Stantec Consulting Ltd. 400 - 1331 Clyde Avenue, Ottawa ON K2C 3G4



March 27, 2018 File: 1604010199

Attention: Wendy Tse

Planner II – Planning Infrastructure and Eco Development Department

110 Laurier Avenue West Ottawa, ON. K1P 1J1

Dear Ms. Tse,

Reference: 1000 Thomas Spratt Place Adequacy of Services

#### **BACKGROUND**

Stantec Consulting Ltd. has been commissioned by Eglise de Dieu D'Expression Française D'Ottawa to prepare a letter in support of a Zoning By-law Amendment for a property situated at 1000 Thomas Spratt Place. The zoning amendment would permit a place of worship as an additional use in the IL – Light Industrial zone. The place of worship will be located on the ground floor and offices will remain on the 2<sup>nd</sup> floor of the existing building.

The site is located at the southwest corner of Thomas Spratt Place and Thurston Drive. The existing 2 storey building is located in the centre of the site and has a gross floor area of 1800 sq. metres. The applicant proposes t to modify the ground floor to support a 1156 sq. m place of worship that will hold up to 300 people while maintaining office use on the second floor. The intent of this letter is to provide an engineering rationale for the modifications with respect to any proposed changes in local infrastructure demands or loading, while adhering to City of Ottawa design guidelines and recommendations and utilizing the existing local infrastructure in accordance with prior consultation with City of Ottawa staff.

The site is currently serviced by connections to the existing 675mm diameter storm sewer, 250mm diameter sanitary sewer and 300mm diameter watermain within the Thomas Spratt ROW near the northeast boundary of the site displayed in **Appendix C**. The property is located within the City's water pressure zone 2C. Ground elevations of the site are approximately 82.7m.

#### **POTABLE WATER**

#### **DEMANDS**

Water demands for the development were estimated using the City of Ottawa Water Distribution Design Guidelines (2009). A daily rate of 28,000 L/gross ha/day has been applied for average day other commercial domestic demands for the office buildings on the second floor. A daily rate of 15 L/(seat/day), has been applied for average day domestic demands for the ground floor place of worship). For detailed domestic water demand estimates, (see **Appendix A**).



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Reference: 1000 Thomas Spratt Place Adequacy of Services

The average day demand (AVDY) for the modified existing building was determined to be 0.07 L/s. The maximum daily demand (MXDY) is 1.5 times the AVDY for both institutional and industrial use equates to 0.11 L/s. The peak hour demand (PKHR) is 1.8 times the MXDY, totaling 0.20 L/s.

Based on the above demands, hydraulic gradelines vary from approximately 124.5m to 130.1m as confirmed through boundary conditions as provided by the City of Ottawa.

Non-combustible construction was considered in the assessment for fire flow requirements according to the FUS Guidelines. Based on calculations per the FUS Guidelines (**Appendix A**), the maximum required fire flows for this development are 117 L/s (7,000L/min).

#### **ANALYSIS**

Based on average existing on-site elevations of 82.7m and expected pressures within the watermain system of 124.5m to 130.1m, on-site pressures are expected to range from 41.8m to 47.4m (59.4 to 67.4 psi). These values are within the recommended pressure range of 275 kPa to 552 kPa (40 to 80 psi), as recommended by the City of Ottawa's Water Distribution Design Guidelines.

Based on anticipated maximum day domestic demand and fire flow requirements per the FUS methodology (**Appendix A**) of 117L/s (the maximum fire flow noted for the modified existing building) the 300mm watermain within Thomas Spratt Place is expected to maintain a residual pressure of 41.8m (59.4 psi). This demonstrates that the existing watermain and nearby hydrants can provide adequate fire flows in excess of the calculated 117L/s fire flow requirement with the required residual pressure of 20 PSI. The nearest existing hydrant is located at the site's northeast boundary, on the south side of Thomas Spratt Place within 90m as per City of Ottawa requirements.

#### **SANITARY SEWER**

The site will continue to be serviced via the existing 250mm diameter sanitary sewer situated within the Thomas Spratt Place ROW at the eastern boundary of the site, (see **Appendix C**). The proposed building modifications will allow the 1000 Thomas Spratt Place property to function as a place of worship on the ground floor and office space on the second floor. The place of worship value of 15 L/seat/day was taken from the Churches section of Appendix 4-A.2 of the City of Ottawa Sewer Design Guidelines (2012). As outlined in the City of Ottawa Sewer Design Guidelines and the MOE's Design Guidelines for Sewage Works, the following criteria were used to calculate estimated wastewater flow rates.

