telephone: (613) 745-6471

e-mail: alston.associates@alston.ca

fax: (613) 745-0796



PROPOSED MIXED-USE DEVELOPMENT PHASE 2A & 2B WATERIDGE VILLAGE OTTAWA, ONTARIO

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Prepared For:

Canada Lands Company CLC Limited 100 Queen Street , Unit 1050 Ottawa, ON K1P 1J9

Prepared By:

Alston Associates
A division of Terrapex Environmental Ltd.

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1 INTRODUCTION

Alston Associates (AA), the geotechnical division of Terrapex Environmental Ltd. (**Terrapex**) has been retained by Canada Lands Company CLC Limited (CLC) to carry out a geotechnical investigation for the proposed mixed-use development of Wateridge Village (Phase 2A and 2B) located at the property of the former Canadian Forces Base (CFB) Rockcliffe in the City of Ottawa, Ontario. Authorization to proceed with this study was given by Mr. Jean Lachance of CLC.

We understand that CLC is seeking approval to develop the land at Wateridge Village referred to as Phase 2A and 2B Lands and construct Parks 1 and 7 including road improvements to existing infrastructure along Hemlock Road.

The Phase 2 (A and B) area is located north of Registered Plans of Subdivisions 4M-1559 and 4M-1581 in Wateridge Village, as shown on Drawing 2 attached in Appendix B of this report. Drawing 2 also shows the proposed land use of the property sub-divided into blocks according to the type of development. According to the proposed development plan, the site is scheduled for a mixed use residential development which would include the following:

- Phase 2A will contain three low to mid-rise mixed use Blocks (8, 10 and 11), one low to mid-rise residential Block (13), one low-rise residential Block (12), Park 1 (Block 9), and Hemlock Road west of Codd's Road.
- Phase 2B will contain two mid-rise mixed use Blocks (6 and 7), four low to mid-rise residential Blocks (1, 2, 4 and 5), and Park 9 (Block 3).

A grading plan dated December 2018 was prepared by IBI Group; attached in Appendix B as Drawings 7, 8, and 9. Drawings 7 and 8 shows the building locations and finish floor and foundation elevations on Blocks 2, 4, and 5. Details regarding building locations and design and municipal infrastructure on the remaining blocks were not available at the time of the investigation, and accordingly the recommendations provided in this report are considered to be preliminary in nature, subject for review and revision upon completion of proposed plans.

The purpose of this investigation was to characterize the subsurface soil and groundwater conditions, to determine the engineering properties of the various soil deposits underlying the site, and to provide geotechnical engineering recommendations pertaining to the proposed development.

The investigation included evaluation of the pavement of the old Hemlock Road to assess the condition of the pavement structure and to provide recommendations for improvements/repairs prior to use for construction traffic, transit vehicles and public access.

This report presents the results of the investigation performed in accordance with the general terms of reference outlined above and is intended for the guidance of the client and the design architects or engineers only. It is assumed that the design will be in accordance with the applicable building codes and standards.

2 BACKGROUND

A number of geotechnical and hydrogeological investigations were completed at the former CFB Rockcliffe property for CLC and documented in the following reports; copies of which were provided to us by CLC:

- "Geotechnical Investigation Phase 1B Development Site Servicing, Wateridge Village at Rockcliffe, Ottawa, Ontario", dated November 2016 (DST File No: IN-SO-026755);
- "Geotechnical Investigation Phase 1A Development Site Servicing, Former CFB Rockcliffe Development, Ottawa, Ontario", dated November 2015 (DST File No: OE-OT- 015358);
- "Final Geotechnical Investigation for Subdivision Approval, Former CFB Rockcliffe Development, Ottawa, Ontario", dated September 2015 (DST File No: OE-OT-015358);
- "Preliminary Geotechnical and Hydrogeological Investigation Proposed Stormwater Management Pond, CLC Rockcliff Lands Hemlock Road and Aviation Parkway, Ottawa, Ontario", dated May 2015 (Golder Associates File No: 1521309);
- "Geotechnical Investigation Report for Preliminary Assessment for Building Foundation, Services Installation and Grade Raise Analysis Mapping – Phase 1 Development, Former CFB Rockcliffe, Ottawa, Ontario", dated April 2014 (DST File No: GS-OT-015358);
- "Hydrogeological Report Stormwater Management Support Studies, Former CFB Rockcliffe, Ottawa, Ontario, dated October 2013" (DST File No: OE-OT- 017184);
- "Preliminary Geotechnical Investigation, Rockcliffe Redevelopment Program", dated March 2006 (DST File No.: OGO6562).

The previous borehole and test pit locations in the Phase 2 development area were extracted from the above referenced reports; shown on Drawing 4 attached in Appendix B of this report. The logs of the previous boreholes and test pits are also attached in Appendix D.

According to the previous borehole and test pit findings, topsoil up to about 200 mm in depth is present across the site. Asphaltic concrete, with a thickness of about 100 mm, is present on existing roads and driveways. Fill material consisting of various silty sand, sand and gravel or clay is present in various areas of the site, with thickness ranging from approximately 0.5 to 4.3 m.

Grey silty clay is the dominant native overburden type in the central and southern portion of the site. The clay layer extends from near surface to a depth of more than 6 m in the south and thins out to the northeast and north where it overlies silty till deposits at depths of 1 to 2 m. The northern and eastern portions of the site are generally underlain by till material consisting of grey compact silt, sand and minor gravel. Where encountered during previous drilling, the till is 1 to 3 m thick.

Boreholes drilled into the bedrock typically encountered horizontally bedded, grey limestone with minor narrow shale bedding, interpreted to be of the Ottawa Group. The bedrock surface is generally unweathered or has a narrow weathering zone, less than one metre thick.

The applicable information from the previous geotechnical investigations are discussed and applied to the comments and recommendations presented in this report.

3 FIELDWORK

The fieldwork for this investigation was carried out during the period between November 13 and 20, and December 14, 2018. It consisted of sixty seven (67) boreholes and twenty four (24) exploratory test pits, advanced by drilling and excavation contractors commissioned by AA. The number and location of the boreholes were chosen by AA and reviewed by IBI Group and CLC to provide general coverage of the site for the proposed development. The locations of the test pits were chosen by AA to provide general coverage between the boreholes to confirm the depth of bedrock. The locations of the boreholes and test pits are shown on Drawing 3; enclosed in Appendix B of this report.

The boreholes; designated as BH101 through BH129, BH131, BH133 through BH150, BH152 through BH167, and BH173 through BH175, were advanced to depths ranging from 0.6 to 4.58 m below ground surface (mbgs). Eight (8) of the boreholes; MW111, MW124, MW125, MW142, MW142, MW152, MW158, and MNW166, were instrumented with monitoring wells to determine the long term groundwater table at the site.

The exploratory test pits (designated as TP201 through TP224) were extended to depths ranging from 0.4 to 4.4 mbgs to confirm the existence and depth of the bedrock.

The ground surface elevations at the locations of the boreholes and test pits were established by **AA** using Topcon Hiper V GNSS Receiver and Trimble R10 GNSS Receiver respectively.

Standard penetration tests were carried out in the course of advancing the boreholes to take representative soil samples and to measure penetration index values (N-values) to characterize the condition of the various soil materials. The number of blows of the striking hammer required to drive the split spoon sampler to 300 mm depth was recorded and these are presented on the logs as penetration index values. Results of SPT are shown on the borehole log sheets in Appendix C of this report.

Groundwater level observations were made in the boreholes and test pits upon completion of each of their advancement, and in the monitoring wells on December 17, 2018. The results of the groundwater measurements are discussed in Section 4.5 of this report.

The fieldwork for this project was carried out under the supervision of an experienced geotechnical technician from this office who laid out the positions of the boreholes and test pits in the field; arranged locates of buried services; effected the drilling, test pit excavation, sampling and in situ testing; observed groundwater conditions; and prepared field borehole and test pit log sheets.

4 LABORATORY TESTS

The soil samples retained from the split spoon sampler were properly sealed, labelled and brought to our laboratory. They were visually classified and water content tests were conducted on all soil samples retained from Boreholes BH101, BH102, BH107, BH 114, BH118, MW124, MW125, BH140, NW142, MW147, MW152, BH154, BH157, BH164, and BH167. The results of the classification, water contents, and Standard Penetration Tests are presented on the borehole logs sheets attached in Appendix C of this report.

Grain-size analyses were carried out on twelve (12) soil samples; Atterberg Limits test was performed on two. The results of these tests are presented as Figures E-1 through E-14 in Appendix E.

In addition, four (4) soil samples were submitted to an analytical laboratory for chemical analyses for pH and soluble sulphate tests. The results of these tests are enclosed in Appendix F; discussed in Section 6.13 of this report.

5 SITE AND SUBSURFACE CONDITIONS

Full details of the subsurface and groundwater conditions at the site are given on the borehole Log sheets attached in Appendix C of this report.

The following paragraphs present a description of the site and a commentary on the engineering properties of the various soil materials contacted in the boreholes.

It should be noted that the boundaries of soil types indicated on the borehole logs are inferred from non-continuous soil sampling and observations made during drilling. These boundaries are intended to reflect transition zones for the purpose of geotechnical design, and therefore, should not be construed as exact planes of geological change.

5.1 Site Description

The subject site is located at the former CFB Rockcliffe property in the City of Ottawa. The former CFB Rockcliffe property is approximately 310 acres; bounded by Aviation Parkway to the west, Sir George Etienne Cartier Parkway to the North, the National Research Council of Canada campus to the east, and existing residential communities and Montfort Hospital to the south. It is bounded by two bedrock escarpments at the south and north boundaries. The Rockcliffe Airport is also located in the vicinity of the site, just north of Sir George Etienne Cartier Parkway.

Our investigation was limited to Phase 2A and 2B including Hemlock Road (west of Codd's Road). The former CFB Rockcliffe property and Phase 2 development area are shown in Drawing 1, attached in Appendix B.

Phase 2A is situated north of Hemlock Road, west of Codd's Road, east of vacant NCC lands, and south of Sir George Etienne Cartier Parkway. It has been divided into Blocks 8 through 13 including Street No. 3, Street No. 4, and Hemlock Road. The north escarpment is located along the north boundary of Phase 2A. The slope of the escarpment is almost vertical with exposed bedrock. There is a storm management pond at the bottom of the escarpment.

There are several old pathways, roadways and driveways traversing throughout Phase 2A from past land use, and new storm and sewer lines have been installed along the alignment of the proposed Street No. 4 and east towards the storm sewer outfall. Stockpiles of fill material from previous phases and ongoing construction activities are located in and around Block 12, within the northern half of Block 8, and scattered throughout the north area of Block 9. The remainder of Phase 2A is covered with light to moderate vegetation with mature trees predominately outlining the perimeters of the blocks, and scattered throughout Block 9 (Proposed Park1). The ground surface topography of phase 2A slopes down from south to north and from east to west, the ground surface elevations at the borehole and test pit locations ranged between 77.25 at Test Pit TP208 to 89.57 m at Borehole BH120.

Phase 2B is situated north of Hemlock Road, east of Codd's Road, west of National Research Council of Canada campus, and south of Wanaki Road. It has been divided into Blocks 1 through 7 including Wanaki Road, Street No. 1, Street No. 2, Moses Tennisco Street, Michael Stoqua Street, Bareille-Snow Street, and Codd's Road.

There are several old pathways, roadways and driveways traversing through Phase 2B from past land use. Stockpiles of fill, topsoil and blast rock material from previous phases and ongoing construction activities are located in and around Block 4, northern half of Block 1, northern half of Block 6 and northeast portion of Block 7. Blast rock and fill material are also present along the north edge of Hemlock Road. The remainder of Phase 2B is covered with light vegetation and mature trees predominately outlining the perimeters of the blocks. The ground surface topography is relatively flat with a gradual slope down from east to west and south to north. The ground surface elevations at the borehole and test pit locations ranged between 88.14 m at Borehole BH140 to 93.99 m at Test Pit TP221.

5.2 Asphaltic Concrete Pavement

Boreholes BH101, BH102, BH103, BH104, BH105, BH107, BH108, BH115, BH121, BH138, BH141, BH144, BH 155, BH162, and BH167 were advanced through the asphaltic concrete pavement. They revealed that the thickness of the asphaltic concrete ranges from approximately 40 to 140 mm.

5.3 Granular Base Course

The base course supporting the asphaltic concrete consists of sandy gravel to gravelly sand. The thickness of this granular soil ranges from approximately 200 to 250 mm.

Penetration resistance of the base course material measured N-values ranging from 19 to 25, indicating its compactness condition is compact. The water content of the tested samples of the granular base from Boreholes BH107 and BH167 was about 5% by weight; being damp in appearance.

Sieve grain size analysis was carried out on one (1) sample of granular base course obtained from Borehole BH102 at 0.2 mbgs (Sample 1A). The test revealed that the soil has 70% sand, 28% gravel, and 2% silt and clay. The result of the grain size analysis is shown as Figure E-1 in Appendix E.

5.4 Topsoil

Topsoil was encountered in Boreholes BH114, BH118, BH131, BH134, BH143, BH145, BH146, BH147, BH150, BH153, BH158, BH159, BH155, BH160, BH164, BH165, BH166 and BH167. The thickness of the topsoil at the boreholes varies between approximately 50 and 250 mm.

It should be noted that the topsoil thickness will vary between boreholes. Thicker topsoil than that found in the boreholes may be present in places.

5.5 Fill Material

Fill material is present in all boreholes below the pavement granular base, the topsoil, or surficial

vegetation with the exception of Boreholes BH118, BH127, BH131, BH146, BH147, and BH150. The fill consists of various gravelly sand to sandy gravel, silty sand to sandy silt with trace of gravel, and clayey silt soils; extending to approximate depths ranging from 0.3 to 2.7 mbgs. The fill contains traces of organic, rootlet, and rock fragment. At the location of Boreholes BH114, BH116, BH118, BH120, BH153, and BH154, the fill material contains trace cinder. At the location of Boreholes BH137, BH139, BH142, BH143, BH148, BH153, BH161, and BH174, the fill contains trace to some brick pieces.

SPT carried out in the silty, sandy, and gravelly fill material measured N-values ranging from 3 to 50/25 mm penetration; indicating very loose to very dense compactness condition; generally being compact. The higher N-values are likely due to the split spoon sampler striking boulders or construction rubble. SPT carried out in the clayey silt fill material measured N-values ranging from 3 to 36; indicating soft to hard consistency; generally being firm.

The fill material is generally brown to dark brown in color and damp to moist in appearance. The water content of the tested fill samples from Boreholes BH101, BH102, BH107, BH114, BH118, MW124, MW125, BH140, NW142, MW147, MW152, BH154, BH157, BH164, and BH167 ranges from 5 to 37% by weight.

5.6 Native Soils

5.6.1 Silty Sand to Sand with trace silt

Silty sand to sand with trace silt soils are present below the fill material in Boreholes BH127, BH131, BH140, BH149, BH152, BH153, BH156, BH157, BH160, BH162, BH163, BH164, BH166 and underneath a clayey silt deposit in Borehole MW147. The sandy soils contain variable proportions of silt classifying the soil as sand with trace to some silt and silty sand.

The silty sand to sand unit is generally brown in colour. The water content of the tested sand samples from Boreholes BH140, BH147, BH154, BH157, and BH164 ranges from approximately 7 to 22% by weight; generally being moist in appearance.

Penetration resistance in the silty sand to sand units provided N-values ranging from 4 to 50/75 mm penetration, indicating loose to very dense compactness condition.

Sieve grain size analysis was carried out on five (5) representative samples of the sandy soils. The results of the grain size analysis are enclosed in Appendix E as Figures E-2 to E-6 and summarized below.

Borehole Number	Sample Depth (mbgs) and No.	Sample Description	Gravel %	Sand %	Silt %	Clay %
BH104	BH104 1.5 (Sample 3) Silty Sand, some gravel		13	66		21
BH140	BH140 1.5 (Sample 3) Sand, trace silt, trace gravel		3	51		2
BH149	BH149 0.76 (Sample 2A) Silty Sand, trace gravel		7	63	;	30
BH158	1.5 (Sample 3)	Sand, some gravel, trace silt	15	81		4
BH163	BH163 2.28 (Sample 4) Sand, some silt, trace gravel		5	76		19

Based on the results of the grain size analysis, the coefficient of permeability (K) of the sand soils range from 10-2 cm/sec to 10-4 cm/sec; medium to high permeability.

5.6.2 Silt with trace sand to sandy silt

Silt with trace sand to sandy silt soils are present below the fill material in Boreholes BH101 through BH105, BH112, BH113, BH116, BH118, BH120, BH124, BH126, BH134, BH136, BH137, BH145, BH146, BH150, BH151, BH154, BH155, BH164, and BH173. This unit contains variable proportions of sand classifying the soil as silt with trace sand to sandy silt.

The sandy silt to silt unit is generally brown in colour. The water content of the tested silt samples from Boreholes BH101, BH124, BH152, and BH164 ranges from approximately 4 to 20% by weight; generally being damp to moist in appearance.

Penetration resistance in the silt unit provided N-values ranging from 11 to 50/25 mm penetration, indicating compact to very dense compactness condition.

Sieve and hydrometer grain size analyses were carried out on three (3) samples of silt soil obtained from Boreholes BH112, BH120, and BH152. The test results are enclosed in Appendix E as Figures E-7 to E-9, and summarized below.

Borehole Number	Sample Depth (mbgs) and No.	Sample Description	Gravel %	Sand %	Silt %	Clay %
BH112	0.76 (Sample 2)	Silt, some clay, trace sand, trace gravel	3	8	73	16
BH120	0.76 (Sample 2)	Silt, some sand, trace clay	0	20	71	9
BH152	2.28 (Sample 4)	Silt, some sand, some clay	0	18	65	14

Based on the results of the grain size analysis, the K values of the silt soils range from 10-5 cm/sec to less than 10-6 cm/sec; low permeability.

5.6.3 Clay and Silt

A deposit of silt and clay to clayey silt ranging in thickness from 0.5 to 2 m is present below the fill material in Boreholes BH104, BH106, BH125, BH133, BH134, BH138, BH141, BH147, BH150, BH151, BH163, and BH173.

The clay and silt unit is generally brown in colour. The water content of the tested clay and silt samples ranges from approximately 11 to 36% by weight; generally being moist to wet in appearance.

Penetration resistance in the clay and silt soil measured N-values ranging from 5 to 28, indicating firm to very stiff consistencies.

Sieve and hydrometer grain size analyses were carried out on three (3) samples of clay and silt soils; Atterberg Limits test on two (2). The test results are enclosed in Appendix E as Figures E-10 through E-14, and summarized below.

Borehole No.	Sample Depth (mbgs) and No.	Sample Description	Gravel %	Sand %	Silt %	Clay %	Liquid Limit	Plasticity Index	Soil Classification
BH104	0.76 (Sample 2)	Clay and Silt, trace sand	0	2	42	56	-	-	-
BH125	1.5 (Sample 3)	Clay and Silt, trace sand	0	1	45	54	58	34	Inorganic clays of high plasticity
BH134	0.8 (Sample 2)	Clay and Silt, trace sand	0	4	37	59	53	28	Inorganic clays of high plasticity

The soil classification was based on the plasticity chart as shown on Figure 3.1 of the CFEM, 4th Edition.

Based on the results of the grain size analysis, the K values of the clay and silt soil is less than 10⁻⁷ cm/sec; very low relative permeability.

5.6.4 Gravelly Sand

A gravelly sand deposit is present in Borehole BH107; positioned at an approximate depth of 1.8 mbgs and extending to the bedrock at 2.2 mbgs.

SPT in the gravelly sand unit had N-value of 75/254 mm penetration, indicating very dense compactness condition. It is greyish brown in colour and has a moist appearance.

5.7 Bedrock

Bedrock was encountered in all boreholes and test pits with the exception of Boreholes BH101, BH102, and BH103 at approximate depths ranging from 0.6 to 4.58 mbgs, corresponding to approximate elevations of 79.51 m to 91.57 m. The bedrock was proven by auger refusal and test pits and was not cored. The test pits confirmed that refusal to further advancement of the boreholes was due to bedrock and not large boulders or buried concrete slabs. The depth and elevation of the bedrock encountered in the test pits is tabulated in the table below.

Test Pit No.	Ground Elevation (m)	Depth of Bedrock (mbgs)	Elevation of Bedrock (m)
TP201	74.35	1.42	72.93
TP202	76.71	1.15	75.56
TP203	85.48	1.64	83.84
TP204	86.64	1.84	84.80
TP205	85.81	1.64	84.17
TP206	84.13	1.60	82.53
TP207	82.29	0.64	81.65
TP208	77.25	0.98	76.27
TP209	83.71	1.70	82.01
TP210	88.84	1.60	87.24
TP211	89.64	1.35	88.29
TP212	89.04	1.07	87.97
TP213	88.05	0.78	87.27

TP214	88.28	1.30	86.98
TP215	88.88	0.76	88.12
TP216	89.75	1.60	88.15
TP217	8.84	2.13	86.71
TP218	90.64	1.41	89.23
TP219	91.02	1.12	89.90
TP220	93.92	0.92	93.00
TP221	93.99	0.38	93.61
TP222	93.61	0.90	92.71
TP223	93.58	4.40	89.18
TP224	93.56	4.12	89.44

Based on the ground surface elevations, the surface of the rock dips down from the east to the west and from the central section of the site toward the north and south.

The bedrock at the base of all test pits with the exceptions of Test Pits TP221 and TP222 consists of grey limestone. The bedrock at the base of Test Pits TP221 and TP222 consists of shale.

Review of available geological mapping and previous geotechnical investigations indicates that the bedrock is of the Ottawa Formation, consisting of limestone with some shale bedding and some sandstone in the basal part. According to the previous investigations at the site, the rock is classified to be strong to very strong.

5.8 Groundwater

Groundwater level and cave-in of the unlined side walls of the boreholes were measured during the course of the borehole drilling and upon completion of the boreholes; shown on the individual borehole logs. All boreholes were open and dry upon completion with the exception of the ones listed in the following table:

Borehole No.	Groundwater Depth (m)	Cave-in Level (mbgs)
BH107	Dry	1.8
BH108	Dry	1.5
BH110	Dry	0.9
BH133	Dry	1.8
BH134	0.9	Open
BH139	Dry	1.1
BH140	Dry	2.8
BH148	Dry	1.9
BH154	3.0	Open
BH157	1.96	Open
BH174	Dry	0.6

Groundwater conditions exposed in the test pit excavations were also observed. All test pits remained dry upon completion of excavation.

Groundwater levels in the monitoring wells were measured on December 17, 2018. The results of the groundwater measurement are shown in the following table.

