

REPORT

PROJECT: 120031-5.2.2

ASSESSMENT OF ADEQUACY OF PUBLIC SERVICES RIVERSIDE SOUTH PHASE 12 LANDS RIVERSIDE SOUTH COMMUNITY RIDEAU RIVER AREA



Prepared for URBANDALE CORPORATION by IBI GROUP

MARCH 2019

Updated: NOVEMBER 2020

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- RIVERSIDE SOUTH PHASE 12
RIVERSIDE SOUTH COMMUNITY
RIDEAU RIVER AREA

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1 INTRODUCTION

1.1 Purpose

The purpose of this report is to investigate and confirm the adequacy of public services for the proposed site. This report will review major municipal infrastructure including water supply, wastewater collection and disposal and management of stormwater. This report will also include a Sedimentation and Erosion Control Plan. A review of traffic components will be the subject of a separate report.

This report is being prepared as a technical document in support of the subdivision submission for the subject site, and was prepared in accordance with the November 2009 "Servicing Study Guidelines for Development Applications" in the City of Ottawa. **Appendix A** contains a customized copy of those guidelines which can be used as a quick reference for the location of each of the guideline items within the study report.

1.2 Background

The Riverside South Community, formerly known as South Urban Community (SUC), is a part of the former City of Gloucester. The Council of the City of Gloucester adopted the first Official Plan for the community in September 1990. The original concept plan for the community served as the basis for both a Gloucester and a Regional OPA. A Master Drainage Plan (MDP) for the community was formulated in June 1992 based on the preliminary land use plan prepared by J. Bousfields and Associates Ltd. in December 1991.

The South Urban Community became a part of the City of Ottawa through amalgamation in 2001 and the new Official Plan of the City of Ottawa designated the areas as "General Urban Area" and "Employment Area" with some adjustments to the urban boundaries. In 2003, the City of Ottawa initiated a Community Design Plan (CDP) for the Riverside South area. The basis of the CDP is the land use plan for the community, which has evolved over the time and has changed significantly since the original plan prepared in early 1990's.

The South Urban Community River Ridge Master Infrastructure Plan (SUC RR MIP) prepared by Ainley Graham and Associates in 1994 presented a preferred servicing strategy for potable water, sanitary and storm infrastructure in the Riverside South community. The Riverside South Infrastructure Servicing Study Update (ISSU) was issued in 2008 as an update to the SUC RR MIP, to account for modifications to the MDP and CDP since 1994.

There have been significant revisions to the CDP, MDP and City of Ottawa Design Guidelines since 2008 so in June 2017, Stantec helped the City of Ottawa complete an update to the 2008 ISSU for a portion of the Riverside Community called Rideau River Area and which includes the lands proposed to be tributary to Pond 5. The 2017 Riverside South Community Infrastructure Servicing Study Update – Rideau River Area (2017 ISSU) report recognized the approved 2016 CDP which considers changes in land use planning and development densities in accordance with Official Plan objectives. For reference a copy of the 2016 Riverside South Community Design Plan – Land use Plan is included in **Appendix A**. The infrastructure analyses also accounted for existing sewer and infrastructure and the stormwater management pond within the study area. The purpose of the 2017 ISSU report was to present a new preferred potable water, sanitary and stormwater infrastructure servicing strategy for the Rideau River Study area. A copy of Figure 1.1, Riverside South Community and Study Area Boundary, from the 2017 report, is also included in **Appendix A** for reference.

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Subsequent to the completion of the revised ISSU, construction of the Riverside South Pond 5 and the River Road reconstruction has been substantially completed.

1.3 Previous Studies

Since the South Urban Community and Riverside South Community have been planned and developed for over twenty five years, there have been numerous background studies dealing with major municipal infrastructure. Many of those reports are listed in the 2017 Updated Report. For reference, pages 1.4 and 1.5 which list these previous studies from that report, are included in **Appendix A**. The following reports however, were referenced prior to completing this assessment:

- 1. Riverside South Community Infrastructure Servicing Study Update (ISSU) Rideau River Area (Stantec, 2017) The report is the most current approved document which reviews the provision of major municipal infrastructure, including water supply, wastewater collection and treatment of storm runoff, in the Rideau River Area of the larger Riverside South Community. The report reviewed many of the recommendations from relevant earlier reports including:
 - a) 2016 Land Use Plan for the Riverside South Community Design Plan
 - b) Riverside South Master Servicing Study (Stantec 2008)

The report provided a macro level servicing plan for the Rideau River Area portion of the Riverside South Community. The subject property is proposed to be developed in accordance with the recommendations of the 2017 Updated report. The more specific details of the development will be part of the final engineering design of the lands.

- 2. Design Brief River Road Reconstruction prepared for Riverside South Development Corporation (IBI Group, 2018) The report is the current approved document which provides details on the now existing water supply, major and minor storm systems and sanitary sewers located in River Road adjacent to and south of the subject lands.
- 3. Design Brief Summerhill Village Phase 2 prepared for Claridge Homes (IBI Group, November 2011) The report provides details on the proposed water supply, major and minor storm systems and sanitary sewers also located in River Road adjacent to the site and within the existing residential subdivision across River Road from the proposed lands.
- 4. Design Report for Phase 9 Riverside South Development Corporation(JL Richards, 2012) The report provides details on the water supply, major and minor storm systems and sanitary sewers adjacent to the proposed site within the existing residential subdivision across River Road from the proposed lands.

1.4 Subject Property

The current draft plan of subdivision for the subject property is shown on **Figure 1.2** which is included in **Appendix A**. The proposed subdivision is split into two sections, the north portion is approximately 9.6 Ha is size while the south portion is 2.4 Ha.

The proposed development will include a mix of single family and townhouse residential units. Additionally the north portion contains a block of lands to be further developed though the City's Site Plan Application process at a later date into a mid-density residential area.

1.5 Existing Infrastructure

Figure 1.3 shows the location of existing major municipal infrastructure in the vicinity of the Riverside South Phase 12 development. The 2017 ISSU report recommended that the subject

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site be serviced with a 305 and 406 mm diameter watermains along River Road which have been constructed and are in service.

Previous studies recommend that wastewater flows from the subject site be routed to two outlets, the majority of the subject lands, all of the south site and the south half of the north site, are to connect to the existing sanitary sewers in River Road and flow eastwards through the River Road sub-trunk sewer located within the Summerhill Street ROW. A smaller portion of the site, the north half of the north section is designed to flow into a sanitary outlet constructed during the Phase 9 Lands development in Ballinville Circle.

All minor stormwater runoff from the site is proposed to be routed to future Pond 5 which is located south of the subject site west of River Road. All trunk sewers required to convey stormwater from the subject lands to the pond have been constructed and are complete, and the pond is currently substantially complete.

1.6 Pre-Consultation

There was a pre-consultation meeting with the City of Ottawa on August 30, 2018. The meeting notes can be found in **Appendix A**. The following are some of the topics reviewed and discussed:

- Zoning information
- Official plan
- Infrastructure
- Noise Study needed
- Traffic Study needed

- Geotechnical conditions
- Assessment of Adequacy of Public Services Report needed

It should be noted that consultation with the Rideau Valley Conservation Authority and the Ontario Ministry of Environment, Conservation and Parks and Parks Canada are to be scheduled forthwith.

1.7 Existing Topography

The property generally slopes from east to west towards the Rideau River. Contours for the site range between 90 and 85 meters. **Figure 1.4**, which is included in **Appendix A**, shows the general topography of the subject property.

Most surface drainage from the property currently flow directly to the Rideau River.

Once developed, the intent will be to maintain existing drainage patterns. For reference, a copy of Drawing GCP-1, Macro Grading Plan from the 2017 report is included in **Appendix A**.

Figure 1.5, located in Appendix A, shows the proposed macro-grading plan for the subject lands.

1.8 Geotechnical Considerations

The subject lands are covered under two geotechnical reports, the following geotechnical investigation report has been prepared by Paterson Group in support of the north section lands.

Report No. PG3320-2-Rev1 dated November 20, 2020.

The following geotechnical investigation report has been prepared by Golder in support of the south section lands.

Report No. 1406631-3-Rev2 dated August 2018

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Among other items, the reports comments on the following:

- Site grading
- Foundation design
- Pavement design
- Sub-surface Conditions

- Seismic design
- Corrosion potential
- · Site Servicing

Groundwater Control

In general, the subsurface profile of the north lands include topsoil, underlain by stiff silty clay. While the south lands consist of topsoil underlain by clayey silt and silt.

One of the recommendations from the Paterson Group study included grade raise restrictions for the north side development. A general grade raise restriction for the north site of 2.5m has been provided and a 4 m grade raise over a small natural ditch, the location of this is shown on the Permissible Grade Raise Plan Drawing PG3320-4 in **Appendix A**.

Regarding the south side, Golder has established a 2.1m grade raise restriction for these lands.

1.9 Watercourses and Setbacks

There are no identified Municipal Drains in the 2017 ISSU report.

The September 2016 Environmental Impact Statement by Dillon Consulting states that the site is not located near any provincially significant wetlands, significant woodlands, areas of natural and scientific interest, significant wildlife habitat, or any other designated natural heritage system constraints. The Dillon study does identify 2 headwater drainage features within the subject lands; however, their study determined that these features had limited functions and they deemed that "no management required".

For the north side development Paterson has conducted a slope stability analysis for the east border that slopes down to the Rideau River. A Limit of Hazard Lands line has been determined and is shown on Drawing PG3320-2 Test Hole Location Plan in **Appendix A**, the line doesn't impact proposed housing.

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2 WATER SUPPLY

2.1 Existing Conditions

As noted in Section 1.5 there is an existing 300 mm watermain on River Road along the north block. The 300 mm watermain was recently extended south on River Road, at Borbridge Avenue the River Road watermain increases to 400 mm in diameter, adjacent to the south block. **Figure 1.3** in **Appendix A** shows the location of the existing watermains.

2.2 Riverside South Community Infrastructure Servicing Study Update – Rideau River Area (2017 ISSU)

The report provided trunk watermain servicing for the Rideau River Area, the location and size of the proposed watermains is shown on Drawing WAT-1 in **Appendix B**.

A hydraulic analysis was conducted for the Rideau River Area trunk watermain as part of the report. The analysis was conducted with the Barrhaven Pump Station operating at a discharge HGL of 147 m and the Ottawa South Pump Station operating at a discharge HGL of 146 m to Zone SUC which includes the Rideau River Area. Water demands were based on recent projections presented in the Riverside South Community Design Plan (CDP) 2016.

Results of the hydraulic modeling under basic day condition shows some areas where the pressure exceeds 552 kPa (80 psi). The high pressure areas are in the low lying land near the Rideau River, and is shown on Figure 5.4 from the Servicing Study Update which is included in **Appendix B**. Buildings in the high pressure area will require pressure reducing valves in accordance with Technical bulletin ISDTB-204.02. The hydraulic analysis showed that no areas fell below the minimum pressure of 276 kPa (40 psi) under peak hour conditions. A fire flow analysis was also conducted which showed that all nodes can provide more than a 13,000 l/min fire flow while maintaining a minimum system pressure of 138 kPa (20 psi).

2.3 Design Criteria

2.3.1 Water Demands

Water demands have been calculated for the site based on per unit population density and consumption rates taken from Tables 4.1 and 4.2 of the City of Ottawa Design Guidelines – Water Distribution and are summarized as follows:

•	Single Family	3.4 person per unit
•	Townhouse and Semi-Detached	2.7 person per unit
•	Average Apartment	1.8 person per unit
•	Residential Average Day Demand	350 l/cap/day
•	Residential Peak Daily Demand	875 l/cap/day
•	Residential Peak Hour Demand	1,925 l/cap/day
•	ICI Average Day Demand	50,000 l/gross ha/day
•	ICI peak Daily Demand	75,000 l/gross ha/day
•	ICI Peak Hour Demand	135,000 l/gross ha/day

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Residential units in the subject site consists of street townhouses, single family lots and multidensity units. A watermain demand calculation sheet is included in **Appendix B** and the total water demands are summarized as follows:

Average Day
 Maximum Day
 Peak Hour
 2.28 l/s
 5.73 l/s
 12.54 l/s

2.3.2 System Pressure

The Ottawa Design Guidelines – Water Distribution (WDG001), July 2010, City of Ottawa, Clause 4.2.2 states that the preferred practice for design of a new distribution system is to have normal operating pressures range between 345 kPa (50 psi) and 552 kPa (80 psi) under maximum daily flow conditions. Other pressure criteria identified in Clause 4.2.2 of the guidelines are as follows:

Minimum Pressure Minimum system pressure under peak hour demand conditions shall not

be less than 276 kPa (40 psi)

Fire Flow During the period of maximum day demand, the system pressure shall

not be less than 140 kPa (20 psi) during a fire flow event.

Maximum Pressure Maximum pressure at any point in the distribution system shall not

exceed 689 kPa (100 psi). In accordance with the Ontario Building/Plumbing Code, the maximum pressure should not exceed 552 kPa (80 psi). Pressure reduction controls will be required for buildings where it is not possible/feasible to maintain the system pressure below

552 kPa.

2.3.3 Fire Flow Rates

In the recent Technical Bulletin 'ISDTB-2014-02, Revisions to Ottawa Design Guidelines – Water', the fire flow requirements for single detached dwellings and traditional town and row houses can be capped at 10,000 l/min provided that there is a minimum separation of 10 meters between the backs of adjacent units and that the town and row house blocks are limited to 600 square meters of building areas and seven dwelling units. The street townhouses in this development meet the requirements of ISDTB-2014-02, the fire flow rate of 10,000 l/min (166.7 l/s) is used in the fire flow analysis.

There are several locations where the rear of the single family home faces the side of an adjacent unit. At these locations the distance between the rear and side of the adjacent building may be less than 10 meters depending on the size of the houses which appears to violate item 4.1 of Technical Bulletin ISDTB-2014-02 which requires a 10 meter separation between the backs of the adjacent units. Without the 10,000 l/min cap the Fire Underwriters Survey (FUS) method of determining fire flow rates cannot be used as wood frame buildings separated by less than 3 meters is considered on fire unit. As the side yard distances between houses are usually less than 3 meters then all adjacent houses are considered one fire unit which results in a very large fire flow which is impractical to achieve. At the locations where the rear yard to side yard distance is less than 10 meters, a fire flow can be determined if a 3 meter separation is provided between adjacent units. For example, on Figure 2.1 Lots 28 and 29 back onto Lot 24, if a 3 meter separation is provided between Lots 27 and 28 then Lots 28 and 29 can be considered a single fire unit and an FUS calculation can be carried out. The FUS calculation will usually result in a required fire flow that is close to the 10,000 l/min rate, the actual fire flow rates will be confirmed during detailed design. The locations of potential 3 meter building separations is shown on Figure 2.1.

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There are several multi-unit buildings proposed at the north end of the north block. Without details of the building, a conservative fire flow rate of 15,000 l/min (250 l/s) is used in the fire flow analysis for these buildings.

2.3.4 Boundary Conditions

The City of Ottawa has provided five boundary conditions in the Riverside South area for various projects. There are two boundary conditions which are near the site. One at River Road at Summerhill Street opposite the north block and another on Borbridge Avenue at Southbridge Street. There are two sets of boundary conditions provided, one for pre-configuration and another for post-configuration. As the post configuration values are higher than the pre-configuration, the post configuration value for maximum HGL is used in the analysis for maximum pressure and the pre-configuration peak hour and max day plus fire values are used for minimum pressure and fire flow. A copy of the boundary condition is included in Appendix B and summarized as follows for the two adjacent locations.

	CONNECTION RIVER ROAD & SUMMERHILL	CONNECTION BORBIRDGE & SOUTHBRIDGE
Max HGL (Basic Day)	147.8 m	147.8 m
Peak Hour	123.9 m	123.9 m
Max Day + Fire		
(10,000 l/min Fire Flow)	111.9 m	121.3 m
(15,000 l/min Fire Flow	117.3 m	117.3 m

2.3.5 Hydraulic Model

A computer model for the subject site has been added to the model for the adjacent Riverside South Phase 15-1 & 2 developments including the River Road watermain and the Rivers Edge Phase 1 development. The model includes existing watermains and the boundary conditions.

2.4 Proposed Water Plan

2.4.1 Modeling Results

The hydraulic model was run under basic day, maximum day with fire flows and under peak hour conditions. Water pipes are sized to provide sufficient pressure and to deliver the required fire flows.

Results of the hydraulic model are include in **Appendix B**, with the Phase 12 nodes highlighted, and summarized as follows:

Scenario

Basic Day (Max HGL) Pressure Range	569.7 to 585.9 kPa
Peak Hour Pressure Range	325.2 to 350.5 kPa
Max Day + 10,000 I/min Fire Flow	180.4 l/s to 398.4 l/s
Max Day + 15.000 I/min Fire Flow	271.8 l/s to 280.7 l/s

A comparison of the results and design criteria is summarized as follows:

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Maximum Pressure All nodes have basic day pressures over 552 kPa, therefore pressure

reducing control is required for this development.

Minimum Pressure All nodes in the model exceed the minimum value of 276 kPa (40 psi).

Fire Flow All townhouse and single family lots exceed the fire flow requirement of

166.7 l/s (10,000 l/min). The nodes at the multi-unit residential building

exceed 250 l/s (15,000 l/min).

2.4.2 Watermain Layout

Figure 2.1 shows the proposed Water Plan for the proposed development.

The north block is serviced by three connections to the existing 300 mm watermains on River Road. 200 mm watermains are required to service the single family lots and 250 mm watermains for the multi-unit area at the north end. For the south block, two connections to the recently constructed 400 mm watermain on River Road are required, 200 mm watermains will service the site.

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3 SANITARY SEWERS

3.1 Existing Conditions

As noted earlier in Section 1.5, sanitary flows from the subject site will be routed either to the existing River Road/Summerhill Street sub-trunk sanitary sewer and/or to the existing sanitary stub left during the Phase 9 Lands development in Ballinville Circle. Again, at the time of detailed design the feasibility of directing all sanitary flows form the subject lands to the River Road/Summerhill Street sub-trunk sewer will likely be examined.

3.2 Riverside South Community Infrastructure Servicing Study Update – Rideau River Area (2017 ISSU)

The report provided a macro level servicing plan for the portion of the Riverside South Community that will be tributary to Pond 5, which is referred to as the Rideau River Study Area. The limits of the study area are shown on Figure 1.1 from the study and a copy is included in **Appendix A**. The subject property is located within the Rideau River Drainage Area.

For reference, a copy of Drawing SAN-1, Sanitary Drainage Plan from the 2017 study is included in **Appendix C**. The 2017 ISSU study recommended that drainage area 2A be tributary to the River Road sewer. A copy of Figure 4.2, Recommended Sanitary Servicing (2017 Update), from the 2017 ISSU Report, together with a related design sheet are both included in **Appendix C**.

3.3 River Road Reconstruction (2018 IBI)

Drainage area plan 114373-400 and the sanitary sewer design sheet for this project have been included in **Appendix C** as they demonstrate that the southern portion of the subject lands have been included in the design calculations for the sanitary sewer recently extended in River Road, the subject lands are identified as drainage area 8A.

3.4 Summerhill Village Phase 1 (2011 IBI)

Drainage area plan 3766-501 and the sanitary sewer design sheet for this project have been included in **Appendix C** as they demonstrate that a portion of the norther lands have been included in the design calculations for the existing sanitary sewer in Summerhill Street. The proposed connection is at MH100A at the intersection of River Road and Summerhill Street. The lands are identified as drainage area "FROM MSS 2b.".

3.5 Riverside South Phase 9 (2012 JLR)

Drainage area plan D1-SAN and the sanitary sewer design sheet for this project have been included in **Appendix C** as they demonstrate that the north portion of the northern lands have been included in the design calculations for the existing sanitary sewer in Ballinville Circle. The proposed connection is at stub 73A. The lands are identified as drainage area "Future Phase 12 Residential".

3.6 Design Criteria

The estimated wastewater flows from the subject site are based on the revised City of Ottawa design criteria. Among other items, these include:

Average residential flow

= 280 I/c/d

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Peak residential flow factor = (Harmon Formula) x 0.80

Average commercial flow = 28,000 l/s/ha
 Average institutional flow = 28,000 l/s/ha

Peak ICI flow factor = 1.5 if ICI area is ≤ 20% total area

1.0 if ICI area is > 20% total area

Inflow and Infiltration Rate = 0.33 l/s/ha
 Minimum Full Flow Velocity = 0.60 m/s
 Maximum Full Flow Velocity = 3.0 m/s

• Minimum Pipe Size = 200 mm diameter

In accordance with the City of Ottawa Sewer Design Guidelines table 4.2, the following density rates are estimated for the subject site:

Single units = 3.4
 Semi units = 2.7
 Townhouse and back to back units = 2.7
 Apartment units = 1.8

3.7 Recommended Sanitary Plan

As noted above the whole of the subject lands have been accounted for in the design and construction of the existing adjacent sanitary sewer systems. The current approved plans call for 3 separate connections to existing sanitary sewer systems. A preliminary sanitary plan is included in **Figure 3.1** in **Appendix C**.

No external sanitary flows are anticipated to cross the subject lands. As such, all sanitary sewers are proposed to be at normal depth and size.

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- RIVERSIDE SOUTH PHASE 12 RIVERSIDE SOUTH COMMUNITY

RIDEAU RIVER AREA

Prepared for: URBANDALE CORPORATION INC.

4 STORMWATER MANAGEMENT

4.1 Existing Conditions

The ultimate storm runoff outlet from the property is the Riverside South Pond 5 which is currently under construction and is located west of River Road.

The lands currently drain westward directly into the Rideau River.

4.2 Riverside South Community Infrastructure Servicing Study Update – Rideau River Area (2017 ISSU) Criteria

The report provided a macro level servicing plan for the Riverside South Community that will be tributary to future Pond 5. That area is referred to as the Rideau River Area and includes the subject property. The limits of the study are shown in Figure 1.1 from the study and a copy is included in **Appendix A**.

The 2017 ISSU report recommended that stormwater runoff from the study area be routed to Riverside South Pond 5, which is currently under construction. Minor storm runoff is proposed to be routed to the trunk storm sewer on River Road. For reference a copy of Drawing STM1, Storm Sewers from the 2017 study is included in **Appendix D**.

4.3 River Road Reconstruction (2018 IBI)

Drainage area plans 114373-500, 114373-501 and the storm sewer design sheet for this project have been included in **Appendix D** as they demonstrate that the whole of the subject lands have been included in the design calculations for the trunk storm sewer recently extended in River Road, the subject lands are identified as drainage area 154 and EXT-1.

It should be noted that during the modelling for the River Road trunk sewers that the subject lands were included in the model with 100 year capture into the minor storm system. Flows in excess of the 100 year event will be provided with an emergency route direct to the Rideau River.

4.4 Summerhill Village Phase 1 (2011 IBI)

Drainage area plan 3766-500A and the storm sewer design sheet for this project have been included in **Appendix D** as they demonstrate that the norther lands have been included in the design calculations for the trunk storm sewer in River Road. The design proposed two connections to River Road.

4.5 Minor Storm Sewer Design Criteria

The minor system storm sewers for the subject site are proposed to be sized based on the rational method, applying standards of both the City of Ottawa and MECP. Some of the key criteria for this site include the following:

Sewer Sizing: Rational Method

Design Return Period: 1:2 year (local streets)

1:5 year (collector streets)

Initial Time of Concentration
 10 minutes

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Manning's: 0.013
Minimum Velocity: 0.80 m/s
Maximum Velocity: 3.00 m/s

PIPE DIAMETER (MM)	SLOPE (%)
250	0.43
300	0.34
375	0.25
450	0.20
525	0.16
600	0.13
675	0.11
750 and larger	0.1

Runoff Coefficients (per ISSU Update, to be confirmed at detailed design stage):

LAND USE		RUNOFF COEFFICIENT
	Low Density	0.65
Residential	Medium Density	0.70
	High Density	0.80
Commercial		0.75
Green Space		0.30
Institutional		0.75
Park		0.20
Transitway		0.82
Arterial Road		0.82
Collector Road		0.82

4.6 Recommended Minor Storm Plan

As noted above the whole of the subject lands have been accounted for in the design and construction of the existing adjacent trunk storm sewer systems. The current approved plans call for 3 separate connections to existing storm sewer systems. A preliminary storm plan is included in **Figure 4.1** in **Appendix D**.

In an effort to reduce disruptions to River Road and cost, the detailed design phase will likely include an analysis to explore the possibility of eliminating the northernmost storm connection for the northern section of lands. A preliminary storm plan demonstrating this concept is also included in **Figure 4.1A** in **Appendix D**.

Some of the storm sewers recommended to service the Rideau River Area are subject to cost sharing as noted in the Draft 2013 Development Changes Study Report Update. For reference a copy of a relevant portion of Table F-2, Stormwater Services South, and Figure STM 4, Riverside South Storm Sewers are included in **Appendix D**. The report identified the larger storm sewers in the Riverside South Community including the River Road Area and the subject site.

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4.7 Dual Drainage

Development of the subject site will include a stormwater strategy using the dual drainage system. The system features a combination of on-site detention (surface ponding) with inlet control devices (ICDs) and direct conveyance with no ponding. It accommodates both minor and major stormwater runoff. During frequent storms the effective runoff collected by catchment areas is directly released via catch basin inlets into the network of storm sewers, called the minor system. During less frequent storms, the balance of the flow (in excess of the minor flow) is accommodated by a system of rear yard swales and street segments (or other forms of underground storage or surface storage such as dry ponds). The main advantage of this arrangement is its ability to adjust the rate of total inflow into the minor system to satisfy the required level of service. The required total inflow is typically maintained by the restriction of the capacity and the density of the inlets directly connected into this system. As noted, during less frequent storms, the balance of the flow is accommodated by the major system. Typically, this accommodation is achieved by the attenuation on catchment surfaces called on-site detention and/or direct conveyance of the flow to a recipient.

River Road, a collector road with a rural cross-section, is a constraint with respect to conveyance of major flow across the road's surface. Specifically, as a collector road, there should be no cross flow during events up to the 100 year event.

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5 EROSION AND SEDIMENTATION CONTROL PLAN

During construction, existing conveyance systems and water courses can be exposed to sediment loading. Development of a subdivision such as this project can potentially create deleterious material which can enter the natural environment and gain access to fish and amphibian habitat. In order to prevent site generated sediments from entering the environment, an Erosion and Sedimentation Control Plan (ESCD) will be implemented prior to development. Although a generic ESCP can be developed as part of this report and subsequent Design Briefs, the final plan will be developed and implemented by the Owner's general contractor.

The erosion and sedimentation control strategy for the subject site could include erection of silt fences, straw bale barriers and rock check dams. These measures will ensure protection of both adjacent developments and the natural environment adjacent to and downstream of the site.

A copy of a potential Erosion and Sedimentation Control Plan (ESCP) is shown on **Figure 5.1**, which is included in **Appendix E**.

Other elements of an ESCP could also include installation of bulkhead barriers at the nearest existing downstream manholes to ensure deleterious material does not gain access to those sewers and potentially the Riverside South Pump Station and/or Pond 5. Also, the final ESCP will incorporate features to deal with disposal of any taken water. Some of the features or general requirements are sometimes conditions of a Permit To Take Water.

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6 APPROVALS AND PERMIT REQUIREMENTS

6.1 City of Ottawa

The City of Ottawa will review all development documents including final working drawings and related reports. Upon completion, the City will approve the local watermains, under Permit No. 008-202; submit the sewer extension MECP application to the province and eventually issue a Commence Work Notification.

6.2 Province of Ontario

The Ministry of Environment, Conservation and Parks (MECP) will approve the local sewers under Section 53 of the Ontario Water Resources Act and issue an Environmental Compliance Approval. A Permit To Take Water may also need to be issued by the MECP.

6.3 Conservation Authority

At this time it is understood that there are no required permits, authorizations or approvals needed expressly for this development from the Conservation Authority; however, this will be confirmed through a subsequent pre-consultation with the RVCA.

6.4 Federal Government

At this time it is understood that there are no required permits, authorizations or approvals needed expressly for this development from the Federal Government; however, this will be confirmed through subsequent consultation with Parks Canada as a minimum.

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7 CONCLUSIONS AND RECOMMENDATIONS

7.1 Conclusion

All infrastructure which is needed to help service the subject site already exists. The development plan will include connections to the infrastructure to adequately service the site with water supply, wastewater collection and disposal and management of stormwater runoff. The extension of the existing watermains through the subject site will provide a reliable source of both drinking water and fire flows. The ultimate wastewater outlets are already in place. A new stormwater management facility, Pond 5, is currently under construction and once completed will provide the necessary treatment for runoff from the subject site. Development of the subject property will include the recommended storm sewer plan. Therefore, there are suitable public services in place to service the subject site.

7.2 Recommendation

From an assessment of major municipal infrastructure perspective, it is recommended that the development application for the Urbandale property known as Riverside South Phase 12 be accepted and that the development of the property move forward.



Lance Erion, P. Eng. Associate

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APPENDIX A

Development Servicing Study Checklist

The following table is a customized copy of the current City of Ottawa's Development Servicing Study Checklist. It is meant to be a quick reference for location of each of the items included on the list. The list contains the various item description and the study section in which the topic is contained.

