





Petrie's Landing I - Towers 3 to 5

Transportation Impact Assessment Strategy Report





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Transportation Impact Assessment Strategy Report

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Strategy Report

1. SCREENING FORM

The screening form was prepared for the subject development and included as part of the subsequent report. The screening form confirmed the need for a Transportation Impact Assessment (TIA) based on the Trip Generation, Location and Safety triggers, given that the proposed development consists of three towers with a total of 806 additional condominium units, located at a lot bounded to the south by OR-174 (speed limit of 90 km/h) and partially within the Trim TOD zone. The screening form is provided in Appendix A.

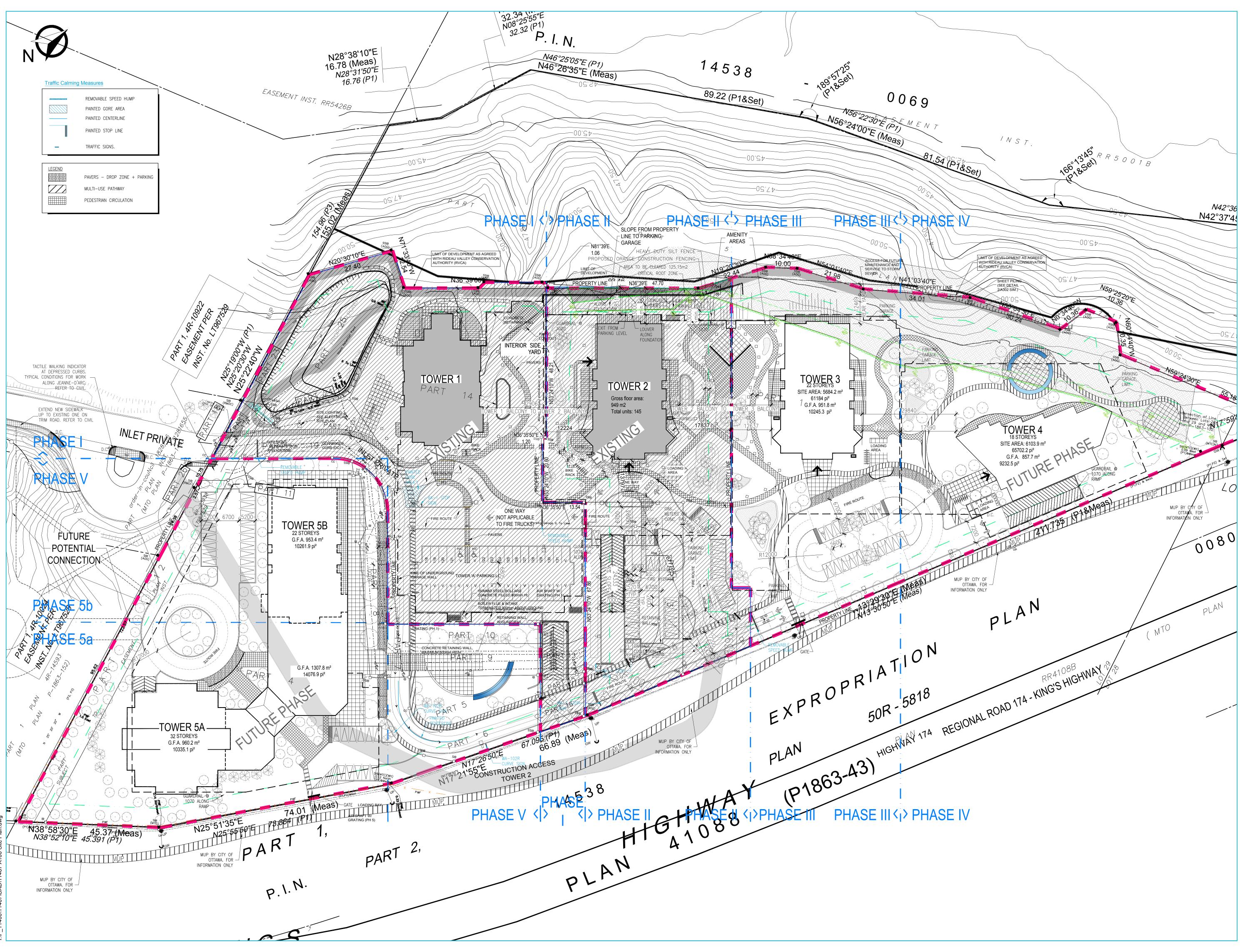
2. DESCRIPTION OF PROPOSED DEVELOPMENT

2.1. PROPOSED DEVELOPMENT

The proposed Brigil's residential development is located at 8900 Jeanne d'Arc Boulevard (formerly 8911 North Service Road). The site is in Ward 1, Orléans, and is designated as R5 Residential Fifth Density Zone according to the Part 6, sec. 163-164 of the Zoning By-Law No. 2008-250. Currently the site consists of a 15-storey tower containing 89 condominium units (Tower 1), approximately 34 surface parking spaces and a second tower in construction that will consist of 145 units (Tower 2). The site's local context is illustrated in Figure 1.



Brigil is proposing to proceed with the construction of Towers 3 to 5 within the planned Petrie's Landing I development. For this assessment, horizon years have been assumed to be the year 2022, representing interim build-out, year 2024, representing full build-out and occupancy of all towers, and the year 2029, representing the plus five years horizon. Tower 3 will consist of 22 storeys and 201 units. Tower 4 will consist of 18 storeys and 137 units. Tower 5A and 5B will consist of 32 storeys, 286 units, and 22 storeys, 182 units, respectively. Access to site will be provided via the existing phases of the development through Jeanne D'Arc Boulevard. The site plan is illustrated in Figure 2.



² 11400\11467\CAD\11467 A100 Site Plan.dwg

NOTES GÉNÉRALES General Notes

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OUVRAGE Project

 PETRIES LANDING I -DOWER 3

 EMPLACEMENT Location OTTAWA, ON
 NO PROJET No. 11467

 NO
 RÉVISION

 NO
 RÉVISION

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 2018.06.01

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SITE PLAN CONCEPT



3. EXISTING CONDITIONS

3.1. AREA ROAD NETWORK

Ottawa Regional Road 174 (OR 174) is an east-west City-owned freeway, which extends from HWY 417 in the west to Trim Road and continues east. Within the study area, OR 174 has a four-lane cross section and auxiliary turn lanes are provided at its intersection with Trim Road. The posted speed limit within the study area is 90 km/h.

Trim Road is classified as an arterial roadway south of OR 174 and as a major collector roadway between OR 174 and Jeanne D'Arc Boulevard (formerly known as North Service Road). North of Jeanne D'Arc Boulevard, Trim Road is classified as a local roadway. Within the study area, Trim Road has a two-lane cross section, a concrete sidewalk on the west side, a multi-use pathway on the east side and one curb cycle lane on each direction. The posted speed limit is 50 km/h.

Jeanne D'Arc Boulevard is a major collector roadway west of Trim Road, with a posted speed limit of 60 km/h. East of Trim Road, Jeanne D'Arc Boulevard (formerly known as North Service Road) is classified as a local roadway with an unposted speed limit assumed to be 50 km/h. Within the study area, Jeanne D'Arc Boulevard has a two-lane cross section.

3.2. PEDESTRIAN AND CYCLING NETWORK

The pedestrian facilities include a concrete sidewalk and a multi-use path on the west and east side of Trim Road, respectively, north of OR 174. A multi-use pathway also exists along the north side of Jeanne D'Arc Boulevard, west of Trim Road.

According to the City's 2013 Official Cycling Plan, Trim Road and Jeanne D'Arc Boulevard (west of Trim Road) are classified as spine routes. Currently, paved shoulders and an off-road multi-use pathway exist along Jeanne D'Arc Boulevard, west of Trim Road. On Trim Road, one bicycle-lane is provided on both sides of the road south of Jeanne D'Arc Boulevard. Figure 3 depicts the existing area of study cycling network.



Figure 3: Area Cycling network

3.3. TRANSIT NETWORK

Transit service within the vicinity of the site is currently provided by OC Transpo Routes #22, 38, 91, 95, 122, 221. Bus stops for Routes #38 and #122 are provided along Jeanne D'Arc Boulevard, approximately 350 m west of the Trim/Jeanne D'Arc intersection. Additional stops are provided for Route #122 on Trim Road, approximately 100 meters south of the

Trim/Jeanne D'Arc intersection as depicted in Figure 4. Bus stops for Routes #22, 91, 95 and 221 are provided at the existing OC Transpo 'Park and Ride' lot, approximately 250 m south of the Trim/OR 174 intersection.



Figure 4: OC Transpo Existing Bus Stops

Regular Routes #91, 95 and 122 provide frequent all-day service. Routes #22, 38 and 221 provide weekday morning and afternoon peak hour service only. Frequency of transit service near the site is approximately three to four buses pear hour, with higher frequency at the OC Transpo 'Park and Ride' lot.



www.octranspo.ca, accessed April 26th, 2018.

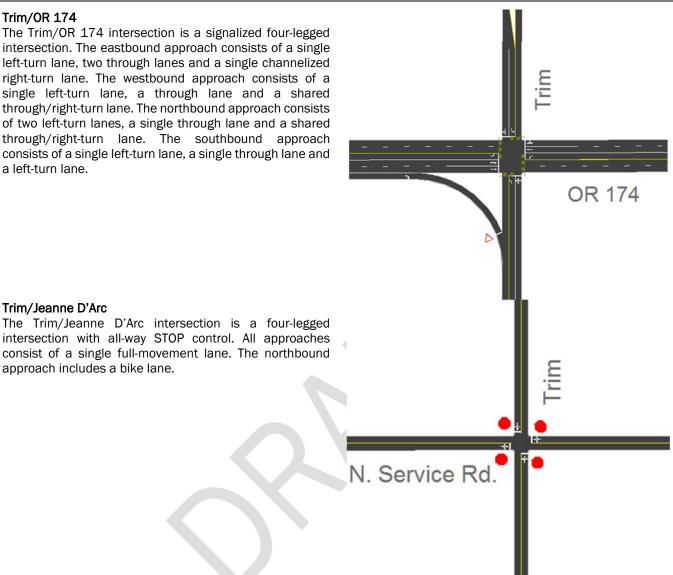
3.4. EXISTING STUDY AREA INTERSECTION

Trim/OR 174

Trim/Jeanne D'Arc

approach includes a bike lane.

The Trim/OR 174 intersection is a signalized four-legged intersection. The eastbound approach consists of a single left-turn lane, two through lanes and a single channelized right-turn lane. The westbound approach consists of a single left-turn lane, a through lane and a shared through/right-turn lane. The northbound approach consists of two left-turn lanes, a single through lane and a shared through/right-turn lane. The southbound approach consists of a single left-turn lane, a single through lane and a left-turn lane.



3.5. EXISTING INTERSECTION VOLUMES

The existing peak hour traffic volumes (illustrated in Figure 6 below) were obtained from the City of Ottawa and from counts performed by Parsons in 2018. The full traffic volume counts are provided in Appendix B.

Figure 6: Existing Peak Hour Traffic Volumes

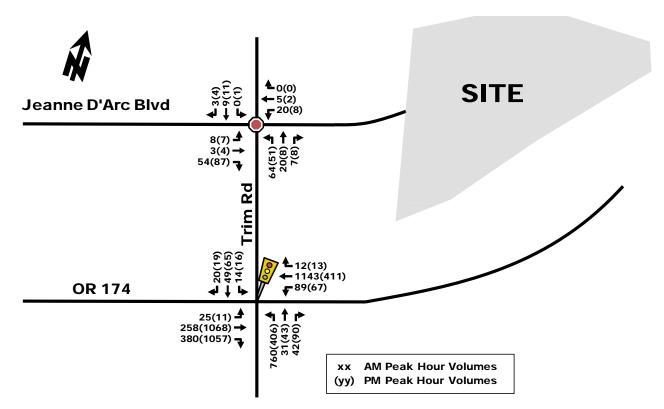


Table 1 provides a summary of the existing traffic operations at study area intersections based on the SYNCHRO (V9) traffic analysis software. The subject intersections were assessed in terms of the volume-to-capacity (v/c) ratio for signalized intersections, delay (s) for stop-controlled and roundabout intersections, and the corresponding Level of Service (LoS) for the critical movement(s). The subject intersections 'as a whole' were assessed based on a weighted v/c ratio or delay, and the SYNCHRO model output of existing conditions is provided within Appendix C.

| | Weekday AM Peak (PM Peak) | | | | | |
|---|---------------------------|--|----------|--------------|------|------------|
| Intersection | Critical Movement | | | Intersection | | |
| | LoS | LoS max. v/c or avg. delay (s) Movement | | Delay (s) | LoS | v/c |
| Jeanne D'Arc/Trim (unsignalized) | A(A) | 7.8(7.7) | NB(NB) | 7.5(7.3) | A(A) | - |
| Trim/OR 174 | D(D) | 0.89(0.82) | NBL(EBT) | 39.4(27.3) | D(C) | 0.84(0.75) |
| Note: Analysis of signalized intersections assumes a PHF of 0.95 and a saturation flow rate of 1800 veh/h/lane. | | | | | | |

| Table 1: Existing Performance at Study Area I | ntersections |
|---|---------------|
| Table 1. Existing renormance at Study Area i | 1110130010113 |

As shown in Table 1, study area intersections 'as a whole' are currently operating at an acceptable LoS 'D' or better during the weekday peak hours. With regard to the 'critical movements' at study area intersections, they are operating at an acceptable LoS 'D' or better.

3.6. EXISTING ROAD SAFETY CONDITIONS

Collision history for study area (2012 to 2016, inclusive) was obtained from the City of Ottawa. All collisions were registered at the Trim Road/OR 174 intersection. The majority (79%, or 55) of collisions involved property damage, 20% or 14 collisions involved non-fatal injuries, and 1 resulted in a fatal injury. The collision that resulted in a fatal injury involved a

vehicle that ran off road while heading in the east direction on February 2014. The road conditions were dry and the environment was clear.

Regarding the type of collision, rear ends accounted for 74% (or 51 collisions) of collisions, turning movements and sideswipe accounted for 9% (or 6 collisions) each, and angled, single vehicle other and other accounted for 3% (or 2 collisions) each. Majority of the rear end collisions took place on OR 174 in the westbound direction and in the eastbound direction involving vehicles slowing down and going ahead. Nine (9) rear end collisions were registered on Trim Road in the northbound direction. Turning movement collisions mainly involved EB vehicles turning left and WB vehicles going ahead during dark conditions. Given the geometry of OR174, high-speeds may be the cause of the collisions at this intersection. Currently, there are "Prepare to Stop when Flashing" signals on OR 174 approximately 600 meters to the west of Trim Road and 600 meters to the east of Trim Road.

Regarding Trim Road at Jeanne D'Arc Boulevard, no collisions were registered between 2012 and 2016.

A standard unit of measure for assessing collisions at an intersection is based on the number collisions per million entering vehicles (MEV). The reported collision rate for Trim Road at OR 174 was 1.11 MEV.

No additional collision mitigation measures are recommended at this time. The stop ahead warning sign and flashers have been provided on either side of the intersection on OR 174, and the intersection has recently been reconstructed. The effects of these improvements should be documented prior to any additional changes by the City. It is anticipated that the grade separation of this intersection in the future will address the collisions along OR-174.

The collision data and related analysis is included in Appendix D.

3.7. EXISTING AREA TRAFFIC MANAGEMENT MEASURES

Within the area of study, the following traffic management measures are identified:

- Two "Prepare to Stop when Flashing" signals on OR 174, each approximately 600 meters to the west of Trim Road and 600 meters to the east of Trim Road; and,
- One High Deer Collision Corridor signal on OR 174 westbound approximately 300 meters to the west of Trim Road.

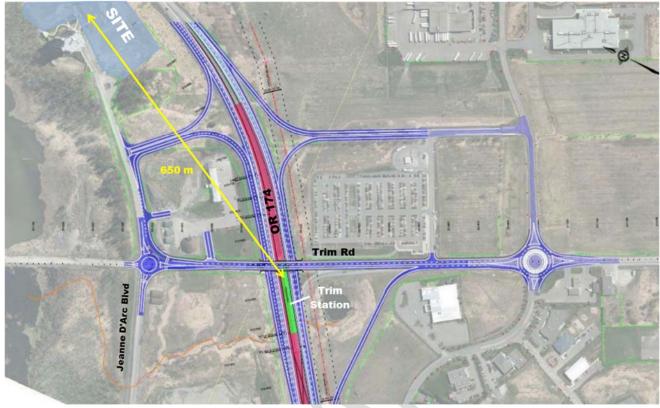
4. PLANNED CONDITIONS

4.1. PLANNED STUDY AREA TRANSPORTATION NETWORK CHANGES

OR 174 Light-Rail

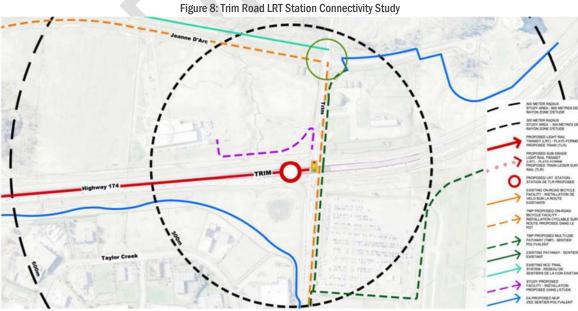
Schedule D of the Official Plan – Rapid Transit and Transit Priority Network identifies the light rail Confederation Line east extension to Trim Road. According to the Confederation Line East Functional Design Report, the LRT east extension includes a grade separated crossing on Trim Road at OR 174 and a light-rail station on OR 174 at Trim Road, with opening year 2022. Figure 7 illustrates the planned LRT station and interchange at Trim road. Other planned adjacent network changes include a roundabout on Trim Road at Jeanne D'Arc Boulevard and access ramps from Jeanne D'Arc to/from OR 174, directly west from the subject site. It is noted that the subject site is located approximately 650 m from the future Trim Road LRT Station and is therefore considered to be within the Trim TOD area.

Figure 7: Confederation Line East Extension Interchange at Trim Road



http://www.stage2lrt.ca/wp-content/uploads/2015/09/Doc 2 --- Confederation Line East Functional Design Report.pdf, accessed May 10th, 2018.

Figure 8**Error! Reference source not found.** illustrates planned connectivity features at Trim Road light-rail station, as presented by the City of Ottawa during a connectivity workshop held in August 2016. A planned City-owned multi-use pathway along Jeanne D'Arc Boulevard, east of Trim Road, that heads south and borders the subject site along the southern edge is noted.



http://www.stage2lrt.ca/resources/, accessed May 10th, 2018.

OR 174 Widening

An Environmental Assessment for the potential widening of OR 174 was conducted by the Townships of Prescott-Russell/City of Ottawa. The widening of OR 174 to six-lanes from Hwy 417 to Trim Road and to four-lanes from Trim Road to the City boundary is identified as a road project in the current 2013 City of Ottawa Transportation Master Plan. However, the widening of OR 174 is not identified as part of the Affordable Network Plan within the TMP. Therefore, the road widening of OR 174 east of Trim Road is unlikely within the foreseeable future.

Cycling Network

Within the Ottawa 2013 Cycling Plan, both Trim Road north of Jeanne D'Arc Boulevard and Jeanne D'Arc Boulevard east of Tim Road are identified as major cycling pathways. To the north, the planned pathway will extend along Trim Road to Petrie Island Beach and to the east, the planned MUP will extend along Jeanne D'Arc Boulevard to Cardinal Creek, bordering the subject site along the southern edge. Trim Road is classified as a Spine route south of Jeanne D'Arc Boulevard.

Jeanne D'Arc Culvert Renewal

According to Ward 1 Construction Map, culvert renewal is planned along Jeanne D'Arc Boulevard, west and east of Trim Road for the period 2018 - 2021.

Petrie's Landing Traffic Calming Concept

Within the TIS for Tower 2 of the Petrie's Landing I Development (prepared by Parsons), an addendum traffic calming plan was prepared. The traffic-calming plan has been developed with the intention to be implemented during the construction of Tower 2, and subsequently as each additional Tower is completed. It is noted that the subject site plan is generally consistent with the traffic calming plan. The aforementioned traffic calming plan is included in Appendix E.

4.2. OTHER AREA DEVELOPMENTS

4.2.1. PETRIE'S LANDING I - 2013 TIS

Delcan (now known as Parsons) prepared a Transportation Impact Study on December 2013 to support the Site Plan Application for Towers I, II, III, IV and a retirement residence within the subject site, for a total of 845 high-rise residential condominium units. The horizon years included in the assessment were 2018 (representing full occupancy of Tower 2) and 2024 (representing full occupancy of Towers III and IV). The proposed towers were projected to generate 297 and 285 veh/h during the weekday morning and afternoon peak hours. A traffic calming plan was prepared as addendum to the TIS and is included as Appendix E. Currently, Tower 1 has been built and Tower 2 is under construction. Vehicle volumes generated by Tower 2 are included in Appendix F.

4.2.2. PETRIE'S LANDING II

Brigil is proposing the construction of a residential development consisting of approximately 300 to 430 residential units. The proposed Petrie's Landing II is located south of Jeanne D'Arc Boulevard, approximately 1.5 km west of the subject site, as illustrated in Figure 9. Currently, over 60% of the development is completed (phases 1 and 2). The projected two-way vehicle trips for this proposed residential development are approximately 150 veh/h during both peak hours. Vehicle volumes generated by this development at study area intersections are included in Appendix F.

4.2.3. PETRIE'S LANDING III

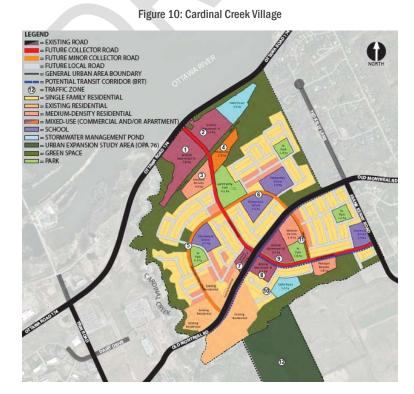
Brigil is proposing the construction of a mixed-use development consisting of approximately 370,000 ft² of office, 23,000 ft² of retail and up to 790 residential units. The proposed Petrie's Landing III is located south of Jeanne D'Arc Boulevard, approximately 1 km west of the subject site, as illustrated in Figure 9. The projected two-way vehicle trips for this proposed mixed-use development is approximately 660 and 685 veh/h during the morning and afternoon peak hours, respectively. Vehicle volumes generated by this development at study area intersections are included in Appendix F.

Figure 9: Petrie's Landing I, II and III Concept Plan



4.2.4. CARDINAL CREEK VILLAGE

Tamarack Homes is currently constructing a 1,446-unit subdivision and a 430,000 ft² shopping centre, south of OR 174 and east of Cardinal Creek, as illustrated in Figure 10. The Transportation Impact Study (prepared by IBI Group) projected approximately 1,460 veh/h and 2,619 veh/h by horizon year 2031 (full build-out) during the morning and afternoon peak hours, respectively. Vehicle volumes generated by this development at study area intersections are included in Appendix F.



4.3. TRANSIT

As mentioned previously, transit is served within the area with bus stops for routes #38 and #122 on Jeanne D'Arc Boulevard, approximately 680 m from the site; for route #122 on Trim Road approximately 500 meters from the site; and bus stops for routes #22, 91, 95 and 221 on Trim Road at the existing OC Transpo 'Park and Ride' lot, approximately 820 m from the site.

4.4. NETWORK CONCEPT

The Bilberry Creek Screenline, SL-45, is in close proximity to the proposed development, capturing east-west traffic on OR 174 and Bilberry Creek. The Frank Kenny Screenline, SL-46, is also in close proximity to the proposed development, capturing east-west traffic on OR 174 and the projection of Ted Kelly Lane. It is not anticipated that this development will have significant impacts on these Screenlines.

4.5. INTERSECTION DESIGN

The proposed site will access the adjacent road network through Jeanne D'Arc Boulevard at Trim Road. The strategy analysis will review and document the access requirements if it is required.

5. TIME PERIODS

Given the land use of the proposed development, the weekday morning and afternoon peak hours will be analyzed.

6. HORIZON YEARS

The subject site is assumed to develop at a 2 year per tower rate for the remaining Petrie's Landing I development, given the current market demand. Therefore, for the purposes of this analysis the site full-occupancy date is assumed to be year 2024. The plus five years horizon will be analyzed for year 2029. An interim 2022 horizon is analyzed to account for transportation demand projections for Towers 3 and 4, prior to the completion of the LRT extension and station at Trim Road.

Considering construction trends of the past years, the following phasing is assumed for other area developments:

Year 2022

- Petrie's Landing I Towers 3 and 4 built;
- Petrie's Landing II 100% built;
- Petrie's Landing III 30% built; and,
- Cardinal Creek 40% built.

Year 2024

- Petrie's Landing I 100% built;
- Petrie's Landing II 100% built;
- Petrie's Landing III 50% built; and,
- Cardinal Creek 60% built.

Year 2029

- Petrie's Landing II 100% built;
- Petrie's Landing III 100% built; and,
- Cardinal Creek 90% built.

7. EXEMPTIONS REVIEW

Based on the foregoing analysis and review of the existing conditions, it is recommended that any future work within the context of this TIA excludes the following modules and elements summarized in Table 3.

Table 2: Exemptions Review Summary

| Module | Element | Exemption Consideration |
|----------------|-------------------------------|---|
| 4.2 Parking | 4.2.2 Parking Spillover | The subject site is located within a 800 meters walk of the planned Trim Road LRT transit station, as depicted in Figure 20. Considering Sections 101(5)(d), 101(5)(e), 102(5), 103(1) and 103(2) of the Zoning By-Law 2008-250-Consolidation-Part 4, the subject development is required to provide 640 parking spaces for residents, 131 parking spaces for visitors and 44 parking spaces for commercial uses, for a total of 796 parking spaces. With a proposed total of 864 underground and surface parking spaces, the subject development is meeting City requirements. |

In addition to the above recommendations of the Exemptions Review, the following exemptions are also proposed for both Step 3 – Forecasting and Step 4 – Analysis and are summarized in Table 3.

| Table 3: Additiona | I Recommended | Exemptions Summary |
|--------------------|---------------|--------------------|
|--------------------|---------------|--------------------|

| Module | Element | Exemption Consideration |
|---|-------------------------------|--|
| 4.4 Access | 4.4.2 Intersection Control | Site access will operate at Jeanne D'Arc Boulevard Dead-End and will not require an intersection screening for a signal or roundabout. |
| Intersection Design | 4.4.3 Intersection Design | Site access will operate at Jeanne D'Arc Boulevard Dead-End and will not require an intersection screening for a signal or roundabout. |
| 4.6 Neighbourhood Traffic Management | All Elements | Given the site's location relative to the existing road network, no cut through traffic is expected. |

Next sections will review the trips generated by the subject development and compare them to the total volume along Trim Road and OR 174 to assess future network operations.

8. DEVELOPMENT GENERATED TRAVEL DEMAND

8.1. TRIP GENERATION AND MODE SHARES

8.1.1. TRIP GENERATION

Appropriate trip generation rates for the proposed development were obtained from the City's TRANS Trip Generation – Residential Trip Rates (Table 6.3 of the TRANS Trip Generation Study) for suburban apartments and are summarized in Table 4.

Table 4: TRANS Recommended Vehicle Trip Generation Rates for Residential Land Uses with Transit Bonus

| Land Use | Data Source | Trip Rate | | | |
|----------|-----------------|-----------|---------|--|--|
| Lanu Use | Data Source | AM Peak | PM Peak | | |
| Tower 3 | TRANS (ITE 232) | 0.46 | 0.46 | | |
| Tower 4 | TRANS (ITE 232) | 0.46 | 0.46 | | |
| Tower 5A | TRANS (ITE 232) | 0.46 | 0.46 | | |
| Tower 5B | TRANS (ITE 232) | 0.46 | 0.46 | | |

Using the TRANS Trip Generation rate, the total amount of vehicle trips generated by the proposed apartment units were projected and the results are summarized in Table 5. From the information provided, it is our understanding that retail uses to be accommodated within Tower 5, will be small scale and oriented to serve retirement units within the same tower. Therefore, they are not expected to impact the adjacent transportation network.

| Land Use | Units | AM Peak (veh/h) | | PM Peak (veh/h) | | | |
|----------|--------|-----------------|-----|-----------------|-----|-----|-------|
| Lanu Use | | In | Out | Total | In | Out | Total |
| Tower 3 | 201 du | 25 | 67 | 92 | 53 | 39 | 92 |
| Tower 4 | 137 du | 17 | 46 | 63 | 36 | 27 | 63 |
| Tower 5A | 286 du | 36 | 96 | 132 | 76 | 56 | 132 |
| Tower 5B | 182 du | 23 | 61 | 84 | 48 | 36 | 84 |
| | Total | 101 | 270 | 371 | 213 | 158 | 371 |

Table 5: TRANS Vehicle Trip Generation

8.1.2. MODE SHARES

Considering the location of the site within Trim TOD area and the planned Light Rail East extension discussed in section 4.1, which will provide Light Rail service within the vicinity of the site, it is anticipated that transit ridership will increase once the LRT starts operation in 2022. To reflect conditions before LRT, Orleans' modal shares obtained from the 2011 Trans O-D Survey have been applied to phases completed before 2022 (Towers 3 and 4). Using the TRANS Auto Trips projected in Table 5 and the modal share percentages from Orleans of the TRANS 2011 O-D Survey, the 2022 total people trips for the proposed development were projected and are summarized in Table 6.

| Table 6: Site Trip | Generation - | 2022 | (Towers 3 and 4) | |
|--------------------|--------------|------|------------------|--|
| | | | | |

| Travel Mode | AM Mode | AM Mode AM Peak (persons/h) | | PM Mode | PM Peak (persons/h) | | | |
|-----------------------|------------------|-----------------------------|-----|---------|---------------------|-----|-----|-------|
| | Share | In | Out | Total | Share | In | Out | Total |
| Auto Driver | 55% | 42 | 113 | 155 | 64% | 89 | 66 | 155 |
| Auto Passenger | 10% | 7 | 20 | 27 | 21% | 28 | 22 | 50 |
| Transit | 35% | 27 | 73 | 100 | 15% | 20 | 17 | 37 |
| Non-motorized | 0% | 0 | 0 | 0 | 0% | 0 | 0 | 0 |
| Total People Trips | 100% | 76 | 206 | 282 | 100% | 137 | 105 | 242 |
| Total 'New' Tower 3 a | and 4 Auto Trips | 42 | 113 | 155 | | 89 | 66 | 155 |

To reflect conditions once the LRT is in service (post-2022), modal share percentages were adjusted to reflect the City of Ottawa transit share targets for TOD areas. Using the TRANS Auto Trips projected in Table 5 and the TRANS 2011 O-D Survey modal share percentages from Orleans the 2024 total people trips for the proposed development were projected. To reflect for the anticipated decrease in traffic generated by Towers 3 and 4 once LRT service starts, the adjusted modal shares were applied to the 2024 total people trips. Table 7 summarizes total people trips and adjusted modal shares due to LRT operation for year 2024.

| Travel Mode | AM Mode Share | AM Peak (persons/h) | | PM Peak (persons/h) | | | |
|-----------------------|------------------|---------------------|-----|---------------------|-----|-----|-------|
| | AIVI WOUL STIATE | In | Out | Total | In | Out | Total |
| Auto Driver | 30% | 56 | 147 | 203 | 100 | 74 | 174 |
| Auto Passenger | 10% | 19 | 49 | 68 | 33 | 25 | 58 |
| Transit | 60% | 111 | 294 | 405 | 200 | 148 | 347 |
| Non-motorized | 0% | 0 | 0 | 0 | 0 | 0 | 0 |
| Total People Trips | 100% | 185 | 490 | 675 | 333 | 246 | 580 |
| Total 'Nev | w' Auto Trips | 56 | 147 | 203 | 100 | 74 | 174 |

Table 7: Total Site Trip Generation – 2024

As shown in Table 7, the proposed site is projected to generate approximately 675 and 580 two-way person-trips per hour during the weekday morning and afternoon peak hours, respectively. Approximately 405 and 347 two-way transit trips per hour and 174 to 203 two-way auto trips per hour are anticipated, during the weekday morning and afternoon periods. It is noted the active mode trips during the peak periods was not considered as the site is bounded by OR 174 to the south, Ottawa River to the north.

8.2. TRIP DISTRIBUTION

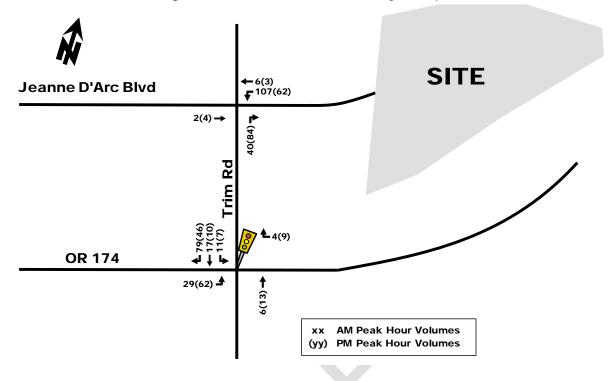
Considering the site's connectivity and the planned adjacent road network, the trip distribution is outlined next:

- (From/To) the East: 10%;
- (From/To) the South: 15%; and,
- (From/To) the West: 75%.

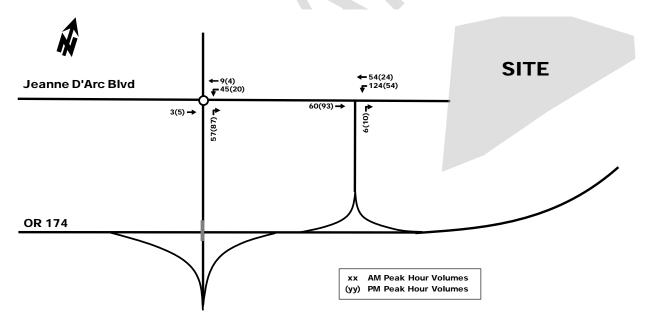
8.3. TRIP ASSIGNMENT

Based on this distribution, site-generated traffic at interim build-out (2022) was assigned to the existing adjacent network and is illustrated in Figure 11. Site-generated traffic at full build-out (2024) was assigned to the planned adjacent network and is illustrated in Figure 12.

Figure 11: Interim Build-Out Site-Generated Traffic (year 2022)







9. BACKGROUND NETWORK TRAVEL DEMAND

9.1. TRANSPORTATION NETWORK PLANS

The transportation network changes have been discussed within Section 4.1 and none are anticipated to impact the transportation analysis for this development.

9.2. BACKGROUND GROWTH

The following background traffic growth through the immediate study area (summarized in Table 8) was calculated based on historical traffic count data (years 2007, 2008, 2010, 2012, and 2017) provided by the City of Ottawa at the Trim/OR 174 intersection. Detailed analysis of the background growth is included in Appendix G.

| | Percent Annual Change | | | | | | |
|-------------|-----------------------|-----------|----------|----------|---------|--|--|
| Time Period | North Leg | South Leg | East Leg | West Leg | Overall | | |
| 8 hrs | 2.64% | 1.03% | -0.66% | -0.05% | 0.13% | | |
| AM Peak | 4.40% | 2.49% | 0.26% | 0.84% | 1.13% | | |
| PM Peak | -3.09% | 0.12% | -0.16% | -0.37% | -0.24% | | |

| Table 8: Trim/OR 174 | Historical Background G | rowth (2007 – 2017) |
|----------------------|-------------------------|---------------------|

As show in Table 8, in past years OR 174 and Trim Road have experienced approximate annual growth in traffic volume of -0.37% to 0.84% and -3.09% to 4.40%, respectively. Therefore, the subsequent analysis of future conditions will assume a 1% annual growth rate along OR 174 and Trim Road, in addition to other area developments-generated traffic.

9.2.1. PROJECTED BACKGROUND 2022 OPERATIONS

Figure 13 illustrates the future background traffic volumes for the year 2022, including both background growth and other area developments. Table 9 summarizes the future background operations for the 2022 future background traffic volumes.

Figure 13: Projected Background 2022 Traffic Volumes

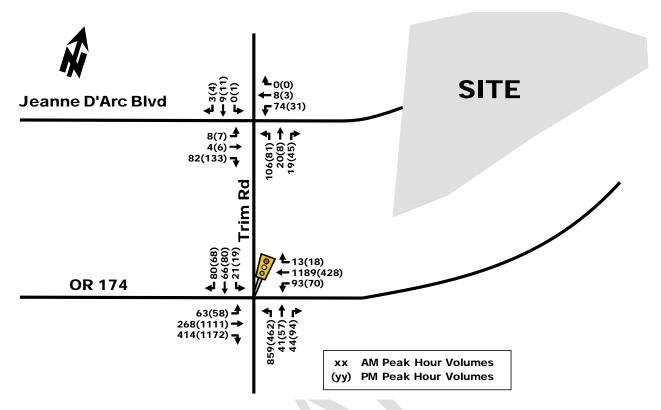


Table 9: Projected Background 2022 Performance at Study Area Intersections

| | Weekday AM Peak (PM Peak) | | | | | | | |
|--------------------------------------|---------------------------|-------------------------------|------------------------|---------------------|------|------------|--|--|
| Intersection | | Critical Movement | | Intersection | | n | | |
| | LoS | max. v/c or avg. delay (s) | Movement | Delay (s) | LoS | v/c | | |
| Jeanne D'Arc/Trim (unsignalized) | A(A) | 8.6(8.2) | NB(NB) | 8.1(7.9) | A(A) | - | | |
| Trim/OR 174 | E(D) | 0.99(0.86) | NBL(EBT) | 48.4(29.9) | E(C) | 0.94(0.79) | | |
| Note: Analysis of signalized interse | ctions assur | nes a PHF of 0.95 and | a saturation flow rate | of 1800 veh/h/lane. | • | • | | |

As shown in Table 9, the unsignalized Jeanne D'Arc/Trim intersection 'as a whole' is projected to continue operating at an excellent LoS 'A' during the weekday peak hours. With regard to the 'critical movements', they are also operating at a LoS 'A'.

The Trim/OR174 intersection is expected to experience lower levels of performance due to additional background traffic. As such, the Trim/OR174 intersection 'as a whole' is projected to operate at a LoS 'E' during peak hours (as compared to existing LoS 'D') with critical movements operating also at a LoS 'E' (as compared to existing LoS 'D'). Mitigative measures are not recommended with the opening of the Trim Road Rapid Transit station and proposed Trim Road overpass projected for 2022. The SYNCHRO model output of 2022 background conditions is provided within Appendix H.

9.2.2. PROJECTED BACKGROUND 2024 OPERATIONS

Figure 14 illustrates the future background traffic volumes for the year 2024, considering planned transportation network changes and including both background growth and other area developments generated traffic. Table 10 summarizes the future background operations for the year 2024 future background traffic volumes.

Figure 14: Projected Background 2024 Traffic Volumes

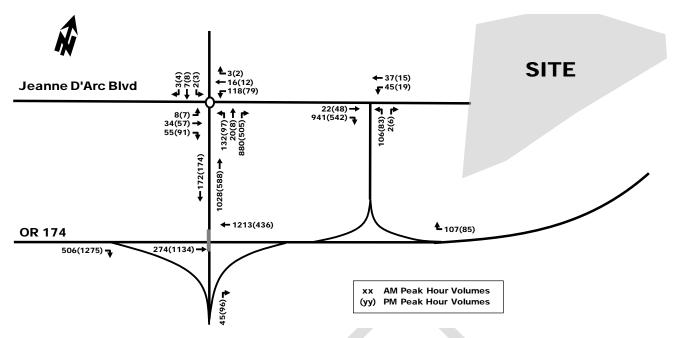


Table 10: Projected Background 2024 Performance at Study Area Intersections

| | | Weekday AM Peak (PM Peak) | | | | | | | | |
|---------------------------------------|---|-------------------------------|----------|--------------|------|------------|--|--|--|--|
| Intersection | | Critical Moven | nent | Intersection | | | | | | |
| | LoS | max. v/c or avg. delay (s) | Movement | Delay (s) | LoS | v/c | | | | |
| Jeanne D'Arc/Trim | A(A) | 8.5(8.1) | SBL(SBL) | 3.7(3.8) | A(A) | 0.51(0.29) | | | | |
| Jeanne D'Arc/OR 174 WB On/Off Ramp | C(B) | 16.6(12.0) | NB(NB) | 1.9(1.7) | A(A) | - | | | | |
| Note: Analysis of signalized intersed | Note: Analysis of signalized intersections assumes a PHF of 0.95 and a saturation flow rate of 1800 veh/h/lane. | | | | | | | | | |

As shown in Table 10, at full build-out and considering planned area network, study area intersections 'as a whole' would operate at an excellent LoS 'A' during the weekday peak hours. With regard to the 'critical movements' at the future unsignalized Jeanne D'Arc/OR 174 WB On-Off Ramp intersection, they would operate at an acceptable LoS 'C' or better. The SYNCHRO model output of 2024 background conditions is provided within Appendix I.

9.2.3. PROJECTED BACKGROUND 2029 OPERATIONS

Figure 15 illustrates the future background traffic volumes for the year 2029, considering planned transportation network changes and including both background growth and other area developments generated traffic. Table 11 summarizes the future background operations for the year 2029 future background traffic volumes.

Figure 15: Projected Background 2029 Traffic Volumes

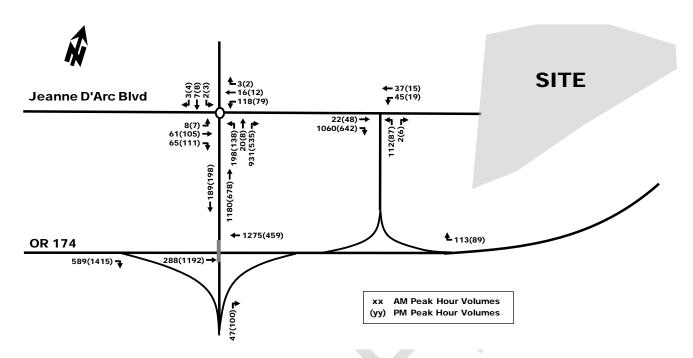


Table 11: Projected Background 2029 Performance at Study Area Intersections

| | Weekday AM Peak (PM Peak) | | | | | | | | |
|---------------------------------------|---------------------------|-------------------------------|----------|-------------|------|------------|--|--|--|
| Intersection | | Critical Moven | Ir | ntersection | า | | | | |
| | LoS | max. v/c or avg. delay (s) | Movement | Delay (s) | LoS | v/c | | | |
| Jeanne D'Arc/Trim | A(A) | 8.5(8.1) | SBL(SBL) | 3.7(3.8) | A(A) | 0.51(0.29) | | | |
| Jeanne D'Arc/OR 174 WB On-Off Ramp | C(B) | 18.4(12.6) | NB(NB) | 1.9(1.6) | A(A) | - | | | |

As shown in Table 11, study area intersections will operate similarly to the 2024 background conditions with slight increases in delay and v/c due the increase in background traffic. The SYNCHRO model output of 2029 background conditions is provided within Appendix J.

9.3. OTHER AREA DEVELOPMENTS

For the purpose of this assessment and given the current state of subject site (Tower 1 has been built, Tower 2 is in construction) and other area developments, the following time horizons are assumed:

The trip generation and distribution for these other area developments are included as Appendix F.

Trips generated by other area developments were obtained from the 2013 Petrie's Landing I TIS and the Cardinal Creek Village 2013 CTS, as summarized in Table 12.

