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Roger Stevens Warehouse 1966 Roger Stevens Drive, Ottawa

Servicing Options Statement & Conceptual Servicing Report

SERVICING OPTIONS STATEMENT & CONCEPTUAL SERVICING REPORT

ROGER STEVENS WAREHOUSE 1966 ROGER STEVENS DRIVE OTTAWA, ONTARIO

Prepared by:

NOVATECH Suite 200, 240 Michael Cowpland Drive Kanata, Ontario K2M 1P6

July 12, 2019

Novatech File No. 119018 Ref No. 2019-128



July 12, 2019

City of Ottawa Planning and Growth Management Department Infrastructure Approvals Division 110 Laurier Avenue West, 4th Floor Ottawa, Ontario K1P 1J1

Attention: Mr. Harry Alvey, P. Eng.

Dear Sir:

Re: 1966 Roger Stevens Drive, Ottawa Servicing Options Statement and Conceptual Servicing Report Our File No.: 119018

Enclosed is a 'Servicing Options Statement and Conceptual Servicing Report' for the proposed distribution centre located at 1966 Roger Stevens Drive, in the City of Ottawa. This report is submitted in support of Re-zoning and Official Plan Amendment applications. This report should be read in conjunction with the Conceptual Stormwater Management Report also prepared by Novatech.

Should you have any questions or require additional information, please contact the undersigned.

Yours truly,

NOVATECH

Cara Ruddle, P. Eng. Senior Project Manager | Land Development Engineering

cc: James Beach – Boundary Road Development Inc.

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1.0 INTRODUCTION

Novatech has been retained to prepare a Servicing Options Statement and Conceptual Servicing Report for the subject development. This report outlines the servicing options for the proposed development with respect to water, sanitary and storm drainage in accordance with the City Official Plan. Conceptual Servicing will also be discussed for the proposed development. This report is being submitted to satisfy the requirements for the application of Re-zoning and Official Plan Amendment. The subject site is located at 1966 Roger Stevens Drive at the intersection Roger Stevens Drive and Highway # 416. The legal description of the site is Part of Lot 21 and 22, Concession 2 (geographic Township of North Gower) now in the City of Ottawa. **Figure 1** is a Key Plan showing the site location.

2.0 EXISTING CONDITIONS

The subject property is located on the south side of Roger Stevens Drive and is bounded by Highway 416 to the east, rural residential and undeveloped forested lands to the south, residential rural estate lots to the west and Roger Stevens Drive and undeveloped/farm lands to the north. The site is approximately 2.5km to east of the Town of North Gower. Currently there is an existing residence and associated farm buildings on the property.

The parcel is approximately 49.4 hectares in size. The topography of the site is perched in the center where the existing farmhouse and barns were located and generally slopes away to the property lines. **Figure 2** is an existing conditions plan showing the current state of the site.

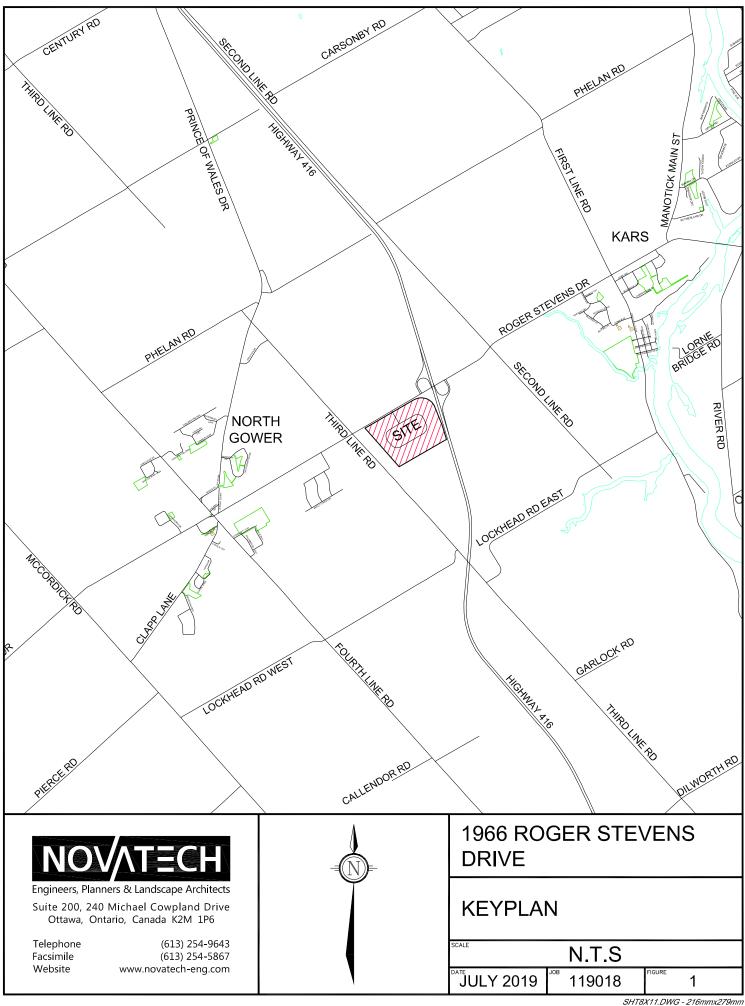
The original development concept for this property is known as the Jordel Acres Subdivision which included a row of single-family homes along Third Line Road South (some of which have been constructed). The remainder of the site was to be a commercial/industrial park. This Plan of Subdivision is registered but the Industrial Park portion of the site was not constructed. The Servicing Options Statement portion of this report will review the servicing options with supporting documentation provided as part of the previous development concept. The Conceptual Servicing portion of the report will review the servicing options and in relation to the previous development concept and what is allowable for the subject property.

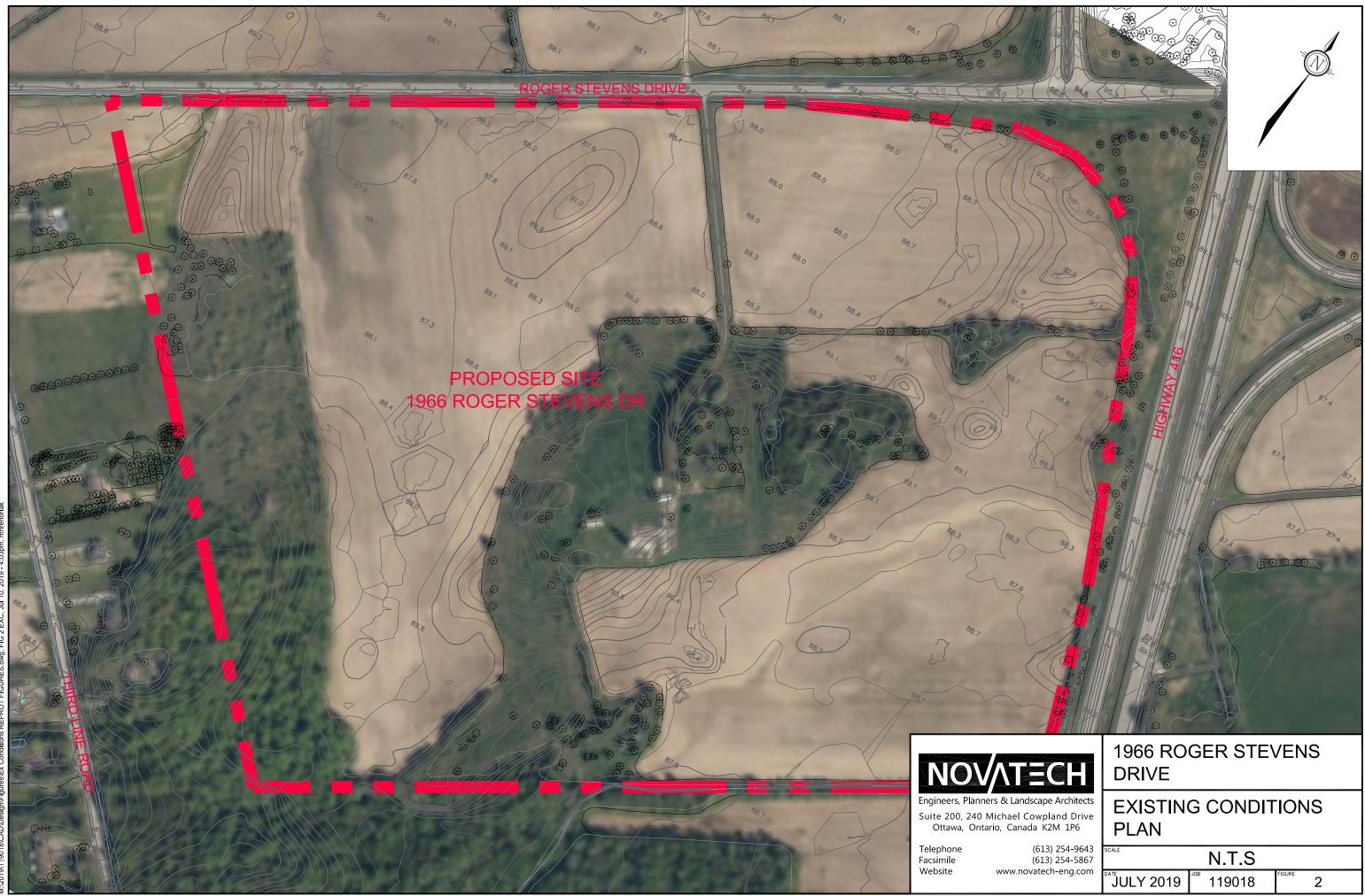
3.0 PROPOSED DEVELOPMENT

The proposed development consists of a single large distribution warehouse, distribution trucking parking lot, staff parking lot, and a stormwater management facility. The site will have two accesses from Rogers Stevens to the staff parking area. A third access from Roger Stevens is provided which will serve as the truck access. **Figure 3** is a proposed Conceptual Site Plan illustrating the proposed development. The original Registered Plan of Subdivision is provided for reference at the rear of the report in **Appendix A**.

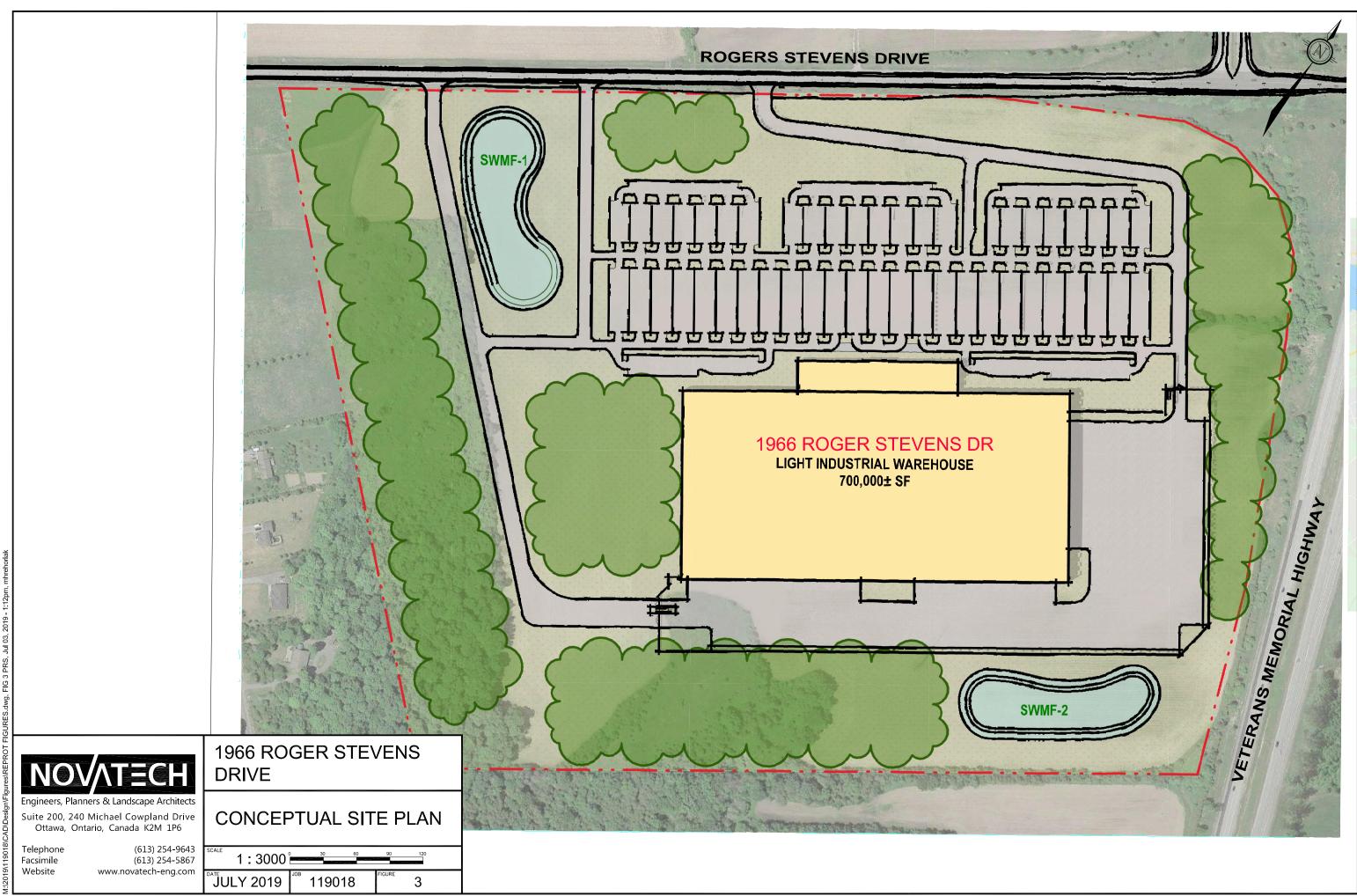
The business type proposed for development will be relatively "dry" (domestic use only) with respect to water and sewage generation. The uses will likely be transportation based fully utilizing the proximity of the site to the Highway # 416 transportation corridor.

It is proposed to service the development with private wells and a private sewage system. This report is written to provide support for this form of servicing for the development.





	N.T.S	
JULY 2019	^{JOB} 119018	FIGURE 2



4.0 EXISTING POLICY FRAMEWORK FOR SERVICING OPTIONS OR TERMS OF REFERENCE

4.1 PROVINCIAL POLICY STATEMENT

The Provincial Policy Statement (PPS, 2005) states that municipal sewage and water services are to be utilized where possible. Private communal sewage and water services can be utilized if a Municipality so chooses where municipal services are not available or where established policies exist to ensure the servicing satisfies criteria outlined in Section 1.6.4.1 of the PPS.

Communal water systems are shared facilities for the distribution of water to multiple residences. Communal sewage systems are shared facilities for the collection, treatment and disposal of sewage. These systems are not connected to a Municipal System. For communal development, the Municipality is responsible for ownership as per Section 52 and 53, Ontario Water Recourses Act, R.S.O. 1990, Part VIII, Environmental Protection Act, R.S.O. 1990.

Individual sewage and water services can be used in development of five units or less where municipal or private communal services are not available and where site conditions are suitable. Rural developments of greater than five units can also use individual sewage and water services where land use is in accordance with Section 1.1.4.1(a) and where site conditions are suitable for long term use of such services. (Refer to Sections 1.6.4.2 to 1.6.4.4 of the Provincial Policy Statement for more details.)

4.2 PROCEDURE D-5-3: SERVICING OPTIONS STATEMENT

A Servicing Options Statement is required for a development where the proposal is to use servicing other than existing municipal services. The Servicing Options Statement must review all possible servicing scenarios including municipal, communal and private servicing. MOE Procedure D-5-3 (March 1995) requires that the Servicing Options Statement should address the proximity of existing servicing and possible future connections to the existing municipal infrastructure, evaluation of each servicing option, and provide any documentation supporting the proposed servicing option for the development.

4.3 CITY OFFICIAL PLAN

Section 2.3.2 – Water and Wastewater Services, item 12 states that 'all development outside of *Public Service Areas will be based on private services.*' Since the subject property is well outside of the Urban Boundary it is not located within a Public Service Area and private servicing is required.

Section 4.4 of the Official Plan states that proponents of development must demonstrate that the servicing proposed for a development is adequate. Since the proposed development is to be serviced by private well and wastewater systems, the policy 4.4.2- Private Water and Wastewater Servicing applies. This policy states that '*Private individual services will mean a privately-owned and maintained well-water supply and a privately-owned and privately-maintained wastewater disposal systems that services the development on the lot upon which they are located and which will remain under one ownership.'*

Policy 1 (items a) to e)) of Section 4.4.2 of the Official Plan states that sufficient information is to be provided to ensure that adequate groundwater exists to service the development, that the groundwater meets the Ontario Drinking Water Standards, Objectives and Guidelines, and any

neighbouring wells will not be negatively impacted. It is also required to show that the wastewater system will not negatively impact the new well or the well on neighbouring properties.

5.0 ENVIRONMENTAL SUITABILITY AND EVALUATION

A Hydrogeological Study Report, Jordel Acres Proposed Subdivision, prepared by Sauriol Environmental Inc. (June 1999) has been completed for the subject site. The following information summarizes their findings.

5.1 SUITABILITY OF THE TERRAIN

5.1.1 TERRAIN

There is a high point that runs diagonally across the site that splits the site drainage. The eastern half of the site drains south easterly to a culvert under the Highway # 416 eventually outletting to Stevens Creek. The western half of the site drains north westerly to the Roger Stevens Drive road side ditch with outlets to a culvert under Roger Stevens Drive. This existing ditch system drains to Stevens Creek.

5.1.2 SOILS

Three (3) test wells were excavated as part of the terrain evaluation. The test wells concluded that there are three types of soils present on site. The ridge area consists of glacial till and the lower areas consist of a clay material with some parts overlain by a thin sand material. The bedrock is approximately 8 to 13 metres below grade.

5.1.3 GROUNDWATER SUPPLY

The Hydrogeology Report indicates there were two existing wells on the property which serviced the existing farm house and barn. Three additional test wells were drilled to assess the quality and quantity of groundwater of the bedrock aquifer. The water bearing zone was found between 15 and 32 metres below grade. Pump and recovery tests were completed on the three wells constructed. These tests concluded that the aquifer can supply adequate water for the domestic demands of the previously proposed industrial/commercial subdivision and that there were no adverse effects on neighbouring wells. It was concluded that the groundwater is good quality and it is recommended that the shallow bedrock zone be used as a source of groundwater since there is less mineralization (lower levels of chloride, sodium and conductivity). There are elevated levels of hardness and at time iron and these aesthetic parameters can be treated with water softeners.

