

## **TECHNICAL MEMORANDUM**

DATE November 10, 2011

**PROJECT No.** 08-1122-0078

TO Michel Kearney, Cheryl McWilliams, Kevin Hall City of Ottawa

CC Frank Cairo, Susan Murphy

FROM Stephen Wilson, P.Geo.

EMAIL srwilson@golder.com

SUMMARY OF THE HYDROGEOLOGICAL INVESTIGATION, PRODUCTION WELL PW09-1 WESTERN DEVELOPMENT LANDS, VILLAGE OF RICHMOND, OTTAWA, ONTARIO

Mattamy Homes Limited (Mattamy) initiated a Water and Sewer Master Servicing Study for the Village of Richmond (Richmond) in 2008. This study, led by Stantec Consulting Ltd. (Stantec), included an investigation of the servicing options for the Village, which include the property controlled by Mattamy (site). The approximate site boundary is shown on Figure 1. The MSS identified communal wells as the preferred water servicing option for the site. In 2010, Mattamy released their option on part of the site, which was purchased by Richmond Village (North) Limited and Richmond Village (South) Limited (together referred to as RV). The Mattamy and RV properties are together referred to as the Western Development Lands.

There are two primary bedrock aquifer systems which can be used for water supply at the site. The upper aquifer is typically contained within the upper 35 metres of the Oxford Formation (limestone/dolostone). The majority of the private residential wells within Richmond are completed within this upper aquifer. The lower aquifer is contained within the upper portion of the Nepean Formation (sandstone) and lower portion of the March Formation (interbedded limestone and sandstone). This lower aquifer tends to be substantially more productive in comparison to the upper aquifer. Communal wells in the area (King's Park and Hyde Park in Richmond, and wells in Almonte, Munster, Kemptville and Merrickville) draw water from the lower aquifer. In some areas the two aquifers are separated by a bedrock aquitard consisting of limestone of the lower Oxford Formation and interbedded limestone and sandstone of the upper March Formations. The presence of this aquitard is often indicated by strong upward vertical gradients between the aquifers. The potentiometric surface of the lower aquifer is typically above ground surface, and wells therefore completed within this aquifer often flow.

Investigations that included well construction and aquifer testing were undertaken to assess the hydrogeological characteristics of the lower sandstone aquifer at the site. In November 2009, a 48-hour pumping test was conducted by Golder Associates Ltd. (Golder) using a pumping rate of 1,273 Litres per minute (L/min) on a well (PW08-1) completed in the lower sandstone aquifer. The transmissivity and storativity values generated by the analysis of drawdown data from the pumping test range from 328 metres squared per day ( $m^2$ /day) to 700  $m^2$ /day and from 9 x 10<sup>-4</sup> to 1 x 10<sup>-2</sup>, respectively. Based on the results of the pumping test, the sustainable yield of the well was estimated to be 2,600 L/min (Golder, 2011).

To allow for additional testing of the deep aquifer at the site, a second production well (PW09-1) was completed in the lower sandstone aquifer. The following provides a summary of the aquifer testing program completed using PW09-1.



## **Production Well Construction (PW09-1)**

In December 2009, a 0.254-metre diameter production well (PW09-1)was drilled to a depth of 70 metres below ground surface (mbgs). PW09-1 is located near the eastern property boundary approximately 650 metres south of Perth Street (see location on Figure 1). The production well was completed with 45.72 metres of steel well casing which was grouted in place. The steel casing was installed through the upper portion of the Oxford Formation (i.e., through the upper aquifer), and groundwater flow to the pumping well is expected to occur primarily from the lower aquifer. A schematic of the well construction details for PW09-1 is provided in Attachment 1.

## **Aquifer Testing Methodology and Observations**

A 72-hour pumping test was conducted at PW09-1 between September 27 and September 30, 2011. Recovery measurements were collected until October 3, 2011. The pumping test was started at a rate of 2,690 L/min. After the first day of pumping, the rate decreased slightly due to a loss of pump efficiency. The remainder of the test was completed at a rate that ranged from 2,690 L/min to 2,410 L/min.

During the pumping test, water level data was collected from the pumping well (PW09-1) and nine observation wells (PW09-2, PW08-1, MW08-1A, MW08-1B, MW08-1C, MW10-3A, OW-1, OW-2 and OW-3). The locations of the observation wells are shown on Figure 1, and the well completion details are provided on the logs in Attachment 1. The following table provides the radial distance from the pumping well, the open portion of the well, the formation the well is completed in, the static water level and the maximum drawdown measured during the pumping test for each location:

Location	Radial Distance (m)  Open Portion of Well (mbgs)		Formation	Static Water Level (mags/mbgs)	Maximum Drawdown Measured During Pumping Test (m)		
PW09-1	0	open hole from 45.72 to 70.00	Upper Nepean	2.07 mags <sup>1</sup>	52.5		
PW09-2	5	open hole from 45.72 to 70.00	Upper Nepean 2.07 mags		4.79		
PW08-1	35	open hole from 45.72 to 137.16	Upper Nepean	2.32 mags	3.82		
MW10-3A	79	4.4 to 6.0	Upper Oxford	0.99 mbgs	0.7		
MW08-1A	93	66.90 to 75.23	Upper Nepean	2.32 mags	3.6		
MW08-1B	93	48.51 to 53.46	Lower Oxford	2.36 mags	3.4		
MW08- 1C	93	7.47 to 12.04	Upper Oxford	1.12 mags	1.9		
OW-1	130	open hole from 6.71 to 31.39	Lower Oxford	0.58 mags	1.8		
OW-2	190	open hole from 6.71 to 31.39	Lower Oxford	0.47 mbgs	0		
OW-3	221	open hole from 10.36 to 37.49	Lower Oxford	1.55 mags	1.7		

mags - metres above ground surface; mbgs - metres below ground surface

1 Static water level could not be measured as well was flowing, static level assumed to equal static level in PW09-2



Water level measurements were collected in the observation wells using pressure transducers and data loggers, with periodic manual water level measurements collected for quality control. Due to the configuration of the pumping equipment that was used in PW09-1, a data logger could not be used appropriately, and only manual measurements were collected from the pumping well.

