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IRON VALLEY 2

5331 Fernbank Road

Site Servicing Report

Prepared for: Claridge Homes

Engineering excellence.

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IRON VALLEY 2
5331 Fernbank Road
OTTAWA, ONTARIO
Site Servicing Report

Prepared By:

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Revised: February 17, 2022
Revised: November 14, 2025
Revised: March 18, 2026
Revised: June 25, 2026

Novatech File: 121011
Ref: R-2021-079

June 25, 2026

City of Ottawa
Planning and Infrastructure Approvals
110 Laurier Street West, 4th Floor
Ottawa, ON, K1P 1J1

Attention: Rubina Rasool

**Reference: Iron Valley 2 - 5331 Fernbank Road
Site Servicing Report
Our File No.: 121011
City File No.: D07-12-25-0151**

Please find enclosed for your review the revised Site Servicing Report including the hydraulic network analysis and stormwater management for the Iron Valley 2 (formerly Fernbank Zens) development at 5331 Fernbank Road. The site is bounded by Cope Drive to the north, the existing SOHO development to the east, Fernbank Road to the south and Terry Fox Drive to the west.

This report addresses the approach to site servicing (sanitary/storm/watermain) and to stormwater management for the subject property. Also, the included hydraulic analysis examines the proposed water distribution system as it relates to the existing infrastructure and future watermain distribution. This report demonstrates that the site servicing and stormwater management can be achieved and that the proposed water distribution system can provide adequate system pressures for servicing and fire protection purposes throughout the development.

This site has previously received Site Plan Approval. Due to the redesign of this development, this Site Servicing Report is submitted in support of the engineering detailed design for the Claridge Homes site plan application resubmission. The enclosed Site Servicing Report has been revised to address comments received from the City of Ottawa dated May 19, 2026.

Trusting this report is adequate for your purposes. Should you have any questions, or require additional information pertaining to the enclosed report, please contact us.

Yours truly,

NOVATECH



Drew Blair, P. Eng.
Senior Project Manager

Cc Marc St. Pierre, Claridge Homes

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121011-GP1	General Plan of Services
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121011-PR	Plan and Profile
121011-GR1	Grading Plan
121011-GR2	Grading Plan
121011-SAN	Sanitary Drainage Areas Plan
121011-STM	Storm Drainage Areas Plan

1.0 INTRODUCTION

This Site Servicing Report was prepared as part of the engineering detailed design for the Iron Valley 2 (formerly Fernbank Zens) residential development at 5331 Fernbank Road (Subject Site).

1.1 Site Description

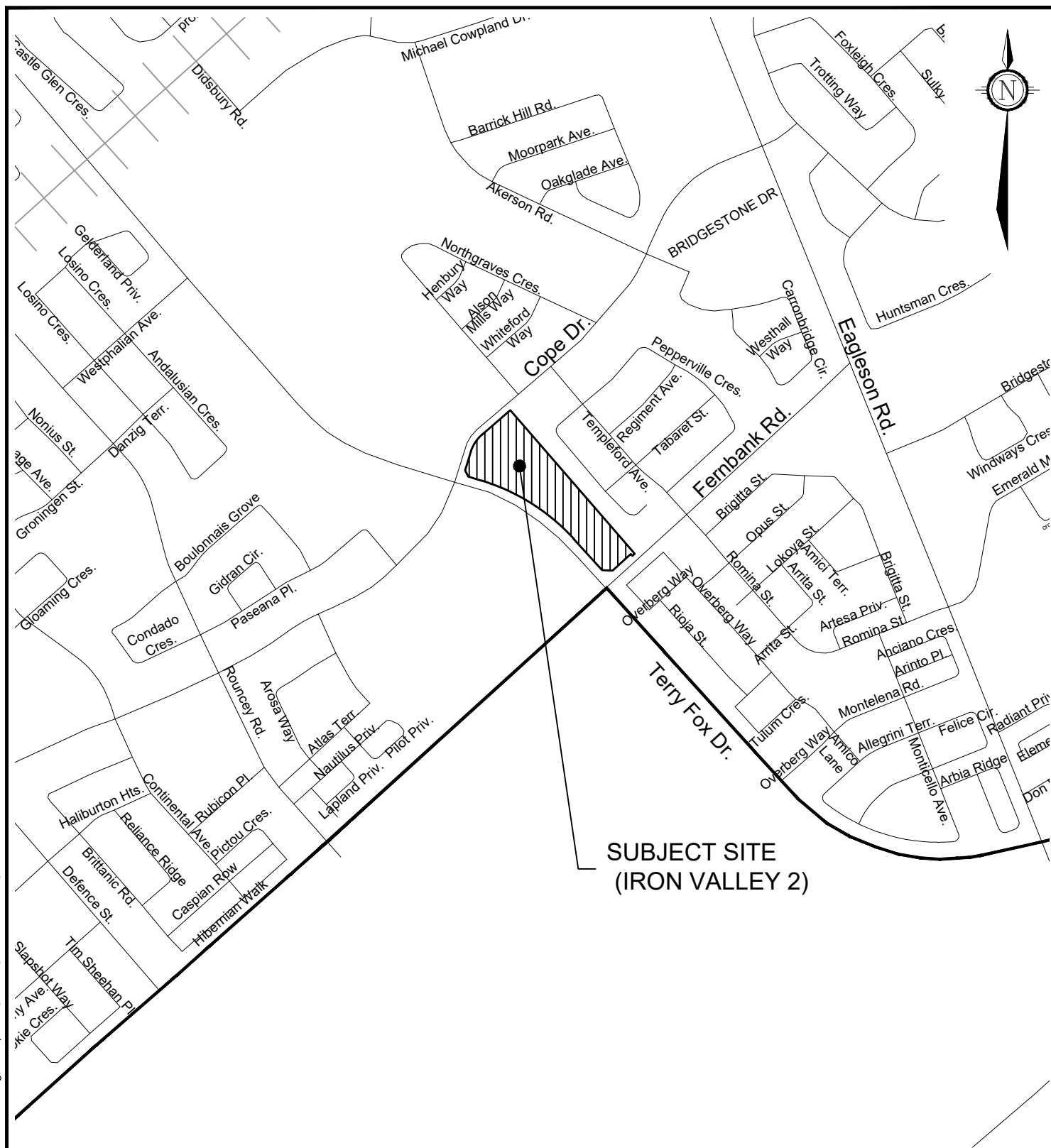
The proposed Iron Valley 2 development (**approximately 3.70 ha**) is owned by Claridge Homes and located within the City of Ottawa. The Subject Site is bounded by Cope Drive to the north, the existing SOHO development to the east, Fernbank Road to the south and Terry Fox Drive to the west as shown on **Figure 1A/1B – Key Plan**.

The legal description of the property is designated as Part of Lot 30 Concession 10, Goulbourn, Part 1 Plan 4R17373, Except Part 4, Plan 4R20112; Ottawa. Subject to an Easement in Favour of Hydro Ottawa Limited Over Parts 5,6, 7, 8 and 9 Plan 4R20112 as in OC455206. Road Allowance Between Lots 30 and 31 Concession 10, Goulbourn Lying Between Parts 3 and 4 on 4R17373 and Part 2 on Plan 4R20112, as Closed by N599928; Ottawa. Part of Lot 31, Concession 10, Goulbourn, Part 1 on Plan 4R19334 City of Ottawa.

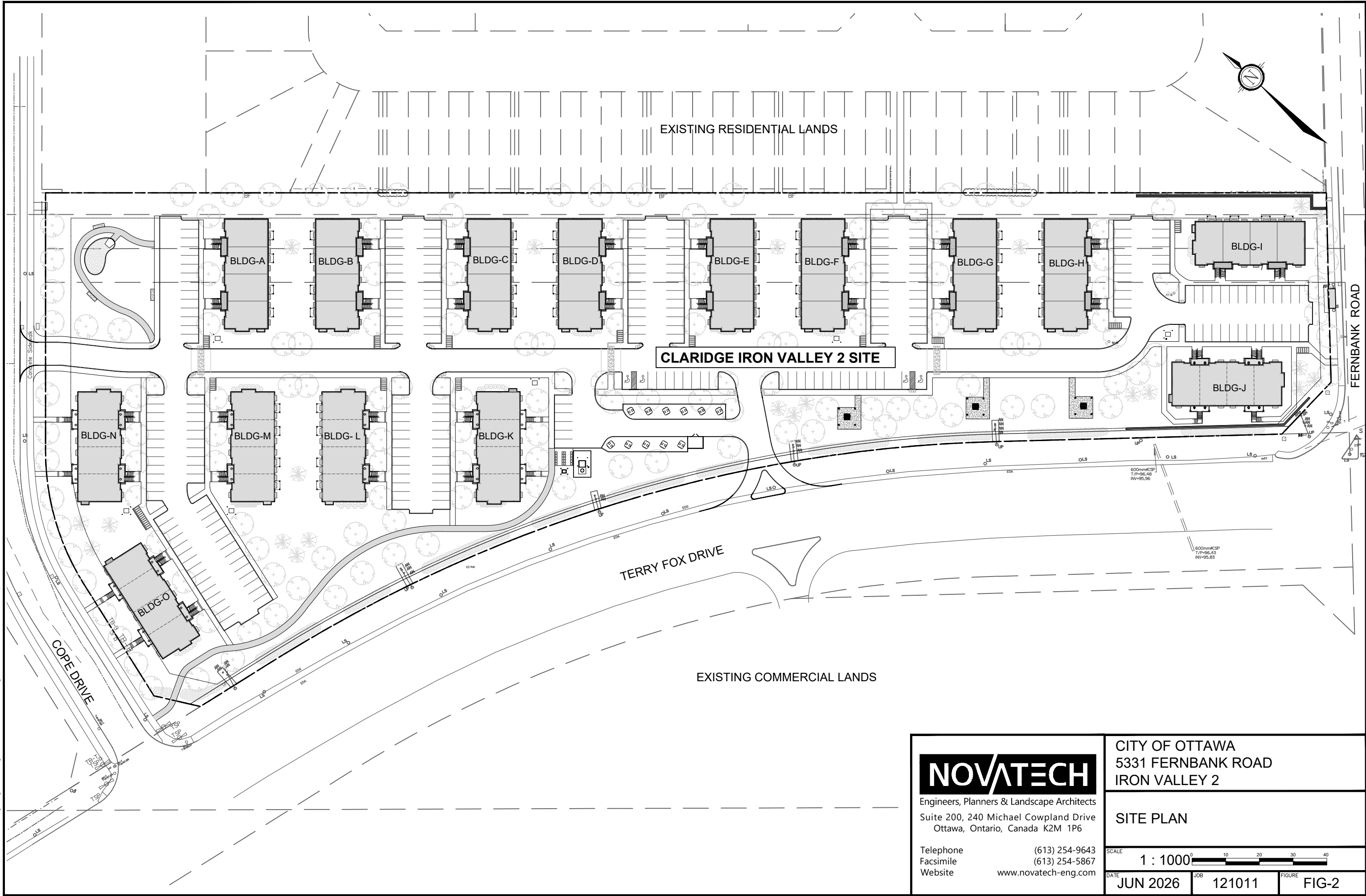
The Subject Site is proposed to be developed as a residential development which will consist of 180 apartment units within 15 buildings (12 units per building), on-site parking and private local roadways with access from Cope Drive and Terry Fox Drive as shown on **Figure 2 – Site Plan**. The existing lands are presently vacant but were previously occupied by farmland as shown on **Figure 3 – Existing Conditions**.

Figure 1A – Key Plan





M:\2021\121011\CAD\Design\Figures\Design Brief\121011-FIG2.dwg, FIG2, Jun 25, 2026 - 12:02pm, smatthews



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CITY OF OTTAWA
5331 FERNBANK ROAD
IRON VALLEY 2

SITE PLAN

SCALE 1 : 1000

DATE JUN 2026 JOB 121011 FIGURE FIG-2

1.2 Planning Context

The subject property is designated General Urban Area in the City of Ottawa Official Plan. General Urban Areas are generally areas of commercial, industrial or medium and high-density residential housing. The proposed development conforms to these policies of the Official Plan.

The Subject Site is currently zoned *General Mixed Use – GM* and subject to Urban Exception number 2411 under the *City of Ottawa's Zoning By-law 2008-250*. The purpose of the *General Mixed Use – GM* is to:

1. *allow residential, commercial and institutional uses, or mixed-use development in the **General Urban Area** and in the Upper Town, Lowertown and Sandy Hill West Character Areas of the Central Area designations of the Official Plan;*
2. *limit commercial uses to individual occupancies or in groupings in well-defined areas such that they do not affect the development of the designated Traditional and Arterial Mainstreets as viable mixed-use areas;*
3. *permit uses that are often large and serve or draw from broader areas than the surrounding community and which may generate traffic, noise or other impacts provided the anticipated impacts are adequately mitigated or otherwise addressed; and*
4. *impose development standards that will ensure that the uses are compatible and complement surrounding land uses.*

The proposed development of a low-density apartment building is a permitted land use within the *General Mixed Use – GM* zone. The building has been designed to be compliant with the standards of the *General Mixed-Use Zone*, and the residential nature of the building is compatible with the surrounding properties.

1.3 Referenced Guidelines

This report has been prepared in accordance with the City of Ottawa Servicing Study Guidelines for Development Applications, the Water Distribution Design Guidelines (July 2010), the MOE Design Guidelines for Drinking-Water Systems (2008), the Ottawa Sewer Design Guidelines (October 2012) and all associated Technical Bulletins issued by the City of Ottawa.

1.4 Additional Reports

This Site Servicing Report provides information on the considerations and approach by which Novatech Engineering Consultants Ltd. has designed and evaluated the proposed servicing system for the Subject Site. This report should be read in conjunction with the following:

- 1) *Geotechnical Investigation – Proposed Residential Development, 5331 Fernbank Road, Ottawa, Ontario, Paterson Group Inc., November 18, 2025. Report No. PG5683-1;*
- 2) *Serviceability Report – Cavanaugh Construction Ltd. / Karam SOHO West – Rev 3, Stantec Consulting Ltd., October 31, 2007;*
- 3) *Cavanaugh Construction – Soho West (Phase 1 and 2), Kanata South, City of Ottawa Stormwater Management Report, Stantec Consulting Ltd. October 31, 2007;*
- 4) *Monahan Drain Constructed Wetlands – Updated Hydrologic and Hydraulic Analysis, City of Ottawa, J.F. Sabourin and Associates Inc (JFSA), March, 2019;*
- 5) *Servicing and Stormwater Management Brief - Van Gaal Lands 5331 Fernbank Road and 1039 Terry Fox Drive, Novatech Engineers, Planners & Landscape Architects, September 1, 2015;*
- 6) *Van Gaal Lands Claridge Developments — 1039 Terry Fox Drive and 5331 Fernbank Road – Site Serviceability and Stormwater Management Report, Novatech, October 2022.*

1.5 Consultations and Approvals

The Subject Site is located upstream of the approved Phase 1 of the Trailwest (formerly SOHO West) Subdivision. The SOHO West Serviceability Report, *SOHO West- Rev. 3, Serviceability Report, Prepared by Stantec, dated October 31st, 2007*, calculated sanitary and stormwater flows to outlet to Cope Drive from the land that makes up 5331 Fernbank Road.

The Ministry of the Environment (MOE) and the Rideau Valley Conservation Authority (RVCA) have been consulted regarding the proposed development.

2.0 PRE-DEVELOPMENT CONDITIONS

2.1 Site Description & Existing Conditions

The proposed Iron Valley 2 development is approximately 3.70 hectares, is currently undeveloped and comprised of former agricultural lands that are currently fallow. The northwest portion of the site has been developed for use as a site trailer and loading bay for the Subject Site. There is access to the site via Cope Drive to the north and Terry Fox Drive to the west. For more details see **Figure 3** – Existing Conditions Plan.

2.2 Existing Drainage

Under existing conditions, the site grading is relatively flat with sheet drainage to an existing ditch to the west along Terry Fox Drive and an existing ditch along the old Hazeldean Side Road on the east side of the parcel. These ditches eventually convey flows to the Monahan Municipal Drain to the north and east of the site.

2.3 Geotechnical Investigation

Paterson Group conducted a geotechnical review in support of the proposed residential development on the Claridge Homes Lands. The findings of this investigation are documented in their report titled *Geotechnical Investigation – Proposed Residential Development, 5331 Fernbank Road*.

The field program for the current geotechnical investigation was carried out in February 2021. It consisted of advancing five (5) boreholes to a maximum depth of 6.7m below ground surface. Previous field investigations were completed by Paterson for the subject site in January 2018 and May 2006. A total of 9 boreholes were advanced to a maximum depth of 14.6 m during the previous investigations. The principal findings are summarized as follows:

- A surficial layer of topsoil of thickness from 0.19m to 0.36m for all boreholes except boreholes BH1-18, BH7-18 and BH8-18. These boreholes had a layer of fill of thickness 0.53m, 0.48m and 0.33m respectively consisting of crushed stone with silt and sand.
- An interbedded brown silty sand with stiff brown clayey silt to silty clay of thickness 1.2m to 3.7m was encountered below the topsoil.
- The brown silty sand with stiff brown clayey silt to silty clay layer is underlain with a deep deposit of firm grey silty clay with some sand of thickness 3.8m to 11.9m.
- Based on geological mapping, the bedrock in this area is part of the Gull River formation, which consists of interbedded limestone and dolomite with an overburden drift thickness ranging between 25 to 50 m.
- Groundwater inflow was observed in test pits. Based on these observations, the long-term groundwater level is expected to be between 1.5 to 2.5 m depth.

- Atterberg limits testing was completed for recovered silty clay samples at selected locations throughout the subject site. Grain size distribution and hydrometer testing was also completed on selected soil samples.
- Based on the results of the Atterberg limit testing mentioned above, the plasticity index was found to be less than 40% in all the tested clay samples. In addition, based on the clay content found in the clay samples from the grain size distribution test results, moisture levels and consistency, the silty clay across the subject site is considered low to medium sensitivity clay and should not be designated as sensitive marine clays.
- The permissible grade raise recommendation for finished grading within 6 m of a building footprint is 1.5 m and the permissible grade raise restriction for finished grading along access lanes and parking lots is 2.0 m.
- Expanded Polystyrene (EPS) geofoam may be used for this site within the porches and garages if the proposed grade raise is greater than allowed.

The report provides engineering guidelines based on Paterson Group's interpretation of the borehole information and project requirements. Refer to the final Geotechnical Report dated November 18, 2025, by Paterson Group for complete details.

3.0 STORMWATER MANAGEMENT

The post-development storm sewer and stormwater management system has been designed in accordance with the Ottawa Sewer Design Guidelines and will adhere to previously established release rates for this area.

3.1 Background Information (Trailwest Subdivision / Monahan Drain Cell 1)

The Subject Site are tributary to the existing storm sewer on Cope Drive, which was designed by Stantec (2007) as part of Phase 1 of the Trailwest (formerly SOHO West) Subdivision. The Fernbank Zens Lands were included in the overall storm drainage design and is represented as subcatchment FUT-13B. Refer to Drawing OSD – Overall Storm Drainage Area Plan, SOHO – Kanata South (Rev. 7), Stantec (February 25, 2009), provided in **Appendix A**.

3.2 Stormwater Management Criteria

SOHO (Trailwest) Subdivision (Stantec, 2007)

As part of the overall storm drainage design for the SOHO Subdivision, storm runoff from the Iron Valley II Lands (catchment FUT13-B) was allocated to MH1013 on Cope Drive based on the following parameters:

Drainage Area Parameters

- Area ID = FUT-13B
- Drainage Area = 3.73 ha
- Runoff Coefficient = 0.65
- Allowable Release Rate = 85 L/s/ha

The stormwater management model for the SOHO subdivision assigned the following stormwater management criteria to catchment FUT-13B:

- Minor system release rate = 317 L/s (85 L/s/ha x 3.73 ha)
- Major system storage = 60 m³/ha
- 100-year Major system release rate = 781 L/s

J.F Sabourin and Associates completed an updated hydrologic and hydraulic assessment of the Monahan Drain SWM Facility which provided an updated 100-year boundary condition of 95.05m at MH1013 in Cope Drive. Excerpts from these reports are provided in **Appendix A**.

3.3 Existing and Proposed Storm Infrastructure

The proposed development will be serviced by approximately 1,175m of storm sewers ranging from 250mm to 825mm in diameter. The minor system outlet is an existing 1200mm x 1800mm concrete box storm sewer at MH1013 on Cope Drive, which runs through the Trailwest Subdivision and conveys runoff to a Vortech hydrodynamic separator for water quality treatment before discharging to Cell 1 of the Monahan Drain. The proposed storm layout can be seen on **Figure 4 – Storm Alignment**.

3.3.1 Minor System (Storm Sewers)

Storm servicing for the Iron Valley 2 development will be provided using a dual-drainage system. Runoff from frequent events will be conveyed by the proposed storm sewers (minor system), while flows from large storm events that exceed the capacity of the minor system will be stored on the surface in road sags and/or conveyed overland along defined overland flow routes (major system).

Storm Sewer Design Criteria

The following is the storm sewer design criteria based on the City of Ottawa Sewer Design Guidelines (Oct. 2025):

- Rational Method (Q) = $2.78CIA$, where
 - Q = peak flow (L/s)
 - C = runoff coefficient
 - $C = (0.70 * \%Imp.) + 0.20$
 - I = rainfall intensity for a 2-year return period (mm/hr)
 - $I_{2yr} = 732.951 / [(Tc(min) + 6.199)]^{0.810}$
 - A = site area (ha)
- Minimum Pipe Size = 250 mm; Minimum / Maximum Full Flow Velocity = 0.8 m/s / 3.0 m/s

The on-site storm sewers will be sized to convey the peak flows corresponding to a 2-year return period storm event. Refer to the storm sewer design sheets provided in **Appendix A**.

Inlet Control Devices

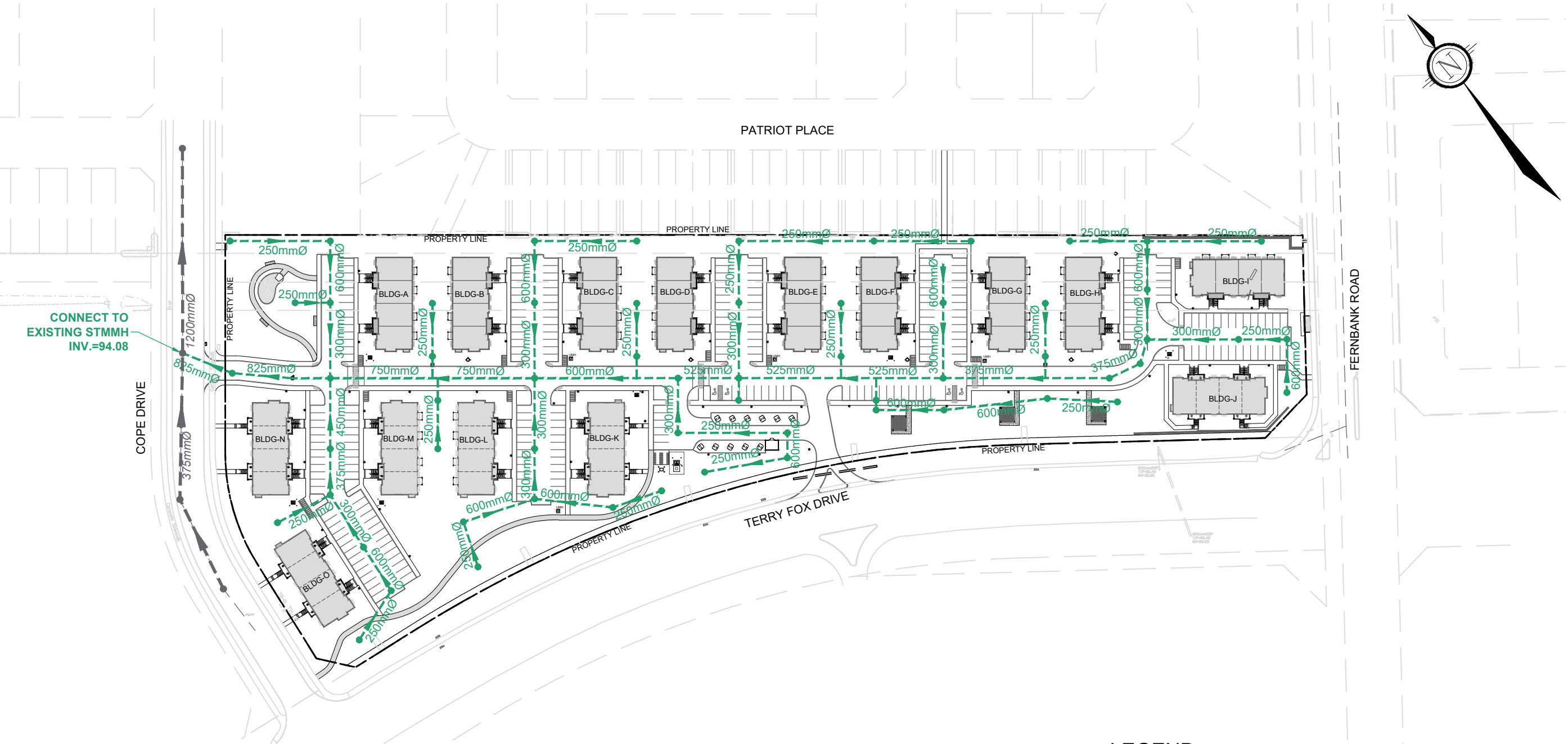
Inlet control devices (ICDs) will be used to restrict inflows to the minor system. ICDs will be sized to control minor system peak flows to the Cope Drive storm sewer to the allowable release rate of 317 L/s.

The uncontrolled flows directed overland have been accounted for as part of the major system design.

Hydraulic Grade Line

The storm sewers will be designed to ensure the hydraulic grade line (HGL) elevation for a 100-year storm event will provide a minimum 0.30 m clearance from the underside of footing (USF) elevation where the buildings are directly connected to the storm sewers.

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LEGEND

- SITE BOUNDARY
- PROPOSED STORM SEWER C/W
FLOW DIRECTION
- EXISTING STORM SEWER C/W
FLOW DIRECTION



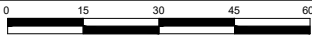
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CITY OF OTTAWA
5331 FERNBANK ROAD
IRON VALLEY 2

STORM ALIGNMENT

1 : 1500



JUN 2026

121011

FIG4-STM

3.3.2 Major System (Overland Flow)

Under post-development conditions, the majority of the site will be graded to provide an overland flow path to convey major system runoff towards Cope Drive. The uncontrolled areas have been graded to direct flows overland to either the adjacent Fernbank Road ROW or Terry Fox Drive ROW. Refer to the Grading Plans (Drawing 121011-GR1 and GR2).

Major System (Overland Flow) Criteria

Runoff from storms that exceed the minor system capacity are to be stored or conveyed overland within the right-of-way and/or defined drainage easements. The following overland flow criteria from the OSDG will be applied to the design:

- Ensure that major system flows have a maximum dynamic depth of 0.35 m (static ponding + dynamic flow) during the 100-year event.
- Ensure the product of velocity x depth does not exceed 0.60 during the 100-year event.

The major system will be evaluated using a hydraulic model to ensure that the maximum total flow depth (static + dynamic) will be restricted to 0.35 m during the 100-year storm event; and water levels will not touch the building envelope / lowest opening during the Stress Test event (100-year +20%).

3.4 Proposed Stormwater Management Strategy

Stormwater Quality Control

The existing Vortech unit immediately upstream the outlet to Cell 1 of the Monahan Drain Constructed Wetlands has been designed to provide an Enhanced level of water quality control for the contributing drainage area, including the Iron Valley 2 Site. The proposed site layout has a slightly smaller drainage area and runoff coefficient than was used to size the Vortech unit, and as such will provide the required level of water quality treatment – refer to **Table 3.1**.

Table 3.1: Vortech Sizing Criteria (Iron Valley 2)

Design	Catchment ID	Parameters	Description
Stantec (2007)	FUT-13B	3.73 ha, C = 0.65	Area to Cope Drive / Vortechics Unit
Novatech (2026)	A1-A32	3.34 ha, C = 0.48	Area to Cope Drive / Vortechics Unit
	U1-U5	0.35 ha, C = 0.40	Uncontrolled Areas
	TOTAL	3.65 ha, C = 0.45	Total Drainage Area (Controlled + Uncontrolled)

Stormwater Quantity Control

Surface/Underground storage will be provided within the road sags/parking areas/oversized underground storage pipes, based on the minimum major system storage requirement of 60 m³/ha taken from the downstream Trailwest (SOHO West) approved design by Stantec.

The Cope Drive storm sewer and Cell 1 of the Monahan Drain Constructed Wetlands have been designed to accommodate post-development runoff from the site based on a contributing drainage area of 3.73 ha and a runoff coefficient of C = 0.65. The proposed development has a total drainage area of 3.65 ha and a runoff coefficient of C = 0.45. Therefore, there will be no increase in runoff volume to the Monahan Drain from the 2007 Stantec design and the 2019 J.F Sabourin review.

3.4.1 Stormwater Management Model Development

The PCSWMM model has been developed to account for both minor and major system flows from the development and ensure no adverse impacts on the downstream watercourses and wetland areas. The results of the analysis were used to:

- Determine the total major and minor system runoff from the site;
- Size the ICDs for each inlet to the storm sewer system;
- Calculate the storm sewer hydraulic grade line for the 100-year storm event;
- Evaluate overland flow depths and ponding volumes during the 100-year event; and
- Ensure no ponding occurs during the 2-year storm event.

3.4.2 PCSWMM Model Parameters

Design Storms

The model includes the following design storms based on the City of Ottawa IDF data presented in the City of Ottawa Sewer Design Guidelines (October 2025). The 24-hour SCS storm distribution was provided by JFSA and was used for the analysis of the Monahan Drain.

- 3-hour Chicago Storm Distribution (10-minute time step)
- 24-hour SCS Storm Distribution from JFSA (12-minute time step)

The 3-hour Chicago storm distribution includes the 2-year, 5-year, 100-year, and 100-year (+20%) return periods while the 24-hour SCS storm distribution includes only the 100-year return period.

PCSWMM Model Schematics, Output Data and Modeling Files

PCSWMM model schematics and output data for the 100-year 3-hour Chicago and 100-year 24-hour SCS (JFSA) storm distributions are provided in **Appendix A**. The PCSWMM modeling files are provided electronically as part of the submission package.

Subcatchment Areas / Runoff Coefficients

- For modeling purposes, the site has been divided into subcatchments based on the drainage areas tributary to each inlet of the proposed storm sewer system. The catchment areas are shown on the Storm Drainage Area Plans (**121011-STM**). Refer to the Grading Plans (**121011-GR1 and GR2**) and the General Plan of Services (**121011-GP1 and GP2**) for the location of high points and low points, and the storm sewer layout, respectively.
- The weighted runoff coefficients and percent impervious values are provided in **Appendix A**. As per the City of Ottawa Sewer Design Guidelines (October 2012), the percent impervious values are based on the following equation:

$$\% \text{ Imp.} = (C - 0.20) / 0.7$$

The hydrologic parameters for each subcatchment were developed based on the Grading Plans and the Storm Drainage Area Plans. An overview of the drainage area parameters is provided in **Table 3.2**.

Table 3.2: Hydrologic Model Parameters

Area ID	Catchment Area (ha)	Runoff Coeff. (C)	Percent Imperv. (%)	No Depression (%)	Flow Path Length (m)	Equivalent Width (m)	Average Slope (%)
Controlled Areas							
A01	0.03	0.25	7	47	11	28	3.7
A02	0.13	0.62	59	37	20	66	1.9
A03	0.12	0.30	14	100	13	94	3.0
A04	0.13	0.58	54	27	19	68	2.3
A05	0.07	0.39	28	100	12	58	3.7
A06	0.19	0.25	8	0	19	99	2.6
A07	0.08	0.63	62	8	24	34	1.2
A08	0.15	0.59	56	36	19	78	1.9
A09	0.07	0.39	28	100	12	57	3.7
A10	0.11	0.29	13	100	12	91	2.0
A11	0.15	0.59	56	36	20	77	2.0
A12	0.11	0.63	61	9	11	100	1.0
A13	0.03	0.70	71	0	22	14	2.5
A14	0.04	0.25	7	0	7	55	2.5
A15	0.13	0.53	47	28	21	63	2.5
A16	0.05	0.30	14	25	9	56	2.5
A17	0.15	0.51	44	29	31	48	2.5
A18	0.24	0.59	55	32	19	124	2.1
A19	0.07	0.39	28	100	12	59	3.5
A20	0.1	0.29	13	100	10	96	3.0
A21	0.06	0.25	7	100	8	76	3.0
A22	0.09	0.41	29	100	16	56	3.5
A23_1	0.14	0.43	33	20	26	92	2.3
A23_2	0.10	0.43	33	20	26	92	0.5
A24	0.11	0.53	47	24	10	105	2.2
A25	0.14	0.61	58	40	18	76	3.7
A26	0.08	0.42	31	100	17	46	3.5
A27	0.15	0.26	9	8	13	120	2.5
A28	0.12	0.60	58	26	17	72	3.0
A29	0.05	0.25	7	100	12	40	1.9
A31	0.05	0.30	14	62	13	38	3.4
A32	0.10	0.29	13	16	8	120	0.5
TOTAL	3.34	0.46	37				
Uncontrolled Areas							
U1	0.09	0.30	14	100	9	103	15.0
U2	0.03	0.29	13	100	6	47	5.0
U3	0.05	0.28	12	0	3	172	15.0
U4	0.09	0.40	29	70	10	90	3.7
U5	0.05	0.40	29	100	15	33	3.7
TOTAL	0.31	0.34	20				

Depression Storage

- The default values for depression storage (1.57mm impervious / 4.67 mm pervious) have been applied to all catchments.
- The 'zero impervious' parameter (areas with no depression storage) for all catchments is based off the percentage of roof top areas to total impervious area.

Subarea Routing

- Subarea routing for all catchments draining to Cope Drive is set to 'Outlet'.

Minor System Conduits (Bend / Exit Losses)

- The minor system network was created in Civil3D and imported into PCSWMM.
- The following exit losses have been inputted into the model. They represent the loss coefficient based on the bend angle, as per the Appendix 6-B in the City of Ottawa Sewer Design Guidelines (October 2025).

<u>Bend Angle</u>	<u>Loss Coefficient</u>
0	0.00
15	0.09
30	0.21
45	0.39
60	0.64
75	0.96
90	1.32

Downstream Boundary Condition (Minor System)

- The storm sewer outlet for Iron Valley II is the existing maintenance hole (MH1013) on Cope Drive.
- The boundary condition for the storm outlet was set at the 100-year HGL elevation of the outgoing sewer (95.05m). This is based on the Sensitivity Analysis completed by JFSA. It represents an ultimate buildout condition of the vacant lands within the watershed. The boundary condition correspondence has been provided in **Appendix E**.

3.5 Minor System

Runoff from the site will be captured by the proposed on-site storm sewer network and attenuated by ICDs. Storage will be provided with a combination of underground storage (i.e. pipes / structures) and surface storage.

Inflows to the storm sewer were modeled based on the characteristics of each inlet. All the catchbasins in the roadways and parking areas are located at low points. Inflows to the storm sewer are based on the ICD specified for the inlet and the maximum depth of ponding. ICDs have been sized to limit the outlet peak flows to the allowable release rate of 317 L/s. Details are outlined as follows in **Table 3.3**. ICD information is indicated on the General Plan of Services (drawing **121011-GP1** and **GP2**).

Table 3.3: Inlet Control Devices and Design Flows

Structure ID	ICD Size & Inlet Rate					
	ICD Type	T/G (m)	Orifice Invert (m)	Max HGL (100-yr) (m)	100-year Head on Orifice (m)	100-year Orifice Peak Flow* (L/s)
CBMH1	Tempest LMF Vortex 70	96.74	94.77	97.00	2.20	6.52
CBMH2	83mm	96.84	94.86	97.11	2.21	20.84
CBMH3	83mm	97.10	94.98	97.29	2.27	21.61
CBMH4	Tempest LMF Vortex 80	97.31	95.12	97.49	2.33	8.76
CBMH5	Tempest LMF Vortex 70	97.38	95.56	97.61	2.02	6.27
CBMH8	Tempest LMF Vortex 70	96.92	94.85	97.15	2.27	6.62
CBMH10	94mm	96.86	94.85	97.02	2.12	26.10
CBMH11	83mm	97.08	94.90	97.25	2.31	21.38
CBMH13	83mm	97.23	94.91	97.38	2.43	21.99
CBMH14	Tempest LMF Vortex 70	97.23	95.09	97.39	2.27	6.61
CBMH15	Tempest LMF Vortex 70	97.50	95.35	97.66	2.28	6.64
CICB1	83mm	97.14	95.42	97.12	1.66	18.85
CICB2	83mm	97.59	96.04	97.66	1.58	18.35
RYE7	94mm	97.22	95.03	95.86	0.78	16.21
RYT13	83mm	97.17	95.59	97.30	1.67	18.90
RYT14	83mm	97.29	95.72	97.43	1.67	18.89
RYT15	83mm	97.48	95.91	97.60	1.65	18.75

*PCSWMM model results for a 3-hour Chicago storm distribution.

3.5.1 Hydraulic Grade Line (PCSWMM)

The Hydraulic Grade Line (HGL) within the storm sewer system was evaluated using the fixed HGL of 95.05 at MH 1013 on Cope Drive during the 100-year storm event. This HGL elevation surcharges the storm sewer on Cope Drive by 0.24m (obvert elevation = 94.81m).

The results of the analysis were used to ensure that a minimum freeboard of 0.30m is provided between the 100-year hydraulic gradeline (HGL) and the designed underside of footing (USF) elevations for all buildings where they are directly connected to the storm sewer. The HGL analysis confirms that all buildings will have at least 0.30m of freeboard between the modeled hydraulic gradeline and the USF elevation. The HGL elevations for a 20% increase (rainfall intensity and total precipitation) in the 100-year storm were also reviewed to ensure that the modeled HGL is below the USF.

Table 3.4 provides a summary of the 100-year HGL elevation at each storm manhole downstream of the buildings storm connections within the proposed development. The 100-year+20% HGL elevations have been provided in **Appendix A. Table 3.5** summarizes the 100-year HGL elevation at the storm manholes that are upstream of the building storm connections. The HGLs in these manholes are above the design USF due to downstream flow controls. Since these manholes are upstream of storm connections to the buildings, the high HGLs are acceptable.

Table 3.4: 100-Year Hydraulic Gradeline Elevations (Downstream of Buildings)

Manhole ID	MH Obvert Elevation (m)	T/G Elevation (m)	HGL Elevation 100yr-3hr (m)	HGL Elevation 100yr+20% (m)	Design USF (m)	Clearance from 100-yr HGL (m)
MH100	94.93	96.96	95.06	95.06	95.41	0.35
MH102	94.96	97.03	95.07	95.08	95.41	0.34
MH104	94.98	97.03	95.08	95.08	95.41	0.33
MH106	95.06	97.11	95.11	95.12	95.46	0.35
MH108	95.13	97.28	95.14	95.15	95.62	0.48
MH110	95.18	97.36	95.15	95.16	95.62	0.47
MH112	95.32	97.50	95.17	95.17	95.85	0.68
MH114	95.47	97.55	95.24	95.24	95.75	0.51
MH116	95.50	97.61	95.25	95.25	95.75	0.50
MH118	95.53	97.67	95.26	95.26	95.75	0.49
MH200	95.07	97.18	95.13	95.15	95.72	0.59

Table 3.5: 100-Year Hydraulic Gradeline Elevations (Upstream of Buildings)

Manhole ID	MH Obvert Elevation (m)	T/G Elevation (m)	HGL Elevation 100yr-3hr (m)	HGL Elevation 100yr+20% (m)	100-Year Surcharge (m)	100-Year Clearance from T/G (m)
MH202	95.48	97.39	97.15	97.17	1.67	0.24
MH204	95.53	97.13	97.13	97.15	1.50	0.10
MH206	96.08	97.76	97.67	97.70	1.59	0.09

3.5.2 Major System

The major system network was evaluated using the PCSWMM model to ensure that the overland flow depths and velocities conform to City standards. A summary of ponding depths at each inlet for the 2-year, 5-year, 100-year and 100-year (+20%) events are provided in **Appendix A**. The maximum static and dynamic ponding depths within the roadways are less than 0.35m during all events and the product of depth x velocity will be less than 0.60.

The underground and surface storage provided upstream of each ICD are represented in the model using a combination of storage curves and oversized storm sewers (**Appendix A**), which use a depth vs area relationship to represent the corresponding storage volumes at a given elevation. The storm sewers have been oversized in some areas to provide the required storage. They are installed at minimum slope however all are accessible at either end for cleaning and maintenance purposes. Access is only provided from the downstream end for conduit 209 from the proposed structure CBMH4.

Table 3.6 provides a summary of the maximum static and 100-year ponding elevation at each catchbasin manhole within the proposed development.

Table 3.6: Overland Flow Results (100-year Event)

Structure	T/G (m)	Max. Static Ponding (Spill Depth)		100-yr Event (3hr)			
		Elev. (m)	Depth (m)	Elev. (m)	Depth (m)	Cascading Flow?	Cascade Depth (m)
CBMH1	96.74	97.06	0.32	97.00	0.26	N	0.00
CBMH2	96.84	97.11	0.27	97.11	0.27	N	0.00
CBMH3	97.10	97.38	0.28	97.29	0.19	N	0.00
CBMH4	97.31	97.54	0.23	97.49	0.18	N	0.00
CBMH5	97.38	97.68	0.30	97.61	0.23	N	0.00
CBMH7	96.78	97.08	0.30	95.12	0.00	N	0.00
CBMH8	96.92	97.16	0.24	97.15	0.23	N	0.00
CBMH10	96.86	97.20	0.34	97.02	0.16	N	0.00
CBMH11	97.08	97.25	0.17	97.25	0.17	N	0.00
CBMH12	97.55	97.66	0.11	97.25	0.00	N	0.00
CBMH13	97.23	97.37	0.14	97.38	0.15	Y	0.01
CBMH14	97.23	97.34	0.11	97.39	0.16	Y	0.05
CBMH15	97.50	97.75	0.25	97.66	0.16	N	0.00
CICB1	96.99	97.11	0.12	97.12	0.13	Y	0.01
CICB2	97.44	97.64	0.20	97.66	0.22	Y	0.02

The model results demonstrate that each storage area provides sufficient underground storage to ensure no surface ponding during the 2-year design event (the 2-year HGL elevation at each structure does not exceed the corresponding top of grate elevation). An expanded table of the ponding depths at low points in the roadway and landscaped areas (including the stress-test event) is provided in **Appendix A**. Based on these results, the proposed storm drainage system will not experience any adverse flooding even with a 20% increase to the 100-year event.

3.5.3 Peak Flows (PCSWMM)

Table 3.7 provides a summary of the minor and major system flows from the Iron Valley 2 Lands to Cope Drive, Fernbank Road ROW and Terry Fox Drive ROW for all storm events up to and including the 100-year.

Table 3.7: Summary of Peak Flows (PCSWMM)

Outfall	Allowable Release Rate	2-year Peak Flow (L/s)	5-year Peak Flow (L/s)	100-year Peak Flow ⁽²⁾ (L/s)		Description
				3-hour Chicago	24-hour SCS	
Minor System	317 L/s	134	192	316	304	To Cope Drive MH1013
Major System	781 L/s	9	23	59	45	Flow to Cope Drive (OF4, OF5)
		1	5	13	10	Flow to Fernbank ROW (OF3, HP-RYE1, HP-RYE16(2))
		6	26	60	45	Flow to Terry Fox ROW (OF1, OF2)
TOTAL	1,098 L/s	150	246	448	404	

⁽²⁾ PCSWMM model results; fixed outfall at 95.05m (100-year HGL elevation at MH 1013 on Cope Drive).

The 100-year minor system peak flow to Cope Drive is controlled to the allowable release rate of 317 L/s for both the 3-hour Chicago and 24-hour SCS distributions.

The major system peak flows are significantly less than the allowable rate of 781 L/s. The PCSWMM model is based on the grading design, which provides significantly more than the required 60m³/ha of major system storage.

4.0 SANITARY SEWER SYSTEM

4.1 Background Information

The Subject Site is located upstream of Phase 1 of the Trailwest (formerly SOHO West) Subdivision. The SOHO West Serviceability Report, *SOHO West- Rev. 3, Serviceability Report, Prepared by Stantec, dated October 31st, 2007*, calculated sanitary flows to outlet to Cope Drive from the lands that make up 1039 Terry Fox Drive and 5331 Fernbank Road, which includes the Subject Site and lands north of the Monahan Drain and lands south of Cope Drive. Sanitary flows in this report were calculated to be 45.95L/s to outlet to the sanitary sewers on Cope Drive, which ultimately outlet to the Hazeldean Pump Station. Refer to **Appendix B** for excerpts.

In 2015, a rezoning application was submitted for the lands located at 5331 Fernbank Road & 1039 Terry Fox Drive. The land north of the Monahan Drain was rezoned from IP4 to IP to allow for the development of office buildings. The Subject Site was rezoned from IP4 to R3X [2410]-h to allow for residential development. And lastly, the land south of Cope Drive to Fernbank Road was rezoned from IP4 to IP with exceptions to all for commercial development. The exceptions would allow for retail store and retail food store to be permitted as secondary uses. As part of the submission a servicing and stormwater report was included titled, *Van Gaal Lands: 5331 Fernbank Road and 1039 Terry Fox Drive, Ottawa, ON, Servicing & Stormwater Management Brief, completed by Novatech, Ref. No.: R-2015-123, dated September 1, 2015*. The 2015 report comprised of two separate outlets for the sanitary flow from 1039 Terry Fox Drive and 5331 Fernbank Road.

The Subject Site and the lands south of Cope Drive outlet to the sanitary sewers on Cope Drive. A sanitary flow of 16.23L/s was calculated for the Cope Drive sanitary sewers.

The business park outlets to the existing 900mm dia. sanitary sewer along Hazeldean Side Road due to its proximity to the Hazeldean Pump Station. A sanitary flow of 25.81L/s was calculated to outlet to the Hazeldean Side Road sewer.

The total sanitary flows to the Hazeldean Pump Station were calculated to be 42.04L/s.

4.2 Existing Sanitary Sewer System

Currently, there is an existing 525mm dia. sanitary trunk sewer along Cope Drive and a 200mm dia. sanitary sewer along Northgraves Crescent to the northeast. The sanitary trunk sewer along Cope Drive currently services the existing commercial plaza located at 5357 Fernbank Road and the existing Trailwest community. The Cope Drive trunk sewer ultimately outlets to the Hazeldean Pump Station via the sanitary pipe system in the Trailwest subdivision. Through pre-consultation with the City of Ottawa for the Van Gaal lands (north of Cope Drive), the underside of footing elevations (USFs) shall be a minimum of 95.30m, which is the emergency overflow elevation at the Pump Station. These conditions should apply to the Subject Site as both developments outlet to the existing Cope Drive sanitary sewer at the same location. Please refer the **Appendix B** for correspondence regarding the minimum USF restrictions for the Subject Site.

4.3 Proposed Sanitary Sewer Outlet

It is proposed that sanitary flows from the Subject Site will outlet directly to the 525mm dia. sanitary trunk sewer along Cope Drive. The proposed outlet is consistent with the approved SOHO West Serviceability Report (Stantec, October 2007) and the approved Servicing & Stormwater Management Report (Novatech, September 2015) as part of the rezoning application for the Van Gaal Lands. Refer to Section 1.3 for report details.

The Subject Site will be serviced by a gravity sanitary sewer system, utilizing 200mm dia. sanitary pipes. Refer to **Figure 5** – Sanitary Alignment for details of the proposed sanitary sewer system.

4.4 Design Criteria

The proposed sanitary sewer system has been designed based on criteria established by the City of Ottawa in the following documents:

- Section 4.0 of the City of Ottawa Sewer Design Guidelines (October 2012).
- Technical Bulletins issued by the City of Ottawa regarding new sanitary design parameters. Design parameters listed in these technical bulletins supersede values from the City of Ottawa Sewer Design Guidelines (2012).

The resulting design parameters are summarized as follows:

Population Flow = 280 L/capita/day

Infiltration = 0.33 L/s/ha

Apartment = 2.1 persons per unit

Maximum Residential Peak Factor = 4.0

Harmon Correction Factor = 0.8

Industrial/Commercial/Institutional Peak Factor

= 1.0, if area is <20% of total contributing area

= 1.5, if area is >20% of total contributing area

Industrial Peaking Factor: As per Appendix 4-B of the City of Ottawa Sewer Design Guidelines

Minimum velocity = 0.6m/s

Manning's n = 0.013

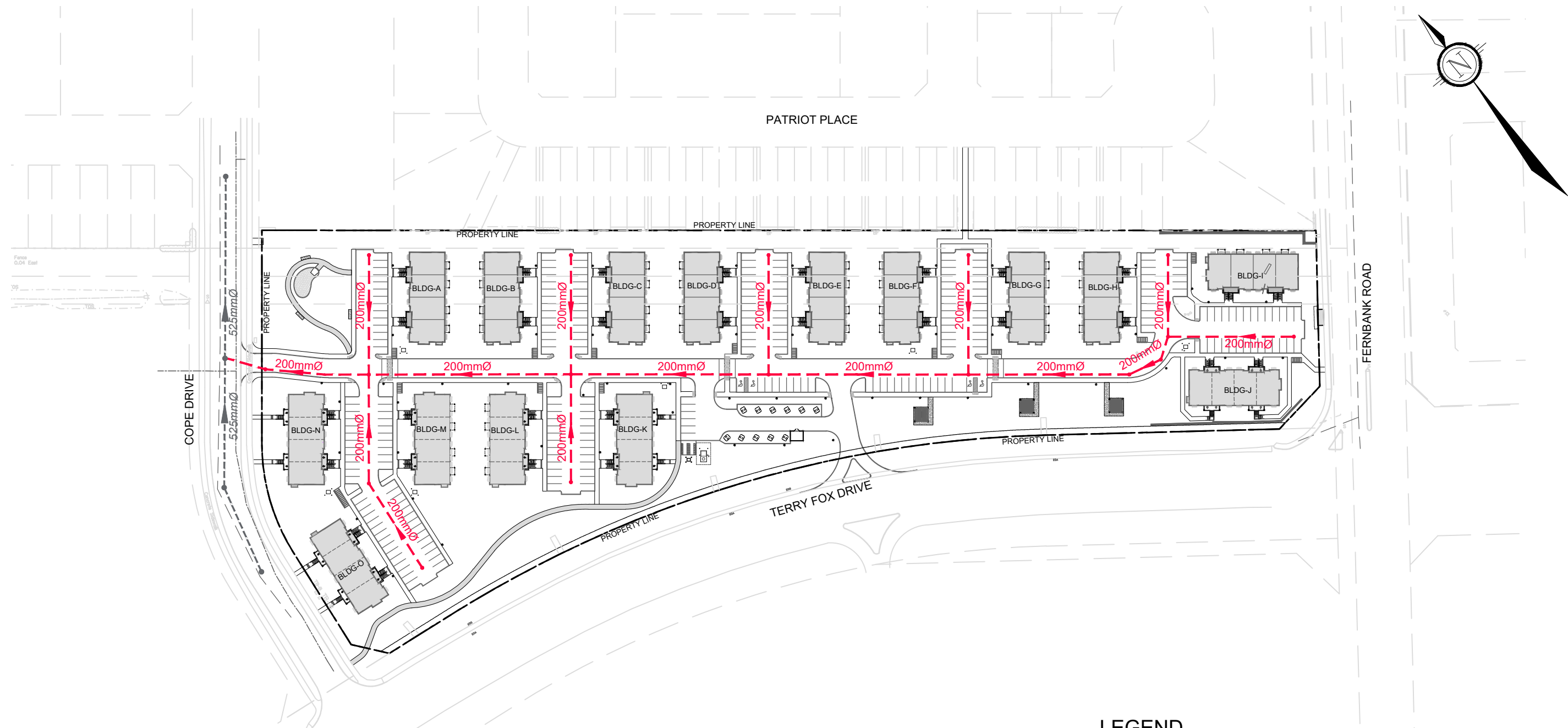
4.5 Proposed Sanitary Sewer System

The calculated peak sanitary design flow for the development is 5.42 L/s. For detailed calculations, refer to the Sanitary Sewer Design Sheet located in **Appendix B** and the Sanitary Drainage Area Plan (**121011-SAN**) located in **Appendix F** for sanitary drainage area details.

Allowable sanitary flows from the Subject Site were previously calculated in the Stantec Serviceability Report (October 2007) and the approved Novatech Servicing & Stormwater Management Report (September 2015) as part of the rezoning application for the Van Gaal Lands. As previously noted, sanitary flows from the lands north of the Monahan Drain will be directed to an existing 900mm diameter sanitary sewer on Hazeldean Side Road with the remaining two parcels outletting to the Cope Drive trunk sewer.

As a result, the proposed sanitary flows directed to the Cope Drive trunk sewer will be significantly less than previously calculated.

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LEGEND

- SITE BOUNDARY
- PROPOSED SANITARY SEWER
C/W FLOW DIRECTION
- EXISTING SANITARY SEWER C/W
FLOW DIRECTION

NOVATECH
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CITY OF OTTAWA
5331 FERNBANK ROAD
IRON VALLEY 2

SANITARY ALIGNMENT

1 : 1500

0 15 30 45 60

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Outlet to Cope Drive Sewers

A comparison of the proposed sanitary flows outletting to the existing Cope Drive sanitary trunk sewer and the allowable sanitary flows outlined in previous serviceability reports are summarized in **Table 4.1**.

Table 4.1: Proposed and Allowable Sanitary Flows Summary

Development Condition	Population	Area (ha)	Peak Flow (L/s)	Peak Ext. + Park Flow (L/s)	Peak Design Flow (L/s)
Proposed Sanitary Flows					
Claridge Residential Site North of Cope Dr. (Van Gaal Lands)	502	8.14	5.49	1.88	7.38
Subject Site	378	3.67	4.20	1.22	5.42
Total Flow (Proposed)					12.80
Allowable Sanitary Flows					
Stantec Serviceability Report (October 2007)	2811	23.14	39.47*	6.48	45.95
Novatech Approved Serviceability Report (rezoning)* (September 2015)		11.87	12.91	3.32	16.23

*Based on Table 4.1 of the rezoning report, Van Gaal Lands: 5331 Fernbank Road and 1039 Terry Fox Drive, Ottawa, ON, Servicing & Stormwater Management Brief, completed by Novatech, Ref. No.: R-2015-123, dated September 1, 2015.

The total proposed sanitary flow from the subject site and the residential area north of Cope Drive (Van Gaal Lands) is 12.80 L/s, which represents a 72% decrease in sanitary flows compared to the calculated flows in the Stantec Serviceability Report (45.95 L/s) and a 21% decrease in sanitary flows compared to the calculated flows from the approved Novatech rezoning Servicing and Stormwater Management report (16.23L/s). This indicates there will be adequate capacity in the existing Cope Drive sanitary sewers to accommodate the proposed development.

For sanitary design sheets, drainage plans and design parameters from the Stantec Serviceability Report (October 2007), refer to excerpts located in **Appendix B**. For excerpts from the approved Novatech rezoning Servicing and Stormwater Management Report (September 2015), refer to **Appendix B**.

5.0 WATER SUPPLY SYSTEM

5.1 Proposed Watermain Distribution Network

As part of the detail design process, the City of Ottawa requires a hydraulic network analysis of the proposed water distribution system within the Iron Valley 2 development to confirm adequate watermain pressure is available to service the development under all operating conditions.

It is proposed to service the Subject Site utilizing a combination of 200mm and 150mm dia. watermains. Two (2) connections will be made to the existing 300mm dia. watermain within Cope Drive to establish a looped system. The first connection will be made to the existing 300mm dia. watermain within Cope Drive approximately 35m southwest of Northgraves Crescent; the second connection, approximately 75m southwest of Northgraves Crescent.

The proposed buildings will be serviced internally with 38mm dia. water services. Each 38mm dia. waterline will service three (3) apartment units with four (4) services per building.

Figure 6 – Water Network Plan highlights the proposed works and connection points. To account for the recently installed Van Gaal Lands watermain network, new watermain boundary conditions have recently been provided by the City of Ottawa and are included in **Appendix C**.

5.2 Design Criteria

The proposed watermain distribution network has been designed in accordance with design criteria listed in the City of Ottawa Water Distribution Guidelines (July 2010) and the MOE Design Guidelines for Drinking-Water Systems (2008). The following design criteria is used to analyze the proposed watermain distribution network:

Residential (Based on MOE Design Guidelines for Developments < 500 Population)

Residential Demand:	280L per person per day
Apartments/Zen Units:	2.1 persons per unit
Maximum Daily Demand:	3.0 x Average Daily Demand
Peak Hour Demand:	4.5 x Average Daily Demand
Fire Flow Demand:	Fire Underwriters Survey
Maximum Fire Demand:	267.0 L/s, per the Fire Underwriter's Survey for Public Fire Protection. Refer to Appendix C for FUS calculation sheets.

System Pressures

Maximum (System):	690 kPa (100 psi), per City of Ottawa Water Distribution Guidelines
Maximum (Service):	550 kPa (80 psi), per Ontario Plumbing Code. pressure reducing valves are to be installed if service pressures exceed 80 psi
Minimum:	275 kPa (40 psi), except during fire flow condition
Minimum (fire):	140 kPa (20 psi)

The City of Ottawa Water Distribution Guidelines indicates the maximum pressure to be 690 kPa (100 psi) for unoccupied areas.