Borehole No.	Ground Elevation (m)	Bottom of the Monitoring Well Depth (m)	Bottom of the Monitoring Well Elevation (m)	Groundwater Depth (mbgs)	Groundwater Elevation (mbgs)
MW111	86.96	2.6	84.36	Dry	-
MW124	90.15	1.7	88.45	Dry	-
MW125	82.65	2.4	80.25	0.25	82.40
MW142	89.85	1.8	88.05	Dry	-
MW147	90.91	2.2	88.71	Dry	-
MW152	92.98	3.0	89.98	Dry	-
MW158	92.86	3.0	89.86	2.25	90.61
MW166	93.54	4.1	89.44	2.55	90.99

It should be noted that groundwater levels are subject to seasonal fluctuations. A higher groundwater level condition will likely develop in the spring and following significant rainfall events.

6 DISCUSSION AND RECOMMENDATIONS

The following discussions and recommendations are based on the factual data obtained from the boreholes and test pits advanced at the site by **AA** and are intended for use by the client and design architects and engineers only.

Contractors bidding on this project or conducting work associated with this project should make their own interpretation of the factual data and/or carry out their own investigations.

On the basis of our fieldwork, laboratory tests and other pertinent information supplied by the client, the following comments and recommendations are made.

6.1 Site Grading

The proposed grading plan prepared and provided for our use by IBI Group and dated December 2018 is included in Appendix B as Drawings 7, 8, and 9.

Based on the proposed grading plan, there will be some modifications to the site grading. The grade will be raised/cut by a maximum of 1m. Given the subsurface conditions at the site; i.e. shallow bedrock, and the absence of thick layers of soft clay, grade raise will not cause any settlement of the subsoil.

6.2 Engineered Fill

The following recommendations regarding construction of engineered fill should be adhered to during the construction stage:

- All surface vegetation, organic materials, softened and disturbed soils must be removed, and
 the exposed subgrade soils proof-rolled with an inspection by the Geotechnical Engineer prior
 to any fill placement.
- In the event that the fill will be used to support structures, the existing fill must be removed in its

- entirety prior to placement of new fill.
- Soils used as engineered fill should be free of organics and/or other unsuitable material. The engineered fill must be placed in lifts not exceeding 200 mm in thickness and compacted to at least 98% Standard Proctor maximum Dry Density (SPMDD).
- Engineered fill operations should be monitored and compaction tests should be performed on a full-time basis by a qualified engineering technician supervised by the project engineer.
- The boundaries of the engineered fill must be clearly and accurately laid out in the field by qualified surveyors prior to the commencement of engineered fill construction. The top of the engineered fill should extend a minimum of 2.5 m beyond the envelope of the proposed structures. Where the depth of engineered fill exceeds 1.5 m, this horizontal distance of 2.5 m beyond the perimeter of the structure should be increased by at least 1 m for each 1.5 m depth of fill. The edges of the engineered fill should be sloped at a maximum of 3 horizontal to 1 vertical in order to avoid weakening of the engineered fill edges due to slope movement.
- Due to the potential detrimental effects of differential settlement between the engineered fill
 and the native soils, any buildings where footings are to be placed engineered fill or partly on
 engineered fill and partly on native soils should include steel reinforcement. The foundation
 walls of house foundations supported on engineered fill should be reinforced to bridge localized
 soft spots and zones of non-uniform compaction, and to minimize structural distress due to
 differential settlement of the engineered fill.
- The engineered fill operation should take place in favorable climatic conditions. If the work is carried out in months where freezing temperatures may occur, all frost affected material must be removed prior to the placement of frost-free fill.
- If unusual soil conditions become apparent during construction, due to subsurface groundwater influences, our office should be contacted in order to assess the conditions and recommend appropriate remedial measures.

6.3 Excavation

Based on the borehole findings, excavation for foundations, potential basements, sewer trenches and utilities will be carried out through fill material, sandy, silty, and clayey native soils, and bedrock. Excavation of the soil strata is not expected to pose any difficulty and can be carried out with heavy hydraulic excavators.

Significant bedrock excavation is anticipated across the site. According to the rock core data from the previous investigations, the bedrock generally consists of strong to very strong limestone with interbedded shale of variable bed thicknesses and depth across the site.

Bedrock excavation is expected to be carried out using line drilling and blasting, hoe ramming or both. Provision should be made in the excavation contract to include the use of these techniques for excavation in bedrock.

Any blasting should be carried out in accordance with City of Ottawa Special Provision S.P. No: F-1201 and under the supervision of a blasting specialist engineer. Vibration monitoring of the blasting operation should be carried out to ensure that the blasting meets the limiting vibration criteria at all times.

The contractor should submit a complete and detailed blasting design and monitoring proposal

prepared by a blasting/vibrations specialist prior to commencing blasting. This would have to be reviewed and accepted in relation to the requirements of the blasting specifications. Vibration monitoring of the blasting should be carried out to ensure that the blasting meets the limiting vibration criteria at all times. A pre-blast condition survey should be carried out of surrounding structures and utilities located within 100 m of the excavation site. The condition survey should also include the National Research Council's Montreal Road Campus located east of the subject site.

All excavations must be carried out in accordance with Occupational Health and Safety Act (OHSA). With respect to OHSA, the near surface fill, compact sandy silt to silt and sand to silty sand, and firm clay and silt soils are expected to conform to Type 3 soils. The dense to very dense sandy silt to silt and sand to silty sand, and stiff to very stiff clay and silt soils can be classified as Type 2 soils. The bedrock is classified as Type 1 soil.

Temporary excavations for slopes in Type 3 soil should not exceed 1.0 horizontal to 1.0 vertical. In the event very loose and/or soft soils are encountered at shallow depths or within zones of persistent seepage, it will be necessary to flatten the side slopes as necessary to achieve stable conditions. In wet sandy soils it may be necessary to slope the excavation at inclinations from 1.0 vertical to 2.0 horizontal to 1.0 vertical to 3.0 horizontal. Excavations in Type 2 soil may be cut with vertical side-walls within the lower 1.2 m height of excavation and 1.0 horizontal to 1.0 vertical above this height. Excavations in the bedrock may be cut with vertical side-walls.

For excavations through multiple soil types, the side slope geometry is governed by the soil with the highest number designation. Excavation side-slopes should not be unduly left exposed to inclement weather. Excavation slopes consisting of sandy soils will be prone to gullying in periods of wet weather, unless the slopes are properly sheeted with tarpaulins.

It should be noted that the on-site fill material may contain boulders, cobbles and remnants of former buildings in the form of buried concrete. Provisions must be made in the excavation and foundation installation contracts for the removal of possible boulders and concrete.

Where workers must enter excavations extending deeper than 1.2 m below grade, the excavation sidewalls must be suitably sloped and/or braced in accordance with the Occupational Health and Safety Act and Regulations for Construction Projects.

It is anticipated that sufficient space will be available to slope the sidewalls of the basement excavation; as such it will not be necessary to shore the basement excavation walls.

6.4 Reuse of On-site Excavated Soil as a Compacted Backfill

On-site excavated inorganic native soils are considered suitable for reuse as backfill material within the roadways and pipeline trench excavations, provided their water content is within 2% of their optimum water contents (OWC) as determined by Standard Proctor test, and the materials are effectively compacted with heavy compaction rollers.

While the quality of the native soils are considered suitable for backfilling; the moisture content of the soils and the lift thickness for compaction must be properly controlled during the backfilling. Alternatively, imported suitable material should be used.

Measured water content ranges from approximately 4 to 36% within the native soils and from 5 to 37% within the fill material; generally being close to the wet side of the material's OWC. On-site native soils that are wetter than their OWC should be dried sufficiently prior to use as backfill in order to achieve the specified degree of compaction. Spreading the material in a wide area and air drying will be required to achieve the specified compaction of the native material. Thorough vertical mixing of the excavated soils will be required to provide a material that can be adequately compacted.

The spoil resulting from excavation through the bedrock will contain a large amount of hard rock slabs which will be virtually impossible to compact. Bedrock crushed on-site can be used as granular material provided that it conforms to OPSS gradation requirements and physical properties.

6.5 Groundwater Control

Based on observations made during drilling of the boreholes and excavation of the test pits, close examination of the soil samples extracted from the boreholes, and groundwater measurements made in the monitoring wells, significant groundwater problems are not anticipated within the presumed excavation depths throughout majority of the site with the exception of the area encompassing Blocks 1 and 2 in the easternmost section of the site. Groundwater is present in sand soil in this section of the site. Active dewatering of the sand layers will be required in the event that the excavation is extended below the water table; it is anticipated that dewatering will be possible using a series of filter sump pumps in the base of the excavation.

In the reminder of the site, some seepage of groundwater from localized permeable layers may occur during construction. It will be possible to remove any such seepage using submersible pumps.

Dewatering can be carried out using existing Permit to Take Water (PTTW) obtained by CLC from the MOECP.

Surface water should be directed away from open excavations.

6.6 Residential and Mixed-Use Buildings

6.6.1 Foundation Design

According to the proposed grading plan; shown on Drawing 7 attached in Appendix B, the proposed buildings on Blocks 2, 4, and 5 will be constructed over a single level basement. Details regarding the remaining blocks were not available at the time of the investigation, and accordingly the recommendations provided in this report are considered to be preliminary in nature, subject for review and revision upon completion of proposed plans. Additional boreholes may have to be advanced by the builders at the site once the details of the proposed buildings are finalized.

Conventionally, footing foundations of heated and unheated buildings are positioned at depths of 1.5 m and 1.8 m respectively below exterior grade in the Ottawa area, in order to provide protection to the foundation soil from freezing temperatures.

The foundations for the mid-rise buildings should be installed on the bedrock.

It is not recommended to install the foundations of the proposed low-rise buildings on the fill material. Based on the borehole findings, the bearing stratum should consist of the bedrock or native soil. The native soil throughout the site is considered suitable for the support of low rise building foundations. Locally, it will be necessary to deepen the foundations where the native soil is less competent in strength.

It should also be noted that intact bedrock will not be subjected to frost heave, and provided that footings are extended to non-fractured intact rock, the minimum founding depth of 1.8 m would not apply, and the footings may be placed at shallower depths.

Foundations may be constructed on engineered fill provided that the existing fill is removed in its entirety and the engineered fill is constructed in accordance with recommendations provided in Section 6.2 of this report.

Conventional spread and strip footings may be used to support the proposed buildings.

Foundations installed on the native soil or certified engineered fill may be designed based on bearing resistance of 100 KPa at Serviceability Limit States (SLS), and factored geotechnical bearing resistances at Ultimate Limit States (ULS) of 150 kPa.

The geotechnical bearing resistances recommended above are for vertical loads (no inclination) and no eccentricity. The total and differential settlements of spread footing foundations founded on the native soil designed in accordance with the recommendations provided in this report should not exceed the conventional limits of 25 mm and 19 mm respectively.

Foundations installed on the bedrock may be designed for a factored bearing resistance at Ultimate Limit States of 1 MPa (ULS). The serviceability limit state is not applicable as bedrock will not undergo settlement.

Due to variations in the consistency of the founding soils and/or loosening caused by to excavating disturbance and/or seasonal frost effects, all footing subgrade must be evaluated by the Geotechnical Engineer prior to placing formwork and foundation concrete to ensure that the soil exposed at the excavation base is consistent with the design geotechnical bearing resistance.

In the event necessary, the stepping of the footings at different elevations should be carried out at an angle no steeper than 2 horizontal (clear horizontal distance between footings) to 1 vertical (difference in elevation) on the native soil and 1 horizontal to 1 vertical on the bedrock. No individual footing step should be greater than 0.6 m.

Rainwater or groundwater seepage entering the foundation excavations must be pumped away (not allowed to pond). The foundation subgrade soils should be protected from freezing, inundation and equipment traffic at all times. If unstable subgrade conditions develop, **AA** should be contacted in order to assess the conditions and make appropriate recommendations.

The native soils and rock tend to weather and deteriorate rapidly on exposure to atmosphere or surface water, so construction scheduling should consider the amount of excavation left exposed to the elements, during foundation preparation. **AA** recommends that footings placed on the exposed soil should be poured on the same day as they are excavated, after removal of all unsuitable founding materials and approval of the bearing surface. Alternatively, a concrete mud slab could be used to

protect a bearing surface where footing construction is to be delayed.

In the absence of a significant clay soil at this site, a tree planting restriction does not apply for the development.

6.6.2 Concrete Slab-on-Grade

For building(s) without basement construction, the subgrade supporting the ground floor slab will in general consist of engineered fill or native soil which is adequate to support a slab-on-grade construction. Subgrade preparation should include the removal of surface vegetation, organic materials, weak and softened soils. After removal of all unsuitable materials, the subgrade should then be proof-rolled with heavy rubber tired equipment and adjudged as satisfactory before preparing the granular base course. The proof-rolling operation should be witnessed by the Geotechnical Engineer. Any soft or unsuitable subgrade areas which deflect significantly should be sub-excavated and replaced with suitable engineered fill material compacted to at least 98% of SPMDD.

For building(s) that include a single level basement, the basement floor slabs will rest on the native soil or bedrock; suitable for slab-on-grade construction. Subgrade preparation should include the removal of any disturbed soils, followed by proof-rolling to confirm the subgrade conditions. Any unsuitable subgrade areas which deflect significantly should be sub-excavated and replaced with suitable engineered fill material compacted to at least 98% of its SPMDD.

Where new fill is required to raise the grade, the excavated earth fill and native sandy silty clay material from the site or similar clean imported fill material may be used, free from topsoil, organic or deleterious matter, provided the material is placed in large areas where it can be compacted with a heavy vibratory roller. The fill material should not be frozen and should not be too dry or too wet for efficient compaction (moisture content at optimum or 2% greater than optimum). The fill placement should not be performed during winter months when freezing temperatures occur persistently or intermittently. All fill placed below the slab on grade areas of the buildings must be placed in thin lifts of 200 mm thickness or less, and compacted to a minimum of 98% of SPMDD.

Provided the subgrade, under-floor fill and granular base are prepared in accordance with the above recommendations, the Modulus of Subgrade Reaction (ks) for floor slab design will be 25,000 kPa/m.

It is recommended that a combined moisture barrier and a leveling course, having a minimum thickness of 150 mm and comprised of free draining material be provided as a base for the slab-ongrade. For building(s) without basement construction, either Granular "A" or 20 mm crusher run limestone may be used. For building(s) with basement construction, 20 mm clear crushed limestone is recommended as the base course. The Granular "A" should be compacted to 100% of its SPMDD; the 20 mm clear stone must be compacted by vibration to a dense state.

For building(s) containing a basement level, an exterior perimeter drainage system, consisting of 100 mm diameter weeping tile wrapped in filter fabric and covered with a minimum 150 mm clear crushed stone should be placed along the exterior foundation walls, below the level of the granular base of the floor slab. The weeping tiles must be connected to a positive frost free outlet from which the water can be removed, or connected to a sump located in the basement. The water from the sump must be pumped out to a suitable discharge point. The installation of the perimeter drains as well as the outlet

must conform to the applicable plumbing code requirements.

For building(s) without basement construction, perimeter drainage at the foundation level is not required provided the finished floor surface is at least 150 mm above the prevailing grade and the surrounding surfaces slope away from the buildings.

For building(s) with basement construction, the basement wall backfill for a minimum lateral distance of 0.6 m out from the wall should consist of free-draining granular material such as OPSS Granular "B" Type I. The native soil may be used to backfill excavations along foundation walls provided that prefabricated drainage sheets must be placed continuously against the walls. Damp-proofing must be applied to the exterior basement walls.

The soils at this site are susceptible to frost effects which would have the potential to deform hard landscaping adjacent to the building. At locations where proposed building is expected to have flush entrances, care must be taken in detailing the exterior slabs / sidewalks, providing insulation / drainage / non-frost susceptible backfill to maintain the flush threshold during freezing weather conditions.

6.7 Park 1: North Community Park

It is understood that the north Community Park will be located on Block 9 along the northern border of the site and occupy an area of 10.34 hectares. It will partially front onto Codd's Road on the east and local roads on the west and south sides. It will overlook the Ottawa River on the north side.

The topography of the park area is not level; generally sloping down from south to north. It contains steep ridges and some significant tree and vegetation groupings along the northern and southern boundaries.

The park will serve as the primary passive-recreational space for the community and contain a multiuse pathway system, a community building, look-out area with water feature, outdoor amphitheatre, shade structure, playground, splash pad, open space free play area, toboggan hill, and community gathering area. The approximate locations of the proposed features are shown on the Parks Master Plan drawing prepared by MMM Group Limited and provided for our use by CLC; shown on Drawing 5 attached in Appendix B.

According to the proposed grading plan, there will be some minor modifications to the park grades.

6.7.1 Community Building

It is anticipated that the proposed community building will be a 3,000 ft², single storey above grade structure: constructed on the west side of the park.

The subsurface conditions for the proposed building are represented by Borehole BH127. The borehole reveals that bedrock is situated at an approximate depth of 1.5 mbgs.

Conventional spread and wall footings may be used to support the proposed building. Footing foundations which rest on the bedrock may be designed to apply a factored bearing resistance at Ultimate Limit States of 1 MPa (ULS). The serviceability limit state is not applicable as bedrock will not

undergo settlement.

The subgrade supporting the floor slab of the community building will consist of native silty sand soil.

Subgrade preparation should include the removal of surface vegetation, organic materials, weak and softened soils. After removal of all unsuitable materials, the subgrade should then be proof-rolled with heavy rubber tired equipment and adjudged as satisfactory before preparing the granular base course. The proof-rolling operation should be witnessed by geotechnical staff. Any soft or unsuitable subgrade areas should be sub-excavated and replaced with suitable approved compacted backfill; placed in maximum lifts of 200 mm and compacted to at least 98% of SPMDD.

Where new fill is required to raise the grade, the excavated earth fill and native sand and silt material from the site or similar clean imported fill material free from topsoil, organic or deleterious matter, may be used, provided the material is placed in large areas where it can be compacted with a heavy vibratory roller. The fill material should not be frozen and should not be too dry or too wet for efficient compaction (moisture content at optimum or 2% greater than optimum). The fill placement should not be performed during winter months when freezing temperatures occur persistently or intermittently. All fill placed below the slab on grade areas of the buildings must be placed in thin lifts of 150 mm thickness or less, and compacted to a minimum of 98% of SPMDD.

It is recommended that a combined moisture barrier and a levelling course, with a minimum thickness of 150 mm and comprised of free draining material be provided as a base for the slab-on-grade, either Granular "A" or 20 mm crusher run limestone may be used and compacted to 100% of its SPMDD.

Perimeter drainage at the foundation level is not required provided the finished floor surface is at least 150 mm above the prevailing grade and the surrounding surfaces slope away from the building at a gradient of at least 2 percent.

The rock tends to weather and deteriorate rapidly on exposure to atmosphere or surface water, so construction scheduling should consider the amount of excavation left exposed to the elements, during foundation preparation. **AA** recommends that footings placed on the exposed bedrock should be poured on the same day as they are excavated, after removal of all unsuitable founding materials and approval of the bearing surface. Alternatively, a concrete mud slab could be used to protect a bearing surface where footing construction is to be delayed.

6.7.2 Look-Out Area

We understand that it is proposed to construct a look-out area with a prominent water feature along the northern boundary to optimize the views to the Ottawa River.

Test Pit (TP208) was advanced in the proposed look-out area and revealed that the stratigraphy in this area consists of fill material extending to an approximate depth of 1.7 mbgs, followed by the bedrock.

Conventional spread and strip footings founded on the bedrock may be used to support the proposed structure. It is recommended that the foundation is designed and prepared in accordance with the recommendations provided in section 6.7.1 of this report.

Due to the proximity of the proposed lookout structure to the crest of the escarpment at the northern

boundary of the park, a slope stability analysis must be carried out based on the profile of the existing slope and subsurface soil and groundwater data collected from the current and previous investigations. The proposed structure must be set a safe distance from the crest of the escarpment.

6.7.3 Shade Structure

Borehole BH128 which was advanced in the proposed shade structure area revealed that the soil stratigraphy consists of fill; extending to an approximate depth of 1 mbgs, followed by bedrock.

Conventional spread and strip footings founded on the bedrock may be used to support the proposed structure. It is recommended that the foundation is designed and prepared in accordance with the recommendations provided in section 6.7.1 of this report.

The subgrade supporting the floor slab of the shade structure will consist of fill soil. It is recommended that the subgrade is prepared in accordance with the recommendations provided in section 6.7.1 of this report.

It is recommended that a combined moisture barrier and a levelling course, with a minimum thickness of 150 mm and comprised of free draining material be provided as a base for the slab-on-grade, either Granular "A" or 20 mm crusher run limestone may be used and compacted to 100% of its SPMDD. The granular material must be adequately drained to minimize frost heave or be provided with insulation.

Uplift resistance should be considered for the design of the canopy structure which is subject to wind uplift forces. The uplift resistance should be provided using the dead weight of the foundation as well the soil weight above the footing of the canopy structures. For design purposes, the unit weight of concrete may be taken as 24 kN/m3 and the backfill placed above the footings is 20 kN/m³. If increased uplift capacities are required, this may be achieved by increasing the weight (size) of the foundation, or alternatively, with the use of rock anchors.

6.7.4 Playground

It is expected that the playground structures will be lightly loaded frame structures, which will probably be supported on a set of foundations.

Borehole BH129 which was advanced in vicinity of the proposed playgroundand revealed that the soil stratigraphy consists of fill extending to an approximate depth of 1.5 mbgs, followed by bedrock.

Conventional spread and strip footings founded on the bedrock may be used to support the proposed structure. It is recommended that the foundation is designed and prepared in accordance with the recommendations provided in section 6.7.1 of this report.

The site preparation should consist of removing the existing topsoil layer and profiling the subgrade to the design grades to provide efficient drainage. The fill should provide a satisfactory subgrade to support the playing field.

If any unsuitable fill is contacted at subgrade elevation, this should be removed to contact the underlying competent native sand and silt (till) soil. The sub-excavation should be upfilled with suitable selected fill material (reuse of site excavated soil) and compacted to a dry density of not less than 95% of the materials SPMDD. Construction of turf and the site subgrade systems should be carried out to

meet the design requirements of the artificial turf supplier.

6.7.5 Splash Pad

It is anticipated that the splash pad will consist of concrete slab on grade. It is recommended that the subgrade is prepared in accordance with the recommendations provided for in section 6.7.1 of this report.

Once the subgrade soils have been improved, it is recommended that a minimum 300 mm thick levelling granular base course (Granular A or 20 mm crusher run limestone) is constructed to provide uniform support to the concrete slab.

