



Stormwater Management Report and Servicing Brief

6310 Hazeldean Road, Ottawa, ON

Prepared for:

9441-6302 Quebec Inc

Attention: Felix Allaire

LRL File No.: 220027

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TABLE OF CONTENTS

1	INTRODUCTION AND SITE DESCRIPTION	1
2	EXISTING SITE AND AVAILABLE SERVICES	1
3	PROPOSED DEVELOPMENT	2
4	SCOPE OF WORK	2
5	REGULATORY APPROVALS	3
6	WATER SUPPLY SERVICING DESIGN	3
6.1	Residential Water Demands.....	4
6.2	Commercial Water Demands	4
6.3	Total Water Demands	5
6.4	Fire Flow Demands.....	5
6.5	Boundary Conditions	6
6.6	Water Distribution Network Hydraulic Modelling	7
7	SANITARY SERVICE	7
8	STORMWATER MANAGEMENT	8
8.1	Existing Stormwater Infrastructure	8
8.2	Design Criteria	8
8.3	Proposed Stormwater Management System	8
9	EROSION & SEDIMENT CONTROL	10
10	CONCLUSION	11
11	REPORT CONDITIONS AND LIMITATIONS	12



APPENDICES

Appendix A	Site Topographical Survey As-built drawings
Appendix B	Site Plan and Architectural Floor Plans
Appendix C	Pre-Con Meeting Notes
Appendix D	Water Demand Calculations Boundary Conditions Fire Hydrant Coverage
Appendix E	Civil Engineering Drawings
Appendix F	Sanitary Calculations
Appendix G	Stormwater Management Design Calculations



LIST OF TABLES

<i>Table 1: City of Ottawa Design Guidelines- Water Design Parameters</i>	3
<i>Table 2: Residential Population Estimate</i>	4
<i>Table 3: Fire Protection Summary Table</i>	6
<i>Table 4: Summary of Boundary Conditions</i>	6
<i>Table 5: Post-development Catchment Areas and Runoff Coefficients</i>	9
<i>Table 6: Summary of 100 Year Release Rates and Storage Requirements</i>	10

LIST OF FIGURES

<i>Figure 1: Aerial View of Subject Site</i>	1
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1 INTRODUCTION AND SITE DESCRIPTION

LRL Associates was retained by Scalia to prepare a Stormwater Management Report and Serviceability Brief to support Site Plan Control application for the proposed development located at 6310 Hazeldean Road, Ottawa, ON.

The subject site is within the Stittsville Ward, located on the east side of Hazeldean Road, and has an approximate area of **1.20 ha**. Under the City of Ottawa Zoning by-law, the property is currently zoned as AM [2102]. The land is currently vacant, consisting mainly of a large mixed paved and gravel area as well as some landscaping area. The aerial view of subject site is shown below in Figure 1.



Figure 1: Aerial View of Subject Site

2 EXISTING SITE AND AVAILABLE SERVICES

The site is currently primarily covered with gravel and some natural landscaping. Based on the topography and site survey information, there is 10 m wide easement along the west property line which includes a ditch collecting and conveying water from the municipal right-of-way, sloping from the northeast corner of the site to the southeast corner. The existing site topographical survey can be found in **Appendix A**.

Sewer and watermain mapping, along with as-built information collected from the City of Ottawa (see **Appendix A**) indicate the following existing infrastructure located within the adjacent rights-of-way:



Hazeldean Road:

- 375 mmØ PVC Sanitary Sewer
- 406 mmØ PVC Watermain

Easement at Parcel West of Site:

- 450 mmØ PVC Sanitary Sewer
- 305 mmØ PVC Watermain

No municipal storm sewers are located in close proximity of the subject site; however, a roadside ditch is present along Hazeldean Road and within an easement on the east side of the site. There are currently no stormwater management measures noted on site. Stormwater runoff flows off the site in an uncontrolled manner towards Hazeldean Road rights-of-way and into the existing ditch.

3 PROPOSED DEVELOPMENT

The proposed development will consist of two multi-storey buildings, identified as Building A and Building B, both of which will be accessible from Hazeldean Road. The development will accommodate a total of 457 residential units, comprising 248 units in Building A and 209 units in Building B. Parking will be provided on two underground levels and two above-ground levels. In addition, bicycle parking spaces will also be available.

Outdoor amenity spaces and green spaces will be located on the third level of Building A. For additional detail of the proposed development, refer to the Site Plan prepared by ACDF in **Appendix B**.

4 SCOPE OF WORK

As per applicable guidelines, the scope of work includes the following:

Stormwater management

- Calculate the allowable stormwater release rate.
- Calculate the anticipated post-development stormwater release rates.
- Demonstrate how the target quantity and quality control objectives will be achieved.

Water services

- Calculate the expected water supply demand at average and peak conditions.
- Calculate the required fire flow as per the Fire Underwriters Survey (FUS) method.
- Confirm the adequacy of water supply and pressure during peak flow and fire flow.
- Describe the proposed water distribution network and connection to the existing system.

Sanitary services

- Describe the existing sanitary sewers available to receive wastewater from the proposed buildings.
- Calculate peak flow rates from the proposed development.
- Describe the proposed sanitary sewer system.



5 REGULATORY APPROVALS

As noted in the pre-consultation meeting notes (**Appendix C**), it is anticipated that an MECP Environmental Compliance Approval (ECA) will be required for the subject site. The Mississippi Valley Conservation Authority (MVCA) will also need to be consulted to obtain municipal approval for site development. No other approval requirements from other regulatory agencies are anticipated.

6 WATER SUPPLY SERVICING DESIGN

The subject property lies within the City of Ottawa 3W water distribution network pressure zone. There is an existing 406 mmØ watermain within Hazeldean Road.

According to the City of Ottawa Water Distribution Guidelines (Technical Bulletin ISTB-2021-03), since the subject site is anticipated to house more than 50 residential units, it is required to be serviced by two water service laterals, separated by an isolation valve, for redundancy and to avoid creation of a vulnerable service area. Hence, the proposed development is proposed to be serviced via two (2) 200 mmØ water services connected to the existing 406 mmØ watermain within Hazeldean Road. For the layout of proposed water servicing network, refer to the Servicing Plan C401 included in **Appendix E**.

Table 1, shown below, summarizes the City of Ottawa Design Guidelines parameters used in the preparation of the water demand estimate and servicing design.

Table 1: City of Ottawa Design Guidelines- Water Design Parameters

Design Parameters	Value
Residential Bachelor / 1 Bedroom Apartment	1.4 P/unit
Residential 2 Bedroom Apartment	2.1 P/unit
Residential 3 Bedroom Apartment	3.1 P/unit
Commercial Average Daily Demand	2.8 L/m ² /d
Average Daily Demand	280 L/c/d
Minimum Depth of Cover	2.4 m from top of watermain to finished grade
Desired operating pressure range during maximum day operating conditions	345 kPa (50 psi) and 552 kPa (80 psi)
During peak hour operating conditions pressure must not drop below	275 kPa (40 psi)
During normal operating conditions pressure shall not exceed	552 kPa (80 psi)
During fire flow operating conditions pressure must not drop below	140 kPa (20 psi)



7 RESIDENTIAL WATER DEMANDS

Anticipated population demands have been calculated based on the architectural Site Plan drawing completed by ACDF Architecture. The proposed development is anticipated to include a total of **457** residential units (248 units in Building 1 and 209 units in Building 2) which translates to a population of approximately **819** people as per the City of Ottawa Water Distribution Design Guidelines. Table 2 below summarizes the proposed population count, based on the criteria outlined in Table 4.1 of the Guidelines.

Table 2: Residential Population Estimate

Unit Type	Persons Per Unit	Number of Units		Population
		Building 1	Building 2	
Studio	1.4	33	12	63
1 Bedroom Apartment	1.4	142	63	287
2 Bedroom Apartment	2.1	67	106	363.3
3 Bedroom Apartment	3.1	6	28	105.4
	Total	248	209	818.7

The required water supply for the residential units in the proposed development has been calculated using the following formula:

Where:

$$Q = (q \times P \times M)$$

q = average water consumption (L/capita/day)

P = design population (capita)

M = peak factor

With reference to *Table 4.2 of the City of Ottawa Water Distribution Design Guidelines*, using an average water consumption rate of 280 L/c/d, a Maximum Daily Demand Factor and Maximum Hour Demand Factor of 2.5 and 2.2, respectively, anticipated demands were calculated as follows:

- Average daily demand is **2.65 L/s**,
- Maximum daily demand is **6.63 L/s**, and
- Maximum hourly demand is **14.59 L/s**.

8 COMMERCIAL WATER DEMANDS

The water supply requirements for the commercial space within the proposed development have been calculated using the following formula:

Where:

$$Q = (q \times A \times M)$$



q = average water consumption (L/ha/day)
A = commercial area (ha)
M = peak factor

With reference to Table 4.2 of the *City of Ottawa Water Distribution Design Guidelines*, using an average water consumption rate of 28,000 L/ha/d, a Maximum Daily Demand Factor and Maximum Hour Demand Factor of 1.5 and 1.8, respectively, anticipated commercial demands were calculated as follows:

- Average daily demand is **0.347 L/s**,
- Maximum daily demand is **0.520 L/s**, and
- Maximum hourly demand is **0.936 L/s**.

9 TOTAL WATER DEMANDS

Based on calculated residential and commercial demands for the proposed development, the total anticipated water demands are as follows:

- Average daily demand is **3.00 L/s**,
- Maximum daily demand is **7.15 L/s**, and
- Maximum hourly demand is **15.53 L/s**.

For greater detail on Water Demand Calculations, please refer to **Appendix D**.

10 FIRE FLOW DEMANDS

The estimated fire flow for the proposed buildings was calculated in accordance with ISTB-2018-02. The following parameters were provided by the Architect:

- Type of construction – Non-combustible Construction.
- Occupancy type – Limited Combustibility, and
- Sprinkler Protection – Automatic & Fully Supervised Sprinkler System.

The Fire Underwriters Survey 2020 was used to calculate the fire flow demand for the site. The total effective area considers the two largest adjoining floor areas plus 50% of all floors immediately above them up to a maximum of eight. Buildings A and B although sharing the same parking garage were considered as two separate buildings since the parking garage is separated from the buildings by a fire separation.

The total effective area was calculated for each building, and to be conservative, the building with the larger total effective area was used for boundary condition request. This was Building A, located on the west side of the site. It had a total effective floor area of **17,520 m²**. Building B was considered in the calculations through consideration of exposure distance. The maximum estimated fire flow demand was calculated to be **13,000 L/min** for Building A, see **Appendix D** for details.



There are at least three (3) existing fire hydrants near the contemplated buildings that are available to provide the maximum required fire flow demands of **13,000 L/min**. Refer to **Appendix D** for the water pressure zone and location of fire hydrants.

Table 3 below summarizes the aggregate fire flow of the contributing hydrants near the proposed development based on Table 18.5.4.3 of *ISTB-2018-02*.

Table 3: Fire Protection Summary Table

	Max. Fire Flow Demand (L/min)	Fire Hydrant(s) within 75m	Fire Hydrant(s) within 150m	Available Combined Fire Flow (L/min)
Proposed Development	13,000	2	1	(2 x 5678) + (1 x 3785) = 15,141

The total available fire flow from contributing hydrants is equal to **15,141 L/min** which is sufficient to provide adequate fire flow for the proposed development. A certified fire protection system specialist will need to be employed to design the building's fire suppression system and confirm the actual fire flow demand.

11 BOUNDARY CONDITIONS

The City of Ottawa was contacted to obtain boundary conditions associated with the estimated water demand, as indicated in the boundary request correspondence included in **Appendix D**. Table 4 below summarizes the boundary conditions for the proposed development.

Table 4: Summary of Boundary Conditions

Scenario	Connection 1@Hazeldean Rd		Connection 2@Hazeldean Rd	
	Head (m)	*Pressure (psi)	Head (m)	*Pressure (psi)
Maximum HGL	160.6	51.0	160.6	51.0
Peak Hour	157.0	46.0	157.0	46.0
Max Day plus Fire Flow #1	156.7	45.5	156.6	45.4

*Assumed Ground Elevation = 124.7m

As shown in Table 4, the pressures in all scenarios satisfy the required pressure ranges stated in the *City of Ottawa Design Guidelines-Water Distribution* (see Table 1). It is important to note that due to the change in the number of units (and consequently the calculated population), the water demands have increased since the initial boundary conditions request as follows:

- Average Day Demand: increased by 12.8%
- Maximum Day Demand: increased by 8.5%
- Peak Hour Demand: increased by 7.4%



It is our opinion that these modest increase in water demand are not expected to have a significant impact on the boundary conditions provided or the resulting residual pressure calculations.

12 WATER DISTRIBUTION NETWORK HYDRAULIC MODELLING

To ensure the adequacy of the proposed water distribution network, a supplementary hydraulic analysis was carried out using EPANET (Version 2.2). The top of water servicing pipe was assumed to be 2.4m below grade. Three scenarios were analyzed, as described below,

- Scenario 1: The anticipated average day demand was applied to the service entry nodes J1 and J2 of the proposed development. The resulting residual pressures within the network ranged from **54.01 to 57.70 psi**.
- Scenario 2: The anticipated peak hour demand was applied to nodes J1 and J2. The resulting residual pressures ranged from **48.86-52.56 psi**, thus exceeding the required minimum pressure of **40 psi**.
- Scenario 3: The anticipated maximum day demand was applied to nodes J1 and J2, the residual pressure within the water servicing network ranged from **48.32-52.16 psi**, thereby exceeding the required minimum pressure of **20 psi**. For this analysis, the boundary condition corresponding to the maximum day demand plus fire flow was applied at the proposed connection point.

For detailed modeling results including residual pressure, flow and velocities, refer to **Appendix D**.

13 SANITARY SERVICE

There is an existing municipal sanitary sewer within an easement located at the neighboring property parallel to the western property line of the subject site. As per pre-consultation with City staff, it is proposed that the proposed development will connect to the existing 450 mm dia. sanitary sewer within the neighboring easement. For this connection, an easement agreement with the neighbouring property is expected to be required.

A single 375 mm dia. sanitary service lateral is proposed to service all buildings within the proposed development through the underground parking garage. The sanitary flow will discharge to the proposed maintenance hole SAN MH01 and subsequently to SAN MH02, located near the southwest corner of the site.

The estimated post-development total sanitary flow is **9.72 L/s** accounting for the proposed residential population, commercial uses and infiltration allowances. The parameters included: an average daily flow of 280L/person/day, a commercial flow of 28,000L/ha/day, an extraneous flow allowance of 0.33L/s/ha, a residential peaking factor of 3.4, a commercial peaking factor of 1 and a total residential population of 819. Details of the sanitary flow calculations are provided in **Appendix F**.

Based on as-built drawings, the existing 450 mm dia. sanitary sewer located southwest of property has a slope of 0.18% and a maximum capacity of **120.96 L/s**. The anticipated peak wastewater



flow from the proposed development represents approximately **8.04%** of the existing sewer's maximum capacity. The City of Ottawa was contacted to confirm the available capacity of the existing sanitary sewer. The City has confirmed that there are no capacity concerns. Refer to the correspondence included in **Appendix D**.

14 STORMWATER MANAGEMENT

14.1 Existing Stormwater Infrastructure

The subject property lies within the Poole Creek Sub-Watershed and is within the Carp River Watershed Plan. There is a ditch located north of the site and a ditch located east of the site within a 10 m-wide easement. There are no municipal storm sewers within the Hazeldean road right-of-way.

In pre-development conditions, the site is relatively flat and primarily covered with gravel, with some grassed areas along the boundaries. Stormwater runoff from the subject site generally flows uncontrolled overland to the north of the site towards Hazeldean roadside ditch and to the east side towards the existing ditch running parallel to the site's east property line. Refer to **Appendix A** for topographical survey showing existing elevations and ditches.

14.2 Design Criteria

The stormwater management criteria for this development is based on pre-consultation with City of Ottawa officials, the City of Ottawa Sewer Design Guidelines, 2012 (City standards), as well as the Ministry of the Environment's Stormwater Management Planning and Design Manual, 2003 (SWMPD Manual).

The stormwater management will need to meet the following design criteria.

- Meet an allowable release rate based on the pre-development Rational Method coefficient or a maximum of 0.50, employing the City of Ottawa IDF parameters for a 5-year storm with a calculated time of concentration equal to or greater than 10 minutes; and
- Attenuate all storms up to and including the City of Ottawa 100-year storm event on site.
- Based on coordination with the MVCA, enhanced quality treatment (80% TSS removal) prior to release from site will be required.

14.3 Proposed Stormwater Management System

Based on pre-consultation with the City of Ottawa, the preferred outlet location of the site will be to the ditch that crosses the site at the eastern limit. This ditch is located within a 10m wide existing drainage easement OC626261. The conditions set out in the easement must be respected.

The proposed area drains on the parking lot along with roof drains on building rooftops will be utilised to collect and direct runoff to the building's mechanical system in the underground garage, and eventually to two cisterns. Storm service lateral outlets will be provided on the east side of the underground garage to discharge controlled runoff from the cisterns to the ditch.

Based on stormwater management criteria, the allowable release rate for the proposed development is calculated **155.00 L/s** for all storms up to and including the 100-year storms. To



meet the quantity control objectives, the contemplated development will utilize subsurface/cistern storage. Due to the high elevation of the proposed ditch outlet, flows from the cisterns will be pumped to the ditch. Table 5 below summarizes post-development drainage areas and runoff coefficients. Detailed calculations can be found in **Appendix G**.

Table 5: Post-development Catchment Areas and Runoff Coefficients

Catchment	Total Area (ha)	Combined C
CA-01 (controlled)	0.497	0.90
CA-02 (controlled)	0.165	0.84
CA-03A (controlled)	0.005	0.68
CA-03B (controlled)	0.005	0.66
CA-03C (controlled)	0.004	0.72
CA-03D (controlled)	0.009	0.53
CA-03E (controlled)	0.008	0.52
CA-03F (controlled)	0.009	0.52
CA-03G (controlled)	0.009	0.47
CA-03H (controlled)	0.011	0.62
CA-04 (controlled)	0.047	0.81
CA-05 (controlled)	0.072	0.88
CA-06 (controlled)	0.033	0.90
CA-07 (controlled)	0.034	0.90
CA-08 (controlled)	0.019	0.90
CA-09 (controlled)	0.019	0.90
CA-10 (uncontrolled)	0.108	0.29
CA-11 (uncontrolled)	0.016	0.63
Total	1.070	0.80

Table 6, below, summarizes post-development flow rates and required storage. Most of the roofs and asphalt parking area between buildings 1 and 2 will be controlled. The landscaped areas



along the north and west property lines will also be controlled. However, the landscaped area to the south and a small portion of the landscaped area at the northwest corner of the site, will remain uncontrolled.

Table 6: Summary of 100 Year Release Rates and Storage Requirements

Catchment	Drainage Area (ha)	100 Year Release Rate (L/s)	100 Year Required Storage(m ³)
CA-01 to CA-03 (cistern 1 controlled)	0.722	97.18	172.41
CA-04 to CA-09 (cistern 2 controlled)	0.224	32.39	50.79
CA-10 to CA-11 (uncontrolled)	0.124	25.42	N/A
Total	1.070	155.00	223.20

Stormwater management calculation shows, during 100-year storm, a total of

- **172.41 m³** of storage is required in Cistern 1 to attenuate the flow to **97.18 L/s**
- **50.79 m³** of storage is required in Cistern 2 to attenuate the flow to **32.39 L/s**

Refer to **Appendix G** for storage calculation details. The proposed cisterns will be installed within the underground parking area. Refer to Stormwater Management Plan C601 for the location of proposed cisterns.

The proposed development will utilize an Oil/Grit Separator (OGS) to achieve the required 80% TSS removal treatment, as specified by MVCA. The OGS will provide treatment for contaminated runoff from the surface parking lot prior to discharge into the roadside ditch. Specifically, the unit will be installed downstream of Cistern 2 to treat runoff collected from catchment areas CA-04 through CA-09. Runoff from roof areas (CA-01 & CA-02), and landscaped area (CA-03) is considered relatively clean and therefore does not require OGS treatment. The location of the proposed OGS is shown on Servicing Pan C401 (**Appendix E**).

15 EROSION & SEDIMENT CONTROL

During construction, best management practices (BMPs) shall be undertaken to Control Erosion and Sediment. These BMPs aim to minimize soil erosion, sedimentation, and other negative impacts on water quality and natural habitats. Some examples of BMPs for erosion and sediment control are:

- Controlling mud tracking by installing, maintaining, and using stabilized construction entrances and exits at all access locations. Mud mats shall be maintained and cleaned on a regular basis.
- Installing inlet sediment control devices to prevent surface erosion from entering any storm sewer system during construction; filter bags shall be placed under grates of nearby catch basins and structures.
- Establishing vegetation such as grasses and trees, can help stabilize soil and prevent erosion. In areas where vegetation is not present, consider planting native species that are well adapted to the local soil and climate conditions.



- Installing silt fences to trap sediment and prevent it from entering nearby waterways, to be erected along the perimeter of the site where runoff has the potential of leaving the site.
- Manage construction activities: Proper management of construction activities is essential to minimize soil disturbance and sedimentation. This may include controlling runoff from disturbed areas, using proper excavation techniques, and minimizing the amount of time that soil is exposed.
- Implement good housekeeping practices: This includes properly managing and disposing of waste materials, regularly maintaining equipment to prevent leaks and spills, and keeping work areas clean and free of debris. It is important to note that the specific BMPs used for erosion and sediment control may vary depending on the site conditions and project requirements. Therefore, it is important to ensure that the appropriate BMPs are selected and implemented for this site.
- A Light Duty Straw Bail Barrier is to be installed downstream of the development's storm outlet within the Ditch as per OPSD 219.100.

16 CONCLUSION

This Stormwater Management and Servicing Report for the development proposed at 6310 Hazeldean Road presents the rationale and details for the servicing requirements for the subject property. In accordance with the report objectives, the servicing requirements for the development are summarized below:

Water Service

- The contemplated development is proposed to be serviced via a **200mmØ** dual connections to the existing 406 mm diameter watermain within Hazeldean Road.
- The calculated total water demands are: **3.00 L/s** (average day demand), **7.15 L/s** (maximum daily demand), and **15.53 L/s** (maximum hourly demand).
- The maximum required fire flow was calculated at **13,000 L/min** using the FUS 2020 method.
- There are at least three (3) existing fire hydrants available to service the proposed development. They will provide a combined fire flow of **15,141 L/min** to the site.
- The hydraulic analysis confirms that adequate pressure is available to service the proposed development.

Sanitary Service

- The post-development total sanitary flow was calculated to be **9.29 L/s**, accounting for the proposed residential populations, commercial areas as well as extraneous flow allowance.
- The proposed development will be serviced via a 375 mm diameter sanitary sewer to be connected to the existing 450 mm diameter sanitary sewer located within the neighbouring easement southwest of the site.



Stormwater Management

- The stormwater runoff will be controlled to a pre-development 5-year release rate of **155.00 L/s** and accommodate **223.20 m³** of stormwater storage during the 100-year storm event.
- The required storage will be accommodated underground in two cisterns located near the northeast (Cistern#1) and southeast corner (Cistern#2) of the site.
- An OGS (Stormceptor EFO4 or approved equivalent) will be installed downstream of Cistern#2 to treat contaminated runoff to an enhanced quality treatment level (80% TSS removal).
- The subject site will outlet to the ditch within the easement located on the east side of the site.

17 REPORT CONDITIONS AND LIMITATIONS

The report conclusions are applicable only to this specific project described in the preceding pages. Any changes, modifications or additions will require a subsequent review by LRL Associates Ltd. to ensure compatibility with the recommendations contained in this document.

If you have any questions or comments, please contact the undersigned.

Prepared by:

LRL Associates Ltd.

Maxime Longtin

Maxime Longtin
Civil Engineering Technologist

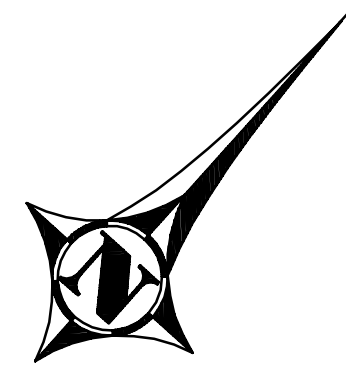


Mohan Basnet, P.Eng.
Civil Engineer



APPENDIX A
As-Built, Topographical Survey





PLAN OF TOPOGRAPHIC SURVEY
 OF PART OF
LOT 22
CONCESSION 12
GEOGRAPHIC TOWNSHIP
OF GOULBOURN
CITY OF OTTAWA

McINTOSH PERRY SURVEYING INC

SCALE 1 : 300

0 5 10 15 20 25 30 Metres

METRIC :
 DISTANCES AND COORDINATES SHOWN ON THIS PLAN ARE IN METRES AND CAN BE CONVERTED TO FEET BY DIVIDING BY 0.3048.

SURVEYOR'S CERTIFICATE

I CERTIFY THAT THIS SURVEY WAS COMPLETED ON APRIL 18, 2018.

DATE: BRIAN W. KERR
 ONTARIO LAND SURVEYOR

LEGEND AND NOTES

- DENOTES MONUMENT PLANTED
- DENOTES MONUMENT FOUND
- IB DENOTES IRON BAR
- SSIB DENOTES STANDARD IRON BAR
- RPL DENOTES SHORT STANDARD IRON BAR
- RIB DENOTES ROUND IRON BAR
- (m) DENOTES MEASURED
- (p) DENOTES PLAN 4R-23111
- (p2) DENOTES PLAN 4R-19395
- (647) DENOTES H.R. FARLEY, OLS
- (857) DENOTES FAIRHALL, MOFFATT & WOODLAND LIMITED
- (OU) DENOTES ORIGIN UNKNOWN
- N DENOTES NORTH
- S DENOTES SOUTH
- W DENOTES WEST
- ORP DENOTES OBSERVED REFERENCE POINT
- INV DENOTES INVERT
- OBV DENOTES OBVERT
- AN DENOTES ANCHOR
- HP DENOTES HYDRO POLE
- FH DENOTES FIRE HYDRANT
- WV DENOTES WATER VALVE
- MH DENOTES MANHOLE
- CSP DENOTES CORRUGATED STEEL PIPE
- ELEV. DENOTES ELEVATION
- CONC. DENOTES CONCRETE
- BM DENOTES BENCHMARK
- LS DENOTES LIGHT STANDARD
- COM BOX DENOTES COMMUNICATION BOX
- TS DENOTES TRAFFIC SIGNAL
- HH DENOTES HAND HOLE
- MH-TR DENOTES TRAFFIC MANHOLE
- MH-SAN DENOTES SANITARY MANHOLE
- T/G DENOTES TOP OF GRATE
- CULV. DENOTES CULVERT
- BPED DENOTES BELL PEDESTAL
- DS DENOTES DOOR SILL
- CB DENOTES CATCH BASIN

ELEVATIONS ARE CANADA GEODETIC VERTICAL DATUM 1928-1978 DERIVED FROM REAL TIME NETWORK GPS OBSERVATIONS WITH GEOD CORRECTION APPLIED.

SITE BENCHMARK 'A' - TOP OF SPINDLE OF FIRE HYDRANT, HAVING AN ELEVATION OF 124.68m.

SITE BENCHMARK 'B' - TOP OF SPINDLE OF FIRE HYDRANT, HAVING AN ELEVATION OF 125.26m.

SITE BENCHMARK 'C' - TOP OF SPINDLE OF FIRE HYDRANT, HAVING AN ELEVATION OF 125.50m.

DISTANCES SHOWN ON THIS PLAN ARE GROUND DISTANCES AND CAN BE CONVERTED TO GRID DISTANCES BY MULTIPLYING BY A COMBINED SCALE FACTOR OF 0.999909.