Table 12: Other Area Developments Vehicle Trip Generation

| | AM Peak (persons/h) | | | PM Peak (persons/h) | | |
|--------------------------------|---------------------|------|-------|---------------------|------|-------|
| | In | Out | Total | In | Out | Total |
| Petrie's Landing I - Tower 2 | 13 | 57 | 70 | 39 | 24 | 63 |
| Petrie's Landing II | 22 | 108 | 130 | 104 | 52 | 156 |
| Petrie's Landing III | 422 | 237 | 659 | 254 | 430 | 584 |
| Cardinal Creek (External Only) | 412 | 940 | 1,352 | 1,246 | 980 | 2,226 |
| Total | 869 | 1342 | 2211 | 1643 | 1486 | 3029 |

9.3.1. PETRIE'S LANDING I - TOWER 2

For the purpose of this assessment and given the current state of subject site (Tower 1 has been built, Tower 2 is in construction), the following time horizons are assumed for Petrie's Landing I – Tower 2:

Year 2022

- Petrie's Landing I
 - Tower 2 100% built.

Considering Table 12 and trip distribution percentages (section 8.2), Petrie's Landing I - Tower 2 projected traffic volumes are illustrated in Figure 16.

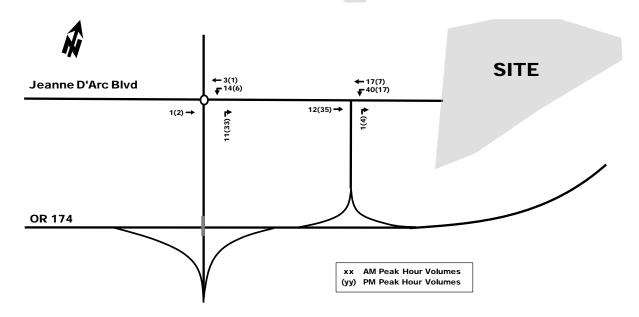


Figure 16: Petrie's Landing I Tower 2 Projected Traffic Volumes

9.3.2. PETRIE'S LANDING II

For the purpose of this assessment and given the current state of other area developments, the following time horizons are assumed for Petrie's Landing II:

Year 2022

• Petrie's Landing II – 100% built.

Year 2024

• Petrie's Landing II – 100% built.

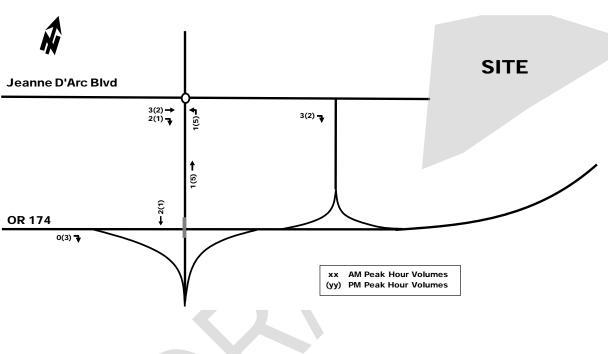


Year 2029

• Petrie's Landing II – 100% built.

Figure 17 illustrates the projected traffic volumes for Petrie's Landing II at full build-out, obtained from the 2013 Petrie's Landing I TIS. Considering assumed time horizons,65% of build-out volumes will be applied in year 2022, 100% in year 2024 and 100% in year 2029.

Figure 17: Petrie's Landing II Projected Traffic Volumes - Full Build Out



9.3.3. PETRIE'S LANDING III

For the purpose of this assessment and given the current state of other area developments, the following time horizons are assumed for Petrie's Landing III:

Year 2022

• Petrie's Landing III – 30% built.

Year 2024

• Petrie's Landing III – 50% built.

Year 2029

• Petrie's Landing III – 100% built.

Figure 18 illustrates the projected traffic volumes for Petrie's Landing III at full build-out, obtained from the 2013 Petrie's Landing I TIS. Considering assumed time horizons, 30% of build-out volumes will be applied in year 2022, 50% in year 2024 and 100% in year 2029.

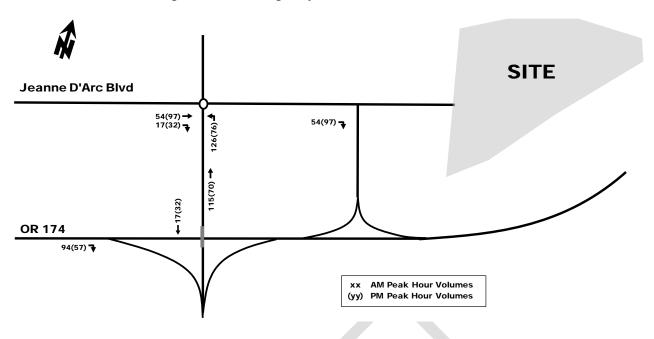


Figure 18: Petrie's Landing III Projected Traffic Volumes - Full Build-Out

9.3.4. CARDINAL CREEK VILLAGE

For the purpose of this assessment and given the current state of other area developments, the following time horizons are assumed for Cardinal Creek Village:

Year 2022

Cardinal Creek – 40% built.

Year 2024

• Cardinal Creek - 60% built.

Year 2029

• Cardinal Creek – 90% built.

Figure 19 illustrates the projected traffic volumes for Cardinal Creek Village at horizon year 2029 at study area intersections (obtained from the 2013 Cardinal Creek Village CTS). Considering assumed time horizons, 40% of full build-out volumes will be applied in year 2022, 60 % in year 2024 and 90% in year 2029.



Figure 19: Cardinal Creek 2029 Projected Traffic Volumes at Study Area Intersections

Based on Cardinal Creek Village Transportation Impact Study (October, 2013), Exhibit 11.

10. DEMAND RATIONALIZATION

The forecasted background volumes do not identify any lane constraints due to capacity for site entry and egress and no changes to the trip generation or distribution analysis is required.

11.DEVELOPMENT DESIGN

The proposed Site Plan includes a network of paved interlocked sidewalks 2.0 meters wide that connect to Towers 1 to 4. Paved interlocked paths connecting to surface parking spaces, garbage collection pads and the planned off-site MUP. As such, the proposed site plan is considered supportive of pedestrian and cycling connectivity towards the future rail station. Considering Tower 5 is located within 600 meters walk of the future LRT Trim Road Station, a further improvement to pedestrian access would be to provide a walking connection to the concrete sidewalk on Inlet Private cul-de-sac from Tower 5. This connection could be planned in conjunction with the opening of the Trim Road LRT station.

The proposed road network consists of two-way roadways 7.0-meter-wide (3.5 meters lanes) and curve radii of 8 to 12 meters. No issues are noted for access of municipal and emergency services HSU vehicles, as shown in turning templates performed by others (Figure 2). Also, the proposed layout of the road network is consistent with traffic calming principles and is considered appropriate for safe sharing of the road with cyclists. The proposed site plan is consistent with the 2016 traffic calming concept prepared by Parsons as addendum # 3 to the Petrie's Landing I 2013 TIS. Table 13 summarizes updated traffic calming measures to be incorporated for Tower 5.

| Phase | Measure | Location | Notes |
|---------|----------------------|---|---|
| Tower 5 | Signage - Meid Signs | Inlet Private cul-de-sac: (i) On Tower 5 underground parking ramp and on circle at Tower 5 underground parking ramp. (ii) On Tower 5 surface parking aisle at circle. | (i) Regulates conflicts between exiting and entering vehicles from/to Tower 5 (ii) Regulates conflicts between exiting and entering vehicles from/to Tower 5 surface parking |
| | Signage – Stop Sign | On Private Approach, for exiting vehicles | Controls conflict of exiting vehicles from the visitor surface parking with vehicles from/to the underground parking |

Table 13: Traffic Calming Measures

One 7.0-meter-wide two-way ramp is proposed for access to Tower 5 underground parking, located at Tower 5 private approach. To access the underground parking of towers 1 to 4, two 7.0-meter-wide two-way ramps located in front of tower 2 and tower 4 are proposed. The ramps providing access to the lower level parking should be within a percent grade safe for the movement of vehicles and pedestrians.

The City's Private Approach By-Law states that a private approach may be greater than 6% but shall not exceed 12% provided that a subsurface melting device sufficient to keep the private approach free of ice at all times is installed and properly maintained. In addition, our review of the available industry literature indicates that ramp grades should ideally not exceed 12%. However, a ramp grade up to 15% is acceptable if pedestrians are specifically excluded from using the ramp and transition grades are provided. Therefore, the proposed ramp grades should function acceptably provided appropriate pedestrian signage is installed, a subsurface melting device is installed for ramps exposed to ice/snow, and the appropriate transition grades are provided.

Regarding site access during construction, easements will have to be provided to avoid conflicts between construction access routes and existing towers access routes, fire routes, sidewalks, parking spaces and City's existing or future MUPs.

12.PARKING SUPPLY

The subject site is located within 600 meters radius and 800 meters walk of the planned Trim Road LRT transit station, as depicted in Figure 20. Considering Sections 101(5)(d), 101(5)(e), 102(5), 103(1) and 103(2) of the Zoning By-Law 2008-250-Consolidation-Part 4, the vehicle and bicycle parking requirements have been estimated and summarized in Table 14 and Table 16, respectively.

Stage 2 Alignment

Figure 20: Site Distance to the Planned Trim Road LRT Station

Table 14: Vehicle Parking Spaces Requirements

| L | Land Use Com | | Residents (rate) | Visitors | Total Spaces |
|---------|------------------|-----|--------------------|----------|--------------|
| Tower 3 | Residential | - / | 241 (1.2 per unit) | 40 | 281 |
| Tower 4 | Residential | - | 164 (1.2 per unit) | 27 | 192 |
| Tower 5 | Retirement (5A) | 22 | 143 (0.5 per unit) | 28 | 193 |
| Towers | Residential (5B) | 22 | 91 (0.5 per unit) | 17 | 130 |
| | Subtotal | 44 | 640 | 131 | 796 |

According to Table 14, the subject development is required to provide 640 parking spaces for residents, 131 parking spaces for visitors and 44 parking spaces for commercial uses, for a total of 796 parking spaces. With a total of 864 proposed underground and surface parking spaces, the subject development is meeting City requirements. Table 15 compares required and proposed parking spaces for each tower.

| Table 15: Total Required and | Proposed Parking Spaces |
|------------------------------|-------------------------|
|------------------------------|-------------------------|

| | Land Use | | Proposed |
|---------|------------------|-----|----------|
| Tower 3 | Residential | 281 | 284 |
| Tower 4 | Residential | 192 | 137 |
| Tower F | Retirement (5A) | 193 | 295 |
| Tower 5 | Residential (5B) | 130 | 148 |
| | Total | 796 | 864 |

Table 16 summarizes bicycle parking requirements as per City of Ottawa Zoning By-Law-Part 4, sections 100-114.

| | Land Use | Units | Bicycle Spaces |
|---------|------------------|-------|----------------|
| Tower 3 | Residential | 201 | 101 |
| Tower 4 | Residential | 137 | 69 |
| Tower 5 | Retirement (5A) | 286 | 72 |
| | Residential (5B) | | 46 |
| | Total | | 286 |

Table 16: Bicycle Parking Requirements

13.BOUNDARY STREET DESIGN

13.1. EXISTING CONDITIONS

Given the development's location within the general urban area and on a Major Pathway, the target levels of service for pedestrians and cyclists are PLoS 'C' and BLoS 'D', respectively. There are currently no MMLoS targets for transit or trucks on Jeanne D'Arc Boulevard within the study area. The multi-modal level of service analysis for the existing road segment adjacent to the site is summarized in Table 17, with detailed analysis provided in Appendix K.

Table 17: MMLOS - Jeanne D'Arc Boulevard Adjacent to the Site - South Side of Existing Road

| | Level of Service | | | | | |
|--|------------------|-----------|----------------|--------|--|--|
| Road Segment | Pedestri | an (PLoS) | Bicycle (BLoS) | | | |
| | PLoS | Target | BLoS | Target | | |
| Existing Conditions (before LRT opening) | | | | | | |
| Jeanne D'Arc Boulevard | С | C | E | D | | |

The MMLOS road segment analysis shows that existing conditions on the south side of Jeanne D'Arc Boulevard does not meet MMLOS area targets for cyclists. To meet the target BLoS 'D' for Jeanne D'Arc Boulevard east of Trim Road, the City can consider reducing vehicle speeds to 40 km/h along Jeanne D'Arc Boulevard or providing a separated cycling facility.

13.2. 2024 CONDITIONS

On year 2024, after LRT opening date, the site context will involve a high-speed road (OR 174) connecting to a local, lowspeed road (Jeanne D'Arc Boulevard) that will function as a connector from the site to the rail station, therefore a significant increase in pedestrians and cyclists volumes are anticipated. As such, speed management measures will be required to achieve necessary speed transitions and minimize speed differentials on Jeanne D'Arc Boulevard. To protect vulnerable users, a reduction of conflict zones should be sought while encouraging rail connectivity.

Given the development's location within 600 meters radius of a transit station, the target levels of service for pedestrians and cyclists will be PLoS 'A' and BLoS 'B', respectively. For the purposes of future conditions analysis, it is assumed that access to the future Trim Road LRT station will be provided both on the west side and east side of the Trim Road overpass to connect to the Trim Road Park & Ride. The multi-modal level of service analysis for the road segment along Jeanne D'Arc Boulevard adjacent to the site, considering planned network (Figure 21), is summarized in Table 18, with detailed analyses provided in Appendix L.



Figure 21: Planned Network MMLOS Analysis - Segments and Intersections

Table 18: MMLOS - Jeanne D'Arc Boulevard adjacent to the Site - South Side of Road-2024

| | Level of Service | | | | | |
|-------------------------------------|------------------|------------|----------------|--------|--|--|
| Road Segment | Pedestr | ian (PLoS) | Bicycle (BLoS) | | | |
| | PLoS | Target | BLoS | Target | | |
| 2024 Planned Transportation Network | | | | | | |
| Jeanne D'Arc Boulevard | С | A | Е | В | | |
| Cul-de-Sac | А | A | D | В | | |
| Site Access | A | A | В | В | | |

The MMLOS analysis shows that planned conditions on the south side of Jeanne D'Arc Boulevard, would not meet MMLOS area targets for both pedestrians and cyclists, with the exception of the Site Access regarding pedestrians and cyclists and the Cul-de-Sac regarding pedestrians. The critical segment for this road is the south side of Jeanne D'Arc Boulevard between Trim Road and OR 174 WB ramp. Assuming a 2.0 m sidewalk with less than 0.5 m curb and given expected traffic volumes on this segment (approximately 1,000 vehicles during the peak hour), would result in a PLoS 'C'. Providing a 2.0 m sidewalk with a minimum boulevard width of 2.0 m and reducing vehicle speeds to 30 km/h or less would result in PLoS 'A'. The bicycle level of service can be improved by provided curbside bike lanes.

14. ACCESS INTERSECTION DESIGN

14.1. LOCATION AND DESIGN OF ACCESS

Site access will operate at the end of Inlet Private, approximately 320 metres to the east of Jeanne D'Arc/ Trim intersection. The site two-way access is proposed to be 7.8 m wide with a throat length of 50 metres and is therefore meeting the City of Ottawa requirements. The nearest existing intersection for future conditions will be Jeanne D'Arc Boulevard at OR 174 On/Off ramps, approximately 100 metres to the west. At full build-out during weekday morning and afternoon peak hours, the site will generate one vehicle every 14 seconds and will attract one vehicle every 22 seconds, approximately. Considering Tower 5 separated access via Inlet Private cul-de-sac and the projected vehicle generation, no issues are anticipated at site access.

It is noted that an interlocked paved sidewalk is proposed on the north side of the driveway, connecting to towers 1 to 4. Given the existing concrete sidewalk on the south side of Jeanne D'Arc Boulevard, a texturized pedestrian crossing is proposed at the site access to connect both sidewalks. Considering Tower 5 is located within 600 meters radius and 800 meters walk of the future LRT Trim Road Station, a further improvement to pedestrian access would be to provide a walking connection between Tower 5 and the Inlet Private cul-de-sac south sidewalk.

15.TRANSPORTATION DEMAND MANAGEMENT

The development generated travel demand has been estimated in Section 12 using modal shares from the 2011 TRANS O-D survey for Orleans. These modal shares reflect conditions for a wide variety of transportation services supply within Orleans. Given site location at Orleans' north-eastern edge, they might not reflect site's current conditions. However, considering development phasing (full occupancy by 2024) and the LRT East Extension to Trim Road at OR 174 by 2022, it is anticipated that transit shares will increase, and auto shares will decrease for the subject site within the horizon analysis.

Once the envisioned LRT East Extension is completed, and to support the anticipated rise in transit ridership, postoccupancy TDM measures are recommended and attached as Appendix M.

16.TRANSIT

16.1. ROUTE CAPACITY

Considering project phasing and Delcan 2013 Petrie's Landing I Transportation Impact Study estimations for tower 2, sitegenerated transit trips on year 2024 are estimated to be 405 and 347 'new' two-way passengers during the weekday morning and afternoon peak hour, respectively, as summarized in **Error! Reference source not found.**Table 19.

| Land Llas | Horizon | AM Peak (persons/h) | | | PM Peak (persons/h) | | |
|----------------|----------|---------------------|-----|-------|---------------------|-----|-------|
| Land Use | HUHZUH | In | Out | Total | In | Out | Total |
| Tower 2 | Existing | 4 | 18 | 22 | 13 | 8 | 21 |
| Towers 3 and 4 | 2022 | 27 | 73 | 100 | 20 | 17 | 37 |
| Towers 3 to 5 | 2024 | 111 | 294 | 405 | 200 | 148 | 347 |
| | Total | 142 | 385 | 527 | 233 | 173 | 405 |

Table 19: Site-Generated Transit Trips

According to Table 19Error! Reference source not found.Error! Reference source not found., the required bus fleet to serve the site-generated transit demand would be;

Year 2022

- Morning inbound passengers: 1 single bus;
- Morning outbound passengers: 1 articulated bus;
- Afternoon inbound passengers: 1 single bus; and,
- Afternoon outbound passengers: 1 single bus.

Year 2024

• Considering the envisioned LRT East extension line is projected to enter operation in 2022 and assuming a similar capacity to that of the Confederation Line (600 passengers per train and 12 trains per hour during peak), it is anticipated that the future transit network will have sufficient capacity to accommodate the subject development transit demand.

16.2. TRANSIT PRIORITY

No transit priority measures are anticipated on Trim Road within the area of study. Although it is projected that in year 2022, before the opening of the overpass on Trim Road/OR 174 NBL movements at Trim Road/OR 174 intersection will operate at an inadequate LoS 'E' due to background traffic, NBT movements will continue operating at an acceptable LoS 'B'. Once the Trim Road overpass at OR 174 is built, NBL traffic will use the WB On-Ramp at Jeanne D'Arc/OR 174, with LoS 'A' at Jeanne D'Arc and LoS 'A' at the WB On-Ramp. Through movements at Trim Road/OR 174 will experience a further improved level of service due to the opening of the overpass.

17.REVIEW OF NETWORK CONCEPT

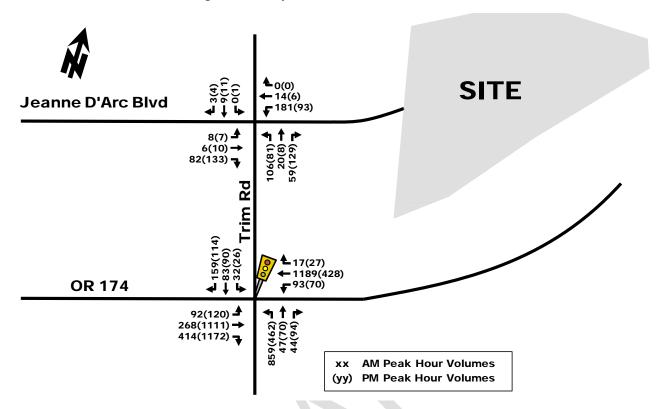
The subject site is designated as R5A [2327] H(109.4) and R5A [2327] H(101), according to the Part 6, sec. 163-164 of the Zoning By-Law No. 2008-250. Considering the planned transportation network includes expanded transit and traffic capacity through the extension of LRT services to Trim Road, the provision of an overpass on Trim Road at OR 174, the construction of a roundabout on Trim Road at Jeanne D'Arc Boulevard and the construction of On/Off ramps to OR 174 from Jeanne D'Arc Boulevard, no changes to network concepts are anticipated to serve the subject development.

18.INTERSECTION DESIGN

18.1. TOTAL PROJECTED 2022 CONDITIONS

The total projected 2022 volumes were derived by superimposing 2022 site-generated volumes (Figure 11) onto 2022 background traffic volumes (Figure 13) and are illustrated as Figure 22. Table 20 provides a performance summary of study area intersections, based on total projected 2022 traffic volumes and existing adjacent road network. The SYNCHRO model output of 2022 projected conditions is provided within Appendix N.

Figure 22: Total Projected 2022 Peak Hour Traffic Volumes



| Table 20: Total Pro | jected 2022 Performance | of Study | Area Intersections |
|---------------------|-------------------------|----------|--------------------|
| 10010 20. 10001110 | Jeeleu 2022 i chomianee | UI Study | Alea Intersections |

| | | Weekday AM Peak (PM Peak) | | | | | | |
|-------------------------------------|------|-------------------------------|----------|------------|--------------|------------|--|--|
| Intersection | | Critical Movement | | | Intersection | | | |
| | LoS | max. v/c or avg. delay (s) | Movement | Delay (s) | LoS | v/c | | |
| Jeanne D'Arc/Trim (unsignalized) | A(A) | 9.7(9.0) | EB(NB) | 9.2(8.7) | A(A) | - | | |
| Trim/OR 174 | F(E) | 1.08(0.98) | WBT(EBT) | 71.5(39.4) | F(D) | 1.06(0.90) | | |

As shown in Table 20, the unsignalized Jeanne D'Arc/Trim intersection 'as a whole' is projected to continue operating at an excellent LoS 'A' during the weekday peak hours. With regard to the 'critical movements', they are also operating at a LoS 'A'.

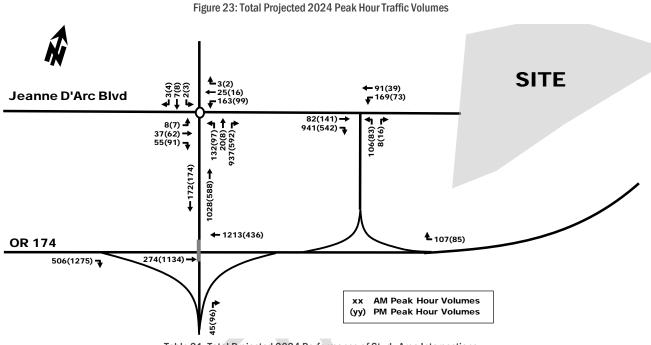
At interim conditions, the Trim/OR 174 intersection is expected to continue experiencing high levels of congestion. While the site generated volumes will not impact the critical movements (east and west bound through movements), the sitegenerated traffic lower the intersections level of service. As such, the Trim/OR 174 intersection 'as a whole' is projected to operate at a LoS 'F' during peak hours (as compared to background LoS 'E') with critical movements operating also at a LoS 'F' (as compared to background LoS 'E'). Mitigative measures are not recommended, however, given the opening of the Trim Road Rapid Transit station and proposed Trim Road overpass projected for 2022.

18.1.1. MULTIMODAL LEVEL OF SERVICE ANALYSIS

As stated in the MMLoS Guidelines, intersection level of service measures is only analysed at signalized intersections. As such, the Jeanne D'Arc/Trim intersection was not considered in this section. Due to the highway nature of the Trim/OR174 intersection, it is also not being considered in this section.

18.2. TOTAL PROJECTED 2024 CONDITIONS

The total projected 2024 volumes were derived by superimposing full build-out site-generated volumes (Figure 12) onto 2024 background traffic volumes (Figure 14) and are illustrated as Figure 23Error! Reference source not found.. Table 21Error! Reference source not found. provides a performance summary of study area intersections, based on total projected 2024 traffic volumes and widened (i.e. six lanes) OR 174. The SYNCHRO model output of 2024 total projected conditions is provided within Appendix O.



| Table 21. Total | Projected | 2024 Per | formance | of Study / | Area Intersections | |
|-----------------|-----------|----------|----------|------------|--------------------|--|

| | Weekday AM Peak (PM Peak) | | | | | | |
|-------------------|-------------------------------|---|--|---|--|--|--|
| Critical Movement | | | Intersection | | | | |
| LoS | max. v/c or avg. delay (s) | Movement | Delay (s) | LoS | v/c | | |
| A(A) | 8.8(8.2) | SBL(SBL) | 3.8(3.7) | A(A) | 0.54(0.34) | | |
| E(C) | 38.1(15.5) | NB(NB) | 4.1(2.4) | A(A) | - | | |
| A | A(A) E(C) | .oS max. v/c or avg. delay (s) A(A) 8.8(8.2) C(C) 38.1(15.5) | .oSmax. v/c or avg. delay (s)Movement.(A)8.8(8.2)SBL(SBL).(C)38.1(15.5)NB(NB) | .oSmax. v/c or avg. delay (s)MovementDelay (s)A(A)8.8(8.2)SBL(SBL)3.8(3.7) | .oS max. v/c or avg. delay (s) Movement Delay (s) LoS A(A) 8.8(8.2) SBL(SBL) 3.8(3.7) A(A) A(C) 38.1(15.5) NB(NB) 4.1(2.4) A(A) | | |

As shown in Table 21Error! Reference source not found., the unsignalized Jeanne D'Arc/Trim intersection 'as a whole' is projected to continue operating at an excellent LoS 'A' during the weekday peak hours. With regard to the 'critical movements', they are also operating at an LoS 'A'.

Considering the planned improvements to area network, the future unsignalized Jeanne D'Arc/OR 174 WB On-Off Ramp intersection 'as a whole' is projected to operate at a LoS 'A' during peak hours with critical movements operating at a LoS 'E' (as compared to background LoS 'C') during the morning peak hour. Given the City planned MUP as well as vehicular volumes at this intersection, the City of Ottawa could consider the provision of a pedestrian cross over on Jeanne D'Arc Boulevard, east of OR 174 WB On-Off Ramp.

18.3. TOTAL PROJECTED 2029 CONDITIONS - PLUS FIVE YEARS

The total projected 2029 volumes were derived by superimposing full build-out site-generated volumes (Figure 12) onto projected 2029 background traffic volumes (Figure 15), and are illustrated as Figure 24**Error! Reference source not found.** Table 22**Error! Reference source not found.** provides a performance summary of study area intersections, based on total projected 2029 traffic volumes, widened (i.e. six lanes) OR 174 and the above-mentioned background 2029 mitigative measures (e.g. dual eastbound left-turn lane and triple northbound left-turn lanes at the Trim/OR 174 intersection). The SYNCHRO model output of these projected conditions is provided within Appendix P.

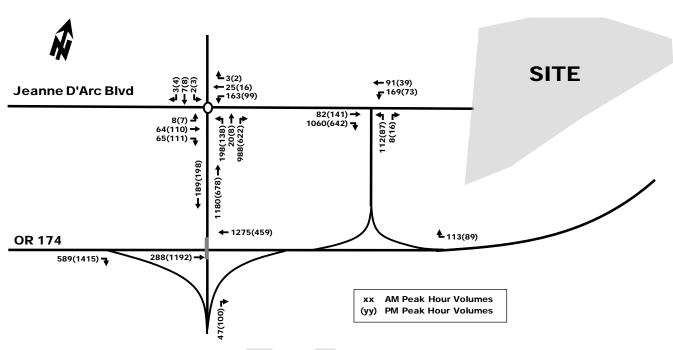


Figure 24: Total Projected 2029 Peak Hour Traffic Volumes

Table 22: Total Projected 2029 Performance of Study Area Intersections

| | Weekday AM Peak (PM Peak) | | | | | | | | | | | | |
|---------------------------------------|---------------------------|-------------------------------|------------------------|---------------------|--------------|------------|--|--|--|--|--|--|--|
| Intersection | | Critical Moven | nent | Ir | Intersection | | | | | | | | |
| | LoS | max. v/c or avg. delay (s) | Movement | Delay (s) | LoS | v/c | | | | | | | |
| Jeanne D'Arc/Trim | A(A) | 9.1(8.4) | SBL(SBL) | 4.0(3.9) | A(A) | 0.57(0.36) | | | | | | | |
| Jeanne D'Arc/OR 174 WB On-Off Ramp | E(C) | 47.1(16.8) | NB(NB) | 4.6(2.3) | A(A) | - | | | | | | | |
| Note: Analysis of signalized intersed | ctions assur | mes a PHF of 0.95 and | a saturation flow rate | of 1800 veh/h/lane. | | | | | | | | | |

As shown in Table 22**Error! Reference source not found.**, the unsignalized Jeanne D'Arc/Trim intersection 'as a whole' is projected to continue operating at an excellent LoS 'A' during the weekday peak hours. With regard to the 'critical movements', they are also operating at an LoS 'A'.

The unsignalized Jeanne D'Arc/OR 174 WB On-Off Ramp intersection 'as a whole' is projected to operate similarly to year 2024 at a LoS 'A' during peak hours with critical movement operating also at a LoS 'E' during the AM peak and LoS 'C' during the PM peak.

18.3.1. MULTIMODAL LEVEL OF SERVICE ANALYSIS

Once the LRT Trim Road station opens, the development will be within 600 meters of high-frequency transit. At such point, the applicable target levels of service for pedestrians and cyclists will be PLoS 'A' and BLoS 'B', respectively. At present, there are no MMLOS targets for transit or trucks on Jeanne D'Arc Boulevard within the area of study.

For the purposes of this analysis, it is assumed that access to the future Trim Road LRT station will be provided both on the west side and east side of the Trim Road overpass. The multi-modal level of service analysis for the roundabout study area intersection, considering the planned network (Figure 21), is summarized in Table 23, with detailed analyses provided in Appendix L. As stated in the MMLoS Guidelines, only signalized or roundabout intersections are considered for the intersection level of service measures.

| | | Level of Service | | | | | | | | | | |
|--------------------------------|-----------|------------------|---------|--------|--|--|--|--|--|--|--|--|
| Intersection | Pedestria | an (PLoS) | Bicycle | (BLoS) | | | | | | | | |
| | PLoS | Target | BLoS | Target | | | | | | | | |
| Trim / Jeanne D'Arc Roundabout | В | А | D | В | | | | | | | | |

Table 23: MMLOS - Trim/Jeanne D'Arc Roundabout, Post LRT Opening

The MMLOS analysis shows that the planned study area intersections, according to information reviewed and assumptions made, would be below the area targets for both the pedestrian and bicycle levels of service. Regarding Trim/Jeanne D'Arc roundabout, the MMLOS analysis has been applied to represent conditions according to the functional designs found on the "Confederation Line East Functional Design Report (Blair Station to Trim Road)".

With regard to pedestrians, the a PLoS 'B' is achieved for the intersection, not reaching the PLoS 'A' target. As the intersection is a roundabout, it is difficult to provide a higher level of service without compromising the design and function of the intersection. To achieve a PLoS 'A', the northbound right-turn slip lane will need to be removed thereby delaying the high northbound right-turn movement.

With regard to cyclists, the MUP on Jeanne D'Arc Boulevard's north side and the curbside bike lanes on Trim Road, result in BLoS 'B' and meet area MMLOS targets for all approaches except for the southbound approach, which results in PLoS 'D'. A pocket bike lane or curbside bike lane on the southbound approach would increase the level of service, achieving a BLOS 'B'.

19.SUMMARY OF IMPROVEMENTS INDICATED AND MODIFICATION OPTIONS

Proposed Development

- The proposed development is located at 8900 Jeanne D'Arc Boulevard (formerly 8911 North Service Road). The site is in Ward 1, Orléans, and is designated as R5 Residential Fifth Density Zone according to the Part 6, sec. 163-164 of the Zoning By-Law No. 2008-250. Currently the site consists of a 15-storey tower containing 89 condominium units (Tower 1), approximately 34 surface parking spaces and a second tower in construction that will consist of 145 units (Tower 2);
- The proposed development will continue with the residential Towers 3 to 5 within the planned Petrie's Landing I
- The horizon years for build-out are anticipated to include Towers 3 and 4 by 2022 and Towers 5a and 5b by 2024; and,
- In total, Tower 3 will consist of 22 storeys and 201 units. Tower 4 will consist of 18 storeys and 137 units. Tower 5A and 5B will consist of 32 storeys, 286 units, and 22 storeys, 182 units, respectively.

Existing Conditions

• Study area intersections 'as a whole' are currently operating at an acceptable LoS 'D' or better during the weekday peak hours; and,

The MMLOS road segment analysis shows that existing conditions on the south side of Jeanne D'Arc Boulevard do
not meet MMLOS area targets for cyclists. To meet the target BLoS 'D' for Jeanne D'Arc Boulevard east of Trim Road,
the City can consider reducing vehicle speeds to 40 km/h along Jeanne D'Arc Boulevard or provide separated cycling
facilities.

Background Conditions

- Background traffic growth was calculated as a 1% annual growth rate along OR 174 and Trim Road based on historical traffic count data provided by the City of Ottawa at the Trim/OR 174 intersection;
- Other area development considered included Petries Landing I existing Towers 1 and 2, Petries Landing II residential development (300 to 430 units), Petries Landing III mixed use development (approximately 370,000 ft² of office, 23,000 ft² of retail and up to 790 residential units) and Cardinal Creek Village (1,446-unit subdivision and a 430,000 ft2 shopping centre);
- Interim build-out is anticipated prior to the grade separation of the Trim / OR 174 intersection and the opening of LRT;
- In year 2022, the Trim/OR 174 intersection is expected to experience lower levels of performance due to additional background traffic. As such, the Trim/OR 174 intersection 'as a whole' is projected to operate at a LoS 'E' during peak hours (as compared to existing LoS 'D') with critical movements operating also at a LoS 'E' (as compared to existing LoS 'D');
- In year 2024 and considering planned improvements to the area network (i.e. Trim Road overpass at OR 174, the Trim Road roundabout at Jeanne D'Arc Boulevard and the westbound On-Off ramps to OR 174 from Jeanne D'Arc Boulevard), study area intersections 'as a whole' would operate at an excellent LoS 'A' during the weekday peak hours. With regard to the 'critical movements' at future unsignalized Jeanne D'Arc/OR 174 WB On-Off Ramp intersection, they would operate at an acceptable LoS 'C'; and,
- In year 2029, study area intersections will operate similarly to the 2024 background conditions with slight increases in delay and v/c due the increase in background traffic.

Trip Generation and Parking

- Interim build-out (year 2022), it is estimated that the site will generate approximately 282 and 242 two-way people trips during the weekday morning and afternoon peak hours, of which 155 trips, both in weekday morning and afternoon peak hours, will be made by car;
- Full build-out (year 2024), the modal share percentages were adjusted to reflect the City of Ottawa transit share targets for TOD areas, and it is estimated that total site will generate approximately 675 and 580 two-way person-trips per hour during the weekday morning and afternoon peak hours, respectively;
- Approximately 405 and 347 two-way transit trips per hour and 174 to 203 two-way auto trips per hour are anticipated, during the weekday morning and afternoon periods; and,
- The subject development will provide a total of 864 underground and surface parking spaces, meeting City requirements.

Projected Conditions

- In year 2022 at interim build-out, the Trim/OR 174 intersection is expected to continue experiencing high levels of congestion. As such, the Trim/OR 174 intersection 'as a whole' is projected to operate at a LoS 'F' during peak hours (as compared to background LoS 'E') with critical movements operating also at a LoS 'F' (as compared to background LoS 'E'). Mitigative measures are not recommended, however, given the opening of the Trim Road Rapid Transit station and proposed Trim Road overpass projected for 2022;
- In year 2024 at full build-out and considering planned improvements to the area network (i.e. Trim Road overpass at OR 174, the Trim Road roundabout at Jeanne D'Arc Boulevard and the westbound On-Off ramps to OR 174 from Jeanne D'Arc Boulevard), the future unsignalized Jeanne D'Arc/OR 174 WB On-Off Ramp intersection 'as a whole' is projected to operate at a LoS 'A' during peak hours with critical movements operating at a LoS 'E' during the morning peak hour (as compared to background LoS 'C');

- In year 2029, The unsignalized Jeanne D'Arc/OR 174 WB On-Off Ramp intersection 'as a whole' is projected to operate similarly to year 2024 at a LoS 'A' during peak hours with critical movements operating also at a LoS 'E'. It is recommended that the city explores the provision of a fully actuated traffic signal at this location; and,
- The MMLoS segment analysis shows that pedestrian and bicycle targets aren't met on the south side of Jeanne D'arc Boulevard and the bicycle targets aren't met at the Cul-de-Sac. Providing a 2.0m sidewalk, 2.0m boulevard and reducing speeds to 30km/h will improve the the PLoS to an 'A'. Similarly, the target BLoS 'B' can be reached by providing curb-side bike lanes; and,
- The MMLOS intersection analysis shows that the planned study area intersections would be below the area targets for both pedestrian and bicycle levels of service. To meet the target PLoS of 'A' and BLoS 'B' within the study area intersections, the City can consider the following options:
 - Remove the northbound sight-turn slip lane; and,
 - Install a pocket or curbside bike lane on the southbound approach.

Site Access, Circulation and Connectivity

- Site access is located at Inlet Private, approximately 320 metres to the east of Jeanne D'Arc / Trim Road intersection. The site two-way access is proposed to be 7.8 m wide with a throat length of 50 metres and is therefore meeting the City of Ottawa requirements;
- The internal road network consists of two-way roadways 7.0-meter-wide (3.5 meters lanes) and curve radii of 8 to 12 meters. No issues are noted for access of municipal and emergency services HSU vehicles;
- The proposed site plan is considered supportive of pedestrian connectivity towards the future rail station by providing a network of paved interlocked sidewalks 2.0 meters wide that connect Towers I to 4 to Jeanne D'Arc Boulevard south sidewalk. Paved interlocked paths connecting to surface parking spaces, garbage collection pads and the planned MUP are also proposed;
- The proposed site plan is considered supportive of cycling connectivity towards the future rail station by providing a road network layout that is consistent with traffic calming principles and safe sharing of the road with bike users. Connections to the City planned MUP to the south of the site are also included; and,
- Considering Tower 5 is located within 600 meters walk of the future LRT Trim Road Station, the following opportunity for further improving pedestrian access to rail is to provide a walking connection to the concrete sidewalk on Inlet private cul-de-sac from Tower 5. This connection would be planned in conjunction with the opening of the Trim Road LRT station.

TRANSIT

- Site-generated transit trips at interim build-out are estimated to be 100 and 37 'new' two-way passengers during the weekday morning and afternoon peak hour, respectively.
- These volumes can be accommodated by an articulated bus during the AM peak and a single bus during the PM peak; and
- Site-generated transit trips at full build-out are estimated to be 405 and 347 'new' two-way passengers during the weekday morning and afternoon peak hour, respectively. Considering the envisioned LRT East extension line is projected to enter operation in 2022 and assuming a similar capacity to that of the Confederation Line (600 passengers per train and 12 trains per hour during peak), it is anticipated that the future transit network will have sufficient capacity to accommodate the subject development transit demand.



Based on the foregoing, the proposed Site Plan for Petrie's Landing I Towers 3 to 5, is recommended from a transportation perspective.