GENERAL CONTENT

	ITEM DESCRIPTION	LOCATION
	Executive Summary (for larger reports only)	N/A
$\sqrt{}$	Date and revision number of the report	Front Cover
~	Location Map and plan showing municipal address, boundary, and layout of proposed development.	Figure 1.1
$\sqrt{}$	Plan showing the site and location of all existing services.	Figure 1.3
~	Development statistics, land use, density, adherence to zoning and official plan, and reference to applicable subwatershed and watershed plans that provide context to which individual developments must adhere.	Section 2.2, 3.2, 3.3, 4.3 Figure 1.1
$\sqrt{}$	Summary of Pre-consultation Meeting with City and other approval agencies.	Section 1.6
√	Reference and confirm conformance to higher level studies and reports (Master Servicing Studies, Environmental Assessments, Community Design Plans), or in the case where it is not in conformance, the proponent must provide justification and develop a defendable design criteria.	Sections 1.3, 2.2, 3.2
1	Statement of objectives and servicing criteria	Section 1.1, 2.2.3, 3.3 & 4.3
1	Identification of existing and proposed infrastructure available in the immediate area.	Figure 1.3
V	Identification of Environmentally Significant Areas, Watercourses and Municipal Drains potentially impacted by the proposed development (Reference can be made to the Natural Heritage Studies, if available).	Sections 1.9
√	Concept level master grading plan to confirm existing and proposed grades in the development. This is required to confirm the feasibility of proposed stormwater management and drainage, soil removal and fill constraints, and potential impacts to neighbouring properties. This is also required to confirm that the proposed grading will not impede existing major system flow paths.	Section 1.8 Detail Design
V	Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts.	N/A
	Proposed phasing of the development, if applicable.	N/A
$\sqrt{}$	Reference to geotechnical studies and recommendations concerning servicing.	Section 1.8

V	All preliminary and formal site plan submissions should have the	
'	following information:	
	Metric scale	
	North arrow (including construction North)	
	Key plan	N1.4. J
	Name and contact information of applicant and property owner	Noted
	Property limits including bearings and dimensions	
	Existing and proposed structures and parking areas	
	Easements, road widening and rights-of-way	
	Adjacent street names	

DEVELOPMENT SERVICING REPORT: WATER

	ITEM DESCRIPTION	LOCATION
	Confirm consistency with Master Servicing Study, if available	Section 2.2
	Availability of public infrastructure to service proposed development	Section 2.1
	Identification of system constraints – external water needed	Sections 2.2
	Identify boundary conditions	N/A
$\sqrt{}$	Confirmation of adequate domestic supply and pressure	Section 2.3 & Appendix B
V	Confirmation of adequate fire flow protection and confirmation that fire flow is calculated as per the Fire Underwriter's Survey. Output should show available fire flow at locations throughout the development.	Section 2.2
1	Provide a check of high pressures. If pressure is found to be high, an assessment is required to confirm the application of pressure reducing valves.	Section 2.2 Appendix B
	Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defining phases of the project including the ultimate design.	Section 2.4
	Address reliability requirements such as appropriate location of shut-off valves.	Detail Design
	Check on the necessity of a pressure zone boundary modification.	N/A
V	Reference to water supply analysis to show that major infrastructure is capable of delivering sufficient water for the proposed land use. This includes data that shows that the expected demands under average day, peak hour and fire flow conditions provide water within the required pressure range.	Section 2.2
V	Description of the proposed water distribution network, including locations of proposed connections to the existing system, provisions for necessary looping, and appurtenances (valves, pressure reducing valves, valve chambers, and fire hydrants) including special metering provisions.	Detail Design
V	Description of off-site required feedermains, booster pumping stations, and other water infrastructure that will be ultimately required to service proposed development, including financing, interim facilities and timing of implementation.	N/A
V	Confirmation that water demands are calculated based on the City of Ottawa Design Guidelines.	Section 2.3
V	Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference.	Detailed Design

DEVELOPMENT SERVICING REPORT: WASTEWATER

ITEM DESCRIPTION	LOCATION
√ Summary of proposed design criteria (Note: Wet-weather flow crishould not deviate from the City of Ottawa Sewer Design Guideli Monitored flow data from relatively new infrastructure cannot be use justify capacity requirements for proposed infrastructure).	lines. ed to Section 3.3
√ Confirm consistency with Master Servicing Study and/or justification deviations.	Section 3.2
√ Consideration of local conditions that may contribute to extraneous flethat are higher than the recommended flows in the guidelines. includes groundwater and soil conditions, and age condition of sew	This Detail Design vers.
√ Description of existing sanitary sewer available for discharge wastewater from proposed development.	le of Section 3.2, Appendix C
√ Verify available capacity in downstream sanitary sewer an identification of upgrades necessary to service the propodevelopment. (Reference can be made to previously completed Ma Servicing Study if applicable)	osed Section 3.1, 3.2, aster 3.4
Calculations related to dry-weather and wet-weather flow rates from development in standard MOE sanitary sewer design table (Appe "C") format.	endix Detail Design
$\sqrt{}$ Description of proposed sewer network including sewers, pum stations and forcemains.	Figure 3.1 in Appendix C
Discussion of previously identified environmental constraints and im on servicing (environmental constraints are related to limitat imposed on the development in order to preserve the physical cond of watercourses, vegetation, soil cover, as well as protecting aga water quantity and quality).	itions dition Section 1.9
√ Pumping stations: impacts of proposed development on exist pumping stations or requirements for new pumping station to ser development.	ervice Section 3.1
√ Forcemain capacity in terms of operational redundancy, surge present and maximum flow velocity.	IN/A
√ Identification and implementation of the emergency overflow sanitary pumping stations in relation to the hydraulic grade line to proagainst basement flooding.	
$\sqrt{}$ Special considerations such as contamination, corrosive environmetc.	ment Detail Design

DEVELOPMENT SERVICING REPORT: STORMWATER CHECKLIST

	ITEM DESCRIPTION	LOCATION
1	Description of drainage outlets and downstream constraints including legality of outlets (i.e. municipal drain, right-of-way, watercourse, or private property)	Section 4.1, 4.4 Appendix D
1	Analysis of available capacity in existing public infrastructure.	Section 4.1, 4.4,
1	A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns, and proposed drainage pattern.	Section 1.7, Figure 1.4 in Appendix A

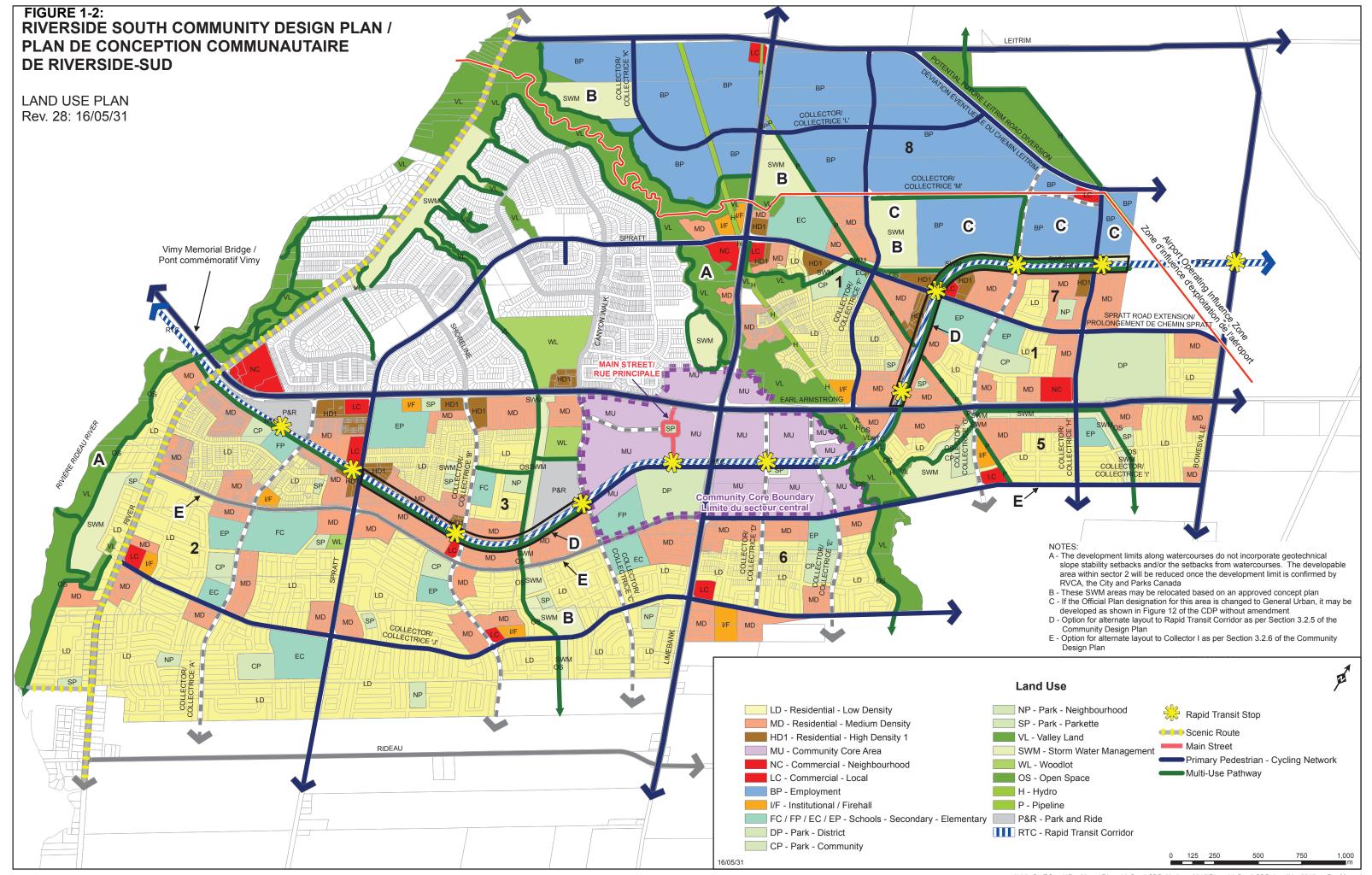
V	Water quantity control objective (e.g. controlling post-development peak flows to pre-development level for storm events ranging from the 2 or 5 year event (dependent on the receiving sewer design) to 100 year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects.	Section 4.5
√ 	Water quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements.	Section 4.5
V	Description of the stormwater management concept with facility locations and descriptions with references and supporting information.	Section 4.3, 4.4, 4.5
	Set-back from private sewage disposal systems.	N/A
$\sqrt{}$	Watercourse and hazard lands setbacks.	Section 1.9, 4.8
V	Record of pre-consultation with the Ontario Ministry of Environment and the Conservation Authority that has jurisdiction on the affected watershed.	Section 1.6
$\sqrt{}$	Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists.	Section 4.2
V	Storage requirements (complete with calculations) and conveyance capacity for minor events (1:5 year return period) and major events (1:100 year return period).	Section 4.5 Detail Design
V	Identification of watercourses within the proposed development and how watercourses will be protected, or, if necessary, altered by the proposed development with applicable approvals.	Section 1.9, 4.8
	Calculate pre and post development peak flow rates including a description of existing site conditions and proposed impervious areas and drainage catchments in comparison to existing conditions.	Detail Design
$\sqrt{}$	Any proposed diversion of drainage catchment areas from one outlet to another.	Section 1.7, 4.4
$\sqrt{}$	Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and stormwater management facilities.	Section 4.2, 4.4, Appendix D
	If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post-development flows up to and including the 100-year return period storm event.	N/A
	Identification of potential impacts to receiving watercourses	N/A
	Identification of municipal drains and related approval requirements.	Section 1.9
√	Descriptions of how the conveyance and storage capacity will be achieved for the development.	Section 4.5 Detail Design
√ √	100 year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading.	Section 4.5 Detail Design
	Inclusion of hydraulic analysis including hydraulic grade line elevations.	Section 4.6
√	Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors.	Section 5
\	Identification of floodplains – proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions.	N/A
V	Identification of fill constraints related to floodplain and geotechnical investigation.	Section 1.8,

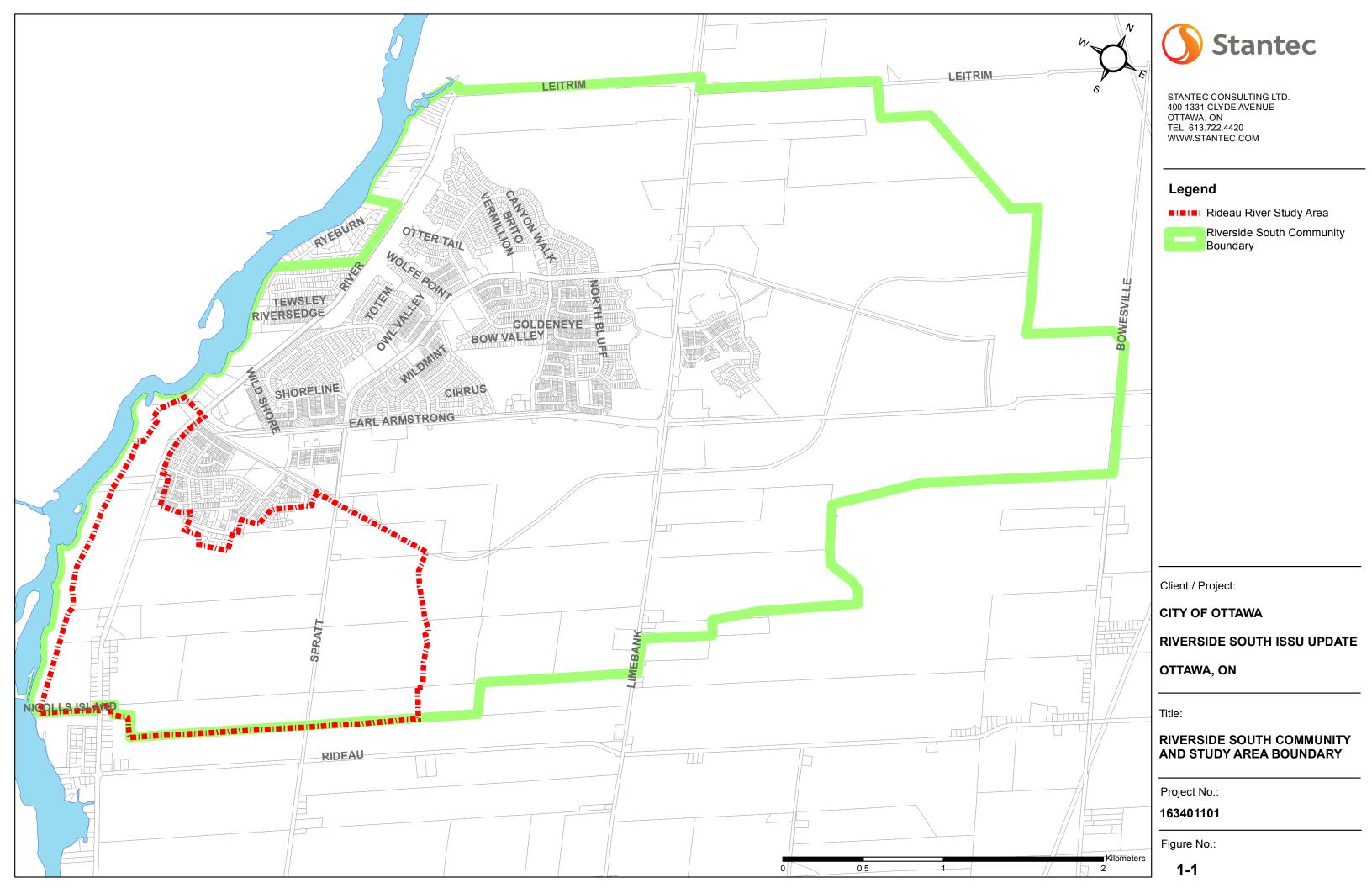
APPROVAL AND PERMIT REQUIREMENTS: CHECKLIST

ITEM DESCRIPTION		LOCATION
V	Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act.	Section 1.6, 1.9
	Application for Certification of Approval (CofA) under the Ontario Water	Section 1.6
	resources Act.	Detail Design
	Changes to Municipal Drains	N/A
1	Other permits (National Capital Commission, Parks Canada, Public Works and Government Services Canada, Ministry of Transportation etc.)	Section 6

CONCLUSION CHECKLIST

	ITEM DESCRIPTION	LOCATION
	Clearly stated conclusions and recommendations	Section 7.1 & 7.2
	Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency.	Detail Design
$\sqrt{}$	All draft and final reports shall be signed and stamped by professional Engineer registered in Ontario.	Completed





Riverside South Community Infrastructure Servicing Study Update – Rideau River Area Introduction June 9, 2017

Revision 28 of the Riverside South Community Design Plan (CDP) (Bousfields, May 2016) was approved by the City of Ottawa Council in June 2016. The current Riverside South Community Infrastructure Servicing Study Update (Stantec, June 2017) is completed to reflect the CDP and Master Drainage Plan (MDP). The CDP Land Use Plan is shown in **Figure 1-2**.

1.3 PREVIOUS RELEVANT STUDIES

The following, previously completed, studies and design briefs were considered in the completed analyses.

1.3.1 Master Drainage Studies

- <u>"South Urban Community Drainage Planning Study"</u> (UMA Engineering Ltd. and Golder Associates, May 1990)
- <u>"City of Gloucester South Urban Community Master Drainage Plan"</u> (Gore & Storrie, July 1992)
- <u>"Riverside South Community Master Drainage Plan Update Final Report"</u> (Stantec Consulting Ltd., September 2008)
- <u>"Riverside South Community Master Drainage Plan Update Rideau River Study Area Final Report"</u> (Stantec Consulting LTD., March 2016)

1.3.2 Master Servicing Studies

- "Riverside South Master Servicing Study" (Stantec Consulting Ltd., September 2008)
- <u>"South Urban Community River Ridge Master Infrastructure Plan"</u> (Ainley Graham and Associates, December 1994)

Pressure Zones Infrastructure Assessment" (Stantec Consulting, 2002)

"Water Master Plan" (Stantec Consulting, 2013)

1.3.3 Sanitary Studies

- "South Urban Community Master Water and Sanitary Sewage Study" (Gore & Storrie, 1992)
- "South Urban Community Rideau River Crossing Facilities Phase" (Gore & Storrie, 1995)
- "Wastewater Master Plan" (RMOC, July 1997)
- "Wastewater IMP" (Stantec, 2013)



Riverside South Community Infrastructure Servicing Study Update - Rideau River Area Introduction June 9, 2017

1.3.4 Design Briefs/Reports

<u>"Design Report - Riverside South Development Corporation - Riverside South Community Phase 9"</u> (J.L. Richards & Associates Limited, December 2011)

"Riverside South Elevated Water Storage Rank Class Environmental Assessment" (Stantec, 2014)

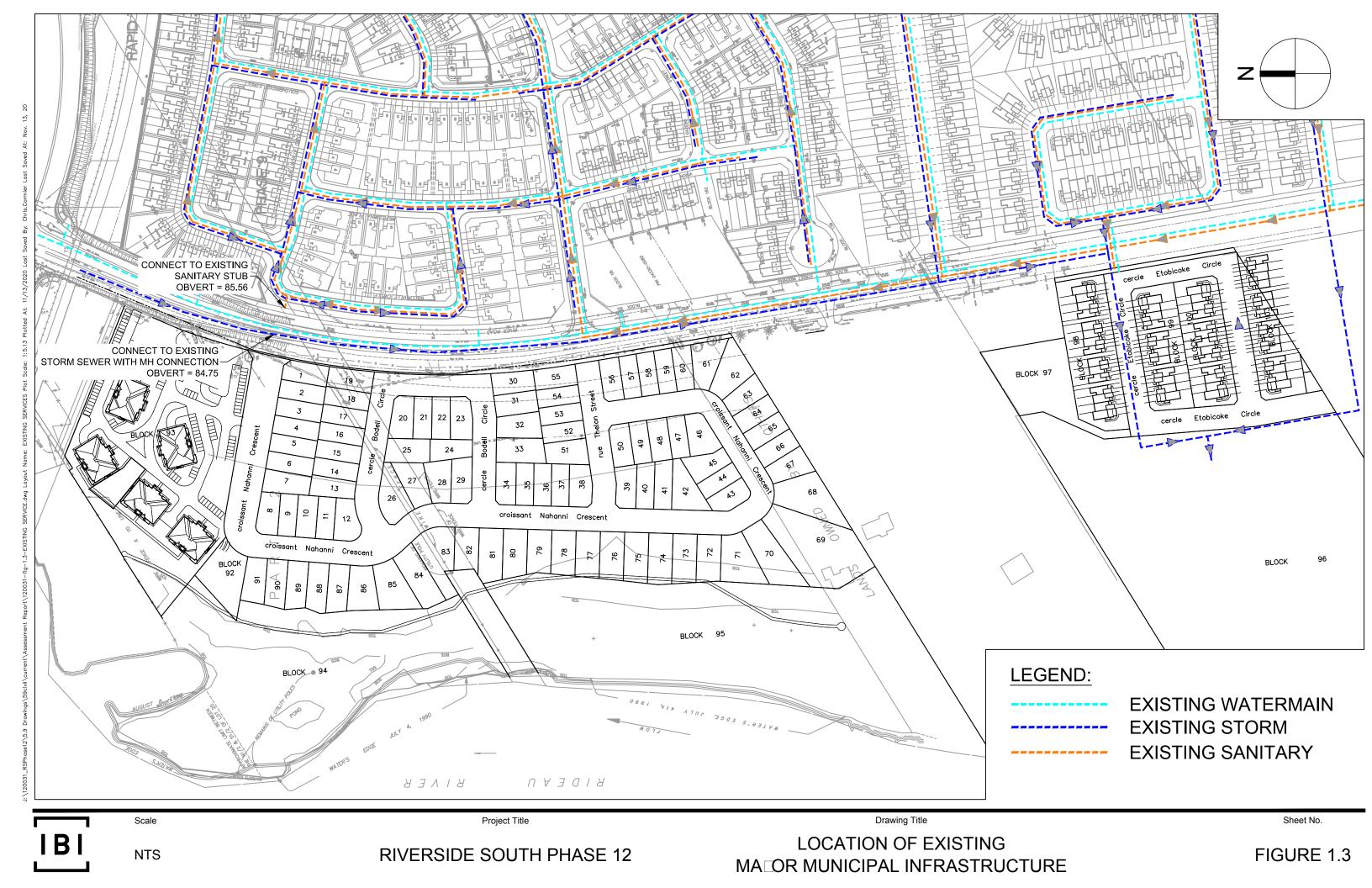


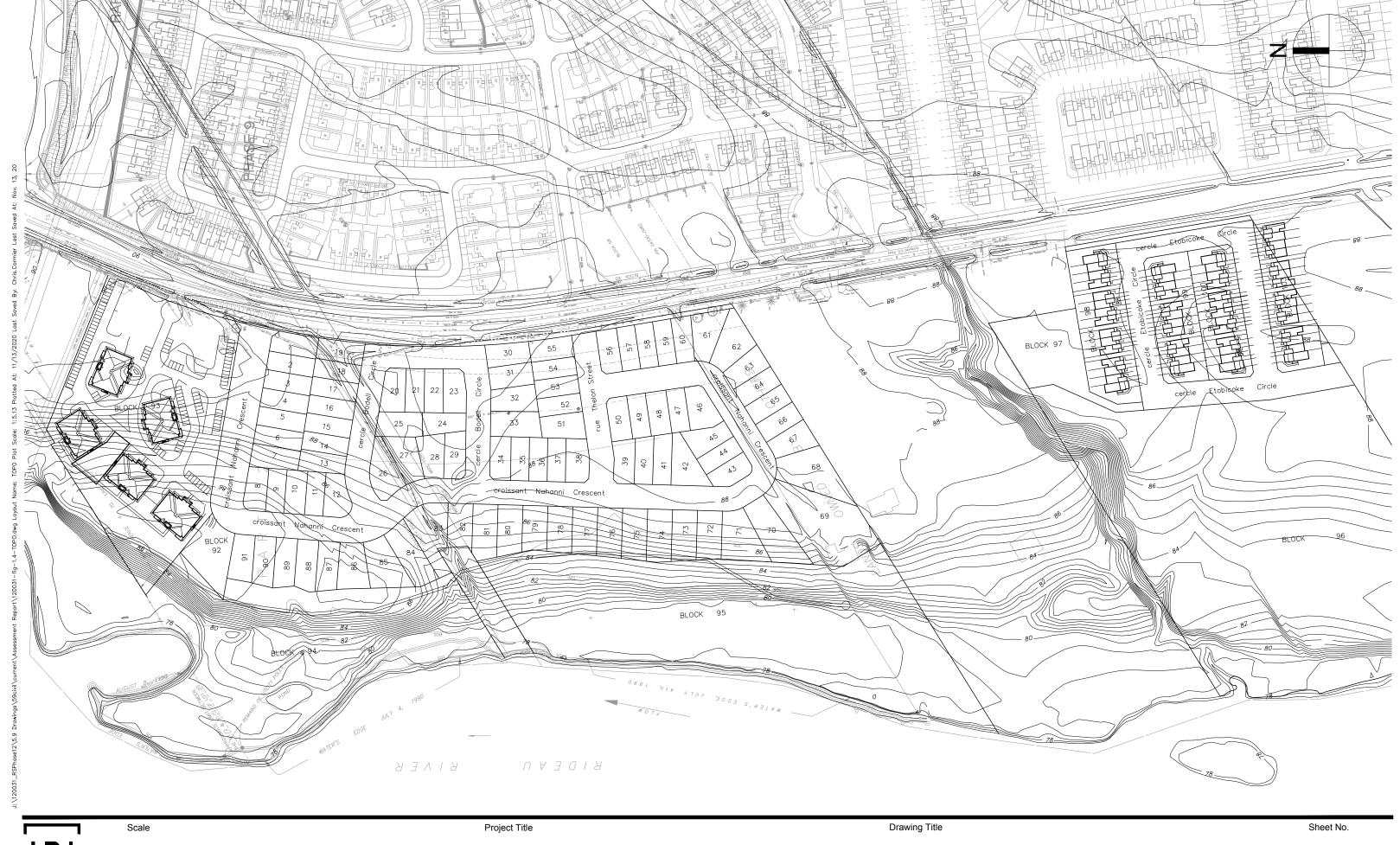


Drawing Title

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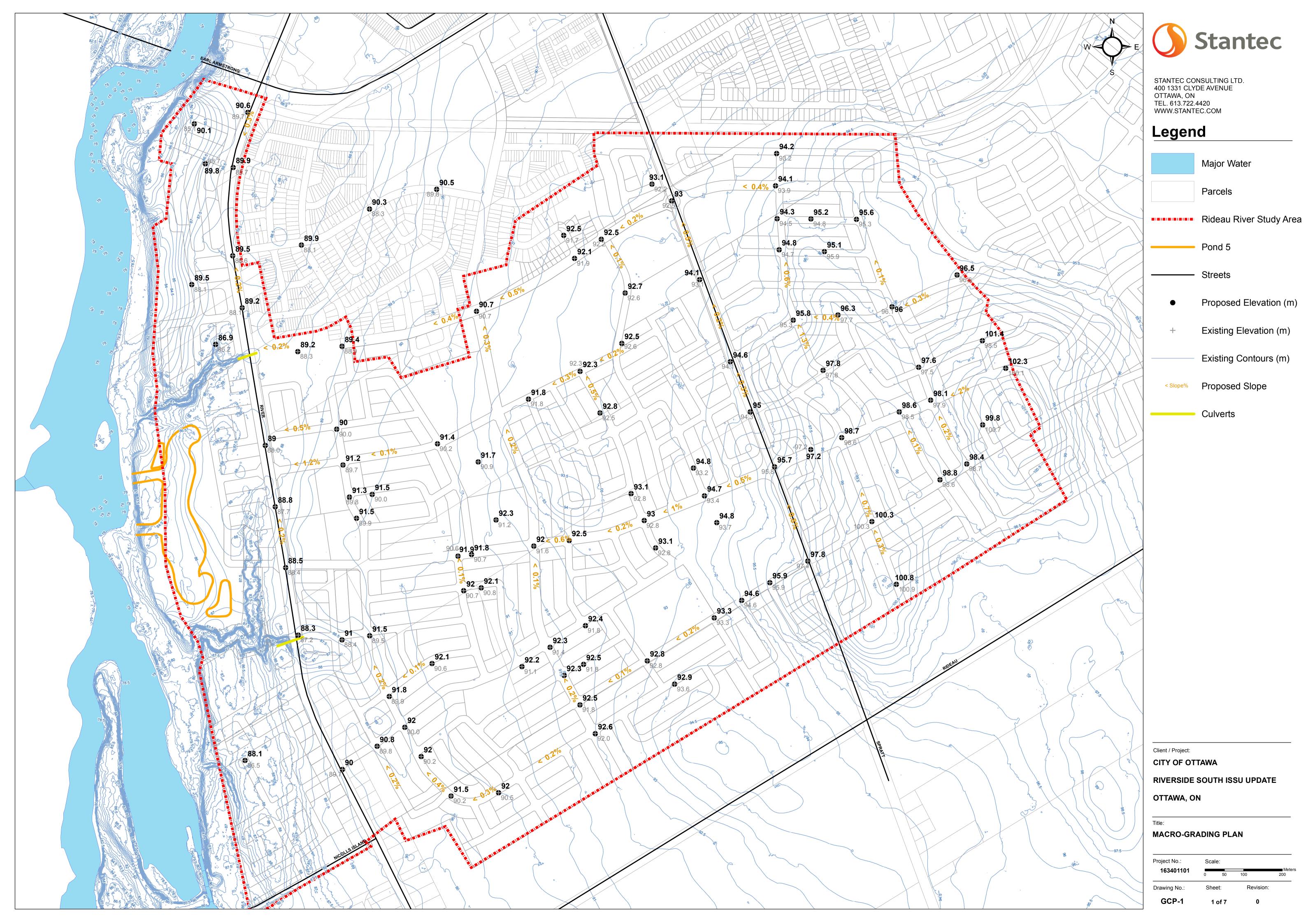
Scale Project Title Drawing Title Sheet No.

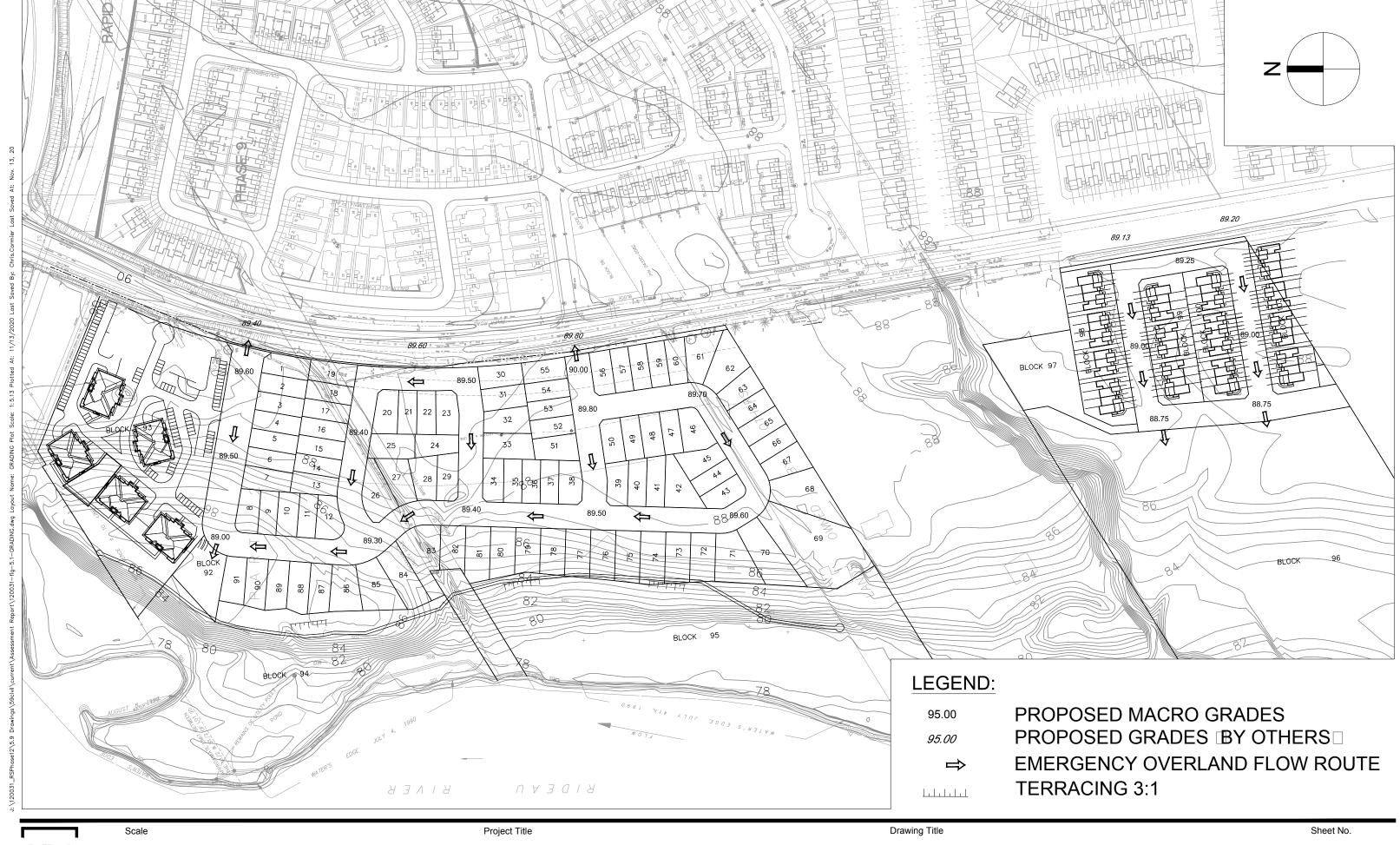


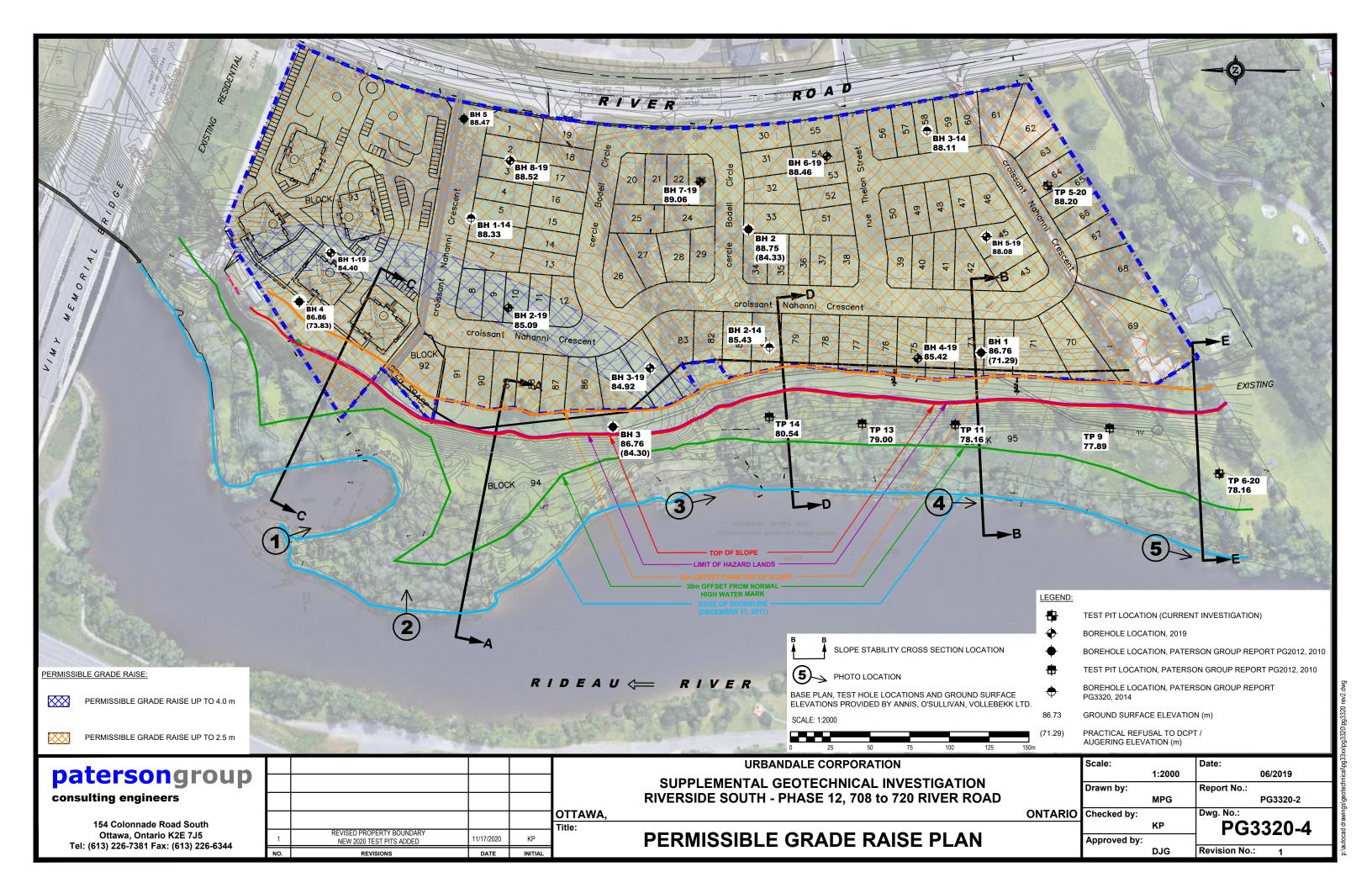


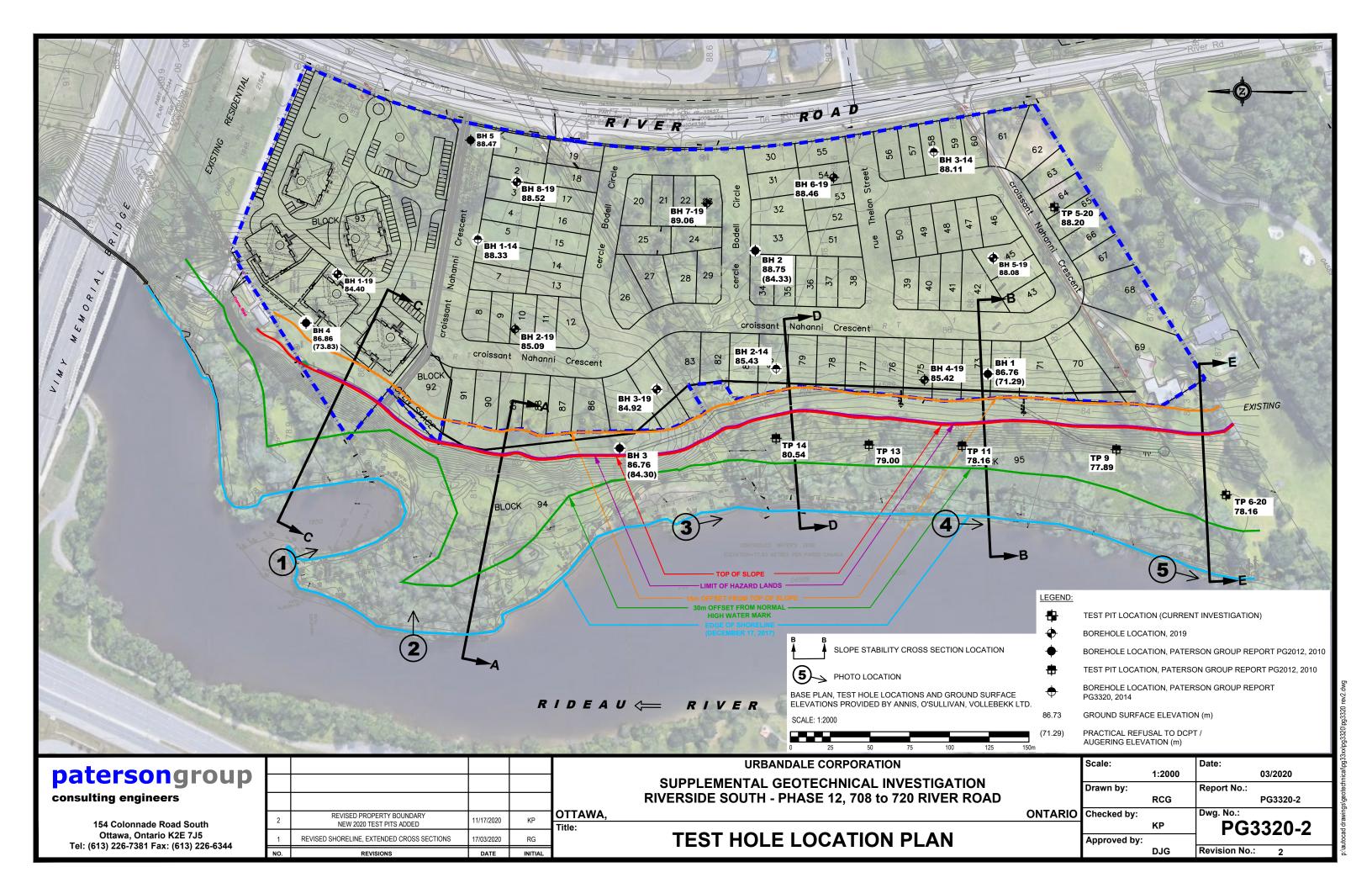
RIVERSIDE SOUTH PHASE 12

FIGURE 1.4











MEMO

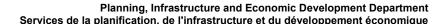
Date:

To / Destinataire	Sean Moore, Planner	
From / Expéditeur	Natasha Baird, Project Manager, Infrastructure Approvals	
Subject / Objet	Pre-Application Consultation 708 River Road, Ward 22	File No. PC2018-0225

Please note the following information regarding the engineering design submission for the above noted site:

- 1. The Servicing Study Guidelines for Development Applications are available at the following address: http://ottawa.ca/en/development-application-review-process-0/servicing-study-guidelines-development-applications
- 2. Servicing and site works shall be in accordance with the following documents:
 - ⇒ Ottawa Sewer Design Guidelines (October 2012)
 - ⇒ Ottawa Design Guidelines Water Distribution (2010)
 - ⇒ Geotechnical Investigation and Reporting Guidelines for Development Applications in the City of Ottawa (2007)

 - ⇒ City of Ottawa Environmental Noise Control Guidelines (January, 2016)
 - ⇒ City of Ottawa Park and Pathway Development Manual (2012)
 - ⇒ City of Ottawa Accessibility Design Standards (2012)
 - ⇒ Ottawa Standard Tender Documents (latest version)
 - ⇒ Ontario Provincial Standards for Roads & Public Works (2013)





- 3. Record drawings and utility plans are also available for purchase from the City (Contact the City's Information Centre by email at lnformationCentre@ottawa.ca or by phone at (613) 580-2424 x.44455).
- 4. The servicing (stormwater, sanitary and water), for the subject lands, is to be based on the Riverside South Community Infrastructure Servicing Study Update – Rideau River Area (June 2017) and the Riverside South Community Master Drainage Plan Update – Rideau River Study Area (March 2016).
- 5. The development will not be permitted until Pond 5 is constructed and has an approved outlet, the sanitary sewer and watermain are extended to 750 River Road.
- 6. Water Boundary condition requests must include the location of the service and the expected loads required by the proposed development. Please provide the following information:
 - Location of service
 - ii. Type of development and the amount of fire flow required (as per FUS, 1999).
 - iii. Average daily demand: ___ l/s.
 - iv. Maximum daily demand: ____l/s.
 - v. Maximum hourly daily demand: ____ l/s.
- 7. Phase 1 ESAs and Phase 2 ESAs must conform to clause 4.8.4 of the Official Plan that requires that development applications conform to Ontario Regulation 153/04.
- 8. This area has a grade raise restriction of 1.8m.
- 9. I will need the following studies and plans:
 - Assessment of Adequacy of Public Services Brief
 - Watermain Analysis
 - Draft Plan of Subdivision

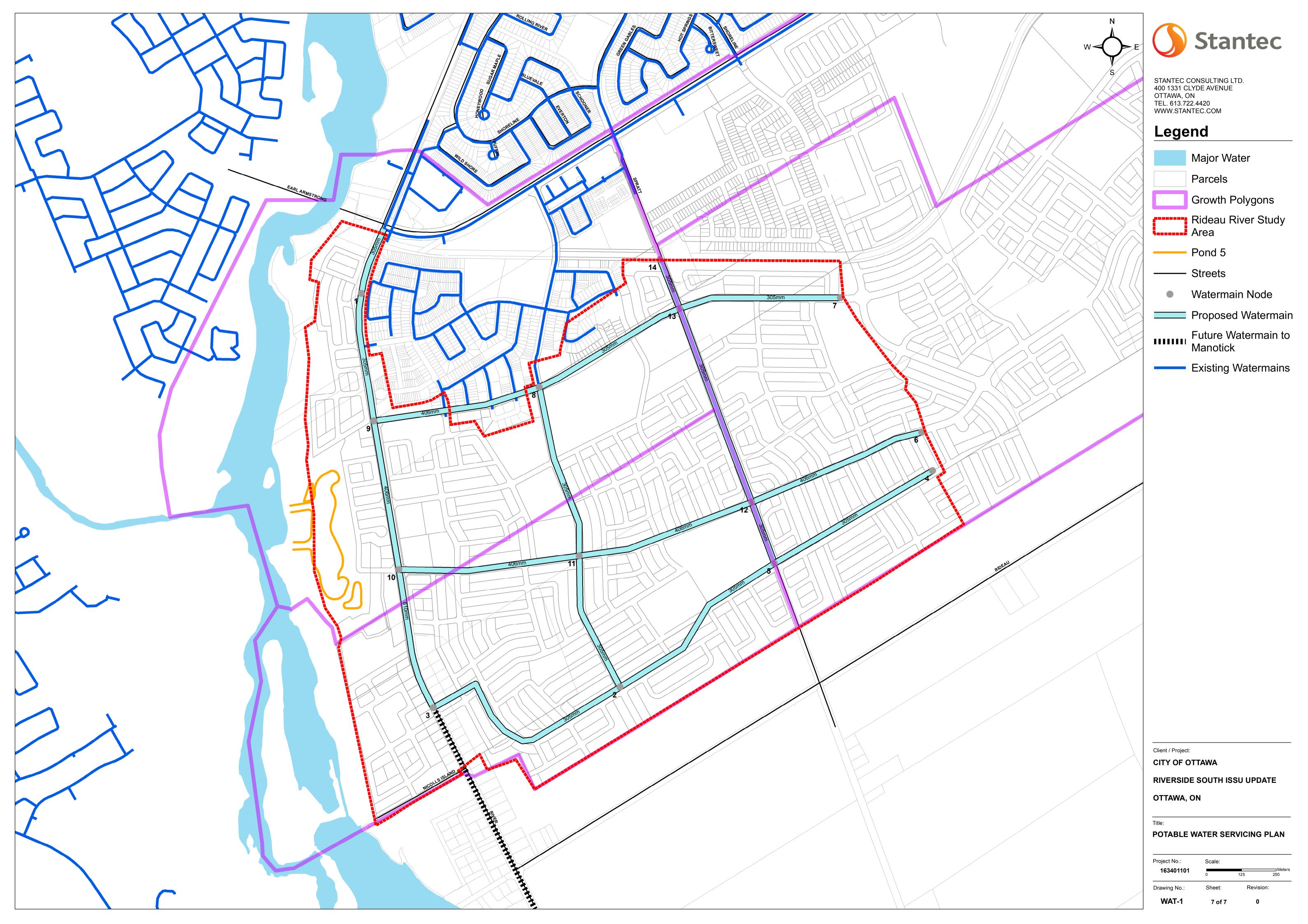


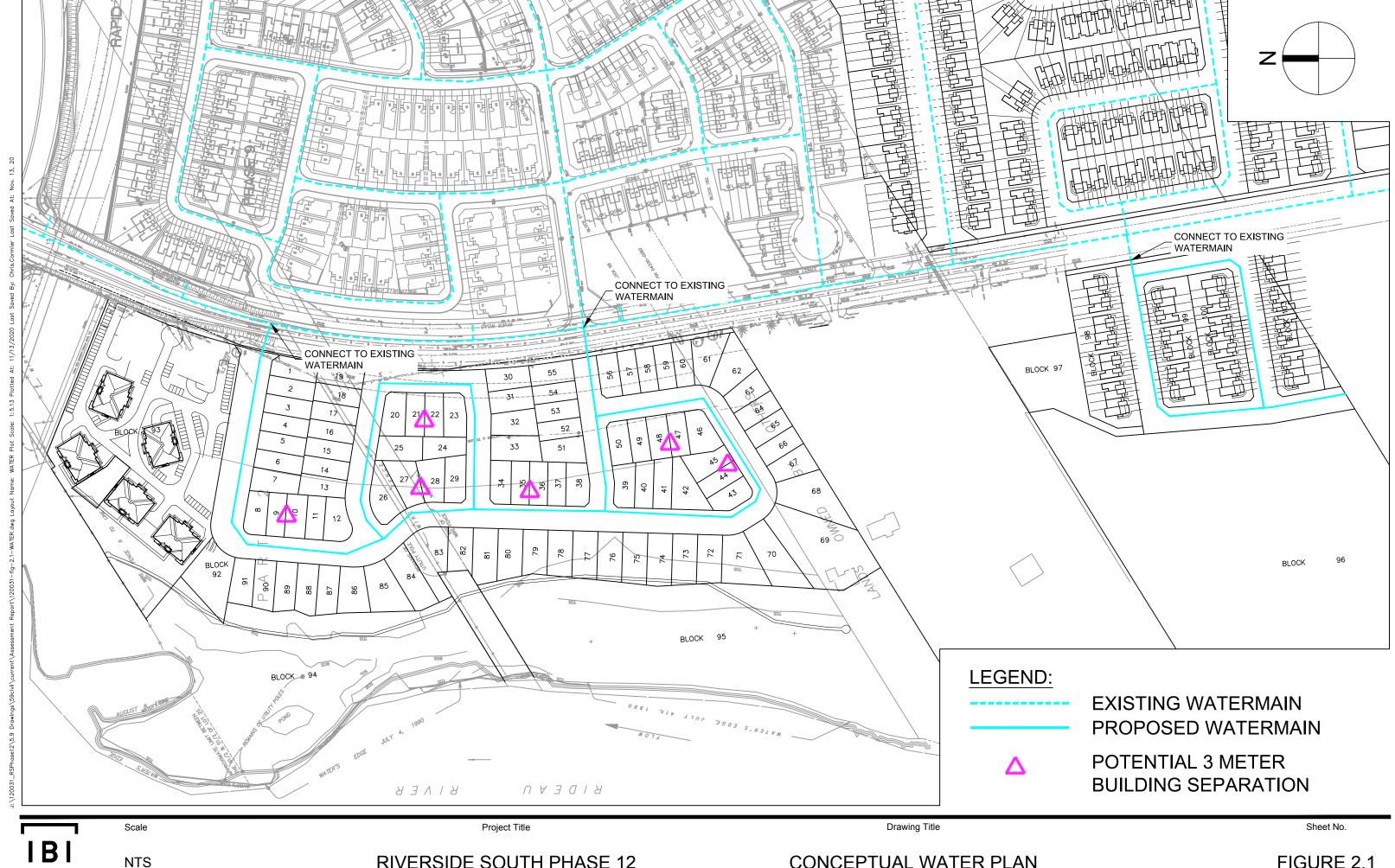
Planning, Infrastructure and Economic Development Department Services de la planification. de l'infrastructure et du développement économique

- geotechnical report
- slope stability analysis

Should you have any questions or require additional information, please contact me directly at (613) 580-2424, 27995 or by email at natasha.baird@ottawa.ca.

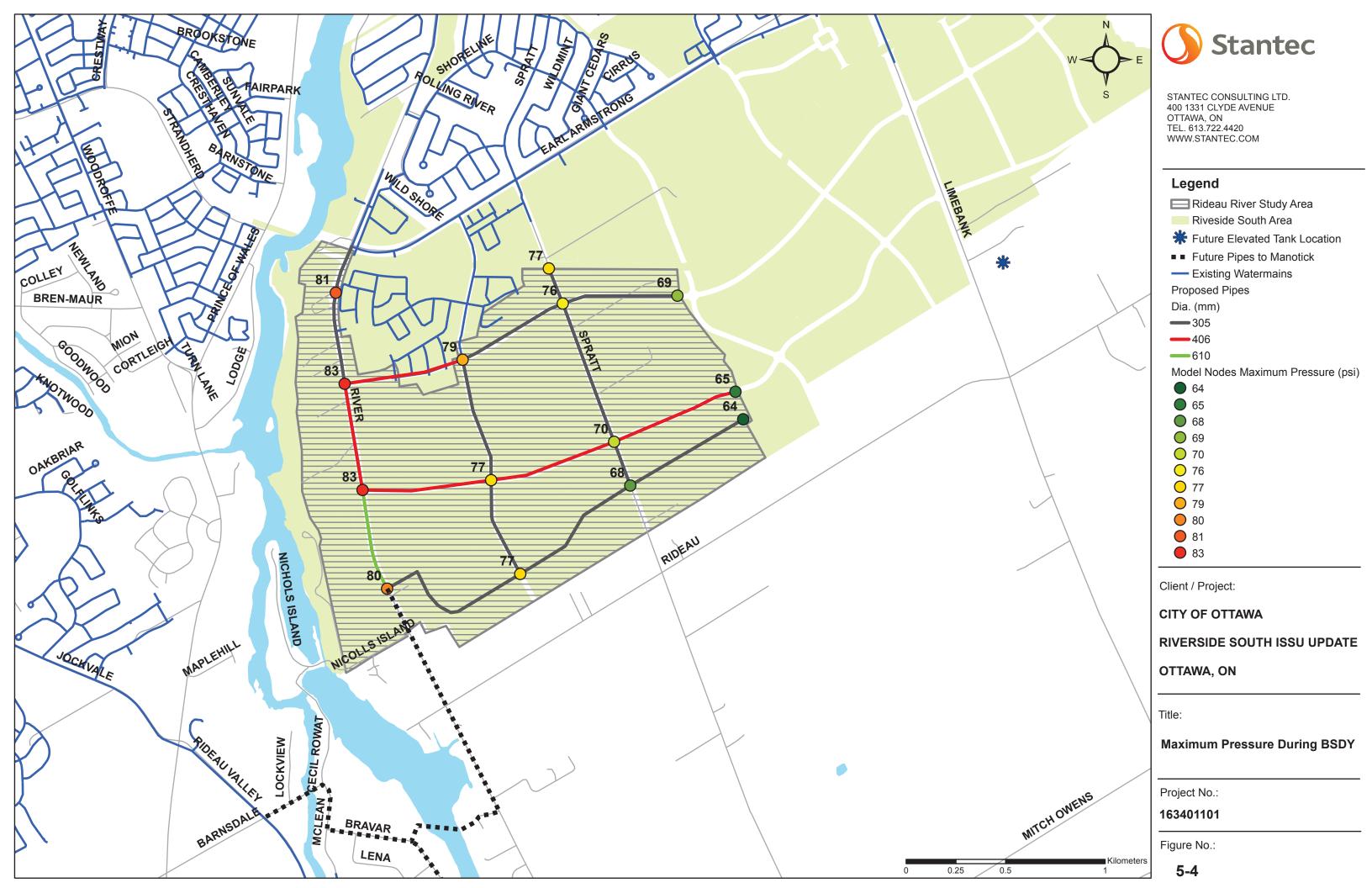






RIVERSIDE SOUTH PHASE 12

CONCEPTUAL WATER PLAN





Boundary Conditions For: Riverside South Phase 15-2 & 760 River Road &4725 Spratt Rd & 4623 Spratt Rd

Date of Boundary Conditions: 2018-Dec-06

Provided Information:

Scenario	Demand	
	L/min	L/s
Average Daily Demand	991.8	16.53
Maximum Daily Demand	2137.2	35.62
Peak Hour	4498.8	75.0
Fire Flow #1 Demand	10,000	166.7
Fire Flow #2 Demand	12,000	200.0
Fire Flow #3 Demand	15,000	250.0

Number Of Connections: 5

Location:





Location 4263 Spratt Road – Connection 5





Results:

Pre_Configuration

Connection #: 1

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	132.8	61.3
Peak Hour	123.9	48.7
Max Day Plus Fire (10,000) L/min	119.9	42.9
Max Day Plus Fire (12,000) L/min	117.9	40.0
Max Day Plus Fire (15,000) L/min	117.3	38.8

¹Elevation: **89.71 m**

Connection #: 2

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	132.8	60.8
Peak Hour	123.9	48.3
Max Day Plus Fire (10,000) L/min	121.3	44.4
Max Day Plus Fire (12,000) L/min	119.8	42.3
Max Day Plus Fire (15,000) L/min	117.3	38.8

¹Elevation: **90.00 m**



Connection #: 3

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	132.8	59.4
Peak Hour	124.0	46.9
Max Day Plus Fire (10,000) L/min	121.7	43.7
Max Day Plus Fire (12,000) L/min	120.4	41.9
Max Day Plus Fire (15,000) L/min	118.2	38.7

¹Elevation: **99.99 m**

Connection #: 4

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	131.9	58.3
Peak Hour	124.0	45.9
Max Day Plus Fire (10,000) L/min	121.3	41.9
Max Day Plus Fire (12,000) L/min	119.8	39.8
Max Day Plus Fire (15,000) L/min	117.2	36.1

¹Elevation: **91.79 m**

Connection #: 5

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	131.8	57.8
Peak Hour	123.7	45.0
Max Day Plus Fire (10,000) L/min	112.8	29.4
Max Day Plus Fire (12,000) L/min	107.9	22.5

¹Elevation: **92.06 m**



${\bf Post_Configuration}$

Connection #: 1

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	147.8	82.6
Peak Hour	144.6	78.0
Max Day Plus Fire (10,000) L/min	142.6	75.2
Max Day Plus Fire (12,000) L/min	141.3	73.3
Max Day Plus Fire (15,000) L/min	139.0	70.1

¹Elevation: **89.71 m**

Connection #: 2

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	147.8	82.2
Peak Hour	144.6	77.6
Max Day Plus Fire (10,000) L/min	142.9	75.2
Max Day Plus Fire (12,000) L/min	141.7	73.5
Max Day Plus Fire (15,000) L/min	139.6	70.6

¹Elevation: **90.00 m**



Connection #: 3

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	147.8	80.7
Peak Hour	144.6	76.2
Max Day Plus Fire (10,000) L/min	143.4	74.5
Max Day Plus Fire (12,000) L/min	142.3	73.0
Max Day Plus Fire (15,000) L/min	140.6	70.5

¹Elevation: **99.99 m**

Connection #: 4

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	147.8	79.7
Peak Hour	144.6	75.2
Max Day Plus Fire (10,000) L/min	143.2	73.1
Max Day Plus Fire (12,000) L/min	142.0	71.5
Max Day Plus Fire (15,000) L/min	140.0	68.7

¹Elevation: **91.79 m**

Connection #: 5

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	147.8	79.3
Peak Hour	144.6	74.8
Max Day Plus Fire (10,000) L/min	137.7	65.1
Max Day Plus Fire (12,000) L/min	134.5	60.5

¹Elevation: **92.06 m**



Notes:

- 1) As per the Ontario Building Code in areas that may be occupied, the static pressure at any fixture shall not exceed 552 kPa (80 psi.) Pressure control measures to be considered are as follows, in order of preference:
 - a) If possible, systems to be designed to residual pressures of 345 to 552 kPa (50 to 80 psi) in all occupied areas outside of the public right-of-way without special pressure control equipment.
 - b) Pressure reducing valves to be installed immediately downstream of the isolation valve in the home/ building, located downstream of the meter so it is owner maintained.
- 2) Watermains extending from Connection #1 to Connection #2 and watermains extending from Connection #4 to Connection #3 as per connection location figure in this boundary condition must be as per Riverside South Community Infrastructure Servicing Study dated June 21 2017 update.
- 3) 4623 Spratt Road proposed development will require an additional connection if the number of homes exceed 50 units.

Disclaimer

The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation. Fire Flow analysis is a reflection of available flow in the watermain; there may be additional restrictions that occur between the watermain and the hydrant that the model cannot take into account.



IBI GROUP 333 PRESTON STREET OTTAWA, ON K1S 5N4

WATERMAIN DEMAND CALCULATION SHEET

FILE: 120031.5.7

1 OF 1

DATE PRINTED: 12-Nov-20

PAGE:

DESIGN: LE

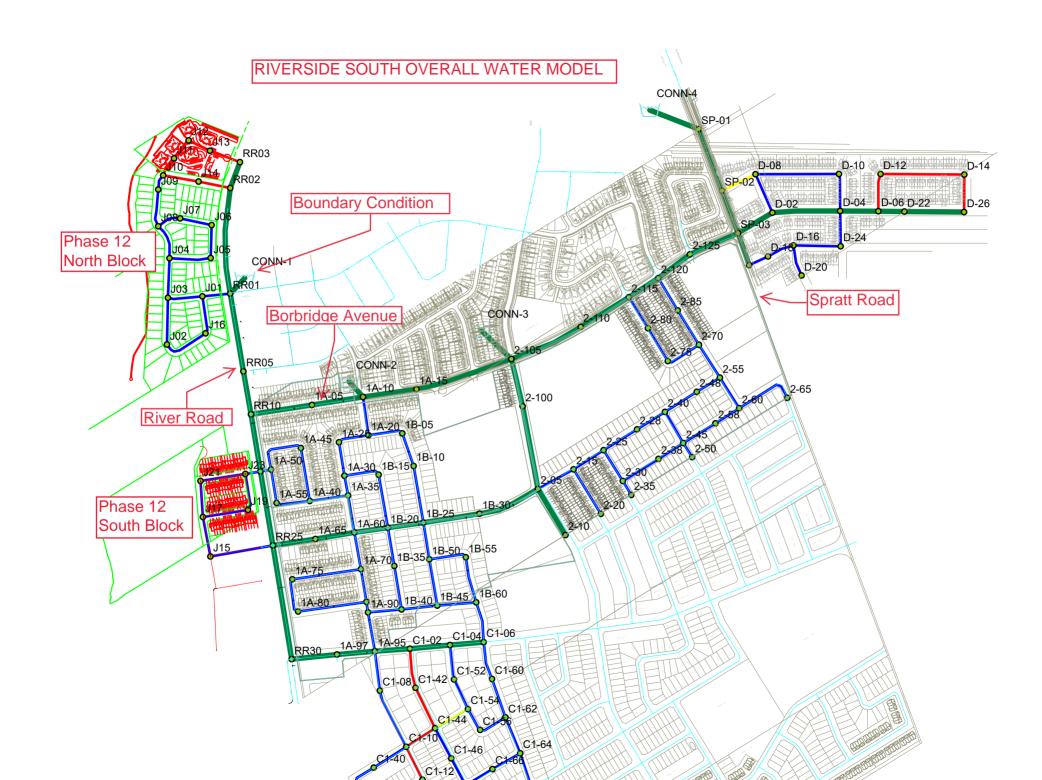
RIVERSIDE SOUTH PHASE 12 CITY OF OTTAWA LOCATION: RIVERSIDE SOUTH DEVELOPMENT CORPORATION

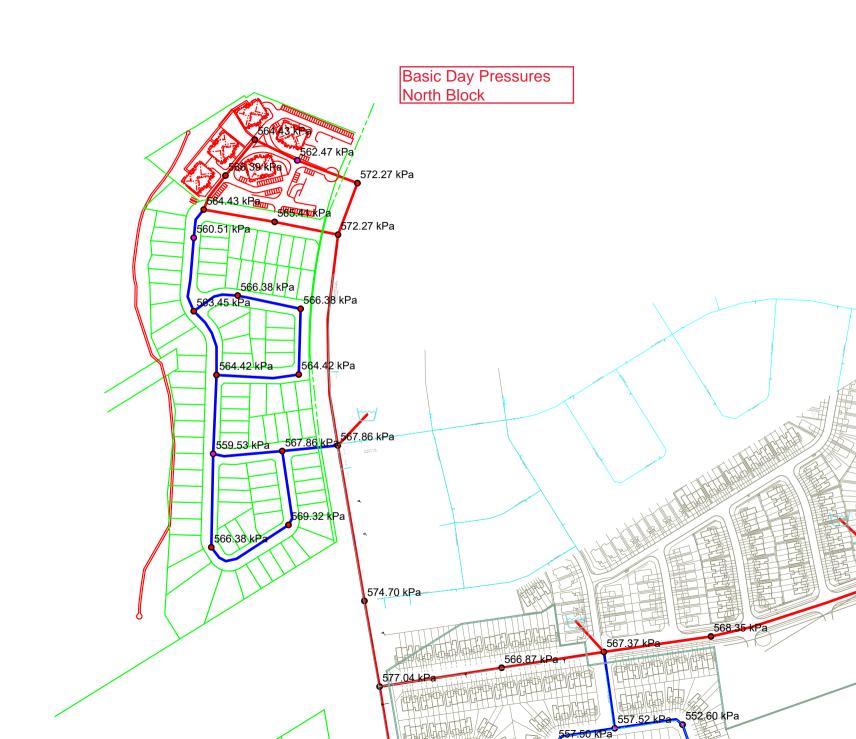
	RESIDENTIAL				NON	-RESIDEN	ITIAL	A۱	/ERAGE D	AILY	MA	XIMUM DA	AILY	MAXIMUM HOURLY			FIRE
NODE		UNITS			INDTRL	COMM.	INST.		DEMAND ((l/s)	D	EMAND (I	/s)	D	EMAND (I	/s)	DEMAND
NOBE	SF	SD & TH	APT	POP'N	(ha.)	(ha.)	(ha.)	Res.	Non-res.	Total	Res.	Non-res.	Total	Res.	Non-res.	Total	(l/min)
RSS Phase 12																	
104	44			37				0.15	0.00	0.45	0.38	0.00	0.00	0.83	0.00	0.00	40.000
J01 J02	11 15			51				0.15	0.00	0.15 0.21	0.38	0.00	0.38	1.14	0.00	0.83	10,000
J02 J03	8			27				0.21	0.00	0.21	0.52	0.00	0.52	0.61	0.00	0.61	10,000
J03	8			27				0.11	0.00	0.11	0.28	0.00	0.28	0.61	0.00	0.61	10,000
J05	7			24				0.10	0.00	0.11	0.24	0.00	0.24	0.53	0.00	0.53	10,000
J06	5			17				0.07	0.00	0.07	0.17	0.00	0.17	0.38	0.00	0.38	10.000
J07	5			17				0.07	0.00	0.07	0.17	0.00	0.17	0.38	0.00	0.38	10,000
J08	9			31				0.12	0.00	0.12	0.31	0.00	0.31	0.68	0.00	0.68	10,000
J09	7			24				0.10	0.00	0.10	0.24	0.00	0.24	0.53	0.00	0.53	10,000
J10	2			7				0.03	0.00	0.03	0.07	0.00	0.07	0.15	0.00	0.15	10,000
J11			36	65				0.26	0.00	0.26	0.66	0.00	0.66	1.44	0.00	1.44	15,000
J12			12	22				0.09	0.00	0.09	0.22	0.00	0.22	0.48	0.00	0.48	15,000
J13			12	22				0.09	0.00	0.09	0.22	0.00	0.22	0.48	0.00	0.48	15,000
J14	6			20				0.08	0.00	0.08	0.21	0.00	0.21	0.45	0.00	0.45	10,000
J16	8			27				0.11	0.00	0.11	0.28	0.00	0.28	0.61	0.00	0.61	10,000
J17		12		32				0.13	0.00	0.13	0.33	0.00	0.33	0.72	0.00	0.72	10,000
J19		15		41				0.16	0.00	0.16	0.41	0.00	0.41	0.90	0.00	0.90	10,000
J21		12		32				0.13	0.00	0.13	0.33	0.00	0.33	0.72	0.00	0.72	10,000
J23		15		41				0.16	0.00	0.16	0.41	0.00	0.41	0.90	0.00	0.90	10,000
Total	01	54	60	563						2.28		-	5.73			12.54	
างเลา	91	54	00	503						2.20		1	5.73			12.54	
	l L													I L			

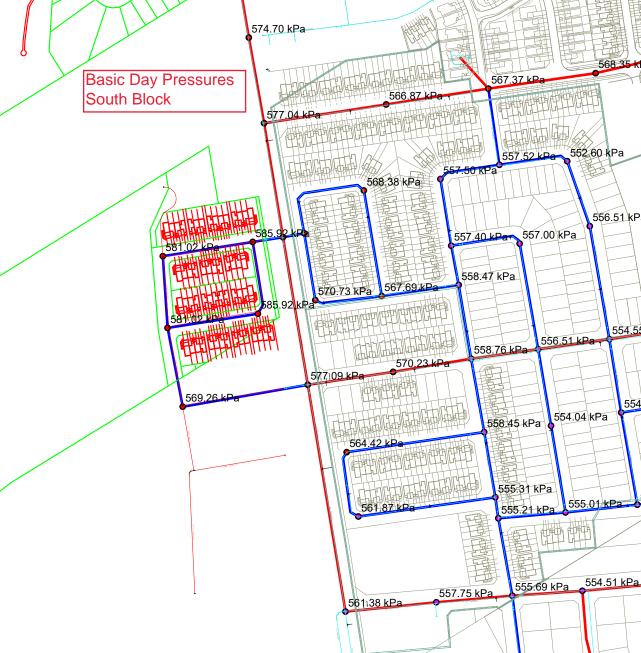
PROJECT:

DEVELOPER:

	ASSUMPTIONS			
RESIDENTIAL DENSITIES	AVG. DAILY DEMAND		MAX. HOURLY DEMAND	
- Single Family (SF)	3.4 p / p / u - Residential	<u>350</u> I / cap / day	- Residential	<u>1,925</u> I / cap / day
	- ICI	<u>50,000</u> I / ha / day	- ICI	<u>135,000</u> I / ha / day
- Semi Detached (SD) & Townhouse (TH)	<u>2.7</u> p/p/u			
			FIRE FLOW	
- Apartment (APT)	1.8 p/p/u MAX. DAILY DEMAND		- SF, SD, TH & ST	10,000 I / min
	- Residential	<u>875</u> l / cap / day	- Back to Back TH	12,000 I / min
-Other	<u>66</u> u / p / ha - ICI	<u>75,000</u> I / ha / day	- ICI/MD	<u>15,000</u> I / min

