

**Wurtemburg Tower  
101 Wurtemburg Street  
Ottawa, Ontario**

**Stormwater Management Report**

**WURTEMBURG TOWER  
101 WURTEMBURG STREET  
OTTAWA, ONTARIO**

**STORMWATER MANAGEMENT REPORT**

**Prepared by:**

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**File No.: 111013  
Report Reference No.: R-2011-034  
February 25, 2011**



February 25, 2011

City of Ottawa  
Planning and Growth Management Department  
Development Review (Urban) Services Branch  
Infrastructure Approvals Division  
110 Laurier Avenue West, 4<sup>th</sup> Floor  
Ottawa ON, K1P 1J1

**Attention: Mr. Bruce Coombe**

Dear Sir:

**Reference: Wurtemburg Tower – 101 Wurtemburg Street  
Stormwater Management Report  
Our File No.: 111013**

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Enclosed herein is the Stormwater Management Report for the proposed residential development at 101 Wurtemburg Street, located on the east side of the intersection of Wurtemburg Street and Clarence Street. This report is submitted in support of the rezoning and site plan applications and presents a stormwater management plan for the re-development of the site.

Trusting this report is adequate for your purposes. Should you have any questions, or require additional information, please contact us.

Yours truly,

**NOVATECH ENGINEERING CONSULTANTS LTD.**

A handwritten signature in blue ink that reads "Greg MacDonald".

Greg MacDonald, P.Eng  
Senior Project Manager

JAG/jag

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- 111013-GP General Plan of Services
- 111013-GR Grading and Erosion Control Plan
- 111013-STM Stormwater Management Plan

## 1.0 INTRODUCTION

The proposed Wurtemburg Tower residential development at 101 Wurtemburg Street is located on the east side of the intersection of Wurtemburg Street and Clarence Street in the City of Ottawa, as shown in Figure 1 - Key Plan. The proposed development will consist of an 18 storey tower with 66 condominium units. Also, a total of 54 parking spaces will be provided on 3 levels of underground parking. Refer to Figure 2 - Site Plan for details.

The subject site consists of approximately 0.0795 ha and is currently occupied by a two-storey residential building, as shown in Figure 3 – Existing Conditions.

This stormwater management report will provide a solution to manage stormwater runoff from the site.

## 2.0 CRITERIA

Through correspondence with the City of Ottawa and our knowledge of development requirements in the area, the following criteria have been adopted to control post-development stormwater discharge from the site:

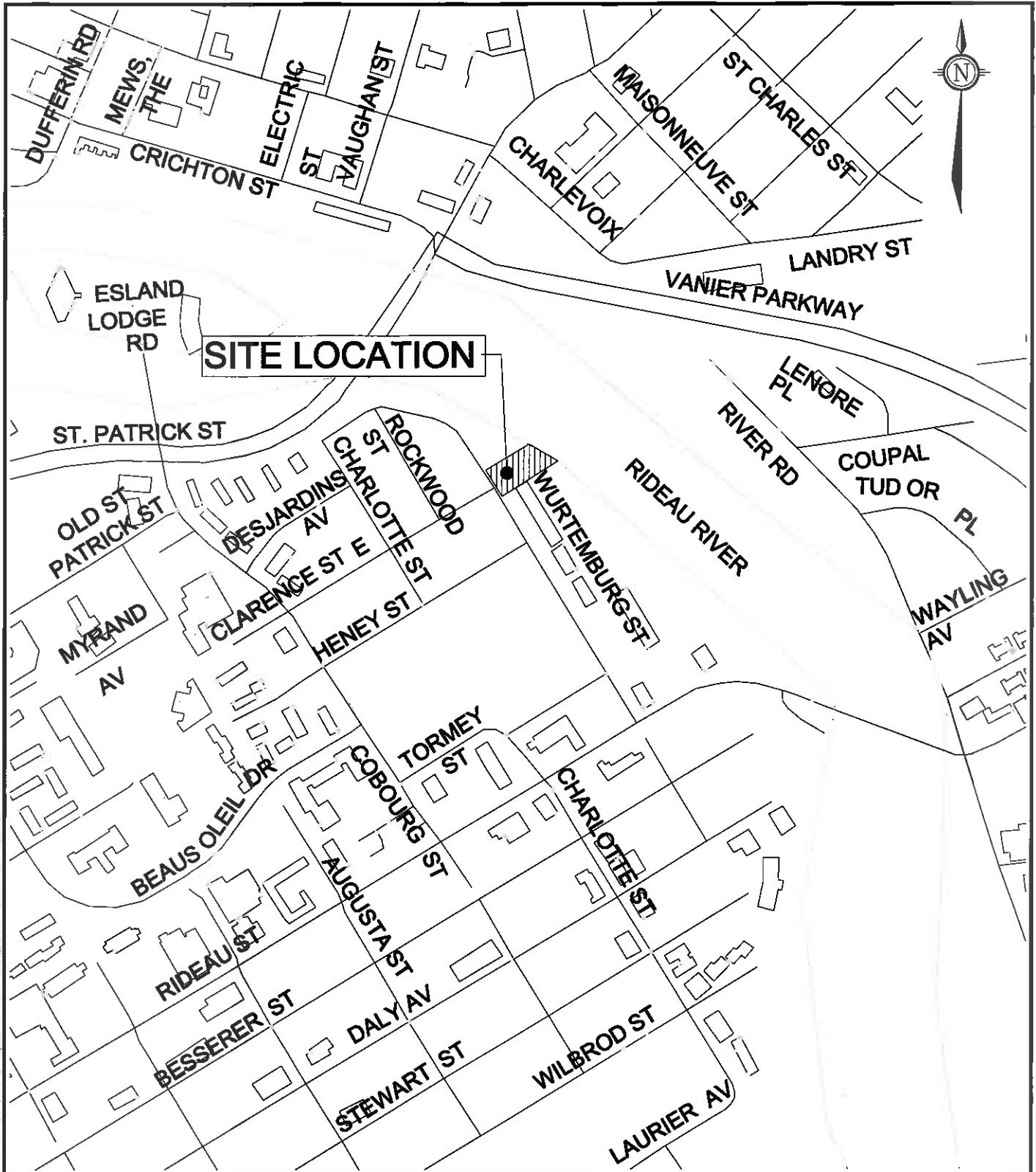
- Control proposed development flows, up to and including the 100-year storm event, to a 5-year allowable release rate calculated using a runoff coefficient (C) of 0.50 and a time of concentration ( $T_c$ ) of 20 minutes;
- Determine size and location of drainage system components;
- Provide source controls which are in conformity with the City of Ottawa requirements, where possible;
- Limit ponding to 0.15 m for all rooftop storage areas; and
- Provide guidelines to ensure that site preparation and construction is in accordance with the current Best Management Practices for Erosion and Sediment Control.

The approach to the stormwater management design is to determine the allowable release rate for the site, calculate the uncontrolled flow, and ensure that the remaining flow, in combination with the uncontrolled flow, does not exceed the allowable release rate. All proposed development runoff in excess of the allowable release rate, will be attenuated on-site prior to being released into the storm sewer on Wurtemburg Street.

## 3.0 EXISTING CONDITIONS

### 3.1 The Site

Under existing conditions, the site consists of a two-storey residential building, as illustrated in Figure 3. Stormwater flows from the site are currently conveyed to the existing storm sewer system via road catchbasins by overland flows. The rear portion of the site discharges overland to the Rideau River.



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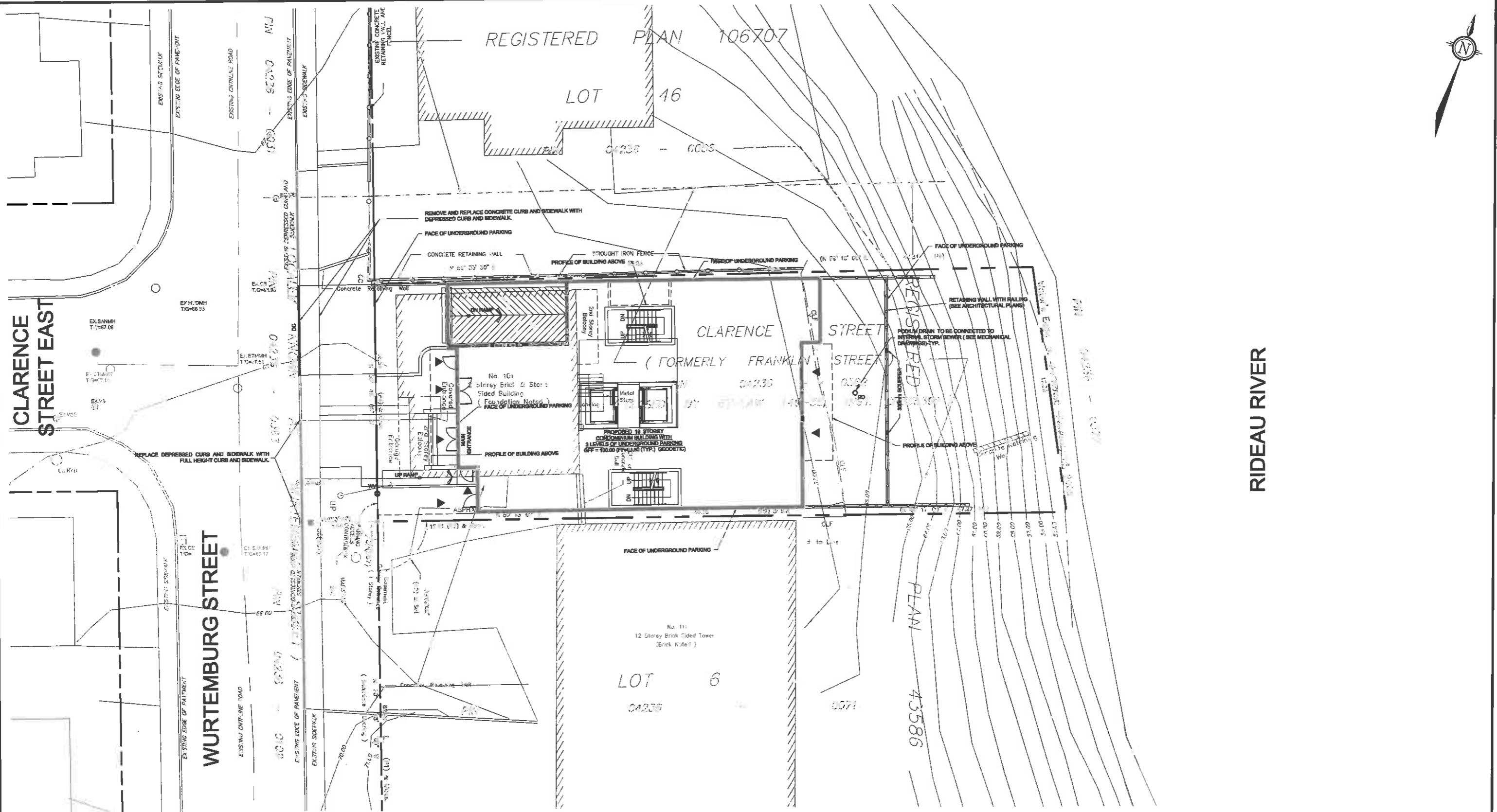
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CITY OF OTTAWA

