

**1000 ROBERT GRANT AVENUE
RENE'S COURT
OTTAWA, ONTARIO**

SERVICEABILITY REPORT

Prepared by:

NOVATECH
Suite 200, 240 Michael Cowpland Drive
Ottawa, Ontario
K2M 1P6

June 27, 2019

Ref: R-2019-096
Novatech File: 117151



June 27, 2019

BY COURIER

City of Ottawa
Planning and Growth Management Department
110 Laurier Avenue West, 4th Floor
Ottawa, Ontario
K1P 1J1

Attention: Kathy Rygus

Dear Ms Rygus:

**Re: 1000 Robert Grant Avenue (Rene's Court)
Serviceability Report
Our File No.: 117151**

Please find enclosed three (3) copies of the above noted report dated June 27, 2019. This report is submitted in support of a Zoning By-law Amendment Application.

If you have any questions, please contact the undersigned.

Yours truly,

NOVATECH

A handwritten signature in blue ink, appearing to read "Cara Ruddle".

Cara Ruddle, P.Eng.
Senior Project Manager, Land Development Engineering

CC:

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1.0. INTRODUCTION

Novatech has been retained to prepare a Serviceability Report for the property located at 1000 Robert Grant Avenue within the City of Ottawa. **Figure 1** is a Key Plan showing the site location. The purpose of this report is to demonstrate that the potential development can be serviced with the existing Municipal infrastructure surrounding the property.

2.0. EXISTING DEVELOPMENT

The property is approximately 2.0 hectares in size and is currently undeveloped, vacant land. The property (1000 Robert Grant Avenue) is currently identified as Block 203 and is included as part of the Phase 1 and 2 Fernbank Crossing Development. The property is bound by Robert Grant Avenue to the west, Livery Street to the east, another mixed-use parcel to the south, and Block 200 a future transit station to the North. The topography of the site gradually slopes towards Livery Street (west to east). **Figure 2** shows the existing site conditions.

3.0. PROPOSED DEVELOPMENT

It is proposed to develop an apartment complex consisting of three apartment buildings and a one-story clubhouse all connected by an underground parking garage. The apartment buildings will consist of a combination of one-bedroom and two-bedroom units. The proposed development will have access from both Livery Street and Robert Grant Avenue. The Robert Grant Avenue entrance will provide access to all buildings at ground level and access to the underground parking garage. The Livery Street site entrance will be to the underground parking garage only. **Figure 3** shows a concept of the potential development plan.

4.0. SERVICING REPORT REFERENCES

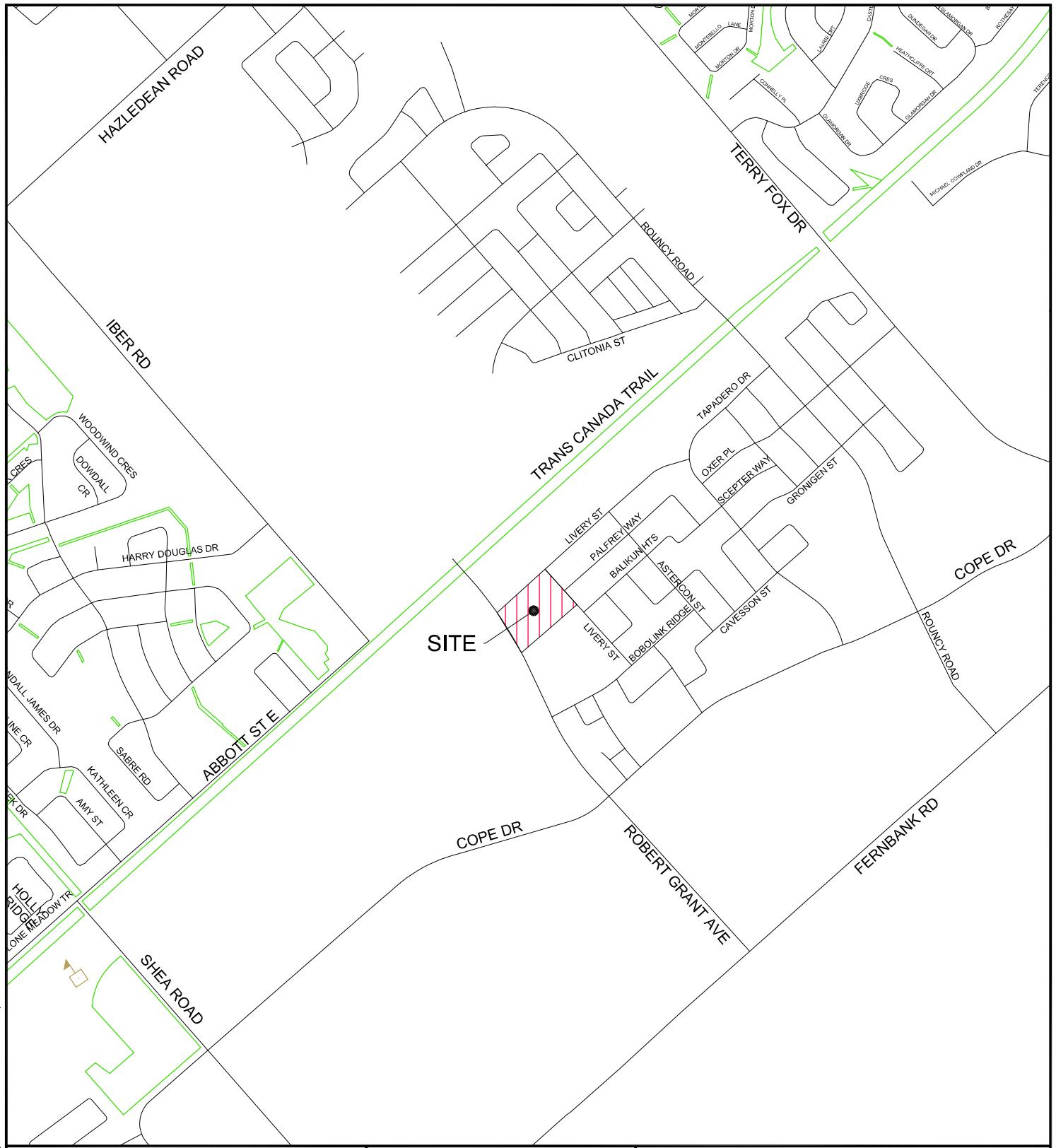
- Novatech, Fernbank Crossing Servicing Design Brief (Phase 1 & 2), Revised Dated August 17, 2012.
- Novatech, Fernbank Crossing Servicing Stormwater Management Report (Phase 1 & 2), Revised Dated August 17, 2012.
- IBI, Conceptual Site Servicing Study Stormwater Site Management Plan and Erosion Sediment Control Plan Westpark – Phase 1 Fernbank Community Date February 2010.

5.0. WATER SERVICING

The property has an existing capped 200mm watermain stub at the corner of Livery Street. There is an existing 200mm diameter watermain within the Livery Street right-of-way. A portion of the City sewer mapping is included in **Appendix A** for reference.

To service the development, it is proposed to extend the existing capped watermain stub into the building and constructing a second water service to the south. The second water service is provided for redundancy purposes as the daily water demand is greater than 50 cubic meters. **Figure 4** Conceptual Servicing Plan shows the potential servicing options for the development.

Water demand and fire flow calculations have been prepared based on the current concept plans for the development. The water demands are calculated from criteria in Section 4 of the City of Ottawa Design Guidelines for Water Distribution Systems and are based on a total



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RENE'S COURT BLOCK 203

KEY PLAN

SCALE

N.T.S

DATE

MAR 2019

JOB 117151

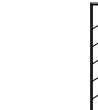
FIGURE 1



ROBERT GRANT AVE

BUILDING B
15 STOREYS

CLUB HOUSE
1 STOREY



BUILDING C
12 STOREYS

6 STOREYS

BUILDING A

5 STOREYS

PARTRIDGE
Estate

LIVERY ST

BLOCK 204B

BLOCK 204A

BLOCK 196A

195

194

PALFREY WAY

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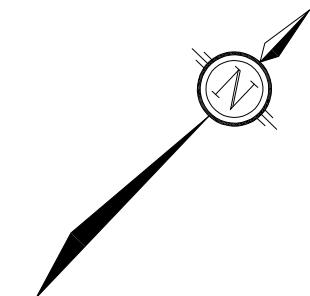
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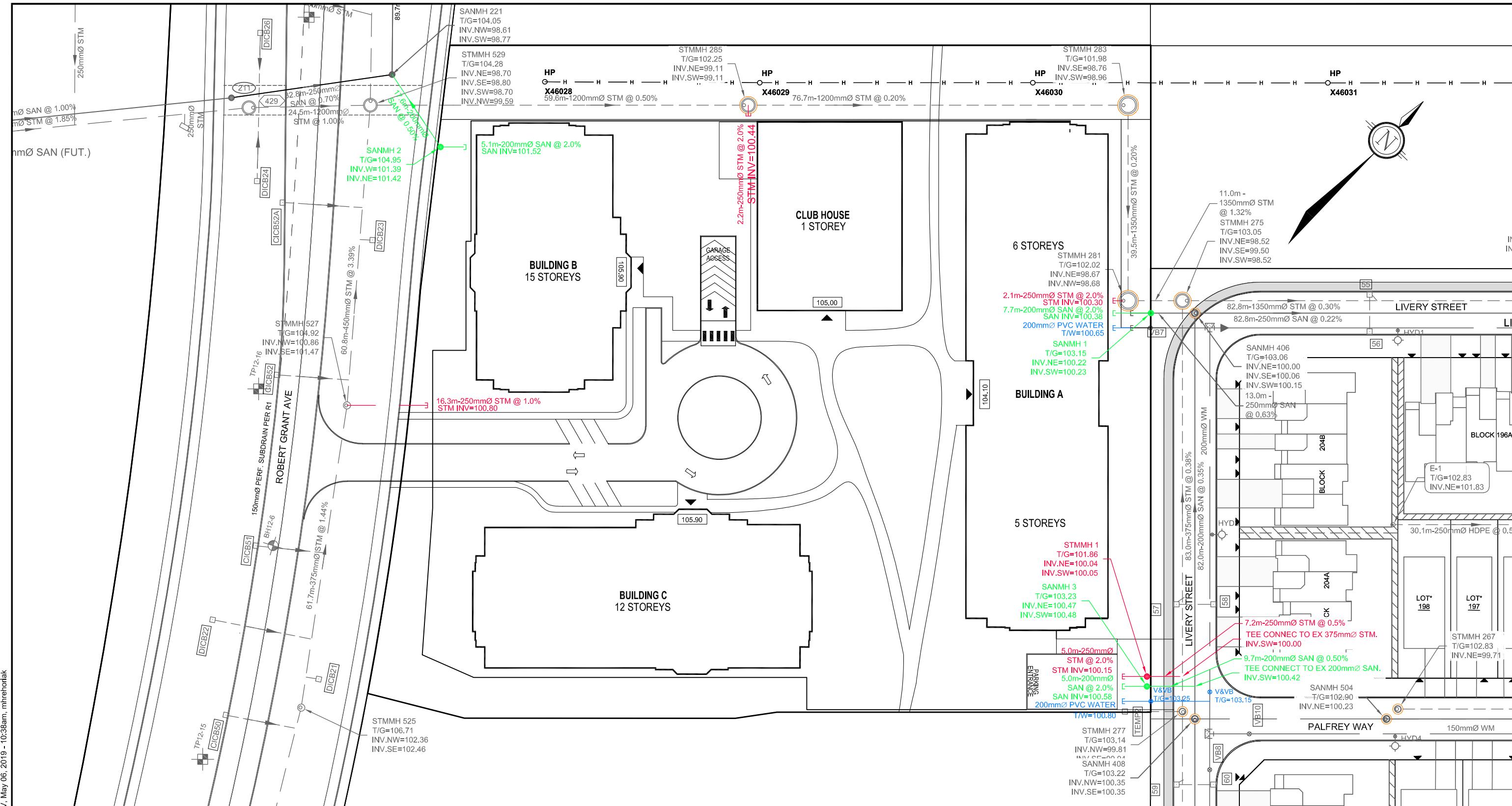
RENE'S COURT BLOCK 203

CONCEPTUAL SITE PLAN

SCALE 1 : 750 0 10 20 30

DATE MAR 2019 JOB 117151 FIGURE 3





population 1019 people from a total of 566 units. Fire flows are calculated using the Fire Underwriters Survey method using assumptions on building construction and sprinkler requirements. Preliminary water demand and fire flows are summarized in **Table 5.1** below.

Table 5.1 Water Demand Summary

| Use | Ave. Daily Demand (L/s) | Max. Daily Demand (L/s) | Peak Hour Demand (L/s) | Fire Flow (L/s) |
|-------------|-------------------------|-------------------------|------------------------|-----------------|
| Residential | 4.13 | 10.32 | 22.70 | 167 |

For the purposes of this report to determine if the proposed development concept can be serviced, excepts from the Novatech Fernbank Crossing (Phase 1 & 2) Servicing Design Brief have been reviewed and are provided in **Appendix A** for reference.

From the Fernbank Crossing (Phase 1 & 2) Design Brief the proposed development is located within the 3W pressure zone and is serviced from the existing 400mm diameter watermain along the Trans Canada Trail and a 400mm diameter watermain in Terry Fox Drive. City boundary conditions and a location map for the connections described above are provided in **Appendix A**. The Fernbank Crossing internal watermain network has been designed to satisfy the following three conditions:

- Average Day Demand, pressures are to be less than 80psi.
- Peak Hour Demand, pressures are to be greater than 40psi.
- Maximum Day plus Fire Flow, pressures are to be greater than 20psi.

The Fernbank Crossing (Phase 1 & 2) watermain network was modelled with epanet using the City provided boundary conditions. A summary of the critical nodes (low pressure, high pressure and pressure at the node nearest Block 203) from the watermain analysis are provided below in **Table 5.2**.

Table 5.2 Water Analysis Results Summary

| Condition | Junction ID | Demand (L/s) | Min/Max Allowable Operating Pressures (psi) | Limits of Design Operating Pressures (psi) |
|---------------------|--------------|--------------|---|--|
| High Pressure | TMU1 (Low) | 9.1 | 80psi (Max) | 80.84 |
| | T12 (High) | | | 89.65 |
| | T1 (Site) | | | 87.38 |
| Max Day + Fire Flow | HYD10 | 125 | 20psi (Min) | 69.28 |
| | HYD33 | 217 | | 40.91 |
| | HYD 3 (Site) | 217 | | 54.12 |
| Peak Hour | TMU1 (Low) | 45.4 | 40psi (Min) | 66.57 |
| | T12 (High) | | | 75.42 |
| | T1 (Site) | | | 72.95 |

The Fernbank Crossing watermain analysis is based on an average day demand contribution of 2.95 L/s from the entirety of the Mixed-Use Block. The subject site area (2.0ha) is approximately 30% of the total mixed-use block area (7.1ha) with an average day demand of 4.13 L/s. The domestic demands are greater than originally anticipated however, there is more than adequate pressure in the existing watermain to service the proposed development for domestic use. The watermain surrounding Block 203 (1000 Robert Grant Avenue) was designed for a fireflow of 217L/s at a pressure of 54.1psi which is greater than the 167L/s required by the proposed development. Therefore, there is also adequate pressure to service the proposed development's fire demand. Pressure reduction valves will likely be required as the watermain pressures exceed the maximum 80psi operating pressure in the average day condition. Refer to **Appendix A** for detailed water demand calculations, fire flow calculations and excerpts from the Fernbank Crossing (Phase 1 & 2) Servicing Design Brief.

6.0. SANITARY SERVICING

The property has an existing capped 250mm diameter sanitary sewer stub at the corner of Livery Street. There is an existing 200mm diameter sanitary sewer fronting the development on Livery Street and a 250mm diameter sanitary sewer at the northwest corner of the development in the Robert Grant Avenue right-of-way. The sanitary sewer in Robert Grant Avenue flows to the north and connects into the Stittsville sanitary trunk sewer (750mm diameter) to the north of Block 203. The sanitary sewer on Livery Street flows to the east and becomes a 375mm diameter sewer at Oxford Place and a 600mm diameter sewer at Rouncey Road. The 600mm diameter sewer on Rouncey Road flows to the north and connects into the Stittsville sanitary trunk sewer (1200mm diameter). A portion of the City sewer mapping is included in **Appendix B** for reference.

Sanitary flows for the proposed development are calculated from criteria in Section 4 of the City of Ottawa Sewer Design Guidelines and are based on a total population 1019 people from a total of 566 units. The peak sanitary flow was calculated to be 11.35 L/s based on an average domestic demand of 280 L/day/person. Detailed sanitary flow calculations are provided in **Appendix B** for reference.

There are multiple sanitary servicing options for the proposed development. Connections can be made to any of the existing sewers noted above. It is likely that multiple services will be required due to the size of the development. **Figure 4** Conceptual Servicing Plan shows the potential servicing options for the development.

The Livery Street sanitary sewer was designed as a part of the Fernbank Crossing Phase 1 & 2 development and drains into the sanitary sewers within the Westpark Phase 1 development. The Fernbank Crossing (Phase 1 & 2) Design Brief prepared by Novatech includes a sanitary sewer design sheet with Block 203 (1000 Robert Grant Avenue, labelled as Area A4-3). The total peak flow allotted for Block 203 is 3.3L/s into the Livery Street sanitary sewer. Since the allotted flows are less than the proposed flows an investigation into the downstream sanitary sewer system is required. A copy of the drainage area plan and design sheet for Fernbank Crossing Phase 1 & 2 are included in **Appendix B**.

Upon review of the downstream sewers, it should be noted that there is one section of sewer within the Westpark Phase 1 sanitary sewer system that is near capacity. The sanitary sewer design sheet for the Westpark Phase 1 development, prepared by IBI, indicates that the existing 375mm diameter sewer on Oxford Place (between MH 103A and MH 202A) is currently

operating at 92% with 6.57L/s of available capacity. This sewer is downstream of Livery Street and is shown on the IBI West Park General Plan of Services provided in **Appendix B**.

The IBI Westpark Phase 1 development sanitary design sheet is dated May 2012. The City of Ottawa design criteria has since been updated in 2018 to reduce theoretical sanitary design flows. The new City of Ottawa criteria reduces design flows by approximately 35% from a reduction in domestic demand and the harmon correction factor. Therefore, the sanitary sewer between MH 103A and MH 202A has more available capacity given the new City design criteria. Also, a portion of the sanitary flows from the proposed development are to be conveyed by the Robert Grant sanitary sewer which is currently operating at 32.2% of capacity. The proposed development flow of 11.35 L/s is greater than originally anticipated however, there is capacity in the existing sewers to service the proposed development. Refer to **Appendix B** for all relevant sanitary sewer drainage area plans and sanitary sewer design sheets.

7.0. STORM SERVICING & STORMWATER MANAGEMENT

Stormwater currently sheet drains across the site towards Livery Street. Stormwater is collected by an existing temporary catchbasin at the south east corner of the property which outlets to the existing 375mm diameter storm sewer fronting the development in Livery Street. Refer to **Appendix C** for the Existing Storm Drainage Area Plan.

There is also an existing 1200mm and 1350mm diameter trunk storm sewer in an easement along the north and a portion of the east property line and an existing 450mm diameter storm sewer in the Robert Grant Avenue right-of-way. All storm sewers described above drain into the existing stormwater management facility (pond 6) to the south of Block 203 at the Asturcon and Cavesson Street intersection. Multiple service connections are possible and may be required due to the size of the development. **Figure 4** Conceptual Servicing Plan shows the potential servicing options for the development.

The following stormwater management design criteria for the proposed development was provided in the Novatech Fernbank Crossing Stormwater Management Report (Phase 1 & 2):

- Quantity control of stormwater is required for up to and including 100-year storm event to a runoff coefficient of 0.8.
- Quality control of stormwater is not required as an enhanced level treatment (80% TSS removal) is provided in downstream SWM facility (pond 6).

Stormwater flows in excess of the allowable release rate must be stored on site for storms up to and including the 100-year storm event. Preliminary stormwater management calculations have been completed for the proposed development. The allowable release rate for the site has been calculated to be 353.0 L/s. Quantity control measures will be proposed in order to meet the allowable release rate. Storage of stormwater will be provided by underground storage tanks. The preliminary stormwater management calculations are summarized below in **Table 7.1**.

Table 7.1 Stormwater Management Summary

| Area ID | Area (ha) | 1:5 Year Weighted Cw | Orifice Size & Type | 100 Year Storm Event | |
|--|-----------|----------------------|---------------------|----------------------|---------------------|
| | | | | Flow (L/s) | Required Vol (cu.m) |
| A1 | 0.323 | 0.35 | N/A | 66.1 | N/A |
| A2 | 0.106 | 0.84 | N/A | 286.9 | 307.2 |
| Total Flow to Pond 6 from development | | | | 353.0 | |
| Allowable Flow to Pond 6 | | | | 353.0 | |

During storms in excess of the 100-year storm event, site grading will provide an overland flow route to Livery Street and ultimately to the stormwater management facility (pond 6) and the Monahan Drain. **Figure 5** Conceptual Grading Plan shows the preliminary conceptual grading design.

In Summary, the existing storm sewer infrastructure can service the proposed development and appropriate stormwater management methods can be used to meet the allowable release rate. Refer to **Appendix C** for preliminary stormwater management calculations and pre and post development drainage area figures.

8.0. EROSION AND SEDIMENT CONTROL MEASURES

Temporary erosion and sediment control measures will be required on-site during construction in accordance with the Best Management Practices for Erosion and Sediment Control. This includes the following temporary measures:

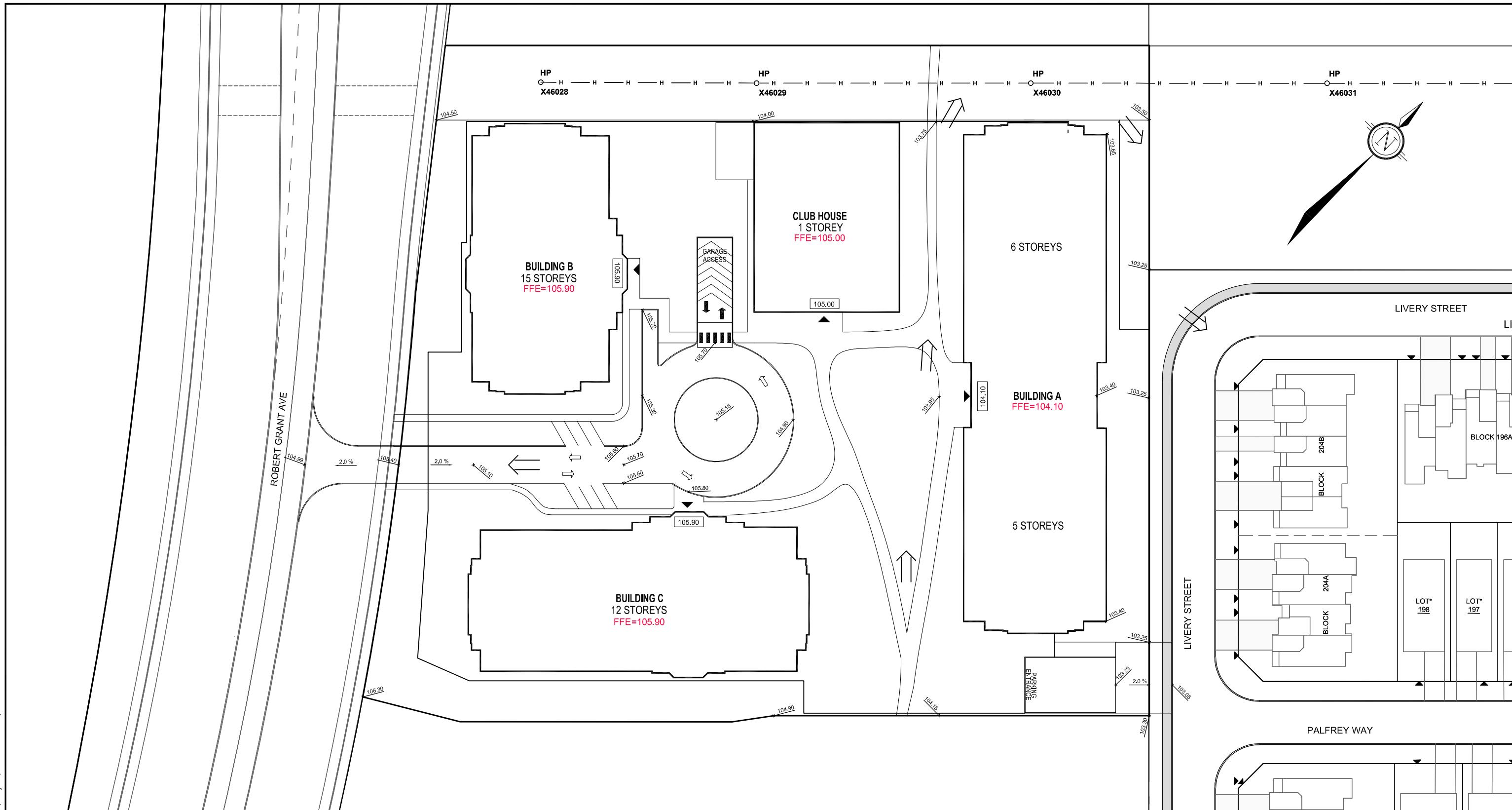
- Filter socks will be placed in existing catchbasins and manholes, and will remain in place until vegetation has been established and construction is completed;
- Silt fencing will be placed along the surrounding construction limits;
- Mud mats will be installed at the site entrances;
- The contractor will be required to perform regular street sweeping and cleaning as required, to suppress dust and to provide safe and clean roadways adjacent to the construction site;

The erosion and sediment control measures will be required prior to construction and will remain in place during all phases of construction. Regular inspection and maintenance of the erosion control measures will be undertaken

9.0. CONCLUSIONS AND RECOMMENDATIONS

The conclusions of this report are as follows:

- Water servicing, including both domestic and fire protection, can be provided by connection to the existing watermain infrastructure within Livery Street. Pressure reduction valves will be required.
- Sanitary servicing can be provided from the existing sanitary sewer infrastructure surrounding the site.



LEGEND

- SLOPE DIRECTION
- MAJOR OVERLAND FLOW ROUTE
- PROPOSED ELEVATION
- PROPOSED FINISHED FLOOR ELEVATION AT ENTRANCE



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RENE'S COURT BLOCK 203

CONCEPTUAL GRADING PLAN

SCALE 1 : 750

DATE MAR 2019 JOB 117151 FIGURE 5

- Storm servicing can be provided for the proposed development. Quantity control of stormwater can be provided through storage of stormwater in underground storage tanks. Quality control is provided in the downstream stormwater management facility (pond 6).
- An overland flow route will be provided to Livery Street.
- Erosion and sediment control measures will be required during construction.

The preceding report is respectfully submitted for review and approval. Please contact the undersigned should you have any questions or require additional information.