During the 72-hour pumping test the water level in OW-2 showed no significant change. Following the pumping test, OW-2 was sounded to confirm the well depth. At that time, the well was found to be blocked at a depth of approximately four metres. As such, OW-2 is not considered to be representative of aquifer conditions at the site, and will not be considered in the discussion provided below.

## **Aquifer Test Analysis**

The drawdown and recovery data obtained during the 72-hour pumping test was analyzed using the Cooper and Jacob equation (Cooper and Jacob, 1946) and the Theis recovery equation (Theis, 1935), respectively, to estimate the local aquifer characteristics (transmissivity and storativity). The following table summarizes the results:

Location	Transmissivity – Drawdown (m²/day)	Transmissivity – Theis Recovery (m²/day)	Storativity – Drawdown (dimensionless)
PW09-1		592	*-
PW09-2	630	599	4.8 x 10 <sup>-3</sup>
PW08-1	672	644	5.9 x 10 <sup>-4</sup>
MW10-3A	-	527	
MW08-1A	663	638	1.4 x 10 <sup>-4</sup>
MW08-1B	567	537	4.6 x 10 <sup>-4</sup>
MW08-1C	637	453	1.0 x 10 <sup>-2</sup>
OW-1	606	453	5.7 x 10 <sup>-3</sup>
OW-2	5	**	
OW-3	755	570	1.4 x 10 <sup>-3</sup>

Curve matching plots developed during the analysis of the drawdown and recovery data are provided in Attachment 2. Drawdown data collected in MW10-3A was sparse during the first 36 hours of the pumping test, and only recovery data could be analyzed. There is some question regarding the cause of the water level changes noted in this monitor, and it may reflect a precipitation event rather than response to pumping. The manual drawdown data from the pumping well PW09-1could not be used with confidence and only recovery data was analyzed. The transmissivity of the lower sandstone aquifer is estimated to range from 500 m²/day to 800 m²/day. The pumping test results indicated that the sustainable yield for well PW09-1 is at least the minimum pumping rate of 2,410 L/min and is likely greater.



## **Preliminary Predictive Simulations**

To estimate the potential drawdown associated with the long-term pumping related to water supply for the Western Development Lands, a simplified three-dimensional numerical groundwater model was constructed based on the results of the aquifer testing program. The code used was MODFLOW (McDonald & Harbaugh). Predictive simulations were completed using the assumed water taking rates required to supply the Western Development Lands. The assumptions are as follows:

- The RV lands will contain 1,000 units, including 650 singles and 350 town homes;
- The Mattamy lands will contain 1,000 singles; and,
- Average water demand is 835 L/day/unit for singles and 720 L/day/unit for town homes.

The number of planned units was provided by representatives of Mattamy and RV. The unit demand rates were taken from the Master Servicing Study (Stantec, 2011).

Using these assumptions, the average water demand for the Western Development Lands is 1,132 L/min.

The results of the numerical simulations suggest that pumping of PW09-1 (completed within the lower sandstone aquifer) at a rate equal to the assumed average daily pumping rate for the Mattamy/RV development (1,132 L/min), will result in a drawdown of approximately 1.0 metre at OW-1, and approximately 0.8 metres at OW-3 after 20 years of pumping. These two observation wells are completed in a similar manner and to a similar depth as typical private wells in Richmond. However, because they are flowing wells, they are considered representative of wells obtaining water from the upper limestone aquifer within an area of enhanced connection to the lower sandstone aquifer. OW-1 is located approximately 130 metres from the pumped well, and is closer than any existing private well. OW-3 is located approximately 220 metres from the pumped well, which is similar to the approximate radial distance of the nearest private well. A drawdown of less than one metre is considered insignificant and would not be noticed by local groundwater users.

If a maximum day demand of 2,320 L/day/unit for single family homes and 720 L/day/unit for town homes (Stantec, 2011) is assumed, a total demand of 2,833 L/min is predicted. This is slightly more than the pumping rate used during the 72 hour pumping test, and could be accommodated by one or both of the production wells without causing significant drawdown in the aquifer. Maximum day is typically not experienced for more than a few days at a time, but a numerical simulation was run using the maximum day rate for a period of 20 years. After this time, the drawdown at OW3 is predicted to be approximately two metres, which is considered minimal.

### **Groundwater Quality**

The lower sandstone aquifer underlying the site is regionally extensive, and is utilized by the King's Park and Hyde Park communal wells in Richmond, as wells as the communal wells systems in Almonte, Munster, Kemptville and Merrickville. In general, the groundwater quality in the lower aquifer is slightly better than in the upper aquifer. The groundwater in the lower aquifer is hard (typical for groundwater sources) and occasionally exceeds the non-health related aesthetic criteria for iron. The exceedances of the aesthetic criteria for iron in the lower aquifer are within the limit treatable using conventional water softening. Overall, wells completed in the lower aquifer are expected to produce groundwater that is safe and aesthetically suitable for human consumption.