WURTEMBURG TOWER  
101 WURTEMBURG STREET

KEY PLAN

FEB. 2011 111013 FIGURE 1





LEGEND

SITE PLAN AREA

NTS

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CITY OF OTTAWA  
WURTEMBURG TOWER  
101 WURTEMBURG STREET  
EXISTING CONDITIONS  
FEB. 2011 111013 FIGURE 3

As part of this development, all stormwater will be controlled on site and discharged via a 200 mm dia. service that will connect to the existing 300 mm dia. storm sewer on Wurtemburg Street. All proposed storm services will be equipped with backwater valves.

### 3.2 Allowable Release Rate

The City requires that on-site stormwater management be implemented to control post-development stormwater discharge for the 100 year storm event to that value calculated using a 5-year storm and a time of concentration ( $T_c$ ) of 20 minutes. The allowable release rate for the proposed 0.0795 ha development was calculated using the Rational Method to be 7.76 L/s as follows:

$$\begin{aligned} \text{Total Drainage Area (A)} &= 0.0795 \text{ ha} & Q_{\text{allow}} &= 2.78 \text{ CIA} \\ \text{Runoff Coefficient (C}_{\text{allow}}\text{)} &= 0.50 & Q_{\text{allow}} &= 2.78 \times 0.50 \times 70.25 \text{ mm/hr} \times 0.0795 \text{ ha} \\ \text{Intensity (I}_{\text{allow}}\text{)} &= 70.25 \text{ mm/hr} & Q_{\text{allow}} &= 7.76 \text{ L/s} \end{aligned}$$

## 4.0 PROPOSED DEVELOPMENT STORMWATER MANAGEMENT DESIGN

Stormwater runoff flow from the site will be a combination of uncontrolled direct runoff and controlled flow. Stormwater management will be achieved through the use of rooftop controls and surface storage. The site will be graded such that flows in excess of the 100-year storm event will be conveyed overland to Wurtemburg Street and to the Rideau River.

The trench drain for the ramp to the underground parking will outlet uncontrolled to the storm sewer on Wurtemburg Street.

### 4.1 Drainage Areas

The development will consist of a number of drainage areas which are highlighted on the Storm Drainage Area Plan (111013-STM) enclosed in the back of this report. The following is a detailed description of how the flows from each area will be managed.

**Table 4.1 Drainage Area Descriptions**

Drainage Area No.	Total area (ha)	Runoff Coefficient - C	Description
A-01	0.00905	0.60	Uncontrolled
A-02	0.01115	0.76	Uncontrolled
A-03	0.01926	0.20	Uncontrolled
R-01	0.01751	0.95	Controlled – Roof Drain
R-02	0.02136	0.95	Controlled – Roof Drain
R-03	0.00073	0.95	Controlled – Roof Drain
R-04	0.00041	0.95	Controlled – Roof Drain
<b>Total =</b>	<b>0.0795</b>		

Drainage Areas A-01 and A-02 are the surficial uncontrolled runoff at the ground elevation and will be collected by area drains that will discharge to the storm sewer on Wurtemburg Street. Drainage Area A-03 is the surficial uncontrolled runoff at the ground elevation and will discharge overland to the Rideau River. Drainage Areas R-01 through R-04 are rooftop areas large enough for surface storage, therefore allowing controlled flow.

All the stormwater runoff from the controlled roof top areas, along with drainage areas A-01 and A-02 will flow internally and then be directed out of the building through a direct connection to the existing 300 mm dia. storm sewer on Wurtemburg Street.

#### 4.2 Uncontrolled Development Flows

The uncontrolled development flows from Areas A-01 to A-03 were calculated using the Rational Method with a time of concentration ( $T_c$ ) of 20 minutes and are summarized in Table 4.2. Detailed calculations are contained in Appendix B.

**Table 4.2 Proposed Development Uncontrolled Flows Summary**

Area No.	POST DEVELOPMENT UNCONTROLLED RUNOFF									
	5-Year Event				100-Year Event					
	C	$T_c$ (min)	I (mm/hr)	Area (ha)	Q (L/s)	C	$T_c$ (min)	I (mm/hr)	Area (ha)	Q (L/s)
A-01	0.60	20	70.25	0.0091	1.06	0.68	20	119.95	0.0091	2.05
A-02	0.76	20	70.25	0.0112	1.65	0.85	20	119.95	0.0112	3.16
A-03	0.20	20	70.25	0.0193	0.75	0.25	20	119.95	0.0193	1.61
<b>Total =</b>				<b>3.46</b>	<b>Total =</b>				<b>6.82</b>	

Based on the above calculations, the 5-year uncontrolled roof flow is 3.46 L/s and the 100-year uncontrolled roof flow is 6.82 L/s.

##### 4.2.1 Remaining Allowable Release Rate

The maximum allowable storm flow for the remaining areas is the allowable release rate for the entire site less the uncontrolled flow from Areas A-01 to A-03. The following table indicates the allowable release rate for the entire site, the uncontrolled runoff from Areas A-01 to A-03, and the remaining allowable release rate for the rest of the rooftop areas for both the 5-year and 100-year storm events.

**Table 4.2.1 Remaining Allowable Release Rate Summary**

Area	Flow (L/s)	
	5-Year	100-Year
Entire Site (Legal Boundary)	Allowable	7.76
A-01 to A-03	Uncontrolled	3.46
Remaining Allowable Flow		4.30
		0.94

#### 4.3 Controlled Development Flows

Stormwater flows from Areas R-01 through R-04 were calculated to be 7.43 L/s for the 5-year storm event and 13.33 L/s for the 100-year storm event. Both events exceed the maximum allowable flow for these areas therefore roof drain flow controls will be required. Detailed calculations are contained in Appendix B.

Due to the extent of hard surface areas and the limited allowable release rate, runoff in excess of the allowable quantity will be stored on site, up to and including the 100-year storm event. Flow from the building roof will be controlled by modified Zurn rooftop drains. Flow through these drains is dependent on the height of water above the drain (H- Head) and the number of notches in the

drain. Flow from each rooftop area has been summarized in Table 4.3. Detailed calculations are included in Appendix B.

**Table 4.3 Roof Drain Flow Summary**

Area No	Zurn Specification	G.P.M per Inch of Head	ZURN ROOFDRAIN CONTROL PARAMETERS			
			5-Year Event		100-Year Event	
			Depth (m)	Total Flow (L/s)	Depth (m)	Total Flow (L/s)
R-01	ZCF121-1W-X3-Z-105-10-77	2.50	0.112	0.83	0.143	1.07
R-02	ZCF121-1W-X2-Z-105-10-77	3.75	0.115	1.29	0.148	1.66
R-03	ZCF121-1W-X4-Z-105-10-77	1.25	0.055	0.20	0.079	0.29
R-04	ZCF121-1W-X4-Z-105-10-77	1.25	0.039	0.14	0.061	0.23
			<b>Total =</b>	<b>2.47</b>	<b>Total =</b>	<b>3.25</b>

The Modified Rational Method was used to determine the storage volume required for the various rooftop drainage areas. Based on a controlled flow provided via the modified Zurn rooftop drains, the ponding depth on the roof above the drains will vary between 0.039 – 0.115 m for the 5-year storm event and 0.061 – 0.148 m for the 100-year storm event, as determined through iterative calculations using the release rate, head, and corresponding storage. The flow rate for a standard Zurn roof drain (per 1 notch) is 5 G.P.M. per inch of head (1.49 L/s per 100mm of ponding), but this can be reduced by designing the weir. Refer to the Appendix B for details outlining the modified rational method used, the ponding depth, and stage-storage curves for each controlled drainage area. Zurn roof drain information, including the specification for the weirs is contained in Appendix C.

#### 4.4 Major Overland Drainage

In the case of a storm event greater than the 100-year, scuppers will be included in the building design at a depth of 0.15 m from the roof drain to provide an overflow for excess runoff. An overland drainage flow route for major system runoff will be provided by grading the site such that excess stormwater runoff will flow overland towards Wurtemburg Street and the Rideau River.