NOVATECH

Prepared by:



Matthew Hrehoriak, P.Eng.
Project Engineer
Land Development Engineering

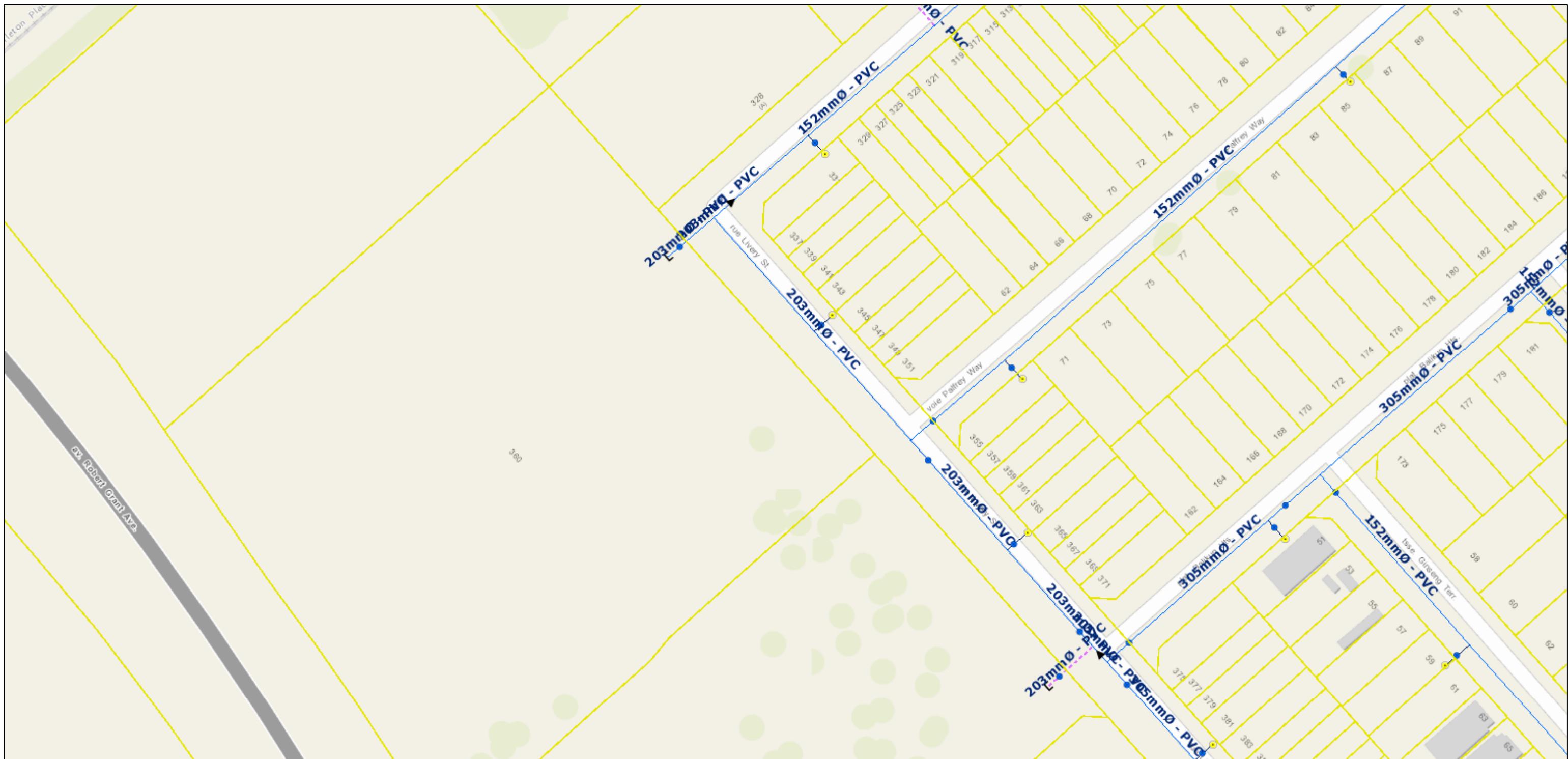
Reviewed by:



Cara Ruddle, P.Eng.
Senior Project Manager
Land Development Engineering

APPENDIX A
Watermain Information

1000 Robert Grant Ave Water Info



March 6, 2019

Property Parcels

Water Labels / Étiquettes

Valves / Vannes

• Valve / Vanne

- TVS, A, D

Water Fittings / Raccords de conduite d'eau

■ Cap / bouchon

◀ Reducer / réducteur

● Hydrants / Bornes-fontaines

— Hydrant Laterals / Branchements de borne-fontaine

Water Mains / Conduites d'eau principales

— Private / Branchement privé

— Public / Branchement public

Misc. Water Structures / Structures d'aqueduc - divers

■ Pumping Station / Station de pompage des eaux

● Well Supply / Alimentation par puits

● Elevated Tank / Château d'eau

■ In Ground Tank / Réervoir souterrain

■ Water Treatment Plant / Usine d'épuration des eaux

1:1,500

0 0.0175 0.035 0.07 mi
0 0.0275 0.055 0.11 km

City of Ottawa

**Table 1
Water Demand**

| | Unit Type | Total Population | Total Demand (L/s) | | |
|-------------|-------------------|------------------|--------------------|------------|-----------|
| | | | Avg Day | Max. Daily | Peak Hour |
| Building ID | Average Apartment | | | | |
| Building A | 146 | 263 | 1.07 | 2.66 | 5.86 |
| Building B | 207 | 373 | 1.51 | 3.78 | 8.31 |
| Building C | 213 | 383 | 1.55 | 3.88 | 8.53 |
| Totals | 566 | 1019 | 4.13 | 10.32 | 22.70 |

Design Parameters:

- Average Apartment = 1.8 persons/unit

Design Criteria from Section 4 Ottawa Design Guidelines Water Distribution

- Average Domestic Flow 350 L/person/day

Max. Daily Demand:

- Residential Peak Factor 2.5 x Avg Day

Peak Hourly Demand:

- Residential Peak Factor 2.2 x Max Day

FUS - Fire Flow Calculations

As per 1999 Fire Underwriter's Survey Guidelines



Engineers, Planners & Landscape Architects

Novatech Project #: 117151

Project Name: Rene's Court

Date: 2/25/2019

Input By: Matt Hrehoriak

Reviewed By: Cara Ruddle

Legend

Input by User

No Information or Input Required

Building Description: 6 Storey Apartment Building A

Fire Resistive Construction

| Step | | Choose | | Value Used | Total Fire Flow (L/min) | |
|---------------------------------|---|---|-------------|----------------------------|-------------------------|--|
| Base Fire Flow | | | | | | |
| 1 | Construction Material | | | Multiplier | | |
| | Coefficient related to type of construction C | Wood frame | | 1.5 | 0.8 | |
| | | Ordinary construction | | 1 | | |
| | | Non-combustible construction | Yes | 0.8 | | |
| | | Modified Fire resistive construction (2 hrs) | | 0.6 | | |
| 2 | Floor Area | | | | | |
| | A | Building Footprint (m ²) | 2848 | | | |
| | | Number of Floors/Storeys | 6 | | | |
| | | Protected Openings (1 hr) | Yes | | | |
| | | Area of structure considered (m ²) | | 4,272 | | |
| | F | Base fire flow without reductions | | | 12,000 | |
| | | $F = 220 C (A)^{0.5}$ | | | | |
| Reductions or Surcharges | | | | | | |
| 3 | Occupancy hazard reduction or surcharge | | | Reduction/Surcharge | | |
| | (1) | Non-combustible | | -25% | 10,200 | |
| | | Limited combustible | Yes | -15% | | |
| | | Combustible | | 0% | | |
| | | Free burning | | 15% | | |
| | | Rapid burning | | 25% | | |
| 4 | Sprinkler Reduction | | | Reduction | | |
| | (2) | Adequately Designed System (NFPA 13) | Yes | -30% | -5,100 | |
| | | Standard Water Supply | Yes | -10% | | |
| | | Fully Supervised System | Yes | -10% | | |
| | | | | Cumulative Total | -50% | |
| 5 | Exposure Surcharge (cumulative %) | | | Surcharge | | |
| | (3) | North Side | 10.1 - 20 m | | 4,590 | |
| | | East Side | 30.1 - 45 m | | | |
| | | South Side | 20.1 - 30 m | | | |
| | | West Side | 10.1 - 20 m | | | |
| | | | | Cumulative Total | 45% | |
| Results | | | | | | |
| 6 | (1) + (2) + (3) | Total Required Fire Flow, rounded to nearest 1000L/min | | | L/min | |
| | | (2,000 L/min < Fire Flow < 45,000 L/min) | | or | L/s | |
| | | | | or | USGPM | |
| 7 | Storage Volume | Required Duration of Fire Flow (hours) | | | Hours | |
| | | Required Volume of Fire Flow (m ³) | | | m ³ | |
| | | | | | 1200 | |

FUS - Fire Flow Calculations

As per 1999 Fire Underwriter's Survey Guidelines



Novatech Project #: 117151

Project Name: Rene's Court

Date: 2/25/2019

Input By: Matt Hrehoriak

Reviewed By: Cara Ruddle

Legend

Input by User

No Information or Input Required

Building Description: 15 Storey Apartment Building B
Fire Resistive Construction

| Step | | Choose | | Value Used | Total Fire Flow (L/min) | | | |
|---------------------------------|---|---|-------------------------|----------------------------|-------------------------|--|--|--|
| Base Fire Flow | | | | | | | | |
| 1 | Construction Material | | | Multiplier | | | | |
| | C Coefficient related to type of construction | Wood frame | | 1.5 | 0.8 | | | |
| | | Ordinary construction | | 1 | | | | |
| | | Non-combustible construction | | Yes | | | | |
| | | Modified Fire resistive construction (2 hrs) | | 0.6 | | | | |
| 2 | Floor Area | | | | | | | |
| | A Building Footprint (m ²) | 1515 | | | | | | |
| | | Number of Floors/Storeys | | 15 | | | | |
| | | Protected Openings (1 hr) | | Yes | | | | |
| | | Area of structure considered (m ²) | | 2,273 | | | | |
| F | Base fire flow without reductions | | | | | | | |
| | $F = 220 C (A)^{0.5}$ | | | 8,000 | | | | |
| Reductions or Surcharges | | | | | | | | |
| 3 | Occupancy hazard reduction or surcharge | | | Reduction/Surcharge | | | | |
| | (1) Non-combustible Limited combustible Combustible Free burning Rapid burning | Non-combustible | | -25% | 6,800 | | | |
| | | Limited combustible | | -15% | | | | |
| | | Combustible | | 0% | | | | |
| | | Free burning | | 15% | | | | |
| 4 | Sprinkler Reduction | | | Reduction | | | | |
| | (2) Adequately Designed System (NFPA 13) Standard Water Supply Fully Supervised System | Yes | | -30% | -3,400 | | | |
| | | Yes | | -10% | | | | |
| | | Yes | | -10% | | | | |
| | | | | Cumulative Total | -50% | | | |
| 5 | Exposure Surcharge (cumulative %) | | | Surcharge | | | | |
| | (3) North Side East Side South Side West Side | North Side | | 10.1 - 20 m | 2,380 | | | |
| | | East Side | | 20.1 - 30 m | | | | |
| | | South Side | | 20.1 - 30 m | | | | |
| | | West Side | | > 45.1m | | | | |
| | | | Cumulative Total | 35% | | | | |
| Results | | | | | | | | |
| 6 | (1) + (2) + (3) | Total Required Fire Flow, rounded to nearest 1000L/min | | | L/min | | | |
| | | (2,000 L/min < Fire Flow < 45,000 L/min) | | | L/s | | | |
| | | | | | USGPM | | | |
| 7 | Storage Volume | Required Duration of Fire Flow (hours) | | | Hours | | | |
| | | Required Volume of Fire Flow (m ³) | | | m ³ | | | |
| | | | | | 720 | | | |

FUS - Fire Flow Calculations

As per 1999 Fire Underwriter's Survey Guidelines



Engineers, Planners & Landscape Architects

Novatech Project #: 117151

Project Name: Rene's Court

Date: 2/25/2019

Input By: Matt Hrehoriak

Reviewed By: Cara Ruddle

Legend

Input by User

No Information or Input Required

Building Description: 12 Storey Apartment Building C

Fire Resistive Construction

| Step | | Choose | | Value Used | Total Fire Flow (L/min) | |
|---------------------------------|---|---|-------------|----------------------------|-------------------------|--|
| Base Fire Flow | | | | | | |
| 1 | Construction Material | | | Multiplier | | |
| | Coefficient related to type of construction C | Wood frame | | 1.5 | 0.8 | |
| | | Ordinary construction | | 1 | | |
| | | Non-combustible construction | Yes | 0.8 | | |
| | | Modified Fire resistive construction (2 hrs) | | 0.6 | | |
| 2 | Floor Area | | | | | |
| | A | Building Footprint (m ²) | 1955 | | | |
| | | Number of Floors/Storeys | 12 | | | |
| | | Protected Openings (1 hr) | Yes | | | |
| | | Area of structure considered (m ²) | | 2,933 | | |
| | F | Base fire flow without reductions | | | 10,000 | |
| | | $F = 220 C (A)^{0.5}$ | | | | |
| Reductions or Surcharges | | | | | | |
| 3 | Occupancy hazard reduction or surcharge | | | Reduction/Surcharge | | |
| | (1) | Non-combustible | | -25% | 8,500 | |
| | | Limited combustible | Yes | -15% | | |
| | | Combustible | | 0% | | |
| | | Free burning | | 15% | | |
| 4 | Sprinkler Reduction | | | Reduction | | |
| | (2) | Adequately Designed System (NFPA 13) | Yes | -30% | -4,250 | |
| | | Standard Water Supply | Yes | -10% | | |
| | | Fully Supervised System | Yes | -10% | | |
| | | | | Cumulative Total | -50% | |
| 5 | Exposure Surcharge (cumulative %) | | | Surcharge | | |
| | (3) | North Side | 20.1 - 30 m | | 2,550 | |
| | | East Side | 30.1 - 45 m | | | |
| | | South Side | 10.1 - 20 m | | | |
| | | West Side | > 45.1m | | | |
| | | | | Cumulative Total | 30% | |
| Results | | | | | | |
| 6 | (1) + (2) + (3) | Total Required Fire Flow, rounded to nearest 1000L/min | | | L/min 7,000 | |
| | | (2,000 L/min < Fire Flow < 45,000 L/min) | | or | L/s 117 | |
| | | | | or | USGPM 1,849 | |
| 7 | Storage Volume | Required Duration of Fire Flow (hours) | | | Hours 2 | |
| | | Required Volume of Fire Flow (m ³) | | | m ³ 840 | |

Boundary Conditions at Fernbank-Abott site

Junction

Max HGL = 162.4m

PKHR = 155.5m

MXDY+Fire (167 L/s) = 152.9m

MXDY+Fire (217 L/s)= 151.2m

**INFORMATION FROM
FERNBANK CROSSING PHASE
1 & 2 SERVICING DESIGN BRIEF**

Note:

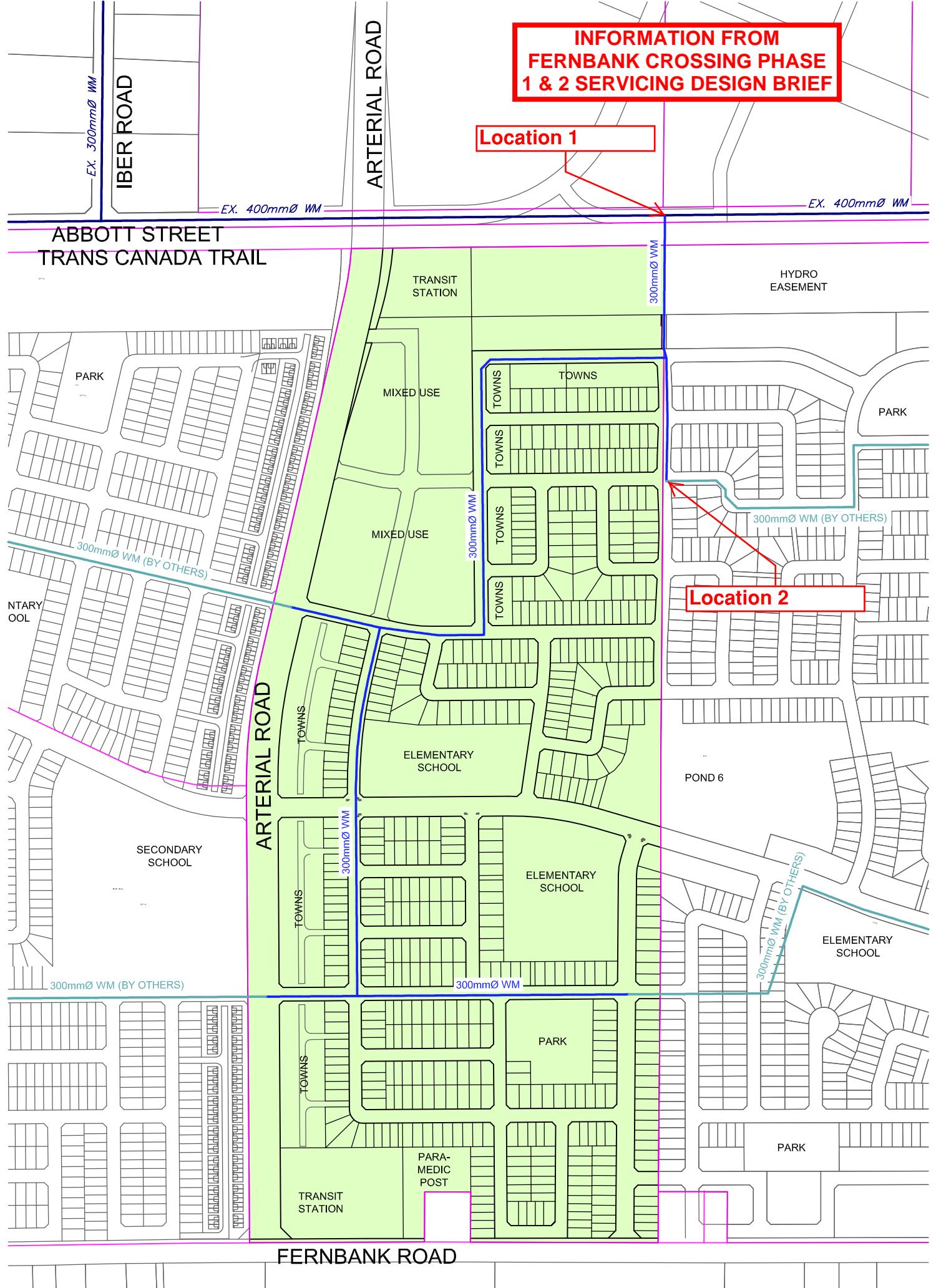
The site exceeds standard Bench Mark of maximum pressure (80 psi). Therefore, according to the City's guidelines it requires Pressure Reducing Valve (PRV) to maintain a safe and continuous water supply.

Location of Connections:

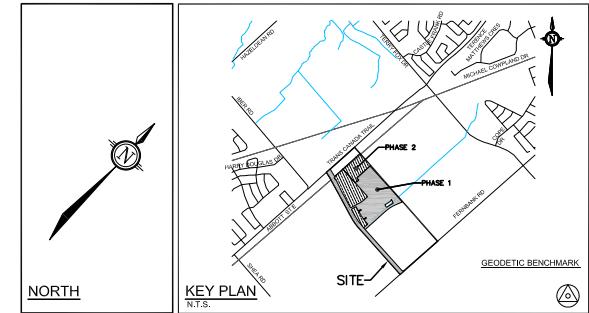
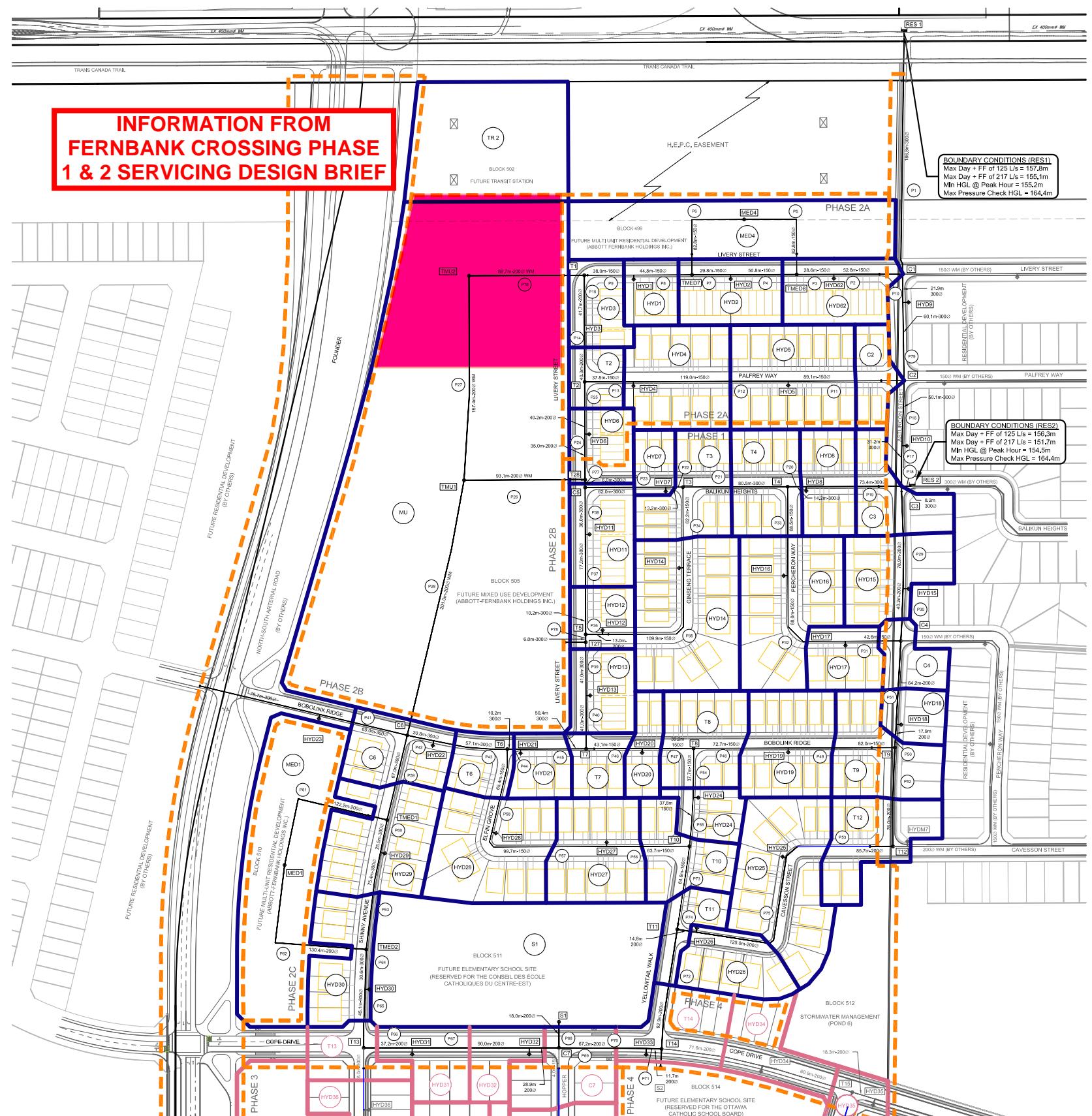


Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation. Fire Flow analysis is a reflection of available flow in the watermain; there may be additional restrictions that occur between the watermain and the hydrant that the model cannot take into account.

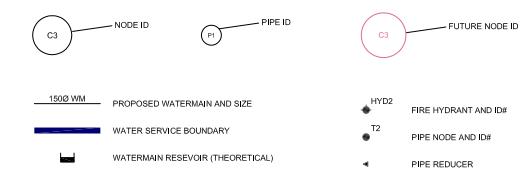
**INFORMATION FROM
FERNBANK CROSSING PHASE
1 & 2 SERVICING DESIGN BRIEF**



**INFORMATION FROM
FERNBANK CROSSING PHASE
1 & 2 SERVICING DESIGN BRIEF**



LEGEND



WATERMAIN NODE TABLE

| NODE ID | FIG ELEVATION | AVG. DAY DEMAND | MAX DAY | PEAK FLOW | FIRE FLOW |
|---------|---------------|-----------------|---------|-----------|-----------|
| C1 | 102.23 | 0.000 | 0.000 | 0.000 | - |
| C2 | 102.07 | 0.055 | 0.138 | 0.303 | - |
| C3 | 101.96 | 0.083 | 0.207 | 0.455 | - |
| C4 | 101.83 | 0.028 | 0.069 | 0.152 | - |
| C5 | 103.52 | 0.000 | 0.000 | 0.000 | - |
| C6 | 104.89 | 0.055 | 0.137 | 0.301 | - |
| C7 | 102.87 | 0.000 | 0.000 | 0.000 | - |
| HYD1 | 102.73 | 0.055 | 0.137 | 0.301 | 125 |
| HYD2 | 102.55 | 0.131 | 0.328 | 0.722 | 125 |
| HYD3 | 103.20 | 0.077 | 0.191 | 0.421 | 217 |
| HYD4 | 102.95 | 0.138 | 0.344 | 0.758 | 125 |
| HYD5 | 102.63 | 0.207 | 0.516 | 1.136 | 125 |
| HYD6 | 103.45 | 0.077 | 0.191 | 0.421 | 217 |
| HYD7 | 102.80 | 0.041 | 0.103 | 0.227 | 125 |
| HYD8 | 102.15 | 0.096 | 0.241 | 0.530 | 125 |
| HYD9 | 102.18 | 0.000 | 0.000 | 0.000 | 125 |
| HYD10 | 101.94 | 0.000 | 0.000 | 0.000 | 125 |
| HYD11 | 103.42 | 0.109 | 0.273 | 0.602 | 217 |
| HYD12 | 103.33 | 0.044 | 0.103 | 0.241 | 217 |
| HYD13 | 103.08 | 0.098 | 0.246 | 0.541 | 217 |
| HYD14 | 102.92 | 0.207 | 0.516 | 1.136 | 125 |
| HYD15 | 101.93 | 0.110 | 0.275 | 0.606 | 125 |
| HYD16 | 102.41 | 0.165 | 0.413 | 0.909 | 125 |
| HYD17 | 101.96 | 0.055 | 0.138 | 0.303 | 125 |
| HYD18 | 101.70 | 0.041 | 0.103 | 0.227 | 125 |
| HYD19 | 102.05 | 0.165 | 0.413 | 0.909 | 125 |
| HYD20 | 102.81 | 0.055 | 0.138 | 0.303 | 125 |
| HYD21 | 103.62 | 0.041 | 0.103 | 0.227 | 217 |
| HYD22 | 104.62 | 0.000 | 0.000 | 0.000 | 217 |
| HYD23 | 106.50 | 0.000 | 0.000 | 0.000 | 217 |
| HYD24 | 102.83 | 0.041 | 0.103 | 0.227 | 125 |
| HYD25 | 101.98 | 0.165 | 0.413 | 0.909 | 125 |
| HYD26 | 102.34 | 0.069 | 0.172 | 0.379 | 217 |
| HYD27 | 103.03 | 0.138 | 0.344 | 0.758 | 125 |
| HYD28 | 103.55 | 0.138 | 0.344 | 0.756 | 125 |
| HYD29 | 104.83 | 0.131 | 0.328 | 0.722 | 125 |
| HYD30 | 104.48 | 0.077 | 0.191 | 0.421 | 217 |
| HYD31 | 104.10 | 0.041 | 0.103 | 0.227 | 217 |
| HYD32 | 103.20 | 0.028 | 0.069 | 0.152 | 217 |
| HYD33 | 102.55 | 0.000 | 0.000 | 0.000 | 217 |
| HYD34 | 102.35 | 0.131 | 0.328 | 0.722 | 125 |
| MED1 | 105.33 | 0.911 | 2.279 | 5.013 | 125 |
| MED4 | 102.75 | 0.687 | 1.717 | 3.776 | 125 |
| S1 | 103.50 | 0.684 | 1.026 | 1.846 | - |
| T1 | 102.98 | 0.000 | 0.000 | 0.000 | - |
| T2 | 103.14 | 0.044 | 0.109 | 0.241 | - |
| T3 | 102.66 | 0.124 | 0.310 | 0.686 | - |
| T4 | 102.42 | 0.110 | 0.275 | 0.606 | - |
| T5 | 103.33 | 0.000 | 0.000 | 0.000 | - |
| T6 | 103.93 | 0.041 | 0.103 | 0.227 | - |
| T7 | 102.97 | 0.041 | 0.103 | 0.227 | - |
| T8 | 102.33 | 0.110 | 0.275 | 0.606 | - |
| T9 | 101.66 | 0.124 | 0.310 | 0.682 | - |
| T10 | 102.65 | 0.083 | 0.207 | 0.455 | - |
| T11 | 102.33 | 0.028 | 0.068 | 0.152 | - |
| T12 | 101.36 | 0.096 | 0.241 | 0.530 | - |
| T13 | 104.37 | 0.000 | 0.000 | 0.000 | - |
| T14 | 102.39 | 0.000 | 0.000 | 0.000 | - |
| T27 | 103.33 | 0.000 | 0.000 | 0.000 | - |
| T28 | 103.58 | 0.000 | 0.000 | 0.000 | - |
| TMED1 | 104.53 | 0.000 | 0.000 | 0.000 | - |
| TMED2 | 104.38 | 0.000 | 0.000 | 0.000 | - |
| TMED7 | 104.53 | 0.000 | 0.000 | 0.000 | - |
| TMED8 | 102.41 | 0.000 | 0.000 | 0.000 | - |
| TMU1 | 107.57 | 2.946 | 6.391 | 13.476 | 217 |
| TMU2 | 103.54 | 0.000 | 0.000 | 0.000 | 217 |

NOTE:
THE POSITION OF ALL POLE LINES, CONDUITS,
WATERMAINS, SEWERS AND OTHER
UNDERGROUND AND OVERGROUND UTILITIES AND
STRUCTURES IS NOT NECESSARILY SHOWN ON
THE CONTRACT DRAWINGS AND WHERE SHOWN,
THE ACCURACY OF THE POSITIONING
OF UTILITIES AND STRUCTURES IS NOT GUARANTEED.
BEFORE STARTING WORK, DETERMINE THE EXACT
LOCATION OF ALL SUCH UTILITIES AND
STRUCTURES AND ASSUME ALL LIABILITY FOR
DAMAGE TO THEM.

FERNBANK
CROSSING
the Heart of the Community

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THE REGIONAL GROUP
Corporate Head Office
175 Woodroffe Avenue, Suite 100
Ottawa, Ontario K2B 7J2
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SCALE
1:1500
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No. REVISION DATE BY

DESIGN
KJM
CHECKED MAB
DRAWN RCH
REVIEWED
KJM
APPROVED MAB
LICENCED PROFESSIONAL ENGINEER
J.J. MURPHY
100123021
PROVINCE OF ONTARIO
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CITY OF OTTAWA
FERNBANK CROSSING
PROJECT NO.
108180-10
REV #
DRAWING NO.
108180-WTR1

WATERMAIN DISTRIBUTION PLAN
PHASE 1 & 2

Fernbank Crossing - Watermain Analysis

Network Table - Nodes - (Peak Hour)

| Node ID | Elevation m | Demand LPS | Head m | Pressure m | Pressure kPa | Pressure psi |
|----------------|---------------|------------|---------------|--------------|---------------|--------------|
| Junc C1 | 102.2 | 0 | 154.75 | 52.52 | 515.22 | 74.73 |
| Junc C2 | 102.07 | 0.3 | 154.61 | 52.54 | 515.42 | 74.75 |
| Junc C3 | 101.96 | 0.46 | 154.5 | 52.54 | 515.42 | 74.75 |
| Junc C4 | 101.83 | 0.15 | 154.44 | 52.61 | 516.10 | 74.85 |
| Junc C5 | 103.52 | 0 | 154.41 | 50.89 | 499.23 | 72.41 |
| Junc C6 | 104.89 | 0.3 | 154.37 | 49.48 | 485.40 | 70.40 |
| Junc C7 | 102.87 | 0 | 154.37 | 51.5 | 505.22 | 73.28 |
| Junc HYD1 | 102.73 | 0.3 | 154.43 | 51.7 | 507.18 | 73.56 |
| Junc HYD2 | 102.55 | 0.72 | 154.47 | 51.92 | 509.34 | 73.87 |
| Junc HYD3 | 103.2 | 0.42 | 154.41 | 51.21 | 502.37 | 72.86 |
| Junc HYD4 | 102.95 | 0.76 | 154.43 | 51.48 | 505.02 | 73.25 |
| Junc HYD5 | 102.63 | 1.14 | 154.51 | 51.88 | 508.94 | 73.82 |
| Junc HYD6 | 103.45 | 0.42 | 154.41 | 50.96 | 499.92 | 72.51 |
| Junc HYD7 | 102.8 | 0.23 | 154.42 | 51.62 | 506.39 | 73.45 |
| Junc HYD8 | 102.15 | 0.53 | 154.46 | 52.31 | 513.16 | 74.43 |
| Junc HYD9 | 102.18 | 0 | 154.71 | 52.53 | 515.32 | 74.74 |
| Junc HYD10 | 101.94 | 0 | 154.54 | 52.6 | 516.01 | 74.84 |
| Junc HYD11 | 103.42 | 0.6 | 154.4 | 50.98 | 500.11 | 72.54 |
| Junc HYD12 | 103.33 | 0.24 | 154.39 | 51.06 | 500.90 | 72.65 |
| Junc HYD13 | 103.08 | 0.54 | 154.39 | 51.31 | 503.35 | 73.00 |
| Junc HYD14 | 102.92 | 1.14 | 154.41 | 51.49 | 505.12 | 73.26 |
| Junc HYD15 | 101.93 | 0.61 | 154.46 | 52.53 | 515.32 | 74.74 |
| Junc HYD16 | 102.41 | 0.91 | 154.45 | 52.04 | 510.51 | 74.04 |
| Junc HYD17 | 101.96 | 0.3 | 154.44 | 52.48 | 514.83 | 74.67 |
| Junc HYD18 | 101.7 | 0.23 | 154.41 | 52.71 | 517.09 | 75.00 |
| Junc HYD19 | 102.05 | 0.91 | 154.39 | 52.34 | 513.46 | 74.47 |
| Junc HYD20 | 102.81 | 0.3 | 154.38 | 51.57 | 505.90 | 73.37 |
| Junc HYD21 | 103.62 | 0.23 | 154.38 | 50.76 | 497.96 | 72.22 |
| Junc HYD22 | 104.62 | 0 | 154.37 | 49.75 | 488.05 | 70.79 |
| Junc HYD23 | 106.5 | 0 | 154.37 | 47.87 | 469.60 | 68.11 |
| Junc HYD24 | 102.63 | 0.23 | 154.38 | 51.75 | 507.67 | 73.63 |
| Junc HYD25 | 101.98 | 0.91 | 154.38 | 52.4 | 514.04 | 74.56 |
| Junc HYD26 | 102.4 | 0.38 | 154.37 | 51.97 | 509.83 | 73.94 |
| Junc HYD27 | 103.03 | 0.76 | 154.37 | 51.34 | 503.65 | 73.05 |
| Junc HYD28 | 103.55 | 0.76 | 154.37 | 50.82 | 498.54 | 72.31 |
| Junc HYD29 | 104.83 | 0.72 | 154.37 | 49.54 | 485.99 | 70.49 |
| Junc HYD30 | 104.48 | 0.42 | 154.37 | 49.89 | 489.42 | 70.98 |
| Junc HYD31 | 104.1 | 0.23 | 154.37 | 50.27 | 493.15 | 71.53 |
| Junc HYD32 | 103.2 | 0.15 | 154.37 | 51.17 | 501.98 | 72.81 |
| Junc HYD33 | 102.55 | 0 | 154.37 | 51.82 | 508.35 | 73.73 |
| Junc HYD62 | 102.35 | 0.72 | 154.59 | 52.24 | 512.47 | 74.33 |
| Junc MED1 | 105.33 | 5.01 | 154.36 | 49.03 | 480.98 | 69.76 |
| Junc MED4 | 102.75 | 3.78 | 154.46 | 51.71 | 507.28 | 73.57 |
| Junc RED112 | 103.12 | 0 | 154.39 | 51.27 | 502.96 | 72.95 |
| Junc S1 | 103.51 | 1.85 | 154.36 | 50.85 | 498.84 | 72.35 |
| Junc T1 | 102.98 | 0 | 154.41 | 51.43 | 504.53 | 73.18 |
| Junc T2 | 103.14 | 0.24 | 154.41 | 51.27 | 502.96 | 72.95 |
| Junc T3 | 102.56 | 0.68 | 154.43 | 51.87 | 508.84 | 73.80 |
| Junc T4 | 102.42 | 0.61 | 154.46 | 52.04 | 510.51 | 74.04 |
| Junc T5 | 103.33 | 0 | 154.39 | 51.06 | 500.90 | 72.65 |
| Junc T6 | 103.93 | 0.15 | 154.38 | 50.45 | 494.91 | 71.78 |
| Junc T7 | 102.97 | 0.23 | 154.38 | 51.41 | 504.33 | 73.15 |
| Junc T8 | 102.33 | 0.61 | 154.38 | 52.05 | 510.61 | 74.06 |
| Junc T9 | 101.66 | 0.68 | 154.41 | 52.75 | 517.48 | 75.05 |
| Junc T10 | 102.65 | 0.46 | 154.37 | 51.72 | 507.37 | 73.59 |
| Junc T11 | 102.33 | 0.15 | 154.37 | 52.04 | 510.51 | 74.04 |
| Junc T12 | 101.38 | 0.53 | 154.39 | 53.01 | 520.03 | 75.42 |
| Junc T13 | 104.37 | 0 | 154.37 | 50 | 490.50 | 71.14 |
| Junc T14 | 102.39 | 0 | 154.37 | 51.98 | 509.92 | 73.96 |
| Junc T27 | 103.33 | 0 | 154.39 | 51.06 | 500.90 | 72.65 |
| Junc T28 | 103.58 | 0 | 154.4 | 50.82 | 498.54 | 72.31 |
| Junc TMED1 | 104.53 | 0 | 154.37 | 49.84 | 488.93 | 70.91 |
| Junc TMED2 | 104.38 | 0 | 154.37 | 49.99 | 490.40 | 71.13 |
| Junc TMED7 | 102.62 | 0 | 154.45 | 51.83 | 508.45 | 73.74 |
| Junc TMED8 | 102.41 | 0 | 154.51 | 52.1 | 511.10 | 74.13 |
| Junc TMU1 | 107.57 | 13.48 | 154.36 | 46.79 | 459.01 | 66.57 |
| Junc TMU2 | 103.54 | 0 | 154.39 | 50.85 | 498.84 | 72.35 |
| Resvr RES1 | 155.2 | -53.02 | 155.2 | 0 | 0.00 | 0.00 |
| Resvr RES2 | 154.5 | 7.57 | 154.5 | 0 | 0.00 | 0.00 |