5.1.4 SUITABILITY FOR SEPTIC SYSTEMS

Sixteen test pits were excavated to complete grain size analyses and percolation tests of the various soil materials to determine the suitability for septic systems to service the proposed industrial/commercial development. The existing clay material has low permeability and imported material will be required for the septic system. The existing neighbouring wells were reviewed for nitrate levels and confirmed that the existing bedrock aquifer is isolated from the existing wells. Therefore, the proposed development can be serviced by septic systems.

5.2 SUITABILITY OF DEVELOPMENT

5.2.1 MUNICIPAL SERVICES

Municipal Infrastructure exists within the Urban Boundary of the City of Ottawa with the exception of some villages such as Richmond, Munster and Manotick. The Official Plan (Section 5.6.1) states that servicing in rural areas or outside the urban boundary is provided with private servicing (wells and sewage systems). The closest municipal watermains are located 12 km away therefore, the option of servicing the subject property with Municipal Services is not a viable option.

5.2.2 COMMUNAL SERVICES

Communal services are the preferred means of servicing development in areas where full municipal sewage and water services are not or cannot be provided and where site conditions are suitable over the long term. Communal servicing is an option where there are five or more units to be serviced. Communal services are also typically used where there is a compact lot layout or higher density units. The cost of providing a water treatment plant, sewage treatment facility and the financial aspects of a responsibility agreement with the City of Ottawa make this option economically challenging. Communal servicing is not a viable option since multiple units are not being proposed in the development concept.

5.2.3 PRIVATE SERVICING

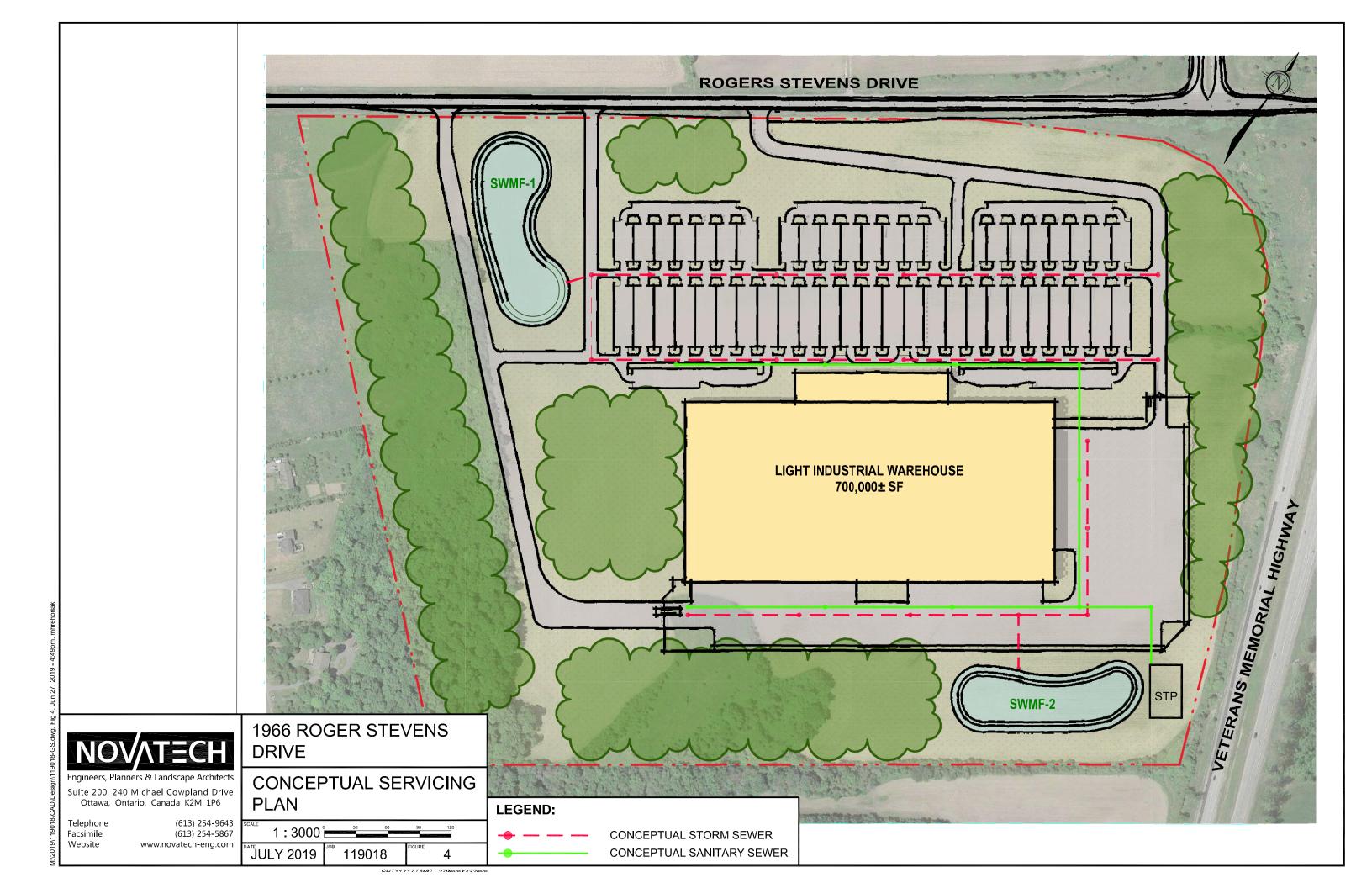
As indicated above the Official Plan states that private servicing is the preferred option for properties outside the Urban Boundary. The subject site is located outside the Urban Boundary and therefore, private servicing is the preferred option.

The Hydrogeological Study Report states that the on-site soils are suitable for septic systems and have made recommendations on the type and size of systems based on the previously proposed industrial/commercial concept. The design will be modified based on the current development proposal. The design flow of the sewage system be greater than 10,000L/day a Ministry of the Environment, Climate and Parks approval would be required.

The Hydrogeological Study Report also indicates that the existing bedrock aquifer can supply good quality groundwater and there is adequate quantity to service the existing Registered Plan of Subdivision. Additional Hydrogeological work will be required at the time of Site Plan to determine the impacts of the proposed development's water taking on the aquifer.

6.0 SITE SERVICING

A preliminary servicing design has been completed to provide a conceptual design and confirm that the proposed development is serviceable. This report will provide information on the preliminary water, sanitary and storm servicing of the proposed development. It is understood that the demands/flows from the proposed development may vary throughout a year period depending on the number of employees on site. Therefore, preliminary calculations are provided for the peak and off-peak seasons. Refer to **Figure 4** Conceptual Servicing Plan for servicing details.



6.1 WATER SERVICING

The proposed development will be serviced with private wells. The following calculations show the various water demands for the proposed development. Water demand is calculated based on employees, truck drivers delivering to and from the facility and internal hose bibs used for cleaning purposes.

Average Day Water Demand

The average day demand of the system is calculated as follows:

Approximate Number of Employees 2,200 employees (Off-Peak Season, January-November) Average demand per employee = 75 Litres/day

2200 x 75 = 165,000 Litres/day

Approximate Truck Traffic

There will also be a water demand related to the truck drivers accessing the facility. During the off-peak season (January- November) there will be approximately 150 trucks/day accessing the facility. Assuming that each driver utilizes the washroom facilities, the average day flows are calculated as follows:

150 x 8L/day = 1,200 Litres/day

Internal Hose Bibs

There will also be miscellaneous internal hose bib use throughout the day. Assuming that the hoses could run for 5 hrs. at a rate of 40 Litres/min., the average day flows are calculated as follows:

5 hrs. x 40Litres/minute = 12,000 Litres/day Average Day Summary Employee use + Truck driver use + internal hose bibs 165,000 Litres/day + 1,200 Litres/day + 12,000 Litres/day = 178,200 Litres / day

<u>Peak Season Demand</u> The average day demand of the system is calculated as follows:

Approximate Number of Employees 3500 employees (Peak Season, November-January) Average demand per employee = 75 Litres/day

3500 x 75 = 262,500 Litres/day

Approximate Truck Traffic

There will also be a water demand related to the truck drivers accessing the facility. During the peak season (November-January) there will be approximately 215 trucks accessing the facility. Assuming that each driver utilizes the washroom facilities, the peak season day flows are calculated as follows:

215 x 8L/day = 1,720 Litres/day

Internal Hose Bib

There will also be miscellaneous internal hose bib use throughout the day. Assuming that the hoses could run for 5 hrs. at a rate of 40 Litres/min., the peak season flows are calculated as follows:

5 hrs. x 40Litres/minute = 12,000 Litres/day

Peak Season (Maximum Day) Summary Employee use + Truck driver use + internal hose bibs 262,500 Litres/day + 1,720 Litres/day + 12,000 Litres/day = 276,220 Litres / day

The peak instantaneous water demand of the facility will be met by the internal water system. The internal water system will consist of storage tanks and a jet pump system to maintain the internal operating pressures.

The wells will be required to meet the peak season average day demand of 276,220 L/day (50USGPM).

Fire Suppression

Fire suppression water will be provided by way of above grade storage tanks. The tanks will supply the proposed pumphouse with fire suppression water. The pumphouse will supply the required demand to the sprinkler system and on-site hydrants. The fire suppression system will be a private system, owned and maintained by the property owner. A fire suppression consultant will be part of the design team for the Site Plan stage of the project.

6.2 SANITARY SERVICING

The proposed development site is not within the City of Ottawa sanitary service area. An on-site, private sewage collection and treatment facility is proposed with surface discharge of the treated effluent to the existing municipal drain and culvert that runs under Highway 417 and drains to Stevens Creek.

Sewage Collection

Similar to the water section of the report, the average sanitary flows are calculated for the offpeak season and the maximum sanitary flows are calculated for the peak season as follows:

3500 employees (Peak Season, November-January) Average flow per employee = 75 Litres/day

3500 x 75 = 262,500 Litres/day

There will also be a sanitary flow related to the truck drivers accessing the facility. During the peak season (November-January) there will be approximately 215 trucks accessing the facility. Assuming that each driver utilizes the washroom facilities, the peak season day flows are calculated as follows:

215 x 8L/day = 1,720 Litres/day

There will also be miscellaneous internal hose bib use throughout the day. Assuming that the hoses could run for 5 hrs. at a rate of 40 Litres/min., the peak season flows are calculated as follows:

5 hrs. x 40Litres/minute = 12,000 Litres/day

Peak Season (Maximum Day) Summary

Employee use + Truck driver use + internal hose bibs 262,500 Litres/day + 1,720 Litres/day + 12,000 Litres/day = 276,220 Litres / day = 3.2 Litres/second

The anticipated extraneous flows are calculated from the equation found in Appendix A-2 of the MOE Guidelines for design of Sanitary Sewer and as is follows:

2.03L/mm Ø / 100m/hr (2.03 x 250) x (1100 / 100) = 5,582.5 Litres/hour = 1.55 Litres/second

The resultant peak sanitary sewage flow to the collection system is as follows:

(Avg. Flow x Peak factor (1.5)) +Extraneous Flows

= (3.20 L/s x 1.5) + 1.55 L/s

= 6.35 L/s

The collection system consists of a series of pipes designed to convey the peak flow. The collection system pipe size is 250 mm and will be installed at a slope of 0.24%. The proposed sanitary sewage collection system will be capable of conveying 30.4 L/sec.

Sewage Treatment Plant

A private sewage treatment plant will be proposed for the treatment of domestic waste from the proposed distribution centre. Based on the Ministry's dry ditch discharge requirements, the system will be designed based on the following discharge parameters (characteristics):

Wastewater Characteristics		
Parameter	Unit	Design Value
Biochemical Oxygen Demand (BOD5) 1	mg/L	350
Total Suspended Solids (TSS) 1	mg/L	350
Total Kjeldahl Nitrogen (TKN) 1	mg/L	70
Total Phosphorus (TP) 1	mg/L	10
Fat, Oil and Grease (FOG) 1	mg/L	<30
рН 1	-	6 to 9
Water Temperature 1	°C	10 to 25
Alkalinity 1	mg/L as CaCO3	520

The treatment plant will be capable of treating raw sewage to "Dry Ditch" discharge requirements as per MOECC guidelines. The discharge effluent criteria is as follows:

Effluent Quality Parameter Biochemical Oxygen	Units mg/L	Regulatory Limit < 10	Design Value < 5
Demand (BOD5) Total Suspended Solids (TSS)	mg/L	< 10	< 1
Ammonia nitrogen (NH3- N)	mg/L	< 3	< 0.5
Total Phosphorus (TP) E. coli	mg/L MPN/100mL	< 0.15 < 200	< 0.05 < 2.2

The discharge location of the final effluent will be to the Johnston Municipal Drain located at the southeast corner of the property.

A pre-consultation meeting will be held with the MECP and the Conservation Authority prior to Site Application to confirm the design parameters above.

6.3 STORM SERVICING

There is a high point that runs diagonally across the site that splits the site drainage. The eastern half of the site drains south easterly to a culvert under the Highway # 416 eventually outletting to Stevens Creek. The western half of the site drains north westerly to the Roger Stevens Drive road side ditch with outlets to a culvert under Roger Stevens Drive. This existing ditch system drains to Stevens Creek.

The proposed development will be serviced by a combination of storm sewers, ditches and two wet ponds designed for quantity and quality control. The front paved parking areas will be serviced with catchbasins and storm sewers that outlet to a stormwater management pond in the northwest corner of the site. This pond will outlet to the Dillon-Wallace Municipal Drain. The location of this proposed pond is within an existing flood plain area and will require cut/fill permit from the Conservation Authority. The remaining proposed landscape areas will sheet drain to ditches.

The rear portion of the site will drain to a second stormwater management pond in the southeast corner of the site. This pond will outlet to the Johnston Municipal Drain. A Conceptual Servicing Plan is provided at the rear of this report for reference.

Refer to the Conceptual Stormwater Management Report prepared by Novatech for further information on the conceptual stormwater management design.

8.0 SUMMARY AND CONCLUSIONS

This report has been prepared in support of zoning by-law amendment and official plan amendment for the proposed distribution warehouse at 1966 Roger Stevens Drive, in the City of Ottawa.

The conclusions are as follows:

• The proposed development site will be serviced with private wells.

- The proposed building will be sprinklered. Water supply for fire suppression will be provided by way of storage tanks. The storage tanks will supply fire suppression water to the proposed pump house which will supply water to the sprinkler system and on-site hydrants.
- The proposed development will be serviced by private sewage collection system and treatment facility that will surface discharge the treated effluent to the Johnston Municipal Drain.
- The stormwater quality and quantity control will be provided in two proposed Stormwater management ponds.

NOVATECH

Prepared by:

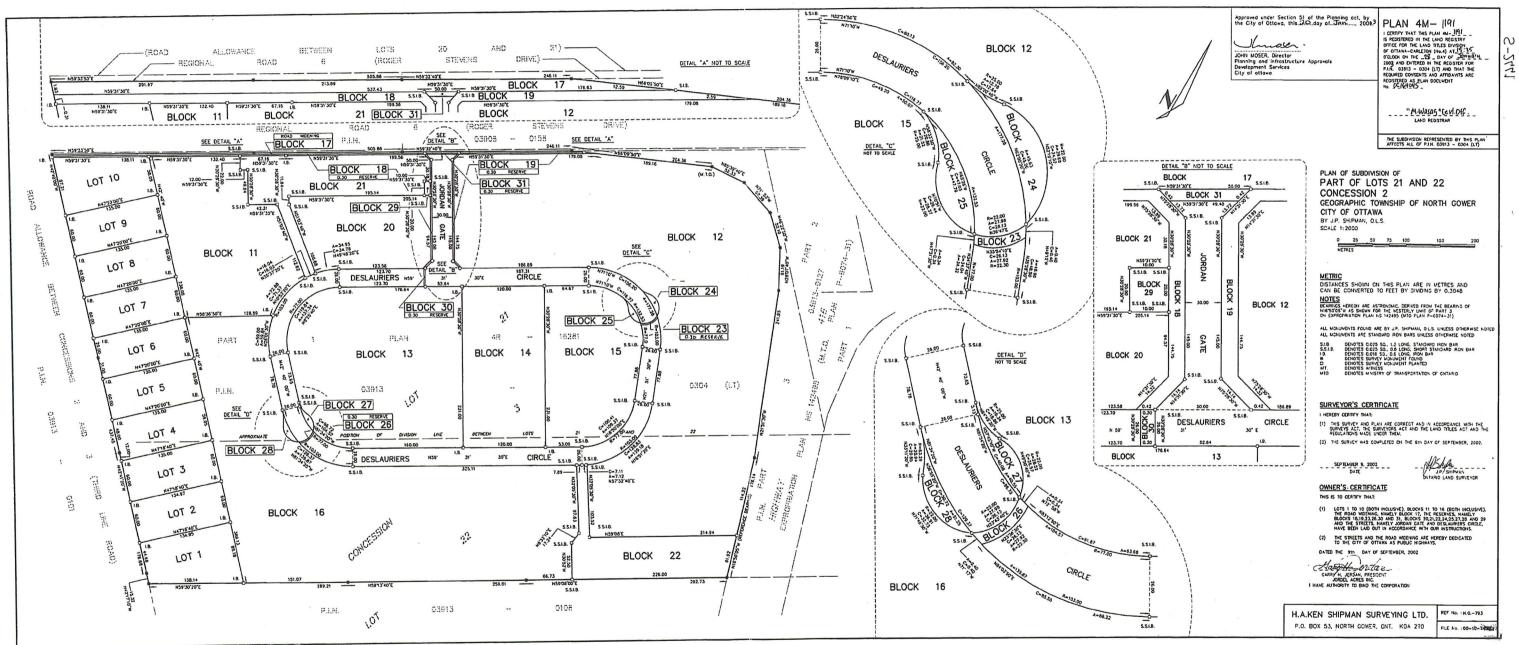


Cara Ruddle, P. Eng. Senior Project Manager Land Development Engineering

Reviewed by:

J. Lee Sheets, C.E.T. Director Land Development & Public Sector Engineering

APPENDIX A Plan 4M-1191



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APPENDIX B Existing Jordel Acres Hydrogeological Study Report

HYDROGEOLOGICAL STUDY REPORT

JORDEL ACRES PROPOSED SUBDIVISION

Report prepared for Pri-Tec Construction Prepared by Sauriol Environmental Inc Our file 9908 Dated: June 1999



SAURIOL ENVIRONMENTAL Inc.

