

## Borrello Subdivision Infrastructure Servicing Brief

Prepared For:

3428 Woodroffe Avenue  
Mr. Antonino Borrello

Prepared By:

Robinson Land Development

Our Project No. 14057  
Revised February 2017

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## 1.0 INTRODUCTION

Robinson Land Development (a division of Robinson Consultants Inc.) has been retained by Mr. Antonino Borrello to provide the detailed engineering design for the water, storm and sanitary servicing for a 30 lot subdivision at 3400-3428 Woodroffe Avenue. The development area is tributary to the existing Strandherd Stormwater Management Facility. The location of the development is shown on **Figure 1**.

This development has been designed in accordance with current City of Ottawa design standards and the recommendations/guidelines stated in the following reports:

South Nepean Urban Master Servicing Study Report, July 1997, revised 1998, prepared by J.L. Richards & Associates.

Cumming Cockburn Ltd. (CCL) detailed serviceability study in 1998 for the Area tributary to the Strandherd Stormwater Management Facility.

Serviceability Report for Draft Plan of Subdivision, April 2004, revised June 2004, prepared by Cecil D. Naraine Associates Limited.

## 2.0 WATERMAIN DISTRIBUTION

The lands will be serviced from the Barrhaven (BAR) high-pressure zone. Boundary conditions for the water distribution system were compared to existing models performed on the surrounding networks and confirmed with the City of Ottawa. Refer to the Watermain Hydraulic Analysis Report prepared by Robinson Land Development dated April 2015 for detailed analysis on the water supply network.

The existing water supply system in the vicinity of this development consists of a 305 mm diameter watermain along Woodroffe Avenue and a 203mm diameter on Stoneleigh Street.

It is proposed to service the site with a 203mm diameter watermain connecting to the existing City of Ottawa watermain infrastructure at the intersection of Woodroffe Avenue and Stoneleigh Street.

## 3.0 SANITARY SEWER DESIGN

Sanitary sewer flows for this proposed development have been calculated based on the current 2012 City of Ottawa's "Sewer Design Guidelines. The design criteria for this development are as follows:

- |  |                               |
|--|-------------------------------|
| • Average residential flow   | 350 Lcap/day                  |
| • Peaking factor for residential flow (Harmon formula)               | $(1 + (14 / (4 + P1/2))) * k$ |
| • (max. = 4.0, min. = 2.0, k = 0.4 to 0.6, P = population in 1000's) |                               |
| • Extraneous flow allowance  | 0.28 L/sec/ha                 |
| • Population density for single family units                         | 3.4                           |
| persons/unit   |                               |
| • Population density for town-home units                             | 2.7                           |
| persons/unit   |                               |



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scale N.T.S.	CLIENT: BORRELLO SUBDIVISION	project no. 14057
date 22/05/15	TITLE:	
drawn by JHB	KEY PLAN	FIG 1.0

• Undeveloped land persons/gross ha.	60
• Minimum full flow velocity	0.6 m/sec
• Maximum velocity	3.0 m/sec
• Minimum pipe size	200 mm
• If 10 or fewer units are tributary to a sewer, than a 200 mm diameter sewer at a minimum grade of 0.65% shall be used.	
• Manhole spacing	< 120 metres
• Minimum cover to pipe obvert	2.5 metres

The sanitary sewer network for the subdivision will be 200mm diameter. The maximum peak sanitary discharge from the development area is expected to be approximately 1.78 L/s. Sanitary and storm stubs to the subdivision were installed in 2014 when the main line sewers were being installed on Woodroffe Avenue. Refer to the as built drawing in Appendix A.

During the design of the Woodroffe Avenue and Stoneleigh Street sanitary sewers there was no allocation for the proposed Borrello Development Property. The majority of the sanitary flow from the development will be directed to the existing sanitary system on Stoneleigh Street. This will increase the flow on the existing sanitary sewer by 1.78 L/s. There are 8 new connections to the existing sanitary sewer on Woodroffe Avenue. The new connections will increase the sanitary flow 0.58 L/s. The existing sanitary sewer system has been analysed downstream of the proposed connections and illustrates that there is excess capacity to convey the increased flows. Refer to Appendix B for the sanitary design sheet and the Sanitary Drainage Area Plan.

#### **4.0 STORM AND STORMWATER MANAGEMENT**

This development has been designed using the dual drainage concept providing a storm sewer system (minor) and utilizing overland flow (major) routes. The minor system drains to the Strandherd Stormwater Management Facility on Prince of Wales Drive.

The minor system has been designed using the rational method, to convey frequent storm events up to the 1:5 year return period. Inflow into the minor system has been restricted using inlet control devices (ICD's) located in all catchbasins that are directly connected to the storm sewer system. The ICDs will restrict inflow to the system to a maximum of 70 L/sec/ha.

The existing minor system on Woodroffe Avenue was designed to accommodate this development. The Woodroffe Avenue minor system design accounted for a drainage area of 2.48 ha (which included the 2.36 ha Borrello Property) for pipe run 201 to 202 which resulted in a peak flow of 242.17 L/s. The detailed design of the Borrello Property will now attribute a 2.58 ha drainage area at a peak flow of 229.49 L/s. Therefore, the proposed flows from the Borrello Development are approximately 13 L/s less than what was assumed in the Woodroffe Avenue minor system design.

The existing Strandherd Stormwater Management Facility was originally not sized to include the minor drainage area flows from the Borrello property, however the overall drainage area used to design and construct the facility was 315 ha (refer to documentation obtained from the Strandherd Stormwater Facility Design Report by CG&S CH2M & Gore & Storrie Limited dated February 1998 in Appendix C). Since the construction of the pond, the former City of Nepean required a more detailed analysis of the drainage area based on future road

patterns. The outcome of this study resulted in the reduction of the total drainage area contributing to the Strandherd Stormwater Management Facility to 300ha. As a result of the reduction of 15 ha in the total drainage there is sufficient capacity in the SWM pond to receive the minor flows from the Borrello lands of approximately 1.5 ha. Documentation from the Cecil D. Naraine Serviceability Report and Cumming Cockburn Ltd. (CCL) detailed serviceability study in 1998 for the Area tributary to the Strandherd Stormwater Management Facility has been included in Appendix C.

The Strandherd Stormwater Facility was also designed based on an imperviousness of 55% for the entire drainage area of 315 ha. The average percent imperviousness for the proposed Borrello property is 41% which therefore meets the requirements the stormwater pond was designed for.

Major overland flow has been routed to drain along the municipal roadways. The roadways have been designed to allow ponding in road sags to a maximum depth of 0.30 m on the local streets. Rear yard swales have been designed to allow ponding to a maximum depth of 0.30m. The drainage system for the proposed development was modelled using DDSWMM (v. 2.1) to determine the overland flow discharges from each sub-drainage area, and the total volume of runoff that will be directed along major overland routes.

#### **4.1    Storm Sewer Hydraulic Grade Line**

The local storm sewer system which outlets to the existing trunk storm sewers on Strandherd Drive have been designed to convey flows based on the City of Ottawa 5 year Intensity Frequency Duration curve. The hydraulic grade line will be contained within the local storm sewer system and will not be elevated above the storm invert. The proposed development drains to the Strandherd SWM Facility and is not affected by the HGL elevation from the SWM Facility.

#### **4.2    Allowable Direct Connection Catchbasins**

The Borrello subdivision is approximately 2.36 hectares. The trunk storm sewer systems are designed to convey minor system flows to the Strandherd Stormwater Management Facility. The existing trunk storm sewer flows along Strandherd Drive, Crestway Drive, Hathaway Drive, Cresthaven Drive, Sunvale Drive, Fairpark Drive and then to the Strandherd Stormwater Management Facility for treatment prior to discharge to the Rideau River.

In accordance with the South Nepean Urban Area Study, storm drainage is to be controlled at the source to limit runoff rates to 70 L/s/ha.

$$70 \text{ L/s/ha} \times 2.36 \text{ ha} \approx 165.2 \text{ L/s}$$

Table 1.0 summarizes the number of proposed catchbasins directly connected to the storm sewer system and release rate in the Borrello Subdivision:

**Table 1.0**  
**Number of Directly Connected Catchbasins and Release Rate**

Location	100 Year Release Rate (L/s)	Max. Head 100 yr (m)	Orifice Diam. (mm)	Orifice Type
CB 1	20.0	1.21	93.3	Plug
CB 2	14.2	1.23	78.3	Plug
CB 3	31.0	1.23	115.7	Plug
DCB 4	20.0	1.10	95.6	Plug
DCB 5	20.0	1.23	92.9	Plug
CB 6	25.0	1.40	100.6	Plug
CB 7	15.0	0.98	85.3	Plug
CB 8	20.0	1.30	91.7	Plug

There are 8 catchbasin connections to the minor system proposed within this development with a total release rate to the minor system of 165.2 L/s.

#### **4.3 Post-Development Average 'C' Value**

The following runoff coefficients used to design the storm sewer system were calculated based on each individual storm area.

C = 0.20 for grassed areas

C = 0.90 for asphalt, sidewalk and roof areas

The runoff coefficient for each storm drainage area has been calculated individually. The runoff coefficient varies from 0.34 to 0.67. The overall average runoff coefficient for the entire site is 0.48. Refer to the storm sewer design sheet for individual runoff coefficients.

#### **4.5 Storage Requirements**

##### **4.5.1 Overall Storage Requirements**

The City of Ottawa has developed design standards for the South Nepean Area that determined an average storage volume of 130 m<sup>3</sup>/ha was necessary to prevent individual sub-drainage areas from flowing overland up to the 100-year design storm. This was identified in the 1998 CCL serviceability study. Using the storage requirement of 130 m<sup>3</sup>/ha, provided by the City of Ottawa for the South Nepean Area, (refer to Appendix C for documentation) the overall storage requirement to prevent major system overland flow from the Borrello Subdivision is:

$$2.36 \text{ ha} \times 130 \text{ m}^3/\text{ha} = 306.8 \text{ m}^3$$

The storage requirement for certain drainage areas is greater than the available storage capacity. Therefore, some areas will flow overland. The development has been designed to provide an overland drainage flow route along the municipal road to the existing ditch on the west side of Woodroffe Avenue, which ultimately discharges into the Rideau River.

A total of 85.4 m<sup>3</sup> of storage is available within the subdivision roadway sags and rear yard subdrain system. Storage in rear yard swales has not been included in accordance with the City's Sewer Design Guidelines.

Flows in excess of the provided volume will overland flow to both Woodroffe Avenue and to the rear of Lots 12-15. The post development contributing area to the existing ditch and culverts on Woodroffe Avenue has been reduced by 0.94 ha from the pre-development conditions. Refer to the Storm Drainage Area Plan STM2 and the Woodroffe Culvert Capacities in Appendix C.

The post development contributing area to the rear of Lots 12-15 has been reduced from the pre-development conditions. Refer to Figure 2 and Figure 3 for the pre and post 5 and 100 year flows. The overland flow will be directed to the rear yard swales which will retain, via surface ponding, all flows up to and including the 100 year storm event. The 100 year storage requirement is 56.6cu.m. which has been calculated using the rational method. The storage provided in the rear yard swale is 57.0cu.m. Refer to the storage requirement in Appendix C. Storms in excess of the 100 year event will outlet at 3 different locations to the lot lines of the existing residential area to the west and directed into existing grass swales to the existing ditch on Newland Drive. Refer to Figure 4 for overland flow locations.

The drainage system has been modelled using City approved DDSWMM (ver. 2.1) software to determine the overland flow discharges from each sub-drainage area, and the total volume of runoff that will be directed along major overland routes. The Chicago 3 Hour – 100 Year storm has been used in the analysis. The main design parameters used in the DDSWMM modelling software (as derived from Section 5 of the Sewer Design Guidelines) are:

Depression storage:	1.57 mm for impervious areas 4.67 mm for pervious areas
Manning's roughness coefficient	0.013 (for impervious areas) 0.25 (for pervious areas)
Sub-area Width (width parameter)	2 x Street Segment Length
Infiltration Parameters	Max. Infiltration – 76.2 mm/hr Min. Infiltration – 13.2 mm/hr
Decay Coefficient (t-1)	0.00115 s-1

The following tables summarize the anticipated peak flows and depth of flow at the curb line for the 100 year storm event. Please refer to Appendix C for the DDSWMM modelling output. The major drainage area I.D. numbers are referenced on drawing 14057-SWM1 in Appendix C.

**Table 2 – DDSWMM Summary of Results**

Drawing #	Drainage Area I.D.	100 Yr Peak Flow (cms)	100 Yr Static Depth (cm)	100 Yr Dynamic Depth (cm)	100 Yr Total Depth (cm)
SWM1	SWM13	0.02	11.0	7.72	18.72
	SWM11	0.03	11.0	8.95	19.95
	SWM8	0.06	13.0	11.36	24.36
	SWM3	0.10	13.0	14.05	27.05
	SWM7	0.08	0.0	4.57	4.57
	SWM1	0.14	13.0	15.73	28.73

**Table 3 – DDSWMM Summary of Results with 20% Stress Test**

Drawing #	Drainage Area I.D.	100 Yr Peak Flow (cms)	100 Yr Static Depth (cm)	100 Yr Dynamic Depth (cm)	100 Yr Total Depth (cm)
SWM1	SWM13	0.03	11.0	8.30	19.30
	SWM11	0.05	11.0	10.34	21.34
	SWM8	0.09	13.0	13.32	26.32
	SWM3	0.14	13.0	15.92	28.92
	SWM7	0.11	0.0	5.17	5.17
	SWM1	0.20	13.0	18.15	31.15

#### **4.5.2 Analysis of Existing Downstream Culverts**

The Borrello Subdivision outlets to an existing ditch system on the west side of the existing Woodroffe Avenue before flowing into the Rideau River on the south side of Prince of Wales Drive. As part of the supporting design analysis for the subdivision, the existing culverts were analysed to ensure that they would continue to provide the required (as per current City of Ottawa Guidelines, Table 6.4 Road Type vs. Culvert Design Storm) level of service (LOS) once the Borrello Subdivision is developed. The required level of service was based on the road type and design storm. All existing culverts will continue to meet the required LOS as per City of Ottawa design guidelines. All existing driveways were analysed based on a 5 year design storm even though driveways do not fall under the Table 6.4 classification. The road cross culverts at Bren Maur Road, Cortleigh Drive, Woodroffe Avenue and Lodge Road have been analysed based on a 25 year design storm and the culvert crossing Prince of Wales Drive has been analysed based on a 50 year design storm. The existing ditch on the west side of Woodroffe Avenue has been analysed for the 100 year post development flow at 3 locations for the impact on the existing residents downstream of the development. The 100 year flows indicated on the cross sections in Appendix C illustrate that the flows are contained within the roadside ditch on Woodroffe Avenue.

See summary Table 4 below and Appendix C for the culvert analyses supporting documentation and drawing #14057-STM2)

**Table 4 – Level of Service (LOS) Analysis for existing Woodroffe Avenue Culverts**

Culvert #	LOS required (year)	Min. Available freeboard (m)
1	5	0.67
2	5	0.45
3	5	0.67
4	25	0.47
5	5	0.44
6	5	0.38
7	5	0.60
8	5	0.43
9	25	0.40
10	25	0.57
11	50	2.03
12	50	1.10

## 5.0 EROSION AND SEDIMENT CONTROL

It will be necessary to implement the following sediment control measures, in accordance with current Ministry of Environment and Climate Change, Best Management Practice guidelines, in order to minimize the transport of sediment to adjacent lands and into the existing storm sewer system. (see Appendix A, 14057-ESC1 for details of the proposed control measures).

As a minimum, the following measures are proposed for this development:

- Installation of straw bale dams within existing drainage ditches
- Silt fence along property boundaries where construction is taking place
- Filter fabric installed between the frame and cover of adjacent manholes and catchbasins
- Minimization, wherever possible, of exposed soils and cleared areas
- Soil stockpiles to be located away from any existing drainage ways and stabilized as soon as possible

These measures will be installed prior to construction and maintained in good order until construction has been completed and vegetation has been re-established in all disturbed areas.

## 6.0 CONCLUSION

The Borrello Subdivision has been designed to direct the 1:100-year overland flow along the municipal roadway to the existing ditch on the west side of Woodroffe Avenue, ultimately to the Rideau River. The overland flow routes are shown on the drawings in Appendix A.

This report satisfactorily addresses the method by which this site will meet the overall stormwater management requirements of the City of Ottawa. Inlet control devices are to be placed in all direct connection catchbasins. Their release rates range from 14.2 to 31.0 L/s for a total release rate from the minor system of 165.2 L/s. The recommended inlet control device is the Tempest MHF (Plug Type), (see Appendix C). The ICD is to be installed in the outlet pipe of all catchbasins directly connected to the storm sewer system. Using 3.5 catchbasins/hectare, and considering the entire area encompassed by the Borrello Subdivision, a total drainage area of 2.36 hectares, there can be a maximum of 8 catchbasins directly connected to the storm sewer system. The proposed design requires 8 catchbasins directly connected to the storm sewer system.

All storm sewers have been designed for a post-development 1:5-year storm event, which meets the current level of service for urban residential development. The storm sewer system will provide the usual 5-year level of service if the City of Ottawa considers it appropriate to remove the inlet control devices at some point in the future.

The design has incorporated current City of Ottawa design standards.

In conclusion, sufficient capacity within the existing water, sanitary and storm municipal infrastructure exists to support the proposed subdivision development.

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Reviewed By:

Sean M. Czaharynski, P.Eng.  
Manager – Land Development

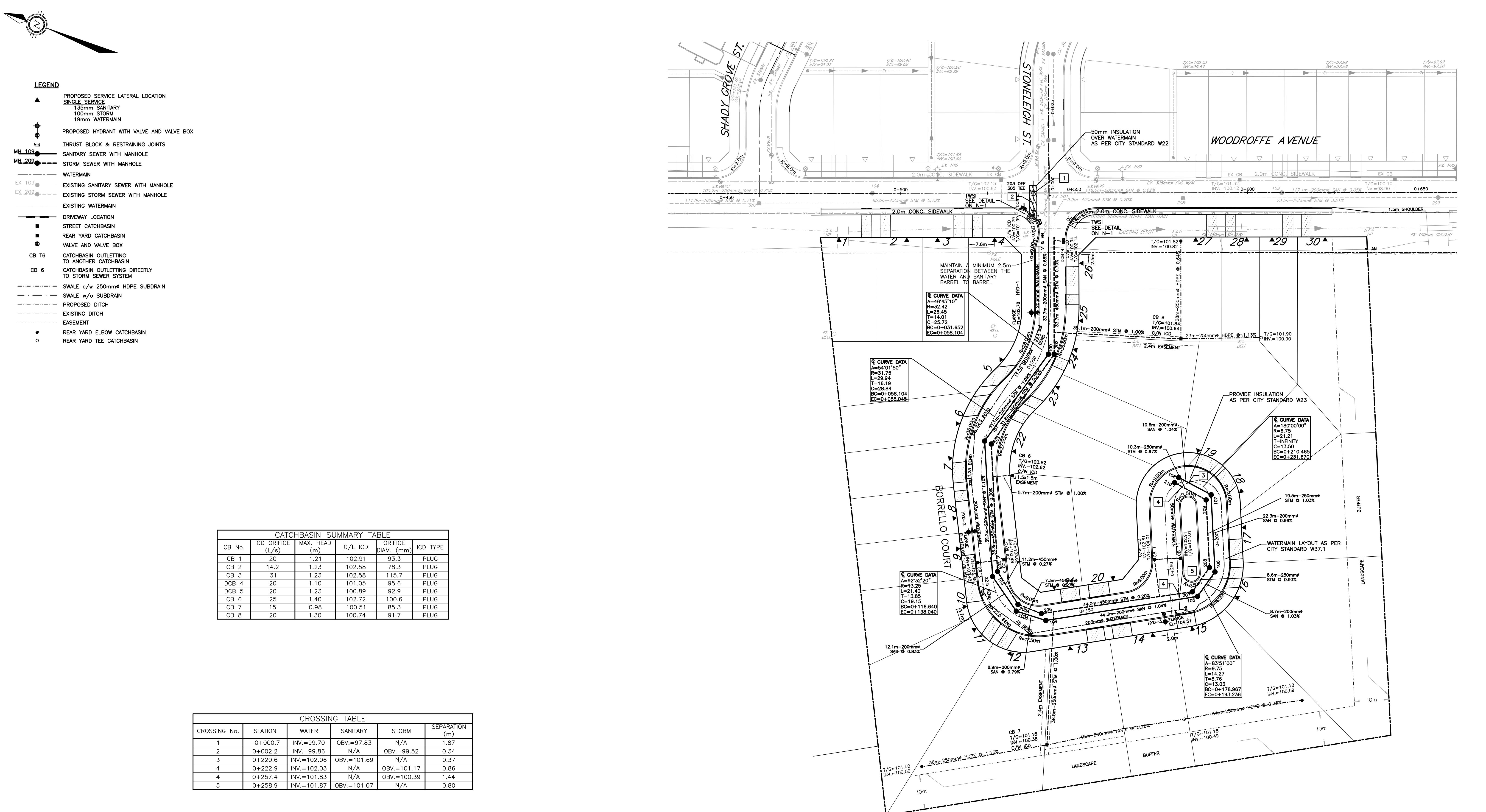
## Appendix A

General Plan of Services  
(Drawing #14057-S1)

Grading and Drainage Plan  
(Drawing #14057-GR1)

Erosion and Sediment Control Plan  
(Drawing #14057-ESC1)

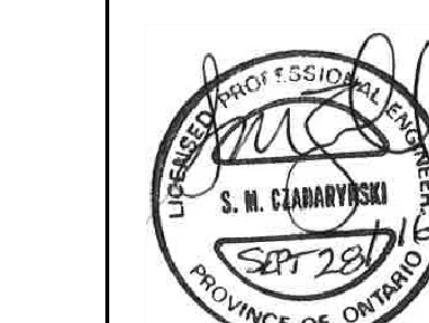
Sanitary and Storm Subdivision As  
Built Stubs



NOTES  
THE POSITION OF ALL POLE LINES, CONDUITS, WATERMAINS, SEWERS AND OTHER UNDERGROUND AND OVERGROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE CONTRACT DRAWINGS. THE OWNER'S ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED. BEFORE STARTING WORK, DETERMINE THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES AND ASSUME ALL LIABILITY FOR DAMAGE TO THEM.

NO.	REVISION DESCRIPTION	DATE	BY
4	REVISED PER CITY COMMENTS	28/09/16	SMC
3	REVISED PER CITY COMMENTS	17/06/16	SMC
2	REVISED PER CITY COMMENTS	10/12/15	SMC
1	ISSUED FOR REVIEW	25/05/15	SMC

SCALE
HORIZ. 1:500



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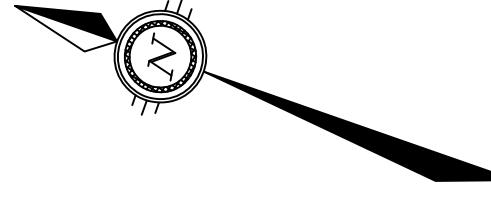
350 PALLADIUM DRIVE  
KANATA, ONTARIO K2V 1A8  
TELEPHONE (613) 592-6060

**BORRELLO SUBDIVISION**  
**514 KOCHAR DRIVE**  
**OTTAWA, ON**  
**K2C 4H3**

DESIGN	JHB
CHECKED	SMC
DRAWN	JHB
CHECKED	SMC
APPROVED	SMC

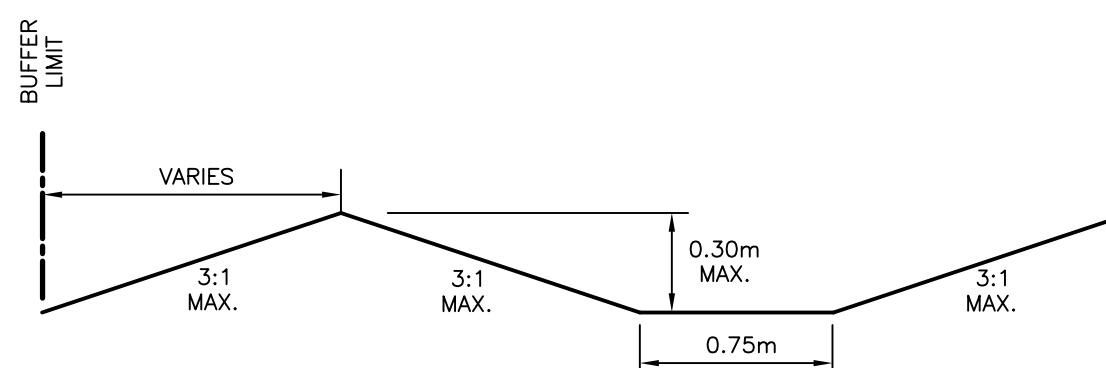
PROJECT NO.  
14057  
SURVEY  
RLD  
DATED  
MAY 2015  
DWG. NO.  
14057-S1

**GENERAL PLAN OF SERVICES**

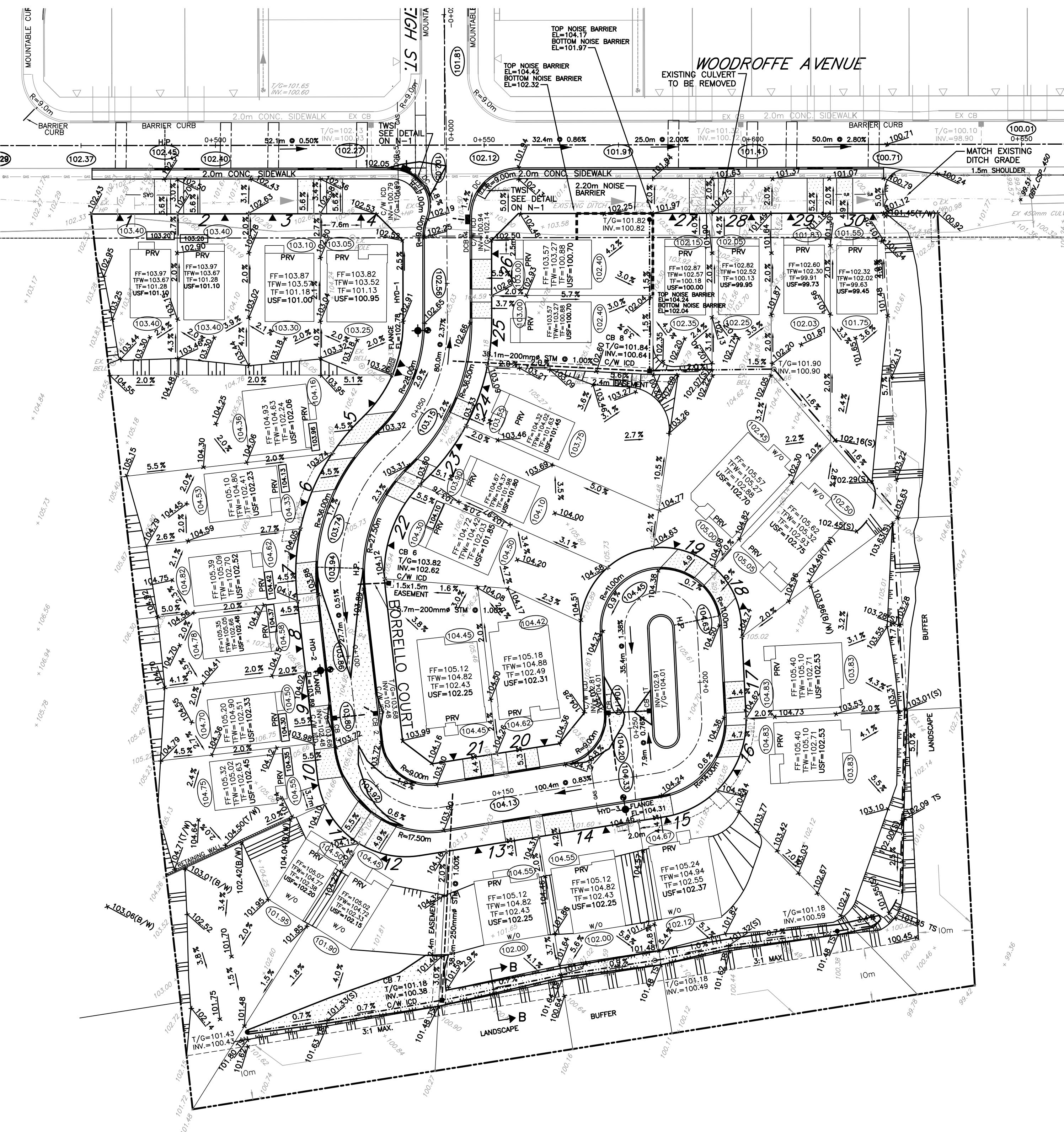


**LEGEND**

- ▲ PROPOSED SERVICE LATERAL LOCATION
- SINGLE SERVICE  
135mm SANITARY  
100mm STORM  
19mm WATERMAIN
- DRIVEWAY LOCATION
- STREET CATCHBASIN
- REAR YARD CATCHBASIN
- CB T6 CATCHBASIN OUTLETING TO ANOTHER CATCHBASIN
- CB 6 CATCHBASIN OUTLETING DIRECTLY TO STORM SEWER SYSTEM
- SWALE c/w SUBDRAIN
- - SWALE w/o SUBDRAIN
- PROPOSED DITCH
- - EXISTING DITCH
- - EASEMENT
- TERRACING
- REAR YARD ELBOW CATCHBASIN
- REAR YARD TEE CATCHBASIN
- PROPOSED TERRACE GRADE OR CENTRELINE ROAD GRADE
- PROPOSED DRIVEWAY GRADE AT GARAGE
- PROPOSED GRADE
- EXISTING ELEVATION
- DRAINAGE DIRECTION AND SLOPE
- PRESSURE REDUCING VALVE REQUIRED
- PONDING AREA



SECTION B-B  
N.T.S.



NOTES  
THE POSITION OF ALL POLE LINES, CONDUITS, WATERMAINS, SEWERS AND OTHER UNDERGROUND AND OVERGROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE DRAWINGS AND WHILE GREAT CARE IS TAKEN IN THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED. BEFORE STARTING WORK, DETERMINE THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES AND ASSUME ALL LIABILITY FOR DAMAGE TO THEM.

7	ISSUED FOR TENDER	15/09/17	SMC	SCALE	HORIZ. 1:500
6	ISSUED FOR ECA APPROVAL	23/06/17	SMC		
5	REVISED PER CITY COMMENTS	21/02/17	SMC		
4	REVISED PER CITY COMMENTS	28/09/16	SMC		
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1	ISSUED FOR REVIEW	25/05/15	SMC		
NO.	REVISION DESCRIPTION	DATE	BY		

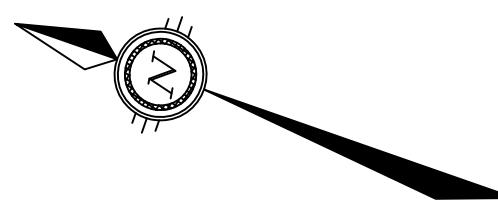
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BORRELLO SUBDIVISION  
514 KOCHAR DRIVE  
OTTAWA, ON  
K2C 4H3

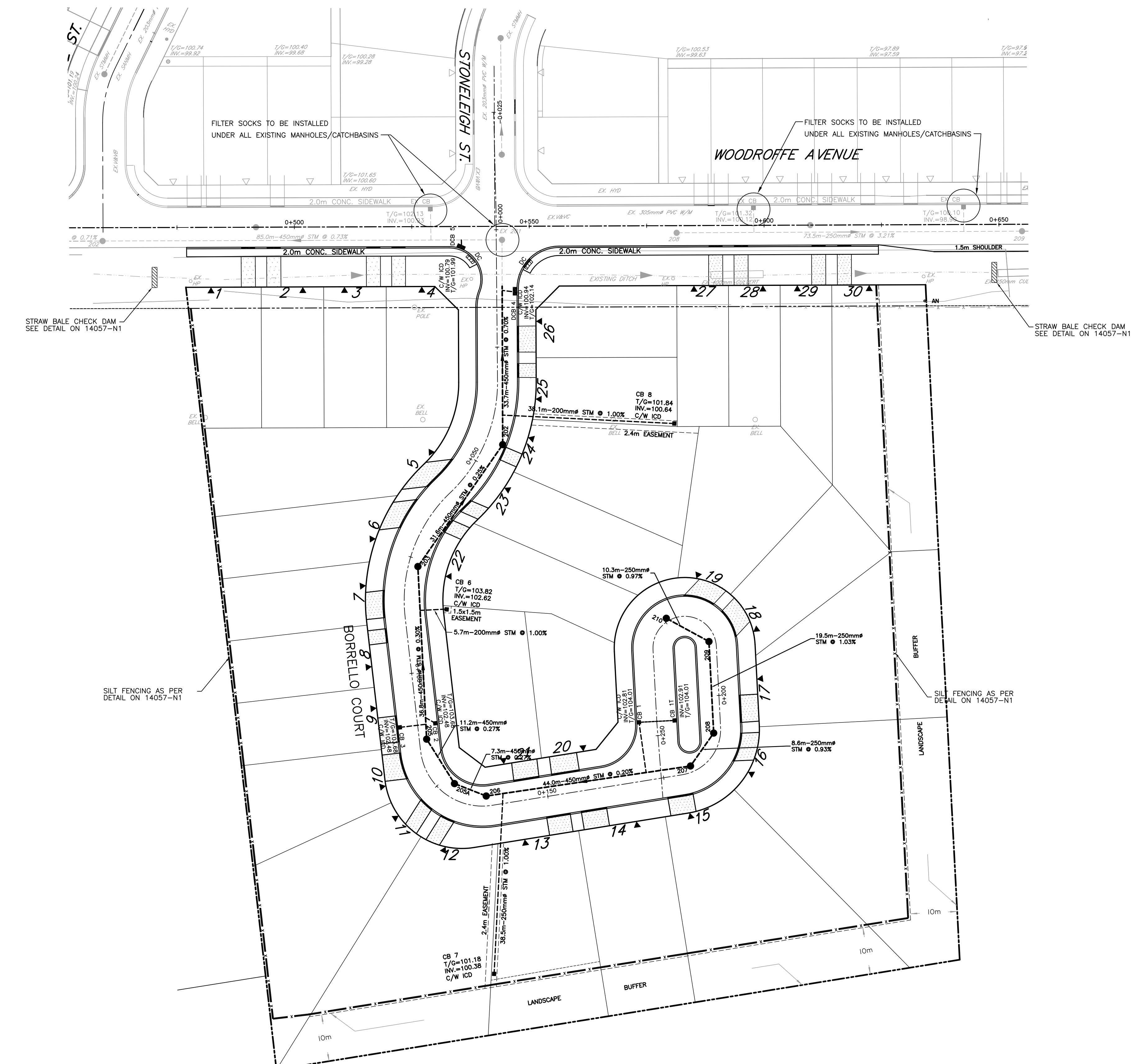
GRADING AND DRAINAGE PLAN

PROJECT NO.  
14057  
SURVEY  
RLD  
DATED  
MAY 2015  
DWG. NO:  
14057-GR1



## LEGEND

- EXISTING STORM SEWER
- EXISTING DITCH
- STORM SEWER
- STORM MANHOLE
- CB
- SILT FENCE
- STRAW BALE CHECK DAM



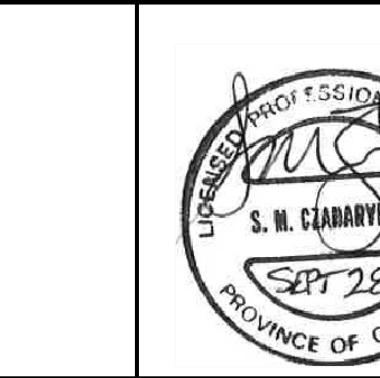
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1	ISSUED FOR CLIENT REVIEW	25/05/15	SMC

SCALE

HORIZ. 1:500

0 5m 10m 20m



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DESIGN JHB

CHECKED SMC

DRAWN JHB

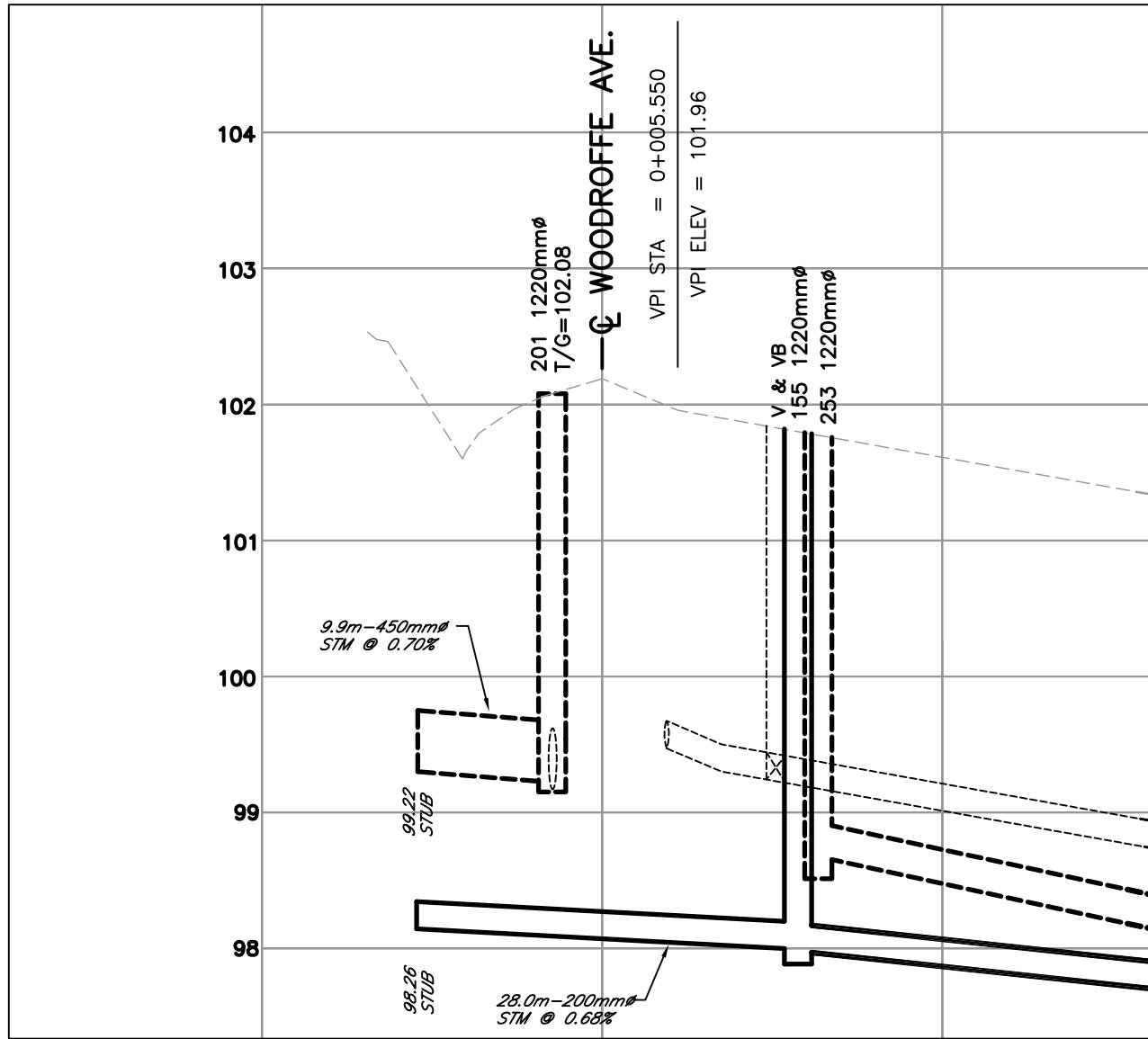
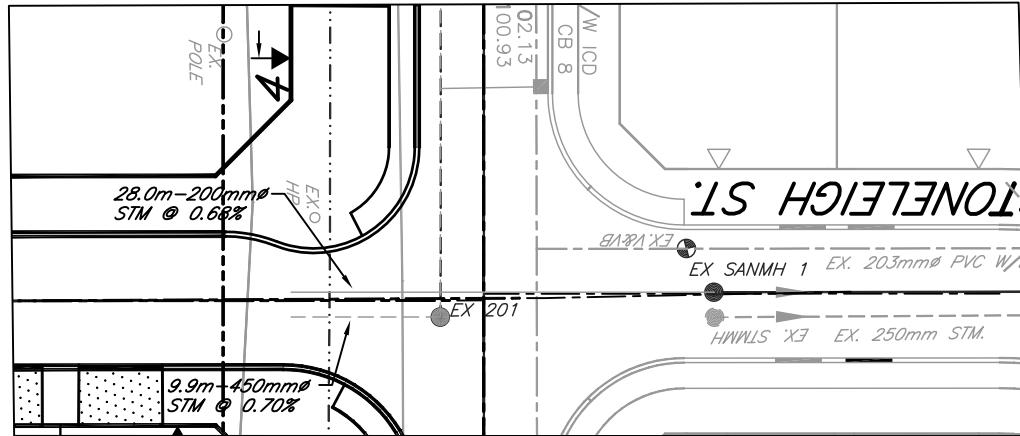
CHECKED SMC

APPROVED SMC

**BORRELLO SUBDIVISION**  
514 KOCHAR DRIVE  
OTTAWA, ON  
K2C 4H3

EROSION AND SEDIMENT  
CONTROL PLAN

PROJECT NO.  
14057  
SURVEY  
RLD  
DATED  
MAY 2015  
DWG. NO:  
14057-EC1



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Land Development

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scale 1:500	CLIENT: BORRELLO PROPERTY	project no. 14057
date 13/11/14		
drawn by JHB	TITLE: SUBDIVISION SERVICES	P1

## Appendix B

Sanitary Sewer Design Sheet  
Sanitary Drainage Area Plan  
(Drawing #14057-SAN1)

SANITARY SEWER DESIGN SHEET  
for  
Borrello Subdivision

LOCATION			PROPOSED		EXISTING		CUMMULATIVE		PEAKING	PEAK	PEAK	PROPOSED SEWER DATA					EXCESS	
STREET	FROM	TO	POP.	AREA	POP.	AREA	POP.	AREA	FACTOR	POP.	EXTRAN.	DESIGN	LENGTH	PIPE	GRADE	CAPACITY	VELOCITY	CAPACITY
	MH	MH		(ha)		(ha)		(ha)	M	FLOW (L/s)	FLOW (L/s)	FLOW (L/s)	(m)	SIZE (mm)	(%)	(L/s)	(m/s)	(L/s)
Borrello Court	108	107	3.40	0.1			3.40	0.10	4.00	0.06	0.03	0.08	10.60	203.2	1.04	34.93	1.08	34.85
Borrello Court	107	106	6.80	0.23			10.20	0.33	4.00	0.17	0.09	0.26	22.30	203.2	0.99	34.08	1.05	33.82
Borrello Court	106	105	3.40	0.19			13.60	0.52	4.00	0.22	0.15	0.37	8.70	203.2	1.03	34.76	1.07	34.40
Borrello Court	105	104	17.00	0.47			30.60	0.99	4.00	0.50	0.28	0.77	44.30	203.2	1.04	34.93	1.08	34.16
Borrello Court	104	103A	3.40	0.15			34.00	1.14	4.00	0.55	0.32	0.87	11.50	203.2	0.61	26.75	0.82	25.88
Borrello Court	103A	103	6.80	0.16			40.80	1.30	4.00	0.66	0.36	1.03	9.60	203.2	1.04	34.93	1.08	33.90
Borrello Court	103	101	13.60	0.24			54.40	1.54	4.00	0.88	0.43	1.31	39.20	203.2	1.10	35.92	1.11	34.61
Borrello Court	101	100	10.20	0.22			64.60	1.76	4.00	1.05	0.49	1.54	31.10	203.2	1.09	35.76	1.10	34.22
Borrello Court	100	EX 155	10.20	0.26			74.80	2.02	4.00	1.21	0.57	1.78	61.70	203.2	0.68	28.24	0.87	26.47
Stoneleigh Street	EX 155	EX 145			18.70	0.24	93.50	2.26	4.00	1.52	0.63	2.15	25.00	203.2	1.60	43.32	1.34	41.18
Stoneleigh Street	EX 145	EX 146			66.50	0.67	160.00	2.93	4.00	2.59	0.82	3.41	96.00	203.2	1.75	45.31	1.40	41.90
Shady Grove Street	EX 146	EX 148			143.50	1.45	303.50	4.38	4.00	4.92	1.23	6.14	72.30	203.2	0.89	32.31	1.00	26.17
Marabrooke Street	EX 148	EX 149			35.00	0.43	338.50	4.81	4.00	5.48	1.35	6.83	46.60	203.2	1.14	36.57	1.13	29.74
Marabrooke Street	EX 149	EX 150			10.50	0.25	349.00	5.06	4.00	5.66	1.42	7.07	11.80	203.2	1.44	41.10	1.27	34.03
Marabrooke Street	EX 150	EX 151			38.50	0.37	387.50	5.43	4.00	6.28	1.52	7.80	68.80	203.2	1.51	42.09	1.30	34.29
Woodroffe Ave.	EX 105	EX 104	3.40	0.04	23.80	0.49	27.20	0.53	4.00	0.44	0.15	0.59	100.20	203.2	0.70	28.66	0.88	28.07
Woodroffe Ave.	EX 104	EX 103	20.40	0.36	13.60	0.21	61.20	1.10	4.00	0.99	0.31	1.30	118.00	203.2	0.62	26.97	0.83	25.67
Woodroffe Ave.	EX 103	EX 141	3.40	0.11	27.20	0.50	91.80	1.71	4.00	1.49	0.48	1.97	117.10	203.2	3.05	59.82	1.84	57.85
Whitewater Dr.	EX 141	EX 151			15.20	0.26	107.00	1.97	4.00	1.73	0.55	2.29	71.30	203.2	1.11	36.09	1.11	33.80
Whitewater Dr.	EX 151	EX 152			8.10	0.14	502.60	7.54	3.97	8.09	2.11	10.20	56.40	203.2	0.55	25.40	0.78	15.20



## Appendix C

Storm Sewer Design Sheet  
Woodroffe Avenue Approved Storm  
Sewer Design Sheet  
Storm Drainage Area Plan  
(Drawing #14057-STM1,STM2)  
Stormwater Management Plan  
(Drawing #14057-SWM1)  
100 Year DDSWMM Computer  
Modelling – Input and Output  
100 Year DDSWMM 20% Stress Test  
Computer Modelling – Input and Output  
DDSWM 20% Stress Test Sketch  
Tempest MHF  
Storage Volume Requirements from  
CCL Report  
Documentation from CG&S Strandherd  
Stormwater Facility Design Brief  
South Nepean Urban Area Tributary to  
the Strandherd Stormwater Facility  
Documentation from Cecil D. Naraine  
Report  
Documentation from City of Ottawa  
Sewer Design Guidelines (Culvert  
Design)  
Woodroffe Ave. Ditch Pre-Development  
Woodroffe Ave. Ditch Post-Development  
Woodroffe Ave. Culvert Capacities  
Pre Development Drainage Area West  
Post Development Drainage Area West  
Lots 11-16 Overland Flow Direction

**STORM SEWER DESIGN SHEET**  
for  
**Borrello Subdivision**

LOCATION				AREA (ha)						INDIV. 2.78AR	ACCUM. 2.78AR	TIME OF CONC. (min.)	RAINFALL INTENSITY I	PEAK FLOW Q (L/s)	PROPOSED SEWER						%FULL	
STREET	FROM MH	TO MH	TOTAL AREA	R= 0.2	R= 0.9	R= 0.5	R= 0.52	R= 0.6	RUNOFF C						PIPE SIZE (mm)	GRADE (%)	LENGTH (m)	CAPACITY (L/s)	FULL FLOW VELOCITY (m/s)	TIME OF FLOW (min)		
Street A	210	209									0.00	10.00	104.19	0.00	254.0	0.97	10.3	61.16	1.21	0.14	0%	
Street A	209	208									0.00	10.14	103.45	0.00	254.0	1.03	19.5	63.03	1.24	0.26	0%	
Street A	208	207									0.00	10.40	102.11	0.00	254.0	0.93	8.6	59.89	1.18	0.12	0%	
REARYARD	RYCB 7	MAIN	0.49	0.40	0.09				0.33	0.45	0.45	15.00	83.56	37.40	254.0	1.00	38.5	62.10	1.23	0.52	60%	
Street A	207	206	0.21	0.09	0.12				0.60	0.35	0.80	10.52	101.50	80.98	457.2	0.20	44.0	133.15	0.81	0.90	61%	
Street A	206	205A									0.80	11.43	97.21	77.56	457.2	0.27	7.3	154.71	0.94	0.13	50%	
Street A	205A	205									0.80	11.56	96.63	77.09	457.2	0.27	11.2	154.71	0.94	0.20	50%	
SIDE YARD	RYCB 6	MAIN	0.1	0.07	0.03				0.41	0.11	0.11	15.00	83.56	9.52	203.2	1.00	5.7	34.25	1.06	0.09	28%	
Street A	205	203	0.36	0.19	0.17				0.53	0.53	1.44	11.76	95.75	138.15	457.2	0.30	36.8	163.08	0.99	0.62	85%	
Street A	203	202									1.44	12.37	93.13	134.37	457.2	0.25	31.6	148.87	0.91	0.58	90%	
REARYARD	RYCB 8	MAIN	0.22	0.16	0.06				0.39	0.24	0.24	15.00	83.56	19.98	203.2	1.00	38.1	34.25	1.06	0.60	58%	
Street A	202	EX201	0.16	0.10	0.07				0.48	0.22	1.90	12.95	90.81	172.48	457.2	0.70	43.6	249.10	1.52	0.48	69%	
Woodroffe Ave.	EX 201	EX 202	0.47				0.47				0.68	2.58	13.43	88.99	229.49	457.2	0.69	85.0	247.32	1.51	0.94	93%
Woodroffe Ave.	EX 202	EX 203	1.17			1.17					1.63	4.21	14.37	85.64	360.12	533.4	0.71	111.9	378.43	1.69	1.10	95%
Woodroffe Ave.	EX 203	EX 204									0.00	4.21	15.48	82.05	345.05	533.4	0.74	6.8	386.34	1.73	0.07	89%

Rainfall Intensity =  $998.071 / (T + 6.053)^{0.814}$    T= time in minutes  
(City of Ottawa, 5 year storm)

Peak Flow =

Accumulated 2.78AR x Rainfall Intensity

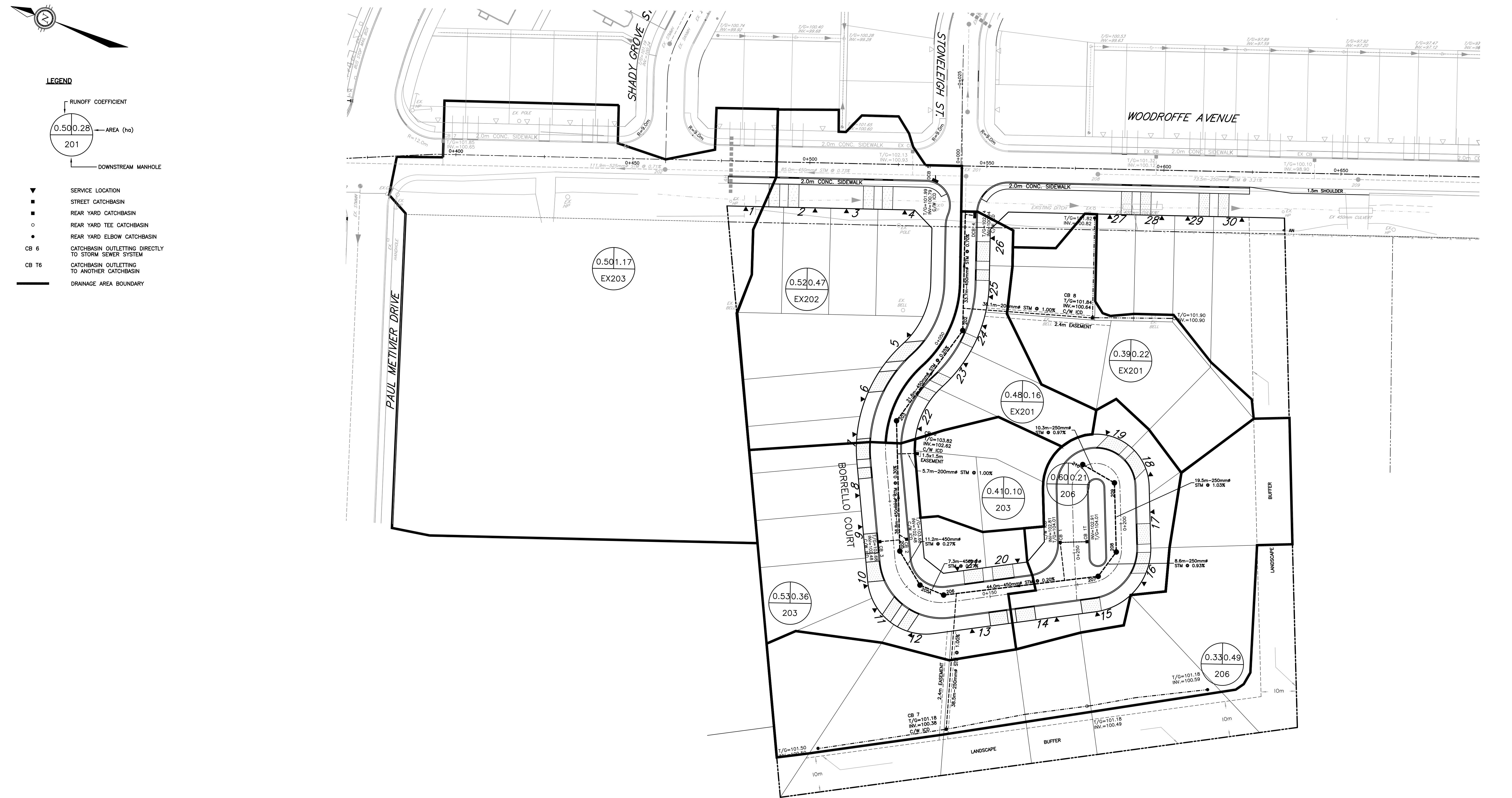
**STORM SEWER CALCULATIONS for  
Chapman Mills  
Woodroffe Avenue**

09/12/2015 2:18 PM

LOCATION					INDIV. 2.78AR	ACCUM. 2.78AR	TIME OF CONC.	RAINFALL INTENSITY I	PEAK FLOW Q (l/s)	PROPOSED SEWER					%FULL		
STREET	FROM MH	TO MH	R= 0.5	R= 0.6						PIPE SIZE (mm)	GRADE (%)	LENGTH (m)	CAPACITY (l/s)	FULL FLOW VELOCITY (m/s)	TIME OF FLOW (min)		
Woodroffe Ave.	201	202	2.48		3.45	3.45	26.00	59.35	204.57	457.2	0.69	85.0	247.32	1.51	0.94	83%	
Woodroffe Ave.	202	203	0.25	0.89	1.83	5.28	26.94	57.96	306.01	533.4	0.71	111.9	378.43	1.69	1.10	81%	
Woodroffe Ave.	203	204			0.00	0.00	5.28	28.04	297.94	533.4	0.74	6.8	386.34	1.73	0.07	77%	
Rear Yard Lead	EX CB	Main			0.18	0.30	0.30	83.56	25.09	203.2	1.00	18.0	34.25	1.06	0.28	73%	
Woodroffe Ave.	204	205			0.15	0.25	5.83	28.11	56.35	328.49	609.6	0.69	39.0	532.63	1.82	0.36	62%
Woodroffe Ave.	205	206			0.43	0.72	6.55	28.46	55.87	365.80	685.8	0.61	71.0	685.60	1.86	0.64	53%
Rear Yard Lead	EX CB	Main			0.51	0.85	0.85	83.56	71.08	254.0	2.00	18.5	87.82	1.73	0.18	81%	
Woodroffe Ave.	206	207			0.47	0.78	8.18	29.10	55.05	450.37	685.8	0.60	120.0	679.95	1.84	1.09	66%
Woodroffe Ave.	207	Ex. Stm MH 1				0.00	8.18	30.19	53.70	439.35	685.8	1.35	67.9	1019.93	2.76	0.41	43%
Woodroffe Ave.	Ex. Stm MH 1	Ex. Stm MH 2			0.00	17.57	30.60	53.21	935.04	762.0	0.89	32.1	1096.78	2.41	0.22	85%	

Run-off Coefficient = 0.6 for all areas, with the following exceptions; Peak Flow = Accumulated 2.78AR x Rainfall Intensity  
= 0.20 for Parkland

Rainfall Intensity =  $998.071 / (T + 6.053)^{0.814}$  T= time in minutes  
(City of Ottawa, 5 year storm)



**NOTES**

THE POSITION OF ALL POLE LINES, CONDUITS, WATERMAINS, SEWERS AND OTHER UNDERGROUND AND OVERGROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE CONTRACT DRAWINGS, AND WHERE SHOWN, THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED. BEFORE STARTING WORK, DETERMINE THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES AND ASSUME ALL LIABILITY FOR DAMAGE TO THEM.

**NOTES**

THE POSITION OF ALL POLE LINES, CONDUITS, WATERMAINS, SEWERS AND OTHER UNDERGROUND AND OVERGROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE CONTRACT DRAWINGS, AND WHERE SHOWN, THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED. BEFORE STARTING WORK, DETERMINE THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES AND ASSUME ALL LIABILITY FOR DAMAGE TO THEM.

TO THEM.

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4	REVISED PER
3	REVISED PER
2	REVISED PER
1	ISSUED

R	CITY COMMENTS
R	CITY COMMENTS
R	CITY COMMENTS
FOR REVIEW	

28/09/16	SMC	
17/06/16	SMC	
10/12/15	SMC	
25/05/15	SMC	

A scale bar diagram consisting of a horizontal line with three vertical tick marks. The first tick mark is labeled '0' below it. The second tick mark is labeled '5m' below it. The third tick mark is labeled '10m' below it. The distance between the first and second tick marks is labeled '5m'. The distance between the second and third tick marks is labeled '5m'. The total length from '0' to '10m' is labeled '10m'.

1000

A circular library stamp from the University of Michigan Library. The text "UNIVERSITY OF MICHIGAN LIBRARIES" is curved along the top edge. In the center, it says "PROFESSOR". At the bottom, it says "S. M. CZAJADA". To the right, there is a signature that appears to be "MUS". At the bottom right, it says "SEPT".