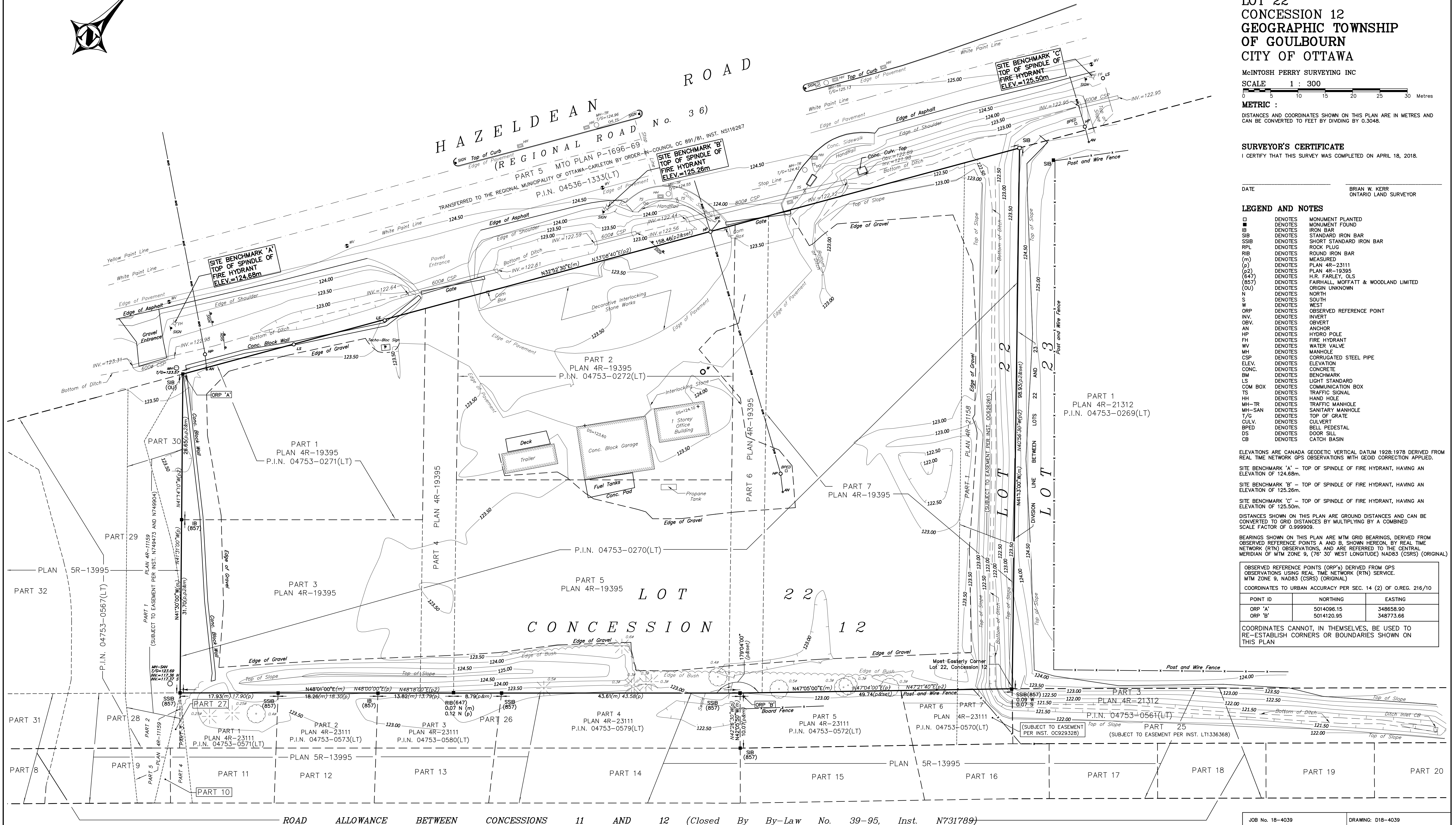
BEARINGS SHOWN ON THIS PLAN ARE MTM GRID BEARINGS, DERIVED FROM OBSERVED REFERENCE POINTS A AND B, SHOWN HEREON, BY REAL TIME NETWORK (RTN) OBSERVATIONS, AND ARE REFERRED TO THE CENTRAL MERIDIAN OF MTM ZONE 9, (76° 30' WEST LONGITUDE) NAD83 (CSRS) (ORIGINAL)

OBSERVED REFERENCE POINTS (ORP's) DERIVED FROM GPS OBSERVATIONS USING REAL TIME NETWORK (RTN) SERVICE. MTM ZONE 9, NAD83 (CSRS) (ORIGINAL)

COORDINATES TO URBAN ACCURACY PER SEC. 14 (2) OF O.REG. 216/10

POINT ID	NORTHING	EASTING
ORP 'A'	5014096.15	348658.90
ORP 'B'	5014120.95	348773.66

COORDINATES CANNOT, IN THEMSELVES, BE USED TO RE-ESTABLISH CORNERS OR BOUNDARIES SHOWN ON THIS PLAN



ROAD ALLOWANCE BETWEEN CONCESSIONS 11 AND 12 (Closed By By-Law No. 39-95, Inst. N731789)

CONCESSION 11

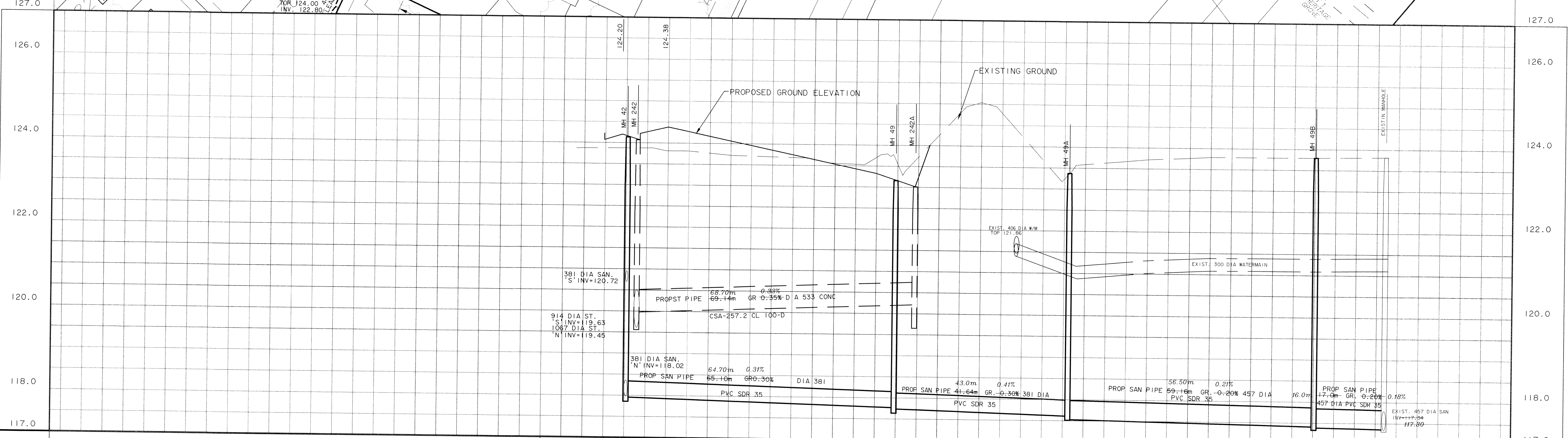
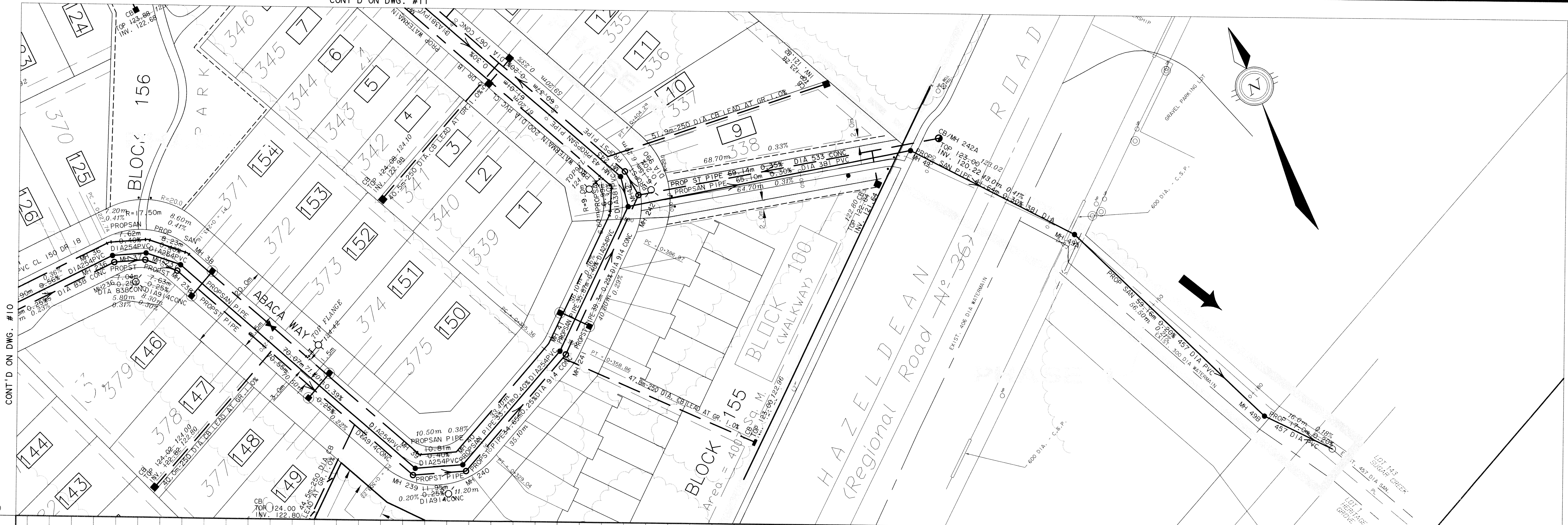
JOB No. 18-4039 DRAWING: D18-4039

THIS PLAN WAS PREPARED FOR: MPCE (Curtis Melanson)

McINTOSH PERRY SURVEYING INC.
 3240 Drummond Con. 5A, R.R. #7, Perth, ON K7H 3C9
 Tel: 613-267-6524 Fax: 613-267-7992
 www.mcintoshperry.com

EXAMINED: CHECK:

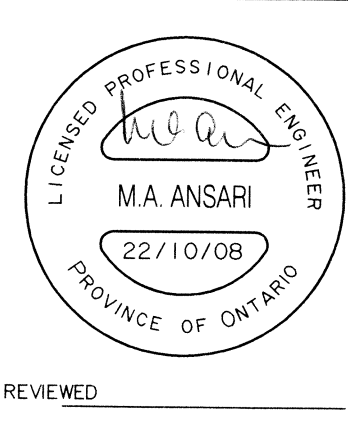
CONT'D ON DWG. #11



0+000	0+015.2	0+020.4	0+023.3	0+030	0+060	0+084.14	0+089.3	0+090	0+120	0+150	0+180	0+185.2	0+202	0+210	

RECORD DRAWING
DATE: 01/05/02

NO.	REVISIONS	DATE	BY	APP'D
3	RECORD DRAWING	01/05/02	ABZ	AA
2	REVISED AS PER CITY COMMENTS NOV21/01 & LOT REVISIONS ON ABACA WAY	30/11/01	GBU	SJC
1	REVISED AS PER CITY COMMENTS OCT22/01 & LOT REVISIONS ON ABACA WAY	12/11/01	GBU	SJC



CLIENT: CBA RIDEAU (STITTSVILLE) LTD.
 PROJECT: TIMBERMERE - PHASE 2 & 3
 TITLE: SANITARY EASEMENT

DESIGN: S. J.C.
 DRAWN: G.B.U.
 CHECKED: M.J.C.

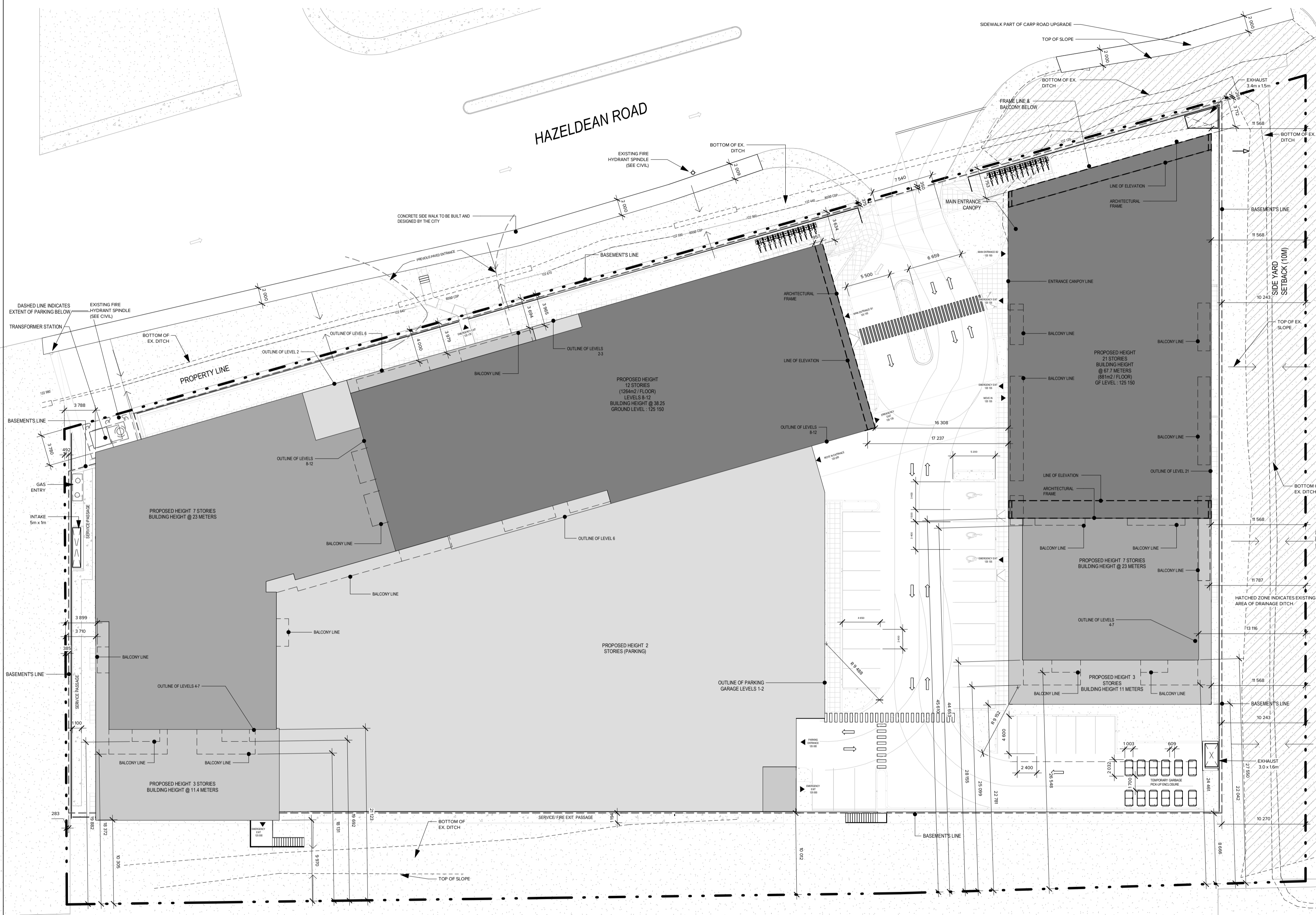
DATE: SEPTEMBER 2001
 SCALE: HORIZ 1:500
 VERT 1:50

DRAWING NO. MP14886A
 SHEET 13 OF 2

CONSULTING ENGINEERS
 HYDROGEOLOGISTS & PLANNERS
 154 COLONNADE RD. SOUTH NEPEAN ONT.
Trow

APPENDIX B
Site Plan





1 SITE PLAN - SPA
A-025
ÉCHELLE: 1 : 300

CLIENT
FELIX ALLAIRE
4329163 CANADA INC.
6310 HAZELDEAN ROAD
P.O. BOX 1791
STITTSVILLE, ON K2S 1B4

CONSULTANTS

PLANNER
PATRICIA WARREN
FOTENN PLANNING
420 O'CONNOR STREET, OTTAWA, ON K2P 1W4

ARCHITECT
MAXIME FRAPPIER
ACDF ARCHITECTURE
201, 6250 RUE HUTCHISON, MONTREAL, QUEBEC H2V 4C3

CIVIL ENGINEER
MAXIME LONGTIN
5430 CANOTEK RD, OTTAWA, ON
SURVEYOR

PROJECT DESCRIPTION:

PROPOSED DESIGN	2 RESIDENTIAL BUILDING
BUILDING 01	12 STOREY
BUILDING 02	21 STOREY
BUILDING 03	21 STOREY
LOCAL AUTHORITY	CITY OF OTTAWA
PNL NUMBER	14753/076, 0771, 0272
MUNICIPAL ADDRESS	6310 HAZELDEAN ROAD
SITE INFORMATION:	
LOT AREA	12,018m ²
LOT FRONTAGE	152m
LOT DEPTH	78.9m

BUILDINGS INFORMATION:

BUILDING AREA 01	5,030m ²
BUILDING AREA 02	1,325m ²
BUILDING FLOOR AREA ABOVE GRADE	
BUILDING 01 PROPOSED USE	HIGH-RISE DWELLING UNITS
BUILDING 02 PROPOSED USE	HIGH-RISE DWELLING UNITS
BUILDING 03 NUMBER OF UNITS	248
BUILDING 02 NUMBER OF UNITS	209
TOTAL NUMBER OF UNITS	457

PROJECT ZONING BY LAW AND APPLICABLE BUILDING CODE:

ZONING TABLE	AMR(2102) S501 Provisions	PROPOSED
MINIMUM LOT AREA	No minimum	12,014m ²
MINIMUM LOT WIDTH	No minimum	154m
MINIMUM FRONT YARD SETBACK	3m	Building 01: 0.3 m Building 02: 0.3 m Building 03 (West): 0.2 m Building 02 (East): 10.2 m Building 02 (West): N/A
MINIMUM REAR YARD SETBACK	10m	8.2 m
MINIMUM BUILDING HEIGHT	Area A: 41 m Area B: 67.7 m Area C: 24 m Area D: 11.4 m Area E: 0 m Area F: 0 m	Area A: 38.25 m Area B: 65.15 m Area C: 23 m Area D: 11.4 m Area E: 0 m Area F: 11.5 m
MINIMUM SETBACK ABOVE 4 th FLOOR FOR ANY PORTION OF A BUILDING 10 FLOOR OR MORE	N/A	Building 1: 1.5 m Above the 6 th floor for a portion of building, no set back for remainder Building 2: 0 m (no setback is proposed)
MINIMUM FLOOR SPACE INDEX	N/A	N/A
AMENITY AREA	Total 6 m ² / Dwelling units (2,736 m ²) Communal: 50% of the required total amenity area (1,368 m ²)	Building 01 Private Amenities: 1191.51m ² Building 02 Private: 2415.29 m ² Total Private Amenities: 3606 m ² Internal Communal Amenities: 951 m ² External Communal Amenities: 2383.3 m ² Total Communal Amenities: 2914.3 m ²
MINIMUM LOT AREA FOR HIGH-RISE BUILDINGS	1800 m ²	12014 m ²
MINIMUM INTERIOR SIDE AND REAR YARD SETBACK	11.5 m	11.5 m
MINIMUM SEPARATION DISTANCE BETWEEN TOWERS ON THE SAME LOT	19 m	17 m
ORNAMENTAL ELEMENTS SUCH AS SILL, RELI COURSES, CORNICES, PARAPETS AND PILASTERS	0.6 m, but not closer than 0.6 m to a lot line	Building 1: 1 m Building 2: 2.2 m
MINIMUM VEHICLE PARKING SPACE RATE	0.75 spaces/ unit (343 spaces)	368 spaces
VEHICLE PARKING SIZE	2.6 m wide x 5.2 long 50% of spaces may be reduced to 2.4 m x 4.6 m for compact cars	360 (2.6 m x 5.2 m), 90 (2.4 m x 4.6 m), 6 (Accessible type A) and 6 (Accessible type B) Total: 450
MINIMUM VISITOR PARKING SPACE	0.2 spaces/ units (91.6 spaces)	92 spaces (2.6 m x 5.2m)
MINIMUM ASLE AND DRIVEWAY SIZE	Asile: 6 m Driveway (double traffic): min: 6 m Max: 6.7 m	6m
MINIMUM LANDSCAPING PROVISIONS FOR PARKING LOTS	15% of the area of any parking lot provided as perimeter of interior landscape area	Provided

OUTDOOR REFUGE	1.5 m landscape buffer	Provided
Section 110	Located 3 m (minimum) from a lot line Screened from view by an opaque screen with a height of 2 m	East setback 12.6 m South (Rear) setback 9 m
MINIMUM BICYCLE PARKING SPACE RATE	1 Space dwelling unit (457 spaces)	457 spaces
LOCATION OF BICYCLE PARKING SPACES	A maximum of 50% of the required bicycles spaces or 15 spaces which ever is greater may be in a landscape area	24 bicycles spaces for visitors in landscape area
MINIMUM BICYCLE PARKING SPACE PROVISIONS	Vertical: 0.5 m x 1.5 m Stacked: 0.37 m x 1.8 m Asile: 1.5 m	Horizontal: 0.6 m x 1.8 m provided Vertical: 0.5 m x 1.5 m Asile: 1.5 m provided

PROJECT STATISTICS:

GFA Calculation - (Zoning by Law Part 1 - Definitions)

Building 01:	
GROUND FLOOR	1058 m ²
2 nd FLOOR	1245 m ²
3 rd FLOOR	1181 m ²
4 th FLOOR	1186 m ²
5 th FLOOR	1805 m ²
6 th FLOOR	1886 m ²
7 th FLOOR	1881 m ²
8 th FLOOR	1047.40 m ²
9 th FLOOR	1047.40 m ²
10 th FLOOR	1047.40 m ²
11 th FLOOR	1047.40 m ²
12 th FLOOR	1047.40 m ²
TOTAL	16,889 m ²
Building 02:	
GROUND FLOOR	721.3 m ²
2 nd FLOOR	1129 m ²
3 rd FLOOR	1200 m ²
4 th FLOOR	1043 m ²
5 th FLOOR	1047 m ²
6 th FLOOR	1047 m ²
7 th FLOOR	1047 m ²
8 th FLOOR	780 m ²
9 th FLOOR	780 m ²
10 th FLOOR	780 m ²
11 th FLOOR	780 m ²
12 th FLOOR	780 m ²
13 th FLOOR	780 m ²
14 th FLOOR	780 m ²
15 th FLOOR	780 m ²
16 th FLOOR	780 m ²
17 th FLOOR	780 m ²
18 th FLOOR	780 m ²
19 th FLOOR	780 m ²
20 th FLOOR	780 m ²
21 st FLOOR	780 m ²
TOTAL	18154.3 m ²

UNIT MIX:

BUILDING 01	STUDIO	1 BEDROOM	3 BEDROOM	3 BEDROOM
BUILDING 02	33	142	67	6
TOTAL	12	303	173	36
TOTAL	45	205	173	36

CAR PARKING BREAKDOWN:

REGULAR PARKING 2.6m x 5.2m	288
SMALL PARKING (COMPACT) 2.4m x 4.2m	88
ACCESSIBLE TYPE A 3.4m x 5.2m	6
ACCESSIBLE TYPE B 2.3 m x 5.2m	6
VISITORS PARKING 2.6m x 5.2m	92
TOTAL	480

BICYCLE BREAKDOWN:

INTERIOR BICYCLE SPACE	433
EXTERIOR BICYCLE SPACE	24
TOTAL	457

OUTDOOR REFUGE:

Section 110	1.5 m landscape buffer	Provided
Section 111	Located 3 m (minimum) from a lot line Screened from view by an opaque screen with a height of 2 m	East setback 12.6 m South (Rear) setback 9 m

MINIMUM BICYCLE PARKING SPACE RATE: 1 Space dwelling unit (457 spaces)

LOCATION OF BICYCLE PARKING SPACES: A maximum of 50% of the required bicycles spaces or 15 spaces which ever is greater may be in a landscape area

MINIMUM BICYCLE PARKING SPACE PROVISIONS: Vertical: 0.5 m x 1.5 m
Stacked: 0.37 m x 1.8 m
Asile: 1.5 m

MINIMUM VISITOR PARKING SPACE: 0.2 spaces/ units (91.6 spaces)

MINIMUM ASLE AND DRIVEWAY SIZE: Asile: 6 m
Driveway (double traffic): min: 6 m
Max: 6.7 m

MINIMUM LANDSCAPING PROVISIONS FOR PARKING LOTS: 15% of the area of any parking lot provided as perimeter of interior landscape area

OUTDOOR REFUGE: 1.5 m landscape buffer
Section 110: Located 3 m (minimum) from a lot line
Screened from view by an opaque screen with a height of 2 m
Section 111: Located 3 m (minimum) from a lot line
Screened from view by an opaque screen with a height of 2 m

MINIMUM BICYCLE PARKING SPACE RATE: 1 Space dwelling unit (457 spaces)

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Asile: 1.5 m

MINIMUM VISITOR PARKING SPACE: 0.2 spaces/ units (91.6 spaces)

MINIMUM ASLE AND DRIVEWAY SIZE: Asile: 6 m
Driveway (double traffic): min: 6 m
Max: 6.7 m

MINIMUM LANDSCAPING PROVISIONS FOR PARKING LOTS: 15% of the area of any parking lot provided as perimeter of interior landscape area

THE CONTRACTOR IS RESPONSIBLE FOR THE VERIFICATION AND COORDINATION OF ALL CONSTRUCTION AND SITE LAYOUT DIMENSIONS. THE CONTRACTOR SHALL NOTIFY THE ARCHITECT OF ANY IRREGULARITY, OMISSION OR DIVERGENCE BETWEEN THESE DOCUMENTS, THOSE OF THE OTHER PROFESSIONALS, AND THE CONDITIONS OBSERVED ON SITE. NO DIMENSION SHALL BE SCALED FROM THE DRAWINGS.

ALL CONSTRUCTION WORK MUST COMPLY WITH THE CURRENT EDITION OF THE LOCAL/ PROVINCIAL CONSTRUCTION CODE WHERE THE CONSTRUCTION IS TAKING PLACE.

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THIS DOCUMENT MUST NOT BE USED FOR CONSTRUCTION PURPOSES

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Solutions structurales
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MONTREAL (QC), H3L 1B7

1 SPA REVISION 01	ÉMISSION	XX-XX-XXXX	PAR
NO.	ÉMISSION	DATE	PAR

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F : 514 288-0418
St-Hyacinthe
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QC J2S 2Z7
T : 450 778-1151
F : 450 778-1594

PROJECT
SCALIA
STITTSVILLE-HAZELDEAN
6310 Hazeldean Rd, Ottawa, ON K2S 0T2

DRAWING
SITE PLAN

SCAUC
DOSSIER / NUMBER
25-1839
DESSIN / DRAWING NO.
A-025
RÉV. NO.
1
DATE
OCTOBER 2025
ÉCHELLE / SCALE
1 : 300
DESIGNÉ PAR / DRAWN BY
FM
VÉRIFIÉ PAR / VERIFIED BY
FM

APPENDIX C
Pre-con Meeting Notes



Pre-Application Consultation Meeting Notes

2:00pm to 3:00pm, November 17, 2021, via Microsoft Teams
Property Address: 6310 Hazeldean Road
File No.: PC2021-0388

Attendees:

Laurel McCreight – Planner, City of Ottawa
Matthew Ippersiel – Urban Designer, City of Ottawa
Justin Armstrong – Project Manager (Infrastructure), City of Ottawa
Josiane Gervais – Project Manager (Transportation), City of Ottawa
Jeffrey Ren – Co-op Student, City of Ottawa
Mark Richardson – Planning Forester, City of Ottawa
Erica Ogden – MVCA
Miguel Tremblay – Fotenn
Rejane Padaratz – Fotenn
Tana Klein – Fotenn
Michael Uberti – Property Owner
Marco Recine – Property Owner

Regrets:

Jaime Posen – Fotenn
Kersten Nitsche – Parks Planner, City of Ottawa

Applicant's Proposal:

- To construct three nine-storey mixed-use buildings with ground floor commercial units. A total of approximately 317 dwelling units are proposed. 2,282 m² of commercial space and 33,544 m² of residential space will be provided along with approximately 96 surface parking spaces and an undetermined number of underground parking spaces, most of the site will have underground parking.

Preliminary comments and questions from staff and agencies, including follow-up actions:

Transportation

- Follow Transportation Impact Assessment Guidelines
 - A TIA is required. Submit a Screening Form at your earliest convenience to josiane.gervais@ottawa.ca.
 - TIAs in support of rezoning must demonstrate the worst-case scenario traffic generated from the zoning being sought.
 - Start this process asap. The application will not be deemed complete until the submission of the draft step 1-4.

- An update to the *TRANS Trip Generation Manual* has been completed (October 2020). This manual is to be utilized for this TIA. A copy of this document can be provided upon request.
- ROW protection on Hazeldean between Stittsville west urban limit and Carp Road is 37.5m even.
- TMP identifies Hazeldean Road as a cycling Spine Route.
- The following notes are provided for information and will be applicable at the time of SPA:
 - TIA would require an update to include the Network Design Component Modules of the TIA.
 - If modifications are required to the traffic signal, this would trigger an RMA.
 - Ensure site access meets the City's Private Approach Bylaw.
 - Ensure site access throat length can adequately accommodate forecast traffic volumes.
 - Provide concrete sidewalk along Hazeldean Rd.
 - Show all details of the roads abutting the site up to and including the opposite curb; include such items as pavement markings, accesses and/or sidewalks.
 - Turning movement diagrams required for all accesses showing the largest vehicle to access/egress the site.
 - Turning movement diagrams required for internal movements (loading areas, garbage).
 - Show all curb radii measurements; ensure that all curb radii are reduced as much as possible and fall within TAC guidelines (Figure 8.5.1).
 - Show dimensions for site elements (i.e. lane/aisle widths, access width and throat length, parking stalls, sidewalks, pedestrian pathways, etc.)
 - Sidewalk is not to be continuous across access as per City Specification 7.1.
 - Show slope of garage ramp on site plan. Note that underground ramps should be limited to a 12% grade and must contain a subsurface melting device when exceeding 6%. Ramp grades greater than 15% can be psychological barriers to some drivers.
 - As the proposed site is commercial/institutional/industrial and for general public use, AODA legislation applies. Consider using the City's Accessibility Design Standards.
 - Ensure all crosswalks located internally on the site provide a TWSI at the depressed curb, per requirements of the Integrated Accessibility Standards Regulation under the AODA.

- Parking stalls at the end of dead-end parking aisles require adequate turning around space.
- Grey out any area that will not be impacted by this application.

Please contact Transportation Project Manager Josiane Gervais (Josiane.Gervais@ottawa.ca) for follow-up questions.

Infrastructure

- The Servicing Study Guidelines for Development Applications are available at the following address: <http://ottawa.ca/en/development-application-review-process-0/servicing-study-guidelines-development-applications>
- Servicing and site works shall be in accordance with the following documents:
 - ⇒ Ottawa Sewer Design Guidelines (October 2012)
 - ⇒ Ottawa Design Guidelines – Water Distribution (2010)
 - ⇒ Geotechnical Investigation and Reporting Guidelines for Development Applications in the City of Ottawa (2007)
 - ⇒ City of Ottawa Slope Stability Guidelines for Development Applications (revised 2012)
 - ⇒ City of Ottawa Environmental Noise Control Guidelines (January, 2016)
 - ⇒ City of Ottawa Park and Pathway Development Manual (2012)
 - ⇒ City of Ottawa Accessibility Design Standards (2012)
 - ⇒ Ottawa Standard Tender Documents (latest version)
 - ⇒ Ontario Provincial Standards for Roads & Public Works (2013)
- Record drawings and utility plans are also available for purchase from the City (Contact the City's Information Centre by email at InformationCentre@ottawa.ca or by phone at (613) 580-2424 x.44455).
- Hazeldean Road was resurfaced in 2019 and the road is under a 3-year Road-Cut moratorium into 2022. As such, any road cuts into Hazeldean that are to be made prior to the lifting of the moratorium will be subject to increased fees and higher reinstatement standards. The exact timeline for moratorium lifting can be explored once a formal submission is made.

Storm

- The Stormwater Management Criteria, for the subject site, is to be based on the following:

- i. The 5-yr storm event using the IDF information derived from the Meteorological Services of Canada rainfall data, taken from the MacDonald Cartier Airport, collected 1966 to 1997.
 - ii. The pre-development runoff coefficient or a maximum equivalent 'C' of 0.5, whichever is less (§ 8.3.7.3).
 - iii. A calculated time of concentration (Cannot be less than 10 minutes).
 - iv. Flows in excess of the 5-year storm release rate, up to and including the 100-year storm event, must be detained on site.
 - v. The stormwater outlet for the site is the ditch that crosses the site at the eastern limit.
 - vi. No ponding on drive aisles and parking areas is permitted during the 2-year event.
 - vii. SWM calculations using the modified rational method is acceptable, however, if a combination of surface ponding and underground storage is used, the consultant is reminded to either: (a) use a dynamic computer model or (b) use the modified rational method assuming an average release rate of 50% of the area-specific peak flow rate where above and below ground storage is provided.
- It has been confirmed that there is a 10m wide existing drainage easement OC626261 in place at the site's eastern limit and that this easement is in favour of the City of Ottawa. The conditions set out in the easement must be respected. One of the most important conditions is unimpeded access. The last time the ditch was cleaned a triaxle, large shovel, mini excavator and a bobcat were all used. The full 10m was used then. The City's Operations Branch can be circulated for further comment once a formal application is submitted.
 - Note that the City's Operations branch has previously been contacted regarding the piping of the drainage ditch along the east property boundary. They provided the following in response: Piping of the drainage ditch may be acceptable as long as a thorough SWM assessment is provided for the system up-to and including the downstream DICB. Regardless of the site's portion of the drainage ditch being piped, City operations would still be responsible to maintain the portion of ditch downstream. Also note that due to the past historic flooding issues for this area the City opposes a reduction in the easement width. Further, drainage maintenance staff also indicated that due to rear yard flooding history at a property on Kyle Ave related to the easement and ditch on 6310 Hazeldean, if piping is proposed, the ditch will need to be piped along the site and through other properties to the downstream DICB.

Sanitary

- The available sanitary sewer is located west of the site on the neighbouring property within an easement in favour of the City of Ottawa. If sanitary service is proposed to connect to this sewer section, an easement with the neighbouring property will be required. This is the City's preferred method of connection for this site.
- The City's Asset Management Branch and Sewer Operations Branch have confirmed that, alternatively, connection can be made to the maintenance hole located within the Hazeldean road boulevard. The preferred connection method under this alignment would be for the owner to provide a small sewer extension in the Hazeldean ROW. The sewer extension would be a standard sewer extension and would require MECP ECA approval. The City would eventually assume ownership of the sewer within the ROW. The connection should be made obvert to obvert with the outlet pipe.
- A monitoring maintenance hole shall be required just inside the property line for all non-residential and multi residential buildings connections from a private sewer to a public sewer. The maintenance hole should be located in an accessible location on private property near the property line (i.e., not in a parking area).

Water

- Water Frontage fees may apply if they have not already been paid.
- In order to avoid the creation of a vulnerable service area (VSA) water service redundancy is required if there are more than 49 dwellings/units proposed and/or there is more than 50m³/day of basic day demand.
- The City's Water Meter Group will only accept a single City water meter per property parcel. For multi-building parcels, all buildings can be privately sub metered, however each building should obtain their water supply downstream of the single City water meter
- Water Boundary condition requests must include the location of the service and the expected loads required by the proposed development. Please provide the following information to the Infrastructure Approvals Project Manager:
 - i. GeoOttawa Snippet showing proposed location of service.
 - ii. Type of development and the amount of fire flow required as per ISTB-2021-03 Section 4.2.11.
 - iii. Average daily demand: ___ l/s.
 - iv. Maximum daily demand: ___ l/s.
 - v. Maximum hourly daily demand: ___ l/s.

MECP

- MECP ECA Requirements
- An MECP Environmental Compliance Approval (Private Sewage Works) will be required for the proposed development if the proposal does not meet exemption requirements as outlined in MECP O.Reg 525/989 (3).
- Phase 1 ESAs and Phase 2 ESAs must conform to clause 4.8.4 of the Official Plan that requires that development applications conform to Ontario Regulation 153/04.

Please contact Infrastructure Project Manager Justin Armstrong (Justin.Armstrong@ottawa.ca) for follow-up questions.

