# SERVICING & STORMWATER MANAGEMENT REPORT RESIDENTIAL BUILDING – 214 SOMERSET STREET



Project No.: CCO-24-0450

City File No.: D07-12-25-0002

Prepared for:

CSV Architects 190 O'Connor Street, Suite 100 Ottawa, ON K2P 2R3

Prepared by:

Egis Canada 750 Palladium Drive – Suite 310 Kanata, ON

August 21, 2025

## TABLE OF CONTENTS

1.0	PROJECT DESCRIPTION	1
1.1	Purpose	1
1.2	Site Description	1
2.0	BACKROUND STUDIES	2
3.0	PRE-CONSULTATION SUMMARY	2
4.0	WATERMAIN	3
4.1	Existing Watermain	3
4.2	Proposed Watermain	3
5.0	SANITARY DESIGN	4
5.1	Existing Sanitary Sewer	4
5.2	Proposed Sanitary Sewer	4
6.0	STORM SEWER DESIGN	5
6.1	Existing Storm Sewers	5
6.2	Proposed Storm Sewers	5
7.0	PROPOSED STORMWATER MANAGEMENT	6
7.1	Design Criteria and Methodology	6
7.2	Runoff Calculations	7
7.3	Pre-Development Drainage	7
7.4	Post-Development Drainage	8
7.5	Quantity Control	8
7.6	Quality Control	10
8.0	EROSION AND SEDIMENT CONTROL	10
8.1	Temporary Measures	10
8.2	Permanent Measures	11
9.0	SUMMARY	11
10.0	RECOMMENDATION	12
11.0	STATEMENT OF LIMITATIONS	13

## LIST OF TABLES

Table 1: Water Demands	3
Table 2: Water Pressure at Junctions per Scenario	
Table 3: Fire Protection Confirmation	
Table 4: Pre-Development Runoff Summary	
Table 5: Post-Development Runoff Summary	
Table 6: Pre-Development Runoff Summary	
Table 7: Post-Development Restricted Runoff Summary	
Table 8: Storage Summary	
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## **APPENDICES**

Appendix A: Site Location Plan

Appendix B: Background Documents

Appendix C: Watermain Calculations

Appendix D: Sanitary Calculations

Appendix E: Pre-Development Drainage Plan

Appendix F: Post-Development Drainage Plan

Appendix G: Stormwater Management Calculations

Appendix H: City of Ottawa Design Checklist

#### 1.0 PROJECT DESCRIPTION

#### 1.1 Purpose

Egis (Formerly McIntosh Perry or MP) has been retained by CSV Architects to prepare this Servicing and Stormwater Management Report in support of the Site Plan Control process for the proposed four-storey residential building, located at 214 Somerset Street East within the City of Ottawa.

The main purpose of this report is to present a servicing design for the development in accordance with the recommendations and guidelines provided by the City of Ottawa (City). This report will address the water, sanitary and storm sewer servicing for the development, ensuring that existing and available services will adequately service the proposed development.

This report should be read in conjunction with the following drawings:

- CCO-24-0450, C101 Site Grading and Drainage Plan, and
- CCO-24-0450, C102 Site Servicing Plan, AND
- CCO-24-0450, REM Removals Plan.

#### 1.2 Site Description

The property is located at 214 Somerset Street East within the Neighbourhood of Sandy Hill. It is described as Plan 45224, Part of Lot E, Broken Front D (Rideau Front), Geographic Township of Nepean, City of Ottawa. The land in question covers approximately 0.05 ha and is located between Henderson Avenue and Nelson Street. The development area for the proposed works is approximately 0.05 ha.

See Site Location Plan in Appendix 'A' for more details.

The site is currently developed with 6 townhomes and a rear yard space. The site has sanitary and water services, however, there are no storm services connected to the City sewer.

The proposed development consists of a 275 m<sup>2</sup>, four-storey community housing residential building. Pathways to building entrances will be provided throughout the site along with landscaping. The rear yard will also consist of amenity space, general storage, and bike storage.





Figure 1: Site Map

## 2.0 BACKROUND STUDIES

Background studies that have been completed for the proposed site include City of Ottawa as-built drawings and a topographical survey.

As-built drawings of existing services within the vicinity of the proposed site were reviewed in order to determine accurate servicing and stormwater management designs for the site.

A topographic survey of the site was completed by Farley, Smith & Denis Surveying Ltd.

## 3.0 PRE-CONSULTATION SUMMARY

A pre-consultation meeting was conducted on April 6<sup>th</sup>, 2023, regarding the proposed site. Specific design parameters to be incorporated within this design include the following:

- Pre-development flows shall be calculated using a time of concentration (Tc) of no less than 10 minutes and post-development flows shall use a Tc of 10 minutes.
- Control 5 through 100-year post-development flows to the 5-year pre-development flows with a combined C value to a maximum of 0.50. (Further correspondence has been had with the City. See Section 7.0).
- Quality control is required to be provided for this site as per RVCA requirements.
- Storm service to connect to 675mm diameter concrete storm sewer on Somerset St. E.



- Sanitary service to connect to 250mm diameter PVC sanitary sewer on Somerset St E.
- Sanitary sewer monitoring maintenance hole is to be installed on the private side of the property line
- A backwater valve is required on the sanitary service for protection.
- Water service to connect to 406mm diameter PVC watermain on Somerset St E.

The notes from the City of Ottawa can be found in Appendix 'B'.

#### 4.0 WATERMAIN

## 4.1 Existing Watermain

There is an existing 406mm diameter PVC watermain within Somerset St. E. The watermain is located in the 1W pressure zone and services multiple adjacent properties and multiple fire hydrants southwest and northeast of the proposed development on Somerset St. E.

## 4.2 Proposed Watermain

A new 100mm diameter PVC watermain is proposed to service the site, complete with a water valve located at the property line, and will be connected to the existing 406mm diameter watermain within Somerset St. E. The watermain is designed to have a minimum of 2.4m cover.

The Ontario 2006 Building Code Compendium (OBC) method was utilized to determine the required fire flow for the site per ISTB-2021-03. The Building Group Classification was Group C for Residential Occupancies. The water supply coefficient ('K' value) was deemed to be 23, under the conservative assumption that the building is of combustible construction. The spatial coefficient ('Stot' value) accounting for the surrounding buildings was 2.0, and the total building volume ('V' value) for the OBC calculation was determined to be 3,025 m³. The results of the calculations yielded a required fire flow of 4,500 L/min. A fire flow of 8,000 L/min was calculated using the Fire Underwriters Survey (FUS) requirements. The detailed calculations for the FUS and OBC can be found in Appendix 'C'.

The water demands for the proposed building have been calculated to adhere to the *Ottawa Design Guidelines* – *Water Distribution* manual and can be found in Appendix 'C'. The results have been summarized below:

 Site Area
 0.05 ha

 Residential
 280 L/c/d

 Average Day Demand (L/s)
 0.11

 Maximum Daily Demand (L/s)
 1.02

 Peak Hourly Demand (L/s)
 1.54

Table 1: Water Demands



OBC Fire Flow Requirement (L/s)	75.00
FUS Fire Flow Requirement (L/s)	133.33

Boundary conditions have been provided by the City of Ottawa for the current conditions and are available in Appendix 'C'. The results determined that the proposed 406mm watermain can adequately service the proposed development and provide sufficient fire flow. Refer to drawing for more details.

The normal operating pressure range is anticipated to be 450 kPa to 550 kPa and will not be less than 275 kPa (40 psi) or exceed 689 kPa (100 psi). The proposed watermain will meet the minimum required 20 psi (140 kPa) at the ground level under maximum day demand and fire flow conditions. The results are available in Appendix 'C' of this report.

Table 2: Water Pressure at Junctions per Scenario

Junction	Average Day (psi)	Peak Hourly (psi)	Max. Day + Fire Flow (psi)
J-1 (BLDG)	78.7	65.4	69.9

To confirm the adequacy of fire flow to protect the proposed development, public and private fire hydrants within 75 m of the proposed building were analyzed per City of Ottawa ISTB 2018-02 Appendix I Table 1. The results are demonstrated below.

Table 3: Fire Protection Confirmation

Duilding	Fire Flow Demand	Fire Hydrant(s) within	Combined Fire Flow
Building	(L/min.)	75m	(L/min.)
214 Somerset St. E. (OBC)	4,500	4	22,800
214 Somerset St. E. (FUS)	8,000	4	22,800

A hydrant cover figure can be found in Appendix 'C'.

## 5.0 SANITARY DESIGN

#### 5.1 Existing Sanitary Sewer

There is an existing 250mm diameter PVC sanitary collection sewer within Somerset St. E. The existing sanitary sewer drains to the Somerset Trunk Sewer.

## 5.2 Proposed Sanitary Sewer

Two new 150mm diameter gravity sanitary service will be connected to the existing 250mm diameter sanitary sewer within Somerset St. E. The west connection will have a monitoring sanitary maintenance hole. Due to space constraints, a monitoring port will be provided within the building for monitoring purposes as per the



*City of Ottawa – Sewer Design Guidelines*, October 2012, Clause 4.4.4.7 and City of Ottawa Sewer-Use By-Law 2003-514 (14).

Based on coordination with the mechanical engineer, only plumbing in the basement (floor drains, washroom) will be pumped. They have confirmed that they will be able to gravity drain the suites from the ground floor and above. Pump details will be specified by mechanical.

The subject site is a proposed four-storey residential building with 22 apartment units. The peak design flows for the proposed building were calculated using criteria from the *City of Ottawa – Sewer Design Guidelines, October 2012*. The proposed site development will generate a peak flow of 0.41 L/s.

The proposed 150 mm diameter gravity sanitary sewers will be installed to service the subject property with a minimum full flow target velocity (cleansing velocity) of 0.6 m/s and a full flow velocity of not more than 3.0 m/s. Design parameters for the site include an infiltration rate of 0.33 l/s/ha.

The proposed service for the site will be connected to existing 250mm diameter sanitary sewer within Somerset St. E. The sanitary flow for the proposed development is expected to be comparable to the existing conditions, therefore it is anticipated that there will be no issues with capacity constraints within the proposed lateral or within the existing sanitary main within Somerset St. E. City staff to confirm if there are any capacity concerns within the municipal system.

See Sanitary Sewer Design Sheet in Appendix 'D' of this report for more details.

## 6.0 STORM SEWER DESIGN

## 6.1 Existing Storm Sewers

The subject property is currently serviced by the city stormwater system by way of catch basins on Nelson St. and Somerset St. E. collecting surface runoff from the site. A portion of the surface runoff is unrestricted into the rear yard.

## 6.2 Proposed Storm Sewers

Runoff from the proposed site will be collected and stored on the roof of the proposed building. A proposed 150mm storm sewer will be installed directing the flow from the roof drains to the existing 675mm diameter storm sewer within Somerset St. E.

A perimeter foundation drainage system is to be provided for the proposed structure. This system will consist of a 100 to 150 mm diameter perforated corrugated plastic pipe, surrounded on all sides by a minimum of 150 mm of 10 mm clear crushed stone. The pipe is installed at the footing level around the exterior perimeter of the structure. For structures with varying basement levels, the drainage pipe is to be installed in two separate segments, splitting at the wall separating the lower and higher basement levels, provided the upper drainage pipe terminates in direct contact with the lower basement drainage board layer. The pipe is to have a positive



outlet, such as a gravity connection to the storm sewer or a sump system. If a sump system is considered, Paterson is to review and advise on a potential underfloor drainage system to collect water that may accumulate below the basement slab.

A storm sewer design sheet was created using the rational method and the City of Ottawa 5-year storm event. The minor storm sewers will be sized for the 5-year flow without any restriction. Drainage area information, along with respective pipe slopes and other necessary information was used to evaluate the performance of the storm sewer network. The time of concentration calculated for the storm sewer system is based on a 10-minute inlet time at the uppermost sewer run. Within the design sheet, pipe capacities and associated full flow velocities have been calculated. Storm flows will be controlled by roof drains to limit flows to the specified allowable release rate.

The sump pump is proposed to outlet to surface 0.6m above the building grade. Drainage will be collected by the proposed catch basin which outlets to the existing 675mm diameter storm sewer within Somerset St. E. via a 150mm catch basin lead.

See CCO-24-0450 - *POST* in Appendix 'F' and *Storm Sewer Design Sheet* in Appendix 'G' of this report for more details. The Stormwater Management design for the subject property will be outlined in Section 7.0.

#### 7.0 PROPOSED STORMWATER MANAGEMENT

## 7.1 Design Criteria and Methodology

Stormwater management for the proposed site will be maintained through positive drainage away from the proposed building and by roof drains that will direct storm water to the sewer as described above. The remainder of the restricted flow will surface drain to catch basins on Somerset St. E. and Nelson St. The unrestricted area is located in the rear-yard and will include permeable pavers and a grassed area. The quantitative and qualitative properties of the storm runoff for both the pre- and post-development flows are further detailed below. Stormwater Best Management Practices (SWM BMP's) will be implemented at the "Lot level", "Conveyance" and "End of Pipe" locations. These concepts will be explained further in Section 7.6.

In summary, the following design criteria have been employed in developing the stormwater management design for the site as directed by the City:

#### **Quality Control**

• The site has been designed with Best Management Practices (BMPs) and it is anticipated that clean stormwater will be leaving the site.



#### **Quantity Control**

• Post-development runoff directed to the right-of-way (ROW) and from the roof is to be restricted to the 5-year pre-development flows using a C of 0.5. An improvement from the existing conditions is proposed for the rear yard area.

#### 7.2 Runoff Calculations

Runoff calculations presented in this report are derived using the Rational Method, given as:

Q = 2.78CIA (L/s)

Where C = Runoff coefficient

= Rainfall intensity in mm/hr (City of Ottawa IDF curves)

A = Drainage area in hectares

It is recognized that the Rational Method tends to overestimate runoff rates. As a result, the conservative calculation of runoff ensures that any SWM facility sized using this method is expected to function as intended.

The following coefficients were used to develop an average C for each area:

Roofs/Concrete/Asphalt	0.90
Gravel	0.60
Permeable areas/Grass	0.20

As per the *City of Ottawa - Sewer Design Guidelines*, the 5-year balanced 'C' value must be increased by 25% for a 100-year storm event to a maximum of 1.0.

As per the pre-consultation meeting with the City of Ottawa the time of concentration (Tc) used for predevelopment shall be calculated using a Tc of 10 minutes and post-development flows shall be calculated using a Tc of 10 minutes.

## 7.3 Pre-Development Drainage

The existing site drainage limits are demonstrated on the Pre-Development Drainage Area Plan. A summary of the Pre-Development Runoff Calculations can be found below.

Table 4: Pre-Development Runoff Summary

Drainage Area	Area (ha)	Runoff Coefficient (2/5-Year)	Runoff Coefficient (100-Year)	2-year Peak Flow (L/s)	5-year Peak Flow (L/s)	100-year Peak Flow (L/s)
A1	0.04	0.90	1.00	7.71	10.50	20.00
A2	0.01	0.70	0.78	1.96	2.67	5.13
Total	0.05			9.67	13.17	25.12

See CCO-24-0450 - PRE in Appendix 'E' and Appendix 'G' for calculations.

## 7.4 Post-Development Drainage

The proposed site drainage limits are demonstrated on the Post-Development Drainage Area Plan. See CCO-24-0450 - *POST* in Appendix 'F' of this report for more details. A summary of the Post-Development Runoff Calculations can be found below.

Drainage Area	Area (ha)	Runoff Coefficient (2/5-Year)	Runoff Coefficient (100-Year)	2-year Peak Flow (L/s)	5-year Peak Flow (L/s)	100-year Peak Flow (L/s)
B1	0.03	0.90	1.00	5.28	7.19	13.69
B2	0.02	0.47	0.55	1.53	2.08	4.17
В3	0.01	0.60	0.70	1.34	1.82	3.60
Total	0.05			8.15	11.09	21.47

Table 5: Post-Development Runoff Summary

See Appendix 'G' for calculations. Runoff from area B1 will be restricted by roof drains before outletting to the existing storm system within Somerset St. E. Runoff for areas B2 and B3 will be unrestricted. Runoff from area B2 will drain towards Nelson Street and Somerset St E. Runoff from area B3 will be an improvement from the pre-development drainage conditions in the rear-yard. A perforated HDPE subdrain and clear-stone trench has been proposed in the rear yard to promote infiltration and additional storage in major events. The quantity and quality control measures are further detailed in Sections 7.5 and 7.6.

## 7.5 Quantity Control

Under current conditions, drainage within the rear yard sheet drains towards the neighboring properties from Area A2. Due to the large existing slopes in the rear yard, directing stormwater toward the Nelson St or Somerset St. ROWs is not viable for Area B2. The works are proposed to reduce the quantity that runs off to adjacent properties with the addition of permeable pavers and a landscaped area. Further, a clear stone trench with a perforated subdrain is proposed in the landscaped area to provide an opportunity for infiltration and add an additional storage measure. The trench will be 5.0 m long and, as per Ottawa Standard Detail Drawing S29, 0.9 m wide and 0.15 to 0.30 m deep, the trench itself has a depth of 1.03 – 1.16 m. Cleaning and flushing of the system through the landscape catch basins is required if sediment build up is present, visual inspection ensuring the system is functioning as designed is recommended every spring following the thaw of snow.

After discussing the stormwater management criteria for the site with City staff, the total post-development runoff for this site has been restricted to match the 5-year pre-development flow rate with a combined C value of 0.50. These values create the following allowable release rates for the site. See Appendix 'B' for preconsultation notes.



Table 6: Pre-Development Runoff Summary

Drainage	С	С	Tc		Q (L/s)	
Area	5-Year	100-Year	(min)	2-Year	5-Year	100-Year
A1	0.50	0.50	10		5.83	
A2	0.70	0.78	10	1.96	2.67	5.13

See Appendix 'G' for calculations.

Reducing site flows will be achieved using flow restrictions and creating onsite storage. Total runoff from areas B1, B2 and B3 will be restricted as shown in the table below.

Table 7: Post-Development Restricted Runoff Summary

Drainage Area	Post Development Unrestricted Flow (L/s)		Post Development Restricted Flow (L/s)		
	5-Year	100-Year	5-Year	100-Year	
B1	7.19	13.69	0.72	1.32	Restricted - Roof Drains
B2	2.08	4.17	2.08	4.17	Unrestricted to ROW
Total Toward ROW	9.27	17.87	2.80	5.49	
В3	1.82	3.60	1.82	3.60	Unrestricted
Total	11.09	21.47	4.62	9.09	

See Appendix 'G' for calculations.