SAURIOL ENVIRONNEMENT CONTAMINANT HYDROGEOLOGY ENVIRONMENTAL STUDIES WATER SUPPLY HYDROGEOLOGY

HYDROGÉOLOGIE DES POLLUANTS ETUDES D'IMPACT HYDROGÉOLOGIE DE L'APPROVISIONNEMENT EN EAU

June 28, 1999

Pri-Tec Construction Ltd P.O. Box 13501 Pri-Tec Industrial Park RR#5 Carp Road Kanata, ON K2K 1X6

Attention: Mr. Richard Lalande President

Re: Hydrogeological Study Report Jordel Acres Proposed Subdivision Lot 21 Concession II Rideau Township Highway 416 and Roger Stevens Drive Our file 9908

Dear Richard:

Please find enclosed five copies of the Hydrogeological Report completed for the Jordel Acres Proposed Subdivision. It includes a review of the groundwater supply availability and quality, a terrain suitability for septic system, and an Environmental Site Assessment Phase One.

Trusting the its contents is to your satisfaction. We were pleased to be of service to Pri-Tec Construction.

Yours Truly

Sauriol Environmental Inc

Jacques Sauriol M. Sc. President

encl.

Hydrogeological Study Report Jordel Acres Proposed Subdivision

1.0 INTRODUCTION

Sauriol Environmental Inc was retained by Pri-Tec Construction, to undertake a Hydrogeological Investigation and a Phase One Environmental Site Assessment for the Jordel Acres proposed subdivision, located on part of Lot 21 Concession II Township of Rideau. The site is located at the South West corner of the intersection of Roger Stevens Drive and Highway 416, as shown on Figure 1. The property has approximately 55 Ha in surface area, and the conceptual plan proposes 41 lots, varying between 0.81 Ha for Residential portion, to 1.0 Ha for the Industrial portion and 1.5 Ha for the Commercial portion.

1.1 Objectives:

The scope of the study is to demonstrate the suitability of the Jordel Acres Property for a proposed Industrial, Commercial and Residential Development based on private services of wells and septic systems. The five main study objectives are as follows:

Assessment of the groundwater supply availability

Assessment of the Groundwater Quality

Assessment of the Terrain Suitability for Septic System

Assessment of any Environmental Liability attached to the Site

Provision of an overall opinion as to the suitability of the proposed Jordel Acres Subdivision.

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1.2 Methodology:

Three Guidelines were used to prepared the present report. These include:

MOE March 1995 Technical Guidelines for Private Wells: Water Supply Assessment MOE March 1995 Technical Guidelines for Individual On-Site Sewage Systems: Water Quality Impact Assessment

CSA Standard Z768-94 dated April 1994

A detailed review of the existing geologic and hydrogeological information of the property was undertaken using published geological maps, water well records and previous regional hydrogeological assessments. Nearby residents were interviewed on the availability and quality of their well water supply. Two nearby private wells were sampled to characterize local groundwater quality. A total of three test wells, in order to assess the aquifer yields. Hydraulic interferences were monitored during these tests. Well water samples were collected, and analytical work was completed to determine the potability of the supply. A backhoe test pit program was completed to assess the terrain suitability for septic system. A total of 16 test pits were excavated, and examined for lithology, stratigraphy, and depth to water table. Grain size analyses were completed on soil samples collected from the test pits.

2.0 GEOLOGIC SETTING

The study property is located in the "North Gower Drumlin Field" Physiographic Region (Chapman & Putman 1984). Drumlins are elongated hills formed at the bottom of the continental Icesheets. Two such Drumlins are located on the property. The long axis of these depositional features are aligned mainly North-South across the property. Regionally, these low hills are formed of glacial tills, are well drained and create undulating topography. The low-lying areas between topographic highs, are composed of marine clays, overlain in places by thin sands. Regionally, these low areas are levelled and dry, with a high water table (Ringrose Roed & Sauriol 1990). The property is drained by the Stevens Creek located to the North of the property, and which flows to the Rideau River.

2.1 Surficial Geology

The Surficial Geology information was taken from Richard's work at the GSC, backhoe test pit stratigraphy, as well as the stratigraphy of the test well on the property. A total of three Surficial Geology Units occurs on the property, namely a Glacial Till Unit, overlain by Offshore Marine Clay Unit (Champlain Sea deposit), overlain in place by a relatively thin Sand Unit. The sand is believed to be "marine re-workings" of the Drumlins, acting as high bars on the former sea floor. The Sand Unit is present as an offshore deposit overlying the clay on the eastern portion of the property. A relatively minor sub unit consists of a "near shore" well-sorted sand and gravel linear beach deposit on the top of the Drumlins.

A review of the aggregate potential by Gorrell Resources Investigation (1992) indicates a low priority for aggregate, with local fill use only, for the linear beach deposit on drumlin tops. No other aggregate potential resource has been identified on the property.

The Site Plan of Figure 2 and the Profile of Figure 3 illustrate the spatial distribution and the stratigraphy of the unconsolidated deposits on the study property.

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2.2 Bedrock Geology

Bedrock Geology is based on OGS mapping (Williams and others), on the stratigraphy of the three test wells on the property, as well as on the nearby water well records. The 8 to 13 metres thick unconsolidated materials of the site are underlain by the limestone and dolomite of the Oxford Formation. This bedrock formation does not outcrop on the ground surface on the property. The bedrock surface is flat-lying at about 83 metres above sea level, and no noticeable bedrock surface sloping trend was noted.

2.3 Regional Hydrogeology

Based on the potentiometric elevations of the site test wells, a low hydraulic gradient was computed at 0.00089 towards the East. Regional bedrock aquifer groundwater flow appears eastward, as is the drainage of Stevens Creek to the Rideau River. Potentiometric elevation on the clay flats were recorded at about 1.8 m below the ground surface. There was concurrence between most water table encounters in the test pits and test well hydrostatic pressures (May 1999). Shallow water table groundwater flow is perceived to follow the local surface topography, hence draining from high till terrain to low clay grounds.

A review of the nearby MOE water well records indicates that the bedrock aquifer is more commonly used as a source of water supply. Regionally, the carbonate rich rock of the Oxford Formation are known to be a good and reliable groundwater aquifer. A survey completed for a nearby subdivision to the West (Kennedy Subdivision) indicates that wells normally encounter water bearing zones between 18 and 42 m., and yield between 45 and 90 Lpm (Geo-analysis 1988).

The Private Individual Servicing Study of the Region (Sauriol & Hanna 1992) classified the study area as having the best regional potential for groundwater quality, as having the area with greatest overburden thickness (mainly composed of fine grained soils), as having a high terrain suitability for septic systems, and as having a high regional development potential based on private services, compared to other area of the RMOC.

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A review of the property's groundwater supply indicates the presence of three older wells. Two of the wells were dug wells and one other well was a drilled well. These older wells are located on the Site Plan of Figure 2.

Dug Well No 1 is located to the south of the farm house, and is constructed with 1.2 m diameter cement tiles. Well sounding indicates that this well is 3.66 m in depth, and there is no cover to the well. Surrounding area is wet and cattle uses the area around the well for grazing.

Dug Well No 2 is a very old well constructed of stones picked from fields. The wooded cover has caved in. There was a very rusty steel hand pump that was non operational. Well sounding indicates that this well is 4.57 m in depth. The well is overgrown with weeds.

The old drilled well is located inside the barn, and likely corresponds to the previous owners (Dillon's) water well record provided in Appendix B. The well produced sufficient water to supply the farm house and 30 heads of cattle. The well is located very closed to a manure pile inside the barn. Recent bacteria testing by the owner indicated acceptable drinking water (personal communication Mr. Jordan).

3.0 GROUNDWATER SUPPLY

The groundwater supply of the proposed Jordel Acres Subdivision was assessed by investigating the groundwater quantity and groundwater quality of the underlying bedrock aquifer.

3.1 Groundwater Quantity

A drilling program was undertaken on the week of May 17 1999. Three test wells were drilled and pressured grouted by Bourgeois Well Drilling. These wells are located on the Site Plan of Figure 2, as TW1, TW2, and TW3. The following sections deals with well specifications, compliance, and hydraulic testing of the three test wells.

3.1.1 Specifications

Well construction specifications are provided in Appendix A. It also includes a Well Certification Statement of the three test wells, for the Regional Municipality of Ottawa Carleton (RMOC). A proposed Well Certification Clause should be inserted in the Subdivision Agreement, to ensure future well construction compliance for each lot created in the Plan of Subdivision, including casing grouting. The final wordings should be in agreement with the Region. Proposed wording is included in Appendix A. The water demand per lot was determined as per MOE Guideline as follows: 4 persons per house * 3.75 Lpm/person = 15 Lpm peak demand, which is in excess of 13.7 Lpm minimum requirements.

3.1.2 Construction

The three test wells were completed in the dolomite of the Oxford Formation. Details on the well characteristics are outlined in Table 1. The thickness of the unconsolidated materials ranges between 7 and 11 metres, water bearing zones were encountered between 15 and 32 metres, and total well depth ranged between 24 and 37 metres. Copies of the water well records of the three test wells are located in Appendix B. Of the three old wells found on the property, the old drilled well record was found in the MOE water well records. It indicates a well formally owned by Mr. Dillon, drilled in 1961 with 12.5 m of overburden and a well depth of 24.7 m. This well has a fairly high water yield with 68 Lpm for 1 hour with 0.6 m of drawdown. A copy of this record is also provided in Appendix B.

3.1.3 Pumping Test Analysis

A series of three pumping tests and three recovery tests were completed on the three test wells constructed on the property. The pumping tests were completed at a rate of 16 Lpm, near the expected water demand from the proposed subdivision. Very little drawdown was observed in the wells when stressed at that pumping rate. Recorded drawdown ranged from 0.02 to 0.16 m at the end of 6 hours of constant discharge. The driller's estimate of the capacity of the wells ranged from 160 to 180 Lpm. Hydraulic test information is provided in Appendix C. Transmissivity values from the TW1 was estimated at 280 m2/day (Table 2). In addition, distance-drawdown relationship was established between the two contiguous lot wells TW1 and TW2 (Figure 4). It shows that an observation well located 60 metres away from a well pumping at 16 Lpm would experience an interference of only 4 cm after 6 hours of pumping. One hundred percent recovery was recorded after a very short period, ranging from 1 to 30 minutes.

The pumping test results indicate that the Oxford Formation Aquifer can supply the domestic, dry-commercial and dry-industrial needs of this proposed subdivision. Yields of in excess of 16 Lpm are available from this aquifer. The induced drawdown generated from neighbouring wells will not have a detrimental effect on well water availability.

The effect of open-loop groundwater source heat pumps have not been evaluated as part of this study. These systems should not be approved as part of the development unless further specific testing be implemented.

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3.1.4 Recommended Well Construction

Future wells on the property should be completed in a manner similar to the construction of the three test wells. Specifications are enclosed in Appendix A. These include the drilling with mud and the pressure grouting from the bottom upward through the casing into the well annulus. The total anticipated well depth should range between 24 and 37 metres below ground surface. It is further recommended that the three old wells located on the property (See Site Plan of Figure 2) should be abandoned as per MOE Guidelines, and that these works be a condition of Approval for the Subdivision. This recommendation is required to shut off any possible surface contaminant migration pathways along non-sealed well casings.

3.2 Groundwater Quality

Two nearby residences were sampled to document the quality of the surrounding aquifer. The three pumping wells were sampled at the beginning and the end of their hydraulic tests, for quality characterization. Field measurements of turbidity were also taken by SEI's staff. Analytical results from Accutest Laboratory are provided in Appendix D. This Appendix also includes the water quality results of the old drilled well taken by the owner in 1997. All sampled wells are located on the Site Plan.

3.2.1 Nearby Residences

The two sampled nearby residences are located to the immediate West of the study property (Gillis and Smith). A Point Of Entry water treatment system could not be by-passed for the sampling of the Gillis House. The surveyed residents (daughters) indicated that they were satisfied with their well water quality. The Smith's water quality result is indicative of the raw groundwater. The raw well water is typical of the Eastern Ontario carbonate rich bedrock aquifers, with elevated water Hardness (361 mg/L). The measured groundwater parameters meet the Ontario Drinking Water Objective (ODWO) for all parameters, except for Iron at 1.77 mg/L. The Gillis water sample is indicative of treated water (softener), and demonstrate the treatability of such a conventional unit. Indeed, the calcium and magnesium (Hardness) and the Iron, were reduced to below detection limits in the well water treated with the ionic exchanger.

3.2.2 Test Well Groundwater Quality

All three Test Wells on the property have very good groundwater quality. Similar to the neighbouring wells, the well water has elevated mineralization, with Total Dissolved Solids (TDS) at about 450 mg/L, and Hardness at about 250 to 300 mg/L. Iron results vary from as low as 0.04 to as high as 0.54 mg/L, exceeding at times the 0.3 mg/L ODWO criteria. Computed Organic Nitrogen is low, and no Hydrogen Sulphide was detected. Sodium concentrations are low, but still warrant a notice the Officer of Health for low sodium diet persons. Based on Chloride, Sodium and Conductivity as overall mineralization, the water of TW3 has less concentrations, suggesting that shallower water bearing zones is producing less mineralized groundwater (20m versus 26m and 32m. for TW3, TW2 and TW1 respectively). It is recommended that where possible, the shallow bedrock water bearing zone be utilized as a source of groundwater, because of less mineralization. Methane gas was field-measured with a Gastech Unit at the head of the three test wells, and no methane was detected above the detection limit of 1 ppm.

The old drilled well sampled by the owner in 1997 produced equivalent quality groundwater, with less Hardness, higher Chloride, Sodium and TDS (Appendix D). It is noted that the old well produced elevated Turbidity that could have been caused by Iron precipitation in the sample jar in 1997.

Between 8 and 13 hours of well development was required before producing acceptable turbidity water. Table 3 lists the field turbidity readings completed with a portable turbidity unit. The chart of Figure 5 plots the turbidity values against time. All last field turbidity readings were below the 1.0 NTU.

Nearby landuses consists mainly of agricultural activities and rural development. The new Highway 416 is contiguous to the East of the property. No land use conflicts have been noted.

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4.0 TERRAIN SUITABILITY FOR SEPTIC SYSTEM

The terrain suitability for the attenuation of septic system effluent was determined by a backhoe test pit program, grain size analyses, percolation tests, and the delineation of terrain unit. A total of 16 backhoe test pits were constructed to 1.8 metres in depth over the property. These pits are located on the Site Plan of Figure 2. The stratigraphy of the test pits are compiled in Appendix E. Two grain size analyses were completed, one to characterize the clay and the other for the sand. Based on upper soil stratigraphy, a total of four Terrain Units were delineated. Two percolation tests were completed, with a bias towards fine grained soils (Appendix E).

4.1 Terrain Suitability

Four Terrain Units were identified on the property, namely a Till Terrain Unit, a Clay Terrain Unit, a Sand-Over-Clay Terrain Unit and a Sand Terrain Unit. Their spatial distribution are provided in Figure 2. Their vertical distributions are provided in the Profile of Figure 3.

4.1.1 Terrain Units

The Till Terrain Unit covers about one third of the property's surface area, and consists of low elongated topographic ridges. Thickness of this unit is estimated to average 11 metres, based on the test well stratigraphy. The till is made of a silty clay matrix with cobbles and boulders. The water table was below 1.8 m in depth in all test pits completed in the till (May 1999). A percolation test was completed on the upper crust of this terrain unit, and yielded a perc rate equal to 7.5 minutes per cm (Perc test No 2; equivalent to K=10-3 cm/sec).

The Marine Clay Terrain Unit covers about one third of the property's surface area, and is located on the topographic flats on the western and central portions of the study area. This unit has a thickness that varies between 2.1 to 2.7 m, based on the stratigraphy of the test wells. A grain size analysis of the upper crust of this material was completed (Appendix E; soil No 2), and was described as clayey silt with minor sand. The water table was ranging between 0.91 and 1.68 m in depth with an average of 1.45 m (May 1999). It is characterized by a low permeability, with a percolation rate of 20 minutes per cm (equivalent to K= 10-5 cm/sec).

The two remaining terrain units are the Sand-Over-Clay Terrain Unit and Sand Terrain Unit. They cover the eastern third of the study property. The Sand Terrain Unit has a thickness in excess of 1.8 m. The thickness of the sand, for the Sand-Over-Clay Terrain Unit, ranges between 0.75 and 0.90 m. A grain size analysis of the sand was completed on a soil samples taken from TP13, and was described as a silty fine sand with some medium sand (Appendix E; Soil No 1). The water table of the Sand Unit is below 1.8 m. The water table of the Sand Over Clay Unit was recorded at 1.52 m (May 1999). The assumed permeability of the sand is high, ranging between 2 to 10 min/cm (equivalent to K=10-3 to 10-2 cm/sec).

4.2 Three Step Assessment Process

The three step assessment process of the MOE Guidelines was reviewed for the Jordel Acres Proposed Subdivision. Step One refers to Lot Size consideration. The development is proposing a series of residential, industrial and commercial lots ranging from 0.81 Ha, 1.0 Ha and 1.5 Ha respectively (Municipal By-Law). The 55 Ha property is to be subdivided into a total of 41 lots, hence an average of 1.34 Ha per lot with no one lot less than 0.8 Ha in surface area. The Ministry believes that one hectare lots will be sufficiently large to reduce the nitrate impact from septic system to an acceptable concentrations in groundwater below the adjacent properties.

The Step Two of the assessment process refers to system isolation considerations. The "main-septic-system-receiving-hydrogeological-unit" is the upper clay or till. The thickness of these fine grained low permeability units are ranging between 7 and 11 metres based on the test well stratigraphy. The upper sand is disregarded for the isolation argument, since it is assumed to be underlain by clay or till. As a mean to measure the overall effectiveness of the isolation between the septic system loading area to the bedrock aquifer, the nitrate concentration of the existing neighbouring wells were reviewed. The Gillis' well had less than 0.1 mg/L NO3, while the Smith's well had 0.14 mg/L NO3. Both results are indicative of no septic system impact onto the bedrock aquifer.

4.3 Septic System Design

Class 4 Sewage System with absorption trenches was assumed for the design requirements. Based on the Ontario Building Code, septic effluent was estimated at 1600 Lpd. When compared with design water demand requirement, we arrived at the following: 450 Lpd/person requirement * 4 persons per home = 1800 Lpd/dwelling. Because the available aquifer is capable of much more yield, we have assumed 3000 Lpd/dwelling. Using the 6 L/m2 daily loading rate of the Building Code, the leaching bed should have 500 m2 in surface area. The sewage envelop is to be estimated with a design of 3Lpm2, (telecon Mezmure Haile Meskale, RVCA), equivalent to 1,000 square metres, including the primary bed and the spare area. It is recommended to dedicate an area of 1,250 m2 per new lot, for the sewage disposal system, and this area should take care of most mantle requirements (15 m in the direction of flow). This area requirement is equivalent to 15 percent of the smallest proposed (residential) lot size of 0.81 Ha. The leaching bed over the Clay Terrain Unit could be constructed over adequate imported soils, to offset the low hydraulic conductivity (K) of the native soils.