MVCA

- The subject property is located within the Poole Creek Subwatershed and is within the Carp River Watershed Subwatershed Plan, which required an annual infiltration rate of 104mm/yr for areas within moderate groundwater recharge.
- The water quality requirement is an enhanced level of protection which requires 80% total suspended solids removal.
- Poole Creek is a cold-cool water system; therefore, temperature mitigation should be incorporated into the stormwater management design.
- For a Zoning By-law Amendment is applied for initially, the stormwater report can be scoped to demonstrate that the above criteria can be achieved on site with the detailed design to follow with Site Plan Control.

Please contact MVCA Planner Erica Ogden (eogden@mvc.on.ca) for follow-up questions.

Urban Design

- Site Organization & Massing
 - Please reorient the middle building to have the front facade follow the geometry of Hazeldean Road. This is supported by the direction of the New Official Plan, the Zoning By-law and the Urban Design Guidelines for Arterial Mainstreets.
 - The space between the two long nine-storey facades will likely create an uncomfortable space. The central building should be shifted to the west and it would be preferable for its footprint to be reconfigured as a “bar” building rather than an “L-shaped” building. If a bar building cannot be achieved, shorten the “arm” of the building from the 46.7m length currently proposed.
- Open Space and Connectivity
 - The inclusion of the POPS/plaza is appreciated, but the space should be relocated to the interior of the site. This would improve access to sunlight, make for a more comfortable, enclosed space, bring needed greening into the courtyard, and could have a better interface with the retail at grade.

- Narrow the pedestrian mid-block connection by shifting the central building footprint to the west and reallocate the space to the east side of the central building. The concept of a mid-block pedestrian connection is supported, but a more valuable location for a strong pedestrian connection would be on the east of the central building, where it can be aligned with the crosswalk on Hazeldean. This will also increase space for wider sidewalks, trees and landscaping, and provide a more prominent “gateway” to the site and greater separation between building facades.
- Ensure that strong and safe pedestrian connections are provided throughout the site.
- Other Design Considerations
 - Reconsider the locations of the garbage enclosures. They should be internalized into the buildings or relocated to the space south of the buildings.
 - Ensure that impacts on the established low-rise residential neighbourhood to the south are minimized. The stepping of the massing is good in this respect. Increase the width of the planting strip along the southern property line and maintain as many existing trees as possible.
- Urban Design Review Panel
 - A Formal Review with the City’s Urban Design Review Panel (UDRP) is required. Please contact the Panel Coordinator to schedule the meeting.
 - Providing the coordinator with an early “heads-up” as to which meeting is being targeted, once it is known, is recommended. A full list of upcoming panel meeting dates, submission deadlines and other information can be found on the UDRP website.
 - Note that a second Formal review with the Panel will be required at the Site Plan Control stage.
- Design Brief
 - A scoped Urban Design Brief is required as a part of your submission. This may be combined with your Planning Rationale report. Please refer to the attached Urban Design Brief Terms of Reference to inform the content of the brief.

Please contact Urban Designer Matthew Ippersiel (Matthew.Ippersiel@ottawa.ca) for follow-up questions.

Parks

- Pursuant to Section 3 and Section 10(1) Parkland Dedication By-law 2009-05, as amended, at the time of Site Plan Control, cash-in-lieu of parkland shall be paid by the Owner as follows:
 - Residential: Uplift of units on the site, not to exceed 10% of the land area of the site
 - Commercial: 2% of site area

- For mixed use development, the parkland requirement for each use will be based upon the above rates prorated proportionately to the GFA allocated to each use

Please contact Parks Planner Kersten Nitsche (Kersten.Nitsche@ottawa.ca) for follow-up questions.

Forestry

TCR Requirements

- A Tree Conservation Report (TCR) must be supplied for review along with the suite of other plans/reports required by the City
- An approved TCR is a requirement of Site Plan approval.
- The TCR may be combined with the LP provided all information is supplied
- As of January 1, 2021, any removal of privately-owned trees 10cm or larger in diameter, or publicly (City) owned trees of any diameter requires a tree permit issued under the Tree Protection Bylaw (Bylaw 2020 – 340); the permit will be based on an approved TCR and made available at or near plan approval.
- The Planning Forester from Planning and Growth Management as well as foresters from Forestry Services will review the submitted TCR
- If tree removal is required, both municipal and privately-owned trees will be addressed in a single permit issued through the Planning Forester
- Compensation may be required for city owned trees – if so, it will need to be paid prior to the release of the tree permit
- The TCR must list all trees on site, as well as off-site trees if the CRZ extends into the developed area, by species, diameter and health condition
- please identify trees by ownership – private onsite, private on adjoining site, city owned, co-owned (trees on a property line)
- the TCR must list all trees on adjacent sites if they have a critical root zone that extends onto the development site
- If trees are to be removed, the TCR must clearly show where they are, and document the reason they cannot be retained
- All retained trees must be shown and all retained trees within the area impacted by the development process must be protected as per City guidelines available at [Tree Protection Specification](#) or by searching Ottawa.ca
- the location of tree protection fencing must be shown on a plan
- show the critical root zone of the retained trees
- if excavation will occur within the critical root zone, please show the limits of excavation

- the City encourages the retention of healthy trees; if possible, please seek opportunities for retention of trees that will contribute to the design/function of the site.
- For more information on the process or help with tree retention options, contact Mark Richardson mark.richardson@ottawa.ca or on [City of Ottawa](#)

LP Tree Planting Requirements

- For additional information on the following please contact tracy.smith@Ottawa.ca
- Minimum Setbacks
 - Maintain 1.5m from sidewalk or MUP/cycle track.
 - Maintain 2.5m from curb
 - Coniferous species require a minimum 4.5m setback from curb, sidewalk or MUP/cycle track/pathway.
 - Maintain 7.5m between large growing trees, and 4m between small growing trees. Park or open space planting should consider 10m spacing.
 - Adhere to Ottawa Hydro's planting guidelines (species and setbacks) when planting around overhead primary conductors.
- Tree specifications
 - Minimum stock size: 50mm tree caliper for deciduous, 200cm height for coniferous.
 - Maximize the use of large deciduous species wherever possible to maximize future canopy coverage
 - Tree planting on city property shall be in accordance with the City of Ottawa's Tree Planting Specification; and include watering and warranty as described in the specification (can be provided by Forestry Services).
 - Plant native trees whenever possible
 - No root barriers, dead-man anchor systems, or planters are permitted.
 - No tree stakes unless necessary (and only 1 on the prevailing winds side of the tree)
- Hard surface planting
 - Curb style planter is highly recommended
 - No grates are to be used and if guards are required, City of Ottawa standard (which can be provided) shall be used.
 - Trees are to be planted at grade
- Soil Volume
 - Please ensure adequate soil volumes are met:

Tree Type/Size	Single Tree Soil Volume (m3)	Multiple Tree Soil Volume (m3/tree)
Ornamental	15	9
Columnar	15	9
Small	20	12
Medium	25	15
Large	30	18
Conifer	25	15

- Please note that these soil volumes are not applicable in cases with Sensitive Marine Clay.

Sensitive Marine Clay

- Please follow the City's 2017 Tree Planting in Sensitive Marine Clay guidelines

Please contact Planning Foresters Mark Richardson (Mark.Richardson@ottawa.ca) and Tracey Smith (Tracey.Smith@ottawa.ca) for follow-up questions.

Planning

- Please note that the New Official Plan was approved by City Council on October 27, 2021 and is subject to review by the Ministry of Municipal Affairs and Housing with approval anticipated in February 2022; the application is expected to fall under the New Official Plan.
- Please review all applicable Official Plan policies when they become available to ensure that the proposed development complies with the policies of the New Official Plan.
- Minimum-density requirements as identified in Table 3a will apply (Minimum 120 People and Jobs per Gross Hectare and Dwellings per Net Hectare, minimum 5% and targeted 10% Large-household Dwellings). Please perform the necessary calculations to ensure that the density requirements of the New Official Plan are being met.
- Please address urbanization of Hazeldean Road. If this section of road is not urbanized, please consider how the treatment of your frontage should be handled to ensure there is adequate room for tree planting.
- Please ensure that a 5-metre-wide landscaped buffer is provided along the rear lot line; if a reduction is sought, please rationalize why a 5-metre-wide landscaped buffer cannot be provided. Although there is a vegetation behind the site, fencing may be appropriate given the rear yard condition of the abutting lots. Please note that the provisions of Urban Exception 2102 are specific to the previously existing garden centre and building supply outlet.
- Please consider aligning the middle building with Hazeldean Road, this will ensure that 50% of the lot width within 3 metres of the front lot line is occupied by building walls.
- A privately owned publicly accessible space may not be appropriate along Hazeldean Road – Hazeldean Road is a busy arterial road, and an alternative placement of the POPS/amenity space may be more welcoming. An amenity area behind the middle building may be more appropriate.

- Please ensure that a sufficient number of visitor parking spaces are provided, the surrounding residential neighbourhood has been vocal about their concerns regarding spillover parking.
- Please note that the subject property is not on a transit priority corridor – if there are any parking reductions that are proposed, it will need to be rationalized in the Planning Rationale.
- Garbage pickup should be internalized within the building.
- Please note that the Ottawa Fire Service (OFS) does not approve a fire route that goes over a parking garage structure. If the applicant wishes to pursue this layout, they will have to build the parking garage deck to bridge standard (15 kPa) and provide a stamped letter from an architect/engineer that it has been designed and built to this requirement. This letter will have to be provided to OFS after completion for our records. Additionally, some signage will have to be installed at the site indicating where the edge of the parking structure begins and that it has been designed to meet OFS requirements.
- Please review the [Urban Design Guidelines for Development along Arterial Mainstreet](#) for general design guidance.
- Please reach out to Councillor Glen Gower (Glen.Gower@ottawa.ca) so that the Ward Councillor is aware of the plans for the site.
- A Minor Zoning By-law Amendment application will be required to permit an increased height, please find the application form and information on fees [here](#).
- The application will be subject to public consultation (conducted through the posting of on-site signage, the notification of community groups, and through the City of Ottawa's DevApps website); the statutory public meeting for Zoning By-law Amendments is Planning Committee, however, please note that the Councillor may also ask for a Community Information and Comment Session.

Please contact File Lead Laurel McCreight (Laurel.McCreight@ottawa.ca) for follow-up questions.

Other

Please refer to the links to the [guide to preparing studies and plans](#) and [development application fees](#) for general information. Additional information is available related to [building permits](#), [development charges](#), and [the Accessibility Design Standards](#). Be aware that other fees and permits may be required, outside of the development review process. You may obtain background drawings by contacting informationcentre@ottawa.ca.

These pre-consultation comments are valid for one year. If you submit a development application(s) after this time, you may be required to meet for another pre-consultation meeting and/or the submission requirements may change. You are as well encouraged to contact us for a follow-up meeting if the plan/concept will be further refined.

APPENDIX D
Water Demand Calculations
Boundary Conditions
Fire Hydrant Coverage





Water Supply Calculations

LRL File No. 220027
 Date 2025-10-24
 Prepared by Sarthak Vora
 Project 6310 Hazeldean Road

Water Demand based on the City of Ottawa Design Guidelines-Water Distribution, 2010

Domestic Demand				
Unit Type	Persons Per Unit	Number of Units		Population
		Building 1	Building 2	
Studio	1.4	33	12	63
1 Bedroom Apartment	1.4	142	63	287
2 Bedroom Apartment	2.1	67	106	363.3
3 Bedroom Apartment	3.1	6	28	105.4
	Total	248	209	818.7

Average Water Consumption Rate	280 L/c/d	(As identified in the Technical Bulletin ISTB-2021-03)
Average Day Demand	229,236 L/d	2.65 L/s
Maximum Day Factor	2.5	(Table 4.2 - City of Ottawa Guidelines - Water Distribution)
Maximum Daily Demand	573,090 L/d	6.63 L/s
Peak Hour Factor	2.2	(Table 4.2 - City of Ottawa Guidelines - Water Distribution)
Maximum Hour Demand	1,260,798 L/d	14.59 L/s

Institutional / Commercial / Industrial Demand					
Demand Type	Unit	Rate	Units		Demand (L/d)
Commercial	28000	L/ha/d	1.07	ha	29960.0

Average Day Demand	29,960 L/d	0.347 L/s
Maximum Day Factor	1.5	(Table 4.2 - City of Ottawa Guidelines - Water Distribution)
Maximum Daily Demand	44,940 L/d	0.520 L/s
Peak Hour Factor	1.8	(Table 4.2 - City of Ottawa Guidelines - Water Distribution)
Maximum Hour Demand	80,892 L/d	0.936 L/s

TOTAL DEMAND				
Average Day Demand	259,196 L/d	3.00 L/s		
Maximum Daily Demand	618,030 L/d	7.15 L/s		
Maximum Hour Demand	1,341,690 L/d	15.53 L/s		

Water Service Pipe Sizing

$$Q = VA$$

Where: V = velocity
 A = area of pipe
 Q = flow rate

Assuming a maximum velocity of 1.8m/s, the diameter of pipe is calculated as:

$$\begin{aligned} \text{Minimum pipe diameter (d)} &= (4Q/\pi V)^{1/2} \\ &= 0.105 \text{ m} \\ &= 105 \text{ mm} \end{aligned}$$

$$\begin{aligned} \text{Proposed pipe diameter (d)} &= 200 \text{ mm} && \text{(considering sprinkler system, to be coordinated with mechanical)} \\ &= 8 \text{ Inches} \end{aligned}$$



Fire Flow Calculations

LRL File No. 220027

Project: Proposed Development

Location: 6310 Hazeldean Rd, Ottawa, ON

Date: July 3, 2025

Method: Fire Underwriter's Survey (FUS)

Prepared by:

BUILDING 1- 12 storey

Step	Task	Term	Options	Multiplier	Choose:	Value	Unit	Fire Flow
Construction Coefficient (C)								
1	Choose frame used for building	Coefficient C related to the type of construction	Wood Frame Construction (Type V)	1.5	Noncombustible Construction (Type II)	0.8		
			Mass Timber Construction (Type IV-A)	0.8				
			Mass Timber Construction (Type IV-B)	0.9				
			Mass Timber Construction (Type IV-C)	1.0				
			Mass Timber Construction (Type IV-D)	1.5				
			Ordinary Construction (Type III)	1.0				
			Noncombustible Construction (Type II)	0.8				
			Fire Resistive Construction (Type I)	0.6				
Floor Area (A)								
2	Total Effective Floor Area					17,520	m ²	
3	Obtain fire flow before reductions	Required fire flow (rounded to nearest 1000)	Fire Flow = 220 x C x A ^{0.5}				L/min	24,000
Occupancy and Contents Adjustment								
4	Choose combustibility of contents	Occupancy hazard reduction or surcharge	Noncombustible	-25%	Limited combustible	-15%	L/min	20,400
			Limited combustible	-15%				
			Combustible	0%				
			Free burning	15%				
			Rapid burning	25%				
Sprinkler Protection								
5	Choose reduction for sprinklers	Sprinkler reduction	Automatic sprinkler protection designed & installed in accordance with NFPA 13	-30%	True	-30%	L/min	10,200
			Water supply is standard for both the system and fire department hose lines	-10%	True	-10%		
			Fully supervised system	-10%	True	-10%		
Exposure Adjustment								
6	Choose separation	Exposure distance	North side	>30m	0%	15%	L/min	13,260
			East side	10.1 to 20m	15%			
			South side	>30m	0%			
			West side	>30m	0%			
Net Required Fire Flow								
7	Obtain fire flow and duration	Minimum required fire flow (rounded to nearest 1000)					L/min	13,000
		Minimum required fire flow					L/s	216.7
		Required duration of fire flow					hr	3



Fire Flow Calculations

LRL File No. 220027

Project: Proposed Development

Location: 6310 Hazeldean Rd, Ottawa, ON

Date: July 3, 2025

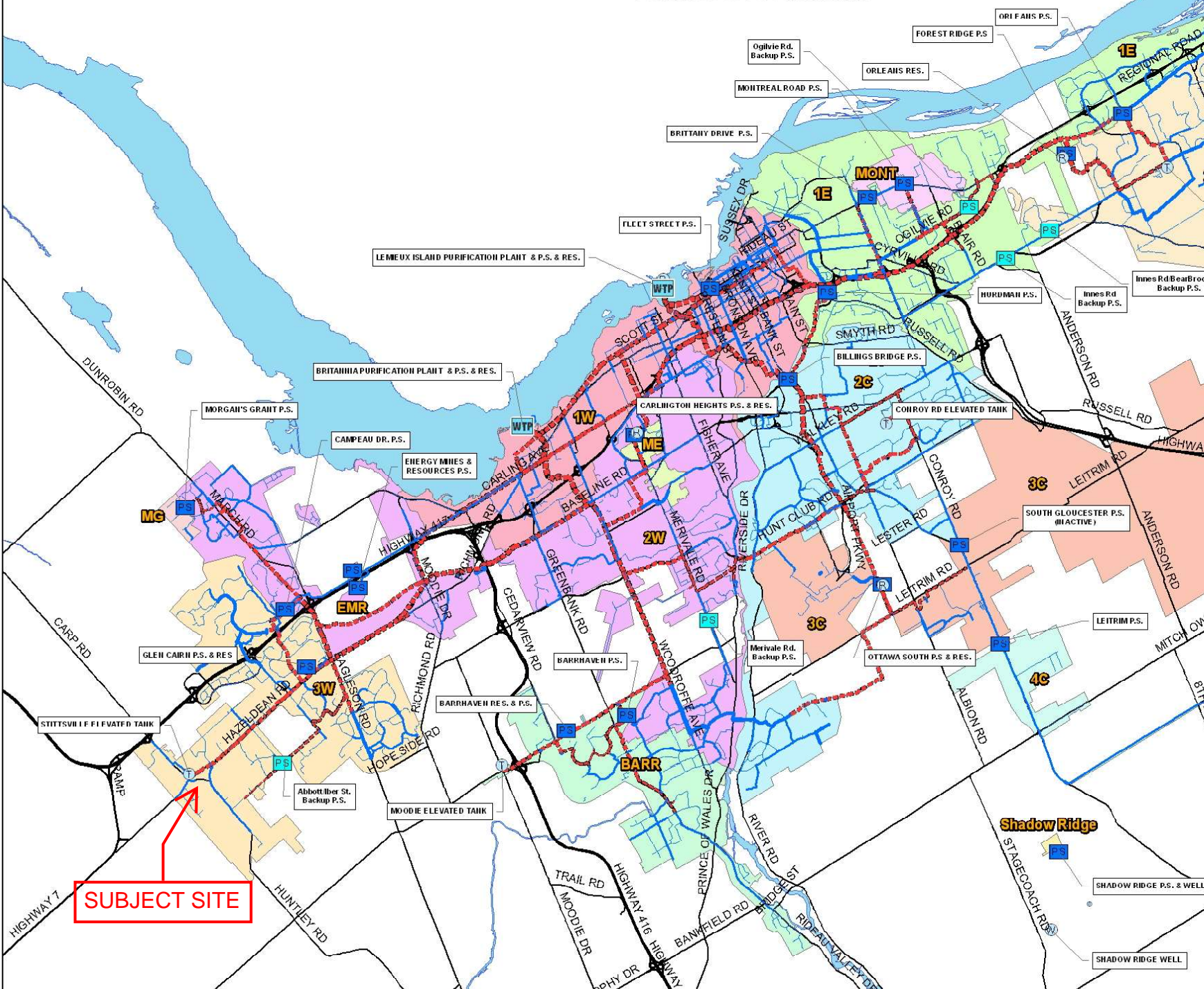
Method: Fire Underwriter's Survey (FUS)

Prepared by:

BUILDING 2- 21 storey

Step	Task	Term	Options	Multiplier	Choose:	Value	Unit	Fire Flow
Construction Coefficient (C)								
1	Choose frame used for building	Coefficient C related to the type of construction	Wood Frame Construction (Type V)	1.5	Noncombustible Construction (Type II)	0.8		
			Mass Timber Construction (Type IV-A)	0.8				
			Mass Timber Construction (Type IV-B)	0.9				
			Mass Timber Construction (Type IV-C)	1.0				
			Mass Timber Construction (Type IV-D)	1.5				
			Ordinary Construction (Type III)	1.0				
			Noncombustible Construction (Type II)	0.8				
			Fire Resistive Construction (Type I)	0.6				
Floor Area (A)								
2	Total Effective Floor Area					7,212	m ²	
3	Obtain fire flow before reductions	Required fire flow (rounded to nearest 1000)	Fire Flow = 220 x C x A ^{0.5}				L/min	15,000
Occupancy and Contents Adjustment								
4	Choose combustibility of contents	Occupancy hazard reduction or surcharge	Noncombustible	-25%	Limited combustible	-15%	L/min	12,750
			Limited combustible	-15%				
			Combustible	0%				
			Free burning	15%				
			Rapid burning	25%				
Sprinkler Protection								
5	Choose reduction for sprinklers	Sprinkler reduction	Automatic sprinkler protection designed & installed in accordance with NFPA 13	-30%	True	-30%	L/min	6,375
			Water supply is standard for both the system and fire department hose lines	-10%	True	-10%		
			Fully supervised system	-10%	True	-10%		
Exposure Adjustment								
6	Choose separation	Exposure distance	North side	>30m	0%	15%	L/min	8,288
			East side	>30m	0%			
			South side	>30m	0%			
			West side	10.1 to 20m	15%			
Net Required Fire Flow								
7	Obtain fire flow and duration	Minimum required fire flow (rounded to nearest 1000)					L/min	8,000
		Minimum required fire flow					L/s	133.3
		Required duration of fire flow					hr	3

City of Ottawa - Water Distribution System Facilities & Feedermains



SUBJECT SITE

LOCATION OF FIRE HYDRANTS FIGURE

LEGEND



Hydrants within 75m



Hydrants within 150m



Hydrants within 300m

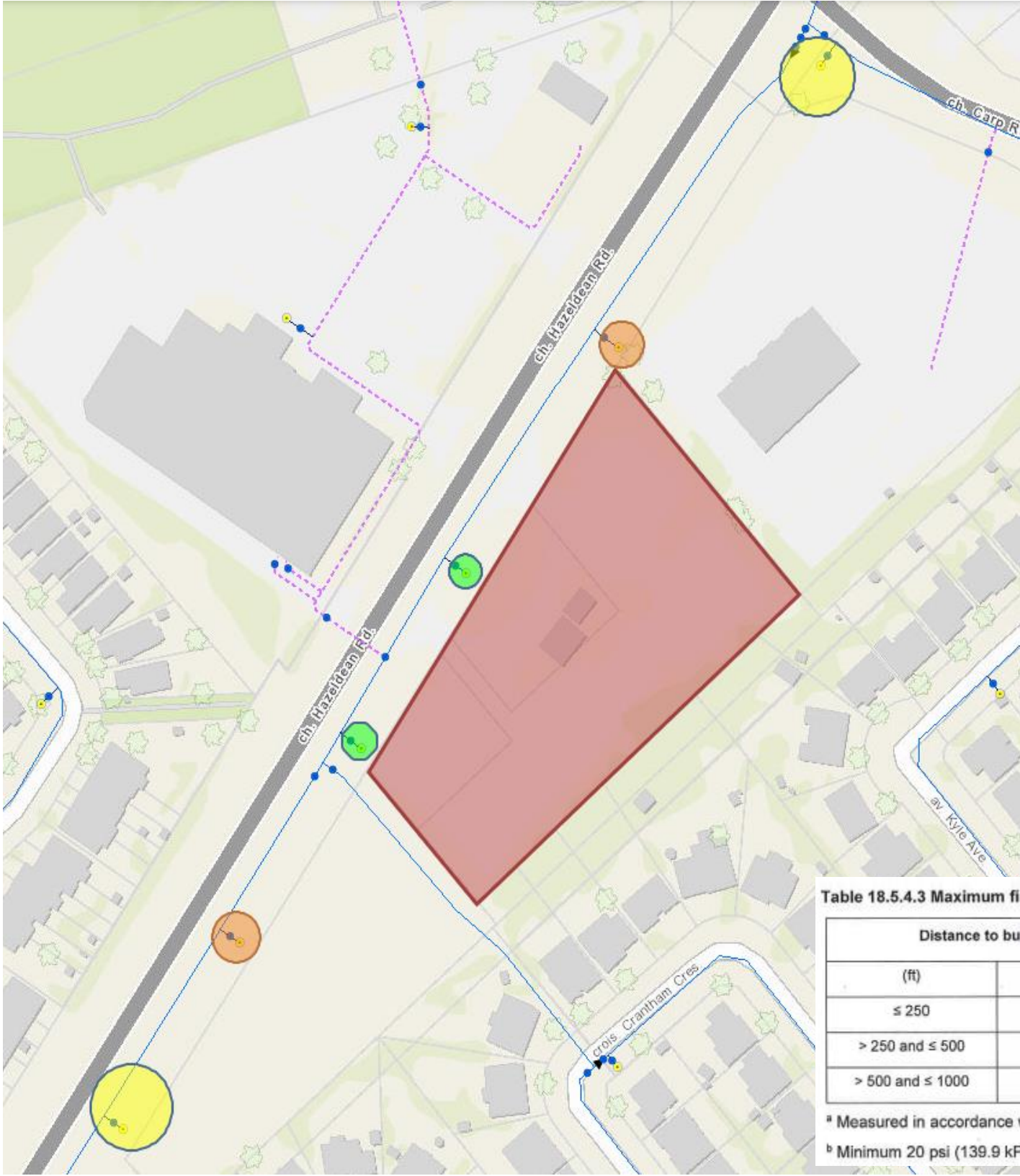


Table 18.5.4.3 Maximum fire flow hydrant capacity

Distance to buildings ^a		Maximum capacity ^b	
(ft)	(m)	(gpm)	(L/min)
≤ 250	≤ 76	1500	5678
> 250 and ≤ 500	> 76 and ≤ 152	1000	3785
> 500 and ≤ 1000	> 152 and ≤ 305	750	2839

^a Measured in accordance with 18.5.1.4 and 18.5.1.5.

^b Minimum 20 psi (139.9 kPa) residual pressure.

Boundary Conditions 6310 Hazeldean Road

Provided Information

Scenario	Demand	
	L/min	L/s
Average Daily Demand	160	2.66
Maximum Daily Demand	395	6.59
Peak Hour	868	14.46
Fire Flow Demand #1	13,000	216.67

Location



Results

Connection 1 – Hazeldean Road

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	160.6	51.0
Peak Hour	157.0	46.0
Max Day plus Fire Flow #1	156.7	45.5

¹ Ground Elevation = 124.7 m

Connection 2 – Hazeldean Road West

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	160.6	51.0
Maximum HGL	157.0	46.0
Max Day plus Fire Flow #1	156.6	45.4

¹ Ground Elevation = 124.7 m

Notes

1. The IWSD has recently updated their water modelling software. Any significant difference between previously received BC results and newly received BC results could be attributed to this update.
2. Per the OWDG Tech Bulletin ISTB-2021-03 Section 4.3.1.:
 - a. Industrial, commercial, institutional service areas with a basic day demand greater than 50 m³/day (0.58 L/s) and residential areas serving 50 or more dwellings shall be connected with a minimum of two watermains, separated by an isolation valve, to avoid the creation of a vulnerable service area. Individual residential facilities with a basic day demand greater than 50 m³/day shall be connected with a minimum of two water services, separated by an isolation valve, to avoid the creation of a vulnerable service area.
3. Any connection to a watermain 400 mm or larger should be approved by DWS as per the **Water Design Guidelines Section 2.4 Review by Drinking Water Services**.

Disclaimer

The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation. Fire Flow analysis is a reflection of available flow in the watermain; there may be additional restrictions that occur between the watermain and the hydrant that the model cannot take into account.

Mohan Basnet

From: Candow, Julie <julie.candow@ottawa.ca>
Sent: July 23, 2025 1:28 PM
To: Sarthak Vora
Cc: Roy, Jean-Miguel; Mohan Basnet; Maxime Longtin
Subject: RE: Boundary Condition request_6310 Hazeldean Rd (LRL 220027)
Attachments: 6310 Hazeldean Boundary Condition(23July2025).docx

Hi Sarthak,

Please see attached the boundary condition results for 6310 Hazeldean Road. Please note that a connection to the 305mm easement watermain was not approved by DWS. As such, the boundary conditions show two separate connections to the 406mm diameter watermain in Hazeldean Road. Please note, as per the OWDG Tech Bulletin ISTB-2021-03 Section 4.3.1, residential areas serving 50 or more dwellings shall be connected with a minimum of two watermains, separated by an isolation valve, to avoid the creation of a vulnerable service area.

There are no capacity concerns in the 375mm / 450mm diameter sanitary sewer crossing Hazeldean Road south-west of the subject property. That said, a sanitary sewer connection to the 450mm diameter sanitary sewer located within the easement is not permitted. The sanitary sewer connection from the subject site must be made within the Hazeldean Road right-of-way.

Let me know if you have any questions.

Thanks,

Julie Candow, P.Eng
Project Manager
Development Review – West Branch
Planning, Development and Building Services Dept.
110 Laurier Avenue West, 4th Floor East
Ottawa, ON K1P 1J1
613.580.2424 ext. 13850

Classified as City of Ottawa - Internal / Ville d'Ottawa - classé interne

From: Candow, Julie
Sent: July 09, 2025 9:32 AM
To: svora@lrl.ca
Cc: Roy, Jean-Miguel <Jean-Miguel.Roy@ottawa.ca>; Fawzi, Mohammed <mohammed.fawzi@ottawa.ca>; Mohan Basnet <mbasnet@lrl.ca>; Maxime Longtin <mlongtin@lrl.ca>
Subject: RE: Re: Boundary Condition request_6310 Hazeldean Rd (LRL 220027)

Hi Sarthak,

Your BC request has been sent to our team in Infrastructure Planning, along with your capacity check for sanitary sewers.

I will forward you the results once I receive them.

Julie Candow, P.Eng

Project Manager
Development Review – West Branch
Planning, Development and Building Services Dept.
110 Laurier Avenue West, 4th Floor East
Ottawa, ON K1P 1J1
613.580.2424 ext. 13850

From: Fawzi, Mohammed <mohammed.fawzi@ottawa.ca>
Sent: July 09, 2025 9:28 AM
To: Candow, Julie <julie.candow@ottawa.ca>
Cc: Roy, Jean-Miguel <Jean-Miguel.Roy@ottawa.ca>
Subject: FW: Re: Boundary Condition request_6310 Hazeldean Rd (LRL 220027)

Hey Julie,

I believe you are the PM on this one. Please see the email below. The Consultant is following up on their boundary conditions request.

Thank you.

Best Regards,

Mohammed Fawzi, P.Eng.

Senior Project Manager (A), Infrastructure Projects
Development Review – West Branch
Planning, Development and Building Services Department (PDBS) | Direction générale des services de la planification, de l'aménagement et du bâtiment (DGSPAB)
City of Ottawa | Ville d'Ottawa
110 Laurier Avenue West | 110 Avenue Laurier Ouest
Ottawa, ON K1P 1J1
613.580.2424 ext./poste 70120, Mohammed.Fawzi@ottawa.ca

Classified as City of Ottawa - Internal / Ville d'Ottawa - classé interne

From: Brault, Ryan <ryan.brault@ottawa.ca>
Sent: July 9, 2025 9:23 AM
To: Fawzi, Mohammed <mohammed.fawzi@ottawa.ca>
Subject: FW: Re: Boundary Condition request_6310 Hazeldean Rd (LRL 220027)

Hey Mo,

FYI, I just received the below follow up for 6310 Hazeldean Rd.

Regards,

Ryan

Classified as City of Ottawa - Internal / Ville d'Ottawa - classé interne

From: Sarthak Vora <svora@lrl.ca>
Sent: Wednesday, July 9, 2025 9:15 AM
To: Brault, Ryan <ryan.brault@ottawa.ca>
Cc: Maxime Longtin <mlongtin@lrl.ca>; Mohan Basnet <mbasnet@lrl.ca>
Subject: RE: Re: Boundary Condition request_6310 Hazeldean Rd (LRL 220027)

CAUTION: This email originated from an External Sender. Please do not click links or open attachments unless you recognize the source.

ATTENTION : Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.

Hi Ryan,

Could you please confirm if my request has been received? This is a critical item currently holding up our submission, and would greatly appreciate an early answer.

