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MEMORANDUM

DATE: 2015-12-11 <u>EMAIL</u>

TO: Ryan Hicks, B.E.D.S., LEED BD+C

Lic. Tech. OAA srm Architects Inc.

SUBJECT: Functional Servicing and Stormwater Management Brief in

support of Site Plan Amendment for 774 Bronson Avenue

OUR FILE: DSEL Project No. 15-807

ATTACHMENTS:

- Previously approved Site Plan prepared by Marco Manini February 27, 2013
- Proposed Site Plan prepared by SRM Architects Inc., dated December 10, 2015
- Reduced Copy of approved Site Servicing Plan by DSEL, dated January 2014
- Previously approved Water Demand Calculation Sheet by DSEL, dated February 2013
- Water Demand Calculation Sheet by DSEL, Dated December 2015
- Updated Boundary Conditions from City of Ottawa, Dated November 2015
- Previously approved Wastewater Discharge Calculation Sheet by DSEL, dated June 2012
- Wastewater Discharge Calculation Sheet by DSEL, Dated December 2015
- Previously approved Stormwater Management Plan (SWM-1) prepared by DSEL, dated February 2013
- Previously approved Stormwater Management Calculation sheet, dated February 2013
- Stormwater Management Plan (SWM-1) prepared by DSEL, December 2015
- Stormwater Management Calculation Sheet by DSEL, Dated December 2015
- Ipex Tempest LMF Flow Curve, provided by Ipex
- Summary of Triton U/G Storage calculation, dated December 2015

DSEL has been retained by SRM Architects Inc. to provide a servicing memo in support of the Site Plan Amendment of a proposed development at 774 Bronson Avenue. DSEL had previously prepared a Functional Servicing and Stormwater Management Report prepared for the Site Plan Application (SPA) for 774 Bronson Avenue and 551 Cambridge Street, approved by the City of Ottawa in February 2013. Since the February 2013 approval, the subject property has been combined into a single parcel, 774 Bronson Avenue. The new proposed plan, dated December 2015, including a 12-storey student residence. See *Appendix* for proposed plan prepared by SRM Architects Inc.

Site Plan Approval (SPA) was obtained for the subject site based on the Functional Servicing Report (FSR) & Site Servicing Plan (SSP) prepared by DSEL, dated February 2013 & October 2013, respectively. A reduced copy of the approved SSP can be found in *Appendix*.

The approved AES and FSR both show that the previously proposed development was supported by existing water, sanitary and stormwater services. The following serviceability study will confirm that the updated concept plan will continue to be sufficiently supported by existing services.

The approved FSR proposed **193** residential units and **804m**² of commercial floorspace. The new application contemplates **181** student residence units and **136m**² of commercial/amenity space.

1.0 Water Servicing

Water servicing is proposed to follow the approved FSR and SSP. As the contemplated development has a water demand greater than 50m³/day a redundant water connection is required as per the *City of Ottawa Water Design Guidelines* (2010). Water servicing will continue to be achieved as per the approved SSP with a dual connection to the existing 200mm diameter watermain within Cambridge Street. *Table 1* summarizes the anticipated water demand for the proposed development. See *Appendix* for detailed calculations of water demand based on the December 2015 concept plan.

| Design Parameter | Anticipated Demand (L/min) | Bronson | Conditions ² Avenue () / kPa) | | | | |
|--|--|---------|--|--|--|--|--|
| Average Daily Demand | 48.5 | 117.1 | 429.3 | | | | |
| Max Day + Fire Flow | 145.0 + 14,000 = 14,145.0 7500 L/min @ 140 kPa | | | | | | |
| Peak Hour | 217.6 | 106.1 | 321.4 | | | | |
| Water demand calculation per <i>Water Supply Guidelines</i> . | | | | | | | |
| 2) Water demand and boundary conditions from City of Ottawa, received October, 2015. | | | | | | | |

Table 1: Water Demand and Boundary Conditions

Fire demand is determined based on the FUS method in accordance with the City of Ottawa Guidelines. The FUS calculation resulted in approximately **14,000 L/min** of water demand required as shown in the attached calculation sheet. From *Table 1*, the municipal system can provide a maximum fire flow of **7500L/min**. Fire flow for the proposed building will be confirmed by a fire suppression system specialist to ensure adequate fire protection is available.

It is our understanding that the city is undertaking off-site watermain improvements that may improve the service to the area.

2.0 Sanitary Servicing

The existing approved FSR proposed sanitary sewer connections to Cambridge and Bronson Avenue. It is proposed to discharge sanitary flow to the existing 250mm diameter combined sewer within Cambridge Street.

Table 2 below summarizes the design guidelines for wastewater sewer systems required by the City of Ottawa.

Design Parameter Value Commercial Floor Space 5 L/m²/d Residential Average Apartment Demand 1.8 person/unit Residential Daily Average 350 L/person/d **Peaking Factor** Harmon's Peaking Factor. Max 4.0, Min 2.0 Institutional Floor Space 5 L/m²/d Office Space 75 L/9.3m²/d Infiltration and Inflow Allowance 0.28L/s/ha Sanitary sewers are to be sized employing the $Q = \frac{1}{4} A R^{\frac{2}{3}} S^{\frac{1}{2}}$ Manning's Equation Minimum Sewer Size 200mm diameter Minimum Manning's 'n' 0.013 2.5m from crown of sewer to grade Minimum Depth of Cover Minimum Full Flowing Velocity 0.6m/s Maximum Full Flowing Velocity 3.0m/s Extracted from Sections 4 and 6 of the City of Ottawa Sewer Design Guidelines, November 2004.

Table 2: Wastewater Design Criteria

Table 3 below summarizes the sanitary discharge from the subject site from the approved FSR and from the proposed December 2015 Plan. See **Appendix** for detailed calculations of anticipated wastewater discharge.

| | Wastewater Discharge (L/s) | | | | |
|------------------------------------|----------------------------|-----------------------|--|--|--|
| Design Parameter | FSR February 2013 | December 2015 Plan | | | |
| Estimated Average Dry Weather Flow | 1.51 | 0.97 | | | |
| Estimated Peak Dry Weather Flow | 5.79 | 3.70 | | | |
| Estimated Peak Wet Weather Flow | 5.79 | 3.70 | | | |

Table 3: Total Anticipated Wastewater Discharge

The approved FSR contemplated wastewater discharge to both Cambridge and Bronson Avenue combined sewers. The December 2015 Plan results in a decrease in total wastewater discharge when compared to what was contemplated in the FSR, however, results in an increase in sanitary discharge directed to the Cambridge Street combined sewer, as shown in *Table 4*. The appropriate calculations have been attached.

3.70

Wastewater Discharge (L/s)

Design Parameter
FSR February
2013
Plan

Estimated Average Dry Weather Flow
0.29
0.97
Estimated Peak Dry Weather Flow
1.15
3.70

Table 4: Anticipated Wastewater Discharge to Cambridge Street

A single outlet to the Cambridge Street is a preferable to the dual connection in the approved FSR to eliminate a connection to the high traffic Bronson Avenue and take advantage of the deeper sewer within Cambridge Street.

1.15

The proposed increase in sanitary flow is accommodated by the anticipated decrease to stormwater flow to the combined sewer through rooftop and subsurface stormwater controls.

3.0 Stormwater Management

Stormwater servicing is contemplated to be achieved by a stormwater connection to the 250mm diameter combined sewer within Cambridge Street and connection to the combined sewer within Bronson Avenue. The approved FSR contemplated 2 outlets to the combined sewer within Cambridge Street and Bronson Avenue.

Consistent with the currently approved FSR, the allowable release rate has been split equally to each of the Cambridge and Bronson Avenue sewers, resulting in an allowable release of **11.0L/s** at each outlet. The total allowable release rate of **11.0L/s** directed to each outlet, described in the approved FSR, was determined by the rational method based on following criteria provided by the City of Ottawa:

Lesser of existing or 0.40 runoff coefficient

Estimated Peak Wet Weather Flow

- Attenuate to the 2-year storm event, design capacity of the existing combined sewer
- Time of concentration of 20 minutes

Attenuation will be provided by a Tempest LMF 55 and Tempest LMF 60 inlet control devices located at **STM103 & STM201**, respectively. Stormwater storage is provided by an internal stormwater cistern controlling flow to Cambridge Street and an underground storage system controlling flow to Bronson Avenue. See attached for manufacturer information on the inlet control devices flow rates and proposed underground storage system used for sizing of the chamber footprint.

Table 5 summarizes the anticipated total release rates and storage requirements from the existing FSR. A calculation sheet of the existing approved plan is attached.

5-Year Release 100-Year **Design Parameter** 5-Year 100-Year Rate Required Release Rate Required (L/s) Storage (L/s) Storage (m³) (m³) 10.3 Cambridge Street 5.0 63.3 128.6 Bronson Avenue 5.1 12.6 10.7 26.7 10.1 75.4 21.0 154.4 Total

Table 5: Proposed Amendment SWM Summary

The contemplated stormwater servicing will be designed to meet the allowable release rate determined in the approved FSR of 11.0L/s at each outlet, with a total release rate of 21.0 L/s. It is anticipated that 154.4m³ of total storage will be required to attenuate stormwater runoff.

4.0 Combined Sewer Servicing

It is contemplated to direct stormwater and sanitary discharge to the combined sewer within Cambridge Street. *Table 6 & 7* below summarizes the combined system flow contemplated in the approved FSR and December 2015 Plan to the Cambridge Street sewer.

| | FSR Febr | uary 2013 | December 2015 Plan | | |
|--|---|-----------|------------------------------|-------------------------------|--|
| Flow Type | Pre- Post- Development Developm (L/s) (L/s) | | Pre- Development (L/s) | Post- Development (L/s) | |
| Sanitary | 0.27 | 1.15 | 0.27 | 3.70 | |
| Storm (2-year uncontrolled, 100-year controlled) | 31.1 | 10.7 | 31.1 | 10.3 | |
| Combined Flow | 31.4 | 11.9 | 31.4 | 13.8 | |

Table 6: Combined Sewer Flow to Cambridge Street

Table 7: Combined Sewer Flow to Bronson Avenue

| | FSR Febr | uary 2013 | December 2015 Plan | | |
|--|-------------|-------------|--------------------|----------------------|--|
| Flow Type | Pre- | Post- | Pre- | Post- Development | |
| | Development | Development | Development | | |
| | (L/s) | (L/s) | (L/s) | (L/s) | |
| Sanitary | 0.27 | 4.64 | 0.27 | 0.00 | |
| Storm (2-year uncontrolled, 100-year controlled) | 31.1 | 10.7 | 31.1 | 10.7 | |
| Combined Flow | 31.4 | 15.3 | 31.4 | 10.7 | |

The proposed sanitary and stormwater servicing contemplated in the December 2015 Plan, results in a net reduction of **17.6** L/s and **20.7** L/s of flow entering the combined sewer on Cambridge and Bronson, respectively. The increase in sanitary discharge to the Cambridge Street combined sewer is accommodated with the significant decrease in stormwater discharge.

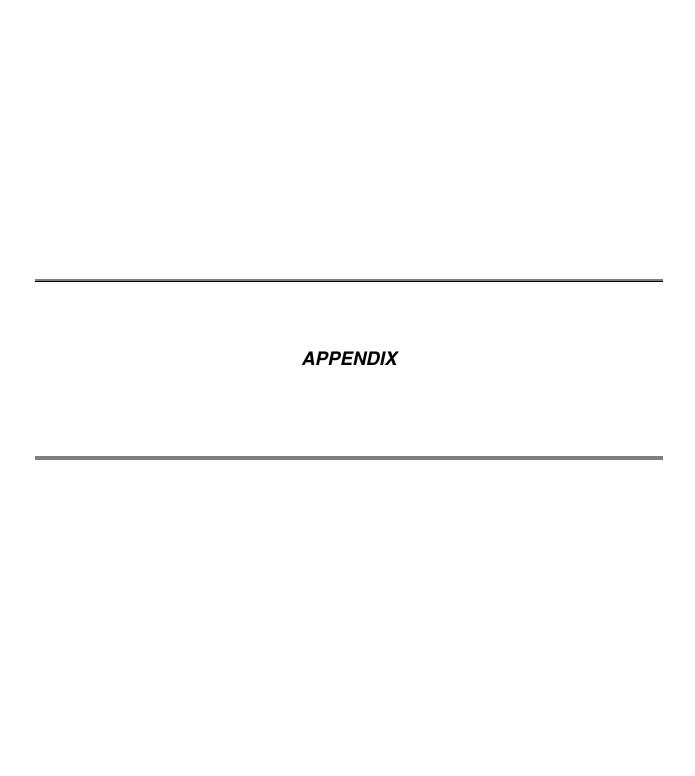
Yours truly, **David Schaeffer Engineering Ltd.**