**INFORMATION FROM
FERNBANK CROSSING PHASE
1 & 2 SERVICING DESIGN BRIEF**

Fernbank Crossing - Watermain Analysis

Network Table - Links - (Peak Hour)

| Link ID | Length m | Diameter mm | Roughness | Flow LPS | Velocity m/s | Headloss m/km | Friction Factor |
|----------|-------------|----------------|-----------|-------------|-----------------|------------------|--------------------|
| Pipe P1 | 187 | 297 | 120 | 53.02 | 0.77 | 2.42 | 0.024 |
| Pipe P2 | 53 | 155 | 100 | -9.09 | 0.48 | 3.07 | 0.040 |
| Pipe P3 | 29 | 155 | 100 | -8.36 | 0.44 | 2.63 | 0.041 |
| Pipe P4 | 51 | 155 | 100 | -4.34 | 0.23 | 0.78 | 0.045 |
| Pipe P5 | 83 | 155 | 100 | 4.02 | 0.21 | 0.68 | 0.045 |
| Pipe P6 | 83 | 155 | 100 | 0.24 | 0.01 | 0.00 | 0.070 |
| Pipe P7 | 30 | 155 | 100 | -3.62 | 0.19 | 0.56 | 0.046 |
| Pipe P8 | 45 | 155 | 100 | 3.87 | 0.20 | 0.63 | 0.046 |
| Pipe P9 | 38 | 155 | 100 | 3.56 | 0.19 | 0.54 | 0.046 |
| Pipe P10 | 22 | 297 | 120 | 43.94 | 0.63 | 1.71 | 0.025 |
| Pipe P11 | 89 | 155 | 100 | -5.25 | 0.28 | 1.11 | 0.044 |
| Pipe P12 | 119 | 155 | 100 | -4.12 | 0.22 | 0.71 | 0.045 |
| Pipe P13 | 38 | 155 | 100 | -3.36 | 0.18 | 0.49 | 0.047 |
| Pipe P14 | 40 | 204 | 110 | -1.25 | 0.04 | 0.02 | 0.047 |
| Pipe P15 | 42 | 204 | 110 | -0.83 | 0.03 | 0.01 | 0.050 |
| Pipe P16 | 50 | 297 | 120 | 38.38 | 0.55 | 1.33 | 0.025 |
| Pipe P17 | 31 | 297 | 120 | 38.38 | 0.55 | 1.33 | 0.025 |
| Pipe P18 | 8 | 297 | 120 | 7.57 | 0.11 | 0.07 | 0.032 |
| Pipe P19 | 73 | 297 | 120 | 22.66 | 0.33 | 0.50 | 0.027 |
| Pipe P20 | 14 | 297 | 120 | 22.13 | 0.32 | 0.48 | 0.027 |
| Pipe P21 | 81 | 297 | 120 | 19.83 | 0.29 | 0.39 | 0.028 |
| Pipe P22 | 13 | 297 | 120 | 16.46 | 0.24 | 0.28 | 0.029 |
| Pipe P23 | 62 | 297 | 120 | 16.23 | 0.23 | 0.27 | 0.029 |
| Pipe P24 | 35 | 204 | 110 | 1.45 | 0.04 | 0.02 | 0.046 |
| Pipe P25 | 40 | 204 | 110 | 1.87 | 0.06 | 0.04 | 0.044 |
| Pipe P26 | 93 | 204 | 110 | -7.31 | 0.22 | 0.45 | 0.036 |
| Pipe P27 | 157 | 204 | 110 | 4.39 | 0.13 | 0.18 | 0.039 |
| Pipe P28 | 201 | 204 | 110 | -1.78 | 0.05 | 0.03 | 0.044 |
| Pipe P29 | 79 | 204 | 110 | 7.70 | 0.24 | 0.50 | 0.036 |
| Pipe P30 | 40 | 204 | 110 | 7.09 | 0.22 | 0.43 | 0.036 |
| Pipe P31 | 43 | 155 | 100 | -0.48 | 0.03 | 0.01 | 0.062 |
| Pipe P32 | 88 | 155 | 100 | -0.78 | 0.04 | 0.03 | 0.058 |
| Pipe P33 | 69 | 155 | 100 | -1.69 | 0.09 | 0.14 | 0.052 |
| Pipe P34 | 62 | 155 | 100 | 2.69 | 0.14 | 0.32 | 0.048 |
| Pipe P35 | 105 | 155 | 100 | -1.56 | 0.08 | 0.12 | 0.052 |
| Pipe P36 | 13 | 204 | 110 | 1.32 | 0.04 | 0.02 | 0.046 |
| Pipe P37 | 77 | 297 | 120 | 9.77 | 0.14 | 0.11 | 0.031 |
| Pipe P38 | 36 | 297 | 120 | 10.37 | 0.15 | 0.12 | 0.031 |
| Pipe P39 | 41 | 297 | 120 | -11.09 | 0.16 | 0.13 | 0.030 |
| Pipe P40 | 41 | 297 | 120 | 10.55 | 0.15 | 0.12 | 0.031 |
| Pipe P41 | 69 | 297 | 120 | 0.00 | 0.00 | 0.00 | 0.000 |
| Pipe P42 | 21 | 297 | 120 | -8.22 | 0.12 | 0.08 | 0.032 |
| Pipe P43 | 57 | 297 | 120 | -8.22 | 0.12 | 0.08 | 0.032 |
| Pipe P44 | 10 | 297 | 120 | -9.28 | 0.13 | 0.10 | 0.031 |
| Pipe P45 | 50 | 297 | 120 | -9.51 | 0.14 | 0.10 | 0.031 |
| Pipe P46 | 43 | 155 | 100 | 0.81 | 0.04 | 0.04 | 0.057 |
| Pipe P47 | 40 | 155 | 100 | 0.51 | 0.03 | 0.01 | 0.061 |
| Pipe P48 | 73 | 155 | 100 | -1.42 | 0.08 | 0.10 | 0.053 |
| Pipe P49 | 82 | 155 | 100 | -2.33 | 0.12 | 0.25 | 0.049 |
| Pipe P50 | 18 | 204 | 110 | -7.19 | 0.22 | 0.44 | 0.036 |
| Pipe P51 | 64 | 204 | 110 | -7.41 | 0.23 | 0.46 | 0.036 |
| Pipe P52 | 76 | 204 | 110 | 4.18 | 0.13 | 0.16 | 0.039 |
| Pipe P53 | 86 | 204 | 110 | 3.65 | 0.11 | 0.12 | 0.040 |
| Pipe P54 | 38 | 155 | 100 | 1.32 | 0.07 | 0.09 | 0.054 |
| Pipe P55 | 38 | 155 | 100 | 1.09 | 0.06 | 0.06 | 0.055 |
| Pipe P56 | 64 | 155 | 100 | 0.61 | 0.03 | 0.02 | 0.060 |
| Pipe P57 | 100 | 155 | 100 | -0.15 | 0.01 | 0.00 | 0.074 |
| Pipe P58 | 65 | 155 | 100 | -0.91 | 0.05 | 0.04 | 0.057 |
| Pipe P59 | 67 | 297 | 120 | 6.14 | 0.09 | 0.04 | 0.033 |
| Pipe P60 | 26 | 297 | 120 | 3.49 | 0.05 | 0.02 | 0.036 |
| Pipe P61 | 122 | 204 | 110 | -2.65 | 0.08 | 0.07 | 0.042 |
| Pipe P62 | 130 | 204 | 110 | -2.36 | 0.07 | 0.06 | 0.043 |
| Pipe P63 | 75 | 297 | 120 | 2.77 | 0.04 | 0.01 | 0.037 |
| Pipe P64 | 31 | 297 | 120 | 0.41 | 0.01 | 0.00 | 0.051 |
| Pipe P65 | 45 | 297 | 120 | -0.01 | 0.00 | 0.00 | 0.000 |
| Pipe P66 | 37 | 204 | 110 | -0.01 | 0.00 | 0.00 | 0.000 |
| Pipe P67 | 90 | 204 | 110 | -0.24 | 0.01 | 0.00 | 0.061 |
| Pipe P68 | 29 | 204 | 110 | -0.39 | 0.01 | 0.00 | 0.053 |
| Pipe P69 | 18 | 204 | 110 | -1.85 | 0.06 | 0.04 | 0.044 |
| Pipe P70 | 61 | 204 | 110 | -2.24 | 0.07 | 0.05 | 0.043 |
| Pipe P71 | 12 | 204 | 110 | -2.24 | 0.07 | 0.05 | 0.043 |
| Pipe P72 | 93 | 204 | 110 | -2.24 | 0.07 | 0.05 | 0.043 |
| Pipe P73 | 65 | 155 | 100 | -0.03 | 0.00 | 0.00 | 0.000 |
| Pipe P74 | 15 | 204 | 110 | 2.36 | 0.07 | 0.06 | 0.042 |
| Pipe P75 | 125 | 204 | 110 | -2.74 | 0.08 | 0.07 | 0.042 |
| Pipe P76 | 89 | 204 | 110 | 4.39 | 0.13 | 0.18 | 0.039 |
| Pipe P77 | 6 | 297 | 120 | -5.86 | 0.08 | 0.04 | 0.033 |
| Pipe P78 | 6 | 297 | 120 | -11.09 | 0.16 | 0.13 | 0.030 |
| Pipe P79 | 60 | 297 | 120 | 43.94 | 0.63 | 1.71 | 0.025 |
| Pipe P80 | 5 | 204 | 110 | -1.56 | 0.05 | 0.03 | 0.046 |

Fernbank Crossing - Watermain Analysis

Network Table - Nodes - (Max Pressure Check)

| Node ID | Elevation m | Demand LPS | Head m | Pressure m | Pressure kPa | Pressure psi |
|-------------|-------------|------------|--------|------------|--------------|--------------|
| Junc C1 | 102.2 | 0 | 164.4 | 62.2 | 610.18 | 88.50 |
| Junc C2 | 102.07 | 0.05 | 164.4 | 62.33 | 611.46 | 88.68 |
| Junc C3 | 101.96 | 0.08 | 164.4 | 62.44 | 612.54 | 88.84 |
| Junc C4 | 101.83 | 0.03 | 164.4 | 62.57 | 613.81 | 89.03 |
| Junc C5 | 103.52 | 0 | 164.39 | 60.87 | 597.13 | 86.61 |
| Junc C6 | 104.89 | 0.05 | 164.39 | 59.5 | 583.70 | 84.66 |
| Junc C7 | 103.87 | 0 | 164.39 | 60.52 | 593.70 | 86.11 |
| Junc HYD1 | 102.73 | 0.05 | 164.39 | 61.66 | 604.88 | 87.73 |
| Junc HYD2 | 102.55 | 0.13 | 164.39 | 61.84 | 606.65 | 87.99 |
| Junc HYD3 | 103.2 | 0.08 | 164.39 | 61.19 | 600.27 | 87.06 |
| Junc HYD4 | 102.95 | 0.14 | 164.39 | 61.44 | 602.73 | 87.42 |
| Junc HYD5 | 102.63 | 0.21 | 164.4 | 61.77 | 605.96 | 87.89 |
| Junc HYD6 | 103.45 | 0.08 | 164.39 | 60.94 | 597.82 | 86.71 |
| Junc HYD7 | 102.8 | 0.04 | 164.39 | 61.59 | 604.20 | 87.63 |
| Junc HYD8 | 102.15 | 0.1 | 164.4 | 62.25 | 610.67 | 88.57 |
| Junc HYD9 | 102.18 | 0 | 164.4 | 62.22 | 610.38 | 88.53 |
| Junc HYD10 | 101.94 | 0 | 164.4 | 62.46 | 612.73 | 88.87 |
| Junc HYD11 | 103.42 | 0.11 | 164.39 | 60.97 | 598.12 | 86.75 |
| Junc HYD12 | 103.33 | 0.04 | 164.39 | 61.06 | 599.00 | 86.88 |
| Junc HYD13 | 103.08 | 0.1 | 164.39 | 61.31 | 601.45 | 87.23 |
| Junc HYD14 | 102.92 | 0.21 | 164.39 | 61.47 | 603.02 | 87.46 |
| Junc HYD15 | 101.93 | 0.11 | 164.4 | 62.47 | 612.83 | 88.88 |
| Junc HYD16 | 102.41 | 0.17 | 164.4 | 61.99 | 608.12 | 88.20 |
| Junc HYD17 | 101.96 | 0.05 | 164.4 | 62.44 | 612.54 | 88.84 |
| Junc HYD18 | 101.7 | 0.04 | 164.39 | 62.69 | 614.99 | 89.20 |
| Junc HYD19 | 102.05 | 0.17 | 164.39 | 62.34 | 611.56 | 88.70 |
| Junc HYD20 | 102.81 | 0.05 | 164.39 | 61.58 | 604.10 | 87.62 |
| Junc HYD21 | 103.62 | 0.04 | 164.39 | 60.77 | 596.15 | 86.46 |
| Junc HYD22 | 104.62 | 0 | 164.39 | 59.77 | 586.34 | 85.04 |
| Junc HYD23 | 106.5 | 0 | 164.39 | 57.89 | 567.90 | 82.37 |
| Junc HYD24 | 102.63 | 0.04 | 164.39 | 61.76 | 605.87 | 87.87 |
| Junc HYD25 | 101.98 | 0.17 | 164.39 | 62.41 | 612.24 | 88.80 |
| Junc HYD26 | 102.4 | 0.07 | 164.39 | 61.99 | 608.12 | 88.20 |
| Junc HYD27 | 103.03 | 0.14 | 164.39 | 61.36 | 601.94 | 87.30 |
| Junc HYD28 | 103.55 | 0.14 | 164.39 | 60.84 | 596.84 | 86.56 |
| Junc HYD29 | 104.83 | 0.13 | 164.39 | 59.56 | 584.28 | 84.74 |
| Junc HYD30 | 104.48 | 0.08 | 164.39 | 59.91 | 587.72 | 85.24 |
| Junc HYD31 | 104.1 | 0.04 | 164.39 | 60.29 | 591.44 | 85.78 |
| Junc HYD32 | 103.2 | 0.03 | 164.39 | 61.19 | 600.27 | 87.06 |
| Junc HYD33 | 102.55 | 0 | 164.39 | 61.84 | 606.65 | 87.99 |
| Junc HYD62 | 102.35 | 0.13 | 164.4 | 62.05 | 608.71 | 88.29 |
| Junc MED1 | 105.33 | 0.91 | 164.39 | 59.06 | 579.38 | 84.03 |
| Junc MED4 | 102.75 | 0.69 | 164.39 | 61.64 | 604.69 | 87.70 |
| Junc RED112 | 103.12 | 0 | 164.39 | 61.27 | 601.06 | 87.18 |
| Junc S1 | 103.51 | 0.69 | 164.39 | 60.88 | 597.23 | 86.62 |
| Junc T1 | 102.98 | 0 | 164.39 | 61.41 | 602.43 | 87.38 |
| Junc T2 | 103.14 | 0.04 | 164.39 | 61.25 | 600.86 | 87.15 |
| Junc T3 | 102.56 | 0.12 | 164.39 | 61.83 | 606.55 | 87.97 |
| Junc T4 | 102.42 | 0.11 | 164.4 | 61.98 | 608.02 | 88.19 |
| Junc T5 | 103.33 | 0 | 164.39 | 61.06 | 599.00 | 86.88 |
| Junc T6 | 103.93 | 0.03 | 164.39 | 60.46 | 593.11 | 86.02 |
| Junc T7 | 102.97 | 0.04 | 164.39 | 61.42 | 602.53 | 87.39 |
| Junc T8 | 102.33 | 0.11 | 164.39 | 62.06 | 608.81 | 88.30 |
| Junc T9 | 101.66 | 0.12 | 164.39 | 62.73 | 615.38 | 89.25 |
| Junc T10 | 102.65 | 0.08 | 164.39 | 61.74 | 605.67 | 87.84 |
| Junc T11 | 102.33 | 0.03 | 164.39 | 62.06 | 608.81 | 88.30 |
| Junc T12 | 101.38 | 0.1 | 164.39 | 63.01 | 618.13 | 89.65 |
| Junc T13 | 104.37 | 0 | 164.39 | 60.02 | 588.80 | 85.40 |
| Junc T14 | 102.39 | 0 | 164.39 | 62 | 608.22 | 88.21 |
| Junc T27 | 103.33 | 0 | 164.39 | 61.06 | 599.00 | 86.88 |
| Junc T28 | 103.58 | 0 | 164.39 | 60.81 | 596.55 | 86.52 |
| Junc TMED1 | 104.53 | 0 | 164.39 | 59.86 | 587.23 | 85.17 |
| Junc TMED2 | 104.38 | 0 | 164.39 | 60.01 | 588.70 | 85.38 |
| Junc TMED7 | 102.62 | 0 | 164.39 | 61.77 | 605.96 | 87.89 |
| Junc TMED8 | 102.41 | 0 | 164.39 | 61.98 | 608.02 | 88.19 |
| Junc TMU1 | 107.57 | 2.95 | 164.39 | 56.82 | 557.40 | 80.84 |
| Junc TMU2 | 103.54 | 0 | 164.39 | 60.85 | 596.94 | 86.58 |
| Resvr RES1 | 164.4 | -1.47 | 164.4 | 0 | 0.00 | 0.00 |
| Resvr RES2 | 164.4 | -7.64 | 164.4 | 0 | 0.00 | 0.00 |

**INFORMATION FROM
FERNBANK CROSSING PHASE
1 & 2 SERVICING DESIGN BRIEF**

Fernbank Crossing - Watermain Analysis

Network Table - Links - (Max Pressure Check)

| Link ID | Length m | Diameter mm | Roughness | Flow LPS | Velocity m/s | Headloss m/km | Friction Factor |
|----------|----------|-------------|-----------|----------|--------------|---------------|-----------------|
| Pipe P1 | 187 | 297 | 120 | 1.47 | 0.02 | 0.00 | 0.041 |
| Pipe P2 | 53 | 155 | 100 | -1.20 | 0.06 | 0.07 | 0.054 |
| Pipe P3 | 29 | 155 | 100 | -1.07 | 0.06 | 0.06 | 0.055 |
| Pipe P4 | 51 | 155 | 100 | 0.55 | 0.03 | 0.02 | 0.061 |
| Pipe P5 | 83 | 155 | 100 | 0.53 | 0.03 | 0.02 | 0.061 |
| Pipe P6 | 83 | 155 | 100 | -0.16 | 0.01 | 0.00 | 0.066 |
| Pipe P7 | 30 | 155 | 100 | 0.41 | 0.02 | 0.01 | 0.066 |
| Pipe P8 | 45 | 155 | 100 | 0.25 | 0.01 | 0.00 | 0.063 |
| Pipe P9 | 73 | 155 | 100 | 0.20 | 0.01 | 0.00 | 0.070 |
| Pipe P10 | 22 | 297 | 120 | 0.27 | 0.00 | 0.00 | 0.000 |
| Pipe P11 | 89 | 155 | 100 | -0.85 | 0.04 | 0.04 | 0.057 |
| Pipe P12 | 119 | 155 | 100 | -0.64 | 0.03 | 0.02 | 0.060 |
| Pipe P13 | 38 | 155 | 100 | -0.50 | 0.03 | 0.01 | 0.061 |
| Pipe P14 | 40 | 204 | 110 | -0.71 | 0.02 | 0.01 | 0.051 |
| Pipe P15 | 42 | 204 | 110 | -0.64 | 0.02 | 0.00 | 0.052 |
| Pipe P16 | 50 | 297 | 120 | -0.64 | 0.01 | 0.00 | 0.026 |
| Pipe P17 | 31 | 297 | 120 | -0.64 | 0.01 | 0.00 | 0.082 |
| Pipe P18 | 8 | 297 | 120 | -7.64 | 0.11 | 0.07 | 0.032 |
| Pipe P19 | 73 | 297 | 120 | 5.22 | 0.08 | 0.03 | 0.034 |
| Pipe P20 | 14 | 297 | 120 | 5.13 | 0.07 | 0.03 | 0.033 |
| Pipe P21 | 81 | 297 | 120 | 4.70 | 0.07 | 0.03 | 0.035 |
| Pipe P22 | 13 | 297 | 120 | 4.00 | 0.06 | 0.02 | 0.035 |
| Pipe P23 | 62 | 297 | 120 | 3.95 | 0.06 | 0.02 | 0.035 |
| Pipe P24 | 35 | 204 | 110 | 0.33 | 0.01 | 0.00 | 0.042 |
| Pipe P25 | 40 | 204 | 110 | -0.25 | 0.01 | 0.00 | 0.062 |
| Pipe P26 | 93 | 204 | 110 | -1.60 | 0.05 | 0.03 | 0.045 |
| Pipe P27 | 157 | 204 | 110 | 0.83 | 0.03 | 0.01 | 0.050 |
| Pipe P28 | 201 | 204 | 110 | -0.51 | 0.02 | 0.00 | 0.054 |
| Pipe P29 | 79 | 204 | 110 | 1.70 | 0.05 | 0.03 | 0.045 |
| Pipe P30 | 40 | 204 | 110 | 1.59 | 0.05 | 0.03 | 0.046 |
| Pipe P31 | 43 | 155 | 100 | -0.09 | 0.00 | 0.00 | 0.054 |
| Pipe P32 | 88 | 155 | 100 | -0.15 | 0.01 | 0.00 | 0.083 |
| Pipe P33 | 69 | 155 | 100 | -0.31 | 0.02 | 0.01 | 0.066 |
| Pipe P34 | 62 | 155 | 100 | 0.58 | 0.03 | 0.02 | 0.060 |
| Pipe P35 | 105 | 155 | 100 | -0.38 | 0.02 | 0.01 | 0.065 |
| Pipe P36 | 13 | 204 | 110 | -0.33 | 0.01 | 0.00 | 0.056 |
| Pipe P37 | 77 | 297 | 120 | 1.91 | 0.03 | 0.01 | 0.039 |
| Pipe P38 | 36 | 297 | 120 | 2.02 | 0.03 | 0.01 | 0.039 |
| Pipe P39 | 41 | 297 | 120 | 2.24 | 0.03 | 0.01 | 0.038 |
| Pipe P40 | 41 | 297 | 120 | 2.15 | 0.03 | 0.01 | 0.039 |
| Pipe P41 | 69 | 297 | 120 | 0.00 | 0.00 | 0.00 | 0.000 |
| Pipe P42 | 21 | 297 | 120 | -1.85 | 0.03 | 0.01 | 0.044 |
| Pipe P43 | 57 | 297 | 120 | -1.85 | 0.03 | 0.00 | 0.037 |
| Pipe P44 | 10 | 297 | 120 | -2.00 | 0.03 | 0.01 | 0.051 |
| Pipe P45 | 50 | 297 | 120 | -2.04 | 0.03 | 0.01 | 0.037 |
| Pipe P46 | 43 | 155 | 100 | 0.06 | 0.00 | 0.00 | 0.000 |
| Pipe P47 | 40 | 155 | 100 | 0.01 | 0.00 | 0.00 | 0.000 |
| Pipe P48 | 73 | 155 | 100 | -0.38 | 0.02 | 0.01 | 0.063 |
| Pipe P49 | 82 | 155 | 100 | -0.54 | 0.03 | 0.02 | 0.061 |
| Pipe P50 | 18 | 204 | 110 | -1.61 | 0.05 | 0.03 | 0.046 |
| Pipe P51 | 64 | 204 | 110 | -1.65 | 0.05 | 0.03 | 0.045 |
| Pipe P52 | 76 | 204 | 110 | 0.95 | 0.03 | 0.01 | 0.048 |
| Pipe P53 | 86 | 204 | 110 | 0.85 | 0.03 | 0.01 | 0.050 |
| Pipe P54 | 38 | 155 | 100 | 0.27 | 0.01 | 0.00 | 0.072 |
| Pipe P55 | 38 | 155 | 100 | 0.23 | 0.01 | 0.00 | 0.069 |
| Pipe P56 | 64 | 155 | 100 | 0.15 | 0.01 | 0.00 | 0.069 |
| Pipe P57 | 100 | 155 | 100 | 0.01 | 0.00 | 0.00 | 0.000 |
| Pipe P58 | 65 | 155 | 100 | -0.12 | 0.01 | 0.00 | 0.060 |
| Pipe P59 | 67 | 297 | 120 | 1.29 | 0.02 | 0.00 | 0.042 |
| Pipe P60 | 26 | 297 | 120 | 0.79 | 0.01 | 0.00 | 0.032 |
| Pipe P61 | 122 | 204 | 110 | 0.49 | 0.02 | 0.00 | 0.054 |
| Pipe P62 | 130 | 204 | 110 | -0.42 | 0.01 | 0.00 | 0.056 |
| Pipe P63 | 75 | 297 | 120 | 0.66 | 0.01 | 0.00 | 0.047 |
| Pipe P64 | 31 | 297 | 120 | 0.24 | 0.00 | 0.00 | 0.000 |
| Pipe P65 | 45 | 297 | 120 | 0.17 | 0.00 | 0.00 | 0.000 |
| Pipe P66 | 37 | 204 | 110 | 0.17 | 0.01 | 0.00 | 0.077 |
| Pipe P67 | 90 | 204 | 110 | 0.13 | 0.00 | 0.00 | 0.056 |
| Pipe P68 | 29 | 204 | 110 | 0.10 | 0.00 | 0.00 | 0.286 |
| Pipe P69 | 18 | 204 | 110 | 0.69 | 0.02 | 0.01 | 0.047 |
| Pipe P70 | 61 | 204 | 110 | -0.59 | 0.02 | 0.00 | 0.053 |
| Pipe P71 | 12 | 204 | 110 | -0.59 | 0.02 | 0.00 | 0.059 |
| Pipe P72 | 93 | 204 | 110 | -0.59 | 0.02 | 0.00 | 0.052 |
| Pipe P73 | 65 | 155 | 100 | 0.00 | 0.00 | 0.00 | 0.000 |
| Pipe P74 | 15 | 204 | 110 | 0.62 | 0.02 | 0.01 | 0.056 |
| Pipe P75 | 125 | 204 | 110 | -0.69 | 0.02 | 0.01 | 0.051 |
| Pipe P76 | 89 | 204 | 110 | 0.83 | 0.03 | 0.01 | 0.050 |
| Pipe P77 | 6 | 297 | 120 | 1.93 | 0.03 | 0.01 | 0.046 |
| Pipe P78 | 6 | 297 | 120 | 2.24 | 0.03 | 0.01 | 0.052 |
| Pipe P79 | 60 | 297 | 120 | 0.27 | 0.00 | 0.00 | 0.000 |
| Pipe P80 | 5 | 204 | 110 | -0.38 | 0.01 | 0.00 | 0.000 |