Thanks,

Sarthak Vora, Civil E.I.T

 **LRL ENGINEERING | INGÉNIERIE**
Head Office – 5430 Canotek Rd., Ottawa, ON
T +1 613-842-3434 C +1 613-915-7633 E svora@lrl.ca
Ottawa | Pembroke | Moncton
www.lrl.ca

From: Sarthak Vora
Sent: Thursday, July 3, 2025 4:55 PM
To: ryan.brault@ottawa.ca
Cc: Maxime Longtin <mlongtin@lrl.ca>; Mohan Basnet <mbasnet@lrl.ca>
Subject: Re: Boundary Condition request_6310 Hazeldean Rd (LRL 220027)

Good Afternoon Ryan,

I would like to request boundary conditions and confirmation on the Sanitary sewer capacity for the Proposed Residential Development located at 6310 Hazeldean Rd.

Boundary Conditions Request:

We are requesting boundary conditions for a proposed development consisting of two residential buildings:

- Building 1: 12 storeys
- Building 2: 21 storeys

The development will accommodate a total of 441 residential units, translating to a projected population of 803, and includes approximately 0.1691 hectares of amenity space.

We are proposing a dual water service connection, with two connection points (see attached PDF):

- Connection #1: To the 305mmØ municipal watermain branching off Hazeldean Road towards the southwest side of the development
- Connection #2: To the 406mmØ municipal watermain within the Hazeldean Road right-of-way

Can you please provide the boundary conditions using the following revised proposed development demands:

	Demand (L/s)
Avg. Daily	2.66
Max. Day	6.59
Peak Hour	14.46

	Demand (L/s)
FUS- Building #1	216.7
FUS- Building #2	133.3

Sanitary Connection

We also determined that the sanitary sewer discharge from the site would be equal to **9.03L/s**. We are proposing to tie into the 450mm sanitary sewer branching off Hazeldean Rd @Connection 1. Please confirm if the existing sanitary sewer will have sufficient capacity to accommodate our discharge.

Attached are the copies of the design sheets for your reference. If any additional information is required, please let me know.

Thanks

Sarthak Vora, Civil E.I.T

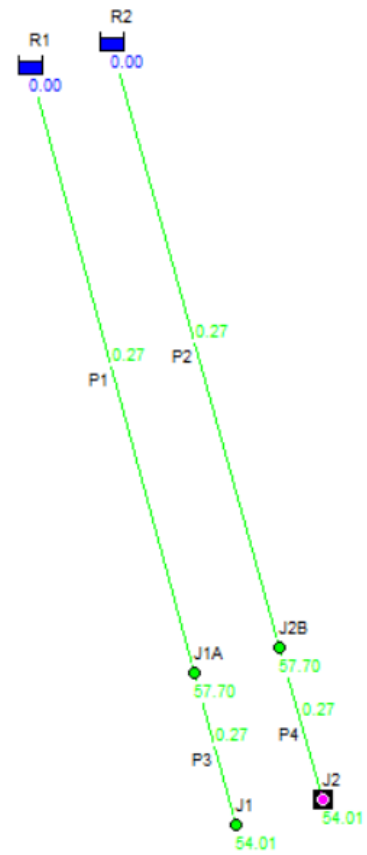
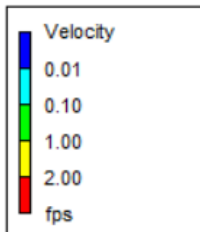
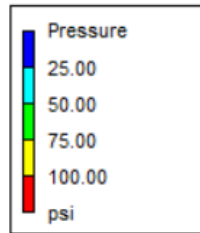
 **LRL ENGINEERING | INGÉNIERIE**
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Ottawa | Pembroke | Moncton
www.lrl.ca

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SUMMARY OF HYDRAULIC ANALYSIS USING EPANET

Scenario 1: Avg. Day




```

*****
*                               E P A N E T                               *
*                               Hydraulic and Water Quality                *
*                               Analysis for Pipe Networks                  *
*                               Version 2.2                                *
*****
    
```

Input File: 220027_Avg Day.net

Link - Node Table:

Link ID	Start Node	End Node	Length ft	Diameter in
P1	R1	J1A	49.2	8
P2	R2	J2B	49.2	8
P3	J1A	J1	12.46	8
P4	J2B	J2	12.46	8

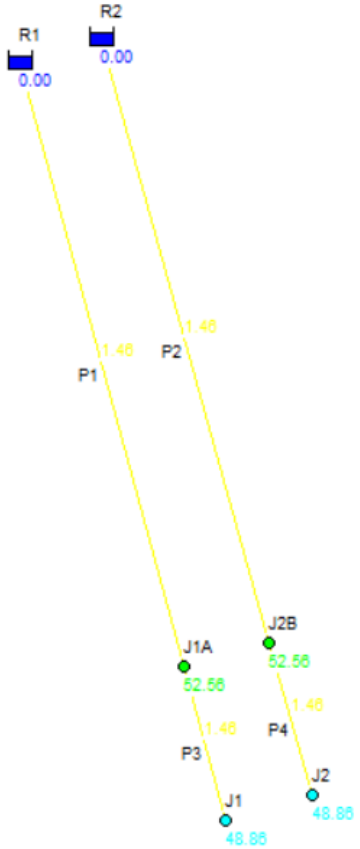
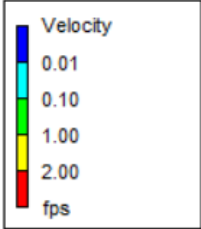
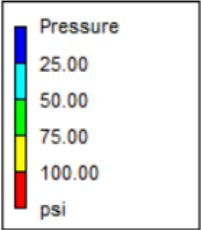
Node Results:

Node ID	Demand GPM	Head ft	Pressure psi	Quality
J1	42.27	526.77	54.01	0.00
J2	42.27	526.77	54.01	0.00
J2B	0.00	526.77	57.70	0.00
J1A	0.00	526.77	57.70	0.00
R1	-42.27	526.77	0.00	0.00 Reservoir
R2	-42.27	526.77	0.00	0.00 Reservoir

Link Results:

Link ID	Flow GPM	Velocity fps	Unit Headloss ft/Kft	Status
P1	42.27	0.27	0.05	Open
P2	42.27	0.27	0.05	Open
P3	42.27	0.27	0.04	Open
P4	42.27	0.27	0.04	Open

Scenario 2: Peak Hour



```

*****
*                               E P A N E T                               *
*                               Hydraulic and Water Quality              *
*                               Analysis for Pipe Networks                *
*                               Version 2.2                              *
*****
    
```

Input File: 220027_Peak Hour.net

Link - Node Table:

Link ID	Start Node	End Node	Length ft	Diameter in
P1	R1	J1A	49.2	8
P2	R2	J2B	49.2	8
P3	J1A	J1	12.46	8
P4	J2B	J2	12.46	8

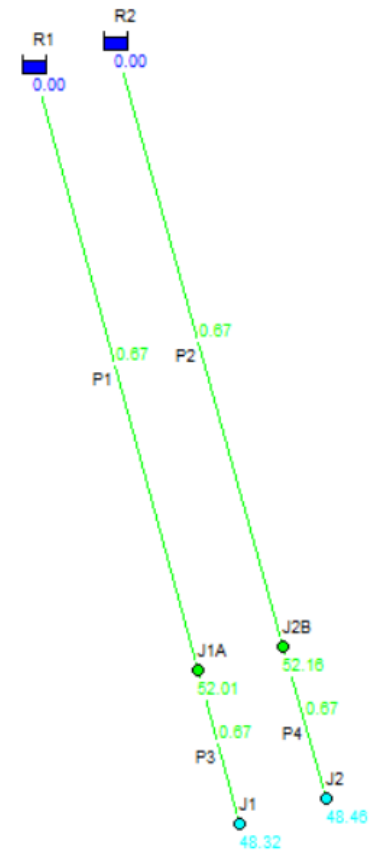
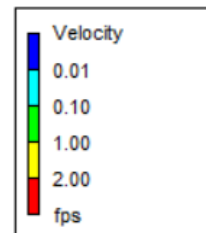
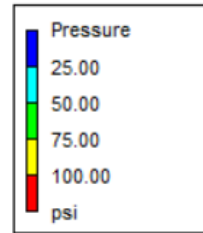
Node Results:

Node ID	Demand GPM	Head ft	Pressure psi	Quality
J1	229.30	514.90	48.86	0.00
J2	229.30	514.90	48.86	0.00
J2B	0.00	514.91	52.56	0.00
J1A	0.00	514.91	52.56	0.00
R1	-229.30	514.96	0.00	0.00 Reservoir
R2	-229.30	514.96	0.00	0.00 Reservoir

Link Results:

Link ID	Flow GPM	Velocity fps	Unit Headloss ft/Kft	Status
P1	229.30	1.46	1.04	Open
P2	229.30	1.46	1.04	Open
P3	229.30	1.46	1.04	Open
P4	229.30	1.46	1.04	Open

Scenario 3: Max. Day + Fire Flow



```
*****
*                               E P A N E T                               *
*                               Hydraulic and Water Quality                 *
*                               Analysis for Pipe Networks                   *
*                               Version 2.2                                *
*****
```

Input File: 220027_Max Day+Fire Flow.net

Link - Node Table:

Link ID	Start Node	End Node	Length ft	Diameter in
P1	R1	J1A	49.2	8
P2	R2	J2B	49.2	8
P3	J1A	J1	12.46	8
P4	J2B	J2	12.46	8

Node Results:

Node ID	Demand GPM	Head ft	Pressure psi	Quality
J1	104.35	513.64	48.32	0.00
J2	104.35	513.97	48.46	0.00
J2B	0.00	513.97	52.16	0.00
J1A	0.00	513.64	52.01	0.00
R1	-104.35	513.65	0.00	0.00 Reservoir
R2	-104.35	513.98	0.00	0.00 Reservoir

Link Results:

Link ID	Flow GPM	Velocity fps	Unit Headloss ft/Kft	Status
P1	104.35	0.67	0.24	Open
P2	104.35	0.67	0.24	Open
P3	104.35	0.67	0.24	Open
P4	104.35	0.67	0.24	Open

APPENDIX E
Civil Engineering Drawings



PROPOSED MIXED USE APARTMENT DEVELOPMENT 6310 HAZELDEAN ROAD OTTAWA, ON

REVISION 02



KEY PLAN (N.T.S.)

DRAWING INDEX	
TITLE PAGE	
GENERAL NOTES	C001
SEDIMENT AND EROSION CONTROL PLAN	C101
DEMOLITION PLAN	C102
GRADING AND DRAINAGE PLAN	C301
SERVICING PLAN	C401
STORMWATER MANAGEMENT PLAN	C601
PRE-DEVELOPMENT WATERSHED PLAN	C701
POST-DEVELOPMENT WATERSHED PLAN	C702
CONSTRUCTION DETAIL PLAN	C901



LRL

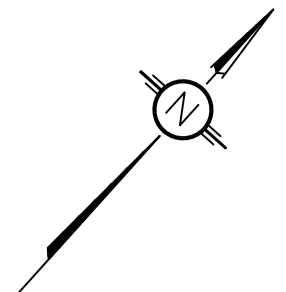
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5430 Canotek Road | Ottawa, ON, K1J 9G2
www.lrl.ca | (613) 842-3434

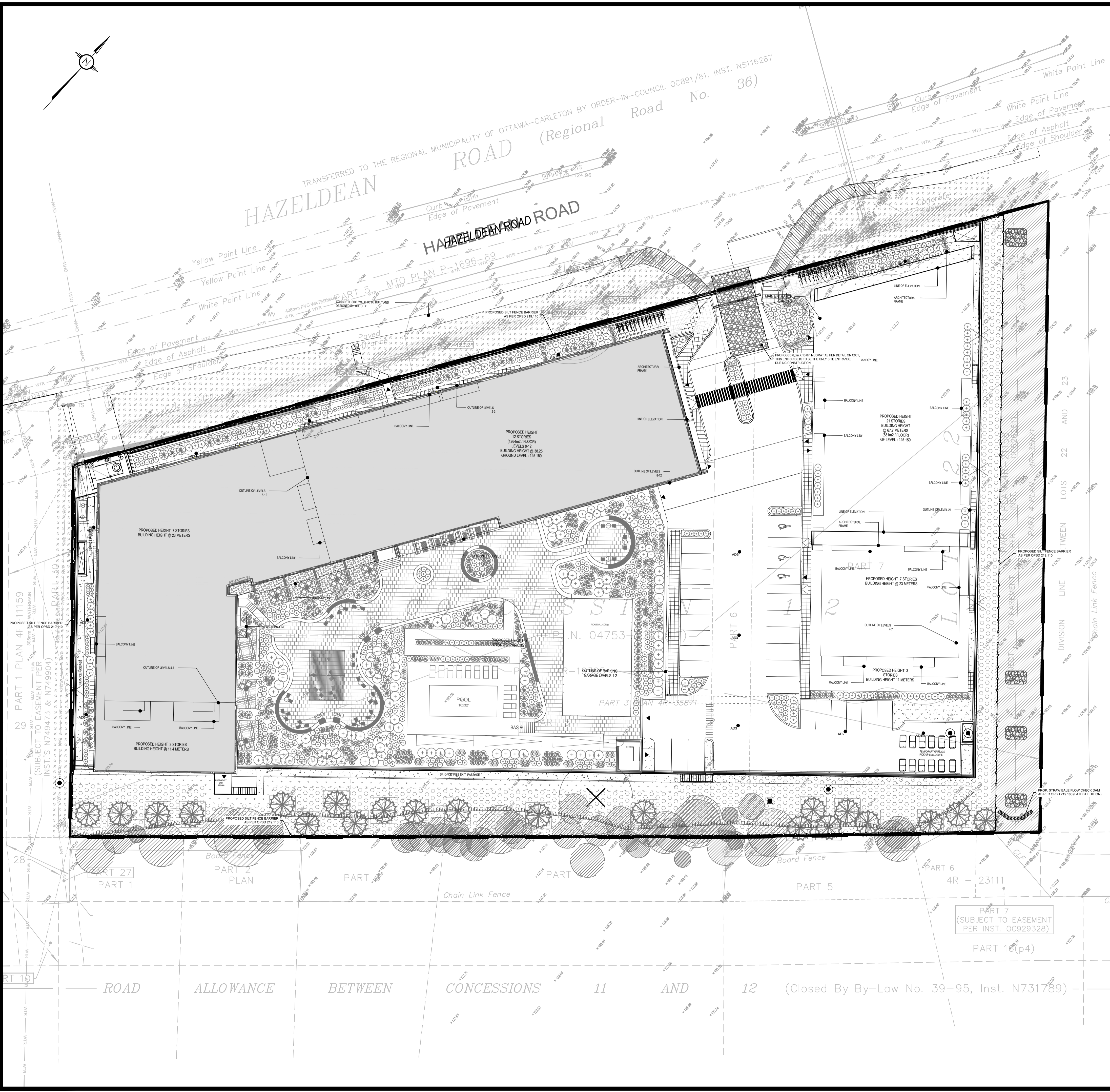
MIXED USE APARTMENT DEVELOPMENT
6310 HAZELDEAN ROAD, OTTAWA, ON
REV.02 - ISSUED FOR APPROVAL - 2025-11-03
LRL PROJECT no: 220027



NOT AUTHENTIC UNLESS SIGNED AND DATED



TRANSFERRED TO THE REGIONAL MUNICIPALITY OF OTTAWA-CARLETON BY ORDER-IN-COUNCIL OC891/81, INST. NS116267
HAZELDEAN ROAD (Regional Road No. 36)
 MTO PLAN P-1696-69



LEGEND:

- EXISTING PROPERTY LINE TO REMAIN
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- PROPOSED DEPRESSED CURB
- PROPOSED TERRACING (3.1 MIN.)
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- MATCH INTO EXISTING ELEVATION
- EXISTING ELEVATION
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- EXISTING CATCHBASIN
- PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN
- PROPOSED MANHOLE
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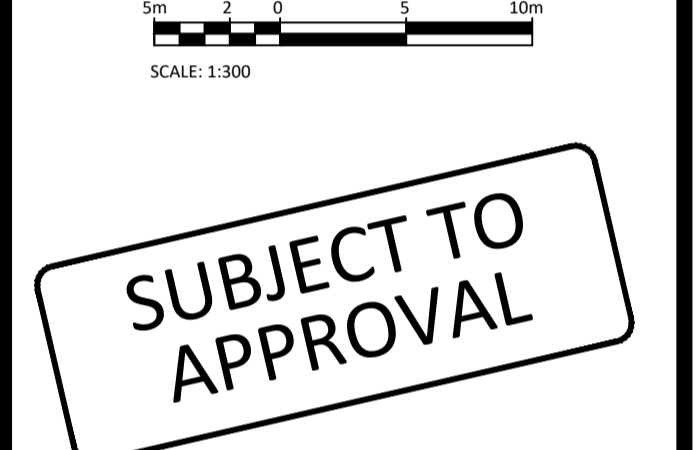
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02	ISSUED FOR APPROVAL	M.L.	03 NOV 2025
01	ISSUED FOR APPROVAL	M.L.	21 AUG 2025
No.	REVISIONS	BY	DATE

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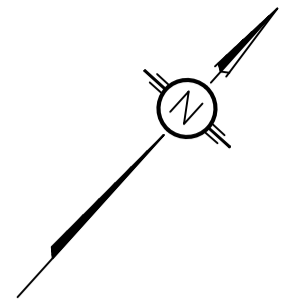
CLIENT: **SCALIA**

DESIGNED BY: M.L. DRAWN BY: M.L. APPROVED BY: M.B.

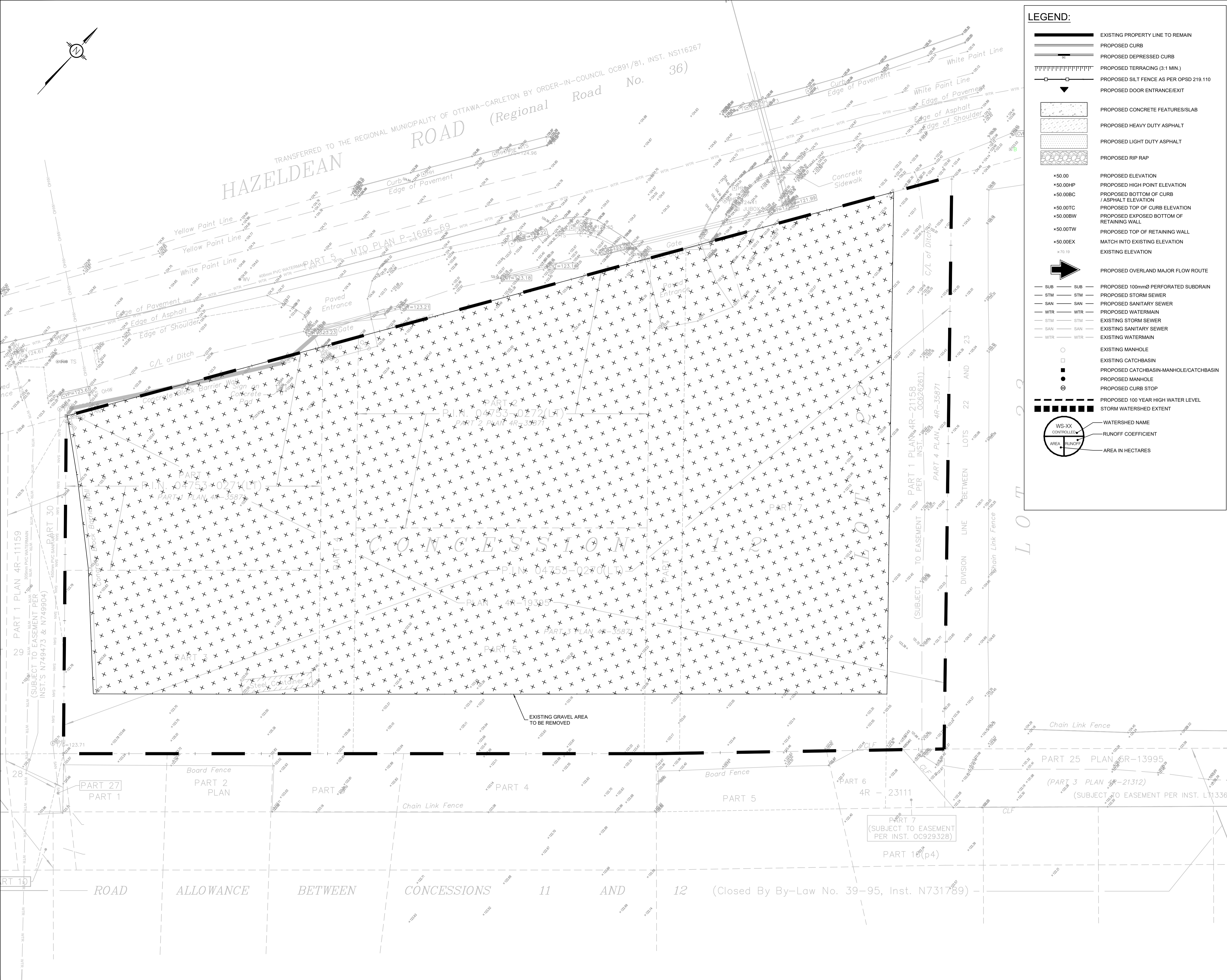
PROJECT: **MIXED USE APARTMENT DEVELOPMENT
 6310 HAZELDEAN ROAD
 OTTAWA, ON**

DRAWING TITLE: **EROSION AND SEDIMENT CONTROL PLAN**

PROJECT NO.: **220027 C101**



TRANSFERRED TO THE REGIONAL MUNICIPALITY OF OTTAWA-CARLETON BY ORDER-IN-COUNCIL OC891/81, INST. NS116267
HAZELDEAN ROAD (Regional Road No. 36)



LEGEND:

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SCALE: 1:300

SUBJECT TO APPROVAL

02	ISSUED FOR APPROVAL	M.L.	03 NOV 2025
01	ISSUED FOR APPROVAL	M.L.	21 AUG 2025
No.	REVISIONS	BY	DATE

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 www.lrl.ca | (613) 842-3434

CLIENT: SCALIA

DESIGNED BY: M.L. DRAWN BY: M.L. APPROVED BY: M.B.

PROJECT: MIXED USE APARTMENT DEVELOPMENT
 6310 HAZELDEAN ROAD
 OTTAWA, ON

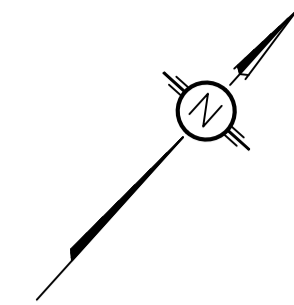
DRAWING TITLE: DEMOLITION PLAN

PROJECT NO.: 220027 **C102**

PAVEMENT STRUCTURE

COURSE	MATERIAL	THICKNESS (mm)	
		AUTOMOBILE PARKING	TRUCK ROUTE (HEAVY TRAFFIC)
SURFACE	HL 3 A/C (PG 58-34)	50	40
BINDER	HL 8 A/C (PG 58-34)	--	50
BASECOURSE	OPSS GRANULAR "A"	150	150
SUBBASE	OPSS GRANULAR "B" TYPE II	300	450

NOTE:
IN PREPARATION FOR PAVEMENT CONSTRUCTION AT THIS SITE, ANY SURFICIAL OR NEAR SURFACE/SUBGRADE LEVEL TOPSOIL AND ANY SOFT, WET OR DELETERIOUS MATERIALS SHOULD BE REMOVED FROM THE PROPOSED PAVED AREAS. THE EXPOSED SUBGRADE SHOULD BE INSPECTED AND APPROVED BY GEOTECHNICAL PERSONNEL AND ANY SOFT AREAS EVIDENT SHOULD BE SUBCAVATED AND REPLACED WITH SUITABLE EARTH BORROW APPROVED BY THE GEOTECHNICAL ENGINEER. THE SUBGRADE SHOULD BE SHAPED AND CROWNED TO PROMOTE DRAINAGE OF THE SITE DRAINAGE STRUCTURES FOLLOWING APPROVAL OF THE PREPARATION OF THE SUBGRADE. THE PAVEMENT GRANULARS MAY BE PLACED. REFER TO GEOTECHNICAL REPORT PREPARED BY PATERSON, DATED NOVEMBER 03rd, 2025.



LEGEND:

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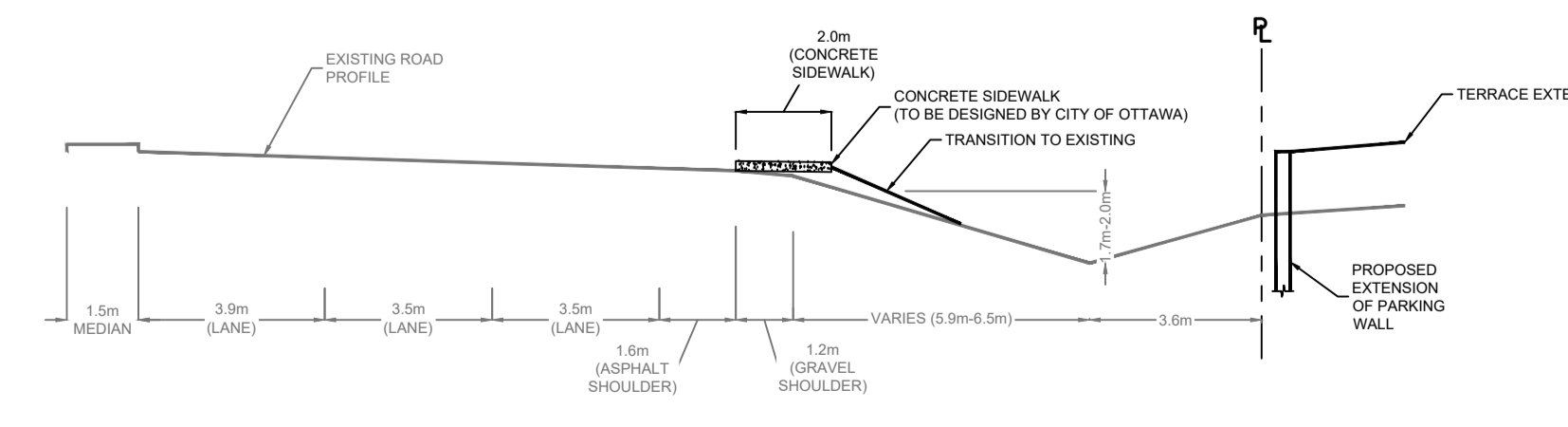
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SUBJECT TO APPROVAL

No.	REVISIONS	BY	DATE
02	ISSUED FOR APPROVAL	M.L.	03 NOV 2025
01	ISSUED FOR APPROVAL	M.L.	21 AUG 2025

NOT AUTHENTIC UNLESS SIGNED AND DATED

LRL
ENGINEERING | INGENIERIE
5430 Canotek Road | Ottawa, ON, K1J 9G2
www.lrl.ca | (613) 842-3434

CLIENT: **SCALIA**

DESIGNED BY: M.L. DRAWN BY: M.L. APPROVED BY: M.B.

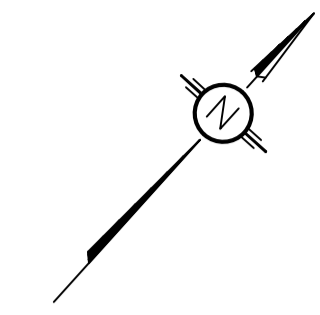
PROJECT: **MIXED USE APARTMENT DEVELOPMENT
6310 HAZELDEAN ROAD
OTTAWA, ON**

DRAWING TITLE: **GRADING AND DRAINAGE PLAN**

PROJECT NO.: **220027 C301**

NOTE:

- STORMWATER RUNOFF FROM AREA DRAINS AD1 - AD5 TO BE DIRECTED TO CISTERN 2
- STORMWATER RUNOFF FROM ROOF DRAINS IN BUILDINGS 1 AND 2 TO BE DIRECTED TO CISTERN 1
- STORMWATER RUNOFF FROM AREA DRAINS AD6 - AD12 TO BE DIRECTED TO CISTERN 1



TRANSFERRED TO THE REGIONAL MUNICIPALITY OF OTTAWA-CARLETON BY ORDER-IN-COUNCIL 0C891/81, INST. NS116267
HAZELDEAN ROAD (Regional Road No. 36)
 White Paint Line
 Edge of Pavement
 Edge of Asphalt
 Edge of Shoulder

LEGEND:

- EXISTING PROPERTY LINE TO REMAIN
- PROPOSED CURB
- PROPOSED DEPRESSED CURB
- PROPOSED TERRACING (3.1 MIN.)
- PROPOSED SILT FENCE AS PER OPSD 219.1.0
- PROPOSED DOOR ENTRANCE/EXIT
- PROPOSED CONCRETE FEATURES/SLAB
- PROPOSED HEAVY DUTY ASPHALT
- PROPOSED LIGHT DUTY ASPHALT
- PROPOSED RIP RAP
- PROPOSED ELEVATION
- PROPOSED HIGH POINT ELEVATION
- PROPOSED BOTTOM OF CURB / ASPHALT ELEVATION
- PROPOSED TOP OF CURB ELEVATION
- PROPOSED EXPOSED BOTTOM OF RETAINING WALL
- PROPOSED TOP OF RETAINING WALL
- MATCH INTO EXISTING ELEVATION
- EXISTING ELEVATION
- PROPOSED OVERLAND MAJOR FLOW ROUTE
- PROPOSED 100mmØ PERFORATED SUBDRAIN
- PROPOSED STORM SEWER
- PROPOSED SANITARY SEWER
- PROPOSED WATERMAIN
- EXISTING STORM SEWER
- EXISTING SANITARY SEWER
- EXISTING WATERMAIN
- EXISTING MANHOLE
- EXISTING CATCHBASIN
- PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN
- PROPOSED MANHOLE
- PROPOSED CURB STOP
- PROPOSED 100 YEAR HIGH WATER LEVEL
- STORM WATERSHED EXTENT
- WATERSHED NAME
- RUNOFF COEFFICIENT
- AREA IN HECTARES

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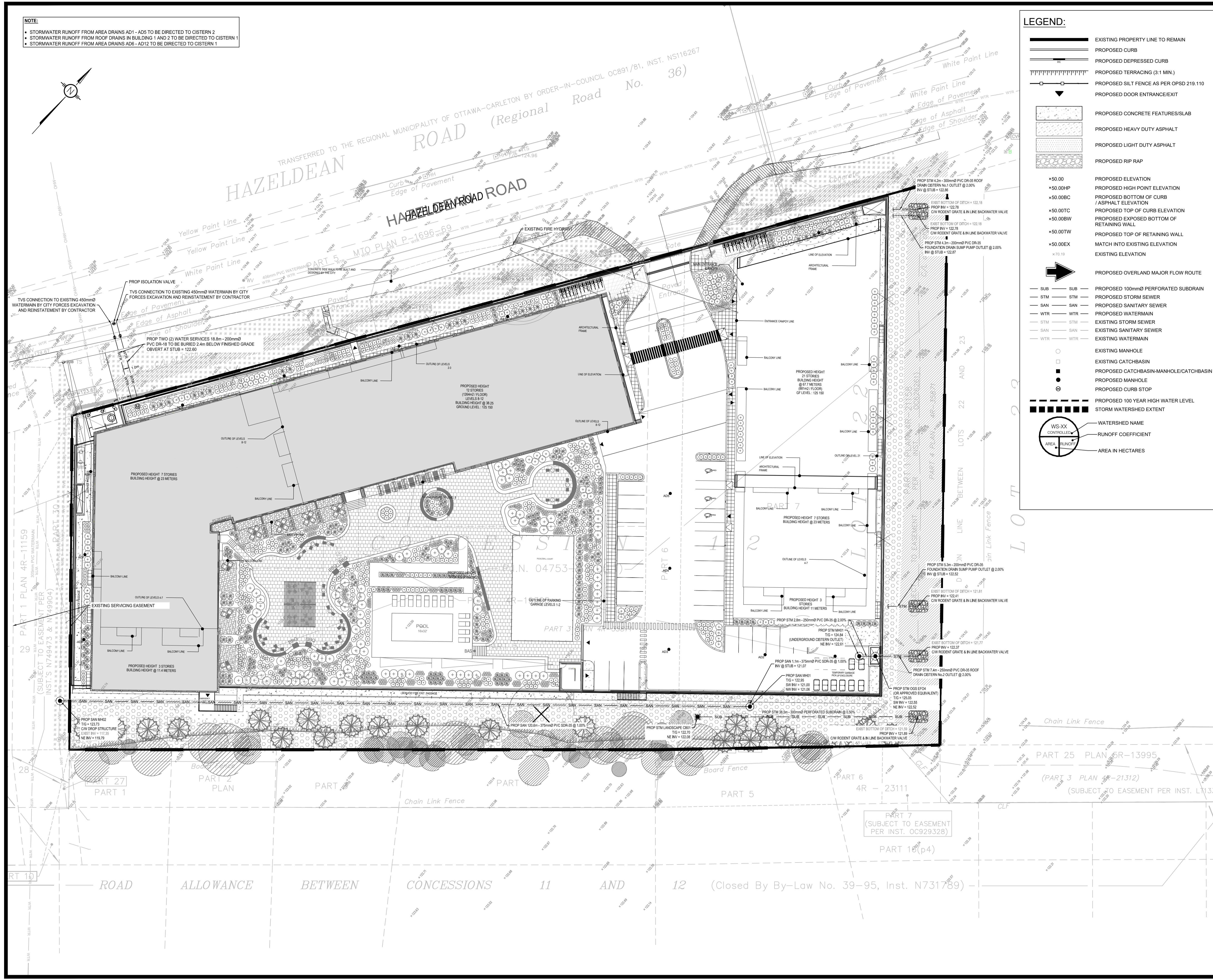
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CLIENT: SCALIA
 DESIGNED BY: M.L. DRAWN BY: M.L. APPROVED BY: M.B.