**Robins**  
Land Dev.

son  
elopment

350 PALLADIUM  
KANATA, ONTARIO  
TELEPHONE

UM DRIVE  
TARIO K2V 1A8  
(613) 592-6060

DESIGN	JHB
CHECKED	SMC
DRAWN	JHB
CHECKED	SMC

BOF

# **RRELLO SU 14 KOCHA OTTAWA**

# JBDIVISION

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N

STORM I

# DRAINAGE

# THE AREA PL

PRO  
SUR  
DATE  
DWG

JECT NO.  
14057  
VEY  
RLD  
ED  
MAY 2015  
. No:



**Robinson**  
Land Developme

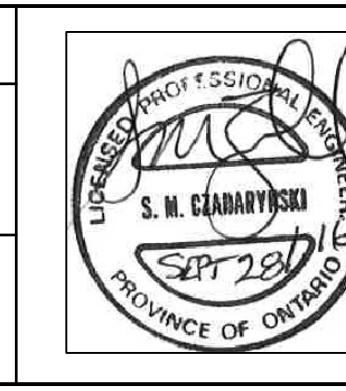
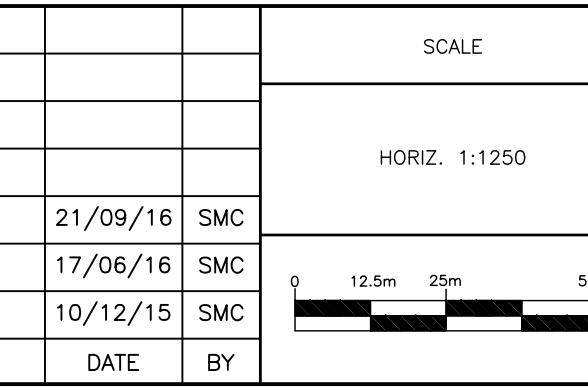
# Robinson Land Developme

# Robinson Land Developme



NOTES  
THE POSITION OF ALL POLE LINES, CONDUITS, WATERMAINS, SEWERS AND OTHER UNDERGROUND AND OVERGROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE CONTRACT DRAWINGS, AND WHERE SHOWN, THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED. BEFORE STARTING WORK, DETERMINE THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES AND ASSUME ALL LIABILITY FOR DAMAGE TO THEM.

NO.	REVISION DESCRIPTION	DATE	BY
3	REVISED PER CITY COMMENTS	21/09/16	SMC
2	REVISED PER CITY COMMENTS	17/06/16	SMC
1	ISSUED FOR REVIEW	10/12/15	SMC



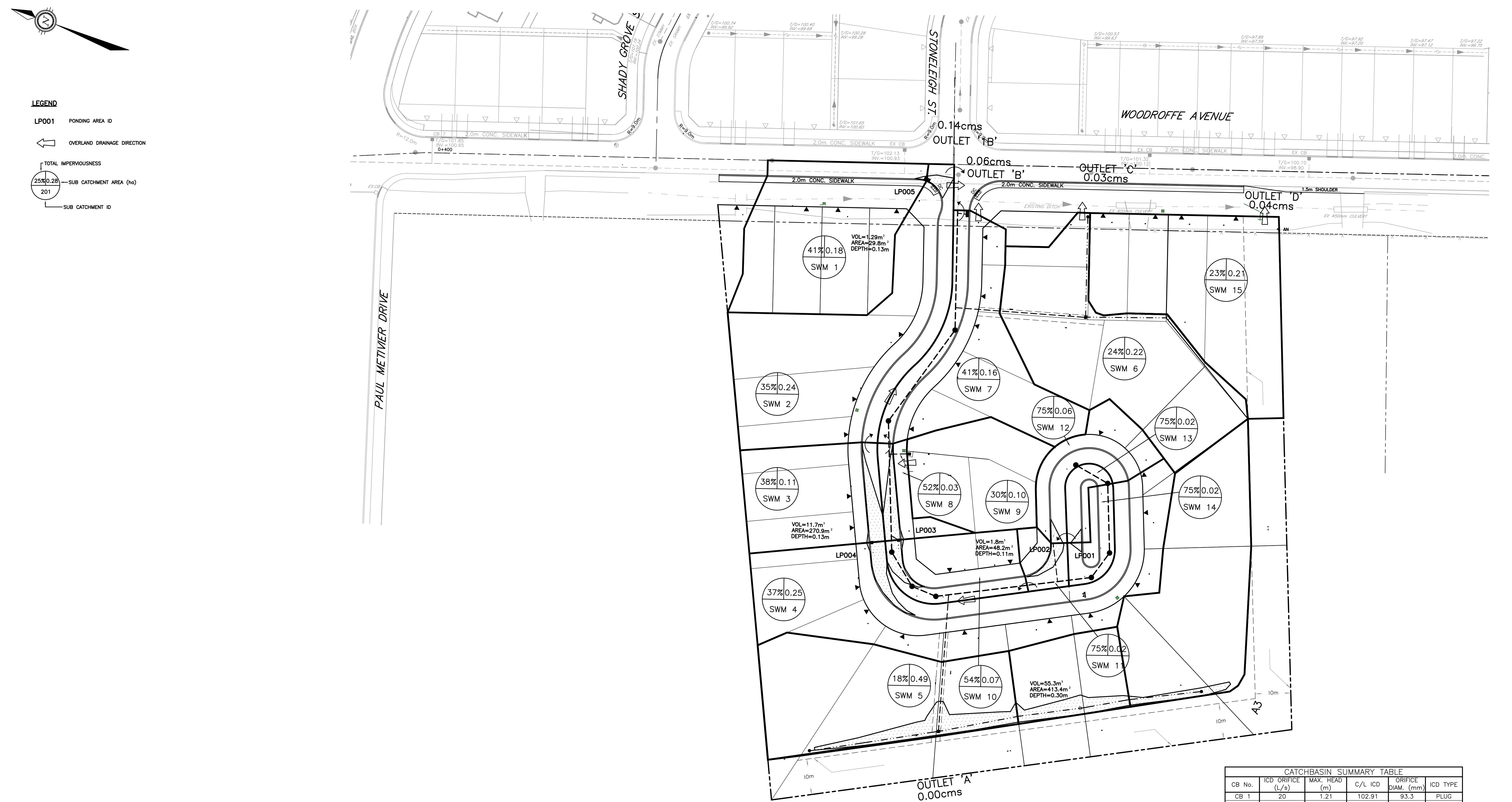
**Robinson**  
Land Development

CONSULTING ENGINEERS  
350 PALLADIUM DRIVE  
KANATA, ONTARIO K2V 1A8  
TELEPHONE (613) 592-6060

**BORRELLO SUBDIVISION**  
514 KOCHAR DRIVE  
OTTAWA, ON  
K2C 4H3

PROJECT NO.  
14057  
SURVEY  
RLD  
DATED  
DECEMBER 2015  
DWG. NO.  
14057-STM2

STORM DRAINAGE AREA



CATCHBASIN SUMMARY TABLE					
CB No.	ICD ORIFICE (L/s)	MAX. HEAD (m)	C/L ICD	ORIFICE DIAM. (mm)	ICD TYPE
CB 1	20	1.21	102.91	93.3	PLUG
CB 2	14.2	1.23	102.58	78.3	PLUG
CB 3	31	1.23	102.58	115.7	PLUG
DCB 4	20	1.10	101.05	95.6	PLUG
DCB 5	20	1.23	100.89	92.9	PLUG
CB 6	25	1.40	102.72	100.6	PLUG
CB 7	15	0.98	100.51	85.3	PLUG
CB 8	20	1.30	100.74	91.7	PLUG

**NOTES**

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4	F
3	F
2	F

D PER CITY COMM  
D PER CITY COMM  
D PER CITY COMM

	28/09/16
	17/06/16
	10/12/15

SCAL  
HORIZ. 10m

20m

A circular stamp with the words "LICENCED PROF" curved along the top edge and "S.M.C." in the center.



# Robinson Land Developmen

350 PALLADIUM DRIVE  
KANATA, ONTARIO K2B 7E1  
TELEPHONE (613) 592-1111

	DESIGN
	CHECKED
A8 60	DRAWN
	CHECKED

**BORRELLO SUBDIVISION**

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# STORM WATER MANAGEMENT PLAN

PROJECT NO.  
**14057**  
SURVEY  
**RLD**  
ATED  
**MAY 2015**  
NG No:

bor100.txt

' Borrellio Subdivision  
' DDSWMM analysis, 3 hour 100 year Chicago Storm  
\*\*\*\*\*  
\* DDSWMM Analysis by RLD - June 2016  
\* Bor100.txt  
\*\*\*\*\*  
\*  
\* IUNIT DELTC NDELTC IEVAL QLIMIT ISTEP  
1 5 72 3 20.0 1  
\* IUNIT =1 for metric  
\* DELTC = time increment for calculation (minutes)  
\* NDELTC = number of computational time steps (maximum = 300)  
\* IEVAL = 1 if pipe sizes are given and it is required to revise  
these sizes, if necessary, based on free surface flow  
\* QLIMIT = Default value of limiting capacity of inlets. Value can be overridden  
for individual inlets by the values assigned to (QLIM) on data group (7)  
\* ISTEP = Interval between print-out  
\*  
\* RAINFALL DATA  
\*\*\*\*\*  
\* JULDAY TZERO  
02290 0.0  
\* JULDAY = Initial Julian calendar  
\* TZERO = initial time [0hrs to 24hrs]  
\* DELTR NDELTR  
10.0 19  
\* 19 STEPS OF RAINFALL INTENSITIES AT 10 MINS INTERVAL  
0 6.046 7.542 10.159 15.969 40.655 178.559 54.049 27.319 18.240 13.737  
11.059 9.285 8.024 7.080 6.347 5.760 5.280 4.879  
\* DELTR = time increment for rainfall hyetograph (minutes)  
\* NDELTR = number of time increments for rainfall hyetograph  
\*  
\* MINOR SYSTEM CHARACTERISTICS  
\* IRTP NP NPD XP SP CP DP QB IPRTP  
\* IRTP=0, routing of minor system flow (for this pipe) will be performed  
\* NP = sewer identification number/name [node point]  
\* NPD = identification number/name of downstream sewer [node point downstream]  
\* XP = length of sewer (m)  
\* SP = invert slope (m/m)  
\* CP = Manning's roughness coefficient  
\* DP = pipe diameter (mm)  
\* QB = base flow (cubes)  
\* IPRTP = option for printing time history of pipe flow (1 or 0) (0=no print)  
\*  
\* Street A  
\* 0 '210' '209' 10.3 0.0097 0.013 254.0 0.0 0  
\* 0 '209' '208' 19.5 0.0103 0.013 254.0 0.0 0  
\* 0 '208' '207' 8.6 0.0093 0.013 254.0 0.0 0  
\* 0 '207' '206' 44.4 0.0020 0.013 457.2 0.0 0  
\* 0 '206' '205a' 7.3 0.0027 0.013 457.2 0.0 0  
\* 0 '205a' '205' 11.2 0.0027 0.013 457.2 0.0 0  
\* 0 '205' '203' 36.8 0.0030 0.013 457.2 0.0 0  
\* 0 '203' '202' 31.6 0.0025 0.013 457.2 0.0 0  
\* 0 '202' '201' 43.6 0.0070 0.013 457.2 0.0 0  
\* 0 '201' '202a' 85.0 0.0073 0.013 457.2 0.0 0  
\* dummy pipe  
\* 0 'X' '210' 85.0 0.0073 0.013 457.2 0.0 0  
\*  
\*ENDMNR  
\* to terminate minor system data entry  
\* if the drainage system has no storage for minor system, enter  
\* terminators as below.

bor100.txt

\*ENDMNR1  
\* must be entered even if no storage is required  
\*ENDMNR2  
\* must be entered even if no storage is required  
\*ENDMNR3  
\* must be entered even if no storage is required  
\* MAJOR SYSTEM CHARACTERISTICS  
\* maximum of 50 storage types  
\* IS W2 SX YCURB CNS SO SROW CNROW YMAX  
\* IS = identification of street segment type  
\* W2 = segment width (m)  
\* SX = pavement cross slope (m/m)  
\* YCURB = height of curb (cm)  
\* CNS = Manning's roughness coefficient for pavement  
\* SO = longitudinal slope  
\* SROW = cross slope of shoulder  
\* CNROW = Manning's roughness coefficient for shoulder  
\* YMAX = Maximum water depth (measured from bottom of curb)  
\* for calculation of street carrying capacity  
\*  
\*  
\* Maximum water depth assumed as 30 cm  
\* Street A  
\*  
1 4.25 0.030 15 0.013 0.0138 0.02 0.025 30  
2 4.25 0.030 15 0.013 0.0076 0.02 0.025 30  
3 4.25 0.030 15 0.013 0.0237 0.02 0.025 30  
4 4.25 0.030 15 0.013 0.0083 0.02 0.025 30  
5 4.25 0.030 15 0.013 0.0050 0.02 0.025 30  
6 4.25 0.030 15 0.013 0.0051 0.02 0.025 30  
7 4.25 0.030 15 0.013 0.0200 0.02 0.025 30  
8 118.00 0.010 30 0.025 0.0090 0.02 0.025 100  
9 4.25 0.030 15 0.013 0.0001 0.02 0.025 30  
\*  
\*  
ENDSTR  
\* terminator for major system characteristics data set  
\* INLET CAPTURE CHARACTERISTICS  
\* IDCB NJC  
1 8  
\* QAPP QCAP  
0. 0.  
10. 10.  
30. 30.  
60. 60.  
90. 90.  
130. 130.  
500. 500.  
1000. 1000.  
ENDIN1  
ENDIN2  
\* applicable for areas  
\* IDCB DET3 NPTS3  
2 55.0 2  
\* QAPP QCAP  
0.0 0.0  
55.0 15.0  
\* applicable for areas  
\* IDCB DET3 NPTS3  
3 1.8 2  
\* QAPP QCAP  
0.0 0.0  
1.8 20.0

bor100.txt

```
* application for areas
*   IDCB    DET3    NPTS3
*     4      5.7      2
*   QAPP    QCAP
*     0.0      0.0
*     17.9     14.2
* application for areas
*   IDCB    DET3    NPTS3
*     5      1.3      2
*   QAPP    QCAP
*     0.0      0.0
*     1.3     20.0
* application for areas
*   IDCB    DET3    NPTS3
*     6      5.7      2
*   QAPP    QCAP
*     0.0      0.0
*     17.9     31.0
* application for areas
*   IDCB    DET3    NPTS3
*     7     20.0      3
*   QAPP    QCAP
*     0.0      0.0
*     1.0     18.0
*     20.0     20.0
* application for areas
*   IDCB    DET3    NPTS3
*     8     25.0      3
*   QAPP    QCAP
*     0.0      0.0
*     1.0     18.0
*     25.0     20.0
* application for areas
*   IDCB    DET3    NPTS3
*     9     30.0      3
*   QAPP    QCAP
*     0.0      0.0
*     1.0     18.0
*     30.0     20.0
* application for areas
*   IDCB    DET3    NPTS3
*    10     35.0      3
*   QAPP    QCAP
*     0.0      0.0
*     1.0     18.0
*     35.0     20.0
* application for areas
*   IDCB    DET3    NPTS3
*    11     50.0      3
*   QAPP    QCAP
*     0.0      0.0
*     1.0     18.0
*     50.0     20.0
* application for areas
*   IDCB    DET3    NPTS3
*    12     75.0      3
*   QAPP    QCAP
*     0.0      0.0
*     1.0     18.0
*     75.0     20.0
* application for areas
*   IDCB    DET3    NPTS3
*    13      1.0      2
```

bor100.txt

```
* QAPP QCAP
  0.0  0.0
  1.0  58.4
* applicabl e for areas
* 1DCB DET3 NPTS3
  14   3.0   3
* QAPP QCAP
  0.0  0.0
  1.0  11.4
  3.0  13.4
* applicabl e for areas
* 1DCB DET3 NPTS3
  15   5.0   3
* QAPP QCAP
  0.0  0.0
  1.0  11.4
  5.0  13.4
* applicabl e for areas
* 1DCB DET3 NPTS3
  16   33.0  3
* QAPP QCAP
  0.0  0.0
  1.0  7.0
  33.0 9.0
* applicabl e for areas
* 1DCB DET3 NPTS3
  17   32.0  3
* QAPP QCAP
  0.0  0.0
  1.0  4.8
  32.0 6.8
* applicabl e for areas
* 1DCB DET3 NPTS3
  18   15.5  3
* QAPP QCAP
  0.0  0.0
  1.0  6.5
  15.5 8.5
* applicabl e for areas
* 1DCB DET3 NPTS3
  19   19.0  3
* QAPP QCAP
  0.0  0.0
  1.0  1.0
  19.0 3.3
* applicabl e for areas
* 1DCB DET3 NPTS3
  20   15.5  3
* QAPP QCAP
  0.0  0.0
  1.0  7.4
  15.5 9.4
*
```

\*\*

ENDI N3

\* MAJOR SYSTEM SEGMENT DATA

\*\*-----

\* IRTS = Option for major system flow routing

\* NS = identification number/name of major system segment

\* NSD = identification number/name of major system segment downstream

\* XS = length of segment

\* IDSS = segment type (as per segment data list)

bor100.txt

\* NUMCB = number of storm inlets within street segment  
 \* IINC = inlet type (as per segment data list)  
 \* QLIM = maximum allowable inlet capture  
 \* NPD = pipe receiving inlet flow  
 \* IPRTS = option for printing time history of segment (=o, no printing)  
 \* routing is performed (for this segment)  
 \*\*-----  
 -----  
 \* IRTS NS NSD XS IDSS NUMCB IINC QLIM NPD  
 IPRTS

* Road Drainage Areas									
0	'SWM14'	'LP001'	40	4	0	1	0.	'X'	0
0	'SWM13'	'LP001'	29	1	0	1	0.	'X'	0
1	'LP001'	'D001'	10	7	0	1	0.	'X'	0
0	'SWM12'	'LP002'	41	1	0	1	0.	'X'	0
0	'SWM11'	'LP002'	16	4	0	1	0.	'X'	0
1	'LP002'	'D002'	10	4	1	3	20.	'207'	0
0	'SWM10'	'LP003'	48	4	0	1	0.	'X'	0
0	'SWM8'	'LP003'	27	6	0	1	0.	'X'	0
1	'LP003'	'D003'	10	6	1	4	14.2	'205'	0
0	'SWM3'	'LP004'	28	6	0	1	0.	'X'	0
0	'SWM4'	'LP004'	107	4	0	1	0.	'X'	0
1	'LP004'	'D004'	10	6	1	6	31.	'205'	0
0	'SWM2'	'LP005'	81	3	0	1	0.	'X'	0
0	'SWM1'	'LP005'	45	5	0	1	0.	'X'	0
1	'LP005'	'D005'	10	7	1	5	20.	'202'	0
0	'SWM7'	'OUTB'	71	3	1	1	20.	'202'	0
* Rear Yard Drainage									
0	'SWM9'	'SWM8'	37	8	1	1	25.	'205'	0
0	'SWM5'	'OUTA'	157	8	1	2	15.	'207'	0
0	'SWM6'	'OUTC'	88	8	1	1	20.	'202'	0
0	'SWM15'	'OUTD'	40	8	0	1	0.	'X'	0
* Dummy Segments									
0	'D001'	'LP002'	7	9	0	1	0.	'X'	1
0	'D002'	'SWM10'	20	9	0	1	0.	'X'	1
0	'D003'	'SWM7'	50	9	0	1	0.	'X'	1
0	'D004'	'SWM2'	65	9	0	1	0.	'X'	1
0	'D005'	'OUT1B'	8	9	0	1	0.	'X'	1

ENDMJR

\* MAJOR SYSTEM STORAGE UNITS

IDSTS	NUSS	NSTOR
'Out1'	1	'OUTA'
'Out2'	1	'OUTB'
'Out3'	1	'OUTC'
'Out4'	1	'OUT1B'
'Out5'	1	'OUTD'

\*

ENDMJSR

\* INFILTRATION PARAMETERS FOR RUNOFF CALCULATIONS

MAX	MIN	DECAY
76.2	13.2	.00115

ENDUAH

\* SUBAREA DATA FOR SWMM RUNOFF

DET1MP	DETP	I PRTW				CNI MP	CNP	S	WLAT
'SWM1'	'SWM1'		0.18	41.	0.013	0.25	0.02	45	1.57
4.67	0								
'SWM2'	'SWM2'		0.24	35.	0.013	0.25	0.02	81	1.57
4.67	0								
'SWM3'	'SWM3'		0.11	38.	0.013	0.25	0.02	28	1.57
4.67	0								
'SWM4'	'SWM4'		0.25	37.	0.013	0.25	0.02	107	1.57
4.67	0								

					bor100. txt				
' SWM5'	' SWM5'	0. 49	18.	0. 013	0. 25	0. 02	157	1. 57	
4. 67	0								
' SWM6'	' SWM6'	0. 22	24.	0. 013	0. 25	0. 02	88	1. 57	
4. 67	0								
' SWM7'	' SWM7'	0. 16	41.	0. 013	0. 25	0. 02	71	1. 57	
4. 67	0								
' SWM8'	' SWM8'	0. 03	52.	0. 013	0. 25	0. 02	27	1. 57	
4. 67	0								
' SWM9'	' SWM9'	0. 10	30.	0. 013	0. 25	0. 02	37	1. 57	
4. 67	0								
' SWM10'	' SWM10'	0. 07	54.	0. 013	0. 25	0. 02	48	1. 57	
4. 67	0								
' SWM11'	' SWM11'	0. 02	51.	0. 013	0. 25	0. 02	16	1. 57	
4. 67	0								
' SWM12'	' SWM12'	0. 06	41.	0. 013	0. 25	0. 02	41	1. 57	
4. 67	0								
' SWM13'	' SWM13'	0. 02	73.	0. 013	0. 25	0. 02	29	1. 57	
4. 67	0								
' SWM14'	' SWM14'	0. 02	70.	0. 013	0. 25	0. 02	40	1. 57	
4. 67	0								
' SWM15'	' SWM15'	0. 21	23.	0. 013	0. 25	0. 02	40	1. 57	
4. 67	0								

\* NW = identification number/name of subarea

\* NSDW = identification number/name of major segment receiving surface runoff

\* ASW area of subarea (ha.)

\* PIMP = percentage impervious

\* CNIMP = Manning's roughness coefficient for impervious area

\* CNP = Manning's roughness coefficient for pervious area

\* S = average slope

\* WLAT = subarea width

\* DETIMP = detention storage for impervious area

\* DETP = detention storage for pervious area

\* IRTW = option for printing and plotting of surface runoff hydrograph (=0, no printing)

ENDSUB1

ENDSUB2

ENDSUB3

bor 100 year out sept 28-16  
\*\*\*\*\*  
\* D D S W M M (release 2.1) \*  
\* The Dual Drainage Storm Water Management Model \*  
\* Copyright \*  
\* ----- \*  
\* AMK Associates International Ltd. \*  
\*\*\*\*\*

This release of DDSWMM will run with a maximum of

500 minor system segments (pipes), including outlets  
500 major system (street) segments, including outlets  
500 subcatchments  
30 storage units for the minor system  
30 storage units for the major system  
300 computational time steps  
300 increments for rainfall hyetograph  
50 storm inlet types  
20 points describing the inlet capture curve  
50 major system segment types  
5 street segments discharging into a street junction  
5 pipes discharging into a pipe junction  
5 subcatchments discharging into a major system segment  
5 inlet groups discharging into a pipe  
30 unit area hydrographs

For other program constraints, please refer to the users manual

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrelli Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

RUN CONTROL PARAMETERS

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Measuring units	Metric
Time increment for calculation	5.00 minutes
Number of computational steps	72
Default limiting capacity of inlets	20.00 l/s
Total simulation time	5:55 (hrs:mins)
Interval between printout	1

Calculation for the minor system is not included in this simulation

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrelli Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

bor 100 year out sept 28-16

RAI NFALL DATA			Initial Julian Date
02290	Initial Time		
0.00 hours			
Time (mm/hr) (hr: min)	Rainfall (mm/hr)	Rainfall Intensity	
0.11E+03	0.14E+03	0.18E+03	0.00E+00 0.36E+02 0.71E+02
0: 0	0.00	*	
0: 10	6.05	**	
0: 20	7.54	***	
0: 30	10.16	***	
0: 40	15.97	*****	
0: 50	40.65	*****	
1: 0	178.56	*****	
1: 10	54.05	*****	
1: 20	27.32	*****	
1: 30	18.24	*****	
1: 40	13.74	****	
1: 50	11.06	****	
2: 0	9.28	***	
2: 10	8.02	***	
2: 20	7.08	**	
2: 30	6.35	**	
2: 40	5.76	**	
2: 50	5.28	**	
3: 0	4.88	**	
			0.00E+00 0.36E+02 0.71E+02
0.11E+03	0.14E+03	0.18E+03	

† Rainfall duration 3:10 (hrs: mins.)

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision  
bor 100 year out sept 28-16

DDSWMM analysis, 3 hour 100 year Chicago Storm

MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Hei ght of Curb (cm)	Manni ng (n)	Long. (m/m)	Shoul der Cross Slope (m/m)	Shoul der Roughness (n)
1 30.0	4.25	0.030	15.0	0.0130	0.014	0.020	0.0250

RATING CURVE

Depth (cm)	Fl ow (cms)	Spread (m)
0.00	0.00	0.00
1.50	0.00	0.50
3.00	0.02	1.00
4.50	0.06	1.50
6.00	0.12	2.00
7.50	0.23	2.50
9.00	0.37	3.00
10.50	0.55	3.50
12.00	0.79	4.00
13.50	1.08	4.25
15.00	1.43	4.25
16.50	1.82	5.00
18.00	2.26	5.75
19.50	2.76	6.50
21.00	3.32	7.25
22.50	3.95	8.00
24.00	4.64	8.75
25.50	5.41	9.50
27.00	6.24	10.25
28.50	7.15	11.00
30.00	8.14	11.75

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

MAJOR SYSTEM RATING CURVE

bor 100 year out sept 28-16

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Hei ght of Curb (cm)	Manni ng (n)	Long. (m/m)	Shoul der Cross Slope (m/m)	Shoul der Roughness (n)
2 30.0	4.25	0.030	15.0	0.0130	0.008	0.020	0.0250

### RATING CURVE

Depth (cm)	Fl ow (cms)	Spread (m)
0.00	0.00	0.00
1.50	0.00	0.50
3.00	0.01	1.00
4.50	0.04	1.50
6.00	0.09	2.00
7.50	0.17	2.50
9.00	0.27	3.00
10.50	0.41	3.50
12.00	0.59	4.00
13.50	0.80	4.25
15.00	1.06	4.25
16.50	1.35	5.00
18.00	1.68	5.75
19.50	2.05	6.50
21.00	2.47	7.25
22.50	2.93	8.00
24.00	3.45	8.75
25.50	4.01	9.50
27.00	4.63	10.25
28.50	5.31	11.00
30.00	6.04	11.75

†

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

### MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth	Pavement Width (m)	Pavement Cross Slope	Hei ght of Curb	Manni ng (n)	Long. (m/m)	Shoul der Cross Slope	Shoul der Roughness (n)
----------------------------------	--------------------------	----------------------------	-----------------------	-----------------	----------------	-----------------------------	-------------------------------

(cm)	bor (m/m)	100 year (cm)	out	sept	28-16		(m/m)
					3	30.0	
30.0	4.25	0.030	15.0	0.0130	0.024	0.020	0.0250

#### RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0.00	0.00	0.00
1.50	0.00	0.50
3.00	0.03	1.00
4.50	0.08	1.50
6.00	0.16	2.00
7.50	0.30	2.50
9.00	0.48	3.00
10.50	0.73	3.50
12.00	1.04	4.00
13.50	1.42	4.25
15.00	1.87	4.25
16.50	2.38	5.00
18.00	2.96	5.75
19.50	3.62	6.50
21.00	4.36	7.25
22.50	5.18	8.00
24.00	6.09	8.75
25.50	7.09	9.50
27.00	8.18	10.25
28.50	9.38	11.00
30.00	10.67	11.75

†

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrellio Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

#### MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. Slope (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness (n)
30.0	4.25	0.030	15.0	0.0130	0.008	0.020	0.0250

bor 100 year out sept 28-16  
RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0. 00	0. 00	0. 00
1. 50	0. 00	0. 50
3. 00	0. 02	1. 00
4. 50	0. 04	1. 50
6. 00	0. 10	2. 00
7. 50	0. 18	2. 50
9. 00	0. 28	3. 00
10. 50	0. 43	3. 50
12. 00	0. 61	4. 00
13. 50	0. 84	4. 25
15. 00	1. 11	4. 25
16. 50	1. 41	5. 00
18. 00	1. 75	5. 75
19. 50	2. 14	6. 50
21. 00	2. 58	7. 25
22. 50	3. 06	8. 00
24. 00	3. 60	8. 75
25. 50	4. 19	9. 50
27. 00	4. 84	10. 25
28. 50	5. 55	11. 00
30. 00	6. 32	11. 75

†

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrellio Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. Slope (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness (n)
5 30. 0	4. 25	0. 030	15. 0	0. 0130	0. 005	0. 020	0. 0250

RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0. 00	0. 00	0. 00
1. 50	0. 00	0. 50

bor	100 year out	sept	28-16
3. 00	0. 01	1. 00	
4. 50	0. 03	1. 50	
6. 00	0. 07	2. 00	
7. 50	0. 14	2. 50	
9. 00	0. 22	3. 00	
10. 50	0. 33	3. 50	
12. 00	0. 48	4. 00	
13. 50	0. 65	4. 25	
15. 00	0. 86	4. 25	
16. 50	1. 09	5. 00	
18. 00	1. 36	5. 75	
19. 50	1. 66	6. 50	
21. 00	2. 00	7. 25	
22. 50	2. 38	8. 00	
24. 00	2. 80	8. 75	
25. 50	3. 25	9. 50	
27. 00	3. 76	10. 25	
28. 50	4. 31	11. 00	
30. 00	4. 90	11. 75	

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)

## Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

## MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Hei ght of Curb (cm)	Manni ng (n)	Long. Slope (m/m)	Shoul der Cross Slope (m/m)	Shoul der Roughness (n)
6 30. 0	4. 25	0. 030	15. 0	0. 0130	0. 005	0. 020	0. 0250

## RATING CURVE

Depth (cm)	Fl ow (cms)	Spread (m)
0. 00	0. 00	0. 00
1. 50	0. 00	0. 50
3. 00	0. 01	1. 00
4. 50	0. 04	1. 50
6. 00	0. 08	2. 00
7. 50	0. 14	2. 50
9. 00	0. 22	3. 00
10. 50	0. 34	3. 50
12. 00	0. 48	4. 00
13. 50	0. 66	4. 25

bor	100 year out	sept	28-16
15.00	0.87	4.25	
16.50	1.10	5.00	
18.00	1.37	5.75	
19.50	1.68	6.50	
21.00	2.02	7.25	
22.50	2.40	8.00	
24.00	2.82	8.75	
25.50	3.29	9.50	
27.00	3.80	10.25	
28.50	4.35	11.00	
30.00	4.95	11.75	

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Burrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

## MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Hei ght of Curb (cm)	Manni ng (n)	Long. Slope (m/m)	Shoul der Cross Slope (m/m)	Shoul der Roughness
7 30.0	4.25	0.030	15.0	0.0130	0.020	0.020	0.0250

## RATING CURVE

Depth (cm)	Fl ow (cms)	Spread (m)
0.00	0.00	0.00
1.50	0.00	0.50
3.00	0.02	1.00
4.50	0.07	1.50
6.00	0.15	2.00
7.50	0.27	2.50
9.00	0.44	3.00
10.50	0.67	3.50
12.00	0.95	4.00
13.50	1.30	4.25
15.00	1.72	4.25
16.50	2.19	5.00
18.00	2.72	5.75
19.50	3.33	6.50
21.00	4.00	7.25
22.50	4.76	8.00
24.00	5.59	8.75
25.50	6.51	9.50

bor 100 year out sept 28-16  
 27.00 7.52 10.25  
 28.50 8.61 11.00  
 30.00 9.80 11.75

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

#### MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness
8 100.0	118.00	0.010	30.0	0.0250	0.009	0.020	0.0250

#### RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0.00	0.00	0.00
5.00	0.10	5.00
10.00	0.61	10.00
15.00	1.81	15.00
20.00	3.89	20.00
25.00	7.06	25.00
30.00	11.47	30.00
35.00	17.31	35.00
40.00	24.71	40.00
45.00	33.83	45.00
50.00	44.80	50.00
55.00	57.77	55.00
60.00	72.86	60.00
65.00	90.19	65.00
70.00	109.90	70.00
75.00	132.10	75.00
80.00	156.91	80.00
85.00	184.44	85.00
90.00	214.81	90.00
95.00	248.12	95.00
100.00	284.49	100.00

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

bor 100 year out sept 28-16

DDSWMM analysis, 3 hour 100 year Chicago Storm

MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Hei ght of Curb (cm)	Manni ng (n)	Long. (m/m)	Shoul der Cross Slope (m/m)	Shoul der Roughness (n)
9 30.0	4. 25	0. 030	15. 0	0. 0130	0. 000	0. 020	0. 0250

RATI NG CURVE

Depth (cm)	Fl ow (cms)	Spread (m)
0. 00	0. 00	0. 00
1. 50	0. 00	0. 50
3. 00	0. 00	1. 00
4. 50	0. 00	1. 50
6. 00	0. 01	2. 00
7. 50	0. 02	2. 50
9. 00	0. 03	3. 00
10. 50	0. 05	3. 50
12. 00	0. 07	4. 00
13. 50	0. 09	4. 25
15. 00	0. 12	4. 25
16. 50	0. 15	5. 00
18. 00	0. 19	5. 75
19. 50	0. 24	6. 50
21. 00	0. 28	7. 25
22. 50	0. 34	8. 00
24. 00	0. 40	8. 75
25. 50	0. 46	9. 50
27. 00	0. 53	10. 25
28. 50	0. 61	11. 00
30. 00	0. 69	11. 75

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

STORM INLET DATA

bor 100 year out sept 28-16

1 Normal Inlet

Inlet Identification No. 1  
No. of Points on Capture Curve 8

Inlet Capture Relationship

Approach Flow (l/s)	Inlet Flow (l/s)
0.00	0.00
10.00	10.00
30.00	30.00
60.00	60.00
90.00	90.00
130.00	130.00
500.00	500.00
1000.00	1000.00

2 Storage Inlet

Inlet Identification No. 2  
Maximum Storage 55.00 cu. m.  
No. of Points on Storage-Capture Curve 2

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
55.00	15.00

3 Storage Inlet

Inlet Identification No. 3  
Maximum Storage 1.80 cu. m.  
No. of Points on Storage-Capture Curve 2

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.80	20.00

bor 100 year out sept 28-16

4 Storage Inlet

Inlet Identification No.	4
Maximum Storage	5.70 cu. m.
No. of Points on Storage-Capture Curve	2
Storage-Inlet Capture Relationship	
Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
17.90	14.20

5 Storage Inlet

Inlet Identification No.	5
Maximum Storage	1.30 cu. m.
No. of Points on Storage-Capture Curve	2
Storage-Inlet Capture Relationship	
Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.30	20.00

6 Storage Inlet

Inlet Identification No.	6
Maximum Storage	5.70 cu. m.
No. of Points on Storage-Capture Curve	2
Storage-Inlet Capture Relationship	
Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
17.90	31.00

7 Storage Inlet

bor 100 year out sept 28-16

Inlet Identification No. 7  
Maximum Storage 20.00 cu. m.  
No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

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Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	18.00
20.00	20.00

8 Storage Inlet

Inlet Identification No. 8  
Maximum Storage 25.00 cu. m.  
No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

---

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	18.00
25.00	20.00

9 Storage Inlet

Inlet Identification No. 9  
Maximum Storage 30.00 cu. m.  
No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

---

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	18.00
30.00	20.00

10 Storage Inlet

bor 100 year out sept 28-16

Inlet Identification No.	10
Maximum Storage	35.00 cu. m.
No. of Points on Storage-Capture Curve	3

Storage-Inlet Capture Relationship

---

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	18.00
35.00	20.00

11 Storage Inlet

Inlet Identification No.	11
Maximum Storage	50.00 cu. m.
No. of Points on Storage-Capture Curve	3

Storage-Inlet Capture Relationship

---

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	18.00
50.00	20.00

12 Storage Inlet

Inlet Identification No.	12
Maximum Storage	75.00 cu. m.
No. of Points on Storage-Capture Curve	3

Storage-Inlet Capture Relationship

---

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	18.00
75.00	20.00

13 Storage Inlet

bor 100 year out sept 28-16

Inlet Identification No. 13  
Maximum Storage 1.00 cu. m.  
No. of Points on Storage-Capture Curve 2

Storage-Inlet Capture Relationship

---

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	58.40

14 Storage Inlet

Inlet Identification No. 14  
Maximum Storage 3.00 cu. m.  
No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

---

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	11.40
3.00	13.40

15 Storage Inlet

Inlet Identification No. 15  
Maximum Storage 5.00 cu. m.  
No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

---

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	11.40
5.00	13.40

16 Storage Inlet

bor 100 year out sept 28-16

Inlet Identification No. 16  
Maximum Storage 33.00 cu. m.  
No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	7.00
33.00	9.00

17 Storage Inlet

Inlet Identification No. 17  
Maximum Storage 32.00 cu. m.  
No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	4.80
32.00	6.80

18 Storage Inlet

Inlet Identification No. 18  
Maximum Storage 15.50 cu. m.  
No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	6.50
15.50	8.50

19 Storage Inlet

bor 100 year out sept 28-16

Inlet Identification No. 19  
Maximum Storage 19.00 cu. m.  
No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	1.00
19.00	3.30

20 Storage Inlet

Inlet Identification No. 20  
Maximum Storage 15.50 cu. m.  
No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	7.40
15.50	9.40

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

MAJOR SYSTEM DATA

Flow History (?)	Street Segment	D/S Segment	Length (m)	Type	No. of C. B.	Inlet Type	Limiting Inlet Capture (l/s)	Connecting Pipe/EXTRAN Inlet
NO	1 SWM14	LP001	40.0	4	0	1 *	0.00	X
NO	2 SWM13	LP001	29.0	1	0	1 *	0.00	X

				bor	100	year	out	sept	28-16	*		
					10.	0	7	0	1	*	0.00	X
NO	3	LP001 "No Routing"	D001									
NO	4	SWM12	LP002		41.0		1	0	1	*	0.00	X
NO	5	SWM11	LP002		16.0		4	0	1	*	0.00	X
NO	6	LP002 "No Routing"	D002		10.0		4	1	3	***	20.00	207
NO	7	SWM10	LP003		48.0		4	0	1	*	0.00	X
NO	8	SWM8	LP003		27.0		6	0	1	*	0.00	X
NO	9	LP003 "No Routing"	D003		10.0		6	1	4	***	4.52	205
NO	10	SWM3	LP004		28.0		6	0	1	*	0.00	X
NO	11	SWM4	LP004		107.0		4	0	1	*	0.00	X
NO	12	LP004 "No Routing"	D004		10.0		6	1	6	***	9.87	205
NO	13	SWM2	LP005		81.0		3	0	1	*	0.00	X
NO	14	SWM1	LP005		45.0		5	0	1	*	0.00	X
NO	15	LP005 "No Routing"	D005		10.0		7	1	5	***	20.00	202
NO	16	SWM7	OUTB		71.0		3	1	1	*	20.00	202
NO	17	SWM9	SWM8		37.0		8	1	1	*	25.00	205
NO	18	SWM5	OUTA		157.0		8	1	2	***	15.00	207
NO	19	SWM6	OUTC		88.0		8	1	1	*	20.00	202
NO	20	SWM15	OUTD		40.0		8	0	1	*	0.00	X
YES	21	D001	LP002		7.0		9	0	1	*	0.00	X
YES	22	D002	SWM10		20.0		9	0	1	*	0.00	X
YES	23	D003	SWM7		50.0		9	0	1	*	0.00	X
YES	24	D004	SWM2		65.0		9	0	1	*	0.00	X
YES	25	D005	OUT1B		8.0		9	0	1	*	0.00	X

\* Normal Inlet.

\*\* Storage Inlet with linear relationship between Storage and Inlet Capture.

\*\*\* Storage Inlet with user-specified relationship between Storage and Inlet Capture.

Total Number of Street segments	25
Total Length of Major System	1055.00 m
Total Number of Inlet C.B.	8
Average Distance Between Inlets	263.75 m

bor 100 year out sept 28-16

Outlets From Major System

Outlet I. D.

OUTB  
OUTA  
OUTC  
OUTD  
OUT1B

Total Number of Outlets from Major System = 5

DATA FOR MAJOR SYSTEM STORAGE

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No.	Storage Unit	No. of Inflow Points	I. D. Nos. of Inflow Points
1	Out1	1	OUTA
2	Out2	1	OUTB
3	Out3	1	OUTC
4	Out4	1	OUT1B
5	Out5	1	OUTD

No. of Detention Structures 5

+

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

SUB-CATCHMENT/SURFACE RUNOFF DATA

Infiltration Parameters

Max. Infiltration Rate 76.20 mm/hr  
Min. Infiltration Rate 13.20 mm/hr  
Decay Rate 0.001150 1/sec.

Unit Area Hydrograph (UAH) Data

bor 100 year out sept 28-16

No Unit Area Hydrograph Data

SUB-CATCHMENT DATA									
No.	Subarea	Street	Area	Imp.	Mann. (N)	Mann. (N)	Slope (m/m)	Width (m)	
Dep.	Storage Flow	Segment	(Ha.)	(%)	(Imp.)	(Perv.)			
Imp.	Perv.	History							
(mm)	(mm)	(?)							
1. 570	4. 670	SWM1	0. 18	41.	0. 0130	0. 2500	0. 020	45.	
2	SWM2	NO	0. 24	35.	0. 0130	0. 2500	0. 020	81.	
1. 570	4. 670	SWM3	0. 11	38.	0. 0130	0. 2500	0. 020	28.	
1. 570	4. 670	SWM4	0. 25	37.	0. 0130	0. 2500	0. 020	107.	
1. 570	4. 670	SWM5	0. 49	18.	0. 0130	0. 2500	0. 020	157.	
1. 570	4. 670	SWM6	0. 22	24.	0. 0130	0. 2500	0. 020	88.	
1. 570	4. 670	SWM7	0. 16	41.	0. 0130	0. 2500	0. 020	71.	
1. 570	4. 670	SWM8	0. 03	52.	0. 0130	0. 2500	0. 020	27.	
1. 570	4. 670	SWM9	0. 10	30.	0. 0130	0. 2500	0. 020	37.	
1. 570	4. 670	SWM10	0. 07	54.	0. 0130	0. 2500	0. 020	48.	
1. 570	4. 670	SWM11	0. 02	51.	0. 0130	0. 2500	0. 020	16.	
1. 570	4. 670	SWM12	0. 06	41.	0. 0130	0. 2500	0. 020	41.	
1. 570	4. 670	SWM13	0. 02	73.	0. 0130	0. 2500	0. 020	29.	
1. 570	4. 670	SWM14	0. 02	70.	0. 0130	0. 2500	0. 020	40.	
1. 570	4. 670	SWM15	0. 21	23.	0. 0130	0. 2500	0. 020	40.	
1. 570	4. 670	NO							

\* Inflow Hydrograph Input Directly

\*\* Inflow hydrograph Input in terms of flow per unit area

Total Drainage Area 2.18 Hectares

Number of Subcatchments 15

<sup>†</sup> Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

bor 100 year out sept 28-16

Simulation Details - Surface Runoff - 15 Subareas

count Subarea

1	SWM1
2	SWM2
3	SWM3
4	SWM4
5	SWM5
6	SWM6
7	SWM7
8	SWM8
9	SWM9
10	SWM10
11	SWM11
12	SWM12
13	SWM13
14	SWM14
15	SWM15

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

Simulation Details - Major System - 30 Segments/Outlets

count	order	segment	time step (min.)	No. of time steps	Max. flow (cms)	Max. depth (cm)
1	2	SWM13	0.69	512	0.01	2.19
2	1	SWM14	1.13	314	0.01	2.48
3	3	LP001			0.02	2.80
4	21	D001	0.84	424	0.02	7.72
5	5	SWM11	0.48	735	0.01	2.25
6	4	SWM12	0.76	467	0.02	3.15
7	11	SWM4	1.74	204	0.08	5.60
8	10	SWM3	0.69	516	0.03	4.35
9	6	LP002			0.05	4.67
10	12	LP004			0.11	6.90
11	17	SWM9	4.07	87	0.03	1.47
12	22	D002	2.17	164	0.03	8.95
13	24	D004	4.83	73	0.10	14.05

			bor	100 year	out	sept	28-16		
14	8	SWM8		0.77	459		0.02	3.47	
15	7	SWM10		0.90	395		0.05	4.52	
16	14	SWM1		0.98	363		0.06	5.31	
17	13	SWM2		0.82	433		0.12	5.19	
18	9	LP003					0.06	5.54	
19	15	LP005					0.16	6.09	
20	23	D003		4.62	77		0.06	11.36	
21	25	D005		0.55	641		0.14	15.73	
22	20	SWM15		2.97	119		0.04	2.18	
23	19	SWM6		4.81	74		0.06	2.96	
24	18	SWM5		5.00	72		0.10	5.06	
25	16	SWM7		0.78	454		0.08	4.57	
26	30	OUT1B					0.14		
27	29	OUTD					0.04		
28	28	OUTC					0.03		
29	27	OUTA					0.06		
30	26	OUTB					0.06		

† Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

#### EXTRAN Interface File Information

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Inlet flows are stored at the following 4 inlets (EXTRAN nodes):

X	207	205	202
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#### DDSWMM-EXTRAN Connectivity

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#### EXTRAN Inlet

#### DDSWMM Inlets (Major System Segments)

X	SWM14	SWM13	LP001	SWM12
SWM11				
207	LP002	SWM5		
205	LP003	LP004		SWM9
202	LP005	SWM7		SWM6

† Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision  
bor 100 year out sept 28-16

DDSWMM analysis, 3 hour 100 year Chicago Storm

### MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment D001

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 5	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 15	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 25	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.000	0.000	0.000	0.000	0.6	0.00
0: 35	0.001	0.000	0.001	0.000	0.000	1.8	0.00
0: 40	0.001	0.000	0.001	0.000	0.001	2.0	0.00
0: 45	0.001	0.000	0.001	0.000	0.001	2.3	0.00
0: 50	0.002	0.000	0.002	0.000	0.002	3.1	0.00
0: 55	0.003	0.000	0.003	0.000	0.003	3.7	0.00
1: 0	0.011	0.000	0.011	0.000	0.009	6.0	0.00
1: 5	0.020	0.000	0.020	0.000	0.018	7.6	0.00
1: 10	0.010	0.000	0.010	0.000	0.012	5.8	0.00
1: 15	0.005	0.000	0.005	0.000	0.006	4.6	0.00
1: 20	0.004	0.000	0.004	0.000	0.004	4.0	0.00
1: 25	0.003	0.000	0.003	0.000	0.003	3.5	0.00
1: 30	0.002	0.000	0.002	0.000	0.002	3.2	0.00
1: 35	0.002	0.000	0.002	0.000	0.002	3.1	0.00
1: 40	0.001	0.000	0.001	0.000	0.002	2.8	0.00
1: 45	0.001	0.000	0.001	0.000	0.001	2.6	0.00
1: 50	0.001	0.000	0.001	0.000	0.001	2.4	0.00
1: 55	0.001	0.000	0.001	0.000	0.001	2.3	0.00
2: 0	0.001	0.000	0.001	0.000	0.001	2.2	0.00
2: 5	0.001	0.000	0.001	0.000	0.001	2.1	0.00
2: 10	0.001	0.000	0.001	0.000	0.001	2.0	0.00
2: 15	0.001	0.000	0.001	0.000	0.001	2.0	0.00
2: 20	0.001	0.000	0.001	0.000	0.001	1.9	0.00
2: 25	0.001	0.000	0.001	0.000	0.001	1.9	0.00
2: 30	0.001	0.000	0.001	0.000	0.001	1.9	0.00
2: 35	0.001	0.000	0.001	0.000	0.001	1.8	0.00
2: 40	0.001	0.000	0.001	0.000	0.001	1.8	0.00
2: 45	0.001	0.000	0.001	0.000	0.001	1.8	0.00
2: 50	0.000	0.000	0.000	0.000	0.001	1.7	0.00
2: 55	0.000	0.000	0.000	0.000	0.000	1.7	0.00
3: 0	0.000	0.000	0.000	0.000	0.000	1.7	0.00
3: 5	0.000	0.000	0.000	0.000	0.000	1.7	0.00
3: 10	0.000	0.000	0.000	0.000	0.000	1.7	0.00
3: 15	0.000	0.000	0.000	0.000	0.000	1.7	0.00
3: 20	0.000	0.000	0.000	0.000	0.000	1.6	0.00
3: 25	0.000	0.000	0.000	0.000	0.000	1.6	0.00
3: 30	0.000	0.000	0.000	0.000	0.000	1.6	0.00
3: 35	0.000	0.000	0.000	0.000	0.000	1.5	0.00
3: 40	0.000	0.000	0.000	0.000	0.000	1.5	0.00
3: 45	0.000	0.000	0.000	0.000	0.000	1.5	0.00

		bor	100	year	out	sept	28-16		
3: 50	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	1. 4	0. 00	
3: 55	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	1. 3	0. 00	
4: 0	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	1. 2	0. 00	
4: 5	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	1. 2	0. 00	
4: 10	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	1. 1	0. 00	
4: 15	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	1. 0	0. 00	
4: 20	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	1. 0	0. 00	
4: 25	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	1. 0	0. 00	
4: 30	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 9	0. 00	
4: 35	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 9	0. 00	
4: 40	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 8	0. 00	
4: 45	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 8	0. 00	
4: 50	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 8	0. 00	
4: 55	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 8	0. 00	
5: 0	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 7	0. 00	
5: 5	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 7	0. 00	
5: 10	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 7	0. 00	
5: 15	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 7	0. 00	
5: 20	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 6	0. 00	
5: 25	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 6	0. 00	
5: 30	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 6	0. 00	
5: 35	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 6	0. 00	
5: 40	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 6	0. 00	
5: 45	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 6	0. 00	
5: 50	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 6	0. 00	
5: 55	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 5	0. 00	

Maximum 0. 021  
Time (h: min) 1: 6

† Dual Drainage Storm Water Management Model (DDSWMM 2.1)

### Borello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

### MAJOR SYSTEM DETAILED SIMULATION RESULTS

#### Major System Segment D002

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 5	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 10	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 15	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 20	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 25	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 30	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 35	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 40	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 45	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 50	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 55	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00

		bor	100	year	out	sept	28-16		
1:	0	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00
1:	5	0.028	0.000	0.028	0.000	0.015	8.6	0.00	
1:	10	0.012	0.000	0.012	0.000	0.019	6.2	0.00	
1:	15	0.000	0.000	0.000	0.000	0.008	0.0	0.00	
1:	20	0.000	0.000	0.000	0.000	0.004	0.0	0.00	
1:	25	0.000	0.000	0.000	0.000	0.003	0.0	0.00	
1:	30	0.000	0.000	0.000	0.000	0.002	0.0	0.00	
1:	35	0.000	0.000	0.000	0.000	0.001	0.0	0.00	
1:	40	0.000	0.000	0.000	0.000	0.001	0.0	0.00	
1:	45	0.000	0.000	0.000	0.000	0.001	0.0	0.00	
1:	50	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
1:	55	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
2:	0	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
2:	5	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
2:	10	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
2:	15	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
2:	20	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
2:	25	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
2:	30	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
2:	35	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
2:	40	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
2:	45	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
2:	50	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
2:	55	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
3:	0	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
3:	5	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
3:	10	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
3:	15	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
3:	20	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
3:	25	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
3:	30	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
3:	35	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
3:	40	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
3:	45	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
3:	50	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
3:	55	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
4:	0	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
4:	5	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
4:	10	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
4:	15	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
4:	20	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
4:	25	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
4:	30	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
4:	35	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
4:	40	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
4:	45	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
4:	50	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
4:	55	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
5:	0	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
5:	5	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
5:	10	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
5:	15	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
5:	20	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
5:	25	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
5:	30	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
5:	35	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
5:	40	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
5:	45	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
5:	50	0.000	0.000	0.000	0.000	0.000	0.0	0.00	
5:	55	0.000	0.000	0.000	0.000	0.000	0.0	0.00	

Maxi mum	0.031	0.031	0.000	0.023	8. 9	0.00
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Time (h: min) 1: 6

bor 100 year out sept 28-16  
1: 6 0: 0 1: 8

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)

## Borrellio Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

## MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment D003

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 5	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 15	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 25	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 35	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 40	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 45	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 50	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 55	0.000	0.000	0.000	0.000	0.000	0.0	0.00
1: 0	0.016	0.000	0.016	0.000	0.005	7.0	0.00
1: 5	0.053	0.000	0.053	0.000	0.023	10.9	0.00
1: 10	0.051	0.000	0.051	0.000	0.042	10.8	0.00
1: 15	0.031	0.000	0.031	0.000	0.041	9.0	0.00
1: 20	0.019	0.000	0.019	0.000	0.031	7.5	0.00
1: 25	0.012	0.000	0.012	0.000	0.022	6.3	0.00
1: 30	0.008	0.000	0.008	0.000	0.016	5.4	0.00
1: 35	0.005	0.000	0.005	0.000	0.011	4.6	0.00
1: 40	0.004	0.000	0.004	0.000	0.008	3.9	0.00
1: 45	0.002	0.000	0.002	0.000	0.006	3.3	0.00
1: 50	0.001	0.000	0.001	0.000	0.004	2.7	0.00
1: 55	0.001	0.000	0.001	0.000	0.003	1.9	0.00
2: 0	0.000	0.000	0.000	0.000	0.002	0.4	0.00
2: 5	0.000	0.000	0.000	0.000	0.002	0.0	0.00
2: 10	0.000	0.000	0.000	0.000	0.002	0.0	0.00
2: 15	0.000	0.000	0.000	0.000	0.001	0.0	0.00
2: 20	0.000	0.000	0.000	0.000	0.001	0.0	0.00
2: 25	0.000	0.000	0.000	0.000	0.001	0.0	0.00
2: 30	0.000	0.000	0.000	0.000	0.001	0.0	0.00
2: 35	0.000	0.000	0.000	0.000	0.001	0.0	0.00
2: 40	0.000	0.000	0.000	0.000	0.001	0.0	0.00
2: 45	0.000	0.000	0.000	0.000	0.001	0.0	0.00
2: 50	0.000	0.000	0.000	0.000	0.000	0.0	0.00
2: 55	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 5	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 15	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00

		bor	100	year	out	sept	28-16		
3: 25	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
3: 30	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
3: 35	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
3: 40	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
3: 45	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
3: 50	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
3: 55	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
4: 0	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
4: 5	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
4: 10	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
4: 15	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
4: 20	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
4: 25	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
4: 30	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
4: 35	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
4: 40	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
4: 45	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
4: 50	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
4: 55	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
5: 0	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
5: 5	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
5: 10	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
5: 15	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
5: 20	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
5: 25	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
5: 30	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
5: 35	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
5: 40	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
5: 45	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
5: 50	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00
5: 55	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00	0. 00

Maximum 0. 059  
Time (h: min) 1: 6

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrellio Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

#### MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment D004

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 5	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 10	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 15	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 20	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 25	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 30	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00

		bor	100	year	out	sept	28-16		
0: 35		0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 40		0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 45		0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 50		0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 55		0.000	0.000	0.000	0.000	0.001	0.001	0.0	0.00
1: 0		0.031	0.000	0.031	0.000	0.009	9.0	9.0	0.00
1: 5		0.088	0.000	0.088	0.000	0.037	13.2	13.2	0.00
1: 10		0.078	0.000	0.078	0.000	0.065	12.6	12.6	0.00
1: 15		0.049	0.000	0.049	0.000	0.066	10.7	10.7	0.00
1: 20		0.032	0.000	0.032	0.000	0.052	9.1	9.1	0.00
1: 25		0.019	0.000	0.019	0.000	0.039	7.5	7.5	0.00
1: 30		0.011	0.000	0.011	0.000	0.028	6.2	6.2	0.00
1: 35		0.007	0.000	0.007	0.000	0.019	4.9	4.9	0.00
1: 40		0.003	0.000	0.003	0.000	0.014	3.5	3.5	0.00
1: 45		0.000	0.000	0.000	0.000	0.010	1.4	1.4	0.00
1: 50		0.000	0.000	0.000	0.000	0.008	0.0	0.0	0.00
1: 55		0.000	0.000	0.000	0.000	0.006	0.0	0.0	0.00
2: 0		0.000	0.000	0.000	0.000	0.005	0.0	0.0	0.00
2: 5		0.000	0.000	0.000	0.000	0.004	0.0	0.0	0.00
2: 10		0.000	0.000	0.000	0.000	0.004	0.0	0.0	0.00
2: 15		0.000	0.000	0.000	0.000	0.003	0.0	0.0	0.00
2: 20		0.000	0.000	0.000	0.000	0.003	0.0	0.0	0.00
2: 25		0.000	0.000	0.000	0.000	0.002	0.0	0.0	0.00
2: 30		0.000	0.000	0.000	0.000	0.002	0.0	0.0	0.00
2: 35		0.000	0.000	0.000	0.000	0.002	0.0	0.0	0.00
2: 40		0.000	0.000	0.000	0.000	0.001	0.0	0.0	0.00
2: 45		0.000	0.000	0.000	0.000	0.001	0.0	0.0	0.00
2: 50		0.000	0.000	0.000	0.000	0.001	0.0	0.0	0.00
2: 55		0.000	0.000	0.000	0.000	0.001	0.0	0.0	0.00
3: 0		0.000	0.000	0.000	0.000	0.001	0.0	0.0	0.00
3: 5		0.000	0.000	0.000	0.000	0.001	0.0	0.0	0.00
3: 10		0.000	0.000	0.000	0.000	0.001	0.0	0.0	0.00
3: 15		0.000	0.000	0.000	0.000	0.001	0.0	0.0	0.00
3: 20		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
3: 25		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
3: 30		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
3: 35		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
3: 40		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
3: 45		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
3: 50		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
3: 55		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
4: 0		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
4: 5		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
4: 10		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
4: 15		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
4: 20		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
4: 25		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
4: 30		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
4: 35		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
4: 40		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
4: 45		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
4: 50		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
4: 55		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
5: 0		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
5: 5		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
5: 10		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
5: 15		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
5: 20		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
5: 25		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
5: 30		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
5: 35		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
5: 40		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00
5: 45		0.000	0.000	0.000	0.000	0.000	0.0	0.0	0.00

		bor	100	year	out	sept	28-16			
5: 50	0. 000	0. 000		0. 000	0. 000	0. 000	0. 000	0. 0		0. 00
5: 55	0. 000	0. 000		0. 000	0. 000	0. 000	0. 000	0. 0		0. 00
Maximum Time (h: min)	0. 103			0. 103	0. 000	0. 072		14. 1		0. 00
1:	7			1: 7	0: 0	1: 12				

♀ Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrelli Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

#### MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment D005

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 5	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 10	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 15	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 20	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 25	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 30	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 35	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 40	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 45	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 50	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 55	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
1: 0	0. 041	0. 000	0. 041	0. 000	0. 034	10. 0	0. 00
1: 5	0. 130	0. 000	0. 130	0. 000	0. 119	15. 4	0. 00
1: 10	0. 134	0. 000	0. 134	0. 000	0. 134	15. 5	0. 00
1: 15	0. 112	0. 000	0. 112	0. 000	0. 114	14. 5	0. 00
1: 20	0. 082	0. 000	0. 082	0. 000	0. 086	12. 9	0. 00
1: 25	0. 054	0. 000	0. 054	0. 000	0. 058	11. 0	0. 00
1: 30	0. 035	0. 000	0. 035	0. 000	0. 038	9. 3	0. 00
1: 35	0. 020	0. 000	0. 020	0. 000	0. 023	7. 6	0. 00
1: 40	0. 010	0. 000	0. 010	0. 000	0. 012	5. 8	0. 00
1: 45	0. 003	0. 000	0. 003	0. 000	0. 005	3. 4	0. 00
1: 50	0. 000	0. 000	0. 000	0. 000	0. 001	0. 0	0. 00
1: 55	0. 000	0. 000	0. 000	0. 000	0. 001	0. 0	0. 00
2: 0	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
2: 5	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
2: 10	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
2: 15	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
2: 20	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
2: 25	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
2: 30	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
2: 35	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
2: 40	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
2: 45	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
2: 50	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
2: 55	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00

		bor	100	year	out	sept	28-16			
3: 0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
3: 5	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
3: 10	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
3: 15	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
3: 20	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
3: 25	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
3: 30	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
3: 35	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
3: 40	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
3: 45	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
3: 50	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
3: 55	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
4: 0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
4: 5	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
4: 10	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
4: 15	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
4: 20	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
4: 25	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
4: 30	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
4: 35	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
4: 40	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
4: 45	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
4: 50	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
4: 55	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
5: 0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
5: 5	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
5: 10	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
5: 15	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
5: 20	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
5: 25	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
5: 30	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
5: 35	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
5: 40	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
5: 45	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
5: 50	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00
5: 55	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00	0.00

Maximum Time (h: min) 0.138 0.138 0.000 0.136 15.7 0.00  
1: 6 1: 6 0: 0 1: 7

♀ Dual Drainage Storm Water Management Model (DDSWMM 2.1)

#### Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

#### RESULTS OF SIMULATION FOR MAJOR SYSTEM STORAGE

Storage Unit Number of Inflow Points	Out1
Discharge Point	1
Peak Inflow (cms)	Peak Time (hr: min.)
OUTA	0.062 1: 20

Time (hr: mi n)	Flow (cms)	Storage (cu. m)	Flow (cms)
			0. 00E+00 0. 12E-01 0. 25E-01
0. 37E-01 0. 49E-01 0. 62E-01			
0: 0	0. 000	0. 00	*
0: 5	0. 000	0. 00	*
0: 10	0. 000	0. 00	*
0: 15	0. 000	0. 00	*
0: 20	0. 000	0. 00	*
0: 25	0. 000	0. 00	*
0: 30	0. 000	0. 00	*
0: 35	0. 000	0. 00	*
0: 40	0. 000	0. 00	*
0: 45	0. 000	0. 00	*
0: 50	0. 000	0. 00	*
0: 55	0. 000	0. 00	*
1: 0	0. 000	0. 00	*
1: 5	0. 000	0. 00	*
1: 10	0. 000	0. 00	*
1: 15	0. 000	0. 00	*
1: 20	0. 062	9. 26	
1: 25	0. 048	25. 74	
1: 30	0. 035	38. 28	*****
1: 35	0. 028	47. 79	*****
1: 40	0. 021	55. 14	*****
1: 45	0. 016	60. 76	*****
1: 50	0. 012	65. 10	*****
1: 55	0. 010	68. 40	*****
2: 0	0. 007	70. 89	*****
2: 5	0. 005	72. 71	*****
2: 10	0. 003	73. 97	***
2: 15	0. 002	74. 77	**

		bor	100 year out sept	28-16
2: 20		0.001	75.17	*
2: 25		0.000	75.28	*
2: 30		0.000	75.28	*
2: 35		0.000	75.28	*
2: 40		0.000	75.28	*
2: 45		0.000	75.28	*
2: 50		0.000	75.28	*
2: 55		0.000	75.28	*
3: 0		0.000	75.28	*
3: 5		0.000	75.28	*
3: 10		0.000	75.28	*
3: 15		0.000	75.28	*
3: 20		0.000	75.28	*
3: 25		0.000	75.28	*
3: 30		0.000	75.28	*
3: 35		0.000	75.28	*
3: 40		0.000	75.28	*
3: 45		0.000	75.28	*
3: 50		0.000	75.28	*
3: 55		0.000	75.28	*
4: 0		0.000	75.28	*
4: 5		0.000	75.28	*
4: 10		0.000	75.28	*
4: 15		0.000	75.28	*
4: 20		0.000	75.28	*
4: 25		0.000	75.28	*
4: 30		0.000	75.28	*
4: 35		0.000	75.28	*
4: 40		0.000	75.28	*
4: 45		0.000	75.28	*
4: 50		0.000	75.28	*
4: 55		0.000	75.28	*

bor 100 year out sept 28-16

5: 0	0. 000	75. 28	*
5: 5	0. 000	75. 28	*
5: 10	0. 000	75. 28	*
5: 15	0. 000	75. 28	*
5: 20	0. 000	75. 28	*
5: 25	0. 000	75. 28	*
5: 30	0. 000	75. 28	*
5: 35	0. 000	75. 28	*
5: 40	0. 000	75. 28	*
5: 45	0. 000	75. 28	*
5: 50	0. 000	75. 28	*
5: 55	0. 000	75. 28	*
-----  -----  -----  -----			0. 00E+00    0. 12E-01    0. 25E-01
0. 37E-01    0. 49E-01    0. 62E-01			
Peak    1: 20	0. 062		

♀ Required Detention Volume                75. 28 cu. m.