Sub-drains are recommended to prevent accumulation of water within the granular material, to intercept excess subsurface moisture and minimize subgrade softening. The invert of sub-drains should be maintained at least 0.3 m below subgrade level.

The foundation soils should be insulated from freezing conditions in order to mitigate movement of the foundation soils as a result of the freeze-thaw cycle.

A styrofoam insulating layer (about 150 mm thick) may be placed to rest on the granular base layer under the concrete slab extending a minimum of 1.8 m beyond the outside limit of the floor slab and is placed at a slight slope grading away from the structure to encourage drainage.

The insulation should be protected against degradation by sunlight and damage from surface traffic (with about 200 mm thick overlay layer consisting of granular material, topsoil or sod).

6.8 Park 7: East Parkette

It is understood that the East Parkette will be located on Block 3 and occupy 0.40 hectares. The park will front onto Hemlock Road on the south, residential block on the north, and local roads on the east and west sides. The topography of the park area is relatively flat and contains little vegetation.

The park will serve as the primary passive-recreational space for the local residents and contain a shade structure, splash pad, and playground in the southern portion, a community gathering area in the central portion, and a free play area in the north end of the park. The approximate locations of the proposed features are shown on the Parks Master Plan drawing prepared by MMM Group Limited and provided for use by CLC; shown on Drawing 6 attached in Appendix B.

According to the proposed grading plan, there will be some minor modifications to the park grade.

Boreholes BH153 and BH154 and Test Pit TP219 were advanced in the park area. They revealed that fill is present in this area; extending to approximate depths ranging from 1.1 to 1.6 mbgs, followed by compact silty sand, and underlain by bedrock at approximate depths ranging from 1.1 to 3.2 mbgs.

The recommendations provided for construction of the shade structure, splash pad, and playground in sections 6.7.3 through 6.7.5 of this report apply to the proposed features in this park.

6.9 Service Trenches

Based on the proposed site grades, sewer pipes and water mains will be supported on the bedrock or undisturbed native sandy and silty soils which are considered suitable for supporting water mains, sewer pipes, manholes, catch basins and other related structures

The type of bedding depends mainly on the strength of the subgrade immediately below the invert levels.

Normal Class 'B' bedding is recommended for underground utilities. Granular 'A' or 19 mm crusher-run limestone can be used as bedding material; all granular materials should meet OPS 1010 specifications. The bedding material should be compacted to a minimum of 95% SPMD. Bedding details should follow the applicable governing design detail (i.e. City of Ottawa, OPSD). Trenches dug for these purposes should not be unduly left exposed to inclement weather.

Pipe bedding and backfill for flexible pipes should be undertaken in accordance with OPSD 802.010. Pipe embedment and cover for rigid pipes should be undertaken in accordance with OPSD 802.030.

If unsuitable bedding conditions occur, careful preparation and strengthening of the trench bases prior to sewer installation will be required. The subgrade may be strengthened by placing a thick mat consisting of 50 mm crusher-run limestone. Field conditions will determine the depth of stone required. Geotextiles and/or geogrids may be helpful and these options should be reviewed by **AA** on a case by case basis.

Sand cover material should be placed as backfill to at least 300 mm above the top of pipes. Placement of additional granular material (thickness dictated by the type of compaction equipment) as required or use of smaller compaction equipment for the first few lifts of native material above the pipe will probably be necessary to prevent damage to the pipe during the trench backfill compaction.

It is recommended that service trenches be backfilled with on-site native materials such that at least 95% of SPMDD is obtained in the lower zone of the trench and 98% of SPMDD for the upper 1000 mm.

Impermeable clay should be provided across the entire width of the service trenches. It is recommended that the seals be at least 1.0 m in length along the trench (in accordance with the city of Ottawa Standard S8). The seals should be constructed at intervals no greater than 100 m along all sewer installations.

In areas of narrow trenches or confined spaces such as around manholes, catch basins, etc., the use of aggregate fill such as Granular 'B' Type I (OPSS 1010) is required if there is to be post-construction grade integrity.

6.10 Pavement Design

6.10.1 On-Grade Construction

Based on the existing topography of the site and the proposed grades, re-grading of the subgrade will be required. It is anticipated that the sub-grade material for the pavement will generally comprise of engineered fill.

The subgrade should be thoroughly proof-rolled and re-compacted to ensure uniformity in subgrade strength and support. Lift thicknesses should not exceed 200 mm in a loose state and the excavated site material should be compacted using heavy vibratory rollers. As an alternative, if suitable on-site native material is not available, the upper part of the subgrade could be improved by placing imported granular material.

If construction is carried out in inclement weather, there is a likelihood that some amount of road sub-base supplement will be required (i.e. some sub-excavation followed by granular replacement).

Given the frost susceptibility and drainage characteristics of the subgrade soils, the pavement design presented below is recommended.

Recommended Asphaltic Concrete Pavement Structure Design (Minimum Component Thicknesses)

Pavement Layer	Compaction Requirements	Light Duty Pavement Local Residential Routes	Heavy Duty Pavement Transit Routes
Surface Course	as per OPSS 310	40 mm Superpave 12.5 Level B Asphalt (PG58-34)	40 mm Superpave 12.5 Level D Asphalt (PG64-34)
Binder Course	as per OPSS 310	50 mm Superpave 19 mm Level B Asphalt (PG58-34)	100 mm Superpave 19 mm Level D Asphalt (PG64-34)
Granular Base	100% SPMDD	150 mm Granular 'A' (OPSS 1010) Pit Run or 19 mm Crusher Run Limestone	150 mm Granular 'A' (OPSS 1010) Pit Run or 19 mm Crusher Run Limestone
Granular Sub-Base	100% SPMDD	450 mm Granular 'B' Type II (OPSS 1010)	600 mm Granular 'B' Type II (OPSS 1010)

The subgrade must be compacted to at least 98% of SPMDD for at least the upper 600 mm and 95% below this level. The granular base and sub-base materials should be compacted to a minimum of 100% SPMDD.

The long-term performance of the proposed pavement structure is highly dependent upon the subgrade support conditions. Stringent construction control procedures should be maintained to ensure that uniform subgrade moisture and density conditions are achieved as much as practically possible when fill is placed and that the subgrade is not disturbed and weakened after it is exposed.

Control of surface water is a significant factor in achieving good pavement life. Grading adjacent to the pavement areas must be designed so that water is not allowed to pond adjacent to the outside edges of the pavement or curb. In addition, the need for adequate drainage cannot be overemphasized. The subgrade must be free of depressions and sloped (preferably at a minimum gradient of three percent) to provide effective drainage toward subgrade drains. Continuous sub-drains are recommended to intercept excess subsurface moisture at the curb lines and catch basins. The invert of sub-drains should be maintained at least 0.3 m below subgrade level.

Additional comments on the construction of pavement areas are as follows:

- As part of the subgrade preparation, the proposed pavement areas should be stripped of vegetation, topsoil, unsuitable earth fill and other obvious objectionable material. The subgrade should be properly shaped and sloped as required, and then proof-rolled. Loose/soft or spongy subgrade areas should be sub-excavated and replaced with suitable approved material compacted to at least 98% of SPMDD.
- Where new fill is needed to increase the grade or replace disturbed portions of the subgrade, excavated inorganic soils or similar clean imported fill materials may be used, provided their moisture content is maintained within 2% of the soil's optimum moisture content. All fill must be placed and compacted to not less than 98% of SPMDD.
- For fine-grained soils, as encountered at the site, the degree of compaction specification alone cannot ensure distress free subgrade. Proof-rolling must be carried out and witnessed by AA personnel for final recommendations of sub-base thicknesses.
- In the event that pavement construction takes place in the spring thaw, the late fall, or following periods of significant rainfall, it should be anticipated that an increase in thickness of the granular sub-base layer will be required to compensate for reduced subgrade strength.

6.10.2 Above Parking Garage Roof

The pavement above the parking garage roof slab may be comprised of a minimum of 75 mm thick layer of granular 'A' topped with asphaltic concrete having a minimum thickness of 80 mm (40 mm HL8 and 40 mm HL3). The asphaltic concrete materials should be rolled and compacted in accordance with OPSS 310 requirements.

The gradation and physical properties of HL-3 and HL-8 asphaltic concrete, and Granular 'A' shall conform to the OPSS standards.

The critical section of pavement will be at the transition between the pavement on grade and the pavement above the garage roof slab. In order to alleviate the detrimental effects of dynamic loading / settlement / pavement depression in the backfill to the rigid garage roof structure, it is recommended that an approach type slab be constructed at the entrance/exit points, by extending the granular subbase to greater depths along the exterior garage wall.

The granular courses of the pavement should be placed in lifts not exceeding 150 mm thick and be compacted to a minimum of 100% SPMDD.

6.11 Pavement Assessment: Old Hemlock Road

Evaluation of the existing pavement along old Hemlock Road was undertaken to assess the condition of the pavement structure and to provide recommendations for improvements/repairs prior to its use for construction traffic, transit vehicles and public access.

At the time of this investigation the road surface was covered with snow. As such, our visual examination of the pavement was limited to the visible sections of the road. It revealed that the pavement is generally in poor to fair condition with few areas of settlement and localized cracking.

Boreholes BH101, BH102, BH103, and BH167 were advanced along old Hemlock Road and extended to

depths ranging from 0.8 to 1.8 mbgs to determine the thickness and composition of the pavement structures as well as the compactness condition/consistency of the underlying subgrade.

The boreholes revealed that the thickness of the asphaltic concrete is about 140 mm. The base course supporting the asphaltic concrete consists of gravelly sand to sandy gravel. The thickness of this granular soil ranges from approximately 200 to 250 mm. Based on SPT results, it is inferred that the granular materials have been moderately to well compacted. The underlying subgrade soil consist of compact sandy silt to silty sand fill materials.

Test Pits TP201 and TP202 which were advanced immediately adjacent to Hemlock Road, revealed that the bedrock is situated at approximate depths of 1.4 and 1.1 mbgs respectively.

Sieve grain size analysis was carried out on one (1) sample of granular base course obtained from Borehole BH102 at 0.2 mbgs (Sample 1A). The test revealed that the soil has 70% sand, 28% gravel, and 2% silt and clay. The result of the grain size analysis is shown as Figure E-1 in Appendix D.

The condition of the existing pavement along old Hemlock Road is satisfactory for its temporary use for construction traffic. However, the thickness of the existing base course is not sufficient for long term use as a permanent public road. The proposed grading plan provided for our use by IBI Group does not include the Hemlock Road extension. However, we understand that it is not planned to change the grade of the current roadway. The provided recommendations are considered to be preliminary in nature, subject for review and revision upon completion of proposed grading plans.

The following recommendations are provided for preparation of the subgrade soils.

- Remove existing granular materials and stockpile selected materials which may be reused as granular sub-base;
- Lower the subgrade to design elevation and shape to promote drainage.
- In the event that soft and/or organic fill materials are contacted at subgrade elevation, these should be removed and replaced with a suitable native or imported soil which is compacted to 98% of the material's SPMDD.
- Densely compact the subgrade to improve the condition of the disturbed layers and fill materials and to ensure uniformity in subgrade strength and support.
- If construction is carried out in inclement weather, there is a likelihood that some amount
 of pavement sub-base supplement will be required (i.e. some sub-excavation followed by
 granular replacement). In such instances, it will be necessary to ensure that granular
 materials are properly drained by lowering the subdrains.

6.12 Lateral Earth Pressure

Parameters used in the determination of earth pressure acting on temporary shoring and basement walls are defined below.

Soil Parameters

Parameter	Definition	Units
Φ'	angle of internal friction	degrees
γ	bulk unit weight of soil	kN/m³
Κα	active earth pressure coefficient (Rankine)	dimensionless
Κο	at-rest earth pressure coefficient (Rankine)	dimensionless
Kp	passive earth pressure coefficient (Rankine)	dimensionless

The appropriate un-factored values for use in the design of structures subject to unbalanced earth pressures at this site are tabulated as follows:

Soil Parameter Values

Soil	Parameter					
	Φ'	Υ	Ka	Кp	K ₀	
Fill Material	28°	18	0.36	2.77	0.53	
Silty Sand to Sand	compact - 32°	19.0	0.31	3.25	0.47	
Silt to Sandy Silt	dense to very dense - 36°	19.0	0.26	3.85	0.41	
Clay and Silt	30°	20	0.33	3.00	0.5	
Bedrock	36°	25	0.26	3.85	0.41	

Walls or bracings subject to unbalanced earth pressures must be designed to resist a pressure that can be calculated based on the following formula:

$P = K (\gamma h + q)$

Where P =lateral pressure in kPa acting at a depth h (m) below ground surface

K = applicable lateral earth pressure coefficient

 γ = bulk unit weight of backfill (kN/m³)

q = the complete surcharge loading (kPa)

This equation assumes that free-draining backfill and positive drainage is provided to ensure that there is no hydrostatic pressure acting in conjunction with the earth pressure.

The coefficient of earth pressure at rest (K_0) should be used in the calculation of the earth pressure on the basement walls.

Resistance to sliding of earth retaining structures is developed by friction between the base of the footing and the soil. This friction (R) depends on the normal load on the soil contact (N) and the frictional resistance of the soil ($\tan \Phi$ ') expressed as: $R = N \tan \Phi$ '. This is an ultimate resistance value and does not contain a factor of safety.

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6.13 Earthquake Design Parameters

The 2012 Ontario Building Code (OBC) stipulates the methodology for earthquake design analysis, as set out in Subsection 4.1.8.7. The determination of the type of analysis is predicated on the importance of the structure, the spectral response acceleration and the site classification.

The parameters for determination of the Site Classification for Seismic Site Response are set out in Table 4.1.8.4.A of the 2012 OBC. The classification is based on the determination of the average shear wave velocity in the top 30 metres of the site stratigraphy, where shear wave velocity (vs) measurements have been taken. In the absence of such measurements, the classification is estimated on the basis of empirical analysis of undrained shear strength or penetration resistance. The applicable penetration resistance is that which has been corrected to a rod energy efficiency of 60% of the theoretical maximum or the (N60) value.

Based on the current and previous borehole and test pit information, the subsurface stratigraphy generally comprises surficial topsoil and asphaltic concrete pavement, underlain by fill material, followed by various native soils consisting of silty sand to sand, sandy silt to silt, and clay and silt soils, underlain by limestone bedrock at shallow depths. Based on the above, the site designation for seismic analysis is estimated to be Class B according to Table 4.1.8.4.A from the quoted code.

The site specific 5% damped spectral acceleration coefficients, and the peak ground acceleration factors are provided in the 2012 Ontario Building Code - Supplementary Standards SB-1 (September 14, 2012), Table 1.2, location Ottawa, Ontario.

6.14 Chemical Characterization of Subsurface Soil

Four (4) soil samples obtained from Boreholes BH108, BH127, BH153, and BH156 were submitted to Maxxam Analytics Inc. for pH index test, water-soluble sulphate, and chloride content to determine the potential of attacking the subsurface concrete and corrosion of steel pipelines. The test results are summarized below:

Soil Parameter	BH108: 0.76 mbgs (Sample 2)	BH127: 0.76 mbgs (Sample 2)	BH153: 1.5 mbgs (Sample 3)	BH156: mbgs (Sample)
рН	7.58	7.54	7.66	7.77
Water-soluble Sulphate (%)	0.0098	0.0026	ND	ND
Chloride (%)	ND*	ND	ND	ND

^{*}ND: Not Detected

The pH of the tested samples indicates a slight alkalinity. The concentration of water-soluble sulphate content of the tested samples is below the CSA Standard of 0.1% water-soluble sulphate (Table 12 of CSA A23.1, Requirements for Concrete Subjected to Sulphate Attack). Special concrete mixes against sulphate attack is therefore not required for the sub-surface concrete of the proposed buildings. The chloride content was not detected in the tested samples.

The Certificate of Analysis provided by the analytical chemical testing laboratory is contained in Appendix G of this report.

7 LIMITATIONS OF REPORT

The Limitations of Report, as quoted in Appendix 'A', are an integral part of this report.

Yours respectfully

alston associates

A division of Terrapex Environmental Ltd.

Rachel Herzog, CET

Geotechnical Technician

Shabnam Aziznejad, M.A.Sc.

Geotechnical Engineering Trainee

Vic Nersesian, P. Eng.

Vice President, Geotechnical Services

APPENDIX A LIMITATIONS OF REPORT

limitations of report

The conclusions and recommendations in this report are based on information determined at the inspection locations. Soil and groundwater conditions between and beyond the test holes may differ from those encountered at the test hole locations, and conditions may become apparent during construction which could not be detected or anticipated at the time of the soil investigation.

The design recommendations given in this report are applicable only to the project described in the text, and then only if constructed substantially in accordance with details of alignment and elevations stated in the report. Since all details of the design may not be known to us, in our analysis certain assumptions had to be made as set out in this report. The actual conditions may, however, vary from those assumed, in which case changes and modifications may be required to our recommendations.

This report was prepared for Canada Lands Company CLC Limited by Alston Associates. The material in it reflects Alston Associates judgement in light of the information available to it at the time of preparation. Any use which a Third Party makes of this report, or any reliance on decisions which the Third Party may make based on it, are the sole responsibility of such Third Parties.

We recommend, therefore, that we be retained during the final design stage to review the design drawings and to verify that they are consistent with our recommendations or the assumptions made in our analysis. We recommend also that we be retained during construction to confirm that the subsurface conditions throughout the site do not deviate materially from those encountered in the test holes. In cases where these recommendations are not followed, the company's responsibility is limited to accurately interpreting the conditions encountered at the test holes, only.

The comments given in this report on potential construction problems and possible methods are intended for the guidance of the design engineer, only. The number of inspection locations may not be sufficient to determine all the factors that may affect construction methods and costs. The contractors bidding on this project or undertaking the construction should, therefore, make their own interpretation of the factual information presented and draw their own conclusions as to how the subsurface conditions may affect their work.