Friction Factors

Size	C-Factor
Less than 200mm	100
200mm-300mm	110

Operating Conditions for Hydraulic Analysis

Average Daily Demand; Maximum Daily Demand plus Fire Flow; and Peak Hour Demand.

5.3 Hydraulic Analysis

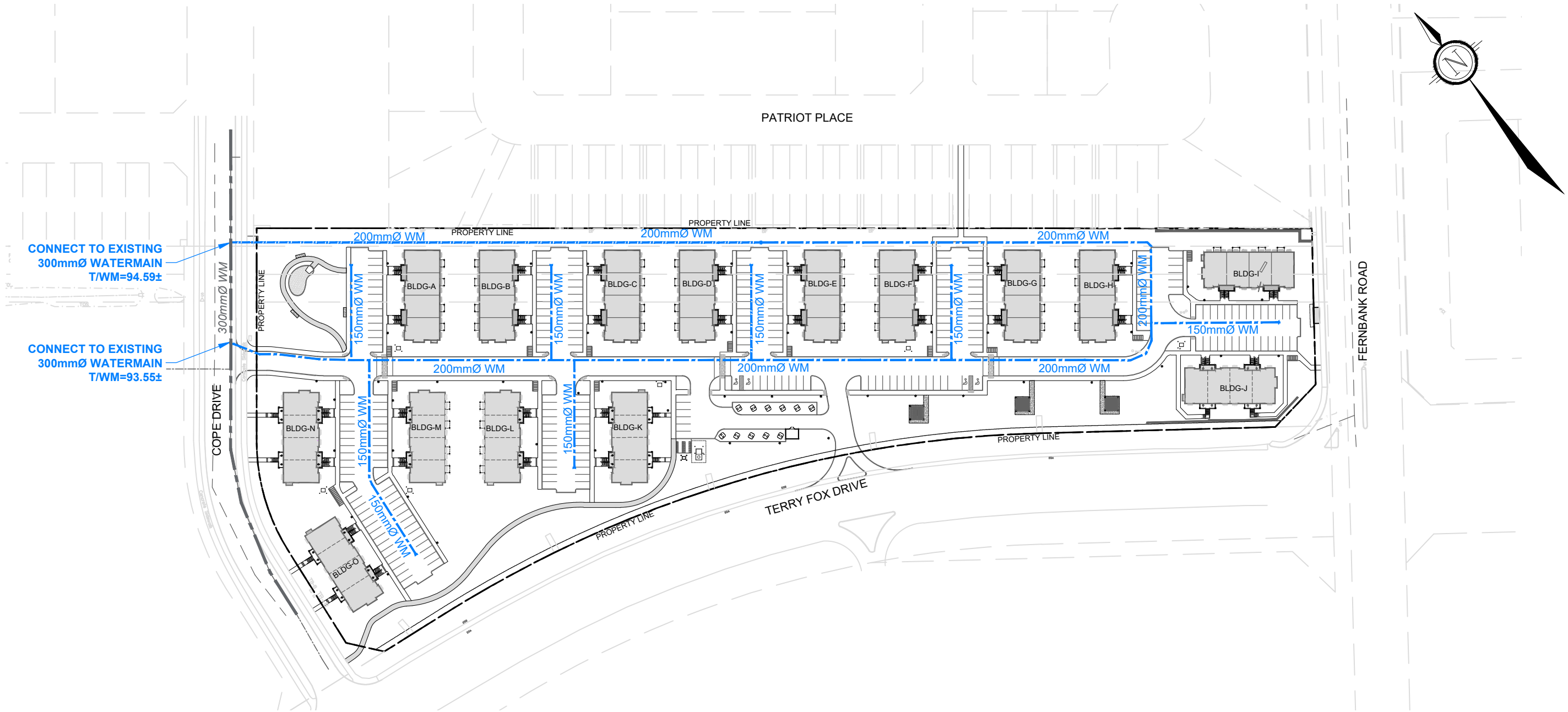
The hydraulic modelling program "EPANET" was used for the purpose of analyzing the performance of the proposed watermain network under various operating conditions.

Table 5.1 summarizes the demands under the various combined operating conditions for the Subject Site. Refer to **Appendix C** for water demands listed by node and operating condition.

Table 5.1: Hydraulic Model Demand – Iron Valley 2

Description	Demand
Population	378 persons
Average Daily Flow	1.23 L/s
Max. Daily Flow (MD)	3.68 L/s
Peak Hour Flow (PH)	5.51 L/s
Maximum Fire Flow (FF)	266.67 L/s

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LEGEND

- SITE BOUNDARY
- PROPOSED WATERMAIN
- EXISTING WATERMAIN

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CITY OF OTTAWA
5331 FERNBANK ROAD
IRON VALLEY 2

WATER NETWORK PLAN

1 : 1500

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A hydraulic analysis of the proposed watermain distribution network was conducted for the Iron Valley 2 development to confirm the proposed watermain layout can provide adequate system pressures to service the development under all operating conditions. The analysis results highlight maximum system pressures as a result of average daily flow, minimum system pressures as a result of maximum daily demand plus fire flow (MD+FF) and the peak hour demand (PH) operating condition. Refer to **Appendix C** for detailed hydraulic calculations and the associated hydraulic analysis node network. **Table 5.2** summarizes results from the hydraulic analysis under each operating condition.

Table 5.2: Hydraulic Model Results – Iron Valley 2

Operating Condition	
Max Daily Demand + Fire Flow	Minimum Operating Pressure
MD = 3.93 L/s FF= 266.67 L/s (at N3)	277.62 kPa 40.27 psi (at N3)
MD = 3.93 L/s FF= 266.67 L/s (at N4)	207.19 kPa 30.05 psi (at N4)
MD = 3.93 L/s FF= 266.67 L/s (at N5)	161.08 kPa 23.36 psi (at N5)
MD = 3.93 L/s FF= 266.67 L/s (at N6)	141.46 kPa 20.52 psi (at N18)
Peak Hour Demand	Minimum Operating Pressure
PH = 5.51 L/s	568.88 kPa 82.51 psi (at N7)
Average Daily Demand	Maximum Operating Pressure
Maximum High Pressure = Node N11	641.57 kPa 93.05 psi
Maximum Water Age = Node N4	4.6 hours

The results indicate that acceptable minimum system pressures will exist throughout the proposed distribution system under all design conditions.

The proposed water distribution system was checked for high pressures during average daily demand operating condition. The hydraulic analysis results indicate that pressures above 550 kPa (80 psi) exist within the site, up to a maximum of 641.57 kPa (93.05 psi). Therefore, pressure reducing valves will be required for all units.

5.4 Fire Flow Demands

The hydraulic analysis of the water distribution network demonstrated that the system has sufficient capacity to provide the required fire flows based on the Fire Underwriters Survey (FUS) calculations. The actual functionality of the system is limited by the available flow rate from each Hydrant. Existing and proposed hydrants are Class AA and the maximum available flow rate at each hydrant is 5,700 L/min. A further evaluation was conducted as per Technical Bulletin ISTB-2018-02 Appendix I: Guideline on Coordination of Hydrant Placement with Required Fire Flow. The results are summarized in **Table 5.3**, refer to **Figure 7 - Fire Hydrant Coverage Plan** for more details.

Table 5.3: Fire Flow Results

Building	Fire Flow Demand (L/min)	Fire Hydrants within 75m	Fire Hydrants within 150m	*Available Fire Flow (L/min)
A	13,000	Existing Hydrant 1 Existing Hydrant 3 Hydrant 1	Existing Hydrant 2 Hydrant 2	24,700
B	16,000	Hydrant 1 Hydrant 2	Existing Hydrant 1 Existing Hydrant 3 Hydrant 3	22,800
C	16,000	Hydrant 1 Hydrant 2	Existing Hydrant 1 Existing Hydrant 3 Hydrant 3	22,800
D	13,000	Hydrant 1 Hydrant 2 Hydrant 3	Hydrant 4 Hydrant 5	24,700
E	13,000	Hydrant 2 Hydrant 3	Hydrant 1 Hydrant 4 Hydrant 5	22,800
F	13,000	Hydrant 2 Hydrant 3 Hydrant 4	Hydrant 1 Hydrant 5	24,700
G	13,000	Hydrant 3 Hydrant 4 Hydrant 5	Hydrant 2	20,900
H	13,000	Hydrant 3 Hydrant 4 Hydrant 5	Hydrant 2	20,900
I	12,000	Hydrant 4 Hydrant 5	Hydrant 3	15,200
J	12,000	Hydrant 4 Hydrant 5	Hydrant 3	15,200
K	12,000	Hydrant 1 Hydrant 2	Existing Hydrant 1 Existing Hydrant 2 Hydrant 3	22,800
L	13,000	Hydrant 1 Hydrant 2	Existing Hydrant 1 Existing Hydrant 2 Existing Hydrant 3	22,800
M	13,000	Existing Hydrant 1 Existing Hydrant 2 Hydrant 1	Existing Hydrant 3 Hydrant 2	24,700
N	13,000	Existing Hydrant 1 Existing Hydrant 2 Hydrant 1	Existing Hydrant 3	20,900
O	13,000	Existing Hydrant 1 Existing Hydrant 2	Existing Hydrant 3 Hydrant 1	19,000

* Existing and proposed hydrants are Class AA and the maximum available flow rate at each hydrant is 5,700 L/min.

The proposed water distribution system and the number of proposed hydrants satisfy the requirements for available flow based on Technical Bulletin ISTB-2018-02 Appendix I: Guideline on Coordination of Hydrant Placement with Required Fire Flow.

6.0 ROADWAYS

6.1 Roadway Characteristics

The Iron Valley 2 development will have a roadway width of 6.7m throughout with parking areas provided within the development limits.

6.2 Traffic

An analysis of the effect from the proposed Fernbank Zens development on the existing traffic patterns has been performed and detailed in the report, *Proposed Residential Development, 5331 Fernbank Road, Transportation Impact Assessment, completed by Novatech, Ref. No.: R-2020-053, dated November 2025*; and is submitted under a separate cover. Please refer to this report for more details.

6.3 Pedestrian Facilities

There are 1.8m wide existing concrete sidewalks along Cope Drive and Fernbank Road and 1.8m wide pathways are proposed within the development. Pathway connections are provided through the development between Cope Drive and Fernbank Road and east to Patriot Place in the existing SOHO development.

6.4 Noise

The analysis of the roadway traffic along Terry Fox Drive, Fernbank Road and Cope Drive indicates that the City of Ottawa's criteria for residential noise will be exceeded, primarily for units in close proximity to the noise sources. Attenuation measures are required, and they may include the installation of central air conditioning, forced air ventilation, specified window and wall assemblies and/or a notice may be placed on title with regards to the noise levels to be expected. The detailed results are included in the Detailed Noise Control Study and is submitted under a separate cover. Refer to *Iron Valley 2, 5331 Fernbank Road, Detailed Noise Control Study, dated June 23, 2026, by Novatech, Report No.: R-2021-074* for more details.

7.0 EROSION AND SEDIMENT CONTROL

Erosion and sediment control measures will be implemented during construction in accordance with the "Guidelines on Erosion and Sediment Control for Urban Construction Sites" (Government of Ontario, May 1987).

Typical erosion and sediment control measures recommended include, but are not limited to, the use of silt fences around perimeter of site (OPSD 219.110), filter fabric or inserts under catch basin/maintenance hole lids, heavy duty silt fence barrier (OPSD 219.130), straw bale check dams (OPSD 219.180), rock check dams (219.210 or OPSD 219.211), riprap (OPSS 511), mud mats, silt bags for dewatering operations, topsoil and sod to disturbed areas and natural grassed waterways. Dewatering and sediment control techniques will be developed for the individual situations based on the above guidelines and utilizing typical measures to ensure erosion and sediment control is controlled in an acceptable manner and there is no negative impact to adjacent lands, water bodies or water treatment/conveyance facilities.

It will be the responsibility of the Contractor to submit a detailed construction schedule and appropriate staging, dewatering and erosion and sediment control plans to the Contract Administrator for review and approval prior to the commencement of work. A copy of the City of Ottawa Special Provision F-1004 is included in the **Appendix D** which will become part of any contract, and which outlines the contractual requirements which includes preparation of a detailed erosion and sediment control plan.

General

- All erosion and sediment control measures are to be installed to the satisfaction of the engineer, the municipality and the conservation authority prior to undertaking any site alterations (filling, grading, removal of vegetation, etc.) and remain present during all phases of site preparation and construction.
- A qualified inspector should conduct daily visits during construction to ensure that the contractor is working in accordance with the design drawings and that mitigation measures are being implemented as specified.
 - A light duty silt fence barrier is to be installed in the locations shown on the Erosion and Sediment Control Plan.
 - Straw bale barriers are to be installed in drainage ditches.
 - Filter cloth is to be placed under the grates of all proposed and existing catchbasins and structures.
 - After complete build-out, all sewers are to be inspected and cleaned and all sediment and construction fencing is to be removed.
- The contractor shall ensure that proper dust control is provided with the application of water (and if required, calcium chloride) during dry periods.
- The contractor shall immediately report to the engineer or inspector any accidental discharges of sediment material into any ditch or sewer system. Appropriate response measures shall be carried out by the contractor without delay.
- The contractor acknowledges that failure to implement erosion and sediment control measures may result in penalties imposed by any applicable regulatory agency.

8.0 UTILITIES

The Iron Valley 2 development will be serviced by hydro, phone, gas and cable, which will be constructed in a four-party trench, as per the City and utility standard right-of-way cross-sections. Canada Post will service the site with community mailboxes. Site lighting will be provided along roadways and walkways as per City standards.

9.0 PHASING

Servicing of the Iron Valley 2 development will be constructed in one phase.

10.0 DEVIATIONS FROM SEWER DESIGN GUIDELINES

The cover over the proposed storm sewers in certain instances is less than the standard outlined in the City of Ottawa Sewer Design Guidelines (October 2012) as some of the proposed storm sewers have been oversized for underground stormwater management. Due to the grade raise restrictions for the Subject Site, if the site grading was raised to meet the minimum storm sewer cover over these few oversized storm sewers, there would be a corresponding large increase in the development cost with the use of lightweight fill over the entire site. The installation of insulation will be required where minimum cover over storm sewers cannot be achieved.

11.0 CONCLUSIONS

- Storm servicing for the development will be provided using a dual drainage system: minor system flows (up to the 2-year event) will be conveyed by storm sewers or stored underground, while major system flows will be stored at low points in the roadways and parking areas. Flows that exceed the storage provided will be conveyed overland along defined overland flow routes to either Cope Drive, Fernbank Road or Terry Fox Drive.
- Water quality control for the proposed development will be provided by the existing approved Vortech units located at the outfall to Cell 1 of the Monahan Drain Constructed Wetlands.
- Peak flows leaving the site will be less than the allowable release rate for both the minor and major systems and will therefore have no adverse impact on the existing development downstream.
- A minimum clearance of 0.30m will be provided between the 100-year hydraulic grade line (HGL) and the designed underside of footing elevations where the buildings are directly connected to the storm sewers.
- Sanitary servicing for the Iron Valley 2 development will be provided by a gravity sanitary sewer system which will utilize 200mm dia. sanitary pipes within the development. Sanitary flows from the Subject Site will outlet to the existing 525mm dia. sanitary trunk sewer along Cope Drive.
- Water servicing for the Iron Valley 2 development will be provided by two (2) connections to the existing 300mm dia. watermain within Cope Drive establishing a looped system. The proposed water distribution network provides adequate operating pressures utilizing a combination of 38mm, 150mm, and 200mm dia. watermains and private fire hydrants within the Subject Site.
- Local private roadways will be 6.7m in width throughout the site with parking areas situated within the development limits. Internal pathways will be provided for pedestrian access within and through the development connecting to existing sidewalks along Cope Drive and Fernbank Road.
- Noise attenuation measures (noise wall) are not required on the site for the outdoor amenity areas. Building façade analysis was completed and the corresponding building requirements are outlined in the Detailed Noise Control Study submitted under separate cover.
- Erosion and sediment control measures (i.e. filter fabric, silt fences, etc.) will be implemented prior to construction and are to remain in place until vegetation is established. Erosion and sediment control measures associated with construction are to be implemented as outlined in Section 7.0.
- The Iron Valley 2 development will be serviced by hydro, phone, gas and cable, which will be constructed in a three-party trench, as per the City of Ottawa and utility standard right-of-way cross-sections. Canada Post will service the Subject Site with community mailboxes. Site lighting will be provided along roadways and pathways as per City of Ottawa standards.

It is recommended that the City of Ottawa approve the findings of this Site Servicing Report in support of the engineering detail design for Site Plan Approval of the Iron Valley 2 (formerly Fernbank Zens) development at 5331 Fernbank Road.

NOVATECH

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Appendix A
STORM SEWER DESIGN

STORM SEWER DESIGN SHEET
IRON VALLEY 2
5331 FERNBANK
FLOW RATES BASED ON RATIONAL METHOD



LOCATION				AREA (ha)			FLOW							TOTAL FLOW	SEWER DATA									
Street	Catchment ID	From MH	To MH	Area (ha)	C	AC (ha)	Indiv 2.78 AC	Accum 2.78 AC	Time of Concentration	Rainfall Intensity 2 Year (mm/hr)	Rainfall Intensity 5 Year (mm/hr)	Rainfall Intensity 10 Year (mm/hr)	Peak Flow (L/s)	Total Peak Flow, Q (L/s)	Dia. (m) Actual	Dia. (mm)	Type	Slope (%)	Length (m)	Capacity (L/s)	Velocity (m/s)	Flow Time (min)	Ratio Q/Q full	
	A1	206	CBMH 15	0.02	0.25	0.01	0.014	0.014	10.00	76.81			1.1	18.1	0.254	250	PVC	0.47	17.1	42.5	0.84	0.34	43%	
						0.00	0.000	0.000	10.00															
						0.00	0.000	0.000	10.00															
	A2			0.13	0.62	0.08	0.222	0.236	10.00	76.81			18.1	17.8	0.305	300	PVC	0.37	32.2	61.3	0.84	0.64	29%	
				0.00	0.000	0.000	10.00																	
				0.00	0.000	0.000	10.34																	
			CBMH 15	118			0.00	0.000	0.236	10.34	75.52			17.8										
							0.00	0.000	0.000	10.34														
							0.00	0.000	0.000	10.98														
	A3	CBMH 5	118	0.12	0.30	0.04	0.099	0.099	10.00	76.81			7.6	22.3	0.305	300	PVC	0.34	17.6	58.8	0.81	0.36	38%	
						0.00	0.000	0.000	10.00															
						0.00	0.000	0.000	10.00															
	A4			0.12	0.58	0.07	0.192	0.291	10.00	76.81			22.3											
				0.00	0.000	0.000	10.00																	
				0.00	0.000	0.000	10.00																	
								10.36																
		118	116			0.00	0.000	0.527	10.98	73.24			38.6	38.6	0.381	375	PVC	0.34	8.9	106.6	0.93	0.16	36%	
						0.00	0.000	0.000	10.98															
						0.00	0.000	0.000	10.98															
		116	114			0.00	0.000	0.527	11.14	72.70			38.3	38.3	0.381	375	PVC	0.25	12.0	91.4	0.80	0.25	42%	
						0.00	0.000	0.000	11.14															
						0.00	0.000	0.000	11.14															
	A5	114	112	0.07	0.39	0.03	0.076	0.603	11.39	71.86			43.4	54.5	0.381	375	PVC	0.26	58.7	93.2	0.82	1.20	59%	
						0.00	0.000	0.000	11.39															
						0.00	0.000	0.000	11.39															
	A32			0.10	0.56	0.06	0.156	0.759	11.39	71.86			54.5											
				0.00	0.000	0.000	11.39																	
				0.00	0.000	0.000	11.39																	
								12.58																
	A8	CHMH 4	112	0.15	0.59	0.09	0.247	0.247	10.00	76.81			19.0	19.0	0.305	300	PVC	0.38	26.6	62.1	0.85	0.52	31%	
						0.00	0.000	0.000	10.00															
						0.00	0.000	0.000	10.00															
									10.52															
	A6	112	110	0.19	0.25	0.05	0.133	1.140	12.58	68.13			77.7	92.4	0.533	525	Conc	0.19	72.1	195.4	0.87	1.37	47%	
						0.00	0.000	0.000	12.58															
						0.00	0.000	0.000	12.58															
	A7			0.08	0.63	0.05	0.140	1.280	12.58	68.13			87.2											
				0.00	0.000	0.000	12.58																	
				0.00	0.000	0.000	12.58																	
	A9			0.07	0.39	0.03	0.076	1.357	12.58	68.13			92.4											
				0.00	0.000	0.000	12.58																	
				0.00	0.000	0.000	12.58																	
								13.96																

STORM SEWER DESIGN SHEET
IRON VALLEY 2
5331 FERNBANK
FLOW RATES BASED ON RATIONAL METHOD



LOCATION				AREA (ha)			FLOW							TOTAL FLOW	SEWER DATA																			
Street	Catchment ID	From MH	To MH	Area (ha)	C	AC (ha)	Indiv 2.78 AC	Accum 2.78 AC	Time of Concentration	Rainfall Intensity 2 Year (mm/hr)	Rainfall Intensity 5 Year (mm/hr)	Rainfall Intensity 10 Year (mm/hr)	Peak Flow (L/s)	Total Peak Flow, Q (L/s)	Dia. (m) Actual	Dia. (mm)	Type	Slope (%)	Length (m)	Capacity (L/s)	Velocity (m/s)	Flow Time (min)	Ratio Q/Q full											
	A10	CBMH 3	110	0.11	0.29	0.03	0.089	0.089	10.00	76.81			6.8	25.8	0.305	300	PVC	0.38	26.6	62.1	0.85	0.52	42%											
						0.00	0.000	0.000	10.00																									
						0.00	0.000	0.000	10.00																									
	A11			0.15	0.59	0.09	0.247	0.336	10.00	76.81			25.8																					
						0.00	0.000	0.000	10.00																									
						0.00	0.000	0.000	10.00																									
								10.00																										
	A12	CBMH 13	110	0.11	0.63	0.07	0.192	0.192	10.00	76.81			14.7	14.7	0.305	300	PVC	0.43	7.8	66.1	0.91	0.14	22%											
						0.00	0.000	0.000	10.00																									
						0.00	0.000	0.000	10.00																									
		110	108			0.00	0.000	1.885	13.96	64.34			121.3	121.3	0.533	525	Conc	0.23	21.5	215.0	0.96	0.37	56%											
						0.00	0.000	0.000	13.96																									
						0.00	0.000	0.000	13.96																									
	A14	CBMH 12	CBMH 11	0.04	0.25	0.01	0.028	0.028	10.00	76.81			2.1	6.6	0.254	250	PVC	0.52	38.6	44.7	0.88	0.73	15%											
						0.00	0.000	0.000	10.00																									
						0.00	0.000	0.000	10.00																									
	A13			0.03	0.70	0.02	0.058	0.086	10.00	76.81			6.6																					
						0.00	0.000	0.000	10.00																									
						0.00	0.000	0.000	10.00																									
A15	CBMH 11	108	0.13	0.53	0.07	0.190	0.277	10.73	74.11			20.5	20.5	0.305	300	PVC	0.35	19.3	59.6	0.82	0.39	34%												
					0.00	0.000	0.000	10.73																										
					0.00	0.000	0.000	10.73																										
	A19	108	106	0.07	0.39	0.03	0.076	2.238	14.33	63.40			141.9	141.9	0.610	600	Conc	0.14	50.6	239.5	0.82	1.03	59%											
						0.00	0.000	0.000	14.33																									
						0.00	0.000	0.000	14.33																									
	A20	CBMH 2	106	0.09	0.29	0.03	0.072	0.072	10.00	76.81			5.6	35.6	0.305	300	PVC	0.38	26.6	62.1	0.85	0.52	57%											
						0.00	0.000	0.000	10.00																									
						0.00	0.000	0.000	10.00																									
	A18			0.24	0.59	0.14	0.391	0.463	10.00	76.81			35.6																					
						0.00	0.000	0.000	10.00																									
						0.00	0.000	0.000	10.00																									
								10.52																										
	A27	204	CBMH10	0.15	0.26	0.04	0.110	0.110	10.00	76.81			8.5	11.7	0.305	300	PVC	0.45	17.7	67.6	0.93	0.32	17%											
						0.00	0.000	0.000	10.00																									
						0.00	0.000	0.000	10.00																									
	A16			0.05	0.30	0.01	0.042	0.152	10.00	76.81			11.7																					
						0.00	0.000	0.000	10.00																									
						0.00	0.000	0.000	10.00																									
A17	CBMH 10	106	0.21	0.51	0.11	0.300	0.451	10.32	75.60			34.1	34.1	0.305	300	PVC	0.36	24.9	60.5	0.83	0.50	56%												
					0.00	0.000	0.000	10.32																										
					0.00	0.000	0.000	10.32																										
								10.82																										

IRON VALLEY 2
5331 Fernbank
Claridge Homes
Project No.: 121011

STORM SEWER DESIGN SHEET
IRON VALLEY 2
5331 FERNBANK
FLOW RATES BASED ON RATIONAL METHOD



LOCATION				AREA (ha)			FLOW							TOTAL FLOW	SEWER DATA																							
Street	Catchment ID	From MH	To MH	Area (ha)	C	AC (ha)	Indiv 2.78 AC	Accum 2.78 AC	Time of Concentration	Rainfall Intensity 2 Year (mm/hr)	Rainfall Intensity 5 Year (mm/hr)	Rainfall Intensity 10 Year (mm/hr)	Peak Flow (L/s)	Total Peak Flow, Q (L/s)	Dia. (m) Actual	Dia. (mm)	Type	Slope (%)	Length (m)	Capacity (L/s)	Velocity (m/s)	Flow Time (min)	Ratio Q/Q full															
	A22	106	104	0.09	0.41	0.04	0.101	3.254	15.36	60.94			198.3	213.8	0.762	750	Conc	0.11	72.1	385.0	0.84	1.42	56%															
						0.00	0.000	0.000	15.36																													
						0.00	0.000	0.000	15.36																													
	A26			0.08	0.42	0.03	0.093	3.347	15.36	60.94			203.9																									
						0.00	0.000	0.000	15.36																													
						0.00	0.000	0.000	15.36																													
	A24			0.11	0.53	0.06	0.161	3.508	15.36	60.94			213.8																									
						0.00	0.000	0.000	15.36																													
						0.00	0.000	0.000	15.36																													
									16.78																													
	A21	CBMH 1	104	0.06	0.25	0.02	0.042	0.042	10.00	76.81			3.2	25.5	0.305	300	PVC	0.34	26.6	58.8	0.81	0.55	43%															
						0.00	0.000	0.000	10.00																													
						0.00	0.000	0.000	10.00																													
	A23			0.24	0.43	0.10	0.290	0.332	10.00	76.81			25.5																									
						0.00	0.000	0.000	10.00																													
						0.00	0.000	0.000	10.00																													
									10.55																													
	A31	202	CBMH8	0.05	0.30	0.02	0.042	0.042	10.00	76.81			3.2	3.2	0.610	600	Conc	0.17	18.2	263.9	0.90	0.34	1%															
							0.00	0.000	0.000	10.00																												
							0.00	0.000	0.000	10.00																												
	A28	CBMH8	200	0.12	0.60	0.07	0.200	0.242	10.34	75.54			18.3	18.3	0.305	300	PVC	0.37	21.9	61.3	0.84	0.43	30%															
							0.00	0.000	0.000	10.34																												
							0.00	0.000	0.000	10.34																												
	A29	200	CBMH 7	0.09	0.25	0.02	0.063	0.305	10.77	73.97			22.6	22.6	0.381	375	PVC	0.25	16.3	91.4	0.80	0.34	25%															
							0.00	0.000	0.000	10.77																												
							0.00	0.000	0.000	10.77																												
	A25	CBMH 7	104	0.14	0.61	0.09	0.236	0.541	11.11	72.79			39.4	39.4	0.457	450	Conc	0.20	24.9	132.9	0.81	0.51	30%															
							0.00	0.000	0.000	11.11																												
							0.00	0.000	0.000	11.11																												
										11.62																												
			104	102			0.00	0.000	4.381	16.78	57.86			253.5	253.5	0.838	825	Conc	0.15	13.3	579.7	1.05	0.21	44%														
									0.00	0.000	0.000	16.78																										
									0.00	0.000	0.000	16.78																										
		102	100			0.00	0.000	4.381	16.99	57.43			251.6	251.6	0.838	825	Conc	0.16	21.3	598.7	1.08	0.33	42%															
								0.00	0.000	0.000	16.99																											
								0.00	0.000	0.000	16.99																											
COPE DR		100	EX STM			0.00	0.000	4.381	17.32	56.79			248.8	248.8	0.838	825	Conc	0.11	18.9	496.4	0.90	0.35	50%															
								0.00	0.000	0.000	17.32																											
								0.00	0.000	0.000	17.32																											
									17.67																													
Q = Peak Flow in Litres per Second (L/s) C = Runoff Coefficient A = Area in hectares (ha) I = Rainfall Intensity (mm/hr)										Date:					November 15, 2025																							
										Revised:					March 18, 2026																							
										Revised:					June 5, 2026																							
										Design By:					AE / BM																							
										Client:					Dwg. Reference:					Checked By:																		
										Claridge Homes					121011-STM					DDB																		

Legend:
* Areas/Runoff Coefficients/Time of Concentration based on detailed storm design sheet and drawing (121011-STM)
10.00 Storm sewers designed to the 2 year event (without ponding) for local roads
10.00 Storm sewers designed to the 5 year event (without ponding) for collector roads
10.00 Storm sewers designed to the 10 year event (without ponding) for arterial roads

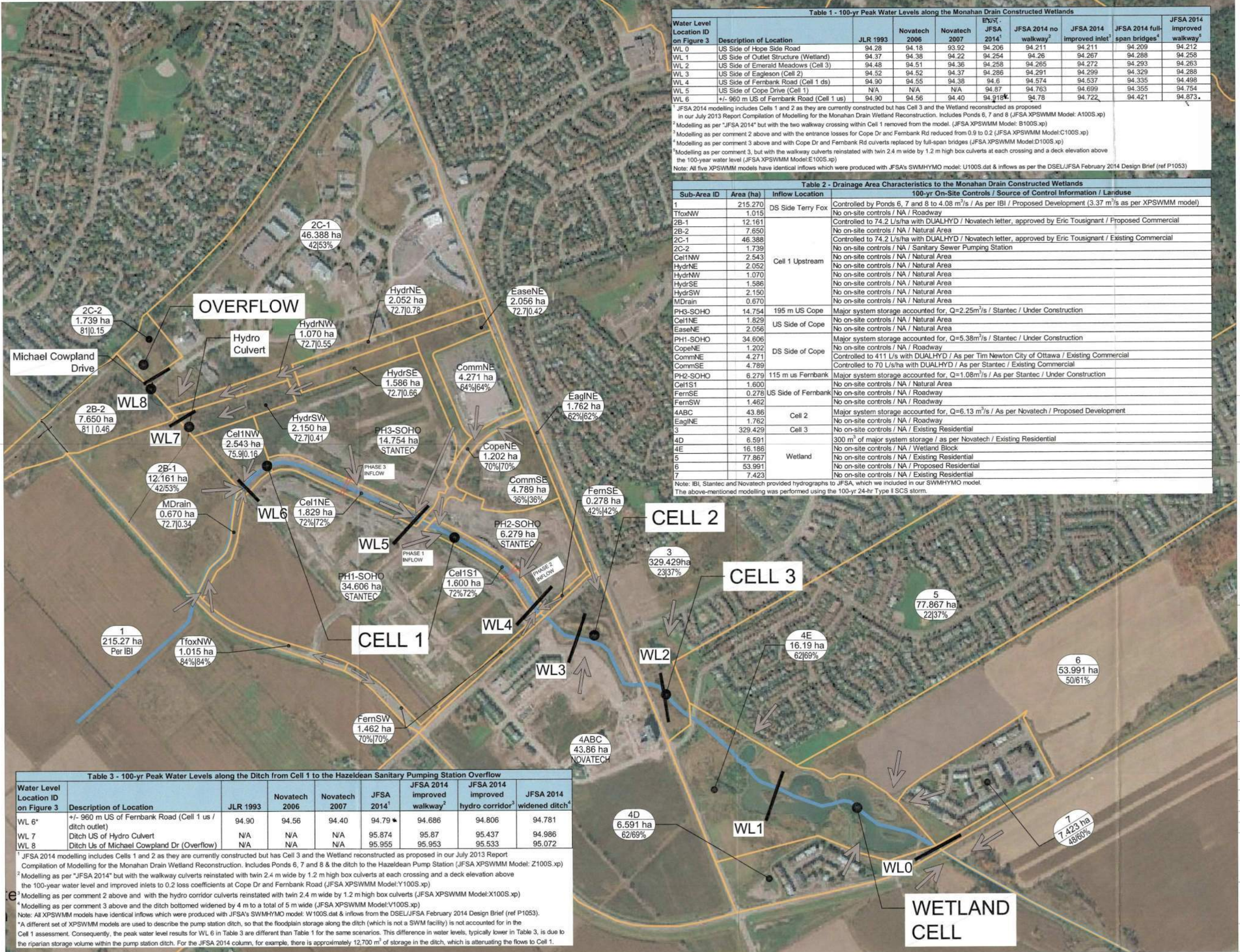


Table 1 - 100-yr Peak Water Levels along the Monahan Drain Constructed Wetlands								
Water Level Location ID on Figure 3	Description of Location	JLR 1993	Novatech 2006	Novatech 2007	JFSAs 2014 ¹	JFSAs 2014 no walkway ²	JFSAs 2014 improved inlet ³	JFSAs 2014 full-span bridges ⁴
WL 0	US Side of Hope Side Road	94.28	94.18	93.92	94.206	94.211	94.211	94.209
WL 1	US Side of Outlet Structure (Wetland)	94.37	94.38	94.22	94.254	94.26	94.267	94.268
WL 2	US Side of Emerald Meadows (Cell 3)	94.48	94.51	94.36	94.258	94.265	94.272	94.293
WL 3	US Side of Eagleson (Cell 2)	94.52	94.52	94.37	94.286	94.291	94.299	94.329
WL 4	US Side of Fernbank Road (Cell 1 ds)	94.90	94.55	94.38	94.6	94.574	94.537	94.498
WL 5	US Side of Cope Drive (Cell 1)	N/A	N/A	N/A	94.87	94.763	94.699	94.355
WL 6	+/- 960 m US of Fernbank Road (Cell 1 us)	94.90	94.56	94.40	94.916	94.78	94.722	94.873

¹ JFSAs 2014 modelling includes Cells 1 and 2 as they are currently constructed but has Cell 3 and the Wetland reconstructed as proposed in our July 2013 Report. Compilation of Modelling for the Monahan Drain Wetland Reconstruction. Includes Ponds 6, 7 and 8 (JFSAs XPSWMM Model: A100S.xp)

² Modelling as per "JFSAs 2014" but with the two walkway crossing within Cell 1 removed from the model. (JFSAs XPSWMM Model: B100S.xp)

³ Modelling as per comment 2 above and with the entrance losses for Cope Dr and Fernbank Rd reduced from 0.9 to 0.2 (JFSAs XPSWMM Model: C100S.xp)

⁴ Modelling as per comment 3 above and with Cope Dr and Fernbank Rd culverts replaced by full-span bridges (JFSAs XPSWMM Model: D100S.xp)

⁵ Modelling as per comment 3, but with the walkway culverts reinstated with twin 2.4 m wide by 1.2 m high box culverts at each crossing and a deck elevation above the 100-year water level (JFSAs XPSWMM Model: E100S.xp)

Note: All five XPSWMM models have identical inflows which were produced with JFSAs's SWMMHYMO model: U100S.dat & inflows as per the DSEL/JFSA February 2014 Design Brief (ref P1053)

Table 2 - Drainage Area Characteristics to the Monahan Drain Constructed Wetlands		
Sub-Area ID	Area (ha)	Inflow Location
1	215.270	DS Side Terry Fox
TfoxNW	1.015	No on-site controls / NA / Roadway
2B-1	12.161	Controlled to 74.2 L/s/ha with DUALHYD / Novatech letter, approved by Eric Tousignant / Proposed Commercial
2B-2	7.650	No on-site controls / NA / Natural Area
2C-1	46.388	Controlled to 74.2 L/s/ha with DUALHYD / Novatech letter, approved by Eric Tousignant / Existing Commercial
2C-2	1.739	No on-site controls / NA / Sanitary Sewer Pumping Station
Cell1NW	2.543	No on-site controls / NA / Natural Area
HydrNE	2.052	No on-site controls / NA / Natural Area
HydrNW	1.070	No on-site controls / NA / Natural Area
HydrSE	1.586	No on-site controls / NA / Natural Area
HydrSW	2.150	No on-site controls / NA / Natural Area
MDrain	0.670	No on-site controls / NA / Natural Area
PH3-SOHO	14.754	195 m US Cope
Cell1NE	1.829	Major system storage accounted for, Q=2.25m³/s / Stantec / Under Construction
EaseNE	2.056	No on-site controls / NA / Natural Area
PH1-SOHO	34.606	US Side of Cope
CopeNE	1.202	No on-site controls / NA / Natural Area
CommNE	4.271	Major system storage accounted for, Q=5.38m³/s / Stantec / Under Construction
CommSE	4.789	No on-site controls / NA / Roadway
PH2-SOHO	6.279	Controlled to 411 L/s with DUALHYD / As per Tim Newton City of Ottawa / Existing Commercial
Cell1S1	1.600	Controlled to 70 L/s/ha with DUALHYD / As per Stantec / Existing Commercial
FernSE	0.278	115 m us Fernbank
FernSW	1.462	Major system storage accounted for, Q=1.08m³/s / As per Stantec / Under Construction
4ABC	43.86	No on-site controls / NA / Roadway
EagleNE	1.762	No on-site controls / NA / Roadway
3	329.429	Cell 2
4D	6.591	No on-site controls / NA / Existing Residential
4E	16.186	300 m³ of major system storage / as per Novatech / Existing Residential
5	77.867	No on-site controls / NA / Wetland Block
6	53.991	No on-site controls / NA / Existing Residential
7	7.423	No on-site controls / NA / Proposed Residential

Note: IBI, Stantec and Novatech provided hydrographs to JFSAs, which we included in our SWMMHYMO model. The above-mentioned modelling was performed using the 100-yr 24-hr Type II SCS storm.

Table 3 - 100-yr Peak Water Levels along the Ditch from Cell 1 to the Hazeldean Sanitary Pumping Station Overflow								
Water Level Location ID on Figure 3	Description of Location	JLR 1993	Novatech 2006	Novatech 2007	JFSAs 2014 ¹	JFSAs 2014 improved walkway ²	JFSAs 2014 improved hydro corridor ³	JFSAs 2014 widened ditch ⁴
WL 6*	+/- 960 m US of Fernbank Road (Cell 1 us / ditch outlet)	94.90	94.56	94.40	94.79	94.686	94.806	94.781
WL 7	Ditch US of Hydro Culvert	N/A	N/A	N/A	95.874	95.87	95.437	94.986
WL 8	Ditch US of Michael Cowpland Dr (Overflow)	N/A	N/A	N/A	95.955	95.953	95.533	95.072

¹ JFSAs 2014 modelling includes Cells 1 and 2 as they are currently constructed but has Cell 3 and the Wetland reconstructed as proposed in our July 2013 Report. Compilation of Modelling for the Monahan Drain Wetland Reconstruction. Includes Ponds 6, 7 and 8 & the ditch to the Hazeldean Pump Station (JFSAs XPSWMM Model: Z100S.xp)

² Modelling as per "JFSAs 2014" but with the walkway culverts reinstated with twin 2.4 m wide by 1.2 m high box culverts at each crossing and a deck elevation above the 100-year water level and improved inlets to 0.2 loss coefficients at Cope Dr and Fernbank Road (JFSAs XPSWMM Model: Y100S.xp)

³ Modelling as per comment 2 above and with the hydro corridor culverts reinstated with twin 2.4 m wide by 1.2 m high box culverts (JFSAs XPSWMM Model: X100S.xp)

⁴ Modelling as per comment 3 above and the ditch bottomed widened by 4 m to a total of 5 m wide (JFSAs XPSWMM Model: V100S.xp)

Note: All XPSWMM models have identical inflows which were produced with JFSAs's SWMMHYMO model: W100S.dat & inflows from the DSEL/JFSA February 2014 Design Brief (ref P1053).

*A different set of XPSWMM models are used to describe the pump station ditch, so that the floodplain storage along the ditch (which is not a SWM facility) is not accounted for in the Cell 1 assessment. Consequently, the peak water level results for WL 6 in Table 3 are different than Table 1 for the same scenarios. This difference in water levels, typically lower in Table 3, is due to the riparian storage volume within the pump station ditch. For the JFSAs 2014 column, for example, there is approximately 12,700 m³ of storage in the ditch, which is attenuating the flows to Cell 1.

LEGEND :

- SUBCATCHMENT BOUNDARY
- MONAHAN DRAIN
- DRAINAGE DIRECTION / INFLOW LOCATION TO XPSWMM
- SUB-CATCHMENT ID (STANDHYD)
- SUB-CATCHMENT AREA (HA)
- DIRECT / TOTAL IMPERVIOUSNESS (%)
- SUB-CATCHMENT ID (NASHYD)
- SUB-CATCHMENT AREA (HA)
- CURVE NUMBER | TIME TO PEAK (H)
- WL1 WATER LEVEL LOCATION refer to Table 1
- APPROXIMATE LOCATION OF WALKWAYS

SCALE :

0 125 250 375 500 m

J.F. Sabourin & Associates Inc.
WATER RESOURCES AND ENVIRONMENTAL CONSULTANTS
OTTAWA (613) 836-3884
GATINEAU (819) 243-6858

CLIENT :

Ottawa

PROJECT :

CELL 1 MODELLING
MONAHAN DRAIN CONSTRUCTED
WETLANDS

CB	Sept/14	FINAL	3
CB	Feb/13	For Review / Comments	2
CB	Dec/13	For Discussion	1
CB	Sept/13	For Discussion	0
BY	DATE	DESCRIPTION	REV

DETAILED DRAINAGE AREAS TO CELL 1
+ WATER LEVELS ALONG the MDCW

FIGURE 3

DESIGNED:	CB
DRAWN:	CB
VERIFIED:	
APPROVED:	
DATE	Sept/14
PROJECT No.	902(03)-13



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- Legend**
- DRAINAGE AREA NO.
RUNOFF COEFFICIENT
STORM DRAINAGE AREA (ha)
 - DRAINAGE AREA BOUNDARY
 - PROPOSED STORM SEWER & MANHOLE
 - PROPOSED CATCH BASIN (ALL ROAD CB'S TO INCLUDE PERFORATED SUB DRAINS EXTENDING OUT FROM THE CB IN TWO DIRECTIONS PARALLEL TO THE ROADWAY. THESE DRAINS ARE TO BE INSTALLED AT THE BOTTOM OF THE SUBBASE LAYER.)
 - PROPOSED SUBDRAIN CATCH BASIN
 - PROPOSED 250mm PERFORATED PIPE
 - STREET CATCHBASINS TO BE INTERCONNECTED WITH ONLY ONE CONNECTION TO STORM SEWER PER PAIR WHERE NOTED.
IPEX TYPE 'A' TO BE INSTALLED IN STREET AND REAR YARD CATCHBASINS WHERE NOTED.
 - PROPOSED CATCH BASIN / MANHOLE c/w IPEX INLET-CONTROL DEVICE TYPE 'A' OR APPROVED EQUIVALENT
 - PONDING AREA LIMITS
DEPTH=0.20m
MAXIMUM PONDING DEPTH
 - DIRECTION OF OVERLAND FLOW
 - FUTURE PHASE OF STORM DRAINAGE WORKS

Notes

1. IPEX TYPE 'A' TO RESTRICT FLOWS TO THE STORM SEWER TO 22L/s AT 1.8m HEAD.

7	REVISED DRIVEWAY & SIDEWALK LOCATIONS, ISSUED FOR FINAL APPROVAL	KJK	JBL	09.02.25
5	REVISED LOT GRADING AND SERVING	KJK	JBL	08.11.03
4	ISSUED FOR CONSTRUCTION	KJK	JBL	08.01.21
3	REVISED AS PER CITY COMMENTS	KJK	JBL	07.10.29
2	REVISED AS PER CITY COMMENTS	KJK	JBL	07.08.17
1	ISSUED FOR CITY COMMENTS	KJK	JBL	07.07.12

Revision		By	Appd.	YY.MM.DD
File Name:	160400502C-S0	KJK	JBL	KJK
		Dwn.	Chkd.	Orgn.
				YY.MM.DD

Permit-Seal

Client/Project
CAVANAGH CONSTRUCTION LTD.

SOHO - KANATA SOUTH

Ottawa ON Canada

Title
OVERALL
STORM DRAINAGE PLAN

Project No.	160400502C	Scale	0 30 60 100m 1:2000
Drawing No.		Sheet	Revision

Iron Valley II - 5331 Fernbank Road (121011)
PCSWMM Model Results (Ponding)

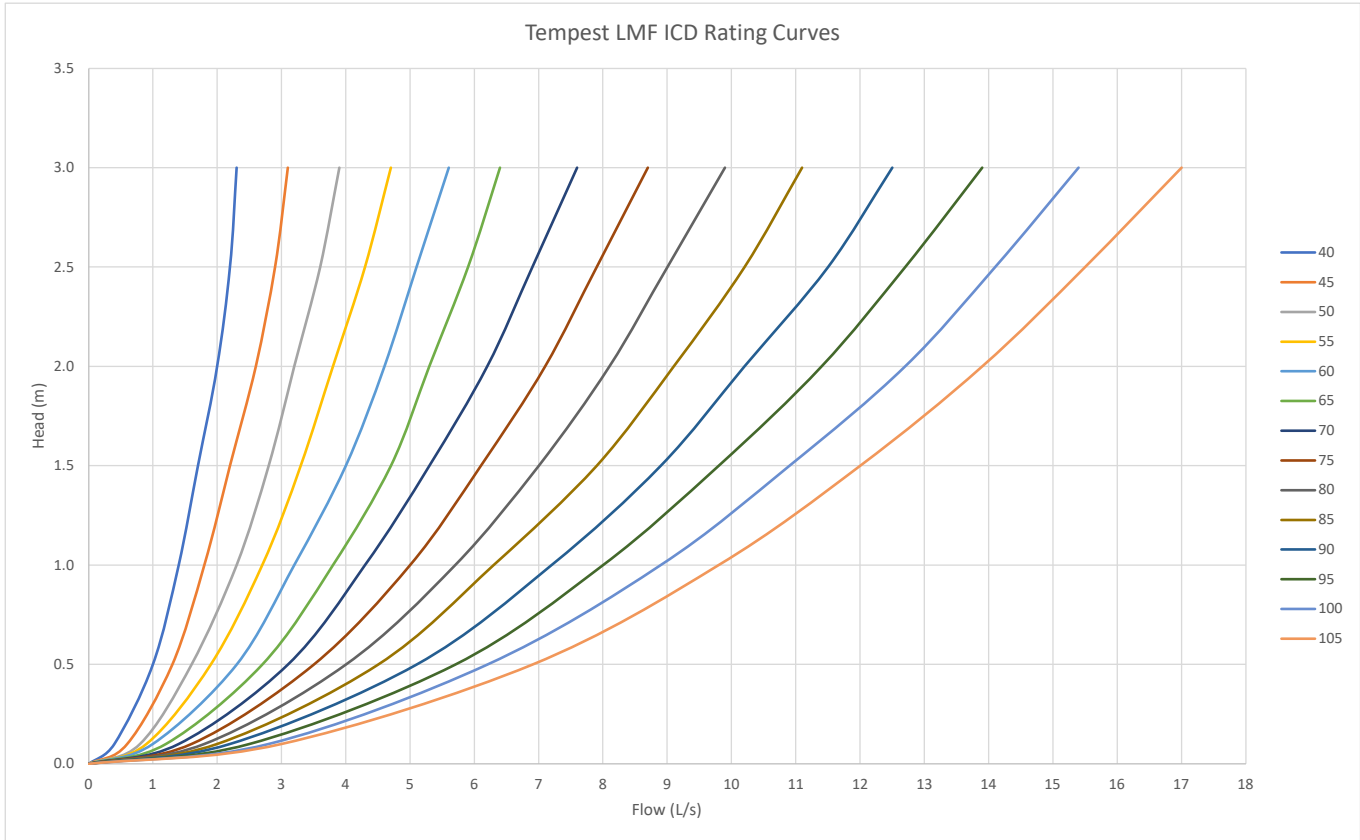
CB ID	Invert Elev. (m)	Rim Elev. (m)	Spill Elev. (m)	Ponding Depth (m)	HGL Elev. (m) ¹				Ponding Depth (m)				Spill Depth (m)			
					2-yr	5-yr	100-yr	100-yr (+20%)	2-yr	5-yr	100-yr	100-yr (+20%)	2-yr	5-yr	100-yr	100-yr (+20%)
CBMH1	94.77	96.74	97.06	0.32	95.49	96.53	97.00	97.09	0.00	0.00	0.26	0.35	0.00	0.00	0.00	0.03
CBMH2	94.86	96.84	97.11	0.27	95.84	96.84	97.11	97.14	0.00	0.00	0.27	0.30	0.00	0.00	0.00	0.03
CBMH3	94.98	97.10	97.38	0.28	95.76	96.31	97.29	97.38	0.00	0.00	0.19	0.28	0.00	0.00	0.00	0.00
CBMH4	95.12	97.31	97.54	0.23	97.15	97.38	97.49	97.52	0.00	0.07	0.18	0.21	0.00	0.00	0.00	0.00
CBMH5	95.29	97.38	97.68	0.30	96.33	97.29	97.61	97.64	0.00	0.00	0.23	0.26	0.00	0.00	0.00	0.00
CBMH7	94.58	96.78	97.08	0.30	94.72	94.77	95.12	95.15	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
CBMH8	94.85	96.92	97.16	0.24	95.77	96.69	97.15	97.17	0.00	0.00	0.23	0.25	0.00	0.00	0.00	0.01
CBMH10	94.85	96.86	97.20	0.34	95.15	95.43	97.02	97.13	0.00	0.00	0.16	0.27	0.00	0.00	0.00	0.00
CBMH11	94.90	97.08	97.25	0.17	95.43	95.80	97.25	97.38	0.00	0.00	0.17	0.30	0.00	0.00	0.00	0.13
CBMH12	95.15	97.55	97.66	0.11	95.43	95.80	97.25	97.38	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
CBMH13	94.91	97.23	97.37	0.14	95.89	97.04	97.38	97.42	0.00	0.00	0.15	0.19	0.00	0.00	0.01	0.05
CBMH14	95.09	97.23	97.37	0.14	95.55	95.99	97.39	97.42	0.00	0.00	0.16	0.19	0.00	0.00	0.02	0.05
CBMH15	95.35	97.50	97.75	0.25	96.45	97.42	97.66	97.70	0.00	0.00	0.16	0.20	0.00	0.00	0.00	0.00
CICB1	95.42	96.99	97.11	0.12	96.37	97.11	97.12	97.14	0.00	0.12	0.13	0.15	0.00	0.00	0.01	0.03
CICB2	96.04	97.44	97.64	0.20	96.86	97.56	97.66	97.66	0.00	0.12	0.22	0.22	0.00	0.00	0.02	0.02
RYE1	95.99	97.47	97.61	0.14	96.33	97.29	97.61	97.62	0.00	0.00	0.14	0.15	0.00	0.00	0.00	0.01
RYE10	95.47	97.37	97.50	0.13	95.49	95.80	97.25	97.38	0.00	0.00	0.00	0.01	0.00	0.00	0.00	0.00
RYE11	95.64	97.14	97.27	0.13	96.38	97.12	97.20	97.26	0.00	0.00	0.06	0.12	0.00	0.00	0.00	0.00
RYE12	95.76	97.16	97.31	0.15	95.81	96.06	97.31	97.33	0.00	0.00	0.15	0.17	0.00	0.00	0.00	0.02
RYE13	95.91	97.31	97.45	0.14	95.96	96.09	97.45	97.46	0.00	0.00	0.14	0.15	0.00	0.00	0.00	0.01
RYE14	96.10	97.50	97.64	0.14	96.15	96.28	97.64	97.67	0.00	0.00	0.14	0.17	0.00	0.00	0.00	0.03
RYE15	95.86	97.38	97.68	0.30	96.33	97.29	97.61	97.64	0.00	0.00	0.23	0.26	0.00	0.00	0.00	0.00
RYE16	95.78	97.58	97.69	0.11	96.45	97.42	97.67	97.70	0.00	0.00	0.09	0.12	0.00	0.00	0.00	0.01
RYE17	96.26	97.66	97.80	0.14	96.86	97.56	97.71	97.75	0.00	0.00	0.05	0.09	0.00	0.00	0.00	0.00
RYE18	94.94	96.80	97.00	0.20	95.49	96.53	97.00	97.11	0.00	0.00	0.20	0.31	0.00	0.00	0.00	0.11
RYE2	95.51	97.50	97.66	0.16	95.56	95.99	97.53	97.70	0.00	0.00	0.03	0.20	0.00	0.00	0.00	0.04
RYE3	95.96	97.40	97.55	0.15	96.00	96.32	97.44	97.55	0.00	0.00	0.04	0.15	0.00	0.00	0.00	0.00
RYE4	95.26	96.90	97.17	0.27	95.85	96.84	97.13	97.23	0.00	0.00	0.23	0.33	0.00	0.00	0.00	0.06
RYE5	95.14	96.85	97.15	0.30	95.49	96.53	97.00	97.10	0.00	0.00	0.15	0.25	0.00	0.00	0.00	0.00
RYE6	95.45	97.46	97.60	0.14	95.78	96.69	97.15	97.17	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
RYE7	95.03	97.22	97.37	0.15	95.06	95.14	95.86	96.44	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
RYE8	95.15	97.20	97.50	0.30	95.19	95.43	97.08	97.44	0.00	0.00	0.00	0.24	0.00	0.00	0.00	0.00
RYE9	95.16	97.37	97.59	0.22	95.19	95.43	97.03	97.14	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
RYT1	95.59	97.35	97.67	0.32	96.33	97.29	97.61	97.64	0.00	0.00	0.26	0.29	0.00	0.00	0.00	0.00
RYT10	94.97	97.47	97.48	0.01	95.15	95.43	97.03	97.13	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
RYT11	95.16	97.58	97.69	0.11	95.43	95.80	97.25	97.38	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
RYT12	95.45	97.07	97.14	0.07	96.37	97.11	97.13	97.14	0.00	0.04	0.06	0.07	0.00	0.00	0.00	0.00
RYT13	95.59	97.17	97.30	0.13	95.77	96.06	97.30	97.31	0.00	0.00	0.13	0.14	0.00	0.00	0.00	0.01
RYT14	95.72	97.29	97.43	0.14	95.85	96.09	97.43	97.43	0.00	0.00	0.14	0.14	0.00	0.00	0.00	0.00
RYT15	95.91	97.48	97.59	0.11	96.04	96.28	97.60	97.60	0.00	0.00	0.12	0.12	0.00	0.00	0.01	0.01
RYT16	96.07	97.64	97.66	0.02	96.86	97.56	97.66	97.67	0.00	0.00	0.02	0.03	0.00	0.00	0.00	0.01
RYT17	94.97	97.08	97.33	0.25	95.15	95.43	97.03	97.13	0.00	0.00	0.00	0.05	0.00	0.00	0.00	0.00
RYT3	95.41	97.44	97.65	0.21	95.55	95.99	97.40	97.44	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
RYT4	95.23	97.26	97.50	0.24	95.55	95.99	97.39	97.43	0.00	0.00	0.13	0.17	0.00	0.00	0.00	0.00
RYT5	95.11	97.23	97.38	0.15	95.55	95.99	97.39	97.42	0.00	0.00	0.16	0.19	0.00	0.00	0.01	0.04
RYT6	95.62	97.18	97.55	0.37	95.77	96.32	97.35	97.44	0.00	0.00	0.17	0.26	0.00	0.00	0.00	0.00
RYT7	95.14	97.15	97.35	0.20	95.76	96.32	97.30	97.38	0.00	0.00	0.15	0.23	0.00	0.00	0.00	0.03
RYT8	94.89	96.90	97.15	0.25	95.84	96.84	97.11	97.14	0.00	0.00	0.21	0.24	0.00	0.00	0.00	0.00
RYT9	94.79	96.85	97.10	0.25	95.49	96.53	97.00	97.09	0.00	0.00	0.15	0.24	0.00	0.00	0.00	0.00

Iron Valley II - 5331 Fernbank Road (121011)
PCSWMM Model Results (HGL)

MH ID	Obvert Elevation (m)	T/G Elevation (m)	HGL Elevation ¹ (m)	Surcharge (m)	Clearance from T/G (m)	HGL in Stress Test ¹ (m)
MH100	94.93	96.96	95.06	0.13	1.90	95.06
MH102	94.96	97.03	95.07	0.11	1.96	95.08
MH104	94.98	97.03	95.08	0.10	1.95	95.08
MH106	95.06	97.11	95.11	0.05	2.00	95.12
MH108	95.13	97.28	95.14	0.01	2.14	95.15
MH110	95.18	97.36	95.15	0.00	2.21	95.16
MH112	95.32	97.50	95.17	0.00	2.33	95.17
MH114	95.47	97.55	95.24	0.00	2.31	95.24
MH116	95.5	97.61	95.25	0.00	2.36	95.25
MH118	95.53	97.67	95.26	0.00	2.41	95.26
MH200	95.07	97.18	95.13	0.06	2.05	95.15
MH202	95.48	97.39	97.15	1.67	0.24	97.17
MH204	95.53	97.13	97.03	1.50	0.10	97.15
MH206	96.08	97.76	97.67	1.59	0.09	97.70

¹ 3-hour Chicago Storm.

