



120 Rue Lusk Street

Functional Servicing and Stormwater Management Report

Project Location:

120 Rue Lusk Street, Ottawa, ON

Prepared for:

NECSA Holdings Corp
532 Newburgh Place
Ottawa, ON K2J 5X7

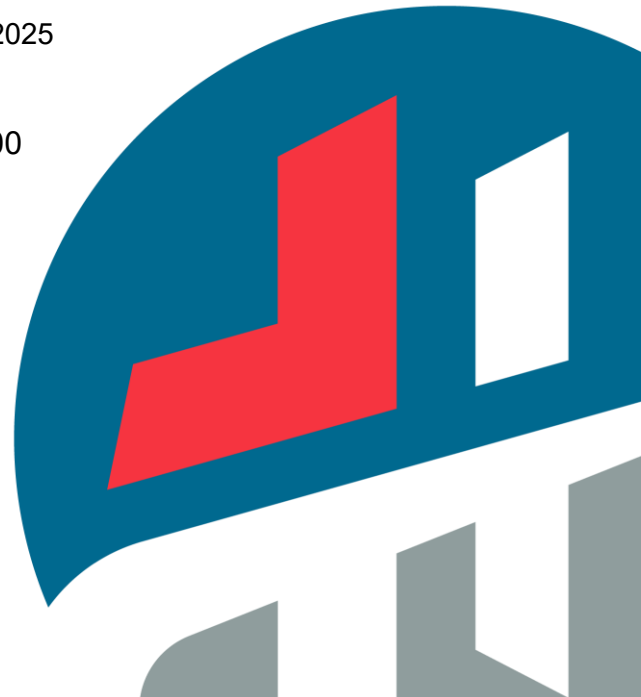
Prepared by:

MTE Consultants
520 Bingemans Centre Drive
Kitchener, ON N2B 3X9

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MTE File No.: 53510-100





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Notes and Details Plan	
MTE Drawing No. C2.3	Separately Appended

1.0 INTRODUCTION

MTE Consultants Inc. was retained by NECSA Holdings Corp to complete the functional servicing and stormwater management design for the Medical Office Building, Restaurant and Daycare to be constructed at 120 Lusk Street in the City of Ottawa (herein referred to as the 'Site').

The Site is 0.60ha in size and referred to as Block 13, located within the O'Keefe Court – 416 Landsat the northeast quadrant of the intersection of Fallowfield Road and Strandherd Drive. The Site is bounded to the north by O'Keefe Court, to the west and east by future commercial development, and to the south by Lusk Street. For the exact location of the Site refer to the key plan located on the separately appended engineering drawings.

The proposed development for the Site is the construction of a three-storey medical office, restaurant, and daycare building, complete with a partial basement with associated driveway and at grade parking areas. The overall imperviousness of the proposed development is approximately 87.0% ($C = 0.81$).

This report addresses the functional servicing and stormwater management (SWM) requirements set forth by the City of Ottawa and the Design Brief for O'Keefe Court Business Park – 416 Lands Commercial Development, prepared by IBI Group, dated May 2018. The design requirements for the Site conforms to the criteria set forth by the City of Ottawa and the Jock River Reach One Subwatershed Study. The site grading, servicing and stormwater management details for the Site are illustrated on the separately appended MTE Engineering Drawings C1.1, C2.1, C2.2 and C2.3.

2.0 SERVICING

The new building is proposed to be serviced with sanitary, storm and water from the municipal services on Lusk Street.

2.1 Sanitary

There is an existing 250mm diameter municipal sanitary sewer within the Lusk Street right-of-way. There is an existing 250mm diameter sanitary service stubbed into the south side of the Site, constructed with an existing sanitary manhole inside the property line. The existing 250mm service stub will be removed up unto the existing manhole. A 200mm sanitary service connection is proposed to be connected to the existing manhole at a greater slope. The new 200mm diameter service connection is proposed to be installed at a slope of 0.6% within the Site, with a capacity of 25.39L/s.

The allowable sanitary flow rate for the Site was determined based on the design criteria within the IBI report, as per the City of Ottawa design criteria of 50,000L/day/ha. For this Site, the allowable sanitary release rate is 0.76L/s, including infiltration allowance. The total anticipated peak flow rate for the Site is calculated to be 0.375L/s, based on the common sewage flow rates for commercial developments, based on City of Ottawa design criteria. Refer to Appendix A for calculation details.

2.2 Storm

There is an existing 975mm diameter municipal storm sewer within the Lusk Street right-of-way. There is an existing 525mm diameter storm service stubbed into the south side of the Site, constructed with an existing storm manhole inside the property line. The existing 525mm service

stub will be removed up unto the existing manhole. Two 375mm diameter storm service connections are proposed to be connected to the existing manhole. The new service connections are proposed to be installed at a slope of 0.6% within the Site, with a capacity of 135.81L/s for each 375mm storm service.

The proposed on-site storm sewers are proposed to convey runoff from the building rooftop and surface runoff within the parking lot. The on-site storm sewer will outlet into the existing 975mm diameter municipal storm sewer within the Lusk Street right-of-way, which is then conveyed to a downstream municipal storm water management facility. During the 5-year storm event, the proposed development will produce a piped stormwater flow rate of 68L/s. Refer to Appendix B for calculation details.

2.3 Water

There is an existing 200mm diameter water service stubbed into the south side of the Site, which connects to the existing 300mm diameter municipal watermain along Lusk Street. There are two existing municipal fire hydrants in close proximity to the Site: one located on the southwest corner of the Site and one located on the southeast corner of the Site. A 200mm diameter water service is proposed to connect to the existing stub and continue north into the Site to service the proposed building. One new on-site hydrant is proposed to provide fire protection for the new building, in addition to the existing municipal hydrants located along the frontage of the Site.

The existing municipal watermain fronting the Site is currently a dead end watermain from the intersection of Lusk Street and Forager Road stubbed west of the Site, with no secondary source. A secondary municipal watermain connection and loop is planned to be constructed as part of Phase 2 of the 416 Lands subdivision; however, the timing of the connection has been delayed. In order for the development at 120 Lusk Street to proceed, the City of Ottawa requires a 200mm watermain loop to be constructed fronting the Site along Lusk Street. Therefore, a smaller 200mm diameter municipal watermain loop is proposed between Block 14 (140 Lusk) and Block 12 (100 Lusk), within the frontage of the properties at 140, 120 and 100 Lusk, to provide the required looping. The 200mm watermain loop will connect to the existing 200mm stubbed water service at 100 Lusk Street, and to the 200mm stubbed water service at the Site (140 Lusk Street), for a total watermain length of approximately 151.0m. Approval has been provided by the property owner at 100 Lusk to connect into their 200mm water service.

The proposed 200mm looped watermain will be constructed as part of the development at 140 Lusk Street as shown on MTE Drawing 52222-100 C3.1.

The following equation was used to determine the OBC (OBC,2012) fire flow demand:

$$Q = K \times V \times S_{tot}$$

Where:

- Q = minimum supply of water (L)
- K = water supply coefficient from Table 1 OBC, 2012
- V = total building volume (m³)
- S_{tot} = total spatial coefficient values from property line exposure on all sides

The following equation was used to determine the FUS (FUS, 2020), fire flow demand:

$$RFF = 220C\sqrt{A}$$

Where:

RFF = the required fire flow (L/min)

C = the construction coefficient – Building Type II Noncombustible Construction

A = total effective floor area

Other factors that affect the FUS fire flow are the occupancy reduction, sprinkler protection and the building exposure. The occupancy reduction for this type of development was determined to be limited combustible components (-15%), the building will be equipped with sprinklers (-30%) and the building exposure was calculated based on the exposure to all property lines (+60%).

The required fire flow under the OBC, FUS and the domestic demands for the proposed building are summarized in the table below.

Table 2.1 – Required Water Demands

Guideline	OBC	FUS	Average Day	Maximum Day	Peak Hour	Maximum Day and Fire Flow
Required Fire Flow (L/s)	150	217	0.12	0.18	0.21	217

Refer to Appendix C for water demand calculations.

3.0 STORMWATER MANAGEMENT

3.1 Criteria

The stormwater management design criteria for the subject Site, as established by the Design Brief for the O’Keefe Court – 416 Lands Commercial Development, prepared by IBI Group, dated May 2018, and the City of Ottawa are as follows:

- Attenuation of the post-development peak flows up to the 100-year storm event from the proposed development to maximum allowable release rate of 108L/s.
- Providing sufficient on-site storage, a minimum of 138.6m³ as required in the O’Keefe Court – 416 Lands Commercial Development Design Brief (IBI Group, 2018), to ensure no overland flow for all storms up to and including the 100-year storm event.
- Water quality control will be provided in the downstream stormwater management facility within the O’Keefe Court – 416 Lands Commercial Development.

3.2 Methodology

In order to successfully complete the stormwater management design for this Site, the following specific tasks were undertaken:

- Calculated the allowable runoff rates using MIDUSS NET.
- Determined the percent impervious of the site and catchment parameters for inclusion in MIDUSS modelling.

- iii) Calculated post-development runoff hydrographs using MIDUSS NET.
- iv) Revised the site grades to attain the required storage for runoff control.

Due to limited information about the 100-year design storm +20%, the intensity of the 100-year design storm was multiplied but 20% and added to the intensity of the 100-year storm. To determine the corresponding IDF parameters to input into MIDUSS, A was also multiplied by 1.2, and B and C were determined by adjusting based on the relationship between the 2-, 5- and 100-year design storms. Before proceeding with the quantity calculations, it was ensured that the intensity of the IDF parameters inputted were 20% more than 100-year design storm.

3.3 Catchment Parameters

Per the Design Brief for the O’Keefe Court – 416 Lands Commercial Development, provided by IBI Group, dated May 2018, the allowable peak flow for the Site is 108L/s for all storm events up to and including the 100-year storm event. The required on-site stormwater storage is 138.6m³. Refer to Appendix D for the 416 Lands Storm Drainage Area Plan, prepared by IBI Group, dated May 18, 2022, for more detail.

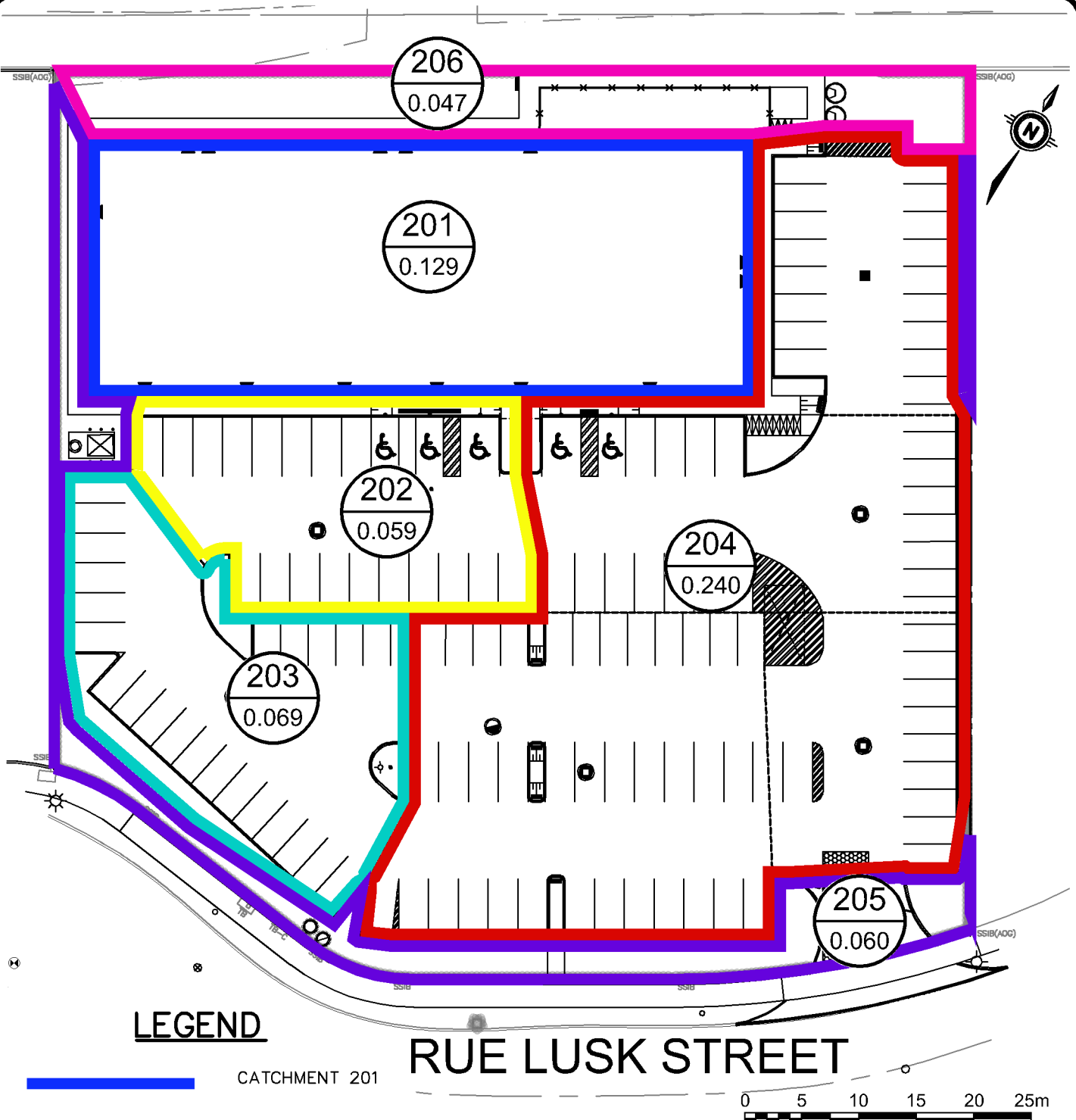
The following Table 3.1 summarizes the catchments used in the modelling of the Site. The post-development condition was separated into six catchment areas: the building rooftop area, the NW Parking Lot, the SW Parking Lot, the controlled area, the uncontrolled area draining towards Lusk Street, and the uncontrolled area towards O’Keefe Court. Figure 1.0 illustrates the limits of the post-development catchment areas.

Table 3.1 – Catchment Parameters

#	Catchment	Area (ha)	% Impervious	Pervious CN	Impervious CN	Slope (%)	Flow Length (m)
Post-Development Catchment Areas							
201	Building Rooftop Area (to Lusk Street)	0.129	100.0	75	98	1.5	10.0
202	NW Parking Lot (uncontrolled)	0.059	100.0	75	98	1.2	10.0
203	SW Parking Lot (controlled)	0.069	100.0	75	98	1.2	10.0
204	Controlled Area (to Lusk Street)	0.240	100.0	75	98	1.2	20.0
205	Uncontrolled Area draining to Lusk Street ROW	0.060	10.3	75	98	17.5	2.0
206	Uncontrolled Area draining to O’Keefe Court Street ROW	0.047	49.0	75	98	25.0	6.0

A geotechnical investigation was completed by Paterson Group on November 18, 2022. A complete copy will be provided for the City’s records. The investigation revealed that the Site consists of silty sand to silty clay. Therefore, a pervious value of 75 for grassed areas is acceptable for the Site.

Groundwater was encountered on the Site, approximately 3.0-4.0m below ground surface.



LEGEND

- CATCHMENT 201
- CATCHMENT 202
- CATCHMENT 203
- CATCHMENT 204
- CATCHMENT 205
- CATCHMENT 206

201
 0.129
 SUB-CATCHMENT
 NUMBER
 AREA (ha.)

RUE LUSK STREET

0 5 10 15 20 25m



Engineers, Scientists, Surveyors

PROJECT

**120 LUSK ST. MEDICAL
BUILDING CIVIL WORKS**

TITLE

**POST DEVELOPMENT
CATCHMENT AREAS**

Drawn

EJJ

Scale

1:500

Figure

Checked

JXN

Project No.

53510-100

Date

2024-06-11

Rev No.

0

F1.0

3.4 Water Quantity – Modelling Results

It is proposed that stormwater runoff from the proposed development to be directed to the existing manhole located at the southwestern property line of the Site, and ultimately draining to the 975mm diameter municipal storm sewer.

In order to achieve the stormwater management requirements for the site, runoff generated from the controlled driveway and parking areas will be captured by the on-site storm sewer system. The controlled flow of the parking lot is separated into two sections: Catchment 203 controlled by a 90mm diameter casting orifice and Catchment 204 controlled by a 85mm diameter online orifice plate on the outlet pipe of CBMH3. Stormwater storage volume will be provided within the driveway and parking areas, on the building rooftop storage, and within the subsurface storm sewer system. The maximum depth of ponding permitted within the parking area by grading is 0.25m.

In addition, four flow control roof drains, single notch, are proposed to be installed on the roof of the proposed building. This will help to further reduce the post-development runoff from the site. Refer to appendix E for the flow control roof drain manufacturer specifications sheet.

The flow equations for the orifice and the IDF parameters for the 2-, 5-, 100-year and 100-year +20% storm events, as well as the MIDUSS NET output are included in Appendix F.

A combination of the surface storage, rooftop storage, and subsurface storage provides approximately 225.7m³ of storage volume, which exceeds the required 138.6m³ by the Design Brief for O’Keefe Commercial Development (IBI Group, 2018). The rooftop will provide a total of 35.95m³ of storage to the maximum height of 15cm. The following tables, Table 3.2 and Table 3.3 illustrates the stage-storage-discharge relationship of on-site storage system.

Table 3.2 – Stage-Storage-Discharge Information – Rooftop (taken from MIDUSS)

Depth (m)	Head (m)	Controlled Flow (m ³ /s)	Volume (m ³)	Remarks
0.00	0	0	0	Rooftop
0.081	2-Year Ponding Elevation			
	0.081	0.008	12.3	8.1cm of ponding on the roof
0.093	5-Year Ponding Elevation			
	0.093	0.009	19.1	9.3cm of ponding on the roof
0.119	100-Year Ponding Elevation			
	0.119	0.012	39.1	11.9cm of ponding on the roof
0.129	100-Year +20% Ponding Elevation			
	0.129	0.013	53.0	12.9cm of ponding on the roof

**Table 3.3 – Stage-Storage-Discharge Information (Horizontal Orifice) – Parking Lot
(taken from MIDUSS)**

Elevation (m)	Head (m)	Orifice Flow (m ³ /s)	Volume (m ³)	Remarks
103.55	0	0	0.0	90mm diameter Casting Orifice
103.622	2-Year Ponding Elevation			
	0.072	0.00742	1.0	7.2cm of Ponding
103.653	5-Year Ponding Elevation			
	0.103	0.00893	4.5	10.3cm of Ponding
103.701	100-Year Ponding Elevation			
	0.151	0.00975	13.8	15.1cm of Ponding
103.714	100-Year +20% Ponding Elevation			
	0.164	0.00994	18.6	16.4cm of Ponding
103.75	0.20	0.01051	30.9	Contour
103.80	0.25	0.01124	54.5	Contour

**Table 3.4 – Stage-Storage-Discharge Information (Online Orifice) – Parking Lot
(taken from MIDUSS)**

Elevation (m)	Head (m)	Orifice Flow (m ³ /s)	Volume (m ³)	Remarks
100.91	0	0	0	85mm diameter Online Orifice
103.55	0	0.02388	12.5	Top of Grate
103.609	2-Year Ponding Elevation			
	0.059	0.02319	13.2	5.9cm of Ponding
103.666	5-Year Ponding Elevation			
	0.116	0.02448	29.9	11.6cm of Ponding
103.70	0.15	0.02465	46.1	Contour
103.724	100-Year Ponding Elevation			
	0.174	0.02477	69.5	17.4cm of Ponding
103.744	100-Year +20% Ponding Elevation			
	0.194	0.02486	92.5	19.4cm of Ponding
103.75	0.20	0.02490	94.8	Contour
103.80	0.25	0.02515	171.2	Contour

With the addition of the 90mm diameter casting orifice plate and the 85mm diameter online orifice plate, the post-development runoff from the controlled portion of the Site for the 2-,5- and 100-year storm events is controlled to 0.049m³/s, 0.058m³/s, and 0.076m³/s respectively. The following Table 3.3 summarizes the flows generated by the whole Site.

Table 3.5 – Summary of Flows

Modelling Condition	2-Year Storm Event (m³/s)	5-Year Storm Event (m³/s)	100-Year Storm Event (m³/s)
Allowable Release Rate	0.108	0.108	0.108
Post-Development – Total Site	0.054	0.071	0.107

*see Table 3.2 above for storage summary for the 2-,5- and 100-year storm events.

3.5 Water Quality Control

The Site is located within the Jock River Reach One Subwatershed, which requires Enhanced Level of Protection water quality control (80% TSS removal). Per the Design Report for the O’Keefe Court – 416 Lands Commercial Development (IBI Group, 2013), the end-of-pipe stormwater management facility within the O’Keefe Court Commercial Business will provide water quality control. Therefore, no additional water quality control is required on-site.

3.6 Erosion & Sediment Control

In order to minimize the effects of erosion during the grading of the Site, the following measures are proposed during construction for erosion and sedimentation control:

- i) Erosion and sedimentation facilities are to be installed prior to any area grading operations.
- ii) All erosion control measures are to be inspected and monitored by the contractor and repairs are to be completed as required.
- iii) All materials and equipment used for the purpose of site preparation and project completion should be operated and stored in a manner that prevents any deleterious substance from leaving the site.
- iv) Re-vegetation of completed areas as soon as possible after construction, including those areas not slated for construction, within 60 days of rough grading.
- v) To minimize the amount of mud being tracked onto the roadway, a mud mat should be installed at the primary construction entrance.

4.0 CONCLUSIONS AND RECOMMENDATIONS

Based on the foregoing analysis, it is concluded that:

- i) The sanitary, storm, and water service connections have adequate capacity to service the proposed development.
- ii) The proposed SWM design provides adequate storage volume and attenuation of the 2-, 5- and 100-year storm events to the allowable release rate set by the Design Brief for O’Keefe Court Commercial Development (IBI Group, 2018).
- iii) Upon completion of construction, the Site will conform to the design criteria specified by the City of Ottawa.