APPENDIX B

DRAWING 1: SITE LOCATION

DRAWING 2: PROPOSED DEVELOPMENT PLAN

DRAWING 3: BOREHOLE AND TEST PIT LOCATION PLAN

DRAWING 4: PREVIOUS BOREHOLE AND TEST PIT LOCATION PLAN

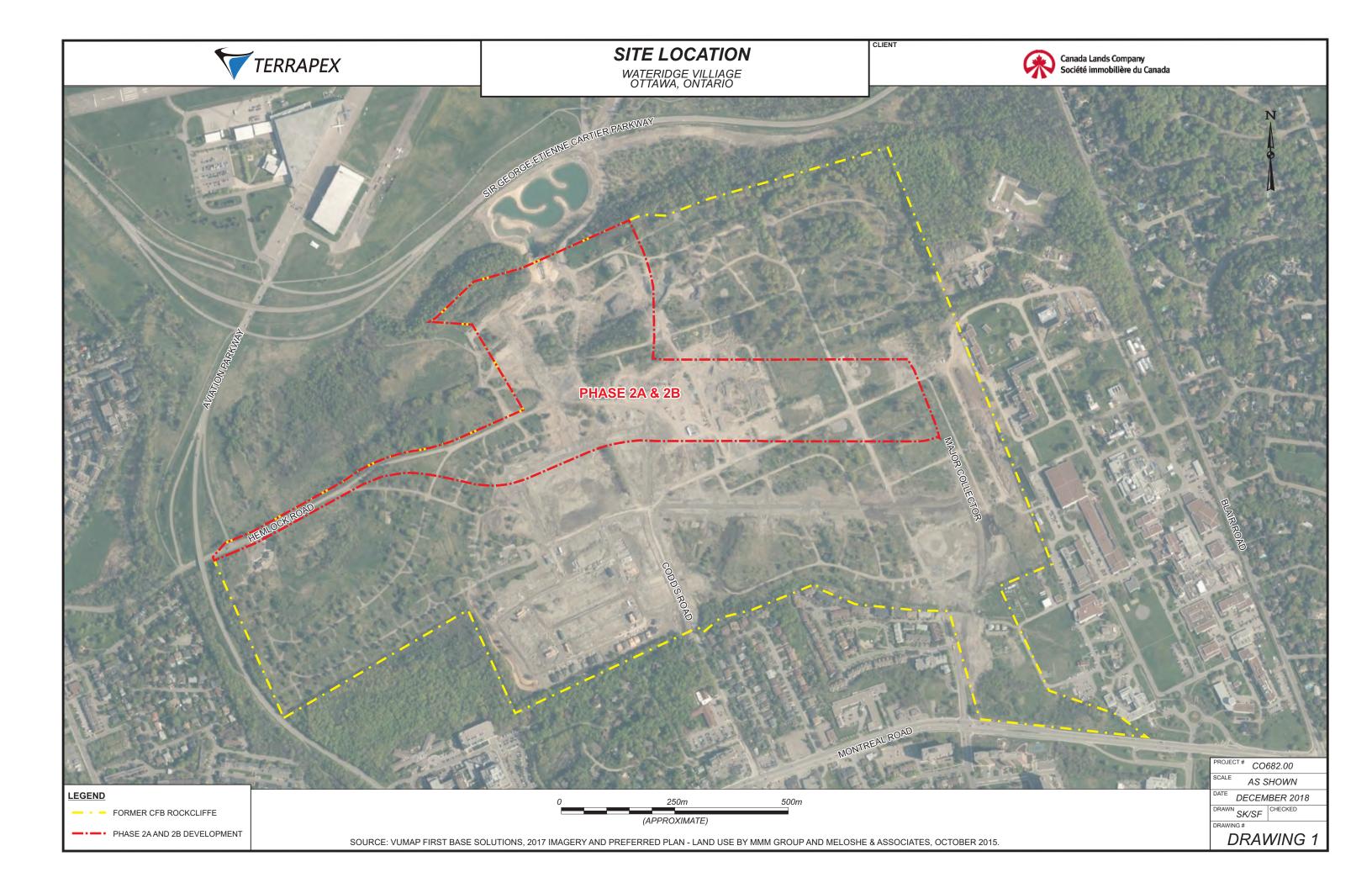
DRAWING 5: PROPOSED PARK 1

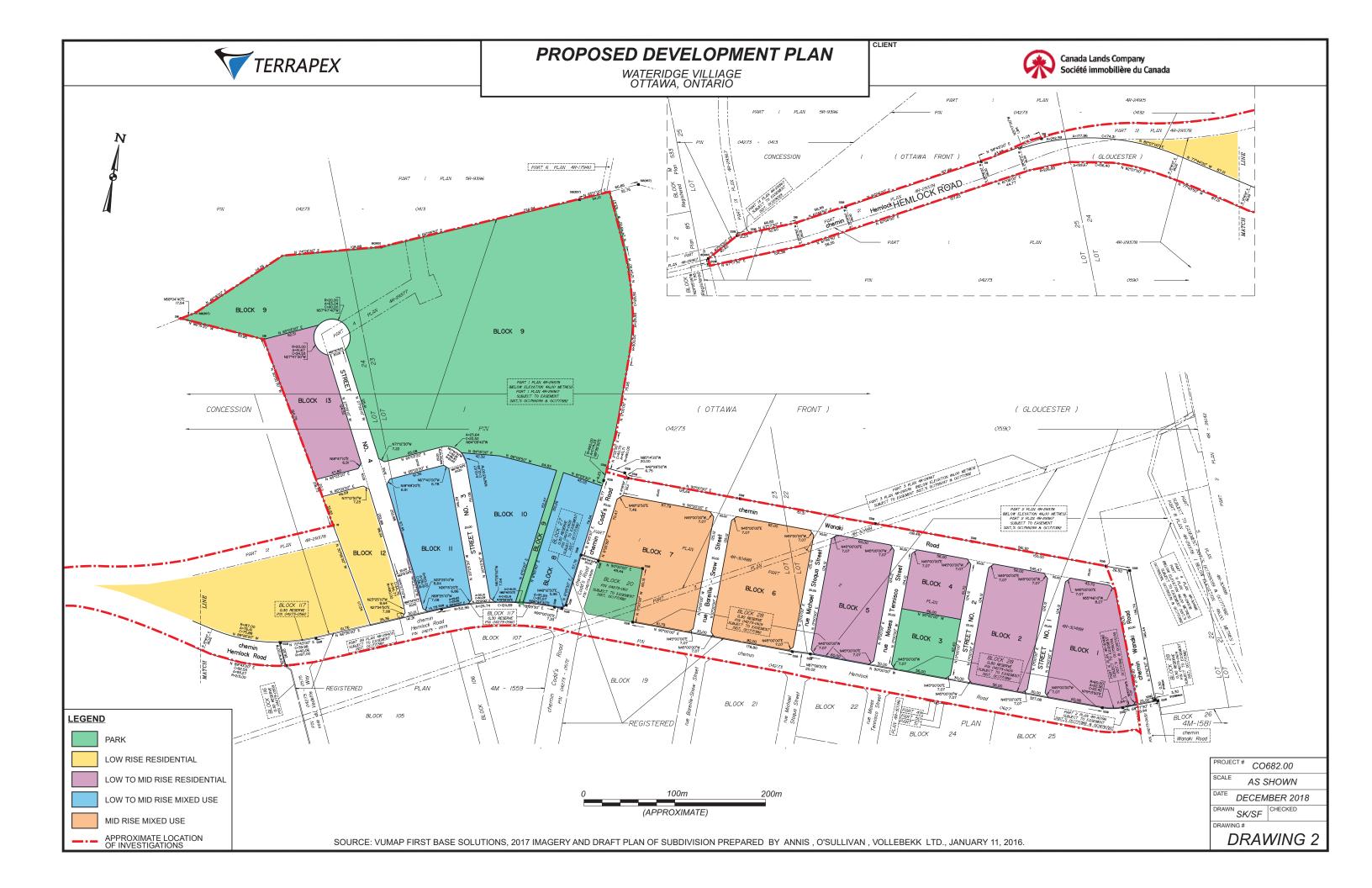
DRAWING 6: PROPOSED PARK 7

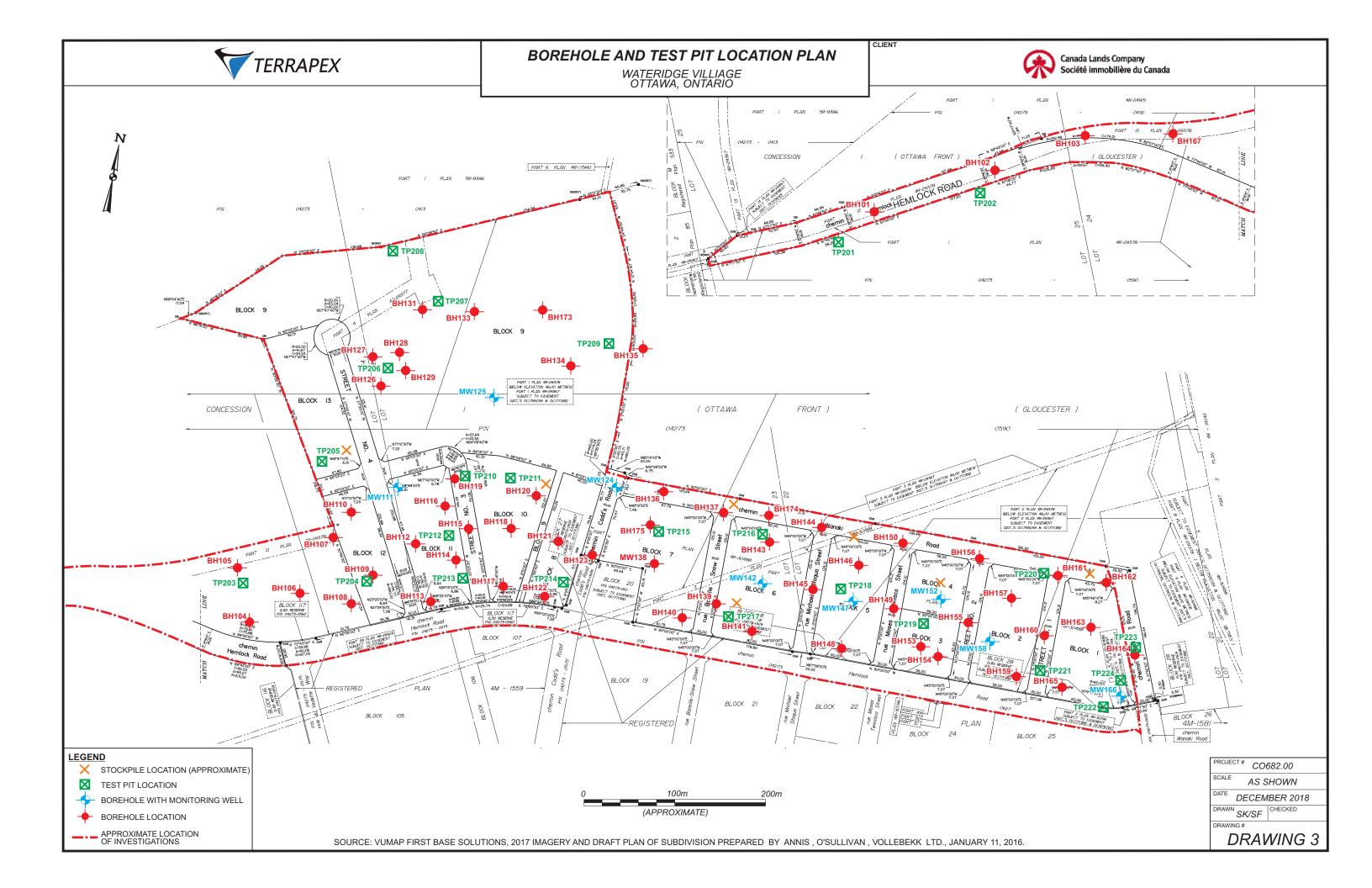
DRAWING 7: PROPOSED GRADING PLAN - PART OF PHASE 2B

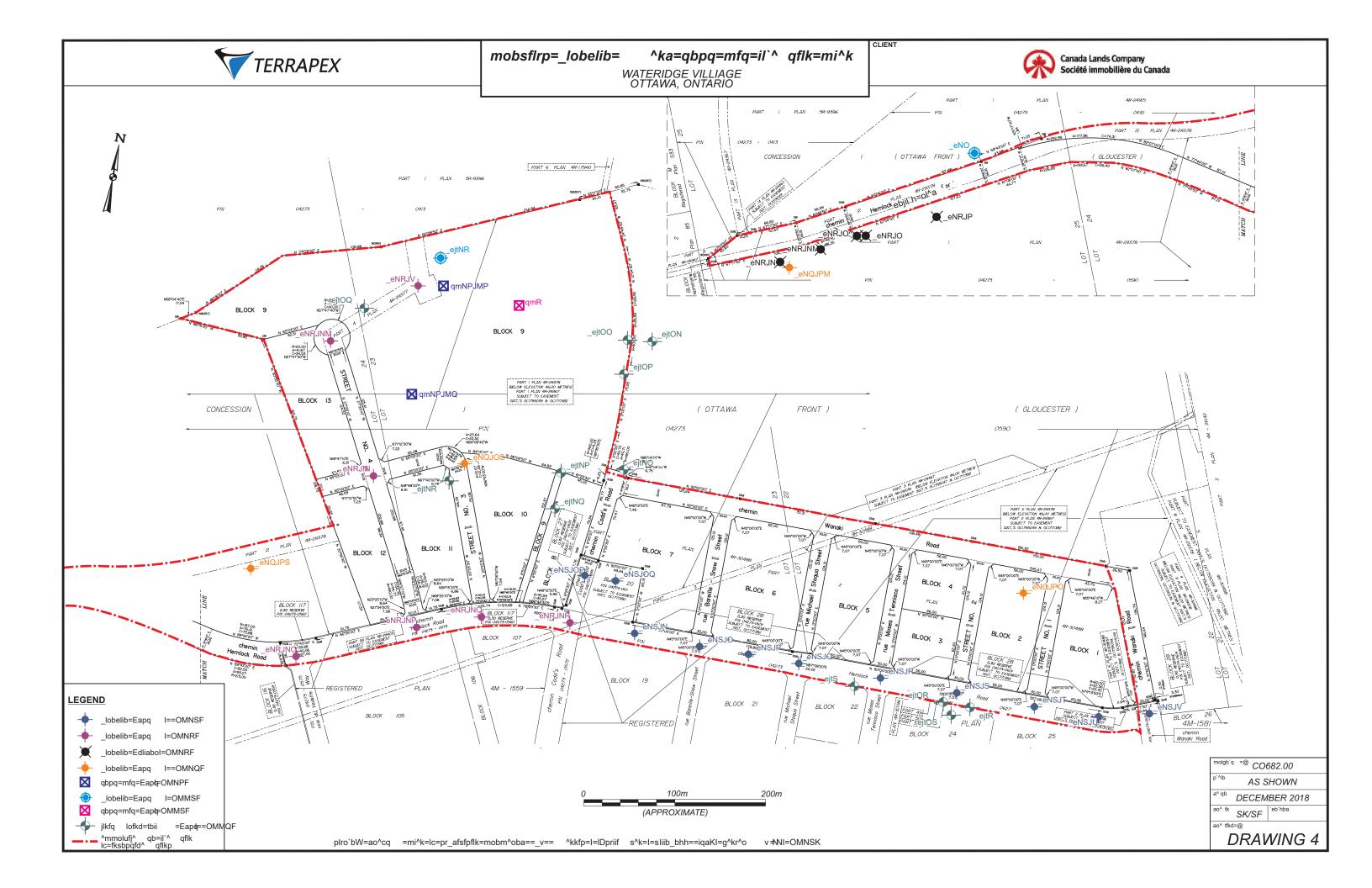
DRAWING 8: PROPOSED GRADING PLAN - PARTS OF PHASE 2A&2B

DRAWING 9: PROPOSED GRADING PLAN - PART OF PHASE 2A





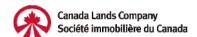






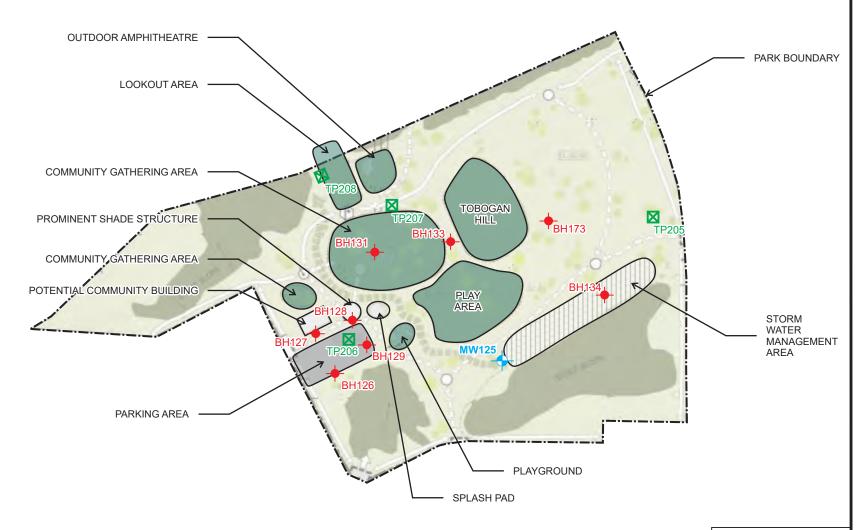
PROPOSED PARK 1: NORTH COMMUNITY PARK

WATERIDGE VILLIAGE OTTAWA, ONTARIO



CLIENT





LEGEND





BOREHOLE LOCATION



TEST PIT LOCATION

0 100m 200m (APPROXIMATE)

SOURCE: PARKS MASTER PLAN, FORMER CFB ROCKCLIFFE REDEVELOPMENT, PREPARED BY MMM GROUP LIMITED.

PROJECT# CO682.00

SCALE AS SHOWN

DATE DECEMBER 2018

DRAWN SF/SK CHECKED

DRAWING #

DRAWING 5

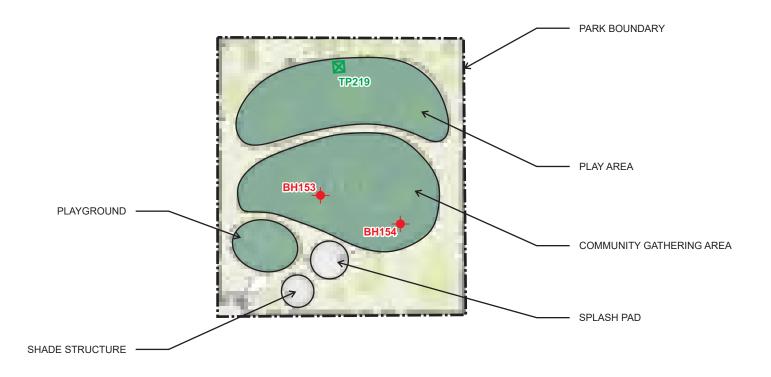


PROPOSED PARK 7: EAST PARKETTE

WATERIDGE VILLIAGE OTTAWA, ONTARIO CLIENT







LEGEND

→ BOREHOLE LOCATION

TEST PIT LOCATION



SOURCE: PARKS MASTER PLAN, FORMER CFB ROCKCLIFFE REDEVELOPMENT, PREPARED BY MMM GROUP LIMITED.

