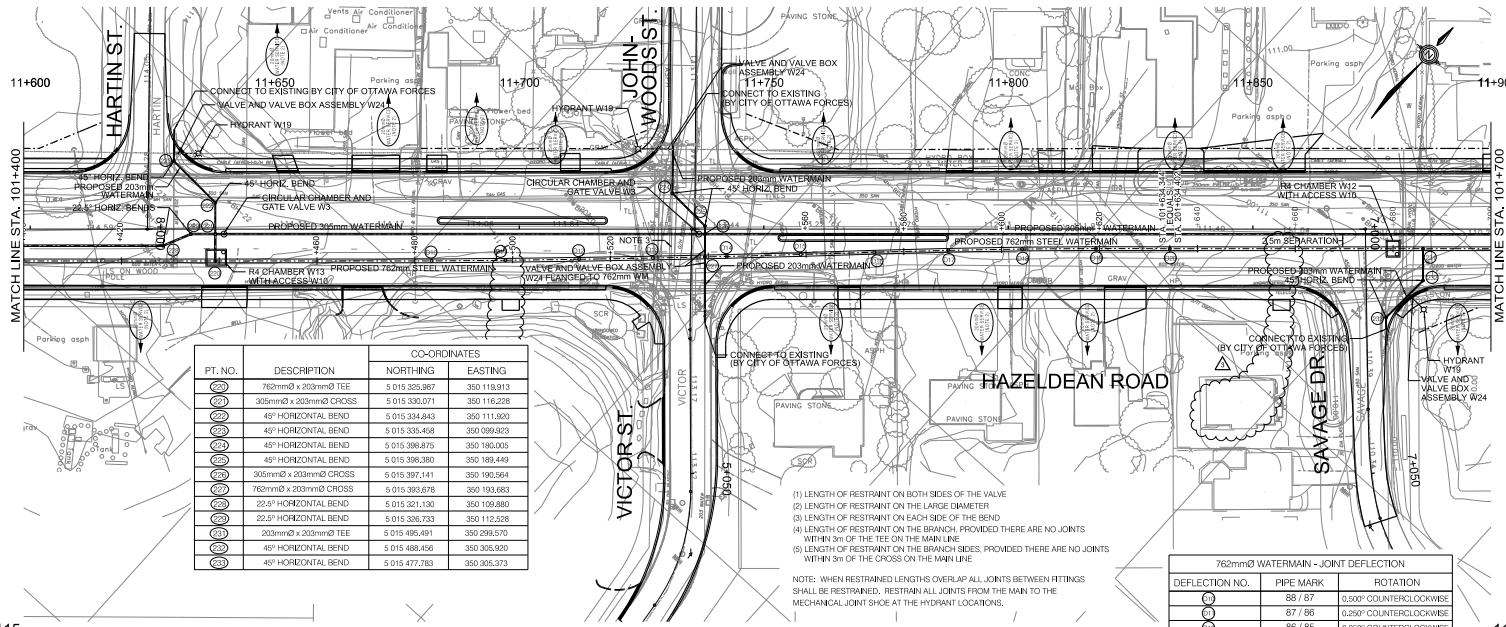
KOSTUCH ENGINEERING LIMITED
CONSULTING ENGINEERS
BROCKVILLE - OTTAWA - BELLEVILLE - CORNWALL



Ministry Of The Environment
Sewage Works Project No. 1-0127
Township Of Goulbourn
Stittsville Sanitary Sewers

SAVAGE DRIVE
STA. 0+325 to STA. 0+377
HIGHWAY No. 7
STA. 0+350 to STA. 0+425

DATE DRAWN	
MAY 1, 1980	
CONT. No.	
6	
DRAWING No.	REV. No.
8	-



HAZELDEAN ROAD WIDENING
100m EAST OF CARP ROAD TO
100m WEST OF IBER ROAD

Contract No. Dwg. No.
ISBN-5044 021
 Sheet 22 of 148
 Asset No.
 Asset Group: **ISB**
 Desc: **JZ/DP** Chk/**X** PH/**X**
 Desc: **MS** Chk/**X** PH
 Utility Circ. No.:
 Const. Inspector:
 Scale: 
 HORIZONTAL

NOTE:
The location of utilities is approximate only. The exact location should be determined by consulting the individual authorities and utility companies.