It is recommended that:

- i) The site grading be undertaken according to the proposed elevations, details and erosion control measures shown on the separately appended engineering drawings.
- ii) The stormwater management system be installed as detailed on the separately appended engineering drawings.
- iii) The stormwater management facilities be inspected by MTE Consultants Inc. during construction and certified to the City of Ottawa upon completion.

All of which is respectfully submitted,

MTE Consultants Inc.



Jolie Nguyen, B.Eng

Designer

519-743-6500

jnquyen@mte85.com



Jeff Lerch, P.Eng

Design Engineer

519-743-6500

jlerch@mte85.com

JHN:dib

https://mte85.sharepoint.com/sites/53510-100/Shared Documents/Reports/rpt_2025-09-16_FSSWM.docx

Appendix A

Sanitary Sewer Design Sheet

120 LUSK STREET CITY OF OTTAWA				SANITARY SEWER DESIGN SHEET ENGINEERING AND PUBLIC WORKS										Design Parameters																				
Project Number: 53510-100 Date: September 12, 2025 Design By: MLW Checked By: CAD File: Q:\53510\100\53510-100-Sanitary Sewer Design Sheet.xlsx														Average Daily Flow Residential 0.00353 L/s/c Commercial 50,000 L/day/Ha Industrial 0.40 L/s/ha Inst. / School 50,000 L/day/Ha																				Mannings "n" 0.013 Min. Velocity 0.8 m/sec Max. Velocity 3.0 m/sec Residential Harmon Peaking Factor F = 1 + 14/(4 + P ^{0.5}) Extraneous Flow 0.25 L/s/ha
				Drainage Area Plan No:																														
LOCATION				RESIDENTIAL AREAS and POPULATION										SCHOOL, INSTITUTIONAL			COMMERCIAL			INDUSTRIAL				INFILTRATION			DESIGN							
STREET	AREA NO.	MANHOLE LOCATION		HECTARES OF EACH DENSITY								POPUL.	CUMUL POPUL.	PEAK FACTOR "F"	PEAK RES. FLOW	HECTARES AND FLOW OF EACH ZONING									TOTALS-C I FLOW	AREA	CUMUL AREA	INFIL FLOW	TOTAL VOLUME FLOW	LENGTH	SLOPE	PIPE SIZE	CAPACITY	FULL FLOW VELOCITY
		FROM MH	TO MH	R2	R3	R4/R5	R6	R7	R8	R9	0.58 L/s/ha					0.58 L/s/ha			0.40 L/s/ha															
				36	72	143	196	312	387	775	AREA					CUMUL AREA	PEAK FLOW	AREA	CUMUL	PEAK FLOW	AREA	CUMUL AREA	PEAK FLOW											
				ha	ha	ha	ha	ha	ha	ha	1000s	1000s	L/sec	ha	ha	L/sec	ha	ha	L/sec	L/sec	ha	ha	L/sec	L/sec	m	%	mm	L/sec	m/s					
	1	Building MH1A	MH1A EX MH-13												0.36	0.36	0.2083				0.2083	0.67 0.00	0.67 0.67	0.1665 0.1665	0.3748 0.3748	28.8 23.7	2.00 2.00	250 250	84.0571 84.0571	1.713 1.713				

**MOE Design Guidelines for Sewage

Appendix B

Storm Sewer Design Sheet

120 LUSK STREET				STORM SEWER DESIGN SHEET								Design Parameters							
CITY OF OTTAWA												ENGINEERING AND PUBLIC WORKS							
Project Number: 53510-100 Date: June 21, 2024 Design By: MLW/JHN Checked By: CAD File: Q:\53510\100\53510-100 - Storm Sewer Design Sheet.xlsx				Drainage Area Plan No:								Q=kAIC, k=0.00278 Manning's "n" 0.013 Intensity (I) = a/(tc+b) ² Min. Velocity 0.800 m/s a = 998 Max. Velocity 6.000 m/s b = 6.053 c = 0.814							
LOCATION				STORMWATER FLOW								DESIGN							
STREET	AREA NUMBER	MANHOLE LOCATION		AREA (A)	RUNOFF COEFF. (C)	A x C	CUMUL. A x C	CONCENTRATION TIME		RAIN INTENSITY (I)	FLOW (Q)	PIPE SIZE	LENGTH	SLOPE	CAPACITY	FULL FLOW VELOCITY			
		FROM MH	TO MH					TOTAL	IN PIPE							m/s	PIPE FULL		
				ha		ha	ha	min	min	mm/hr	L/s	mm	m	%	L/s	m/s	%		
	201	Building	CBMH1	0.129	0.90	0.1161	0.1161	10.0000	0.1701	104.19303	33.62914	250	11.7	0.80	53.18937	1.0836	63.23		
	202	CBMH1	CBMH2	0.059	0.90	0.0531	0.1692	10.1701	0.2410	103.30283	48.59117	300	16.3	0.60	74.90409	1.0597	64.87		
	203	CBMH2	Ex. MH-STM	0.069	0.90	0.0621	0.2313	10.4111	0.2885	102.07045	65.63273	375	21.1	0.60	135.81014	1.2296	48.33		
	204	CB6	CBMH5	0.043	0.90	0.0383	0.0383	10.0000	0.4568	104.19303	11.10544	300	20.8	0.60	74.90409	1.0597	14.83		
		CBMH5	CBMH4	0.072	0.90	0.0644	0.1027	10.4568	0.3392	101.84028	29.07318	300	20.2	0.60	74.90409	1.0597	38.81		
		CBMH4	CBMH3	0.040	0.90	0.0362	0.1389	10.7960	0.3808	100.16818	38.67079	300	24.4	0.60	74.90409	1.0597	51.63		
		CBMH3	Ex. MH-STM	0.086	0.90	0.0771	0.2160	11.1768	0.3877	98.36239	59.06465	375	27.6	0.60	135.81014	1.2296	43.49		

Appendix C

Water Demand Analysis



120 Lusk Street - Medical Office Building
FIRE FLOW DEMANDS

Ottawa, Ontario

Project #: 53510-100

Date: September 12, 2025

Date Printed: 9/16/2025

By: JHN

Development Information ¹							Fire Flow ²													Domestic Flow ^{3,4}								
							Ontario Building Code					Fire Underwriters Survey																
Node ID / Area ID / Building #	F.F.E. (m.a.s.l.)	Description	Area		Bldg Area (1 st Floor)	Total Bldg Area	Building Volume	K	V	S _{tot}	Q	F	F	C	A	F	(2) Occupancy Reduction	(3) Sprinkler Protection ⁵	(4) Building Exposure ⁵	F	F	Fire Flow (Max OBC/FUS)	Per Ottawa Design Guidelines	Average Day	Max Day	Peak Hour	Max Day + Fire Flow	
			m ²		m ²	m ²	m ³				L	L/min	L/s		m ²	L/min					L/min	L/s	L/s	L/s	L/s	L/s	L/s	L/s
1																												
2																												
3																												

Notes:

- 1 Building is assumed to be classified as non-combustible construction type.
- 2 Building is classified as occupancy group E (Mercantile Occupancies)
- 3 Average Daily Demands for the building are based on "Ottawa Design Guildines - Water Distribution" by City of Ottawa, dated July 2010:

Commercial28,000 L/gross ha/day
- 4 Peaking Factors based on ISD-2010-02 in Ottawa Water Design Guildines by City of Ottawa.

Maximum Day =1.8 x Average Day

Maximum Hour =1.5 x Average Day
- 5 The complete building will be equipped with automatic sprinkler protection in accordance to NFPA 13, therefore, 30% sprinkler reduction will be applied as per FUS Water Supply for Publick Protection (2010).

The building exposure reduction assumptions are as per below:

Direction	Separation from Building or PL (m)	OBC	FUS
N	6	0.4	20
S	35	0.0	0
E	19	0.0	15
W	3	0.5	25
		1.9	60

Appendix D

416 Lands Storm Discharge Area Plan (IBI Group, 2022)

Diagram illustrating the components of a catchment area symbol:

- AREA NUMBER (S168)
- RUNOFF COEFFICIENT (0.80)
- AREA IN HECTARES (2.01)
- EMERGENCY FLOW ROUTE (indicated by a double arrow pointing to the bottom of the symbol)

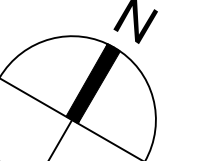
□ MINIMUM BUILDING OPENING TO BE
CONFIRMED AT SITE PLAN STAGE.

14			
13			
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5	REVISED PER CITY COMMENTS	DGY	18:05:22
4	REVISED PER CITY COMMENTS	DGY	18:04:06
3	REVISED PER CITY COMMENTS	DGY	18:01:10
2	REVISED PER CITY COMMENTS	DGY	17:09:26
1	ISSUED FOR CITY REVIEW	DGY	17:05:04
No.	REVISIONS	By	Date



IBI GROUP
400 – 333 Preston Street
Ottawa ON K1S 5N4 Canada
tel 613 225 1311 fax 613 225 9868
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416 LANDS
4401 FALLOWFIELD ROAD



STORM DRAINAGE AREA PLAN

Project No.	Drawing No.
00711	500

Appendix E

Roof Drain Specifications



SPECIFICATION DRAINAGE

Control-Flo

Roof Drainage System



www.zurn.com



Control-Flo...Today's Successful Answer to More

THE ZURN "CONTROL-FLO CONCEPT"

Originally, Zurn introduced the scientifically-advanced "Control-Flo" drainage principle for dead-level roofs. Today, after thousands of successful applications in modern, large dead-level roof areas, Zurn engineers have adapted the comprehensive "Control-Flo" data to **sloped roof** areas.

WHAT IS "CONTROL-FLO"?

It is an advanced method of removing rain water off dead-level or sloped roofs. As contrasted with conventional drainage practices, which attempt to drain off storm water as quickly as it falls on the roof's surface, "Control-Flo" drains the roof at a controlled rate. Excess water accumulates on the roof under controlled conditions...then drains off at a lower rate after a storm abates.

CUTS DRAINAGE COSTS

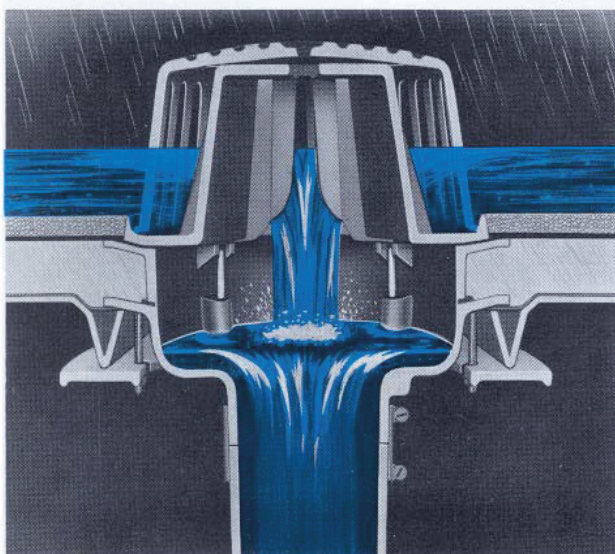
Fewer roof drains, smaller diameter piping, smaller sewer sizes, and lower installation costs are possible with a "Control-Flo" drainage system because roof areas are utilized as temporary storage reservoirs.

REDUCES PROBABILITY OF STORM DAMAGE

Lightens load on combination sewers by reducing rate of water drained from roof tops during severe storms thereby reducing probability of flooded sewers, and consequent backflow into basements and other low areas.

THANKS TO EXCLUSIVE ZURN "AQUA-WEIR" ACTION

Key to successful "Control-Flo" drainage is a unique scientifically-designed weir containing accurately calibrated notches with sides formed by parabolic curves which provide flow rates directly proportional to the head. Shape and size of notches are based on predetermined flow rates, and all factors involved in roof drainage to assure permanent regulation of drainage flow rates for specific geographic locations and rainfall intensities.

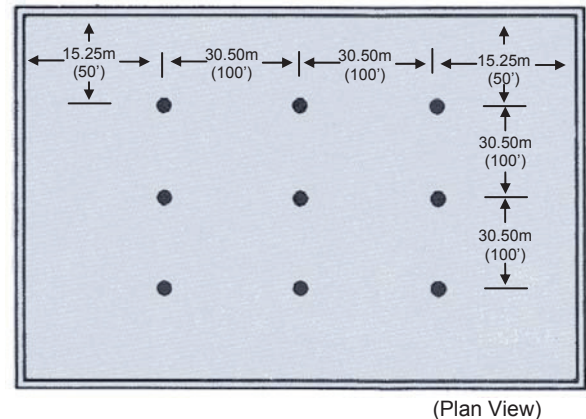


DEFINITION

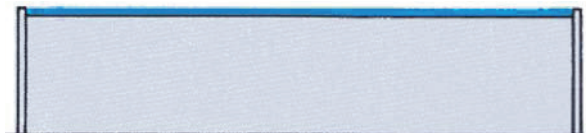
DEAD LEVEL ROOFS

DIAGRAM "A"

A dead-level roof for purposes of applying the Zurn "Control-Flo" drainage principle is one which has been designed for zero slope across its entire surface. Measurements shown are for maximum distances.



(Plan View)

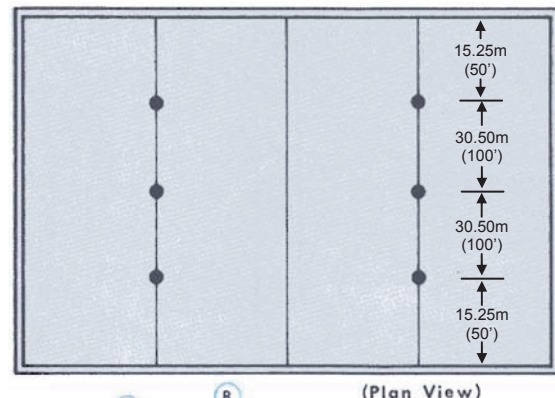


(Section View)

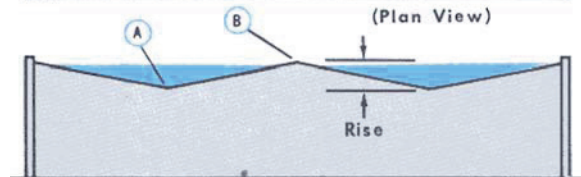
SLOPED ROOFS

DIAGRAM "B"

A sloped roof is one designed commonly with a shallow slope. The Zurn "Control-Flo" drainage system can be applied to any slope which results in a total rise up to 152mm (6"). The total rise of a roof as calculated for "Control-Flo" application is defined as the vertical increase in height in inches, from the low point or valley of a sloping roof (A) to the top of the sloping section (B). (Example: a roof that slopes 3mm (1/8") per foot having a 7.25m (24') span would have a rise of 7.25m x 3mm or 76mm (24' x 1/8" or 3"). Measurements shown are for maximum distances.



(Plan View)

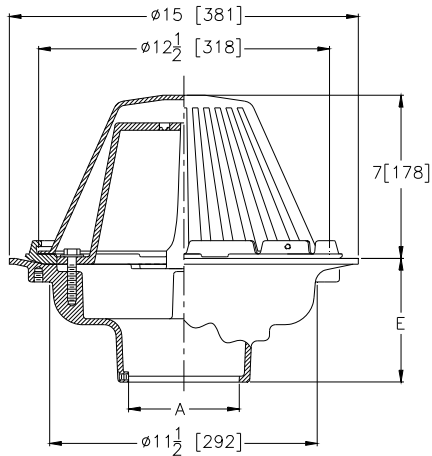


(Section View)

Economical Roof Drainage Installations



SPECIFICATION DATA



ENGINEERING SPECIFICATION: ZURN Z-105 "Control-Flo" roof drain for dead-level or sloped roof construction, Dura-Coated cast iron body. "Control-Flo" weir shall be linear functioning with integral membrane flashing clamp/gravel guard and Poly-Dome. All data shall be verified proportional to flow rates.

ROOF DESIGN RECOMMENDATIONS

Basic roofing design should incorporate protection that will prevent roof overloading by installing adequate overflow scuppers in parapet walls.

GENERAL INFORMATION

The "Control-Flo" roof drainage data is tabulated for four areas (232.25m² (2500 sq. ft.), 464.502m² (5000 sq. ft.), 696.75m² (7500 sq. ft.), 929m² (10,000 sq. ft.) notch areas ratings) for each locality. For each notch area rating the maximum discharge in L.P.M. (G.P.M.) - draindown in hours, and maximum water depth at the drain in inches for a dead level roof — 51mm (2 inch) rise — 102mm (4 inch) rise and 152mm (6 inch) rise—are tabulated. The rise is the total change in elevation from the valley to the peak. Values for areas, rise or combination thereof other than those listed, can be arrived at by extrapolation. All data listed is based on the fifty-year return frequency storm. In other words the maximum conditions as listed will occur on the average of once every fifty years.

NOTE: The tabulated "Control-Flo" data enables the individual engineer to select his own design limiting condition. The limiting condition can be draindown time, roof load factor, or maximum water depth at the drain. If draindown time is the limiting factor because of possible freezing conditions, it must be recognized that the maximum time listed will occur on the average of once every 50 years and would most likely be during a heavy summer thunder storm. Average winter draindown times would be much shorter in duration than those listed.

GENERAL RECOMMENDATIONS

On sloping roofs, we recommend a design depth referred to as an equivalent depth. An equivalent depth is the depth of water attained at the drains that results in the same roof stresses as those realized on a dead-level roof. In all cases this equivalent depth is almost equal to that attained by using the same notch area rating for the different rises to 152mm (6"). With the same depth of water at the drain the roof stresses will decrease with increasing total rise. Therefore, it would be possible to have a depth in excess of 152mm (6") at the drain on a sloping roof without exceeding stresses normally encountered in a 152mm (6") depth on a dead-level roof. However, it is recommended that scuppers be placed to limit the maximum water depth on any roof to 152mm (6") to prevent the overflow of the weirs on the drains and consequent overloading of drain piping. In the few cases where the data shows a flow rate in excess of 136 L.P.M. (30 G.P.M.) if all drains and drain lines are sized according to recommendations, and the one storm in fifty years occurs, the only consequence will be a brief flow through the scuppers or over-flow drains.

NOTE: An equivalent depth is that depth of water attained at the drains at the lowest line or valley of the roof with all other conditions such as notch area and rainfall intensity being equal. For Toronto, Ontario a notch area rating of 464.50m² (5,000 sq. ft.) results in a 74mm (2.9 inch) depth on a dead level roof for a 50-year storm. For the same notch area and conditions, equivalent depths for a 51mm (2"), 102mm (4") and 152mm (6") rise respectively on a sloped roof would be 86mm (3.4"), 104mm (4.1") and 124mm (4.9"). Roof stresses will be approximately equal in all cases.



Control-Flo Drain Selection Is Quick and Easy...

The exclusive Zurn "Selecta-Drain" Chart (pages 8—11) tabulates selection data for 34 localities in Canada. Proper use of this chart constitutes your best assurance of sure, safe, economical application of Zurn "Control-Flo" systems for your specific geographical area. If the "Selecta-Drain" Chart does not cover your specific design criteria, contact Zurn Industries Limited, Mississauga, Ontario, for additional data for your locality. Listed below is additional information pertinent to proper engineering of the "Control-Flo" system.

ROOF USED AS TEMPORARY RETENTION

The key to economical "Control-Flo" is the utilization of large roof areas to temporarily store the maximum amount of water without overloading average roofs or creating excessive draindown time during periods of heavy rainfall. The data shown in the "Selecta-Drain" Chart enables the engineer to select notch area ratings from 232.25 m² (2,500 ft.²) to 929m² (10,000 ft.²) and to accurately predict all other design factors such as maximum roof load, L.P.M. (G.P.M.) discharge, draindown time and water depth at the drain. Obviously, as design factors permit the notch area rating to increase the resulting money saved in being able to use small leaders and drain lines will also increase.

ROOF LOADING AND RUN-OFF RATES

The four values listed in the "Selecta-Drain" Chart for notch area ratings for different localities will normally span the range of good design. If areas per notch below 232.25m² (2,500 ft.²) are used considerable economy of the "Control-Flo" concept is being lost. The area per notch is limited to 929m² (10,000 ft.²) to keep the drain-down time within reasonable limits. Extensive studies show that stresses due to water load on a sloping roof for any fixed set of conditions are very nearly the same as those on a dead-level roof. A sloping roof tends to concentrate more water in the valleys and increase the water depth at this point. The greater depth around the drain leads to a faster run-off rate, particularly a faster early run-off rate. As a result, the total volume of water stored on the roof is less, and the total load on the sloping roof is less. By using the same area on the sloping roof as on the dead-level roof the increase in roof stresses due to increased water depth in the valleys is offset by the decrease in the total load due to less water stored. The net result of the maximum roof stress is approximately the same for any single span rise and fixed set of conditions. A fixed set of conditions, would be the same notch area, the same frequency store, and the same locality.

SPECIAL CONSIDERATIONS FOR STRUCTURAL SAFETY: Normal practice of roof design is based on 18kg (40 lbs.) per 929 cm² (sq ft.). (Subject to local codes and by-laws.) Thus it is extremely important that design is in accordance with normal load factors so deflection will be slight enough in any bay to prevent progressive deflection which could cause water depths to load the roof beyond its design limits.

ADDITIONAL NOTCH RATINGS

The 'Selecta-Drain' Chart along with Tables I and II enables the engineer to select "Control-Flo" Drains and drain pipe sizes for most Canadian applications. These calculations are computed for a proportional flow weir that is sized to give a flow of 23 L.P.M. (5 G.P.M.) per inch of head. The 23 L.P.M. (5 G.P.M.) per inch of head notch opening is selected as the bases of design as it offers the most economical installation as applied to actual rainfall experienced in Canada.

Should you require design criteria for locations outside of Canada or for special project applications please contact Zurn Industries Limited, Mississauga, Ontario.