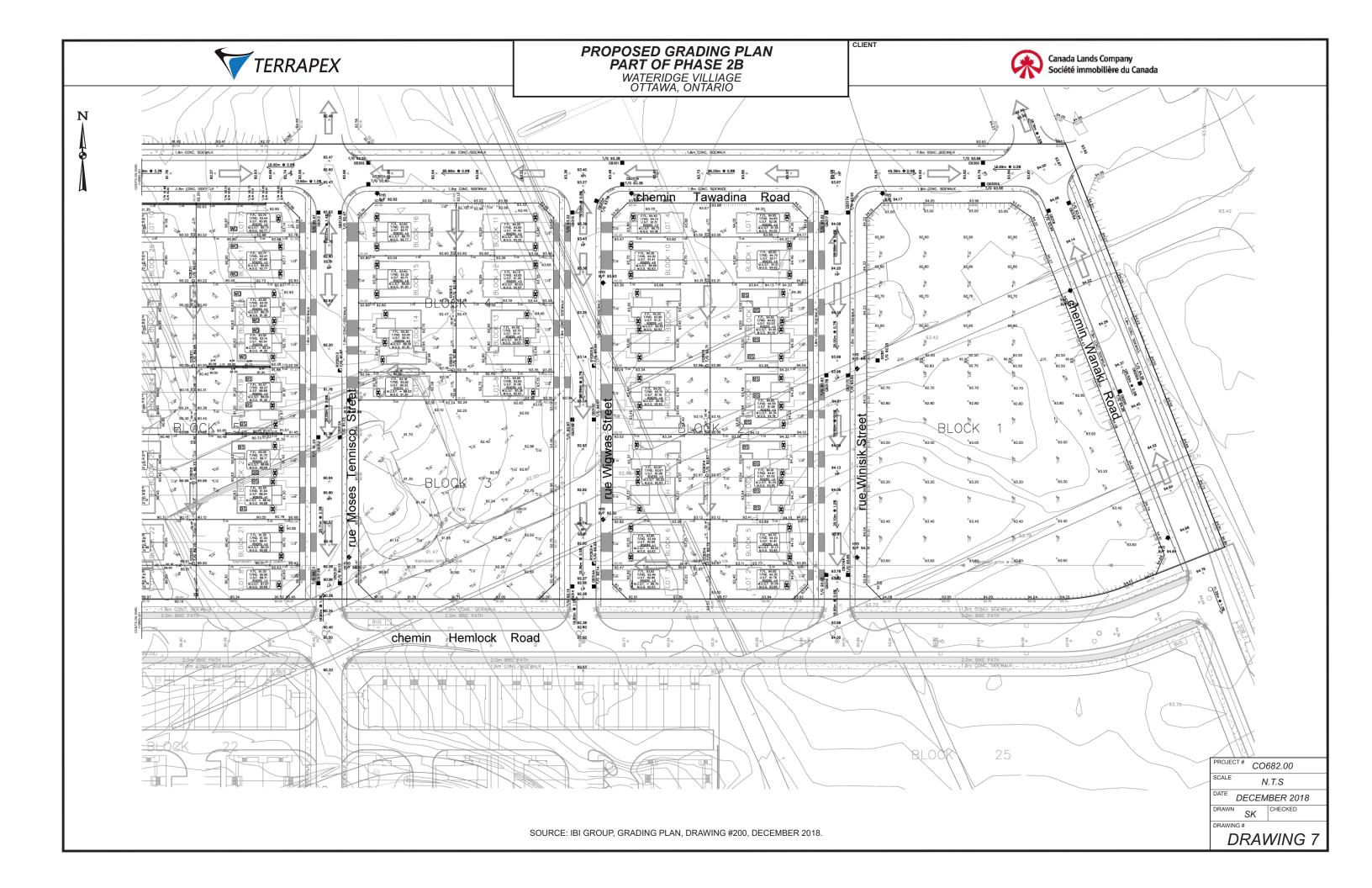
PROJECT# CO682.00

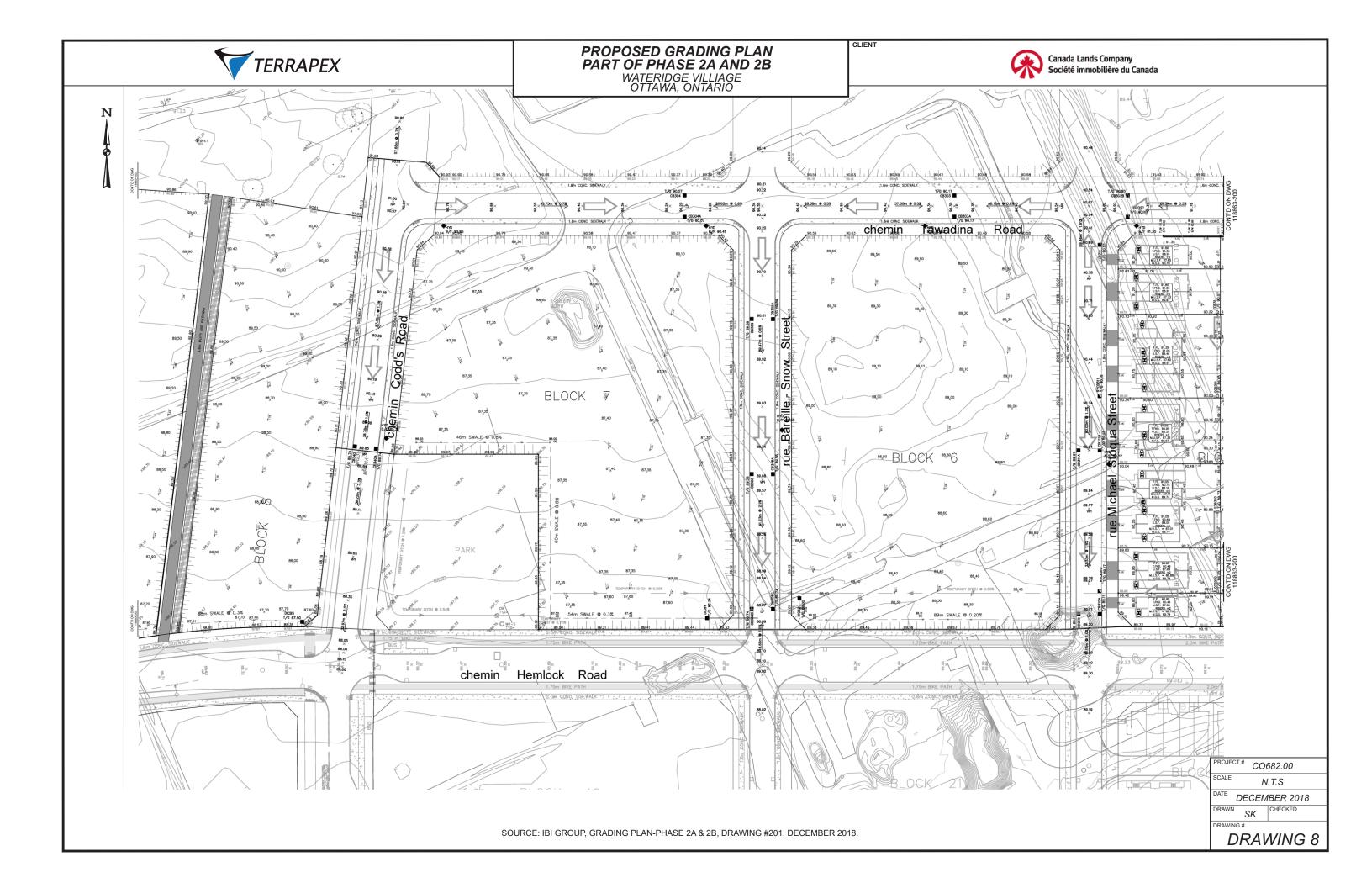
SCALE AS SHOWN

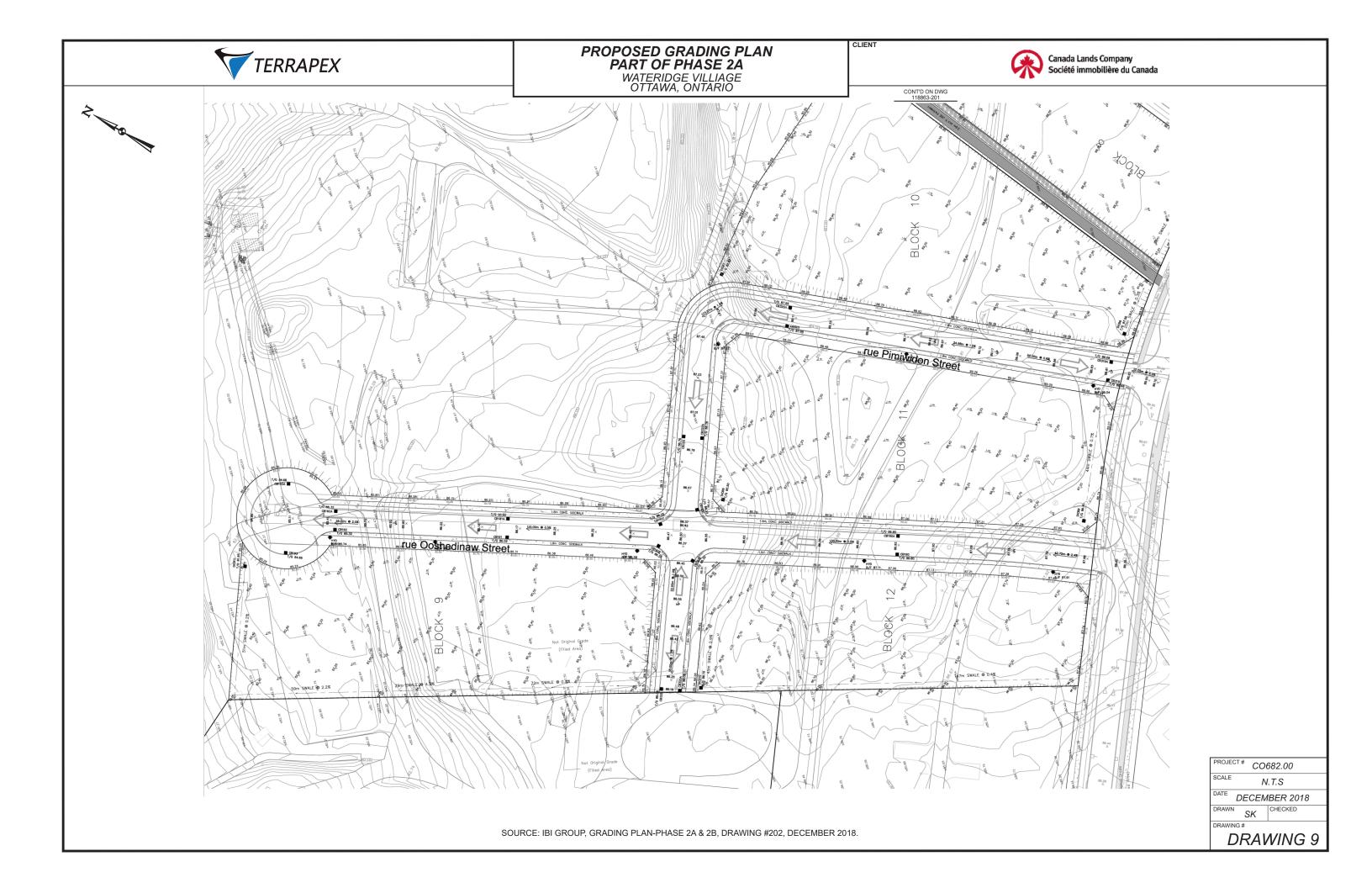
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DRAWING #

DRAWING 6







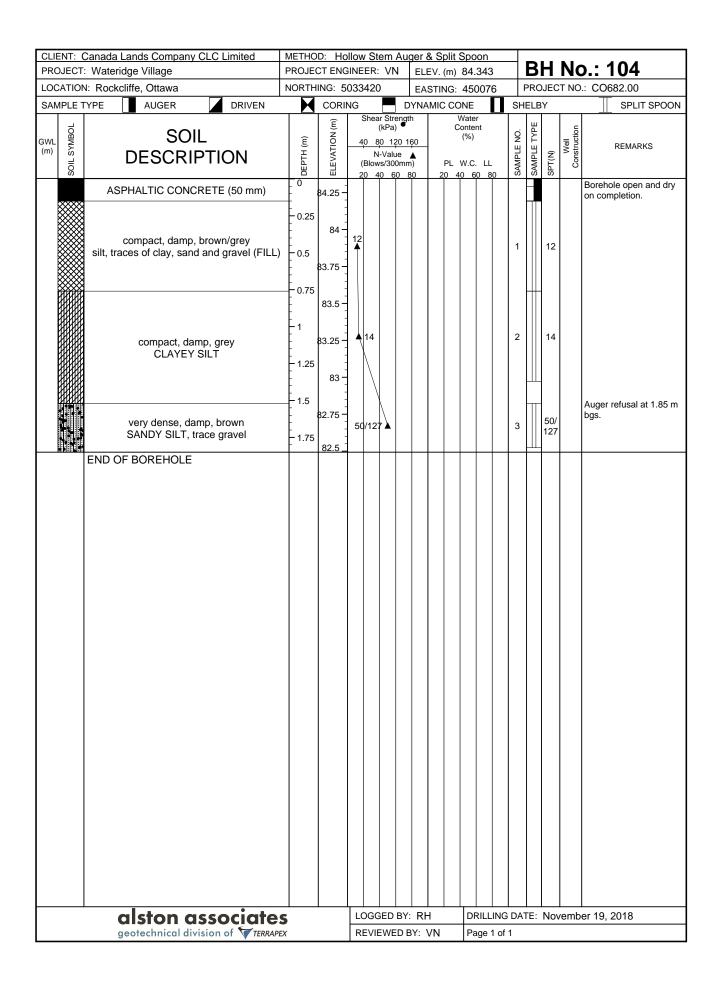
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۸	divisio	n of Torranov Environmental Ltd	

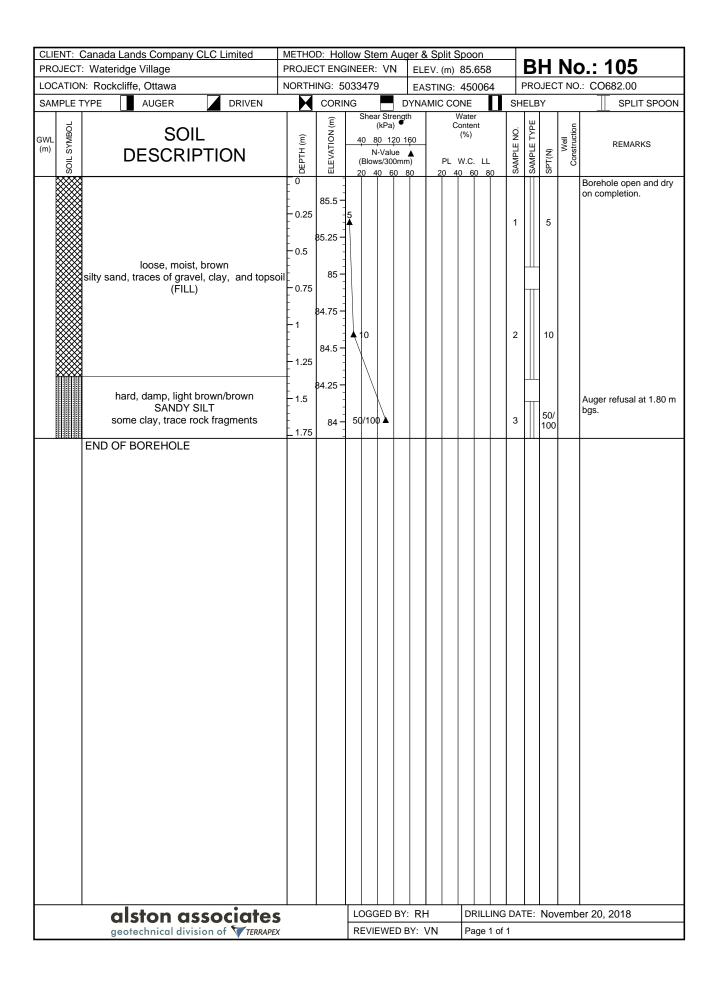
APPENDIX C BOREHOLE AND TEST PIT LOG SHEETS

CLIENT: Canada Lands Company CLC Limited	METHC PROJE					Г						-	R	Н	N	o.: 101
PROJECT: Wateridge Village LOCATION: Rockcliffe, Ottawa	NORTH				VIN				74.4							0:: CO682.00
SAMPLE TYPE AUGER DRIVEN	H	CORI		<u> </u>		DYNA				,033 [_	SHE			- 110	SPLIT SPOON
GWL OF SOIL DESCRIPTION	DEPTH (m)	ELEVATION (m)	4((E	Blows/	Streng 2a) 120 alue 300m	160 A m)		PL \	Water conter (%) W.C.	LL		Š.	SAMPLE TYPE	SPT(N)	Well Construction	
ASPHALTIC CONCRETE (140 mm)	0	-	20	0 40	60	80	2	20 4	0 60	0 80)	S	S	S		Borehole open and dry
	-0.25	74.25 - 74 - 73.75 - 73.5 - 73.25 -		25			5					1A 1B 1C 2		25		Borehole open and dry on completion.
alston associates geotechnical division of TERRAPEX			LC	GGE	D B	r: RI	Η		DF	RILLI	NG I	DAT	E:	Nov	remb	er 20, 2018

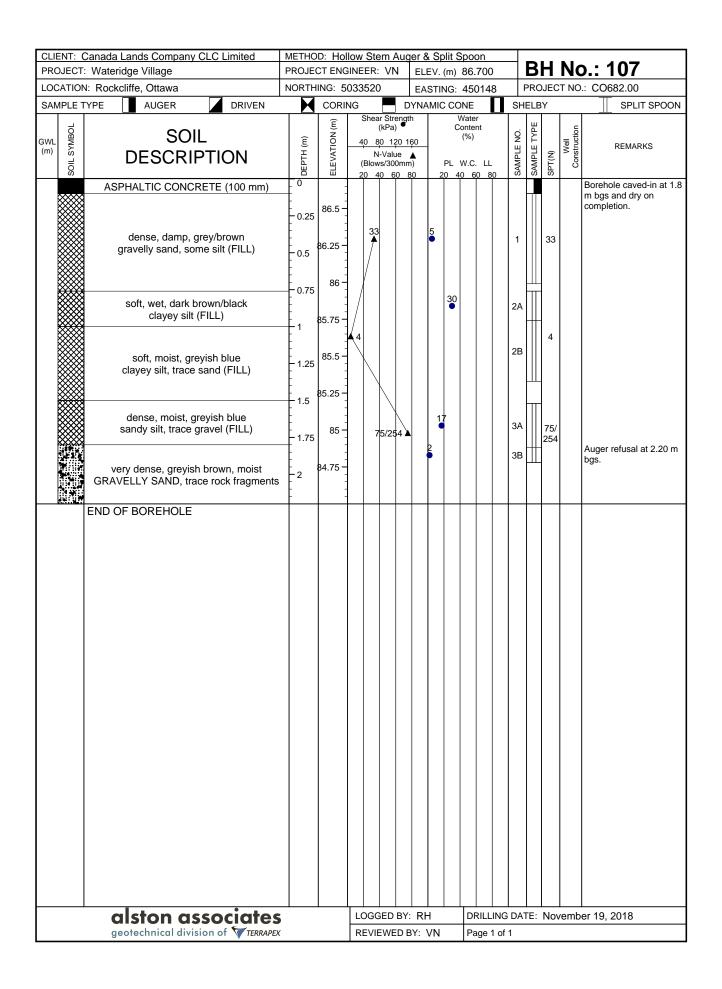
CLIENT: Canada Lands Company CLC Limited PROJECT: Wateridge Village	METHO PROJE					Г	r & S					R	Н	No	o.: 102
LOCATION: Rockcliffe, Ottawa	NORTH				V 1 4		:ASTI				\dashv				o: CO682.00
SAMPLE TYPE AUGER DRIVEN	H	CORII					NAMI			77.07		IELE			SPLIT SPOON
SOIL DESCRIPTION	DEРТН (m)	ELEVATION (m)	4((I	N-Y Blows) 120 Value 5/300	160 mm)		PL	Water Conter (%) W.C.	LL	SAMPLE NO.	ш		Well	
ASPHALTIC CONCRETE (140 mm)	0	77.5	20	0 40	60	80		20 4	40 60	0 80	- v	S	S		Borehole open and dry on completion.
GRANULAR BASE (250 mm)	0.25	77.25 -									1.4				on completion.
compact, damp, brown/dark brown silty sand, some gravel (FILL)	0.5	77 -	20								1E	;	20		
loose, moist, brown silt, some sand, traces of gravel and organics (FILL)	- 0.75 - - - - 1	76.75 <u> </u>		13			6				24		13		
compact, damp, brown SANDY SILT, trace rock fragments	- - 1.25	76.5 - 76.25 <u>-</u>									2E				
alston associates geotechnical division of TERRAPE	S =x		_			BY: F	RH : VN]	+	ge 1 d		TE:	No	vemb	er 20, 2018

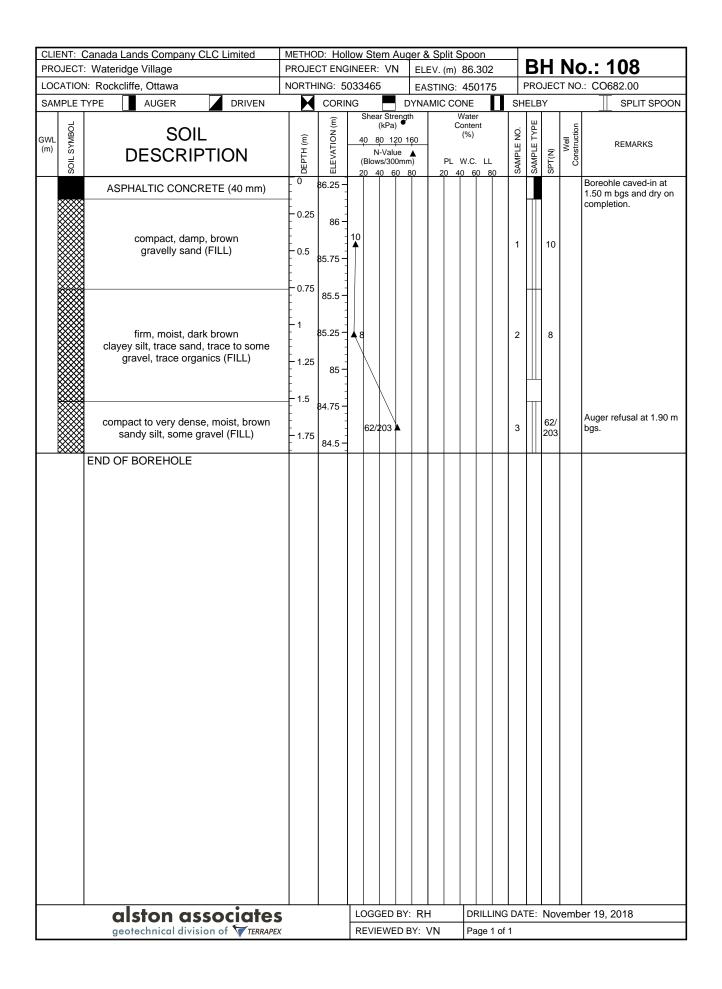
1			D: Ho						Spl V. (n				7	R	Н	No	o.: 103
	• •		ING: 5						STING								D.: CO682.00
SAMPLE TYP		H	CORII		.51				MIC			Π̈		ELB			SPLIT SPOON
GWL SYMBOL	SOIL DESCRIPTION	DEPTH (m)	ELEVATION (m)	41 (I	N- Blows	0 12 -Valu s/300	0 160 e 🛦)	Р	Wa Con (%	ater ntent %)		SAMPLE NO.	SAMPLE TYPE		Well	
65	ASPHALTIC CONCRETE (130 mm)	0	-	20	0 40	0 60	80		20	40	60	80	0)	0)	(O)		Borehole open and dry on completion.
	GRANULAR BASE (200 mm)	0.25	83.75 - - -										1A				
CC	ompact, damp, brown, sandy silt, traces of gravel and clay (FILL)		83.5 - - - - - 83.25 -	15	9								1B		19		
t	compact, damp, light brown layered SANDY SILT trace gravel, occassional oxidized layers.	- - - - - 1	83 - - - - 82.75 - -	23									2		23		
E	ND OF BOREHOLE																
	alston associates			LC	OGG	ED	BY:	 RH		_	 DRII	LING	DA ⁻	<u> </u> ГЕ:	Nov	emb	er 20, 2018
	geotechnical division of TERRAPEX			-			D BY			-		e 1 of					

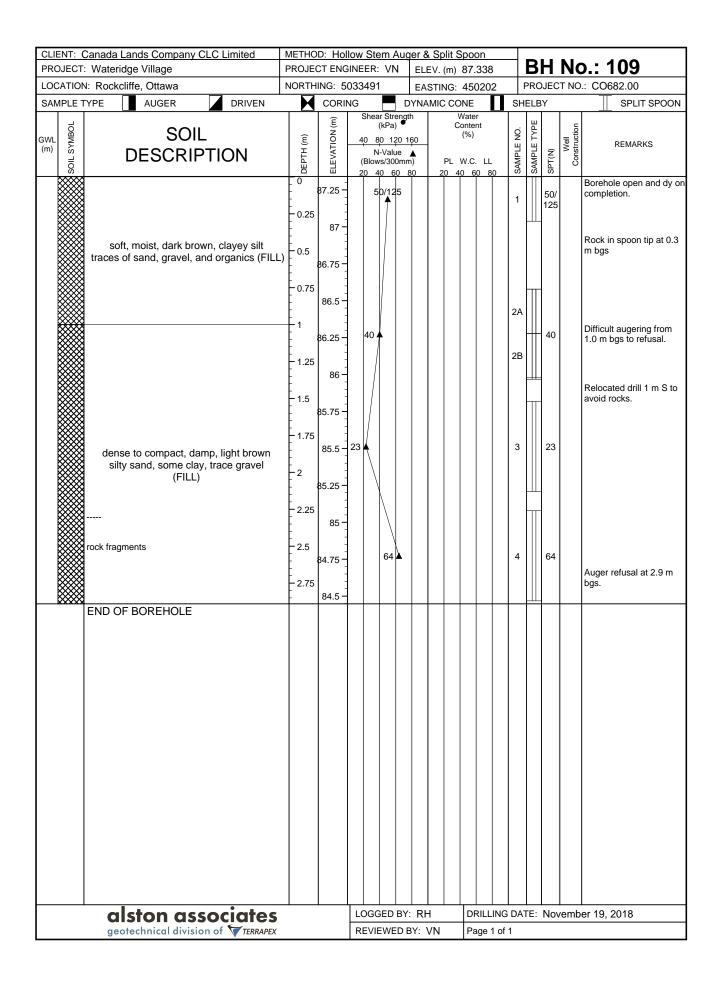




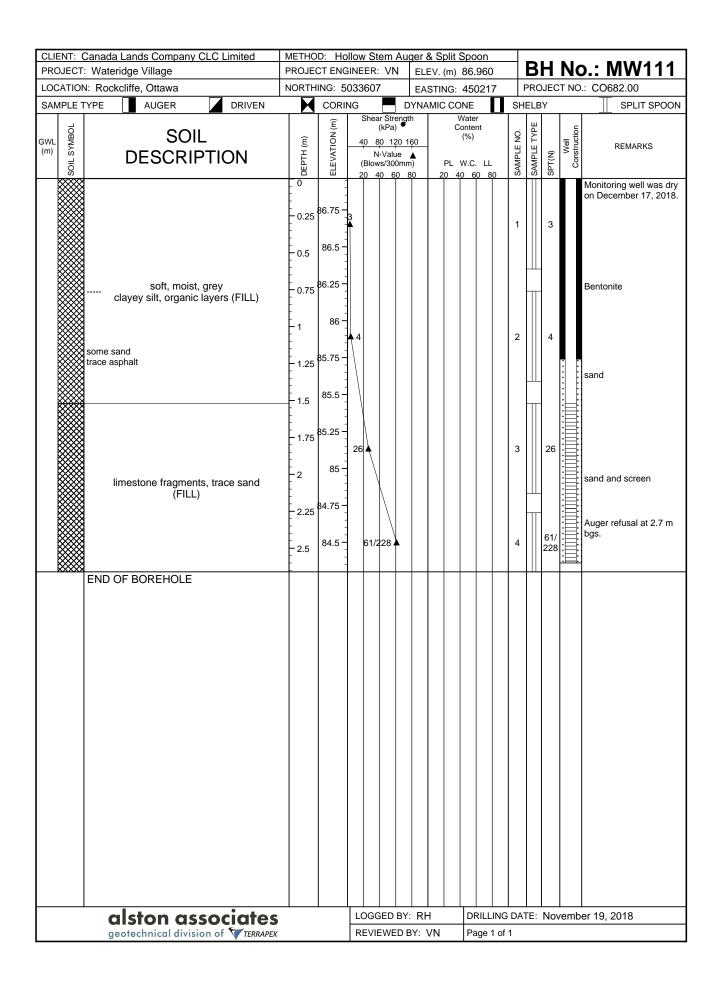
	Canada Lands Company CLC Limited Wateridge Village	METHO PROJE					1						R	Н	N	o.: 106
	l: Rockcliffe, Ottawa	NORTH				VIN				35.12 4501						0:: CO682.00
SAMPLE T		H	CORII		100		DYNA				П	SH			71 110	SPLIT SPOON
GWL SYMBOL SOIL SYMBOL	SOIL DESCRIPTION	DEРТН (m)	ELEVATION (m)	40 (B	Blows/	Stren Pa) 120 alue 300n	160 mm)	·	W Coi (ater Intent (%)		SAMPLE NO.	SAMPLE TYPE		Well	
, j	compact, moist, grey gravelly sand (FILL)		85 -	20	40	60	80	20) 40	60	80	1A	Š	S		Borehole open and dry on completion.
	very stiff, moist, brown CLAYEY SILT trace gravel, sand, and organics, occassional oxidized pockets	- 0.25 0.5 0.75	84.75 — 84.75 — 84.5 —	16								1B		16		Difficult to auger from 0.61 m bgs to refusal. Auger refusal at 1 m bgs.
	rock fragments END OF BOREHOLE	1	84.25 -	50	0/75	\						2		50/ 75		Auger refusal at 1 m bys.
	alston associates	-			GGE	:D P	Y: RI		\dashv	ייפח	LINIC	<u> </u>	L	No	/amh	l er 19, 2018
	alston associates geotechnical division of TERRAPE	5		-			BY: KI		_		± 1 of		ı E:	140/	/emb	19, 2018
	goolocilinear arvision or W TERRAPE	^		···	. v . L V	•	. J	V 1 N		. age	ان ، د	•				