Hence, the bedrock aquifer is well isolated from the main septic system receiving hydrogeological unit, and proposed lots are large. Residential, commercial or industrial proponents with design sewage flow rates exceeding 3.0 m3/day should complete a specific predictive assessment of the waste water system.

Any loading in excess of 3,000 litres per day should have its septic system design review for actual sizing requirements. Any system with design flow rate in excess of 10 m3/day will require an engineered septic system design, and a groundwater impact assessment as per MOE Guideline B-7(the Reasonable Use Guideline).

5.0 ENVIRONMENTAL SITE ASSESSMENT

An Environmental Site Assessment (ESA) Phase One was completed for the study property. The ESA Report is included in Appendix F of this document.

The potential environmental concerns for the property may include: 1 underground storage tank (UST), with suspected contaminant soils 1 above ground storage tank evidence of oil spills in the garage floor minor asbestos containing materials in some floor or ceiling tiles, and minor PCB containing ballasts in fluorescent light fixtures

Recommendations include the removal of the UST and the completion of a Phase Two ESA near the two diesel tanks and in the garage floor

6.0 CONCLUSIONS

Three test wells and three pumping tests demonstrated that the Oxford bedrock aquifer below the property can supply a good quality groundwater at a rate in excess of the requirements for the intended use. Yields of in excess of 16 Lpm are representative of the yields which are likely to be obtained from wells, in the long term. Water quality is expected to be elevated in water Hardness and at times Iron. This report has shown that a water softener as a Point-Of-Entry treatment unit can treat these aesthetic parameters very effectively. Low sodium diet purchasers should be informed of the sodium concentrations of 30 to 70 mg/L. Low sodium diet individuals may wish to include a separate tap which by-passes the softener, in order to supply unsoftened drinking water. New wells will likely require about 10 hours of development before generating turbidity level below 1.0 NTU. Well certification will be required for each new well, to ensure that the wells are built as per Regulation 903 of the Ontario Water Resources Act, and that proper well grouting is completed. This well certification will demand an on-site inspection during the well construction. Old drilled and dug wells on the property should be abandoned as a condition of Draft Approval. Pumps should be of submersible type with pitless adaptor connection, and adequate crowning at the well head to promote runoff away from the well.

The four terrain units identified on the property have acceptable suitability for the construction of individual septic system. Minimum lot sizes, called for by the Municipal By-Law, are ranging between 0.8, 1.0 and 1.5 Ha for residential, industrial and commercial landuses respectively, and are perceived acceptable for the attenuation of leaching bed effluent. An area of 1,250 m2 should be reserved on each new lot for the leaching bed, its spare area and its mantle. The area of the proposed leaching bed including spare area, should be identified on each lot and fenced off to avoid any compaction during construction, particular over the Clay Terrain Unit. Excavation should avoid the creation of smearing, particularly in the clay soils. In the Till Terrain Unit, any large cobbles and boulders should be removed from the trench area. Each lot septic system should be located downslope to its well in order to maximize the separation distance to this contaminant point source. Septic system should be as per Ontario Building Code Specifications.

Trusting that this report is satisfactory.

Yours Truly

Sauriol Environmental Inc.

Jacques Sauriol M. Sc. President

TABLE 1: TEST WELL CHARACTERISTICS								
	TW1	TW2	TW3					
Ground elevation (masl)	. 89	88.8	94					
Static Level (mbtc)	1.85	1.82	7.2					
Potentiometric Elevation (approx. masl)	87.15	86.98	86.8					
Overburden Thickness (m)	7.3	7.3	11					
Depth to Water Bearing Zones (mbgs)	15; 32	26	20					
Well Depth (mbgs)	37	32	24					
Estimated Well Yield (Lpm)	160	180	180					

masl = meters above sea level mbgs = metres below ground surface mbtc = metres below top of casing Lpm = litres per minute

Table 2: Transmissivities TW1							
Method	transmissivity (m2/day)						
Theis	280						
Jacob	280						
Papadopulos	277						
Hantush	286						

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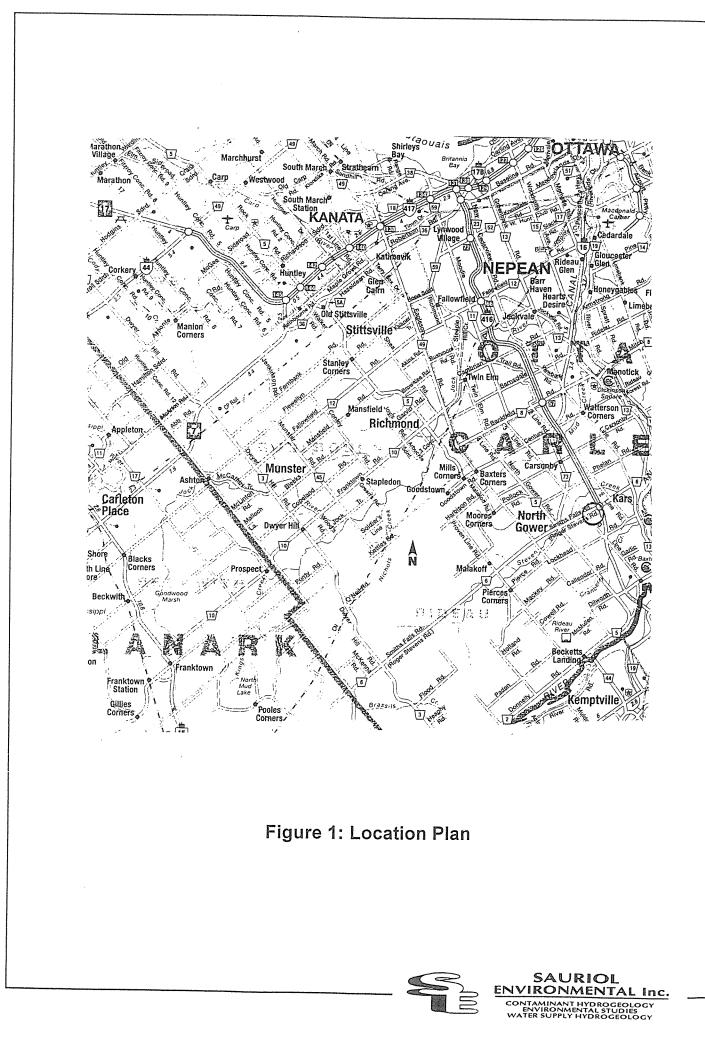
Table 3: Field Turbidity Readings									
Pumping test	Turbio	Turbidity readings (NTU)							
Time (min)	TW1	TW2	TW3						
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2									
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20		1							
25	3.55								
30									
40									
50									
60	1.95	4.62	8.00						
120		2.30							
180	1.80	1.00	5.70						
240	1.60	0.95	3.30						
300	1.20	0.71	1.92						
360	0.94	0.68	1.10						
480			0.93						

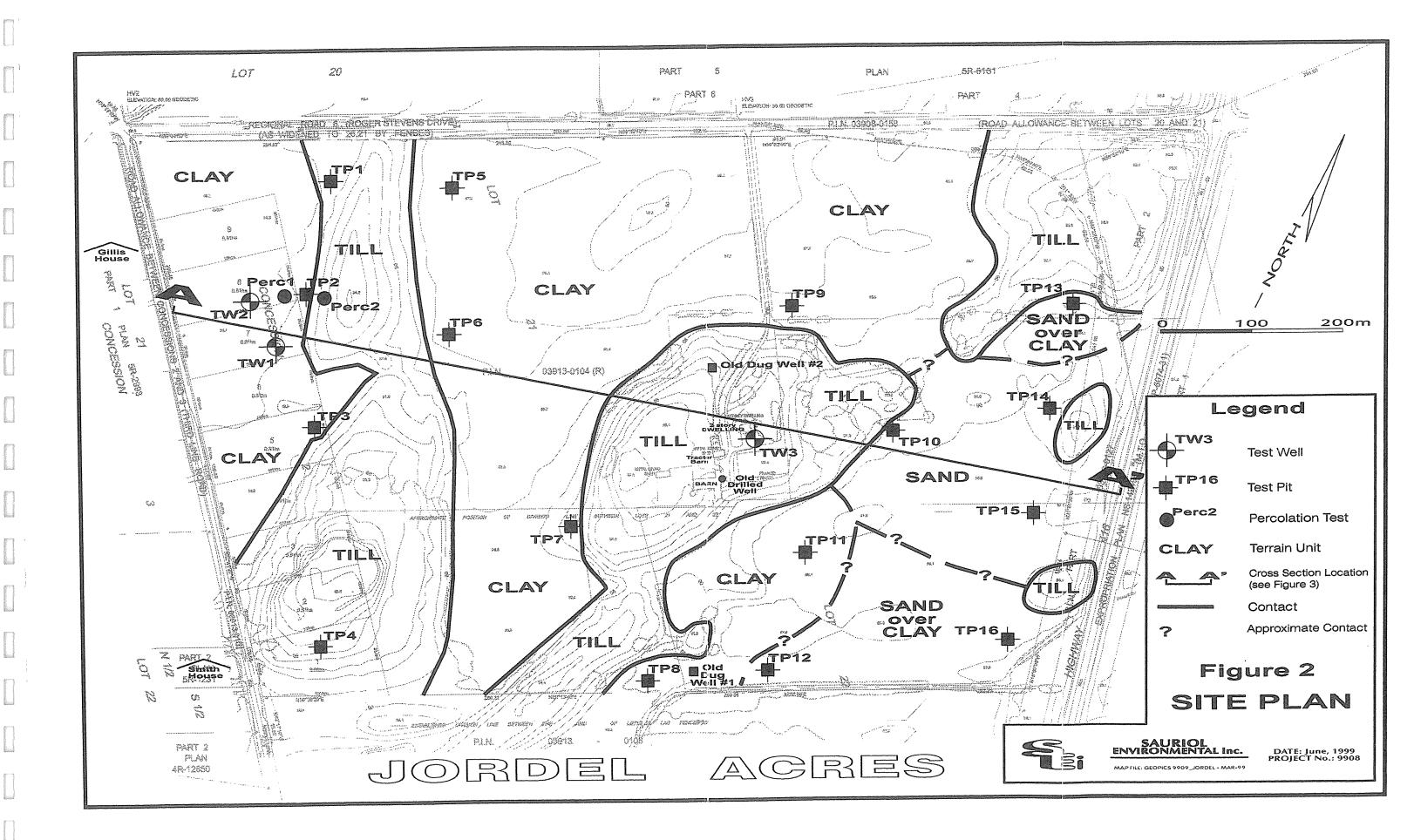
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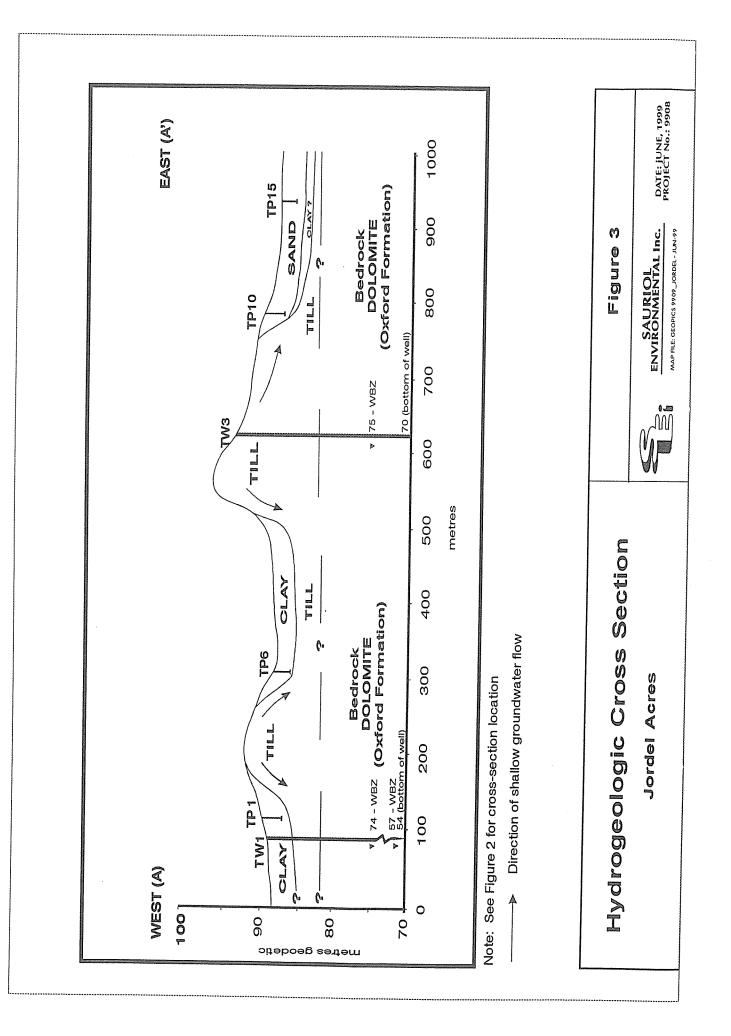
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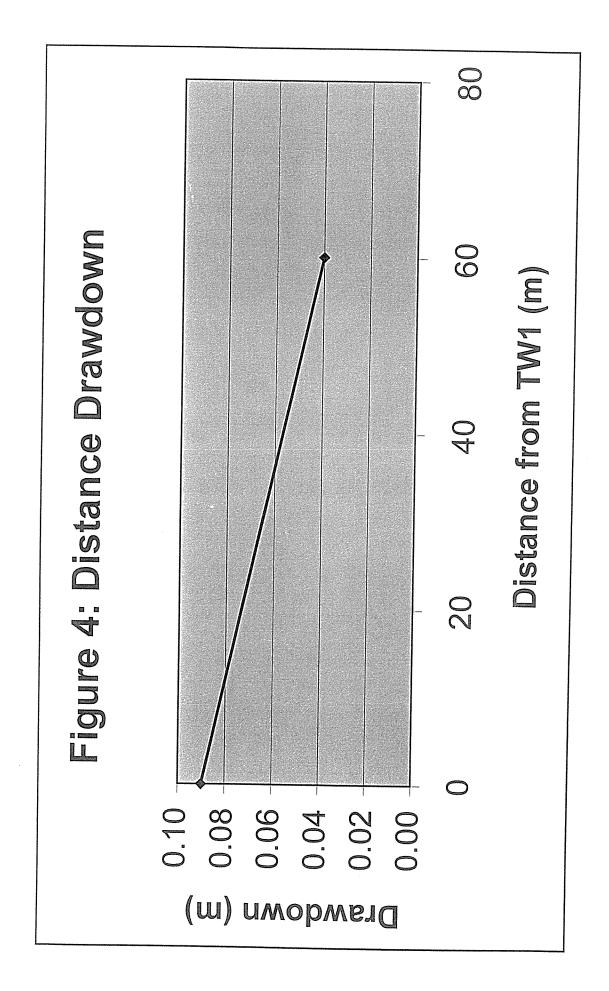
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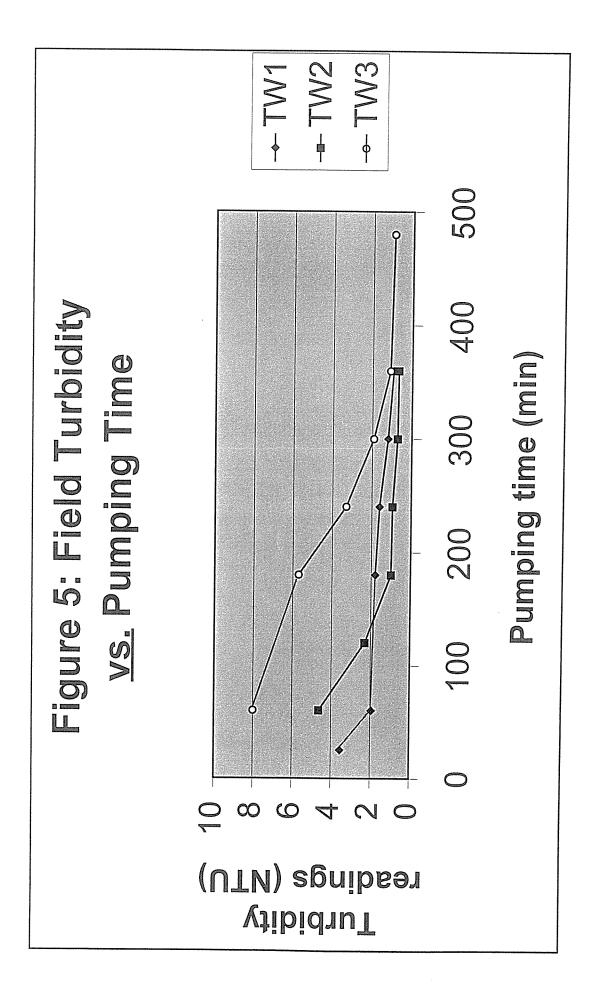
E.











APPENDIX A

WELL CERTIFICATION & WELL SPECIFICATIONS

WELL CERTIFICATION STATEMENT

Property:

Jordel Acres Proposed Subdivision Lot 21 Con 3 (North Gower) Rideau Township 3 test wells constructed for the purpose of completing a Hydrogeological and Terrain Analysis Report

Certification:

We hereby agree that the three test wells constructed on the above captioned property, have been completed in accordance to MOE Regulation 903, and in particular the well casings have been properly pressure grouted.

Jacques Sauriol M. Sc. Sauriol Environmental Inc

Dated: 28 (hay 1999

J. David McManus, P. Eng. CME

June 2/99 Dated:

Specifications Drilling of Well Testing of Well Jordel Acres Proposed Subdivision Lot 21 Con 2 Rideau Township

At a location indicated on the Plan of Subdivision, construct a well in the bedrock aquifer. The owner will provide the required physical access to the drill site, including temporary gravel road and culvert as required. The owner will also field locate any buried utilities.

1.0 Drilling

Drill open hole 200mm in diameter to approximately 11m in depth for a minimum of 0.3m into the rock surface, using drilling mud.

Drop 150mm casing with centralizer and drive shoe.

Pressure grout the annulus space of the casing with high early cement grout mixture installed by grout pump from the bottom of the casing upward through annulus, until full cement circulation is encountered at the surface.

Let cement cure overnight.

