URBAN ECOSYSTEMS LIMITED

7050 WESTON ROAD, SUITE 705

WOODBRIDGE, ONTARIO L4L 8G7

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STORMWATER MANAGEMENT REPORT

RIVERSIDE SOUTH RETAIL CENTRE (BLDGS A TO K)

1420 EARL ARMSTRONG ROAD

CITY OF OTTAWA

FILE No: 12007.100

DATE: APRIL 9,2014

revised JULY 20, 2014 revised JULY 20, 2014 revised Jauary 20, 2016 DATE:

APRIL 9,2014 revised July 20,2014 revised Jauary 20, 2016 URBAN ECOSYSTEMS LIMITED 7050 WESTON ROAD, SUITE 705 WOODBRIDGE, ONTARIO L4L 8G7

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STORMWATER MANAGEMENT REPORT

RIVERSIDE SOUTH RETAIL CENTRE (BLDGS A TO K) 1420 EARL ARMSTRONG ROAD **CITY OF OTTAWA** 12007,100

FILE NO:

1.0 INTRODUCTION

The purpose of this report is to provide recommended grading and drainage prooposals with the objective to control storm runoff from the above proposed commercial development. The report provides an analysis of the overall site bounded by Earl Amstrong Road to the north, Limebank Road to the west, proposed Collector Road 'D' to the east and future Transit Road to the south. The property is located within in the Riverside South Community Phase 6, City of Ottawa. The Report also addresses Tributary No. 14, an external drainage area south of the subject property. Details are included in Appendix B to this Report.

In September 2008, Stantec prepared a report entitled, Riverside South Community Master Drainage Plan Update, Final Report. That study established the overall storm drainage strategy for the Riverside South Community and determined parameters for future developments within the community plan.

In January 2012, J.L. Richards & Associates Limited prepared a Design Report for Riversdie South Community Phase 6. That study provided further details and design parameters with respect storm drainage of future developments within the study area.

The Stantec and the J.L. Richards studies established maximum allowable runoff from development blocks within the Riverside South Community area, inlouding for the Subject Property. On site detention of excess runoff from the Subject Property will be required in order not to exceed the allowable site release rate.

The intent of this hydrologic evaluation is to outline the proposed stormwater management necessary to satisfy the site storage requirements produced by the occurance of the 100 year return frequency design storm. The maximum volume of storm runoff for the site was determined using the modified rational method MRM, as outlined in the American Public Works Association Publication title Practice in Detention of Urban Stormwater Runoff. Copies of the Proposed Site Plan, Site Grading Plan, Servicing Plan and the SWM Drainage Plan are included in the rear pockets of this Report. The rainfall intensities are derived from the City of Ottawa IDF curves.

2.0 ALLOWABLE SITE RUNOFF

The Master Dralnage Study by Stantec and the Design Report by J.L. Richards established that the maximum allowable post development storm runoff from the subject property shall not exceed 203 L/s/ha for all storms up to and including the 1:100 year event.

All excess runoff shall be detained on site through surface, roof and underground storage.

ALLOWABLE RELEASE RATE

Site Area =

6.54 ha. x

203 L/s/ha

1327 L/s

3.0 POST-DEVELOPMENT SITE CONDITION

	unit	Total	System A
Total Site Area	(m ²)	65367	65367
Pavement Area	(m ²)	48578	48578
Landscaped Area	(m ²)	484	484
Building Area	(m ²)	10367	10367
Uncontrolled Pavement Area	(m ²)	413	413
Uncontrolled Landscape Area	(m ²)	5525	5525

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4.0 EVALUATION OF SITE RUNOFF - SYSTEM A

4.1 Roof Top Storage

Proposed roofs to be equipped with control flow drains.

Model ID: Zurn Control Flo Z-105-5

Weir Rating 6 USGPM per inch head (0.15 L/s/cm head)

Quantity: One weir per hopper. Based on manufacturers table, one hopper drains

a maximum roof area of 465m² with a maximum head of 10.16 cm

For this building 33 weirs

Total roof outflow is calculated as:

$$Q_{roof}$$
 33 x 0.15 L/s/cm hd, x 10 cm head = 49.5 L/s

From Appendix - Table 1 maximum storage volumes:

required =
$$416.8 \text{ m}^3$$

available = 702.2 m^3

As shown, the available storage volume for the roof can easily contain the respective required maximum roof storage volumes.