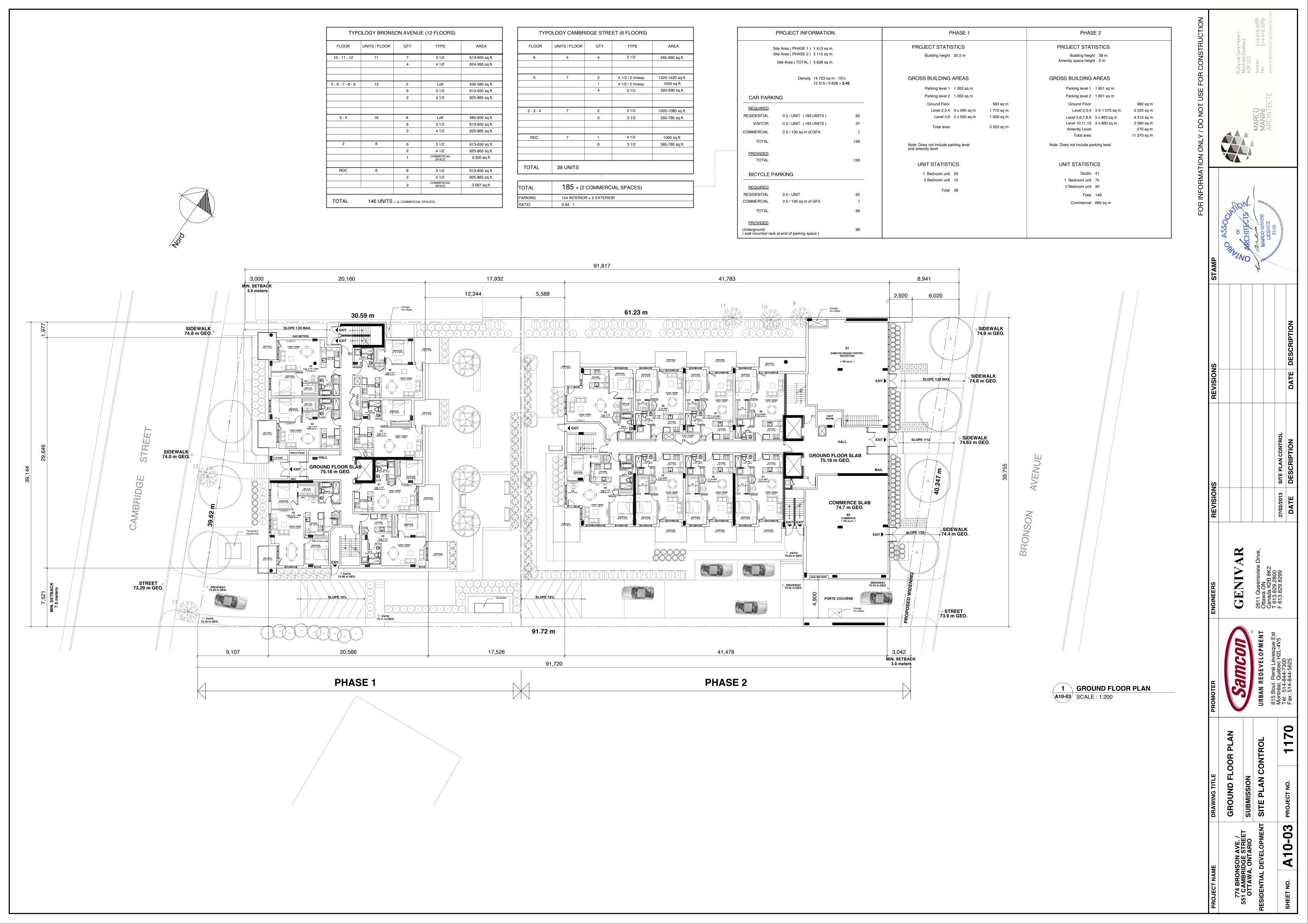
Yours truly, **David Schaeffer Engineering Ltd.**



Per: Robert D. Freel, P.Eng.

Per: Steven L. Merrick, EIT.

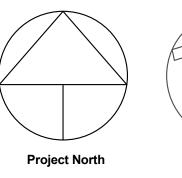


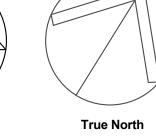


| STANDARD ZONING MECHANISM - AMI | | | | | | | |
|---|---|--|--|--|--|--|--|
| PROVISION | REQUIREMENT | PROPOSED | | | | | |
| MINIMUM LOT WIDTH | No Minimum | 39.14 m | | | | | |
| MINIMUM LOT AREA | No Minimum | 3628 m ² | | | | | |
| MINIMUM FRONT YARD SETBACK | No Minimum | 5.50 m | | | | | |
| VINIMUM INTERIOR SIDE YARD SETBACKS | No minimum unless abutting a residential zone (7.5 m) | 4.24 m | | | | | |
| MINIMUM REAR YARD SETBACK | 3 m | 3 m | | | | | |
| MAXIMUM BUILDING HEIGHT* | Ranges from 11 to 25 m | 39.25 m | | | | | |
| VAXIMUM FLOOR SPACE INDEX* | 3.5 (if 80% of parking is below grade), 2 (otherwise) | 3.02 | | | | | |
| VINIMUM WIDTH OF LANDSCAPED AREA (abutting a residential zone)* | 3 m | 4.24 m | | | | | |
| VINIMUM RESIDENT PARKING RATE | 0.5 spaces per dwelling unit (91 spaces) | | | | | | |
| VINIMUM VISITOR PARKING RATE* | 0.2 spaces per dwelling unit, first 12 units exempt (34 spaces) | 31 spaces | | | | | |
| VINIMUM BICYCLE PARKING RATE | 0.5 spaces per dwelling unit (91 spaces) | 95 spaces | | | | | |
| PARKING SPACE SIZE PROVISION | 2.6 m (width) by 5.2 m (length) | 2.6 m by 5.2 m | | | | | |
| PARKING AISLE AND DRIVEWAY SIZE PROVISION | 6.7 m minimum width for double traffic lane | 6.7 m minimum | | | | | |
| BICYCLE PARKING SPACE SIZE PROVISION | 0.6 m by 1.8 m | 0.6 m by 1.8 m | | | | | |
| MINIMUM AMENITY AREA | 6m ² per dwelling unit, 50% minimum communal amenity area (1,086m ²) | 720.14 m ² (interior) + 599.92 m ² (exterior) = 1,320.06 m^2 | | | | | |

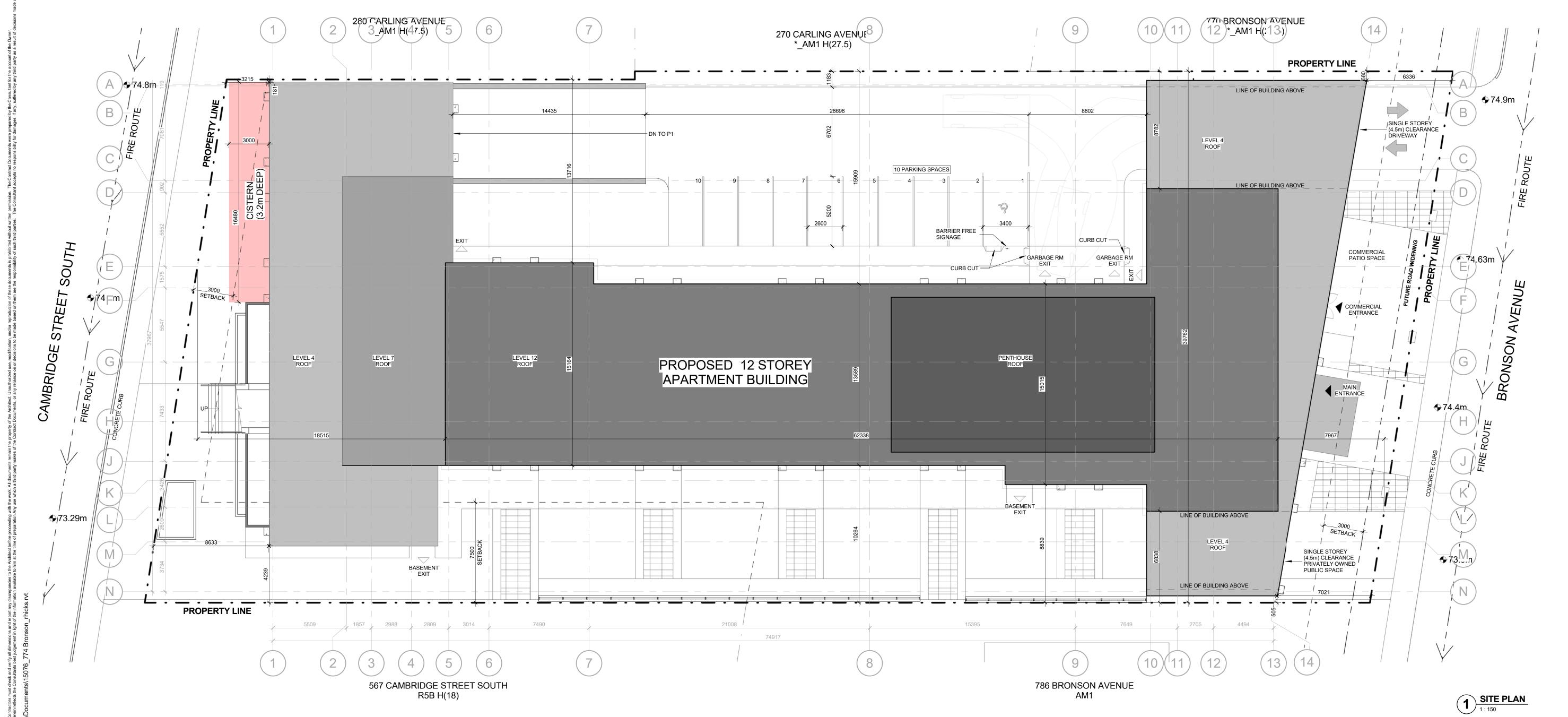
| SITE DATA CHART | | | | | | |
|-----------------|---------------------------------|-------------------------------------|--|--|--|--|
| | DATA | REQUIREMENT | PROPOSED | | | |
| ZONIN | G | Arterial Main S | treet - AM1 Zone | | | |
| LOT AI | REA | 3,628 | 8.09 m ² | | | |
| TOTAL | DENSITY | | 181 units (341 beds) | | | |
| GROSS | FLOOR AREA (m²) | | 10,965.52 m ² | | | |
| NUMB | ER OF STOREYS | | 12 | | | |
| BUILD | ING HEIGHT (m) | maximum 41.5 m | 39.25 m | | | |
| COMM | MERCIAL / RETAIL AREA (m) | | 135.62 m ² | | | |
| AMEN | ITY AREA | minimum 6m² / unit | 1,320.06 m ² | | | |
| LANDS | SCAPE AREA (%) | | 1,088 m ² ÷ 3,628 m ² = 29.9 | | | |
| | CAPE AREA (m ²) | | 1,088 m ² | | | |
| (5 | RESIDENTIAL | 0.5 / unit = 91 | | | | |
| PARKING | VISITOR (first 12 units exempt) | 0.2 / unit = 34 | 31 | | | |
| AR | TOTAL | 125 | | | | |
| Ъ | BARRIER FREE SPACES | | 1 (incl.) | | | |
| (7 | RESIDENTIAL | 0.5 / unit = 91 | | | | |
| BICYCLE | COMMERCIAL | MERCIAL $2.5 / 100 \text{ m}^2 = 4$ | | | | |
| TOTAL TOTAL | | 95 | 95 | | | |







2 KEY PLAN
1:2000

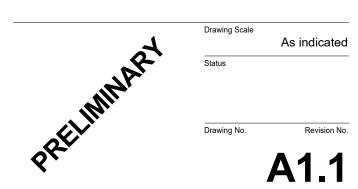


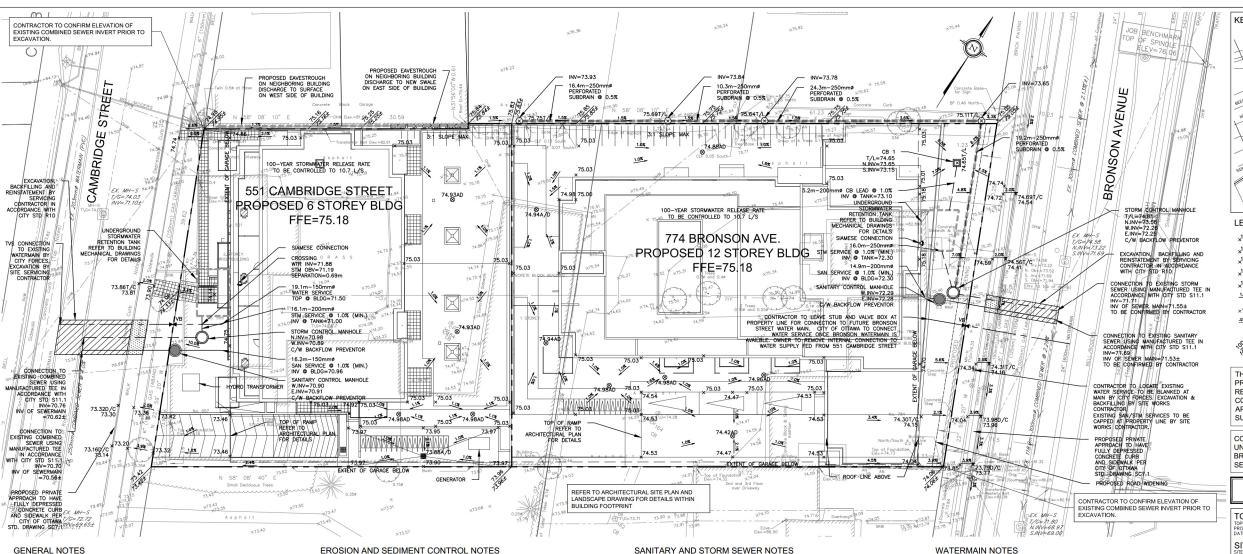




774 BRONSON AVENUE, OTTAWA

SITE PLAN





- ALL WORKS AND MATERIALS SHALL CONFORM TO THE LATEST REVISION OF THE STANDARDS AND SPECIFICATIONS FOR THE CITY OF OTTAWA, ONTARIO PROVINCIAL STANDARD DRAWNSS (OPES), AND SPECIFICATIONS (OPES), WHERE APPLICABLE, LOCAL UTILITY STANDARDS AND MINISTRY OF TRANSPORTATIONS STANDARDS WILL APPLY WHERE REQUIRED.
- VITAMO, INVARION PROVINCIAL STANDARD DRAWNESS (DPSD) AND SPECIFICATIONS (OPS), WHERE APPLICABLE LICAL VITLINY STANDARDS AND MINISTRY OF TRANSPORTATION STANDARDS WILL APPLY WHERE REQUIRED.