Drill open hole 150mm diameter to first water bearing zone, in the rock, typically 30m in depth from the ground surface. (The target yield is about 3 to 5 gpm)

Complete a 5 hour well development with water discharge to the nearby ditch at a constant rate of 3 gpm. Record water level and turbidity hourly

2.0 Pumping test

One well will be pump-tested

Set-up submersible pump with trimmie pipe for water level indicator probe, and generator. Chlorinate well and ensure well bore water mixing. Let sit overnight.

Record static water level of the wells

From a fully recovered well (original Static Level), complete a constant discharge pumping test for a duration of 6 hours at a constant rate of 3 gpm. The contractor is to record the time-drawdown at least an hour interval.

Do a minimum of 4 hours recovery test or until a 95 % recovery is achieved.

Record drawdown and recovery time information with a water level indicator to be provided by the contractor.

Sample well water near the beginning and near the end of the 6 hour test.

Submit two water samples per well for analytical work (parameters = subdivision listing of parameters)

All the above work to comply with Ontario Regulations. Submit water well records and hydraulic test notes

Additional notes on grouting:

Grouting inspections were carried out on the three new wells to ensure cement circulation was completed in the annulus to ground surface. The Driller mixed 5 bags of high early cement per well and trimmied the cement down through the inside of the casing. Cement was observed displacing the drilling mud, and coming and staying at surface at all three well heads.

Proposed Clause for Well Certification,

to be verified with the RMOC for final wording

Lot owners will be required to provide certification by a Professional Engineer that the well construction is in accordance with the recommendation of the approved Hydrogeological and Terrain Analysis Report. This certification shall be submitted to the Part VIII Director under the Environmental Protection Act, prior to the issuance of a Use Permit for sewage disposal system associated with each lot created in the Plan of Subdivision.



NN:NI EEEIVIS 9875291

BOURGOIS WELL DRILL*

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Ontario	Ministry of Environme and Energ
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PAGE Ø1 The Ontario Water Resources Act WATER WELL RECORD

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BOURGOIS WELL DRILL*



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Grey 11	Shale	Kayered	24 39 39 104

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iest hole () Abandoned	Door quality [Replacer (Other)	ment well				
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WATER USE						<i>M</i>
II Stock II Municipal						8
I Imgation I.) Public suppl	Li Other					- 5
I Industrial D Cooling & ai	r conditioning					N N
METHOD OF CONSTRUCTION						. 2
I Cable tool [] Air percussio	n C Driving			1		21, 1
Hotary (conventional)] Boring	L' Digging					~ 1
Bolory (air) i] Jetting	U other					197100
						TOLTOO
Name of Well Contractor	ADA Well Contractor's	LICENCE No. 1			······································	
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1 - CONTRACTOR'É C	OPY					0508 (07/94) Front Form 9

BUURGUIS WELL DRILL*

🗑 Ontario Ministry of the Environment

Print only in spaces provided. Mark corroot box with a checkmark, where applicable.

The Ontario Water Resources Act WATER WELL RECORD

TW3

County Di sului)
County or District Ottown CARLETON Owner's surname County or District Name	Townshipsborough/City/Town/Vilage Con block	tract survey, et	tr. Lot 21
EAR ALAS	Moth Davis	Date completed	9 05 99
- que banniei		day	y month year
100.05.01			

LOG OF	OVERBURDEN AND BEDROCK MATT	FRIAL & Incoming			
Most common material	Other materials		Depth - leet		
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11	U	- Obuse	-12	8	
limestone.	Shale	Kanpa ed		36 58	
limestone		HARG	58	79	
		·			
	LOG OF Most common material TIII Im estone	TIL Boulders	Induction Other materials General description TIII Bouldees Souse II II II	Till Boulders Shale Lingered 36	

	ATER RECO	-dF	1	CASING & O	PEN HOLE	RECORD		Sizes of opening	Diame	101	
Water found at - feet	Kind of		Inside diam inches	Material	Well thicknese		- feet To		L'haine	Inches	engtin taat
65	C Salty	Sulphur Minerals Gas Sulphur Gas Minerals Minerals	87 "	U Steal Gatvanized Concrete Open hole Plastic	inches	D	40	Material and type		Depth at b	op of screen toet
	 ↓ Fresh ↓ Salty □ Fresh □ Fresh 	☐ Bas ☐ Sulphur ☐ Minerais ☐ Gas ☐ Sulphur ☐ Sulphur	64"	-Briteel Galvanized Concrete Open hole Plastic	1.88	+2	40	PLUG Br Annula Deptih set at - keet From To	GING & SEALI repace Material and type	C Abando	nment
	□ Fresh □ Salty	☐ Gae ☐ Sulphur ☐ Minerals ☐ Gae	6"	Galvanized Galvanized Concrete Gpen hole Plastic		40	79	4 70	Comen		int
I) Pump State level State level State level State level State level State level State level I commend I: shatow FINAL STAT Stoter I course I c	end of pumping and and and and and and and and and and	15 mhulee 3 2 // feet 2 Pump Intake set a Recommended pump setting - - - - - - - - - - - - - -	0 minutes 24 teat 2 total 2	24 feet Water at end of trat U Clear Recommended pump rate	Mina Recovery 20 minutes 24 feet Cloudy 5 GPM ent well		In diagra Indicate (LOCATION m below show distar north by arrow. T N Cam at y	NOF WELL Incas of well from		lot line.
1 Rotary (1 Rotary (TRotary ((conventional)	Air percussion Boring Diamond Jetting		Driving Digging Other			ł			2000	
Nerrie of Well Con Address Sharing cl Well Techn SA Lug Signature of Techni Signature of Techni	ALL ALL Inician Contractor	ERT Parymo	Daill Dort	Well Commerce's L		International Contraction of Contrac				2060	149
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APPENDIX C HYDRAULIC TESTS

JORDEL ACRES TW#1 6 HOUR PUMPING TEST DATE: 26 MAY 1999 DRILLER: BOURGEOIS WELL DRILLING

							Observa	tion well TW2
TIME	DURATION	DURATION		DRAWDOWN	FLOW	RATE	DYNAMIC	DRAWDOWN
			LEVEL		OF W	ELL 1	LEVEL	
	MINUTES	DAYS	METRES	METRES	M3/DAY	LPM	METRES	METRES
11:30	0	0	1.85	0.00	23.04	16	1.85	0.00
	2	0.0014	1.91	0.06				
	4	0.0028	1.91	0.06				
	6	0.0042	1.91	0.06				
	8	0.0056	1.92	0.07				
	10	0.0069	1.92	0.07			1.87	0.02
	15	0.0104	1.92	0.07				0.02
	20	0.0139	1.92	0.07				
	25	0.0174	1.93	0.08				
	60	0.0417	1.94	0.09			1.89	0.04
	120	0.0833	1.94	0.09			1.00	0.04
	180	0.1250	1.94	0.09			1.89	0.04
	240	0.1667	1.94	0.09			1.89	0.04
	300	0.2083	1.94	0.09			1.89	0.04
	360	0.2500	1.94	0.09			1.89	0.04

Separation distance between TW1 and TW2 = 60 metres

TIME	DURATION	DURATION	DYNAMIC LEVEL	DRAWDOWN	RESIDUAL DRAWDOWN	FLOW OF W	RATE /ELL 1
	MINUTES	DAYS	METRES	METRES	METRES	M3/DAY	LPM
11:30	0	0	1.85	0		23.04	16
17:30	360	0.2500	1.94	0.09			
17:30	0	0	1.94		0.09		
	1	0.0007	1.88		0.03		
	2	0.0014	1.87		0.02		
	5	0.0035	1.87		0.02		
	10	0.0069	1.86		0.01		
	30	0.0208	1.85		0.00		

JORDEL ACRES TW#2 6 HOUR PUMPING TEST DATE: 27 MAY 1999 DRILLER: BOURGEOIS WELL DRILLING

							Observat	ion well TW1
TIME	URATIO	DURATION		DRAWDOWN	FLOW	RATE	DYNAMIC	DRAWDOWN
			LEVEL		OF W	ELL 2	LEVEL	
	MINUTES	DAYS	METRES	METRES	M3/DAY	LPM	METRES	METRES
11:30	0	0	1.82	0.00	23.04	16	1.82	0.00
	. 2	0.0014	1.94	0.12				
	4	0.0028	1.94	0.12				
	6	0.0042	1.95	0.13				
	8	0.0056	1.95	0.13				
	10	0.0069	1.95	0.13			1.84	0.02
	20	0.0139	1.96	0.14			1.87	0.05
	30	0.0208	1.97	0.15				
	60	0.0417	1.97	0.15			1.87	0.05
	120	0.0833	1.98	0.16				
	180	0.1250	1.98	0.16			1.88	0.06
	240	0.1667	1.98	0.16				0.00
	300	0.2083	1.98	0.16				
	360	0.2500	1.98	0.16			1.88	0.06

Separation distance between TW1 and TW2 = 60 metres

н

TIME	DURATION		DYNAMIC LEVEL	DRAWDOWN	RESIDUAL DRAWDOWN		RATE /ELL 2
	MINUTES	DAYS	METRES	METRES	METRES	M3/DAY	LPM
11:30	0	0	1.82	0		23.04	16
17:30	360	0.2500	1.98	0.16			
17:30	0	0	1.98		0.16		
	1	0.0007	1.85		0.03	·	
	2	0.0014	1.85		0.03		
	5	0.0035	1.84		0.02		
	10	0.0069	1.83		0.01		
	15	0.0104	1.83		0.01		
	20	0.0139	1.83		0.01		
	25	0.0174	1.83		0.01		
	30	0.0208	1.82		0.00		

JORDEL ACRES TW#3 6 HOUR PUMPING TEST DATE: 25 MAY 1999 DRILLER: BOURGEOIS WELL DRILLING

TIME	DURATION	DURATION	DYNAMIC	DRAWDOWN	FLOW	RATE
			LEVEL			VELL 3
	MINUTES	DAYS	METRES	METRES	M3/DAY	LPM
7:30	0	0	7.20	0.00	21.60	15
	2	0.0014	7.20	0.00		
	4	0.0028	7.20	0.00		
	6	0.0042	7.21	0.01		
	8	0.0056	7.21	0.01		
	10	0.0069	7.21	0.01		
	20	0.0139	7.21	0.01		
	30	0.0208	7.21	0.01		
	40	0.0278	7.21	0.01		
	50	0.0347	7.21	0.01		
	60	0.0417	7.21	0.01		
	120	0.0833	7.21	0.01		
	180	0.1250	7.21	0.01		
	240	0.1667	7.22	0.02		
	300	0.2083	7.22	0.02		
	360	0.2500	7.22	0.02		
	480	0.3333	7.22	0.02		

JORDEL ACRES TW#3 RECOVERY TEST DATE: 25 MAY 1999 DRILLER: BOURGEOIS WELL DRILLING

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in the second

TIME	DURATION	DURATION	DYNAMIC	DRAWDOWN	RESIDUAL	FLOW	/ RATE
			LEVEL		DRAWDOWN		VELL 3
	MINUTES	DAYS	METRES	METRES	METRES	M3/DAY	LPM
7:30	0	0	7.2	0		21.60	15
15:30	480	0.3333	7.22	0.02			10
				alanna ann an a			9407.0422040307.2538423470778.86586398
15:30	0	0	7.22		0.02		
	1	0.0007	7.20		0.00		

APPENDIX D WATER QUALITY

Client:

Sauriol Environmental

Attn: Mr. Jacques Sauriol

Report Number: Date: Date Submitted: Date Collected: Project:

9904192 Jun 15,1999 May 27,1999 May 26,1999 9908

PARAMETER UNITS MDL TW1 1hr TW1 6hr Fe mg/L 0.01 0.19 0.22 Mn mg/L 0.01 ND ND Hardness mg/L 0.203 1 252 252 Alkalinity mg/L CaCO3 1 252 252 Alkalinity mg/L CaCO3 2 250 246 pH 7.64 7.61 7.64 7.61 Conductivity umhos/cm 3 789 770 F mg/L 0.10 0.58 0.58 Na mg/L 0.10 ND 0.15 N-NO3 mg/L 0.02 0.08 SO4 mg/L 1 88 93 Phenols mg/L 0.01 ND Colour Pt/Co units 2 ND				·····	Matrix:	·····	WATER	
Twin Twin <th< th=""><th></th><th></th><th></th><th>sample</th><th>sample</th><th>sample</th><th>sample</th><th>sample</th></th<>				sample	sample	sample	sample	sample
Mn mg/L 0.01 ND ND Hardness mg/L CaCO3 1 252 252 Alkalinity mg/L CaCO3 2 250 246 pH 7.64 7.61 Conductivity conductivity umhos/cm 3 789 770 F mg/L 0.10 0.58 0.58 Na mg/L 1 65 71 N-NO3 mg/L 0.10 ND ND N-NO2 mg/L 0.10 ND ND N-NH3 mg/L 0.02 0.08 SO4 mg/L 1 86 93 Phenols mg/L 0.001 ND Furbidity NTU 0.1 2.3 Colour Pt/Co units 2 ND Ca mg/L 1 48 48 Mg mg/L 1 32 32 Canini & Lignin mg/L 0.05 0.12 Ca mg/L 1 7 7 CoC mg/L 0.4 1.0 Ca mg/L 0.4 1.0 Ca mg/L 0.4 1.0 Ca <	FARAMETER	UNITS	MDL	TW1 1hr	TW1 6hr			
Mn mg/L 0.01 ND ND Hardness mg/L CaCO3 1 252 252 Alkalinity mg/L CaCO3 2 250 246 pH 7.64 7.61 Conductivity umhos/om 3 789 770 F mg/L 0.10 0.58 0.58 0.58 0.58 Na mg/L 1 65 71 0.00 ND N-NO3 mg/L 0.10 ND 0.15 0.08 0.08 SO4 mg/L 0.02 0.08 0.08 0.08 0.08 SO4 mg/L 0.001 ND ND 0.10 ND Phenols mg/L 0.001 ND 0.23 0.08 0.08 SO4 mg/L 1 88 93 0.01 ND 0.08 Colour Pt/Co units 2 ND ND 0.01 ND Colour mg/L 0.1 <td>Fe</td> <td>mg/L</td> <td>0.01</td> <td>0.19</td> <td>0.22</td> <td></td> <td></td> <td></td>	Fe	mg/L	0.01	0.19	0.22			
Hardness mg/L CaCO3 1 252 252 Alkalinity mg/L CaCO3 2 250 246 pH 7.64 7.61 7.61 Conductivity umhos/cm 3 789 770 F mg/L 0.10 0.58 0.58 Na mg/L 0.10 ND 0.15 N-NO3 mg/L 0.10 ND ND N-NO2 mg/L 0.02 0.08 0.08 SO4 mg/L 3 42 42 22 Cl mg/L 1 88 93 Phenols mg/L 0.001 ND ND Colour Pt/Co units 2 ND ND Ca mg/L 1 48 48 Mg mg/L 1 32 32 Canin & Lignin mg/L 0.05 0.12 Coc mg/L 1 7 7 Coc mg/L 1 7 7 Colour mg/L 0.4 <td>Mn</td> <td></td> <td></td> <td>1</td> <td>1</td> <td></td> <td></td> <td></td>	Mn			1	1			
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N-NO3 mg/L 0.10 ND 0.15 N-NO2 mg/L 0.10 ND N-NH3 mg/L 0.02 0.08 SO4 mg/L 3 42 42 Cl mg/L 1 88 93 Phenols mg/L 0.001 ND Curbidity NTU 0.1 2.3 Colour Pt/Co units 2 ND Ca mg/L 1 48 48 Mg mg/L 1 32 32 Ca mg/L 1 32 32 Fannin & Lignin mg/L 0.1 ND Total Kjeldahl Nitrogen mg/L 0.05 0.12 Co mg/L 1 7 7 OOC mg/L 0.4 1.0 ND TDS mg/L 0.01 ND ND	Na	-) (
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N-NH3 mg/L 0.02 0.08 SO4 mg/L 3 42 42 CI mg/L 1 88 93 Phenols mg/L 0.001 ND Furbidity NTU 0.1 2.3 Colour Pt/Co units 2 ND Ca mg/L 1 48 48 Mg mg/L 1 32 32 Fannin & Lignin mg/L 0.1 ND Total Kjeldahl Nitrogen mg/L 0.05 0.12 Co mg/L 0.4 1.0 DS mg/L 0.01 ND GL mg/L 0.4 1.0 Tannin & Lignin mg/L 0.4 1.0 Total Kjeldahl Nitrogen mg/L 0.4 1.0 TDS mg/L 2 452 H2S mg/L 0.01 ND	N-NO2		1	ND				
SO4 mg/L 3 42 42 Cl mg/L 1 88 93 Phenols mg/L 0.001 ND Furbidity NTU 0.1 2.3 Colour Pt/Co units 2 ND Ca mg/L 1 48 48 Mg mg/L 1 32 32 Fannin & Lignin mg/L 0.1 ND Total Kjeldahl Nitrogen mg/L 0.05 0.12 Mo mg/L 1 7 7 OOC mg/L 0.4 1.0 TDS mg/L 0.01 ND Paperate 0.01 ND	N-NH3				1			
Cl mg/L 1 88 93 Phenols mg/L 0.001 ND Furbidity NTU 0.1 2.3 Colour Pt/Co units 2 ND Ca mg/L 1 48 48 Ag mg/L 1 32 32 Fannin & Lignin mg/L 0.1 ND Total Kjeldahl Nitrogen mg/L 0.1 ND OOC mg/L 1 7 7 OOC mg/L 0.4 1.0 TDS mg/L 2 452 Mg/L 0.01 ND	504			42				
Phenols mg/L 0.001 ND Furbidity NTU 0.1 2.3 Colour Pt/Co units 2 ND Ca mg/L 1 48 48 Mg mg/L 1 32 32 Fannin & Lignin mg/L 0.1 ND Total Kjeldahl Nitrogen mg/L 0.05 0.12 COC mg/L 1 7 7 OOC mg/L 0.4 1.0 TDS mg/L 0.01 ND PS mg/L 0.01 ND		-	4					
Turbidity NTU 0.1 2.3 Colour Pt/Co units 2 ND Ca mg/L 1 48 48 Mg mg/L 1 32 32 Fannin & Lignin mg/L 0.1 ND Fotal Kjeldahl Nitrogen mg/L 1 7 QOC mg/L 1 7 Mg Mg/L 1 7 Fotal Kjeldahl Nitrogen mg/L 0.4 1.0 TDS mg/L 0.01 ND H2S mg/L 0.01 ND	^{>} henols			00				
Colour Pt/Co units 2 ND Ca mg/L 1 48 48 Mg mg/L 1 32 32 Fannin & Lignin mg/L 0.1 ND Total Kjeldahl Nitrogen mg/L 0.05 0.12 Mg mg/L 1 7 7 OOC mg/L 0.4 1.0 TDS mg/L 2 452 H2S mg/L 0.01 ND			1		1			
Ca mg/L 1 48 48 Mg mg/L 1 32 32 Fannin & Lignin mg/L 0.1 ND Total Kjeldahl Nitrogen mg/L 0.05 0.12 Kooc mg/L 1 7 OOC mg/L 0.4 1.0 TDS mg/L 2 452 H2S mg/L 0.01 ND	-							
Mg mg/L 1 32 32 Fannin & Lignin mg/L 0.1 ND Fotal Kjeldahl Nitrogen mg/L 0.05 0.12 K mg/L 1 7 7 DOC mg/L 0.4 1.0 TDS mg/L 2 452 H2S mg/L 0.01 ND			1	10	1			
Fannin & Lignin mg/L 0.1 ND Fotal Kjeldahl Nitrogen mg/L 0.05 0.12 Mg/L 1 7 7 OOC mg/L 0.4 1.0 TDS mg/L 0.01 ND Mg/L 0.4 1.0 Mg/L 0.01 ND			1	4				
Total Kjeldahl Nitrogen mg/L 0.1 ND K 0.05 0.12 Mg/L 1 7 7 OOC mg/L 0.4 1.0 TDS mg/L 2 452 H2S mg/L 0.01 ND	-	-		32				
Mg/L 1 7 7 DOC mg/L 0.4 1.0 DS mg/L 2 452 12S mg/L 0.01 ND		-	1					
DOC mg/L 0.4 1.0 'DS mg/L 2 452 12S mg/L 0.01 ND	<		1	_				
DS mg/L 2 452 i2S mg/L 0.01 ND		-	- 1	1				
12S mg/L 0.01 ND								
			1					
on Balance		mg/L	0.01		ND			
	on Balance			0.96	0.99			
	1DI =Method Detection Limit					¢		