Prepared By:

Reviewed By:

Andrés Pena, M.Sc. Engineer in Training Andrew Harte, P.Eng. Senior Transportation Engineer





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| City of Ottawa 2017 TIA Guidelines | Date | 13-Jun-18 |
|---|----------------|----------------------------------|
| TIA Screening Form | Project | Petrie's Landing I Towers 3 to 5 |
| | Project Number | 476705 |
| Results of Screening | Y | (es/No |
| Development Satisfies the Trip Generation Trigger | | Yes |
| Development Satisfies the Location Trigger | | Yes |
| Development Satisfies the Safety Trigger | | Yes |

| Module 1.1 - Description of Proposed Development | |
|--|---|
| Municipal Address | 8900 Jeanne D'Arc Boulevard, Orleans, ON, K4A 0S9 |
| Description of location | Existing tower with 89 residential units and a second tower consisting of 145 residential units currently under construction. Access to tower 1 provided at the end of Jeanne D'Arc Boulevard. Construction access to tower 2 provided through Jeanne D'Arc former Cul-De-Sac. |
| Land Use | Residential |
| Development Size | 806 Apartment Units (high-rise) distributed in Towers 3, 4, 5A and 5B. |
| Number of Accesses and Locations | 1 vehicular access from the West via Jeanne D'Arc Blvd to towers 3, 4 and 5. 1 additional vehicular access from Jeanne D'Arc Blvd to tower 5 via Inlet Private former Cul-De-Sac. |
| Development Phasing | Two Phases: Towers 3 to 4 by 2022. Tower 5 by 2024. |
| Buildout Year | Year 2024 (Towers 3 to 5) |
| Sketch Plan / Site Plan | See attached |

| Module 1.2 - Trip Generation Trigger | |
|--------------------------------------|-------------------------|
| Land Use Type | Townhomes or Apartments |
| Development Size | 806 Units |
| Trip Generation Trigger Met? | Yes |

| Module 1.3 - Location Triggers | | |
|--|-----|--|
| Development Proposes a new driveway to a boundary street that is designated as part of the City's Transit Priority, Rapid Transit, or Spine Bicycle Networks (See Sheet 3) | No | |
| Development is in a Design Priority Area (DPA) or Transit- oriented Development (TOD) zone. (See Sheet 3) | Yes | Development is partially within Trim TOD Zone |
| Location Trigger Met? | Yes | |

| Module 1.4 - Safety Triggers | | | |
|---|-----|------|--|
| Posted Speed Limit on any boundary road | >80 | km/h | |
| Horizontal / Vertical Curvature on a boundary street limits | No | | |
| sight lines at a proposed driveway | NO | | |
| | | | |
| A proposed driveway is within the area of influence of an | | | |
| adjacent traffic signal or roundabout (i.e. within 300 m of | No | | |
| intersection in rural conditions, or within 150 m of intersection | NO | | |
| in urban/ suburban conditions) or within auxiliary lanes of an | | | |
| intersection; | | | |
| A proposed driveway makes use of an existing median break | No | | |
| that serves an existing site | NO | | |
| There is a documented history of traffic operations or safety | | | |
| concerns on the boundary streets within 500 m of the | No | | |
| development | | | |
| The development includes a drive-thru facility | No | | |
| Safety Trigger Met? | Yes | | |

Appendix B City of Ottawa Traffic Data



Turning Movement Count - 15 Minute Summary Report

REGIONAL RD 174 @ TRIM RD

| Sur | vey D | ate: | ١ | Wedne | esday, | | 19, 20 | | | | | Obse | rved l | J-Turr | IS | | | | | |
|------------------|--------|------|--------|-------|----------|-----|---------|-----|----------|------------|-----------------|---------|--------|----------|-----|---------|----|-------------|------------|----------------|
| | | | | | | | | | | orthbou | - | 2 | | uthboun | 0 |) | | | | |
| | | | | _ | | _ | | | E | Eastboui | nd: (| 5 | | estboun | 0 | | | | | |
| | | | | | RIM RI | | | | | | REGIONAL RD 174 | | | | | | | | | |
| | | No | orthbo | und | N | So | uthbour | nd | 6 | етр | Ea | stbound | | F | We | stbound | | \A/ | етр | Crond |
| Time F | Period | LT | ST | RT | N TOT | LT | ST | RT | S TOT | STR TOT | LT | ST | RT | Е ТОТ | LT | ST | RT | W TOT | STR TOT | Grand Total |
| 07:00 | 07:15 | 227 | 6 | 9 | 242 | 1 | 4 | 5 | 10 | 252 | 1 | 53 | 83 | 137 | 17 | 300 | 2 | 319 | 456 | 708 |
| 07:15 | 07:30 | 183 | 4 | 5 | 192 | 3 | 8 | 1 | 12 | 204 | 4 | 73 | 101 | 178 | 19 | 323 | 2 | 344 | 522 | 726 |
| 07:30 | 07:45 | 162 | 9 | 21 | 192 | 2 | 6 | 2 | 10 | 202 | 7 | 65 | 110 | 182 | 23 | 312 | 6 | 341 | 523 | 725 |
| 07:45 | 08:00 | 188 | 12 | 7 | 207 | 2 | 9 | 3 | 14 | 221 | 13 | 67 | 86 | 166 | 30 | 208 | 2 | 240 | 406 | 627 |
| 08:00 | 08:15 | 169 | 10 | 13 | 192 | 3 | 11 | 4 | 18 | 210 | 4 | 64 | 89 | 157 | 23 | 227 | 2 | 252 | 409 | 619 |
| 08:15 | 08:30 | 172 | 9 | 15 | 196 | 8 | 11 | 4 | 23 | 219 | 9 | 75 | 105 | 189 | 16 | 194 | 3 | 213 | 402 | 621 |
| 08:30 | 08:45 | 161 | 11 | 17 | 189 | 6 | 11 | 4 | 21 | 210 | 4 | 87 | 83 | 174 | 20 | 228 | 1 | 249 | 423 | 633 |
| 08:45 | 09:00 | 159 | 6 | 15 | 180 | 2 | 12 | 5 | 19 | 199 | 5 | 94 | 96 | 195 | 24 | 227 | 2 | 253 | 448 | 647 |
| 09:00 | 09:15 | 134 | 6 | 11 | 151 | 1 | 5 | 6 | 12 | 163 | 4 | 94 | 82 | 180 | 22 | 162 | 2 | 186 | 366 | 529 |
| 09:15 | 09:30 | 155 | 11 | 10 | 176 | 3 | 6 | 5 | 14 | 190 | 1 | 92 | 83 | 176 | 13 | 199 | 0 | 212 | 388 | 578 |
| 09:30 | 09:45 | 147 | 6 | 14 | 167 | 3 | 11 | 3 | 17 | 184 | 10 | 84 | 85 | 180 | 11 | 197 | 1 | 209 | 389 | 573 |
| 09:45 | 10:00 | 102 | 8 | 18 | 128 | 1 | 10 | 5 | 16 | 144 | 4 | 93 | 92 | 192 | 14 | 148 | 1 | 163 | 355 | 499 |
| 11:30 | 11:45 | 114 | 11 | 13 | 138 | 3 | 18 | 5 | 26 | 164 | 6 | 125 | 99 | 230 | 11 | 135 | 2 | 148 | 378 | 542 |
| 11:45 | 12:00 | 89 | 11 | 13 | 113 | 4 | 11 | 2 | 17 | 130 | 8 | 91 | 108 | 207 | 18 | 137 | 5 | 160 | 367 | 497 |
| 12:00 | 12:15 | 81 | 8 | 17 | 106 | 2 | 11 | 3 | 16 | 122 | 3 | 124 | 90 | 217 | 19 | 134 | 3 | 156 | 373 | 495 |
| 12:15 | 12:30 | 80 | 6 | 7 | 93 | 0 | 10 | 8 | 18 | 111 | 5 | 138 | 117 | 260 | 9 | 123 | 4 | 136 | 396 | 507 |
| 12:30 | 12:45 | 68 | 9 | 9 | 86 | 3 | 5 | 4 | 12 | 98 | 2 | 125 | 111 | 238 | 18 | 144 | 3 | 165 | 403 | 501 |
| 12:45 | 13:00 | 98 | 12 | 12 | 122 | 0 | 10 | 7 | 17 | 139 | 5 | 116 | 126 | 247 | 13 | 131 | 3 | 147 | 394 | 533 |
| 13:00 | 13:15 | 90 | 9 | 14 | 113 | 3 | 10 | 2 | 15 | 128 | 7 | 126 | 106 | 239 | 6 | 116 | 2 | 124 | 363 | 491 |
| 13:15 | 13:30 | 92 | 6 | 14 | 114 | 3 | 11 | 3 | 17 | 131 | 6 | 130 | 113 | 249 | 9 | 95 | 2 | 106 | 355 | 486 |
| 15:00 | 15:15 | 95 | 10 | 27 | 132 | 2 | 9 | 3 | 14 | 146 | 6 | 240 | 210 | 456 | 8 | 105 | 2 | 115 | 571 | 717 |
| 15:15 | 15:30 | 110 | 11 | 21 | 142 | 12 | 11 | 7 | 30 | 172 | 5 | 245 | 205 | 455 | 10 | 105 | 5 | 120 | 575 | 747 |
| 15:30 | 15:45 | 82 | 12 | 22 | 116 | 5 | 13 | 5 | 23 | 139 | 3 | 258 | 211 | 473 | 11 | 79 | 2 | 92 | 565 | 704 |
| 15:45 | 16:00 | 91 | 14 | 27 | 132 | 3 | 21 | 10 | 34 | 166 | 3 | 265 | 233 | 501 | 16 | 100 | 5 | 121 | 622 | 788 |
| 16:00 | 16:15 | 109 | 10 | 18 | 137 | 6 | 25 | 6 | 37 | 174 | 2 | 300 | 250 | 552 | 14 | 98 | 3 | 115 | 667 | 841 |
| 16:15 | 16:30 | 110 | 10 | 17 | 137 | 3 | 8 | 1 | 12 | 149 | 3 | 274 | 280 | 557 | 20 | 106 | 3 | 129 | 686 | 835 |
| 16:30 | 16:45 | 96 | 9 | 28 | 133 | 4 | 11 | 2 | 17 | 150 | 3 | 229 | 294 | 526 | 17 | 107 | 2 | 126 | 652 | 802 |
| 16:45 | 17:00 | 96 | 12 | 18 | 126 | 4 | 12 | 3 | 19 | 145 | 6 | 256 | 237 | 499 | 15 | 99 | 1 | 115 | 614 | 759 |
| 17:00 | 17:15 | 117 | 7 | 23 | 147 | 6 | 13 | 6 | 25 | 172 | 2 | 270 | 266 | 538 | 15 | 93 | 2 | 110 | 648 | 820 |
| 17:15 | 17:30 | 135 | 4 | 29 | 168 | 1 | 14 | 6 | 21 | 189 | 3 | 246 | 252 | 502 | 15 | 116 | 2 | 133 | 635 | 824 |
| 17:30 | 17:45 | 111 | 11 | 12 | 134 | 5 | 7 | 2 | 14 | 148 | 6 | 259 | 246 | 511 | 11 | 90 | 1 | 102 | 613 | 761 |
| 17:45 | 18:00 | 115 | 6 | 17 | 138 | 1 | 13 | 6 | 20 | 158 | 6 | 194 | 240 | 440 | 17 | 104 | 0 | 121 | 561 | 719 |
| TOTAL | .: 3 | 938 | 286 | 513 | 4739 | 105 | 347 | 138 | 590 | 5329 | 156 | 4952 | 4889 | 10003 | 504 | 4942 | 76 | 55 2 | 22 15525 | 20854 |
| TOTAL Note: U | | | | | | 105 | 347 | 138 | 590 | | 156 Comm | | 4889 | 10003 | 504 | 4942 | 76 | 552 | 22 15 | 525 |



Turning Movement Count - Cyclist Volume Report

Work Order

36942

REGIONAL RD 174 @ TRIM RD

| Count Da | te: Wednesda | y, April 19, 2017 | 7 | | | Start Time: | 07:00 |
|-------------|--------------|-------------------|--------------|-----------|--------------|--------------|-------------|
| | | TRIM RD | | R | EGIONAL RD 1 | 74 | |
| Time Period | Northbound | Southbound | Street Total | Eastbound | Westbound | Street Total | Grand Total |
| 07:00 08:00 | 0 | 0 | 0 | 5 | 0 | 5 | 5 |
| 08:00 09:00 | 3 | 0 | 3 | 0 | 0 | 0 | 3 |
| 09:00 10:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 12:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 13:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:00 16:00 | 1 | 0 | 1 | 3 | 0 | 3 | 4 |
| 16:00 17:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:00 18:00 | 1 | 0 | 1 | 0 | 0 | 0 | 1 |
| Total | 5 | 0 | 5 | 8 | 0 | 8 | 13 |

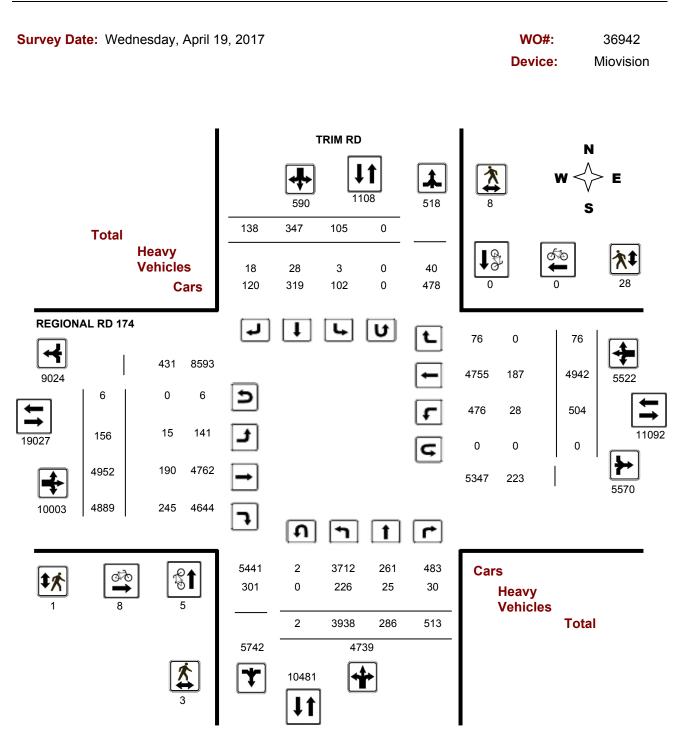
Comment:

Note: These volumes consists of bicycles only (no mopeds or motorcycles) and ARE NOT included in the Turning Movement Count Summary.



Transportation Services - Traffic Services Turning Movement Count - Full Study Diagram

REGIONAL RD 174 @ TRIM RD





Turning Movement Count - Heavy Vehicle Report

REGIONAL RD 174 @ TRIM RD

Survey Date: Wednesday, April 19, 2017

| | | | | TRIM | RD | | | | REGIONAL RD 174 | | | | | | | | | | | |
|------------------|---------|--------|--------|------|----------|--------|------|----|-----------------|------------|--------|------|-----|----------|--------|------|----|----------|------------|----------------|
| | | Northb | ound | | (| Southb | ound | | | | Eastbo | ound | | ١ | Westbo | ound | | | | |
| Time F | Period | LT | ST | RT | N TOT | LT | ST | RT | S TOT | STR TOT | LT | ST | RT | E TOT | LT | ST | RT | W TOT | STR TOT | Grand Total |
| 07:00 | 08:00 | 33 | 2 | 5 | 40 | 0 | 2 | 2 | 4 | 44 | 5 | 22 | 34 | 61 | 3 | 29 | 0 | 32 | 93 | 137 |
| 08:00 | 09:00 | 32 | 4 | 5 | 41 | 0 | 4 | 0 | 4 | 45 | 3 | 28 | 41 | 72 | 1 | 31 | 0 | 32 | 104 | 149 |
| 09:00 | 10:00 | 36 | 3 | 5 | 44 | 1 | 2 | 2 | 5 | 49 | 1 | 45 | 39 | 85 | 6 | 22 | 0 | 28 | 113 | 162 |
| 11:30 | 12:30 | 25 | 4 | 2 | 31 | 2 | 3 | 2 | 7 | 38 | 2 | 34 | 31 | 67 | 10 | 34 | 0 | 44 | 111 | 149 |
| 2:30 | 13:30 | 21 | 3 | 6 | 30 | 0 | 3 | 2 | 5 | 35 | 4 | 28 | 27 | 59 | 2 | 27 | 0 | 29 | 88 | 123 |
| 5:00 | 16:00 | 32 | 4 | 3 | 39 | 0 | 6 | 2 | 8 | 47 | 0 | 13 | 31 | 44 | 0 | 23 | 0 | 23 | 67 | 114 |
| 6:00 | 17:00 | 23 | 3 | 3 | 29 | 0 | 6 | 3 | 9 | 38 | 0 | 16 | 28 | 44 | 5 | 15 | 0 | 20 | 64 | 102 |
| 17:00 | 18:00 | 24 | 2 | 1 | 27 | 0 | 2 | 5 | 7 | 34 | 0 | 4 | 14 | 18 | 1 | 6 | 0 | 7 | 25 | 59 |
| Sub ⁻ | Total | 226 | 25 | 30 | 281 | 3 | 28 | 18 | 49 | 330 | 15 | 190 | 245 | 450 | 28 | 187 | 0 | 215 | 665 | 995 |
| l-Turn | s (Heav | vy Veh | icles) | | 0 | | | | 0 | 0 | | | | 0 | | | | 0 | 0 | 0 |
| Tot | tal | 226 | 25 | 30 | 0 | 3 | 28 | 18 | 49 | 330 | 15 | 190 | 245 | 450 | 28 | 187 | 0 | 215 | 665 | 995 |



Work Order

36942

Turning Movement Count - Pedestrian Volume Report

REGIONAL RD 174 @ TRIM RD

| Count Dat | e: Wednesday, | April 19, 2017 | | | | Start Time: | 07:00 |
|-------------|----------------------------------|----------------------------------|--------|----------------------------------|----------------------------------|-------------|-------------|
| Time Period | NB Approach (E or W Crossing) | SB Approach (E or W Crossing) | Total | EB Approach (N or S Crossing) | WB Approach (N or S Crossing) | Total | Grand Total |
| 07:00 07:15 | 0 | 0 | 0 | 0 | 1 | 1 | 1 |
| 07:15 07:30 | 0 | 1 | 1 | 0 | 2 | 2 | 3 |
| 07:30 07:45 | 1 | 1 | 2 | 0 | 1 | 1 | 3 |
| 07:45 08:00 | 0 | 0 | 0 | 0 | 3 | 3 | 3 |
| 07:00 08:00 | 1 | 2 | 3 | 0 | 7 | 7 | 10 |
| 08:00 08:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:15 08:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:30 08:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:45 09:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:00 09:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 09:00 09:15 | 0 | 0 | 0 | 0 | 2 | 2 | 2 |
| 09:15 09:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 09:30 09:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 09:45 10:00 | 0 | 0 | 0 | 0 | 4 | 4 | 4 |
| 09:00 10:00 | 0 | 0 | 0 | 0 | 6 | 6 | 6 |
| 11:30 11:45 | 0 | 0 | 0 | 0 | 1 | 1 | 1 |
| 11:45 12:00 | 0 | 0 | 0 | 0 | 1 | 1 | 1 |
| 12:00 12:15 | 0 | 0 | 0 | 0 | 1 | 1 | 1 |
| 12:15 12:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 12:30 | 0 | 0 | 0 | 0 | 3 | 3 | 3 |
| 12:30 12:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 13:00 | 0 | 1 | 1 | 0 | 1 | 1 | 2 |
| 13:00 13:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 13:15 13:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 13:30 | 0 | 1 | 1 | 0 | 1 | 1 | 2 |
| 15:00 15:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:15 15:30 | 0 | 1 | 1 | 0 | 1 | 1 | 2 |
| 15:30 15:45 | 0 | 0 | 0 | 0 | 1 | 1 | 1 |
| 15:45 16:00 | 0 | 2 | 2 | 0 | 4 | 4 | 6 |
| 15:00 16:00 | 0 | 3 | 3 | 0 | 6 | 6 | 9 |
| 16:00 16:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:15 16:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:30 16:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:45 17:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:00 17:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:00 17:15 | 0 | 0 | 0 | 1 | 0 | 1 | 1 |
| 17:15 17:30 | 0 | 0 | ů 0 | 0 | - 1 | 1 | 1 |
| 17:30 17:45 | 2 | 1 | 3 | 0 | 3 | 3 | 6 |
| 17:45 18:00 | 0 | 1 | 1 | 0 | 1 | 1 | 2 |
| 17:00 18:00 | 2 | 2 | 4 | 1 | 5 | 6 | 10 |
| Total | 3 | 8 | 11 | 1 | 28 | 29 | 40 |

Comment:



36942

Turning Movement Count - Full Study Summary Report

REGIONAL RD 174 @ TRIM RD

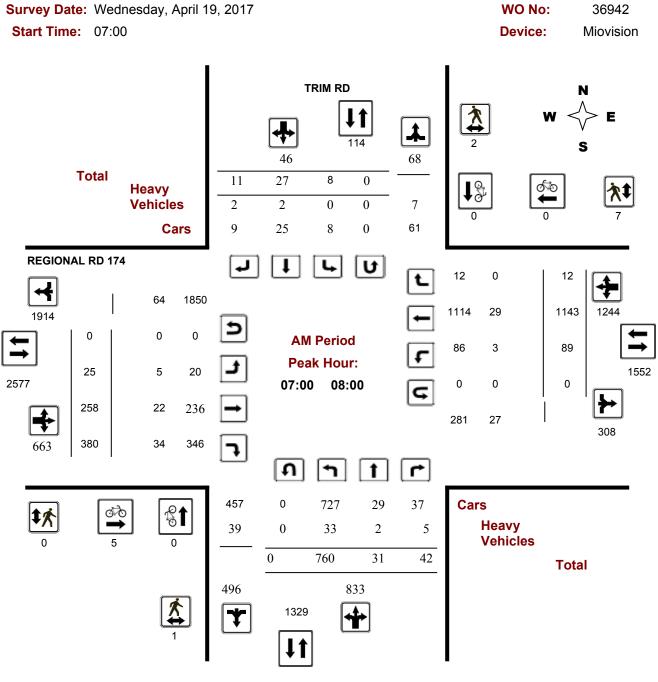
| Survey D | ate: V | Vedne | esday, | April 1 | 19, 20 | 17 | | | Total C |)bser | ved U | -Turn | s | | | | AAD | AADT Factor | | |
|-------------|-----------|-----------|----------|------------|-----------|----------|----------|-----------------|------------|---------|---------|----------|-----------|------|-------|------|-----------|-------------|--------------|--|
| | | | | | | | 1 | Northbou | nd: 2 | | Sout | hbound | l: 0 | | | | .90 | | | |
| | | | | | | | | Eastboui | nd: 6 | | Wes | stbound | : 0 | | | | | | | |
| | | | | | | | | F | ull Stu | ıdy | | | | | | | | | | |
| | | | | TRIM | RD | | | REGIONAL RD 174 | | | | | | | | | | | | |
| - | Ν | lorthbo | ound | | S | Southb | ound | | _ | | Eastb | ound | | | Westb | ound | | | | |
| Period | LT | ST | RT | NB TOT | LT | ST | RT | SB TOT | STR TOT | LT | ST | RT | EB TOT | LT | ST | RT | WB TOT | STR TOT | Gran Tota | |
| 07:00 08:00 | 760 | 31 | 42 | 833 | 8 | 27 | 11 | 46 | 879 | 25 | 258 | 380 | 663 | 89 | 1143 | 12 | 1244 | 1907 | 278 | |
| 08:00 09:00 | 661 | 36 | 60 | 757 | 19 | 45 | 17 | 81 | 838 | 22 | 320 | 373 | 715 | 83 | 876 | 8 | 967 | 1682 | 2520 | |
| 09:00 10:00 | 538 | 31 | 53 | 622 | 8 | 32 | 19 | 59 | 681 | 19 | 363 | 342 | 724 | 60 | 706 | 4 | 770 | 1494 | 2175 | |
| 11:30 12:30 | 364 | 36 | 50 | 450 | 9 | 50 | 18 | 77 | 527 | 22 | 478 | 414 | 914 | 57 | 529 | 14 | 600 | 1514 | 204 1 | |
| 12:30 13:30 | 348 | 36 | 49 | 433 | 9 | 36 | 16 | 61 | 494 | 20 | 497 | 456 | 973 | 46 | 486 | 10 | 542 | 1515 | 2009 | |
| 15:00 16:00 | 378 | 47 | 97 | 522 | 22 | 54 | 25 | 101 | 623 | 17 | 1008 | 859 | 1884 | 45 | 389 | 14 | 448 | 2332 | 2955 | |
| 16:00 17:00 | 411 | 41 | 81 | 533 | 17 | 56 | 12 | 85 | 618 | 14 | 1059 | 1061 | 2134 | 66 | 410 | 9 | 485 | 2619 | 3237 | |
| 17:00 18:00 | 478 | 28 | 81 | 587 | 13 | 47 | 20 | 80 | 667 | 17 | 969 | 1004 | 1990 | 58 | 403 | 5 | 466 | 2456 | 3123 | |
| Sub Total | 3938 | 286 | 513 | 4737 | 105 | 347 | 138 | 590 | 5327 | 156 | 4952 | 4889 | 9997 | 504 | 4942 | 76 | 5522 | 15519 | 20846 | |
| U Turns | | | | 2 | | | | 0 | 2 | | | | 6 | | | | 0 | 6 | 8 | |
| Total | 3938 | 286 | 513 | 4739 | 105 | 347 | 138 | 590 | 5329 | 156 | 4952 | 4889 | 10003 | 504 | 4942 | 76 | 5522 | 15525 | 20854 | |
| EQ 12Hr | 5474 | 398 | 713 | 6587 | 146 | 482 | 192 | 820 | 7407 | 217 | 6883 | 6796 | 13904 | 701 | 6869 | 106 | 7676 | 21580 | 28987 | |
| Note: These | values ar | re calcul | lated by | y multiply | ying the | totals b | y the ap | opropriate | e expans | ion fac | tor. | | | 1.39 | | | | | | |
| AVG 12Hr | 4926 | 358 | 642 | 5928 | 131 | 434 | 173 | 738 | 6666 | 195 | 6195 | 6116 | 12514 | 631 | 6182 | 95 | 6908 | 19422 | 26088 | |
| Note: These | volumes | are calc | culated | by multi | plying th | ne Equiv | alent 12 | 2 hr. tota | s by the | AADT | factor. | | | .90 | | | | | | |
| AVG 24Hr | 6454 | 469 | 841 | 7766 | 172 | 569 | 226 | 967 | 8733 | 256 | 8115 | 8012 | 16393 | 826 | 8099 | 125 | 9050 | 25443 | 34176 | |
| Note: These | volumes | are calc | culated | by multi | plying th | ne Avera | age Dail | y 12 hr. t | otals by | 12 to 2 | 4 expan | sion fac | ctor. | 1.31 | | | | | | |

Comments:

Note: U-Turns provided for approach totals. Refer to 'U-Turn' Report for specific breakdown.

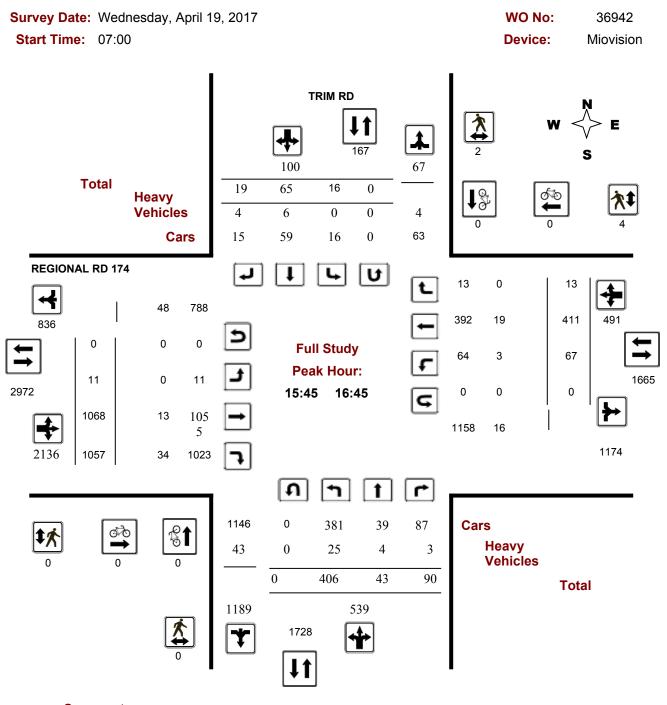


Turning Movement Count - Full Study Peak Hour Diagram REGIONAL RD 174 @ TRIM RD



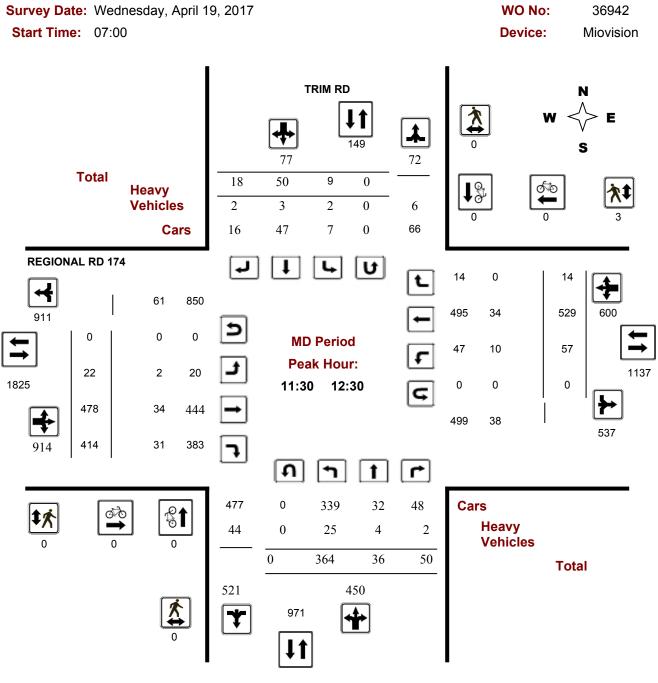


Turning Movement Count - Full Study Peak Hour Diagram REGIONAL RD 174 @ TRIM RD



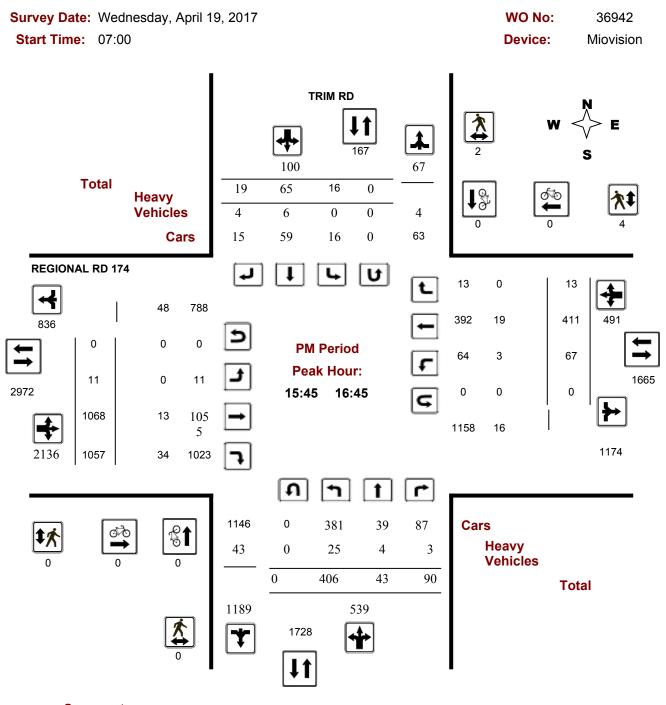


Turning Movement Count - Full Study Peak Hour Diagram REGIONAL RD 174 @ TRIM RD





Turning Movement Count - Full Study Peak Hour Diagram REGIONAL RD 174 @ TRIM RD

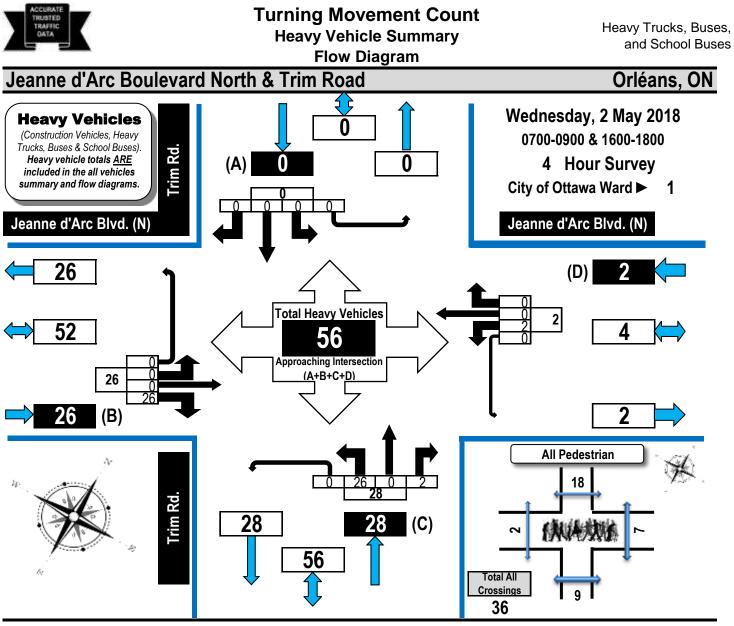




Turning Movement Count - 15 Min U-Turn Total Report

REGIONAL RD 174 @ TRIM RD

| | | | | <u> </u> | | |
|--------------|-------|----------------------------|----------------------------|---------------------------|---------------------------|-------|
| Survey Date: | We | dnesday, April 19 | 9, 2017 | | | |
| Time Pe | riod | Northbound U-Turn Total | Southbound U-Turn Total | Eastbound U-Turn Total | Westbound U-Turn Total | Total |
| 07:00 | 07:15 | 0 | 0 | 0 | 0 | 0 |
| 07:15 | 07:30 | 0 | 0 | 0 | 0 | 0 |
| 07:30 | 07:45 | 0 | 0 | 0 | 0 | 0 |
| 07:45 | 08:00 | 0 | 0 | 0 | 0 | 0 |
| 08:00 | 08:15 | 0 | 0 | 0 | 0 | 0 |
| 08:15 | 08:30 | 0 | 0 | 0 | 0 | 0 |
| 08:30 | 08:45 | 0 | 0 | 0 | 0 | 0 |
| 08:45 | 09:00 | 0 | 0 | 0 | 0 | 0 |
| 09:00 | 09:15 | 0 | 0 | 0 | 0 | 0 |
| 09:15 | 09:30 | 0 | 0 | 0 | 0 | 0 |
| 09:30 | 09:45 | 0 | 0 | 1 | 0 | 1 |
| 09:45 | 10:00 | 0 | 0 | 3 | 0 | 3 |
| 11:30 | 11:45 | 0 | 0 | 0 | 0 | 0 |
| 11:45 | 12:00 | 0 | 0 | 0 | 0 | 0 |
| 12:00 | 12:15 | 0 | 0 | 0 | 0 | 0 |
| 12:15 | 12:30 | 0 | 0 | 0 | 0 | 0 |
| 12:30 | 12:45 | 0 | 0 | 0 | 0 | 0 |
| 12:45 | 13:00 | 0 | 0 | 0 | 0 | 0 |
| 13:00 | 13:15 | 0 | 0 | 0 | 0 | 0 |
| 13:15 | 13:30 | 2 | 0 | 0 | 0 | 2 |
| 15:00 | 15:15 | 0 | 0 | 0 | 0 | 0 |
| 15:15 | 15:30 | 0 | 0 | 0 | 0 | 0 |
| 15:30 | 15:45 | 0 | 0 | 1 | 0 | 1 |
| 15:45 | 16:00 | 0 | 0 | 0 | 0 | 0 |
| 16:00 | 16:15 | 0 | 0 | 0 | 0 | 0 |
| 16:15 | 16:30 | 0 | 0 | 0 | 0 | 0 |
| 16:30 | 16:45 | 0 | 0 | 0 | 0 | 0 |
| 16:45 | 17:00 | 0 | 0 | 0 | 0 | 0 |
| 17:00 | 17:15 | 0 | 0 | 0 | 0 | 0 |
| 17:15 | 17:30 | 0 | 0 | 1 | 0 | 1 |
| 17:30 | 17:45 | 0 | 0 | 0 | 0 | 0 |
| 17:45 | 18:00 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | |
| Total | | 2 | 0 | 6 | 0 | 8 |

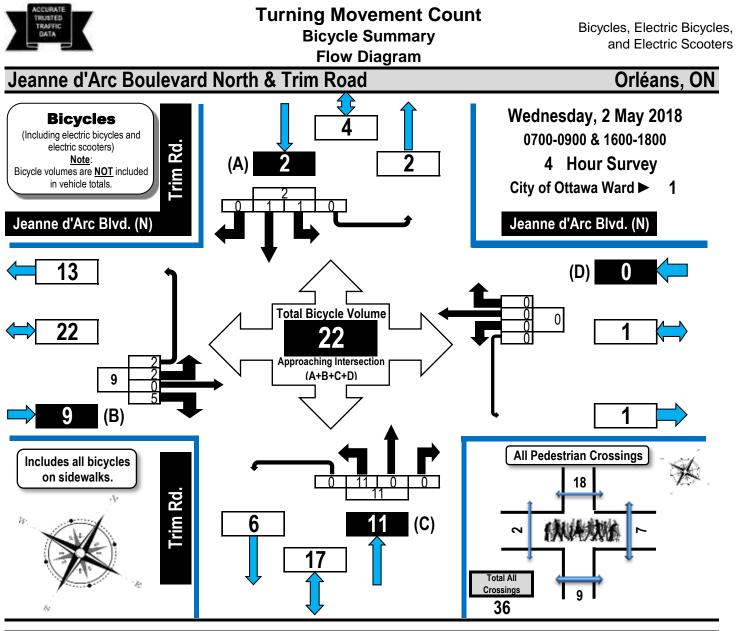


Jeanne d'Arc Boulevard North & Trim Road

Orléans, ON

Survey Date:Wednesday, 2 May 2018Start Time:0700Weather:Clear 17C/Overcast 20CSurvey Duration:4 Hrs.Survey Hours:0700-0900 & 1600-1800(AM/PM)

| | | | | | | | | | | | - | | | | | | | | | | |
|-------------|-----|-------|-------|------|--------|-----|-------|--------|------|--------|----|----|--------|-----|--------|----|----|-------|-----|--------|--------|
| . , | Jea | nne c | l'Arc | Blvd | . (N) | Jea | nne o | d'Arc | Blvd | . (N) | | Tr | rim F | ld. | | | Tr | 'im F | Rd. | | |
| | | Ea | stbou | nd | | | We | estbou | Ind | | | No | rthbou | und | | | So | uthbo | und | | |
| Time Period | LT | ST | RT | UT | S. Tot | LT | ST | RT | UT | S. Tot | LT | ST | RT | UT | S. Tot | LT | ST | RT | UT | S. Tot | G.Tot. |
| 0700-0800 | 0 | 0 | 3 | 0 | 3 | 1 | 0 | 0 | 0 | 1 | 9 | 0 | 1 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 14 |
| 0800-0900 | 0 | 0 | 7 | 0 | 7 | 1 | 0 | 0 | 0 | 1 | 10 | 0 | 1 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 19 |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| 1600-1700 | 0 | 0 | 9 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 14 |
| 1700-1800 | 0 | 0 | 7 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 9 |
| Totals | 0 | 0 | 26 | 0 | 26 | 2 | 0 | 0 | 0 | 2 | 26 | 0 | 2 | 0 | 28 | 0 | 0 | 0 | 0 | 0 | 56 |



Jeanne d'Arc Boulevard North & Trim Road

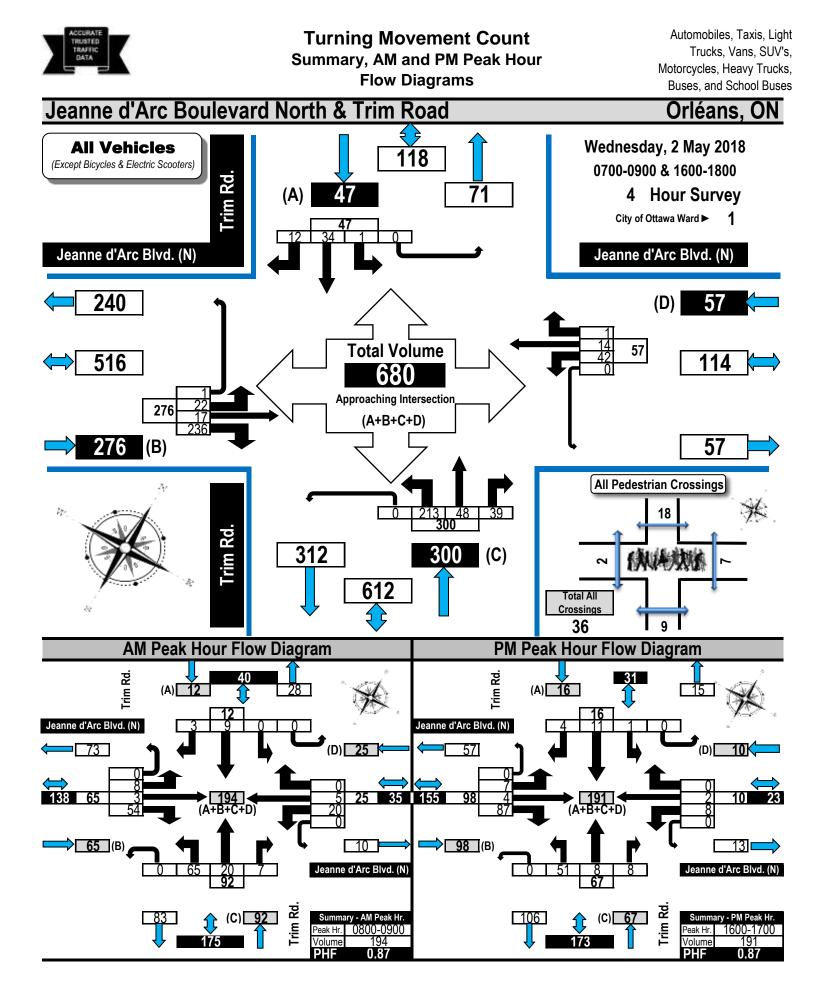
Orléans, ON

 Survey Date:
 Wednesday, 2 May 2018
 Start Time:
 0700

 Weather:
 Clear 17C/Overcast 20C
 Survey Duration:
 4 Hrs.
 Survey Hours:
 0700-0900 & 1600-1800

 (AM/PM)
 Operation:
 4 Hrs.
 Survey Hours:
 0700-0900 & 1600-1800

| (וא ואאר) | Jea | | <mark>l'Arc</mark> stbou | | . (N) | Jea | | 'Arc stbou | | . (N) | | | r <mark>im R</mark> rthbou | | | | | r <mark>im R</mark> uthbo | | | |
|-------------|-----|----|-----------------------------|---|--------|-----|----|----------------------|---|--------|----|----|-------------------------------|---|--------|----|----|------------------------------|---|--------|--------|
| Time Period | LT | ST | RT | | S. Tot | LT | ST | RT | | S. Tot | LT | ST | RT | | S. Tot | LT | ST | RT | | S. Tot | G.Tot. |
| 0700-0800 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 7 |
| 0800-0900 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 3 |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| 1600-1700 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | • | 3 |
| 1700-1800 | 2 | 0 | 4 | 1 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 2 | 9 |
| Totals | 2 | 0 | 5 | 2 | 9 | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 11 | 1 | 1 | 0 | 0 | 2 | 22 |



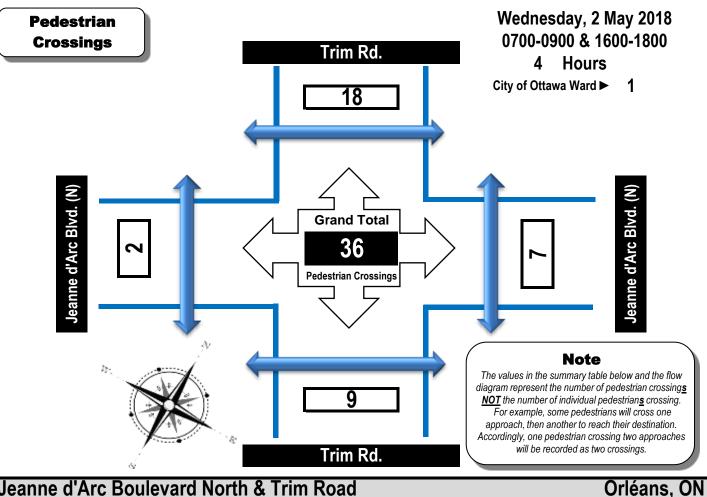


Pedestrian Crossings Summary and Flow Diagram



Jeanne d'Arc Boulevard North & Trim Road

Orléans, ON



Jeanne d'Arc Boulevard North & Trim Road

0700 Survey Date: Wednesday, 2 May 2018 Start Time: Weather: Clear 17C/Overcast 20C Survey Duration: 4 Hrs. Survey Hours: 0700-0900 & 1600-1800 (AM/PM)

| Time Period | West Side Crossing Jeanne d'Arc Blvd. (N) | East Side Crossing Jeanne d'Arc Blvd. (N) | | South Side Crossing Trim Rd. | North Side Crossing Trim Rd. | Street Total | Grand Total |
|-------------|--|--|---|---------------------------------|---------------------------------|-----------------|----------------|
| 0700-0800 | 0 | 1 | 1 | 1 | 3 | 4 | 5 |
| 0800-0900 | 1 | 5 | 6 | 5 | 8 | 13 | 19 |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| 1600-1700 | 1 | 0 | 1 | 1 | 2 | 3 | 4 |
| 1700-1800 | 0 | 1 | 1 | 2 | 5 | 7 | 8 |
| Totals | 2 | 7 | 9 | 9 | 18 | 27 | 36 |



Turning Movement Count

Summary Report Including AM/PM Peak Hours,

Automobiles, Taxis, Light Trucks, Vans, SUV's, Motorcycles, Heavy Trucks, Buses, and School Buses

PHF, AADT and Expansion Factors

Jeanne d'Arc Boulevard North & Trim Road

Orléans, ON 0700 **AADT Factor:** Survey Date: Wednesday, 2 May 2018 Start Time: 0.9 Weather-AM/PM Clear 17C/Overcast 20C 4 Hrs. Survey Hours: 0700-0900 & 1600-1800 Survey Duration: Trim Rd Jeanne d'Arc Blvd. (N) Jeanne d'Arc Blvd. (N) Trim Rd Northbound Southbound Westbound Eastbound Time W/B E/B Street N/B S/B Street Grand LT ST RT UT LT ST RT UT LT ST RT UT LT ST RT UT Tot Tot Total Tot Tot Total Total Period 0700-0800 42 44 51 59 10 14 83 88 139 1 0 3 4 0 0 0 0 5 0 5 0 8 3 20 5 25 90 20 0 9 0800-0900 54 0 65 0 0 65 7 0 92 3 0 12 104 194 1600-1700 87 98 8 2 10 108 51 0 67 16 191 7 4 0 0 0 8 8 1 11 4 0 83 1700-1800 6 9 53 69 11 3 0 15 84 38 10 10 0 58 0 9 5 0 14 72 156 1 Totals 22 236 42 14 57 333 213 48 39 0 300 1 34 0 47 347 680 17 276 1 0 12 1 Equivalent 12 & 24-hour Vehicle Volumes Including the Annual Average Daily Traffic (AADT) Factor Applicable to the Day and Month of the Turning Movement Count Expansion factors are applied exclusively to standard weekday 8-hour turning movement counts Equivalent 12-hour vehicle volumes. These volumes are calculated by multiplying the 8-hour totals by the 8 => 12 expansion factor of 1.39 Eau. 12 Hr n/a Average daily 12-hour vehicle volumes. These volumes are calculated by multiplying the equivalent 12-hour totals by the AADT factor of: 0.9 AADT 12-hr n/a 24-Hour AADT. These volumes are calculated by multiplying the average daily 12-hour vehicle volumes by the 12 🏓 24 expansion factor of 1.31 AADT 24 Hr n/a AM Peak Hour Factor Highest Hourly Vehicle Volume between 0700h & 1000h 0.87 AM Peak Hr LT ST RT UT TOT ST RT UT TOT S.TOT LT ST RT UT тот LT ST RT UT TOT S.TOT G.TOT LT 0800-0900 65 20 25 90 65 20 92 9 104 8 3 54 ٥ 5 0 ٥ ٥ ٥ 3 Λ 12 194 7 OFF Peak Hour Factor ### Highest Hourly Vehicle Volume between 1130h & 1330h Off Peak Hr LT ST RT UT TOT S.TOT ST UT TOT LT ST RT UT TOT S.TOT UT TOT LT ST RT LT RT G.TOT N/A PM Peak Hour Factor 📫 Highest Hourly Vehicle Volume between 1500h & 1800h 0.87 PM Peak Hr LT ST RT UT тот ST RT UT TOT S.TOT LT ST RT UT TOT LT ST RT UT TOT S.TOT G.TOT LT 1600-1700 7 4 87 98 8 2 10 108 51 8 8 0 0 67 11 4 16 83 0 0 191

Comments

Heavy vehicle totals consist primarily of OC Transpo and school buses. Bicycle volumes include those using sidewalks.