REVISIONS		The contractor shall prove the location of existing and shall be responsible for adequate protection from damage.	
No.	Description	By	Date
	ISSUED FOR REVIEW	P.H.	24/07/2020
	ISSUED FOR TENDER	P.H.	11/08/2020
	ISSUED FOR CONSTRUCTION	P.H.	26/11/2020

REVISIONS PER CITY COMMENTS P.M. 13/01/20
REVISIONS PER CITY COMMITMENTS AND REALIGNMENT M&B 09/01/20

THESE DESIGN DOCUMENTS ARE PREPARED SOLELY FOR THE USE BY THE PARTY WITH WHOM THE DESIGN PROFESSIONAL HAS ENTERED INTO A CONTRACT AND

THESE ARE NOT REPRESENTATIONS OF ANY KIND MADE BY THE DESIGN PROFESSIONAL TO ANY PARTY WITH WHOM THE DESIGN PROFESSIONAL HAS NOT ENTERED INTO A CONTRACT		AS-BUILT	
REVISIONS	No.	Description	By Date
		REISSUED FOR CONSTRUCTION	M.B. 07/05/20
		762mm/305mm/203mm WATERMAIN DESIGN CHANGE	M.B. 08/09/20

NOTE:
1. FOR GENERAL NOTES, SEE DWG. NO. ISB09-5044-017

1. FOR GENERAL NOTES SEE DWG. NO. ISB90-5044-017
2. WATER SERVICE TO COME FROM 305mm² DISTRIBUTION MAIN.
3. A PORTION OF THE EXISTING JOHNSON STREET 203mm² BRANCH WATERMAIN MUST BE REMOVED PRIOR TO CONSTRUCTION OF THE NEW LINE. THIS LINE MUST BE STAGED SUCH THAT THE MARTIN STREET CONNECTION REMAINS UNOBSTRUCTED UNTIL THE EXISTING JOHNSON STREET BRANCH IS DISCONNECTED.
4. POSSIBLE ASBESTOS PIPE USED FOR EXISTING SANITARY SEWER.
5. FOR THE PURPOSES OF CLARITY THE DRAWING REVISIONS AND COMMENTS WITHIN THE TRIANGLE HAVE BEEN REMOVED FROM THIS DRAWING.

RESTRAINT TABLE			
203mmØ WATERMAIN - SAVAGE DRIVE			
STATION	FITTING TYPE	RESTRAINT LENGTH	
		UPPER BEND	LOWER BEND
+0000.00	762mmØ x 203mmØ TEE		3 (4)
+0065.52	203mmØ x 45°VB		3 (3)
+0140.60	203mmØ x 120mmØ TEE		(4)
+0174.74	203mmØ x 22.5°VB		6 (3)
+0164.40	203mmØ x 22.5°VB		6 (3)
+0172.00	203mmØ x 45°VB		3 (3)

RESTRAINT TABLE			
203mmØ WATERMAIN - HARTIN STREET		RESTRAINT LENGTH	
STATION	FITTING TYPE	UPPER BEND	LOWER BEND
+000.00	762mmØ x 203mmØ TEE		3 (4)
+998.95	203mmØ VALVE		9 (1)
+994.28	203mmØ x 355mmØ CROSS		3 (5)
+998.15	203mmØ x 40° HB		3 (3)

+976,14	203mmØ x 45° HB	3 (3)
+974,53	203mmØ x 152mmØ TEE	(4)
RESTRAINT TABLE		
203mmØ WATERMAN - JOHNWOODS & VICTOR STREET		
STATION	FITTING TYPE	RESTRAINT LENGTH
		UPPER BEND / LOWER BEND
+976,90	203mmØ x 152mmØ TEE	(4)
+965,89	203mmØ x 45° HB	3 (3)
+965,35	203mmØ x 45° HB	3 (3)

+997.00	203mm ² x 305mm ² CROSS	3 (5)
+998.50	203mm ² VALVE	9 (1)
+000.00	762mm ² x 203mm ² CROSS	3 (5)
+001.50	203mm ² VALVE	9 (1)
+002.70	203mm ² x 22.5° VB	6 (3)
+003.98	203mm ² x 22.5° VB	6 (3)
+008.61	203mm ² x 22.5° VB	6 (3)
+012.12	203mm ² x 22.5° VB	6 (3)