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

#### RESULTS OF SIMULATION FOR MAJOR SYSTEM STORAGE

Storage Unit	Out2
Number of Inflow Points	1
Discharge Point	Peak Inflow (cms)
OUTB	0. 060
	Peak Time (hr: min.)
	1: 6

Time (hr: min.)	Flow (cms)	Storage (cu. m)	Flow (cms)
			0. 00E+00    0. 11E-01    0. 23E-01
0. 34E-01    0. 46E-01    0. 57E-01			
-----  -----  -----  -----			

		bor	100	year	out	sept	28-16
				0.00			*
0: 0		0.000		0.00			*
0: 5		0.000		0.00			*
0: 10		0.000		0.00			*
0: 15		0.000		0.00			*
0: 20		0.000		0.00			*
0: 25		0.000		0.00			*
0: 30		0.000		0.04			*
0: 35		0.001		0.20			*
0: 40		0.001		0.49			*
0: 45		0.001		0.85			**
0: 50		0.003		1.44			***
0: 55		0.004		2.38			****
1: 0		0.014		5.03			*****
1: 5		0.052		14.93			
1: 10		0.057		32.30			
1: 15		0.046		47.75			
1: 20		0.030		59.17			*****
1: 25		0.018		66.34			*****
1: 30		0.013		70.92			*****
1: 35		0.009		74.27			*****
1: 40		0.007		76.74			*****
1: 45		0.005		78.60			*****
1: 50		0.004		80.01			***
1: 55		0.003		81.08			**
2: 0		0.002		81.91			**
2: 5		0.002		82.57			**
2: 10		0.002		83.12			**
2: 15		0.001		83.60			**
2: 20		0.001		84.02			**
2: 25		0.001		84.40			**
2: 30		0.001		84.74			*
2: 35		0.001		85.04			*

		bor	100 year out sept 28-16
2: 40		0. 001	85. 33   *
2: 45		0. 001	85. 59   *
2: 50		0. 001	85. 82   *
2: 55		0. 001	86. 05   *
3: 0		0. 001	86. 25   *
3: 5		0. 001	86. 45   *
3: 10		0. 001	86. 63   *
3: 15		0. 000	86. 79   *
3: 20		0. 000	86. 91   *
3: 25		0. 000	87. 00   *
3: 30		0. 000	87. 07   *
3: 35		0. 000	87. 13   *
3: 40		0. 000	87. 18   *
3: 45		0. 000	87. 23   *
3: 50		0. 000	87. 26   *
3: 55		0. 000	87. 30   *
4: 0		0. 000	87. 33   *
4: 5		0. 000	87. 36   *
4: 10		0. 000	87. 39   *
4: 15		0. 000	87. 42   *
4: 20		0. 000	87. 44   *
4: 25		0. 000	87. 47   *
4: 30		0. 000	87. 49   *
4: 35		0. 000	87. 51   *
4: 40		0. 000	87. 53   *
4: 45		0. 000	87. 55   *
4: 50		0. 000	87. 57   *
4: 55		0. 000	87. 59   *
5: 0		0. 000	87. 61   *
5: 5		0. 000	87. 62   *
5: 10		0. 000	87. 64   *

		bor	100 year out sept 28-16		
5: 15		0. 000	87. 65	*	
5: 20		0. 000	87. 67	*	
5: 25		0. 000	87. 68	*	
5: 30		0. 000	87. 70	*	
5: 35		0. 000	87. 71	*	
5: 40		0. 000	87. 73	*	
5: 45		0. 000	87. 74	*	
5: 50		0. 000	87. 75	*	
5: 55		0. 000	87. 77	*	
0. 34E-01	-----	0. 46E-01	-----	0. 57E-01	-----
Peak	0. 034	1:	0. 060	6	
					0. 00E+00 0. 11E-01 0. 23E-01

<sup>♀</sup>      Requi red Detention Volum e      87. 77 cu. m.  
<sup>†</sup>      Dual Drai nage Storm Water Management Model (DDSWMM 2. 1)

Borrel lo Subdi vi si on

DDSWMM anal ysis, 3 hour 100 year Chi cago Storm

#### RESULTS OF SIMULATION FOR MAJOR SYSTEM STORAGE

Storage Unit	Out3			
Number of Inflow Points	1			
Discharge Point	Peak Inflow (cms)	Peak Time (hr: min.)		
OUTC	0. 027	1: 15		
Time (hr: min.)	Flow (cms)	Storage (cu. m)	Flow (cms)	
0. 16E-01	0. 22E-01	0. 27E-01	0. 00E+00 0. 55E-02 0. 11E-01	
0: 0		0. 000	0. 00	*
0: 5		0. 000	0. 00	*
0: 10		0. 000	0. 00	*
0: 15		0. 000	0. 00	*

bor 100 year out sept 28-16

0: 20	0. 000	0. 00	*
0: 25	0. 000	0. 00	*
0: 30	0. 000	0. 00	*
0: 35	0. 000	0. 00	*
0: 40	0. 000	0. 01	*
0: 45	0. 000	0. 03	*
0: 50	0. 000	0. 06	*
0: 55	0. 000	0. 15	*
1: 0	0. 002	0. 46	****
1: 5	0. 006	1. 55	*****
1: 10	0. 027	6. 50	
1: 15	0. 027	14. 72	
1: 20	0. 019	21. 59	
1: 25	0. 016	26. 77	*****
1: 30	0. 013	30. 98	*****
1: 35	0. 011	34. 46	*****
1: 40	0. 009	37. 41	*****
1: 45	0. 008	39. 96	*****
1: 50	0. 007	42. 21	*****
1: 55	0. 006	44. 23	*****
2: 0	0. 006	46. 05	*****
2: 5	0. 005	47. 73	*****
2: 10	0. 005	49. 28	*****
2: 15	0. 005	50. 72	*****
2: 20	0. 004	52. 08	*****
2: 25	0. 004	53. 36	*****
2: 30	0. 004	54. 57	*****
2: 35	0. 004	55. 72	*****
2: 40	0. 004	56. 81	*****
2: 45	0. 003	57. 85	*****
2: 50	0. 003	58. 84	*****

		bor	100 year out sept	28-16
2: 55		0. 003	59. 79	*****
3: 0		0. 003	60. 70	*****
3: 5		0. 003	61. 57	*****
3: 10		0. 003	62. 42	*****
3: 15		0. 003	63. 23	*****
3: 20		0. 003	64. 02	*****
3: 25		0. 002	64. 78	*****
3: 30		0. 002	65. 52	*****
3: 35		0. 002	66. 23	*****
3: 40		0. 002	66. 93	*****
3: 45		0. 002	67. 61	*****
3: 50		0. 002	68. 27	****
3: 55		0. 002	68. 91	****
4: 0		0. 002	69. 53	****
4: 5		0. 002	70. 14	****
4: 10		0. 002	70. 74	****
4: 15		0. 002	71. 32	****
4: 20		0. 002	71. 88	****
4: 25		0. 002	72. 44	****
4: 30		0. 002	72. 98	****
4: 35		0. 002	73. 51	****
4: 40		0. 002	74. 03	****
4: 45		0. 002	74. 54	****
4: 50		0. 002	75. 03	***
4: 55		0. 002	75. 52	***
5: 0		0. 002	76. 00	***
5: 5		0. 002	76. 47	***
5: 10		0. 002	76. 93	***
5: 15		0. 001	77. 38	***
5: 20		0. 001	77. 83	***
5: 25		0. 001	78. 26	***
5: 30		0. 001	78. 69	***

			bor 100 year out sept 28-16
5: 35	0. 001	79. 11	***
5: 40	0. 001	79. 53	***
5: 45	0. 001	79. 93	***
5: 50	0. 001	80. 33	***
5: 55	0. 001	80. 73	***
-----  -----  -----  -----			
0. 16E-01	0. 22E-01	0. 27E-01	0. 00E+00 0. 55E-02 0. 11E-01
Peak	1: 15	0. 027	

♀ Required Detention Volume            80. 73 cu. m.  
 † Dual Drainage Storm Water Management Model (DDSWMM 2.1)

#### Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

#### RESULTS OF SIMULATION FOR MAJOR SYSTEM STORAGE

Storage Unit Number of Inflow Points	Out4		
Discharge Point	Peak Inflow (cms)	Peak Time (hr: min.)	
OUT1B	0. 136	1: 7	
Time (hr: min.)	Flow (cms)	Storage (cu. m)	Flow (cms)
0. 80E-01	0. 11E+00	0. 13E+00	0. 00E+00 0. 27E-01 0. 54E-01
-----  -----  -----  -----			
0: 0	0. 000	0. 00	*
0: 5	0. 000	0. 00	*
0: 10	0. 000	0. 00	*
0: 15	0. 000	0. 00	*
0: 20	0. 000	0. 00	*
0: 25	0. 000	0. 00	*
0: 30	0. 000	0. 00	*

	bor	100	year	out	sept	28-16
0: 35	0. 000	0. 00			*	
0: 40	0. 000	0. 00			*	
0: 45	0. 000	0. 00			*	
0: 50	0. 000	0. 00			*	
0: 55	0. 000	0. 01			*	
1: 0	0. 034	5. 16			*****	
1: 5	0. 119	28. 22			*****	
1: 10	0. 134	67. 86			*****	
1: 15	0. 114	105. 06			*****	
1: 20	0. 086	135. 06			*****	
1: 25	0. 058	156. 71			*****	
1: 30	0. 038	171. 17			*****	
1: 35	0. 023	180. 32			*****	
1: 40	0. 012	185. 57			****	
1: 45	0. 005	188. 08			**	
1: 50	0. 001	188. 96			*	
1: 55	0. 001	189. 22			*	
2: 0	0. 000	189. 33			*	
2: 5	0. 000	189. 39			*	
2: 10	0. 000	189. 43			*	
2: 15	0. 000	189. 45			*	
2: 20	0. 000	189. 47			*	
2: 25	0. 000	189. 48			*	
2: 30	0. 000	189. 50			*	
2: 35	0. 000	189. 51			*	
2: 40	0. 000	189. 51			*	
2: 45	0. 000	189. 52			*	
2: 50	0. 000	189. 52			*	
2: 55	0. 000	189. 53			*	
3: 0	0. 000	189. 53			*	
3: 5	0. 000	189. 54			*	
3: 10	0. 000	189. 54			*	

bor 100 year out sept 28-16

3: 15		0.000	189.54	*
3: 20		0.000	189.54	*
3: 25		0.000	189.55	*
3: 30		0.000	189.55	*
3: 35		0.000	189.55	*
3: 40		0.000	189.55	*
3: 45		0.000	189.55	*
3: 50		0.000	189.55	*
3: 55		0.000	189.55	*
4: 0		0.000	189.55	*
4: 5		0.000	189.56	*
4: 10		0.000	189.56	*
4: 15		0.000	189.56	*
4: 20		0.000	189.56	*
4: 25		0.000	189.56	*
4: 30		0.000	189.56	*
4: 35		0.000	189.56	*
4: 40		0.000	189.56	*
4: 45		0.000	189.56	*
4: 50		0.000	189.56	*
4: 55		0.000	189.56	*
5: 0		0.000	189.56	*
5: 5		0.000	189.56	*
5: 10		0.000	189.56	*
5: 15		0.000	189.56	*
5: 20		0.000	189.56	*
5: 25		0.000	189.56	*
5: 30		0.000	189.56	*
5: 35		0.000	189.56	*
5: 40		0.000	189.56	*
5: 45		0.000	189.56	*

			bor	100	year	out	sept	28-16	
5: 50		0. 000		189.	56		*		
5: 55		0. 000		189.	56		*		
-----  -----  -----  -----							0. 00E+00	0. 27E-01	0. 54E-01
0. 80E-01	0. 11E+00	0. 13E+00							
Peak	1:	7		0. 136					

Required Detention Volume      189. 56 cu. m.

<sup>†</sup> Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

#### RESULTS OF SIMULATION FOR MAJOR SYSTEM STORAGE

Storage Unit                        Out5  
Number of Inflow Points            1

Discharge Point	Peak Inflow (cms)	Peak Time (hr:min.)
OUTD	0. 038	1: 8

Time (hr:min.)	Flow (cms)	Storage (cu.m.)	Flow (cms)			
			0. 00E+00    0. 75E-02    0. 15E-01			
0. 22E-01	0. 30E-01	0. 37E-01				
-----  -----  -----  -----						
0: 0	0. 000	0. 00	*			
0: 5	0. 000	0. 00	*			
0: 10	0. 000	0. 00	*			
0: 15	0. 000	0. 00	*			
0: 20	0. 000	0. 00	*			
0: 25	0. 000	0. 00	*			
0: 30	0. 000	0. 00	*			
0: 35	0. 000	0. 02	*			
0: 40	0. 000	0. 05	*			
0: 45	0. 000	0. 10	*			
0: 50	0. 001	0. 22	*			

bor 100 year out sept 28-16

0: 55	0. 001	0. 49	**
1: 0	0. 006	1. 52	*****
1: 5	0. 022	5. 59	*****
1: 10	0. 037	15. 55	*****
1: 15	0. 032	25. 98	*****
1: 20	0. 027	34. 83	*****
1: 25	0. 023	42. 28	*****
1: 30	0. 018	48. 45	*****
1: 35	0. 016	53. 57	*****
1: 40	0. 013	57. 89	*****
1: 45	0. 011	61. 57	*****
1: 50	0. 010	64. 76	*****
1: 55	0. 009	67. 56	*****
2: 0	0. 008	70. 03	*****
2: 5	0. 007	72. 25	*****
2: 10	0. 006	74. 24	*****
2: 15	0. 006	76. 06	*****
2: 20	0. 005	77. 72	*****
2: 25	0. 005	79. 25	*****
2: 30	0. 005	80. 67	*****
2: 35	0. 004	82. 00	*****
2: 40	0. 004	83. 24	*****
2: 45	0. 004	84. 41	*****
2: 50	0. 004	85. 52	****
2: 55	0. 003	86. 56	****
3: 0	0. 003	87. 56	****
3: 5	0. 003	88. 50	****
3: 10	0. 003	89. 41	***
3: 15	0. 003	90. 27	***
3: 20	0. 003	91. 10	***
3: 25	0. 003	91. 90	***

		bor	100 year out sept	28-16
3: 30		0. 003	92. 68	****
3: 35		0. 002	93. 42	****
3: 40		0. 002	94. 15	****
3: 45		0. 002	94. 85	****
3: 50		0. 002	95. 53	***
3: 55		0. 002	96. 18	***
4: 0		0. 002	96. 82	***
4: 5		0. 002	97. 45	***
4: 10		0. 002	98. 05	***
4: 15		0. 002	98. 64	***
4: 20		0. 002	99. 21	***
4: 25		0. 002	99. 77	***
4: 30		0. 002	100. 32	***
4: 35		0. 002	100. 85	***
4: 40		0. 002	101. 37	***
4: 45		0. 002	101. 88	***
4: 50		0. 002	102. 38	***
4: 55		0. 002	102. 86	***
5: 0		0. 002	103. 34	***
5: 5		0. 002	103. 81	***
5: 10		0. 002	104. 26	***
5: 15		0. 001	104. 71	**
5: 20		0. 001	105. 15	**
5: 25		0. 001	105. 58	**
5: 30		0. 001	106. 00	**
5: 35		0. 001	106. 41	**
5: 40		0. 001	106. 82	**
5: 45		0. 001	107. 22	**
5: 50		0. 001	107. 61	**
5: 55		0. 001	108. 00	**
-----  -----  -----  -----  -----				
				0. 00E+00 0. 75E-02 0. 15E-01

0.22E-01 0.30E-01 0.37E-01  
 Peak 1: 8 0.038  
 bor 100 year out sept 28-16

<sup>♀</sup> Required Detention Volume 108.00 cu. m.  
 Dual Drainage Storm Water Management Model (DDSWMM 2.1)

#### Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm

#### MAJOR SYSTEM

#### SUMMARY OF SIMULATION RESULTS

No.	Segment Max.	Peak Flow (cms)	Peak Time (hr: min.)	Max. Depth (cm)	Max. Capture (l/s)	Inlet Restriction (?)	D/S Pipe
1 SWM14	0.00	0.011	1: 5	2.48	0.00	-	X
2 SWM13	0.00	0.011	1: 5	2.19	0.00	-	X
3 LP001	0.00	0.021	1: 6	2.80	0.00	-	X
4 SWM12	0.00	0.023	1: 5	3.15	0.00	-	X
5 SWM11	0.00	0.009	1: 5	2.25	0.00	-	X
6 LP002	1.80	0.051	1: 6	4.67	20.00	N/A	207
7 SWM10	0.00	0.046	1: 5	4.52	0.00	-	X
8 SWM8	0.00	0.019	1: 9	3.47	0.00	-	X
9 LP003	5.70	0.063	1: 6	5.54	4.52	N/A	205
10 SWM3	0.00	0.033	1: 5	4.35	0.00	-	X
11 SWM4	0.00	0.083	1: 5	5.60	0.00	-	X
12 LP004	5.70	0.113	1: 7	6.90	9.87	N/A	205
13 SWM2	0.00	0.116	1: 12	5.19	0.00	-	X
14 SWM1	0.00	0.056	1: 5	5.31	0.00	-	X
15 LP005	1.30	0.158	1: 6	6.09	20.00	N/A	202
16 SWM7	0.00	0.080	1: 5	4.57	20.00	YES	202
17 SWM9	0.00	0.028	1: 5	1.47	11.64	NO	205
18 SWM5	55.00	0.103	1: 5	5.06	15.00	N/A	207
19 SWM6	0.00	0.057	1: 5	2.96	20.00	YES	202

		bor	100	year	out	sept	28-16		
20 SWM15	0. 042	1:	5		2. 18		0. 00	-	X
0. 00									
21 D001	0. 021	1:	6		7. 72		0. 00	-	X
0. 00									
22 D002	0. 031	1:	6		8. 95		0. 00	-	X
0. 00									
23 D003	0. 059	1:	6		11. 36		0. 00	-	X
0. 00									
24 D004	0. 103	1:	7		14. 05		0. 00	-	X
0. 00									
25 D005	0. 138	1:	6		15. 73		0. 00	-	X
0. 00									

\*\*\* SIMULATION ENDED NORMALLY \*\*\*

```
*****
* Simulation Starting Date      September 08, 16
*                   Time          08:45:39.13
* Simulation Ending   Date      September 08, 16
*                   Time          08:45:40.21
* Duration of Simulation        0.02 Minutes
*****
```

#### Data Files

-----  
Input Data File Name                               bor100.txt  
Output File Name                                     sept8

bor100+20%.txt

' Borrellio Subdivision  
' DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

\*\*\*\*\*  
\* DDSWMM Analysis by RLD - September 2016  
\* Bor100+20%.txt  
\*\*\*\*\*  
\*  
\* IUNIT DELTC NDELTC IEVAL QLIMIT STEP  
1 5 72 3 20.0 1  
\* IUNIT =1 for metric  
\* DELTC = time increment for calculation (minutes)  
\* NDELTC = number of computational time steps (maximum = 300)  
\* IEVAL = 1 if pipe sizes are given and it is required to revise  
these sizes, if necessary, based on free surface flow  
\* QLIMIT = Default value of limiting capacity of inlets. Value can be overridden  
for individual inlets by the values assigned to (QLIM) on data group (7)  
\* STEP = Interval between print-out  
  
\* RAINFOAL DATA  
\*\*\*\*\*  
\* JULDAY TZERO  
02290 0.0  
\* JULDAY = Initial Julian calendar  
\* TZERO = initial time [0hrs to 24hrs]  
\* DELTR NDELTR  
10.0 19  
\* 19 STEPS OF RAINFOAL INTENSITIES AT 10 MINS INTERVAL  
0 7.255 9.05 12.191 19.163 48.786 214.271 64.859 32.783 21.888 16.484  
13.271 11.142 9.629 8.496 7.616 6.912 6.336 5.855  
\* DELTR = time increment for rainfall hyetograph (minutes)  
\* NDELTR = number of time increments for rainfall hyetograph  
  
\* MINOR SYSTEM CHARACTERISTICS  
\* IRTP NP NPD XP SP CP DP QB IPRTP  
\* IRTP=0, routing of minor system flow (for this pipe) will be performed  
\* NP = sewer identification number/name [node point]  
\* NPD = identification number/name of downstream sewer [node point downstream]  
\* XP = length of sewer (m)  
\* SP = invert slope (m/m)  
\* CP = Manning's roughness coefficient  
\* DP = pipe diameter (mm)  
\* QB = base flow (cubes)  
\* IPRTP = option for printing time history of pipe flow (1 or 0) (0=no print)  
  
\* Street A  
\* 0 '210' '209' 10.3 0.0097 0.013 254.0 0.0 0  
\* 0 '209' '208' 19.5 0.0103 0.013 254.0 0.0 0  
\* 0 '208' '207' 8.6 0.0093 0.013 254.0 0.0 0  
\* 0 '207' '206' 44.4 0.0020 0.013 457.2 0.0 0  
\* 0 '206' '205a' 7.3 0.0027 0.013 457.2 0.0 0  
\* 0 '205a' '205' 11.2 0.0027 0.013 457.2 0.0 0  
\* 0 '205' '203' 36.8 0.0030 0.013 457.2 0.0 0  
\* 0 '203' '202' 31.6 0.0025 0.013 457.2 0.0 0  
\* 0 '202' '201' 43.6 0.0070 0.013 457.2 0.0 0  
\* 0 '201' '202a' 85.0 0.0073 0.013 457.2 0.0 0  
\* dummy pipe  
\* 0 'X' '210' 85.0 0.0073 0.013 457.2 0.0 0  
  
\*ENDMNR  
\* to terminate minor system data entry  
\* if the drainage system has no storage for minor system, enter

bor100+20%.txt

\* terminators as below.  
\*ENDMNR1  
\* must be entered even if no storage is required  
\*ENDMNR2  
\* must be entered even if no storage is required  
\*ENDMNR3  
\* must be entered even if no storage is required  
\* MAJOR SYSTEM CHARACTERISTICS  
\* maximum of 50 storage types  
\* IS W2 SX YCURB CNS SO SROW CNROW YMAX  
\* IS = identification of street segment type  
\* W2 = segment width (m)  
\* SX = pavement cross slope (m/m)  
\* YCURB = height of curb (cm)  
\* CNS = Manning's roughness coefficient for pavement  
\* SO = longitudinal slope  
\* SROW = cross slope of shoulder  
\* CNROW = Manning's roughness coefficient for shoulder  
\* YMAX = Maximum water depth (measured from bottom of curb)  
\* for calculation of street carrying capacity  
\*  
\*  
\* Maximum water depth assumed as 30 cm  
\* Street A  
\*  

1	4.25	0.030	15	0.013	0.0138	0.02	0.025	30
2	4.25	0.030	15	0.013	0.0076	0.02	0.025	30
3	4.25	0.030	15	0.013	0.0237	0.02	0.025	30
4	4.25	0.030	15	0.013	0.0083	0.02	0.025	30
5	4.25	0.030	15	0.013	0.0050	0.02	0.025	30
6	4.25	0.030	15	0.013	0.0051	0.02	0.025	30
7	4.25	0.030	15	0.013	0.0200	0.02	0.025	30
8	118.00	0.010	30	0.025	0.0090	0.02	0.025	100
9	4.25	0.030	15	0.013	0.0001	0.02	0.025	30

*	*
*	*
ENDSTR	
* terminator for major system characteristics data set	
* INLET CAPTURE CHARACTERISTICS	
* IDCB NJC	
1      8	
* QAPP QCAP	
0.      0.	
10.     10.	
30.     30.	
60.     60.	
90.     90.	
130.    130.	
500.    500.	
1000.   1000.	

ENDIN1	
ENDIN2	
* application for areas	
* IDCB DET3 NPTS3	
2      55.0      2	
* QAPP QCAP	
0.0    0.0	
55.0   15.0	
* application for areas	
* IDCB DET3 NPTS3	
3      1.8      2	
* QAPP QCAP	
0.0    0.0	

bor100+20%.txt

```
    1.8   20.0
* applicabl e for areas
*  IDCB   DET3   NPTS3
  4      5.7      2
* QAPP   QCAP
  0.0   0.0
 17.9   14.2
* applicabl e for areas
*  IDCB   DET3   NPTS3
  5      1.3      2
* QAPP   QCAP
  0.0   0.0
 1.3   20.0
* applicabl e for areas
*  IDCB   DET3   NPTS3
  6      5.7      2
* QAPP   QCAP
  0.0   0.0
 17.9   31.0
* applicabl e for areas
*  IDCB   DET3   NPTS3
  7      20.0     3
* QAPP   QCAP
  0.0   0.0
 1.0   18.0
 20.0   20.0
* applicabl e for areas
*  IDCB   DET3   NPTS3
  8      25.0     3
* QAPP   QCAP
  0.0   0.0
 1.0   18.0
 25.0   20.0
* applicabl e for areas
*  IDCB   DET3   NPTS3
  9      30.0     3
* QAPP   QCAP
  0.0   0.0
 1.0   18.0
 30.0   20.0
* applicabl e for areas
*  IDCB   DET3   NPTS3
 10     35.0     3
* QAPP   QCAP
  0.0   0.0
 1.0   18.0
 35.0   20.0
* applicabl e for areas
*  IDCB   DET3   NPTS3
 11     50.0     3
* QAPP   QCAP
  0.0   0.0
 1.0   18.0
 50.0   20.0
* applicabl e for areas
*  IDCB   DET3   NPTS3
 12     75.0     3
* QAPP   QCAP
  0.0   0.0
 1.0   18.0
 75.0   20.0
* applicabl e for areas
*  IDCB   DET3   NPTS3
```

bor100+20%.txt

```
*      13      1.0      2
*    QAPP    QCAP
  0.0      0.0
  1.0     58.4
* appli cable for areas
*    IDCB    DET3    NPTS3
  14      3.0      3
*    QAPP    QCAP
  0.0      0.0
  1.0     11.4
  3.0     13.4
* appli cable for areas
*    IDCB    DET3    NPTS3
  15      5.0      3
*    QAPP    QCAP
  0.0      0.0
  1.0     11.4
  5.0     13.4
* appli cable for areas
*    IDCB    DET3    NPTS3
  16     33.0      3
*    QAPP    QCAP
  0.0      0.0
  1.0      7.0
 33.0     9.0
* appli cable for areas
*    IDCB    DET3    NPTS3
  17     32.0      3
*    QAPP    QCAP
  0.0      0.0
  1.0     4.8
 32.0     6.8
* appli cable for areas
*    IDCB    DET3    NPTS3
  18     15.5      3
*    QAPP    QCAP
  0.0      0.0
  1.0     6.5
 15.5     8.5
* appli cable for areas
*    IDCB    DET3    NPTS3
  19     19.0      3
*    QAPP    QCAP
  0.0      0.0
  1.0     1.0
 19.0     3.3
* appli cable for areas
*    IDCB    DET3    NPTS3
  20     15.5      3
*    QAPP    QCAP
  0.0      0.0
  1.0     7.4
 15.5     9.4
*
```

\*\*

ENDIN3

\* MAJOR SYSTEM SEGMENT DATA

\*\*-----

\* IRTS = Option for major system flow routing

\* NS = identification number/name of major system segment

\* NSD = identification number/name of major system segment downstream

\* XS = length of segment

bor100+20%.txt

\* IDSS = segment type (as per segment data list)  
 \* NUMCB = number of storm inlets within street segment  
 \* IINC = inlet type (as per segment data list)  
 \* QLIM = maximum allowable inlet capture  
 \* NPD = pipe receiving inlet flow  
 \* IPRTS = option for printing time history of segment (=o, no printing)  
 \* routing is performed (for this segment)

---

	IRTS	NS	NSD	XS	IDSS	NUMCB	IINC	QLIM	NPD
IPRTS									
* Road Drainage Areas									
0	'SWM14'	'LP001'	40	4	0	1	0.	'X'	0
0	'SWM13'	'LP001'	29	1	0	1	0.	'X'	0
1	'LP001'	'D001'	10	7	0	1	0.	'X'	0
0	'SWM12'	'LP002'	41	1	0	1	0.	'X'	0
0	'SWM11'	'LP002'	16	4	0	1	0.	'X'	0
1	'LP002'	'D002'	10	4	1	3	20.	'207'	0
0	'SWM10'	'LP003'	48	4	0	1	0.	'X'	0
0	'SWM8'	'LP003'	27	6	0	1	0.	'X'	0
1	'LP003'	'D003'	10	6	1	4	14.2	'205'	0
0	'SWM3'	'LP004'	28	6	0	1	0.	'X'	0
0	'SWM4'	'LP004'	107	4	0	1	0.	'X'	0
1	'LP004'	'D004'	10	6	1	6	31.	'205'	0
0	'SWM2'	'LP005'	81	3	0	1	0.	'X'	0
0	'SWM1'	'LP005'	45	5	0	1	0.	'X'	0
1	'LP005'	'D005'	10	7	1	5	20.	'202'	0
0	'SWM7'	'OUTB'	71	3	1	1	20.	'202'	0
* Rear Yard Drainage									
0	'SWM9'	'SWM8'	37	8	1	1	25.	'205'	0
0	'SWM5'	'OUTA'	157	8	1	2	15.	'207'	0
0	'SWM6'	'OUTC'	88	8	1	1	20.	'202'	0
0	'SWM15'	'OUTD'	40	8	0	1	0.	'X'	0
* Dummy Segments									
0	'D001'	'LP002'	7	9	0	1	0.	'X'	1
0	'D002'	'SWM10'	20	9	0	1	0.	'X'	1
0	'D003'	'SWM7'	50	9	0	1	0.	'X'	1
0	'D004'	'SWM2'	65	9	0	1	0.	'X'	1
0	'D005'	'OUT1B'	8	9	0	1	0.	'X'	1

#### ENDMJR

\* MAJOR SYSTEM STORAGE UNITS

IDSTS	NUSS	NSTOR
'Out1'	1	'OUTA'
'Out2'	1	'OUTB'
'Out3'	1	'OUTC'
'Out4'	1	'OUT1B'
'Out5'	1	'OUTD'

\*

#### ENDMJRS

\* INFILTRATION PARAMETERS FOR RUNOFF CALCULATIONS

MAX	MIN	DECAY
76.2	13.2	.00115

#### ENDUAH

\* SUBAREA DATA FOR SWMM RUNOFF

DET1 MP	DET2	IPRTW	NWDW	ASW	PIMP	CNIMP	CNP	S	WLAT
'SWM1'	'SWM1'		0.18	41.	0.013	0.25	0.02	45	1.57
4.67	0								
'SWM2'	'SWM2'		0.24	35.	0.013	0.25	0.02	81	1.57
4.67	0								
'SWM3'	'SWM3'		0.11	38.	0.013	0.25	0.02	28	1.57
4.67	0								
'SWM4'	'SWM4'		0.25	37.	0.013	0.25	0.02	107	1.57

bor100+20%.txt

4.67	0	'SWM5'	0.49	18.	0.013	0.25	0.02	157	1.57
4.67	0	'SWM6'	0.22	24.	0.013	0.25	0.02	88	1.57
4.67	0	'SWM7'	0.16	41.	0.013	0.25	0.02	71	1.57
4.67	0	'SWM8'	0.03	52.	0.013	0.25	0.02	27	1.57
4.67	0	'SWM9'	0.10	30.	0.013	0.25	0.02	37	1.57
4.67	0	'SWM10'	0.07	54.	0.013	0.25	0.02	48	1.57
4.67	0	'SWM11'	0.02	51.	0.013	0.25	0.02	16	1.57
4.67	0	'SWM12'	0.06	41.	0.013	0.25	0.02	41	1.57
4.67	0	'SWM13'	0.02	73.	0.013	0.25	0.02	29	1.57
4.67	0	'SWM14'	0.02	70.	0.013	0.25	0.02	40	1.57
4.67	0	'SWM15'	0.21	23.	0.013	0.25	0.02	40	1.57

\* NW = identification number/name of subarea

\* NSDW = identification number/name of major segment receiving surface runoff

\* ASW area of subarea (ha.)

\* PI MP = percentage impervious

\* CNI MP = Manning's roughness coefficient for impervious area

\* CNP = Manning's roughness coefficient for pervious area

\* S = average slope

\* WLAT = subarea width

\* DETIMP = detention storage for impervious area

\* DETP = detention storage for pervious area

\* IRTW = option for printing and plotting of surface runoff hydrograph (=0, no printing)

ENDSUB1

ENDSUB2

ENDSUB3

bor100-20% out sept 28-16  
\*\*\*\*\*  
\* D D S W M M (release 2.1) \*  
\* The Dual Drainage Storm Water Management Model \*  
\* Copyright \*  
\* ----- \*  
\* AMK Associates International Ltd. \*  
\*\*\*\*\*

This release of DDSWMM will run with a maximum of

500 minor system segments (pipes), including outlets  
500 major system (street) segments, including outlets  
500 subcatchments  
30 storage units for the minor system  
30 storage units for the major system  
300 computational time steps  
300 increments for rainfall hyetograph  
50 storm inlet types  
20 points describing the inlet capture curve  
50 major system segment types  
5 street segments discharging into a street junction  
5 pipes discharging into a pipe junction  
5 subcatchments discharging into a major system segment  
5 inlet groups discharging into a pipe  
30 unit area hydrographs

For other program constraints, please refer to the users manual

<sup>†</sup> Dual Drainage Storm Water Management Model (DDSWMM 2.1)

#### Borrelli Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

#### RUN CONTROL PARAMETERS

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Measuring units	Metric
Time increment for calculation	5.00 minutes
Number of computational steps	72
Default limiting capacity of inlets	20.00 l/s
Total simulation time	5:55 (hrs:mins)
Interval between printout	1

<sup>†</sup> Calculation for the minor system is not included in this simulation

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

#### Borrelli Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

bor100-20% out sept 28-16

RAI NFALL DATA			Initial Julian Date
02290	Initial Time		
0.00 hours			
Time (mm/hr)	Rainfall (hr: min)	Rainfall (mm/hr)	Rainfall intensity
0.13E+03	0.17E+03	0.21E+03	0.00E+00 0.43E+02 0.86E+02
0: 0	0.00		*
0: 10	7.26		**
0: 20	9.05		***
0: 30	12.19		***
0: 40	19.16		*****
0: 50	48.79		*****
1: 0	214.27		
1: 10	64.86		*****
1: 20	32.78		*****
1: 30	21.89		*****
1: 40	16.48		****
1: 50	13.27		****
2: 0	11.14		***
2: 10	9.63		***
2: 20	8.50		**
2: 30	7.62		**
2: 40	6.91		**
2: 50	6.34		**
3: 0	5.86		**
0.13E+03	0.17E+03	0.21E+03	0.00E+00 0.43E+02 0.86E+02

† Rainfall duration 3:10 (hrs: mins.)

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision  
bor100-20% out sept 28-16

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness (n)
1 30.0	4.25	0.030	15.0	0.0130	0.014	0.020	0.0250

RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0.00	0.00	0.00
1.50	0.00	0.50
3.00	0.02	1.00
4.50	0.06	1.50
6.00	0.12	2.00
7.50	0.23	2.50
9.00	0.37	3.00
10.50	0.55	3.50
12.00	0.79	4.00
13.50	1.08	4.25
15.00	1.43	4.25
16.50	1.82	5.00
18.00	2.26	5.75
19.50	2.76	6.50
21.00	3.32	7.25
22.50	3.95	8.00
24.00	4.64	8.75
25.50	5.41	9.50
27.00	6.24	10.25
28.50	7.15	11.00
30.00	8.14	11.75

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

MAJOR SYSTEM RATING CURVE

bor100-20% out sept 28-16

---

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Hei ght of Curb (cm)	Manni ng (n)	Long. Slope (m/m)	Shoul der Cross Slope (m/m)	Shoul der Roughness (n)
2 30.0	4.25	0.030	15.0	0.0130	0.008	0.020	0.0250

RATING CURVE

Depth (cm)	Fl ow (cms)	Spread (m)
0.00	0.00	0.00
1.50	0.00	0.50
3.00	0.01	1.00
4.50	0.04	1.50
6.00	0.09	2.00
7.50	0.17	2.50
9.00	0.27	3.00
10.50	0.41	3.50
12.00	0.59	4.00
13.50	0.80	4.25
15.00	1.06	4.25
16.50	1.35	5.00
18.00	1.68	5.75
19.50	2.05	6.50
21.00	2.47	7.25
22.50	2.93	8.00
24.00	3.45	8.75
25.50	4.01	9.50
27.00	4.63	10.25
28.50	5.31	11.00
30.00	6.04	11.75

†

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

MAJOR SYSTEM RATING CURVE

---

Type Maximum Flow Depth	Pavement Width (m)	Pavement Cross Slope	Hei ght of Curb	Manni ng (n)	Long. Slope (m/m)	Shoul der Cross Slope	Shoul der Roughness (n)
----------------------------------	--------------------------	----------------------------	-----------------------	-----------------	-------------------------	-----------------------------	-------------------------------

(cm)		bor100-20% out sept 28-16 (m/m)					(m/m)
3	4. 25	0. 030	15. 0	0. 0130	0. 024	0. 020	0. 0250
30. 0							

#### RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0. 00	0. 00	0. 00
1. 50	0. 00	0. 50
3. 00	0. 03	1. 00
4. 50	0. 08	1. 50
6. 00	0. 16	2. 00
7. 50	0. 30	2. 50
9. 00	0. 48	3. 00
10. 50	0. 73	3. 50
12. 00	1. 04	4. 00
13. 50	1. 42	4. 25
15. 00	1. 87	4. 25
16. 50	2. 38	5. 00
18. 00	2. 96	5. 75
19. 50	3. 62	6. 50
21. 00	4. 36	7. 25
22. 50	5. 18	8. 00
24. 00	6. 09	8. 75
25. 50	7. 09	9. 50
27. 00	8. 18	10. 25
28. 50	9. 38	11. 00
30. 00	10. 67	11. 75

†

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrellio Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

#### MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. Slope (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness (n)
4 30. 0	4. 25	0. 030	15. 0	0. 0130	0. 008	0. 020	0. 0250

bor100-20% out sept 28-16  
RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0. 00	0. 00	0. 00
1. 50	0. 00	0. 50
3. 00	0. 02	1. 00
4. 50	0. 04	1. 50
6. 00	0. 10	2. 00
7. 50	0. 18	2. 50
9. 00	0. 28	3. 00
10. 50	0. 43	3. 50
12. 00	0. 61	4. 00
13. 50	0. 84	4. 25
15. 00	1. 11	4. 25
16. 50	1. 41	5. 00
18. 00	1. 75	5. 75
19. 50	2. 14	6. 50
21. 00	2. 58	7. 25
22. 50	3. 06	8. 00
24. 00	3. 60	8. 75
25. 50	4. 19	9. 50
27. 00	4. 84	10. 25
28. 50	5. 55	11. 00
30. 00	6. 32	11. 75

◊

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrellio Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. Slope (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness (n)
5 30. 0	4. 25	0. 030	15. 0	0. 0130	0. 005	0. 020	0. 0250

RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0. 00	0. 00	0. 00
1. 50	0. 00	0. 50

bor100-20%	out	sept	28-16
3. 00	0. 01	1. 00	
4. 50	0. 03	1. 50	
6. 00	0. 07	2. 00	
7. 50	0. 14	2. 50	
9. 00	0. 22	3. 00	
10. 50	0. 33	3. 50	
12. 00	0. 48	4. 00	
13. 50	0. 65	4. 25	
15. 00	0. 86	4. 25	
16. 50	1. 09	5. 00	
18. 00	1. 36	5. 75	
19. 50	1. 66	6. 50	
21. 00	2. 00	7. 25	
22. 50	2. 38	8. 00	
24. 00	2. 80	8. 75	
25. 50	3. 25	9. 50	
27. 00	3. 76	10. 25	
28. 50	4. 31	11. 00	
30. 00	4. 90	11. 75	

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

## Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

## MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Hei ght of Curb (cm)	Manni ng (n)	Long. Slope (m/m)	Shoul der Cross Slope (m/m)	Shoul der Roughness (n)
6 30. 0	4. 25	0. 030	15. 0	0. 0130	0. 005	0. 020	0. 0250

## RATI NG CURVE

Depth (cm)	Fl ow (cms)	Spread (m)
0. 00	0. 00	0. 00
1. 50	0. 00	0. 50
3. 00	0. 01	1. 00
4. 50	0. 04	1. 50
6. 00	0. 08	2. 00
7. 50	0. 14	2. 50
9. 00	0. 22	3. 00
10. 50	0. 34	3. 50
12. 00	0. 48	4. 00
13. 50	0. 66	4. 25

bor100-20%	out	sept	28-16
15.00	0.87	4.25	
16.50	1.10	5.00	
18.00	1.37	5.75	
19.50	1.68	6.50	
21.00	2.02	7.25	
22.50	2.40	8.00	
24.00	2.82	8.75	
25.50	3.29	9.50	
27.00	3.80	10.25	
28.50	4.35	11.00	
30.00	4.95	11.75	

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

## Burrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

## MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. Slope (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness (n)
7 30.0	4.25	0.030	15.0	0.0130	0.020	0.020	0.0250

## RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0.00	0.00	0.00
1.50	0.00	0.50
3.00	0.02	1.00
4.50	0.07	1.50
6.00	0.15	2.00
7.50	0.27	2.50
9.00	0.44	3.00
10.50	0.67	3.50
12.00	0.95	4.00
13.50	1.30	4.25
15.00	1.72	4.25
16.50	2.19	5.00
18.00	2.72	5.75
19.50	3.33	6.50
21.00	4.00	7.25
22.50	4.76	8.00
24.00	5.59	8.75
25.50	6.51	9.50

bor100-20% out sept 28-16  
 27.00 7.52 10.25  
 28.50 8.61 11.00  
 30.00 9.80 11.75

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

#### MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. Slope (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness
8 100.0	118.00	0.010	30.0	0.0250	0.009	0.020	0.0250

#### RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0.00	0.00	0.00
5.00	0.10	5.00
10.00	0.61	10.00
15.00	1.81	15.00
20.00	3.89	20.00
25.00	7.06	25.00
30.00	11.47	30.00
35.00	17.31	35.00
40.00	24.71	40.00
45.00	33.83	45.00
50.00	44.80	50.00
55.00	57.77	55.00
60.00	72.86	60.00
65.00	90.19	65.00
70.00	109.90	70.00
75.00	132.10	75.00
80.00	156.91	80.00
85.00	184.44	85.00
90.00	214.81	90.00
95.00	248.12	95.00
100.00	284.49	100.00

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

bor100-20% out sept 28-16

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Hei ght of Curb (cm)	Manni ng (n)	Long. (m/m)	Shoul der Cross Slope (m/m)	Shoul der Roughness (n)
9 30.0	4.25	0.030	15.0	0.0130	0.000	0.020	0.0250

RATING CURVE

Depth (cm)	Fl ow (cms)	Spread (m)
0.00	0.00	0.00
1.50	0.00	0.50
3.00	0.00	1.00
4.50	0.00	1.50
6.00	0.01	2.00
7.50	0.02	2.50
9.00	0.03	3.00
10.50	0.05	3.50
12.00	0.07	4.00
13.50	0.09	4.25
15.00	0.12	4.25
16.50	0.15	5.00
18.00	0.19	5.75
19.50	0.24	6.50
21.00	0.28	7.25
22.50	0.34	8.00
24.00	0.40	8.75
25.50	0.46	9.50
27.00	0.53	10.25
28.50	0.61	11.00
30.00	0.69	11.75

+

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

STORM INLET DATA

bor100-20% out sept 28-16

1 Normal Inlet

Inlet Identification No. 1  
No. of Points on Capture Curve 8

Inlet Capture Relationship

Approach Flow (l/s)	Inlet Flow (l/s)
0.00	0.00
10.00	10.00
30.00	30.00
60.00	60.00
90.00	90.00
130.00	130.00
500.00	500.00
1000.00	1000.00

2 Storage Inlet

Inlet Identification No. 2  
Maximum Storage 55.00 cu. m.  
No. of Points on Storage-Capture Curve 2

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
55.00	15.00

3 Storage Inlet

Inlet Identification No. 3  
Maximum Storage 1.80 cu. m.  
No. of Points on Storage-Capture Curve 2

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.80	20.00

4 Storage Inlet

Inlet Identification No.	4
Maximum Storage	5.70 cu. m.
No. of Points on Storage-Capture Curve	2
Storage-Inlet Capture Relationship	
Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
17.90	14.20

5 Storage Inlet

Inlet Identification No.	5
Maximum Storage	1.30 cu. m.
No. of Points on Storage-Capture Curve	2
Storage-Inlet Capture Relationship	
Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.30	20.00

6 Storage Inlet

Inlet Identification No.	6
Maximum Storage	5.70 cu. m.
No. of Points on Storage-Capture Curve	2
Storage-Inlet Capture Relationship	
Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
17.90	31.00

7 Storage Inlet

bor100-20% out sept 28-16

Inlet Identification No. 7  
Maximum Storage 20.00 cu. m.  
No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

---

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	18.00
20.00	20.00

8 Storage Inlet

Inlet Identification No. 8  
Maximum Storage 25.00 cu. m.  
No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

---

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	18.00
25.00	20.00

9 Storage Inlet

Inlet Identification No. 9  
Maximum Storage 30.00 cu. m.  
No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

---

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	18.00
30.00	20.00

10 Storage Inlet

bor100-20% out sept 28-16

Inlet Identification No.	10
Maximum Storage	35.00 cu. m.
No. of Points on Storage-Capture Curve	3

Storage-Inlet Capture Relationship

---

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	18.00
35.00	20.00

11 Storage Inlet

Inlet Identification No.	11
Maximum Storage	50.00 cu. m.
No. of Points on Storage-Capture Curve	3

Storage-Inlet Capture Relationship

---

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	18.00
50.00	20.00

12 Storage Inlet

Inlet Identification No.	12
Maximum Storage	75.00 cu. m.
No. of Points on Storage-Capture Curve	3

Storage-Inlet Capture Relationship

---

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	18.00
75.00	20.00

13 Storage Inlet

bor100-20% out sept 28-16

Inlet Identification No. 13  
Maximum Storage 1.00 cu. m.  
No. of Points on Storage-Capture Curve 2

Storage-Inlet Capture Relationship

---

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	58.40

14 Storage Inlet

Inlet Identification No. 14  
Maximum Storage 3.00 cu. m.  
No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

---

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	11.40
3.00	13.40

15 Storage Inlet

Inlet Identification No. 15  
Maximum Storage 5.00 cu. m.  
No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

---

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	11.40
5.00	13.40

16 Storage Inlet

bor100-20% out sept 28-16

Inlet Identification No. 16  
Maximum Storage 33.00 cu. m.  
No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	7.00
33.00	9.00

17 Storage Inlet

Inlet Identification No. 17  
Maximum Storage 32.00 cu. m.  
No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	4.80
32.00	6.80

18 Storage Inlet

Inlet Identification No. 18  
Maximum Storage 15.50 cu. m.  
No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	6.50
15.50	8.50

19 Storage Inlet

bor100-20% out sept 28-16

Inlet Identification No. 19  
Maximum Storage 19.00 cu. m.  
No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	1.00
19.00	3.30

20 Storage Inlet

Inlet Identification No. 20  
Maximum Storage 15.50 cu. m.  
No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
1.00	7.40
15.50	9.40

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

MAJOR SYSTEM DATA

Flow History (?)	Street Segment	D/S Segment	Length (m)	Type	No. of C. B.	Inlet Type	Limiting Inlet Capture (l/s)	Connecting Pipe/EXTRAN Inlet
NO	1 SWM14	LP001	40.0	4	0	1 *	0.00	X
NO	2 SWM13	LP001	29.0	1	0	1 *	0.00	X

				bor	100-20%	out	sept	28-16				
					10. 0	7	0	1	*	0. 00	X	
NO	3	LP001 "No Routing"	D001									
NO	4	SWM12	LP002		41. 0	1	0	1	*	0. 00	X	
NO	5	SWM11	LP002		16. 0	4	0	1	*	0. 00	X	
NO	6	LP002 "No Routing"	D002		10. 0	4	1	3	***	20. 00	207	
NO	7	SWM10	LP003		48. 0	4	0	1	*	0. 00	X	
NO	8	SWM8	LP003		27. 0	6	0	1	*	0. 00	X	
NO	9	LP003 "No Routing"	D003		10. 0	6	1	4	***	4. 52	205	
NO	10	SWM3	LP004		28. 0	6	0	1	*	0. 00	X	
NO	11	SWM4	LP004		107. 0	4	0	1	*	0. 00	X	
NO	12	LP004 "No Routing"	D004		10. 0	6	1	6	***	9. 87	205	
NO	13	SWM2	LP005		81. 0	3	0	1	*	0. 00	X	
NO	14	SWM1	LP005		45. 0	5	0	1	*	0. 00	X	
NO	15	LP005 "No Routing"	D005		10. 0	7	1	5	***	20. 00	202	
NO	16	SWM7	OUTB		71. 0	3	1	1	*	20. 00	202	
NO	17	SWM9	SWM8		37. 0	8	1	1	*	25. 00	205	
NO	18	SWM5	OUTA		157. 0	8	1	2	***	15. 00	207	
NO	19	SWM6	OUTC		88. 0	8	1	1	*	20. 00	202	
NO	20	SWM15	OUTD		40. 0	8	0	1	*	0. 00	X	
YES	21	D001	LP002		7. 0	9	0	1	*	0. 00	X	
YES	22	D002	SWM10		20. 0	9	0	1	*	0. 00	X	
YES	23	D003	SWM7		50. 0	9	0	1	*	0. 00	X	
YES	24	D004	SWM2		65. 0	9	0	1	*	0. 00	X	
YES	25	D005	OUT1B		8. 0	9	0	1	*	0. 00	X	

\* Normal Inlet.

\*\* Storage Inlet with linear relationship between Storage and Inlet Capture.

\*\*\* Storage Inlet with user-specified relationship between Storage and Inlet Capture.

Total Number of Street segments	25
Total Length of Major System	1055. 00
Total Number of Inlet C. B.	8
Average Distance Between Inlets	263. 75

bor100-20% out sept 28-16

Outlets From Major System

Outlet I. D.

OUTB  
OUTA  
OUTC  
OUTD  
OUT1B

Total Number of Outlets from Major System = 5

DATA FOR MAJOR SYSTEM STORAGE

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No.	Storage Unit	No. of Inflow Points	I. D. Nos. of Inflow Points
1	Out1	1	OUTA
2	Out2	1	OUTB
3	Out3	1	OUTC
4	Out4	1	OUT1B
5	Out5	1	OUTD

No. of Detention Structures 5

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

SUB-CATCHMENT/SURFACE RUNOFF DATA

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Infiltration Parameters

Max. Infiltration Rate	76.20	mm/hr
Min. Infiltration Rate	13.20	mm/hr
Decay Rate	0.001150	1/sec.