PCSWMM Model Results (HGL)



Iron Valley II - 5331 Fernbank Road (121011)
PCSWMM Model Schematics

Overall Model Schematic



Iron Valley II - 5331 Fernbank Road (121011)
PCSWMM Model Schematics

Subcatchments



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Iron Valley II - 5331 Fernbank Road (121011)
PCSWMM Model Schematics

Minor System (MH IDs)



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Iron Valley II - 5331 Fernbank Road (121011)
PCSWMM Model Schematics

Major System (CB IDs) and Outfalls



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EPA STORM WATER MANAGEMENT MODEL - VERSION 5.2 (Build 5.2.4)

WARNING 04: minimum elevation drop used for Conduit MS-RYE2(5)
 WARNING 03: negative offset ignored for Link MS-RYT10(1)
 WARNING 03: negative offset ignored for Link MS-RYT10(2)
 WARNING 04: minimum elevation drop used for Conduit MS-RYT12
 WARNING 04: minimum elevation drop used for Conduit MS-RYT3(3)
 WARNING 04: minimum elevation drop used for Conduit MS-RYT4(3)

 Element Count

Number of rain gages 1
 Number of subcatchments ... 37
 Number of nodes 130
 Number of links 177
 Number of pollutants 0
 Number of land uses 0

 Raingage Summary

Name	Data Source	Data Type	Recording Interval
RG-1	C3hr-100YR	INTENSITY	10 min.

 Subcatchment Summary

Name Outlet	Area	Width	%Imperv	%Slope	Rain Gage
A1 RYE16	0.03	27.62	7.00	3.7000	RG-1
A10 RYE3	0.11	91.36	13.00	2.0000	RG-1
A11 CBMH3	0.15	76.57	56.00	2.0000	RG-1
A12 CBMH13	0.11	99.73	61.00	1.0000	RG-1
A13 HP-RYT11(2)	0.03	13.95	71.00	2.5000	RG-1
A14 RYE10	0.04	54.65	7.00	2.5000	RG-1
A15 CBMH11	0.13	62.89	47.00	2.5000	RG-1
A16 RYE9	0.05	56.18	14.00	2.5000	RG-1
A17 CBMH10	0.15	48.11	44.00	2.5000	RG-1
A18 CBMH2	0.24	123.58	55.00	2.1000	RG-1

Iron Valley II - 5331 Fernbank Road (121011)
 PCSWMM Model Output
 100yr, 3-hour Chicago Storm

A19	0.07	59.02	28.00	3.5000	RG-1
RYE13					
A2	0.13	66.39	59.00	1.9000	RG-1
CBMH15					
A20	0.10	96.43	13.00	3.0000	RG-1
RYE4					
A21	0.06	76.24	7.00	3.0000	RG-1
RYE5					
A22	0.09	56.43	29.00	3.5000	RG-1
RYE11					
A23_1	0.14	54.33	33.00	2.3000	RG-1
CBMH1					
A23_2	0.10	37.98	33.00	2.3000	RG-1
RYE18					
A24	0.11	105.36	47.00	0.5000	RG-1
CICB1					
A25	0.14	76.29	58.00	2.2000	RG-1
CBMH7					
A26	0.08	46.08	31.00	3.7000	RG-1
RYE12					
A27	0.15	120.00	9.00	3.5000	RG-1
RYE8					
A28	0.12	72.33	58.00	2.5000	RG-1
CBMH8					
A29	0.05	40.19	7.00	3.0000	RG-1
RYE7					
A3	0.12	94.12	14.00	3.0000	RG-1
RYT1					
A31	0.05	37.88	14.00	3.4000	RG-1
RYE6					
A32	0.10	120.19	51.00	0.5000	RG-1
CICB2					
A4	0.13	68.17	54.00	2.3000	RG-1
CBMH5					
A5	0.07	58.00	28.00	3.7000	RG-1
RYE17					
A6	0.19	99.11	7.00	2.6000	RG-1
RYE2					
A7	0.08	33.94	61.00	1.2000	RG-1
CBMH14					
A8	0.15	78.25	56.00	1.9000	RG-1
CBMH4					
A9	0.07	57.14	28.00	3.7000	RG-1
RYE14					
U1	0.09	103.45	14.00	15.0000	RG-1
OF1					
U2	0.03	46.95	12.00	5.0000	RG-1
OF3					
U3	0.05	171.82	7.00	15.0000	RG-1
OF2					
U4	0.09	90.00	29.00	3.7000	RG-1
OF4					
U5	0.05	33.16	29.00	3.7000	RG-1
OF5					

 Node Summary

Invert	Max.	Ponded	External
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Name	Type	Elev.	Depth	Area	Inflow
-----	-----	-----	-----	-----	-----
CBMH4-Dummy	JUNCTION	95.22	3.00	0.0	
HP-CBMH1	JUNCTION	97.08	1.00	0.0	
HP-CBMH1 (2)	JUNCTION	97.06	1.00	0.0	
HP-CBMH10	JUNCTION	97.20	1.00	0.0	
HP-CBMH11	JUNCTION	97.25	1.00	0.0	
HP-CBMH12	JUNCTION	97.70	1.00	0.0	
HP-CBMH13	JUNCTION	97.66	1.00	0.0	
HP-CBMH14	JUNCTION	97.34	1.00	0.0	
HP-CBMH15	JUNCTION	97.75	1.00	0.0	
HP-CBMH2	JUNCTION	97.11	1.00	0.0	
HP-CBMH3	JUNCTION	97.37	1.00	0.0	
HP-CBMH4	JUNCTION	97.54	1.00	0.0	
HP-CBMH5	JUNCTION	97.68	1.00	0.0	
HP-CBMH7	JUNCTION	97.16	1.00	0.0	
HP-CBMH8	JUNCTION	97.27	1.00	0.0	
HP-CICB1	JUNCTION	97.11	1.00	0.0	
HP-CICB2	JUNCTION	97.64	1.00	0.0	
HP-RYE10	JUNCTION	97.50	1.00	0.0	
HP-RYE12	JUNCTION	97.33	1.00	0.0	
HP-RYE12 (2)	JUNCTION	97.31	1.00	0.0	
HP-RYE15	JUNCTION	97.68	1.00	0.0	
HP-RYE16 (1)	JUNCTION	97.85	1.00	0.0	
HP-RYE18	JUNCTION	96.98	1.00	0.0	
HP-RYE2 (1)	JUNCTION	97.68	0.30	0.0	
HP-RYE2 (2)	JUNCTION	97.66	0.30	0.0	
HP-RYE2 (3)	JUNCTION	97.70	1.00	0.0	
HP-RYE3 (1)	JUNCTION	97.52	0.30	0.0	
HP-RYE3 (2)	JUNCTION	97.69	0.30	0.0	
HP-RYE3 (3)	JUNCTION	97.55	1.00	0.0	
HP-RYE4	JUNCTION	97.35	1.00	0.0	
HP-RYE4 (2)	JUNCTION	97.45	1.00	0.0	
HP-RYE5	JUNCTION	97.15	1.00	0.0	
HP-RYE6	JUNCTION	97.60	1.00	0.0	
HP-RYE7	JUNCTION	97.37	1.00	0.0	
HP-RYE8	JUNCTION	97.50	1.00	0.0	
HP-RYE9	JUNCTION	97.59	1.00	0.0	
HP-RYT1 (1)	JUNCTION	97.76	0.30	0.0	
HP-RYT1 (2)	JUNCTION	97.67	1.00	0.0	
HP-RYT10 (1)	JUNCTION	97.58	1.00	0.0	
HP-RYT10 (2)	JUNCTION	97.45	1.00	0.0	
HP-RYT11 (1)	JUNCTION	97.69	1.00	0.0	
HP-RYT11 (2)	JUNCTION	97.77	1.00	0.0	
HP-RYT13	JUNCTION	97.30	1.00	0.0	
HP-RYT14	JUNCTION	97.43	1.00	0.0	
HP-RYT15	JUNCTION	97.59	1.00	0.0	
HP-RYT3 (1)	JUNCTION	97.66	0.30	0.0	
HP-RYT3 (2)	JUNCTION	97.65	0.30	0.0	
HP-RYT4	JUNCTION	97.65	0.30	0.0	
HP-RYT4 (2)	JUNCTION	97.50	0.30	0.0	
HP-RYT5 (1)	JUNCTION	97.38	1.00	0.0	
HP-RYT5 (2)	JUNCTION	97.50	0.30	0.0	
HP-RYT5 (3)	JUNCTION	97.38	0.30	0.0	
HP-RYT6	JUNCTION	97.49	1.00	0.0	
HP-RYT7	JUNCTION	97.57	1.00	0.0	
HP-RYT7 (2)	JUNCTION	97.35	1.00	0.0	

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HP-RYT8 (1)	JUNCTION	97.17	1.00	0.0
HP-RYT8 (2)	JUNCTION	97.15	1.00	0.0
HP-RYT9 (1)	JUNCTION	97.44	1.00	0.0
HP-RYT9 (2)	JUNCTION	97.10	1.00	0.0
HP-RYE1	OUTFALL	97.61	1.00	0.0
HP-RYE16 (2)	OUTFALL	97.69	1.00	0.0
MH1013	OUTFALL	94.08	0.82	0.0
OF1	OUTFALL	97.00	0.00	0.0
OF2	OUTFALL	97.73	0.00	0.0
OF3	OUTFALL	97.15	0.00	0.0
OF4	OUTFALL	96.85	2.35	0.0
OF5	OUTFALL	0.00	0.00	0.0
CBMH1	STORAGE	94.77	2.97	0.0
CBMH10	STORAGE	94.85	3.01	0.0
CBMH11	STORAGE	94.90	3.18	0.0
CBMH12	STORAGE	95.15	3.40	0.0
CBMH13	STORAGE	94.91	3.32	0.0
CBMH14	STORAGE	95.09	3.14	0.0
CBMH15	STORAGE	95.35	3.15	0.0
CBMH2	STORAGE	94.86	2.98	0.0
CBMH3	STORAGE	94.98	3.12	0.0
CBMH4	STORAGE	95.12	3.19	0.0
CBMH5	STORAGE	95.29	3.09	0.0
CBMH7	STORAGE	94.58	3.20	0.0
CBMH8	STORAGE	94.85	3.07	0.0
CICB1	STORAGE	95.42	2.72	0.0
CICB2	STORAGE	96.04	2.55	0.0
MH100	STORAGE	94.10	2.86	0.0
MH102	STORAGE	94.13	2.90	0.0
MH104	STORAGE	94.15	2.88	0.0
MH106	STORAGE	94.31	2.80	0.0
MH108	STORAGE	94.53	2.75	0.0
MH110	STORAGE	94.65	2.71	0.0
MH112	STORAGE	94.79	2.71	0.0
MH114	STORAGE	95.09	2.46	0.0
MH116	STORAGE	95.12	2.49	0.0
MH118	STORAGE	95.15	2.52	0.0
MH200	STORAGE	94.69	2.49	0.0
MH202	STORAGE	94.88	2.51	0.0
MH204	STORAGE	94.93	2.20	0.0
MH206	STORAGE	95.48	2.28	0.0
RYE1	STORAGE	95.99	2.48	0.0
RYE10	STORAGE	95.47	2.90	0.0
RYE11	STORAGE	95.64	2.50	0.0
RYE12	STORAGE	95.76	2.40	0.0
RYE13	STORAGE	95.91	2.40	0.0
RYE14	STORAGE	96.10	2.40	0.0
RYE15	STORAGE	95.86	2.52	0.0
RYE16	STORAGE	95.78	2.80	0.0
RYE17	STORAGE	96.26	2.40	0.0
RYE18	STORAGE	94.94	2.86	0.0
RYE2	STORAGE	95.51	2.99	0.0
RYE3	STORAGE	95.96	2.44	0.0
RYE4	STORAGE	95.26	2.64	0.0
RYE5	STORAGE	95.14	2.71	0.0
RYE6	STORAGE	95.45	3.01	0.0
RYE7	STORAGE	95.03	3.19	0.0

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RYE8	STORAGE	95.15	3.05	0.0
RYE9	STORAGE	95.16	3.21	0.0
RYT1	STORAGE	95.59	2.76	0.0
RYT10	STORAGE	94.97	3.50	0.0
RYT11	STORAGE	95.16	3.42	0.0
RYT12	STORAGE	95.45	2.62	0.0
RYT13	STORAGE	95.59	2.58	0.0
RYT14	STORAGE	95.72	2.57	0.0
RYT15	STORAGE	95.91	2.57	0.0
RYT16	STORAGE	96.07	2.57	0.0
RYT17	STORAGE	94.97	3.11	0.0
RYT3	STORAGE	95.40	3.04	0.0
RYT4	STORAGE	95.23	3.03	0.0
RYT5	STORAGE	95.11	3.12	0.0
RYT6	STORAGE	95.62	2.56	0.0
RYT7	STORAGE	95.14	3.01	0.0
RYT8	STORAGE	94.89	3.01	0.0
RYT9	STORAGE	94.79	3.06	0.0

Link Summary

Name	From Node	To Node	Type	Length	%
Slope Roughness					

100_(STM)	MH202	CBMH8	CONDUIT	18.2	
0.1651 0.0130					
104_(STM)	RYT9	CBMH1	CONDUIT	20.8	
0.0962 0.0130					
106_(STM)	RYE5	RYT9	CONDUIT	35.4	
0.9896 0.0130					
116_(STM)	RYT8	CBMH2	CONDUIT	20.8	
0.1444 0.0130					
118_(STM)	RYE4	RYT8	CONDUIT	36.0	
0.9989 0.0130					
124_(STM)	RYT7	CBMH3	CONDUIT	21.8	
0.5051 0.0130					
128_(STM)	RYT6	RYT7	CONDUIT	47.6	
1.0074 0.0130					
130_(STM)	RYE3	RYT6	CONDUIT	34.3	
0.9925 0.0130					
132_(STM)	RYT1	CBMH5	CONDUIT	17.1	
0.1755 0.0130					
136_(STM)	RYE6	MH202	CONDUIT	20.7	
1.0141 0.0130					
150_(1)_(STM)	RYE2	RYT3	CONDUIT	22.8	
0.4831 0.0130					
152_(1)_(STM)	RYT3	RYT4	CONDUIT	34.7	
0.4902 0.0130					
173_(STM)	RYE1	RYT1	CONDUIT	40.3	
0.9931 0.0130					
175_(STM)	CBMH12	CBMH11	CONDUIT	38.6	
0.5179 0.0130					
207_(STM)	RYT4	RYT5	CONDUIT	21.4	
0.5145 0.0130					
209_(STM)	CBMH4-Dummy	CBMH4	CONDUIT	13.7	
0.1461 0.0130					

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229_ (STM)	MH104	MH102	CONDUIT	13.3
0.1503 0.0130				
233_ (STM)	MH204	CBMH10	CONDUIT	17.7
0.4520 0.0130				
236(1)_ (STM)	RYE8	RYT17	CONDUIT	16.6
1.0223 0.0130				
240_ (STM)	MH118	MH116	CONDUIT	8.9
0.3382 0.0130				
250_ (STM)	RYT17	MH204	CONDUIT	25.4
0.1575 0.0130				
252_ (STM)	RYT10	MH204	CONDUIT	26.8
0.1493 0.0130				
253_ (STM)	RYE9	RYT10	CONDUIT	18.1
0.9918 0.0130				
260_ (STM)	RYT5	CBMH14	CONDUIT	3.5
0.5797 0.0130				
266_ (STM)	RYE10	RYT11	CONDUIT	29.6
1.0129 0.0130				
270_ (STM)	RYT11	CBMH12	CONDUIT	7.8
0.1280 0.0130				
277_ (STM)	RYE11	RYT12	CONDUIT	18.7
1.0156 0.0130				
278_ (STM)	RYT12	CICB1	CONDUIT	3.5
0.8696 0.0130				
279_ (STM)	RYE12	RYT13	CONDUIT	17.1
0.9954 0.0130				
281_ (STM)	RYE13	RYT14	CONDUIT	18.7
1.0156 0.0130				
283_ (STM)	RYE14	RYT15	CONDUIT	18.7
1.0156 0.0130				
285_ (STM)	RYE15	RYT1	CONDUIT	22.4
1.2049 0.0130				
286_ (STM)	RYE17	RYT16	CONDUIT	18.7
1.0156 0.0130				
287_ (STM)	RYT16	CICB2	CONDUIT	3.5
0.8696 0.0130				
288_ (STM)	RYE16	MH206	CONDUIT	17.8
0.1690 0.0130				
304_ (STM)	RYE18	CBMH1	CONDUIT	12.4
0.9678 0.0130				
49_ (STM)	MH100	MH1013	CONDUIT	18.9
0.1058 0.0130				
50_ (STM)	MH114	MH112	CONDUIT	58.6
0.2558 0.0130				
51_ (STM)	MH112	MH110	CONDUIT	72.1
0.1942 0.0130				
52_ (STM)	MH110	MH108	CONDUIT	21.5
0.2328 0.0130				
53_ (STM)	MH108	MH106	CONDUIT	50.6
0.1383 0.0130				
55_ (STM)	MH106	MH104	CONDUIT	72.1
0.1110 0.0130				
56_ (STM)	MH102	MH100	CONDUIT	21.4
0.1405 0.0130				
85_ (STM)	MH206	CBMH15	CONDUIT	17.1
0.4687 0.0130				
87_ (STM)	MH116	MH114	CONDUIT	12.0
0.2500 0.0130				
97(1)_ (STM)	CBMH7	MH104	CONDUIT	24.9
0.2008 0.0130				

Iron Valley II - 5331 Fernbank Road (121011)
 PCSWMM Model Output
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97_ (STM)	MH200	CBMH7	CONDUIT	16.3	
0.2459 0.0130					
MS-CBMH1 (1)	CBMH1	HP-CBMH1	CONDUIT	2.0	-
17.2511 0.0130					
MS-CBMH1 (2)	HP-CBMH1	CBMH7	CONDUIT	2.0	
15.1717 0.0130					
MS-CBMH1 (3)	CBMH1	HP-CBMH1 (2)	CONDUIT	2.0	-
16.2088 0.0130					
MS-CBMH1 (4)	HP-CBMH1 (2)	OF4	CONDUIT	2.0	-
69.3731 0.0130					
MS-CBMH10 (1)	CBMH10	HP-CBMH10	CONDUIT	2.0	-
17.2511 0.0130					
MS-CBMH10 (2)	HP-CBMH10	HP-CBMH2	CONDUIT	2.0	
4.5046 0.0130					
MS-CBMH10 (3)	HP-CBMH2	CICB1	CONDUIT	2.0	
6.0108 0.0130					
MS-CBMH11 (1)	CBMH11	HP-CBMH11	CONDUIT	2.0	-
8.5309 0.0130					
MS-CBMH11 (2)	HP-CBMH11	HP-RYT14	CONDUIT	2.0	-
9.0367 0.0130					
MS-CBMH12 (1)	HP-CBMH12	CBMH12	CONDUIT	2.0	
7.5212 0.0130					
MS-CBMH12 (2)	HP-CBMH12	CBMH11	CONDUIT	2.0	
32.6063 0.0130					
MS-CBMH13 (1)	CBMH12	HP-CBMH13	CONDUIT	2.0	-
5.5083 0.0130					
MS-CBMH13 (2)	HP-CBMH13	CBMH13	CONDUIT	2.0	
22.0148 0.0130					
MS-CBMH14 (1)	CBMH14	HP-CBMH14	CONDUIT	2.0	-
5.5083 0.0130					
MS-CBMH14 (2)	HP-CBMH14	CBMH13	CONDUIT	2.0	
5.5083 0.0130					
MS-CBMH15 (1)	CBMH15	HP-CBMH15	CONDUIT	2.0	-
12.5988 0.0130					
MS-CBMH15 (2)	HP-CBMH15	CBMH5	CONDUIT	2.0	
18.8249 0.0130					
MS-CBMH2	HP-CBMH2	CBMH2	CONDUIT	2.0	
13.6247 0.0130					
MS-CBMH3 (1)	CBMH3	HP-CBMH3	CONDUIT	2.0	-
13.6247 0.0130					
MS-CBMH3 (2)	HP-CBMH3	CBMH13	CONDUIT	2.0	
7.0172 0.0130					
MS-CBMH3 (3)	HP-CBMH3	HP-CBMH11	CONDUIT	2.0	
6.0108 0.0130					
MS-CBMH4 (1)	CBMH4	HP-CBMH4	CONDUIT	2.0	-
11.5768 0.0130					
MS-CBMH4 (2)	HP-CBMH4	CBMH14	CONDUIT	2.0	
15.6896 0.0130					
MS-CBMH5	CBMH5	HP-CBMH5	CONDUIT	2.0	-
15.1717 0.0130					
MS-CBMH5 (2)	HP-CBMH5	CICB2	CONDUIT	2.0	
12.0873 0.0130					
MS-CBMH7 (1)	CBMH7	HP-CBMH7	CONDUIT	2.0	-
19.3525 0.0130					
MS-CBMH7 (2)	HP-CBMH7	CBMH8	CONDUIT	2.0	
12.0873 0.0130					
MS-CBMH8 (1)	CBMH8	HP-CBMH8	CONDUIT	2.0	-
17.7743 0.0130					
MS-CBMH8 (2)	HP-CBMH8	RYT17	CONDUIT	2.0	
9.5432 0.0300					

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MS-CICB1 (1)	CICB1	HP-CICB1	CONDUIT	2.0	-
6.0108 0.0130					
MS-CICB1 (2)	HP-CICB1	CBMH1	CONDUIT	2.0	
18.8249 0.0130					
MS-CICB2 (1)	CICB2	HP-CICB2	CONDUIT	2.0	-
10.0504 0.0130					
MS-CICB2 (2)	HP-CICB2	CBMH14	CONDUIT	2.0	
20.9448 0.0130					
MS-RYE (1)	HP-RYE2 (1)	RYE2	CONDUIT	8.9	
2.0229 0.0300					
MS-RYE1	RYE1	HP-RYE1	CONDUIT	2.0	-
7.0172 0.0300					
MS-RYE10 (1)	RYE10	HP-RYE10	CONDUIT	2.0	-
6.5138 0.0300					
MS-RYE10 (2)	HP-RYE10	RYE9	CONDUIT	2.0	
7.5212 0.0300					
MS-RYE10 (3)	HP-RYE10	CBMH11	CONDUIT	2.0	
21.4790 0.0130					
MS-RYE12 (1)	RYE12	HP-RYE12	CONDUIT	2.0	-
8.5309 0.0300					
MS-RYE12 (2)	HP-RYE12	RYT17	CONDUIT	2.0	
12.5988 0.0300					
MS-RYE12 (3)	RYE12	HP-RYE12 (2)	CONDUIT	2.0	-
7.5212 0.0300					
MS-RYE12 (4)	HP-RYE12 (2)	RYT13	CONDUIT	2.0	
7.0172 0.0300					
MS-RYE15 (1)	RYE15	HP-RYE15	CONDUIT	16.1	-
1.8637 0.0300					
MS-RYE15 (2)	HP-RYE15	RYT1	CONDUIT	11.2	
2.9477 0.0300					
MS-RYE16 (1)	RYE16	HP-RYE16 (1)	CONDUIT	2.0	-
13.6247 0.0300					
MS-RYE16 (2)	HP-RYE16 (1)	CBMH15	CONDUIT	2.0	
17.7743 0.0130					
MS-RYE16 (3)	RYE16	HP-RYE16 (2)	CONDUIT	2.0	-
5.5083 0.0300					
MS-RYE18 (1)	RYE18	HP-RYE18	CONDUIT	2.0	-
9.0367 0.0130					
MS-RYE18 (2)	HP-RYE18	CBMH1	CONDUIT	2.0	
12.0873 0.0130					
MS-RYE2 (2)	RYE2	HP-RYE2 (2)	CONDUIT	9.3	-
1.7207 0.0300					
MS-RYE2 (3)	RYE2	HP-RYE2 (3)	CONDUIT	2.0	-
10.0504 0.0300					
MS-RYE2 (4)	HP-RYE2 (3)	CICB2	CONDUIT	2.0	
13.1113 0.0130					
MS-RYE2 (5)	HP-RYE2 (2)	HP-RYT3 (1)	CONDUIT	2.8	
0.0109 0.0130					
MS-RYE3 (1)	HP-RYE3 (1)	RYE3	CONDUIT	5.4	
2.2228 0.0300					
MS-RYE3 (2)	RYE3	HP-RYE3 (2)	CONDUIT	14.0	-
2.0719 0.0300					
MS-RYE3 (3)	HP-RYE3 (2)	RYE15	CONDUIT	20.8	
1.9234 0.0300					
MS-RYE3 (4)	RYE3	HP-RYE3 (3)	CONDUIT	2.0	-
7.5212 0.0300					
MS-RYE3 (5)	HP-RYE3 (3)	CBMH4	CONDUIT	2.0	
12.0873 0.0130					
MS-RYE4 (1)	RYE4	HP-RYE4	CONDUIT	22.5	-
2.0004 0.0300					

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 PCSWMM Model Output
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MS-RYE4 (2)	HP-RYE4	RYT7	CONDUIT	13.5	
1.4816 0.0300					
MS-RYE4 (3)	RYE4	HP-RYE4 (2)	CONDUIT	2.0	-
28.6028 0.0300					
MS-RYE4 (4)	HP-RYE4 (2)	RYE13	CONDUIT	2.0	
7.0172 0.0300					
MS-RYE5 (1)	RYE5	HP-RYE5	CONDUIT	14.9	-
2.0138 0.0300					
MS-RYE5 (2)	HP-RYE5	RYT9	CONDUIT	20.5	
1.4636 0.0300					
MS-RYE6 (1)	RYE6	HP-RYE6	CONDUIT	2.0	-
7.0172 0.0300					
MS-RYE6 (2)	HP-RYE6	CBMH8	CONDUIT	2.0	
36.1538 0.0130					
MS-RYE7 (1)	RYE7	HP-RYE7	CONDUIT	2.0	-
7.5212 0.0300					
MS-RYE7 (2)	HP-RYE7	CBMH7	CONDUIT	2.0	
30.8740 0.0130					
MS-RYE8 (1)	RYE8	HP-RYE8	CONDUIT	2.0	-
15.1717 0.0300					
MS-RYE8 (2)	HP-RYE8	RYT17	CONDUIT	2.0	
21.4790 0.0300					
MS-RYE9 (1)	RYE9	HP-RYE9	CONDUIT	2.0	-
11.0672 0.0300					
MS-RYE9 (2)	HP-RYE9	RYT10	CONDUIT	2.0	
6.0108 0.0300					
MS-RYT (1)	RYT11	HP-RYT11 (1)	CONDUIT	7.7	-
1.4287 0.0300					
MS-RYT1 (1)	RYT1	HP-RYT1 (1)	CONDUIT	20.7	-
1.9811 0.0300					
MS-RYT1 (2)	HP-RYT1 (1)	RYE1	CONDUIT	19.6	
1.4798 0.0300					
MS-RYT1 (3)	RYT1	HP-RYT1 (2)	CONDUIT	2.0	-
16.2088 0.0300					
MS-RYT1 (4)	HP-RYT1 (2)	CBMH5	CONDUIT	2.0	
14.6549 0.0130					
MS-RYT10 (1)	RYT10	HP-RYT10 (1)	CONDUIT	2.0	-
5.5083 0.0300					
MS-RYT10 (2)	HP-RYT10 (1)	HP-RYT10 (2)	CONDUIT	2.0	
6.5138 0.0300					
MS-RYT10 (3)	HP-RYT10 (2)	CBMH10	CONDUIT	2.0	
30.8740 0.0130					
MS-RYT11 (2)	HP-RYT11 (1)	RYE10	CONDUIT	21.9	
1.4613 0.0300					
MS-RYT11 (3)	RYT11	HP-RYT11 (2)	CONDUIT	2.0	-
9.5432 0.0300					
MS-RYT11 (4)	HP-RYT11 (2)	CBMH12	CONDUIT	2.0	
11.0672 0.0130					
MS-RYT12	RYT12	CICB1	CONDUIT	2.0	
0.0152 0.0130					
MS-RYT13 (1)	RYT13	HP-RYT13	CONDUIT	2.0	-
6.5138 0.0300					
MS-RYT13 (2)	HP-RYT13	CICB1	CONDUIT	2.0	
15.6896 0.0130					
MS-RYT14 (1)	RYT14	HP-RYT14	CONDUIT	2.0	-
7.0172 0.0300					
MS-RYT14 (2)	HP-RYT14	HP-CBMH2	CONDUIT	2.0	
16.2088 0.0130					
MS-RYT15 (1)	RYT15	HP-RYT15	CONDUIT	2.0	-
5.5083 0.0300					

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MS-RYT15 (2)	HP-RYT15	CBMH13	CONDUIT	2.0	
18.2989 0.0130					
MS-RYT3 (1)	HP-RYT3 (1)	RYT3	CONDUIT	13.3	
1.6544 0.0300					
MS-RYT3 (2)	RYT3	HP-RYT3 (2)	CONDUIT	9.4	-
2.2346 0.0300					
MS-RYT3 (3)	HP-RYT3 (2)	HP-RYT4	CONDUIT	2.8	
0.0109 0.0130					
MS-RYT4 (1)	HP-RYT4	RYT4	CONDUIT	25.0	
1.5602 0.0300					
MS-RYT4 (2)	RYT4	HP-RYT4 (2)	CONDUIT	11.0	-
2.1823 0.0300					
MS-RYT4 (3)	HP-RYT4 (2)	HP-RYT5 (2)	CONDUIT	2.8	
0.0109 0.0130					
MS-RYT5 (1)	RYT5	HP-RYT5 (1)	CONDUIT	2.0	-
7.5212 0.0300					
MS-RYT5 (2)	HP-RYT5 (1)	CBMH14	CONDUIT	2.0	
7.5212 0.0130					
MS-RYT5 (3)	HP-RYT5 (2)	RYT5	CONDUIT	10.1	
2.6742 0.0300					
MS-RYT5 (4)	RYT5	HP-RYT5 (3)	CONDUIT	8.0	-
1.8753 0.0300					
MS-RYT6	RYT6	HP-RYT6	CONDUIT	20.4	-
1.5198 0.0300					
MS-RYT7 (1)	RYT7	HP-RYT7	CONDUIT	28.2	-
1.4895 0.0300					
MS-RYT7 (2)	HP-RYT7	RYT6	CONDUIT	19.5	
2.0004 0.0300					
MS-RYT7 (3)	RYT7	HP-RYT7 (2)	CONDUIT	2.0	-
10.0504 0.0300					
MS-RYT7 (4)	HP-RYT7 (2)	CBMH3	CONDUIT	2.0	
12.5988 0.0130					
MS-RYT8 (1)	RYT8	HP-RYT8 (1)	CONDUIT	18.0	-
1.5002 0.0300					
MS-RYT8 (2)	HP-RYT8 (1)	RYE4	CONDUIT	18.0	
1.5002 0.0300					
MS-RYT8 (3)	RYT8	HP-RYT8 (2)	CONDUIT	2.0	-
12.5988 0.0300					
MS-RYT8 (4)	HP-RYT8 (2)	CBMH2	CONDUIT	2.0	
15.6896 0.0130					
MS-RYT9 (1)	RYT9	HP-RYT9 (1)	CONDUIT	36.0	-
1.6391 0.0300					
MS-RYT9 (2)	HP-RYT9 (1)	RYT8	CONDUIT	36.0	
1.5002 0.0300					
MS-RYT9 (3)	RYT9	HP-RYT9 (2)	CONDUIT	2.0	-
12.5988 0.0300					
MS-RYT9 (4)	HP-RYT9 (2)	CBMH1	CONDUIT	2.0	
18.2989 0.0130					
O-CBMH10	CBMH10	MH106	ORIFICE		
O-CBMH11	CBMH11	MH108	ORIFICE		
O-CBMH13	CBMH13	MH110	ORIFICE		
O-CBMH2	CBMH2	MH106	ORIFICE		
O-CBMH3	CBMH3	MH110	ORIFICE		
O-CICB1	CICB1	MH106	ORIFICE		
O-CICB2	CICB2	MH114	ORIFICE		
O-RYE7	RYE7	MH200	ORIFICE		
O-RYT13	RYT13	MH106	ORIFICE		
O-RYT14	RYT14	MH108	ORIFICE		
O-RYT15	RYT15	MH112	ORIFICE		

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O-CBMH1	CBMH1	MH104	OUTLET
O-CBMH14	CBMH14	MH112	OUTLET
O-CBMH15	CBMH15	MH118	OUTLET
O-CBMH4	CBMH4	MH112	OUTLET
O-CBMH5	CBMH5	MH118	OUTLET
O-CBMH8	CBMH8	MH200	OUTLET

 Cross Section Summary

Full Conduit Flow	Shape	Full Depth	Full Area	Hyd. Rad.	Max. Width	No. of Barrels

100_ (STM) 249.51	CIRCULAR	0.60	0.28	0.15	0.60	1
104_ (STM) 190.50	CIRCULAR	0.60	0.28	0.15	0.60	1
106_ (STM) 59.16	CIRCULAR	0.25	0.05	0.06	0.25	1
116_ (STM) 233.37	CIRCULAR	0.60	0.28	0.15	0.60	1
118_ (STM) 59.44	CIRCULAR	0.25	0.05	0.06	0.25	1
124_ (STM) 42.26	CIRCULAR	0.25	0.05	0.06	0.25	1
128_ (STM) 59.69	CIRCULAR	0.25	0.05	0.06	0.25	1
130_ (STM) 59.25	CIRCULAR	0.25	0.05	0.06	0.25	1
132_ (STM) 257.27	CIRCULAR	0.60	0.28	0.15	0.60	1
136_ (STM) 59.89	CIRCULAR	0.25	0.05	0.06	0.25	1
150_ (1)_ (STM) 41.34	CIRCULAR	0.25	0.05	0.06	0.25	1
152_ (1)_ (STM) 429.92	CIRCULAR	0.60	0.28	0.15	0.60	1
173_ (STM) 59.27	CIRCULAR	0.25	0.05	0.06	0.25	1
175_ (STM) 42.80	CIRCULAR	0.25	0.05	0.06	0.25	1
207_ (STM) 440.45	CIRCULAR	0.60	0.28	0.15	0.60	1
209_ (STM) 234.70	CIRCULAR	0.60	0.28	0.15	0.60	1
229_ (STM) 556.46	CIRCULAR	0.82	0.53	0.21	0.82	1
233_ (STM) 65.02	CIRCULAR	0.30	0.07	0.07	0.30	1
236 (1)_ (STM) 60.13	CIRCULAR	0.25	0.05	0.06	0.25	1
240_ (STM) 101.97	CIRCULAR	0.38	0.11	0.09	0.38	1
250_ (STM) 243.73	CIRCULAR	0.60	0.28	0.15	0.60	1

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 PCSWMM Model Output
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252_(STM) 237.23	CIRCULAR	0.60	0.28	0.15	0.60	1
253_(STM) 59.23	CIRCULAR	0.25	0.05	0.06	0.25	1
260_(STM) 45.28	CIRCULAR	0.25	0.05	0.06	0.25	1
266_(STM) 59.85	CIRCULAR	0.25	0.05	0.06	0.25	1
270_(STM) 219.72	CIRCULAR	0.60	0.28	0.15	0.60	1
277_(STM) 59.93	CIRCULAR	0.25	0.05	0.06	0.25	1
278_(STM) 55.46	CIRCULAR	0.25	0.05	0.06	0.25	1
279_(STM) 59.33	CIRCULAR	0.25	0.05	0.06	0.25	1
281_(STM) 59.93	CIRCULAR	0.25	0.05	0.06	0.25	1
283_(STM) 59.93	CIRCULAR	0.25	0.05	0.06	0.25	1
285_(STM) 65.28	CIRCULAR	0.25	0.05	0.06	0.25	1
286_(STM) 59.93	CIRCULAR	0.25	0.05	0.06	0.25	1
287_(STM) 55.46	CIRCULAR	0.25	0.05	0.06	0.25	1
288_(STM) 252.44	CIRCULAR	0.60	0.28	0.15	0.60	1
304_(STM) 58.51	CIRCULAR	0.25	0.05	0.06	0.25	1
49_(STM) 466.98	CIRCULAR	0.82	0.53	0.21	0.82	1
50_(STM) 88.67	CIRCULAR	0.38	0.11	0.09	0.38	1
51_(STM) 189.55	CIRCULAR	0.53	0.22	0.13	0.53	1
52_(STM) 207.50	CIRCULAR	0.53	0.22	0.13	0.53	1
53_(STM) 228.39	CIRCULAR	0.60	0.28	0.15	0.60	1
55_(STM) 370.91	CIRCULAR	0.75	0.44	0.19	0.75	1
56_(STM) 538.11	CIRCULAR	0.82	0.53	0.21	0.82	1
85_(STM) 40.71	CIRCULAR	0.25	0.05	0.06	0.25	1
87_(STM) 87.67	CIRCULAR	0.38	0.11	0.09	0.38	1
97(1)_(STM) 127.77	CIRCULAR	0.45	0.16	0.11	0.45	1
97_(STM) 86.94	CIRCULAR	0.38	0.11	0.09	0.38	1
MS-CBMH1 (1) 68188.85	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH1 (2) 63947.17	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH1 (3) 66096.82	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH1 (4) 136741.48	RECT_OPEN	1.00	3.00	0.60	3.00	1

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MS-CBMH10 (1) 68188.85	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH10 (2) 34844.26	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH10 (3) 40250.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH11 (1) 47951.44	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH11 (2) 49352.50	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH12 (1) 45024.40	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH12 (2) 93746.62	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH13 (1) 38531.43	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH13 (2) 77030.48	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH14 (1) 38531.43	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH14 (2) 38531.43	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH15 (1) 58273.32	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH15 (2) 71231.45	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH2 60599.46	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH3 (1) 60599.46	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH3 (2) 43489.78	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH3 (3) 40250.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH4 (1) 55859.79	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH4 (2) 65029.60	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH5 63947.17	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH5 (2) 57078.21	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH7 (1) 72222.70	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH7 (2) 57078.21	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH8 (1) 69215.12	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH8 (2) 21977.24	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CICB1 (1) 40250.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CICB1 (2) 71231.45	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CICB2 (1) 52047.05	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CICB2 (2) 75135.17	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE (1) 594.50	TRIANGULAR	0.30	0.45	0.15	3.00	1

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MS-RYE1 18845.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE10 (1) 18156.97	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE10 (2) 19510.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE10 (3) 76087.17	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE12 (1) 20778.96	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE12 (2) 25251.77	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE12 (3) 19510.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE12 (4) 18845.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE15 (1) 570.63	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYE15 (2) 717.64	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYE16 (1) 26259.77	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE16 (2) 69215.12	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE16 (3) 16696.95	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE18 (1) 49352.50	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE18 (2) 57078.21	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE2 (2) 548.30	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYE2 (3) 22553.72	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE2 (4) 59446.62	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE2 (5) 286.67	RECT_OPEN	0.30	0.90	0.25	3.00	1
MS-RYE3 (1) 623.18	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYE3 (2) 601.66	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYE3 (3) 579.70	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYE3 (4) 19510.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE3 (5) 57078.21	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE4 (1) 591.19	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYE4 (2) 508.79	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYE4 (3) 38047.95	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE4 (4) 18845.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE5 (1) 593.17	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYE5 (2) 505.68	TRIANGULAR	0.30	0.45	0.15	3.00	1

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MS-RYE6 (1) 18845.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE6 (2) 98714.78	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE7 (1) 19510.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE7 (2) 91222.33	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE8 (1) 27710.44	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE8 (2) 32971.11	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE9 (1) 23667.10	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE9 (2) 17441.92	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT (1) 499.62	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYT1 (1) 588.32	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYT1 (2) 508.47	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYT1 (3) 28641.95	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT1 (4) 62848.65	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT10 (1) 16696.95	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT10 (2) 18156.97	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT10 (3) 91222.33	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT11 (2) 505.29	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYT11 (3) 21977.24	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT11 (4) 54616.39	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT12 2026.74	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT13 (1) 18156.97	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT13 (2) 65029.60	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT14 (1) 18845.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT14 (2) 66096.82	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT15 (1) 16696.95	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT15 (2) 70229.11	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT3 (1) 537.63	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYT3 (2) 624.84	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYT3 (3) 286.67	RECT_OPEN	0.30	0.90	0.25	3.00	1
MS-RYT4 (1) 522.10	TRIANGULAR	0.30	0.45	0.15	3.00	1

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MS-RYT4 (2)	TRIANGULAR	0.30	0.45	0.15	3.00	1
617.49						
MS-RYT4 (3)	RECT_OPEN	0.30	0.90	0.25	3.00	1
286.67						
MS-RYT5 (1)	RECT_OPEN	1.00	3.00	0.60	3.00	1
19510.57						
MS-RYT5 (2)	RECT_OPEN	1.00	3.00	0.60	3.00	1
45024.40						
MS-RYT5 (3)	TRIANGULAR	0.30	0.45	0.15	3.00	1
683.54						
MS-RYT5 (4)	TRIANGULAR	0.30	0.45	0.15	3.00	1
572.41						
MS-RYT6	TRIANGULAR	0.30	0.45	0.15	3.00	1
515.30						
MS-RYT7 (1)	TRIANGULAR	0.30	0.45	0.15	3.00	1
510.14						
MS-RYT7 (2)	TRIANGULAR	0.30	0.45	0.15	3.00	1
591.19						
MS-RYT7 (3)	RECT_OPEN	1.00	3.00	0.60	3.00	1
22553.72						
MS-RYT7 (4)	RECT_OPEN	1.00	3.00	0.60	3.00	1
58273.32						
MS-RYT8 (1)	TRIANGULAR	0.30	0.45	0.15	3.00	1
511.96						
MS-RYT8 (2)	TRIANGULAR	0.30	0.45	0.15	3.00	1
511.96						
MS-RYT8 (3)	RECT_OPEN	1.00	3.00	0.60	3.00	1
25251.77						
MS-RYT8 (4)	RECT_OPEN	1.00	3.00	0.60	3.00	1
65029.60						
MS-RYT9 (1)	TRIANGULAR	0.30	0.45	0.15	3.00	1
535.14						
MS-RYT9 (2)	TRIANGULAR	0.30	0.45	0.15	3.00	1
511.96						
MS-RYT9 (3)	RECT_OPEN	1.00	3.00	0.60	3.00	1
25251.77						
MS-RYT9 (4)	RECT_OPEN	1.00	3.00	0.60	3.00	1
70229.11						

Analysis Options

Flow Units LPS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method HORTON

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 05/19/2021 00:00:00

Ending Date 05/21/2021 00:00:00

Antecedent Dry Days 0.0

Report Time Step 00:01:00

Wet Time Step 00:02:00
 Dry Time Step 00:05:00
 Routing Time Step 1.00 sec
 Variable Time Step YES
 Maximum Trials 8
 Number of Threads 4
 Head Tolerance 0.001500 m

	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm
*****	-----	-----
Initial LID Storage	0.001	0.348
Total Precipitation	0.262	71.667
Evaporation Loss	0.000	0.000
Infiltration Loss	0.104	28.470
Surface Runoff	0.158	43.395
Final Storage	0.001	0.348
Continuity Error (%)	-0.275	

	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.158	1.584
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.001	0.005
External Outflow	0.159	1.589
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.012	0.117
Final Stored Volume	0.012	0.118
Continuity Error (%)	-0.019	

 Highest Continuity Errors

 Node CBMH8 (1.26%)
 Node MH200 (-1.19%)

 Time-Step Critical Elements

 None

 Highest Flow Instability Indexes

 Link O-CBMH3 (139)
 Link O-RYE7 (132)
 Link O-CBMH1 (87)

Link O-CBMH8 (69)
 Link O-CBMH10 (26)

 Most Frequent Nonconverging Nodes

 Convergence obtained at all time steps.

 Routing Time Step Summary

 Minimum Time Step : 0.50 sec
 Average Time Step : 1.00 sec
 Maximum Time Step : 1.00 sec
 % of Time in Steady State : 0.00
 Average Iterations per Step : 2.00
 % of Steps Not Converging : 0.00
 Time Step Frequencies :
 1.000 - 0.871 sec : 99.73 %
 0.871 - 0.758 sec : 0.20 %
 0.758 - 0.660 sec : 0.04 %
 0.660 - 0.574 sec : 0.01 %
 0.574 - 0.500 sec : 0.02 %

 Subcatchment Runoff Summary

Perv	Total	Total	Total	Total	Total	Total	Imperv
Runoff	Runoff	Precip	Peak	Runoff	Evap	Infil	Runoff
Subcatchment	Runoff	Runoff	Runoff	Runoff	mm	mm	mm
mm	mm	10^6 ltr	mm	Coeff			

A1			71.67	0.00	0.00	41.18	5.02
25.69	30.71	0.01	11.51	0.429			
A10			71.67	0.00	0.00	38.77	9.32
23.74	33.06	0.04	39.63	0.461			
A11			71.67	0.00	0.00	19.53	40.24
12.10	52.34	0.08	65.50	0.730			
A12			71.67	0.00	0.00	17.22	43.82
10.84	54.66	0.06	50.03	0.763			
A13			71.67	0.00	0.00	12.79	51.03
8.08	59.11	0.02	14.01	0.825			
A14			71.67	0.00	0.00	41.05	5.02
25.84	30.86	0.01	15.92	0.431			
A15			71.67	0.00	0.00	23.59	33.76
14.50	48.26	0.06	54.25	0.673			
A16			71.67	0.00	0.00	38.03	10.04
23.82	33.86	0.02	19.90	0.472			
A17			71.67	0.00	0.00	25.22	31.62
14.99	46.61	0.07	57.01	0.650			

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A18			71.67	0.00	0.00	19.97	39.52
12.38	51.89	0.12	104.59	0.724			
A19			71.67	0.00	0.00	31.81	20.08
19.97	40.05	0.03	29.20	0.559			
A2			71.67	0.00	0.00	18.19	42.40
11.29	53.69	0.07	57.53	0.749			
A20			71.67	0.00	0.00	38.51	9.32
24.04	33.36	0.03	39.15	0.466			
A21			71.67	0.00	0.00	41.06	5.02
25.84	30.85	0.02	23.89	0.431			
A22			71.67	0.00	0.00	31.51	20.80
19.52	40.32	0.04	36.06	0.563			
A23_1			71.67	0.00	0.00	30.20	23.70
17.91	41.61	0.06	49.83	0.581			
A23_2			71.67	0.00	0.00	30.20	23.70
17.91	41.61	0.04	34.84	0.581			
A24			71.67	0.00	0.00	23.65	33.77
14.43	48.20	0.05	45.09	0.673			
A25			71.67	0.00	0.00	18.59	41.67
11.61	53.28	0.07	62.38	0.743			
A26			71.67	0.00	0.00	30.64	22.24
18.96	41.19	0.03	32.12	0.575			
A27			71.67	0.00	0.00	40.40	6.45
25.01	31.47	0.05	55.85	0.439			
A28			71.67	0.00	0.00	18.55	41.66
11.66	53.32	0.06	54.13	0.744			
A29			71.67	0.00	0.00	41.36	5.02
25.48	30.50	0.02	18.09	0.426			
A3			71.67	0.00	0.00	38.20	10.04
23.61	33.65	0.04	45.21	0.470			
A31			71.67	0.00	0.00	38.18	10.04
23.64	33.67	0.02	18.96	0.470			
A32			71.67	0.00	0.00	21.73	36.63
13.50	50.13	0.05	43.26	0.699			
A4			71.67	0.00	0.00	20.40	38.79
12.67	51.46	0.07	56.72	0.718			
A5			71.67	0.00	0.00	31.81	20.08
19.98	40.06	0.03	29.24	0.559			
A6			71.67	0.00	0.00	41.88	5.02
24.91	29.93	0.06	57.39	0.418			
A7			71.67	0.00	0.00	17.43	43.86
10.59	54.45	0.04	34.30	0.760			
A8			71.67	0.00	0.00	19.53	40.24
12.10	52.33	0.08	65.47	0.730			
A9			71.67	0.00	0.00	31.81	20.08
19.97	40.05	0.03	29.18	0.559			
U1			71.67	0.00	0.00	37.68	10.03
24.29	34.32	0.03	38.88	0.479			
U2			71.67	0.00	0.00	38.63	8.60
24.74	33.34	0.01	12.77	0.465			
U3			71.67	0.00	0.00	40.57	5.02
26.53	31.55	0.02	21.58	0.440			
U4			71.67	0.00	0.00	31.30	20.79
19.79	40.58	0.04	38.45	0.566			
U5			71.67	0.00	0.00	31.47	20.80
19.58	40.38	0.02	20.32	0.563			

Node Depth Summary

Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days hr:min	Reported Max Depth Meters
CBMH4-Dummy	JUNCTION	0.10	2.27	97.49	0 01:30	2.27
HP-CBMH1	JUNCTION	0.00	0.00	97.08	0 00:00	0.00
HP-CBMH1 (2)	JUNCTION	0.00	0.00	97.06	0 00:00	0.00
HP-CBMH10	JUNCTION	0.00	0.00	97.20	0 00:00	0.00
HP-CBMH11	JUNCTION	0.00	0.01	97.26	0 01:14	0.01
HP-CBMH12	JUNCTION	0.00	0.00	97.70	0 00:00	0.00
HP-CBMH13	JUNCTION	0.00	0.00	97.66	0 00:00	0.00
HP-CBMH14	JUNCTION	0.00	0.04	97.38	0 01:14	0.04
HP-CBMH15	JUNCTION	0.00	0.00	97.75	0 00:00	0.00
HP-CBMH2	JUNCTION	0.00	0.01	97.12	0 01:10	0.01
HP-CBMH3	JUNCTION	0.00	0.01	97.38	0 01:14	0.01
HP-CBMH4	JUNCTION	0.00	0.00	97.54	0 00:00	0.00
HP-CBMH5	JUNCTION	0.00	0.00	97.68	0 00:00	0.00
HP-CBMH7	JUNCTION	0.00	0.00	97.16	0 00:00	0.00
HP-CBMH8	JUNCTION	0.00	0.00	97.27	0 00:00	0.00
HP-CICB1	JUNCTION	0.00	0.01	97.12	0 01:10	0.01
HP-CICB2	JUNCTION	0.00	0.01	97.65	0 01:10	0.01
HP-RYE10	JUNCTION	0.00	0.00	97.50	0 00:00	0.00
HP-RYE12	JUNCTION	0.00	0.00	97.33	0 00:00	0.00
HP-RYE12 (2)	JUNCTION	0.00	0.00	97.31	0 01:11	0.00
HP-RYE15	JUNCTION	0.00	0.00	97.68	0 00:00	0.00
HP-RYE16 (1)	JUNCTION	0.00	0.00	97.85	0 00:00	0.00
HP-RYE18	JUNCTION	0.00	0.02	97.00	0 01:47	0.02
HP-RYE2 (1)	JUNCTION	0.00	0.00	97.68	0 00:00	0.00
HP-RYE2 (2)	JUNCTION	0.00	0.00	97.66	0 00:00	0.00
HP-RYE2 (3)	JUNCTION	0.00	0.00	97.70	0 00:00	0.00
HP-RYE3 (1)	JUNCTION	0.00	0.00	97.52	0 00:00	0.00
HP-RYE3 (2)	JUNCTION	0.00	0.00	97.69	0 00:00	0.00
HP-RYE3 (3)	JUNCTION	0.00	0.00	97.55	0 00:00	0.00
HP-RYE4	JUNCTION	0.00	0.00	97.35	0 00:00	0.00
HP-RYE4 (2)	JUNCTION	0.00	0.00	97.45	0 00:00	0.00
HP-RYE5	JUNCTION	0.00	0.00	97.15	0 00:00	0.00
HP-RYE6	JUNCTION	0.00	0.00	97.60	0 00:00	0.00
HP-RYE7	JUNCTION	0.00	0.00	97.37	0 00:00	0.00
HP-RYE8	JUNCTION	0.00	0.00	97.50	0 00:00	0.00
HP-RYE9	JUNCTION	0.00	0.00	97.59	0 00:00	0.00
HP-RYT1 (1)	JUNCTION	0.00	0.00	97.76	0 00:00	0.00
HP-RYT1 (2)	JUNCTION	0.00	0.00	97.67	0 00:00	0.00
HP-RYT10 (1)	JUNCTION	0.00	0.00	97.58	0 00:00	0.00
HP-RYT10 (2)	JUNCTION	0.00	0.00	97.45	0 00:00	0.00
HP-RYT11 (1)	JUNCTION	0.00	0.00	97.69	0 00:00	0.00
HP-RYT11 (2)	JUNCTION	0.00	0.00	97.77	0 01:10	0.00
HP-RYT13	JUNCTION	0.00	0.00	97.30	0 01:11	0.00
HP-RYT14	JUNCTION	0.00	0.00	97.43	0 00:00	0.00
HP-RYT15	JUNCTION	0.00	0.00	97.59	0 01:10	0.00
HP-RYT3 (1)	JUNCTION	0.00	0.00	97.66	0 00:00	0.00
HP-RYT3 (2)	JUNCTION	0.00	0.00	97.65	0 00:00	0.00
HP-RYT4	JUNCTION	0.00	0.00	97.65	0 00:00	0.00
HP-RYT4 (2)	JUNCTION	0.00	0.00	97.50	0 00:00	0.00
HP-RYT5 (1)	JUNCTION	0.00	0.01	97.39	0 01:14	0.01

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HP-RYT5 (2)	JUNCTION	0.00	0.00	97.50	0	00:00	0.00
HP-RYT5 (3)	JUNCTION	0.00	0.01	97.39	0	01:12	0.01
HP-RYT6	JUNCTION	0.00	0.00	97.49	0	00:00	0.00
HP-RYT7	JUNCTION	0.00	0.00	97.57	0	00:00	0.00
HP-RYT7 (2)	JUNCTION	0.00	0.00	97.35	0	00:00	0.00
HP-RYT8 (1)	JUNCTION	0.00	0.00	97.17	0	00:00	0.00
HP-RYT8 (2)	JUNCTION	0.00	0.00	97.15	0	00:00	0.00
HP-RYT9 (1)	JUNCTION	0.00	0.00	97.44	0	00:00	0.00
HP-RYT9 (2)	JUNCTION	0.00	0.00	97.10	0	00:00	0.00
HP-RYE1	OUTFALL	0.00	0.00	97.61	0	00:00	0.00
HP-RYE16 (2)	OUTFALL	0.00	0.00	97.69	0	00:00	0.00
MH1013	OUTFALL	0.97	0.97	95.05	0	00:00	0.97
OF1	OUTFALL	0.00	0.00	97.00	0	00:00	0.00
OF2	OUTFALL	0.00	0.00	97.73	0	00:00	0.00
OF3	OUTFALL	0.00	0.00	97.15	0	00:00	0.00
OF4	OUTFALL	0.00	0.00	96.85	0	00:00	0.00
OF5	OUTFALL	0.00	0.00	0.00	0	00:00	0.00
CBMH1	STORAGE	0.48	2.23	97.00	0	01:47	2.23
CBMH10	STORAGE	0.24	2.17	97.02	0	01:24	2.17
CBMH11	STORAGE	0.20	2.35	97.25	0	01:22	2.35
CBMH12	STORAGE	0.04	2.10	97.25	0	01:23	2.10
CBMH13	STORAGE	0.18	2.47	97.38	0	01:14	2.47
CBMH14	STORAGE	0.12	2.30	97.39	0	01:14	2.30
CBMH15	STORAGE	0.14	2.31	97.66	0	01:33	2.31
CBMH2	STORAGE	0.27	2.25	97.11	0	01:22	2.25
CBMH3	STORAGE	0.14	2.31	97.29	0	01:25	2.31
CBMH4	STORAGE	0.11	2.37	97.49	0	01:30	2.37
CBMH5	STORAGE	0.45	2.32	97.61	0	01:42	2.32
CBMH7	STORAGE	0.47	0.54	95.12	0	01:10	0.54
CBMH8	STORAGE	0.32	2.30	97.15	0	01:33	2.30
CICB1	STORAGE	0.03	1.70	97.12	0	01:10	1.70
CICB2	STORAGE	0.02	1.62	97.66	0	01:10	1.62
MH100	STORAGE	0.95	0.96	95.06	0	01:10	0.96
MH102	STORAGE	0.92	0.94	95.07	0	01:10	0.94
MH104	STORAGE	0.90	0.93	95.08	0	01:10	0.93
MH106	STORAGE	0.74	0.80	95.11	0	01:10	0.80
MH108	STORAGE	0.52	0.61	95.14	0	01:10	0.61
MH110	STORAGE	0.40	0.50	95.15	0	01:10	0.50
MH112	STORAGE	0.26	0.38	95.17	0	01:11	0.38
MH114	STORAGE	0.01	0.15	95.24	0	01:21	0.15
MH116	STORAGE	0.01	0.13	95.25	0	01:21	0.13
MH118	STORAGE	0.01	0.11	95.26	0	01:21	0.11
MH200	STORAGE	0.36	0.44	95.13	0	01:10	0.43
MH202	STORAGE	0.29	2.27	97.15	0	01:33	2.27
MH204	STORAGE	0.16	2.10	97.03	0	01:23	2.10
MH206	STORAGE	0.13	2.19	97.67	0	01:33	2.19
RYE1	STORAGE	0.13	1.62	97.61	0	01:43	1.62
RYE10	STORAGE	0.03	1.78	97.25	0	01:20	1.78
RYE11	STORAGE	0.02	1.56	97.20	0	01:10	1.56
RYE12	STORAGE	0.01	1.55	97.31	0	01:11	1.55
RYE13	STORAGE	0.01	1.54	97.45	0	01:11	1.53
RYE14	STORAGE	0.01	1.54	97.64	0	01:10	1.53
RYE15	STORAGE	0.14	1.75	97.61	0	01:41	1.75
RYE16	STORAGE	0.10	1.89	97.67	0	01:33	1.88
RYE17	STORAGE	0.02	1.45	97.71	0	01:10	1.45
RYE18	STORAGE	0.31	2.06	97.00	0	01:47	2.06
RYE2	STORAGE	0.08	2.02	97.53	0	01:10	2.02