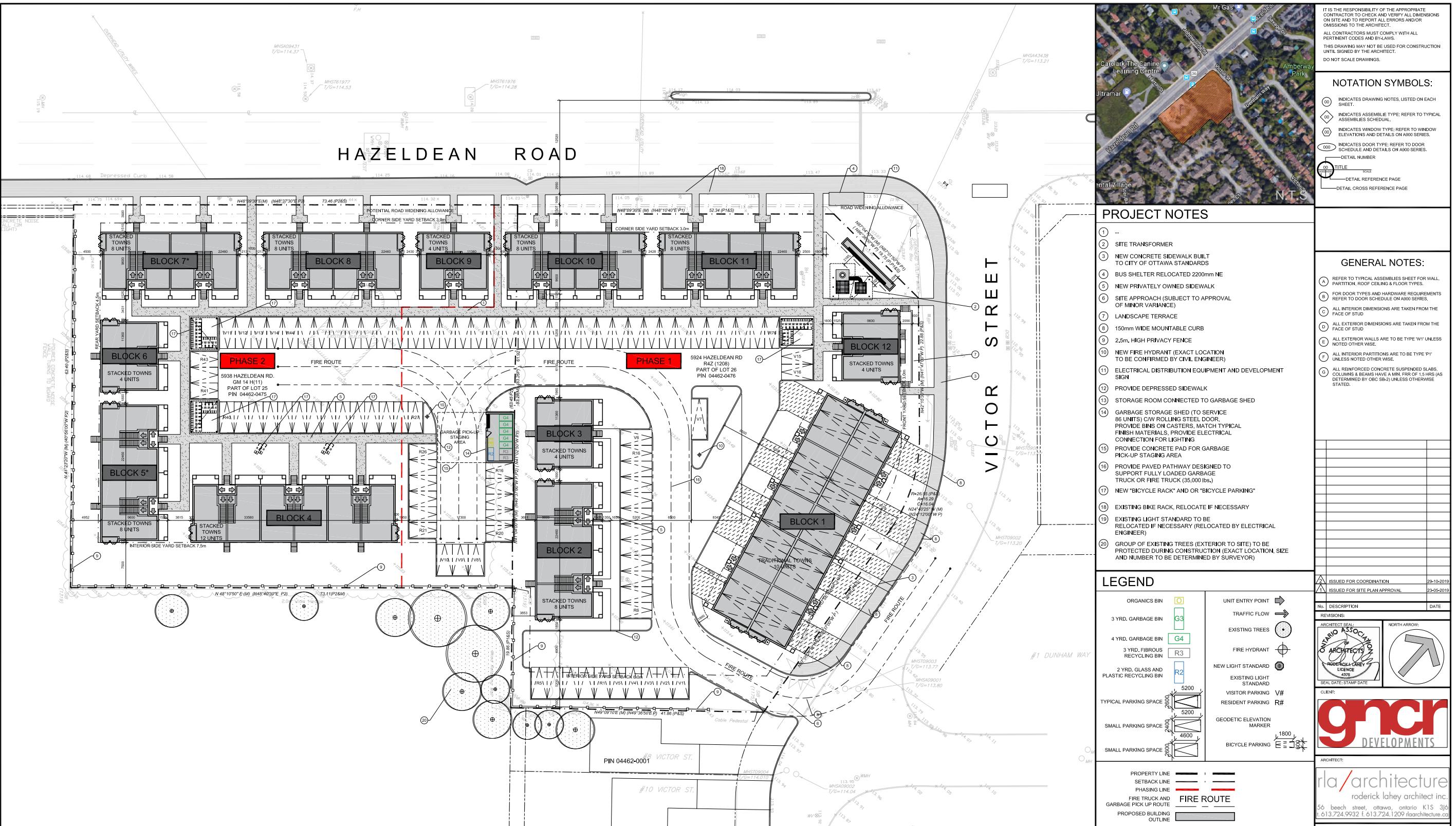
Appendix K – Drawings

Other Drawings (All 11x17 Reduction, Scale: NTS)

- Site Plan, Roderick Lahey Architect Inc. Dwg SP-0 (11x17 Reduction)
- Topographic Survey, Fairhall Moffatt Woodland, April 09, 2019 (11x17 Reduction)

Engineering Drawings (Included Separately)

- Existing Conditions and Removals Plan, Drawing C000, Rev4
- Legends and Notes, Drawing C001, Rev4
- Site Servicing Plan, Drawing C100, Rev4
- Site Servicing Tables, Drawing C100, Rev4
- Site Grading Plan, Drawing C200, Rev4
- Erosion & Sediment Control Plan, Drawing C300, Rev4
- Post-Development Storm Drainage Plan, Drawing C400, Rev4
- Detail Sheet, Drawing C700, Rev4



PROJECT DEVELOPER
GNCR DEVELOPMENTS

CIVIL ENGINEER
EXP SERVICES INC.