Runoff from Area B1 will be restricted through two (2) roof drains before discharging to the new storm sewer connection to outlet to Somerset St. E. The total flow leaving the roof will be 0.72 L/s and 1.32 L/s during the 5 and 100-year storm events, respectively. Restrictions result in ponding depths of 30 and 55 mm for 5 and 100-year storm events, respectively. All of the storage required for this area will be located on the proposed roof, and emergency roof scuppers will be installed to ensure ponding does not exceed the proposed ponding limits and depths. See below table for details of the required and provided storage volumes.

Table 8: Storage Summary

Drainage Area	Depth of Ponding (m)	Storage Required (m³)	Storage Available (m³)	Depth of Ponding (m)	Storage Required (m³)	Storage Available (m³)
71100	5-Year				100-Year	
B1	0.030	5.6	6.2	0.055	10.8	11.3

See Appendix 'G' for calculations.

Runoff from the southwest and northwest portions of Area B2 will drain northwest toward the Somerset Street East ROW. The northeast and southeast portions of Area B2 will drain northeast to the Nelson Street ROW.



Area B3 in the scenario of emergency overland flow will runoff over the south property line, ensuring a lower rate than existing conditions.

## 7.6 Quality Control

The development of this lot will employ Best Management Practices (BMP's) wherever possible. The intent of implementing stormwater BMP's is to ensure that water quality and quantity concerns are addressed at all stages of development. Lot level BMP's typically include temporary retention of the parking lot runoff, minimizing ground slopes and maximizing landscaped areas. Some of these BMP's cannot be provided for this site due to site constraints and development requirements.

As the majority of the runoff from the site will be captured and conveyed through roof drains to the existing sewer system, it can be assumed that this is clean water leaving the site. The runoff from additional areas of the site is mainly from pervious landscaped areas in the rear yard, which can also be considered clean water. Therefore, it is believed that quality control is achieved.

#### 8.0 EROSION AND SEDIMENT CONTROL

#### 8.1 Temporary Measures

Before construction begins, temporary silt fence, straw bale or rock flow check dams will be installed at all natural runoff outlets from the property. It is crucial that these controls be maintained throughout construction and inspection of sediment and erosion control will be facilitated by the Contractor or Contract Administration staff throughout the construction period.

The Contractor, at their discretion or at the instruction of the City, Conservation Authority or the Contract Administrator shall increase the quantity of sediment and erosion controls on-site to ensure that the site is operating as intended and no additional sediment finds its way off site. The rock flow, straw bale & silt fence check dams and barriers shall be inspected weekly and after rainfall events. Care shall be taken to properly remove sediment from the fences and check dams as required. Fibre roll barriers are to be installed at all existing curb inlet catchbasins and filter fabric is to be placed under the grates of all existing catchbasins and manholes along the frontage of the site and any new structures immediately upon installation. The measures for the existing/proposed structures is to be removed only after all areas have been paved. Care shall be taken at the removal stage to ensure that any silt that has accumulated is properly handled and disposed of. Removal of silt fences without prior removal of the sediments shall not be permitted.

Although not anticipated, work through winter months shall be closely monitored for erosion along sloped areas. Should erosion be noted, the Contractor shall be alerted and shall take all necessary steps to rectify the situation. Should the Contractor's efforts fail at remediating the eroded areas, the Contractor shall contact the City and/or Conservation Authority to review the site conditions and determine the appropriate course of action. As the ground begins to thaw, the Contractor shall place silt fencing at all required locations as soon as



ground conditions warrant. Please see the *Site Grading, Drainage and Sediment & Erosion Control Plan* for additional details regarding the temporary measures to be installed and their appropriate OPSD references.

#### 8.2 Permanent Measures

Rip rap is to be placed at erosion prone locations as identified by the Contractor / Contract Administrator / City or Conservation Authority.

It is expected that the Contractor will promptly ensure that all disturbed areas receive topsoil and seed/sod and that grass be established as soon as possible. Any areas of excess fill shall be removed or levelled as soon as possible and must be located a sufficient distance from any watercourse to ensure that no sediment is washed out into the watercourse. As the vegetation growth within the site provides a key component to the control of sediment for the site, it must be properly maintained once established. Once the construction is complete, it will be up to the landowner to maintain the vegetation and ensure that the vegetation is not overgrown or impeded by foreign objects.

#### 9.0 SUMMARY

- A new 275m² four-storey residential building will be constructed along the property line at 214 Somerset St. E.
- A new 100mm watermain will be installed to service the site, connecting to the 400mm watermain on Somerset St. E.
- Two new 150mm sanitary sewer will be installed to service the proposed residential building and connect to Somerset St. E.
- Two proposed 150mm storm sewers will be installed to direct flow from both the roof and sump pump to the existing storm sewer on Somerset St. E.
- Storage for the 5- through 100-year storm events will be provided by roof drains on the proposed building.



## 10.0 RECOMMENDATION

Based on the information presented in this report, we recommend that the City of Ottawa approve this Servicing and Stormwater Management Report in support of the proposed residential building.

This report is respectfully being submitted for approval.

Regards,

Egis Canada Ltd.



Jessica Burden, P.Eng. Project Engineer, Land Development T: 613.266-5779

E: jessica.burden@egis-group.com

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Robbie Pickard, EIT Engineering Intern, Land Development T: 613.808.3427

E: robert.pickard@egis-group.com

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#### 11.0 STATEMENT OF LIMITATIONS

This report was produced for the exclusive use of CSV Architects. The purpose of the report is to assess the existing stormwater management system and provide recommendations and designs for the post-construction scenario that are in compliance with the guidelines and standards from the Ministry of the Environment, Conservation and Parks, City of Ottawa and local approval agencies. Egis Canada Ltd. reviewed the site information and background documents listed in Section 2.0 of this report. While the previous data was reviewed by Egis Canada Ltd. and site visits were performed, no field verification/measures of any information were conducted.

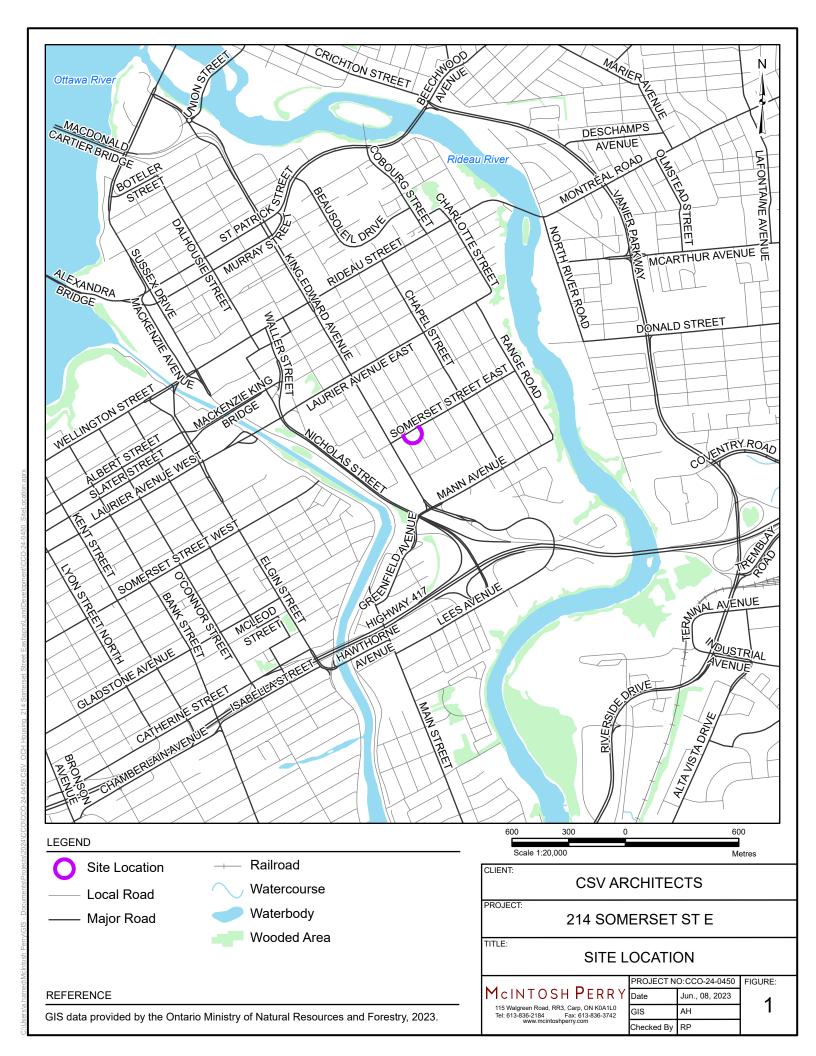
Any use of this review by a third party, or any reliance on decisions made based on it, without a reliance report is the responsibility of such third parties. Egis Canada Ltd. accepts no responsibility for damages, if any, suffered by any third party as a result of decisions or actions made based on this review.

The findings, conclusions and/or recommendations of this report are only valid as of the date of this report. No assurance is made regarding any changes in conditions subsequent to this date. If additional information is discovered or becomes available at a future date, Egis Canada Ltd. should be requested to re-evaluate the conclusions presented in this report, and provide amendments, if required.



## APPENDIX A KEY PLAN

McINTOSH PERRY



## APPENDIX B BACKGROUND DOCUMENTS

McINTOSH PERRY

#### Robbie Pickard

From: Bernier, John < John.Bernier@ottawa.ca>

Sent: Monday, May 1, 2023 2:57 PM

To: Jessie Smith

Cc: McMahon, Patrick; Kadri, Nader; Bakhit, Reza; Smith, Jack; Jessie Smith; John Verbaas;

leaning@csv.ca; freeman@fotenn.com; alain@fotenn.com; Dylan Bennett; Barron

Meyerhoffer; Gauthier, Steve; Richardson, Mark 214 Somerset Ste E - Preconsult - Follow-up

Attachments: 214 Somerset Street\_TOR Design Brief.pdf; Plans and Study list\_214 Somerset.pdf

#### Good afternoon,

Subject:

Sorry for the delay in getting these notes to you regarding your Somerset Street proposal. Please refer to the below [and/or attached notes] regarding the Pre-Application Consultation (pre-con) Meeting held on April 6, 2023 for the proposed development which includes demolition of existing rooming houses and replacement with new 4-storey, 22-unit apartment building with common amenity space. I have attached the required Plans & Study List for application submission.

Below [or attached] are staff's preliminary comments based on the information available at the time of pre-con meeting:

#### Planning Comments – John Bernier:

Official Plan: Downtown Core Transect, designated Minor Corridor (Sec 6.2) Secondary Plan: Central and East Downtown Core Secondary Plan

- Designated 'Corridor' on Schedule B
- Permits four storey, all-residential buildings
- Concerned with the provison in this secondary plan that requires an active frontage on the corridor:
  - "2) Development will provide a continuity of active frontages along the ground floor fronting all corridors. This includes functional main entrances that are directly accessible from the public realm for each unit on the ground floor. For further specification, this includes residential, retail and commercial units."

**Zoning:** R4UC[480]-c, which permits a Rooming House, the provisions of a low-rise apartment would apply, I encourage you to examine the UC subzone provisions closely - Sec 161, but will mention a few key points.

#### **General Comments:**

- Concerns with the deep wells proposed for the ground floor. What type of barrier will be used (OBC requirement) to protect people and how will this become a visual barrier along a fairly important frontage?
- Waste management does not appear to have been considered here. Please provide details regarding the garbage room (dimensions of the room and doorways), the bins intended for use, and the path and staging area for the containers. See Sec 143
- Consider a completely fenced rear yard with controlled access for safety purposes.

Encourage light fixtures to be included in on the initial plan.

#### **Zoning Comments:**

 30% of the lot area must be provided as landscaped area for a lot containing an apartment low rise

The front facade must comprise at least 25 per cent windows, and furthermore

- Any part of the rear yard not occupied by drive aisles, pathways accessory structures, must be softscaped.
  - 50% of rear yard must be softscaped.
- Based on the size of the building, 25% of units must be two-bedroom
- Front and corner yards shall include permanent fixtures that prevent illegal parking such as: planters, benches, bollards, trees, ornamental fencing, raised planters, etc.
- Accessory buildings subject to Sec. 55 specifically, maximum of two accessory structures are permitted. So you'll need to unify these structures.
- Alternative setbacks apply see Sec 144.

#### **Vehicular Circulation/ Parking:**

• The site is located within Area X and therefore parking is required. 0.25 spaces per rooming unit. However, I would be supportive of a variance given the proposed use.

#### **Bicycle Parking:**

- A variance or zoning amendment would need to be supported by a rationale as to why
  the reduction is appropriate. I would suggest that you include a 1:1 ratio of units to
  bicycle lockups.
- Provide enclosed and covered locations (required for multi-unit dwellings).
- Should not include racks near the public realm. Locate these in easy to access and highly visible areas.
- See Sec. 111 for further information on the specs required.

#### Applications:

- Site Plan Control Application (complex)
- Minor Variance or Zoning By-law Amendment

## Urban Design Comments - Nader Kadri:

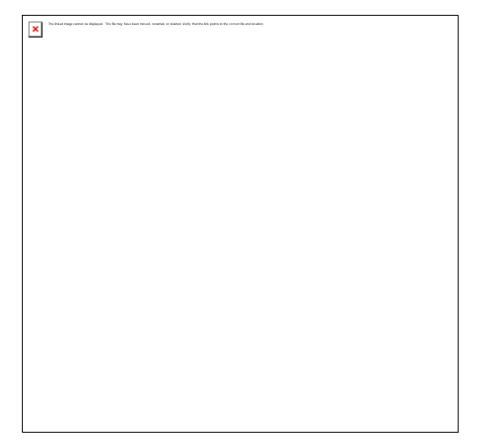
- Design Brief required TOR attached.
- Please ensure that there is sufficient light access for units. Windows appear to be very small and narrow.
- Please explore the potential for active entrances along public streets.
- Please explore the potential for additional tree planting.
- Please ensure that there is sufficient bike parking for the development.
- Please explore the use of materials that are prevalent within the area.
- Staff understand that the building will excel relative to modern day sustainability practices, please provide additional details as part of your submission.
- Indoor and outdoor amenity needed to support the number of small units within the building.

#### **Engineering Comments – Reza Bakhit:**

#### General:

- It is the sole responsibility of the consultant to investigate the location of existing underground utilities in the proposed servicing area and submit a request for locates to avoid conflict(s). The location of existing utilities and services shall be documented on an **Existing Conditions** Plan.
- Any easements on the subject site shall be identified and respected by any development proposal and shall adhere to the conditions identified in the easement agreement. A legal survey plan shall be provided, and all easements shall be shown on the engineering plans.
- Concern about the slope stability of the site as it appears that the site has slopes (existing or proposed) steeper than 5 horizontals to 1 vertical (i.e., 11 degree inclination from horizontal).
   The geotechnical engineer should investigate the stability of the slope.
- Concern about protection of 610mm backbone watermain on Nelson Street. Vibration and settlement monitoring plan will be required. Details of the Vibration Monitoring plan will depend on the depth of any underground levels for the development and the shoring method.
- Reference documents for information purposes :
  - Ottawa Sewer Design Guidelines (October 2012)
  - Technical Bulletin PIEDTB-2016-01
  - Technical Bulletins ISTB-2018-01, ISTB-2018-02 and ISTB-2018-03.
  - Ottawa Design Guidelines Water Distribution (2010)
  - Technical Bulletin ISTB-2021-03
  - Geotechnical Investigation and Reporting Guidelines for Development Applications in the City of Ottawa (2007)
  - City of Ottawa Slope Stability Guidelines for Development Applications (revised 2012)
  - City of Ottawa Environmental Noise Control Guidelines (January 2016)
  - City of Ottawa Accessibility Design Standards (2012) (City recommends development be in accordance with these standards on private property)
  - Ottawa Standard Tender Documents (latest version)
  - Ontario Provincial Standards for Roads & Public Works (2013)
  - Record drawings and utility plans are also available for purchase from the City (Contact the City's Information Centre by email at <a href="mailto:lnformationCentre@ottawa.ca">lnformationCentre@ottawa.ca</a> or by phone at (613) 580-424 x.44455).

Please note that this is the applicant responsibility to refer to the latest applicable guidelines while preparing reports and studies.



#### Disclaimer:

The City of Ottawa does not guarantee the accuracy or completeness of the data and information contained on the above image(s) and does not assume any responsibility or liability with respect to any damage or loss arising from the use or interpretation of the image(s) provided. This image is for schematic purposes only.

#### **Stormwater Management Criteria and Information:**

- Water Quantity Control: In the absence of area specific SWM criteria please control post-development runoff from the subject site, up to and including the 100-year storm event, to a 5-year pre-development level. The pre-development runoff coefficient will need to be determined as per existing conditions but in no case more than 0.5. [If 0.5 applies it needs to be clearly demonstrated in the report that the pre-development runoff coefficient is greater than 0.5]. The time of concentration (T<sub>c</sub>) used to determine the pre-development condition should be calculated. Tc should not be less than 10 min. since IDF curves become unrealistic at less than 10 min; T<sub>c</sub> of 10 minutes shall be used for all post-development calculations].
- Considering the size of the site, it would be acceptable to control the roof portion only (100-year storm event, to a 2-year pre-development level) and leave the remainder of the site uncontrol as long as the uncontrolled portion is directed towards the right of way. This approach should be discussed in the SWM report. Also, the grading plan should clearly demonstrate that the runoff from the uncontrolled portion of the site will be directed towards the ROW
- Any storm events greater than the established 5-year allowable release rate, up to and including the 100-year storm event, shall be detained on-site. The SWM measures required to avoid impact on downstream sewer system will be subject to review.

- Please note that foundation drainage is to be independently connected to sewer main unless being pumped with appropriate back up power, sufficient sized pump and back flow prevention. It is recommended that the foundation drainage system be drained by a sump pump connection to the storm sewer to minimize risk of basement flooding as it will provide the best protection from the uncontrolled sewer system compared to relying on the backwater valve.
- Water Quality Control: Please consult with the local conservation authority (RVCA) regarding
  water quality criteria prior to submission of a Site Plan Control Proposal application to establish
  any water quality control restrictions, criteria and measures for the site. Correspondence and
  clearance shall be provided in the Appendix of the report.
- Please note that as per Technical Bulletin PIEDTB-2016-01 section 8.3.11.1 (p.12 of 14) there shall be no surface ponding on private parking areas during the 5-year storm rainfall event.
- Underground Storage: Please note that the Modified Rational Method for storage computation in the Sewer Design Guidelines was originally intended to be used for above ground storage (i.e. parking lot) where the change in head over the orifice varied from 1.5 m to 1.2 m (assuming a 1.2 m deep CB and a max ponding depth of 0.3 m). This change in head was small and hence the release rate fluctuated little, therefore there was no need to use an average release rate.