- Minimum Velocity 0.6 m/s (0.8 m/s for upstream sections)
- Maximum Velocity 3.0 m/s



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Reference: 1000 Thomas Spratt Place Adequacy of Services

- Manning roughness coefficient for all smooth wall pipes 0.013
- Average Wastewater Generation 15 L/person/day (Churches)
- Average Wastewater Generation 28,000L/ha/day (institutional)
- Residential Peak Factor 4.0 (Harmon's)
- Institutional Peak Factor 1.5 (Harmon's)
- Extraneous Flow Allowance 0.28 l/s/ha (conservative value)

Based on the above, the sites existing peak sanitary discharge to the downstream 250mm sanitary sewer for the existing building use is 0.23 L/s and for the proposed change in building use is 0.38 L/s, (see **Appendix B**).

## **STORM SEWER**

The site is currently serviced via an existing 675mm diameter storm sewer situated within the Thomas Spratt ROW at the northeast boundary of the site, displayed in **Appendix C**. There is no proposed increase to the amount of impervious on the site or area modifications proposed to the exterior of the 1000 Thomas Spratt building for this application, and as such, no increases in the estimated peak discharge rate for the site have been identified.

#### **UTILITIES**

As the subject site lies within a developed industrial community, Hydro, Bell, Gas and Cable servicing for the proposed development should be readily available. It is anticipated that existing infrastructure will be sufficient to provide a means of distribution for the proposed site. No off-site works are anticipated to be required for redevelopment of the subject site.

# **RECOMMENDATIONS**

Based on the findings above, it is anticipated that the current servicing infrastructure for the 1000 Thomas Spratt Place property will be adequate for rezoning purposes to permit the addition of a place of worship on the subject property.



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Reference: 1000 Thomas Spratt Place Adequacy of Services

Regards,

## STANTEC CONSULTING LTD.

Dustin Thiffault, P.Eng.

Project Engineer, Community Development

Phone: (613) 724-4385 Fax: (613) 722-2799

Dustin.Thiffault@Stantec.com

Attachment: Appendix A:

Boundary Conditions, Water Demand Estimates

**FUS Calculations** 

Appendix B:

Sanitary Discharge Calculations

Appendix C:

Existing Watermain Services Existing Sanitary Services Existing Stormwater Services

Floor Plan Drawings – Existing Building

W:\active\1 planning\_landscape\1604 Projects\160410199\_1000 Thomas Spratt Place\design\report\Service Adequacy Report/\_2018\_03\_27\_Servicing.docx



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Reference: 1000 Thomas Spratt Place Adequacy of Services

# **APPENDIX A**

# **Odam, Cameron**

From: Baker, Adam <adam.baker@ottawa.ca>

**Sent:** Monday, April 09, 2018 9:18 AM

**To:** Tse, Wendy; Oram, Cody; Odam, Cameron

**Subject:** RE: 1000 Thomas Spratt Place - Boundary Conditions Request

**Attachments:** 1000 Thomas Spratt April 2018.pdf

# Hi Cameron,

# Please see attached the requested water boundary conditions:

The following are boundary conditions, HGL, for hydraulic analysis at 1000 Thomas Spratt (zone 2C) assumed to be connected to the 305mm on Thomas Spratt (see attached PDF for location).

Minimum HGL = 125.1m

Maximum HGL = 130.1m

MaxDay + FireFlow (117 L/s) = 124.5m

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

# Thanks,

#### Adam Baker, EIT

**Engineering Intern** 

Planning, Infrastructure and Economic Development Department - Services de la planification, de l'infrastructure et du développement économique

Development Review - South Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste 26552, Adam.Baker@ottawa.ca

From: Baker, Adam

Sent: Thursday, April 05, 2018 1:30 PM

To: Tse, Wendy < Wendy. Tse@ottawa.ca>; Oram, Cody < Cody. Oram@ottawa.ca>; 'cameron.odam@stantec.com'

<cameron.odam@stantec.com>

Subject: RE: 1000 Thomas Spratt Place - Boundary Conditions Request

Hi Cameron,

The boundary condition request has been forwarded to our water resources group. I'll send you the boundary conditions as soon as I receive them.