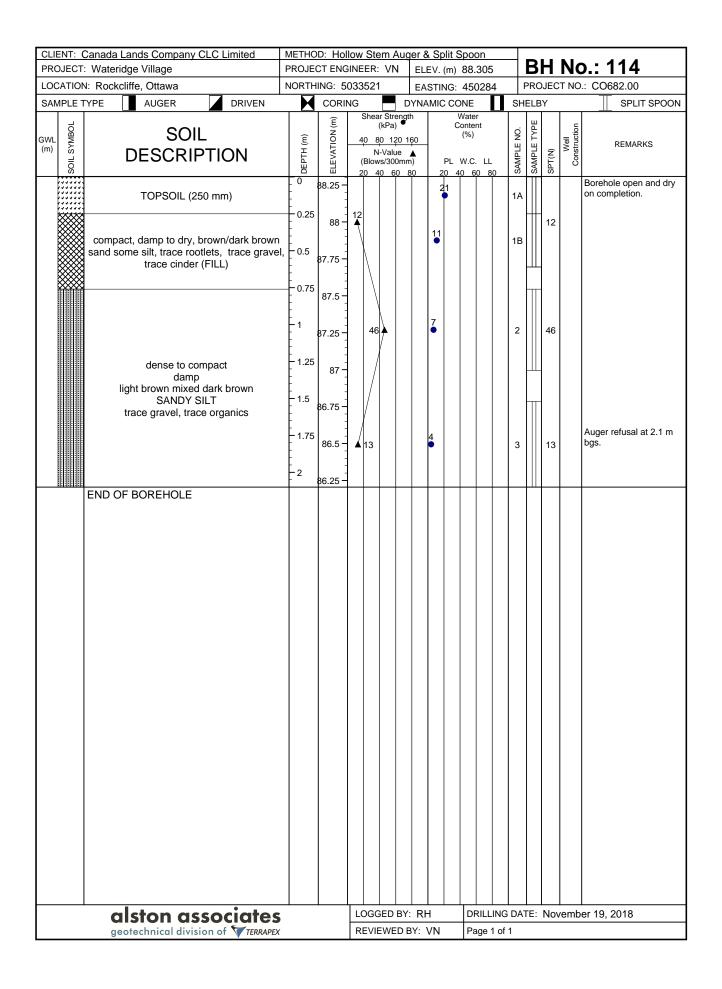


		METHC PROJE					7				oon 6.37	4		R	H	No	o.: 110
		NORTH					-+				5013						:: CO682.00
SAMPLE 1		H	CORII				_		VIC (П	SH				SPLIT SPOON
SOIL SYMBOL	SOIL DESCRIPTION	DEРТН (m)	ELEVATION (m)	41	0 8 N- Blow	0 12 -Valu	ength 20 160 le A Omm)		Pl	Wa Con (%	ter tent 6)		SAMPLE NO.	SAMPLE TYPE	SPT(N)	Well Construction	
	FROZEN GROUND	0	86.25		0 4	0 6	0 80		20	40	60 8	30	0,	0)	0)		Borehole caved-in at 0.91 m bgs and dry on
	very dense, damp, grey gravel, some sand (FILL)	- 0.25 - - - - - 0.5	86 — 				80	,					1A		80		completion.
	compact, damp to wet, brown sandy silt, some gravel, trace organics trace oxidization (FILL)	- - 0.75 - - - - - 1	-	31	ı 🛦								1B 2A		31		Auger refusal at 1.40 m bgs.
	compact to very dense, moist to wet, dark brown, silty gravel, trace sand, trace organics and rock fragments	1.25	-										2B				
	END OF BOREHOLE																
	alston associates			LC	ogg	ED	BY:	RH		[DRILL	ING	DAT	ΓE:	Nον	/emb	er 19, 2018
	geotechnical division of TERRAPEX			RE	VIE	WE	D BY	/: V	'N	F	Page	1 of	1				



	Canada Lands Company CLC Limited	METHO										Τ.		<u> </u>	NI.	. 112
	CT: Wateridge Village	PROJE:				'N	 		m) 88							D.: 112 D:: CO682.00
SAMPLE	ON: Rockcliffe, Ottawa	NORTH	CORI)34 =		_		G: 4		_	SHE			, I NO	SPLIT SPOON
GMT SYMBOL SYMBOL SYMBOL	SOIL DESCRIPTION	DEPTH (m)	ELEVATION (m)	40 (E	hear S (kP) 80 N-Va Blows/3	treng a) 120 ilue 00mi	160 A m)	P	War Cont (%	ter ent		SAMPLE NO.	SAMPLE TYPE	SPT(N)	Well Construction	
W W	FROZEN GROUND	0	— — - -	20	40	60	80	20	40	60 8	80	S	S	S		borehole open and dry on completion.
	dense, moist, brown sand and gravel, trace organics (FILL)	0.25	88.25 -									1A				
	very dense, damp, light brown	0.5	88 -		36							1B		36		
	SANDY SILT trace organics	0.75	87.75 -		0/220							•		58/		Auger refusal at 1.2 m
	rock fragments occassional oxidized pockets	- 1 - - -	87.5		8/228							2		228		bgs.
	END OF BOREHOLE															
	alston associates			-	GGE				-				E:	Nov	/emb	er 19, 2018
	geotechnical division of TERRAPE	(KE	VIEW	בט	BY:	VIV		age	ı Of 1	_				

CLIENT: Canada Lands Company CLC Limited PROJECT: Wateridge Village	METHO PROJE							87.8			R	Н	No	o.: 113
LOCATION: Rockcliffe, Ottawa	NORTH				••			450		\dashv				0:: CO682.00
SAMPLE TYPE AUGER DRIVEN	H	CORI		—	-	DYNA			П	_	IELE			SPLIT SPOON
SOIL DESCRIPTION	DEPTH (m)	ELEVATION (m)	40 (B	hear S (kP 80 N-Va llows/3	treng a) 120 ilue 00mi	160 A m)	V C	Vater ontent (%) W.C.	LL	SAMPLE NO.	SAMPLE TYPE		Well	
compact, damp, dark brown sandy gravel mixed with organics (FILL)	- 0.25 0.5 	87.5 - 87.25 -	10							1		10		Borehole open and dry on completion. Difficult augering to 0.76
silty sand, large gravel (FILL) END OF BOREHOLE	- 0.75 - - - - - 1	87 -	50)/75						2		50/ 75		m to refusal at 1.0 m bgs
alston associates	_ '		LO	GGE	D BY	′: RI		DR	ILLIN	G DA	TE:	Nov	/emb	er 19, 2018



	Canada Lands Company CLC Limited	METHO										_	4	_ D	ш	NI.	o.: 115
	: Wateridge Village N: Rockcliffe, Ottawa	PROJE NORTH							V. (m				-				:: CO682.00
SAMPLE 1		NORTH	CORI		JJJ				MIC C			is	_	ELB		, I NO	SPLIT SPOON
GWL (W)	SOIL DESCRIPTION	DEPTH (m)	ELEVATION (m)	4!	0 80 N- Blows	0 12 Valu s/300	0 160 e A 0mm)	0	PL	War Cont (%	ter tent 6)		SAMPLE NO.	SAMPLE TYPE	SPT(N)	Well	
	ASPHALTIC CONCRETE (40 mm) dense, damp, brown gravelly sand, trace asphalt (FILL) very dense, damp, brown sandy silt, traces of gravel and rock fragments (FILL) END OF BOREHOLE	- 0.25 0.25 0.5 0.75	89 — 88.75 — 88.5 —	20	Blow:	s/300 0 60	e				C. LI		1 2	SAMP	1 44 50/100		Borehole open and dry on completion. Relocated drill 1 m N, confirmed bedrock depth of 1.0 m bgs. Auger refusal at 1.0 m bgs.
	alston associates	S					BY: D BY			-	DRILI Page			TE:	Nov	/emb	er 19, 2018

	Canada Lands Company CLC Limited : Wateridge Village	METHO PROJE							Spli V. (n			3	Ŧ	R	H	No	o.: 116
	Rockcliffe, Ottawa	NORTH					-		STING								.: CO682.00
SAMPLE T		H	CORII				_		MIC (П	SH				SPLIT SPOON
SOIL SYMBOL	SOIL DESCRIPTION	DEPTH (m)	ELEVATION (m)	4	Shear 0 8 N- Blow	0 12 -Valu	20 16 le	0 \	Pl	Wa Con (%	ater ntent %)		SAMPLE NO.	ш	SPT(N)	Well	
	stiff, moist-wet, grey clayey silt (FILL) loose, moist, brown/dark brown sandy silt, traces of organics and cinder (FILL) very dense, damp, light brown	- 0.25 - 0.5 - 0.75	89 88.75 88.5	9		5/22			20	40			1A 1B		9		Borehole open and dry on completion. Auger refusal at 1.44 m
	SANDY SILT occassional oxidized pockets	1.25	88 - - - - 87.75 -												228		bgs.
	alston associates	'		Lo	OGG	ED	BY:	RH	1		DRIL	LING	DA ⁻	<u>'</u> ΓΕ:	Nον	/emb	er 19, 2018
	geotechnical division of TERRAPEX			R	EVIE	WE	D B	Y: \	/N	-	Page						

	Canada Lands Company CLC Limited : Wateridge Village	METHO PROJE									poo 88.0			F		1	No	o.: 117
	N: Rockcliffe, Ottawa	NORTH					\dashv				450							:: CO682.00
SAMPLE T		H	CORI				D,		MIC				s		BY			SPLIT SPOON
SOIL SYMBOL	SOIL DESCRIPTION	DEPTH (m)	ELEVATION (m)	4	0 8 N (Blow	ar Stre (kPa) 30 12 I-Valu vs/300	ength	0 \	F	V Co	Vater ontent (%) W.C.	LL	CN H IDMAN		1 Y P E		Well Construction	
	compact, moist, brown mixed grey sandy silt, traces of clay and gravel (FILL) loose, moist, dark brown/black sandy silt, some organics (FILL)	-0.5	87.75 - 87.5 - 87.25 -	12									1/	A		12		Borehole open and dry on completion. Auger refusal at 1.23 m
	firm, moist, brownish grey clayey silt, trace sand (FILL)	- - 1 -	87 -		10								2			10		bgs.
	END OF BOREHOLE																	
	alston associates		<u> </u>	_		EWE					_	ILLIN ge 1 d		ATE	: N	lov.	emb	er 16, 2018

	Canada Lands Company CLC Limited : Wateridge Village	METHO PROJE									Spoo 88.				R	Н	N	o.: 118
	N: Rockcliffe, Ottawa	NORTH					٧				450			-				D.: CO682.00
SAMPLE T		H	CORI		301		D.	YNA				J340	П	SH.			71 140	SPLIT SPOON
GWL SYMBOL SOIL SYMBOL	SOIL DESCRIPTION	DEPTH (m)	ELEVATION (m)	4 (1	Blow	0 12 -Valu	ength 20 16 ue 2 0mm	0 (0 (1)) C	Water conter (%)	nt . LL		SAMPLE NO.	SAMPLE TYPE	SPT(N)	Well	
(11111111111111111111111111111111111111	TOPSOIL (200 mm)	0	88 -	2	0 4	0 6	0 8	0	2	37	0 6	0 80	0	1A		0)		Borehole open and dry on completion.
	loose, moist, dark brown sandy silt, traces of cinder and rootlet (FILL	L	87.75 - 87.75 - 87.5 -	5						31				1B		5		
	dense, moist brown with grey mottling SANDY SILT, some clay, trace gravel occassional oxidized pockets END OF BOREHOLE	0.75	87.25 -	5	0/50				12					2		50/ 50		Auger refusal at 0.96 m bgs.
	alston associates			LC	OGG	ED	BY:	RH	<u>. </u>	_	DF	RILLI	ING	DA	ΓE:	Nov	vemb	er 16, 2018
	geotechnical division of TERRAPEX			RI	EVIE	WE	DΒ	Y: \	/N		Pa	ige 1	l of	1				

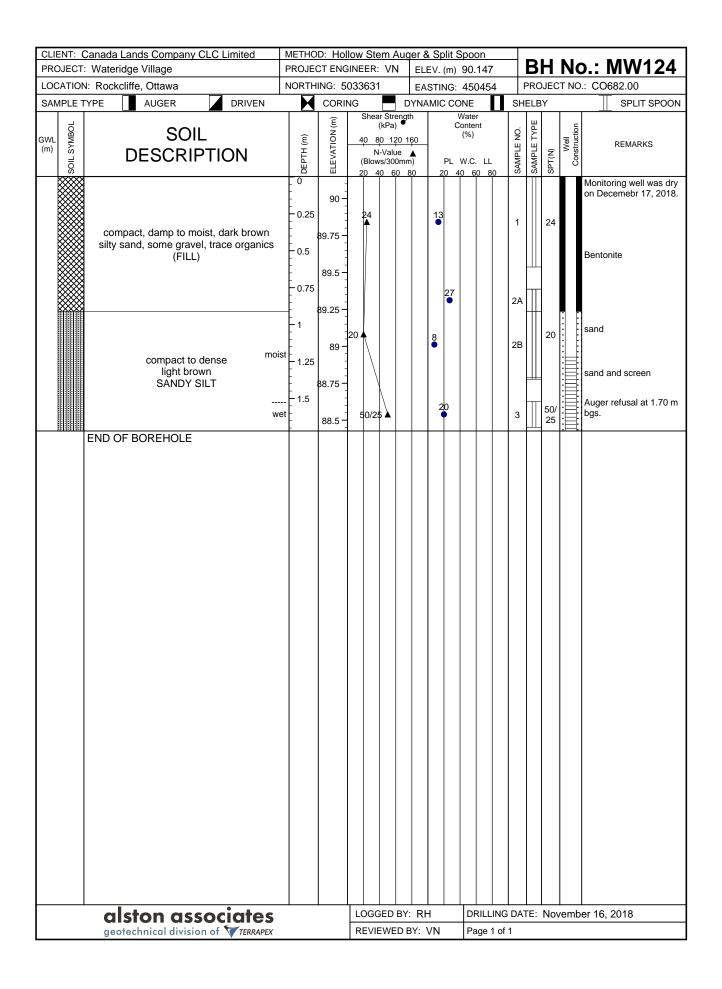
	Canada Lands Company CLC Limited	METHO PROJE					7				-	R	Н	N	o.: 119
	: Wateridge Village N: Rockcliffe, Ottawa	NORTH					_	'. (m) 'ING:							D.: CO682.00
SAMPLE T		H	CORI		010			IC CC		J201	SHI			1110	SPLIT SPOON
GWL SYMBOL GRAND	SOIL DESCRIPTION	DEРТН (m)	ELEVATION (m)	4!	N- Blows	0 12 Value s/300	160 mm)	PL	Wate Conte (%)	nt . LL	SAMPLE NO.	rype		Well	
(E) (S) (S) (S) (S) (S) (S) (S) (S) (S) (S	very dense, moist, dark brown sand and gravel, large rock in spoon (FILL) END OF BOREHOLE	_ 0 - -	88.5 - 88.25 -	(1	N- Blows	Value s/300	• 🛦	PL 20 4			Nample Sample	SAMPLE -	80 SPT(N)	W	Borehole open and dry on completion. Auger refusal at 0.65 m bgs.
	alston associates	.		-			BY: R	J	_	RILL		ΓE:	Nov	/emb	er 19, 2018

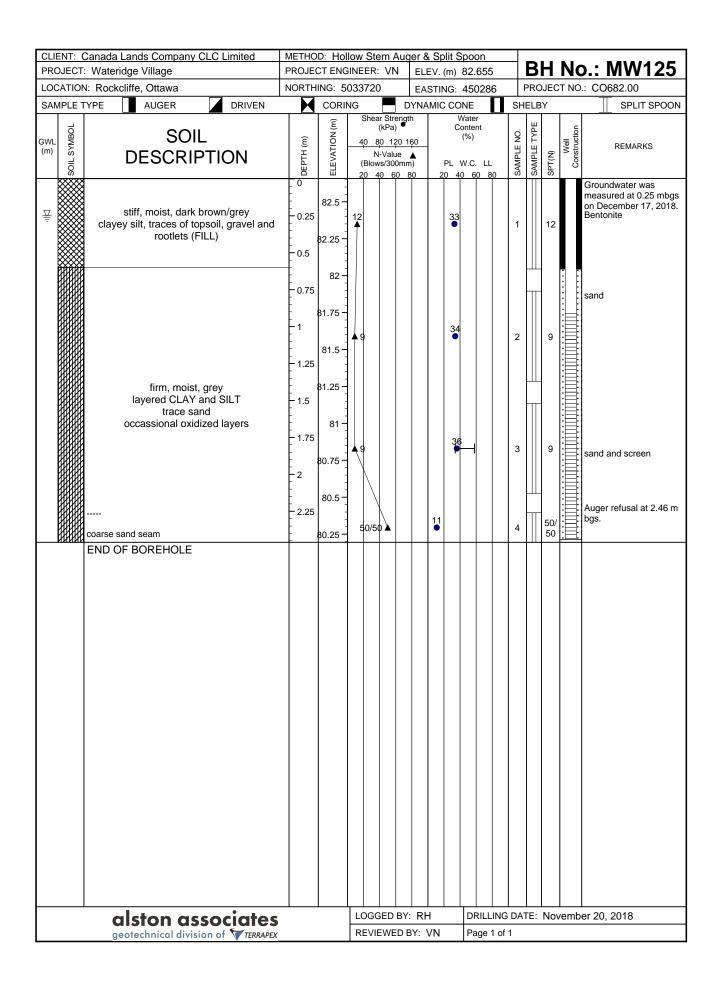
compact, moist, dark brown/brown gravelly sand, traces of inder and rootlets (FiLL) 10.5 89.25 14 15 15 15 15 15 15 15 15 15 15 15 15 15			METHO					7						\exists	R	—	N	n · 120
SOIL DESCRIPTION SOIL SOIL SOIL SOIL SOIL SOIL SOIL SOI								-										
SOIL DESCRIPTION SOIL DESCRIP						000						1340	_				71 110	
compact, moist, dark brown/brown gravelly sand, traces of cinder and rootlets - 0.25 89.25 - 13	GWL SYMBOL	SOIL			4((E	0 80 N- Blows) 12 Valu	ngth 0 160 e 🛦 mm)		PL	Wate Conte (%)	nt . LL					Well	
very dense, damp, light brown SILT some sand, trace clay 1 88.5 100/280 1 2 100/2 20 Auger refusal at 1.20 n bgr. END OF BOREHOLE 2 1 100/280 1 2 100/2 20 Auger refusal at 1.20 n bgr.		gravelly sand, traces of cinder and rootlets	0 - 0.25	89.5		0 40) 60	0 80		20 2	40 6	0 80						Borehole open and dry on completion.
alston associates LOGGED BY: RH DRILLING DATE: November 16, 2018		SILT	- - - - - - - - -	88.75 - 			10	00/280								100/ 280	(Auger refusal at 1.20 m bgs.
	Marianalli:	END OF BOREHOLE											\top					
		alston associates			LC) GGI	ED I	 3Y: F	LL RH		DF	LLLI RILLI	NG I	LL DAT	Œ:	No۱	/emb	Ler 16, 2018
geotechnical division of TERRAPEX REVIEWED BY: VN Page 1 of 1		geotechnical division of TERRAPEX								J	_							

	Canada Lands Company CLC Limited	METHO											4	D	ш	NI.	o.: 121
	: Wateridge Village N: Rockcliffe, Ottawa	PROJE					-			n) 88 G: 45							.: CO682.00
SAMPLE		NORTH	CORI		5550	,				ONE		$\overline{\Box}$		ELB		, I INC	SPLIT SPOON
GWL (m)	SOIL DESCRIPTION	DEРТН (m)	ELEVATION (m)	4	0 8 N Blow	r Stre (kPa) 0 12 -Valu	ength 60 160 e 🛦	0	PL	Wat Conte (%)	er ent)		SAMPLE NO.	ΓΥΡΕ		Well	
AS TIOS AS TIO	ASPHALTIC CONCRETE (75 mm) compact, moist to wet, dark brown sandy gravel, trace asphalt (FILL) END OF BOREHOLE	-0.25	88.25 - 88.25 - 88 -	(N Blow	-Valu	e ▲ Omm)	١.		L W.C.			1 1	SAMPLE	(N) LdS	W Constr	Borehole open and dry on completion. Auger refusal at 0.80 m bgs.
	alston associates	5		-		SED EWE				-	RILL age			TE:	Nov	/emb	er 16, 2018

	Canada Lands Company CLC Limited : Wateridge Village	METHO PROJE					T I	-	(m)	88.02	20		В	Н	No	o.: 122
	N: Rockcliffe, Ottawa	NORTH				-				4503						.: CO682.00
SAMPLE 1		H	CORI				DYN				П	SH	ELE	SY		SPLIT SPOON
SOIL SYMBOL	SOIL DESCRIPTION	DEPTH (m)	ELEVATION (m)	4((I	Shear (k 0 80 N-V Blows	120 /alue /300r	160 nm)		PL V	Vater ontent (%) W.C.		SAMPLE NO.	SAMPLE TYPE	SPT(N)	Well	
	moist, dark brown/black silt, some sand, some gravel (FILL)	- - - - 0.5	87.75 - 87.5 - 87.5 -													Borehole open and dry on completion.
	greyish blue, moist, hard clayey silt, trace sand, trace gravel (FILL)	- 1 - 1 - 1 - 1.25 - 1.5	87 - 86.75 -		36							1		36		Auger refusal at 1.52 m bgs.
	alston associates			-			Y: R BY:			 	LING e 1 of		TE:	Nov	/emb	er 16, 2018