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RYE3	STORAGE	0.03	1.48	97.44	0	01:10	1.48
RYE4	STORAGE	0.07	1.87	97.13	0	01:12	1.87
RYE5	STORAGE	0.20	1.86	97.00	0	01:45	1.86
RYE6	STORAGE	0.09	1.70	97.15	0	01:34	1.70
RYE7	STORAGE	0.02	0.83	95.86	0	01:10	0.81
RYE8	STORAGE	0.04	1.93	97.08	0	01:11	1.90
RYE9	STORAGE	0.04	1.87	97.03	0	01:23	1.87
RYT1	STORAGE	0.17	2.02	97.61	0	01:41	2.02
RYT10	STORAGE	0.12	2.06	97.03	0	01:23	2.06
RYT11	STORAGE	0.04	2.09	97.25	0	01:23	2.09
RYT12	STORAGE	0.02	1.68	97.13	0	01:10	1.68
RYT13	STORAGE	0.01	1.71	97.30	0	01:11	1.71
RYT14	STORAGE	0.01	1.71	97.43	0	01:11	1.70
RYT15	STORAGE	0.01	1.69	97.60	0	01:10	1.68
RYT16	STORAGE	0.02	1.59	97.66	0	01:10	1.59
RYT17	STORAGE	0.12	2.06	97.03	0	01:23	2.06
RYT3	STORAGE	0.10	2.00	97.40	0	01:11	1.99
RYT4	STORAGE	0.11	2.16	97.39	0	01:11	2.16
RYT5	STORAGE	0.12	2.28	97.39	0	01:14	2.28
RYT6	STORAGE	0.04	1.73	97.35	0	01:12	1.73
RYT7	STORAGE	0.06	2.16	97.30	0	01:23	2.16
RYT8	STORAGE	0.24	2.22	97.11	0	01:23	2.22
RYT9	STORAGE	0.46	2.21	97.00	0	01:46	2.21

 Node Inflow Summary

Total Flow		Maximum Lateral	Maximum Total	Time of Max		Lateral Inflow	
Inflow Volume	Balance Error	Inflow	Inflow	Occurrence		Volume	
Node ltr	Type Percent	LPS	LPS	days	hr:min	10^6 ltr	10^6

CBMH4-Dummy	JUNCTION	0.00	6.51	0	01:00	0	
0.00204	-11.678						
HP-CBMH1	JUNCTION	0.00	0.00	0	00:00	0	
0 0.000 ltr							
HP-CBMH1 (2)	JUNCTION	0.00	0.00	0	00:00	0	
0 0.000 ltr							
HP-CBMH10	JUNCTION	0.00	0.00	0	00:00	0	
0 0.000 ltr							
HP-CBMH11	JUNCTION	0.00	17.71	0	01:14	0	
0.00933	0.001						
HP-CBMH12	JUNCTION	0.00	0.00	0	00:00	0	
0 0.000 ltr							
HP-CBMH13	JUNCTION	0.00	0.00	0	00:00	0	
0 0.000 ltr							
HP-CBMH14	JUNCTION	0.00	67.30	0	01:12	0	
0.0442	-0.007						
HP-CBMH15	JUNCTION	0.00	0.00	0	00:00	0	
0 0.000 ltr							

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HP-CBMH2	JUNCTION	0.00	30.11	0	01:10	0
0.0162 0.093						
HP-CBMH3	JUNCTION	0.00	45.10	0	01:14	0
0.0238 -0.000						
HP-CBMH4	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-CBMH5	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-CBMH7	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-CBMH8	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-CICB1	JUNCTION	0.00	31.82	0	01:10	0
0.0156 0.128						
HP-CICB2	JUNCTION	0.00	53.95	0	01:10	0
0.0216 0.150						
HP-RYE10	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE12	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE12(2)	JUNCTION	0.00	2.81	0	01:11	0
0.000143 0.027						
HP-RYE15	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE16(1)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE18	JUNCTION	0.00	5.83	0	01:25	0
0.00907 -0.010						
HP-RYE2(1)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE2(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE2(3)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE3(1)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE3(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE3(3)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE4	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE4(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE5	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE6	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE7	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE8	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE9	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT1(1)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT1(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT10(1)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						

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HP-RYT10(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT11(1)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT11(2)	JUNCTION	14.01	14.01	0	01:10	0.0177
0.0177 -0.040						
HP-RYT13	JUNCTION	0.00	2.31	0	01:11	0
4.33e-05 0.003						
HP-RYT14	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT15	JUNCTION	0.00	10.27	0	01:10	0
0.000516 -0.008						
HP-RYT3(1)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT3(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT4	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT4(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT5(1)	JUNCTION	0.00	16.60	0	01:14	0
0.00623 0.000						
HP-RYT5(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT5(3)	JUNCTION	0.00	0.99	0	01:11	0
1.73e-05 0.000 ltr						
HP-RYT6	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT7	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT7(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT8(1)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT8(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT9(1)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT9(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE1	OUTFALL	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE16(2)	OUTFALL	0.00	0.00	0	00:00	0
0 0.000 ltr						
MH1013	OUTFALL	0.00	316.44	0	01:10	0
1.48 0.000						
OF1	OUTFALL	38.88	38.88	0	01:10	0.0309
0.0309 0.000						
OF2	OUTFALL	21.58	21.58	0	01:10	0.0158
0.0158 0.000						
OF3	OUTFALL	12.77	12.77	0	01:10	0.01
0.01 0.000						
OF4	OUTFALL	38.45	38.45	0	01:10	0.0365
0.0365 0.000						
OF5	OUTFALL	20.32	20.32	0	01:10	0.0202
0.0202 0.000						
CBMH1	STORAGE	49.83	133.95	0	01:09	0.0588
0.152 -0.313						
CBMH10	STORAGE	57.01	83.96	0	01:11	0.0699
0.151 0.006						

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CBMH11		STORAGE	54.25	65.54	0	01:10	0.0627
0.11	0.032						
CBMH12		STORAGE	0.00	24.79	0	01:04	0
0.0405	-0.011						
CBMH13		STORAGE	50.03	91.59	0	01:11	0.0601
0.104	-0.011						
CBMH14		STORAGE	34.30	128.92	0	01:10	0.0436
0.147	-0.046						
CBMH15		STORAGE	57.53	73.68	0	01:07	0.0698
0.0918	0.003						
CBMH2		STORAGE	104.59	151.53	0	01:09	0.125
0.184	-0.018						
CBMH3		STORAGE	65.50	84.82	0	01:10	0.0785
0.142	0.017						
CBMH4		STORAGE	65.47	65.47	0	01:10	0.0785
0.0808	0.044						
CBMH5		STORAGE	56.72	83.94	0	01:09	0.0669
0.118	-0.002						
CBMH7		STORAGE	62.38	84.29	0	01:10	0.0746
0.177	-0.008						
CBMH8		STORAGE	54.13	75.10	0	01:07	0.064
0.0956	1.281						
CICB1		STORAGE	45.09	80.84	0	01:10	0.053
0.0927	-0.003						
CICB2		STORAGE	43.26	72.38	0	01:10	0.0501
0.079	-0.002						
MH100		STORAGE	0.00	315.90	0	01:10	0
1.48	-0.000						
MH102		STORAGE	0.00	315.13	0	01:10	0
1.48	-0.000						
MH104		STORAGE	0.00	313.63	0	01:10	0
1.49	0.031						
MH106		STORAGE	0.00	235.91	0	01:12	0
1.17	0.000						
MH108		STORAGE	0.00	151.87	0	01:12	0
0.773	0.000						
MH110		STORAGE	0.00	111.63	0	01:12	0
0.644	-0.002						
MH112		STORAGE	0.00	65.00	0	01:11	0
0.43	-0.001						
MH114		STORAGE	0.00	31.12	0	01:20	0
0.243	0.002						
MH116		STORAGE	0.00	12.94	0	01:33	0
0.186	0.002						
MH118		STORAGE	0.00	12.91	0	01:38	0
0.186	-0.000						
MH200		STORAGE	0.00	22.72	0	01:10	0
0.103	-1.176						
MH202		STORAGE	0.00	30.73	0	01:06	0
0.0297	-0.061						
MH204		STORAGE	0.00	53.47	0	01:10	0
0.0879	-0.002						
MH206		STORAGE	0.00	31.38	0	01:06	0
0.0255	-0.051						
RYE1		STORAGE	0.00	14.96	0	01:02	0
0.00547	-0.043						
RYE10		STORAGE	15.92	15.92	0	01:10	0.0123
0.0126	-0.065						
RYE11		STORAGE	36.06	36.06	0	01:10	0.0363
0.0363	-0.007						

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RYE12		STORAGE	32.12	32.12	0	01:10	0.033
0.033	-0.014						
RYE13		STORAGE	29.20	29.20	0	01:10	0.028
0.028	-0.021						
RYE14		STORAGE	29.18	29.18	0	01:10	0.028
0.028	-0.009						
RYE15		STORAGE	0.00	18.15	0	01:07	0
0.0078	0.006						
RYE16		STORAGE	11.51	14.09	0	01:06	0.00921
0.0127	0.078						
RYE17		STORAGE	29.24	29.24	0	01:10	0.028
0.028	-0.009						
RYE18		STORAGE	34.84	34.84	0	01:10	0.0411
0.0435	-0.001						
RYE2		STORAGE	57.39	57.39	0	01:10	0.0569
0.0569	-0.052						
RYE3		STORAGE	39.63	39.63	0	01:10	0.0364
0.0364	-0.103						
RYE4		STORAGE	39.15	39.15	0	01:10	0.0334
0.0339	0.012						
RYE5		STORAGE	23.89	23.89	0	01:10	0.0185
0.0192	-0.002						
RYE6		STORAGE	18.96	18.96	0	01:10	0.0168
0.0172	0.015						
RYE7		STORAGE	18.09	18.09	0	01:10	0.0153
0.0177	0.277						
RYE8		STORAGE	55.85	55.85	0	01:10	0.0472
0.0472	-0.010						
RYE9		STORAGE	19.90	19.90	0	01:10	0.0169
0.0169	-0.020						
RYT1		STORAGE	45.21	65.57	0	01:07	0.0404
0.0642	0.049						
RYT10		STORAGE	0.00	26.01	0	01:10	0
0.0237	0.017						
RYT11		STORAGE	0.00	18.19	0	01:03	0
0.0213	-0.006						
RYT12		STORAGE	0.00	35.99	0	01:10	0
0.0368	0.003						
RYT13		STORAGE	0.00	26.30	0	01:09	0
0.033	0.009						
RYT14		STORAGE	0.00	23.85	0	01:09	0
0.028	0.008						
RYT15		STORAGE	0.00	28.83	0	01:10	0
0.028	-0.002						
RYT16		STORAGE	0.00	29.19	0	01:10	0
0.0289	0.010						
RYT17		STORAGE	0.00	49.73	0	01:10	0
0.0481	-0.011						
RYT3		STORAGE	0.00	60.67	0	01:05	0
0.0588	0.020						
RYT4		STORAGE	0.00	68.37	0	01:05	0
0.0762	0.040						
RYT5		STORAGE	0.00	69.40	0	01:09	0
0.0989	0.014						
RYT6		STORAGE	0.00	35.54	0	01:10	0
0.0396	0.048						
RYT7		STORAGE	0.00	28.95	0	01:05	0
0.0502	0.311						
RYT8		STORAGE	0.00	52.60	0	01:04	0
0.0462	0.028						

Iron Valley II - 5331 Fernbank Road (121011)
 PCSWMM Model Output
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RYT9 STORAGE 0.00 40.83 0 01:06 0
 0.0327 0.002

 Node Surcharge Summary

Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Meters	Min. Depth Below Rim Meters
CBMH4-Dummy	JUNCTION	2.23	1.666	0.734
MH204	STORAGE	1.25	1.498	0.102
RYE17	STORAGE	0.60	1.200	0.950

 Node Flooding Summary

No nodes were flooded.

 Storage Volume Summary

Max	Maximum	Average	Avg	Evap	Exfil	Maximum	Max	Time of
Occurrence	Outflow	Volume	Pcnt	Pcnt	Pcnt	Volume	Pcnt	
Storage Unit		1000 m ³	Full	Loss	Loss	1000 m ³	Full	days
hr:min	LPS							
CBMH1		0.004	0.5	0.0	0.0	0.068	7.2	0
01:47	43.36							
CBMH10		0.000	0.1	0.0	0.0	0.019	3.1	0
01:24	46.26							
CBMH11		0.001	0.1	0.0	0.0	0.021	3.8	0
01:22	32.83							
CBMH12		0.000	1.3	0.0	0.0	0.002	61.7	0
01:23	24.20							
CBMH13		0.000	0.1	0.0	0.0	0.017	2.9	0
01:14	67.00							
CBMH14		0.000	0.1	0.0	0.0	0.010	3.2	0
01:14	75.79							
CBMH15		0.001	0.1	0.0	0.0	0.030	3.0	0
01:33	37.78							
CBMH2		0.002	0.2	0.0	0.0	0.062	8.0	0
01:22	64.44							
CBMH3		0.001	0.1	0.0	0.0	0.039	3.9	0
01:25	46.66							

Iron Valley II - 5331 Fernbank Road (121011)
 PCSWMM Model Output
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CBMH4		0.001	0.1	0.0	0.0	0.034	3.4	0
01:30	11.19							
CBMH5		0.002	0.3	0.0	0.0	0.037	5.8	0
01:42	36.81							
CBMH7		0.001	0.1	0.0	0.0	0.001	0.1	0
01:10	84.13							
CBMH8		0.001	0.2	0.0	0.0	0.029	5.8	0
01:33	30.97							
CICB1		0.000	0.9	0.0	0.0	0.001	62.6	0
01:10	80.78							
CICB2		0.000	0.9	0.0	0.0	0.001	63.4	0
01:10	72.30							
MH100		0.002	33.2	0.0	0.0	0.002	33.6	0
01:10	316.44							
MH102		0.002	31.7	0.0	0.0	0.002	32.5	0
01:10	315.90							
MH104		0.002	31.3	0.0	0.0	0.002	32.3	0
01:10	315.13							
MH106		0.001	26.5	0.0	0.0	0.001	28.7	0
01:10	236.48							
MH108		0.001	19.0	0.0	0.0	0.001	22.3	0
01:10	152.29							
MH110		0.000	14.8	0.0	0.0	0.001	18.6	0
01:10	112.28							
MH112		0.000	9.7	0.0	0.0	0.000	14.0	0
01:11	68.75							
MH114		0.000	0.5	0.0	0.0	0.000	6.2	0
01:21	31.12							
MH116		0.000	0.4	0.0	0.0	0.000	5.2	0
01:21	13.09							
MH118		0.000	0.4	0.0	0.0	0.000	4.3	0
01:21	12.94							
MH200		0.000	14.5	0.0	0.0	0.000	17.5	0
01:10	24.28							
MH202		0.001	11.6	0.0	0.0	0.004	90.4	0
01:33	25.41							
MH204		0.000	7.5	0.0	0.0	0.002	95.4	0
01:23	50.42							
MH206		0.000	5.6	0.0	0.0	0.002	95.9	0
01:33	20.95							
RYE1		0.000	5.1	0.0	0.0	0.000	65.3	0
01:43	6.22							
RYE10		0.000	1.2	0.0	0.0	0.000	61.4	0
01:20	13.65							
RYE11		0.000	0.8	0.0	0.0	0.000	62.5	0
01:10	35.99							
RYE12		0.000	0.5	0.0	0.0	0.000	64.7	0
01:11	26.30							
RYE13		0.000	0.4	0.0	0.0	0.000	64.0	0
01:11	23.85							
RYE14		0.000	0.4	0.0	0.0	0.000	64.3	0
01:10	28.83							
RYE15		0.000	5.5	0.0	0.0	0.000	69.4	0
01:41	2.21							
RYE16		0.000	3.7	0.0	0.0	0.000	67.3	0
01:33	19.29							
RYE17		0.000	0.7	0.0	0.0	0.000	60.4	0
01:10	29.19							
RYE18		0.000	10.8	0.0	0.0	0.000	72.1	0
01:47	32.96							

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RYE2		0.000	2.7	0.0	0.0	0.000	67.6	0
01:10	55.36							
RYE3		0.000	1.4	0.0	0.0	0.000	60.8	0
01:10	35.54							
RYE4		0.000	2.8	0.0	0.0	0.000	70.8	0
01:12	22.73							
RYE5		0.000	7.2	0.0	0.0	0.000	68.7	0
01:45	24.80							
RYE6		0.000	3.1	0.0	0.0	0.000	56.5	0
01:34	19.95							
RYE7		0.000	0.7	0.0	0.0	0.000	25.9	0
01:10	16.21							
RYE8		0.000	1.3	0.0	0.0	0.000	63.1	0
01:11	49.73							
RYE9		0.000	1.2	0.0	0.0	0.000	58.2	0
01:23	14.06							
RYT1		0.000	6.2	0.0	0.0	0.002	73.1	0
01:41	38.54							
RYT10		0.000	3.6	0.0	0.0	0.002	58.8	0
01:23	13.87							
RYT11		0.000	1.2	0.0	0.0	0.002	61.1	0
01:23	16.73							
RYT12		0.000	0.9	0.0	0.0	0.000	64.2	0
01:10	36.11							
RYT13		0.000	0.5	0.0	0.0	0.000	66.3	0
01:11	21.21							
RYT14		0.000	0.4	0.0	0.0	0.000	66.5	0
01:11	18.89							
RYT15		0.000	0.4	0.0	0.0	0.000	65.6	0
01:10	29.01							
RYT16		0.000	0.8	0.0	0.0	0.000	62.0	0
01:10	29.30							
RYT17		0.000	4.0	0.0	0.0	0.000	66.2	0
01:23	37.93							
RYT3		0.000	3.3	0.0	0.0	0.000	65.6	0
01:11	64.66							
RYT4		0.000	3.5	0.0	0.0	0.000	71.4	0
01:11	51.71							
RYT5		0.000	3.8	0.0	0.0	0.000	73.0	0
01:14	64.96							
RYT6		0.000	1.8	0.0	0.0	0.000	67.5	0
01:12	25.57							
RYT7		0.000	2.0	0.0	0.0	0.000	71.6	0
01:23	21.73							
RYT8		0.000	8.1	0.0	0.0	0.003	73.9	0
01:23	33.90							
RYT9		0.001	15.0	0.0	0.0	0.002	72.3	0
01:46	33.93							

 Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow LPS	Max Flow LPS	Total Volume 10^6 ltr
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Iron Valley II - 5331 Fernbank Road (121011)
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HP-RYE1	0.00	0.00	0.00	0.000
HP-RYE16(2)	0.00	0.00	0.00	0.000
MH1013	78.58	11.07	316.44	1.481
OF1	6.36	3.04	38.88	0.031
OF2	6.30	1.58	21.58	0.016
OF3	6.30	0.99	12.77	0.010
OF4	6.43	3.50	38.45	0.037
OF5	6.41	1.93	20.32	0.020

System	13.80	22.12	443.31	1.595

 Link Flow Summary

Link	Type	Maximum	Time of Max		Maximum	Max/	Max/
		Flow	Occurrence		Veloc	Full	Full
		LPS	days	hr:min	m/sec	Flow	Depth

100_(STM)	CONDUIT	25.41	0	01:07	0.09	0.10	1.00
104_(STM)	CONDUIT	37.26	0	01:06	0.13	0.20	1.00
106_(STM)	CONDUIT	24.80	0	01:07	0.51	0.42	1.00
116_(STM)	CONDUIT	45.26	0	01:04	0.16	0.19	1.00
118_(STM)	CONDUIT	22.73	0	01:10	0.46	0.38	1.00
124_(STM)	CONDUIT	28.95	0	01:05	0.59	0.68	1.00
128_(STM)	CONDUIT	25.57	0	01:11	0.52	0.43	1.00
130_(STM)	CONDUIT	35.54	0	01:10	0.88	0.60	1.00
132_(STM)	CONDUIT	30.93	0	01:07	0.11	0.12	1.00
136_(STM)	CONDUIT	19.95	0	01:07	0.43	0.33	1.00
150_(1)_(STM)	CONDUIT	55.36	0	01:10	1.13	1.34	1.00
152_(1)_(STM)	CONDUIT	64.66	0	01:10	0.35	0.15	1.00
173_(STM)	CONDUIT	14.96	0	01:02	0.33	0.25	1.00
175_(STM)	CONDUIT	24.20	0	01:11	0.49	0.57	1.00
207_(STM)	CONDUIT	64.96	0	01:05	0.24	0.15	1.00
209_(STM)	CONDUIT	6.51	0	01:00	0.11	0.03	1.00
229_(STM)	CONDUIT	315.13	0	01:10	0.59	0.57	1.00
233_(STM)	CONDUIT	50.42	0	01:11	0.71	0.78	1.00
236(1)_(STM)	CONDUIT	49.73	0	01:10	1.01	0.83	1.00
240_(STM)	CONDUIT	12.94	0	01:33	0.56	0.13	0.32
250_(STM)	CONDUIT	37.93	0	01:11	0.13	0.16	1.00
252_(STM)	CONDUIT	13.87	0	01:11	0.06	0.06	1.00
253_(STM)	CONDUIT	14.06	0	01:10	0.29	0.24	1.00
260_(STM)	CONDUIT	69.40	0	01:09	1.41	1.53	1.00
266_(STM)	CONDUIT	13.65	0	01:10	0.28	0.23	1.00
270_(STM)	CONDUIT	16.73	0	01:10	0.13	0.08	1.00
277_(STM)	CONDUIT	35.99	0	01:10	0.73	0.60	1.00
278_(STM)	CONDUIT	31.71	0	01:10	0.65	0.57	1.00
279_(STM)	CONDUIT	26.30	0	01:09	0.54	0.44	1.00
281_(STM)	CONDUIT	23.85	0	01:09	0.49	0.40	1.00
283_(STM)	CONDUIT	28.83	0	01:10	0.59	0.48	1.00
285_(STM)	CONDUIT	18.15	0	01:07	0.37	0.28	1.00
286_(STM)	CONDUIT	29.19	0	01:10	0.59	0.49	1.00
287_(STM)	CONDUIT	29.30	0	01:10	0.60	0.53	1.00
288_(STM)	CONDUIT	19.29	0	01:07	0.17	0.08	1.00
304_(STM)	CONDUIT	32.96	0	01:10	0.67	0.56	1.00

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49_(STM)	CONDUIT	316.44	0	01:10	0.59	0.68	1.00
50_(STM)	CONDUIT	31.12	0	01:21	0.65	0.35	0.51
51_(STM)	CONDUIT	68.75	0	01:12	0.36	0.36	0.84
52_(STM)	CONDUIT	112.28	0	01:12	0.52	0.54	0.98
53_(STM)	CONDUIT	152.29	0	01:12	0.54	0.67	1.00
55_(STM)	CONDUIT	236.48	0	01:12	0.54	0.64	1.00
56_(STM)	CONDUIT	315.90	0	01:10	0.59	0.59	1.00
85_(STM)	CONDUIT	31.38	0	01:06	0.64	0.77	1.00
87_(STM)	CONDUIT	13.09	0	01:33	0.56	0.15	0.38
97(1)_(STM)	CONDUIT	84.13	0	01:10	0.53	0.66	1.00
97_(STM)	CONDUIT	24.28	0	01:10	0.22	0.28	1.00
MS-CBMH1 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.13
MS-CBMH1 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-CBMH1 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.13
MS-CBMH1 (4)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-CBMH10 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.08
MS-CBMH10 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-CBMH10 (3)	CONDUIT	30.11	0	01:10	0.14	0.00	0.07
MS-CBMH11 (1)	CONDUIT	17.71	0	01:14	0.10	0.00	0.08
MS-CBMH11 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-CBMH12 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-CBMH12 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.08
MS-CBMH13 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-CBMH13 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.08
MS-CBMH14 (1)	CONDUIT	67.30	0	01:12	0.26	0.00	0.10
MS-CBMH14 (2)	CONDUIT	65.35	0	01:12	0.26	0.00	0.10
MS-CBMH15 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.08
MS-CBMH15 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.11
MS-CBMH2	CONDUIT	30.09	0	01:10	0.96	0.00	0.14
MS-CBMH3 (1)	CONDUIT	27.39	0	01:14	0.13	0.00	0.10
MS-CBMH3 (2)	CONDUIT	45.10	0	01:14	0.18	0.00	0.08
MS-CBMH3 (3)	CONDUIT	17.71	0	01:14	0.78	0.00	0.01
MS-CBMH4 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.09
MS-CBMH4 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.08
MS-CBMH5	CONDUIT	0.00	0	00:00	0.00	0.00	0.11
MS-CBMH5 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.11
MS-CBMH7 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-CBMH7 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.12
MS-CBMH8 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.12
MS-CBMH8 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-CICB1 (1)	CONDUIT	31.82	0	01:10	0.15	0.00	0.07
MS-CICB1 (2)	CONDUIT	31.83	0	01:10	1.18	0.00	0.13
MS-CICB2 (1)	CONDUIT	53.95	0	01:10	0.16	0.00	0.11
MS-CICB2 (2)	CONDUIT	53.96	0	01:10	1.67	0.00	0.08
MS-RYE (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.05
MS-RYE1	CONDUIT	0.00	0	00:00	0.00	0.00	0.07
MS-RYE10 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYE10 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYE10 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.08
MS-RYE12 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.08
MS-RYE12 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYE12 (3)	CONDUIT	2.81	0	01:11	0.01	0.00	0.08
MS-RYE12 (4)	CONDUIT	2.60	0	01:11	0.01	0.00	0.07
MS-RYE15 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.38
MS-RYE15 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.43
MS-RYE16 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.04
MS-RYE16 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.08

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MS-RYE16 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.04
MS-RYE18 (1)	CONDUIT	5.83	0	01:25	0.02	0.00	0.11
MS-RYE18 (2)	CONDUIT	5.89	0	01:26	0.02	0.00	0.14
MS-RYE2 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.05
MS-RYE2 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.02
MS-RYE2 (4)	CONDUIT	0.00	0	00:00	0.00	0.00	0.11
MS-RYE2 (5)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYE3 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.07
MS-RYE3 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.07
MS-RYE3 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.50
MS-RYE3 (4)	CONDUIT	0.00	0	00:00	0.00	0.00	0.02
MS-RYE3 (5)	CONDUIT	0.00	0	00:00	0.00	0.00	0.09
MS-RYE4 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.38
MS-RYE4 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.24
MS-RYE4 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.11
MS-RYE4 (4)	CONDUIT	0.00	0	00:00	0.00	0.00	0.07
MS-RYE5 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.25
MS-RYE5 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.25
MS-RYE6 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYE6 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.12
MS-RYE7 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYE7 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYE8 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYE8 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYE9 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYE9 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYT (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYT1 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.43
MS-RYT1 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.23
MS-RYT1 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.13
MS-RYT1 (4)	CONDUIT	0.00	0	00:00	0.00	0.00	0.11
MS-RYT10 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYT10 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYT10 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.08
MS-RYT11 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYT11 (3)	CONDUIT	4.02	0	01:10	0.29	0.00	0.00
MS-RYT11 (4)	CONDUIT	9.98	0	01:10	0.71	0.00	0.00
MS-RYT12	CONDUIT	4.49	0	01:10	0.16	0.00	0.01
MS-RYT13 (1)	CONDUIT	2.31	0	01:11	0.01	0.00	0.07
MS-RYT13 (2)	CONDUIT	1.69	0	01:11	0.01	0.00	0.07
MS-RYT14 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.07
MS-RYT14 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYT15 (1)	CONDUIT	10.27	0	01:10	0.06	0.00	0.06
MS-RYT15 (2)	CONDUIT	10.26	0	01:10	0.06	0.00	0.08
MS-RYT3 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYT3 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYT3 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYT4 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.22
MS-RYT4 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.22
MS-RYT4 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYT5 (1)	CONDUIT	16.60	0	01:14	0.07	0.00	0.08
MS-RYT5 (2)	CONDUIT	16.60	0	01:14	0.07	0.00	0.08
MS-RYT5 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.26
MS-RYT5 (4)	CONDUIT	0.99	0	01:11	0.03	0.00	0.28
MS-RYT6	CONDUIT	0.00	0	00:00	0.00	0.00	0.28
MS-RYT7 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.24
MS-RYT7 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.28

MS-RYT7 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.07
MS-RYT7 (4)	CONDUIT	0.00	0	00:00	0.00	0.00	0.10
MS-RYT8 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.36
MS-RYT8 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.38
MS-RYT8 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.11
MS-RYT8 (4)	CONDUIT	0.00	0	00:00	0.00	0.00	0.14
MS-RYT9 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.25
MS-RYT9 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.36
MS-RYT9 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.08
MS-RYT9 (4)	CONDUIT	0.00	0	00:00	0.00	0.00	0.13
O-CBMH10	ORIFICE	26.10	0	01:26			1.00
O-CBMH11	ORIFICE	21.38	0	01:24			1.00
O-CBMH13	ORIFICE	21.99	0	01:31			1.00
O-CBMH2	ORIFICE	20.84	0	01:34			1.00
O-CBMH3	ORIFICE	21.61	0	01:34			1.00
O-CICB1	ORIFICE	18.85	0	01:10			1.00
O-CICB2	ORIFICE	18.35	0	01:10			1.00
O-RYE7	ORIFICE	16.21	0	01:10			1.00
O-RYT13	ORIFICE	18.90	0	01:11			1.00
O-RYT14	ORIFICE	18.89	0	01:11			1.00
O-RYT15	ORIFICE	18.75	0	01:10			1.00
O-CBMH1	DUMMY	6.52	0	01:47			
O-CBMH14	DUMMY	6.61	0	01:14			
O-CBMH15	DUMMY	6.64	0	01:33			
O-CBMH4	DUMMY	8.76	0	01:30			
O-CBMH5	DUMMY	6.27	0	01:42			
O-CBMH8	DUMMY	6.62	0	01:33			

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Flow Classification Summary
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	Adjusted	Fraction of Time in Flow Class							
	/Actual	Up	Down	Sub	Sup	Up	Down	Norm	
Inlet Conduit Ctrl	Length	Dry	Dry	Dry	Crit	Crit	Crit	Crit	Ltd
100_ (STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
104_ (STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
106_ (STM) 0.00	1.00	0.00	0.82	0.00	0.18	0.00	0.00	0.00	0.87
116_ (STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
118_ (STM) 0.00	1.00	0.00	0.90	0.00	0.10	0.00	0.00	0.00	0.95
124_ (STM) 0.00	1.00	0.00	0.90	0.00	0.10	0.00	0.00	0.00	0.96
128_ (STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.96
130_ (STM) 0.00	1.00	0.00	0.00	0.00	0.97	0.03	0.00	0.00	0.95

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132_(STM) 0.00	1.00	0.00	0.00	0.00	0.17	0.00	0.00	0.83	0.01
136_(STM) 0.00	1.00	0.00	0.00	0.00	0.07	0.00	0.00	0.93	0.01
150_(1)_(STM) 0.00	1.00	0.00	0.87	0.00	0.13	0.00	0.00	0.00	0.92
152_(1)_(STM) 0.00	1.00	0.00	0.00	0.00	0.10	0.00	0.00	0.90	0.01
173_(STM) 0.00	1.00	0.00	0.87	0.00	0.13	0.00	0.00	0.00	0.88
175_(STM) 0.00	1.00	0.00	0.78	0.00	0.22	0.00	0.00	0.00	0.96
207_(STM) 0.00	1.00	0.00	0.00	0.00	0.11	0.00	0.00	0.89	0.01
209_(STM) 0.00	1.00	0.00	0.00	0.00	0.07	0.00	0.00	0.93	0.00
229_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
233_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
236(1)_(STM) 0.00	1.00	0.00	0.91	0.00	0.09	0.00	0.00	0.00	0.96
240_(STM) 0.00	1.00	0.00	0.27	0.00	0.73	0.00	0.00	0.00	0.86
250_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
252_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
253_(STM) 0.00	1.00	0.00	0.91	0.00	0.09	0.00	0.00	0.00	0.96
260_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
266_(STM) 0.00	1.00	0.00	0.00	0.00	0.04	0.00	0.00	0.96	0.01
270_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.12
277_(STM) 0.00	1.00	0.00	0.02	0.00	0.97	0.01	0.00	0.00	0.97
278_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.06
279_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.08
281_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.99
283_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.99
285_(STM) 0.00	1.00	0.00	0.88	0.00	0.12	0.00	0.00	0.00	0.87
286_(STM) 0.00	1.00	0.00	0.00	0.00	0.99	0.01	0.00	0.00	0.98
287_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.95
288_(STM) 0.00	1.00	0.00	0.00	0.00	0.07	0.00	0.00	0.93	0.00
304_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
49_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
50_(STM) 0.00	1.00	0.00	0.68	0.00	0.32	0.00	0.00	0.00	1.00

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PCSWMM Model Output
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51_ (STM)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
52_ (STM)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
53_ (STM)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
55_ (STM)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
56_ (STM)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
85_ (STM)	1.00	0.00	0.00	0.00	0.09	0.00	0.00	0.91	0.01
87_ (STM)	1.00	0.00	0.02	0.00	0.98	0.00	0.00	0.00	0.07
97 (1)_ (STM)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
97_ (STM)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
MS-CBMH1 (1)	1.00	0.91	0.09	0.00	0.00	0.00	0.00	0.00	0.00
MS-CBMH1 (2)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
MS-CBMH1 (3)	1.00	0.91	0.09	0.00	0.00	0.00	0.00	0.00	0.00
MS-CBMH1 (4)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
MS-CBMH10 (1)	1.00	0.99	0.01	0.00	0.00	0.00	0.00	0.00	0.00
MS-CBMH10 (2)	1.00	0.99	0.01	0.00	0.00	0.00	0.00	0.00	0.00
MS-CBMH10 (3)	1.00	0.99	0.00	0.00	0.01	0.00	0.00	0.00	0.00
MS-CBMH11 (1)	1.00	0.99	0.01	0.00	0.01	0.00	0.00	0.00	0.98
MS-CBMH11 (2)	1.00	0.99	0.01	0.00	0.00	0.00	0.00	0.00	0.00
MS-CBMH12 (1)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
MS-CBMH12 (2)	1.00	0.99	0.01	0.00	0.00	0.00	0.00	0.00	0.00
MS-CBMH13 (1)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
MS-CBMH13 (2)	1.00	0.98	0.02	0.00	0.00	0.00	0.00	0.00	0.00
MS-CBMH14 (1)	1.00	0.97	0.01	0.00	0.01	0.00	0.00	0.00	0.96
MS-CBMH14 (2)	1.00	0.98	0.00	0.00	0.01	0.00	0.00	0.00	0.97
MS-CBMH15 (1)	1.00	0.95	0.05	0.00	0.00	0.00	0.00	0.00	0.00
MS-CBMH15 (2)	1.00	0.93	0.07	0.00	0.00	0.00	0.00	0.00	0.00
MS-CBMH2	1.00	0.96	0.03	0.00	0.01	0.00	0.00	0.00	0.97
MS-CBMH3 (1)	1.00	0.98	0.02	0.00	0.01	0.00	0.00	0.00	0.98
MS-CBMH3 (2)	1.00	0.98	0.01	0.00	0.01	0.00	0.00	0.00	0.97
MS-CBMH3 (3)	1.00	0.99	0.00	0.00	0.00	0.01	0.00	0.00	0.97

Iron Valley II - 5331 Fernbank Road (121011)
PCSWMM Model Output
100yr, 3-hour Chicago Storm

MS-RYT11 (3)	1.00	0.93	0.00	0.00	0.00	0.00	0.00	0.07	0.00
MS-RYT11 (4)	1.00	0.93	0.00	0.00	0.00	0.00	0.00	0.07	0.00
MS-RYT12	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT13 (1)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.98
MS-RYT13 (2)	1.00	0.99	0.01	0.00	0.00	0.00	0.00	0.00	0.98
MS-RYT14 (1)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT14 (2)	1.00	0.99	0.01	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT15 (1)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.98
MS-RYT15 (2)	1.00	0.98	0.01	0.00	0.00	0.00	0.00	0.00	0.98
MS-RYT3 (1)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT3 (2)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT3 (3)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT4 (1)	1.00	0.98	0.02	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT4 (2)	1.00	0.98	0.02	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT4 (3)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT5 (1)	1.00	0.97	0.02	0.00	0.00	0.00	0.00	0.00	0.97
MS-RYT5 (2)	1.00	0.97	0.02	0.00	0.00	0.00	0.00	0.00	0.98
MS-RYT5 (3)	1.00	0.97	0.03	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT5 (4)	1.00	0.00	0.00	0.00	0.03	0.00	0.00	0.97	0.98
MS-RYT6	1.00	0.98	0.02	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT7 (1)	1.00	0.98	0.02	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT7 (2)	1.00	0.98	0.02	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT7 (3)	1.00	0.98	0.02	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT7 (4)	1.00	0.98	0.02	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT8 (1)	1.00	0.97	0.03	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT8 (2)	1.00	0.97	0.03	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT8 (3)	1.00	0.97	0.03	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT8 (4)	1.00	0.96	0.04	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT9 (1)	1.00	0.92	0.08	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT9 (2)	1.00	0.97	0.03	0.00	0.00	0.00	0.00	0.00	0.00

Iron Valley II - 5331 Fernbank Road (121011)
 PCSWMM Model Output
 100yr, 3-hour Chicago Storm

MS-RYT9 (3)	1.00	0.92	0.08	0.00	0.00	0.00	0.00	0.00	0.00
0.00									
MS-RYT9 (4)	1.00	0.91	0.09	0.00	0.00	0.00	0.00	0.00	0.00
0.00									

 Conduit Surcharge Summary

Conduit	Hours Full			Hours	
	Both Ends	Upstream	Dnstream	Above Full Normal Flow	Capacity Limited
100_ (STM)	3.20	3.20	3.23	0.01	0.01
104_ (STM)	5.53	5.53	5.55	0.01	0.01
106_ (STM)	5.52	5.52	22.99	0.01	0.01
116_ (STM)	2.13	2.13	2.15	0.01	0.01
118_ (STM)	2.12	2.12	2.62	0.01	0.01
124_ (STM)	1.65	1.65	1.77	0.01	0.01
128_ (STM)	1.44	1.44	1.65	0.01	0.01
130_ (STM)	1.32	1.32	1.44	0.01	0.01
132_ (STM)	4.37	4.37	4.41	0.01	0.01
136_ (STM)	3.00	3.00	3.19	0.01	0.01
150_ (1)_ (STM)	2.92	2.92	3.22	0.06	0.07
152_ (1)_ (STM)	2.51	2.51	2.75	0.01	0.01
173_ (STM)	4.31	4.31	5.11	0.01	0.01
175_ (STM)	1.33	1.33	1.66	0.01	0.01
207_ (STM)	2.77	2.77	3.02	0.01	0.01
209_ (STM)	2.23	2.23	2.24	0.01	0.01
229_ (STM)	48.00	48.00	48.00	0.01	0.01
233_ (STM)	1.66	1.66	1.88	0.01	0.01
236 (1)_ (STM)	1.38	1.38	1.66	0.01	0.02
250_ (STM)	1.22	1.22	1.25	0.01	0.01
252_ (STM)	1.22	1.22	1.25	0.01	0.01
253_ (STM)	1.36	1.36	1.66	0.01	0.01
260_ (STM)	4.33	4.33	4.41	0.07	0.01
266_ (STM)	1.11	1.11	1.31	0.01	0.01
270_ (STM)	1.09	1.09	1.09	0.01	0.01
277_ (STM)	0.68	0.68	0.84	0.01	0.01
278_ (STM)	0.84	0.84	0.88	0.01	0.01
279_ (STM)	0.37	0.37	0.44	0.01	0.01
281_ (STM)	0.31	0.31	0.39	0.01	0.01
283_ (STM)	0.31	0.31	0.39	0.01	0.01
285_ (STM)	4.49	4.49	5.19	0.01	0.01
286_ (STM)	0.60	0.60	0.74	0.01	0.01
287_ (STM)	0.74	0.74	0.79	0.01	0.01
288_ (STM)	2.79	2.79	2.81	0.01	0.01
304_ (STM)	5.97	5.97	6.44	0.01	0.01
49_ (STM)	48.00	48.00	48.00	0.01	0.01
52_ (STM)	0.01	0.01	0.17	0.01	0.01
53_ (STM)	0.10	0.10	1.19	0.01	0.01
55_ (STM)	1.19	1.19	48.00	0.01	0.01
56_ (STM)	48.00	48.00	48.00	0.01	0.01
85_ (STM)	3.58	3.58	3.66	0.01	0.01
97 (1)_ (STM)	48.00	48.00	48.00	0.01	0.01

Iron Valley II - 5331 Fernbank Road (121011)
PCSWMM Model Output
100yr, 3-hour Chicago Storm

97_(STM)	0.49	0.49	48.00	0.01	0.01
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Analysis begun on: Mon Jun 22 10:08:24 2026
Analysis ended on: Mon Jun 22 10:08:34 2026
Total elapsed time: 00:00:10

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.2 (Build 5.2.4)

WARNING 04: minimum elevation drop used for Conduit MS-RYE2(5)
 WARNING 04: minimum elevation drop used for Conduit MS-RYT12
 WARNING 04: minimum elevation drop used for Conduit MS-RYT3(3)
 WARNING 04: minimum elevation drop used for Conduit MS-RYT4(3)

Element Count

Number of rain gages 1
 Number of subcatchments ... 37
 Number of nodes 130
 Number of links 177
 Number of pollutants 0
 Number of land uses 0

Raingage Summary

Name	Data Source	Data Type	Recording Interval
RG-1	S24hr-100yr-JFSA	INTENSITY	12 min.

Subcatchment Summary

Name Outlet	Area	Width	%Imperv	%Slope	Rain Gage
A1	0.03	27.62	7.00	3.7000	RG-1
RYE16					
A10	0.11	91.36	13.00	2.0000	RG-1
RYE3					
A11	0.15	76.57	56.00	2.0000	RG-1
CBMH3					
A12	0.11	99.73	61.00	1.0000	RG-1
CBMH13					
A13	0.03	13.95	71.00	2.5000	RG-1
HP-RYT11(2)					
A14	0.04	54.65	7.00	2.5000	RG-1
RYE10					
A15	0.13	62.89	47.00	2.5000	RG-1
CBMH11					
A16	0.05	56.18	14.00	2.5000	RG-1
RYE9					
A17	0.15	48.11	44.00	2.5000	RG-1
CBMH10					
A18	0.24	123.58	55.00	2.1000	RG-1
CBMH2					
A19	0.07	59.02	28.00	3.5000	RG-1
RYE13					

Iron Valley II - 5331 Fernbank Road (121011)
 PCSWMM Model Output
 100yr, 24-hour SCS Storm

A2	0.13	66.39	59.00	1.9000	RG-1
CBMH15					
A20	0.10	96.43	13.00	3.0000	RG-1
RYE4					
A21	0.06	76.24	7.00	3.0000	RG-1
RYE5					
A22	0.09	56.43	29.00	3.5000	RG-1
RYE11					
A23_1	0.14	54.33	33.00	2.3000	RG-1
CBMH1					
A23_2	0.10	37.98	33.00	2.3000	RG-1
RYE18					
A24	0.11	105.36	47.00	0.5000	RG-1
CICB1					
A25	0.14	76.29	58.00	2.2000	RG-1
CBMH7					
A26	0.08	46.08	31.00	3.7000	RG-1
RYE12					
A27	0.15	120.00	9.00	3.5000	RG-1
RYE8					
A28	0.12	72.33	58.00	2.5000	RG-1
CBMH8					
A29	0.05	40.19	7.00	3.0000	RG-1
RYE7					
A3	0.12	94.12	14.00	3.0000	RG-1
RYT1					
A31	0.05	37.88	14.00	3.4000	RG-1
RYE6					
A32	0.10	120.19	51.00	0.5000	RG-1
CICB2					
A4	0.13	68.17	54.00	2.3000	RG-1
CBMH5					
A5	0.07	58.00	28.00	3.7000	RG-1
RYE17					
A6	0.19	99.11	7.00	2.6000	RG-1
RYE2					
A7	0.08	33.94	61.00	1.2000	RG-1
CBMH14					
A8	0.15	78.25	56.00	1.9000	RG-1
CBMH4					
A9	0.07	57.14	28.00	3.7000	RG-1
RYE14					
U1	0.09	103.45	14.00	15.0000	RG-1
OF1					
U2	0.03	46.95	12.00	5.0000	RG-1
OF3					
U3	0.05	171.82	7.00	15.0000	RG-1
OF2					
U4	0.09	90.00	29.00	3.7000	RG-1
OF4					
U5	0.05	33.16	29.00	3.7000	RG-1
OF5					

 Node Summary

Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
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CBMH4-Dummy	JUNCTION	95.22	3.00	0.0	
HP-CBMH1	JUNCTION	97.08	1.00	0.0	
HP-CBMH1 (2)	JUNCTION	97.06	1.00	0.0	
HP-CBMH10	JUNCTION	97.20	1.00	0.0	
HP-CBMH11	JUNCTION	97.25	1.00	0.0	
HP-CBMH12	JUNCTION	97.70	1.00	0.0	
HP-CBMH13	JUNCTION	97.66	1.00	0.0	
HP-CBMH14	JUNCTION	97.34	1.00	0.0	
HP-CBMH15	JUNCTION	97.75	1.00	0.0	
HP-CBMH2	JUNCTION	97.11	1.00	0.0	
HP-CBMH3	JUNCTION	97.37	1.00	0.0	
HP-CBMH4	JUNCTION	97.54	1.00	0.0	
HP-CBMH5	JUNCTION	97.68	1.00	0.0	
HP-CBMH7	JUNCTION	97.16	1.00	0.0	
HP-CBMH8	JUNCTION	97.27	1.00	0.0	
HP-CICB1	JUNCTION	97.11	1.00	0.0	
HP-CICB2	JUNCTION	97.64	1.00	0.0	
HP-RYE10	JUNCTION	97.50	1.00	0.0	
HP-RYE12	JUNCTION	97.33	1.00	0.0	
HP-RYE12 (2)	JUNCTION	97.31	1.00	0.0	
HP-RYE15	JUNCTION	97.68	1.00	0.0	
HP-RYE16 (1)	JUNCTION	97.85	1.00	0.0	
HP-RYE18	JUNCTION	96.98	1.00	0.0	
HP-RYE2 (1)	JUNCTION	97.68	0.30	0.0	
HP-RYE2 (2)	JUNCTION	97.66	0.30	0.0	
HP-RYE2 (3)	JUNCTION	97.70	1.00	0.0	
HP-RYE3 (1)	JUNCTION	97.52	0.30	0.0	
HP-RYE3 (2)	JUNCTION	97.69	0.30	0.0	
HP-RYE3 (3)	JUNCTION	97.55	1.00	0.0	
HP-RYE4	JUNCTION	97.35	1.00	0.0	
HP-RYE4 (2)	JUNCTION	97.45	1.00	0.0	
HP-RYE5	JUNCTION	97.15	1.00	0.0	
HP-RYE6	JUNCTION	97.60	1.00	0.0	
HP-RYE7	JUNCTION	97.37	1.00	0.0	
HP-RYE8	JUNCTION	97.50	1.00	0.0	
HP-RYE9	JUNCTION	97.59	1.00	0.0	
HP-RYT1 (1)	JUNCTION	97.76	0.30	0.0	
HP-RYT1 (2)	JUNCTION	97.67	1.00	0.0	
HP-RYT10 (1)	JUNCTION	97.48	1.00	0.0	
HP-RYT10 (2)	JUNCTION	97.45	1.00	0.0	
HP-RYT11 (1)	JUNCTION	97.69	1.00	0.0	
HP-RYT11 (2)	JUNCTION	97.77	1.00	0.0	
HP-RYT13	JUNCTION	97.30	1.00	0.0	
HP-RYT14	JUNCTION	97.43	1.00	0.0	
HP-RYT15	JUNCTION	97.59	1.00	0.0	
HP-RYT3 (1)	JUNCTION	97.66	0.30	0.0	
HP-RYT3 (2)	JUNCTION	97.65	0.30	0.0	
HP-RYT4	JUNCTION	97.65	0.30	0.0	
HP-RYT4 (2)	JUNCTION	97.50	0.30	0.0	
HP-RYT5 (1)	JUNCTION	97.38	1.00	0.0	
HP-RYT5 (2)	JUNCTION	97.50	0.30	0.0	
HP-RYT5 (3)	JUNCTION	97.38	0.30	0.0	
HP-RYT6	JUNCTION	97.49	1.00	0.0	
HP-RYT7	JUNCTION	97.57	1.00	0.0	
HP-RYT7 (2)	JUNCTION	97.35	1.00	0.0	
HP-RYT8 (1)	JUNCTION	97.17	1.00	0.0	

Iron Valley II - 5331 Fernbank Road (121011)
 PCSWMM Model Output
 100yr, 24-hour SCS Storm

HP-RYT8 (2)	JUNCTION	97.15	1.00	0.0
HP-RYT9 (1)	JUNCTION	97.44	1.00	0.0
HP-RYT9 (2)	JUNCTION	97.10	1.00	0.0
HP-RYE1	OUTFALL	97.61	1.00	0.0
HP-RYE16 (2)	OUTFALL	97.69	1.00	0.0
MH1013	OUTFALL	94.08	0.82	0.0
OF1	OUTFALL	97.00	0.00	0.0
OF2	OUTFALL	97.73	0.00	0.0
OF3	OUTFALL	97.15	0.00	0.0
OF4	OUTFALL	96.85	2.35	0.0
OF5	OUTFALL	0.00	0.00	0.0
CBMH1	STORAGE	94.77	2.97	0.0
CBMH10	STORAGE	94.85	3.01	0.0
CBMH11	STORAGE	94.90	3.18	0.0
CBMH12	STORAGE	95.15	3.40	0.0
CBMH13	STORAGE	94.91	3.32	0.0
CBMH14	STORAGE	95.09	3.14	0.0
CBMH15	STORAGE	95.35	3.15	0.0
CBMH2	STORAGE	94.86	2.98	0.0
CBMH3	STORAGE	94.98	3.12	0.0
CBMH4	STORAGE	95.12	3.19	0.0
CBMH5	STORAGE	95.29	3.09	0.0
CBMH7	STORAGE	94.58	3.20	0.0
CBMH8	STORAGE	94.85	3.07	0.0
CICB1	STORAGE	95.42	2.72	0.0
CICB2	STORAGE	96.04	2.55	0.0
MH100	STORAGE	94.10	2.86	0.0
MH102	STORAGE	94.13	2.90	0.0
MH104	STORAGE	94.15	2.88	0.0
MH106	STORAGE	94.31	2.80	0.0
MH108	STORAGE	94.53	2.75	0.0
MH110	STORAGE	94.65	2.71	0.0
MH112	STORAGE	94.79	2.71	0.0
MH114	STORAGE	95.09	2.46	0.0
MH116	STORAGE	95.12	2.49	0.0
MH118	STORAGE	95.15	2.52	0.0
MH200	STORAGE	94.69	2.49	0.0
MH202	STORAGE	94.88	2.51	0.0
MH204	STORAGE	94.93	2.20	0.0
MH206	STORAGE	95.48	2.28	0.0
RYE1	STORAGE	95.99	2.48	0.0
RYE10	STORAGE	95.47	2.90	0.0
RYE11	STORAGE	95.64	2.50	0.0
RYE12	STORAGE	95.76	2.40	0.0
RYE13	STORAGE	95.91	2.40	0.0
RYE14	STORAGE	96.10	2.40	0.0
RYE15	STORAGE	95.86	2.52	0.0
RYE16	STORAGE	95.78	2.80	0.0
RYE17	STORAGE	96.26	2.40	0.0
RYE18	STORAGE	94.94	2.86	0.0
RYE2	STORAGE	95.51	2.99	0.0
RYE3	STORAGE	95.96	2.44	0.0
RYE4	STORAGE	95.26	2.64	0.0
RYE5	STORAGE	95.14	2.71	0.0
RYE6	STORAGE	95.45	3.01	0.0
RYE7	STORAGE	95.03	3.19	0.0
RYE8	STORAGE	95.15	3.05	0.0

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 PCSWMM Model Output
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RYE9	STORAGE	95.16	3.21	0.0
RYT1	STORAGE	95.59	2.76	0.0
RYT10	STORAGE	94.97	3.50	0.0
RYT11	STORAGE	95.16	3.42	0.0
RYT12	STORAGE	95.45	2.62	0.0
RYT13	STORAGE	95.59	2.58	0.0
RYT14	STORAGE	95.72	2.57	0.0
RYT15	STORAGE	95.91	2.57	0.0
RYT16	STORAGE	96.07	2.57	0.0
RYT17	STORAGE	94.97	3.11	0.0
RYT3	STORAGE	95.40	3.04	0.0
RYT4	STORAGE	95.23	3.03	0.0
RYT5	STORAGE	95.11	3.12	0.0
RYT6	STORAGE	95.62	2.56	0.0
RYT7	STORAGE	95.14	3.01	0.0
RYT8	STORAGE	94.89	3.01	0.0
RYT9	STORAGE	94.79	3.06	0.0

Link Summary

Name	From Node	To Node	Type	Length	%
Slope Roughness					

100_(STM)	MH202	CBMH8	CONDUIT	18.2	
0.1651 0.0130					
104_(STM)	RYT9	CBMH1	CONDUIT	20.8	
0.0962 0.0130					
106_(STM)	RYE5	RYT9	CONDUIT	35.4	
0.9896 0.0130					
116_(STM)	RYT8	CBMH2	CONDUIT	20.8	
0.1444 0.0130					
118_(STM)	RYE4	RYT8	CONDUIT	36.0	
0.9989 0.0130					
124_(STM)	RYT7	CBMH3	CONDUIT	21.8	
0.5051 0.0130					
128_(STM)	RYT6	RYT7	CONDUIT	47.6	
1.0074 0.0130					
130_(STM)	RYE3	RYT6	CONDUIT	34.3	
0.9925 0.0130					
132_(STM)	RYT1	CBMH5	CONDUIT	17.1	
0.1755 0.0130					
136_(STM)	RYE6	MH202	CONDUIT	20.7	
1.0141 0.0130					
150_(1)_(STM)	RYE2	RYT3	CONDUIT	22.8	
0.4831 0.0130					
152_(1)_(STM)	RYT3	RYT4	CONDUIT	34.7	
0.4902 0.0130					
173_(STM)	RYE1	RYT1	CONDUIT	40.3	
0.9931 0.0130					
175_(STM)	CBMH12	CBMH11	CONDUIT	38.6	
0.5179 0.0130					
207_(STM)	RYT4	RYT5	CONDUIT	21.4	
0.5145 0.0130					
209_(STM)	CBMH4-Dummy	CBMH4	CONDUIT	13.7	
0.1461 0.0130					
229_(STM)	MH104	MH102	CONDUIT	13.3	0.15

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233_(STM)	MH204	CBMH10	CONDUIT	17.7
0.4520 0.0130				
236(1)_(STM)	RYE8	RYT17	CONDUIT	16.6
1.0223 0.0130				
240_(STM)	MH118	MH116	CONDUIT	8.9
0.3382 0.0130				
250_(STM)	RYT17	MH204	CONDUIT	25.4
0.1575 0.0130				
252_(STM)	RYT10	MH204	CONDUIT	26.8
0.1493 0.0130				
253_(STM)	RYE9	RYT10	CONDUIT	18.1
0.9918 0.0130				
260_(STM)	RYT5	CBMH14	CONDUIT	3.5
0.5797 0.0130				
266_(STM)	RYE10	RYT11	CONDUIT	29.6
1.0129 0.0130				
270_(STM)	RYT11	CBMH12	CONDUIT	7.8
0.1280 0.0130				
277_(STM)	RYE11	RYT12	CONDUIT	18.7
1.0156 0.0130				
278_(STM)	RYT12	CICB1	CONDUIT	3.5
0.8696 0.0130				
279_(STM)	RYE12	RYT13	CONDUIT	17.1
0.9954 0.0130				
281_(STM)	RYE13	RYT14	CONDUIT	18.7
1.0156 0.0130				
283_(STM)	RYE14	RYT15	CONDUIT	18.7
1.0156 0.0130				
285_(STM)	RYE15	RYT1	CONDUIT	22.4
1.2049 0.0130				
286_(STM)	RYE17	RYT16	CONDUIT	18.7
1.0156 0.0130				
287_(STM)	RYT16	CICB2	CONDUIT	3.5
0.8696 0.0130				
288_(STM)	RYE16	MH206	CONDUIT	17.8
0.1690 0.0130				
304_(STM)	RYE18	CBMH1	CONDUIT	12.4
0.9678 0.0130				
49_(STM)	MH100	MH1013	CONDUIT	18.9
0.1058 0.0130				
50_(STM)	MH114	MH112	CONDUIT	58.6
0.2558 0.0130				
51_(STM)	MH112	MH110	CONDUIT	72.1
0.1942 0.0130				
52_(STM)	MH110	MH108	CONDUIT	21.5
0.2328 0.0130				
53_(STM)	MH108	MH106	CONDUIT	50.6
0.1383 0.0130				
55_(STM)	MH106	MH104	CONDUIT	72.1
0.1110 0.0130				
56_(STM)	MH102	MH100	CONDUIT	21.4
0.1405 0.0130				
85_(STM)	MH206	CBMH15	CONDUIT	17.1
0.4687 0.0130				
87_(STM)	MH116	MH114	CONDUIT	12.0
0.2500 0.0130				
97(1)_(STM)	CBMH7	MH104	CONDUIT	24.9
0.2008 0.0130				
97_(STM)	MH200	CBMH7	CONDUIT	16.3
0.2459 0.0130				