The following description of the water quality and required treatment was provided by the City of Ottawa in the 2010 Annual Report for the King's Park communal well system:



The Kings Park water supply (serving a subdivision of Richmond) draws ground water from either one of two wells. The two wells are located at opposite ends of the Kings Park subdivision. The source water has consistently been found to be clear of bacteria and chemical contaminants, has a high hardness level and a noticeable concentration of naturally occurring iron and hydrogen sulfide.

The treatment process in Kings Park consists of the following steps:

- Disinfection (free chlorine using sodium hypochlorite) which also oxidizes hydrogen sulphide; and,
- Chlorine contact time.

This treatment process results in water that is clear and safe to drink. There is a slight noticeable taste of elemental sulphur in the finished water.

A similar treatment process and resulting acceptable water quality for drinking is reported by the Almonte, Munster, Kemptville and Merrickville communal well systems supplied by the lower sandstone aquifer. Based on the available water quality data from the existing communal well systems, high quality potable water is available from the lower sandstone aquifer underlying the site. To confirm that the water quality in the sandstone aquifer at the site is consistent with the water quality measured at the existing communal wells, water quality testing was completed at three intervals during the pumping test at PW09-1.

Following 20 hours of pumping and 44 hours of pumping at PW09-1, samples were collected for the "General Geochemistry of Groundwater package" which includes basic inorganic and metals parameters of interest in groundwater. Following 72 hours of pumping at PW09-1, samples were collected for a suite of volatile organic compounds (VOCs), as well as the "Subdivision Package" which includes a variety of organic, inorganic, metals and bacteriological parameters. All groundwater samples obtained from PW09-1 were collected using appropriate sampling and preservation techniques, placed in coolers with ice packs and delivered to Exova Laboratories Ltd. of Ottawa, Ontario.

The results of the water quality testing for PW09-1 are provided in Table 1. The water from PW09-1 is of excellent quality, meeting all of the health related Ontario Drinking Water Quality Standards and all of the established aesthetic objectives for the parameters tested. The hardness concentration of 286 to 305 milligrams per Litre (mg/L) at PW09-1 exceeds the operational guideline of 100 mg/L, but is considered typical for groundwater derived from a bedrock aquifer. The water quality measured at PW09-1 remained stable during the pumping test, and is consistent with the water quality observed at the existing communal wells completed in Richmond, and the water quality observed during the previous pumping test at PW08-1 (Golder, 2011). As a result, it is expected that communal wells completed at the site will provide high quality potable water.

### Summary

This memorandum summarizes the aquifer testing and subsequent analysis completed at PW09-1 by Golder as part of the ongoing hydrogeological investigation for the Western Development Lands. A 72-hour pumping testing was completed on production well PW09-1. Based on the results of the pumping test, the sustainable yield at PW09-1 is at least 2,410 L/min. Analysis of the drawdown and recovery data gathered during the pumping test result in transmissivity estimates that ranged from 500 m²/day to 800 m²/day. Preliminary predictive numerical simulations were completed to estimate the potential impact of long-term pumping of the lower aquifer on private wells in Richmond. The preliminary modelling results, as wells as the drawdown observed during the 72-hour pumping test, suggest that long-term pumping of the lower aquifer will not interfere with water supply from the upper aquifer.



**GOLDER ASSOCIATES LTD.** 

Jame Oxtobee, M.Sc., P.Geo. Senior Hydrogeologist/Associate Stephen Wilson, P.Geo. Senior Hydrogeologist/Associate

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JPAO/SRW/sg n:\active\2008\1122 - environmental\08-1122-0078 mattamy richmond\aquifer testing (2011-sept-27)\reporting\10nov2011 aquifer testing at pw09-1(memo to city).docx

Attachments: Table 1 – PW09-1 Water Quality Results

Figure 1 – Site Plan

Attachment 1 - Water Well Records and Borehole Logs

Attachment 2 - Drawdown and Recovery Plots

### References

- Cooper, H.H., and C.E., Jacob, 1946. A Generalized Graphical Method for Evaluating Formation Constants and Summarizing Well Field History, Am. Geophys. Union Trans., vol. 27, pp. 526-534.
- Golder Associates Ltd., 2011. Summary of Hydrogeological Investigation: Mattamy Richmond Lands, Ottawa, Ontario. March 25, 2011.
- McDonald, M.G., and Harbaugh, A.W. (1988). A modular three-dimensional finite-difference ground-water flow model. Techniques of Water-Resources Investigations, Book 6. U.S. Geological Survey.
- Stantec Consulting Ltd., 2011. Village of Richmond Water and Sewer Master Servicing Study. July 22, 2011
- Theis, C.V., 1935. The Relationship between the Lowering of the Piezometric Surface and the Rate and Duration of Discharge of a Well Using Groundwater Storage, Trans. Amer. Geophys. Union, Vol. 16, pp. 519-524.