MDL=Method Detection Limit

ND=Not Detected

Comment:

U Approval:

Client: Sauriol Environmental

Attn: Mr. Jacques Sauriol

 Report Number:
 9904192

 Date:
 Jun 15,1999

 Date Submitted:
 May 27,1999

 Date Collected:
 May 26,1999

 Project:
 9908

				Matrix:		WATER	
	T		sample	sample	sample	sample	sample
PARAMETER	UNITS	MDL	TW1 6hr				Sumple
Total Coliforms Faecal Coliforms Faecal Streptococci E. Coli Standard Plate Count (48hrs)	cts/100mls cts/100mls cts/100mls cts/100mls cts/1ml		0 0 0 12				

MDL=Method Detection Limit

ND=Not Detected

Comment:

Approval:

Client:

Sauriol Environmental

Attn: Mr. Jacques Sauriol

 Report Number:
 9904224

 Date:
 Jun 14,1999

 Date Submitted:
 May 28,1999

 Date Collected:
 May 28,1999

 Project:
 9908

				Matrix:		WATER	
			sample	sample	sample	sample	sample
PARAMETER	UNITS	MDL	TW2 6hrs	TW2 1hr	Gillis	Smith	
Fe	mg/L	0.01	0.10	0.54	ND	1.77	
Mn	mg/L	0.01	ND	ND	ND	ND	
Hardness	mg/L CaCO3	1	249	265	ND	361	
Alkalinity	mg/L CaCO3	2	245	254	284	309	
рН			7.62	7.58	7.67	7.53	
Conductivity	umhos/cm	3	790	781	714	7.00	
F	mg/L	0.10	0.59	0.55	0.34	0.27	
Na	mg/L	1	73	66	187	16	
N-NO3	mg/L	0.10	ND	ND	ND	0.14	
N-NO2	mg/L	0.10	ND	ND	ND		
N-NH3	mg/L	0.02	0.07	ND	ND	ND	
SO4	mg/L	3	42	41	38	20	
CI	mg/L	1	99	86	30 42	36	
Phenols	mg/L	0.001	ND	00	42	35	
Turbidity	NTU	0.1	1.2				
Colour	Pt/Co units	2	ND				
Са	mg/L	1	47	50			
Mg	mg/L	1	32	50	ND	72	
Tannin & Lignin	mg/L	0.1		34	ND	44	
Total Kjeldahl Nitrogen	mg/L		ND				
K	mg/L	0.05	0.15	_			
000	· · ·	1	7	7	ND	4	
rds	mg/L	0.4	0.8				
	mg/L	2	464				
-25	mg/L	0.01	ND				
H2S	-	1			{	1	

MDL=Method Detection Limit

ND=Not Detected

Comment:

Client:

Sauriol Environmental

Attn: Mr. Jacques Sauriol

Report Number: Date: Date Submitted: Date Collected: Project: 9904224 Jun 14,1999 May 28,1999 May 28,1999 9908

	1	····		Matrix:		WATER	
DADAMETED		8401	sample	sample	sample	sample	sample
PARAMETER	UNITS	MDL	TW2 6hrs				
Total Coliforms	cts/100mls		2				
Faecal Coliforms	cts/100mls		0				
Faecal Streptococci	cts/100mls		0				
E. Coli	cts/100mls		0				
Standard Plate Count (48hrs)	cts/1ml		0				
MDL=Method Detection Limit	l						

MDL=Method Detection Limit

ND=Not Detected

Comment:

Client:

Sauriol Environmental

Attn: Mr. Jacques Sauriol

Report Number: Date: Date Submitted: Date Collected: Project: 9904093 Jun 9,1999 May 26,1999 May 25,1999 9908

PARAMETER UNITS MDL TW3 1Hr TW3 8Hr Jumps Jumps <thjumps< th=""> Jumps Jumps</thjumps<>					Matrix:		WATER	
Fe mg/L 0.01 TW3 1Hr TW3 8Hr Mn mg/L 0.01 ND ND Hardness mg/L CaCO3 1 285 304 Alkalinity mg/L CaCO3 2 276 290 OH				sample	sample	sample	sample	sample
Mn mg/L 0.01 ND ND Hardness mg/L CaCO3 1 285 304 Alkalinity mg/L CaCO3 2 276 290 pH 7.71 7.68 7.68 Conductivity umhos/cm 3 774 679 F mg/L 0.10 0.49 0.33 Na mg/L 1 57 32 N-NO3 mg/L 0.10 1.56 1.13 N-NO2 mg/L 0.10 0.17 ND SO4 mg/L 3 46 33 Cl mg/L 0.001 ND ND SO4 mg/L 0.001 ND ND Phenols mg/L 0.001 ND ND Ca mg/L 0.01 1.77 ND Colour Pt/Co units 2 ND ND Ca mg/L 1 58 64 Mg mg/L 1 34 35 Fannin & Lignin mg/L <td< td=""><td>PARAMETER</td><td>UNITS</td><td>MDL</td><td>TW3 1Hr</td><td>TW3 8Hr</td><td></td><td></td><td></td></td<>	PARAMETER	UNITS	MDL	TW3 1Hr	TW3 8Hr			
Mn mg/L 0.01 ND ND Hardness mg/L CaCO3 1 285 304 Alkalinity mg/L CaCO3 2 276 290 pH 7.71 7.68 7.78 Conductivity umhos/cm 3 774 679 F mg/L 0.10 0.49 0.33 Na mg/L 0.10 1.56 1.13 N-NO3 mg/L 0.10 0.17 NND N-NO2 mg/L 0.02 ND S04 SO4 mg/L 3 46 33 Cl mg/L 0.001 ND ND SO4 mg/L 0.001 ND ND Turbidity NTU 0.1 1.77 S02 Colour Pt/Co units 2 ND S04 Mg mg/L 1 34 35 Fannin & Lignin mg/L 0.1 ND CoC	Fe	mg/L	0.01	0.28	0.04			
Hardness mg/L CaCO3 1 285 304 Alkalinity mg/L CaCO3 2 276 290 pH 7.71 7.68 Conductivity umhos/cm 3 774 679 F mg/L 0.10 0.49 0.33 Na mg/L 1 57 32 N-NO3 mg/L 0.10 1.56 1.13 N-NO2 mg/L 0.02 ND SO4 mg/L 3 46 33 CI mg/L 1 72 41 Phenols mg/L 0.001 ND Turbidity NTU 0.1 1.7 Colour Pt/Co units 2 ND Ca mg/L 1 58 64 Mg mg/L 1 34 35 Tannin & Lignin mg/L 0.05 0.13 CA mg/L 0.05 0.13 COC mg/L 1 ND Total Kjeldahi Nitrogen mg/L 0.01	Mn			1	1 1			
Alkalinity mg/L CaCO3 2 276 290 pH 7.71 7.68 Conductivity umhos/cm 3 774 679 F mg/L 0.10 0.49 0.33 Na mg/L 1 57 32 N-NO3 mg/L 0.10 1.56 1.13 N-NO2 mg/L 0.02 ND SO4 mg/L 3 46 33 CI mg/L 0.02 ND SO4 mg/L 1 72 41 Phenols mg/L 0.001 ND ND SO4 mg/L 1 72 41 Phenols mg/L 0.001 ND ND Ca mg/L 1 58 64 Mg mg/L 0.1 ND ND Ca mg/L 0.1 ND ND Ca mg/L 0.1 ND ND Total Kjeldahl Nitrogen mg/L 0.4 1.7 TDS	Hardness			1				
pH r.7.1 7.68 Conductivity umhos/cm 3 774 679 F mg/L 0.10 0.49 0.33 Na mg/L 1 57 32 N-NO3 mg/L 0.10 1.56 1.13 N-NO2 mg/L 0.10 0.17 N-NH3 mg/L 0.02 ND SO4 mg/L 3 46 33 Cl mg/L 1 72 41 Phenols mg/L 0.001 ND 1.7 Colour Pt/Co units 2 ND ND Ca mg/L 1 58 64 Mg mg/L 1 34 35 Tannin & Lignin mg/L 0.1 ND Coc mg/L 0.1 ND ND Coc mg/L 0.1 ND ND Coc mg/L 0.1 ND ND Coc mg/L 0.4 1.7 1.7 Coc mg/L	Alkalinity				I i			
Conductivity umhos/cm 3 774 679 F mg/L 0.10 0.49 0.33 Na mg/L 1 57 32 N-N03 mg/L 0.10 1.56 1.13 N-NO2 mg/L 0.10 0.17 N-NH3 mg/L 0.02 ND SO4 mg/L 3 46 33 Cl mg/L 1 72 41 Phenols mg/L 0.001 ND Turbidity NTU 0.1 1.7 Colour Pt/Co units 2 ND Ca mg/L 1 58 64 Mg mg/L 1 34 35 Tannin & Lignin mg/L 0.1 ND Cocc mg/L 0.05 0.13 Cocc mg/L 0.4 1.7 TDS mg/L 0.4 1.7 TDS mg/L 0.01	рН	Ŭ			1 1			
F mg/L 0.10 0.49 0.33 Na mg/L 1 57 32 N-N03 mg/L 0.10 1.56 1.13 N-N02 mg/L 0.10 0.17 N-NH3 mg/L 0.02 ND SO4 mg/L 3 46 33 Cl mg/L 1 72 41 Phenols mg/L 0.001 ND Turbidity NTU 0.1 1.77 Colour Pt/Co units 2 ND Ca mg/L 1 58 64 Mg mg/L 1 34 35 Tannin & Lignin mg/L 0.16 ND Total Kjeldahl Nitrogen mg/L 0.05 0.13 K mg/L 0.4 1.7 COC mg/L 0.4 1.7 TOS mg/L 0.1 ND COC mg/L 0.05 0.13 K mg/L 0.4 1.7 TDS m	Conductivity	umhos/cm	3					
Na mg/L 1 57 32 N-NO3 mg/L 0.10 1.56 1.13 N-NO2 mg/L 0.10 0.17 N-NH3 mg/L 0.02 ND SO4 mg/L 3 46 33 Cl mg/L 1 72 41 Phenols mg/L 0.001 ND Turbidity NTU 0.1 1.7 Colour Pt/Co units 2 ND Ca mg/L 1 58 64 Mg mg/L 1 34 35 Tannin & Lignin mg/L 0.1 ND Total Kjeldahl Nitrogen mg/L 0.1 ND OCC mg/L 0.4 1.7 TDS mg/L 2 408 H2S mg/L 0.01 ND	F	1 1			1			
N-NO3 mg/L 0.10 1.56 1.13 N-NO2 mg/L 0.10 0.17 N-NH3 mg/L 0.02 ND SO4 mg/L 3 46 33 Cl mg/L 1 72 41 Phenols mg/L 0.001 ND Turbidity NTU 0.1 1.77 Colour Pt/Co units 2 ND Ca mg/L 1 58 64 Mg mg/L 1 34 35 Tannin & Lignin mg/L 0.1 ND Total Kjeldahl Nitrogen mg/L 0.4 1.7 DOC mg/L 0.4 1.7 TDS mg/L 0.1 ND Add 35 0.13 1.7 TDS mg/L 0.4 1.7 TDS mg/L 0.4 1.7 TDS mg/L 0.01 ND ang/L 0.01 ND ND ang/L 0.01 ND <t< td=""><td>Na</td><td>- 1</td><td></td><td></td><td></td><td></td><td></td><td></td></t<>	Na	- 1						
N-NO2 mg/L 0.10 0.17 N-NH3 mg/L 0.02 ND SO4 mg/L 3 46 33 CI mg/L 1 72 41 Phenols mg/L 0.001 ND Turbidity NTU 0.1 1.7 Colour Pt/Co units 2 ND Ca mg/L 1 58 64 Mg mg/L 1 34 35 Tannin & Lignin mg/L 0.1 ND Total Kjeldahl Nitrogen mg/L 0.05 0.13 K mg/L 0.4 1.7 DOC mg/L 0.4 1.7 TDS mg/L 0.4 1.7 TDS mg/L 0.01 ND mg/L 0.01 ND ND	N-NO3							
N-NH3 mg/L 0.02 ND SO4 mg/L 3 46 33 Cl mg/L 1 72 41 Phenols mg/L 0.001 ND Turbidity NTU 0.1 1.7 Colour Pt/Co units 2 ND Ca mg/L 1 58 64 Mg mg/L 1 34 35 Tannin & Lignin mg/L 0.1 ND Total Kjeldahl Nitrogen mg/L 0.05 0.13 K mg/L 0.4 1.7 FDS mg/L 0.4 1.7 TDS mg/L 0.05 0.13 MS mg/L 0.4 1.7 FDS mg/L 0.4 1.7 FDS mg/L 0.4 1.7 FDS mg/L 0.01 ND mg/L 0.01 ND ND	N-NO2	-		1.00	1			
SO4 mg/L 3 46 33 Cl mg/L 1 72 41 Phenols mg/L 0.001 ND Turbidity NTU 0.1 1.7 Colour Pt/Co units 2 ND Ca mg/L 1 58 64 Mg mg/L 1 34 35 Tannin & Lignin mg/L 0.1 ND Total Kjeldahl Nitrogen mg/L 0.05 0.13 K mg/L 0.4 1.7 TDS mg/L 0.4 1.7 TDS mg/L 0.05 0.13 MD ND ND ND DOC mg/L 0.4 1.7 TDS mg/L 2 408 H2S mg/L 0.01 ND	N-NH3							
Cl mg/L 1 72 41 Phenols mg/L 0.001 ND Turbidity NTU 0.1 1.7 Colour Pt/Co units 2 ND Ca mg/L 1 58 64 Mg mg/L 1 34 35 Tannin & Lignin mg/L 0.1 ND Total Kjeldahl Nitrogen mg/L 0.05 0.13 K mg/L 1 ND DOC mg/L 0.4 1.7 TIDS mg/L 0.01 ND H2S mg/L 0.01 ND	SO4			46				
Phenols mg/L 0.001 ND Turbidity NTU 0.1 1.7 Colour Pt/Co units 2 ND Ca mg/L 1 58 64 Mg mg/L 1 34 35 Tannin & Lignin mg/L 0.1 ND Total Kjeldahl Nitrogen mg/L 0.05 0.13 Kooc mg/L 1 ND ND DOC mg/L 0.4 1.7 TDS mg/L 0.01 ND H2S mg/L 0.01 ND	CI		(
Turbidity NTU 0.1 1.7 Colour Pt/Co units 2 ND Ca mg/L 1 58 64 Mg mg/L 1 34 35 Tannin & Lignin mg/L 0.1 ND Total Kjeldahl Nitrogen mg/L 1 ND MQ mg/L 1 ND OCC mg/L 1 ND DOC mg/L 0.4 1.7 TDS mg/L 0.4 1.7 H2S mg/L 0.01 ND	Phenols		· · ·	12	1			
Colour Pt/Co units 2 ND Ca mg/L 1 58 64 Mg mg/L 1 34 35 Tannin & Lignin mg/L 0.1 ND Total Kjeldahl Nitrogen mg/L 1 ND K mg/L 1 ND DOC mg/L 0.4 1.7 TDS mg/L 0.4 1.7 H2S mg/L 0.01 ND					1			
Ca mg/L 1 58 64 Mg mg/L 1 34 35 Tannin & Lignin mg/L 0.1 ND Total Kjeldahl Nitrogen mg/L 0.05 0.13 K mg/L 1 ND DOC mg/L 0.4 1.7 TDS mg/L 2 408 H2S mg/L 0.01 ND			1					
Mg mg/L 1 30 64 Tannin & Lignin mg/L 1 34 35 Total Kjeldahl Nitrogen mg/L 0.05 0.13 K mg/L 1 ND DOC mg/L 0.4 1.7 TDS mg/L 2 408 H2S mg/L 0.01 ND				EQ				
Tannin & Lignin mg/L 0.1 ND Total Kjeldahl Nitrogen mg/L 0.05 0.13 K mg/L 1 ND DOC mg/L 0.4 1.7 TDS mg/L 2 408 H2S mg/L 0.01 ND				1				
Total Kjeldahl Nitrogen mg/L 0.05 0.13 K mg/L 1 ND ND COC mg/L 0.4 1.7 TDS mg/L 2 408 H2S mg/L 0.01 ND	-	-		34				
K mg/L 1 ND ND DOC mg/L 0.4 1.7 TDS mg/L 2 408 H2S mg/L 0.01 ND			1		1			
DOC mg/L 0.4 1.7 TDS mg/L 2 408 H2S mg/L 0.01 ND			1					
TDS mg/L 2 408 H2S mg/L 0.01 ND			1	ND				
H2S mg/L 0.01 ND								
			1					
on Balance 0.96 0.98		Ing/L	0.01		ND			
	on Balance			0.96	0.08			
	ADL=Method Detection Limit							