Notes:

- Includes all vehicle types except bicycles and electric scooters.
- 2. Expansion factors are not applied to turning movement counts if they are less than 8-hours in duration.
- 3. When expansion and AADT factors are applied, the results will differ slightly due to rounding.

Disclaimer:

The information contained in this data summary is for information purposes only, and may not apply to your situation. Every effort is made to ensure the traffic count information is accurate for the survey date provided on the summary and flow diagram forms. The author, publisher, and distributor provide no warranty about the content or accuracy of either the data summary or flow diagrams. Information provided is subjective. The author, publisher, and distributor shall not be liable for any loss of profit or any other commercial damages resulting from use of this data.

Appendix C SYNCHRO Capacity Analysis: Existing Conditions

Existing AM 1: Trim & Jeanne D'Arc

| | ٦ | - | \rightarrow | < | ← | • | 1 | 1 | 1 | 1 | Ŧ | - |
|-----------------------------------|-------|------|---------------|-------|----------------|-------|------|------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | \$ | | | \$ | | | 4 | | | 4 | |
| Sign Control | | Stop | | | Stop | | | Stop | | | Stop | |
| Traffic Volume (vph) | 8 | 3 | 54 | 20 | 5 | 0 | 64 | 20 | 7 | 0 | 9 | 3 |
| Future Volume (vph) | 8 | 3 | 54 | 20 | 5 | 0 | 64 | 20 | 7 | 0 | 9 | 3 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 9 | 3 | 60 | 22 | 6 | 0 | 71 | 22 | 8 | 0 | 10 | 3 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total (vph) | 72 | 28 | 101 | 13 | | | | | | | | |
| Volume Left (vph) | 9 | 22 | 71 | 0 | | | | | | | | |
| Volume Right (vph) | 60 | 0 | 8 | 3 | | | | | | | | |
| Hadj (s) | -0.44 | 0.19 | 0.13 | -0.10 | | | | | | | | |
| Departure Headway (s) | 3.7 | 4.4 | 4.2 | 4.1 | | | | | | | | |
| Degree Utilization, x | 0.07 | 0.03 | 0.12 | 0.01 | | | | | | | | |
| Capacity (veh/h) | 928 | 789 | 820 | 847 | | | | | | | | |
| Control Delay (s) | 7.0 | 7.6 | 7.8 | 7.2 | | | | | | | | |
| Approach Delay (s) | 7.0 | 7.6 | 7.8 | 7.2 | | | | | | | | |
| Approach LOS | А | А | А | А | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Delay | | | 7.5 | | | | | | | | | |
| Level of Service | | | А | | | | | | | | | |
| Intersection Capacity Utilization | | | 24.9% | ICI | J Level of Sei | rvice | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Existing AM 2: Trim & OR174

| | ٦ | - | \rightarrow | ∢ | + | • | Ť | × | Ŧ | 4 | |
|------------------------------------|-----------------------|------------|---|-------|--------------|------------|-------|---------------|----------|---|----|
| ane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR | |
| ane Configurations | 1 | †† | 1 | ۲. | ≜ †⊅ | ሻሻ | A⊅ | ٦ | † | 1 | |
| Fraffic Volume (vph) | 25 | 258 | 380 | 89 | 1143 | 760 | 31 | 14 | 49 | 20 | |
| uture Volume (vph) | 25 | 258 | 380 | 89 | 1143 | 760 | 31 | 14 | 49 | 20 | |
| ane Group Flow (vph) | 28 | 287 | 422 | 99 | 1283 | 844 | 81 | 16 | 54 | 22 | |
| urn Type | Prot | NA | Perm | Prot | NA | Prot | NA | pm+pt | NA | Perm | |
| Protected Phases | 5 | 2 | | 1 | 6 | 3 | 8 | 7 | 4 | | |
| Permitted Phases | | | 2 | | | | | 4 | | 4 | |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 3 | 8 | 7 | 4 | 4 | |
| Switch Phase | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 5.0 | 10.0 | 5.0 | 10.0 | 10.0 | |
| /inimum Split (s) | 12.1 | 41.2 | 41.2 | 12.5 | 41.2 | 12.2 | 42.4 | 11.9 | 17.4 | 17.4 | |
| otal Split (s) | 15.0 | 50.0 | 50.0 | 20.0 | 55.0 | 42.0 | 43.0 | 17.0 | 18.0 | 18.0 | |
| otal Split (%) | 11.5% | 38.5% | 38.5% | 15.4% | 42.3% | 32.3% | 33.1% | 13.1% | 13.8% | 13.8% | |
| ellow Time (s) | 3.3 | 5.1 | 5.1 | 3.3 | 5.1 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | |
| All-Red Time (s) | 3.8 | 2.1 | 2.1 | 4.2 | 2.1 | 3.9 | 4.1 | 3.6 | 4.1 | 4.1 | |
| ost Time Adjust (s) | -3.1 | -3.2 | -3.2 | -3.5 | -3.2 | -3.2 | -3.4 | -2.9 | -3.4 | -3.4 | |
| otal Lost Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| .ead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lead | |
| .ead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | |
| Recall Mode | None | C-Max | C-Max | None | C-Max | None | Max | None | Max | Max | |
| Act Effct Green (s) | 10.1 | 47.9 | 47.9 | 14.7 | 57.7 | 37.3 | 48.5 | 24.3 | 14.0 | 14.0 | |
| Actuated g/C Ratio | 0.08 | 0.37 | 0.37 | 0.11 | 0.44 | 0.29 | 0.37 | 0.19 | 0.11 | 0.11 | |
| /c Ratio | 0.21 | 0.23 | 0.52 | 0.52 | 0.85 | 0.89 | 0.07 | 0.06 | 0.28 | 0.06 | |
| Control Delay | 59.8 | 29.5 | 5.2 | 64.0 | 40.5 | 57.3 | 14.8 | 25.9 | 57.7 | 0.3 | |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Fotal Delay | 59.8 | 29.5 | 5.2 | 64.0 | 40.5 | 57.3 | 14.8 | 25.9 | 57.7 | 0.3 | |
| -OS | E | C | A | E | D | E | В | C | E | A | |
| Approach Delay | _ | 16.7 | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | L. | 42.2 | - | 53.6 | Ū | 38.4 | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | |
| Approach LOS | | В | | | D | | D | | D | | |
| Queue Length 50th (m) | 6.8 | 27.2 | 0.0 | 24.0 | 166.6 | 106.3 | 2.5 | 2.5 | 12.9 | 0.0 | |
| Queue Length 95th (m) | 16.6 | 38.3 | 22.3 | 42.3 | #216.1 | #138.6 | 9.3 | 6.8 | 26.2 | 0.0 | |
| nternal Link Dist (m) | 10.0 | 222.6 | 22.0 | 12.0 | 537.2 | # 100.0 | 301.4 | 0.0 | 202.0 | 0.0 | |
| Furn Bay Length (m) | 155.0 | 222.0 | 200.0 | 130.0 | 557.2 | 180.0 | 501.4 | 120.0 | 202.0 | 60.0 | |
| Base Capacity (vph) | 143 | 1250 | 810 | 208 | 1503 | 961 | 1171 | 303 | 192 | 357 | |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Reduced v/c Ratio | 0.20 | 0.23 | 0.52 | 0.48 | 0.85 | 0.88 | 0.07 | 0.05 | 0.28 | 0.06 | |
| | 0.20 | 0.25 | 0.52 | 0.40 | 0.05 | 0.00 | 0.07 | 0.05 | 0.20 | 0.00 | |
| ntersection Summary | | | | | | | | | | | |
| Cycle Length: 130 | | | | | | | | | | | |
| Actuated Cycle Length: 130 | | L (MDT O | | | | | | | | | |
| Offset: 20 (15%), Referenced to pl | nase 2:EBT an | d 6:WB1, S | tart of Greek | n | | | | | | | |
| Vatural Cycle: 110 | | | | | | | | | | | |
| Control Type: Actuated-Coordinate | ÐĘ | | | | | | | | | | |
| laximum v/c Ratio: 0.89 | | | | | | 00 D | | | | | |
| ntersection Signal Delay: 39.4 | 7.50/ | | | | tersection L | | | | | | |
| tersection Capacity Utilization 77 | 1.5% | | | IC | U Level of S | Service D | | | | | |
| nalysis Period (min) 15 | | | | | | | | | | | |
| 95th percentile volume exceed | | eue may be | longer. | | | | | | | | |
| Queue shown is maximum afte | | | | | | | | | | | |
| | 2174 | | | | | | | | | | |
| Splits and Phases: 2: Trim & OF | | | | | | 104 | | 1 (72) | | | |
| Splits and Phases: 2: Trim & OF | R174 02 (R) | | | | | \$ø4 | | 1 Ø3 | | | |
| Splits and Phases: 2: Trim & OF | | | | | | Ø4 18 s | | ¶Ø3 42 s | | 1 - | |
| Splits and Phases: 2: Trim & OF | 02 (R) | | | | | | | | | | Ø7 |

Existing PM 1: Trim Rd & Jeanne D'Arc

| | ٨ | - | \mathbf{i} | 4 | + | ×. | • | Ť | / | 1 | Ļ | 1 |
|-----------------------------------|-------|------|--------------|-------|---------------|--------|------|------|----------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | • NBR | SBL | SBT | SBR |
| Lane Configurations | | \$ | | | \$ | | | 4 | | | 4 | |
| Sign Control | | Stop | | | Stop | | | Stop | | | Stop | |
| Traffic Volume (vph) | 7 | 4 | 87 | 8 | 2 | 0 | 51 | 8 | 8 | 1 | 11 | 4 |
| Future Volume (vph) | 7 | 4 | 87 | 8 | 2 | 0 | 51 | 8 | 8 | 1 | 11 | 4 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 8 | 4 | 97 | 9 | 2 | 0 | 57 | 9 | 9 | 1 | 12 | 4 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total (vph) | 109 | 11 | 75 | 17 | | | | | | | | |
| Volume Left (vph) | 8 | 9 | 57 | 1 | | | | | | | | |
| Volume Right (vph) | 97 | 0 | 9 | 4 | | | | | | | | |
| Hadj (s) | -0.49 | 0.20 | 0.11 | -0.10 | | | | | | | | |
| Departure Headway (s) | 3.6 | 4.4 | 4.3 | 4.1 | | | | | | | | |
| Degree Utilization, x | 0.11 | 0.01 | 0.09 | 0.02 | | | | | | | | |
| Capacity (veh/h) | 963 | 793 | 813 | 842 | | | | | | | | |
| Control Delay (s) | 7.1 | 7.5 | 7.7 | 7.2 | | | | | | | | |
| Approach Delay (s) | 7.1 | 7.5 | 7.7 | 7.2 | | | | | | | | |
| Approach LOS | А | А | А | А | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Delay | | | 7.3 | | | | | | | | | |
| Level of Service | | | А | | | | | | | | | |
| Intersection Capacity Utilization | | | 23.4% | ICI | J Level of Se | ervice | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Existing PM 2: Trim Rd & OR 174

| | ٦ | → | \mathbf{r} | 4 | + | • | 1 | 1 | ţ | 1 | |
|---|------------|--------------|--------------|-----------|---------------|-------------|-------------|-----------|--------------|----------|-------------|
| ane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR | |
| ane Configurations | ۲ | <u></u> | 1 | ٦ | <u></u> ∱1≽ | ኸኘ | ≜ †} | 7 | 1 | 1 | |
| raffic Volume (vph) | 11 | 1068 | 1057 | 67 | 411 | 406 | 43 | 16 | 65 | 19 | |
| uture Volume (vph) | 11 | 1068 | 1057 | 67 | 411 | 406 | 43 | 16 | 65 | 19 | |
| ane Group Flow (vph) | 12 | 1187 | 1174 | 74 | 471 | 451 | 148 | 18 | 72 | 21 | |
| Turn Type | Prot | NA | Free | Prot | NA | Prot | NA | pm+pt | NA | Perm | |
| Protected Phases | 5 | 2 | | 1 | 6 | 3 | 8 | 7 | 4 | | |
| Permitted Phases | | | Free | | | | | 4 | | 4 | |
| Detector Phase | 5 | 2 | | 1 | 6 | 3 | 8 | 7 | 4 | 4 | |
| Switch Phase | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 10.0 | | 5.0 | 10.0 | 5.0 | 10.0 | 5.0 | 10.0 | 10.0 | |
| Ainimum Split (s) | 12.1 | 41.2 | | 12.5 | 41.2 | 12.2 | 42.4 | 11.9 | 17.4 | 17.4 | |
| Total Split (s) | 16.0 | 54.0 | | 16.0 | 54.0 | 33.0 | 43.0 | 17.0 | 27.0 | 27.0 | |
| otal Split (%) | 12.3% | 41.5% | | 12.3% | 41.5% | 25.4% | 33.1% | 13.1% | 20.8% | 20.8% | |
| 'ellow Time (s) | 3.3 | 5.1 | | 3.3 | 5.1 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | |
| II-Red Time (s) | 3.8 | 2.1 | | 4.2 | 2.1 | 3.9 | 4.1 | 3.6 | 4.1 | 4.1 | |
| ost Time Adjust (s) | -3.1 | -3.2 | | -3.5 | -3.2 | -3.2 | -3.4 | -2.9 | -3.4 | -3.4 | |
| otal Lost Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| ead/Lag | Lead | Lag | | Lead | Lag | Lag | Lead | Lag | Lead | Lead | |
| ead-Lag Optimize? | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | |
| Recall Mode | None | C-Max | | None | C-Max | None | Max | None | Max | Max | |
| Act Effct Green (s) | 9.6 | 55.8 | 130.0 | 12.4 | 63.5 | 25.6 | 45.9 | 33.2 | 23.0 | 23.0 | |
| actuated g/C Ratio | 0.07 | 0.43 | 1.00 | 0.10 | 0.49 | 0.20 | 0.35 | 0.26 | 0.18 | 0.18 | |
| /c Ratio | 0.10 | 0.43 | 0.77 | 0.46 | 0.29 | 0.70 | 0.33 | 0.05 | 0.23 | 0.05 | |
| Control Delay | 57.3 | 39.8 | 3.9 | 65.3 | 22.0 | 54.4 | 11.7 | 24.2 | 48.2 | 0.03 | |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.2 | |
| Total Delay | 57.3 | 39.8 | 3.9 | 65.3 | 22.0 | 54.4 | 11.7 | 24.2 | 48.2 | 0.0 | |
| .OS | 57.5 E | 57.0 D | 3.9 A | 05.5 E | 22.0 C | J4.4 D | В | 24.2 C | 40.2 D | 0.2 A | |
| Approach Delay | L | 22.1 | ~ | L | 27.9 | D | 43.9 | C | 35.2 | ~ | |
| Approach LOS | | 22.1 C | | | C | | 43.7 D | | 55.2 D | | |
| Queue Length 50th (m) | 2.9 | 149.6 | 0.0 | 17.9 | 33.3 | 55.6 | 3.8 | 2.8 | 16.0 | 0.0 | |
| Queue Length 95th (m) | 9.3 | #191.8 | 0.0 | 34.1 | 58.2 | 71.5 | 12.6 | 7.4 | 30.1 | 0.0 | |
| nternal Link Dist (m) | 7.5 | 313.9 | 0.0 | 34.1 | 321.3 | 71.5 | 154.2 | 7.4 | 204.2 | 0.0 | |
| Furn Bay Length (m) | 150.0 | 313.7 | 200.0 | 130.0 | 321.3 | 230.0 | 104.2 | 120.0 | 204.2 | 55.0 | |
| Base Capacity (vph) | 150.0 | 1455 | 1517 | 166 | 1649 | 733 | 1129 | 376 | 315 | 450 | |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 450 | |
| | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| pillback Cap Reductn Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Reduced v/c Ratio | 0.08 | 0.82 | 0.77 | 0.45 | 0.29 | 0.62 | 0.13 | 0.05 | 0.23 | 0.05 | |
| | 0.00 | 0.02 | 0.77 | 0.40 | 0.29 | 0.02 | 0.15 | 0.05 | 0.25 | 0.05 | |
| ntersection Summary | | | | | | | | | | | |
| Cycle Length: 130 | | | | | | | | | | | |
| Actuated Cycle Length: 130 | | | | | | | | | | | |
| Offset: 0 (0%), Referenced to phase | 2:EBT and | 6:WBT, Starl | t of Green | | | | | | | | |
| latural Cycle: 110 | | | | | | | | | | | |
| Control Type: Actuated-Coordinated | | | | | | | | | | | |
| laximum v/c Ratio: 0.82 | | | | | | | | | | | |
| tersection Signal Delay: 27.0 | | | | | tersection LC | | | | | | |
| tersection Capacity Utilization 74.5 | % | | | IC | U Level of S | ervice D | | | | | |
| | | | | | | | | | | | |
| nalysis Period (min) 15 | | eue may be | longer. | | | | | | | | |
| nalysis Period (min) 15 95th percentile volume exceeds of | | | | | | | | | | | |
| nalysis Period (min) 15 | | , | | | | | | | | | |
| nalysis Period (min) 15 95th percentile volume exceeds o Queue shown is maximum after tw | wo cycles. | , | | | | | | | | | |
| analysis Period (min) 15 95th percentile volume exceeds of Queue shown is maximum after tw splits and Phases: 2: Trim Rd & O | wo cycles. | , | | | Ţ, | 614 | | | 1 Ø3 | | |
| nalysis Period (min) 15 95th percentile volume exceeds o Queue shown is maximum after tw plits and Phases: 2: Trim Rd & O ✓Ø1 →Ø2 (R) | wo cycles. | | | | | Ø4 | | | 1 Ø3 | | |
| Analysis Period (min) 15 95th percentile volume exceeds of Queue shown is maximum after tw Splits and Phases: 2: Trim Rd & O | wo cycles. | , | | | | ∲ Ø4 7 s | | | ▲ Ø3 33 s | 1 | ▶ ø7 |

Appendix D Collision Data and Analysis

Total Area

| Classification of Accident | Rear End | Turning Movement | Sideswipe | Angle | Approaching | Single Vehicle (other) | Single vehicle (Unattended vehicle) | Other | Total | |
|-------------------------------|-----------|---------------------|-----------|----------|-------------|---------------------------|---|----------|-------|------|
| P.D. only | 39 | 5 | 6 | 1 | 0 | 2 | 0 | 2 | 55 | 80% |
| Non-fatal injury | 12 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 14 | 20% |
| Non reportable | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0% |
| Total | 51 | 6 | 6 | 2 | 0 | 2 | 0 | 2 | 69 | 100% |
| | #1 or 74% | #2 or 9% | #2 or 9% | #4 or 3% | #7 or 0% | #4 or 3% | #7 or 0% | #4 or 3% | | _ |

REGIONAL RD 174/TRIM RD

| Years | Total # Collisions | 24 Hr AADT Veh Volume | Days | Collisions/MEV |
|-----------|-----------------------|--------------------------|------|----------------|
| 2012-2016 | 69 | 34,176 | 1825 | 1.11 |

| Classification of Accident | Rear End | Turning Movement | Sideswipe | Angle | Approaching | Single Vehicle (other) | Single vehicle (Unattended vehicle) | Other | Total | |
|-------------------------------|----------|---------------------|-----------|-------|-------------|---------------------------|---|-------|-------|------|
| P.D. only | 39 | 5 | 6 | 1 | 0 | 2 | 0 | 2 | 55 | 80% |
| Non-fatal injury | 12 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 14 | 20% |
| Non reportable | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0% |
| Total | 51 | 6 | 6 | 2 | 0 | 2 | 0 | 2 | 69 | 100% |
| | 74% | 9% | 9% | 3% | 0% | 3% | 0% | 3% | | - |

JEANNE D'ARC BOULEVARD/TRIM RD

| Years | Total # Collisions | 24 Hr AADT Veh Volume | Days | Collisions/MEV |
|-----------|-----------------------|--------------------------|------|----------------|
| 2012-2016 | 0 | 2,391 | 1825 | 0.00 |

| Classification of Accident | Rear End | Turning Movement | Sideswipe | Angle | Approaching | Single Vehicle (other) | Single vehicle (Unattended vehicle) | Other | Total |
|-------------------------------|----------|---------------------|-----------|-------|-------------|---------------------------|---|-------|-------|
| P.D. only | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Non-fatal injury | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Non reportable | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

0%

Appendix E Petrie's Landing I Traffic Calming Concept



30 August 2016

OUR REF: 982847-02311

Brigil 98 rue Lois Gatineau (Hull), QC J8Y 3R7

Attention: Jean-Luc Rivard, Director - Land Development

Dear Jean-Luc:

Re: Petrie's Landing I TIS Towers II, III and IV – Addendum #3

This Addendum #3 has been prepared in response to the City of Ottawa's comments regarding potential traffic calming concerns within the Petrie's Landing development. The concerns raised to date include potential sight line issues at underground parking entrances, vehicle conflict zones with multiple accesses or bends on Inlet Private, and speeding along Inlet Private along the south limits of the site. To address these, a conceptual traffic-calming plan was developed and provided to the City for comment on June 30, 2016. Subsequent to this conceptual submission, additional comments were provided by the City and the plan was revised to focus solely on Tower II.

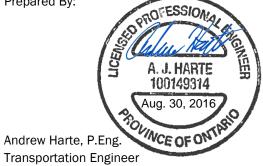
The traffic-calming plan has been developed with the intention of the Tower II recommendations to be implemented during construction. The Tower I recommendations are conceptual in nature and can be implemented during Tower II construction. Table 1 summarizes the traffic calming measures proposed for Petrie's Landing and Figure 1 illustrates the location of each of the proposed/conceptual features.

Table 1 Petrie's Landing Proposed Traffic Calming Measures

| Phase | Measure | Location | | Notes | | |
|-------------------------|-----------------------------------|--|--|---|--|--|
| | Removable Speed Hump | Along one-way access between Tower I and II site limits | | Introduces vertical deflection along the one-way access road to limit cut through vehicles and speed in front of Towers I and II | | |
| Tower II | Removable Speed Hump | Along Inlet Private, between Tower II and III site limits | | Introduces vertical deflection along Inlet Private between Towers II and III to limit speed along the road | | |
| | Signage – Stop Signs | Introduce all-way stop control at the Tower II underground parking exit to Inlet Private | | Controls access to Inlet Private | | |
| | Pavement Markings – Gore Area | Exit from Tower I drop off area onto Inlet Private | | Delineates approach angle and lane width for exiting vehicles from the Tower I drop- off area to reduce vehicle conflicts on Inlet Private | | |
| Tower I (conceptual) | Pavement Markings - Centerline | Along Inlet Private at the 90 bend in the southwest corner of the site | | Delineates the lane widths (3.5m) and improve adherence to driving line on the curve | | |
| | Signage – Stop Sign | At one-way access from Towers I and II to Inlet Private, south of Tower I | | Controls access to Inlet Private | | |
| | Signage – Warning Curve Sign | On Inlet Private on both sides of the 90 degree bend in the southwest corner of the site | | Warning for vehicles approaching the curve to reduce speed, in conjunction with the centerline pavement marking | | |

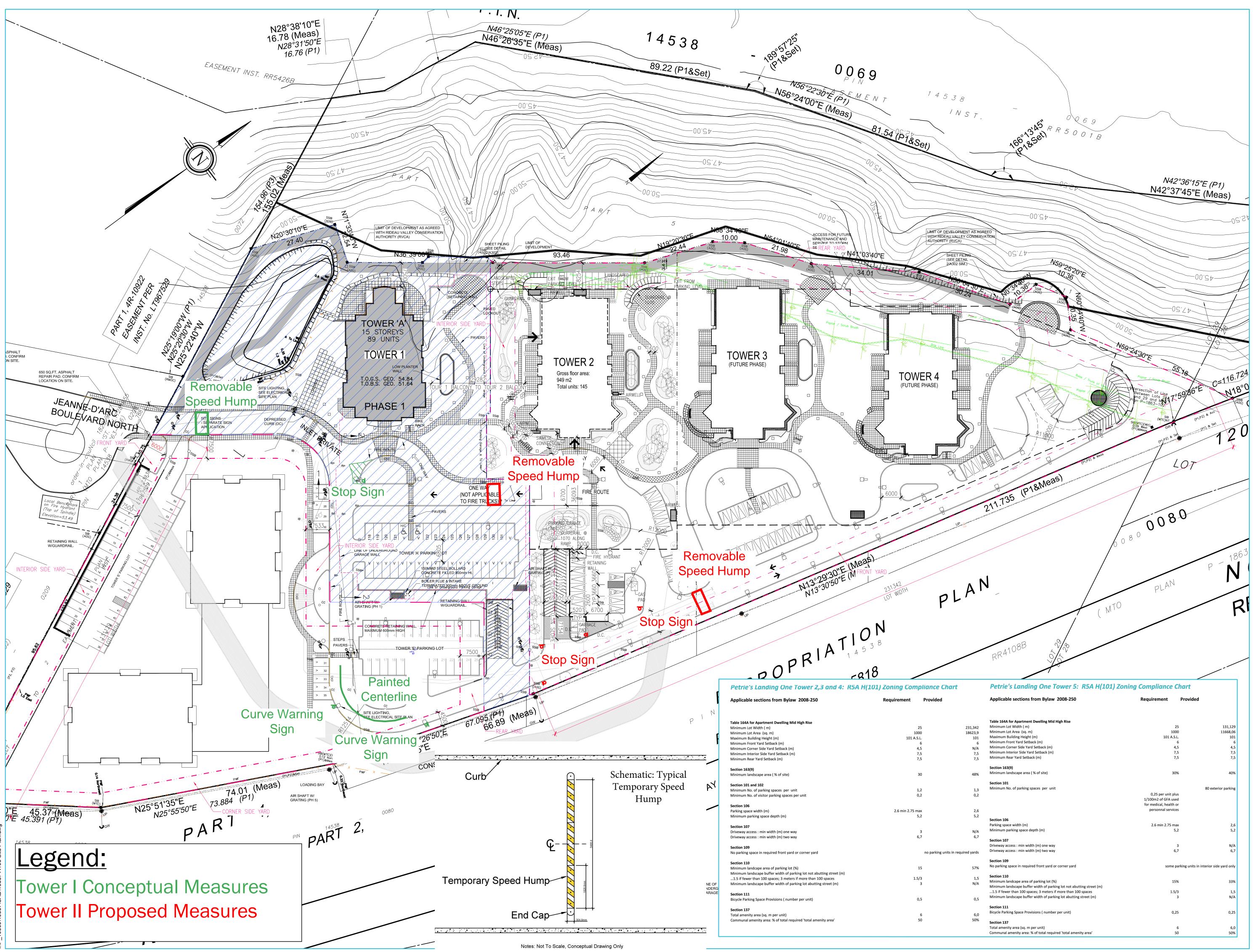
In conclusion, the proposed traffic calming measures are anticipated to address the City's comments and aggregated public feedback regarding the existing and future site operations. Should the conceptual plans be agreed upon, they can be implemented into the existing Tower II Site Plan Control submission and further implemented as the Petrie's Landing site develops.

Prepared By:



Reviewed by:

Christopher Gordon, P, Eng. Senior Project Manager



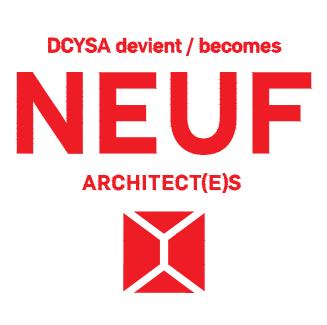
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ARCHITECTURE DE PAYSAGE Landscape architect CIVIL Civil

ARCHITECTES Architect NEUF architect(e)s

630, boul. René-Lévesque O. 32e étage, Montréal QC H3B 1S6 T 514 847 1117 NEUFarchitectes.com SCEAU Seal



CLIENT Client

OUVRAGE Project Petrie's Landing I, Phase 2

| | ACEMENT Location | NO PROJET №. 10557 |
|--------------------|---------------------------|------------------------|
| NO | RÉVISION | DATE (aa.mm.jj) |
| A | SITE APPROVAL | 2013-12-20 |
| | FOR COORDINATION | 2016.01.18 |
| č | SITE PLAN APPROVAL 4TH | 2016.06.03 |
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NO. DESSIN Dwg Number

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RÉVISION Revision

Appendix F Adjacent Developments Trip Generation and Distribution

PARSONS

1223 Michael Street, Suite 100 • Ottawa, Ontario K1J 7T2 • (613) 738-4160 • Fax: (613) 739-7105 • www.parsons.com

24 February 2015

OUR REF: TO3131TOY

Brigil 98 rue Lois Gatineau (Hull), QC J8Y 3R7

Attention: Jean-Luc Rivard

Dear Jean-Luc:

Re: Petrie's Landing I TIS Towers II, III and IV - Addendum #2

This Addendum #2 has been prepared in response to a City of Ottawa comment regarding the number of assumed residential units identified in the original TIS prepared December 2013 by Delcan (now known as Parsons). It has come to the City's attention that number of proposed residential units identified in the original TIS is less than the number of residential units identified in the Zoning By-Law Amendment/Official Plan Amendment for Towers I to IV.

Based on information provided at the time, the number of residential units identified in the original TIS are as follows:

Petrie's Landing I - original TIS

- Phase I consists of a 89 unit residential tower (Tower I);
- Phase II consists of a 336 unit retirement building; and
- **Phase III** consists of Towers II, III and IV, each comprised of 140 residential condo units for a total of 420 residential condo units.

The number of residential units identified in the Zoning By-Law Amendment/Official Plan Amendment is as follows:

Petrie's Landing I - Zoning By-Law Amendment/Official Plan Amendment

- Phase I consists of a 89 unit residential tower (Tower I);
- Phase II consists of a 314 unit retirement building; and
- **Phase III** consists of Towers II, III and IV, each comprised of 145, 175 and 145 residential condo units, respectively, for a total of 465 residential condo units.

The net difference between the original TIS and the Zoning By-Law Amendment/Official Plan Amendment equates to 23 fewer residential units assumed in the original TIS. As such, the following Tables 1 and 2 summarize the projected site-generated traffic from the original TIS report and the revised projected site-generated traffic, respectively. The revised projected site-generated traffic summarized in Table 2 is based on the number of residential units identified in the Zoning By-Law Amendment/Official Plan Amendment and the same appropriate trip generation rates/modal shares identified in the original TIS.

| | Dwelling | AM Peak (veh/hr) PM Peak (veh | | | | Peak (veh | /hr) |
|----------------------|---------------|-------------------------------|-----|-------|-----|---|-------|
| Land Use | Units | In | Out | Total | In | Out 24 14 24 14 24 24 | Total |
| Retirement Residence | 336 | 17 | 33 | 50 | 39 | 24 | 63 |
| Tower I | 89 | 8 | 35 | 43 | 22 | 14 | 36 |
| Tower II | 140 | 13 | 55 | 68 | 38 | 24 | 62 |
| Tower III | 140 | 13 | 55 | 68 | 38 | 24 | 62 |
| Tower IV | 140 | 13 | 55 | 68 | 38 | 24 | 62 |
| Total 'Nev | w' Auto Trips | 64 | 233 | 297 | 175 | 110 | 285 |

Table 1: Original Projected Site-Generated Traffic

As shown in Table 1, the total projected two-way site-generated traffic for Petrie's Landing I is approximately 300 and 285 veh/h during the weekday morning and afternoon peak hours, respectively.

The following Table 2 summarizes the projected two-way site-generated traffic for Petrie's Landing I based on the number of residential units identified in the Zoning By-Law Amendment/Official Plan Amendment.

| Land Use | Dwelling | AM | Peak (veh | /hr) | PM Peak (veh/hr) | | | |
|----------------------|---------------|----|-----------|-------|------------------|---|-------|--|
| Lanu Use | Units | In | Out | Total | In | Out 24 14 24 24 | Total | |
| Retirement Residence | 314 | 16 | 30 | 46 | 35 | 24 | 59 | |
| Tower I | 89 | 8 | 35 | 43 | 22 | 14 | 36 | |
| Tower II | 145 | 13 | 57 | 70 | 39 | 24 | 63 | |
| Tower III | 175 | 15 | 63 | 78 | 45 | 28 | 73 | |
| Tower IV | 145 | 13 | 57 | 70 | 39 | 24 | 63 | |
| Total 'New | w' Auto Trips | 65 | 242 | 307 | 180 | 114 | 294 | |

Table 2: Revised Project Site-Generated Traffic

As shown in Table 2, the total projected two-way site-generated traffic for Petrie's Landing I, based on the number of residential units identified in the Zoning By-Law Amendment/Official Plan Amendment, is approximately 310 and 295 veh/h during the weekday morning and afternoon peak hours, respectively.

The approximate net difference in the total projected two-way site-generated traffic equates to an additional 10 veh/h (or approximately 1 additional vehicle every 6 minutes) during both weekday morning and afternoon peak hours. This amount of additional site-generated is considered negligible and will have <u>no</u> effect on the results, findings or conclusions included in the original TIS or the subsequent Addendum #1.

Therefore, based on the foregoing, the results, findings and conclusions include in the original TIS and the subsequent Addendum #1 remain valid and no further analysis is required from a transportation perspective. If there any questions, please call.

Prepared By:

Gordon R. Scobie, P.Eng. Transportation Engineer Ottawa Operations





| ITE Vehicle Trip Generation Rates | | | | | | | | |
|-------------------------------------|---------|---------|---------|--|--|--|--|--|
| Land Use | Data | Trip | Rate | | | | | |
| Lanu Use | Source | AM Peak | PM Peak | | | | | |
| Residential Condominiums/Townhouses | ITE 230 | 0.44 | 0.52 | | | | | |

Modified Person Trip Generation Rates

| Land Use | Data | Person T | Trip Rate | |
|-------------------------------------|---------|----------|-----------|--|
| Eand Use | Source | AM Peak | PM Peak | |
| Residential Condominiums/Townhouses | ITE 230 | 0.57 | 0.68 | |
| | | | | |

Note: 1.3 factor to account for typical North American auto occupancy values of approximately 1.15 and combined transit and non-motorized modal shares of less than 10%

ITE Fitted Curve Equations

| Land Use | Data | Data Fitted Curve Equation | | | | | |
|-------------------------------------|---------|----------------------------|-----------|--------|---------|-----------|--------|
| Land Use | Source | | AM Peak | | | PM Peak | |
| Residential Condominiums/Townhouses | ITE 230 | Ln(T)= | 0.80Ln(x) | + 0.26 | Ln(T) = | 0.82Ln(x) | + 0.32 |

Modified Person Trip Generation

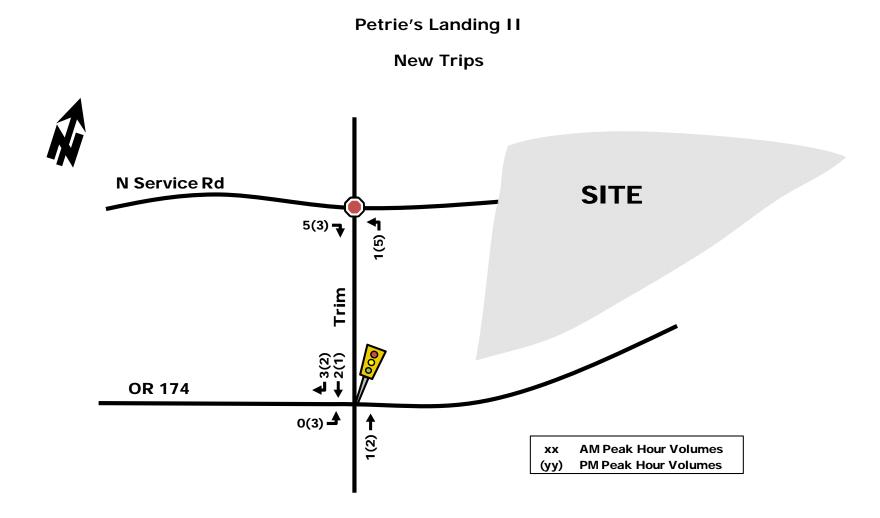
| Land Use | Data | Area | AM F | Peak (Persons | s/hr) | PM P | Peak (Persons | s/hr) |
|-------------------------------------|---------|--------|------|---------------|-------|------|---------------|-------|
| Land Use | Source | Area | In | Out | Total | In | Out | Total |
| | | Units | 17% | 83% | | 67% | 33% | |
| Residential Condominiums/Townhouses | ITE 230 | 430 du | 36 | 180 | 216 | 172 | 86 | 258 |
| | | Total | 36 | 180 | 216 | 172 | 86 | 258 |

Total Site Trip Generation

| Travel Mode | Mode Share | AM | Peak (Person: | s/hr) | PM Peak (Persons/hr) | | |
|--------------------|------------------------|----|---------------|-------|----------------------|-----|-------|
| Travel Mode | mode share | In | Out | Total | In | Out | Total |
| Auto Driver | 60% | 22 | 108 | 130 | 104 | 52 | 156 |
| Auto Passenger | 10% | 4 | 18 | 22 | 17 | 9 | 26 |
| Transit | 25% | 9 | 45 | 54 | 43 | 21 | 64 |
| Non-motorized | 5% | 1 | 9 | 10 | 8 | 4 | 12 |
| Total Person Trips | 100% | 36 | 180 | 216 | 172 | 86 | 258 |
| | Total 'New' Auto Trips | 22 | 108 | 130 | 104 | 52 | 156 |

Total Site Vehicle Trip Generation

| Travel Mode | AN | l Peak (veh/ł | ۱r) | PM Peak (veh/hr) | | |
|----------------------------|----|---------------|-------|------------------|-----|-------|
| Traver wode | In | Out | Total | In | Out | Total |
| Total Site Trip Generation | 22 | 108 | 130 | 104 | 52 | 156 |
| Total 'New' Auto Trips | 22 | 108 | 130 | 104 | 52 | 156 |



ITE Vehicle Trip Generation Rates

| Land Use | Data | Trip | ₹ate | |
|-------------------------------------|---------|---------|---------|--|
| Land Use | Source | AM Peak | PM Peak | |
| Residential Condominiums/Townhouses | ITE 230 | 0.44 | 0.52 | |
| General Office | ITE 710 | 1.56 | 1.49 | |
| Specialty Retail | ITE 826 | 1.36 | 2.71 | |
| | | | | |

Modified Person Trip Generation Rates

| Land Use | Data | Person T | rip Rate |
|-------------------------------------|---------|----------|----------|
| Land Use | Source | AM Peak | PM Peak |
| Residential Condominiums/Townhouses | ITE 230 | 0.57 | 0.68 |
| General Office | ITE 710 | 2.03 | 1.94 |
| Specialty Retail | ITE 826 | 1.76 | 3.52 |
| | | | |

Note: 1.3 factor to account for typical North American auto occupancy values of approximately 1.15 and combined transit and non-motorized modal shares of less than 10%

ITE Fitted Curve Equations

| Land Use | Data | Fitted Curve Equation | | | | | |
|-------------------------------------|---------|-----------------------|-----------|---------|---------|-----------|---------|
| Land Use | Source | | AM Peak | | PM Peak | | |
| Residential Condominiums/Townhouses | ITE 230 | Ln(T)= | 0.80Ln(x) | + 0.26 | Ln(T)= | 0.82Ln(x) | + 0.32 |
| General Office | ITE 710 | Ln(T)= | 0.80Ln(x) | + 1.57 | T= | 1.12(x) | + 78.45 |
| Specialty Retail | ITE 826 | T= | 1.20(x) | + 10.74 | T= | 2.40(x) | + 21.48 |

Modified Person Trip Generation

| Land Use | Data | Area | AM F | Peak (Person: | s/hr) | PM F | eak (Persons/hr) | |
|-------------------------------------|---------|-------------------------|------|---------------|-------|------|------------------|-------|
| Land Use | Source | Area | In | Out | Total | In | Out | Total |
| | | Units | 17% | 83% | | 67% | 33% | |
| Residential Condominiums/Townhouses | ITE 230 | 790 du | 59 | 292 | 351 | 285 | 141 | 426 |
| | | ft² | 88% | 12% | | 17% | 83% | |
| General Office | ITE 710 | 370,000 ft ² | 623 | 86 | 709 | 108 | 533 | 641 |
| | | ft² | 56% | 44% | | 44% | 56% | |
| Specialty Retail | ITE 826 | 23,000 ft ² | 28 | 22 | 50 | 44 | 56 | 100 |
| | | Total | 710 | 400 | 1,110 | 437 | 730 | 1,167 |

Residential Condominiums/Townhouses Trip Generation

| Travel Mode | Mode Share | AM F | Peak (Person: | s/hr) | PM Peak (Persons/hr) | | | |
|-------------------------------------|------------|------|---------------|-------|----------------------|-----|-------|--|
| Traver Mode | Mode Share | In | Out | Total | In | Out | Total | |
| Auto Driver | 60% | 36 | 176 | 212 | 171 | 85 | 256 | |
| Auto Passenger | 10% | 6 | 29 | 35 | 29 | 14 | 43 | |
| Transit | 25% | 15 | 73 | 88 | 71 | 35 | 106 | |
| Non-motorized | 5% | 2 | 14 | 16 | 14 | 7 | 21 | |
| Total Person Trips | 100% | 59 | 292 | 351 | 285 | 141 | 426 | |
| Total 'New' Residential Condominium | 36 | 176 | 212 | 171 | 85 | 256 | | |

General Office Trip Generation

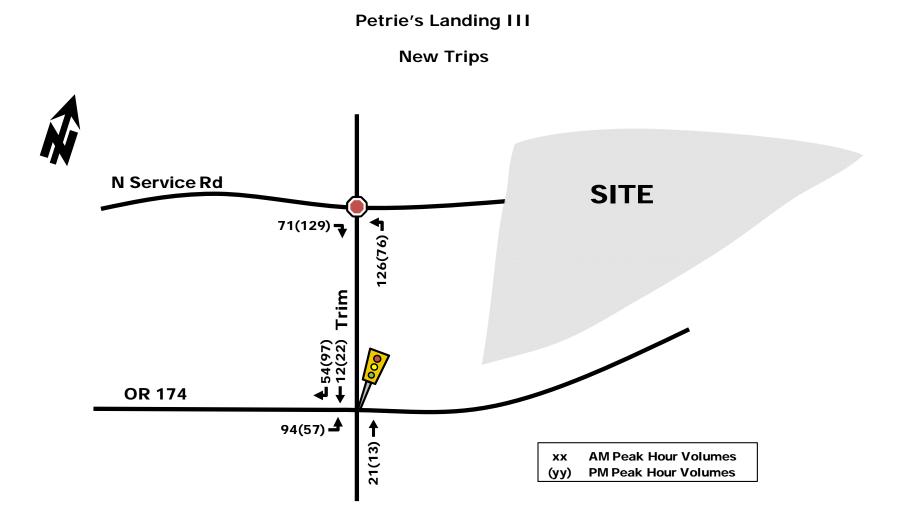
| Travel Mode | Mode Share | AM F | Peak (Person | s/hr) | PM | Peak (Person: | s/hr) |
|--------------------|---------------------------|------|--------------|-------|-----|---------------|-------|
| Traver Mode | Node Share | In | Out | Total | In | Out | Total |
| Auto Driver | 60% | 374 | 52 | 426 | 65 | 320 | 385 |
| Auto Passenger | 10% | 63 | 9 | 72 | 11 | 54 | 65 |
| Transit | 25% | 155 | 21 | 176 | 27 | 133 | 160 |
| Non-motorized | 5% | 31 | 4 | 35 | 5 | 26 | 31 |
| Total Person Trips | 100% | 623 | 86 | 709 | 108 | 533 | 641 |
| Total 'New' | General Office Auto Trips | 374 | 52 | 426 | 65 | 320 | 385 |