When underground storage is used, the release rate fluctuates from a maximum peak flow based on maximum head down to a release rate of zero. This difference is large and has a significant impact on storage requirements. We therefore require that an average release rate equal to 50% of the peak allowable rate shall be applied to estimate the required volume. Alternatively, the consultant may choose to use a submersible pump in the design to ensure a constant release rate.

In the event that there is a disagreement from the designer regarding the required storage, The City will require that the designer demonstrate their rationale utilizing dynamic modelling, that will then be reviewed by City modellers in the Water Resources Group.

Please provide information on UG storage pipe. Provide required cover over pipe and details, chart of storage values, capacity etc. How will this pipe be cleaned of sediment and debris? Provide information on type of underground storage system including product name and model, number of chambers, chamber configuration, confirm invert of chamber system, top of chamber system, required cover over system and details, interior bottom slope (for self-cleansing), chart of storage values, length, width and height, capacity, entry ports (maintenance) etc.

Provide a cross section of underground chamber system showing invert and obvert/top, major and minor HWLs, top of ground, system volume provided during major and minor events. UG storage to provide actual 2- and 100-year event storage requirements.

In regard to all proposed UG storage, ground water levels (and in particular HGW levels) will need to be reviewed to ensure that the proposed system does not become surcharged and thereby ineffective.

Modeling can be provided to ensure capacity for both storm and sanitary sewers for the proposed development by City's Water Distribution Dept. – Modeling Group, through PM and upon request.

 Please note that the minimum orifice dia. for a plug style ICD is 83mm and the minimum flow rate from a vortex ICD is 6 L/s in order to reduce the likelihood of plugging.

- Post-development site grading shall match existing property line grades in order to minimize disruption to the adjacent residential properties. A topographical plan of survey shall be provided as part of the submission and a note provided on the plans.
- Please provide a Pre-Development Drainage Area Plan to define the pre-development drainage areas/patterns. Existing drainage patterns shall be maintained and discussed as part of the proposed SWM solution.
- If rooftop control and storage is proposed as part of the SWM solutions sufficient details (Cl. 8.3.8.4) shall be discussed and document in the report and on the plans. Roof drains are to be connected downstream of any incorporated ICDs within the SWM system and not to the foundation drain system. Provide a Roof Drain Plan as part of the submission.
- If Window wells are proposed, they are to be indirectly connected to the footing drains. A
  detail of window well with indirect connection is required, as is a note at window well location
  speaking to indirect connection.
- There must be at least 15cm of vertical clearance between the spill elevation and the ground elevation at the building envelope that is in proximity of the flow route or ponding area. The exception in this case would be at reverse sloped loading dock locations. At these locations, a minimum of 15cm of vertical clearance must be provided below loading dock openings. Ensure to provide discussion in report and ensure grading plan matches if applicable.
- Rear yard on grade parking to be permeable pavement. Refer to City Standard Detail Drawings SC26 (maintenance/temp parking areas), SC27 or permeable asphalt materials. No gravel or stone dust parking areas permitted.

#### Storm Sewer:

A 675mm dia. CONC storm sewer (1992) is available within Somerset St E.

Note: A 1800mm Brick Combined collector Sewer is located within the Nelson Street. No connection is permitted to this pipe.

#### **Sanitary Sewer:**

- A 250mm dia. PVC Sanitary sewer (1992) is available within Somerset St E.
- Please provide the new Sanitary sewer discharge and we confirm if sanitary sewer main has the capacity. An analysis and demonstration that there is sufficient/adequate residual capacity to accommodate any increase in wastewater flows in the receiving and downstream wastewater system is required to be provided. Needs to be demonstrated that there is adequate capacity to support any increase in wastewater flow.
- Please apply the wastewater design flow parameters in Technical Bulletin PIEDTB-2018-01.
- Sanitary sewer monitoring maintenance hole is required to be installed at the property line (on the private side of the property) as per City of Ottawa Sewer-Use By-Law 2003-514 (14) Monitoring Devices.
- A backwater valve is required on the sanitary service for protection.

Note: There is a 610mm backbone water main is located within Nelson Street . No connection is permitted to this pipe . Also , a Vibration and settlement monitoring plan will be required .

#### Water:

- A 406 mm dia. PVC watermain (1996) is available within Somerset St E.
- Existing residential service to be blanked at the main.
- Water Supply Redundancy: Residential buildings with a basic day demand greater than 50m³/day (0.57 L/s) are required to be connected to a minimum of two water services

- separated by an isolation valve to avoid a vulnerable service area as per the *Ottawa Design Guidelines Water Distribution*, WDG001, July 2010 Clause 4.3.1 Configuration.
- Please review Technical Bulletin ISTB-2018-0, maximum fire flow hydrant capacity is provided in Section 3 Table 1 of Appendix I. A hydrant coverage figure shall be provided and demonstrate there is adequate fire protection for the proposal. Two or more public hydrants are anticipated to be required to handle fire flow.
- Boundary conditions are required to confirm that the require fire flows can be achieved as well as availability of the domestic water pressure on the City street in front of the development. Use Table 3-3 of the MOE Design Guidelines for Drinking-Water System to determine Maximum Day and Maximum Hour peaking factors for 0 to 500 persons and use Table 4.2 of the Ottawa Design Guidelines, Water Distribution for 501 to 3,000 persons. Please provide the following information to the City of Ottawa via email to request water distribution network boundary conditions for the subject site. Please note that once this information has been provided to the City of Ottawa it takes approximately 5-10 business days to receive boundary conditions.
  - Type of Development and Units
  - Site Address
  - A plan showing the proposed water service connection location.
  - Average Daily Demand (L/s)
  - Maximum Daily Demand (L/s)
  - Peak Hour Demand (L/s)
  - Fire Flow (L/min)

[Fire flow demand requirements shall be based on **Fire Underwriters Survey (FUS)** Water Supply for Public Fire Protection 1999

[Fire flow demand requirements shall be based on ISTB-2021-03]

Note: The OBC method can be used if the fire demand for the private property is less than 9,000 L/min. If the OBC fire demand reaches 9000 L/min, then the FUS method is to be used. Exposure separation distances shall be defined on a figure to support the FUS calculation and required fore flow (RFF).

 Hydrant capacity shall be assessed to demonstrate the RFF can be achieved. Please identify which hydrants are being considered to meet the RFF on a fire hydrant coverage plan as part of the boundary conditions request.

#### **Snow Storage:**

Any portion of the subject property which is intended to be used for permanent or temporary snow storage shall be as shown on the approved site plan and grading plan. Snow storage shall not interfere with approved grading and drainage patters or servicing. Snow storage areas shall be setback from the property lines, foundations, fencing or landscaping a minimum of 1.5m. Snow storage areas shall not occupy driveways, aisles, required parking spaces or any portion of a road allowance. If snow is to be removed from the site please indicate this on the plan(s).

## Gas pressure regulating station

A gas pressure regulating station may be required depending on HVAC needs (typically for 12+ units). Be sure to include this on the Grading, Site Servicing, SWM and Landscape plans. This is to ensure that there are no barriers for overland flow routes (SWM) or conflicts with any proposed grading or landscape features with installed structures and has nothing to do with supply and demand of any product.



## **Regarding Quantity Estimates:**

Please note that external Garbage and/or bicycle storage structures are to be added to QE under Landscaping as it is subject to securities. In addition, sump pumps for Sanitary and Storm laterals and/or cisterns are to be added to QE under Hard items as it is subject to securities, even though it is internal and is spoken to under SWM and Site Servicing Report and Plan.

#### Road Reinstatement

Where servicing involves three or more service trenches, either a full road width or full lane width 40 mm asphalt overlay will be required, as per amended Road Activity By-Law 2003-445 and City Standard Detail Drawing R10. The amount of overlay will depend on condition of roadway and width of roadway(s).

## **Required Engineering Plans and Studies:**

#### **PLANS:**

- Existing Conditions and Removals Plan
- Site Servicing Plan
- Grade Control and Drainage Plan
- Erosion and Sediment Control Plan
- Roof Drainage Plan
- Topographical survey

#### **REPORTS:**

- Site Servicing and Stormwater Management Report
- Geotechnical Study/Investigation
- Slope Stability Assessment Reports ( Please see the requirements below)
- Noise Control Study
- Phase I ESA
- Phase II ESA (Depending on recommendations of Phase I ESA)
- Site lighting certificate
- Vibration and settlement monitoring plan for 610mm watermain

## Please refer to the City of Ottawa Guide to Preparing Studies and Plans [Engineering]:

Specific information has been incorporated into both the <u>Guide to Preparing Studies and Plans</u> for a site plan. The guide outlines the requirement for a statement to be provided on the plan about where the property boundaries have been derived from.

Added to the general information for servicing and grading plans is a note that an O.L.S. should be engaged when reporting on or relating information to property boundaries or existing conditions. The importance of engaging an O.L.S. for development projects is emphasized.

#### **Phase One Environmental Site Assessment:**

 A Phase I ESA is required to be completed in accordance with Ontario Regulation 153/04 in support of this development proposal to determine the potential for site contamination.
 Depending on the Phase I recommendations a Phase II ESA may be required.

- The Phase I ESA shall provide all the required Environmental Source Information as required by O. Reg. 153/04. ERIS records are available to public at a reasonable cost and need to be included in the ESA report to comply with O.Reg. 153/04 and the Official Plan. The City will not be in a position to approve the Phase I ESA without the inclusion of the ERIS reports.
- Official Plan Section 4.8.4:

https://ottawa.ca/en/city-hall/planning-and-development/official-plan-and-master-plans/official-plan/volume-1-official-plan/section-4-review-development-applications#4-8-protection-health-and-safety

#### Geotechnical Investigation:

- A Geotechnical Study/Investigation shall be prepared in support of this development proposal.
- Reducing the groundwater level in this area can lead to potential damages to surrounding structures due to excessive differential settlements of the ground. The impact of groundwater lowering on adjacent properties needs to be discussed and investigated to ensure there will be no short term and long term damages associated with lowering the groundwater in this area.
- Geotechnical Study shall be consistent with the Geotechnical Investigation and Reporting Guidelines for Development Applications.

https://documents.ottawa.ca/sites/documents/files/geotech\_report\_en.pdf

#### **Slope Stability Assessment Reports**

- A report addressing the stability of slopes, prepared by a qualified geotechnical engineer licensed in the Province of Ontario, should be provided wherever a site has slopes (existing or proposed) steeper than 5 horizontal to 1 vertical (i.e., 11 degree inclination from horizontal) and/or more than 2 metres in height.
- A report is also required for sites having retaining walls greater than 1 metre high, that addresses the global stability of the proposed retaining walls.
   <a href="https://documents.ottawa.ca/en/document/slope-stability-guidelines-development-applications">https://documents.ottawa.ca/en/document/slope-stability-guidelines-development-applications</a>

#### Noise Study:

- A Transportation Noise Assessment is required as the subject development is located within 100m proximity of an Arterial or collector Road
- A Stationary Noise Assessment is required in order to assess the noise impact of the proposed sources of stationary noise (mechanical HVAC system/equipment) of the development onto the surrounding residential area to ensure the noise levels do not exceed allowable limits specified in the City Environmental Noise Control Guidelines.

https://documents.ottawa.ca/sites/default/files/documents/enviro\_noise\_guide\_en.pdf

#### Vibration and settlement monitoring on Backbone Watermain:

A 610mm dia. backbone watermain is located within Nelson Street. Please note that to ensure the integrity of the nearby watermain the applicant may be required to develop a Vibration and Settlement Monitoring Program. A Vibration and settlement Monitoring Specialist Engineer shall undertake monitoring, develop a vibration and settlement monitoring plan, and prepare a protection plan, an emergency response plan, ensure conformance and shall issue certificates of conformance. The Vibration and settlement Monitoring Specialist Engineer shall be a licensed engineer in the Province of Ontario with a minimum of five years of experience in the field of Vibration and settlement monitoring. Vibration and settlement monitors are to be to be placed directly on the watermain. The maximum peak particle velocities are to be in accordance with Table 1 of the City of Ottawa Specification F-1201.

Note: In addition to requirement of a vibration specialist engineer required to design and monitor vibration, a certificate of liability insurance shall be submitted to the City wherein the Owner is the named insured and the City of Ottawa is an additional insured. The limits of the policy shall be in the amount of \$25,000,000 and shall be kept in full force and effect for the term of the construction work.

https://documents.ottawa.ca/sites/default/files/documents/enviro\_noise\_guide\_en.pdf

#### **Exterior Site Lighting:**

Any proposed light fixtures (both pole-mounted and wall mounted) must be part of the approved Site Plan. All external light fixtures must meet the criteria for Full Cut-off Classification as recognized by the Illuminating Engineering Society of North America (IESNA or IES), and must result in minimal light spillage onto adjacent properties (as a guideline, 0.5 fc is normally the maximum allowable spillage). In order to satisfy these criteria, the please provide the City with a Certification (Statement) Letter from an acceptable professional engineer stating that the design is compliant.

#### Fourth (4<sup>th</sup>) Review Charge:

Please be advised that additional charges for each review, after the 3<sup>rd</sup> review, will be applicable to each file. There will be no exceptions.

**Construction approach** – Please contact the Right-of-Ways Permit Office <u>TMconstruction@ottawa.ca</u> early in the Site Plan process to determine the ability to construct site and copy File Lead on this request.

Please note that these comments are considered <u>preliminary based on the information available</u> to date and therefore maybe amended as additional details become available and presented to the City. It is the responsibility of the applicant to <u>verify the above information</u>. The applicant may contact me for follow-up questions related to engineering/infrastructure prior to submission of an application if necessary.

#### Forestry Comments - Mark Richardson

- Please note that all process for reviewing and approving TCRs are changing at the City

   in order to effectively review your submission in a timely manner the Planning
   Forester will need to ensure that all TCR requirements have been addressed
- 2. If there are trees on site, or if there are trees with a critical root zone that extends onto the development site, a Tree Conservation Report (TCR) must be supplied
  - a. an approved TCR is a requirement of Site Plan approval.
- 3. Any removal of privately-owned trees 10cm or larger in diameter, or city-owned trees of any diameter requires a tree permit issued under the Tree Protection Bylaw (Bylaw 2020 340); the permit will be based on an approved TCR and made available at or near plan approval.
- 4. The TCR must contain 2 separate plans:
  - a. Plan/Map 1 show existing conditions with tree cover information
  - b. Plan/Map 2 show proposed development with tree cover information
  - c. Please ensure retained trees are shown on the landscape plan
- 5. the TCR must list all trees on site, as well as off-site trees if the CRZ extends into the developed area, by species, diameter and health condition
- 6. please identify trees by ownership private onsite, private on adjoining site, city owned, coowned (trees on a property line)
  - a. Compensation may be required for the removal of city owned trees.

- 7. If trees are to be removed, the TCR must clearly show where they are, and document the reason they cannot be retained
- 8. All retained trees must be shown, and all retained trees within the area impacted by the development process must be protected as per City guidelines available at <a href="Tree Protection Specification">Tree Protection Specification</a> or by searching Ottawa.ca
  - a. the location of tree protection fencing must be shown on the plan
  - b. show the critical root zone of the retained trees
- 9. the City encourages the retention of healthy trees; if possible, please seek opportunities for retention of trees that will contribute to the design/function of the site.
- 10. For more information on the process or help with tree retention options, contact Mark Richardson mark.richardson@ottawa.ca or on City of Ottawa

#### Planning Forester LP tree planting requirements:

Please note that all process for reviewing and approving LP tree planting has changed at the City – in order to effectively review your submission in a timely manner the Planning Forester will need to ensure that all the bullets listed below have been addressed

- 1) Minimum Setbacks
  - Maintain 1.5m from sidewalk or MUP/cycle track or water service laterals.
  - Maintain 2.5m from curb
  - Coniferous species require a minimum 4.5m setback from curb, sidewalk or MUP/cycle track/pathway.
  - Maintain 7.5m between large growing trees, and 4m between small growing trees.
     Park or open space planting should consider 10m spacing, except where otherwise approved in naturalization / afforestation areas. Adhere to Ottawa Hydro's planting guidelines (species and setbacks) when planting around overhead primary conductors.
- 2) Tree specifications
  - Minimum stock size: 50mm tree caliper for deciduous, 200cm height for coniferous.
  - Maximize the use of large deciduous species wherever possible to maximize future canopy coverage
  - Tree planting on city property shall be in accordance with the City of Ottawa's Tree Planting Specification; and include watering and warranty as described in the specification (can be provided by Forestry Services).
  - Plant native trees whenever possible
  - No root barriers, dead-man anchor systems, or planters are permitted.
  - No tree stakes unless necessary (and only 1 on the prevailing winds side of the tree)
- 3) Hard surface planting
  - Curb style planter is highly recommended
  - No grates are to be used and if guards are required, City of Ottawa standard (which can be provided) shall be used.
  - Trees are to be planted at grade
- 4) Soil Volume
  - <u>Please document on the LP that adequate soil volumes can be met:</u>

Tree		Multiple Tree
Type/Size	Volume (m3)	Soil Volume (m3/tree)
Ornamental	15	9

Columnar	15	9
Small	20	12
Medium	25	15
Large	30	18
Conifer	25	15

#### Sensitive Marine Clay

Please follow the City's 2017 Tree Planting in Sensitive Marine Clay guidelines

#### <u>Transportation Comments – Patrick McMahon:</u>

- A TIA is not required.
- As this is a spine route with future planned infrastructure works, a 3mx3m corner triangle is requested at Nelson/Somerset St. E.
- Noise Impact Study is required at site plan for road noise given the proximity to Somerset St E.
- On site plan:
  - Dimension all pathways. The main connection to the building needs to meet AODA requirements, however pathways widths of at least 1.5m are recommended throughout the site.
- Ensure that at least the minimum number of bicycle parking stalls are provided. A ratio of one per unit is recommended to justify the reduction in vehicular parking.
- The applicant is encouraged to review and complete the TDM checklists on Ottawa.ca and to provide as many measures as possible to support sustainable transportation modes.

#### Other

You are encouraged to contact the Councillor Plante to discuss the proposal.

Please refer to the links to "Guide to preparing studies and plans" and fees for general information. Additional information is available related to building permits, development charges, and the Accessibility Design Standards. Be aware that other fees and permits may be required, outside of the development review process. You may obtain background drawings by contacting informationcentre@ottawa.ca.

