

memorandum

re: Geotechnical Review of Grading Plans

Proposed Residential Development

5618 Hazeldean Road - Abbott's Run - Block 13 - Ottawa, Ontario

to: Minto Communities Inc. – Erin Harrington – eharrington@minto.com

date: October 27, 2025 file: PG7640-MEMO.02

Further to your request and authorization, Paterson Group (Paterson) has prepared the current memorandum to document our review of the available grading plans, and to provide associated recommendations from a geotechnical perspective for the aforementioned project. The present memorandum should be read in conjunction with Paterson Group Geotechnical Report PG7460-1 Revision 1 dated May 28, 2025. Relevant design information is presented in Table 1 – Summary of Design Details for the subject blocks.

The relevant design and inspection information presented in Table 1 – Summary includes the following:

Block number
Unit number
Original ground surface elevation based on available ground surface elevations
Proposed finished grade elevations
Proposed underside of footing (USF) elevation
Proposed finished floor elevation (FFE)
Bearing resistance values at SLS
Seismic Site Designation
Maximum allowable grade raise
Estimated engineered fill thickness required below footings
Lightweight Fill (LWF) recommendations
Frost protection recommendations
Design recommendations for lateral support zone interferences

Grading Plan Review

Paterson reviewed the following grading plan prepared by DSEL for the aforementioned residential development:

Grading Plan - Project No.	1295_Block13 -	Sheet No.	14 - Revision 2,	dated
October 24, 2025.				

Based on our review of the above-noted drawing, the proposed grades throughout the subject site are within the recommended permissible grade raise restriction of 2 m provided in the aforementioned geotechnical investigation report. Therefore, the proposed grading is considered acceptable from a geotechnical perspective such that lightweight fill (LWF) or any further measures will not be required to be taken for the proposed development. Further, sufficient soil cover has been provided to perimeter and exterior pad footings to mitigate the migration of frost within the founding subsoils.

Bearing Resistance Values for Foundation Design

Using continuously applied loads, conventional footings can be designed using the bearing resistance values presented in the following table.

Table 2 - Bearing Resistance Values										
Bearing Surface	Bearing Resistance Value at SLS (kPa)	Factored Bearing Resistance Value at ULS (kPa)								
Stiff to Very Stiff Brown Silty Clay	150	300								
Firm Grey Silty Clay	75	110								

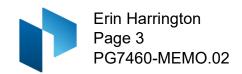
Note:

- Strip and pad footings, up to 3 and 6 m wide, respectively, can be designed using the bearing resistance values provided for an undisturbed, silty clay bearing surface.
- Bearing resistance values for footing design should be confirmed on a per block basis by the Paterson personnel at the time of construction.

An undisturbed soil bearing surface consists of a surface from which all topsoil and deleterious materials, such as loose, frozen or disturbed soil, whether in situ or not, have been removed, in the dry, prior to the placement of concrete footings. A geotechnical resistance factor of 0.5 was applied to the above noted bearing resistance values at ULS. The bearing resistance value at SLS, provided above, will be subjected to potential post-construction total and differential settlements of 25 and 20 mm, respectively.

Minor Adjustments to Lot Grading and Design Details During Construction Phase

It is anticipated that there may be minor discrepancies between the latest reviewed grading plan and the permit plot plans that will be prepared for some of the proposed blocks during the final permitting and construction phase of the proposed structures. The discrepancies are anticipated to arise due to minor changes required by the building designer to accommodate finishes such as risers and entrances to the design grading. In our experience, minor adjustments are required to the design USF elevations and occasionally finished grades surrounding the structure.

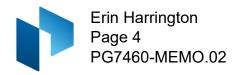


Based on Paterson's review of site-specific conditions, provided all of the following criteria are met if further adjustments to the grading plan details are made on lot/block permit plot plans (i.e., changes made to plot plans, not to the current grading plans), additional review by Paterson to ensure the permit plot plans are satisfactory from a geotechnical perspective is not considered required during the construction phase:

Plot plan USF is not more or less than 10 cm from the design USF elevation and
Paterson field personnel prepared memorandums documenting their field review
of the bearing medium and bearing surfaces for the structure.
Plot plan finished grade does not fluctuate more than 10 cm from the design
finished grade.
Plot plan finished grade remains more than 30 cm below the recommended
permissible grade raise elevation.
There is not an existing recommendation to consider lightweight fill around the
perimeter and/or in the garage/front porches of the building (i.e., if Table 1 provides
a recommendation for LWF, any adjustment to grading and/or founding elevations
must be reviewed by Paterson if they do not conform to those noted in Table 1).
Sufficient soil cover remains to provide protection against the migration of frost to
the soil subgrade (i.e., 1.5 m below finished grade for heated structures).
If one of these conditions is not met, it is recommended that Paterson be contacted
to review the permit plot plan during the construction phase for conformance to our
grading requirements from a geotechnical perspective at that time.

Should the revised founding depth be located within 1.5 m from finished grade around the building perimeter, it is recommended that Paterson review and advise on frost protection measures, such as foundation insulation, on a lot-by-lot basis when this condition exists.

Any updates to the current grading plans should be reviewed and advised upon by Paterson. However, once approved and adjustments are made on plot plans, the adjusted plot plans may not require additional review to verify adequacy to the proposed grading matrix from a geotechnical perspective provided adjustments are within the ranges noted herein. Alternatively, permit plot plans may be circulated to Paterson prior to submission to approvals to ensure the grading and design values are consistent with our recommendations for the proposed residential development. It should be noted that this portion of the memorandum is only considered applicable for the subject site.



We trust that this information is satisfactory for your immediate requirements.

Best Regards,

Paterson Group Inc.

Nicholas F. R. Versolato, CPI, B.Eng

Drew Petahtegoose P.Eng.

Attachments:

☐ Table 1 – Summary of Design Details

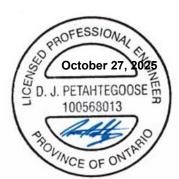


Table 1 - Summary of Design Details																				
PG7460 - Minto Communities - Abbott's Run - Block 13																				
						Underside of	Finished	Bearing			Above	Above	Engineered Fill	Engineered Fill			Minimum	Minimum	Frost	
Block	Limit Niverbox	Original GS	Proposed GS Front	Original GS		Footing	Floor	Resistance	Seismic Site		Permissible	Permissible	Required Below	_	Frost Check -	Frost Check -	Thickness LWF	Thickness LWF and	Protection	Site Servicing Lateral Support Notes (USF/Concrete Trench Depth Recommendations - Reference
Number	Unit Number	Front	GS Front	Rear	GS Rear	Elevation	Elevation	Value at SLS	Designation	Grade Raise	Grade Raise Front	Grade Raise Rear	USF - Front	USF - Rear	Front	Rear	in Front Porch	Extents Around Structure	Notes	to be made to PG7460-MEMO.03)
		(m)	(m)	(m)	(m)	(m)	(m)	(kPa)		(m)	(m)	(m)	(m)	(m)	(m)	(m)	(m)	(m)		
	Unit 1	101.60	103.40	101.60	n/a	101.51	104.81	150	XD	2.00	0.00	n/a	0.21	0.21	1.89	n/a	n/a	n/a	n/a	Lean concrete recommended helpsy stategies feetings (see Table 1 in above noted memorandum for details)
	Onit 1	101.60	103.40	101.60	п/а	101.51	104.81	150	XD	2.00	0.00	II/ d	0.21	0.21	1.89	11/ a	11/ d	II/a	II/a	Lean concrete recommended below staircase footings (see Table 1 in above-noted memorandum for details)
	Unit 2	101.60	103.40	101.60	n/a	101.51	104.81	150	XD	2.00	0.00	n/a	0.21	0.21	1.89	n/a	n/a	n/a	n/a	Lean concrete recommended below staircase footings (see Table 1 in above-noted memorandum for details)
	11'2	404.60	402.40	101.60		404.54	404.04	450	VP	2.00	0.00	- 1-	0.24	0.24	4.00	/-	/	- 1-	/ -	Table 4 is a second of the sec
	Unit 3	101.60	103.40	101.60	n/a	101.51	104.81	150	XD	2.00	0.00	n/a	0.21	0.21	1.89	n/a	n/a	n/a	n/a	Lean concrete recommended below staircase footings (see Table 1 in above-noted memorandum for details)
	Unit 4	101.60	103.40	101.60	n/a	101.51	104.81	150	XD	2.00	0.00	n/a	0.21	0.21	1.89	n/a	n/a	n/a	n/a	Lean concrete recommended below staircase footings (see Table 1 in above-noted memorandum for details)
	Unit 5	101.60	103.40	101.60	n/a	101.51	104.81	150	XD	2.00	0.00	n/a	0.21	0.21	1.89	n/a	n/a	n/a	n/a	
BLOCK 1	Unit 6	101.60	103.40	101.60	n/a	101.51	104.81	150	XD	2.00	0.00	n/a	0.21	0.21	1.89	n/a	n/a	n/a	n/a	
	Unit 7	101.60	103.40	101.60	n/a	101.51	104.81	150	XD	2.00	0.00	n/a	0.21	0.21	1.89	n/a	n/a	n/a	n/a	Lean concrete recommended below staircase footings (see Table 1 in above-noted memorandum for details)
	Unit 8	101.60	103.40	101.60	n/a	101.51	104.81	150	XD	2.00	0.00	n/a	0.21	0.21	1.89	n/a	n/a	n/a	n/a	Lean concrete recommended below staircase footings (see Table 1 in above-noted memorandum for details)
	Unit 9	101.60	103.40	101.60	n/a	101.51	104.81	150	XD	2.00	0.00	n/a	0.21	0.21	1.89	n/a	n/a	n/a	n/a	
	Unit 10 Unit 11	101.60 101.60	103.40 103.40	101.60 101.60	n/a n/a	101.51 101.51	104.81 104.81	150 150	XD XD	2.00	0.00	n/a n/a	0.21 0.21	0.21 0.21	1.89 1.89	n/a n/a	n/a n/a	n/a n/a	n/a n/a	
	Unit 12	101.60	103.40	101.60	n/a	101.51	104.81	150	XD	2.00	0.00	n/a	0.21	0.21	1.89	n/a	n/a	n/a	n/a	