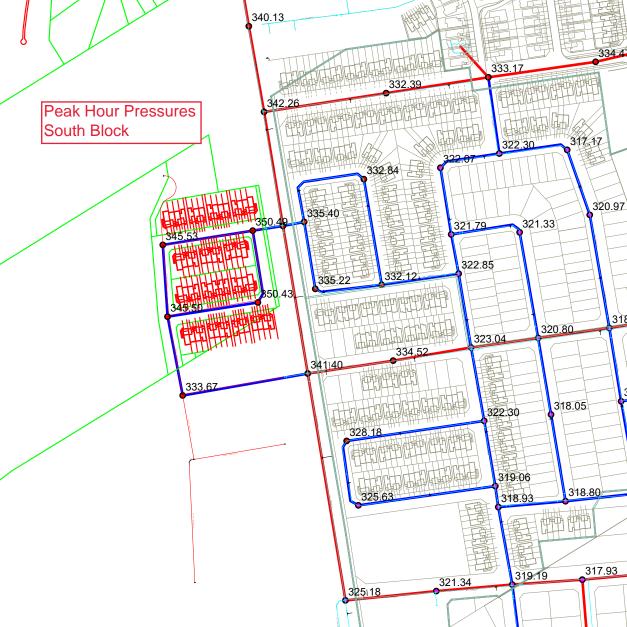






Peak Hour Pressures North Block

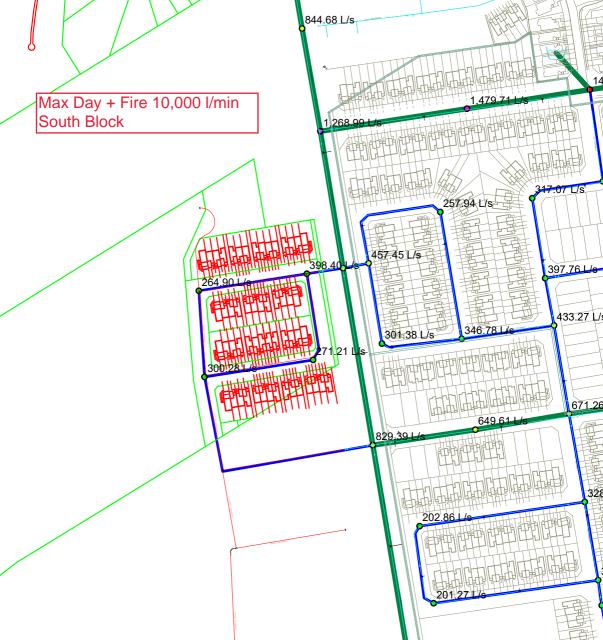






Max Day + Fire 15,000 l/min North Block





		ID	Demand (L/s)	Elevation (m)	Head (m)	Pressure (kPa)	Water Age (hrs)
101		D-08	0.34	93.00	147.79	536.86	0.00
102		D-10	0.40	93.45	147.78	532.43	0.00
103		D-12	0.43	93.85	147.78	528.50	0.00
104		D-14	0.31	95.00	147.78	517.23	0.00
105		D-16	0.27	92.90	147.78	537.83	0.00
106		D-18	0.16	92.80	147.79	538.81	0.00
107		D-20	0.05	92.90	147.78	537.83	0.00
108		D-22	0.19	92.90	147.78	537.81	0.00
109		D-24	0.18	92.90	147.78	537.82	0.00
110		D-26	1.70	95.00	147.78	517.23	0.00
111		J01	0.15	89.85	147.80	567.86	0.00
112		J02	0.17	90.00	147.80	566.38	0.00
113		J03	0.11	90.70	147.80	559.53	0.00
114		J04	0.11	90.20	147.80	564.42	0.00
115		J05	0.10	90.20	147.80	564.42	0.00
116		J06	0.07	90.00	147.80	566.38	0.00
117		J07	0.07	90.00	147.80	566.38	0.00
118		J08	0.12	90.30	147.80	563.45	0.00
119		J09	0.10	90.60	147.80	560.51	0.00
120		J10	0.03	90.20	147.80	564.43	0.00
121	$\overline{\Box}$	J11	0.26	90.00	147.80	566.39	0.00
122		J12	0.09	90.20	147.80	564.43	0.00
123		J13	0.09	90.40	147.80	562.47	0.00
124		J14	0.08	90.10	147.80	565.41	0.00
125	$\overline{\Box}$	J15	0.00	89.70	147.79	569.26	0.00
126		J16	0.60	89.70	147.80	569.32	0.00
127		J17	0.13	88.50	147.79	581.02	0.00
128		J19	0.16	88.00	147.79	585.92	0.00
129		J21	0.13	88.50	147.79	581.02	0.00
130		J23	0.16	88.00	147.79	585.92	0.00
131		RR01	0.00	89.85	147.80	567.86	0.00
132		RR02	0.00	89.40	147.80	572.27	0.00
133		RR03	0.00	89.40	147.80	572.27	0.00
134		RR05	0.00	89.15	147.80	574.70	0.00
135		RR10	0.23	88.91	147.80	577.04	0.00
136		RR15	0.00	89.15	147.79	574.66	0.00
137		RR25	0.08	88.90	147.79	577.09	0.00
138		RR30	0.00	90.50	147.79	561.38	0.00
139		SP-01	0.00	92.55	147.80	541.41	0.00
140		SP-02	0.07	93.20	147.79	534.95	0.00
141		SP-03	0.09	93.00	147.79	536.86	0.00
142		SP-04	1.70	90.87	147.79	557.73	0.00

		ID	Demand (L/s)	Elevation (m)	Head (m)	Pressure (kPa)	Water Age (hrs)
101	П	D-08	1.86	93.00	123.81	301.89	0.00
102	Ħ	D-10	2.23	93.45	123.80	297.36	0.00
103	Ħ	D-12	2.35	93.85	123.79	293.36	0.00
104	Ħ	D-14	1.68	95.00	123.79	282.09	0.00
105	ಠ	D-16	1.50	92.90	123.80	302.78	0.00
106	ಠ	D-18	0.90	92.80	123.81	303.83	0.00
107	靣	D-20	0.30	92.90	123.80	302.78	0.00
108		D-22	1.02	92.90	123.79	302.68	0.00
109		D-24	0.96	92.90	123.80	302.75	0.00
110		D-26	1.70	95.00	123.79	282.09	0.00
111		J01	0.83	89.85	123.89	333.56	0.00
112		J02	1.14	90.00	123.89	332.06	0.00
113		J03	0.61	90.70	123.89	325.20	0.00
114		J04	0.61	90.20	123.89	330.09	0.00
115		J05	0.53	90.20	123.88	330.08	0.00
116		J06	0.38	90.00	123.88	332.04	0.00
117		J07	0.38	90.00	123.88	332.04	0.00
118		J08	0.68	90.30	123.89	329.11	0.00
119		J09	0.53	90.60	123.89	326.19	0.00
120		J10	0.15	90.20	123.89	330.12	0.00
121		J11	1.44	90.00	123.89	332.08	0.00
122		J12	0.48	90.20	123.89	330.13	0.00
123		J13	0.48	90.40	123.89	328.18	0.00
124		J14	0.45	90.10	123.89	331.12	0.00
125		J15	0.00	89.70	123.75	333.67	0.00
126		J16	0.61	89.70	123.89	335.01	0.00
127		J17	0.72	88.50	123.76	345.50	0.00
128		J19	0.90	88.00	123.76	350.43	0.00
129		J21	0.72	88.50	123.76	345.53	0.00
130		J23	0.90	88.00	123.77	350.49	0.00
131		RR01	0.00	89.85	123.90	333.66	0.00
132		RR02	0.00	89.40	123.89	337.99	0.00
133		RR03	0.00	89.40	123.89	337.99	0.00
134		RR05	0.00	89.15	123.86	340.13	0.00
135		RR10	1.26	88.91	123.84	342.26	0.00
136		RR15	0.00	89.15	123.78	339.33	0.00
137		RR25	0.45	88.90	123.74	341.40	0.00
138		RR30	0.00	90.50	123.68	325.18	0.00
139		SP-01	0.00	92.55	124.00	308.18	0.00
140		SP-02	0.36	93.20	123.88	300.61	0.00
141		SP-03	0.48	93.00	123.82	301.98	0.00
142		SP-04	1.70	90.87	123.81	322.82	0.00

Max Day + Fire - Fireflow Design Report

		ID	Total Demand (L/s)	Available Flow at Hydrant (L/s)	Critical Node ID	Critical Node Pressure (kPa)	Critical Node Head (m)	Design Flow (L/s)	Design Pressure (kPa)	Design Fire Node Pressure (kPa)
85		C1-52	166.86	265.81	C1-52	139.96	105.58	265.81	139.96	139.96
86		C1-54	166.86	268.63	C1-54	139.96	105.43	268.63	139.96	139.96
87		C1-56	166.79	249.39	C1-56	139.96	105.73	249.39	139.96	139.96
88		C1-60	166.97	263.81	C1-60	139.96	105.28	263.81	139.96	139.96
89		C1-62	166.82	278.78	C1-62	139.96	105.78	278.78	139.96	139.96
90		C1-64	166.79	252.90	C1-64	139.96	105.93	252.90	139.96	139.96
91		C1-66	166.82	221.78	C1-66	139.96	105.83	221.78	139.96	139.98
92		C1-68	166.75	231.65	C1-68	139.96	106.03	231.65	139.96	139.99
93		C1-70	166.71	197.54	C1-70	139.96	106.13	197.54	139.96	139.97
94		C1-72	166.77	207.76	C1-72	139.96	106.28	207.76	139.96	139.97
95		C1-74	166.84	214.80	C1-74	139.96	106.18	214.80	139.96	139.97
96		C1-76	166.81	224.43	C1-76	139.96	105.98	224.43	139.96	139.98
97		C1-78	166.78	213.46	C1-78	139.96	106.08	213.46	139.96	139.97
98		D-02	166.99	401.65	D-14	124.12	107.67	374.85	139.96	156.40
99		D-04	166.98	311.53	D-14	133.58	108.63	302.67	139.96	146.36
100		D-06	166.85	253.39	D-14	135.06	108.78	247.80	139.96	144.87
101		D-08	167.01	266.46	D-08	139.96	107.28	266.46	139.96	139.96
102		D-10	167.07	218.65	D-10	139.96	107.73	218.65	139.96	139.96
103		D-12	167.10	217.55	D-12	139.96	108.13	217.55	139.96	139.96
104		D-14	166.98	196.50	D-14	139.96	109.28	196.50	139.96	139.96
105	\Box	D-16	166.94	225.03	D-20	139.96	107.18	225.03	139.96	139.96
106		D-18	166.83	262.75	D-18	139.96	107.08	262.75	139.96	139.97
107		D-20	166.72	144.10	D-20	139.96	107.18	144.10	139.96	139.96
108	П	D-22	166.86	251.12	D-14	125.02	107.76	235.24	139.96	155.56
109	П	D-24	166.85	231.05	D-24	139.96	107.18	231.05	139.96	139.96
110		J01	167.05	310.21	J01	139.96	104.13	310.21	139.96	139.96
111		J02	167.19	204.24	J02	139.96	104.28	204.24	139.96	139.96
112		J03	166.95	258.72	J03	139.96	104.98	258.72	139.96	139.96
113	Ħ	J04	166.95	233.92	J04	139.96	104.48	233.92	139.96	139.96
114		J05	166.91	183.50	J05	139.96	104.48	183.50	139.96	139.96
115	П	J06	166.84	180.38	J06	139.96	104.28	180.38	139.96	139.96
116	Ħ	J07	166.84	195.39	J07	139.96	104.28	195.39	139.96	139.96
117	П	J08	166.98	234.77	J08	139.96	104.58	234.77	139.96	139.96
118	Ħ	J09	166.91	270.57	J09	139.96	104.88	270.57	139.96	139.96
119	f	J10	166.74	327.20	J10	139.96	104.48	327.20	139.96	139.97
120	f	J11	250.66	310.06	J11	139.96	104.28	310.06	139.96	139.96
121	Ħ	J12	250.22	300.67	J12	139.96	104.48	300.67	139.96	139.96
122	T	J13	250.22	304.95	J13	139.96	104.68	304.95	139.96	139.96
123	Ħ	J14	166.88	327.95	J14	139.96	104.38	327.95	139.96	139.96
124	Ħ	J16	166.95	213.95	J16	139.96	103.98	213.95	139.96	139.96
125	Ħ	J17	167.00	300.28	J17	139.96	102.78	300.28	139.96	139.96
126	Ħ	J19	167.08	271.21	J19	139.96	102.28	271.21	139.96	139.96

Date: Thursday, November 12, 2020, Page 3

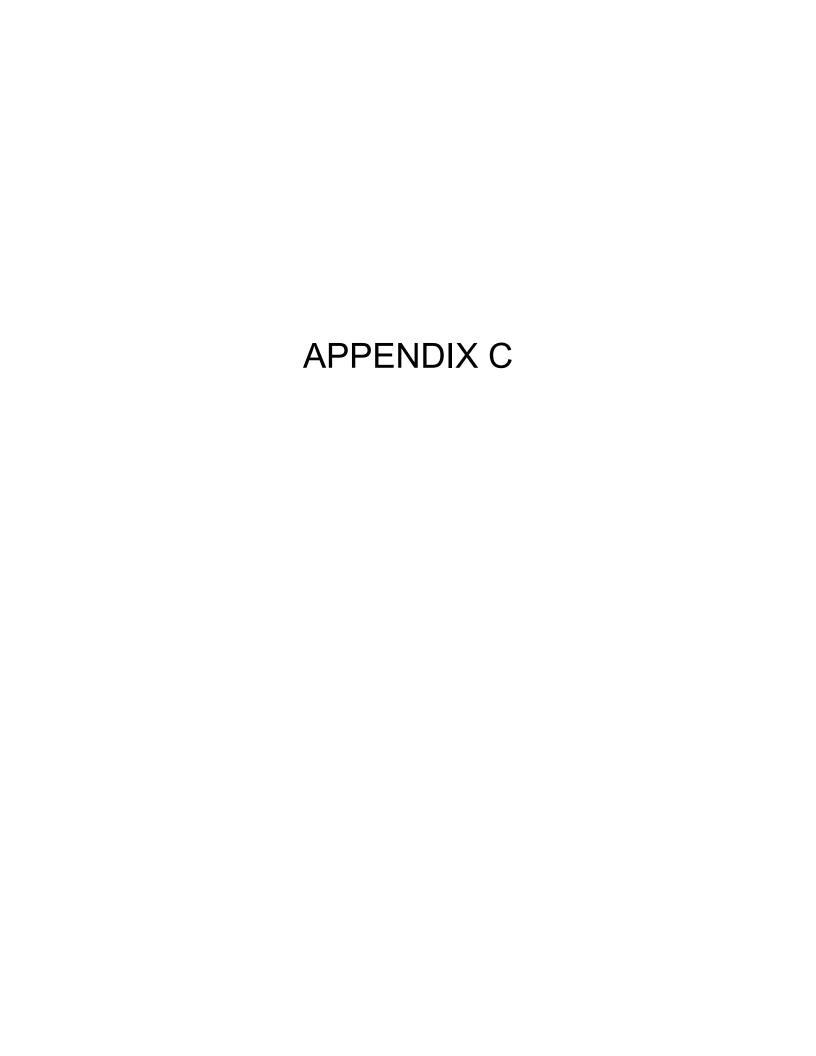
	ID	Total Demand (L/s)	Available Flow at Hydrant (L/s)	Critical Node ID	Critical Node Pressure (kPa)	Critical Node Head (m)	Design Flow (L/s)	Design Pressure (kPa)	Design Fire Node Pressure (kPa)
127	J21	167.00	264.90	J21	139.96	102.78	264.90	139.96	139.96
128	J23	167.08	398.40	J23	139.96	102.28	398.40	139.96	139.96
129	RR01	166.67	6,362.94	J03	131.75	104.15	6,178.49	139.96	148.32
130	RR05	166.67	844.68	RR05	139.96	103.43	844.69	139.96	139.96
131	RR10	166.90	1,268.99	RR10	139.97	103.19	1,269.02	139.96	139.96
132	RR15	166.67	964.93	C1-72	133.33	105.61	941.42	139.96	147.57
133	RR25	166.75	829.39	C1-72	122.27	104.48	778.37	139.96	159.11
134	RR30	166.67	592.61	C1-72	135.87	105.87	583.56	139.96	144.36
135	SP-02	166.74	567.08	SP-02	139.96	107.48	567.08	139.96	139.96
136	SP-03	166.76	509.96	D-14	121.20	107.37	470.30	139.96	158.86

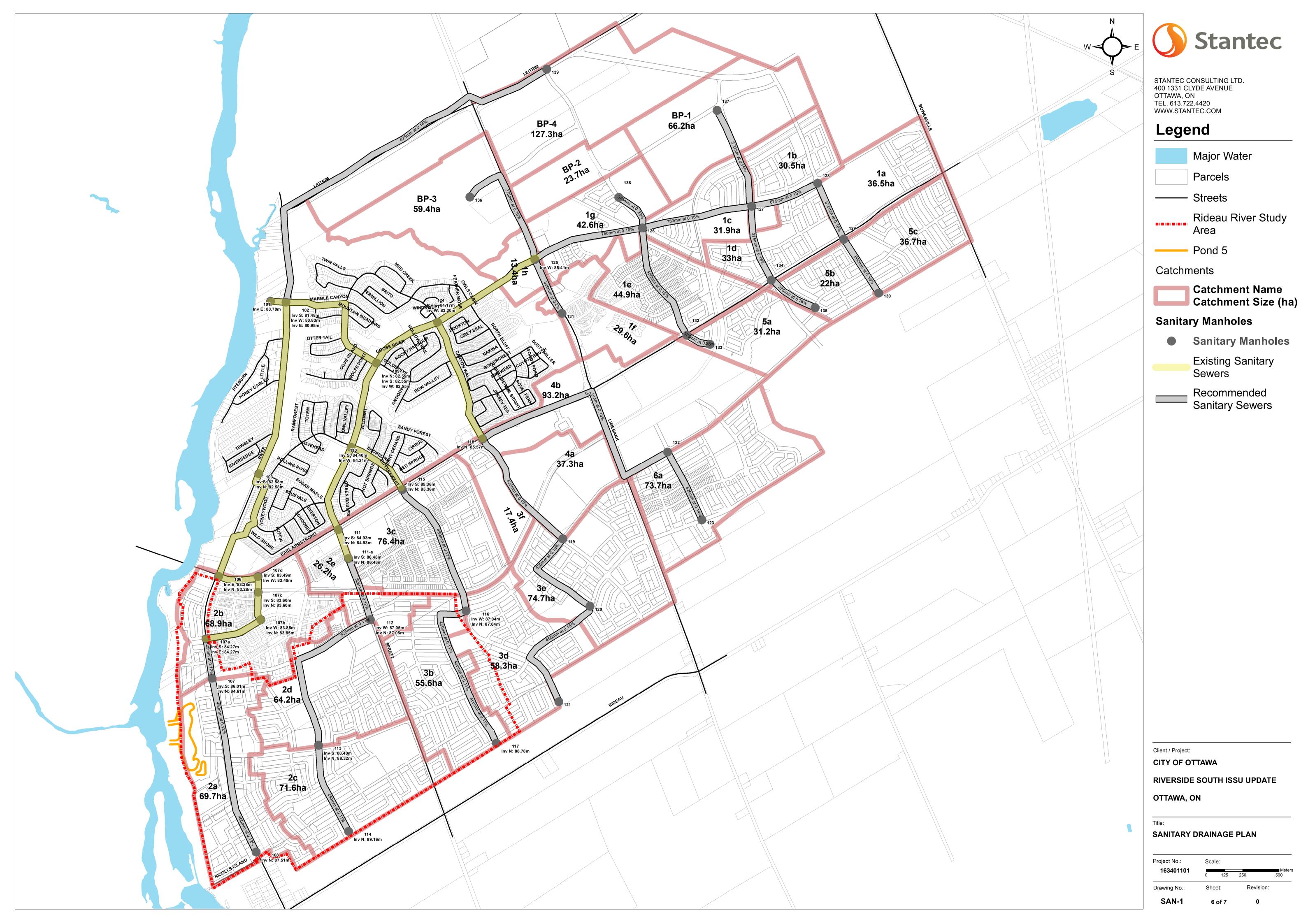
	ID	Total Demand (L/s)	Available Flow at Hydrant (L/s)	Critical Node ID	Critical Node Pressure (kPa)	Critical Node Head (m)	Design Flow (L/s)	Design Pressure (kPa)	Design Fire Node Pressure (kPa)
1	1A-97	251.72	481.71	1A-97	139.96	105.15	481.71	139.96	139.97
2	1B-30	250.12	484.92	1B-30	139.96	105.68	484.93	139.96	139.96
3	2-05	250.11	497.39	2-05	139.96	106.33	497.40	139.96	139.97
4	2-100	252.29	634.14	2-100	139.96	105.08	634.15	139.96	139.98
5	2-110	253.57	518.03	2-110	139.96	105.87	518.03	139.96	139.98
6	J11	250.66	280.67	J11	139.96	104.28	280.67	139.96	139.96
7	J12	250.22	271.77	J12	139.96	104.48	271.77	139.96	139.96
8	J13	250.22	275.24	J13	139.96	104.68	275.24	139.96	139.96
9	RR30	250.00	516.20	RR30	139.96	104.78	516.21	139.96	139.97

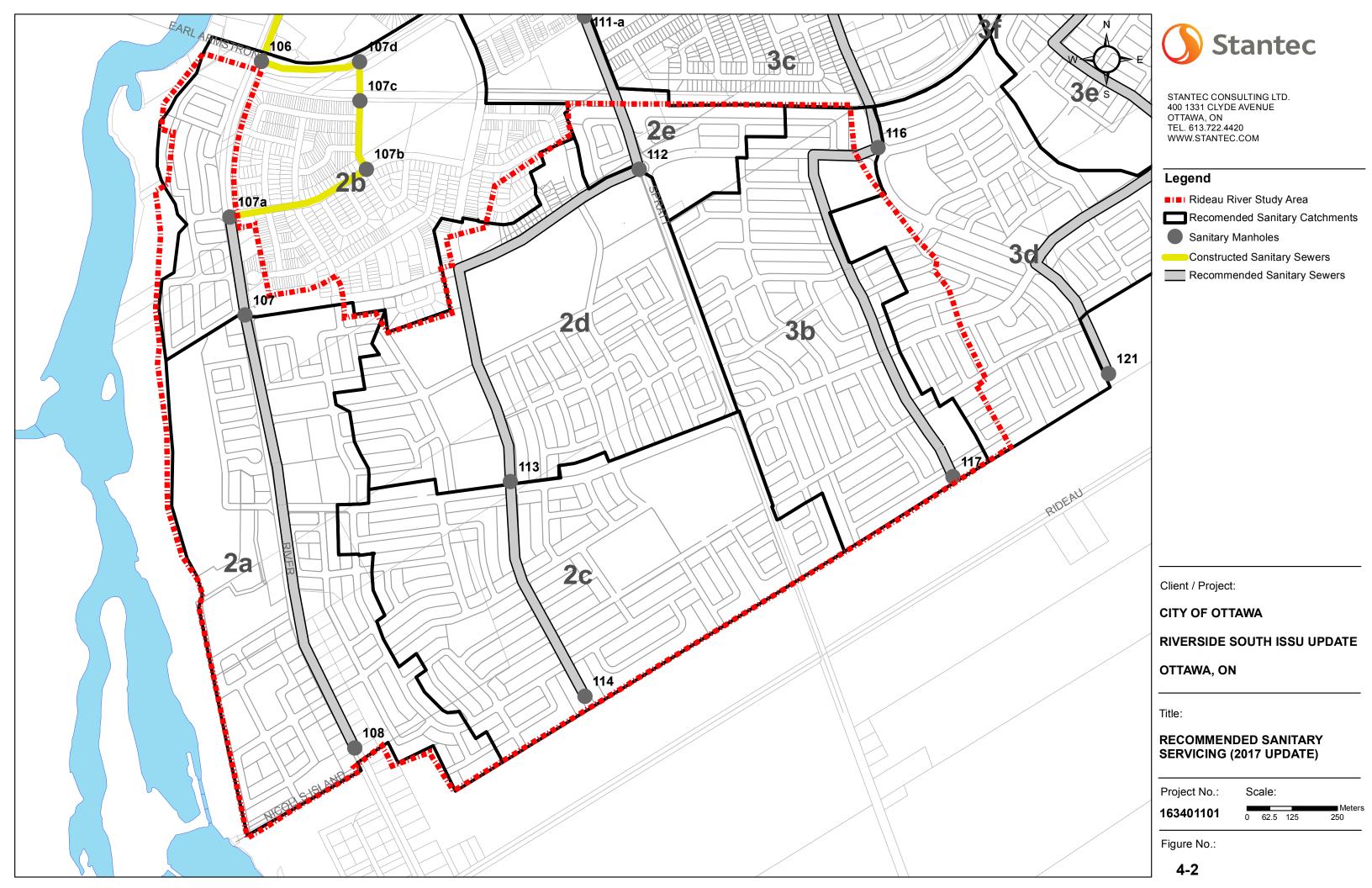
Peak Hour - Pipe Report

		From Node	To Node	Length (m)	Diameter (mm)	Roughness	Flow (L/s)	Velocity (m/s)	Headloss (m)	HL/1000 (m/k-m)	Status	Flow Reversal Count	Water Age (hrs)
141	311	D-24	D-16	105.66	204.00	110.00	-1.66	0.05	0.00	0.03	Open	0	0.00
142	313	D-24	D-04	78.93	204.00	110.00	0.70	0.02	0.00	0.01	Open	0	0.00
143	327	D-26	D-22	133.63	297.00	120.00	-2.80	0.04	0.00	0.01	Open	0	0.00
144	P13	J01	J03	77.80	204.00	110.00	1.91	0.06	0.00	0.04	Open	0	0.00
145	P15	J01	J16	84.58	204.00	110.00	1.50	0.05	0.00	0.02	Open	0	0.00
146	P17	J02	J03	104.57	204.00	110.00	-0.25	0.01	0.00	0.00	Open	0	0.00
147	P19	J03	J04	88.45	204.00	110.00	1.05	0.03	0.00	0.01	Open	0	0.00
148	P41	J04	J05	92.46	204.00	110.00	0.59	0.02	0.00	0.00	Open	0	0.00
149	P21	J04	J08	79.74	204.00	110.00	-0.15	0.00	0.00	0.00	Open	0	0.00
150	P43	J05	J06	73.58	204.00	110.00	0.06	0.00	0.00	0.00	Open	0	0.00
151	P45	J06	J07	75.07	204.00	110.00	-0.32	0.01	0.00	0.00	Open	0	0.00
152	P47	J07	J08	54.79	204.00	110.00	-0.70	0.02	0.00	0.01	Open	0	0.00
153	P23	J08	J09	84.07	204.00	110.00	-1.53	0.05	0.00	0.02	Open	0	0.00
154	P25	J10	J09	34.85	204.00	110.00	2.06	0.06	0.00	0.04	Open	0	0.00
155	P27	J10	J14	80.56	250.00	110.00	-2.18	0.04	0.00	0.02	Open	0	0.00
156	P33	J11	J12	51.90	250.00	110.00	-1.47	0.03	0.00	0.01	Open	0	0.00
157	P31	J11	J10	45.66	250.00	110.00	0.03	0.00	0.00	0.00	Open	0	0.00
158	P35	J12	J13	53.01	250.00	110.00	-1.95	0.04	0.00	0.01	Open	0	0.00
159	P37	J13	RR03	71.84	250.00	110.00	-2.43	0.05	0.00	0.02	Open	0	0.00
160	P29	J14	RR02	72.33	250.00	110.00	-2.63	0.05	0.00	0.03	Open	0	0.00
161	P57	J15	J17	89.98	204.00	110.00	-2.90	0.09	0.01	0.08	Open	0	0.00
162	P69	J16	J02	104.73	204.00	110.00	0.89	0.03	0.00	0.01	Open	0	0.00
163	P65	J17	J19	102.31	204.00	110.00	-1.79	0.05	0.00	0.03	Open	0	0.00
164	P59	J17	J21	80.61	204.00	110.00	-1.83	0.06	0.00	0.03	Open	0	0.00
165	P63	J19	J23	82.81	204.00	110.00	-2.69	0.08	0.01	0.07	Open	0	0.00
166	P61	J21	J23	101.79	204.00	110.00	-2.55	80.0	0.01	0.06	Open	0	0.00
167	P11	RR01	J01	62.52	204.00	110.00	4.24	0.13	0.01	0.16	Open	0	0.00
168	P51	RR02	RR01	237.65	297.00	120.00	-5.06	0.07	0.01	0.03	Open	0	0.00
169	P49	RR03	RR02	61.62	297.00	120.00	-2.43	0.04	0.00	0.01	Open	0	0.00
170	69	RR05	RR01	176.52	297.00	120.00	-14.75	0.21	0.04	0.23	Open	0	0.00
171	13	RR10	RR15	129.52	393.00	120.00	44.97	0.37	0.06	0.46	Open	0	0.00
172	19	RR10	1A-05	138.19	393.00	120.00	-31.48	0.26	0.03	0.24	Open	0	0.00
173	11	RR10	RR05	97.51	297.00	120.00	-14.75	0.21	0.02	0.23	Open	0	0.00
174	15	RR15	RR25	167.66	393.00	120.00	31.43	0.26	0.04	0.23	Open	0	0.00
175	P67	RR15	J23	34.23	204.00	110.00	6.14	0.19	0.01	0.33	Open	0	0.00

Date: Thursday, November 12, 2020,, Page 5









Riverside South Community Infrastructure Servicing Study

File Number: 1634-01101

Revision Date: June 5, 2017 Designed by: Megan Young Checked By: Amanda Lynch

SANITARY SEWER DESIGN SHEET

CITY CRITERIA & DENSITIES Approved area

Average Daily Flow / Person: Minimum Velocity: Max Peaking Factor:
Min. Peaking Factor:
Peaking Factor Industrial:
Peaking Factor Comm. / Inst.:

350 l/p/day Commercial: 0.60 m/s Employment Infiltration: Low Density: Medium Density:

0.013

4.0

2.0

Based on Appendix 4-B 1.5

DESIGN PARAMETERS

0.579 l/s/ha 0.280 l/s/ha 3.2 pers/unit2.4 pers/unit1.9 pers/unit

0.579 l/s/ha

0.579 l/s/ha

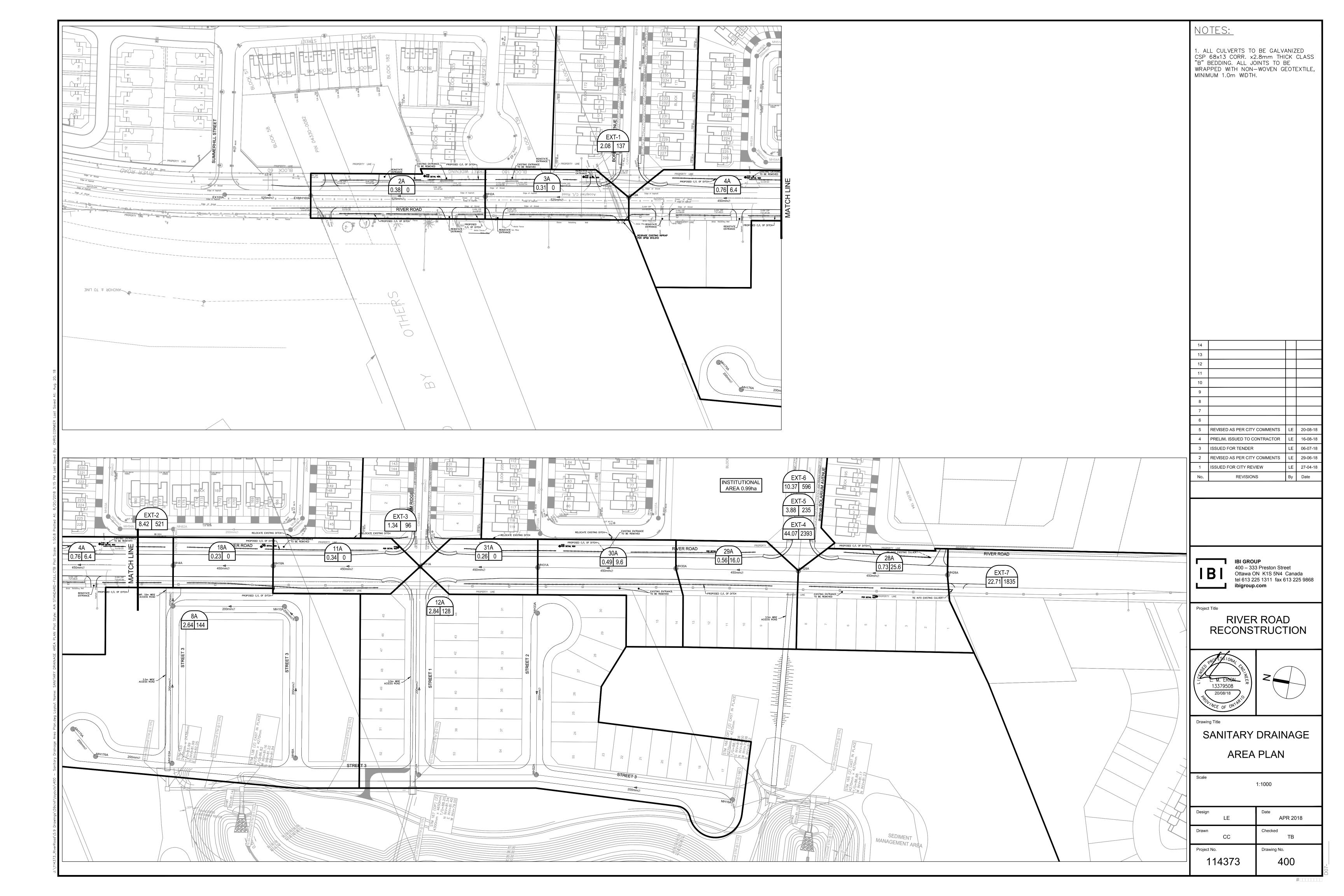
High Density:

Existing Sanitary Sewer flows estimated by existing land use. Existing Phase 9 area

																																n JLR 2011		cxioting id	ind doc. Ex	sting i nasc	o area	1
STREET	ID Area		То			1.011			MED		RESIDE					1	Б.	I 5 :		MMERCIAL	EMPLO			UTIONAL	C+I+I		DAD		INFILTRATION			D: /	In: .	01	PIPE	0 "		
		MH I	МН	AREA	Area	LOW	Accum.	Area	MED	Accum.	Area	HIGH	Accum.	-	Accum.	Total Accum.	Peak Factor	Peak Flow	Area	Accum. Area	Area	Accum. Area	Area	Accum. Area	Peak Flow	Area	Accum. Area	Total Area	Accum. Area	Infilt. Flow	Total Flow	Distance	Diameter	Slope	Qa/Qc	Capacity (Full)	Velo (Full)	ocity (Actual)
				(ha)	(ha)	Pop.	Pop.	(ha)	Pop.	Pop.	(ha)	Pop.	Pop.	Units	Units	Pop.		(l/s)	(ha)	(ha)	(ha)	(ha)	(ha)	(ha)	(l/s)	(ha)	(ha)	(ha)	(ha)	(l/s)	(l/s)	(m)	(mm)	(%)		(l/s)	(m/s)	(m/s)
RIVER ROAD RIVER ROAD RIVER ROAD	2a 2b Future 2b Existing (Phase 9)	107 1	07a	50.51 12.21 43.20	44.40 10.22 43.20	2189 502 2351	2189 2691 5042	6.11 1.99 0.00	389 127 0	389 516 516	0.00 0.00 0.00	0 0 0	0 0 0	846 210 N/A	846 1056 1056	2578 3207 5558	3.5 3.4 3.2	36.5 44.4 72.1	1.19 0.00 0.00	1.19 1.19 1.19	0.00 0.00 0.00	0.00 0.00 0.00	1.01 0.00 2.46	1.01 1.01 3.47	1.9 1.9 4.0	4.48 2.64 0.00	4.48 7.12 7.12	57.18 14.85 45.66	57.18 72.03 117.69	16.0 20.2 33.0	54.4 66.5 109.1	1255 254 405	450 525 525	0.12 0.12 0.10	0.53 0.43 0.76	103.0 155.4 144.5	0.63 0.70 0.65	0.63 0.66 0.71
RIVER ROAD RIVER ROAD	Ex3	107c 1 107d	07d 106	0.00 0.00 0.00 17.90	0.00 0.00 0.00 10.04	0 0 0 413	5042 5042 5042 5455	0.00 0.00 0.00 7.86	0 0 0 564	516 516 516 1080	0.00 0.00 0.00 0.00	0 0 0	0 0 0	0 0 0 364	1056 1056 1056 1420	5558 5558 5558 6535	3.2 3.2 3.2 3.1	72.1 72.1 72.1 83.0	0.00 0.00 0.00 5.35	1.19 1.19 1.19 6.54	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	3.47 3.47 3.47 3.47	4.0 4.0 4.0 8.7	0.00 4.70 0.00 0.00	7.12 11.82 11.82 11.82	0.00 4.70 0.00 23.25	117.69 122.39 122.39 145.64	33.0 34.3 34.3 40.8	109.1 110.4 110.4 132.5	217 107 278 835	525 525 525 525	0.12 0.10 0.08 0.10	0.72 0.77 0.90 0.93	152.3 143.9 123.3 141.9	0.68 0.64 0.55 0.63	0.74 0.71 0.63 0.73
	Ex2			16.42	16.42	573	6028	0.00	0	1080	0.00	0	0	179	1599	7108	3.1	89.3	0.00	6.54	0.00	0.00	0.00	3.47	8.7	5.11	16.93	21.53	167.17	46.8	144.8	1100	525	0.10	1.02	141.9	0.63	0.74
SPRATT SOUTH SPRATT SOUTH SPRATT SOUTH SPRATT SOUTH	2c 2d 2e	113 1 112 1 111-a	112 11-a 111	53.79 39.28 17.48 0.00	51.84 28.89 0.00 0.00	2554 1424 0	2554 3978 3978 3978	1.95 10.40 13.28 0.00	847 0	125 790 1637 1637	0.00 0.00 4.19 0.00	0 0 479	0 0 479 479	850 722 605	850 1572 2177 2177	2679 4768 6094 6094	3.5 3.3 3.2 3.2	37.8 63.0 78.1 78.1	0.00 0.00 2.55 0.00	0.00 0.00 2.55 2.55	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	7.68 14.95 0.00 0.00	7.68 22.63 22.63 22.63	6.7 19.7 21.9 21.9	5.93 5.45 6.14 0.00	5.93 11.38 17.52 17.52	67.41 59.69 26.17 0.00	67.41 127.09 153.26 153.26	18.9 35.6 42.9 42.9	63.4 118.3 142.9	695 1155 470 215	450 525 525 525	0.11 0.11 0.12 0.11	0.64 0.79 0.92 0.96	98.6 148.8 155.4 148.8	0.60 0.67 0.70 0.67	0.64 0.74 0.80 0.77
SPRATT SOUTH	Ex4	111	110	14.93	13.31	90	4068	1.62	468	2105	0.00	0	479	223	2400	6652	3.1	84.3	0.91	3.46	0.00	0.00	0.00	22.63	22.7	0.00	17.52	15.84	169.10	47.3	154.3	600	525	0.12	0.99	155.4	0.70	0.81
SHORELINE DRIVE SHORELINE DRIVE SHORELINE DRIVE	3b 3c Ex5		115	48.13 47.51 20.60	43.40 27.40 14.47	1350	2138 3488 3968	4.73 15.47 6.13	302 989 302	302 1291 1593	0.00 4.64 0.00	0 530 0	0 530 530	794 1113 276	794 1907 2183	2440 5309 6091	3.5 3.2 3.2	34.8 69.3 78.1	0.66 0.00 0.80	0.66 0.66 1.46	0.00 0.00 0.00	0.00 0.00 0.00	0.05 11.13 3.16	0.05 11.17 14.33	0.6 10.3 13.7	2.77 10.02 0.00	2.77 12.79 12.79	51.60 68.67 24.56	51.60 120.26 144.82	14.4 33.7 40.6	49.8 113.2 132.3	1270 990 480	450 450 450	0.11 0.17 0.20	0.51 0.92 0.99	98.6 122.6 133.0	0.60 0.75 0.81	0.60 0.86 0.94
SPRATT SOUTH	Ex6	110	109	25.47	20.32	822	8858	5.15	288	3986	0.00	0	1009	377	4960	13853	2.8	157.9	0.00	4.92	0.00	0.00	2.39	39.36	38.5	0.00	30.31	27.86	341.78	95.7	292.0	675	675	0.12	0.96	303.8	0.82	0.95
CANYON WALK DRIVE	3d	121	120	46.05	35.39	1744	1744	10.66	679	679	0.00	0	0	828	828	2423	3.5	34.5	0.60	0.60	0.00	0.00	3.72	3.72	3.8	5.41	5.41	55.78	55.78	15.6	53.9	820	450	0.15	0.47	115.2	0.70	0.69
CANYON WALK DRIVE CANYON WALK DRIVE	3e 3f-4a		119	54.06 17.44	40.27 0.00	1984 0	3728 3728	13.79 3.06		1560 1754	0.00 14.38	0 1007	0 1007	987 577	1815 2392	5288 6489	3.2 3.1	69.0 82.5	0.00 6.01	0.60 6.61	0.00	0.00 0.00	3.91 5.28	7.63 12.92	7.2 17.0	9.21 16.75	14.62 31.37	67.19 45.49	122.97 168.46	34.4 47.2	110.6 146.6	925 880	525 525	0.18 0.19	0.58 0.75	190.3 195.6	0.85 0.88	0.89 0.97
internal south ARMSTRONG ROAD	6a 4b			49.84 58.24	31.53 0.00	1555 0	1555 1555	18.31 0.00	1169 0	1169 1169	0.00 58.24	0 4070	0 4070	973 2005	973 2978	2724 6794	3.5 3.1	38.4 85.8	1.18 24.34	1.18 25.53	0.00 0.00	0.00 0.00	5.33 0.00	5.33 5.33	5.7 26.8	6.44 24.91	6.44 31.35	62.80 107.49	62.80 170.29	17.6 47.7	61.6 160.3	600 1810	525 600	0.14 0.13	0.37 0.69	167.9 231.0	0.75 0.79	0.68 0.86
CANYON WALK DRIVE	Ex1	118	124	45.64	22.12	896	6179	23.52	1687	4610	0.00	0	5077	983	6353	15866	2.8	177.0	1.55	33.69	0.00	0.00	0.00	18.25	45.1	0.00	62.72	47.19	385.94	108.1	330.2	860	750	0.15	0.73	449.8	0.99	1.08
SPRATT ROAD SPRATT ROAD SPRATT ROAD	5c 1a 1b	129	128	25.52 10.26 18.80	20.06 7.00 4.11	989 346 202	989 1335 1537	5.46 3.26 13.56	348 209 866	348 557 1423	0.00 0.00 1.13	0 0 129	0 0 129	454 195 492	454 649 1141	1337 1892 3089	3.7 3.6 3.4	20.1 27.6 42.9	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	2.38 0.00 2.82	2.38 2.38 5.20	2.1 2.1 4.5	4.86 7.76 5.34	4.86 12.63 17.97	32.77 18.02 26.97	32.77 50.79 77.76	9.2 14.2 21.8	31.4 43.9 69.2	420 450 490	600 675 675	0.15 0.15 0.15	0.13 0.13 0.20	248.1 339.6 339.6	0.85 0.92 0.92	0.56 0.61 0.70
internal north internal north	5b 1d			17.31 21.95	10.06 12.43	496 611	496 1107	7.25 9.52	463 607	463 1070	0.00 0.00	0 0	0 0	348 444	348 792	959 2177	3.8 3.6	14.8 31.4	0.00 2.66	0.00 2.66	0.00 0.00	0.00 0.00	0.03 0.01	0.03 0.04	0.0 2.3	1.32 4.33	1.32 5.66	18.66 28.95	18.66 47.61	5.2 13.3	20.1 47.0	385 550	375 375	0.15 0.15	0.28 0.66	70.8 70.8	0.62 0.62	0.53 0.67
	BP-1	137	127	39.70	20.70	1173	1173	17.00	1019	1019	2.00	398	398	891	891	2590	3.5	36.7	0.00	0.00	16.18	16.18	0.00	0.00	9.4	6.81	6.81	62.69	62.69	17.6	63.6	725	375	0.15	0.90	70.8	0.62	0.71
SPRATT ROAD	1c	127	126	14.01	0.00	0	3817	8.98	574	4086	5.03	574	1101	541	3365	9004	3.0	109.4	0.74	3.40	0.00	16.18	6.60	11.84	22.6	6.42	36.86	27.77	215.82	60.4	192.4	795	750	0.15	0.43	449.8	0.99	0.94
internal north internal north	5a 1e			11.48 34.06	4.65 22.08	230 1088	230 1318	6.83 11.98	437 766	437 1203	0.00 0.00	0 0	0 0	254 659	254 913	667 2521	3.9 3.5	10.6 35.8	1.02 0.00	1.02 1.02	0.00 0.00	0.00 0.00	1.15 1.37	1.15 2.52	1.9 3.1	4.02 6.18	4.02 10.21	17.68 41.61	17.68 59.29	5.0 16.6	17.4 55.5	410 810	375 450	0.15 0.15	0.25 0.48	70.8 115.2	0.62 0.70	0.50 0.69
	BP-2	138	126	0.11	0.00	0	0	0.11	7	7	0.00	0	0	3	3	7	4.0	0.1	0.00	0.00	15.00	15.00	0.00	0.00	8.7	1.48	1.48	16.59	16.59	4.6	13.4	440	375	0.15	0.19	70.8	0.62	0.46
SPRATT ROAD	1g	126	125	14.19	1.66	83	5218	9.47	605	5901	3.05	348	1449	461	4742	12568	2.9	145.4	0.98	5.40	0.00	31.18	10.12	24.48	44.0	3.45	52.00	28.74	320.44	89.7	279.1	710	750	0.17	0.58	478.9	1.05	1.09
SPRATT ROAD	1f	131	125	9.29	5.05	250	250	4.24	271	271	0.00	0	0	191	191	521	4.0	8.4	0.00	0.00	0.00	0.00	0.00	0.00	0.0	3.48	3.48	12.77	12.77	3.6	11.9	420	300	0.20	0.26	45.1	0.62	0.51
	ВР3	136	125	0.00	0.00	0	0	0.00	0	0	0.00	0	0	0	0	0	0.0	0.0	0.00	0.00	38.46	38.46	0.00	0.00	22.3	5.69	5.69	44.15	44.15	12.4	34.6	986	375	0.14	0.51	68.4	0.60	0.60
SPRATT ROAD	1h	125	124	1.69	0.00	0	5468	1.69	108	6280	0.00	0	1449	45	4978	13197	2.8	151.5	2.20	7.60	0.00	69.64	1.66	26.14	69.6	3.04	64.20	8.59	385.95	108.1	329.2	830	900	0.15	0.45	731.4	1.11	1.07
SPRATT ROAD	Ex7	124	109	17.26	11.40	768	12415	3.00	250	11140	2.86	327	6853	516	11847	30408	2.5	304.4	0.64	41.93	0.00	69.64	0.00	44.39	115.3	0.00	126.93	17.90	789.79	221.1	640.9	515	1050	0.15	0.58	1103.3	1.23	1.28
CANYON WALK DRIVE	Ex8												7862		17535		2.3	432.5	0.00	46.85		69.64							1193.42				1050	0.15	0.83	1103.3	1.23	1.39
SPRATT ROAD	BP-4				0.00				0	0	0.00	0	0	0	0	0	0.0	0.0	0.00	0.00		127.52		0.00					147.28				675	0.15	0.62	339.6	0.92	0.97
	<u> </u>			3.00	0.00	J	J	3.00	Ü	J	3.00	J	Ü		J		0.0	0.0	3.00	5.00	,.02		0.00	0.00	.00.0	.5.70	.5.70	20		. 1.2				5.10	3.02	000.0	5.52	0.57
CROSSING		102 1	101	0			29451			16340			7862		19134	53653	2.2	486.0		53.39		197.16		87.21	384.7		199.37	0	1507.87	422.2	1292.9	145	1200	0.11	0.96	1349.0	1.16	1.33

CROSSING

^{*}Note:
Area BP-4 also accounts for additional 39ha area outside the CDP that was accounted for in calculation of Employment Area
PIPE Capacity (Full) calculated using ACTUAL PIPE SIZE
Limiting Capacity Calculated based on 1200 mm pipe @ 0.11% between Rideau Road and River
Additional sanitary flow of 29.21 L/s from Rideau Carleton Raceway (RCR) is not included in the above calculation, as it is proposed that flow from this area be pumped into the system at off-peak times



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River Road City of Ottawa Riverside South Development Corporation

	LOCATION							RESIDENTIA	\L								ICI AREAS	3			INFILTE	ATION ALLO	WANCE	EIVED E		TOTAL			PROPO	SED SEWER	R DESIGN		
	LOCATION			AREA		UNIT T	YPES	AREA	POPU	JLATION	PEAK	CORR.	PEAK			ARE	A (Ha)			PEAK	ARE	A (Ha)	FLOW	FIXED F	LOW (L/s)	FLOW	CAPACITY	LENGTH	DIA	SLOPE	VELOCITY	AVAIL	ABLE
STREET	AREA ID	FROM	ТО	w/ Units	SF	SD	TH	APT w/o Units	IND	CUM	FACTOR	FACTOR	FLOW		JTIONAL		IERCIAL		TRIAL	FLOW	IND	CUM	(L/s)	IND	CUM	(L/s)	(L/s)	(m)	(mm)	(%)	(full)	CAPA	
	7	MH	MH	(Ha)	J .			(Ha)					(L/s)	IND	CUM	IND	CUM	IND	CUM	(L/s)			(=, 0)			(= 0)	(20)	(,	()	(75)	(m/s)	L/s	(%)
Divor Dood	EXT - 7				 			22.71	1,835.0	1,835.0	2.61	0.00	17.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	22.71	22.71	7.40	0.00	0.00	24.69		 			<u> </u>		
River Road	28A	MH28A	MH29A	0.73	Ω			22.71	25.6	1,860.6	3.61	0.80	17.20 17.41	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.73	23.44	7.49 7.74	0.00	0.00	25.15	103.03	101.51	450	0.12	0.628	77.89	75.59%
	20A	IVII IZOA	IVII IZ9A	0.73	8				23.0	1,000.0	3.01	0.00	17.41	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.73	23.44	7.74	0.00	0.00	23.13	103.03	101.51	430	0.12	0.028	11.09	73.3976
Solarium Avenue	EXT - 4, 5, 6	STUB	MH29A	58.32	652		474		3,224.0	3,224.0	3.42	0.80	28.55	0.99	0.99	0.00	0.00	0.00	0.00	0.48	59.31	59.31	19.57	0.00	0.00	48.60	81.80	25.00	375	0.20	0.717	33.20	40.58%
		0.02		00.02					5,==	5,==		0.00		1	0.00	1		0.00	0.00	00	00.0.	00.01	10101	0.00	0.00		0.100		0.0	00	+	33.25	1010070
River Road	29A	MH29A	MH30A	0.56	5				16.0	5,100.6	3.24	0.80	42.80	0.00	0.99	0.00	0.00	0.00	0.00	0.48	0.56	83.31	27.49	0.00	0.00	70.78	103.03	83.34	450	0.12	0.628	32.26	31.31%
	30A	MH30A	MH31A	0.49	3				9.6	5,110.2	3.24	0.80	42.88	0.00	0.99	0.00	0.00	0.00	0.00	0.48	0.49	83.80	27.65	0.00	0.00	71.01	103.03	93.99	450	0.12	0.628	32.02	31.08%
River Road	31A	MH31A	MH11A	0.25					0.0	5,110.2	3.24	0.80	42.88	0.00	0.99	0.00	0.00	0.00	0.00	0.48	0.25	84.05	27.74	0.00	0.00	71.09	103.03	80.00	450	0.12	0.628	31.94	31.00%
Atrices Distric	EVT 2	CTUD	NALIA A A	4.04	 		40		00.0	00.0	4.00	0.00	4.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	4.04	4.04	0.44	0.00	0.00	4 44	44.04	25.04	200	4.50	4.000	40.47	00 570/
Atrium Ridge	EXT - 3	STUB	MH11A	1.34			40		96.0	96.0	4.00	0.80	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.34	1.34	0.44	0.00	0.00	1.44	41.91	25.04	200	1.50	1.292	40.47	96.57%
Street No. 1 West	12A	STUB	MH11A	2.84	40				128.0	128.0	4.00	0.80	1.33	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.84	2.84	0.94	0.00	0.00	2.26	24.19	22.70	200	0.50	0.746	21.93	90.64%
Olicci No. 1 West	12/1	0100	IVIIIII	2.04	+ +				120.0	120.0	7.00	0.00	1.55	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.04	2.04	0.54	0.00	0.00	2.20	24.13	22.70	200	0.50	0.740	21.00	30.0470
River Road	11A	MH11A	MH18A	0.34					0.0	5,334.2	3.22	0.80	44.51	0.00	0.99	0.00	0.00	0.00	0.00	0.48	0.34	88.57	29.23	0.00	0.00	74.22	103.03	100.00	450	0.12	0.628	28.81	27.96%
	18A	MH18A	MH4A	0.23					0.0	5,334.2	3.22	0.80	44.51	0.00	0.99	0.00	0.00	0.00	0.00	0.48	0.23	88.80	29.30	0.00	0.00	74.30	103.03	68.01	450	0.12	0.628	28.73	27.89%
Capricorn Circle	EXT - 2	STUB	MH4A	8.42	69		125		520.8	520.8	3.97	0.80	5.35	0.00	0.00	0.00	0.00	0.00	0.00	0.00	8.42	8.42	2.78	0.00	0.00	8.13	20.24	18.89	200	0.35	0.624	12.11	59.83%
Other to Mind	0.4	OTUD	B 41 1 4 A	0.04			00		4440	4440	4.00	0.00	4.40	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.04	0.04	0.07	0.00	0.00	0.00	04.40	17.10	000	0.50		04.00	00.000/
Street 3 West	8A	STUB	MH4A	2.64	 		60	 	144.0	144.0	4.00	0.80	1.49	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.64	2.64	0.87	0.00	0.00	2.36	24.19	17.13	200	0.50	0.746	21.83	90.23%
River Road	4A	MH4A	MH3A	0.76	2			 	6.4	6,005.4	3.17	0.80	49.36	0.00	0.99	0.00	0.00	0.00	0.00	0.48	0.76	100.62	33.20	0.00	0.00	83.05	103.03	129.23	450	0.12	0.628	19.99	19.40%
TAVOI TAGA	77.1	IVII I TY	1011 137 (0.70					0.4	0,000.4	0.17	0.00	43.50	0.00	0.55	0.00	0.00	0.00	0.00	0.40	0.70	100.02	33.20	0.00	0.00	00.00	100.00	123.23	430	0.12	0.020	13.33	13.4070
Borbridge Avenue	EXT - 1	STUB	MH3A	2.08			57		136.8	136.8	4.00	0.80	1.42	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.08	2.08	0.69	0.00	0.00	2.11	19.36	20.00	200	0.32	0.597	17.25	89.12%
River Road	3A	MH3A	MH2A	0.31					0.0	6,142.2			50.34	0.00	0.99	0.00	0.00	0.00	0.00	0.48	0.31	103.01	33.99	0.00	0.00	84.81	155.42	97.77	525	0.12	0.696	70.61	45.43%
	2A		EX. MH160A						0.0	6,142.2	3.16	0.80	50.34	0.00	0.99	0.00	0.00	0.00	0.00	0.48	0.38	103.39	34.12	0.00	0.00	84.94	155.42	118.68	525	0.12	0.696	70.48	45.35%
		EX MH106A	EX MH 100A	0.19					0.0	6,142.2	3.16	0.80	50.34	0.00	0.99	0.00	0.00	0.00	0.00	0.48	0.19	103.58	34.18	0.00	0.00	85.00	141.88	58.85	525	0.10	0.635	56.88	40.09%
					 											1								<u> </u>				 			<u> </u>		
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Design Parameters:				Notes:				<u> </u>			Designed	<u> </u>	<u> </u>	LME			No.						Revisio	1							Date		
Doorgii i arameters.				1. Mannings	coefficient (r	n) =		0.013			Designed	•					1						Submission								27/04/2018		
Residential		ICI Areas		2. Demand (., –	280	L/day									2.						Submission I								3/07/2018		
SF 3.2 p/p/u			Peak Factor	3. Infiltration				B L/s/Ha			Checked:						3.						Submission I								20/08/2018		
TH/SD 2.4 p/p/u	INST 28,000	L/Ha/day	1.5	4. Residentia	al Peaking Fa	actor:																											
APT 1.9 p/p/u	COM 28,000	L/Ha/day	1.5		Harmon For	mula = 1+(1																											
Other 81 p/p/Ha	IND 35,000	L/Ha/day	MOE Chart		where $P = p$						Dwg. Refe	erence:		114373-50	1																		
					Correctio	on Factor =	0.8	}										ile Referenc						Date:							Sheet No:		
																		114373.5.7.	1					2018-08-20	J						1 of 1		



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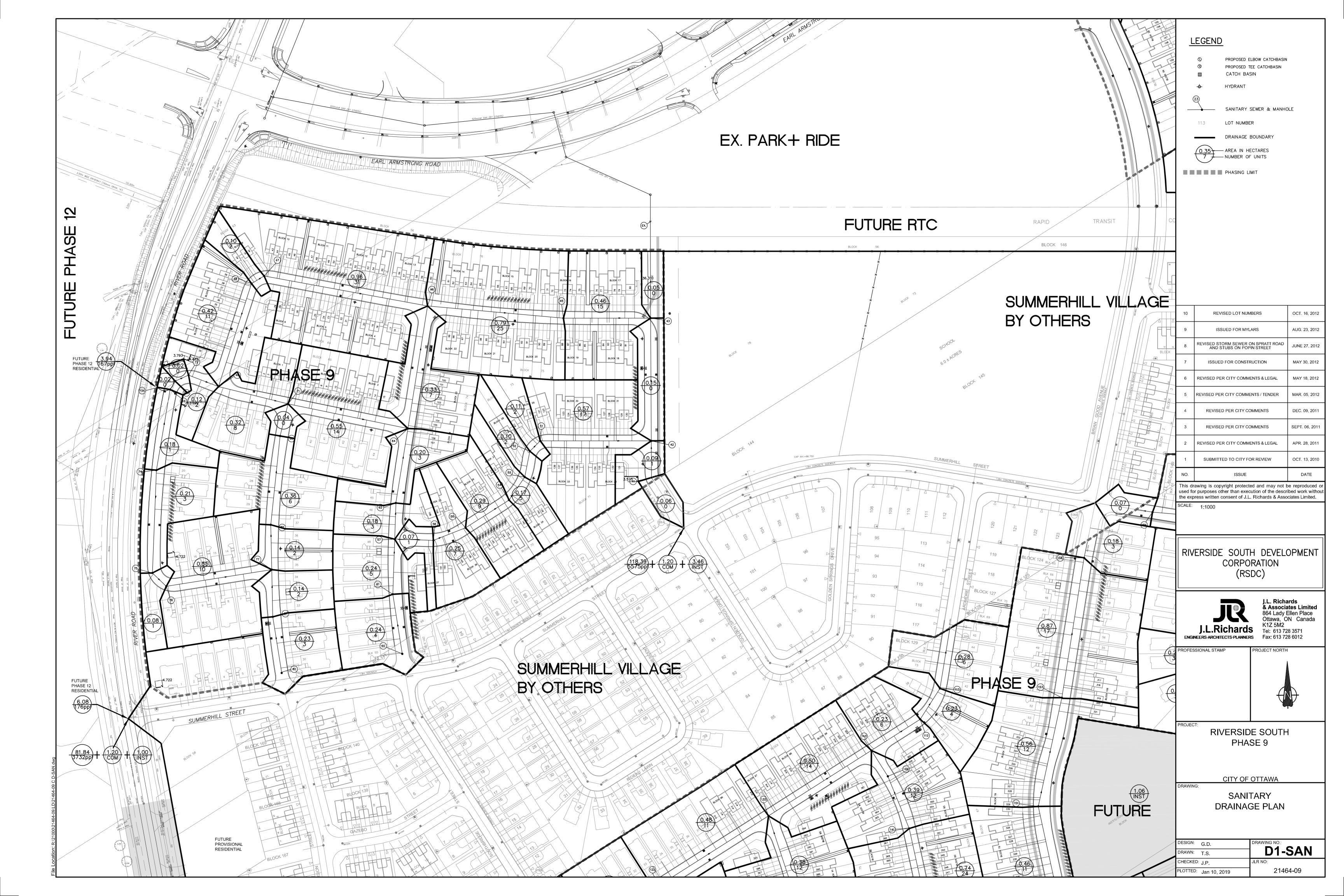
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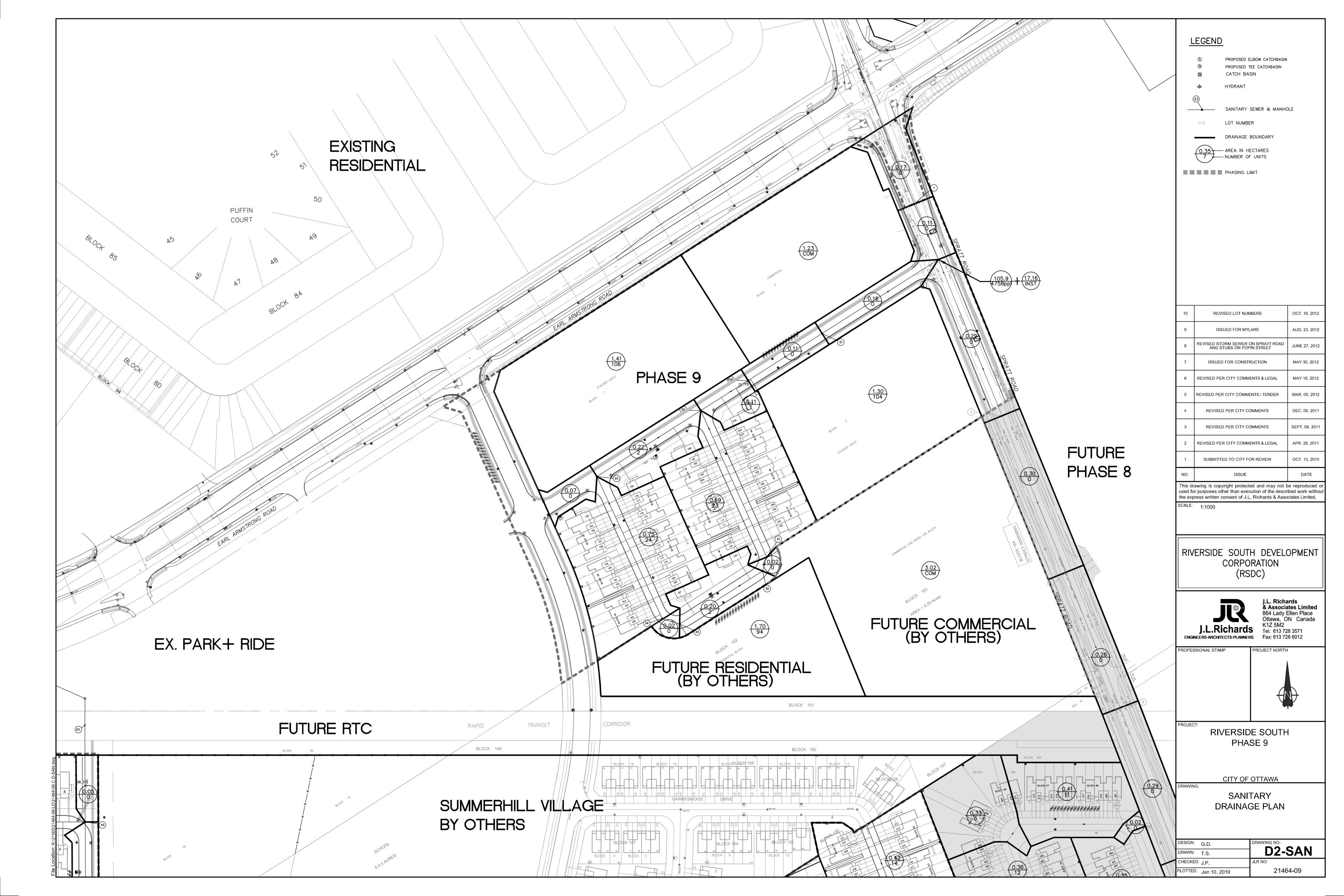
SANITARY SEWER DESIGN SHEET