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- CONTROL DEVOCES PER CHIEST AMENDMENT.

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- 9. ALL DURISHONS ARE IN METRIS UNIESS SPECIFIED OTHERWIS.

 10. THERE MILL BE NO SUBSTITUTION OF MATERIAS UNLESS PROCE WITTEN APPROVAL IS RECEIVED FROM THE ENGINEER.

 11. ALL CONSTRUCTION SHALL BE CARRED OUT IN ACCORDANCE WITH THE RECOMMENDATIONS MADE IN THE ECOTECHNICAL REPORT.

 12. FOR DEFAULS RELATING TO STORMWATER MANAGEMENT AND ROOF DRAINAGE REFER TO THE SITE SERVICING AND STORMWATER MANAGEMENT AND ROOF DRAINAGE REFER TO THE SITE SERVICING AND STORMWATER MANAGEMENT AND ROOF DRAINAGE REFER TO THE SITE SERVICING AND STORMWATER MANAGEMENT AND ROOF DRAINAGE REFER TO THE SITE SERVICING AND STORMWATER MANAGEMENT AND ROOF DRAINAGE REFER TO THE SITE SERVICING AND STORMWATER MANAGEMENT AND ROOF DRAINAGE REFER TO THE SITE SERVICING AND STORMWATER MANAGEMENT AND ROOF DRAINAGE REFER TO THE SITE SERVICING AND STORMWATER MANAGEMENT AND ROOF DRAINAGE REFER TO THE SITE SERVICING AND STORMWATER MANAGEMENT AND ROOF DRAINAGE REFER TO THE SITE SERVICING AND STORMWATER MANAGEMENT AND ROOF DRAINAGE REFER TO THE SITE SERVICING AND STORMWATER MANAGEMENT AND ROOF DRAINAGE REFER TO THE SITE SERVICING AND STORMWATER MANAGEMENT AND ROOF DRAINAGE REFER TO THE SITE SERVICING AND STORMWATER MANAGEMENT AND ROOF DRAINAGE REFER TO THE SITE SERVICING AND STORMWATER MANAGEMENT AND ROOF DRAINAGE REFER TO THE SITE SERVICING AND STORMWATER MANAGEMENT AND ROOF DRAINAGE REFER TO THE SITE SERVICING AND STORMWATER MANAGEMENT AND ROOF DRAINAGE REFER TO THE SITE SERVICING AND STORMWATER MANAGEMENT AND ROOF DRAINAGE REFER TO THE SITE SERVICING AND STORMWATER MANAGEMENT AND ROOF DRAINAGE REFER TO THE SITE SERVICING AND STORMWATER MANAGEMENT AND ROOF DRAINAGE REFER TO THE STORM STORM AND STORM S
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 3. ALL SEWERS CONSTRUCTED WITH GRADES LESS THAN 1.0% SHALL BE INSTALLED USING LASER ALIGNMENT AND CHECKED WITH LEVEL INSTRUMENT PRIOR TO RACKELLING.
- INSTRUMENT PROOR TO BACKFILLING.

 14 HE CONTRACTOR RESPONSEE FOR CREANING ALL FERMITS REQUESTED AND TO BEAR THE COST OF THE SAME.

 15 HE CONTRACTOR WILL BE RESPONSIBLE FOR ADDITIONAL BEDDING, OR ADDITIONAL STRENGTH PIPE IF THE MAXIMUM TRENCH WITH AS SPECIFIED BY ORDS 15 EXCEEDED.

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- 21. BENCHMARKS: IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY THAT THE SITE BENCHMARK(S) HAS NOT BEEN ALTERED OR DISTURBED AND THAT ITS RELATIVE ELEVATION AND DESCRIPTION AGREES WITH THE INFORMATION DEPICTED ON THIS PLAN.

- PRIOR TO THE COMMINISCENSIT OF THE SITE GRADING WORKS, ALL SILTATION CONTROL DEVICES SHALL BE INSTALLED AND OP PER EROSION CONTROL PLAN.
 ALL GRANILLAR AND PARKEMENT FOR ROADS/PARKING AREAS SHALL BE CONSTRUCTED IN ACCORDANCE WITH GEOTECHNICAL ENGINEET'S RECOMMENSATIONS.
- ALL TOPSOIL AND ORGANIC MATERIAL SHALL BE STRIPPED WITHIN THE ROAD AND PARKING AREAS ALLOWANCE PRIOR TO THE COMMENCEMENT OF CONSTRUCTION.
- CONTINUE.

 PAYMENT REINSTATEMENT FOR SERVICE AND UTILITY CUTS SHALL BE IN ACCORDANCE WITH THE CITY OF OTTAWA STD. RIO AND OPSD 509.010, AND OPSS 310.
- ILL BE PLACED TO A MINIMUM THICKNESS OF 300mm AROUND ALL STRUCTURES WITHIN THE PAVEMENT AREA.
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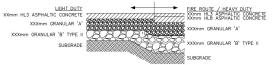
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- 10. ALL PAVEMENT MARKING FEATURES AND SITE SIGNAGE SHALL BE PLACED PER ARCHITECTURAL SITE PLAN. LINE PAINTING AND DIRECTIONAL SYMOBOLS SHALL BE APPLIED WITH A MINIMUM OF TWO COATS OF ORGANIC SOLVENT PAINT.
- 11. REFER TO ARCHITECTURAL SITE PLAN FOR DIMENSIONS AND SITE DETAILS.

 12. STEP JOINTS ARC TO BE USED WHERE PROPOSED ASPHALT MEETS EXSTING ASPHALT. ALL JOINTS MUST BE SEALED.

 13. SIDEWAKES TO BE 20mm BELOW THE PRINSHED FLOOR SLAB LEVATION AT ENTRANCES UNLESS OTHERWISE NOTED.

PAVEMENT STRUCTURE



CENERAL
THE CONTRACTOR ACKNOWLEDGES THAT SURFACE EROSON AND SEDIMENT RUNOFF RESULTING FROM THEIR CONSTRUCTION
OPERATIONS HAS POTENTIAL TO CAUSE A DETRIMENTAL IMPACT TO ANY DOWNSTREAM WATERCOURSE OR SEWER, AND
THAT TALL CONSTRUCTION OPERATIONS THAT MAY IMPACT UPON WATER QUALITY SHALL BE CARRIED OUT IN A MANNER
THAT STRICTLY MEETS THE REQUIREMENTS OF ALL APPLICABLE LEGISLATION AND REQULATIONS.

THE CONTRACTOR SHALL BE RESPONSIBLE FOR CARRYING OUT THEIR OPERATIONS, AND SUPPLYING AND ANY APPROPRIATE CONTROL MEASURES, SO AS TO PREVENT SEDIMENT LADEN RUNOFF FROM ENTERING ANY WATERCOURSE WITHIN OR DOWNSTREAM OF THE WORKING AREA.

THE CONTRACTOR ACKNOWLEDGES THAT NO ONE MEASURE IS LIKELY TO BE 100% EFFECTIVE FOR EROSION PROTECTION AND CONTROLLING SEDIMENT RUNOFF AND DISCHARGES FROM THE SITE. THEREFORE, WHERE NECESSARY THE CONTRACTOR SHALL IMPLEMENT ADDITIONAL MEASURES ARRANCED IN SUCH A MANNER AS TO MITIGATE SEDIMENT RELEASE FROM THE CONSTRUCTION OPERATIONS AND ACHIEVE SPECIFIC MAXIMUM PERMITTED CRITERIA WHERE APPLICABLE. SUGGESTED ON-SITE MEASURES AND RULOED BY A MALL NOT BE LEMBED TO, HE FOLDOWING METHODS SECTION FILTER BOSS, PIMER BOSS, PIM

CONTRACTOR'S ESPONSBULITES
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OF THE IMPORTANCE OF THE EROSION AND SEDIMENT CONTROL MEASURES AND INFORMED OF THE CONSEQUENCES OF THE
FAILURE TO COUNCY! WITH THE RECOURTEMENTS OF ALL REGULATORY AGENCIES.

CONTRACTOR SHALL PERSONCALLY, AND WHEN REQUESTED BY THE CONTRACT ADMINISTRATOR, CLEAN OUT
UNDALATED SEDMENT DEPOSITS AS REQUIRED AT THE SEDMENT CONTROL DEVICES, INCLUDING THOSE EPPOSITS THAT
WHEN THAT PREVENTS THE DEPOSITION OF THIS MATERIAL INTO ANY SEMER OR WATERCOURSE AND AVOIDS DAMAGE TO
CONTROL MEASURE. THE SEDMENT SHALL BE REMOVED FROM THE SITE AT THE CONTRACTOR'S EXPENSE AND
AGED. IN COMPLIANCE WITH THE REQUIREMENTS FOR EXCESS EARTH MATERIAL, AS SPECIFIED EXSEMBLES IN

WHERE, IN THE OPINION OF EITHER THE CONTRACT ADMINISTRATOR OR A REQULATORY AGENCY, ANY OF THE TERMS SPECIFIED HEREIN HAVE NOT BEEN COMPULED WITH OR PERFORMED IN SUITABLE MANNER, OR AT ALL, THE CONTRACT ADMINISTRATOR OR REQULATORY AGENCY HAS THE RIGHT TO IMMEDIATELY WHITDAWN ITS PERMISSION TO CONTINUE WORK BUT MAY RENEW ITS PERMISSION UPON BEING SATISFIED THAT THE DEFAULTS OR DEPICIENCES IN THE PERFORMANCE OF THIS SPECIFICATION BY THE CONTRACTOR HAVE BEEN REMEDIED.

SPILL CONTROL NOTES

- ALL CONSTRUCTION EQUIPMENT SHALL BE RE-FUELED, MAINTAINED, AND STORED NO LESS THAN 30 METRES FROM WATERCOURSES, STREAMS, CREEKS, WOODLOTS, AND ANY ENVIRONMENTALLY SENSITIVE AREAS, OR AS OTHERWISE SPECIFIED.

 THE CONTRACTOR MUST IMPLEMENT ALL MERCENCIA WATER AND ANY ENVIRONMENTALLY SENSITIVE AREAS, OR AS OTHERWISE SPECIFICAL WATER AND ANY ENVIRONMENTALLY SENSITIVE AREAS, OR AS OTHERWISE SPECIFICAL WATER AND ANY ENVIRONMENTALLY SENSITIVE AREAS, OR AS OTHERWISE SPECIFICAL WATER AND ANY ENVIRONMENTALLY SENSITIVE AREAS, OR AS OTHERWISE SPECIFICAL WATER AND ANY ENVIRONMENTALLY SENSITIVE AREAS, OR AS OTHERWISE SPECIFICAL WATER AND ANY ENVIRONMENTALLY SENSITIVE AREAS, OR AS OTHERWISE SPECIFICAL WATER AND ANY ENVIRONMENTALLY SENSITIVE AREAS, OR AS OTHER WATER AND ANY ENVIRONMENTALLY SENSITIVE AREAS, OR AS OTHER WATER AND ANY ENVIRONMENTALLY SENSITIVE AREAS, OR AS OTHER WATER AND ANY ENVIRONMENTALLY SENSITIVE AREAS, OR AS OTHER WATER AND ANY ENVIRONMENTALLY SENSITIVE AREAS, OR AS OTHER WATER AND ANY ENVIRONMENTALLY SENSITIVE AREAS, OR AS OTHER WATER AND ANY ENVIRONMENTALLY SENSITIVE AREAS, OR AS OTHER WATER AND ANY ENVIRONMENTALLY SENSITIVE AREAS, OR AS OTHER WATER AND ANY ENVIRONMENTALLY SENSITIVE AREAS, OR AS OTHER WATER AND ANY ENVIRONMENTALLY SENSITIVE AREAS AND ANY ENVIRONMENTALLY SENSITIVE AREAS AND ANY ENVIRONMENTAL AND ANY ENVIRONMENTAL AND ANY ENVIRONMENTAL AND ANY ENVIRONMENTAL AND AND ANY ENVIRONMENTAL AND
- PECIFIED.

 HE CONTRACTOR MUST IMPLEMENT ALL NECESSARY MEASURES IN ORDER TO PREVENT LEAKS, DISCHARGES OR SPILLS
 F POLLUTANTS, DELETEROUS MATERIALS, OR OTHER SUCH MATERIALS OR SUBSTANCES WHICH WOULD OR COULD
 ALUSE ANA DOVERSE MEMOAT TO HE NATURAL ENVIRONMENT. THAT
 IN THE VEHAT OF A LEAK DISCHARGE OR SPILL OF A POLLUTANT, DELETERIOUS MATERIAL OR OTHER SUCH MATERIAL
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 3.3. RESTORE THE APPRICED BARE TO TOTHE ORDAIN, CONDITION OF BETTER TO THE SATISFACTION OF THE AUTHORITIES

SANITARY AND STORM SEWER NOTES

- NERAL

 IASER ALIGNMENT CONTROL TO BE UTILIZED ON ALL SEWER INSTALLATIONS

- CEMENDAL

 I. LASER AUGMENT CONTROL TO BE UTILIZED ON ALL SEWER INSTALLATIONS.

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 S. SERVES TO BULDINGS TO BE TERMANIZED LOW FROM THE CONTROL FACE OF BULDING UNLESS OTHERWISE NOTED.