Unit Area Hydrograph (UAH) Data

No Unit Area Hydrograph Data

SUB-CATCHMENT DATA									
No.	Subarea	Street	Area	Imp.	Mann. (N)	Mann. (N)	Slope (m/m)	Width (m)	
Dep.	Storage Flow	Segment	(Ha.)	(%)	(Imp.)	(Perv.)			
Imp.	Perv.	History							
(mm)	(mm)	(?)							
1. 570	4. 670	SWM1	0. 18	41.	0. 0130	0. 2500	0. 020	45.	
2	SWM2	NO	0. 24	35.	0. 0130	0. 2500	0. 020	81.	
1. 570	4. 670	SWM3	0. 11	38.	0. 0130	0. 2500	0. 020	28.	
1. 570	4. 670	SWM4	0. 25	37.	0. 0130	0. 2500	0. 020	107.	
1. 570	4. 670	SWM5	0. 49	18.	0. 0130	0. 2500	0. 020	157.	
1. 570	4. 670	SWM6	0. 22	24.	0. 0130	0. 2500	0. 020	88.	
1. 570	4. 670	SWM7	0. 16	41.	0. 0130	0. 2500	0. 020	71.	
1. 570	4. 670	SWM8	0. 03	52.	0. 0130	0. 2500	0. 020	27.	
1. 570	4. 670	SWM9	0. 10	30.	0. 0130	0. 2500	0. 020	37.	
1. 570	4. 670	SWM10	0. 07	54.	0. 0130	0. 2500	0. 020	48.	
1. 570	4. 670	SWM11	0. 02	51.	0. 0130	0. 2500	0. 020	16.	
1. 570	4. 670	SWM12	0. 06	41.	0. 0130	0. 2500	0. 020	41.	
1. 570	4. 670	SWM13	0. 02	73.	0. 0130	0. 2500	0. 020	29.	
1. 570	4. 670	SWM14	0. 02	70.	0. 0130	0. 2500	0. 020	40.	
1. 570	4. 670	SWM15	0. 21	23.	0. 0130	0. 2500	0. 020	40.	
1. 570	4. 670	NO							

\* Inflow Hydrograph Input Directly

\*\* Inflow hydrograph Input in terms of flow per unit area

Total Drainage Area 2.18 Hectares

Number of Subcatchments 15

<sup>†</sup> Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

bor100-20% out sept 28-16

Simulation Details - Surface Runoff - 15 Subareas

count Subarea

1	SWM1
2	SWM2
3	SWM3
4	SWM4
5	SWM5
6	SWM6
7	SWM7
8	SWM8
9	SWM9
10	SWM10
11	SWM11
12	SWM12
13	SWM13
14	SWM14
15	SWM15

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

Simulation Details - Major System - 30 Segments/Outlets

count	order	segment	time step (min.)	No. of time steps	Max. flow (cms)	Max. depth (cm)
1	2	SWM13	0.65	546	0.01	2.40
2	1	SWM14	1.05	337	0.01	2.75
3	3	LP001			0.03	3.07
4	21	D001	0.80	445	0.03	8.30
5	5	SWM11	0.44	801	0.01	2.56
6	4	SWM12	0.72	495	0.03	3.45
7	11	SWM4	1.61	220	0.11	6.28
8	10	SWM3	0.64	553	0.04	4.82
9	6	LP002			0.07	5.10
10	12	LP004			0.15	7.75
11	17	SWM9	2.96	119	0.04	2.02
12	22	D002	1.97	180	0.05	10.34
13	24	D004	4.52	78	0.14	15.92

			bor	100-20%	out	sept	28-16		
14	8	SWM8		0.69	514		0.03	4.11	
15	7	SWM10		0.82	430		0.07	5.17	
16	14	SWM1		0.90	394		0.07	5.98	
17	13	SWM2		0.75	476		0.16	5.99	
18	9	LP003					0.09	6.44	
19	15	LP005					0.22	6.82	
20	23	D003		3.98	89		0.09	13.32	
21	25	D005		0.57	621		0.20	18.15	
22	20	SWM15		2.15	165		0.06	3.01	
23	19	SWM6		3.42	104		0.08	4.17	
24	18	SWM5		4.80	74		0.15	5.50	
25	16	SWM7		0.72	491		0.11	5.17	
26	30	OUT1B					0.20		
27	29	OUTD					0.06		
28	28	OUTC					0.05		
29	27	OUTA					0.11		
30	26	OUTB					0.09		

♀ Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

#### EXTRAN Interface File Information

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Inlet flows are stored at the following 4 inlets (EXTRAN nodes):

X	207	205	202
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#### DDSWMM-EXTRAN Connectivity

##### EXTRAN Inlet

##### DDSWMM Inlets (Major System Segments)

X	SWM14	SWM13	LP001	SWM12
SWM11				
207	LP002	SWM5		
205	LP003	LP004	SWM9	
202	LP005	SWM7	SWM6	

♀ Dual Drainage Storm Water Management Model (DDSWMM 2.1)

bor100-20% out sept 28-16  
Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

#### MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment D001

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 5	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 15	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 25	0.000	0.000	0.000	0.000	0.000	0.6	0.00
0: 30	0.001	0.000	0.001	0.000	0.000	1.8	0.00
0: 35	0.001	0.000	0.001	0.000	0.001	2.0	0.00
0: 40	0.001	0.000	0.001	0.000	0.001	2.3	0.00
0: 45	0.001	0.000	0.001	0.000	0.001	2.7	0.00
0: 50	0.003	0.000	0.003	0.000	0.002	3.4	0.00
0: 55	0.004	0.000	0.004	0.000	0.004	4.0	0.00
1: 0	0.014	0.000	0.014	0.000	0.012	6.6	0.00
1: 5	0.024	0.000	0.024	0.000	0.023	8.2	0.00
1: 10	0.012	0.000	0.012	0.000	0.015	6.2	0.00
1: 15	0.007	0.000	0.007	0.000	0.008	4.9	0.00
1: 20	0.005	0.000	0.005	0.000	0.005	4.4	0.00
1: 25	0.003	0.000	0.003	0.000	0.004	3.7	0.00
1: 30	0.003	0.000	0.003	0.000	0.003	3.4	0.00
1: 35	0.002	0.000	0.002	0.000	0.002	3.2	0.00
1: 40	0.002	0.000	0.002	0.000	0.002	3.1	0.00
1: 45	0.002	0.000	0.002	0.000	0.002	2.9	0.00
1: 50	0.001	0.000	0.001	0.000	0.001	2.6	0.00
1: 55	0.001	0.000	0.001	0.000	0.001	2.5	0.00
2: 0	0.001	0.000	0.001	0.000	0.001	2.4	0.00
2: 5	0.001	0.000	0.001	0.000	0.001	2.3	0.00
2: 10	0.001	0.000	0.001	0.000	0.001	2.2	0.00
2: 15	0.001	0.000	0.001	0.000	0.001	2.1	0.00
2: 20	0.001	0.000	0.001	0.000	0.001	2.1	0.00
2: 25	0.001	0.000	0.001	0.000	0.001	2.0	0.00
2: 30	0.001	0.000	0.001	0.000	0.001	2.0	0.00
2: 35	0.001	0.000	0.001	0.000	0.001	1.9	0.00
2: 40	0.001	0.000	0.001	0.000	0.001	1.9	0.00
2: 45	0.001	0.000	0.001	0.000	0.001	1.9	0.00
2: 50	0.001	0.000	0.001	0.000	0.001	1.8	0.00
2: 55	0.001	0.000	0.001	0.000	0.001	1.8	0.00
3: 0	0.001	0.000	0.001	0.000	0.001	1.8	0.00
3: 5	0.001	0.000	0.001	0.000	0.001	1.8	0.00
3: 10	0.001	0.000	0.001	0.000	0.001	1.8	0.00
3: 15	0.001	0.000	0.001	0.000	0.001	1.8	0.00
3: 20	0.000	0.000	0.000	0.000	0.000	1.7	0.00
3: 25	0.000	0.000	0.000	0.000	0.000	1.6	0.00
3: 30	0.000	0.000	0.000	0.000	0.000	1.6	0.00
3: 35	0.000	0.000	0.000	0.000	0.000	1.6	0.00
3: 40	0.000	0.000	0.000	0.000	0.000	1.5	0.00
3: 45	0.000	0.000	0.000	0.000	0.000	1.5	0.00

bor100-20% out sept 28-16						
3: 50	0.000	0.000	0.000	0.000	0.000	1.5
3: 55	0.000	0.000	0.000	0.000	0.000	0.00
4: 0	0.000	0.000	0.000	0.000	0.000	0.00
4: 5	0.000	0.000	0.000	0.000	0.000	0.00
4: 10	0.000	0.000	0.000	0.000	0.000	0.00
4: 15	0.000	0.000	0.000	0.000	0.000	0.00
4: 20	0.000	0.000	0.000	0.000	0.000	0.00
4: 25	0.000	0.000	0.000	0.000	0.000	0.00
4: 30	0.000	0.000	0.000	0.000	0.000	0.00
4: 35	0.000	0.000	0.000	0.000	0.000	0.9
4: 40	0.000	0.000	0.000	0.000	0.000	0.9
4: 45	0.000	0.000	0.000	0.000	0.000	0.9
4: 50	0.000	0.000	0.000	0.000	0.000	0.8
4: 55	0.000	0.000	0.000	0.000	0.000	0.8
5: 0	0.000	0.000	0.000	0.000	0.000	0.00
5: 5	0.000	0.000	0.000	0.000	0.000	0.7
5: 10	0.000	0.000	0.000	0.000	0.000	0.7
5: 15	0.000	0.000	0.000	0.000	0.000	0.7
5: 20	0.000	0.000	0.000	0.000	0.000	0.7
5: 25	0.000	0.000	0.000	0.000	0.000	0.7
5: 30	0.000	0.000	0.000	0.000	0.000	0.6
5: 35	0.000	0.000	0.000	0.000	0.000	0.6
5: 40	0.000	0.000	0.000	0.000	0.000	0.6
5: 45	0.000	0.000	0.000	0.000	0.000	0.6
5: 50	0.000	0.000	0.000	0.000	0.000	0.6
5: 55	0.000	0.000	0.000	0.000	0.000	0.6

Maximum 0.026 0.026 0.000 0.024 8.3 0.00  
Time (h:min) 1: 6 1: 6 0: 0 1: 6

♀ Dual Drainage Storm Water Management Model (DDSWMM 2.1)

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### DDSWMM analysis: 3 hour 100 year Chicago Storm + 20% STRESS TEST

## MAJOR SYSTEM DETAILED SIMULATION RESULTS

## Major System Segment D002

Maximum 0.045 0.045 0.000 0.037 10.3 0.00

Time (h: min) 1: 6

bor100-20% out sept 28-16

1: 6 0: 0 1: 8

†

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

## Borrellio Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

## MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment D003

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 5	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 15	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 25	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 35	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 40	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 45	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 50	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 55	0.000	0.000	0.000	0.000	0.000	0.0	0.00
1: 0	0.027	0.000	0.027	0.000	0.009	8.4	0.00
1: 5	0.081	0.000	0.081	0.000	0.039	12.8	0.00
1: 10	0.073	0.000	0.073	0.000	0.068	12.3	0.00
1: 15	0.043	0.000	0.043	0.000	0.060	10.1	0.00
1: 20	0.025	0.000	0.025	0.000	0.044	8.2	0.00
1: 25	0.015	0.000	0.015	0.000	0.030	6.8	0.00
1: 30	0.011	0.000	0.011	0.000	0.020	6.0	0.00
1: 35	0.007	0.000	0.007	0.000	0.014	5.1	0.00
1: 40	0.005	0.000	0.005	0.000	0.010	4.6	0.00
1: 45	0.004	0.000	0.004	0.000	0.008	3.9	0.00
1: 50	0.002	0.000	0.002	0.000	0.006	3.3	0.00
1: 55	0.001	0.000	0.001	0.000	0.004	2.8	0.00
2: 0	0.001	0.000	0.001	0.000	0.003	2.0	0.00
2: 5	0.000	0.000	0.000	0.000	0.002	1.1	0.00
2: 10	0.000	0.000	0.000	0.000	0.002	0.0	0.00
2: 15	0.000	0.000	0.000	0.000	0.002	0.0	0.00
2: 20	0.000	0.000	0.000	0.000	0.001	0.0	0.00
2: 25	0.000	0.000	0.000	0.000	0.001	0.0	0.00
2: 30	0.000	0.000	0.000	0.000	0.001	0.0	0.00
2: 35	0.000	0.000	0.000	0.000	0.001	0.0	0.00
2: 40	0.000	0.000	0.000	0.000	0.001	0.0	0.00
2: 45	0.000	0.000	0.000	0.000	0.001	0.0	0.00
2: 50	0.000	0.000	0.000	0.000	0.000	0.0	0.00
2: 55	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 5	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 15	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00

		bor	100-20%	out	sept	28-16		
3: 25	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
3: 30	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
3: 35	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
3: 40	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
3: 45	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
3: 50	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
3: 55	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
4: 0	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
4: 5	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
4: 10	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
4: 15	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
4: 20	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
4: 25	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
4: 30	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
4: 35	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
4: 40	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
4: 45	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
4: 50	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
4: 55	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
5: 0	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
5: 5	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
5: 10	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
5: 15	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
5: 20	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
5: 25	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
5: 30	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
5: 35	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
5: 40	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
5: 45	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
5: 50	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
5: 55	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00

Maximum 0. 089  
Time (h: min) 1: 6 0. 089 0. 000 0. 068 13. 3 0. 00

†

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

### Borrellio Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

### MAJOR SYSTEM DETAILED SIMULATION RESULTS

#### Major System Segment D004

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 5	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 10	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 15	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 20	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 25	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 30	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00

		bor100-20%	out	sept	28-16		
0: 35	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 40	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 45	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 50	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 55	0. 000	0. 000	0. 000	0. 000	0. 001	0. 0	0. 00
1: 0	0. 045	0. 000	0. 045	0. 000	0. 014	10. 3	0. 00
1: 5	0. 122	0. 000	0. 122	0. 000	0. 056	15. 0	0. 00
1: 10	0. 105	0. 000	0. 105	0. 000	0. 095	14. 2	0. 00
1: 15	0. 066	0. 000	0. 066	0. 000	0. 090	11. 9	0. 00
1: 20	0. 043	0. 000	0. 043	0. 000	0. 069	10. 1	0. 00
1: 25	0. 027	0. 000	0. 027	0. 000	0. 050	8. 4	0. 00
1: 30	0. 017	0. 000	0. 017	0. 000	0. 036	7. 1	0. 00
1: 35	0. 011	0. 000	0. 011	0. 000	0. 026	6. 0	0. 00
1: 40	0. 006	0. 000	0. 006	0. 000	0. 018	4. 9	0. 00
1: 45	0. 003	0. 000	0. 003	0. 000	0. 013	3. 8	0. 00
1: 50	0. 001	0. 000	0. 001	0. 000	0. 009	2. 1	0. 00
1: 55	0. 000	0. 000	0. 000	0. 000	0. 007	0. 0	0. 00
2: 0	0. 000	0. 000	0. 000	0. 000	0. 006	0. 0	0. 00
2: 5	0. 000	0. 000	0. 000	0. 000	0. 005	0. 0	0. 00
2: 10	0. 000	0. 000	0. 000	0. 000	0. 004	0. 0	0. 00
2: 15	0. 000	0. 000	0. 000	0. 000	0. 003	0. 0	0. 00
2: 20	0. 000	0. 000	0. 000	0. 000	0. 003	0. 0	0. 00
2: 25	0. 000	0. 000	0. 000	0. 000	0. 002	0. 0	0. 00
2: 30	0. 000	0. 000	0. 000	0. 000	0. 002	0. 0	0. 00
2: 35	0. 000	0. 000	0. 000	0. 000	0. 002	0. 0	0. 00
2: 40	0. 000	0. 000	0. 000	0. 000	0. 002	0. 0	0. 00
2: 45	0. 000	0. 000	0. 000	0. 000	0. 001	0. 0	0. 00
2: 50	0. 000	0. 000	0. 000	0. 000	0. 001	0. 0	0. 00
2: 55	0. 000	0. 000	0. 000	0. 000	0. 001	0. 0	0. 00
3: 0	0. 000	0. 000	0. 000	0. 000	0. 001	0. 0	0. 00
3: 5	0. 000	0. 000	0. 000	0. 000	0. 001	0. 0	0. 00
3: 10	0. 000	0. 000	0. 000	0. 000	0. 001	0. 0	0. 00
3: 15	0. 000	0. 000	0. 000	0. 000	0. 001	0. 0	0. 00
3: 20	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
3: 25	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
3: 30	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
3: 35	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
3: 40	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
3: 45	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
3: 50	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
3: 55	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
4: 0	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
4: 5	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
4: 10	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
4: 15	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
4: 20	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
4: 25	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
4: 30	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
4: 35	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
4: 40	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
4: 45	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
4: 50	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
4: 55	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
5: 0	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
5: 5	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
5: 10	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
5: 15	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
5: 20	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
5: 25	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
5: 30	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
5: 35	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
5: 40	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
5: 45	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00

			bor	100-20%	out	sept	28-16			
5: 50	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
5: 55	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 0	0. 00
Maxi mum Time (h: mi n)	1: 7			0. 142	1: 7	0: 0	0. 102	1: 11	15. 9	0. 00

♀ Dual Drainage Storm Water Management Model (DDSWMM 2.1)

### Borrellio Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

### MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment D005

Time (hr: mi n)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 5	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 10	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 15	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 20	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 25	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 30	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 35	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 40	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 45	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 50	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
0: 55	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
1: 0	0. 062	0. 000	0. 062	0. 000	0. 053	11. 6	0. 00
1: 5	0. 187	0. 000	0. 187	0. 000	0. 172	17. 8	0. 00
1: 10	0. 192	0. 000	0. 192	0. 000	0. 193	18. 0	0. 00
1: 15	0. 156	0. 000	0. 156	0. 000	0. 160	16. 6	0. 00
1: 20	0. 113	0. 000	0. 113	0. 000	0. 118	14. 6	0. 00
1: 25	0. 075	0. 000	0. 075	0. 000	0. 080	12. 5	0. 00
1: 30	0. 050	0. 000	0. 050	0. 000	0. 054	10. 7	0. 00
1: 35	0. 032	0. 000	0. 032	0. 000	0. 035	9. 1	0. 00
1: 40	0. 019	0. 000	0. 019	0. 000	0. 022	7. 5	0. 00
1: 45	0. 010	0. 000	0. 010	0. 000	0. 012	5. 8	0. 00
1: 50	0. 003	0. 000	0. 003	0. 000	0. 005	3. 6	0. 00
1: 55	0. 000	0. 000	0. 000	0. 000	0. 001	0. 0	0. 00
2: 0	0. 000	0. 000	0. 000	0. 000	0. 001	0. 0	0. 00
2: 5	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
2: 10	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
2: 15	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
2: 20	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
2: 25	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
2: 30	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
2: 35	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
2: 40	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
2: 45	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
2: 50	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00
2: 55	0. 000	0. 000	0. 000	0. 000	0. 000	0. 0	0. 00

		bor100-20%	out	sept	28-16		
3: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 5	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 15	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 25	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 35	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 40	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 45	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 50	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 55	0.000	0.000	0.000	0.000	0.000	0.0	0.00
4: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
4: 5	0.000	0.000	0.000	0.000	0.000	0.0	0.00
4: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
4: 15	0.000	0.000	0.000	0.000	0.000	0.0	0.00
4: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
4: 25	0.000	0.000	0.000	0.000	0.000	0.0	0.00
4: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
4: 35	0.000	0.000	0.000	0.000	0.000	0.0	0.00
4: 40	0.000	0.000	0.000	0.000	0.000	0.0	0.00
4: 45	0.000	0.000	0.000	0.000	0.000	0.0	0.00
4: 50	0.000	0.000	0.000	0.000	0.000	0.0	0.00
4: 55	0.000	0.000	0.000	0.000	0.000	0.0	0.00
5: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
5: 5	0.000	0.000	0.000	0.000	0.000	0.0	0.00
5: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
5: 15	0.000	0.000	0.000	0.000	0.000	0.0	0.00
5: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
5: 25	0.000	0.000	0.000	0.000	0.000	0.0	0.00
5: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
5: 35	0.000	0.000	0.000	0.000	0.000	0.0	0.00
5: 40	0.000	0.000	0.000	0.000	0.000	0.0	0.00
5: 45	0.000	0.000	0.000	0.000	0.000	0.0	0.00
5: 50	0.000	0.000	0.000	0.000	0.000	0.0	0.00
5: 55	0.000	0.000	0.000	0.000	0.000	0.0	0.00

Maximum 0.197  
Time (h: min) 1: 6 0.197 0.000 0.195 18.2 0.00

♀ Dual Drainage Storm Water Management Model (DDSWMM 2.1)

### Borelli Subdivision

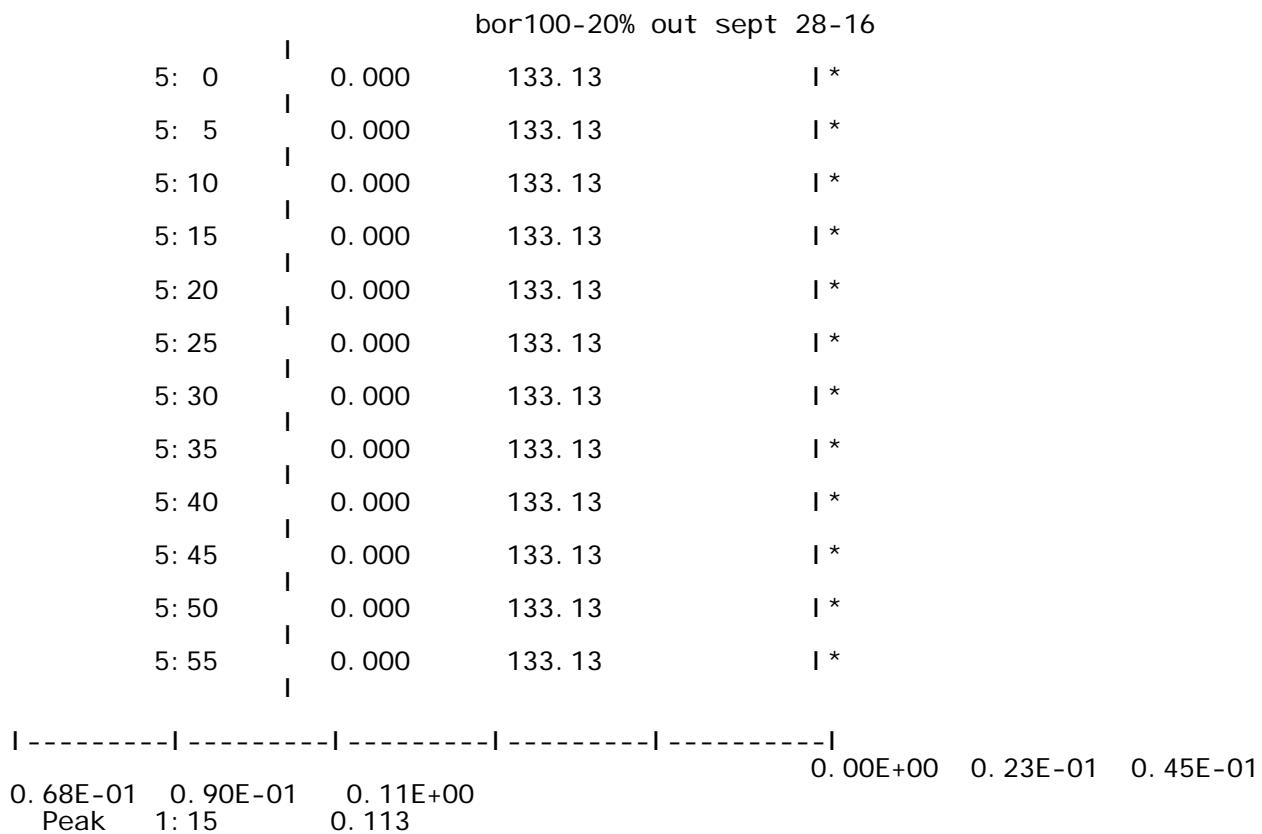
DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

### RESULTS OF SIMULATION FOR MAJOR SYSTEM STORAGE

Storage Unit Number of Inflow Points	Out1
Discharge Point	Peak
	Inflow (cms)
OUTA	0.113
	Peak Time (hr: min.)
	1: 15

Time (hr: mi n)	Flow (cms)	Storage (cu. m)	Flow (cms)
			0. 00E+00 0. 23E-01 0. 45E-01
0. 68E-01 0. 90E-01	0. 11E+00		
0: 0	0. 000	0. 00	*
0: 5	0. 000	0. 00	*
0: 10	0. 000	0. 00	*
0: 15	0. 000	0. 00	*
0: 20	0. 000	0. 00	*
0: 25	0. 000	0. 00	*
0: 30	0. 000	0. 00	*
0: 35	0. 000	0. 00	*
0: 40	0. 000	0. 00	*
0: 45	0. 000	0. 00	*
0: 50	0. 000	0. 00	*
0: 55	0. 000	0. 00	*
1: 0	0. 000	0. 00	*
1: 5	0. 000	0. 00	*
1: 10	0. 000	0. 00	*
1: 15	0. 113	16. 92	
1: 20	0. 084	46. 37	
1: 25	0. 062	68. 16	*****
1: 30	0. 046	84. 25	*****
1: 35	0. 035	96. 35	*****
1: 40	0. 027	105. 66	*****
1: 45	0. 021	112. 84	*****
1: 50	0. 016	118. 42	*****
1: 55	0. 013	122. 75	*****
2: 0	0. 010	126. 07	****
2: 5	0. 007	128. 59	***
2: 10	0. 005	130. 44	**
2: 15	0. 003	131. 74	

		bor100-20%	out	sept	28-16
2: 20		0.002	132.57		*
2: 25		0.001	133.01		*
2: 30		0.000	133.13		*
2: 35		0.000	133.13		*
2: 40		0.000	133.13		*
2: 45		0.000	133.13		*
2: 50		0.000	133.13		*
2: 55		0.000	133.13		*
3: 0		0.000	133.13		*
3: 5		0.000	133.13		*
3: 10		0.000	133.13		*
3: 15		0.000	133.13		*
3: 20		0.000	133.13		*
3: 25		0.000	133.13		*
3: 30		0.000	133.13		*
3: 35		0.000	133.13		*
3: 40		0.000	133.13		*
3: 45		0.000	133.13		*
3: 50		0.000	133.13		*
3: 55		0.000	133.13		*
4: 0		0.000	133.13		*
4: 5		0.000	133.13		*
4: 10		0.000	133.13		*
4: 15		0.000	133.13		*
4: 20		0.000	133.13		*
4: 25		0.000	133.13		*
4: 30		0.000	133.13		*
4: 35		0.000	133.13		*
4: 40		0.000	133.13		*
4: 45		0.000	133.13		*
4: 50		0.000	133.13		*
4: 55		0.000	133.13		*



♀ Required Detention Volume                  133.13 cu. m.

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

#### RESULTS OF SIMULATION FOR MAJOR SYSTEM STORAGE

Storage Unit	Out2	
Number of Inflow Points	1	
Discharge Point	Peak Inflow (cms)	Peak Time (hr: min.)
OUTB	0. 095	1: 6

Time (hr: min.)	Flow (cms)	Storage (cu. m)	Flow (cms)
0. 56E-01	0. 74E-01	0. 93E-01	0. 00E+00    0. 19E-01    0. 37E-01

		bor100-20%	out	sept	28-16
0: 0	0.000	0.00		*	
0: 5	0.000	0.00		*	
0: 10	0.000	0.00		*	
0: 15	0.000	0.00		*	
0: 20	0.000	0.00		*	
0: 25	0.000	0.01		*	
0: 30	0.001	0.14		*	
0: 35	0.001	0.41		*	
0: 40	0.001	0.77		*	
0: 45	0.002	1.22		*	
0: 50	0.003	1.94		**	
0: 55	0.005	3.09		***	
1: 0	0.019	6.67		*****	
1: 5	0.084	22.23			
1: 10	0.093	50.14			
1: 15	0.072	74.86			
1: 20	0.047	92.79			
1: 25	0.026	103.81			
1: 30	0.016	110.19			
1: 35	0.012	114.42			
1: 40	0.009	117.53			
1: 45	0.007	119.89			
1: 50	0.005	121.70			
1: 55	0.004	123.10			
2: 0	0.003	124.20			
2: 5	0.003	125.07			
2: 10	0.002	125.76			
2: 15	0.002	126.34			
2: 20	0.002	126.84			
2: 25	0.001	127.28			
2: 30	0.001	127.68			
2: 35	0.001	128.03			

bor100-20% out sept 28-16

2: 40		0. 001	128. 36	*
2: 45		0. 001	128. 66	*
2: 50		0. 001	128. 94	*
2: 55		0. 001	129. 20	*
3: 0		0. 001	129. 44	*
3: 5		0. 001	129. 66	*
3: 10		0. 001	129. 88	*
3: 15		0. 001	130. 06	*
3: 20		0. 000	130. 19	*
3: 25		0. 000	130. 28	*
3: 30		0. 000	130. 36	*
3: 35		0. 000	130. 42	*
3: 40		0. 000	130. 47	*
3: 45		0. 000	130. 51	*
3: 50		0. 000	130. 56	*
3: 55		0. 000	130. 59	*
4: 0		0. 000	130. 63	*
4: 5		0. 000	130. 66	*
4: 10		0. 000	130. 69	*
4: 15		0. 000	130. 71	*
4: 20		0. 000	130. 74	*
4: 25		0. 000	130. 76	*
4: 30		0. 000	130. 79	*
4: 35		0. 000	130. 81	*
4: 40		0. 000	130. 83	*
4: 45		0. 000	130. 85	*
4: 50		0. 000	130. 87	*
4: 55		0. 000	130. 89	*
5: 0		0. 000	130. 91	*
5: 5		0. 000	130. 92	*
5: 10		0. 000	130. 94	*

			bor100-20% out sept 28-16
5: 15	0. 000	130. 95	*
5: 20	0. 000	130. 97	*
5: 25	0. 000	130. 99	*
5: 30	0. 000	131. 00	*
5: 35	0. 000	131. 01	*
5: 40	0. 000	131. 03	*
5: 45	0. 000	131. 04	*
5: 50	0. 000	131. 05	*
5: 55	0. 000	131. 07	*
----- ----- ----- -----			
0. 56E-01	0. 74E-01	0. 93E-01	0. 00E+00 0. 19E-01 0. 37E-01
Peak	1: 6	0. 095	

<sup>♀</sup>      Required Detention Volume        131. 07 cu. m.  
<sup>†</sup>      Dual Drainage Storm Water Management Model (DDSWMM 2.1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

#### RESULTS OF SIMULATION FOR MAJOR SYSTEM STORAGE

Storage Unit	Out3		
Number of Inflow Points	1		
Discharge Point	Peak Inflow (cms)	Peak Time (hr: min.)	
OUTC	0. 052	1: 8	
Time (hr: min.)	Flow (cms)	Storage (cu. m)	Flow (cms)
0. 31E-01	0. 41E-01	0. 51E-01	0. 00E+00 0. 10E-01 0. 20E-01
----- ----- ----- -----			
0: 0	0. 000	0. 00	*
0: 5	0. 000	0. 00	*
0: 10	0. 000	0. 00	*
0: 15	0. 000	0. 00	*

bor100-20% out sept 28-16

0: 20	0. 000	0. 00	*
0: 25	0. 000	0. 00	*
0: 30	0. 000	0. 00	*
0: 35	0. 000	0. 01	*
0: 40	0. 000	0. 03	*
0: 45	0. 000	0. 05	*
0: 50	0. 000	0. 10	*
0: 55	0. 001	0. 22	*
1: 0	0. 002	0. 59	**
1: 5	0. 014	2. 93	*****
1: 10	0. 051	14. 62	
1: 15	0. 040	28. 31	
1: 20	0. 026	38. 27	*****
1: 25	0. 018	44. 95	*****
1: 30	0. 014	49. 86	*****
1: 35	0. 012	53. 84	*****
1: 40	0. 010	57. 17	*****
1: 45	0. 009	60. 02	*****
1: 50	0. 008	62. 50	*****
1: 55	0. 007	64. 70	*****
2: 0	0. 006	66. 68	*****
2: 5	0. 006	68. 48	*****
2: 10	0. 005	70. 13	*****
2: 15	0. 005	71. 65	****
2: 20	0. 005	73. 08	****
2: 25	0. 004	74. 41	****
2: 30	0. 004	75. 67	****
2: 35	0. 004	76. 87	***
2: 40	0. 004	78. 00	***
2: 45	0. 004	79. 08	***
2: 50	0. 003	80. 10	***

		bor100-20%	out sept	28-16
2: 55	0. 003	81. 08	****	
3: 0	0. 003	82. 02	****	
3: 5	0. 003	82. 93	***	
3: 10	0. 003	83. 79	***	
3: 15	0. 003	84. 63	***	
3: 20	0. 003	85. 44	***	
3: 25	0. 003	86. 22	***	
3: 30	0. 002	86. 97	***	
3: 35	0. 002	87. 71	***	
3: 40	0. 002	88. 42	***	
3: 45	0. 002	89. 11	***	
3: 50	0. 002	89. 79	***	
3: 55	0. 002	90. 44	***	
4: 0	0. 002	91. 08	***	
4: 5	0. 002	91. 71	***	
4: 10	0. 002	92. 31	**	
4: 15	0. 002	92. 91	**	
4: 20	0. 002	93. 48	**	
4: 25	0. 002	94. 05	**	
4: 30	0. 002	94. 60	**	
4: 35	0. 002	95. 14	**	
4: 40	0. 002	95. 67	**	
4: 45	0. 002	96. 19	**	
4: 50	0. 002	96. 69	**	
4: 55	0. 002	97. 19	**	
5: 0	0. 002	97. 68	**	
5: 5	0. 002	98. 16	**	
5: 10	0. 002	98. 62	**	
5: 15	0. 002	99. 08	**	
5: 20	0. 001	99. 53	**	
5: 25	0. 001	99. 98	**	
5: 30	0. 001	100. 41	**	

bor100-20% out sept 28-16				
5: 35	0. 001	100. 84	**	
5: 40	0. 001	101. 26	**	
5: 45	0. 001	101. 67	**	
5: 50	0. 001	102. 08	**	
5: 55	0. 001	102. 48	**	
-----  -----  -----  -----				
0. 31E-01	0. 41E-01	0. 51E-01	0. 00E+00	0. 10E-01
Peak	1: 8	0. 052		0. 20E-01

♀ Required Detention Volume        102. 48 cu. m.  
 † Dual Drainage Storm Water Management Model (DDSWMM 2.1)

#### Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

#### RESULTS OF SIMULATION FOR MAJOR SYSTEM STORAGE

Storage Unit Number of Inflow Points	Out4 1		
Discharge Point	Peak Inflow (cms)	Peak Time (hr: min.)	
OUT1B	0. 195	1: 7	
Time (hr: min.)	Flow (cms)	Storage (cu. m.)	Flow (cms)
0. 12E+00	0. 15E+00	0. 19E+00	0. 00E+00
-----  -----  -----  -----			
0: 0	0. 000	0. 00	*
0: 5	0. 000	0. 00	*
0: 10	0. 000	0. 00	*
0: 15	0. 000	0. 00	*
0: 20	0. 000	0. 00	*
0: 25	0. 000	0. 00	*
0: 30	0. 000	0. 00	*

		bor100-20%	out	sept	28-16
0: 35	0. 000	0. 00		*	
0: 40	0. 000	0. 00		*	
0: 45	0. 000	0. 00		*	
0: 50	0. 000	0. 00		*	
0: 55	0. 000	0. 00		*	
1: 0	0. 053	7. 93		*****	
1: 5	0. 172	41. 66			
1: 10	0. 193	98. 56			
1: 15	0. 160	151. 51			
1: 20	0. 118	193. 24		*****	
1: 25	0. 080	222. 95		*****	
1: 30	0. 054	243. 08		*****	
1: 35	0. 035	256. 45		*****	
1: 40	0. 022	264. 94		*****	
1: 45	0. 012	269. 95		***	
1: 50	0. 005	272. 46		**	
1: 55	0. 001	273. 39		*	
2: 0	0. 001	273. 67		*	
2: 5	0. 000	273. 79		*	
2: 10	0. 000	273. 85		*	
2: 15	0. 000	273. 89		*	
2: 20	0. 000	273. 92		*	
2: 25	0. 000	273. 94		*	
2: 30	0. 000	273. 95		*	
2: 35	0. 000	273. 96		*	
2: 40	0. 000	273. 97		*	
2: 45	0. 000	273. 98		*	
2: 50	0. 000	273. 99		*	
2: 55	0. 000	273. 99		*	
3: 0	0. 000	274. 00		*	
3: 5	0. 000	274. 00		*	
3: 10	0. 000	274. 00		*	

bor100-20% out sept 28-16

3: 15	0.000	274.01	*
3: 20	0.000	274.01	*
3: 25	0.000	274.01	*
3: 30	0.000	274.01	*
3: 35	0.000	274.02	*
3: 40	0.000	274.02	*
3: 45	0.000	274.02	*
3: 50	0.000	274.02	*
3: 55	0.000	274.02	*
4: 0	0.000	274.02	*
4: 5	0.000	274.02	*
4: 10	0.000	274.02	*
4: 15	0.000	274.02	*
4: 20	0.000	274.02	*
4: 25	0.000	274.02	*
4: 30	0.000	274.02	*
4: 35	0.000	274.03	*
4: 40	0.000	274.03	*
4: 45	0.000	274.03	*
4: 50	0.000	274.03	*
4: 55	0.000	274.03	*
5: 0	0.000	274.03	*
5: 5	0.000	274.03	*
5: 10	0.000	274.03	*
5: 15	0.000	274.03	*
5: 20	0.000	274.03	*
5: 25	0.000	274.03	*
5: 30	0.000	274.03	*
5: 35	0.000	274.03	*
5: 40	0.000	274.03	*
5: 45	0.000	274.03	*

			bor100-20% out sept 28-16	
5: 50		0. 000	274. 03	*
5: 55		0. 000	274. 03	*
-----  -----  -----  -----				0. 00E+00 0. 39E-01 0. 77E-01
0. 12E+00	0. 15E+00	0. 19E+00		
Peak	1: 7	0. 195		

♀ Required Detention Volume 274. 03 cu. m.

† Dual Drainage Storm Water Management Model (DDSWMM 2. 1)

Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

#### RESULTS OF SIMULATION FOR MAJOR SYSTEM STORAGE

Storage Unit Out5  
Number of Inflow Points 1

Discharge Point	Peak Inflow (cms)	Peak Time (hr: min.)
OUTD	0. 056	1: 7

Time (hr: min.)	Flow (cms)	Storage (cu. m.)	Flow (cms)
0. 31E-01	0. 42E-01	0. 52E-01	0. 00E+00 0. 10E-01 0. 21E-01
-----  -----  -----  -----			
0: 0	0. 000	0. 00	*
0: 5	0. 000	0. 00	*
0: 10	0. 000	0. 00	*
0: 15	0. 000	0. 00	*
0: 20	0. 000	0. 00	*
0: 25	0. 000	0. 00	*
0: 30	0. 000	0. 01	*
0: 35	0. 000	0. 04	*
0: 40	0. 000	0. 09	*
0: 45	0. 000	0. 17	*
0: 50	0. 001	0. 34	*

bor100-20% out sept 28-16

0: 55	0. 002	0. 73	**
1: 0	0. 008	2. 18	*****
1: 5	0. 037	8. 93	
1: 10	0. 052	24. 12	
1: 15	0. 043	38. 46	
1: 20	0. 035	50. 26	
1: 25	0. 029	59. 90	*****
1: 30	0. 023	67. 66	*****
1: 35	0. 019	73. 99	*****
1: 40	0. 016	79. 26	*****
1: 45	0. 014	83. 70	*****
1: 50	0. 012	87. 50	*****
1: 55	0. 010	90. 81	*****
2: 0	0. 009	93. 71	*****
2: 5	0. 008	96. 28	*****
2: 10	0. 007	98. 58	*****
2: 15	0. 007	100. 66	*****
2: 20	0. 006	102. 54	*****
2: 25	0. 006	104. 27	*****
2: 30	0. 005	105. 86	*****
2: 35	0. 005	107. 33	*****
2: 40	0. 004	108. 69	*****
2: 45	0. 004	109. 97	****
2: 50	0. 004	111. 18	****
2: 55	0. 004	112. 31	****
3: 0	0. 003	113. 38	***
3: 5	0. 003	114. 40	***
3: 10	0. 003	115. 37	***
3: 15	0. 003	116. 29	***
3: 20	0. 003	117. 18	***
3: 25	0. 003	118. 03	***

		bor100-20%	out	sept	28-16	
3: 30	0. 003	118. 85		***		
3: 35	0. 003	119. 64		***		
3: 40	0. 003	120. 40		***		
3: 45	0. 002	121. 14		***		
3: 50	0. 002	121. 86		***		
3: 55	0. 002	122. 55		***		
4: 0	0. 002	123. 22		***		
4: 5	0. 002	123. 87		***		
4: 10	0. 002	124. 51		**		
4: 15	0. 002	125. 12		**		
4: 20	0. 002	125. 72		**		
4: 25	0. 002	126. 30		**		
4: 30	0. 002	126. 87		**		
4: 35	0. 002	127. 43		**		
4: 40	0. 002	127. 97		**		
4: 45	0. 002	128. 50		**		
4: 50	0. 002	129. 02		**		
4: 55	0. 002	129. 52		**		
5: 0	0. 002	130. 01		**		
5: 5	0. 002	130. 50		**		
5: 10	0. 002	130. 97		**		
5: 15	0. 002	131. 43		**		
5: 20	0. 001	131. 89		**		
5: 25	0. 001	132. 33		**		
5: 30	0. 001	132. 77		**		
5: 35	0. 001	133. 19		**		
5: 40	0. 001	133. 61		**		
5: 45	0. 001	134. 03		**		
5: 50	0. 001	134. 43		**		
5: 55	0. 001	134. 83		**		
-----  -----  -----  -----  -----						
				0. 00E+00	0. 10E-01	0. 21E-01

0.31E-01 0.42E-01 0.52E-01      bor100-20% out sept 28-16  
 Peak 1: 7      0.056

♀ Required Detention Volume      134.83 cu. m.  
 Dual Drainage Storm Water Management Model (DDSWMM 2.1)

#### Borrello Subdivision

DDSWMM analysis, 3 hour 100 year Chicago Storm + 20% STRESS TEST

#### MAJOR SYSTEM

#### SUMMARY OF SIMULATION RESULTS

No.	Segment Max.	Peak Flow (cms)	Peak Time (hr: min.)	Max. Depth (cm)	Max. Capture (l/s)	Inlet Restriction (?)	D/S Pipe
Storage (cu. m.)							
1 SWM14 0.00	0.013	1: 5	2.75	0.00	-	X	
2 SWM13 0.00	0.013	1: 5	2.40	0.00	-	X	
3 LP001 0.00	0.026	1: 6	3.07	0.00	-	X	
4 SWM12 0.00	0.031	1: 5	3.45	0.00	-	X	
5 SWM11 0.00	0.011	1: 5	2.56	0.00	-	X	
6 LP002 1.80	0.065	1: 6	5.10	20.00	N/A	207	
7 SWM10 0.00	0.068	1: 5	5.17	0.00	-	X	
8 SWM8 0.00	0.029	1: 8	4.11	0.00	-	X	
9 LP003 5.70	0.094	1: 6	6.44	4.52	N/A	205	
10 SWM3 0.00	0.044	1: 5	4.82	0.00	-	X	
11 SWM4 0.00	0.112	1: 5	6.28	0.00	-	X	
12 LP004 5.70	0.152	1: 7	7.75	9.87	N/A	205	
13 SWM2 0.00	0.163	1: 11	5.99	0.00	-	X	
14 SWM1 0.00	0.075	1: 5	5.98	0.00	-	X	
15 LP005 1.30	0.217	1: 6	6.82	20.00	N/A	202	
16 SWM7 0.00	0.115	1: 5	5.17	20.00	YES	202	
17 SWM9 0.00	0.039	1: 5	2.02	17.47	NO	205	
18 SWM5 55.00	0.148	1: 5	5.50	15.00	N/A	207	
19 SWM6 0.00	0.081	1: 5	4.17	20.00	YES	202	

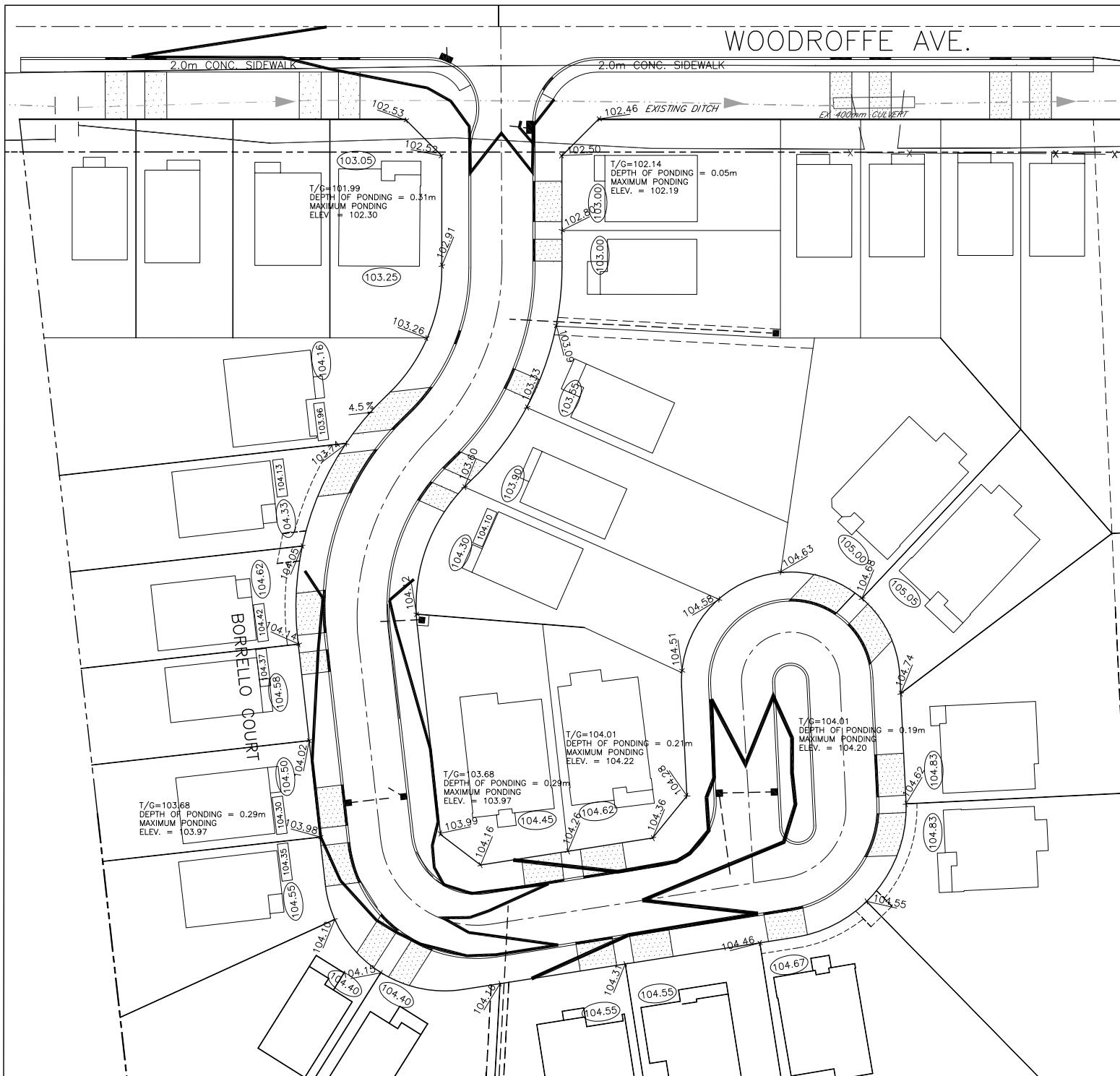
			bor100-20%	out	sept	28-16		
20 SWM15 0.00	0.058	1: 5		3.01	0.00	-	X	
21 D001 0.00	0.026	1: 6		8.30	0.00	-	X	
22 D002 0.00	0.045	1: 6		10.34	0.00	-	X	
23 D003 0.00	0.089	1: 6		13.32	0.00	-	X	
24 D004 0.00	0.142	1: 7		15.92	0.00	-	X	
25 D005 0.00	0.197	1: 6		18.15	0.00	-	X	

\*\*\* SIMULATION ENDED NORMALLY \*\*\*

```
*****
*           *
*   Simulation Starting Date      September 13, 16      *
*           Time      08:25:25.57          *
*           *
*   Simulation Ending   Date      September 13, 16      *
*           Time      08:25:28.26          *
*           *
*   Duration of Simulation       0.04 Minutes          *
*****
```

#### Data Files

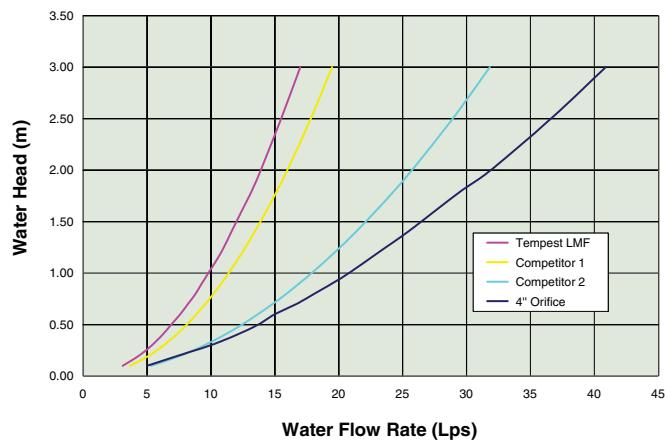
-----  
Input Data File Name                        bor100+20%.txt  
Output File Name                            bor100-20  
EXTRAN Interface (ASCII) File Name    ssdgsa



**Robinson**  
Land Development

scale	N.T.S.	BORRELLO SUBDIVISION	project no.
date	15/09/16		14057
drawn by	JHB		20% STRESS TEST
			SWM-2

**Tempest Inlet Control Devices restrict flow to a narrower range than traditional methods regardless of head**



## THE NEXT GENERATION IN STORM SEWER INLET CONTROLS



[www.ipexinc.com](http://www.ipexinc.com)

### THE TEMPEST FAMILY OF SYSTEMS

#### TEMPEST LMF



##### Restricts:

- ✓ Flow
- ✓ Odours
- ✓ Floatables

#### LOW to MODERATE FLOW RATES

2 L/s (32 GPM) – 17 L/s (270 GPM)

14 pre-set flow rates

The Tempest LMF system features a vortex inlet design that allows a low flow rate to be set and eliminates the passage of odours and floatables and allows for debris and sediment to collect in the structure.

#### TEMPEST HF & HF SUMP



##### Restricts:

- ✓ Flow
- ✓ Odours
- ✓ Floatables

#### HIGH FLOW RATES

15L/s (240 GPM) or greater

5 pre-set flow rates

The standard Tempest HF system allows a near constant discharge rate to be set and eliminates the passage of odours and floatables and allows for debris and sediment to collect in the structure.

The Tempest HF SUMP system is designed for catch basins & manholes in which there is no sump or the outlet pipe is too low to install standard Tempest device.

#### TEMPEST MHF



##### Restricts:

- ✓ Flow

#### MEDIUM TO HIGH FLOW RATES

9L/s (143 GPM) or greater

Specified pre-set flow rates

The Tempest MHF is a standard orifice plate or plug device designed to allow a specified flow volume through the outlet pipe at a specified head.



### **5.3 Levels of Service**

#### **5.3.1. Minor System**

- I. Lateral sewer system to be designed using the Rational Method and the 5-year Intensity Duration Frequency Curve - Nepean DWG IDF-93 (See Appendix E).
  - I-a Inlet time in typical residential areas = 20 min
  - I-b Average runoff coefficient for residential areas does not exceed  $C_{max} = 0.55$  (asphalt = 0.9, grass = 0.2)
  - I-c Calculation of the hydraulic grade line to be conducted only for the surcharged lateral sewers that are connected to the trunk sewer at surcharged sections.
  - I-d Surcharge calculations to be based on the steady state Darcy-Weisbach formula using maximum water level in the trunk junction as the starting hydraulic grade line elevation.
  - I-e Maximum permitted hydraulic grade line elevation to be 0.30m below the underside of building foundations.
- II. Density of inlets connected to the minor system to be restricted to a maximum of 3.5 inlets per hectare with the equivalent capacity of Inlet Control Device SCEPTOR type "A" – 20.0 l/s or the equivalent of 70 l/s/ha.
- III. Trunk storm sewers to be designed based on the results of hydrological/hydrodynamic modeling using XP-SWMM.
  - III-a Modeling to be based on the 5 and 100 year Chicago design storm of 12 hour duration and 20 minutes time step, derived from the Nepean IDF-93 curves (see Appendix E).
  - III-b Modeling to be based on the inlet densities and restrictions specified in paragraph II above.
  - III-c Hydraulic grade line modeling to be based on the hydrodynamic fluctuation of the water levels in the Strandherd SWM facility.
  - III-d Maximum permitted hydraulic grade line elevation to be 0.30m below the underside of basement floor slab (top of footing).

#### **5.3.2 Major system**

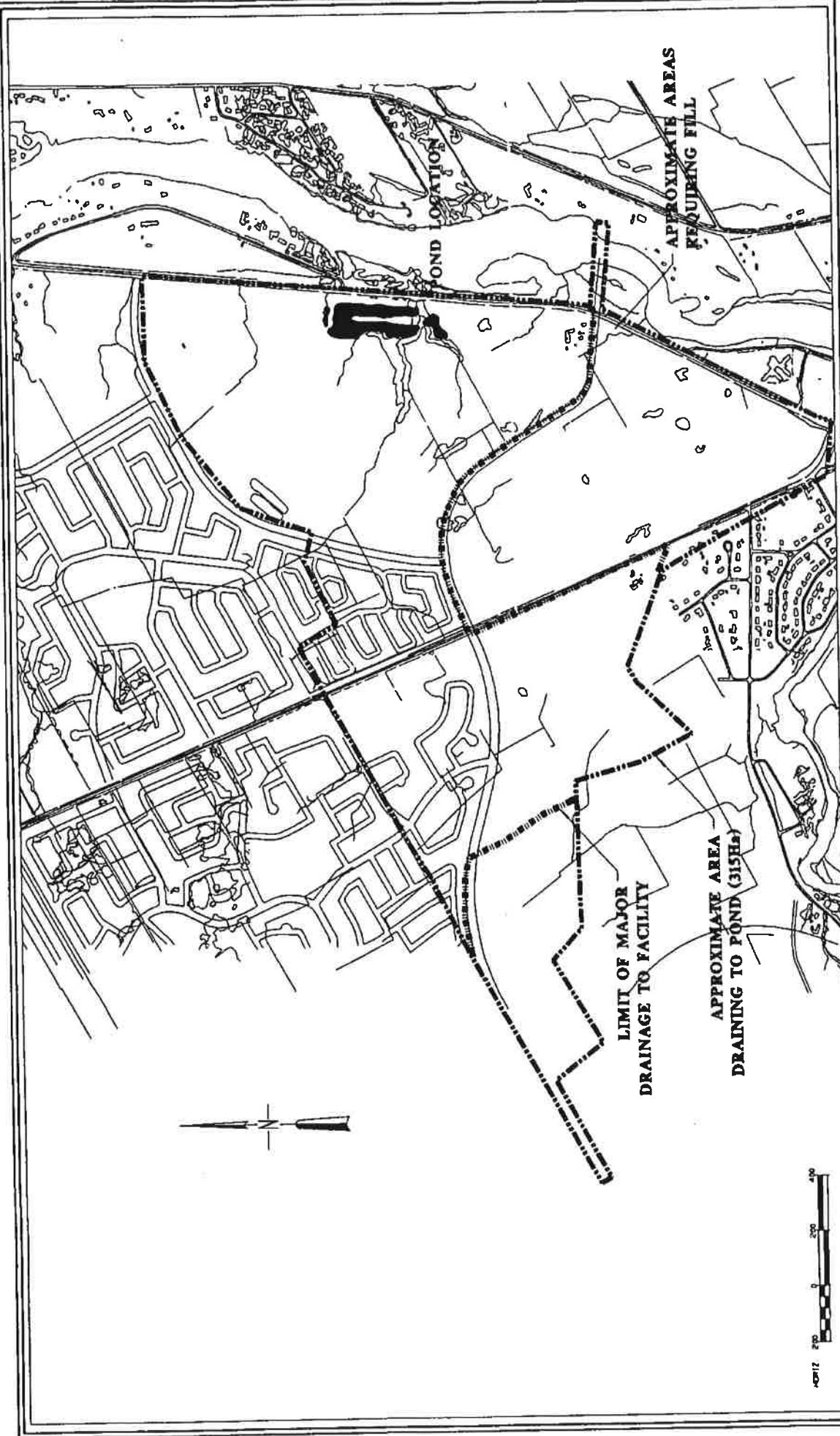
- I Major flow to be accommodated by a combination of on-site detention and overland flow conveyance with no-ponding
- II The storage versus conveyance requirements for areas of average runoff coefficient less than  $c = 0.55$  to be determined using the chart enclosed in Appendix F.
- III Residential Development:  
Modeling is not required for densities with the average runoff coefficient lower than  $C = 0.55$ . The maximum on-site detention storage requirement during the 100 year storm is  $130 \text{ m}^3/\text{ha}$  assuming no-overflow and that the average runoff coefficient does not exceed 0.55.
  - III-a On-site detention storage may be provided by:
    - low laying park surfaces, and/or,
    - fairly evenly distributed road/rear yard sawtoothing design, and/or,
    - combination of both sawtoothing design and park storage
  - III-b Maximum hydrostatic depth in roadways sags = 0.25m

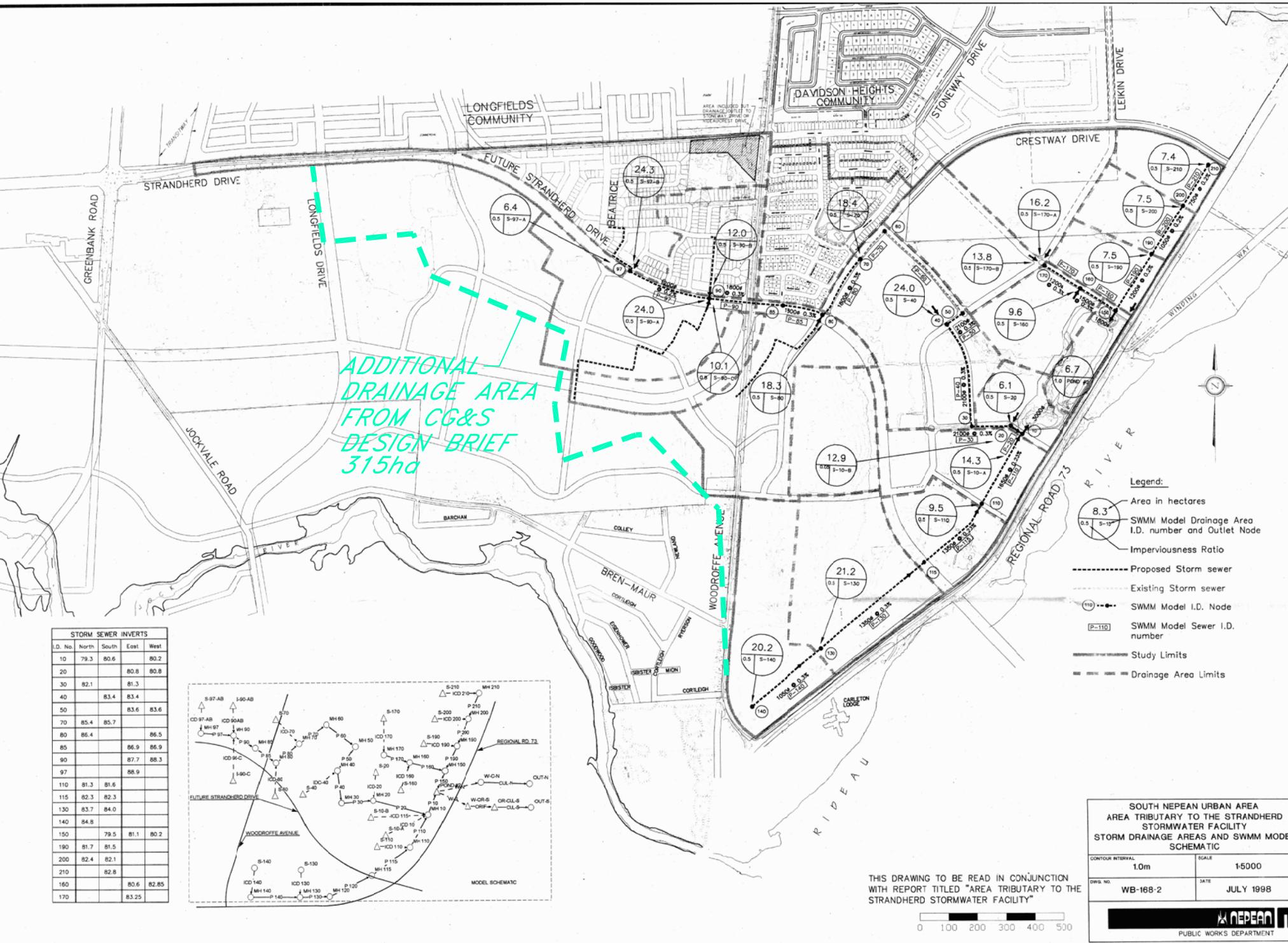
FIGURE DBB

FACILITY DRAINAGE BOUNDARIES

Title:

CITY OF NEPEAN  
PUBLIC WORKS DEPARTMENT  
**CG&S**  
CH2M Gore & Sonne Limited







David McManus  
Engineering Ltd.

JUNIE 2/04  
Smc

June 2, 2004

Cecil D. Naraine Associates Limited  
Consulting Engineers  
1097 Lena Avenue  
Manotick, Ontario  
K4M 1E7

Attn: Mr. D. Cecil Naraine, P.Eng.

Dear Sir:

**Re: Borrello's Property, Woodroffe Avenue - Our File 2420**

We have received your letter of April 13, 2004 requesting that capacity for the Borrello property be provided in the future storm sewer system that will be constructed on Woodroffe Avenue. We have discussed this request with Minto Developments Inc. and they have agreed to provide capacity for Borrello, subject to Borrello cost sharing on applicable works. Your client must negotiate with Minto directly on cost sharing.

As you know, the storm sewer system in this area outlets to the Strandherd SWM facility on Prince of Wales Drive. CH2M Gore & Storrie Limited prepared the *South Nepean Strandherd Stormwater Facility Design Brief (February 1998)* for the stormwater management facility on Prince of Wales Drive. This report indicates that the Strandherd SWM facility has capacity to accommodate minor system flows from 315 ha of developed area. The drainage area from Minto's lands and the Borrello property is a total of 300 ha. Therefore there is capacity in the Strandherd SWM facility. We have attached information from the CH2M Gore & Storrie Design Brief for your information.