Fernbank Crossing - Watermain Analysis

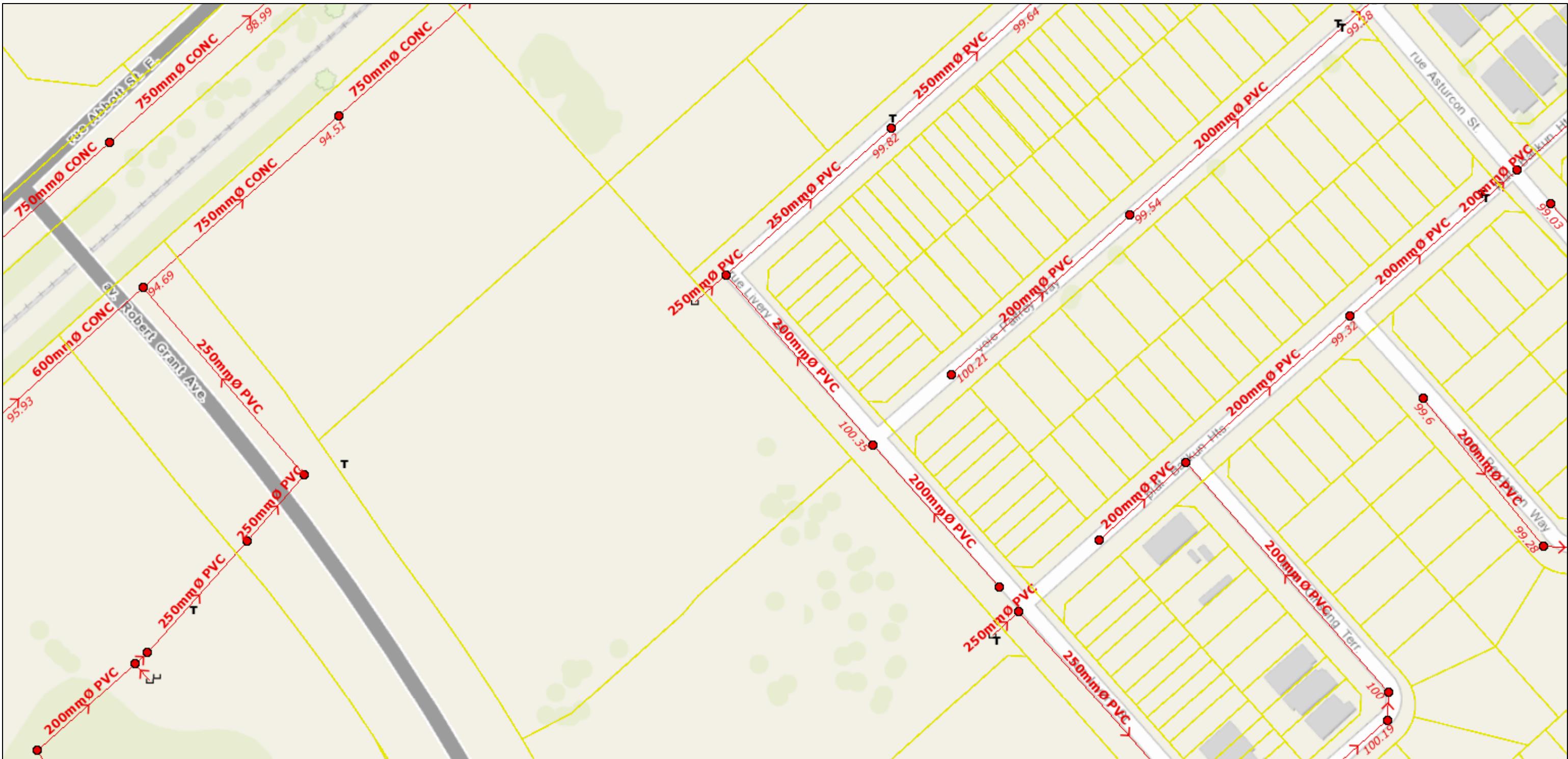
Network Table - Nodes - (Fire Flow Summary)

| Fire Flow | | Minimum Pressure | | |
|-----------|------------|------------------|----------------|-------|
| Node | Flow (L/s) | Pressure (kPa) | Pressure (PSI) | Node |
| HYD1 | 125 | 432.62 | 62.75 | HYD1 |
| HYD2 | 125 | 386.61 | 56.07 | HYD2 |
| HYD3 | 217 | 373.17 | 54.12 | HYD3 |
| HYD4 | 125 | 428.60 | 62.16 | HYD4 |
| HYD5 | 125 | 397.50 | 57.65 | HYD5 |
| HYD6 | 217 | 396.62 | 57.52 | TMU1 |
| HYD7 | 125 | 466.07 | 67.60 | 23 |
| HYD8 | 125 | 472.16 | 68.48 | 23 |
| HYD9 | 125 | 477.45 | 69.25 | TMU1 |
| HYD10 | 125 | 477.65 | 69.28 | TMU1 |
| HYD11 | 217 | 396.13 | 57.45 | TMU1 |
| HYD12 | 217 | 397.40 | 57.64 | TMU1 |
| HYD13 | 217 | 393.28 | 57.04 | HYD23 |
| HYD14 | 125 | 424.48 | 61.57 | HYD14 |
| HYD15 | 125 | 474.41 | 68.81 | TMU1 |
| HYD16 | 125 | 421.83 | 61.18 | HYD16 |
| HYD17 | 125 | 438.90 | 63.66 | HYD17 |
| HYD18 | 125 | 471.17 | 68.34 | TMU1 |
| HYD19 | 125 | 410.65 | 59.56 | HYD19 |
| HYD20 | 125 | 445.86 | 64.67 | HYD20 |
| HYD21 | 217 | 383.28 | 55.59 | HYD23 |
| HYD22 | 217 | 374.94 | 54.38 | HYD23 |
| HYD23 | 217 | 350.12 | 50.78 | HYD23 |
| HYD24 | 125 | 430.86 | 62.49 | HYD24 |
| HYD25 | 125 | 459.40 | 66.63 | HYD25 |
| HYD26 | 217 | 308.03 | 44.68 | HYD26 |
| HYD27 | 125 | 375.04 | 54.39 | HYD27 |
| HYD28 | 125 | 385.04 | 55.85 | HYD28 |
| HYD29 | 125 | 462.15 | 67.03 | HYD23 |
| HYD30 | 217 | 360.32 | 52.26 | HYD30 |
| HYD31 | 217 | 322.45 | 46.77 | HYD31 |
| HYD32 | 217 | 284.59 | 41.28 | HYD32 |
| HYD33 | 217 | 282.04 | 40.91 | HYD33 |
| HYD62 | 125 | 436.15 | 63.26 | HYD62 |
| MED1 | 125 | 436.45 | 63.30 | MED1 |
| MED4 | 125 | 335.40 | 48.65 | MED4 |
| TMU1 | 217 | 342.66 | 49.70 | TMU1 |
| TMU2 | 217 | 328.64 | 47.66 | TMU2 |

**INFORMATION FROM
FERNBANK CROSSING PHASE
1 & 2 SERVICING DESIGN BRIEF**

APPENDIX B
Sanitary Calculations

1000 Robert Grant Ave Sanitary Info



March 6, 2019

1:2,000

0 0.0225 0.045 0.075 0.09 mi
0 0.0375 0.075 0.15 km

□ Property Parcels

Upstream Invert / Radier amont

Downstream Invert / Radier aval

Sanitary Pipe Details / Détails de la conduite de réseau d'égout domestique

Sewer Fittings / Raccords

■ Cap / bouchon

■ Tee / raccord en T

● Sanitary Manholes / Regards d'égout domestique

Sanitary Pipes / Conduites d'égout domestique

—> Private / Branchement privé

—> Public / Branchement public

—> Combined Manholes / Regards d'égout unitaire

Combined Pipes / Conduites d'égout unitaire

—> Public / Branchement public

—> Private / Branchement privé

City of Ottawa

Sanitary Pump Stations and Treatment Plants / Installations d'infrastructure

■ Sanitary Pump Station / Station de pompage des eaux usées

■ Wastewater Treatment Plant / Usine d'épuration des eaux usées

RENE'S COURT SANITARY FLOWS

| LOCATION | | | | | | | | INFILTRATION | | | Total Flow (l/s) | PIPE | | | | | |
|-----------|------|----|-----------------|------|-------|-------------|-------------|-----------------|------------------|---------------------|------------------|-----------|------------|----------------|----------------------|-------------------------|-------|
| AREA | FROM | TO | Apartment Units | | TOTAL | | | Total Area (ha) | Accum. Area (ha) | Infiltr. Flow (l/s) | Size (mm) | Slope (%) | Length (m) | Capacity (l/s) | Full Flow Vel. (m/s) | Q/Q _{full} (%) | |
| | | | Avg Unit | Pop. | Pop. | Accum. Pop. | Peak Factor | | | | | | | | | | |
| Block 203 | EX | | 566 | 1019 | 1019 | 1019 | 3.2 | 10.69 | 2.017 | 2.017 | 0.67 | 11.35 | 200 | 2.00 | N/A | 46.3 | 1.48 |
| | | | | | | | | | | | | | | | | | 24.5% |

Design Parameters:

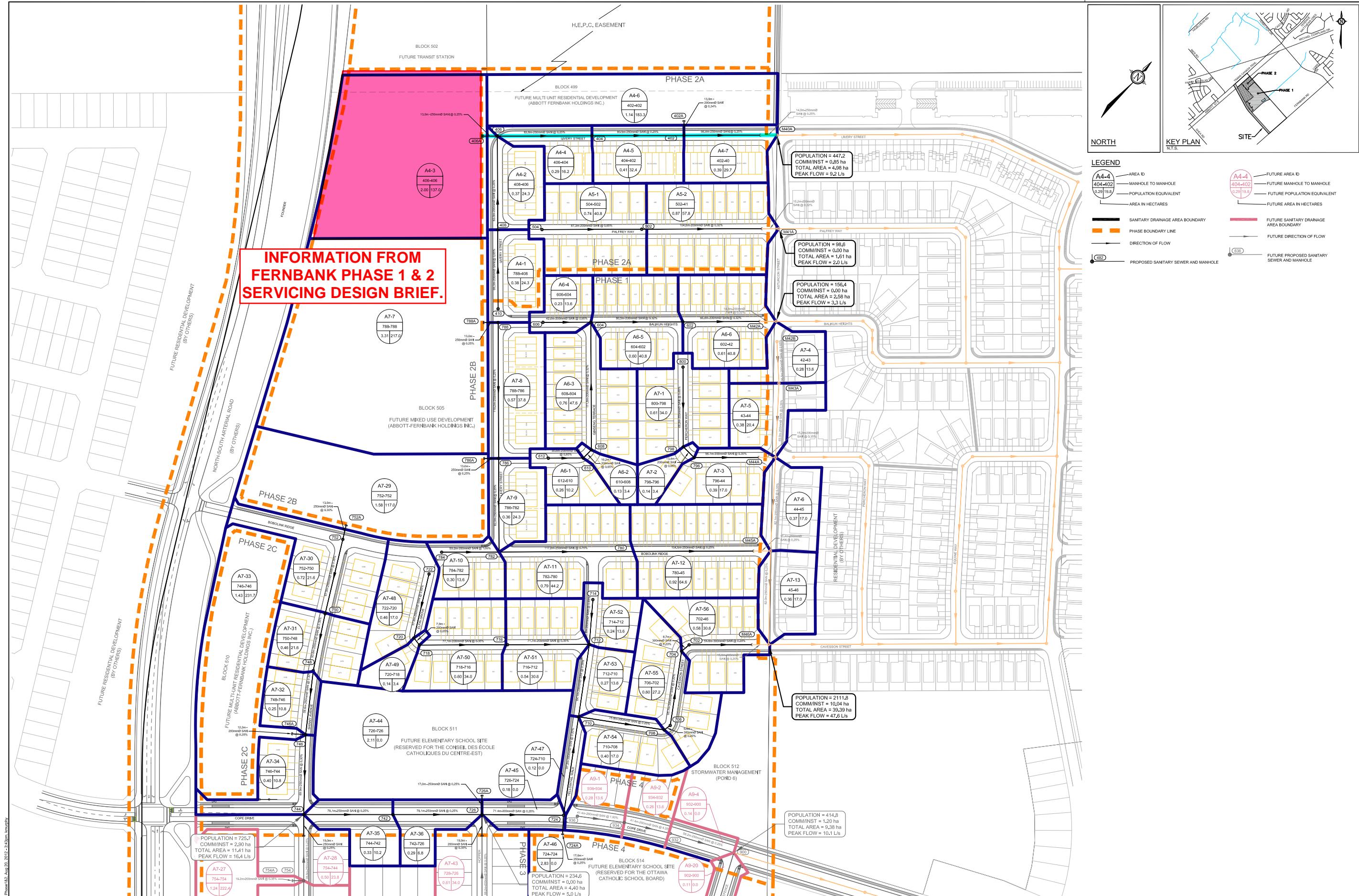
- Average Apartment = 1.8 persons/unit

Section 4.0 Ottawa Sewer Design Guidelines

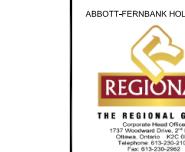
- Average Domestic Flow 280 L/person L/person/day

- Extraneous Flows 0.33 l/s/ha l/s/ha

Residential Peaking Factor Harmon Equation



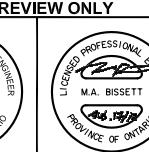
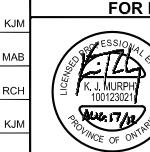
NOTE:
THE POSITION OF ALL POLE LINES, CONDUITS,
WATERMANS, SEWERS AND OTHER
UNDERGROUND AND OVERGROUND UTILITIES AND
STRUCTURES IS NOT NECESSARILY SHOWN ON
THE CONTRACT DRAWINGS, AND WHERE SHOWN,
THE ACCURACY OF THE POSITION OF SUCH
UTILITIES AND STRUCTURES IS NOT GUARANTEED.
BEFORE STARTING WORK, DETERMINE THE EXACT
LOCATION OF ALL SUCH UTILITIES AND
STRUCTURES AND ASSUME ALL LIABILITY FOR
DAMAGES TO THEM.



NC.

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|------------------------------------|
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| |
| 3. ISSUED FOR APPROVAL (PHASE 1&2) |
| 2. ISSUED FOR APPROVAL (PHASE 1&2) |
| 1. ISSUED FOR APPROVAL |

| | | SCALE | DESIGN |
|-----------|-----|------------------|----------|
| | | 1:1250 | CHECKED |
| | | | DRAWN |
| AUG 17/12 | KJM | | CHECKED |
| JUN 21/12 | KJM | 0 10 20 30 40 50 | APPROVED |
| MAR 9/12 | KJM | 1:1250 | |



| | | |
|---|---|---|
|  <p>NOVATECH ENGINEERING CONSULTANTS LTD. <small>ENGINEERS & PLANNERS</small></p> <p>Suite 200, 240 Michael Cowper Drive Ottawa, Ontario, Canada K2B 1P6 Telephone (613) 224-8625 Facsimile (613) 224-8627 Email: novattech-eng@novatech.ca</p> | <p>CITY OF OTTAWA FERNBANK CROSSING</p> <p>SANITARY DRAINAGE AREA PLAN PHASE 1 & 2</p> | <p>PROJECT #:</p> <p>108180-10</p> <p>REV:</p> <p>REV # 3</p> <p>DRAWN BY: [Signature]</p> <p>DKS/MS/ED 14c</p> |
|---|---|---|

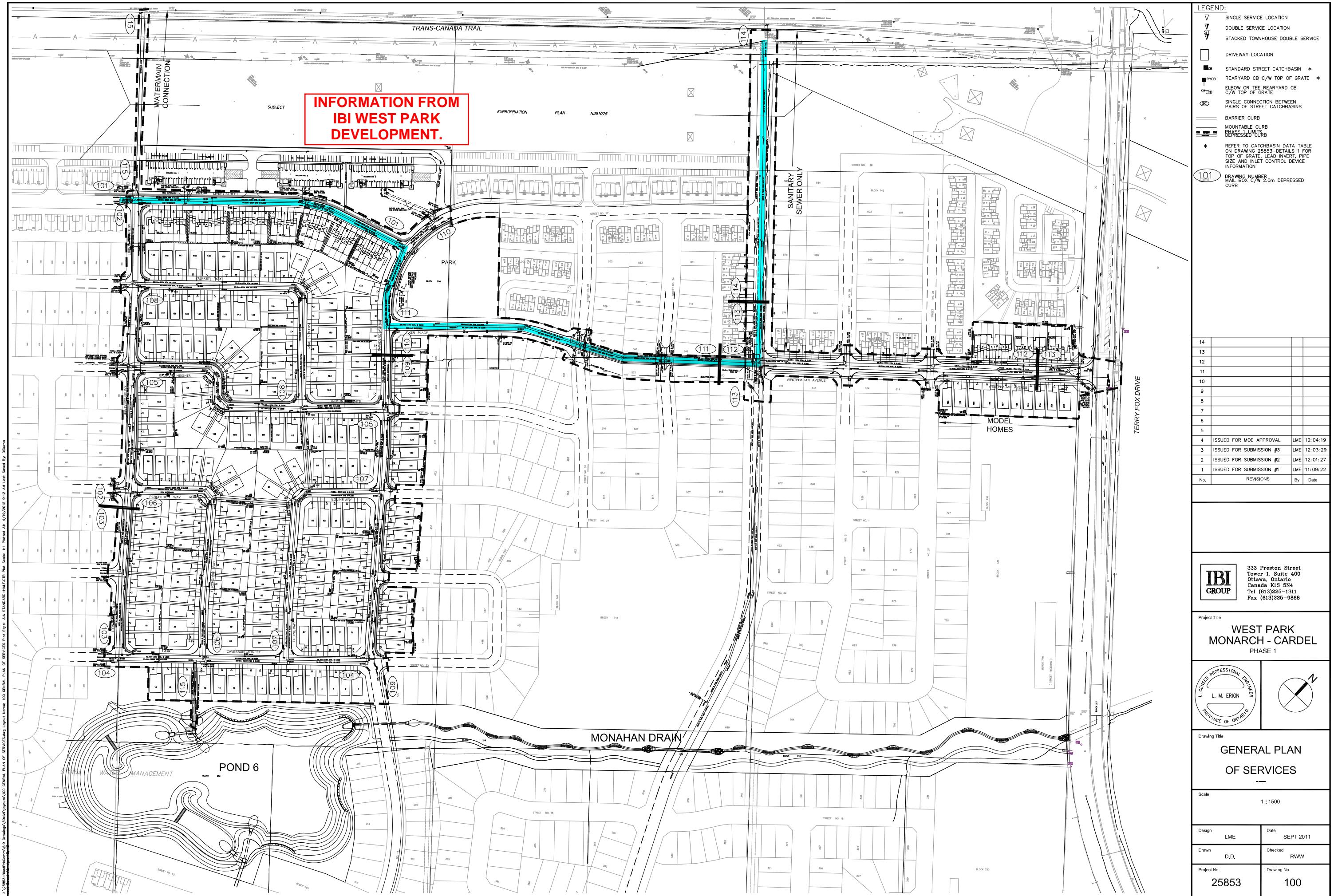
Fernbank Crossing - Sanitary Sewer Design Sheet

FLOW ALLOTED
FROM BLOCK 203

| AREA | | | RESIDENTIAL | | | | | | | | | | ICI | | | | INFILTRATION | | | Total Flow (l/s) | PIPE | | | | | | | |
|-------------------|------|-----|-------------|------|-------|------|------|-----------|---------------|-------|-------|-------------|----------------------|-------------------------|------------------|-----------------|-----------------|------------------|--------------------|------------------|-----------|-----------|------------|----------------|----------------------|-------------------------|------|-------|
| ID | From | To | SINGLES | | TOWNS | | | MIXED USE | | TOTAL | | | Commercial Area (ha) | Institutional Area (ha) | Accum. Area (ha) | Peak Flow (l/s) | Total Area (ha) | Accum. Area (ha) | Infilt. Flow (l/s) | | Size (mm) | Slope (%) | Length (m) | Capacity (l/s) | Full Flow Vel. (m/s) | Q/Q _{full} (%) | | |
| | | | Units | Pop. | Units | Pop. | Area | Pop. | Net Area (ha) | Pop. | Pop. | Accum. Pop. | Peak Factor | Peak Flow (l/s) | | | | | | | | | | | | | | |
| Outlet 400 | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 4-1 | 410 | 408 | 0 | 0.0 | 9 | 24.3 | 0.0 | 0.0 | 0.00 | 0.0 | 24.3 | 24.3 | 4.0 | 0.4 | 0.00 | 0.00 | 0.00 | 0.0 | 0.38 | 0.38 | 0.1 | 0.5 | 200 | 0.65 | 69.3 | 27.6 | 0.85 | 1.8% |
| 4-2 | 408 | 406 | 0 | 0.0 | 9 | 24.3 | 0.0 | 0.0 | 0.00 | 0.0 | 24.3 | 48.6 | 4.0 | 0.8 | 0.00 | 0.00 | 0.00 | 0.0 | 0.37 | 0.75 | 0.2 | 1.0 | 200 | 0.35 | 82.0 | 20.2 | 0.62 | 4.9% |
| 4-3 | 406A | 406 | 0 | 0.0 | 0 | 0.0 | 0.0 | 0.0 | 1.70 | 137.0 | 137.0 | 137.0 | 4.0 | 2.2 | 0.85 | 0.00 | 0.85 | 0.5 | 2.00 | 2.00 | 0.6 | 3.3 | 250 | 0.25 | 11.0 | 31.0 | 0.61 | 10.6% |
| 4-4 | 406 | 404 | 0 | 0.0 | 6 | 16.2 | 0.0 | 0.0 | 0.00 | 0.0 | 16.2 | 201.8 | 4.0 | 3.3 | 0.00 | 0.00 | 0.85 | 0.5 | 0.29 | 3.04 | 0.9 | 4.6 | 250 | 0.25 | 82.8 | 31.0 | 0.61 | 14.9% |
| 4-5 | 404 | 402 | 0 | 0.0 | 12 | 32.4 | 0.0 | 0.0 | 0.00 | 0.0 | 32.4 | 234.2 | 4.0 | 3.8 | 0.00 | 0.00 | 0.85 | 0.5 | 0.41 | 3.45 | 1.0 | 5.3 | 250 | 0.25 | 80.5 | 31.0 | 0.61 | 17.0% |
| 4-6 | 402A | 402 | 0 | 0.0 | 0 | 0.0 | 1.1 | 183.3 | 0.00 | 0.0 | 183.3 | 183.3 | 4.0 | 3.0 | 0.00 | 0.00 | 0.00 | 0.0 | 1.14 | 1.14 | 0.3 | 3.3 | 200 | 0.35 | 11.0 | 20.2 | 0.62 | 16.3% |
| 4-7 | 402 | 40A | 0 | 0.0 | 11 | 29.7 | 0.0 | 0.0 | 0.00 | 0.0 | 29.7 | 447.2 | 4.0 | 7.2 | 0.00 | 0.00 | 0.85 | 0.5 | 0.39 | 4.98 | 1.4 | 9.2 | 250 | 0.25 | 81.3 | 31.0 | 0.61 | 29.5% |
| Outlet 500 | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 5-1 | 504 | 502 | 12 | 40.8 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 40.8 | 40.8 | 4.0 | 0.7 | 0.00 | 0.00 | 0.00 | 0.0 | 0.74 | 0.74 | 0.2 | 0.9 | 200 | 0.65 | 87.3 | 27.6 | 0.85 | 3.2% |
| 5-2 | 502 | 41A | 17 | 57.8 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 57.8 | 98.6 | 4.0 | 1.6 | 0.00 | 0.00 | 0.00 | 0.0 | 0.87 | 1.61 | 0.5 | 2.0 | 200 | 0.32 | 120.0 | 19.4 | 0.60 | 10.6% |
| Outlet 600 | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6-1 | 612 | 610 | 3 | 10.2 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 10.2 | 10.2 | 4.0 | 0.2 | 0.00 | 0.00 | 0.00 | 0.0 | 0.26 | 0.26 | 0.1 | 0.2 | 200 | 0.65 | 30.6 | 27.6 | 0.85 | 0.9% |
| 6-2 | 610 | 608 | 1 | 3.4 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 3.4 | 13.6 | 4.0 | 0.2 | 0.00 | 0.00 | 0.00 | 0.0 | 0.13 | 0.39 | 0.1 | 0.3 | 200 | 0.65 | 10.2 | 27.6 | 0.85 | 1.2% |
| 6-3 | 608 | 604 | 14 | 47.6 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 47.6 | 61.2 | 4.0 | 1.0 | 0.00 | 0.00 | 0.00 | 0.0 | 0.76 | 1.14 | 0.3 | 1.3 | 200 | 0.32 | 111.8 | 19.4 | 0.60 | 6.8% |
| 6-4 | 606 | 604 | 4 | 13.6 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 13.6 | 13.6 | 4.0 | 0.2 | 0.00 | 0.00 | 0.00 | 0.0 | 0.23 | 0.23 | 0.1 | 0.3 | 200 | 0.65 | 42.0 | 27.6 | 0.85 | 1.0% |
| 6-5 | 604 | 602 | 12 | 40.8 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 40.8 | 115.6 | 4.0 | 1.9 | 0.00 | 0.00 | 0.00 | 0.0 | 0.60 | 1.97 | 0.6 | 2.4 | 200 | 0.32 | 80.5 | 19.4 | 0.60 | 12.5% |
| 6-6 | 602 | 42A | 12 | 40.8 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 40.8 | 156.4 | 4.0 | 2.5 | 0.00 | 0.00 | 0.00 | 0.0 | 0.61 | 2.58 | 0.7 | 3.3 | 200 | 0.32 | 81.6 | 19.4 | 0.60 | 16.8% |
| Outlet 700 | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 7-1 | 800 | 798 | 10 | 34.0 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 34.0 | 34.0 | 4.0 | 0.6 | 0.00 | 0.00 | 0.00 | 0.0 | 0.61 | 0.61 | 0.2 | 0.7 | 200 | 0.65 | 69.9 | 27.6 | 0.85 | 2.6% |
| 7-2 | 798 | 796 | 1 | 3.4 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 3.4 | 37.4 | 4.0 | 0.6 | 0.00 | 0.00 | 0.00 | 0.0 | 0.14 | 0.75 | 0.2 | 0.8 | 200 | 0.65 | 13.4 | 27.6 | 0.85 | 3.0% |
| 7-3 | 796 | 44A | 5 | 17.0 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 17.0 | 54.4 | 4.0 | 0.9 | 0.00 | 0.00 | 0.00 | 0.0 | 0.39 | 1.14 | 0.3 | 1.2 | 200 | 0.35 | 71.3 | 20.2 | 0.62 | 5.9% |
| 7-4 | 42B | 43A | 4 | 13.6 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 13.6 | 13.6 | 4.0 | 0.2 | 0.00 | 0.00 | 0.00 | 0.0 | 0.28 | 0.28 | 0.1 | 0.3 | 200 | 0.65 | 36.5 | 27.6 | 0.85 | 1.1% |
| 7-5 | 43A | 44A | 6 | 20.4 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 20.4 | 34.0 | 4.0 | 0.6 | 0.00 | 0.00 | 0.00 | 0.0 | 0.38 | 0.66 | 0.2 | 0.7 | 200 | 0.35 | 65.0 | 20.2 | 0.62 | 3.6% |
| 7-6 | 44A | 45A | 5 | 17.0 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 17.0 | 105.4 | 4.0 | 1.7 | 0.00 | 0.00 | 0.00 | 0.0 | 0.37 | 2.17 | 0.6 | 2.3 | 200 | 0.35 | 82.1 | 20.2 | 0.62 | 11.4% |
| 7-7 | 788A | 788 | 0 | 0.0 | 0 | 0.0 | 0.0 | 0.0 | 2.68 | 217.0 | 217.0 | 217.0 | 4.0 | 3.5 | 1.34 | 0.00 | 1.34 | 0.8 | 3.31 | 3.31 | 0.9 | 5.3 | 250 | 0.25 | 11.0 | 31.0 | 0.61 | 17.0% |
| 7-8 | 788 | 786 | 0 | 0.0 | 14 | 37.8 | 0.0 | 0.0 | 0.00 | 0.0 | 37.8 | 254.8 | 4.0 | 4.1 | 0.00 | 0.00 | 1.34 | 0.8 | 0.57 | 3.89 | | | | | | | | |

Fernbank Crossing - Sanitary Sewer Design Sheet

| AREA | | | RESIDENTIAL | | | | | | | | | | ICI | | | | INFILTRATION | | | Total Flow (l/s) | PIPE | | | | | | | |
|--------|------|-----|-------------|-------|-------|------|------|-----------|---------------|-------|-------|-------------|----------------------|-------------------------|------------------|-----------------|-----------------|------------------|---------------------|------------------|-----------|-----------|------------|----------------|----------------------|-------------------------|------|-------|
| ID | From | To | SINGLES | | TOWNS | | | MIXED USE | | TOTAL | | | Commercial Area (ha) | Institutional Area (ha) | Accum. Area (ha) | Peak Flow (l/s) | Total Area (ha) | Accum. Area (ha) | Infiltr. Flow (l/s) | | Size (mm) | Slope (%) | Length (m) | Capacity (l/s) | Full Flow Vel. (m/s) | Q/Q _{full} (%) | | |
| | | | Units | Pop. | Units | Pop. | Area | Pop. | Net Area (ha) | Pop. | Pop. | Accum. Pop. | Peak Factor | Peak Flow (l/s) | | | | | | | | | | | | | | |
| Future | | 744 | 101 | 343.4 | 0 | 0.0 | 2.4 | 382.3 | 0.00 | 0.0 | 725.7 | 725.7 | 3.9 | 11.4 | 0.00 | 2.90 | 2.90 | 1.8 | 11.41 | 11.41 | 3.2 | 16.4 | | | | | | |
| 7-29 | 752A | 752 | 0 | 0.0 | 0 | 0.0 | 0.0 | 0.0 | 1.45 | 117.0 | 117.0 | 117.0 | 4.0 | 1.9 | 0.73 | 0.00 | 0.73 | 0.4 | 1.58 | 1.58 | 0.4 | 2.8 | 250 | 0.30 | 11.0 | 34.0 | 0.67 | 8.2% |
| 7-30 | 752 | 750 | 0 | 0.0 | 8 | 21.6 | 0.0 | 0.0 | 0.00 | 0.0 | 21.6 | 138.6 | 4.0 | 2.2 | 0.00 | 0.00 | 0.73 | 0.4 | 0.72 | 2.30 | 0.6 | 3.3 | 250 | 0.30 | 67.0 | 34.0 | 0.67 | 9.8% |
| 7-31 | 750 | 748 | 0 | 0.0 | 8 | 21.6 | 0.0 | 0.0 | 0.00 | 0.0 | 21.6 | 160.2 | 4.0 | 2.6 | 0.00 | 0.00 | 0.73 | 0.4 | 0.44 | 2.74 | 0.8 | 3.8 | 250 | 0.30 | 51.6 | 34.0 | 0.67 | 11.2% |
| 7-32 | 748 | 746 | 0 | 0.0 | 4 | 10.8 | 0.0 | 0.0 | 0.00 | 0.0 | 10.8 | 171.0 | 4.0 | 2.8 | 0.00 | 0.00 | 0.73 | 0.4 | 0.23 | 2.97 | 0.8 | 4.0 | 250 | 0.30 | 55.9 | 34.0 | 0.67 | 11.9% |
| 7-33 | 746A | 746 | 0 | 0.0 | 0 | 0.0 | 1.4 | 231.7 | 0.00 | 0.0 | 231.7 | 231.7 | 4.0 | 3.8 | 0.00 | 0.00 | 0.00 | 0.0 | 1.43 | 1.43 | 0.4 | 4.2 | 200 | 0.35 | 10.2 | 20.2 | 0.62 | 20.5% |
| 7-34 | 746 | 744 | 0 | 0.0 | 4 | 10.8 | 0.0 | 0.0 | 0.00 | 0.0 | 10.8 | 413.5 | 4.0 | 6.7 | 0.00 | 0.00 | 0.73 | 0.4 | 0.40 | 4.80 | 1.3 | 8.5 | 250 | 0.30 | 69.9 | 34.0 | 0.67 | 25.0% |
| 7-35 | 744 | 742 | 3 | 10.2 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 10.2 | 1149.3 | 3.8 | 17.5 | 0.00 | 0.00 | 3.76 | 2.3 | 0.33 | 16.54 | 4.6 | 24.4 | 250 | 0.25 | 78.1 | 31.0 | 0.61 | 78.7% |
| 7-36 | 742 | 726 | 2 | 6.8 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 6.8 | 1156.1 | 3.8 | 17.6 | 0.00 | 0.00 | 3.76 | 2.3 | 0.29 | 16.83 | 4.7 | 24.6 | 250 | 0.25 | 78.1 | 31.0 | 0.61 | 79.3% |
| Future | | 726 | 69 | 234.6 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 234.6 | 234.6 | 4.0 | 3.8 | 0.00 | 0.00 | 0.00 | 0.0 | 4.40 | 4.40 | 1.2 | 5.0 | | | | | | |
| 7-44 | 726A | 726 | 0 | 0.0 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 0.0 | 0.0 | 4.0 | 0.0 | 0.00 | 2.12 | 2.12 | 1.3 | 2.12 | 2.12 | 0.6 | 1.9 | 250 | 0.25 | 15.0 | 31.0 | 0.61 | 6.1% |
| 7-45 | 726 | 724 | 0 | 0.0 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 0.0 | 1390.7 | 3.7 | 20.9 | 0.00 | 0.00 | 5.87 | 3.6 | 0.18 | 23.53 | 6.6 | 31.0 | 300 | 0.20 | 71.4 | 45.1 | 0.62 | 68.7% |
| 7-46 | 724A | 724 | 0 | 0.0 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 0.0 | 0.0 | 4.0 | 0.0 | 0.00 | 2.83 | 2.83 | 1.7 | 2.83 | 2.83 | 0.8 | 2.5 | 250 | 0.25 | 15.0 | 31.0 | 0.61 | 8.1% |
| 7-47 | 724 | 710 | 0 | 0.0 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 0.0 | 1390.7 | 3.7 | 20.9 | 0.00 | 0.00 | 8.70 | 5.3 | 0.11 | 26.47 | 7.4 | 33.6 | 300 | 0.20 | 87.2 | 45.1 | 0.62 | 74.4% |
| 7-48 | 722 | 720 | 5 | 17.0 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 17.0 | 17.0 | 4.0 | 0.3 | 0.00 | 0.00 | 0.00 | 0.0 | 0.46 | 0.46 | 0.1 | 0.4 | 200 | 0.65 | 57.6 | 27.6 | 0.85 | 1.5% |
| 7-49 | 720 | 718 | 1 | 3.4 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 3.4 | 20.4 | 4.0 | 0.3 | 0.00 | 0.00 | 0.00 | 0.0 | 0.14 | 0.60 | 0.2 | 0.5 | 200 | 0.65 | 7.9 | 27.6 | 0.85 | 1.8% |
| 7-50 | 718 | 716 | 10 | 34.0 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 34.0 | 54.4 | 4.0 | 0.9 | 0.00 | 0.00 | 0.00 | 0.0 | 0.60 | 1.20 | 0.3 | 1.2 | 200 | 0.35 | 75.7 | 20.2 | 0.62 | 6.0% |
| 7-51 | 716 | 712 | 9 | 30.6 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 30.6 | 85.0 | 4.0 | 1.4 | 0.00 | 0.00 | 0.00 | 0.0 | 0.54 | 1.74 | 0.5 | 1.9 | 200 | 0.35 | 73.1 | 20.2 | 0.62 | 9.2% |
| 7-52 | 714 | 712 | 4 | 13.6 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 13.6 | 13.6 | 4.0 | 0.2 | 0.00 | 0.00 | 0.00 | 0.0 | 0.23 | 0.23 | 0.1 | 0.3 | 200 | 0.65 | 39.4 | 27.6 | 0.85 | 1.0% |
| 7-53 | 712 | 710 | 4 | 13.6 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 13.6 | 112.2 | 4.0 | 1.8 | 0.00 | 0.00 | 0.00 | 0.0 | 0.28 | 2.25 | 0.6 | 2.4 | 200 | 0.35 | 64.1 | 20.2 | 0.62 | 12.1% |
| 7-54 | 710 | 708 | 5 | 17.0 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 17.0 | 1519.9 | 3.7 | 22.6 | 0.00 | 0.00 | 8.70 | 5.3 | 0.40 | 29.11 | 8.2 | 36.1 | 300 | 0.20 | 75.8 | 45.1 | 0.62 | 79.9% |
| | 708 | 706 | 0 | 0.0 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 0.0 | 1519.9 | 3.7 | 22.6 | 0.00 | 0.00 | 8.70 | 5.3 | 0.00 | 29.11 | 8.2 | 36.1 | 300 | 0.20 | 6.6 | 45.1 | 0.62 | 79.9% |
| 7-55 | 706 | 704 | 8 | 27.2 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 27.2 | 1547.1 | 3.7 | 23.0 | 0.00 | 0.00 | 8.70 | 5.3 | 0.60 | 29.71 | 8.3 | 36.6 | 300 | 0.20 | 65.7 | 45.1 | 0.62 | 81.1% |
| | 704 | 702 | 0 | 0.0 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 0.0 | 1547.1 | 3.7 | 23.0 | 0.00 | 0.00 | 8.70 | 5.3 | 0.00 | 29.71 | 8.3 | 36.6 | 300 | 0.20 | 8.7 | 45.1 | 0.62 | 81.1% |
| 7-56 | 702 | 46A | 9 | 30.6 | 0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.0 | 30.6 | 1577.7 | 3.7 | 23.4 | 0.00 | 0.00 | 8.70 | 5.3 | 0.58 | 30.29 | 8.5 | 37.2 | 300 | 0.20 | 69.6 | 45.1 | 0.62 | 82.4% |
| | 46A | | | | | | | | | | | | | | | | | | | | | | | | | | | |