TRAFFIC ENGINEER
EXP SERVICES INC.

SITE INFORMATION
ZONING (5924) R4Z [1208]
MAX BUILDING HEIGHT 14.5 M.
LOT AREA 4,930.9 SQ. M.

DEVELOPMENT STATISTICS
SITE BACKSETS (5924) REQUIRED PROVIDED PARKING REQUIRED
FRONT YARD (HAZELDEAN) 3.0m 3.0m RESIDENTIAL: 1.2 PER DWELLING
CORNER SIDE YARD 3.0m VISITOR: 0.2 PER DWELLING
REAR YARD 6.0m 14.85m² TRADITIONAL TOWNS
RESIDENTIAL: 1.0 PER DWELLING
VISITOR: 0.2 PER DWELLING
PARKING PROVIDED
STACKED TOWNS RESIDENTIAL: 91 76
VISITOR: 15 16
BICYCLE: 38 44
TRADITIONAL TOWNS RESIDENTIAL: 10 18
VISITOR: 2 17
TOTAL LANDSCAPE SPACE (%) - 45.3

SITE COVERAGE
SPACE AREA (sq.m.)
BUILDING FOOTPRINT - 2,746.6
PARKING LOT - 2,889.0
SIDEWALKS - 636.5
DRIVEWAYS - 240.2
LOT AREA - 4,930.9
5924 HAZELDEAN RD. - 5938 HAZELDEAN RD. - 9,576.5
TOTAL - 4,645.6
LANDSCAPE SPACE - 3,700.7

ADDITIONAL NOTES

** 600mm DRIVE AISLES WILL BE SUBJECT TO APPROVAL OF A MINOR VARIANCE ALLOWING DRIVE AISLES NARROWER THAN 6700mm
*** WINTER SNOW STORAGE WILL NOT BE PROVIDED ON SITE. SNOW WILL BE REQUIRED TO BE TRUCKED OFF SITE AS REQUIRED.

*SNOW STORAGE WILL NOT BE PROVIDED ON SITE. SNOW WILL BE REQUIRED TO BE TRUCKED OFF SITE AS REQUIRED.

PHASE 1
STACKED: 32
TRADITIONAL TOWN: 10

PHASE 2
STACKED: 44

TRADITIONAL TOWN: 0

TOTAL: 86

PHASE 1
STACKED: 32
TRADITIONAL TOWN: 10

PHASE 2
STACKED: 44

TRADITIONAL TOWN: 0

TOTAL: 86

Konaklar Mh, Akasyali Sk,
No:26 34330
Beşiktaş İstanbul Turkey

PHONE: +90 212 212 60 60
FAX: +90 212 284 82 77

2650 QUEENSVIEW DRIVE
SUITE 100
OTTAWA, ONTARIO
K2B 8H6

PHONE: 613 688 1899

2650 QUEENSVIEW DRIVE
SUITE 100
OTTAWA, ONTARIO
K2B 8H6

PHONE: 613 688 1899

ZONING (5938) GM14 H[11]
MAX BUILDING HEIGHT 11.0 M.
LOT AREA 4,645.6 SQ. M.