 ALL MAINTENANCE STRICTURE AND CALLY BOARD CANADINATION TO BE ADMINISTED TO BE USED IN LIEU OF BRICKING.

 S. "MODILICA" OR APPROVED PRE-CAST MAINTENANCE STRUCTURE AND CATCH BASIN ADJUSTERS TO BE USED IN LIEU OF BRICKING.

 S. SHETT PLATFORMS SHALL BE FER CROSS 404.02.

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NULLEY ALL SANTARY SEWER INSTALLATION SHALL CONFORM TO THE LATEST REVISIONS OF THE CITY OF OTTAWA AND THE ONTARIO PROVINCIAL STANDARD DRAWINGS (CPSD) AND SPECIPICATIONS (CPSS). ALL SANTARY REAVITY SEMES THE EP FOR SIDE 39, DEVER FAMO-THE (OR APPROVED EQUIVALENT) PER CSA STANDARD B182.2 OR LATEST AMENDMENT, UNLESS SPECIPED OTHERWISE. LEVISION MAINTENANCE STRUCTURES TO BE RE-ELECTHED WHERE A NEW CONNECTION IS MADIE. S. SANTARY CRAVITY SEWER TRENCH AND BEDDING SHALL BE PER CITY OF OTTAWA STD. S6 AND S7, CLASS '8' BEDDING, UNLESS SPECIFIED OTHERWISE.

- REINFORCED CONCRETE STORM SEWER PIPE SHALL BE IN ACCORDANCE WITH CSA A257.2, OR LATEST AMENDMENT. ALL REINFORCED CONCRETE STORM SEWER PIPE SHALL BE IN ACCORDANCE WITH CSA A257.1, OR LATEST AMENDMENT, PIPE SHALL DINCE WITH STOR TUBBER CASKETS AS PER CSA A257.3. OR LATEST AMENDMENT.

- BE CONCID WITH STO. RUBBER CASMETS AS PER CSA A2573, OF LATEST AMERIOWANT.

 ALL STOME SEVER PREMICH AND BEDROM SHALL BE IN ACCORDANCE WITH CITY OF OTTAMA STD. SE AND ST CASS YE UNLESS
 OTHERWISE SPECIFIED BEDROM AND COVER MATERIAL SHALL BE SPECIFIED OF PROVIDE CHOICE, DISNIERER.

 ALL PCX. STOME SEMENS ARE TO BE SEM SEA APPROVED FOR CSA. BIRD.2 OR LATEST AMERIOWANT, OULLES OTHERWISE SPECIFIED.

 C. ALTO BESON LEADS SHALL BE 2000M DIA. AT ITS SLOPE (WIN) UNLESS SPECIFIED OTHERWISE.

 Z. ALL CATOL BESON SHALL BASE SOON SURSES, LIVELES SPECIFIED OTHERWISE.

 Z. ALL CATOL BESON LEAD INVERTS TO BE 1.5% BESTOW FINISHED CRADE UNLESS SPECIFIED OTHERWISE.

 Z. ALL CATOL BESON LEAD SHALL BE SEED IN DESCRIBED OTHERWISE.

 Z. ALL CATOL BESON LEAD SHALL BE SEED IN DESCRIBED OTHERWISE.

 J. BE STOME SEVER CLASSES HAVE BEEN DESCRIBED ASSED ON BEDONIC CONTROL SPECIFIED ABOVE. WHERE THE SPECIFIED TRINCH
 PERMANENT REPAIRS MADE RECESSARY BY THE WICHED TRINCH.

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 PERMANENT REPAIRS MADE RECESSARY BY THE WICHED TRINCH.

 PERMANEN
- WHERE APPLICABLE.

 RIP-RAP TEEATMENT FOR SEWER AND CULVERT OUTLETS PER OPSD 810,010.

 ALL STORM SEWERS / CULVERTS TO BE INSTALLED WITH FROST TREATMENT PER OPSD 803,031 WHERE APPLICABLE

STORM DRAIN INLET PROTECTION CATCH BASIN LID -CATCH BASIN (TYP) NOT TO SCALE

- I ETRIMAIN NULLES

 ALL MATERIAN INSTALLATION SHALL CONCION TO THE LATEST REVISIONS OF THE CITY OF OTTAMA AND THE ONTARIO PROVINCIAL

 ALL PARTICIPATION SHALL BE AND CAPOLLASS TO SEE 16 OF APPROVED EQUIVALENT.

 MATERIANN TENENH AND BEDONG SHALL BE IN ACCORDANCE WITH CITY OF OTTAMA STANDARD WIT. UNLESS SPECIFED OTHERWISE.

 BEDING AND COOR MATERIAL SHALL BE SEPCIFED BY THE PROJECT ECOTORICHALLE MORNER.

 ALL PIC MATERIANIS SHALL BE INSTALLED WITH A 10 GAUGE STRANGED COPPER TWU OF RWU TRACER WIRE IN ACCORDANCE WITH

 CITY OF OTTAMA STID. MS.6.

- ALL PUE WASSIAMEN SHALL BE INSTALLD WITH A 10 GAUGE STRANGED COPPLEX TWO OR NOW THACLER WIRE. IN ACCORDANCE WITH CATHOOP ROFIDETION IS REQUIRED ON ALL METALLO FITTINGS PER CITY OF OTTAMA STD. W40 AND W42.
 VALVE BOXES SHALL BE INSTALLED FIRE CITY OF OTTAMA STD W24.
 WASTERMAN IN FILE AREAS TO BE INSTALLED WITH RESTRAND JOINTS PER CITY OF OTTAMA STD. 253. AND W25.4.
 THE CONTRACTOR SHALL PROVIDE ALL TEMPORARY CAPS, PLUSS, BLOW—OFFS, AND OXIZES REQUIRED FOR TESTING AND DISN'ECTION OF THE WATERMANN.

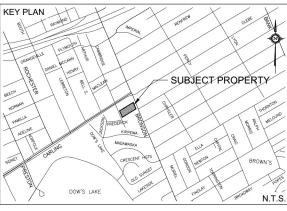
 WASTERMANN, CORSISMO OVER AND BELOW SEVERS SHALL BE IN ACCORDANCE WITH CITY OF OTTAWA STD. W25.2 AND W25.
- NESTECTIVELT.

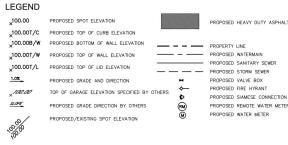
 WATER SERVICES ARE TO BE INSULATED PER CITY STD. W23 WHERE SEPARATION BETWEEN SERVICES AND MAINTENANCE HOLES ARE
 LESS THAN 2-4m.

- MINIMUM OF 12M BACK FROM STUB.

 ALL WATERMAINS SHALL BE HYDROSTATICALLY TESTED IN ACCORDANCE WITH THE CITY OF OTTAWA AND ONTARIO GUIDELINES UNLESS OTHERWISE DIRECTED, PROMISIONS FOR FLUSHING WATER LINE PRIOR TO TESTING, ETC. MUST BE PROVIDED.
- B. ALL WATERWANDS UNDELLED. PROVISIONS FOR FLOSHING WATER LINE PHOLIVE OLD ESTING, ELL, MOST BE PROVIDED. TO A CONTROL WATER TO BE ACCEPTANCE WITH THE CITY OF TOTAMS AND ONTARIO OUDELINES. ALL OLD GRANATED WATER TO BE DISCHARGED AND PRETECTED TO ACCEPTANCE LEVELS PROPE TO DISCHARGE, ALL DISCHARGED WATER MUST BE CONTROLLED AND TREATED SO AS NOT TO ANOMERSELY EFFORT THE ENVIRONMENT, IT IS THE RESPONSIBILITY OF THE CONTROLLED AND TREATED AND AND/OR PROMINGIAL REQUIREMENTS ARE FOLLOWED.

 9. ALL WATERWAND STUBS SHALL BE LETERMANED WITH A PULL ON 300 THE MEDICATION OF TO MESSES NOTED.





THE CONTRACTOR SHALL IMPLEMENT BEST MANAGEMENT PRACTICES, TO PROVIDE FOR PROTECTION OF THE AREA DRAINAGE SYSTEM AND THE RECEIVING WATERCOURSE, DURING CONSTRUCTION ACTIVITIES. THE CONTRACTOR ACKNOWLEDGES THAT THE FAILURE TO IMPLEMENT APPROPRIATE EROSION AND SEDIMENT CONTROL MEASURES MAY BE SUBJECT TO PENALTIES IMPOSED BY ANY APPLICABLE REGULATORY AGENCY.

CONTRACTOR TO CONFIRM ELEVATIONS AND LOCATIONS OF EXISTING UNDERGROUND SERVICES AND UTILITIES WITHIN CAMBRIDGE STREET AND BRONSON AVENUE RIGHTS OF WAY PRIOR TO INSTALLATION OF SITE SERVICING INFRASTRUCTURE.

NOT FOR CONSTRUCTION

TOPOGRAPHIC INFORMATION

TOPOGRAPHIC INFORMATION PROVIDED BY ANNIS, O'SULLIVAN, VOLLEBEKK LTD. PROJ. NO. 12483-11 SAMCON LTS 3,4,37&38 PI 28 T D3
DATED JUNE 2012

SITE PLAN INFORMATION

PROJ. NO. 1170 DATE DECEMBER 12, 2013

GEOTECHNICAL STUDY

PROJ. NO. 111-26060-00 DATED DECEMBER 2011

SITE SERVICING AND STORMWATER MANAGEMENT STUDY

BENCH MARK

A.D.F. 13.10.21 REVISED PER SITE PLAN (ADDED PARKING SPACE SOUTH OF BRONSON PHA A.D.F. 13.10.21 REVISED PER MUNICIPAL COMMENTS A.D.F. 13.10.03 ISSUED FOR MUNICIPAL REVIEW



SITE SERVICING & GRADING PLAN 774 BRONSON/551 CAMBRIDGE

SAMCON REDEVELOPPEMENT URBAIN

815 Boul. Rene Levesque Est Montreal, Quebec H2L-4V5



Stittsville, Ontario, K2S 1E9 Tel. (613) 836-0856 www.DSEL.ca Fax. (613) 836-7183

© DSEL

DRAWN BY: B.N.C. CHECKED BY: R.M.W. DRAWING NO. | DESIGNED BY: R.M.W. | CHECKED BY: | SCALE: | 1: 200 | DATE: | JUNE 2013 | SSGP-1 1 of 1

z:\projects\12-557_samcon_bronson-cambridge\b_design\b2_drawings\b2-2_main (dsel)\spa_sub_2\2014-01-08.dwg

774 Bronson Ave/551 Cambridge St Samcon Proposed Conditions

Water Demand Design Flows per Unit Count City of Ottawa - Water Distribution Guidelines, July 2010



Domestic Demand

| Type of Housing | Per / Unit | Units | Pop |
|-----------------|------------|-------|-----|
| Single Family | 3.4 | | 0 |
| Semi-detached | 2.7 | | 0 |
| Townhouse | 2.7 | | 0 |
| Apartment | | | 0 |
| Bachelor | 1.4 | | 0 |
| 1 Bedroom | 1.4 | | 0 |
| 2 Bedroom | 2.1 | | 0 |
| 3 Bedroom | 3.1 | | 0 |
| Average | 1.8 | 193 | 348 |

| | Pop | Avg. Daily | | Max Day | | Peak Hour | | |
|-----------------------|-----|------------|-------|---------|-------|-----------|-------|--|
| | | m³/d | L/min | m³/d | L/min | m³/d | L/min | |
| Total Domestic Demand | 348 | 121.8 | 84.6 | 365.4 | 253.8 | 548.1 | 380.6 | |

Institutional / Commercial / Industrial Demand

| | | | | Avg. 🛭 | Daily | Max I | Day | Peak I | Hour |
|------------------------|--------|------------------------|----------|--------|-------|-------|-------|--------|-------|
| Property Type | Unit | Rate | Units | m³/d | L/min | m³/d | L/min | m³/d | L/min |
| Commercial floor space | 2.5 | L/m ² /d | 804 | 2.01 | 1.4 | 3.0 | 2.1 | 5.4 | 3.8 |
| Office | 75 | L/9.3m ² /d | | 0.00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Industrial - Light | 35,000 | L/gross ha/d | | 0.00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Industrial - Heavy | 55,000 | L/gross ha/d | | 0.00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Total I/CI I | Demand _ | 2.0 | 1.4 | 3.0 | 2.1 | 5.4 | 3.8 |
| | | Total I | Demand | 123.8 | 86.0 | 368.4 | 255.8 | 553.5 | 384.4 |

774 Bronson Ave SRM Architects Proposed Conditions

Water Demand Design Flows per Unit Count City of Ottawa - Water Distribution Guidelines, July 2010



Domestic Demand

| Type of Housing | Per / Unit | Units | Pop |
|-----------------|------------|-------|-------|
| Single Family | 3.4 | | 0 |
| Semi-detached | 2.7 | | 0 |
| Townhouse | 2.7 | | 0 |
| Apartment | | | 0 |
| Bachelor | 1.4 | | 0 |
| 1 Bedroom | 1.4 | | 0 |
| 2 Bedroom | 2.1 | | 0 |
| 3 Bedroom | 3.1 | | 0 |
| Average | 1.8 | | 0 |
| Type of Housing | Per/Bed | Beds | Рор |
| Boarding* | 1 | 34 | 1 341 |

| | Pop | Avg. Daily | | Max Day | | Peak Hour | |
|-----------------------|-----|------------|-------|---------|-------|-----------|-------|
| | | m³/d | L/min | m³/d | L/min | m³/d | L/min |
| Total Domestic Demand | 341 | 68.2 | 47.4 | 204.6 | 142.1 | 306.9 | 213.1 |