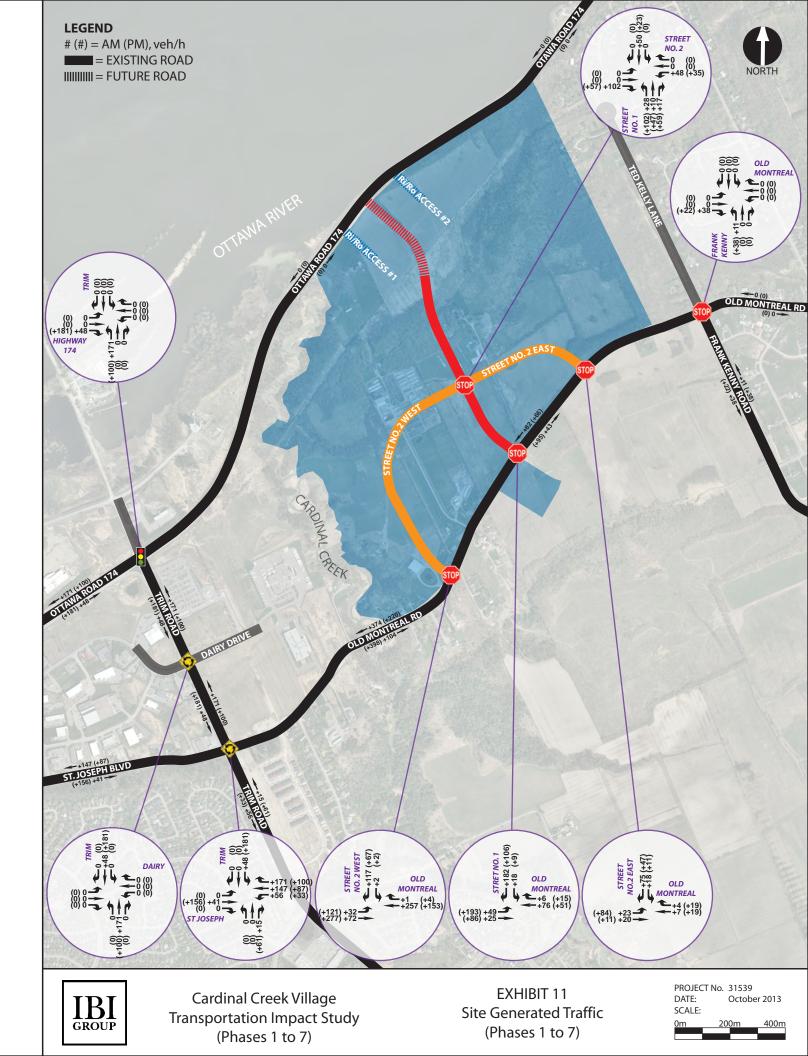
Specialty Retail Trip Generation

| Travel Mode | Mode Share | AM F | Peak (Person | s/hr) | PM F | Peak (Person: | s/hr) |
|--------------------|---|------|--------------|-------|------|---------------|-------|
| Traver Mode | Mode Share | In | Out | Total | In | Out | Total |
| Auto Driver | 60% | 17 | 14 | 31 | 27 | 34 | 61 |
| Auto Passenger | 10% | 3 | 2 | 5 | 4 | 6 | 10 |
| Transit | 25% | 7 | 5 | 12 | 11 | 14 | 25 |
| Non-motorized | 5% | 1 | 1 | 2 | 2 | 2 | 4 |
| Total Person Trips | 100% | 28 | 22 | 50 | 44 | 56 | 100 |
| | Less Pass-by (30%) | -5 | -5 | -10 | -9 | -9 | -18 |
| | Total 'New' Specialty Retail Auto Trips | 12 | 9 | 21 | 18 | 25 | 43 |

Total Site Vehicle Trip Generation

| Travel Mode | AN | l Peak (veh/l | וr) | PN | PM Peak (veh/hr) | | | |
|--|-----|---------------|-------|-----|------------------|-------|--|--|
| Traver Mode | In | Out | Total | In | Out | Total | | |
| ondominiums/Townhouses Trip Generation | 36 | 176 | 212 | 171 | 85 | 256 | | |
| General Office Trip Generation | 374 | 52 | 426 | 65 | 320 | 385 | | |
| Specialty Retail Trip Generation | 17 | 14 | 31 | 27 | 34 | 61 | | |
| Less Specialty Retail Pass-by (30%) | -5 | -5 | -10 | -9 | -9 | -18 | | |
| Total 'New' Auto Trips | 422 | 237 | 659 | 254 | 430 | 684 | | |





Appendix G Background Growth Analysis

Trim/OR 174 <u>8 hrs</u>

| Year | Date | Nort | h Leg | Sout | h Leg | East | : Leg | Wes | t Leg | Total |
|------|----------------------|------|-------|------|-------|------|-------|-------|-------|-------|
| | Date | SB | NB | NB | SB | WB | EB | EB | WB | Total |
| 2007 | Wednesday 31 January | 322 | 242 | 4191 | 4602 | 5927 | 5317 | 8831 | 9110 | 38542 |
| 2008 | Friday 20 June | 618 | 391 | 4770 | 5319 | 6281 | 6058 | 10034 | 9935 | 43406 |
| 2010 | Friday 9 July | 744 | 722 | 5389 | 4539 | 6433 | 6484 | 9542 | 10363 | 44216 |
| 2012 | Friday 8 June | 329 | 441 | 4696 | 4430 | 5833 | 5818 | 8875 | 9044 | 39466 |
| 2017 | Wednesday 19 April | 590 | 518 | 4739 | 5742 | 5522 | 5570 | 10003 | 9024 | 41708 |

| Γ | Year | | Cou | nts | | | % Cł | nange | |
|-----------------------|------|-------|-------|-------|-------|--------|--------|--------|--------|
| North Leg | real | NB | SB | NB+SB | INT | NB | SB | NB+SB | INT |
| | 2007 | 242 | 322 | 564 | 38542 | | | | |
| | 2008 | 391 | 618 | 1009 | 43406 | 61.6% | 91.9% | 78.9% | 12.6% |
| | 2010 | 722 | 744 | 1466 | 44216 | 84.7% | 20.4% | 45.3% | 1.9% |
| | 2012 | 441 | 329 | 770 | 39466 | -38.9% | -55.8% | -47.5% | -10.7% |
| | 2017 | 518 | 590 | 1108 | 41708 | 17.5% | 79.3% | 43.9% | 5.7% |
| | | | | | | | | | |
| Regression Estimate | 2007 | 393 | 490 | 883 | 41312 | | | | |
| Regression Estimate | 2017 | 576 | 570 | 1147 | 41722 | | | | |
| Average Annual Change | | 3.89% | 1.53% | 2.64% | 0.10% | | | | |

| Average Annual Change | | 3.89% | 1.53% |
|-----------------------|------|-------|-------|
| Regression Estimate | 2017 | 5/6 | |

| Γ | Year | | Cou | nts | | | % Cł | | | | | |
|---------------------|------|-------|-------|-------|-------|-------|--------|--------|--------|--|--|--|
| West Leg | Teal | EB | WB | EB+WB | INT | EB | WB | EB+WB | INT | | | |
| | 2007 | 8831 | 9110 | 17941 | 38542 | | | | | | | |
| | 2008 | 10034 | 9935 | 19969 | 43406 | 13.6% | 9.1% | 11.3% | 12.6% | | | |
| | 2010 | 9542 | 10363 | 19905 | 44216 | -4.9% | 4.3% | -0.3% | 1.9% | | | |
| | 2012 | 8875 | 9044 | 17919 | 39466 | -7.0% | -12.7% | -10.0% | -10.7% | | | |
| | 2017 | 10003 | 9024 | 19027 | 41708 | 12.7% | -0.2% | 6.2% | 5.7% | | | |
| _ | | | | | | | | | | | | |
| Regression Estimate | 2007 | 9252 | 9733 | 18985 | | | | | | | | |
| Regression Estimate | 2017 | 9791 | 9108 | 18899 | | | | | | | | |

Average Annual Change

0.57% -0.66%

-0.05%

| Г | Year | | Cou | nts | | % Change | | | | | |
|-----------------------|------|--------|--------|--------|-------|----------|-------|-------|--------|--|--|
| East Leg | fear | EB | WB | EB+WB | INT | EB | WB | EB+WB | INT | | |
| | 2007 | 5317 | 5927 | 11244 | 38542 | | | | | | |
| | 2008 | 6058 | 6281 | 12339 | 43406 | 13.9% | 6.0% | 9.7% | 12.6% | | |
| | 2010 | 6484 | 6433 | 12917 | 44216 | 7.0% | 2.4% | 4.7% | 1.9% | | |
| | 2012 | 5818 | 5833 | 11651 | 39466 | -10.3% | -9.3% | -9.8% | -10.7% | | |
| L | 2017 | 5570 | 5522 | 11092 | 41708 | -4.3% | -5.3% | -4.8% | 5.7% | | |
| Dogrossion Estimate | 2007 | 5900 | 6242 | 17147 | | | | | | | |
| Regression Estimate | | | 6242 | 12143 | | | | | | | |
| Regression Estimate | 2017 | 5767 | 5602 | 11369 | | | | | | | |
| Average Annual Change | | -0.23% | -1.08% | -0.66% | | | | | | | |

% Change Counts Year South Leg NB SB NB+SB INT NB SB NB+SB INT 2007 4191 4602 8793 38542 2008 4770 5319 10089 43406 13.8% 15.6% 14.7% 12.6% 2010 5389 4539 9928 44216 13.0% -14.7% -1.6% 1.9% 2012 4696 4430 9126 39466 -12.9% -2.4% -8.1% -10.7% 2017 4739 5742 41708 10481 0.9% 29.6% 14.8% 5.7% **Regression Estimate** 2007 9300 4671 4630 **Regression Estimate** 2017 4898 5411 10308 Average Annual Change 0.48% 1.57% 1.03%

Trim/OR 174 <u>AM Peak</u>

| Voor | Data | Nort | h Leg | Sout | h Leg | East | : Leg | West Leg | | Total |
|-----------|----------------------|------|-------|------|-------|------|-------|----------|------|-------|
| Year Date | Date | SB | NB | NB | SB | WB | EB | EB | WB | TOLAI |
| 2007 | Wednesday 31 January | 50 | 32 | 626 | 402 | 1346 | 395 | 658 | 1651 | 5160 |
| 2008 | Friday 20 June | 34 | 14 | 649 | 439 | 1326 | 294 | 674 | 1836 | 5266 |
| 2010 | Friday 9 July | 42 | 46 | 819 | 454 | 1309 | 387 | 720 | 2003 | 5780 |
| 2012 | Friday 8 June | 62 | 64 | 875 | 414 | 1292 | 313 | 578 | 2016 | 5614 |
| 2017 | Wednesday 19 April | 48 | 51 | 807 | 537 | 1324 | 428 | 727 | 1890 | 5812 |

| | Year | | Cou | nts | | | % Cł | nange | |
|-----------------------|------|--------------------|--------------------|---------------------|-------|--------|--------|--------|-------|
| North Leg | fear | NB | SB | NB+SB | INT | NB | SB | NB+SB | INT |
| | 2007 | 32 | 50 | 82 | 5160 | | | | |
| | 2008 | 14 | 34 | 48 | 5266 | -56.3% | -32.0% | -41.5% | 2.1% |
| | 2010 | 46 | 42 | 88 | 5780 | 228.6% | 23.5% | 83.3% | 9.8% |
| | 2012 | 64 | 62 | 126 | 5614 | 39.1% | 47.6% | 43.2% | -2.9% |
| | 2017 | 51 | 48 | 99 | 5812 | -20.3% | -22.6% | -21.4% | 3.5% |
| Degraccion Estimate | 2007 | 20 | 11 | 74 | 5207 | | | | |
| Regression Estimate | 2007 | 30 | 44 | 74 | 5297 | | | | |
| Regression Estimate | 2017 | 61 7.45% | 52 1.78% | 113 4.40% | 5901 | | | | |
| Average Annual Change | | 714370 | 1.7070 | 4140 /0 | 1.09% | | | | |
| Г | Year | | Cou | nts | | | % Cł | nange | |
| West Leg | real | EB | WB | EB+WB | INT | EB | WB | EB+WB | INT |
| | 2007 | 658 | 1651 | 2309 | 5160 | | | | |
| | 2008 | 674 | 1836 | 2510 | 5266 | 2.4% | 11.2% | 8.7% | 2.1% |
| | 2010 | 720 | 2003 | 2723 | 5780 | 6.8% | 9.1% | 8.5% | 9.8% |
| | 2012 | 578 | 2016 | 2594 | 5614 | -19.7% | 0.6% | -4.7% | -2.9% |
| | 2017 | 727 | 1890 | 2617 | 5812 | 25.8% | -6.3% | 0.9% | 3.5% |
| Regression Estimate | 2007 | 657 | 1811 | 2468 | | | | | |
| Regression Estimate | 2007 | 0.077 | 1011 | 2700 | | | | | |
| Regression Estimate | 2017 | 695 | 1990 | 2685 | | | | | |

Regression Estimate Average Annual Change

695 1990 0.56% 0.94%

2685 0.84%

| Г | Veer | | Cou | nts | | % Change | | | | | |
|-----------------------|------|-------|--------|-------|------|----------|-------|-------|-------|--|--|
| East Leg | Year | EB | WB | EB+WB | INT | EB | WB | EB+WB | INT | | |
| Γ | 2007 | 395 | 1346 | 1741 | 5160 | | | | | | |
| | 2008 | 294 | 1326 | 1620 | 5266 | -25.6% | -1.5% | -7.0% | 2.1% | | |
| | 2010 | 387 | 1309 | 1696 | 5780 | 31.6% | -1.3% | 4.7% | 9.8% | | |
| | 2012 | 313 | 1292 | 1605 | 5614 | -19.1% | -1.3% | -5.4% | -2.9% | | |
| | 2017 | 428 | 1324 | 1752 | 5812 | 36.7% | 2.5% | 9.2% | 3.5% | | |
| Rogrossion Estimato | 2007 | 339 | 1326 | 1666 | | | | | | | |
| Regression Estimate | | | | | | | | | | | |
| Regression Estimate | 2017 | 402 | 1308 | 1710 | | | | | | | |
| Average Annual Change | | 1.72% | -0.14% | 0.26% | | | | | | | |

| Г | Year | | Cou | nts | | | % C | hange | |
|-----------------------|------|-------|-------|-------|------|-------|-------|-------|-------|
| South Leg | rear | NB | SB | NB+SB | INT | NB | SB | NB+SB | INT |
| | 2007 | 626 | 402 | 1028 | 5160 | | | | |
| | 2008 | 649 | 439 | 1088 | 5266 | 3.7% | 9.2% | 5.8% | 2.1% |
| | 2010 | 819 | 454 | 1273 | 5780 | 26.2% | 3.4% | 17.0% | 9.8% |
| | 2012 | 875 | 414 | 1289 | 5614 | 6.8% | -8.8% | 1.3% | -2.9% |
| | 2017 | 807 | 537 | 1344 | 5812 | -7.8% | 29.7% | 4.3% | 3.5% |
| Regression Estimate | 2007 | 682 | 406 | 1089 | | | | | |
| Regression Estimate | 2017 | 874 | 519 | 1393 | | | | | |
| Average Annual Change | | 2.50% | 2.47% | 2.49% | | | | | |

Trim/OR 174 <u>PM Peak</u>

| Year | Date | North Leg | | Sout | h Leg | East | t Leg | Wes | t Leg | Total |
|------|----------------------|-----------|----|------|-------|------|-------|------|-------|-------|
| real | Date | SB | NB | NB | SB | WB | EB | EB | WB | Totai |
| 2007 | Wednesday 31 January | 144 | 50 | 455 | 788 | 672 | 1440 | 2018 | 911 | 6478 |
| 2008 | Friday 20 June | 64 | 60 | 494 | 1051 | 424 | 1354 | 2206 | 723 | 6376 |
| 2010 | Friday 9 July | 107 | 40 | 603 | 1007 | 664 | 1334 | 2131 | 1124 | 7010 |
| 2012 | Friday 8 June | 94 | 69 | 634 | 905 | 624 | 1353 | 2024 | 1049 | 6752 |
| 2017 | Wednesday 19 April | 56 | 61 | 587 | 801 | 657 | 1284 | 1839 | 993 | 6278 |

| Γ | Year | | Cou | nts | | % Change | | | | | | |
|-----------------------|------|-------|--------|--------|---------------|----------|--------|--------|-------|--|--|--|
| North Leg | rear | NB | SB | NB+SB | INT | NB | SB | NB+SB | INT | | | |
| Γ | 2007 | 50 | 144 | 194 | 6478 | | | | | | | |
| | 2008 | 60 | 64 | 124 | 6376 | 20.0% | -55.6% | -36.1% | -1.6% | | | |
| | 2010 | 40 | 107 | 147 | 7010 | -33.3% | 67.2% | 18.5% | 9.9% | | | |
| | 2012 | 69 | 94 | 163 | 6752 | 72.5% | -12.1% | 10.9% | -3.7% | | | |
| | 2017 | 61 | 56 | 117 | 6278 | -11.6% | -40.4% | -28.2% | -7.0% | | | |
| Regression Estimate | 2007 | 52 | 114 | 166 | 6642 | | | | | | | |
| Regression Estimate | 2007 | 63 | 58 | 100 | 6475 | | | | | | | |
| Average Annual Change | | 2.00% | -6.52% | -3.09% | -0.25% | | | | | | | |
| Г | Year | | Cou | nts | % Change | | | | | | | |
| | redr | | | | | | | | | | | |

| | Voor | | 004 | | | ,o enange | | | | | |
|-----------------------|------|--------|-------|--------|------|-----------|--------|-------|-------|--|--|
| West Leg | Year | EB | WB | EB+WB | INT | EB | WB | EB+WB | INT | | |
| | 2007 | 2018 | 911 | 2929 | 6478 | | | | | | |
| | 2008 | 2206 | 723 | 2929 | 6376 | 9.3% | -20.6% | 0.0% | -1.6% | | |
| | 2010 | 2131 | 1124 | 3255 | 7010 | -3.4% | 55.5% | 11.1% | 9.9% | | |
| | 2012 | 2024 | 1049 | 3073 | 6752 | -5.0% | -6.7% | -5.6% | -3.7% | | |
| | 2017 | 1839 | 993 | 2832 | 6278 | -9.1% | -5.3% | -7.8% | -7.0% | | |
| | | | | | | | | | | | |
| Regression Estimate | 2007 | 2148 | 898 | 3045 | | | | | | | |
| Regression Estimate | 2017 | 1874 | 1062 | 2936 | | | | | | | |
| Average Annual Change | | -1.35% | 1.69% | -0.37% | | | | | | | |

| Г | Year | | Cou | nts | | % Change | | | | | | |
|-----------------------|------|--------|-------|--------|------|----------|--------|--------|-------|--|--|--|
| East Leg | fear | EB | WB | EB+WB | INT | EB | WB | EB+WB | INT | | | |
| | 2007 | 1440 | 672 | 2112 | 6478 | | | | | | | |
| | 2008 | 1354 | 424 | 1778 | 6376 | -6.0% | -36.9% | -15.8% | -1.6% | | | |
| | 2010 | 1334 | 664 | 1998 | 7010 | -1.5% | 56.6% | 12.4% | 9.9% | | | |
| | 2012 | 1353 | 624 | 1977 | 6752 | 1.4% | -6.0% | -1.1% | -3.7% | | | |
| | 2017 | 1284 | 657 | 1941 | 6278 | -5.1% | 5.3% | -1.8% | -7.0% | | | |
| | | | | | | | | | | | | |
| Regression Estimate | 2007 | 1398 | 575 | 1973 | | | | | | | | |
| Regression Estimate | 2017 | 1279 | 663 | 1942 | | | | | | | | |
| Average Annual Change | | -0.88% | 1.43% | -0.16% | | | | | | | | |

| | Year | | Cou | nts | | % Change | | | | | |
|-----------------------|------|-------|--------|-------|------|----------|--------|-------|-------|--|--|
| South Leg | rear | NB | SB | NB+SB | INT | NB | SB | NB+SB | INT | | |
| | 2007 | 455 | 788 | 1243 | 6478 | | | | | | |
| | 2008 | 494 | 1051 | 1545 | 6376 | 8.6% | 33.4% | 24.3% | -1.6% | | |
| | 2010 | 603 | 1007 | 1610 | 7010 | 22.1% | -4.2% | 4.2% | 9.9% | | |
| | 2012 | 634 | 905 | 1539 | 6752 | 5.1% | -10.1% | -4.4% | -3.7% | | |
| | 2017 | 587 | 801 | 1388 | 6278 | -7.4% | -11.5% | -9.8% | -7.0% | | |
| | | | | | | | | | | | |
| Regression Estimate | 2007 | 506 | 952 | 1458 | | | | | | | |
| Regression Estimate | 2017 | 634 | 842 | 1476 | | | | | | | |
| Average Annual Change | | 2.29% | -1.22% | 0.12% | | | | | | | |

| Time | | Perce | nt Annual Cl | hange | |
|---------|-----------|----------|--------------|--------|--------|
| Period | North Leg | West Leg | Overall | | |
| 8 hrs | 2.64% | 1.03% | -0.66% | -0.05% | 0.13% |
| AM Peak | 4.40% | 2.49% | 0.26% | 0.84% | 1.13% |
| PM Peak | -3.09% | 0.12% | -0.16% | -0.37% | -0.24% |

Appendix H SYNCHRO Capacity Analysis: 2022 Background Conditions

Background 2022 AM 2: Trim & OR174

| | ≯ | → | * | 4 | 4 | • | Ť | × | ţ | 1 | |
|-------------------------------------|-----------------|----------------|---------------|-------|--------------|-----------|-------------|-----------------|----------|-------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR | |
| ane Configurations | ۲ | <u>††</u> | 1 | ۲ | ≜ †⊅ | ሻሻ | ≜ †₽ | ۲ | † | 1 | |
| raffic Volume (vph) | 63 | 268 | 414 | 93 | 1189 | 859 | 41 | 21 | 66 | 80 | |
| uture Volume (vph) | 63 | 268 | 414 | 93 | 1189 | 859 | 41 | 21 | 66 | 80 | |
| ane Group Flow (vph) | 70 | 298 | 460 | 103 | 1335 | 954 | 95 | 23 | 73 | 89 | |
| une ereup rien (ipi) | Prot | NA | Perm | Prot | NA | Prot | NA | pm+pt | NA | Perm | |
| Protected Phases | 5 | 2 | 1 OIIII | 1 | 6 | 3 | 8 | 7 | 4 | 1 Onn | |
| Permitted Phases | 5 | 2 | 2 | | 0 | 5 | 0 | 4 | Т | 4 | |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 3 | 8 | 7 | 4 | 4 | |
| Switch Phase | 5 | 2 | 2 | | 0 | J | 0 | / | т | т | |
| Ainimum Initial (s) | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 5.0 | 10.0 | 5.0 | 10.0 | 10.0 | |
| | 12.1 | 41.2 | 41.2 | 12.5 | 41.2 | 12.2 | 42.4 | 11.9 | 17.4 | 17.4 | |
| Ainimum Split (s) | 12.1 | 50.0 | 50.0 | | | | | | | 17.4 | |
| otal Split (s) | | | | 20.0 | 55.0 | 42.0 | 43.0 | 17.0 | 18.0 | | |
| otal Split (%) | 11.5% | 38.5% | 38.5% | 15.4% | 42.3% | 32.3% | 33.1% | 13.1% | 13.8% | 13.8% | |
| ellow Time (s) | 3.3 | 5.1 | 5.1 | 3.3 | 5.1 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | |
| II-Red Time (s) | 3.8 | 2.1 | 2.1 | 4.2 | 2.1 | 3.9 | 4.1 | 3.6 | 4.1 | 4.1 | |
| ost Time Adjust (s) | -3.1 | -3.2 | -3.2 | -3.5 | -3.2 | -3.2 | -3.4 | -2.9 | -3.4 | -3.4 | |
| otal Lost Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| ead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lead | |
| ead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | |
| Recall Mode | None | C-Max | C-Max | None | C-Max | None | Max | None | Max | Max | |
| Act Effct Green (s) | 10.7 | 47.2 | 47.2 | 14.8 | 54.0 | 38.0 | 45.8 | 25.2 | 14.0 | 14.0 | |
| ctuated g/C Ratio | 0.08 | 0.36 | 0.36 | 0.11 | 0.42 | 0.29 | 0.35 | 0.19 | 0.11 | 0.11 | |
| /c Ratio | 0.50 | 0.24 | 0.56 | 0.53 | 0.95 | 0.99 | 0.08 | 0.08 | 0.38 | 0.25 | |
| control Delay | 70.0 | 29.9 | 5.4 | 64.6 | 52.3 | 73.2 | 16.9 | 25.9 | 60.3 | 1.7 | |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| otal Delay | 70.0 | 29.9 | 5.4 | 64.6 | 52.3 | 73.2 | 16.9 | 25.9 | 60.3 | 1.7 | |
| .0S | E | С | А | Е | D | E | В | С | E | А | |
| pproach Delay | | 19.7 | | _ | 53.2 | _ | 68.1 | - | 27.8 | | |
| Approach LOS | | В | | | D | | E | | C | | |
| Queue Length 50th (m) | 17.4 | 28.3 | 0.0 | 25.0 | ~180.6 | 125.8 | 4.4 | 3.4 | 17.7 | 0.0 | |
| Queue Length 95th (m) | 33.0 | 39.5 | 23.2 | 43.6 | #230.8 | #169.6 | 11.0 | 8.8 | 33.1 | 0.0 | |
| nternal Link Dist (m) | 33.0 | 222.6 | 20.2 | 40.0 | 537.2 | #107.0 | 301.4 | 0.0 | 202.0 | 0.0 | |
| Furn Bay Length (m) | 155.0 | 222.0 | 200.0 | 130.0 | JJ1.2 | 180.0 | 301.4 | 120.0 | 202.0 | 60.0 | |
| Base Capacity (vph) | 143 | 1229 | 828 | 208 | 1405 | 961 | 1122 | 301 | 192 | 357 | |
| Starvation Cap Reductn | 0 | 0 | 020 | 208 | 0 | 901 0 | 0 | | 0 | 0 | |
| | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Spillback Cap Reductn | | | | | | | | | | | |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| educed v/c Ratio | 0.49 | 0.24 | 0.56 | 0.50 | 0.95 | 0.99 | 0.08 | 0.08 | 0.38 | 0.25 | |
| ntersection Summary | | | | | | | | | | | |
| Cycle Length: 130 | | | | | | | | | | | |
| Actuated Cycle Length: 130 | | | | | | | | | | | |
| Offset: 20 (15%), Referenced to ph | ase 2:EBT an | d 6:WBT, S | tart of Greer | า | | | | | | | |
| latural Cycle: 120 | | | | | | | | | | | |
| Control Type: Actuated-Coordinate | d | | | | | | | | | | |
| laximum v/c Ratio: 0.99 | | | | | | | | | | | |
| tersection Signal Delay: 48.4 | | | | In | tersection L | OS: D | | | | | |
| tersection Capacity Utilization 81. | .8% | | | IC | U Level of S | Service D | | | | | |
| nalysis Period (min) 15 | | | | | | | | | | | |
| Volume exceeds capacity, queu | ue is theoretic | ally infinite. | | | | | | | | | |
| Queue shown is maximum after | | | | | | | | | | | |
| 95th percentile volume exceeds | | elle mav he | longer | | | | | | | | |
| Queue shown is maximum after | | cae may be | ionger. | | | | | | | | |
| | | | | | | | | | | | |
| | | | | | | A | | • | | | |
| Ø1 • • Ø2 | 2 (R) | | | | | ♥ Ø4 | | [▲] øз | | | |

| Ø1 | ∎ 🖘 Ø2 (R) | ₽ Ø4 | 1 Ø3 |
|------|---------------------|-----------------|-------------|
| 20 s | 50 s | 18 s | 42 s |
| | ← # 6 (R) | [†] ø8 | ₩ø7 |
| 15 s | 55 s | 43 s | 17 s |

Background 2022 AM 1: Trim & Jeanne D'Arc

| | ٦ | - | \rightarrow | - | - | • | 1 | Ť | 1 | ¥ | ŧ | - |
|-----------------------------------|-------|------|---------------|-------|---------------|-------|------|------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | \$ | | | \$ | | | \$ | | | \$ | |
| Sign Control | | Stop | | | Stop | | | Stop | | | Stop | |
| Traffic Volume (vph) | 8 | 4 | 82 | 74 | 8 | 0 | 106 | 20 | 19 | 0 | 9 | 3 |
| Future Volume (vph) | 8 | 4 | 82 | 74 | 8 | 0 | 106 | 20 | 19 | 0 | 9 | 3 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 9 | 4 | 91 | 82 | 9 | 0 | 118 | 22 | 21 | 0 | 10 | 3 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total (vph) | 104 | 91 | 161 | 13 | | | | | | | | |
| Volume Left (vph) | 9 | 82 | 118 | 0 | | | | | | | | |
| Volume Right (vph) | 91 | 0 | 21 | 3 | | | | | | | | |
| Hadj (s) | -0.47 | 0.21 | 0.10 | -0.10 | | | | | | | | |
| Departure Headway (s) | 3.9 | 4.6 | 4.5 | 4.4 | | | | | | | | |
| Degree Utilization, x | 0.11 | 0.12 | 0.20 | 0.02 | | | | | | | | |
| Capacity (veh/h) | 868 | 735 | 773 | 758 | | | | | | | | |
| Control Delay (s) | 7.5 | 8.2 | 8.6 | 7.5 | | | | | | | | |
| Approach Delay (s) | 7.5 | 8.2 | 8.6 | 7.5 | | | | | | | | |
| Approach LOS | А | А | А | А | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Delay | | | 8.1 | | | | | | | | | |
| Level of Service | | | А | | | | | | | | | |
| Intersection Capacity Utilization | | | 33.3% | ICI | J Level of Se | rvice | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Background 2022 PM 2: Trim Rd & OR 174

| | ۶ | + | ¥ | 4 | + | • | t | 1 | ţ | 1 | |
|--|-------------|-------------|------------|-------------|--------------|-------------|-------------|------------|---------------|-------------|-----|
| ane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR | |
| ne Configurations | ۲ | †† | 1 | ۲ | ∱1 ≽ | ኘኘ | A⊅ | ۲. | 1 | 1 | |
| affic Volume (vph) | 58 | 1111 | 1172 | 70 | 428 | 462 | 57 | 19 | 80 | 68 | |
| ture Volume (vph) | 58 | 1111 | 1172 | 70 | 428 | 462 | 57 | 19 | 80 | 68 | |
| ine Group Flow (vph) | 64 | 1234 | 1302 | 78 | 496 | 513 | 167 | 21 | 89 | 76 | |
| rn Type | Prot | NA | Free | Prot | NA | Prot | NA | pm+pt | NA | Perm | |
| otected Phases | 5 | 2 | | 1 | 6 | 3 | 8 | 7 | 4 | | |
| ermitted Phases | | | Free | | | | | 4 | | 4 | |
| tector Phase | 5 | 2 | | 1 | 6 | 3 | 8 | 7 | 4 | 4 | |
| vitch Phase | | | | | | | | | | | |
| nimum Initial (s) | 5.0 | 10.0 | | 5.0 | 10.0 | 5.0 | 10.0 | 5.0 | 10.0 | 10.0 | |
| nimum Split (s) | 12.1 | 41.2 | | 12.5 | 41.2 | 12.2 | 42.4 | 11.9 | 17.4 | 17.4 | |
| tal Split (s) | 16.0 | 54.0 | | 16.0 | 54.0 | 33.0 | 43.0 | 17.0 | 27.0 | 27.0 | |
| tal Split (%) | 12.3% | 41.5% | | 12.3% | 41.5% | 25.4% | 33.1% | 13.1% | 20.8% | 20.8% | |
| llow Time (s) | 3.3 | 5.1 | | 3.3 | 5.1 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | |
| -Red Time (s) | 3.8 | 2.1 | | 4.2 | 2.1 | 3.9 | 4.1 | 3.6 | 4.1 | 4.1 | |
| st Time Adjust (s) | -3.1 | -3.2 | | -3.5 | -3.2 | -3.2 | -3.4 | -2.9 | -3.4 | -3.4 | |
| tal Lost Time (s) | -3.1 | -3.2 | | -3.5 | -3.2 4.0 | -3.2 4.0 | -3.4 4.0 | -2.9 | -3.4 4.0 | -3.4 | |
| | 4.0 Lead | | | 4.0 Lead | | | 4.0 Lead | | 4.0 Lead | 4.0 Lead | |
| ad/Lag | Yes | Lag Yes | | Yes | Lag Yes | Lag | Yes | Lag Yes | | Yes | |
| ad-Lag Optimize? | | | | | | Yes | | | Yes | | |
| call Mode | None | C-Max | 120.0 | None | C-Max | None | Max | None | Max | Max | |
| t Effct Green (s) | 11.5 | 54.8 | 130.0 | 12.0 | 55.1 | 27.1 | 44.0 | 34.1 | 23.0 | 23.0 | |
| tuated g/C Ratio | 0.09 | 0.42 | 1.00 | 0.09 | 0.42 | 0.21 | 0.34 | 0.26 | 0.18 | 0.18 | |
| Ratio | 0.43 | 0.86 | 0.86 | 0.50 | 0.35 | 0.75 | 0.15 | 0.06 | 0.28 | 0.17 | |
| ntrol Delay | 65.2 | 43.1 | 6.8 | 67.9 | 27.3 | 55.6 | 13.4 | 23.9 | 49.2 | 0.8 | |
| eue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| tal Delay | 65.2 | 43.1 | 6.8 | 67.9 | 27.3 | 55.6 | 13.4 | 23.9 | 49.2 | 0.8 | |
| S | E | D | А | E | С | E | В | С | D | А | |
| proach Delay | | 25.4 | | | 32.8 | | 45.3 | | 26.6 | | |
| proach LOS | | С | | | С | | D | | С | | |
| ieue Length 50th (m) | 15.7 | 159.5 | 0.0 | 19.3 | 47.4 | 63.1 | 6.0 | 3.1 | 20.0 | 0.0 | |
| ieue Length 95th (m) | 30.5 | #205.0 | 0.0 | 35.8 | 62.1 | 81.9 | 14.5 | 8.2 | 36.0 | 0.0 | |
| ernal Link Dist (m) | | 313.9 | | | 321.3 | | 154.2 | | 204.2 | | |
| rn Bay Length (m) | 150.0 | | 200.0 | 130.0 | | 230.0 | | 120.0 | | 55.0 | |
| se Capacity (vph) | 157 | 1429 | 1517 | 160 | 1429 | 733 | 1098 | 368 | 315 | 450 | |
| arvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| illback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| orage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| duced v/c Ratio | 0.41 | 0.86 | 0.86 | 0.49 | 0.35 | 0.70 | 0.15 | 0.06 | 0.28 | 0.17 | |
| | 0.111 | 0.00 | 0.00 | 0117 | 0.00 | 0110 | 0.10 | 0.00 | 0120 | 0.1.7 | |
| ersection Summary cle Length: 130 | | | | | | | | | | | |
| tuated Cycle Length: 130 fset: 0 (0%), Referenced to phas | e 2:EBT and | 6:WBT, Star | t of Green | | | | | | | | |
| tural Cycle: 110 | 4 | | | | | | | | | | |
| ntrol Type: Actuated-Coordinate | u | | | | | | | | | | |
| iximum v/c Ratio: 0.86 | | | | | | | | | | | |
| ersection Signal Delay: 29.9 | 00/ | | | | ersection LC | | | | | | |
| ersection Capacity Utilization 75 | .8% | | | IC | U Level of S | ervice D | | | | | |
| alysis Period (min) 15 | | | | | | | | | | | |
| 95th percentile volume exceeds Queue shown is maximum after | | eue may be | longer. | | | | | | | | |
| | 00 174 | | | | | | | | | | |
| lits and Phases: 2: Trim Rd & | OR 174 | | | | | | | | | | |
| lits and Phases: 2: Trim Rd & | | | | | | 04 | | | A (72) | | |
| lits and Phases: 2: Trim Rd & | | | | | | Ø4 | | | 1 øз | | |
| lits and Phases: 2: Trim Rd & | | | | | | ∲_Ø4 7 s | | | ▲ Ø3 33 s | 1 - | |
| lits and Phases: 2: Trim Rd & |) | | | | | | | | | | ¥ø7 |

Background 2022 PM 1: Trim Rd & Jeanne D'Arc

| | , | | | | | | | | | | | |
|-----------------------------------|-------|------|--------------|-------|---------------|--------|------|------|------|------|------|------|
| | ≯ | - | \mathbf{i} | ∢ | - | • | • | † | 1 | 1 | Ļ | ~ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | \$ | | | \$ | | | \$ | | | \$ | |
| Sign Control | | Stop | | | Stop | | | Stop | | | Stop | |
| Traffic Volume (vph) | 7 | 6 | 133 | 31 | 3 | 0 | 81 | 8 | 45 | 1 | 11 | 4 |
| Future Volume (vph) | 7 | 6 | 133 | 31 | 3 | 0 | 81 | 8 | 45 | 1 | 11 | 4 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 8 | 7 | 148 | 34 | 3 | 0 | 90 | 9 | 50 | 1 | 12 | 4 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total (vph) | 163 | 37 | 149 | 17 | | | | | | | | |
| Volume Left (vph) | 8 | 34 | 90 | 1 | | | | | | | | |
| Volume Right (vph) | 148 | 0 | 50 | 4 | | | | | | | | |
| Hadj (s) | -0.50 | 0.22 | -0.05 | -0.10 | | | | | | | | |
| Departure Headway (s) | 3.8 | 4.7 | 4.3 | 4.4 | | | | | | | | |
| Degree Utilization, x | 0.17 | 0.05 | 0.18 | 0.02 | | | | | | | | |
| Capacity (veh/h) | 902 | 728 | 799 | 764 | | | | | | | | |
| Control Delay (s) | 7.6 | 7.9 | 8.2 | 7.5 | | | | | | | | |
| Approach Delay (s) | 7.6 | 7.9 | 8.2 | 7.5 | | | | | | | | |
| Approach LOS | А | А | А | А | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Delay | | | 7.9 | | | | | | | | | |
| Level of Service | | | А | | | | | | | | | |
| Intersection Capacity Utilization | | | 37.4% | ICI | J Level of Se | ervice | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Appendix I SYNCHRO and SIDRA Capacity Analysis: 2024 Background Conditions

Background 2024 AM 3: Jeanne D'Arc

| | _ | > | 4 | + | • | 1 | |
|-----------------------------------|------|------|-----------|------|--------------|------------|--|
| | | • | - | 1107 | 1 | - | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR | |
| Lane Configurations | 4 | | | ्र | Y | | |
| Traffic Volume (veh/h) | 22 | 941 | 45 | 37 | 106 | 2 | |
| Future Volume (Veh/h) | _ 22 | 941 | 45 | 37 | 106 | 2 | |
| Sign Control | Free | | | Free | Stop | | |
| Grade | 0% | | | 0% | 0% | | |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | |
| Hourly flow rate (vph) | 23 | 991 | 47 | 39 | 112 | 2 | |
| Pedestrians | | | | | | | |
| Lane Width (m) | | | | | | | |
| Walking Speed (m/s) | | | | | | | |
| Percent Blockage | | | | | | | |
| Right turn flare (veh) | | | | | | | |
| Median type | None | | | None | | | |
| Median storage veh) | | | | | | | |
| Upstream signal (m) | | | | | | | |
| pX, platoon unblocked | | | | | | | |
| vC, conflicting volume | | | 23 | | 652 | 518 | |
| vC1, stage 1 conf vol | | | 20 | | 002 | 0.0 | |
| vC2, stage 2 conf vol | | | | | | | |
| vCu, unblocked vol | | | 23 | | 652 | 518 | |
| tC, single (s) | | | 4.1 | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | т. I | | U.T | 0.2 | |
| tF (s) | | | 2.2 | | 3.5 | 3.3 | |
| p0 queue free % | | | 2.2 97 | | 73 | 3.3 100 | |
| | | | 1592 | | 420 | 557 | |
| cM capacity (veh/h) | | | 1092 | | 420 | 557 | |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | | | | |
| Volume Total | 1014 | 86 | 114 | | | | |
| Volume Left | 0 | 47 | 112 | | | | |
| Volume Right | 991 | 0 | 2 | | | | |
| cSH | 1700 | 1592 | 422 | | | | |
| Volume to Capacity | 0.60 | 0.03 | 0.27 | | | | |
| Queue Length 95th (m) | 0.0 | 0.7 | 8.2 | | | | |
| Control Delay (s) | 0.0 | 4.1 | 16.7 | | | | |
| Lane LOS | | A | С | | | | |
| Approach Delay (s) | 0.0 | 4.1 | 16.7 | | | | |
| Approach LOS | 0.0 | | C | | | | |
| Intersection Summary | | | | | | | |
| | | | 1.0 | | | | |
| Average Delay | | | 1.9 | | | | |
| Intersection Capacity Utilization | | | 75.7% | ICI | U Level of S | ervice | |
| Analysis Period (min) | | | 15 | | | | |