**INFORMATION FROM IBI WEST
PARK DEVELOPMENT**


IBI Group
333 Preston Street - Suite 400
Ottawa, Ontario
K1S 5N4

SANITARY SEWER DESIGN SHEET

**PROJECT:
DEVELOPER:**
WEST PARK IN FERNBANK - PHASE 1
MONARCH CORPORATION

JOB #: 25853-5.7
DATE PRINTED: 01-May-12
DESIGN: LE

**FLOW FROM FERNBANK
CROSSING LIVERY STREET**

| STREET | LOCATION | | INDIVIDUAL | | | CUM. RES. FLOW | | | ICI | | | | INFILTRATION | | | TOTAL DESIGN FLOW (l/s) | PROPOSED SEWER | | | | | | FLOW DEPTH | | | | |
|-----------------|----------|-------|--------------|-------------|-----------|----------------|------|------------|-----------------|-----------------|-------------------|----------------|-----------------|-----------------|----------------|-------------------------|----------------|----------|-----------|-----------|---------|-----------------|-------------------|-----------------|------------|-------------|------|
| | FROM MH | TO MH | RESID. UNITS | | | POP. | POP. | PEAK FACT. | PEAK FLOW (l/s) | COMM. AREA (Ha) | INSTIT. AREA (Ha) | CUM. AREA (Ha) | PEAK FLOW (l/s) | INCR. AREA (Ha) | CUM. AREA (Ha) | FLOW (l/s) | | CAP. l/s | PIPE (mm) | LGTH. (m) | SLOPE % | VEL. (full) m/s | AVAIL. CAP. (l/s) | AVAIL. CAP. (%) | Flow qa/Qa | Depth da/Df | |
| | | | Sngls | Towns Semis | Multi Res | | | | | | | | | | | | | | | | | | | | | | |
| Private Site | 211 A | 100 A | | | 45 | 103.5 | 104 | 4.00 | 1.70 | | | | | 0.72 | 0.72 | 0.20 | 1.90 | 26.49 | 200 | 8.5 | 0.60 | 0.82 | 24.60 | 93% | | | |
| Tapadero Avenue | 100 A | 101 A | | | 0.0 | 104 | 4.00 | 1.70 | | | | | | 0.09 | 0.81 | 0.23 | 1.92 | 26.49 | 200 | 41.0 | 0.60 | 0.82 | 24.57 | 93% | | | |
| External | Stub | 40 A | | | | 468.1 | 468 | 3.99 | 7.66 | | | | | 5.05 | 5.05 | 1.41 | 9.07 | 31.01 | 250 | 15.0 | 0.25 | 0.61 | 21.94 | 71% | 0.29 | 0.37 | |
| Livery Street | 40 A | 90 A | | 6 | | 16.2 | 484 | 3.98 | 7.91 | | | | | 0.22 | 5.27 | 1.48 | 9.38 | 70.74 | 250 | 51.1 | 1.30 | 1.40 | 61.36 | 87% | 0.13 | 0.25 | |
| Private Site | 240 A | 90 A | | | 56 | 128.8 | 129 | 4.00 | 2.11 | | | | | 0.49 | 0.49 | 0.14 | 2.25 | 34.21 | 200 | 9.5 | 1.00 | 1.06 | 31.96 | 93% | | | |
| Livery Street | 90 A | 91 A | | 16 | | 43.2 | 656 | 3.91 | 10.52 | | | | | 0.55 | 6.31 | 1.77 | 12.29 | 39.22 | 250 | 111.5 | 0.40 | 0.77 | 26.93 | 69% | 0.31 | 0.39 | |
| Private Site | 241 A | 91 A | | | 45 | 103.5 | 104 | 4.00 | 1.70 | | | | | 0.43 | 0.43 | 0.12 | 1.82 | 34.21 | 200 | 9.5 | 1.00 | 1.06 | 32.40 | 95% | | | |
| Livery Street | 91 A | 92 A | | 3 | | 8.1 | 768 | 3.87 | 12.19 | | | | | 0.11 | 6.85 | 1.92 | 14.11 | 62.02 | 250 | 27.0 | 1.00 | 1.22 | 47.92 | 77% | 0.23 | 0.33 | |
| | 92 A | 101 A | | 10 | | 27.0 | 795 | 3.86 | 12.59 | | | | | 0.39 | 7.24 | 2.03 | 14.61 | 53.71 | 250 | 83.0 | 0.75 | 1.06 | 39.10 | 73% | 0.27 | 0.35 | |
| Tapadero Avenue | 101 A | 102 A | | | 0.0 | 898 | 3.83 | 14.11 | | | | | | 0.07 | 8.12 | 2.27 | 16.38 | 34.00 | 250 | 46.2 | 0.30 | 0.67 | 17.62 | 52% | 0.48 | 0.49 | |
| | 102 A | 103 A | | 3 | | 10.2 | 909 | 3.83 | 14.25 | | | | | 0.22 | 8.34 | 2.34 | 16.59 | 34.00 | 250 | 33.0 | 0.30 | 0.67 | 17.41 | 51% | 0.49 | 0.49 | |
| Asturcon Street | 42 B | 43 A | 4 | | | 13.6 | 14 | 4.00 | 0.22 | | | | | 0.28 | 0.28 | 0.08 | 0.30 | 27.60 | 200 | 36.5 | 0.65 | 0.85 | 27.30 | 99% | | | |
| Asturcon Street | 43 A | 44 A | 7 | | | 23.8 | 37 | 4.00 | 0.61 | | | | | 0.38 | 0.66 | 0.18 | 0.80 | 20.24 | 200 | 65.0 | 0.35 | 0.62 | 19.44 | 96% | | | |
| External | Stub | 44 A | | | | 52.8 | 53 | 4.00 | 0.87 | | | | | 1.14 | 1.14 | 0.32 | 1.19 | 20.24 | 200 | 15.0 | 0.35 | 0.62 | 19.05 | 94% | | | |
| Asturcon Street | 44 A | 45 A | 5 | | | 17.0 | 107 | 4.00 | 1.76 | | | | | 0.36 | 2.16 | 0.60 | 2.36 | 20.24 | 200 | 82.2 | 0.35 | 0.62 | 17.87 | 88% | | | |
| External | Stub | 45 A | | | | 412.1 | 412 | 4.00 | 6.76 | | 1.40 | | 1.40 | 0.85 | 6.39 | 6.39 | 1.79 | 9.40 | 31.01 | 250 | 15.0 | 0.25 | 0.61 | 21.61 | 70% | 0.30 | 0.38 |
| Asturcon Street | 45 A | 46 A | 5 | | | 17.0 | 536 | 3.96 | 8.70 | | | 1.40 | 0.85 | 0.37 | 8.92 | 2.50 | 12.05 | 31.01 | 250 | 82.0 | 0.25 | 0.61 | 18.96 | 61% | 0.39 | 0.43 | |
| External | Stub | 46 A | | | | 1586.4 | 1586 | 3.66 | 23.82 | 0.73 | 5.15 | 5.88 | 3.57 | 28.97 | 28.97 | 8.11 | 35.50 | 45.09 | 300 | 15.0 | 0.20 | 0.62 | 9.59 | 21% | 0.79 | 0.67 | |
| Cavesson Street | 46 A | 31 A | 3 | | | 10.2 | 2133 | 3.56 | 31.17 | | | 7.28 | 4.42 | 0.29 | 38.18 | 10.69 | 46.28 | 127.18 | 300 | 82.0 | 1.59 | 1.74 | 80.90 | 64% | 0.36 | 0.41 | |
| Percheron Way | 50 A | 51 A | 6 | | | 20.4 | 20 | 4.00 | 0.33 | | | | | 0.38 | 0.38 | 0.11 | 0.44 | 28.64 | 200 | 74.4 | 0.70 | 0.88 | 28.19 | 98% | | | |
| | 51 A | 52 A | 2 | | | 6.8 | 27 | 4.00 | 0.45 | | | | | 0.21 | 0.59 | 0.17 | 0.61 | 61.68 | 200 | 10.7 | 3.25 | 1.90 | 61.07 | 99% | | | |
| | 52 A | 53 A | 15 | | | 51.0 | 78 | 4.00 | 1.28 | | | | | 0.83 | 1.42 | 0.40 | 1.68 | 22.96 | 200 | 107.8 | 0.45 | 0.71 | 21.28 | 93% | | | |
| | 53 A | 31 A | 6 | | | 20.4 | 99 | 4.00 | 1.62 | | | | | 0.37 | 1.79 | 0.50 | 2.12 | 42.61 | 200 | 48.6 | 1.55 | 1.31 | 40.49 | 95% | | | |
| Cavesson Street | 31 A | 30 A | 6 | | | 20.4 | 2252 | 3.55 | 32.73 | | | 7.28 | 4.42 | 0.39 | 40.36 | 11.30 | 48.46 | 59.69 | 300 | 82.0 | 0.35 | 0.82 | 11.23 | 19% | 0.81 | 0.68 | |

Where Q = average daily per capita flow (350 l/cap.d.) or (0.0041l/sec.cap)

Population Density

Singles 3.4
Multi Residential 2.7

I = Unit of peak extraneous flow (0.28 l/sec/ha)

M = Residential Peaking factor = Harmon Peaking Factor , M = $1 + \frac{1}{4} + \frac{1}{4}P^{0.5}$, where P = population in thousan

Towns/Semis

Towns/Semis

Q(p) = Peak population flow (l/s)

Q(i) = peak extraneous flow (l/s)

Commercial, Office Space and School - Average flow 35,000 l/day/ha (0.405 l/s/ha) with Peaking Factor = 1.5



IBI Group
333 Preston Street - Suite 400
Ottawa, Ontario
K1S 5N4

SANITARY SEWER DESIGN SHEET

PROJECT: WEST PARK IN FERNBANK - PHASE 1
DEVELOPER: MONARCH CORPORATION

JOB #: 25853-5.7
DATE PRINTED: 01-May-12
DESIGN: LE

| STREET | LOCATION | | | INDIVIDUAL | | | CUM. RES. FLOW | | | ICI | | | INFILTRATION | | | TOTAL DESIGN FLOW (l/s) | PROPOSED SEWER | | | | | | FLOW DEPTH | | | | | | | |
|-----------------|------------|-------|--------------|-------------|-----------|-------|----------------|------------|-----------------|-----------------|-------------------|----------------|-----------------|-----------------|----------------|-------------------------|----------------|----------|-----------|-----------|-----------|-----------------|-------------------|-----------------|------------|-------------|-------|------|------|------|
| | FROM MH | TO MH | RESID. UNITS | | | POP. | POP. | PEAK FACT. | PEAK FLOW (l/s) | COMM. AREA (Ha) | INSTIT. AREA (Ha) | CUM. AREA (Ha) | PEAK FLOW (l/s) | INCR. AREA (Ha) | CUM. AREA (Ha) | FLOW (l/s) | | CAP. l/s | PIPE (mm) | LGTH. (m) | SLOPE % | VEL. (full) m/s | AVAIL. CAP. (l/s) | AVAIL. CAP. (%) | Flow qa/Qa | Depth da/Df | | | | |
| | | | Sngls | Towns Semis | Multi Res | | | | | | | | | | | | | | | | | | | | | | | | | |
| Equine Way | 60 A | 61 A | 3 | | | 10.2 | 10 | 4.00 | 0.17 | | | | | | 0.23 | 0.23 | 0.06 | 0.23 | 34.21 | 200 | 12.0 | 1.00 | 1.06 | 33.98 | 99% | | | | | |
| | 61 A | 62 A | 15 | | | 51.0 | 61 | 4.00 | 1.00 | | | | | | 0.77 | 1.00 | 0.28 | 1.28 | 21.63 | 200 | 109.8 | 0.40 | 0.67 | 20.35 | 94% | | | | | |
| | 62 A | 30 A | 4 | | | 13.6 | 75 | 4.00 | 1.23 | | | | | | 0.24 | 1.24 | 0.35 | 1.57 | 37.49 | 200 | 45.4 | 1.20 | 1.16 | 35.91 | 96% | | | | | |
| Cavesson Street | 30 A | 107 A | 12 | | | 40.8 | 2368 | 3.53 | 34.24 | | | | | | 7.28 | 4.42 | 0.62 | 42.22 | 11.82 | 50.49 | 63.77 | 300 | 79.4 | 0.40 | 0.87 | 13.29 | 21% | 0.79 | 0.66 | |
| Tapadero Avenue | 107 A | 106 A | 9 | | | 30.6 | 2398 | 3.52 | 34.64 | | | | | | 7.28 | 4.42 | 0.50 | 42.72 | 11.96 | 51.02 | 70.80 | 375 | 82.2 | 0.15 | 0.62 | 19.77 | 28% | 0.72 | 0.62 | |
| | 106 B | 105 A | 8 | | | 27.2 | 2425 | 3.52 | 34.99 | | | | | | 7.28 | 4.42 | 0.45 | 43.17 | 12.09 | 51.50 | 70.80 | 375 | 82.2 | 0.15 | 0.62 | 19.30 | 27% | 0.73 | 0.63 | |
| Equine Way | 60 A | 105 A | 10 | | | 34.0 | 34 | 4.00 | 0.56 | | | | | | | | 0.55 | 0.55 | 0.15 | 0.71 | 56.23 | 200 | 73.9 | 2.70 | 1.73 | 55.52 | 99% | | | |
| Tapadero Avenue | 105 A | 104 A | 5 | | | 17.0 | 2476 | 3.51 | 35.66 | | | | | | | 7.28 | 4.42 | 0.34 | 44.06 | 12.34 | 52.41 | 70.80 | 375 | 82.1 | 0.15 | 0.62 | 18.39 | 26% | 0.74 | 0.63 |
| External | Stub | 42 A | | | | 151.8 | 152 | 4.00 | 2.49 | | | | | | | | 2.59 | 2.59 | 0.73 | 3.21 | 20.24 | 200 | 15.0 | 0.35 | 0.62 | 17.02 | 84% | | | |
| Balikun Heights | 42 A | 70 A | 6 | | | 20.4 | 172 | 4.00 | 2.82 | | | | | | | | 0.37 | 2.96 | 0.83 | 3.65 | 21.63 | 200 | 76.2 | 0.40 | 0.67 | 17.98 | 83% | | | |
| | 70 A | 71 A | 2 | | | 6.8 | 179 | 4.00 | 2.94 | | | | | | | | 0.18 | 3.14 | 0.88 | 3.81 | 21.63 | 200 | 11.5 | 0.40 | 0.67 | 17.82 | 82% | | | |
| | 71 A | 72 A | 3 | | | 10.2 | 189 | 4.00 | 3.10 | | | | | | | | 0.18 | 3.32 | 0.93 | 4.03 | 21.63 | 200 | 19.4 | 0.40 | 0.67 | 17.60 | 81% | | | |
| | 72 A | 73 A | 3 | | | 10.2 | 199 | 4.00 | 3.27 | | | | | | | | 0.27 | 3.59 | 1.01 | 4.28 | 21.63 | 200 | 13.5 | 0.40 | 0.67 | 17.35 | 80% | | | |
| | 73 A | 74 A | 5 | | | 17.0 | 216 | 4.00 | 3.55 | | | | | | | | 0.35 | 3.94 | 1.10 | 4.65 | 28.64 | 200 | 72.5 | 0.70 | 0.88 | 23.98 | 84% | | | |
| External | Stub | 41 A | | | | 95.7 | 96 | 4.00 | 1.57 | | | | | | | | 1.61 | 1.61 | 0.45 | 2.02 | 20.24 | 200 | 15.0 | 0.35 | 0.62 | 18.22 | 90% | | | |
| Palfrey Way | 41 A | 80 A | 7 | | | 23.8 | 120 | 4.00 | 1.96 | | | | | | | | 0.39 | 2.00 | 0.56 | 2.52 | 30.61 | 200 | 60.0 | 0.80 | 0.94 | 28.09 | 92% | | | |
| | 80 A | 81 A | 13 | | | 44.2 | 164 | 4.00 | 2.68 | | | | | | | | 0.76 | 2.76 | 0.77 | 3.46 | 21.63 | 200 | 95.5 | 0.40 | 0.67 | 18.17 | 84% | | | |
| | 81 B | 82 A | 1 | | | 3.4 | 167 | 4.00 | 2.74 | | | | | | | | 0.09 | 2.85 | 0.80 | 3.54 | 54.09 | 200 | 11.5 | 2.50 | 1.67 | 50.55 | 93% | | | |
| | 82 A | 74 A | 15 | | | 51.0 | 218 | 4.00 | 3.58 | | | | | | | | 0.91 | 3.76 | 1.05 | 4.63 | 21.63 | 200 | 110.2 | 0.40 | 0.67 | 17.00 | 79% | | | |
| Balikun Heights | 74 A | 104 A | 5 | | | 17.0 | 452 | 4.00 | 7.40 | | | | | | | | 0.36 | 8.06 | 2.26 | 9.66 | 39.01 | 200 | 82.0 | 1.30 | 1.20 | 29.36 | 75% | | | |
| Tapadero Avenue | 104 A | 103 A | 10 | | | 34.0 | 2962 | 3.45 | 41.86 | | | | | | | 7.28 | 4.42 | 0.58 | 52.70 | 14.76 | 61.04 | 70.80 | 375 | 82.0 | 0.15 | 0.62 | 9.76 | 14% | 0.86 | 0.72 |
| Oxer Place | 103 A | 200 A | 3 | | | 10.2 | 3881 | 3.35 | 53.22 | | | | | | | 7.28 | 4.42 | 0.20 | 61.24 | 17.15 | 74.79 | 81.86 | 375 | 68.5 | 0.20 | 0.72 | 7.07 | 9% | 0.91 | 0.75 |
| | 200 A | 201 A | 4 | | | 13.6 | 3894 | 3.34 | 53.39 | | | | | | | 7.28 | 4.42 | 0.30 | 61.54 | 17.23 | 75.04 | 81.86 | 375 | 66.7 | 0.20 | 0.72 | 6.82 | 8% | 0.92 | 0.75 |
| | 201 A | 202 A | 4 | | | 13.6 | 3908 | 3.34 | 53.55 | | | | | | | 7.28 | 4.42 | 0.28 | 61.82 | 17.31 | 75.28 | 81.86 | 375 | 57.2 | 0.20 | 0.72 | 6.57 | 8% | 0.92 | 0.76 |
| Street No. 26 | Stub North | 202 A | 7 | 19 | | 75.1 | 75 | 4.00 | 1.23 | | | | | | | | | 1.00 | 1.00 | 0.28 | 1.51 | 41.90 | 200 | 11.0 | 1.50 | 1.29 | 40.39 | 96% | | |
| Street No. 26 | Stub South | 202 A | 31 | | | 105.4 | 105 | 4.00 | 1.73 | | | | | | | | | 1.80 | 1.80 | 0.50 | 2.23 | 48.38 | 200 | 6.5 | 2.00 | 1.49 | 46.15 | 95% | | |
| Block 205 | 202 A | 203 A | | | | 0.0 | 4088 | 3.32 | 55.73 | | | | | | | | 7.28 | 4.42 | | 64.62 | 18.09</td | | | | | | | | | |



IBI Group
333 Preston Street - Suite 400
Ottawa, Ontario
K1S 5N4

SANITARY SEWER DESIGN SHEET

PROJECT: WEST PARK IN FERNBANK - PHASE 1
DEVELOPER: MONARCH CORPORATION

JOB #: 25853-5.7
DATE PRINTED: 01-May-12
DESIGN: LE

| STREET | FROM MH | TO MH | INDIVIDUAL | | | CUM. RES. FLOW | | | ICI | | | | INFILTRATION | | | TOTAL DESIGN FLOW (l/s) | PROPOSED SEWER | | | | | | FLOW DEPTH | | | | | | | | | | |
|--------------------|------------|-------|--------------|-------------|-----------|----------------|------|------------|-----------------|-----------------|-------------------|----------------|-----------------|-----------------|----------------|-------------------------|----------------|----------|-----------|-----------|---------|-----------------|-------------------|-----------------|------------|-------------|-------|------|-------|-------|------|------|------|
| | | | RESID. UNITS | | | POP. | POP. | PEAK FACT. | PEAK FLOW (l/s) | COMM. AREA (Ha) | INSTIT. AREA (Ha) | CUM. AREA (Ha) | PEAK FLOW (l/s) | INCR. AREA (Ha) | CUM. AREA (Ha) | FLOW (l/s) | | CAP. l/s | PIPE (mm) | LGTH. (m) | SLOPE % | VEL. (full) m/s | AVAIL. CAP. (l/s) | AVAIL. CAP. (%) | Flow qa/Qa | Depth da/Df | | | | | | | |
| | | | Sngls | Towns Semis | Multi Res | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Street No. 24 | Stub North | 204 A | 15 | 29 | 46 | 235.1 | 235 | 4.00 | 3.86 | | | | | | 3.53 | 3.53 | 0.99 | 4.84 | 37.49 | 200 | 12.0 | 1.20 | 1.16 | 32.64 | 87% | | | | | | | | |
| Street No. 24 | Stub South | 204 A | 82 | | | 278.8 | 279 | 4.00 | 4.57 | | | | | | 5.09 | 5.09 | 1.43 | 6.00 | 21.63 | 200 | 10.0 | 0.40 | 0.67 | 15.63 | 72% | 0.28 | 0.36 | | | | | | |
| Block 204 | 204 A | 205 B | | | | 0.0 | 4602 | 3.28 | 61.86 | | | | | | 7.28 | 4.42 | | 73.24 | 20.51 | 86.79 | 129.29 | 375 | 89.7 | 0.50 | 1.13 | 42.50 | 33% | 0.67 | 0.62 | | | | |
| Westphalian Avenue | Stub North | 209 A | | 42 | | 113.4 | 113 | 4.00 | 1.86 | | | | | | | | | 1.42 | 1.42 | 0.40 | 2.26 | 21.63 | 200 | 13.8 | 0.40 | 0.67 | 19.37 | 90% | | | | | |
| | 209 A | 208 A | 6 | 9 | | 44.7 | 158 | 4.00 | 2.59 | | | | | | | | | 0.67 | 2.09 | 0.59 | 3.18 | 27.60 | 200 | 64.9 | 0.65 | 0.85 | 24.42 | 88% | | | | | |
| | 208 A | 207 A | 4 | 4 | | 24.4 | 183 | 4.00 | 2.99 | | | | | | | | | 0.41 | 2.50 | 0.70 | 3.69 | 45.27 | 200 | 67.5 | 1.75 | 1.40 | 41.58 | 92% | | | | | |
| Street No. 28 | Stub North | 207 A | 12 | 35 | | 135.3 | 135 | 4.00 | 2.22 | | | | | | | | | 1.48 | 1.48 | 0.41 | 2.63 | 34.21 | 200 | 19.0 | 1.00 | 1.06 | 31.58 | 92% | | | | | |
| Street No. 21 | Stub South | 207 A | 97 | | | 329.8 | 330 | 4.00 | 5.41 | | | | | | | | | 6.02 | 6.02 | 1.69 | 7.09 | 31.01 | 250 | 19.0 | 0.25 | 0.61 | 23.92 | 77% | 0.23 | 0.33 | | | |
| Westphalian Avenue | 207 A | 206 A | | 9 | | 24.3 | 672 | 3.90 | 10.76 | | | | | | | | | 0.38 | 10.38 | 2.91 | 13.66 | 45.09 | 300 | 82.0 | 0.20 | 0.62 | 31.43 | 70% | 0.30 | 0.38 | | | |
| Street No. 28 | Stub North | 206 A | 20 | | | 68.0 | 68 | 4.00 | 1.12 | | | | | | | | | 1.16 | 1.16 | 0.32 | 1.44 | 38.27 | 200 | 20.0 | 1.25 | 1.18 | 36.83 | 96% | | | | | |
| Westphalian Avenue | 206 A | 205 A | | 9 | | 24.3 | 764 | 3.87 | 12.13 | | | | | | | | | 0.40 | 11.94 | 3.34 | 15.48 | 45.09 | 300 | 85.0 | 0.20 | 0.62 | 29.62 | 66% | 0.34 | 0.40 | | | |
| Street No. 1 | Stub South | 205 B | 27 | | | 91.8 | 92 | 4.00 | 1.51 | | | | | | | | | 0.90 | 0.90 | 0.25 | 1.76 | 21.63 | 200 | 20.0 | 0.40 | 0.67 | 19.87 | 92% | | | | | |
| Street No. 1 | Stub North | 205 B | 10 | 15 | | 74.5 | 75 | 4.00 | 1.22 | | | | | | | | | 1.40 | 1.40 | 0.39 | 1.61 | 40.47 | 200 | 18.0 | 1.40 | 1.25 | 38.86 | 96% | | | | | |
| Street No. 1 | 205 B | 205 A | | | | 0.0 | 4769 | 3.26 | 63.81 | | | | | | | | | | 7.28 | 4.42 | | 75.54 | 21.15 | 89.39 | 129.29 | 375 | 2.5 | 0.50 | 1.13 | 39.90 | 31% | 0.69 | 0.63 |
| Street No. 1 | Stub South | 205 A | 506 | 260 | 86 | 2620.2 | 2620 | 3.49 | 37.51 | | | | | | | | | 2.90 | 2.90 | 1.76 | 57.88 | 57.88 | 16.21 | 55.48 | 132.98 | 450 | 20.0 | 0.20 | 0.81 | 77.50 | 58% | 0.42 | 0.47 |
| Street No. 1 | 205 A | 222 A | | | | 0.0 | 8153 | 3.04 | 101.69 | | | | | | | | | 10.18 | 6.18 | 0.30 | 145.66 | 40.78 | 148.66 | 221.82 | 600 | 120.0 | 0.12 | 0.76 | 73.16 | 33% | 0.67 | 0.62 | |
| Street No. 1 | 222 A | 221 A | | | | 0.0 | 8153 | 3.04 | 101.69 | | | | | | | | | 10.18 | 6.18 | 0.26 | 145.92 | 40.86 | 148.73 | 221.82 | 600 | 100.0 | 0.12 | 0.76 | 73.08 | 33% | 0.67 | 0.62 | |
| Street No. 1 | 221 A | FT06 | | | | 0.0 | 8153 | 3.04 | 101.69 | | | | | | | | | 10.18 | 6.18 | 0.19 | 146.11 | 40.91 | 148.79 | 221.82 | 600 | 94.0 | 0.12 | 0.76 | 73.03 | 33% | 0.67 | 0.62 | |

Where Q = average daily per capita flow (350 l/cap.d.) or (0.0041l/sec./cap)

Population Density

| | |
|---------|-----|
| Singles | 3.4 |
| 2.7 | |
| 2.3 | |
| | |
| | |

Commercial, Office Space and School - Average flow 35,000 l/day/ha (0.405 l/s/ha) with Peaking Factor = 1.5