PROJECT: MIXED USE APARTMENT DEVELOPMENT
 6310 HAZELDEAN ROAD
 OTTAWA, ON

DRAWING TITLE: SERVICING PLAN

PROJECT NO.: 220027 C401



PART 1 PLAN 4R-11159
 (SUBJECT TO EASEMENT PER INST. S/N 49904)

PART 2 PLAN

PART 3 PLAN 4R-21312
 (SUBJECT TO EASEMENT PER INST. L713363)

PART 7 (SUBJECT TO EASEMENT PER INST. 0C929328)

PART 18(p4)

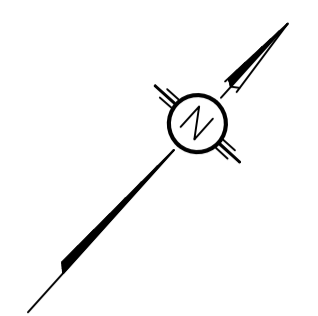
PART 25 PLAN 5R-13995

(PART 3 PLAN 4R-21312)

ROAD ALLOWANCE BETWEEN CONCESSIONS 11 AND 12 (Closed By By-Law No. 39-95, Inst. N731789)

NOTE:

- STORMWATER RUNOFF FROM AREA DRAINS AD1 - AD5 TO BE DIRECTED TO CISTERN 2
- STORMWATER RUNOFF FROM ROOF DRAINS IN BUILDING 1 AND 2 TO BE DIRECTED TO CISTERN 1
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TRANSFERRED TO THE REGIONAL MUNICIPALITY OF OTTAWA-CARLETON BY ORDER-IN-COUNCIL OC891/81, INST. N5116267

HAZELDEAN ROAD (Regional Road No. 36)

White Point Line

Edge of Pavement

Edge of Asphalt

Edge of Shoulder

Curbside

MIQ PLAN P-1696-69

APPROX. LOCATION OF CISTERN No.1 (TO BE COORDINATED WITH MECHANICAL) REQUIRED 100-YR VOLUME = 172.4m³ PUMP 100-YR Q = 97.18L/s REFER TO MECHANICAL & ARCHITECTURAL DWGS FOR DETAIL.

LEGEND:

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- PROPOSED DEPRESSED CURB
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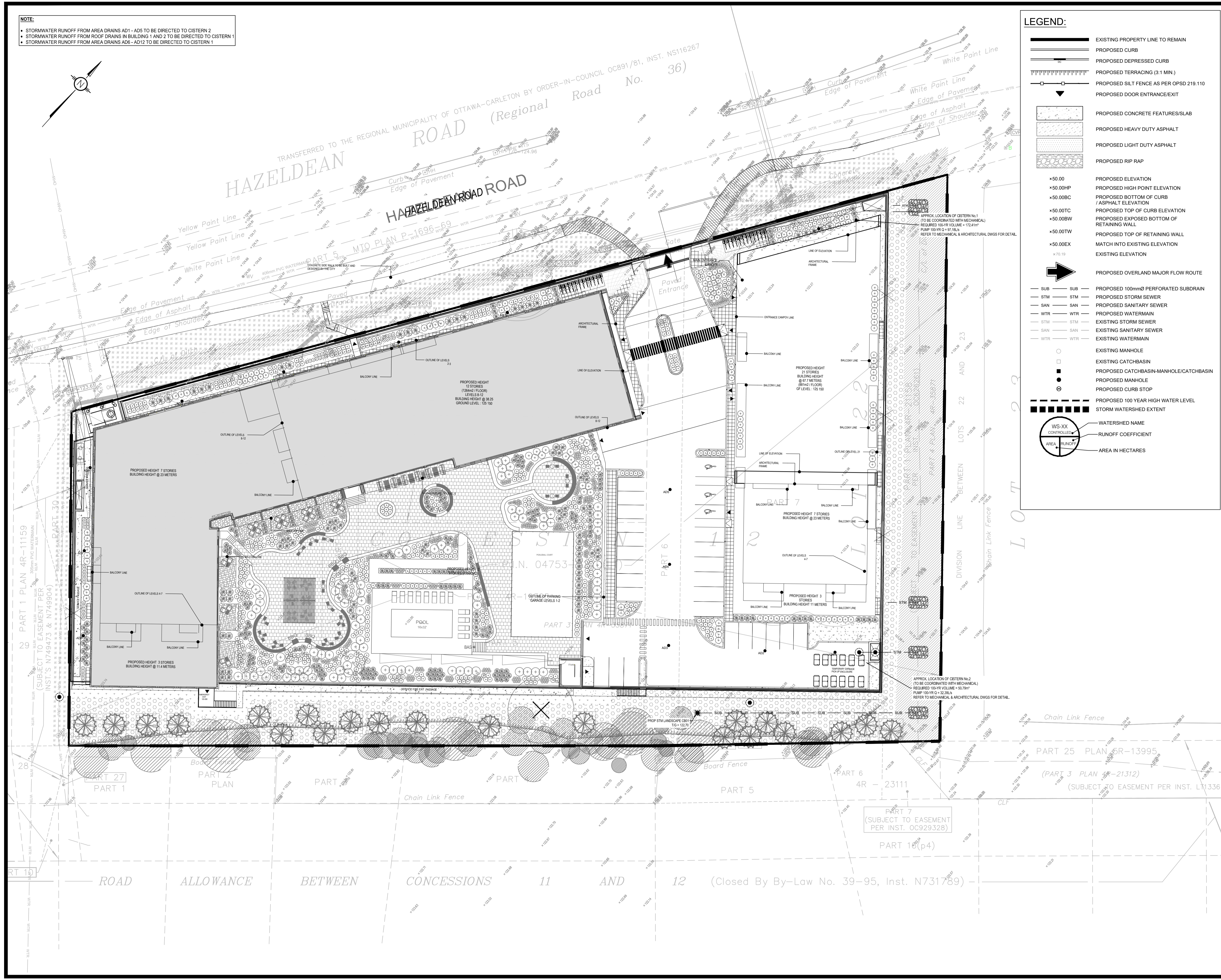
CLIENT: SCALIA

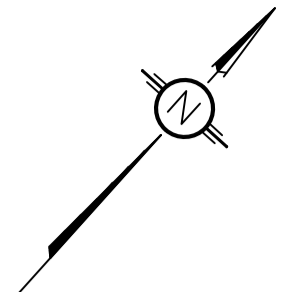
DESIGNED BY: M.L. DRAWN BY: M.L. APPROVED BY: M.B.

PROJECT: MIXED USE APARTMENT DEVELOPMENT
6310 HAZELDEAN ROAD
OTTAWA, ON

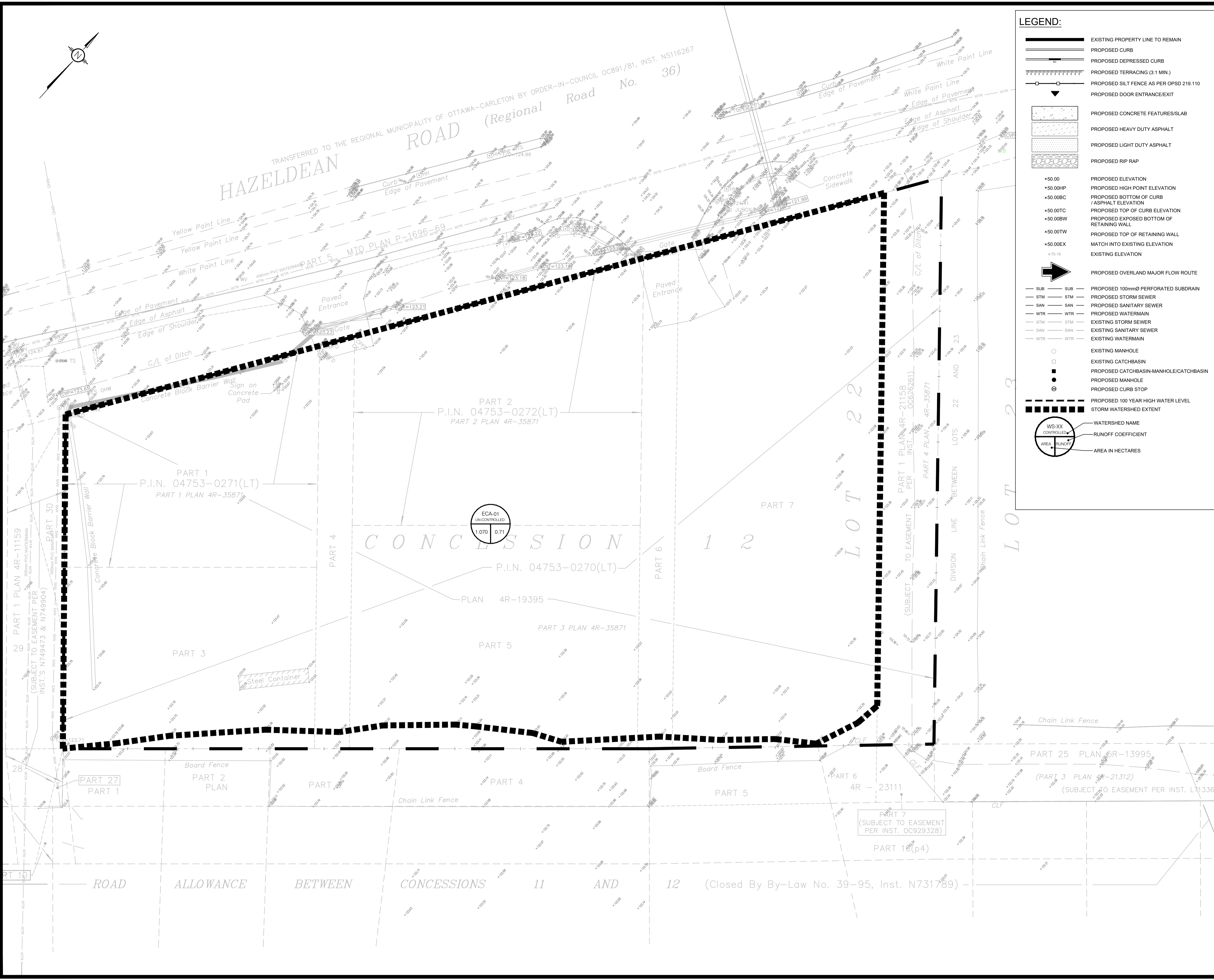
DRAWING TITLE: STORMWATER MANAGEMENT PLAN

PROJECT NO.: 220027 C601





TRANSFERRED TO THE REGIONAL MUNICIPALITY OF OTTAWA-CARLETON BY ORDER-IN-COUNCIL OC891/81, INST. NS116267
HAZELDEAN ROAD (Regional Road No. 36)



LEGEND:

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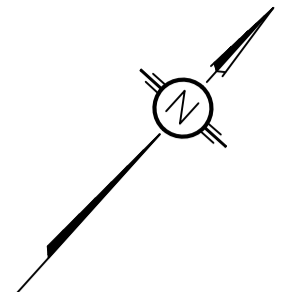
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DESIGNED BY: M.L. DRAWN BY: M.L. APPROVED BY: M.B.

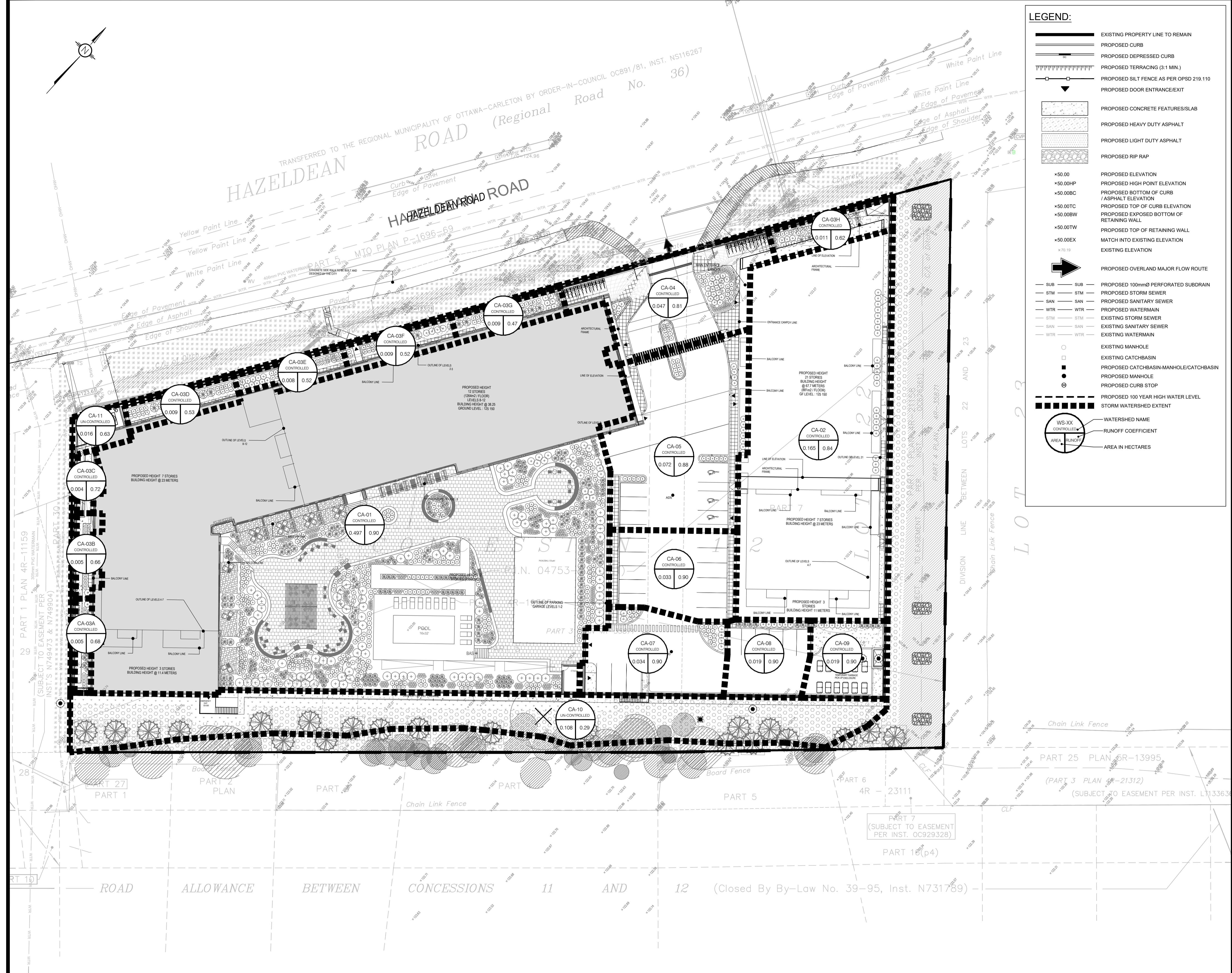
PROJECT: **MIXED USE APARTMENT DEVELOPMENT
 6310 HAZELDEAN ROAD
 OTTAWA, ON**

DRAWING TITLE: **PRE-DEVELOPMENT
 WATERSHED PLAN**

PROJECT NO.: **220027 C701**



TRANSFERRED TO THE REGIONAL MUNICIPALITY OF OTTAWA-CARLETON BY ORDER-IN-COUNCIL OC891/81, INST. N5116267
 ROAD No. 36)
 HAZELDEAN ROAD (Regional Road No. 36)



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- WATERSHED NAME
- RUNOFF COEFFICIENT
- AREA IN HECTARES

USE AND INTERPRETATION OF DRAWINGS

GENERAL CONDITIONS OF THE CONTRACT FOR CONSTRUCTION ARE PART OF THE CONTRACT DOCUMENTS AND DESCRIBE USE AND INTENT OF THE DRAWING. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS AND APPROVALS FROM THE LOCAL AUTHORITIES. THESE DRAWINGS ARE COMPLEMENTARY AND NOT TO BE USED IN ISOLATION. ANY CHANGES TO THE DRAWINGS SHALL BE MADE BY THE ENGINEER. UNLESS THE REVISION TITLE IS "ISSUED FOR CONSTRUCTION", THESE DRAWINGS SHALL BE CONSIDERED PRELIMINARY AND SHALL NOT BE USED AS A CONSTRUCTION DOCUMENT.

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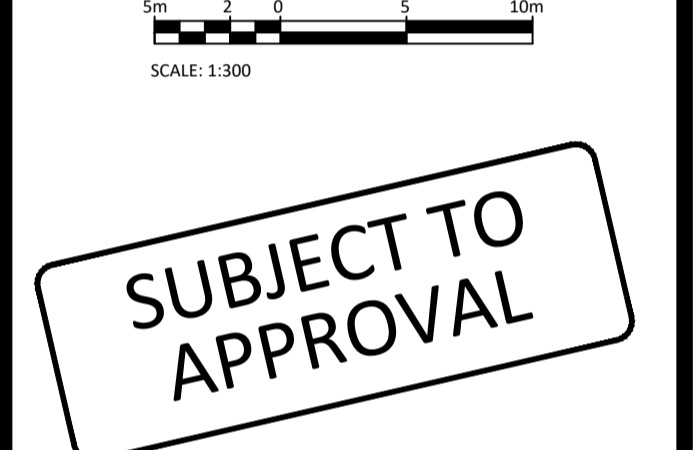
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CONTRACTOR IS ADVISED TO COLLECT INFORMATION ON SOIL CONDITIONS BEFORE START OF CONSTRUCTION.

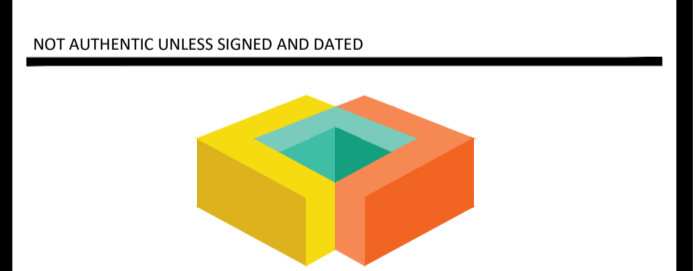
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CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS.