Institutional / Commercial / Industrial Demand

| | | | Avg. ۵ | Daily | Max | Day | Peak I | Hour |
|--------------------------|---------------------------|---------------|--------|-------|-------|-------|--------|-------|
| Property Type | Unit Rate | Units | m³/d | L/min | m³/d | L/min | m³/d | L/min |
| Commercial floor space** | 2.5 L/m ² /d | 136 | 0.34 | 0.2 | 0.5 | 0.4 | 0.9 | 0.6 |
| Office | 75 L/9.3m ² /d | | 0.00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Industrial - Light | 35,000 L/gross ha/ | d | 0.00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Industrial - Heavy | 55,000 L/gross ha/ | d | 0.00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Tota | I I/CI Demand | 0.3 | 0.2 | 0.5 | 0.4 | 0.9 | 0.6 |
| | , | Total Demand | 68.5 | 47.6 | 205.1 | 142.4 | 307.8 | 213.8 |

^{*} Based on a daily demand of 200L/day per person as identified by Appendix 4-A of the Sewer design guidelines

^{**} Comprises all proposed commercial and amenity space

SRM Architects Inc. 774 Bronson Ave. FUS-Fire Flow Demand

Fire Flow Estimation per Fire Underwriters Survey

Water Supply For Public Fire Protection - 1999



Fire Flow Required

1. Base Requirement

 $F=220C\sqrt{A}$ L/min Where **F** is the fire flow, **C** is the Type of construction and **A** is the Total floor area

Type of Construction: Non-Combustible Construction

C 0.8 Type of Construction Coefficient per FUS Part II, Section 1
 A 10965.0 m² Total floor area based on FUS Part II section 1

Fire Flow 18429.6 L/min

18000.0 L/min rounded to the nearest 1,000 L/min

Adjustments

2. Reduction for Occupancy Type

Non-Combustible -25%

Fire Flow 13500.0 L/min

3. Reduction for Sprinkler Protection

Sprinklered -50%

Reduction -6750 L/min

4. Increase for Separation Distance

 N
 3.1m-10m
 20%

 S
 3.1m-10m
 20%

 E
 >45m
 0%

 W
 20.1m-30m
 10%

% Increase 50% value not to exceed 75% per FUS Part II, Section 4

Increase 6750.0 L/min

Total Fire Flow

| Fire Flow | 13500.0 L/min | fire flow not to exceed 45,000 L/min nor be less than 2,000 L/min per FUS Section 4 |
|-----------|---------------|---|
| | 14000.0 L/min | rounded to the nearest 1,000 L/min |

Notes:

- -Type of construction, Occupancy Type and Sprinkler Protection information provided by SRM Architects Inc.
- -Calculations based on Fire Underwriters Survey Part II

Steve Merrick

To: Steve Merrick

Subject: RE: 774 Bronson Ave - Water Boundary Conditions

From: White, Joshua [mailto:Joshua.White@ottawa.ca]

Sent: November-12-15 3:41 PM

To: 'Steve Merrick' <smerrick@dsel.ca>

Subject: RE: 774 Bronson Ave - Water Boundary Conditions

Hello Steve,

Please find the Boundary Conditions for the proposal at 774 Bronson. If you have any questions please let me know.

Josh

The following are boundary conditions, HGL, for hydraulic analysis at 774 Bronson (zone 1W) assumed to be connected to the 203mm on Cambridge (see attached PDF for location).

Minimum HGL = 106.1m

Maximum HGL = 117.1m

Available Flow = 125 L/s, assuming a residual of 20 psi and a ground elevation of 73.9m

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

From: Steve Merrick [mailto:smerrick@dsel.ca]
Sent: Monday, November 09, 2015 5:03 PM

To: White, Joshua **Cc:** Wu, John

Subject: RE: 774 Bronson Ave - Water Boundary Conditions

Thanks Josh,

You are correct, a bit of a miscommunication between Adam and I on the proposed connections to the municipal system. Let me know if you get any updating timing for the new watermain within Bronson Ave. In the meantime, can we proceed with the boundary conditions request assuming a dual connection to the Cambridge Street watermain as per the approved servicing plan?

Thanks,

Steve Merrick, EIT.
Project Coordinator / Junior Designer

DSEL

david schaeffer engineering ltd.

120 Iber Road, Unit 103 Stittsville, ON K2S 1E9

phone: (613) 836-0856 ext. 561

cell: (613) 222-7816 email: smerrick@DSEL.ca

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From: White, Joshua [mailto:Joshua.White@ottawa.ca]

Sent: November-09-15 2:55 PM

To: 'Steve Merrick' < smerrick@dsel.ca <a href="mailto:cc: Vu, John < John. Wu@ottawa.ca">wu, John < John. Wu@ottawa.ca wu, John < John. Wu @ottawa.ca wu, John < John < John < John wu, John < John wu, John < John wu, John <a href="mailt

Subject: RE: 774 Bronson Ave - Water Boundary Conditions

Hey Steve,

I will go through my email and check and see if we heard back from public works. It should be noted that the previous approval <u>did not</u> contemplate a connection into the 600 mm water main on Bronson as it is a back bone water main. In the previous approval the site would be serviced off of Cambridge entirely with a new connection into Bronson when the new local water main is installed during the future reconstruction of Bronson.

Josh

Joshua White, P.Eng.
Project Manager, Infrastructure Approvals
Development Review, Urban Services, City of Ottawa
Please consider the environment before printing this e-mail.



City of Ottawa | Ville d'Ottawa 613.580.2424 ext./poste 15843 Email: joshua.white@ottawa.ca

ottawa.ca/planning / ottawa.ca/urbanisme

From: Steve Merrick [mailto:smerrick@dsel.ca]
Sent: Monday, November 09, 2015 1:14 PM

To: White, Joshua; Wu, John

Subject: RE: 774 Bronson Ave - Water Boundary Conditions

Hi John & Josh,

I don't believe we received boundary conditions based on the correspondence below. There have been updates to the site plan that have led to a decrease in total demand as shown below:

| | L/min | L/s |
|------------|-------|------|
| Avg. Daily | 48.6 | 0.81 |
| Max Day | 145.4 | 2.42 |
| Peak Hour | 218.2 | 3.64 |

Please use the above demands and the connection points and assumptions as discussed below to provide boundary conditions for the subject site.

Thanks,

Steve Merrick, EIT.
Project Coordinator / Junior Designer

DSEL

david schaeffer engineering ltd.

120 Iber Road, Unit 103 Stittsville, ON K2S 1E9

phone: (613) 836-0856 ext. 561

cell: (613) 222-7816 email: smerrick@DSEL.ca

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From: Steve Merrick [mailto:smerrick@dsel.ca]

Sent: August-26-15 2:29 PM

To: White, Joshua (Joshua.White@ottawa.ca) < Joshua.White@ottawa.ca>; 'Wu, John' < John.Wu@ottawa.ca>

Subject: 774 Bronson Ave - Water Boundary Conditions

Hi John,

This job has been previously submitted and approved by Josh White back in October 2013. The lands have since changed hands and the site plan has been modified since our last submission. We are starting by preparing a serviceability letter for the client and hope that in Josh's absence you could forward on a boundary condition request

for this site. We are hoping to provide the client with the serviceability letter by the end of the week and hope you can forward this on to the water resources group as soon as possible for their analysis.

The approved plans contemplated a looped water connection to the existing 600mm watermain within Bronson Avenue and the existing 200mm watermain on Cambridge Street. The proposed water service will be achieved by the same way, see attached sketch

I have summarized the development water demands below:

| | L/min | L/s |
|------------|-------|------|
| Avg. Daily | 55.0 | 0.92 |
| Max Day | 163.6 | 2.73 |
| Peak Hour | 245.8 | 4.10 |

As the plan is still in the preliminary concept phase, we don't have a calculated FUS and will require available fire flow @ 20 psi.



Thanks in advance!

Steve Merrick, EIT. Project Coordinator / Junior Designer

DSEL

david schaeffer engineering ltd.

120 Iber Road, Unit 103 Stittsville, ON K2S 1E9

phone: (613) 836-0856 ext. 561

fax: (613) 836-7183 email: smerrick@DSEL.ca

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774 Bronson Avenue Samcon **Existing Conditions**

Wastewater Design Flows per Unit Count City of Ottawa Sewer Design Guidelines, 2004



Site Area 0.18 ha

Extraneous Flow Allowances

Infiltration / Inflow* 0.00 L/s

*Additional flow due to infiltration is taken into account in stormwater calculations

| _ | | _ | | |
|--------|------|------|-------|--------|
| I IAMA | CtIC | 1.0n | tribi | utions |
| | | | | |

| Unit Type | Unit Rate | Units | Pop |
|--------------------------|-----------|-----------|-----|
| Single Family | 3.4 | | 0 |
| Semi-detached and duplex | 2.7 | | 0 |
| Townhouse | 2.7 | | 0 |
| Stacked Townhouse | 2.3 | | 0 |
| Apartment | | | |
| Bachelor | 1.4 | | 0 |
| 1 Bedroom | 1.4 | | 0 |
| 2 Bedroom | 2.1 | | 0 |
| 3 Bedroom | 3.1 | | 0 |
| Average | 1.8 | 154 | 278 |
| | | Total Pop | 278 |

Total Pop

Average Domestic Flow 1.13 L/s

> **Peaking Factor** 4.00

Peak Domestic Flow 4.50 L/s

Institutional / Commercial / Industrial Contributions

| Property Type | Unit | Rate | No. of Units | Avg Wastewater (L/s) |
|-------------------------|--------|---------------------|--------------|----------------------|
| Commercial floor space* | 5 | L/m ² /d | 804 | 0.09 |
| Institutional | 5 | L/m ² /d | | 0.00 |
| Hospitals | 900 | L/bed/d | | 0.00 |
| School | 70 | L/student/d | | 0.00 |
| Industrial - Light** | 35,000 | L/gross ha/d | | 0.00 |
| Industrial - Heavy** | 55,000 | L/gross ha/d | | 0.00 |

| 0.09 |
|------|
| |
| 0.14 |
| 0.00 |
| 0.14 |
| |

^{*} assuming a 12 hour commercial operation

^{**} peak industrial flow per City of Ottawa Sewer Design Guidelines Appendix 4B

| Total Estimated Average Dry Weather Flow Rate | 1.22 L/s |
|---|----------|
| Total Estimated Peak Dry Weather Flow Rate | 4.64 L/s |
| Total Estimated Peak Wet Weather Flow Rate | 4.64 L/s |

774 Bronson Avenue Samcon Existing Conditions

Wastewater Design Flows per Unit Count City of Ottawa Sewer Design Guidelines, 2004



Site Area 0.19 ha

Extraneous Flow Allowances

Infiltration / Inflow* 0.00 L/s

*Additional flow due to infiltration is taken into account in stormwater calculations

| _ | | | _ | | •• | |
|------|----|------|---|-----|-----|---------|
| - 11 | Λm | Act: | • | ۱nt | rıh | ons |
| | | | | | | |

| Unit Type | Unit Rate | Units | Pop |
|--------------------------|-----------|-----------|-----|
| Single Family | 3.4 | | 0 |
| Semi-detached and duplex | 2.7 | | 0 |
| Townhouse | 2.7 | | 0 |
| Stacked Townhouse | 2.3 | | 0 |
| Apartment | | | |
| Bachelor | 1.4 | | 0 |
| 1 Bedroom | 1.4 | | 0 |
| 2 Bedroom | 2.1 | | 0 |
| 3 Bedroom | 3.1 | | 0 |
| Average | 1.8 | 39 | 71 |
| | | Total Pop | 71 |
| | | - | |

Average Domestic Flow 0.29 L/s

Peaking Factor 4.00

Peak Domestic Flow 1.15 L/s

Institutional / Commercial / Industrial Contributions

| Property Type | Unit | Rate | No. of Units | Avg Wastewater (L/s) |
|-------------------------|--------|---------------------|--------------|----------------------|
| Commercial floor space* | 5 | L/m ² /d | | 0.00 |
| Institutional | 5 | L/m ² /d | | 0.00 |
| Hospitals | 900 | L/bed/d | | 0.00 |
| School | 70 | L/student/d | | 0.00 |
| Industrial - Light** | 35,000 | L/gross ha/d | | 0.00 |
| Industrial - Heavy** | 55,000 | L/gross ha/d | | 0.00 |

| Average I/C/I Flow | 0.00 |
|--------------------------------------|------|
| Peak Institutional / Commercial Flow | 0.00 |
| Peak Industrial Flow** | 0.00 |
| Peak I/C/I Flow | 0.00 |

^{*} assuming a 12 hour commercial operation

^{**} peak industrial flow per City of Ottawa Sewer Design Guidelines Appendix 4B

| Total Estimated Average Dry Weather Flow Rate | 0.29 L/s |
|---|----------|
| Total Estimated Peak Dry Weather Flow Rate | 1.15 L/s |
| Total Estimated Peak Wet Weather Flow Rate | 1.15 L/s |

Wastewater Design Flows per Unit Count City of Ottawa Sewer Design Guidelines, 2012