These pre-con comments are valid for one year. If you submit a development application(s) after this time, you may be required to meet for another pre-consultation meeting and/or the submission requirements may change. You are as well encouraged to contact us for a follow-up meeting if the plan/concept will be further refined.

Please do not hesitate to contact me if you have any questions.

Regards,

### John Bernier, MCIP, RPP Planner II | *Urbaniste II*

Development Review, Central | Examen des projets d'aménagement, Central Planning, Real Estate and Economic Development Department | Direction générale de la planification, des biens immobiliers et du développement City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West. Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1 613.580.2424 ext./poste 21576 ottawa.ca/planning / ottawa.ca/urbanisme

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13

#### **PICKARD Robert**

From: Bakhit, Reza <reza.bakhit@ottawa.ca> Sent: Thursday, July 20, 2023 10:16 AM

To: Robbie Pickard Cc: Curtis Melanson

Subject: RE: Request for Boundary Conditions - Proposed Development at 214 Somerset St E

Attachments: 214 Somerset Street June 2023.pdf

Hi Robbie,

Here is the BC info.

Please note that I moved to another position in the City. Once you submit the application , the planner assigned to the file will inform you who is the Engineer PM going forward.

The following are boundary conditions, HGL, for hydraulic analysis at 214 Somerset Street, (zone 1W) assumed to be connected to the 406 mm watermain on Somerset Street (see attached PDF for location).

Min HGL: 106.0 m Max HGL: 115.3 m

Max Day + FF (75 L/s): 109.1 m Max Day + FF (133.3 L/s): 108.8 m

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

Regards,

Reza Bakhit, P.Eng. C.E.T Asset Management Analyst Building and Park Assets Unit 613.580.2424 ext 19346

u

🖾 <u>reza.bakhit@ottawa.ca</u>

Pronouns: he / him

From: Robbie Pickard <r.pickard@mcintoshperry.com>

Sent: July 19, 2023 10:57 AM

To: Bakhit, Reza <reza.bakhit@ottawa.ca>

Cc: Curtis Melanson <c.melanson@mcintoshperry.com>

Subject: RE: Request for Boundary Conditions - Proposed Development at 214 Somerset St E

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Hi Reza,

Hope all is well.

Would it be possible to provide an update on our request below?

Thank you,

#### Robbie Pickard

**Engineering Intern - Land Development** 

T. 343.317.6702

r.pickard@mcintoshperry.com | www.mcintoshperry.com

## McINTOSH PERRY



#### Turning Possibilities Into Reality

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Platinum member

From: Bakhit, Reza < reza.bakhit@ottawa.ca > Sent: Wednesday, June 7, 2023 1:11 PM

To: Robbie Pickard < <a href="mailto:r.pickard@mcintoshperry.com">r.pickard@mcintoshperry.com</a> Cc: Curtis Melanson < <a href="mailto:c.melanson@mcintoshperry.com">c.melanson@mcintoshperry.com</a>

Subject: RE: Request for Boundary Conditions - Proposed Development at 214 Somerset St E

Hi Robbie,

Thanks for the update.

I sent your request to the modeling team and will update you as soon as we get the results. Please note that it could take up to two weeks for them to get back to us.

Regards,

Reza Bakhit, P.Eng, C.E.T

**Project Manager** 

Planning, Real Estate and Economic Development Department / Direction générale de la planification, des biens immobiliers et du développement économique

Development Review - Centeral Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

#### 613.580.2424 ext./poste 19346, reza.bakhit@ottawa.ca

Please note: Given the current pandemic, I will be working from home until further notice; reaching me by email is the easiest. I will be checking my voicemail, just not as frequently as I normally would be.

From: Robbie Pickard < r.pickard@mcintoshperry.com >

Sent: Wednesday, June 07, 2023 11:28 AM To: Bakhit, Reza < reza.bakhit@ottawa.ca>

Cc: Curtis Melanson <c.melanson@mcintoshperry.com>

Subject: RE: Request for Boundary Conditions - Proposed Development at 214 Somerset St E

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Hi Reza,

After putting together a calculation sheet as per the attached. The estimated fire flow with the OBC calculation is 4500 L/min.

Again, please reach out with anything else.

Thank you,

#### **Robbie Pickard**

**Engineering Intern - Land Development** 

T. 343.317.6702

r.pickard@mcintoshperry.com | www.mcintoshperry.com

### McINTOSH PERRY

Turning Possibilities Into Reality

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From: Bakhit, Reza < <a href="mailto:reza.bakhit@ottawa.ca">reza.bakhit@ottawa.ca</a> Sent: Wednesday, June 7, 2023 10:28 AM

To: Robbie Pickard < <a href="mailto:r.pickard@mcintoshperry.com">r.pickard@mcintoshperry.com</a> Cc: Curtis Melanson < <a href="mailto:c.melanson@mcintoshperry.com">c.melanson@mcintoshperry.com</a>

Subject: RE: Request for Boundary Conditions - Proposed Development at 214 Somerset St E

Hi Robbie,

Could you please confirm that the OBC calculation yields a fire flow greater than 9,000 L/min? Please note the ISTB-2021-03 here and confirm.

4.2.11	Fire Demand Calculation Method	50	Replace section 4.2.11 in its entirety with the following:
			When calculating the fire flow requirements and affected pipe sizing, designers shall use the method developed by the Fire Underwriters Survey, and follow the protocol for application of the method as provided in Appendix H: Protocol to Clarify the Application of the Fire Flow calculation method Published by Fire Underwriters Survey (FUS).
			The requirements for levels of fire protection on private property in urban areas are covered in Section 7.2.11 of the Ontario Building code. If this approach yields a fire flow greater than 9,000 L/min then the Fire

## TECHNICAL BULLETIN ISTB-2021-03



	Underwriters Survey method shall be used to determine these requirements instead. The requirements for levels of fire protection on private property in rural areas are based on the FUS method in all cases.
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#### Regards,

Reza Bakhit, P.Eng, C.E.T

**Project Manager** 

Planning, Real Estate and Economic Development Department / Direction générale de la planification, des biens immobiliers et du développement économique

Development Review - Centeral Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste 19346, reza.bakhit@ottawa.ca

Please note: Given the current pandemic, I will be working from home until further notice; reaching me by email is the easiest. I will be checking my voicemail, just not as frequently as I normally would be.

From: Robbie Pickard < r.pickard@mcintoshperry.com >

Sent: Wednesday, June 07, 2023 10:20 AM To: Bakhit, Reza < reza.bakhit@ottawa.ca>

Cc: Curtis Melanson < c.melanson@mcintoshperry.com >

Subject: Request for Boundary Conditions - Proposed Development at 214 Somerset St E

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ATTENTION: Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.

Hello,

We would like to request boundary conditions for a proposed development at 214 Somerset St E. The development consists of a new four-story residential building. We will require boundary conditions for a potential connection to the existing 406 CI watermain within Somerset Street.

Attached is a map highlighting the proposed connection location, along with calculations prepared for the following demands.

The estimated fire flow is 8,000 L/min based on the 2020 FUS

Average daily demand: 0.11 L/s
Maximum daily demand: 1.02 L/s
Maximum hourly daily: 1.54 L/s

Should you have any questions or require further clarification, please do not hesitate to reach out.

Thank you,

### Robbie Pickard

Engineering Intern - Land Development
T. 343.317.6702
r.pickard@mcintoshperry.com | www.mcintoshperry.com

### McINTOSH PERRY

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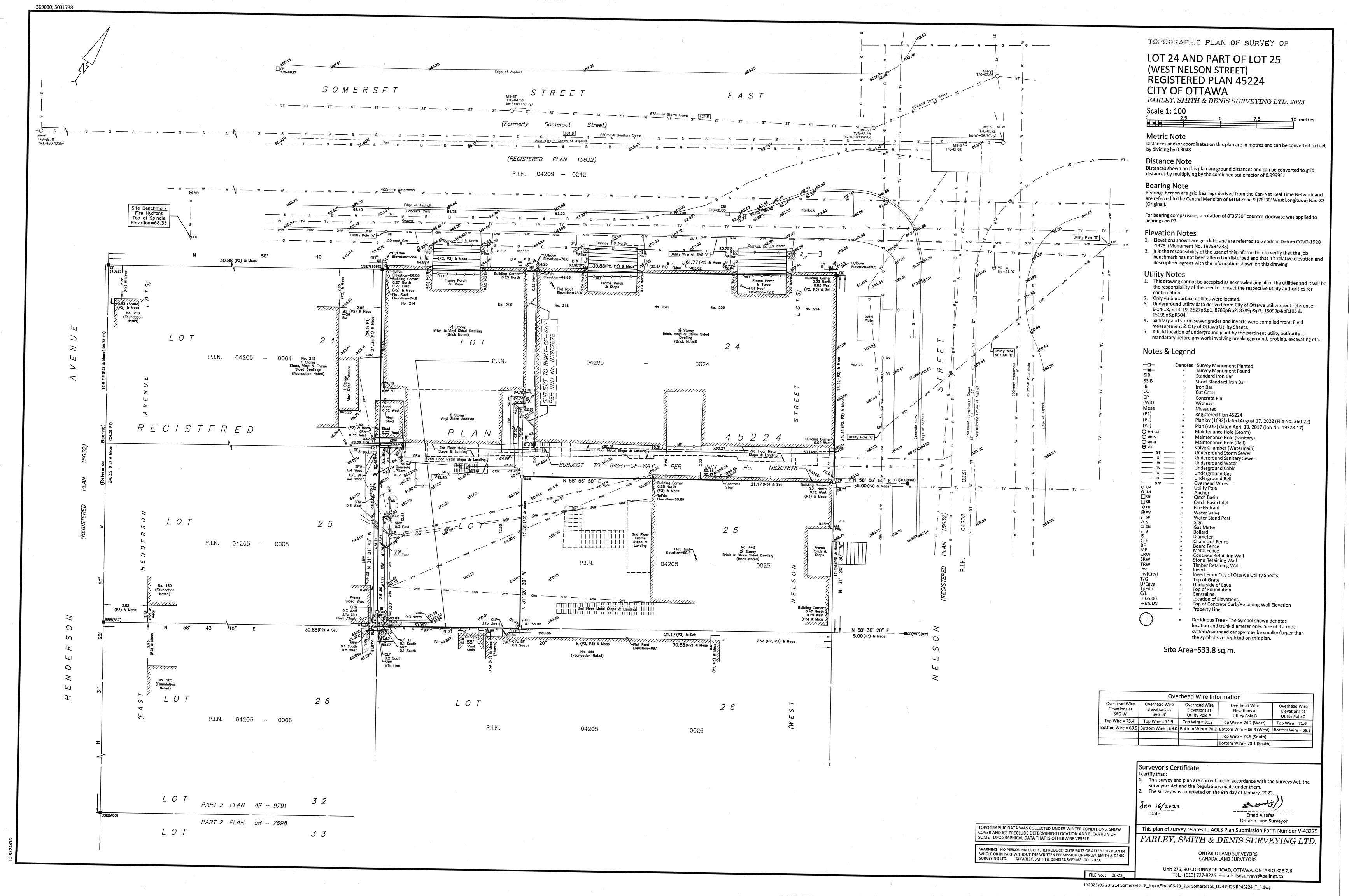
Le présent courriel a été expédié par le système de courriels de la Ville d'Ottawa. Toute distribution, utilisation ou reproduction du courriel ou des renseignements qui s'y trouvent par une personne autre que son destinataire prévu est interdite. Je vous remercie de votre collaboration.

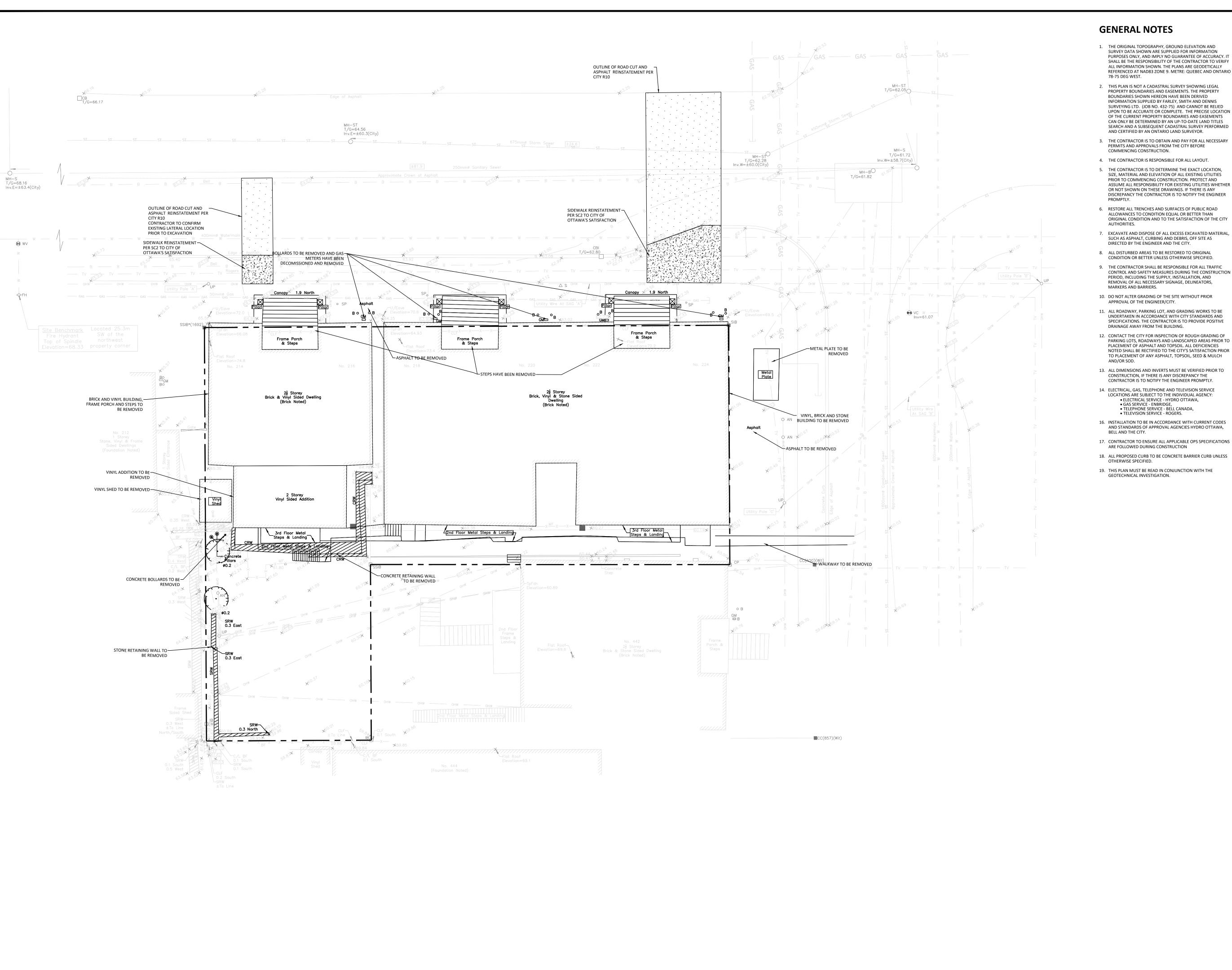
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- SURVEY DATA SHOWN ARE SUPPLIED FOR INFORMATION PURPOSES ONLY, AND IMPLY NO GUARANTEE OF ACCURACY. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY ALL INFORMATION SHOWN. THE PLANS ARE GEODETICALLY REFERENCED AT NAD83 ZONE 9. METRE: QUEBEC AND ONTARIO
- 2. THIS PLAN IS NOT A CADASTRAL SURVEY SHOWING LEGAL PROPERTY BOUNDARIES AND EASEMENTS. THE PROPERTY INFORMATION SUPPLIED BY FARLEY, SMITH AND DENNIS SURVEYING LTD. (JOB NO. 432-75) AND CANNOT BE RELIED UPON TO BE ACCURATE OR COMPLETE. THE PRECISE LOCATION

- 5. THE CONTRACTOR IS TO DETERMINE THE EXACT LOCATION, SIZE, MATERIAL AND ELEVATION OF ALL EXISTING UTILITIES PRIOR TO COMMENCING CONSTRUCTION. PROTECT AND ASSUME ALL RESPONSIBILITY FOR EXISTING UTILITIES WHETHER OR NOT SHOWN ON THESE DRAWINGS. IF THERE IS ANY DISCREPANCY THE CONTRACTOR IS TO NOTIFY THE ENGINEER
- ALLOWANCES TO CONDITION EQUAL OR BETTER THAN ORIGINAL CONDITION AND TO THE SATISFACTION OF THE CITY
- SUCH AS ASPHALT, CURBING AND DEBRIS, OFF SITE AS
- CONDITION OR BETTER UNLESS OTHERWISE SPECIFIED.
- 9. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL TRAFFIC CONTROL AND SAFETY MEASURES DURING THE CONSTRUCTION PERIOD, INCLUDING THE SUPPLY, INSTALLATION, AND REMOVAL OF ALL NECESSARY SIGNAGE, DELINEATORS,
- UNDERTAKEN IN ACCORDANCE WITH CITY STANDARDS AND SPECIFICATIONS. THE CONTRACTOR IS TO PROVIDE POSITIVE
- PARKING LOTS, ROADWAYS AND LANDSCAPED AREAS PRIOR TO PLACEMENT OF ASPHALT AND TOPSOIL. ALL DEFICIENCIES NOTED SHALL BE RECTIFIED TO THE CITY'S SATISFACTION PRIOR TO PLACEMENT OF ANY ASPHALT, TOPSOIL, SEED & MULCH
- CONSTRUCTION, IF THERE IS ANY DISCREPANCY THE
- LOCATIONS ARE SUBJECT TO THE INDIVIDUAL AGENCY:
- AND STANDARDS OF APPROVAL AGENCIES HYDRO OTTAWA,
- 17. CONTRACTOR TO ENSURE ALL APPLICABLE OPS SPECIFICATIONS
- 19. THIS PLAN MUST BE READ IN CONJUNCTION WITH THE



LEGEND

LIMIT OF CONSTRUCTION — PROPERTY LINE CONCRETE BARRIER — DRAINAGE SWALE CONCRETE WALKWAY — — — DRAINAGE DITCH SLOPING AT 3:1
UNLESS SPECIFIED 95,50 SURFACE ELEVATION SWALE ELEVATION