# TABLE 1 PW09-1 WATER QUALITY RESULTS RICHMOND MATTAMY LANDS, OTTAWA, ONTARIO

ocation				PW09-1 (21 Houn
Date Sampled	ODWSOG	28-Sep-11	29-Sep-11	30-Sep-11
Parameter				
Bacteria				
Escherichia Coli (units - CFU/100mL)	0 (MAC)			0
otal Coliforms (units - CFU/100mL)	0 (MAC)	**		0
/olatile Organic Compouns - VOCs				
,1,1,2-tetrachloroethane		**		<0.5
,1,1-trichloroethane		**		<0.4
1,2,2-tetrachloroethane		>>		<0.5
,1,2-trichloroethane		**	:=66)	<0.4
,1-dichloroethane			240	<0.4
1.1-dichloroethylene	14 (MAC)			<0.5
2-dibromoethane	000 (140)	22	77	<0.2
,2-dichlorobenzene	200 (MAC)		- 3	<0.4
,2-dichloroethane	5 (MAC)		320	<0.2
.2-dichloropropane				<0.5 <0.3
,3,5-trimethylbenzene				<0.4
,3-dichlorobenzene ,4-dichlorobenzene	5 (MAC)			<0.4
A-dichioropenzene Benzene	5 (MAC)		- :-	<0.4
Bromodichloromethane	5 (WAG)		- :-	<0.3
Bromodicniorometnane Bromoform			- :-	<0.4
Bromomethane		•••		<0.5
c-1,2-Dichloroethylene				<0.4
-1,3-Dichloropropylene		**	**	<0.2
Carbon Tetrachloride	5 (MAC)			<0.5
Chloroethane	O (IVI) LOT			<0.2
Chloroform		(4)4	**	<0.5
Chloromethane			**	<0.2
Dibromochloromethane		464		<0.3
Dichlorodifluromethane		**		<0.5
Dichloromethane	50 (MAC)			<4.0
Ethylbenzene	2.4 (AO)	122	- 22	<0.5
n/p-xylene				<0.5
Monochlorobenzene	80 (MAC)			<0.2
General Chemistry				
Alkalinity as CaCO3	500 (OG)	259	258	258
Calcium		75	81	79
Chloride	250 (AO)	43	43	44
Conductivity (Lab) (units uS/cm)		664	673	676
Conductivity (Field) (units uS/cm)		627	593	647
Colour (units - TCU)	5.0 (AO)	**	**	<2
Dissolved Organic Carbon	5.0 (AO)	5-40	1997	1
luoride	1.5 (MAC)	0.25	0.25	0.25
ron	0.3 (AO)	0.13	0.11	0.16
Ludes and Culmbide	0.05 (AO)	**	8.0	<0,01
Hardness as CaCO3	100 (OG)	286	305	296
Hardness as CaCO3 on Balance		286	22	0.95
Hardness as CaCO3 on Balance Magnesium	100 (OG)	286  24	25	0.95 24
fardness as CaCO3 on Balance Magnesium Manganese		286  24 <0.01	25 <0.01	0.95 24 <0.01
Hardness as CaCO3 on Balance Magnesium Manganese Ammonia (N-NH3)	100 (OG) 0.05 (AO)	286  24 <0.01	25 <0.01	0.95 24 <0.01 0.04
lardness as CaCO3 on Balance Aagnesium Aanganese Ammonia (N-NH3) Vitrite (N-NO2)	0.05 (AO)	286  24 <0.01	25 <0.01	0.95 24 <0.01 0.04 <0.1
lardness as CaCO3 on Balance Magnesium Manganese Ammonia (N-NH3) Vitrie (N-NO2) Vitrate (N-NO3)	100 (OG) 0.05 (AO)	286 	25 <0.01	0.95 24 <0.01 0.04 <0.1 <0.1
Aardness as CaCO3 on Balance Aagnesium Aanganese Ammonia (N-NH3) Vitrite (N-NO2) Vitrate (N-NO3) OH (Lab) (pH units)	0.05 (AO)	286 	25 <0.01  <0.10 7.97	0.95 24 <0.01 0.04 <0.1 <0.1 7.98
Hardness as CaCO3 on Balance Magnesium Manganese Ammonia (N-NH3) Vilirite (N-NO2) Vilirite (N-NO3) OH (Lab) (pH units) OH (Field) (pH units)	0.05 (AO)	286 	25 <0.01  <0.10 7.97 6.41	0.95 24 <0.01 0.04 <0.1 <0.1 7.98 6.47
Hardness as CaCO3 on Balance Magnesium Manganese Ammonia (N-NH3) Vitrite (N-NO2) Vitrate (N-NO3) bH (Lab) (pH units) bH (Field) (pH units)	0.05 (AO)	286 	25 <0.01   <0.10 7.97 6.41	0.95 24 <0.01 0.04 <0.1 <0.1 7.98 6.47 <0.001
Hardness as CaCO3 on Balance Magnesium Manganese Ammonia (N-NH3) Nitrite (N-NO2) Nitrate (N-NO3) OH (Lab) (pH units) OH (Field) (pH units) Phenols Potassium	100 (OG)  0.05 (AO)  1.0 (MAC)  10 (MAC)	286 	25 <0.01 	0.95 24 <0.01 0.04 <0.1 <0.1 7.98 6.47 <0.001 3
Hardness as CaCO3 on Balance Magnesium Manganese Ammonia (N-NH3) Nitrite (N-NO2) Nitrate (N-NO3) HH (Field) (pH units) Phenols Polassium Sodium	1.0 (OG)  0.05 (AO)  1.0 (MAC)  10 (MAC)  200° (AO)	286 	25 <0.01  <0.10 7.97 6.41  24	0.95 24 <0.01 0.04 <0.1 7.98 6.47 <0.001 3
Hardness as CaCO3 on Balance Magnesium Manganese Ammonia (N-NH3) Hifrite (N-NO2) Hifrite (N-NO3) H (Lab) (pH units) DH (Field) (pH units) Phenols Potassium Sodium Sulphate	100 (OG)  0.05 (AO)  1.0 (MAC)  10 (MAC)	286 	25 <0.01  <0.10 7.97 6.41  24	0.95 24 <0.01 0.04 <0.1 7.98 6.47 <0.001 3 23
Hardness as CaCO3 on Balance Magnesium Manganese Ammonia (N-NH3) Mitrite (N-NO2) Mitrate (N-NO3) HI (Lab) (pH units) HH (Field) (pH units) Phenols Potassium Sodium Sulphate Fannin & Lignin	1.0 (OG)  0.05 (AO)  1.0 (MAC)  10 (MAC)  200° (AO)	286 	25 <0.01  <0.10 7.97 6.41  24 46 0.2	0.95 24 <0.01 0.04 <0.1 7.98 6.47 <0.001 3 23 47 <0.1
Hydrogen Sulphide Hardness as CaCO3 Ion Balance Magnesium Manganese Armnonia (N-NH3) Nitrite (N-NO2) Nitrite (N-NO3) Id (Lab) (pH units) Id (Field) (pH units) Phenols Potassium Sulphate Tannin & Lignin Temperature (Field) (*C)	1.0 (OG)  0.05 (AO)  1.0 (MAC)  10 (MAC)  200° (AO)	286 24 <0.01 <0.10 7.93 6.32 24 46 <0.1 11.6	25 <0.01  <0.10 7.97 6.41  24 46 0.2 10	0.95 24 <0.01 0.04 <0.1 7.98 6.47 <0.001 3 23 47 <0.1 10.8
Hardness as CaCO3 on Balance Magnesium Manganese Ammonia (N-NH3) Nitrite (N-NO2) Nitrite (N-NO3) OH (Lab) (pH units) OH (Field) (pH units) Phenols Potassium Sodium Sulphate Fannin & Lignin	1.0 (OG)  0.05 (AO)  1.0 (MAC)  10 (MAC)  200° (AO)	286 	25 <0.01  <0.10 7.97 6.41  24 46 0.2	0.95 24 <0.01 0.04 <0.1 7.98 6.47 <0.001 3 23 47 <0.1