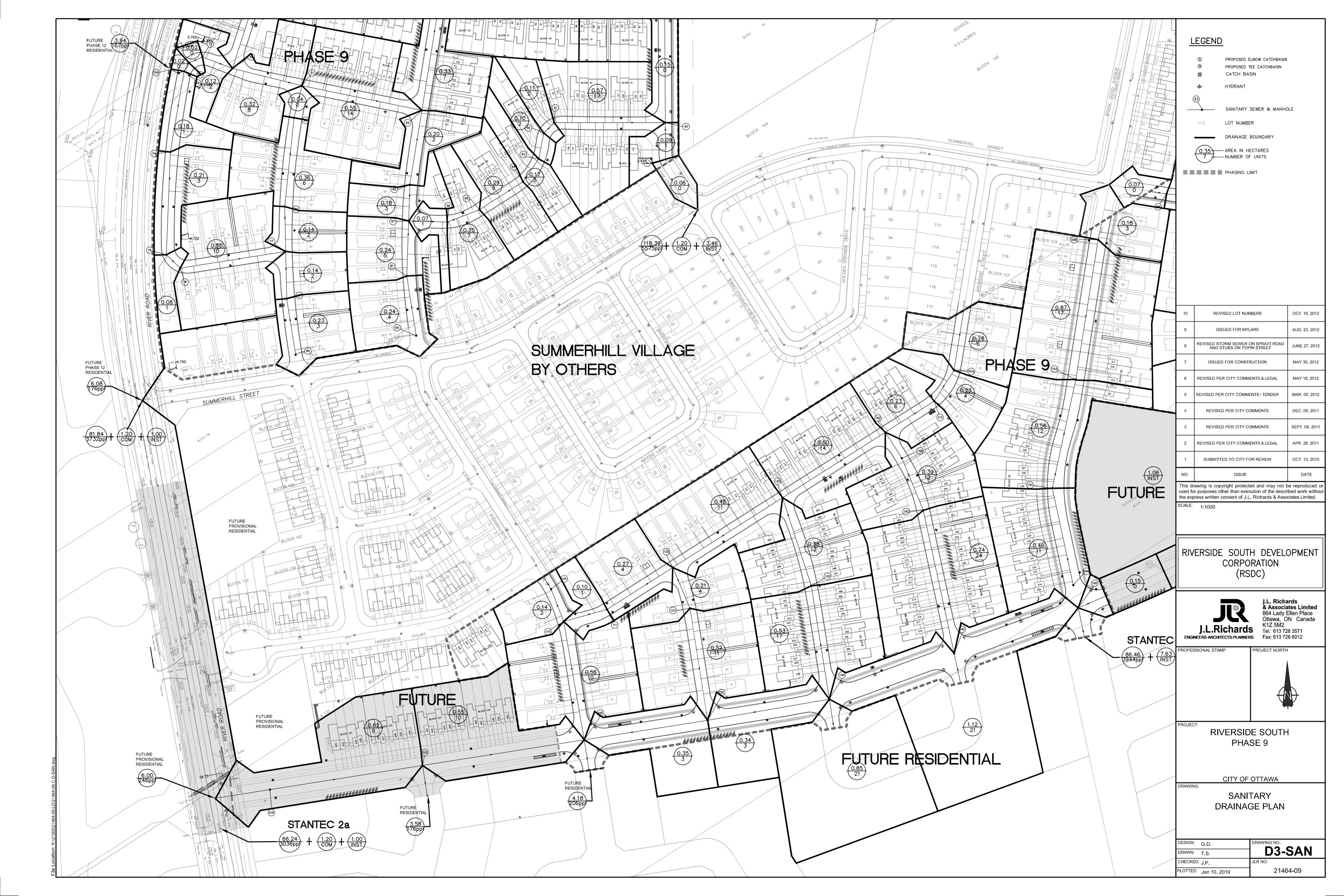
PROJECT: SUMMERHILL VILLAGE - PHASE 1

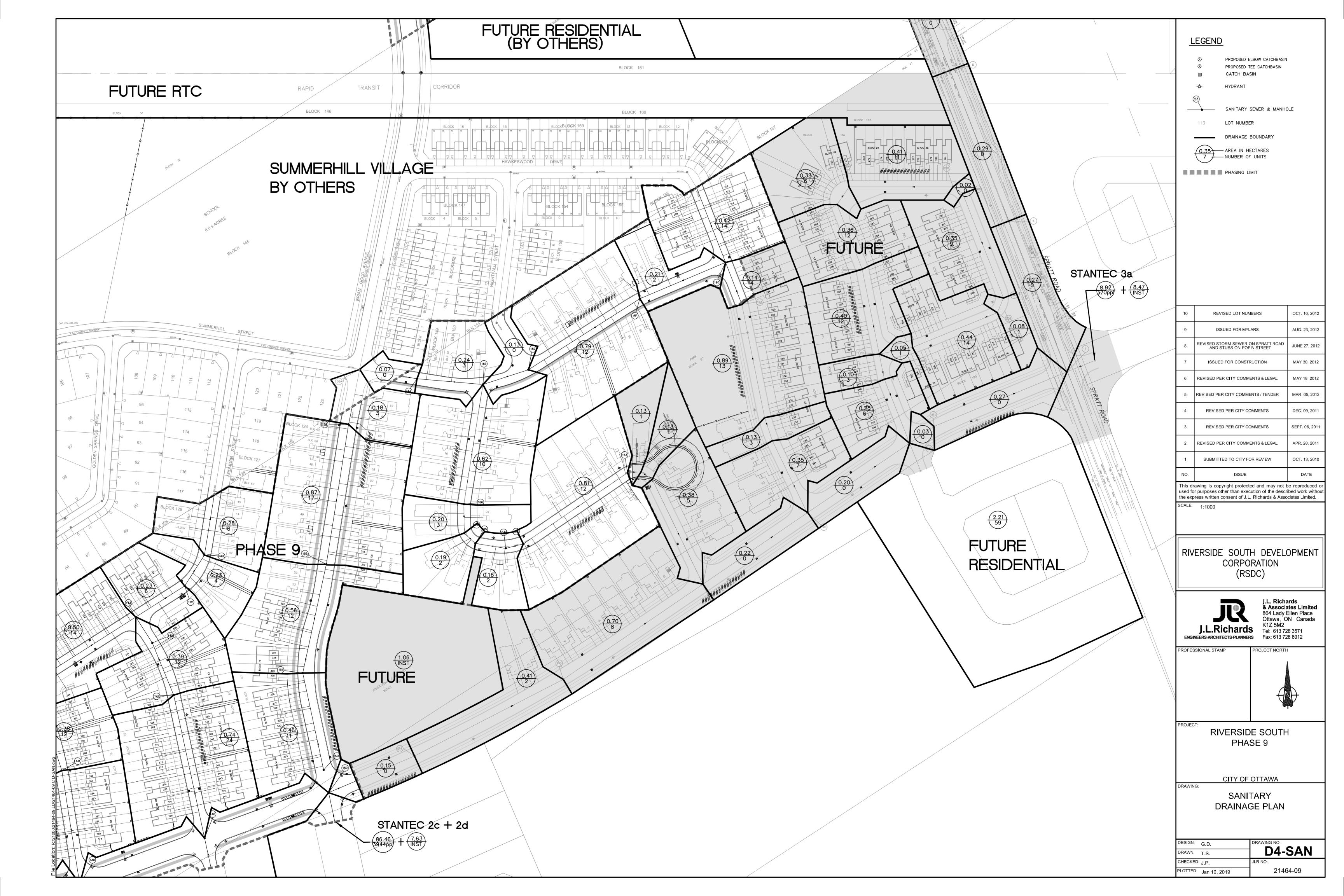
CLIENT: CLARIDGE HOMES

LOCATION							RESIDEN	ITIAL					INSTITU	TIONAL (OMMER	CIAL INDUSTR	RIAL	INFILTRA	TION ALLOY	NANCE	TOTAL			PROPOSE	D SEWER I	DESIGN	_	_
LOCATION				LINIT	TYPES		KEOIDEN	POPUL	ATION	CUMULAT	TIVE FLOW			AREA	(ha)					- FI	FLOW	Canaaltu	Pipe Size	Longth	Slope	Velocity(f)	Avail.	Cap.
Street	From	То	Singles	Semis		Stacked	Area	INDIV.	CUM.	Peaking	Peak Flow			COMME		INDUSTRIAL			Cum. Area	Flow (I/s)	(I/s)	(l/s)	(mm)	(M)	(%)	M/sec	Lis	(%)
Street	1 MH	мн	omg.cc		1.4.11.114		(Ha.)		043347000	Factor	(I/s)	Indiv	Cumm.	Indiv	Cumm.	Indiv Cumm	n. (I/s)	(Ha.)	(Ha.)	(115)	(1/5)	(1/3)	(iiiii)	()	17.97			
												1.00	4.00	4.00	4.20		-	76.19	76.19									
xternal (River Road South) Area 2a		MH160A					73.99	3417.0	3417.0			1.00	0.00	1.20	0.00			1.85	78.04									
xternal (River Road South) Area 2b		MH160A					1.85	68.0	3485.0			-	0.00		0.00		+	5.81	83.85									
xternal (River Road West) Area 2b		MH160A					5.81	246.0	3731.0 3731.0	3.36	50.79	0.00	1.00	0.00	1.20		1.91	0.19	84.04	23.53	76.23	141.88	525	58.60	0.10	0.64	65.65	46.2
	MH160A	MH160A					0.19 6.08	0.0 176.0	3907.0	3.30	30.73	0.00	1.00				0.00	6.08	6.08						0.40	0.04	61.58	42.7
External (River Road West) Area 2b	1 1 1 1 0 0 4	MH100A	5		-		0.49	16.0	3923.0	3.34	53.09	0.00	1.00	0.00	1.20		1.91	0.49	90.61	25.37	80.37	141.95	525	107.88	0.10	0.64	61.56	43.
Summerhill Street	MHTOUA	MH101A	3				0.40	10.0	.002010			ı ii								0.00	0.04	00.50	200	29.51	0.60	0.82	26.26	99
Vision Street	MH125A	MH126A			4		0.28	9.6	9.6	4.00	0.16						0.00	0.28	0.28	0.08	0.24 1.41	26.50 19.36	200	29.51	0.32	0.60	17.95	
ture Medium Residential		MH126A			32		0.62	76.8	76.8	4.00	1.24						0.00	0.62	0.62 1.61	0.17	2.67	26.50	200	107.43	0.60	0.82	23.83	
Vision Street		MH101A			21		0.71	50.4	136.8	4.00	2.22	\vdash					0.00	0.71	1.01	0.45	2.01	20.00		10.11.0				
			ĵ.								5170	-	4.00		1.20		1.91	0.14	92.36	25.86	82.49	141.88	525	83.00	0.10	0.64	59.39	41.
Summerhill Street	MH101A	MH102A					0.14	0.0	4059.8	3.33	54.72		1.00		1.20		1.01	0.11	02.00									
							0.00	40.0	42.0	4.00	0.19						0.00	0.30	0.30	0.08	0.27	48.70	200	26.00	2.03	1.50	48.43	
Haresfield Street		MH120A			5		0.30	12.0 48.0	12.0 48.0	4.00	0.78						0.00	0.37	0.37	0.10	0.88	0.00	200	17.00	0.00	0.00	-0.88	
iture Medium Residential		MH120A			12		0.37	28.8	88.8	4.00	1.44						0.00	0.45	1.12	0.31	1.75	0.00	200	61.73	0.00	0.00	-1.75 16.86	
		MH121A			16		0.45	38.4	127.2	4.00	2.06						0.00	0.51	1.63	0.46	2.52	19.38	200	65.89	0.32	0.60	16.50	
Haresfield Street Haresfield Street		MH122A MH116A			8		0.31	19.2	146.4	4.00	2.37						0.00	0.31	1.94	0.54	2.91	19.41	200	68.70	0.32	0.00	10.00	<u> </u>
Harestield Street	WITTIZZA	IVITTION	Information	n provide		chards(Sec	JLR spreadshee)								0.00	4.00	1.80	0.50	2.00	 	1					
Southbridge Street (External South)		Bulkhead					1.80	92.8	92.8	4.00	1.50						0.00	1.80 0.04	1.84	0.52	2.08	19.35	200	9.17	0.32	0.60	17.27	89
Southbridge Street	Bulkhead	MH116A					0.04	3.2	96.0	4.00	1.56	1	_		-		0.00	0.04	1.04	0.02	2.00	10.00						
											4.50	-					0.00	0.53	4.31	1.21	5.71	19.36	200	73.82	0.32	0.60	13.65	70
Southbridge Street	MH116A	MH117A	11				0.53	35.2	277.6	4.00	4.50	_			 		1 0.00	0.00										_
					200		0.05	00.0	28.8	4.00	0.47						0.00	0.35	0.35	0.10	0.57	28.63	200	37.56	0.70	0.88	28.06	
Gazebo Street		MH124A			12		0.35	28.8 7.2	36.0	4.00	0.58						0.00	0.13	0.48	0.13	0.71	28.63	200	53.84	0.70	0.88	27.92	97
Gazebo Street	MH124A	MH117A	A		3		0.13	1.2	30.0	4.00	0.00													00.01	0.00	0.60	12.28	63
0 11 11 - 011	N411447A	MH118A	10	-	1		0.50	32.0	345.6	4.00	5.60						0.00	0.50	5.29	1.48	7.08	19.36	200	66.24 24.27	0.32	0.60	12.25	
Southbridge Street Southbridge Street		MH102A	-				0.08	3.2	348.8	4.00	5.65						0.00	0.08_	5.37	1.50	7.15	19.40	200	24.21	0.02	0.00	12.20	100
Southbridge Street	IVITTION	WILLIOZA	1														101	0.45	97.88	27.41	88.24	141.79	525	36.04	0.10	0.64	53.55	37.
Summertime Street	MH102A	MH103A	2				0.15	6.4	4415.0	3.29	58.92	-	1.00		1.20		1.91	0.15 0.14	98.02	27.45	1			32.36	0.10	0.63	52.73	37
Summertime Street		MH104A	-				0.14	6.4	4421.4	3.29	59.00	-	1.00	-	1.20		1.91	0.14	30.02	21,40	00.00	1						
										1.00	0.05	-			-		0.00	0.09	0.09	0.03	0.08	26.42	200	9.56	0.60	0.82	26.34	
Rideau Lawn Crescent		MH131A			_		0.09	3.2	3.2 57.6	4.00	0.05						0.00	0.86	0.95	0.27	1.20	26.50	200	110.18	0.60	0.82	25.30	95
Rideau Lawn Crescent	MH131A	MH104A	17		_		0.86	54.4	37.6	4.00	0.00											000000000			0.40	0.04	50.07	20
		1405	6		-		0.33	19.2	4498.2	3.29	59.90		1.00		1.20		1,91	0.33	99.30	27.80	89.61	141.88	525	74.00	0.10	0.64	52.27	30
Summertime Street	MH104A	MH105/	4 6	-			0.33	10.2	4400.2	0.20	30.00								12724		0.05	00.54		60.49	0.60	0.82	26.16	98
Rideau Lawn Crescent	MH1307	MH132A	A 5	1	_		0.31	16.0	16.0	4.00	0.26						0.00	0.31	0.31	0.09	0.35		200	9.55	0.60	0.82	25.94	_
Rideau Lawn Crescent		MH133/					0.17	6.4	22.4	4.00	0.36				-		0.00	0.17	1.22	0.13	1.48			110.29	0.32	0.60	17.88	
Rideau Lawn Crescent		MH105/					0.74	48.0	70.4	4.00	1,14			1	+		0.00	0.74	1.22	0.34	1.40	15.50	200	110.20	1			
Tipose aprili biografii	1							18170	79,902,007,2		00.01	-	1.00	¥	1.20		1.91	0.31	100.83	28.23	91.05	141.88	525	73.99	0.10	0.64	50.83	35
Summertime Street	MH105A	MH106A	A 5				0.31	16.0	4584.6	3.28	60.91	1	1.00	+	1.20		1.51	0.01	100.00		1							
					v					4.00	0.16	\vdash	 	-	+ -		0.00	0.21	0.21	0.06	0.22			12.15	0.75	0.91	29.39	
Hawkeswood Drive		MH143/		_	4	+	0.21	9.6 33.6	9.6	4.00	0.70	+	 	1	1		0.00	0.41	0.62	0.17				61.20	0.75	0.91	28.76	
Hawkeswood Drive		MH144/		-	14	-	0.41	36.0	79.2	4.00	1.28						0.00	0.39	1.01	0.28	1.56	37.48	200	58.93	1.20	1.16	35.92	95
Hawkeswood Drive	MH144/	MH145/	<u> </u>	-	15		0.39	50.0	10.2	1.00	1,100									6.11		00.40	200	GE 44	0.60	0.82	25.81	97
Nightfell Circui	MH447	MH148/	<u> </u>	-	14		0.50	33.6	33.6	4.00	0.54						0.00	0.50	0.50	0.14	0.68	26.49 26.49	200 200	65.41 37.72	0.60	0.82	25.80	
Nightfall Street Nightfall Street		MH145			1-14	1	0.05	0.0	33.6	4.00	0.54						0.00	0.05	0.55	0.15	0.69	26.49	200	31.12	0.00	0.02	20.00	1
Mightiali Street	140/	T WILLIAM													-		0.00	0.47	2.03	0.57	3.02	19.34	200	75.41	0.32	0.60	16.32	84
Hawkeswood Street	MH145/	MH146/	A		16		0.47	38.4	151.2	4.00	2.45	-		-	-		0.00	0.47	2.35	0.57	3.30	19.35	200	64.39	0.32	0.60	16.05	82
Brian Good Avenue		MH149			5		0.32	12.0	163.2	4.00	2.64	-	-	+	-	+	0.00	0.32	2.68	0.75	3.71	19.38	200	72.35	0.32	0.60	15.67	80
Brian Good Avenue	MH149	MH108/	A		8		0.33	19.20	182.40	4.00	2.96		_				0.00	7.00		1								
esigned:			for City Co			08/2011	Population Per l	Jnit:	3.2	For Single				ICI Rate	is.	Peak	Factor	Infiltration	n Allowance	e: 0.2	8 l/sec/h	ła	Assum	ed pipe roug	hness coef	ficient =	0.01	3
P.K.			or City Com			07/2011	4		2.4 1.9	Townhous Mixed Use) I/ha/day												
			or City Com		_	05/2011	A D C	Flour Botos	1.9 350	I/day				Commerci	al 50000) I/ha/day	1.5	1				1						
hecked:			or City Com			3/2011	Avg. Per Capita Residential Peal		300	iruay			Ι `	Industri	al 35000) I/ha/day MOE	Guidelines	1										
J.I.M.	1. Subm		or City Com	ments		DATE	Harm	ion Formula = 1	+(14/(4+P^0.5)) where P	pop'n in the	ousands	1			•		1				1						
	0.00		VISION) etc.	-	eet No.	1	.c onaia = 1	(()	,,								1										
Dwg Reference:		e Ref: i6 - 5.7	III	Date: 2/2011		of 3	1						1					1										







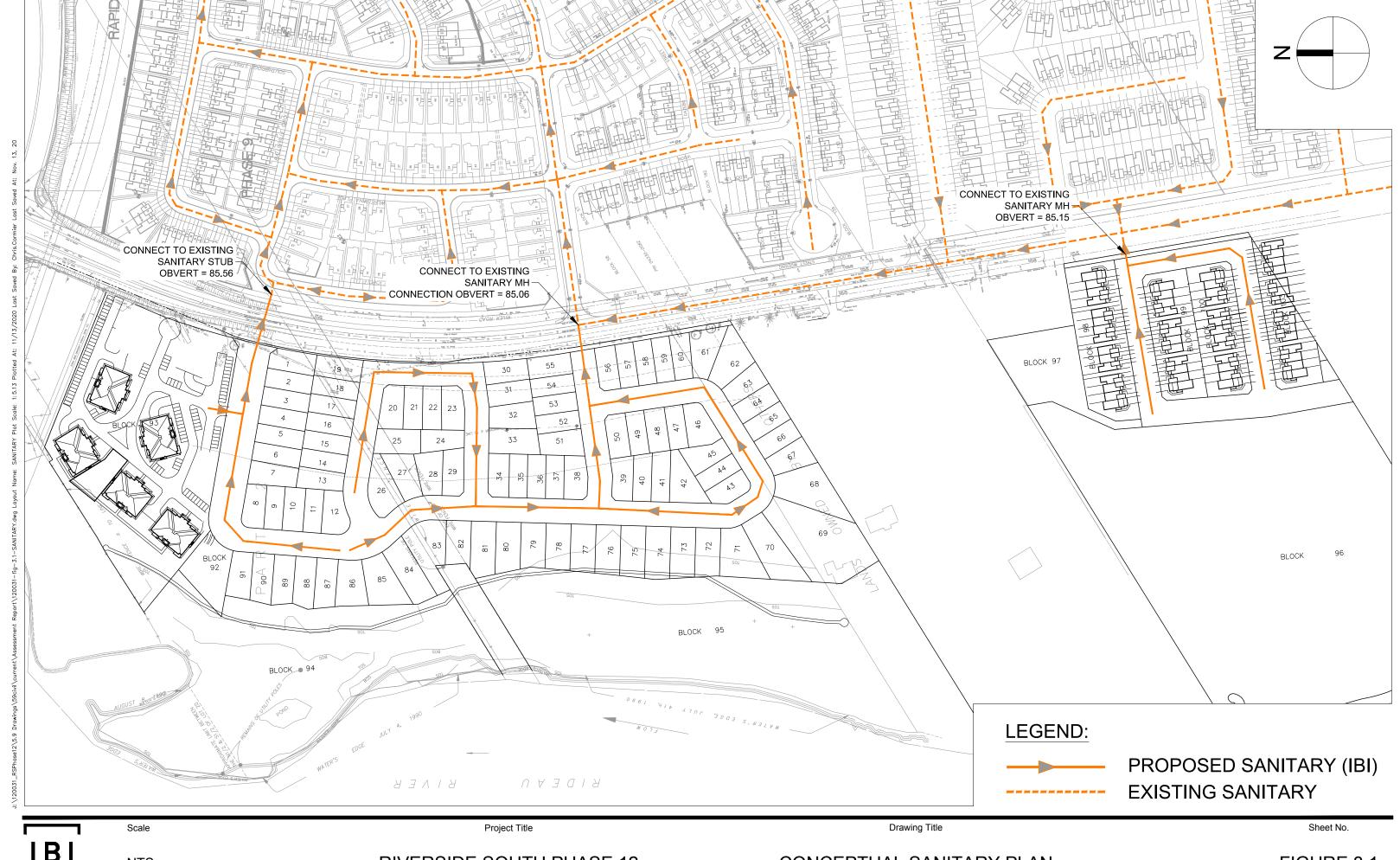


CITY OF OTTAWA RIVERSIDE SOUTH DEVELOPMENT CORPORATION **RIVERSIDE SOUTH PHASE 9**

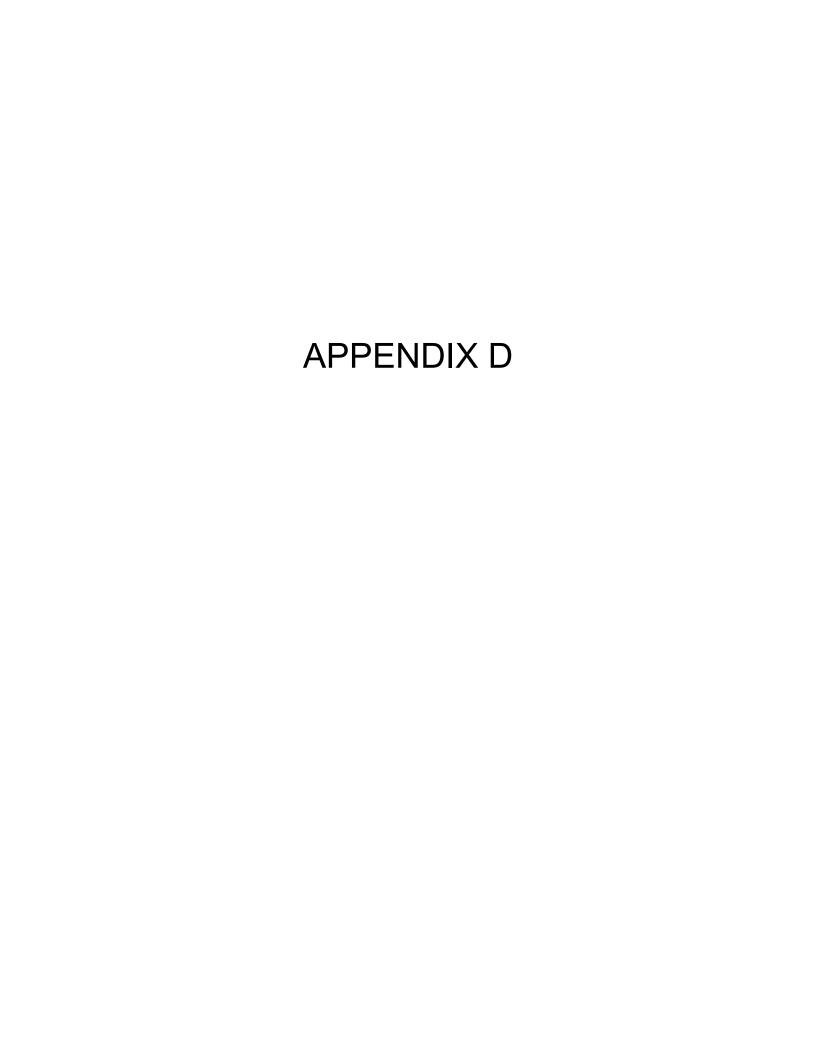
SANITARY SEWER CALCULATION SHEET

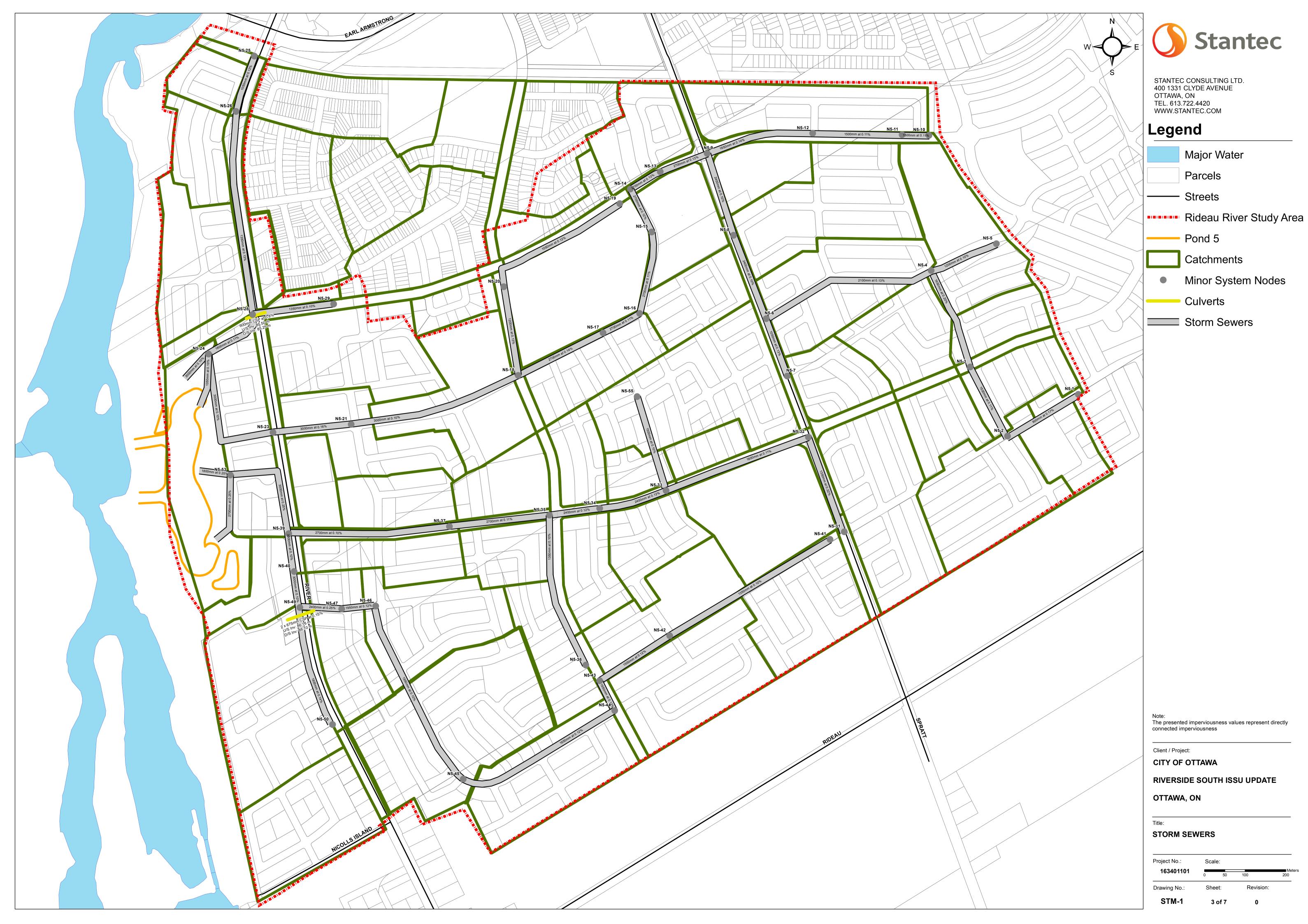
DESIGN PARAMETERS G.C. Dumencu, EIT Riverside South Development Corporation LEGEND = 50,000 L/d/ha (Peaking Factor = 1.5)
= 50,000 L/d/ha (Peaking Factor = 1.5)
= 35,000 L/d/ha (Peaking Factor = Per MOE Graph)
= 0.28 L/s/ha
= 0.013 pers/unit pers/unit pers/unit L/cap/d Commercial Institutional DENOTES FUTURE OR EXISTING SEWERS, AND EXTERNAL FLOWS Population Density (Stacks, Towns)
Population Density (Mixed) 2.4 1.9 DENOTES AS-CONSTRUCTED INFORMATION (MEASURED)
DENOTES AS-CONSTRUCTED INFORMATION (CALCULATED) J.L. Párraga, P.Eng City of Ottawa Light Industrial Infiltration (Residential) Per Capita Flow (Residential) JLR NO.: Dec-11 Feb-12 Manning's Coefficient, n 21464-09 Oct-11 May-12 Sep-12 FINAL Oct-12