Background 2024 PM 3: Jeanne D'Arc

| Movement EBT EBR WBL WBT NBL NBR Lane Configurations 1 4 4 542 19 15 83 6 Future Volume (veh/h) 48 542 19 15 83 6 Sign Control Free Free Stop 0% 0% 0% Grade 0% 0.95 0.95 0.95 0.95 0.95 0.95 Houry flow rate (vph) 51 571 20 16 87 6 Peak Hour Factor 0.95 0.95 0.95 0.95 0.95 0.95 Hane Width (m) Walking Speed (m/s) Free None None Movement Weaking Speed (m/s) Percent Blockage 71 392 336 VC, conflicting volume 51 392 336 VC1, stage 1 conf vol 51 392 336 VC1, stage 1 conf vol VC2, stage 2 conf vol <t< th=""><th></th><th></th><th>~</th><th>4</th><th>+</th><th>•</th><th>~</th></t<> | | | ~ | 4 | + | • | ~ |
|--|-----------------------------------|----------|------|------|------|--------------|--------|
| Lane Configurations 4 $4'$ $4'$ Traffic Volume (veh/h) 48 542 19 15 83 6 Future Volume (Veh/h) 48 542 19 15 83 6 Future Volume (Veh/h) 48 542 19 15 83 6 Sign Control Free Free Stop 0% 0% 0% Grade 0% 0.95 0.95 0.95 0.95 0.95 0.95 Hourly flow rate (vph) 51 571 20 16 87 6 Pedestrians Petestrians Petestrians Petestrians Petestrians Petestrians Lane Width (m) Walking Speed (m/s) Petestrians Petestrians Petestrians Petestrians Lane Width (m) Walking Speed (m/s) None None None None Median storage veh) Upstream signal (m) Py, platoon unblocked Vc, conflicting volume 51 392 336 VC1, unblocked vol 51 392 336 Py Kd 4.1 6. | Mayamant | - EDT | FDD | - | | NDI | • |
| Traffic Volume (veh/h) 48 542 19 15 83 6 Future Volume (Veh/h) 48 542 19 15 83 6 Sign Control Free Stop 83 6 6 Grade 0% 0% 0% 0% 0% Peak Hour Factor 0.95< | | | FRK | WBL | | | NRK |
| Future Volume (Veh/h) 48 542 19 15 83 6 Sign Control Free Free Stop Grade 0% <td></td> <td>10</td> <td>E10</td> <td>10</td> <td></td> <td></td> <td>4</td> | | 10 | E10 | 10 | | | 4 |
| Sign Control Free Free Stop Grade 0% <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> | | | | | | | |
| Grade 0% 0% 0% Peak Hour Factor 0.95 0.95 0.95 0.95 0.95 0.95 Hourly flow rate (vph) 51 571 20 16 87 6 Pedestrians | | | 542 | 19 | | | 0 |
| Peak Hour Factor 0.95 | | | | | | | |
| Hourly flow rate (vph) 51 571 20 16 87 6 Pedestrians Lane Width (m) | | | 0.05 | 0.05 | | | 0.05 |
| Pedestrians Lane Width (m) Walking Speed (m/s) Percent Blockage Right turn flare (veh) Median type None Median type Some Median type Some Volume Storage veh) Upstream signal (m) pX, platoon unblocked vc. conflicting volume vC2, stage 1 conf vol VC2, stage 2 conf vol vC2, stage 2 conf vol vc. vC2, stage (s) 4.1 6.4 6.2 tC, single (s) 4.1 6.4 6.2 tC, single (s) 2.2 3.5 3.3 p0 queue free % 99 86 99 cM capacity (veh/h) 1555 604 706 Direction, Lane # EB 1 WB 1 NB 1 Volume Total 622 36 93 Volume Right 571 0 6 cSH 1700 1555 610 | | | | | | | |
| Lane Width (m) Walking Speed (m/s) Percent Blockage Right turn flare (veh) Median storage veh) Upstream signal (m) pX, platoon unblocked vC, conflicting volume S1 392 336 vC1, stage 1 conf vol vC2, stage 2 conf vol vC2, stage 3 2 conf vol vC3 1 392 336 tC, single (s) tC, 2 stage 3 2 conf vol tF (s) 2 2 3.5 3.3 p0 queue free % 99 86 99 cM capacity (veh/h) 1 555 604 706 Direction, Lane # EB 1 WB 1 NB 1 Volume Total 622 36 93 Volume Left 0 20 87 Volume Right 571 0 6 cSH 1700 1555 610 Volume to Capacity 0.37 0.01 0.15 Queue Length 95th (m) 0.0 4.1 12.0 Lane LOS A B Approach Delay (s) 0.0 4.1 12.0 | | 51 | 5/1 | 20 | 16 | 87 | 6 |
| Walking Speed (m/s) Percent Blockage Right turn flare (veh) Median type None Median storage veh) Upstream signal (m) pX, platoon unblocked vC, conflicting volume 51 vC, stage 1 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol vC4, unblocked vol tC, single (s) tC, single (s) tC, stage (s) tF (s) p0 queue free % tP (s) tO (control belay (s) Volume total 622 36 Volume total 622 Volume Total 622 0 20 871 0 0 20 871 0 0 20 1000 1555 610 100 Volume Total 622 0 20 100 1555 610 100 Volume Right 571 0 CSH 1700 1555 | | | | | | | |
| Percent Blockage Right turn flare (veh) Median type None Median type None Median storage veh) None Upstream signal (m) None pX, platoon unblocked 51 392 336 vC, conflicting volume 51 392 336 vC1, stage 1 conf vol 51 392 336 vC2, stage 2 conf vol VC1 51 392 336 vC2, stage (s) 4.1 6.4 6.2 6.2 tF (s) 2.2 3.5 3.3 90 99 86 99 cd capacity (veh/h) 1555 604 706 706 706 Direction, Lane # EB 1 WB 1 NB 1 Volume Total 622 36 93 706 Volume Total 622 36 93 706 706 706 706 Volume Total 622 36 93 706 706 706 706 706 706 706 706 706 706 706 706 706 | | | | | | | |
| Right turn flare (veh) None None Median type None None Median storage veh) Upstream signal (m) None pX, platoon unblocked 51 392 336 vC1, stage 1 conf vol vc2, stage 2 conf vol vc2, stage 2 conf vol vc2, stage 2 conf vol vC2, stage 2 conf vol 51 392 336 tC, single (s) 4.1 6.4 6.2 tC, stage (s) 1 55 3.3 p0 queue free % 99 86 99 cd capacity (veh/h) 1555 604 706 Direction, Lane # EB 1 WB 1 NB 1 Volume Total 622 36 93 Volume Total 622 36 93 Volume Right 571 0 6 CSH 1700 1555 610 Volume to capacity 0.37 0.01 0.15 Queue Length 95th (m) 0.0 0.3 4.1 Control Delay (s) 0.0 4.1 12.0 Lane LOS A B <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<> | | | | | | | |
| Median type None None Median storage veh) Upstream signal (m) <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> | | | | | | | |
| Median storage veh) Upstream signal (m) pX, platoon unblocked 51 392 336 vC, conflicting volume 51 392 336 vC1, stage 1 conf vol vc2, stage 2 conf vol vc2, stage 2 conf vol vc2, unblocked vol 51 392 336 vCu, unblocked vol 51 392 336 vc2, stage 2 conf vol vc2, unblocked vol 51 392 336 tC, single (s) 4.1 6.4 6.2 tc tc, 2 stage (s) tc, 2 stage (veh/h) 1555 604 706 51 51 53 3.3 53 53 53 53 53 53 53 53 53 53 54 54 56 56 56 56 56 56 56 56 56 56 57 56 56 57 56 57 56 57 56 57 56 57 56 57 56 57 56 57 56 57 56 57 56 57 | | | | | | | |
| Upstream signal (m) pX, platoon unblocked vC, conflicting volume 51 392 336 vC1, stage 1 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol vC2, unblocked vol 51 392 336 vC2, stage 2 conf vol 51 392 336 vC2, stage 2 conf vol 51 392 336 vC2, unblocked vol 51 392 336 tC, 2 stage (s) 4.1 6.4 6.2 tF (s) 2.2 3.5 3.3 90 p0 queue free % 99 86 99 cM capacity (veh/h) 1555 604 706 Direction, Lane # EB 1 WB 1 NB 1 Volume Total 622 36 93 Volume Total 622 36 93 Volume Right 571 0 6 cSH 1700 1555 610 Volume Right 571 0 6 cSH 1700 1555 610 Volume to Capacity 0.37 0.01 <td></td> <td>None</td> <td></td> <td></td> <td>None</td> <td></td> <td></td> | | None | | | None | | |
| pX, platoon unblocked 51 392 336 vC, conflicting volume 51 392 336 vC1, stage 1 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol vCu, unblocked vol 51 392 336 tC, single (s) 4.1 6.4 6.2 tC, 2 stage (s) | | | | | | | |
| vC, conflicting volume 51 392 336 vC1, stage 1 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol vCu, unblocked vol 51 392 336 tC, single (s) 4.1 6.4 6.2 tC, 2 stage (s) vC2, stage (s) vC2, stage (s) vC2, stage (s) tF (s) 2.2 3.5 3.3 p0 queue free % 99 86 99 cM capacity (veh/h) 1555 604 706 Direction, Lane # EB1 WB 1 NB 1 VOIume Total 622 36 93 Volume Total 622 36 93 Volume Left 0 20 87 Volume Right 571 0 6 c 51 20 20 Volume Right 0.37 0.01 0.15 0 20 87 20 2 | | | | | | | |
| vC1, stage 1 conf vol vC2, stage 2 conf vol vCu, unblocked vol 51 392 336 tC, single (s) 4.1 6.4 6.2 tC, 2 stage (s) 1 6.4 6.2 tF (s) 2.2 3.5 3.3 3 99 86 99 6 64 706 <t< td=""><td>pX, platoon unblocked</td><td></td><td></td><td></td><td></td><td></td><td></td></t<> | pX, platoon unblocked | | | | | | |
| vC2, stage 2 conf vol vCu, unblocked vol 51 392 336 tC, single (s) 4.1 6.4 6.2 tC, 2 stage (s) tF (s) 2.2 3.5 3.3 p0 queue free % 99 86 99 cM capacity (veh/h) 1555 604 706 Direction, Lane # EB 1 WB 1 NB 1 Volume Total 622 36 93 Volume Total 622 36 93 Volume Left 0 20 87 Volume Right 571 0 6 cSH 1700 1555 610 Volume to Capacity 0.37 0.01 0.15 Queue Length 95th (m) 0.0 0.3 4.1 Control Delay (s) 0.0 4.1 12.0 | | | | 51 | | 392 | 336 |
| vCu, unblocked vol 51 392 336 tC, single (s) 4.1 6.4 6.2 tC, 2 stage (s) | | | | | | | |
| tC, single (s) 4.1 6.4 6.2 tC, 2 stage (s) 2.2 3.5 3.3 p0 queue free % 99 86 99 cM capacity (veh/h) 1555 604 706 Direction, Lane # EB 1 WB 1 NB 1 Volume Total 622 36 93 Volume Total 622 36 93 Volume Right 571 0 6 cSH 1700 1555 610 Volume to Capacity 0.37 0.01 0.15 Queue Length 95th (m) 0.0 0.3 4.1 Control Delay (s) 0.0 4.1 12.0 Lane LOS A B Approach Delay (s) 0.0 | | | | | | | |
| tC, 2 stage (s) tF (s) 2.2 3.5 3.3 p0 queue free % 99 86 99 cM capacity (veh/h) 1555 604 706 Direction, Lane # EB 1 WB 1 NB 1 Volume Total 622 36 93 Volume Total 622 36 93 Volume Right 571 0 6 cSH 1700 1555 610 Volume to Capacity 0.37 0.01 0.15 Queue Length 95th (m) 0.0 0.3 4.1 Control Delay (s) 0.0 4.1 12.0 Lane LOS A B Approach Delay (s) 0.0 | vCu, unblocked vol | | | 51 | | 392 | 336 |
| tC, 2 stage (s) tF (s) 2.2 3.5 3.3 p0 queue free % 99 86 99 cM capacity (veh/h) 1555 604 706 Direction, Lane # EB 1 WB 1 NB 1 Volume Total 622 36 93 Volume Total 622 36 93 Volume Right 571 0 6 cSH 1700 1555 610 Volume to Capacity 0.37 0.01 0.15 Queue Length 95th (m) 0.0 0.3 4.1 Control Delay (s) 0.0 4.1 12.0 Lane LOS A B Approach Delay (s) 0.0 | tC, single (s) | | | 4.1 | | 6.4 | 6.2 |
| tF (s) 2.2 3.5 3.3 p0 queue free % 99 86 99 cM capacity (veh/h) 1555 604 706 Direction, Lane # EB 1 WB 1 NB 1 Volume Total 622 36 93 Volume Total 622 36 93 | | | | | | | |
| p0 queue free % 99 86 99 cM capacity (veh/h) 1555 604 706 Direction, Lane # EB 1 WB 1 NB 1 Volume Total 622 36 93 Volume Total 622 36 93 | tF (s) | | | 2.2 | | 3.5 | 3.3 |
| cM capacity (veh/h) 1555 604 706 Direction, Lane # EB 1 WB 1 NB 1 Volume Total 622 36 93 Volume Total 0 20 87 Volume Right 571 0 6 cSH 1700 1555 610 Volume to Capacity 0.37 0.01 0.15 Queue Length 95th (m) 0.0 0.3 4.1 Control Delay (s) 0.0 4.1 12.0 Lane LOS A B Approach Delay (s) 0.0 4.1 12.0 | | | | | | 86 | |
| Direction, Lane # EB 1 WB 1 NB 1 Volume Total 622 36 93 Volume Left 0 20 87 Volume Right 571 0 6 cSH 1700 1555 610 Volume to Capacity 0.37 0.01 0.15 Queue Length 95th (m) 0.0 0.3 4.1 Control Delay (s) 0.0 4.1 12.0 Lane LOS A B Approach Delay (s) 0.0 4.1 | | | | | | 604 | 706 |
| Volume Total 622 36 93 Volume Left 0 20 87 Volume Right 571 0 6 cSH 1700 1555 610 Volume to Capacity 0.37 0.01 0.15 Queue Length 95th (m) 0.0 0.3 4.1 Control Delay (s) 0.0 4.1 12.0 Lane LOS A B Approach Delay (s) 0.0 4.1 12.0 | Direction, Lane # | EB 1 | WB 1 | NB 1 | | | |
| Volume Left 0 20 87 Volume Right 571 0 6 cSH 1700 1555 610 Volume to Capacity 0.37 0.01 0.15 Queue Length 95th (m) 0.0 0.3 4.1 Control Delay (s) 0.0 4.1 12.0 Lane LOS A B Approach Delay (s) 0.0 4.1 12.0 | · · · | | | | | | |
| Volume Right 571 0 6 cSH 1700 1555 610 Volume to Capacity 0.37 0.01 0.15 Queue Length 95th (m) 0.0 0.3 4.1 Control Delay (s) 0.0 4.1 12.0 Lane LOS A B Approach Delay (s) 0.0 4.1 12.0 | | | | | | | |
| cSH 1700 1555 610 Volume to Capacity 0.37 0.01 0.15 Queue Length 95th (m) 0.0 0.3 4.1 Control Delay (s) 0.0 4.1 12.0 Lane LOS A B Approach Delay (s) 0.0 4.1 12.0 | | | | | | | |
| Volume to Capacity 0.37 0.01 0.15 Queue Length 95th (m) 0.0 0.3 4.1 Control Delay (s) 0.0 4.1 12.0 Lane LOS A B Approach Delay (s) 0.0 4.1 12.0 | | | | | | | |
| Queue Length 95th (m) 0.0 0.3 4.1 Control Delay (s) 0.0 4.1 12.0 Lane LOS A B Approach Delay (s) 0.0 4.1 12.0 | | | | | | | |
| Control Delay (s) 0.0 4.1 12.0 Lane LOS A B Approach Delay (s) 0.0 4.1 12.0 | Queue Length 95th (m) | | | | | | |
| Lane LOS A B Approach Delay (s) 0.0 4.1 12.0 | | | | | | | |
| Approach Delay (s) 0.0 4.1 12.0 | Lane LOS | 0.0 | | | | | |
| | | 0.0 | | | | | |
| | | 0.0 | 4.1 | | | | |
| | | | | D | | | |
| Intersection Summary | | | | | | | |
| Average Delay 1.7 | | | | | | | |
| Intersection Capacity Utilization 49.9% ICU Level of Service | Intersection Capacity Utilization | | | | ICI | J Level of S | ervice |
| Analysis Period (min) 15 | Analysis Period (min) | | | 15 | | | |

MOVEMENT SUMMARY

Site: [Jeanne D'Arc/Trim]

Background 2024 AM Roundabout

| Move | Movement Performance - Vehicles | | | | | | | | | | | |
|--------|---------------------------------|----------------|-----|-------|---------|----------|----------|----------|--------|-----------|---------|--|
| Mov | OD | Demand | | Deg. | Average | Level of | 95% Back | | Prop. | Effective | Average | |
| ID | Mov | Total veh/h | HV | Satn | Delay | Service | Vehicles | Distance | Queued | Stop Rate | Speed | |
| South | · Trim | ven/n | % | v/c | sec | _ | veh | m | _ | per veh | km/h | |
| 1 | L2 | 139 | 2.0 | 0.100 | 7.5 | LOS A | 0.6 | 4.4 | 0.18 | 0.55 | 46.7 | |
| 2 | T1 | 21 | 2.0 | 0.100 | 3.0 | LOS A | 0.6 | 4.4 | 0.18 | 0.55 | 46.5 | |
| 3 | R2 | 926 | 2.0 | 0.507 | 2.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.36 | 48.5 | |
| Appro | bach | 1086 | 2.0 | 0.507 | 3.1 | LOS A | 0.6 | 4.4 | 0.03 | 0.39 | 48.2 | |
| East: | Jeanne D' | Arc | | | | | | | | | | |
| 4 | L2 | 124 | 2.0 | 0.124 | 8.3 | LOS A | 0.7 | 5.2 | 0.39 | 0.58 | 46.2 | |
| 5 | T1 | 17 | 2.0 | 0.124 | 3.8 | LOS A | 0.7 | 5.2 | 0.39 | 0.58 | 46.0 | |
| 6 | R2 | 3 | 2.0 | 0.124 | 3.8 | LOS A | 0.7 | 5.2 | 0.39 | 0.58 | 45.0 | |
| Appro | bach | 144 | 2.0 | 0.124 | 7.7 | LOS A | 0.7 | 5.2 | 0.39 | 0.58 | 46.1 | |
| North | : Trim | | | | | | | | | | | |
| 7 | L2 | 2 | 2.0 | 0.012 | 8.5 | LOS A | 0.1 | 0.4 | 0.41 | 0.45 | 47.7 | |
| 8 | T1 | 7 | 2.0 | 0.012 | 4.0 | LOS A | 0.1 | 0.4 | 0.41 | 0.45 | 47.6 | |
| 9 | R2 | 3 | 2.0 | 0.012 | 4.0 | LOS A | 0.1 | 0.4 | 0.41 | 0.45 | 46.5 | |
| Appro | bach | 13 | 2.0 | 0.012 | 4.8 | LOS A | 0.1 | 0.4 | 0.41 | 0.45 | 47.3 | |
| West: | Jeanne D | 'Arc | | | | | | | | | | |
| 10 | L2 | 8 | 2.0 | 0.085 | 8.1 | LOS A | 0.5 | 3.6 | 0.35 | 0.43 | 48.2 | |
| 11 | T1 | 35 | 2.0 | 0.085 | 3.6 | LOS A | 0.5 | 3.6 | 0.35 | 0.43 | 48.1 | |
| 12 | R2 | 58 | 2.0 | 0.085 | 3.6 | LOS A | 0.5 | 3.6 | 0.35 | 0.43 | 47.0 | |
| Appro | bach | 101 | 2.0 | 0.085 | 4.0 | LOS A | 0.5 | 3.6 | 0.35 | 0.43 | 47.4 | |
| All Ve | hicles | 1344 | 2.0 | 0.507 | 3.7 | LOS A | 0.7 | 5.2 | 0.09 | 0.41 | 47.9 | |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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MOVEMENT SUMMARY

Site: [Jeanne D'Arc/Trim]

Background 2024 PM Roundabout

| Move | Movement Performance - Vehicles | | | | | | | | | | | |
|-----------|---------------------------------|--------------------------|------------------|---------------------|-------------------------|---------------------|-------------------------------|---------------------------|-----------------|-----------------------------------|--------------------------|--|
| Mov ID | OD Mov | Demand Total veh/h | Flows HV % | Deg. Satn v/c | Average Delay sec | Level of Service | 95% Back o Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h | |
| South | | | | | | | | | | | | |
| 1 | L2 | 101 | 2.0 | 0.072 | 7.6 | LOS A | 0.4 | 3.0 | 0.23 | 0.55 | 46.4 | |
| 2 | T1 | 8 | 2.0 | 0.072 | 3.1 | LOS A | 0.4 | 3.0 | 0.23 | 0.55 | 46.3 | |
| 3 | R2 | 532 | 2.0 | 0.291 | 2.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.36 | 48.5 | |
| Appro | ach | 641 | 2.0 | 0.291 | 3.2 | LOS A | 0.4 | 3.0 | 0.04 | 0.40 | 48.1 | |
| East: | Jeanne D' | Arc | | | | | | | | | | |
| 4 | L2 | 83 | 2.0 | 0.080 | 8.0 | LOS A | 0.5 | 3.3 | 0.32 | 0.56 | 46.4 | |
| 5 | T1 | 13 | 2.0 | 0.080 | 3.5 | LOS A | 0.5 | 3.3 | 0.32 | 0.56 | 46.2 | |
| 6 | R2 | 2 | 2.0 | 0.080 | 3.5 | LOS A | 0.5 | 3.3 | 0.32 | 0.56 | 45.2 | |
| Appro | ach | 98 | 2.0 | 0.080 | 7.3 | LOS A | 0.5 | 3.3 | 0.32 | 0.56 | 46.3 | |
| North: | Trim | | | | | | | | | | | |
| 7 | L2 | 3 | 2.0 | 0.013 | 8.1 | LOS A | 0.1 | 0.5 | 0.34 | 0.44 | 47.9 | |
| 8 | T1 | 8 | 2.0 | 0.013 | 3.6 | LOS A | 0.1 | 0.5 | 0.34 | 0.44 | 47.7 | |
| 9 | R2 | 4 | 2.0 | 0.013 | 3.7 | LOS A | 0.1 | 0.5 | 0.34 | 0.44 | 46.6 | |
| Appro | ach | 16 | 2.0 | 0.013 | 4.5 | LOS A | 0.1 | 0.5 | 0.34 | 0.44 | 47.5 | |
| West: | Jeanne D | 'Arc | | | | | | | | | | |
| 10 | L2 | 7 | 2.0 | 0.128 | 7.9 | LOS A | 0.8 | 5.6 | 0.30 | 0.41 | 48.5 | |
| 11 | T1 | 60 | 2.0 | 0.128 | 3.4 | LOS A | 0.8 | 5.6 | 0.30 | 0.41 | 48.3 | |
| 12 | R2 | 96 | 2.0 | 0.128 | 3.4 | LOS A | 0.8 | 5.6 | 0.30 | 0.41 | 47.2 | |
| Appro | ach | 163 | 2.0 | 0.128 | 3.6 | LOS A | 0.8 | 5.6 | 0.30 | 0.41 | 47.7 | |
| All Ve | hicles | 918 | 2.0 | 0.291 | 3.8 | LOS A | 0.8 | 5.6 | 0.12 | 0.42 | 47.8 | |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Appendix J SYNCHRO and SIDRA Capacity Analysis: 2029 Background Conditions

Background 2029 AM 3: Jeanne D'Arc

| | | ~ | 4 | + | • | ~ |
|-----------------------------------|------|----------|-------|------|--------------|--------|
| | | • | - | |) | - |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | €Î. | | | र्भ | Y | |
| Traffic Volume (veh/h) | 22 | 1060 | 45 | 37 | 112 | 2 |
| Future Volume (Veh/h) | 22 | 1060 | 45 | 37 | 112 | 2 |
| Sign Control | Free | | | Free | Stop | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Hourly flow rate (vph) | 23 | 1116 | 47 | 39 | 118 | 2 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | | | None | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | | | 23 | | 714 | 581 |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | | | 23 | | 714 | 581 |
| tC, single (s) | | | 4.1 | | 6.4 | 6.2 |
| tC, 2 stage (s) | | | | | | |
| tF (s) | | | 2.2 | | 3.5 | 3.3 |
| p0 queue free % | | | 97 | | 69 | 100 |
| cM capacity (veh/h) | | | 1592 | | 386 | 514 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | | | 011 |
| Volume Total | 1139 | 86 | 120 | | | |
| Volume Left | 0 | 86 47 | 120 | | | |
| | | | | | | |
| Volume Right | 1116 | 0 | 2 | | | |
| cSH | 1700 | 1592 | 388 | | | |
| Volume to Capacity | 0.67 | 0.03 | 0.31 | | | |
| Queue Length 95th (m) | 0.0 | 0.7 | 9.8 | | | |
| Control Delay (s) | 0.0 | 4.1 | 18.4 | | | |
| Lane LOS | | А | С | | | |
| Approach Delay (s) | 0.0 | 4.1 | 18.4 | | | |
| Approach LOS | | | С | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 1.9 | | | |
| Intersection Capacity Utilization | | | 83.8% | ICI | J Level of S | ervice |
| Analysis Period (min) | | | 15 | 100 | 2 20101010 | |
| | | | 15 | | | |

Background 2029 PM 3: Jeanne D'Arc

| | - | ~ | 4 | + | • | 1 |
|-----------------------------------|------------------|------|----------|----------|-----------------|--------|
| Movement | EBT | EBR | ▼ WBL | WBT | NBL | NBR |
| Lane Configurations | | EDK | VVDL | <u> </u> | | NDK |
| Traffic Volume (veh/h) | 1 3 48 | 642 | 19 | 4 15 | "" 87 | 6 |
| Future Volume (Veh/h) | 48 | 642 | 19 | 15 | 87 | 6 |
| Sign Control | Free | 042 | 17 | Free | Stop | 0 |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Hourly flow rate (vph) | 51 | 676 | 20 | 16 | 92 | 6 |
| Pedestrians | 51 | 070 | 20 | 10 | 72 | 0 |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | | | None | | |
| Median storage veh) | NULLE | | | NOLIC | | |
| Upstream signal (m) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | | | 51 | | 445 | 389 |
| vC1, stage 1 conf vol | | | JI | | 445 | 307 |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | | | 51 | | 445 | 389 |
| tC, single (s) | | | 4.1 | | 6.4 | 6.2 |
| tC, 2 stage (s) | | | т. і | | U.T | 0.2 |
| tF (s) | | | 2.2 | | 3.5 | 3.3 |
| p0 queue free % | | | 99 | | 84 | 99 |
| cM capacity (veh/h) | | | 1555 | | 563 | 659 |
| | | | | | 505 | 037 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | | | |
| Volume Total | 727 | 36 | 98 | | | |
| Volume Left | 0 | 20 | 92 | | | |
| Volume Right | 676 | 0 | 6 | | | |
| cSH | 1700 | 1555 | 568 | | | |
| Volume to Capacity | 0.43 | 0.01 | 0.17 | | | |
| Queue Length 95th (m) | 0.0 | 0.3 | 4.7 | | | |
| Control Delay (s) | 0.0 | 4.1 | 12.6 | | | |
| Lane LOS | | А | В | | | |
| Approach Delay (s) | 0.0 | 4.1 | 12.6 | | | |
| Approach LOS | | | В | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 1.6 | | | |
| Intersection Capacity Utilization | | | 56.7% | ICI | J Level of S | ervice |
| Analysis Period (min) | | | 15 | | | |
| | | | 10 | | | |

MOVEMENT SUMMARY

Site: [Jeanne D'Arc/Trim]

Background 2029 AM Roundabout

| Move | ement Pe | rformance - | Vehicle | es | | | | | | | |
|-----------|-----------|-----------------|---------|--------------|------------------|---------------------|------------------------|----------|-----------------|------------------------|------------------|
| Mov ID | OD Mov | Demand Total | ΗV | Deg. Satn | Average Delay | Level of Service | 95% Back o Vehicles | Distance | Prop. Queued | Effective Stop Rate | Average Speed |
| South | · Trim | veh/h | % | v/c | sec | _ | veh | m | _ | per veh | km/h |
| 1 | L2 | 208 | 2.0 | 0.148 | 7.6 | LOS A | 1.0 | 6.8 | 0.25 | 0.55 | 46.4 |
| 2 | T1 | 21 | 2.0 | 0.148 | 3.1 | LOSA | 1.0 | 6.8 | 0.25 | 0.55 | 46.2 |
| 3 | R2 | 980 | 2.0 | 0.537 | 2.5 | LOSA | 0.0 | 0.0 | 0.00 | 0.36 | 48.5 |
| Appro | | 1209 | 2.0 | 0.537 | 3.4 | LOS A | 1.0 | 6.8 | 0.05 | 0.40 | 48.0 |
| East: | Jeanne D' | Arc | | | | | | | | | |
| 4 | L2 | 124 | 2.0 | 0.141 | 8.8 | LOS A | 0.8 | 6.0 | 0.47 | 0.61 | 46.1 |
| 5 | T1 | 17 | 2.0 | 0.141 | 4.3 | LOS A | 0.8 | 6.0 | 0.47 | 0.61 | 46.0 |
| 6 | R2 | 13 | 2.0 | 0.141 | 4.3 | LOS A | 0.8 | 6.0 | 0.47 | 0.61 | 45.0 |
| Appro | ach | 154 | 2.0 | 0.141 | 7.9 | LOS A | 0.8 | 6.0 | 0.47 | 0.61 | 46.0 |
| North | : Trim | | | | | | | | | | |
| 7 | L2 | 2 | 2.0 | 0.012 | 8.8 | LOS A | 0.1 | 0.4 | 0.45 | 0.47 | 47.6 |
| 8 | T1 | 7 | 2.0 | 0.012 | 4.3 | LOS A | 0.1 | 0.4 | 0.45 | 0.47 | 47.4 |
| 9 | R2 | 3 | 2.0 | 0.012 | 4.4 | LOS A | 0.1 | 0.4 | 0.45 | 0.47 | 46.3 |
| Appro | ach | 13 | 2.0 | 0.012 | 5.1 | LOS A | 0.1 | 0.4 | 0.45 | 0.47 | 47.2 |
| West: | Jeanne D | 'Arc | | | | | | | | | |
| 10 | L2 | 8 | 2.0 | 0.118 | 8.1 | LOS A | 0.7 | 5.2 | 0.36 | 0.43 | 48.2 |
| 11 | T1 | 64 | 2.0 | 0.118 | 3.6 | LOS A | 0.7 | 5.2 | 0.36 | 0.43 | 48.0 |
| 12 | R2 | 68 | 2.0 | 0.118 | 3.6 | LOS A | 0.7 | 5.2 | 0.36 | 0.43 | 46.9 |
| Appro | ach | 141 | 2.0 | 0.118 | 3.9 | LOS A | 0.7 | 5.2 | 0.36 | 0.43 | 47.5 |
| All Ve | hicles | 1517 | 2.0 | 0.537 | 3.9 | LOS A | 1.0 | 6.8 | 0.12 | 0.42 | 47.8 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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MOVEMENT SUMMARY

Site: [Jeanne D'Arc/Trim]

Background 2029 PM Roundabout

| Move | ement Pe | rformance - | Vehicle | es | | | | | | | |
|-----------|-----------|--------------------------|------------------|---------------------|-------------------------|---------------------|-------------------------------|---------------------------|-----------------|-----------------------------------|--------------------------|
| Mov ID | OD Mov | Demand Total veh/h | Flows HV % | Deg. Satn v/c | Average Delay sec | Level of Service | 95% Back o Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South | : Trim | | | | | | | | | | |
| 1 | L2 | 145 | 2.0 | 0.106 | 7.8 | LOS A | 0.6 | 4.6 | 0.31 | 0.57 | 46.1 |
| 2 | T1 | 8 | 2.0 | 0.106 | 3.3 | LOS A | 0.6 | 4.6 | 0.31 | 0.57 | 46.0 |
| 3 | R2 | 563 | 2.0 | 0.308 | 2.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.36 | 48.5 |
| Appro | bach | 717 | 2.0 | 0.308 | 3.5 | LOS A | 0.6 | 4.6 | 0.07 | 0.41 | 48.0 |
| East: | Jeanne D' | Arc | | | | | | | | | |
| 4 | L2 | 83 | 2.0 | 0.084 | 8.3 | LOS A | 0.5 | 3.5 | 0.38 | 0.57 | 46.2 |
| 5 | T1 | 13 | 2.0 | 0.084 | 3.7 | LOS A | 0.5 | 3.5 | 0.38 | 0.57 | 46.1 |
| 6 | R2 | 2 | 2.0 | 0.084 | 3.7 | LOS A | 0.5 | 3.5 | 0.38 | 0.57 | 45.1 |
| Appro | ach | 98 | 2.0 | 0.084 | 7.6 | LOS A | 0.5 | 3.5 | 0.38 | 0.57 | 46.2 |
| North | : Trim | | | | | | | | | | |
| 7 | L2 | 3 | 2.0 | 0.014 | 8.3 | LOS A | 0.1 | 0.5 | 0.38 | 0.45 | 47.8 |
| 8 | T1 | 8 | 2.0 | 0.014 | 3.8 | LOS A | 0.1 | 0.5 | 0.38 | 0.45 | 47.6 |
| 9 | R2 | 4 | 2.0 | 0.014 | 3.9 | LOS A | 0.1 | 0.5 | 0.38 | 0.45 | 46.5 |
| Appro | bach | 16 | 2.0 | 0.014 | 4.7 | LOS A | 0.1 | 0.5 | 0.38 | 0.45 | 47.3 |
| West: | Jeanne D | 'Arc | | | | | | | | | |
| 10 | L2 | 7 | 2.0 | 0.181 | 7.9 | LOS A | 1.2 | 8.4 | 0.31 | 0.40 | 48.4 |
| 11 | T1 | 111 | 2.0 | 0.181 | 3.4 | LOS A | 1.2 | 8.4 | 0.31 | 0.40 | 48.3 |
| 12 | R2 | 117 | 2.0 | 0.181 | 3.4 | LOS A | 1.2 | 8.4 | 0.31 | 0.40 | 47.2 |
| Appro | ach | 235 | 2.0 | 0.181 | 3.5 | LOS A | 1.2 | 8.4 | 0.31 | 0.40 | 47.7 |
| All Ve | hicles | 1065 | 2.0 | 0.308 | 3.9 | LOS A | 1.2 | 8.4 | 0.15 | 0.42 | 47.7 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Appendix K Multimodal Level of Service Analysis: Existing Conditions

Multi-Modal Level of Service - Intersections Form

Consultant Scenario Comments PARSONSProjectJeanne D'Arc @ TrimDateYear 2022 Before LRT Conditions

Petries Landing I 7/12/2018

| | INTERSECTIONS | | Existing C | Conditions | | | | | |
|-------------|--------------------------------------|-----------------------------|--------------------------------------|-----------------------------|--------------------------------------|--|--|--|--|
| | Crossing Side | NORTH | SOUTH | EAST | WEST | | | | |
| | Lanes | 0 - 2 | 0 - 2 | 0 - 2 | 0 - 2 | | | | |
| | Median | No Median - 2.4 m | No Median - 2.4 m | No Median - 2.4 m | No Median - 2.4 m | | | | |
| | Conflicting Left Turns | Permissive | Permissive | Permissive | Permissive | | | | |
| | Conflicting Right Turns | Permissive or yield control | Permissive or yield control | Permissive or yield control | Permissive or yield control | | | | |
| | Right Turns on Red (RToR) ? | RTOR allowed | RTOR allowed | RTOR allowed | RTOR allowed | | | | |
| | Ped Signal Leading Interval? | No | No | No | No | | | | |
| ian | Right Turn Channel | No Channel | No Channel | No Channel | No Channel | | | | |
| str | Corner Radius | 10-15m | 10-15m | 10-15m | 10-15m | | | | |
| Pedestrian | Crosswalk Type | Std transverse markings | Std transverse markings | Std transverse markings | Std transverse markings | | | | |
| - | PETSI Score | 85 | 85 | 85 | 85 | | | | |
| | Ped. Exposure to Traffic LoS | В | В | В | В | | | | |
| | Cycle Length | | | | | | | | |
| | Effective Walk Time | | | | | | | | |
| | Average Pedestrian Delay | | | | | | | | |
| | Pedestrian Delay LoS | - | - | - | - | | | | |
| | | В | В | В | В | | | | |
| | Level of Service | В | | | | | | | |
| | Approach From | NORTH | SOUTH | EAST | WEST | | | | |
| | Bicycle Lane Arrangement on Approach | Mixed Traffic | Curb Bike Lane, Cycletrack or MUP | Mixed Traffic | Curb Bike Lane, Cycletrack or MUP | | | | |
| | Right Turn Lane Configuration | ≤ 50 m | Not Applicable | ≤ 50 m | Not Applicable | | | | |
| | Right Turning Speed | ≤ 25 km/h | ≤ 25 km/h | ≤ 25 km/h | ≤ 25 km/h | | | | |
| a | Cyclist relative to RT motorists | D | Not Applicable | D | Not Applicable | | | | |
| V cl | Separated or Mixed Traffic | Mixed Traffic | Separated | Mixed Traffic | Separated | | | | |
| Bicycle | Left Turn Approach | No lane crossed | 1 lane crossed | No lane crossed | 1 lane crossed | | | | |
| | Operating Speed | > 50 to < 60 km/h | > 50 to < 60 km/h | > 50 to < 60 km/h | ≥ 60 km/h | | | | |
| | Left Turning Cyclist | С | D | С | E | | | | |
| | | D | D | D | E | | | | |
| | Level of Service | | E | - | | | | | |

| Consultant | PARSONS | | | Petrie's Landing I | |
|------------|---|----------|------------------------|------------------------------|-----------------------|
| Scenario | Jeanne D'Arc East of Trim | | Date | 5/18/2018 | |
| Comments | Existing Conditions and Possible | | - | | |
| | Improvements | | J | | |
| SEGMENTS | | Street A | Section Site Access | Section Former Cul-de-Sac | Section Mid-block |
| | Sidewalk Width Boulevard Width | | ≥ 2 m < 0.5 | ≥ 2 m < 0.5 | ≥ 2 m < 0.5 |
| | Avg Daily Curb Lane Traffic Volume | | ≤ 3000 | ≤ 3000 | ≤ 3000 |
| Pedestrian | Operating Speed On-Street Parking | | > 30 to 50 km/h no | > 30 to 50 km/h no | > 50 to 60 km/h no |
| est | Exposure to Traffic PLoS | - | В | В | С |
| ede | Effective Sidewalk Width Pedestrian Volume | | 2.0 m | 2.0 m | 2.0 m |
| | Crowding PLoS | | - | - | - |
| | Level of Service | | - | - | - |
| | Type of Cycling Facility | | Mixed Traffic | Mixed Traffic | Mixed Traffic |
| | Number of Travel Lanes | | 2-3 lanes total | 2-3 lanes total | 2-3 lanes total |
| | Operating Speed | | ≤ 40 km/h | >40 to <50 km/h | ≥ 50 to 60 km/h |
| | # of Lanes & Operating Speed LoS | | В | D | E |
| <u>e</u> | Bike Lane (+ Parking Lane) Width | | | | |
| Bicycle | Bike Lane Width LoS | Α | - | - | - |
| | Bike Lane Blockages | | | | |
| | Blockage LoS | | - | - | - |
| | Median Refuge Width (no median = < 1.8 m) | | | | |
| | No. of Lanes at Unsignalized Crossing Sidestreet Operating Speed | | | | |
| | Unsignalized Crossing - Lowest LoS | | - | - | - |
| | Level of Service | | - | - | - |

Multi-Modal Level of Service - Segments Form

Appendix L Multimodal Level of Service Analysis: Planned Network

Multi-Modal Level of Service - Intersections Form

| Consultant Scenario | PARSONS Jeanne D'Arc @ Trim | | Project Date | Petries Landing 6/26/2018 | g l | | | |
|------------------------|--------------------------------------|---------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--|--|--|
| Comments | Post-2022 Conditions: LRT Over | | | | | | | |
| | OR 174 Ramp, Jeanne D'Arc Rou | ndabout | | | | | | |
| | INTERSECTIONS | | Jeanne D'Arc@1 | rim Roundabou | ıt | | | |
| | Crossing Side | NORTH | SOUTH | EAST | WEST | | | |
| | Lanes Median | 0 - 2 No Median - 2.4 m | 3 Median > 2.4 m | 3 Median > 2.4 m | 0 - 2 Median > 2.4 m | | | |
| | Conflicting Left Turns | Permissive | Permissive | Permissive | Permissive | | | |
| | Conflicting Right Turns | Permissive or yield control | Permissive or yield control | Permissive or yield control | Permissive or yield control | | | |
| | Right Turns on Red (RToR) ? | RTOR allowed | RTOR allowed | RTOR allowed | RTOR allowed | | | |
| | Ped Signal Leading Interval? | No | No | No | No | | | |
| ian | Right Turn Channel | No Channel | Conventional with Receiving Lane | No Channel | No Channel | | | |
| str | Corner Radius | 10-15m | 10-15m | 10-15m | 10-15m | | | |
| Pedestrian | Crosswalk Type | Zebra stripe hi-vis markings | Zebra stripe hi-vis markings | Zebra stripe hi-vis markings | Zebra stripe hi-vis markings | | | |
| | PETSI Score | 93 | 79 | 78 | 93 | | | |
| | Ped. Exposure to Traffic LoS | А | В | В | А | | | |
| | Cycle Length | 0 | 0 | 0 | 0 | | | |
| | Effective Walk Time | | | | | | | |
| | Average Pedestrian Delay | | | | | | | |
| | Pedestrian Delay LoS | - | - | - | - | | | |
| | Level of Service | A | В | В | A | | | |
| | | В | | | | | | |
| | Approach From | NORTH | SOUTH | EAST | WEST | | | |
| | Bicycle Lane Arrangement on Approach | Mixed Traffic | Curb Bike Lane, Cycletrack or MUP | Curb Bike Lane, Cycletrack or MUP | Curb Bike Lane, Cycletrack or MUP | | | |
| | Right Turn Lane Configuration | ≤ 50 m | Not Applicable | Not Applicable | Not Applicable | | | |
| | Right Turning Speed | ≤ 25 km/h | Not Applicable | Not Applicable | Not Applicable | | | |
| U | Cyclist relative to RT motorists | D | Not Applicable | Not Applicable | Not Applicable | | | |
| ycl | Separated or Mixed Traffic | Mixed Traffic | Separated | Separated | Separated | | | |
| Bicycle | Left Turn Approach | No lane crossed | No lane crossed | No lane crossed | No lane crossed | | | |
| | Operating Speed | ≤ 40 km/h | ≤ 40 km/h | ≤ 40 km/h | ≤ 40 km/h | | | |
| | Left Turning Cyclist | В | В | В | В | | | |
| | | D | В | В | В | | | |
| | Level of Service | | | C | | | | |

Multi-Modal Level of Service - Segments Form

| Consultant Scenario Comments | PARSONS Jeanne D'Arc East of Trim Post-2022 Conditions: LRT Overpas OR 174 Ramp, Jeanne D'Arc Rounda | | Project Date | Petrie's Landing I 6/26/2018 | |
|------------------------------------|---|----------|---------------------------|---------------------------------|---------------------------|
| SEGMENTS | | Street A | Site Access South Side | Former Cul-de-Sac South Side | Mid-block A South Side |
| | Sidewalk Width Boulevard Width | | ≥ 2 m > 2 m | ≥ 2 m > 2 m | ≥ 2 m < 0.5 |
| | Avg Daily Curb Lane Traffic Volume | | ≤ 3000 | ≤ 3000 | > 3000 |
| Pedestrian | Operating Speed On-Street Parking | | > 30 to 50 km/h no | > 30 to 50 km/h no | > 30 to 50 km/h no |
| est | Exposure to Traffic PLoS | - | А | А | С |
| eq | Effective Sidewalk Width | | | | |
| ۵. | Pedestrian Volume | | | | |
| | Crowding PLoS | | - | - | - |
| | Level of Service | | - | - | - |
| | Type of Cycling Facility | | Mixed Traffic | Mixed Traffic | Mixed Traffic |
| | Number of Travel Lanes | | 2-3 lanes total | 2-3 lanes total | 2-3 lanes total |
| | Operating Speed | | ≤ 40 km/h | >40 to <50 km/h | >40 to <50 km/h |
| | # of Lanes & Operating Speed LoS | | В | D | D |
| Bicycle | Bike Lane (+ Parking Lane) Width | | | | |
| Č | Bike Lane Width LoS | E | - | - | - |
| <u>.</u> | Bike Lane Blockages | | | | |
| | Blockage LoS | | - | - | - |
| | Median Refuge Width (no median = < 1.8 m) | | | ≥ 1.8 m refuge | < 1.8 m refuge |
| | No. of Lanes at Unsignalized Crossing | | | ≤ 3 lanes | ≤ 3 lanes |
| | Sidestreet Operating Speed Unsignalized Crossing - Lowest LoS | | | ≤ 40 km/h A | ≥ 65 km/h E |
| | Level of Service | | - | D | E |

Appendix M Transportation Demand Management Checklist

Introduction

The City of Ottawa's *Transportation Impact Assessment (TIA) Guidelines* (specifically Module 4.3—Transportation Demand Management) requires proponents of qualifying developments to assess the context, need and opportunity for transportation demand management (TDM) measures at their development. The guidelines require that proponents complete the City's **TDM Measures Checklist**, at a minimum, to identify any TDM measures being proposed.

The remaining sections of this document are:

- Using the Checklist
- Glossary
- TDM Measures Checklist: Non-Residential Developments
- TDM Measures Checklist: Residential developments

Using the Checklist

The City's *TIA Guidelines* are designed so that *Module 3.1—Development-Generated Travel Demand*, *Module 4.1—Development Design*, and *Module 4.2—Parking* are complete before a proponent begins *Module 4.3—Transportation Demand Management*.