all units are in mg/L unless otherwise noted ODWSOG - Ontario Drinking Water Standards, Objectives and Guidelines AO - aesthetic objective

OG - operational guideline

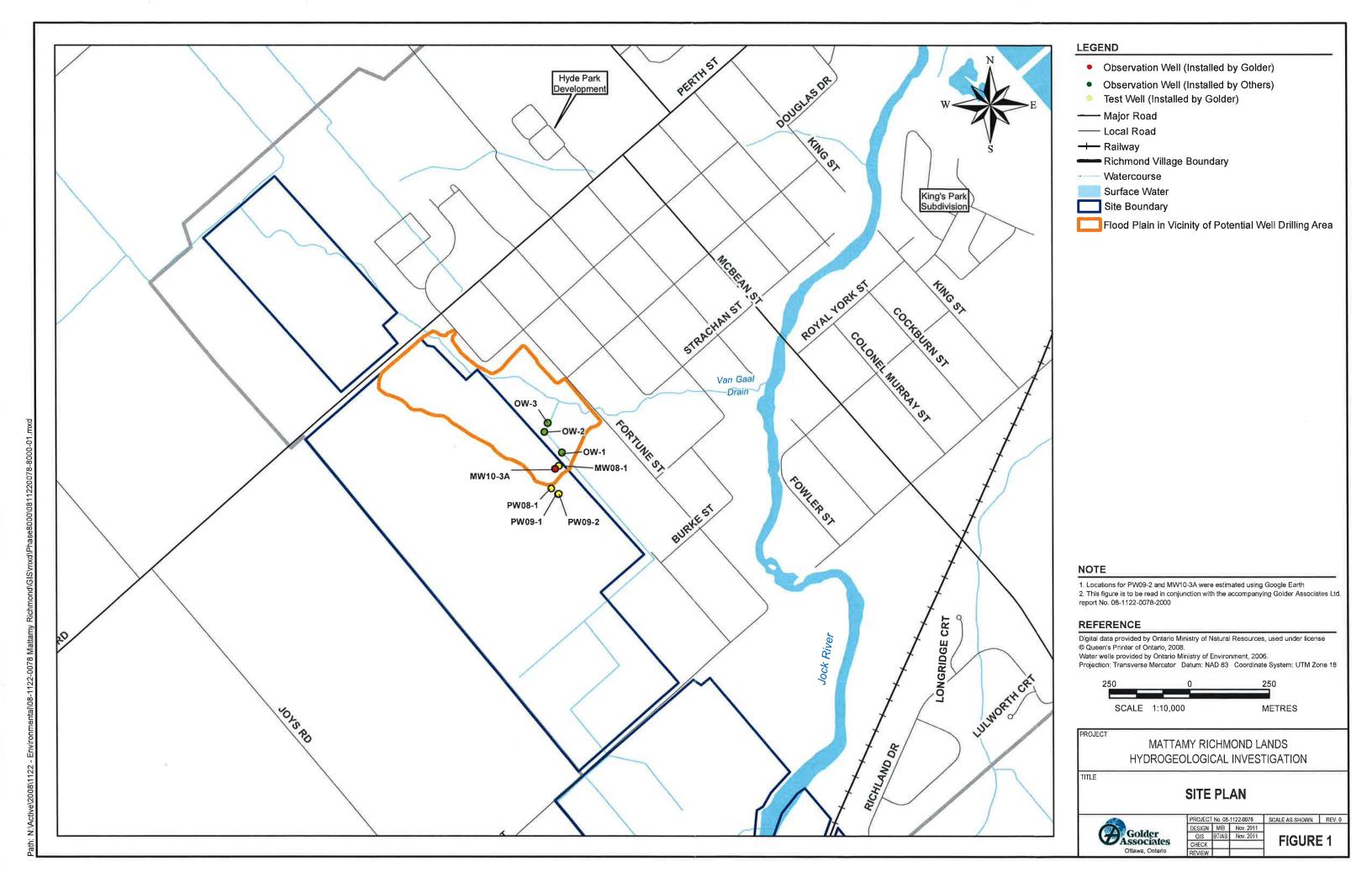
MAC - maximum acceptable concentration

Bold Values - indicate an exceedance of ODWSOG

a - the aesthetic objective for sodium in drinking water is 200 mg/L. The local Medical Officer of Health should be notified when sodium concentrations exceed 20 mg/L.

TCU - true colour units

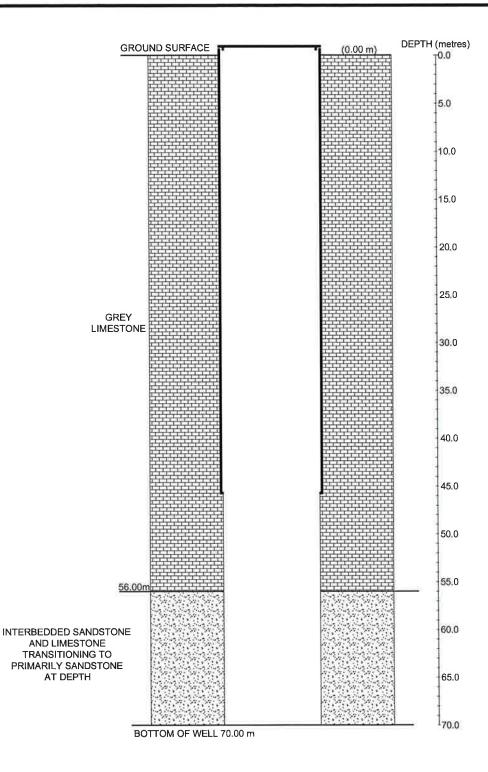
NTU - nephelometric turbidity unit



# **ATTACHMENT 1**

Water Well Records/Borehole Logs (PW09-1, PW09-2, PW08-1, MW08-1, MW10-3A, OW-1, OW-2 and OW-3)





NOTE

- 1. THIS FIGURE IS TO BE READ IN CONJUNCTION WITH THE ACCOMPANYING GOLDER ASSOCIATES LTD. REPORT No. 08-1122-0078
  - 2. WELL DIAMETER 0.254 m
- 3. OPEN HOLE FROM 45.72 m TO 70.00 m

			SCALE			NTS
Golder			DATE	4	Nov.	2011
Associat	PC		DESIGN			
Ottawa, Onta			CADD			PG
FILE No. 0811220078-8000-03.dwg	3		CHECK			
PROJECT No. 08-1122-0078	REV.	0	REVIEW			