**INFORMATION FROM
ROBERT GRANT AVENUE
(NS ARTERIAL) DESIGN**

| AREA | | | RESIDENTIAL | | | | | | | | ICI | | | | INFILTRATION | | | PIPE | | | | | | | |
|-------------------------|------|------|-------------|------|-------|------|---------------|------|-------|-------------|-------------|----------------------|-------------------------|------------------|-----------------|-----------------|------------------|--------------------|------------------|-----------|-----------|------------|----------------|----------------------|-------------------------|
| ID | From | To | SINGLES | | TOWNS | | MIXED USE | | TOTAL | | | Commercial Area (ha) | Institutional Area (ha) | Accum. Area (ha) | Peak Flow (l/s) | Total Area (ha) | Accum. Area (ha) | Infill. Flow (l/s) | Total Flow (l/s) | Size (mm) | Slope (%) | Length (m) | Capacity (l/s) | Full Flow Vel. (m/s) | Q/Q _{full} (%) |
| | | | Units | Pop. | Units | Pop. | Net Area (ha) | Pop. | Pop. | Accum. Pop. | Peak Factor | | | | | | | | | | | | | | |
| Founder Avenue to Trunk | | | | | | | | | | 523.9* | | | | | | | | 6.47* | | 10.22* | | | | | |
| HYD1 | 209 | 211 | 0.0 | 0.0 | 0.0 | 0.0 | 523.9 | 4.0 | 8.41 | 0.00 | 0.00 | 0.0 | 5.12 | 11.59 | 3.25 | 11.66 | 250 | 0.70 | 49 | 51.9 | 1.02 | 22.5% | | | |
| | 211 | 221 | 0.0 | 0.0 | 0.0 | 0.0 | 523.9 | 4.0 | 8.41 | 0.00 | 0.00 | 0.0 | 0.00 | 11.59 | 3.25 | 11.66 | 250 | 0.70 | 33 | 51.9 | 1.02 | 22.5% | | | |
| FAV1 | 221 | F118 | 0.0 | 0.0 | 0.0 | 0.0 | 523.9 | 4.0 | 8.41 | 0.00 | 0.00 | 0.0 | 0.54 | 12.13 | 3.40 | 11.81 | 250 | 0.35 | 88 | 36.7 | 0.72 | 32.2% | | | |

Design Parameters:

Avg Flow/Person = 350 l/day
Comm./Inst. Flow = 35000 l/ha/day
Infiltration = 0.28 l/s/ha
Pipe Friction n = 0.013

Residential Peaking Factor = Harmon Equation (max 4, min 2)

Peaking Factor Comm./Inst. = 1.5

*Accumulated Population, Area and Total Flow from CRT Lands Phase 1 Design Brief

Population Density:
ppl/unit units/net ha
Mixed Use 1.80 90
Singles 3.30
Towns 2.50

Project: Founder Avenue (101108)

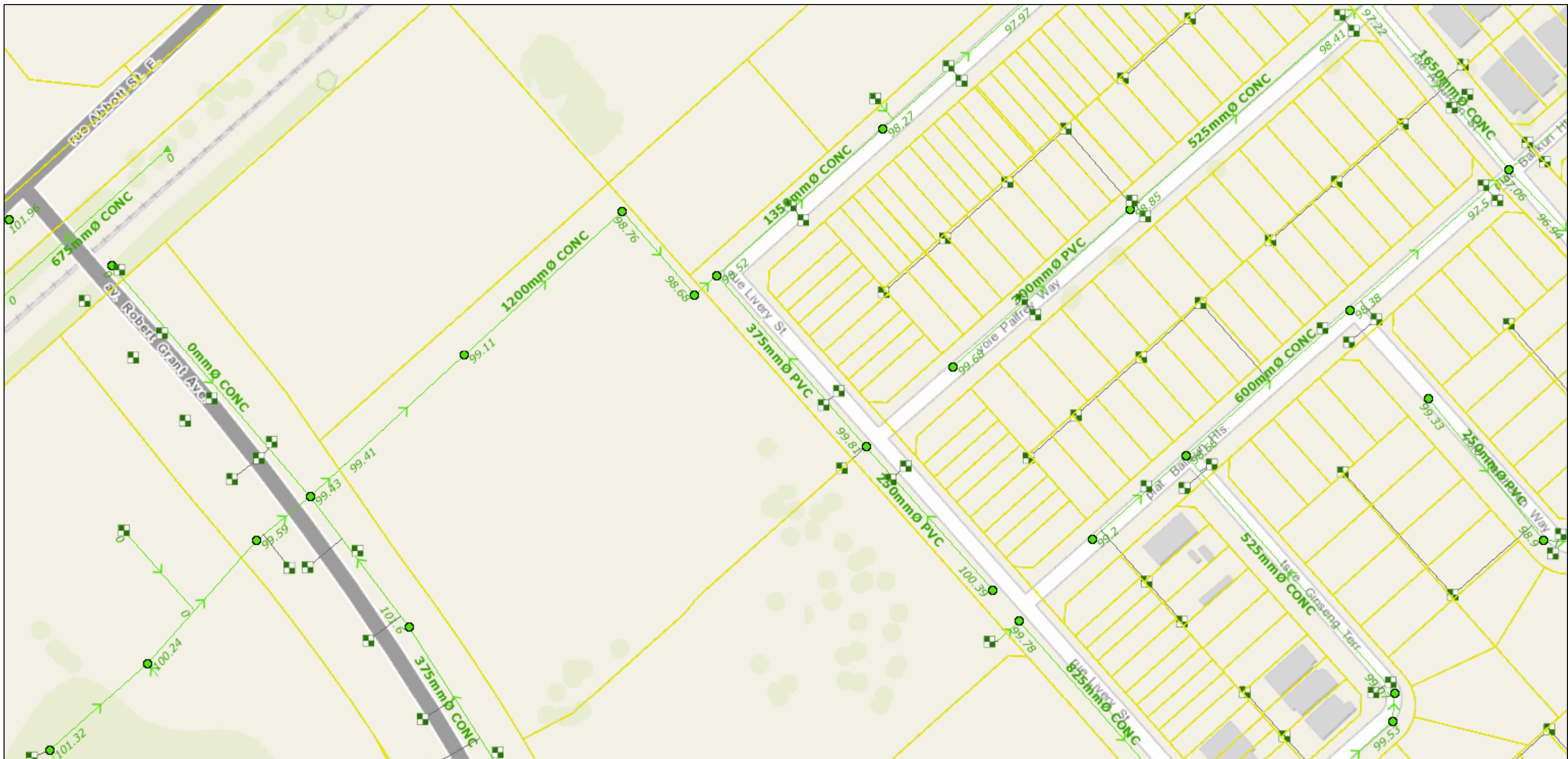
Designed: SML

Checked: MAB

Date: May 7, 2014

APPENDIX C
Stormwater Management Calculations

1000 Robert Grant Ave Storm Info



March 6, 2019

- Property Parcels
 - Upstream Invert / Radier amont
 - Downstream Invert / Radier aval

Storm Pipe Details / Détails de la conduite d'eaux pluviales

- Catch Basins / Puisards
 - Storm Inlets / Prises d'entrée des eaux pluviales

Storm Pipes / Conduites d'eaux pluviales

- Private / Branchement privé
 - ↗ Public / Branchement public

Storm Pump Stations / Stations de pompage des eaux pluviales

- Storm Pump Station / Station de pompage des eaux pluviales
 - Combined Manholes / Regards d'égout unitaire

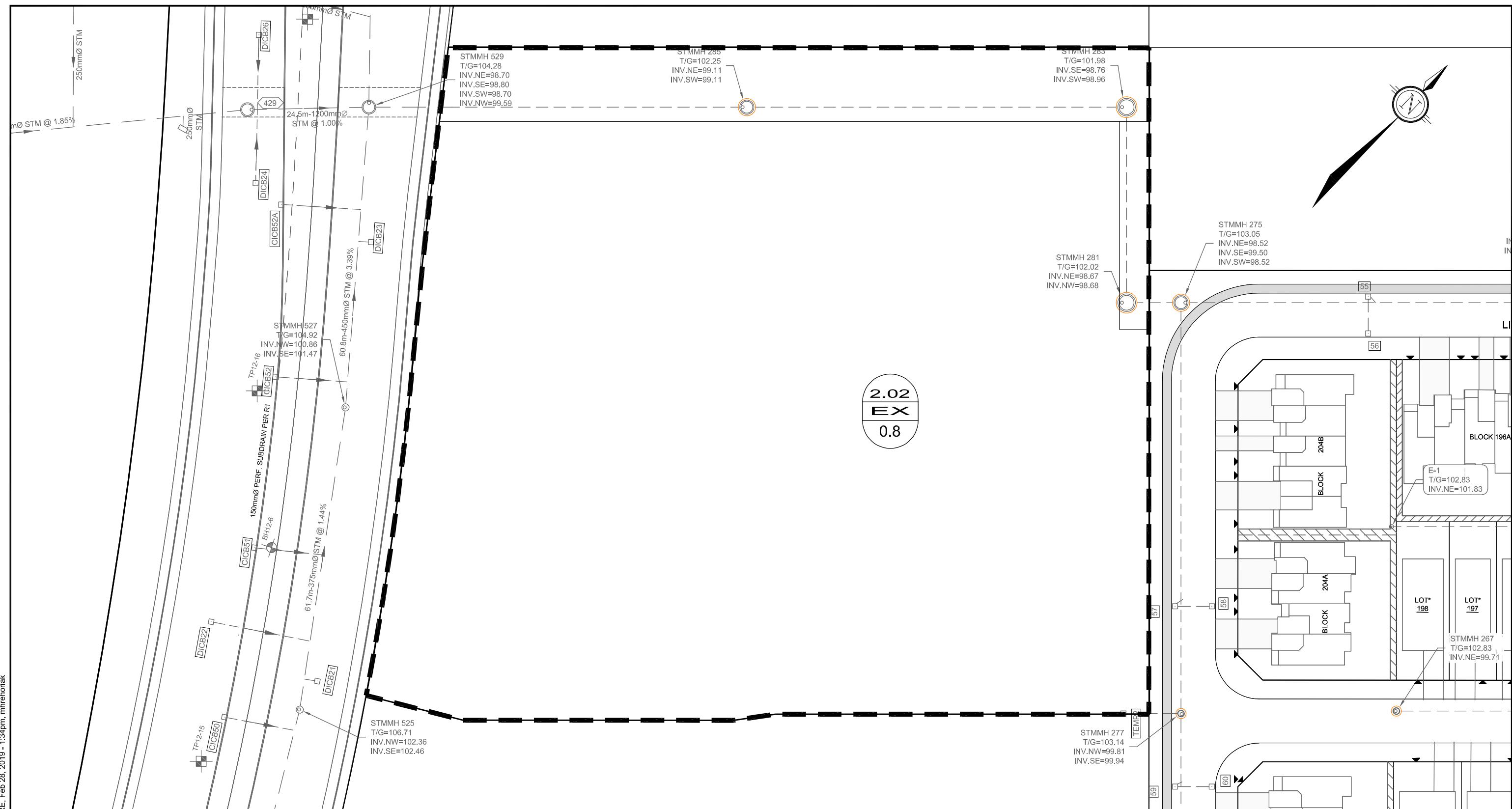
Combined Pipes / Conduites d'égout unitaire

- ⊕ Public / Branchement public
 - ⊕ Private / Branchement privé

City of Ottawa

1:2,000

0.09 mi



LEGEND

EXISTING STORM SEWER AND MANHOLE

— — —

STORMWATER DRAINAGE AREA

DRAINAGE AREA (ha)

DRAINAGE AREA ID

RUNOFF COEFFICIENT 'C'

1.694
A-2
0.84

NOVATECH

Engineers, Planners & Landscape Architects
Suite 200, 240 Michael Cowpland Drive

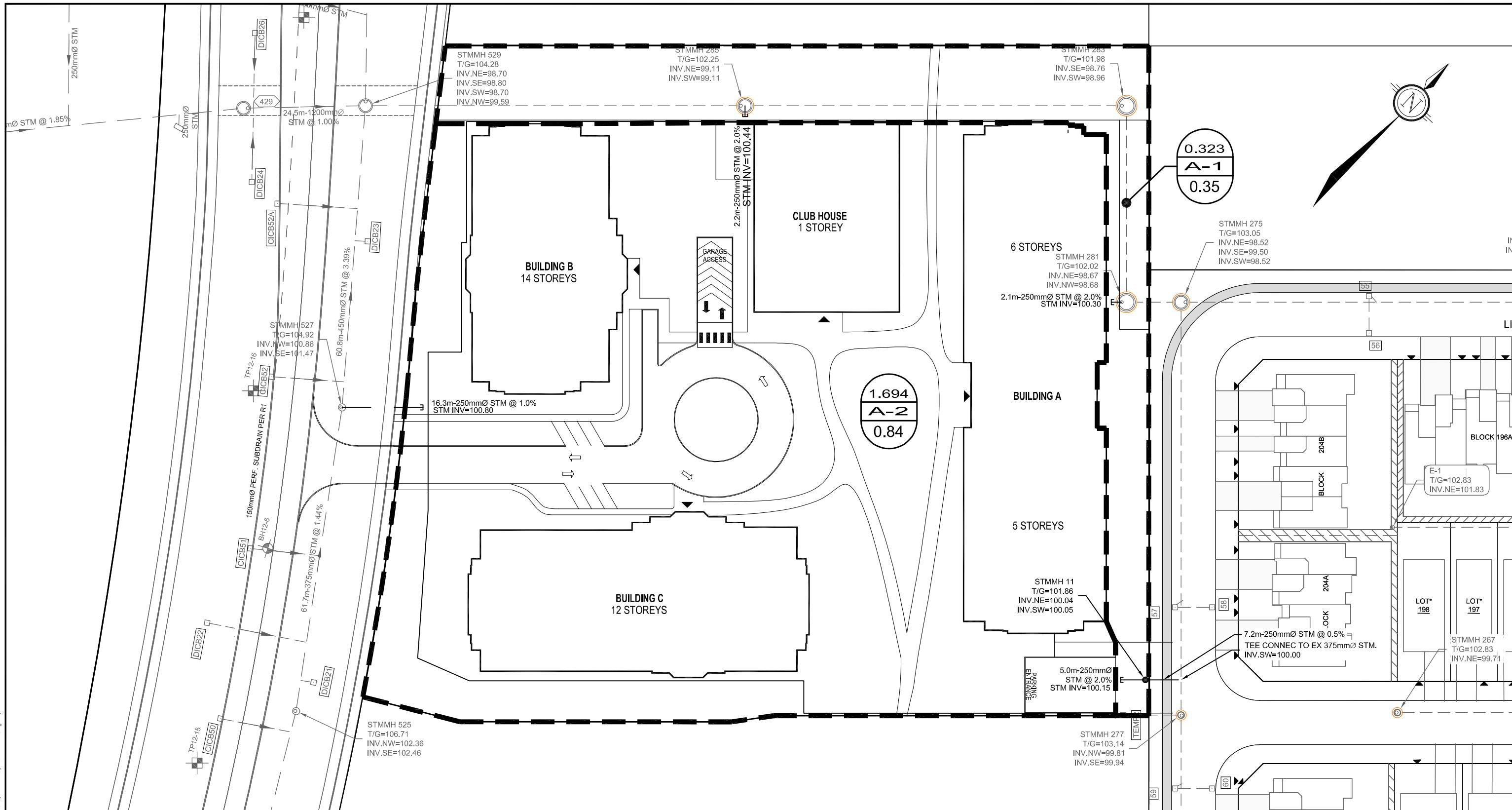
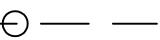
Telephone (613) 254-9643
Facsimile (613) 254-5867
Website www.novatech-eng.com

RENE'S COURT BLOCK 203

PRE DEVELOPMENT DRAINAGE AREA PLAN

CALE 1 750 0 10 20 30

1 : 750

**LEGEND**

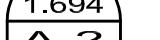
PROPOSED STORM SEWER AND MANHOLE



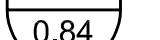
STORMWATER DRAINAGE AREA



DRAINAGE AREA (ha)



DRAINAGE AREA ID



RUNOFF COEFFICIENT 'C'



Engineers, Planners & Landscape Architects

Suite 200, 240 Michael Cowpland Drive
Ottawa, Ontario, Canada K2M 1P6Telephone (613) 254-9643
Facsimile (613) 254-5867
Website www.novatech-eng.com**RENE'S COURT BLOCK 203****POST DEVELOPMENT
DRAINAGE AREA PLAN**SCALE 1 : 750
DATE MAR 2019 JOB 117151 FIGURE 7

TABLE 1A: Allowable Runoff Coefficient "C"

| Area | "C" |
|-------|------|
| Total | 0.80 |
| 2.017 | |

TABLE 1B: Allowable Flows

| Outlet Options | Area (ha) | "C" | Tc (min) | Q _{5 Year} (L/s) | Q _{5 Year} (L/s/ha) |
|----------------|-----------|------|----------|---------------------------|------------------------------|
| Maritime Way | 2.017 | 0.80 | 16.61 | 353.0 | 175.0 |

Time of Concentration T_c= 17 min

Intensity (5 Year Event) I₅= 78.69 mm/hr

Intensity (100 Year Event) I₁₀₀= 134.50 mm/hr

$$100 \text{ year Intensity} = 1735.688 / (\text{Time in min} + 6.014)^{0.820}$$

$$5 \text{ year Intensity} = 998.071 / (\text{Time in min} + 6.053)^{0.814}$$

TABLE 2A: Post-Development Runoff Coefficient "C" - A-1

| Area | Surface | Ha | "C" | C _{avg} | *C ₁₀₀ | Runoff Coefficient Equation |
|-------|---------|-------|------|------------------|-------------------|--|
| Total | Hard | 0.070 | 0.90 | | 0.35 | C = (A _{hard} x 0.9 + A _{soft} x 0.2)/A _{Tot} |
| 0.323 | Soft | 0.253 | 0.20 | | 0.41 | * Runoff Coefficient increases by 25% up to a maximum value of 1.00 for the 100-Year event |

TABLE 2B: Post-Development A-1 Flows

| Outlet Options | Area (ha) | C _{avg} | Tc (min) | Q _{5 Year} (L/s) | Q _{100 Year} |
|----------------|-----------|------------------|----------|---------------------------|-----------------------|
| Livery Street | 0.323 | 0.35 | 10 | 32.7 | 66.1 |

Time of Concentration Tc= 10 min
 Intensity (5 Year Event) I₅= 104.19 mm/hr
 Intensity (100 Year Event) I₁₀₀= 178.56 mm/hr

$$100 \text{ year Intensity} = 1735.688 / (\text{Time in min} + 6.014)^{0.820}$$

$$5 \text{ year Intensity} = 998.071 / (\text{Time in min} + 6.053)^{0.814}$$

TABLE 3A: Post-Development Runoff Coefficient "C" - A-2

| Area | Surface | Ha | 5 Year Event | | 100 Year Event | |
|-------|---------|------|--------------|------------------|----------------|-------------------|
| | | | "C" | C _{avg} | "C" + 25% | *C _{avg} |
| 1.694 | Total | Hard | 0.799 | 0.90 | 0.84 | 1.00 |
| | | Roof | 0.745 | 0.90 | | 1.00 |
| | | Soft | 0.150 | 0.20 | | 0.25 |

TABLE 3B: 100 YEAR EVENT QUANTITY STORAGE REQUIREMENT - A-2

1.694 =Area (ha)
 0.93 = C

| Return Period | Time (min) | Intensity (mm/hr) | Flow Q (L/s) | Allowable Runoff (L/s) | Net Flow to be Stored (L/s) | Storage Req'd (m ³) |
|---------------|------------|-------------------|---------------|------------------------|-----------------------------|---------------------------------|
| 100 YEAR | 5 | 242.70 | 1067.06 | 286.9 | 780.16 | 234.05 |
| | 10 | 178.56 | 785.05 | 286.9 | 498.15 | 298.89 |
| | 15 | 142.89 | 628.24 | 286.9 | 341.34 | 307.21 |
| | 20 | 119.95 | 527.37 | 286.9 | 240.47 | 288.56 |
| | 25 | 103.85 | 456.57 | 286.9 | 169.67 | 254.51 |

Equations:

Flow Equation

$$Q = 2.78 \times C \times I \times A$$

Where:

C is the runoff coefficient

I is the rainfall intensity, City of Ottawa IDF

A is the total drainage area

Runoff Coefficient Equation

$$C_s = (A_{\text{hard}} \times 0.9 + A_{\text{soft}} \times 0.2) / A_{\text{Tot}}$$

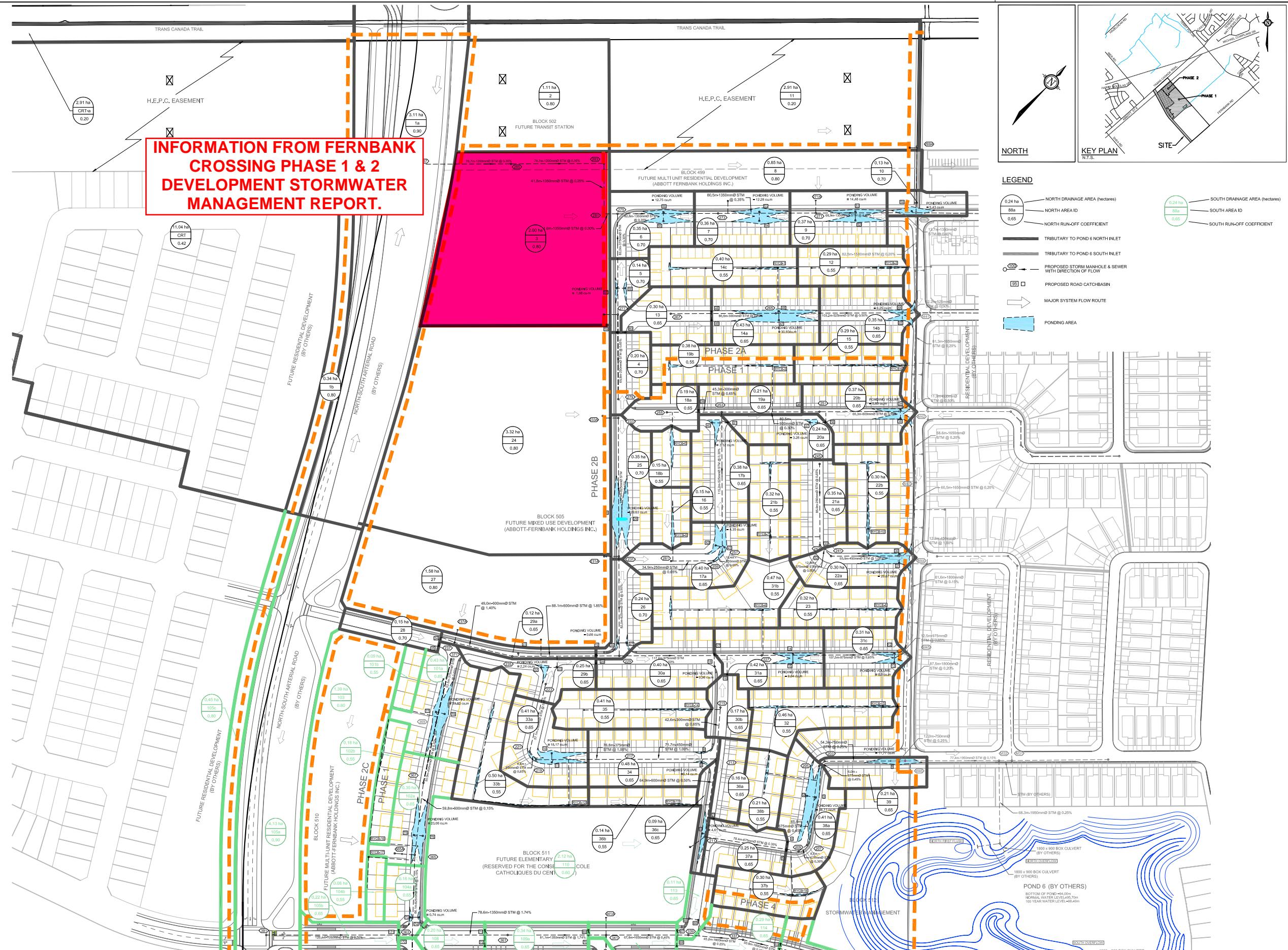
$$C_{100} = (A_{\text{hard}} \times 1.0 + A_{\text{soft}} \times 0.25) / A_{\text{Tot}}$$

Table 4: Post-Development Stormwater Management Summary

| Area ID | Area (ha) | 1:5 Year Weighted Cw | 1:100 Year Weighted Cw | Outlet Location | 100 Year Storm Event | | | |
|------------------|-----------|----------------------|------------------------|-----------------|----------------------|-----------------------|------------------|----------------------------|
| | | | | | Release (L/s) | Max Ponding Depth (m) | Req'd Vol (cu.m) | Max. Vol. Provided (cu.m.) |
| A-1 | 0.323 | 0.35 | 0.41 | Livery | 66.1 | N/A | N/A | N/A |
| A-2 | 1.694 | 0.84 | 0.93 | Livery | 286.9 | N/A | 307.2 | 307.2 |
| Total | | | | | 353.0 | | | |
| Allowable | | | | | 353.0 | | | |

| STM MANHOLE TABLE | |
|-------------------|--|
| MANHOLE ID | OBVERT |
| 203 | S#98.33 NE#98.33 |
| 205 | SE#98.38 NW#98.35 |
| 207 | S#98.72 NW#98.68 |
| 209 | SW#98.78 NW#98.74 |
| 211 | NW#98.01 NE#98.01 |
| 213 | SW#98.33 NW#98.33 SE#98.33 |
| 215 | SE#98.61 |
| 217 | SW#100.05 NE#100.05 |
| 219 | W#100.82 NE#100.82 |
| 221 | NW#100.90 E#100.87 |
| 223 | SE#101.27 |
| 227 | SW#98.12 NE#98.12 |
| 229 | SW#98.70 NE#98.70 NW#98.70 |
| 231 | SE#100.11 SW#100.18 NW#100.11 |
| 233 | SE#100.63 SW#100.68 |
| 235 | SW#101.33 NE#101.33 |
| 237 | NE#102.02 |
| 241 | W#99.13 NE#99.13 |
| 243 | NW#99.21 E#99.21 |
| 245 | SE#98.65 |
| 251 | SW#98.09 NE#98.09 |
| 253 | SE#99.34 SW#99.34 NE#99.34 |
| 255 | NE#99.63 |
| 257 | S#99.68 NW#98.68 |
| 259 | SW#98.78 NW#98.75 |
| 261 | NE#100.01 |
| 265 | SW#98.45 NE#98.45 |
| 267 | NE#100.01 |
| 269A | SE#98.19 |
| 271 | SW#98.37 NW#98.37 NE#98.37 |
| 273 | SW#98.65 NE#98.65 |
| 275 | SW#98.94 SE#98.94 NE#98.94 |
| 277 | SE#100.18 NW#100.19 |
| 279 | NW#100.64 |
| 281 | NW#100.03 NE#99.97 |
| 283 | SW#100.13 SE#100.13 |
| 285 | SW#100.40 NE#100.40 |
| 287 | NE#100.67 |
| 301 | SW#98.59 SE#98.59 NE#98.59 |
| 335 | SW#98.76 SE#98.76 NE#98.76 |
| 337 | SW#98.89 NE#98.89 |
| 339 | SW#98.00 NE#98.00 |
| 341 | SW#98.27 NW#98.27 SE#98.27 NE#98.27 |
| 361 | SW#100.68 NE#100.68 |
| 363 | NW#102.05 SE#102.05 SE#102.11 NE#102.05 |
| 365 | NW#102.15 SW#102.15 SE#102.15 |
| 367 | NW#102.24 SE#102.24 |
| 369 | NW#102.34 SE#102.34 |
| 371 | SE#102.69 |
| 391 | NE#102.65 |

**INFORMATION FROM FERNBANK
CROSSING PHASE 1 & 2
DEVELOPMENT STORMWATER
MANAGEMENT REPORT.**



NOTE:
THE POSITION OF ALL POLE LINES, CONDUITS,
WATERMAINS, SEWERS AND OTHER
UNDERGROUND AND OVERGROUND UTILITIES AND
STRUCTURES IS NOT NECESSARILY SHOWN ON
THE CONTRACT DRAWINGS AND WHERE SHOWN,
THE ACCURACY OF THE POSITIONING
OF UTILITIES AND STRUCTURES IS NOT GUARANTEED,
BEFORE STARTING WORK, DETERMINE THE EXACT
LOCATION OF ALL SUCH UTILITIES AND
STRUCTURES AND ASSUME ALL LIABILITY FOR
DAMAGE TO THEM.