MDL=Method Detection Limit

ND=Not Detected

Comment:

Client: Sauriol Environmental

Attn: Mr. Jacques Sauriol

Report Number: Date: Date Submitted: Date Collected: Project:

9904093 Jun 9,1999 May 26,1999 May 25,1999 9908

			·	Matrix:		WATER	
PARAMETER			sample	sample	sample	sample	sample
FARAMETER	UNITS	MDL	TW3 8Hr				
Total Coliforms	cts/100mls		0				
Faecal Coliforms	cts/100mls		0				
Faecal Streptococci	cts/100mls		0				
E. Coli	cts/100mls		0				
Standard Plate Count (48hrs)	cts/1ml		8				•
				i			
DL=Method Detection Limit		VD=Not De	tootod				

Ind Detection Limit

ND=Not Detected

Comment:

LAB USE ONLY Report Number:	to:	lts to:	ults to:	⇔ Indirate: E-Eithered or D-Deconced	CRITERIA CRITERIA REQUIRED * (i.e. MOE Table A, CCME, PWQO, ODWO, Québec)		Sample Description/Remarks								Comments		** There may be a surcharge applied to "Rush" service. Please check with lab.
CORD	Fax Results to:	E-mail Results to:	Copy of Results to:	ANALYSIS REQUIRED										Date/Time:	Mcy 26 99 Date/Time:	Date/Time:	may be a surcharge applied
	Address:	City/Prov: Postal Code:	Project # 9908 * Quotation #	SAMPLE ANALYS	of Containers Bequired ** S=Standard (hemistry hockage	Service	- N	7 5	2	- 2 7					Utition CGr Received By:	Received By Lab:	
7-5692			Pro		nple Matrix G=Grab	ns2	Ŗ	3	20	5 N				Date/Time:	Date/Time:	Date/Time:	is will proceed only
ACCUTEST LABORATORIES LTD. 146 Colonnade Rd, Unit 8 Nepean, ON K2E 7Y1 Phone: (613) 727-5692	Company Name: Sauriol Environmente	Attention:	Phone: 749-6066	Invoice to: (if different from above)		Sample ID Date Time Collected Collected	m'	5 8 hr Mc 25/99	14-	Soil # 2 Mr. 22189 4. 000				Sampled By: Ru Lindlan	7	Relinquished By: Rob Find Rob	Page of

LAB USE ONLY Report Number:	sults to:	E-mail Results to:	Copy of Results to:		a Indicate: F=Filtered or P=Preserved	uo	PWQ0, ODW0, Québec)	deJ mebl	Sample Description/Remarks								Comments		(Inf) []	** There may be a surcharge applied to "Rush" service. Please check with Ish	
CORD	Fax Results to:	E-mail I	Copy of	IS REQUIRED													Date/Time:	1 85	Date/Time:	may be a surcharge ap	•
CHAIN OF CUSTODY RECORD Fax: (613) 727-522	ess:	City/Prov: 1/00.65 Postal Code:	15	SAMPLE ANALYSIS REQUIRED	¥4	* bəıir	рэЯ е	ز ګړ ۱۹۱ ز ګړ ۱۹۱ عود ۲۹۱ عود ۲۹۱ عود ۲۹۱	S	2 2	~ 7					Chimmed Vice	$\mathcal{D}(\mathcal{X}\mathcal{C}\mathcal{X}\mathcal{A})$	Received By (Received By Lab:		
			Project			i=Gral	·····	San C=Cor		3	m G					 Date/Time:	Mex 27/99	Date/Time:	Date/Time: Mc. ううくなび	s will proceed only	
ACCUTEST LABORATORIES LTD. 146 Colonnade Rd., Unit 8 Nepean, ON K2E 7Y1 Phone: (613) 727-5692	Company Name: Squiriol Environmenta	Attention:	Phone: 749-6066	Invoice to: (if different from above)				Sample ID Collected Time	(mm/dd/yy)	1 14C 1110 - 11	1W 1 0 hr My 26 199 5:30 pr					Sąmplęd Byj., VI,	Kib Findlay	veiludaisued by:	Relinquighed By: Acceived By Lab:	* Indicates a required field, If not complete, analysis	Page í of l

es: White - Sampler, Yellow - Laboratory, Pink - With Report

7-5222 Preport Number: Report Number: IL Fax Results to:	ion # Copy of Results to:	ANALYSIS REQUIRED									Date/Time: Mr. 2) 60 Date/Time	ime: / 28 / 94
ostal Code:	ion #	ANAL						 			Date MC	Date/Time:) /// Date/Time:)
. 72	1/anier 49708	SAMPLE	r of Containers e Required ** h S=Standard	Servic	2	7 7	7			Shimod Vic.	Pictured By C.C. C.C.	eived By Lab:
	Project		mple Matrix mp. G=Grab	o)=)	E C	A A C I	7r (U & -			Date/Time.	Mr. 27 5:0 Date/Time:	Date/Time: Date/Time: Aec <i>Wig-28</i> ((G complete, analysis will proceed only on verifi
	-1999 - 60 66	Invoice to: (if different from above)		Date Collected (mm/dd/yy)	May 27/99	ENT " 5:300	u h 3:000				Relinquished By:	Relinquished BY:

REPORT OF ANALYSIS

Client

Golder Associates

Attn: Mr. Brian Stratton

Report Number: Date: Date Submitted: Dato Collected: Project:

A7-1684 Apr. 1, 1997 Mar. 27, 1997 Mar. 26, 1997 971-2630

				Matrix:		WATER	
PARAMETER	UNITS	MDL	sample	sample	sample	sample	sample
	enne		SA 1				
Fe							
Mn	mg/L	0.01	0.17				
Hardness	mg/L	0.01	ND				
	mg/L CaCO3		222				
Alkalinity	mg/L CaCO3	2	221				
pH			7.83				,
Conductivity	umhos/cm	3	856				<i>x</i>
F	mg/L	0 _10	0.78		× .		
Na	mg/L	1	95				
N-NO3	mg/L	0.10	ND				
N-NO2	mg/L	0.10	ND				
N-NH3	mg/L	0.02	0,18				
504	mg/L	3	52				
	mg/L	1	114				
Phenois	mg/L	0.002	ND				
luplaty	NTU	0.1	2.4				_
Calaur	PVCo units	2	ND				ŗ
Ca	mg/L	1	41				
1g	mg/L	1	29	1			
annin & Lignin	mg/L	0.1	ND				
oral Kjeldahl Nitrogen	mg/L	0.05					
	mg/L	1	0.23	1			
oc	mg/L	0.2	8				
DS	mg/L	2	1.1				
25		1	508				
	mg/L	0.01	ND				
on Balanca			1.00				
						2	

MDL=Method Detection Limit

ND=Not Detected

Somment

FIELD MEASUREMENTS Conductionale = 890 Tomp = 6°C

Approval:

ł

CUTEST LABORATORIES

REPORT OF ANALYSIS

Golder Associates

3

à.

Client

Attn: Mr. Brian Stratton

Report Number: Date: Date Submitted: Date Collected: Project:

A7-1684 Apr. 1, 1997 Mar. 27, 1997 Mar. 26, 1997 971-2830

	1	1		Matrix:		WATER	
PARAMETER	UNITS	MDL	sample	sample	sample	sample	sample
		Incit	SA 1				aanihia
otal Coliforms	cts/100mls		0				
aecal Coliforms	cts/100mls		a				
aecal Streptococci . Coli	cts/100mls		ō			1	
	cts/100mls		ō				
andard Plata Count (48hrs)	cts/1mi	-	õ				
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Method Detection Limit	ND	=Not Detac	ter				
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APPENDIX E

BACKHOE TEST PITS & GRAIN SIZE & PERC TESTS

Jordel Acres Subdivision

.

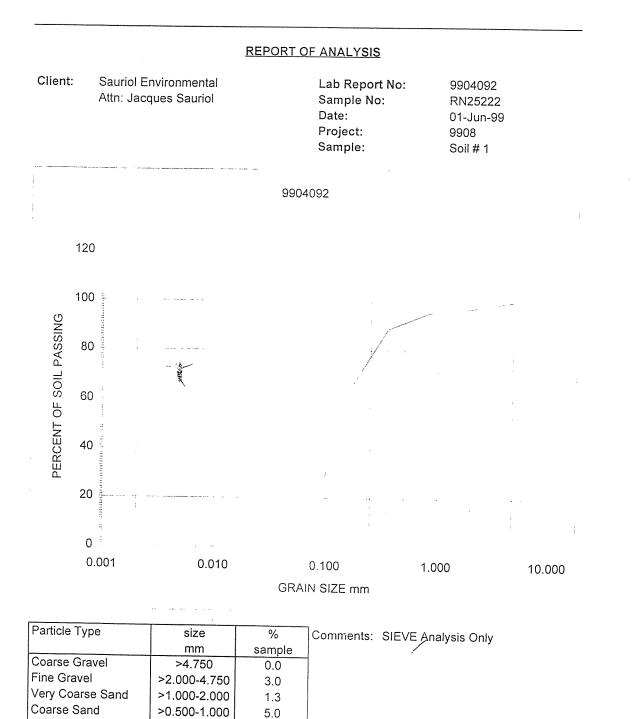
ł

Back hoe test pit May 20 1999

TP1 0 0.1	0.1 1.83	topsoil brown silty clayey till with boulders dry
TP2 0 0.1	0.1 1.83	topsoil brown silty clay dry
TP3 0 0.13	0.13 1.83	topsoil brown silty clay dry
TP4 0 0.1	0.1 1.83	topsoil brown silty clayey till with large boulders dry
TP5 0 0.1 0.61	0.1 0.61 1.83	topsoil brown silty clay grey silty clay (soil sample No 2) water table 0.91m
TP6 0 0.1 0.61	0.1 0.61 1.83	topsoil brown silty clay grey silty clay water table 1.68m
TP7 0 0.1 0.61	0.1 0.61 1.83	topsoil brown silty clay grey silty clay water table 1.68m
TP8 0 0.13	0.13 1.83	topsoil brown silty clay water table 1.52
TP9 0 0.15	0.15 1.83	topsoil brown silty clay dry

TP10 0 0.18	0.18 1.83	topsoil brown sand and gravel dry				
TP11 0 0.08	0.08 1.83	topsoil brown silty clay dry				
TP12 0 0.20 0.91	0.20 0.91 1.83	topsoil brown silty sand grey and brown silty clay dry				
TP13 0 0.20 0.76	0.20 0.76 1.83	sandy topsoil reddish brown silty sand (soil sample No 1) grey silty clay water table 1.52				
TP14 0 0.15	0.15 1.83	topsoil brown sand and gravel with boulders dry				
TP15 0 0.10 0.91	0.10 0.91 1.83	topsoil brown silty sand grey silty sand dry				
TP16 0 0.20 0.71	0.20 0.71 1.83	topsoil brown silty sand grey and brown silty clay dry				
Perco	lation t	ests June 2 1999				
Perc test No 1 silty clay (near TW2) total depth 0.43 m 3 hours saturation perc rate = 30 min / 1.5 cm = 20 min / cm						
perc rate = 30 min / 1.5 cm = 20 min / cm Perc test No 2 till (near TW2) total depth 0.49 m 2 hours saturation perc rate = 15 min / 2.0 cm = 7.5 min /cm						

ACCUTEST LABORATORIES LTD.



14.9

47.8

>0.250-0.500

>0.100-0.250

Medium Sand

Fine Sand

Fines

t: Anils

146 Colonnade Road, Unit 8, Nepean, Ontario K2E 7Y1 Tel:(613)727-5692 Fax:(613)727-5222

REPORT OF ANALYSIS

Client: Sauriol Environmental Attn: Jaques Sauriol

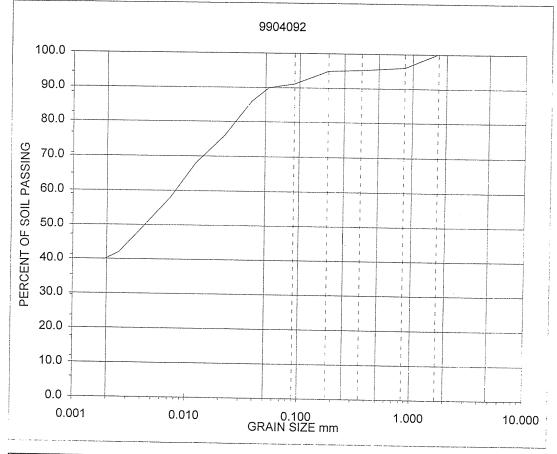
 Lab Report No:
 9904092

 Sample No:
 RN25223

 Date:
 07-Jun-99

 Project:
 9908

 Sample:
 soil 2



Particle Type	size	%	Comments:
	mm	sample	
Coarse Gravel	>4.750	0.0	Ī
Fine Gravel	>2.000-4.750	-0.1	
Very Coarse Sand	>1.000-2.000	3.3	
Coarse Sand	>0.500-1.000	1.3	
Medium Sand	>0.250-0.500	0.5	
Fine Sand	>0.100-0.250	3.5	
Very Fine Sand	>0.050-0.100	2.5	
Silt	>0.002-0.050	49.0	
Clay	<=0.002	40.0	

Analyst:

Anvilson

146 Colonnade Road, Unit 8, Nepean, Ontario K2E 7Y1 Tel:(613)727-5692 Fax:(613)727-5222

Environmental Site Assessment

ESA 1.0 Introduction

We are providing you with an Environmental Site Assessment (ESA) report for the property owned by Mr. Garry Jordan, located on lot 21 Concession 2 in Rideau Township. This environmental opinion was requested by Mr. Richard Lalande of Pri-Tec Construction, to act as supporting documents for the application of a Plan of Subdivision.

ESA 1.1 Purpose of the Study

The purpose of the Phase One ESA is to provide a report that highlights areas of potential concerns regarding environmental liabilities of the property.

ESA 1.2 Methodology

The property was visited with the owner Mr. Garry Jordan on the week of June 7 1999. The source of information described in the present document was provided from conversations with Mr. Jordan, our observations during this site visit and pertinent information from archives, including historical air photography. Local geological maps were also reviewed. An Environmental Screening Questionnaire is attached in Appendix. No boreholes for the purpose of detailed site characterization (i.e. Phase Two) were conducted during this survey.

The site was checked for Polychlorinated Biphenyls (PCBs) and for Urea Formaldehyde Foam Insulation (UFFI). We looked for stained soils and evidence of storage tanks, and waste management on site.

The Court House Archives provided the registry of previous owners of the property. No insurance plan or fire records were available. The former coal gasification plants and landfill surveys (Interra) report were out of bound for the study area.

ESA 1.3 Site Description

The property has ca. 55 Ha in surface area, and is located on Roger Stevens Road, off New Highway 416, near North Gower.

ESA 2.0 Site History and Setting

A review of the archives indicates historical ownership dating back to 1809. The property has been owned by the Dillon family since 1890. The present owners possess the property since 1984. Copies of the listing of previous owners is provided in Appendix.

ESA 3.0Site ConditionsESA 3.1Physical Setting of the Property

There are four significant structures on the property, all mainly located in the center of the land.

The house is a two storey dwelling, and is likely a century old. The building appears to be concrete block foundation with brick walls, with an attic and shingle roof. A basement is present below the main building, with no sump. The house is heated by electric base boards. There was no evidence of previous heating system (i.e. heating oil or coal). Its water is supplied by a drilled well located in the barn. Its waste water is handled by a septic system likely located to the north of the house. Urea Formaldehyde Foam Insulation (UFFI) which was largely used during the Canadian Home Insulation Program in the 1970's, was not used in this building (personal communication Mr. Jordan). Ozone depleting substances are likely contained in a refrigerator and in an air conditioning system. Because of the age of the building, the occurrence of minor quantities of lead base paints is suspected.

The barn a is wood structure with cracked / fissured concrete floor. Manure spread on the main floor, with manure piles outside the barn on the east side were noted. The second floor is a hay loft. A well of ca. 1961 construction is located in the barn and supplies the house. There may be approximately a dozen fluorescent light fixtures. The relative age of the fixtures suggests a possible concern with the ballast containing PCB oils. No individual ballasts were inspected during this visit. Because of the age of the building, the occurrence of minor quantities of asbestos in ceiling and floor tiles is suspected in the back room.

The tractor shed has a dirt floor with pails of fuel, hydraulic fluids and oils.

The garage has crushed stone floors, and hosts a variety of fuels, solvents, paints and oils in minor quantities. There were evidences of spills under a tarp on the garage floor. An older underground storage tank (UST) is located on the East side of the Garage. The newer above ground storage tank (AST) has 250 gal capacity, and holds diesel. Next to the above ground tank, are two drums of hydraulic fluids, with minor spills near the drums. There was no evidence of herbicide or pesticide storage on the property. Spraying of the fields are currently contracted out. The historical storage of these chemicals are unknown.

In addition to the old drilled well, there are two old dug wells on the property. Presently the property is serviced by aerial services of Hydro and Bell. Storm water is managed by road side ditches and a tributary of Roger Stevens Creek.

The surface topography is approximately at 90 m geodetic. Surficial Geology consists of a relatively thick glacial till on the hills, overlain by marine clay in flats, and sand over clay on the eastern part of the property. The bedrock does not outcrop and consists of dolomite of the Oxford Formation. The till hills are naturally well drained and the clay flat have enhanced drainage by drain tiles. There was no evidence of recent fill imported on the property, even along the recent Highway 416 construction, on the East of the property.

Cash Crop Fields likely have a history of herbicide and pesticide spreading activities.

ESA 3.2 Previous Landuses of the Study Property

Based on the airphoto coverage, the property's previous landuses were identical to the present one. Agricultural activities have been the dominant landuse of this property.

ESA 3.3 Landuses of Nearby Properties

The property is bounded as follows: North: Roger Stevens road East: Highway 416 South: Agricultural Fields / wood lots West: Agricultural Fields and a few private dwellings

ESA 4.0 Environmental Situation of the Study Property

It appears that for the last 200 years, the main landuse of the property has been agricultural. Concerned environmental products handled on the property include hydraulic and engine oils, diesel fuel, pesticides and herbicides. Evidences of spills of engine waste oil and of hydraulic oil were noted in the garage. The competence of the two tanks is questioned. Other minor concerned products on the property may include the presence of the original electric light fixture ballasts containing PCBs for their thermal protection.