LEADER AND DRAIN PIPE SIZING

Since all data in the "Selecta-Drain" Chart is based on the 50-year-storm it is possible to exceed the water depth listed in these charts if a 100-year or 1000-year storm would occur. Therefore, for good design it is recommended that scuppers or other methods be used to limit water depth to the design depth and tables I and II be used to size the leaders and drain pipes. If the roof is capable of supporting more water than the design depth it is permissible to locate the scuppers or other overflow means at a height that will allow a greater water depth on the roof. However, in this case the leader and drain pipes should be sized to handle the higher flow rates possible based on a flow rate of 23 L.P.M. (5 G.P.M.) per inch of depth at the drain.

PROPER DRAIN LOCATION

The following good design practice is recommended for selecting the proper number of "Control-Flo" drains for a given area. **On dead-level roofs**, drains should be located no further than 15.25m (50 feet) from edge of roof and no further than 30.50m (100 feet) between drains. See diagram "A" page 2. **On sloping roofs**, drains should be located in the valleys at a distance no greater than 15.25m (50 feet) from each end of the valleys and no further than 30.50m (100 feet) between drains. See diagram "B" page 2. Compliance with these recommendations will assure good run off regardless of wind direction.



Saves Specification Time, Assures Proper Application

QUICK, EASY SELECTION

Using the "Selecta-Drain" Chart (pages 9—13) in combination with the steps and examples appearing below, should save you countless hours in engineering specification time. This vast compilation of data is related to the proper selection of drains for 34 cities. All cities in alphabetical order by province. If a specific city does not appear in the tabulation, chooses the city nearest your area and select the proper drain using these factors.

3 EASY STEPS...

AND 3 TYPICAL EXAMPLES FOR APPLICATION OF SURE, SCIENTIFIC CONTROL OF DRAINAGE FROM DEAD-LEVEL AND SLOPING ROOFS WITH THE ZURN CONCEPT.

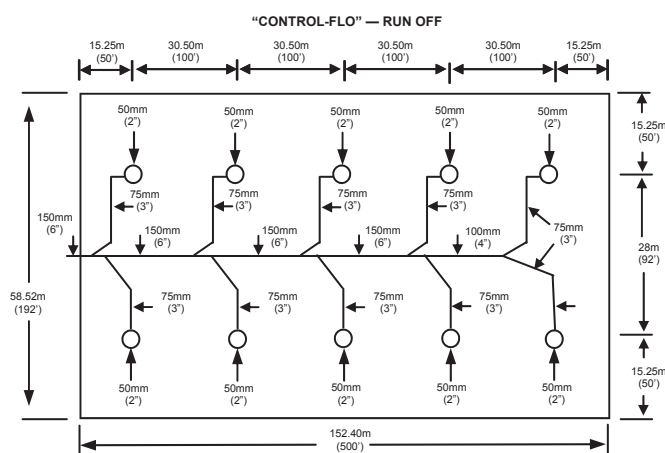
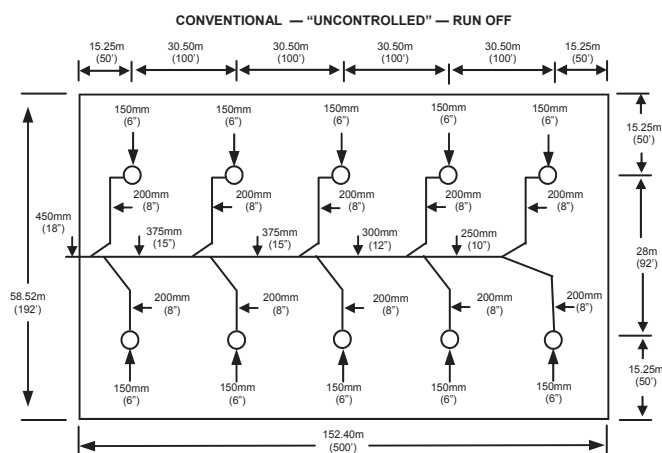
NOTE: Where roof area to be drained is adjacent to one or more vertical walls projecting above the roof, then a percentage of the of the wall(s) must be added to the roof area in determining total roof area to be drained.

TORONTO, ONTARIO		DEAD-LEVEL ROOF	102mm (4 INCH) SLOPE	152mm (6 INCH) SLOPE
1	Determine total roof area or individual areas when roof is divided by expansion joints or peaks in the case of sloping roof.	Roof Area: 56.52m x 152.40m = 8918.40m ² (192ft x 500ft = 96,000 sq. ft.) (See Z105 layout bottom of this page.)	3 Individual Roof Areas: 19.50m x 152.40m = 2972.80m ² (64ft x 500ft = 32,000 sq. ft.) Valleys 152.40m (500ft) long 3 x 2972.80 = 8918.40m ² (3 x 32,000 = 96,000 sq. ft.)	2 Individual Roof Areas: 29.87m x 152.40m = 4552m ² (98ft x 500ft = 49,000 sq. ft.) Valleys 152.40m (500ft) long 2 x 4552 = 9104m ² (2 x 49,000 = 98,000 sq. ft.)
2	Divide roof area or individual areas by Zurn Notch Area Rating selected to obtain the total number of notches required.	Zurn Notch Area Rating selected for Toronto = 464.50m ² (5,000 sq. ft.) from "Selecta-Drain Chart, page 11. Total Roof Area = 8918.40m ² (96,000 sq. ft.) Entire roof. 464.50m ² (5,000 sq. ft.) notch area = 19.2 notches—USE 20.	Zurn Notch Area Rating selected for Toronto = 464.50m ² (5,000 sq. ft.) from "Selecta-Drain Chart, page 11. Total Roof Area = 2972.80m ² (32,000 sq. ft.) Each area. 464.50m ² (5,000 sq. ft.) notch area = 6.4 notches—USE 7 PER AREA.	Zurn Notch Area Rating selected for Toronto = 464.50m ² (5,000 sq. ft.) from "Selecta-Drain Chart, page 11. Total Roof Area = 4552m ² (49,000 sq. ft.) Each area. 464.50m ² (5,000 sq. ft.) notch area = 9.8 notches—USE 10 PER AREA.
3	Determine total number of drains required by not exceeding maximum spacing dimensions in the preceding instructions. See Diagrams "A" or "B", page 2. Divide total number of notches required to determine the number of notches per drain. Note maximum water depth at drain and use this dimension to determine scupper height. Maximum scupper height to be used is 152mm (6"). <i>Use this flow rate to size leaders and drain lines.</i>	*10 drains required. All drains must have two notches each for a total of 20 notches. Flow rate is 66 L.P.M. (14.5 G.P.M.) per notch. Size leaders for 2 notch weirs for a flow rate of 66 L.P.M. (14.5 G.P.M.) 50 mm (two inch) pipe size leaders required. Maximum water depth and scupper height is 74mm (2.9"). Requires 19 hours drain-down time maximum. For drain, vertical and horizontal pipe sizing data see Tables I and II on page 6 and 7.	**5 drains per area required located in the valleys 15.25m (50ft.) from each end with 3 in the middle at 30.50m (100ft.) spacings. Two drains on ends with two notches—3 drains in middle on notch each for a total of 7 notches. Maximum flow rate 93 L.P.M. (20.5 G.P.M.) per notch. Leader size 50mm (2") for single notch weirs—75mm (3") notch weirs. Maximum water depth and scupper height is 104mm (4.1"). Requires 11 hours draindown time maximum. For drain, vertical and horizontal pipe sizing data see Tables I and II on page 6 and 7.	**5 drains per area required located in the valleys 15.25m (50ft.) from each end with 3 in the middle at 30.50m (100ft.) spacing in the middle. 10 notches are required therefore all drains must have two notches. Flow rate is 111 L.P.M. (24.5 G.P.M.) per notch. Size all leaders for 2 notch weirs. 75mm (3") pipe size required. Maximum water depth and scupper height is 124mm (4.9"). Requires 9 hours draindown time maximum. For drain, vertical and horizontal pipe sizing data see Tables I and II on page 6 and 7.

*See Diagram "A" page 2 for recommended drain placement.
**See Diagram "B" page 2 for recommended drain placement.

*See Diagram "A" page 2 for recommended drain placement.
**See Diagram "B" page 2 for recommended drain placement.

DEAD LEVEL ROOF 6mm (1/4") PER FT. SLOPE STORM DRAIN





Select The Proper Vertical Drain Leaders

ROOF DRAINAGE DATA

The flow rate for any design condition can be easily read from the data contained on the following pages; the tabulations shown below (and on the opposite page) can be used to simplify selection of drain line sizes.

TABLE 1 - SUGGESTED RELATION OF DRAIN OUTLET AND VERTICAL LEADER SIZE TO ZURN CONTROL-FLO ROOF DRAINS (BASED ON NATIONAL PLUMBING CODE ASA -A40.8 DATA ON VERTICAL LEADERS).

No. of Notches in Drain	Max. Flow per Notch in L.P.M. (G.P.M.)		
	Pipe Size		
	50mm (2")	75mm (3")	100mm (4")
1	136* (30*)	—	—
2	68 (15)	136* (30*)	—
3	45 (10)	136* (30*)	—
4	—	105 (23)	136* (30*)
5	—	82 (18)	136* (30*)
6	—	68 (15)	136* (30*)

*Maximum flow obtainable from 1 notch with 152mm (6") water depth at drain.

Table 1 should be used to select **vertical drain** leaders which at the same time establishes the drain outlet size. This table illustrates the minimum flow per notch in L.P.M. (G.P.M.) Since the Z-105 drain is available with a minimum of one and a maximum of six notches, calculations have already been made and are listed in this table for any quantity of weir notch openings established in your design. It was determined ten drains with two notches each weir would be required in the Dead-Level Roof example on page 5. A 66 L.P.M. (14.5 G.P.M.) discharge per notch flow rate was also established.

Once this design criteria has been determined it will be the key to the proper selection of all drain outlet sizes, vertical and horizontal storm drain sizes in Table I and II. Enter the column "Number of Notches in Drain", Table I, read down the column to the figure 2 which indicates two notches in weir, then read across until you reach a figure equal to or closest figure in excess of 66 L.P.M. (14.5 G.P.M.) You will find fifteen in the column under 50mm (2") which represents the pipe size. Therefore all drain outlets and vertical leaders are 50mm (2") size.

Let us digress for a moment assuming a specific structure requires a total of six drains each containing a weir with a different number of notches. One with 1, one with 2, etc. Table 1 discloses the pipe size for one notch is 50mm (2"), two notch is 50mm (2"), three notch is 75mm (3"), four notch is 75mm (3"), five notch is 75mm (3") and six notch is 75mm (3") as they all equal or closely exceed the 66 L.P.M. (14.5 G.P.M.) design.

NOTE: Although pipe size calculations should be based on accumulated flow rate, local by-laws should be referred to for minimum pipe size requirements and roof drain spacing.

TABLE II should be used to select **horizontal** storm drain piping. Use the same flow rate 66 L.P.M. (14.5 G.P.M.) used to establish the vertical leaders to size the storm drainage system and main storm drain. Let us assume the ten drains each with two notch weirs were actually on the roof in two separate lines of five drains each and joined at a common point before leaving the building. Since Table II includes 3mm (1/8"), 6mm (1/4") and 13mm (1/2") per foot slope, let us **use 6mm (1/4") as our basis for selection** which will take us to the centre section. Starting with the first of five drains we enter the extreme left column in Table II and read down to the figure 2 since this drain has two notches in weir, read across horizontally and the size of first section of horizontal storm drain is 75mm (3") between 1st and 2nd drain, return to left hand column proceed reading down until you reach figure 4 then read across horizontally and the pipe size will be 100mm (4") between 2nd and 3rd drain, 100mm (4") between 3rd and 4th and 125mm (5") (if available) between 4th and 5th. If not available use 150mm (6"). (You may be tempted to use 100mm (4") since the capacity is close. We recommend you go to the larger size.) Pipe size leaving 5th drain would be 150mm (6"). The same sizing would hold true for the second line of five drains. Since both columns of five drains each are being joined together before leaving the building there will be total of twenty notches discharging into the main building storm sewer. Enter left hand column Table II, read down until you reach the figure twenty, then read across horizontally to the 6mm (1/4") per 305mm (1') slope column and you will see a 150mm (6") storm drain will handle the job adequately. The same procedure should be followed for sloped roof installations. The above method of sizing was done to better acquaint you with Table II and its use. The more economical and practical way of laying out and installing this same job is illustrated in the control-flo layout shown on bottom of page 5.

NOTE: Although pipe size calculations should be based on accumulated flow rates, local by-laws should be referred to for minimum pipe size requirements and roof drain spacing.

Select Proper Horizontal Storm Drain Piping



Table II — SUGGESTED RELATION OF HORIZONTAL STORM DRAIN SIZE TO ZURN CONTROL-FLO ROOF DRAINAGE

Total No. of Notches Discharging to Storm Drain	MAX. FLOW PER NOTCH IN L.P.M. (G.P.M.)								MAX. FLOW PER NOTCH IN L.P.M. (G.P.M.)								MAX. FLOW PER NOTCH IN L.P.M. (G.P.M.)							
	Storm Drain Size 3mm (1/8") per 305mm (1') Slope								Storm Drain Size 6mm (1/4") per 305mm (1') Slope								Storm Drain Size 13mm (1/2") per 305mm (1') Slope							
	75 (3")	100 (4")	125 (5")	150 (6")	200 (8")	250 (10")	300 (12")	375 (15")	75 (3")	100 (4")	125 (5")	150 (6")	200 (8")	250 (10")	300 (12")	75 (3")	100 (4")	125 (5")	150 (6")	200 (8")	250 (10")	300 (12")		
1	136* (30*)	—	—	—	—	—	—	—	136* (30*)	—	—	—	—	—	—	136* (30*)	—	—	—	—	—	—		
2	77 (17)	136* (30*)	—	—	—	—	—	—	109 (24)	136* (30*)	—	—	—	—	—	136* (30*)	—	—	—	—	—	—		
3	50 (11)	118 (26)	136* (30*)	—	—	—	—	—	73 (16)	136* (30*)	—	—	—	—	—	100 (22)	136* (30*)	—	—	—	—	—		
4	36 (8)	86 (19)	136* (30*)	—	—	—	—	—	55 (12)	127 (28)	136* (30*)	—	—	—	—	77 (17)	136* (30*)	—	—	—	—	—		
5	—	65 (15)	127* (28*)	136* (30*)	—	—	—	—	—	100 (22)	136* (30*)	—	—	—	—	59 (13)	136* (30*)	—	—	—	—	—		
6	—	59 (13)	105 (23)	136* (30*)	—	—	—	—	—	82 (18)	136* (30*)	—	—	—	—	50 (11)	118 (26)	136* (30*)	—	—	—	—		
7	—	50 (11)	91 (20)	136* (30*)	—	—	—	—	—	73 (16)	127 (28)	136* (30*)	—	—	—	—	100 (22)	136* (30*)	—	—	—	—		
8	—	—	77 (17)	127 (28)	136* (30*)	—	—	—	—	64 (14)	114 (25)	136* (30*)	—	—	—	—	86 (19)	136* (30*)	—	—	—	—		
9	—	—	68 (15)	114 (25)	136* (30*)	—	—	—	—	55 (12)	100 (22)	136* (30*)	—	—	—	—	77 (17)	136* (30*)	—	—	—	—		
10	—	—	64 (14)	100 (22)	136* (30*)	—	—	—	—	—	91 (20)	136* (30*)	—	—	—	—	68 (15)	123 (27)	136* (30*)	—	—	—		
11	—	—	55 (12)	91 (20)	136* (30*)	—	—	—	—	—	82 (18)	132 (29)	136* (30*)	—	—	—	64 (14)	114 (25)	136* (30*)	—	—	—		
12	—	—	—	82 (18)	136* (30*)	—	—	—	—	—	73 (16)	118 (26)	136* (30*)	—	—	—	59 (13)	105 (23)	136* (30*)	—	—	—		
13	—	—	—	77 (17)	136* (30*)	—	—	—	—	—	68 (15)	109 (24)	136* (30*)	—	—	—	55 (12)	95 (21)	136* (30*)	—	—	—		
14	—	—	—	73 (16)	136* (30*)	—	—	—	—	—	64 (14)	100 (22)	136* (30*)	—	—	—	—	86 (19)	136* (30*)	—	—	—		
15	—	—	—	68 (15)	136* (30*)	—	—	—	—	—	59 (13)	95 (21)	136* (30*)	—	—	—	—	82 (18)	132 (29)	136* (30*)	—	—		
16	—	—	—	64 (14)	136* (30*)	—	—	—	—	—	—	91 (20)	136* (30*)	—	—	—	—	77 (17)	123 (27)	136* (30*)	—	—		
17	—	—	—	59 (13)	127 (28)	136* (30*)	—	—	—	—	—	82 (18)	136* (30*)	—	—	—	—	73 (16)	118 (26)	136* (30*)	—	—		
18	—	—	—	55 (12)	118 (26)	136* (30*)	—	—	—	—	—	77 (17)	136* (30*)	—	—	—	—	68 (15)	109 (24)	136* (30*)	—	—		
19	—	—	—	—	114 (25)	136* (30*)	—	—	—	—	—	73 (16)	136* (30*)	—	—	—	—	64 (14)	105 (23)	136* (30*)	—	—		
20	—	—	—	—	109 (24)	136* (30*)	—	—	—	—	—	68 (15)	136* (30*)	—	—	—	—	59 (13)	100 (22)	136* (30*)	—	—		
23	—	—	—	—	91 (20)	136* (30*)	—	—	—	—	—	64 (14)	132 (29)	136* (30*)	—	—	—	55 (12)	86 (19)	136* (30*)	—	—		
25	—	—	—	—	86 (19)	136* (30*)	—	—	—	—	—	59 (13)	123 (27)	136* (30*)	—	—	—	—	77 (17)	136* (30*)	—	—		
30	—	—	—	—	73 (16)	127 (28)	136* (30*)	—	—	—	—	—	100 (22)	136* (30*)	—	—	—	—	64 (14)	136* (30*)	—	—		
35	—	—	—	—	59 (13)	109 (24)	136* (30*)	—	—	—	—	—	86 (19)	136* (30*)	—	—	—	—	55 (12)	123 (27)	136* (30*)	—		
40	—	—	—	—	55 (12)	95 (21)	136* (30*)	—	—	—	—	—	77 (17)	136* (30*)	—	—	—	—	—	105 (23)	136* (30*)	—		
45	—	—	—	—	—	86 (19)	136* (30*)	—	—	—	—	—	68 (15)	123 (27)	136* (30*)	—	—	—	—	95 (21)	136* (30*)	—		
50	—	—	—	—	—	77 (17)	123 (27)	136* (30*)	—	—	—	—	59 (13)	109 (24)	136* (30*)	—	—	—	—	86 (19)	136* (30*)	—		
55	—	—	—	—	—	68 (15)	114 (25)	136* (30*)	—	—	—	—	—	100 (22)	136* (30*)	—	—	—	—	77 (17)	136* (30*)	—		
60	—	—	—	—	—	64 (14)	105 (23)	136* (30*)	—	—	—	—	—	91 (20)	136* (30*)	—	—	—	—	68 (15)	127 (28)	136* (30*)		
65	—	—	—	—	—	59 (13)	95 (21)	136* (30*)	—	—	—	—	—	82 (18)	136* (30*)	—	—	—	—	64 (14)	118 (26)	136* (30*)		
70	—	—	—	—	—	55 (12)	91 (20)	136* (30*)	—	—	—	—	—	77 (17)	127 (28)	—	—	—	—	59 (13)	109 (24)	136* (30*)		

*Maximum flow obtainable from 1 notch with 152mm (6") water depth at drain.



Select Proper Horizontal Storm Drain Piping

TABLE III - TO BE USED WHEN ROOF STORM WATER RUN OFF AND OTHER SURFACE WATER RUN OFF IS BEING CONSOLIDATED INTO ONE COMMON MAIN HORIZONTAL STORM SEWER.

Flow capacity of vertical leaders litres per minute (gallons per minute)

Pipe Size	Maximum Capacity L.P.M. (G.P.M.)
50mm (2")	136 (30)
75mm (3")	409 (90)
100mm (4")	864 (190)
†125mm (5")	1582 (348)
150mm (6")	2550 (561)

†In some areas 125mm (5") drainage pipe may not be available.

Flow capacity of horizontal storm sewers litres per minute (gallons per minute).

Pipe Size	Slope per 305mm (1'0")		
	3mm (1/8")	6mm (1/4")	13mm (1/2")
75mm (3")	163 (36)	232 (51)	327 (72)
100mm (4")	355 (78)	505 (111)	714 (157)
†125mm (5")	646 (142)	914 (201)	1291 (284)
150mm (6")	1050 (231)	1487 (327)	2100 (462)
200mm (8")	2264 (498)	3205 (705)	4528 (996)
250mm (10")	4100 (902)	5796 (1275)	8201 (1804)
300mm (12")	6669 (1467)	9437 (2076)	13338 (2934)
375mm (15")	12120 (2666)	17157 (3774)	24239 (5332)

Note: Although pipe size calculations should be based on accumulated flow rate, local by-laws should be referred to for minimum pipe size requirements and roof drain spacing.

SCUPPER AND OVERFLOW DRAINS

Roofing members and understructures, weakened by seepage and rot resulting from improper drainage and roof construction can give away under the weight of rapidly accumulated water during flash storms. Thus, it is recommended, and often required by building codes, to install scuppers and overflow drains in parapet-type roofs. Properly selected and sized scuppers and overflow drains are vital to a well-engineered drainage system to prevent excessive loading, erosion, seepage and rotting.