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MS-CBMH1 (1)	CBMH1	HP-CBMH1	CONDUIT	2.0	-
17.2511 0.0130					
MS-CBMH1 (2)	HP-CBMH1	CBMH7	CONDUIT	2.0	
15.1717 0.0130					
MS-CBMH1 (3)	CBMH1	HP-CBMH1 (2)	CONDUIT	2.0	-
16.2088 0.0130					
MS-CBMH1 (4)	HP-CBMH1 (2)	OF4	CONDUIT	2.0	-
69.3731 0.0130					
MS-CBMH10 (1)	CBMH10	HP-CBMH10	CONDUIT	2.0	-
17.2511 0.0130					
MS-CBMH10 (2)	HP-CBMH10	HP-CBMH2	CONDUIT	2.0	
4.5046 0.0130					
MS-CBMH10 (3)	HP-CBMH2	CICB1	CONDUIT	2.0	
6.0108 0.0130					
MS-CBMH11 (1)	CBMH11	HP-CBMH11	CONDUIT	2.0	-
8.5309 0.0130					
MS-CBMH11 (2)	HP-CBMH11	HP-RYT14	CONDUIT	2.0	-
9.0367 0.0130					
MS-CBMH12 (1)	HP-CBMH12	CBMH12	CONDUIT	2.0	
7.5212 0.0130					
MS-CBMH12 (2)	HP-CBMH12	CBMH11	CONDUIT	2.0	
32.6063 0.0130					
MS-CBMH13 (1)	CBMH12	HP-CBMH13	CONDUIT	2.0	-
5.5083 0.0130					
MS-CBMH13 (2)	HP-CBMH13	CBMH13	CONDUIT	2.0	
22.0148 0.0130					
MS-CBMH14 (1)	CBMH14	HP-CBMH14	CONDUIT	2.0	-
5.5083 0.0130					
MS-CBMH14 (2)	HP-CBMH14	CBMH13	CONDUIT	2.0	
5.5083 0.0130					
MS-CBMH15 (1)	CBMH15	HP-CBMH15	CONDUIT	2.0	-
12.5988 0.0130					
MS-CBMH15 (2)	HP-CBMH15	CBMH5	CONDUIT	2.0	
18.8249 0.0130					
MS-CBMH2	HP-CBMH2	CBMH2	CONDUIT	2.0	
13.6247 0.0130					
MS-CBMH3 (1)	CBMH3	HP-CBMH3	CONDUIT	2.0	-
13.6247 0.0130					
MS-CBMH3 (2)	HP-CBMH3	CBMH13	CONDUIT	2.0	
7.0172 0.0130					
MS-CBMH3 (3)	HP-CBMH3	HP-CBMH11	CONDUIT	2.0	
6.0108 0.0130					
MS-CBMH4 (1)	CBMH4	HP-CBMH4	CONDUIT	2.0	-
11.5768 0.0130					
MS-CBMH4 (2)	HP-CBMH4	CBMH14	CONDUIT	2.0	
15.6896 0.0130					
MS-CBMH5	CBMH5	HP-CBMH5	CONDUIT	2.0	-
15.1717 0.0130					
MS-CBMH5 (2)	HP-CBMH5	CICB2	CONDUIT	2.0	
12.0873 0.0130					
MS-CBMH7 (1)	CBMH7	HP-CBMH7	CONDUIT	2.0	-
19.3525 0.0130					
MS-CBMH7 (2)	HP-CBMH7	CBMH8	CONDUIT	2.0	
12.0873 0.0130					
MS-CBMH8 (1)	CBMH8	HP-CBMH8	CONDUIT	2.0	-
17.7743 0.0130					
MS-CBMH8 (2)	HP-CBMH8	RYT17	CONDUIT	2.0	
9.5432 0.0300					
MS-CICB1 (1)	CICB1	HP-CICB1	CONDUIT	2.0	-
6.0108 0.0130					

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MS-CICB1 (2)	HP-CICB1	CBMH1	CONDUIT	2.0	
18.8249 0.0130					
MS-CICB2 (1)	CICB2	HP-CICB2	CONDUIT	2.0	-
10.0504 0.0130					
MS-CICB2 (2)	HP-CICB2	CBMH14	CONDUIT	2.0	
20.9448 0.0130					
MS-RYE (1)	HP-RYE2 (1)	RYE2	CONDUIT	8.9	
2.0229 0.0300					
MS-RYE1	RYE1	HP-RYE1	CONDUIT	2.0	-
7.0172 0.0300					
MS-RYE10 (1)	RYE10	HP-RYE10	CONDUIT	2.0	-
6.5138 0.0300					
MS-RYE10 (2)	HP-RYE10	RYE9	CONDUIT	2.0	
7.5212 0.0300					
MS-RYE10 (3)	HP-RYE10	CBMH11	CONDUIT	2.0	
21.4790 0.0130					
MS-RYE12 (1)	RYE12	HP-RYE12	CONDUIT	2.0	-
8.5309 0.0300					
MS-RYE12 (2)	HP-RYE12	RYT17	CONDUIT	2.0	
12.5988 0.0300					
MS-RYE12 (3)	RYE12	HP-RYE12 (2)	CONDUIT	2.0	-
7.5212 0.0300					
MS-RYE12 (4)	HP-RYE12 (2)	RYT13	CONDUIT	2.0	
7.0172 0.0300					
MS-RYE15 (1)	RYE15	HP-RYE15	CONDUIT	16.1	-
1.8637 0.0300					
MS-RYE15 (2)	HP-RYE15	RYT1	CONDUIT	11.2	
2.9477 0.0300					
MS-RYE16 (1)	RYE16	HP-RYE16 (1)	CONDUIT	2.0	-
13.6247 0.0300					
MS-RYE16 (2)	HP-RYE16 (1)	CBMH15	CONDUIT	2.0	
17.7743 0.0130					
MS-RYE16 (3)	RYE16	HP-RYE16 (2)	CONDUIT	2.0	-
5.5083 0.0300					
MS-RYE18 (1)	RYE18	HP-RYE18	CONDUIT	2.0	-
9.0367 0.0130					
MS-RYE18 (2)	HP-RYE18	CBMH1	CONDUIT	2.0	
12.0873 0.0130					
MS-RYE2 (2)	RYE2	HP-RYE2 (2)	CONDUIT	9.3	-
1.7207 0.0300					
MS-RYE2 (3)	RYE2	HP-RYE2 (3)	CONDUIT	2.0	-
10.0504 0.0300					
MS-RYE2 (4)	HP-RYE2 (3)	CICB2	CONDUIT	2.0	
13.1113 0.0130					
MS-RYE2 (5)	HP-RYE2 (2)	HP-RYT3 (1)	CONDUIT	2.8	
0.0109 0.0130					
MS-RYE3 (1)	HP-RYE3 (1)	RYE3	CONDUIT	5.4	
2.2228 0.0300					
MS-RYE3 (2)	RYE3	HP-RYE3 (2)	CONDUIT	14.0	-
2.0719 0.0300					
MS-RYE3 (3)	HP-RYE3 (2)	RYE15	CONDUIT	20.8	
1.9234 0.0300					
MS-RYE3 (4)	RYE3	HP-RYE3 (3)	CONDUIT	2.0	-
7.5212 0.0300					
MS-RYE3 (5)	HP-RYE3 (3)	CBMH4	CONDUIT	2.0	
12.0873 0.0130					
MS-RYE4 (1)	RYE4	HP-RYE4	CONDUIT	22.5	-
2.0004 0.0300					
MS-RYE4 (2)	HP-RYE4	RYT7	CONDUIT	13.5	
1.4816 0.0300					

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MS-RYE4 (3)	RYE4	HP-RYE4 (2)	CONDUIT	2.0	-
28.6028 0.0300					
MS-RYE4 (4)	HP-RYE4 (2)	RYE13	CONDUIT	2.0	
7.0172 0.0300					
MS-RYE5 (1)	RYE5	HP-RYE5	CONDUIT	14.9	-
2.0138 0.0300					
MS-RYE5 (2)	HP-RYE5	RYT9	CONDUIT	20.5	
1.4636 0.0300					
MS-RYE6 (1)	RYE6	HP-RYE6	CONDUIT	2.0	-
7.0172 0.0300					
MS-RYE6 (2)	HP-RYE6	CBMH8	CONDUIT	2.0	
36.1538 0.0130					
MS-RYE7 (1)	RYE7	HP-RYE7	CONDUIT	2.0	-
7.5212 0.0300					
MS-RYE7 (2)	HP-RYE7	CBMH7	CONDUIT	2.0	
30.8740 0.0130					
MS-RYE8 (1)	RYE8	HP-RYE8	CONDUIT	2.0	-
15.1717 0.0300					
MS-RYE8 (2)	HP-RYE8	RYT17	CONDUIT	2.0	
21.4790 0.0300					
MS-RYE9 (1)	RYE9	HP-RYE9	CONDUIT	2.0	-
11.0672 0.0300					
MS-RYE9 (2)	HP-RYE9	RYT10	CONDUIT	2.0	
6.0108 0.0300					
MS-RYT (1)	RYT11	HP-RYT11 (1)	CONDUIT	7.7	-
1.4287 0.0300					
MS-RYT1 (1)	RYT1	HP-RYT1 (1)	CONDUIT	20.7	-
1.9811 0.0300					
MS-RYT1 (2)	HP-RYT1 (1)	RYE1	CONDUIT	19.6	
1.4798 0.0300					
MS-RYT1 (3)	RYT1	HP-RYT1 (2)	CONDUIT	2.0	-
16.2088 0.0300					
MS-RYT1 (4)	HP-RYT1 (2)	CBMH5	CONDUIT	2.0	
14.6549 0.0130					
MS-RYT10 (1)	RYT10	HP-RYT10 (1)	CONDUIT	2.0	-
0.5000 0.0300					
MS-RYT10 (2)	HP-RYT10 (1)	HP-RYT10 (2)	CONDUIT	2.0	
1.5002 0.0300					
MS-RYT10 (3)	HP-RYT10 (2)	CBMH10	CONDUIT	2.0	
30.8740 0.0130					
MS-RYT11 (2)	HP-RYT11 (1)	RYE10	CONDUIT	21.9	
1.4613 0.0300					
MS-RYT11 (3)	RYT11	HP-RYT11 (2)	CONDUIT	2.0	-
9.5432 0.0300					
MS-RYT11 (4)	HP-RYT11 (2)	CBMH12	CONDUIT	2.0	
11.0672 0.0130					
MS-RYT12	RYT12	CICB1	CONDUIT	2.0	
0.0152 0.0130					
MS-RYT13 (1)	RYT13	HP-RYT13	CONDUIT	2.0	-
6.5138 0.0300					
MS-RYT13 (2)	HP-RYT13	CICB1	CONDUIT	2.0	
15.6896 0.0130					
MS-RYT14 (1)	RYT14	HP-RYT14	CONDUIT	2.0	-
7.0172 0.0300					
MS-RYT14 (2)	HP-RYT14	HP-CBMH2	CONDUIT	2.0	
16.2088 0.0130					
MS-RYT15 (1)	RYT15	HP-RYT15	CONDUIT	2.0	-
5.5083 0.0300					
MS-RYT15 (2)	HP-RYT15	CBMH13	CONDUIT	2.0	
18.2989 0.0130					

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MS-RYT3 (1)	HP-RYT3 (1)	RYT3	CONDUIT	13.3	
1.6544 0.0300					
MS-RYT3 (2)	RYT3	HP-RYT3 (2)	CONDUIT	9.4	-
2.2346 0.0300					
MS-RYT3 (3)	HP-RYT3 (2)	HP-RYT4	CONDUIT	2.8	
0.0109 0.0130					
MS-RYT4 (1)	HP-RYT4	RYT4	CONDUIT	25.0	
1.5602 0.0300					
MS-RYT4 (2)	RYT4	HP-RYT4 (2)	CONDUIT	11.0	-
2.1823 0.0300					
MS-RYT4 (3)	HP-RYT4 (2)	HP-RYT5 (2)	CONDUIT	2.8	
0.0109 0.0130					
MS-RYT5 (1)	RYT5	HP-RYT5 (1)	CONDUIT	2.0	-
7.5212 0.0300					
MS-RYT5 (2)	HP-RYT5 (1)	CBMH14	CONDUIT	2.0	
7.5212 0.0130					
MS-RYT5 (3)	HP-RYT5 (2)	RYT5	CONDUIT	10.1	
2.6742 0.0300					
MS-RYT5 (4)	RYT5	HP-RYT5 (3)	CONDUIT	8.0	-
1.8753 0.0300					
MS-RYT6	RYT6	HP-RYT6	CONDUIT	20.4	-
1.5198 0.0300					
MS-RYT7 (1)	RYT7	HP-RYT7	CONDUIT	28.2	-
1.4895 0.0300					
MS-RYT7 (2)	HP-RYT7	RYT6	CONDUIT	19.5	
2.0004 0.0300					
MS-RYT7 (3)	RYT7	HP-RYT7 (2)	CONDUIT	2.0	-
10.0504 0.0300					
MS-RYT7 (4)	HP-RYT7 (2)	CBMH3	CONDUIT	2.0	
12.5988 0.0130					
MS-RYT8 (1)	RYT8	HP-RYT8 (1)	CONDUIT	18.0	-
1.5002 0.0300					
MS-RYT8 (2)	HP-RYT8 (1)	RYE4	CONDUIT	18.0	
1.5002 0.0300					
MS-RYT8 (3)	RYT8	HP-RYT8 (2)	CONDUIT	2.0	-
12.5988 0.0300					
MS-RYT8 (4)	HP-RYT8 (2)	CBMH2	CONDUIT	2.0	
15.6896 0.0130					
MS-RYT9 (1)	RYT9	HP-RYT9 (1)	CONDUIT	36.0	-
1.6391 0.0300					
MS-RYT9 (2)	HP-RYT9 (1)	RYT8	CONDUIT	36.0	
1.5002 0.0300					
MS-RYT9 (3)	RYT9	HP-RYT9 (2)	CONDUIT	2.0	-
12.5988 0.0300					
MS-RYT9 (4)	HP-RYT9 (2)	CBMH1	CONDUIT	2.0	
18.2989 0.0130					
O-CBMH10	CBMH10	MH106	ORIFICE		
O-CBMH11	CBMH11	MH108	ORIFICE		
O-CBMH13	CBMH13	MH110	ORIFICE		
O-CBMH2	CBMH2	MH106	ORIFICE		
O-CBMH3	CBMH3	MH110	ORIFICE		
O-CICB1	CICB1	MH106	ORIFICE		
O-CICB2	CICB2	MH114	ORIFICE		
O-RYE7	RYE7	MH200	ORIFICE		
O-RYT13	RYT13	MH106	ORIFICE		
O-RYT14	RYT14	MH108	ORIFICE		
O-RYT15	RYT15	MH112	ORIFICE		
O-CBMH1	CBMH1	MH104	OUTLET		
O-CBMH14	CBMH14	MH112	OUTLET		

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O-CBMH15	CBMH15	MH118	OUTLET
O-CBMH4	CBMH4	MH112	OUTLET
O-CBMH5	CBMH5	MH118	OUTLET
O-CBMH8	CBMH8	MH200	OUTLET

 Cross Section Summary

Full Conduit Flow	Shape	Full Depth	Full Area	Hyd. Rad.	Max. Width	No. of Barrels

100_ (STM) 249.51	CIRCULAR	0.60	0.28	0.15	0.60	1
104_ (STM) 190.50	CIRCULAR	0.60	0.28	0.15	0.60	1
106_ (STM) 59.16	CIRCULAR	0.25	0.05	0.06	0.25	1
116_ (STM) 233.37	CIRCULAR	0.60	0.28	0.15	0.60	1
118_ (STM) 59.44	CIRCULAR	0.25	0.05	0.06	0.25	1
124_ (STM) 42.26	CIRCULAR	0.25	0.05	0.06	0.25	1
128_ (STM) 59.69	CIRCULAR	0.25	0.05	0.06	0.25	1
130_ (STM) 59.25	CIRCULAR	0.25	0.05	0.06	0.25	1
132_ (STM) 257.27	CIRCULAR	0.60	0.28	0.15	0.60	1
136_ (STM) 59.89	CIRCULAR	0.25	0.05	0.06	0.25	1
150_ (1)_ (STM) 41.34	CIRCULAR	0.25	0.05	0.06	0.25	1
152_ (1)_ (STM) 429.92	CIRCULAR	0.60	0.28	0.15	0.60	1
173_ (STM) 59.27	CIRCULAR	0.25	0.05	0.06	0.25	1
175_ (STM) 42.80	CIRCULAR	0.25	0.05	0.06	0.25	1
207_ (STM) 440.45	CIRCULAR	0.60	0.28	0.15	0.60	1
209_ (STM) 234.70	CIRCULAR	0.60	0.28	0.15	0.60	1
229_ (STM) 556.46	CIRCULAR	0.82	0.53	0.21	0.82	1
233_ (STM) 65.02	CIRCULAR	0.30	0.07	0.07	0.30	1
236 (1)_ (STM) 60.13	CIRCULAR	0.25	0.05	0.06	0.25	1
240_ (STM) 101.97	CIRCULAR	0.38	0.11	0.09	0.38	1
250_ (STM) 243.73	CIRCULAR	0.60	0.28	0.15	0.60	1
252_ (STM) 237.23	CIRCULAR	0.60	0.28	0.15	0.60	1

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253_(STM) 59.23	CIRCULAR	0.25	0.05	0.06	0.25	1
260_(STM) 45.28	CIRCULAR	0.25	0.05	0.06	0.25	1
266_(STM) 59.85	CIRCULAR	0.25	0.05	0.06	0.25	1
270_(STM) 219.72	CIRCULAR	0.60	0.28	0.15	0.60	1
277_(STM) 59.93	CIRCULAR	0.25	0.05	0.06	0.25	1
278_(STM) 55.46	CIRCULAR	0.25	0.05	0.06	0.25	1
279_(STM) 59.33	CIRCULAR	0.25	0.05	0.06	0.25	1
281_(STM) 59.93	CIRCULAR	0.25	0.05	0.06	0.25	1
283_(STM) 59.93	CIRCULAR	0.25	0.05	0.06	0.25	1
285_(STM) 65.28	CIRCULAR	0.25	0.05	0.06	0.25	1
286_(STM) 59.93	CIRCULAR	0.25	0.05	0.06	0.25	1
287_(STM) 55.46	CIRCULAR	0.25	0.05	0.06	0.25	1
288_(STM) 252.44	CIRCULAR	0.60	0.28	0.15	0.60	1
304_(STM) 58.51	CIRCULAR	0.25	0.05	0.06	0.25	1
49_(STM) 466.98	CIRCULAR	0.82	0.53	0.21	0.82	1
50_(STM) 88.67	CIRCULAR	0.38	0.11	0.09	0.38	1
51_(STM) 189.55	CIRCULAR	0.53	0.22	0.13	0.53	1
52_(STM) 207.50	CIRCULAR	0.53	0.22	0.13	0.53	1
53_(STM) 228.39	CIRCULAR	0.60	0.28	0.15	0.60	1
55_(STM) 370.91	CIRCULAR	0.75	0.44	0.19	0.75	1
56_(STM) 538.11	CIRCULAR	0.82	0.53	0.21	0.82	1
85_(STM) 40.71	CIRCULAR	0.25	0.05	0.06	0.25	1
87_(STM) 87.67	CIRCULAR	0.38	0.11	0.09	0.38	1
97(1)_(STM) 127.77	CIRCULAR	0.45	0.16	0.11	0.45	1
97_(STM) 86.94	CIRCULAR	0.38	0.11	0.09	0.38	1
MS-CBMH1 (1) 68188.85	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH1 (2) 63947.17	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH1 (3) 66096.82	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH1 (4) 136741.48	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH10 (1) 68188.85	RECT_OPEN	1.00	3.00	0.60	3.00	1

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MS-CBMH10 (2) 34844.26	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH10 (3) 40250.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH11 (1) 47951.44	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH11 (2) 49352.50	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH12 (1) 45024.40	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH12 (2) 93746.62	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH13 (1) 38531.43	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH13 (2) 77030.48	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH14 (1) 38531.43	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH14 (2) 38531.43	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH15 (1) 58273.32	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH15 (2) 71231.45	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH2 60599.46	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH3 (1) 60599.46	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH3 (2) 43489.78	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH3 (3) 40250.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH4 (1) 55859.79	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH4 (2) 65029.60	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH5 63947.17	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH5 (2) 57078.21	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH7 (1) 72222.70	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH7 (2) 57078.21	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH8 (1) 69215.12	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CBMH8 (2) 21977.24	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CICB1 (1) 40250.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CICB1 (2) 71231.45	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CICB2 (1) 52047.05	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-CICB2 (2) 75135.17	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE (1) 594.50	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYE1 18845.57	RECT_OPEN	1.00	3.00	0.60	3.00	1

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 PCSWMM Model Output
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MS-RYE10 (1) 18156.97	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE10 (2) 19510.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE10 (3) 76087.17	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE12 (1) 20778.96	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE12 (2) 25251.77	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE12 (3) 19510.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE12 (4) 18845.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE15 (1) 570.63	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYE15 (2) 717.64	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYE16 (1) 26259.77	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE16 (2) 69215.12	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE16 (3) 16696.95	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE18 (1) 49352.50	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE18 (2) 57078.21	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE2 (2) 548.30	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYE2 (3) 22553.72	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE2 (4) 59446.62	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE2 (5) 286.67	RECT_OPEN	0.30	0.90	0.25	3.00	1
MS-RYE3 (1) 623.18	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYE3 (2) 601.66	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYE3 (3) 579.70	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYE3 (4) 19510.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE3 (5) 57078.21	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE4 (1) 591.19	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYE4 (2) 508.79	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYE4 (3) 38047.95	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE4 (4) 18845.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE5 (1) 593.17	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYE5 (2) 505.68	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYE6 (1) 18845.57	RECT_OPEN	1.00	3.00	0.60	3.00	1

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 PCSWMM Model Output
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MS-RYE6 (2) 98714.78	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE7 (1) 19510.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE7 (2) 91222.33	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE8 (1) 27710.44	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE8 (2) 32971.11	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE9 (1) 23667.10	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYE9 (2) 17441.92	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT (1) 499.62	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYT1 (1) 588.32	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYT1 (2) 508.47	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYT1 (3) 28641.95	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT1 (4) 62848.65	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT10 (1) 5030.54	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT10 (2) 8713.59	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT10 (3) 91222.33	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT11 (2) 505.29	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYT11 (3) 21977.24	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT11 (4) 54616.39	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT12 2026.74	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT13 (1) 18156.97	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT13 (2) 65029.60	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT14 (1) 18845.57	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT14 (2) 66096.82	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT15 (1) 16696.95	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT15 (2) 70229.11	RECT_OPEN	1.00	3.00	0.60	3.00	1
MS-RYT3 (1) 537.63	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYT3 (2) 624.84	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYT3 (3) 286.67	RECT_OPEN	0.30	0.90	0.25	3.00	1
MS-RYT4 (1) 522.10	TRIANGULAR	0.30	0.45	0.15	3.00	1
MS-RYT4 (2) 617.49	TRIANGULAR	0.30	0.45	0.15	3.00	1

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MS-RYT4 (3)	RECT_OPEN	0.30	0.90	0.25	3.00	1
286.67						
MS-RYT5 (1)	RECT_OPEN	1.00	3.00	0.60	3.00	1
19510.57						
MS-RYT5 (2)	RECT_OPEN	1.00	3.00	0.60	3.00	1
45024.40						
MS-RYT5 (3)	TRIANGULAR	0.30	0.45	0.15	3.00	1
683.54						
MS-RYT5 (4)	TRIANGULAR	0.30	0.45	0.15	3.00	1
572.41						
MS-RYT6	TRIANGULAR	0.30	0.45	0.15	3.00	1
515.30						
MS-RYT7 (1)	TRIANGULAR	0.30	0.45	0.15	3.00	1
510.14						
MS-RYT7 (2)	TRIANGULAR	0.30	0.45	0.15	3.00	1
591.19						
MS-RYT7 (3)	RECT_OPEN	1.00	3.00	0.60	3.00	1
22553.72						
MS-RYT7 (4)	RECT_OPEN	1.00	3.00	0.60	3.00	1
58273.32						
MS-RYT8 (1)	TRIANGULAR	0.30	0.45	0.15	3.00	1
511.96						
MS-RYT8 (2)	TRIANGULAR	0.30	0.45	0.15	3.00	1
511.96						
MS-RYT8 (3)	RECT_OPEN	1.00	3.00	0.60	3.00	1
25251.77						
MS-RYT8 (4)	RECT_OPEN	1.00	3.00	0.60	3.00	1
65029.60						
MS-RYT9 (1)	TRIANGULAR	0.30	0.45	0.15	3.00	1
535.14						
MS-RYT9 (2)	TRIANGULAR	0.30	0.45	0.15	3.00	1
511.96						
MS-RYT9 (3)	RECT_OPEN	1.00	3.00	0.60	3.00	1
25251.77						
MS-RYT9 (4)	RECT_OPEN	1.00	3.00	0.60	3.00	1
70229.11						

Analysis Options

Flow Units LPS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method HORTON

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 05/19/2021 00:00:00

Ending Date 05/21/2021 00:00:00

Antecedent Dry Days 0.0

Report Time Step 00:01:00

Wet Time Step 00:02:00

Dry Time Step 00:05:00

Routing Time Step 1.00 sec
 Variable Time Step YES
 Maximum Trials 8
 Number of Threads 4
 Head Tolerance 0.001500 m

	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm
*****	-----	-----
Initial LID Storage	0.001	0.348
Total Precipitation	0.377	103.232
Evaporation Loss	0.000	0.000
Infiltration Loss	0.178	48.743
Surface Runoff	0.199	54.617
Final Storage	0.001	0.348
Continuity Error (%)	-0.123	

	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.199	1.994
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.003
External Outflow	0.200	1.997
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.012	0.117
Final Stored Volume	0.012	0.118
Continuity Error (%)	-0.020	

 Highest Continuity Errors

 Node MH200 (-12.53%)
 Node CBMH8 (11.66%)
 Node CBMH1 (5.81%)
 Node RYE7 (2.45%)

 Time-Step Critical Elements

 None

 Highest Flow Instability Indexes

 Link O-RYE7 (90)
 Link O-CBMH3 (74)
 Link O-CBMH1 (68)

Link O-CBMH8 (54)
 Link O-CBMH10 (13)

 Most Frequent Nonconverging Nodes

 Convergence obtained at all time steps.

 Routing Time Step Summary

 Minimum Time Step : 0.42 sec
 Average Time Step : 1.00 sec
 Maximum Time Step : 1.00 sec
 % of Time in Steady State : 0.00
 Average Iterations per Step : 2.00
 % of Steps Not Converging : 0.00
 Time Step Frequencies :
 1.000 - 0.871 sec : 99.93 %
 0.871 - 0.758 sec : 0.03 %
 0.758 - 0.660 sec : 0.01 %
 0.660 - 0.574 sec : 0.01 %
 0.574 - 0.500 sec : 0.02 %

 Subcatchment Runoff Summary

Perv	Total	Total	Total	Total	Total	Total	Imperv
Runoff	Runoff	Precip	Peak	Runoff	Evap	Infil	Runoff
Subcatchment	Runoff	Runoff	Runoff	Runoff	mm	mm	mm
mm	mm	10^6 ltr	mm	Coeff			

A1		103.23		0.00	0.00	70.70	7.23
25.43	32.66	0.01	9.30	0.316			
A10		103.23		0.00	0.00	66.42	13.42
23.49	36.91	0.04	33.50	0.358			
A11		103.23		0.00	0.00	33.51	57.89
11.97	69.87	0.10	49.51	0.677			
A12		103.23		0.00	0.00	29.59	63.06
10.73	73.78	0.08	36.84	0.715			
A13		103.23		0.00	0.00	21.99	73.41
7.99	81.40	0.02	10.18	0.789			
A14		103.23		0.00	0.00	70.56	7.23
25.58	32.81	0.01	12.51	0.318			
A15		103.23		0.00	0.00	40.43	48.58
14.35	62.93	0.08	42.10	0.610			
A16		103.23		0.00	0.00	65.32	14.45
23.58	38.03	0.02	15.71	0.368			
A17		103.23		0.00	0.00	43.06	45.49
14.80	60.29	0.09	46.54	0.584			

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 100yr, 24-hour SCS Storm

A18		103.23	0.00	0.00	34.26	56.86
12.25	69.11	0.17 79.14	0.669			
A19		103.23	0.00	0.00	54.66	28.92
19.77	48.69	0.03 22.46	0.472			
A2		103.23	0.00	0.00	31.20	61.00
11.17	72.17	0.09 43.16	0.699			
A20		103.23	0.00	0.00	66.13	13.42
23.80	37.22	0.04 31.28	0.361			
A21		103.23	0.00	0.00	70.12	7.23
26.03	33.25	0.02 18.86	0.322			
A22		103.23	0.00	0.00	54.06	29.96
19.32	49.28	0.04 28.57	0.477			
A23_1		103.23	0.00	0.00	51.23	34.11
18.00	52.11	0.07 42.63	0.505			
A23_2		103.23	0.00	0.00	51.23	34.11
18.00	52.11	0.05 29.80	0.505			
A24		103.23	0.00	0.00	40.50	48.59
14.27	62.86	0.07 35.37	0.609			
A25		103.23	0.00	0.00	31.92	59.96
11.49	71.45	0.10 46.55	0.692			
A26		103.23	0.00	0.00	52.56	32.02
18.76	50.78	0.04 25.43	0.492			
A27		103.23	0.00	0.00	68.86	9.29
25.19	34.49	0.05 46.39	0.334			
A28		103.23	0.00	0.00	31.87	59.95
11.55	71.50	0.09 40.03	0.693			
A29		103.23	0.00	0.00	70.90	7.23
25.22	32.44	0.02 15.23	0.314			
A3		103.23	0.00	0.00	65.52	14.45
23.37	37.82	0.05 37.13	0.366			
A31		103.23	0.00	0.00	65.50	14.45
23.39	37.85	0.02 15.50	0.367			
A32		103.23	0.00	0.00	37.29	52.72
13.36	66.07	0.07 32.84	0.640			
A4		103.23	0.00	0.00	35.01	55.82
12.54	68.36	0.09 42.86	0.662			
A5		103.23	0.00	0.00	54.65	28.92
19.78	48.69	0.03 22.47	0.472			
A6		103.23	0.00	0.00	71.05	7.23
25.04	32.27	0.06 54.15	0.313			
A7		103.23	0.00	0.00	29.65	63.07
10.66	73.73	0.06 26.31	0.714			
A8		103.23	0.00	0.00	33.51	57.89
11.97	69.86	0.10 49.51	0.677			
A9		103.23	0.00	0.00	54.66	28.92
19.77	48.69	0.03 22.46	0.472			
U1		103.23	0.00	0.00	64.95	14.45
24.01	38.46	0.03 28.71	0.373			
U2		103.23	0.00	0.00	66.54	12.39
24.47	36.86	0.01 9.54	0.357			
U3		103.23	0.00	0.00	70.07	7.24
26.22	33.46	0.02 15.83	0.324			
U4		103.23	0.00	0.00	53.48	29.95
19.93	49.88	0.04 29.15	0.483			
U5		103.23	0.00	0.00	54.01	29.95
19.38	49.33	0.02 15.94	0.478			

Node Depth Summary

Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days hr:min	Reported Max Depth Meters
CBMH4-Dummy	JUNCTION	0.09	2.25	97.47	0 12:06	2.25
HP-CBMH1	JUNCTION	0.00	0.00	97.08	0 00:00	0.00
HP-CBMH1 (2)	JUNCTION	0.00	0.00	97.06	0 00:00	0.00
HP-CBMH10	JUNCTION	0.00	0.00	97.20	0 00:00	0.00
HP-CBMH11	JUNCTION	0.00	0.01	97.26	0 12:01	0.01
HP-CBMH12	JUNCTION	0.00	0.00	97.70	0 00:00	0.00
HP-CBMH13	JUNCTION	0.00	0.00	97.66	0 00:00	0.00
HP-CBMH14	JUNCTION	0.00	0.05	97.39	0 12:01	0.05
HP-CBMH15	JUNCTION	0.00	0.00	97.75	0 00:00	0.00
HP-CBMH2	JUNCTION	0.00	0.01	97.12	0 12:00	0.01
HP-CBMH3	JUNCTION	0.00	0.01	97.38	0 12:01	0.01
HP-CBMH4	JUNCTION	0.00	0.00	97.54	0 00:00	0.00
HP-CBMH5	JUNCTION	0.00	0.00	97.68	0 00:00	0.00
HP-CBMH7	JUNCTION	0.00	0.00	97.16	0 00:00	0.00
HP-CBMH8	JUNCTION	0.00	0.00	97.27	0 00:00	0.00
HP-CICB1	JUNCTION	0.00	0.01	97.12	0 12:00	0.01
HP-CICB2	JUNCTION	0.00	0.01	97.65	0 12:00	0.01
HP-RYE10	JUNCTION	0.00	0.00	97.50	0 00:00	0.00
HP-RYE12	JUNCTION	0.00	0.00	97.33	0 00:00	0.00
HP-RYE12 (2)	JUNCTION	0.00	0.00	97.31	0 00:00	0.00
HP-RYE15	JUNCTION	0.00	0.00	97.68	0 00:00	0.00
HP-RYE16 (1)	JUNCTION	0.00	0.00	97.85	0 00:00	0.00
HP-RYE18	JUNCTION	0.00	0.01	96.99	0 12:26	0.00
HP-RYE2 (1)	JUNCTION	0.00	0.00	97.68	0 00:00	0.00
HP-RYE2 (2)	JUNCTION	0.00	0.00	97.66	0 00:00	0.00
HP-RYE2 (3)	JUNCTION	0.00	0.00	97.70	0 00:00	0.00
HP-RYE3 (1)	JUNCTION	0.00	0.00	97.52	0 00:00	0.00
HP-RYE3 (2)	JUNCTION	0.00	0.00	97.69	0 00:00	0.00
HP-RYE3 (3)	JUNCTION	0.00	0.00	97.55	0 00:00	0.00
HP-RYE4	JUNCTION	0.00	0.00	97.35	0 00:00	0.00
HP-RYE4 (2)	JUNCTION	0.00	0.00	97.45	0 00:00	0.00
HP-RYE5	JUNCTION	0.00	0.00	97.15	0 00:00	0.00
HP-RYE6	JUNCTION	0.00	0.00	97.60	0 00:00	0.00
HP-RYE7	JUNCTION	0.00	0.00	97.37	0 00:00	0.00
HP-RYE8	JUNCTION	0.00	0.00	97.50	0 00:00	0.00
HP-RYE9	JUNCTION	0.00	0.00	97.59	0 00:00	0.00
HP-RYT1 (1)	JUNCTION	0.00	0.00	97.76	0 00:00	0.00
HP-RYT1 (2)	JUNCTION	0.00	0.00	97.67	0 00:00	0.00
HP-RYT10 (1)	JUNCTION	0.00	0.00	97.48	0 00:00	0.00
HP-RYT10 (2)	JUNCTION	0.00	0.00	97.45	0 00:00	0.00
HP-RYT11 (1)	JUNCTION	0.00	0.00	97.69	0 00:00	0.00
HP-RYT11 (2)	JUNCTION	0.00	0.00	97.77	0 12:00	0.00
HP-RYT13	JUNCTION	0.00	0.00	97.30	0 00:00	0.00
HP-RYT14	JUNCTION	0.00	0.00	97.43	0 00:00	0.00
HP-RYT15	JUNCTION	0.00	0.00	97.59	0 00:00	0.00
HP-RYT3 (1)	JUNCTION	0.00	0.00	97.66	0 00:00	0.00
HP-RYT3 (2)	JUNCTION	0.00	0.00	97.65	0 00:00	0.00
HP-RYT4	JUNCTION	0.00	0.00	97.65	0 00:00	0.00
HP-RYT4 (2)	JUNCTION	0.00	0.00	97.50	0 00:00	0.00
HP-RYT5 (1)	JUNCTION	0.00	0.01	97.39	0 12:01	0.01

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HP-RYT5 (2)	JUNCTION	0.00	0.00	97.50	0	00:00	0.00
HP-RYT5 (3)	JUNCTION	0.00	0.01	97.39	0	12:01	0.01
HP-RYT6	JUNCTION	0.00	0.00	97.49	0	00:00	0.00
HP-RYT7	JUNCTION	0.00	0.00	97.57	0	00:00	0.00
HP-RYT7 (2)	JUNCTION	0.00	0.00	97.35	0	00:00	0.00
HP-RYT8 (1)	JUNCTION	0.00	0.00	97.17	0	00:00	0.00
HP-RYT8 (2)	JUNCTION	0.00	0.00	97.15	0	00:00	0.00
HP-RYT9 (1)	JUNCTION	0.00	0.00	97.44	0	00:00	0.00
HP-RYT9 (2)	JUNCTION	0.00	0.00	97.10	0	00:00	0.00
HP-RYE1	OUTFALL	0.00	0.00	97.61	0	00:00	0.00
HP-RYE16 (2)	OUTFALL	0.00	0.00	97.69	0	00:00	0.00
MH1013	OUTFALL	0.97	0.97	95.05	0	00:00	0.97
OF1	OUTFALL	0.00	0.00	97.00	0	00:00	0.00
OF2	OUTFALL	0.00	0.00	97.73	0	00:00	0.00
OF3	OUTFALL	0.00	0.00	97.15	0	00:00	0.00
OF4	OUTFALL	0.00	0.00	96.85	0	00:00	0.00
OF5	OUTFALL	0.00	0.00	0.00	0	00:00	0.00
CBMH1	STORAGE	0.47	2.21	96.98	0	12:26	2.21
CBMH10	STORAGE	0.24	2.17	97.02	0	12:06	2.17
CBMH11	STORAGE	0.19	2.32	97.22	0	12:05	2.32
CBMH12	STORAGE	0.04	2.07	97.22	0	12:04	2.07
CBMH13	STORAGE	0.18	2.48	97.39	0	12:01	2.48
CBMH14	STORAGE	0.13	2.30	97.39	0	12:01	2.30
CBMH15	STORAGE	0.14	2.30	97.65	0	12:10	2.30
CBMH2	STORAGE	0.27	2.24	97.10	0	12:06	2.24
CBMH3	STORAGE	0.12	2.29	97.27	0	12:07	2.29
CBMH4	STORAGE	0.10	2.35	97.47	0	12:06	2.35
CBMH5	STORAGE	0.45	2.30	97.59	0	12:22	2.30
CBMH7	STORAGE	0.47	0.52	95.10	0	12:00	0.52
CBMH8	STORAGE	0.31	2.28	97.13	0	12:10	2.28
CICB1	STORAGE	0.03	1.70	97.12	0	12:00	1.70
CICB2	STORAGE	0.03	1.61	97.65	0	12:00	1.61
MH100	STORAGE	0.95	0.96	95.06	0	12:00	0.96
MH102	STORAGE	0.92	0.94	95.07	0	12:00	0.94
MH104	STORAGE	0.90	0.93	95.08	0	12:00	0.93
MH106	STORAGE	0.74	0.80	95.11	0	12:00	0.80
MH108	STORAGE	0.52	0.61	95.14	0	12:00	0.61
MH110	STORAGE	0.40	0.50	95.15	0	12:00	0.50
MH112	STORAGE	0.26	0.37	95.16	0	12:01	0.37
MH114	STORAGE	0.02	0.15	95.24	0	12:02	0.15
MH116	STORAGE	0.02	0.13	95.25	0	12:03	0.13
MH118	STORAGE	0.02	0.11	95.26	0	12:03	0.11
MH200	STORAGE	0.36	0.42	95.11	0	12:00	0.42
MH202	STORAGE	0.28	2.25	97.13	0	12:10	2.25
MH204	STORAGE	0.16	2.10	97.03	0	12:01	2.10
MH206	STORAGE	0.11	2.17	97.65	0	12:09	2.17
RYE1	STORAGE	0.12	1.60	97.59	0	12:17	1.60
RYE10	STORAGE	0.03	1.75	97.22	0	12:00	1.75
RYE11	STORAGE	0.02	1.53	97.17	0	12:00	1.53
RYE12	STORAGE	0.01	1.53	97.29	0	12:00	1.53
RYE13	STORAGE	0.01	1.46	97.37	0	12:00	1.46
RYE14	STORAGE	0.01	1.49	97.59	0	12:00	1.49
RYE15	STORAGE	0.13	1.73	97.59	0	12:19	1.73
RYE16	STORAGE	0.09	1.87	97.65	0	12:09	1.87
RYE17	STORAGE	0.02	1.43	97.69	0	11:52	1.42
RYE18	STORAGE	0.30	2.05	96.99	0	12:26	2.04
RYE2	STORAGE	0.08	2.06	97.57	0	12:00	2.06

RYE3	STORAGE	0.03	1.48	97.44	0	12:00	1.48
RYE4	STORAGE	0.07	1.88	97.14	0	12:01	1.88
RYE5	STORAGE	0.19	1.85	96.99	0	12:26	1.84
RYE6	STORAGE	0.08	1.68	97.13	0	12:09	1.68
RYE7	STORAGE	0.02	0.70	95.73	0	12:00	0.69
RYE8	STORAGE	0.04	2.02	97.17	0	12:00	2.02
RYE9	STORAGE	0.04	1.88	97.04	0	12:00	1.88
RYT1	STORAGE	0.17	2.00	97.59	0	12:20	2.00
RYT10	STORAGE	0.12	2.06	97.03	0	12:01	2.06
RYT11	STORAGE	0.04	2.06	97.22	0	12:04	2.06
RYT12	STORAGE	0.02	1.68	97.13	0	12:00	1.68
RYT13	STORAGE	0.02	1.68	97.27	0	12:01	1.68
RYT14	STORAGE	0.01	1.64	97.36	0	12:00	1.64
RYT15	STORAGE	0.01	1.67	97.58	0	12:00	1.66
RYT16	STORAGE	0.02	1.59	97.66	0	11:52	1.59
RYT17	STORAGE	0.12	2.06	97.03	0	12:01	2.06
RYT3	STORAGE	0.10	2.00	97.40	0	12:00	2.00
RYT4	STORAGE	0.11	2.17	97.40	0	12:01	2.17
RYT5	STORAGE	0.12	2.28	97.39	0	12:01	2.28
RYT6	STORAGE	0.04	1.74	97.36	0	12:01	1.74
RYT7	STORAGE	0.05	2.14	97.28	0	12:05	2.14
RYT8	STORAGE	0.24	2.21	97.10	0	12:07	2.21
RYT9	STORAGE	0.45	2.20	96.99	0	12:25	2.20

 Node Inflow Summary

-----			Maximum	Maximum	Lateral		
Total	Flow		Lateral	Total	Time of Max	Inflow	
Inflow	Balance		Inflow	Inflow	Occurrence	Volume	
Volume	Error	Type	LPS	LPS	days hr:min	10^6 ltr	
Node	Percent					10^6	
ltr							

CBMH4-Dummy		JUNCTION	0.00	4.10	0 11:40	0	
0.00215	-6.678						
HP-CBMH1		JUNCTION	0.00	0.00	0 00:00	0	
0	0.000 ltr						
HP-CBMH1(2)		JUNCTION	0.00	0.00	0 00:00	0	
0	0.000 ltr						
HP-CBMH10		JUNCTION	0.00	0.00	0 00:00	0	
0	0.000 ltr						
HP-CBMH11		JUNCTION	0.00	24.99	0 12:01	0	
0.00648	0.001						
HP-CBMH12		JUNCTION	0.00	0.00	0 00:00	0	
0	0.000 ltr						
HP-CBMH13		JUNCTION	0.00	0.00	0 00:00	0	
0	0.000 ltr						
HP-CBMH14		JUNCTION	0.00	95.45	0 12:00	0	
0.0362	-0.011						
HP-CBMH15		JUNCTION	0.00	0.00	0 00:00	0	
0	0.000 ltr						

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HP-CBMH2	JUNCTION	0.00	21.72	0	12:00	0
0.0118 0.001						
HP-CBMH3	JUNCTION	0.00	63.58	0	12:01	0
0.0165 -0.002						
HP-CBMH4	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-CBMH5	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-CBMH7	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-CBMH8	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-CICB1	JUNCTION	0.00	23.33	0	12:00	0
0.0128 0.129						
HP-CICB2	JUNCTION	0.00	36.96	0	12:00	0
0.0192 0.126						
HP-RYE10	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE12	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE12(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE15	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE16(1)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE18	JUNCTION	0.00	2.47	0	12:18	0
0.00319 -0.004						
HP-RYE2(1)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE2(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE2(3)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE3(1)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE3(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE3(3)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE4	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE4(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE5	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE6	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE7	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE8	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE9	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT1(1)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT1(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT10(1)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						

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HP-RYT10(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT11(1)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT11(2)	JUNCTION	10.18	10.18	0	12:00	0.0244
0.0244 -0.035						
HP-RYT13	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT14	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT15	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT3(1)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT3(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT4	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT4(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT5(1)	JUNCTION	0.00	31.62	0	12:01	0
0.0067 -0.001						
HP-RYT5(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT5(3)	JUNCTION	0.00	0.44	0	11:59	0
2.62e-05 0.000 ltr						
HP-RYT6	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT7	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT7(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT8(1)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT8(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT9(1)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYT9(2)	JUNCTION	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE1	OUTFALL	0.00	0.00	0	00:00	0
0 0.000 ltr						
HP-RYE16(2)	OUTFALL	0.00	0.00	0	00:00	0
0 0.000 ltr						
MH1013	OUTFALL	0.00	304.48	0	12:00	0
1.87 0.000						
OF1	OUTFALL	28.71	28.71	0	12:00	0.0346
0.0346 0.000						
OF2	OUTFALL	15.83	15.83	0	12:00	0.0167
0.0167 0.000						
OF3	OUTFALL	9.54	9.54	0	12:00	0.0111
0.0111 0.000						
OF4	OUTFALL	29.15	29.15	0	12:00	0.0449
0.0449 0.000						
OF5	OUTFALL	15.94	15.94	0	12:00	0.0247
0.0247 0.000						
CBMH1	STORAGE	42.63	107.62	0	11:59	0.0736
0.173 6.171						
CBMH10	STORAGE	46.54	98.17	0	11:59	0.0904
0.173 0.001						

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CBMH11		STORAGE	42.10	73.55	0	12:00	0.0818
0.131	-0.000						
CBMH12		STORAGE	0.00	22.13	0	11:59	0
0.0446	-0.007						
CBMH13		STORAGE	36.84	129.94	0	12:00	0.0812
0.118	0.010						
CBMH14		STORAGE	26.31	111.72	0	12:00	0.059
0.159	-0.040						
CBMH15		STORAGE	43.16	59.02	0	11:53	0.0938
0.116	-0.003						
CBMH2		STORAGE	79.14	113.99	0	11:58	0.166
0.224	0.003						
CBMH3		STORAGE	49.51	91.53	0	12:00	0.105
0.164	0.012						
CBMH4		STORAGE	49.51	49.51	0	12:00	0.105
0.107	0.014						
CBMH5		STORAGE	42.86	67.35	0	11:55	0.0889
0.143	0.000						
CBMH7		STORAGE	46.55	67.81	0	12:00	0.1
0.225	0.022						
CBMH8		STORAGE	40.03	57.61	0	11:54	0.0858
0.118	13.198						
CICB1		STORAGE	35.37	63.90	0	12:00	0.0691
0.114	-0.004						
CICB2		STORAGE	32.84	55.29	0	12:00	0.0661
0.1	-0.014						
MH100		STORAGE	0.00	304.32	0	12:00	0
1.87	-0.000						
MH102		STORAGE	0.00	304.16	0	12:00	0
1.87	0.002						
MH104		STORAGE	0.00	304.04	0	12:00	0
1.86	-0.540						
MH106		STORAGE	0.00	234.84	0	12:01	0
1.49	0.000						
MH108		STORAGE	0.00	150.28	0	12:01	0
0.98	0.000						
MH110		STORAGE	0.00	110.87	0	12:02	0
0.821	-0.002						
MH112		STORAGE	0.00	65.05	0	12:00	0
0.562	-0.000						
MH114		STORAGE	0.00	31.09	0	12:01	0
0.319	0.000						
MH116		STORAGE	0.00	12.91	0	12:10	0
0.238	0.001						
MH118		STORAGE	0.00	12.85	0	12:14	0
0.238	0.000						
MH200		STORAGE	0.00	21.34	0	12:00	0
0.113	-11.135						
MH202		STORAGE	0.00	23.32	0	11:53	0
0.0297	-0.087						
MH204		STORAGE	0.00	56.06	0	11:58	0
0.0881	-0.001						
MH206		STORAGE	0.00	23.19	0	11:53	0
0.0243	-0.032						
RYE1		STORAGE	0.00	9.24	0	11:52	0
0.00498	-0.073						
RYE10		STORAGE	12.51	12.51	0	12:00	0.0131
0.0132	-0.081						
RYE11		STORAGE	28.57	28.57	0	12:00	0.0444
0.0444	-0.005						

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RYE12		STORAGE	25.43	25.43	0	12:00	0.0406
0.0406	-0.010						
RYE13		STORAGE	22.46	22.46	0	12:00	0.0341
0.0341	-0.005						
RYE14		STORAGE	22.46	22.46	0	12:00	0.0341
0.0341	-0.009						
RYE15		STORAGE	0.00	16.42	0	11:53	0
0.00718	0.010						
RYE16		STORAGE	9.30	10.58	0	11:53	0.0098
0.0125	0.064						
RYE17		STORAGE	22.47	22.47	0	12:00	0.0341
0.0341	-0.006						
RYE18		STORAGE	29.80	29.80	0	12:00	0.0515
0.0529	-0.008						
RYE2		STORAGE	54.15	54.15	0	12:00	0.0613
0.0613	-0.037						
RYE3		STORAGE	33.50	33.50	0	12:00	0.0406
0.0406	-0.081						
RYE4		STORAGE	31.28	31.28	0	12:00	0.0372
0.0375	0.005						
RYE5		STORAGE	18.86	18.86	0	12:00	0.02
0.0203	-0.000						
RYE6		STORAGE	15.50	15.50	0	12:00	0.0189
0.019	0.039						
RYE7		STORAGE	15.23	15.23	0	12:00	0.0162
0.0184	2.507						
RYE8		STORAGE	46.39	46.39	0	12:00	0.0517
0.0517	-0.009						
RYE9		STORAGE	15.71	15.71	0	12:00	0.019
0.019	-0.018						
RYT1		STORAGE	37.13	55.29	0	11:53	0.0454
0.066	-0.002						
RYT10		STORAGE	0.00	19.11	0	11:57	0
0.0245	0.013						
RYT11		STORAGE	0.00	15.33	0	11:59	0
0.022	0.042						
RYT12		STORAGE	0.00	28.55	0	12:00	0
0.0444	-0.002						
RYT13		STORAGE	0.00	22.03	0	12:00	0
0.0406	0.003						
RYT14		STORAGE	0.00	20.43	0	12:00	0
0.0341	0.008						
RYT15		STORAGE	0.00	21.97	0	11:58	0
0.0341	0.012						
RYT16		STORAGE	0.00	22.46	0	12:00	0
0.0341	0.008						
RYT17		STORAGE	0.00	45.64	0	12:00	0
0.0521	-0.015						
RYT3		STORAGE	0.00	51.66	0	12:00	0
0.0618	-0.007						
RYT4		STORAGE	0.00	56.36	0	11:57	0
0.0745	0.004						
RYT5		STORAGE	0.00	51.64	0	11:57	0
0.0938	0.002						
RYT6		STORAGE	0.00	31.54	0	11:57	0
0.0419	0.014						
RYT7		STORAGE	0.00	24.58	0	12:00	0
0.0496	0.112						
RYT8		STORAGE	0.00	32.34	0	11:50	0
0.0463	0.009						

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RYT9 STORAGE 0.00 35.34 0 11:52 0
 0.0324 -0.027

 Node Surcharge Summary

Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Meters	Min. Depth Below Rim Meters
CBMH4-Dummy	JUNCTION	1.91	1.649	0.751
MH204	STORAGE	1.13	1.502	0.098
RYE17	STORAGE	0.54	1.180	0.970

 Node Flooding Summary

No nodes were flooded.