	Unit 1	101.70	103.53	101.70	n/a	101.64	104.94	150	XD	2.00	0.00	n/a	0.24	0.24	1.89	n/a	n/a	n/a	n/a	
	Unit 2	101.70	103.53	101.70	n/a	101.64	104.94	150	XD	2.00	0.00	n/a	0.24	0.24	1.89	n/a	n/a	n/a	n/a	
	Unit 3 Unit 4	101.70 101.70	103.53 103.53	101.70 101.70	n/a n/a	101.64 101.64	104.94 104.94	150 150	XD XD	2.00	0.00	n/a n/a	0.24 0.24	0.24 0.24	1.89 1.89	n/a n/a	n/a n/a	n/a n/a	n/a n/a	
	Unit 5	101.70	103.53	101.70	n/a	101.64	104.94	150	XD	2.00	0.00	n/a	0.24	0.24	1.89	n/a	n/a	n/a	n/a	
BLOCK 2	Unit 6	101.70	103.53	101.70	n/a	101.64	104.94	150	XD	2.00	0.00	n/a	0.24	0.24	1.89	n/a	n/a	n/a	n/a	
	Unit 7 Unit 8	101.70 101.70	103.53 103.53	101.70 101.70	n/a n/a	101.64 101.64	104.94 104.94	150 150	XD XD	2.00	0.00	n/a n/a	0.24 0.24	0.24 0.24	1.89 1.89	n/a n/a	n/a n/a	n/a n/a	n/a n/a	
	Unit 9	101.70	103.53	101.70	n/a	101.64	104.94	150	XD	2.00	0.00	n/a	0.24	0.24	1.89	n/a	n/a	n/a	n/a	
	Unit 10	101.70	103.53	101.70	n/a	101.64	104.94	150	XD	2.00	0.00	n/a	0.24	0.24	1.89	n/a	n/a	n/a	n/a	
	Unit 11	101.70	103.53	101.70	n/a	101.64	104.94	150	XD	2.00	0.00	n/a	0.24	0.24	1.89	n/a	n/a	n/a	n/a	
	Unit 12 Unit 1	101.70 101.75	103.53 103.69	101.70 101.75	n/a n/a	101.64 101.80	104.94 105.10	150 150	XD XD	2.00	0.00	n/a n/a	0.24	0.24 0.35	1.89 1.89	n/a n/a	n/a n/a	n/a n/a	n/a n/a	
	Unit 2	101.75	103.69	101.75	n/a	101.80	105.10	150	XD	2.00	0.00	n/a	0.35	0.35	1.89	n/a	n/a	n/a	n/a	
	Unit 3	101.80	103.69	101.80	n/a	101.80	105.10	150	XD	2.00	0.00	n/a	0.30	0.30	1.89	n/a	n/a	n/a	n/a	
	Unit 4 Unit 5	101.80 101.90	103.69 103.69	101.80 101.90	n/a n/a	101.80 101.80	105.10 105.10	150 150	XD XD	2.00	0.00	n/a n/a	0.30 0.20	0.30 0.20	1.89 1.89	n/a n/a	n/a n/a	n/a n/a	n/a n/a	
DI OCK 3	Unit 6	101.90	103.69	101.90	n/a	101.80	105.10	150	XD	2.00	0.00	n/a	0.20	0.20	1.89	n/a	n/a	n/a	n/a	
BLOCK 3	Unit 7	101.90	103.69	101.90	n/a	101.80	105.10	150	XD	2.00	0.00	n/a	0.20	0.20	1.89	n/a	n/a	n/a	n/a	
	Unit 8 Unit 9	101.90 101.80	103.69 103.69	101.90 101.80	n/a n/a	101.80 101.80	105.10 105.10	150 150	XD XD	2.00	0.00	n/a n/a	0.20	0.20 0.30	1.89 1.89	n/a n/a	n/a n/a	n/a n/a	n/a n/a	
	Unit 10	101.80	103.69	101.80	n/a	101.80	105.10	150	XD	2.00	0.00	n/a	0.30	0.30	1.89	n/a	n/a	n/a	n/a	
	Unit 11	101.75	103.69	101.75	n/a	101.80	105.10	150	XD	2.00	0.00	n/a	0.35	0.35	1.89	n/a	n/a	n/a	n/a	
	Unit 12	101.75	103.69	101.75	n/a	101.80	105.10	150	XD	2.00	0.00	n/a	0.35	0.35	1.89	n/a	n/a	n/a	n/a	
	Unit 1 Unit 2	102.20 102.20	103.91 103.91	102.20 102.20	n/a n/a	102.02 102.02	105.32 105.32	150 150	XD XD	2.00	0.00	n/a n/a	0.12 0.12	0.12 0.12	1.89 1.89	n/a n/a	n/a n/a	n/a n/a	n/a n/a	
	Unit 3	102.25	103.91	102.25	n/a	102.02	105.32	150	XD	2.00	0.00	n/a	0.07	0.07	1.89	n/a	n/a	n/a	n/a	
BLOCK 4	Unit 4	102.25	103.91	102.25	n/a	102.02	105.32	150	XD	2.00	0.00	n/a	0.07	0.07	1.89	n/a	n/a	n/a	n/a	
	Unit 5 Unit 6	102.25 102.25	103.91 103.91	102.25 102.25	n/a n/a	102.02 102.02	105.32 105.32	150 150	XD XD	2.00	0.00	n/a n/a	0.07 0.07	0.07 0.07	1.89 1.89	n/a n/a	n/a n/a	n/a n/a	n/a n/a	
	Unit 7	102.20	103.91	102.20	n/a	102.02	105.32	150	XD	2.00	0.00	n/a	0.12	0.12	1.89	n/a	n/a	n/a	n/a	
	Unit 8	102.20	103.91	102.20	n/a	102.02	105.32	150	XD	2.00	0.00	n/a	0.12	0.12	1.89	n/a	n/a	n/a	n/a	