XT/W95.50 TOP OF WALL ELEVATION BOTTOM OF WALL ELEVATION MH#A T/G SANITARY SEWER MANHOLE OVERLAND FLOW ROUTE SILT FENCE BARRIER

STRAW BALE CHECK DAM

MUD MAT

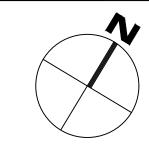
WATER METER ROOF DRAIN EXIT/ENTRY LOCATION 1.0% PROPOSED SLOPE

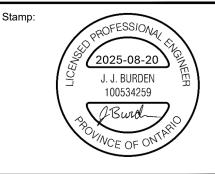
WATER VALVE

09	REISSUED PER CITY COMMENTS	08/20/2025	
08	ISSUED FOR SUBMISSION	07/30/2025	
07	ISSUED FOR SUBMISSION	05/14/2025	
06	ISSUED FOR CONSTRUCTION	03/21/2025	
05	ISSUED FOR PERMIT	02/27/2025	
04	ISSUED FOR SUBMISSION	02/15/2025	
03	ISSUED FOR SUBMISSION	12/10/2024	
02	ISSUED FOR RE-ZONING	08/28/2023	
01	ISSUED FOR REVIEW	08/24/2023	
No.	Revisions Date		
Cheo befo	Check and verify all dimensions before proceeding with the work Do not scale drawing		

SCALE 1:100







CSV ARCHITECTS
190 O'CONNOR STREET, SUITE 100 OTTAWA, ON

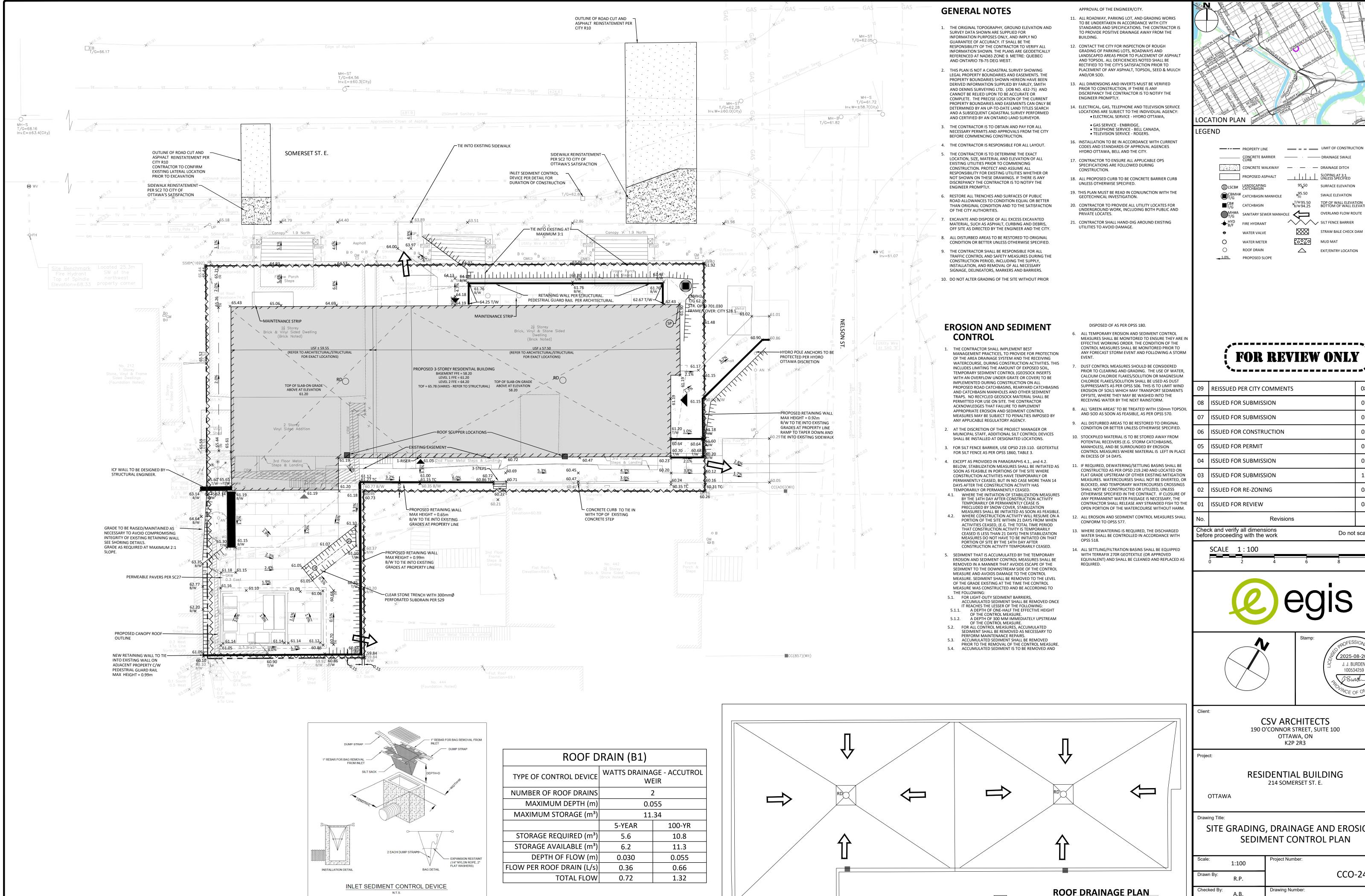
RESIDENTIAL BUILDING 214 SOMERSET ST. E.

K2P 2R3

SITE REMOVALS PLAN

			$\simeq$
Scale:	1:100	Project Number:	)-5:
Drawn By:	R.P.	CCO-24-0450	2-2
Checked By:	A.B.	Drawing Number:	7-1
Designed By:	R.P.	The second of th	9

ON



LIMIT OF CONSTRUCTION — PROPERTY LINE \_ CONCRETE BARRIER ----- DRAINAGE SWALE CONCRETE WALKWAY — — DRAINAGE DITCH SLOPING AT 3:1 UNLESS SPECIFIED

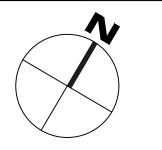
SURFACE ELEVATION SWALE ELEVATION TOP OF WALL ELEVATION BOTTOM OF WALL ELEVATION OVERLAND FLOW ROUTE

SILT FENCE BARRIER STRAW BALE CHECK DAM MUD MAT

EXIT/ENTRY LOCATION

9	REISSUED PER CITY COMMENTS	08/20/2025
8	ISSUED FOR SUBMISSION	07/30/2025
7	ISSUED FOR SUBMISSION	05/14/2025
16	ISSUED FOR CONSTRUCTION	03/21/2025
)5	ISSUED FOR PERMIT	02/27/2025
)4	ISSUED FOR SUBMISSION	02/14/2025
3	ISSUED FOR SUBMISSION	12/10/2024
)2	ISSUED FOR RE-ZONING	08/28/2023
)1	ISSUED FOR REVIEW	08/24/2023
О.	Revisions	Date





REFER TO ARCHITECTURAL DRAWING FOR FURTHER DETAIL



ON

Do not scale drawings

**CSV ARCHITECTS** 190 O'CONNOR STREET, SUITE 100 OTTAWA, ON K2P 2R3

> RESIDENTIAL BUILDING 214 SOMERSET ST. E.

SITE GRADING, DRAINAGE AND EROSION & SEDIMENT CONTROL PLAN

				$\sim$
Scale:	1:100	Project Number:		2-(
Drawn By:	R.P.		CCO-24-0450	2-2
Checked By:	A.B.	Drawing Number:		7-1
Designed By:	R.P.		C101	00
			#10200	Š

# **SEWER NOTES**

TO BE PVC SDR-28.

SPECIFICATIONS, AS WELL AS CITY.

- CONSTRUCT ALL SEWERS, CATCH BASINS, MANHOLES AND APPURTENANCES IN ACCORDANCE WITH OPSD STANDARDS AND
- SEWER TRENCHING AND BEDDING SHALL CONFORM TO OPSD 802.010 AND 802.013 UNLESS NOTED OTHERWISE. .1. BEDDING SHALL BE A MINIMUM 150mm OF GRANULAR "A", COMPACTED TO MINIMUM 95% STANDARD PROCTOR DRY DENSITY. CLEAR STONE BEDDING SHALL NOT BE PERMITTED. 2.2. SUB-BEDDING, IF REQUIRED SHALL CONSIST OF 450mm OF
- COMPACTED GRANULAR "B" TYPE 1. 2.3. BACKFILL TO AT LEAST 300mm ABOVE TOP OF PIPE WITH GRANULAR "A" OR GRANULAR "B" TYPE 1. 2.4. TO MINIMIZE DIFFERENTIAL FROST HEAVING, TRENCH BACKFILL (FROM PAVEMENT SUBGRADE TO 2.0 METRES
- SANITARY SEWERS AND CONNECTIONS 150mmØ AND SMALLER

BELOW FINISHED GRADE) SHALL MATCH EXISTING SOIL

SEWERS AND CONNECTIONS 200mmØ AND LARGER TO BE PVC SDR-35. BEDDING TO BE TYPE "B" EXCEPT AT RISERS, UNLESS NOTED OTHERWISE.

- 5. INSULATE ALL STORM AND SANITARY SEWERS/SERVICES THAT HAVE LESS THAN 2.0m OF COVER WITH THERMAL INSULATION AS
- 6. SEWER CONNECTIONS ARE TO BE MADE ABOVE THE SPRINGLINE OF THE SEWERMAIN AS PER CITY OF OTTAWA STANDARD DRAWING S11, S11.1 & S11.2.
- 7. SUPPLY AND INSTALL ALL PIPING AND APPURTENANCES AS SHOWN AND DETAILED TO WITHIN 1.0m OF BUILDING. ALL ENDS OF SERVICES TO BE PROPERLY CAPPED AND LOCATED WITH 2"x4"X8' LONG MARKER.
- 8. CONTRACTOR TO TELEVISE (CCTV) ALL PROPOSED SEWERS ON SITE, OUTLET CONNECTION TO THE MAIN AND PIPES 150mmØ OR GREATER PRIOR TO BASE COURSE ASPHALT. UPON COMPLETION OF CONTRACT, THE CONTRACTOR IS RESPONSIBLE TO FLUSH AND
- CLEAN ALL SEWERS & APPURTENANCES. 9. DYE TESTING IS TO BE COMPLETED ON SANITARY SERVICE TO CONFIRM PROPER CONNECTION TO SANITARY SEWER MAIN.

THE MAIN, TO THE SATISFACTION OF THE CITY.

10. ALL SERVICES PASSING THROUGH FOUNDATION WALL TO BE 11. ALL EXISTING SERVICES NOT TO BE USED SHALL BE BLANKED AT

# **WATERMAIN NOTES**

- 1. CONSTRUCT ALL WATERMAINS AND APPURTENANCES IN ACCORDANCE WITH OPSD STANDARDS AND SPECIFICATIONS, AS WELL AS CITY
- 2. INDUSTRIAL/COMMERCIAL SERVICE CONNECTIONS TO BE 50mm COPPER PIPING AND SHALL CONFORM TO ASTM B88 TYPE 'K' SOFT.
- 3. WATERMAINS AND/OR WATER SERVICES ARE TO HAVE A MINIMUM COVER OF 2.4m. OTHERWISE THERMAL INSULATION IS REQUIRED AS PER CITY STANDARDS (IF AVAILABLE) OR OPSD 1109.030.
- 4. IF THE WATERMAIN MUST BE DEFLECTED TO MEET ALIGNMENT, ENSURE THAT THE AMOUNT OF DEFLECTION USED IS EQUAL TO OR LESS THAN THAT WHICH IS RECOMMENDED BY THE MANUFACTURER.
- 5. THERMAL INSULATION OF WATERMAINS AT OPEN STRUCTURES AS PER
- CITY STANDARDS (IF AVAILABLE) OR OPSD 1109.030. 6. VALVES TO BE OPERATED BY CITY STAFF ONLY. 7. NO CONNECTION TO EXISTING WATER NETWORK SHALL BE

COMPLETED UNTIL A WATER PERMIT IS OBTAINED FROM THE CITY

CITY TO BE PRESENT FOR WATERMAIN CONNECTION. CONNECTION,

EXCAVATION, BACKFILLING AND REINSTATEMENT TO BE COMPLETED

- 8. ANY WATERMAIN CONNECTION(S) REQUIRED TO BE COMPLETED BY
- 9. ALL WATERMAINS SHALL BE EQUIPPED WITH BUTTERFLY AND GATE VALVES AS PER OPSD 1100.011.
- 10. ALL FIRE HYDRANTS, VALVE AND VALVE BOX HSALL CONFORM TO OPSD
- 11. CONCRETE THRUST BLOCKS TO CONFORM TO OPSD 1103.010 AND
- 12. ALL WATERMAIN TO BE CLASS 150 DR-18 OR APPROVED EQUIVALENT. 13. ALL WATERMAIN TO BE EQUIPPED WITH TRACER WIRE.
- 14. WATER SERVICE PASSING THROUGH FOUNDATION WALL TO BE SLEEVED AS REQUIRED.

16. ALL EXISTING SERVICES NOT TO BE USED SHALL BE BLANKED AT THE

MAIN, TO THE SATISFACTION OF THE CITY.

15. IF TEMPORARY WATER SUPPLY IS SPECIFIED IN THE CONTRACT DOCUMENTS, THE CONTRACTOR SHALL COORDINATE WITH THE CITY AND PROVIDE TEMPORARY SERVICING AT THEIR OWN EXPENSE.

### GENERAL NOTES

- 1. THE ORIGINAL TOPOGRAPHY, GROUND ELEVATION AND SURVEY DATA SHOWN ARE SUPPLIED FOR INFORMATION PURPOSES. ONLY, AND IMPLY NO GUARANTEE OF ACCURACY, IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY ALL INFORMATION SHOWN. THE PLANS ARE GEODETICALLY REFERENCED AT NAD83 ZONE 9. METRE: QUEBEC AND ONTARIO 78-75
- THIS PLAN IS NOT A CADASTRAL SURVEY SHOWING LEGAL PROPERTY BOUNDARIES AND EASEMENTS. THE PROPERTY BOUNDARIES SHOWN HEREON HAVE BEEN DERIVED INFORMATION SUPPLIED BY FARLEY, SMITH AND DENNIS SURVEYING LTD. (JOB NO. 432-75) AND CANNOT BE RELIED UPON TO BE ACCURATE OR COMPLETE. THE PRECISE LOCATION OF THE CURRENT PROPERTY BOUNDARIES AND EASEMENTS CAN ONLY BE DETERMINED BY AN UP-TO-DATE LAND TITLES SEARCH AND A SUBSEQUENT CADASTRAL SURVEY PERFORMED AND CERTIFIED BY AN ONTARIO LAND SURVEYOR.
- 3. THE CONTRACTOR IS TO OBTAIN AND PAY FOR ALL NECESSARY PERMITS AND APPROVALS FROM THE CITY BEFORE COMMENCING CONSTRUCTION.
- 4. THE CONTRACTOR IS RESPONSIBLE FOR ALL LAYOUT.

DIRECTED BY THE ENGINEER AND THE CITY.

- 5. THE CONTRACTOR IS TO DETERMINE THE EXACT LOCATION, SIZE, MATERIAL AND ELEVATION OF ALL EXISTING UTILITIES PRIOR TO COMMENCING CONSTRUCTION. PROTECT AND ASSUME ALL RESPONSIBILITY FOR EXISTING UTILITIES WHETHER OR NOT SHOWN ON THESE DRAWINGS. IF THERE IS ANY DISCREPANCY THE CONTRACTOR IS TO NOTIFY THE ENGINEER PROMPTLY
- 6. RESTORE ALL TRENCHES AND SURFACES OF PUBLIC ROAD ALLOWANCES TO CONDITION EQUAL OR BETTER THAN ORIGINAL
- CONDITION AND TO THE SATISFACTION OF THE CITY AUTHORITIES. 7. EXCAVATE AND DISPOSE OF ALL EXCESS EXCAVATED MATERIAL, SUCH AS ASPHALT, CURBING AND DEBRIS, OFF SITE AS
- 8. ALL DISTURBED AREAS TO BE RESTORED TO ORIGINAL CONDITION OR BETTER UNLESS OTHERWISE SPECIFIED.
- 9. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL TRAFFIC CONTROL AND SAFETY MEASURES DURING THE CONSTRUCTION
- PERIOD, INCLUDING THE SUPPLY, INSTALLATION, AND REMOVAL OF ALL NECESSARY SIGNAGE, DELINEATORS, MARKERS AND
- 10. DO NOT ALTER GRADING OF THE SITE WITHOUT PRIOR APPROVAL OF THE ENGINEER/CITY.
- 11. ALL ROADWAY, PARKING LOT, AND GRADING WORKS TO BE UNDERTAKEN IN ACCORDANCE WITH CITY STANDARDS AND SPECIFICATIONS. THE CONTRACTOR IS TO PROVIDE POSITIVE DRAINAGE AWAY FROM THE BUILDING.
- 12. CONTACT THE CITY FOR INSPECTION OF ROUGH GRADING OF PARKING LOTS. ROADWAYS AND LANDSCAPED AREAS PRIOR TO PLACEMENT OF ASPHALT AND TOPSOIL. ALL DEFICIENCIES NOTED SHALL BE RECTIFIED TO THE CITY'S SATISFACTION PRIOR TO PLACEMENT OF ANY ASPHALT, TOPSOIL, SEED & MULCH AND/OR SOD.
- 13. ALL DIMENSIONS AND INVERTS MUST BE VERIFIED PRIOR TO CONSTRUCTION, IF THERE IS ANY DISCREPANCY THE CONTRACTOR IS TO NOTIFY THE ENGINEER PROMPTLY.
- 14. ELECTRICAL, GAS, TELEPHONE AND TELEVISION SERVICE LOCATIONS ARE SUBJECT TO THE INDIVIDUAL AGENCY: • ELECTRICAL SERVICE - HYDRO OTTAWA, GAS SERVICE - ENBRIDGE,
  TELEPHONE SERVICE - BELL CANADA,
- TELEVISION SERVICE ROGERS. 16. INSTALLATION TO BE IN ACCORDANCE WITH CURRENT CODES AND STANDARDS OF APPROVAL AGENCIES HYDRO OTTAWA, BELL AND THE CITY.
- 17. CONTRACTOR TO ENSURE ALL APPLICABLE OPS SPECIFICATIONS ARE FOLLOWED DURING CONSTRUCTION.
- 18. ALL PROPOSED CURB TO BE CONCRETE BARRIER CURB UNLESS OTHERWISE SPECIFIED.
- 19. THIS PLAN MUST BE READ IN CONJUNCTION WITH THE GEOTECHNICAL INVESTIGATION.
- 20. THE PRIVATE SANITARY AND STORM SERVICE LATERALS ARE TO BE REGULARLY MAINTAINED & INSPECTED, ALL ASSOCIATED COSTS ARE TO BE BORNE BY THE OWNER. THE CITY OF OTTAWA WILL NOT BE RESPONSIBLE FOR ANY COMPLICATIONS WHICH MAY ARISE DUE TO THE CONFIGURATIONS OF THE PRIVATE SERVICE LATERALS.
- 21. CONTRACTOR TO PROVIDE ALL UTILITY LOCATES FOR UNDERGROUND WORK, INCLUDING BOTH PUBLIC AND PRIVATE
- 22. CONTRACTOR SHALL HAND-DIG AROUND EXISTING UTILITIES TO AVOID DAMAGE.
- 23. CONTRACTOR TO ASSUME ALL LIABILITY WHEN ORDERING STRUCTURES PRIOR TO CONFIRMING INVERTS.