SUBJECT TO APPROVAL

02	ISSUED FOR APPROVAL	M.L.	03 NOV 2025
01	ISSUED FOR APPROVAL	M.L.	21 AUG 2025
No.	REVISIONS	BY	DATE



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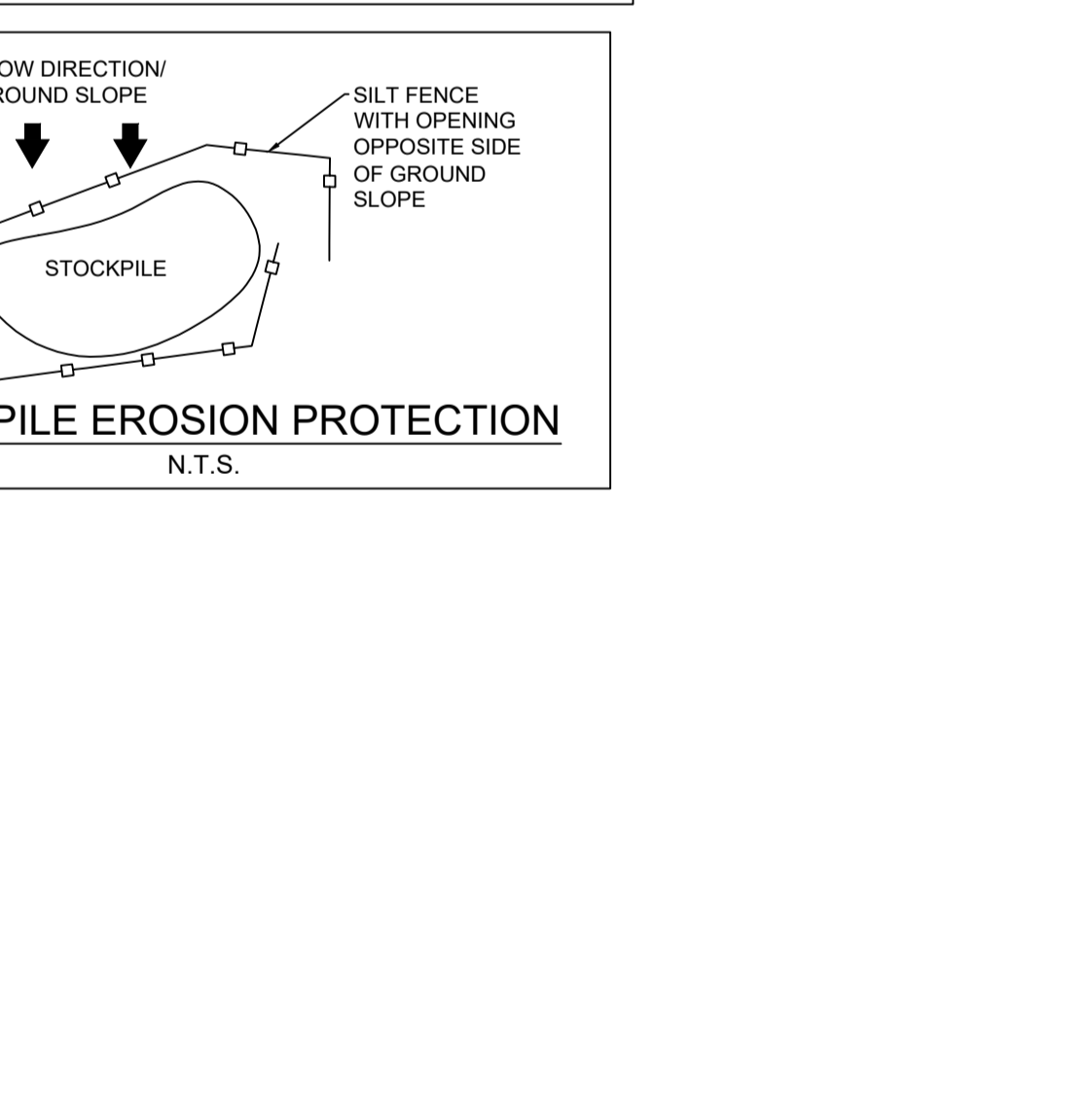
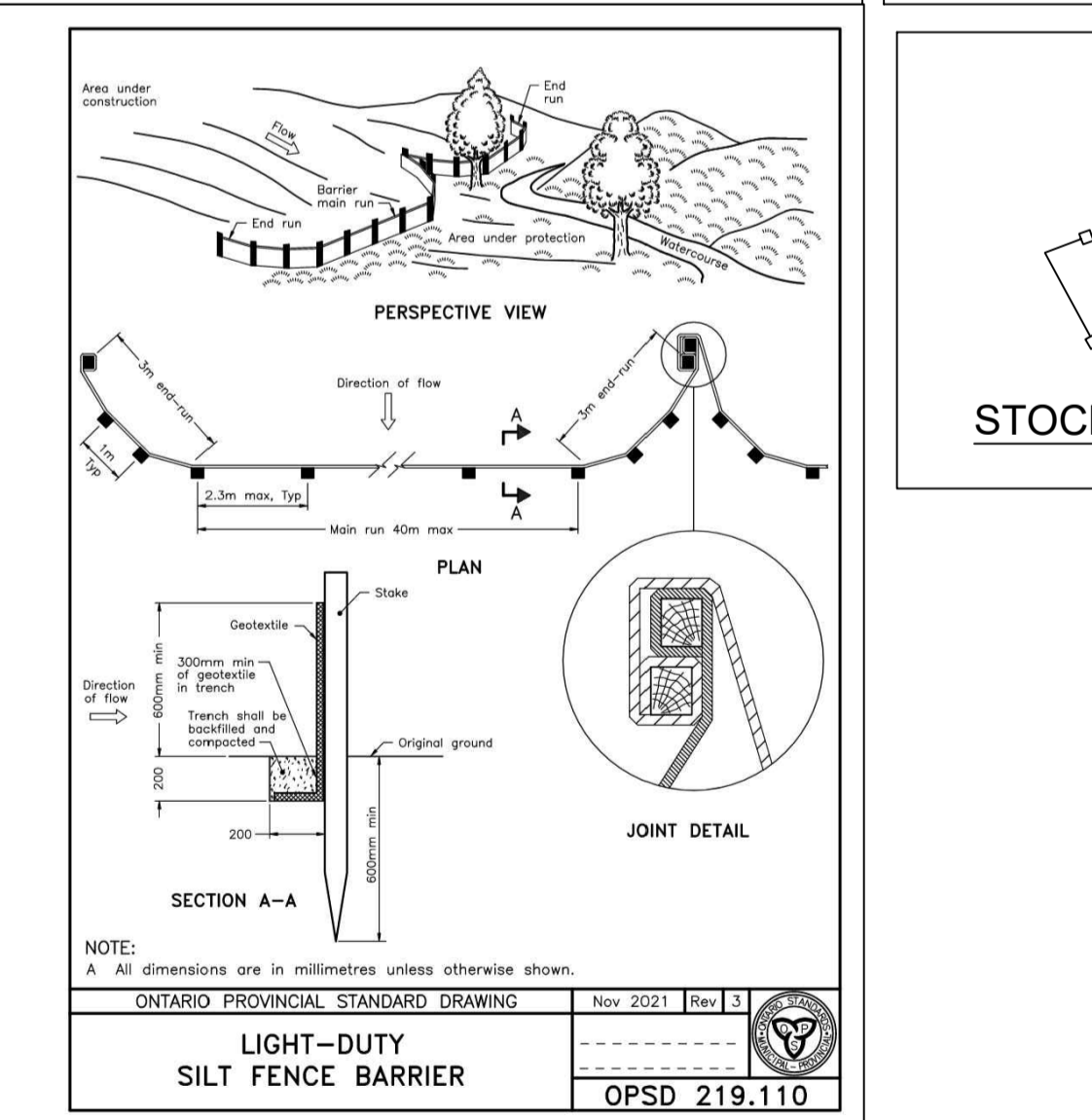
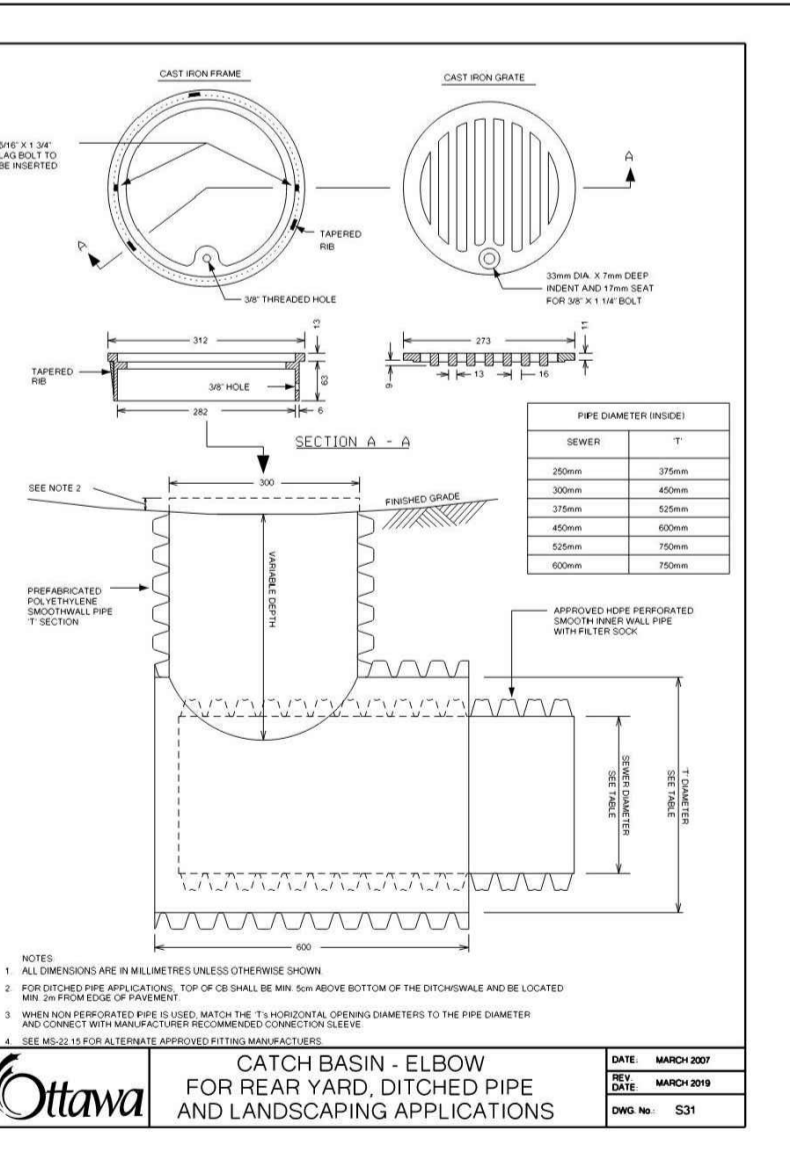
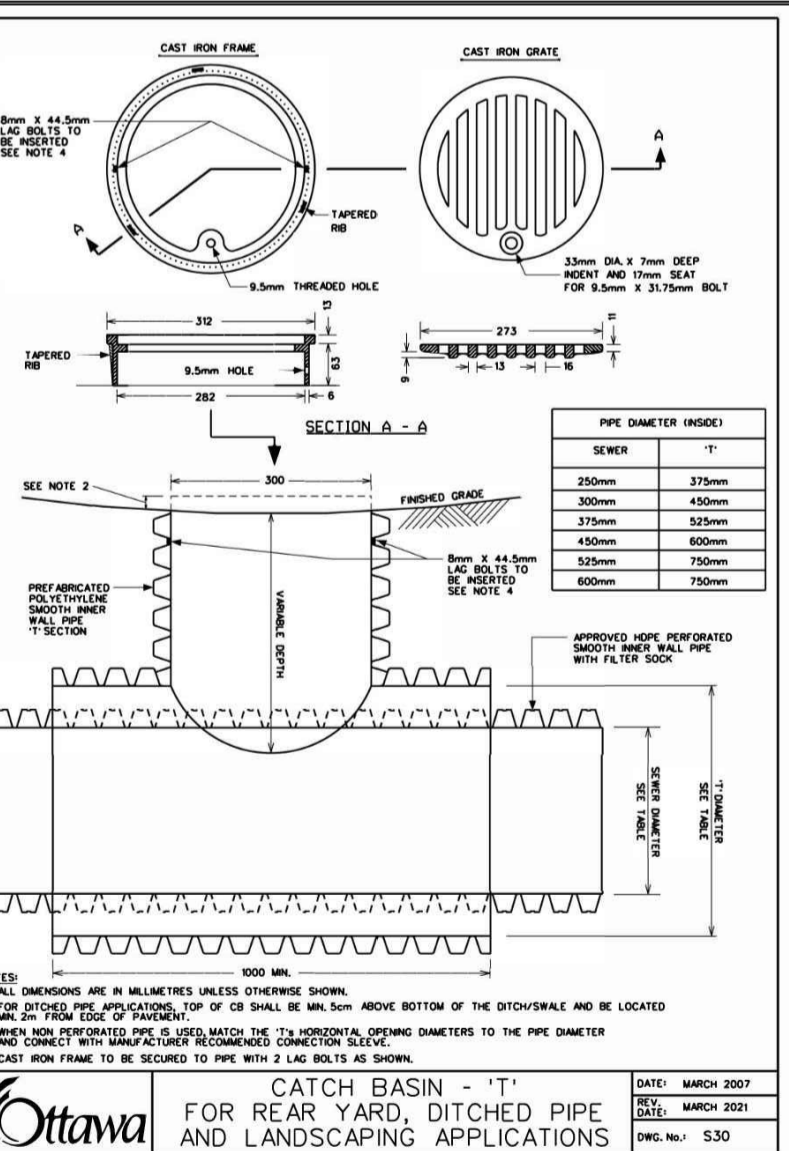
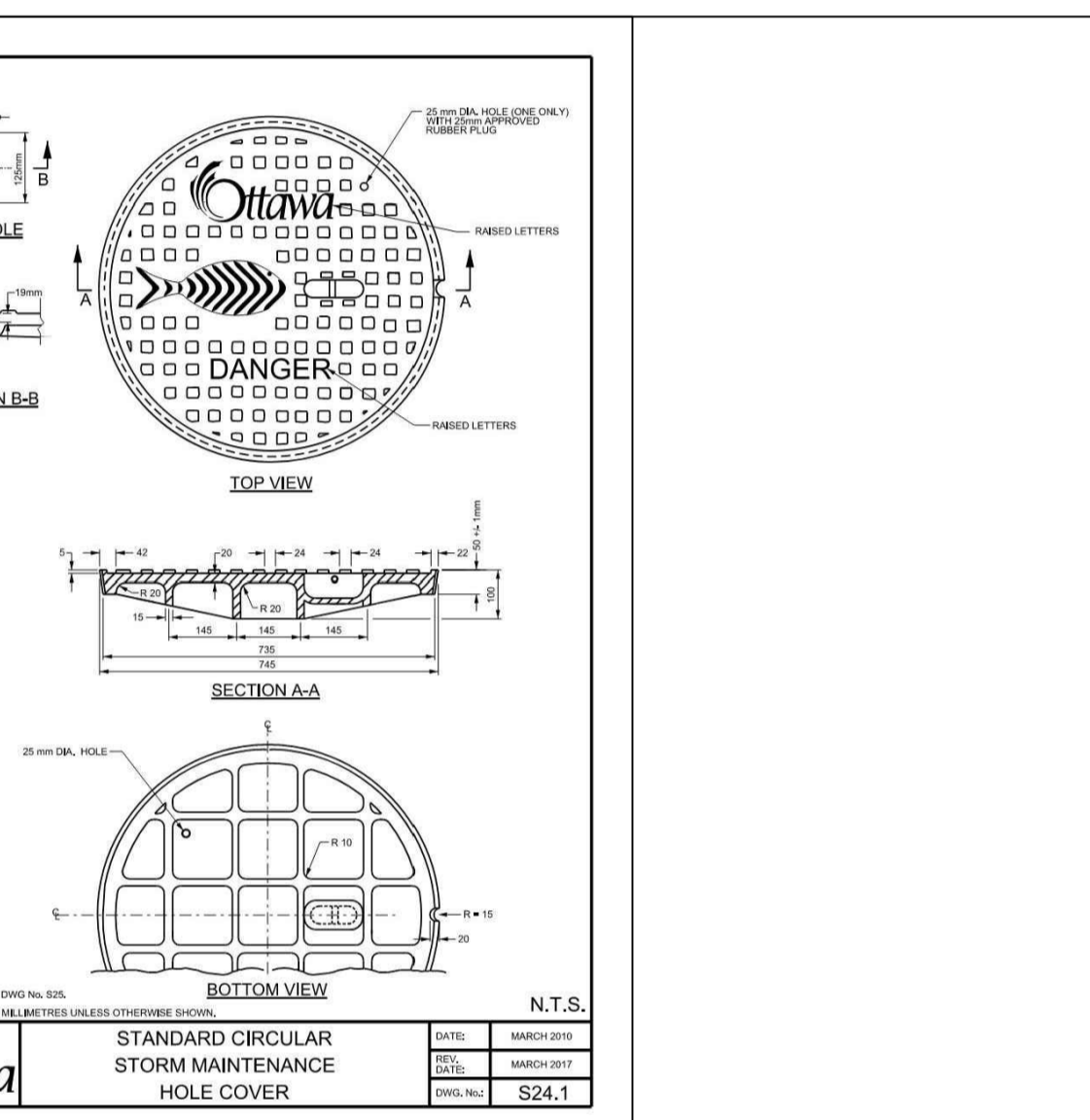
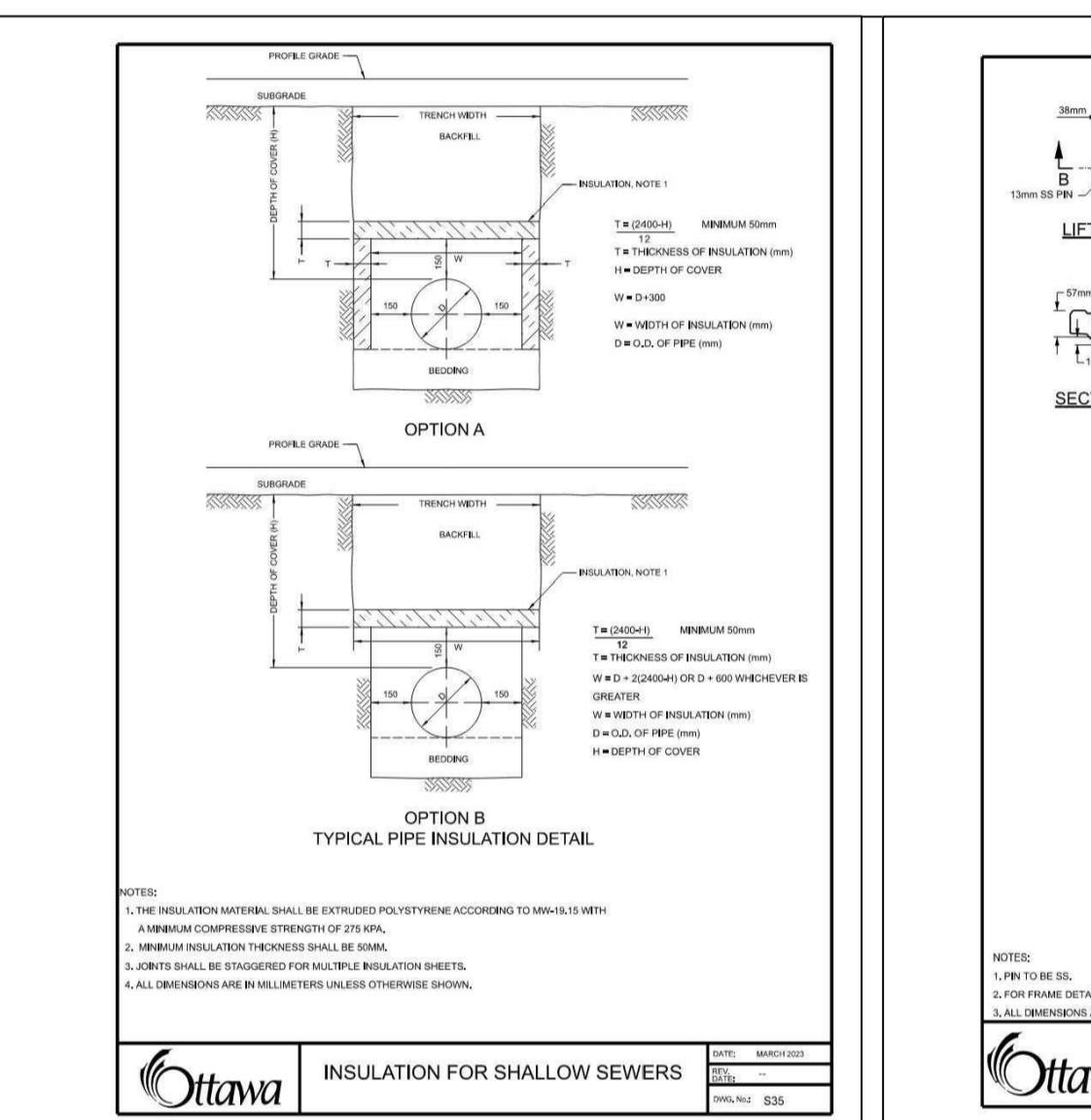
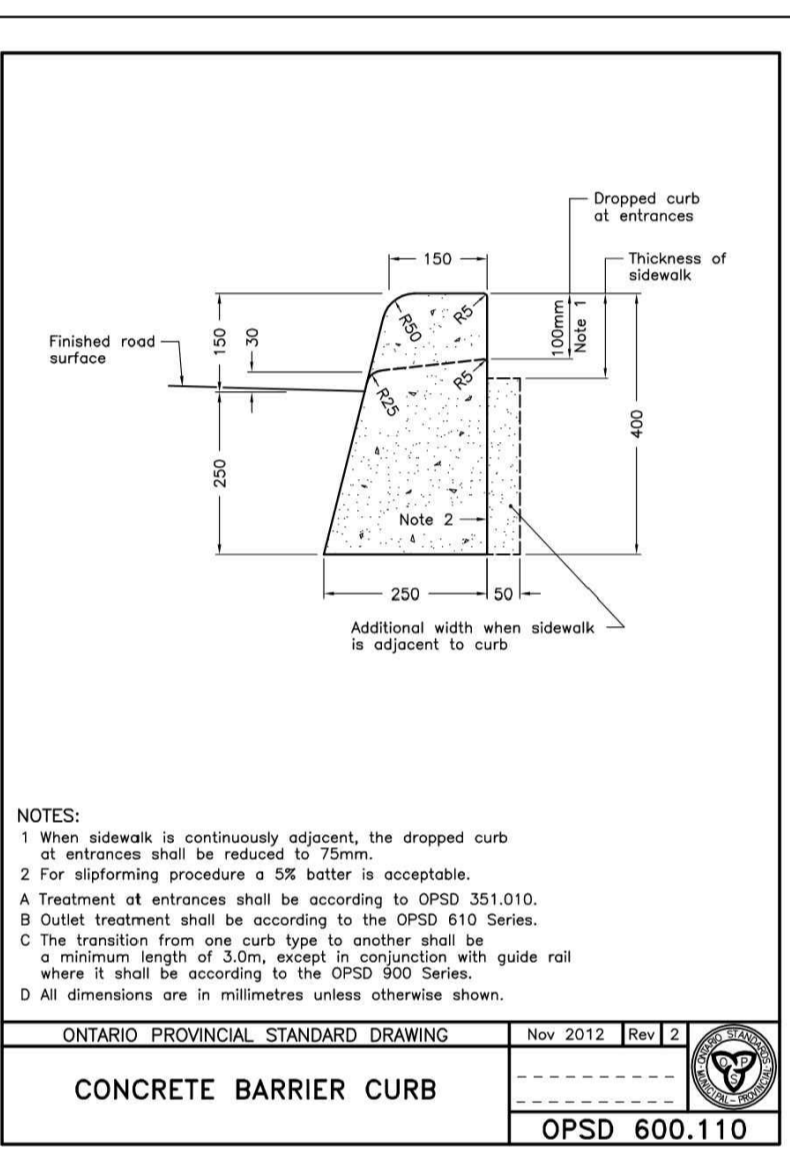
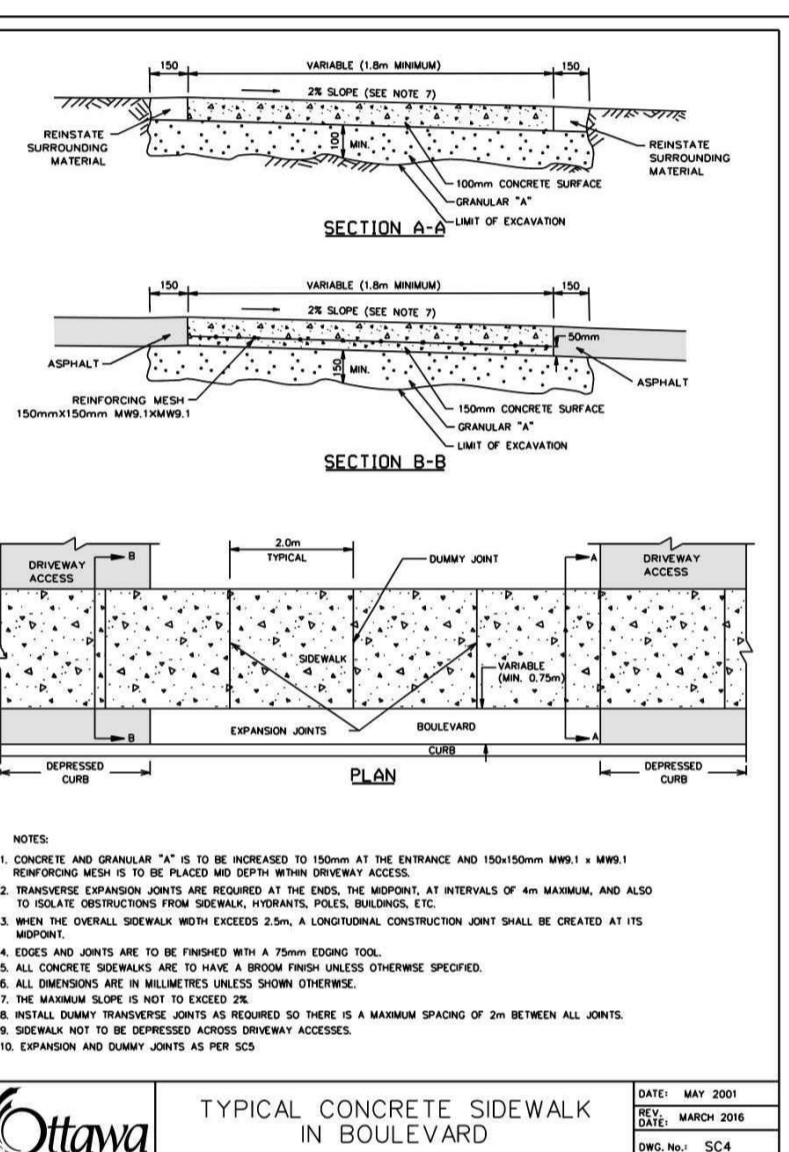
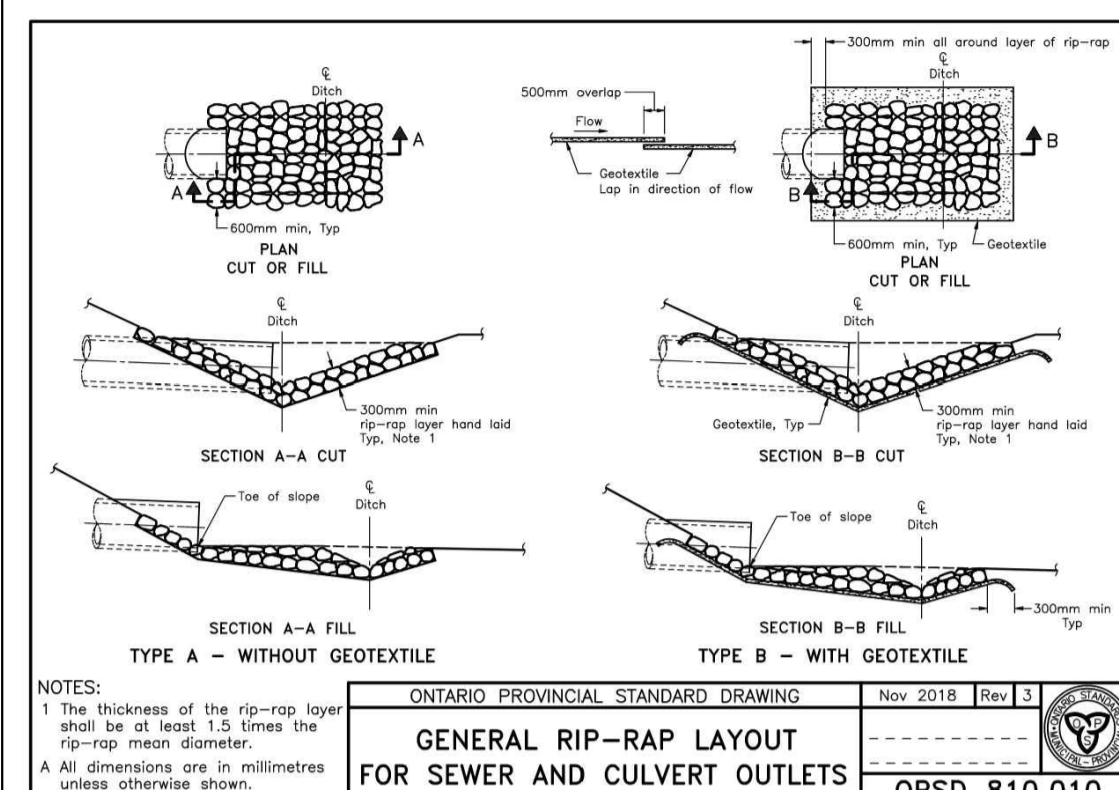
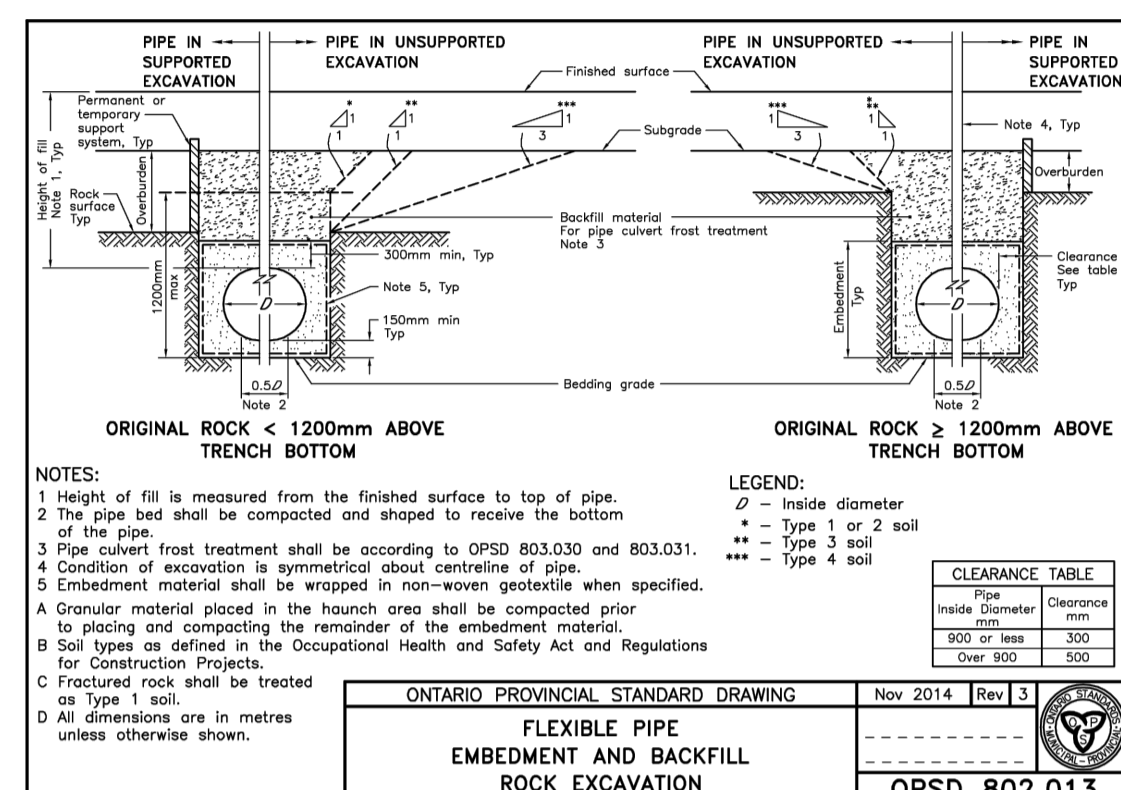
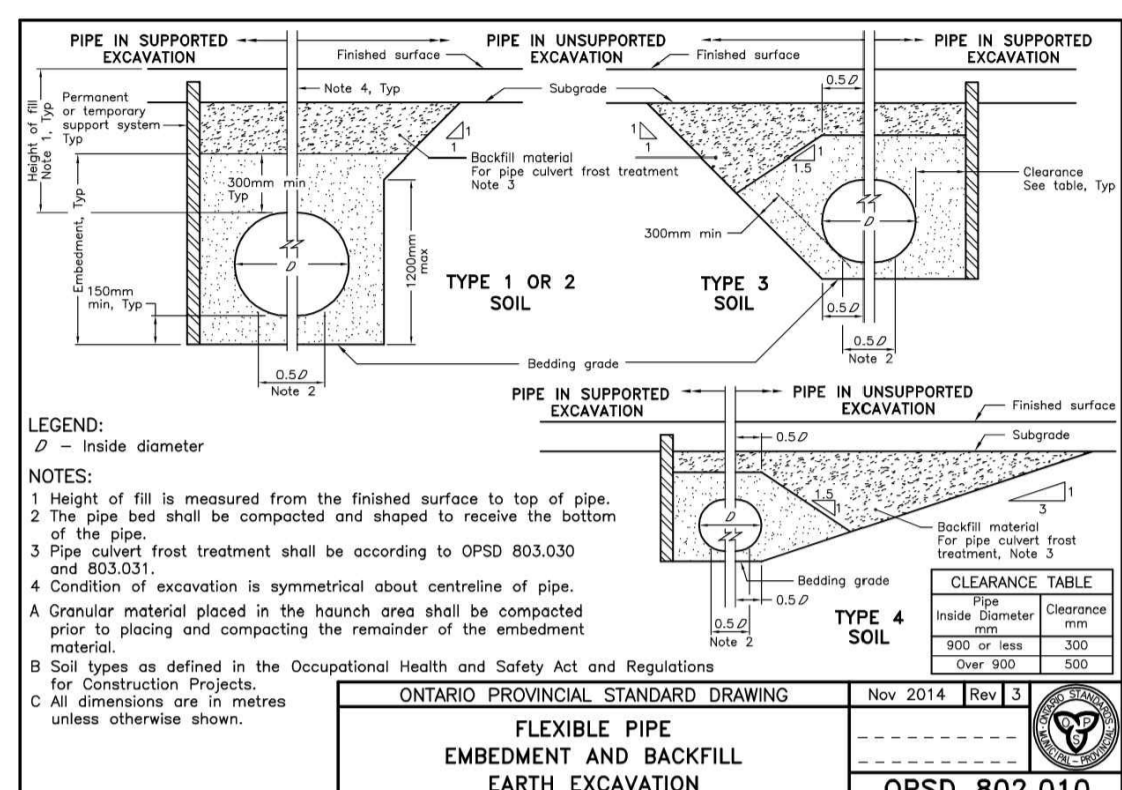
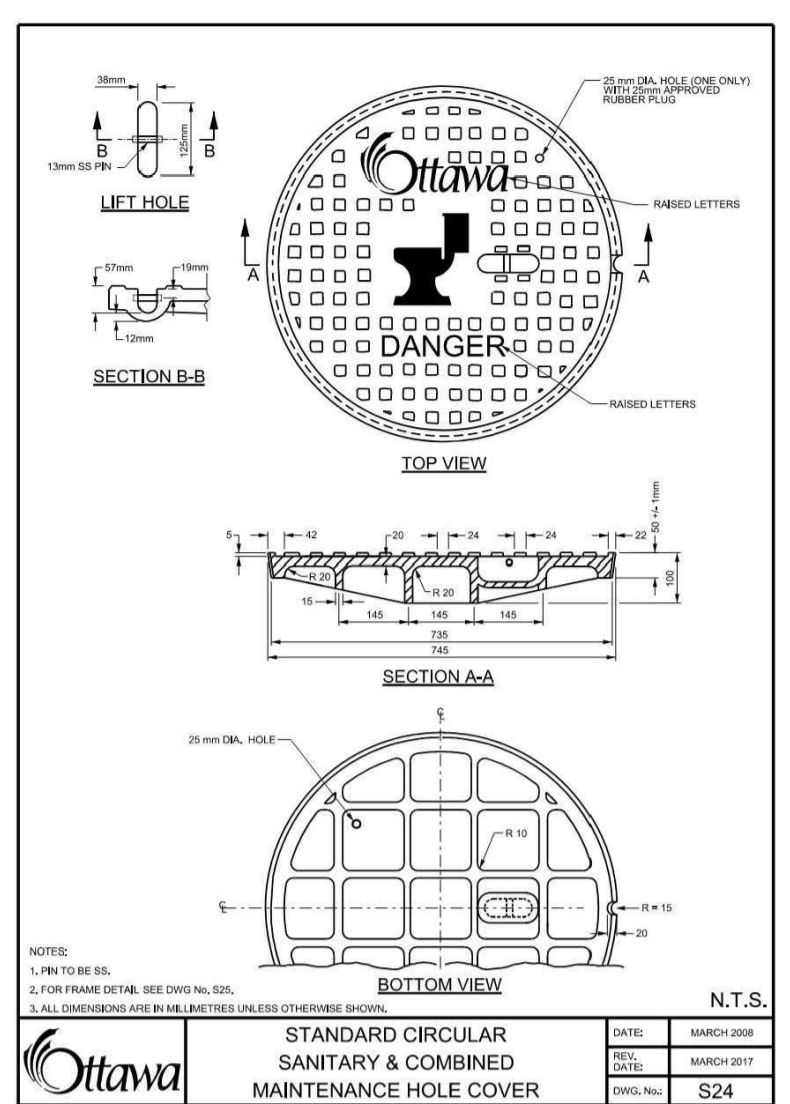
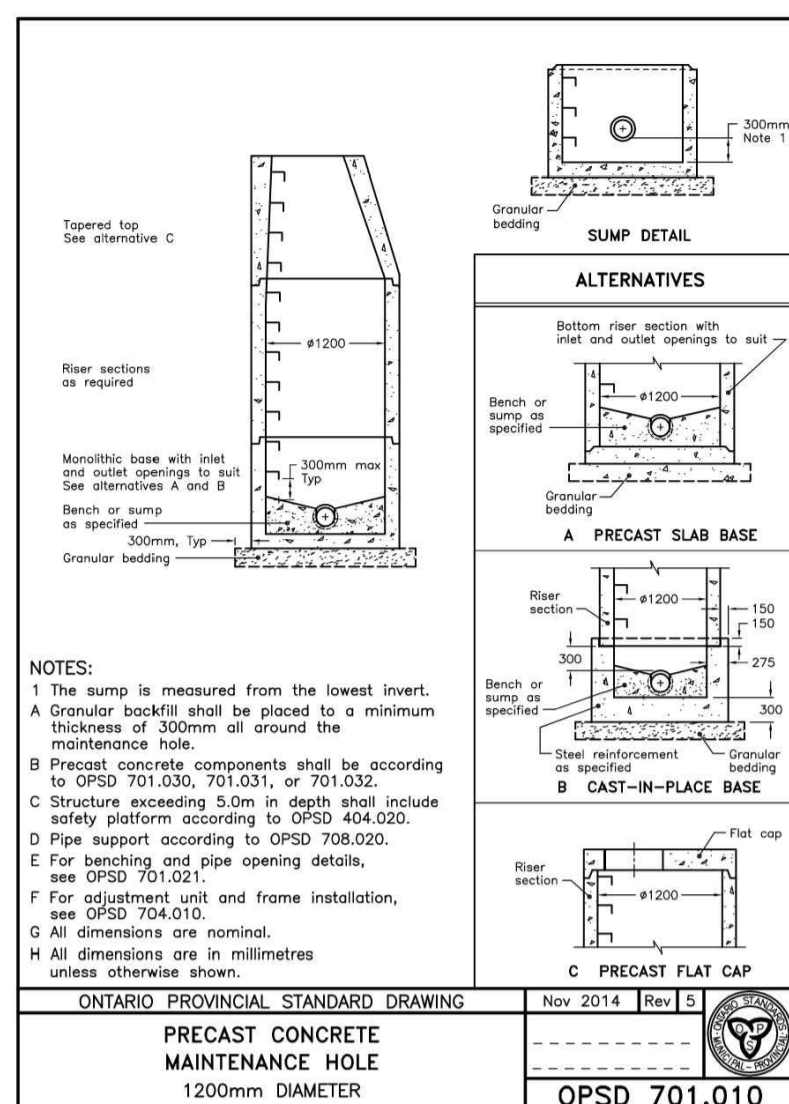
CLIENT: **SCALIA**

DESIGNED BY: M.L. DRAWN BY: M.L. APPROVED BY: M.B.

PROJECT: **MIXED USE APARTMENT DEVELOPMENT
 6310 HAZELDEAN ROAD
 OTTAWA, ON**

DRAWING TITLE: **POST-DEVELOPMENT
 WATERSHED PLAN**

PROJECT NO. **220027 C702**



USE AND INTERPRETATION OF DRAWINGS

GENERAL CONDITIONS OF THE CONTRACT FOR CONSTRUCTION ARE PART OF THE CONTRACT DOCUMENTS AND DESCRIBE THE USE AND INTENT OF THE DRAWING. THE CONTRACT DOCUMENTS INCLUDE NOT ONLY THE DRAWINGS, BUT ALSO THE OWNER-CONTRACTOR AGREEMENT, CONDITIONS OF THE CONTRACT, THE SPECIFICATIONS, ADDENDA, AND MODIFICATIONS ISSUED AFTER EXECUTION OF THE CONTRACT. THESE CONTRACT DOCUMENTS ARE COMPLEMENTARY, AND WHAT IS REQUIRED BY ANY ONE SHALL BE BINDING AS IF REQUIRED BY ALL. WORK NOT COMPLETELY DELINEATED HEREON SHALL BE CONSTRUCTED OF THE SAME MATERIALS AND DETAILED SIMILARLY AS WORK SHOWN MORE COMPLETELY ELSEWHERE IN THE CONTRACT DOCUMENTS.

BY USE OF THE DRAWINGS FOR CONSTRUCTION OF THE PROJECT, THE OWNER CONFIRMS THAT HE HAS REVIEWED AND APPROVED THE DRAWINGS. THE CONTRACTOR CONFIRMS THAT HE HAS VISITED THE SITE, FAMILIARIZED HIMSELF WITH THE LOCAL CONDITIONS, VERIFIED FIELD DIMENSIONS AND CORRELATED HIS OBSERVATIONS WITH THE REQUIREMENTS OF THE CONTRACT DOCUMENTS.

AS INSTRUMENTS OF SERVICE, ALL DRAWINGS, SPECIFICATIONS, CAD FILES OR OTHER ELECTRONIC MEDIA AND COPIES THEREOF FURNISHED BY THE ENGINEER ARE HIS PROPERTY. THEY ARE TO BE USED ONLY FOR THIS PROJECT AND ARE NOT TO BE USED ON ANY OTHER PROJECT, INCLUDING REPEATS OF THE PROJECT. CHANGES TO THE DRAWINGS MAY ONLY BE MADE BY THE ENGINEER.

UNLESS THE REVISION TITLE IS ISSUED FOR CONSTRUCTION, THESE DRAWINGS SHALL BE CONSIDERED PRELIMINARY AND SHALL NOT BE USED AS A CONSTRUCTION DOCUMENT.

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SUBJECT TO APPROVAL

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No. REVISIONS BY DATE

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www.lrl.ca | (613) 842-3434

CLIENT: **SCALIA**

DESIGNED BY: M.L. DRAWN BY: M.L. APPROVED BY: M.B.