Site Area 0.37 ha

Extraneous Flow Allowances

Infiltration / Inflow* 0.00 L/s

*Additional flow due to infiltration is taken into account in stormwater calculations

| _ | | _ | | | |
|--------|------|-------|-------|--------|--|
| I IAMA | CtIC | (·) | ntrih | utions | |
| | | | | | |

| Domestic Contributions | | | |
|--------------------------|-------------|-------------|----------|
| Unit Type | Unit Rate | Units | Pop |
| Single Family | 3.4 | | 0 |
| Semi-detached and duplex | 2.7 | | 0 |
| Townhouse | 2.7 | | 0 |
| Stacked Townhouse | 2.3 | | 0 |
| Apartment | | | |
| Bachelor | 1.4 | | 0 |
| 1 Bedroom | 1.4 | | 0 |
| 2 Bedroom | 2.1 | | 0 |
| 3 Bedroom | 3.1 | | 0 |
| Average | 1.8 | | 0 |
| Type of Housing | Per/Bed | Beds | Pop |
| Boarding* | 1 | 341 | 341 |
| | | Total Pop | 341 |
| | Average Dor | nestic Flow | 0.79 L/s |
| | Pea | king Factor | 4.00 |
| | Peak Dor | nestic Flow | 3.16 L/s |
| | | | |

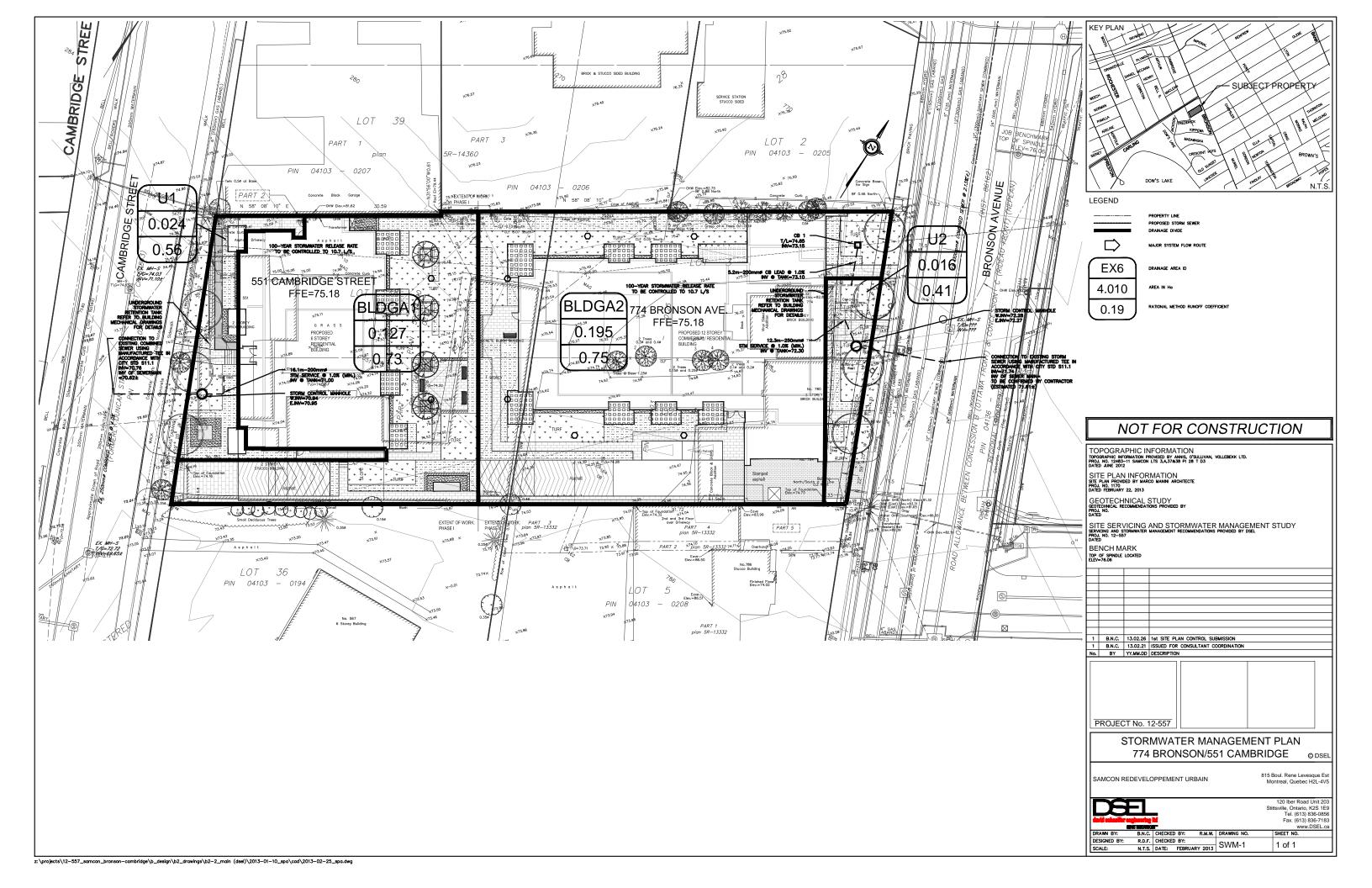
Institutional / Commercial / Industrial Contributions

| Property Type | Unit | | No. of Units | Avg Wastewater (L/s) |
|--------------------------|----------|---------------------|------------------|----------------------|
| Commercial floor space** | 5 | L/m ² /d | 136 | 0.02 |
| Industrial - Light** | 35,000 | L/gross ha/d | | 0.00 |
| Industrial - Heavy** | 55,000 | L/gross ha/d | | 0.00 |
| | | Ave | erage I/C/I Flow | 0.02 |
| | Peak In: | stitutional / Co | mmercial Flow | 0.02 |
| | | Peak In | dustrial Flow** | 0.00 |
| | | | Peak I/C/I Flow | 0.02 |

^{*} assuming a 12 hour commercial operation

^{**} peak industrial flow per City of Ottawa Sewer Design Guidelines Appendix 4B

| Total Estimated Average Dry Weather Flow Rate | 0.81 L/s |
|---|----------|
| Total Estimated Peak Dry Weather Flow Rate | 3.18 L/s |
| Total Estimated Peak Wet Weather Flow Rate | 3.18 L/s |



774 Bronson Avenue Samcon **Proposed Conditions**

Stormwater - Proposed Development City of Ottawa Sewer Design Guidelines, 2004



Target Flow Rate

Area 0.19 ha

0.40 Rational Method runoff coefficient

20.0 min

2-year

52.0 mm/hr Q 10.7 L/s

Estimated Post Development Peak Flow from Unattenuated Areas

Area ID: U2

Total Area 0.02 ha

0.41 Rational Method runoff coefficient

| | | 5-year | | | | | 100-year | | | | |
|---|----------------|---------|---------------------|----------------------|---------------------|---------------------|----------|-----------------|----------------------|---------------------|---------------------|
| ĺ | t _c | i | Q _{actual} | Q _{release} | Q _{stored} | V_{stored} | i | Q actual | Q _{release} | Q _{stored} | V_{stored} |
| | (min) | (mm/hr) | (L/s) | (L/s) | (L/s) | (m³) | (mm/hr) | (L/s) | (L/s) | (L/s) | (m³) |
| | 10.0 | 104.2 | 1.9 | 1.9 | 0.0 | 0.0 | 178.6 | 4.1 | 4.1 | 0.0 | 0.0 |

Estimated Post Development Peak Flow from Attenuated Areas

Area ID: A2

Total Area

0.75 Rational Method runoff coefficient

| | 5-year | | | | | 100-year | | | | |
|----------------|---------|---------------------|----------------------|---------------------|---------------------|----------|-----------------|----------------------|---------------------|---------------------|
| t _c | i | Q _{actual} | Q _{release} | Q _{stored} | V _{stored} | i | Q actual | Q _{release} | Q _{stored} | V _{stored} |
| (min) | (mm/hr) | (L/s) | (L/s) | (L/s) | (m³) | (mm/hr) | (L/s) | (L/s) | (L/s) | (m³) |
| 10 | 104.2 | 42.3 | 3.1 | 39.2 | 23.5 | 178.6 | 90.7 | 6.7 | 84.0 | 50.4 |
| 15 | 83.6 | 33.9 | 3.1 | 30.8 | 27.7 | 142.9 | 72.6 | 6.7 | 65.9 | 59.3 |
| 20 | 70.3 | 28.5 | 3.1 | 25.4 | 30.5 | 120.0 | 60.9 | 6.7 | 54.2 | 65.1 |
| 25 | 60.9 | 24.7 | 3.1 | 21.6 | 32.4 | 103.8 | 52.7 | 6.7 | 46.1 | 69.1 |
| 30 | 53.9 | 21.9 | 3.1 | 18.8 | 33.8 | 91.9 | 46.7 | 6.7 | 40.0 | 72.0 |
| 35 | 48.5 | 19.7 | 3.1 | 16.6 | 34.8 | 82.6 | 41.9 | 6.7 | 35.3 | 74.1 |
| 40 | 44.2 | 17.9 | 3.1 | 14.8 | 35.6 | 75.1 | 38.2 | 6.7 | 31.5 | 75.6 |
| 45 | 40.6 | 16.5 | 3.1 | 13.4 | 36.1 | 69.1 | 35.1 | 6.7 | 28.4 | 76.7 |
| 50 | 37.7 | 15.3 | 3.1 | 12.2 | 36.5 | 64.0 | 32.5 | 6.7 | 25.8 | 77.4 |
| 55 | 35.1 | 14.3 | 3.1 | 11.1 | 36.7 | 59.6 | 30.3 | 6.7 | 23.6 | 77.9 |
| 60 | 32.9 | 13.4 | 3.1 | 10.2 | 36.9 | 55.9 | 28.4 | 6.7 | 21.7 | 78.2 |
| 65 | 31.0 | 12.6 | 3.1 | 9.5 | 36.9 | 52.6 | 26.7 | 6.7 | 20.1 | 78.3 |
| 70 | 29.4 | 11.9 | 3.1 | 8.8 | 36.9 | 49.8 | 25.3 | 6.7 | 18.6 | 78.2 |
| 75 | 27.9 | 11.3 | 3.1 | 8.2 | 36.8 | 47.3 | 24.0 | 6.7 | 17.3 | 78.0 |
| 80 | 26.6 | 10.8 | 3.1 | 7.6 | 36.7 | 45.0 | 22.8 | 6.7 | 16.2 | 77.7 |
| 85 | 25.4 | 10.3 | 3.2 | 7.2 | 36.5 | 43.0 | 21.8 | 6.7 | 15.1 | 77.2 |
| 90 | 24.3 | 9.9 | 3.2 | 6.7 | 36.3 | 41.1 | 20.9 | 6.7 | 14.2 | 76.7 |
| 95 | 23.3 | 9.5 | 3.2 | 6.3 | 36.0 | 39.4 | 20.0 | 6.7 | 13.4 | 76.1 |
| 100 | 22.4 | 9.1 | 3.2 | 5.9 | 35.7 | 37.9 | 19.2 | 6.7 | 12.6 | 75.5 |
| 105 | 21.6 | 8.8 | 3.2 | 5.6 | 35.4 | 36.5 | 18.5 | 6.7 | 11.9 | 74.8 |
| 110 | 20.8 | 8.5 | 3.2 | 5.3 | 35.0 | 35.2 | 17.9 | 6.7 | 11.2 | 74.0 |

100-year Q_{attenuated} 6.67 L/s 3.15 L/s 5-year Q_{attenuated} 36.9 m³ 78.3 m³ 5-year Max. Storage Required 100-year Max. Storage Required

Summary of Release Rates and Storage Volumes

| Control Area | 5-Year Release Rate (L/s) | 5-Year Storage (m³) | 100-Year Release Rate (L/s) | 100-Year Storage (m³) |
|--------------------|------------------------------------|---------------------------|--------------------------------------|-----------------------------|
| Unattenuated Areas | 1.9 | 0.0 | 4.1 | 0.0 |
| Attenutated Areas | 3.1 | 36.9 | 6.7 | 78.3 |
| Total | 5.0 | 36.9 | 10.7 | 78.3 |

551 Cambridge Street Samcon **Proposed Conditions**

Stormwater - Proposed Development City of Ottawa Sewer Design Guidelines, 2004



Target Flow Rate

Area 0.19 ha

С 0.40 Rational Method runoff coefficient

20.0 min

2-year

52.0 mm/hr Q 10.7 L/s

Estimated Post Development Peak Flow from Unattenuated Areas

Area ID: U1

Total Area 0.02 ha

0.56 Rational Method runoff coefficient

| | 5-year | | | | | 100-year | | | | |
|----------------|---------|---------------------|----------------------|---------------------|---------------------|----------|---------------------|----------------------|---------------------|---------------------|
| t _c | i | Q _{actual} | Q _{release} | Q _{stored} | V_{stored} | i | Q _{actual} | Q _{release} | Q _{stored} | V _{stored} |
| (min) | (mm/hr) | (L/s) | (L/s) | (L/s) | (m³) | (mm/hr) | (L/s) | (L/s) | (L/s) | (m³) |
| 10.0 | 104.2 | 3.6 | 3.6 | 0.0 | 0.0 | 178.6 | 7.6 | 7.6 | 0.0 | 0.0 |