Please call if you have any questions or concerns.

Regards,

A handwritten signature in black ink, appearing to read "Sean Czaharynski".

Sean Czaharynski, P.Eng.  
Senior Project Manager

cc Mr. Marcel Denomme, Minto Developments Inc.

400 - 30 Camelot Drive, Nepean, Ontario K2G 5X8  
Tel: 613-225-1929 Fax: 613-225-7330 E-mail: mcmanus@dmel.on.ca

Municipal and Land Development Consultants

## 1.0 TREATMENT FACILITY OVERVIEW

### 1.1 General

The Strandherd Stormwater Facility will receive stormwater flow from developments in South Nepean. The purpose of the proposed works is to provide treatment for influent stormwater prior to discharge into the Rideau River in order to achieve water quality targets for the Rideau River and to meet provincial water quality standards. Figure DB 'A' shows the location of the facility with respect to other areas in South Nepean. The following sections outline the general shape and configuration, operating water levels and hydraulic operation of the facility.

Inflow to the facility will be routed first into either the north or south forebay prior to discharge into the main cell. A constant outflow rate will be maintained from the facility during discharge events, with a typical water level fluctuation of approximately 1.1 m during these events. This constant outflow is an operational requirement for the potential future UV facility, but in the interim (prior to installation of UV) the flow control will help enhance the water quality of facility effluent by increasing facility mean retention times.

Storm events up to 5-year return period which exceed the treatment level in the facility will be discharged via the main southern outlet from the facility through the existing culvert on Strandherd Creek. This outlet will be designed to pass 2.3 m<sup>3</sup>/s at 5-year pond water levels. Flows from storms beyond this 5-year return period in excess of the capacity of the main outlet will be bypassed via the high level overflow spillway for the facility located near the south entrance to Winding Way. This outlet will ensure that water levels in the facility do not exceed an elevation of 82.5 m under storms equal to the 100-year design storm event. It is expected that the discharge from this outlet will be approximately 7 m<sup>3</sup>/s in this event.

Flow measurement and water quality monitoring equipment will be required at each of the inlets and at the main (south) facility outlet. This equipment will be used to monitor the performance of the facility with respect to water quality parameters of concern.

### 1.2 Facility Sizing

Sizing of the stormwater facility was performed as part of the pre-design process. This sizing was based on several criteria; the level of protection required based on fisheries habitat in receiving waters, the size of the contributing area, and the imperviousness of this contributing area all affect the facility size required. The portion of the major flows from the development to be directed through the facility as well as the outlet configuration and operation were also considered in the design.

#### 1.2.1 Drainage Area

The facility is designed to accommodate minor system flows from 315 ha of developed area with an average runoff coefficient of 0.47. The facility provides enough storage to meet MOEE (1994) Level 1 protection sizing guidelines for a 55% impervious area, which is based on a reduction in the incoming suspended solids load by an average of 80%.

## SECTION 6

## MISCELLANEOUS SANITARY AND STORM SEWERS

**6.4.2 Culvert Design**

Hydraulic analysis must consider the presence of culverts for roadway and driveway crossings since these facilities usually provide the most significant head loss. Culverts shall be sized/designed using the methodology outlined in Chapter 5 of the MTO Drainage Manual.

The designer shall submit hydraulic design calculations to identify design flow conditions and inlet head requirements for culverts. The need for energy dissipation, erosion control measures, and grates shall be considered for each design.

The minimum culvert diameter (including private entrances/driveways) shall be 500 mm to allow for reliability and ease of maintenance. The culvert length shall be sufficient to keep fill from obstructing the waterway. Lengths should be minimized to avoid fish passage problems or uplift pressures that may lead to failure. Normal stream velocities should also be low enough to allow for the passage of native fish species. If extra length is required to accommodate future road-widening potential, uplift pressures should also be checked under these future conditions. Depth of cover will affect the required material thickness. Refer to the OPSD 800 series for material minimum thickness. Check the Standard for detail drawings, approved materials, and special provisions to the OPS construction specifications.

When designing a culvert under a roadway, the designer must also check first to see if the waterway falls under the authority of one of the conservation authorities that will likely have their own return frequency requirements.

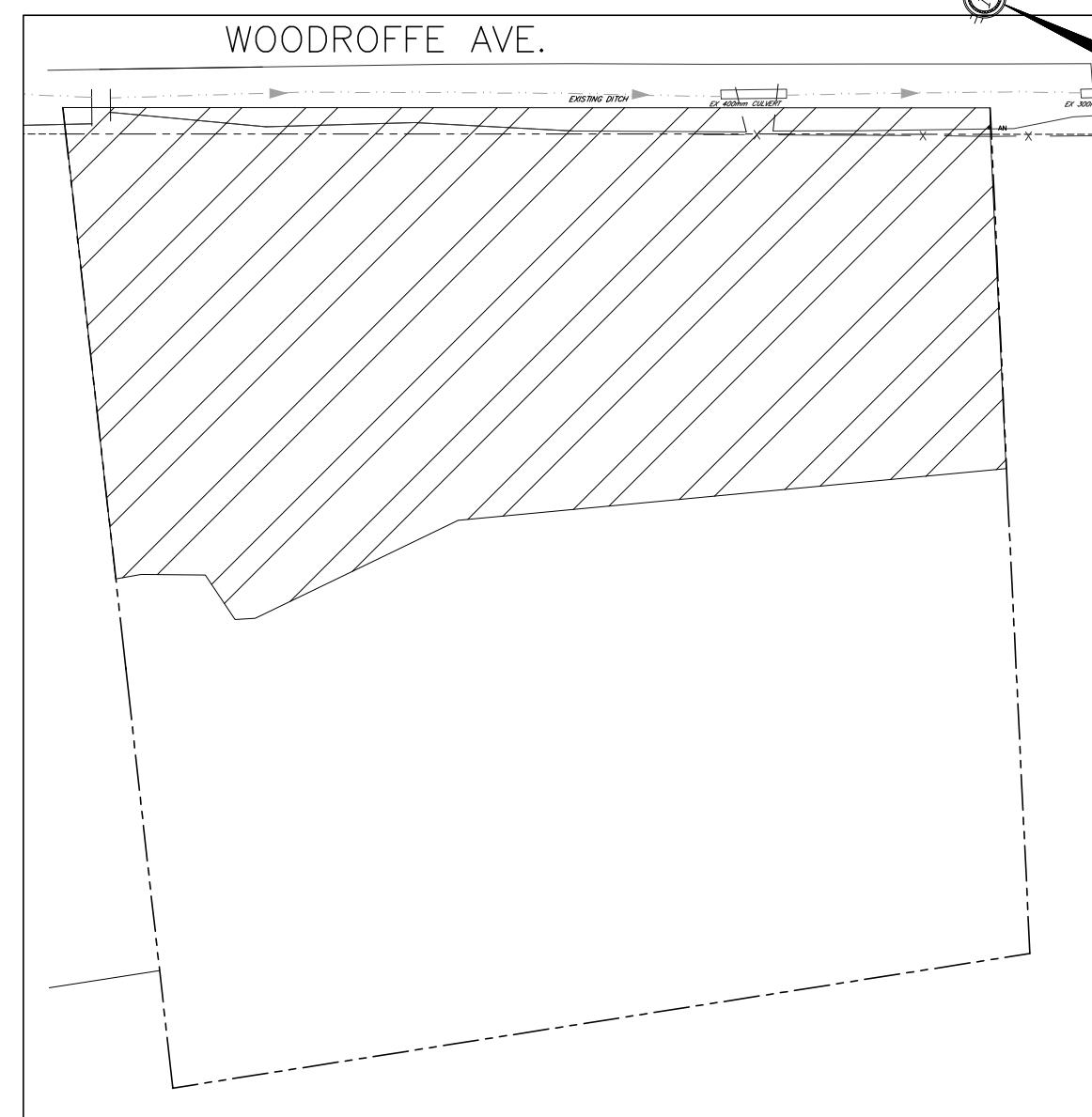
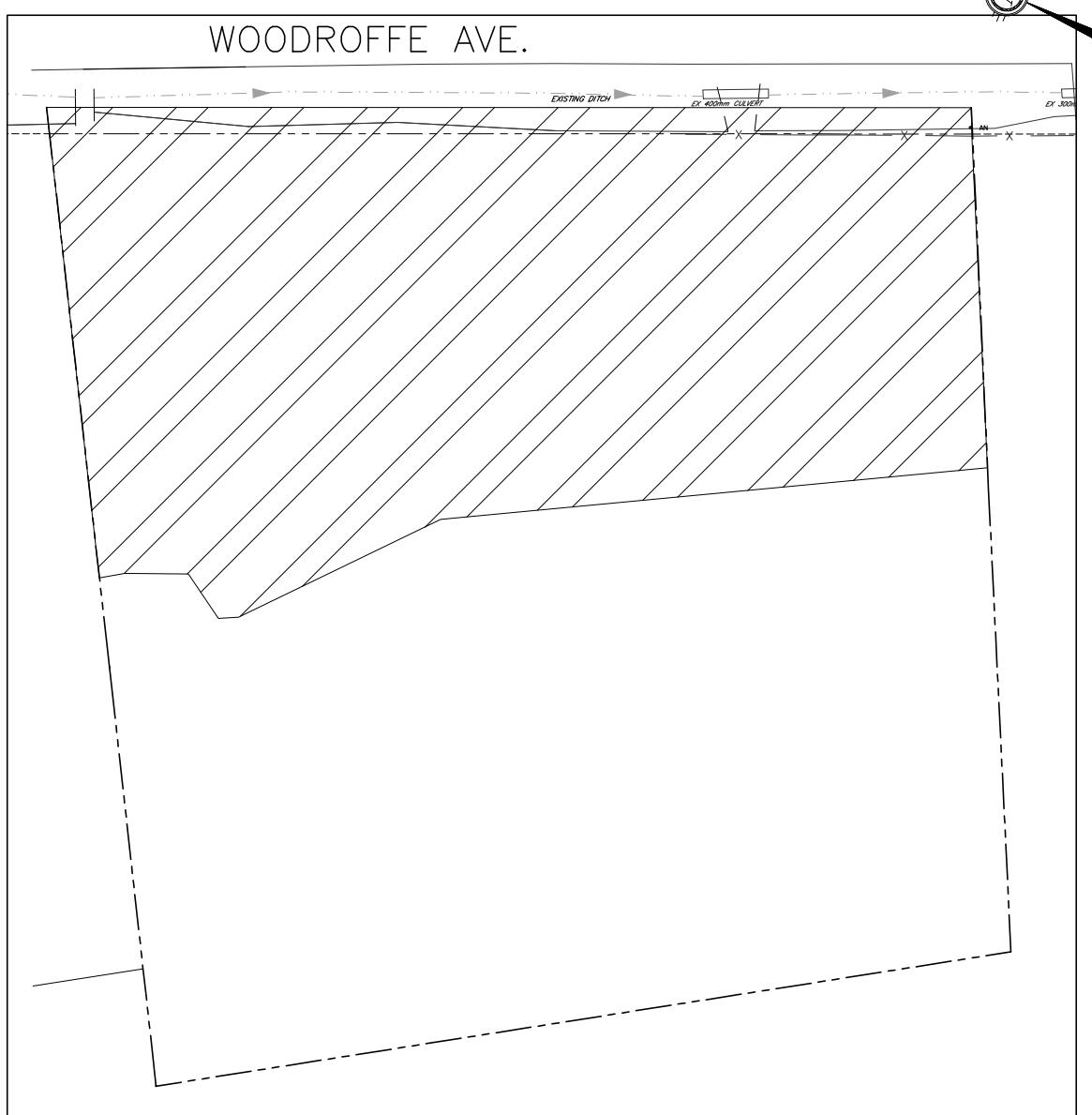
For all other road culverts the following applies. Ensure that the roadway will not be overtopped for at least the following return frequencies:

**Table 6.4 Road Type vs. Culvert Design Storm**

ROAD CLASSIFICATION	UNDER 6M SPAN	OVER 6M SPAN
Local Rural Road	10 Years	25 Years
Local Urban Road	25 Years	50 Years
Collector	25 Years	50 Years
Rural arterial	25 Year	50 Years
Urban Arterial	50 Years	100 Years

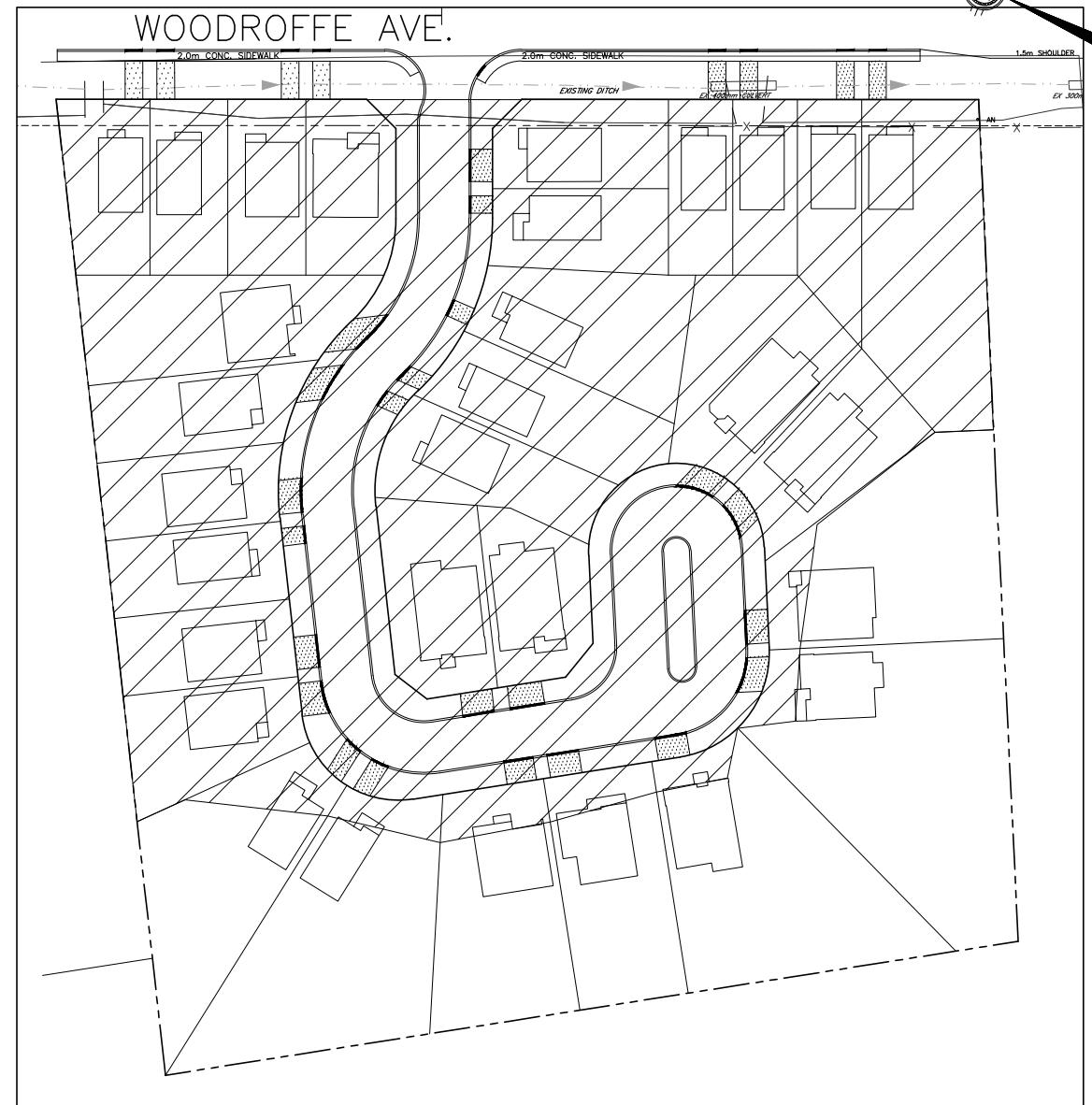
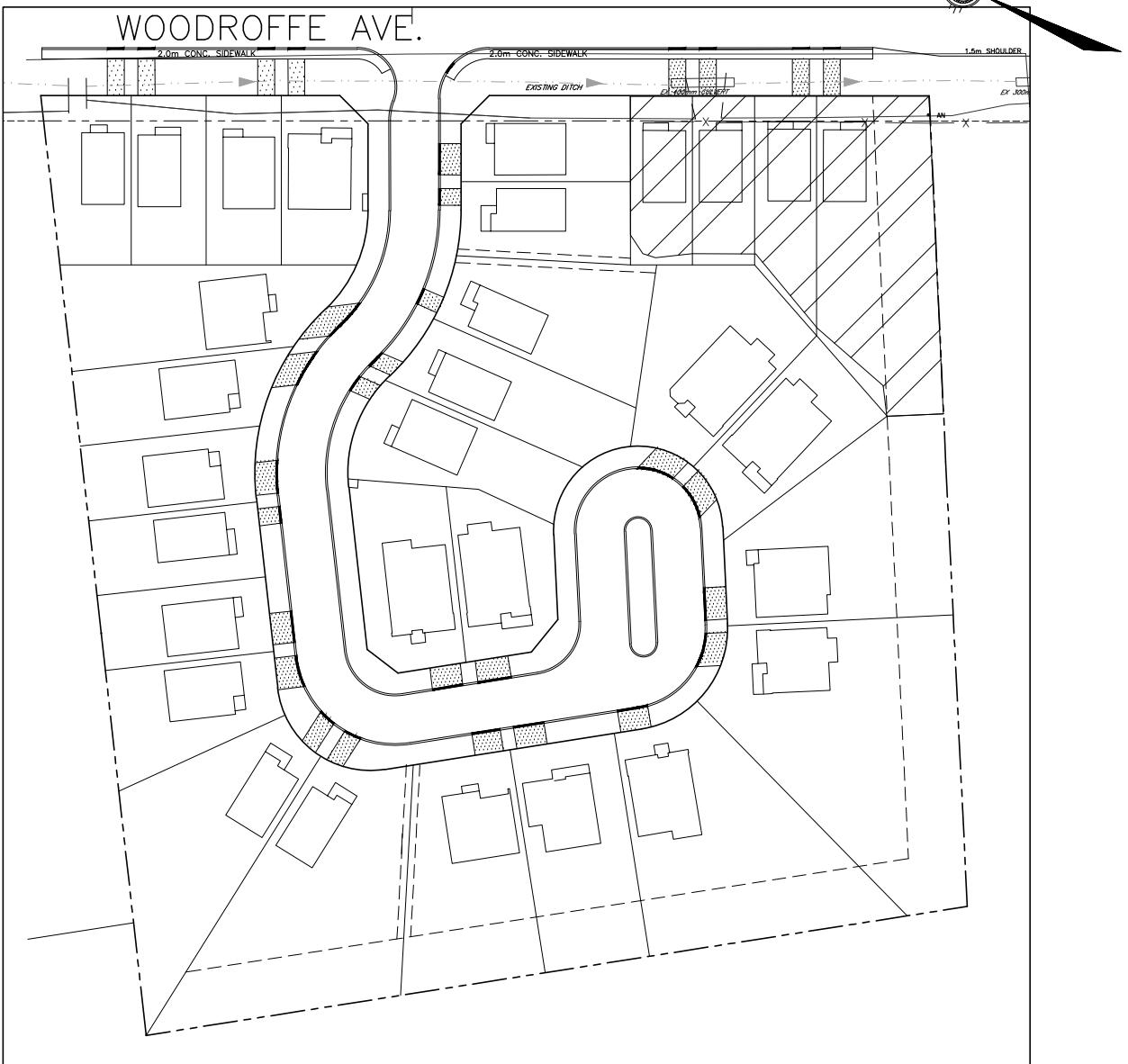
**6.4.3 Water Table Considerations**

All development shall ensure that each foundation footing is above the average water table elevation.



PRE-DEVELOPMENT RUNOFF			
RETURN PERIOD	T <sub>c</sub> (min.)	C VALUE	FLOW (L/s)
5 YEAR	14.8	0.20	51.40
100 YEAR	14.8	0.25	110.10

scale N.T.S.	BORRELLO SUBDIVISION PRE-DEVELOPMENT DRAINAGE TO WOODROFFE DITCH	project no. 14057
date 02/05/16	drawn by BLM	
		PRE-SOUTH



POST-DEVELOPMENT RUNOFF			
RETURN PERIOD	T <sub>c</sub> (min.)	C VALUE	FLOW (L/s)
5 YEAR	14.5	0.36	93.80
100 YEAR	31.5	0.53	144.00

**Robinson**  
Land Development

scale N.T.S.	BORRELLO SUBDIVISION POST-DEVELOPMENT DRAINAGE TO WOODROFFE DITCH	project no. 14057
date 02/05/16		drawn by BLM

## **Drainage Area Characteristics**

5 Year Storm Event

**Time of Concentration,  $t_c$**

**5 Year Storm Event**

Method	Equation	A1	A2	A3	A4	A5	A6
		$t_c$ (min)					
		5 year					
Airport (FAA)	$t_c = \frac{3.26 \times (1.1 - C) \times L^{0.5}}{S_w^{0.33}}$	20.0	8.4	17.8	19.4	28.0	19.6

Method	Equation	A7	A8	A9	A10	A11	A12
		$t_c$ (min)					
		5 year					
Airport (FAA)	$t_c = \frac{3.26 \times (1.1 - C) \times L^{0.5}}{S_w^{0.33}}$	28.0	42.2	24.5	20.3	42.7	28.3

**Table B.1****Rational Method Calculation Sheet****5 Year Storm Event**

Drainage Area ID	Area (ha)	Runoff	Time	Rainfall	Peak Design Flow	Cumulative Peak
		Coefficient, C	Conc.5yr	Intensity	(m <sup>3</sup> /s)	Design Flow (m <sup>3</sup> /s)
		C <sub>5yr</sub>	(min.)	5 year	5 year	5 year
A1	0.47	0.46	20.0	70.25	0.042	0.042
A2	0.18	0.39	8.4	113.47	0.022	0.064
A3	0.53	0.34	17.8	75.44	0.038	0.102
A4	1.89	0.32	19.4	71.64	0.120	0.223
A5	0.64	0.33	28.0	56.50	0.033	0.256
A6	0.21	0.33	19.6	71.22	0.014	0.270
A7	0.22	0.28	28.0	56.45	0.010	0.279
A8	0.56	0.28	42.2	42.56	0.019	0.298
A9	0.18	0.28	24.5	61.73	0.009	0.306
A10	0.36	0.34	20.3	69.61	0.024	0.330
A11	8.13	0.25	42.7	42.19	0.238	0.568
A12	1.23	0.55	28.3	56.02	0.105	0.674

**Q = 0.00278 A x I x C (m<sup>3</sup>/s), Where:**

5 yr
998.071
6.053
0.814

## Culvert Sizing Calculation Sheet

**Location:** Woodroffe Avenue  
**Watercourse:** Roadside Ditch to Jock River  
**Road Classification:** Various  
**Design Flow:** 5 Year  
**Existing Structure:** Various CSP culverts

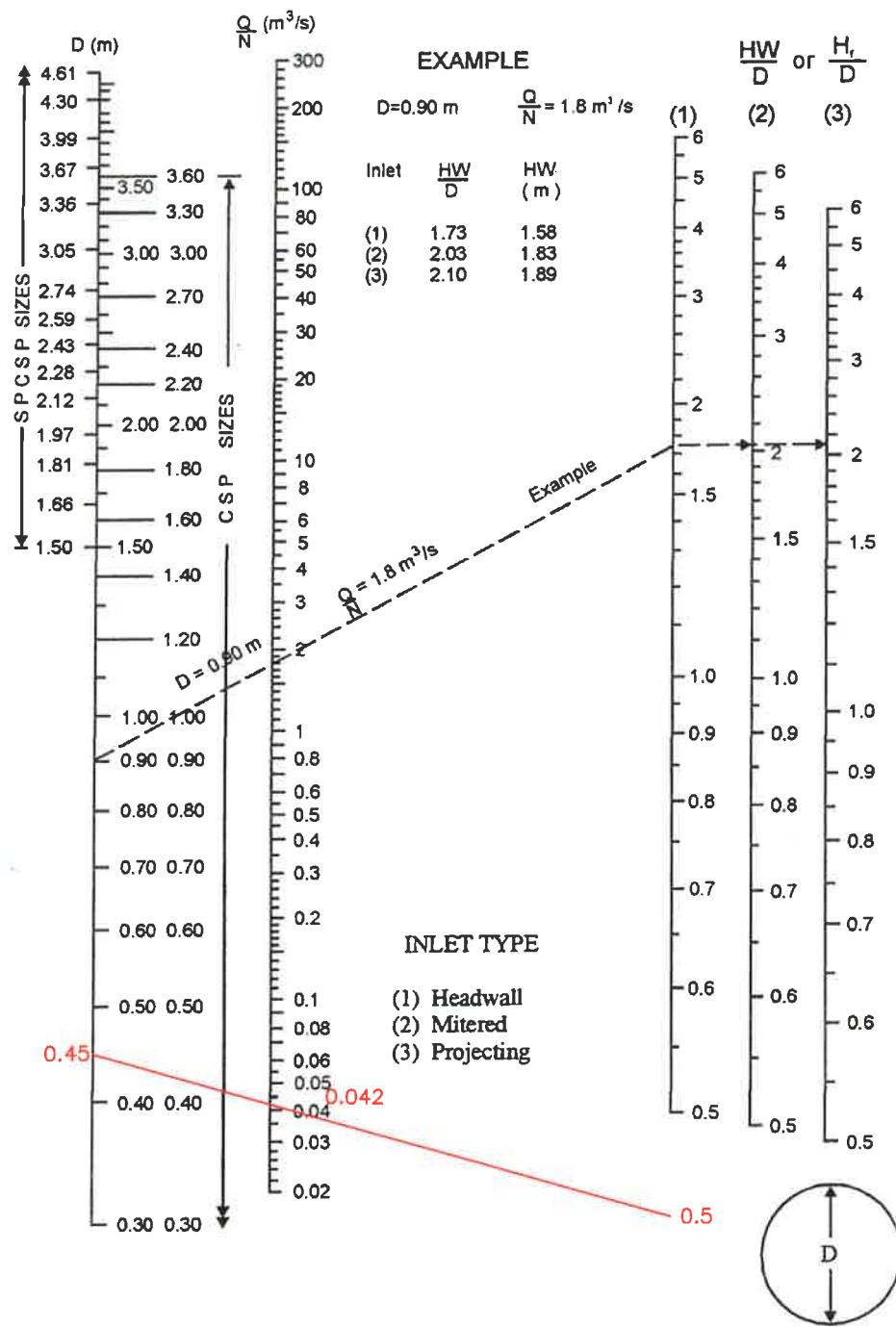
STRUCTURE	DESIGN DATA								CULVERT DATA												INLET CONTROL		OUTLET CONTROL						31	32	33	34	35		
	1 Return Year	2 Q <sub>peak</sub>	3 Type	4 Length	5 Slope	6 Top of Road	7 U/S invert	8 D/S invert	9 B	10 D	11 t	12 B/D	13 TW	14 N	15 Q/N	16 Q/NB	17 A	18 V	19 P	20 R	21 n	22 ke	23 HW/D	24 HW	25 H	26 dc	27 (dc+D)/2	28 H <sub>o</sub>	29 LS	30 HW	Gov'g HW	Water Surface	Obvert	Cover	Free board
Existing Culvert #1 450mm CSP	5	0.042	CSP	9.4	0.032	99.95	99.06	98.76	--	0.45	0.02	--		1	0.042	--	0.159	0.27	--	--	0.024	0.9	1.45	0.65	0.42	0.31	0.38	0.38	0.30	0.50	0.65	99.71	99.51	0.44	0.24
Existing Culvert #2 450mm CSP	5	0.064	CSP	12.3	0.046	98.99	98.28	97.72	--	0.45	0.02	--		1	0.064	--	0.159	0.40	--	--	0.024	0.9	1.45	0.65	0.55	0.31	0.38	0.38	0.56	0.37	0.65	98.93	98.73	0.26	0.06
Existing Culvert #3 500mm CSP	5	0.102	CSP	9.2	0.032	95.72	94.72	94.43	--	0.5	0.02	--		1	0.102	--	0.196	0.52	--	--	0.024	0.9	1.08	0.54	0.27	0.31	0.41	0.41	0.29	0.39	0.54	95.26	95.22	0.50	0.46
Existing Culvert #5 500mm CSP	5	0.256	CSP	12.5	0.002	93.85	92.70	92.67	--	0.5	0.02	--		1	0.256	--	0.196	1.30	--	--	0.024	0.9	1.11	0.56	0.29	0.31	0.41	0.41	0.03	0.66	0.66	93.37	93.20	0.65	0.48
Existing Culvert #6 500mm CSP	5	0.270	CSP	13	0.002	93.80	92.64	92.61	--	0.5	0.02	--		1	0.270	--	0.196	1.37	--	--	0.024	0.9	1.11	0.56	0.32	0.31	0.41	0.41	0.03	0.69	0.69	93.34	93.14	0.66	0.47
Existing Culvert #7 500mm CSP	5	0.279	CSP	14.5	0.002	94.00	92.57	92.54	--	0.5	0.02	--		1	0.279	--	0.196	1.42	--	--	0.024	0.9	1.2	0.60	0.38	0.31	0.41	0.41	0.03	0.76	0.76	93.33	93.07	0.93	0.67
Existing Culvert #8 500mm CSP	5	0.298	CSP	10	0.002	93.25	92.00	91.98	--	0.5	0.02	--		1	0.298	--	0.196	1.52	--	--	0.024	0.9	1.2	0.60	0.32	0.31	0.41	0.41	0.02	0.71	0.71	92.71	92.50	0.75	0.55

# EXISTING CULVERT #1

## 450mmØ CSP

MTO Drainage Management Manual

### Design Chart 2.32: Inlet Control: Circular CSP and SPCSP Culverts



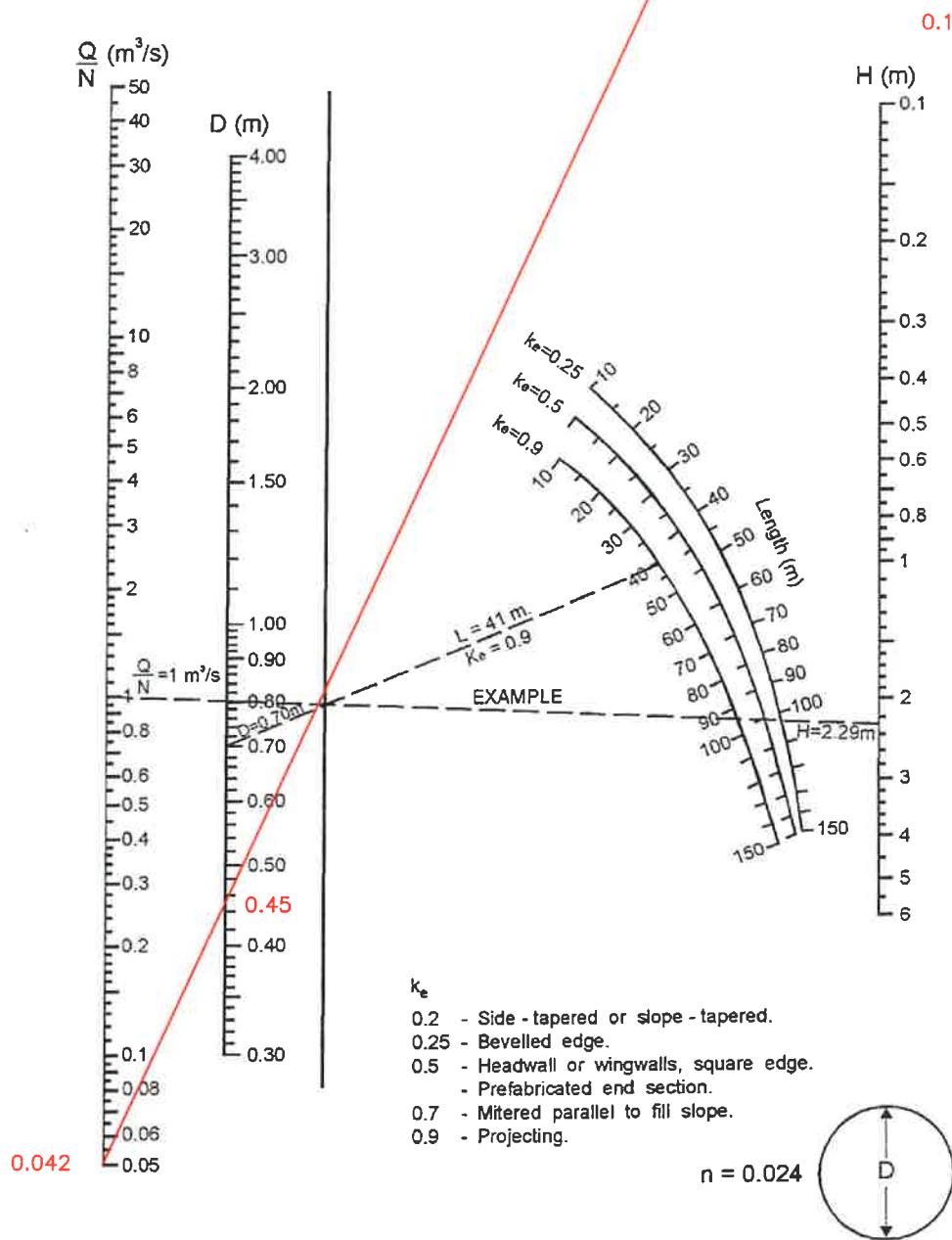
Source: Herr (1977)

# EXISTING CULVERT #1

## 450mmØ CSP

[Design Charts](#)

**Design Chart 2.35: Outlet Control: CSP Culvert - Flowing Full**



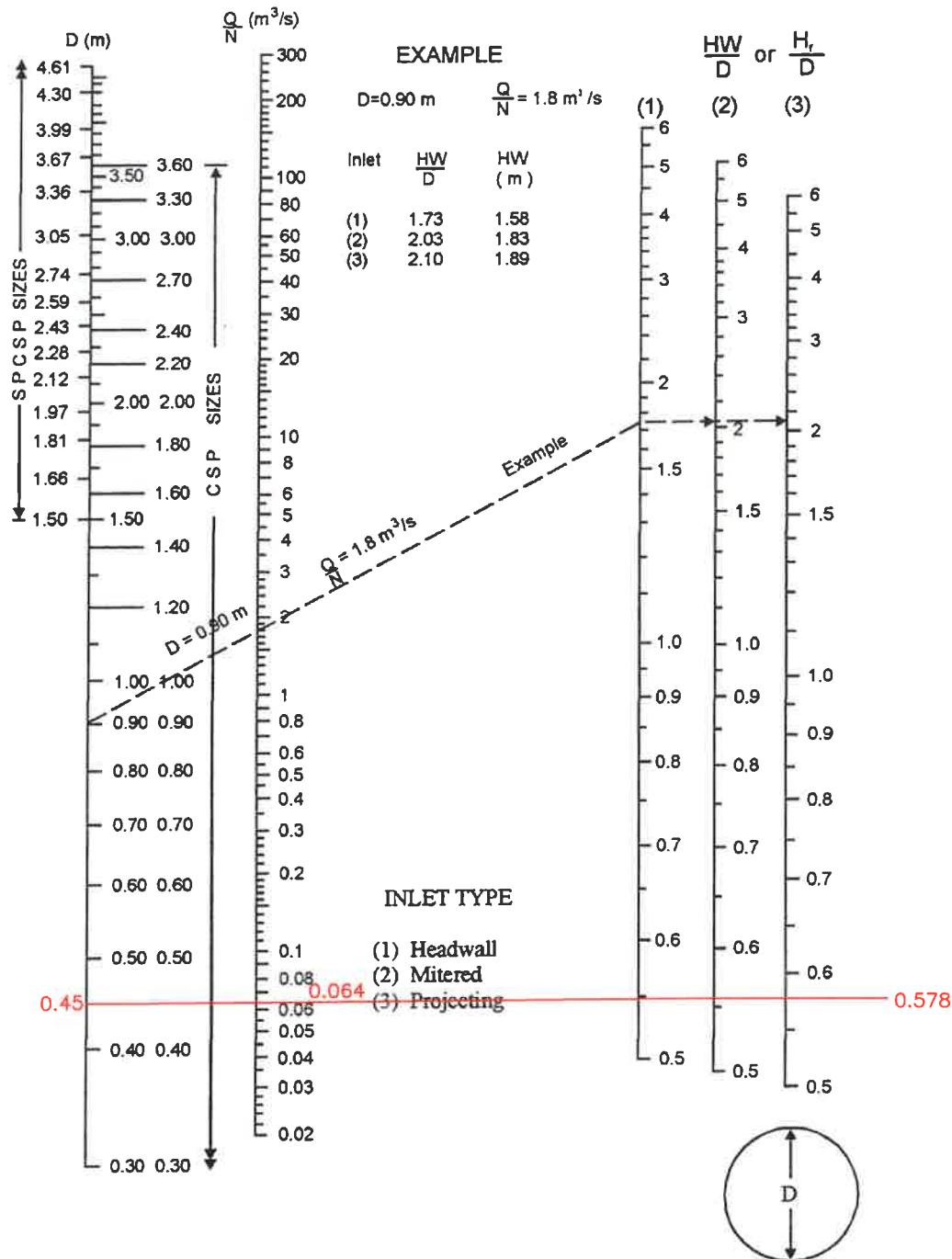
Source: Herr (1977)

# EXISTING CULVERT #2

## 450mmØ CSP

MTO Drainage Management Manual

### Design Chart 2.32: Inlet Control: Circular CSP and SPCSP Culverts



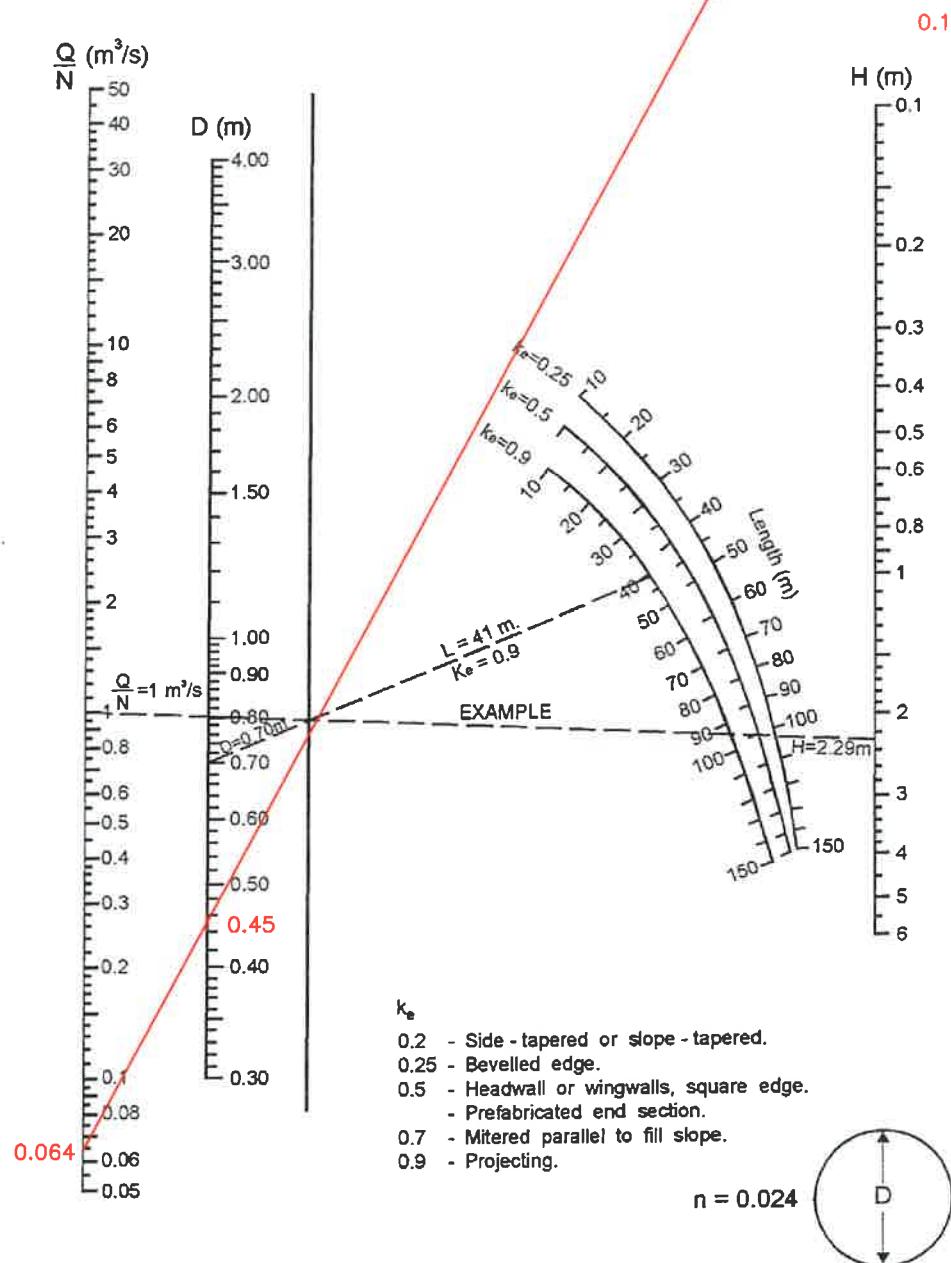
Source: Herr (1977)

# EXISTING CULVERT #2

## 450mmØ CSP

[Design Charts](#)

Design Chart 2.35: Outlet Control: CSP Culvert - Flowing Full



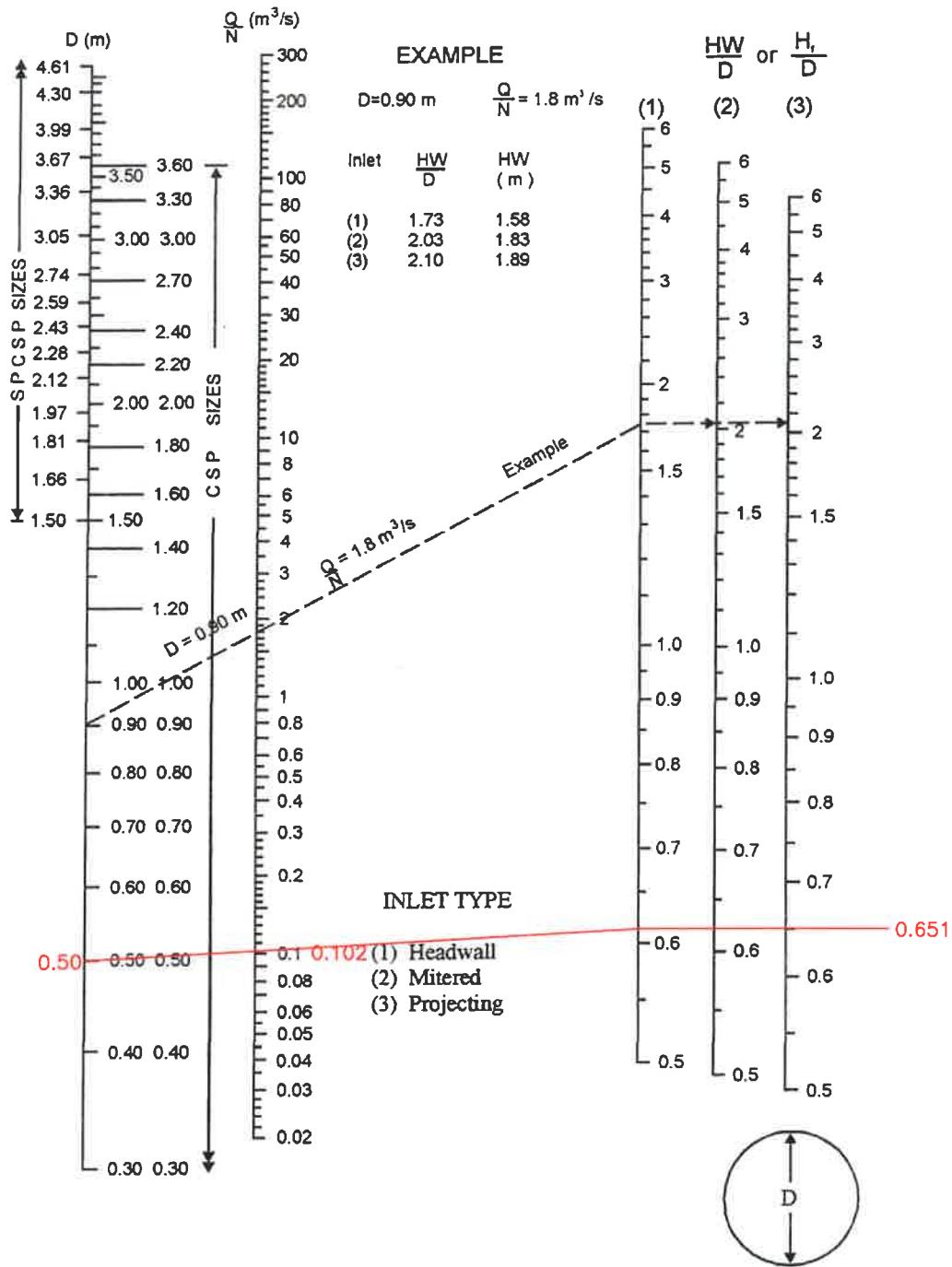
Source: Herr (1977)

# EXISTING CULVERT #3

## 500mmØ CSP

MTO Drainage Management Manual

### Design Chart 2.32: Inlet Control: Circular CSP and SPCSP Culverts



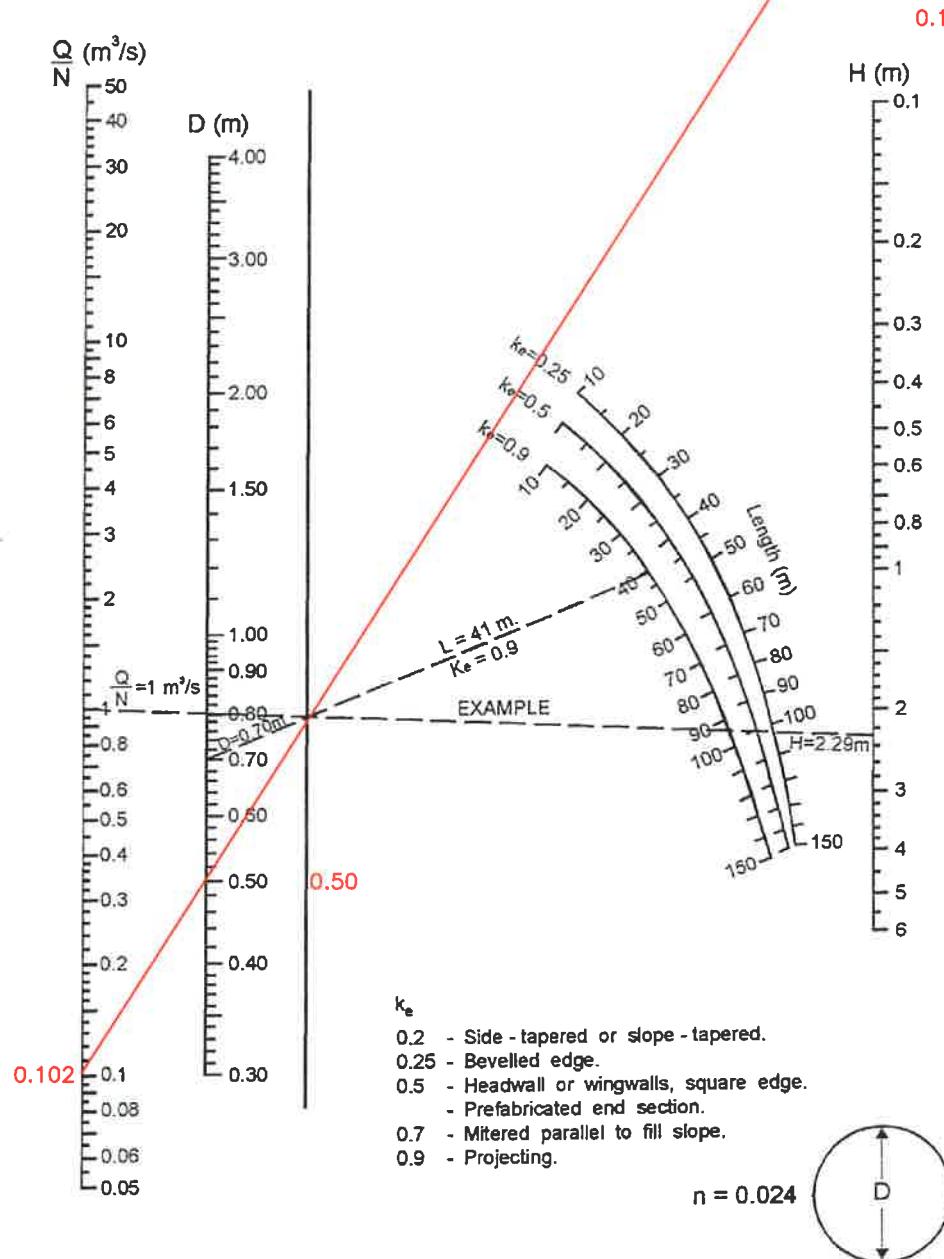
Source: Herr (1977)

# EXISTING CULVERT #3

## 500mmØ CSP

[Design Charts](#)

Design Chart 2.35: Outlet Control: CSP Culvert - Flowing Full

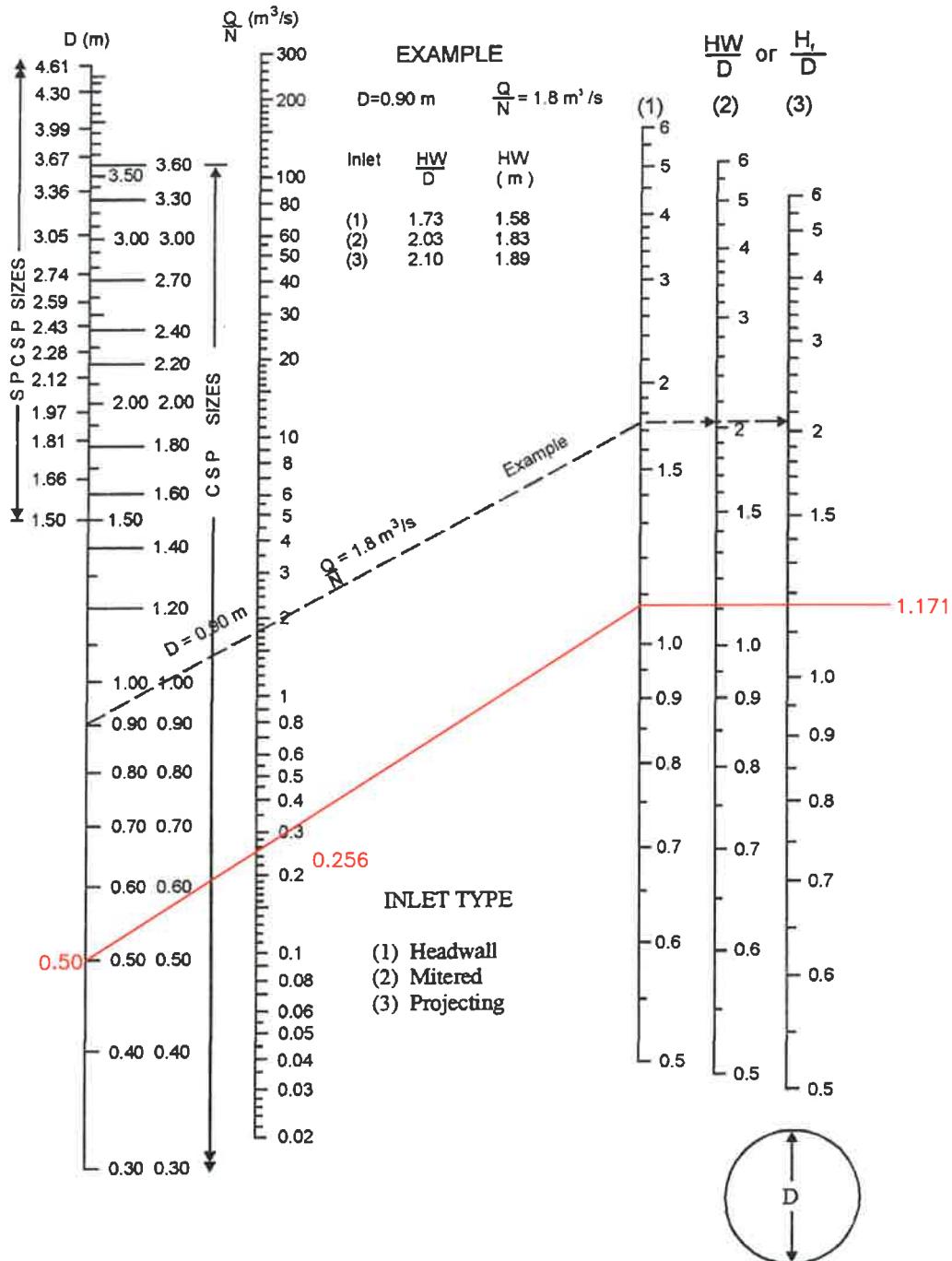


Source: Herr (1977)

EXISTING CULVERT #5  
500mmØ CSP

## MTO Drainage Management Manual

### **Design Chart 2.32: Inlet Control: Circular CSP and SPCSP Culverts**



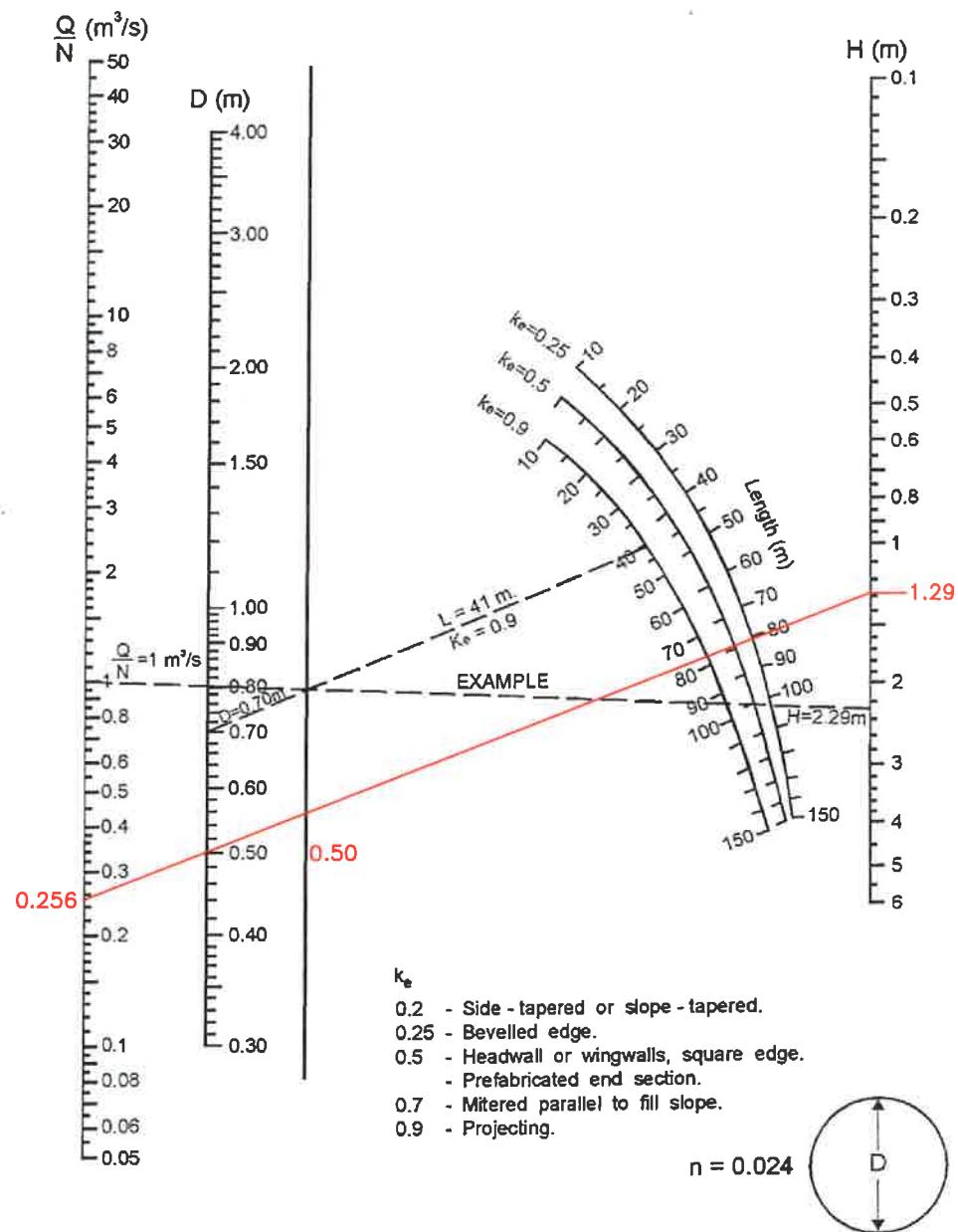
Source: Herr (1977)

# EXISTING CULVERT #5

## 500mmØ CSP

[Design Charts](#)

**Design Chart 2.35: Outlet Control: CSP Culvert - Flowing Full**



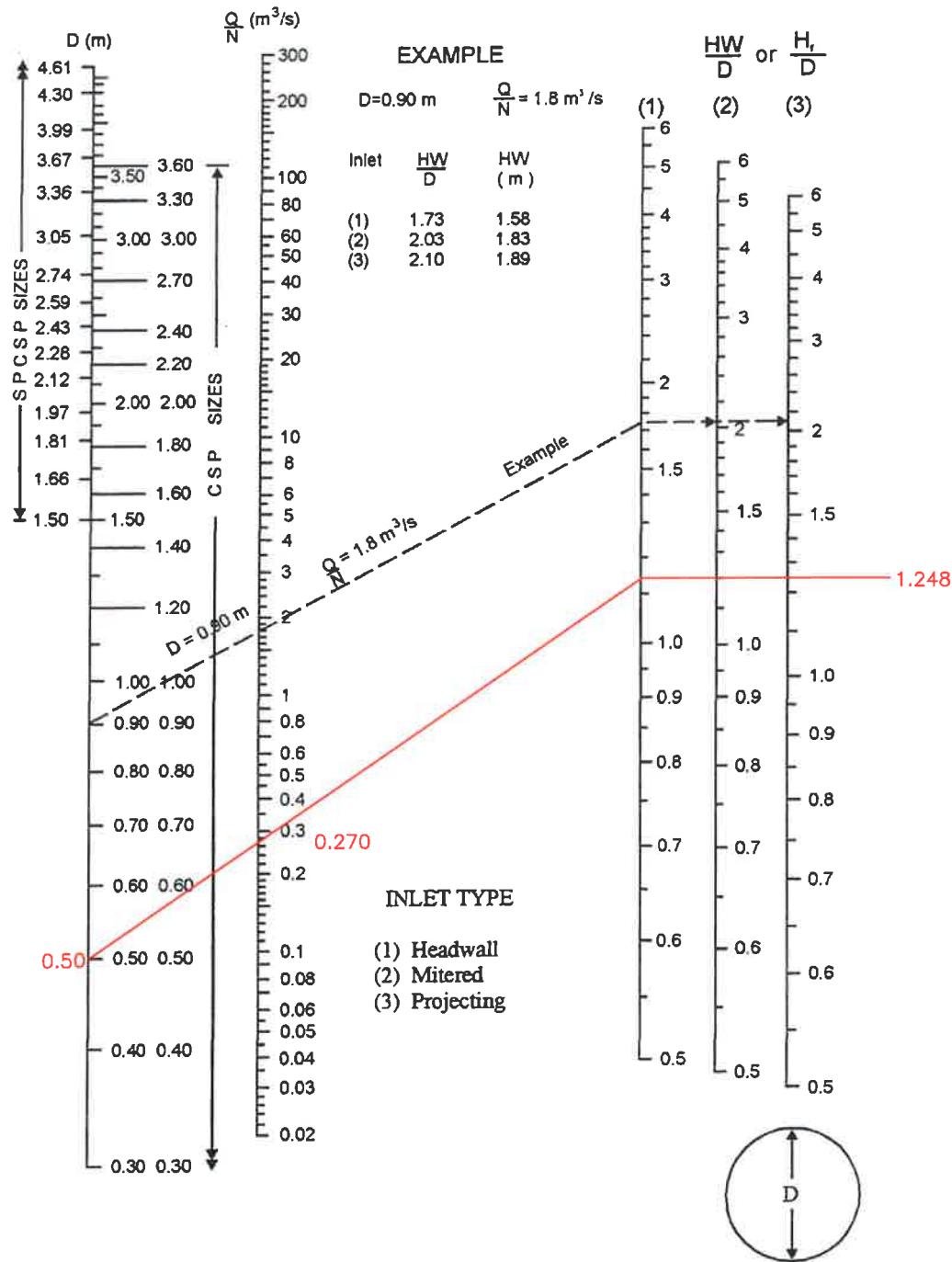
Source: Herr (1977)