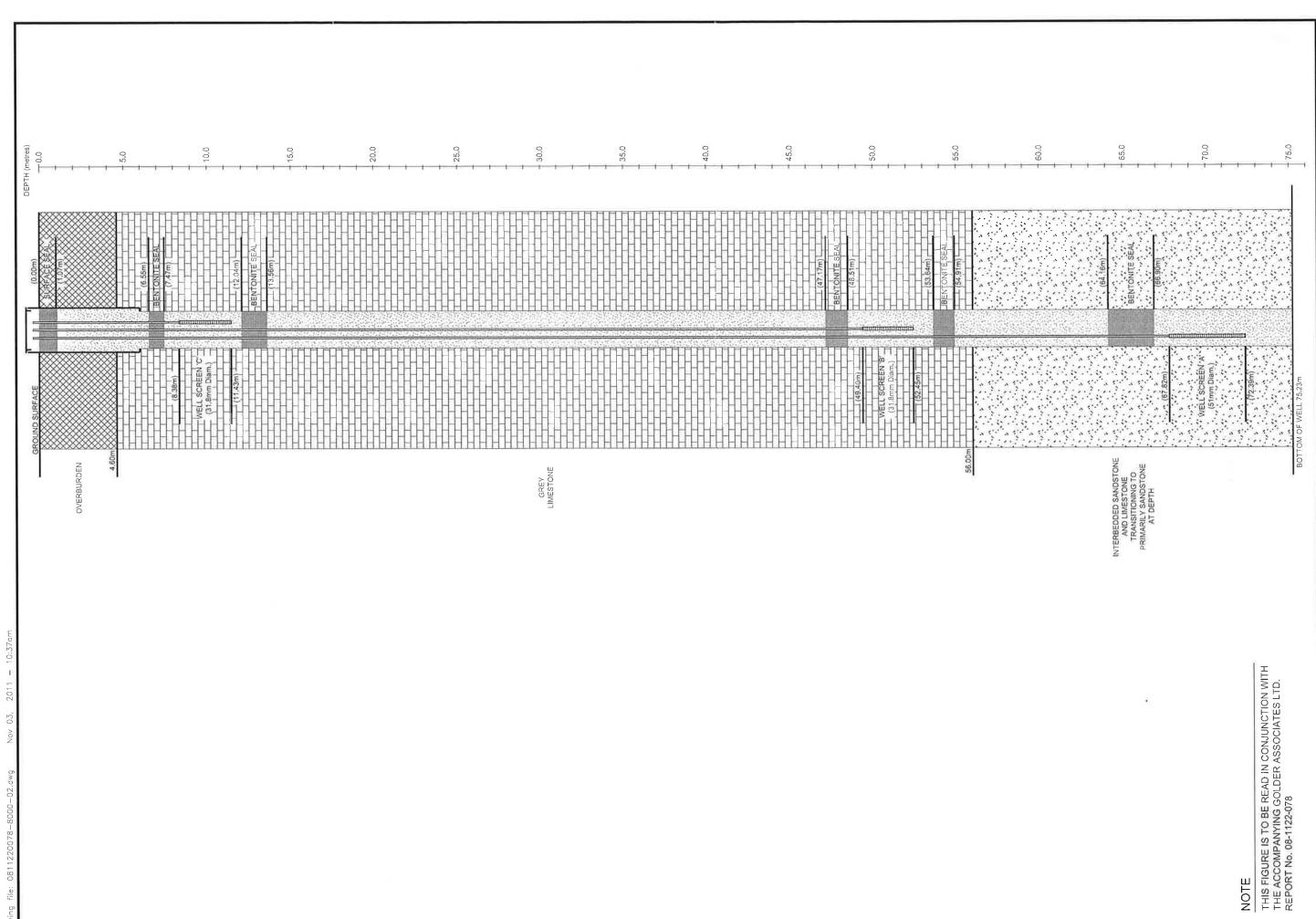
# PRODUCTION WELL CONSTRUCTION DETAILS FOR PW09-1

MATTAMY RICHMOND LANDS HYDROLOGICAL INVESTIGATION

FIGURE

1

Environmental\08-1122-0078 Mattamy Richmond\ACAD\Phase 8000\0811220078-8000-03.dwg FILENAME: N:\Active\2008\1122



MATTAMY RICHMOND LANDS HYDROGEOLOGICAL INVESTIGATION

Golder Associates Ottowa, Ontario

MONITORING WELL
CONSTRUCTION DETAILS
FOR MW 08-1

PROJECT No.08-1122-007 FILE No. 0811220078-8000-02.dw REV. 0 SCALE DESIGN MIB Nov. 201 CADD CHECK JM Nov. 201

FIGURE 2

Franktown

Well Contractor and Well Contractor's Licence No 3 | 7 | 4 | 9. Clarendon witchen rd Postal Code | Business E-mail Address | Busi

er found at Depth Kind of Water; Fresh Win (mill) Gas Olher, specify
Vater found at Depth Kind of Water: Fresh / (m/ft) ☐ Gas ☐ Other, specify

1 0 5 0

Y Y Y Y Y M M D D /res 2016010103 Ministry Use Only 2103267

DIO MIMO YIOLG Ministry's Copy

255 10/8

PROJECT: 08-1122-0078

# RECORD OF BOREHOLE: 10-3

SHEET 1 OF 2

LOCATION: See Site Plan

DEPTH SCALE

1:50

BORING DATE: Apr. 28-29, 2010

DATUM: Geodetic

LOGGED: Jp.

CHECKED:

SAMPLER HAMMER, 64kg; DROP, 760mm

PENETRATION TEST HAMMER, 64kg; DROP, 760mm

8	SOIL PROFILE		SA	MPLE	S	DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m	HYDRÁULIC CONDUCTIVITY, k, cm/s	49 9	PIEZOMETER
BORING METHOD	DESCRIPTION	STRATA PLOT  STRATA PLOT	NUMBER	TYPE	BLOWS/0 3m	20 49 60 80 SHEAR STRENGTH nat V. + Q - Cu, kPa rem V. ① U - C	10 <sup>4</sup> 10 <sup>4</sup> 10 <sup>15</sup> WATER CONTENT PERCENT	ADDITIONAL LAB TESTING	OR STANDPIPE INSTALLATION