PROJECT: **MIXED USE APARTMENT DEVELOPMENT
6310 HAZELDEAN ROAD
OTTAWA, ON**

DRAWING TITLE: **CONSTRUCTION DETAIL PLAN**

PROJECT NO.: **220027 C901**

APPENDIX F
Sanitary Calculations



LRL Associates Ltd.
Sanitary Sewer Design Sheet



LRL File No.: 220027
Project: Mixed Use Apartment Development
Location: 6310 Hazeldean Road
Designed: ML
Checked: MB
Date: October 24, 2025
DWG. Reference: C401

Sanitary Design Parameters

Commercial & Institutional Flow = 28000 L/ha/day
 Light Industrial Flow = 35000 L/ha/day
 Heavy Industrial Flow = 55000 L/ha/day
 Maximum Residential Peak Factor = 4.0
 Commercial & Institutional Peak Factor = 1

Average Daily Flow = 280 L/p/day
 Industrial Peak Factor = as per Appendix 4-B
 Extraneous Flow = 0.33 L/s/ha

Pipe Design Parameters

Maximum Velocity = 3.00 m/s
 Minimum Velocity = 0.60 m/s
 Manning's n = 0.013

LOCATION			RESIDENTIAL						COMMERCIAL		INDUSTRIAL			INSTITUTIONAL		C+I+I	INFILTRATION			TOTAL FLOW, Q	PIPE								
STREET/SITE	FROM	TO	AREA	POP.	ACCU.		PEAK FACT.	PEAK FLOW	AREA	ACCU. AREA	AREA	ACCU. AREA	PEAK FACT.	AREA	ACCU. AREA	PEAK FLOW	TOTAL AREA	ACCU. AREA	INFILT. FLOW		LENGTH	DIA.	SLOPE	MATERIAL	CAP. Q _{FULL}	VEL. V _{FULL}	RATIO Q/Q _{FULL}	RATIO V _{ACT} /V _{FULL}	VEL. V _{ACT}
			(Ha)		AREA	POP.		(L/s)	(Ha)	(Ha)		(Ha)		(Ha)	(Ha)	(L/s)	(Ha)	(Ha)	(L/s)	(L/s)	(m)	(mm)	(%)		(L/s)	(m/s)			
Site	BLDG /STUB	SAN MH01	1.070	819	1.070	819	3.4	9.02	1.070	1.070						0.35	1.070	1.070	0.35	9.72	1.1	375	1.00%	PVC	175.33	1.59	0.055	0.54	0.85
Easement	SAN MH01	SAN MH02																		9.72	120.6	375	1.00%	PVC	175.33	1.59	0.055	0.54	0.85

Notes: Existing inverts and slopes are estimated. They are to be confirmed on-site.

APPENDIX G
Stormwater Management Design Calculations



LRL Associates Ltd.

Storm Watershed Summary



LRL File No. 220027

Project: Mixed Use Apartment Development

Location: 6310 Hazeldean Road

Date: October 20, 2025

Designed: Maxime Longtin

Checked: Mohan Basnet

Dwg Reference: C701, C702

Pre-Development Catchments

Catchment	C = 0.20	C = 0.80	C = 0.90	Total Area (ha)	Combined C
ECA-01 (uncontrolled)	0.155	0.900	0.016	1.070	0.71
Total	0.155	0.900	0.016	1.070	0.71

Post-Development Catchments

Catchment	C = 0.20	C = 0.8	C = 0.90	Total Area (ha)	Combined C
CA-01 (controlled)	0.000	0.000	0.497	0.497	0.90
CA-02 (controlled)	0.013	0.000	0.152	0.165	0.84
CA-03A (controlled)	0.002	0.000	0.004	0.005	0.68
CA-03B (controlled)	0.002	0.000	0.003	0.005	0.66
CA-03C (controlled)	0.001	0.000	0.003	0.004	0.72
CA-03D (controlled)	0.005	0.000	0.004	0.009	0.53
CA-03E (controlled)	0.004	0.000	0.004	0.008	0.52
CA-03F (controlled)	0.005	0.000	0.004	0.009	0.52
CA-03G (controlled)	0.005	0.000	0.003	0.009	0.47
CA-03H (controlled)	0.005	0.000	0.007	0.011	0.62
CA-04 (controlled)	0.006	0.000	0.041	0.047	0.81
CA-05 (controlled)	0.002	0.000	0.071	0.072	0.88
CA-06 (controlled)	0.000	0.000	0.033	0.033	0.90
CA-07 (controlled)	0.000	0.000	0.034	0.034	0.90
CA-08 (controlled)	0.000	0.000	0.019	0.019	0.90
CA-09 (controlled)	0.000	0.000	0.019	0.019	0.90
CA-10 (uncontrolled)	0.095	0.000	0.013	0.108	0.29
CA-11 (uncontrolled)	0.006	0.000	0.010	0.016	0.63
Total	0.150	0.000	0.920	1.070	0.80



LRL File No. 220027
Project: Mixed Use Apartment Development
Location: 6310 Hazeldean Road
Date: October 20, 2025
Designed: Maxime Longtin
Checked: Mohan Basnet
Drawing Ref.: C601

**Stormwater Management
Design Sheet**

STORM - 5 YEAR

Runoff Equation

$$Q = 2.78CIA \text{ (L/s)}$$

C = Runoff coefficient

$$I = \text{Rainfall intensity (mm/hr)} = A / (T_d + C)^B$$

A = Area (ha)

T_d = Time of duration (min)

Pre-Development Release Rate

IDF Curve Equations

$$I_5 = 998.071 / (T_d + 6.053)^{0.814}$$

$$A = 998.071$$

$$B = 0.814$$

$$C = 6.053$$

C = 0.50 (max of 0.5 as per City Guidelines)

I₅ = 104.2 mm/hr

T_d = 10 min

A = 1.07 ha

5 Year Release Rate = 155.00 L/s



LRL File No. 220027
Project: Mixed Use Apartment Development
Location: 6310 Hazeldean Road
Date: October 20, 2025
Designed: Maxime Longtin
Checked: Mohan Basnet
Drawing Ref.: C601

**Stormwater Management
 Design Sheet**

STORM - 100 YEAR

Runoff Equation

Q = 2.78CIA (L/s)
 C = Runoff coefficient
 I = Rainfall intensity (mm/hr) = $A / (T_d + C)^B$
 A = Area (ha)
 T_d = Time of duration (min)

Pre-Development Release Rate

IDF Curve Equations

$I_{100} = 1735.688 / (T_d + 6.014)^{0.820}$ A = 1735.688 B = 0.820 C = 6.014

C = 0.50 (max of 0.5 as per City Guidelines)
 I₁₀₀ = 178.6 mm/hr
 T_d = 10 min
 A = 1.07 ha
 100 Year Release Rate = 265.62 L/s
 Allowable Release Rate = 155.00 L/s (5 Year Pre-development Release Rate)

Post-development Stormwater Management

				ΣR =	ΣR _{2&5}	ΣR ₁₀₀
Total Site Area =	1.070	ha		ΣR =	0.80	1.00
CA-01 (controlled)	0.497	ha		R =	0.90	1.00
CA-02 (controlled)	0.165	ha		R =	0.84	1.00
CA-03A (controlled)	0.005	ha		R =	0.68	0.86
CA-03B (controlled)	0.005	ha		R =	0.66	0.82
CA-03C (controlled)	0.004	ha		R =	0.72	0.89
CA-03D (controlled)	0.009	ha		R =	0.53	0.66
CA-03E (controlled)	0.008	ha		R =	0.52	0.65
CA-03F (controlled)	0.009	ha		R =	0.52	0.65
CA-03G (controlled)	0.009	ha		R =	0.47	0.59
CA-03H (controlled)	0.011	ha		R =	0.62	0.77
Cistern 1 controlled	0.722	ha		R =	0.86	1.00
CA-04 (controlled)	0.047	ha		R =	0.81	1.00
CA-05 (controlled)	0.072	ha		R =	0.88	1.00
CA-06 (controlled)	0.033	ha		R =	0.90	1.00
CA-07 (controlled)	0.034	ha		R =	0.90	1.00
CA-08 (controlled)	0.019	ha		R =	0.90	1.00
CA-09 (controlled)	0.019	ha		R =	0.90	1.00
Cistern 2 controlled	0.224	ha		R =	0.88	1.00
Total (controlled)	0.946	ha		R =	0.86	1.00
CA-10 (uncontrolled)	0.108	ha		R =	0.29	0.36
CA-11 (uncontrolled)	0.016	ha		R =	0.63	0.78
Total (uncontrolled)	0.124	ha		R =	0.33	0.41
Total	1.070	ha		R =	0.80	1.00

100 Year Post-development Stormwater Management (Cistern 1)

Time (min)	Intensity (mm/hr)	Controlled Runoff (L/s)	Storage Volume (m ³)	Controlled Release Rate (L/s)	Uncontrolled Runoff (L/s)	Total Release Rate (L/s)
10	178.56	358.55	156.82	97.18	25.42	122.60
15	142.89	286.93	170.77	97.18	20.34	117.52
20	119.95	240.86	172.41	97.18	17.07	114.26
25	103.85	208.52	167.01	97.18	14.78	111.97
30	91.87	184.47	157.11	97.18	13.08	110.26
35	82.58	165.82	144.13	97.18	11.75	108.94
40	75.15	150.89	128.90	97.18	10.70	107.88
45	69.05	138.65	111.96	97.18	9.83	107.01
50	63.95	128.42	93.70	97.18	9.10	106.29
55	59.62	119.72	74.38	97.18	8.49	105.67
60	55.89	112.24	54.18	97.18	7.96	105.14



LRL File No. 220027
Project: Mixed Use Apartment Development
Location: 6310 Hazeldean Road
Date: October 20, 2025
Designed: Maxime Longtin
Checked: Mohan Basnet
Drawing Ref.: C601

**Stormwater Management
 Design Sheet**

65	52.65	105.71	33.26	97.18	7.49	104.68
70	49.79	99.98	11.73	97.18	7.09	104.27
75	47.26	94.89	0.00	97.18	6.73	103.91
80	44.99	90.34	0.00	97.18	6.40	103.59
85	42.95	86.25	0.00	97.18	6.11	103.30
90	41.11	82.55	0.00	97.18	5.85	103.04
95	39.43	79.18	0.00	97.18	5.61	102.80
100	37.90	76.11	0.00	97.18	5.39	102.58
105	36.50	73.29	0.00	97.18	5.19	102.38
110	35.20	70.69	0.00	97.18	5.01	102.20
115	34.01	68.28	0.00	97.18	4.84	102.03
120	32.89	66.05	0.00	97.18	4.68	101.87

On-site stormwater detention

Storage required = 172.41 m³ (Refer to DWG C601)

100 Year Post-development Stormwater Management (Cistern 2)

Time (min)	Intensity (mm/hr)	Controlled Runoff (L/s)	Storage Volume (m ³)	Controlled Release Rate (L/s)	Uncontrolled Runoff (L/s)	Total Release Rate (L/s)
10	178.56	110.99	47.16	32.39	0.00	32.39
15	142.89	88.82	50.79	32.39	0.00	32.39
20	119.95	74.56	50.60	32.39	0.00	32.39
25	103.85	64.55	48.24	32.39	0.00	32.39
30	91.87	57.11	44.48	32.39	0.00	32.39
35	82.58	51.33	39.77	32.39	0.00	32.39
40	75.15	46.71	34.36	32.39	0.00	32.39
45	69.05	42.92	28.42	32.39	0.00	32.39
50	63.95	39.75	22.08	32.39	0.00	32.39
55	59.62	37.06	15.40	32.39	0.00	32.39
60	55.89	34.74	8.46	32.39	0.00	32.39
65	52.65	32.73	1.29	32.39	0.00	32.39
70	49.79	30.95	0.00	32.39	0.00	32.39
75	47.26	29.37	0.00	32.39	0.00	32.39
80	44.99	27.97	0.00	32.39	0.00	32.39
85	42.95	26.70	0.00	32.39	0.00	32.39
90	41.11	25.55	0.00	32.39	0.00	32.39
95	39.43	24.51	0.00	32.39	0.00	32.39
100	37.90	23.56	0.00	32.39	0.00	32.39
105	36.50	22.69	0.00	32.39	0.00	32.39
110	35.20	21.88	0.00	32.39	0.00	32.39
115	34.01	21.14	0.00	32.39	0.00	32.39
120	32.89	20.45	0.00	32.39	0.00	32.39

On-site stormwater detention

Storage required = 50.79 m³ (Refer to DWG C601)

Summary

Catchment	Release Rate	Required Storage	Remarks
	(L/s)	(m ³)	
CA-01 to CA-03 (Cistern 1)	97.18	172.41	Controlled
CA-04 to CA-09 (Cistern 2)	32.39	50.79	Controlled
CA-10 to CA-11	25.42	N/A	Uncontrolled
Total	155.00	223.20	

LRL Associates Ltd.
Storm Sewer Design Sheet



LRL File No. 220027
Project: Mixed Use Apartment Development
Location: 6310 Hazeldean Road
Date: October 27, 2025
Designed: Maxime Longtin
Checked: Mohan Basnet
Dwg. Ref.: C401,C702

Rational Method
 Q = 2.78CIA
 Q = Peak flow (L/s)
 A = Drainage area (ha)
 C = Runoff coefficient
 I = Rainfall intensity (mm/hr)
Runoff coefficient (C)
 Grass = 0.2
 Gravel = 0.8
 Asphalt / rooftop = 0.9

IDF curve
 Ottawa Macdonald-Cartier International Airport
 Storm event: 5 Years
Intensity equation:
 $I_s = 998.071 / (Td + 6.053)^{0.814}$ (mm/hr)
Pipe Design Parameters
 Minimum velocity = 0.80 m/s
 Manning's "n" = 0.013

LOCATION			AREA (ha)			FLOW						STORM SEWER							
WATERSHED / STREET	From MH	To MH	C = 0.20	C = 0.80	C = 0.90	Indiv. 2.78AC	Accum. 2.78AC	Time of Conc.	Rainfall Intensity	Peak Flow (Q)	Controlled Flow (Q)	Pipe Dia.	Type	Slope	Length	Capacity Full (Q _{FULL})	Velocity Full	Time of Flow	Ratio Q/Q _{FULL}
									(mm/hr)	(L/s)	(L/s)								
Cistern 1																			
CA-01			0.000	0.000	0.497	1.24	1.24												
CA-02			0.013	0.000	0.152	0.39	1.63												
CA-03			0.028	0.000	0.032	0.10	1.73												
	STM STUB	Ex. Ditch					1.73	10.00	104.19	179.94	97.18	300	PVC	2.00%	4.2	136.76	1.93	0.04	0.71
Cistern 2																			
CA-04			0.006	0.000	0.041	0.11	0.11												
CA-05			0.002	0.000	0.071	0.18	0.28												
CA-06			0.000	0.000	0.033	0.08	0.37												
CA-07			0.000	0.000	0.034	0.08	0.45												
CA-08			0.000	0.000	0.019	0.05	0.50												
CA-09			0.000	0.000	0.019	0.05	0.54												
	STM MH01	OGS					0.54	10.00	104.19	56.69	32.39	250	PVC	2.00%	2.8	84.10	1.71	0.03	0.39
	OGS	Ex. Ditch					0.54	10.03	104.05	56.61	32.39	250	PVC	2.00%	7.4	84.10	1.71	0.07	0.39

Stormceptor®EF Sizing Report

Imbrium® Systems		08/07/2025																	
ESTIMATED NET ANNUAL SEDIMENT (TSS) LOAD REDUCTION																			
Province:	Ontario	Project Name:	Hazeldean Residential Towers																
City:	Ottawa	Project Number:	220027																
Nearest Rainfall Station:	OTTAWA CDA RCS	Designer Name:	Jessica Steffler																
Climate Station Id:	6105978	Designer Company:	Forterra Pipe & Precast																
Years of Rainfall Data:	20	Designer Email:	jessica.steffler@RinkerPipe.com																
Site Name:	6310 Hazeldean Road OGS	Designer Phone:	519-239-6958																
Drainage Area (ha):	0.22	EOR Name:	Maxime Longtin																
Runoff Coefficient 'c':	0.84	EOR Company:	LRL Engineering																
Particle Size Distribution:	Fine	EOR Email:	mlongtin@lrl.ca																
Target TSS Removal (%):	80.0	EOR Phone:	613-842-3434																
Required Water Quality Runoff Volume Capture (%):	90.00	<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th colspan="2" style="text-align: center;">Net Annual Sediment (TSS) Load Reduction Sizing Summary</th> </tr> <tr> <th style="width: 50%;">Stormceptor Model</th> <th style="width: 50%;">TSS Removal Provided (%)</th> </tr> </thead> <tbody> <tr> <td style="background-color: yellow;">EFO4</td> <td style="background-color: yellow;">94</td> </tr> <tr> <td>EFO5</td> <td>96</td> </tr> <tr> <td>EFO6</td> <td>98</td> </tr> <tr> <td>EFO8</td> <td>99</td> </tr> <tr> <td>EFO10</td> <td>100</td> </tr> <tr> <td>EFO12</td> <td>100</td> </tr> </tbody> </table>		Net Annual Sediment (TSS) Load Reduction Sizing Summary		Stormceptor Model	TSS Removal Provided (%)	EFO4	94	EFO5	96	EFO6	98	EFO8	99	EFO10	100	EFO12	100
Net Annual Sediment (TSS) Load Reduction Sizing Summary																			
Stormceptor Model	TSS Removal Provided (%)																		
EFO4	94																		
EFO5	96																		
EFO6	98																		
EFO8	99																		
EFO10	100																		
EFO12	100																		
Estimated Water Quality Flow Rate (L/s):	5.96																		
Oil / Fuel Spill Risk Site?	Yes																		
Upstream Flow Control?	No																		
Peak Conveyance (maximum) Flow Rate (L/s):	28.99																		
Influent TSS Concentration (mg/L):	200																		
Estimated Average Annual Sediment Load (kg/yr):	253																		
Estimated Average Annual Sediment Volume (L/yr):	206																		
Recommended Stormceptor EFO Model:		EFO4																	
Estimated Net Annual Sediment (TSS) Load Reduction (%):		94																	
Water Quality Runoff Volume Capture (%):		> 90																	



Stormceptor® **EF** Sizing Report

THIRD-PARTY TESTING AND VERIFICATION

► **Stormceptor® EF and Stormceptor® EFO** are the latest evolutions in the Stormceptor® oil-grit separator (OGS) technology series, and are designed to remove a wide variety of pollutants from stormwater and snowmelt runoff. These technologies have been third-party tested in accordance with the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators** and performance has been third-party verified in accordance with the **ISO 14034 Environmental Technology Verification (ETV)** protocol.

PERFORMANCE

► **Stormceptor® EF and EFO** remove stormwater pollutants through gravity separation and floatation, and feature a patent-pending design that generates positive removal of total suspended solids (TSS) throughout each storm event, including high-intensity storms. Captured pollutants include sediment, free oils, and sediment-bound pollutants such as nutrients, heavy metals, and petroleum hydrocarbons. Stormceptor is sized to remove a high level of TSS from the frequent rainfall events that contribute the vast majority of annual runoff volume and pollutant load. The technology incorporates an internal bypass to convey excessive stormwater flows from high-intensity storms through the device without resuspension and washout (scour) of previously captured pollutants. Proper routine maintenance ensures high pollutant removal performance and protection of downstream waterways.

PARTICLE SIZE DISTRIBUTION (PSD)

► The **Canadian ETV PSD** shown in the table below was used, or in part, for this sizing. This is the identical PSD that is referenced in the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators** for both sediment removal testing and scour testing. The Canadian ETV PSD contains a wide range of particle sizes in the sand and silt fractions, and is considered reasonably representative of the particle size fractions found in typical urban stormwater runoff.

Particle Size (µm)	Percent Less Than	Particle Size Fraction (µm)	Percent
1000	100	500-1000	5
500	95	250-500	5
250	90	150-250	15
150	75	100-150	15
100	60	75-100	10
75	50	50-75	5
50	45	20-50	10
20	35	8-20	15
8	20	5-8	10
5	10	2-5	5
2	5	<2	5



Stormceptor®EF Sizing Report

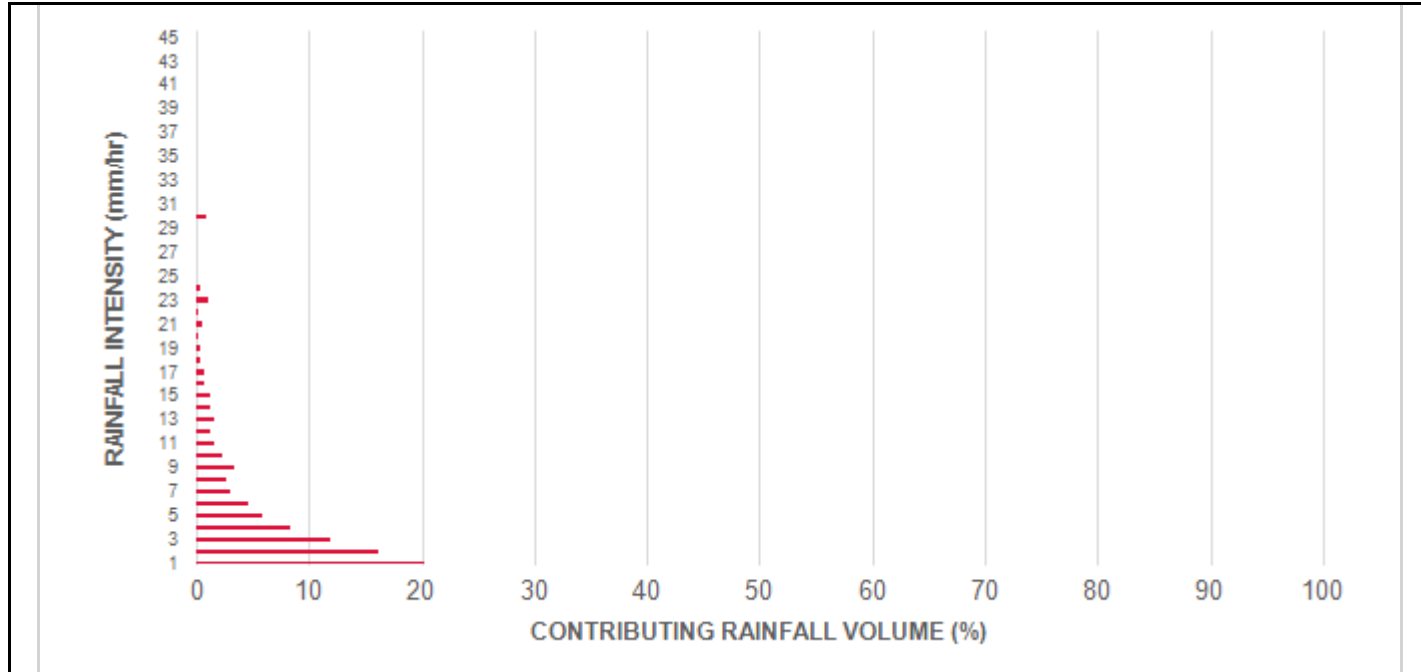
Rainfall Intensity (mm / hr)	Percent Rainfall Volume (%)	Cumulative Rainfall Volume (%)	Flow Rate (L/s)	Flow Rate (L/min)	Surface Loading Rate (L/min/m²)	Removal Efficiency (%)	Incremental Removal (%)	Cumulative Removal (%)
0.50	8.6	8.6	0.26	15.0	13.0	100	8.6	8.6
1.00	20.3	29.0	0.51	31.0	26.0	100	20.3	29.0
2.00	16.2	45.2	1.03	62.0	51.0	100	16.2	45.2
3.00	12.0	57.2	1.54	92.0	77.0	100	12.0	57.2
4.00	8.4	65.6	2.05	123.0	103.0	96	8.1	65.3
5.00	5.9	71.6	2.57	154.0	128.0	93	5.6	70.8
6.00	4.6	76.2	3.08	185.0	154.0	89	4.1	75.0
7.00	3.1	79.3	3.60	216.0	180.0	86	2.6	77.6
8.00	2.7	82.0	4.11	247.0	205.0	83	2.3	79.9
9.00	3.3	85.3	4.62	277.0	231.0	82	2.7	82.6
10.00	2.3	87.6	5.14	308.0	257.0	81	1.9	84.4
11.00	1.6	89.2	5.65	339.0	283.0	79	1.2	85.7
12.00	1.3	90.5	6.16	370.0	308.0	78	1.0	86.7
13.00	1.7	92.2	6.68	401.0	334.0	77	1.3	88.1
14.00	1.2	93.5	7.19	432.0	360.0	76	0.9	89.0
15.00	1.2	94.6	7.71	462.0	385.0	75	0.9	89.8
16.00	0.7	95.3	8.22	493.0	411.0	73	0.5	90.4
17.00	0.7	96.1	8.73	524.0	437.0	72	0.5	90.9
18.00	0.4	96.5	9.25	555.0	462.0	71	0.3	91.2
19.00	0.4	96.9	9.76	586.0	488.0	70	0.3	91.5
20.00	0.2	97.1	10.27	616.0	514.0	69	0.1	91.6
21.00	0.5	97.5	10.79	647.0	539.0	67	0.3	91.9
22.00	0.2	97.8	11.30	678.0	565.0	66	0.2	92.1
23.00	1.0	98.8	11.82	709.0	591.0	65	0.7	92.7
24.00	0.3	99.1	12.33	740.0	616.0	65	0.2	92.9
25.00	0.0	99.1	12.84	771.0	642.0	64	0.0	92.9
30.00	0.9	100.0	15.41	925.0	771.0	63	0.6	93.5
35.00	0.0	100.0	17.98	1079.0	899.0	62	0.0	93.5
40.00	0.0	100.0	20.55	1233.0	1027.0	61	0.0	93.5
45.00	0.0	100.0	23.12	1387.0	1156.0	58	0.0	93.5
Estimated Net Annual Sediment (TSS) Load Reduction =								94 %

Climate Station ID: 6105978 Years of Rainfall Data: 20

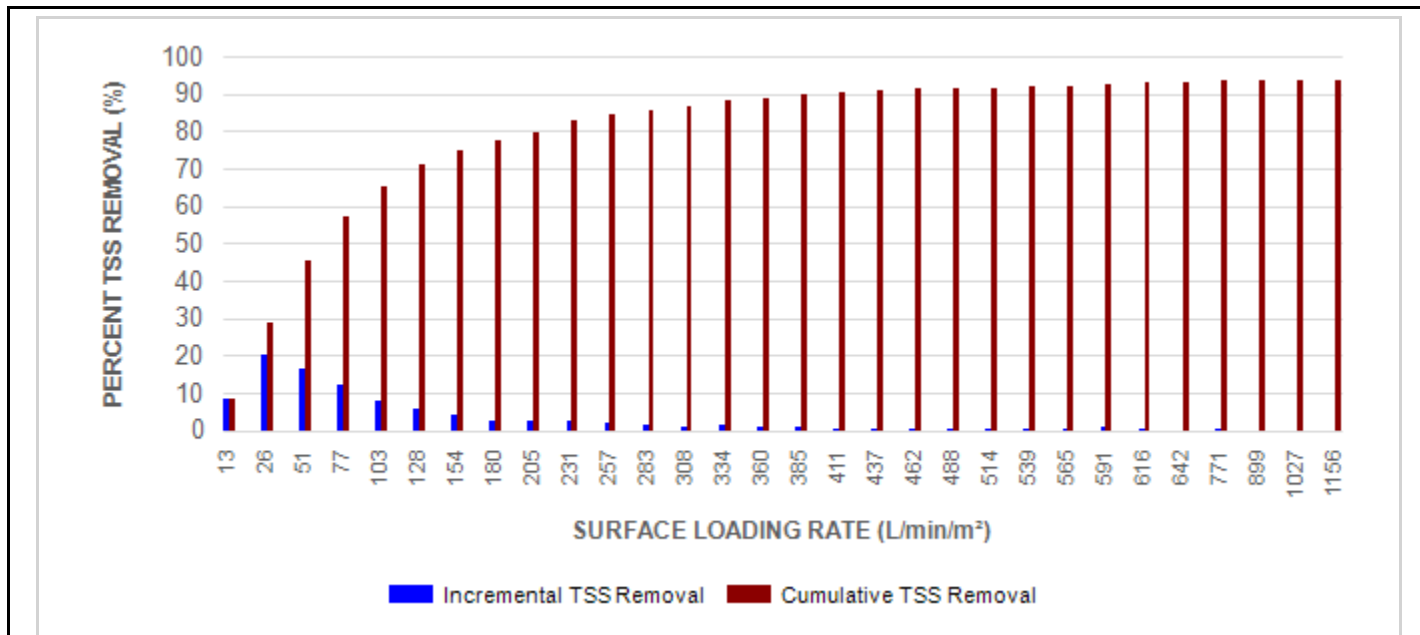


Stormceptor® EF Sizing Report

RAINFALL DATA FROM OTTAWA CDA RCS RAINFALL STATION



INCREMENTAL AND CUMULATIVE TSS REMOVAL FOR THE RECOMMENDED STORMCEPTOR® MODEL



Stormceptor® EF Sizing Report

Maximum Pipe Diameter / Peak Conveyance

Stormceptor EF / EFO	Model Diameter		Min Angle Inlet / Outlet Pipes	Max Inlet Pipe Diameter		Max Outlet Pipe Diameter		Peak Conveyance Flow Rate	
	(m)	(ft)		(mm)	(in)	(mm)	(in)	(L/s)	(cfs)
EF4 / EFO4	1.2	4	90	609	24	609	24	425	15
EF5 / EFO5	1.5	5	90	762	30	762	30	710	25
EF6 / EFO6	1.8	6	90	914	36	914	36	990	35
EF8 / EFO8	2.4	8	90	1219	48	1219	48	1700	60
EF10 / EFO10	3.0	10	90	1828	72	1828	72	2830	100
EF12 / EFO12	3.6	12	90	1828	72	1828	72	2830	100

SCOUR PREVENTION AND ONLINE CONFIGURATION

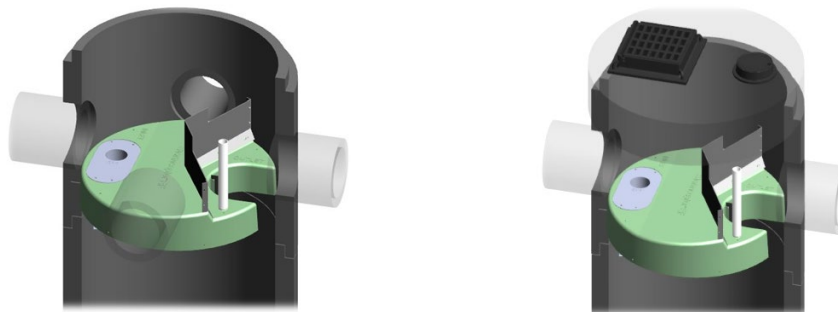
► Stormceptor® EF and EFO feature an internal bypass and superior scour prevention technology that have been demonstrated in third-party testing according to the scour testing provisions of the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators, and the exceptional scour test performance has been third-party verified in accordance with the ISO 14034 ETV protocol. As a result, Stormceptor EF and EFO are approved for online installation, eliminating the need for costly additional bypass structures, piping, and installation expense.

DESIGN FLEXIBILITY

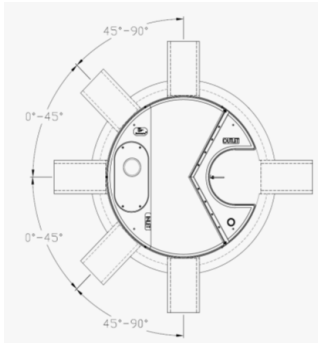
► Stormceptor® EF and EFO offers design flexibility in one simplified platform, accepting stormwater flow from a single inlet pipe or multiple inlet pipes, and/or surface runoff through an inlet grate. The device can also serve as a junction structure, accommodate a 90-degree inlet-to-outlet bend angle, and can be modified to ensure performance in submerged conditions.

OIL CAPTURE AND RETENTION

► While Stormceptor® EF will capture and retain oil from dry weather spills and low intensity runoff, Stormceptor® EFO has demonstrated superior oil capture and greater than 99% oil retention in third-party testing according to the light liquid re-entrainment testing provisions of the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators. Stormceptor EFO is recommended for sites where oil capture and retention is a requirement.



Stormceptor® EF Sizing Report



INLET-TO-OUTLET DROP

Elevation differential between inlet and outlet pipe inverts is dictated by the angle at which the inlet pipe(s) enters the unit.

0° - 45° : The inlet pipe is 1-inch (25mm) higher than the outlet pipe.

45° - 90° : The inlet pipe is 2-inches (50mm) higher than the outlet pipe.

HEAD LOSS

The head loss through Stormceptor EF is similar to that of a 60-degree bend structure. The applicable K value for calculating minor losses through the unit is 1.1. For submerged conditions the applicable K value is 3.0.