ABBOTT-FERNBANK HOLDINGS INC.
Corporate Head Office
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Ottawa, Ontario, Canada
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Fax: 613-220-2962

3. ISSUED FOR APPROVAL (PHASE 1&2) AUG 17/12 KJM

2. ISSUED FOR APPROVAL (PHASE 1&2) JUN 21/12 KJM

1. ISSUED FOR APPROVAL MAR 9/12 KJM

No. REVISION DATE BY

SCALE

DESIGN

FOR REVIEW ONLY

KJM

CHECKED MAB

DRAWN RCH

APPROVED MAB

LICENSED PROFESSIONAL ENGINEER
J.J. MURPHY
10123021
PROVINCE OF ONTARIO

LICENSED PROFESSIONAL PLANNER
M.A. BISSETT
PROVINCE OF ONTARIO

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CITY OF OTTAWA
FERNBANK CROSSING

STORM DRAINAGE AREA PLAN
PHASE 1 & 2

PROJECT NO.
108180-10

REV
REV # 3

DRAWING NO.
108180-STM1

PLAN# 7200 - 700mmx700mm

Fernbank Crossing - Storm Sewer Design Sheet (Rational Method)

| LOCATION | | | AREA | | | | | | | | | | | | FLOW | | | | | Total Peak Flow (Q) (L/s) | PROPOSED SEWER | | | | | | | | | |
|---------------------------|-----------|---------|-----------|--------------|----------------|-------------------|---------|-------|----------------|---------------------|-------------------|------------------|-----------------|------------|-----------------------------|----------------|---------------|-----------------------|------------------------|---------------------------|-----------------|-----------|-----------|-----------|------------|----------------|--------------------------|---------------------|-------------|-------|
| Location | From node | To node | Mixed Use | Park N' Ride | Paramedic Post | Arterial Road ROW | Schools | Parks | Hydro Corridor | Singles Front Yards | Singles Rear Yard | Towns Front Yard | Towns Rear Yard | Total Area | Weighted Runoff Coefficient | Indivi 2.78 AR | Accum 2.78 AR | Time of Concentration | Rain Intensity (mm/hr) | | Peak Flow (L/s) | Pipe Type | Size (mm) | Grade (%) | Length (m) | Capacity (l/s) | Full Flow Velocity (m/s) | Time of Flow (min.) | Q/Qfull (%) | |
| | | | | | | | | | | | | | | | 5yr | | 10yr | | | | | | | | | | | | | |
| POND 6 North Inlet | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| CRT | CRT | 287 | | | | | | | | 2.91 | | | | | 13.95 | 0.38 | 14.54 | 14.54 | 15.00 | 83.6 | 1215.2 | 1215.2 | | | | | | | | |
| 1 | 287 | 285 | 0.34 | 3.11 | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 15.00 | 0.0 | | | | | | | | | | |
| | 285 | 283 | | | | | | | | | | | | | 3.45 | 0.89 | 8.54 | 8.54 | 10.00 | 122.1 | 1042.8 | 2257.9 | CONC | 1200 | 0.35 | 76.7 | 2406.2 | 2.06 | 0.62 | 93.8% |
| 2 | 283 | 281 | 1.11 | | | | | | | | | | | | 0.00 | 0.00 | 14.54 | 14.54 | 15.62 | 81.6 | 1186.8 | | CONC | 1200 | 0.35 | 76.7 | 2406.2 | 2.06 | 0.62 | 83.2% |
| 3 | 281 | 275 | 2.00 | | | | | | | | | | | | 2.00 | 0.80 | 4.45 | 21.46 | 16.61 | 78.7 | 1688.9 | 2475.5 | CONC | 1350 | 0.30 | 11.0 | 3049.8 | 2.06 | 0.09 | 81.2% |
| | | | | | | | | | | | | | | | 0.00 | 0.00 | 8.54 | 8.54 | 16.61 | 92.1 | 786.6 | | | | | | | | | |
| 4 | 279 | 277 | | | | | | | | 0.20 | | | | | 0.20 | 0.70 | 0.39 | 0.39 | 10.00 | 104.2 | 40.6 | 40.6 | PVC | 250 | 0.65 | 69.8 | 50.0 | 0.99 | 1.18 | 81.1% |
| 5 | 277 | 275 | | | | | | | | 0.14 | | | | | 0.14 | 0.70 | 0.27 | 0.66 | 11.18 | 98.4 | 65.1 | | PVC | 375 | 0.30 | 83.0 | 100.2 | 0.88 | 1.57 | 65.0% |
| 6 | 275 | 273 | | | | | | | | 0.35 | | | | | 0.35 | 0.70 | 0.68 | 22.80 | 16.70 | 78.4 | 1788.8 | 2572.9 | CONC | 1350 | 0.35 | 82.8 | 3294.2 | 2.23 | 0.62 | 78.1% |
| 7 | 273 | 271 | | | | | | | | 0.36 | | | | | 0.36 | 0.70 | 0.70 | 23.50 | 17.32 | 76.8 | 1803.9 | | CONC | 1350 | 0.35 | 80.5 | 3294.2 | 2.23 | 0.60 | 78.0% |
| 8 | 271A | 271 | 0.85 | | | | | | | | | | | | 0.85 | 0.80 | 1.89 | 1.89 | 10.00 | 104.2 | 197.0 | 197.0 | CONC | 525 | 0.25 | 8.5 | 224.3 | 1.00 | 0.14 | 87.8% |
| 9,10 | 271 | M40 | | | | | | | | 0.50 | | | | | 0.50 | 0.70 | 0.97 | 26.37 | 17.92 | 75.2 | 1982.2 | | CONC | 1350 | 0.40 | 82.6 | 3521.6 | 2.38 | 0.58 | 77.6% |
| 11 | 269A | M40 | | | | | | | | 2.91 | | | | | 2.91 | 0.20 | 1.62 | 1.62 | 15.00 | 83.6 | 135.2 | 135.2 | CONC | 450 | 0.25 | 54.5 | 148.7 | 0.91 | 1.00 | 90.9% |
| 13 | 267 | 265 | | | | | | | | 0.30 | | | | | 0.30 | 0.65 | 0.54 | 0.54 | 10.00 | 104.2 | 56.5 | | PVC | 300 | 0.65 | 86.6 | 81.3 | 1.11 | 1.29 | 69.4% |
| 14 | 265 | M41 | | | | | | | | 0.78 | 0.40 | | | | 1.18 | 0.62 | 2.02 | 2.56 | 15.00 | 83.6 | 214.2 | 214.2 | CONC | 525 | 0.50 | 115.4 | 317.2 | 1.42 | 1.35 | 67.5% |
| 16 | 261 | 259 | | | | | | | | 0.15 | | | | | 0.15 | 0.55 | 0.23 | 0.23 | 15.00 | 83.6 | 19.2 | | PVC | 250 | 0.65 | 34.9 | 50.0 | 0.99 | 0.59 | 38.3% |
| | 259 | 257 | | | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 15.00 | 0.0 | 18.7 | 18.7 | PVC | 250 | 0.65 | 10.4 | 50.0 | 0.99 | 0.18 | 37.5% |
| 17 | 257 | 253 | | | | | | | | 0.79 | | | | | 0.79 | 0.65 | 1.43 | 1.66 | 15.76 | 81.2 | 134.5 | | CONC | 525 | 0.30 | 115.2 | 245.7 | 1.10 | 1.75 | 54.7% |
| 18 | 255 | 253 | | | | | | | | 0.19 | 0.15 | | | | 0.34 | 0.61 | 0.57 | 0.57 | 15.00 | 83.6 | 47.9 | 47.9 | PVC | 300 | 0.65 | 45.3 | 81.3 | 1.11 | 0.68 | 58.8% |
| 19 | 253 | 251 | | | | | | | | 0.21 | 0.38 | | | | 0.59 | 0.59 | 0.96 | 3.19 | 17.51 | 76.2 | 243.2 | | CONC | 600 | 0.30 | 80.5 | 350.8 | 1.20 | 1.12 | 69.3% |
| 20 | 251 | M42 | | | | | | | | 0.61 | | | | | 0.61 | 0.65 | 1.10 | 4.29 | 18.63 | 73.4 | 315.1 | 315.1 | CONC | 600 | 0.50 | 77.2 | 452.9 | 1.55 | 0.83 | 69.6% |

**INFORMATION FROM FERNBANK
CROSSING PHASE 1 & 2
DEVELOPMENT STORMWATER
MANAGEMENT REPORT.**

Fernbank Crossing - Storm Sewer Design Sheet (Rational Method)

| LOCATION | | | AREA | | | | | | | | | | | FLOW | | | | | Total Peak Flow (Q) (L/s) | PROPOSED SEWER | | | | | | | | |
|----------|-----------|---------|-----------|--|-------------------|---------|-------|----------------|---------------------|-------------------|------------------|-----------------|------|-----------------------------|----------------|---------------|-----------------------|------------------------|---------------------------|-----------------|-----------|-----------|-----------|------------|----------------|--------------------------|---------------------|-------------|
| Location | From node | To node | Mixed Use | Park N' Ride Paramedic Post Medium Block | Arterial Road ROW | Schools | Parks | Hydro Corridor | Singles Front Yards | Singles Rear Yard | Towns Front Yard | Towns Rear Yard | | Weighted Runoff Coefficient | Indivi 2.78 AR | Accum 2.78 AR | Time of Concentration | Rain Intensity (mm/hr) | | Peak Flow (L/s) | Pipe Type | Size (mm) | Grade (%) | Length (m) | Capacity (l/s) | Full Flow Velocity (m/s) | Time of Flow (min.) | Q/Qfull (%) |
| | | | | | | | | | | | | | | | | | | 5yr | 10yr | | | | | | | | | |
| | | | 0.80 | 0.80 | 0.90 | 0.60 | 0.40 | 0.20 | 0.65 | 0.55 | 0.70 | 0.60 | (ha) | | | | | | (L/s) | | | | | | | | | |
| 21 | 245 | 243 | | | | | | | 0.32 | | | 0.32 | 0.55 | 0.49 | 0.49 | 15.00 | 83.6 | | 40.9 | | PVC | 250 | 0.65 | 66.9 | 50.0 | 0.99 | 1.13 | 81.7% |
| | 243 | 241 | | | | | | | 0.35 | | | 0.35 | 0.65 | 0.63 | 1.12 | 16.13 | 80.1 | | 0.0 | | PVC | 375 | 0.65 | 12.9 | 147.5 | 1.29 | 0.17 | 60.9% |
| 22 | 241 | M44 | | | | | | | 0.30 | 0.30 | | 0.60 | 0.60 | 1.00 | 2.12 | 16.30 | 79.6 | | 168.9 | | CONC | 450 | 1.00 | 67.3 | 297.4 | 1.81 | 0.62 | 56.8% |
| 24 | 233A | 233 | 3.32 | | | | | | | | | 3.32 | 0.80 | 7.38 | 7.38 | 10.00 | 104.2 | | 769.3 | | CONC | 825 | 0.45 | 8.5 | 1004.6 | 1.82 | 0.08 | 76.6% |
| 25 | 233 | 231 | | | | | | | 0.35 | | | 0.35 | 0.70 | 0.68 | 8.06 | 10.08 | 103.8 | | 837.0 | | CONC | 825 | 0.45 | 114.0 | 1004.6 | 1.82 | 1.04 | 83.3% |
| 26 | 231 | 229 | | | | | | | 0.24 | | | 0.24 | 0.70 | 0.47 | 8.53 | 11.12 | 98.6 | | 841.4 | | CONC | 825 | 0.50 | 82.0 | 1058.9 | 1.92 | 0.71 | 79.5% |
| 27 | 237A | 237 | 1.58 | | | | | | | | | 1.58 | 0.80 | 3.51 | 3.51 | 10.00 | 104.2 | | 366.1 | | CONC | 600 | 0.50 | 9.0 | 452.9 | 1.55 | 0.10 | 80.8% |
| 28 | 237 | 235 | | | | | | | 0.15 | | | 0.15 | 0.70 | 0.29 | 3.81 | 10.10 | 103.7 | | 394.6 | | CONC | 600 | 1.40 | 49.0 | 757.9 | 2.60 | 0.31 | 52.1% |
| 29 | 235 | 229 | | | | | | | 0.37 | | | 0.37 | 0.65 | 0.67 | 4.47 | 10.41 | 102.1 | | 456.7 | | CONC | 600 | 1.85 | 88.1 | 871.3 | 2.99 | 0.49 | 52.4% |
| 30 | 229 | 227 | | | | | | | 0.57 | | | 0.57 | 0.65 | 1.03 | 14.04 | 11.83 | 95.4 | | 1339.2 | | CONC | 975 | 0.50 | 117.4 | 1653.2 | 2.15 | 0.91 | 81.0% |
| 31 | 227 | M45 | | | | | | | 0.73 | 0.47 | | 1.20 | 0.61 | 2.04 | 16.07 | 15.00 | 83.6 | | 1343.1 | | CONC | 975 | 0.65 | 120.0 | 1884.9 | 2.45 | 0.82 | 71.3% |
| | 223 | 221 | | | | | | | | | | 0.00 | | 0.00 | 0.00 | 10.00 | | | 0.0 | | PVC | 250 | 0.65 | 57.1 | 50.0 | 0.99 | 0.96 | 0.0% |
| | 221 | 219 | | | | | | | | | | 0.00 | | 0.00 | 0.00 | 10.00 | | | 0.0 | | PVC | 250 | 0.65 | 8.6 | 50.0 | 0.99 | 0.15 | 0.0% |
| 33 | 219 | 217 | | | | | | | 0.41 | 0.50 | | 0.91 | 0.60 | 1.51 | 1.51 | 15.00 | 83.6 | | 125.8 | | PVC | 375 | 1.00 | 76.8 | 182.9 | 1.60 | 0.80 | 68.8% |
| 34 | 217 | 213 | | | | | | | 0.48 | | | 0.48 | 0.65 | 0.87 | 2.37 | 15.80 | 81.1 | | 192.3 | | CONC | 450 | 1.00 | 71.7 | 297.4 | 1.81 | 0.66 | 64.7% |
| 35 | 215 | 213 | | | | | | | 0.41 | | | 0.41 | 0.55 | 0.63 | 0.63 | 15.00 | 83.6 | | 52.4 | | PVC | 300 | 0.65 | 42.6 | 81.3 | 1.11 | 0.64 | 64.4% |
| 36 | 213 | 211 | | | | | | | 0.25 | 0.14 | | 0.39 | 0.61 | 0.67 | 3.67 | 16.46 | 79.1 | | 290.0 | | CONC | 600 | 0.50 | 64.9 | 452.9 | 1.55 | 0.70 | 64.0% |
| 37 | 211 | 209 | | | | | | | 0.25 | 0.30 | | 0.55 | 0.60 | 0.91 | 4.58 | 17.15 | 77.2 | | 353.2 | | CONC | 675 | 0.30 | 78.4 | 480.3 | 1.30 | 1.00 | 73.5% |
| | 209 | 207 | | | | | | | | | | 0.00 | | 0.00 | 4.58 | 18.16 | 74.6 | | 341.2 | | CONC | 675 | 0.30 | 8.7 | 480.3 | 1.30 | 0.11 | 71.0% |
| 38 | 207 | 205 | | | | | | | 0.41 | 0.21 | | 0.62 | 0.62 | 1.06 | 5.64 | 18.27 | 74.3 | | 418.8 | | CONC | 675 | 0.45 | 65.8 | 588.3 | 1.59 | 0.69 | 71.2% |
| | 205 | 203 | | | | | | | | | | 0.00 | | 0.00 | 5.64 | 18.96 | 72.6 | | 409.4 | | CONC | 675 | 0.45 | 6.0 | 588.3 | 1.59 | 0.06 | 69.6% |
| | 203 | M46 | | | | | | | 0.21 | | | 0.21 | 0.65 | 0.38 | 6.02 | 19.02 | 72.5 | | 436.1 | | CONC | 750 | 0.25 | 66.3 | 580.7 | 1.27 | 0.87 | 75.1% |

Fernbank Crossing - Storm Sewer Design Sheet (Rational Method)

| LOCATION | | | AREA | | | | | | | | | | | | FLOW | | | | | Total Peak Flow (Q) (L/s) | PROPOSED SEWER | | | | | | | | | |
|--------------|-----------|---------|-----------|--------------|----------------|-------------------|---------|-------|----------------|---------------------|-------------------|------------------|-----------------|------------|-----------------------------|----------------|---------------|-----------------------|------------------------|---------------------------|-----------------|-----------|-----------|-----------|------------|----------------|--------------------------|---------------------|-------------|-------|
| Location | From node | To node | Mixed Use | Park N' Ride | Paramedic Post | Arterial Road ROW | Schools | Parks | Hydro Corridor | Singles Front Yards | Singles Rear Yard | Towns Front Yard | Towns Rear Yard | Total Area | Weighted Runoff Coefficient | Indivi 2.78 AR | Accum 2.78 AR | Time of Concentration | Rain Intensity (mm/hr) | | Peak Flow (L/s) | Pipe Type | Size (mm) | Grade (%) | Length (m) | Capacity (l/s) | Full Flow Velocity (m/s) | Time of Flow (min.) | Q/Qfull (%) | |
| | | | | | | | | | | | | | | | | | | | 5yr | | | | | | | | | | | |
| South Outlet | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 107 | FUT | 363 | | | 5.15 | | | | | 3.90 | 1.36 | | | 10.41 | 0.71 | 20.58 | 20.58 | 20.48 | 69.2 | 1424.5 | 1424.5 | CONC | 1350 | 0.20 | 58.8 | 2490.2 | 1.69 | 0.58 | 57.2% | |
| 105 | 391 | 363 | | | 0.64 | 4.13 | | | | 0.22 | | | | 0.22 | 0.65 | 0.40 | 0.40 | 15.00 | 83.6 | 33.2 | 1469.2 | CONC | 1050 | 0.50 | 120.4 | 2014.4 | 2.25 | 0.89 | 72.9% | |
| 101 | 371 | 369 | | | | | | | | 0.42 | 0.09 | | | 0.51 | 0.63 | 0.90 | 0.90 | 15.00 | 83.6 | 74.9 | PVC | 375 | 0.65 | 53.5 | 147.5 | 1.29 | 0.69 | 50.8% | | |
| 369 | 367 | | | | | | | | | 0.00 | | | | 0.00 | 0.00 | 0.00 | 0.00 | 15.00 | | 0.0 | 73.0 | CONC | 450 | 0.20 | 50.9 | 133.0 | 0.81 | 1.05 | 54.9% | |
| 102 | 367 | 365 | | | | | | | | 0.35 | 0.18 | | | 0.53 | 0.62 | 0.91 | 1.80 | 16.74 | 78.3 | 141.3 | CONC | 600 | 0.15 | 59.8 | 248.1 | 0.85 | 1.17 | 57.0% | | |
| 103 | 365A | 365 | | | 1.39 | | | | | 1.39 | 0.80 | | | 3.09 | 3.09 | 10.00 | 104.2 | | 322.1 | 322.1 | CONC | 600 | 0.30 | 8.7 | 350.8 | 1.20 | 0.12 | 91.8% | | |
| 104 | 365 | 363 | | | | | | | | 0.18 | 0.08 | | | 0.26 | 0.62 | 0.45 | 5.34 | 17.91 | 75.2 | 401.8 | CONC | 825 | 0.15 | 66.1 | 580.0 | 1.05 | 1.05 | 69.3% | | |
| 108 | 363 | 361 | | | | | | | | 0.20 | | | | 0.20 | 0.65 | 0.36 | 6.10 | 20.48 | 69.2 | 422.4 | 1374.6 | CONC | 1350 | 1.74 | 78.6 | 7344.9 | 4.97 | 0.26 | 18.7% | |
| 109 | 361 | 341 | | | | | | | | 0.34 | 0.36 | | | 0.70 | 0.60 | 1.16 | 7.27 | 20.74 | 68.7 | 499.0 | 1443.6 | CONC | 1350 | 1.74 | 81.1 | 7344.9 | 4.97 | 0.27 | 19.7% | |
| 111 | FUT | 341 | | | | | | | | 3.23 | 1.67 | | | 4.90 | 0.62 | 8.39 | 8.39 | 19.28 | 71.9 | 603.1 | 603.1 | CONC | 825 | 1.88 | 86.2 | 2053.3 | 3.72 | 0.39 | 29.4% | |
| 110 | 341A | 341 | | | | | | | | 2.12 | | | | 2.12 | 0.60 | 3.54 | 3.54 | 10.00 | 104.2 | 368.4 | 368.4 | CONC | 675 | 0.25 | 12.5 | 438.5 | 1.19 | 0.18 | 84.0% | |
| 112 | 341 | 339 | | | | | | | | 0.18 | | | | 0.18 | 0.65 | 0.33 | 19.52 | 21.01 | 68.1 | 1329.2 | 2266.1 | CONC | 1650 | 0.40 | 67.8 | 6013.7 | 2.72 | 0.41 | 37.7% | |
| 113 | 339 | 337 | | | | | | | | 0.11 | | | | 0.11 | 0.65 | 0.20 | 19.72 | 21.43 | 67.3 | 1326.2 | 2251.5 | CONC | 1800 | 0.25 | 45.2 | 5995.9 | 2.28 | 0.33 | 37.6% | |
| 114 | 337 | 335 | | | | | | | | 0.29 | | | | 0.29 | 0.65 | 0.52 | 20.24 | 21.76 | 66.6 | 1348.3 | 2264.6 | CONC | 1800 | 0.25 | 50.8 | 5995.9 | 2.28 | 0.37 | 37.8% | |
| 115 | 335A | 335 | | | 2.83 | | | | | 2.83 | 0.60 | | | 4.72 | 4.72 | 10.00 | 104.2 | | 491.8 | 491.8 | CONC | 750 | 0.25 | 17.9 | 580.7 | 1.27 | 0.23 | 84.7% | | |
| 116 | 335 | 301 | | | | | | | | 0.21 | | | | 0.21 | 0.65 | 0.38 | 25.34 | 22.13 | 65.9 | 1669.9 | 2576.4 | CONC | 1800 | 0.30 | 57.7 | 6568.2 | 2.50 | 0.38 | 39.2% | |
| 117 | FUT | 301 | | | | | | | | 1.20 | 5.13 | 1.57 | | 7.90 | 0.59 | 11.67 | 11.67 | 23.33 | 63.7 | 743.4 | 743.4 | CONC | 975 | 0.61 | 54.7 | 1826.0 | 2.37 | 0.38 | 40.7% | |
| 118 | 301 | M97 | | | | | | | | | 0.30 | | | | 0.30 | 0.70 | 0.58 | 37.60 | 23.76 | 63.0 | 2366.8 | 3232.6 | CONC | 1950 | 0.30 | 78.3 | 8131.0 | 2.64 | 0.49 | 39.8% |
| 119 | M97 | M98 | | | | | | | | 0.94 | 0.40 | | | 1.34 | 0.59 | 2.22 | 39.81 | 24.25 | 62.1 | 2473.0 | 3327.2 | CONC | 2100 | 0.20 | 78.3 | 8089.5 | 2.26 | 0.58 | 41.1% | |
| 119 | M98 | M99 | | | | | | | | | 0.00 | | | | 0.00 | 0.00 | 0.00 | 11.76 | 24.83 | 61.2 | 2435.3 | 3276.4 | CONC | 2400 | 0.15 | 29.6 | 10002.3 | 2.14 | 0.23 | 32.8% |

Q = 2.78 AIR

WHERE : Q = PEAK FLOW IN LITRES PER SECOND (L/s)

A = AREA IN HECTARES (ha)

I = RAINFALL INTENSITY IN MILLIMETERS PER HOUR (mm/hr)

R = WEIGHTED RUNOFF COEFFICIENT

Q = (1/n) A R(2/3)So(1/2)

WHERE :

Q = CAPACITY (L/s)

n = MANNING COEFFICIENT OF ROUGHNESS (0.013)

A = FLOW AREA (m²)

Project: Fernbank Crossing (108180-10)

Designed: KJM

Checked: MAB

Date: August 17 2012



NOVATECH
ENGINEERING
CONSULTANTS LTD.

Fernbank Crossing - Storm Sewer Design Sheet (Fixed Tc)

| LOCATION | | | AREA | | | | | | | | | | | | | FLOW | | | | | | | Total Peak Flow (Q) (L/s) | PROPOSED SEWER | | | | | | | | | | | |
|---------------------|-----------|---------|-----------|-----------------------------|---------------|---------|-------|----------------|---------------------|--------------------|-------------|------------|---------------------|---------------------|-----------------------------|-----------------------------|----------|----------|------------------------|--------|----------|--------------------|---------------------------|----------------|-----------|-----------|------------|----------------|--------------------------|---------------------|-------------|-------|-------|-------|-------|
| Location | From node | To node | Mixed Use | Park N' Ride | Arterial Road | Schools | Parks | Hydro Corridor | Singles Front Yards | Singles Rear Yards | Towns Front | Towns Rear | Total Area (10 min) | Total Area (15 min) | Weighted Runoff Coefficient | Weighted Runoff Coefficient | 2.78 AR | 2.78 AR | Rain Intensity (mm/hr) | | | Peak Flow (10 min) | Peak Flow (15 min) | Pipe Type | Size (mm) | Grade (%) | Length (m) | Capacity (l/s) | Full Flow Velocity (m/s) | Time of Flow (min.) | Q/Qfull (%) | | | | |
| | | | | Paramedic Post Medium Block | ROW | | | | | | | | (ha) | (ha) | (10 min) | (15 min) | (10 min) | (15 min) | 5yr | 10yr | (10 min) | (15 min) | (L/s) | (L/s) | | | | | | | | | | | |
| | | | 0.80 | 0.80 | 0.90 | 0.60 | 0.40 | 0.20 | 0.65 | 0.55 | 0.70 | 0.60 | (ha) | (ha) | (10 min) | (15 min) | (10 min) | (15 min) | 10.00 | 15.00 | 10.00 | 15.00 | | | | | | | | | | | | | |
| North Outlet | | | | | | | | | | | | | 0.00 | 13.95 | | 0.38 | 0.00 | 14.54 | 104.2 | 83.6 | | 0.0 | 1215.2 | | | | | | | | | | | | |
| CRT | CRT | 287 | | | | | | | | | | | 0.00 | | | 0.00 | 0.00 | 0.00 | 0.00 | | 122.1 | 97.85 | | 0.0 | 1215.2 | | | | | | | | | | |
| 1 | 287 | 285 | 0.34 | 3.11 | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 104.19 | 83.56 | | | | 0.00 | 2257.9 | CONC | 1200 | 0.35 | 76.7 | 2406.2 | 2.06 | 0.62 | 93.8% | | | |
| | 285 | 283 | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 104.19 | 83.56 | | | | 0.00 | 2257.9 | CONC | 1200 | 0.35 | 76.7 | 2406.2 | 2.06 | 0.62 | 93.8% | | | |
| 2 | 283 | 281 | 1.11 | | | | | | | | | | 1.11 | 0.00 | 0.80 | 0.00 | 2.47 | 0.00 | 104.19 | 83.56 | | | | 2515.1 | CONC | 1350 | 0.25 | 41.5 | 2784.1 | 1.88 | 0.37 | 90.3% | | | |
| 3 | 281 | 275 | 2.00 | | | | | | | | | | 2.00 | 0.00 | 0.80 | 0.00 | 4.45 | 0.00 | 104.19 | 83.56 | | | | 2978.6 | CONC | 1350 | 0.30 | 11.0 | 3049.8 | 2.06 | 0.09 | 97.7% | | | |
| 4 | 279 | 277 | | | | | | | | | | | 0.20 | 0.20 | 0.00 | 0.70 | 0.00 | 0.39 | 0.00 | 104.19 | 83.56 | | | | 40.6 | PVC | 250 | 0.65 | 69.8 | 50.0 | 0.99 | 1.18 | 81.1% | | |
| 5 | 277 | 275 | | | | | | | | | | | 0.14 | 0.14 | 0.00 | 0.70 | 0.00 | 0.27 | 0.00 | 104.19 | 83.56 | | | | 68.9 | PVC | 375 | 0.30 | 83.0 | 100.2 | 0.88 | 1.57 | 68.8% | | |
| 6 | 275 | 273 | | | | | | | | | | | 0.35 | 0.35 | 0.00 | 0.70 | 0.00 | 0.68 | 0.00 | 104.19 | 83.56 | | | | 3118.5 | CONC | 1350 | 0.35 | 82.8 | 3294.2 | 2.23 | 0.62 | 94.7% | | |
| 7 | 273 | 271 | | | | | | | | | | | 0.36 | 0.36 | 0.00 | 0.70 | 0.00 | 0.70 | 0.00 | 104.19 | 83.56 | | | | 3191.5 | CONC | 1350 | 0.35 | 80.5 | 3294.2 | 2.23 | 0.60 | 96.9% | | |
| 8 | 271A | 271 | 0.85 | | | | | | | | | | 0.85 | 0.00 | 0.80 | 0.00 | 1.89 | 0.00 | 104.19 | 83.56 | | | | 197.0 | CONC | 525 | 0.25 | 8.5 | 224.3 | 1.00 | 0.14 | 87.8% | | | |
| 9,10 | 271 | M40 | | | | | | | | | | | 0.50 | 0.50 | 0.00 | 0.70 | 0.00 | 0.97 | 0.00 | 104.19 | 83.56 | | | | 3489.8 | CONC | 1350 | 0.40 | 82.6 | 3521.6 | 2.38 | 0.58 | 99.1% | | |
| 11 | 269A | M40 | | | | | | | | | | | 2.91 | | 0.00 | 2.91 | 0.00 | 0.20 | 0.00 | 1.62 | 104.19 | 83.56 | | | | 135.2 | CONC | 450 | 0.25 | 54.5 | 148.7 | 0.91 | 1.00 | 90.9% | |
| 13 | 267 | 265 | | | | | | | | | | | 0.30 | 0.30 | 0.00 | 0.65 | 0.00 | 0.54 | 0.00 | 104.19 | 83.56 | | | | 56.5 | PVC | 300 | 0.65 | 86.6 | 81.3 | 1.11 | 1.29 | 69.4% | | |
| 14 | 265 | M41 | | | | | | | | | | | 0.78 | 0.40 | 0.78 | 0.40 | 0.65 | 0.55 | 1.41 | 0.61 | 104.19 | 83.56 | | | | 254.4 | CONC | 525 | 0.50 | 115.4 | 317.2 | 1.42 | 1.35 | 80.2% | |
| 16 | 261 | 259 | | | | | | | | | | | 0.15 | | 0.00 | 0.15 | 0.00 | 0.55 | 0.00 | 0.23 | 104.19 | 83.56 | | | | 19.2 | PVC | 250 | 0.65 | 34.9 | 50.0 | 0.99 | 0.59 | 38.3% | |
| | 259 | 257 | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.90 | 0.00 | 0.00 | 0.00 | 122.14 | 97.85 | | | | 19.2 | PVC | 250 | 0.65 | 10.4 | 50.0 | 0.99 | 0.18 | 38.3% |
| 17 | 257 | 253 | | | | | | | | | | | 0.79 | 0.79 | 0.00 | 0.65 | 0.00 | 1.43 | 0.00 | 104.19 | 83.56 | | | | 167.9 | CONC | 525 | 0.30 | 115.2 | 245.7 | 1.10 | 1.75 | 68.3% | | |
| 18 | 255 | 253 | | | | | | | | | | | 0.19 | 0.15 | 0.19 | 0.15 | 0.65 | 0.55 | 0.34 | 0.23 | 104.19 | 83.56 | | | | 54.9 | PVC | 300 | 0.65 | 45.3 | 81.3 | 1.11 | 0.68 | 67.5% | |
| 19 | 253 | 251 | | | | | | | | | | | 0.21 | 0.38 | 0.21 | 0.38 | 0.65 | 0.55 | 0.38 | 0.58 | 104.19 | 83.56 | | | | 310.9 | CONC | 600 | 0.30 | 80.5 | 350.8 | 1.20 | 1.12 | 88.6% | |
| 20 | 251 | M42 | | | | | | | | | | | 0.61 | | 0.61 | 0.00 | 0.65 | 0.00 | 1.10 | 0.00 | 104.19 | 83.56 | | | | 425.8 | CONC | 600 | 0.50 | 77.2 | 452.9 | 1.55 | 0.83 | 94.0% | |