Selecta-Drain Chart

LOCATION	SQUARE METRE (SQUARE FOOT)	ROOF LOAD FACTOR KGS. (LBS.)	TOTAL ROOF SLOPE											
			DEAD LEVEL			51mm (2") RISE			102mm (4") RISE			152mm (6") RISE		
			L.P.M. (G.P.M.) Discharge	Draindown Time Hrs.	mm (in.) Water Depth	L.P.M. (G.P.M.) Discharge	Draindown Time Hrs.	mm (in.) Water Depth	L.P.M. (G.P.M.) Discharge	Draindown Time Hrs.	mm (in.) Water Depth	L.P.M. (G.P.M.) Discharge	Draindown Time Hrs.	mm (in.) Water Depth
Calgary, Alberta	232 (2,500)	4.7 (10.4)	45.5 (10)	7	51 (2)	57 (12.5)	6	63.5 (2.5)	72.5 (16)	4	81.5 (3.2)	86.5 (19)	3.2	96.5 (3.8)
	465 (5,000)	5.9 (13)	57 (12.5)	17	63.5 (2.5)	66 (14.5)	14	73.5 (2.9)	82 (18)	9	91.5 (3.6)	97.5 (21.5)	7.5	109 (4.3)
	697 (7,500)	6.4 (14)	61.5 (13.5)	28	68.5 (2.7)	72.5 (16)	22	81.5 (3.2)	88.5 (19.5)	15	99 (3.9)	104.5 (23)	12	117 (4.6)
	929 (10,000)	6.8 (15.1)	66 (14.5)	38	73.5 (2.9)	77.5 (17)	31	86.5 (3.4)	93 (20.5)	22	104 (4.1)	109 (24)	17	122 (4.8)
Edmonton, Alberta	232 (2,500)	4.5 (9.9)	43 (9.5)	7	48.5 (1.9)	57 (12.5)	6	63.5 (2.5)	72.5 (16)	4	81.5 (3.2)	82 (18)	3	91.5 (3.6)
	465 (5,000)	5.9 (13)	57 (12.5)	17	63.5 (2.5)	68 (15)	14.5	76 (3)	84 (18.5)	9.5	94 (3.7)	97.5 (21.5)	7.5	109 (4.3)
	697 (7,500)	6.6 (14.5)	63.5 (14)	28	71 (2.8)	75 (16.5)	24	84 (3.3)	97.5 (21.5)	16	104 (4.1)	107 (23.5)	12	119.5 (4.7)
	929 (10,000)	7.1 (15.6)	68 (15)	38	76 (3.0)	79.5 (17.5)	32	89 (3.5)	100 (22)	22	112 (4.4)	113.5 (25)	18	127 (5.0)
Penticton, British Columbia	232 (2,500)	3.8 (8.3)	36.5 (8)	6	40.5 (1.6)	38.5 (8.5)	4	43 (1.7)	52.5 (11.5)	3	58.5 (2.3)	61.5 (13.5)	2.3	68.5 (2.7)
	465 (5,000)	4.0 (8.8)	38.5 (8.5)	13	43 (1.7)	41 (9)	9	45.5 (1.8)	57 (12.5)	6	63.5 (2.5)	68 (15)	5	76 (3)
	697 (7,500)	4.2 (9.3)	41 (9)	21	45.5 (1.8)	43 (9.5)	14.5	48.5 (1.9)	61.5 (13.5)	10.5	68.5 (2.7)	72.5 (16)	8	81.5 (3.2)
	929 (10,000)	4.2 (9.3)	41 (9)	27	45.5 (1.8)	45.5 (10)	20	51 (2)	63.5 (14)	14	71 (2.8)	75 (16.5)	11	84 (3.3)
Vancouver, British Columbia	232 (2,500)	3.3 (7.3)	32 (7)	5.5	35.5 (1.4)	38.5 (8.5)	4	43 (1.7)	47.5 (10.5)	2.8	53.5 (2.1)	57 (12.5)	2	63.5 (2.5)
	465 (5,000)	4.0 (8.8)	38.5 (8.5)	13	43 (1.7)	45.5 (10)	10	51 (2)	57 (12.5)	6	63.5 (2.5)	68 (15)	5	76 (3)
	697 (7,500)	4.5 (9.9)	43 (9.5)	22	48.5 (1.9)	50 (11)	17	56 (2.2)	63.5 (14)	11	71 (2.8)	75 (16.5)	8.5	84 (3.3)
	929 (10,000)	4.9 (10.9)	47.5 (10.5)	30	53.5 (2.1)	54.5 (12)	24	61 (2.4)	68 (15)	15	76 (3)	79.5 (17.5)	12	89 (3.5)
Victoria, British Columbia	232 (2,500)	3.3 (7.3)	32 (7)	5.5	35.5 (1.4)	38.5 (8.5)	4	43 (1.7)	43 (9.5)	2.5	48.5 (1.9)	54.5 (12)	2	61 (2.4)
	465 (5,000)	4.0 (8.8)	38.5 (8.5)	13	43 (1.7)	45.5 (10)	10	51 (2)	54.5 (12)	6	61 (2.4)	68 (15)	5	76 (3)
	697 (7,500)	4.5 (9.9)	43 (9.5)	22	48.5 (1.9)	50 (11)	16	56 (2.2)	59 (13)	10	66 (2.6)	75 (16.5)	8	84 (3.3)
	929 (10,000)	4.7 (10.4)	45.5 (10)	30	51 (2)	54.5 (12)	23	61 (2.4)	63.5 (14)	14	71 (2.8)	79.5 (17.5)	12	89 (3.5)
Brandon, Manitoba	232 (2,500)	5.9 (13)	57 (12.5)	8	63.5 (2.5)	68 (15)	7	76 (3)	82 (18)	4.5	91.5 (3.6)	92.5 (21)	3.5	106.5 (4.2)
	465 (5,000)	7.3 (16.1)	73 (16)	20	81.5 (3.2)	84 (18.5)	17	94 (3.7)	97.5 (21.5)	11	109 (4.3)	113.5 (25)	8.5	127 (5)
	697 (7,500)	8.3 (18.2)	79.5 (17.5)	32	89 (3.5)	93 (20.5)	27	104 (4.1)	107 (23.5)	19	119.5 (4.7)	125 (27.5)	15	139.5 (5.5)
	929 (10,000)	9.0 (19.8)	86.5 (19)	43	96.5 (3.8)	100 (22)	38	112 (4.4)	113.5 (25)	26	127 (5.0)	132 (29)	21	147.5 (5.8)
Winnipeg, Manitoba	232 (2,500)	4.7 (10.4)	45.5 (10)	7	51 (2)	57 (12.5)	6	63.5 (2.5)	75 (16.5)	4	84 (3.3)	86.5 (19)	3.2	96.5 (3.8)
	465 (5,000)	5.9 (13)	57 (12.5)	17	63.5 (2.5)	68 (15)	15	76 (3)	84 (18.5)	10	94 (3.7)	100 (22)	7.5	112 (4.4)
	697 (7,500)	6.6 (14.5)	63.5 (14)	28	71 (2.8)	75 (16.5)	24	84 (3.3)	93 (20.5)	16	104 (4.1)	107 (23.5)	12	119.5 (4.7)
	929 (10,000)	7.1 (15.6)	68 (15)	39	76 (3)	82 (18)	32	91.5 (3.6)	97.5 (21.5)	22	109 (4.3)	113.5 (25)	17	127 (5.0)
Campbellton, New Brunswick	232 (2,500)	6.4 (14)	62 (13.5)	9	68.5 (2.7)	70.5 (15.5)	7	78.5 (3.1)	79.5 (17.5)	4.5	89 (3.5)	91 (20)	3.5	101.5 (4.0)
	465 (5,000)	9.0 (19.8)	86.5 (19)	22	96.5 (3.8)	91 (20)	18	101.5 (4)	102.5 (22.5)	12	115 (4.5)	113.5 (25)	9	127 (5.0)
	697 (7,500)	10.4 (22.9)	100 (22)	35	112 (4.4)	102.5 (22.5)	28	114.5 (4.5)	118 (26)	20	132 (5.2)	132 (29)	15	147.5 (5.8)
	929 (10,000)	11.3 (25)	109 (24)	47	122 (4.8)	111.5 (24.5)	40	124.5 (4.9)	127.5 (28)	29	142 (5.6)	141 (31)	22	157.5 (6.2)



Selecta-Drain Chart

LOCATION	SQUARE METRE (SQUARE FOOT)	ROOF LOAD FACTOR KGS. (LBS.)	TOTAL ROOF SLOPE											
			DEAD LEVEL			51mm (2") RISE			102mm (4") RISE			152mm (6") RISE		
			L.P.M. (G.P.M.) Discharge	Draindown Time Hrs.	mm (in.) Water Depth	L.P.M. (G.P.M.) Discharge	Draindown Time Hrs.	mm (in.) Water Depth	L.P.M. (G.P.M.) Discharge	Draindown Time Hrs.	mm (in.) Water Depth	L.P.M. (G.P.M.) Discharge	Draindown Time Hrs.	mm (in.) Water Depth
Chatham, New Brunswick	232 (2,500)	4.5 (9.9)	43 (9.5)	7	48.5 (1.9)	52.5 (11.5)	5.5	58.5 (2.3)	63.5 (14)	3.5	71 (2.8)	77.5 (17)	2.9	86.5 (3.4)
	465 (5,000)	5.7 (12.5)	54.5 (12)	16	61 (2.4)	63.5 (14)	13	71 (2.8)	77.5 (17)	9	86.5 (3.4)	91 (20)	7	101.5 (4.0)
	697 (7,500)	6.4 (14)	61.5 (13.5)	27	68.5 (2.7)	68 (15)	22	76 (3)	84 (18.5)	14	94 (3.7)	102.5 (22.5)	12	114.5 (4.5)
	929 (10,000)	6.6 (14.6)	63.5 (14)	37	71 (2.8)	75 (16.5)	30	84 (3.3)	91 (20)	20	101.5 (4.0)	107 (23.5)	16	119.5 (4.7)
Moncton, New Brunswick	232 (2,500)	4.3 (9.4)	41 (9)	7	45.5 (1.8)	54.5 (12)	6	61 (2.4)	63.5 (14)	3.5	71 (2.8)	72.5 (16)	2.7	81.5 (3.2)
	465 (5,000)	5.9 (13)	57 (12.5)	17	63.5 (2.5)	68 (15)	14	76 (3)	82 (18)	9	91.5 (3.6)	93 (20.5)	7	104 (4.1)
	697 (7,500)	6.6 (14.6)	63.5 (14)	28	71 (2.8)	79.5 (17.5)	24	89 (3.5)	93 (20.5)	16	104 (4.1)	104.5 (23)	12	117 (4.6)
	929 (10,000)	7.5 (16.6)	73.5 (16)	39	81.5 (3.2)	84 (18.5)	34	94 (3.7)	100 (22)	23	112 (4.4)	113.5 (25)	17	127 (5.0)
Saint John, New Brunswick	232 (2,500)	5.7 (12.5)	54.5 (12)	8	61 (2.4)	57 (12.5)	6	63.5 (2.5)	75 (16.5)	4	84 (3.3)	86.5 (19)	3	96.5 (3.8)
	465 (5,000)	7.5 (16.6)	72.5 (16)	20	81.5 (3.2)	79.5 (17.5)	16	89 (3.5)	95.5 (21)	11	106.5 (4.2)	104.5 (23)	8	117 (4.6)
	697 (7,500)	8.7 (19.2)	84 (18.5)	32	94 (3.7)	93 (20.5)	27	104 (4.1)	107 (23.5)	19	119.5 (4.7)	118 (26)	13.5	132 (5.2)
	929 (10,000)	9.7 (21.3)	93 (20.5)	44	104 (4.1)	104.5 (23)	38	117 (4.6)	113.5 (25)	27	127 (5.0)	127.5 (28)	20	142 (5.6)
Gander, Newfound- land	232 (2,500)	3.5 (7.8)	34 (7.5)	5.5	38 (1.5)	45.5 (10)	5	51 (2.0)	57 (12.5)	3.5	63.5 (2.5)	68 (15)	2.5	76 (3.0)
	465 (5,000)	4.7 (10.4)	45.5 (10)	15	51 (2.0)	57 (12.5)	12	63.5 (2.5)	72.5 (16)	8	81.5 (3.2)	82 (18)	6.5	91.5 (3.6)
	697 (7,500)	5.7 (12.5)	54.5 (12)	25	61 (2.4)	63.5 (14)	21	71 (2.8)	79.5 (17.5)	13.5	89 (3.5)	93 (20.5)	11	104 (4.1)
	929 (10,000)	6.1 (13.5)	59 (13)	35	66 (2.6)	70.5 (15.5)	29	78.5 (3.1)	84 (18.5)	19	94 (3.7)	100 (22)	15	112 (4.4)
St. Andrews, Newfound- land	232 (2,500)	3.5 (7.8)	34 (7.5)	5.5	38 (1.5)	45.5 (10)	5	51 (2.0)	59 (13)	3.5	66 (2.6)	63.5 (14)	2.5	71 (2.8)
	465 (5,000)	5.2 (11.4)	47.5 (10.5)	15	53.5 (2.1)	59 (13)	13	66 (2.6)	72.5 (16)	8	81.5 (3.2)	79.5 (17.5)	6	89 (3.5)
	697 (7,500)	5.9 (13)	57 (12.5)	26	63.5 (2.5)	66 (14.5)	21	73.5 (2.9)	82 (18)	14	91.5 (3.6)	88.5 (19.5)	10	99 (3.9)
	929 (10,000)	6.6 (14.6)	63.5 (14)	36	71 (2.8)	72.5 (16)	30	81.5 (3.2)	86.5 (19)	20	96.5 (3.8)	95.5 (21)	14.5	106.5 (4.2)
St. John's, Newfound- land	232 (2,500)	5.9 (13)	57 (12.5)	8	63.5 (2.6)	68 (15)	7	76 (3.0)	77.5 (17)	4.5	86.5 (3.4)	86.5 (19)	3.2	96.5 (3.8)
	465 (5,000)	8.5 (18.7)	82 (18)	21	91.5 (3.6)	91 (20)	18	101 (4.0)	100 (22)	11	112 (4.4)	113.5 (25)	9	127 (5.0)
	697 (7,500)	10.6 (23.4)	102.5 (22.5)	34	114.5 (4.5)	109 (24)	29	122 (4.8)	122.5 (27)	21	137 (5.4)	132 (29)	15	147.5 (5.8)
	929 (10,000)	11.8 (26)	113.5 (25)	48	127 (5.0)	129.5 (28.5)	43	145 (5.7)	143 (31.5)	33	160 (6.3)	150 (33)	24	167.5 (6.6)
Torbay, Newfound- land	232 (2,500)	4.9 (10.9)	47.5 (10.5)	7.5	53.5 (2.1)	61.5 (13.5)	6.5	68.5 (2.7)	75 (16.5)	4	84 (3.3)	84 (18.5)	3	94 (3.7)
	465 (5,000)	6.4 (14)	61.5 (13.5)	18	68.5 (2.7)	75 (16.5)	15.5	84 (3.3)	88.5 (19.5)	10	99 (3.9)	102.5 (22.5)	8	114.5 (4.5)
	697 (7,500)	7.3 (16.1)	70.5 (15.5)	29	78.5 (3.1)	84 (18.5)	25	94 (3.7)	100 (22)	17.5	112 (4.4)	113.5 (25)	13	127 (5)
	929 (10,000)	8.0 (17.7)	77.5 (17)	40	86.5 (3.4)	88.5 (19.5)	34	99 (3.9)	107 (23.5)	24	119.5 (4.7)	122.5 (27)	19	137 (5.4)
Halifax, Nova Scotia	232 (2,500)	5.9 (13)	57 (12.5)	8	63.5 (2.5)	68 (15)	7	76 (3.0)	77.5 (17)	4.5	86.5 (3.4)	86.5 (19)	3.2	96.5 (3.8)
	465 (5,000)	8.5 (18.7)	82 (18)	21	91.5 (3.6)	91 (20)	18	101.5 (4.0)	100 (22)	11	112 (4.4)	113.5 (25)	9	127 (5.0)
	697 (7,500)	10.6 (23.4)	102.5 (22.5)	34	114.5 (4.5)	109 (24)	29	122 (4.8)	122.5 (27)	21	137 (5.4)	132 (29)	15	147.5 (5.8)
	929 (10,000)	11.8 (26)	113.5 (25)	48	127 (5.0)	129.5 (28.5)	43	145 (5.7)	143 (31.5)	33	160 (6.3)	150 (33)	24	167.5 (6.6)



Selecta-Drain Chart

LOCATION	SQUARE METRE (SQUARE FOOT)	ROOF LOAD FACTOR KGS. (LBS.)	TOTAL ROOF SLOPE											
			DEAD LEVEL			51mm (2") RISE			102mm (4") RISE			152mm (6") RISE		
			L.P.M. (G.P.M.) Discharge	Draindown Time Hrs.	mm (in.) Water Depth	L.P.M. (G.P.M.) Discharge	Draindown Time Hrs.	mm (in.) Water Depth	L.P.M. (G.P.M.) Discharge	Draindown Time Hrs.	mm (in.) Water Depth	L.P.M. (G.P.M.) Discharge	Draindown Time Hrs.	mm (in.) Water Depth
Sydney, Nova Scotia	232 (2,500)	4.3 (9.4)	41 (9)	6.5	45.5 (1.8)	45.5 (10)	5	51 (2.0)	57 (12.5)	3.5	6.5 (2.5)	68 (15)	2.5	76 (3)
	465 (5,000)	5.7 (12.5)	54.5 (12)	16	61 (2.4)	59 (13)	13	66 (2.6)	75 (16.5)	8	84 (3.3)	84 (18.5)	6.5	94 (3.7)
	697 (7,500)	6.4 (14)	61.5 (13.5)	28	68.5 (2.7)	68 (15)	22	76 (3)	84 (18.5)	14	94 (3.7)	97.5 (21.5)	11	109 (4.3)
	929 (10,000)	7.1 (15.6)	68 (15)	38	76 (3)	75 (16.5)	30	84 (3.3)	91 (20)	20	101.5 (4)	104.5 (23)	16	117 (4.6)
Yarmouth, Nova Scotia	232 (2,500)	6.4 (14)	61.5 (13.5)	9	68.5 (2.7)	70.5 (15.5)	7.5	78.5 (3.1)	82 (18)	4.5	91.5 (3.6)	91 (20)	3.5	101.5 (4)
	465 (5,000)	8.3 (18.2)	79.5 (17.5)	21	89 (3.5)	88.5 (19.5)	18	99 (3.9)	104.5 (23)	12	117 (4.6)	116 (25.5)	9	129.5 (5.1)
	697 (7,500)	9.4 (20.8)	91 (20)	34	101.5 (4)	102.5 (22.5)	29	114.5 (4.5)	118 (26)	21	132 (5.2)	132 (29)	15	147.5 (5.8)
	929 (10,000)	10.4 (22.9)	100 (22)	45	112 (4.4)	109 (24)	41	122 (4.8)	129.5 (28.5)	29	145 (5.7)	141 (31)	22	157.5 (6.2)
Thunder Bay, Ontario	232 (2,500)	4.9 (10.9)	47.5 (10.5)	7.5	53.5 (2.1)	61.5 (13.5)	6.5	68.5 (2.7)	75 (16.5)	4	84 (3.3)	88.5 (19.5)	3.5	91.5 (3.6)
	465 (5,000)	6.1 (13.5)	59 (13)	18	66 (2.6)	72.5 (16)	15	81.5 (3.2)	86.5 (19)	9.5	96.5 (3.8)	102.5 (22.5)	7.5	114.5 (4.5)
	697 (7,500)	6.6 (14.6)	63.5 (14)	28	71 (2.8)	77.5 (17)	24	86.5 (3.4)	93 (20.5)	16	104 (4.1)	109 (24)	13	122 (4.8)
	929 (10,000)	7.1 (15.6)	68 (15)	38	76 (3)	84 (18.5)	33	94 (3.7)	97.5 (21.5)	22	109 (4.3)	116 (25.5)	18	129.5 (5.1)
Guelph, Ontario	232 (2,500)	5.7 (12.5)	54.5 (12)	8	61 (2.4)	63.5 (14)	7	71 (2.8)	86.5 (19)	5	96.5 (3.8)	100 (22)	3.7	112 (4.4)
	465 (5,000)	6.6 (14.6)	63.5 (14)	19	71 (2.8)	75 (16.5)	15.5	84 (3.3)	97.5 (21.5)	11	109 (4.3)	116 (25.5)	9	129.5 (5.1)
	697 (7,500)	7.3 (16.1)	70.5 (15.5)	29	78.5 (3.1)	82 (18)	25	91.5 (3.6)	104.5 (23)	18	117 (4.6)	125 (27.5)	14	139.5 (5.5)
	929 (10,000)	8.0 (17.7)	77.5 (17)	40	86.5 (3.4)	84 (18.5)	34	94 (3.7)	109 (24)	26	122 (4.8)	132 (29)	20	147.5 (5.8)
Hamilton, Ontario	232 (2,500)	5.9 (13)	57 (12.5)	8.5	63.5 (2.5)	72.5 (16)	7.5	81.5 (3.2)	93 (20.5)	5	104 (4.1)	109 (24)	4	122 (4.8)
	465 (5,000)	6.6 (14.6)	63.5 (14)	19	71 (2.8)	79.5 (17.5)	16	89 (3.5)	104.5 (23)	12	117 (4.6)	122.5 (27)	9	137 (5.4)
	697 (7,500)	6.8 (15.1)	66 (14.5)	28	73.5 (2.9)	84 (18.5)	26	94 (3.7)	111.5 (24.5)	20	124.5 (4.9)	127.5 (28)	15	142 (5.6)
	929 (10,000)	7.1 (15.6)	68 (15)	39	76 (3)	86.5 (19)	34	96.5 (3.8)	116 (25.5)	27	129.5 (5.1)	134 (29.5)	21	150 (5.9)
Kingston, Ontario	232 (2,500)	6.4 (14)	61.5 (13.5)	9	68.5 (2.7)	77.5 (17)	8	86.5 (3.4)	91 (20)	5	101.5 (4)	109 (24)	4	122 (4.8)
	465 (5,000)	7.5 (16.6)	72.5 (16)	20	81.5 (3.2)	86.5 (19)	18	96.5 (3.8)	104.5 (23)	12	117 (4.6)	122.5 (27)	9.5	137 (5.4)
	697 (7,500)	8.5 (18.7)	82 (18)	31	91.5 (3.6)	93 (20.5)	28	104 (4.1)	111.5 (24.5)	20	124.5 (4.9)	132 (29)	15	147.5 (5.8)
	929 (10,000)	8.7 (19.2)	86.5 (19)	42	96.5 (3.8)	97.5 (21.5)	38	109 (4.3)	116 (25.5)	27	129.5 (5.1)	68 (15)	21	152.5 (6)
London, Ontario	232 (2,500)	6.1 (13.5)	59 (13)	8.5	66 (2.6)	72.5 (16)	7.5	81.5 (3.2)	88.5 (19.5)	5	99 (3.9)	107 (23.5)	4	119.5 (4.7)
	465 (5,000)	7.1 (15.6)	68 (15)	20	76 (3)	84 (18.5)	17	94 (3.7)	102.5 (22.5)	12	114.5 (4.5)	122.5 (27)	9.5	137 (5.4)
	697 (7,500)	8.0 (17.7)	77.5 (17)	30	86.5 (3.4)	88.5 (19.5)	27	99 (3.9)	109 (24)	19	122 (4.8)	129.5 (28.5)	15	145 (5.7)
	929 (10,000)	8.5 (18.7)	82 (18)	41	91.5 (3.6)	91 (20)	36	101.5 (4)	113.5 (25)	27	127 (5)	134 (29.5)	21	150 (5.9)
North Bay, Ontario	232 (2,500)	5.7 (12.5)	54.5 (12)	8	61 (2.4)	68 (15)	7	76 (3)	86.5 (19)	5	96.5 (3.8)	100 (22)	3.8	112 (4.4)
	465 (5,000)	6.6 (14.6)	63.5 (14)	19	71 (2.8)	79.5 (17.5)	16	89 (3.5)	97.5 (21.5)	11	109 (4.3)	113.5 (25)	9	127 (5)
	697 (7,500)	7.5 (16.6)	72.5 (16)	30	81.5 (3.2)	86.5 (19)	26	96.5 (3.8)	107 (23.5)	19	119.5 (4.7)	122.5 (27)	14	137 (5.4)
	929 (10,000)	8.3 (18.2)	77.5 (17)	40	86.5 (3.4)	93 (20.5)	36	104 (4.1)	111.5 (24.5)	26	124.5 (4.9)	127.5 (28)	20	142 (5.6)