LEGEND

LIMIT OF CONSTRUCTION — -- PROPERTY LINE \_\_ CONCRETE BARRIER ----- DRAINAGE SWALE CONCRETE WALKWAY — — — DRAINAGE DITCH SLOPING AT 3:1
UNLESS SPECIFIED SURFACE ELEVATION SWALE ELEVATION TOP OF WALL ELEVATION BOTTOM OF WALL ELEVATION OVERLAND FLOW ROUTE MH#A SANITARY SEWER MANHOLE

SILT FENCE BARRIER STRAW BALE CHECK DAM

WATER VALVE ROOF DRAIN

PROPOSED SLOPE

1.0%

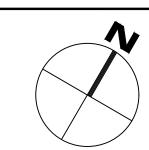
MUD MAT EXIT/ENTRY LOCATION

**\*------**

09	REISSUED PER CITY COMMENTS	08/20/2025
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07	ISSUED FOR SUBMISSION	05/14/2025
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03	ISSUED FOR SUBMISSION	12/10/2024
02	ISSUED FOR RE-ZONING	08/28/2023
01	ISSUED FOR REVIEW	08/24/2023
No.	Revisions	Date

before proceeding with the work SCALE 1:100





Check and verify all dimensions

J. J. BURDEN 100534259

Do not scale drawings

CSV ARCHITECTS 190 O'CONNOR STREET, SUITE 100 OTTAWA, ON, K2P 2R3

RESIDENTIAL BUILDING 214 SOMERSET ST E

OTTAWA

SITE SERVICING PLAN

				9
Scale:	1:100	Project Number:		5-(
Drawn By:	R.P.		CCO-24-0450	2-5
Checked By:	A.B.	Drawing Number:		7-1
Designed By:			C102	0

# CROSSING CONFLICT TABLE

1 250mmØ SAN SEWER OBV 59.69 150mmØ STM SERVICE INV 60.41 2 400mmØ WTR MAIN OBV 59.95 150mmØ STM SERVICE INV 60.45 3 150mmØ SAN SERVICE OBV 59.82 4 000mmØ WTR MAIN INV 60.32 250mmØ SAN SEWER OBV 59.67 150mmØ STM SERVICE INV 60.39 400mmØ WTR MAIN OBV 59.93 150mmØ STM SERVICE INV 60.43 6 150mmØ SAN SERVICE INV 60.43 150mmØ SAN SERVICE INV 60.43 150mmØ STM SERVICE INV 61.02 1.13	LOCATION	DESCRIPTION	SEPARATION
150mmØ STM SERVICE INV 60.41 400mmØ WTR MAIN OBV 59.95 150mmØ STM SERVICE INV 60.45 150mmØ SAN SERVICE OBV 59.82 400mmØ WTR MAIN INV 60.32 250mmØ SAN SEWER OBV 59.67 150mmØ STM SERVICE INV 60.39 400mmØ WTR MAIN OBV 59.93 150mmØ STM SERVICE INV 60.43 150mmØ STM SERVICE INV 60.43 150mmØ SAN SERVICE INV 60.43 150mmØ SAN SERVICE INV 61.02	1	250mmØ SAN SEWER OBV 59.69	0.72
150mmØ STM SERVICE INV 60.45 150mmØ SAN SERVICE OBV 59.82 400mmØ WTR MAIN INV 60.32 250mmØ SAN SEWER OBV 59.67 150mmØ STM SERVICE INV 60.39 400mmØ WTR MAIN OBV 59.93 150mmØ STM SERVICE INV 60.43 150mmØ SAN SERVICE OBV 59.89 150mmØ SAN SERVICE INV 61.02	1		0.72
150mmØ STM SERVICE INV 60.45 150mmØ SAN SERVICE OBV 59.82 400mmØ WTR MAIN INV 60.32 250mmØ SAN SEWER OBV 59.67 150mmØ STM SERVICE INV 60.39 400mmØ WTR MAIN OBV 59.93 150mmØ STM SERVICE INV 60.43 150mmØ SAN SERVICE OBV 59.89 150mmØ SAN SERVICE INV 61.02	2	400mmØ WTR MAIN OBV 59.95	0.50
4 400mmØ WTR MAIN INV 60.32 250mmØ SAN SEWER OBV 59.67 0.72 150mmØ STM SERVICE INV 60.39 400mmØ WTR MAIN OBV 59.93 0.50 150mmØ STM SERVICE INV 60.43 150mmØ SAN SERVICE OBV 59.89 150mmØ STM SERVICE INV 61.02	2		0.50
4 250mmØ WTR MAIN INV 60.32 250mmØ SAN SEWER OBV 59.67 150mmØ STM SERVICE INV 60.39 400mmØ WTR MAIN OBV 59.93 150mmØ STM SERVICE INV 60.43 150mmØ SAN SERVICE OBV 59.89 150mmØ STM SERVICE INV 61.02	2	150mmØ SAN SERVICE OBV 59.82	0.50
5 150mmØ STM SERVICE INV 60.39 400mmØ WTR MAIN OBV 59.93 150mmØ STM SERVICE INV 60.43 150mmØ SAN SERVICE OBV 59.89 150mmØ STM SERVICE INV 61.02	5	400mmØ WTR MAIN INV 60.32	0.50
150mmØ STM SERVICE INV 60.39 400mmØ WTR MAIN OBV 59.93 150mmØ STM SERVICE INV 60.43 150mmØ SAN SERVICE OBV 59.89 150mmØ STM SERVICE INV 61.02	1		0.72
6 150mmØ STM SERVICE INV 60.43 150mmØ SAN SERVICE OBV 59.89 150mmØ STM SERVICE INV 61.02	4	150mmØSTM SERVICE INV 60.39	0.72
150mmØ STM SERVICE INV 60.43 150mmØ SAN SERVICE OBV 59.89 150mmØ STM SERVICE INV 61.02	5		0.50
6 150mmØ STM SERVICE INV 61.02	<u> </u>		0.50
150mmØ STM SERVICE INV 61.02	6	·	1 13
1 100	0	150mmØ STM SERVICE INV 61.02	1.13
1 / 1 1 193	7	100mmØ WTR SERVICE OBV 60.08	0.93
150mmØ STM SERVICE INV 61.01	/	150mmØ STM SERVICE INV 61.01	0.55

WATER COVER TABLE					
LOCATION	STATION	FINISHED GRADE	TOP OF PIPE	COVER	
A - 400 X 150 TEE	0+000.00	62.50	60.10	2.40	
VALVE	0+004.98	62.44	60.04	2.40	
BIIIIDING	0+007.66	61.76	59.95	1 21	

BUILDING | 0+007.00 | 01.70 | 59.95 | 1.81 | ON

APPENDIX C WATERMAIN CALCULATIONS

### CCO-24-0450 - 214 Somerset St E - Water Demands

 Project:
 214 Somerset St E

 Project No.:
 CCO-24-0450

 Designed By:
 RP

 Checked By:
 AB

 Date:
 August 2, 2023

 Site Area:
 0.05 gross ha

Residential NUMBER OF UNITS UNIT RATE Single Family homes 3.4 persons/unit Semi-detached 2.7 persons/unit homes 2.7 persons/unit Townhouse homes Bachelor Apartment units 1.4 persons/unit 1 Bedroom Apartment 23 units persons/unit 2 Bedroom Apartment units 2.1 persons/unit 3 Bedroom Apartment units 3.1 persons/unit Average Apartment units 1.8 persons/unit

Total Population 33 persons

 Commercial
 71 m2

 Industrial - Light
 m2

 Industrial - Heavy
 m2

#### AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	]
Residential	280	L/c/d	1
Industrial - Light	35,000	L/gross ha/d	
Industrial - Heavy	55,000	L/gross ha/d	
Shopping Centres	2,500	L/(1000m² /d	
Hospital	900	L/(bed/day)	
Schools	70	L/(Student/d)	
Trailer Park with no Hook-Ups	340	L/(space/d)	
Trailer Park with Hook-Ups	800	L/(space/d)	
Campgrounds	225	L/(campsite/d)	
Mobile Home Parks	1,000	L/(Space/d)	
Motels	150	L/(bed-space/d)	
Hotels	225	L/(bed-space/d)	
Tourist Commercial	28,000	L/gross ha/d	
Other Commercial	28,000	L/gross ha/d	
	Residential	0.11	L/s
AVERAGE DAILY DEMAND	Commercial/Industrial		
	/Institutional	0.00	L/s

### MAXIMUM DAILY DEMAND

DEMAND TYPE	Į.	AMOUNT	UNITS
Residential	9.5	x avg. day	L/c/d
Industrial	1.5	x avg. day	L/gross ha/d
Commercial	1.5	x avg. day	L/gross ha/d
Institutional	1.5	x avg. day	L/gross ha/d
	Residential	1.02	L/s
MAXIMUM DAILY DEMAND	Commercial/Industrial		
	/Institutional	0.00	L/s

### MAXIMUM HOUR DEMAND

DEMAND TYPE	Į.	AMOUNT	UNITS
Residential	14.3	x avg. day	L/c/d
Industrial	1.8	x max. day	L/gross ha/d
Commercial	1.8	x max. day	L/gross ha/d
Institutional	1.8	x max. day	L/gross ha/d
	Residential	1.53	L/s
MAXIMUM HOUR DEMAND (	Commercial/Industrial		
	/Institutional	0.01	L/s

WATER DEMAND DESIGN FLOWS PER UNIT COUNT
CITY OF OTTAWA - WATER DISTRIBUTION GUIDELINES, JULY 2010

AVERAGE DAILY DEMAND	0.11	L/s
MAXIMUM DAILY DEMAND	1.02	L/s
MAXIMUM HOUR DEMAND	1.54	L/s

### CCO-24-0450 - 214 Somerset St E - OBC Fire Calculations

Project: 214 Somerset St E Project No.: CCO-24-0450 Designed By: RP Checked By: RRR Date: August 2, 2023

Ontario 2006 Building Code Compendium (Div. B - Part 3)

Water Supply for Fire-Fighting - Residential Building

Building is classified as Group:

(from table 3.2.2.55)

\*approximate distances

Building is of combustible construction. Floor assemblies are fire separations but with no fire-resistance ratings. Roof assemblies, mezzanies, loadbearing walls, columns and arches do not have a fire-resistance rating.

From Div. B A-3.2.5.7. of the Ontario Building Code - 3. Building On-Site Water Supply:

(a)  $Q = K \times V \times Stot$ 

#### where:

Q = minimum supply of water in litres

K = water supply coefficient from Table 1

V = total building volume in cubic metres

Stot = total of spatial coefficient values from the property line exposures on all sides as obtained from the formula:

Stot = 1.0 + [Sside1+Sside2+Sside3+...etc.]

K	23	(from Table 1 pg A-31) (Worst case occupancy {E / F2} 'K' value used)			From Figur
V	3,025	(Total building volume in m <sup>3</sup> .)			1 (A-32)
Stot	2.0	(From figure 1 pg A-32 )	Snorth	2.5	m 0.5
Q =	139,150.0	) L	Seast	1.5	m 0.5
			Ssouth	2.1	m 0.5
From Table 2: Required Minimum	Water Supply Flor	/ Rate (L/s)	Swest	1.5	m 0.5

if Q > 135.000 L and < 162.000 L 4500 L/min 1189 gpm

### CP-24-0450 - 214 Somerset St E - Fire Underwriters Survey

 Project:
 214 Somerset St E

 Project No.:
 CP-24-0450

 Designed By:
 RP

 Checked By:
 AB

 Date:
 August 2, 2023

#### From the Fire Underwriters Survey (2020)

From Part II – Guide for Determination of Required Fire Flow Copyright I.S.O.: City of Ottawa Technical Bulletin ISTB-2018-02 Applied Where Applicable

#### A. BASE REQUIREMENT (Rounded to the nearest 1000 L/min)

F = 220 x C x vA Where:

F = Required fire flow in liters per minute

C = Coefficient related to the type of construction.

A = The total floor area in square meters (including all storey's, but excluding basements at least 50 percent below grade) in the

-15%

building being considered.

Construction Type Ordinary Construction

1 A 1,235.0 m<sup>2</sup>

Total Floor Area (per the 2020 FUS Page 20 - Total Effective Area) 1,235.0 m<sup>2</sup> \*Unprotected Vertical Openings

Calculated Fire Flow 7,731.4 L/min

B. REDUCTION FOR OCCUPANCY TYPE (No Rounding) From Page 24 of the Fire Underwriters Survey:

Limited Combustible

Fire Flow 6,800.0 L/min

C. REDUCTION FOR SPRINKLER TYPE (No Rounding)

Non-Sprinklered 0%

R	eduction			0.0	L/min		
D. INCR	EASE FOR EXPOSURE (No Roundi	ng)					
	Separation Distance (m)	Cons.of Exposed Wall	Length Exposed Adjacent Wall (m)	Height (Stories)	Length-Height Factor		
Exposure 1	3.1 to 10	Fire Resistive - Non Combustible (Unprotected Openings)	10.6	2	21.2	7%	
Exposure 2	20.1 to 30	Wood frame	9.1	2	18.2	0%	
Exposure 3	0 to 3	Fire Resistive - Non Combustible (Unprotected Openings)	10.22	3	30.7	11%	
Exposure 4	20.1 to 30	Fire Resistive - Non Combustible (Unprotected Openings)	13.8	3	41.4	1%	
					% Increase*	19%	

ncrease\* 1,292.0 L/min

E. Total Fire Flow (Rounded to the Nearest 1000 L/min)

Fire Flow 8,092.0 L/min
Fire Flow Required\*\* 8,000.0 L/min

<sup>\*</sup>In accordance with Part II, Section 4, the Increase for separation distance is not to exceed 75%

 $<sup>^{\</sup>star\star} \text{In accordance with Section 4 the Fire flow is not to exceed } 45,000 \, \text{L/min or be less than 2,000 L/min}$ 

### CCO-24-0450 - 214 Somerset St E - Boundary Condition Unit Conversion

Project: 214 Somerset St E

Project No.: CCO-24-0450

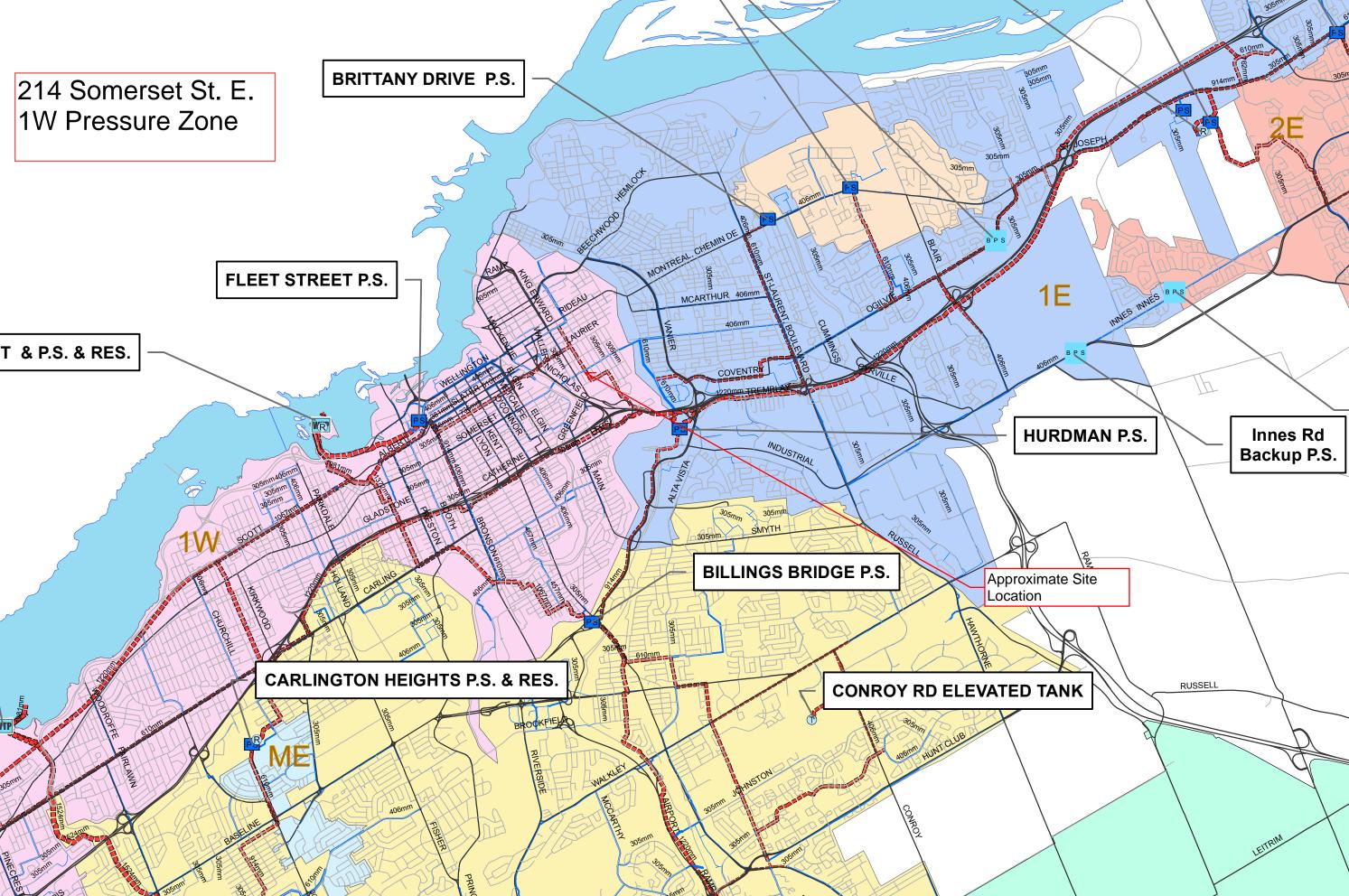
Designed By: RP Checked By: AB

Date: August 11, 2023

### **Boundary Conditions Unit Conversion**

### Somerset St E

Scenario	Height (m)	Elevation (m)	m H₂O	PSI	kPa
Avg. DD	115.3	60.0	55.3	78.7	542.5
Fire Flow (75 L/s or 4500 L/min)	109.1	60.0	49.1	69.9	481.7
Peak Hour	106.0	60.0	46.0	65.4	451.3



