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Site Servicing & Stormwater Management Report

Building Expansion 64 Cleopatra Drive

City of Ottawa

Project No. 15031-1

Prepared for:

2336925 Ontario Inc. 64 Cleopatra Drive Ottawa, Ontario K2G 0B4

June 26, 2015

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1.0 INTRODUCTION

The subject site is located on the west side of Cleopatra Drive (#64), at the west end of Caesar Avenue in the City of Ottawa. The site currently has an existing two (2) storey industrial/office building and an asphalt parking lot. The existing building is to remain and shall be expanded with a proposed one (1) storey addition of approximately 3,820sq.ft. The existing asphalt parking lot (i.e. along the east and south sides of the existing building) will be reconfigured; therefore, increasing the landscaped area which in return reduces the imperviousness of the site. The north side of the existing building (i.e. gravel parking lot / storage area), will be removed to accommodate the new building addition. The overall site has an area of 0.28ha, however only 0.066ha is being redeveloped.

The existing building is serviced from a 10 inch (250mm) diameter sanitary sewer along Cleopatra Drive. As for water, the site is currently serviced by an on-site well. Approximately half the site drains overland to the existing hydro easement along the west side of the site, where as the other half of the site drains overland easterly ultimately draining to catchbasins along Cleopatra Drive.

A site investigation was undertaken to verify the existing site conditions and to establish the impact the new building expansion would have on the site. The City of Ottawa was contacted to verify existing civil infrastructure services along Cleopatra Drive, and information on the servicing requirements for this project were provided back in 2011.

2.0 WATER SERVICE

As mentioned above, the building is currently serviced by an on-site water well. The intent is to decommission the existing water well and connect to the existing 12 inch (300mm) diameter watermain along Cleopatra Drive. Using the MOE guideline of 35 cu.m/ha.d for light industrial use, the anticipated average daily demand for the site has been calculated at 9.8cu.m/day or 0.11L/s. Therefore, the anticipated peak hourly rate shall be in the magnitude of 0.45L/s, which is minimal. No fire sprinklers are anticipated at this time.

3.0 SANITARY SEWER SERVICE

As mentioned above, the site is currently serviced from a 10 inch (250mm) diameter sanitary sewer along Cleopatra Drive. Under City of Ottawa policy, secondary sanitary service connections to a property are not generally permitted. The intent is to provide a new sanitary service up to the Mechanical room of the existing building (decommissioning and/or removing the old service), and branching off a secondary line (on-site) towards the new building addition. The secondary line to the new building addition is intended to service the floor drains only, therefore no additional flows are expected.

4.0 DRAINAGE & STORM WATER SYSTEM

The stormwater management facility for this development has been designed to attenuate the release of stormwater runoff from the redeveloped area of the site to a rate not greater than the 5 year pre-development runoff rate of 9.5 l/s, (see section 4.1).

Due to the existing topography, a small section of the proposed redeveloped area (drainage area A-3) will drain uncontrolled to the west side of the site. As well, a small section of the proposed redeveloped area (drainage area A-2) will drain uncontrolled to the east towards Cleopatra Drive. Therefore, over controlling drainage area A-1 (proposed building and grassed area to the north) will be required.

This has been achieved by installing an inlet control device (vertical hydrovex valve) in the ditch inlet catchbasin and by providing the appropriate ponding volume within the swale/ditch system, (refer to the Removals, Site Servicing and Grading Plan (15031-GR1) contained in Appendix A).

4.1 5 YEAR PRE-DEVELOPMENT FLOW

 $Q = R \times A \times I \times N$

Redeveloped Site Area A = 0.066 hectares Runoff Coefficient R = 0.50 (gravel) Time of Concentration R = 0.50 (gravel) R = 0.50 (gravel) R = 0.50 (gravel) R = 0.50 (gravel)

5 year Pre-Dev. Flow: $Q = 0.50 \times 0.066 \times 104.19 \times 2.778$ Q = 9.5 l/s

4.2 100 YEAR POST-DEVELOPMENT FLOW (AREA A1)