Selecta-Drain Chart



LOCATION	SQUARE METRE (SQUARE FOOT)	ROOF LOAD FACTOR KGS. (LBS.)	TOTAL ROOF SLOPE											
			DEAD LEVEL			51mm (2") RISE			102mm (4") RISE			152mm (6") RISE		
			L.P.M. (G.P.M.) Discharge	Draindown Time Hrs.	mm (in.) Water Depth	L.P.M. (G.P.M.) Discharge	Draindown Time Hrs.	mm (in.) Water Depth	L.P.M. (G.P.M.) Discharge	Draindown Time Hrs.	mm (in.) Water Depth	L.P.M. (G.P.M.) Discharge	Draindown Time Hrs.	mm (in.) Water Depth
Ottawa, Ontario	232 (2,500)	4.7 (10.4)	45.5 (10)	7	51 (2)	59 (13)	6.5	66 (2.6)	77.5 (17)	4.5	86.5 (3.4)	86.5 (19)	3.2	96.5 (3.8)
	465 (5,000)	5.9 (13)	57 (12.5)	17	63.5 (2.5)	68 (15)	14	76 (3)	86.5 (19)	10	96.5 (3.8)	100 (22)	7.5	112 (4.4)
	697 (7,500)	6.4 (14)	61.5 (13.5)	27	68.5 (2.7)	75 (16.5)	23	84 (3.3)	93 (20.5)	16	104 (4.1)	107 (23.5)	12	119.5 (4.7)
	929 (10,000)	6.6 (14.6)	63.5 (14)	36	71 (2.8)	79.5 (17.5)	32	89 (3.5)	97.5 (21.5)	22	109 (4.3)	113.5 (25)	18	127 (5)
St. Thomas, Ontario	232 (2,500)	5.7 (12.5)	54.5 (12)	8	61 (2.4)	68 (15)	7	76 (3.0)	86.5 (19)	5	96.5 (3.8)	104.5 (23)	4	117 (4.6)
	465 (5,000)	6.6 (14.6)	63.5 (14)	19	71 (2.8)	77.5 (17)	16	86.5 (3.4)	97.5 (21.5)	11	109 (4.3)	118 (26)	9	132 (5.2)
	697 (7,500)	7.1 (16.6)	68 (15)	29	76 (3.0)	82 (18)	26	91.5 (3.6)	102.5 (22.5)	18	114.5 (4.5)	125 (27.5)	15	139.5 (5.5)
	929 (10,000)	7.5 (16.6)	72.5 (16)	40	81.5 (3.2)	86.5 (19)	34	96.5 (3.8)	107 (23.5)	24	119.5 (4.7)	132 (29)	20	147.5 (5.8)
Timmins, Ontario	232 (2,500)	4.3 (9.4)	41 (9)	7	45.5 (1.8)	57 (12.5)	6	63.5 (2.5)	72.5 (16)	4	81.5 (3.2)	86.5 (19)	3.3	96.5 (3.8)
	465 (5,000)	5.7 (12.5)	54.5 (12)	16	61 (2.4)	63.5 (14)	14	71 (2.8)	82 (18)	9	91.5 (3.6)	97.5 (21.5)	7.5	109 (4.3)
	697 (7,500)	6.4 (14)	61.5 (13.5)	27	68.5 (2.7)	70.5 (15.5)	22	78.5 (3.1)	86.5 (19)	15	96.5 (3.8)	104.5 (23)	12	117 (4.6)
	929 (10,000)	6.6 (14.6)	63.5 (14)	36	71 (2.8)	72.5 (16)	30	81.5 (3.2)	91 (20)	21	101.5 (4.0)	109 (24)	17	122 (4.8)
Toronto, Ontario	232 (2,500)	5.7 (12.5)	54.5 (12)	8	61 (2.4)	66 (14.5)	7	73.5 (2.9)	82 (18)	4.5	91.5 (3.6)	97.5 (21.5)	3.5	109 (4.3)
	465 (5,000)	6.8 (15.1)	66 (14.5)	19	73.5 (2.9)	77.5 (17)	16	86.5 (3.4)	93 (20.5)	11	104 (4.1)	111.5 (24.5)	9	124.5 (4.9)
	697 (7,500)	8.0 (17.7)	77.5 (17)	30	86.5 (3.4)	84 (18.5)	26	94 (3.7)	100 (22)	18	112 (4.4)	120.5 (26.5)	14	134.5 (5.3)
	929 (10,000)	8.7 (19.2)	82 (18)	42	91.5 (3.6)	86.5 (19)	34	96.5 (3.8)	104.5 (23)	24	117 (4.6)	127.5 (28)	20	142 (5.6)
Windsor, Ontario	232 (2,500)	6.1 (13.5)	59 (13)	8.5	66 (2.6)	70.5 (15.5)	7.5	78.5 (3.1)	84 (18.5)	4.5	94 (3.7)	107 (23.5)	4	119.5 (4.7)
	465 (5,000)	7.1 (15.6)	68 (15)	20	76 (3.0)	79.5 (17.5)	16	89 (3.5)	97.5 (21.5)	11	109 (4.3)	118 (26)	9	132 (5.2)
	697 (7,500)	8.0 (17.7)	77.5 (17)	30	86.5 (3.4)	86.5 (19)	26	96.5 (3.8)	107 (23.5)	18	119.5 (4.7)	125 (27.5)	15	139.5 (5.5)
	929 (10,000)	8.7 (19.2)	82 (18)	42	91.5 (3.6)	91 (20)	36	101.5 (4.0)	113.5 (25)	26	127 (5.0)	129.5 (28.5)	20	145 (5.7)
Charlottetown, Prince Edward Island	232 (2,500)	4.9 (10.9)	47.5 (10.5)	7.5	53.5 (2.1)	57 (12.5)	6	63.5 (2.5)	68 (15)	3.8	76 (3.0)	79.5 (17.5)	3	89 (3.5)
	465 (5,000)	6.6 (14.6)	63.5 (14)	19	71 (2.8)	75 (16.5)	15.5	84 (3.3)	88.5 (19.5)	10	99 (3.9)	100 (22)	7.5	112 (4.4)
	697 (7,500)	7.8 (17.2)	75 (16.5)	31	84 (3.3)	86.5 (19)	26	96.5 (3.8)	102.5 (22.5)	18	114.5 (4.5)	113.5 (25)	13	127 (5.0)
	929 (10,000)	8.7 (19.2)	84 (18.5)	42	94 (3.7)	97.5 (21.5)	37	106.5 (4.2)	111.5 (24.5)	26	124.5 (4.9)	125 (27.5)	20	139.5 (5.5)
Montreal, Quebec	232 (2,500)	5.2 (11.4)	50 (11)	7.5	56 (2.2)	61.5 (13.5)	7	68.5 (2.7)	79.5 (17.5)	4.5	89 (3.5)	97.5 (21.5)	3.5	109 (4.36)
	465 (5,000)	5.9 (13)	57 (12.5)	17	63.5 (2.5)	70.5 (15.5)	15	78.5 (3.1)	88.5 (19.5)	10	99 (3.9)	109 (24)	8	122 (4.8)
	697 (7,500)	6.1 (13.5)	59 (13)	27	66 (2.6)	72.5 (16)	23	81.5 (3.2)	93 (20.5)	16	104 (4.1)	113.5 (25)	13	127 (5.0)
	929 (10,000)	6.4 (14)	61.5 (13.5)	36	68.5 (2.7)	77.5 (17)	31	86.5 (3.4)	95.5 (21)	22	106.5 (4.2)	120.5 (26.5)	19	134.5 (5.3)
Quebec City, Quebec	232 (2,500)	5.4 (12)	52.5 (11.5)	8	58.5 (2.3)	63.5 (14)	7	71 (2.8)	79.5 (17.5)	4.5	89 (3.5)	97.5 (21.5)	3.5	109 (4.3)
	465 (5,000)	6.4 (14)	61.5 (13.5)	18	68.5 (2.7)	70.5 (15.5)	15	78.5 (3.1)	84 (18.5)	10	94 (3.7)	104.5 (23)	8	117 (4.6)
	697 (7,500)	6.6 (14.6)	63.5 (14)	28	71 (2.8)	72.5 (16)	23	81.5 (3.2)	86.5 (19)	15	96.5 (3.8)	107 (23.5)	12	119.5 (4.7)
	929 (10,000)	7.1 (15.6)	68 (15)	37	76 (3.0)	77.5 (17)	31	86.5 (3.4)	88.5 (19.5)	20	99 (3.9)	109 (24)	17	122 (4.8)

Selecta-Drain Chart



LOCATION	SQUARE METRE (SQUARE FOOT)	ROOF LOAD FACTOR KGS. (LBS.)	TOTAL ROOF SLOPE											
			DEAD LEVEL			51mm (2") RISE			102mm (4") RISE			152mm (6") RISE		
			L.P.M. (G.P.M.) Discharge	Draindown Time Hrs.	mm (in.) Water Depth	L.P.M. (G.P.M.) Discharge	Draindown Time Hrs.	mm (in.) Water Depth	L.P.M. (G.P.M.) Discharge	Draindown Time Hrs.	mm (in.) Water Depth	L.P.M. (G.P.M.) Discharge	Draindown Time Hrs.	mm (in.) Water Depth
Regina, Saskatchewan	232 (2,500)	4.5 (9.9)	43 (9.5)	7	48.5 (1.9)	54.5 (12)	6	61 (2.4)	72.5 (16)	4	81.5 (3.2)	79.5 (17.5)	3	89 (3.5)
	465 (5,000)	6.4 (14)	61.5 (13.5)	18	68.5 (2.7)	68 (15)	14	76 (3.0)	86.5 (19)	10	96.5 (3.8)	97.5 (21.5)	7.5	109 (4.3)
	697 (7,500)	7.3 (16.1)	70.5 (15.5)	29	78.5 (3.1)	77.5 (17)	24	86.5 (3.4)	100 (22)	17	112 (4.4)	109 (24)	12	122 (4.8)
	929 (10,000)	8.3 (18.2)	79.5 (17.5)	40	89 (3.5)	82 (18)	32	91.5 (3.6)	104.5 (23)	24	117 (4.6)	118 (26)	18	132 (5.2)
Saskatoon, Saskatchewan	232 (2,500)	4.0 (8.8)	38.5 (8.5)	6	43 (1.7)	57 (12.5)	6	63.5 (2.5)	66 (14.5)	3.8	73.5 (2.9)	77.5 (17)	2.8	86.5 (3.4)
	465 (5,000)	5.7 (12.5)	54.5 (12)	16	61 (2.4)	68 (15)	14.5	76 (3.0)	82 (18)	9	91.5 (3.6)	95.5 (21)	7	106.5 (4.2)
	697 (7,500)	6.6 (14.6)	63.5 (14)	28	71 (2.8)	75 (16.5)	24	84 (3.3)	91 (20)	16	101.5 (4.0)	104.5 (23)	12	117 (4.6)
	929 (10,000)	7.1 (15.6)	68 (15)	38	76 (3.0)	82 (18)	32	91.5 (3.6)	97.5 (21.5)	22	109 (4.3)	113.5 (25)	18	127 (5.0)



ZURN INDUSTRIES LIMITED
3544 NASHUA DRIVE · MISSISSAUGA, ONT L4V 1L2
PHONE: 905/405-8272 · FAX: 905/405-1292

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Appendix F

MIDUSS Calculations, IDF Parameters & MIDUSS Output

CALCULATIONS

Orifice Equation (MIDUSS NET)

$$Q = C_c \frac{\pi}{4} D^5 \sqrt{2g(H-2/3D)}$$

where C_c coefficient of contraction
 H head relative to the invert of the orifice
 D orifice diameter
 g gravitational acceleration

IDF Parameters

IDF Parameters	2-Year Storm Event	5-Year Storm Event	100-Year Storm Event	100-Year Storm Event + 20%
A	732.951	998.071	1735.688	2082.82
B	6.199	6.053	6.014	5.890
C	0.810	0.814	0.820	0.824

```

"          MIDUSS Output ----->"
"          MIDUSS version                      Version 2.25  rev. 473"
"          MIDUSS created                      Sunday, February 7, 2010"
"          10  Units used:                      ie METRIC"
"          Job folder:                        Q:\53510\100\MIDUSS\JHN"
"          Output filename:                    2 year v3.out"
"          Licensee name:                      A"
"          Company                            "
"          Date & Time last used:              6/21/2024 at 2:47:51 PM"
" 31      TIME PARAMETERS"
"          5.000  Time Step"
"          180.000 Max. Storm length"
"          1500.000 Max. Hydrograph"
" 32      STORM Chicago storm"
"          1  Chicago storm"
"          732.951 Coefficient A"
"          6.199  Constant B"
"          0.810  Exponent C"
"          0.400  Fraction R"
"          180.000 Duration"
"          1.000  Time step multiplier"
"          Maximum intensity          103.571  mm/hr"
"          Total depth                31.880  mm"
"          6  002hyd  Hydrograph extension used in this file"
" 33      CATCHMENT 201"
"          1  Triangular SCS"
"          1  Equal length"
"          1  SCS method"
"          201 Building Rooftop"
"          100.000 % Impervious"
"          0.129  Total Area"
"          10.000 Flow length"
"          1.500  Overland Slope"
"          0.000  Pervious Area"
"          10.000 Pervious length"
"          1.500  Pervious slope"
"          0.129  Impervious Area"
"          10.000 Impervious length"
"          1.500  Impervious slope"
"          0.250  Pervious Manning 'n'"
"          75.000 Pervious SCS Curve No."
"          0.000  Pervious Runoff coefficient"
"          0.100  Pervious Ia/S coefficient"
"          8.467  Pervious Initial abstraction"
"          0.015  Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.827  Impervious Runoff coefficient"
"          0.100  Impervious Ia/S coefficient"
"          0.518  Impervious Initial abstraction"
"          0.028      0.000      0.000      0.000 c.m/sec"

```

	Catchment 201	Pervious	Impervious	Total Area	
	Surface Area	0.000	0.129	0.129	hectare"
	Time of concentration	16.174	1.278	1.278	minutes"
	Time to Centroid	122.762	89.774	89.774	minutes"
	Rainfall depth	31.880	31.880	31.880	mm"
	Rainfall volume	0.00	41.12	41.12	c.m"
	Rainfall losses	26.820	5.515	5.515	mm"
	Runoff depth	5.060	26.364	26.364	mm"
	Runoff volume	0.00	34.01	34.01	c.m"
	Runoff coefficient	0.000	0.827	0.827	"
	Maximum flow	0.000	0.028	0.028	c.m/sec"
40	HYDROGRAPH Add Runoff "				
	4 Add Runoff "				
	0.028	0.028	0.000	0.000"	
54	POND DESIGN"				
	0.028	Current peak flow	c.m/sec"		
	0.037	Target outflow	c.m/sec"		
	34.0	Hydrograph volume	c.m"		
	11.	Number of stages"			
	0.000	Minimum water level	metre"		
	0.150	Maximum water level	metre"		
	0.000	Starting water level	metre"		
	0	Keep Design Data: 1 = True; 0 = False"			
		Level Discharge	Volume"		
		0.000	0.000	0.000"	
		0.01500	0.00151	0.07760"	
		0.03000	0.00302	0.6208"	
		0.04500	0.00454	2.095"	
		0.06000	0.00605	4.966"	
		0.07500	0.00756	9.700"	
		0.09000	0.00907	16.762"	
		0.1050	0.01058	26.617"	
		0.1200	0.01210	39.715"	
		0.1350	0.01361	54.265"	
		0.1500	0.01512	68.815"	
	1.	ROOFTOP"			
		Roof area	Store area	Area/drain	Drain flow
		hectare	hectare	sq.metre	L/min/25mm
		0.129	0.097	250.000	37.800
		Roof slope"			
		g H:1V"			
		66.667"			
		Using 4 roofdrains on roofstorage area of 970. square metre"			
		Peak outflow	0.008	c.m/sec"	
		Maximum level	0.081	metre"	
		Maximum storage	12.319	c.m"	
		Centroidal lag	1.744	hours"	
		0.028	0.028	0.008	0.000 c.m/sec"
40		HYDROGRAPH	Combine	1"	
	6	Combine "			
	1	Node #"			
		Total Site"			
		Maximum flow	0.008	c.m/sec"	

"		Hydrograph volume	33.972	c.m"
"		0.028 0.028 0.008	0.008"	
" 40		HYDROGRAPH Start - New Tributary"		
"	2	Start - New Tributary"		
"		0.028 0.000 0.008	0.008"	
" 33		CATCHMENT 202"		
"	1	Triangular SCS"		
"	1	Equal length"		
"	1	SCS method"		
"	202	West Parking Lot 1"		
"	100.000	% Impervious"		
"	0.059	Total Area"		
"	10.000	Flow length"		
"	1.200	Overland Slope"		
"	0.000	Pervious Area"		
"	10.000	Pervious length"		
"	1.200	Pervious slope"		
"	0.059	Impervious Area"		
"	10.000	Impervious length"		
"	1.200	Impervious slope"		
"	0.250	Pervious Manning 'n'"		
"	75.000	Pervious SCS Curve No."		
"	0.000	Pervious Runoff coefficient"		
"	0.100	Pervious Ia/S coefficient"		
"	8.467	Pervious Initial abstraction"		
"	0.015	Impervious Manning 'n'"		
"	98.000	Impervious SCS Curve No."		
"	0.829	Impervious Runoff coefficient"		
"	0.100	Impervious Ia/S coefficient"		
"	0.518	Impervious Initial abstraction"		
"		0.013 0.000 0.008	0.008 c.m/sec"	
"		Catchment 202 Pervious Impervious Total Area "		
"		Surface Area 0.000 0.059 0.059	hectare"	
"		Time of concentration 17.293 1.367 1.367	minutes"	
"		Time to Centroid 124.048 89.900 89.899	minutes"	
"		Rainfall depth 31.880 31.880 31.880	mm"	
"		Rainfall volume 0.00 18.81 18.81	c.m"	
"		Rainfall losses 26.815 5.445 5.445	mm"	
"		Runoff depth 5.065 26.435 26.435	mm"	
"		Runoff volume 0.00 15.60 15.60	c.m"	
"		Runoff coefficient 0.000 0.829 0.829	"	
"		Maximum flow 0.000 0.013 0.013	c.m/sec"	
" 40		HYDROGRAPH Add Runoff "		
"	4	Add Runoff "		
"		0.013 0.013 0.008	0.008"	
" 40		HYDROGRAPH Copy to Outflow"		
"	8	Copy to Outflow"		
"		0.013 0.013 0.013	0.008"	
" 40		HYDROGRAPH Combine 1"		
"	6	Combine "		


```

"      1 Node #"
"      Total Site"
"      Maximum flow      0.019 c.m/sec"
"      Hydrograph volume 49.568 c.m"
"      0.013 0.013 0.013 0.019"
" 40 HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      0.013 0.000 0.013 0.019"
" 33 CATCHMENT 203"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      203 SW Parking Lot"
" 100.000 % Impervious"
"      0.069 Total Area"
"      10.000 Flow length"
"      1.200 Overland Slope"
"      0.000 Pervious Area"
"      10.000 Pervious length"
"      1.200 Pervious slope"
"      0.069 Impervious Area"
"      10.000 Impervious length"
"      1.200 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      75.000 Pervious SCS Curve No."
"      0.000 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      8.467 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.829 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.015 0.000 0.013 0.019 c.m/sec"
"      Catchment 203 Pervious Impervious Total Area "
"      Surface Area 0.000 0.069 0.069 hectare"
"      Time of concentration 17.293 1.367 1.367 minutes"
"      Time to Centroid 124.048 89.900 89.899 minutes"
"      Rainfall depth 31.880 31.880 31.880 mm"
"      Rainfall volume 0.00 22.00 22.00 c.m"
"      Rainfall losses 26.815 5.445 5.445 mm"
"      Runoff depth 5.065 26.435 26.435 mm"
"      Runoff volume 0.00 18.24 18.24 c.m"
"      Runoff coefficient 0.000 0.829 0.829 "
"      Maximum flow 0.000 0.015 0.015 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.015 0.015 0.013 0.019"
" 54 POND DESIGN"
"      0.015 Current peak flow c.m/sec"