Estimated Post Development Peak Flow from Attenuated Areas

Area ID: A1

Total Area

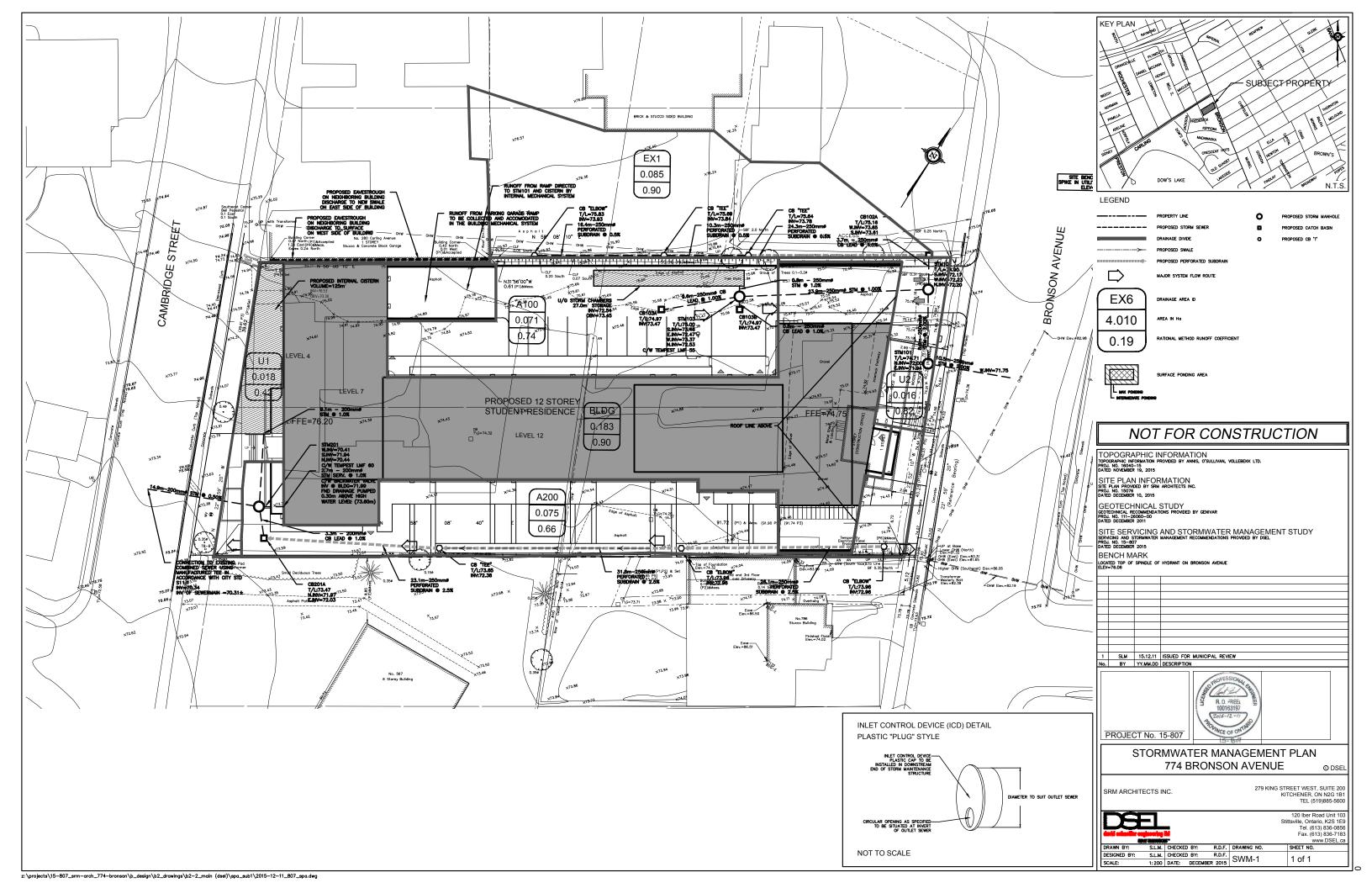
0.73 Rational Method runoff coefficient

| | 5-year | | | | | 100-year | | | | |
|----------------|---------|---------------------|----------------------|---------------------|---------------------|----------|-----------------|----------------------|---------------------|---------------------|
| t _c | i | Q _{actual} | Q _{release} | Q _{stored} | V_{stored} | i | Q actual | Q _{release} | Q _{stored} | V _{stored} |
| (min) | (mm/hr) | (L/s) | (L/s) | (L/s) | (m³) | (mm/hr) | (L/s) | (L/s) | (L/s) | (m³) |
| 10 | 104.2 | 26.8 | 1.4 | 25.4 | 15.2 | 178.6 | 57.5 | 3.1 | 54.4 | 32.6 |
| 15 | 83.6 | 21.5 | 1.4 | 20.1 | 18.1 | 142.9 | 46.0 | 3.1 | 42.9 | 38.6 |
| 20 | 70.3 | 18.1 | 1.4 | 16.6 | 20.0 | 120.0 | 38.6 | 3.1 | 35.5 | 42.6 |
| 25 | 60.9 | 15.7 | 1.4 | 14.2 | 21.4 | 103.8 | 33.4 | 3.1 | 30.3 | 45.5 |
| 30 | 53.9 | 13.9 | 1.4 | 12.4 | 22.4 | 91.9 | 29.6 | 3.1 | 26.5 | 47.7 |
| 35 | 48.5 | 12.5 | 1.4 | 11.0 | 23.2 | 82.6 | 26.6 | 3.1 | 23.5 | 49.4 |
| 40 | 44.2 | 11.4 | 1.4 | 9.9 | 23.8 | 75.1 | 24.2 | 3.1 | 21.1 | 50.7 |
| 45 | 40.6 | 10.5 | 1.4 | 9.0 | 24.3 | 69.1 | 22.2 | 3.1 | 19.1 | 51.7 |
| 50 | 37.7 | 9.7 | 1.5 | 8.2 | 24.7 | 64.0 | 20.6 | 3.1 | 17.5 | 52.5 |
| 55 | 35.1 | 9.0 | 1.5 | 7.6 | 25.1 | 59.6 | 19.2 | 3.1 | 16.1 | 53.2 |
| 60 | 32.9 | 8.5 | 1.5 | 7.0 | 25.3 | 55.9 | 18.0 | 3.1 | 14.9 | 53.7 |
| 65 | 31.0 | 8.0 | 1.5 | 6.5 | 25.5 | 52.6 | 16.9 | 3.1 | 13.9 | 54.1 |
| 70 | 29.4 | 7.6 | 1.5 | 6.1 | 25.7 | 49.8 | 16.0 | 3.1 | 12.9 | 54.4 |
| 75 | 27.9 | 7.2 | 1.5 | 5.7 | 25.8 | 47.3 | 15.2 | 3.1 | 12.1 | 54.6 |
| 80 | 26.6 | 6.8 | 1.5 | 5.4 | 25.9 | 45.0 | 14.5 | 3.1 | 11.4 | 54.7 |
| 85 | 25.4 | 6.5 | 1.5 | 5.1 | 25.9 | 43.0 | 13.8 | 3.1 | 10.7 | 54.8 |
| 90 | 24.3 | 6.3 | 1.5 | 4.8 | 25.9 | 41.1 | 13.2 | 3.1 | 10.2 | 54.8 |
| 95 | 23.3 | 6.0 | 1.5 | 4.5 | 25.9 | 39.4 | 12.7 | 3.1 | 9.6 | 54.8 |
| 100 | 22.4 | 5.8 | 1.5 | 4.3 | 25.9 | 37.9 | 12.2 | 3.1 | 9.1 | 54.7 |
| 105 | 21.6 | 5.6 | 1.5 | 4.1 | 25.8 | 36.5 | 11.7 | 3.1 | 8.7 | 54.6 |
| 110 | 20.8 | 5.4 | 1.5 | 3.9 | 25.8 | 35.2 | 11.3 | 3.1 | 8.3 | 54.5 |

3.08 L/s 1.46 L/s 100-year Q_{attenuated} 5-year Q_{attenuated} 25.9 m³ 54.8 m³ 5-year Max. Storage Required 100-year Max. Storage Required

Summary of Release Rates and Storage Volumes

| Control Area | 5-Year Release Rate (L/s) | 5-Year Storage (m³) | 100-Year Release Rate (L/s) | 100-Year Storage (m³) |
|--------------------|------------------------------------|---------------------------|--------------------------------------|-----------------------------|
| Unattenuated Areas | 3.6 | 0.0 | 7.6 | 0.0 |
| Attenutated Areas | 1.5 | 25.9 | 3.1 | 54.8 |
| Total | 5.0 | 25.9 | 10.7 | 54.8 |



SRM Architects 774 Bronson Stormwater to Bronson

Stormwater - Proposed Development City of Ottawa Sewer Design Guidelines, 2012

DSEL

Target Flow Rate

Area 0.1900 ha

C 0.40 Rational Method runoff coefficient

t_c 20.0 min

2 year

i 52.0 mm/hr

Q 11.0 L/s

Estimated Post Development Peak Flow from Unattenuated Areas

Total Area 0.02 ha

C 0.82 Rational Method runoff coefficient

| | 5-year | | | | | 100-year | | | | | | |
|----------------|---------|---------------------|----------------------|---------------------|---------------------|----------|---------------------|----------------------|---------------------|---------------------|--|--|
| t _c | i | Q _{actual} | Q _{release} | Q _{stored} | V_{stored} | i | Q _{actual} | Q _{release} | Q _{stored} | V_{stored} | | |
| (min) | (mm/hr) | (L/s) | (L/s) | (L/s) | (m³) | (mm/hr) | (L/s) | (L/s) | (L/s) | (m³) | | |
| 10.0 | 104.2 | 3.8 | 3.8 | 0.0 | 0.0 | 178.6 | 7.9 | 7.9 | 0.0 | 0.0 | | |

Note:

C value for the 100-year storm is increased by 25%, to a maximum of 1.0 per Ottawa Sewer Design Guidelines (5.4.5.2.1)

Contributions to Building Cistern

Total Area 0.071 ha

0.74 Rational Method runoff coefficient

| | 5-year | | | | | 100-year | | | | |
|----------------|---------|---------------------|----------------------|---------------------|---------------------|----------|---------------------|----------------------|---------------------|---------------------|
| t _c | i | Q _{actual} | Q _{release} | Q _{stored} | V _{stored} | i | Q _{actual} | Q _{release} | Q _{stored} | V _{stored} |
| (min) | (mm/hr) | (L/s) | (L/s) | (L/s) | (m³) | (mm/hr) | (L/s) | (L/s) | (L/s) | (m³) |
| 10 | 104.2 | 15.2 | 1.3 | 13.9 | 8.3 | 178.6 | 32.6 | 2.8 | 29.8 | 17.9 |
| 20 | 70.3 | 10.3 | 1.3 | 8.9 | 10.7 | 120.0 | 21.9 | 2.8 | 19.1 | 22.9 |
| 30 | 53.9 | 7.9 | 1.3 | 6.6 | 11.8 | 91.9 | 16.8 | 2.8 | 14.0 | 25.2 |
| 40 | 44.2 | 6.4 | 1.3 | 5.1 | 12.3 | 75.1 | 13.7 | 2.8 | 10.9 | 26.3 |
| 50 | 37.7 | 5.5 | 1.3 | 4.2 | 12.6 | 64.0 | 11.7 | 2.8 | 8.9 | 26.7 |
| 60 | 32.9 | 4.8 | 1.3 | 3.5 | 12.6 | 55.9 | 10.2 | 2.8 | 7.4 | 26.7 |
| 70 | 29.4 | 4.3 | 1.3 | 3.0 | 12.5 | 49.8 | 9.1 | 2.8 | 6.3 | 26.5 |
| 80 | 26.6 | 3.9 | 1.3 | 2.6 | 12.3 | 45.0 | 8.2 | 2.8 | 5.4 | 26.1 |
| 90 | 24.3 | 3.5 | 1.3 | 2.2 | 12.1 | 41.1 | 7.5 | 2.8 | 4.7 | 25.5 |
| 100 | 22.4 | 3.3 | 1.3 | 2.0 | 11.8 | 37.9 | 6.9 | 2.8 | 4.1 | 24.9 |
| 110 | 20.8 | 3.0 | 1.3 | 1.7 | 11.4 | 35.2 | 6.4 | 2.8 | 3.7 | 24.1 |
| 120 | 19.5 | 2.8 | 1.3 | 1.5 | 11.1 | 32.9 | 6.0 | 2.8 | 3.2 | 23.3 |
| 130 | 18.3 | 2.7 | 1.3 | 1.4 | 10.6 | 30.9 | 5.6 | 2.8 | 2.9 | 22.4 |
| 140 | 17.3 | 2.5 | 1.3 | 1.2 | 10.2 | 29.2 | 5.3 | 2.8 | 2.5 | 21.4 |
| 150 | 16.4 | 2.4 | 1.3 | 1.1 | 9.7 | 27.6 | 5.0 | 2.8 | 2.3 | 20.4 |
| 160 | 15.6 | 2.3 | 1.3 | 1.0 | 9.3 | 26.2 | 4.8 | 2.8 | 2.0 | 19.4 |
| 170 | 14.8 | 2.2 | 1.3 | 0.9 | 8.8 | 25.0 | 4.6 | 2.8 | 1.8 | 18.3 |
| 180 | 14.2 | 2.1 | 1.3 | 0.8 | 8.3 | 23.9 | 4.4 | 2.8 | 1.6 | 17.2 |
| 190 | 13.6 | 2.0 | 1.3 | 0.7 | 7.7 | 22.9 | 4.2 | 2.8 | 1.4 | 16.1 |
| 200 | 13.0 | 1.9 | 1.3 | 0.6 | 7.2 | 22.0 | 4.0 | 2.8 | 1.2 | 14.9 |
| 210 | 12.6 | 1.8 | 1.3 | 0.5 | 6.6 | 21.1 | 3.9 | 2.8 | 1.1 | 13.7 |

5-year Q_{attenuated} 5-year Max. Storage Required Storage Elevation 1.3 L/s 12.6 m³ 72.94 m 100-year Q_{attenuated} 00-year Max. Storage Required Storage Elevation 2.8 L/s 26.7 m³ 73.44 m