### 5.0 EROSION AND SEDIMENT CONTROL MEASURES

Temporary and permanent erosion and sediment control measures will be implemented prior to, during and after construction; and will be inspected regularly.

To prevent sediment and debris from entering the storm system during construction, the following erosion and sediment control measures will be implemented during construction in accordance with the "Guidelines on Erosion and Sediment Control for Urban Construction Sites" (Government of Ontario, May 1987):

- Filter cloth will be placed under the grates of all area drains and remain in place until vegetation has been established and construction is completed;
- Street sweeping and cleaning will be performed on all roads adjacent to active construction on a regular basis;
- Stockpiles will be stabilized against erosion, and;
- Silt fence will be placed along the surrounding property lines to prevent contaminated surface runoff from migrating towards adjacent sites and straw bale check dams will be used if necessary.

As for permanent measures, seeding of disturbed areas and establishing grass growth will be utilized.

## 6.0 CONCLUSIONS AND RECOMMENDATIONS

Based on the findings of this report, a stormwater management scheme has been identified that will achieve the allowable release rate required by the City. Therefore, the following conclusions are made:

- On-site stormwater management will be provided to control the stormwater discharge from the 5-year and 100-year storm events.
- Stormwater discharge from the site for the 5-year storm event (5.94 L/s) is less than the allowable flow rate of 7.76 L/s.
- Stormwater discharge from the site for the 100-year storm event (10.05 L/s) is greater than the allowable flow rate of 7.76 L/s, however, this would have negligible impact on the existing City storm sewer system.
- The site will be graded such that flows in excess of the 100-year storm event will be conveyed overland to Wurtemburg Street and the Rideau River.
- Sediment and erosion control measures will be implemented during construction.

## 7.0 CLOSURE

This report has been prepared in accordance with the requirements for site plan submission and is hereby submitted for approval.

### NOVATECH ENGINEERING CONSULTANTS LTD.

Prepared by:



Justin Gauthier, B.Eng.  
Junior Engineer

Reviewed by:



Greg MacDonald, P.Eng.  
Senior Project Manager

## **APPENDIX A**

### **IDF CURVES, RATIONAL METHOD, RUNOFF**

## RATIONAL METHOD

The Rational Method was used to determine both the allowable runoff as well as the proposed development runoff for the site. The equation is as follows:

$$Q=2.78 \text{ CIA}$$

Where:

Q is the runoff in L/s

C is the weighted runoff coefficient\*

I is the rainfall intensity in mm/hr\*\*

A is the area in hectares

\*The weighted runoff coefficient is determined for each of the catchment areas as follows:

$$C = \frac{(A_{perv} \times C_{perv}) + (A_{imp} \times C_{imp})}{A_{tot}}$$

Where:

$A_{perv}$  is the pervious area in hectares

$C_{perv}$  is the pervious area runoff coefficient ( $C_{perv}=0.20$ )

$A_{imp}$  is the impervious area in hectares

$C_{imp}$  is the impervious area runoff coefficient ( $C_{imp}=0.90$ )

$A_{tot}$  is the catchment area ( $A_{perv} + A_{imp}$ ) in hectares

\*\* The rainfall intensity is taken from the City of Ottawa IDF Curves with a time of concentration of 20 min (refer to attached IDF Curves) as specified by the City of Ottawa.

## ALLOWABLE RELEASE RATE AS SPECIFIED BY THE CITY

The allowable release rate was calculated for the 0.0795 ha re-developed site, using a runoff coefficient (C) of 0.50 and a time of concentration (Tc) of 20 minutes, as specified by the City of Ottawa.

Drainage Area (A) = 0.0795 ha

Runoff Coefficient (C) = 0.50

Intensity (I5) = 70.25 mm/hr

Q5= 2.78 CIA

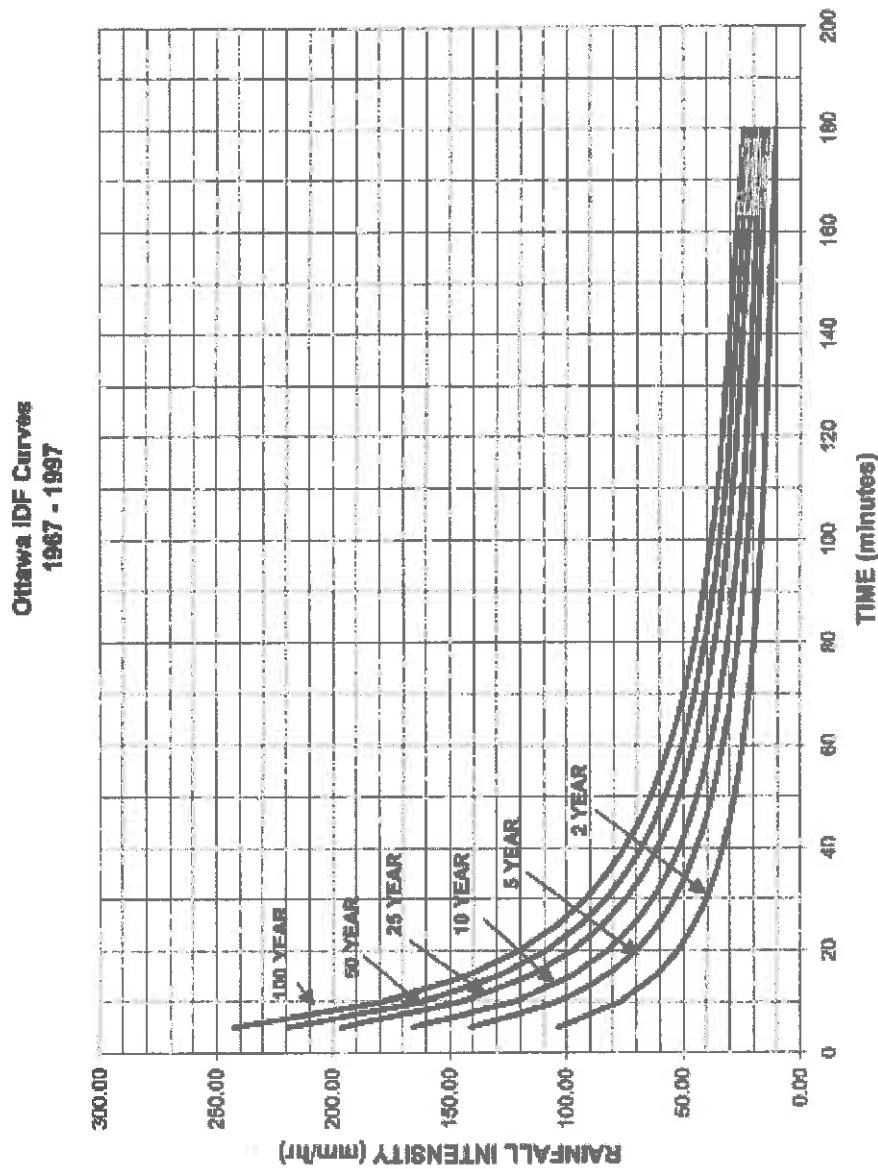
Q5= 2.78 x 0.50 x 70.25 mm/hr x 0.0795 ha

Q5= 7.76 L/s

## Ottawa Sewer Design Guidelines

## APPENDIX 5-A

## OTTAWA INTENSITY DURATION FREQUENCY (IDF) CURVE



City of Ottawa

Appendix 5-A.1

November 2004

\* IDF CURVE FROM OTTAWA SEWER DESIGN GUIDELINES – NOV 2004

**APPENDIX B**

**SWM CALCULATIONS**

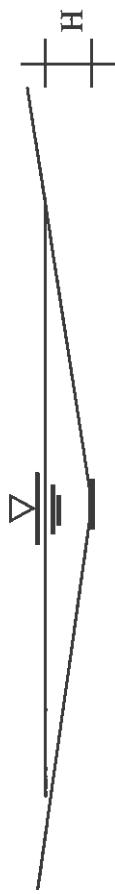
**Runoff Coefficients**

Drainage Area	Total Area (m <sup>2</sup> )	Hard Surface Area		Grass Area		5-Year Runoff Coefficient	100-Year Runoff Coefficient
		Area (m <sup>2</sup> )	C	Area (m <sup>2</sup> )	C		
R-01	175.1	175.1	0.95	0.0	0.2	0.95	1.00
R-02	213.6	213.6	0.95	0.0	0.2	0.95	1.00
R-03	7.3	7.3	0.95	0.0	0.2	0.95	1.00
R-04	4.1	4.1	0.95	0.0	0.2	0.95	1.00
A-01	90.5	51.66	0.9	38.86	0.2	0.60	0.68
A-02	111.5	88.99	0.9	22.51	0.2	0.76	0.85
A-03	192.6	0.00	0.9	192.64	0.2	0.20	0.25
<b>Total</b>	<b>794.8</b>	<b>540.8</b>	<b>0.94</b>	<b>254.0</b>	<b>0.20</b>	<b>0.70</b>	<b>0.76</b>

# WURTEMBURG TOWER: 101 WURTEMBURG STREET

## Zurn Roof Drains

Opening	GPM Per Inch of Head	LPM Per Inch of Head (25 mm) of Head	L/s Per Metre of Head	L/s Per Metre of Head
Standard - X1	5.00	22.730	14.915	2.237
Reduced - X2	3.75	17.048	11.186	1.678
Reduced - X3	2.50	11.365	7.458	1.119
Max Reduced - X4	1.25	5.683	3.729	0.559



## SAMPLE CALCULATION:

### AREA R-01

No. of Notches



Number of notches (N) = 1  
Head (H) = 0.112 m for 5-year event  
Head (H) = 0.143 m for 100-year event

$$\begin{aligned}
 Q_{5\text{ all}} &= 7.458 \text{ L/s/m/notch} \times H \times N \\
 Q_{5\text{ all}} &= 7.458 \text{ L/s/m/notch} \times 0.112 \text{ m} \times 1 \text{ notch} \\
 Q_{5\text{ all}} &= 0.83 \text{ L/s}
 \end{aligned}$$

$$\begin{aligned}
 Q_{100\text{ all}} &= 7.458 \text{ L/s/m/notch} \times H \times N \\
 Q_{100\text{ all}} &= 7.458 \text{ L/s/m/notch} \times 0.143 \text{ m} \times 1 \text{ notch} \\
 Q_{100\text{ all}} &= 1.07 \text{ L/s}
 \end{aligned}$$

# WURTEMBURG TOWER: 101 WURTEMBURG STREET

## Controlled Flow

5 YR						
Area No	Area (ha)	C <sub>trvr</sub>	Time (min)	Intensity mm/hr	Uncontrolled runoff L/s	Control System
R-1	0.0175	0.95	20.00	70.25	3.25	Zurn Roof
R-2	0.0214	0.95	20.00	70.25	3.96	Zurn Roof
R-3	0.0007	0.95	20.00	70.25	0.14	Zurn Roof
R-4	0.0004	0.95	20.00	70.25	0.08	Zurn Roof
A-01	0.0091	0.60	20.00	70.25	1.06	no control
A-02	0.0112	0.76	20.00	70.25	1.65	no control
A-03	0.0193	0.20	20.00	70.25	0.75	no control
Total:	0.0795				10.89	

## 100 YR

100 YR						
Area ID	Area (ha)	C <sub>trvr</sub>	Time (min)	Intensity mm hr	Uncontrolled runoff L/s	Control System
R-1	0.0175	1.00	20.00	119.95	5.84	Zurn Roof
R-2	0.0214	1.00	20.00	119.95	7.12	Zurn Roof
R-3	0.0007	1.00	20.00	119.95	0.24	Zurn Roof
R-4	0.0004	1.00	20.00	119.95	0.14	Zurn Roof
A-01	0.0091	0.68	20.00	119.95	2.05	no control
A-02	0.0112	0.85	20.00	119.95	3.16	no control
A-03	0.0193	0.25	20.00	119.95	1.61	no control
Total:	0.0795				20.15	

Note: In all cases, there is only one notch in the Zurn roof drain and flows through each drain is further reduced with and adjustable weir. See Zum roof drains sheet and adjustable weir specification for more details on the reduction of flow.

## Allowable release rate

Area	0.0795 ha	Runoff	Storage available	Storage used
		5 year event L/s	100 year event L/s	5 year event L/s
Controlled				
Roof	0.0400	2.47	3.25	14.88
Uncontrolled				
A-1	0.0091	1.06	2.05	0.00
A-2	0.0112	1.65	3.16	0.00
A-3	0.0193	0.75	1.61	0.00
Total:	0.08	5.94	10.05	14.88
				6.24
				13.13

## Summary table

Area ID	Runoff	Storage available	Storage used
	5 year event L/s	100 year event L/s	5 year event L/s
Controlled			
Roof	0.0400	2.47	14.88
Uncontrolled			
A-1	0.0091	1.06	0.00
A-2	0.0112	1.65	0.00
A-3	0.0193	0.75	0.00
Total:	0.08	5.94	14.88
			6.24
			13.13

# WUTEMBURG TOWER: 101 WURTEMBURG STREET

REQUIRED STORAGE - 5 YEAR EVENT			
AREA	R-1	BUILDING ROOF	
OTTAWA IDF CURVE	0.018	ha	Qallow = 0.83
Area = 0.95			Volumax = 3.00
			Netmax = 1.58
Time (min)	Intensity (mm/hr)	Q (L/s)	Qnet (m³)
6	141.18	6.63	5.70
10	104.19	4.82	3.99
15	83.56	3.86	3.03
20	70.25	3.26	2.42
25	60.90	2.82	1.99
30	53.93	2.49	1.66
35	48.52	2.24	1.41
40	44.18	2.04	1.21
45	40.63	1.88	1.05
50	37.65	1.74	0.91
55	35.12	1.62	0.79
60	32.94	1.52	0.69
65	31.04	1.44	0.61
70	29.37	1.36	0.53
75	27.89	1.29	0.46
80	26.56	1.23	0.40
85	25.37	1.17	0.34
90	24.29	1.12	0.29

Notes:  
Vol = Qnet x time  
Qnet = Q - Qallow

Ponding Depth vs Year Storage			
Area	V $\text{m}^3$	H $\text{m}$	H $\text{m}$
0	0.00	0.00	0.00
1	0.00	0.01	0.01
3	0.02	0.02	0.02
6	0.06	0.03	0.03
11	0.14	0.04	0.04
17	0.27	0.05	0.05
25	0.46	0.06	0.06
34	0.73	0.07	0.07
44	1.09	0.08	0.08
56	1.55	0.09	0.09
69	2.13	0.10	0.10
84	2.84	0.11	0.11
100	3.68	0.12	0.12
117	4.68	0.13	0.13
136	5.85	0.14	0.14
156	7.19	0.15	0.15

1	0.15	H = 0.112 m	Qallow = 0.00	H = 0.143 m
0.12	H	0.11		
3.68	3.00	2.84		

Note: Qallow is the flow rate through an overcontrolled Zum Roof Drain (7.46 L/sm of head.)

REQUIRED STORAGE - 5 YEAR EVENT			
AREA	R-1	BUILDING ROOF	
OTTAWA IDF CURVE	0.018	ha	Qallow = 0.83
Area = 0.95			Volumax = 3.00
			Netmax = 1.58
Time (min)	Intensity (mm/hr)	Q (L/s)	Qnet (m³)
5	0.15	178.56	8.69
10	0.15	142.89	6.96
15	0.15	119.95	5.84
20	0.15	103.85	5.06
25	0.15	91.87	4.47
30	0.15	82.58	4.02
35	0.15	75.15	3.66
40	0.15	69.05	3.36
45	0.15	63.95	3.11
50	0.15	59.62	2.90
55	0.15	55.89	2.72
60	0.15	52.65	2.56
65	0.15	49.79	2.42
70	0.15	47.26	2.30
75	0.15	44.99	2.19
80	0.15	42.95	2.09
85	0.15	41.11	2.00
90	0.15	40.44	1.96

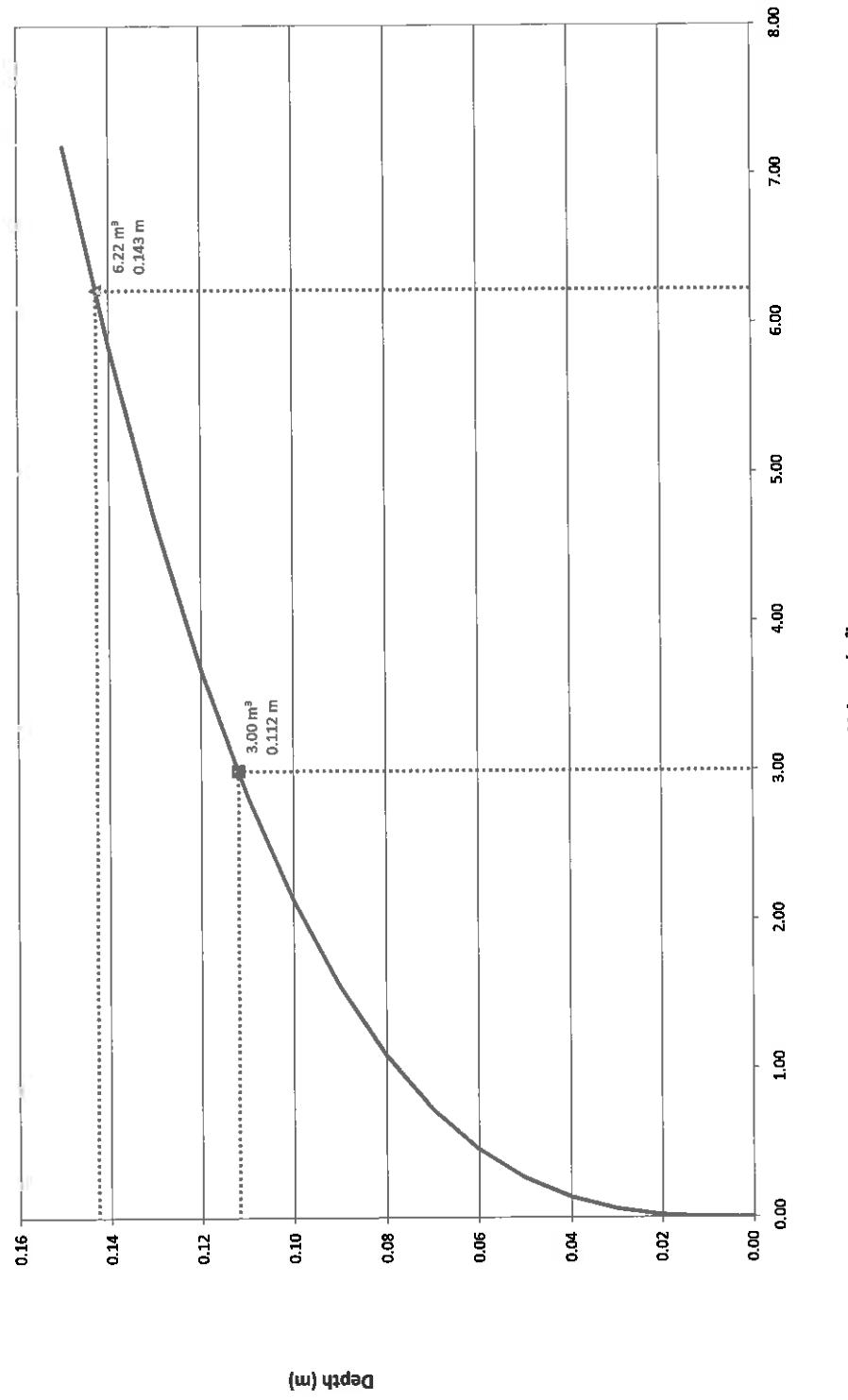
Notes:  
Vol = Qnet x time  
Qnet = Q - Qallow

Ponding Depth vs Year Storage			
Area	V $\text{m}^3$	H $\text{m}$	H $\text{m}$
0	0.00	0.00	0.00
1	0.00	0.01	0.01
3	0.02	0.02	0.02
6	0.06	0.03	0.03
11	0.14	0.04	0.04
17	0.27	0.05	0.05
25	0.46	0.06	0.06
34	0.73	0.07	0.07
44	1.09	0.08	0.08
56	1.55	0.09	0.09
69	2.13	0.10	0.10
84	2.84	0.11	0.11
100	3.68	0.12	0.12
117	4.68	0.13	0.13
136	5.85	0.14	0.14
156	7.19	0.15	0.15

Ponding Depth vs Year Storage			
Area	V $\text{m}^3$	H $\text{m}$	H $\text{m}$
0.018	0.018	0.112	0.112
1.00	1.00	0.143	0.143

M:\2011\11\10\13\DATA\Calculations\Sewer Calc1\SWM\20110211-111013-SWM Calculations.xlsx  
Note: Qallow is the flow rate through an overcontrolled Zum Roof Drain (7.46 L/sm of head.)

**Stage-Storage Curve**  
**Area R-1**



# WURTEMBURG TOWER: 101 WURTEMBURG STREET

NECESSARY DURATION - 5-YEAR EVENT			
R-2 BUILDING ROOF			
AREA	OTTAWA IDF CURVE	Qallow =	Qnet(max) =
Area = 0.021 ha	0.021 ha	Qallow = 1.29 m³	Qnet(max) = 3.22 m³
C = 0.95			
Time (min)	Intensity (mm/hr)	Q (L/s)	Vol (m³)
5	141.18	7.96	6.67
10	104.19	5.88	4.59
15	83.56	4.71	3.42
20	70.25	3.44	2.67
25	60.90	3.44	2.15
30	53.93	3.04	1.75
35	48.52	2.74	1.45
40	44.18	2.49	1.20
45	40.63	2.29	1.00
50	37.65	2.12	0.83
55	35.12	1.98	0.69
60	32.94	1.86	0.57
65	31.04	1.75	0.46
70	29.37	1.66	0.37
75	27.89	1.57	0.28
80	26.56	1.50	0.21
85	25.37	1.43	0.14
90	24.29	1.37	0.08
			0.43

Notes: Vol = Qnet x time  
Qnet = Q - Qallow

Pending Depth (5-Year Storm)			
Area	V	R <sup>2</sup>	H
0	0.00	0.00	0.00
1	0.00	0.01	0.01
3	0.02	0.02	0.02
6	0.06	0.03	0.03
11	0.13	0.04	0.04
18	0.26	0.05	0.05
26	0.45	0.06	0.06
35	0.72	0.07	0.07
46	1.07	0.08	0.08
58	1.52	0.09	0.09
71	2.09	0.10	0.10
86	2.78	0.11	0.11
102	3.61	0.12	0.12
120	4.60	0.13	0.13
140	5.74	0.14	0.14
160	7.06	0.15	0.15

Notes: Vol = Qnet x time  
Qnet = Q - Qallow

NECESSARY DURATION - 5-YEAR EVENT			
R-2 BUILDING ROOF			
AREA	OTTAWA IDF CURVE	Area = 0.021 ha	Qallow = 1.66 m³
Area = 0.95	C = 1	Qallow = 3.22 m³	Qnet(max) = 1
Time (min)	Intensity (mm/hr)	Q (L/s)	Vol (m³)
5	141.18	7.96	6.67
10	104.19	5.88	4.59
15	83.56	4.71	3.08
20	70.25	3.44	2.31
25	60.90	3.44	2.32
30	53.93	3.04	2.15
35	48.52	2.74	1.95
40	44.18	2.49	1.89
45	40.63	2.29	1.71
50	37.65	2.12	1.50
55	35.12	1.98	1.28
60	32.94	1.86	1.20
65	31.04	1.75	1.06
70	29.37	1.66	0.97
75	27.89	1.57	0.88
80	26.56	1.50	0.81
85	25.37	1.43	0.72
90	24.29	1.37	0.68
			0.43

Notes: Vol = Qnet x time  
Qnet = Q - Qallow

Pending Depth (100-Year Storm)			
Area	V	R <sup>2</sup>	H
0	0.00	0.00	0.00
1	0.00	0.01	0.01
3	0.02	0.02	0.02
6	0.06	0.03	0.03
11	0.13	0.04	0.04
18	0.26	0.05	0.05
26	0.45	0.06	0.06
35	0.72	0.07	0.07
46	1.07	0.08	0.08
58	1.52	0.09	0.09
71	2.09	0.10	0.10
86	2.78	0.11	0.11
102	3.61	0.12	0.12
120	4.60	0.13	0.13
140	5.74	0.14	0.14
160	7.06	0.15	0.15

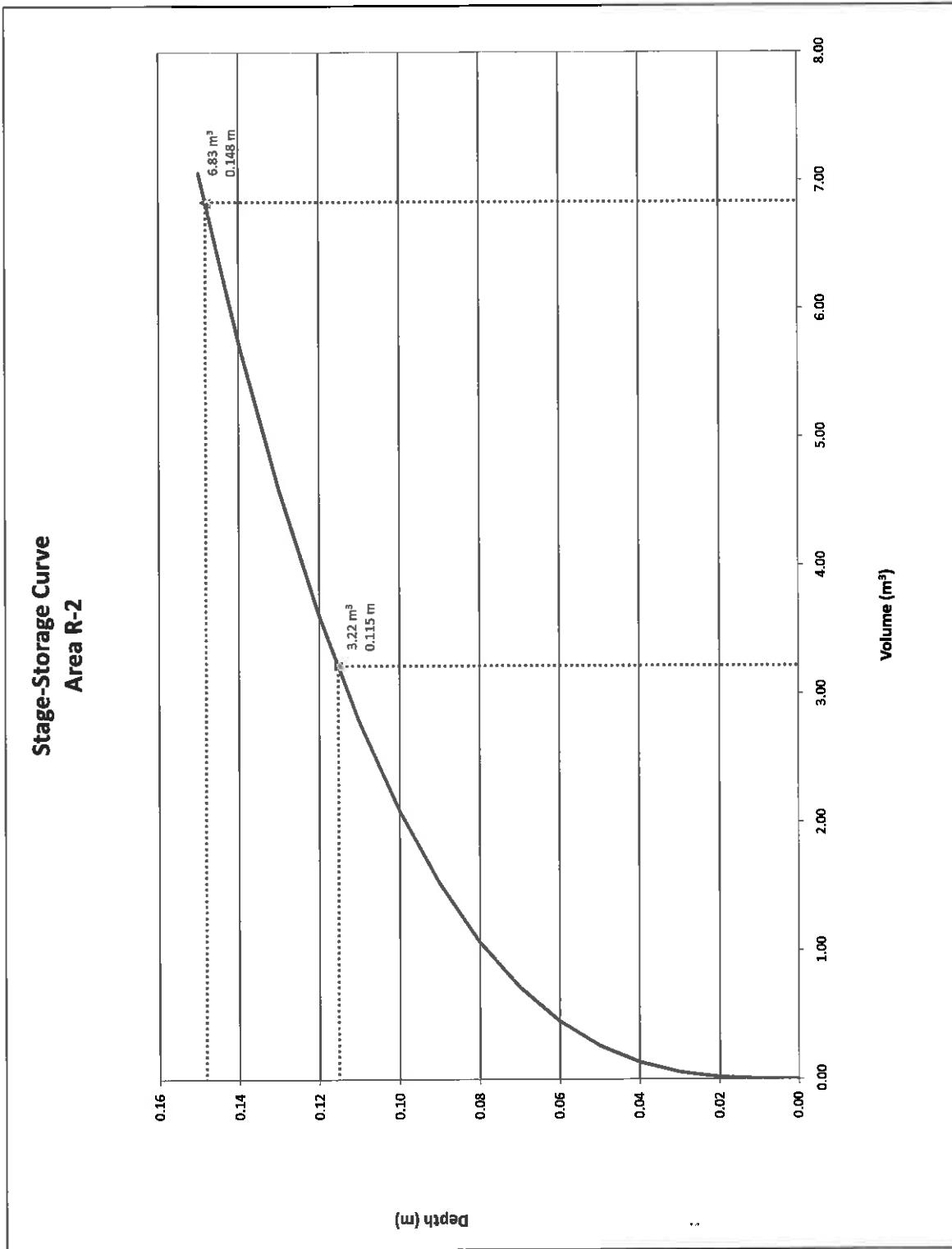
Notes: Vol = Qnet x time  
Qnet = Q - Qallow

Time (min)	Intensity (mm/hr)	Q (L/s)	Vol (m³)	Qallow = 1.66 m³
5	242.70	14.41	12.75	3.63
10	178.56	10.60	8.94	5.37
15	142.89	8.49	6.83	6.14
20	119.95	7.12	5.46	6.56
25	103.85	6.17	4.51	6.76
30	91.87	5.46	3.80	6.83
35	82.58	4.90	3.24	6.81
40	75.15	4.46	2.80	6.73
45	69.05	4.10	2.44	6.59
50	63.95	3.80	2.14	6.41
55	59.62	3.54	1.88	6.21
60	55.89	3.32	1.66	5.97
65	52.65	3.13	1.47	5.72
70	49.79	2.96	1.30	5.45
75	47.26	2.81	1.16	5.16
80	44.99	2.67	1.01	4.86
85	42.95	2.55	0.89	4.54
90	41.11	2.44	0.78	4.22

Note: Qallow is the flow rate through an overcontrolled Zum Roof Drain (11.19 L/s/m of head.)

Time (min)	Intensity (mm/hr)	Q (L/s)	Vol (m³)	Qallow = 1.66 m³
0.15	6.83	5.74	0.148 m	1.66 m³
7.06				

Note: Qallow is the flow rate through an overcontrolled Zum Roof Drain (11.19 L/s/m of head.)



# WURTEMBURG TOWER: 101 WURTEMBURG STREET

REVERSED STORM SURGE - 100 YEAR EVENT					
AREA		H-3 BUILDING ROOF			
OTTAWA IDF CURVE		Qallow = 0.20 ha		Vol(max) = 0.02 ha	
Area = 0.96	C = 0.95	Qallow = 0.20	Vol(max) = 0.02	Netmax = 1.00	
Time (min)	Intensity (mm/hr)	Q (L/s)	Qnet (L/s)	Vol (m³)	
5	141.18	0.27	0.07	0.02	
10	104.19	0.20	0.00	0.00	
15	83.56	0.16	-0.04	-0.04	
20	70.25	0.14	-0.07	-0.08	
25	60.90	0.12	-0.09	-0.13	
30	53.93	0.10	-0.10	-0.18	
35	48.52	0.09	-0.11	-0.23	
40	44.18	0.09	-0.12	-0.29	
45	40.63	0.08	-0.13	-0.34	
50	37.65	0.07	-0.13	-0.39	
55	35.12	0.07	-0.14	-0.45	
60	32.94	0.06	-0.14	-0.51	
65	31.04	0.06	-0.14	-0.56	
70	29.37	0.06	-0.15	-0.62	
75	27.89	0.05	-0.15	-0.68	
80	26.56	0.05	-0.15	-0.73	
85	25.37	0.05	-0.16	-0.79	
90	24.29	0.05	-0.16	-0.85	

Notes:  
Vol = Qnet x time  
Qnet = Q - Qallow

REVERSED STORM SURGE - 100 YEAR EVENT					
AREA		H-3 BUILDING ROOF			
OTTAWA IDF CURVE		Qallow = 0.20 ha		Vol(max) = 0.02 ha	
Area = 0.96	C = 0.95	Qallow = 0.20	Vol(max) = 0.02	Netmax = 1.00	
Time (min)	Intensity (mm/hr)	Q (L/s)	Qnet (L/s)	Vol (m³)	
5	141.18	0.27	0.07	0.02	
10	104.19	0.20	0.00	0.00	
15	83.56	0.16	-0.04	-0.04	
20	70.25	0.14	-0.07	-0.08	
25	60.90	0.12	-0.09	-0.13	
30	53.93	0.10	-0.10	-0.18	
35	48.52	0.09	-0.11	-0.23	
40	44.18	0.09	-0.12	-0.29	
45	40.63	0.08	-0.13	-0.34	
50	37.65	0.07	-0.13	-0.39	
55	35.12	0.07	-0.14	-0.45	
60	32.94	0.06	-0.14	-0.51	
65	31.04	0.06	-0.14	-0.56	
70	29.37	0.06	-0.15	-0.62	
75	27.89	0.05	-0.15	-0.68	
80	26.56	0.05	-0.15	-0.73	
85	25.37	0.05	-0.16	-0.79	
90	24.29	0.05	-0.16	-0.85	

Notes:  
Vol = Qnet x time  
Qnet = Q - Qallow

Pumping Depth (100 Year Storm)					
Area		V	H	V	H
0	0.00	0.00	0.00	0.00	0.00
0	0.00	0.01	0.01	0.00	0.01
0	0.00	0.02	0.02	0.00	0.02
0	0.00	0.03	0.03	0.00	0.03
1	0.01	0.04	0.04	0.01	0.04
1	0.02	0.05	0.05	0.02	0.05
1	0.03	0.06	0.06	0.03	0.06
2	0.04	0.07	0.07	0.04	0.07
2	0.06	0.08	0.08	0.06	0.08
3	0.09	0.09	0.09	0.09	0.09
3	0.12	0.10	0.10	0.12	0.10
4	0.16	0.11	0.11	0.16	0.11
5	0.21	0.12	0.12	0.21	0.12
6	0.27	0.13	0.13	0.27	0.13
6	0.33	0.14	0.14	0.33	0.14
7	0.41	0.15	0.15	0.41	0.15

Notes:  
Vol = Qnet x time  
Qnet = Q - Qallow

Pumping Depth (100 Year Storm)					
Area		V	H	V	H
0	0.00	0.00	0.00	0.00	0.00
0	0.00	0.01	0.01	0.00	0.01
0	0.00	0.02	0.02	0.00	0.02
0	0.00	0.03	0.03	0.00	0.03
1	0.01	0.04	0.04	0.01	0.04
1	0.02	0.05	0.05	0.02	0.05
1	0.03	0.06	0.06	0.03	0.06
2	0.04	0.07	0.07	0.04	0.07
2	0.06	0.08	0.08	0.06	0.08
3	0.09	0.09	0.09	0.09	0.09
3	0.12	0.10	0.10	0.12	0.10
4	0.16	0.11	0.11	0.16	0.11
5	0.21	0.12	0.12	0.21	0.12
6	0.27	0.13	0.13	0.27	0.13
6	0.33	0.14	0.14	0.33	0.14
7	0.41	0.15	0.15	0.41	0.15

Notes:  
Vol = Qnet x time  
Qnet = Q - Qallow

Underdrain Pumping					
Area		H	H	H	H
0.06	0.06	0.06	0.06	0.06	0.06
0.03	0.02	0.02	0.02	0.02	0.02

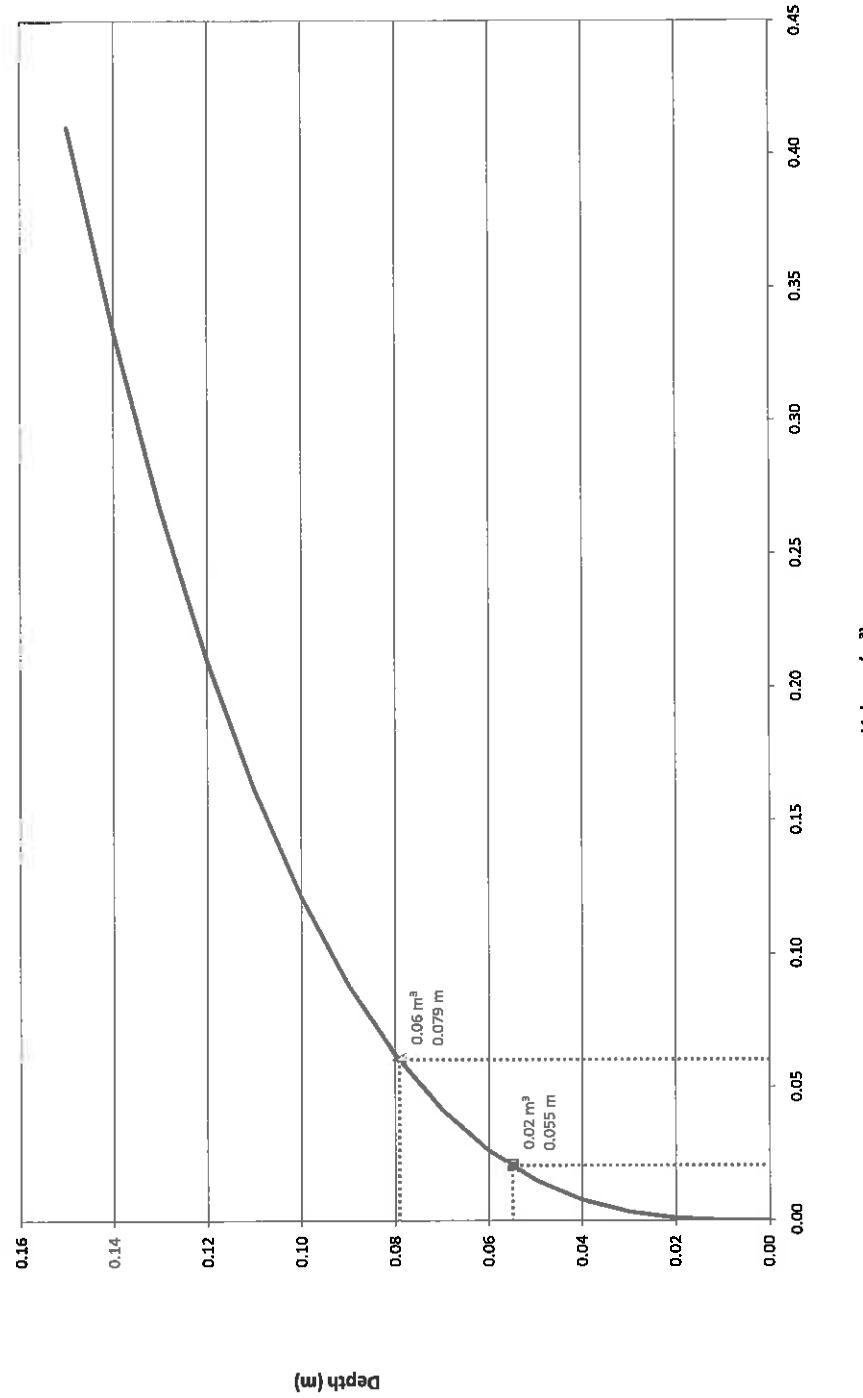
Underdrain Pumping					
Area		H	H	H	H
0.08	0.08	0.07	0.07	0.07	0.07
0.06	0.06	0.06	0.06	0.06	0.06

Underdrain Pumping					
Area		H	H	H	H
0.08	0.08	0.07	0.07	0.07	0.07
0.06	0.06	0.06	0.06	0.06	0.06

Note: Qallow is the flow rate through an overcontrolled Zum Roof Drain (3.73 L/s/m of head.)

Note: Qallow is the flow rate through an overcontrolled Zum Roof Drain (3.73 L/s/m of head.)

**Stage-Storage Curve  
Area R-3**



# WURTEMBURG TOWER: 101 WURTEMBURG STREET

REQUIRED 3-YEAR 10-YEAR EVENT			
AREA	R-4	BUILDING ROOF	
OTTAWA IDF CURVE			
Area = 0.000 ha		Qallow = 0.14 m <sup>3</sup>	
C = 0.95		Volumax = 0.00 m <sup>3</sup>	
		Note: Qallow = Volumax = 1.	
Time (min)	Intensity (mm/hr)	Q (L/s)	Qnet (L/s)
5	141.18	0.15	0.01
10	104.19	0.11	-0.03
15	83.56	0.09	-0.05
20	70.25	0.08	-0.06
25	60.90	0.07	-0.08
30	53.93	0.06	-0.10
35	48.52	0.05	-0.10
40	44.18	0.05	-0.09
45	40.63	0.04	-0.10
50	37.65	0.04	-0.10
55	35.12	0.04	-0.10
60	32.94	0.04	-0.11
65	31.04	0.03	-0.11
70	29.37	0.03	-0.11
75	27.89	0.03	-0.11
80	26.56	0.03	-0.11
85	25.37	0.03	-0.11
90	24.29	0.03	-0.11

Notes:  
Voi = Qnet x time  
Qnet = Q - Qallow

Ponding Depth (5-Year Storm)			
Area m <sup>2</sup>	V	H	H
0	0.00	0.00	0.00
0	0.00	0.01	0.01
0	0.00	0.02	0.02
0	0.00	0.03	0.03
0	0.00	0.04	0.04
0	0.01	0.05	0.05
1	0.01	0.06	0.06
1	0.02	0.07	0.07
1	0.03	0.08	0.08
1	0.04	0.09	0.09
2	0.06	0.10	0.10
2	0.08	0.11	0.11
3	0.10	0.12	0.12
3	0.13	0.13	0.13
4	0.18	0.14	0.14
4	0.22	0.15	0.15

Notes:  
Voi = Qnet x time  
Qnet = Q - Qallow

Ponding Depth (10-Year Storm)			
Area m <sup>2</sup>	V	H	H
0	0.00	0.00	0.00
0	0.00	0.01	0.01
0	0.00	0.02	0.02
0	0.00	0.03	0.03
0	0.00	0.04	0.04
0	0.01	0.05	0.05
1	0.01	0.06	0.06
1	0.02	0.07	0.07
1	0.03	0.08	0.08
1	0.04	0.09	0.09
2	0.06	0.10	0.10
2	0.08	0.11	0.11
3	0.10	0.12	0.12
3	0.13	0.13	0.13
4	0.18	0.14	0.14
4	0.22	0.15	0.15

Notes:  
Voi = Quiet x time  
Qnet = Q - Qallow

REQUIRED 3-YEAR 10-YEAR EVENT			
AREA	R-4	BUILDING ROOF	
OTTAWA IDF CURVE			
Area = 0.000 ha		Qallow = 0.14 m <sup>3</sup>	
C = 0.95		Volumax = 0.00 m <sup>3</sup>	
		Note: Qallow = Volumax = 1.	
Time (min)	Intensity (mm/hr)	Q (L/s)	Qnet (L/s)
5	141.18	0.15	0.01
10	104.19	0.11	-0.03
15	83.56	0.09	-0.05
20	70.25	0.08	-0.06
25	60.90	0.07	-0.08
30	53.93	0.06	-0.10
35	48.52	0.05	-0.10
40	44.18	0.05	-0.09
45	40.63	0.04	-0.10
50	37.65	0.04	-0.10
55	35.12	0.04	-0.10
60	32.94	0.04	-0.11
65	31.04	0.03	-0.11
70	29.37	0.03	-0.11
75	27.89	0.03	-0.11
80	26.56	0.03	-0.11
85	25.37	0.03	-0.11
90	24.29	0.03	-0.11

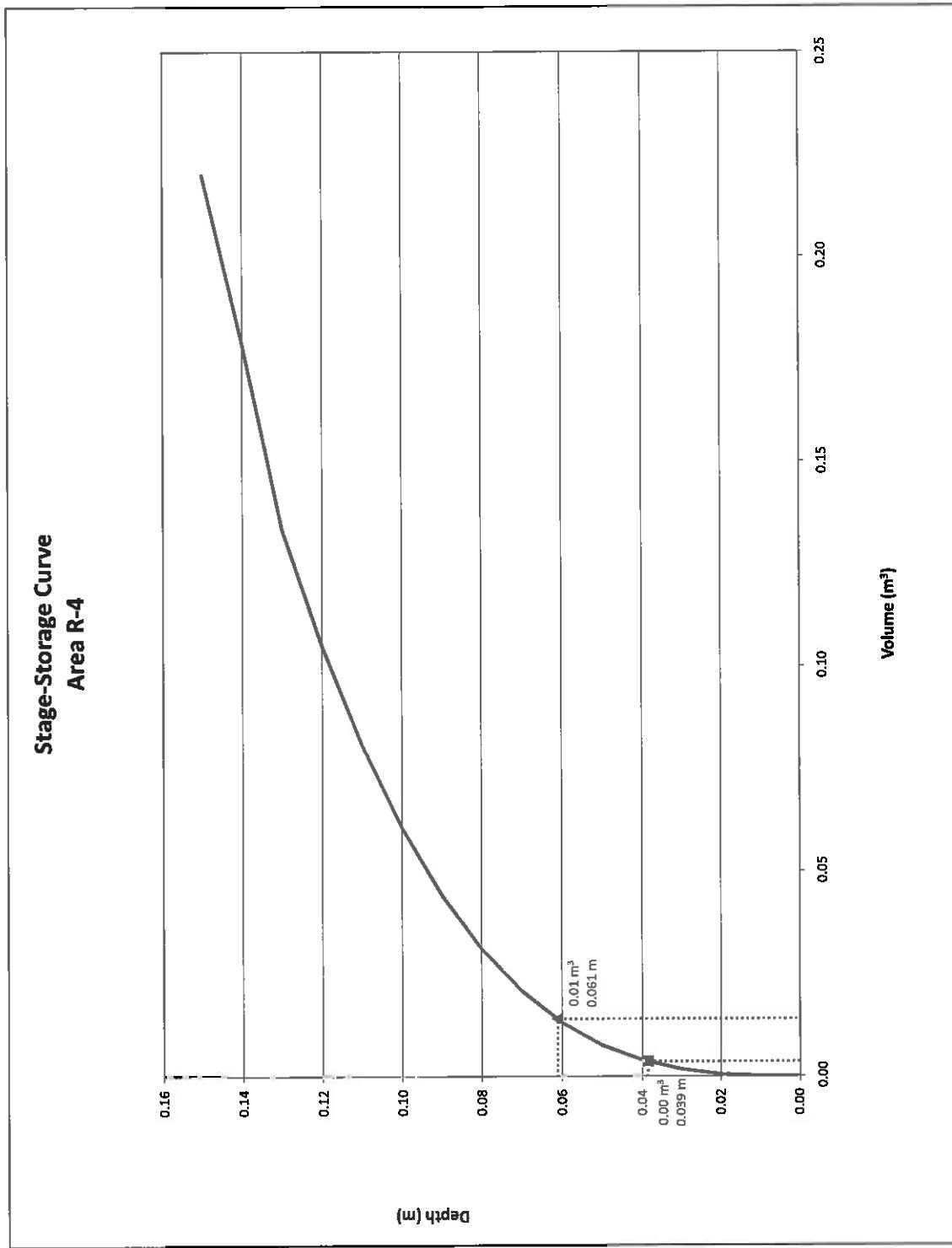
Notes:  
Voi = Quiet x time  
Qnet = Q - Qallow

Required Intensity (5-Year Event)			
Area	H	H	H
0.04	0.03	0.08	0.08
0.00	0.00	0.09	0.09
0.04	0.06	0.10	0.10
2	0.08	0.11	0.11
3	0.10	0.12	0.12
3	0.13	0.13	0.13
4	0.18	0.14	0.14
4	0.22	0.15	0.15

Note: Qallow is the flow rate through an overcontrolled Zum Roof Drain (3.73 L/s/m of head.)

Required Intensity (10-Year Event)			
Area	H	H	H
0.07	0.01	0.06	0.06
0.02	0.01	0.01	0.01
0.07	0.04	0.09	0.09
2	0.06	0.10	0.10
2	0.08	0.11	0.11
3	0.10	0.12	0.12
3	0.13	0.13	0.13
4	0.18	0.14	0.14
4	0.22	0.15	0.15

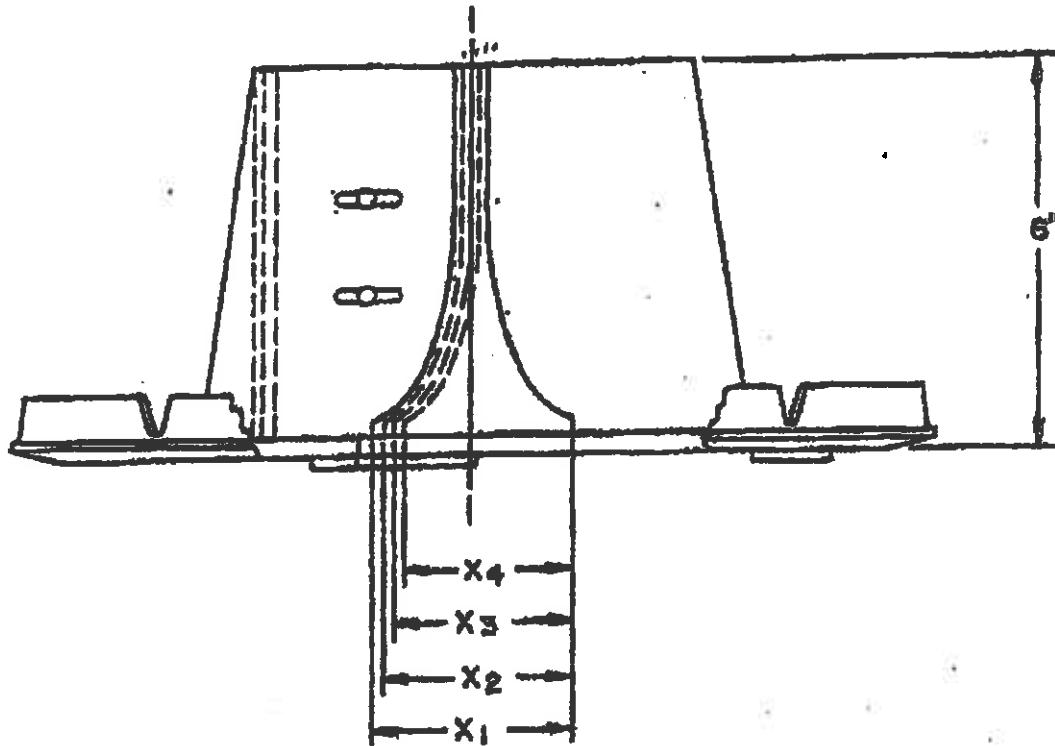
Note: Qallow is the flow rate through an overcontrolled Zum Roof Drain (3.73 L/s/m of head.)



**APPENDIX C**  
**ZURN ROOF DRAIN INFORMATION**

## NOTE:

ADJUSTABLE WEIR CAN BE ADJUSTED TO FLOW AT VARIOUS  
RATES. FOR SIZING CONTACT ZURN IND. INC.



OPENING	G.P.M. PER INCH OF HEAD	MAX FLOW G.P.M.
X <sub>1</sub>	10.5	60.50
X <sub>2</sub>	7.5	45.225
X <sub>3</sub>	5.0	30.15
X <sub>4</sub>	2.5	15.25

ADJUSTABLE WEIR FOR SLOPED-ROOF  
"CONTROL-FLO" ROOF DRAIN

PRODUCT NUMBER

Z-105-10-77

91980 BY  
ZURN IND., INC.**ZURN**

&amp; SUD GROD &amp; TUMMEL

ZURN INDUSTRIES, INC.  
ERIE, PA. U.S.A. 16512DRAWING NUMBER  
P-13521

**APPENDIX D**  
**CORRESPONDENCE**

## Justin Gauthier

---

**From:** Coombe, Bruce [Bruce.Coombe@ottawa.ca]  
**Sent:** Thursday, February 10, 2011 2:11 PM  
**To:** j.gauthier@novatech-eng.com  
**Subject:** RE: 101 Wurtemburg Street  
**Attachments:** 101 Wurtemburg.pdf

**Follow Up Flag:** Follow up  
**Flag Status:** Completed

Hi Justin,

Infrastructure Services Department provide the following comments:

No objections to the proposed sanitary flows and SWM criteria using C=0.50, 5-year storm and store up to 100 year storm on site. Install full-port backwater valves on all sanitary and storm services.

The following are boundary conditions, HGL, for hydraulic analysis at Location 1 (see attached PDF for location).

Max Day + FF = 109.0 m assuming a fire flow of 44.16 L/s

Minimum Pressure during Peak Hour = 109.8 m

Max Pressure Check = 119.28 m

These are for current conditions and are based on computer model simulation.

*Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.*

Thanks, Bruce

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**From:** Justin Gauthier [mailto:j.gauthier@novatech-eng.com]  
**Sent:** February 07, 2011 11:29 AM  
**To:** Coombe, Bruce  
**Subject:** RE: 101 Wurtemburg Street

Hi Bruce,

The following is in response to the information you require to proceed with our request for design criteria's for the site (STM, etc.) and obtain water boundary conditions:

- Average sanitary flow (L/sec): based on City of Ottawa =  $(350 \text{ L/c/d} * 48 \text{ units} * 1.8 \text{ c/unit}) = 30,240 \text{ L/d} = 0.35 \text{ L/s}$ ;
- Peak sanitary flow (L/sec): based on City of Ottawa =  $4.0 * \text{avg. flow} = 4.0 * 0.35 \text{ L/s} = 1.40 \text{ L/s}$  ( $\text{PF} = 4.26 \therefore \text{used } 4.0 \Rightarrow \text{max}$ ).
- Infiltration Allowance (L/sec): based on City of Ottawa =  $0.28 \text{ L/s/effective gross ha} * 0.0795 \text{ ha} = 0.022 \text{ L/s}$
- Approximate existing sanitary flow (L/sec): based on City of Ottawa  $\cong 350 \text{ L/c/d} * 1 \text{ unit} * 3.4 \text{ c/unit} \cong 1,190 \text{ L/d} \cong 0.014 \text{ L/s}$

⇒ with PF = 4.45 ∴ used 4.0 ⇒ max, approx. existing peak sanitary flow  $\cong 0.056 \text{ L/s}$

⇒ Existing flows could be more and definitely larger flows can be anticipated since zoning currently in place is R5C [926] F(2.5).

- Location of Service: on south side of building fronting Wurtemburg Street, the mechanical room is located to the south limit of the site;
- Type of development (plus # of Units): 13 storey condo building with 48 units (as shown on the site plan);
- Amount of Fire Flow required: mechanical informed that 44.16 L/s with fire pump (700 US gal/min) would be required;
- Average daily demand (L/sec): based on City of Ottawa =  $(350 \text{ L/c/d} * 48 \text{ units} * 1.8 \text{ c/unit}) = 30,240 \text{ L/d} = 0.35 \text{ L/s}$ ;
- Maximum daily demand (L/sec): based on City of Ottawa =  $2.5 * \text{avg. day} = 2.5 * 0.35 \text{ L/s} = 0.875 \text{ L/s}$   
based on MOE (less than 500 c) =  $4.9 * \text{avg. day} = 4.9 * 0.35 \text{ L/s} = 1.715 \text{ L/s}$ ;
- Maximum hour demand (L/sec): based on City of Ottawa =  $2.2 * \text{max. day} = 2.2 * 0.875 \text{ L/s} = 1.925 \text{ L/s}$   
based on MOE (less than 500 c) =  $7.4 * \text{avg. day} = 7.4 * 0.35 \text{ L/s} = 2.590 \text{ L/s}$ .

⇒ The mechanical informed that the max peak day to size the meter would be 5.68 L/s (75 imp gal/min), there seems to be a large variance.

Don't hesitate to call if you want to discuss any issues.

Also, do you have any expected timeline for the other information requested previously and will you be able to provide the map?

Should you have any questions, or require additional information, don't hesitate to contact me.

Regards,

**Justin Gauthier, B.A.Sc.**

EIT

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**From:** Coombe, Bruce [<mailto:Bruce.Coombe@ottawa.ca>]  
**Sent:** Thursday, February 03, 2011 1:43 PM  
**To:** [j.gauthier@novatech-eng.com](mailto:j.gauthier@novatech-eng.com)  
**Subject:** RE: 101 Wurtemburg Street

Hi Justin,

Please provide the existing and proposed sanitary flows.

For water boundary conditions, please provide the following information:

**Location of Service**

Type of development & amount of fire flow

Average daily demand: L/sec

Maximum daily demand: L/sec

Maximum hourly daily demand: L/sec

Thanks, Bruce

---

**From:** Justin Gauthier [<mailto:j.gauthier@novatech-eng.com>]

**Sent:** February 02, 2011 3:10 PM

**To:** Coombe, Bruce

**Subject:** 101 Wurtemburg Street

**Importance:** High

Hi Bruce,

I am working on the 101 Wurtemburg Street project which is located north east of the Clarence Street East and Wurtemburg Street intersection. Find attached PDF's showing the site location, partial survey and proposed 13 storey condo building development. If you could please inform of the design criteria's for the site (STM, etc.) as well as if you have specific instructions with regards to connection locations/constraints (e.g. 1 on each street). Also, if you could please provide the w/m boundary conditions as well as the schematic showing the servicing information of the area in question (location, direction, size, etc.). Thanks in advance for your help.

Should you have any questions, or require additional information, don't hesitate to contact me.

Regards,

**Justin Gauthier, B.A.Sc.**

*EIT*

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Location 1

PATRIOT ST

DE 60

**ATTACHED DRAWINGS**

- 7 111013-GP GENERAL PLAN OF SERVICES
- 8 111013-GR GRADING AND EROSION CONTROL PLAN
- 9 111013-STM STORMWATER MANAGEMENT PLAN