CLIENT: Canada Lands Compa	any CLC Limited	METHO												Ŧ		ш	NI.		122	
PROJECT: Wateridge Village LOCATION: Rockcliffe, Ottawa		PROJEC									88.5 450								123 682.00	
SAMPLE TYPE AUGER	DRIVEN	NORTH	CORI		ააყ		_		MIC		450 NE	433 •	_	_	LB		INO	UU		T SPOON
GWL SO	OIL RIPTION	DEPTH (m)	ELEVATION (m)	4((I	N- Blow	0 12 Valu s/300	ength 20 16 le 🎍 Omm)	0	F	OC PL V	Vater onten (%) W.C.	t LL		ō.	rype		Well Construction		REMAR	
loose, m	oist, brown e gravel, trace clay	- 0.25 - 0.5 - 0.75	88.5	8	N- Blow	-Valu s/300 0 60	e 🛦	1		PL V				1 SAMPLEN	SAMPLE T	(N) LdS 8 50/25	Weil	Boreh on co	ole oper mpletion	and dry
alston (associates			-			BY:				_	ILLINge 1		DAT	E:	Nov	/emb	er 16,	2018	



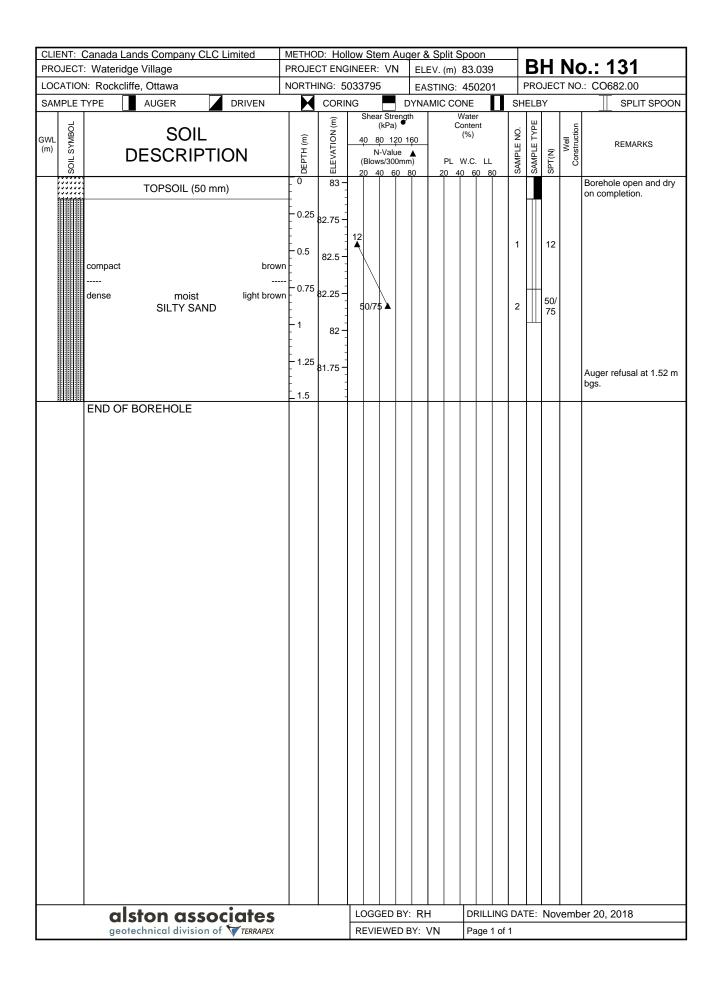


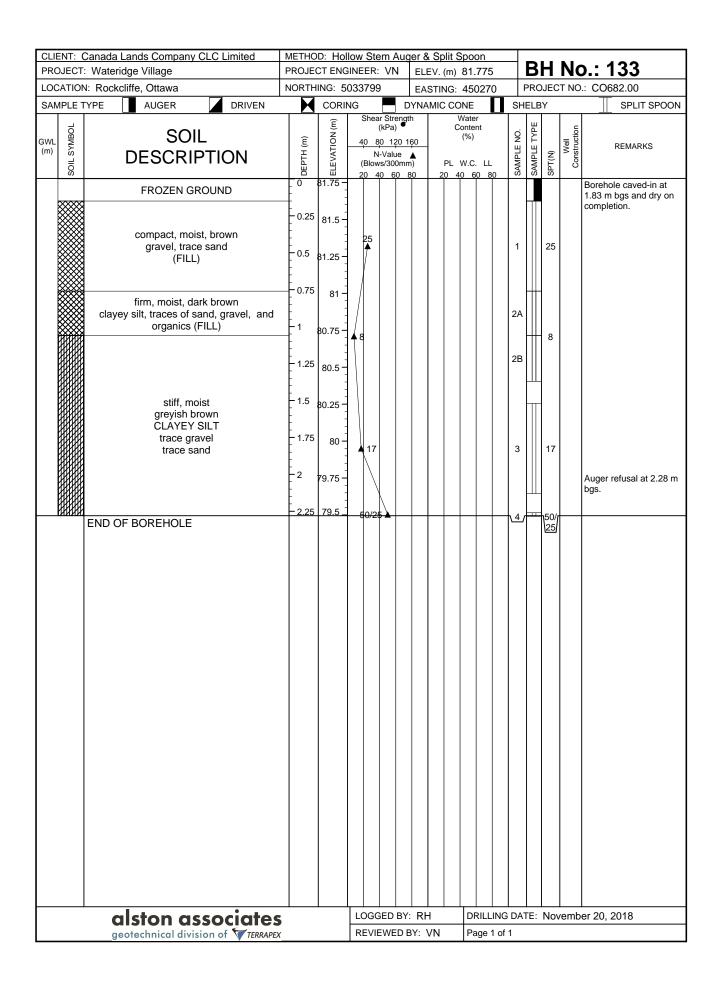
	Canada Lands Company CLC Limited : Wateridge Village	METHO PROJE							Spl V. (r					-	R	Н	N	o.: 126
	N: Rockcliffe, Ottawa	NORTH					-+		STIN									:: CO682.00
SAMPLE T		H	CORII						MIC				_	SHI				SPLIT SPOON
SOIL SYMBOL	SOIL DESCRIPTION	DE РТН (m)	ELEVATION (m)	4!	Shear 0 80 N- Blows	0 12 Valu s/300	20 16 le	0 \	P	W Co	/ater onten (%)	t LL		SAMPLE NO.	SAMPLE TYPE	SPT(N)	Well	
	compact, moist, brown gravelly sand, trace rock fragments (FILL)	0.25	84.25 — 	12	0 40	J 60	U 80	U	20) 40) 60) 80		1		12		Borehole open and dry on completion.
	compact, dry, brown SANDY SILT occassional oxidized layers trace rock fragments	- 0.75	83.75 - 83.5 - 83.25 -	25		\								2		25		
		- 1.5 -		50	/125	$ \mathbf{\lambda} $								3	П	50/ 125		Auger refusal at 1.65 m bgs.
	alatan aasasiatsa				ogg	ED	RV.	Pι			DB	11.7	NG	ראם	FF.	No	/amh	er 20, 2018
	alston associates geotechnical division of TERRAPEX			-	EVIE						-	ge 1			(C)	INUV	-CIIID	GI ZU, ZU IO

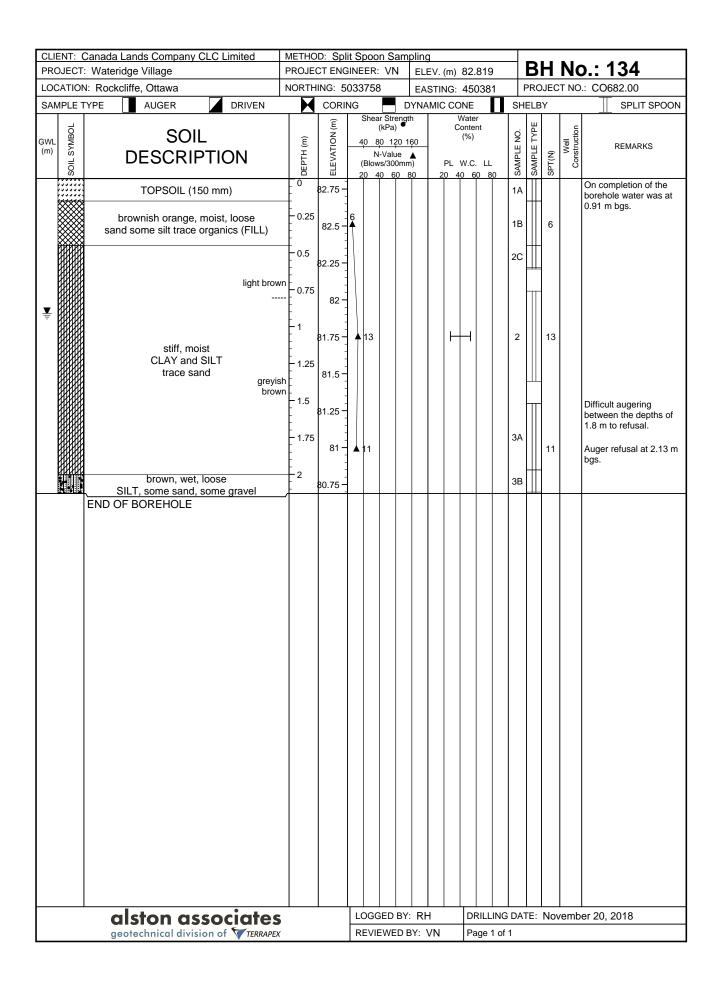
CLIENT: Canada Lands Company CLC Limited PROJECT: Wateridge Village	METHO PROJE							7	R	н	Nic	o.: 127
LOCATION: Rockcliffe, Ottawa	NORTH				+		84.156 450159					D:: CO682.00
SAMPLE TYPE AUGER DRIVEN	M	CORII				AMIC CO			ELB			SPLIT SPOON
SOIL DESCRIPTION	DEРТН (m)	ELEVATION (m)	Shea (40 8 N (Blow	r Streng (kPa) 0 120 -Value	160 (mm)	PL	Water Content (%) W.C. LL	SAMPLE NO.	ш	SPT(N)	Well Construction	
brown, moist compact to dense SILTY SAND some rock fragments	-0.25 -0.5 -0.75 -1	83.75 – 83.25 – 83.25 – 83.25 –	19	0 60		20 4	40 60 80	1 2		19		Borehole open and dry on completion. Difficult augering between the depths of 0.76 and 1.52 m bgs. Auger refusal at 1.52 m bgs.
END OF BOREHOLE												
alston associates			LOGG				DRILLING Page 1 of		TE:	Nov	/emb	er 20, 2018

CLIENT: Canada Lands Company CLC Limited	1		low Stem Au				1	ь Ц	NI	120
PROJECT: Wateridge Village LOCATION: Rockcliffe, Ottawa	1		033735		.EV. (m)		$\overline{}$			128 CO682.00
SAMPLE TYPE AUGER DRIVEN	NORTH	CORII			ASTING:		SHEL		JI NO	SPLIT SPOON
SOIL DESCRIPTION	DEPTH (m)	ELEVATION (m)	Shear Stren (kPa) 40 80 120 N-Value (Blows/300n	gth 160 nm)	Co PL V	Vater ontent (%)	SAMPLE NO.	L L	Well	
FROZEN GROUND	0	84 -	20 40 60	80	20 40	0 60 80	S) (S	n o		Borehole open and dry
compact, moist, brown silty sand, trace gravel (FILL) rock fragments END OF BOREHOLE	-0.25 -0.5 -0.75	84	50/75				2]	50/75		Borehole open and dry on completion. Auger refusal at 1.0 m bgs.
alston associates			LOGGED B	Y: RI	H	DRILLING I	DATE	: No	vemb	er 20, 2018
uisioli ussociale:	X									,

RTHING: COF (w) Hadded 84.25 0.25 84.25 0.75 83.75 83.25 83.25	(E) HE AS A SECOND SECO	9: 500 ORIN (@) NO I PA 25 T	0337 IG Sh 40 (B 20	18 near Si (kP	D C C C C C C C C C C C C C C C C C C C	EAS DYNA th	STIN	IG: 4 CON Con (f	34.31 4502(NE 'ater ntent %)	03 	SH SAMPLE NO.	PRO LL SAMPLE TYPE	DJEC BY	Well Construction	SPLIT SPOON REMARKS Borehole open and dry on completion. Auger refusal at 1.52 m bgs.
(a) NOLLY 313 84.25 84.25 83.75 83.25 83.25 83.25 83.25	(E) HLAND 10 84.2 10 10 10 10 10 10 10 10 10 10 10 10 10	ORINNOI (a) (b) (25 - 1 - 25 - 1 - 25 - 1 - 25 - 25 - 25	10 (B 20	near Si (kP. 80 N-Va lows/3 40	120 1 120 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	DYNA th 160	MIC	CON W: Coi ('	NE rater ntent %)	L	SAMPLE NO.	SAMPLE TYPE II	(x) Lides 10	Well	SPLIT SPOON REMARKS Borehole open and dry on completion.
(w) NOLLY NOT	(E) HEAD STATE OF THE PROPERTY	(E) NOIL	Sh 40 (B 20 10 10 10 10 10 10 10 10 10 10 10 10 10	N-Va lows/3 40	120 1 120 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	th 160 A m)	Р	W: Coi ('	ater ntent %)		SAMPLE NO.	SAMPLE TYPE	(Z) Lds		REMARKS Borehole open and dry on completion. Auger refusal at 1.52 m
34.25 34.25 84 3.75 33.75 83.5 83.25 83.25	- 0 84.2 - 0.25 8 - 0.5 83.7 - 0.75 83.7 - 1 83.2 - 1 83.2	25 – 84 – 75 –	10			80	20	0 40	60	80	1		10		on completion. Auger refusal at 1.52 m
			LOG	GGEL	D BY	: RH			DRIL	LING	DA GO	TE:	Nov	vemb	er 20, 2018
								LOGGED BY: RH REVIEWED BY: VN							







	Canada Lands Company CLC Limited	METHO					-					D	ш	NI.	. 125
	: Wateridge Village	PROJE				/N			84.9						o.: 135
	N: Rockcliffe, Ottawa	NORTH			790 ■				450	447 ■	_			, I NC	D.: CO682.00
SAMPLE TO	SOIL DESCRIPTION	DЕРТН (m)	CORII	4((E	Blows/3	Strence Pa) 120 alue 300m	160 (m)	PL '	Water onten (%) W.C.	t LL	SAMPLE NO.	AMPLE TYPE		Well	SPLIT SPOON REMARKS
WAS TIOS WAS TIOS		0.25	84.75 -	(E	N-V	alue 300m 60	m)	PL '			Nample Na	SAMPLE T	(N) LdS 50	Well	Borehole open and dry on completion. Auger refusal at 0.70 m bgs.
	alston associates geotechnical division of TERRAPEX			-	DGGE				+	ILLIN ge 1 c		TE:	Nov	/emb	er 20, 2018

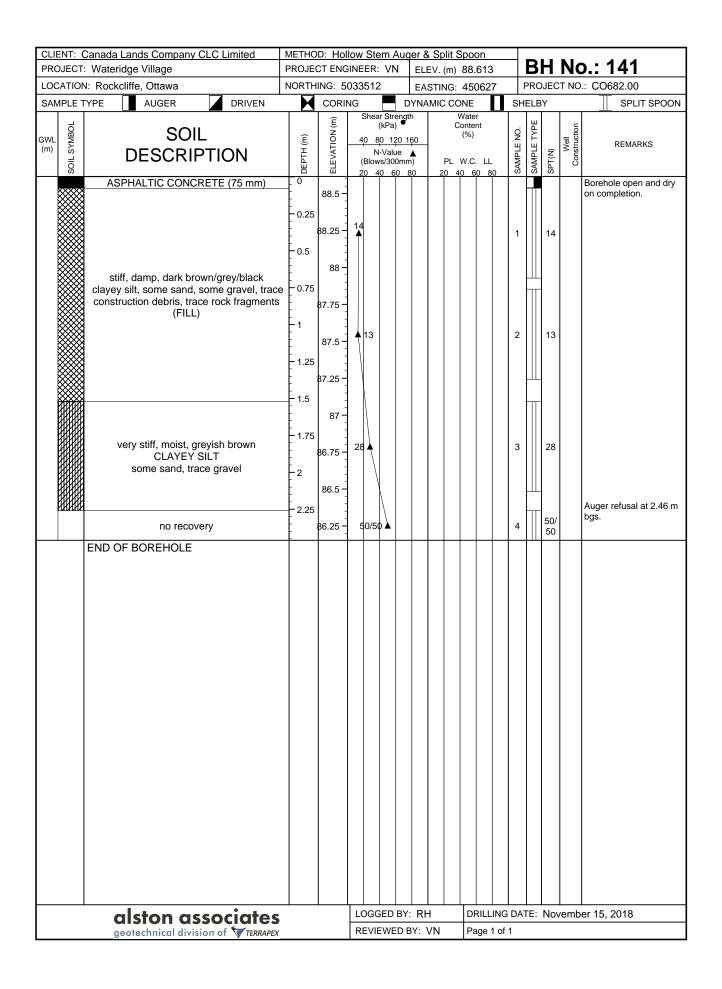
	Canada Lands Company CLC Limited Wateridge Village	METHO PROJE					- 1	-	(m)	89.2	202		B	H	N	o.: 136
		NORTH				V 1 4	_			450		\dashv				D.: CO682.00
SAMPLE T		H	CORII		<u> </u>		DYN					_	HEL			SPLIT SPOON
GWL SYMBOL SYMBOL	SOIL DESCRIPTION	DEPTH (m)	ELEVATION (m)	40 (E) 120 Value 5/300	ngth 0 160 mm)) C	Water conten (%) W.C.	t LL	SAMPLE NO.	ш		Well	T
	very dense, moist, dark brown and black, gravelly sand, trace asphalt pieces (FILL)	0	-	20	J 40	0 60	80	T	20 4	0 60) 80	1.4	т	- "		Borehole open and dry on completion.
	very stiff, damp, dark brown clayey silt, some gravel (FILL)	0.25	89 -		29							1E	3	29		
****	very dense, damp. light brown SANDY SILT	-0.5 -0.75 -0.75 -1 -1	88.75 — 88.5 — 88.25 — 88.25 —	50	0/75	\						2		50/75		Auger refusal at 1.37 m bgs.
11:11:11:11:11	END OF BOREHOLE	†	 	\forall	1		+	\dagger	\vdash	\vdash	+	+	\dagger	1		
	alston associates		•	LO	GGI	ED E	3Y: R	H		DR	ILLIN	IG DA	TE:	No	vemb	per 16, 2018
	geotechnical division of TERRAPEX			RE	VIE	WE	D BY:	VN		Pa	ge 1 d	of 1				

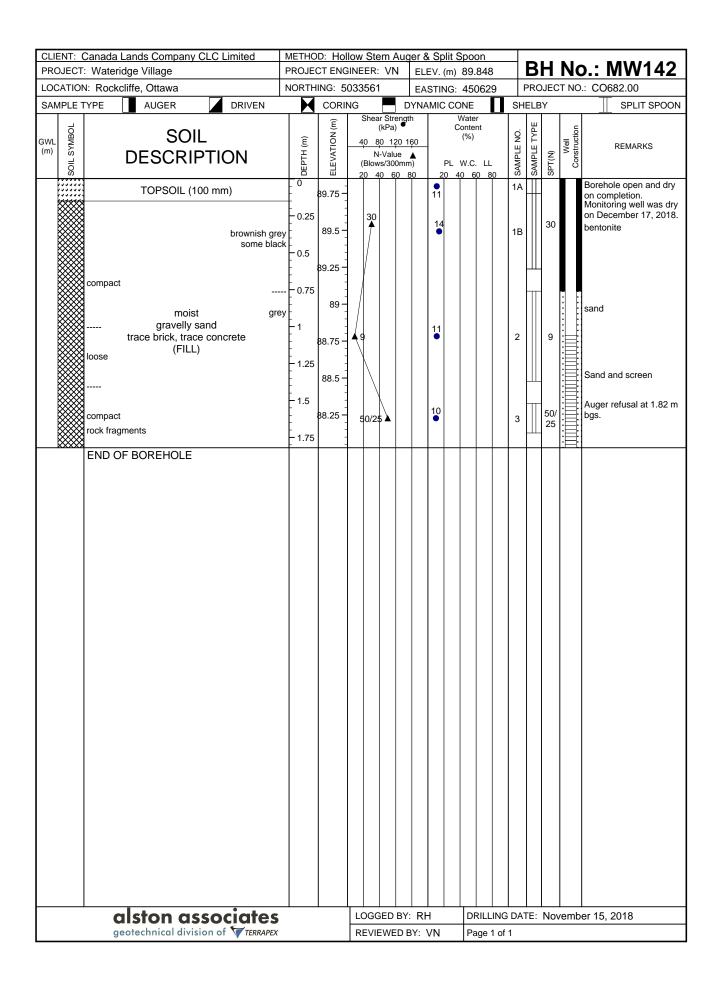
NORTHURS: 5033622		· · ·			low Ste							R	Н	N	o.: 137
SOIL DESCRIPTION COMPANY COUNTY COUNTY							_								
SOIL DESCRIPTION							_			П					SPLIT SPOON
compact, moist-wet, light brown/brown/grey o.5 silty sand to sand, some gravel, trace brick, frace concrete, black organics (FILL)	GWL (m) SX	SOIL			Shea 40 8 N (Blow	0 120 -Value rs/300n	160 nm)	PL	Water Content (%)	LL	ō.	ΓΥΡΕ		Well	T
- 1.5 SANDY SILT rock fragments END OF BOREHOLE - 1.75 88 - 62/203 3 3 3 62/203 Auger refusal at 1.87		silty sand to sand, some gravel, trace brick,	-0.25	89.5 — 89.25 — 89.25 — 89 — 88 —		3 30					1 2A		17		Borehole open and dry on completion.
		SANDY SILT rock fragments	- - -	88 -	62/2	203					3		62/ 203		Auger refusal at 1.87 m bgs.
LOCGED DV. DIL DRILLING DATE: Nevember 45, 2049															
geotechnical division of TERRAPEX LOGGED BY: RH DRILLING DATE: November 15, 2018 REVIEWED BY: VN Page 1 of 1		alston associates	1						_			TE:	Nov	l /emb	er 15, 2018