# 214 Somerset St. E. Hydrant Cover Figure

### 4 Hydrants present within 75m



# APPENDIX D SANITARY CALCULATIONS

### CCO-24-0450 - 214 Somerset St E - Sanitary Demands

Project: Project No.:	214 Somerset St E CCO-24-0450
Designed By:	R.P.
Checked By:	C.M.
Date:	October 2, 2024
Site Area 1 Bedroom	0.05 Gross ha 23 1.40 Persons per unit
Total Population	33 Persons
Commercial Area	0.00 m <sup>2</sup>
Amenity Space	71.31 m <sup>2</sup>

#### DESIGN PARAMETERS

Institutional/Commercial Peaking Factor

Residential Peaking Factor 3.68 \* Using Harmon Formula =  $1+(14/(4+P^0.5))*0.8$ 

where P = population in thousands, Harmon's Correction Factor = 0.8

 Mannings coefficient (n)
 0.013

 Demand (per capita)
 280
 L/day

 Infiltration allowance
 0.33
 L/s/Ha

### EXTRANEOUS FLOW ALLOWANCES

Infiltration / Inflow	Flow (L/s)
Dry	0.00
Wet	0.02
Total	0.02

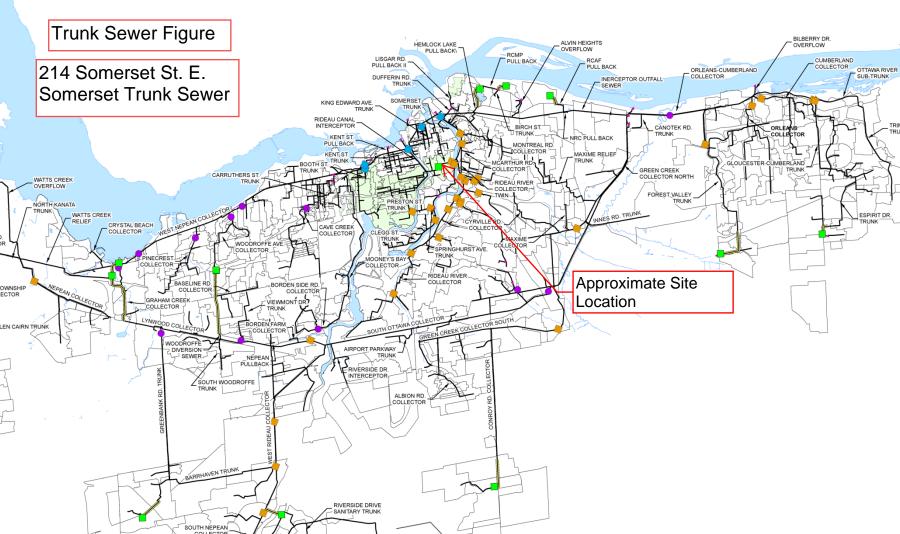
#### AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	POPULATION / AREA	Flow (L/s)
Residential	280	L/c/d	33	0.11
Industrial - Light**	35,000	L/gross ha/d		0
Industrial - Heavy**	55,000	L/gross ha/d		0
Commercial / Amenity	2,800	L/(1000m² /d )	71.31	0.002
Hospital	900	L/(bed/day)		0
Schools	70	L/(Student/d)		0
Trailer Parks no Hook-Ups	340	L/(space/d)		0
Trailer Park with Hook-Ups	800	L/(space/d)		0
Campgrounds	225	L/(campsite/d)		0
Mobile Home Parks	1,000	L/(Space/d)		0
Motels	150	L/(bed-space/d)		0
Hotels	225	L/(bed-space/d)		0
Office	75	L/7.0m <sup>2</sup> /d		0
Tourist Commercial	28,000	L/gross ha/d		0
Other Commercial	28,000	L/gross ha/d		0

AVERAGE RESIDENTIAL FLOW	0.11	L/s
PEAK RESIDENTIAL FLOW	0.39	L/s
	·	·
AVERAGE ICI FLOW	0.002	L/s
PEAK INSTITUTIONAL/COMMERCIAL FLOW	0.003	L/s
PEAK INDUSTRIAL FLOW	0.000	L/s
TOTAL PEAK ICI FLOW	0.003	L/s

### TOTAL SANITARY DEMAND

TOTAL ESTIMATED AVERAGE DRY WEATHER FLOW	0.11	L/s
TOTAL ESTIMATED PEAK DRY WEATHER FLOW	0.40	L/s
TOTAL ESTIMATED PEAK WET WEATHER FLOW	0.41	L/s



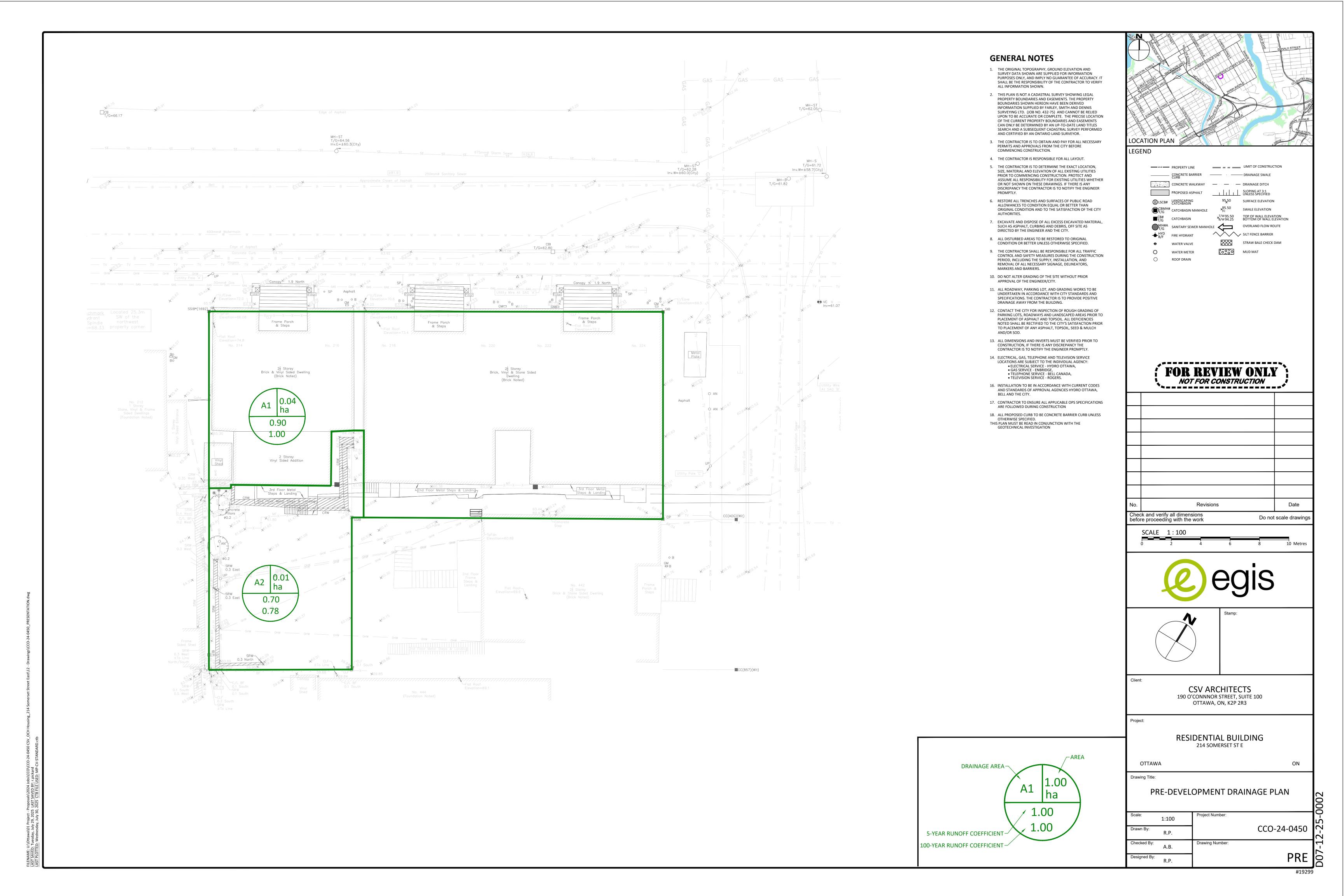
### SANITARY SEWER DESIGN SHEET

PROJECT:

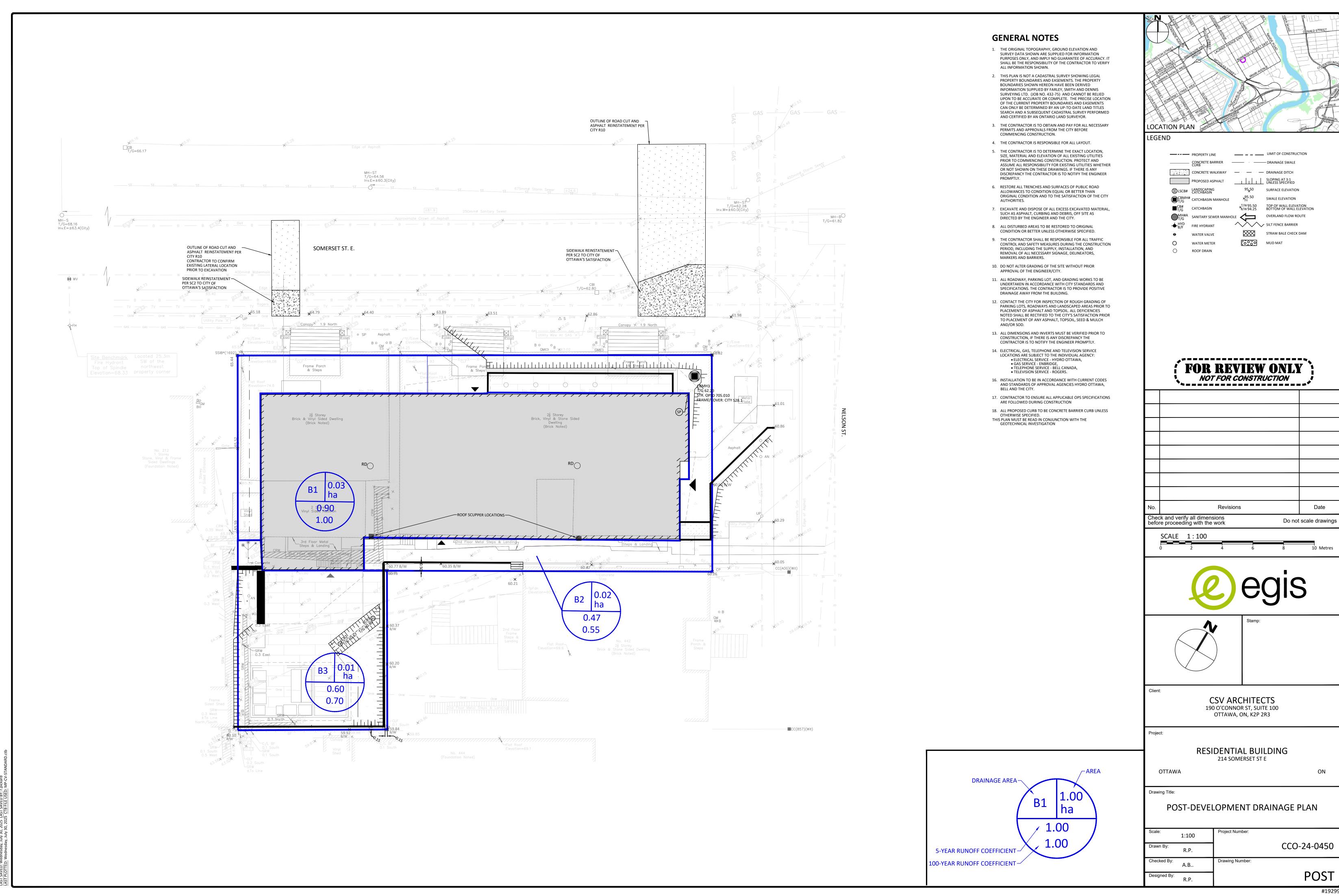
LOCATION:
CLIENT: 214 Somerset
CSV Architects

	LOC	ATION							RESIDENTIA	L							ICI AREAS				INFILTR	ATION ALLC	WANCE	FLOW				SEWER DAT	А		
1	2		3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
						UNIT	TYPES	•	AREA	POPU	LATION		PEAK			ARE	A (ha)	•		PEAK	ARE.	A (ha)	FLOW	DESIGN	CAPACITY	LENGTH	DIA	SLOPE	VELOCITY	AVAI	LABLE
STREET	AREA	ID	FROM	TO	1-Bed	2-Bed	APT	TH	(ha)	IND	CUM	PEAK	FLOW	INSTITU	JTIONAL	COMN	1ERCIAL	INDU	STRIAL	FLOW	IND	CUM	(L/s)	FLOW	(L/s)	(m)	(mm)	(%)	(full)	CAPA	ACITY
			MH	MH	1-beu	z-beu	AFI	1111	(Ha)	IND	COIVI	FACTOR	(L/s)	IND	CUM	IND	CUM	IND	CUM	(L/s)	IIVD	COIVI	(L/3)	(L/s)	(L/3)	(111)	(111111)	(70)	(m/s)	L/s	(%)
Somerset St E	A-1		Duilding	N 41 11 A	22				0.05	32.2	22.2	270	0.20	0.01	0.01		0.00		0.00	0.003	0.05	0.05	0.02	0.41	15.89	0.30	150	1.00	0.87	15 40	07.45
		-	Building	MH1A	23			1			32.2	3.68	0.38				0.00				0.05						150	1.00		15.48	97.45
Somerset St E	A-2		MH1A	East Service	23				0.05	32.2	32.2	3.68	0.38	0.01	0.01		0.00		0.00	0.003	0.06	0.06	0.02	0.41	11.23	16.50	150	0.50	0.62	10.83	96.38
Somerset St E	A-2		Building	Connection	23				0.05	32.2	32.2	3.68	0.38	0.01	0.01		0.00		0.00	0.003	0.06	0.06	0.02	0.41	11.23	8.90	150	0.50	0.62	10.83	96.38
Design Parameters:				<u>.</u>	Notes:	<u> </u>	1		1	ļ		Designed:	ļ	RP	<u> </u>	<u> </u>	No.					Revision		L		L			Date		
					1. Mannir	ngs coefficien	nt (n) =		0.013								1.				Ci	ty Submissio	on						5/13/2025		
Residential		ļ	ICI Areas		2. Deman	nd (per capita	):	280	) L/day																						
1-Bed 1.4 p/p/u	-			Peak Factor	3. Infiltrat	tion allowand	ce:	0.33	3 L/s/Ha			Checked:		AB																	
2-Bed 2.1 p/p/u	INST	28,000 L	L/Ha/day	1.5	4. Resider	ntial Peaking	Factor:																								
APT 1.8 p/p/u	COM	28,000 L	L/Ha/day	1.5		Harmon Fo	ormula = 1+(	14/(4+P^0.5	(8.0*(																						
Other 60 p/p/Ha	IND	35,000 L	L/Ha/day	MOE Chart		where P =						Project No.	.:	CCO-24-04	50																-
																													Sheet No:		
																													1 of 1		

# APPENDIX E PRE-DEVELOPMENT DRAINAGE PLAN



# APPENDIX F POST-DEVELOPMENT DRAINAGE PLAN



# APPENDIX G STORMWATER MANAGEMENT CALCULATIONS

#### CO-24-0450 - 214 Somerset St E - SWM Calculations

1	of

Tc (min)		Intensity (mm/hr)		
(11111)	2-Year	5-Year	100-Year	
10	76.5	104.2	178.6	PRE-DEVELOPMENT
10	76.5	104.2	178.6	POST-DEVELOPMENT

C-Values									
Impervious	0.90								
Gravel/Pavers	0.60								
Pervious	0.20								

### Pre-Development Runoff Coefficient

Drainage Area	Impervious Area (m²)	Gravel (m²)	Pervious Area (m²)	Average C (2-year)	Average C (5-year)	Average C (100-year)
A1	403	0	0	0.90	0.90	1.00
A2	94	0	38	0.70	0.70	0.78

#### Pre-Development Runoff Calculations

Drainage	Area	С	C	C	Tc		Q (L/s)			
Area	(ha)	2-Year	5-Year	100-Year	(min)	2-Year	5-Year	100-Year		
A1	0.040	0.90	0.90	1.00	10	7.71	10.50	20.00		
A2	0.013	0.70	0.70	0.78	10	1.96	2.67	5.13		
Total	0.05					9.67	13.17	25.12		

#### Post-Development Runoff Coefficient

Drainage Area	Impervious Area (m²)	Gravel/Permeable Pavers (m²)	Pervious Area (m²)	Average C (2-year)	Average C (5-year)	Average C (100-year)
B1	276	0	0	0.90	0.90	1.00
B2	46	22	86	0.47	0.47	0.55
B3	48	21	35	0.60	0.60	0.70

#### Post-Development Runoff Calculations

Droipogo		C	C	C	To	Q (L/s)		
Drainage Area	Area (ha)	2-Year	5-Year	100-Year	Tc (min)		Q (L/S)	
Aica	(ria)	Z Tour	5 rear	100 Teal	(11111)	2-Year	5-Year	100-Year
B1	0.028	0.90	0.90	1.00	10	5.28	7.19	13.69
B2	0.015	0.47	0.47	0.55	10	1.53	2.08	4.17
B3	0.010	0.60	0.60	0.70	10	1.34	1.82	3.60
Total	0.05					8.15	11.09	21.47

Restricted Unrestricted to ROWs Unrestricted rear yard

#### Required Restricted Flow

Drainage	Area	С	С	С	Tc		Q (L/s)		
Area	(ha)	2-Year	5-Year	100-Year	(min)	2-Year	5-Year	100-Year	
A1	0.040	0.50	0.50	0.50	10	4.28	5.83	10.00	Toward ROW
A2	0.013	0.70	0.70	0.78	10	1.96	2.67	5.13	Rear Yard Runoff
Total	0.05					6.24	8.50	15.12	

### Post-Development Restricted Runoff Calculations

Drainage	Unrestricted Flow		Restricted Flow		Storage Required (m³)		Storage Provided (m³)					
Area	2-year	5-year	100-Year	2-Year	5-Year	100-Year	2-Year	5-Year	100-Year	2-Year	5-Year	100-Year
Directed to City of Ottawa ROW												
B1	5.28	7.19	13.69	0.60	0.72	1.32	4.0	5.6	10.8	5.2	6.2	11.3
B2	1.53	2.08	4.17	1.53	2.08	4.17						
Total Toward ROW	6.81	9.27	17.87	2.13	2.80	5.49	4.00	5.65	10.77	5.16	6.19	11.34
B3	1.34	1.82	3.60	1.34	1.82	3.60						
Total	8.15	11.09	21.47	3.47	4.62	9.09	4.00	5.65	10.77	5.16	6.19	11.34

<sup>\*</sup>Overall Post-Development runoff is approximately 35% of Pre-Development, the section directed toward the ROWs is below the pre-development 5-year flow with C=0.5 \*Post-Development rear-yard runoff is less than Pre-Development conditions.