 Storage Volume Summary

Max	Maximum	Average	Avg	Evap	Exfil	Maximum	Max	Time of
Occurrence	Outflow	Volume	Pcnt	Pcnt	Pcnt	Volume	Pcnt	
Storage Unit		1000 m ³	Full	Loss	Loss	1000 m ³	Full	days
hr:min	LPS							
CBMH1		0.004	0.4	0.0	0.0	0.060	6.4	0
12:26	36.93							
CBMH10		0.000	0.1	0.0	0.0	0.018	3.0	0
12:06	36.87							
CBMH11		0.001	0.1	0.0	0.0	0.016	3.0	0
12:05	26.94							
CBMH12		0.000	1.1	0.0	0.0	0.002	60.9	0
12:04	20.83							
CBMH13		0.000	0.1	0.0	0.0	0.018	3.1	0
12:01	85.49							
CBMH14		0.000	0.1	0.0	0.0	0.010	3.5	0
12:01	102.06							
CBMH15		0.001	0.1	0.0	0.0	0.024	2.4	0
12:10	29.59							
CBMH2		0.001	0.2	0.0	0.0	0.056	7.1	0
12:06	40.74							
CBMH3		0.000	0.0	0.0	0.0	0.032	3.2	0
12:07	36.67							

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CBMH4		0.001	0.1	0.0	0.0	0.028	2.8	0
12:06	8.90							
CBMH5		0.002	0.3	0.0	0.0	0.032	5.0	0
12:22	31.52							
CBMH7		0.001	0.1	0.0	0.0	0.001	0.1	0
12:00	67.78							
CBMH8		0.001	0.2	0.0	0.0	0.024	4.7	0
12:10	22.49							
CICB1		0.000	1.1	0.0	0.0	0.001	62.5	0
12:00	63.88							
CICB2		0.000	1.1	0.0	0.0	0.001	63.2	0
12:00	55.28							
MH100		0.002	33.2	0.0	0.0	0.002	33.6	0
12:00	304.48							
MH102		0.002	31.7	0.0	0.0	0.002	32.5	0
12:00	304.32							
MH104		0.002	31.3	0.0	0.0	0.002	32.2	0
12:00	304.16							
MH106		0.001	26.5	0.0	0.0	0.001	28.5	0
12:00	235.54							
MH108		0.001	19.0	0.0	0.0	0.001	22.1	0
12:00	150.88							
MH110		0.000	14.8	0.0	0.0	0.001	18.4	0
12:00	111.61							
MH112		0.000	9.7	0.0	0.0	0.000	13.8	0
12:01	67.74							
MH114		0.000	0.9	0.0	0.0	0.000	6.2	0
12:02	31.08							
MH116		0.000	0.8	0.0	0.0	0.000	5.2	0
12:03	13.08							
MH118		0.000	0.7	0.0	0.0	0.000	4.3	0
12:03	12.91							
MH200		0.000	14.5	0.0	0.0	0.000	16.7	0
12:00	22.81							
MH202		0.000	11.0	0.0	0.0	0.004	89.5	0
12:10	19.05							
MH204		0.000	7.3	0.0	0.0	0.002	95.5	0
12:01	52.38							
MH206		0.000	5.0	0.0	0.0	0.002	95.1	0
12:09	18.60							
RYE1		0.000	4.7	0.0	0.0	0.000	64.5	0
12:17	4.83							
RYE10		0.000	0.9	0.0	0.0	0.000	60.5	0
12:00	12.42							
RYE11		0.000	0.8	0.0	0.0	0.000	61.2	0
12:00	28.55							
RYE12		0.000	0.5	0.0	0.0	0.000	63.7	0
12:00	22.03							
RYE13		0.000	0.5	0.0	0.0	0.000	61.0	0
12:00	20.43							
RYE14		0.000	0.5	0.0	0.0	0.000	62.3	0
12:00	21.97							
RYE15		0.000	5.1	0.0	0.0	0.000	68.6	0
12:19	1.96							
RYE16		0.000	3.2	0.0	0.0	0.000	66.7	0
12:09	12.84							
RYE17		0.000	0.7	0.0	0.0	0.000	59.6	0
11:52	22.46							
RYE18		0.000	10.4	0.0	0.0	0.000	71.5	0
12:26	29.78							

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RYE2		0.000	2.7	0.0	0.0	0.000	69.1	0
12:00	51.66							
RYE3		0.000	1.3	0.0	0.0	0.000	60.6	0
12:00	31.54							
RYE4		0.000	2.5	0.0	0.0	0.000	71.1	0
12:01	20.84							
RYE5		0.000	6.9	0.0	0.0	0.000	68.1	0
12:26	20.81							
RYE6		0.000	2.7	0.0	0.0	0.000	55.7	0
12:09	17.57							
RYE7		0.000	0.7	0.0	0.0	0.000	21.8	0
12:00	14.78							
RYE8		0.000	1.3	0.0	0.0	0.000	66.3	0
12:00	45.64							
RYE9		0.000	1.2	0.0	0.0	0.000	58.5	0
12:00	15.51							
RYT1		0.000	6.1	0.0	0.0	0.002	72.5	0
12:20	34.76							
RYT10		0.000	3.4	0.0	0.0	0.002	58.9	0
12:01	13.34							
RYT11		0.000	1.1	0.0	0.0	0.002	60.3	0
12:04	14.89							
RYT12		0.000	0.9	0.0	0.0	0.000	64.0	0
12:00	28.64							
RYT13		0.000	0.6	0.0	0.0	0.000	65.3	0
12:01	18.75							
RYT14		0.000	0.5	0.0	0.0	0.000	63.7	0
12:00	18.48							
RYT15		0.000	0.5	0.0	0.0	0.000	64.9	0
12:00	18.65							
RYT16		0.000	0.8	0.0	0.0	0.000	61.8	0
11:52	22.51							
RYT17		0.000	3.9	0.0	0.0	0.000	66.3	0
12:01	44.07							
RYT3		0.000	3.2	0.0	0.0	0.000	65.7	0
12:00	56.36							
RYT4		0.000	3.5	0.0	0.0	0.000	71.5	0
12:01	51.64							
RYT5		0.000	3.9	0.0	0.0	0.000	73.2	0
12:01	49.11							
RYT6		0.000	1.5	0.0	0.0	0.000	67.8	0
12:01	24.58							
RYT7		0.000	1.8	0.0	0.0	0.000	71.1	0
12:05	20.04							
RYT8		0.000	7.8	0.0	0.0	0.002	73.4	0
12:07	26.55							
RYT9		0.001	14.6	0.0	0.0	0.002	71.7	0
12:25	26.90							

 Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow LPS	Max Flow LPS	Total Volume 10^6 ltr

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HP-RYE1	0.00	0.00	0.00	0.000
HP-RYE16 (2)	0.00	0.00	0.00	0.000
MH1013	87.67	12.40	304.48	1.867
OF1	49.99	0.41	28.71	0.035
OF2	14.62	0.64	15.83	0.017
OF3	15.43	0.39	9.54	0.011
OF4	50.05	0.53	29.15	0.045
OF5	49.95	0.29	15.94	0.025

System	33.46	14.67	402.90	1.999

 Link Flow Summary

Link	Type	Maximum	Time of Max		Maximum	Max/	Max/
		Flow	Occurrence		Veloc	Full	Full
		LPS	days	hr:min	m/sec	Flow	Depth

100_ (STM)	CONDUIT	19.05	0	11:53	0.07	0.08	1.00
104_ (STM)	CONDUIT	31.23	0	11:52	0.11	0.16	1.00
106_ (STM)	CONDUIT	20.81	0	11:53	0.42	0.35	1.00
116_ (STM)	CONDUIT	26.55	0	11:51	0.09	0.11	1.00
118_ (STM)	CONDUIT	20.84	0	11:59	0.42	0.35	1.00
124_ (STM)	CONDUIT	20.72	0	11:51	0.42	0.49	1.00
128_ (STM)	CONDUIT	24.58	0	12:00	0.50	0.41	1.00
130_ (STM)	CONDUIT	31.54	0	11:57	0.78	0.53	1.00
132_ (STM)	CONDUIT	26.30	0	11:55	0.09	0.10	1.00
136_ (STM)	CONDUIT	17.57	0	11:53	0.46	0.29	1.00
150_ (1) (STM)	CONDUIT	51.66	0	12:00	1.05	1.25	1.00
152_ (1) (STM)	CONDUIT	56.36	0	11:57	0.36	0.13	1.00
173_ (STM)	CONDUIT	9.24	0	11:52	0.19	0.16	1.00
175_ (STM)	CONDUIT	20.83	0	11:59	0.42	0.49	1.00
207_ (STM)	CONDUIT	51.64	0	11:57	0.24	0.12	1.00
209_ (STM)	CONDUIT	4.10	0	11:40	0.09	0.02	1.00
229_ (STM)	CONDUIT	304.16	0	12:00	0.57	0.55	1.00
233_ (STM)	CONDUIT	52.38	0	11:59	0.74	0.81	1.00
236 (1) (STM)	CONDUIT	45.64	0	12:00	0.93	0.76	1.00
240_ (STM)	CONDUIT	12.91	0	12:10	0.56	0.13	0.32
250_ (STM)	CONDUIT	44.07	0	11:59	0.16	0.18	1.00
252_ (STM)	CONDUIT	13.34	0	11:58	0.05	0.06	1.00
253_ (STM)	CONDUIT	15.51	0	11:58	0.32	0.26	1.00
260_ (STM)	CONDUIT	51.36	0	11:52	1.05	1.13	1.00
266_ (STM)	CONDUIT	12.42	0	11:59	0.26	0.21	1.00
270_ (STM)	CONDUIT	14.89	0	11:59	0.16	0.07	1.00
277_ (STM)	CONDUIT	28.55	0	12:00	0.58	0.48	1.00
278_ (STM)	CONDUIT	27.53	0	12:00	0.56	0.50	1.00
279_ (STM)	CONDUIT	22.03	0	12:00	0.45	0.37	1.00
281_ (STM)	CONDUIT	20.43	0	12:00	0.42	0.34	1.00
283_ (STM)	CONDUIT	21.97	0	11:58	0.45	0.37	1.00
285_ (STM)	CONDUIT	16.42	0	11:53	0.33	0.25	1.00
286_ (STM)	CONDUIT	22.46	0	12:00	0.46	0.37	1.00
287_ (STM)	CONDUIT	22.51	0	12:00	0.46	0.41	1.00
288_ (STM)	CONDUIT	12.84	0	11:55	0.14	0.05	1.00
304_ (STM)	CONDUIT	28.48	0	11:59	0.58	0.49	1.00

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49_(STM)	CONDUIT	304.48	0	12:00	0.57	0.65	1.00
50_(STM)	CONDUIT	31.08	0	12:02	0.64	0.35	0.50
51_(STM)	CONDUIT	67.74	0	12:02	0.36	0.36	0.83
52_(STM)	CONDUIT	111.61	0	12:02	0.52	0.54	0.98
53_(STM)	CONDUIT	150.88	0	12:01	0.53	0.66	1.00
55_(STM)	CONDUIT	235.54	0	12:01	0.53	0.64	1.00
56_(STM)	CONDUIT	304.32	0	12:00	0.57	0.57	1.00
85_(STM)	CONDUIT	23.19	0	11:53	0.47	0.57	1.00
87_(STM)	CONDUIT	13.08	0	12:11	0.54	0.15	0.38
97(1)_(STM)	CONDUIT	67.78	0	12:00	0.43	0.53	1.00
97_(STM)	CONDUIT	22.81	0	12:00	0.21	0.26	1.00
MS-CBMH1 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.12
MS-CBMH1 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-CBMH1 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.12
MS-CBMH1 (4)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-CBMH10 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.08
MS-CBMH10 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-CBMH10 (3)	CONDUIT	21.72	0	12:00	0.11	0.00	0.07
MS-CBMH11 (1)	CONDUIT	24.98	0	12:01	0.14	0.00	0.07
MS-CBMH11 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-CBMH12 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-CBMH12 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.07
MS-CBMH13 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-CBMH13 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.08
MS-CBMH14 (1)	CONDUIT	95.45	0	12:00	0.36	0.00	0.11
MS-CBMH14 (2)	CONDUIT	94.47	0	12:00	0.36	0.00	0.11
MS-CBMH15 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.07
MS-CBMH15 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.10
MS-CBMH2	CONDUIT	21.72	0	12:00	0.42	0.00	0.13
MS-CBMH3 (1)	CONDUIT	38.60	0	12:01	0.17	0.00	0.09
MS-CBMH3 (2)	CONDUIT	63.58	0	12:01	0.25	0.00	0.09
MS-CBMH3 (3)	CONDUIT	24.99	0	12:01	0.89	0.00	0.01
MS-CBMH4 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.08
MS-CBMH4 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.08
MS-CBMH5	CONDUIT	0.00	0	00:00	0.00	0.00	0.10
MS-CBMH5 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.11
MS-CBMH7 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-CBMH7 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.10
MS-CBMH8 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.10
MS-CBMH8 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-CICB1 (1)	CONDUIT	23.33	0	12:00	0.11	0.00	0.07
MS-CICB1 (2)	CONDUIT	23.33	0	12:00	1.05	0.00	0.12
MS-CICB2 (1)	CONDUIT	36.96	0	12:00	0.11	0.00	0.11
MS-CICB2 (2)	CONDUIT	36.96	0	12:00	1.43	0.00	0.08
MS-RYE (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.12
MS-RYE1	CONDUIT	0.00	0	00:00	0.00	0.00	0.06
MS-RYE10 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYE10 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYE10 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.07
MS-RYE12 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.06
MS-RYE12 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYE12 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.06
MS-RYE12 (4)	CONDUIT	0.00	0	00:00	0.00	0.00	0.05
MS-RYE15 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.35
MS-RYE15 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.40
MS-RYE16 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.03
MS-RYE16 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.07

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MS-RYE16 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.03
MS-RYE18 (1)	CONDUIT	2.47	0	12:18	0.01	0.00	0.10
MS-RYE18 (2)	CONDUIT	2.46	0	12:18	0.01	0.00	0.12
MS-RYE2 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.12
MS-RYE2 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.04
MS-RYE2 (4)	CONDUIT	0.00	0	00:00	0.00	0.00	0.11
MS-RYE2 (5)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYE3 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.06
MS-RYE3 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.06
MS-RYE3 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.50
MS-RYE3 (4)	CONDUIT	0.00	0	00:00	0.00	0.00	0.02
MS-RYE3 (5)	CONDUIT	0.00	0	00:00	0.00	0.00	0.08
MS-RYE4 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.40
MS-RYE4 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.22
MS-RYE4 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.12
MS-RYE4 (4)	CONDUIT	0.00	0	00:00	0.00	0.00	0.03
MS-RYE5 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.23
MS-RYE5 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.23
MS-RYE6 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYE6 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.10
MS-RYE7 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYE7 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYE8 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYE8 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYE9 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYE9 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYT (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYT1 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.40
MS-RYT1 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.20
MS-RYT1 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.12
MS-RYT1 (4)	CONDUIT	0.00	0	00:00	0.00	0.00	0.10
MS-RYT10 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYT10 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYT10 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.08
MS-RYT11 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYT11 (3)	CONDUIT	2.92	0	12:00	0.25	0.00	0.00
MS-RYT11 (4)	CONDUIT	7.26	0	12:00	0.63	0.00	0.00
MS-RYT12	CONDUIT	1.17	0	12:00	0.09	0.00	0.00
MS-RYT13 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.05
MS-RYT13 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.06
MS-RYT14 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.03
MS-RYT14 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYT15 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.05
MS-RYT15 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.08
MS-RYT3 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYT3 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYT3 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYT4 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.23
MS-RYT4 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.23
MS-RYT4 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.00
MS-RYT5 (1)	CONDUIT	31.62	0	12:01	0.12	0.00	0.09
MS-RYT5 (2)	CONDUIT	31.62	0	12:01	0.12	0.00	0.09
MS-RYT5 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.27
MS-RYT5 (4)	CONDUIT	0.44	0	11:59	0.01	0.00	0.30
MS-RYT6	CONDUIT	0.00	0	00:00	0.00	0.00	0.29
MS-RYT7 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.22
MS-RYT7 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.29

MS-RYT7 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.07
MS-RYT7 (4)	CONDUIT	0.00	0	00:00	0.00	0.00	0.09
MS-RYT8 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.33
MS-RYT8 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.40
MS-RYT8 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.10
MS-RYT8 (4)	CONDUIT	0.00	0	00:00	0.00	0.00	0.13
MS-RYT9 (1)	CONDUIT	0.00	0	00:00	0.00	0.00	0.23
MS-RYT9 (2)	CONDUIT	0.00	0	00:00	0.00	0.00	0.33
MS-RYT9 (3)	CONDUIT	0.00	0	00:00	0.00	0.00	0.07
MS-RYT9 (4)	CONDUIT	0.00	0	00:00	0.00	0.00	0.12
O-CBMH10	ORIFICE	26.07	0	12:08			1.00
O-CBMH11	ORIFICE	21.22	0	12:08			1.00
O-CBMH13	ORIFICE	22.00	0	12:13			1.00
O-CBMH2	ORIFICE	20.76	0	12:13			1.00
O-CBMH3	ORIFICE	21.52	0	12:14			1.00
O-CICB1	ORIFICE	18.83	0	12:00			1.00
O-CICB2	ORIFICE	18.32	0	12:00			1.00
O-RYE7	ORIFICE	14.78	0	12:00			1.00
O-RYT13	ORIFICE	18.75	0	12:01			1.00
O-RYT14	ORIFICE	18.48	0	12:00			1.00
O-RYT15	ORIFICE	18.65	0	12:00			1.00
O-CBMH1	DUMMY	6.50	0	12:26			
O-CBMH14	DUMMY	6.62	0	12:01			
O-CBMH15	DUMMY	6.61	0	12:10			
O-CBMH4	DUMMY	8.73	0	12:06			
O-CBMH5	DUMMY	6.24	0	12:22			
O-CBMH8	DUMMY	6.59	0	12:10			

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Flow Classification Summary
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	Adjusted	Fraction of Time in Flow Class							
	/Actual	Up	Down	Sub	Sup	Up	Down	Norm	
Inlet	Length	Dry	Dry	Dry	Crit	Crit	Crit	Crit	Ltd
Conduit									
Ctrl									
100_ (STM)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00									
104_ (STM)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00									
106_ (STM)	1.00	0.00	0.47	0.00	0.53	0.00	0.00	0.00	0.88
0.00									
116_ (STM)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
0.00									
118_ (STM)	1.00	0.00	0.46	0.00	0.54	0.00	0.00	0.00	0.95
0.00									
124_ (STM)	1.00	0.00	0.47	0.00	0.53	0.00	0.00	0.00	0.96
0.00									
128_ (STM)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.97
0.00									
130_ (STM)	1.00	0.00	0.00	0.00	0.86	0.14	0.00	0.00	0.53
0.00									

Iron Valley II - 5331 Fernbank Road (121011)
 PCSWMM Model Output
 100yr, 24-hour SCS Storm

132_(STM) 0.00	1.00	0.00	0.00	0.00	0.58	0.00	0.00	0.42	0.78
136_(STM) 0.00	1.00	0.00	0.00	0.00	0.07	0.00	0.00	0.93	0.01
150_(1)_(STM) 0.00	1.00	0.00	0.46	0.00	0.54	0.00	0.00	0.00	0.92
152_(1)_(STM) 0.00	1.00	0.00	0.00	0.00	0.11	0.00	0.00	0.89	0.02
173_(STM) 0.00	1.00	0.00	0.87	0.00	0.13	0.00	0.00	0.00	0.66
175_(STM) 0.00	1.00	0.00	0.35	0.00	0.65	0.00	0.00	0.00	0.97
207_(STM) 0.00	1.00	0.00	0.00	0.00	0.18	0.00	0.00	0.82	0.05
209_(STM) 0.00	1.00	0.00	0.00	0.00	0.07	0.00	0.00	0.93	0.01
229_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
233_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
236(1)_(STM) 0.00	1.00	0.00	0.47	0.00	0.53	0.00	0.00	0.00	0.96
240_(STM) 0.00	1.00	0.00	0.11	0.00	0.89	0.00	0.00	0.00	0.79
250_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
252_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
253_(STM) 0.00	1.00	0.00	0.47	0.00	0.53	0.00	0.00	0.00	0.96
260_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.30
266_(STM) 0.00	1.00	0.00	0.00	0.00	0.04	0.01	0.00	0.95	0.01
270_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.55
277_(STM) 0.00	1.00	0.00	0.00	0.00	0.86	0.14	0.00	0.00	0.98
278_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.49
279_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.51
281_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.99
283_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.99
285_(STM) 0.00	1.00	0.00	0.88	0.00	0.12	0.00	0.00	0.00	0.65
286_(STM) 0.00	1.00	0.00	0.00	0.00	0.88	0.12	0.00	0.00	0.98
287_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.95
288_(STM) 0.00	1.00	0.00	0.00	0.00	0.07	0.00	0.00	0.93	0.00
304_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
49_(STM) 0.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
50_(STM) 0.00	1.00	0.00	0.26	0.00	0.74	0.00	0.00	0.00	1.00

MS-RYT11 (3)	1.00	0.49	0.00	0.00	0.00	0.00	0.00	0.51	0.00
MS-RYT11 (4)	1.00	0.49	0.00	0.00	0.00	0.00	0.00	0.51	0.00
MS-RYT12	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT13 (1)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT13 (2)	1.00	0.99	0.01	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT14 (1)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT14 (2)	1.00	0.99	0.01	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT15 (1)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT15 (2)	1.00	0.99	0.01	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT3 (1)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT3 (2)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT3 (3)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT4 (1)	1.00	0.98	0.02	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT4 (2)	1.00	0.98	0.02	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT4 (3)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT5 (1)	1.00	0.98	0.02	0.00	0.00	0.00	0.00	0.00	0.75
MS-RYT5 (2)	1.00	0.98	0.02	0.00	0.00	0.00	0.00	0.00	0.75
MS-RYT5 (3)	1.00	0.98	0.02	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT5 (4)	1.00	0.00	0.00	0.00	0.02	0.00	0.00	0.98	0.75
MS-RYT6	1.00	0.98	0.02	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT7 (1)	1.00	0.98	0.02	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT7 (2)	1.00	0.98	0.02	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT7 (3)	1.00	0.98	0.02	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT7 (4)	1.00	0.98	0.02	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT8 (1)	1.00	0.97	0.03	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT8 (2)	1.00	0.97	0.03	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT8 (3)	1.00	0.97	0.03	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT8 (4)	1.00	0.97	0.03	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT9 (1)	1.00	0.93	0.07	0.00	0.00	0.00	0.00	0.00	0.00
MS-RYT9 (2)	1.00	0.97	0.03	0.00	0.00	0.00	0.00	0.00	0.00

Iron Valley II - 5331 Fernbank Road (121011)
 PCSWMM Model Output
 100yr, 24-hour SCS Storm

MS-RYT9(3)	1.00	0.93	0.07	0.00	0.00	0.00	0.00	0.00	0.00
0.00									
MS-RYT9(4)	1.00	0.91	0.09	0.00	0.00	0.00	0.00	0.00	0.00
0.00									

 Conduit Surcharge Summary

Conduit	Hours Full			Hours	
	Both Ends	Upstream	Dnstream	Above Full Normal Flow	Capacity Limited
100_(STM)	2.97	2.97	3.01	0.01	0.01
104_(STM)	5.38	5.38	5.41	0.01	0.01
106_(STM)	5.37	5.37	26.31	0.01	0.01
116_(STM)	1.94	1.94	1.96	0.01	0.01
118_(STM)	1.93	1.93	2.51	0.01	0.01
124_(STM)	1.49	1.49	1.57	0.01	0.01
128_(STM)	1.20	1.20	1.49	0.01	0.01
130_(STM)	1.08	1.08	1.20	0.01	0.01
132_(STM)	4.24	4.24	4.30	0.01	0.01
136_(STM)	2.69	2.69	2.95	0.01	0.01
150_(1)_(STM)	2.90	2.90	3.26	0.09	0.09
152_(1)_(STM)	2.41	2.41	2.70	0.01	0.01
173_(STM)	4.16	4.16	5.17	0.01	0.01
175_(STM)	1.17	1.17	1.50	0.01	0.01
207_(STM)	2.72	2.72	3.01	0.01	0.01
209_(STM)	1.91	1.91	1.92	0.01	0.01
229_(STM)	48.00	48.00	48.00	0.01	0.01
233_(STM)	1.56	1.56	1.81	0.01	0.01
236(1)_(STM)	1.26	1.26	1.56	0.01	0.01
250_(STM)	1.10	1.10	1.13	0.01	0.01
252_(STM)	1.10	1.10	1.13	0.01	0.01
253_(STM)	1.24	1.24	1.56	0.01	0.01
260_(STM)	4.63	4.63	4.71	0.05	0.01
266_(STM)	0.91	0.91	1.15	0.01	0.01
270_(STM)	0.90	0.90	0.90	0.01	0.01
277_(STM)	0.60	0.60	0.75	0.01	0.01
278_(STM)	0.75	0.75	0.78	0.01	0.01
279_(STM)	0.33	0.33	0.38	0.01	0.01
281_(STM)	0.28	0.28	0.34	0.01	0.01
283_(STM)	0.28	0.28	0.34	0.01	0.01
285_(STM)	4.40	4.40	5.24	0.01	0.01
286_(STM)	0.54	0.54	0.68	0.01	0.01
287_(STM)	0.68	0.68	0.71	0.01	0.01
288_(STM)	2.43	2.43	2.45	0.01	0.01
304_(STM)	5.88	5.88	6.42	0.01	0.01
49_(STM)	48.00	48.00	48.00	0.01	0.01
52_(STM)	0.01	0.01	0.15	0.01	0.01
53_(STM)	0.11	0.11	1.04	0.01	0.01
55_(STM)	1.04	1.04	48.00	0.01	0.01
56_(STM)	48.00	48.00	48.00	0.01	0.01
85_(STM)	3.44	3.44	3.55	0.01	0.01
97(1)_(STM)	48.00	48.00	48.00	0.01	0.01

Iron Valley II - 5331 Fernbank Road (121011)
PCSWMM Model Output
100yr, 24-hour SCS Storm

97_ (STM)	0.35	0.35	48.00	0.01	0.01
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Analysis begun on: Wed Jun 17 14:26:30 2026
Analysis ended on: Wed Jun 17 14:26:41 2026
Total elapsed time: 00:00:11

HGL Summary Phase 1 (JFSA - 2019)

Notes:

1) both 24hr SCS and 3hr CHI storm HGL uses 24hr SCS dynamic BC from JFSA Monahan Drain Future-VII VURL model (March 2019) a fixed BC = 94.708 (100 yr SCS peak at PH1 outlet) was also used for the 3hr CHI event

Name	Ground (m)	USF (m)	HGL (m)			Difference USF-HGL (m)			Invert (m)
			24hr SCS	3hr CHI	Fixed 3hr CHI BC = 94.708	24hr SCS	3hr CHI	Fixed 3hr CHI BC=94.708	
1001	98.17	96.15	95.32	95.32	95.32	0.83	0.83	0.83	95.32
1002	97.85	96.08	95.28	95.28	95.28	0.80	0.80	0.80	95.07
1004E	97.91	95.84	95.17	95.17	95.17	0.67	0.67	0.67	95.43
1004N	97.91	95.84	95.53	95.53	95.53	0.31	0.31	0.31	-
1005	97.91	95.70	94.97	94.97	95.09	0.73	0.73	0.61	94.91
1006	97.70	95.50	94.83	94.74	95.05	0.67	0.76	0.45	94.35
1007	98.02	N/A	95.16	95.16	95.16	-	-	-	95.16
1008	97.95	N/A	95.10	95.10	95.13	-	-	-	94.89
1009	97.74	95.88	94.99	95.00	95.09	0.89	0.88	0.79	94.69
1010	97.67	95.77	94.82	94.78	95.05	0.95	0.99	0.72	94.44
1011	97.35	95.23	94.76	94.71	95.00	0.47	0.52	0.23	94.11
1012	97.02	N/A	94.76	94.71	95.00	-	-	-	93.91
1013	96.92	N/A	94.78	94.71	95.05	-	-	-	93.61
1014	97.00	N/A	94.77	94.71	95.03	-	-	-	93.53
1015	97.49	N/A	94.75	94.71	94.99	-	-	-	93.43
1016	96.79	N/A	94.74	94.71	94.95	-	-	-	93.33
1017	97.86	96.00	95.14	95.14	95.14	0.86	0.86	0.86	95.14
1018	97.78	95.60	95.05	95.05	95.07	0.55	0.55	0.53	94.85
1019	97.44	95.67	94.85	94.77	95.04	0.82	0.90	0.63	94.59
1020	97.40	95.32	94.85	94.72	95.04	0.47	0.60	0.28	94.49
1021	97.25	95.32	94.84	94.71	95.03	0.48	0.61	0.29	94.38
1022	97.53	95.70	95.12	95.12	95.15	0.58	0.58	0.55	94.88
1023	97.34	95.29	94.93	94.92	95.10	0.36	0.37	0.19	94.57
1024	97.19	95.27	94.83	94.71	95.03	0.44	0.56	0.24	94.18
1025	97.17	95.27	94.82	94.71	95.01	0.45	0.56	0.26	94.04
1026	97.55	95.47	94.89	94.89	95.07	0.58	0.58	0.40	94.76
1027	97.31	95.39	94.86	94.76	95.06	0.53	0.63	0.33	94.44
1028	97.09	95.31	94.81	94.71	95.00	0.50	0.60	0.31	94.18
1029	96.95	95.09	94.80	94.71	94.98	0.29	0.38	0.11	93.91
1030	98.00	95.23	94.75	94.71	94.91	0.48	0.52	0.32	94.39
1031	98.00	95.10	94.74	94.71	94.90	0.36	0.39	0.20	94.01
1033N	97.50	95.85	95.23	95.23	95.23	0.62	0.62	0.62	95.23
1033S	97.50	95.85	95.32	95.32	95.32	0.53	0.53	0.53	-
1034	97.43	95.75	95.32	95.32	95.32	0.43	0.43	0.43	95.11
1035	97.20	95.65	95.18	95.18	95.24	0.47	0.47	0.41	94.99
1035N	97.20	95.65	95.03	95.03	95.09	0.62	0.62	0.56	-
1036	97.34	95.51	94.91	94.89	95.07	0.60	0.62	0.44	94.60
1037	97.50	95.73	95.13	95.13	95.13	0.60	0.60	0.60	95.13
1038	97.33	95.58	95.12	95.12	95.12	0.46	0.46	0.46	94.94
1039	97.26	95.27	94.84	94.78	95.05	0.43	0.49	0.22	94.46
1040	97.15	95.40	94.89	94.89	95.02	0.51	0.51	0.38	94.76
1041	97.14	95.28	94.81	94.71	95.02	0.47	0.57	0.26	94.48
1042	97.19	95.14	94.79	94.71	95.00	0.35	0.43	0.14	94.09
1043	97.07	95.42	94.90	94.82	95.12	0.52	0.60	0.30	94.45
1044	97.02	95.32	94.79	94.79	94.99	0.53	0.53	0.33	94.65
1045	97.00	95.09	94.77	94.71	94.98	0.32	0.38	0.11	94.25
1046	96.70	95.00	94.76	94.71	94.96	0.24	0.29	0.04	93.86
1047	96.63	94.90	94.74	94.71	94.94	0.16	0.19	-0.04	93.74
1048	96.50	N/A	94.74	94.71	94.91	-	-	-	-
1048A	96.07	N/A	94.75	94.71	94.93	-	-	-	-
1049	96.86	95.05	94.74	94.71	94.92	0.31	0.34	0.13	93.72
1050	96.83	95.02	94.73	94.71	94.91	0.29	0.31	0.11	93.70
1051	96.75	95.02	94.75	94.71	94.89	0.27	0.31	0.13	93.58
1052	97.04	N/A	94.76	94.71	94.83	-	-	-	93.13
1053	97.22	95.42	95.06	95.06	95.22	0.36	0.36	0.20	94.72
1053B	97.20	N/A	94.81	95.15	94.80	-	-	-	93.09
DIVERSION	95.65	N/A	94.80	94.69	94.83	-	-	-	93.09
Monahan	95.05	N/A	94.71	94.71	94.71	-	-	-	92.88
N138	95.65	N/A	94.74	94.71	94.74	-	-	-	93.08

Level of clearance to USF less than 0.3 m
Level of clearance to USF less than 0.0 m



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Notes

- | 8 | AS RECORDED - SIDEWALK 'A' | DT | JR | 09.06.16 |
|----------|--|-----------|-----------|-----------------|
| 7 | REVISED DRIVEWAY & STAKE/Locations, ISSUED FOR FINAL APPROVAL | KJK | JBL | 09.02.25 |
| 6 | REVISED FINISHED ROAD GRADES ON COPE, TEMPLEDORF AND NORTHGRAVES (s) | KJK | JBL | 08.11.12 |
| 5 | REVISED LOT GRADING AND SERVING | KJK | JBL | 08.11.03 |
| 4 | ISSUED FOR CONSTRUCTION | KJK | JBL | 08.01.21 |
| 3 | REVISED AS PER CITY COMMENTS AND FINAL APPROVAL | KJK | JBL | 07.10.29 |
| 2 | REVISED AS PER CITY COMMENTS | KJK | JBL | 07.08.17 |
| 1 | ISSUED FOR CITY COMMENTS | KJK | JBL | 07.07.12 |
| Revision | | By | Appd. | YY.MM.DD |

Seal

DATE JUN.16/09

SOHO - KANATA SOUTH

Ottawa ON Canada

Project No. 160400502C

Scale
1:500H
1:50V

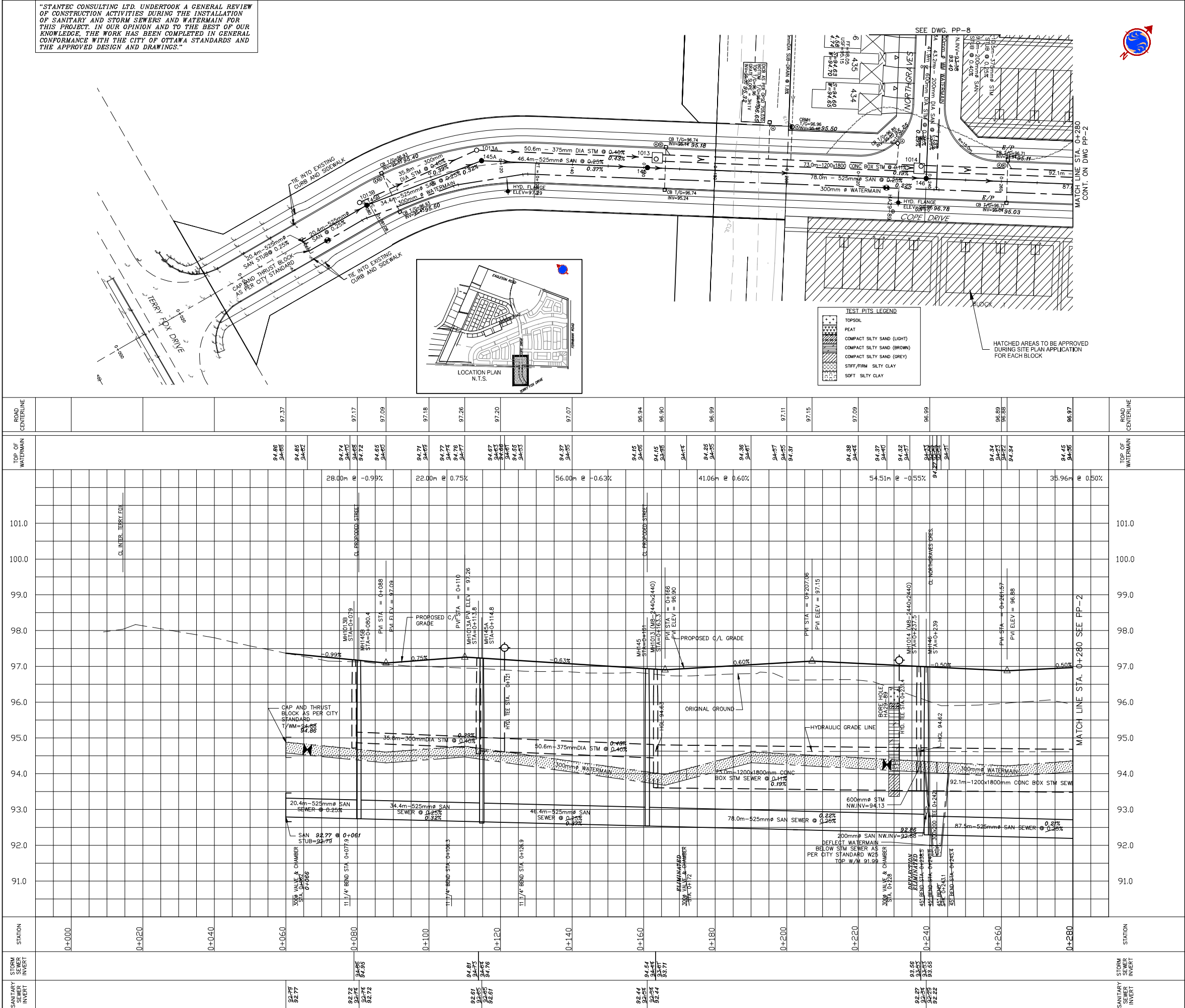


The scale bar consists of two horizontal lines. The top line is labeled '1:500H' and has markings at 0, 5, 15, and 25m. The bottom line is labeled '1:50V' and has markings at 0, 0.5, 1.5, and 2.5m. The horizontal line is divided into segments of 5m, 10m, and 15m. The vertical line is divided into segments of 0.5m, 1.0m, and 1.5m.

Drawing No. Sheet Revision

7 of 58

8



SITE SERVICING AND STORMWATER MANAGEMENT REPORT – TERRY FOX DRIVE AND COPE DRIVE COMMERCIAL SHOPPING DEVELOPMENT

Stormwater Management
July 26, 2018

Surface Storage & Overland Flow

- Building openings to be a minimum of 0.30m above the 100-year water level (City of Ottawa).
- Major system flow to be restricted to 781 L/s during the 100 year storm event (Soho West (Phase 1 and 2), Stormwater Management Report)
- Rooftop and parking lot storage to be maximized where possible.
- Maximum depth of flow under either static or dynamic conditions shall be less than 0.30m (City of Ottawa).
- Provide adequate emergency overflow conveyance off-site (City of Ottawa).
- Enhanced quality control (80% TSS removal) has been provided downstream of the development in Vortechs Cell 1 hydrodynamic separator.

5.2.1 Allowable Release Rate

The overall approach for storm servicing and stormwater management for the proposed development was initially outlined in the Serviceability Report – Cavanaugh Construction Ltd. / Karam SOHO West – Rev 3, Stantec Consulting Ltd., October 31, 2007 and Cavanaugh Construction – Soho West (Phase 1 and 2), Stormwater Management Report, Stantec Consulting Ltd. October 31, 2007

Discharge rates were assigned to the undeveloped parcels upstream of the SOHO Phase 1 subdivision. These are summarized in **Table 1** below. The external contributions are also identified on the Overall Storm Drainage Plan, OSD, SOHO-Kanata South included in **Appendix C.4**. The subject lands were identified as FUT-13B in the SOHO Phase 1 design.

Table 1: Target Release Rates for External Development Lands – SOHO-Kanata South

Drainage Area	Description	Minor System 100 Year Storm (L/s)	Major System 100 Year Storm (L/s)	Total Flow 100 Year Storm (L/s)
FUT-13A	Claridge Residential Lands	702.10	1,537	2,239
FUT-13B	Commercial Shopping Development (subject lands)	317.10	781	1,098

**CAVANAUGH CONSTRUCTION – SOHO WEST (PHASE 1 AND 2), KANATA WEST, CITY OF
OTTAWA STORMWATER MANAGEMENT REPORT**

October 31, 2007

Segment	Maximum Volume Used (m ³)	Max. Ponding Depth (cm)	Depth at Curb/Swale (cm)	Max. ICD Inflow (L/s)	Overflow Peak ¹ (L/s)
1-6CR	4.1	10.00	10.25	44.00	282
1-6DS	-	-	26.17	22.00	32
1-7AR	-	-	4.44	0.00	42
1-8AR	21.2	19.00	10.86	44.00	334
1-8BS	-	-	27.45	22.00	47
1-9AR	0.7	6.00	3.79	22.00	6
1-9BS	-	-	25.55	22.00	26
1-10AR	4.3	10.00	7.02	22.00	102
1-10BS	-	-	28.50	22.00	51
1-10CS	-	-	15.92	9.74	0
1-11AR	4.3	12.00	10.12	22.00	293
1-11BS	-	-	16.02	9.92	0
1-12AP	19.9	20.00	0.89	22.00	27
1-12BP	14.2	15.00	0.67	19.82	0
FUT-13AR	495.6	N/A	23.26	702.10	1,537
FUT-13BR	223.8	N/A	16.56	317.10	781
COPE-13AR	21.2	19.00	20.01	22.00	1,817
COPE-13BR	14.9	16.00	6.02	22.00	53
1-13AR	-	13.00	5.24	22.00	37
1-13BS	-	-	24.63	22.00	36
1-14R	62.0	22.00	20.07	22.00	1,833
1-15AR	43.8	22.00	20.22	22.00	1,869
1-15BR	21.3	17.00	10.64	22.00	337
1-16AS	-	-	31.33*	22.00	93
1-16BR	9.3	24.00	12.78	22.00	552
1-17AR	19.9	16.00	6.53	22.00	79
1-18AR	4.3	9.00	7.79	22.00	140
1-18BS	-	-	28.79	22.00	66
1-20AR	4.3	9.00	9.74	22.00	262
1-22AR	4.3	11.00	11.28	22.00	392
1-22BR	4.3	10.00	11.90	22.00	444
1-22CS	-	-	27.28	22.00	43
1-23AR	49.2	27.00	14.91	44.00	800
1-23BR	21.3	20.00	12.37	22.00	500
1-23CS	-	-	29.47	22.00	58
1-23DS	-	-	13.7	MINOR SYSTEM: SITE AREA = 3.73ha ALLOWABLE = 317.10 L/s (85L/s/ha)	
1-23ES	-	-	24.3		
1-25AR	6.3	12.00	15.0		
1-26AR	6.3	12.00	6.41	MAJOR SYSTEM STORAGE: SITE AREA = 3.73ha MAXIMUM VOLUME USED = 223.8m³ (60m³/ha)	
1-27AR	1.8	7.00	7.05		
1-27BR	1.8	7.00	7.81		
1-27CS	-	-	28.7		
1-27DS	-	-	28.1		
1-27ES	-	-	27.2		
1-28AR	21.2	20.00	16.1		
1-30AR	32.0	21.00	6.60		
1-31AR	32.0	18.00	17.5		

M:\2021\121011\CAD\Design\Figures\Culvert\121011-Culvert.dwg, CULVERT, Feb 18, 2022 - 2:21pm, rgrayton



NOVATECH

Engineers, Planners & Landscape Architects
Suite 200, 240 Michael Cowpland Drive
Ottawa, Ontario, Canada K2M 1P6

Telephone (613) 254-9643
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Website www.novatech-eng.com

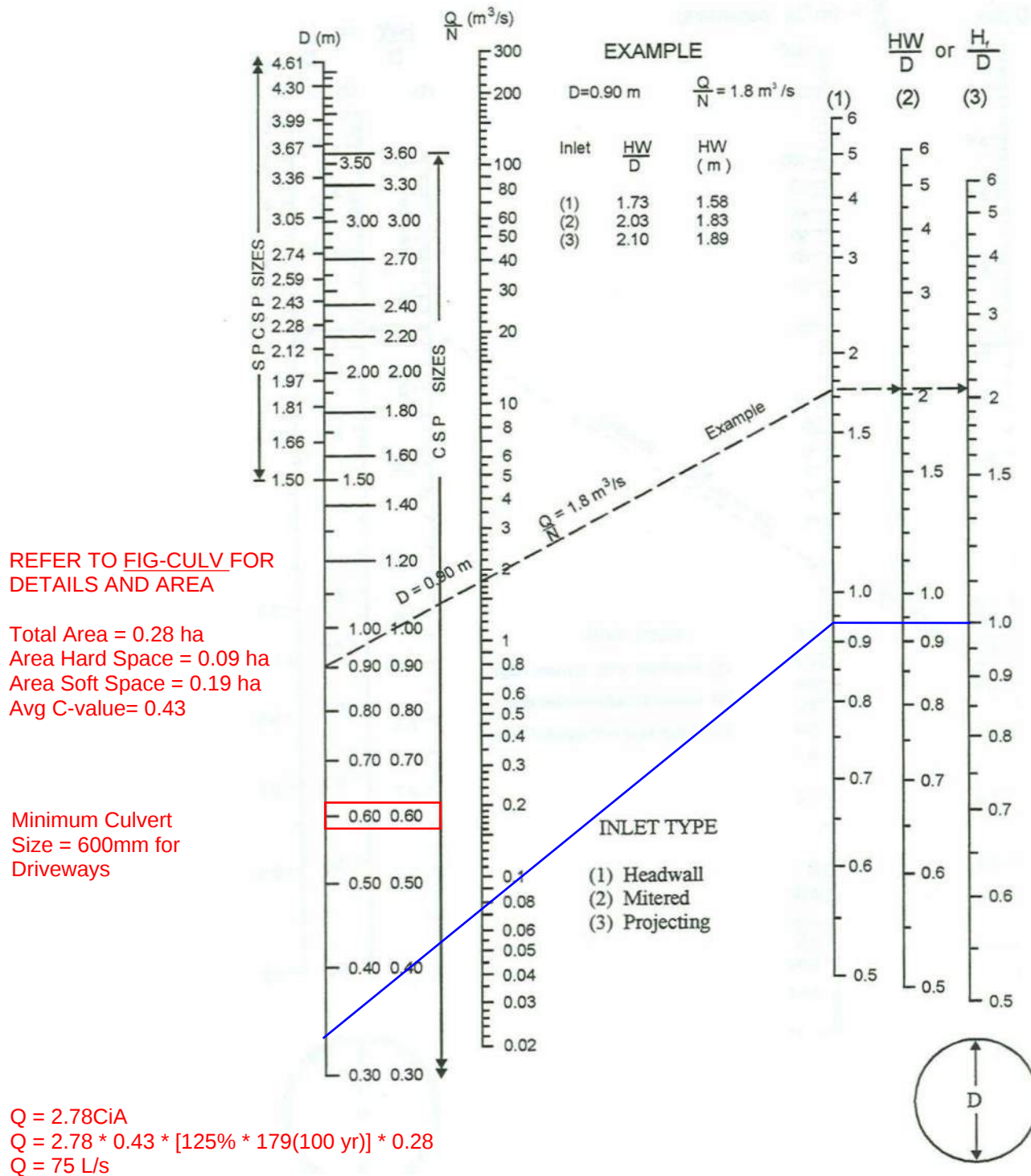
CITY OF OTTAWA
5331 FERNBANK ROAD
IRON VALLEY 2

POST DEVELOPMENT AREA
TRIBUTARY TO CULVERT AT TERRY
FOX DRIVE

1 : 1500

NOV 2025 121011 FIG-CULV

SHT11X17.DWG - 279mmX432mm

Design Chart 2.32: Inlet Control: Circular CSP and SPCSP Culverts

Source: Herr (1977)

Appendix B
SANITARY SEWER DESIGN

SANITARY SEWER DESIGN SHEET
IRON VALLEY 2 - 5331 FERNBANK RD
Developer: Claridge Homes



PROJECT # : 121011
DESIGNED BY : AE/BM
CHECKED BY : DDB
DATE PREPARED : 14-Nov-25
DATE REVISED : 23-Jun-26

LOCATION				RESIDENTIAL								PARK			INFILTRATION			FLOW	PROPOSED SEWER									
				INDIVIDUAL				CUMULATIVE				AREA (ha.)	Accu. AREA (ha.)	PARK FLOW Qc(p) (L/s)	Total Area (ha.)	Accu. Total AREA (ha.)	PEAK EXTRAN. FLOW Q(i) (L/s)	PEAK DESIGN FLOW Q(d) (L/s)										
STREET	FROM MH	TO MH	Area	Single Units	Townhouse Units	Apartment Units	Population (in 1000's)	AREA (ha.)	Population (in 1000's)	AREA (ha.)	PEAK FACTOR M								POPULATION FLOW Qr(p) (L/s)							LENGTH (m)	PIPE SIZE (mm)	PIPE ID (mm)
	217	117	A1			24	0.050	0.31	0.050	0.31	3.7	0.60		0.00	0.00	0.31	0.31	0.10	0.70	44.0	200	203.20	DR 35	1.00	34.2	1.06	2.0%	0.00
	215	117	A2			9	0.019	0.13	0.019	0.13	3.7	0.23		0.00	0.00	0.13	0.13	0.04	0.27	29.0	200	203.20	DR 35	1.00	34.2	1.06	0.8%	0.00
	117	115	A3			3	0.006	0.02	0.076	0.46	3.6	0.89		0.00	0.00	0.02	0.46	0.15	1.04	8.6	200	203.20	DR 35	0.35	20.2	0.62	5.1%	0.16
	115	113	A4					0.02	0.076	0.48	3.6	0.89	0.04	0.04	0.00	0.06	0.52	0.17	1.06	12.6	200	203.20	DR 35	0.40	21.6	0.67	4.9%	0.12
	113	111	A5					0.18	0.076	0.66	3.6	0.89	0.11	0.15	0.01	0.29	0.81	0.27	1.16	58.0	200	203.20	DR 35	0.33	19.7	0.61	5.9%	0.16
	213	111	A6			24	0.050	0.20	0.050	0.20	3.7	0.60		0.00	0.00	0.20	0.20	0.07	0.66	43.0	200	203.20	DR 35	1.00	34.2	1.06	1.9%	0.00
	111	109	A7					0.31	0.126	1.17	3.6	1.46	0.06	0.21	0.01	0.37	1.38	0.46	1.92	72.1	200	203.20	DR 35	0.33	19.7	0.61	9.8%	0.19
	211	109	A8			24	0.050	0.20	0.050	0.20	3.7	0.60		0.00	0.00	0.20	0.20	0.07	0.66	43.0	200	203.20	DR 35	1.00	34.2	1.06	1.9%	0.00
	109	107	A9					0.41	0.176	1.78	3.5	2.02		0.21	0.01	0.41	1.99	0.66	2.69	71.2	200	203.20	DR 35	0.34	20.0	0.62	13.5%	0.23
	209	107	A10			24	0.050	0.20	0.050	0.20	3.7	0.60		0.00	0.00	0.20	0.20	0.07	0.66	43.0	200	203.20	DR 35	1.00	34.2	1.06	1.9%	0.00
	207	107	A11			24	0.050	0.30	0.050	0.30	3.7	0.60		0.00	0.00	0.30	0.30	0.10	0.70	39.0	200	203.20	DR 35	1.00	34.2	1.06	2.0%	0.00
	107	105	A12					0.30	0.277	2.58	3.5	3.12		0.21	0.01	0.30	2.79	0.92	4.05	72.9	200	203.20	DR 35	0.34	20.0	0.62	20.3%	0.30
	205	105	A13			12	0.025	0.25	0.025	0.25	3.7	0.30		0.00	0.00	0.25	0.25	0.08	0.38	43.0	200	203.20	DR 35	1.00	34.2	1.06	1.1%	0.00
	203	201	A14			12	0.025	0.35	0.025	0.35	3.7	0.30		0.00	0.00	0.35	0.35	0.12	0.42	36.0	200	203.20	DR 35	1.00	34.2	1.06	1.2%	0.00
	201	105	A15			24	0.050	0.16	0.076	0.51	3.6	0.89		0.00	0.00	0.16	0.51	0.17	1.06	39.2	200	203.20	DR 35	0.33	19.7	0.61	5.4%	0.16
	105	103	A16					0.12	0.378	3.46	3.4	4.20		0.21	0.01	0.12	3.67	1.21	5.42	15.9	200	203.20	DR 35	0.38	21.1	0.65	25.7%	0.34
	103	101						0.00	0.378	3.46	3.4	4.20		0.21	0.01	0.00	3.67	1.21	5.42	21.6	200	203.20	DR 35	2.00	48.4	1.49	11.2%	0.23
COPE DRIVE	101	EX SANMH						0.00	0.378	3.46	3.4	4.20		0.21	0.01	0.00	3.67	1.21	5.42	15.0	200	203.20	DR 35	2.00	48.4	1.49	11.2%	0.23

Notes:
1. Q(d) = Qr(p) + Q(i) + Qc(p)
2. Q(i) = 0.33 L/sec/ha
3. Qr(p) = (P*q*M/86,400)
3. Qc(p) = (A*q*Pf)/86,400

Definitions:
Q(d) = Design Flow (L/sec)
Qr(p) = Population Flow (L/sec), Residential
Q(i) = Extraneous Flow (L/sec)
Qc(p) = Population Flow (L/sec), Commercial/Institutional/Park

P = Population (3.4 persons per single unit, 2.7 persons per townhouse unit, 2.1 persons per apartment unit)
q = Average per capita flow = 280 L/cap/day - Residential
q = Average per gross ha. flow = 3700 L/gross ha/day - Park (20L/day/person, 185 persons/ha - as per Appendix 4-A of the City of Ottawa Sewer Design Guidelines)
M = Harmon Formula (maximum of 4.0)
Min pipe size 200mm @ min. slope 0.32%
Mannings n = 0.013
Pf = Peak factor (Commercial/Insttional/Park) = 1.0 (less than 20% of total contributing areas), 1.5 (if area is 20% or greater of total contributing area)

day and maximum day demands. At a residual pressure of 20 psi, the available fire flow in the adjacent distribution systems was greater than 10,000 L/min.

4.0 SANITARY SEWER

4.1 Design Flows

The design criteria used to determine the sanitary flows produced by the proposed development is as follows;

Design Residential Domestic Flow per capita 350 L/cap/day

Capita per dwelling 2.7 persons per townhouse

Residential Peak Factor Where P is population in 1000s;

$$P.F. = 1 + \frac{14}{\sqrt{4 + P^{0.5}}}$$

Commercial Flow 50,000 L/ha/day

Commercial Peak Factor 1.5

Light Industrial Flow 35,000 L/ha/day

Light Industrial (Business Park) Peak Factor 4 (Appendix 4-B Ottawa Sewer Design Guidelines)

Infiltration 0.28 L/ha/day

Minimum Velocity 0.60 m/s

Minimum Pipe Size 250 mm dia. (0.432 % slope)

Table 4.1 - Sanitary Design Flows under Proposed Land Use and Zoning

	Proposed Zoning	Area (ha)	Pop. (1000's)	Peak Popul. Flow Q(p) (L/s)	Peak Busi. Flow Q(i) (L/s)	Peak Comm. Flow Q(c) (L/s)	Peak Extran. Flow Q(e) (L/s)	Peak Design Flow Q(d) (L/s)
Business Park (Light Industrial)	IP	13.58			22.00		3.80	25.81
Residential	R4	8.14	0.608	9.67			2.28	11.95
Commercial	IP	3.73				3.24	1.04	4.28
Total		25.45	0.608	9.67	22.00	3.24	7.13	42.04

16.23 L/s
SAN
Flow to
Cope Dr.

Serviceability Report

Cavanagh Construction Ltd. / Karam
SOHO West – Rev 3



Project #604-00502

Urban Land
1505 Laperriere Avenue
Ottawa, Ontario
K1Z 7T1
(613) 722-4420

October 31, 2007



Stantec



Cavanagh Construction
SOHO Development Phase 1 and 2

DATE: April 2007
REVISION: October 2007
DESIGNED BY: MJS
CHECKED BY: KK

**SANITARY SEWER
DESIGN SHEET**

(City of Ottawa)

FILE NUMBER: 1604-00502

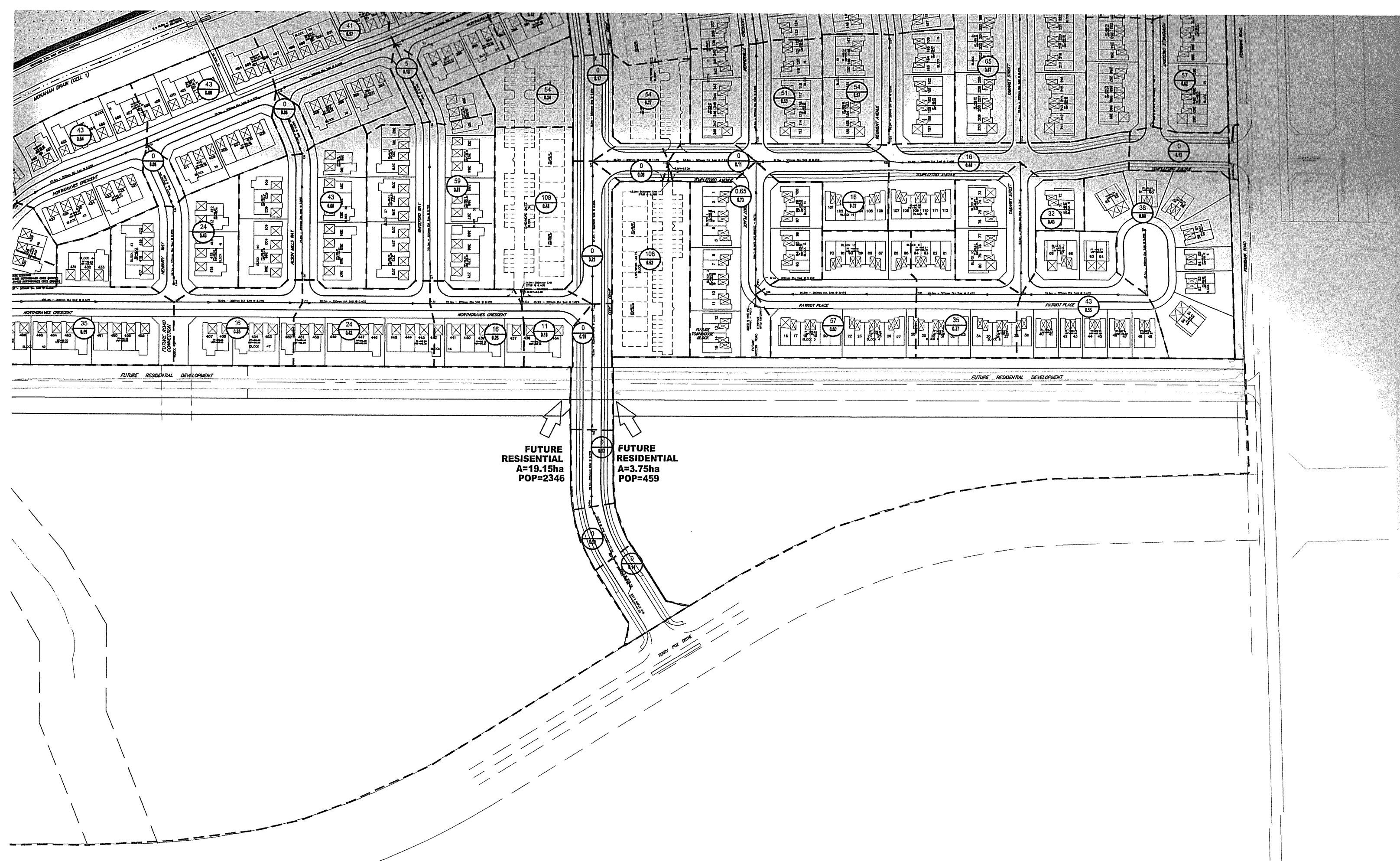
DESIGN PARAMETERS

AVG. DAILY FLOW / PERSON = 350 l/p/day
MINIMUM VELOCITY = 0.60 m/s
n = 0.013
MAX PEAK FACTOR = 4.0
MIN PEAK FACTOR = 2.4

COMMERCIAL 50,000.00 l/Ha/day
LIGHT INDUSTRIAL 35,000.00 l/Ha/day
INSTITUTIONAL 0.60 l/s/Ha
INFILTRATION 0.28 l/s/Ha
RESIDENTIAL HARMON PEAKING FACTOR PERSONS/UNIT = 4.0
KANATA WEST REPORT PERSONS/UNIT = 3.0
POPULATION DENSITY PER UNIT = Single Family = 3.4
Townhouse = 2.7

Peaking Factor Industrial: 1.5
Peaking Factor Comm. / Inst.: 1.5

LOCATION			RESIDENTIAL AREA AND POPULATION								COMM		INDUST		INSTH		C+I	INFILTRATION				PIPE					
STREET	FROM M.H.	TO M.H.	AREA (ha)	UNITS Singles	UNITS Towns	UNITS (KWR)	POP.	CUMULATIVE AREA (ha)	POP.	PEAK FACT	PEAK FLOW (l/s)	AREA (ha)	ACCU AREA (ha)	AREA (ha)	ACCU AREA (ha)	PEAK FLOW (l/s)	TOTAL AREA (ha)	ACCU AREA (ha)	INFILT FLOW (l/s)	TOTAL FLOW (l/s)	DIST (m)	DIA (mm)	SLOPE (%)	CAP. (FULL) (l/s)	VEL (FULL) (m/s)	VEL (ACT.) (m/s)	
Phase 1																											
PATRIOT PLACE	101	102	0.80		14	0	38	0.80	38	4.00	0.62					0.00	0.80	0.80	0.224	0.84	40.5	200	0.65	26.88	0.84	0.34	
PATRIOT PLACE	102	104	0.55		16	0	43	1.35	81	4.00	1.34					0.00	0.55	1.35	0.378	1.69	76.9	200	0.45	22.40	0.70	0.36	
PATRIOT PLACE	104	105	0.37		13	0	35	1.72	116	4.00	1.88					0.00	0.37	1.72	0.482	2.36	64.0	200	0.45	22.40	0.70	0.43	
PATRIOT PLACE	105	106	0.60		21	0	57	2.32	173	4.00	2.80					0.00	0.60	2.32	0.650	3.45	98.0	200	0.45	22.40	0.70	0.48	
PATRIOT PLACE	106	109	0.73		24	0	65	3.05	238	4.00	3.86					0.00	0.73	3.05	0.854	4.71	81.0	200	0.45	22.40	0.70	0.53	
TABARET STREET	104	107	0.43		12	0	32	0.43	32	4.00	0.52					0.00	0.43	0.43	0.120	0.64	83.8	200	0.70	27.84	0.87	0.35	
TEMPLEFORD AVENUE	107	108	0.48		6	0	16	0.91	48	4.00	0.78					0.00	0.48	0.91	0.255	1.04	81.0	200	0.45	22.40	0.70	0.33	
TEMPLEFORD AVENUE	108	109	0.31		6	0	16	1.22	64	4.00	1.04					0.00	0.31	1.22	0.342	1.38	81.0	200	0.45	22.40	0.70	0.36	
TEMPLEFORD AVENUE	109	110	0.11		0	0	0	4.38	302	4.00	4.89					0.00	0.11	4.38	1.226	6.12	53.6	200	0.84	30.72	0.96	0.71	
BLOCK 1	110B	110	0.52		40	0	108	0.52	108	4.00	1.75					0.00	0.52	0.52	0.146	1.90	111.5	200	0.75	29.12	0.91	0.47	
TEMPLEFORD AVENUE	110	147	0.08		0	0	0	4.98	410	4.00	5.64					0.00	0.08	4.98	1.394	8.03	46.5	200	1.18	36.48	1.14	0.89	
NORTHGRAVES	129	130	0.20		3	0	8	0.20	8	4.00	0.13					0.00	0.20	0.20	0.056	0.19	13.0	200	0.65	26.88	0.84	0.00	
NORTHGRAVES	130	131	0.59		13	0	35	0.79	43	4.00	0.70					0.00	0.59	0.79	0.221	0.92	105.2	200	0.45	22.40	0.70	0.33	
NORTHGRAVES	131	132	0.35		6	0	16	1.14	59	4.00	0.96					0.00	0.35	1.14	0.319	1.28	78.0	200	0.45	22.40	0.70	0.33	
NORTHGRAVES	132	133	0.42		9	0	24	1.56	83	4.00	1.34					0.00	0.42	1.56	0.437	1.78	78.0	200	0.45	22.40	0.70	0.36	
NORTHGRAVES	133	133A	0.26		6	0	16	1.82	99	4.00	1.60					0.00	0.26	1.82	0.510	2.11	55.4	200	0.45	22.40	0.70	0.41	
BLOCK 34 ****	133C	133B	0.24		20	0	54	0.24	54	4.00	0.88					0.00	0.24	0.24	0.067	0.95	42.5	200	0.65	26.88	0.84	0.34	
BLOCK 34 ****	133B	133A	0.48		40	0	108	0.72	162	4.00	2.63					0.00	0.48	0.72	0.202	2.83	113.0	200	0.40	21.12	0.66	0.44	
NORTHGRAVES	133A	146	0.16		4	0	11	2.70	272	4.00	4.41					0.00	0.16	2.70	0.756	5.17	43.2	200	1.09	34.88	1.09	0.75	
COPE DR ***	STUB	145B	125.14		0	0	8075	125.14	8075	3.05	99.77		28.72	28.72		17.45	153.86	153.86	43.681	160.30	20.4	525	0.25	223.00	1.00	1.09	
COPE DR	145B	145A	0.09		0	0	0	125.23	8075	3.05	99.77			28.72		17.45	0.09	153.95	43.106	160.33	34.4	525	0.25	223.00	1.00	1.09	
COPE DR	145A	145	0.12		0	0	0	125.35	8075	3.05	99.77			28.72		17.45	0.12	154.07	43.140	160.36	46.4	525	0.25	223.00	1.00	1.09	
COPE DR	145	146	23.14		0	0	2811	148.49	10886	2.92	128.72			28.72		17.45	23.14	177.21	49.619	195.84	78.0	525	0.25	223.00	1.00	1.14	
HENBURY WAY	134A	134	0.43		9	0	24	0.43	24	4.00	0.39					0.00	0.43	0.43	0.120	0.51	58.3	200	0.65	26.88	0.84	0.00	
HENBURY WAY	134	141	0.06		0	0	0	0.49	24	4.00	0.39					0.00	0.06	0.49	0.137	0.53	42.6	200	0.65	26.88	0.84	0.00	
ALSON MILLS WAY	135	136	0.68		16	0	43	0.68	43	4.00	0.70					0.00	0.68	0.68	0.190	0.89	79.9	200	0.65	26.88	0.84	0.34	
ALSON MILLS WAY	136	142	0.06		0	0	0	0.74	43	4.00	0.70					0.00	0.06	0.74	0.207	0.91	41.6	200	0.82	30.40	0.95	0.38	
WHITEFORD WAY	137	138	0.81		22	0	59	0.81	59	4.00	0.96					0.00	0.81	0.81	0.227	1.19	101.1	200	0.78	29.44	0.92	0.43	
WHITEFORD WAY	138	143	0.18		2	0	5	0.99	64	4.00	1.04					0.00	0.18	0.99	0.277	1.32	54.4	200	0.78	29.44	0.92	0.43	
NORTHGRAVES	129	139	0.22		4	0	11	0.22	11	4.00	0.18					0.00	0.22	0.22	0.062	0.24	26.7	200	0.65	26.88	0.84	0.00	
NORTHGRAVES	139	140	0.29		7	0	19	0.51	30	4.00	0.49					0.00	0.29	0.51	0.143	0.63	31.2	200	0.45	22.40	0.70	0.28	
NORTHGRAVES	140	141	0.64		16	0	43	1.15	73	4.00	1.18					0.00	0.64	8.00	2.240	3.42	87.6	200	0.65	26.88	0.84	0.55	
NORTHGRAVES	141	142	0.60		16	0	43	2.24	140	4.00	2.27					0.00	0.60	9.09	2.545	4.82	85.7	200	0.35	19.84	0.62	0.50	
NORTHGRAVES	142	143	0.57		15	0	41	3.55	224	4.00	3.63					0.00	0.57	10.40	2.912	6.54	79.8	200	0.55	24.96	0.78	0.64	
NORTHGRAVES	143	144	0.44		11	0	30	4.98	318	4.00	5.15					0.00	0.44	11.83	3.312	8.46	60.0	200	0.69	27.84	0.87	0.76	
NORTHGRAVES	144	149	0.42		10	0	27	5.40	345	4.00	5.59					0.00	0.42	12.25	3.450	9.02	64.5	200	0.69	27.84	0.87	0.77	



Trevor McKay

From: Cripps, Brad <brad.cripps@ottawa.ca>
Sent: Wednesday, March 20, 2019 11:52 AM
To: Trevor McKay
Cc: Surprenant, Eric
Subject: RE: Comment Clarification - D07-16-190001 & D07-16-18-0027

Hello Trevor,

The comment that was provided related to the Bridlewood 3 application was provided by the water resources group. I have reached out to them to confirm what was meant by that comment and the implications. My understanding now is that there is a spill relief protection for the Fernbank and Stittsville trunk lines near the Hazeldean PS at 95.3m, however there is no such spill point in the South Glencairn trunk line. The operation of the pump station has been set up so that during large events the Fernbank and Stittsville trunk lines will be isolated and allowed to spill if there is a need while the pump station capacity will be reserved for the South Glencairn trunk line.