```

```

"      0.037 Target outflow c.m/sec"
"      18.2 Hydrograph volume c.m"
"      7. Number of stages"
"    103.400 Minimum water level metre"
"    103.750 Maximum water level metre"
"    103.400 Starting water level metre"
"      0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge Volume"
"    103.400 0.000 0.000"
"    103.550 0.00689 1.01E-05"
"    103.600 0.00795 0.7100"
"    103.650 0.00889 4.340"
"    103.700 0.00973 13.820"
"    103.750 0.01051 30.870"
"    103.800 0.01124 54.500"
"    1. HOR. ORIFICES"
"      Orifice Orifice Orifice Number of"
"      invert coefficie diameter orifices"
"    103.400 0.630 0.0900 1.000"
"      Peak outflow 0.008 c.m/sec"
"      Maximum level 103.622 metre"
"      Maximum storage 2.302 c.m"
"      Centroidal lag 1.528 hours"
"      0.015 0.015 0.008 0.019 c.m/sec"
" 40 HYDROGRAPH Combine 1"
"    6 Combine "
"    1 Node #"
"      Total Site"
"      Maximum flow 0.027 c.m/sec"
"      Hydrograph volume 67.482 c.m"
"      0.015 0.015 0.008 0.027"
" 40 HYDROGRAPH Start - New Tributary"
"    2 Start - New Tributary"
"      0.015 0.000 0.008 0.027"
" 33 CATCHMENT 204"
"    1 Triangular SCS"
"    1 Equal length"
"    1 SCS method"
"      204 Controlled Area"
"    100.000 % Impervious"
"      0.240 Total Area"
"      20.000 Flow length"
"      1.200 Overland Slope"
"      0.000 Pervious Area"
"      20.000 Pervious length"
"      1.200 Pervious slope"
"      0.240 Impervious Area"
"      20.000 Impervious length"
"      1.200 Impervious slope"
"      0.250 Pervious Manning 'n'"

```

```

"      75.000  Pervious SCS Curve No."
"      0.000  Pervious Runoff coefficient"
"      0.100  Pervious Ia/S coefficient"
"      8.467  Pervious Initial abstraction"
"      0.015  Impervious Manning 'n'"
"    98.000  Impervious SCS Curve No."
"      0.832  Impervious Runoff coefficient"
"      0.100  Impervious Ia/S coefficient"
"      0.518  Impervious Initial abstraction"
"          0.049      0.000      0.008      0.027 c.m/sec"
"      Catchment 204      Pervious      Impervious Total Area "
"      Surface Area      0.000      0.240      0.240      hectare"
"      Time of concentration 26.212      2.072      2.072      minutes"
"      Time to Centroid      134.673      90.977      90.977      minutes"
"      Rainfall depth      31.880      31.880      31.880      mm"
"      Rainfall volume      0.00      76.51      76.51      c.m"
"      Rainfall losses      26.812      5.351      5.351      mm"
"      Runoff depth      5.068      26.528      26.528      mm"
"      Runoff volume      0.00      63.67      63.67      c.m"
"      Runoff coefficient      0.000      0.832      0.832      "
"      Maximum flow      0.000      0.049      0.049      c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"      4      Add Runoff "
"          0.049      0.049      0.008      0.027"
" 54      POND DESIGN"
"      0.049      Current peak flow      c.m/sec"
"      0.037      Target outflow      c.m/sec"
"      63.7      Hydrograph volume      c.m"
"      7.      Number of stages"
"    101.220      Minimum water level      metre"
"    103.800      Maximum water level      metre"
"    101.220      Starting water level      metre"
"      0      Keep Design Data: 1 = True; 0 = False"
"          Level Discharge      Volume"
"    101.220      0.000      0.000"
"    103.550      0.02388      12.450"
"    103.600      0.02414      13.960"
"    103.650      0.02439      22.230"
"    103.700      0.02465      46.120"
"    103.750      0.02490      94.800"
"    103.800      0.02515      171.200"
"      1.      ORIFICES"
"          Orifice      Orifice      Orifice Number of"
"          invert coefficie      diameter      orifices"
"    101.220      0.630      0.0850      1.000"
"      Peak outflow      0.024      c.m/sec"
"      Maximum level      103.622      metre"
"      Maximum storage      17.609      c.m"
"      Centroidal lag      1.675      hours"
"          0.049      0.049      0.024      0.027 c.m/sec"

```

" 40	HYDROGRAPH	Combine	1"		
"	6	Combine "			
"	1	Node #"			
"		Total Site"			
"		Maximum flow	0.049	c.m/sec"	
"		Hydrograph volume	130.989	c.m"	
"		0.049	0.049	0.024	0.049"
" 40	HYDROGRAPH	Start - New Tributary"			
"	2	Start - New Tributary"			
"		0.049	0.000	0.024	0.049"
" 33	CATCHMENT	205"			
"	1	Triangular SCS"			
"	1	Equal length"			
"	1	SCS method"			
"	205	Uncontrolled to Lusk"			
"	10.300	% Impervious"			
"	0.060	Total Area"			
"	2.000	Flow length"			
"	17.500	Overland Slope"			
"	0.054	Pervious Area"			
"	2.000	Pervious length"			
"	17.500	Pervious slope"			
"	0.006	Impervious Area"			
"	2.000	Impervious length"			
"	17.500	Impervious slope"			
"	0.250	Pervious Manning 'n'"			
"	75.000	Pervious SCS Curve No."			
"	0.156	Pervious Runoff coefficient"			
"	0.100	Pervious Ia/S coefficient"			
"	8.467	Pervious Initial abstraction"			
"	0.015	Impervious Manning 'n'"			
"	98.000	Impervious SCS Curve No."			
"	0.729	Impervious Runoff coefficient"			
"	0.100	Impervious Ia/S coefficient"			
"	0.518	Impervious Initial abstraction"			
"		0.002	0.000	0.024	0.049 c.m/sec"
"		Catchment 205	Pervious	Impervious	Total Area "
"		Surface Area	0.054	0.006	0.060 hectare"
"		Time of concentration	2.947	0.233	1.998 minutes"
"		Time to Centroid	107.105	87.928	100.402 minutes"
"		Rainfall depth	31.880	31.880	31.880 mm"
"		Rainfall volume	17.16	1.97	19.13 c.m"
"		Rainfall losses	26.915	8.650	25.034 mm"
"		Runoff depth	4.965	23.230	6.846 mm"
"		Runoff volume	2.67	1.44	4.11 c.m"
"		Runoff coefficient	0.156	0.729	0.215 "
"		Maximum flow	0.001	0.001	0.002 c.m/sec"
" 40	HYDROGRAPH	Add Runoff "			
"	4	Add Runoff "			
"		0.002	0.002	0.024	0.049"

" 40	HYDROGRAPH Copy to Outflow"				
"	8	Copy to Outflow"			
"		0.002	0.002	0.002	0.049"
" 40	HYDROGRAPH Combine 1"				
"	6	Combine "			
"	1	Node #"			
"		Total Site"			
"			0.051	c.m/sec"	
"			135.097	c.m"	
"		0.002	0.002	0.002	0.051"
" 40	HYDROGRAPH Start - New Tributary"				
"	2	Start - New Tributary"			
"		0.002	0.000	0.002	0.051"
" 33	CATCHMENT 206"				
"	1	Triangular SCS"			
"	1	Equal length"			
"	1	SCS method"			
"	206	Uncontrolled to O'Keefe"			
"	49.000	% Impervious"			
"	0.047	Total Area"			
"	6.000	Flow length"			
"	25.000	Overland Slope"			
"	0.024	Pervious Area"			
"	6.000	Pervious length"			
"	25.000	Pervious slope"			
"	0.023	Impervious Area"			
"	6.000	Impervious length"			
"	25.000	Impervious slope"			
"	0.250	Pervious Manning 'n'"			
"	75.000	Pervious SCS Curve No."			
"	0.158	Pervious Runoff coefficient"			
"	0.100	Pervious Ia/S coefficient"			
"	8.467	Pervious Initial abstraction"			
"	0.015	Impervious Manning 'n'"			
"	98.000	Impervious SCS Curve No."			
"	0.751	Impervious Runoff coefficient"			
"	0.100	Impervious Ia/S coefficient"			
"	0.518	Impervious Initial abstraction"			
"		0.005	0.000	0.002	0.051 c.m/sec"
"	Catchment 206	Pervious	Impervious	Total Area	"
"	Surface Area	0.024	0.023	0.047	hectare"
"	Time of concentration	5.119	0.405	1.252	minutes"
"	Time to Centroid	109.571	89.027	92.719	minutes"
"	Rainfall depth	31.880	31.880	31.880	mm"
"	Rainfall volume	7.64	7.34	14.98	c.m"
"	Rainfall losses	26.839	7.931	17.574	mm"
"	Runoff depth	5.041	23.949	14.306	mm"
"	Runoff volume	1.21	5.52	6.72	c.m"
"	Runoff coefficient	0.158	0.751	0.449	"
"	Maximum flow	0.001	0.005	0.005	c.m/sec"

" 40	HYDROGRAPH Add Runoff "				
"	4 Add Runoff "				
"		0.005	0.005	0.002	0.051"
" 40	HYDROGRAPH Copy to Outflow"				
"	8 Copy to Outflow"				
"		0.005	0.005	0.005	0.051"
" 40	HYDROGRAPH Combine 1"				
"	6 Combine "				
"	1 Node #"				
"	Total Site"				
"	Maximum flow		0.054	c.m/sec"	
"	Hydrograph volume		141.821	c.m"	
"		0.005	0.005	0.005	0.054"
" 38	START/RE-START TOTALS 206"				
"	3 Runoff Totals on EXIT"				
"	Total Catchment area		0.604	hectare"	
"	Total Impervious area		0.526	hectare"	
"	Total % impervious		87.121"		
" 19	EXIT"				


```

"          MIDUSS Output ----->"
"          MIDUSS version                      Version 2.25  rev. 473"
"          MIDUSS created                      Sunday, February 7, 2010"
"          10  Units used:                      ie METRIC"
"          Job folder:                        Q:\53510\100\MIDUSS\JHN"
"          Output filename:                    5 year v3.out"
"          Licensee name:                      A"
"          Company                            "
"          Date & Time last used:              6/21/2024 at 2:45:17 PM"
" 31      TIME PARAMETERS"
"          5.000  Time Step"
"          180.000 Max. Storm length"
"          1500.000 Max. Hydrograph"
" 32      STORM Chicago storm"
"          1  Chicago storm"
"          998.071 Coefficient A"
"          6.053  Constant B"
"          0.814  Exponent C"
"          0.400  Fraction R"
"          180.000 Duration"
"          1.000  Time step multiplier"
"          Maximum intensity          141.178  mm/hr"
"          Total depth                42.540  mm"
"          6  005hyd Hydrograph extension used in this file"
" 33      CATCHMENT 201"
"          1  Triangular SCS"
"          1  Equal length"
"          1  SCS method"
"          201 Building Rooftop"
"          100.000 % Impervious"
"          0.129  Total Area"
"          10.000 Flow length"
"          1.500  Overland Slope"
"          0.000  Pervious Area"
"          10.000 Pervious length"
"          1.500  Pervious slope"
"          0.129  Impervious Area"
"          10.000 Impervious length"
"          1.500  Impervious slope"
"          0.250  Pervious Manning 'n'"
"          75.000 Pervious SCS Curve No."
"          0.000  Pervious Runoff coefficient"
"          0.100  Pervious Ia/S coefficient"
"          8.467  Pervious Initial abstraction"
"          0.015  Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.855  Impervious Runoff coefficient"
"          0.100  Impervious Ia/S coefficient"
"          0.518  Impervious Initial abstraction"
"          0.041  0.000  0.000  0.000 c.m/sec"

```

	Catchment 201	Pervious	Impervious	Total Area	
	Surface Area	0.000	0.129	0.129	hectare"
	Time of concentration	11.398	1.115	1.115	minutes"
	Time to Centroid	114.963	88.504	88.504	minutes"
	Rainfall depth	42.540	42.540	42.540	mm"
	Rainfall volume	0.00	54.88	54.88	c.m"
	Rainfall losses	32.792	6.152	6.152	mm"
	Runoff depth	9.748	36.388	36.388	mm"
	Runoff volume	0.00	46.94	46.94	c.m"
	Runoff coefficient	0.000	0.855	0.855	"
	Maximum flow	0.000	0.041	0.041	c.m/sec"
40	HYDROGRAPH Add Runoff "				
	4 Add Runoff "				
	0.041	0.041	0.000	0.000"	
54	POND DESIGN"				
	0.041	Current peak flow	c.m/sec"		
	0.037	Target outflow	c.m/sec"		
	46.9	Hydrograph volume	c.m"		
	11.	Number of stages"			
	0.000	Minimum water level	metre"		
	0.150	Maximum water level	metre"		
	0.000	Starting water level	metre"		
	0	Keep Design Data: 1 = True; 0 = False"			
		Level Discharge	Volume"		
		0.000	0.000	0.000"	
		0.01500	0.00151	0.07760"	
		0.03000	0.00302	0.6208"	
		0.04500	0.00454	2.095"	
		0.06000	0.00605	4.966"	
		0.07500	0.00756	9.700"	
		0.09000	0.00907	16.762"	
		0.1050	0.01058	26.617"	
		0.1200	0.01210	39.715"	
		0.1350	0.01361	54.265"	
		0.1500	0.01512	68.815"	
	1.	ROOFTOP"			
		Roof area	Store area	Area/drain	Drain flow
		hectare	hectare	sq.metre	L/min/25mm
		0.129	0.097	250.000	37.800
					g H:1V"
					66.667"
		Using 4 roofdrains on roofstorage area of 970. square metre"			
		Peak outflow		0.009	c.m/sec"
		Maximum level		0.093	metre"
		Maximum storage		19.057	c.m"
		Centroidal lag		1.819	hours"
		0.041	0.041	0.009	0.000 c.m/sec"
40		HYDROGRAPH	Combine	1"	
	6	Combine "			
	1	Node #"			
		Total Site"			
		Maximum flow		0.009	c.m/sec"

"		Hydrograph volume	46.938	c.m"
"		0.041 0.041 0.009	0.009"	
" 40		HYDROGRAPH Start - New Tributary"		
"	2	Start - New Tributary"		
"		0.041 0.000 0.009	0.009"	
" 33		CATCHMENT 202"		
"	1	Triangular SCS"		
"	1	Equal length"		
"	1	SCS method"		
"	202	West Parking Lot 1"		
"	100.000	% Impervious"		
"	0.059	Total Area"		
"	10.000	Flow length"		
"	1.200	Overland Slope"		
"	0.000	Pervious Area"		
"	10.000	Pervious length"		
"	1.200	Pervious slope"		
"	0.059	Impervious Area"		
"	10.000	Impervious length"		
"	1.200	Impervious slope"		
"	0.250	Pervious Manning 'n'"		
"	75.000	Pervious SCS Curve No."		
"	0.000	Pervious Runoff coefficient"		
"	0.100	Pervious Ia/S coefficient"		
"	8.467	Pervious Initial abstraction"		
"	0.015	Impervious Manning 'n'"		
"	98.000	Impervious SCS Curve No."		
"	0.859	Impervious Runoff coefficient"		
"	0.100	Impervious Ia/S coefficient"		
"	0.518	Impervious Initial abstraction"		
"		0.018 0.000 0.009	0.009 c.m/sec"	
"		Catchment 202 Pervious Impervious Total Area "		
"		Surface Area 0.000 0.059 0.059	hectare"	
"		Time of concentration 12.187 1.192 1.192	minutes"	
"		Time to Centroid 115.968 88.643 88.643	minutes"	
"		Rainfall depth 42.540 42.540 42.540	mm"	
"		Rainfall volume 0.00 25.10 25.10	c.m"	
"		Rainfall losses 32.779 6.010 6.010	mm"	
"		Runoff depth 9.761 36.530 36.530	mm"	
"		Runoff volume 0.00 21.55 21.55	c.m"	
"		Runoff coefficient 0.000 0.859 0.859	"	
"		Maximum flow 0.000 0.018 0.018	c.m/sec"	
" 40		HYDROGRAPH Add Runoff "		
"	4	Add Runoff "		
"		0.018 0.018 0.009	0.009"	
" 40		HYDROGRAPH Copy to Outflow"		
"	8	Copy to Outflow"		
"		0.018 0.018 0.018	0.009"	
" 40		HYDROGRAPH Combine 1"		
"	6	Combine "		

```

"      1  Node #"
"      Total Site"
"      Maximum flow          0.026    c.m/sec"
"      Hydrograph volume     68.490    c.m"
"      0.018    0.018    0.018    0.026"
" 40    HYDROGRAPH Start - New Tributary"
"      2  Start - New Tributary"
"      0.018    0.000    0.018    0.026"
" 33    CATCHMENT 203"
"      1  Triangular SCS"
"      1  Equal length"
"      1  SCS method"
"      203  SW Parking Lot"
" 100.000  % Impervious"
"      0.069  Total Area"
"      10.000  Flow length"
"      1.200  Overland Slope"
"      0.000  Pervious Area"
"      10.000  Pervious length"
"      1.200  Pervious slope"
"      0.069  Impervious Area"
"      10.000  Impervious length"
"      1.200  Impervious slope"
"      0.250  Pervious Manning 'n'"
"      75.000  Pervious SCS Curve No."
"      0.000  Pervious Runoff coefficient"
"      0.100  Pervious Ia/S coefficient"
"      8.467  Pervious Initial abstraction"
"      0.015  Impervious Manning 'n'"
"      98.000  Impervious SCS Curve No."
"      0.859  Impervious Runoff coefficient"
"      0.100  Impervious Ia/S coefficient"
"      0.518  Impervious Initial abstraction"
"      0.022    0.000    0.018    0.026 c.m/sec"
"      Catchment 203      Pervious      Impervious      Total Area  "
"      Surface Area      0.000      0.069      0.069      hectare"
"      Time of concentration 12.187      1.192      1.192      minutes"
"      Time to Centroid    115.968      88.643      88.643      minutes"
"      Rainfall depth      42.540      42.540      42.540      mm"
"      Rainfall volume      0.00      29.35      29.35      c.m"
"      Rainfall losses      32.779      6.010      6.010      mm"
"      Runoff depth        9.761      36.530      36.530      mm"
"      Runoff volume        0.00      25.21      25.21      c.m"
"      Runoff coefficient    0.000      0.859      0.859      "
"      Maximum flow        0.000      0.022      0.022      c.m/sec"
" 40    HYDROGRAPH Add Runoff "
"      4  Add Runoff "
"      0.022    0.022    0.018    0.026"
" 54    POND DESIGN"
"      0.022  Current peak flow    c.m/sec"

```

```

"      0.037 Target outflow c.m/sec"
"      25.2 Hydrograph volume c.m"
"      7. Number of stages"
"    103.400 Minimum water level metre"
"    103.750 Maximum water level metre"
"    103.400 Starting water level metre"
"      0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge Volume"
"    103.400 0.000 0.000"
"    103.550 0.00689 1.01E-05"
"    103.600 0.00795 0.7100"
"    103.650 0.00889 4.340"
"    103.700 0.00973 13.820"
"    103.750 0.01051 30.870"
"    103.800 0.01124 54.500"
"    1. HOR. ORIFICES"
"      Orifice Orifice Orifice Number of"
"      invert coefficie diameter orifices"
"    103.400 0.630 0.0900 1.000"
"      Peak outflow 0.009 c.m/sec"
"      Maximum level 103.653 metre"
"      Maximum storage 4.991 c.m"
"      Centroidal lag 1.540 hours"
"      0.022 0.022 0.009 0.026 c.m/sec"
" 40 HYDROGRAPH Combine 1"
"    6 Combine "
"    1 Node #"
"      Total Site"
"      Maximum flow 0.034 c.m/sec"
"      Hydrograph volume 93.551 c.m"
"      0.022 0.022 0.009 0.034"
" 40 HYDROGRAPH Start - New Tributary"
"    2 Start - New Tributary"
"      0.022 0.000 0.009 0.034"
" 33 CATCHMENT 204"
"    1 Triangular SCS"
"    1 Equal length"
"    1 SCS method"
"      204 Controlled Area"
"    100.000 % Impervious"
"      0.240 Total Area"
"      20.000 Flow length"
"      1.200 Overland Slope"
"      0.000 Pervious Area"
"      20.000 Pervious length"
"      1.200 Pervious slope"
"      0.240 Impervious Area"
"      20.000 Impervious length"
"      1.200 Impervious slope"
"      0.250 Pervious Manning 'n'"