K2B 1B9

DEVELOPMENT STATISTICS
SITE BACKSETS (5938) REQUIRED PROVIDED PARKING REQUIRED
FRONT YARD (HAZELDEAN) 3.0m 3.0m RESIDENTIAL: 1.2 PER DWELLING
REAR YARD 7.5m 7.5m VISITOR: 0.2 PER DWELLING
INTERIOR SIDE YARD (SW ONLY) 3.0m 3.0m TRADITIONAL TOWNS
RESIDENTIAL: 1.0 PER DWELLING
VISITOR: 0.2 PER DWELLING
PARKING PROVIDED
STACKED TOWNS RESIDENTIAL: 91 76
VISITOR: 15 16
BICYCLE: 38 44
TRADITIONAL TOWNS RESIDENTIAL: 10 18
VISITOR: 2 17
TOTAL LANDSCAPE SPACE (%) - 45.3

SITE COVERAGE
SPACE AREA (sq.m.)
BUILDING FOOTPRINT - 2,746.6
PARKING LOT - 2,889.0
SIDEWALKS - 636.5
DRIVEWAYS - 240.2
LOT AREA - 4,930.9
5924 HAZELDEAN RD. - 5938 HAZELDEAN RD. - 9,576.5
TOTAL - 4,645.6
LANDSCAPE SPACE - 3,700.7

ADDITIONAL NOTES

** 600mm DRIVE AISLES WILL BE SUBJECT TO APPROVAL OF A MINOR VARIANCE ALLOWING DRIVE AISLES NARROWER THAN 6700mm
*** WINTER SNOW STORAGE WILL NOT BE PROVIDED ON SITE. SNOW WILL BE REQUIRED TO BE TRUCKED OFF SITE AS REQUIRED.

*SNOW STORAGE WILL NOT BE PROVIDED ON SITE. SNOW WILL BE REQUIRED TO BE TRUCKED OFF SITE AS REQUIRED.

PHASE 1
STACKED: 32
TRADITIONAL TOWN: 10

PHASE 2
STACKED: 44

TRADITIONAL TOWN: 0

TOTAL: 86

3332 CARLING AVE.
OTTAWA, ONTARIO, CANADA
K2H 5A8

PHONE: 613 722 5168
FAX: 1 866 343 3942

3332 CARLING AVE.
OTTAWA, ONTARIO, CANADA
K2H 5A8

3332 CARLING AVE.
OTTAWA, ONTARIO, CANADA
K2H 5A8

SITE AREA
TOTAL SITE AREA 9,576.5 SQ. M.

RESIDENTIAL UNITS
STACKED TOWNSHOUSES: 76
TRADITIONAL TOWNSHOUSES: 10
TOTAL UNITS: 86

BUILDING STATISTICS
STACKED TOWN TYPE A - 1,038 SQFT 4 6,144 SQFT
STACKED TOWN TYPE B (2) - 1,053 SQFT 16 16,848 SQFT
STACKED TOWN TYPE C (1) - 1,311 SQFT 22 28,842 SQFT
STACKED TOWN TYPE D (2B) - 1,171 SQFT 16 18,736 SQFT

PHASING
TOTAL - 86 101,874 SQFT (9,205.2 SQM)

PHASE 1
STACKED: 32
TRADITIONAL TOWN: 10

PHASE 2
STACKED: 44

TRADITIONAL TOWN: 0

TOTAL: 86

PHONE: 613 722 5168
FAX: 1 866 343 3942

PHONE: 613 688 1899

PHONE: 613 688 1899

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PHASING
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PHASE 1
STACKED: 32
TRADITIONAL TOWN: 1

UTILITY NOTES

1. THIS DRAWING CANNOT BE ACCEPTED AS ACKNOWLEDGING ALL OF THE UNDERGROUND UTILITIES AND IT WILL BE THE RESPONSIBILITY OF THE USER TO CONTACT THE RESPECTIVE UTILITY AUTHORITIES FOR A DETAILED FIELD LOCATION.
 2. UNDERGROUND UTILITIES AS REPORTED ON THIS DRAWING, ARE NOT BASED ON AN ACTUAL "FIELD LOCATE" BY THE RESPECTIVE UTILITY AGENCIES BUT HAVE BEEN COMPILED FROM DATA OBTAINED FROM THE FOLLOWING SOURCE:
 - a) CITY OF OTTAWA PUBLIC UTILITIES REGISTRY.
 3. BEFORE CONDUCTING ANY PROBING, EXCAVATING, ETC., A FIELD LOCATION OF UNDERGROUND PLUMBING BY THE PERTINENT UTILITY AUTHORITY IS MANDATORY.