In speaking with infrastructure planning their recommendation is to use 95.3m as an approximate design value for selecting appropriate USF elevations to provide some level of protection during a large event. In your email below a reference to 99.3m as a minimum USF, can you confirm where this value was determined?

If you would like to discuss further please feel free to contact me.

Brad Cripps, P.Eng.

Project Manager, Infrastructure Approvals
Development Review West
City of Ottawa
110 Laurier Avenue West, Ottawa ON, K1P 1J1
613-580-2424, Ext. 28699
Brad.Cripps@ottawa.ca

From: Surprenant, Eric <Eric.Surprenant@ottawa.ca>
Sent: March 18, 2019 3:21 PM
To: Cripps, Brad <brad.cripps@ottawa.ca>
Subject: FW: Comment Clarification - D07-16-190001 & D07-16-18-0027

Hi Brad,

Could you review the below. I was sure that you had spoken to me about this. Any information you can provide them on this?

Thanks
Eric S.

From: Trevor McKay <t.mckay@novatech-eng.com>
Sent: March 18, 2019 1:55 PM
To: Surprenant, Eric <Eric.Surprenant@ottawa.ca>
Cc: Drew Blair <D.Blair@novatech-eng.com>; Marc St.Pierre <m.stpierre@novatech-eng.com>
Subject: Comment Clarification - D07-16-190001 & D07-16-18-0027

Eric,

Further to my voicemail early last week, we are requesting clarification on the intent/meaning of comments that we have received in response to the submissions for draft plan approval on the Van Gaal Lands (1039 Terry Fox Drive & 5331 Fernbank Road, D07-16-18-0027) and Bridlewood 3 (866 & 898 Eagleson Road and 1355 & 1365 Terry Fox Drive, D07-16-190001).

We have been informed that you will be the Engineering lead on both files, taking over from Gabrielle Schaeffer.

We have received different information regarding the sanitary sewer outlet conditions on both projects.

1. On the Van Gaal lands project we were informed during the pre-consultation that the sanitary sewer had an overflow at the Hazledean Pump Station and that an elevation of 99.30 should be used for the minimum USF on site.
2. On the Bridlewood 3 project, we have received a comment (#46) which states that the Hazledean PS does not have an overflow for this branch of the sanitary sewer.

Based on our understanding of the sanitary sewer system, both proposed outlets flow to the trunk sewer on Akerson Road. They share a common outlet from the corner of Cope Drive and Akerson Road to the Hazledean Pump Station.

We would also like clarification on what the requirements relating to the submission of an HGL analysis for the sanitary sewer are for draft approval. We understand the request for an HGL analysis, however it is our suggestion that based on the proposed USF elevations being higher than downstream developments, that this should be a requirement at the detail design phase.

Your clarification is appreciated. We are available should you wish to call and discuss.

Trevor McKay, B.Eng., E.I.T., Project Coordinator | Engineering/Contract Administration

NOVATECH Engineers, Planners & Landscape Architects

240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 Ext: 291 | Cell: 613.263.9113 | Fax: 613.254.5867

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Appendix C
HYDRAULIC ANALYSIS

Population and Consumption Rate Calculations

Node	Number of Units	Persons per Unit	Population	Consumption Rates (L/s)		
				Average Daily	Maximum Daily	Maximum Hourly
R1	0	2.10	0	0.00	0.00	0.00
R2	0	2.10	0	0.00	0.00	0.00
N1	0	2.10	0	0.00	0.00	0.00
N2	0	2.10	0	0.00	0.00	0.00
N3	0	2.10	0	0.00	0.00	0.00
N4	0	2.10	0	0.00	0.00	0.00
N5	0	2.10	0	0.00	0.00	0.00
N6	12	2.10	25	0.08	0.25	0.37
N7	0	2.10	0	0.00	0.00	0.00
N8	0	2.10	0	0.00	0.00	0.00
N9	0	2.10	0	0.00	0.00	0.00
N10	0	2.10	0	0.00	0.00	0.00
N11	24	2.10	50	0.16	0.49	0.74
N12	12	2.10	25	0.08	0.25	0.37
N13	12	2.10	25	0.08	0.25	0.37
N14	24	2.10	50	0.16	0.49	0.74
N15	24	2.10	50	0.16	0.49	0.74
N16	24	2.10	50	0.16	0.49	0.74
N17	24	2.10	50	0.16	0.49	0.74
N18	24	2.10	50	0.16	0.49	0.74
Total	180	2.10	378	1.23	3.68	5.51

Water Demand Parameters

Zen Units	2.10	persons/unit
Residential Demand	280	L/c/day
Residential Max Day	3.0	x Avg Day
Residential Peak Hour	4.5	x Avg Day
Max Fire Flow (FF1)	266.67	L/s

Junction Report

Node ID	Elevation m	Demand LPS	Total Head m	Pressure m	Pressure kPa	Pressure psi	Age hours
Resvr R1	162.20	2.80	162.20	0.00	0.00	0.00	0.0
Resvr R2	162.30	-4.00	162.30	0.00	0.00	0.00	0.0
Junc N1	96.90	0.00	162.20	65.30	640.59	92.91	1.7
Junc N2	97.00	0.00	162.20	65.20	639.61	92.77	1.5
Junc N3	97.20	0.00	162.21	65.01	637.75	92.50	1.3
Junc N4	97.40	0.00	162.22	64.82	635.88	92.23	1.2
Junc N5	97.60	0.00	162.23	64.63	634.02	91.96	1.0
Junc N6	97.60	0.08	162.24	64.64	634.12	91.97	0.8
Junc N7	97.70	0.00	162.25	64.55	633.24	91.84	0.7
Junc N8	97.40	0.00	162.27	64.87	636.37	92.30	0.4
Junc N9	97.00	0.00	162.29	65.29	640.49	92.90	0.1
Junc N10	96.90	0.00	162.30	65.40	641.57	93.05	0.0
Junc N11	97.40	0.16	162.20	64.80	635.69	92.20	2.4
Junc N12	97.30	0.08	162.20	64.90	636.67	92.34	4.6
Junc N13	97.00	0.08	162.20	65.20	639.61	92.77	3.9
Junc N14	97.10	0.16	162.21	65.11	638.73	92.64	2.6
Junc N15	97.00	0.16	162.21	65.21	639.71	92.78	2.5
Junc N16	97.30	0.16	162.22	64.92	636.87	92.37	2.3
Junc N17	97.50	0.16	162.23	64.73	635.00	92.10	2.1
Junc N18	97.70	0.16	162.24	64.54	633.14	91.83	2.3

	Maximum Pressure
	Maximum Age

Pipe Report

Link ID	Length m	Diameter mm	Roughness	Flow LPS	Velocity m/s	Headloss m/km	Friction Factor
Pipe 1	47.0	200	110	-2.80	0.09	0.08	0.041
Pipe 1.1	1.0	200	110	2.80	0.09	0.09	0.046
Pipe 2	75.0	200	110	-3.12	0.10	0.10	0.041
Pipe 3	67.0	200	110	-3.44	0.11	0.12	0.040
Pipe 4	72.0	200	110	-3.60	0.11	0.13	0.040
Pipe 5	82.0	200	110	-3.76	0.12	0.14	0.040
Pipe 6	29.0	200	110	-4.00	0.13	0.16	0.039
Pipe 7	144.0	200	110	-4.00	0.13	0.16	0.039
Pipe 8	141.0	200	110	-4.00	0.13	0.16	0.039
Pipe 9	46.0	200	110	-4.00	0.13	0.16	0.039
Pipe 9.1	1.0	200	110	-4.00	0.13	0.15	0.036
Pipe 10	44.0	150	100	0.24	0.01	0.00	0.067
Pipe 11	36.0	150	100	0.08	0.00	0.00	0.074
Pipe 12	38.0	150	100	-0.08	0.00	0.00	0.070
Pipe 13	42.0	150	100	0.16	0.01	0.00	0.064
Pipe 14	38.0	150	100	-0.16	0.01	0.00	0.070
Pipe 15	38.0	150	100	-0.16	0.01	0.00	0.070
Pipe 16	38.0	150	100	-0.16	0.01	0.00	0.070
Pipe 17	50.0	150	100	0.16	0.01	0.00	0.080

Junction Report

Node ID	Elevation m	Demand LPS	Total Head m	Pressure m	Pressure kPa	Pressure psi
Resvr R1	155.70	-3.58	155.70	0.00	0.00	0.00
Resvr R2	155.70	-1.60	155.70	0.00	0.00	0.00
Junc N1	96.90	0.00	155.70	58.80	576.83	83.66
Junc N2	97.00	0.00	155.69	58.69	575.75	83.51
Junc N3	97.20	0.00	155.69	58.49	573.79	83.22
Junc N4	97.40	0.00	155.69	58.29	571.82	82.94
Junc N5	97.60	0.00	155.69	58.09	569.86	82.65
Junc N6	97.60	0.37	155.69	58.09	569.86	82.65
Junc N7	97.70	0.00	155.69	57.99	568.88	82.51
Junc N8	97.40	0.00	155.69	58.29	571.82	82.94
Junc N9	97.00	0.00	155.70	58.70	575.85	83.52
Junc N10	96.90	0.00	155.70	58.80	576.83	83.66
Junc N11	97.40	0.74	155.69	58.29	571.82	82.94
Junc N12	97.30	0.37	155.69	58.39	572.81	83.08
Junc N13	97.00	0.37	155.69	58.69	575.75	83.51
Junc N14	97.10	0.37	155.69	58.59	574.77	83.36
Junc N15	97.00	0.74	155.69	58.69	575.75	83.51

Pipe Report

Link ID	Length m	Diameter mm	Roughness	Flow LPS	Velocity m/s	Headloss m/km	Friction Factor
Pipe 1	47.0	200	110	3.58	0.11	0.13	0.040
Pipe 1.1	1.0	200	110	-3.58	0.11	0.14	0.042
Pipe 2	75.0	200	110	2.10	0.07	0.05	0.043
Pipe 3	67.0	200	110	0.99	0.03	0.01	0.048
Pipe 4	72.0	200	110	0.25	0.01	0.00	0.054
Pipe 5	82.0	200	110	-0.49	0.02	0.00	0.054
Pipe 6	29.0	200	110	-1.60	0.05	0.03	0.045
Pipe 7	144.0	200	110	-1.60	0.05	0.03	0.045
Pipe 8	141.0	200	110	-1.60	0.05	0.03	0.045
Pipe 9	46.0	200	110	-1.60	0.05	0.03	0.045
Pipe 9.1	1.0	200	110	-1.60	0.05	0.04	0.057
Pipe 10	44.0	150	100	1.11	0.06	0.07	0.055
Pipe 11	36.0	150	100	0.37	0.02	0.01	0.064
Pipe 12	38.0	150	100	-0.37	0.02	0.01	0.064
Pipe 13	42.0	150	100	0.37	0.02	0.01	0.064

Junction Report

Node ID	Elevation m	Demand LPS	Total Head m	Pressure m	Pressure kPa	Pressure psi
Resvr R1	150.50	-188.66	150.50	0.00	0.00	0.00
Resvr R2	150.50	-81.70	150.50	0.00	0.00	0.00
Junc N1	96.90	0.00	150.30	53.40	523.85	75.98
Junc N2	97.00	0.00	140.69	43.69	428.60	62.16
Junc N3	97.20	266.67	125.50	28.30	277.62	40.27
Junc N4	97.40	0.00	128.30	30.90	303.13	43.97
Junc N5	97.60	0.00	131.33	33.73	330.89	47.99
Junc N6	97.60	0.25	134.83	37.23	365.23	52.97
Junc N7	97.70	0.00	136.09	38.39	376.61	54.62
Junc N8	97.40	0.00	142.34	44.94	440.86	63.94
Junc N9	97.00	0.00	148.46	51.46	504.82	73.22
Junc N10	96.90	0.00	150.46	53.56	525.42	76.21
Junc N11	97.40	0.49	140.68	43.28	424.58	61.58
Junc N12	97.30	0.25	140.68	43.38	425.56	61.72
Junc N13	97.00	0.25	140.69	43.69	428.60	62.16
Junc N14	97.10	0.49	125.50	28.40	278.60	40.41
Junc N15	97.00	0.49	125.50	28.50	279.59	40.55
Junc N16	97.30	0.49	128.29	30.99	304.01	44.09
Junc N17	97.50	0.49	131.33	33.83	331.87	48.13
Junc N18	97.70	0.49	134.83	37.13	364.25	52.83

	Minimum Pressure
	Applied Fire Flow

Pipe Report

Link ID	Length m	Diameter mm	Roughness	Flow LPS	Velocity m/s	Headloss m/km	Friction Factor
Pipe 1	47.0	200	110	188.66	6.01	204.46	0.022
Pipe 1.1	1.0	200	110	-188.66	6.01	204.47	0.022
Pipe 2	75.0	200	110	187.67	5.97	202.48	0.022
Pipe 3	67.0	200	110	-79.98	2.55	41.72	0.025
Pipe 4	72.0	200	110	-80.47	2.56	42.20	0.025
Pipe 5	82.0	200	110	-80.96	2.58	42.67	0.025
Pipe 6	29.0	200	110	-81.70	2.60	43.40	0.025
Pipe 7	144.0	200	110	-81.70	2.60	43.40	0.025
Pipe 8	141.0	200	110	-81.70	2.60	43.40	0.025
Pipe 9	46.0	200	110	-81.70	2.60	43.40	0.025
Pipe 9.1	1.0	200	110	-81.70	2.60	43.40	0.025
Pipe 10	44.0	150	100	0.74	0.04	0.03	0.058
Pipe 11	36.0	150	100	0.25	0.01	0.00	0.068
Pipe 12	38.0	150	100	-0.25	0.01	0.00	0.068
Pipe 13	42.0	150	100	0.49	0.03	0.02	0.061
Pipe 14	38.0	150	100	-0.49	0.03	0.02	0.061
Pipe 15	38.0	150	100	-0.49	0.03	0.02	0.062
Pipe 16	38.0	150	100	-0.49	0.03	0.02	0.062

Junction Report

Node ID	Elevation m	Demand LPS	Total Head m	Pressure m	Pressure kPa	Pressure psi
Resvr R1	150.50	-170.93	150.50	0.00	0.00	0.00
Resvr R2	150.50	-99.43	150.50	0.00	0.00	0.00
Junc N1	96.90	0.00	150.33	53.43	524.15	76.02
Junc N2	97.00	0.00	142.32	45.32	444.59	64.48
Junc N3	97.20	0.00	129.69	32.49	318.73	46.23
Junc N4	97.40	266.67	118.52	21.12	207.19	30.05
Junc N5	97.60	0.00	122.91	25.31	248.29	36.01
Junc N6	97.60	0.25	127.96	30.36	297.83	43.20
Junc N7	97.70	0.00	129.77	32.07	314.61	45.63
Junc N8	97.40	0.00	138.76	41.36	405.74	58.85
Junc N9	97.00	0.00	147.57	50.57	496.09	71.95
Junc N10	96.90	0.00	150.44	53.54	525.23	76.18
Junc N11	97.40	0.49	142.32	44.92	440.67	63.91
Junc N12	97.30	0.25	142.32	45.02	441.65	64.06
Junc N13	97.00	0.25	142.32	45.32	444.59	64.48
Junc N14	97.10	0.49	129.69	32.59	319.71	46.37
Junc N15	97.00	0.49	129.69	32.69	320.69	46.51
Junc N16	97.30	0.49	118.52	21.22	208.17	30.19
Junc N17	97.50	0.49	122.91	25.41	249.27	36.15
Junc N18	97.70	0.49	127.96	30.26	296.85	43.05

	Minimum Pressure
	Applied Fire Flow

Pipe Report

Link ID	Length m	Diameter mm	Roughness	Flow LPS	Velocity m/s	Headloss m/km	Friction Factor
Pipe 1	47.0	200	110	170.93	5.44	170.32	0.023
Pipe 1.1	1.0	200	110	-170.93	5.44	170.32	0.023
Pipe 2	75.0	200	110	169.94	5.41	168.49	0.023
Pipe 3	67.0	200	110	168.96	5.38	166.70	0.023
Pipe 4	72.0	200	110	-98.20	3.13	61.01	0.025
Pipe 5	82.0	200	110	-98.69	3.14	61.58	0.024
Pipe 6	29.0	200	110	-99.43	3.16	62.43	0.024
Pipe 7	144.0	200	110	-99.43	3.16	62.43	0.024
Pipe 8	141.0	200	110	-99.43	3.16	62.43	0.024
Pipe 9	46.0	200	110	-99.43	3.16	62.43	0.024
Pipe 9.1	1.0	200	110	-99.43	3.16	62.44	0.024
Pipe 10	44.0	150	100	0.74	0.04	0.03	0.058
Pipe 11	36.0	150	100	0.25	0.01	0.00	0.068
Pipe 12	38.0	150	100	-0.25	0.01	0.00	0.068
Pipe 13	42.0	150	100	0.49	0.03	0.02	0.062
Pipe 14	38.0	150	100	-0.49	0.03	0.02	0.062
Pipe 15	38.0	150	100	-0.49	0.03	0.02	0.062
Pipe 16	38.0	150	100	-0.49	0.03	0.02	0.062

Junction Report

Node ID	Elevation m	Demand LPS	Total Head m	Pressure m	Pressure kPa	Pressure psi
Resvr R1	150.50	-154.77	150.50	0.00	0.00	0.00
Resvr R2	150.50	-115.59	150.50	0.00	0.00	0.00
Junc N1	96.90	0.00	150.36	53.46	524.44	76.06
Junc N2	97.00	0.00	143.70	46.70	458.13	66.45
Junc N3	97.20	0.00	133.20	36.00	353.16	51.22
Junc N4	97.40	0.00	123.93	26.53	260.26	37.75
Junc N5	97.60	266.67	114.02	16.42	161.08	23.36
Junc N6	97.60	0.25	120.71	23.11	226.71	32.88
Junc N7	97.70	0.00	123.10	25.40	249.17	36.14
Junc N8	97.40	0.00	134.99	37.59	368.76	53.48
Junc N9	97.00	0.00	146.62	49.62	486.77	70.60
Junc N10	96.90	0.00	150.42	53.52	525.03	76.15
Junc N11	97.40	0.49	143.70	46.30	454.20	65.88
Junc N12	97.30	0.25	143.70	46.40	455.18	66.02
Junc N13	97.00	0.25	143.70	46.70	458.13	66.45
Junc N14	97.10	0.49	133.20	36.10	354.14	51.36
Junc N15	97.00	0.49	133.20	36.20	355.12	51.51
Junc N16	97.30	0.49	123.93	26.63	261.24	37.89
Junc N17	97.50	0.49	114.02	16.52	162.06	23.50
Junc N18	97.70	0.49	120.71	23.01	225.73	32.74

	Minimum Pressure
	Applied Fire Flow

Pipe Report

Link ID	Length m	Diameter mm	Roughness	Flow LPS	Velocity m/s	Headloss m/km	Friction Factor
Pipe 1	47.0	200	110	154.77	4.93	141.70	0.023
Pipe 1.1	1.0	200	110	-154.77	4.93	141.70	0.023
Pipe 2	75.0	200	110	153.78	4.89	140.02	0.023
Pipe 3	67.0	200	110	152.80	4.86	138.37	0.023
Pipe 4	72.0	200	110	152.31	4.85	137.55	0.023
Pipe 5	82.0	200	110	-114.85	3.66	81.55	0.024
Pipe 6	29.0	200	110	-115.59	3.68	82.52	0.024
Pipe 7	144.0	200	110	-115.59	3.68	82.52	0.024
Pipe 8	141.0	200	110	-115.59	3.68	82.52	0.024
Pipe 9	46.0	200	110	-115.59	3.68	82.52	0.024
Pipe 9.1	1.0	200	110	-115.59	3.68	82.53	0.024
Pipe 10	44.0	150	100	0.74	0.04	0.03	0.058
Pipe 11	36.0	150	100	0.25	0.01	0.00	0.068
Pipe 12	38.0	150	100	-0.25	0.01	0.00	0.068
Pipe 13	42.0	150	100	0.49	0.03	0.02	0.062
Pipe 14	38.0	150	100	-0.49	0.03	0.02	0.062
Pipe 15	38.0	150	100	-0.49	0.03	0.02	0.061
Pipe 16	38.0	150	100	-0.49	0.03	0.02	0.062

Junction Report

Node ID	Elevation m	Demand LPS	Total Head m	Pressure m	Pressure kPa	Pressure psi
Resvr R1	150.50	-137.84	150.50	0.00	0.00	0.00
Resvr R2	150.50	-132.52	150.50	0.00	0.00	0.00
Junc N1	96.90	0.00	150.39	53.49	524.74	76.11
Junc N2	97.00	0.00	145.01	48.01	470.98	68.31
Junc N3	97.20	0.00	136.55	39.35	386.02	55.99
Junc N4	97.40	0.00	129.09	31.69	310.88	45.09
Junc N5	97.60	0.00	121.13	23.53	230.83	33.48
Junc N6	97.60	266.92	112.12	14.52	142.44	20.66
Junc N7	97.70	0.00	115.21	17.51	171.77	24.91
Junc N8	97.40	0.00	130.52	33.12	324.91	47.12
Junc N9	97.00	0.00	145.50	48.50	475.79	69.01
Junc N10	96.90	0.00	150.39	53.49	524.74	76.11
Junc N11	97.40	0.49	145.01	47.61	467.05	67.74
Junc N12	97.30	0.25	145.01	47.71	468.04	67.88
Junc N13	97.00	0.25	145.01	48.01	470.98	68.31
Junc N14	97.10	0.49	136.55	39.45	387.00	56.13
Junc N15	97.00	0.49	136.55	39.55	387.99	56.27
Junc N16	97.30	0.49	129.09	31.79	311.86	45.23
Junc N17	97.50	0.49	121.13	23.63	231.81	33.62
Junc N18	97.70	0.49	112.12	14.42	141.46	20.52

	Minimum Pressure
	Applied Fire Flow

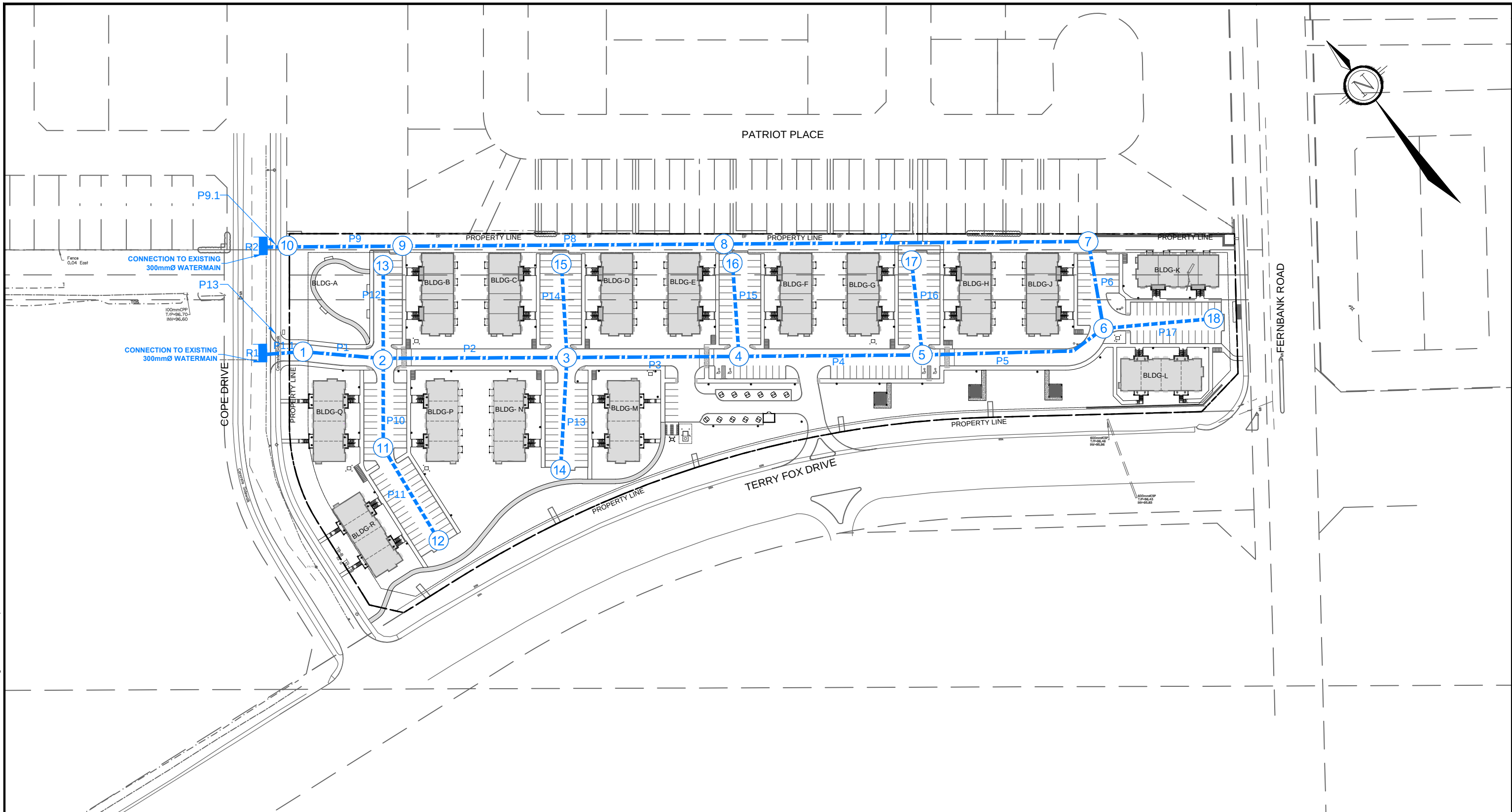
Pipe Report

Link ID	Length m	Diameter mm	Roughness	Flow LPS	Velocity m/s	Headloss m/km	Friction Factor
Pipe 1	47.0	200	110	137.84	4.39	114.33	0.023
Pipe 1.1	1.0	200	110	-137.84	4.39	114.33	0.023
Pipe 2	75.0	200	110	136.85	4.36	112.81	0.023
Pipe 3	67.0	200	110	135.87	4.32	111.32	0.023
Pipe 4	72.0	200	110	135.38	4.31	110.58	0.023
Pipe 5	82.0	200	110	134.89	4.29	109.84	0.023
Pipe 6	29.0	200	110	-132.52	4.22	106.30	0.023
Pipe 7	144.0	200	110	-132.52	4.22	106.30	0.023
Pipe 8	141.0	200	110	-132.52	4.22	106.30	0.023
Pipe 9	46.0	200	110	-132.52	4.22	106.30	0.023
Pipe 9.1	1.0	200	110	-132.52	4.22	106.31	0.023
Pipe 10	44.0	150	100	0.74	0.04	0.03	0.058
Pipe 11	36.0	150	100	0.25	0.01	0.00	0.068
Pipe 12	38.0	150	100	-0.25	0.01	0.00	0.068
Pipe 13	42.0	150	100	0.49	0.03	0.02	0.061
Pipe 14	38.0	150	100	-0.49	0.03	0.02	0.062
Pipe 15	38.0	150	100	-0.49	0.03	0.02	0.062
Pipe 16	38.0	150	100	-0.49	0.03	0.02	0.062

Maximum day plus fire flow demand was modeled for each of the following nodes.
The following is a summary of the minimum pressures that occurred for each operating condition.

	Demand (L/s)						
Fire at Junction	Maximum Daily	Fire Flow	Max Day + Fire	Minimum Pressure			
				(m)	kPa	psi	Node
Ultimate Condition							
N3	3.68	266.67	270.35	28.30	277.62	40.27	N3
N4	3.68	266.67	270.35	21.12	207.19	30.05	N4
N5	3.68	266.67	270.35	16.42	161.08	23.36	N5
N6	3.68	266.67	270.35	14.42	141.46	20.52	N18

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LEGEND

- SITE BOUNDARY
- PROPOSED 200mm WATERMAIN
- PROPOSED 100mm WATERMAIN
- PROPOSED NODE AND ID NUMBER
- EXISTING RESERVOIR AND ID NUMBER

NOVATECH

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CITY OF OTTAWA
5331 FERNBANK ROAD
IRON VALLEY 2

PROPOSED WATER NETWORK PLAN

SCALE 1 : 1500

DATE JUN 2026 JOB 121011 FIGURE FIG-6

CUT11V17 DWG 270mm X 122mm

Boundary Conditions 5331 Fernbank Road

Provided Information

Scenario	Demand	
	L/min	L/s
Average Daily Demand	79	1.31
Maximum Daily Demand	236	3.93
Peak Hour	353	5.89
Fire Flow Demand #1	12,000	200.00
Fire Flow Demand #2	13,000	216.67
Fire Flow Demand #3	16,000	266.67

Location



Results

Connection 1 – Cope Drive West

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	162.2	93.0
Peak Hour	155.7	83.6
Max Day plus Fire Flow #1	153.2	80.1
Max Day plus Fire Flow #2	152.6	79.2
Max Day plus Fire Flow #3	150.5	76.3

¹ Ground Elevation = 96.9 m

Connection 2 – Cope Drive East

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	162.3	93.1
Peak Hour	155.7	83.6
Max Day plus Fire Flow #1	153.2	80.2
Max Day plus Fire Flow #2	152.6	79.3
Max Day plus Fire Flow #3	150.5	76.4

¹ Ground Elevation = 96.8 m

Notes

1. The IWSD has recently updated their water modelling software. Any significant difference between previously received BC results and newly received BC results could be attributed to this update.
2. As per the Ontario Building Code in areas that may be occupied, the static pressure at any fixture shall not exceed 552 kPa (80 psi.) Pressure control measures to be considered are as follows, in order of preference:
 - a. If possible, systems to be designed to residual pressures of 345 to 552 kPa (50 to 80 psi) in all occupied areas outside of the public right-of-way without special pressure control equipment.
 - b. Pressure reducing valves to be installed immediately downstream of the isolation valve in the home/ building, located downstream of the meter so it is owner maintained.

Disclaimer

The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation. Fire Flow analysis is a reflection of available flow in the watermain; there may be additional restrictions that occur between the watermain and the hydrant that the model cannot take into account.

5331 Fernbank Road - Iron Valley Phase 2
Water Demand

	Number of Units	Design Population	Average Day Demand (L/s)	Maximum Day Demand (L/s)	Peak Hour Demand (L/s)
Multi-Unit Apartment Blocks	192	404	1.31	3.93	5.89
Total	192	404	1.31	3.93	5.89

Water Demand Parameters

Multi-Unit Apartment Blocks	2.1	persons/unit
Residential Demand	280.0	L/c/day
Residential Maximum Daily Demand	3.0	x Avg Day
Residential Hour Demand	4.5	x Avg Day

Fireflow Demand 1 (FF1) - Max Fire Flow **267** L/s

Fireflow Demand 2 (FF2) **217** L/s

Fireflow Demand 3 (FF3) **200** L/s

Notes:

- 1) Water demand based on MOE Design Guidelines for Drinking Water Systems 2008 (< 500 population)
- 2) Fireflows calculated as per 2020 Fire Underwriter's Survey Guidelines.

FUS - Fire Flow Calculations

Novatech Project #: 121011
Project Name: 5331 Fernbank Road - Iron Valley Phase 2
Date: 9/5/2025
Input By: Billy McEwen
Reviewed By: Drew Blair
Drawing Reference: 121011-Figure-BC1

Legend: Input by User

No Input Required

Reference: Fire Underwriter's Survey Guideline (2020)
Formula Method

Building Description: Multi-Unit Apartment Blocks
Type V - Wood frame

Step			Choose		Value Used	Total Fire Flow (L/min)
Base Fire Flow						
1	Construction Material			Multiplier		1.5
	Coefficient related to type of construction C	Type V - Wood frame	Yes	1.5	1.5	
		Type IV - Mass Timber		Varies		
		Type III - Ordinary construction		1		
		Type II - Non-combustible construction		0.8		
		Type I - Fire resistive construction (2 hrs)		0.6		
2	Floor Area					12,000
	A	Building Footprint (m ²)	425	1,275		
		Number of Floors/Storeys	3			
		Protected Openings (1 hr) if C<1.0	No			
		Area of structure considered (m ²)				
	F	Base fire flow without reductions				
F = 220 C (A)^{0.5}						
Reductions or Surcharges						
3	Occupancy hazard reduction or surcharge		FUS Table 3	Reduction/Surcharge		10,200
	(1)	Non-combustible		-25%	-15%	
		Limited combustible	Yes	-15%		
		Combustible		0%		
		Free burning		15%		
		Rapid burning		25%		
4	Sprinkler Reduction		FUS Table 4	Reduction		0
	(2)	Adequately Designed System (NFPA 13)	No	-30%	0%	
		Standard Water Supply	No	-10%		
		Fully Supervised System	No	-10%		
		Cumulative Sub-Total		0%		
		Area of Sprinklered Coverage (m²)		0		
Cumulative Total		0%				
5	Exposure Surcharge		FUS Table 5	Surcharge		6,120
	(3)	North Side	3.1 - 10 m	15%	20%	
		East Side	20.1 - 30 m		10%	
		South Side	10.1 - 20 m		15%	
		West Side	10.1 - 20 m		15%	
		Cumulative Total			60%	
Results						
6	(1) + (2) + (3)	Total Required Fire Flow, rounded to nearest 1000L/min			L/min	16,000
		(2,000 L/min < Fire Flow < 45,000 L/min)		or	L/s	267
				or	USGPM	4,227

FUS - Fire Flow Calculations

Novatech Project #: 121011
Project Name: 5331 Fernbank Road - Iron Valley Phase 2
Date: 9/5/2025
Input By: Billy McEwen
Reviewed By: Drew Blair
Drawing Reference: 121011-Figure-BC1

Legend: Input by User

No Input Required

Reference: Fire Underwriter's Survey Guideline (2020)
Formula Method

Building Description: Multi-Unit Apartment Blocks
Type V - Wood frame

Step			Choose		Value Used	Total Fire Flow (L/min)
Base Fire Flow						
1	Construction Material			Multiplier		1.5
	Coefficient related to type of construction C	Type V - Wood frame	Yes	1.5	1.5	
		Type IV - Mass Timber		Varies		
		Type III - Ordinary construction		1		
		Type II - Non-combustible construction		0.8		
		Type I - Fire resistive construction (2 hrs)		0.6		
2	Floor Area					12,000
	A	Building Footprint (m ²)	425	1,275		
		Number of Floors/Storeys	3			
		Protected Openings (1 hr) if C<1.0	No			
		Area of structure considered (m ²)				
	F	Base fire flow without reductions				
F = 220 C (A)^{0.5}						
Reductions or Surcharges						
3	Occupancy hazard reduction or surcharge			FUS Table 3	Reduction/Surcharge	10,200
	(1)	Non-combustible		-25%	-15%	
		Limited combustible	Yes	-15%		
		Combustible		0%		
		Free burning		15%		
		Rapid burning		25%		
4	Sprinkler Reduction			FUS Table 4	Reduction	0
	(2)	Adequately Designed System (NFPA 13)	No	-30%		
		Standard Water Supply	No	-10%		
		Fully Supervised System	No	-10%		
		Cumulative Sub-Total		0%		
		Area of Sprinklered Coverage (m²)	0	0%		
Cumulative Total		0%				
5	Exposure Surcharge			FUS Table 5	Surcharge	2,550
	(3)	North Side	10.1 - 20 m	25%		
		East Side	20.1 - 30 m			
		South Side	>30m			
		West Side	>30m			
		Cumulative Total			25%	
Results						
6	(1) + (2) + (3)	Total Required Fire Flow, rounded to nearest 1000L/min			L/min	13,000
		(2,000 L/min < Fire Flow < 45,000 L/min)		or	L/s	217
				or	USGPM	3,435

FUS - Fire Flow Calculations

Novatech Project #: 121011
Project Name: 5331 Fernbank Road - Iron Valley Phase 2
Date: 9/5/2025
Input By: Billy McEwen
Reviewed By: Drew Blair
Drawing Reference: 121011-Figure-BC1

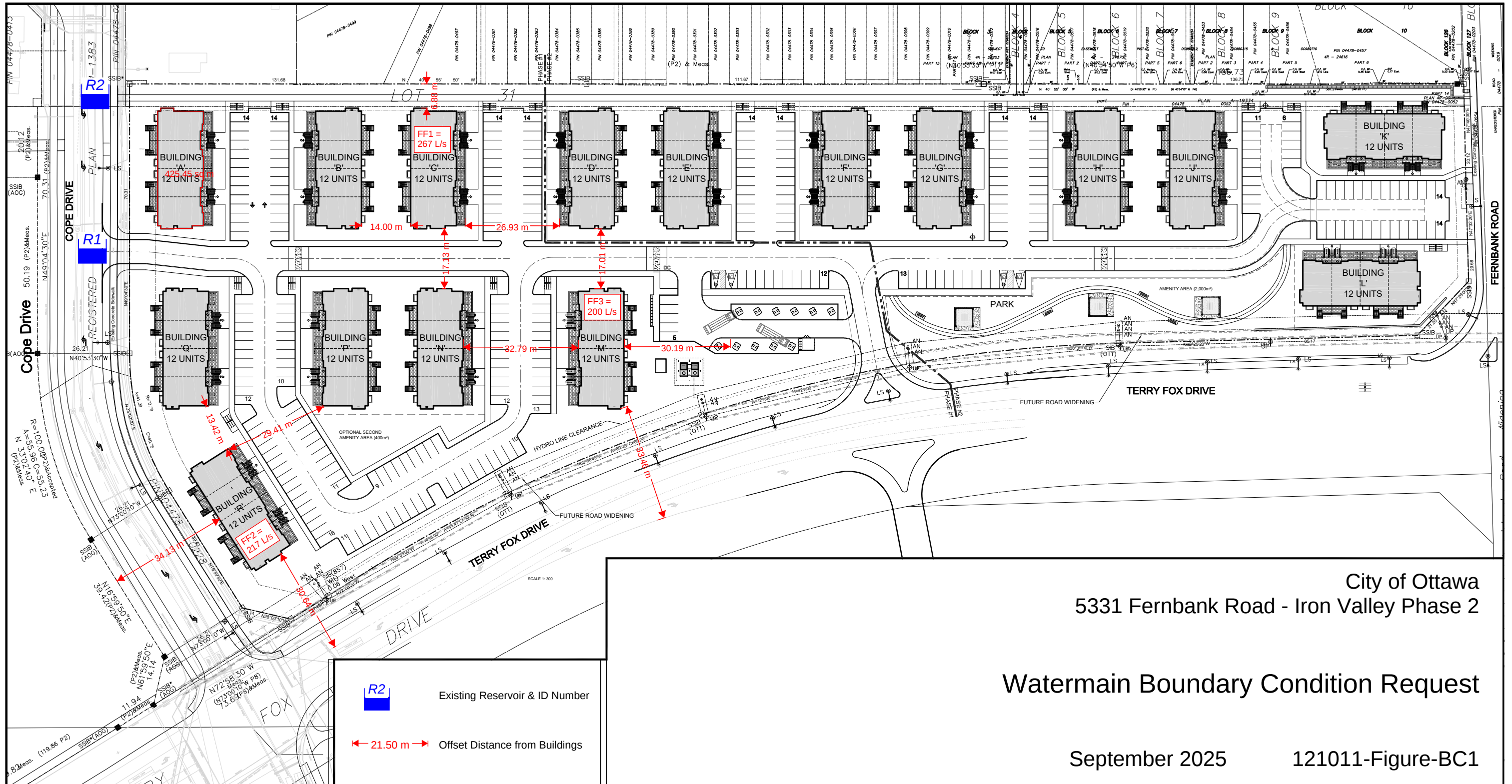
Legend: Input by User

No Input Required

Reference: Fire Underwriter's Survey Guideline (2020)
Formula Method

Building Description: Multi-Unit Apartment Blocks
Type V - Wood frame

Step			Choose		Value Used	Total Fire Flow (L/min)
Base Fire Flow						
1	Construction Material			Multiplier		1.5
	Coefficient related to type of construction C	Type V - Wood frame	Yes	1.5	1.5	
		Type IV - Mass Timber		Varies		
		Type III - Ordinary construction		1		
		Type II - Non-combustible construction		0.8		
		Type I - Fire resistive construction (2 hrs)		0.6		
2	Floor Area					12,000
	A	Building Footprint (m ²)	425	1,275		
		Number of Floors/Storeys	3			
		Protected Openings (1 hr) if C<1.0	No			
		Area of structure considered (m ²)				
	F	Base fire flow without reductions				
F = 220 C (A)^{0.5}						
Reductions or Surcharges						
3	Occupancy hazard reduction or surcharge			FUS Table 3	Reduction/Surcharge	10,200
	(1)	Non-combustible		-25%	-15%	
		Limited combustible	Yes	-15%		
		Combustible		0%		
		Free burning		15%		
		Rapid burning		25%		
4	Sprinkler Reduction			FUS Table 4	Reduction	0
	(2)	Adequately Designed System (NFPA 13)	No	-30%	0%	
		Standard Water Supply	No	-10%		
		Fully Supervised System	No	-10%		
		Cumulative Sub-Total		0%		
		Area of Sprinklered Coverage (m²)	0	0%		
Cumulative Total		0%				
5	Exposure Surcharge			FUS Table 5	Surcharge	1,530
	(3)	North Side	10.1 - 20 m	0%	15%	
		East Side	>30m		0%	
		South Side	>30m		0%	
		West Side	>30m		0%	
		Cumulative Total			15%	
Results						
6	(1) + (2) + (3)	Total Required Fire Flow, rounded to nearest 1000L/min			L/min	12,000
		(2,000 L/min < Fire Flow < 45,000 L/min)		or	L/s	200
				or	USGPM	3,170



Appendix D
EROSION AND SEDIMENT CONTROL

EROSION AND SEDIMENT CONTROL PLAN, MONITORING, AND MEASURES

Scope of Work

The work under the applicable items includes the preparation, implementation and monitoring of an Erosion and Sediment Control Plan to prevent sediment-laden runoff resulting from the Contractor's construction operations from entering all sewers and watercourses both within and downstream from the Working Area. The plan shall include management and monitoring of water discharged from dewatering operations. The specification is limited to the management of sediment laden water and the management of contaminants such as hydrocarbons and volatile organic compounds present within groundwater at the site shall be managed as described elsewhere in the contract documents.

General

The Contractor acknowledges that surface erosion and sediment runoff resulting from construction operations has potential to cause a detrimental impact to any downstream watercourse, and that all construction operations that may impact upon water quality shall be carried out in a manner that strictly meets the requirements of all applicable legislation and regulations.

Accordingly, the Contractor shall be responsible for determining and conforming to the requirements of the Ontario Ministry of the Environment (MOE), the Ontario Ministry of Natural Resources, the City of Ottawa, applicable Conservation Authorities and any other Governmental Regulatory Agencies (collectively "Regulatory Agencies") having jurisdiction in the Working Area or over any potentially affected watercourses.

Erosion and Sediment Control Plan

Before commencing the Work, the Contractor shall submit to the Contract Administrator six copies of a detailed Erosion and Sediment Control Plan. The ESC Plan will consist of a written description and detailed drawings indicating the on-site activities and measures to be used to control erosion and sediment movement for each step of the Work. The written description shall be signed by, and the drawings shall bear the stamp and signature of a qualified Professional Engineer licensed in Ontario, herein designated as the Engineer of Record (EOR).

The Contractor acknowledges that the scheduling of the implementation of erosion and sediment controls is the key component for successful sediment control. Accordingly, the ESC Plan will contain a detailed schedule which identifies the following:

- Phasing of the steps for the installation of all control measures.
- Inspection, monitoring and maintenance of all control measures during construction.

EROSION AND SEDIMENT CONTROL PLAN, MONITORING, AND MEASURES

- Phasing of the removal and disposal of the control measures.

The Contractor acknowledges that no one measure is likely to be 100% effective for erosion protection and controlling sediment runoff and water discharges from the site. Therefore, where necessary the ESC Plan will implement sequential measures arranged in such a manner so as to mitigate sediment release from construction operations and achieve specific maximum permitted criteria where applicable. Suggested on-site measures may include, but shall not be limited to, the following methods: sediment ponds, filter bags, pump filters, settling tanks, silt fences, straw bales, filter cloths, check dams and/or berms, or other recognized technologies and methods available at the time of construction. Specific measures shall be installed in accordance with the requirements of OPSS 805 where appropriate, or in accordance with manufacturer's recommendations.

Inspection and Monitoring of Mitigation Measures

The Contractor shall be solely responsible for inspecting, monitoring and maintaining the effectiveness of the ESC Plan upon implementation. The Contractor shall submit to the Contract Administrator weekly inspection reports demonstrating the performance of the installed measures, identifying deficiencies and indentifying required maintenance issues. These reports shall be prepared, signed by the EOR and provided to the Contract Administrator within 48 hours of the inspection.

- Maintenance issues are defined as any measure which is not functioning to the satisfaction of the EOR and in the opinion of the EOR may be repaired by the contractor with subsequent re-inspection at the next scheduled EOR site inspection.
- Deficiencies are defined as any measure or lack of measure which has potential to cause an adverse environmental impact at the site given the current/forecasted conditions and schedule of the work.

Maintenance issues which have previously been identified but not adequately corrected shall be considered deficiencies.

Deficiencies shall be immediately corrected. Corrective actions shall be re-inspected and documented by the EOR. Re-inspection reports shall be specific to the deficiency observed and may be written field reports.

EOR monitoring reports submitted shall include:

- The date and time of the inspection and monitoring.
- General description of the mitigating measures being utilized at the site.
- Confirmation as to the effectiveness of the measures inspected.

EROSION AND SEDIMENT CONTROL PLAN, MONITORING, AND MEASURES

- Description of any maintenance issue which requires minor repair, improvement or maintenance.
- Description of any deficiency observed including timeline for correction and re-inspection.
- Deficiency re-inspection reports outstanding for the site.

The Contractor shall notify the Contract Administrator in all situations where a regulatory agency has identified deficiencies in erosion/sediment control measures, quality of runoff or quality of water quality discharged from dewatering operation.

Where in the opinion of the Contract Administrator either the proof of performance submitted is or the measures implemented are considered inadequate, the Contractor shall have the EOR review measures in the presence of the Contract Administrator within 24 hours of being notified in writing.

The Contractor shall monitor all weather forecasts and schedule the Work in order to minimize the risk of sediment-laden water from entering any watercourse or sewer system. The ESC Plan shall contain a Contingency Plan to include the provision of additional labour, equipment or materials to install additional control measures, and detail an emergency response plan in case of an accidental event. As such, the Contractor shall have additional control materials on site at all times which are easily accessible and may be implemented at a moment's notice.

Contractor's Responsibilities

The Contractor shall ensure that all workers, including sub-contractors, in the Working Area are aware of the importance of the erosion and sediment control measures and informed of the consequences of the failure to comply with the requirements of all Regulatory Agencies and the specifications detailed herein.

The Contractor shall periodically, and when requested by the Contract Administrator or EOR, clean out accumulated sediment deposits as required at the sediment control devices, including those deposits that may originate from outside the construction area. Accumulated sediment shall be removed in such a manner that prevents the deposition of this material into any sewer or watercourse and avoids damage to the control measure. The sediment shall be removed from the site at the Contractor's expense and managed in compliance with the requirements for excess earth material, as specified elsewhere in the Contract.

The Contractor shall immediately report to applicable regulatory agencies and the Contract Administrator any accidental discharges of sediment material into either the watercourse or the storm sewer system. Failure to report will constitute a breach of this specification and the Contractor may also be subject to the penalties imposed by any

EROSION AND SEDIMENT CONTROL PLAN, MONITORING, AND MEASURES

applicable Regulatory Agency. Appropriate response measures, including any repairs to existing control measures or the implementation of additional control measures, shall be carried out by the Contractor without delay.

The sediment control measures shall be removed when, in the opinion of the EOR, the measure(s) is no longer required. No control measure may be permanently removed without prior written authorization from the EOR. All sediment and erosion control measures shall be removed in a manner that avoids the entry of sediment or debris into any sewer or watercourse within or downstream of the Working Area. All accumulated sediment shall be removed from the Working Area at the Contractor's expense and managed in compliance with the requirements for excess earth material, as specified elsewhere in the Contract. Any seeding and mulching, temporary cover, sodding or original turf cover that is disturbed by the removal of the control measures and accumulated sediment, shall be brought to final grade and restored. Payment for the supply and placing of ground cover at these locations shall be made under the applicable items listed elsewhere in the Contract.

Where, in the opinion of either the Contract Administrator or a Regulatory Agency, any of the terms specified herein have either not been complied with or not performed in a suitable manner, the Contract Administrator or Regulatory Agency has the right to immediately withdraw its permission to continue the work but may renew its permission upon being satisfied that the defaults and/or deficiencies in the performance of this specification by the Contractor have been remedied. No compensation will be made to the Contractor for the withdrawal of permission to do the work resulting from non-compliance with the requirements of this specification and the Regulatory Agencies.

In addition to any other remedy and/or penalty provided by law, where there has been default or non-compliance with any of the terms specified herein and the Contractor refuses to perform or rectify same within forty-eight (48) hours of the receipt of the written demand of the Contract Administrator to do so, the Owner is hereby entitled to enter upon the Working Area and either complete the work in conformity with the Contract or have the work done that it considers necessary to complete the Work to its intended condition, whichever, in the Owner's sole opinion, is the most reasonable course of action. The Contractor and the Owner further agree that the costs incurred for any such work shall be retained by the Owner from monies otherwise due to the Contractor.

Monitoring of Water Quality Impacts and Point Source Discharges

The Contractor shall monitor runoff quality and quantity of water discharged from dewatering operations. The work shall include turbidity monitoring of impacts to watercourses (upstream vs downstream conditions), total suspended solids (TSS) monitoring of point sources such as those from dewatering operations. Discharge shall be in accordance with site specific constraints, regulatory requirements and sewer use bylaw

EROSION AND SEDIMENT CONTROL PLAN, MONITORING, AND MEASURES

requirements. Where no specific criteria has otherwise been identified, the contractor shall meet the following discharge objective.

Source	Objective	Monitoring Frequency (min)
Watercourse Impacts	Downstream turbidity not to exceed upstream levels by greater than 25%	Minimum of daily for first three days of operation Minimum of twice weekly on an ongoing basis Daily for situations where the work is being conducted within 20 metres of a watercourse.
Discharge from Dewatering Operations	TSS maximum level of 25 mg/L	Minimum of daily for first three days of operation Minimum of twice weekly on an ongoing basis

Monitoring frequency to increase where scheduled construction operations have potential to impair water quality.

Mitigation and Action by Contractor Where Monitoring Indicates Water Impacts or Discharges Over Criteria or Objectives

Where site specific criteria or objectives are not attained, the Contractor and/or EOR shall immediately notify applicable regulatory agency of the monitoring results and possible impacts to sewers and watercourses. The Contractor shall implement an Action/Mitigation Plan acceptable to the EOR and applicable regulatory agency prior to continuing or resuming construction activities.

Measurement and Basis of Payment

Item – Erosion and Sediment Control Plan and Monitoring

Payment at the Contract price for the item “Erosion and Sediment Control Plan and Monitoring” shall be full compensation for the preparation and monitoring of the Erosion and Sediment Control Plan.

Payment shall be based upon the following schedule:

- a) 25% upon satisfactory submission and implementation of the ESC Plan; and,
- b) 75% pro-rated into equal payments over the term of the contract.