# EXISTING CULVERT #6

## 500mm $\varnothing$ CSP

MTO Drainage Management Manual

### Design Chart 2.32: Inlet Control: Circular CSP and SPCSP Culverts



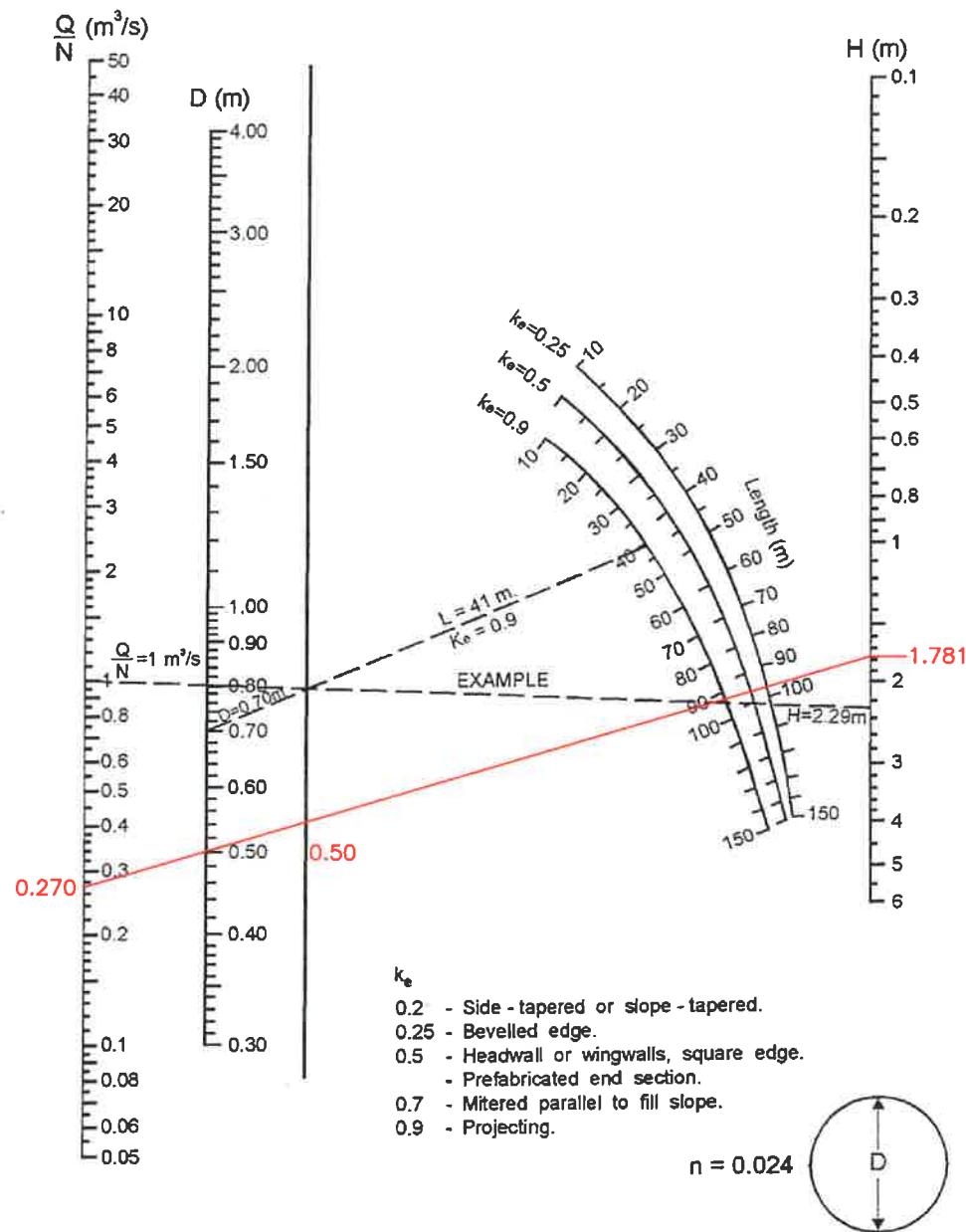
Source: Herr (1977)

# EXISTING CULVERT #6

## 500mmØ CSP

[Design Charts](#)

**Design Chart 2.35: Outlet Control: CSP Culvert - Flowing Full**



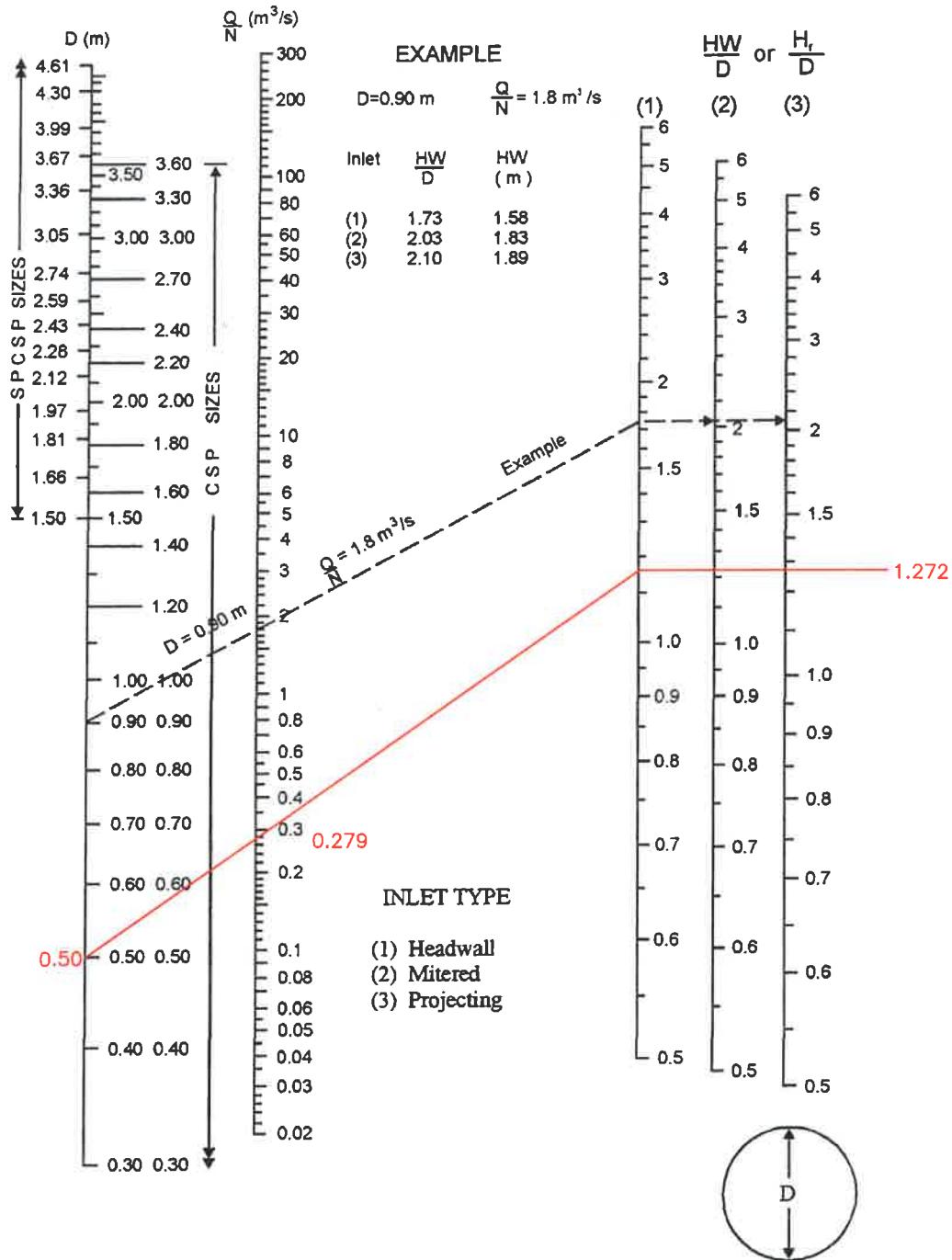
Source: Herr (1977)

# EXISTING CULVERT #7

## 500mmØ CSP

MTO Drainage Management Manual

### Design Chart 2.32: Inlet Control: Circular CSP and SPCSP Culverts



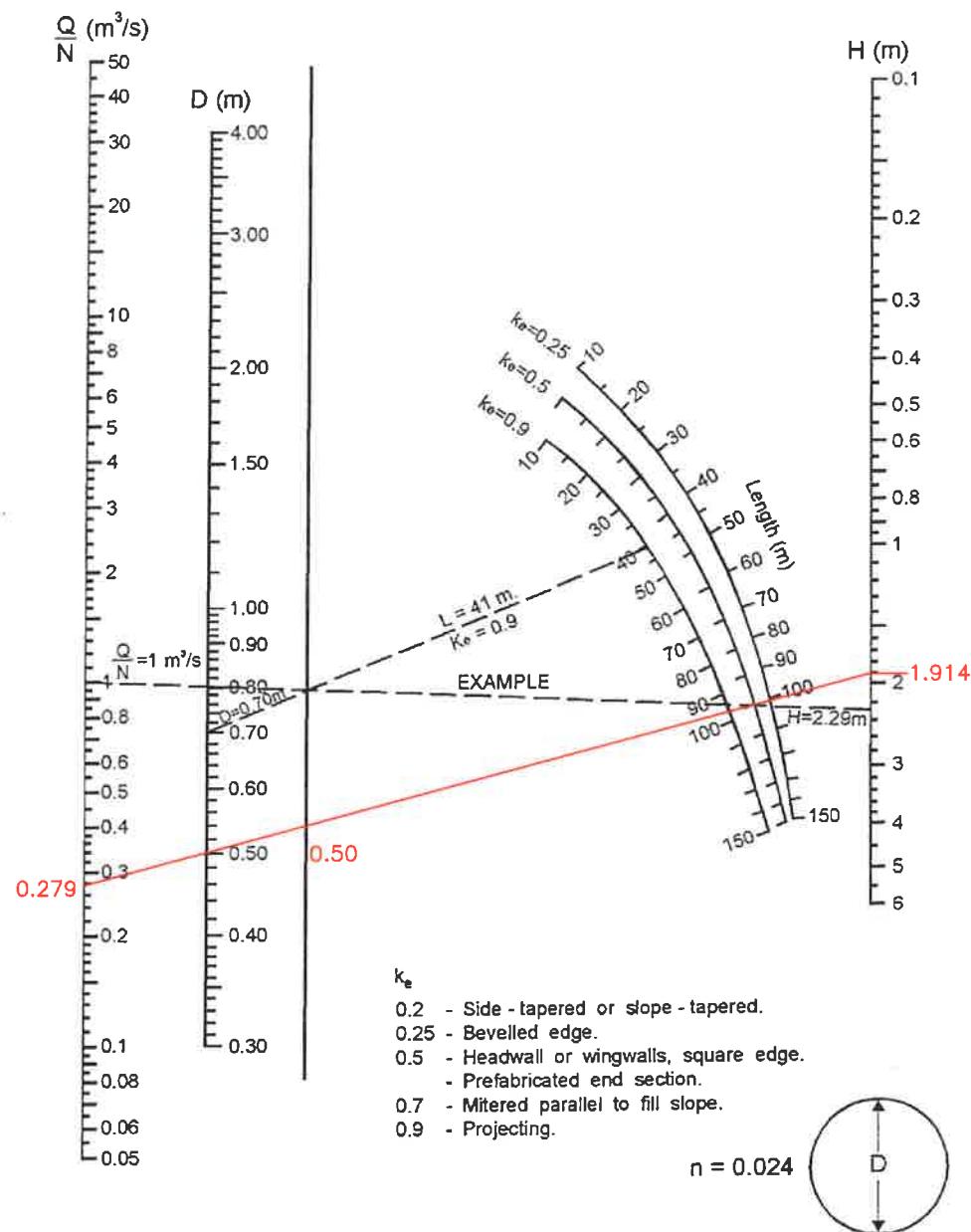
Source: Herr (1977)

# EXISTING CULVERT #7

## 500mmØ CSP

### Design Charts

**Design Chart 2.35: Outlet Control: CSP Culvert - Flowing Full**



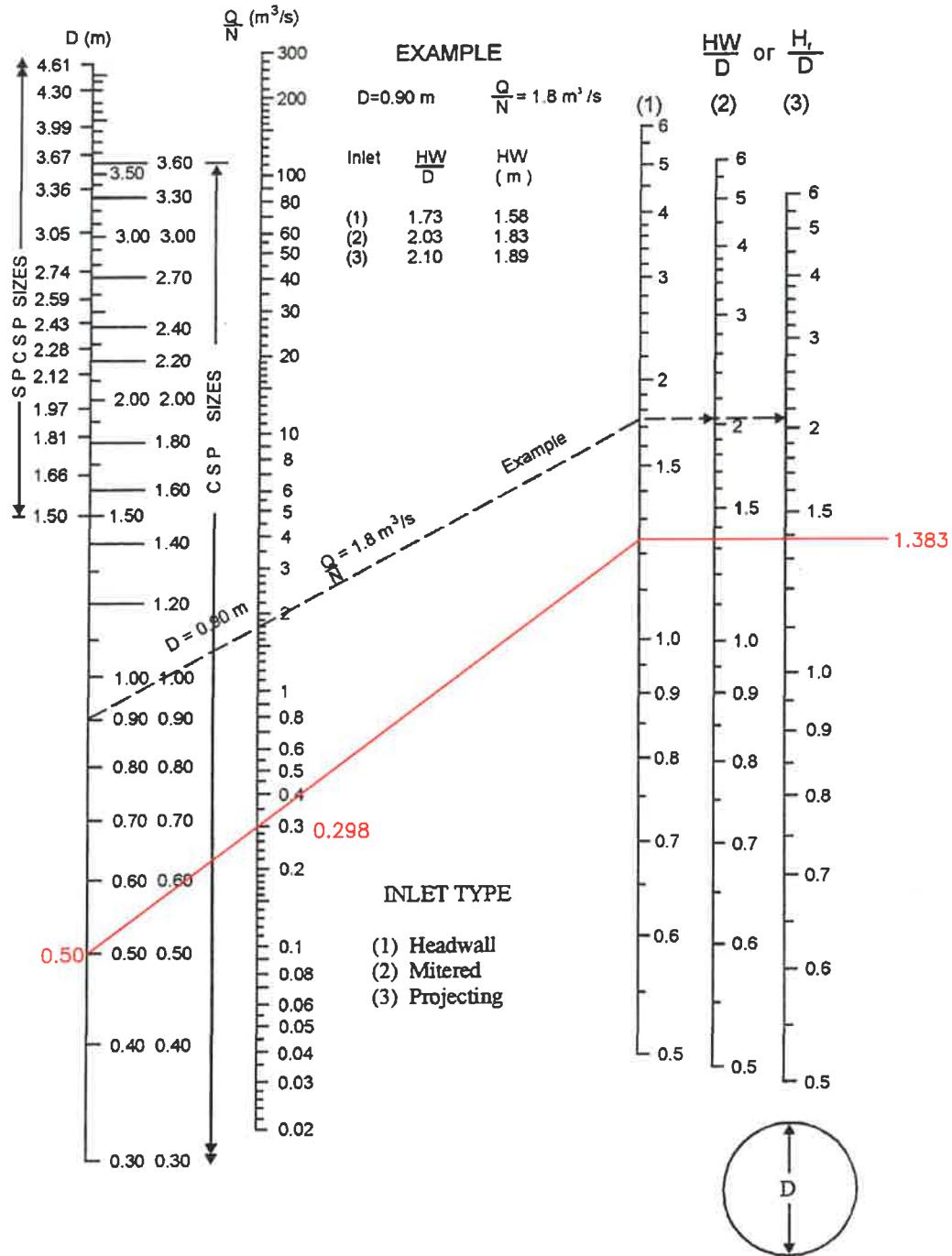
Source: Herr (1977)

# EXISTING CULVERT #8

## 500mm $\phi$ CSP

MTO Drainage Management Manual

### Design Chart 2.32: Inlet Control: Circular CSP and SPCSP Culverts



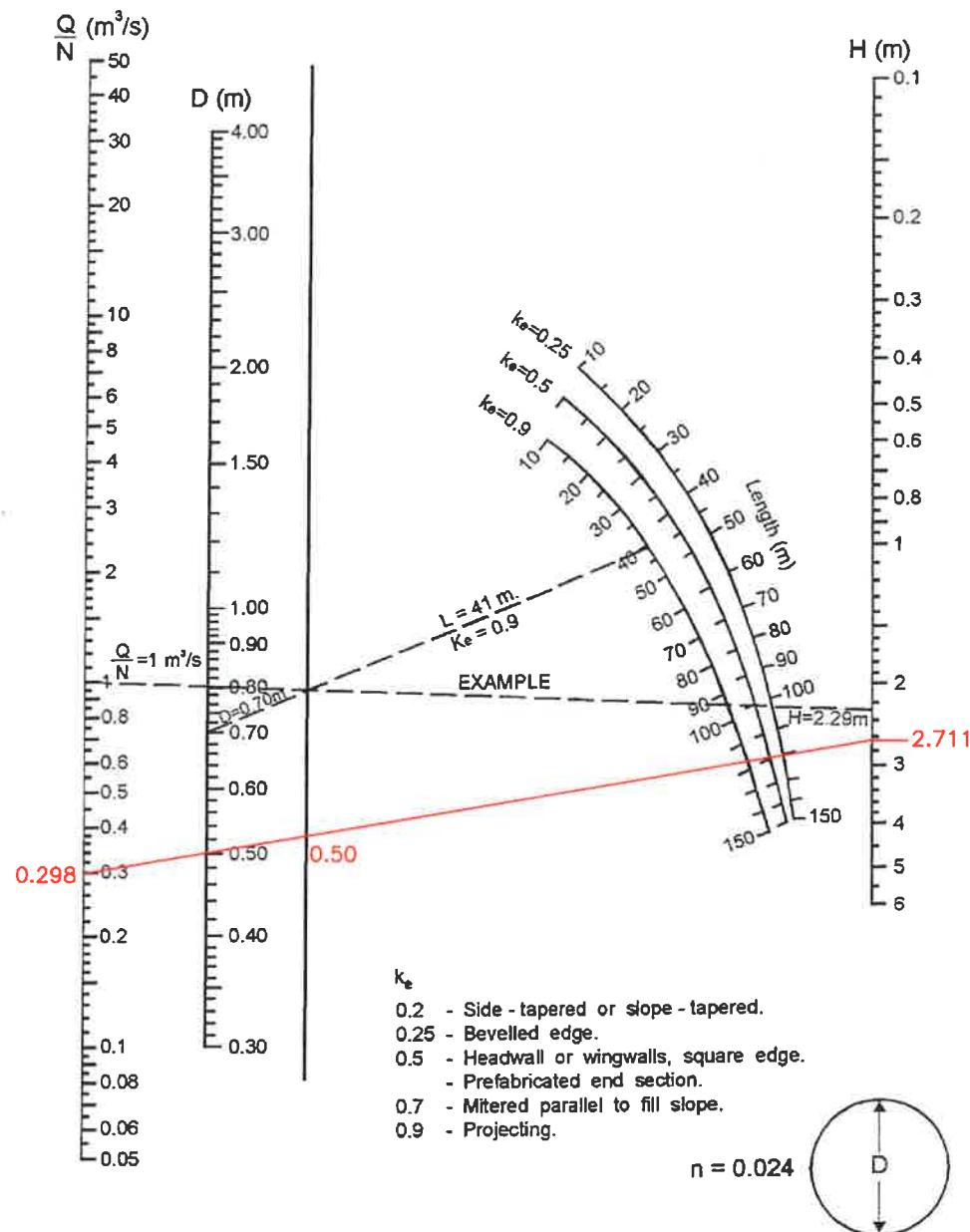
Source: Herr (1977)

# EXISTING CULVERT #8

## 500mmØ CSP

Design Charts

Design Chart 2.35: Outlet Control: CSP Culvert - Flowing Full



Source: Herr (1977)

## **Drainage Area Characteristics**

## **25, 50 Year Storm Event**

Return Frequency	A	B	C	$Q = 2.78 CIA$ $I = (A / T_c + C)^B$ <p>Where Q = peak flow (L/s) A = area (ha) I = rainfall intensity (mm/hr) C = runoff coefficient <math>T_c</math> = time of concentration (min)</p>	<b>Table 1</b> <b>SWM DESIGN SHEET</b> <b>PROPOSED CONDITIONS (25 yr)</b> <small>IDF - Macdonald-Cartier Airport, 1967-1997 RCI_STM v1.02 (130204)</small>	Project Information						<b>Robinson</b> <b>Consultants</b> <small>Page 1 of 1</small>								
	2 yr	732.951	0.810	6.199																
5 yr	998.071	0.814	6.053																	
10 yr	1174.184	0.816	6.014																	
25 yr	1402.884	0.819	6.018																	
50 yr	1569.580	0.820	6.014																	
100 yr	1735.688	0.820	6.014																	
<b>LOCATION</b>				<b>CATCHMENT AREA</b>				<b>FLOW DATA</b>				<b>SEWER DATA</b>								
DRAINAGE AREA	LOCATION	EX. PIPE ID / PROPOSED	Start	End	10-Yr Design Storm			Time of Concentration $T_c$ (min)	Rainfall Intensity	Peak Flow	Total Peak Flow $Q_{total}$ (m³/s)	<b>PHYSICAL PROPERTIES</b>				<b>FLOW &amp; VELOCITY DATA</b>				
					Area A (ha)	C	Individual 2.78 AC		25-Yr $I_{25yr}$ (mm/hr)	25-Yr $Q_{25yr}$ (m³/s)		Material Type	Roughness Coefficient (n)	Slope (%)	Water Depth (m)	Flow Area (m²)	Length (m)	Capacity Q (m³/s)	Full Flow Velocity (m/s)	Time of Flow (min)
<b>Woodroffe Ave. (Stoneleigh St. to Prince of Wales Dr.)</b>																				
SD	Woodroffe	Ditch	SD Outlet	End A1				125.00 *(1)	25.88	0.16 *(2)	0.16	Grass	0.035	0.0667	0.0443	0.12	105.00		1.42	1.23
A1	Woodroffe	Ditch	SD Outlet	End A1	0.47	0.51	0.66	126.23	25.68	0.17	0.17	Grass	0.035	0.0320	0.0443	0.12	105.00		1.42	1.23
A2	Woodroffe	Ditch	End A1	End A2	0.18	0.43	0.21	127.46	25.49	0.18	0.18	Grass	0.035	0.0385	0.0429	0.12	25.60		1.52	0.28
A3	Woodroffe	Ditch	End A2	End A3	0.53	0.37	0.55	127.74	25.44	0.19	0.19	Grass	0.035	0.0390	0.0393	0.11	79.40		1.82	0.73
A4	Woodroffe	Ditch	End A3	End A4	1.89	0.35	1.85	128.47	25.33	0.24	0.24	Grass	0.035	0.0168	0.0368	0.18	136.25		1.33	1.71
A5	Woodroffe	Ditch	End A4	End A5	0.64	0.36	0.65	130.18	25.07	0.25	0.25	Grass	0.035	0.0015	0.3555	0.38	53.75		0.66	1.36
A6	Woodroffe	Ditch	End A5	End A6	0.21	0.36	0.21	131.54	24.87	0.26	0.26	Grass	0.035	0.0024	0.3335	0.34	26.25		0.76	0.58
A7	Woodroffe	Ditch	End A6	End A7	0.22	0.31	0.19	132.11	24.78	0.26	0.26	Grass	0.035	0.0022	0.3384	0.35	37.50		0.75	0.84
A8	Woodroffe	Ditch	End A7	End A8	0.56	0.31	0.48	132.95	24.66	0.27	0.27	Grass	0.035	0.0021	0.3461	0.36	108.10		0.74	2.42
A9	Woodroffe	Ditch	End A8	End A9	0.18	0.31	0.15	135.38	24.31	0.27	0.27	Grass	0.035	0.0070	0.2876	0.25	35.60		1.07	0.55
A10	Woodroffe	Ditch	End A9	End A10	0.36	0.37	0.37	135.93	24.23	0.28	0.28	Grass	0.035	0.0105	0.2732	0.23	68.10		1.23	0.93
<b>Prince of Wales Dr. (Woodroffe Ave. to Lodge Rd.)</b>																				
A11	Prince of Wales	Ditch	End A10	End A11	8.13	0.28	6.22	136.85	24.11	0.43	0.43	Grass	0.035	0.0092	0.3171	0.30	340.00		1.40	4.05
A12	Prince of Wales	Ditch	End A11	End A12	1.23	0.61	2.07	140.91	23.56	0.47	0.47	Grass	0.035	0.0128	0.3097	0.29	57.50		1.60	0.60

Note 1: Time of Concentration for Subdivision (SD) calculated from Time of Peak for peak outlet flows from Subdivision. Equation used is TP/0.6 (From SWMHYMO Manual)

$$T_c = TP/0.6 = 75/0.6 = 125$$

Note 2: Total Peak Flow for Subdivision (SD) calculated from DDSWMM Output table.

Return Frequency	A	B	C	$Q = 2.78 CIA$ $I = (A / T_c + C)^B$ Where Q = peak flow (L/s) A = area (ha) I = rainfall intensity (mm/hr) C = runoff coefficient $T_c$ = time of concentration (min)	<b>Table 2</b> <b>SWM DESIGN SHEET</b> <b>PROPOSED CONDITIONS (50 yr)</b> IDF - Macdonald-Cartier Airport, 1967-1997 RCI_STM v1.02 (130204)	Project Information						<b>Robinson</b> <b>Consultants</b> Page 1 of 1								
	2 yr	732.951	0.810	6.199		Project Name	Borrello Subdivision SWM													
	5 yr	998.071	0.814	6.053		File No.	14057		Contract No.											
	10 yr	1174.184	0.816	6.014		Name			Company	Date										
	25 yr	1402.884	0.819	6.018		Design	CN	RCI	20/10/2016											
	50 yr	1569.580	0.820	6.014		Check	BSA	RCI	21/10/2016											
	100 yr	1735.688	0.820	6.014																
<b>LOCATION</b>					<b>CATCHMENT AREA</b>					<b>FLOW DATA</b>						<b>SEWER DATA</b>				
DRAINAGE AREA	LOCATION	EX. PIPE ID / PROPOSED	Start	End	10-Yr Design Storm			Time of Concentration $T_c$ (min)	Rainfall Intensity	Peak Flow	Total Peak Flow $Q_{total}$ (m³/s)	<b>PHYSICAL PROPERTIES</b>						<b>FLOW &amp; VELOCITY DATA</b>		
					Area A (ha)	C	Individual 2.78 AC		50-Yr $I_{50yr}$ (mm/hr)	50-Yr $Q_{50yr}$ (m³/s)		Material Type	Roughness Coefficient (n)	Slope (%)	Water Depth (m)	Flow Area (m²)	Length (m)	Capacity Q (m³/s)	Full Flow Velocity (m/s)	Time of Flow (min)
<b>Woodroffe Ave. (Stoneleigh St. to Prince of Wales Dr.)</b>																				
SD	Woodroffe	Ditch	SD Outlet	End A1				125.00 *(1)	28.81	0.20 *(2)	0.20	Grass	0.035	0.0667	0.0491	0.14	105.00		1.55	1.13
A1	Woodroffe	Ditch	SD Outlet	End A1	0.47	0.55	0.72	126.13	28.61	0.22	0.22	Grass	0.035	0.0320	0.0475	0.13	105.00		1.65	1.06
A2	Woodroffe	Ditch	End A1	End A2	0.18	0.47	0.23	127.19	28.42	0.22	0.22	Grass	0.035	0.0385	0.0436	0.12	25.60		1.98	0.22
A3	Woodroffe	Ditch	End A2	End A3	0.53	0.41	0.60	127.40	28.39	0.24	0.24	Grass	0.035	0.0390	0.0414	0.20	79.40		1.44	0.92
A4	Woodroffe	Ditch	End A3	End A4	1.89	0.38	2.02	128.32	28.23	0.29	0.29	Grass	0.035	0.0168	0.3775	0.43	136.25		0.71	3.18
A5	Woodroffe	Ditch	End A4	End A5	0.64	0.40	0.70	131.50	27.69	0.31	0.31	Grass	0.035	0.0015	0.3543	0.38	53.75		0.82	1.09
A6	Woodroffe	Ditch	End A5	End A6	0.21	0.40	0.23	132.59	27.51	0.31	0.31	Grass	0.035	0.0024	0.3594	0.39	26.25		0.81	0.54
A7	Woodroffe	Ditch	End A6	End A7	0.22	0.34	0.21	133.14	27.42	0.32	0.32	Grass	0.035	0.0022	0.3676	0.41	37.50		0.80	0.78
A8	Woodroffe	Ditch	End A7	End A8	0.56	0.34	0.52	133.91	27.30	0.33	0.33	Grass	0.035	0.0021	0.3060	0.28	108.10		1.17	1.55
A9	Woodroffe	Ditch	End A8	End A9	0.18	0.34	0.17	135.46	27.05	0.33	0.33	Grass	0.035	0.0070	0.2907	0.26	35.60		1.33	0.45
A10	Woodroffe	Ditch	End A9	End A10	0.36	0.41	0.41	135.90	26.98	0.34	0.34	Grass	0.035	0.0105	0.3371	0.34	68.10		1.52	0.75
<b>Prince of Wales Dr. (Woodroffe Ave. to Lodge Rd.)</b>																				
A11	Prince of Wales	Ditch	End A10	End A11	8.13	0.30	6.78	136.65	26.87	0.52	0.52	Grass	0.035	0.0092	0.3371	0.34	340.00		1.52	3.74
A12	Prince of Wales	Ditch	End A11	End A12	1.23	0.66	2.26	140.39	26.30	0.57	0.57	Grass	0.035	0.0128	0.3294	0.33	57.50		1.73	0.55

Note 1: Time of Concentration for Subdivision (SD) calculated from Time of Peak for peak outlet flows from DDSWMM. Equation used is TP/0.6 (From SWMHYMO Manual)

$$T_c = TP/0.6 = 75/0.6 = 125$$

Note 2: Total Peak Flow for Subdivision (SD) calculated from DDSWMM Output table.

Return Frequency	A	B	C	$Q = 2.78 CIA$ $I = (A / T_c + C)^B$ <p>Where Q = peak flow (L/s) A = area (ha) I = rainfall intensity (mm/hr) C = runoff coefficient <math>T_c</math> = time of concentration (min)</p> <p>IDF - Macdonald-Cartier Airport, 1967-1997 RCI_STM v1.02 (130204)</p>			Project Information				<b>Robinson Consultants</b> Borrello Subdivision SWM File No. 14057 Contract No. Name Date Design CN RCI 20/10/2016 Check BSA RCI 21/10/2016 Page 1 of 1								
2 yr	732.951	0.810	6.199																
5 yr	998.071	0.814	6.053																
10 yr	1174.184	0.816	6.014																
25 yr	1402.884	0.819	6.018																
50 yr	1569.580	0.820	6.014																
100 yr	1735.688	0.820	6.014																
LOCATION					CATCHMENT AREA			FLOW DATA			SEWER DATA								
DRAINAGE AREA	LOCATION	EX. PIPE ID / PROPOSED	Start	End	10-Yr Design Storm			Time of Concentration $T_c$ (min)	Rainfall Intensity	Peak Flow	Total Peak Flow $Q_{total}$ (m³/s)	PHYSICAL PROPERTIES				FLOW & VELOCITY DATA			
					Area A (ha)	C	Individual 2.78 AC					Material Type	Roughness Coefficient (n)	Slope (%)	Water Depth (m)	Flow Area (m²)	Length (m)	Capacity Q (m³/s)	Full Flow Velocity (m/s)
<b>Woodroffe Ave. (Stoneleigh St. to Prince of Wales Dr.)</b>																			
SD	Woodroffe	Ditch	SD Outlet	End A1				125.00 *(1)	31.86	0.23 *(2)	0.23	Grass	0.035	0.0667	0.0524	0.15	105.00	1.64	1.07
A1	Woodroffe	Ditch	SD Outlet	End A1	0.47	0.58	0.75	126.07	31.65	0.25	0.25	Grass	0.035	0.0320	0.0507	0.15	105.00	1.75	1.00
A2	Woodroffe	Ditch	End A1	End A2	0.18	0.49	0.24	127.07	31.45	0.25	0.25	Grass	0.035	0.0385	0.0466	0.13	25.60	2.10	0.20
A3	Woodroffe	Ditch	End A2	End A3	0.53	0.43	0.63	127.27	31.42	0.27	0.27	Grass	0.035	0.0390	0.0446	0.22	79.40	1.53	0.87
A4	Woodroffe	Ditch	End A3	End A4	1.89	0.40	2.10	128.14	31.25	0.34	0.34	Grass	0.035	0.0168	0.3937	0.47	136.25	0.75	3.01
A5	Woodroffe	Ditch	End A4	End A5	0.64	0.41	0.73	131.15	30.69	0.35	0.35	Grass	0.035	0.0015	0.3696	0.41	53.75	0.87	1.03
A6	Woodroffe	Ditch	End A5	End A6	0.21	0.41	0.24	132.18	30.50	0.36	0.36	Grass	0.035	0.0024	0.3750	0.43	26.25	0.86	0.51
A7	Woodroffe	Ditch	End A6	End A7	0.22	0.35	0.21	132.69	30.41	0.36	0.36	Grass	0.035	0.0022	0.3836	0.45	37.50	0.85	0.73
A8	Woodroffe	Ditch	End A7	End A8	0.56	0.35	0.54	133.43	30.27	0.38	0.38	Grass	0.035	0.0021	0.3193	0.31	108.10	1.23	1.46
A9	Woodroffe	Ditch	End A8	End A9	0.18	0.35	0.18	134.89	30.02	0.38	0.38	Grass	0.035	0.0070	0.3034	0.28	35.60	1.41	0.42
A10	Woodroffe	Ditch	End A9	End A10	0.36	0.43	0.43	135.31	29.94	0.39	0.39	Grass	0.035	0.0105	0.3520	0.38	68.10	1.61	0.71
<b>Prince of Wales Dr. (Woodroffe Ave. to Lodge Rd.)</b>																			
A11	Prince of Wales	Ditch	End A10	End A11	8.13	0.31	7.06	136.02	29.82	0.60	0.60	Grass	0.035	0.0092	0.3520	0.38	340.00	1.61	3.53
A12	Prince of Wales	Ditch	End A11	End A12	1.23	0.69	2.35	139.55	29.23	0.66	0.66	Grass	0.035	0.0128	0.3440	0.36	57.50	1.84	0.52

Note 1: Time of Concentration for Subdivision (SD) calculated from Time of Peak for peak outlet flows from DDSWMM. Equation used is TP/0.6 (From SWMHYMO Manual)

$$T_c = TP/0.6 = 75/0.6 = 125$$

Note 2: Total Peak Flow for Subdivision (SD) calculated from DDSWMM Output table.

Location:	<b>Table 4</b> <b>Culvert Sizing Design Sheet</b>													Project Information								Page 1 of 1																															
	Project Name		Borrello Subdivision SWM																																																		
Watercourse:	Roadside Ditch to Jock River		Road Classification:	Urban Local, Arterial		Design Flow:	25, 50 year		Existing Structure:	Various CSP Culverts		File No.	14057		Contract No.			Name	Company		Date																																
Design	CN		Check	BSA		Design	RCI		Check	RCI		20/10/2016																																									
STRUCTURE	DESIGN DATA						INLET CONTROL						OUTLET CONTROL						22	23	24	25	26																														
1	2	3	4	5	6	D (m)	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	Return Year	Length (m)	Slope (m/m)	Top of Road	U/S invert	D/S invert	t (m)	Q (m³/s)	A (m²)	V (m/s)	n	ke	HW/D	HW	H	dc	(dc+D)/2	H₀	LS	HW	Gov'g HW	Water Surface	Obvert	Cover	Free board		
Culvert #4	<b>25</b>	<b>16.70</b>	<b>0.0006</b>	<b>93.85</b>	<b>92.74</b>	<b>92.73</b>	<b>0.6</b>	<b>0.02</b>	<b>0.238</b>	<b>0.283</b>	<b>0.84</b>	<b>0.024</b>	<b>0.9</b>	<b>0.82</b>	<b>0.49</b>	<b>0.16</b>	<b>0.30</b>	<b>0.49</b>	<b>0.49</b>	<b>0.01</b>	<b>0.64</b>	<b>0.64</b>	<b>93.38</b>	<b>93.34</b>	<b>0.51</b>	<b>0.47</b>	600mm CSP	50	16.70	0.0006	93.85	92.74	92.73	0.6	0.02	0.337	0.283	1.19	0.024	0.9	0.93	0.56	0.24	0.34	0.49	0.49	0.01	0.72	0.72	93.46	93.34	0.51	0.39
Culvert #9	<b>25</b>	<b>20.00</b>	<b>0.0120</b>	<b>92.73</b>	<b>91.80</b>	<b>91.56</b>	<b>0.6</b>	<b>0.02</b>	<b>0.270</b>	<b>0.283</b>	<b>0.95</b>	<b>0.024</b>	<b>0.9</b>	<b>0.87</b>	<b>0.52</b>	<b>0.21</b>	<b>0.32</b>	<b>0.54</b>	<b>0.54</b>	<b>0.24</b>	<b>0.51</b>	<b>0.52</b>	<b>92.32</b>	<b>92.40</b>	<b>0.33</b>	<b>0.40</b>	600mm CSP	50	20.00	0.0120	92.73	91.80	91.56	0.6	0.02	0.381	0.283	1.35	0.024	0.9	0.99	0.59	0.32	0.38	0.54	0.54	0.24	0.62	0.62	92.42	92.40	0.33	0.30
Culvert #10	<b>25</b>	<b>34.80</b>	<b>0.0089</b>	<b>92.35</b>	<b>91.18</b>	<b>90.87</b>	<b>0.6</b>	<b>0.02</b>	<b>0.278</b>	<b>0.283</b>	<b>0.98</b>	<b>0.024</b>	<b>0.9</b>	<b>0.89</b>	<b>0.53</b>	<b>0.33</b>	<b>0.32</b>	<b>0.56</b>	<b>0.56</b>	<b>0.31</b>	<b>0.58</b>	<b>0.58</b>	<b>91.76</b>	<b>91.78</b>	<b>0.57</b>	<b>0.59</b>	600mm CSP	50	34.80	0.0089	92.35	91.18	90.87	0.6	0.02	0.393	0.283	1.39	0.024	0.9	1.02	0.61	0.48	0.38	0.56	0.56	0.31	0.73	0.73	91.91	91.78	0.57	0.44
Culvert #11	<b>25</b>	31.90	0.0094	89.34	86.75	86.45	1.2	0.02	0.426	1.131	0.38	0.024	0.9	0.41	0.49	0.00	0.33	0.64	0.64	0.30	0.34	0.49	87.24	87.95	1.39	2.10	1200mm CSP	<b>50</b>	<b>31.90</b>	<b>0.0094</b>	<b>89.34</b>	<b>86.75</b>	<b>86.45</b>	<b>1.2</b>	<b>0.02</b>	<b>0.602</b>	<b>1.131</b>	<b>0.53</b>	<b>0.024</b>	<b>0.9</b>	<b>0.47</b>	<b>0.56</b>	<b>0.01</b>	<b>0.38</b>	<b>0.64</b>	<b>0.64</b>	<b>0.30</b>	<b>0.35</b>	<b>0.56</b>	<b>87.31</b>	<b>87.95</b>	<b>1.39</b>	<b>2.03</b>
Culvert #12	25	26.50	0.0162	87.50	85.81	85.38	1.2	0.02	0.465	1.131	0.41	0.024	0.9	0.44	0.53	0.00	0.34	0.62	0.62	0.43	0.19	0.53	86.34	87.01	0.49	1.16	1200mm CSP	<b>50</b>	<b>26.50</b>	<b>0.0162</b>	<b>87.50</b>	<b>85.81</b>	<b>85.38</b>	<b>1.2</b>	<b>0.02</b>	<b>0.659</b>	<b>1.131</b>	<b>0.58</b>	<b>0.024</b>	<b>0.9</b>	<b>0.49</b>	<b>0.59</b>	<b>0.02</b>	<b>0.39</b>	<b>0.62</b>	<b>0.62</b>	<b>0.43</b>	<b>0.21</b>	<b>0.59</b>	<b>86.40</b>	<b>87.01</b>	<b>0.49</b>	<b>1.10</b>

\*Bold indicates required design return period

Return Frequency	A	B	C	Q = 2.78 CIA I = (A / T <sub>c</sub> + C) <sup>B</sup> Where Q = peak flow (L/s) A = area (ha) I = rainfall intensity (mm/hr) C = runoff coefficient T <sub>c</sub> = time of concentration (min)	<b>Table 5</b> <b>SWM DESIGN SHEET</b> <b>PROPOSED CONDITIONS</b> <b>(100 yr Pre-Development)</b> <small>IDF - Macdonald-Cartier Airport, 1967-1997 RCL_STM v1.02 (130204)</small>			Project Information						<b>Robinson</b> <b>Consultants</b>						
2 yr	732.951	0.810	6.199		Project Name	Borrello Subdivision SWM														
5 yr	998.071	0.814	6.053		File No.	14057		Contract No.												
10 yr	1174.184	0.816	6.014		Name			Company	Date											
25 yr	1402.884	0.819	6.018		Design	CN		RCI	20/10/2016											
50 yr	1569.580	0.820	6.014		Check	BSA		RCI	21/10/2016											
100 yr	1735.688	0.820	6.014		Page 1 of 1															
<b>LOCATION</b>					<b>CATCHMENT AREA</b>			<b>FLOW DATA</b>			<b>SEWER DATA</b>									
DRAINAGE AREA	LOCATION	EX. PIPE ID / PROPOSED	Start	End	10-Yr Design Storm			Time of Concentration T <sub>c</sub> (min)	Rainfall Intensity	Peak Flow	Total Peak Flow Q <sub>total</sub> (m <sup>3</sup> /s)	<b>PHYSICAL PROPERTIES</b>					<b>FLOW &amp; VELOCITY DATA</b>			
					Area A (ha)	C	Individual 2.78 AC					Material Type	Roughness Coefficient (n)	Slope (%)	Water Depth (m)	Flow Area (m <sup>2</sup> )	Length (m)	Capacity Q (m <sup>3</sup> /s)	Full Flow Velocity (m/s)	Time of Flow (min)
<b>Woodroffe Ave. (Stoneleigh St. to Prince of Wales Dr.)</b>																				
SD	Woodroffe	Ditch	SD Outlet	End A1	2.18	0.55	3.33	125.00 *(1)	31.86	0.11	0.11	Grass	0.035	0.0667	0.0383	0.10	105.00		1.26	1.39
A1	Woodroffe	Ditch	SD Outlet	End A1	0.47	0.58	0.75	126.39	31.59	0.13	0.13	Grass	0.035	0.0320	0.0375	0.10	105.00		1.36	1.29
A2	Woodroffe	Ditch	End A1	End A2	0.18	0.49	0.24	127.67	31.34	0.14	0.14	Grass	0.035	0.0385	0.0353	0.09	25.60		1.67	0.26
A3	Woodroffe	Ditch	End A2	End A3	0.53	0.43	0.63	127.93	31.29	0.16	0.16	Grass	0.035	0.0390	0.0351	0.17	79.40		1.28	1.03
A4	Woodroffe	Ditch	End A3	End A4	1.89	0.40	2.10	128.96	31.09	0.22	0.22	Grass	0.035	0.0168	0.3487	0.37	136.25		0.64	3.54
A5	Woodroffe	Ditch	End A4	End A5	0.64	0.41	0.73	132.50	30.44	0.24	0.24	Grass	0.035	0.0015	0.3282	0.33	53.75		0.74	1.21
A6	Woodroffe	Ditch	End A5	End A6	0.21	0.41	0.24	133.71	30.22	0.24	0.24	Grass	0.035	0.0024	0.3338	0.34	26.25		0.73	0.60
A7	Woodroffe	Ditch	End A6	End A7	0.22	0.35	0.21	134.30	30.12	0.25	0.25	Grass	0.035	0.0022	0.3434	0.36	37.50		0.74	0.85
A8	Woodroffe	Ditch	End A7	End A8	0.56	0.35	0.54	135.15	29.97	0.26	0.26	Grass	0.035	0.0021	0.2863	0.25	108.10		1.07	1.69
A9	Woodroffe	Ditch	End A8	End A9	0.18	0.35	0.18	136.84	29.68	0.27	0.27	Grass	0.035	0.0070	0.2730	0.23	35.60		1.22	0.48
A10	Woodroffe	Ditch	End A9	End A10	0.36	0.43	0.43	137.33	29.60	0.28	0.28	Grass	0.035	0.0105	0.3296	0.33	68.10		1.47	0.77
<b>Prince of Wales Dr. (Woodroffe Ave. to Lodge Rd.)</b>																				
A11	Prince of Wales	Ditch	End A10	End A11	8.13	0.31	7.06	138.10	29.47	0.48	0.48	Grass	0.035	0.0092	0.3296	0.33	340.00		1.47	3.85
A12	Prince of Wales	Ditch	End A11	End A12	1.23	0.69	2.35	141.95	28.84	0.54	0.54	Grass	0.035	0.0128	0.3243	0.32	57.50		1.70	0.56

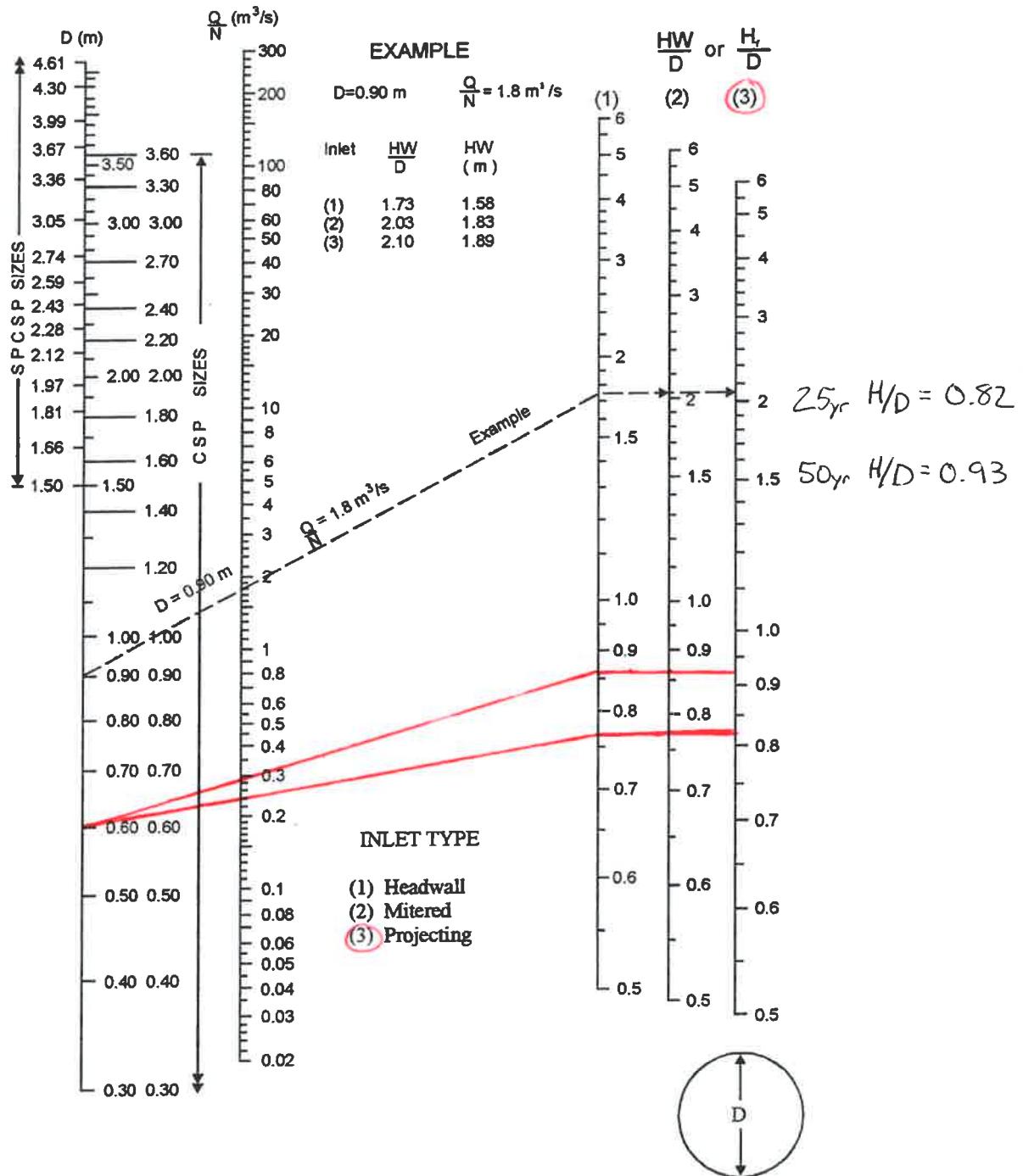
Note 1: Time of Concentration for Subdivision (SD) calculated from Time of Peak for peak outlet flows from DDSWMM. Equation used is TP/0.6 (From SWMHYMO Manual)

$$T_c = TP/0.6 = 75/0.6 = 125$$

# Culvert #4 600<sub>mm</sub> CSP

MTO Drainage Management Manual

## Design Chart 2.32: Inlet Control: Circular CSP and SPCSP Culverts

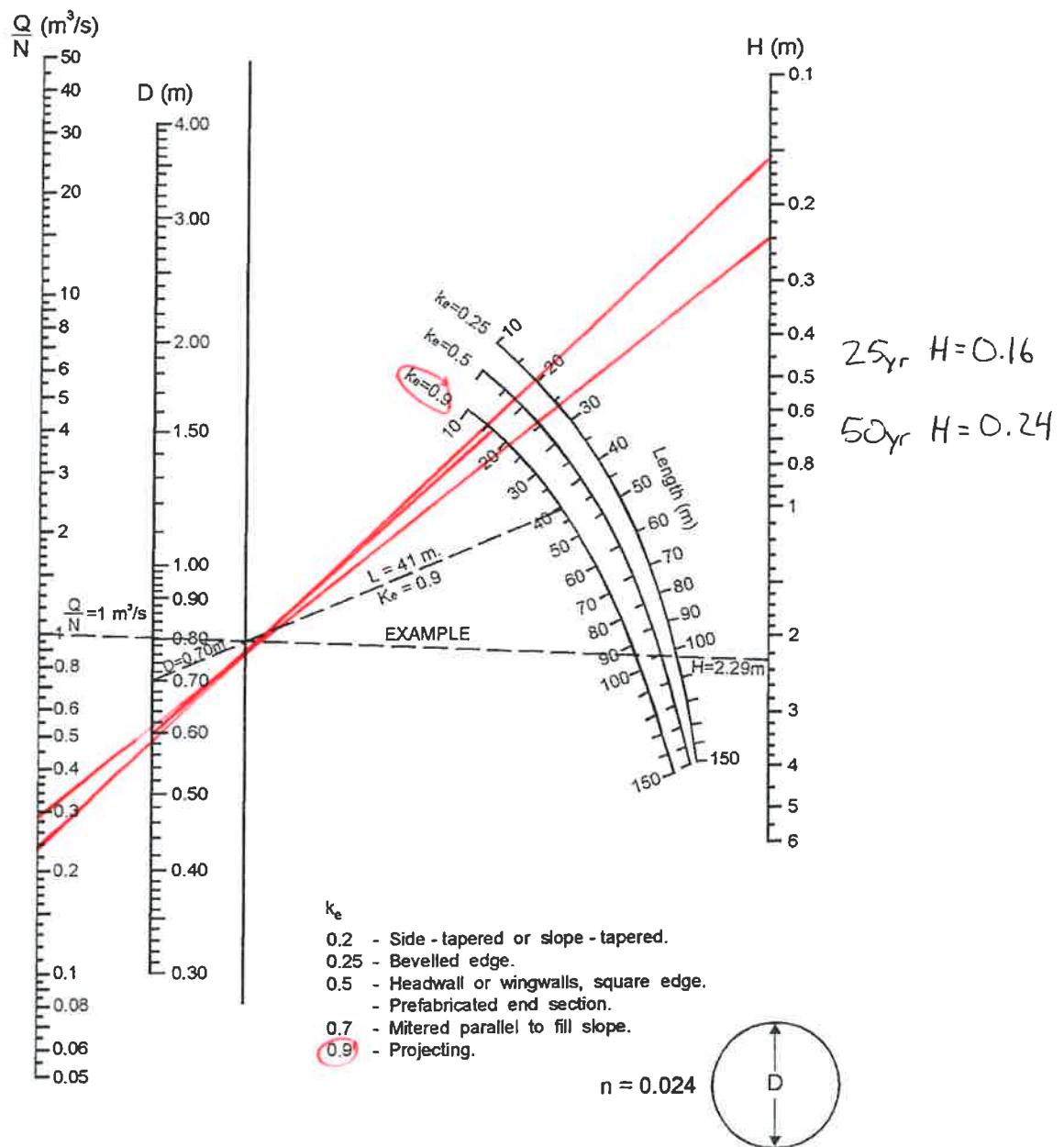


Source: Herr (1977)

# Culvert #4 600<sub>mm</sub> CSP

## Design Charts

**Design Chart 2.35: Outlet Control: CSP Culvert - Flowing Full**

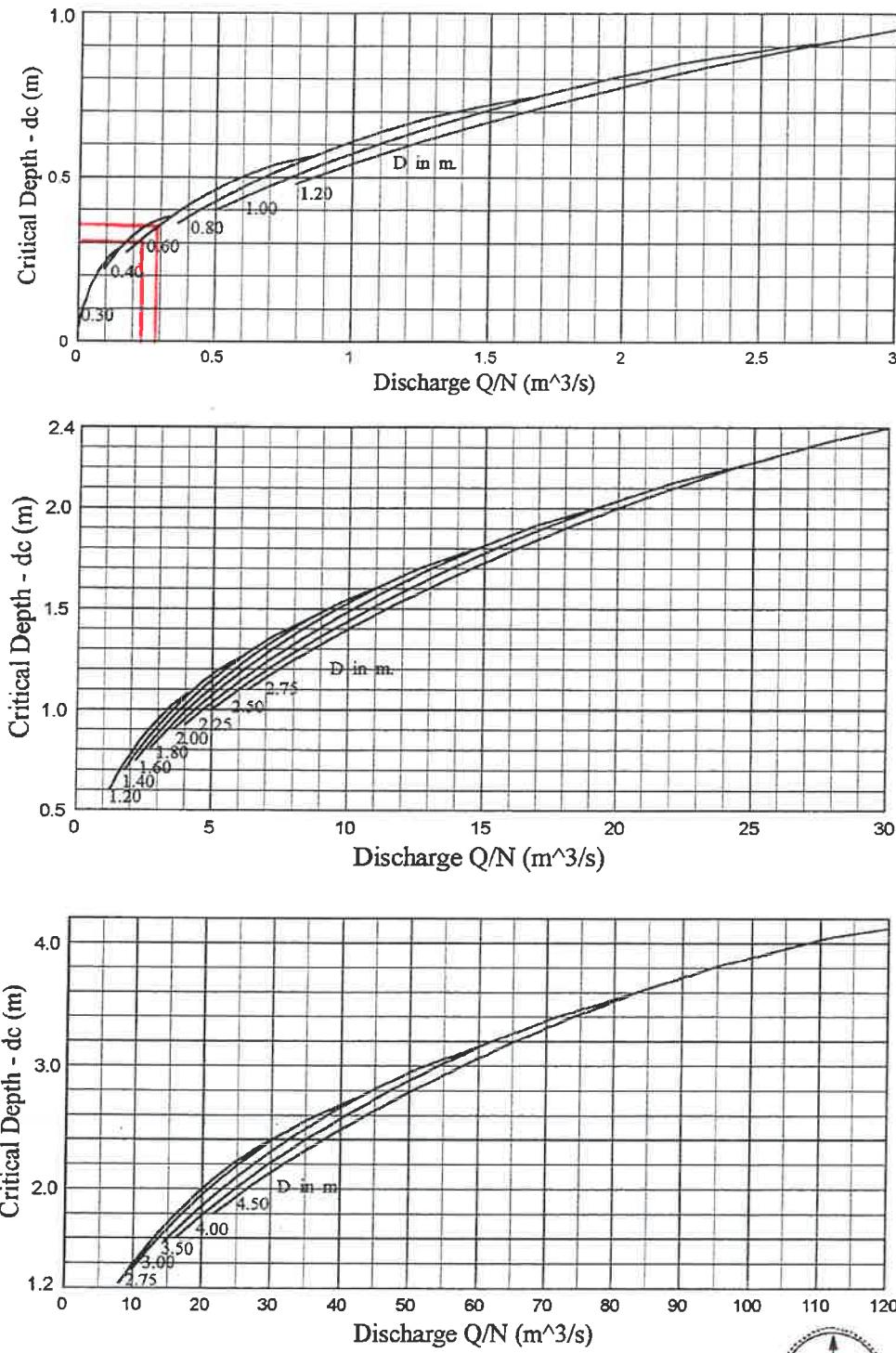


Source: Herr (1977)

# Culvert #4 600<sub>mm</sub> CSP

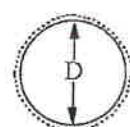
Design Charts

Design Chart 2.37: Critical Depth Chart for Circular Pipes



Source: Herr (1977)