Within Module 4.3, *Element 4.3.1—Context for TDM* and *Element 4.3.2—Need and Opportunity* are intended to create an understanding of the need for any TDM measures, and of the results they are expected to achieve or support. Once those two elements are complete, proponents begin *Element 4.3.3—TDM Program* that requires proponents to identify proposed TDM measures using the **TDM Measures Checklist**, at a minimum. The *TIA Guidelines* note that the City may require additional analysis for large or complex development proposals, or those that represent a higher degree of performance risk; as well, proponents proposing TDM measures for a new development must also propose an implementation plan that addresses planning and coordination, funding and human resources, timelines for action, performance targets and monitoring requirements.

This **TDM Measures Checklist** document includes two actual checklists, one for non-residential developments (office, institutional, retail or industrial) and one for residential developments (multi-family, condominium or subdivision). Readers may download the applicable checklist in electronic format and complete it electronically, or print it out and complete it by hand. As an alternative, they may create a freestanding document that lists the TDM measures being proposed and provides additional detail on them, including an implementation plan as required by the City's *TIA Guidelines*.

Each measure in the checklist is numbered for easy reference. Each measure is also flagged as:

- BASIC The measure is generally feasible and effective, and in most cases would benefit the development and its users.
- **BETTER** The measure could maximize support for users of sustainable modes, and optimize development performance.
- The measure is one of the most dependably effective tools to encourage the use of sustainable modes.

Readers are encouraged to contact the City of Ottawa's TDM Officer for any guidance and assistance they require to complete this checklist.

Glossary

This glossary defines and describes the following measures that are identified in the **TDM Measures Checklist**:

TDM program management

- Program coordinator
- Travel surveys

Parking

Priced parking

Walking & cycling

- Information on walking/cycling routes & destinations
- Bicycle skills training
- Valet bike parking

Transit

- Transit information
- Transit fare incentives
- Enhanced public transit service
- Private transit service

Ridesharing

- Ridematching service
- Carpool parking price incentives
- Vanpool service

Carsharing & bikesharing

- Bikeshare stations & memberships
- Carshare vehicles & memberships

TDM marketing & communications

- Multimodal travel information
- Personalized trip planning
- Promotions

Other incentives & amenities

- Emergency ride home
- Alternative work arrangements
- Local business travel options
- Commuter incentives
- On-site amenities

For further information on selecting and implementing TDM measures (particularly as they apply to non-residential developments, with a focus on workplaces), readers may find it helpful to consult Transport Canada's *Workplace Travel Plans: Guidance for Canadian Employers*, which can be downloaded in English and French from the ACT Canada website at www.actcanada.com/resources/act-resources.

TDM program management

While some TDM measures can be implemented with a minimum of effort through routine channels (e.g. parking or human resources), more complex measures or a larger development site may warrant assigning responsibility for TDM program coordination to a designated person either inside or outside the implementing organization. Similarly, some TDM measures are more effective if they are targeted or customized for specific audiences, and would benefit from the collection of related information.

Program coordinator. This person is charged with day-to-day TDM program development and implementation. Only in very large employers with thousands of workers is this likely to be a full-time, dedicated position. Usually, it is added to an existing role in parking, real estate, human resources or environmental management. In practice, this role may be called TDM coordinator, commute trip reduction coordinator or employee transportation coordinator. The City of Ottawa can identify external resources (e.g. non-profit organizations or consultants) that could provide these services.

Travel surveys. Travel surveys are most commonly conducted at workplaces, but can be helpful in other settings. They identify how and why people travel the way they do, and what barriers and opportunities exist for different behaviours. They usually capture the following information:

- Personal data including home address or postal code, destination, job type or function, employment status (full-time, part-time and/or teleworker), gender, age and hours of work
- Commute information including distance or time for the trip between home and work, usual methods of commuting, and reasons for choosing them
- Barriers and opportunities including why other commuting methods are unattractive, willingness to consider other options, and what improvements to other options could make them more attractive

Parking

Priced parking. Charging for parking is typically among the most effective ways of getting drivers to consider other travel options. While drivers may not support parking fees, they can be more accepting if the revenues are used to improve other travel options (e.g. new showers and change rooms, improved bicycle parking or subsidized transit passes). At workplaces or daytime destinations, parking discounts (e.g. early bird specials, daily passes that cost significantly less than the equivalent hourly charge, monthly passes that cost significantly less than the equivalent hourly charge, monthly passes that cost significantly less than the equivalent daily charge) encourage long-term parking and discourage the use of other travel options. For residential uses, unbundling parking costs from dwelling purchase, lease or rental costs provides an incentive for residents to own fewer cars, and can reduce car use and the costs of parking provision.

Walking & cycling

Active transportation options like cycling and walking are particularly attractive for short trips (typically up to 5 km and 2 km, respectively). Other supportive factors include an active, health-conscious audience, and development proximity to high-quality walking and cycling networks. Common challenges to active transportation include rain, darkness, snowy or icy conditions, personal safety concerns, the potential for bicycle theft, and a lack of shower and change facilities for those making longer trips.

Information on walking/cycling routes & destinations. Ottawa, Gatineau and the National Capital Commission all publish maps to help people identify the most convenient and comfortable walking or cycling routes.

Bicycle skills training. Potential cyclists can be intimidated by the need to ride on roads shared with motor vehicles. This barrier can be reduced or eliminated by offering cycling skills training to interested cyclists (e.g. CAN-BIKE certification courses).

Valet bike parking. For large events, temporary "valet parking" areas can be easily set up to maximize convenience and security for cyclists. Experienced local non-profit groups can help.

Transit

Transit information. Difficulty in finding or understanding basic information on transit fares, routes and schedules can prevent people from trying transit. Employers can help by providing online links to OC Transpo and STO websites. Transit users also appreciate visible maps and schedules of transit routes that serve the site; even better, a screen that shows real-time transit arrival information is particularly useful at sites with many transit users and an adjacent transit stop or station.

Transit fare incentives. Free or subsidized transit fares are an attractive incentive for nontransit riders to try transit. Many non-users are unsure of how to pay a fare, and providing tickets or a preloaded PRESTO card (or, for special events, pre-arranging with OC Transpo that transit fares are included with event tickets) overcome that barrier.

Enhanced public transit service. OC Transpo may adjust transit routes, stop locations, service hours or frequencies for an agreed fee under contract, or at no cost where warranted by the potential ridership increase. Information provided by a survey of people who travel to a given development can support these decisions.

Private transit service. At remote suburban or rural workplaces, a poor transit connection to the nearest rapid transit station can be an obstacle for potential transit users, and an employer in this situation could initiate a private shuttle service to make transit use more feasible or attractive. Other circumstances where a shuttle makes sense include large special events, or a residential development for people with limited independent mobility who still require regular access to shops and services.

Ridesharing

Ridesharing's potential is greatest in situations where transit ridership is low, where parking costs are high, and/or where large numbers of car commuters (e.g. employees or full-time students) live reasonably far from the workplace.

Ridematching service. Potential carpoolers in Ottawa are served by www.OttawaRideMatch.com, an online service to help people find carpool partners. Employers can arrange for a dedicated portal where their employees can search for potential carpool partners only among their colleagues, if they desire. Some very large employers may establish internal ridematching services, to maximize employee uptake and corporate control.

Ridematching service providers typically include a waiver to relieve employers of liability when their employees start carpooling through a ridematching service. Ridesharing with co-workers also tends to eliminate security concerns.

Carpool parking price incentives. Discounted parking fees for carpools can be an extra incentive to rideshare.

Vanpool service. Vanpools operate in the Toronto and Vancouver metropolitan areas, where vans that carry up to about ten occupants are driven by one of the vanpool members. Vanpools tend to operate on a cost-recovery basis, and are most practical for long-distance commutes where transit is not an option. Current legislation in Ontario does not permit third-party (i.e. private or non-profit) vanpool services, but does permit employers to operate internal vanpools.

Carsharing & bikesharing

Bikeshare station & memberships. VeloGO Bike Share and Right Bike both operate bikesharing services in Ottawa. Developments that would benefit from having a bikeshare station installed at or near their development may negotiate directly with either service provider.

Carshare vehicles & memberships. VRTUCAR and Zipcar both operate carsharing services in Ottawa, for use by the general public or by businesses as an alternative to corporate fleets. Carsharing services offer 24-hour access, self-serve reservation systems, itemized monthly billings, and outsourcing of all financing, insurance, maintenance and administrative responsibilities.

► TDM marketing & communications

Multimodal travel information. Aside from mode-specific information discussed elsewhere in this document, multimodal information that identifies and explains the full range of travel options available to people can be very influential—especially when provided at times and locations where individuals are actively choosing among those options. Examples include: employees when their employer is relocating, or when they are joining a new employer; students when they are starting a program at a new institution; visitors or customers travelling to an unfamiliar destination, or when faced with new options (e.g. shuttle services or parking restrictions); and residents when they purchase or occupy a residence that is new to them.

Personalized trip planning. As an extension to the simple provision of information, this technique (also known as *individualized marketing*) is effective in helping people make more sustainable travel choices. The approach involves identifying who is most likely to change their travel choices (notably relocating employees, students or residents) giving them customized information, training and incentives to support them in making that change. It may be conducted with assistance from an external service provider with the necessary skills, and delivered in a variety of settings including workplaces and homes.

Promotions. Special events and incentives can raise awareness and encourage individuals to examine and try new travel options.

- Special events can help attract attention, build participation and celebrate successes. Events that have been held in Ottawa include Earth Day (in April) Bike to Work Month (in May), Environment Week (early June), International Car Free Day (September 22), and Canadian Ridesharing Week (October). At workplaces or educational institutions, similarly effective internal events could include workshops, lunch-and-learns, inter-departmental challenges, pancake breakfasts, and so on.
- Incentives can encourage trial of sustainable modes, and might include loyalty rewards for duration or consistency of activity (e.g. 1,000 km commuted by bicycle), participation prizes (e.g. for completing a survey or joining a special event), or personal recognition that highlights individual accomplishments.

Other incentives & amenities

Emergency ride home. This measure assures non-driving commuters that they will be able to get home quickly and conveniently in case of family emergency (or in some workplaces, in case of unexpected overtime, severe weather conditions, or the early departure of a carpool driver) by offering a chit or reimbursement for taxi, carshare or rental car usage. Limits on annual usage or cost per employee may be set, although across North America the actual rates of usage are typically very low.

Alternative work arrangements. A number of alternatives to the standard 9-to-5, Monday-to-Friday workweek can support sustainable commuting (and work-life balance) at workplaces:

- Flexible working hours allow transit commuters to take advantage of the fastest and most convenient transit services, and allow potential carpoolers to include people who work slightly different schedules in their search for carpool partners. They also allow active commuters to travel at least one direction in daylight, either in the morning or the afternoon, during the winter.
- Compressed workweeks allow employees to work their required hours over fewer days (e.g. five days in four, or ten days in nine), eliminating the need to commute on certain days. For employees, this can promote work-life balance and gives flexibility for appointments. For employers, this can permit extended service hours as well as reduced parking demands if employees stagger their days off.
- Telework is a normal part of many workplaces. It helps reduce commuting activity, and can lead to significant cost savings through workspace sharing. Telework initiatives involve many stakeholders, and may face as much resistance as support within an organization. Consultation, education and training are helpful.

Local business travel options. A common obstacle for people who might prefer to not drive to work is that their employer requires them to bring a car to work so they can make business trips during the day. Giving employees convenient alternatives to private cars for local business travel during the workday makes walking, cycling, transit or carpooling in someone else's car more practical.

- Walking and cycling—Active transportation can be a convenient and enjoyable way to make short business trips. They can also reduce employer expenses, although they may require extra travel time. Providing a fleet of shared bikes, or reimbursing cyclists for the kilometres they ride, are inexpensive ways to validate their choice.
- Public transit—Transit can be convenient and inexpensive compared to driving.
 OC Transpo's PRESTO cards are transferable among employees and automatically reloadable, making them the perfect tool for enabling transit use during the day.
- Ridesharing—When multiple employees attend the same off-site meeting or event, they can be reminded to carpool whenever possible.
- Taxis or ride-hailing—Taxis and ride-hailing can eliminate parking costs, save time and eliminate collision liability concerns. Taxi chits eliminate cash transactions and minimize paperwork.
 - *Fleet vehicles or carsharing*—Fleet vehicles can be cost-effective for high travel volumes, while carsharing is a great option for less frequent trips.
 - Interoffice shuttles—Employers with multiple worksites in the region could use a shuttle service to move people as well as mail or supplies.
 - *Videoconferencing*—New technologies mean that staying in the office to hold meetings electronically is more viable, affordable and productive than ever.

Commuter incentives. Financial incentives can help create a level playing field and support commuting by sustainable modes. A "commuting allowance" given to all employees as a taxable benefit is one such incentive; employees who choose to drive could then be charged for parking, while other employees could use the allowance for transit fares or cycling equipment, or for spending or saving. (Note that in the United States this practice is known as "parking cash-out," and is popular because commuting allowances are not taxable up to a certain limit). Alternatively, a monthly commuting allowance for non-driving employees would give drivers an incentive to choose a different commuting mode. Another practical incentive for active commuters or transit users is to offer them discounted "rainy day" parking passes for a small number of days each month.

On-site amenities. Developments that offer services to limit employees' need for a car during their commute (e.g. to drop off clothing at the dry cleaners) or during their workday (e.g. to buy lunch) can free employees to make the commuting decision that otherwise works best for them.

TDM Measures Checklist:

Residential Developments (multi-family, condominium or subdivision)

Legend

BASIC The measure is generally feasible and effective, and in most cases would benefit the development and its users

BETTER The measure could maximize support for users of sustainable modes, and optimize development performance

The measure is one of the most dependably effective tools to encourage the use of sustainable modes

| | TDM | measures: Residential developments | Check if proposed & add descriptions |
|---------|-------|--|---|
| | 1. | TDM PROGRAM MANAGEMENT | |
| | 1.1 | Program coordinator | |
| BASIC ★ | 1.1.1 | Designate an internal coordinator, or contract with an external coordinator | |
| | 1.2 | Travel surveys | |
| BETTER | 1.2.1 | Conduct periodic surveys to identify travel-related behaviours, attitudes, challenges and solutions, and to track progress | |
| | 2. | WALKING AND CYCLING | |
| | 2.1 | Information on walking/cycling routes & des | tinations |
| BASIC | 2.1.1 | Display local area maps with walking/cycling access routes and key destinations at major entrances (multi-family, condominium) | |
| | 2.2 | Bicycle skills training | |
| BETTER | 2.2.1 | Offer on-site cycling courses for residents, or subsidize off-site courses | |

| | TDM | measures: Residential developments | Check if proposed & add descriptions |
|----------|-------|---|--|
| | 3. | TRANSIT | |
| | 3.1 | Transit information | |
| BASIC | 3.1.1 | Display relevant transit schedules and route maps at entrances (multi-family, condominium) | |
| BETTER | 3.1.2 | Provide real-time arrival information display at entrances (multi-family, condominium) | ✓ After LRT openning |
| | 3.2 | Transit fare incentives | |
| BASIC ★ | 3.2.1 | Offer PRESTO cards preloaded with one monthly transit pass on residence purchase/move-in, to encourage residents to use transit | During first 6 months after LRT openning |
| BETTER | 3.2.2 | Offer at least one year of free monthly transit passes on residence purchase/move-in | |
| | 3.3 | Enhanced public transit service | |
| BETTER ★ | 3.3.1 | Contract with OC Transpo to provide early transit services until regular services are warranted by occupancy levels (subdivision) | |
| | 3.4 | Private transit service | |
| BETTER | 3.4.1 | Provide shuttle service for seniors homes or lifestyle communities (e.g. scheduled mall or supermarket runs) | For phase 5 - Retirement Units |
| | 4. | CARSHARING & BIKESHARING | |
| | 4.1 | Bikeshare stations & memberships | |
| BETTER | 4.1.1 | Contract with provider to install on-site bikeshare station (<i>multi-family</i>) | |
| BETTER | 4.1.2 | Provide residents with bikeshare memberships, either free or subsidized <i>(multi-family)</i> | |
| | 4.2 | Carshare vehicles & memberships | |
| BETTER | 4.2.1 | Contract with provider to install on-site carshare vehicles and promote their use by residents | |
| BETTER | 4.2.2 | Provide residents with carshare memberships, either free or subsidized | |
| | 5. | PARKING | |
| | 5.1 | Priced parking | |
| BASIC ★ | 5.1.1 | Unbundle parking cost from purchase price (condominium) | |
| BASIC 🛧 | 5.1.2 | Unbundle parking cost from monthly rent (multi-family) | |

| | TDM | measures: Residential developments | Check if proposed & add descriptions |
|----------|-------|--|---|
| | 6. | TDM MARKETING & COMMUNICATIONS | |
| | 6.1 | Multimodal travel information | |
| BASIC ★ | 6.1.1 | Provide a multimodal travel option information package to new residents | |
| | 6.2 | Personalized trip planning | |
| BETTER ★ | 6.2.1 | Offer personalized trip planning to new residents | |

Introduction

The City of Ottawa's *Transportation Impact Assessment (TIA) Guidelines* (specifically Module 4.1—Development Design) requires proponents of qualifying developments to use the City's **TDM-Supportive Development Design and Infrastructure Checklist** to assess the opportunity to implement design elements that are supportive of sustainable modes. The goal of this assessment is to ensure that the development provides safe and efficient access for all users, while creating an environment that encourages walking, cycling and transit use.

The remaining sections of this document are:

- Using the Checklist
- Glossary
- TDM-Supportive Development Design and Infrastructure Checklist: Non-Residential Developments
- TDM-Supportive Development Design and Infrastructure Checklist: Residential Developments

Readers are encouraged to contact the City of Ottawa's TDM Officer for any guidance and assistance they require to complete this checklist.

Using the Checklist

This **TDM-Supportive Development Design and Infrastructure Checklist** document includes two actual checklists, one for non-residential developments (office, institutional, retail or industrial) and one for residential developments (multi-family or condominium only; subdivisions are exempt). Readers may download the applicable checklist in electronic format and complete it electronically, or print it out and complete it by hand. As an alternative, they may create a freestanding document that lists the design and infrastructure measures being proposed and provides additional detail on them.

Each measure in the checklist is numbered for easy reference. Each measure is also flagged as:

- REQUIRED The Official Plan or Zoning By-law provides related guidance that must be followed.
- **BASIC** —The measure is generally feasible and effective, and in most cases would benefit the development and its users.
- **BETTER** —The measure could maximize support for users of sustainable modes, and optimize development performance.

Glossary

This glossary defines and describes the following measures that are identified in the **TDM-Supportive Development Design and Infrastructure Checklist**:

Walking & cycling: Routes

- Building location & access points
- Facilities for walking & cycling
- Amenities for walking & cycling

Walking & cycling: End-of-trip facilities

- Bicycle parking
- Secure bicycle parking
- Shower & change facilities
- Bicycle repair station

Transit

- Walking routes to transit
- Customer amenities

Ridesharing

- Pick-up & drop-off facilities
- Carpool parking

Carsharing & bikesharing

- Carshare parking spaces
- Bikeshare station location

Parking

- Number of parking spaces
- Separate long-term & short-term parking areas

Other

On-site amenities to minimize off-site trips

In addition to specific references made in this glossary, readers should consult the City of Ottawa's design and planning guidelines for a variety of different land uses and contexts, available on the City's website at www.ottawa.ca. Readers may also find the following resources to be helpful:

- Promoting Sustainable Transportation through Site Design, Institute of Transportation Engineers, 2004 (www.cite7.org/wpdm-package/iterp-promoting-sustainable-transportation)
- Bicycle End-of-Trip Facilities: A Guide for Canadian Municipalities and Employers, Transport Canada, 2010 (www.fcm.ca/Documents/tools/GMF/Transport_Canada/BikeEndofTrip_EN.pdf)

Walking & cycling: Routes

Building location & access points. Correctly positioning buildings and their entrances can help make walking convenient, comfortable and safe. Minimizing travel distances and maximizing visibility are key.

Facilities for walking & cycling. The Official Plan gives clear direction on the provision and design of walking and cycling facilities for both access and circulation. On larger, busier sites (e.g. multi-building campuses) the inclusion of sidewalks, pathways, marked crossings, stop signs and traffic calming features can create a safer and more supportive environment for active transportation.

Amenities for walking & cycling. Lighting, landscaping, benches and wayfinding can make walking and cycling safer and more secure, comfortable and accessible.

Walking & cycling: End-of-trip facilities

Bicycle parking. The Official Plan and Zoning By-law both address the need for adequate bicycle parking at developments. Weather protection and theft prevention are major concerns for commuters who spend hundreds or thousands of dollars on a quality bicycle. Bicycle racks should have a design that enables secure locking while preventing damage to wheels. They should be located within sight of busy areas such as main building entrances or staffed parking kiosks.

Secure bicycle parking. Ottawa's Zoning By-law requires a secure area for bicycles at office or residential developments having more than 50 bicycle parking spaces. Lockable outdoor bike cages or indoor storage rooms that limit access to registered users are ideal.

Shower & change facilities. Longer-distance cyclists, joggers and even pedestrians can need a place to shower and change at work; the lack of such facilities is a major barrier to active commuting. Lockers and drying racks provide a place to store gear away from workspaces, and showers and grooming stations allow commuters to make themselves presentable for the office.

Bicycle repair station. Cycling commuters can experience maintenance issues that make the homeward trip difficult or impossible. A small supply of tools (e.g. air pump, Allen keys, wrenches) and supplies (e.g. inner tube patches, chain lubricant) in the workplace can help.

Transit

Customer amenities. Larger developments that feature an on-site transit stop can make transit use more attractive by providing shelters, lighting and benches. Even better, they could integrate the passenger waiting area into a building entrance.

Ridesharing

Pick-up & drop-off facilities. Having a safe place to load or unload passengers (for carpools as well as taxis and ride-hailing services) without obstructing pedestrians, cyclists or other vehicles can help make carpooling work.

Carpool parking. At destinations with large parking lots (or lots that regularly fill to capacity), signed priority carpool parking spaces can be an effective ridesharing incentive. Priority spaces are frequently abused by non-carpoolers, so a system to provide registered users with vehicle identification tags is recommended.

Carsharing & bikesharing

Carshare parking spaces. For developments where carsharing could be an attractive option for employees, visitors or residents, ensuring an attractive location for future carshare parking spaces can avoid challenges associated with future retrofits.

Bikeshare station location. For developments where bikesharing could be an attractive option for employees, visitor or residents, ensuring an attractive location for a future bikeshare station can avoid challenges associated with future retrofits.

Parking

Number of parking spaces. Parking capacity is an important variable in development design, as it can either support or subvert the mode share targets set during the transportation impact analysis (TIA). While the Zoning By-law establishes any minimum and/or maximum requirements for parking capacity, it also allows a reduction in any minimum to reflect the existence of on-site shower, change and locker rooms provided for cyclists.

Separate long-term & short-term parking areas. Because access to unused parking spaces can be a powerful incentive to drive, developments can better manage their parking supply and travel behaviours by separating long-term from short-term parking through the use of landscaping, gated controls or signs. Doing so makes it difficult for long-term parkers (e.g. commuters) to park in short-term areas (e.g. for visitors) as long as enforcement occurs; it also protects long-term parking capacity for its intended users.

Other

On-site amenities to minimize off-site trips. Developments that offer facilities to limit employees' need for a car during their commute (e.g. to drop off children at daycare) or during their workday (e.g. to hit the gym) can free employees to make the commuting decision that otherwise works best for them.

TDM-Supportive Development Design and Infrastructure Checklist:

Residential Developments (multi-family or condominium)

| Legend | | | | | | | | | |
|----------|--|--|--|--|--|--|--|--|--|
| REQUIRED | The Official Plan or Zoning By-law provides related guidance that must be followed | | | | | | | | |
| BASIC | The measure is generally feasible and effective, and in most cases would benefit the development and its users | | | | | | | | |
| BETTER | The measure could maximize support for users of sustainable modes, and optimize development performance | | | | | | | | |

| | TDM-s | supportive design & infrastructure measures: Residential developments | Check if completed & add descriptions, explanations or plan/drawing references |
|----------|-------|---|---|
| | 1. | WALKING & CYCLING: ROUTES | |
| | 1.1 | Building location & access points | |
| BASIC | 1.1.1 | Locate building close to the street, and do not locate parking areas between the street and building entrances | |
| BASIC | 1.1.2 | Locate building entrances in order to minimize walking distances to sidewalks and transit stops/stations | \square |
| BASIC | 1.1.3 | Locate building doors and windows to ensure visibility of pedestrians from the building, for their security and comfort | \square |
| | 1.2 | Facilities for walking & cycling | |
| REQUIRED | 1.2.1 | Provide convenient, direct access to stations or major stops along rapid transit routes within 600 metres; minimize walking distances from buildings to rapid transit; provide pedestrian-friendly, weather-protected (where possible) environment between rapid transit accesses and building entrances; ensure quality linkages from sidewalks through building entrances to integrated stops/stations (see Official Plan policy 4.3.3) | Phase V: a further improvement would be to provide a walking connection between Tower V west entrance and Inlet Private sidewalk |
| REQUIRED | 1.2.2 | Provide safe, direct and attractive pedestrian access from public sidewalks to building entrances through such measures as: reducing distances between public sidewalks and major building entrances; providing walkways from public streets to major building entrances; within a site, providing walkways along the front of adjoining buildings, between adjacent buildings, and connecting areas where people may congregate, such as courtyards and transit stops; and providing weather protection through canopies, colonnades, and other design elements wherever possible (see Official <i>Plan policy 4.3.12</i>) | |

| | TDM-s | supportive design & infrastructure measures: Residential developments | Check if completed & add descriptions, explanations or plan/drawing references |
|----------|-------|---|--|
| REQUIRED | 1.2.3 | Provide sidewalks of smooth, well-drained walking surfaces of contrasting materials or treatments to differentiate pedestrian areas from vehicle areas, and provide marked pedestrian crosswalks at intersection sidewalks (see Official Plan policy 4.3.10) | |
| REQUIRED | 1.2.4 | Make sidewalks and open space areas easily accessible through features such as gradual grade transition, depressed curbs at street corners and convenient access to extra-wide parking spaces and ramps (see Official Plan policy 4.3.10) | |
| REQUIRED | 1.2.5 | Include adequately spaced inter-block/street cycling and pedestrian connections to facilitate travel by active transportation. Provide links to the existing or planned network of public sidewalks, multi-use pathways and on- road cycle routes. Where public sidewalks and multi-use pathways intersect with roads, consider providing traffic control devices to give priority to cyclists and pedestrians (see Official Plan policy 4.3.11) | |
| BASIC | 1.2.6 | Provide safe, direct and attractive walking routes from building entrances to nearby transit stops | ⊠ See 1.2.1 |
| BASIC | 1.2.7 | Ensure that walking routes to transit stops are secure, visible, lighted, shaded and wind-protected wherever possible | |
| BASIC | 1.2.8 | Design roads used for access or circulation by cyclists using a target operating speed of no more than 30 km/h, or provide a separated cycling facility | \bowtie |
| | 1.3 | Amenities for walking & cycling | |
| BASIC | 1.3.1 | Provide lighting, landscaping and benches along walking and cycling routes between building entrances and streets, sidewalks and trails | |
| BASIC | 1.3.2 | Provide wayfinding signage for site access (where required, e.g. when multiple buildings or entrances exist) and egress (where warranted, such as when directions to reach transit stops/stations, trails or other common destinations are not obvious) | \square |

| | TDM-s | supportive design & infrastructure measures: Residential developments | Check if completed & add descriptions, explanations or plan/drawing references |
|----------|-------|--|--|
| | 2. | WALKING & CYCLING: END-OF-TRIP FACILI | TIES |
| | 2.1 | Bicycle parking | |
| REQUIRED | 2.1.1 | Provide bicycle parking in highly visible and lighted areas, sheltered from the weather wherever possible (see Official Plan policy 4.3.6) | |
| REQUIRED | 2.1.2 | Provide the number of bicycle parking spaces specified for various land uses in different parts of Ottawa; provide convenient access to main entrances or well- used areas (see Zoning By-law Section 111) | Bicycle parking spaces will be required for Phase V should independent living seniors reside in Tower 5 |
| REQUIRED | 2.1.3 | Ensure that bicycle parking spaces and access aisles meet minimum dimensions; that no more than 50% of spaces are vertical spaces; and that parking racks are securely anchored (see Zoning By-law Section 111) | |
| BASIC | 2.1.4 | Provide bicycle parking spaces equivalent to the expected number of resident-owned bicycles, plus the expected peak number of visitor cyclists | |
| | 2.2 | Secure bicycle parking | |
| REQUIRED | 2.2.1 | Where more than 50 bicycle parking spaces are provided for a single residential building, locate at least 25% of spaces within a building/structure, a secure area (e.g. supervised parking lot or enclosure) or bicycle lockers (see Zoning By-law Section 111) | |
| BETTER | 2.2.2 | Provide secure bicycle parking spaces equivalent to at least the number of units at condominiums or multi-family residential developments | |
| | 2.3 | Bicycle repair station | |
| BETTER | 2.3.1 | Provide a permanent bike repair station, with commonly used tools and an air pump, adjacent to the main bicycle parking area (or secure bicycle parking area, if provided) | One bike repair station to serve all residents and users of City planned MUP |
| | 3. | TRANSIT | |
| | 3.1 | Customer amenities | |
| BASIC | 3.1.1 | Provide shelters, lighting and benches at any on-site transit stops | |
| BASIC | 3.1.2 | Where the site abuts an off-site transit stop and insufficient space exists for a transit shelter in the public right-of-way, protect land for a shelter and/or install a shelter | |
| BETTER | 3.1.3 | Provide a secure and comfortable interior waiting area by integrating any on-site transit stops into the building | |

| | TDM-s | upportive design & infrastructure measures: Residential developments | Check if completed & add descriptions, explanations or plan/drawing references |
|----------|-------|---|--|
| | 4. | RIDESHARING | |
| | 4.1 | Pick-up & drop-off facilities | |
| BASIC | 4.1.1 | Provide a designated area for carpool drivers (plus taxis and ride-hailing services) to drop off or pick up passengers without using fire lanes or other no-stopping zones | |
| | 5. | CARSHARING & BIKESHARING | |
| | 5.1 | Carshare parking spaces | |
| BETTER | 5.1.1 | Provide up to three carshare parking spaces in an R3, R4 or R5 Zone for specified residential uses <i>(see Zoning By-law Section 94)</i> | |
| | 5.2 | Bikeshare station location | |
| BETTER | 5.2.1 | Provide a designated bikeshare station area near a major building entrance, preferably lighted and sheltered with a direct walkway connection | |
| | 6. | PARKING | |
| | 6.1 | Number of parking spaces | |
| REQUIRED | 6.1.1 | Do not provide more parking than permitted by zoning, nor less than required by zoning, unless a variance is being applied for | \square |
| BASIC | 6.1.2 | Provide parking for long-term and short-term users that is consistent with mode share targets, considering the potential for visitors to use off-site public parking | \square |
| BASIC | 6.1.3 | Where a site features more than one use, provide shared parking and reduce the cumulative number of parking spaces accordingly <i>(see Zoning By-law</i> <i>Section 104)</i> | |
| BETTER | 6.1.4 | Reduce the minimum number of parking spaces required by zoning by one space for each 13 square metres of gross floor area provided as shower rooms, change rooms, locker rooms and other facilities for cyclists in conjunction with bicycle parking <i>(see Zoning By-law Section 111)</i> | |
| | 6.2 | Separate long-term & short-term parking areas | |
| BETTER | 6.2.1 | Provide separate areas for short-term and long-term parking (using signage or physical barriers) to permit access controls and simplify enforcement (i.e. to discourage residents from parking in visitor spaces, and vice versa) | |

Appendix N SYNCHRO Capacity Analysis: 2022 Total Projected Conditions

FT 2022 AM 2: Trim & OR174

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|-----------------------------------|---------------|----------------|---------------|-------|--------------|-----------|-------|-----------------|-------|---------|--|
| ane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR | |
| ane Configurations | ۲ | †† | 1 | ۲ | ŧ₽ | ሻሻ | A | ۲ | 1 | 1 | |
| Fraffic Volume (vph) | 92 | 268 | 414 | 93 | 1189 | 859 | 47 | 32 | 83 | 159 | |
| uture Volume (vph) | 92 | 268 | 414 | 93 | 1189 | 859 | 47 | 32 | 83 | 159 | |
| ane Group Flow (vph) | 102 | 298 | 460 | 103 | 1340 | 954 | 101 | 36 | 92 | 177 | |
| une ereap nen (tpn) | Prot | NA | Perm | Prot | NA | Prot | NA | pm+pt | NA | Perm | |
| rotected Phases | 5 | 2 | 1 0.111 | 1 | 6 | 3 | 8 | 7 | 4 | 1 01111 | |
| ermitted Phases | Ū | - | 2 | • | Ū | | Ū | 4 | • | 4 | |
| etector Phase | 5 | 2 | 2 | 1 | 6 | 3 | 8 | 7 | 4 | 4 | |
| witch Phase | 0 | 2 | 2 | | Ū | Ū | 0 | , | • | | |
| finimum Initial (s) | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 5.0 | 10.0 | 5.0 | 10.0 | 10.0 | |
| linimum Split (s) | 12.1 | 41.2 | 41.2 | 12.5 | 41.2 | 12.2 | 42.4 | 11.9 | 17.4 | 17.4 | |
| otal Split (s) | 15.0 | 50.0 | 50.0 | 20.0 | 55.0 | 42.0 | 43.0 | 17.0 | 17.4 | 18.0 | |
| otal Split (%) | 11.5% | 38.5% | 38.5% | 15.4% | 42.3% | 32.3% | 33.1% | 13.1% | 13.8% | 13.8% | |
| ellow Time (s) | | 5.1 | 5.1 | | | 32.370 | 3.178 | 3.3 | | | |
| ., | 3.3 | | | 3.3 | 5.1 | | | | 3.3 | 3.3 | |
| I-Red Time (s) | 3.8 | 2.1 | 2.1 | 4.2 | 2.1 | 3.9 | 4.1 | 3.6 | 4.1 | 4.1 | |
| ost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| otal Lost Time (s) | 7.1 | 7.2 | 7.2 | 7.5 | 7.2 | 7.2 | 7.4 | 6.9 | 7.4 | 7.4 | |
| ead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lead | |
| ead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | |
| ecall Mode | None | C-Max | C-Max | None | C-Max | None | Max | None | Max | Max | |
| ct Effct Green (s) | 7.9 | 43.9 | 43.9 | 11.4 | 47.8 | 34.8 | 42.4 | 19.4 | 10.6 | 10.6 | |
| ctuated g/C Ratio | 0.06 | 0.34 | 0.34 | 0.09 | 0.37 | 0.27 | 0.33 | 0.15 | 0.08 | 0.08 | |
| c Ratio | 0.99 | 0.26 | 0.57 | 0.70 | 1.08 | 1.08 | 0.10 | 0.17 | 0.63 | 0.55 | |
| ontrol Delay | 146.6 | 32.3 | 5.9 | 81.6 | 88.4 | 100.5 | 18.9 | 29.9 | 77.7 | 9.8 | |
| ueue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| otal Delay | 146.6 | 32.3 | 5.9 | 81.6 | 88.4 | 100.5 | 18.9 | 29.9 | 77.7 | 9.8 | |
| OS | F | С | А | F | F | F | В | С | E | А | |
| pproach Delay | | 31.7 | | | 87.9 | | 92.7 | | 32.6 | | |
| pproach LOS | | С | | | F | | F | | С | | |
| ueue Length 50th (m) | 26.6 | 29.4 | 0.0 | 25.8 | ~201.4 | ~140.9 | 5.2 | 5.5 | 23.2 | 0.0 | |
| ueue Length 95th (m) | #63.1 | 41.1 | 24.7 | #48.2 | #244.3 | #180.7 | 12.2 | 12.4 | #45.4 | 11.4 | |
| iternal Link Dist (m) | | 222.6 | | | 537.2 | | 301.4 | | 202.0 | | |
| urn Bay Length (m) | 155.0 | | 200.0 | 130.0 | | 180.0 | | 120.0 | | 60.0 | |
| ase Capacity (vph) | 103 | 1145 | 803 | 162 | 1244 | 880 | 1048 | 235 | 145 | 323 | |
| tarvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| pillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| torage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| educed v/c Ratio | 0.99 | 0.26 | 0.57 | 0.64 | 1.08 | 1.08 | 0.10 | 0.15 | 0.63 | 0.55 | |
| | 0.99 | 0.20 | 0.57 | 0.04 | 1.00 | 1.00 | 0.10 | 0.15 | 0.03 | 0.00 | |
| tersection Summary | | | | | | | | | | | |
| ycle Length: 130 | | | | | | | | | | | |
| ctuated Cycle Length: 130 | | | | | | | | | | | |
| ffset: 20 (15%), Referenced to p | nase 2:EBT an | a 6:WBT, S | lant of Greek | 1 | | | | | | | |
| atural Cycle: 110 | | | | | | | | | | | |
| ontrol Type: Actuated-Coordinat | ea | | | | | | | | | | |
| aximum v/c Ratio: 1.08 | | | | | | | | | | | |
| tersection Signal Delay: 71.5 | | | | | tersection L | | | | | | |
| tersection Capacity Utilization 9 | 1.3% | | | IC | U Level of S | Service F | | | | | |
| nalysis Period (min) 15 | | | | | | | | | | | |
| Volume exceeds capacity, que | | ally infinite. | | | | | | | | | |
| Queue shown is maximum after | | | | | | | | | | | |
| 95th percentile volume exceed | | eue may be | longer. | | | | | | | | |
| Queue shown is maximum after | | 2 | ÿ | | | | | | | | |
| plits and Phases: 2: Trim & O | R174 | | | | | | | | | | |
| | 1117 | | | | Т | Ø4 | | • | | | |
| 🖌 Ø1 | 02 (R) | | | | | | | [™] Ø3 | | | |

| 🔨 Ø1 | ● 🖘 ● Ø2 (R) | ₽ ™ø4 | Ø3 |
|------|---------------------|-----------------|------|
| 20 s | 50 s | 18 s 42 s | 5 |
| | ← # 6 (R) | [†] ø8 | ▶ø7 |
| 15 s | 55 s | 43 s | 17 s |

FT 2022 AM 1: Trim & Jeanne D'Arc

| | ٦ | - | \rightarrow | 1 | ← | * | 1 | † | 1 | 1 | Ļ | ~ |
|-----------------------------------|-------|------|---------------|-------|----------------|------|------|----------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | \$ | | | \$ | | | \$ | | | \$ | |
| Sign Control | | Stop | | | Stop | | | Stop | | | Stop | |
| Traffic Volume (vph) | 8 | 6 | 82 | 181 | 14 | 0 | 106 | 20 | 59 | 0 | 9 | 3 |
| Future Volume (vph) | 8 | 6 | 82 | 181 | 14 | 0 | 106 | 20 | 59 | 0 | 9 | 3 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 9 | 7 | 91 | 201 | 16 | 0 | 118 | 22 | 66 | 0 | 10 | 3 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total (vph) | 107 | 217 | 206 | 13 | | | | | | | | |
| Volume Left (vph) | 9 | 201 | 118 | 0 | | | | | | | | |
| Volume Right (vph) | 91 | 0 | 66 | 3 | | | | | | | | |
| Hadj (s) | -0.46 | 0.22 | -0.04 | -0.10 | | | | | | | | |
| Departure Headway (s) | 4.3 | 4.8 | 4.6 | 4.8 | | | | | | | | |
| Degree Utilization, x | 0.13 | 0.29 | 0.27 | 0.02 | | | | | | | | |
| Capacity (veh/h) | 794 | 715 | 731 | 670 | | | | | | | | |
| Control Delay (s) | 7.9 | 9.7 | 9.3 | 7.9 | | | | | | | | |
| Approach Delay (s) | 7.9 | 9.7 | 9.3 | 7.9 | | | | | | | | |
| Approach LOS | А | А | А | А | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Delay | | | 9.2 | | | | | | | | | |
| Level of Service | | | А | | | | | | | | | |
| Intersection Capacity Utilization | | | 42.5% | ICI | U Level of Ser | vice | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

FT 2022 PM 2: Trim Rd & OR 174

| | ٦ | - | \rightarrow | 4 | Ļ | N | t | × | Ŧ | ~ | |
|---|--|----------------|---------------|-------------------|------------------------------|-----------|-------|-------|-------------|-------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR | |
| Lane Configurations | ۲ | <u>†</u> † | 1 | ۲ | ≜ †⊅ | ሻሻ | A | ۲ | 1 | 1 | |
| Traffic Volume (vph) | 120 | 1111 | 1172 | 70 | 428 | 462 | 70 | 26 | 90 | 114 | |
| Future Volume (vph) | 120 | 1111 | 1172 | 70 | 428 | 462 | 70 | 26 | 90 | 114 | |
| Lane Group Flow (vph) | 133 | 1234 | 1302 | 78 | 506 | 513 | 182 | 29 | 100 | 127 | |
| Turn Type | Prot | NA | Free | Prot | NA | Prot | NA | pm+pt | NA | Perm | |
| Protected Phases | 5 | 2 | 1100 | 1 | 6 | 3 | 8 | 7 | 4 | 1 onn | |
| Permitted Phases | 0 | - | Free | • | | Ū | Ū | 4 | | 4 | |
| Detector Phase | 5 | 2 | 1100 | 1 | 6 | 3 | 8 | 7 | 4 | 4 | |
| Switch Phase | 5 | 2 | | | 0 | 5 | 0 | , | - | 7 | |
| Minimum Initial (s) | 5.0 | 10.0 | | 5.0 | 10.0 | 5.0 | 10.0 | 5.0 | 10.0 | 10.0 | |
| Vinimum Split (s) | 12.1 | 41.2 | | 12.5 | 41.2 | 12.2 | 42.4 | 11.9 | 17.4 | 17.4 | |
| | | | | | | | | | | | |
| Total Split (s) | 16.0 | 54.0 | | 16.0 | 54.0 | 33.0 | 43.0 | 17.0 | 27.0 | 27.0 | |
| Total Split (%) | 12.3% | 41.5% | | 12.3% | 41.5% | 25.4% | 33.1% | 13.1% | 20.8% | 20.8% | |
| Yellow Time (s) | 3.3 | 5.1 | | 3.3 | 5.1 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | |
| All-Red Time (s) | 3.8 | 2.1 | | 4.2 | 2.1 | 3.9 | 4.1 | 3.6 | 4.1 | 4.1 | |
| ost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Fotal Lost Time (s) | 7.1 | 7.2 | | 7.5 | 7.2 | 7.2 | 7.4 | 6.9 | 7.4 | 7.4 | |
| Lead/Lag | Lead | Lag | | Lead | Lag | Lag | Lead | Lag | Lead | Lead | |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | |
| Recall Mode | None | C-Max | | None | C-Max | None | Max | None | Max | Max | |
| Act Effct Green (s) | 10.8 | 48.5 | 130.0 | 8.6 | 46.8 | 23.9 | 40.6 | 28.3 | 19.6 | 19.6 | |
| Actuated g/C Ratio | 0.08 | 0.37 | 1.00 | 0.07 | 0.36 | 0.18 | 0.31 | 0.22 | 0.15 | 0.15 | |
| v/c Ratio | 0.95 | 0.98 | 0.86 | 0.70 | 0.42 | 0.85 | 0.18 | 0.10 | 0.37 | 0.31 | |
| Control Delay | 122.9 | 60.6 | 6.8 | 89.7 | 32.3 | 65.0 | 15.8 | 26.8 | 54.3 | 1.9 | |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Delay | 122.9 | 60.6 | 6.8 | 89.7 | 32.3 | 65.0 | 15.8 | 26.8 | 54.3 | 1.9 | |
| LOS | F | E | А | F | С | E | В | С | D | А | |
| Approach Delay | | 37.5 | | | 39.9 | | 52.1 | - | 25.2 | | |
| Approach LOS | | D | | | D | | D | | С | | |
| Queue Length 50th (m) | ~38.5 | ~169.4 | 0.0 | 19.9 | 50.4 | 65.2 | 7.8 | 4.5 | 23.3 | 0.0 | |
| Queue Length 95th (m) | #80.9 | #216.7 | 0.0 | #44.5 | 65.9 | 84.5 | 17.1 | 10.6 | 40.9 | 0.0 | |
| Internal Link Dist (m) | #00.7 | 313.9 | 0.0 | # 1 .5 | 321.3 | 04.5 | 154.2 | 10.0 | 204.2 | 0.0 | |
| Turn Bay Length (m) | 150.0 | 515.7 | 200.0 | 130.0 | JZ 1.J | 230.0 | 134.2 | 120.0 | 204.2 | 55.0 | |
| Base Capacity (vph) | 140 | 1265 | 1517 | 115 | 1211 | 652 | 1030 | 306 | 268 | 416 | |
| | 0 | 1205 | 0 | 0 | 0 | 052 | 0 | 0 | 208 | 410 | |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | |
| Storage Cap Reductn | 0.95 | | 0.86 | | 0.42 | 0 0.79 | | | | | |
| Reduced v/c Ratio | 0.95 | 0.98 | 0.86 | 0.68 | 0.42 | 0.79 | 0.18 | 0.09 | 0.37 | 0.31 | |
| ntersection Summary Cycle Length: 130 Actuated Cycle Length: 130 Diffset: 0 (0%), Referenced to phase Natural Cycle: 120 Control Type: Actuated-Coordinated Maximum v/c Ratio: 0.98 ntersection Signal Delay: 39.5 ntersection Capacity Utilization 84 Analysis Period (min) 15 - Volume exceeds capacity, que Queue shown is maximum after # 95th percentile volume exceed | ed 1.2% uue is theoretic r two cycles. Is capacity, qu | ally infinite. | | | tersection L U Level of S | | | | | | |
| Queue shown is maximum after Splits and Phases: 2: Trim Rd & | | | | | | | | | | | |
| ✔Ø1 ● Ø2 (R |) | | | | | \$ ø4 | | | ≜ Ø3 | | |
| 16 s 54 s | | | | | | 7 s | | | 33 s | | |

| Ø1 | →Ø2 (R) | ₽ ø4 | Ø 3 |
|------------------|---------|-------------|------------|
| 16 s | 54 s | 27 s | 33 s |
| ∕× _{Ø5} | ₩Ø6 (R) | 1 ø8 | Ø7 |
| 16 s | 54 s | 43 s | 17 s |