Note: Peak rate of runoff, eg:

x 2.778

4.2 Parking Lot Storage and Release Rate

Note: 100 year runoff coefficients:

pavements - C_{100} = $C_5 \times 0.5 + 0.5 = 0.9 \times 0.5 + 0.5 = 0.95$

landscaped - C_{100} = 0.25 x 0.5 + 0.5 = 0.625

4.2.1 The composite runoff coefficients for the site, excluding building, are calculated as follows:

$$C_c = 48578 \times 0.95 + 484 \times 0.625$$
 $C_c = 0.95$

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4.2.2 Release rate calculations are based on orifice flow formula:

 $Q = C \times A \times (2gH)^{1/2}$

where,

Q = discharge in m³/s

C = shape coefficient, 0.62 for orifice plate, dimensionless

A = area of orifice in m²

g = acceleration due to gravity in m/s²

H = head from centre of orifice to ponding level in m

Orifice Plate at Existing Storm Manhole

max. ponding level	(m)	92.5
invert of orifice	(m)	88.15
head	(m)	4.125
diameter of orifice	(mm)	450
Q, orifice discharge	(l/s)	887.1

Using the Modified Rational Method, the maximum storage volume required on the parking lot was calculated. As shown in Appendix A, Table 2 and dwg 3 of 8,SWM drainage Plan, Urban Ecosystems Limited Project No. 12007.100 The required pond volume was calculated to b 906 m³

Available site storage:

Total site storage =

			Surface Pavement Storage=	1278.0	m³
12.5	m -	1050	dia. stm =	10.8	m ³
81	m -	900	dia. stm =	51.5	m^3
87.5	m -	750	dia. stm =	38.7	m^3
91	m -	675	dia. stm =	32.6	m^3
135	m -	600	dia. stm =	38.2	m^{s}
174	m -	525	dia. stm =	37.7	m^3
137	m -	450	dia. stm =	21.8	m^3
37.5	m -	375	dia. stm =	4.1	m^{s}
299.5	m -	300	dia. stm =	21.2	m^3
113.5	m -	250	dia. stm =	5.6	m^3
0	m -	200	dia. stm =	0.0	m^3
2		2400 mm dia mh(@	2 m avg depth) =	18.1	m^3
2		1800 mm dia mh(@	2 m avg depth) =	10.2	m^3
8		1500 mm dia mh(@	2 m avg depth) =	28.3	m^{s}
19		1200 mm dia mh(@	2 m avg depth) =	43.0	m^3
			Manhole / Pipe Storage=	361.6	m ³

Required Storage	m ³	906
Available Storage	m³	1640

1639.6

Therefore, there is sufficient storage in the parking lot to self contain the drainage and control the 100 year runoff to the allowable rate within the site.

m3

Note:P	eak runoff rate, Q =	RAIN	+ Qroof			
	0.95	X	4.9062	x I x 2.778 +		50
Note:						
Table 3	3 indicates that the	uncontrolle	ed runoff will to	tal	190.7	l/s
	(Landscape =	5525	m ² and pave	ment =	413	m^2)

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3.0 WATER QUALITY CONTROL

Storm runoff from the subject property will be directed to a proposed 1800 mm dia storm sewer to be constructed on Collector Road 'D'. This storm sewer connects to the existing storm sewers on Earl Armstrong Road and Limebank Road discharging to Riverside South Stormwater Management Pond No. 2, which provides for water quality controls. The Riverside South retail centre development is therefore not required to include onsite stormwater quality features.

7.0 SUMMARY

The following table summarizes the results presented in this report.

SYSTEM		100 YR STM	5 YR STM
orifice size	mm	450	450
total site release rate	L/s	1077.8	905.0
allowable site release rate	L/s	1327.0	1327.0
maximum ponding elevation	m	92.5	92.2
catchbasin elevation	m	92.2	92.2
ponding depth	m.	0.3	0
required storage	m ³	906	279
available storage	m ³	1640	362

Respectfully submitted,

Urban Ecosystems Limited

Rosario Sacco, P. Eng.

DATED

revised Jauary

BOLINCE OF ONTARIO

Page 5

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APPENDIX A

RIVERSIDE SOUTH RETAIL CENTRE (BLDGS A to K) CITY OF OTTAWA

12007.100

MUNICIPALITY:

FILE NO.: Date:

PROJECT:

revised Jauary 20, 2016
1420 EARL ARMSTRONG ROAD

LOCATION:

URBAN ECOSYSTEMS LIMITED WOODBRIDGE, CNTARIO L4L 8G7 7050 WESTON ROAD, SUITE 705

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SUMMARY

SITE STORM WATER MANAGEMENT

		_	П			
	65367	48578	484	10367	413	5525
Total	65367	48578	484	10367	413	5525
	Site area (sq.m):	Controlled Pavement area (sq.m) :	Controlled Landscaped area (sq.m):	BLDGs B,C,D,E,F,G,H,I,J,K Roof area (sq.m):	Uncontrolled Pavement area (sq.m.):	Uncontrolled Landscape area (sq.m.):
				BLDGs		