SRM Architects 774 Bronson Stormwater to Bronson

Total Available Storage

T/L

| Stage | Α | A h _o | | ٧ | V _{acc} | Q _{release} | |
|-------|------|------------------|------|-------|------------------|----------------------|--|
| (m) | (m²) | (m) | (m) | (m³) | (m³) | (L/s) | |
| 72.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.0 | 0.0 | |
| 73.45 | 0.00 | 0.96 | 0.96 | 27.00 | 27.0 | 2.8 | |

Orifice Loc STM103 LMF

55

Summary of Release Rates and Storage Volumes

| Control Area | 5-Year | 5-Year | 100-Year | 100-Year |
|--------------|---------|-------------------|----------|-------------------|
| | Release | Storage | Release | Storage |
| | Rate | | Rate | |
| | (L/s) | (m ³) | (L/s) | (m ³) |
| Unattenuated | 3.8 | 0.0 | 7.9 | 0.0 |
| Areas | | | | |
| Attenutated | 1.3 | 12.6 | 2.8 | 26.7 |
| Areas | | | | |
| Total | 5.1 | 12.6 | 10.7 | 26.7 |

SRM Architects Inc. 774 Bronson Stormwater to Cambridge

Stormwater - Proposed Development City of Ottawa Sewer Design Guidelines, 2012



Target Flow Rate

Area 0.1900 ha

C 0.40 Rational Method runoff coefficient

t_c 20.0 min

2 year

i 52.0 mm/hrQ 11.0 L/s

Estimated Post Development Peak Flow from Unattenuated Areas

Total Area 0.02 ha

C 0.43 Rational Method runoff coefficient

| | | 5-year | | | | | 100-year | | | | | | |
|---|----------------|---------|---------------------|----------------------|---------------------|---------------------|----------|---------------------|----------------------|---------------------|---------------------|--|--|
| | t _c | i | Q _{actual} | Q _{release} | Q _{stored} | V_{stored} | i | Q _{actual} | Q _{release} | Q _{stored} | V_{stored} | | |
| l | (min) | (mm/hr) | (L/s) | (L/s) | (L/s) | (m³) | (mm/hr) | (L/s) | (L/s) | (L/s) | (m³) | | |
| ſ | 10.0 | 104.2 | 2.2 | 2.2 | 0.0 | 0.0 | 178.6 | 4.8 | 4.8 | 0.0 | 0.0 | | |

Note:

C value for the 100-year storm is increased by 25%, to a maximum of 1.0 per Ottawa Sewer Design Guidelines (5.4.5.2.1)

Estimated Post Development Peak Flow from Attenuated Areas

Area ID: A200

Total Area 0.072

C 0.66

Area ID: BLDG

Total Area 0.184

C 0.90

Total Area 0.256 ha

C 0.83 Rational Method runoff coefficient

| | 5-year | | | | | 100-year | | | | |
|----------------|---------|---------------------|----------------------|---------------------|---------------------|----------|---------------------|----------------------|---------------------|---------------------|
| t _c | i | Q _{actual} | Q _{release} | Q _{stored} | V_{stored} | i | Q _{actual} | Q _{release} | Q _{stored} | V_{stored} |
| (min) | (mm/hr) | (L/s) | (L/s) | (L/s) | (m³) | (mm/hr) | (L/s) | (L/s) | (L/s) | (m³) |
| 10 | 104.2 | 61.7 | 2.7 | 59.0 | 35.4 | 178.6 | 127.0 | 5.5 | 121.4 | 72.9 |
| 20 | 70.3 | 41.6 | 2.7 | 38.9 | 46.6 | 120.0 | 85.3 | 5.5 | 79.8 | 95.7 |
| 30 | 53.9 | 31.9 | 2.7 | 29.2 | 52.6 | 91.9 | 65.3 | 5.5 | 59.8 | 107.6 |
| 40 | 44.2 | 26.2 | 2.7 | 23.4 | 56.2 | 75.1 | 53.4 | 5.5 | 47.9 | 114.9 |
| 50 | 37.7 | 22.3 | 2.7 | 19.6 | 58.7 | 64.0 | 45.5 | 5.5 | 39.9 | 119.8 |
| 60 | 32.9 | 19.5 | 2.7 | 16.8 | 60.4 | 55.9 | 39.7 | 5.5 | 34.2 | 123.1 |
| 70 | 29.4 | 17.4 | 2.7 | 14.7 | 61.6 | 49.8 | 35.4 | 5.5 | 29.9 | 125.4 |
| 80 | 26.6 | 15.7 | 2.7 | 13.0 | 62.4 | 45.0 | 32.0 | 5.5 | 26.5 | 127.0 |
| 90 | 24.3 | 14.4 | 2.7 | 11.6 | 62.9 | 41.1 | 29.2 | 5.5 | 23.7 | 127.9 |
| 100 | 22.4 | 13.3 | 2.7 | 10.5 | 63.2 | 37.9 | 27.0 | 5.5 | 21.4 | 128.5 |
| 110 | 20.8 | 12.3 | 2.7 | 9.6 | 63.3 | 35.2 | 25.0 | 5.5 | 19.5 | 128.6 |
| 120 | 19.5 | 11.5 | 2.7 | 8.8 | 63.3 | 32.9 | 23.4 | 5.5 | 17.9 | 128.5 |
| 130 | 18.3 | 10.8 | 2.7 | 8.1 | 63.2 | 30.9 | 22.0 | 5.5 | 16.4 | 128.2 |
| 140 | 17.3 | 10.2 | 2.7 | 7.5 | 62.9 | 29.2 | 20.7 | 5.5 | 15.2 | 127.6 |
| 150 | 16.4 | 9.7 | 2.7 | 7.0 | 62.6 | 27.6 | 19.6 | 5.5 | 14.1 | 126.8 |
| 160 | 15.6 | 9.2 | 2.7 | 6.5 | 62.2 | 26.2 | 18.7 | 5.5 | 13.1 | 125.9 |
| 170 | 14.8 | 8.8 | 2.7 | 6.1 | 61.7 | 25.0 | 17.8 | 5.5 | 12.2 | 124.9 |
| 180 | 14.2 | 8.4 | 2.7 | 5.7 | 61.2 | 23.9 | 17.0 | 5.5 | 11.5 | 123.7 |
| 190 | 13.6 | 8.0 | 2.7 | 5.3 | 60.6 | 22.9 | 16.3 | 5.5 | 10.7 | 122.5 |
| 200 | 13.0 | 7.7 | 2.7 | 5.0 | 60.0 | 22.0 | 15.6 | 5.5 | 10.1 | 121.1 |
| 210 | 12.6 | 7.4 | 2.7 | 4.7 | 59.3 | 21.1 | 15.0 | 5.5 | 9.5 | 119.6 |

5-year Q_{attenuated} 2.7 L/s 100-year Q_{attenuated} 5.5 L/s
5-year Max. Storage Required 63.3 m³ 00-year Max. Storage Required 128.6 m³
Storage Elevation 71.82 m Storage Elevation 73.27 m

SRM Architects Inc. 774 Bronson Stormwater to Cambridge

Total Available Storage

T/L

| Stage | Α | h_o | delta d | ٧ | V_{acc} | Q _{release} |
|-------|------|-------|---------|--------|-----------|----------------------|
| (m) | (m²) | (m) | (m) | (m³) | (m³) | (L/s) |
| 70.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.0 | 0.0 |
| 73.30 | 0.00 | 2.89 | 2.89 | 130.00 | 130.0 | 5.6 |

60

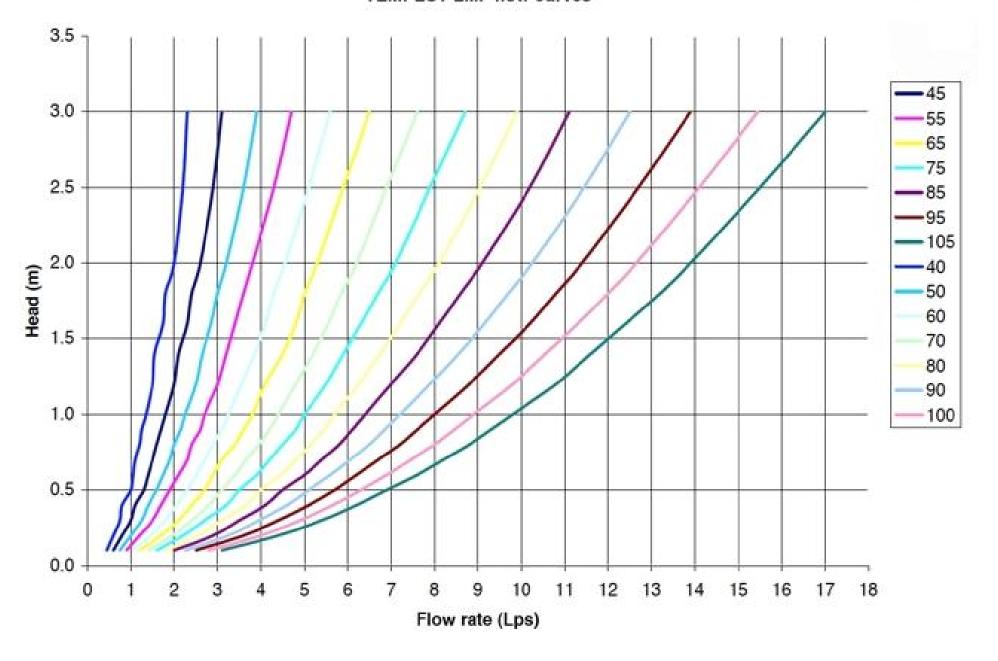
Orifice Location STM201 LMF

Summary of Release Rates and Storage Volumes

| Control Area | 5-Year Release Rate | 5-Year Storage | 100-Year Release | 100-Year Storage |
|---------------|------------------------|-------------------|---------------------|---------------------|
| | (L/s) | (m ³) | Rate (L/s) | (m³) |
| Lingttonuctod | ` ' | | , , | |
| Unattenuated | 2.2 | 0.0 | 4.8 | 0.0 |
| Areas | | | | |
| Attenutated | 2.7 | 63.3 | 5.5 | 128.6 |
| Areas | | | | |
| Total | 5.0 | 63.3 | 10.3 | 128.6 |

| | | | | | | | | | | | | | S | ewer Data | | | | |
|----------|---------|-----------|-------|------|-----------|---------|----------------|---------|-------|------|-------|--------|------------------------|-----------|----------|-------|-----------|----------|
| Area ID | Up | Down | Area | С | Indiv AxC | Acc AxC | T _C | I | Q | DIA | Slope | Length | A _{hydraulic} | R | Velocity | Qcap | Time Flow | Q/Q full |
| | | | (ha) | (-) | | | (min) | (mm/hr) | (L/s) | (mm) | (%) | (m) | (m²) | (m) | (m/s) | (L/s) | (min) | (-) |
| TO BRONS | SON AVE | | | | | | | | | | | | | | | | | |
| A100 | STM103 | STM102 | 0.071 | 0.74 | 0.05 | 0.05 | 10.0 | 104.2 | 15.2 | 250 | 1.00 | 23.9 | 0.049 | 0.063 | 1.21 | 59.5 | 0.3 | 0.26 |
| | | | | | | | | | | | | | | | | | | |
| EX1 | CB102A | STM102 | 0.085 | 0.90 | 0.08 | 0.13 | 10.0 | 104.2 | 37.3 | 250 | 1.00 | 3.7 | 0.049 | 0.063 | 1.21 | 59.5 | 0.1 | 0.63 |
| | | | | | | | | | | | | | | | | | | |
| | STM102 | STM101 | 0.000 | 0.00 | 0.00 | 0.18 | 10.3 | 102.5 | 51.7 | 250 | 2.00 | 8.6 | 0.049 | 0.063 | 1.71 | 84.1 | 0.1 | 0.61 |
| | STM101 | EX. CMBMH | 0.000 | 0.00 | 0.00 | 0.18 | 10.4 | 102.1 | 51.5 | 250 | 2.00 | 10.5 | 0.049 | 0.063 | 1.71 | 84.1 | 0.1 | 0.61 |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |

TEMPEST LMF flow curves



of Chambers long: 18 # of rows: 1

Actual Trench Length: 17.597 M Actual Trench Width: 2.108 M

Field Diagram

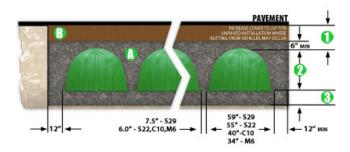


Chamber Type



Dimensions 59" x 36" x 35" (WxHxL) 1498.6mm x 914.4mm x 889mm **Weight** 32 lbs / 14.5 kg **Bare Chamber Storage** 29 ft³ / 0.82 m³

Project Results



- 1 Total Cover Over Chambers: 45.72 cm
- W Height of Chamber: 91.44 cm
- 6 Embedment Stone Under Chambers: 15.24 cm
- 1 Volume of Embedment Stone Required: 29 Cu. M
- 10 Volume of Fill Material Required: 11 Cu. M

Total Storage Provided: 27.4 Cu. M
Type of Distribution Chambers: S-29
of Distribution Chambers Required: 18
of end caps required: 4
Type of header row chambers required: S-29
of header row chambers required: 2

12/10/2015 See the advanatges of the Tritonsws products over Stormtech, Cultec, Contech, Kingstar, Atlantis, GEOlight, JFC and Hydrologic Products

Floors: 0
Bins: 0
Dumpsters: 0

Required Bed Size: 37.1 Sq. M
Volume of Embedment Stone Required: 29.65 Cu. M
Volume of Fill Material Required: 11.31 Cu. M
Volume of Excavation: 56.54 Cu. M
Area of Filter Fabric: 85.15 Sq. M

of Chambers long: 18 # of rows: 1

Actual Trench Length: 17.597 M Actual Trench Width: 2.108 M





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