



FUNCTIONAL SERVICING AND STORMWATER MANAGEMENT REPORT

FOR

RICHCRAFT GROUP OF COMPANIES 590 RIDEAU STREET

CITY OF OTTAWA

PROJECT NO.: 16-849

APRIL 2016 – REV 1 © DSEL

FUNCTIONAL SERVICING AND STORMWATER MANAGEMENT REPORT 590 RIDEAU STREET RICHCRAFT GROUP OF COMPANIES

TABLE OF CONTENTS

1.0	INTRODUCTION	1
1.1	Existing Conditions	2
1.2	Required Permits / Approvals	3
1.3	Pre-consultation	3
2.0	GUIDELINES, PREVIOUS STUDIES, AND REPORTS	4
2.1	Existing Studies, Guidelines, and Reports	4
3.0	WATER SUPPLY SERVICING	5
3.1	Existing Water Supply Services	5
3.2	Water Supply Servicing Design	5
3.3	Water Supply Conclusion	6
4.0	WASTEWATER SERVICING	7
4.1	Existing Wastewater Services	7
4.2	Wastewater Design	7
4.3	Wastewater Servicing Conclusions	8
5.0	STORMWATER MANAGEMENT	9
5.1	Existing Stormwater Services	9
5.2	Post-development Stormwater Management Target	9
5.3	Proposed Stormwater Management System	10
5.4	Stormwater Servicing Conclusions	11
6.0	UTILITIES	12
7.0	EROSION AND SEDIMENT CONTROL	13
8.0	CONCLUSION AND RECOMMENDATIONS	14

FIGURES

Figure 1	Site Location
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TABLES

Table 1	Water Supply Design Criteria
Table 2	Water Demand and Boundary Conditions Proposed
	Conditions
Table 3	Wastewater Design Criteria
Table 4	Summary of Estimated Peak Wastewater Flow
Table 5	Summary of Existing Peak Storm Flow Rates
Table 6	Stormwater Flow Rate Summary

APPENDICES

Appendix A	Pre-consultation Notes
Appendix B	Water Supply

Appendix C Wastewater Collection
Appendix D Stormwater Management

Drawings / Figures Proposed Site Plan

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1.0 INTRODUCTION

David Schaeffer Engineering Limited (DSEL) has been retained to prepare a Functional Servicing and Stormwater Management report in support of the application for Site Plan Control (SPC) at 590 Rideau Street.

The subject property is located within the City of Ottawa urban boundary, in the Rideau-Vanier ward. As illustrated in *Figure 1*, the subject property is bounded by Rideau Street to the north; Besserer Street to the south and Cobourg Street to the west. The subject property measures approximately *0.137ha*.



Figure 1: Site Location

Richcraft are proposing a 7-storey residential/commercial building fronting onto Rideau Street. The proposed development would include approximately 347m² of ground level retail on the 1st level and 2-storeys of underground parking fronting onto Rideau Street. The residential component is comprised of 68 units. A copy of the proposed site plan is included in *Drawings/Figures*.

The objective of this report is to support the application for SPC by providing sufficient detail to demonstrate that the proposed development is supported by existing municipal servicing infrastructure and that the site design conforms to current City of Ottawa design standards.

1.1 Existing Conditions

The existing site currently consists of a public park space. Historical photos indicate that prior to 2012 the subject site consisted of single family homes with retail or commercial use and an asphalt parking area.

A detailed survey of the property was prepared by Annis, O'Sullivan, Vollebekk Ltd, March 31, 2016. The elevations range between **72.16m** and **71.19m** generally sloping from the north-east to south-west of the property.

Sewer and watermain mapping collected from the City of Ottawa indicate that the following services exist across the property frontages within the adjacent municipal right-of-ways:

Rideau Street

- 305mm diameter PVC watermain.
- 300mm diameter sanitary sewer
- 375mm diameter sanitary sewer

Charlotte Street

- 150mm diameter watermain
- 300mm diameter storm sewer
- 250mm diameter sanitary sewer

1.2 Required Permits / Approvals

The proposed development is subject to the site plan control approval process. The City of Ottawa must approve the engineering design drawings and reports prior to the issuance of site plan control.

1.3 Pre-consultation

Pre-Consultation was conducted with interested parties at the City of Ottawa via e-mail in March 2016.

Requirements for Stormwater management were reviewed with the City of Ottawa, and included allowable release rate based on a maximum Rational Method Coefficient of 0.50, employing IDF parameters for a 5-year storm with a calculated time of concentration equal to or greater than 10 minutes. Furthermore storms up to and including the City of Ottawa 100-year design event are to be attenuated on site.

As per pre-consultation with the City of Ottawa, the Rational Method Coefficient will be determined based on the historic use of the site. As discussed, the historic use was made up building and asphalt parking lot, essentially 100% impervious surface.

Pre-consultation correspondence, along with the servicing guidelines checklist, is located in *Appendix A*.

2.0 GUIDELINES, PREVIOUS STUDIES, AND REPORTS

2.1 Existing Studies, Guidelines, and Reports

The following studies were utilized in the preparation of this report.

- Ottawa Sewer Design Guidelines, City of Ottawa, SDG002, October 2012 (City Standards)
- Ottawa Design Guidelines Water Distribution
 City of Ottawa, July 2010.
 (Water Supply Guidelines)
 - Technical Bulletin ISD-2010-2
 City of Ottawa, December 15, 2010.
 (ISD-2010-2)
 - Technical Bulletin ISDTB-2014-02
 City of Ottawa, May 27, 2014.
 (ISDTB-2014-02)
- Design Guidelines for Sewage Works,
 Ministry of the Environment, 2008.
 (MOE Design Guidelines)
- Stormwater Planning and Design Manual,
 Ministry of the Environment, March 2003.
 (SWMP Design Manual)
- Ontario Building Code Compendium Ministry of Municipal Affairs and Housing Building Development Branch, January 1, 2010 Update (OBC)
- Water Supply for Public Fire Protection
 Fire Underwriters Survey, 1999.
 (FUS)

3.0 WATER SUPPLY SERVICING

3.1 Existing Water Supply Services

The subject property lies within the City of Ottawa 1W pressure zone. A local 300mm diameter watermain exist within the Rideau Street right-of-way. In addition, a 150mm diameter exist within Charlotte Street. An excerpt from the City of Ottawa Pressure Zone map has been included in *Appendix B*.

3.2 Water Supply Servicing Design

Water servicing will be achieved by a single 250mm diameter water service connection from the 300mm diameter watermain within Rideau Street. A 250mm diameter water service has been constructed and stubbed close to the property during the watermain reconstruction within Rideau Street between 2013 and 2015.

Table 1 summarizes the **Water Supply Guidelines** employed in the preparation of the preliminary water demand estimate.

Table 1
Water Supply Design Criteria

Design Parameter	Value
Residential Bachelor/1 Bedroom Apartment	1.4 P/unit
Residential 2 Bedroom Apartment	2.1 P/unit
Residential Average Daily Demand	350 L/d/P
Residential Maximum Daily Demand	4.9 x Average Daily *
Residential Maximum Hourly	7.4 x Average Daily *
Commercial Retail	2.5 L/m ² /d
Commercial Office	75 L/9.3m ² /d
Commercial Maximum Daily Demand	1.5 x avg. day
Commercial Maximum Hour Demand	1.8 x max. day
Minimum Watermain Size	150mm diameter
Minimum Depth of Cover	2.4m from top of watermain to finished grade
During normal operating conditions desired	350kPa and 480kPa
operating pressure is within	
During normal operating conditions pressure must	275kPa
not drop below	
During normal operating conditions pressure must	552kPa
not exceed	
During fire flow operating pressure must not drop	140kPa
below	

^{*}Daily average based on Appendix 4-A from Water Supply Guidelines

^{**} Residential Max. Daily and Max. Hourly peaking factors per MOE Guidelines for Drinking-Water Systems Table 3-3 for 0 to 500 persons.

⁻Table updated to reflect ISD-2010-2

Table 2 summarizes the anticipated water supply demand and boundary conditions for the proposed development based on the **Water Supply Guidelines**.

Table 2
Water Demand and Boundary Conditions
Proposed Conditions

Design Parameter	Anticipated Demand ¹ Boundary Co (L/min) (m H ₂ O /		
Average Daily Demand	27.6	46.5	456.2
Max Day + Fire Flow	133.1 + 5,000 = 5,133.1	40,500 L/mii	n @ 140 kPa
Peak Hour	201.3	34.0	333.5
1) Water demand calculation per Water Supply Guidelines . See Appendix B for detailed calculations.			

water demand calculation per *Water Supply Guidelines*. See *Appendix B* for detailed calculations.
 Boundary conditions supplied by the City of Ottawa for the demands indicated in the correspondence; assumed ground elevation 59m. See *Appendix B*.

The City provided both the anticipated minimum and maximum water pressures, as well as the maximum flow at 140 kPa (20 PSI) indicated by the correspondence in **Appendix B**.

Initial boundary conditions obtained indicate residual pressures within what is recommended in *Table 1*. It is recommended that a pressure check be conducted at during construction to determine if pressure controls are required.

Fire flow requirements are to be determined in accordance with Local Guidelines (*FUS*), City of Ottawa *Water Supply Guidelines*, and the Ontario Building Code.

Using the *FUS* method a conservative estimation of fire flow had been established. Based on information received from *Graziani & Corazza Architects*, the following assumptions were assumed:

- Type of construction Fire Resistive Construction
- Occupancy type Limited Combustibility
- Sprinkler Protection Supervised Sprinkler System

The above assumptions result in an estimated fire flow of approximately **5,000 L/min**; actual building materials selected will affect the estimated flow, see **Appendix B** for detailed FUS calculations. Approximately **40,500 L/min** flow is available within the municipal system at minimum pressure, sufficient to service the proposed development.

3.3 Water Supply Conclusion

Anticipated water demand under proposed conditions was submitted to the City of Ottawa for establishing boundary conditions. As demonstrated by *Table 2*, based on the City's model, the municipal system is capable of delivering water within the *Water Supply Guidelines* pressure range. Sufficient flow is available at minimum pressure

within the municipal system to provide fire protection for the site. The proposed water supply design conforms to all relevant City Guidelines and Policies.

4.0 WASTEWATER SERVICING

4.1 Existing Wastewater Services

The subject site is tributary to the Interceptor Sewer. An existing 200mm diameter sanitary sewers has been installed, stubbed at the property line, discharging to the 300mm sanitary sewer located within Rideau Street.

The site currently consists of open space and construction staging area, historical uses for the site included asphalt parking lot and single family residence.

4.2 Wastewater Design

The proposed development will use the existing 200mm sanitary sewer stub.

Table 3 summarizes the **City Standards** employed in the design of the proposed wastewater sewer system.

Table 3
Wastewater Design Criteria

Design Parameter	Value		
Residential 1 Bedroom Apartment	1.4 P/unit		
Residential 2 Bedroom Apartment	2.1 P/unit		
Average Daily Demand	350 L/d/per		
Peaking Factor	Harmon's Peaking Factor. Max 4.0, Min 2.0		
Commercial Floor Space	5 L/m ² /d		
Commercial Office Space	75 L/9.3m ² /d		
Infiltration and Inflow Allowance	0.28L/s/ha		
Industrial Peaking Factor	7.0 per City of Ottawa Sewer Design Guidelines Appendix 4B		
Sanitary sewers are to be sized employing the Manning's Equation	$Q = \frac{1}{n} A R^{\frac{2}{3}} S^{\frac{1}{2}}$		
Minimum Sewer Size	200mm diameter		
Minimum Manning's 'n'	0.013		
Minimum Depth of Cover	2.5m from crown of sewer to grade		
Minimum Full Flowing Velocity	0.6m/s		
Maximum Full Flowing Velocity	3.0m/s		
Extracted from Sections 4 and 6 of the City of Ottawa Sewer Design Guidelines, October 2012.			

Table 4 demonstrates the anticipated peak flow from the proposed development. See **Appendix C** for associated calculations.

Table 4
Summary of Estimated Peak Wastewater Flow

Design Parameter	Total Flow (L/s)	
Estimated Average Dry Weather Flow	0.49	
Estimated Peak Dry Weather Flow	1.86	
Estimated Peak Wet Weather Flow	1.90	

The estimated sanitary flow based on the proposed plan provided in *Drawings/Figures* anticipates a peak wet weather flow of *1.90 L/s*.

An analysis of the sanitary sewer fronting the subject site within Rideau Street was completed in March 2012 by Delcan for the City of Ottawa. As per the **Delcan Design Brief**, the subject site is included as part of **SAN 3** drainage area to the sanitary sewer, see **Appendix C** for drainage map. Based on the sanitary analysis prepared by Declan, the most restrictive section of sanitary sewer is located directly upstream of the existing 750mm diameter sanitary sewer east of Chapel Street. The most restrictive section has **50.1 L/s** of residual capacity, see **Appendix C** for excerpt from **Delcan Design Brief**. The analysis was only completed up to the eventual discharge to the existing 750mm diameter sanitary sewer within Chapel Street.

Based on the sanitary analysis included in the **Declan Design Brief**, the controlling section of the local sewer system is located within Rideau Street, east of Chapel Street, with an available residual capacity of **50.1L/s**.

The analysis above indicates that sufficient capacity is available in the local sewers to accommodate the proposed development.

4.3 Wastewater Servicing Conclusions

The site is tributary to the Rideau River Collector sewer; based on the sanitary analysis sufficient capacity is available to accommodate the anticipated 1.90 L/s peak wet weather flow from the proposed development.

The proposed wastewater design conforms to all relevant *City Standards*.

5.0 STORMWATER MANAGEMENT

5.1 Existing Stormwater Services

Stormwater runoff from the subject property is tributary to the Ottawa River. As such, approvals for proposed development within this area are under the approval authority of the City of Ottawa.

Flows that influence the watershed in which the subject property is located are further reviewed by the principal authority. The subject property is located within the Ottawa River watershed, and is therefore subject to review by the Rideau Valley Conservation Authority (RVCA).

A portion of the subject site's runoff is directed to existing catch basins and assumed to discharge to surrounding municipal sewers. The remainder of the site is directed off-site via overland flow to adjacent properties and the municipal right-of-ways.

Two existing 250mm diameter storm sewers have been extended to the limit of the site during the reconstruction and separation of the Rideau Street combined sewer system.

It is appears that the existing site has no stormwater management controls. Predevelopment runoff rates were generated assuming the original asphalt prior to the landowner converting the lands to park space.

The estimated pre-development peak flows for the 2, 5, and 100-year are summarized in *Table 5*:

Table 5
Summary of Existing Peak Storm Flow Rates

City of Ottawa Design Storm	Estimated Peak Flow Rate (L/s)	
2-year	11.7	
5-year	15.9	
100-year	34.0	

5.2 Post-development Stormwater Management Target

Stormwater management requirements for the proposed development were reviewed with the City of Ottawa, see correspondence in *Appendix A*, where the proposed development is required to:

Control to an allowable release rate based on a Rational Method Coefficient of 0.50, employing the City of Ottawa IDF parameters for a 5-year storm with a calculated time of concentration no less than 10 minutes;

- Attenuate all storms up to and including the City of Ottawa 100-year design event are to be attenuated on site;
- The proposed development does not contemplate surface parking, therefore, quality controls are not required, see correspondence with RVCA in *Appendix A*

Based on the above the allowable release rate for the proposed development is **19.8** *L/s*.

5.3 Proposed Stormwater Management System

It is proposed to re-use the existing 250mm diameter storm sewer, stubbed at the edge of the site. The existing storm sewers discharge to the existing 375mm diameter storm sewer within Rideau Street. The storm sewer to be used will be selected by the mechanical engineer, based on the internal mechanical layout.

In order to achieve the allowable post-development stormwater runoff release rate identified in **Section 5.2** above, the proposed development will employ flow attenuation using cistern storage. It is proposed to pump stormwater to the allowable release rate form the stormwater storage to the existing 250mm diameter storm sewer stubbed at the property.

Table 6 presents the estimated release rates, storage requirements and available storage for the proposed development.

Table 6
Stormwater Flow Rate Summary

Control Area	5-Year 5-Year 100-Year		100-Year	
	Release Rate	Storage	Release Rate	Storage
	(L/s)	(m³)	(L/s)	(m³)
Unattenuated Areas	4.2	0.0	8.9	0.0
Attenuated Areas	5.7	18.5	10.9	35.6
Total	9.9	18.5	19.8	35.6

As indicated in **Table 6** it is anticipated that **35.6** m^3 of onsite storage will be required to attenuate stormwater runoff to the allowable release rate of **19.8** L/s. The proposed drainage boundaries and overland flow routes are illustrated by **SWM-1** included with this report.

As discussed in **Section 5.2**, the proposed development does not proposed surface parking, therefore, stormwater quality controls are not required, as per correspondence with the RVCA in **Appendix A**.

5.4 Stormwater Servicing Conclusions

Post development stormwater runoff will be attenuated onsite for storm events up to and including the 1:100 year in accordance with *City Standards*. *35.6 m*³ of onsite storage will be required to attenuate stormwater runoff to the site's allowable release rate.

No on-site quality controls are required as the proposed site plan does not consider any surface parking spaces.

The design of the proposed storm sewer system conforms to all relevant *City Standards*.

FUNCTIONAL SERVICING AND STORMWATER MANAGEMENT REPORT RICHCRAFT GROUP OF COMPANIES APRIL 2016 – REV 1 590 RIDEAU STREET

6.0 UTILITIES

Gas, Bell and Hydro services currently exist within the Rideau Street and Besserer Street right-of-ways. Utility servicing will be coordinated with the individual utility companies prior to site development.

7.0 EROSION AND SEDIMENT CONTROL

Soil erosion occurs naturally and is a function of soil type, climate and topography. The extent of erosion losses is exaggerated during construction where vegetation has been removed and the top layer of soil becomes agitated.

Prior to topsoil stripping, earthworks or underground construction, erosion and sediment controls will be implemented and will be maintained throughout construction.

Silt fence will be installed around the perimeter of the site and will be cleaned and maintained throughout construction. Silt fence will remain in place until the working areas have been stabilized and re-vegetated.

Catch basins will have filter fabric installed under the grate during construction to protect from silt entering the storm sewer system.

A mud mat will be installed at the construction access in order to prevent mud tracking onto adjacent roads.

Erosion and sediment controls must be in place during construction. The following recommendations to the contractor will be included in contract documents.

- Limit extent of exposed soils at any given time.
- Re-vegetate exposed areas as soon as possible.
- Minimize the area to be cleared and grubbed.
- Protect exposed slopes with plastic or synthetic mulches.
- Install silt fence to prevent sediment from entering existing ditches.
- No refueling or cleaning of equipment near existing watercourses.
- Provide sediment traps and basins during dewatering.
- Install filter cloth between catch basins and frames.
- Plan construction at proper time to avoid flooding.

Establish material stockpiles away from watercourses, so that barriers and filters may be installed.

The contractor will, at every rainfall, complete inspections and guarantee proper performance. The inspection is to include:

- Verification that water is not flowing under silt barriers.
- Clean and change filter cloth at catch basins.

8.0 CONCLUSION AND RECOMMENDATIONS

David Schaeffer Engineering Ltd. (DSEL) has been retained to prepare an Assessment of Adequacy of Public Services report in support of the application for a Zoning By-law Amendment (ZBLA) and Site Plan Control (SPC) at 590 Rideau Street. The preceding report outlines the following:

- Based on boundary conditions provided by the City the existing municipal water infrastructure is capable of providing the proposed development with water within the City's required pressure range;
- A pressure check be conducted at the completion of construction to determine if pressure controls are required;
- The FUS method for estimating fire flow indicated approximately **5,000 L/min** is required for the proposed development;
- The proposed development is anticipated to have a peak wet weather flow of **1.90 L/s**; Based on the sanitary analysis conducted the existing municipal sewer infrastructure has sufficient capacity to support the development;
- Based on pre-consultation with the City of Ottawa, stormwater quantity controls are required to attenuate peak flow to 19.8 L/s;
- It is proposed that stormwater objectives will be met through storm water retention via subsurface storage, it is anticipated that **35.6** m^3 of onsite storage will be required to attenuate flow to the established release rate above;
- The development does not contemplate any surface parking, therefore, quality controls are not required.

Prepared by,

David Schaeffer Engineering Ltd.

Reviewed by,

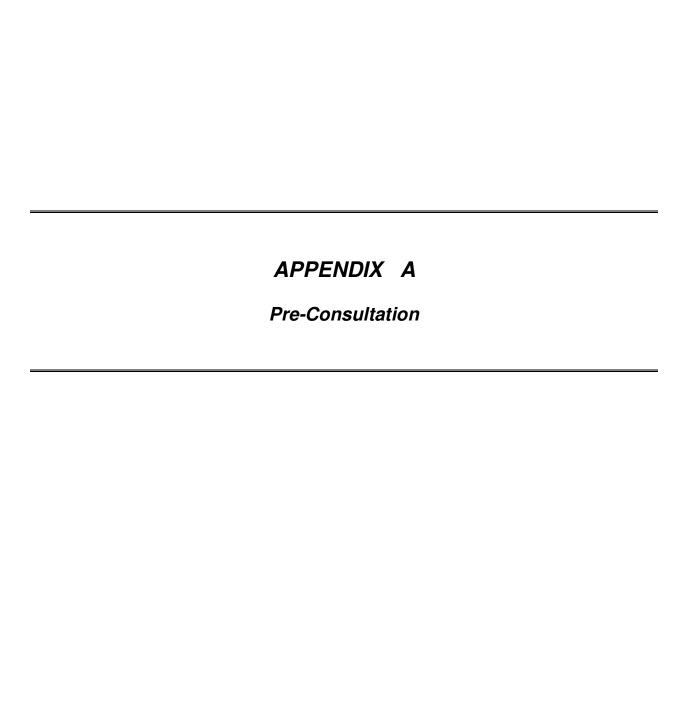
David Schaeffer Engineering Ltd.

PROFESSIONAL

A. D. FOBER 100090626

Per: Steve L. Merrick, EIT.

Per: Adam D. Fobert, P.Eng



DEVELOPMENT SERVICING STUDY CHECKLIST

15-849 20/04/2016

11	General Content	
4.1	Executive Summary (for larger reports only).	N/A
	Date and revision number of the report.	Report Cover Sheet
	Location map and plan showing municipal address, boundary, and layout of	Report Cover Sileet
\boxtimes	proposed development.	Drawings/Figures
\boxtimes	Plan showing the site and location of all existing services.	Figure 1
	Development statistics, land use, density, adherence to zoning and official plan,	
	and reference to applicable subwatershed and watershed plans that provide	
\boxtimes	context to applicable subwatershed and watershed plans that provide context	Section 1.0
	to which individual developments must adhere.	
\boxtimes	Summary of Pre-consultation Meetings with City and other approval agencies.	Section 1.3
	Reference and confirm conformance to higher level studies and reports (Master	
\boxtimes	Servicing Studies, Environmental Assessments, Community Design Plans), or in	Section 2.1
	the case where it is not in conformance, the proponent must provide	Section 2.1
	justification and develop a defendable design criteria.	
\boxtimes	Statement of objectives and servicing criteria.	Section 1.0
\boxtimes	Identification of existing and proposed infrastructure available in the immediate	Sections 3.1, 4.1, 5.1
	area.	300000000000000000000000000000000000000
_	Identification of Environmentally Significant Areas, watercourses and Municipal	
	Drains potentially impacted by the proposed development (Reference can be	N/A
	made to the Natural Heritage Studies, if available).	
	Concept level master grading plan to confirm existing and proposed grades in	
	the development. This is required to confirm the feasibility of proposed	CD 1
\boxtimes	stormwater management and drainage, soil removal and fill constraints, and	GP-1
	potential impacts to neighbouring properties. This is also required to confirm	
	that the proposed grading will not impede existing major system flow paths. Identification of potential impacts of proposed piped services on private	
	services (such as wells and septic fields on adjacent lands) and mitigation	N/A
ш	required to address potential impacts.	N/A
	Proposed phasing of the development, if applicable.	N/A
\boxtimes	Reference to geotechnical studies and recommendations concerning servicing.	Section 1.4
	All preliminary and formal site plan submissions should have the following	Section 1.4
	information:	
	-Metric scale	
	-North arrow (including construction North)	
	-Key plan	
\boxtimes	-Name and contact information of applicant and property owner	SSP-1
	-Property limits including bearings and dimensions	
	-Existing and proposed structures and parking areas	
	-Easements, road widening and rights-of-way	
	-Adjacent street names	
4.2	Development Servicing Report: Water	
	Confirm consistency with Master Servicing Study, if available	N/A

4.2	4.2 Development Servicing Report: Water						
	Confirm consistency with Master Servicing Study, if available	N/A					
\boxtimes	Availability of public infrastructure to service proposed development	Section 3.1					
\boxtimes	Identification of system constraints	Section 3.1					
\boxtimes	Identify boundary conditions	Section 3.1, 3.2					
\boxtimes	Confirmation of adequate domestic supply and pressure	Section 3.3					

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fire flow at locations throughout the development. Provide a check of high pressures. If pressure is found to be high, an assessment	ection 3.2
fire flow at locations throughout the development. Provide a check of high pressures. If pressure is found to be high, an assessment	
Provide a check of high pressures. If pressure is found to be high, an assessment	
is required to confirm the application of pressure reducing valves.	N/A
Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defined phases of the project including the ultimate design	N/A
Address reliability requirements such as appropriate location of shut-off valves	N/A
☐ Check on the necessity of a pressure zone boundary modification	N/A
Reference to water supply analysis to show that major infrastructure is capable	•
of delivering sufficient water for the proposed land use. This includes data that	
shows that the expected demands under average day, peak hour and fire flow	tion 3.2, 3.3
conditions provide water within the required pressure range	
Description of the proposed water distribution network, including locations of	
proposed connections to the existing system, provisions for necessary looping,	NI/A
and appurtenances (valves, pressure reducing valves, valve chambers, and fire	N/A
hydrants) including special metering provisions.	
Description of off-site required feedermains, booster pumping stations, and	
other water infrastructure that will be ultimately required to service proposed	N/A
development, including financing, interim facilities, and timing of	N/A
implementation.	
Confirmation that water demands are calculated based on the City of Ottawa	oction 3 /
Design Guidelines.	ection 3.2
Design Guidelines. Provision of a model schematic showing the boundary conditions locations,	
Design Guidelines. Provision of a model schematic showing the boundary conditions locations.	N/A
Design Guidelines. Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference.	
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Design Guidelines. Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference. 4.3 Development Servicing Report: Wastewater Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitored flow data from relatively new infrastructure cannot be used to justify capacity requirements for proposed infrastructure). Confirm consistency with Master Servicing Study and/or justifications for	N/A
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ii DSEL©

	Pumping stations: impacts of proposed development on existing pumping stations or requirements for new pumping station to service development.	N/A
	Forcemain capacity in terms of operational redundancy, surge pressure and	N/A
	maximum flow velocity. Identification and implementation of the emergency overflow from sanitary pumping stations in relation to the hydraulic grade line to protect against basement flooding.	N/A
	Special considerations such as contamination, corrosive environment etc.	N/A
4.4	Development Servicing Report: Stormwater Checklist	
\boxtimes	Description of drainage outlets and downstream constraints including legality of outlets (i.e. municipal drain, right-of-way, watercourse, or private property)	Section 5.1
\boxtimes	Analysis of available capacity in existing public infrastructure.	Section 5.1, Appendix D
\boxtimes	A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns, and proposed drainage pattern.	Drawings/Figures
\boxtimes	Water quantity control objective (e.g. controlling post-development peak flows to pre-development level for storm events ranging from the 2 or 5 year event (dependent on the receiving sewer design) to 100 year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects.	Section 5.2
\boxtimes	Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements.	Section 5.2
\boxtimes	Description of the stormwater management concept with facility locations and descriptions with references and supporting information	Section 5.3
	Set-back from private sewage disposal systems.	N/A
	Watercourse and hazard lands setbacks.	N/A
\boxtimes	Record of pre-consultation with the Ontario Ministry of Environment and the	Appendix A
	Conservation Authority that has jurisdiction on the affected watershed.	Appendix A
	Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists.	N/A
\boxtimes	Storage requirements (complete with calculations) and conveyance capacity for minor events (1:5 year return period) and major events (1:100 year return period).	Section 5.3
	Identification of watercourses within the proposed development and how watercourses will be protected, or, if necessary, altered by the proposed development with applicable approvals.	N/A
\boxtimes	Calculate pre and post development peak flow rates including a description of existing site conditions and proposed impervious areas and drainage catchments in comparison to existing conditions.	Section 5.1, 5.3
	Any proposed diversion of drainage catchment areas from one outlet to another.	N/A
	Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and stormwater management facilities.	N/A
	If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post-development flows up to and including the 100-year return period storm event.	N/A
	Identification of potential impacts to receiving watercourses	N/A
	Identification of municipal drains and related approval requirements.	N/A

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\boxtimes	Descriptions of how the conveyance and storage capacity will be achieved for the development.	Section 5.3
	100 year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading.	N/A
	Inclusion of hydraulic analysis including hydraulic grade line elevations.	N/A
\boxtimes	Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors.	Section 6.0
	Identification of floodplains – proponent to obtain relevant floodplain	
	information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions.	N/A
	Identification of fill constraints related to floodplain and geotechnical investigation.	N/A
4.5	Approval and Permit Requirements: Checklist	
\boxtimes	Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement ct. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act.	Section 1.2
	Application for Certificate of Approval (CofA) under the Ontario Water Resources Act.	N/A
	Changes to Municipal Drains.	N/A
	Other permits (National Capital Commission, Parks Canada, Public Works and Government Services Canada, Ministry of Transportation etc.)	N/A
4.6	Conclusion Checklist	
\boxtimes	Clearly stated conclusions and recommendations	Section 8.0
	Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency.	
	All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario	

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Steve Merrick

From: White, Joshua < Joshua. White@ottawa.ca>

Sent: March-01-16 1:43 PM

To: 'Steve Merrick'

Subject: RE: 590 Rideau - Engineering Pre-consultation

Hi Steve,

I can confirm that the below is correct and meets the Cities requirements for the site.

Joshua White, P.Eng.
Project Manager, Infrastructure Approvals
Development Review, Urban Services, City of Ottawa
Please consider the environment before printing this e-mail.



City of Ottawa | Ville d'Ottawa 613.580.2424 ext./poste 15843 Email: joshua.white@ottawa.ca

attana a s/alamaian / attana a s/

ottawa.ca/planning / ottawa.ca/urbanisme

From: Steve Merrick [mailto:smerrick@dsel.ca] **Sent:** Tuesday, March 01, 2016 1:26 PM

To: White, Joshua

Subject: 590 Rideau - Engineering Pre-consultation

Hi Josh,

I believe that you have already been through the pre-consultation process on the above noted project, we just wanted to confirm some of the requirements for the site. I understand that even though the current site is a city park and landscaped that the allowable release rate will be based on the previous land use (100% impervious) and therefore runoff coefficient of 0.50 is acceptable.

We hope you can confirm the criteria for determining the allowable release rate (0.50 RC, calculated Tc, 5-year storm) and confirm if the City has a preferred sanitary outlet (Rideau or Charlotte).

We will be sending over a boundary condition request in the near future.



Steve Merrick, EIT. Project Coordinator / Junior Designer

DSEL

david schaeffer engineering ltd.

120 Iber Road, Unit 103 Stittsville, ON K2S 1E9

phone: (613) 836-0856 ext. 561

cell: (613) 222-7816 email: smerrick@DSEL.ca

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Steve Merrick

From: Jocelyn Chandler < jocelyn.chandler@rvca.ca>

Sent: April-20-16 9:58 AM **To:** Steve Merrick

Subject: RVCA RE: 590 Rideau St - Quality Control Requirements

Hello Steve,

Based on the information you have provided, the development appears to have limited hard surfaces for parking or drive aisles. For the purpose of surface water quality protection, roof top runoff is deemed clean. The RVCA will not be advising that additional quality controls are required on-site provided the site plan reflects the above described condition. Jocelyn.

Jocelyn Chandler M.Pl. MCIP, RPP Planner, RVCA

t) 613-692-3571 x1137

f) 613-692-0831

jocelyn.chandler@rvca.ca

www.rvca.ca

mail: Box 599 3889 Rideau Valley Dr., Manotick, ON K4M 1A5

courier: 3889 Rideau Valley Dr., Nepean, ON K2C 3H1

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From: Steve Merrick [mailto:smerrick@dsel.ca]

Sent: Tuesday, April 19, 2016 3:22 PM

To: Jocelyn Chandler < jocelyn.chandler@rvca.ca> **Subject:** 590 Rideau St - Quality Control Requirements

Hi Jocelyn,

We have been retained to provide our services for a development located at 590 Rideau Street. The proposed development will include a 7 storey residential building with associated underground parking, see attached site plan. The building footprint takes up the majority of the site, flow attenuation is provided by an internal cistern. The storm is directed to a newly separated storm sewer within Rideau and based on best available information, travels approx. 2.5km prior to discharging to the Ottawa River, see sketch below.



We would like to confirm the quality control requirement for the above noted site.

Thanks,

Steve Merrick, EIT.
Project Coordinator / Junior Designer

DSEL

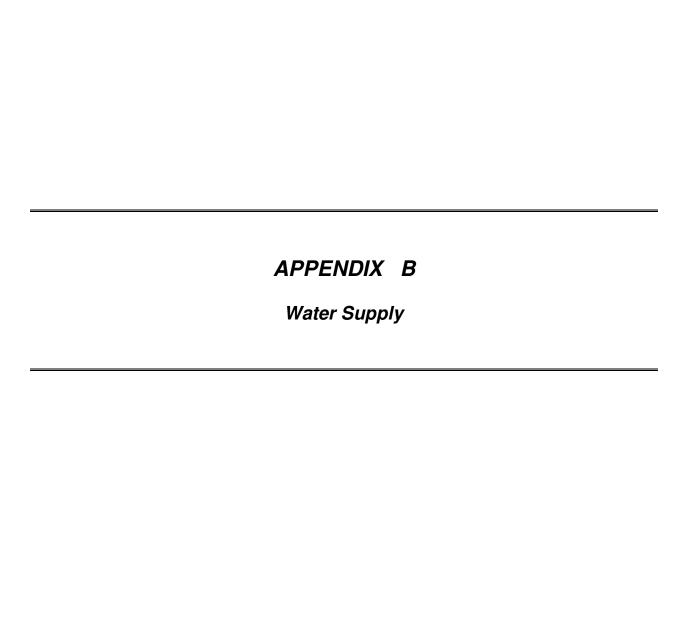
david schaeffer engineering ltd.

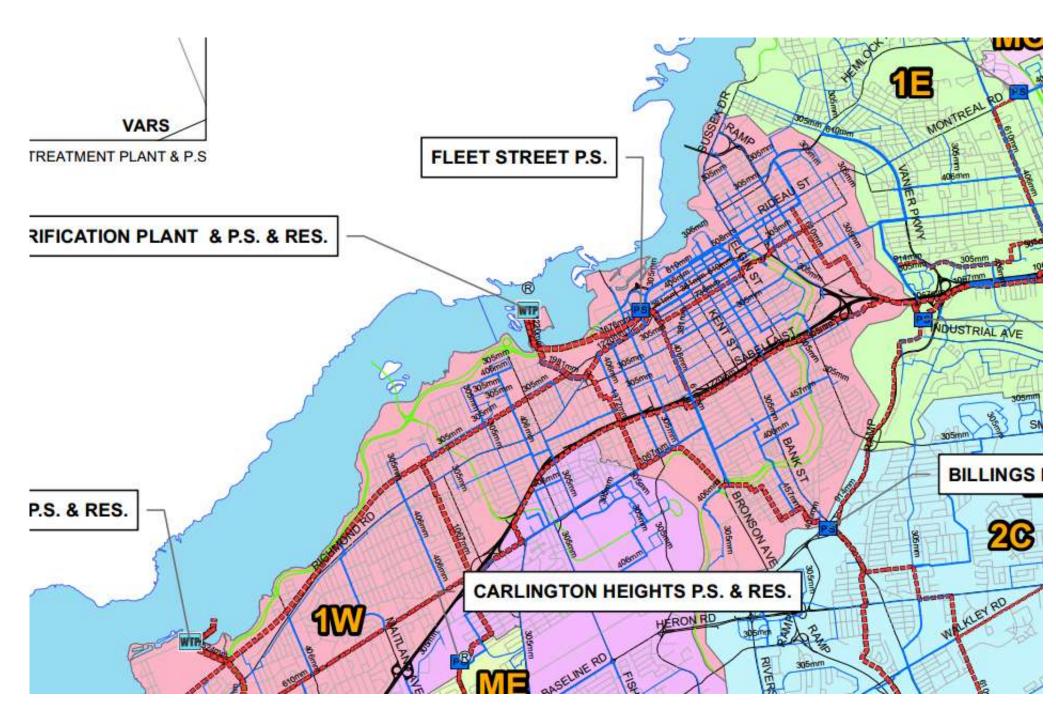
120 Iber Road, Unit 103 Stittsville, ON K2S 1E9

phone: (613) 836-0856 ext. 561 **cell**: (613) 222-7816

email: smerrick@DSEL.ca

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Steve Merrick

From: White, Joshua <Joshua.White@ottawa.ca>

Sent: March-15-16 2:22 PM

To: 'Steve Merrick'

Subject: FW: 590 Rideau St - Water Boundary Condition

Attachments: 590 Rideau MArch 2016.pdf

Hi Steve,

Please find below the boundary conditions for 590 Rideau St.

Josh

****The following information may be passed on to the consultant, but do NOT forward this e-mail directly.****

The following are boundary conditions, HGL, for hydraulic analysis at 590 Rideau (zone 1W) assumed to be connected to the 305mm on Rideau (see attached PDF for location).

Minimum HGL = 105.5m

Maximum HGL = 118.0m

Available Flow = 675 L/s assuming a residual of 20 psi and a ground elevation of 71.5m

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

From: Steve Merrick [mailto:smerrick@dsel.ca]
Sent: Tuesday, March 01, 2016 5:07 PM

To: White, Joshua

Subject: 590 Rideau St - Water Boundary Condition

Hi Josh

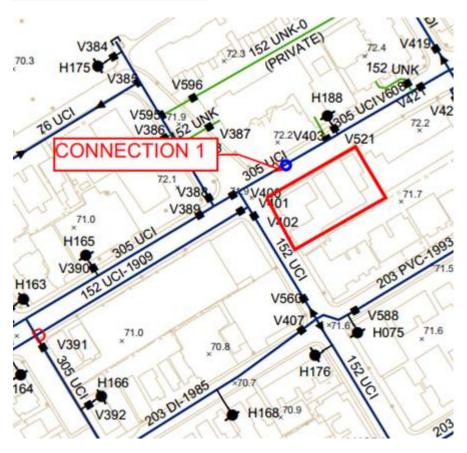
We would like to request boundary conditions for the contemplated development of 590 Rideau Street. The proposed development will consist of a 7 storey building totaling 68 residential units. It is proposed to provide a 150mm service connection to the existing 305mm watermain within Rideau Street, see attached sketch.

We hope that you can provide the maximum flow from the existing connection point at a minimum pressure of 140 kPa (20 PSI) as we do not have sufficient building information to provide an estimate of fire flow based on the FUS at this

time. Once information is available we will calculate fire flow as per the FUS and compare to the provided maximum flow rate.

The anticipated water demands are summarized below:

	L/min	L/s
Avg. Daily	27.6	0.46
Max Day	133.1	2.22
Peak Hour	201.3	3.35



Steve Merrick, EIT.
Project Coordinator / Junior Designer

DSEL

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Water Demand Design Flows per Unit Count City of Ottawa - Water Distribution Guidelines, July 2010



Domestic Demand

Type of Housing	Per / Unit	Units	Pop
Single Family	3.4		0
Semi-detached	2.7		0
Townhouse	2.7		0
Apartment			0
Bachelor	1.4	10	14
1 Bedroom	1.4	37	52
2 Bedroom	2.1	21	45
3 Bedroom	3.1		0
Average	1.8		0

	Pop	Avg. Daily		Max Day		Peak Hour	
		m³/d	L/min	m³/d	L/min	m³/d	L/min
Total Domestic Demand	111	38.9	27.0	190.4	132.2	287.5	199.6

Institutional / Commercial / Industrial Demand

				Avg. D	Daily	Max I	Day	Peak I	lour
Property Type	Unit	Rate Uni	its	m³/d	L/min	m³/d	L/min	m³/d	L/min
Commercial floor space	2.5	L/m ² /d	347	0.87	0.6	1.3	0.9	2.3	1.6
Office	75	L/9.3m ² /d		0.00	0.0	0.0	0.0	0.0	0.0
Industrial - Light	35,000	L/gross ha/d		0.00	0.0	0.0	0.0	0.0	0.0
Industrial - Heavy	55,000	L/gross ha/d		0.00	0.0	0.0	0.0	0.0	0.0
		Total I/CI Dem	nand	0.9	0.6	1.3	0.9	2.3	1.6
		Total Dem	nand _	39.7	27.6	191.7	133.1	289.8	201.3

Richcraft Group of Companies 590 Rideau Street FUS-Fire Flow Demand

Fire Flow Estimation per Fire Underwriters Survey

Water Supply For Public Fire Protection - 1999

DEL

Fire Flow Required

1. Base Requirement

 $F=220C\sqrt{A}$ L/min Where **F** is the fire flow, **C** is the Type of construction and **A** is the Total floor area

Type of Construction: Fire-Resistive Construction

C 0.6 Type of Construction Coefficient per FUS Part II, Section 1
 A 1233.3 m² Total floor area based on FUS Part II section 1

Fire Flow 4635.6 L/min

5000.0 L/min rounded to the nearest 1,000 L/min

Adjustments

2. Reduction for Occupancy Type

Limited Combustible -15%

Fire Flow 4250.0 L/min

3. Reduction for Sprinkler Protection

Sprinklered -50%

Reduction -2125 L/min

4. Increase for Separation Distance

 N
 20.1m-30m
 10%

 S
 3.1m-10m
 20%

 E
 0m-3m
 25%

 W
 20.1m-30m
 10%

% Increase 65% value not to exceed 75% per FUS Part II, Section 4

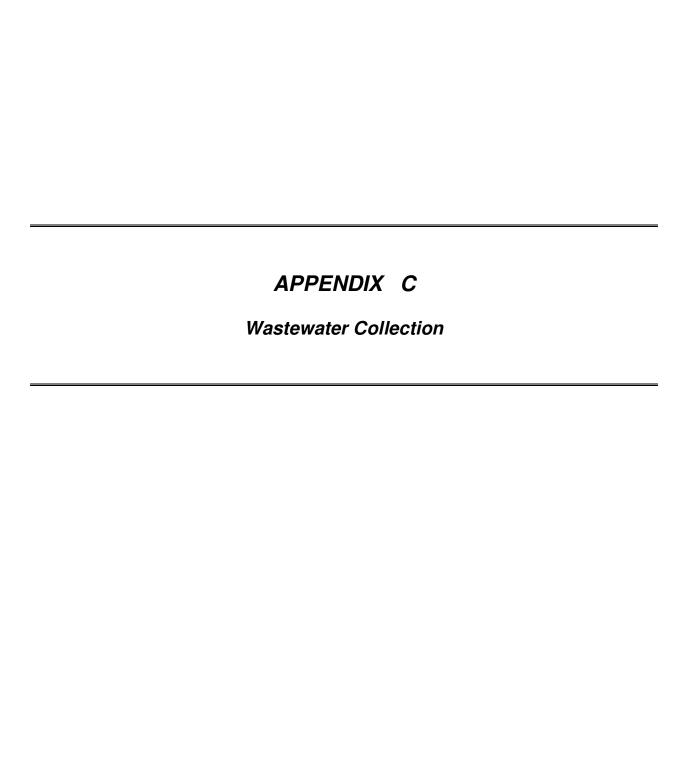
Increase 2762.5 L/min

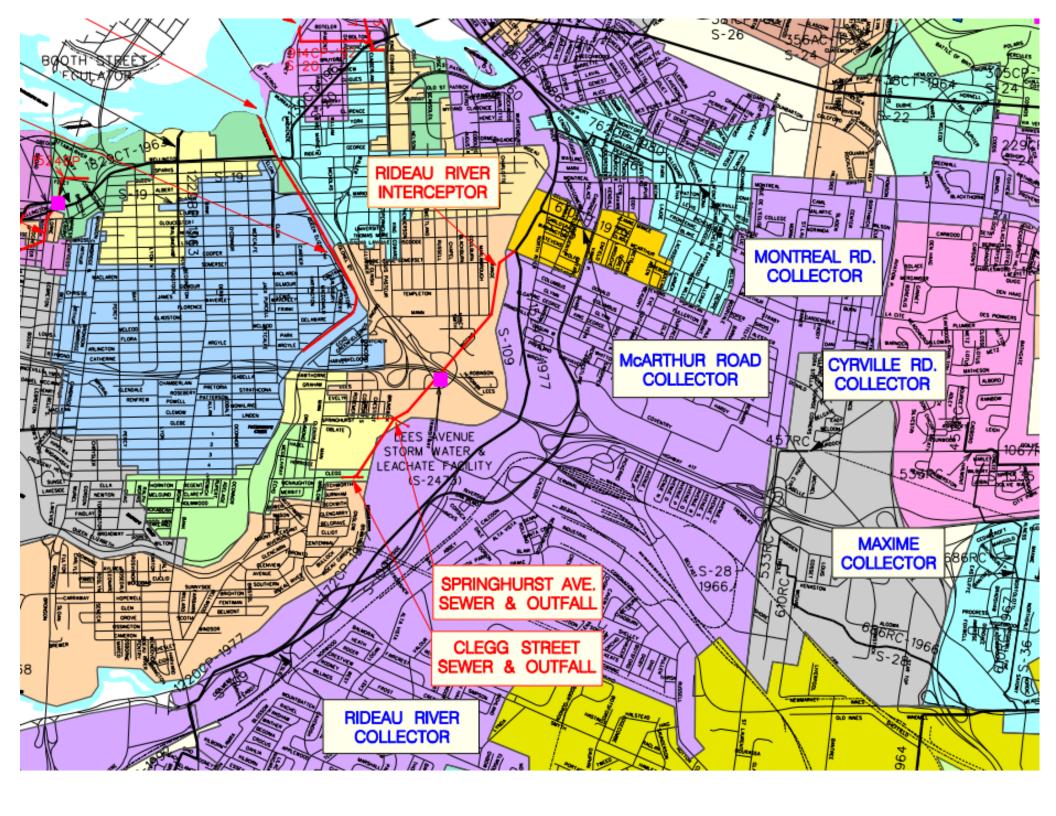
Total Fire Flow

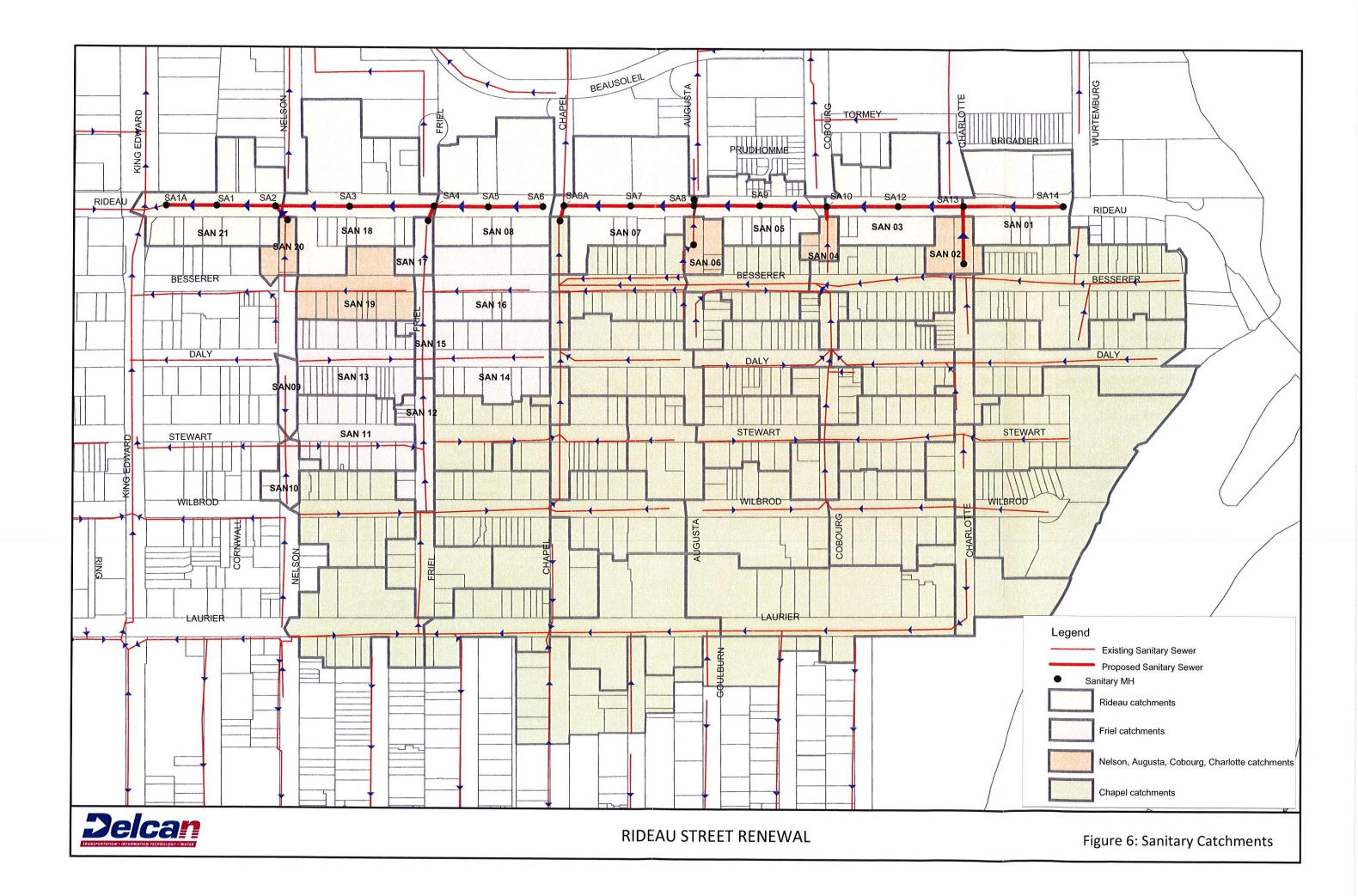
Fire Flow	4887.5 L/min	fire flow not to exceed 45,000 L/min nor be less than 2,000 L/min per FUS Section 4
	5000.0 L/min	rounded to the nearest 1,000 L/min

Notes:

- -Type of construction, Occupancy Type and Sprinkler Protection information provided by Graziani & Corazza Architects
- -Calculations based on Fire Underwriters Survey Part II









SANITARY SEWER DESIGN SHEET

Design Flow Rates (based on monitoring data)

Extraneous (as per City design guidelines)

Residential

Infiltration

Foundation

Commercial (COMM)

Institutional (INST)

Industrial (INDUS)

RIDEAU STREET - KING EDWARD AVENUE to WURTEMBURG STREET & CHARLOTTE STREET - RIDEAU STREET to BESSERER STREET

'K" correction factor (Residential)

ommercial/Institutional

Multi Unit Townhomes (MLT)

Peaking Factors

Single Family (SF)

Apartment (APT)

10,000 L/ha/day Residential Densities

 $\frac{\textbf{Formulas}}{Q(d)=Q(p)+Q(c)+Q(l)} \quad \text{(L/s)}$ Q(d) = Peak Design Flow (L/s)

Q(p) = Peak Population Flow (L/s) Q(c) = Commercial and Institutional Flow (L/s)

Q(I) = Peak Extraneous Flow (L/s)

Q(p)=PQM/86.4 (L/s)

P = Population Q= Average Daily Flow per Capita (Lpcd)

Q(I)=IA (L/s)

A = Area (ha)

I = Unit of Peak Extraneous flow (L/s/ha)

M=[1+(14/4+(P/1000)^0.5)]*K (Harmon formula) K = Correction Factor

M = Peak Factor

Mannings n = 0.013
Minimum Velocity (full) = 0.60 m/sec

300 Lpcd

17,000 L/ha/day

0.28 L/s/ha

3.00 L/s/ha

10,000 L/ha/day Type

	1					RES	SIDENTIAL	FLOW					INDUSTRI	AL/COMMERCIA	ALJINSTITUTIO	NAL (ICI) ARE	A FLOW				EXTR	ANEOUS FL	.ows		PEAK DESIGN				5	EWER DAT	Α				
STREET	FROM	то	AREA	UNIT	COUNTS		ACCUM	AVERAG	E PEAK	PEAK	сомм	INDUS	INST		ACCUMULATE	D	AVERAGE	PEAK	PEAK		ACCUM			PEAK	FLOW	TYPE	PIPE DI	AMETER	SLOPE	CAF	PACITY	VEI	LOCITY		
	STREET (MH)	STREET (MH)	ID	05 1		POP	POP	FLOW		1	AREA	AREA	AREA		INDUS AREA			FACTOR		AREA	AREA	INFILT.	FOUND.	FLOW	Q(d)	OF PIPE		nm) (act.)	(%)	Q (full)	Q(d) /Q(f) (%)	V (full) m/sec	actual m/sec		EMARKS
		-		SF /	API MLI	(persons	(persons)) L/s	М	L/s	ha	ha	ha	ha	ha	ha	L/s		L/s	ha	ha	L/s	L/s	L/s	L/s	PIPE	(nom.)	(act.)	 	L/s	(70)	Hilsec	HUSEC		
RIDEAU	WURTEMBURG (SA14)	CHARLOTTE (SA13)	SAN 01	0	115 0	207	207	0.7	1.6	1.2	0.31	0.00	0.00	0.31	0.00	0.00	0.1	1.50	0.1	1.07	1.07	0.3	3.2	3.5	4.8	PVC	300	305	0.70	84.4	5.63	1.16	0.53	4	
				- 1000			2000000	75.50		10000	300086							2201000					33355						1,108,000						
CHARLOTTE	CHARLOTTE S. (SA33)	RIDEAU (SA13)	SAN 02	0	10 0	18	18	0.1	1.6	0.1	0.15	0.00	0.00	0.15	0.00	0.00	0.0	1.50	0.0	0.30	0.30	0.1	0.9	1.0	1.1	PVC	250	254	1.00	62.0	1.82	1.22	0.45	NEW SEWER S	OUTH (Min Diameter)
RIDEAU	CHARLOTTE (SA13)	RIDEAU (SA12)	SAN 03	0 :	216 0	389	614	2.1	1.6	3.3	0.44	0.00	0.00	0.90	0.00	0.00	0.2	1.50	0.3	1.14	2.51	0.7	7.5	8.2	11.8	PVC	300	305	1.60	127.6	9.28	1.75	0.93		
RIDEAU	RIDEAU (SA12)	COBOURG (SA10)	all the				614	2.1	1.6	3.3	3 1 7 2			0.90	0.00	0.00	0.2	1.50	0.3		2.51	0.7	7.5	8.2	11.8	PVC	300	305	1.80	135.3	8.75	1.85	0.98	4	
	COBOURG South	RIDEAU (SA10)	SAN 04	0	0 1	3	3	0.0	1.6	0.0	0.03	0.00	0.00	0.03	0.00	0.00	0.0	1.50	0.0	0.15	0.15	0.0	0.5	0.5	0.5	PVC	250	254	2.56	99.3	0.52	1.96	0.63	CAPTURE EXIS	TING SEWER SOUT
RIDEAU	COBOURG (SA10)	RIDEAU (SA9)	SAN 05	0	6 8	32	649	2.3	1.6	3.5	0.39	0.00	0.00	1.32	0.00	0.00	0.3	1.50	0.4	0.77	3.43	1.0	10.3	11.3	15.2	PVC	300	305	0.44	70.1	21.64	0.92	0.61		
RIDEAU	RIDEAU (SA9)	AUGUSTA (SA8)			F		649	2.3	1.6	3.5	7 - 1 7	1 4 7	10.416.1	1.32	0.00	0.00	0.3	1.50	0.4		3.43	1.0	10.3	11.3	15.2	PVC	300	305	0.44	69.0	21.99	0.92	0.61		
																					,										1				
	AUGUSTA S. (SA38806) RIDEAU (SA8)	SAN 06	1	0 2	9	9	0.0	1.6	0.1	0.07	0.00	0.00	0.07	0.00	0.00	0.0	1.50	0.0	0.24	0.24	0.1	0.7	0.8	0.9	PVC	250	254	2.10	89.9	0.95	1.77	0.57	CAPTURE EXIST	TING SEWER SOUT
RIDEAU	AUGUSTA (SA8)	RIDEAU (SA7)	SAN 07	0	0 0	0	658	2.3	1.6	3.6	0.77	0.00	0.37	2.16	0.00	0.37	0.5	1.50	0.7	1.48	5.15	1.4	15.5	16.9	21.2	PVC	300	305	0.50	71.3	29.67	0.98	0.70	(t)	
RIDEAU	RIDEAU (SA7)	CHAPEL (SA6a)	11.1		7.7		658	2.3	1.6	3.6	9 9 7			2.16	0.00	0.37	0.5	1.50	0.7		5.15	1.4	15.5	16.9	21.2	PVC	300	305	0.50	71.3	29.67	0.98	0.70		MOST
																																$\overline{}$			
CHAPEL	CHAPEL South	RIDEAU (SA6a)	Chapel S	185 1	1361 587	4,664	4,664	16.2	1.3	21.2	1.05	0.00	1.06	1.05	0.00	1.06	0.3	1.50	0.5	33.59	33.59	9.4	100.8	110.2	131.9	CONC	750	762	1.96	1626.0	8.11	3.57	1.85		RESTRIC
	RIDEAU (SA6a)	CHAPEL North (Exist)					5,322	18.5	1.3	23.8				3.21	0.00	1.43	0.8	1.50	1.2		38.74	10.8	116.2	127.1	152.1	CONC	750	762	3.00	2011.6	7.56	4.41	2.29	Existing Outlet S	SECTION
																																			50.1 L/S
	:========	=========	‡====i	 	=====	=====	=====	=====	======	=====	=====:	=====:	=====:	======	======	 	=====	====	=====	====#	=====	=====	=====	=====	1======	=====	====			=====			=====		CAPACI
RIDEAU	CHAPEL (SA6)	RIDEAU (SA5)	SAN 08	0	370 0	666	666	2.3	1.6	3.6	0.71	0.00	0.00	0.71	0.00	0.00	0.1	1.50	0.2	1.49	1.49	0.4	4.5	4.9	8.7	PVC	300	305	1.50	123.6	7.05	1.69	0.85		CAI ACI
RIDEAU	RIDEAU (SA5)	FRIEL (SA4)					666	2.3	1.6	3.6	1000			0.71	0.00	0.00	0.1	1.50	0.2		1.49	0.4	4.5	4.9	8.7	PVC	300	305	3.00	174.7	4.99	2.39	1.10	71	
	FRIEL South	RIDEAU (SA4)	SAN 09	0	0 0	0	0				0.00	0.00	0.00	0.00	0.00	0.00				0.16	0.16			-					1			_			
	FRIEL South		SAN 10	0	0 14	38	38				0.00	0.00	0.00	0.00	0.00	0.00				0.23	0.39														
	FRIEL South		SAN 11	4	14 31	123	161				0.00	0.00	0.00	0.00	0.00	0.00				0.87	1.26											_			
	FRIEL South		SAN 12	1	0 5	17	178				0.04	0.00	0.00	0.04	0.00	0.00				0.40	1.66											-			
	FRIEL South		SAN 13	2	6 35	112	290				0.00	0.00	0.00	0.04	0.00	0.00				0.95	2.61														
	FRIEL South		SAN 14	0	109 17	242	532				0.00	0.00	0.00	0.04	0.00	0.00				0.98	3.59														
	FRIEL South		SAN 15	0	0 2	5	537				0.00	0.00	0.00	0.04	0.00	0.00				0.25	3.84										1				
	FRIEL South		SAN 16	0 :	226 3	415	952				0.00	0.00	0.00	0.04	0.00	0.00				0.95	4.79														
	FRIEL South (SA31)	RIDEAU (SA4)	SAN 17	0	0 0	0	952	3.3	1.5	5.0	0.03	0.00	0.00	0.07	0.00	0.00	0.0	1.50	0.0	0.18	4.97	1.4	14.9	16.3	21.4	PVC	300	305	3.20	180.5	11.84	2.47	1.41	CAPTURE EXIS	STING SEWER SOUT
RIDEAU	FRIEL (SA4)	RIDEAU (SA3)	SAN 18	0	10 0	18	1636	5.7	1.5	8.3	0.97	0.00	0.32	1.75	0.00	0.32	0.4	1.50	0.6	1.87	8.33	2.3	25.0	27.3	36.2	PVC	300	305	3.00	174.7	20.71	2.39	1.58		
RIDEAU	RIDEAU (SA3)	NELSON (SA2)					1636	5.7	1.5	8.3				1.75	0.00	0.32	0.4	1.50	0.6	30000	8.33	2.3	25.0	27.3	36.2	PVC	300	305	1.30	115.0	31.47	1.58			
					-																														
	NELSON South	RIDEAU (SA2)	SAN 19	4	46 27	169	169				0.00	0.00	0.00	0.00	0.00	0.00				0.73	0.73											\top			
	NELSON South (SA30)	RIDEAU (SA2)	SAN 20	0	0 9	24	193	0.7	1.6	1.1	0.00	0.00	0.00	0.00	0.00	0.00	0.0	1.50	0.0	0.19	0.92	0.3	2.8	3.0	4.1	PVC	300	305	5.80	243.0	1.68	3.33	1.23	CAPTURE EXIS	STING SEWER SOUT
RIDEAU	NELSON (SA2)	RIDEAU (SA1)	SAN 21	0	0 0	0	1829	6.4	1.4	9.2	0.83	0.00	0.00	2.58	0.00	0.32	0.5	1.50	0.8	1.14	10.39	2.9	31.2	34.1	44.1	PVC	300	305	0.65		54.20	1.11			
RIDEAU	RIDEAU (SA1)	K. EDWARD (Ex. SA1a)					1829	6.4	1.4	9.2				2.58	0.00	0.32	0.5	1.50	0.8		10.39	2.9	31.2	34.1	44.1	PVC	300	305	0.65	81.3	54.20	1.11		6	
	K. EDWARD (Ex. SA1a)	K. EDWARD (Ex. SA1)					1829	6.4	1.4	9.2				2.58	0.00	0.32	0.5	1.50	0.8		10.39	2.9	31.2	34.1	44.1	PVC	300	305	0.44	66.9	65.87	0.92		Existing Outlet S	Sewer

0.40

1.5

Person/Unit

3.4 2.7

1.8

(based on monitoring data)

TABLE 5

Richcraft Group of Companies 590 Rideau Road Proposed Conditions

0 0 0

Wastewater Design Flows per Unit Count City of Ottawa Sewer Design Guidelines, 2012



Site Area 0.137 ha

Extraneous Flow Allowances

Extraneous Flow Anowalices	Infiltration / Inflow	0.04 L/s
Damastia Cantributions		

Domestic Contributions			
Unit Type	Unit Rate	Units	Pop
Single Family	3.4		
Semi-detached and duplex	2.7		
Townhouse	2.7		
Stacked Townhouse	2.3		
Apartment			
Bachelor	1.4	10	1
1 Podroom	1 1	27	-

Stacked Townhouse	2.3		0
Apartment			
Bachelor	1.4	10	14
1 Bedroom	1.4	37	52
2 Bedroom	2.1	21	45
3 Bedroom	3.1		0
Average	1.8		0

Total Pop 111

Average Domestic Flow 0.45 L/s

Peaking Factor 4.00

Peak Domestic Flow 1.80 L/s

Institutional / Commercial / Industrial Contributions

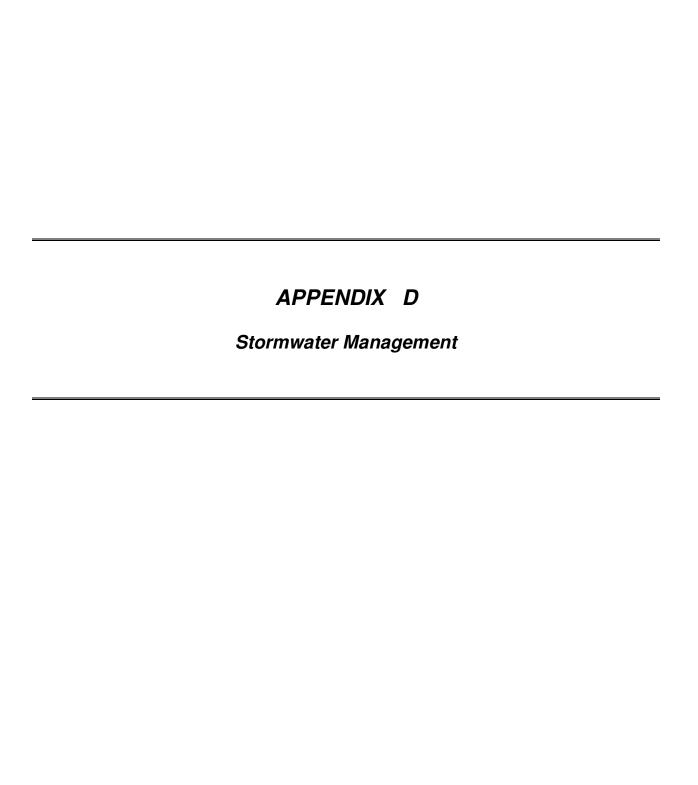
Property Type	Unit	Rate	No. of Units	Avg Wastewater (L/s)
Commercial floor space*	5	L/m ² /d	347	0.04
Hospitals	900	L/bed/d		0.00
School	70	L/student/d		0.00
Industrial - Light**	35,000	L/gross ha/d		0.00
Industrial - Heavy**	55,000	L/gross ha/d		0.00

Average I/C/I Flow	0.04
Peak Institutional / Commercial Flow	0.06
Peak Industrial Flow**	0.00
Peak I/C/I Flow	0.06

^{*} assuming a 12 hour commercial operation

^{**} peak industrial flow per City of Ottawa Sewer Design Guidelines Appendix 4B

Total Estimated Average Dry Weather Flow Rate	0.49 L/s
Total Estimated Peak Dry Weather Flow Rate	1.86 L/s
Total Estimated Peak Wet Weather Flow Rate	1.90 L/s



Richcraft Group of Companies 590 Rideau Street Existing Conditions

Estimated Peak Stormwater Flow Rate City of Ottawa Sewer Design Guidelines, 2012



Existing Drainage Charateristics From Internal Site

Area	0.1370 ha
С	0.40 Rational Method runoff coefficient
L	30 m
Up Elev	72.15 m
Dn Elev	71.48 m
Slope	2.2 %
Tc	10 min

1) Time of Concentration per Federal Aviation Administration

$$t_c = \frac{1.8(1.1 - C)L^{0.5}}{S^{0.333}}$$

tc, in minutes

C, rational method coefficient, (-)

L, length in ft

S, average watershed slope in %

Estimated Peak Flow

	2-year	5-year	100-year	
i	76.8	104.2	178.6	mm/hr
Q	11.7	15.9	34.0	L/s

Richcraft Group of Companies 590 Rideau Street Proposed Site Conditions

Stormwater - Proposed Development City of Ottawa Sewer Design Guidelines, 2012



Target Flow Rate

Area 0.137 ha

C 0.50 Rational Method runoff coefficient

t_c 10.0 min

5-year

i 104.2 mm/hr **Q** 19.8 L/s

Estimated Post Development Peak Flow from Unattenuated Areas

Total Area

0.02 ha

C 0.80 Rational Method runoff coefficient

	5-year					100-year				
t _c (min)	i (mm/hr)	Q _{actual} (L/s)	Q _{release} (L/s)	Q _{stored} (L/s)	V _{stored} (m ³)	i (mm/hr)	Q _{actual} (L/s)	Q _{release} (L/s)	Q _{stored} (L/s)	V _{stored} (m³)
(111111)	(11111111111111111111111111111111111111	(43)	(113)	(13)	() ,	(1111111111111111111111111111111111111	(113)	(113)	(43)	(111)
10.0	104.2	4.2	4.2	0.0	0.0	178.6	8.9	8.9	0.0	0.0

Estimated Post Development Peak Flow from Attenuated Areas

BLDG Area 0.093

C 0.9

A1 Area 0.027 C 0.85

Total Area 0.12 ha

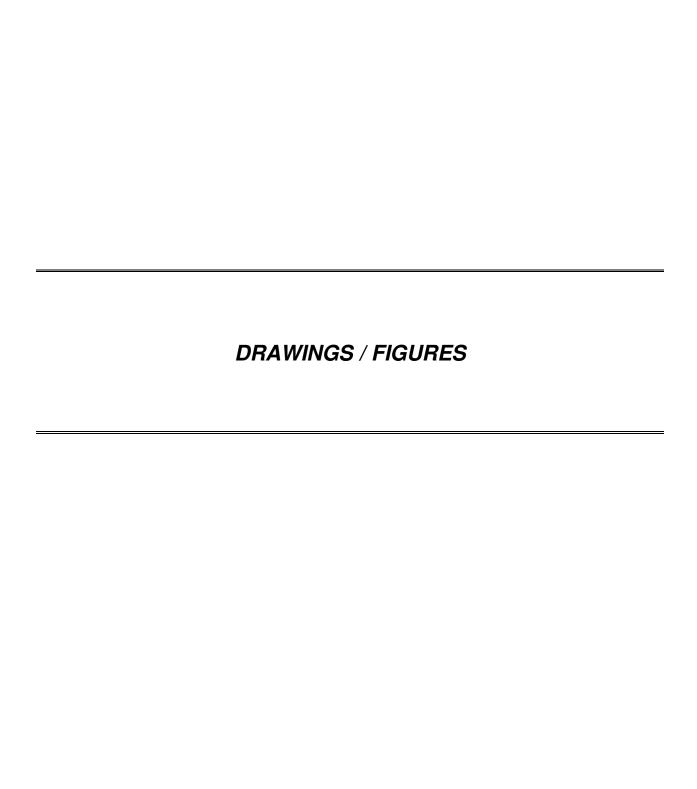
0.89 Rational Method runoff coefficient

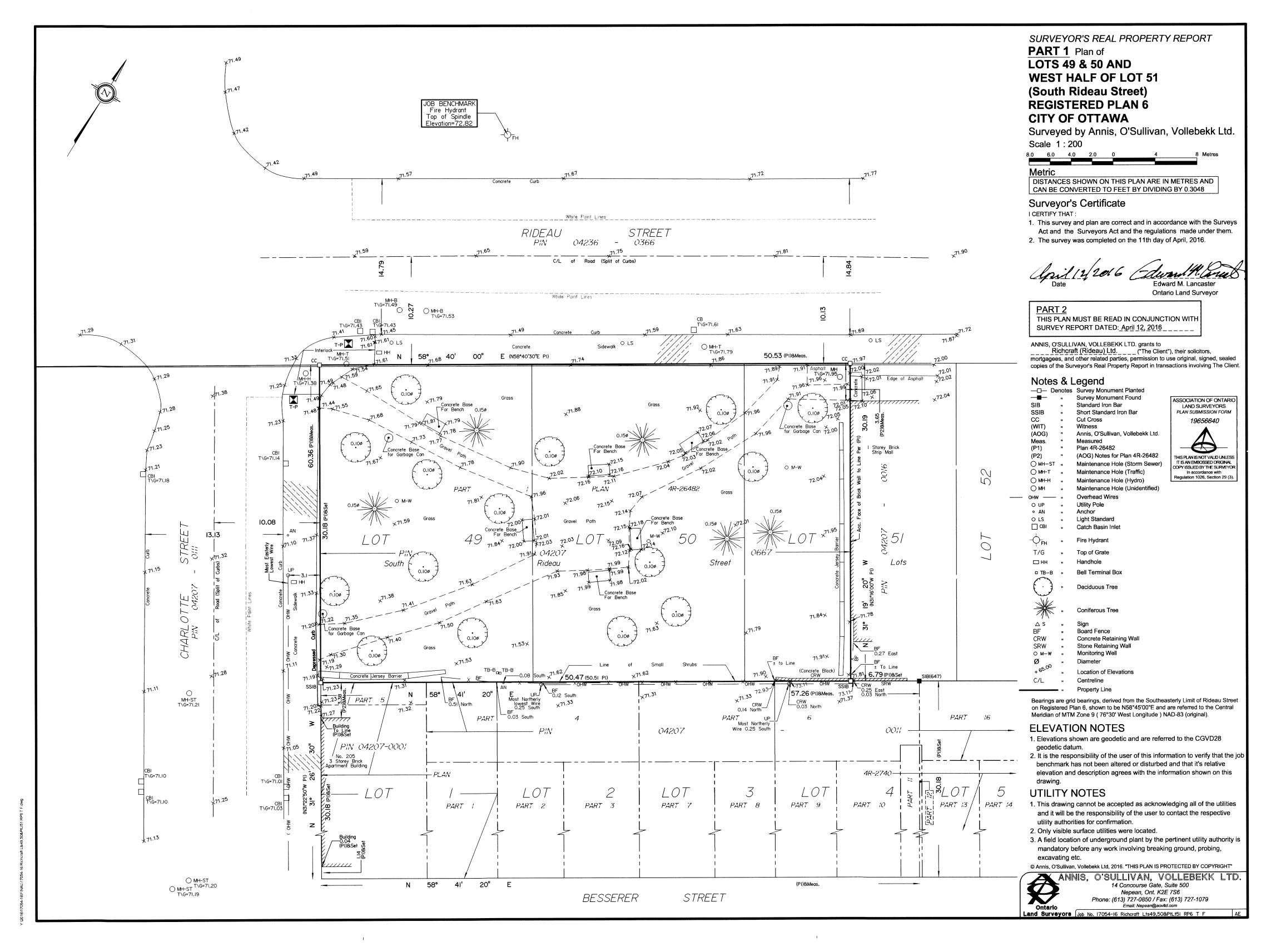
	5-year					100-year				
t _c	i	Q _{actual}	Q _{release}	Q _{stored}	V_{stored}	i	Q _{actual}	Q _{release}	Q _{stored}	V_{stored}
(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m³)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m³)
10	104.2	30.9	5.7	25.2	15.1	178.6	59.5	10.9	48.6	29.2
15	83.6	24.8	5.7	19.1	17.2	142.9	47.6	10.9	36.7	33.1
20	70.3	20.8	5.7	15.1	18.2	120.0	40.0	10.9	29.1	34.9
25	60.9	18.0	5.7	12.4	18.5	103.8	34.6	10.9	23.7	35.6
30	53.9	16.0	5.7	10.3	18.5	91.9	30.6	10.9	19.7	35.5
35	48.5	14.4	5.7	8.7	18.2	82.6	27.5	10.9	16.6	34.9
40	44.2	13.1	5.7	7.4	17.7	75.1	25.0	10.9	14.2	34.0
45	40.6	12.0	5.7	6.3	17.1	69.1	23.0	10.9	12.1	32.7
50	37.7	11.2	5.7	5.5	16.4	64.0	21.3	10.9	10.4	31.3
55	35.1	10.4	5.7	4.7	15.5	59.6	19.9	10.9	9.0	29.6
60	32.9	9.8	5.7	4.1	14.6	55.9	18.6	10.9	7.7	27.8
65	31.0	9.2	5.7	3.5	13.6	52.6	17.5	10.9	6.7	25.9
70	29.4	8.7	5.7	3.0	12.5	49.8	16.6	10.9	5.7	23.9
75	27.9	8.3	5.7	2.5	11.5	47.3	15.8	10.9	4.9	21.8
80	26.6	7.9	5.7	2.2	10.3	45.0	15.0	10.9	4.1	19.7
85	25.4	7.5	5.7	1.8	9.2	43.0	14.3	10.9	3.4	17.4
90	24.3	7.2	5.7	1.5	8.0	41.1	13.7	10.9	2.8	15.2
95	23.3	6.9	5.7	1.2	6.7	39.4	13.1	10.9	2.2	12.8
100	22.4	6.6	5.7	0.9	5.5	37.9	12.6	10.9	1.7	10.4
105	21.6	6.4	5.7	0.7	4.2	36.5	12.2	10.9	1.3	8.0
110	20.8	6.2	5.7	0.4	2.9	35.2	11.7	10.9	0.8	5.5

5-year Q_{attenuated} 5.73 L/s 100-year Q_{attenuated} 10.90 L/s 5-year Max. Storage Required 18.5 m³ 100-year Max. Storage Required 35.6 m³

Summary of Release Rates and Storage Volumes

Control Area	5-Year	5-Year Storage	100-Year Release Rate	100-Year Storage
	Release Rate (L/s)	Storage (m³)	Release Rate (L/s)	Storage (m³)
Unattenuated Areas	4.2	0.0	8.9	0.0
Attenutated Areas	5.7	18.5	10.9	35.6
Total	9.9	18.5	19.8	35.6



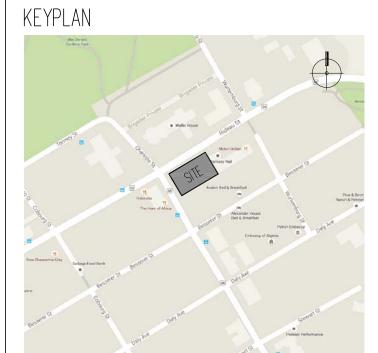




GENERAL NOTES

- 1. For landscaping, refer to landscape drawings.
- 2. For proposed grading, refer to landscape drawings.
- Land to be conveyed to the city free and clear of all encumbrnaces at a nominal cost for lane widening purposes at no expense to the city.

A201 UNDERGROUND PLANS 3. All perimeter existing information indicated taken from survey. A301 GROUND FLOOR PLAN A302 2ND – 7TH FLOORS PLANS 4. All work to be done in conformance with the 2012 Ontario Building Code. [O.B.C., as amended] A401 ELEVATIONS



SURVEY INFORMATION PLAN OF SURVEY OF LOTS 49, 50 AND THE WEST HALF OF LOT 51 (South Rideau Street) REGISTERED PLAN 6 CITY OF OTTAWA ANNIS, O'SULLIVAN, VOLLEBEKK LTD. ONTARIO LAND SURVEYOR SUITE 500 14 CONCOURSE GATE NEPEAN, ONTARIO

TEL (613) 727-0850 FAX (613) 727-1079

LIST OF DRAWINGS

A101 CONTEXT PLAN & STATISTICS A102 SITE PLAN

This drawing, as an instrument of service, is provided by and is the property of Graziani + Corazza Architects Inc. The contractor must verify and accept responsibility for all dimensions and conditions on site and must notify Graziani + Corazza Architects Inc. of any variations from the supplied information. Graziani + Corazza Architects Inc. is not responsible for the accuracy of survey, structural, mechanical, electrical, etc., engineering information shown on this drawing. Refer to the appropriate engineering drawings before proceeding with the work. Construction must conform to all applicable codes and requirements of the authorities having jurisdiction. Unless otherwise noted, no investigation has been undertaken or reported on by this office in regards to the environmental condition of this site.

This drawing is not to be used for construction purposes until countersigned by the

This drawing is not to be scaled. All architectural symbols indicated on this drawing are graphic representation's only.

01. XXX.XX.2016 ISSUED FOR SPA

STATISTICAL INFO	RMATION			
	REQUIRED	PROVIDED		
1. SITE AREA		± 1,525 m2 ± 16,413 ft2 ± 0.38 ha ± 0.15 ac		
2. G.F.A.		GROUND ± 377 m2 ± 4,058 ft2 2ND - 3RD ± 1,405 m2 ± 15,126 ft2 4TH ± 668 m2 ± 7,188 ft2 5TH - 6TH ± 1,336 m2 ± 14,377 ft2 7TH ± 520 m2 ± 5,595 ft2		
		TOTAL G.F.A. ± 4,306 m2 ± 46,344 ft2		
3. F.S.I.	MAXIMUM F.S.I. = 3	2.82		
4. BUILDING HEIGHT	MAXIMUM PERMITTED HEIGHT 22 m AND NO GREATER THAN 7 STOREYS	7 STOREYS 28.5 m 24.5 m + 4 m MECH. (FROM GROUND FLOOR TO TOP OF ROOF SLAB)		
5. UNIT COUNT		GROUND = 0 u 2ND - 3RD (12 u/fir x 2 firs) = 24 u 4TH = 12 u 5TH - 6TH (12 u/fir x 2 firs) = 24 u 7TH = 8 u		
		TOTAL UNITS 68 u		
6. UNIT BREAKDOWN		STUDIO = 10 u (15%) 1B = 14 u (20%) 1B+D = 23 u (34%) 2B = 19 u (28%) 2B+D = 2 u (3%)		
		TOTAL UNITS 68 u		
7. AMENITY	AS PER URBAN EXCEPTION 1697:	INDOOR OUTDOOR		
i.) INDOOR i.) OUTDOOR	A MINIMUM OF 18.5 m2 TOTAL AMENITY AREA MUST BE PROVIDED FOR EACH DWELLING UNIT, OF WHICH HALF MUST BE PROVIDED AS UNCOVERED OUTDOOR AMENITY AREA 9.25 x 68 = 629 m2 9.25 x 68 = 629 m2	GROUND ± 202 m2 GROUND ± 182 m2 2ND-3RD ± 191 m2 4TH ± 121 m2 5TH-6TH ± 165 m2 7TH ± 165 m2 SUBTOTAL ± 828 m2		
	TOTAL REQUIRED ± 1,258 m2	TOTAL PROVIDED ± 1,030 m2		
8. PARKING i.) RESIDENTS 0.5 SPACES/UNIT	= 0.5 x 68 u = 34 SPACES	P2 = 29 sp P1 = 5 sp		
	34 SPACES	34 SPACES		
ii.) VISITORS NONE FOR FIRST 12 UNITS AND 0.2 SPACES/UNIT FOR NEXT 300 UNITS	= 0.2 x 56 u = 11.2 = 11 SPACES	P1 = 11 sp		
	11 SPACES	11 SPACES		
iii.) RETAIL 2.5 SPACES/100 m2	= 2.5/100 x 347 m2 = 8.675 = 9 SPACES	P1 = 9 sp		
	9 SPACES	9 SPACES		
	TOTAL REQUIRED 54 SPACES	TOTAL PROVIDED 54 SPACES		
9. BIKE STORAGE i.) RESIDENTS 0.5 SPACES/UNIT	= 0.5 x 68 u = 34 SPACES	GROUND = 34 sp		
	34 SPACES	34 SPACES		
iii.) RETAIL 1 SPACES/250 m2	= 1/250 x 347 m2 = 1.39 = 1 SPACES	GROUND = 1 sp		
	1 SPACES	1 SPACES		
	TOTAL REQUIRED 35 SPACES	TOTAL PROVIDED 35 SPACES		
10. SETBACKS i.) NORTH FRONT YARD	2 m MINIMUM ABOVE 6 STOREYS 3 m MINIMUM ABOVE 6 STOREYS WHERE	2 m BELOW 4 STOREYS 4 m ABOVE 4 STOREYS 3 m		
i.) EAST INTERIOR SIDE YARD	THE MAX. BUILDING HEIGHT IS MORE THAN 16 m 7.5 m MINIMUM	7.5 m BELOW 6 STOREYS		
i.) EAST	THE MAX. BUILDING HEIGHT IS MORE THAN 16 m	7.5 m BELOW 6 STOREYS 10.5 m ABOVE 6 STOREYS		



PROPOSED MIXED USE DEVELOPMENT 590 Rideau

Group of Companies ONTARIO E. Corazza L. Wong L. Wong D. Biase Apr 01, 2016 Plot Date:

> CONTEXT PLAN & STATISTICS

1313.15Z



TITLEBLOCK SIZE: 610 x 950