## Thanks,

#### Adam Baker, EIT

**Engineering Intern** 

Planning, Infrastructure and Economic Development Department - Services de la planification, de l'infrastructure et du développement économique

Development Review - South Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste 26552, Adam.Baker@ottawa.ca

From: Odam, Cameron < Cameron. Odam@stantec.com>

**Sent:** Thursday, April 05, 2018 11:39 AM **To:** Tse, Wendy < Wendy. Tse@ottawa.ca>

Cc: Meloshe, Nancy < Nancy. Meloshe@stantec.com >

Subject: 1000 Thomas Spratt Place - Boundary Conditions Request

Hi Wendy,

Could you please forward the following boundary conditions request for 1000 Thomas Spratt Place, including the attachment, to the contact at the city who would be able to provide them.

I am looking for watermain hydraulic boundary conditions for an existing site located at 1000 Thomas Spratt Place. A portion of the existing office warehouse building, the entire ground floor is proposed to be used as a place of worship. We will continue to connect to the existing 305mm watermain on Thomas Spratt Place to service the site.

Attached are the FUS calculations for the proposed building.

Estimated domestic demands and fire flow requirements for the site are as follows:

Average Day Demand - 0.07L/s
Max Day Demand - 0.11L/s
Peak Hour Demand - 0.20L/s

Fire Flow Requirement per FUS - 117L/s

Thanks,

Cameron

#### **Cameron Odam**

Direct: +16137244353 Fax: +16137222799

Stantec Consulting Ltd. 400 - 1331 Clyde Avenue Ottawa ON K2C 3G4 CA



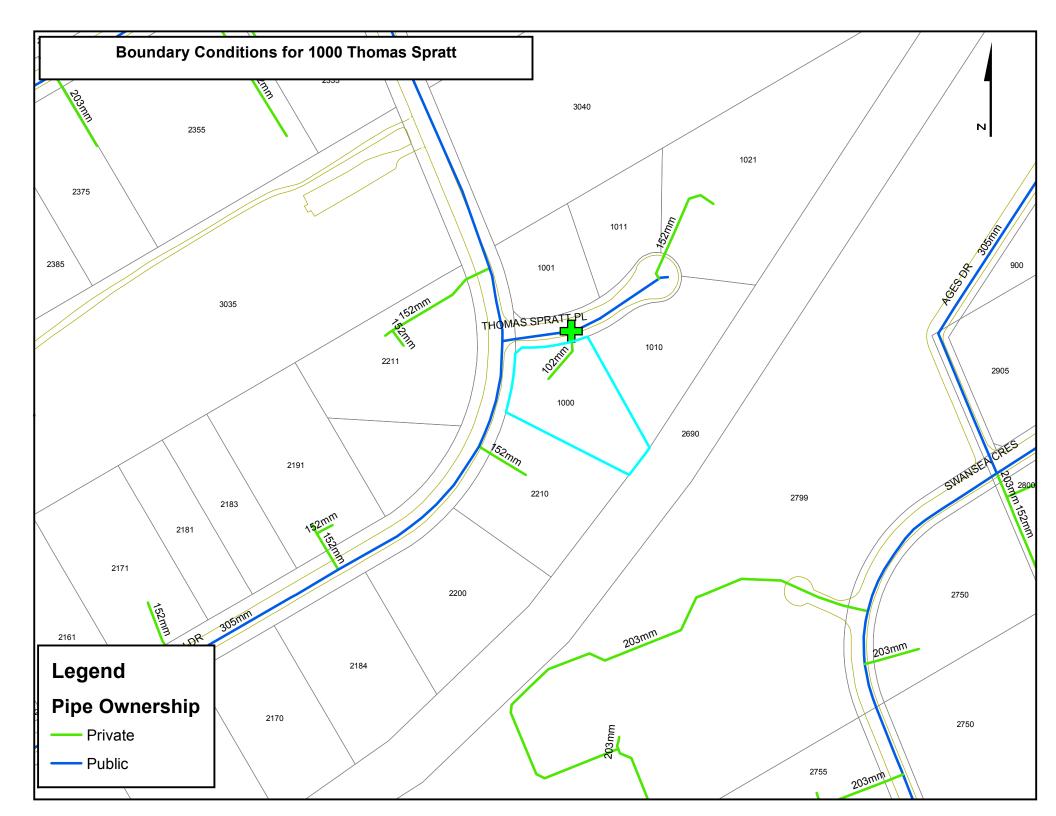


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# <u>1000 Thomas Spratt Place - Domestic Water Demand Estimates</u> - Based on Douglas Clancey Architectural Site Plan (160410199)