	Unit 1		103.90		n/a	102.01	105.31	150 150	XD XD	2.00	0.00	n/a n/a	0.00	0.00	1.89	n/a	n/a n/a	n/a	n/a	
	Unit 2 Unit 3	102.55 102.50		102.55 102.50		102.01 102.01	105.31 105.31	150	XD	2.00	0.00	n/a	0.00	0.00	1.89	n/a n/a	n/a	n/a n/a	n/a n/a	
	Unit 4	102.45	103.90	102.45	n/a	102.01	105.31	150	XD	2.00	0.00	n/a	0.00	0.00	1.89	n/a	n/a	n/a	n/a	Lean concrete recommended below staircase footings (see Table 1 in above-noted memorandum for details)
	Oille 4	102.43	103.50	102.45	11/4	102.01	103.51	150	, AD	2.00	0.00	11/4	0.00	0.00	1.03	11/4	11/4	11/4	11/4	Ecul conference recommended below stancase rootings (see rusic 1 in upove noted memoralidam for details)
	Unit 5	102.40	103.90	102.40	n/a	102.01	105.31	150	XD	2.00	0.00	n/a	0.00	0.00	1.89	n/a	n/a	n/a	n/a	Lean concrete recommended below staircase footings (see Table 1 in above-noted memorandum for details)
BLOCK 5	Unit 6	102.35	103.90	102.35	n/a	102.01	105.31	150	XD	2.00	0.00	n/a	0.00	0.00	1.89	n/a	n/a	n/a	n/a	
	Unit 7	102.35	103.90	102.35	n/a	102.01	105.31	150	XD	2.00	0.00	n/a	0.00	0.00	1.89	n/a	n/a	n/a	n/a	
	Unit 8 Unit 9	102.40 102.45	103.90 103.90	102.40 102.45	n/a n/a	102.01 102.01	105.31 105.31	150 150	XD XD	2.00	0.00	n/a n/a	0.00	0.00	1.89 1.89	n/a n/a	n/a n/a	n/a n/a	n/a n/a	
	Unit 10	102.45	103.90	102.45	n/a n/a	102.01	105.31	150	XD	2.00	0.00	n/a n/a	0.00	0.00	1.89	n/a n/a	n/a n/a	n/a n/a	n/a n/a	
	Unit 11	102.55	103.90	102.55	n/a	102.01	105.31	150	XD	2.00	0.00	n/a	0.00	0.00	1.89	n/a	n/a	n/a	n/a	
	Unit 12	102.60	103.90	102.60	n/a	102.01	105.31	150	XD	2.00	0.00	n/a	0.00	0.00	1.89	n/a	n/a	n/a	n/a	
	Unit 1 Unit 2	101.80 101.80	103.59 103.59	101.80 101.80	n/a n/a	101.70 101.70	105.00 105.00	150 150	XD XD	2.00	0.00	n/a n/a	0.20 0.20	0.20	1.89 1.89	n/a n/a	n/a n/a	n/a n/a	n/a n/a	
	Unit 3	101.80	103.59	101.80	n/a	101.70	105.00	150	XD	2.00	0.00	n/a	0.20	0.20	1.89	n/a	n/a	n/a	n/a	
вьоск 6	Unit 4	101.80	103.59	101.80	n/a	101.70	105.00	150	XD	2.00	0.00	n/a	0.20	0.20	1.89	n/a	n/a	n/a	n/a	
	Unit 5 Unit 6	101.80 101.80	103.59 103.59	101.80 101.80	n/a n/a	101.70 101.70	105.00 105.00	150 150	XD XD	2.00	0.00	n/a n/a	0.20 0.20	0.20	1.89 1.89	n/a n/a	n/a n/a	n/a n/a	n/a n/a	
1	Unit 7	101.80	103.59	101.80	n/a	101.70	105.00	150	XD	2.00	0.00	n/a	0.20	0.20	1.89	n/a	n/a	n/a	n/a	
	Unit 8	101.80		101.80		101.70	105.00	150	XD	2.00	0.00	n/a	0.20	0.20	1.89	n/a	n/a	n/a	n/a	
Notes: Proposed grade	raise information was	s hased on the	following arad	ling plane prop	ared by DSEI .															



Notes:.

Proposed grade raise information was based on the following grading plans prepared by DSEL:

- Project No. 1295_Block13, Sheet No. 14, Revision No. 2 dated October 24, 2025

Current Block and Lot numbers assigned based on above noted grading plans.

"Original Ground Surface" elevations are based on topographic ground surface elevations measured at test hole locations by Paterson obtained during the geotechnical field investigation on May 7, 2025.

All engineered fill thickness recommendations consider a minimum 300 mm thick layer of topsoil requiring to be removed from the ground surface prior to placing fill, and is considered in the thickness provided herein.