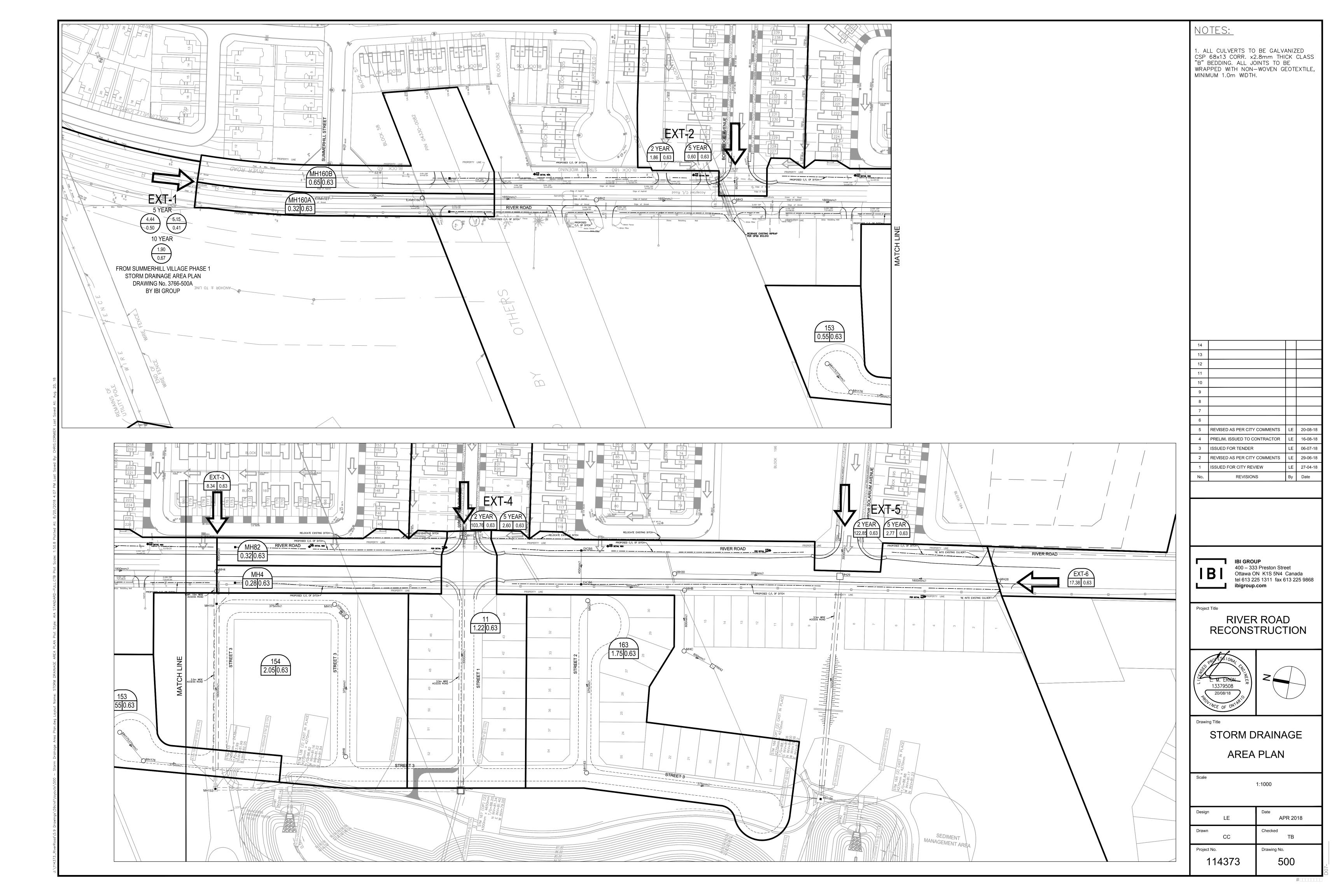
								RESIDENT																														т	
								RESIDENT					COMMERC	AL		INSTITU	TIONAL		ICI	INFILTRA		Peak				EWER DAT		_			TREAM				DOWNSTR	_		₫	
STREET	PHASE	1	MH NUMBER		NUME Towns Star	BER OF U				CUMULATIVE Pop. Area			Cum. Area Area	Comm. Flow		Cum. Area			reak ICI Tota Flow Are				Qd/Qcap		Slope Q fu (%) (L/s		V partial Le		Prop. O centreline [Obvert	Invert C		Prop. Obve Centreline Drop	ert Obver	Invert	Cover	REMARKS	CAPACITY OK?
		FROM	то	Singles	Iowns Star			Pop. Ar people) (h		eonle) (ha)		Flow (L/s)	Area Area (ha) (I/s)	(I /e)	(ha)			(L/s)	(L/s) Are			(L/s)		(mm)	(%) (L/s	s) (m/s)	(m/s)	(m) C	entreine	Jrop				entreline Drop	'				OK?
Northwest Quadrant (Flow North to Ex. S	tub in Danid			dy Way)	+ +	Oil	into (p	people) (ii	на) (р	eopie) (IIa)	-	(L/5)	(Ha) (L/5)	(L/5)	(IIa)	(D5)		(115)	(DS) (Ha	(IIa)	(L/5)	(L/s)	1	H				- H -			-						_	 	+
BALLINVILLE CIRCLE		74	75	T 2		-	3	10 0.	.21	10 0.21	4.00	0.16				_			0.2	1 0.21	0.06	0.21	0.01	200	0.62 26.9	91 0.83	0.22 7	2.94	89.86	-	6.660	86.521	3.20	89.84	86.20	86.070	3.63		Y
BALLINVILLE CIRCLE	9	75	76	- 1						13 0.29									0.0				0.01		0.62 26.8				89.84					89.88	86.14			+	Y
BALLINVILLE CIRCLE	0	76	77	10						45 0.84									0.5				0.04		0.44 22.0				89.88					89.80	85.84			+	Y
BALLINVILLE CIRCLE	9	76	- "	10		- 19	10	32 0.	.55	45 0.04	4.00	0.73			_			-	0.5	0.04	0.24	0.96	0.04	200	0.41 21.8	93 0.00	0.35 /	3.05	09.00	- '	0.149	00.010	5.73	09.00	05.041	05.710	3.95		-
WILHELMINA PLACE		80	81	2			3	10 0.	.23	10 0.23	4.00	0.16							0.2	3 0.23	0.06	0.22	0.01	200	0.73 29.2	22 0.00	0.23 3	8.65	89.68		6.427	86.302	3.25	89.53	86.145	86.020	3.38	+	Y
WILHELMINA PLACE	9	81	77	3						16 0.23									0.1				0.01		0.73 29.2				89.53					89.80 0.12					, ,
WILHELMINA PLACE	9	01	- 11				2	b U.	.14	16 0.37	4.00	0.26						_	0.1	¥ U.37	0.10	0.30	0.01	200	0.55 25.3	30 0.70	0.20	11.07	69.53		0.145	00.012	.30	09.00 0.12	1 65.970	00.03	3.03		1
		-					_	_	_							_						+	1	-		_													_
WILHELMINA PLACE	_	77	82	_			2	6 0.	.14	67 1.35	4.00	1.09						_	0.1	1.35	0.38	1.47	0.07		0.40 21.6		0.41 3	0.79	89.80		5.849		3.95	89.62	85.726	85,592	2 3.89		Y
WILHELMINA PLACE	9	82	82	2																									89.62		5.726			89.62					Y
	9			6		6	6											-	0.3				0.09		0.40 21.6										85.482				
WILHELMINA PLACE	9	83	71	1	-	_		0.	.04	86 1.75	4.00	1.40	1 1		_				0.0	1.75	0.49	1.89	0.08	200	0.45 22.9	5 0.71	0.45 2	1./8	89.75	8	5.482	85.322	1.27	90.00 0.21	5 85.384	85.224	4.62	 	Y
0.411.00.00.00.00.00.00.00.00.00.00.00.00.0				1										1		1					0.4-	1	H	H														 	-
BALLINVILLE CIRCLE	9	74	73	1	1	1	1	3 0.	.18	3 0.18	4.00	0.05							0.1	0.18	0.05	0.10	0.00	200	0.65 27.6	51 0.85	0.16 5	3.31	89.86	8	5.877	85.737	3.98	89.73	85.530	85.390	4.20		Y
																		_																					
BALLINVILLE CIRCLE	FUT	STUB	73	11	55	66	56	167 3.	.94	167 3.94	4.00	2.71							3.9	3.94	1.10	3.81	0.19	200	0.33 19.6	66 0.61	0.49	9.00	89.87	8	5.560	85.360	1.31	89.73	85.530	85.330	4.20	Cross Over - River Road STM OBV 84.97	
BALLINVILLE CIRCLE	9	73	72A							170 4.14		2.76							0.0				0.20		0.33 19.5			7.32			5.530			89.78	85.500				Y
BALLINVILLE CIRCLE	9	72A	72							170 4.16									0.0						0.49 23.9			0.18						89.88		85.306			Y
BALLINVILLE CIRCLE	9	72	49	1	1	2	2	6 0.	.12	176 4.28	4.00	2.85							0.1	2 4.28	1.20	4.05	0.18	200	0.45 23.0	0.71	0.54 2	0.72	89.88	8	5.456	85.301	1.42	90.10	85.362	85.207	4.74		Y
MATTINGLY WAY	9	48 (S)	49		11	11	11	26 0.	.42	26 0.42	4.00	0.43							0.4	0.42	0.12	0.55	0.01	200	1.36 39.8	34 1.23	0.42 7	4.50	90.16	8	6.372	86.232	3.79	90.10	85.362	85.222	4.74		Y
BALLINVILLE CIRCLE	9	49	71	4	4	8	8	22 0.	.32	225 5.02	4.00	3.64							0.3	5.02	1.41	5.05	0.23	200	0.40 21.5	55 0.66	0.57 4	8.65	90.10	8	5.362	85.200	1.74	90.00	85.169	85.007	7 4.83		Y
BALLINVILLE CIRCLE	9	71	64	5	9	14	14	38 0.	.55	349 7.32	4.00	5.65							0.5	7.32	2.05	7.70	0.13	300	0.33 58.2	0.80	0.59 8	3.84	90.00	8	5.169	84.950	1.83	90.10	84.890	84.671	5.21		Y
SOUTHBRIDGE STREET	9	60	61	4		4		13 0.		13 0.24		0.21							0.2			0.27	0.01			33 0.86			89.77					89.65	86.190				Y
SOUTHBRIDGE STREET	9	61	57	4	1	5	5	15 0.	.24	28 0.48	4.00	0.45							0.2	0.48	0.13	0.59	0.03			74 0.67			89.65					90.00	86.039	85.911	3.96		Y
SOUTHBRIDGE STREET	9	57	62	2	1	3	3	9 0.		37 0.66	4.00	0.60							0.1	0.66	0.18				0.58 26.1			4.13	90.00		6.039	85.911	1.96	89.77	85.898	85.770	3.87		Y
SOUTHBRIDGE STREET	9	62	64	- 1	2	3	3	8 0.	.20	45 0.86	4.00	0.73							0.2	0.86	0.24	0.97	0.03	200	0.84 31.2	29 0.96	0.43 5	0.00	89.77	8	5.898	85.761	1.87	90.10 0.59	0 85.480	85.343	4.62		Y
SOUTHBRIDGE STREET	9	64	46		7	7	7	17 0.	.33	410 8.51	4.00	6.65							0.3	8.51	2.38	9.03	0.16	300	0.30 54.9	99 0.75	0.56 8	4.14	90.10	8	4.890	84.669	i.21	90.20	84.640	84.419	5.56		Y
MATTINGLY WAY	9	48 (E)	47		2	2	2	5 0.		5 0.10	4.00	0.08							0.10	0.10	0.03	0.11	0.00		0.73 29.2				90.16			86.412	1.64	90.17	86.444	86.337	3.73		Y
MATTINGLY WAY	9	47	46		31	31	31	74 0.	.96	79 1.06	4.00	1.28							0.9	1.06	0.30	1.58	0.04	200	1.58 43.0	02 1.33	0.63 11	14.13	90.17	8	6.444	86.336	1.73	90.20	84.640	84.532	5.56		Y
MATTINGLY WAY	9	46	45		25	25	25	60 0.	.79	550 10.36	3.95	8.80							0.79	10.36	2.90	11.70	0.21	300	0.29 54.7	79 0.75	0.61 9	2.21	90.20	8	4.640	84.394	i.56	90.05	84.368	84.122	5.68		Y
MATTINGLY WAY	9	45	43	1	15	15	15	36 0.	.46	586 10.82	3.94	9.34							0.4	10.82	3.03	12.37	0.22	300	0.32 56.8	31 0.78	0.65 5	8.66	90.05	8	4.368	84.111	i.68	90.00	84.182	83.925	5.82		Y
		1		1	1 1								1										1																
									_														1																
TENNANT WAY	9	57 (E)	56	1	1	1	1	2 0.	.07	2 0.07	4.00	0.04							0.0	7 0.07	0.02	0.06	0.00	200	0.42 22.1	16 0.68	0.12 2	5.76	90.00	8	6.378	86.222	1.62	89.75	86.270	86.114	3.48		Y
TENNANT WAY	9	56	55	1	7	7				19 0.32									0.2				0.02		0.37 20.9				89.75		6.270			89.75	86.183				Y
TENNANT WAY	9	55	54	1	9	9	9	22 0.		41 0.61		0.66			1				0.2				0.04			33 0.68			89.75					89.93	86.036				Y
TENNANT WAY	9	54	53	1	5					53 0.78				1					0.1				0.05			78 0.67			89.93		6.036			90.03	85.958				Y
TENNANT WAY	9	53	52	1	2					58 0.88		0.93		1					0.10			1.18	0.05			27 0.72			90.03					90.13	85.896				Y
TENNANT WAY	9	52	51	1	2			5 0.		62 0.99		1.01			1				0.1			1.29	0.06			74 0.67			90.13					90.11	85.854			 	Ÿ
TENNANT WAY		51	42	t -	17		_	41 0.		103 1.56			1 1	_	1	+			0.5				0.10		0.40 21.7				90.11		5.854			90.07 1.24				Drop Pipe	Y
				-	T			0.		1.00	7.00	1.07	+ + +	+					0.5	1.30	0.44		0.10	200	22.0	0.00	3.40	/0			554			1.24	- 00.04	00.370			

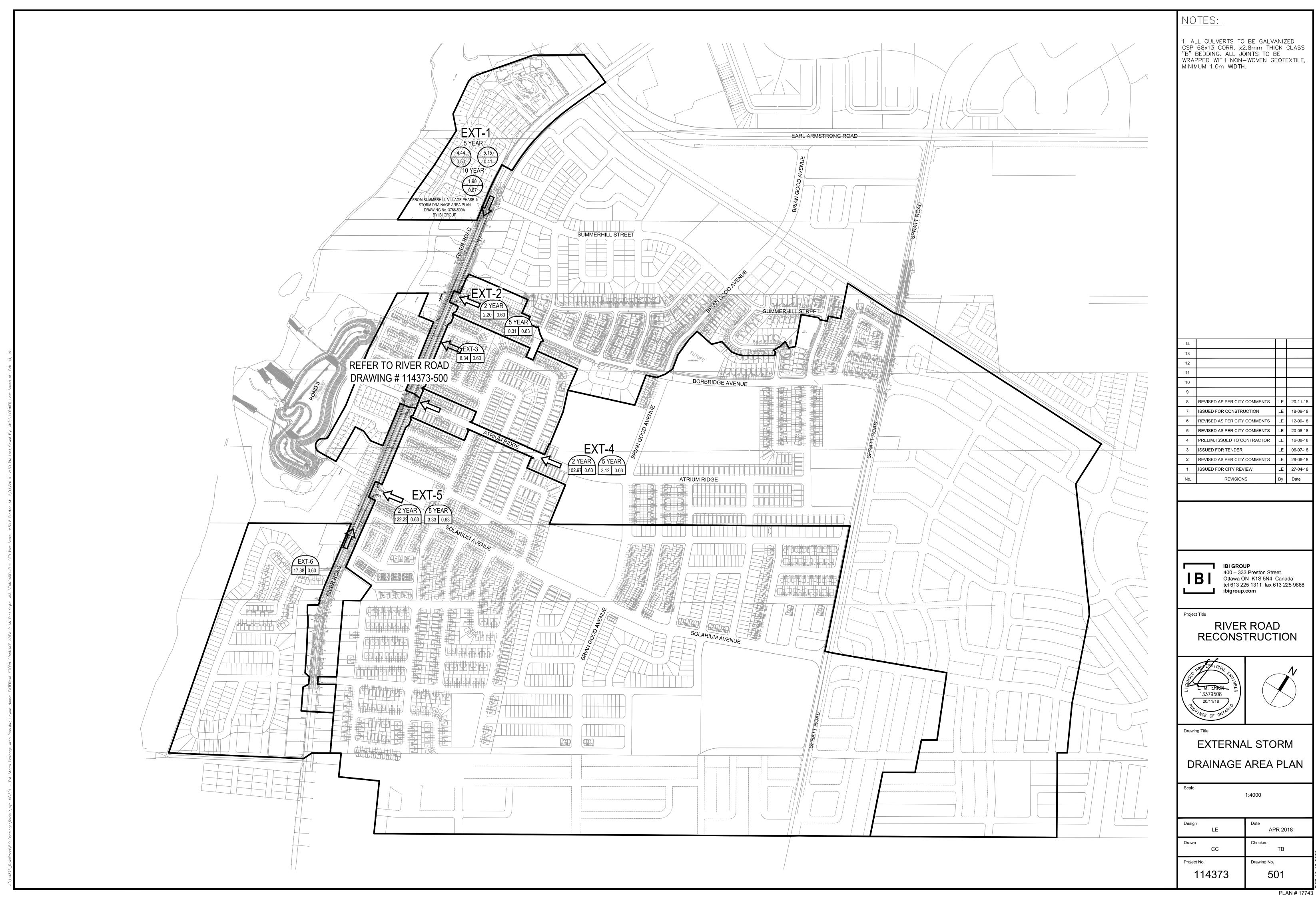


NTS











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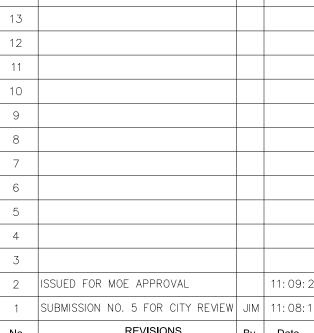
River Road City of Ottawa Riverside South Development Corporation

	LOCATION				AREA	(Ha)									RATION	AL DESIGN	FLOW				T						SEWER DA	TA		
				Existing C=	Single Family C= C=	Townhouse C= C=	Walden C=	2 Yea		Year	IND	Year CUM	INLET	TIME	TOTAL	i (2)	i (5)	i (10)	2yr PEAK	5yr PEAK	10yr PEAK	FIXED	DESIGN	CAPACITY	LENGTH	PE SIZE (m	n SLOPE	VELOCITY	Y AVA	IL CAP
STREET	AREA ID	FROM	ТО						78AC 2.78A			1		IN PIPE	(min)	(mm/hr)	(mm/hr)	` '	1 -	-	_		FLOW (L/s)		(m)	DIA	(%)	(m/s)	(L/s)	
North Outlet																														
River Road	EXT-1		EXMH160		5.15 4.44		1.90	0.00	0.00 12.04	1 12.04	3.54	3.54	12.78			67.56	91.50	107.20	0.00	1,101.80	379.36		1,481.16							
River Road	160A&B	EXMH160	MH2			0.9	7	0.00	0.00 1.70	13.74	0.00	3.54	12.78	1.45	14.23	67.56	91.50	107.20	0.00	1,257.24	379.36		1,636.60	3,006.86	118.40	1650	0.10	1.362	1370.26	45.57%
River Road		MH2	MH3					0.00	0.00 0.00	13.74	0.00	3.54	14.23	1.15	15.37	63.66	86.14	100.89	0.00	1,183.64	357.06		1,540.70	3,006.86	93.83	1650	0.10	1.362	1466.16	48.76%
Borbridge Avenue	EXT-2	CAP	MH3			1.86 0.60	0	3.26	3.26 1.05	1.05	0.00	0.00	12.56	0.21	12.77	68.21	92.39	108.24	222.21	97.08	0.00		319.29	572.93	25.02	600	0.80	1.963	253.64	44.27%
River Road		MH3	MH4					0.00	3.26 0.00	14.79	0.00	3.54	15.37	1.49	16.87	60.90	82.37	96.45	198.38	1,218.32	341.34		1,758.04	3,792.13	129.25	1800	0.10	1.444	2034.09	53.64%
Capricorn Circle	EXT-3, 83	CAP	MH4			8.34 0.32	2	14.61	14.61 0.56	0.56	0.00	0.00	16.67	0.22	16.89	58.09	78.53	91.94	848.57	44.01	0.00		892.58	1,117.30	22.89	900	0.35	1.701	224.72	20.11%
Street No. 3 West		MH4	MH154			0.28 0.28	8	0.49	18.35 0.49	15.84	0.00	3.54	16.87	0.26	17.12	57.69	77.98	91.29	1,058.82	1,235.29	323.06		2,617.18	3,792.13	22.11	1800	0.10	1.444	1174.95	30.98%
Street No. 3 West	154	MH154	CAP			2.05		3.59 2	21.95 0.00	15.84	0.00	3.54	17.12	1.36	18.48	57.17	77.28	90.47	1,254.71	1,224.20	320.15		2,799.06	3,792.13	117.91	1800	0.10	1.444	993.07	26.19%
Atrium Ridge	EXT-4	CAP	MH11			103.76 2.60	0	181.73 1	81.73 4.55	4.55	0.00	0.00	33.75	0.08	33.83	36.97	49.75	58.15	6,718.47	226.56	0.00		6,945.03	14,807.43	9.29	3000	0.10	2.029	7862.40	53.10%
Street No. 1 West	11	MH11	CAP			1.22		2.14 1	83.86 0.00	4.55	0.00	0.00	33.83	1.33	33.75	36.91	49.68	58.06	6,786.97	226.21	0.00		7,013.18	14,807.43	162.00	3000	0.10	2.029	7794.25	52.64%
South Outlet																														
River Road	EXT-6		MH28			17.38		30.44	30.44 0.00	0.00	0.00	0.00	16.67			58.09	78.53	91.94	1,768.36	0.00	0.00		1,768.36							
River Road		MH28	MH29					0.00	30.44 0.00	0.00	0.00	0.00	16.67	1.05	17.72	58.09	78.53	91.94	1,768.36	0.00	0.00		1,768.36	4,486.91	107.73	1800	0.14	1.708	2718.55	60.59%
Solarium Avenue	EXT-5	CAP	MH29			122.85 2.77	7	215.16 2	45.60 4.85	4.85	0.00	0.00	23.33	0.27	23.60	47.22	63.69	74.51	11,597.38	309.00	0.00		11,906.38	14,807.43	33.00	3000	0.10	2.029	2901.05	19.59%
River Road		MH30	MH29					0.00	0.00	0.00	0.00	0.00	10.00	1.65	11.65	76.81	104.19	122.14	0.00	0.00	0.00		0.00	129.34	112.57	375	0.50	1.134	129.34	100.00%
		MH29	CAP					0.00 2	76.04 0.00	4.85	0.00	0.00	23.60	1.17	24.78	46.87	63.22	73.95	12,938.66	306.70	0.00		13,245.36	14,807.43	142.90	3000	0.10	2.029	1562.08	10.55%
Roadside Ditch Conve	eyance																													
Culvert STA 1+280	S1B, S2B*	MHA	Outlet																			190*	325.00	2,178.02	28.32	900	1.33	3.317	1853.02	85.08%
Culvert STA 1+680	S3B, XS4B*	DICB3	DICB4																			137*	150.00	162.91	23.00	450	0.30	0.992	12.91	7.93%
	S3A, XS4A*	DICB4	MHB																			116*	311.00	350.85	70.37	600	0.30	1.202	39.85	11.36%
		MHB	MHC																				311.00	350.85	41.32	600	0.30	1.202	39.85	11.36%
		MHC	HW42																				311.00	350.85	22.06	600	0.30	1.202	39.85	11.36%
Definitions:				Notes:									Designed:		LME			No.				Povi	sion						Date	
Q = 2.78CiA, where:					nings coefficient ((n) = 0.0	13						Dosignicu.		_171_			1.				City submis	ssion No. 1					27-0	04-2018	
Q = Peak Flow in Litres A = Area in Hectares (H				*	Drainage Areas _I	per Figure 4.3	3 and 100 y	ear flows fr	om Table 4.2	of the Des	ign Brief		Checked:					2. 3.				City submis)7-2018)8-2018	
i = Rainfall intensity in i [i = 732.951 / (TC+6.	millimeters per hou	r (mm/hr) 2 YEAR			<u> </u>	. 5	,		_		-		-									,	-							
[i = 998.071 / (TC+6.	053)^0.814]	5 YEAR											Dwg. Refer	ence:		114373-500)		File Defe				5	•					of No.	
[i = 1174.184 / (TC+6	o.U14)^U.816]	10 YEAR																	File Referenc 114373.5.7.1				Dat 8/20/2						eet No: of 1	

Inlet Time

External Draiinage Area	Length of Pipe Upstream (m)	Velocity (m/s)	Travel Time (min)	Inlet Time (min)
EXT-1	250	1.50	2.78	12.78
EXT-2	230	1.50	2.56	12.56
EXT-3	600	1.50	6.67	16.67
EXT-4	2,850	2.00	23.75	33.75
EXT-5	1,600	2.00	13.33	23.33
EXT-6	600	1.50	6.67	16.67





J.I.M.	JULY '10
Drawn M.M.	Checked P.K.
Project No.	Drawing No.
3766	500A

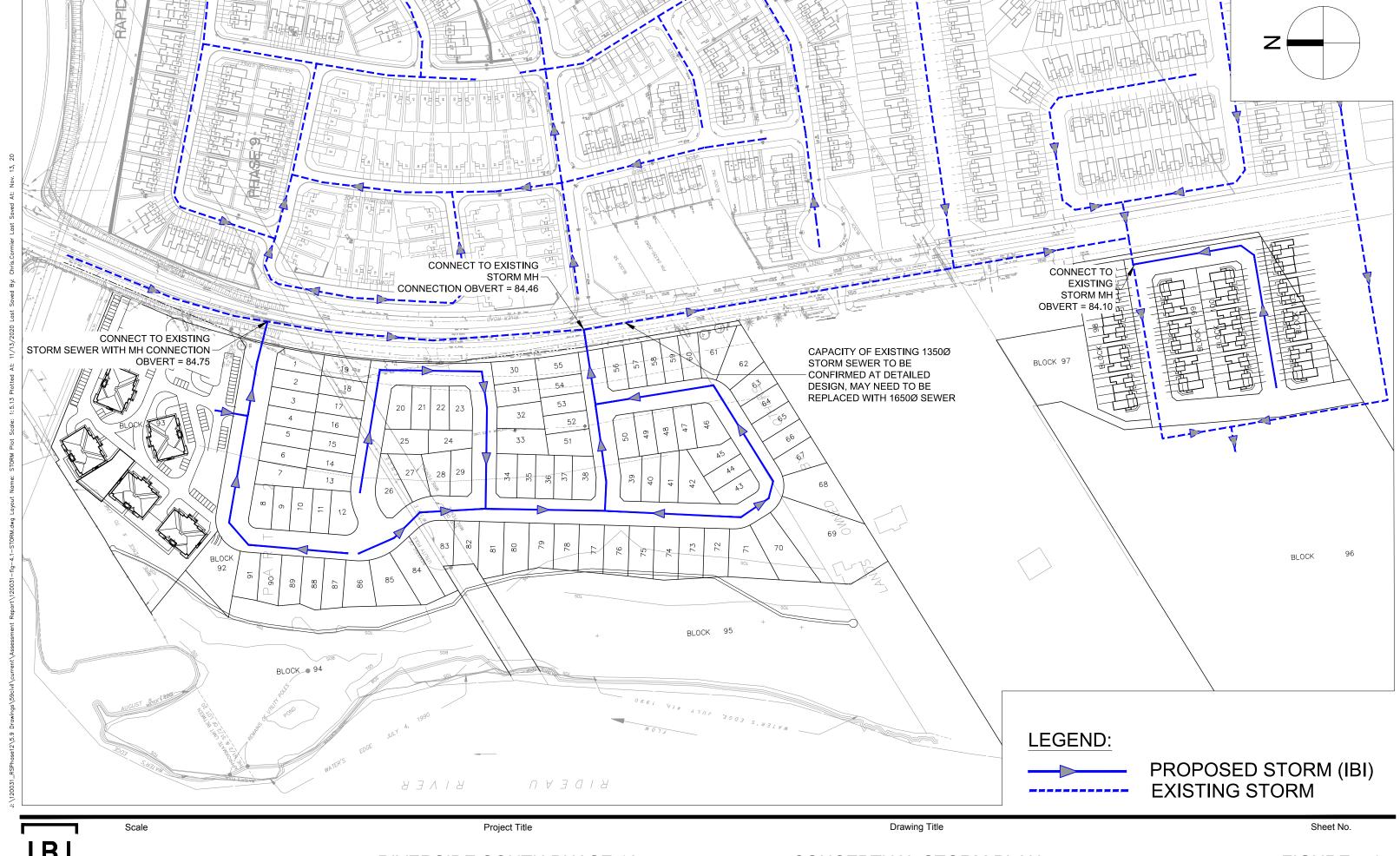


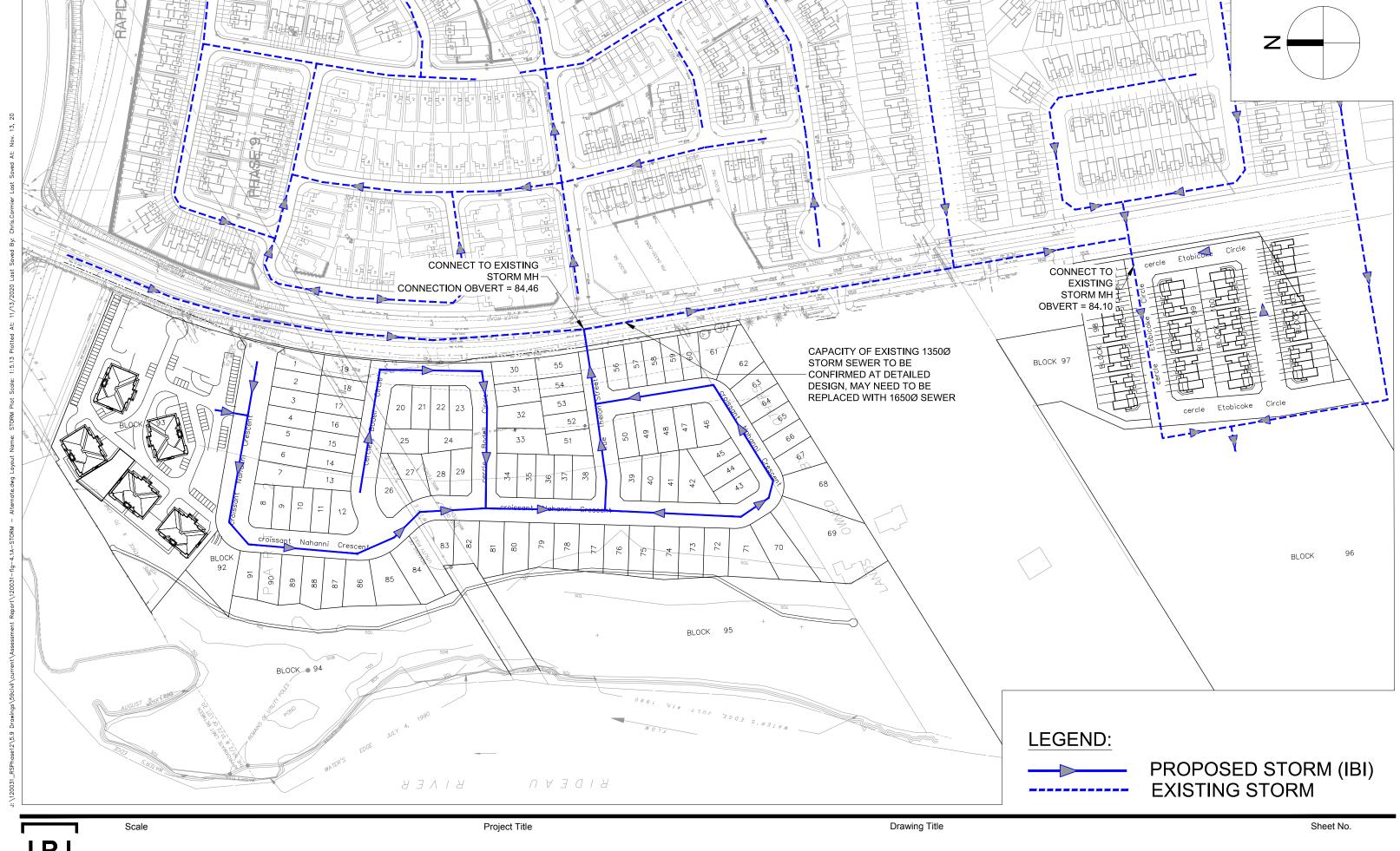
IBI Group 333 Preston Street - Suite 400 Ottawa, Ontario K1S 5N4