Building ID	Area	Population	Daily Rate of	Avg Day I	Demand <sup>2</sup>	Max Day	Demand <sup>3</sup>	Peak Hour Demand 3				
	(m <sup>2</sup> )		Demand 1	(L/min)	(L/s)	(L/min)	(L/s)	(L/min)	(L/s)			
Place of worship	1156	300	15	3.1	0.052	4.7	0.078	8.4	0.141			
Office	644	-	28,000	1.3	0.021	1.9	0.031	3.4	0.056			
Total Site :	1800			4.4	0.07	6.6	0.11	11.8	0.20			

<sup>1</sup> For the purpose of this study it is predicted that other commercial facilities will be operated 12 hours per day generating 28,000 L/gross ha/d, and the place of worship is based on 15 L/(sanctuary seat/d). These values reference the MOE Drinking water demand guidelines (2008)

<sup>2</sup> City of Ottawa water demand criteria used to estimate peak demand rates for industrial and insitutional areas are as follows: maximum day demand rate = 1.5 x average day demand rate maximum hour demand rate = 1.8 x maximum day demand rate



# **FUS Fire Flow Calculation**

Calculations based on: "Water Supply for Public Fire Protection" by Fire Underwriters' Survey, 1999

Stantec Project #: 1604-10199

Project Name: 1000 Thomas Spratt Place

Date: April 5, 2018

Data input by: Cameron Odam

Notes:

Building Classification A and D

Fire Flow Calculation #: 1

Building Type/Description/Name: Office Space/Place of worship

		Table A: Fire U	Inderwriters Survey Determination	n of Required Fir	e Flow - Long Method	d								
Step	Task	Term	Options	Multiplier Associated with Option	Choose:	Value Used	Unit	Total Fire Flow (L/min)						
			Fra											
	Choose Frame Used		Wood Frame	1.5										
1	for Construction of	Coefficient related to	Ordinary construction	1	Non-combustible									
	Unit	type of construction	Non-combustible construction	0.8	construction	0.8	-							
		(C)	Fire resistive construction (> 3 hrs)	0.6										
	Chassa Turas of		, ,	oor Space Area										
	Choose Type of Housing (if TH,		1	our space Area		1								
2	Enter Number of		Single Family	1	Other (Comm, Ind, Apt									
	Units Per TH Block)	Type of Housing	Townhouse - indicate # of units	8	etc.)	1	Units							
	Offics Per TH Block)		Other (Comm, Ind, Apt etc.)	1	<u> </u>									
2.2	# of Storeys	Number of Floors/Storeys in the Unit (do not include basement):  2 Storeys												
3	Enter Ground Floor	Average Floor Area (A) based on fire resistive building design when vertical openings are inadequately protected:  Square Metres (m2)  Are Sq Metres (m2)												
	Area of One Unit													
4	Obtain Required Fire Flow without Reductions	Required Fire Flow (without reductions or increases per FUS) (F = 220 * C * VA)  Round to nearest 1000L/min												
5	Apply Factors Affecting Burning		Reductions/Increases	S Due to Factors	Affecting Burning			<u>I</u>						
			Non-combustible	-0.25										
	Choose	Occupancy content	Limited combustible	-0.15										
5.1	Combustibility of	hazard reduction or	Combustible	0	Limited combustible	-0.15	N/A	5,950						
	Building Contents	surcharge	Free burning	0.15										
			Rapid burning	0.25										
		Sprinkler reduction	Adequate Sprinkler conforms to NFPA13	-0.3	None	0	N/A	0						
			None	0										
			Water supply is standard for sprinkler and	-0.1		0								
	Choose Reduction	Matau Comalio Candit	fire dept. hose line	*	Water supply is not			0						
	5.2 Due to Presence of	i water Subbly Credit				0	N/A							
5.2	Due to Presence of Sprinklers	Water Supply Credit	Water supply is not standard or N/A	0	standard or N/A	0	N/A							
5.2		Sprinkler Supervision	Water supply is not standard or N/A  Sprinkler system is fully supervised	-0.1	standard or N/A Sprinkler not fully	0	N/A N/A	0						
5.2			***	-	standard or N/A									
5.2	Sprinklers	Sprinkler Supervision	Sprinkler system is fully supervised	-0.1	standard or N/A Sprinkler not fully									
	Sprinklers  Choose Separation	Sprinkler Supervision Credit Exposure Distance	Sprinkler system is fully supervised  Sprinkler not fully supervised or N/A  North Side East Side	-0.1 0 30.1 to 45.0m 45.1m or greater	Sprinkler not fully supervised or N/A  0.05 0	0	N/A	0						
5.3	Sprinklers	Sprinkler Supervision Credit	Sprinkler system is fully supervised  Sprinkler not fully supervised or N/A  North Side East Side South Side	-0.1 0 30.1 to 45.0m 45.1m or greater 20.1 to 30.1m	standard or N/A  Sprinkler not fully supervised or N/A  0.05 0 0.1									
	Sprinklers  Choose Separation Distance Between	Sprinkler Supervision Credit Exposure Distance Between Units	Sprinkler system is fully supervised  Sprinkler not fully supervised or N/A  North Side  East Side  South Side  West Side	-0.1 0 30.1 to 45.0m 45.1m or greater 20.1 to 30.1m 45.1m or greater	Sprinkler not fully supervised or N/A  0.05 0 0.1 0	0 0.15	N/A m	0 893						
	Sprinklers  Choose Separation Distance Between Units	Sprinkler Supervision Credit Exposure Distance Between Units	Sprinkler system is fully supervised  Sprinkler not fully supervised or N/A  North Side East Side South Side	-0.1  0  30.1 to 45.0m  45.1m or greater 20.1 to 30.1m  45.1m or greater to nearest 1000	standard or N/A  Sprinkler not fully supervised or N/A  0.05 0 0.1 0	0 0.15 n limits a	N/A m	0 893 <b>7,000</b>						
	Sprinklers  Choose Separation Distance Between	Sprinkler Supervision Credit Exposure Distance Between Units	Sprinkler system is fully supervised  Sprinkler not fully supervised or N/A  North Side  East Side  South Side  West Side	-0.1  0  30.1 to 45.0m  45.1m or greater 20.1 to 30.1m  45.1m or greater to nearest 1000	standard or N/A  Sprinkler not fully supervised or N/A  0.05 0 0.1 0 1 L/min, with max/min tal Required Fire Flow	0 0.15 n limits a	n/A m pplied:	0 893 7,000 117						
5.3	Sprinklers  Choose Separation Distance Between Units  Obtain Required	Sprinkler Supervision Credit Exposure Distance Between Units	Sprinkler system is fully supervised  Sprinkler not fully supervised or N/A  North Side  East Side  South Side  West Side	-0.1  0  30.1 to 45.0m  45.1m or greater 20.1 to 30.1m  45.1m or greater to nearest 1000	standard or N/A  Sprinkler not fully supervised or N/A  0.05 0 0.1 0	0 0.15 n limits a v (above,	N/A m pplied: ) in L/s: w (hrs)	0 893 <b>7,000</b>						



March 27, 2018 Wendy Tse Planner II – Planning Infrastructure and Eco Development Department Page 6 of 7

Reference: 1000 Thomas Spratt Place Adequacy of Services

# **APPENDIX B**

Stantec

# 1000 THOMAS SPRATT PLACE

DATE: REVISION: DESIGNED BY: CHECKED BY: 4/17/2018 1 CO

# SANITARY SEWER DESIGN SHEET (City of Ottawa)

FILE NUMBER: 160410199

# DESIGN PARAMETERS

MAX PEAK FACTOR (RES.)= AVG. DAILY FLOW / PERSON MINIMUM VELOCITY 0.60 m/s 4.0 15 l/p/day MIN PEAK FACTOR (RES.)= 2.0 COMMERCIAL 50,000 l/ha/day 3.00 m/s MAXIMUM VELOCITY PEAKING FACTOR (INDUSTRIAL): 2.4 INDUSTRIAL (HEAVY) 55,000 l/ha/day MANNINGS n 0.013 PEAKING FACTOR (COMM., INST.): 1.5 INDUSTRIAL (LIGHT) 35,000 l/ha/day BEDDING CLASS В PERSONS / SINGLE 1.0 INSTITUTIONAL 28,000 l/ha/day MINIMUM COVER 2.50 m 0.28 l/s/Ha

PERSONS / TOWNHOME 1.0 INFILTRATION

				<u> </u>												PERSONS / APARTMENT 1.0																		
LOC	CATION		RESIDENTIAL AREA AND POPULATION						COMMERCIAL INDUSTR		STRIAL (L) INDUSTRIAL (H)		INSTITUTIONAL		GREEN / UNUSED C+I+		C+I+I	INFILTRATION		٧	TOTAL		PIPE											
AREA ID NUMBER	FROM M.H.	TO M.H.	AREA Populatio	UNITS	APT	POP.	CUMULA AREA	ATIVE POP.	PEAK FACT.	PEAK FLOW	AREA	ACCU. AREA	AREA	ACCU. AREA	AREA	ACCU. AREA	AREA	ACCU. AREA	AREA	ACCU. AREA	PEAK FLOW	TOTAL AREA	ACCU. AREA	INFILT. FLOW	FLOW	LENGTH	DIA	MATERIAL	CLASS	SLOPE	CAP.	CAP. V PEAK FLOW	VEL.	VEL. (ACT.)
NOWBER	IVI.I I.	IVI.I I.	(ha)	1 100014	ALI		(ha)	ror.	TACT.	(l/s)	(ha)	(ha)	(ha)	(ha)	(ha)	(ha)	(ha)	(ha)	(ha)	(ha)	(l/s)	(ha)	(ha)	(l/s)	(l/s)	(m)	(mm)			(%)	(I/s)	(%)	(m/s)	(m/s)
PRE	BLDG	MAIN	0.000 0	0	0	0	0.00	0	4.00	0.00	0.000	0.00	0.000	0.00	0.000	0.00	0.180	0.18	0.340	0.34	0.09	0.52	0.52	0.15	0.23	41.5	250 200	PVC	SDR 35	1.00	60.6	0.38%	1.22	0.23
POST	BLDG	MAIN	0.120 300	0	0	300	0.12	300	4.00	0.21	0.000	0.00	0.000	0.00	0.000	0.00	0.060	0.06	0.340	0.34	0.03	0.52	0.52	0.15	0.38	41.5	250	PVC	SDR 35	1.00	60.6	0.63%	1.22	0.30
																											200							

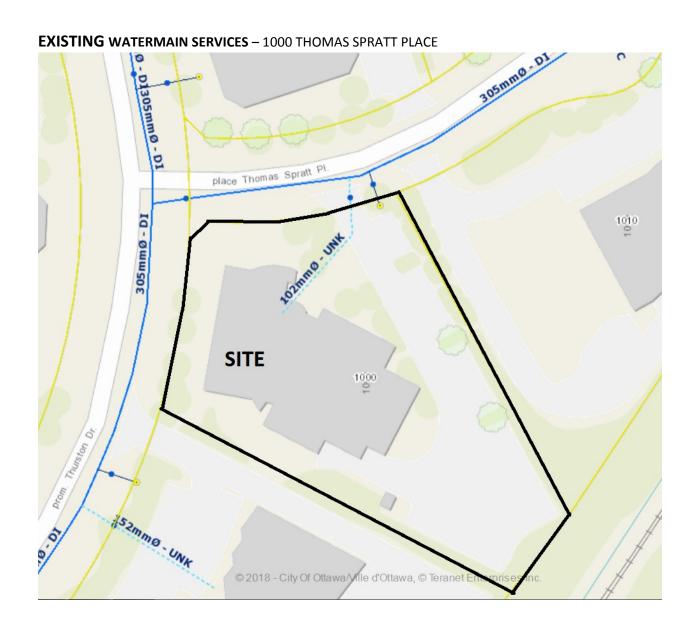
1 of 1 2018-04-17-160410199.xlsx



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Reference: 1000 Thomas Spratt Place Adequacy of Services

# **APPENDIX C**



**EXISTING SANITARY SERVICES** – 1000 THOMAS SPRATT PLACE SITE 1000

# **EXISTING STORMWATER SERVICES** – 1000 THOMAS SPRATT PLACE 92m - 525mm conc 80.04 9. Anace Thomas Spratt Pl. SITE 1000 © 2018 - City Of Ottawa/Ville d'Ottawa, © Teranet E