FT 2022 PM 1: Trim Rd & Jeanne D'Arc

| T. THILLING & Jeanne D AIG |) | | | | | | | | | | | |
|-----------------------------------|-------|------|--------------|-------|---------------|-------|------|------|------|------|------|------|
| | ٦ | - | \mathbf{i} | ∢ | ← | • | 1 | † | 1 | 1 | Ļ | - |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | \$ | | | 4 | | | 4 | |
| Sign Control | | Stop | | | Stop | | | Stop | | | Stop | |
| Traffic Volume (vph) | 7 | 10 | 133 | 93 | 6 | 0 | 81 | 8 | 129 | 1 | 11 | 4 |
| Future Volume (vph) | 7 | 10 | 133 | 93 | 6 | 0 | 81 | 8 | 129 | 1 | 11 | 4 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 8 | 11 | 148 | 103 | 7 | 0 | 90 | 9 | 143 | 1 | 12 | 4 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total (vph) | 167 | 110 | 242 | 17 | | | | | | | | |
| Volume Left (vph) | 8 | 103 | 90 | 1 | | | | | | | | |
| Volume Right (vph) | 148 | 0 | 143 | 4 | | | | | | | | |
| Hadj (s) | -0.49 | 0.22 | -0.25 | -0.10 | | | | | | | | |
| Departure Headway (s) | 4.2 | 4.9 | 4.3 | 4.7 | | | | | | | | |
| Degree Utilization, x | 0.19 | 0.15 | 0.29 | 0.02 | | | | | | | | |
| Capacity (veh/h) | 815 | 685 | 791 | 693 | | | | | | | | |
| Control Delay (s) | 8.1 | 8.8 | 9.1 | 7.8 | | | | | | | | |
| Approach Delay (s) | 8.1 | 8.8 | 9.1 | 7.8 | | | | | | | | |
| Approach LOS | А | А | А | А | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Delay | | | 8.7 | | | | | | | | | |
| Level of Service | | | А | | | | | | | | | |
| Intersection Capacity Utilization | | | 45.6% | ICI | J Level of Se | rvice | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Appendix O SYNCHRO and SIDRA Capacity Analysis: 2024 Total Projected Conditions

Future 2024 AM 3: Jeanne D'Arc

| | _ | ~ | 4 | + | • | 1 |
|-----------------------------------|------|------|-------|------------|--------------|--------|
| N 4 | FDT. | • | | WDT |) NDI | - |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ₽ | 0.41 | 1/0 | र्स | Y | 0 |
| Traffic Volume (veh/h) | 82 | 941 | 169 | 91 | 106 | 8 |
| Future Volume (Veh/h) | 82 | 941 | 169 | 91 | 106 | 8 |
| Sign Control | Free | | | Free | Stop | |
| Grade | 0% | 0.05 | 0.05 | 0% | 0% | 0.05 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Hourly flow rate (vph) | 86 | 991 | 178 | 96 | 112 | 8 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | | | None | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | | | 86 | | 1034 | 582 |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | | | 86 | | 1034 | 582 |
| tC, single (s) | | | 4.1 | | 6.4 | 6.2 |
| tC, 2 stage (s) | | | | | | |
| tF (s) | | | 2.2 | | 3.5 | 3.3 |
| p0 queue free % | | | 88 | | 51 | 98 |
| cM capacity (veh/h) | | | 1510 | | 227 | 513 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | | | |
| Volume Total | 1077 | 274 | 120 | | | |
| Volume Left | 0 | 178 | 112 | | | |
| Volume Right | 991 | 0 | 8 | | | |
| cSH | 1700 | 1510 | 236 | | | |
| Volume to Capacity | 0.63 | 0.12 | 0.51 | | | |
| Queue Length 95th (m) | 0.0 | 3.0 | 20.0 | | | |
| Control Delay (s) | 0.0 | 5.3 | 35.1 | | | |
| Lane LOS | | A | E | | | |
| Approach Delay (s) | 0.0 | 5.3 | 35.1 | | | |
| Approach LOS | 0.0 | 0.0 | E | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 3.9 | | | |
| Intersection Capacity Utilization | | | 97.6% | 101 | U Level of S | onvico |
| | | | 97.6% | ICI | D Level OF S | ervice |
| Analysis Period (min) | | | 15 | | | |

Future 2024 PM 3: Jeanne D'Arc

| - | | | | | | |
|-----------------------------------|------|--------------|-----------|------|--------------|-----------|
| | -+ | \mathbf{i} | - | - | • | 1 |
| Marran | EDT | | • | WDT | | - |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | Þ | E 40 | 70 | 4 | M | |
| Traffic Volume (veh/h) | 141 | 542 | 73 | 39 | 83 | 16 |
| Future Volume (Veh/h) | 141 | 542 | 73 | 39 | 83 | 16 |
| Sign Control | Free | | | Free | Stop | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Hourly flow rate (vph) | 148 | 571 | 77 | 41 | 87 | 17 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | | | None | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | | | 148 | | 628 | 434 |
| vC1, stage 1 conf vol | | | 110 | | 020 | 101 |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | | | 148 | | 628 | 434 |
| tC, single (s) | | | 4.1 | | 6.4 | 6.2 |
| tC, 2 stage (s) | | | 7.1 | | U.T | 0.2 |
| tF (s) | | | 2.2 | | 3.5 | 3.3 |
| p0 queue free % | | | 2.2 95 | | 3.5 79 | 3.3 97 |
| | | | | | | |
| cM capacity (veh/h) | | | 1434 | | 422 | 622 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | | | |
| Volume Total | 719 | 118 | 104 | | | |
| Volume Left | 0 | 77 | 87 | | | |
| Volume Right | 571 | 0 | 17 | | | |
| cSH | 1700 | 1434 | 446 | | | |
| Volume to Capacity | 0.42 | 0.05 | 0.23 | | | |
| Queue Length 95th (m) | 0.0 | 1.3 | 6.8 | | | |
| Control Delay (s) | 0.0 | 5.1 | 15.5 | | | |
| Lane LOS | | A | C | | | |
| Approach Delay (s) | 0.0 | 5.1 | 15.5 | | | |
| Approach LOS | 0.0 | 0.1 | 13.5 C | | | |
| | | | 5 | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 2.4 | | | |
| Intersection Capacity Utilization | | | 65.4% | IC | U Level of S | ervice |
| Analysis Period (min) | | | 15 | | | |
| | | | | | | |

MOVEMENT SUMMARY

Site: [Jeanne D'Arc/Trim]

Future 2024 AM Roundabout

| Movement Performance - Vehicles | | | | | | | | | | | | | |
|---------------------------------|-----------|--------|-----|-------|---------|----------|----------|----------|--------|-----------|---------|--|--|
| Mov | OD | Demand | | Deg. | Average | Level of | 95% Back | | Prop. | Effective | Average | | |
| ID | Mov | Total | HV | Satn | Delay | Service | Vehicles | Distance | Queued | Stop Rate | Speed | | |
| South | · Trim | veh/h | % | v/c | sec | _ | veh | m | | per veh | km/h | | |
| | | 100 | 2.0 | 0.400 | 7 5 | | 0.0 | 4 5 | 0.40 | 0.55 | 40.0 | | |
| 1 | L2 | 139 | 2.0 | 0.100 | 7.5 | LOS A | 0.6 | 4.5 | 0.19 | 0.55 | 46.6 | | |
| 2 | T1 | 21 | 2.0 | 0.100 | 3.0 | LOS A | 0.6 | 4.5 | 0.19 | 0.55 | 46.5 | | |
| 3 | R2 | 992 | 2.0 | 0.543 | 2.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.36 | 48.5 | | |
| Appro | bach | 1152 | 2.0 | 0.543 | 3.1 | LOS A | 0.6 | 4.5 | 0.03 | 0.39 | 48.2 | | |
| East: | Jeanne D' | Arc | | | | | | | | | | | |
| 4 | L2 | 175 | 2.0 | 0.173 | 8.4 | LOS A | 1.1 | 7.6 | 0.40 | 0.59 | 46.1 | | |
| 5 | T1 | 24 | 2.0 | 0.173 | 3.9 | LOS A | 1.1 | 7.6 | 0.40 | 0.59 | 46.0 | | |
| 6 | R2 | 3 | 2.0 | 0.173 | 3.9 | LOS A | 1.1 | 7.6 | 0.40 | 0.59 | 45.0 | | |
| Appro | ach | 202 | 2.0 | 0.173 | 7.8 | LOS A | 1.1 | 7.6 | 0.40 | 0.59 | 46.1 | | |
| North | : Trim | | | | | | | | | | | | |
| 7 | L2 | 2 | 2.0 | 0.012 | 8.8 | LOS A | 0.1 | 0.4 | 0.45 | 0.47 | 47.6 | | |
| 8 | T1 | 7 | 2.0 | 0.012 | 4.3 | LOS A | 0.1 | 0.4 | 0.45 | 0.47 | 47.4 | | |
| 9 | R2 | 3 | 2.0 | 0.012 | 4.3 | LOS A | 0.1 | 0.4 | 0.45 | 0.47 | 46.4 | | |
| Appro | ach | 13 | 2.0 | 0.012 | 5.0 | LOS A | 0.1 | 0.4 | 0.45 | 0.47 | 47.2 | | |
| West: | Jeanne D | 'Arc | | | | | | | | | | | |
| 10 | L2 | 8 | 2.0 | 0.092 | 8.4 | LOS A | 0.5 | 3.9 | 0.41 | 0.46 | 48.0 | | |
| 11 | T1 | 38 | 2.0 | 0.092 | 3.9 | LOS A | 0.5 | 3.9 | 0.41 | 0.46 | 47.9 | | |
| 12 | R2 | 58 | 2.0 | 0.092 | 3.9 | LOS A | 0.5 | 3.9 | 0.41 | 0.46 | 46.8 | | |
| Appro | bach | 104 | 2.0 | 0.092 | 4.3 | LOS A | 0.5 | 3.9 | 0.41 | 0.46 | 47.3 | | |
| All Ve | hicles | 1471 | 2.0 | 0.543 | 3.8 | LOS A | 1.1 | 7.6 | 0.11 | 0.42 | 47.8 | | |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

SIDRA INTERSECTION 7.0 | Copyright © 2000-2016 Akcelik and Associates Pty Ltd | sidrasolutions.com Organisation: PARSONS TRANSPORTATION GROUP | Processed: Friday, July 06, 2018 11:48:53 AM Project: H:\ISO\476705\1000\DATA\Sidra\Future\FT 2024 AM.sip7

MOVEMENT SUMMARY

Site: [Jeanne D'Arc/Trim]

Future 2024 PM Roundabout

| Move | Movement Performance - Vehicles | | | | | | | | | | | | | |
|-----------|---------------------------------|--------------------------|------------------|---------------------|-------------------------|---------------------|-------------------------------|---------------------------|-----------------|-----------------------------------|--------------------------|--|--|--|
| Mov ID | OD Mov | Demand Total veh/h | Flows HV % | Deg. Satn v/c | Average Delay sec | Level of Service | 95% Back o Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h | | | |
| South | : Trim | | | | | | | | | | | | | |
| 1 | L2 | 101 | 2.0 | 0.072 | 7.6 | LOS A | 0.4 | 3.1 | 0.24 | 0.55 | 46.4 | | | |
| 2 | T1 | 8 | 2.0 | 0.072 | 3.1 | LOS A | 0.4 | 3.1 | 0.24 | 0.55 | 46.2 | | | |
| 3 | R2 | 624 | 2.0 | 0.342 | 2.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.36 | 48.5 | | | |
| Appro | ach | 734 | 2.0 | 0.342 | 3.1 | LOS A | 0.4 | 3.1 | 0.04 | 0.39 | 48.2 | | | |
| East: | Jeanne D' | Arc | | | | | | | | | | | | |
| 4 | L2 | 103 | 2.0 | 0.100 | 8.0 | LOS A | 0.6 | 4.2 | 0.32 | 0.56 | 46.4 | | | |
| 5 | T1 | 17 | 2.0 | 0.100 | 3.5 | LOS A | 0.6 | 4.2 | 0.32 | 0.56 | 46.2 | | | |
| 6 | R2 | 2 | 2.0 | 0.100 | 3.5 | LOS A | 0.6 | 4.2 | 0.32 | 0.56 | 45.2 | | | |
| Appro | ach | 122 | 2.0 | 0.100 | 7.3 | LOS A | 0.6 | 4.2 | 0.32 | 0.56 | 46.3 | | | |
| North | : Trim | | | | | | | | | | | | | |
| 7 | L2 | 3 | 2.0 | 0.014 | 8.2 | LOS A | 0.1 | 0.5 | 0.36 | 0.45 | 47.8 | | | |
| 8 | T1 | 8 | 2.0 | 0.014 | 3.7 | LOS A | 0.1 | 0.5 | 0.36 | 0.45 | 47.7 | | | |
| 9 | R2 | 4 | 2.0 | 0.014 | 3.8 | LOS A | 0.1 | 0.5 | 0.36 | 0.45 | 46.6 | | | |
| Appro | ach | 16 | 2.0 | 0.014 | 4.6 | LOS A | 0.1 | 0.5 | 0.36 | 0.45 | 47.4 | | | |
| West: | Jeanne D |)'Arc | | | | | | | | | | | | |
| 10 | L2 | 7 | 2.0 | 0.136 | 8.0 | LOS A | 0.8 | 5.9 | 0.33 | 0.42 | 48.4 | | | |
| 11 | T1 | 65 | 2.0 | 0.136 | 3.5 | LOS A | 0.8 | 5.9 | 0.33 | 0.42 | 48.2 | | | |
| 12 | R2 | 96 | 2.0 | 0.136 | 3.5 | LOS A | 0.8 | 5.9 | 0.33 | 0.42 | 47.1 | | | |
| Appro | ach | 168 | 2.0 | 0.136 | 3.7 | LOS A | 0.8 | 5.9 | 0.33 | 0.42 | 47.6 | | | |
| All Ve | hicles | 1040 | 2.0 | 0.342 | 3.7 | LOS A | 0.8 | 5.9 | 0.12 | 0.42 | 47.8 | | | |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Appendix P SYNCHRO and SIDRA Capacity Analysis: 2029 Total Projected Conditions

Future 2029 AM 3: Jeanne D'Arc

| | → | 1 | 4 | t | • | ~ |
|-----------------------------------|-----------------|-------------|-------------|----------------|--------------|--------|
| Movement | EBT | EBR | ▼ WBL | WBT | NBL | NBR |
| Lane Configurations | EDI | EDK | VVDL | | MDL M | NDK |
| Traffic Volume (veh/h) | ₽ 82 | 1060 | 169 | 4 91 | 112 | 8 |
| Future Volume (Veh/h) | 82 | 1060 | 169 | 91 | 112 | 8 |
| Sign Control | Free | 1000 | 107 | Free | Stop | 0 |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Hourly flow rate (vph) | 86 | 1116 | 178 | 96 | 118 | 8 |
| Pedestrians | 00 | 1110 | 170 | 70 | 110 | 0 |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | | | None | | |
| Median storage veh) | NOTIC | | | None | | |
| Upstream signal (m) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | | | 86 | | 1096 | 644 |
| vC1, stage 1 conf vol | | | 00 | | 1070 | 011 |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | | | 86 | | 1096 | 644 |
| tC, single (s) | | | 4.1 | | 6.4 | 6.2 |
| tC, 2 stage (s) | | | | | 0.1 | 0.2 |
| tF (s) | | | 2.2 | | 3.5 | 3.3 |
| p0 queue free % | | | 88 | | 43 | 98 |
| cM capacity (veh/h) | | | 1510 | | 208 | 473 |
| | ED 1 | | | | 200 | |
| Direction, Lane # | EB 1 1202 | WB 1 274 | NB 1 126 | | | |
| Volume Lotal | 1202 | 274 178 | 126 | | | |
| | 0 1116 | 1/8 | 8 | | | |
| Volume Right cSH | 1700 | 0 1510 | 8 216 | | | |
| | 0.71 | | 0.58 | | | |
| Volume to Capacity | | 0.12 | | | | |
| Queue Length 95th (m) | 0.0 | 3.0 | 24.8 | | | |
| Control Delay (s) Lane LOS | 0.0 | 5.3 | 42.7 E | | | |
| | 0.0 | A | | | | |
| Approach Delay (s) | 0.0 | 5.3 | 42.7 | | | |
| Approach LOS | | | E | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 4.3 | | | |
| Intersection Capacity Utilization | | | 105.7% | ICI | U Level of S | ervice |
| Analysis Period (min) | | | 15 | | | |

Future 2029 PM 3: Jeanne D'Arc

| $\begin{tabular}{ c c c c } \hline \begin{tabular}{ c c c } \hline \begin{tabular}{ c c c c } \hline \hline \begin{tabular}{ c c c c } \hline \begin{tabular}{ c c c c } \hline \begin{tabular}{ c c c } \hline \begin{tabular}{ c c c c } \hline \hline \begin{tabular}{ c c c } \hline \begin{tabular}{ c c c c } \hline \hline \begin{tabular}{ c c c c c } \hline \hline \begin{tabular}{ c c c } \hline \hline \begin{tabular}{ c $ | | | | | | | |
|---|-----------------------|------|---------------|------|------|--------------|--------|
| Movement EBT EBR WBL WBT NBL NBR Lane Configurations ↓ | | - | \rightarrow | < | - | - | 1 |
| Lane Configurations ↓ | Movement | FRT | FRR | | WRT | NRI | - |
| Traffic Volume (veh/h) 141 642 73 39 87 16 Future Volume (Veh/h) 141 642 73 39 87 16 Sign Control Free Free Stop Grade 0% 0% 0% 0% Peak Hour Factor 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 Hourly flow rate (vph) 148 676 77 41 92 17 Pedestrians | | | LDK | VVDL | | | NDK |
| Future Volume (Veh/h) 141 642 73 39 87 16 Sign Control Free Stop | | | 640 | 70 | | | 14 |
| Sign Control Free Free Stop Grade 0% 0% 0% 0% Peak Hour Factor 0.95 0.95 0.95 0.95 0.95 Peak Hour Factor 0.95 0.95 0.95 0.95 0.95 Pedestrians 148 676 77 41 92 17 Pedestrians Percent Blockage Right turn flare (veh) Velockage Velockage <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<> | | | | | | | |
| Grade 0% 0% 0% 0% Peak Hour Factor 0.95 0.95 0.95 0.95 0.95 0.95 Hourly flow rate (vph) 148 676 77 41 92 17 Pedestrians Integration Integration <t< td=""><td></td><td></td><td>042</td><td>/3</td><td></td><td></td><td>10</td></t<> | | | 042 | /3 | | | 10 |
| Peak Hour Factor 0.95 0.95 0.95 0.95 0.95 0.95 0.95 Houry flow rate (vph) 148 676 77 41 92 17 Pedestrians Lane Widh (m) Validity 92 17 Walking Speed (m/s) Percent Blockage None None Median storage veh) Upstream signal (m) None Validity yC, conflicting volume 148 681 486 vC1, stage 1 conf vol Validity Validity Validity vC2, stage 2 conf vol Vic1, stage 1 conf vol Validity Validity vC2, stage 2 conf vol Vic1, stage (s) 4.1 6.4 6.2 tC, 2 stage (s) T Signal 394 581 Direction, Lane # EB1 WB 1 NB1 Validity Va | | | | | | | |
| Hourly flow rate (vph) 148 676 77 41 92 17 Pedestrians Lane Width (m) Walking Speed (m/s) Percent Blockage None None Right turn flare (veh) Median type None None Median type (veh) Volume (veh) Median storage veh) Upstream signal (m) Volution unblocked Volution vehicle (veh) Volution vehicle (veh) VC2, stage 1 conf vol VC2, stage 2 conf vol Volution vehicle (vehicle (v | | | 0.05 | 0.05 | | | 0.05 |
| Pedestrians Image: Second | | | | | | | |
| Lane Width (m) Walking Speed (m/s) Percent Blockage Right turn flare (veh) Median type None None Median storage veh) Upstream signal (m) pX, platoon unblocked vC, conflicting volume vC, conflicting volume vC2, stage 1 conf vol vC2, stage 2 conf vol vC2, stage 3 Direction, Lane # EB1 WB1 NB1 Volume Ictal 824 118 109 Volume Right 676 0 17 CSH 1700 1434 415 Volume Coapacity 0 A B B C C C Intersection Summary Average Delay Intersection Capacity VIIIiZation 72.1% ICU Level of Service | | 148 | 676 | 77 | 41 | 92 | 17 |
| Walking Speed (m/s) Percent Blockage Right turn flare (veh) Median type None Median type None Wasser (m/s) None Upstream signal (m) pX, platoon unblocked vC, conflicting volume 148 681 486 vC1, stage 1 conf vol vc. vc. vc. vC2, stage 2 conf vol vc. vc. vc. vC1, single (s) 4.1 6.4 6.2 tC, single (s) 2.2 3.5 3.3 p0 queue free % 95 77 97 cd capacity (veh/h) 1434 394 581 Direction, Lane # EB 1 WB 1 NB 1 Volume Total 824 118 109 Volume Left 0 77 92 Volume Right 676 0 17 cSH 1700 1434 415 Volume Right 0.01 1.3 7.9 2.0 2.0 Control Delay (s) 0.0 5.1 16.8 Lane LOS A <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> | | | | | | | |
| Percent Blockage Right turn flare (veh) None Median type None Median storage veh) Vone Upstream signal (m) VX. pX. platoon unblocked VC. conflicting volume 148 681 486 vC1, stage 1 conf vol VC2, stage 2 conf vol VC2, stage 2 conf vol VC2, unblocked vol 148 681 486 VC2, stage 2 conf vol VC2, unblocked vol 148 681 486 VC3, stage 2 conf vol VC4 148 681 486 VC2, stage 2 conf vol VC2 3.5 3.3 90 VC2, unblocked vol 148 681 486 120 120 VC3, stage (s) E V 1434 394 581 Direction, Lane # EB 1 WB 1 NB 1 VOlume Total 824 118 109 Volume Left 0 77 92 Volume Right 676 0 17 CSH VOlume Right 676 0 17 CSH VOlume Left | | | | | | | |
| Right turn flare (veh) None None Median storage veh) Upstream signal (m) None pX, platoon unblocked vC, conflicting volume 148 681 486 vC1, stage 1 conf vol vC2, stage 2 conf vol vC2, stage (s) 4.1 6.4 6.2 tC, single (s) 4.1 6.4 6.2 tC, single (s) vC2, stage (s) vC2 3.5 3.3 p0 queue free % 95 77 97 GR 95 77 97 GR 2.2 3.5 3.3 p0 queue free % 95 77 97 GR GR 486 | | | | | | | |
| Median type None None Median storage veh) Upstream signal (m) pX, platon unblocked 148 681 486 vC1, stage 1 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol 486 vC2, stage 2 conf vol 486 vC2, stage 2 conf vol 486 681 486 tC, single (s) 4.1 6.4 6.2 2.2 3.5 3.3 309 90 queue free % 95 77 97 CM capacity (veh/h) 1434 394 581 581 581 581 | | | | | | | |
| Median storage veh) Upstream signal (m) pX, platoon unblocked vC, conflicting volume 148 681 486 vC1, stage 1 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol vC1, unblocked vol 148 681 486 tC, single (s) 4.1 6.4 6.2 tC, stage (s) 2.2 3.5 3.3 p0 queue free % 95 77 97 cM capacity (veh/h) 1434 394 581 Direction, Lane # EB1 WB1 NB Volume Total 824 118 109 Volume Total 824 118 109 Volume total 824 118 109 Volume Right 676 0 17 55 5 5 5 Volume Left 0 77 92 Volume to Capacity 0.48 0.05 0.26 2 2 2 3 5 5 1 6 8 4 4 4 3 4 3 5 1 5 | | | | | | | |
| Upstream signal (m) pX, platoon unblocked vC, conflicting volume 148 681 486 vC1, stage 1 conf vol vC2, stage 2 conf vol vC2, unblocked vol 148 681 486 vCu, unblocked vol 148 681 486 486 426 vC2, stage 2 conf vol vC2, unblocked vol 148 681 486 426 vC1, stage (s) 4.1 6.4 6.2 vC1, stage (s) vC2 3.5 3.3 90 95 77 97 vCM capacity (veh/h) 1434 394 581 95 77 97 vCM capacity (veh/h) 1434 394 581 91 94 581 94 581 94 581 94 95 77 97 vCM capacity (veh/h) 1434 394 581 94 581 94 581 94 581 94 581 95 77 97 vCM capacity (veh/h) 1434 394 581 94 581 94 581 94 581 94 581 94 581 94 581 94 581 94 | | None | | | None | | |
| Upstream signal (m) pX, platoon unblocked vC, conflicting volume 148 681 486 vC1, stage 1 conf vol vC2, stage 2 conf vol vC2, unblocked vol 148 681 486 vCu, unblocked vol 148 681 486 486 426 vC2, stage 2 conf vol vC2, unblocked vol 148 681 486 426 vC1, stage (s) 4.1 6.4 6.2 vC1, stage (s) vC2 3.5 3.3 90 95 77 97 vCM capacity (veh/h) 1434 394 581 95 77 97 vCM capacity (veh/h) 1434 394 581 91 94 581 94 581 94 581 94 95 77 97 vCM capacity (veh/h) 1434 394 581 94 581 94 581 94 581 94 581 95 77 97 vCM capacity (veh/h) 1434 394 581 94 581 94 581 94 581 94 581 94 581 94 581 94 581 94 | Median storage veh) | | | | | | |
| pX, platoon unblocked 148 681 486 vC, conflicting volume 148 681 486 vC2, stage 1 conf vol vCu, unblocked vol 148 681 486 vCu, unblocked vol 148 681 486 tC, single (s) 4.1 6.4 6.2 tC, 2 stage (s) ************************************ | | | | | | | |
| vC, conflicting volume 148 681 486 vC1, stage 1 conf vol vC2, stage 2 conf vol vCu, unblocked vol 148 681 486 vC2, stage 2 conf vol 148 681 486 461 62 vC1, unblocked vol 148 681 486 62 41 6.4 6.2 62 62 62 62 62 62 62 62 63 33 90 95 77 97 66 71 97 66 62 62 63 63 486 63 486 63 486 63 486 62 63 | | | | | | | |
| vC1, stage 1 conf vol vC2, stage 2 conf vol vCu, unblocked vol 148 681 486 tC, single (s) 4.1 6.4 6.2 tC, 2 stage (s) | | | | 148 | | 681 | 486 |
| vC2, stage 2 conf vol vCu, unblocked vol 148 681 486 tC, single (s) 4.1 6.4 6.2 tC, 2 stage (s) | | | | | | | |
| vCu, unblocked vol 148 681 486 tC, single (s) 4.1 6.4 6.2 tC, 2 stage (s) | | | | | | | |
| tC, single (s) 4.1 6.4 6.2 tC, 2 stage (s) | | | | 148 | | 681 | 486 |
| tC, 2 stage (s) tF (s) 2.2 3.5 3.3 p0 queue free % 95 77 97 cM capacity (veh/h) 1434 394 581 Direction, Lane # EB 1 WB 1 NB 1 Volume Total 824 118 109 Volume Total 824 118 109 Volume Left 0 77 92 Volume Right 676 0 17 cSH 1700 1434 415 Volume to Capacity 0.48 0.05 0.26 Queue Length 95th (m) 0.0 1.3 7.9 Control Delay (s) 0.0 5.1 16.8 Lane LOS A C Approach LOS C Intersection Summary Average Delay 2.3 ICU Level of Service | | | | | | | |
| tF (s) 2.2 3.5 3.3 p0 queue free % 95 77 97 cM capacity (veh/h) 1434 394 581 Direction, Lane # EB 1 WB 1 NB 1 Volume Total 824 118 109 Volume Total 0 77 92 Volume Right 676 0 17 cSH 1700 1434 415 Volume to Capacity 0.48 0.05 0.26 Queue Length 95th (m) 0.0 1.3 7.9 Control Delay (s) 0.0 5.1 16.8 Lane LOS A C Approach Delay (s) 0.0 5.1 16.8 Approach LOS C C Intersection Summary 2.3 ICU Level of Service | | | | | | 0.1 | 0.2 |
| p0 queue free % 95 77 97 cM capacity (veh/h) 1434 394 581 Direction, Lane # EB 1 WB 1 NB 1 Volume Total 824 118 109 Volume Total 0 77 92 Volume Left 0 77 92 Volume Right 676 0 17 cSH 1700 1434 415 Volume to Capacity 0.48 0.05 0.26 Queue Length 95th (m) 0.0 1.3 7.9 Control Delay (s) 0.0 5.1 16.8 Lane LOS A C Approach Delay (s) 0.0 5.1 16.8 Approach LOS C C Intersection Summary 2.3 ICU Level of Service | tF (s) | | | 2.2 | | 35 | 33 |
| CM capacity (veh/h) 1434 394 581 Direction, Lane # EB 1 WB 1 NB 1 Volume Total 824 118 109 Volume Total 824 118 109 Volume Left 0 77 92 Volume Right 676 0 17 CSH 1700 1434 415 Volume to Capacity 0.48 0.05 0.26 Queue Length 95th (m) 0.0 1.3 7.9 Control Delay (s) 0.0 5.1 16.8 Lane LOS A C Approach Delay (s) 0.0 5.1 16.8 Approach LOS C Itersection Summary Average Delay 2.3 ICU Level of Service | | | | | | | |
| Direction, Lane # EB 1 WB 1 NB 1 Volume Total 824 118 109 Volume Left 0 77 92 Volume Right 676 0 17 CSH 1700 1434 415 Volume to Capacity 0.48 0.05 0.26 Queue Length 95th (m) 0.0 1.3 7.9 Control Delay (s) 0.0 5.1 16.8 Lane LOS A C Approach Delay (s) 0.0 5.1 16.8 Approach LOS C Intersection Summary Average Delay 2.3 ICU Level of Service | | | | | | | |
| Volume Total 824 118 109 Volume Left 0 77 92 Volume Right 676 0 17 cSH 1700 1434 415 Volume to Capacity 0.48 0.05 0.26 Queue Length 95th (m) 0.0 1.3 7.9 Control Delay (s) 0.0 5.1 16.8 Lane LOS A C Approach Delay (s) 0.0 5.1 16.8 Approach LOS C C Intersection Summary 2.3 ICU Level of Service | civi capacity (ven/n) | | | | | 394 | 100 |
| Volume Left 0 77 92 Volume Right 676 0 17 cSH 1700 1434 415 Volume to Capacity 0.48 0.05 0.26 Queue Length 95th (m) 0.0 1.3 7.9 Control Delay (s) 0.0 5.1 16.8 Lane LOS A C Approach Delay (s) 0.0 5.1 16.8 Approach LOS C C Intersection Summary 2.3 ICU Level of Service | | | | | | | |
| Volume Right 676 0 17 cSH 1700 1434 415 Volume to Capacity 0.48 0.05 0.26 Queue Length 95th (m) 0.0 1.3 7.9 Control Delay (s) 0.0 5.1 16.8 Lane LOS A C Approach Delay (s) 0.0 5.1 16.8 Approach LOS C C Intersection Summary 2.3 ICU Level of Service | Volume Total | 824 | | | | | |
| cSH 1700 1434 415 Volume to Capacity 0.48 0.05 0.26 Queue Length 95th (m) 0.0 1.3 7.9 Control Delay (s) 0.0 5.1 16.8 Lane LOS A C Approach Delay (s) 0.0 5.1 16.8 Approach LOS C Intersection Summary Average Delay 2.3 ICU Level of Service | | 0 | 77 | | | | |
| Volume to Capacity 0.48 0.05 0.26 Queue Length 95th (m) 0.0 1.3 7.9 Control Delay (s) 0.0 5.1 16.8 Lane LOS A C Approach Delay (s) 0.0 5.1 16.8 Approach LOS C Intersection Summary Average Delay 2.3 ICU Level of Service | Volume Right | 676 | 0 | 17 | | | |
| Oueue Length 95th (m) 0.0 1.3 7.9 Control Delay (s) 0.0 5.1 16.8 Lane LOS A C Approach Delay (s) 0.0 5.1 16.8 Approach LOS C Intersection Summary Average Delay 2.3 ICU Level of Service | cSH | 1700 | 1434 | 415 | | | |
| Queue Length 95th (m) 0.0 1.3 7.9 Control Delay (s) 0.0 5.1 16.8 Lane LOS A C Approach Delay (s) 0.0 5.1 16.8 Approach LOS C C Intersection Summary 2.3 ICU Level of Service | Volume to Capacity | 0.48 | 0.05 | 0.26 | | | |
| Control Delay (s) 0.0 5.1 16.8 Lane LOS A C Approach Delay (s) 0.0 5.1 16.8 Approach LOS C C Intersection Summary 2.3 Intersection Capacity Utilization 72.1% ICU Level of Service | | | | | | | |
| Lane LOS A C Approach Delay (s) 0.0 5.1 16.8 Approach LOS C Intersection Summary Average Delay 2.3 Intersection Capacity Utilization 72.1% ICU Level of Service | Control Delay (s) | 0.0 | 5.1 | | | | |
| Approach Delay (s) 0.0 5.1 16.8 Approach LOS C Intersection Summary Average Delay 2.3 Intersection Capacity Utilization 72.1% ICU Level of Service | Lane LOS | | | | | | |
| Approach LOS C Intersection Summary 2.3 Average Delay 2.3 Intersection Capacity Utilization 72.1% ICU Level of Service | | 0.0 | | | | | |
| Intersection Summary 2.3 Average Delay 2.3 Intersection Capacity Utilization 72.1% ICU Level of Service | | 0.0 | 0.1 | | | | |
| Average Delay 2.3 Intersection Capacity Utilization 72.1% ICU Level of Service | | | | Ű | | | |
| Intersection Capacity Utilization 72.1% ICU Level of Service | | | | | | | |
| | | | | | | | |
| | | | | | IC | U Level of S | ervice |
| Analysis Period (min) 15 | Analysis Period (min) | | | 15 | | | |

MOVEMENT SUMMARY

Site: [Jeanne D'Arc/Trim]

Future 2029 AM Roundabout

| Move | Movement Performance - Vehicles | | | | | | | | | | | | | |
|-----------|---------------------------------|--------------------------|------------------|---------------------|-------------------------|---------------------|-------------------------------|---------------------------|-----------------|-----------------------------------|--------------------------|--|--|--|
| Mov ID | OD Mov | Demand Total veh/h | Flows HV % | Deg. Satn v/c | Average Delay sec | Level of Service | 95% Back o Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h | | | |
| South | : Trim | | | | | | | | | | | | | |
| 1 | L2 | 208 | 2.0 | 0.149 | 7.7 | LOS A | 1.0 | 7.0 | 0.26 | 0.55 | 46.4 | | | |
| 2 | T1 | 21 | 2.0 | 0.149 | 3.1 | LOS A | 1.0 | 7.0 | 0.26 | 0.55 | 46.2 | | | |
| 3 | R2 | 1045 | 2.0 | 0.572 | 2.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.36 | 48.4 | | | |
| Appro | bach | 1275 | 2.0 | 0.572 | 3.3 | LOS A | 1.0 | 7.0 | 0.05 | 0.40 | 48.0 | | | |
| East: | Jeanne D' | 'Arc | | | | | | | | | | | | |
| 4 | L2 | 175 | 2.0 | 0.189 | 8.9 | LOS A | 1.2 | 8.4 | 0.49 | 0.62 | 46.0 | | | |
| 5 | T1 | 27 | 2.0 | 0.189 | 4.4 | LOS A | 1.2 | 8.4 | 0.49 | 0.62 | 45.8 | | | |
| 6 | R2 | 3 | 2.0 | 0.189 | 4.4 | LOS A | 1.2 | 8.4 | 0.49 | 0.62 | 44.8 | | | |
| Appro | bach | 205 | 2.0 | 0.189 | 8.2 | LOS A | 1.2 | 8.4 | 0.49 | 0.62 | 45.9 | | | |
| North | : Trim | | | | | | | | | | | | | |
| 7 | L2 | 2 | 2.0 | 0.013 | 9.1 | LOS A | 0.1 | 0.5 | 0.50 | 0.49 | 47.4 | | | |
| 8 | T1 | 7 | 2.0 | 0.013 | 4.6 | LOS A | 0.1 | 0.5 | 0.50 | 0.49 | 47.3 | | | |
| 9 | R2 | 3 | 2.0 | 0.013 | 4.7 | LOS A | 0.1 | 0.5 | 0.50 | 0.49 | 46.2 | | | |
| Appro | bach | 13 | 2.0 | 0.013 | 5.4 | LOS A | 0.1 | 0.5 | 0.50 | 0.49 | 47.0 | | | |
| West: | Jeanne D | 0'Arc | | | | | | | | | | | | |
| 10 | L2 | 8 | 2.0 | 0.128 | 8.4 | LOS A | 0.8 | 5.6 | 0.43 | 0.47 | 48.0 | | | |
| 11 | T1 | 67 | 2.0 | 0.128 | 3.9 | LOS A | 0.8 | 5.6 | 0.43 | 0.47 | 47.8 | | | |
| 12 | R2 | 68 | 2.0 | 0.128 | 3.9 | LOS A | 0.8 | 5.6 | 0.43 | 0.47 | 46.7 | | | |
| Appro | bach | 144 | 2.0 | 0.128 | 4.2 | LOS A | 0.8 | 5.6 | 0.43 | 0.47 | 47.3 | | | |
| All Ve | hicles | 1637 | 2.0 | 0.572 | 4.0 | LOS A | 1.2 | 8.4 | 0.14 | 0.43 | 47.7 | | | |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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MOVEMENT SUMMARY

Site: [Jeanne D'Arc/Trim]

Future 2029 PM Roundabout

| Movement Performance - Vehicles | | | | | | | | | | | | | |
|---------------------------------|-----------|----------------|---------|-------------|---------|----------|-----------------|----------|--------|-----------|---------------|--|--|
| Mov | OD | Demand | | Deg. | Average | Level of | 95% Back | | Prop. | Effective | Average | | |
| ID | Mov | Total veh/h | HV % | Satn v/c | Delay | Service | Vehicles veh | Distance | Queued | Stop Rate | Speed km/h | | |
| South | · Trim | ven/n | % | V/C | Sec | _ | ven | m | _ | per veh | Km/n | | |
| 1 | L2 | 146 | 2.0 | 0.107 | 7.9 | LOS A | 0.7 | 4.7 | 0.32 | 0.57 | 46.1 | | |
| 2 | T1 | 8 | 2.0 | 0.107 | 3.4 | LOS A | 0.7 | 4.7 | 0.32 | 0.57 | 46.0 | | |
| 3 | R2 | 656 | 2.0 | 0.359 | 2.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.36 | 48.5 | | |
| Appro | ach | 811 | 2.0 | 0.359 | 3.4 | LOS A | 0.7 | 4.7 | 0.06 | 0.40 | 48.0 | | |
| East: | Jeanne D' | Arc | | | | | | | | | | | |
| 4 | L2 | 103 | 2.0 | 0.105 | 8.3 | LOS A | 0.6 | 4.4 | 0.39 | 0.57 | 46.2 | | |
| 5 | T1 | 17 | 2.0 | 0.105 | 3.8 | LOS A | 0.6 | 4.4 | 0.39 | 0.57 | 46.1 | | |
| 6 | R2 | 2 | 2.0 | 0.105 | 3.8 | LOS A | 0.6 | 4.4 | 0.39 | 0.57 | 45.1 | | |
| Appro | ach | 122 | 2.0 | 0.105 | 7.6 | LOS A | 0.6 | 4.4 | 0.39 | 0.57 | 46.2 | | |
| North | : Trim | | | | | | | | | | | | |
| 7 | L2 | 3 | 2.0 | 0.014 | 8.4 | LOS A | 0.1 | 0.5 | 0.40 | 0.46 | 47.7 | | |
| 8 | T1 | 8 | 2.0 | 0.014 | 3.9 | LOS A | 0.1 | 0.5 | 0.40 | 0.46 | 47.6 | | |
| 9 | R2 | 4 | 2.0 | 0.014 | 4.0 | LOS A | 0.1 | 0.5 | 0.40 | 0.46 | 46.5 | | |
| Appro | bach | 16 | 2.0 | 0.014 | 4.8 | LOS A | 0.1 | 0.5 | 0.40 | 0.46 | 47.3 | | |
| West: | Jeanne D | 'Arc | | | | | | | | | | | |
| 10 | L2 | 7 | 2.0 | 0.191 | 8.0 | LOS A | 1.2 | 8.9 | 0.35 | 0.42 | 48.3 | | |
| 11 | T1 | 116 | 2.0 | 0.191 | 3.5 | LOS A | 1.2 | 8.9 | 0.35 | 0.42 | 48.1 | | |
| 12 | R2 | 117 | 2.0 | 0.191 | 3.5 | LOS A | 1.2 | 8.9 | 0.35 | 0.42 | 47.0 | | |
| Appro | bach | 240 | 2.0 | 0.191 | 3.7 | LOS A | 1.2 | 8.9 | 0.35 | 0.42 | 47.6 | | |
| All Ve | hicles | 1188 | 2.0 | 0.359 | 3.9 | LOS A | 1.2 | 8.9 | 0.16 | 0.42 | 47.7 | | |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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