TOPOGRAPHIC SURVEY OF
PART OF LOTS 25 & 26
CONCESSION 11

GEOGRAPHIC TOWNSHIP OF

**GOULBOURN
CITY OF OTTAWA**

SCALE 1 : 250

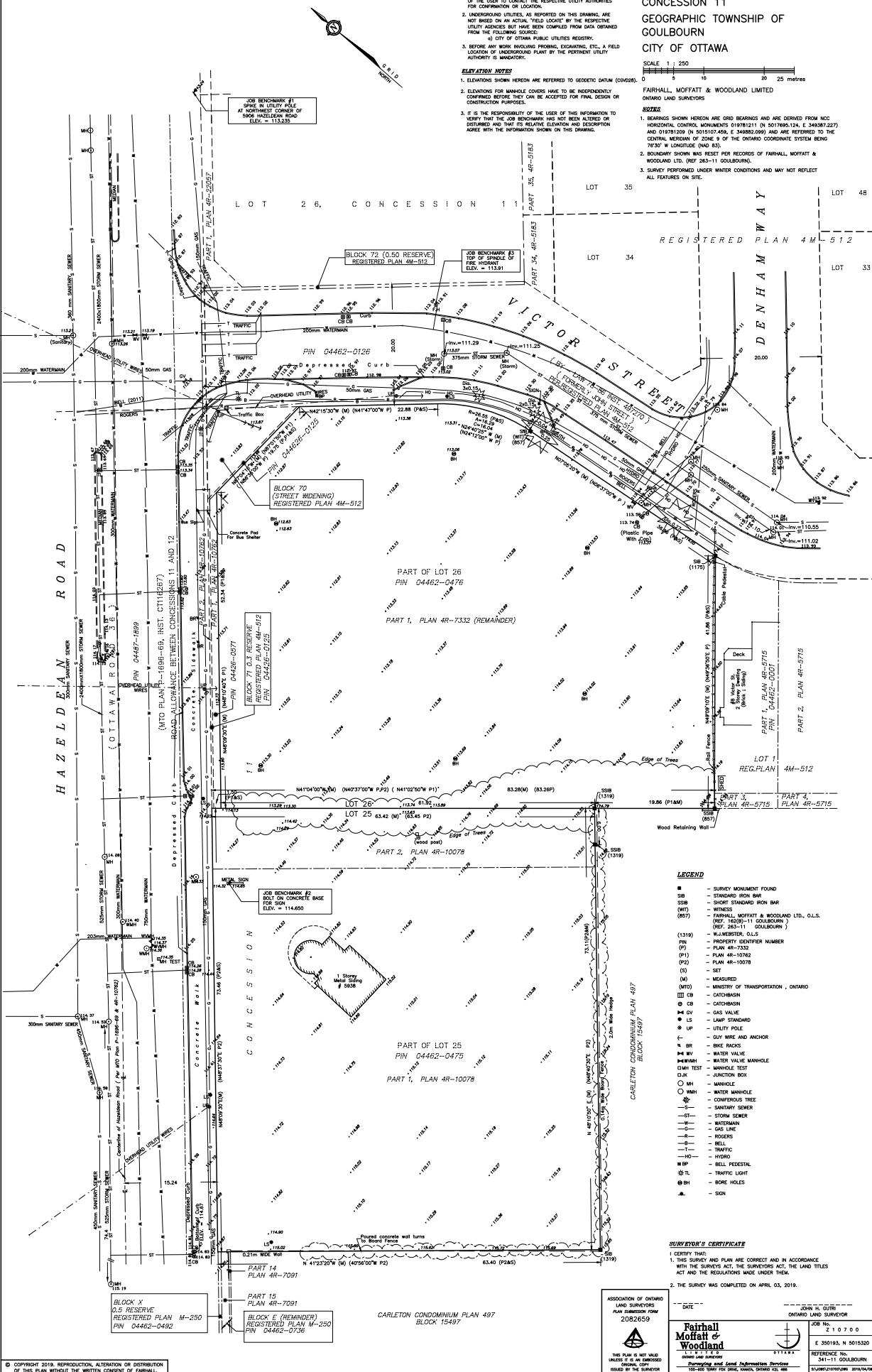
0 5 10 20 25 metres
FAIRHALL, MOFFATT & WOODLAND LIMITED
ONTARIO LAND SURVEYORS

ELEVATION NOT

1. ELEVATIONS SHOWN HEREON ARE REFERRED TO GEODETIC DATUM (CGPS).
 2. ELEVATIONS FOR MANHOLE COVERS HAVE TO BE INDEPENDENTLY CONFIRMED BEFORE THEY CAN BE ACCEPTED FOR FINAL DESIGN OR CONSTRUCTION PURPOSES.
 3. IT IS THE RESPONSIBILITY OF THE USER OF THIS INFORMATION TO VERIFY THAT THE JOB BENCHMARK HAS NOT BEEN ALTERED OR DISTURBED AND THAT ITS RELATIVE ELEVATION AND DESCRIPTION AGREE WITH THE INFORMATION SHOWN ON THIS DRAWING.