ESA 4.1 Opinion

A preliminary review of the environmental situation was completed on the Jordel Acres Proposed Subdivision property, located on Lot 21 Concession 2 Rideau Township. This review noted evidences of spills from concerned products on the property (e. g. waste engine oil and or hydraulic oil). The absence of concrete floor could facilitate the migration of petroleum hydrocarbon contaminants in the subsurface. It is the opinion of the assessor that based on the evidences examined, the property shows some concerns for environmental contamination. With regards to older fixture ballasts, the anticipated numbers (i. e. likely less than 10 old units) would be non-regulated (re: PCBs), and would only require normal acceptable disposal (Andy Lewis MOE). It is recommended that these old ballast fixtures be progressively replaced with new PCB free units. It is understood that the owners which to remove the 2 storage tanks from the property. Soils and groundwater quality control of the excavations should be completed to confirm the cleanness of the subsoil environment.

If a greater level of confidence is required about the status of the perceived risk of subsurface contamination about the 2 storage tanks and the Garage, additional site specific characterization (ESA Phase Two) should be completed at these locations. This could include a drilling program near the two tanks and in the Garage, as well as the sampling of the nearby old drilled well. Analyses should include BTEX and TPH.

ENVIRONMENTAL SCREENING QUESTIONNAIRE,

LIST OF PREVIOUS OWNERS, & AIR PHOTOGRAPHS

Summary of Air Photography

A28051 42 ; 1994 A31480 45 ; 1987 (colour) A24878 194; 1977 A20327 44; 1968

National Air Photo Library

SAURIOL ENVIRONMENTAL INC.

ENVIRONMENTAL SCREENING QUESTIONNAIRE

ESA 5.0 Limitations:

During this study, no control by boreholes, and soil and groundwater samplings was completed. The bulk of the information was obtained from conversations with the present owner, complemented by few historical documents. The site inspection was completed during the week of June 7 1999. Conditions in the future may change with time. No guaranty is provided on future site conditions nor on the quality of soil and groundwater since these were not tested. This study has for objective to reduce the risk, and not necessarily to eliminate the risk, of environmental concerns regarding the potential presence of contaminants which could have a detrimental impact on the property.

Sauriol Environmental Inc. (SEI) warrants that this Phase One Environmental Site Assessment was performed in general compliance with current acceptable practices for environmental site investigations. The report is intended for client use only. Any third party use or reliance are sole responsibility of such third parties. SEI accepts no responsibility for damages suffered by any third party as a results of decision made based on this report. No other warranties are implied or expressed.

Trusting that this letter of opinion is satisfactory.

Yours Truly

Sauriol Environmental Inc.

Jadques Sauriol M. Sc. President

ENVIRONMENTAL SCREENING QUESTIONNAIRE

Project No	9908	_ Location: Nor M. Sower	-		
Inspector:	RF	Date Completed: Wetch	50	7	1399

1.0 RECORDS REVIEW / INTERVIEWS

		Completed	Significant Findings
1.1	Aerial Photographs	ø	
1.2	Fire Insurance Plans	\Box n/a	
1.3	City Directories		
1.4	Interviews	F	
1.5	Ottawa Archives	₽	
1.6	Property Zoning		
1.7	Ottawa Env. Management		
1.8	Topographic Maps	,F	
1.9	Geologic Maps	Ş	
1.10	Landfill Site Inventory		
1.11	Coal Gasification Study	ø	
1.12	Other (specify)		

ENVIRONMENTAL SCREENING QUESTIONNAIRE

1.0 SITE DESCRIPTION & FINDINGS

2.1	Legal Description (22) Gac 2 Riduou
2.2	Current Address Rofer Stovens Arive
2.3	Roll #
2.4	Areal Extent 5.5. I-la
2.5	Zoning
2.6	Current Site Use Agriculture 🖳 Residential 🗆 Commercial 🗆 Industrial 🗆 Other 🗆 Describe:
2.7	Domestic Well (3) Yes & No BLocation HC Strong
2.8	Pits Yes I No ZLocation
2.9	Lagoon Yes D No ZLocation
2.10	Wastewater Yes I No I Location <u>Spolar Spolar</u>
2.11	Topography 2.11.1 Site:
2.12	Drainage Patterns 2.12.1 Surficial: <u>tribe farzes y Rozer Strives Crick</u> 2.12.2 Catchbasins/Manholes: 2.12.3 Ditches: 2.12.4 Streams/Creeks: 2.12.5 Rivers/Lakes: 2.12.6 Other(specify):
2.13	Surface Cover <u>Approximate Area</u> <u>Condition</u>
	2.13.1 Buildings:
	2.13.2 Asphalt/Concrete:
	2.13.3 Gravel: <u>acus Col / lapenon</u>
	2.13.4 Vegetation: $\frac{1}{2} \frac{1}{2} \frac$
2.14	Surface Water <u>Approximate Area</u> <u>Condition</u>
2.15 2.16	Geology 2.15.1 Surficial Geology <u>1,11</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u>
	Approx.area Approx.depth Poss.Staining Material Location Poss. Source
2.17	Stressed Vegetation
	Approx.area Location Possible Cause

 2.18.1 Visual evidence of fill observed on site? Yes □ No ☑ If Yes, describe: 2.18.2 Does fill contain any deleterious material? Yes □ No □ If Yes, describe: 2.18.3 Does fill possess any unusual type of odour? Yes □ No □ If Yes, describe: 2.19 Buildings 2.19.1 Are buildings present on the site? Yes ☑ No □
If Yes, describe: 2.18.2 Does fill contain any deleterious material? Yes □ No □ If Yes, describe: 2.18.3 Does fill possess any unusual type of odour? Yes □ No □ If Yes, describe: 2.19 Buildings 2.19.1 Are buildings present on the site? Yes □ No □
 2.18.2 Does fill contain any deleterious material? Yes □ No □ If Yes, describe: 2.18.3 Does fill possess any unusual type of odour? Yes □ No □ If Yes, describe: 2.19 Buildings 2.19.1 Are buildings present on the site? Yes □ No □
11 Yes, describe: 2.18.3 Does fill possess any unusual type of odour? Yes □ No □ If Yes, describe: 2.19 Buildings 2.19.1 Are buildings present on the site? Yes □ No □
2.19 Buildings present on the site? Yes ☑ No □
2.19 Buildings 2.19.1 Are buildings present on the site? Yes ☑ No □
2.19 Buildings 2.19.1 Are buildings present on the site? Yes ☑ No □
2.19.1 Åre buildings present on the site? Yes \square No \square
If Yes, complete the following:
Size: Estimated Age: $100yrs$ +
Use/Occupancy residence Condition
2.19.2 Construction
Building No. <u>hearse</u>
of Storeys
Underground Parking
Basement Tes
Crawl Space <u>Construction</u>
Roof Construction <u>shingle</u>
Ex. Wall Construction <u>bc.ck</u>
+ sanafe + barn + fractor shed
2.19.3 Heating/Cooling System/Fuel Source
Heating:electral
Cooling: A/c
2.19.4 Have any changes to the heating system occurred? Yes \square No \square \square \square
If Yes, list past heating systems:
Suspect 3.1 or coal.
2.19.5 Describe utilities present on site: a wal Bull Hydro
provide the second state and t

2.20 Are there potential special attention items present (i.e. asbestos, PCSs, ureaformaldehyde foam insulation, ozone depleting substances, radon or electromagnetic radiation?) Yes □ No □ If Yes, complete the following::

Asbestos	Inkity presence	of ten	llos 1	ierl, my	diles
Type of Material Condition	Approx. Quantity Location		with and	Lidos f	, because

If asbestos is suspected has an asbestos survey and management plan been completed? Yes \Box No \square

 PCSs
 Image: Serial No._____

 PCBs present
 Yes
 No
 Serial No._____

 Lamp Ballast
 Approx. Amount: 10-20
 Number inspected: 0
 Image: Number of ballasts the presence of PCBs is suspected: 10-20

 No
 Condensers
 Type: ________Number: ______Serial No.______
 Serial No.______

 PCBs present
 Yes
 No
 Image: Serial No.______

 Ureaformaldehyde Foam Insulation (UFFI)
 Is evidence of foam insulation present?
 Yes
 No

 Useription: ________
 Image: No
 Image: No
 Image: No
 Image: No

	Ozone Depleting Substances (ODS) Description Yes No A/C Units Water Coolers
	Radon Is the bedrock comprises of black shale or granite? Yes □ No □ If Yes, complete the following: Basement Ventilation: Occupants of Basement: Complaints by Occupants:
	Electromagnetic Radiation (EMR) Yes D No
2.21	Describe: Storage Tanks $(\]$ 2.21.1 Is evidence of above ground storage tanks (ASTs) observed on site? Yes $< \Box$ No \Box If Yes, complete the following: <u>Size Tank Material Contents Date of Installation Protection Spill Containment</u>
ı I	Ust????????????????????????????????????
2.22	Waste management waste 2.22.1 Are significant quantities of debris/solid waste on site? Yes D No D If Yes, describe:
	2.22.2 Are any signs of liquid wastes present on site? Yes \Box No \Box
	2.22.3 Is any registerable waste present on site? Yes □ No □ If Yes, describe:
2.23	Material? Chemical Handling 2.23.1 Are chemicals or hazardous materials stored on site? Yes I No I If Yes, describe: Amount Environmental Significance ADJACENT PROPERTIES
3.0	ADJACENT PROPERTIES
3.1	Land Uses 3.1.1. Northwest: Agriculture Aresidential Commercial Industrial Other Describe: ASTs Yes No VSTs Yes No Solid/Liquid Wastes Yes No F Environmental Concerns: No Vo Any basement within 60 m of the site? Yes No Vo
	3.1.2 Southeest: Agriculture ☐ Residential □ Commercial □ Industrial □ Other □ Describe: Some word Lot

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ASTs Yes D No D USTs Yes D No Solid/Liquid Wastes Yes D No Environmental Concerns: مصرم Any basement within 60 m of the site? Yes D No

3.1.3 East:

Agriculture \square Residential \square Commercial \square Industrial \square Other \square e:_______+ $\vdash \square \Downarrow$ Describe: ASTs Yes D No D USTs Yes D No D Solid/Liquid Wastes Yes D No Environmental Concerns: No Any basement within 60 m of the site? Yes D No D

3.1.4 West:

Agriculture . Residential Commercial Industrial Other Describe: ASTs Yes D No D USTs Yes D No D Solid/Liquid Wastes Yes D No D Environmental Concerns:_____ NO Any basement within 60 m of the site? Yes I No I

4.0 OTHER POTENTIAL SIGNIFICANT FEATURES

4.1 Are wetland habitats or other environmentally significant features present on or within 120m of the site? Yes D No

Are there any other environmental concerns? Yes D No 4.2 If Yes, describe:_____

5.0 SUMMARY OF ENVIRONMENTAL CONCERNS:

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6.0 **RECOMMENDATIONS:**

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APPENDIX

LIST OF PREVIOUS OWNERS

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RO711	2 B& 9 B&		848 19JULJ	851 Alexander Wylie etu	x Jeremiah O'Connor		
RO 712				854 John Callaghan etur	Villiam Hedgins	8.2	
RO1026	3 Will		1		I John Phelan	I A AND AND AND AND AND AND AND AND AND A	
RO 24914			55 5Eov.1		Cormack McGuire	I.	
RO 24915	- B&		65 16Mar.10	0 40TH013	Daniel O'Connors	R. f of S.f	
RO 24916		3Mar.16	65 161 ar.1	365 John Phelen etur 865 Daniel O'Connor	Daniel O'Connora	R. J OT H. J.	
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-1446			14 13207.18	· · · · · · · · · · · · · · · · · · ·	Daniel O'Connor.	- F. F of S. F, 50 Δ.	×
1596-		18807,168			George D. Euro		
-1517	Chi D. H.	1	1,27 10, 10		Dan'1. 0'Connor	300 Ho. 1149	
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3825	B & S.	18Apl.1890	285ep.1900	Russell Andrews & w.	Cormiok KoCuize		1 of 2. 2 lot 21.
· 4092	Will	4Cct.1902	7jan.1903	John Dillon	John Dillon		or W. 2. A. C. L.
	н п	Π		17 E	Eichard E. Dillon Samuel C. Dillon	R. or W. 2 lot 21.	
п	n	7	я , п	π π	Vergaret Dillon		
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-71			7	C #	Ellen J. Hyland		• • • • • •
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TOWN	SHIP OF	NORÍTE	I GOWER,	. Lot No. 2/	Concession R.
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JCONTINUED FROM PRECEDING PAGE - Chen - Market -bontimed from Page 104 Book B EXPLANATIONS A.O.L.—Among other Lands, N.R.F.—Nit Keylstered is Fult. S.I. –See Instrument. Suhj.—Subject. Township of North Gower, Lot No. 21 Concession 2 DATE OF REGISTRY NUMBER OF INSTRUMENT INSTRUMENT ITS DATE GRANTOR QUANTITY OF GRANTEE CONSIDERATION REMARKS N.G.11264 Grant 14 Nov 1961. 15 Nov. 1961. Executors Will of Richard H. S. Dillon. \$1.00 W1/2 Let 21 even or W1 Richard H. Dillon Lat 22. see moto Gib 12.700 \$5. Dee mist. 4259 Filed This 11th Day Ung. U. A. 1965. pesit # 50 July 1865 25 any 1965 Furm Gredit Corps Bulta EK_ LE -Marjoin Hy malal 9298 N.G. 13989 Disignation 39 Can 196931 Can 1969 Lept of Highways P-6074 -2,0 Re 67 attac lev Nelosit . # 142157 filed tris 6th Nay of Oct. a.D. 1511. he Hyland , Br sky. Re: Road Widening . Windell 41 terno land 2546-1975 1975 Corporation . Sharm Creata scharging 1976 Corporation true lan FORWARD TO NEXT PAGE Ŕ ۲. 1.4.1.2

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	MINISTRY OF CONSUMER AND COMMERCIAL RELATIONS	PROPERTY DESCRIPTION: PROPERTY REMARKS: ESTATE/QUALIFIER	ACLUDES ALL	■ THIS ABSTFACT INCLUDES ALL INSTRUMENTS AND DOC ■ FOR THE PREVIOUS ABSTRACT SEE ABSTRACT BOOK ==	1984/06/04	10/20/6661			NOTE: NOTE: NOTE:	
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=	5-21-	INSTRUMENT	DATE OF	REGISTRATION				
ų .	has	· ·			GRANTOR	GRANTEE	CONSIDERATIO	LAND AND REMARKS
		MED MAR 1 1	- 5500 (Ja re inot #	n. <i>Ja. 1981.)</i> 9227.	being a reference	plan, being pt lot	21. 20	sts 1-3
	2365	×8 Q.C.	1981	YEAR MONTH C 81 07 1	Detricia M. Hyland	Werdell T. Hyland	\$109	El/2 of Jot 21. See tax affidava
v.	2372. 24023	5 Grant Grant		81 07 11 YEAR MONTH DA 81 07 1	Y.	The Regional Municipal- ity of Ottawa-Carleton	\$1,00	Pl. lot 21 desig as pt. Lon 5P. See tax afficiant See Inst.
	4024	Mortgage				Jotina Developments Ltd.,	\$104,157.0	D. Rt. of lot 21, being pt. 3 on 5R-55 Consent of planning board. See inst.
1	vergied b	NS24548h	Dep Land Neg CO	6/06/84 MONTH YEA	R. Joseph Palmerio	- Kondell T. Hyland	\$54,000.00	Pt. of Lot 21, being pt. 3 on 58-550
 D	-5130	R-Plan		13 11 81				Seg inst. Part - Re: Parts 1,2,3 & 4 Re: Inst No
F	2151 -	R-Plan	ан.	27 11 8				9227, NS 123725 E NS 124023 - OL. Part. Re. part 10. O.L.
i ji	42459	Cert. of A	proval	05 02 82	HIC			Re: inst. no. 142157.
	42495 	Expropriatio	n Plan	05 02 82		Mrc		Pt. OL re: pts 2,3 ⁴ Pt. re: pts 1 and 2 ⁴ / _A re: inst. # 9227
	33990	By-Law. 31		24 03 83	The Regional Municipality		A	by-law to assume for public use
	•		e e e come		of Ottawa-Carleton		8	establish as common & public ighway certain lands to become
		· · · · ·	· .			a de la companya de	1	t. of the Regional Rd. System,
-		Grant			and a second	· · · · · · · · · · · · · · · · · · ·		eing pt. & OL, being pt. 2 on R-5500
			· · · · · · · · ·	06 06 83	Jotina Developments Ltd.	PALMERIO, Joseph SJ PALMERIO, Tecia	ł	., being pt. 3 on 5R-5500
•		······································	·	• •		JT	ex	ve & except pt. 1 on propriated plan NS 142495, e Tax Affidavit.
2	4762 -		en en en	· · · · · · · · · · · · · · · · · · ·	Estate of DILLON, Richard HD	DILLON, Barbara H. #1		1/2 + 0: L. see tax affidavit
ند. مع	<u>~</u>	Deposit			See Deposit NS 235247		P 1	-0.6 as in 4092
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AATION IDER	INSTRUMENT	DATE OF INSTRUMENT	REGISTRATION	GRANTOR	GRANTEE	CONSIDERATIO	N LAND AND REMARKS
1249	b Grant		04 06 84	DILLON, Barbara H.	JORDAN, Garry H JORDAN, Nicole L	\$225,00	2 [™] Rear or W1/2. O.L. Save and except pts.
≥491	Mort		04 06 84	JORDAN, Garry H JORDAN, Nicole L.	Scotia Mortgage	#63.000.	
4516	Grant		18 06 84	PALMERIO, Joseph PALMERIO, Tecla	DALY, John S. DALY, Nellie E. JT	\$100,000	
	Order In Co	uncil	02 11 88	H.M. The Queen (Ontario)			Pt. OL.
345	Order in	Council	30 08 89	H.M. The Queen Ontario			Revokes all the 1969 Highway 416 designation.
	harge		92-08-14	JORDAN, Garry H.	Royal Bank Of Canada	\$160,000,00	
367	Charge				N735610 64.96 DED 3¥# AD€T DEP LAND REG 26	01 25	Pts desc'd, OL.
			13 14 08	JORDAN, Garry H. JORDAN, Nicole Lise	Bank of Montreal	200,000	Bear or Wile. Save except pt. desc.d.
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APPENDIX F

ENVIRONMENTAL SITE ASSESSMENT





IN HER MATECAA THE UNEEN IN BIGHT OF CANADA DEDARTMENT OF ENERGY MINES AND BESONDERES 1



NAPL REPRODUCTION CENTRE - ENERGY, MINES & RESOURCES - CANADIAN GOVT. COPYRIGHT