**INFORMATION FROM FERNBANK
CROSSING PHASE 1 & 2
DEVELOPMENT STORMWATER
MANAGEMENT REPORT.**

Fernbank Crossing - Storm Sewer Design Sheet (Fixed Tc)

| LOCATION | | | AREA | | | | | | | | | | | | | FLOW | | | | | | | | PROPOSED SEWER | | | | | | | | | | |
|----------|-----------|---------|-----------|-----------------------------|---------------|---------|-------|----------------|---------------------|--------------------|------------------|-----------------|---------------------|---------------------|-----------------------------|-----------------------------|----------|----------|------------------------|----------|----------|--------------------|--------------------|----------------|--------|-------|--------|----------|--------------------------|---------------------|-------------|------|-------|-------|
| Location | From node | To node | Mixed Use | Park N' Ride | Arterial Road | Schools | Parks | Hydro Corridor | Singles Front Yards | Singles Rear Yards | Towns Front Yard | Towns Rear Yard | Total Area (10 min) | Total Area (15 min) | Weighted Runoff Coefficient | Weighted Runoff Coefficient | 2.78 AR | 2.78 AR | Rain Intensity (mm/hr) | | | Peak Flow (10 min) | Peak Flow (15 min) | Pipe | Size | Grade | Length | Capacity | Full Flow Velocity (m/s) | Time of Flow (min.) | Q/Qfull (%) | | | |
| | | | | Paramedic Post Medium Block | ROW | | | | | | | | (ha) | (ha) | (10 min) | (15 min) | (10 min) | (15 min) | 5yr | 10yr | (10 min) | (15 min) | (L/s) | (L/s) | | | | | | | | | | |
| | | | 0.80 | 0.80 | 0.90 | 0.60 | 0.40 | 0.20 | 0.65 | 0.55 | 0.70 | 0.60 | (ha) | (ha) | (10 min) | (15 min) | (10 min) | (15 min) | (10 min) | (15 min) | (L/s) | (L/s) | | | | | | | | | | | | |
| 21 | 245 | 243 | | | | | | | 0.32 | | | | 0.00 | 0.32 | 0.00 | 0.55 | 0.00 | 0.49 | 104.19 | 83.56 | | | 0.00 | 40.88 | 40.9 | PVC | 250 | 0.65 | 66.9 | 50.0 | 0.99 | 1.13 | 81.7% | |
| | | | | | | | | | | | | | 0.00 | 0.00 | 0.90 | 0.00 | 0.00 | | | 122.14 | 97.85 | | | 0.00 | | | | | | | | | | |
| | | 243 | 241 | | | | | | 0.35 | | | | 0.35 | 0.00 | 0.65 | 0.00 | 0.63 | 0.00 | 104.19 | 83.56 | | | 65.90 | 0.00 | 106.8 | PVC | 375 | 0.65 | 12.9 | 147.5 | 1.29 | 0.17 | 72.4% | |
| 22 | 241 | M44 | | | | | | | 0.30 | 0.30 | | | 0.30 | 0.30 | 0.65 | 0.55 | 0.54 | 0.46 | 104.19 | 83.56 | | | 56.48 | 38.33 | 201.6 | CONC | 450 | 1.00 | 67.3 | 297.4 | 1.81 | 0.62 | 67.8% | |
| | | | | | | | | | | | | | 0.00 | 0.00 | 0.90 | 0.00 | 0.00 | | | 122.14 | 97.85 | | | 0.00 | | | | | | | | | | |
| 24 | 233A | 233 | 3.32 | | | | | | | | | | 3.32 | 0.00 | 0.80 | 0.00 | 7.38 | 0.00 | 104.19 | 83.56 | | | 769.33 | 0.00 | 769.3 | CONC | 825 | 0.45 | 8.5 | 1004.6 | 1.82 | 0.08 | 76.6% | |
| | | | | | | | | | | | | | 0.00 | 0.00 | 0.90 | 0.00 | 0.00 | | | 122.14 | 97.85 | | | 0.00 | | | | | | | | | | |
| 25 | 233 | 231 | | | | | | | 0.35 | | | | 0.35 | 0.00 | 0.70 | 0.00 | 0.68 | 0.00 | 104.19 | 83.56 | | | 70.97 | 0.00 | 840.3 | CONC | 825 | 0.45 | 114.0 | 1004.6 | 1.82 | 1.04 | 83.6% | |
| 26 | 231 | 229 | | | | | | | | | | | 0.24 | 0.24 | 0.00 | 0.70 | 0.00 | 0.47 | 0.00 | 104.19 | 83.56 | | | 48.66 | 0.00 | 889.0 | CONC | 825 | 0.50 | 82.0 | 1058.9 | 1.92 | 0.71 | 84.0% |
| | | | | | | | | | | | | | 0.00 | 0.00 | 0.90 | 0.00 | 0.00 | | | 122.14 | 97.85 | | | 0.00 | | | | | | | | | | |
| 27 | 237A | 237 | 1.58 | | | | | | | | | | 1.58 | 0.00 | 0.80 | 0.00 | 3.51 | 0.00 | 104.19 | 83.56 | | | 366.13 | 0.00 | 366.1 | CONC | 600 | 0.50 | 9.0 | 452.9 | 1.55 | 0.10 | 80.8% | |
| | | | | | | | | | | | | | 0.00 | 0.00 | 0.90 | 0.00 | 0.00 | | | 122.14 | 97.85 | | | 0.00 | | | | | | | | | | |
| 28 | 237 | 235 | | | | | | | 0.15 | | | | 0.15 | 0.00 | 0.70 | 0.00 | 0.29 | 0.00 | 104.19 | 83.56 | | | 30.41 | 0.00 | 396.5 | CONC | 600 | 1.40 | 49.0 | 757.9 | 2.60 | 0.31 | 52.3% | |
| | | | | | | | | | | | | | 0.00 | 0.00 | 0.90 | 0.00 | 0.00 | | | 122.14 | 97.85 | | | 0.00 | | | | | | | | | | |
| 29 | 235 | 229 | | | | | | | 0.37 | | | | 0.37 | 0.00 | 0.65 | 0.00 | 0.67 | 0.00 | 104.19 | 83.56 | | | 69.66 | 0.00 | 466.2 | CONC | 600 | 1.85 | 88.1 | 871.3 | 2.99 | 0.49 | 53.5% | |
| | | | | | | | | | | | | | 0.00 | 0.00 | 0.90 | 0.00 | 0.00 | | | 122.14 | 97.85 | | | 0.00 | | | | | | | | | | |
| 30 | 229 | 227 | | | | | | | 0.57 | | | | 0.57 | 0.00 | 0.65 | 0.00 | 1.03 | 0.00 | 104.19 | 83.56 | | | 107.32 | 0.00 | 1462.5 | CONC | 975 | 0.50 | 117.4 | 1653.2 | 2.15 | 0.91 | 88.5% | |
| | | | | | | | | | | | | | 0.00 | 0.00 | 0.90 | 0.00 | 0.00 | | | 122.14 | 97.85 | | | 0.00 | | | | | | | | | | |
| 31 | 227 | M45 | | | | | | | 0.73 | 0.47 | | | 0.73 | 0.47 | 0.65 | 0.55 | 1.32 | 0.72 | 104.19 | 83.56 | | | 137.44 | 60.05 | 1660.0 | CONC | 975 | 0.65 | 120.0 | 1884.9 | 2.45 | 0.82 | 88.1% | |
| | | | | | | | | | | | | | 0.00 | 0.00 | 0.90 | 0.00 | 0.00 | | | 122.14 | 97.85 | | | 0.00 | | | | | | | | | | |
| | 223 | 221 | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 104.19 | 83.56 | | | 0.00 | 0.00 | 0.0 | PVC | 250 | 0.65 | 57.1 | 50.0 | 0.99 | 0.96 | 0.0% | |
| | | 221 | 219 | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 104.19 | 83.56 | | | 0.00 | 0.00 | 0.0 | PVC | 250 | 0.65 | 8.6 | 50.0 | 0.99 | 0.15 | 0.0% | |
| 33 | 219 | 217 | | | | | | | 0.41 | 0.50 | | | 0.41 | 0.50 | 0.65 | 0.55 | 0.74 | 0.76 | 104.19 | 83.56 | | | 77.19 | 63.88 | 141.1 | PVC | 375 | 1.00 | 76.8 | 182.9 | 1.60 | 0.80 | 77.1% | |
| | | | | | | | | | | | | | 0.00 | 0.00 | 0.90 | 0.00 | 0.00 | | | 122.14 | 97.85 | | | 0.00 | | | | | | | | | | |
| 34 | 217 | 213 | | | | | | | 0.48 | | | | 0.48 | 0.00 | 0.65 | 0.00 | 0.87 | 0.00 | 104.19 | 83.56 | | | 90.37 | 0.00 | 231.4 | CONC | 450 | 1.00 | 71.7 | 297.4 | 1.81 | 0.66 | 77.8% | |
| | | | | | | | | | | | | | 0.00 | 0.00 | 0.90 | 0.00 | 0.00 | | | 122.14 | 97.85 | | | 0.00 | | | | | | | | | | |
| 35 | 215 | 213 | | | | | | | 0.41 | | | | 0.00 | 0.41 | 0.00 | 0.55 | 0. | | | | | | | | | | | | | | | | | |

Fernbank Crossing - Storm Sewer Design Sheet (Fixed Tc)

| LOCATION | | | AREA | | | | | | | | | | | | | FLOW | | | | | | | | PROPOSED SEWER | | | | | | | | | | | | |
|--------------|-----------|---------|-----------|-----------------------------|---------------|---------|-------|----------------|---------------------|--------------------|------------------|-----------------|---------------------|---------------------|-----------------------------|-----------------------------|----------|----------|------------------------|--------|----------|--------------------|--------------------|----------------|-----------|-----------|------------|----------------|--------------------------|---------------------|-------------|---------|--------|-------|-------|-------|
| Location | From node | To node | Mixed Use | Park N' Ride | Arterial Road | Schools | Parks | Hydro Corridor | Singles Front Yards | Singles Rear Yards | Towns Front Yard | Towns Rear Yard | Total Area (10 min) | Total Area (15 min) | Weighted Runoff Coefficient | Weighted Runoff Coefficient | 2.78 AR | 2.78 AR | Rain Intensity (mm/hr) | | | Peak Flow (10 min) | Peak Flow (15 min) | Pipe Type | Size (mm) | Grade (%) | Length (m) | Capacity (l/s) | Full Flow Velocity (m/s) | Time of Flow (min.) | Q/Qfull (%) | | | | | |
| | | | | Paramedic Post Medium Block | ROW | | | | | | | | (ha) | (ha) | (10 min) | (15 min) | (10 min) | (15 min) | 5yr | 10yr | (10 min) | (15 min) | (10 min) | (15 min) | (L/s) | (L/s) | | | | | | | | | | |
| | | | 0.80 | 0.80 | 0.90 | 0.60 | 0.40 | 0.20 | 0.65 | 0.55 | 0.70 | 0.60 | (ha) | (ha) | (10 min) | (15 min) | (10 min) | (15 min) | | | | | | | | | | | | | | | | | | |
| South Outlet | | | | | | | | | 3.90 | 1.36 | | | 9.05 | 1.36 | 0.74 | 0.55 | 18.50 | 2.08 | 104.19 | 83.56 | | | 1927.66 | 173.75 | | | | | | | | | | | | |
| 107 | FUT | 363 | | 5.15 | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | | 122.14 | 97.85 | 0.00 | | 2101.4 | CONC | 1350 | 0.20 | 58.8 | 2490.2 | 1.69 | 0.58 | 84.4% | | | |
| 105 | 391 | 363 | | 0.82 | 5.18 | | | | 0.22 | | | | 6.00 | | 0.89 | 14.78 | 0.00 | | | 122.14 | 97.85 | 1805.75 | 0.00 | | 1847.2 | CONC | 1050 | 0.50 | 120.4 | 2014.4 | 2.25 | 0.89 | 91.7% | | | |
| 101 | 371 | 369 | | | | | | | 0.42 | 0.09 | | | 0.42 | 0.09 | 0.65 | 0.55 | 0.76 | 0.14 | 104.19 | 83.56 | | | 79.08 | 11.50 | | | 90.6 | PVC | 375 | 0.65 | 53.5 | 147.5 | 1.29 | 0.69 | 61.4% | |
| 369 | 367 | | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | | 122.14 | 97.85 | 0.00 | | | 90.6 | CONC | 450 | 0.20 | 50.9 | 133.0 | 0.81 | 1.05 | 68.1% | | |
| 102 | 367 | 365 | | | | | | | 0.35 | 0.18 | | | 0.35 | 0.18 | 0.65 | 0.55 | 0.63 | 0.28 | 104.19 | 83.56 | | | 65.90 | 23.00 | | | 179.5 | CONC | 600 | 0.15 | 59.8 | 248.1 | 0.85 | 1.17 | 72.3% | |
| 103 | 365A | 365 | | 1.39 | | | | | | | | | 1.39 | 0.00 | 0.80 | 0.00 | 3.09 | 0.00 | 104.19 | 83.56 | | | 322.10 | 0.00 | | | 322.1 | CONC | 600 | 0.30 | 8.7 | 350.8 | 1.20 | 0.12 | 91.8% | |
| 104 | 365 | 363 | | | | | | | 0.18 | 0.08 | | | 0.18 | 0.08 | 0.65 | 0.55 | 0.33 | 0.12 | 104.19 | 83.56 | | | 33.89 | 10.22 | | | 545.7 | CONC | 825 | 0.15 | 66.1 | 580.0 | 1.05 | 1.05 | 94.1% | |
| 108 | 363 | 361 | | | | | | | 0.20 | | | | 0.20 | 0.00 | 0.65 | 0.00 | 0.36 | 0.00 | 104.19 | 83.56 | | | 37.66 | 0.00 | | | 4531.9 | CONC | 1350 | 1.74 | 78.6 | 7344.9 | 4.97 | 0.26 | 61.7% | |
| 109 | 361 | 341 | | | | | | | 0.34 | 0.36 | | | 0.34 | 0.36 | 0.65 | 0.55 | 0.61 | 0.55 | 104.19 | 83.56 | | | 64.01 | 45.99 | | | 4641.9 | CONC | 1350 | 1.74 | 81.1 | 7344.9 | 4.97 | 0.27 | 63.2% | |
| 111 | FUT | 341 | | | | | | | 3.23 | 1.67 | | | 3.23 | 1.67 | 0.65 | 0.55 | 5.84 | 2.55 | 104.19 | 83.56 | | | 608.13 | 213.36 | | | 821.5 | CONC | 825 | 1.88 | 86.2 | 2053.3 | 3.72 | 0.39 | 40.0% | |
| 110 | 341A | 341 | | 2.12 | | | | | | | | | 2.12 | 0.00 | 0.60 | 0.00 | 3.54 | 0.00 | 104.19 | 83.56 | | | 368.44 | 0.00 | | | 368.4 | CONC | 675 | 0.25 | 12.5 | 438.5 | 1.19 | 0.18 | 84.0% | |
| 112 | 341 | 339 | | | | | | | 0.18 | | | | 0.18 | 0.00 | 0.65 | 0.00 | 0.33 | 0.00 | 104.19 | 83.56 | | | 33.89 | 0.00 | | | 5865.8 | CONC | 1650 | 0.40 | 67.8 | 6013.7 | 2.72 | 0.41 | 97.5% | |
| 113 | 339 | 337 | | | | | | | 0.11 | | | | 0.11 | 0.00 | 0.65 | 0.00 | 0.20 | 0.00 | 104.19 | 83.56 | | | 20.71 | 0.00 | | | 5886.5 | CONC | 1800 | 0.25 | 45.2 | 5995.9 | 2.28 | 0.33 | 98.2% | |
| 114 | 337 | 335 | | | | | | | 0.29 | | | | 0.29 | 0.00 | 0.65 | 0.00 | 0.52 | 0.00 | 104.19 | 83.56 | | | 54.60 | 0.00 | | | 5941.1 | CONC | 1800 | 0.25 | 50.8 | 5995.9 | 2.28 | 0.37 | 99.1% | |
| 115 | 335A | 335 | | 2.83 | | | | | | | | | 2.83 | 0.00 | 0.60 | 0.00 | 4.72 | 0.00 | 104.19 | 83.56 | | | 491.84 | 0.00 | | | 491.8 | CONC | 750 | 0.25 | 17.9 | 580.7 | 1.27 | 0.23 | 84.7% | |
| 116 | 335 | 301 | | | | | | | 0.21 | | | | 0.21 | 0.00 | 0.65 | 0.00 | 0.38 | 0.00 | 104.19 | 83.56 | | | 39.54 | 0.00 | | | 6472.4 | CONC | 1800 | 0.30 | 57.7 | 6568.2 | 2.50 | 0.38 | 98.5% | |
| 117 | FUT | 301 | | | | | | | 1.20 | 5.13 | 1.57 | | 5.13 | 2.77 | 0.65 | 0.49 | 9.27 | 3.73 | 104.19 | 83.56 | | | 965.86 | 312.08 | | | 1277.9 | CONC | 975 | 0.61 | 54.7 | 1826.0 | 2.37 | 0.38 | 70.0% | |
| 118 | 301 | M97 | | | | | | | | | | | 0.30 | 0.30 | 0.00 | 0.70 | 0.00 | 0.58 | 0.00 | 104.19 | 83.56 | | | 60.83 | 0.00 | | | 7811.2 | CONC | 1950 | 0.30 | 78.3 | 8131.0 | 2.64 | 0.49 | 96.1% |
| 119 | M97 | M98 | | | | | | | | 0.94 | 0.40 | | | 0.40 | 0.94 | 0.70 | 0.55 | 0.78 | 1.44 | 104.19 | 83.56 | | | 81.10 | 120.09 | | | 8012.4 | CONC | 2100 | 0.20 | 78.0 | 8089.5 | 2.26 | 0.57 | 99.0% |
| | M98 | M99 | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 104.19 | 83.56 | | | 0.00 | 0.00 | | | 8012.4 | CONC | 2400 | 0.15 | 29.6 | 10002.3 | 2.14 | 0.23 | 80.1% | |

Q = 2.78 AIR

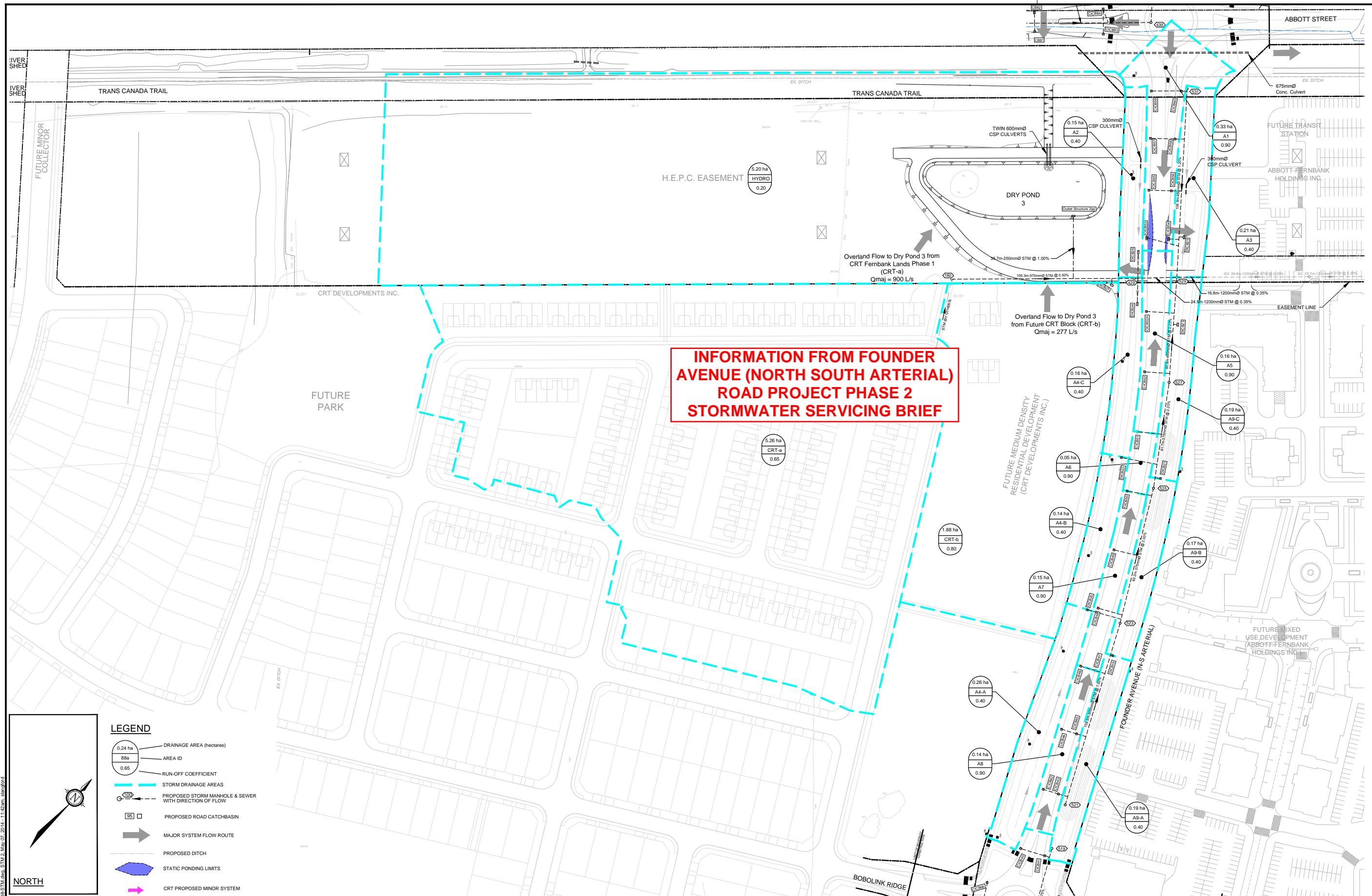
WHERE : Q = PEAK FLOW IN LITRES PER SECOND (L/s)

Q = (1/n) A R(2/3)S^{0.5}

WHERE :

Q = CAPACITY (L/s)

n = MANNING COEFFICIENT OF ROUGHNESS (0.013)

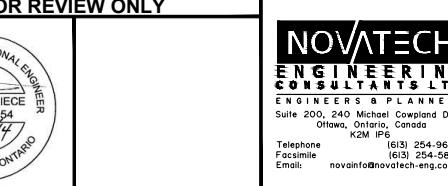
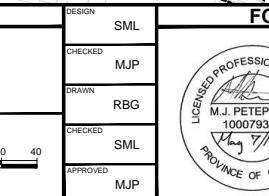


NOTE:
THE POSITION OF ALL POLE LINES, CONDUITS,
WATERMAINS, SEWERS AND OTHER
UNDERGROUND AND OVERGROUND UTILITIES AND
STRUCTURES IS NOT NECESSARILY SHOWN ON
THE CONTRACT DRAWINGS, AND WHERE SHOWN,
THE ACCURACY OF THE POSITION OF SUCH
UTILITIES AND STRUCTURES IS NOT GUARANTEED.
BEFORE STARTING WORK, DETERMINE THE EXACT
LOCATION OF ALL SUCH UTILITIES AND
STRUCTURES AND ASSUME ALL LIABILITY FOR
DAMAGE TO THEM.

FLOW CONNECTION

| 3. ISSUED WITH PHASE II ECA APPLICATION | MAY 7/14 | MJP |
|---|-----------|---------|
| 2. ISSUED WITH PHASE 2 RESPONSE TO COMMENTS | MAR 24/14 | MJP |
| 1. ISSUED WITH STORM WATER SERVICING BRIEF | DEC 18/13 | MJP |
| No. | REVISION | DATE BY |

| SCALE | SML | RBG | SML | MJP |
|---------------|-----|-----|--------|-----|
| 1:1000 | | | 1:1000 | |
| 0 10 20 30 40 | | | | |



| | |
|--|----------------------------|
| LOCATION City of Ottawa Fernbank Community Founder Avenue (N-S Arterial) | PROJECT No. 101108-07 |
| DRAWING NAME FOUNDER AVENUE (N-S ARTERIAL) INTERIM STORM DRAINAGE AREA PLAN | REV # 3 |
| | DRAWING No. 101108-STM2 |

Founder Avenue (North South Arterial) - Storm Sewer Design Sheet - Ultimate Design (Typical)

| LOCATION | | | AREA | | | | | | | | | | | | FLOW | | | | | | Total Peak Flow (Q) (L/s) | PROPOSED SEWER | | | | | | | | |
|---------------------|-----------|----------|-----------|--|-------------------|---------|-------|----------------|---------------------|--------------------|-----------------|----------------|-----------------|---------------------|-----------------------------|----------|----------------|-----------------------|------------------------|----------|------------------------------|----------------|-----------|-----------|------------|----------------|--------------------------|---------------------|-------------|-------|
| Location | From node | To node | Mixed Use | Park N' Ride Paramedic Post Medium Block | Arterial Road ROW | Schools | Parks | Hydro Corridor | Singles Front Yards | Singles Rear Yards | CRT Front Yards | CRT Rear Yards | Towns Rear Yard | Total Area (10 min) | Weighted Runoff Coefficient | 2.78 AR | Accum* 2.78 AR | Time of Concentration | Rain Intensity (mm/hr) | | Peak Flow (10 min)** | Pipe | Size (mm) | Grade (%) | Length (m) | Capacity (l/s) | Full Flow Velocity (m/s) | Time of Flow (min.) | Q/Qfull (%) | |
| | | | | | | | | | | | | | | | | | | | 5yr | 10yr | | | | | | | | | | |
| | | | 0.80 | 0.80 | 0.90 | 0.60 | 0.40 | 0.20 | 0.65 | 0.55 | 0.75 | 0.80 | 0.60 | (ha) | (10 min) | (10 min) | | | (10 min) | (10 min) | (L/s) | | | | | | | | | |
| North Outlet | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| DRY POND | DI | STM PIPE | | | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 10.00 | 104.19 | 0.00 | 30.0 | PVC | 250 | 1.00 | 35.7 | 62.0 | 1.22 | 0.49 | 48.4% |
| CRT/HYDRO | 180 | 429 | | | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 13.67 | 13.52 | 88.66 | 0.00 | 1230.5 | CONC | 975 | 0.50 | 105.3 | 1653.2 | 2.15 | 0.82 | 74.4% |
| ART (SW) | 421 | 423 | | | 0.20 | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 10.00 | 104.19 | 0.00 | 61.6 | PVC | 300 | 0.75 | 109.3 | 87.4 | 1.20 | 1.52 | 70.5% |
| ART (SW) | 423 | 425 | | | 0.12 | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 11.52 | 96.79 | 0.00 | 94.8 | PVC | 300 | 2.00 | 67.9 | 142.7 | 1.96 | 0.58 | 66.4% |
| ART (SW) | 425 | 427 | | | 0.11 | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 12.10 | 94.27 | 0.00 | 126.0 | PVC | 300 | 2.25 | 68.0 | 151.3 | 2.07 | 0.55 | 83.3% |
| ART (SW) | 427 | 429 | | | 0.06 | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 12.65 | 92.02 | 0.00 | 142.2 | PVC | 375 | 2.27 | 65.8 | 275.6 | 2.42 | 0.45 | 51.6% |
| ART (NW) | 431 | 429 | | | 0.27 | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 10.00 | 104.19 | 0.00 | 82.5 | PVC | 375 | 1.09 | 112.3 | 191.0 | 1.67 | 1.12 | 43.2% |
| ART | 429 | 529 | | | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 13.10 | 90.24 | 0.00 | 1455.2 | CONC | 1200 | 0.35 | 24.5 | 2406.2 | 2.06 | 0.20 | 60.5% |
| ART (SW) | 521 | 523 | | | 0.29 | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 10.00 | 104.19 | 0.00 | 88.6 | PVC | 300 | 1.00 | 109.5 | 100.9 | 1.38 | 1.32 | 87.8% |
| ART (SW) | 523 | 525 | | | 0.27 | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 11.32 | 97.70 | 0.00 | 166.0 | PVC | 375 | 2.00 | 80.2 | 258.7 | 2.27 | 0.59 | 64.2% |
| ART (SW) | 525 | 527 | | | 0.19 | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 11.91 | 95.09 | 0.00 | 218.9 | PVC | 375 | 2.20 | 61.7 | 271.3 | 2.38 | 0.43 | 80.7% |
| ART (SW) | 527 | 529 | | | 0.17 | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 12.34 | 93.26 | 0.00 | 265.5 | CONC | 450 | 2.20 | 60.8 | 441.2 | 2.69 | 0.38 | 60.2% |
| ART (NW) | 531 | 529 | | | 0.58 | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 10.00 | 104.19 | 0.00 | 177.2 | CONC | 450 | 1.20 | 109.9 | 325.8 | 1.98 | 0.92 | 54.4% |
| | 529 | 285 | | | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 13.30 | 89.49 | 0.00 | 1898.0 | CONC | 1200 | 0.35 | 76.4 | 2406.2 | 2.06 | 0.62 | 78.9% |

Q = 2.78 AIR

WHERE : Q = PEAK FLOW IN LITRES PER SECOND (L/s)

Q = (1/n) A R(2/3)So(1/2)

WHERE :

Q = CAPACITY (L/s)

A = AREA IN HECTARES (ha)

n = MANNING COEFFICIENT OF ROUGHNESS (0.013)

I = RAINFALL INTENSITY IN MILLIMETERS PER HOUR (mm/hr)

A = FLOW AREA (m2)

R = WEIGHTED RUNOFF COEFFICIENT

Project: Fernbank Crossing (108180-10)

Designed: SML

Checked: MJP

Date: May 7, 2014

Notes:

*From CRT Lands Storm Sewer Design Sheet

**A 10min Time of Concentration was used at the most upstream node, increasing the Time of Concentration by the Time of Flow between each pipe length to determine the Peak Flow.

**INFORMATION FROM FOUNDER
AVENUE (NORTH SOUTH ARTERIAL)
ROAD PROJECT PHASE 2
STORMWATER SERVICING BRIEF**


Founder Avenue (North South Arterial) - Storm Sewer Design Sheet - Ultimate Design (Fixed Inlet Time)

| LOCATION | | | AREA | | | | | | | | | | | | FLOW | | | | | | Total Peak Flow (Q) (L/s) | PROPOSED SEWER | | | | | | | | |
|--------------|-----------|----------|--|-----------------------------|-------------------|---------|-------|----------------|---------------------|--------------------|-----------------|----------------|-----------------|---------------------|--|----------|----------------|------------------------|------|----------------------|----------------------------|----------------|-----------|------------|----------------|--------------------------|--|-------------|-------|--|
| Location | From node | To node | Mixed Use | Park N' Ride | Arterial Road ROW | Schools | Parks | Hydro Corridor | Singles Front Yards | Singles Rear Yards | CRT Front Yards | CRT Rear Yards | Towns Rear Yard | Total Area (10 min) | Weighted Runoff Coefficient | 2.78 AR | Accum* 2.78 AR | Rain Intensity (mm/hr) | | Peak Flow (10 min)** | Pipe Type | Size (mm) | Grade (%) | Length (m) | Capacity (l/s) | Full Flow Velocity (m/s) | Time of Flow (min.) | Q/Qfull (%) | | |
| | | | | Paramedic Post Medium Block | ROW | | | | | | | | | (ha) | (10 min) | (10 min) | (10 min) | (L/s) | 5yr | 10yr | | | | | | | | | | |
| North Outlet | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| DRY POND | DI | STM PIPE | | | | | | | | | | | | | 0.80 | 0.80 | 0.90 | 0.60 | 0.40 | 0.20 | 0.65 | 0.55 | 0.75 | 0.80 | 0.60 | (ha) | (10 min) | (10 min) | (L/s) | |
| CRT/HYDRO | 180 | 429 | | | | | | | | | | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| ART (SW) | 421 | 423 | | | 0.20 | | | | | | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| ART (SW) | 423 | 425 | | | 0.12 | | | | | | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| ART (SW) | 425 | 427 | | | 0.11 | | | | | | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| ART (SW) | 427 | 429 | | | 0.06 | | | | | | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| ART (NW) | 431 | 429 | | | 0.27 | | | | | | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| ART | 429 | 529 | | | | | | | | | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| ART (SW) | 521 | 523 | | | 0.29 | | | | | | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| ART (SW) | 523 | 525 | | | 0.27 | | | | | | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| ART (SW) | 525 | 527 | | | 0.19 | | | | | | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| ART (SW) | 527 | 529 | | | 0.17 | | | | | | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| ART (NW) | 531 | 529 | | | 0.58 | | | | | | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| | 529 | 285 | | | | | | | | | | | | | | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| Q = 2.78 AIR | | | WHERE : Q = PEAK FLOW IN LITRES PER SECOND (L/s) | | | | | | | | | | | | Q = (1/n) A R(2/3)S _o (1/2) | | | | | | WHERE : Q = CAPACITY (L/s) | | | | | | Project: Fernbank Crossing (108180-10) | | | |
| | | | A = AREA IN HECTARES (ha) | | | | | | | | | | | | n = MANNING COEFFICIENT OF ROUGHNESS (0.013) | | | | | | Designed: SML | | | | | | Checked: MJP | | | |
| | | | I = RAINFALL INTENSITY IN MILLIMETERS PER HOUR (mm/hr) | | | | | | | | | | | | R = WEIGHTED RUNOFF COEFFICIENT | | | | | | Date: May 7, 2014 | | | | | | | | | |

Notes:

*From CRT Lands Storm Sewer Design Sheet

**A fixed 10min Time of Concentration has been used to determine the Peak Flow.

**INFORMATION FROM FOUNDER
AVENUE (NORTH SOUTH ARTERIAL)
ROAD PROJECT PHASE 2
STORMWATER SERVICING BRIEF**