Includes Building A

	SYSTEM A	
CONTROLLED	Orifice release rate (I/sec) : Site release rate (I/sec) :	887.1 190.7
TOTAL	Site release rate (l/sec) :	1077.8
ALLOWABLE	Site release rate (I/sec) :	1327.0

LIMILED

SYSTEM A 100 YR STOKM RIVERSIDE SOUTH RETAIL CENTRE (BLDGS A to K)

moneilPALFITT OF CHAMA

PROJECT:

JOB NO.: DATE

SITE STORM WATER MANAGEMENT

1420 EARL ARMSTRONG ROAD revised Jauary 20, 2016 LOCATION:

SITE PLAN CHARACTERISTICS - S Y S T E M S . A

ainfall intensity (mm/hr): Controlled Pavement area (sq.m): 48578 Proposed Roof area (sq.m): 10367 Site area (sq.m): 65367 Controlled Landscaped area (sq.m): 484

Uncontrolled Pavement area (sq.m.): 413 Uncontrolled Landscaped area (sq.m.): 5525

Landscape coefficient: 0.625 Pavement coefficient: 0.95 Roof area coefficient: 0.95 732.951/(6.199+t)^.810 998.071/(6.053+t)^.814 1735.688/(6.014+t)^.820 1 100yr =

Total roof area (sq. m) Total number of roof hoppers: Total number of weirs

Max. sloped roof storage (cu.m): 175,55 Max. parapit roof storage (cu.m): 526.64

33 33 50.8 Max. sloped roof depth (mm):

33 hoppers @ 1 weir = hoppers @ 2 weir =

10.16 50.3

Weir area rating (sq. m.): 465

Weir rating (I/sec):

ROOF DRAINAGE CHARACTERISTICS

Maximum head (cm): Peak roof outflow rate (I/sec):

33 hoppers

TABLE 1 - ROOF DRAINAGE SYSTEM

Total

33 weir ဗ္ဗ ဝ

	702.2	Available roof storage (cu. m.):	ole roof stora	Availab				, DO	Peak roof outflow rate =	ufflow rate =	Peak roof outflow rate =		2 736 x (1'sec)	æ	Qroof=
	416.8	Required max. roof storage (cu. m.)	ax. roof stora	Required ma		•					•		•		
	368.80	290.59	7.53	429.14	230.24	29.52	5.96	91.56	175.55	267.10	392.28	659.38	64:34	30.30	000
	374.43	279.36	7.52	429.01	224.78	29.97	6.05	101.06	175.55	276.60	377.19	653.79	87.17	31.86	125
	379.81	268.19	7.52	429.01	218.98	30,41	6.14	110.34	175.55	285.89	362.10	647.99	90.00	32.89	120
	384.91	257.05	7.53	429.11	212.84	30.85	6.23	119.39	175.55	294.94	347.01	641.95	93.04	34.01	115
	389.73	245.93	7.53	429.30	206.36	31.27	6.32	128.19	175.55	303.73	331.93	635.66	96.31	35.20	110
	394.26	234.83	7.53	429.55	199.54	31.67	6.40	136.70	175.55	312.25	316.84	629.09	99.86	36,50	105
	398.49	223.72	7.53	429.82	192.39	32.06	6.48	144.91	175,55	320.45	301.75	622.21	103.70	37.90	9
	402.38	212.60	7.54	430.07	184.91	32.44	6.55	152.77	175.55	328.32	286.66	614.98	107.89	39.43	96
	405.91	201.47	7.54	430.27	177,11	32.80	6.63	160.25	175.55	335.80	271.58	607.38	112.48	41.11	6
	409.06	190.30	7.54	430.36	168.99	33,13	69.9	167.32	175.55	342.86	256,49	599,35	117.52	42.95	82
	411.76	179.09	7.54	430.29	160.56	33,45	92.9	173.90	175.55	349.45	241.40	590.85	123.09	44.99	80
	413,97	167.83	7,53	429.98	151.82	33.74	6.82	179.94	175.55	355.49	226.31	581.80	129.29	47.26	75
	415.62	156.51	7.53	429.35	142.79	34.00	6.87	185.36	175.55	360.91	211.23	572.13	136.22	49.79	02
	416.62	145.13	7.52	428.29	133.46	34.22	6.91	190.06	175.55	365,61	196.14	561.75	144.04	52.65	92
\ \ \	416.84	133,69	7.50	426.67	123.86	34.41	6.95	193.93	175.55	369.48	181.05	550.53	152.93	55.89	09
	416.14	122.18	7.48	424.33	113.99	34.54	96.9	196.81	175.55	372.36	165.96	538.32	163.13	59.65	22
	414.32	110,61	7.45	421.05	103.87	34.62	6.99	198.50	175.55	374.05	150.88	524.93	174.98	63.95	20
	411.12	98.97	7.40	416.56	93.52	34.64	7.00	198.74	175.55	374,29	135.79	510.08	188.92	69.05	45
	406.15	87.27	7.35	410.48	82,55	34.56	6.98	197.18	175.55	372.73	120.70	493.43	205.59	75.15	40
	398.92	75.54	7.27	402.27	72.19	34.38	6.94	193.29	175.55	368.84	105,61	474.46	225.93	82.58	35
	388.63	63.79	7.16	391.15	61.28	34.04	6.88	186.35	175.55	361.90	90.53	452.43	251.35	91.87	30
	374.11	52.07	7.01	375,91	50.27	33.51	6,77	175.20	175.55	350.74	75.44	426.18	284.12	103.85	22
	353.38	40.43	6.81	354.59	39.22	32.69	09:9	157.92	175.55	333.46	60.35	393,81	328 18	119.95	8
	322.86	17.95 28.99	6.51	323.59	28.26	31.40	6.34	131.05	175.55	306.59	45,26	351.86	390 95	142.89	<u>5</u>
	191.44	101	2.50	2 1 2 2	5.6	0.00	5 4	00.00	175.55	262.04	20.18	203 12	188 53	178 56	÷
	191 44	7.7.7	5.23	191.54	7.67	25.56	5.16	8.57	175.55	184.12	15.09	199.21	664 03	242.70	S
	volume (cu.m)	volume (cu.m)	hoppers (cm)	volume (cu.m)	volume (cu.m)	rate (I/sec)	hoppers (cm)	roof parapit (cu.m)	areas (cu.m)	volume (cu.m)	volume (cu.m)	volume (cu.m.)	(Jes/I)	(mm/hr)	(min.)
	Required storage	Roof outflow	Total head on roof	Required storage	Roof	Roof outflow	Total head on roof	Volume contained by	Volume in sloped roof	Required storage	Peak roof outflow	Peak Runoff	Peak rate of runoff	Rainfall Intensity	į
_		3rd ITERATION	9			2nd ITERATION	2nd					1st ITERATION	*		

head x weir rating x no. of hoppers

Roof outflow rate =

no. of hoppers x weir rating x max. head

2.736 x | (1.7 sec)

50.3 l/sec

4.95

= head x

50.3 x time x 60/1000 cu. m.

Peak roof outflow volume =

TE I MATTE D

100 YR STORM SYSTEM A

SITE STORM WATER MANAGEMENT

SITE CHARACTERISTICS

Controlled Pavement area (sq.m): 48578

Controlled Landscaped area (sq.m); 484

Total area - excl. Bldg (sq.m); 49062

Composite runoff coefficent; 0.95

TABLE 2 - System Storage

0.15904

Orifice diameter (mm): 450 Orifice coefficient: Area of orifice (sq.m):

OUTLET CHARACTERISTICS

Max. ponding elev.: 92.50 Catchbasin elev.: 92.20

	,
Required storage volume (cu.m.)	880.42 906.43 853.29 754.91
Orifice Outflow volume (cu.m)	532.25 798.38 1064.51 1330.64
Runoff volume (cu.m)	1412.68 1704.81 1917.80 2085.54
Peak rate of runoff Q (Vsec)	2354.46 1894.23 1598.16 1390.36
Intensity I (mm/hr)	178.56 142.89 119.95 103.85
Time (min.)	10 20 25
	•

Orifice center line elev. :: 88.375

Head (m): 4.125

Orifice release rate (l/sec): 887.1

Orifice invert: 88.15

Ponding depth. ; 0.30

906 1640 Required site storage (cu. m) : Available site storage (cu. m) : SEE DRAWING SP-1

50.3 l/sec Qsite= RAIN + Qroof 12.904

TABLE 3 - Uncontrolled Runoff

UNCONTROLLED SITE CHARACTERISTICS		Incontrolled Pavement area (sq.m.) : 413	controlled Landscaped area (sq.m.): 5525	Total area (sq.m): 5938	Composite runoff coefficent: 0.648	>			
Peak rate	of runoff	σ	(Nsec)			190.75	152.65	128.14	
	Intensity	_	(mm/hr)			178.56	142.89	119.95	
		Тіте	(min.)			9	15	20	

Peak runoff (L/sec): 190.7

100 YR STORM SYSTEM A SITE SUMMARY

190.7 1077.8 Orifice release rate (I/sec):

Uncontrolled release rate (I/sec):
Total site release rate (I/sec):

1327.0 Allowable site release rate (I/sec): TI MILE D

RIVERSIDE SOUTH RETAIL CENTRE (BLDGS A to K) PROJECT:

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revised Jauary 20, 2016 1420 EARL ARMSTRONG ROAD LOCATION:

JOB NO.: DATE

SITE STORM WATER MANAGEMENT

- SYSTEM A

5 YR STORM

ROOF DRAINAGE CHARACTERISTICS

Landscape coefficient: 0.25 Roof area coefficient: 0.95 Pavement coefficient: 0.9 (ainfall intensity (mm/hr): ⋖ SITE PLAN CHARACTERISTICS - S Y S T E M S 48578 Controlled Landscaped area (sq.m): 484 Proposed Roof area (sq.m): 10367 Site area (sq.m): 65367 Controlled Pavement area (sq.m):

998.071/(6.053+t)^.814 1735.688/(6.014+t)^.820 732.951/(6.199+t)^.810 | 2yr = | 5yr = | 100yr =

Uncontrolled Pavement area (sq.m.): 413 Uncontrolled Landscaped area (sq.m.): 5525

10367 33 33 50.8 Max. sloped roof depth (mm): Total roof area (sq. m): Total number of roof hoppers: Total number of weirs:

10.16 50.3

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465

Weir area rating (sq. m.): Maximum head (cm): Peak roof outflow rate (I/sec)

Weir rating (l/sec): 0.15

Max. sloped roof storage (cu.m): Max. parapit roof storage (cu.m):

175.55 526.64

33 hoppers @ 1 weir = 0 hoppers @ 2 weir =

33 hoppers Total

33 weir TABLE 1 - ROOF DRAINAGE SYSTEM

Required storage volume (cu.m)
100 79
140.87
160.48
174.48
175.05
173.14
169.43
64.34
58.18
151.15
143.42
135.10
126.29
117.04
107.43
97.49
87.26
76.78
66.08
55.17
44.07
32.80
21.39
9.83
-1.86
٦.

2.736 x l (l / sec) RAIN Qroof=

50.3 x time x 60/1000 cu. m. no. of hoppers x weir rating x max. head 50.3 l/sec Peak roof outflow volume = Peak roof outflow rate = 11

4.95 I/sec Roof outflow rate = head x weir rating x no. of hoppers = head x

224.2 702.2

Required max. roof storage (cu. m.) : Available roof storage (cu. m.) :

THI MALTE D

PROJECT:

RIVERSIDE SOUTH RETAIL CENTRE (BLDGS A to K)

5 YR STORM SITE STORM WATER MANAGEMENT **SYSTEM A**

SITE CHARACTERISTICS

Controlled Pavement area (sq.m): 48578
Controlled Landscaped area (sq.m): 484
Total area - excl. Bldg (sq.m): 49062
Composite runoff coefficent: 0.89

OUTLET CHARACTERISTICS

0.15904 92.20 Orifice diameter (mm): Area of orifice (sq.m): Orifice coefficient:

92.20 Orifice invert: 88.15 0.00 Max. ponding elev.: Catchbasin elev.: Ponding depth.:

88.375 Orifice center line elev.:

3.825 Head (m):

Orifice release rate (I/sec): 854.2

TABLE 2 - System Storage

Time (min.)	Intensity I (mm/hr)	Peak rate of runoff Q (I/sec)	Runoff volume (cu.m)	Orifice Outflow volume (cu.m)	Required storage volume (cu.m.)	
10 15 20 25	104.19 83.56 70.25 60.90	1319.27 1067.94 905.89 791.95	791.56 961.15 1087.06 1187.92	512.53 768.80 1025.07 1281.34	279.03 192.35 61.99 -93.41	ļ
		Rec	Required site storage (cu. m) : Available site storage (cu. m) : SEE DRAWING SP-1	site storage (cu. m) : site storage (cu. m) : SEE DRAWING SP-1	279 362	
Osite= =		roof ×	50.3 l/sec			

NO SURFACE PONDING

TABLE 3 - Uncontrolled Runoff

Incontrolled Pavement area (sq.m.): 413 controlled Landscaped area (sq.m.): 5525 Total area (sq.m); 5938 Composite runoff coefficent; 0.295 SITE CHARACTERISTICS UNCONTROLLED of runoff Peak rate (ces/I) 50.74 40.69 34.21 ø Intensity (mm/hr) 104.19 83.56 70.25 (min.) Time 2 12 2

50.7 Peak runoff (L/sec):

5 YR STORM SYSTEM A SITE SUMMARY

854.2 Orifice release rate (I/sec): Uncontrolled release rate (I/sec): Total site release rate (I/sec):

50.7 905.0 1327.0 Allowable site release rate (I/sec):

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APPENDIX B



Tributary No. 14

Approximately 68.38 ha of upstream lands to the south, are currently draining through the Subject Property via Tributary No. 14. Ultimately, the storm runoff from this area will be controlled as established through the Riverside South Community Master Drainage Area Plan. The storm drainage will be collected in local storm sewers and conveyed to the sewers on Limebank Road, ultimately discharging to Riverside South Stormwater Management Pond No. 2.

The peak flows from the upstream 68.38 ha of undeveloped lands, based on pasture lands and an estimated time to peak of 1.73 hours, were calculated to be 1.719 m ³/s. It is noted that this flow is significantly higher than what was reported in the Riverside South Community Master Drainage Plan, primarily due to a shorter time to peak. An External Storm Drainage Area Plan, Drawing 8 of 8, is included in the rear pocket.

In the interim, it is proposed that a temporary interceptor swale will be constructed (by others), immediately south of future Town Square Boulevard. The swale will convey all storm flows from the undeveloped upstream lands, discharging to the proposed storm sewers on Ceremonial Road.

The drainage from the Town Square Boulevard right of way, will be intercepted by a temporary swale located immediately south of the Subject Property. The swale will flow westerly, discharging to a temporary inlet catchbaisn to be located on the east side of Limebank Road and connected to the Limebank Road storm sewer systems.

Rideau Valley Conservation Authority has confirmed that Tributary no. 14 is approved in principle to be enclosed. Prior to commencing any construction on this Subject Property, including grading or any site alteration works, Morguard Investments Limited will file an application under Ontario Regulation 174/06 Section 28 with Rideau Valley Conservation Authority, for a Permit to enclose/alter Tributary No. 14.

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                                                  # 2637819
     StormWater Management HYdrologic Model
                                        999
                                             999
                                                  _____
*********************
******* A single event and continuous hydrologic simulation model *******
******** based on the principles of HYMO and its successors *******
****** Distributed by:
                   J.F. Sabourin and Associates Inc.
Ottawa, Ontario: (613) 836-3884
Gatineau, Quebec: (819) 243-6858
E-Mail: swmhymo@jfsa.Com
******
******
**********************
+++++++ Licensed user: The Sernas Group
                  whitby
                                  SERIAL#:2637819
                                                  ++++++++
**********************
******
              +++++ PROGRAM ARRAY DIMENSIONS ++++++
******
              Maximum value for ID numbers :
                                        10
                                                  ******
******
              Max. number of rainfall points: 105408
***** DESCRIPTION SUMMARY TABLE HEADERS (units depend on METOUT in START) *****
      ID: Hydrograph IDentification numbers, (1-10).
HYD: Hydrograph reference numbers, (6 digits or characters).
REA: Drainage area associated with hydrograph, (ac.) or (ha.).
REAK: Peak flow of simulated hydrograph, (ft^3/s) or (m^3/s).
to to to to to to
****
     NHYD:
****
                                                     ****
***** QPEAK:
***** TpeakDate_hh:mm is the date and time of the peak flow.
     R.V.: Runoff Volume of simulated hydrograph, (in) or (mm).
R.C.: Runoff Coefficient of simulated hydrograph, (ratio).
*************************
****************************
DATE: 2014-06-10 TIME: 15:29:25
                                  RUN COUNTER: 000270
***********************
* Input filename: C:\DDRIVE~1\PreOtt.dat
 Output filename: C:\DDRIVE~1\PreOtt.out
                                                        4
 Summary filename: C:\DDRIVE~1\PreOtt.sum
                                                        *
 User comments:
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Pre0tt
 *****************
<u>#**********************</u>
  Project Name: [Riverside Ottawa]
                             Project Number: [8811895.400]
           : 07-22-2004
#
  Date
  Modeller
           : [Ken Chow]
  Company
            GHD
           : 2640114
  License #
#********************
 ** END OF RUN :
               1
********************
 RUN: COMMAND#
002:0001----
   START
             .00 hrs on
     TZERO =
                          0]
                (1=imperial, 2=metric output)]
     METOUT=
            2
     NSTORM=
    NRUN
#****************
                            Project Number: [8811895.400]
  Project Name: [Riverside Ottawa]
          : 07-22-2004
  Modeller
           : [Ken Chow]
           : GHD
  Company
  License #
           : 2640114
#***************
   MASS STORM
    Filename = C:\D DRIVE\24SCSII.mst
    Comment = 24 hour SCS II storm mass curve
    [SDT= 2.00:SDUR= 24.00:PTOT= 103.20]
002:0003-----ID:NHYD------AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.
   DESIGN NASHYD
                 01:200
                              63.30
                                     2.056 No_date
                                                 13:22
                                                       51.59
.500
    [CN = 72.0: N = 3.00]
    [Tp= 1.37:DT= 2.00]
002:0004-----ID:NHYD------AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.
                 01:200
                              63.30
                                     2.056 No_date
   PRINT HYD
                                                 13:22
                                                      51.59
n/a
002:0005-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.
   DESIGN NASHYD
                 01:200
                              63.30
                                     1.719 No_date
                                                 13:48
                                                      51.59
.500
    [CN= 72.0: N= 3.00]
[Tp- 1.73:DT- 2.00]
002:0006-----ID:NHYD------AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.
```

			Preutt			
n/a	PRINT HYD	01:200	63.30	1.719 No_date	13:48	51.59
002:	0007					
	FINISH					
 ****	****	****	****	****	*****	****
**						
	WARNINGS / ERR	ORS / NOTES				
S	imulation ended	on 2014-06-10	at 15:29:2	5		
====						

```
Metric units
*#**************
*#
   Project Name: [Riverside Ottawa]
                               Project Number: [8811895.400]
*#
            : 07-22-2004
*#
            : [Ken Chow]
   Modeller
*#
   Company
            : GHD
   License # : 2640114
*#
*#************************
START
* SCS 24 hours distribution
* Parameters taken from IDF curve parameters provided by City of Ottawa
* Sewer Guidelines October 2012
                           ----------
*100 year event
                PTOTAL=[103.2](mm), CSDT=[2](min),
CURVE_FILENAME=["C:\D DRIVE\24SCSII.mst"]
MASS STORM
*********
* EXTERNAL AREAS based on Row Crops and a Tp of 1.37
                DESIGN NASHYD
PRINT HYD
                      # OF PCYCLES=[-1]
                ID=[1],
**********
* EXTERNAL AREAS based on Pasture and a Tp of 1.73
                ID=[1], NHYD=["200"], DT=[2]min, AREA=[63.3](ha),
DWF=[0](cms), CN/C=[72], TP=[1.73]hrs,
RAINFALL=[ , , , , ](mm/hr), END=-1
DESIGN NASHYD
PRINT HYD
                ID=[1], # OF PCYCLES=[-1]
FINISH
```

Pre0tt

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                                       9
                                          # 2637819
                                  999
                                      999
     StormWater Management HYdrologic Model
****************
******* SWMHYMO Ver/4.05
                            ******
       A single event and continuous hydrologic simulation model
******
         based on the principles of HYMO and its successors
*****
****** Distributed by:
                J.F. Sabourin and Associates Inc.
                Ottawa, Ontario: (613) 836-3884
Gatineau, Quebec: (819) 243-6858
*****
                E-Mail: swmhymo@jfsa.Com
*****
*******************
+++++++ Licensed user: The Sernas Group
+++++++
               whitby
                            SERIAL#:2637819
                                          ++++++++
****************
******
            +++++ PROGRAM ARRAY DIMENSIONS ++++++
*****
            Maximum value for ID numbers :
                                 10
                                          ******
*****
            Max. number of rainfall points: 105408
                                          *****
******
            Max. number of flow points
                              : 105408
*****************
********
               DETAILED
                          OUTPUT
                                  ********
*********************
      DATE: 2014-06-10
                  TIME: 15:29:25
                              RUN COUNTER: 000270
**********************
      filename: C:\DDRIVE~1\PreOtt.dat
 Output filename: C:\DDRIVE~1\PreOtt.out
 Summary filename: C:\DDRIVE~1\PreOtt.sum
 User comments:
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 2:
****************
001:0001-----
*#
  Project Name: [Riverside Ottawa]
                       Project Number: [8811895.400]
×#
          07-22-2004
  Date
*#
  Modeller
          [Ken Chow]
*#
  Company
          GHD
  License #
         : 2640114
*#********************
 ** END OF RUN :
***********
```

```
| Project dir.: C:\DDRIVE~1\
----- Rainfall dir.: C:\DDRIVE~1\
            .00 hrs on 0
2 (output = METRIC)
   METOUT=
   NRUN = 002
   NSTORM=
             1====
            2=ibution
002:0002----
*#***************************
*# Project Name: [Riverside Ottawa] Project Number: [8811895.400]
*# Date
         : 07-22-2004
              : [Ken Chow]
*#
   Modeller
*#
   Company : GHD
License # : 2640114
*#**********************
002:0002----
* Parameters taken from IDF curve parameters provided by City of Ottawa
* Sewer Guidelines October 2012
*100 year event
I MASS STORM I
                     Filename: C:\D DRIVE\24SCSII.mst
| Ptotal=103.20 mm |
                     Comments: 24 hour SCS II storm mass curve
                     Duration of storm
                                                24.00 hrs
                     Mass curve time step
                                                12.00 min
                                         =
                     Selected storm time step =
                                                 2.00 min
                     Volume of derived storm = 103.20 mm
            TIME
                    RAIN
                            TIME
                                   RAIN |
                                           TIME
                                                   RAIN
                                                           TIME
                                                                  RAIN
                   mm/hr
                                  mm/hr
             hrs
                            hrs
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                                  2.064
                                           12.03
                                                 20.640
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                            6.03
                                                          18.03
                                                                 1.548
                                           12.07
             .07
                   1.032
                            6.07
                                  2.064
                                                 20.640
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                   1.032
                            6.10
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                                                 20.640
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Page 3

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8.73 8.77 8.80 8.83 8.87 8.90 8.93 8.97 9.00 9.03 9.07 9.13 9.27 9.23 9.27 9.23 9.27 9.33 9.40 9.43 9.47 9.53 9.63 9.77 9.80 9.97 9.97 9.98 9.97 10.00 10.13 10.17 10.23 10.27 10.33 10.40 10.43 10.47 10.50 10.63 10.77 10.80
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14.73 14.77 14.80 14.83 14.90 14.97 15.03 15.07 15.13 15.23 15.37 15.33 15.37 15.43 15.53 15.53 15.63 15.73 15.63 15.73 15.73 15.83 15.73 15.83 15.73 15.83 15.93 16.03 16.13 16.23 16.33 16.33 16.33 16.43 16.43 16.53 16.53 16.63 16.73 16.80
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20.73 20.77 20.80 20.83 20.97 21.00 21.03 21.07 21.13 21.17 21.20 21.33 21.37 21.40 21.43 21.47 21.50 21.53 21.77 21.63 21.77 21.63 21.77 21.80 21.73 21.77 21.80 21.97 22.00 22.13 22.17 22.20 22.33 22.17 22.20 22.33 22.40 22.43 22.47 22.50 22.53 22.77 22.80
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11.90 116.100 | 17.90

11.93 116.100 | 17.93

11.97 116.100 | 17.97

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___ 002:0003-----

```
* EXTERNAL AREAS based on Row Crops and a Tp of 1.37
```

*

Unit Hyd Qpeak (cms)= 1.765

```
PEAK FLOW (cms)= 2.056 (i)
TIME TO PEAK (hrs)= 13.367
RUNOFF VOLUME (mm)= 51.591
TOTAL RAINFALL (mm)= 103.200
RUNOFF COEFFICIENT = .500
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0004-----

```
ID=01 (200
 PRINT HYD
                 AREA
                          (ha)=
                                63.300
                         (cms) =
                 QPEAK
                                2.056 (i)
DT= 2.00 PCYC=-1
                 TPEAK
                         (hrs)=
                                13.367
                                51.591
                 VOLUME
                          (mm) =
   (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
*******
* EXTERNAL AREAS based on Pasture and a Tp of 1.73
| DESIGN NASHYD | 01:200 DT= 2.00 |
| DESIGN NASHYD
                   Area
                         (ha)=
                               63.30
                                     Curve Number (CN)=72.00
                              1.500
                         (mm) =
                                     # of Linear Res.(N)= 3.00
                  Ia
                  U.H. Tp(hrs)=
                               1.730
    Unit Hyd Qpeak (cms)=
                       1.398
    PEAK FLOW
TIME TO PEAK
                (cms) =
                       1.719 (i)
                       13.800
                (hrs)=
    RUNOFF VOLUME
                 (mm) =
                      51.591
                (mm) = 103.200
    TOTAL RAINFALL
    RUNOFF COEFFICIENT
    (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
002:0006-----
de:
| PRINT HYD | | ID=01 (200 ) |
                AREA
                         (ha) = 63.300
                         (cms)=
                QPEAK
                                1.719 (i)
DT= 2.00 PCYC=-1
                                13.800
                 TPEAK
                         (hrs)=
                          (mm)=
                 VOLUME
                                51.591
    (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
002:0007-----
    FINISH
**********************
   WARNINGS / ERRORS / NOTES
  Simulation ended on 2014-06-10
                          at 15:29:25
```