### CO-24-0450 - 214 Somerset St E - SWM Calculations

Storage Requirements for Area B1

2 of 4

#### 2-Year Storm Event

Tc (min)	l (mm/hr)	Runoff (L/s) B1	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
10	76.8	5.30	0.60	4.70	2.82
30	40.0	2.76	0.60	2.16	3.89
50	28.0	1.93	0.60	1.33	4.00
70	21.9	1.51	0.60	0.91	3.83
90	18.1	1.25	0.60	0.65	3.51
	Maximum S	Storage Regui	red 5-year =	4.0	$m^3$

#### 5-Year Storm Event

Tc (min)	l (mm/hr)	Runoff (L/s) B1	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
10	104.2	7.19	0.72	6.47	3.88
30	53.9	3.72	0.72	3.00	5.40
50	37.7	2.60	0.72	1.88	5.65
70	29.4	2.03	0.72	1.31	5.50
90	24.3	1.68	0.72	0.96	5.17
	Mavimum	torogo Dogui	rod E voor	E 4	3

#### 100-Year Storm Even

Tc (min)	l (mm/hr)	Runoff (L/s) B1	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
10	178.6	13.70	1.32	12.38	7.43
20	120.0	9.20	1.32	7.88	9.46
30	91.9	7.05	1.32	5.73	10.31
40	75.1	5.76	1.32	4.44	10.66
50	64.0	4.91	1.32	3.59	10.77
60	55.9	4.29	1.32	2.97	10.68
70	49.8	3.82	1.32	2.50	10.50
80	45.0	3.45	1.32	2.13	10.23
90	41.1	3.15	1.32	1.83	9.89
100	37.9	2.91	1.32	1.59	9.52

Maximum Storage Required 100-year = 10.8 m<sup>3</sup>

2-Year Storm Event Storage Summary

Roof Storage								
Location	Area*	Depth	Volume (m³)					
Roof	206.25	0.025	5.16					

5-Year Storm Event Storage Summary

Roof Storage									
Location	Area*	Depth	Volume (m³)						
Roof	206.25	0.030	6.19						

100-Year Storm Event Storage Summary

Roof Storage								
Location	Area*	Depth	Volume (m³)					
Roof	206.25	0.055	11.34					

\*Area is 75% of the total roof area

Storage Available (m³) =	5.16
Storage Required (m³) =	4.00

Storage Available (m³) =	6.19
Storage Required (m <sup>3</sup> ) =	5.65

Storage Available (m³) =	11.34
Storage Required (m3) =	10.77

### CO-24-0450 - 214 Somerset St E - SWM Calculations

### Roof Drain Flow (B1)

Roof Drains Summary								
Type of Control Device	Watts Drainage - Accutrol Weir							
Number of Roof Drains	2							
	2-Year 5-Year 100-Year							
Rooftop Storage (m <sup>3</sup> )	5.16	6.19	11.34					
Storage Depth (m)	0.025	0.030	0.055					
Flow (Per Roof Drain) (L/s)	0.30	0.36	0.66					
Total Flow (L/s)	0.60	0.72	1.32					

Flow Rate Vs. Build-Up (One Weir)					
Depth (mm)	Flow (L/s)				
15	0.18				
20	0.24				
25	0.30				
30	0.36				
35	0.42				
40	0.48				
45	0.54				
50	0.60				
55	0.66				

<sup>\*</sup>Roof Drain model to be Accutrol Weirs, See attached sheets
\*Roof Drain Flow information taken from Watts Drainage website

### **CALCULATING ROOF FLOW EXAMPLES**

1 roof drain during a 5 year storm elevation of water = 25mm Flow leaving 1 roof drain = (1 x 0.30 L/s) = 0.30 L/s

1 roof drain during a 100 year storm elevation of water = 50mm Flow leaving 1 roof drain = (1 x 0.60 L/s) = 0.60 L/s

4 roof drains during a 5 year storm elevation of water = 25mm Flow leaving 4 roof drains = (4 x 0.30 L/s) = 1.20 L/s

4 roof drains during a 100 year storm elevation of water = 50mm Flow leaving 4 roof drains = (4 x 0.60 L/s) = 2.40 L/s

	Roof Drain Flo	DW
Flow (I/s)	Storage Depth (mm)	Drains Flow (I/s)
0.18	15	0.36
0.24	20	0.48
0.30	25	0.60
0.36	30	0.72
0.42	35	0.84
0.48	40	0.96
0.54	45	1.08
0.60	50	1.20
0.66	55	1.32
0.72	60	1.44
0.78	65	1.56
0.84	70	1.68
0.90	75	1.80
0.96	80	1.92
1.02	85	2.04
1.08	90	2.16
1.14	95	2.28
1.20	100	2.40
1.26	105	2.52
1.32	110	2.64
1.38	115	2.76
1.44	120	2.88
1.50	125	3.00
1.56	130	3.12
1.62	135	3.24
1.68	140	3.36
1.74	145	3.48
1.80	150	3.60

3 of 4

Note: The flow leaving through a restricted roof drain is based on flow vs. head information

### CO-24-0450 - 214 Somerset St E - SWM Calculations

4 of 4

### Time of Concentration Pre-Development

Drainage Area	Sheet Flow	Slope of	Tc (min)	Tc (min)
ID	Distance (m)	Land (%)	(5-Year)	(100-Year)
A1	35	10.00	2	1

Therefore, a Tc of 10 can be used

Tc= (3.26(1.1-c)L^0.5/S^0.33)

 $\begin{array}{ll} \text{C =} & \text{Balanced Runoff Coefficient} \\ \text{L =} & \text{Length of drainage area} \\ \text{S =} & \text{Average slope of watershed} \end{array}$ 

### STORM SEWER DESIGN SHEET

PROJECT:

214 Somerset St E LOCATION: CLIENT: CSV Architects

	LOCA	TION			CONTRIBUTING AREA (ha	a)						R.A	TIONAL DESIG	SN FLOW									SEWER DATA	A			
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28
STREET	AREA ID	FROM	TO	C-VALUE	AREA	INDIV	CUMUL	INLET	TIME	TOTAL (min)	i (5)	i (10)	i (100)	5yr PEAK	10yr PEAK	100yr PEAK	FIXED		CAPACITY	LENGTH	DIA	PIPE SIZE (mn	1)	SLOPE	VELOCITY	AVAIL (	CAP (5yr)
		MH	IVIH			AC	AC	(min)	IN PIPE	(min)	(mm/hr)	(mm/hr)	(mm/hr)	FLOW (L/s)	(L/S)	(m)	DIA	VV	Н	(%)	(m/s)	(L/S)	(%)				
Somerset St E	N/A	CBMH1	Connection	0.75	0.02	0.02	0.02	10.00	0.22	10.22	104.19	122.14	178.56	4.34	5.09	7.45		4.34	15.89	11.30	150			1.00	0.871	11.54	72.65%
Somerset St E	B1	Building	East Service	0.90	0.02	0.01	0.01	10.00	0.57	10.57	104.19	122.14	178.56	3.91	4.58	6.70		3.91	11.23	21.20	150			0.50	0.616	7.32	65.19%
Somerset St E	B1	Building	Connection	0.90	0.02	0.01	0.03	10.57	0.34	10.92	101.26	118.68	173.48	7.60	8.91	13.02		7.60	11.23	12.70	150			0.50	0.616	3.63	32.35%
Definitions:				Notes:				Designed:					No.				<u> </u>	Revision		<u> </u>					Date		
Q = 2.78CiA, where:				1. Mannings coefficient (n) =	=		0.013	_					1.				Ci	ty Submission							5/13/2025		
Q = Peak Flow in Litres p								R.P.																			
A = Area in Hectares (ha								Checked:																			
i = Rainfall intensity in n																											
[i = 998.071 / (TC+6.05		5 YEAR						A.B.																			
[i = 1174.184 / (TC+6.0		10 YEAR						Project No.:																			
[i = 1735.688 / (TC+6.0	014)^0.820]	100 YEAR						l									Dat								Sheet No:		
								CCO-23-045	0								2023.0	1.12							1 of 1		

# APPENDIX H CITY OF OTTAWA DESIGN CHECKLIST

### **City of Ottawa**

### 4. Development Servicing Study Checklist

The following section describes the checklist of the required content of servicing studies. It is expected that the proponent will address each one of the following items for the study to be deemed complete and ready for review by City of Ottawa Infrastructure Approvals staff.

The level of required detail in the Servicing Study will increase depending on the type of application. For example, for Official Plan amendments and re-zoning applications, the main issues will be to determine the capacity requirements for the proposed change in land use and confirm this against the existing capacity constraint, and to define the solutions, phasing of works and the financing of works to address the capacity constraint. For subdivisions and site plans, the above will be required with additional detailed information supporting the servicing within the development boundary.

### 4.1 General Content

Criteria	Location (if applicable)
☐ Executive Summary (for larger reports only).	N/A
☐ Date and revision number of the report.	On Cover
<ul> <li>Location map and plan showing municipal address, boundary, and layout of proposed development.</li> </ul>	Appendix A
☐ Plan showing the site and location of all existing services.	Site Servicing Plan (C102)
☐ Development statistics, land use, density, adherence to zoning and official plan, and reference to applicable subwatershed and	1.1 Purpose
watershed plans that provide context to which individual developments must adhere.	1.2 Site Description
	6.0 Stormwater Management
☐ Summary of pre-consultation meetings with City and other approval agencies.	Appendix B
☐ Reference and confirm conformance to higher level studies and reports (Master Servicing Studies, Environmental Assessments,	1.1 Purpose
Community Design Plans), or in the case where it is not in conformance, the proponent must provide justification and	1.2 Site Description
develop a defendable design criteria.	6.0 Stormwater Management
$\ \square$ Statement of objectives and servicing criteria.	3.0 Pre-Consultation Summary



☐ Identification of existing and proposed infrastructure available in the immediate area.	N/A
☐ Identification of Environmentally Significant Areas, watercourses and Municipal Drains potentially impacted by the proposed development (Reference can be made to the Natural Heritage Studies, if available).	Site Grading Plan (C101)
☐ Concept level master grading plan to confirm existing and proposed grades in the development. This is required to confirm the feasibility of proposed stormwater management and drainage, soil removal and fill constraints, and potential impacts to neighbouring properties. This is also required to confirm that the proposed grading will not impede existing major system flow paths.	Site Grading Plan (C101)
☐ Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts.	N/A
☐ Proposed phasing of the development, if applicable.	N/A
Reference to geotechnical studies and recommendations concerning servicing.	Section 2.0 Background Studies, Standards and References
<ul> <li>All preliminary and formal site plan submissions should have the following information:</li> <li>Metric scale</li> <li>North arrow (including construction North)</li> <li>Key plan</li> <li>Name and contact information of applicant and property owner</li> <li>Property limits including bearings and dimensions</li> <li>Existing and proposed structures and parking areas</li> <li>Easements, road widening and rights-of-way</li> <li>Adjacent street names</li> </ul>	Site Grading Plan (C101)

### **4.2** Development Servicing Report: Water

Criteria	Location (if applicable)
☐ Confirm consistency with Master Servicing Study, if available	N/A
Availability of public infrastructure to service proposed development	N/A
☐ Identification of system constraints	N/A
☐ Identify boundary conditions	Appendix C
☐ Confirmation of adequate domestic supply and pressure	N/A
<ul> <li>Confirmation of adequate fire flow protection and confirmation that fire flow is calculated as per the Fire Underwriter's Survey.</li> <li>Output should show available fire flow at locations throughout the development.</li> </ul>	Appendix C
<ul> <li>Provide a check of high pressures. If pressure is found to be high, an assessment is required to confirm the application of pressure reducing valves.</li> </ul>	N/A
<ul> <li>Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defined phases of the project including the ultimate design</li> </ul>	N/A
☐ Address reliability requirements such as appropriate location of shut-off valves	N/A
☐ Check on the necessity of a pressure zone boundary modification.	N/A
Reference to water supply analysis to show that major infrastructure is capable of delivering sufficient water for the proposed land use. This includes data that shows that the expected demands under average day, peak hour and fire flow conditions provide water within the required pressure range	Appendix C, Section 4.2

<ul> <li>Description of the proposed water distribution network, including locations of proposed connections to the existing system, provisions for necessary looping, and appurtenances (valves, pressure reducing valves, valve chambers, and fire hydrants) including special metering provisions.</li> </ul>	Site Servicing Plan (C101)
<ul> <li>Description of off-site required feedermains, booster pumping stations, and other water infrastructure that will be ultimately required to service proposed development, including financing, interim facilities, and timing of implementation.</li> </ul>	N/A
☐ Confirmation that water demands are calculated based on the City of Ottawa Design Guidelines.	Appendix C
<ul> <li>Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference.</li> </ul>	N/A

### **4.3 Development Servicing Report: Wastewater**

Criteria	Location (if applicable)
Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitored flow data from relatively new infrastructure cannot be used to justify capacity requirements for proposed infrastructure).	N/A
☐ Confirm consistency with Master Servicing Study and/or justifications for deviations.	N/A
☐ Consideration of local conditions that may contribute to extraneous flows that are higher than the recommended flows in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers.	N/A
Description of existing sanitary sewer available for discharge of wastewater from proposed development.	Section 5.2 Proposed Sanitary Sewer

☐ Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable)	Section 5.3 Proposed Sanitary Design
☐ Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format.	N/A
<ul> <li>Description of proposed sewer network including sewers, pumping stations, and forcemains.</li> </ul>	Section 5.2 Proposed Sanitary Sewer
Discussion of previously identified environmental constraints and impact on servicing (environmental constraints are related to limitations imposed on the development in order to preserve the physical condition of watercourses, vegetation, soil cover, as well as protecting against water quantity and quality).	N/A
<ul> <li>Pumping stations: impacts of proposed development on existing pumping stations or requirements for new pumping station to service development.</li> </ul>	N/A
☐ Forcemain capacity in terms of operational redundancy, surge pressure and maximum flow velocity.	N/A
☐ Identification and implementation of the emergency overflow from sanitary pumping stations in relation to the hydraulic grade line to protect against basement flooding.	N/A
☐ Special considerations such as contamination, corrosive environment etc.	N/A

### **4.4 Development Servicing Report: Stormwater Checklist**

Criteria	Location (if applicable)
<ul> <li>Description of drainage outlets and downstream constraints including legality of outlets (i.e. municipal drain, right-of-way, watercourse, or private property)</li> </ul>	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
Analysis of available capacity in existing public infrastructure.	N/A
<ul> <li>A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns, and proposed drainage pattern.</li> </ul>	Pre & Post-Development Plans
☐ Water quantity control objective (e.g. controlling post-development peak flows to pre-development level for storm events ranging from the 2 or 5-year event (dependent on the receiving sewer design) to 100-year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
☐ Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
<ul> <li>Description of the stormwater management concept with facility locations and descriptions with references and supporting information.</li> </ul>	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
☐ Set-back from private sewage disposal systems.	N/A
☐ Watercourse and hazard lands setbacks.	N/A
Record of pre-consultation with the Ontario Ministry of Environment and the Conservation Authority that has jurisdiction on the affected watershed.	N/A
☐ Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists.	N/A
<ul> <li>Storage requirements (complete with calculations) and conveyance capacity for minor events (1:5-year return period) and major events (1:100-year return period).</li> </ul>	Appendix G

☐ Identification of watercourses within the proposed development and how watercourses will be protected, or, if necessary, altered by the proposed development with applicable approvals.	Site Grading Plan
☐ Calculate pre-and post development peak flow rates including a description of existing site conditions and proposed impervious areas and drainage catchments in comparison to existing conditions.	Section 7.0 Proposed Stormwater Management Appendix G
Any proposed diversion of drainage catchment areas from one outlet to another.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
<ul> <li>Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and stormwater management facilities.</li> </ul>	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
☐ If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post-development flows up to and including the 100-year return period storm event.	N/A
☐ Identification of potential impacts to receiving watercourses	N/A
☐ Identification of municipal drains and related approval requirements.	N/A
<ul> <li>Descriptions of how the conveyance and storage capacity will be achieved for the development.</li> </ul>	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
100-year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading.	Site Grading Plan (C101)
☐ Inclusion of hydraulic analysis including hydraulic grade line elevations.	N/A

<ul> <li>Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors.</li> </ul>	Section 8.0 Sediment & Erosion Control
☐ Identification of floodplains — proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions.	N/A
☐ Identification of fill constraints related to floodplain and geotechnical investigation.	N/A

### 4.5 Approval and Permit Requirements: Checklist

The Servicing Study shall provide a list of applicable permits and regulatory approvals necessary for the proposed development as well as the relevant issues affecting each approval. The approval and permitting shall include but not be limited to the following:

Criteria	Location (if applicable)
Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act.	N/A
Application for Certificate of Approval (CofA) under the Ontario Water Resources Act.	N/A
☐ Changes to Municipal Drains.	N/A
☐ Other permits (National Capital Commission, Parks Canada, Public Works and Government Services Canada, Ministry of Transportation etc.)	N/A

### **4.6 Conclusion Checklist**

Criteria	Location (if applicable)
Clearly stated conclusions and recommendations	Section 9.0 Summary
	Section 10.0 Recommendations
☐ Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency.	All are stamped
☐ All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario	All are stamped