```

"	75.000	Pervious SCS Curve No."			
"	0.000	Pervious Runoff coefficient"			
"	0.100	Pervious Ia/S coefficient"			
"	8.467	Pervious Initial abstraction"			
"	0.015	Impervious Manning 'n'"			
"	98.000	Impervious SCS Curve No."			
"	0.868	Impervious Runoff coefficient"			
"	0.100	Impervious Ia/S coefficient"			
"	0.518	Impervious Initial abstraction"			
"		0.071	0.000	0.009	0.034 c.m/sec"
"		Catchment 204	Pervious	Impervious	Total Area "
"		Surface Area	0.000	0.240	0.240 hectare"
"		Time of concentration	18.473	1.807	1.807 minutes"
"		Time to Centroid	124.045	89.542	89.542 minutes"
"		Rainfall depth	42.540	42.540	42.540 mm"
"		Rainfall volume	0.00	102.10	102.10 c.m"
"		Rainfall losses	32.771	5.622	5.622 mm"
"		Runoff depth	9.769	36.918	36.918 mm"
"		Runoff volume	0.00	88.60	88.60 c.m"
"		Runoff coefficient	0.000	0.868	0.868 "
"		Maximum flow	0.000	0.071	0.071 c.m/sec"
" 40		HYDROGRAPH Add Runoff "			
"	4	Add Runoff "			
"		0.071	0.071	0.009	0.034"
" 54		POND DESIGN"			
"	0.071	Current peak flow	c.m/sec"		
"	0.037	Target outflow	c.m/sec"		
"	88.6	Hydrograph volume	c.m"		
"	7.	Number of stages"			
"	101.220	Minimum water level	metre"		
"	103.800	Maximum water level	metre"		
"	101.220	Starting water level	metre"		
"	0	Keep Design Data: 1 = True; 0 = False"			
"		Level Discharge	Volume"		
"	101.220	0.000	0.000"		
"	103.550	0.02388	12.450"		
"	103.600	0.02414	13.960"		
"	103.650	0.02439	22.230"		
"	103.700	0.02465	46.120"		
"	103.750	0.02490	94.800"		
"	103.800	0.02515	171.200"		
"	1.	ORIFICES"			
"		Orifice Orifice	Orifice Number of"		
"		invert coefficie	diameter orifices"		
"		101.220	0.630	0.0850	1.000"
"		Peak outflow	0.024	c.m/sec"	
"		Maximum level	103.666	metre"	
"		Maximum storage	30.094	c.m"	
"		Centroidal lag	1.705	hours"	
"		0.071	0.071	0.024	0.034 c.m/sec"

" 40	HYDROGRAPH	Combine	1"		
"	6	Combine "			
"	1	Node #"			
"		Total Site"			
"		Maximum flow	0.058	c.m/sec"	
"		Hydrograph volume	182.355	c.m"	
"		0.071	0.071	0.024	0.058"
" 40	HYDROGRAPH	Start - New Tributary"			
"	2	Start - New Tributary"			
"		0.071	0.000	0.024	0.058"
" 33	CATCHMENT	205"			
"	1	Triangular SCS"			
"	1	Equal length"			
"	1	SCS method"			
"	205	Uncontrolled to Lusk"			
"	10.300	% Impervious"			
"	0.060	Total Area"			
"	2.000	Flow length"			
"	17.500	Overland Slope"			
"	0.054	Pervious Area"			
"	2.000	Pervious length"			
"	17.500	Pervious slope"			
"	0.006	Impervious Area"			
"	2.000	Impervious length"			
"	17.500	Impervious slope"			
"	0.250	Pervious Manning 'n'"			
"	75.000	Pervious SCS Curve No."			
"	0.227	Pervious Runoff coefficient"			
"	0.100	Pervious Ia/S coefficient"			
"	8.467	Pervious Initial abstraction"			
"	0.015	Impervious Manning 'n'"			
"	98.000	Impervious SCS Curve No."			
"	0.757	Impervious Runoff coefficient"			
"	0.100	Impervious Ia/S coefficient"			
"	0.518	Impervious Initial abstraction"			
"		0.005	0.000	0.024	0.058 c.m/sec"
"		Catchment 205	Pervious	Impervious	Total Area "
"		Surface Area	0.054	0.006	0.060 hectare"
"		Time of concentration	2.077	0.203	1.557 minutes"
"		Time to Centroid	102.829	86.644	98.341 minutes"
"		Rainfall depth	42.540	42.540	42.540 mm"
"		Rainfall volume	22.90	2.63	25.52 c.m"
"		Rainfall losses	32.895	10.317	30.570 mm"
"		Runoff depth	9.645	32.223	11.970 mm"
"		Runoff volume	5.19	1.99	7.18 c.m"
"		Runoff coefficient	0.227	0.757	0.281 "
"		Maximum flow	0.003	0.002	0.005 c.m/sec"
" 40	HYDROGRAPH	Add Runoff "			
"	4	Add Runoff "			
"		0.005	0.005	0.024	0.058"

" 40	HYDROGRAPH Copy to Outflow"				
"	8	Copy to Outflow"			
"		0.005	0.005	0.005	0.058"
" 40	HYDROGRAPH Combine 1"				
"	6	Combine "			
"	1	Node #"			
"	Total Site"				
"			0.063	c.m/sec"	
"			189.537	c.m"	
"		0.005	0.005	0.005	0.063"
" 40	HYDROGRAPH Start - New Tributary"				
"	2	Start - New Tributary"			
"		0.005	0.000	0.005	0.063"
" 33	CATCHMENT 206"				
"	1	Triangular SCS"			
"	1	Equal length"			
"	1	SCS method"			
"	206	Uncontrolled to O'Keefe"			
"	49.000	% Impervious"			
"	0.047	Total Area"			
"	6.000	Flow length"			
"	25.000	Overland Slope"			
"	0.024	Pervious Area"			
"	6.000	Pervious length"			
"	25.000	Pervious slope"			
"	0.023	Impervious Area"			
"	6.000	Impervious length"			
"	25.000	Impervious slope"			
"	0.250	Pervious Manning 'n'"			
"	75.000	Pervious SCS Curve No."			
"	0.225	Pervious Runoff coefficient"			
"	0.100	Pervious Ia/S coefficient"			
"	8.467	Pervious Initial abstraction"			
"	0.015	Impervious Manning 'n'"			
"	98.000	Impervious SCS Curve No."			
"	0.774	Impervious Runoff coefficient"			
"	0.100	Impervious Ia/S coefficient"			
"	0.518	Impervious Initial abstraction"			
"		0.008	0.000	0.005	0.063 c.m/sec"
"	Catchment 206	Pervious	Impervious	Total Area	"
"	Surface Area	0.024	0.023	0.047	hectare"
"	Time of concentration	3.607	0.353	1.107	minutes"
"	Time to Centroid	105.245	87.761	91.815	minutes"
"	Rainfall depth	42.540	42.540	42.540	mm"
"	Rainfall volume	10.20	9.80	19.99	c.m"
"	Rainfall losses	32.985	9.598	21.526	mm"
"	Runoff depth	9.555	32.942	21.014	mm"
"	Runoff volume	2.29	7.59	9.88	c.m"
"	Runoff coefficient	0.225	0.774	0.494	"
"	Maximum flow	0.001	0.007	0.008	c.m/sec"

" 40	HYDROGRAPH Add Runoff "				
"	4 Add Runoff "				
"		0.008	0.008	0.005	0.063"
" 40	HYDROGRAPH Copy to Outflow"				
"	8 Copy to Outflow"				
"		0.008	0.008	0.008	0.063"
" 40	HYDROGRAPH Combine 1"				
"	6 Combine "				
"	1 Node #"				
"	Total Site"				
"	Maximum flow		0.071	c.m/sec"	
"	Hydrograph volume		199.413	c.m"	
"		0.008	0.008	0.008	0.071"
" 38	START/RE-START TOTALS 206"				
"	3 Runoff Totals on EXIT"				
"	Total Catchment area		0.604	hectare"	
"	Total Impervious area		0.526	hectare"	
"	Total % impervious		87.121"		
" 19	EXIT"				

```

"          MIDUSS Output ----->"
"          MIDUSS version                Version 2.25  rev. 473"
"          MIDUSS created                Sunday, February 7, 2010"
"          10  Units used:                ie METRIC"
"          Job folder:                    Q:\53510\100\MIDUSS\JHN"
"          Output filename:                100 year v3.out"
"          Licensee name:                  A"
"          Company                        "
"          Date & Time last used:          6/21/2024 at 2:40:26 PM"
" 31      TIME PARAMETERS"
"          5.000  Time Step"
"          180.000 Max. Storm length"
"          1500.000 Max. Hydrograph"
" 32      STORM Chicago storm"
"          1  Chicago storm"
"          1735.688 Coefficient A"
"          6.014  Constant B"
"          0.820  Exponent C"
"          0.400  Fraction R"
"          180.000 Duration"
"          1.000  Time step multiplier"
"          Maximum intensity                242.704  mm/hr"
"          Total depth                    71.708  mm"
"          6  100hyd  Hydrograph extension used in this file"
" 33      CATCHMENT 201"
"          1  Triangular SCS"
"          1  Equal length"
"          1  SCS method"
"          201  Building Rooftop"
"          100.000 % Impervious"
"          0.129  Total Area"
"          10.000  Flow length"
"          1.500  Overland Slope"
"          0.000  Pervious Area"
"          10.000  Pervious length"
"          1.500  Pervious slope"
"          0.129  Impervious Area"
"          10.000  Impervious length"
"          1.500  Impervious slope"
"          0.250  Pervious Manning 'n'"
"          75.000  Pervious SCS Curve No."
"          0.000  Pervious Runoff coefficient"
"          0.100  Pervious Ia/S coefficient"
"          8.467  Pervious Initial abstraction"
"          0.015  Impervious Manning 'n'"
"          98.000  Impervious SCS Curve No."
"          0.886  Impervious Runoff coefficient"
"          0.100  Impervious Ia/S coefficient"
"          0.518  Impervious Initial abstraction"
"          0.073  0.000  0.000  0.000 c.m/sec"

```

	Catchment 201	Pervious	Impervious	Total Area	
	Surface Area	0.000	0.129	0.129	hectare"
	Time of concentration	7.086	0.886	0.886	minutes"
	Time to Centroid	106.059	86.668	86.668	minutes"
	Rainfall depth	71.708	71.708	71.708	mm"
	Rainfall volume	0.00	92.50	92.50	c.m"
	Rainfall losses	44.867	8.171	8.171	mm"
	Runoff depth	26.841	63.536	63.536	mm"
	Runoff volume	0.00	81.96	81.96	c.m"
	Runoff coefficient	0.000	0.886	0.886	"
	Maximum flow	0.000	0.073	0.073	c.m/sec"
40	HYDROGRAPH Add Runoff "				
	4 Add Runoff "				
	0.073	0.073	0.000	0.000"	
54	POND DESIGN"				
	0.073	Current peak flow	c.m/sec"		
	0.037	Target outflow	c.m/sec"		
	82.0	Hydrograph volume	c.m"		
	11.	Number of stages"			
	0.000	Minimum water level	metre"		
	0.150	Maximum water level	metre"		
	0.000	Starting water level	metre"		
	0	Keep Design Data: 1 = True; 0 = False"			
		Level Discharge	Volume"		
		0.000	0.000	0.000"	
		0.01500	0.00151	0.07760"	
		0.03000	0.00302	0.6208"	
		0.04500	0.00454	2.095"	
		0.06000	0.00605	4.966"	
		0.07500	0.00756	9.700"	
		0.09000	0.00907	16.762"	
		0.1050	0.01058	26.617"	
		0.1200	0.01210	39.715"	
		0.1350	0.01361	54.265"	
		0.1500	0.01512	68.815"	
	1.	ROOFTOP"			
		Roof area	Store area	Area/drain	Drain flow
		hectare	hectare	sq.metre	L/min/25mm
		0.129	0.097	250.000	37.800
					g H:1V"
					66.667"
		Using 4 roofdrains on roofstorage area of 970. square metre"			
		Peak outflow		0.012	c.m/sec"
		Maximum level		0.119	metre"
		Maximum storage		39.059	c.m"
		Centroidal lag		2.028	hours"
		0.073	0.073	0.012	0.000 c.m/sec"
40		HYDROGRAPH	Combine	1"	
	6	Combine "			
	1	Node #"			
		Total Site"			
		Maximum flow		0.012	c.m/sec"

"		Hydrograph volume	81.883	c.m"
"		0.073 0.073 0.012	0.012"	
" 40		HYDROGRAPH Start - New Tributary"		
"	2	Start - New Tributary"		
"		0.073 0.000 0.012	0.012"	
" 33		CATCHMENT 202"		
"	1	Triangular SCS"		
"	1	Equal length"		
"	1	SCS method"		
"	202	West Parking Lot 1"		
"	100.000	% Impervious"		
"	0.059	Total Area"		
"	10.000	Flow length"		
"	1.200	Overland Slope"		
"	0.000	Pervious Area"		
"	10.000	Pervious length"		
"	1.200	Pervious slope"		
"	0.059	Impervious Area"		
"	10.000	Impervious length"		
"	1.200	Impervious slope"		
"	0.250	Pervious Manning 'n'"		
"	75.000	Pervious SCS Curve No."		
"	0.000	Pervious Runoff coefficient"		
"	0.100	Pervious Ia/S coefficient"		
"	8.467	Pervious Initial abstraction"		
"	0.015	Impervious Manning 'n'"		
"	98.000	Impervious SCS Curve No."		
"	0.891	Impervious Runoff coefficient"		
"	0.100	Impervious Ia/S coefficient"		
"	0.518	Impervious Initial abstraction"		
"		0.033 0.000 0.012	0.012 c.m/sec"	
"		Catchment 202 Pervious Impervious Total Area "		
"		Surface Area 0.000 0.059 0.059	hectare"	
"		Time of concentration 7.577 0.947 0.947	minutes"	
"		Time to Centroid 106.707 86.768 86.768	minutes"	
"		Rainfall depth 71.708 71.708 71.708	mm"	
"		Rainfall volume 0.00 42.31 42.31	c.m"	
"		Rainfall losses 44.799 7.852 7.852	mm"	
"		Runoff depth 26.909 63.856 63.856	mm"	
"		Runoff volume 0.00 37.67 37.67	c.m"	
"		Runoff coefficient 0.000 0.891 0.891	"	
"		Maximum flow 0.000 0.033 0.033	c.m/sec"	
" 40		HYDROGRAPH Add Runoff "		
"	4	Add Runoff "		
"		0.033 0.033 0.012	0.012"	
" 40		HYDROGRAPH Copy to Outflow"		
"	8	Copy to Outflow"		
"		0.033 0.033 0.033	0.012"	
" 40		HYDROGRAPH Combine 1"		
"	6	Combine "		

"	1	Node #"			
"		Total Site"			
"		Maximum flow	0.043	c.m/sec"	
"		Hydrograph volume	119.558	c.m"	
"		0.033	0.033	0.033	0.043"
" 40		HYDROGRAPH Start - New Tributary"			
"	2	Start - New Tributary"			
"		0.033	0.000	0.033	0.043"
" 33		CATCHMENT 203"			
"	1	Triangular SCS"			
"	1	Equal length"			
"	1	SCS method"			
"	203	SW Parking Lot"			
"	100.000	% Impervious"			
"	0.069	Total Area"			
"	10.000	Flow length"			
"	1.200	Overland Slope"			
"	0.000	Pervious Area"			
"	10.000	Pervious length"			
"	1.200	Pervious slope"			
"	0.069	Impervious Area"			
"	10.000	Impervious length"			
"	1.200	Impervious slope"			
"	0.250	Pervious Manning 'n'"			
"	75.000	Pervious SCS Curve No."			
"	0.000	Pervious Runoff coefficient"			
"	0.100	Pervious Ia/S coefficient"			
"	8.467	Pervious Initial abstraction"			
"	0.015	Impervious Manning 'n'"			
"	98.000	Impervious SCS Curve No."			
"	0.891	Impervious Runoff coefficient"			
"	0.100	Impervious Ia/S coefficient"			
"	0.518	Impervious Initial abstraction"			
"		0.039	0.000	0.033	0.043 c.m/sec"
"		Catchment 203	Pervious	Impervious	Total Area "
"		Surface Area	0.000	0.069	0.069 hectare"
"		Time of concentration	7.577	0.947	0.947 minutes"
"		Time to Centroid	106.707	86.768	86.768 minutes"
"		Rainfall depth	71.708	71.708	71.708 mm"
"		Rainfall volume	0.00	49.48	49.48 c.m"
"		Rainfall losses	44.799	7.852	7.852 mm"
"		Runoff depth	26.909	63.856	63.856 mm"
"		Runoff volume	0.00	44.06	44.06 c.m"
"		Runoff coefficient	0.000	0.891	0.891 "
"		Maximum flow	0.000	0.039	0.039 c.m/sec"
" 40		HYDROGRAPH Add Runoff "			
"	4	Add Runoff "			
"		0.039	0.039	0.033	0.043"
" 54		POND DESIGN"			
"	0.039	Current peak flow	c.m/sec"		

```

"      0.037 Target outflow c.m/sec"
"      44.1 Hydrograph volume c.m"
"      7. Number of stages"
"    103.400 Minimum water level metre"
"    103.750 Maximum water level metre"
"    103.400 Starting water level metre"
"      0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge Volume"
"    103.400 0.000 0.000"
"    103.550 0.00689 1.01E-05"
"    103.600 0.00795 0.7100"
"    103.650 0.00889 4.340"
"    103.700 0.00973 13.820"
"    103.750 0.01051 30.870"
"    103.800 0.01124 54.500"
"    1. HOR. ORIFICES"
"      Orifice Orifice Orifice Number of"
"      invert coefficie diameter orifices"
"    103.400 0.630 0.0900 1.000"
"      Peak outflow 0.010 c.m/sec"
"      Maximum level 103.701 metre"
"      Maximum storage 14.142 c.m"
"      Centroidal lag 1.645 hours"
"      0.039 0.039 0.010 0.043 c.m/sec"
" 40 HYDROGRAPH Combine 1"
"    6 Combine "
"    1 Node #"
"      Total Site"
"      Maximum flow 0.052 c.m/sec"
"      Hydrograph volume 164.090 c.m"
"      0.039 0.039 0.010 0.052"
" 40 HYDROGRAPH Start - New Tributary"
"    2 Start - New Tributary"
"      0.039 0.000 0.010 0.052"
" 33 CATCHMENT 204"
"    1 Triangular SCS"
"    1 Equal length"
"    1 SCS method"
"      204 Controlled Area"
"    100.000 % Impervious"
"      0.240 Total Area"
"      20.000 Flow length"
"      1.200 Overland Slope"
"      0.000 Pervious Area"
"      20.000 Pervious length"
"      1.200 Pervious slope"
"      0.240 Impervious Area"
"      20.000 Impervious length"
"      1.200 Impervious slope"
"      0.250 Pervious Manning 'n'"

```

"	75.000	Pervious SCS Curve No."			
"	0.000	Pervious Runoff coefficient"			
"	0.100	Pervious Ia/S coefficient"			
"	8.467	Pervious Initial abstraction"			
"	0.015	Impervious Manning 'n'"			
"	98.000	Impervious SCS Curve No."			
"	0.910	Impervious Runoff coefficient"			
"	0.100	Impervious Ia/S coefficient"			
"	0.518	Impervious Initial abstraction"			
"		0.131	0.000	0.010	0.052 c.m/sec"
"		Catchment 204	Pervious	Impervious	Total Area "
"		Surface Area	0.000	0.240	0.240 hectare"
"		Time of concentration	11.484	1.436	1.436 minutes"
"		Time to Centroid	111.952	87.537	87.537 minutes"
"		Rainfall depth	71.708	71.708	71.708 mm"
"		Rainfall volume	0.00	172.10	172.10 c.m"
"		Rainfall losses	44.682	6.464	6.464 mm"
"		Runoff depth	27.026	65.244	65.244 mm"
"		Runoff volume	0.00	156.59	156.59 c.m"
"		Runoff coefficient	0.000	0.910	0.910 "
"		Maximum flow	0.000	0.131	0.131 c.m/sec"
" 40		HYDROGRAPH Add Runoff "			
"	4	Add Runoff "			
"		0.131	0.131	0.010	0.052"
" 54		POND DESIGN"			
"	0.131	Current peak flow	c.m/sec"		
"	0.037	Target outflow	c.m/sec"		
"	156.6	Hydrograph volume	c.m"		
"	7.	Number of stages"			
"	101.220	Minimum water level	metre"		
"	103.800	Maximum water level	metre"		
"	101.220	Starting water level	metre"		
"	0	Keep Design Data: 1 = True; 0 = False"			
"		Level Discharge	Volume"		
"	101.220	0.000	0.000"		
"	103.550	0.02388	12.450"		
"	103.600	0.02414	13.960"		
"	103.650	0.02439	22.230"		
"	103.700	0.02465	46.120"		
"	103.750	0.02490	94.800"		
"	103.800	0.02515	171.200"		
"	1.	ORIFICES"			
"		Orifice Orifice	Orifice Number of"		
"		invert coefficie	diameter orifices"		
"		101.220	0.630	0.0850	1.000"
"		Peak outflow	0.025	c.m/sec"	
"		Maximum level	103.724	metre"	
"		Maximum storage	69.850	c.m"	
"		Centroidal lag	1.900	hours"	
"		0.131	0.131	0.025	0.052 c.m/sec"

" 40	HYDROGRAPH	Combine	1"		
"	6	Combine "			
"	1	Node #"			
"		Total Site"			
"		Maximum flow	0.076	c.m/sec"	
"		Hydrograph volume	320.510	c.m"	
"		0.131	0.131	0.025	0.076"
" 40	HYDROGRAPH	Start - New Tributary"			
"	2	Start - New Tributary"			
"		0.131	0.000	0.025	0.076"
" 33	CATCHMENT	205"			
"	1	Triangular SCS"			
"	1	Equal length"			
"	1	SCS method"			
"	205	Uncontrolled to Lusk"			
"	10.300	% Impervious"			
"	0.060	Total Area"			
"	2.000	Flow length"			
"	17.500	Overland Slope"			
"	0.054	Pervious Area"			
"	2.000	Pervious length"			
"	17.500	Pervious slope"			
"	0.006	Impervious Area"			
"	2.000	Impervious length"			
"	17.500	Impervious slope"			
"	0.250	Pervious Manning 'n'"			
"	75.000	Pervious SCS Curve No."			
"	0.369	Pervious Runoff coefficient"			
"	0.100	Pervious Ia/S coefficient"			
"	8.467	Pervious Initial abstraction"			
"	0.015	Impervious Manning 'n'"			
"	98.000	Impervious SCS Curve No."			
"	0.796	Impervious Runoff coefficient"			
"	0.100	Impervious Ia/S coefficient"			
"	0.518	Impervious Initial abstraction"			
"		0.014	0.000	0.025	0.076 c.m/sec"
"		Catchment 205	Pervious	Impervious	Total Area "
"		Surface Area	0.054	0.006	0.060 hectare"
"		Time of concentration	1.291	0.161	1.067 minutes"
"		Time to Centroid	97.800	84.840	95.225 minutes"
"		Rainfall depth	71.708	71.708	71.708 mm"
"		Rainfall volume	38.59	4.43	43.02 c.m"
"		Rainfall losses	45.258	14.609	42.101 mm"
"		Runoff depth	26.450	57.098	29.606 mm"
"		Runoff volume	14.24	3.53	17.76 c.m"
"		Runoff coefficient	0.369	0.796	0.413 "
"		Maximum flow	0.011	0.004	0.014 c.m/sec"
" 40	HYDROGRAPH	Add Runoff "			
"	4	Add Runoff "			
"		0.014	0.014	0.025	0.076"