STORM SEWER DESIGN SHEET

PROJECT: SUMMERHILL VILLAGE - PHASE 1 LOCATION: CITY OF OTTAWA CLIENT: CLARIDGE HOMES

	LOCATION			_				AREA (H	a)	_				RATIO	ONAL DES	IGN FLOW			GENERIC CAP	TURE RATE	s				SEWER			2.72
	LOCATION	FROM	то	C=	C=	C=	C= I	C=	C=	C=	INDIV.	ACCUM.	INLET	TIME	TOTAL	1	PEAK		REA (ha)	FLOW			LENGTH	7000 89	SLOPE	VEL.	AVAIL.	
5	STREET	MH	MH	0.20		0.41			0.67		2.78AC	1 - 1 - 1 - 1 - 1 - 1 - 1	(min.)	IN PIPE		(mm/Hr)	FLOW (L/s)	INDIV.	ACCUM.	INDIV.	ACCUM.	(L/s)	(M)	(mm)	(%)	(M/s)	(L/s)	(%)
																07.04	704.04	0.04	8.37	19.92	694.71	900.98	85.52	1050	0.10	1.008	199.14	22.10%
Sumr	merhill Street	MH108	MH109		0.24				_	_	0,27	10.33	21.09	1.41	22.51	67.94	701.84	0.24	6.37	10.02	054.71	300.30	00.02	1000				
			N414400		0.00		1.54	4.23			8.10	8,10	Tc = 22.7	S areas ar	nd pipe inf	o from J.L.	Richards (Sec	JLR spr	eadsheet in Ap	pendix F)				975	0.12			
	eet (External South)	MH139	MH139 MH109		0.26	-	1,04	4.23			0.75		22.75	1.83						55.61	556.10	739.10	105.45	975	0.10	0.959	166.15	22.48%
Ardi	more Street	WILLIOS	WITTOS		0.07																							
																15min = 20.		0.40	0.40	204.18	204.18	239.62	10.00	600	0.14	0.821	51.07	21.319
	School	Bulkhead	MH109		2.46						2.74	2.74	20.67	0.20	20.87	68.81	188.55	2.46	2.46	204,10	204.10	200.02	10.00	- 550				
		1111100	NU1440	_	-		_				0.00	21.92	24.58	0.52	25.10	61.57	1,349.61	0.00	17.53	0.00	1454.99	1,761.25	37.18	1350	0.10	1.192	411.64	23.37%
	merhill Street merhill Street	MH109 MH110	MH110 MH111	-	0.18						0.20		25.10					0.18	17.71	14.94	1469.93	1,761.25	47,21	1350	0.10	1.192	417.86	23.729
Sumi	mermi Sireet	WITTIO	IVIIIII	1	0.10																F4.40	04.44	444.22	375	0.25	0.802	17.07	18.679
Golder	n Spring Drive	MH135	MH111		0.80						0.89	0.89	15.00	2.38	17.38	83.56	74.37	0.80	0.80	54.40	54.40	91.44	114.33	3/3	0,25	0.002	17.07	10.0.7
	n - Comba								_		0.00	00.04	05.70	0.52	26.29	59.70	1,373.80	0.00	18.51	0.00	1536.33	1,761.25	37.36	1350	0,10	1.192	387.45	22.009
Sumr	merhill Street	MH111	MH112	2.00		_					1.12		25.76 26.29					2.02		167.66	167.66		11.00	450		1.215	133.48	66.929
Cum	Park merhill Street	CBMH MH112	MH112-113 MH113	2.02	0.52				_		0.58		26.29					0.52		43.16	1747.15	1,745.00	38.71	1350	0.10	1.181	289.11	16.579
Sum	meniii oneet	IVIIIIIZ	WILLIAM		0.02																47147145	4 704 05	41.66	1350	0.10	1,192	325.07	18.469
Sumi	merhill Street	MH113	MH106								0.00	24.71	26.83	0.58	27.41	58,12	1,436.18	0.00	21.05	0.00	1747.15	1,761.25	41.00	1330	0,10	1,102	020.01	10.10
											0.77	,	45.00	0.81	15.81	83.56	64.34	0.66	0.66	44.88	44.88	91.32	38.88	375	0.25	0.801	26.98	29.55%
	n Spring Drive	MH135	MH136	1	0_41	-	0.25		_		0.77	0.77								0.00	-		11.25	375	0,25	0.800	28.81	31.599
	n Spring Drive	MH136	MH137 MH106	-	0.38		_				0.00	1.19	16.04		-					25.84			110.90	450	0.20	0.811	37.55	28.209
Golde	n Spring Drive	MH137	WITTOO		0.30						U. 12	,,,,										0.000.55	00.71	4050	0.10	1,362	747.63	24.879
Ma	attingly Way	MH106	541					0.13			0,18		27,41							8.84		3,006.23	36.74 27.10	1650 1650		1.362	772.05	25.689
	attingly Way	541	542								0.00		27.86	0.33	28.20	56.68	2,234.18	0.00		0.00 61.20		3,000.23	21.10	1000	0,10	1.004	7,18,55	
Ma	attingly Way		542					0.90			1,25		20.20	0.87	29.06	56.23	2,316.62	-		25.84		5,720.52	83,10	2100	0.10	1.600	3,403.90	59.509
	attingly Way	542	543	_	0.04		0.04	0.38			9.18		28,20	0.87	29.00	30.23	2,310.02	7.21		490.28								72500020
	attingly Way	543	543 544	-	2,64	-	0.81	3./6	_		0.00	_	3 29.06	0.34	29.40	55.10	2,775.80			0.00						1.600	2,944.72	51.489
	easement easement	544	EX. Outlet								0.00		29.40		29.7	1 54.67	2,754.24	0.00	41.62	0.00	2830.16	5,720.52	30.03	2100	0.10	1.600	2,966.28	51.85%
	Sascinant	1 011	Lyti Gallet																0.00	202.70	323.70	900.98	13.93	1050	0.10	1.008	190.58	21.15
Brian	Good Avenue	MH 151	Stub (JLR)						3.90		7.26	7.26							3.90 Refer to design	323.70					0.10	11000	100.00	
				_				0.00			0.00	0.00			mation in	82.82	provided by JL 0.00						T					
	Good Avenue	Stub (JLR)	MH 512	-	-			0.00	0.00		0.00				-	96.99												27.45
LRT Corridor at 10 y Total LRT and Brian				+	-		-		0.00		0.00	1.2.	15.23		16.3			0.00					65.20	1050	0.10	1.008	190.58	21.15
	Good Avenue	MH 512	MH 511					0.32			0.4	0.4	16.3	1		79.50									_	-		
LRT Corridor at 10	MICOLO HISTORICA PROPERTY								0.00		0.00	7.20				93.1	- AND THE RESERVE						48.74	1050	0.10	1.008	189.73	21.06
Total LRT and Brian	Good Avenue									0.00			16.3													-	18.43	3.84
Park And Ride (Exte	ernal-west)	Stub	MH 511		-					2.09	4.7	7 4.7	7 11.50	0.19	11.03	9 90.0	401.70	2.0.	2.00									
(Catamat) and		Stub	MH 511	-	-			6.07	_	3.59	16.4	2 16.4	2 24.4	0.30	24.70	0 61.8	7 1,015.92	9.6	6 9.66	656.88	656.88	1,286.53	20.00	1200	0.10	1.102	270.61	21.03
(External Lands-	east)	Stub	IMF1 J I I					0.0.		0.00											1017.01		-					
Brian	Good Avenue	MH 511	Ex MH 102	2				0.26			0.3					61.3												
LRT Corridor at 10	year Intensity								0.00		0.0	0 7.2			25.0	71 ₋₇							92.00	1500	0.10	1.278	460.66	19.76
Total LRT and Brian	n Good Avenue			-		-				1	-	-	24.7	0 1.2	0 25.9	0 01.3	1,070.00	0.0	10.20	0.00								
		-	-	+-	-	-	_	-	_	-	+	-	1															
River Road Exte	ernal			+				4.44			6.1	7 6.1	7					4.4						-				
River Road Exte	271101								0.90		1.6	8 1.6	8					0.9				0	_	-	-			
River Road (5	5 yr)	Ex MH	162			0.00					0.0				-	57.1				0.00		2	1	_		1		
	10 yr)			1	-			-	0,31	-	0.5	8 2.2	6 27.5 27.5		8 28.5	66.8	6 151.1 503.8						5 77.00	1350	0.10	1.192	1,257.37	71.39
Total	•	100	404	-		0.00	-				0.0	0 6.1			20.5	55.7				0.0	0.0	0						
River Road (5		162	161	+-	-	0.00		\vdash	0.44	-	0.8					65.1			4 6.09	78.7							101075	00.00
Total	10 yr)			+	1	0.00			J.44		1 0.0	0.0	28.5	8 1.0	8 29.6	5	544.5	0 0.4					5 77.00	1350	0.10	1.192	1,216.75	69.08
River Road (5	5 vr)	161	160	\top		5.15					5.8		4 29.6	5		54.3							-	-				-
	10 yr)								0.25		0.4	7 3.5				63.5							5 62.50	1350	0.1	0 1.192	881.26	50.04
Total	100					2							29.6	5 0.8	7 30.5	3	879.9	9 5.4	11.49	301.2	1000.0	1,101,2	02.5	1000	V. 1	1		
			1			fi					041007	1014	-					+		1		1		-		-1		
Designed:			sion 5 for C			3	_			-	01/09/2		0 - 2.79	AIC, where	a.			Level o	f Service= 1-1	68.0	0 L/s/Ha		Man	nings Coef	ficient (n) :	= 0.013	;	
	P.K.		sion 4 for Cit sion 3 for Cit	4							30/05/2					econd (I/s)		Level of	f Service= 1-4		0 L/s/Ha	1						
Checked:			for City Com								11/03/2		A = Area	in Hectare	es (hai)				f Service= 5-1		0 L/s/Ha	1						
CHECKEU.	J.I.M.		for City Corr								23/07/2	010				ters per Ho	ur (mm/hr)		f Service= 5-1A		0 L/s/Ha 0 L/s/Ha	1						
					Revision))					Date				6.053)0.81		T Corrodor		f Service= 5-2 f Service= 5-2A		0 L/s/Ha							
Dwg. Reference:			File Ref:				Date:				Sheet 2 of		[1=11	74.184/(TC River Roa		816] For LR	Conodoi	Level 0	Jervice- J-ZA	1130	5 25,110							
	3766 - 500		3766 - 5.7				9/3/201	Ц			2 01	0		LUAGE LOS	iu.													





RIVERSIDE SOUTH PHASE 12

ALTERNATE CONCEPTUAL STORM PLAN

Table F-2: Storm Water Sewers - South

The control of the		:: Storm Water Sewers - South										2013 D	C Growth Relate	d Costs		٦
Section Process Control Process Cont					Storn	n Pipe Attrib	utes		Estimated	2013 Oversizing	Cost v				0040 DO Durin	
Part Control Accounts Control Part Part Control Part Part Control Part Part Control Part Part Control Part Part Control Part Part Control Part	Line ID	Project Name	Description	From	То					Unit Cost	Tota	al Cost		Paid		
First Servicial Service (Land Condense Name 2017) Service (Lan		South Leitrim														
First disrivation and, Lifering Decomposed And 262 76 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100		Leitrim Storm Sewers (STM5)														
Final Secretary Secretar		Final Servicibility report, Leitrim Development Area, 2007	Residential Storm	825	230	1800	672	Green	Pre 2013			-				Existing Sewer Under FEA
Proof of Services (1997) Proof of Services (Final Servicibility report, Leitrim Development Area, 2007	Residential Storm	230	730	3000	510	Green	Pre 2013	-						Existing Sewer Under FEA
Part		Final Servicibility report, Leitrim Development Area, 2007	Residential Storm	730	770	3000	398	Green	Pre 2013	-	-					Existing Sewer Under FEA
Part Service Programme Part P		Final Servicibility report, Leitrim Development Area, 2007	Residential Storm	770	790	3600	240	Green	Pre 2013	-		-				Existing 3000 by 3600 box equivalent to 3600 dia. Under FEA
Proc Supplemental Section Services on Trades Learning Control and adjustance accounts where the Control of Proc 2013 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,572,444 \$ 6,5		Final Servicibility report, Leitrim Development Area, 2007	Residential Storm	790	Pond 1	3600	215	Green	Pre 2013	-		-				
Paralle Sandotal Variant Development Area, 2007 Paraller Several	1A	Subtotal Storm Sewers on Tartan Lands											\$ 6,572,444		\$ 6,572,44	pond and oversizing. The oversizing costs and applicable sewers where amended from the 2004 -303 By-Law resulting from changes to the back ground study. Overpayment balance continues on DC repayment. Includes \$500,000 for
Subhold Findly Cree Drive Sewer Subh			Residential Storm	401	400	1800	349	Green	Pre 2013			174,892				· ·
Fruit Servicibility report. Lethin Development Aves, 2007 Fruit Servicibility report. Lethin Devel		Final Servicibility report, Leitrim Development Area, 2007	Residential Storm	400	230	1950	440	Green	Pre 2013	\$ 988	\$	434,674				Existing Sewer Not Under FEA
First Servicibility report. Leithirn Development Area, 2007 Readeried Slorm 636 770 246 Green 2015 3 5,00 5 5,00,000	1B	Subtotal Findlay Creek Drive Sewers							Pre 2013		\$	609,566			\$ 609,56	5
Final Servicibility report, Lettimn Development Aria. 2007 Substant Storm Severe on Tartan/Relimer Lands Sum Severe		Final Servicibility report, Leitrim Development Area, 2007	Residential Storm	616	629	1800	348	Green	2015	\$ 501	\$	174,391				
Som Severs on Tartan/Reimer Land Som Severs on Tartan/Reimer Land		Final Servicibility report, Leitrim Development Area, 2007	Residential Storm	629	636	1950	376	Green	2015	\$ 988	\$	371,448				
Column Substitution Substituti		Final Servicibility report, Leitrim Development Area, 2007	Residential Storm	636	770	2100	245	Green	2015	\$ 1,509	\$	369,696				
Final Servicibility report, Leibrim Development Area, 2007 Industrial Storm 1280 1270 1800 300 Green 2025 \$ 988 \$ 780,316 \$ 780,316 \$ 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$ 8 780,316 \$	1C	Subtotal Storm Sewers on Tartan/Reimer Lands							2021		\$	915,536			\$ 915,53	6
Final Servicibility report, Leitrim Development Area, 2007 Industrial Storm 1270 1285 1980 280 Green 2025 \$ 5.001 \$ 150,337 Final Servicibility report, Leitrim Development Area, 2007 Industrial Storm 1285 830 2100 300 Green 2025 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$ 5.000 \$		Final Servicibility report, Leitrim Development Area, 2007		1060	Pond 1	1950	800	Green	2010	\$ 988	\$	790,316				
Final Servicibility report, Leitrim Development Area, 2007 Industrial Storm 1270 1285 1950 280 Green 2025 \$ 988 \$ 276,611 128	1D	Subtotal Storm Sewer from Analdea to Pond 1									\$	790,316			\$ 790,31	6 Paid through subdivision agreement
Final Servicibility report. Leitrim Development Area, 2007 Industrial Storm 1285 830 2100 390 Green 2025 \$ 1,509 \$ 588,495		Final Servicibility report, Leitrim Development Area, 2007	Industrial Storm	1260	1270	1800	300	Green	2025	\$ 501	\$	150,337				
Time Subtotal Sewers to Pond 2		Final Servicibility report, Leitrim Development Area, 2007	Industrial Storm	1270	1285	1950	280	Green	2025	\$ 988	\$	276,611				
Final Servicibility report, Leltrim Development Area, 2007 Industrial Storm 1102 1100 1800 201 Green 2015 \$ 5.01 FEA (no internal order) Final Servicibility report, Leltrim Development Area, 2007 Industrial Storm 1100 830 2100 315 Green 2015 \$ 1,509 FEA (no internal order) Final Servicibility report, Leltrim Development Area, 2007 Industrial Storm 830 Pond 2 3000 45 Green 2015 \$ 5,548 FEA (no internal order) If Subtotal Industrial Sewers to Pond 2 Subtotal Industrial Sewers to Pond 2 Riverside South Infrastructure Servicing Study Update 2008		Final Servicibility report, Leitrim Development Area, 2007	Industrial Storm	1285	830	2100	390	Green	2025	\$ 1,509	\$	588,495				
Final Servicibility report, Leitrim Development Area, 2007 Industrial Storm 1100 830 2100 315 Green 2015 \$ 1,509 FEA (no internal order)	1E	Subtotal Sewers to Pond 2									\$	1,015,443			\$ 1,015,44	3
Final Servicibility report, Leitrim Development Area, 2007 Industrial Storm 1100 830 2100 315 Green 2015 \$ 1,509 FEA (no internal order)																
Final Servicibility report, Leitrim Development Area, 2007 Industrial Storm 830 Pond 2 3000 45 Green 2015 \$ 5,546 FEA (no internal order)			Industrial Storm	1102	1100	1800	201	Green	2015	\$ 501		-				FEA (no internal order)
1 Subtotal Leitrim (S-2) Riverside South Infrastructure Servicing Study Update 2008						2100		Green	2015			-				· '
Riverside South SWM Pond 1 Storm Sewers Riverside South Infrastructure Servicing Study Update 2008		Final Servicibility report, Leitrim Development Area, 2007	Industrial Storm	830	Pond 2	3000	45	Green	2015	\$ 5,546		-				FEA (no internal order)
Riverside South SWM Pond 1 Storm Sewers Riverside South Infrastructure Servicing Study Update 2008	1F	Subtotal Industrial Sewers to Pond 2											\$ 741,961			
Riverside South Infrastructure Servicing Study Update 2008	1	Subtotal Leitrim (S-2)									\$:	3,330,861	\$ 7,314,405		\$ 10,645,26	Oversizing cost for storm sewers is a blended mix of existing with FEA and new that will require a future FEA
Riverside South Infrastructure Servicing Study Update 2008		Riverside South														
Riverside South Infrastructure Servicing Study Update 2008		Riverside South SWM Pond 1 Storm Sewers														
Riverside South Infrastructure Servicing Study Update 2008 2100 32 Green Pre 2013 Fre 2013 Green Pre 2013		Riverside South Infrastructure Servicing Study Update 2008				2100	107	Green	Pre 2013	-		-				
Riverside South Infrastructure Servicing Study Update 2008 Riverside South Infrastructure Servicing Study Update 2008 2100 32 Green Pre 2013 Green Pre 2013		Riverside South Infrastructure Servicing Study Update 2008			N	2100	100	Green	Pre 2013			-				
Riverside South Infrastructure Servicing Study Update 2008 2100 32 Green Pre 2013		Riverside South Infrastructure Servicing Study Update 2008				2100	100	Green	Pre 2013			-				
		Riverside South Infrastructure Servicing Study Update 2008				2100	185	Green	Pre 2013			-				
Riverside South Infrastructure Servicing Study Update 2008 2100 83 Green Pre 2013	1	Riverside South Infrastructure Servicing Study Update 2008				2100	32	Green	Pre 2013			-				
		Riverside South Infrastructure Servicing Study Update 2008				2100	83	Green	Pre 2013	-		-				

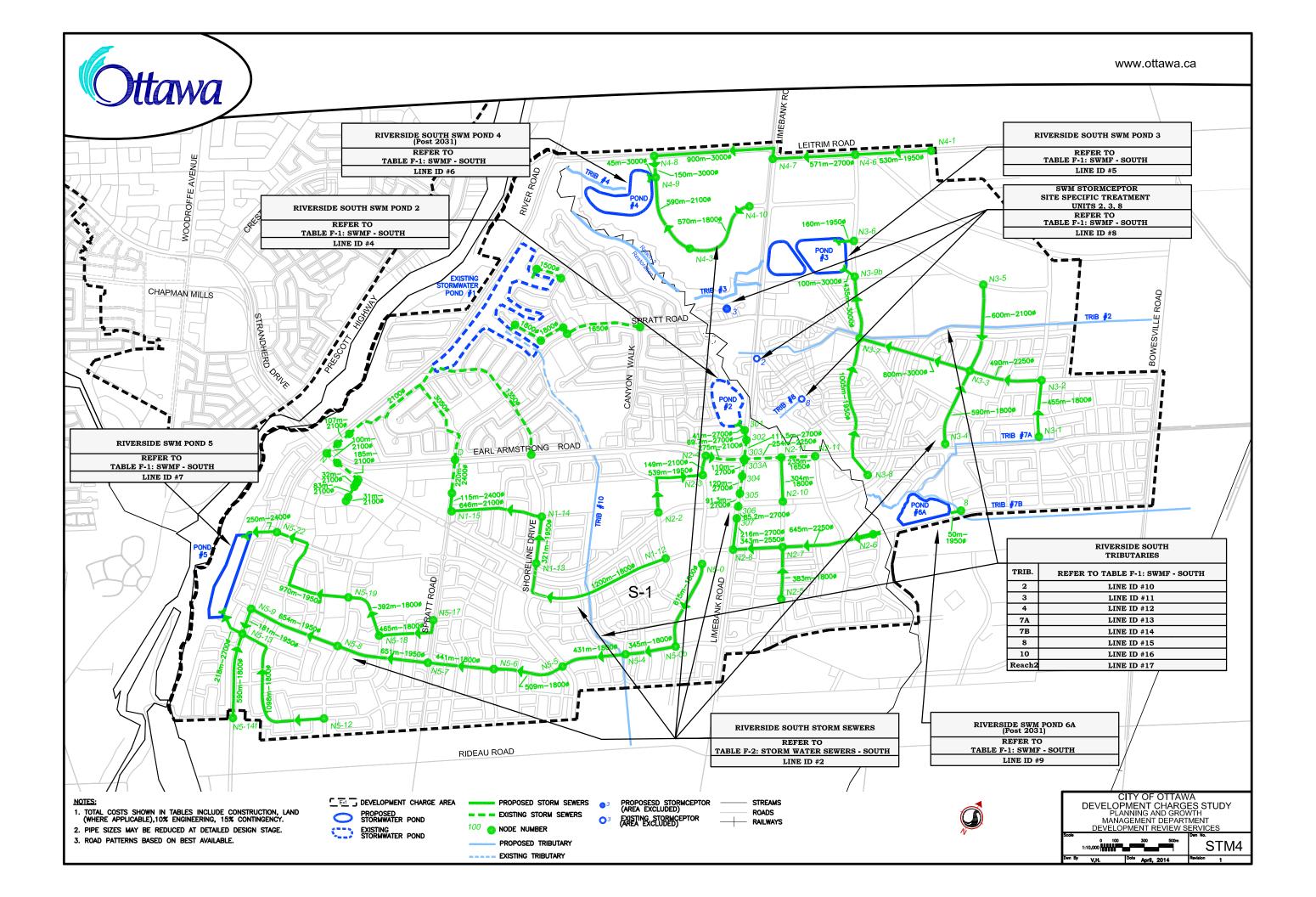
Table F-2: Storm Water Sewers - South

											2013 [OC Growth Relate	d Costs			
				Storr	n Pipe Attrib	r		Estimated	2013 Ove	ersizing	Cost w/o F.E.A.	F.E.A.		2013	B DC Project	
Line ID	Project Name	Description	From	То	Pipe Size	Pipe Length (m)	Green/ Brown	Construction Year	Unit C	Cost	Total Cost	Approved	Paid		tanding Cost	Comments
	Riverside South Infrastructure Servicing Study Update 2008				(mm) 2100	31	Green	Pre 2013		_						
	Riverside South Infrastructure Servicing Study Update 2008		N1-12	N1-13	1800	1200	Green	2020								
								2020								
	Riverside South Infrastructure Servicing Study Update 2008		N1-13	N1-14	1950	321	Green			-						
	Riverside South Infrastructure Servicing Study Update 2008		N1-14	N1-15	2100	646	Green	2015	-	-						
	Riverside South Infrastructure Servicing Study Update 2008		N1-15	N1-16	2400	115	Green	2015	•	-	-					
	Riverside South Infrastructure Servicing Study Update 2008		N1-16	Ex.	2400	220	Green	Pre 2013	•	-	-					
2A	Subtotal Pond 1 Storm Sewers											\$ 4,032,000		\$	4,032,000	FEA not found. Reference made in Lynn Lowes table to the to 2009 DC
																background study. The 2008 DC oversizing cost for Stm to pond 1 is \$4,032,000
	Riverside South SWM Pond 2 Storm Sewers															
	Riverside South Infrastructure Servicing Study Update 2008		N2-2	N2-3	1950	539	Green	2020	•	-						Existing Sewer Under FEA
	Riverside South Infrastructure Servicing Study Update 2008		N2-3	N2-4	2100	149	Green	2018	•	-						Existing Sewer Under FEA
	Riverside South Infrastructure Servicing Study Update 2008		N2-4	303	2100	275	Green	2016		-	-					Existing Sewer Under FEA
	Riverside South Infrastructure Servicing Study Update 2008		N2-8	307	2700	216	Green	2015		-	-					Existing Sewer Under FEA
	Riverside South Infrastructure Servicing Study Update 2008 Riverside South Infrastructure Servicing Study Update 2008		307 306	306 305	2700 2700	85.2 91.3	Green Green	Pre 2013 Pre 2013								Existing Sewer Under FEA Existing Sewer Under FEA
	Riverside South Infrastructure Servicing Study Update 2008		305	303	2700	120	Green	Pre 2013								Existing Sewer Under FEA Existing Sewer Under FEA
	Riverside South Infrastructure Servicing Study Opdate 2008 Riverside South Infrastructure Servicing Study Update 2008		303	303	2700	110	Green	Pre 2013		_	_					Existing Sewer Under FEA Existing Sewer Under FEA
	Riverside South Infrastructure Servicing Study Update 2008		303	302	2700	111.5	Green	Pre 2013		_						Existing Sewer Under FEA Existing Sewer Under FEA
	Riverside South Infrastructure Servicing Study Update 2008		302	301	2700	69.7	Green	Pre 2013		_						Existing Sewer Under FEA
	Riverside South Infrastructure Servicing Study Update 2008		301	Pond #2	2700	41	Green	Pre 2013		_						Existing Sewer Under FEA
	Riverside South Infrastructure Servicing Study Update 2008		N2-11	303	2250	254	Green	Pre 2013		-						Existing Sewer Under FEA
	Riverside South Infrastructure Servicing Study Update 2008		N2-11	N2-10	1800	304	Green	Pre 2013		-						Existing Sewer Under FEA
	Subtotal											\$ 4,924,975	¢ _	\$	4,924,975	ACS2005-PGM-APR-0159 - FEA Trunk Storm Sewer Oversizing for sewers
												φ 4,924,975	φ -	7	4,324,313	which are tributary to Pond 2
	Riverside South Infrastructure Servicing Study Update 2008	Part of Sewers East of Limebank	N2-5	N2-7	1800	383	Green		\$	501	\$ 191,931					
	Riverside South Infrastructure Servicing Study Update 2008	Limebank	N2-6	N2-7	2250	645	Green		\$	2,079	\$ 1,341,115					
	Riverside South Infrastructure Servicing Study Update 2008		N2-7	N2-8	2550	343	Green		\$	3,514	\$ 1,205,269					
	Subtotal										\$ 2,738,314			\$	2,738,314	
2B	Subtotal Pond 2 Storm Sewers													\$	7,663,289	
	Riverside South SWM Pond 3	POND 3														
	Riverside South Infrastructure Servicing Study Update 2008		N3-1	N3-2	1800	455	Green	2030		-						
	Riverside South Infrastructure Servicing Study Update 2008		N3-2	N3-3	2250	490	Green	2030	-	-						
	Riverside South Infrastructure Servicing Study Update 2008		N3-4	N3-3	1800	590	Green	2030		-				1		
	Riverside South Infrastructure Servicing Study Update 2008		N3-5	N3-3	2100	600	Green	2025	-	-				1		
	Riverside South Infrastructure Servicing Study Update 2008		N3-3	N3-7	3000	800	Green	2025		-						
	Riverside South Infrastructure Servicing Study Update 2008		N3-8	N3-7	1950	1005	Green	2020		-	-			1		
	Riverside South Infrastructure Servicing Study Update 2008		N3-7	N3-9b	3000	435	Green	2015		-						
	Riverside South Infrastructure Servicing Study Update 2008		N3-9b	N3-IN2	3000	100	Green	2015	-	-						
	Riverside South Infrastructure Servicing Study Update 2008		N3-6	N3-IN1	1950	160	Green	2015	· .	-						
2C	Subtotal Pond 3 Storm Sewers										\$ 9,877,000		\$ -	\$	9,877,000	ACS2011-ICS-PGM-0199. Requires an internal order number.
	Riverside South SWM Pond 4 Storm Sewers	POND 4														
	Riverside South Infrastructure Servicing Study Update 2008		N4-1	N4-6	1950	530	Green	Post 2031	\$	988	\$ 523,584					
	Riverside South Infrastructure Servicing Study Update 2008		N4-6	N4-7	2700	571	Green	Post 2031	\$	4,225	\$ 2,412,517			1		
	Riverside South Infrastructure Servicing Study Update 2008		N4-7	N4-8	3000	900	Green	Post 2031	\$	5,546						
	Riverside South Infrastructure Servicing Study Update 2008		N4-8	N4-9	3000	150	Green	Post 2031		5,546	\$ 831,881			1		
									\$					1		
	Riverside South Infrastructure Servicing Study Update 2008		N4-10	N4-3	1800	570	Green	Post 2031	\$	501	\$ 285,641					
	Riverside South Infrastructure Servicing Study Update 2008		N4-3	N4-9	2100	590	Green	Post 2031	\$	1,509	\$ 890,288			1		

Table F-2: Storm Water Sewers - South

	: Storm water Sewers - South											2013 D	C Growth Relate	ed Costs		
				Storm	Pipe Attribu	utes		Estimated	2013	Oversizing	Cos	t w/o F.E.A.	F.E.A.		2013 DC Project	
Line ID	Project Name	Description	From	То	Pipe Size (mm)	Pipe Length (m)	Green/ Brown	Construction Year	U	nit Cost	Т	otal Cost	Approved	Paid	Outstanding Cost	Comments
	Riverside South Infrastructure Servicing Study Update 2008		N4-9	4-inlet	3000	45	Green	Post 2031	\$	5,546	\$	249,564				
2D	Subtotal Pond 4 Storm Sewers										\$	10,184,763				Post 2031 cost. Not included in total 2013 outstanding cost.
	Riverside South SWM Pond 5 Storm Sewers	POND 5														
	Rverside South Infrastructure Servicing Study Update 2008		N5-0	N5-0b	1800	615	Green	Post 2031	\$	501	\$	308,191				
	Riverside South Infrastructure Servicing Study Update 2008		N5-0b	N5-4	1800	345	Green	Post 2031	\$	501	\$	172,888				
	Riverside South Infrastructure Servicing Study Update 2008		N5-4	N5-5	1800	431	Green	Post 2031	\$	501	\$	215,985				
	Riverside South Infrastructure Servicing Study Update 2008		N5-5	N5-6	1800	509	Green	Post 2031	\$	501	\$	255,072				
	Riverside South Infrastructure Servicing Study Update 2008		N5-6	N5-7	1800	441	Green	Post 2031	\$	501	\$	220,996				
	Riverside South Infrastructure Servicing Study Update 2008		N5-7	N5-8	1950	651	Green	2025	\$	988	\$	643,119				
	Riverside South Infrastructure Servicing Study Update 2008		N5-8	N5-9	1950	654	Green	2025	\$	988	\$	646,083				
	Riverside South Infrastructure Servicing Study Update 2008		N5-9	N5-13	1950	181	Green	2020	\$	988	\$	178,809				
	Riverside South Infrastructure Servicing Study Update 2008		N5-12	N5-13	1800	1098	Green	2020	\$	501	\$	550,235				
	Riverside South Infrastructure Servicing Study Update 2008		N5-14f	N5-13	1800	590	Green	2017	\$	501	\$	295,663				
	Riverside South Infrastructure Servicing Study Update 2008		N5-13	Pond #5	2700	218	Green	2017	\$	4,225	\$	921,066				
	Riverside South Infrastructure Servicing Study Update 2008		N5-17	N5-18	1800	465	Green	2015	\$	501	\$	233,023				
	Riverside South Infrastructure Servicing Study Update 2008		N5-18	N5-19	1800	392	Green	2015	\$	501	\$	196,441				
	Riverside South Infrastructure Servicing Study Update 2008		N5-19	N5-22	1950	970	Green	2015	\$	988	\$	958,258				
	Riverside South Infrastructure Servicing Study Update 2008		N5-22	Pond #5	2400	250	Green	2015	\$		\$	704,996				
2E	Subtotal Pond 5 Storm Sewers										\$	6,500,826			\$ 6,500,826	
			8	Int. Pond 6a	1950	50	Green	Post 2031	\$	988	\$	49,395			, ,,,,,,,	
2F	Subtotal Pond 6A Storm Sewers								Ť		\$	49,395				Post 2031 cost. Not included in total 2013 outstanding cost.
2	Subtotal Gloucester SUC (S-1)										\$	19,473,298	\$ 4,032,000		\$ 28,073,115	2005-Council approved 10.65M for Pond 2 (2008)
	South Nepean (North of Jock River)															
	Foster SWM Pond Storm Sewers (STM 3)															
			111	110	2550	425	Green	Pre 2013	\$	3,514		1,493,409				
			110	109	2550	273	Green	Pre 2013	\$	3,514		957,539				
			109	108B	2700	240 99	Green Green	Pre 2013 Pre 2013	\$ \$	4,225 5,546		1,014,018 547,378				
			108B 106	OUTLET 108A	3000 2250	99 927	Green	Pre 2013	\$	2,079		1,927,047				
3	Subtotal Foster Pond Storm Sewers		100	100/1	2200	321	Ordon	1102010	T T	2,010	\$	5,939,390			\$ 5,939,390	
	Kennedy Burnett Pond Storm Sewers (STM 3)	Kennedy Burrnet Pond														
	, , ,	Storm Sewers														
	South Nepean Urban Area Master Servicing Study Environmental Study Report	3000x1200 Box Culvert Equivalent Size φ	1600	1590	2100	200	Green	2015	\$	1,509	\$	301,793				
	South Nepean Urban Area Master Servicing Study Environmental Study Report	2400x1200 Box Culvert Equivalent Size φ	1570	1560	1950	250	Green	2016	\$	988	\$	246,974				
	South Nepean Urban Area Master Servicing Study Environmental Study Report	4200x1800 Box Culvert Equivalent Size φ	1560	1520 (Pond)	3000	450	Green	2017	\$	5,546	\$	2,495,643				
	South Nepean Urban Area Master Servicing Study Environmental Study Report	3600x1500 Box Culvert Equivalent Size φ	1510	1500	2700	70	Green	2018	\$	4,225	\$	295,755				
4	Subtotal Kennedy Burnett Storm Sewers										\$	3,340,165			\$ 3,340,165	
5	Subtotal for North of Jock (S-3)										\$	9,279,555			\$ 9,279,555	
	(5-5)						1		<u> </u>		<u> </u>	, -,			, .,,,,,,	

CONSTRUCTED



6.0 INFRASTRUCTURE PHASING

The total study area encompasses 300ha of development lands. It is recognized that this development will take several decades to reach full build-out and as such phasing of infrastructure planning and construction was considered to the extent possible in developing the servicing plans. This study has assumed that the interim condition will consist of all development west of Spratt Road except for the Cardel Lands located north of the urban boundary between River Road and Spratt Road. Areas east of Spratt Road to the limit of the study area and the Cardel Lands are assumed to be developed as part of the ultimate scenario. Phasing boundaries are illustrated in **Figure 6-1**. Phasing considerations related to natural features and proposed infrastructure are summarized in this section.

6.1 HEADWATER DRAINAGE FEATURES

A headwater drainage features assessment (HDFA) was completed by Stantec and identified recommendations for each reach of the ravines adjacent to Pond 5. Based on the recommendations of the HDFA, base flow to these ravines will need to be maintained throughout both in the interim and ultimate condition of development.

The construction of Phase 15 will cut off much of the source of base flow for downstream ravines North and South of the Pond 5 block, specifically reaches 1A, 2A and 2B as shown in **Figure 6-1** below. Subdivision designs for areas within the existing tributary areas to the ravines will need to provide measures to ensure baseflows are maintained per the HDFA recommendations.

Observations noted in the HDFA indicate that the watercourses to be preserved and or mitigated, experience seasonally intermittent flow with groundwater inferred to be a significant contributing source of flow. As such, the RVCA has indicated that the use of pond flows or OGS discharge will not provide sufficient replication of the existing flow regime since the temperature of the water from these sources would be too warm. A solution that utilizes foundation drains, or rear-yard drainage or LIDs and conveys flows subsurface for cooling is preferred.

The combined base flow and storm runoff from this system would need to remain below the existing conditions peak flow for each storm event to ensure the erosion thresholds are not exceeded. The approximate pre-development flow rates for each of these reaches is summarized in **Table 6-1** below:

Table 6-1: Pre-Development Tributary Ravine Flows for Varying Storm Events

		Flo	ow (L/s)	
Reach	2-yr 12hr SCS	5-yr 12hr SCS	10-yr 12hr SCS	100-yr 12hr SCS
North Ravine				
1A	310	580	840	1690
South Ravine				
2A	640	1210	1730	3500
2B	240	450	640	1290