30RIN	DESCRIPTION	(m) TRAT	NOM		BLOW		Wp 1 1 441	PAB A	
-	GROUND SURFACE	93 g	,			20 40 50 80	20 40 60 80		
П	TOPSOIL Very stiff to stiff grey brown SILTY CLAY, some sand (Weathered Crust)	80	8						Ź
	CLAY, some sand (Weathered Crust)		1	50 DO	9				Bentonite Seal
Power Auger Zoomm Diam (Hollow Stern)	Country weeks		2		3				S#cu Sand
Powe mm Otam	Compact to dense grey brown fine	91 6 2 1							32mm Diam PVC
2002	SANDY SILT		3	50 DO	20				#10 Slot Screen 'B'
			4	50 DO	47				Silica Sand
	Dense grey brown SANDY SILT, some oravel (GLACIAI, TILL) Very thinky to medium bedded light grey interbedded SANDSTONE and DOLOSTONE BEDROCK	3,0							Bentonite Seal
	Interbedded SANDSTONE and DOLOSTONE BEDROCK		C1	NO RC	DĐ				
Retary Delli	N D CGra		C	2 NQ	ממ				32mm Diem PVC #10 Stol Screen 'A'
		87	96I 00						
	End of Borehole		Ou						W.L. in screen 'A' at Elev. 93.77m on Apr. 30, 2010
7									W.L. in screen 'B' at Elev 93.17m on Apr 30, 2010
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\$)) <sup>*</sup>									
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			_1						

PROJECT: 08-1122-0078

## RECORD OF DRILLHOLE: 10-3

SHEET 2 OF 2

LOCATION: See Site Plan INCLINATION: -90°

AZIMUTH: ---

DRILLING DATE: Apr. 28-29, 2010

DRILL RIG: CME 55

FR/FX-FRACTURE F-FAULT

DRILLING CONTRACTOR: Marathon Drilling

SM-SMOOTH

FL-FLEXURED

DATUM:

CL-CLEAVAGE UE-UNEVEN MB-MECH BREAK J-JOHT B-ROUGH DRILLING RECOR DEPTH SCALE METRES SH-SHEAH P-POLISHED ST-STEPPED M-MVAA B-BEDDING RUN No ELEV. WATER LEVELS INSTRUMENTATION VN-VEIN S-SLICKENSIDED PL-PLANAR C-CURVED DESCRIPTION DISCONTINUITY DATA DEPTH HYDRAULIG (m) DP will CORE AND K, cm/sec 8880 BEDROCK SURFACE 90.33 3.88 Very thinly to medium bodded light grey interbodded SANDSTONE and DOLOSTONE BEDROCK Jemonite Seal 32mm Diant PVC #10 Slot Screen 'A' 67 00 End of Borehole W.L. in screen 'A' at Elev. 93.77m on Apr. 30, 2010 W.L. an screen '8' at Elev. 93 17m on Apr. 30, 2010 10 15 0811220078-9500 (ROCK) GPJ GAL-MISS.GDT 6/3/10 12 13 MIS-RCK 001

DEPTH SCALE

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LOGGED: J.D CHECKED:

# The Ontoria Water Resources Act WATER WELL RECORD

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# The Onlario Water Resources Act WATER WELL RECOR!

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The Ontaria Water Resources Act WATER WELL RECORD Environment Ontario IL PRINT ONLY IN SPACES PROVIDER
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# **ATTACHMENT 2**

**Drawdown and Recovery Plots** 

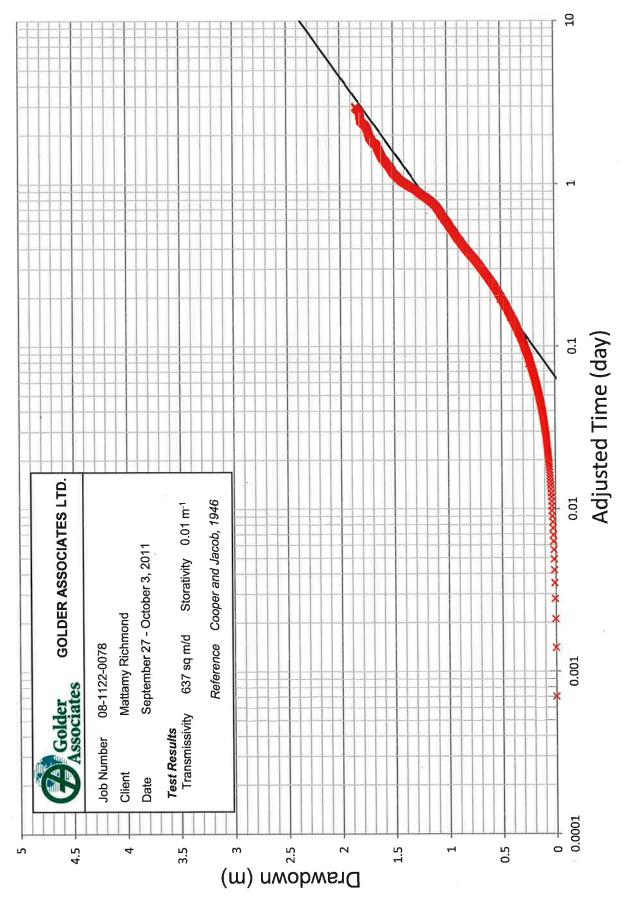


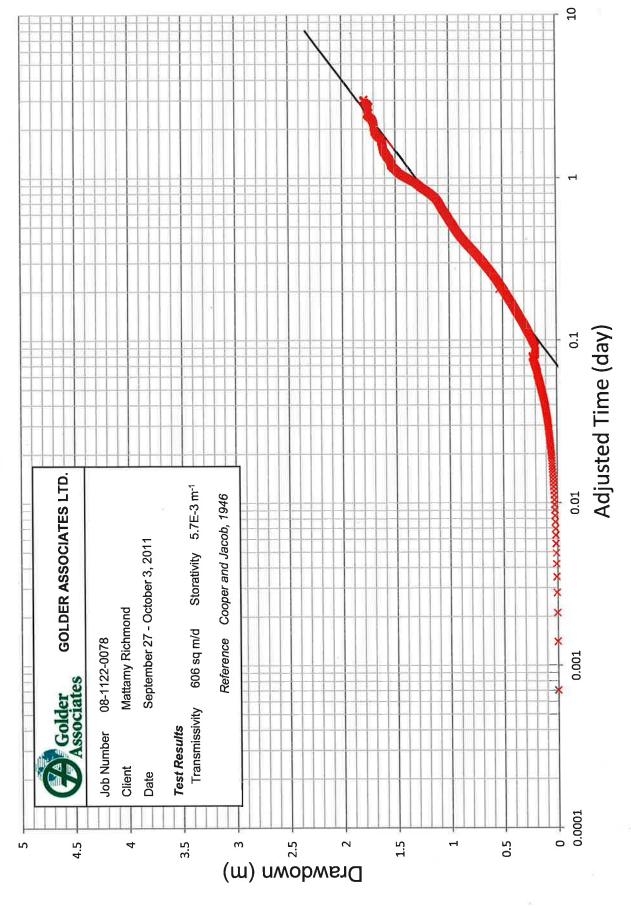
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**OW-3** 

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