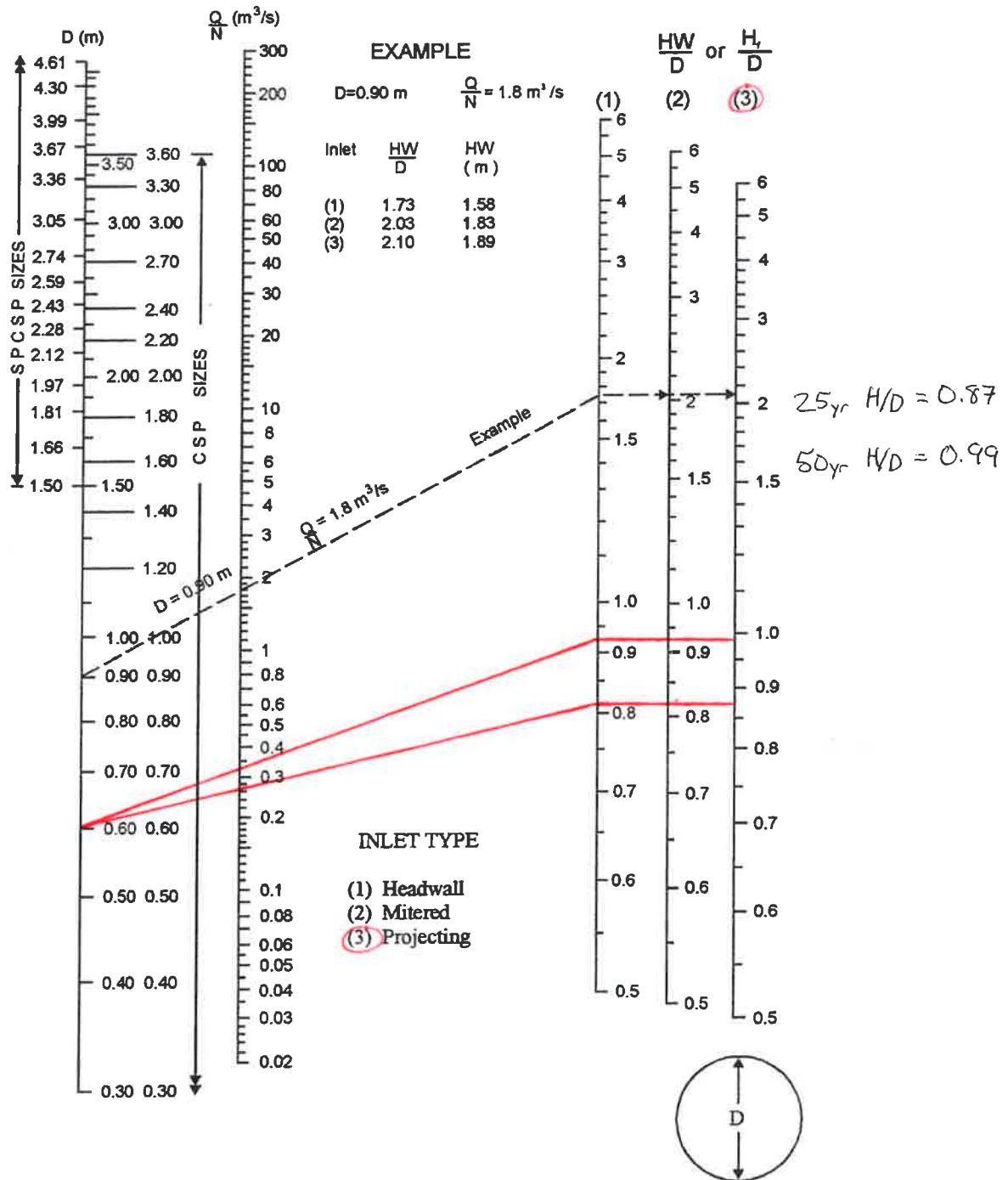
( $dc \geq D$ )



# Culvert #9 600m CSP

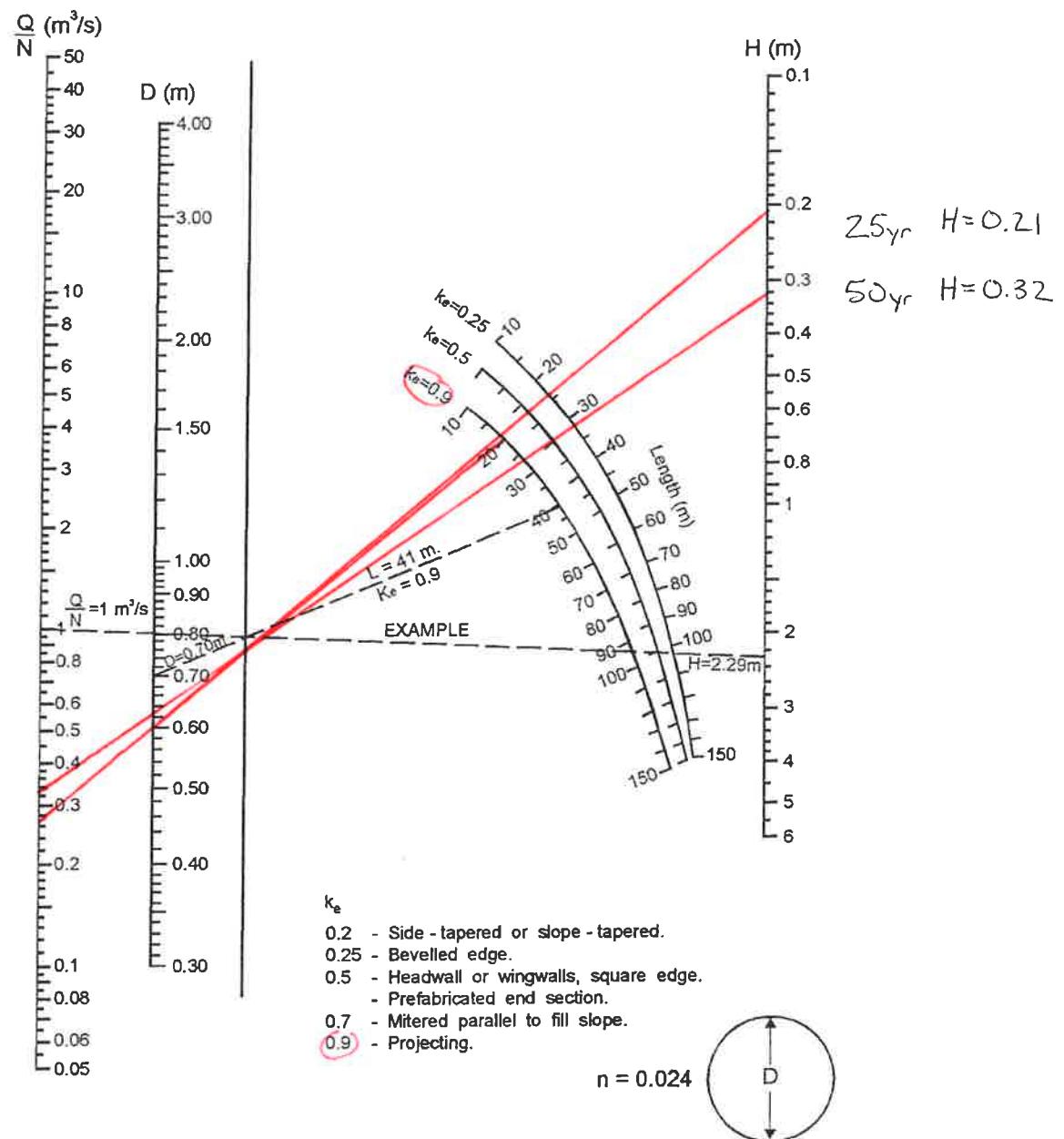
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## Design Chart 2.32: Inlet Control: Circular CSP and SPCSP Culverts

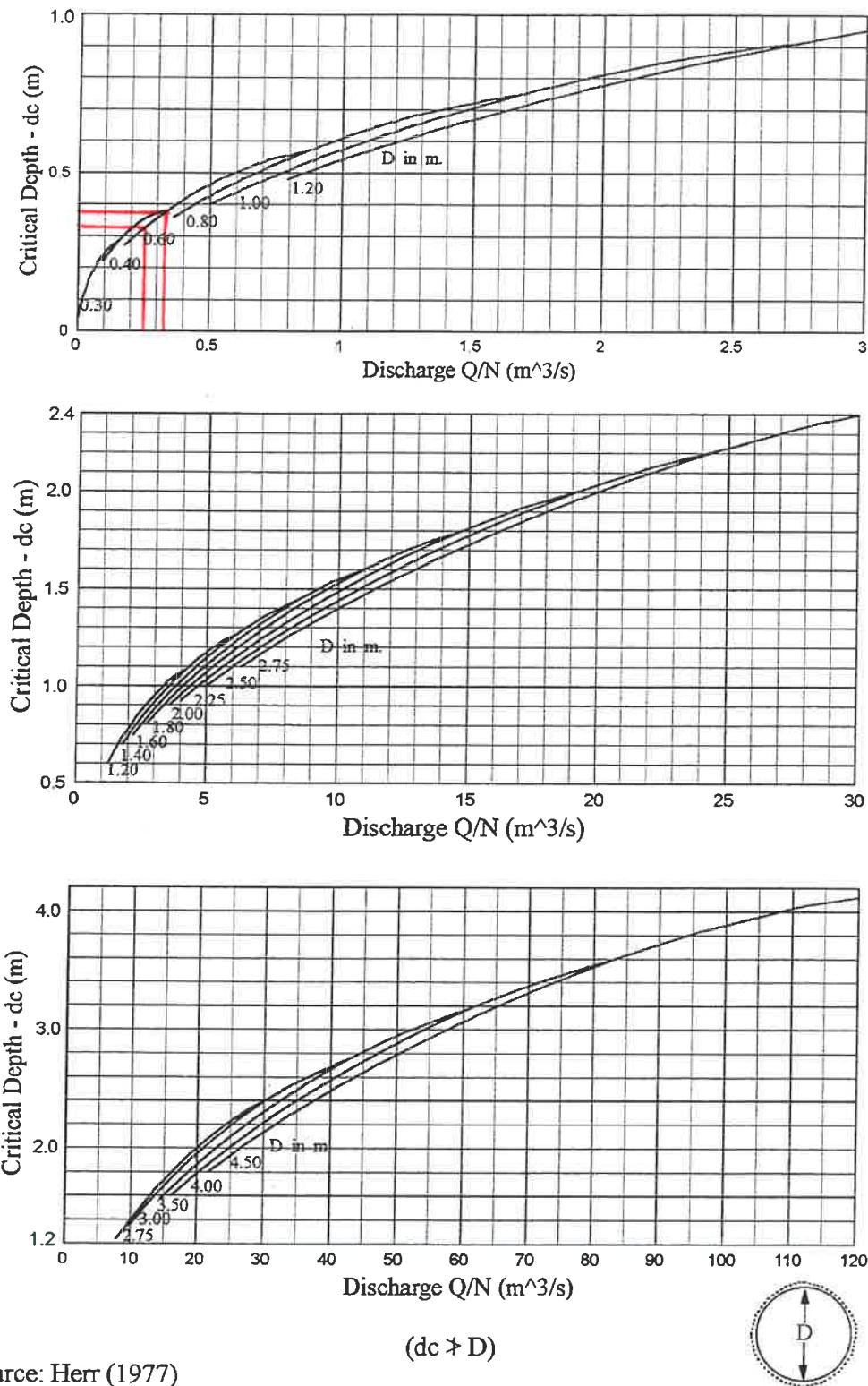


Source: Herr (1977)

**Design Chart 2.35: Outlet Control: CSP Culvert - Flowing Full**



Source: Herr (1977)

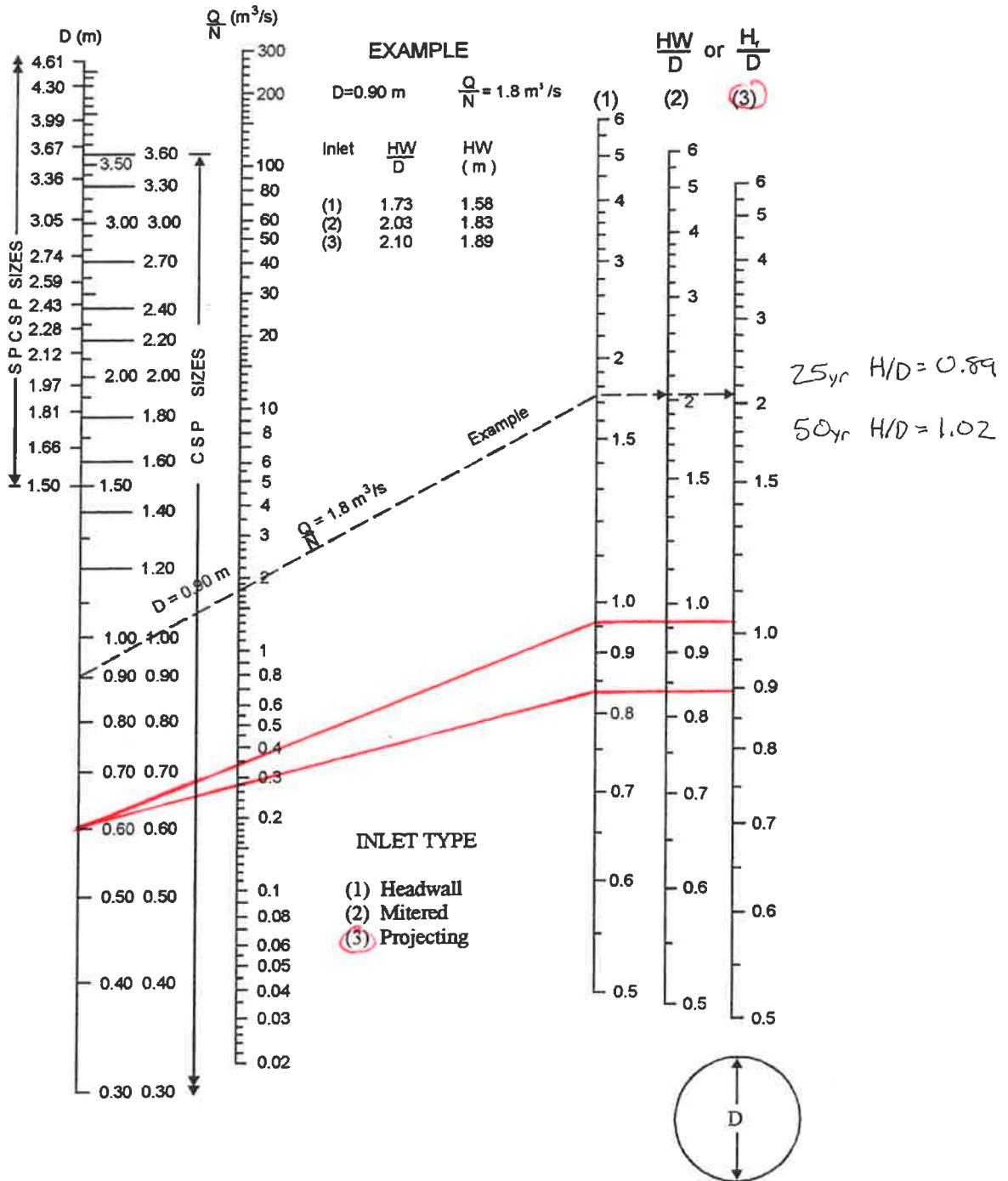
**Design Chart 2.37: Critical Depth Chart for Circular Pipes**


Source: Herr (1977)

# Culvert #10 600mm CSP

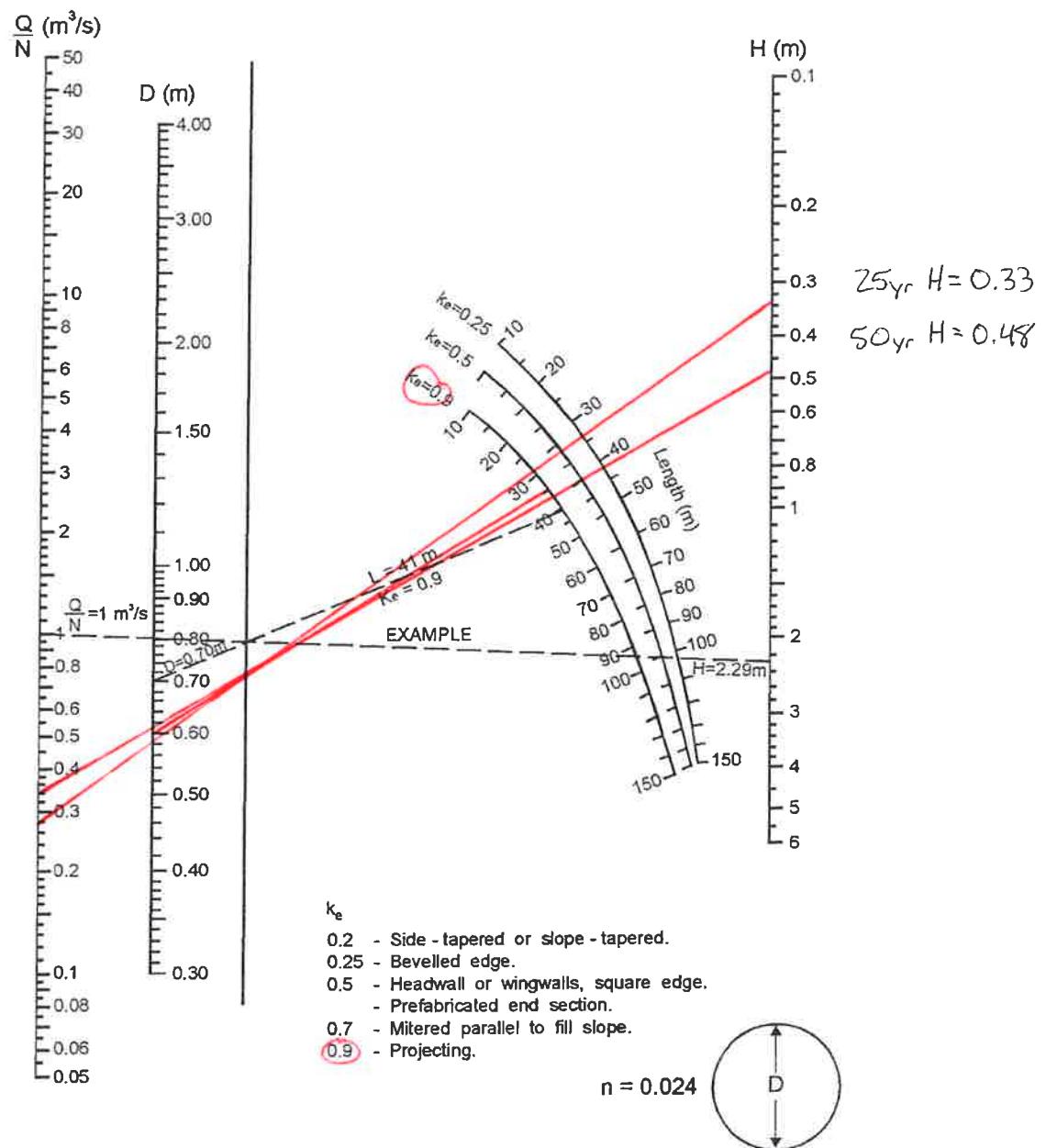
MTO Drainage Management Manual

## Design Chart 2.32: Inlet Control: Circular CSP and SPCSP Culverts



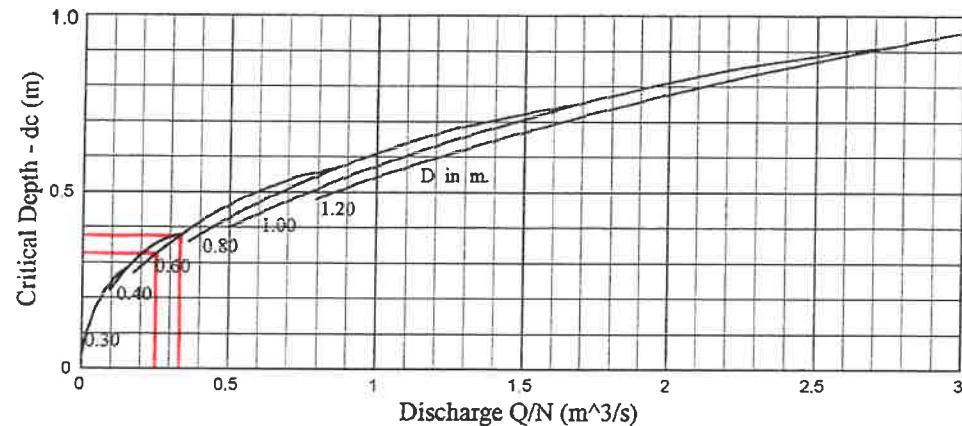
Source: Herr (1977)

**Design Chart 2.35: Outlet Control: CSP Culvert - Flowing Full**



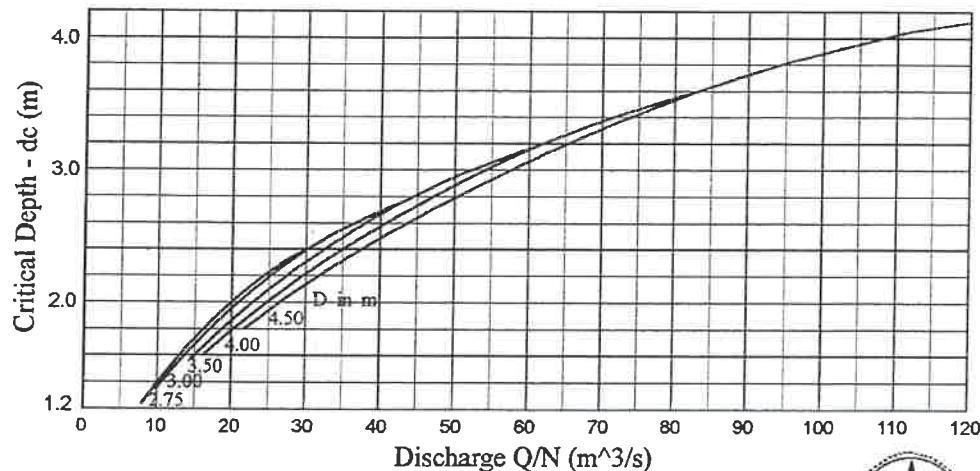
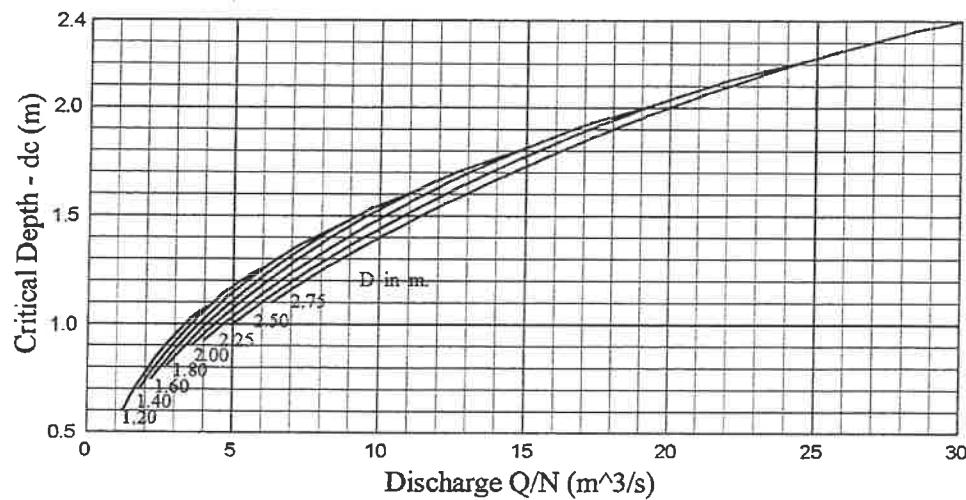
Source: Herr (1977)

**Design Chart 2.37: Critical Depth Chart for Circular Pipes**



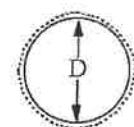
25yr  $d_c = 0.32$

50yr  $d_c = 0.38$



$(d_c \geq D)$

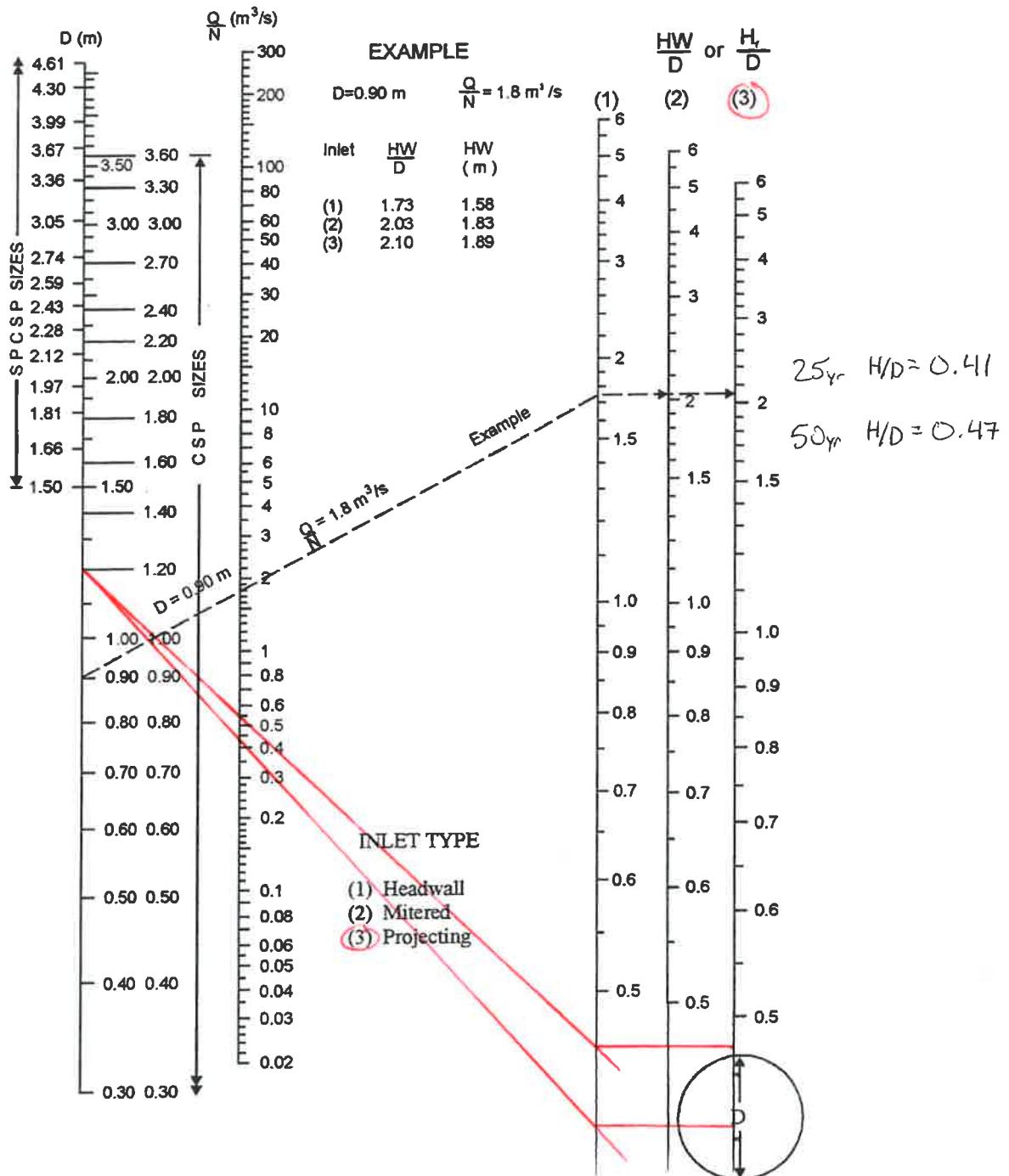
Source: Hett (1977)



# Culvert #11 1200mm CSP

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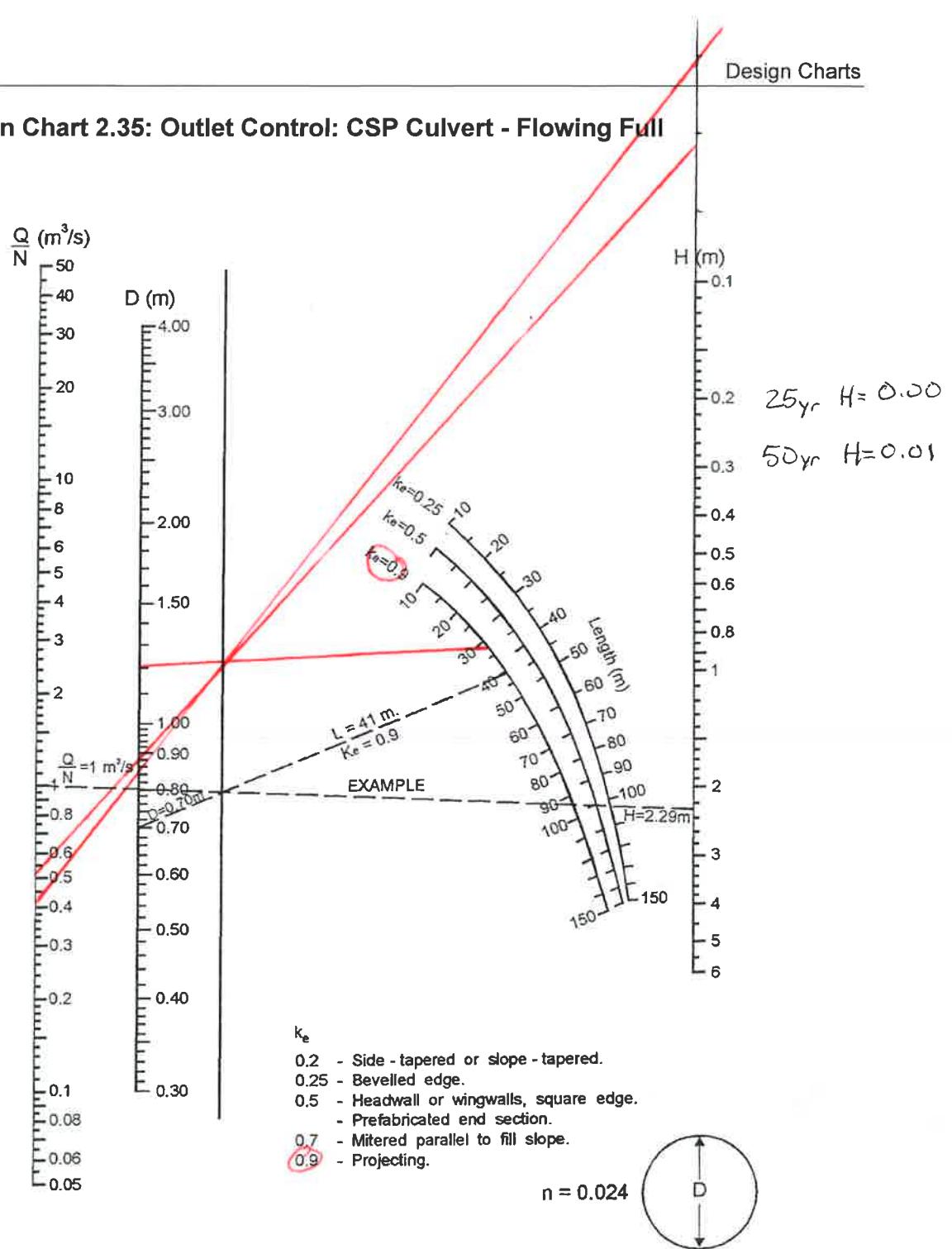
### Design Chart 2.32: Inlet Control: Circular CSP and SPCSP Culverts



Source: Herr (1977)

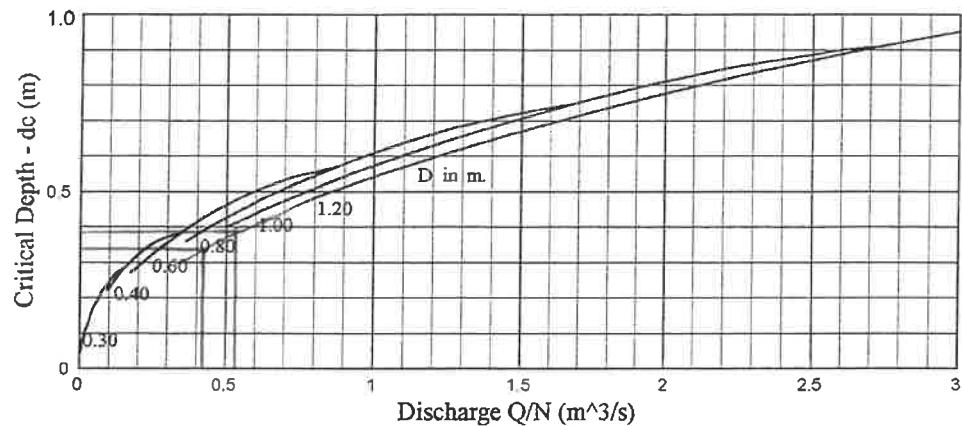
Design Charts

Design Chart 2.35: Outlet Control: CSP Culvert - Flowing Full



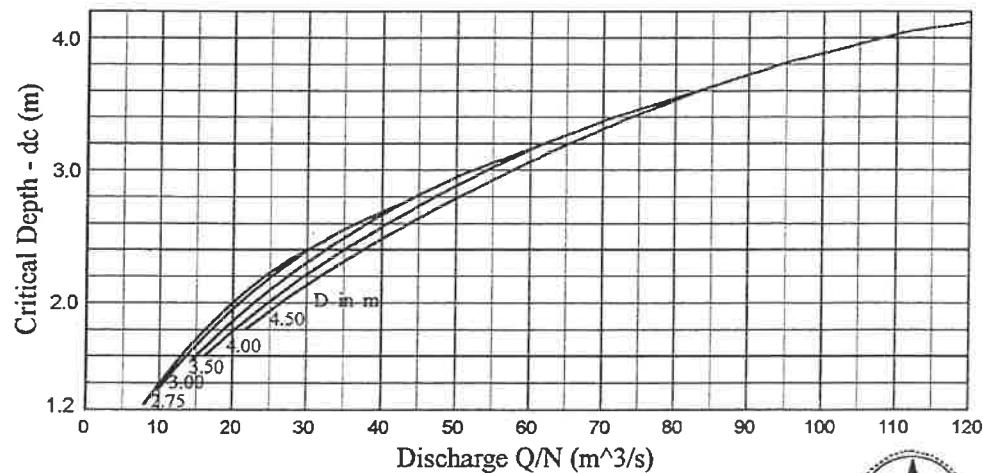
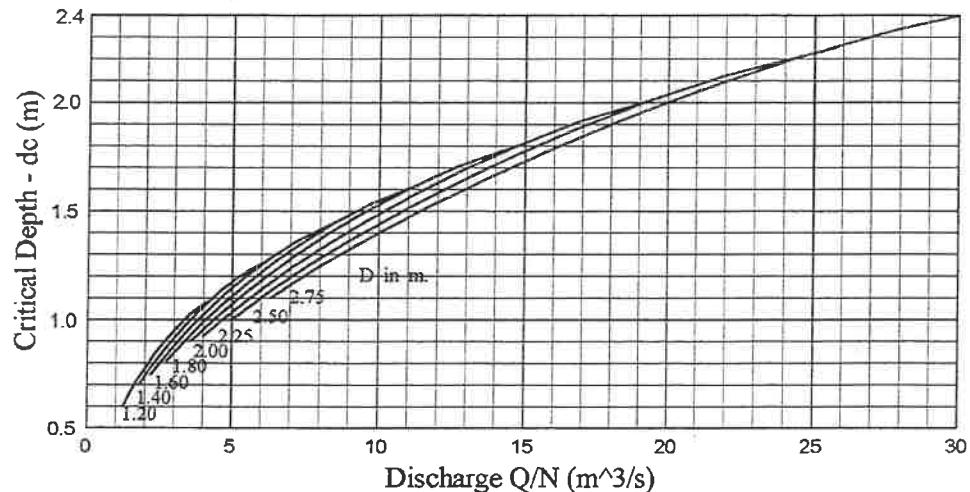
Source: Herr (1977)

**Design Chart 2.37: Critical Depth Chart for Circular Pipes**



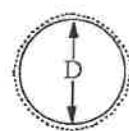
25yr dc = 0.33

50yr dc = 0.38

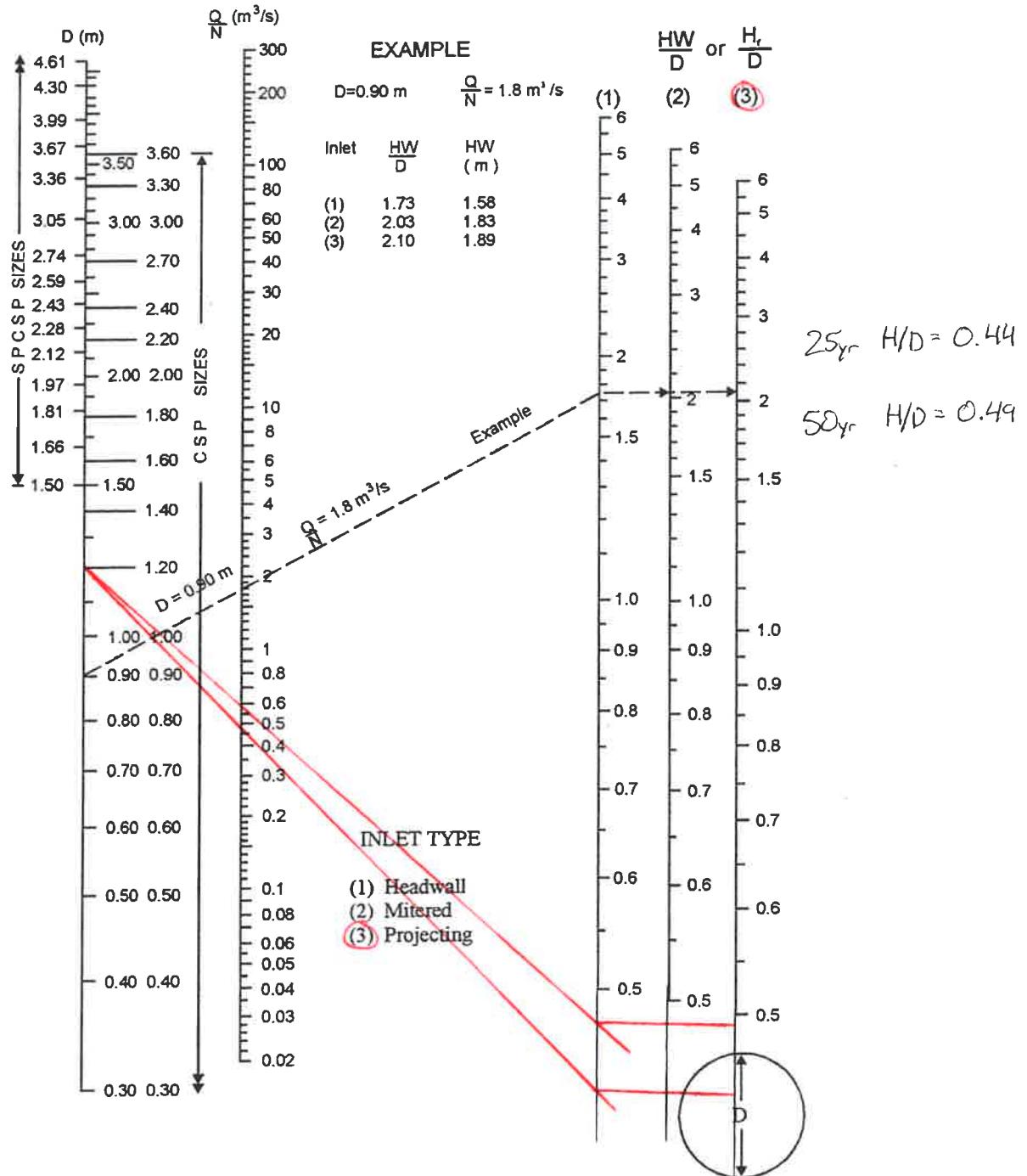


(dc  $\geq$  D)

Source: Herr (1977)



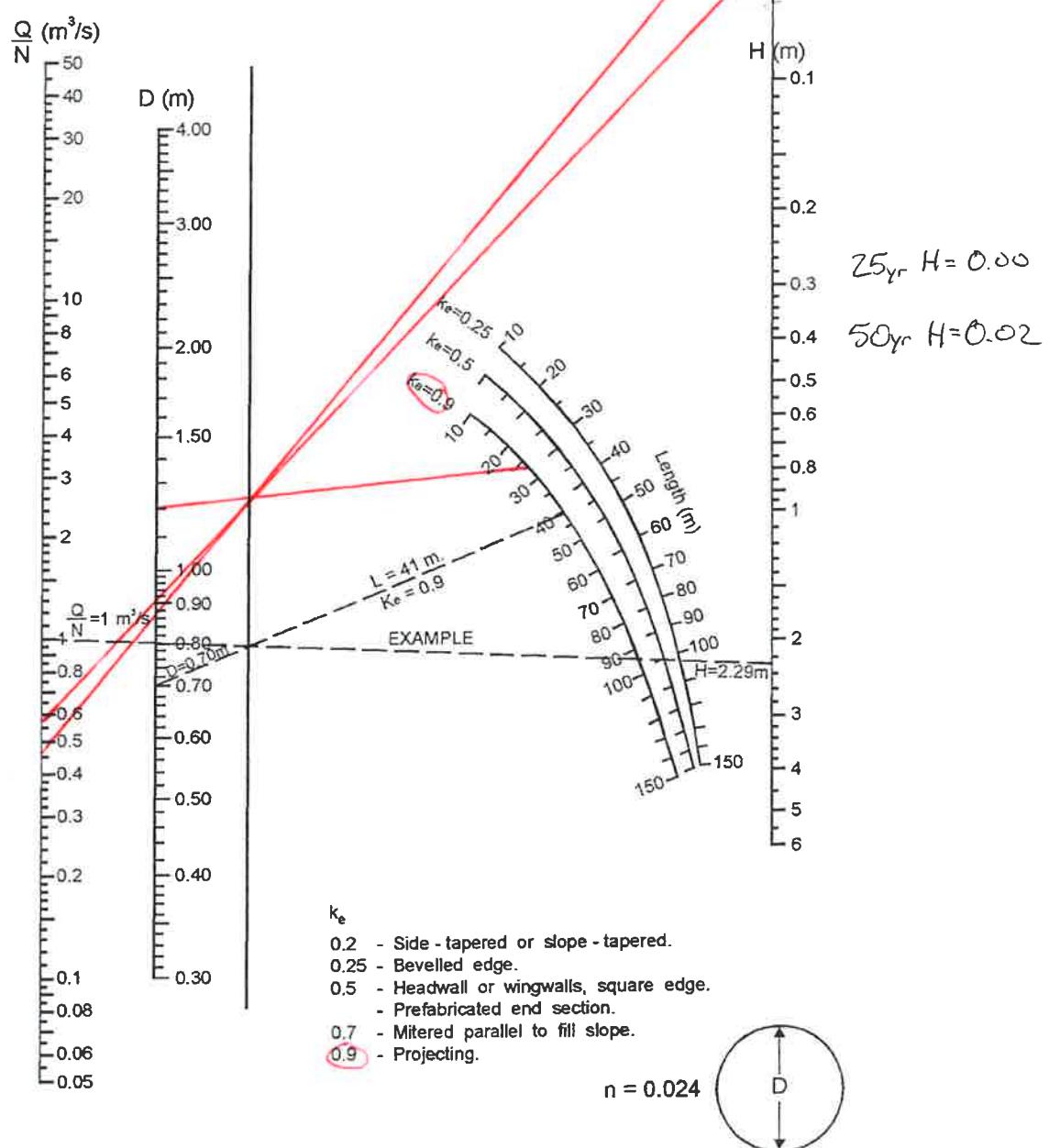
**Design Chart 2.32: Inlet Control: Circular CSP and SPCSP Culverts**



# Culvert #12 1200<sub>mm</sub> CSP

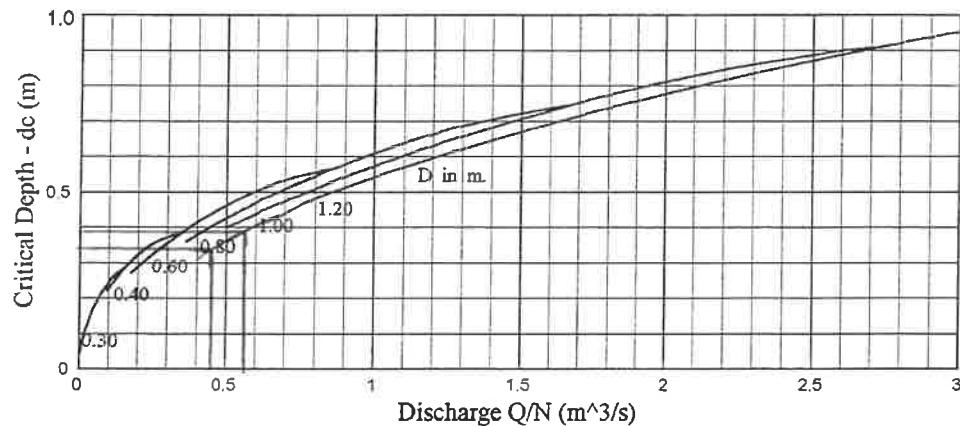
Design Charts

Design Chart 2.35: Outlet Control: CSP Culvert - Flowing Full



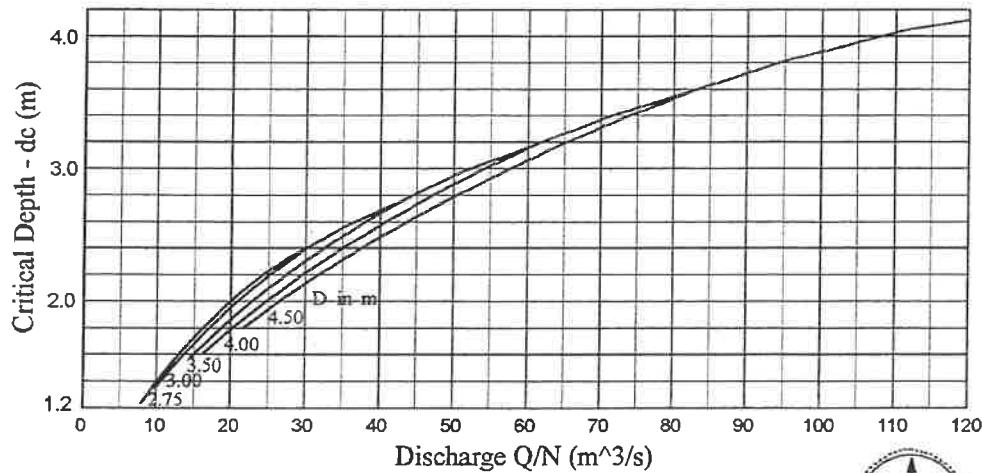
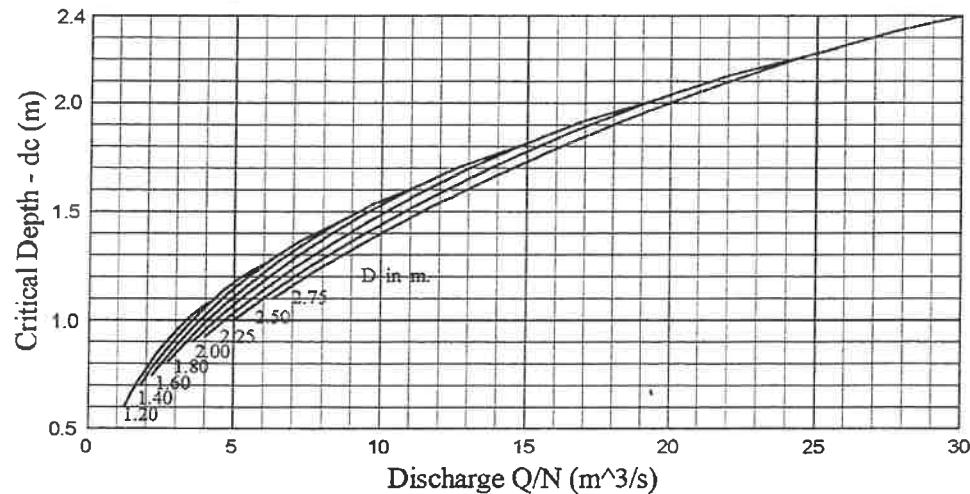
Source: Herr (1977)

**Design Chart 2.37: Critical Depth Chart for Circular Pipes**



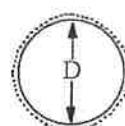
25<sub>yr</sub>  $d_c = 0.34$

50<sub>yr</sub>  $d_c = 0.39$



$(d_c \geq D)$

Source: Herr (1977)



**Table B.3****Rational Method Calculation Sheet****100 Year Storm Event (Ditch Capacity Check)**

Ditch Section ID	Area (ha)	Runoff Coefficient, C	Time Conc. 25yr	Time Conc. 50yr	Rainfall Intensity (mm/hr)	Peak Design Flow (m <sup>3</sup> /s)	Cumulative Peak Design Flow (m <sup>3</sup> /s)
		C <sub>100yr</sub>	(min.)	(min.)	100 year	100 year	100 year
Section A-A	0.53	0.43	17.0	15.8	138.45	0.087	0.558
Section B-B	1.89	0.40	18.6	17.4	130.80	0.275	0.833
Section C-C	0.21	0.41	18.7	17.5	130.45	0.031	0.940

$Q = 0.00278 A \times I \times C$  (m<sup>3</sup>/s), Where:

$I = A/(T_c + C)^B$ , where:

100y yr	
A =	1735.688
C =	6.014
B =	0.820

# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Thursday, Nov 3 2016

## Ditch Section A-A (Pre-Development Ditch Capacity)

### Trapezoidal

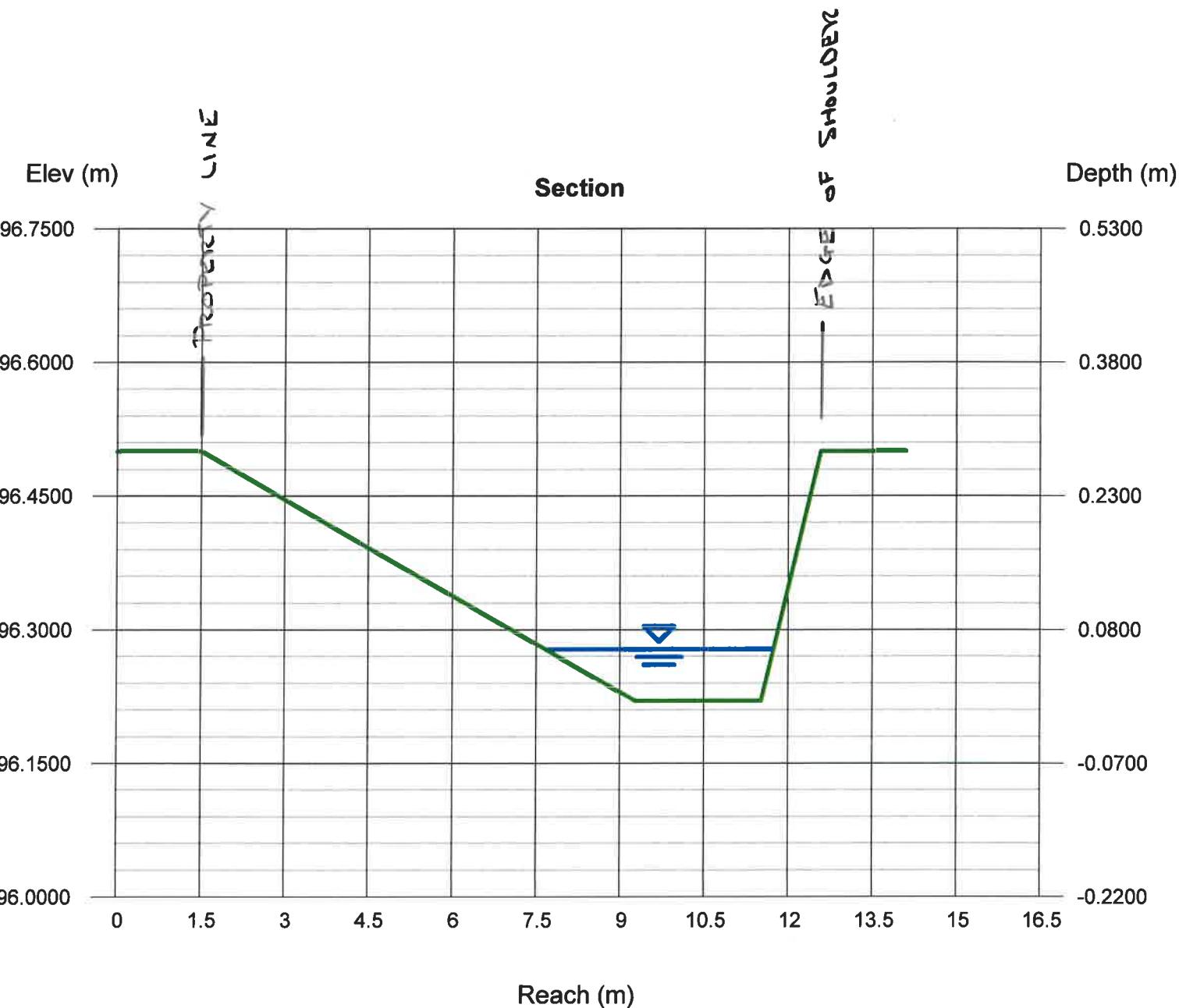
Bottom Width (m) = 2.2400  
Side Slopes (z:1) = 27.7700, 3.8000  
Total Depth (m) = 0.2800  
Invert Elev (m) = 96.2200  
Slope (%) = 4.4000  
N-Value = 0.030

### Highlighted

Depth (m) = 0.0579  
Q (cms) = 0.160  
Area (sqm) = 0.1827  
Velocity (m/s) = 0.8759  
Wetted Perim (m) = 4.0768  
Crit Depth, Yc (m) = 0.0701  
Top Width (m) = 4.0683  
EGL (m) = 0.0970

### Calculations

Compute by: Known Q  
Known Q (cms) = 0.1600



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Thursday, Nov 3 2016

## Ditch Section B-B (Pre-Development Ditch Capacity)

### Triangular

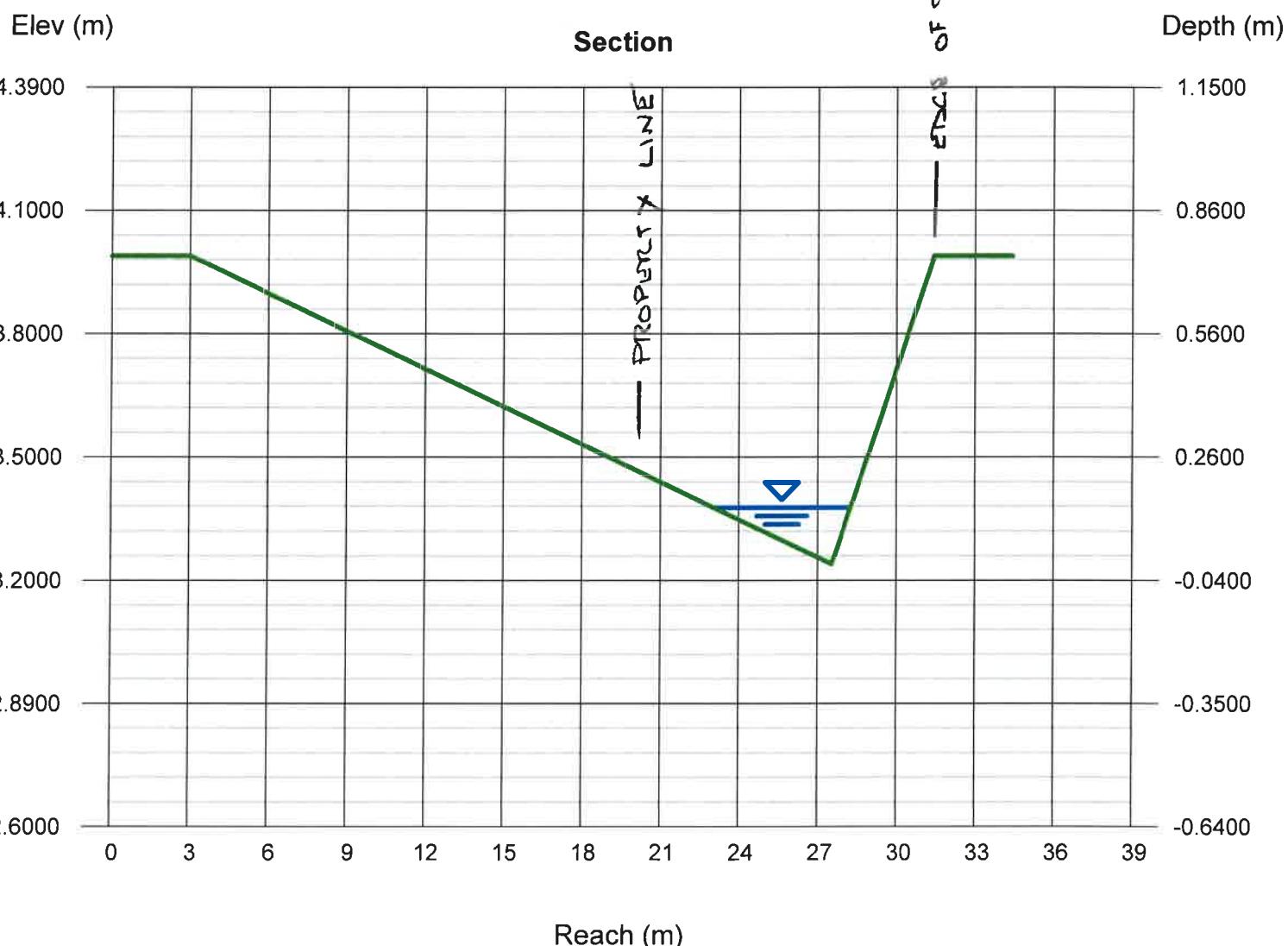
Side Slopes (z:1)	= 32.7000, 5.2000
Total Depth (m)	= 0.7500
Invert Elev (m)	= 93.2400
Slope (%)	= 1.3600
N-Value	= 0.030

### Calculations

Compute by:	Known Q
Known Q (cms)	= 0.2200

### Highlighted

Depth (m)	= 0.1372
Q (cms)	= 0.220
Area (sqm)	= 0.3565
Velocity (m/s)	= 0.6171
Wetted Perim (m)	= 5.2135
Crit Depth, Yc (m)	= 0.1250
Top Width (m)	= 5.1984
EGL (m)	= 0.1566



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Thursday, Nov 3 2016

## Ditch Section C-C (Pre-Development Ditch Capacity)

### Triangular

Side Slopes (z:1) = 3.0000, 3.0000  
Total Depth (m) = 1.5000  
  
Invert Elev (m) = 93.8200  
Slope (%) = 0.2000  
N-Value = 0.030

### Highlighted

Depth (m) = 0.4054  
Q (cms) = 0.240  
Area (sqm) = 0.4930  
Velocity (m/s) = 0.4868  
Wetted Perim (m) = 2.5639  
Crit Depth, Yc (m) = 0.2652  
Top Width (m) = 2.4323  
EGL (m) = 0.4175