" 40	HYDROGRAPH Copy to Outflow"				
"	8	Copy to Outflow"			
"		0.014	0.014	0.014	0.076"
" 40	HYDROGRAPH Combine 1"				
"	6	Combine "			
"	1	Node #"			
"	Total Site"				
"			0.090	c.m/sec"	
"			338.274	c.m"	
"		0.014	0.014	0.014	0.090"
" 40	HYDROGRAPH Start - New Tributary"				
"	2	Start - New Tributary"			
"		0.014	0.000	0.014	0.090"
" 33	CATCHMENT 206"				
"	1	Triangular SCS"			
"	1	Equal length"			
"	1	SCS method"			
"	206	Uncontrolled to O'Keefe"			
"	49.000	% Impervious"			
"	0.047	Total Area"			
"	6.000	Flow length"			
"	25.000	Overland Slope"			
"	0.024	Pervious Area"			
"	6.000	Pervious length"			
"	25.000	Pervious slope"			
"	0.023	Impervious Area"			
"	6.000	Impervious length"			
"	25.000	Impervious slope"			
"	0.250	Pervious Manning 'n'"			
"	75.000	Pervious SCS Curve No."			
"	0.372	Pervious Runoff coefficient"			
"	0.100	Pervious Ia/S coefficient"			
"	8.467	Pervious Initial abstraction"			
"	0.015	Impervious Manning 'n'"			
"	98.000	Impervious SCS Curve No."			
"	0.806	Impervious Runoff coefficient"			
"	0.100	Impervious Ia/S coefficient"			
"	0.518	Impervious Initial abstraction"			
"		0.017	0.000	0.014	0.090 c.m/sec"
"	Catchment 206	Pervious	Impervious	Total Area	"
"	Surface Area	0.024	0.023	0.047	hectare"
"	Time of concentration	2.243	0.280	0.917	minutes"
"	Time to Centroid	99.241	85.825	90.178	minutes"
"	Rainfall depth	71.708	71.708	71.708	mm"
"	Rainfall volume	17.19	16.51	33.70	c.m"
"	Rainfall losses	45.035	13.919	29.789	mm"
"	Runoff depth	26.672	57.788	41.919	mm"
"	Runoff volume	6.39	13.31	19.70	c.m"
"	Runoff coefficient	0.372	0.806	0.585	"
"	Maximum flow	0.004	0.013	0.017	c.m/sec"

" 40	HYDROGRAPH Add Runoff "				
"	4 Add Runoff "				
"		0.017	0.017	0.014	0.090"
" 40	HYDROGRAPH Copy to Outflow"				
"	8 Copy to Outflow"				
"		0.017	0.017	0.017	0.090"
" 40	HYDROGRAPH Combine 1"				
"	6 Combine "				
"	1 Node #"				
"	Total Site"				
"	Maximum flow		0.107	c.m/sec"	
"	Hydrograph volume		357.976	c.m"	
"		0.017	0.017	0.017	0.107"
" 38	START/RE-START TOTALS 206"				
"	3 Runoff Totals on EXIT"				
"	Total Catchment area		0.604	hectare"	
"	Total Impervious area		0.526	hectare"	
"	Total % impervious		87.121"		
" 19	EXIT"				

```

"          MIDUSS Output ----->"
"          MIDUSS version                      Version 2.25  rev. 473"
"          MIDUSS created                      Sunday, February 7, 2010"
"          10  Units used:                      ie METRIC"
"          Job folder:                        Q:\53510\100\MIDUSS\JHN"
"          Output filename:                    100 year + 20%  v3.out"
"          Licensee name:                      A"
"          Company                            "
"          Date & Time last used:              6/21/2024 at 2:46:37 PM"
" 31      TIME PARAMETERS"
"          5.000  Time Step"
"          180.000 Max. Storm length"
"          1500.000 Max. Hydrograph"
" 32      STORM Chicago storm"
"          1  Chicago storm"
"          2082.820 Coefficient A"
"          5.890  Constant B"
"          0.824  Exponent C"
"          0.400  Fraction R"
"          180.000 Duration"
"          1.000  Time step multiplier"
"          Maximum intensity                291.166  mm/hr"
"          Total depth                      84.315  mm"
"          6  120hyd  Hydrograph extension used in this file"
" 33      CATCHMENT 201"
"          1  Triangular SCS"
"          1  Equal length"
"          1  SCS method"
"          201  Building Rooftop"
"          100.000 % Impervious"
"          0.129  Total Area"
"          10.000  Flow length"
"          1.500  Overland Slope"
"          0.000  Pervious Area"
"          10.000  Pervious length"
"          1.500  Pervious slope"
"          0.129  Impervious Area"
"          10.000  Impervious length"
"          1.500  Impervious slope"
"          0.250  Pervious Manning 'n'"
"          75.000  Pervious SCS Curve No."
"          0.000  Pervious Runoff coefficient"
"          0.100  Pervious Ia/S coefficient"
"          8.467  Pervious Initial abstraction"
"          0.015  Impervious Manning 'n'"
"          98.000  Impervious SCS Curve No."
"          0.891  Impervious Runoff coefficient"
"          0.100  Impervious Ia/S coefficient"
"          0.518  Impervious Initial abstraction"
"          0.088  0.000  0.000  0.000 c.m/sec"

```

	Catchment 201	Pervious	Impervious	Total Area	
	Surface Area	0.000	0.129	0.129	hectare"
	Time of concentration	6.211	0.822	0.822	minutes"
	Time to Centroid	103.769	86.143	86.143	minutes"
	Rainfall depth	84.315	84.315	84.315	mm"
	Rainfall volume	0.00	108.77	108.77	c.m"
	Rainfall losses	48.746	9.212	9.212	mm"
	Runoff depth	35.569	75.103	75.103	mm"
	Runoff volume	0.00	96.88	96.88	c.m"
	Runoff coefficient	0.000	0.891	0.891	"
	Maximum flow	0.000	0.088	0.088	c.m/sec"
40	HYDROGRAPH Add Runoff "				
	4 Add Runoff "				
	0.088	0.088	0.000	0.000"	
54	POND DESIGN"				
	0.088	Current peak flow	c.m/sec"		
	0.037	Target outflow	c.m/sec"		
	96.9	Hydrograph volume	c.m"		
	11.	Number of stages"			
	0.000	Minimum water level	metre"		
	0.150	Maximum water level	metre"		
	0.000	Starting water level	metre"		
	0	Keep Design Data: 1 = True; 0 = False"			
		Level Discharge	Volume"		
		0.000	0.000	0.000"	
		0.01500	0.00151	0.07760"	
		0.03000	0.00302	0.6208"	
		0.04500	0.00454	2.095"	
		0.06000	0.00605	4.966"	
		0.07500	0.00756	9.700"	
		0.09000	0.00907	16.762"	
		0.1050	0.01058	26.617"	
		0.1200	0.01210	39.715"	
		0.1350	0.01361	54.265"	
		0.1500	0.01512	68.815"	
	1.	ROOFTOP"			
		Roof area	Store area	Area/drain	Drain flow
		hectare	hectare	sq.metre	L/min/25mm
		0.129	0.097	250.000	37.800
		Using 4 roofdrains on roofstorage area of 970. square metre"			
		Peak outflow	0.013	c.m/sec"	
		Maximum level	0.129	metre"	
		Maximum storage	48.317	c.m"	
		Centroidal lag	2.114	hours"	
		0.088	0.088	0.013	0.000 c.m/sec"
40		HYDROGRAPH	Combine	1"	
	6	Combine "			
	1	Node #"			
		Total Site"			
		Maximum flow	0.013	c.m/sec"	

"		Hydrograph volume	96.990	c.m"
"		0.088 0.088 0.013	0.013"	
" 40		HYDROGRAPH Start - New Tributary"		
"	2	Start - New Tributary"		
"		0.088 0.000 0.013	0.013"	
" 33		CATCHMENT 202"		
"	1	Triangular SCS"		
"	1	Equal length"		
"	1	SCS method"		
"	202	West Parking Lot 1"		
"	100.000	% Impervious"		
"	0.059	Total Area"		
"	10.000	Flow length"		
"	1.200	Overland Slope"		
"	0.000	Pervious Area"		
"	10.000	Pervious length"		
"	1.200	Pervious slope"		
"	0.059	Impervious Area"		
"	10.000	Impervious length"		
"	1.200	Impervious slope"		
"	0.250	Pervious Manning 'n'"		
"	75.000	Pervious SCS Curve No."		
"	0.000	Pervious Runoff coefficient"		
"	0.100	Pervious Ia/S coefficient"		
"	8.467	Pervious Initial abstraction"		
"	0.015	Impervious Manning 'n'"		
"	98.000	Impervious SCS Curve No."		
"	0.895	Impervious Runoff coefficient"		
"	0.100	Impervious Ia/S coefficient"		
"	0.518	Impervious Initial abstraction"		
"		0.040 0.000 0.013	0.013 c.m/sec"	
"		Catchment 202 Pervious Impervious Total Area "		
"		Surface Area 0.000 0.059 0.059	hectare"	
"		Time of concentration 6.641 0.879 0.879	minutes"	
"		Time to Centroid 104.399 86.209 86.209	minutes"	
"		Rainfall depth 84.315 84.315 84.315	mm"	
"		Rainfall volume 0.00 49.75 49.75	c.m"	
"		Rainfall losses 48.839 8.819 8.819	mm"	
"		Runoff depth 35.476 75.496 75.496	mm"	
"		Runoff volume 0.00 44.54 44.54	c.m"	
"		Runoff coefficient 0.000 0.895 0.895	"	
"		Maximum flow 0.000 0.040 0.040	c.m/sec"	
" 40		HYDROGRAPH Add Runoff "		
"	4	Add Runoff "		
"		0.040 0.040 0.013	0.013"	
" 40		HYDROGRAPH Copy to Outflow"		
"	8	Copy to Outflow"		
"		0.040 0.040 0.040	0.013"	
" 40		HYDROGRAPH Combine 1"		
"	6	Combine "		

```

"      1 Node #"
"      Total Site"
"      Maximum flow      0.050 c.m/sec"
"      Hydrograph volume 141.532 c.m"
"      0.040 0.040 0.040 0.050"
" 40 HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      0.040 0.000 0.040 0.050"
" 33 CATCHMENT 203"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      203 SW Parking Lot"
" 100.000 % Impervious"
"      0.069 Total Area"
"      10.000 Flow length"
"      1.200 Overland Slope"
"      0.000 Pervious Area"
"      10.000 Pervious length"
"      1.200 Pervious slope"
"      0.069 Impervious Area"
"      10.000 Impervious length"
"      1.200 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      75.000 Pervious SCS Curve No."
"      0.000 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      8.467 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.895 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.047 0.000 0.040 0.050 c.m/sec"
"      Catchment 203 Pervious Impervious Total Area "
"      Surface Area 0.000 0.069 0.069 hectare"
"      Time of concentration 6.641 0.879 0.879 minutes"
"      Time to Centroid 104.399 86.209 86.209 minutes"
"      Rainfall depth 84.315 84.315 84.315 mm"
"      Rainfall volume 0.00 58.18 58.18 c.m"
"      Rainfall losses 48.840 8.819 8.819 mm"
"      Runoff depth 35.476 75.496 75.496 mm"
"      Runoff volume 0.00 52.09 52.09 c.m"
"      Runoff coefficient 0.000 0.895 0.895 "
"      Maximum flow 0.000 0.047 0.047 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.047 0.047 0.040 0.050"
" 54 POND DESIGN"
"      0.047 Current peak flow c.m/sec"

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"      0.037 Target outflow c.m/sec"
"      52.1 Hydrograph volume c.m"
"      7. Number of stages"
" 103.400 Minimum water level metre"
" 103.750 Maximum water level metre"
" 103.400 Starting water level metre"
"      0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge Volume"
"      103.400 0.000 0.000"
"      103.550 0.00689 1.01E-05"
"      103.600 0.00795 0.7100"
"      103.650 0.00889 4.340"
"      103.700 0.00973 13.820"
"      103.750 0.01051 30.870"
"      103.800 0.01124 54.500"
" 1. HOR. ORIFICES"
"      Orifice Orifice Orifice Number of"
"      invert coefficie diameter orifices"
"      103.400 0.630 0.0900 1.000"
"      Peak outflow 0.010 c.m/sec"
"      Maximum level 103.714 metre"
"      Maximum storage 18.622 c.m"
"      Centroidal lag 1.693 hours"
"      0.047 0.047 0.010 0.050 c.m/sec"
" 40 HYDROGRAPH Combine 1"
" 6 Combine "
" 1 Node #"
"      Total Site"
"      Maximum flow 0.060 c.m/sec"
"      Hydrograph volume 193.519 c.m"
"      0.047 0.047 0.010 0.060"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
"      0.047 0.000 0.010 0.060"
" 33 CATCHMENT 204"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      204 Controlled Area"
" 100.000 % Impervious"
"      0.240 Total Area"
"      20.000 Flow length"
"      1.200 Overland Slope"
"      0.000 Pervious Area"
"      20.000 Pervious length"
"      1.200 Pervious slope"
"      0.240 Impervious Area"
"      20.000 Impervious length"
"      1.200 Impervious slope"
"      0.250 Pervious Manning 'n'"

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"      75.000  Pervious SCS Curve No."
"      0.000  Pervious Runoff coefficient"
"      0.100  Pervious Ia/S coefficient"
"      8.467  Pervious Initial abstraction"
"      0.015  Impervious Manning 'n'"
"    98.000  Impervious SCS Curve No."
"      0.918  Impervious Runoff coefficient"
"      0.100  Impervious Ia/S coefficient"
"      0.518  Impervious Initial abstraction"
"          0.159      0.000      0.010      0.060 c.m/sec"
"      Catchment 204      Pervious      Impervious Total Area "
"      Surface Area      0.000      0.240      0.240      hectare"
"      Time of concentration 10.066      1.332      1.332      minutes"
"      Time to Centroid 109.081      86.965      86.965      minutes"
"      Rainfall depth      84.315      84.315      84.315      mm"
"      Rainfall volume      0.00      202.36      202.36      c.m"
"      Rainfall losses      48.746      6.899      6.899      mm"
"      Runoff depth      35.570      77.416      77.416      mm"
"      Runoff volume      0.00      185.80      185.80      c.m"
"      Runoff coefficient      0.000      0.918      0.918      "
"      Maximum flow      0.000      0.159      0.159      c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"      4      Add Runoff "
"          0.159      0.159      0.010      0.060"
" 54      POND DESIGN"
"      0.159      Current peak flow      c.m/sec"
"      0.037      Target outflow      c.m/sec"
"      185.8      Hydrograph volume      c.m"
"      7.      Number of stages"
"    101.220      Minimum water level      metre"
"    103.800      Maximum water level      metre"
"    101.220      Starting water level      metre"
"      0      Keep Design Data: 1 = True; 0 = False"
"          Level Discharge      Volume"
"    101.220      0.000      0.000"
"    103.550      0.02388      12.450"
"    103.600      0.02414      13.960"
"    103.650      0.02439      22.230"
"    103.700      0.02465      46.120"
"    103.750      0.02490      94.800"
"    103.800      0.02515      171.200"
"      1.      ORIFICES"
"          Orifice Orifice Orifice Number of"
"          invert coefficie diameter orifices"
"    101.220      0.630      0.0850      1.000"
"      Peak outflow      0.025      c.m/sec"
"      Maximum level      103.744      metre"
"      Maximum storage      89.077      c.m"
"      Centroidal lag      2.009      hours"
"          0.159      0.159      0.025      0.060 c.m/sec"

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" 40	HYDROGRAPH	Combine	1"		
"	6	Combine "			
"	1	Node #"			
"		Total Site"			
"		Maximum flow	0.084	c.m/sec"	
"		Hydrograph volume	379.431	c.m"	
"		0.159	0.159	0.025	0.084"
" 40	HYDROGRAPH	Start - New Tributary"			
"	2	Start - New Tributary"			
"		0.159	0.000	0.025	0.084"
" 33	CATCHMENT	205"			
"	1	Triangular SCS"			
"	1	Equal length"			
"	1	SCS method"			
"	205	Uncontrolled to Lusk"			
"	10.300	% Impervious"			
"	0.060	Total Area"			
"	2.000	Flow length"			
"	17.500	Overland Slope"			
"	0.054	Pervious Area"			
"	2.000	Pervious length"			
"	17.500	Pervious slope"			
"	0.006	Impervious Area"			
"	2.000	Impervious length"			
"	17.500	Impervious slope"			
"	0.250	Pervious Manning 'n'"			
"	75.000	Pervious SCS Curve No."			
"	0.413	Pervious Runoff coefficient"			
"	0.100	Pervious Ia/S coefficient"			
"	8.467	Pervious Initial abstraction"			
"	0.015	Impervious Manning 'n'"			
"	98.000	Impervious SCS Curve No."			
"	0.806	Impervious Runoff coefficient"			
"	0.100	Impervious Ia/S coefficient"			
"	0.518	Impervious Initial abstraction"			
"		0.019	0.000	0.025	0.084 c.m/sec"
"		Catchment 205	Pervious	Impervious	Total Area "
"		Surface Area	0.054	0.006	0.060 hectare"
"		Time of concentration	1.132	0.150	0.952 minutes"
"		Time to Centroid	96.382	84.305	94.171 minutes"
"		Rainfall depth	84.315	84.315	84.315 mm"
"		Rainfall volume	45.38	5.21	50.59 c.m"
"		Rainfall losses	49.494	16.361	46.082 mm"
"		Runoff depth	34.821	67.954	38.234 mm"
"		Runoff volume	18.74	4.20	22.94 c.m"
"		Runoff coefficient	0.413	0.806	0.453 "
"		Maximum flow	0.015	0.004	0.019 c.m/sec"
" 40	HYDROGRAPH	Add Runoff "			
"	4	Add Runoff "			
"		0.019	0.019	0.025	0.084"

```

" 40      HYDROGRAPH Copy to Outflow"
"      8  Copy to Outflow"
"          0.019      0.019      0.019      0.084"
" 40      HYDROGRAPH  Combine      1"
"      6  Combine "
"      1  Node #"
"          Total Site"
"          Maximum flow          0.103      c.m/sec"
"          Hydrograph volume      402.371      c.m"
"          0.019      0.019      0.019      0.103"
" 40      HYDROGRAPH Start - New Tributary"
"      2  Start - New Tributary"
"          0.019      0.000      0.019      0.103"
" 33      CATCHMENT 206"
"      1  Triangular SCS"
"      1  Equal length"
"      1  SCS method"
"      206  Uncontrolled to O'Keefe"
"      49.000  % Impervious"
"      0.047  Total Area"
"      6.000  Flow length"
"      25.000  Overland Slope"
"      0.024  Pervious Area"
"      6.000  Pervious length"
"      25.000  Pervious slope"
"      0.023  Impervious Area"
"      6.000  Impervious length"
"      25.000  Impervious slope"
"      0.250  Pervious Manning 'n'"
"      75.000  Pervious SCS Curve No."
"      0.419  Pervious Runoff coefficient"
"      0.100  Pervious Ia/S coefficient"
"      8.467  Pervious Initial abstraction"
"      0.015  Impervious Manning 'n'"
"      98.000  Impervious SCS Curve No."
"      0.813  Impervious Runoff coefficient"
"      0.100  Impervious Ia/S coefficient"
"      0.518  Impervious Initial abstraction"
"          0.022      0.000      0.019      0.103 c.m/sec"
"      Catchment 206      Pervious      Impervious Total Area "
"      Surface Area      0.024      0.023      0.047      hectare"
"      Time of concentration 1.966      0.260      0.855      minutes"
"      Time to Centroid      97.607      85.226      89.547      minutes"
"      Rainfall depth      84.315      84.315      84.315      mm"
"      Rainfall volume      20.21      19.42      39.63      c.m"
"      Rainfall losses      49.001      15.753      32.709      mm"
"      Runoff depth      35.314      68.563      51.606      mm"
"      Runoff volume      8.46      15.79      24.25      c.m"
"      Runoff coefficient      0.419      0.813      0.612      "
"      Maximum flow      0.006      0.016      0.022      c.m/sec"

```

" 40	HYDROGRAPH Add Runoff "				
"	4 Add Runoff "				
"		0.022	0.022	0.019	0.103"
" 40	HYDROGRAPH Copy to Outflow"				
"	8 Copy to Outflow"				
"		0.022	0.022	0.022	0.103"
" 40	HYDROGRAPH Combine 1"				
"	6 Combine "				
"	1 Node #"				
"	Total Site"				
"	Maximum flow		0.125	c.m/sec"	
"	Hydrograph volume		426.626	c.m"	
"		0.022	0.022	0.022	0.125"
" 38	START/RE-START TOTALS 206"				
"	3 Runoff Totals on EXIT"				
"	Total Catchment area		0.604	hectare"	
"	Total Impervious area		0.526	hectare"	
"	Total % impervious		87.121"		
" 19	EXIT"				