1. BEARINGS SHOWN HEREON ARE GRID BEARINGS AND ARE DERIVED FROM HORIZONTAL CONTROL MONUMENTS 019781211 (N 017695.124, E 3.01) AND 019781209 (N 5015107.459, E 340882.099) AND ARE REFERRED TO THE CENTRAL MERIDIAN OF ZONE 9 OF THE ONTARIO COORDINATE SYSTEM. 76°30' W LONGITUDE (NAD 83).
2. BOUNDARY SHOWN WAS RESET PER RECORDS OF FAIRHALL, MOFFATT WOODLAND LTD. (REC 263-11 GOULBURN).
3. SURVEY PERFORMED UNDER WINTER CONDITIONS AND MAY NOT REFLECT MAJOR FEATURES ON SITE.

ALL FEATURES ON SITE.



www.vipsoft.com

- SURVEYOR'S CERTIFICATE**

I CERTIFY THAT:
1. THIS SURVEY AND PLAN ARE CORRECT AND IN ACCORDANCE
WITH THE SURVEYS ACT, THE SURVEYORS ACT, THE LAND TITLES
ACT AND THE REGULATIONS MADE UNDER THEM.

2. THE SURVEY WAS COMPLETED ON APRIL 03, 2019.



*exp Services Inc
Hazeldean Crossing Inc.
5924 Hazeldean Road
OTT-00250806-B0
January 22, 2020*

Appendix L – Checklist

4.1 General Content

- Executive Summary (for larger reports only).

Comments:

- Date and revision number of the report.

Comments:

- Location map and plan showing municipal address, boundary, and layout of proposed development.

Comments:

- Plan showing the site and location of all existing services.

Comments:

- Development statistics, land use, density, adherence to zoning and official plan, and reference to applicable subwatershed and watershed plans that provide context to which individual developments must adhere.

Comments:

- Summary of Pre-consultation Meetings with City and other approval agencies.

Comments:

- Reference and confirm conformance to higher level studies and reports (Master Servicing Studies, Environmental Assessments, Community Design Plans), or in the case where it is not in conformance, the proponent must provide justification and develop a defendable design criteria.

Comments:

- Statement of objectives and servicing criteria.

Comments:

- Identification of existing and proposed infrastructure available in the immediate area.

Comments:

- Identification of Environmentally Significant Areas, watercourses and Municipal Drains potentially impacted by the proposed development (Reference can be made to the Natural Heritage Studies, if available).

Comments:

- Concept level master grading plan to confirm existing and proposed grades in the development. This is required to confirm the feasibility of proposed stormwater management and drainage, soil removal and fill constraints, and potential impacts to neighbouring properties. This is also required to confirm that the proposed grading will not impede existing major system flow paths.

Comments:

- Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts.

Comments:

- Proposed phasing of the development, if applicable.

Comments:

- Reference to geotechnical studies and recommendations concerning servicing.

Comments:

- All preliminary and formal site plan submissions should have the following information:

- Metric scale
- North arrow (including construction North)
- Key plan
- Name and contact information of applicant and property owner
- Property limits including bearings and dimensions
- Existing and proposed structures and parking areas
- Easements, road widening and rights-of-way
- Adjacent street names

Comments:

4.2 Development Servicing Report: Water

- Confirm consistency with Master Servicing Study, if available
Comments:
- Availability of public infrastructure to service proposed development
Comments:
- Identification of system constraints
Comments:
- Identify boundary conditions
Comments:
- Confirmation of adequate domestic supply and pressure
Comments:
- Confirmation of adequate fire flow protection and confirmation that fire flow is calculated as per the Fire Underwriter's Survey. Output should show available fire flow at locations throughout the development.
Comments:
- Provide a check of high pressures. If pressure is found to be high, an assessment is required to confirm the application of pressure reducing valves.
Comments:
- Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defined phases of the project including the ultimate design
Comments:
- Address reliability requirements such as appropriate location of shut-off valves
Comments:
- Check on the necessity of a pressure zone boundary modification.
Comments:

- Reference to water supply analysis to show that major infrastructure is capable of delivering sufficient water for the proposed land use. This includes data that shows that the expected demands under average day, peak hour and fire flow conditions provide water within the required pressure range

Comments:

- Description of the proposed water distribution network, including locations of proposed connections to the existing system, provisions for necessary looping, and appurtenances (valves, pressure reducing valves, valve chambers, and fire hydrants) including special metering provisions.