Pollutant Capacity

Stormceptor EF / EFO	Model Diameter		Depth (Outlet Pipe Invert to Sump Floor)		Oil Volume		Recommended Sediment Maintenance Depth *		Maximum Sediment Volume *		Maximum Sediment Mass **	
	(m)	(ft)	(m)	(ft)	(L)	(Gal)	(mm)	(in)	(L)	(ft³)	(kg)	(lb)
EF4 / EFO4	1.2	4	1.52	5.0	265	70	203	8	1190	42	1904	5250
EF5 / EFO5	1.5	5	1.62	5.3	420	111	305	10	2124	75	2612	5758
EF6 / EFO6	1.8	6	1.93	6.3	610	160	305	12	3470	123	5552	15375
EF8 / EFO8	2.4	8	2.59	8.5	1070	280	610	24	8780	310	14048	38750
EF10 / EFO10	3.0	10	3.25	10.7	1670	440	610	24	17790	628	28464	78500
EF12 / EFO12	3.6	12	3.89	12.8	2475	655	610	24	31220	1103	49952	137875

*Increased sump depth may be added to increase sediment storage capacity

** Average density of wet packed sediment in sump = 1.6 kg/L (100 lb/ft³)

Feature	Benefit	Feature Appeals To
Patent-pending enhanced flow treatment and scour prevention technology	Superior, verified third-party performance	Regulator, Specifying & Design Engineer
Third-party verified light liquid capture and retention for EFO version	Proven performance for fuel/oil hotspot locations	Regulator, Specifying & Design Engineer, Site Owner
Functions as bend, junction or inlet structure	Design flexibility	Specifying & Design Engineer
Minimal drop between inlet and outlet	Site installation ease	Contractor
Large diameter outlet riser for inspection and maintenance	Easy maintenance access from grade	Maintenance Contractor & Site Owner

STANDARD STORMCEPTOR EF/EFO DRAWINGS

For standard details, please visit <http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef>

STANDARD STORMCEPTOR EF/EFO SPECIFICATION

For specifications, please visit <http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef>

STANDARD PERFORMANCE SPECIFICATION FOR “OIL GRIT SEPARATOR” (OGS) STORMWATER QUALITY TREATMENT DEVICE

PART 1 – GENERAL

1.1 WORK INCLUDED

This section specifies requirements for selecting, sizing, and designing an underground Oil Grit Separator (OGS) device for stormwater quality treatment, with third-party testing results and a Statement of Verification in accordance with ISO 14034 Environmental Management – Environmental Technology Verification (ETV).

1.2 REFERENCE STANDARDS & PROCEDURES

ISO 14034:2016 Environmental management – Environmental technology verification (ETV)

Canadian Environmental Technology Verification (ETV) Program’s **Procedure for Laboratory Testing of Oil-Grit Separators**

1.3 SUBMITTALS

1.3.1 All submittals, including sizing reports & shop drawings, shall be submitted upon request with each order to the contractor then forwarded to the Engineer of Record for review and acceptance. Shop drawings shall detail all OGS components, elevations, and sequence of construction.

1.3.2 Alternative devices shall have features identical to or greater than the specified device, including: treatment chamber diameter, treatment chamber wet volume, sediment storage volume, and oil storage volume.

1.3.3 Unless directed otherwise by the Engineer of Record, OGS stormwater quality treatment product substitutions or alternatives submitted within ten days prior to project bid shall not be accepted. All alternatives or substitutions submitted shall be signed and sealed by a local registered Professional Engineer, based on the exact same criteria detailed in Section 3, in entirety, subject to review and approval by the Engineer of Record.

PART 2 – PRODUCTS

2.1 OGS POLLUTANT STORAGE

The OGS device shall include a sump for sediment storage, and a protected volume for the capture and storage of petroleum hydrocarbons and buoyant gross pollutants. The minimum sediment & petroleum hydrocarbon storage capacity shall be as follows:

2.1.1	4 ft (1219 mm) Diameter OGS Units:	1.19 m ³ sediment / 265 L oil
	5 ft (1524 mm) Diameter OGS Units:	1.95 m ³ sediment / 420 L oil
	6 ft (1829 mm) Diameter OGS Units:	3.48 m ³ sediment / 609 L oil
	8 ft (2438 mm) Diameter OGS Units:	8.78 m ³ sediment / 1,071 L oil

Stormceptor® EF Sizing Report

10 ft (3048 mm) Diameter OGS Units: 17.78 m³ sediment / 1,673 L oil
 12 ft (3657 mm) Diameter OGS Units: 31.23 m³ sediment / 2,476 L oil

PART 3 – PERFORMANCE & DESIGN

3.1 GENERAL

The OGS stormwater quality treatment device shall be verified in accordance with ISO 14034:2016 Environmental management – Environmental technology verification (ETV). The OGS stormwater quality treatment device shall remove oil, sediment and gross pollutants from stormwater runoff during frequent wet weather events, and retain these pollutants during less frequent high flow wet weather events below the insert within the OGS for later removal during maintenance. The Manufacturer shall have at least ten (10) years of local experience, history and success in engineering design, manufacturing and production and supply of OGS stormwater quality treatment device systems, acceptable to the Engineer of Record.

3.2 SIZING METHODOLOGY

The OGS device shall be engineered, designed and sized to provide stormwater quality treatment based on treating a minimum of 90 percent of the average annual runoff volume and a minimum removal of an annual average 60% of the sediment (TSS) load based on the Particle Size Distribution (PSD) specified in the sizing report for the specified device. Sizing of the OGS shall be determined by use of a minimum ten (10) years of local historical rainfall data provided by Environment Canada. Sizing shall also be determined by use of the sediment removal performance data derived from the ISO 14034 ETV third-party verified laboratory testing data from testing conducted in accordance with the Canadian ETV protocol Procedure for Laboratory Testing of Oil-Grit Separators, as follows:

3.2.1 Sediment removal efficiency for a given surface loading rate and its associated flow rate shall be based on sediment removal efficiency demonstrated at the seven (7) tested surface loading rates specified in the protocol, ranging 40 L/min/m² to 1400 L/min/m², and as stated in the ISO 14034 ETV Verification Statement for the OGS device.

3.2.2 Sediment removal efficiency for surface loading rates between 40 L/min/m² and 1400 L/min/m² shall be based on linear interpolation of data between consecutive tested surface loading rates.

3.2.3 Sediment removal efficiency for surface loading rates less than the lowest tested surface loading rate of 40 L/min/m² shall be assumed to be identical to the sediment removal efficiency at 40 L/min/m². No extrapolation shall be allowed that results in a sediment removal efficiency that is greater than that demonstrated at 40 L/min/m².

3.2.4 Sediment removal efficiency for surface loading rates greater than the highest tested surface loading rate of 1400 L/min/m² shall assume zero sediment removal for the portion of flow that exceeds 1400 L/min/m², and shall be calculated using a simple proportioning formula, with 1400 L/min/m² in the numerator and the higher surface loading rate in the denominator, and multiplying the resulting fraction times the sediment removal efficiency at 1400 L/min/m².

The OGS device shall also have sufficient annual sediment storage capacity as specified and calculated in Section 2.1.

Stormceptor[®] EF Sizing Report

3.3 CANADIAN ETV or ISO 14034 ETV VERIFICATION OF SCOUR TESTING

The OGS device shall have Canadian ETV or ISO 14034 ETV Verification of third-party scour testing conducted in accordance with the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators**.

3.3.1 To be acceptable for on-line installation, the OGS device must demonstrate an average scour test effluent concentration less than 10 mg/L at each surface loading rate tested, up to and including 2600 L/min/m².

3.4 LIGHT LIQUID RE-ENTRAINMENT SIMULATION TESTING

The OGS device shall have Canadian ETV or ISO 14034 ETV Verification of completed third-party Light Liquid Re-entrainment Simulation Testing in accordance with the Canadian ETV **Program's Procedure for Laboratory Testing of Oil-Grit Separators**, with results reported within the Canadian ETV or ISO 14034 ETV verification. This re-entrainment testing is conducted with the device pre-loaded with low density polyethylene (LDPE) plastic beads as a surrogate for light liquids such as oil and fuel. Testing is conducted on the same OGS unit tested for sediment removal to assess whether light liquids captured after a spill are effectively retained at high flow rates.

3.4.1 For an OGS device to be an acceptable stormwater treatment device on a site where vehicular traffic occurs and the potential for an oil or fuel spill exists, the OGS device must have reported verified performance results of greater than 99% cumulative retention of LDPE plastic beads for the five specified surface loading rates (ranging 200 L/min/m² to 2600 L/min/m²) in accordance with the Light Liquid Re-entrainment Simulation Testing within the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators**. However, an OGS device shall not be allowed if the Light Liquid Re-entrainment Simulation Testing was performed with screening components within the OGS device that are effective at retaining the LDPE plastic beads, but would not be expected to retain light liquids such as oil and fuel.

STANDARD SPECIFICATION FOR “OIL GRIT SEPARATOR” (OGS) STORMWATER QUALITY TREATMENT DEVICE WITH THIRD-PARTY VERIFIED LIGHT LIQUID RE-ENTRAINMENT SIMULATION PERFORMANCE TESTING RESULTS

PART 1 – GENERAL

1.1 WORK INCLUDED

This section specifies requirements for selecting, sizing, designing, maintaining, and constructing an underground Oil Grit Separator (OGS) device for stormwater quality treatment, **specifically an OGS device that has been third-party tested for oil and fuel retention capability using a protocol for light liquid re-entrainment simulation testing, with testing results and a Statement of Verification in accordance with all the provisions of ISO 14034 Environmental Management – Environmental Technology Verification (ETV).** Work includes supply and installation of concrete bases, precast sections, and the appropriate precast section with OGS internal components correctly installed within the system, watertight sealed to the precast concrete prior to arrival to the project site.

1.2 REFERENCE STANDARDS

1.2.1 For Canadian projects only, the following reference standards apply:

CAN/CSA-A257.4-14: Joints for Circular Concrete Sewer and Culvert Pipe, Manhole Sections, and Fittings Using Rubber Gaskets

CAN/CSA-A257.4-14: Precast Reinforced Circular Concrete Manhole Sections, Catch Basins, and Fittings

CAN/CSA-S6-00: Canadian Highway Bridge Design Code

1.2.2 For ALL projects, the following reference standards apply:

ASTM D-4097: Contact Molded Glass Fiber Reinforced Chemical Resistant Tanks

ASTM C 478: Specification for Precast Reinforced Concrete Manhole Sections

ASTM C 443: Specification for Joints for Concrete Pipe and Manholes, Using Rubber Gaskets

ASTM C 891: Standard Practice for Installation of Underground Precast Concrete Utility Structures

ASTM D2563: Standard Practice for Classification of Visual Defects in Reinforced Plastics

1.3 SHOP DRAWINGS

1.3.1 Shop drawings shall be submitted upon request with each order to the contractor then forwarded to the Engineer of Record for review and acceptance. Shop drawings shall detail the precast concrete components and OGS internal components prior to shipment, including the sequence for installation.

1.3.2 Unless directed otherwise by the Engineer of Record, OGS stormwater quality treatment product substitutions or alternatives submitted within ten days prior to project bid shall not be accepted. All alternatives or substitutions submitted shall be based on the exact same criteria detailed in Section 3, in entirety, subject to review and approval by the Engineer of Record. Any and all changes to project cost estimates, bonding amounts, plan check fees for revision of approved documents, or design impacts due to regulatory requirements as a result of a product substitution shall be coordinated by the Contractor with the Engineer of Record.

1.4 HANDLING AND STORAGE

Prevent damage to materials during storage and handling.

1.4.1 OGS internal components supplied by the Manufacturer for attachment to the precast concrete vessel shall be pre-fabricated, bolted to the precast and watertight sealed to the precast vessel surface prior to site delivery to ensure Manufacturer's internal assembly process and quality control processes are fully adhered to, and to prevent materials damage on site.

1.4.2 Follow all instructions including the sequence for installation in the shop drawings during installation.

PART 2 – PRODUCTS

2.1 GENERAL

2.1.1 The OGS vessel shall be cylindrical and constructed from precast concrete riser and slab components.

2.1.2 The precast concrete OGS internal components shall include a fiberglass insert bolted and watertight sealed inside the precast concrete vessel, prior to site delivery. Primary internal components that are to be anchored and watertight sealed to the precast concrete vessel shall be done so only by the Manufacturer prior to arrival at the job site to ensure product quality.

2.1.3 The OGS shall be allowed to be specified and have the ability to function as a 240-degree bend structure in the stormwater drainage system, or as a junction structure.

2.1.4 The OGS to be specified shall have the capability to accept influent flow from an inlet grate and an inlet pipe.

2.2 PRECAST CONCRETE SECTIONS

All precast concrete components shall be designed and manufactured to meet highway loading conditions per State/Provincial or local requirements.

2.3 GASKETS

Only profile neoprene or nitrile rubber gaskets that are oil resistant shall be accepted. For Canadian projects only, gaskets shall be in accordance to CSA A257.4-14. Mastic sealants, butyl tape/rope or Conseal CS-101 alone are not acceptable gasket materials.

2.4 JOINTS

The concrete joints shall be watertight and meet the design criteria according to ASTM C-990. For projects where joints require gaskets, the concrete joints shall be watertight and oil resistant and meet the design criteria according to ASTM C-443. Mastic sealants or butyl tape/rope alone are not an acceptable alternative.

2.5 FRAMES AND COVERS

Frames and covers shall be manufactured in accordance with State/Provincial or local requirements for inspection and maintenance access purposes. A minimum of one cover, at least 22-inch (560 mm) in diameter, shall be clearly embossed with the OGS manufacturer's product name to properly identify this asset's purpose is for stormwater quality treatment.

2.6 PRECAST CONCRETE

All precast concrete components shall conform to the appropriate CSA or ASTM specifications.

2.7 FIBERGLASS

The fiberglass portion of the OGS device shall be constructed in accordance with ASTM D2563, and in accordance with the PS15-69 manufacturing standard, and shall only be installed, bolted and watertight sealed to the precast concrete by the Manufacturer prior to arrival at the project site to ensure product quality.

2.8 OGS POLLUTANT STORAGE

The OGS device shall include a sump for sediment storage, and a fiberglass insert for the capture and storage of petroleum hydrocarbons and buoyant gross pollutants. The total sediment storage capacity shall be a minimum 40 ft³ (1.1 m³). The total petroleum hydrocarbon storage capacity shall be a minimum 50 gallons (189 liters). The access opening to the sump of the OGS device for periodic inspection and maintenance purposes shall be a minimum 16 inches (406 mm) in diameter.

2.9 LADDERS

Ladder rungs shall be provided upon request or to comply with State/Provincial or local requirements.

2.10 INSPECTION

All precast concrete sections shall be level and inspected to ensure dimensions, appearance, integrity of internal components, and quality of the product meets State/Provincial or local specifications and associated standards.

PART 3 – PERFORMANCE & DESIGN

3.1 GENERAL

The OGS stormwater quality treatment device shall be verified in accordance with ISO 14034:2016 Environmental management – Environmental technology verification (ETV). The OGS stormwater quality treatment device shall remove oil, sediment and gross pollutants from stormwater runoff during frequent wet weather events, and retain these pollutants during less frequent high flow wet weather events below the insert within the OGS for later removal during maintenance. The Manufacturer shall have at least ten (10) years of local experience, history and success in engineering design, manufacturing and production and supply of OGS stormwater quality treatment device systems, acceptable to the Engineer of Record.

3.2 HYDROLOGY AND RUNOFF VOLUME

The OGS device shall be engineered, designed and sized to treat a minimum of 90 percent of the average annual runoff volume, unless otherwise stated by the Engineer of Record, using historical rainfall data. Rainfall data sets should be comprised of a minimum 15-years of rainfall data or a longer continuous period if available for a given location, but in all cases a minimum 5-year period of rainfall data.

3.3 ANNUAL (TSS) SEDIMENT LOAD AND STORAGE CAPACITY

The OGS device shall be capable of removing and have sufficient storage capacity for the calculated annual total suspended solids (TSS) mass load and volume without scouring previously captured pollutants prior to maintenance being required. The annual (TSS) sediment load and volume transported from the drainage area should be calculated and compared to the OGS device's available storage capacity by the specifying Engineer to ensure adequate capacity between maintenance cycles. Sediment loadings shall be determined by land use and defined as a minimum of 450 kg (992 lb) of sediment (TSS) per impervious hectare of drainage area per year, or greater based on land use, as noted in Table 1 below.

Annual sediment volume calculations shall be performed using the projected average annual treated runoff volume, a typical sediment bulk density of 1602 kg/m³ (100 lbs/ft³) and an assumed Event Mean Concentration (EMC) of 125 mg/L TSS in the runoff, or as otherwise determined by the Engineer of Record.

Example calculation for a 1.3-hectares parking lot site:

- 1.28 meters of rainfall depth, per year
- 1.3 hectares of 100% impervious drainage area
- EMC of 125 mg/L TSS in runoff
- Treatment of 90% of the average annual runoff volume
- Target average annual TSS removal rate of 60% by OGS

Annual Runoff Volume:

- 1.28 m rain depth x 1.3 ha x 10,000 m²/ha= 16,640 m³ of runoff volume
- 16,640 m³ x 1000 L/m³ = 16,640,000 L of runoff volume
- 16,640,000 L x 0.90 = 14,976,000 L to be treated by OGS unit

Annual Sediment Mass and Sediment Volume Load Calculation:

- 14,976,000 L x 125 mg/L x kg/1,000,000 mg = 1,872 kg annual sediment mass
- 1,872 kg x m³/1602 kg = 1.17 m³ annual sediment volume
- 1.17 m³ x 60% TSS removal rate by OGS = 0.70 m³ minimum expected annual storage requirement in OGS

As a guideline, the U.S. EPA has determined typical annual sediment loads per drainage area for various sites by land use (see Table 1). Certain States, Provinces and local jurisdictions have also established such guidelines.

Table 1 – Annual Mass Sediment Loading by Land Use								
	Commercial	Parking Lot	Residential			Highways	Industrial	Shopping Center
			High	Med.	Low			
(lbs/acre/yr)	1,000	400	420	250	10	880	500	440
(kg/hectare/yr)	1,124	450	472	281	11	989	562	494

Source: U.S. EPA Stormwater Best Management Practice Design Guide Volume 1, Appendix D, Table D-1, Burton and Pitt 2002

3.4 SIZING METHODOLOGY

The OGS device shall be engineered, designed and sized to provide stormwater quality treatment based on treating a minimum of 90 percent of the average annual runoff volume and a minimum removal of an annual average 60% of the sediment (TSS) load based on the Particle Size Distribution (PSD) specified in Table 2, Section 3.5, and based on third-party performance testing conducted in accordance with the Canadian Environmental Technology Verification (ETV) Program's **Procedure for Laboratory Testing of Oil-Grit Separators**. Sizing of the OGS shall be determined by use of a minimum ten (10) years of local historical rainfall data provided by Environment Canada. Sizing shall also be determined by use of the sediment removal performance data derived from the ISO 14034 ETV third-party verified laboratory testing data from testing conducted in accordance with the Canadian ETV protocol *Procedure for Laboratory Testing of Oil-Grit Separators*, as follows:

3.4.1 Sediment removal efficiency for a given surface loading rate and its associated flow rate shall be based on sediment removal efficiency demonstrated at the seven (7) tested surface loading rates specified in the protocol, ranging 40 L/min/m² to 1400 L/min/m², and as stated in the ISO 14034 ETV Verification Statement for the OGS device.

3.4.2 Sediment removal efficiency for surface loading rates between 40 L/min/m² and 1400 L/min/m² shall be based on linear interpolation of data between consecutive tested surface loading rates.

3.4.3 Sediment removal efficiency for surface loading rates less than the lowest tested surface loading rate of 40 L/min/m² shall be assumed to be identical to the sediment removal efficiency at 40 L/min/m². No extrapolation shall be allowed that results in a sediment removal efficiency that is greater than that demonstrated at 40 L/min/m².

3.4.4 Sediment removal efficiency for surface loading rates greater than the highest tested surface loading rate of 1400 L/min/m² shall assume zero sediment removal for the portion of flow that exceeds 1400 L/min/m², and shall be calculated using a simple proportioning formula, with 1400 L/min/m² in the numerator and the higher surface loading rate in the denominator, and multiplying the resulting fraction times the sediment removal efficiency at 1400 L/min/m².

The OGS device shall also have sufficient annual sediment storage capacity as specified and calculated in Section 3.3.

3.4.5 The Peclet Number is not an approved method or model for calculating TSS removal, sizing, or scaling OGS devices.

3.4.6 If an alternate OGS device is proposed, supporting documentation shall be submitted that demonstrates:

- Canadian ETV or ISO 14034 ETV Verification Statement which verifies third-party performance testing conducted in accordance with the **Procedure for Laboratory Testing of Oil-Grit Separators**, including the Light Liquid Re-entrainment Simulation Testing.
- Equal or better sediment (TSS) removal of the PSD specified in Table 2 at equivalent surface loading rates, as compared to the OGS device specified herein.
- Equal or better Light Liquid Re-entrainment Simulation Test results (using low-density polyethylene beads as a surrogate for light liquids such as oil and fuel) at equivalent surface loading rates, as compared to the OGS device specified herein. However, an alternative OGS device shall not be allowed as a substitute if the Light Liquid Re-entrainment Simulation Test was performed with screening components within the OGS device that are effective at retaining the low-density polyethylene beads, but would not be expected to retain light liquids such as oil and fuel.
- Equal or greater sediment storage capacity, as compared to the OGS device specified herein.
- Supporting documentation shall be signed and sealed by a local registered Professional Engineer. All costs associated with preparing and certifying this documentation shall be born solely by the Contractor.

3.5 PARTICLE SIZE DISTRIBUTION (PSD) FOR SIZING

The OGS device shall be sized to achieve the Engineer-specified average annual percent sediment (TSS) removal based solely on the test sediment used in the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators**. This test sediment is comprised of inorganic ground silica with a specific gravity of 2.65, uniformly mixed, and containing a broad range of particle sizes as specified in Table 2. No alternative PSDs or deviations from Table 2 shall be accepted.

Table 2 Canadian ETV Program Procedure for Laboratory Testing of Oil-Grit Separators Particle Size Distribution (PSD) of Test Sediment		
Particle Diameter (Microns)	% by Mass of All Particles	Specific Gravity
1000	5%	2.65
500	5%	2.65
250	15%	2.65
150	15%	2.65
100	10%	2.65
75	5%	2.65
50	10%	2.65
20	15%	2.65
8	10%	2.65
5	5%	2.65
2	5%	2.65

3.6 CANADIAN ETV or ISO 14034 ETV VERIFICATION OF SCOUR TESTING

The OGS device shall have Canadian ETV or ISO 14034 ETV Verification of completed third-party scour testing conducted and have in accordance with the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators**. This scour testing is conducted with the device pre-loaded with test sediment comprised of the particle size distribution (PSD) illustrated in Table 2.

3.6.1 To be acceptable for on-line installation, the OGS device must demonstrate an average scour test effluent concentration less than 10 mg/L at each surface loading rate tested, up to and including 2600 L/min/m².

Data generated from laboratory scour testing performed with an OGS device pre-loaded with a coarser PSD than in Table 2 (i.e. the coarser PSD has no particles in the 1-micron to 50-micron size range, or the D₅₀ of the test sediment exceeds 75 microns) shall not be acceptable for the determination of the device's suitability for on-line installation.

3.7 DESIGN ACCOUNTING FOR BYPASS

3.7.1 The OGS device shall be specified to achieve the TSS removal performance and water quality objectives without washout of previously captured pollutants. The OGS device shall also have sufficient hydraulic conveyance capacity to convey the peak storm event, in accordance with hydraulic conditions per the Engineer of Record. To ensure this is achieved, there are two design options with associated requirements:

3.7.1.1 The OGS device shall be placed **off-line** with an upstream diversion structure (typically in an upstream manhole) that only allows the water quality volume to be diverted to the OGS device, and excessive flows diverted downstream around the OGS device to prevent high flow washout of pollutants previously captured. This design typically incorporates a triangular layout including an upstream bypass manhole with an appropriately engineered weir wall, the OGS device, and a downstream junction manhole, which is connected to both the OGS device and bypass structure. In this case with an external bypass required, the OGS device manufacturer must provide calculations and designs for all structures, piping and any other required material applicable to the proper functioning of the system, stamped by a Professional Engineer.

3.7.1.2 Alternatively, OGS devices in compliance with Section 3.6 shall be acceptable for an **on-line** design configuration, thereby eliminating the requirement for an upstream bypass manhole and downstream junction manhole.

3.7.2 The OGS device shall also have sufficient hydraulic conveyance capacity to convey the peak storm event, in accordance with hydraulic conditions per the Engineer of Record. If an alternate OGS device is proposed, supporting documentation shall be submitted that demonstrates equal or better hydraulic conveyance capacity as compared to the OGS device specified herein. This documentation shall be signed and sealed by a local registered Professional Engineer. All costs associated with preparing and certifying this documentation shall be born solely by the Contractor.

3.8 LIGHT LIQUID RE-ENTRAINMENT SIMULATION TESTING

The OGS device shall have Canadian ETV or ISO 14034 ETV Verification of completed third-party Light Liquid Re-entrainment Simulation Testing in accordance with the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators**, with results reported within the Canadian ETV or ISO 14034 ETV verification. This re-entrainment testing is conducted with the device pre-loaded with low density polyethylene (LDPE) plastic beads as a surrogate for light liquids such as oil and fuel. Testing is conducted on the same OGS unit tested for sediment removal to assess whether light liquids captured after a spill are effectively retained at high flow rates.

3.8.1 For an OGS device to be an acceptable stormwater treatment device on a site where vehicular traffic occurs and the potential for an oil or fuel spill exists, the OGS device must have reported verified performance results of greater than 99% cumulative retention of LDPE plastic beads for the five specified surface loading rates (ranging 200 L/min/m² to 2600 L/min/m²) in accordance with the Light Liquid Re-entrainment Simulation Testing within the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators**. However, an OGS device shall not be allowed if the Light Liquid Re-entrainment Simulation Testing was performed with screening components within the OGS device that are effective at retaining the LDPE plastic beads, but would not be expected to retain light liquids such as oil and fuel.

3.9 PETROLEUM HYDROCARBONS AND FLOATABLES STORAGE CAPACITY

Petroleum hydrocarbons and floatables storage capacity in the OGS device shall be a minimum 50 gallons (189 Liters), or more as specified.

3.9.1 The OGS device shall have gasketed precast concrete joints that are watertight, and oil resistant and meet the design criteria according to ASTM C-443 to provide safe oil and other hydrocarbon materials storage and ground water protection. Mastic sealants or butyl tape/rope alone are not an acceptable alternative.

3.10 SURFACE LOADING RATE SCALING OF DIFFERENT MODEL SIZES

The reference device for scaling shall be an OGS device that has been third-party tested in accordance with the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators**. Other model sizes of the tested device shall only be scaled such that the claimed TSS removal efficiency of the scaled device shall be no greater than the TSS removal efficiency of the tested device at identical **surface loading rates** (flow rate divided by settling surface area). The depth of other model sizes of the tested device shall be scaled in accordance with the depth scaling provisions within Section 6.0 of the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators**.

3.10.1 The Peclet Number and volumetric scaling are not approved methods for scaling OGS devices.

PART 4 – INSPECTION & MAINTENANCE

The OGS manufacturer shall provide an Owner's Manual upon request. Maintenance shall be performed by a professional service provider who has experience in cleaning OGS devices and has been trained and certified in applicable health and safety practices, including confined space entry procedures.

- 4.1 A Quality Assurance Plan that provides inspection for a minimum of 5 years shall be included with the OGS stormwater quality device, and written into the Environmental Compliance Approval (ECA) or the appropriate State/Provincial or local approval document.
- 4.2 OGS device inspection shall include determination of sediment depth and presence of petroleum hydrocarbons below the insert. Inspection shall be easily conducted from finished grade through a frame and cover of at least 22 inch (560 mm) in diameter.
- 4.3 Inspection and pollutant removal shall be conducted periodically. For routine maintenance cleaning activities, pollutant removal shall typically utilize a truck equipped with vacuum apparatus, and shall be easily conducted from finished grade through a frame and cover of at least 22-inches (560 mm) in diameter.
- 4.4 Diameter of the maintenance access opening to the lower chamber and sump shall be scaled consistently across all model sizes, and shall be 1/3 the inside diameter of the OGS structure, or larger.
- 4.5 No confined space entry shall be required for routine inspection and maintenance cleaning activities.

- 4.6 For OGS model sizes of diameter 72 inches (1828 mm) and greater, the access opening to the OGS device's lower chamber and sump shall be large enough to allow a maintenance worker to enter the lower chamber to facilitate non-routine maintenance cleaning activities and repairs, as needed.
- 4.7 The orifice-containing component (i.e. drop pipe, duct, chute, etc.) of the OGS device used to control flow rate into the lower chamber shall be removable from the insert to facilitate cleaning, repair, or replacement of the orifice-containing component, as needed.

PART 5 – EXECUTION

5.1 PRECAST CONCRETE INSTALLATION

The installation of the precast concrete OGS stormwater quality treatment device shall conform to ASTM C 891, ASTM C 478, ASTM C 443, CAN/CSA-A257.4-14, CAN/CSA-A257.4-14, CAN/CSA-S6-00 and all highway, State/Provincial, or local specifications for the construction of manholes. Selected sections of a general specification that are applicable are summarized below. The Contractor shall furnish all labor, equipment and materials necessary to offload, assemble as needed the OGS internal components as specified in the Shop Drawings.

5.2 EXCAVATION

5.2.1 Excavation for the installation of the OGS stormwater quality treatment device shall conform to highway, State/Provincial or local specifications. Topsoil that is removed during the excavation for the OGS stormwater quality treatment device shall be stockpiled in designated areas and not be mixed with subsoil or other materials. Topsoil stockpiles and the general site preparation for the installation of the OGS stormwater quality device shall conform to highway, State/Provincial or local specifications.

5.2.2 The OGS device shall not be installed on frozen ground. Excavation shall extend a minimum of 12 inch (300 mm) from the precast concrete surfaces plus an allowance for shoring and bracing where required. If the bottom of the excavation provides an unsuitable foundation additional excavation may be required.

5.2.3 In areas with a high water table, continuous dewatering shall be provided to ensure that the excavation is stable and free of water.

5.3 BACKFILLING

Backfill material shall conform to highway, State/Provincial or local specifications. Backfill material shall be placed in uniform layers not exceeding 12 inches (300 mm) in depth and compacted to highway, State/Provincial or local specifications.

5.4 OGS WATER QUALITY DEVICE CONSTRUCTION SEQUENCE

5.4.1 The precast concrete OGS stormwater quality treatment device is installed and leveled in sections in the following sequence:

- aggregate base
- base slab, or base
- riser section(s) (if required)
- riser section w/ pre-installed fiberglass insert
- upper riser section(s)
- internal OGS device components
- connect inlet and outlet pipes
- riser section, top slab and/or transition (if required)
- frame and access cover

5.4.2 The precast concrete base shall be placed level at the specified grade. The entire base shall be in contact with the underlying compacted granular material. Subsequent sections, complete with oil resistant, watertight joint seals, shall be installed in accordance with the precast concrete manufacturer's recommendations.

5.4.3 Adjustment of the OGS stormwater quality treatment device can be performed by lifting the upper sections free of the excavated area, re-leveling the base, and re-installing the sections. Damaged sections and gaskets shall be repaired or replaced as necessary. Once the OGS stormwater quality treatment device has been constructed, any lift holes must be plugged with mortar.

5.5 DROP PIPE AND OIL INSPECTION PIPE

Once the upper precast concrete riser has been attached to the lower precast concrete riser section, the OGS device Drop Pipe and Oil Inspection Pipe must be attached, and watertight sealed to the fiberglass insert using Sikaflex 1a. Installation instructions and required materials shall be provided by the OGS manufacturer.

5.6 INLET AND OUTLET PIPES

Inlet and outlet pipes shall be securely set using grout or approved pipe seals (flexible boot connections, where applicable) so that the structure is watertight. Non-secure inlets and outlets will result in improper performance.

5.7 FRAME AND COVER OR FRAME AND GRATE INSTALLATION

Precast concrete adjustment units shall be installed to set the frame and cover/grate at the required elevation. The adjustment units shall be laid in a full bed of mortar with successive units being joined using sealant recommended by the manufacturer. Frames for the cover/grate should be set in a full bed of mortar at the elevation specified.

5.7.1 A minimum of one cover, at least 22-inch (560 mm) in diameter, shall be clearly embossed with the OGS device brand or product name to properly identify this asset's purpose is for stormwater quality treatment.