 $Q = R \times A \times I \times N$

Redeveloped Site Area A = 0.053 hectares

Runoff Coefficient $R = (0.014 \times 0.20) + (0.039 \times 0.90)$

0.053

R = 0.72Time of Concentration Tc = 10 min

Rainfall Intensity (100yr) I = 178.56 mm/hr

100 year Post-Dev. Flow: $Q = 0.72 \times 0.053 \times 178.56 \times 2.778$

 $Q = 18.9 \, l/s$

4.3 100 YEAR POST-DEVELOPMENT FLOW (AREA A2)

 $Q = R \times A \times I \times N$

Redeveloped Site Area

A = 0.005 hectares

Runoff Coefficient

 $R = (0.003 \times 0.20) + (0.002 \times 0.90)$

0.005

R = 0.43

Time of Concentration

Tc = 10 min

Rainfall Intensity (100yr)

I = 178.56 mm/hr

100 year Post-Dev. Flow:

 $Q = 0.43 \times 0.005 \times 178.56 \times 2.778$

Q = 1.1 l/s

4.4 100 YEAR POST-DEVELOPMENT FLOW (AREA A3)

 $Q = R \times A \times I \times N$

Redeveloped Site Area

A = 0.008 hectares

Runoff Coefficient

R = 0.90 (asphalt)

Time of Concentration

Tc = 10 min

Rainfall Intensity (100yr)

I = 178.56 mm/hr

100 year Post-Dev. Flow:

 $Q = 0.90 \times 0.008 \times 178.56 \times 2.778$

 $Q = 3.6 \, l/s$

4.5 STORAGE REQUIREMENTS

As noted previously, the site has been designed to limit the rate of runoff (for the redeveloped portion of the site) to the 5 year pre-development release rate of 9.5 l/s for rainfall events up to and including the 100 year post-development event.

Over controlling Area A1 to 4.8 l/s [9.5 l/s (pre-dev.) - 1.1 l/s (Area A2) - 3.6 (area A3)] ensures the 5 year pre-development release rate of 9.5 l/s is achieved.

Storage volume requirements were determined by applying the 5-year and 100-year rainfall intensity values at 10-minute intervals until a peak storage volume was attained.

Return	Time	Intensity	Flow	Controlled	Net Runoff To	Storage Reg'd
Period	(min)	(mm/hr)	Q (L/s)	Release	Be Stored (L/s)	m3
	10	104.19	11.00	4.8	6.2	3.7
5 Year	20	70.25	7.42	4.8	2.6	3.1
11.1	30	53.93	5.69	4.8	0.9	1.6
	40	44.18	4.67	4.8	-0.1	-0.3
	50	37.65	3.98	4.8	-0.8	-2.5
	10	178.56	18.85	4.8	14.0	8.4
100 Year	20	119.95	12.66	4.8	7.9	9.4
	30	91.87	9.70	4.8	4.9	8.8
	40	75.15	7.93	4.8	3.1	7.5
	50	63.95	6.75	4.8	1.9	5.8

Therefore, the resulting 100-year release rate from the redeveloped portion of the site is less/equal to the allowable release rate of 9.5 l/s by providing 9.4 cu.m of storage within the swale/ditch system on the north side of the proposed building expansion.

5.0 CONCLUSION

- 1. The intent is to decommission the existing water well and connect to the existing 300mm diameter watermain along Cleopatra Drive. The anticipated peak hourly rate has been calculated at 0.45L/s.
- 2. No increase in sanitary flows is anticipated.
- 3. The redeveloped portion of the site has been designed to limit the rate of runoff to the 5 year pre-development release rate for rainfall events up to and including the 100 year post-development event.

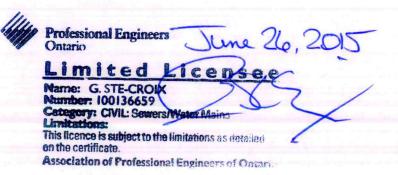
We trust that this report meets all of your requirements.

Should you have any questions or require further clarification, please do not hesitate to contact our office.

Sincerely,

Prepared by:

Ainley Graham and Associates Ltd.



Guy Ste-Croix, LEL, C.E.T., PMP Branch Manager

APPENDIX A

• Removals, Site Servicing and Grading Plan

• Storm Drainage Area Plan

(Dwg. 15031-GR1)

(Dwg. 15031-STM1)