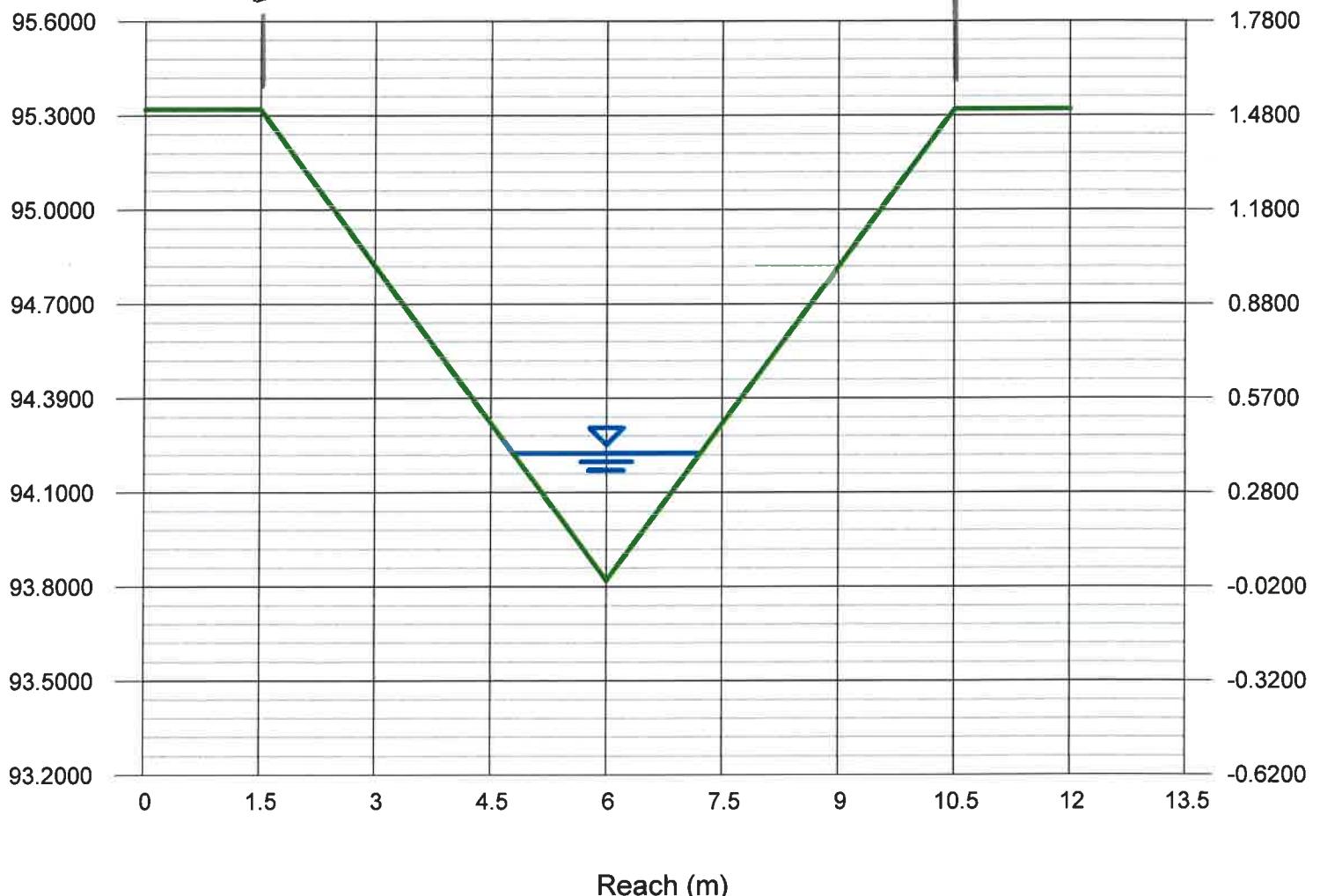
### Calculations

Compute by: Known Q  
Known Q (cms) = 0.2400

PROBLEMS  
Elev (m)

### Section

Depth (m)



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Thursday, Nov 3 2016

## Ditch Section A-A (Post-Development Ditch Capacity)

### Trapezoidal

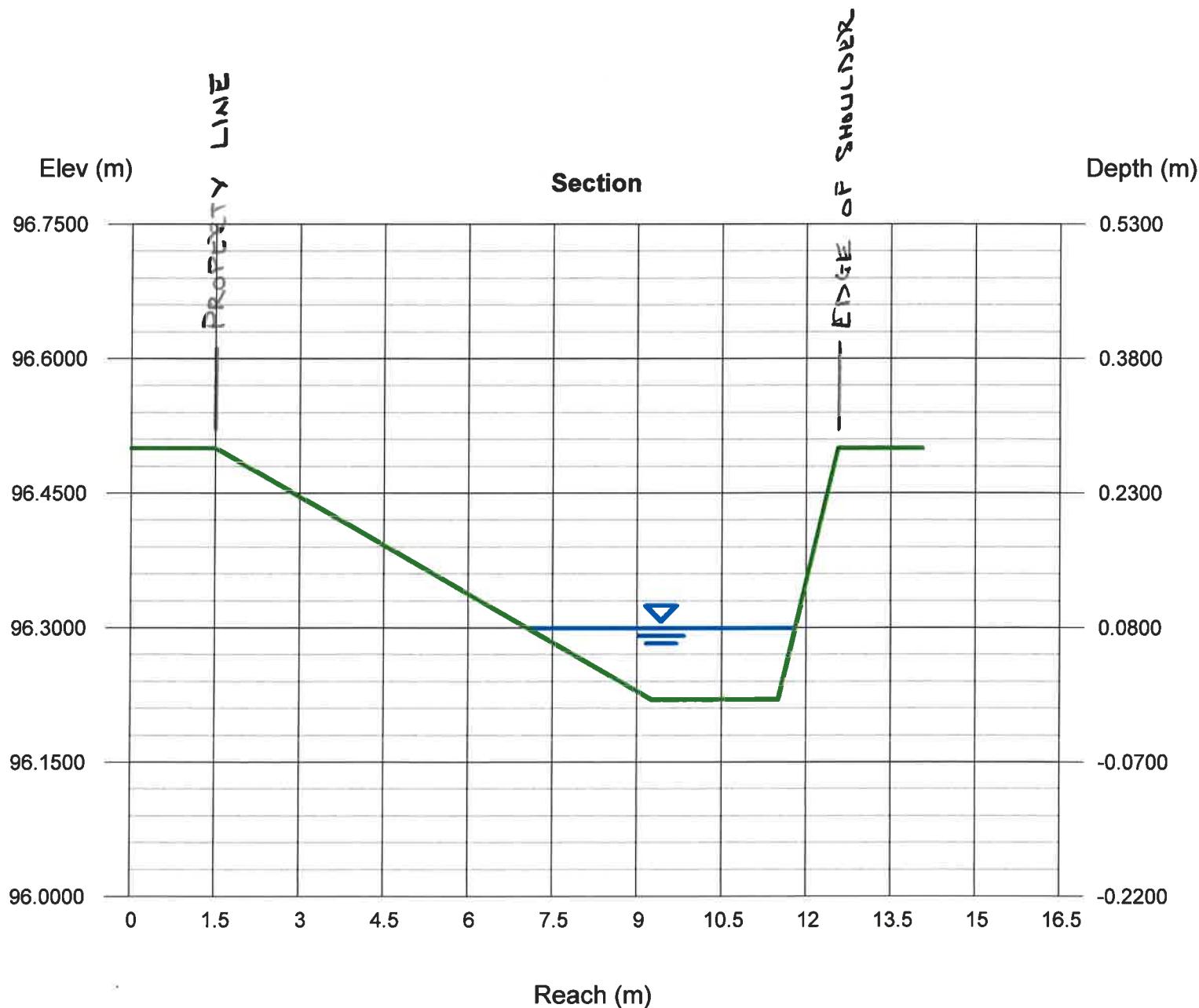
Bottom Width (m)	= 2.2400
Side Slopes (z:1)	= 27.7000, 3.8000
Total Depth (m)	= 0.2800
Invert Elev (m)	= 96.2200
Slope (%)	= 4.4000
N-Value	= 0.030

### Highlighted

Depth (m)	= 0.0792
Q (cms)	= 0.270
Area (sqm)	= 0.2764
Velocity (m/s)	= 0.9767
Wetted Perim (m)	= 4.7480
Crit Depth, Yc (m)	= 0.0914
Top Width (m)	= 4.7363
EGL (m)	= 0.1279

### Calculations

Compute by:	Known Q
Known Q (cms)	= 0.2700



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Thursday, Nov 3 2016

## Ditch Section B-B (Post Development Ditch Capacity)

### Triangular

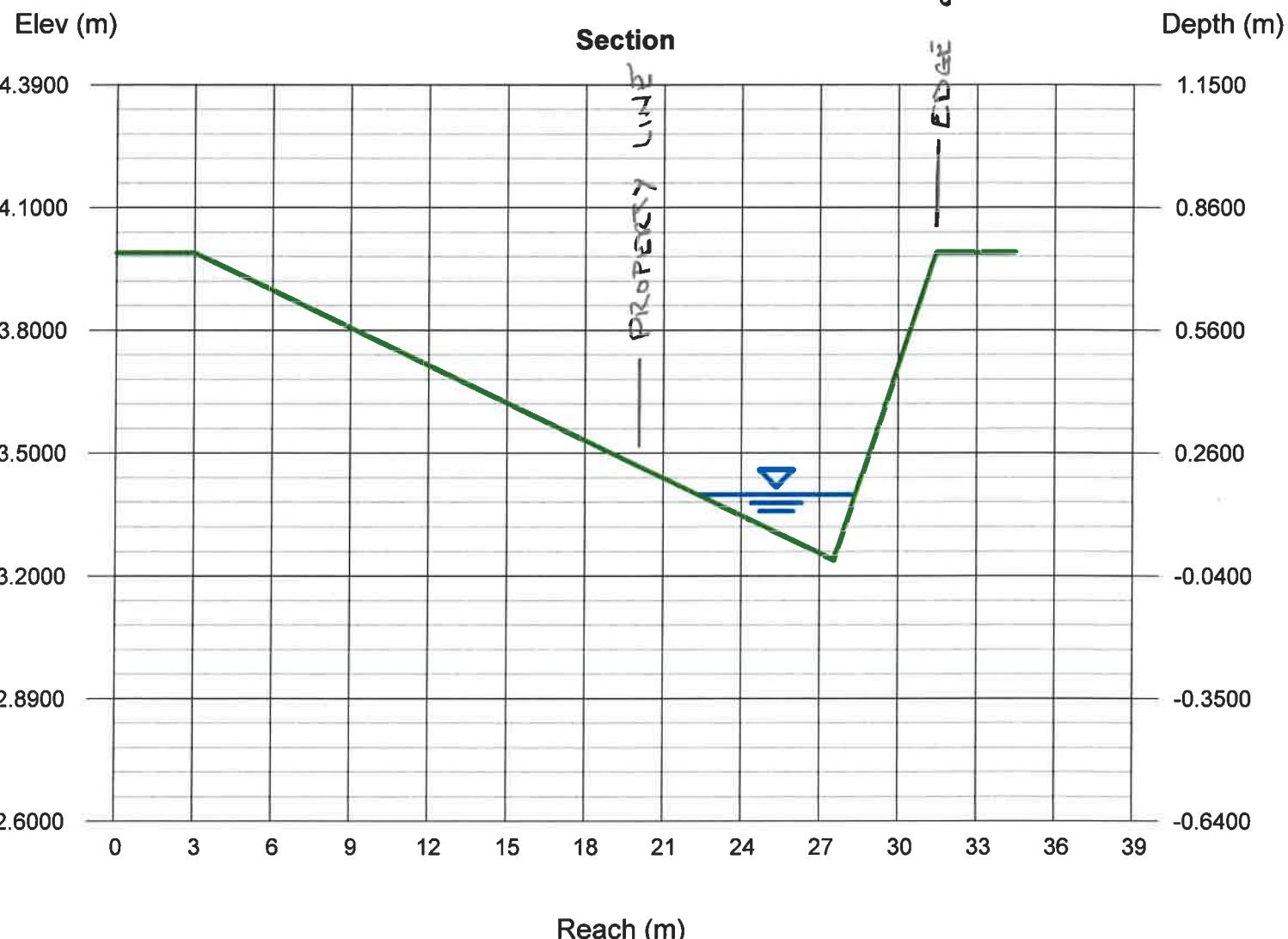
Side Slopes (z:1)	= 32.7000, 5.2000
Total Depth (m)	= 0.7500
Invert Elev (m)	= 93.2400
Slope (%)	= 1.3600
N-Value	= 0.030

### Calculations

Compute by:	Known Q
Known Q (cms)	= 0.3400

### Highlighted

Depth (m)	= 0.1585
Q (cms)	= 0.3400
Area (sqm)	= 0.4760
Velocity (m/s)	= 0.7142
Wetted Perim (m)	= 6.0245
Crit Depth, Yc (m)	= 0.1463
Top Width (m)	= 6.0070
EGL (m)	= 0.1845



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Thursday, Nov 3 2016

## Ditch Section C-C (Post-Development Ditch Capacity)

### Triangular

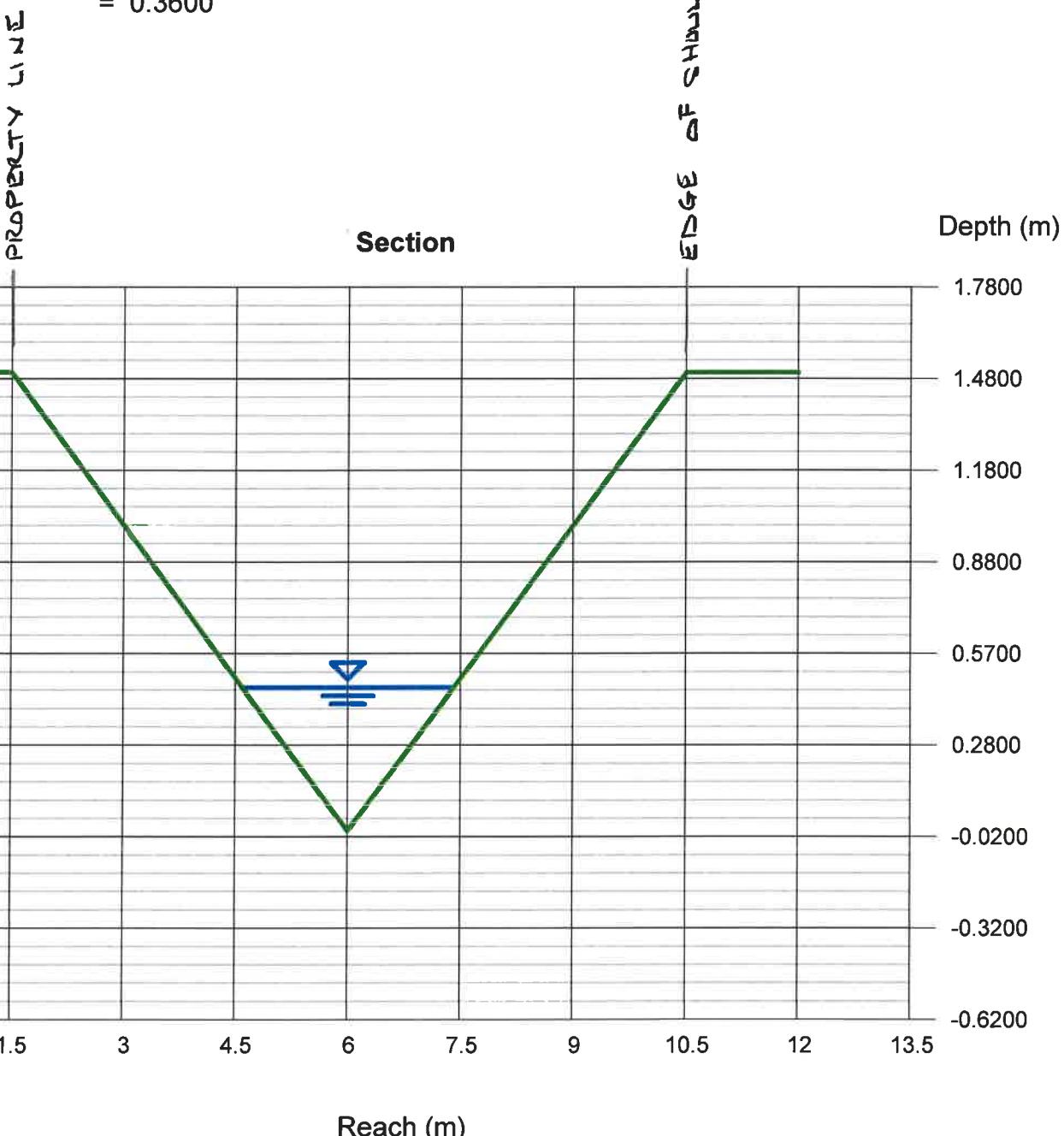
Side Slopes (z:1) = 3.0000, 3.0000  
Total Depth (m) = 1.5000  
  
Invert Elev (m) = 93.8200  
Slope (%) = 0.2000  
N-Value = 0.030

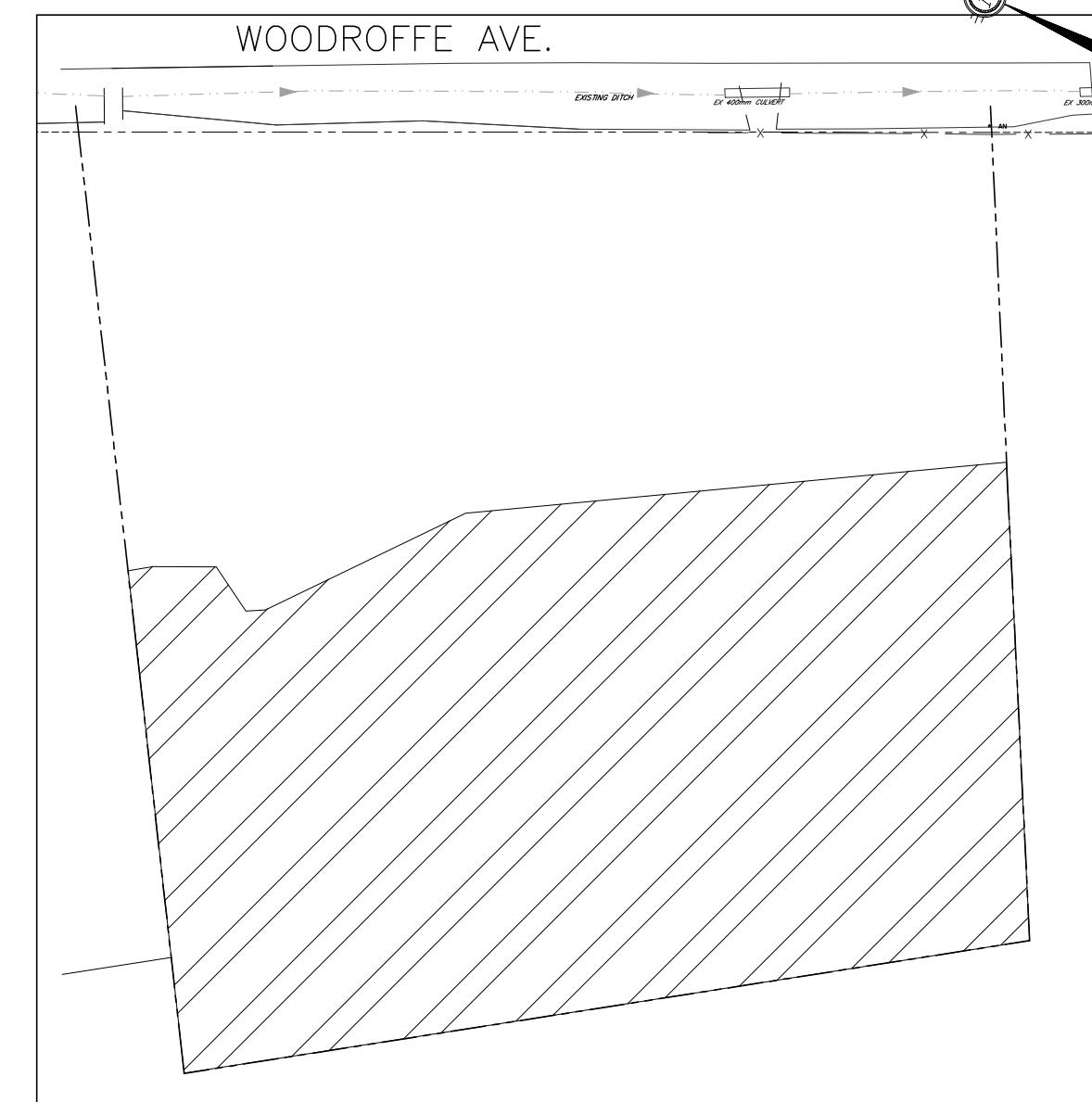
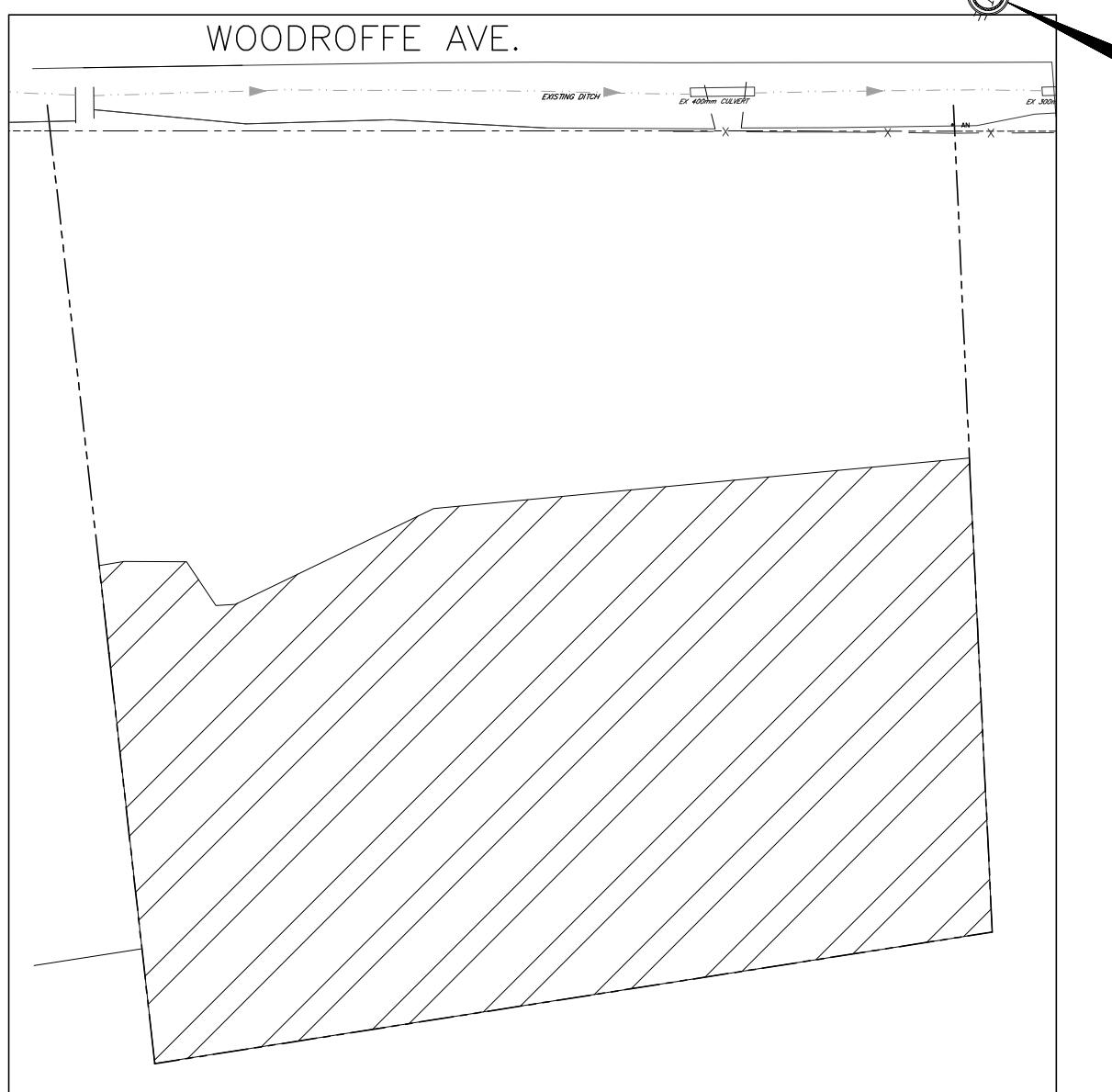
### Highlighted

Depth (m) = 0.4694  
Q (cms) = 0.3600  
Area (sqm) = 0.6610  
Velocity (m/s) = 0.5446  
Wetted Perim (m) = 2.9687  
Crit Depth, Yc (m) = 0.3139  
Top Width (m) = 2.8164  
EGL (m) = 0.4845

### Calculations

Compute by: Known Q  
Known Q (cms) = 0.3600

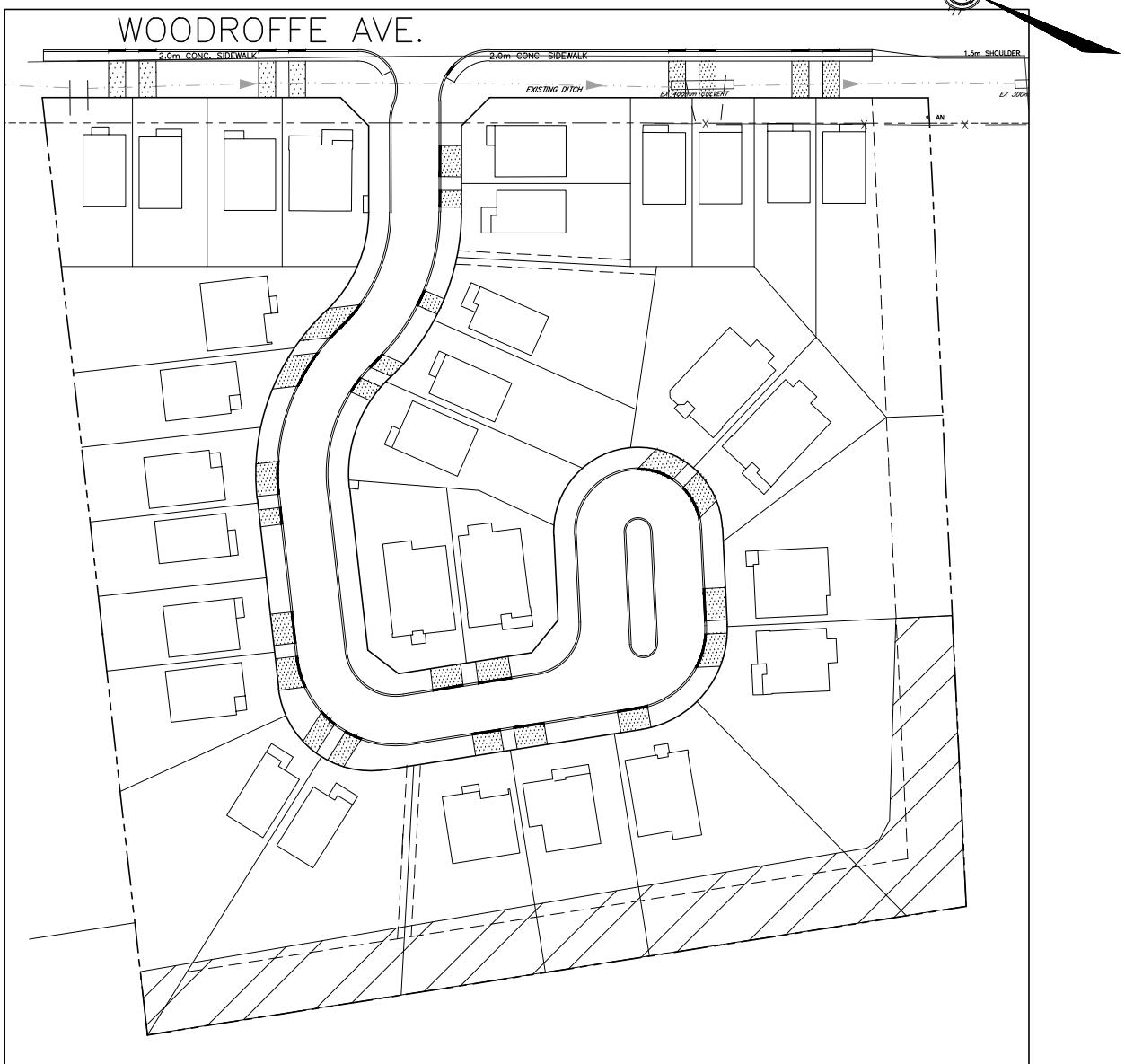




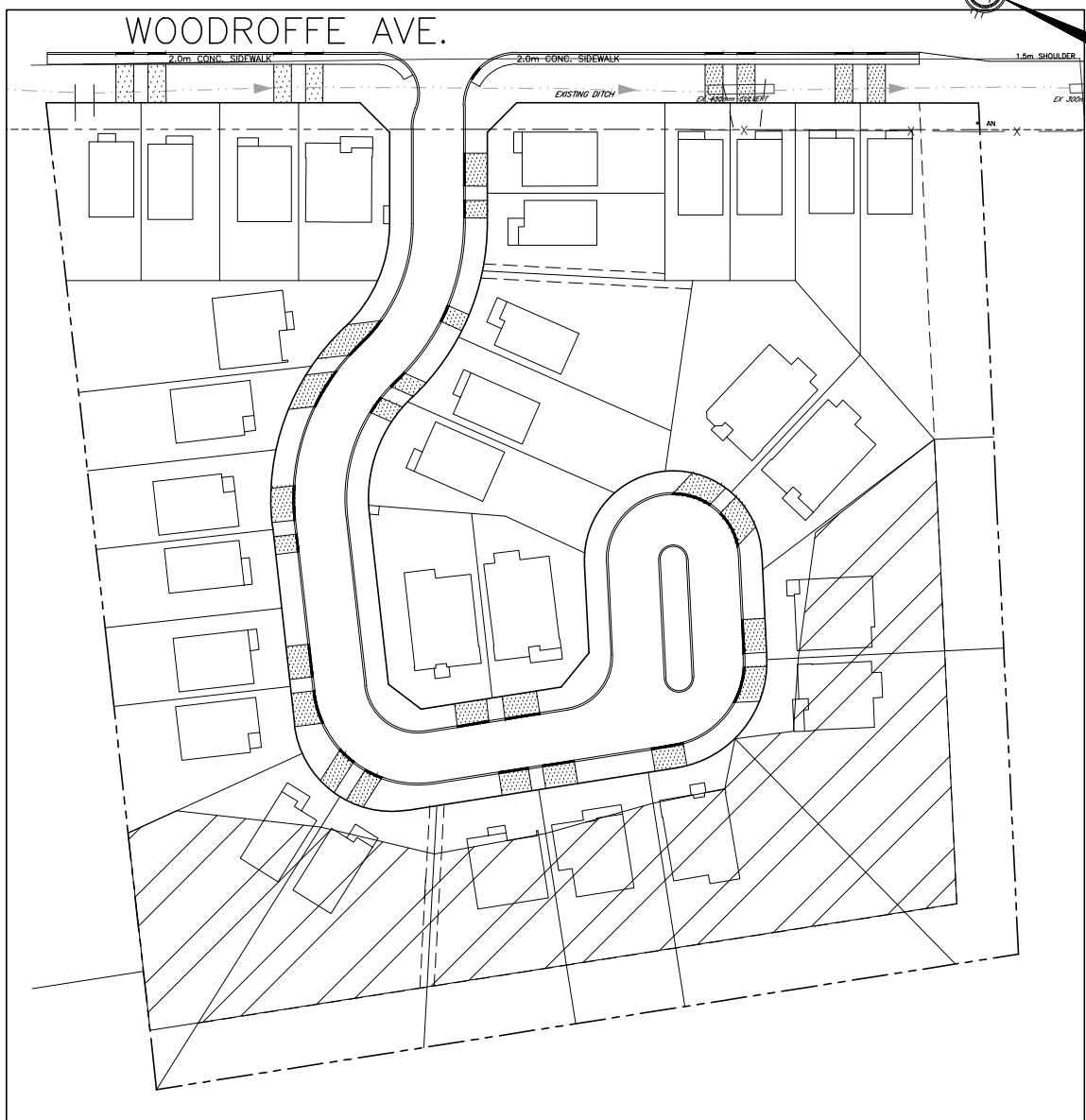
PRE-DEVELOPMENT RUNOFF			
RETURN PERIOD	T <sub>c</sub> (min.)	C VALUE	FLOW (L/s)
5 YEAR	7.7	0.20	142.30
100 YEAR	7.7	0.25	177.80

scale N.T.S.	project no. 14057
date 10/12/15	BORRELLO SUBDIVISION
drawn by BLM	PRE-DEVELOPMENT DRAINAGE PRE-WEST

**Robinson**  
Land Development



5 YEAR POST-DEVELOPMENT DRAINAGE BOUNDARY

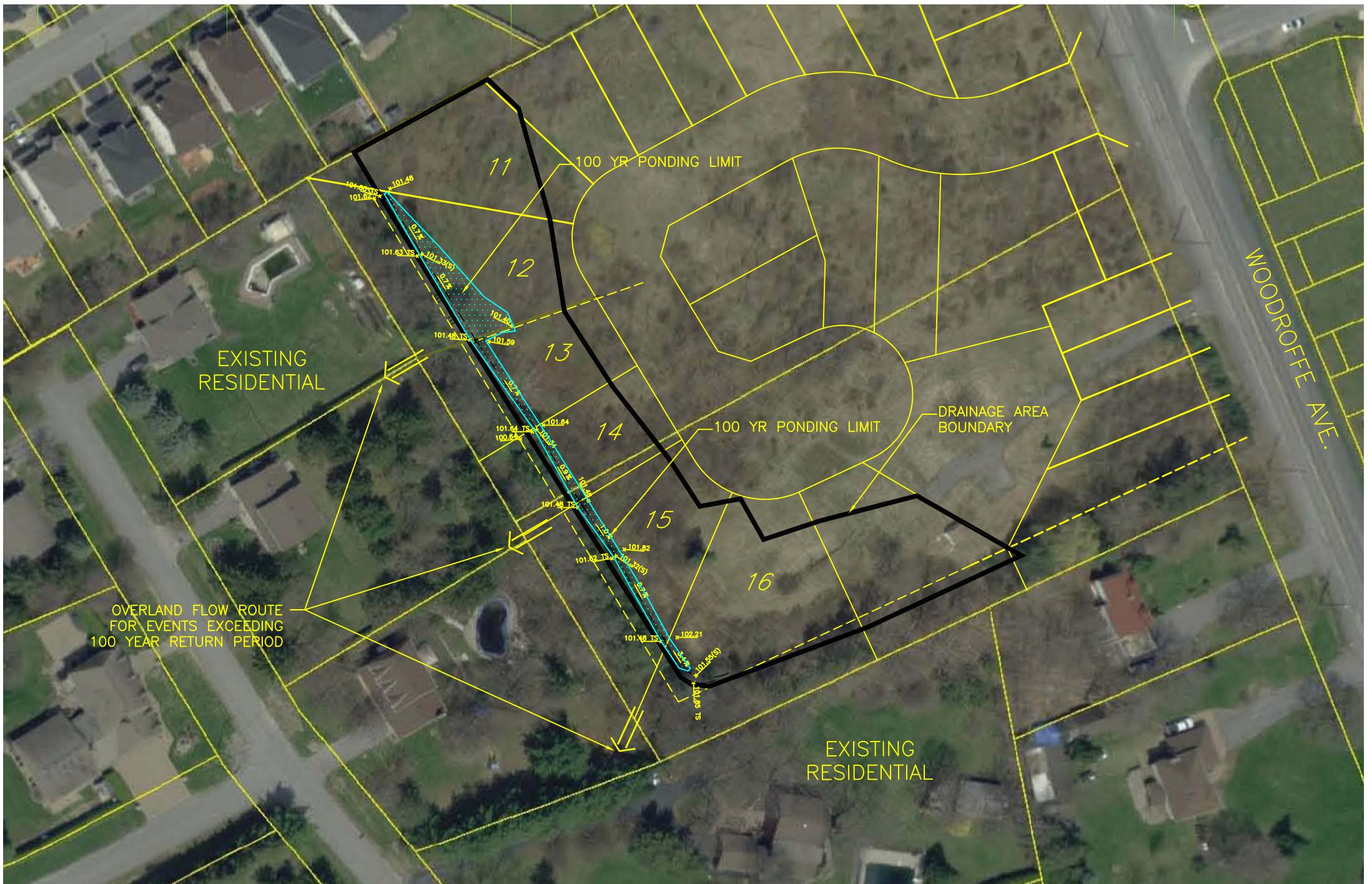


100 YEAR POST-DEVELOPMENT DRAINAGE BOUNDARY

POST-DEVELOPMENT RUNOFF			
RETURN PERIOD	T <sub>c</sub> (min.)	C VALUE	FLOW (L/s)
5 YEAR	5.0	0.20	30.50
100 YEAR	10.0	0.34	89.20

**Robinson**  
Land Development

scale N.T.S.	BORRELLO SUBDIVISION	project no. 14057
date 10/12/15		
drawn by BLM	POST-DEVELOPMENT DRAINAGE	POST-WEST



100 YR PONDING  
ELEVATION = 101.48  
STORAGE PROVIDED =  $57.0 \text{ m}^3$   
STORAGE REQUIRED =  $56.6 \text{ m}^3$

**Robinson**  
Land Development

scale N.T.S.	BORRELLO SUBDIVISION	project no. 14057
date 10/12/15		
drawn by BLM	LOT 11-16 OVERLAND FLOW DIRECTION	OFD

Appendix D  
Watermain Hydraulic Analysis Report

## Borrello Subdivision Hydraulic Analysis Report

Prepared For:

3428 Woodroffe Avenue  
Antonino Borrello

Prepared By:

Robinson Land Development

Our Project No. 14057  
November 2015

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2.2.2	Peak Hour and Maximum Pressure.....	3
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2.2.4	High Pressure .....	4
3.0	CONCLUSION .....	4

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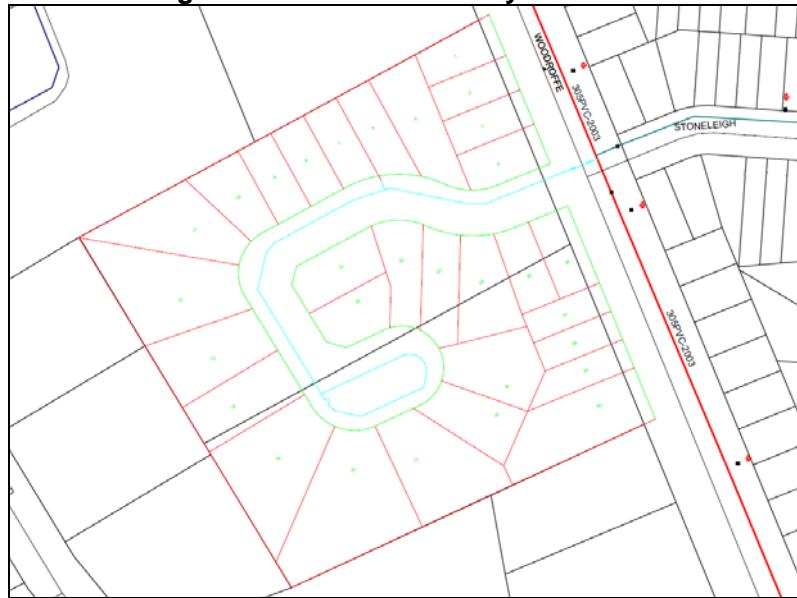
## LIST OF TABLES

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## 1.0 INTRODUCTION

The proposed Borrello subdivision is a 30 lot subdivision located on the west side of Woodroffe Avenue south of Strandherd Drive near Stoneleigh Crescent. The water supply for this subdivision will be provided by connecting to the existing 305mm diameter PVC watermain on Woodroffe Avenue. As per the City of Ottawa standard detail for cul-de-sac streets, the watermain will be reduced to 51mm in diameter after the last hydrant. (See Figure D1)

**Figure D1 : Subdivision Layout**

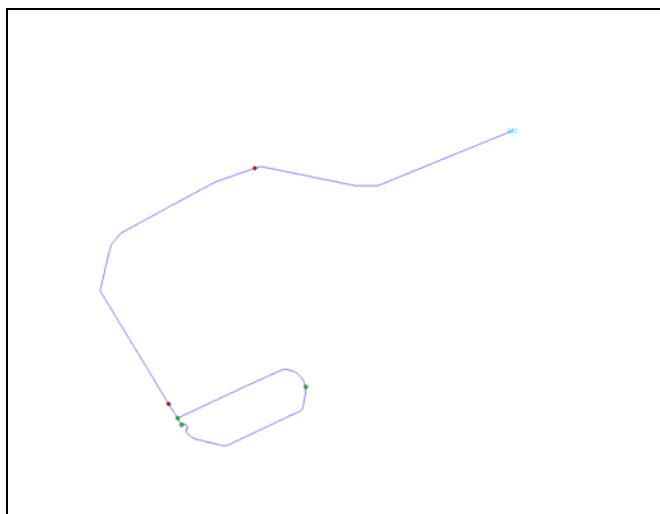


## 2.0 WATER NETWORK HYDRAULIC ANALYSIS

A steady-state water hydraulic model was created, utilizing the boundary conditions provided by the City of Ottawa. (See Figure D2) The boundary conditions provided by the City are shown below. The model was run for the following conditions:

- Peak Hour
- Maximum Day plus fire flow
- High Pressure Check

**Figure D2 : Hydraulic Model Set-up**



### **Boundary Conditions at Borrello Subdivision**

#### **Information Provided:**

Date provided: 27 October 2015

Criteria	Demand (L/s)
Average Demand	0.30
Maximum Daily Demand	0.76
Peak Hourly Demand	1.67
Fire Flow Demand	167
Maximum Daily + Fire Flow Demand	167.3

#### **Location:**



#### **Results:**

Criteria	Head (m)	Pressure (psi)
Max HGL	166.3	91.5
PKHR	137.6	50.7
MXDY + Fire Flow (167.3 L/s)	122.2	28.8

Note: The site is located in future 3C pressure zone and assessed for both pre and post zone reconfiguration conditions. The provided boundary conditions represent the governing set of BCs.

#### **Considerations:**

1. According to the City of Ottawa Water Design Guidelines as well as the Ontario Building Code, the maximum pressure at any point within a distribution system shall not exceed 80 psi in occupied areas. Measures should be taken to try to reduce the residual pressure

below 80 psi without the use of special pressure control equipment. In circumstances where the residual pressure cannot be reduced below 80 psi without the use of pressure control equipment, pressure reducing valve (s) (**PRV**) should be installed at site.

## Disclaimer

*The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation. Fire Flow analysis is a reflection of available flow in the watermain; there may be additional restrictions that occur between the watermain and the hydrant that the model cannot take into account.*

## 2.2 Hydraulic Modelling Results

### 2.2.1 Hydraulic Model Summary

Based on the boundary conditions provided by the City, the peak hour demand conditions are based on future system operation within the reconfigured 3C pressure zone. Maximum pressure and maximum day plus fireflow are based on present day system configuration. Junction elevations used in the model are based on ground elevations from the proposed grading plan.

An initial sensitivity check was performed considering a pipe diameter of 152mm, which quickly yielded fireflow results that were lower than desired. For this reason, the pipe diameter up to the final hydrant was set at 203mm in diameter, with a c-value of 110. Pipe tables including diameter and c-values are presented in Appendix 'A'.

### 2.2.2 Peak Hour and Maximum Pressure

A simulation was completed for peak hour demand, as well as for maximum pressures, using the boundary conditions provided. The results are shown in below.

**Table D1: Peak Hour and Maximum Pressure Results**

Junction	Peak Hour (psi)	Maximum Pressure (psi)
J1	48.1	88.9
J2	48.0	88.8

Results of the peak hour simulation show a pressure range of 48 psi to 89 psi. The site is located in the future 3C pressure zone, which is reflected in the boundary condition for peak hour demands that was provided by the City of Ottawa. Since pressure will be above 80 psi for the maximum pressure check, it is recommended that pressure reducing valves be installed in each home.

### 2.2.3 Fire Flow Simulation

The Fire Underwriter's Survey – Long form was utilized to determine the required fire flow for a 2 storey, wood frame building. The required fire flow from this calculation is 9,000 lpm, which is included at the end of this appendix. To ensure that Technical Bulletin ISDTB-2014-02 is being satisfied, the required fireflow was rounded up to 167 l/s (10,000 lpm).

**Table D2**  
**Fireflow Simulation Results**

	ID	Static Demand (Lpm)	Fire-Flow Demand (Lpm)	Available Flow at Hydrant (Lpm)
1	12	8.40	10,019.93	21,108.56
2	14	10.20	10,019.93	13,576.83

The fire flow results indicate that there is significantly more than the required fireflow of 10,000 lpm available for a 203mm diameter watermain.

#### **2.2.4 High Pressure**

It was found, based on the boundary conditions provided by the City, that the expected maximum pressure will be greater than 80 psi and therefore pressure reducing valves are recommended in each home.

### **3.0 CONCLUSION**

The hydraulic modelling has demonstrated that the proposed Borrello Subdivision can be serviced by a new 203mm diameter watermain. Due to pressure being higher than 80psi, pressure reducing valves are being recommended for installation in each home.

Borrello Subdivision - Customized Pipe Report

	PIPE: ID (Char)	PIPEHYD: LENGTH (Num)	PIPEHYD: DIAMETER (Num)	PIPEHYD: ROUGHNESS (Num)
1	80002	4.90	203.00	110.00
2	80003	2.28	203.00	110.00
3	11	80.31	203.00	110.00
4	80001	101.24	203.00	110.00
5	79	43.49	51.00	90.00
6	75	48.13	51.00	90.00

## WATERMAIN DESIGN SHEET

Borrello Subdivision  
Project No. 14057

### TABLE

Junction Node Number	RESIDENTIAL POPULATION				NON-RES		AVG. DAILY				MAX. DAILY				MAX. HOURLY			
	ACTUAL COUNT				COMM. (HA)	INST. (HA)	DEMAND (l/s)				DEMAND (l/s)				DEMAND (l/s)			
	Low Density	Medium Density	High Density	Total Population			RES.	COMM.	INST.	TOTAL	RES.	COMM.	INST.	TOTAL	RES.	COMM.	INST.	TOTAL
1	10			34.00			0.14			0.14	0.34			0.34	0.76		0.76	
2	12			40.80			0.17			0.17	0.41			0.41	0.91		0.91	
Total	22			74.80			0.30			0.30	0.76			0.76	1.67		1.67	

#### Residential Densities

Low Density (SFH's) =	3.4	cap/unit
Medium Density (Townhouses) =	2.7	cap/unit
High Density (Apartments) =	1.8	cap/unit

#### Avg. Daily Demand:

Residential =      350      L/cap/day

#### Max. Daily Demand:

2.5    x Avg. Day

#### Max. Hourly Demand:

2.2    x Max. Day

## FUS Fire Flow Calculations

**Robinson**  
Consultants

Project #:

14057

Calculations Based on 1999 Publication "Water Supply  
for Public Fire Protection" by Fire Underwriters' Survey

(FUS)

Project Name: Borrello Subdivision  
Date: 1 May, 2015

Building Type/Description/Name:

Single Family Dwellings

Table A: Fire Underwriters Survey Determination of Required Fire Flow - Long Method

Step	Task	Term	Options	Multiplier Associated with Option	Choose:	Value Used	Unit	Total Fire Flow (L/min)				
<b>Framing Material</b>												
1	Choose Frame Used for Construction of Unit	Coefficient related to type of construction (C)	Wood Frame	1.5	Wood Frame	1.5	m					
			Ordinary Construction	1								
			Non-combustible construction	0.8								
			Fire resistive construction (< 2 hrs)	0.7								
			Fire resistive construction (> 2 hrs)	0.6								
2	Choose Type of Housing (if TH, Enter Number of Units per TH Block)	<b>Floor Space Area</b>										
		Type of Housing	Single Family	1	Single Family	1	Units					
			Townhouse - indicate # of units	3								
2.2	# of Storeys	Number of Floors/Storeys in the Unit (do not include basement):										
3	Enter Ground Floor Area of One Unit	Enter Ground Floor Area (A) of One Unit Only:										
		Measurement Units	Square Feet (ft <sup>2</sup> )	0.09290304	Square Feet (ft <sup>2</sup> )	222.9673	Area in Square Metres (m <sup>2</sup> )					
			Square Metres (m <sup>2</sup> )	1								
			Hectares (ha)	10,000								
4	Obtain Required Fire Flow Without Reductions	Required Fire Flow (without reductions or increases per FUS) (F=220*C*VA), round to nearest 1000 L/min										
5	Apply Factors Affecting Burning	<b>Reductions/Increases Due to Factors Affecting Burning</b>										
5.1	Choose Combustibility of Building Contents	Occupancy content hazard reduction or surcharge	Non-combustible	-0.25	Combustible	0	N/A	5000				
			Limited Combustible	-0.15								
			Combustible	0								
			Free burning	0.15								
			Rapid Burning	0.25								
5.2	Choose Reduction Due to Presence of Sprinklers	Sprinkler reduction	Complete Automatic Sprinkler Protection	-0.3	None	0	N/A	0				
			None	0								
5.3	Choose Separation Distance Between Units	Exposure Distance Between Units	North Side	10.1 to 20m	0.7	0.15	N/A	3500				
			East Side	3.1 to 10m								
			South Side	10.1 to 20m								
			West Side	3.1 to 10m								
6	Obtain Required Fire Flow, Duration & Volume	<b>Total Required Fire Flow, rounded to nearest 1000 L/min:</b>										
		<b>Total Required Fire Flow (above) in L/s:</b>										
		<b>Required Duration of Fire Flow (hrs)</b>										
		<b>Required Volume of Fire Flow (m<sup>3</sup>)</b>										

Note: The most current FUS document should be referenced before design to ensure that the above figures are consistent with the intent of the Guidelines

Legend	
Drop down menu - choose option, or enter value	
No information, No input required	

## **Appendix E**

### **Development Servicing Study Checklist**

## 4.1 General Content

- Executive Summary (for larger reports only).

*Comments:* *N/A due to report length*

- Date and revision number of the report.

*Comments:* *See title page*

- Location map and plan showing municipal address, boundary, and layout of proposed development.

*Comments:* *See Figure 1.0 in report*

- Plan showing the site and location of all existing services.

*Comments:* *see Servicing Plan 14057-S1 for services*

- Development statistics, land use, density, adherence to zoning and official plan, and reference to applicable subwatershed and watershed plans that provide context to which individual developments must adhere.

*Comments:* *The applicable governing reports are documented in Section 1.0. Adherence to zoning has been covered in consultation with City staff.*

- Summary of Pre-consultation Meetings with City and other approval agencies.

*Comments:* *Various pre-consultations have taken place between land owner and City staff for the subdivision configuration*

- Reference and confirm conformance to higher level studies and reports (Master Servicing Studies, Environmental Assessments, Community Design Plans), or in the case where it is not in conformance, the proponent must provide justification and develop a defendable design criteria.

*Comments:* *See Section 1.0*

- Statement of objectives and servicing criteria.

*Comments:* *Stated throughout the report*

- Identification of existing and proposed infrastructure available in the immediate area.

*Comments:* *see Servicing Plan 14057-S1 for services*

- Identification of Environmentally Significant Areas, watercourses and Municipal Drains potentially impacted by the proposed development (Reference can be made to the Natural Heritage Studies, if available).

*Comments:* N/A

- Concept level master grading plan to confirm existing and proposed grades in the development. This is required to confirm the feasibility of proposed stormwater management and drainage, soil removal and fill constraints, and potential impacts to neighbouring properties. This is also required to confirm that the proposed grading will not impede existing major system flow paths.

*Comments:* see Grading Plan 14057-GR1 in Appendix A

- Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts.

*Comments:* N/A

- Proposed phasing of the development, if applicable.

*Comments:* Any proposed phasing is not known at this time.

- Reference to geotechnical studies and recommendations concerning servicing.

*Comments:* A geotechnical Report is being completed by Golder Associates and will be forwarded when complete. No exceptional geotechnical requirements are

[+]

- All preliminary and formal site plan submissions should have the following information:

- Metric scale
- North arrow (including construction North)
- Key plan
- Name and contact information of applicant and property owner
- Property limits including bearings and dimensions
- Existing and proposed structures and parking areas
- Easements, road widening and rights-of-way
- Adjacent street names

*Comments:* N/A

## 4.2 Development Servicing Report: Water

- Confirm consistency with Master Servicing Study, if available

*Comments:* *Water as per City standards and updated design guidelines*
- Availability of public infrastructure to service proposed development

*Comments:* *See Section 2.0 and Appendix D*
- Identification of system constraints

*Comments:* *N/A*
- Identify boundary conditions

*Comments:* *See Section 2.0 and Appendix D*
- Confirmation of adequate domestic supply and pressure

*Comments:* *See Section 2.0 and Appendix D*
- Confirmation of adequate fire flow protection and confirmation that fire flow is calculated as per the Fire Underwriter's Survey. Output should show available fire flow at locations throughout the development.

*Comments:* *See Section 2.0 and Appendix D*
- Provide a check of high pressures. If pressure is found to be high, an assessment is required to confirm the application of pressure reducing valves.

*Comments:* *See Section 2.0 and Appendix D*
- Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defined phases of the project including the ultimate design

*Comments:* *No constraints.*
- Address reliability requirements such as appropriate location of shut-off valves

*Comments:* *N/A*
- Check on the necessity of a pressure zone boundary modification.

*Comments:* *N/A*

- Reference to water supply analysis to show that major infrastructure is capable of delivering sufficient water for the proposed land use. This includes data that shows that the expected demands under average day, peak hour and fire flow conditions provide water within the required pressure range

*Comments:* *See section 2.0 and Appendix D*

- Description of the proposed water distribution network, including locations of proposed connections to the existing system, provisions for necessary looping, and appurtenances (valves, pressure reducing valves, valve chambers, and fire hydrants) including special metering provisions.

*Comments:* *See section 2.0 and Appendix D and servicing drawing.*

- Description of off-site required feedermains, booster pumping stations, and other water infrastructure that will be ultimately required to service proposed development, including financing, interim facilities, and timing of implementation.

*Comments:* *N/A*

- Confirmation that water demands are calculated based on the City of Ottawa Design Guidelines.

*Comments:* *See Section 2.0 and Appendix D*

- Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference.

*Comments:* *See Appendix D*

## 4.3 Development Servicing Report: Wastewater

- Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitored flow data from relatively new infrastructure cannot be used to justify capacity requirements for proposed infrastructure).

*Comments:* *See Section 3.0 and Appendix B*

- Confirm consistency with Master Servicing Study and/or justifications for deviations.

*Comments:* *See Section 3.0 and Appendix B*

- Consideration of local conditions that may contribute to extraneous flows that are higher than the recommended flows in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers.

*Comments:* *N/A*

- Description of existing sanitary sewer available for discharge of wastewater from proposed development.

*Comments:* *see Section 3.0, design sheets and drawing 14057-S1 and 14057-SAN1*

- Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable)

*Comments:* *Verified in sewer design sheet*

- Identification and implementation of the emergency overflow from sanitary pumping stations in relation to the hydraulic grade line to protect against basement flooding.

*Comments:* *N/A*

- Special considerations such as contamination, corrosive environment etc.

*Comments:* *N/A*

## 4.4 Development Servicing Report: Stormwater

- Description of drainage outlets and downstream constraints including legality of outlets (i.e. municipal drain, right-of-way, watercourse, or private property)
 

*Comments:* **Minor system goes to Woodroffe Avenue sewer, major overland to Woodroffe Avenue - See Section 4.0**
- Analysis of available capacity in existing public infrastructure.
 

*Comments:* **See storm sewer design sheet.**
- A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns, and proposed drainage pattern.
 

*Comments:* **See drawing 14057-S1 and 14057-STM1**
- Water quantity control objective (e.g. controlling post-development peak flows to pre-development level for storm events ranging from the 2 or 5 year event (dependent on the receiving sewer design) to 100 year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects.
 

*Comments:* **See Section 4.0 and 5.0 for various details. Quality control is provided by the Nepean South Chapman Mills SWM Pond**
- Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements.
 

*Comments:* **Quality control is provided by the Strandherd SWM Pond.**
- Description of the stormwater management concept with facility locations and descriptions with references and supporting information.
 

*Comments:* **See Section 4.0 and 5.0 for various details.**
- Set-back from private sewage disposal systems.
 

*Comments:* **N/A**
- Watercourse and hazard lands setbacks.
 

*Comments:* **N/A**
- Record of pre-consultation with the Ontario Ministry of Environment and the Conservation Authority that has jurisdiction on the affected watershed.
 

*Comments:* **SWM pond has already been approved and the site is not in close proximity to any watercourses. Pre-consult not required.**

- Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists.
- Comments:* *See discussion in Section 4.0*
- Storage requirements (complete with calculations) and conveyance capacity for minor events (1:5 year return period) and major events (1:100 year return period).
- Comments:* *See Section 4.0 and Appendix C*
- Identification of watercourses within the proposed development and how watercourses will be protected, or, if necessary, altered by the proposed development with applicable approvals.
- Comments:* *N/A*
- Calculate pre and post development peak flow rates including a description of existing site conditions and proposed impervious areas and drainage catchments in comparison to existing conditions.
- Comments:* *See Section 4.0 and Appendix C. Pre/post not required. Design is based upon a prescribed 70 L/s/ha*
- Any proposed diversion of drainage catchment areas from one outlet to another.
- Comments:* *N/A*
- Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and stormwater management facilities.
- Comments:* *See drawings 14057-S1 and SWM1 in Appendix A and C*
- If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post-development flows up to and including the 100-year return period storm event.
- Comments:* *Quantity control is proposed. See Section 4.0 for details*
- Identification of potential impacts to receiving watercourses
- Comments:* *N/A*
- Identification of municipal drains and related approval requirements.
- Comments:* *N/A*

- Descriptions of how the conveyance and storage capacity will be achieved for the development.

*Comments:* *See Section 4.0 and Appendix C for details of surface storage.*
- 100 year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading.

*Comments:* *Maximum ponding levels of 0.3m on local roads and 0.25m on collector roads. Major flow routing to Woodroffe Avenue.*
- Inclusion of hydraulic analysis including hydraulic grade line elevations.

*Comments:* *See Section 4.0*
- Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors.

*Comments:* *See Section 5.0 and Erosion and Sediment Control drawing*
- Identification of floodplains - proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions.

*Comments:* *N/A*
- Identification of fill constraints related to floodplain and geotechnical investigation.

*Comments:* *N/A*

## 4.5 Approval and Permit Requirements: Checklist

The Servicing Study shall provide a list of applicable permits and regulatory approvals necessary for the proposed development as well as the relevant issues affecting each approval. The approval and permitting shall include but not be limited to the following:

- Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act.

*Comments:* N/A

- Application for Certificate of Approval (CofA) under the Ontario Water Resources Act.

*Comments:* *The development will require an application for the installation of the sanitary and storm sewers.*

- Changes to Municipal Drains.

*Comments:* N/A

- Other permits (National Capital Commission, Parks Canada, Public Works and Government Services Canada, Ministry of Transportation etc.)

*Comments:* N/A

## 4.6 Conclusion Checklist

- Clearly stated conclusions and recommendations

*Comments:* See Section 6.0

- Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency.

*Comments:* N/A

- All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario

*Comments:* Report are signed.