EROSION AND SEDIMENT CONTROL PLAN, MONITORING, AND MEASURES

This payment schedule may only be modified as agreed upon in writing between the Contractor and the Contract Administrator.

Item – Erosion and Sediment Control Measures

Payment at the Contract price for the item “Erosion and Sediment Control Measures” shall be full compensation for the implementation and maintenance of erosion and sediment control measures required for the site, and shall include all labour, equipment and materials to supply, construct, monitor and maintain all erosion and sediment control measures detailed therein.

Payment shall be based upon the following schedule:

- a) 20% upon satisfactory installation of the control measures;
- b) 70% pro-rated into equal payments over the term of the contract; and,
- c) 10% upon successful completion and removal of the ESC Plan protection measures.

This payment schedule may only be modified as agreed upon in writing between the Contractor and the Contract Administrator.

Warrant: For work which is conducted in close proximity to watercourses or environmentally sensitive areas.

Appendix E
CORRESPONDENCE

Drew Blair

From: Mike Petepiece
Sent: Friday, May 7, 2021 2:00 PM
To: Marc St.Pierre; Drew Blair
Subject: FW: SOHO Phase 1 - Monahan Drain

Hi Drew/MSP,

I met with Jonathon Burnett at JFSA this morning and he confirmed that the latest modeling for our area has a minor system inlet rate of 85 L/s/ha (316 L/s divided by 3.73 ha).

See email below.

Michael Petepiece, P.Eng., Senior Project Manager | Water Resources

NOVATECH Engineers, Planners & Landscape Architects

240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 Ext: 235 | Cell: 613.299.4677 | Fax: 613.254.5867

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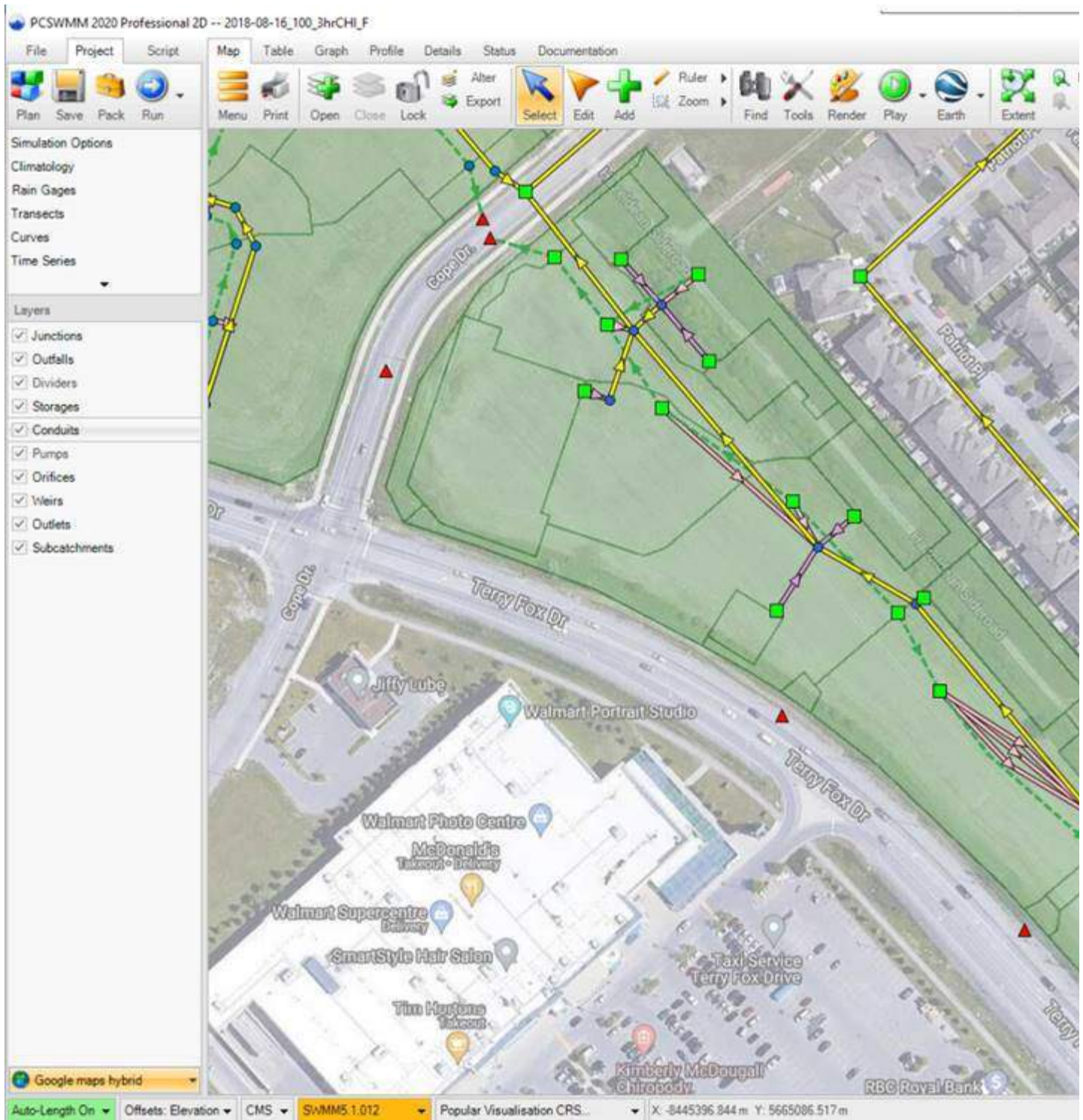
From: Jonathon Burnett <jburnett@jfsa.com>
Sent: Friday, May 7, 2021 1:04 PM
To: Mike Petepiece <m.petepiece@novatech-eng.com>
Subject: SOHO Phase 1 - Monahan Drain

Hi Mike,

Looking over the Stantec model we have on file, I can confirm that the peak 100-Year minor system flow is 316 L/s (from memory I think the report you showed me today said 317 L/s).

Although I was not able to replicate the major system overflow as the model has many overflow locations.

Below is a screenshot from the model; it appears that Stantec did model these lands in reasonably high detail in the past.



Regards,
Jono Burnett, B.Eng., P.Eng
 Water Resources Engineer



52 Springbrook Drive, Ottawa ON, K2S 1B9
 Tel.: 613-322-1253 | Email: jburnett@jfsa.com | Website: www.jfsa.com
 Ottawa-Paris(ON)-Gatineau-Montréal-Québec

Drew Blair

From: Kuruvilla, Santhosh <Santhosh.Kuruvilla@ottawa.ca>
Sent: Wednesday, May 12, 2021 9:50 AM
To: Drew Blair
Cc: Marc St.Pierre
Subject: RE: Pre-Consultation Follow-Up: 5331 Fernbank

Hi Drew,

Please go ahead and use the JFSA figure.

Thanks,

From: Kuruvilla, Santhosh
Sent: May 11, 2021 2:44 PM
To: Drew Blair <D.Blair@novatech-eng.com>
Cc: Marc St.Pierre <m.stpierre@novatech-eng.com>
Subject: RE: Pre-Consultation Follow-Up: 5331 Fernbank

Hi Drew,

Thanks for your quick response.

I will check with my colleague who gave me the quantity control criteria for this site (70L/S/Ha) and get back to you.

Thanks,

Santhosh

From: Drew Blair <D.Blair@novatech-eng.com>
Sent: May 11, 2021 2:14 PM
To: Kuruvilla, Santhosh <Santhosh.Kuruvilla@ottawa.ca>
Cc: Marc St.Pierre <m.stpierre@novatech-eng.com>
Subject: RE: Pre-Consultation Follow-Up: 5331 Fernbank

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It's not clearly spelled out in the text of the 2019 JFSA report. It is contained in the modelling files (provided by Stantec) that JFSA used for the overall Monahan Drain analysis including our site. I have attached the email we received from JFSA that confirms the 85L/s/Ha release rate for our site.

Please let us know if you need anything further.

Thanks,

Drew

Drew Blair, P.Eng., Project Manager | Land Development Engineering

NOVATECH Engineers, Planners & Landscape Architects

240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 x 236 | Fax: 613.254.5867

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From: Kuruvilla, Santhosh <Santhosh.Kuruvilla@ottawa.ca>

Sent: Tuesday, May 11, 2021 2:09 PM

To: Drew Blair <D.Blair@novatech-eng.com>

Cc: Marc St.Pierre <m.stpierre@novatech-eng.com>

Subject: RE: Pre-Consultation Follow-Up: 5331 Fernbank

Hi Drew,

Thanks for your email.

Could you please let me know where (on what page) you found the stormwater quantity control criteria (85 L/s/Ha) for this development in the 2019 JFSA report?

Thanks,

Santhosh

From: Drew Blair <D.Blair@novatech-eng.com>

Sent: May 10, 2021 3:11 PM

To: Kuruvilla, Santhosh <Santhosh.Kuruvilla@ottawa.ca>

Cc: Marc St.Pierre <m.stpierre@novatech-eng.com>

Subject: FW: Pre-Consultation Follow-Up: 5331 Fernbank

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We are currently working on our review of the stormwater design criteria from the 2019 J. F. Sabourin & Associates (JFSA) Monahan Drain Constructed Wetlands report that includes our site at 5331 Fernbank and have a question for you. The following statement "stormwater quantity control criteria – post development peak flow from the site shall be controlled to 70 L/s/ha" was provided in the pre-consultation notes below from the City for this site. From our review with JFSA and their 2019 report, our understanding from them is that the post development peak 100-Year minor system flow is 316 L/s for our site which divided by the site area of 3.7Ha is a minor system peak release rate of 85L/s/Ha. We will provide the background information and correspondence as part of our site plan submission.

Please confirm that we can proceed with the post development peak flow rate of 85L/s/Ha as per the 2019 JFSA report.

Please let us know if you need any further information.

Thanks,

Drew

Drew Blair, P.Eng., Project Manager | Land Development Engineering

NOVATECH Engineers, Planners & Landscape Architects

240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 x 236 | Fax: 613.254.5867

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From: Vincent Denomme <vincent.denomme@claridgehomes.com>

Sent: Thursday, February 18, 2021 9:14 AM

To: Shawn Malhotra <shawn.malhotra@claridgehomes.com>; Drew Blair <D.Blair@novatech-eng.com>; Marc St.Pierre <m.stpierre@novatech-eng.com>; Colleen McKeracher <cmckeracher@rlaarchitecture.ca>; Jim Burghout <jim.burghout@claridgehomes.com>; Brad Byvelds <B.Byvelds@novatech-eng.com>; Greg Winters <G.Winters@novatech-eng.com>

Subject: Fwd: Pre-Consultation Follow-Up: 5331 Fernbank

All,

See pre-consult comments for your review.

----- Forwarded message -----

From: **McCreight, Laurel** <Laurel.McCreight@ottawa.ca>

Date: Wed, Feb 17, 2021 at 8:05 AM

Subject: Pre-Consultation Follow-Up: 5331 Fernbank

To: Vincent Denomme <vincent.denomme@claridgehomes.com>

Hi Vincent,

Please refer to the below regarding the Pre-Application for 5331 Fernbank Road for a Site Plan Control Application for a residential development containing 16 walk-up apartment buildings. I have also attached the required Plans & Study List for application submission.

Below are staff's preliminary comments based on the information available at the time of the pre-consultation meeting:

Planning / Urban Design

- A public parkette should be provided as discussed in the pre-consult meeting.
 - Parks staff have indicated that a minimum size of 0.266 ha would be required based on the dedication requirements.
 - An illustration of a preferred location has been provided.

- The pathway block located on the east side of the subject site should be provided with a public outlet to Terry Fox Drive, and/or Cope Drive/Fernbank Road.
 - This could be achieved by way of a pathway block, or private pathways with a public pedestrian easement.
- Garbage buildings in various locations are preferable to the current proposed molok/earth bin proposal.
 - Please consult the waste management guidelines for planned unit developments.
- Variation of the building placement along the east edge of the site is encouraged.
 - Slightly off setting the blocks would create visual interest and allow for additional plantings abutting the north/south private drive aisle.
- Internal walkways should connect to existing and planned sidewalks within the right of way.
- Concrete sidewalks should be provided internal to the site.
- Parking areas should be consolidated to the greatest extent possible to allow for additional landscaping on site.
- The proposed amenity areas labelled as park should be designed to provide buffering from Terry Fox Drive for future users.
 - This is not an ideal location for a private amenity on-site, and if retained should be designed for passive use vs. active play etc.
- Please ensure that the final landscape design incorporates four season design – wind, shadow, conifers etc. and CPTED principles.
- There are areas that do not appear to provide the appropriate landscape buffers for parking areas.
- Consideration should be given to alternatives to the loop at the south end of the site (hammerhead etc.) to reduce the amount of hard surface required in that area.
- A design brief is required as part of the subject application.
 - A terms of reference is attached.
- You are encouraged to contact the Ward Councillor, Councillor [Allan Hubley](#), about the proposal.

Parks

- Parkland dedication required rather than cash-in-lieu of parkland.
- Density and location of existing/proposed parks nearby are not close enough to serve these residents.
- Park size of approximately 0.266 ha requirement based on current unit types/property area - at the small end of our park sizes, but still appropriate for some play features for residents of this development.
- The area around Block A is best location due to frontage requirements and it is quieter than Terry Fox.
 - Full park requirements can be seen in the City's Park Development Manual.
- Pathway block at the end of Tabaret – important to provide connectivity to that existing path and new park (see comments above from Planning/Urban Design).
- What are intentions for narrow parcel – Part 1, Block 98?
 - We would like to see a pathway connection here with the park.
 - Consider dedicating a pathway block in the former ROW lands to provide the connectivity, especially if there are concerns regarding crossing privately-owned lands.

Please contact Infrastructure Parks Planner [Reid Shepherd](#) for follow-up questions.

Engineering

- Stormwater quantity control criteria – post development peak flow from the site shall be controlled to 70 L/s/ha.

- Existing sanitary sewer is available on Cope Drive to make service connection.
- Existing storm sewer is available on Cope Drive to make service connection.
- Existing watermain is available on Cope Drive to make service connection.
- If looping is required for water, a second service connection is required.
- Stormwater quality control – Consult with the Conservation Authority (RVCA) for their requirements.
 - Include the correspondence with RVCA in the stormwater/site servicing report.
- As per the City of Ottawa Slope Stability Guidelines for Development Applications an engineering report is required for any retaining walls proposed 1.0 m or greater in height within the subject site that addresses the global stability of the wall and provides structural details.
 - A Retaining Wall Stability Analysis Report and Retaining Wall Structural Details are required to be provided from a Professional Engineer licensed in the Province of Ontario that demonstrates the proposed retaining wall structure has been assessed for global instability as per City standards.
 - Please ensure the analysis and required documentation are provided as part of the submission to address this comment.
- Emergency routes will need to be satisfactory to Fire Services.
 - Please show fire routes on the site plan.
 - For information regarding fire route provisions, please consult with Kevin Heiss at kevin.heiss@ottawa.ca.
- Clearly show and label the property lines on all sides of the property.
- Clearly show and label all the easements (if any) on the property, on all plans.
- When calculating the post development composite runoff coefficient (C), please provide a drawing showing the individual drainage area and its runoff coefficient.
- When using the modified rational method to calculate the storage requirements for the site, the underground storage should not be included in the overall available storage.
 - The modified rational method assumes that the restricted flow rate is constant throughout the storm which, in this case, underestimates the storage requirement prior to the 1:100-year head elevation being reached. Alternately, if you wish to include the underground storage, you may use an assumed average release rate equal to 50% of the peak allowable rate.
 - Otherwise, disregard the underground storage as available storage or provide modeling to support the design.
- Engineering plans are to be submitted on standard A1 size (594mm x 841mm) sheets.
- Phase 1 ESA and Phase 2 ESA must conform to clause 4.8.4 of the Official Plan that requires that development applications conform to Ontario Regulation 153/04.

1. Provide the following information for water main boundary conditions:

1. Location map with water service connection location(s).
 2. Average daily demand (l/s).
 3. Maximum daily demand (l/s).
 4. Maximum hourly demand (l/s).
 5. Fire flow demand (provide detailed fire flow calculations based on Fire Underwriters survey (FUS) Water Supply for Public Fire Protection). Exposure separation distances shall be defined on a figure to support the FUS calculation and required fire flow (RFF).
 6. Hydrant capacity shall be assessed to demonstrate the RFF can be achieved. Please identify which hydrants are being considered to meet the RFF on a fire hydrant coverage plan as part of the boundary conditions request.
- If you are proposing any exterior light fixtures, all must be included and approved as part of the site plan approval. Therefore, the lights must be clearly identified by make, model and part number. All external light

fixtures must meet the criteria for full cut-off classification as recognized by the Illuminating Engineering Society of North America (IESNA or IES), and must result in minimal light spillage onto adjacent properties (as a guideline, 0.5 fc is normally the maximum allowable spillage). In order to satisfy these criteria, the applicant must provide certification from an acceptable professional engineer. The location of all exterior fixtures, a table showing the fixture types (including make, model, part number), and the mounting heights must be included on a plan.

References and Resources

- As per section 53 of the Professional Engineers Act, O. Reg 941/40, R.S.O. 1990, all documents prepared by engineers must be signed and dated on the seal.
- All required plans are to be submitted on standard A1 size sheets (594mm x 841mm) sheets, utilizing a reasonable and appropriate metric scale as per City of Ottawa Servicing and Grading Plan Requirements: title blocks are to be placed on the right of the sheets and not along the bottom. Engineering plans may be combined, but the Site Plans must be provided separately. Plans shall include the survey monument used to confirm datum. Information shall be provided to enable a non-surveyor to locate the survey monument presented by the consultant.
- All required plans & reports are to be provided in *.pdf format (at application submission and for any, and all, re-submissions)
- Please find relevant City of Ottawa Links to Preparing Studies and Plans below:
- <https://ottawa.ca/en/city-hall/planning-and-development/information-developers/development-application-review-process/development-application-submission/guide-preparing-studies-and-plans#standards-policies-and-guidelines>
- To request City of Ottawa plan(s) or report information please contact the City of Ottawa Information Centre:
InformationCentre@ottawa.ca<<mailto:InformationCentre@ottawa.ca>>

(613) 580-2424 ext. 44455

Please contact Infrastructure Project Manager [Santhosh Kuruvilla](#) for follow-up questions.

Transportation

- Follow Traffic Impact Assessment Guidelines
 - A TIA is required. Submit Scoping report at your earliest convenience.
 - Start this process asap. The application will not be deemed complete until the submission of the draft step 1-4, including the functional draft RMA package (if applicable) and/or monitoring report (if applicable).
 - Although a full review of the TIA Strategy report (Step 4) is not required prior to an application, it is strongly recommended.
 - Synchro files are required at Step 4.
 - Request base mapping asap if RMA is required. Contact Engineering Services (<https://ottawa.ca/en/city-hall/planning-and-development/engineering-services>)
- ROW protection on Terry Fox and Cope is 44.5 and 24 metres, respectively.
- A sidewalk on Terry Fox is strongly recommended.
- No full movement access will be permitted on this segment of Terry Fox.
- A Road Noise Impact Study is required.

- For the two private accesses, provide enough throat length for arterial/collector as per TAC guidelines.
- On site plan:
 - Show all details of the roads abutting the site up to and including the opposite curb; include such items as pavement markings, accesses and/or sidewalks.
 - Turning movement diagrams required for all accesses showing the largest vehicle to access/egress the site.
 - Turning movement diagrams required for internal movements (loading areas, garbage).
 - Show all curb radii measurements; ensure that all curb radii are reduced as much as possible
 - Show lane/aisle widths.
 - Sidewalk is to be continuous across access as per City Specification 7.1.
 - Grey out any area that will not be impacted by this application.
- The City recommends development on private property be in accordance with the Accessibility Design Standards (AODA legislation). As the site proposed is residential, it is suggested that the design conforms to the Site Plan Checklist, which summarizes AODA requirements (attached).

Please contact Transportation Project Manager, [Mike Giampa](#) for follow-up questions.

Other

Please refer to the links to “[Guide to preparing studies and plans](#)” and [fees](#) for general information. Additional information is available related to [building permits](#), [development charges](#), and the [Accessibility Design Standards](#). Be aware that other fees and permits may be required, outside of the development review process. You may obtain background drawings by contacting informationcentre@ottawa.ca.

These pre-consultation comments are valid for one year. If you submit a development application(s) after this time, you may be required to meet for another pre-consultation meeting and/or the submission requirements may change. You are as well encouraged to contact us for a follow-up meeting if the plan/concept will be further refined.

Please do not hesitate to contact me if you have any questions.

Regards,

Laurel

Laurel McCreight MCIP, RPP

Planner

Development Review West

Urbaniste

Examen des demandes d'aménagement ouest

City of Ottawa | Ville d'Ottawa

☎ 613.580.2424 ext./poste 16587

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Vincent Dénommé
613-233-6030 ex 247



www.claridgehomes.com

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**SITE PLAN CONTROL APPLICATION
DELEGATED AUTHORITY REPORT
MANAGER, DEVELOPMENT REVIEW, WEST**

Site Location: 5331 Fernbank Road

File No.: D07-12-21-0080

Date of Application: June 4, 2021

This SITE PLAN CONTROL application submitted by 2808761 Ontario Limited, is APPROVED as shown on the following plan(s):

1. **Site Plan (North-West)**, SP-1, prepared by rla/architecture, dated 2021-02-03, revision 9 dated 2022-04-06.
2. **Site Plan (South-East)**, SP-2, prepared by rla/architecture, dated 2021-02-03, revision 9 dated 2022-04-06.
3. **Site Plan (Overall)**, SP-3, prepared by rla/architecture, dated 2021-02-03, revision 9 dated 2022-04-06.
4. **Landscape Plan (North-West)**, L-1, prepared by James B. Lennox & Associates Inc., dated 06/18/2021, revision 5 dated 04/08/2022.
5. **General Plan of Services**, Drawing 121011-GP1, prepared by Novatech, Project No. 121011-00, dated June 02, 2021, revision 3, dated February 17, 2022.
6. **General Plan of Services**, Drawing 121011-GP2, prepared by Novatech, Project No. 121011-00, dated June 02, 2021, revision 3, dated February 17, 2022.
7. **Grading Plan**, Drawing 121011-GR1, prepared by Novatech, Project No. 121011-00, dated June 02, 2021, revision 3, dated February 17, 2022.
8. **Grading Plan**, Drawing 121011-GR2, prepared by Novatech, Project No. 121011-00, dated June 02, 2021, revision 3, dated February 17, 2022.
9. **Storm Drainage Area Plan**, Drawing 121011-STM, prepared by Novatech, Project No. 121011-00, dated June 02, 2021, revision 3, dated February 17, 2022.
10. **Sanitary Drainage Area Plan**, Drawing 121011-SAN, prepared by Novatech, Project No. 121011-00, dated June 02, 2021, revision 3, dated February 17, 2022.
11. **Erosion and Sediment Control Plan**, Drawing 121011-ESC, prepared by Novatech, Project No. 121011-00, dated June 02, 2021, revision 3, dated February 17, 2022.
12. **Plan and Profile**, Drawing 121011-PR, prepared by Novatech, Project No. 121011-00, dated November 05, 2021, revision 2, dated February 17, 2022.
13. **Notes, Legends and Details**, Drawing 121011-NLD, prepared by Novatech, Project No. 121011-00, dated June 02, 2021, revision 3, dated February 17, 2022.
14. **Proposed Retaining Wall**, Drawing PG5683-2, prepared by Paterson Group, Project No. PG5683, dated March 02, 2022, revision 2, dated May 26, 2022.

And as detailed in the following report(s):

1. **Transportation Impact Assessment**, prepared by Novatech, dated June 3, 2021, revised November 8, 2021.
2. **Fernbank Zens Site Servicing Report**, prepared by Novatech, Ref #R-2021-079, dated June 02, 2021, revised February 17, 2022.
3. **Geotechnical Investigation Report**, prepared by Paterson Group, Report #PG5683-1, dated March 5, 2021
4. **Geotechnical Memorandum**, prepared by Paterson Group, File PG5683-Memo-02 Revision 3, dated March 10, 2021.

And subject to the following Requirements, General and Special Conditions:

General Conditions

1. Execution of Agreement Within One Year

The Owner shall enter into this Site Plan Control Agreement, including all standard and special conditions, financial and otherwise, as required by the City. In the event that the Owner fails to sign this Agreement and complete the conditions to be satisfied prior to the signing of this Agreement within one (1) year of Site Plan approval, the approval shall lapse.

2. Permits

The Owner shall obtain such permits as may be required from municipal or provincial authorities and shall file copies thereof with the General Manager, Planning, Infrastructure and Economic Development.

3. Barrier Curbs

The Owner acknowledges and agrees that the parking areas and entrances shall have barrier curbs and shall be constructed in accordance with the drawings of a design professional, such drawings to be approved by the General Manager, Planning, Infrastructure and Economic Development.

4. Water Supply for Fire Fighting

The Owner shall provide adequate water supply for fire fighting for every building. Water supplies may be provided from a public water works system, automatic fire pumps, pressure tanks or gravity tanks.

5. Reinstatement of City Property

The Owner shall reinstate, at its expense and to the satisfaction of the General Manager, Planning, Infrastructure and Economic Development, any property of the City, including, but not limited to, sidewalks, curbs and boulevards, which is damaged as a result of the subject development.

6. Construction Fencing

The Owner acknowledges and agrees to install construction fencing, at its expense, in such a location as may be determined by the General Manager, Planning, Infrastructure and Economic Development.

7. Extend Internal Walkway

The Owner shall extend internal walkways beyond the limits of the subject lands to connect to existing or proposed public sidewalks, at the sole expense of the Owner, to the satisfaction of the General Manager, Planning, Infrastructure and Economic Development.

8. Completion of Works

The Owner acknowledges and agrees that no new building will be occupied on the lands until all requirements with respect to completion of the Works as identified in this Agreement have been carried out and received Approval by the General Manager, Planning, Infrastructure and Economic Development, including the installation of municipal numbering provided in a permanent location visible during both day and night and the installation of any street name sign on relevant streets. Notwithstanding the non-completion of the foregoing Works, occupancy of a lot or structure may otherwise be permitted, if in the sole opinion of the General Manager, Planning, Infrastructure and Economic Development, the aforesaid Works are proceeding satisfactorily toward completion. The Owner shall obtain the prior consent of the General Manager, Planning, Infrastructure and Economic Development for such occupancy in writing.

Until all requirements with respect to completion of the Works as identified in this Agreement have been carried out and received Approval by the General Manager, Planning, Infrastructure and Economic Development, the Owner shall give notice to the City of a proposed conveyance of title to any building at least thirty (30) days prior to any such conveyance. No conveyance of title to any building shall be effective unless the Owner has complied with this provision.

Nothing in this clause shall be construed as prohibiting or preventing the approval of a consent for severance and conveyance for the purposes of obtaining financing.

9. Development Charges

The Owner shall pay development charges to the City in accordance with the bylaws of the City.

10. Development Charges – Instalment Option

- (a) The Owner acknowledges that for building permits issued after January 15, 2010, payment of non-residential development charges, excluding development charges for institutional developments, may be calculated in two (2) installments at the option of the Owner, such option to be exercised by the Owner at the time of the application for the building permit. The non-discounted portion of the development charge shall be paid at the time of issuance of the building permit and the discounted portion of the development charge shall be payable a maximum of two (2) years from the date of issuance of the initial building permit subject to the following conditions:
 - i. a written acknowledgement from the Owner of the obligation to pay the discounted portion of the development charges;
 - ii. no reduction in the Letter of Credit below the amount of the outstanding discounted development charges; and
 - iii. indexing of the development charges in accordance with the provisions of the City's Development Charges By-law, as amended.

- (b) The Owner further acknowledges and agrees that Council may terminate the eligibility for this two (2) stage payment at any time without notice, including for the lands subject to this Agreement and including for a building permit for which an application has been filed but not yet issued.
- (c) For the purposes of this provision,
 - i. “discounted portion” means the costs of eligible services, except fire, police and engineered services, that are subject to 90% cost recovery of growth-related net capital costs for purposes of funding from development charges. The 10% discounted portion, for applicable services, must be financed from non-development charge revenue sources.
 - ii. “non-discounted portion” means the costs of eligible services, fire, police and engineered services, that are subject to 100% cost recovery of growth-related net capital costs for purposes of funding from development charges.

Special Conditions

11. Permanent Features

The Owner acknowledges and agrees that no permanent features shall be permitted above and below grade within the City’s widened right-of-way or corner sight triangle, including commercial signage.

12. Geotechnical Investigation

The Owner acknowledges and agrees that it shall retain the services of a geotechnical engineer, licensed in the Province of Ontario, to ensure that the recommendations of the Geotechnical Investigation Report (the “Report”), referenced in Schedule “E” herein, are fully implemented. The Owner further acknowledges and agrees that it shall provide the General Manager, Planning, Real Estate and Economic Development with confirmation issued by the geotechnical engineer that the Owner has complied with all recommendations and provisions of the Report, prior to construction of the foundation and at the completion of the Works, which confirmation shall be to the satisfaction of the General Manager, Planning, Real Estate and Economic Development.

13. Retaining Wall - Stability

The Owner acknowledges and agrees to install the proposed retaining walls along the north-east property line in accordance with the Retaining Wall Design and as shown on the approved Grading Plan (GR2), both referenced in Schedule “E” hereto. The Owner shall provide written confirmation, satisfactory to the General Manager, Planning, Real Estate and Economic Development, that a Geotechnical Engineer/Professional Structural Engineer, licensed in the Province of Ontario, has inspected and confirmed that the retaining walls have been constructed in accordance with the said Retaining Wall Design. The Owner further acknowledges and agrees to provide an Internal Compound Stability (ICS) analysis from a Geotechnical Engineer / Professional Structural Engineer, licensed in the Province of Ontario, that all retaining walls, which are greater than one metre in height have been checked for global stability, have a factor of safety of at least 1.5 for static conditions (as calculated through SLIDE) and 1.1 for seismic conditions is achieved, which shall be to the satisfaction of the General Manager, Planning, Real Estate and Economic Development. The report shall provide structural details of the retaining wall(s).

The Owner further acknowledge and agrees to retain the services of a Professional Structural Engineer and a Soils Engineer, licensed in the Province of Ontario, to inspect any retaining walls on the subject lands and confirm that the retaining walls have been constructed in accordance with the approved retaining wall details.

14. Re-Grading and Maintenance of Ditch

The Owner acknowledges and agrees it shall be responsible for various grading and maintenance measures along Terry Fox Drive which include the following:

- a. Re-grade the shoulders of the ditch within the road allowance abutting the subject lands, to the satisfaction of the General Manager, Planning, Real Estate and Economic Development Department;
- b. Obtain utility clearances prior to the re-grading of any ditch if applicable;
- c. Maintain a grass cover within the road allowance abutting the subject lands, to the satisfaction of the General Manager, Planning, Real Estate and Economic Development Department.

15. Protection of City Sewers

- a. Prior to the issuance of a Commence Work Notification, the Owner shall, at its expense
 - obtain a video inspection of the City Sewers within Cope Drive prior to any construction to determine the condition of the existing City Sewer Systems prior to construction on the lands and to provide said video inspection to the General Manager, Planning, Real Estate and Economic Development.
- b. Upon completion of construction on the lands, the Owner shall, at its expense and to the satisfaction of the General Manager, Planning, Real Estate and Economic Development:
 - i. obtain a video inspection of the existing City Sewer Systems within Cope Drive to determine if the City Sewer System sustained any damages as a result of construction on the lands; and
 - ii. assume all liability for any damages caused to the City Sewer System within Cope Drive and compensate the City for the full amount of any required repairs to the City Sewer System.

16. Inlet Control Devices (ICDs)

The Owner acknowledges and agrees to install and maintain in good working order the required in-ground stormwater inlet control devices, as recommended in the approved Site Servicing Report and General Plan of Services, referenced in Schedule "E" herein. The Owner further acknowledges and agrees it shall assume all maintenance and replacement responsibilities in perpetuity. The Owner shall keep all records of inspection and maintenance in perpetuity and shall provide said records to the City upon its request.

17. Professional Engineering Inspection

The Owner shall have competent Professional Engineering inspection personnel on-site during the period of construction, to supervise the Works, and the General Manager, Planning, Real Estate and Economic Development, shall have the right at all times to inspect the installation of the Works. The Owner acknowledges and agrees that should it be found in the sole opinion of the General Manager, Planning, Real Estate and Economic Development, that such personnel are not on-site or are incompetent in the performance of their duties, or that the said Works are not being carried out in accordance with the approved plans or specifications and in accordance with good engineering practice, then the General Manager, Planning, Real Estate and Economic Development, may order all Work in the project to be stopped, altered, retested or changed to the satisfaction of the General Manager, Planning, Real Estate and Economic Development.

18. Stormwater Works Certification

Upon completion of all stormwater management Works, the Owner acknowledges and agrees to retain the services of a Professional Engineer, licensed in the Province of Ontario, to ensure that all measures have been implemented in conformity with the approved Site Servicing Report and General Plan of Services, referenced in Schedule "E" herein. The Owner further acknowledges and agrees to provide the General Manager, Planning, Real Estate and Economic Development with certificates of compliance issued by a Professional Engineer, licensed in the Province of Ontario, confirming that all recommendations and provisions have been implemented in accordance with the approved Site Servicing Report and General Plan of Services referenced in Schedule "E" herein.

19. Site Dewatering

The Owner acknowledges and agrees that while the site is under construction, any water discharged to the sanitary sewer due to dewatering shall meet the requirements of the City's Sewer Use By-law No. 2003-514, as amended.

20. Water Plant

The Owner acknowledges and agrees that the water plant within the lands is a private watermain. The Owner further acknowledges and agrees that the private watermain and appurtenances thereto are to be maintained by the Owner at its own expense, in perpetuity. The Owner performing maintenance on critical infrastructure, such as private watermains and private fire hydrants, shall maintain adequate records as proof of having done so in accordance with applicable regulations, and that the records shall be retained for review by the City and or the Ottawa Fire Services when requested.

21. Private Storm Sewer Connection to City Sewer System

The Owner acknowledges and agrees that any new storm sewers to be installed as part of this development shall not be connected to the City's existing storm sewer system until such time as either:

- a. a certificate of conformance and As-built Drawings have been received from a Professional Engineer, licensed in the Province of Ontario, certifying that all required inlet control devices have been properly installed to City Standards or Specifications, and that the storm sewer system has been installed in accordance with the approved engineering drawings for site development and City Sewer Design Guidelines. The inlet control devices shall be free of any debris; or

- b. a flow limiting orifice plate, designed by a Professional Engineer licensed in the Province of Ontario and to the satisfaction of the City, has been installed at the storm water outlet prior to connecting any upstream storm sewers. Such orifice plate shall not be removed until subsection (a) above has been satisfied and approved by the General Manager, Planning, Real Estate and Economic Development.

22. Leak Survey

The Owner acknowledges and agrees that the Water Plant and sewer service within the lands is a private system, including Private Services and sewer services and appurtenances, and the Owner acknowledges and agrees that it is responsible for the operation, maintenance and/or replacement, in perpetuity, of the Private Services and sewer system, including the Private Watermains, private hydrants, private sanitary and storm sewer infrastructure (collectively the “private system”) which are located on the lands and that the Owner will retain copies of all the associated Work and maintenance contracts, and make said contracts available for inspection upon demand by the City.

Further, the Owner acknowledges and agrees to have a Professional Engineer, licensed in the Province of Ontario, conduct regular inspections of the water system and sewer system, which includes a leak detection survey at least every five (5) years and a video of the sanitary sewer system to check for major water infiltration into the private system. Copies of the inspection reports and videos shall be provided to the General Manager, Public Works and Environmental Services and Fire Services. The Owner further acknowledges and agrees that as part of the Owner’s ongoing maintenance responsibility for the private system, repairs to the system must be completed immediately to correct any deficiencies which contribute to water loss or leakage of infiltration within the private system. Any deficiencies shall be immediately reported to the City. The Owner acknowledges and agrees to notify the General Manager, Public Works and Environmental Services when such repairs have been completed.

23. Site Lighting Certificate

- a. In addition to the requirements contained in clause 19 of Schedule “C” hereto, the Owner acknowledges and agrees, prior to the issuance of a building permit, to provide the City with a certificate from an acceptable professional engineer, licensed in the Province of Ontario, which certificate shall state that the exterior site lighting has been designed to meet the following criteria:
 - i. it must be designed using only fixtures that meet the criteria for full cut-off (sharp cut-off) classification, as recognized by the Illuminating Engineering Society of North America (IESNA or IES);
 - ii. and it must result in minimal light spillage onto adjacent properties. As a guideline, 0.5 fc is normally the maximum allowable spillage.
- b. The Owner acknowledges and agrees that, upon completion of the lighting Works and prior to the City releasing any associated securities, the Owner shall provide certification satisfactory to the General Manager, Planning, Real Estate and Economic Development, from a Professional Engineer, licensed in the Province of Ontario, that the site lighting has been constructed in accordance with the Owner’s approved design plan.

24. Snow Storage – no interference with servicing

In addition to the requirements of Clause 17 of Schedule “C” of this Agreement, the Owner further acknowledges and agrees that any portion of the subject lands which is intended to be used for snow storage shall not interfere with the servicing of the subject lands.

25. Joint Use, Maintenance and Liability Agreement

- a. The Owner acknowledges and agrees that should the lands be severed in the future, it shall ensure that the future owner of the freehold units shall enter into a Joint Use, Maintenance and Liability Agreement which shall be binding upon the owners and all subsequent purchasers to deal with the joint use, maintenance and liability of the common elements, including but not limited to any private roadway(s) and concrete sidewalks; common grass areas; common party walls, exterior walls; common structural elements such as the roof, foundations; common parking areas; sewers and watermains, for the mutual benefit and joint use of the owners; and any other elements located in the common property; and the Joint Use, Maintenance and Liability Agreement shall be filed with the General Manager, Planning, Real Estate and Economic Development.
- b. The Owner shall file with the General Manager, Planning, Real Estate and Economic Development, an opinion from a solicitor authorized to practice law in the Province of Ontario that the Joint Use, Maintenance and Liability Agreement is binding upon the owners of the land and all subsequent purchasers to deal with the matters referred to Paragraph (a) above.
- c. The Owner acknowledges and agrees that the Joint Use, Maintenance and Liability Agreement shall be registered on the Owner’s lands at no cost to the City, and a copy of the registered agreement shall be provided to the General Manager, Planning, Real Estate and Economic Development.
- d. The Owner acknowledges and agrees that the Joint Use, Maintenance and Liability Agreement shall include a clause that transfers all legal and financial obligations required under the Joint Use, Maintenance and Liability Agreement to future owners, successors and assigns in title of the subject lands.

26. New Multi-Unit Residential

The Owner acknowledges that this Site Plan approval is for a residential development subject to the Monahan Drain Area-Specific Development Charge for Stormwater Management Facilities, pursuant to the City’s applicable Development Charges By-law. The Owner acknowledges and agrees that the applicable residential Area-Specific Development Charge is based on the units as set out in the following table.

Unit Type	Number of Units	Value per Unit (subject to indexing)	Total Charge
Apartment Dwelling	192 (16 apartment blocks)	\$ 1,544.00	\$ 296,448.00
Total	192		\$ 296,448.00

Upon execution of this Agreement, the Owner shall pay the Area-Specific Development Charge, as referenced in Schedule "B" herein and subject to indexing, for the above referenced residential units.

27. Archaeological Potential

In the event that archaeological or human remains are discovered on or buried within the subject lands during development activities, the Owner acknowledges and agrees to stop all construction and soil disturbance and shall notify the Ministry of Tourism, Culture and Sport of such findings. As required under Part VI of the Ontario Heritage Act, R.S.O. 1990, c.O.18.

28. Exterior Elevations Drawings

The Owner acknowledges and agrees to construct the proposed building in accordance with the approved Elevations Plans, referenced in Schedule "E" herein. The Owner further acknowledges and agrees that any subsequent proposed changes to the approved Elevations Plans shall be filed with the General Manager, Planning, Infrastructure and Economic Development and agreed to by both the Owner and the City prior to the implementation of such changes. No amendment to this Agreement shall be required.

29. Waste and Recycling Collection (Standard Collection)

(a) Residential Units

The Owner acknowledges and agrees that the City will provide waste collection and cart (and/or container) recycling collection for the residential units. The Owner shall provide an adequate storage room or space for waste containers and recycling carts (and/or containers). The Owner acknowledges and agrees that it is recommended that the containers and carts be placed on a concrete floor. The Owner shall provide an adequate constructed road access to the waste/recycling storage room or area suitable for waste/recycling vehicles as direct access to the containers and carts is required. The Owner acknowledges and agrees that any additional services (i.e. winching of containers) may result in extra charges.

30. Cash-in-Lieu of Parkland

The Owner shall pay cash-in-lieu of parkland in accordance with the Parkland Dedication By-law of the City of Ottawa, as well as the fee for appraisal services. The monies are to be paid at the time of execution of the Site Plan Agreement.

31. Installation of Signs on Private Property

The Owner acknowledges and agrees it shall obtain approval from the Chief Building Official, Building Code Services prior to installation of any signs on the subject lands. The Owner further acknowledges and agrees that any such signs shall be installed in a location to the satisfaction of the Chief Building Official, Building Code Services and the General Manager, Planning, Infrastructure and Economic Development, and in accordance with the City's Permanent Signs on Private Property By-law No. 2016-326, as amended.

32. Road Modifications

The Owner agrees to complete all road modifications required to accommodate this development, as identified in the Pavement Marking and Signage Plan referenced in Schedule "E" hereto, and further acknowledges and agrees that it is responsible for all costs associated with the public roadway modifications.

33. Transportation Impact Assessment

The Owner has undertaken a Transportation Impact Assessment for this site, referenced in Schedule "E" herein, to determine the infrastructure and programs needed to mitigate the impact of the proposed development on the local transportation network and to establish the site design features needed to support system-wide transportation objectives. The Owner shall ensure that the recommendations of the Transportation Impact Assessment, are fully implemented, to the satisfaction of the General Manager, Planning, Real Estate and Economic Development.

34. Private Approach Detail

The Owner acknowledges and agrees that all private approaches serving the proposed development shall be designed and constructed, at the sole expense of the Owner, in accordance with the City's "Curb Return Entrances – Uncontrolled Intersections" Plan, Drawing No. SC7.1, dated March 2007 and revised March 2021, and the Owner shall comply with the City's Private Approach By-law, being No. 2003-447, as amended.

35. Road Widening

Prior to registration of this Agreement, the Owner acknowledges and agrees to convey to the City, at no cost to the City, an unencumbered road widening across the complete Terry Fox Drive frontage of the lands, measuring 22.25 metres from the existing centreline of pavement/the abutting right-of-way. The exact widening must be determined by legal survey. The Owner shall provide a reference plan for registration, indicating the widening, to the City Surveyor for review and approval prior to its deposit in the Land Registry Office. Such reference plan must be tied to the Horizontal Control Network in accordance with the municipal requirements and guidelines for referencing legal surveys. The Owner acknowledges and agrees to provide an electronic copy of the Transfer and a copy of the deposited reference plan to the City Solicitor prior to the execution of this Agreement by the City. All costs shall be borne by the Owner.

36. Bus Pad Easement

Prior to the registration of this Agreement, the Owner shall grant to the City, at no cost to the City, an unencumbered 1.2 metres x 8.2 metres easement for the transit stop bus pad along Fernbank Road, as shown on the approved Site Plan referenced in Schedule "E" hereto, if applicable, to the satisfaction of the City. The Owner shall provide a Reference Plan for registration, indicating the Bus Pad easement, to the City Surveyor for review and approval prior to its deposit in the Land Registry Office. Such reference plan must be tied to the Horizontal Control Network in accordance with the municipal requirements and guidelines for referencing legal surveys. The Owner acknowledges and agrees to provide an electronic copy of the Transfer and a copy of the deposited reference plan to the City Solicitor prior to registration of the easement. All costs shall be borne by the Owner.

37. Noise Control Attenuation Measures

The Owner acknowledges and agrees to implement the noise control attenuation measures recommended in the approved Fernbank Zens Detailed Noise Control Study, referenced in Schedule "E" of this Agreement, as follows:

- a. Buildings C, D, E, F, G, H, J, K, L, M, N, P and Q are to be equipped with central air conditioning;
- b. Buildings A, B and R are to be fitted with a forced air heating system and ducting, and shall be sized to accommodate central air conditioning;
- c. further to subsection (b) above, the location and installation of any outdoor air conditioning device(s) shall comply with the noise criteria of the Ministry of the Environment, Conservation and Parks' Publication NPC-216, dated 1993, and the Environmental Noise Guidelines for Installation of Residential Air Conditioning Devices, dated September 1994, as amended, in order to minimize the noise impacts both on and off the immediate vicinity of the subject lands.
- d. prior to the issuance of a building permit for Buildings C, D, E, F, G, H, J, K, L, M, N, P and Q, a review of building components (windows, walls, doors) is required and must be designed to achieve indoor sound levels within the City's and the Ministry of the Environment, Conservation and Parks' noise criteria;
- e. notice respecting noise shall be registered against the lands, at no cost to the City, and a warning clause shall be included in all agreements of purchase and sale or lease agreements, as detailed in Condition 46 below.

38. Notice on Title – Noise Control Attenuation Measures

The Owner, or any subsequent owner of the whole or any part of the subject lands, acknowledges and agrees that all agreements of purchase and sale or lease agreements shall contain the following clauses, which shall be covenants running with the subject lands:

Buildings A, B and R: Type C – Forced Air Heating System and Ducting

"The Purchaser/Lessee for himself, his heirs, executors, administrators, successors and assigns acknowledges being advised that this dwelling unit has been fitted with a forced air heating system and the ducting, etc. was sized to accommodate central air conditioning. Installation of central air conditioning by the Purchaser/Lessee will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the City of Ottawa's and the Ministry of the Environment, Conservation and Parks' noise criteria."

"The Purchaser/Lessee for himself, his heirs, executors, administrators, successors and assigns acknowledges and agrees it shall identify the location and install any outdoor air conditioning device(s) so as to comply with the noise criteria of the Ministry of the Environment, Conservation and Parks' Publication NPC-216, dated 1993, and the Environmental Noise Guidelines for Installation of Residential Air Conditioning Devices, dated September 1994, as amended, in order to minimize the noise impacts both on and off the immediate vicinity of the subject lands."

Buildings C, D, E, F, G, H, J, K, L, M, N, P and Q: Type D – Central Air Conditioning

"The Purchaser/Lessee for himself, his heirs, executors, administrators, successors and assigns acknowledges being advised that this development has been supplied with a central air conditioning system which will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the City of Ottawa's and the Ministry of the Environment, Conservation and Parks' noise criteria."

"The Purchaser/Lessee covenants with the Vendor/Lessor that the above clauses, verbatim, shall be included in all subsequent agreements of purchase and sale, and lease agreements for the lands described herein, which covenant shall run with the said lands."

39. Certification Letter for Noise Control Measures

- a. The Owner acknowledges and agrees that upon completion of the development and prior to occupancy and/or final building inspection, it shall retain a Professional Engineer, licensed in the Province of Ontario with expertise in the subject of acoustics related to land use planning, to visit the lands, inspect the installed noise control measures and satisfy himself that the installed recommended interior noise control measures comply with the measures in the Fernbank Zens Detailed Noise Control Study referenced in Schedule "E" hereto, as approved by the City and/or the approval agencies and authorities (The Ministry of the Environment, Conservation and Parks) or noise thresholds identified in the City's Environmental Noise Control Guidelines. The Professional Engineer shall prepare a letter to the General Manager, Planning, Real Estate and Economic Development (the "Certification Letter") stating that he certifies acoustical compliance with all requirements of the applicable conditions in this Agreement, to the satisfaction of the General Manager, Planning, Real Estate and Economic Development.
- b. The Certification Letter shall be unconditional and shall address all requirements as well as all relevant information relating to the development, including project name, building identification, drawing numbers, noise study report number, dates of relevant documents and in particular reference to the documents used for the building permits and site grading applications. The Certification Letter(s) shall bear the certification stamp of a Professional Engineer, licensed in the Province of Ontario, and shall be signed by said Professional Engineer.

All of the information required in subsections (a) and (b) above shall be submitted to the General Manager, Planning, Real Estate and Economic Development, and shall be to his satisfaction.

40. Public Access Easement

Prior to the registration of this Agreement, the Owner shall grant to the City, at no cost to the City, an unencumbered 2 metre easement for public access along the north-south pathway, as shown on the approved Site Plan referenced in Schedule "E" hereto, to the satisfaction of the City. The Owner shall provide a Reference Plan for registration, indicating the Public Access easement, to the City Surveyor for review and approval prior to its deposit in the Land Registry Office. Such reference plan must be tied to the Horizontal Control Network in accordance with the municipal requirements and guidelines for referencing legal surveys. The Owner acknowledges and agrees to provide an electronic copy of the Transfer and a copy of the deposited reference plan to the City Solicitor prior to registration of the easement. All costs shall be borne by the Owner.

41. Private Road Naming Agreement

The Owner acknowledges and agrees that a private road naming agreement will be required for the subject development.

32. Maintenance and Liability Agreement for Landscaping

The Owner acknowledges and agrees it shall be required to enter into a Maintenance and Liability Agreement with the City, for all plant and landscaping material (except municipal trees), decorative paving and street furnishings placed in the City's right-of-way along Terry Fox Drive in accordance with City Specifications, and the Maintenance and Liability Agreement shall be registered on title, at the Owner's expense, immediately after the registration of this Agreement. The Owner shall assume all maintenance and replacement responsibilities in perpetuity.

39. School Accommodation

(a) The Owner acknowledges and agrees to inform prospective purchasers that school accommodation pressures exist in the Ottawa-Carleton District School Board schools designated to serve this development, which are currently being addressed by the utilization of portable classrooms and/or by directing students to schools outside their community.

(b) The Owner acknowledges and agrees that a notice-on-title respecting school accommodation concerns, shall be registered on title to the subject lands, at the Owner's expense, and a warning clause shall be included in all agreements of purchase and sale and lease agreements.

June 2, 2022

Date



Allison Hamlin
(A) Manager, Development Review, West
Planning, Real Estate and Economic Development
Department

Enclosure: Site Plan Control Application approval – Supporting Information

SITE PLAN CONTROL APPROVAL APPLICATION SUPPORTING INFORMATION

File Number: D07-12-21-0080

SITE LOCATION

5331 Fernbank Road, and as shown on Document 1.

SYNOPSIS OF APPLICATION

The site is located on the northeast corner of the intersection at Terry Fox Drive and Fernbank Road, with frontage also on Cope Drive. The subject site is approximately 3.68 hectares in area and is currently vacant. To the north of the site is a currently undeveloped portion of the "Van Gaal" lands and is slated for a future residential development. To the south and east, there are low and medium density residential neighbourhoods. To the west, there are various large format commercial uses, as well as an automobile service station. Additionally, the southwest corner of the site is situated along the urban boundary, which culminates at the intersection of Fernbank Road and Terry Fox Drive and continues running parallel with roads in their respective directions.

The applicant is proposing to construct a planned unit development (PUD) consisting of 16 three-storey low rise apartment buildings with 12 dwelling units each. The development will have a total of 192 dwelling units and a gross floor area of 20,084 square metres. Communal amenity spaces can be found surrounding each building and in the form of a private park block within the PUD, along Terry Fox Drive. 268 surface level parking spaces are proposed, including 230 resident parking spaces and 38 visitor parking spaces; 96 bicycle parking spaces are also proposed.

DECISION AND RATIONALE

This application is approved for the following reasons:

- The proposal conforms to the applicable Official Plan policies, including the Official Plan policies relating to residential housing within the General Urban Area.
- The proposal is in compliance with all applicable zoning provisions including the provisions of the General Mixed Use, Urban Exception 2411, GM[2411] of the zoning bylaw.
- The proposed development is compatible with the surrounding uses.
- The proposed site design represents good planning.

PARKLAND DEDICATION

Parkland dedication, in accordance with By-law 2009-95, is being satisfied within this approval through the taking of cash-in-lieu of parkland as detailed in the above conditions.

CONSULTATION DETAILS

Councillor's Concurrence

Councillor Allan Hubley was aware of the application related to this report.

Councillor has concurred with the proposed conditions of approval.

Public Comments

Summary of public comments and responses

1. Concern with lack of commercial amenities within the area

- Lack of restaurants in the area
- A medical facility is needed
- Lack of gas stations

Response:

The proposal complies with the Zoning By-law. Commercial uses are not required by the zoning and residential uses are permitted.

2. Concerns with increased traffic / Request for more public parking

- Traffic on Cope Drive is already quite high
- Would like a pedestrian tunnel under Cope to get to the water park

Response:

The applicant submitted a Transportation Impact Assessment, which has been reviewed by staff and has been deemed satisfactory.

The applicant is not required to provide public parking by the Zoning By-law, only parking for residents and visitors.

3. Lack of greenspace / request for a public park

- Need more trees and greenspace
- Limited trees and wild spaces for birds and critters

Response:

The applicant submitted a landscape plan as part of their submission which has been reviewed by staff. Staff are satisfied that adequate trees and landscaping are provided.

The applicant is not providing a public park and therefore will be required to pay cash-in-lieu of parkland.

4. Density

- The proposal is too dense
- Eliminate buildings

Staff have reviewed the proposal and are satisfied that the development meets the City's goals for intensification and provides additional housing opportunities in Kanata South.

Technical Agency/Public Body Comments

All technical agency correspondence was forwarded to the applicant, and the applicant was advised to contact technical agencies directly for additional information and requirements.

Advisory Committee Comments

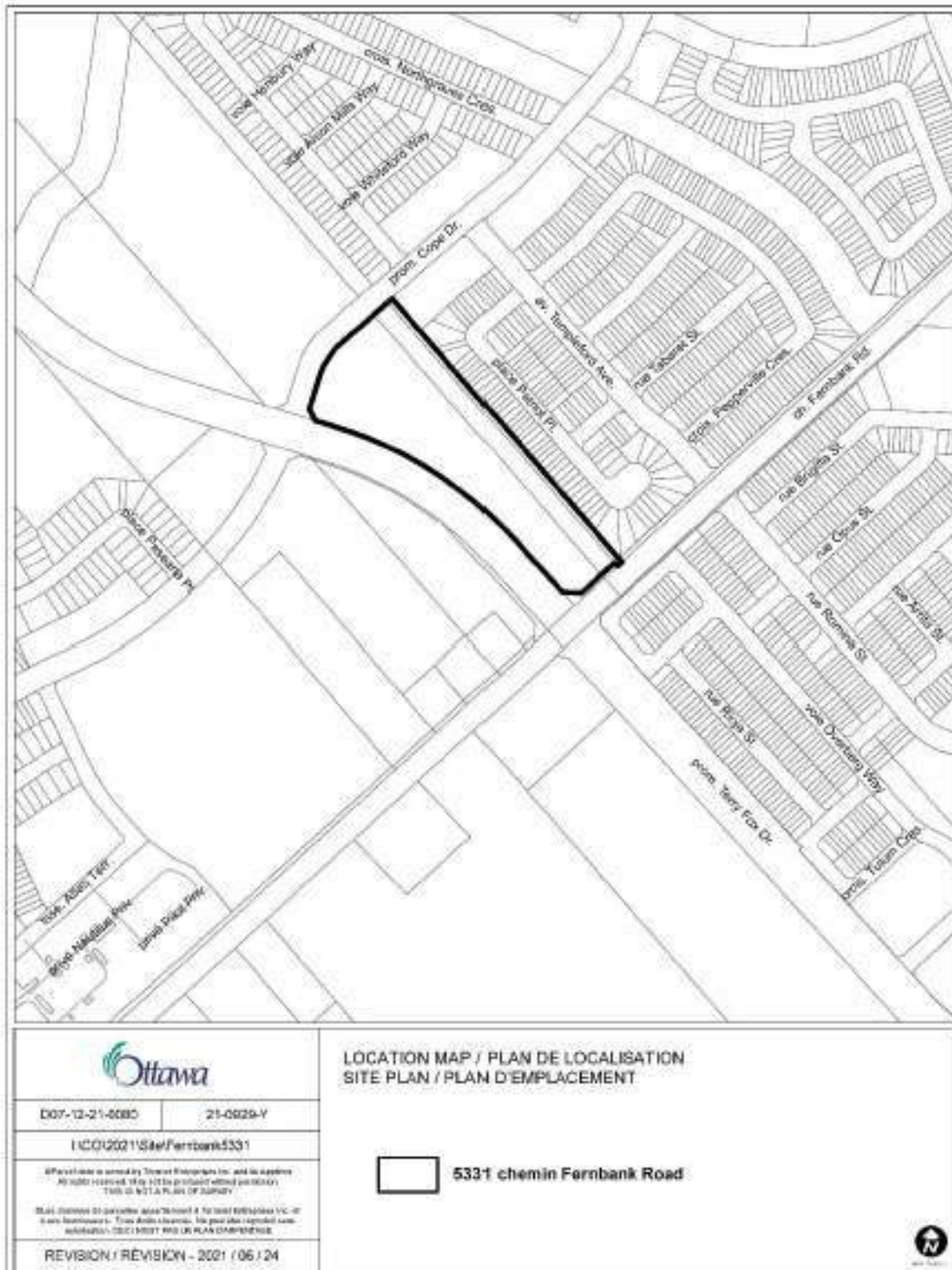
N/A

APPLICATION PROCESS TIMELINE STATUS

This Site Plan application was not processed by the On Time Decision Date established for the processing of an application that has Manager Delegated Authority due to the complexity of issues associated with the site.

Contact: Laurel McCreight Tel: 613-580-2424, ext. 16587 or e-mail: laurel.mccreight@ottawa.ca

Document 1 – Location Map



Appendix F
DRAWINGS