Comments:

- Description of off-site required feedermains, booster pumping stations, and other water infrastructure that will be ultimately required to service proposed development, including financing, interim facilities, and timing of implementation.

Comments:

- Confirmation that water demands are calculated based on the City of Ottawa Design Guidelines.

Comments:

- Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference.

Comments:

4.3 Development Servicing Report: Wastewater

- Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitored flow data from relatively new infrastructure cannot be used to justify capacity requirements for proposed infrastructure).

Comments:

- Confirm consistency with Master Servicing Study and/or justifications for deviations.

Comments:

- Consideration of local conditions that may contribute to extraneous flows that are higher than the recommended flows in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers.

Comments:

- Description of existing sanitary sewer available for discharge of wastewater from proposed development.

Comments:

- Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable)

Comments:

- Identification and implementation of the emergency overflow from sanitary pumping stations in relation to the hydraulic grade line to protect against basement flooding.

Comments:

- Special considerations such as contamination, corrosive environment etc.

Comments:

4.4 Development Servicing Report: Stormwater

- Description of drainage outlets and downstream constraints including legality of outlets (i.e. municipal drain, right-of-way, watercourse, or private property)
Comments:
- Analysis of available capacity in existing public infrastructure.
Comments:
- A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns, and proposed drainage pattern.
Comments:
- Water quantity control objective (e.g. controlling post-development peak flows to pre-development level for storm events ranging from the 2 or 5 year event (dependent on the receiving sewer design) to 100 year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects.
Comments:
- Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements.
Comments:
- Description of the stormwater management concept with facility locations and descriptions with references and supporting information.
Comments:
- Set-back from private sewage disposal systems.
Comments:
- Watercourse and hazard lands setbacks.
Comments:
- Record of pre-consultation with the Ontario Ministry of Environment and the Conservation Authority that has jurisdiction on the affected watershed.
Comments:

- Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists.

Comments:

- Storage requirements (complete with calculations) and conveyance capacity for minor events (1:5 year return period) and major events (1:100 year return period).

Comments:

- Identification of watercourses within the proposed development and how watercourses will be protected, or, if necessary, altered by the proposed development with applicable approvals.

Comments:

- Calculate pre and post development peak flow rates including a description of existing site conditions and proposed impervious areas and drainage catchments in comparison to existing conditions.

Comments:

- Any proposed diversion of drainage catchment areas from one outlet to another.

Comments:

- Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and stormwater management facilities.

Comments:

- If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post-development flows up to and including the 100-year return period storm event.

Comments:

- Identification of potential impacts to receiving watercourses

Comments:

- Identification of municipal drains and related approval requirements.

Comments:

- Descriptions of how the conveyance and storage capacity will be achieved for the development.

Comments:

- 100 year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading.

Comments:

- Inclusion of hydraulic analysis including hydraulic grade line elevations.

Comments:

- Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors.

Comments:

- Identification of floodplains - proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions.

Comments:

- Identification of fill constraints related to floodplain and geotechnical investigation.

Comments:

4.5 Approval and Permit Requirements: Checklist

The Servicing Study shall provide a list of applicable permits and regulatory approvals necessary for the proposed development as well as the relevant issues affecting each approval. The approval and permitting shall include but not be limited to the following:

- Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act.

Comments:

- Application for Certificate of Approval (CofA) under the Ontario Water Resources Act.

Comments:

- Changes to Municipal Drains.

Comments:

- Other permits (National Capital Commission, Parks Canada, Public Works and Government Services Canada, Ministry of Transportation etc.)

Comments:

4.6 Conclusion Checklist

- Clearly stated conclusions and recommendations

Comments:

- Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency.

Comments:

- All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario

Comments: