



### **FUNCTIONAL SERVICING REPORT**

#### **FOR**

## 3194 JOCKVALE ROAD BARRHAVEN TOWN CENTRE RICHCRAFT HOMES

CITY OF OTTAWA

**PROJECT NO.: 14-735** 

DEC 2018– 1<sup>ST</sup> SUBMISSION © DSEL

#### FUNCTIONAL SERVICING REPORT FOR 3194 JOCKVALE ROAD BARRHAVEN TOWN CENTRE RICHCRAFT HOMES

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# FUNCTIONAL SERVICING REPORT FOR 3194 JOCKVALE ROAD BARRHAVEN TOWN CENTRE RICHCRAFT HOMES

DEC 2018 - 1<sup>ST</sup> SUBMISSION

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#### 1.0 INTRODUCTION

Richcraft Homes have retained David Schaeffer Engineering Ltd. (DSEL) to prepare a Functional Servicing Report (FSR) in support of their application for draft plan approval.

Richcraft Homes is proposing a mix of residential and commercial development on 3194 Jockvale Road (PIN 045951677) within the South Nepean Town Centre (SNTC). The study area is subject to development permit and zoning by-law amendment applications. The FSR study area measures approximately 10.6 ha and is located north of the future extension of Chapman Mills Drive, east of the existing Kennedy-Burnett Stormwater Management Facility Road, west of Greenbank Road and south of an existing commercial development.

The preliminary municipal servicing for the SNTC was originally considered in the *South Nepean Town Centre Community Design Plan* (2006 CDP) (City of Ottawa, July 2006). The 2006 CDP considered the study area to consist of high-rise and mid-rise mixed use land uses and a portion of a neighbourhood park. Per the 2006 CDP, the mixed-use land uses permit apartments, and a variety of retail office and commercial uses. The excerpted land use breakdown and corresponding development statistics from the 2006 CDP are also included in *Appendix B*, and summarized in *Table 1* below. The design plan was completed in order to prepare an over-arching vision for the servicing strategy and cohesive development of the SNTC (165 ha total area). The report identifies existing infrastructure, environmental constraints and identifies the neighbourhood-level trunk services that will service all properties within the SNTC and support the proposed development of the SNTC.

The proposed draft plan of subdivision contemplates approximately 3.86 ha of residential development and 5.9 ha of commercial development. At the time of this FSR, latest estimates report approximately 240 condo flats within the residential area. This is subject to change as the design of the study area advances. The realignment of Jockvale Road is proposed to run through the study area and a future collector road is proposed at the southern boundary of the study area. Both roads have 20 m wide Right-of-Way (ROW)

widths. The proposed plan of subdivision can be seen in *Appendix A*. Corresponding development stats can be seen in *Table 1* below.

**Table 1: Summary of Land Uses and Population Projections** 

	SNTC CDP JULY 2006			3194 JOCKVALE RD. FSR DEC 2018			018	
Land Use	Gross Area (ha)	Projected Residential Units*	Residential Pop. per Unit **	Pop.	Gross Area (ha)	Projected Residential Units	Residential Pop. per Unit **	Pop.
High-Rise M.U.	5.34	1335	1.8	2403				
Mid-Rise M.U.	3.29	658	1.8	1184				
Neigh. Park	0.72							
Collector Roads	1.26				0.82			
Residential					3.86	240	2.1	504
Commercial					5.93			
Total	10.61	1993		3587	10.61	240		504

<sup>\*</sup>NOTE: Projected residential units based on unit densities (250 units/ha – High Rise Mixed-Use & 200 units/ha – Mid-Rise Mixed-Use) taken from the South Nepean Town Centre Community Design Plan (City of Ottawa, July 2006).

This FSR is provided to demonstrate conformance with the design criteria of the City of Ottawa, the *2006 CDP*, other background studies, and general industry practice. This FSR has also been prepared in accordance with the City of Ottawa's Servicing Study Guidelines for Development Applications, as demonstrated by the checklist included in *Appendix A*.

#### 1.1 Existing Conditions

Under existing conditions, the study area is predominantly occupied by agricultural uses. A forested area exists in the northeast corner of the study area. A remnant and unused segment of old Jockvale Road runs through the study area.

The existing elevations within the study area generally range from 93m to 96.5m. Per the *Geotechnical Investigation - Proposed Commercial Development - Greenbank Road* (Paterson Group, February 2012), the soil profile in the area consists of topsoil or fill, underlain by a silty clay layer followed by glacial till deposit. Groundwater is expected between 2m to 3m depth and permissible grade raise restrictions were reported to be bewtween 0.8m to 1.5m. Additional geotechnical details can be found within the *Geotechnical Investigation - Proposed Commercial Development - Greenbank Road* (Paterson Group, February 2012).

<sup>\* \*</sup>NOTE: Population projections may differ from population estimates used in background Transportation Studies, Planning Rationale, and other studies. Population projection and residential population per unit values are based on Ministry of Environment and Climate Change guidelines for servicing demand calculations. Local & Private Roads included in Block estimates above.

The study area is located within the Jock River – Barrhaven sub-watershed which is within the jurisdiction of the Rideau Valley Conservation Authority (RVCA).

A north-south municipal drain (Burnett Drain) is located in the central portion of the study area. The Burnett Drain ultimately outlets into the Jock River to the south. Per discussions with City staff, it is understood that the proposed plan of subdivision triggers the need for the existing Burnett Drain to be abandoned. This is to be completed per the appropriate process outlined in the *Drainage Act*.

#### 1.2 Required Permits / Approvals

The City of Ottawa must approve detailed engineering design drawings and reports prior to construction of the municipal infrastructure identified in this report. This is expected to occur as part of the approval process for *Planning Act* development applications.

The following additional approvals and permits listed in *Table 2* could be expected to be required prior to construction of the municipal infrastructure detailed herein. Please note that other permits and approvals may be required, as detailed in the other studies submitted as part of the *Planning Act* development applications (e.g. *Tree Conservation Report, Environmental Impact Statement, Phase 1 Environmental Site Assessment, etc.*).

**Table 2: Anticipated Permit/Approval Requirements** 

Agency	Permit/Approval Required	Trigger	Remarks
RVCA	Application for "Development, Interference with Wetlands and Alteration to Shorelines and Watercourses" Ont. Reg. 174/06	Alterations of existing watercourse.	Existing watercourses through the site may be altered as part of development.
MOECP	Environmental Compliance Approval	Construction of new sanitary, storm sewers, and appurtenances.	The MOECP is expected to review the stormwater collection system, and wastewater collection system by transfer of review submission.
MOECP	Permit to Take Water	Construction of proposed land uses (e.g. basements for residential homes) and services.	Pumping of groundwater or surface water may be required during construction.
City of Ottawa	MOE Form 1 – Record of Watermains Authorized as a Future Alteration.	Construction of watermains.	The City of Ottawa is expected to review the watermains on behalf of the MOE through the Form 1 – Record of Watermains Authorized as a Future Alteration.
City of Ottawa	Commence Work Notification (CWN)	Construction of new sanitary and storm sewer throughout the subdivision.	The City of Ottawa will issue a commence work notification for construction of the sanitary and storm sewers once an ECA is issued by the MOECP.

City of	Permission/license to	Construction of	Construction activities and
Ottawa /	access/occupation and/or	servicing	permanent infrastructure beyond
Private	legal property	infrastructure (e.g.	the FSR study area may trigger
Landowners	instruments.	sewer, overland flow	legal agreements.
		route) beyond the	
		FSR study area.	

#### 1.3 Summary of Pre-Consultation

#### 1.3.1 City of Ottawa, October 11th, 2018

A formal Pre-Application Consultation with City of Ottawa staff occurred October 11<sup>th</sup>, 2018. The purpose of the meeting was to discuss the proposed development, review technical considerations and identify/confirm the studies required to accompany the submission of a Plan of Subdivision application. A copy of the Pre-Application Consultation meeting notes can be found in *Appendix A*.

#### 2.0 GUIDELINES, PREVIOUS STUDIES, AND REPORTS

#### 2.1 Existing Studies, Guidelines, and Reports

- Ottawa Sewer Design Guidelines, City of Ottawa, SDG002, October 2012. (Sewer Design Guidelines)
  - Technical Bulletin ISDTB-2014-01, Revisions to Ottawa Design Guidelines Sewer, City of Ottawa, February 5, 2014. (ISDTB-2014-01)
  - Technical Bulletin PIEDTB-2016-01, Revisions to Ottawa Design Guidelines Sewer, City of Ottawa, September 6, 2016. (PIEDTB-2016-01)
  - Technical Bulletin ISTB-2018-01, Revisions to Ottawa Design Guidelines Sewer, City of Ottawa, March 21, 2018. (ISTB-2018-01)
- Ottawa Design Guidelines Water Distribution, City of Ottawa, July 2010. (Water Supply Guidelines)
  - o Technical Bulletin ISD-2010-2, City of Ottawa, December 15, 2010. (ISDTB-2010-2)
  - o Technical Bulletin ISDTB-2014-02, City of Ottawa, May 27, 2014. (ISDTB-2014-02)
  - o Technical Bulleting ISTB-2018-02, City of Ottawa, March 21, 2018. (ISTB-2018-02)
- ➤ Design Guidelines for Sewage Works, Ministry of the Environment, 2008. (MOE Design Guidelines)
- Stormwater Planning and Design Manual, Ministry of the Environment, March 2003. (SWMP Design Manual)
- Drainage Act, Ministry of the Environment, 1990. (Drainage Act)
- ➤ Erosion & Sediment Control Guidelines for Urban Construction, Greater Golden Horseshoe Area Conservation Authorities, December 2006. (E&S Guidelines)
- South Nepean Town Centre Community Design Plan, City of Ottawa, July 2006. (CDP)
- > Appendix 1 South Nepean Town Centre Community Design Plan, Preliminary Serviceability Report, Cumming Cockburn Limited, December 2005.
- ➤ Geotechnical Investigation Proposed Commercial Development Greenbank Road, Paterson Group, February 2, 2012.
- ➤ Kennedy Burnett Potable Water Master Servicing Study, Stantec Consulting Ltd, April 29, 2014.
- > South Nepean Collector: Phase 2, Hydraulics Review, Technical Memorandum, Novatech, August 20, 2015.
- ➤ Kennedy-Burnett Stormwater Management Facility Functional Design Report, CH2M, February 17, 2017.
- South Nepean Town Centre Updated Land Use Plan and Stats, Fotenn, April 26, 2018.

#### 3.0 WATER SUPPLY SERVICING

#### 3.1 Existing Water Supply Services

The study area lies within the existing City of Ottawa BARR pressure zone. An existing 750mm diameter trunk watermains exist within Greenbank Road to the east of the study area. A 300mm diameter watermain exists to the north of the study area, servicing the existing commercial development of off the Greenbank Road trunk watermain.

#### 3.2 Water Supply Servicing Design

The water supply servicing strategy for the study area was considered within the 2006 CDP. In accordance with the 2006 CDP, the study area will be serviced with potable water by a trunk watermain network connecting to the reservoir and pumping station on Fallowfield Road.

More recently, the study area's water supply servicing was considered as a part of the *Kennedy Burnett Potable Water Master Servicing Study* (Stantec, April 2014). The Stantec April 2014 report identifies 300mm trunk watermains within the future alignment of Jockvale Road and the collector road at the southern boundary of the study area. Despite minor changes to the watermain network layout, the general water supply servicing strategy in the Stantec April 2014 report remained consistent with the strategy laid out in the *2006 CDP*. The proposed plan of subdivision presents no apparent constraints to the *2006 CDP* and the Stantec April 2014 water supply servicing strategy for the area.

The proposed development will be serviced by a network of pressurized local watermains connecting to trunk infrastructure detailed in the Stantec April 2014 report. See *Figure 1* and *Appendix C* for details. *Table 3* summarizes the design criteria that will be employed in the detailed design of the watermain network.

**Table 3: Water Supply Design Criteria** 

Value
3.4 P/unit
2.7 P/unit
2.1 P/unit
1.8 P/unit
280 L/d/P
2.5 x Average Daily *
5.5 x Average Daily *
150mm diameter
2.4m from top of watermain
350kPa and 480kPa
275kPa
552kPa
140kPa

<sup>\*\*</sup> Residential Max. Daily and Max. Hourly peaking factors per MOE Guidelines for Drinking-Water Systems Table 3-3 for 0 to 500 persons. City Guidelines used for populations greater than 500 persons.

The water demands for the 2006 CDP land use plan and the proposed plan of subdivision were calculated using consumption rates from **Table 3** and the City of Ottawa's **Water Supply Guidelines**. Results can be found in **Table 4** below, with calculations provided in **Appendix C**. The water demand associated with the proposed plan of subdivision is roughly 25% of the demand anticipated in the 2006 CDP land use plan.

**Table 4: Summary of Water Demands** 

	Avg. Daily Water Demand (L/s)
SNTC CDP JULY 2006	14.42
3194 JOCKVALE RD. FSR DEC 2018	3.56

Through the detailed design of the study area, a complete hydraulic analysis will be prepared for the water distribution network to confirm that water supply is available within the required pressure range under the anticipated demands during average day, peak hour and fire flow conditions. Per the Stantec April 2014 report, fire flows upwards of 15,000 L/min @ 20 psi are available to the subject lands. As the design process advances, these fire flows will be further analyzed and respected through the use of fire walls, sprinklers and/or other means to ensure the fire flow requirement does not exceed the rate of supply. In circumstances where infrastructure may be required outside of the study area, land owner agreements will be put in place to facilitate cost sharing and access when necessary.

#### 3.3 Water Supply Conclusion

Potable water will be delivered to the proposed study area via pressurized 300mm diameter watermains. In accordance with the 2006 CDP and the Kennedy Burnett Potable Water Master Servicing Study (Stantec, April 2014) the study area's watermain network will connect to the existing external trunk watermain system detailed in the Stantec April 2014 report.

The proposed plan of subdivision represents a decrease in water demand when compared to the *2006 CDP* land uses. A complete hydraulic analysis will be prepared at the time of detailed design. The watermain network will be sized to meet maximum hour and maximum day plus fire flow demands and conform to all relevant City of Ottawa and MOECP Guidelines and Policies.

#### 4.0 WASTEWATER SERVICING

#### 4.1 Existing Wastewater Services

The study area is tributary to the South Nepean Collector (SNC) sewer, which exists south of the study area and conveys wastewater to the east, and under the Jock River.

#### 4.2 Wastewater Design

The wastewater servicing strategy for the study area was considered within the 2006 CDP. In accordance with the 2006 CDP, the study area's sanitary sewer system will ultimately discharge to the existing SNC sanitary sewer, within the future extension of Chapman Mills Drive, south of the study area. See **Figure 1** for details.

The South Nepean Collector: Phase 2, Hydraulics Review, Technical Memorandum (Novatech, Aug 2015) more recently considered the wastewater servicing for the study area, reporting that wastewater flows will enter the SNC sewer between nodes 90-80.

The proposed development will be serviced by a network of gravity sewers to be designed in accordance with the wastewater design parameters from *ISTB-2018-01* and the *Sewer Design Guidelines*, summarized in *Table 5*. Where infrastructure may be required outside of the study area, there will be agreements in place facilitating cost sharing and access when necessary.

**Table 5: Wastewater Design Criteria** 

Design Parameter	Value		
Residential - Single Family	3.4p/unit		
Residential – Townhome/ Semi	2.7p/unit		
Residential Townhouse/Back-to-Back	2.1 P/unit		
Residential Apartment (High Density)	1.8 P/unit		
Average Daily Demand	280 L/d/per		
Peaking Factor	Harmon's Peaking Factor, where K=0.8		
Commercial / Institutional Flows	28,000 L/gross ha/day		
Commercial / Institutional Peak Factor	1.5 if contribution >20%, otherwise 1.0		
Light Industrial Flows	35,000 L/gross ha/day		
Industrial Peaking Factor	Per Figure in Appendix 4-B, City of Ottawa		
	Guidelines		
Infiltration and Inflow Allowance	0.33 L/s/gross ha for all areas		
Park Peaking Factor	1.0		
Sanitary sewers are to be sized employing the	$Q = \frac{1}{1} A R^{\frac{2}{3}} S^{\frac{1}{2}}$		
Manning's Equation	$Q = -AK^{7/3}S^{7/2}$		
Minimum Sewer Size	200mm diameter		
Minimum Manning's 'n'	0.013		
Minimum Depth of Cover	2.5m from crown of sewer to grade		
Minimum Full Flowing Velocity	0.6m/s		
Maximum Full Flowing Velocity	3.0m/s		
Extracted from Sections 4 and 6 of the City of Ottawa Sewer Design Guidelines, October 2012,			
Technical Bulletins, and recent residential subdivision in City of Ottawa.			

**Table 6** shows anticipated wastewater flows for the study area for both the proposed plan of subdivision and the 2006 CDP land use plan using the design criteria detailed in **Table 5**. Reported wastewater flows from the study area within the **South Nepean Collector:** Phase 2, Hydraulics Review, Technical Memorandum (Novatech, Aug 2015) are also included in **Table 6**. Refer to **Appendix D** for excerpts and detailed calculations.

**Table 6: Comparison of Wastewater Flows** 

		Flow (L/s)			
	Total Area (Ha)	Res.	ICI	Infiltration	Total
SNTC CDP JULY 2006	10.61	33.7	4.3	3.5	41.5
SNC: PH2 HYDRAULICS REVIEW AUG 2015	11.01	14.1	0.0	3.1	17.2
3194 JOCKVALE RD. FSR DEC 2018	10.61	5.5	2.9	3.5	11.9

The anticipated wastewater flows from the study area are lower than those anticipated in both the 2006 CDP and the South Nepean Collector: Phase 2, Hydraulics Review, Technical Memorandum (Novatech, Aug 2015). The anticipated peak design flow is 29% and 69% of the 2006 CDP and Novatech Aug 2015 reported flows respectively. It is noted that the Novatech Aug 2015 report uses wastewater design criteria that represents a flow increase compared to the design criteria detailed in **Table 5**.

#### 4.3 Wastewater Servicing Conclusions

A network of local gravity sewers is proposed within the study area to convey flow to the existing SNC sanitary sewer, in accordance with the *2006 CDP* and the *South Nepean Collector: Phase 2, Hydraulics Review, Technical Memorandum* (Novatech, Aug 2015). The sewers are to be designed in conformance with all relevant City of Ottawa and MOECP Guidelines and Policies.

The proposed plan of subdivision represents a decrease in estimated wastewater flow rates when compared to the *2006 CDP* land uses and what was considered in the Novatech Aug 2015 report. As such, the SNC sanitary sewer can accommodate the proposed plan of subdivision.

#### 5.0 STORMWATER MANAGEMENT

#### 5.1 Existing Stormwater Drainage

The study area is located to the east of the existing Kennedy-Burnett Stormwater Management Facility (KB SWMF). A north-south municipal drain is located in the central portion of the study area. Under existing conditions the western portion of the study area drains to the KB SWMF while the remaining portion of the study area drains to the Jock River via the municipal drain and roadside ditches.

#### 5.2 Stormwater Management Strategy

The stormwater management strategy for the study area was considered within the 2006 CDP. In accordance with the 2006 CDP, the study area's storm sewer system will ultimately discharge to the existing KB SWMF, west of the study area. See **Figure 1** for details.

The Kennedy-Burnett Stormwater Management Facility and Functional Design Report (CH2M, Feb 2017) more recently considered the stormwater management strategy for the study area. The preferred servicing option in the CH2M Feb 2017 report plans for minor system flows (5-year capture) to be conveyed via trunk storm sewers and passed through a Hydro Dynamic Separator unit for quality control, prior to outletting to the KB SWMF. Major flows are to be routed overland to the KB SWMF. Excerpts from the Kennedy-Burnett Stormwater Management Facility and Functional Design Report (CH2M, Feb 2017) can be found in **Appendix E**. The study area is shown to be slightly larger, area reported as 10.9 ha as opposed to 10.6 ha, and was assigned a runoff coefficient of 0.8 based on the land uses in the 2006 CDP.

Runoff coefficients taken from the *Kennedy-Burnett Stormwater Management Facility and Functional Design Report* (CH2M, Feb 2017) have been assigned to the proposed plan of subdivision. Results can be found in *Table 7* below.

Table 7: Anticipated Runoff Calculations

C Area

Land Use	C (Runoff Coef)	Area (ha)	A*C
Low/Med Density Res.	0.65	3.86	2.509
Commercial	0.85	5.93	5.0405
Roads	0.80	0.82	0.656
	Total	10.61	8.2055
	Avg C	0.7	77
	CH2M Feb 2017 Avg C	0.80	

The reduced runoff coefficient for the study area indicates that a decrease in stormwater runoff is anticipated for the plan of subdivision from what was considered in the CH2M

Feb 2017 report. As the design of the study area advances, it is to account for the rates of minor system capture, major system conveyance and onsite stormwater detention storage required to accommodate the limitations of the KB SWMF.

The proposed development will be serviced by a network of gravity sewers. *Table 8* summarizes the design criteria that will be employed in the detailed design of the trunk and local storm sewers. Where infrastructure may be required outside of the study area, there will be agreements in place facilitating cost sharing and access when necessary.

**Table 8: Storm Sewer Design Criteria** 

Design Parameter	Value
Minor System Design Return Period	2-Year (Local Streets), 5-Year (Collector Streets), 10-Year
	(Arterial Streets) – PIEDTB-2016-01
Major System Design Return Period	100-Year
Intensity Duration Frequency Curve	. A
(IDF)	$i = \frac{A}{(t_0 + B)^C}$
2-year storm event:	$(l_c + D)$
A = 723.951, B = 6.199, C = 0.810	
5-year storm event: A = 998.071, B = 6.053, C = 0.814	
Minimum Time of Concentration	10 minutes
Rational Method	Q = CiA
	0.90
Runoff coefficient for paved and roof areas	0.90
Runoff coefficient for landscaped areas	0.20
Storm sewers are to be sized	$Q = \frac{1}{4} A R^{\frac{2}{3}} S^{\frac{1}{2}}$
employing the Manning's Equation	$Q = -AR^{7/3}S^{7/2}$
Minimum Sewer Size	250 mm diameter
Minimum Manning's 'n'	0.013
Service Lateral Size	100mm dia PVC SDR 28 with a minimum slope of 1.0%.
Minimum Depth of Cover	1.5m from crown of sewer to grade (based on recent
	residential subdivisions in City of Ottawa)
Minimum Full Flowing Velocity	0.8 m/s
Maximum Full Flowing Velocity	6.0 m/s
Clearance from 100-Year Hydraulic	0.30 m
Grade Line to Building Opening	05 are all are suffer (DIEDED 0040 04)
Max. Allowable Flow Depth on	35 cm above gutter (PIEDTB-2016-01)
Municipal Roads Extent of Major System	To be contained within the municipal right-of-way or adjacent
Extent of Major System	to the right-of-way provided that the water level must not
	touch any part of the building envelope and must remain
	below the lowest building opening during the stress test event
	(100-year + 20%) and 15cm vertical clearance is maintained
	between spill elevation on the street and the ground elevation
	at the nearest building envelope (PIEDTB-2016-01)
Stormwater Management Model	DDSWMM (release 2.1), SWMHYMO (v. 5.02) and XPSWMM (v. 10)
Model Parameters	Fo = 76.2 mm/hr, Fc = 13.2 mm/hr, DCAY = 4.14/hr,
	D.Stor.Imp. = 1.57 mm, D.Stor.Per. = 4.67 mm
Imperviousness	Based on runoff coefficient (C) where
	Percent Imperviousness = (C - 0.2) / 0.7 x 100%.

Design Storms	Chicago 3-hour Design Storms and 24-hour SCS Type II				
	Design Storms. Maximum intensity averaged over 10				
	minutes.				
Historical Events July 1st, 1979, August 4th, 1988 and August 8th, 19					
Climate Change Street Test 20% increase in the 100-year, 3-hour Chicago storm					
Extracted from City of Ottawa Sewer Design Guidelines, October 2012, as amended by PIEDTB-2016-01, and based on					
recently approved residential subdivision designs in City of Ottawa.					

Consistent with the 2006 CDP and the CH2M Feb 2017 report, the major system drainage strategy proposes to direct overland flow towards the existing KB SWMF. See *Figure 2* for details. As shown in the proposed grading plan, it is anticipated that certain areas, particularly the western portion of the site, may exceed the permissible grade raises detailed in the *Geotechnical Investigation - Proposed Commercial Development - Greenbank Road* (Paterson Group, February 2012). Note that the proposed grading plan is subject to change as the design of the subject area advances. The grading plan has been produced to best respect the grade restrictions in the study area and to provide appropriate cover (minimum 1.5m depth) for the storm sewers. Due to these grading constraints, below grade structures requiring gravity drainage (basements) may not be permissible for any buildings in the study area.

#### 5.3 Stormwater Servicing Conclusions

A network of local gravity storm sewers is proposed within the study area to convey stormwater runoff to the existing KB SWMF, in accordance with the 2006 CDP and the Kennedy-Burnett Stormwater Management Facility and Functional Design Report (CH2M, Feb 2017). The sewers are to be designed in conformance with all relevant City of Ottawa and MOECP Guidelines and Policies.

The proposed plan of subdivision represents a decrease to estimated stormwater runoff when compared to the CH2M Feb 2017 report. As such, the KB SWMF can accommodate the proposed plan of subdivision.

#### 6.0 EROSION AND SEDIMENT CONTROL

Soil erosion occurs naturally and is a function of soil type, climate and topography. The extent of erosion losses is exaggerated during construction where vegetation has been removed and the top layer of soil becomes agitated.

Prior to topsoil stripping, earthworks or underground construction, erosion and sediment controls will be implemented and will be maintained throughout construction.

Silt fence will be installed around the perimeter of the active part of the site and will be cleaned and maintained throughout construction. Silt fence will remain in place until the working areas have been stabilized and re-vegetated.

Catchbasins will have catchbasin inserts installed during construction to protect from silt entering the storm sewer system.

Specifically, the following recommendations to the Contractor will be included in contract documents.

- Limit extent of exposed soils at any given time.
- Re-vegetate exposed areas as soon as possible.
- Minimize the area to be cleared and grubbed.
- Protect exposed slopes with plastic or synthetic mulches.
- Install silt fence to prevent sediment from exiting the construction area and entering existing ditches/stormwater systems.
- > Install mud mat at the construction access in order to prevent mud tracking onto adjacent roads.
- No refueling or cleaning of equipment near existing watercourses.
- Provide sediment traps and basins during dewatering.
- Install catchbasin inserts.
- Plan construction at proper time to avoid flooding.

The Contractor will, at every rainfall, complete inspections and guarantee proper performance. The inspection is to include:

- Verification that water is not flowing under silt barriers.
- Clean and change inserts at catch basins.

#### 7.0 CONCLUSIONS AND RECOMMENDATIONS

This Functional Servicing Study (FSR) (DSEL, December 2018) provides details on the planned on-site and off-site municipal services for the subject property. Results of this FSR indicate that the proposed plan of subdivision results in reduced or equivalent water supply, wastewater servicing and stormwater management servicing requirements when compared to the 2006 CDP. Existing and proposed infrastructure planned to support the 2006 CDP lands is considered adequate to service the proposed plan of subdivision.

Prior to detailed design of the infrastructure presented in this report, this FSR will require approval under the *Planning Act* as supporting information for the development applications. Project-specific approvals are also expected to be required for the infrastructure presented in this report from the City of Ottawa, Ministry of Environment, Conservation and Parks, and the Rideau Valley Conservation Authority.

Prepared by, **David Schaeffer Engineering Ltd.** 

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Reviewed by, **David Schaeffer Engineering Ltd.** 



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# **Appendix A**

Development Study Checklist, Record of Pre-Consultation, Plan of Subdivision, Record of City Pre-Consultation

#### **DEVELOPMENT SERVICING STUDY CHECKLIST**

4.1	General Content	
	Executive Summary (for larger reports only).	N/A
	Date and revision number of the report.	Title Page
	Location map and plan showing municipal address, boundary, and layout of proposed development.	Figure 1
	Plan showing the site and location of all existing services.	Figures 1
	Development statistics, land use, density, adherence to zoning and official plan, and reference to applicable subwatershed and watershed plans that provide context to applicable subwatershed and watershed plans that provide context to which individual developments must adhere.	Section 1.0 & Section 2.0
	Summary of Pre-consultation Meetings with City and other approval agencies.	Section 1.3 & Appendix A
	Reference and confirm conformance to higher level studies and reports (Master Servicing Studies, Environmental Assessments, Community Design Plans), or in the case where it is not in conformance, the proponent must provide justification and develop a defendable design criteria.	All sections
	Statement of objectives and servicing criteria.	Section 1.0 & Section 3.2, Section 4.2, and Section 5.2
	Identification of existing and proposed infrastructure available in the immediate area.	Sections 3.1, Section 4.1, and Section 5.1
	Identification of Environmentally Significant Areas, watercourses and Municipal Drains potentially impacted by the proposed development (Reference can be made to the Natural Heritage Studies, if available).	Sections 1.1 & 1.2
	Concept level master grading plan to confirm existing and proposed grades in the development. This is required to confirm the feasibility of proposed stormwater management and drainage, soil removal and fill constraints, and potential impacts to neighbouring properties. This is also required to confirm that the proposed grading will not impede existing major system flow paths.	Figure 2
	Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts.	To be addressed in at detailed design.
	Proposed phasing of the development, if applicable.	N/A. Depends on landowner preferred timing
	Reference to geotechnical studies and recommendations concerning servicing.	Section 1.1
	All preliminary and formal site plan submissions should have the following information:  -Metric scale -North arrow (including construction North) -Key plan -Name and contact information of applicant and property owner -Property limits including bearings and dimensions -Existing and proposed structures and parking areas -Easements, road widening and rights-of-way -Adjacent street names	Figures
	4.2 Development Servicing Report: Water	
	Confirm consistency with Master Servicing Study, if available	Section 3.2
	Availability of public infrastructure to service proposed development	Section 3.2
	Identification of system constraints	Section 3.2
	Identify boundary conditions	Detailed hydraulic assessment N/A for FSR

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Kennedy Burnett Potable Water Master Servicing Study, Stantec Consulting Ltd, April 29, 2014. Detailed hydraulic assessment N/A for FSR.	Confirmation of adequate domestic supply and pressure	
ould show available Detailed hydraulic assessment N/A for FSR.	Confirmation of adequate fire flow protection and conf calculated as per the Fire Underwriter's Survey. Output fire flow at locations throughout the development.	
- I I I I I I I I I I I I I I I I I I I	Provide a check of high pressures. If pressure is found to is required to confirm the application of pressure reduced to the confirm the application of the confirmation of the c	
HIGH DAILE THE PROPERTY OF THE	Definition of phasing constraints. Hydraulic modeling is servicing for all defined phases of the project including	
on of shut-off valves  Detailed hydraulic assessment N/A for FSR.	Address reliability requirements such as appropriate loc	
cation Stantec April 2014.	Check on the necessity of a pressure zone boundary mo	
s includes data that hour and fire flow  Stantec April 2014.  Detailed hydraulic assessment	Reference to water supply analysis to show that major of delivering sufficient water for the proposed land use shows that the expected demands under average day, productions provide water within the required pressure of the same of th	
r necessary looping, Stantec April 2014. Section 3.2	Description of the proposed water distribution network proposed connections to the existing system, provisions and appurtenances (valves, pressure reducing valves, valydrants) including special metering provisions.	
to service proposed Stantes April 2014	Description of off-site required feedermains, booster poother water infrastructure that will be ultimately required development, including financing, interim facilities, and implementation.	
the City of Ottawa Section 3.2 & Appendix C	Confirmation that water demands are calculated based Design Guidelines.	
ditions locations, Detailed hydraulic assessment N/A for FSR.	Provision of a model schematic showing the boundary of streets, parcels, and building locations for reference.	
Renort: Wastewater	4 3 Develonment Servic	
es. Monitored flow	not deviate from the City of Ottawa Sewer Design Guide data from relatively new infrastructure cannot be used requirements for proposed infrastructure).	
stifications for Section 4.2	Confirm consistency with Master Servicing Study and/o deviations.	
traneous flows that South Nepean Collector: Phase	Consideration of local conditions that may contribute to	
This includes 2, Hydraulics Review, Technical	are higher than the recommended flows in the guidelin groundwater and soil conditions, and age and condition	
4.2	Description of existing sanitary sewer available for discription proposed development.	
NOVATECH AUG 71115 & SECTION	Verify available capacity in downstream sanitary sewer upgrades necessary to service the proposed developme	
Report: Wastewater  Ilow criteria should es. Monitored flow ustify capacity  Section 4.2  traneous flows that This includes sewers.  Memorandum, No August 20, 20: 4.2  Vor identification of  Novatech Aug 2015 8	4.3 Development Servic  Summary of proposed design criteria (Note: Wet-weath not deviate from the City of Ottawa Sewer Design Guide data from relatively new infrastructure cannot be used requirements for proposed infrastructure).  Confirm consistency with Master Servicing Study and/o deviations.  Consideration of local conditions that may contribute to are higher than the recommended flows in the guidelin groundwater and soil conditions, and age and condition.  Description of existing sanitary sewer available for disch from proposed development.  Verify available capacity in downstream sanitary sewer	

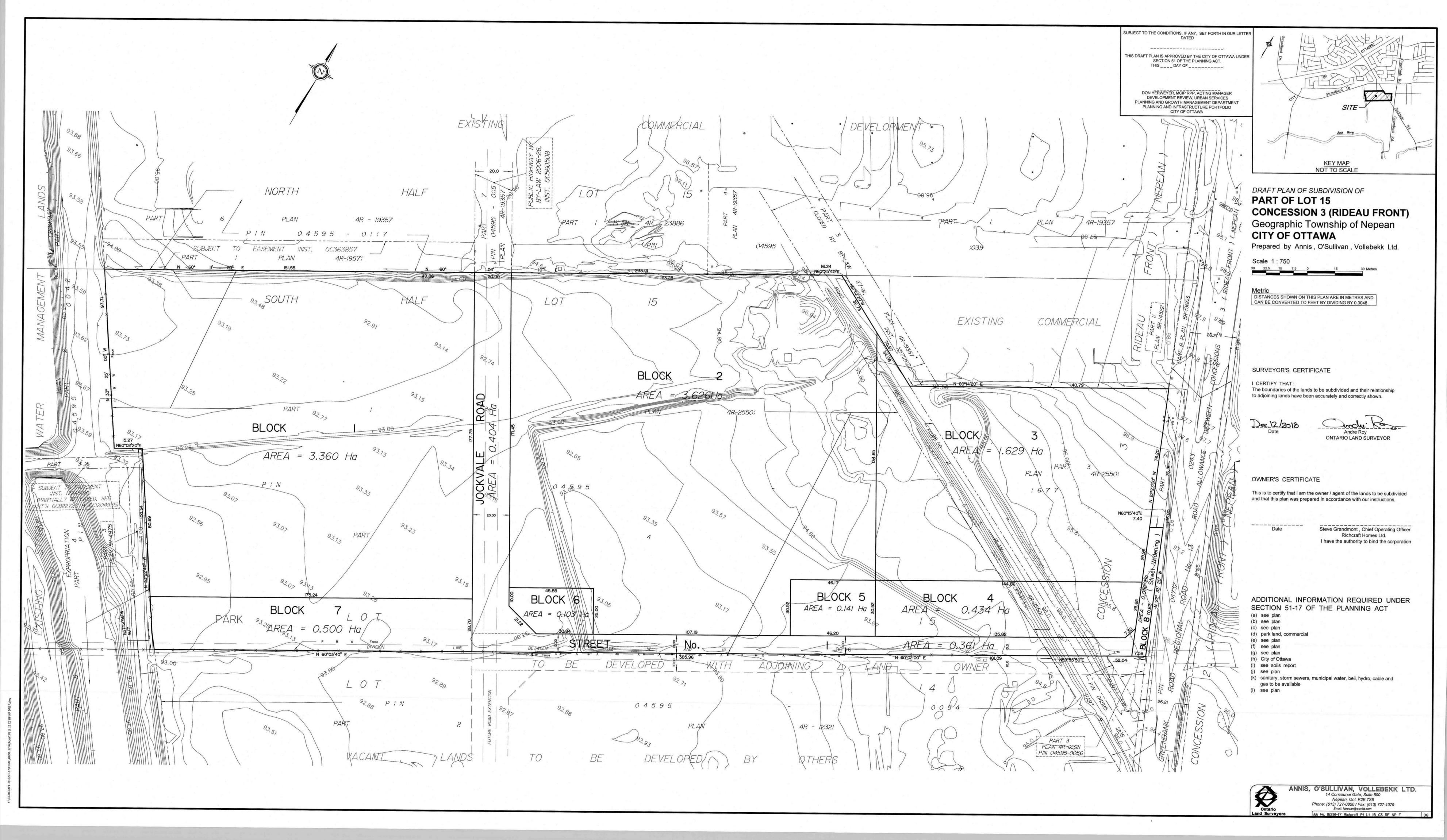
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	Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format.	Novatech Aug 2015, Section 4.2 & Appendix D
	Description of proposed sewer network including sewers, pumping stations, and forcemains.	Section 4.2 & Figure 1
	Discussion of previously identified environmental constraints and impact on servicing (environmental constraints are related to limitations imposed on the development in order to preserve the physical condition of watercourses, vegetation, soil cover, as well as protecting against water quantity and quality).	Novatech Aug 2015
	Pumping stations: impacts of proposed development on existing pumping stations or requirements for new pumping station to service development.	Novatech Aug 2015
	Forcemain capacity in terms of operational redundancy, surge pressure and maximum flow velocity.	Novatech Aug 2015
	Identification and implementation of the emergency overflow from sanitary pumping stations in relation to the hydraulic grade line to protect against basement flooding.	Novatech Aug 2015
	Special considerations such as contamination, corrosive environment etc.	N/A
	A A Double a mount Compieire Borne the Character Ch	a aldiat
	4.4 Development Servicing Report: Stormwater Ch	ecklist
	Description of drainage outlets and downstream constraints including legality of outlets (i.e. municipal drain, right-of-way, watercourse, or private property)	Section 1.1 ,5.1 & 5.2
	Analysis of available capacity in existing public infrastructure.	Kennedy-Burnett Stormwater Management Facility Functional Design Report, CH2M, February 17, 2017 & Section 5.2
	A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns, and proposed drainage pattern.	CH2M Feb 2017
	Water quantity control objective (e.g. controlling post-development peak flows to pre-development level for storm events ranging from the 2 or 5 year event (dependent on the receiving sewer design) to 100 year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects.	CH2M Feb 2017 & Section 5.2
	Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements.	CH2M Feb 2017 & Section 5.2
	Description of the stormwater management concept with facility locations and descriptions with references and supporting information	CH2M Feb 2017, Section 5.2 & Figure 1
	Set-back from private sewage disposal systems.	N/A
	Watercourse and hazard lands setbacks.	N/A
_	Record of pre-consultation with the Ontario Ministry of Environment and the	Record of consultation
	Conservation Authority that has jurisdiction on the affected watershed.	forthcoming.
	Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists.	CH2M Feb 2017 & Section 5.2
	Storage requirements (complete with calculations) and conveyance capacity for minor events (1:5 year return period) and major events (1:100 year return period).	Detailed modelling N/A for FSR.

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catchments in comparison to existing conditions.  Any proposed diversion of drainage catchment areas from one outlet to another.  Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and stormwater management facilities.  If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post-development flows up to and including the 100-year return period storm event.  Identification of potential impacts to receiving watercourses  Identification of municipal drains and related approval requirements.  Descriptions of how the conveyance and storage capacity will be achieved for the development.  100 year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading.	N/A  Section 5.2 & Figure 1  N/A  CH2M Feb 2017  Section 1.1  N/A at FSR level, future work described in Section 5.3  N/A at FSR level future work described in Section 5.2  Section 6.0  CH2M Feb 2017
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investigation.  4.5 Approval and Permit Requirements: Checklist	
	Section 1.1
floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement  Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement ct. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act.	Section 1.2
Application for Certificate of Approval (CofA) under the Ontario Water Resources Act.	Section 1.2
☐ Changes to Municipal Drains.	Section 1.1
Other permits (National Capital Commission, Parks Canada, Public Works and Government Services Canada, Ministry of Transportation etc.)	Section 1.2
4.6 Conclusion Checklist	
☐ Clearly stated conclusions and recommendations	Section 7.0
Comments received from review agencies including the City of Ottawa and	0000.000
information on how the comments were addressed. Final sign-off from the responsible reviewing agency.	N/A – first submission

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#### **Braden Kaminski**

**Subject:** FW: Richcraft subdivision / South Nepean Town Centre

Attachments: 18291-17 Richcraft Pt Lt 15 C3 RF NP CONCEPT SK D6.pdf; Document4

\_Recommended\_Pond.pdf; Harmony Subdivision.pdf; Jockvale\_Blakely\_Flats CONCEPT

SITE PLAN(s)\_216 and 240 Units\_11Dec2017.pdf

From: Moore, Sean < Sean. Moore@ottawa.ca>

**Sent:** October 19, 2018 11:20 AM

To: Jennifer Murray < jenniferkmurray@outlook.com >; Miguel Tremblay < tremblay@fotenn.com >

**Cc:** Krabicka, Jeannette < <u>Jeannette.Krabicka@ottawa.ca</u>>; Shillington, Jeffrey < <u>jeff.shillington@ottawa.ca</u>>; Baggs, Rosanna < <u>Rosanna.Baggs@ottawa.ca</u>>; Moise, Christopher < <u>christopher.moise@ottawa.ca</u>>; Stevens, Lorraine < <u>Lorraine.Stevens@ottawa.ca</u>>; Reed, Kerry < <u>kerry.reed@ottawa.ca</u>>

Subject: RE: Richcraft subdivision / South Nepean Town Centre

Hi Jennifer,

Regarding our preconsultation meeting on Thursday October 11<sup>th</sup> for a plan of subdivision and rezoning please find the submission requirements and preliminary comments below.

#### List of required Plans/Reports with your applications:

#### **Required Plans/Studies:**

- Draft Plan of Subdivision (15 copies)
- Survey Plan (2 copies)
- Planning Rationale, with Integrated Environmental Review (3 copies) please include a Parks rationale for the park location, size, configuration and how it meets the parks policies / guidelines of the City of Ottawa
- Stormwater Management Report / Brief (3 copies)
- Serviceability Study (3 copies)
- Transportation Impact Assessment (3 copies)
- Noise Feasibility Study (3 copies)
- Geotechnical Study (3 copies)
- Phase 1 ESA (2 copies) to conformity with OReg 153/04
- Tree Conservation Report (3 copies)
- Archaeological Resource Assessment (3 copies)
- Roadway Modification Plan (3 copies) for functional design of any road mods / intersections / medians etc
- Concept Plan ultimate use of lands (3 copies)
- No EIS required

#### Link to Plan of Subdivision application form:

https://ottawa.ca/en/city-hall/planning-and-development/information-developers/development-application-review-process/development-application-submission/development-application-forms#plan-subdivision

<sup>\*</sup>All required plans & reports are to be provided in digital format (\*.pdf) at application submission in addition to any required hard copies.

#### Link to Plan of Zoning By-law amendment application form:

https://ottawa.ca/en/city-hall/planning-and-development/information-developers/development-application-review-process/development-application-submission/development-application-forms#zoning-law-amendment

Link to SNTC CDP – see appendix for Street Cross Sections that are discussed below: <a href="https://ottawa.ca/en/city-hall/planning-and-development/community-plans-and-design-guidelines/community-plans-and-studies/community-design-plans/south-nepean-town-centre-community-design-plan</a>

#### **Preliminary Staff Comments:**

- Any block configuration that contemplates commercial is premature until the concurrent OPA process (D01-01-18-0006) has determined commercial uses are permitted within this area of the Town Centre. Submitting a Plan of Subdivision and Zoning By-law application in advance of the OPA process is at the discretion of the applicant and can be circulated and reviewed but cannot proceed to draft approval until the OPA has come to a final conclusion (such as Council approval through its appeal period).
- Any park design will need to be determined through the concurrent OPA process. Parkland size and location cannot be finalized in advance of the larger picture OPA currently under review
- Street No. 1 cross section and Jockvale Road will have to be determined through the OPA process currently underway. The CDP cross sections call for 12m asphalt curb to curb (see CDP appendix), but these are outdated and new direction on street cross sections will need to come out of that OPA process. This will need to address cycling, pedestrian, on-street parking, landscaping and utility/infrastructure considerations.
- Minimum 2 public street frontages on the new city park are in line with City direction for park design. Frontage of city parks via a cul-de-sac will not be supported by Staff.
- If the city park is determined to remain adjacent to Block 1, Street No. 1 should provide a vista across the stormwater pond, thus extending and providing street frontage along the park edge (see conceptually image attached). This would also provide direct connectivity from a public road to the pathway that crosses the storm pond.
- A public street should enter the residential area (Block 1) to break up this block, provide public access to the pathways along the pond, and to provide a single loaded element along the pond.
- If commercial is permitted on Blocks 1-6, zoning and policy will need to be drafted to ensure Blocks 4, 5 and 6 can achieve active building frontages along Street No.1 – this is to be coordinated with the active OPA application
- If commercial is permitted within the OPA at this location, Staff would look to an example such as Grant Crossing on Hazeldean Road to either allow public access, or access which 'appears' public in nature to divide Blocks 2 and 3 (as conceptually illustrated in the attachment). This would line up with the future road extension shown on the applicant's concept plan (attached).
- Development should tie into the retrofitted Kennedy-Burnett storm pond where there are proposed pathways along the pond (see attached functional design plan entitled 'Document 4 Recommended Pond). The detail design of the pond retrofit is currently with Novatech, led by the City's ISD (Patrick Chamney). I understand landowners will be notified shortly of this detail design plan. I have also attached the grading plan for Harmony Subdivision, across the pond to the west, where you can see how the pathway will cross the pond making a good opportunity to link the pathway where it crosses the pond to a public road on Richcrafts land.

#### Sean Moore MCIP, RPP

Planner III | Urbaniste III

Development Review (South Services) | Examen des projets d'aménagement (services sud) Planning, Infrastructure and Economic Development | Services de planification, d'infrastructure et de développement économique

City of Ottawa | Ville d'Ottawa

613.580.2424 ext./poste 16481

ottawa.ca/planning / ottawa.ca/urbanisme

# **Appendix B**

Excerpts from the South Nepean Town Centre Community Design Plan (City of Ottawa, July 2006)



# South Nepean Town Centre Community Design Plan



Planning and Growth Management Department Community Planning and Design Division July 2006 Publication #03-14

### Land Use

**Table 1 – Land Use Distribution** 

Policy Area	Net Area (hectares)	% of Total Area
High Rise Mixed-Use	26.5	16.1%
Mid Rise Mixed-Use	34.2	20.7%
High Rise Residential	3.4	2.1%
Mid Rise Residential	21.9	13.2%
School	7.9	4.8%
Civic Complex	2.2	1.3%
District Park	21.6	13.1%
Neighbourhood Park	4.5	2.7%
Streets	42.8	25.9%
Total	165.0	100.0%

**Table 2 – Dwelling Type Distribution** 

<b>Dwelling Type</b>	# of Dwellings	% of Total Dwellings	
Phase 2			
Street Townhouses	1,000	14%	
Stacked Townhouses	750	10%	
Apartments	5,500	76%	
Total	7,250	100%	
Phase 3			
Street Townhouses	1,000	9%	
Stacked Townhouses	750	7%	
Apartments	9,300	84%	
Total	11,050	100%	

**Table 3 – Land Use Statistics** 

Phase	Retail Gross Floor Area (m²)	Office Gross Floor Area (m²)	# of Dwelling Units	Population	Employment
Phase 1 – Initial	78,000	1,000	0	0	1,000
Phase 2 – Interim Built Out	208,250	158,250	7,250	14,500	7,300
Phase 3 – Ultimate Build Out	217,000	350,500	11,000	22,500	12,600

#### Notes:

<sup>(1)</sup> Tables 2 and 3 indicate projections of different build out scenarios. Given the long-term nature of the scenarios, these figures should only be considered as potential build out projections based on permissions by the policies in this CDP.

<sup>(2)</sup> Numbers for each phase are total, not cumulative.

<sup>(3)</sup> Phase 1 does not include the limited residential units currently within the Town Centre.

<sup>(4)</sup> The type of units identified in Table 2 are intended to only illustrate the intensity of units, and not necessarily limit the form of units.

#### 4.2 Policy Area – High Rise Mixed-Use

The High Rise Mixed-Use policy area represents the primary retail and mixed-use development area within the Town Centre. The High Rise Mixed-Use policy area will be a lively and active mixed-use shopping district, with an emphasis on commercial and residential uses in the same building with retail uses located at-grade, but also single use retail and office commercial uses and residential apartments.

#### **Policies**

For the High Rise Mixed-Use policy area:

- (1) Apartments, a broad variety of retail, office and service commercial activities, public and institutional uses, schools, places of worship, and community facilities are permitted.
- (2) The minimum building height is 6 storeys and the maximum building height is 12 storeys.
- (3) The net density target for residential uses is 250 units per hectare.
- (4) The maximum lot coverage for stand-alone residential buildings is 30% of the total area of any block.
- (5) All building frontage along Greenbank Road and Chapman Mills Drive must have non-residential uses at grade.
- (6) The City will encourage that all buildings along the BRT route north of Chapman Mills Drive incorporate the route as much as possible into the design of the building, through such means as clear windows or secondary doors.
- (7) The above policies in Section 4.2 or the policies and guidelines of Section 5.0 do not apply to future development in the "Strandherd Retail District" that is permitted by existing zoning or master site plans, provided that this development does not jeopardize the long-term acquisition of the public streets identified on Schedule 2 or public parkland identified on Schedule 5. For this new development, the City will still encourage the consideration of the

urban design policies and guidelines in Section 5.0, as they may apply, during the development review process.

#### 4.3 Policy Area – Mid Rise Mixed-Use

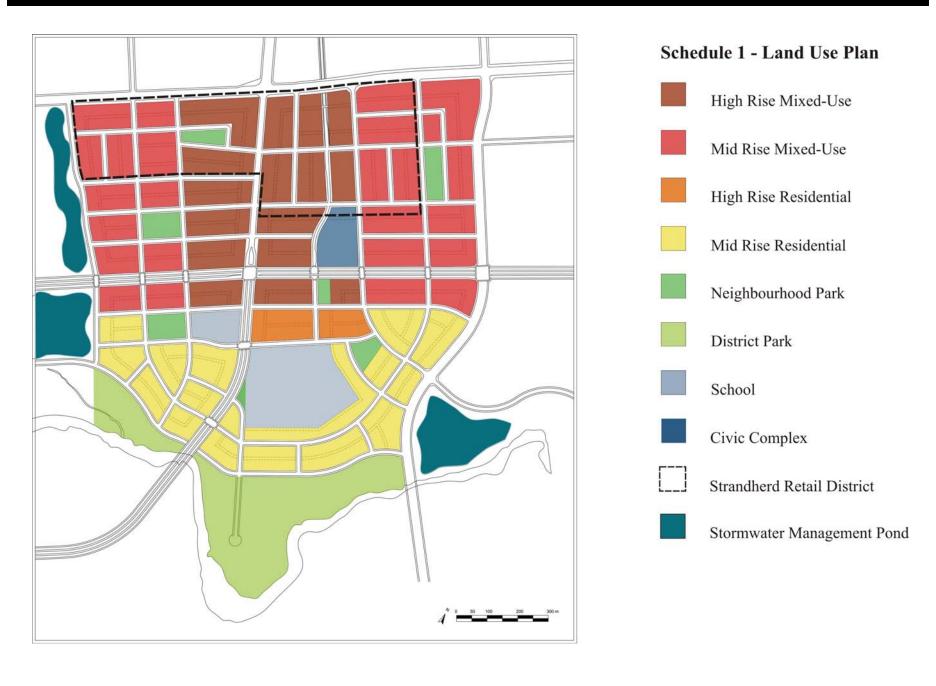
The Mid Rise Mixed-Use policy area represents a lower scale, mixed-use area within the Town Centre with the intent of establishing opportunities for live-work units and medium density housing forms. The Mid Rise Mixed-Use policy area is intended to be a transition between the High Rise Mixed-Use policy area and the adjacent lower density residential neighbourhoods, both within the Town Centre an in surrounding communities.

#### **Policies**

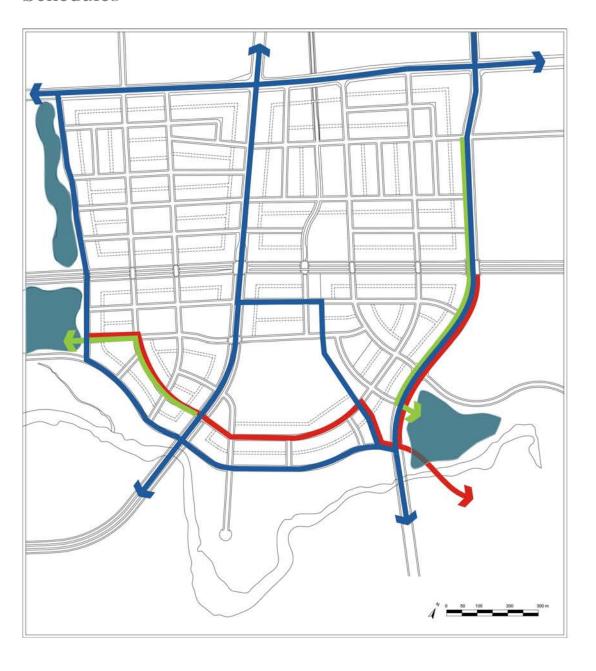
For the Mid Rise Mixed-Use policy area:

- (1) Apartments, live-work units, retail, office and service commercial uses, public and institutional uses, schools, places of worship and community facilities are permitted.
- (2) The minimum building height is 4 storeys and the maximum building height is 6 storeys.
- (3) The net density target for residential uses is 200 units per hectare.
- (4) The maximum lot coverage for stand-alone residential buildings is 50% of the total area of any block.
- (5) The above policies in Section 4.3 or the policies and guidelines of Section 5.0 do not apply to future development in the "Strandherd Retail District" that is permitted by existing zoning or master site plans, provided that such development does not jeopardize the long-term acquisition of the public streets identified on Schedule 2 or public parkland identified on Schedule 5. For this new development, the City will still encourage the consideration of the urban design policies and guidelines in Section 5.0, as they may apply, during the development review process.

Section 9.0 Schedules



### Schedules



### Schedule 6 Servicing Network Plan



Trunk Watermain

Trunk Storm Sewer

Wastewater Collector Sewer

# **Appendix C**

Water Supply Servicing

#### Richcraft Homes 3194 Jockvale Road Proposed Plan of Subdivision

Water Demand Design Flows per Unit Count City of Ottawa - Water Distribution Guidelines, July 2010



#### **Domestic Demand**

Type of Housing	Per / Unit	Units	Pop
Single Family	3.4	-	0
Semi-detached	2.7	-	0
Townhouse	2.7	-	0
Apartment			504
Bachelor	1.4	-	0
1 Bedroom	1.4	-	0
2 Bedroom	2.1	-	0
3 Bedroom	3.1	-	0
Average	1.8	-	0

	Pop	Avg. Daily		Max Day		Peak Hour	
		m³/d	L/min	m³/d	L/min	m³/d	L/min
<b>Total Domestic Demand</b>	504	141.1	98.0	352.8	245.0	776.2	539.0

#### Institutional / Commercial / Industrial Demand

			Avg. [	Daily	Max	Day	Peak I	Hour
Property Type	Unit Rate	Units	m³/d	L/min	m³/d	L/min	m³/d	L/min
Commercial Area	28,000 L/gross ha/d	5.93	166.04	115.3	249.1	173.0	448.3	311.3
Office	75 L/9.3m <sup>2</sup> /d	-	0.00	0.0	0.0	0.0	0.0	0.0
Restaurant	125 L/seat/d	-	0.00	0.0	0.0	0.0	0.0	0.0
Industrial - Light	35,000 L/gross ha/d	-	0.00	0.0	0.0	0.0	0.0	0.0
Industrial - Heavy	55,000 L/gross ha/d	-	0.00	0.0	0.0	0.0	0.0	0.0
	Total I/C	Demand _	166.0	115.3	249.1	173.0	448.3	311.3
	Tota	al Demand _	307.2	213.3	601.9	418.0	1224.5	850.3

	L/min	L/s
Avg. Daily	213.3	3.56
Max Day	418.0	6.97
Peak Hour	850.3	14.17

Water Demand Design Flows per Unit Count City of Ottawa - Water Distribution Guidelines, July 2010



## **Domestic Demand**

Type of Housing	Per / Unit	Units	Pop
Single Family	3.4	-	0
Semi-detached	2.7	-	0
Townhouse	2.7	-	0
Apartment			0
Bachelor	1.4	-	0
1 Bedroom	1.4	-	0
2 Bedroom	2.1	-	0
3 Bedroom	3.1	-	0
Average	1.8	1,993	3588

	Pop	Avg. D	Daily	Max I	Day	Peak H	lour
		m³/d	L/min	m³/d	L/min	m³/d	L/min
Total Domestic Demand	3588	1004.6	697.7	2511.6	1744.2	5525.5	3837.2

## Institutional / Commercial / Industrial Demand

			Avg. [	Daily	Max I	Day	Peak I	Hour
Property Type Ui	nit Rate	Units	m³/d	L/min	m³/d	L/min	m³/d	L/min
Commercial Area* 28,0	00 L/m²/d	8.63	241.64	167.8	362.5	251.7	652.4	453.1
Office	75 L/9.3m²/d	-	0.00	0.0	0.0	0.0	0.0	0.0
Restaurant 12	25 L/seat/d	-	0.00	0.0	0.0	0.0	0.0	0.0
Industrial - Light 35,0	00 L/gross ha/d	-	0.00	0.0	0.0	0.0	0.0	0.0
Industrial - Heavy 55,0	00 L/gross ha/d	-	0.00	0.0	0.0	0.0	0.0	0.0
	Total I/C	Demand _	241.6	167.8	362.5	251.7	652.4	453.1
	Tota	l Demand	1246.3	865.5	2874.1	1995.9	6177.9	4290.2

<sup>\*</sup> Mixed Use Area taken as Commercial to account for both Population and Commercial demands

	L/min	L/s
Avg. Daily	865.5	14.42
Max Day	1995.9	33.26
Peak Hour	4290.2	71.50

# Kennedy-Burnett Potable Water Master Servicing Study



Prepared for: City of Ottawa 100 Constellation Crescent Ottawa, ON K2G 6G8

Prepared by: Stantec Consulting Ltd. 400-1331 Clyde Avenue Ottawa, ON K2C 3G4

File No. 1634-01221

# KENNEDY-BURNETT POTABLE WATER MASTER SERVICING STUDY

Hydraulic Assessment April 29, 2014

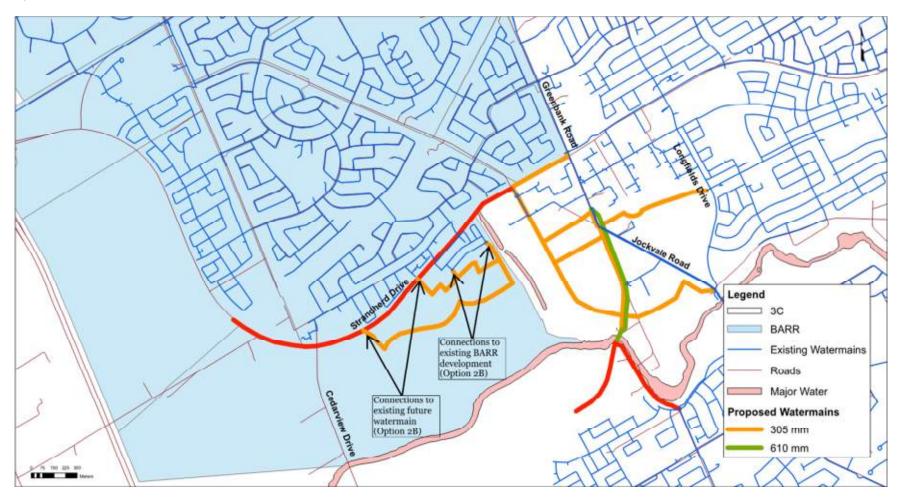


Figure 2-6: Proposed Pipe Layout Post Zone Reconfiguration – Scenario 2B



# **Appendix D**

Wastewater Servicing

## SANITARY SEWER CALCULATION SHEET

NEW PROPOSED DESIGN PARAMETERS

LOCATION: 3194 Jockvale Rd.

FILE REF: 14-735 18-Dec-18 DATE:

Avg. Daily Flow Res. 280 L/p/d Peak Fact Res. Per Harmons: Min = 2.0, Max =4.0 Infiltration / Inflow 0.33 L/s/ha Peak Fact. Comm. 1.5 Min. Pipe Velocity 0.60 m/s full flowing Avg. Daily Flow Comm. 28,000 L/ha/d Park Flow 9,300 L/ha/d Peak Fact. Instit. 1.5 Max. Pipe Velocity 3.00 m/s full flowing

Avg. Daily Flow Indust. 35,000 L/ha/d Peak Fact. Indust. per MOE graph Harmens Corr Factor 0.8

Mannings N 0.013



Location	n Residential Area and Population Commercial* Institutional Park		rk			Infiltration	า																
Area ID	INFO		Area Number of Units			Pop.	Cum	ulative	Peak.	$Q_{res}$	Area	Accu.	Area	Accu.	Area	Accu.	$Q_{C+I+I}$	Total	Accu.	Infiltration	Total		
					by t	уре			Area	Pop.	Fact.			Area		Area		Area		Area	Area	Flow	Flow
			(ha)	Singles	MidRise	Town's	Apt's		(ha)		(-)	(L/s)	(ha)	(ha)	(ha)	(ha)	(ha)	(ha)	(L/s)	(ha)	(ha)	(L/s)	(L/s)
SNTC CDP JULY 2006			0.000				1993	3587.0	0.000	3587.0	2.90	33.71	8.63	8.63		0.00	0.72	0.72			10.610		41.53
																				*Includes 1	.26 ha of it	nfiltration for	collector roads
3194 JOCKVALE RD. FSR DEC 2018			3.860				240	504.0	3.860	504.0	3.38	5.52	5.93	5.93		0.00		0.00					11.90
																				*Includes 0	.82 ha of in	nfiltration for	collector roads

<sup>\*</sup> Mixed Use areas taken as commercial area to account for commercial & population flows



Land / Site Development

Municipal Infrastructure

Environmental / Water Resources

Traffic/

Transportation

Structural

Recreational

# **Planning**

Land/Site Development

Planning Application Management

Municipal

Planning Documents &

**Studies** 

**Expert Witness** (OMB)

Wireless Industry

# Landscape **Architecture**

Urban Design & Streetscapes

Recreation & Parks

**Planning** 

Environmental

Restoration

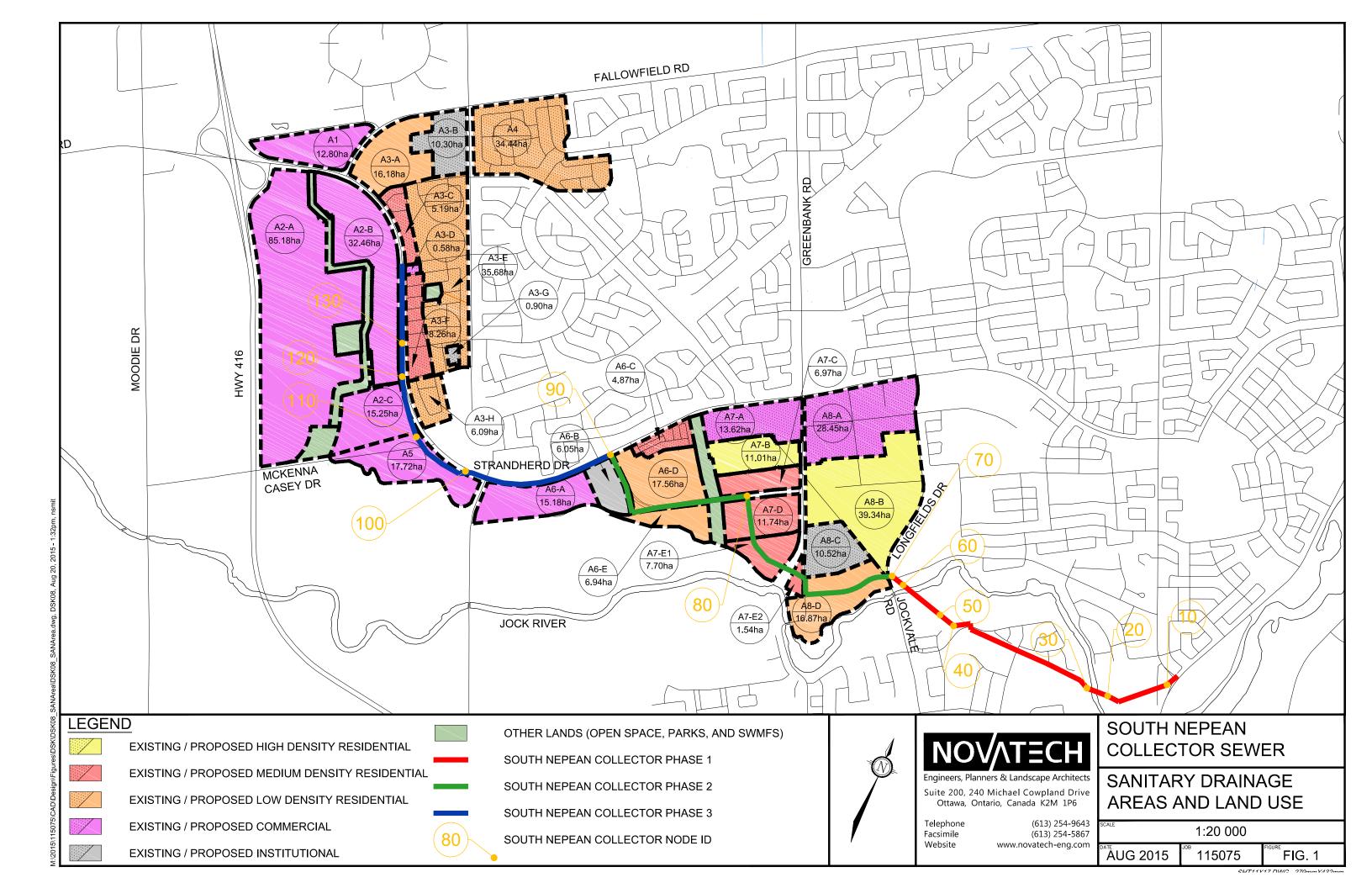
Sustainable Design

# **South Nepean Collector: Phase 2**

Hydraulics Review / Assessment

**Technical Memorandum** 

Prepared for the City of Ottawa



# **SANITARY SEWER DESIGN SHEET**

South Nepean Collector - Phase 2 & 3

 PROJECT #:
 115075

 DESIGNED BY:
 CMS

 CHECKED BY:
 MJP

 DATE:
 August 2:

August 20, 2015 Theoretical Future Full Service Peak Wastewater Flow



	Location			Α	reas			Pop	ulation		In	dividual Design Flo	ws	Cumulative Design Flows				
Area I.D.	Existing / Proposed Land Use	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Total Gross Area (ha)	Residential Popultation Density (people / ha)	Individual Residential Population	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn <sup>1</sup> )	Commercial Peak Flow Rate <sup>2</sup> (50,000 L/ha/d) (L/s)	Institutional Peak Flow Rate <sup>2</sup> (50,000 L/ha/d) (L/s)	Infiltration / Inflow Rate (0.28 L/s/ha) (L/s)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (350 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)
A1	Commercial	130	12.80			12.80					11.1	0.0	3.6	11.1	0.0	3.6	0.0	14.7
A2-A	Commercial	130	85.18			85.18					73.9	0.0	23.9	85.1	0.0	27.4	0.0	112.5
A2-B	Commercial	130	32.46			32.46					28.2	0.0	9.1	113.2	0.0	36.5	0.0	149.8
A3-A	Low Density Residential	130			16.18	16.18	95.2	1540	1540	3.67	0.0	0.0	4.5	113.2	0.0	41.1	22.9	177.2
A3-B	Institutional	130		10.30		10.30			1540	3.67	0.0	8.9	2.9	113.2	8.9	43.9	22.9	189.0
A3-C	Medium Density Residential	130			5.19	5.19	162.0	841	2381	3.53	0.0	0.0	1.5	113.2	8.9	45.4	34.0	201.6
A3-D	Commercial	130	0.58			0.58			2381	3.53	0.5	0.0	0.2	113.7	8.9	45.6	34.0	202.2
A3-E	Low Density Residential	130			35.68	35.68	95.2	3397	5778	3.19	0.0	0.0	10.0	113.7	8.9	55.5	74.6	252.8
A3-F	Medium Density Residential	130			8.26	8.26	162	1338	7116	3.10	0.0	0.0	2.3	113.7	8.9	57.9	89.4	269.9
A3-G	Institutional	130		0.90		0.90			7116	3.10	0.0	0.8	0.3	113.7	9.7	58.1	89.4	270.9
A4	Low Density Residential	130			34.44	34.44	95.2	3279	10395	2.94	0.0	0.0	9.6	113.7	9.7	67.8	123.7	314.9
A2-C	Commercial (ex. snow dump)	120	15.25			15.25			10395	2.94	13.2	0.0	4.3	127.0	9.7	72.0	123.7	332.4
АЗ-Н	Low Density Residential	120			6.09	6.09	95.2	580	10974	2.91	0.0	0.0	1.7	127.0	9.7	73.7	129.6	340.0
A5	Commercial	110	17.72			17.72			10974	2.91	15.4	0.0	5.0	142.4	9.7	78.7	129.6	360.3
A6-A	Commercial	100	15.18			15.18			10974	2.91	13.2	0.0	4.3	155.5	9.7	82.9	129.6	377.8
A6-B	Institutional	100		6.05		6.05			10974	2.91	0.0	5.3	1.7	155.5	15.0	84.6	129.6	384.7
A6-C	Medium Density Residential	90			4.87	4.87	162.0	789	11763	2.88	0.0	0.0	1.4	155.5	15.0	86.0	137.4	393.9
A6-D	Low Density Residential	90			17.56	17.56	95.2	1672	13435	2.83	0.0	0.0	4.9	155.5	15.0	90.9	153.8	415.2
A6-E	Low Density Residential	90			6.94	6.94	95.2	661	14096	2.81	0.0	0.0	1.9	155.5	15.0	92.9	160.2	423.6
A7-A	Commercial	90	13.62			13.62			14096	2.81	11.8	0.0	3.8	167.4	15.0	96.7	160.2	439.2
A7-B	High Density Residential	90			11.01	11.01	135.0	1486	15582	2.76	0.0	0.0	3.1	167.4	15.0	99.8	174.3	456.4
A7-C	Medium Density Residential	90			6.97	6.97	162.0	1129	16711	2.73	0.0	0.0	2.0	167.4	15.0	101.7	184.9	468.9
A7-D	Medium Density Residential	90			11.74	11.74	162.0	1902	18613	2.68	0.0	0.0	3.3	167.4	15.0	105.0	202.4	489.7
A7-E1/E2	Medium Density Residential	90			9.24	9.24	162.0	1497	20110	2.65	0.0	0.0	2.6	167.4	15.0	107.6	215.9	505.8
A8-A	Commercial	80	28.45			28.45			20110	2.65	24.7	0.0	8.0	192.0	15.0	115.5	215.9	538.5
A8-B	High Density Residential	80			39.34	39.34	135.0	5311	25421	2.55	0.0	0.0	11.0	192.0	15.0	126.6	262.4	596.0
A8-C	Institutional	80		10.52		10.52			25421	2.55	0.0	9.1	2.9	192.0	24.1	129.5	262.4	608.1
A8-D	Low Density Residential	80			16.87	16.87	120.9	2040	27461	2.52	0.0	0.0	4.7	192.0	24.1	134.2	279.8	630.2
ROW Along SNC Sewer																		
Alignment	-	80				14.34			27461	2.52	0.0	0.0	4.0	192.0	24.1	138.2	279.8	634.2
TO	DTAL	80	221.24	27.77	230.38	493.73	-	27461	27461	2.52	192.0	24.1	134.2	192.0	24.1	138.2	279.8	634.2

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha	
Low Density	26 – 28	2.7 – 3.4	95.2	
(singles and semis)	(28 used)	(3.4 used)	93.2	
Medium Density	50 – 60	2.7	162.0	
(row/townhouse)	(60 used)	2.1	102.0	
High Density	60 – 75	1.8	135.0	
(anartments)	(75 used)	1.0	133.0	

## Notes:

1. Harmon Equation = 1 + [14 / (4+(P/1000)<sup>1/2</sup>)] x K

Where: P = population; K = correction factor = 1.0

2. Instituional / Commercial Peaking Factor = 1.5

## Reported Design Flows / Assumptions:

- 1. Area A4: Existing single family units currently serviced by Jockvale pump station to be redirected to SNC
- 2. Area A8-D: proposed 600 medium density residential units

# **Appendix E**

Stormwater Management Servicing

# Kennedy-Burnett Stormwater Management Facility Project File and Functional Design Report

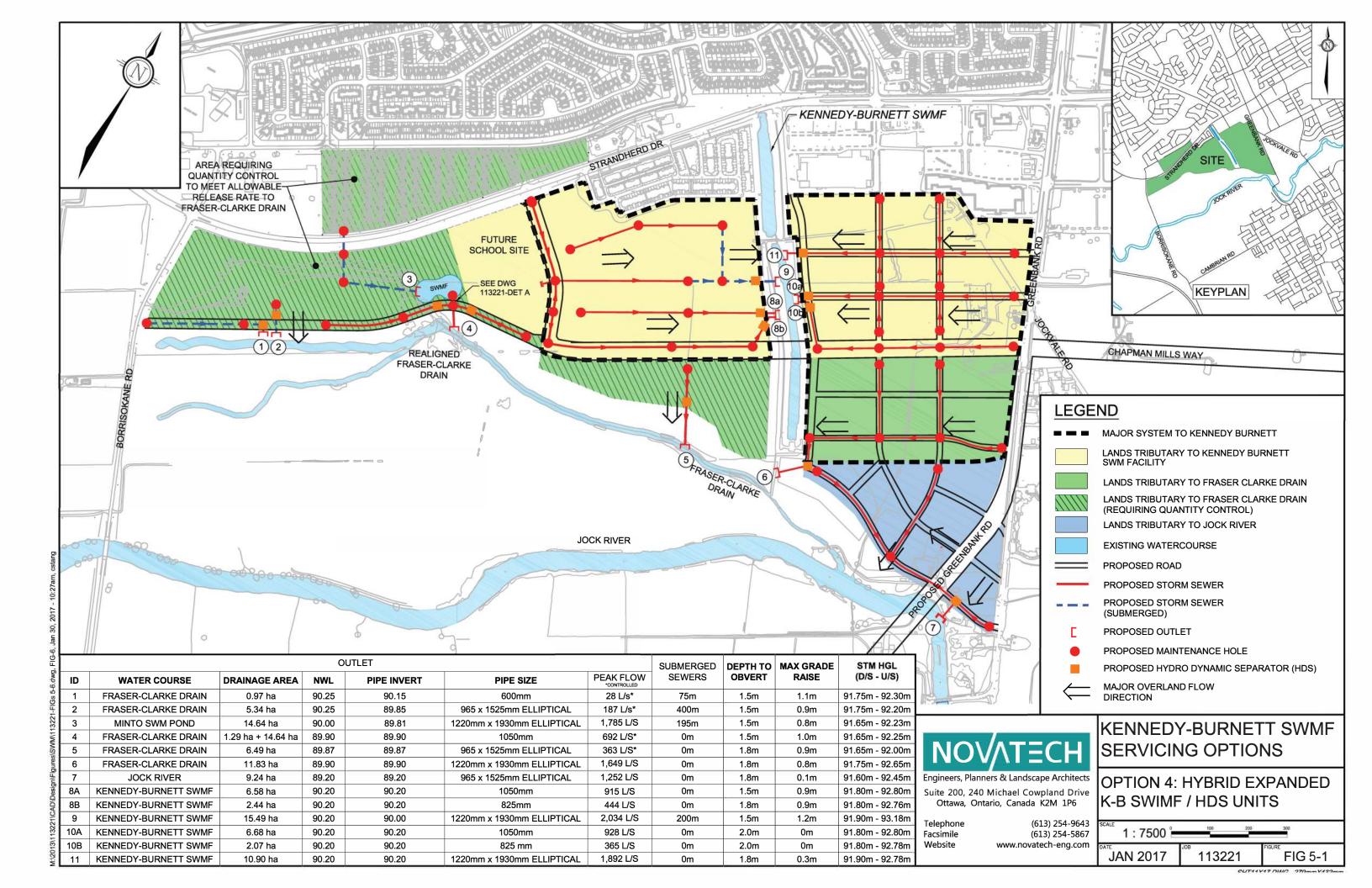
Prepared for City of Ottawa

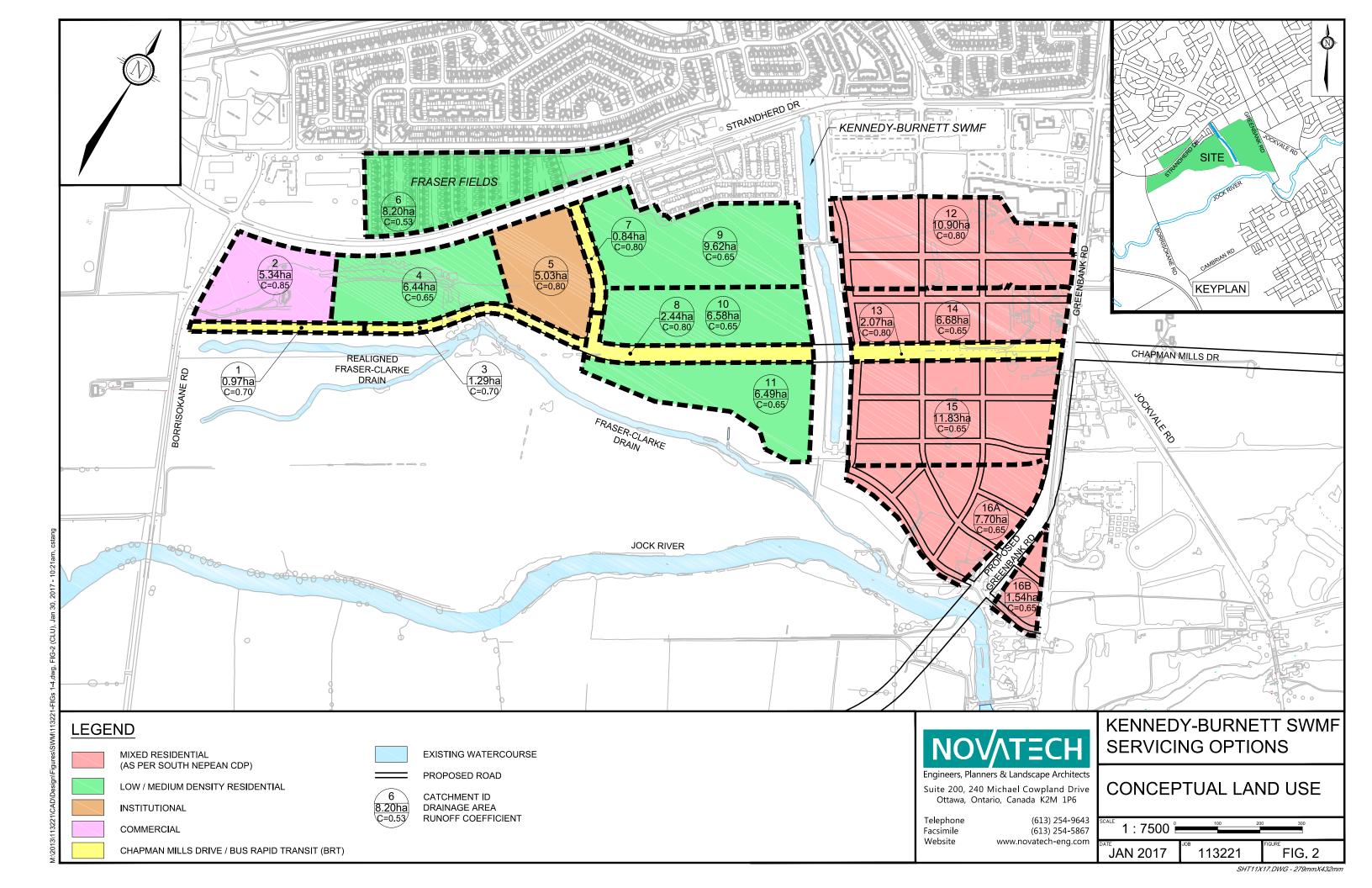


February 17, 2017



CH2M Hill Canada Ltd. 1101 Prince of Wales Drive Suite 330 Ottawa, ON K2C 3W7





# **FIGURES**