	Canada Lands Company CLC Limited : Wateridge Village	METHO PROJE									poor 8.51			R	H	N	o.: 138
	N: Rockcliffe, Ottawa	NORTH					-				505						o: CO682.00
SAMPLE T		H	CORI		J J F		_			CON		ĬΠ	SH.				SPLIT SPOON
SOIL SYMBOL	SOIL DESCRIPTION	DEPTH (m)	ELEVATION (m)	4	0 80 N- Blows	0 12 Valu s/300	ength 20 160 le A Omm)	0	P	Wa Cor (9	ater ntent %)		SAMPLE NO.	ш	SPT(N)	Well	
0)	ASPHALTIC CONCRETE (75 mm)	0	88.5	2	0 40	0 60	0 80	+	20	40	60	80	0)	0)	0)		Borehole open and dry
	damp, brown gravelly sand (FILL)	0.5	88.25 - - - - - - - - - - - - - - - - - - -			50							1		50		on completion.
	hard, moist, brown CLAYEY SILT, some sand, some gravel END OF BOREHOLE	- - - - 1 - - - - 1.25	87.5 – 87.5 – - - 87.25 –	5	3/254	4 🛦							2		53/ 254		Auger refusal at 1.37 m bgs.
	alston associates			LC	OGG	ED	BY:	RH			DRIL	LING	DA ⁻	TE:	Nov	/emb	er 16, 2018
	geotechnical division of TERRAPEX			RI	EVIE	WE	D BY	/: V	'N		Page	1 of	1				

		METHO													D	ш	NI.	o.: 139
		PROJE(NORTH					١		EV. (D.: CO682.00
SAMPLE 1		NORTH	CORII				D,		STIN MIC)) <i>[</i>			ELE			SPLIT SPOON
GWL (m)	SOIL DESCRIPTION	DEРТН (m)	ELEVATION (m)	4	0 8 N Blow	r Stre (kPa) 0 12 -Valu	ength 20 16 ie	0 (0 (1)	ı	V C	Vater onter (%) W.C.	nt LL	- 1	SAMPLE NO.	SAMPLE TYPE	SPT(N)	Well	
	compact to dense, damp, brown/grey gravelly sand, traces of brick and concrete (FILL) metal fragments no recovery END OF BOREHOLE	- 0.25 0.25 0.5 0.75 1	89.55 — 89.25 — 89.25 — 88.75 — 88.25 — 88.25 —	2		0 6						0 80	- 1	NS 1 2 3		30 15 50/25		Borehole caved-in at 1.10 m bgs and dry on completion. Auger refusal at 1.70 m bgs.
	alston associates geotechnical division of TERRAPEX	1		-		SED					-	RILLI ge 1			TE:	Nov	/emb	er 15, 2018

	Canada Lands Company CLC Limited : Wateridge Village	METHC PROJE									oon 8.144	1		В	H	No	o.: 140
	N: Rockcliffe, Ottawa	NORTH									5054						:: CO682.00
SAMPLE T	TYPE AUGER DRIVEN	H	CORII	NG			DY	'NAN	лс (CON	E	П	SHI	ELB	Υ		SPLIT SPOON
SOIL SYMBOL	SOIL DESCRIPTION	DEРТН (m)	ELEVATION (m)	40 (E	0 80 N- Blows	0 12 -Valu s/300	20 160 le A Omm)	0		Con (% L W	ater itent 6) .C. LL		SAMPLE NO.	SAMPLE TYPE	SPT(N)	Well Construction	REMARKS
	compact, damp, brown/grey gravelly sand, trace organics (FILL)	0 - 0.25	88 -	15	0 40	0 6	0 80	3		40	00 6		1A 1B		15		Borehole caved-in at 2.85 m bgs and dry on completion.
	stiff, moist, brown clayey silt, some sand, trace gravel (FILL)	0.75	:														
	stiff, moist, greyish brown clayey silt, some sand, trace large gravel	- 1 - 1 1.25	87.25 - 87 - 87 - 86.75 -		. 18				9				2		18		
	compact	-2	86.25 -	1	15				16				3		15		Difficult augering at 2.13 m bgs due to large
	SAND trace gravel trace silt occassional oxidized dense pockets some gravel	- 2.25 - 2.5 - 2.75	85.75 - 85.5 -	3	s6 A				10				4		36		gravel.
	greyish brow	3 	85 -	5	0/75			-	7				5		50/ 75		Auger refusal at 3.27 m bgs.
	alakan aasaa ista -)GC	ED	RV.	ㅁㅁ		4	י יופח	INIC	- ۸ م	L	No.	l mb	er 16, 2019
	alston associates			\vdash			BY:		N.I	-				E:	1001	/emb	er 16, 2018
	geotechnical division of TERRAPEX			KE	_ V I 🗆	. v v 🗀	D BY	. V	IN		Page	1 01					



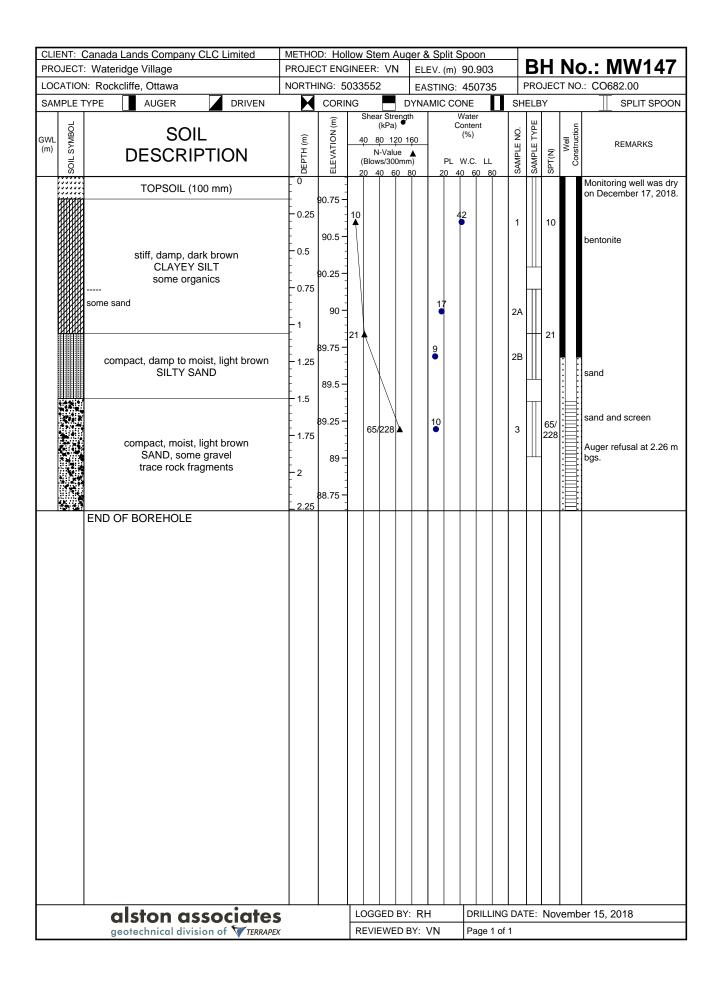


CLIENT: Canada Lands Company CLC Limited	METHO											L	NI.	. 112
PROJECT: Wateridge Village LOCATION: Rockcliffe, Ottawa	PROJE				N		EV. (m) STING:							D.: 143 D.: CO682.00
SAMPLE TYPE AUGER DRIVEN	NORTH	CORII		, <u>,</u>	D.		MIC CC		1632		HEL) INC	SPLIT SPOON
GWL OBSCRIPTION SOIL DESCRIPTION	DEРТН (m)	ELEVATION (m)	40 (Blo	ear Str (kPa 80 1: N-Vali	ength) 20 16 ue 0mm	n 60 ▲	PL	Wate Conter (%)	nt LL	ON HIGMAN	ц		Well	
compact, damp, brown sandy silt trace clay trace brick trace concrete (FILL) some brick trace limestone fragments END OF BOREHOLE	-0.25 -0.5 -0.75 -1 -1.25	89.75	(Bicci) 33	0 40 6	0mm	1)			LL 0 80	1 1 2 2 3		(A) LdS 30 30 19 19 50/75		Borehole open and dry on completion. Auger refusal at 1.75 m bgs.
alston associates			-	GED				+	RILLIN		ATE:	No	vemb	per 15, 2018

	Canada Lands Company CLC Limited Wateridge Village	METHO PROJE					7			Spoo 88.9			F			Nc	o.: 144
	I: Rockcliffe, Ottawa	NORTH					_			450							:: CO682.00
SAMPLE T		M	CORII		J 10		DYNA				<u> </u>	_		BY			SPLIT SPOON
GWL SYMBOL SYMBOL	SOIL DESCRIPTION	DEPTH (m)	ELEVATION (m)	40 (E	3lows/	120 /alue /300r	ngth 0 160 mm)) C	Water conten (%) W.C.	t LL	CN	Т	SAMPLE I YPE	(N)	Well Construction	REMARKS
99	ASPHALTIC CONCRETE (75 mm) compact, moist, brown gravelly sand (FILL) stiff, moist, brown/grey/black clayey silt, some sand, trace gravel very dense, damp, light brown	0.25	88.75 — 88.5 — 88.5 —	20			80	2	20 4	0 60	0 80	11/	3	2	20		Borehole open and dry on completion. Difficult augering between 0.91 to refusal.
	sandy silt, trace rock fragments (FILL) END OF BOREHOLE	- - - 1	88 - 88 - - - - 87.75 -	50	0/50	\						2		5 5	60		Auger refusal at 1.22 m bgs.
-	alston associates		•	LO	GGE	D E	Y: RI	H		DR	ILLIN	NG D	ΛΤΕ	: N	ove	emb	er 15, 2018
	geotechnical division of TERRAPEX			RE	VIEV	NED	BY:	VN		+	ge 1						

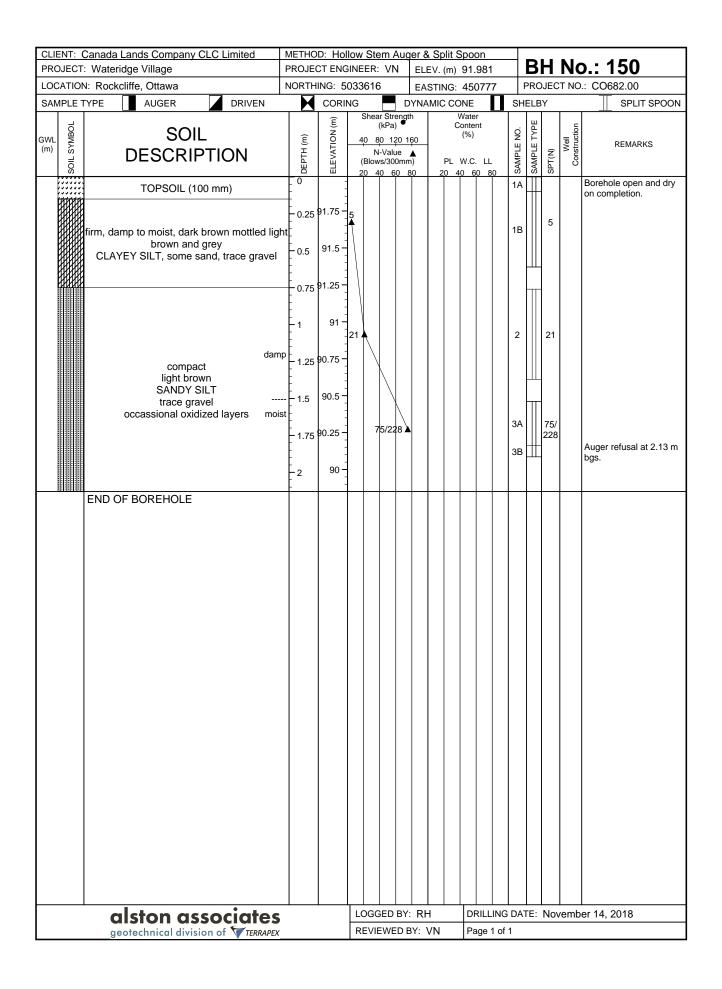
	Canada Lands Company CLC Limited	METHO					7							D	ш	NI.	o.: 145
	Wateridge Village I: Rockcliffe, Ottawa	PROJE:				VΝ	\neg		/. (m) /ING:								D.: 143 D.: C0682.00
SAMPLE T		NORTH	CORII		336 				IC CO		_	B T	SHI			INC	SPLIT SPOON
GWL WBOL (m)	SOIL DESCRIPTION	DEPTH (m)	ELEVATION (m)	4(12 Value	ngth 0 160		(Wate Conte (%)	er nt		SAMPLE NO.	SAMPLE TYPE	SPT(N)	Well	
	TOPSOIL (75 mm)		_	20	0 40	60	80	-	20 4	40 6	8 08	0	_		ß		
lios de la companya d	Compact, damp, brown gravelly sand (FILL) compact, moist, brown sand, some silt, trace gravel (FILL) very dense, damp, light brown SANDY SILT, trace rock fragments END OF BOREHOLE	-0.25	88.75 - 88.75 - 88.25 - 88.25 -	,	Blows 0 40	300	mm)						1A 1B 2A 2B		1)LdS 62	OO	Borehole open and dry on completion. Auger refusal at 1.20 m bgs.
	alston associates			LC	DGGI	ED I	BY: I	RH		DI	RILL	IING	DAT	<u>Γ</u> Ε:	Nov	/emb	er 15, 2018
	geotechnical division of TERRAPEX	,		_						_							, _0, _0, _0
	georechnical division of W TERRAPEX			KE	VIE	vv⊏l) BY	. Vľ	٧	l Pa	age 1	ı Oİ	1				

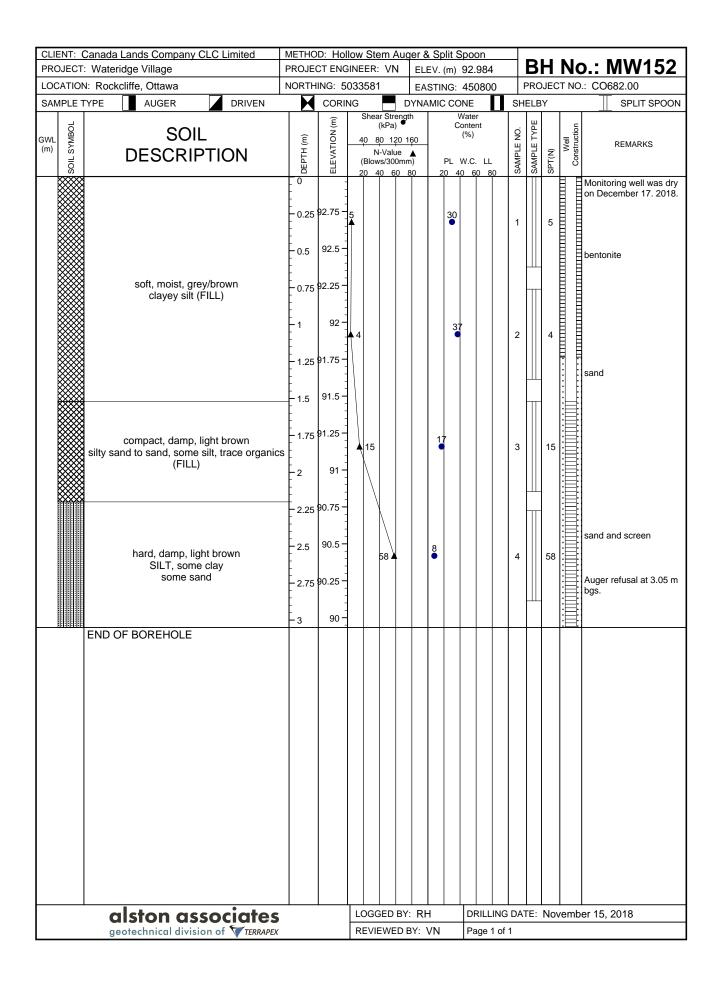
LOCATION: Rockcliffe, Ottawa SAMPLE TYPE AUGER DRIVEN CORING DYNAMIC CONE SHELBY SPLIT S SHELBY S		Canada Lands Company CLC Limited	METHO										1	R	Н	N	o.: 146
SAMPLE TYPE							VIN	\dashv					$\overline{}$				
SOIL DESCRIPTION						1		_			Ī	_	_				SPLIT SPOON
TOPSOIL (220 mm) 1A 1B 1B 1B 1B 1B 1B 1B 1B 1B	GWL SYMBOL	SOIL			4((E	0 80 N-' Blows	120 Value 3/300	160 mm)	PL	Wate Conter (%)	nt LL	•	ō Ö	LYPE		Well	
compact, damp, light brown SANDY SILT trace gravel trace sand trace rock fragments 190.25 190.25 190.25 390.25 190.25 190 190 190 190 190 190 190 19	(33333)	TOPSOIL (220 mm)				0 4 0	000	80	20 2	+0 6	0 80	1		Ï			Borehole open and dry on completion.
		SANDY SILT trace gravel trace sand	-0.5 -0.75 -1 -1 -1.25	90.75	N		\						2		19		Auger refusal at 1.83 m bgs.
1		END OF BOREHOLE															
alston associates geotechnical division of TERRAPEX BLOGGED BY: RH DRILLING DATE: November 14, 2018 REVIEWED BY: VN Page 1 of 1		alston associates		<u> </u>	-					+				E:	Nov	l /emb	er 14, 2018

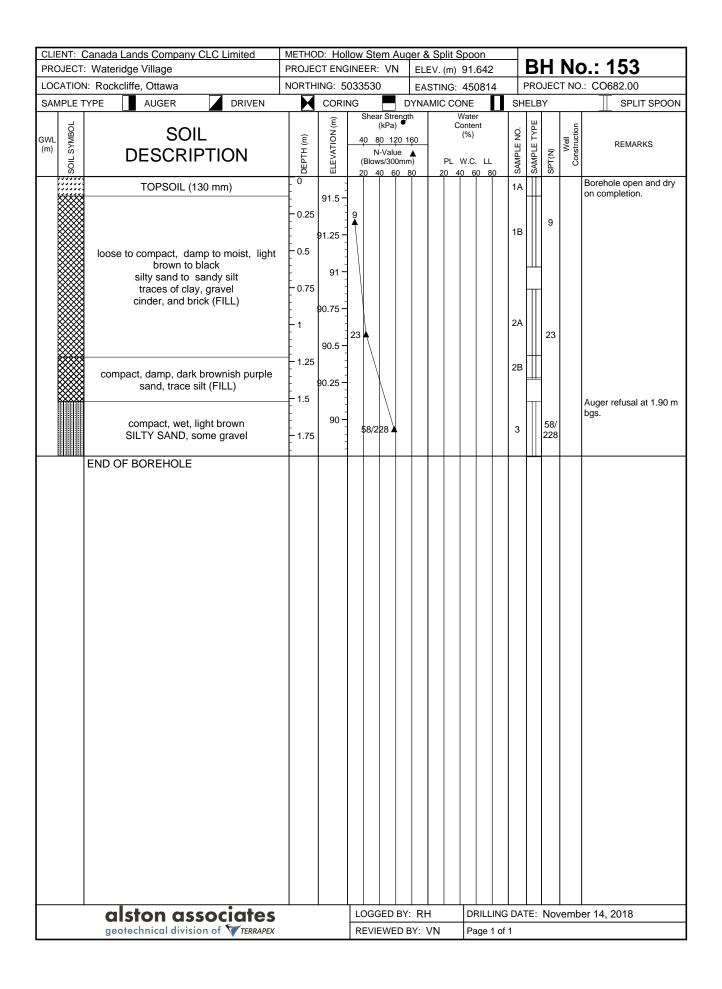


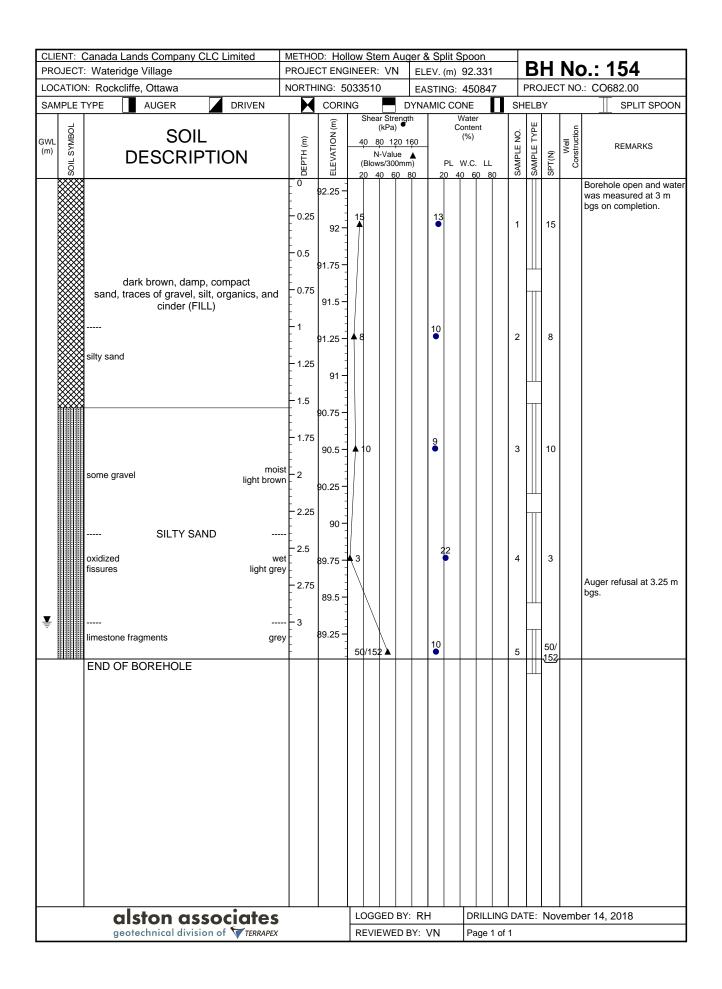
	Canada Lands Company CLC Limited : Wateridge Village	1		low Stem Au			R	н	lo.: 148
	N: Rockcliffe, Ottawa	+		033518		90.484 6: 450732			NO.: CO682.00
SAMPLE 1		H	CORII		DYNAMIC C		SHELE		SPLIT SPOON
GWL SYMBOL	SOIL DESCRIPTION	DEPTH (m)	ELEVATION (m)	Shear Streng (kPa) 40 80 120 N-Value (Blows/300m	160 A nm) PL	Water Content (%)	SAMPLE NO.		Ooustruction REMARKS
)SC	trace organics compact, moist, brown gravelly sand (FILL) brick fragments	- 0.25 - 0.25 - 0.75 - 0.75 - 1.25 - 1.25 - 1.75	90.25 - 90 - 90 - 89.75 - 89.5 - 89.25 - 89 - 88.75 - 88.75 -	20 40 60	· .		5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	20	Borehole caved-in at 1.92 m bgs and dry on completion.
	rock fragments	- 2.25 - -	88.25 <u>-</u> - -	50/50 🛦			4	50/ 50	Auger refusal at 2.44 m bgs.
	END OF BOREHOLE								
	alston associates	 ;		LOGGED B	Y: RH	DRILLING D	ATE:	Nover	mber 14, 2018
	geotechnical division of TERRAPEX	(REVIEWED	BY: VN	Page 1 of 1			

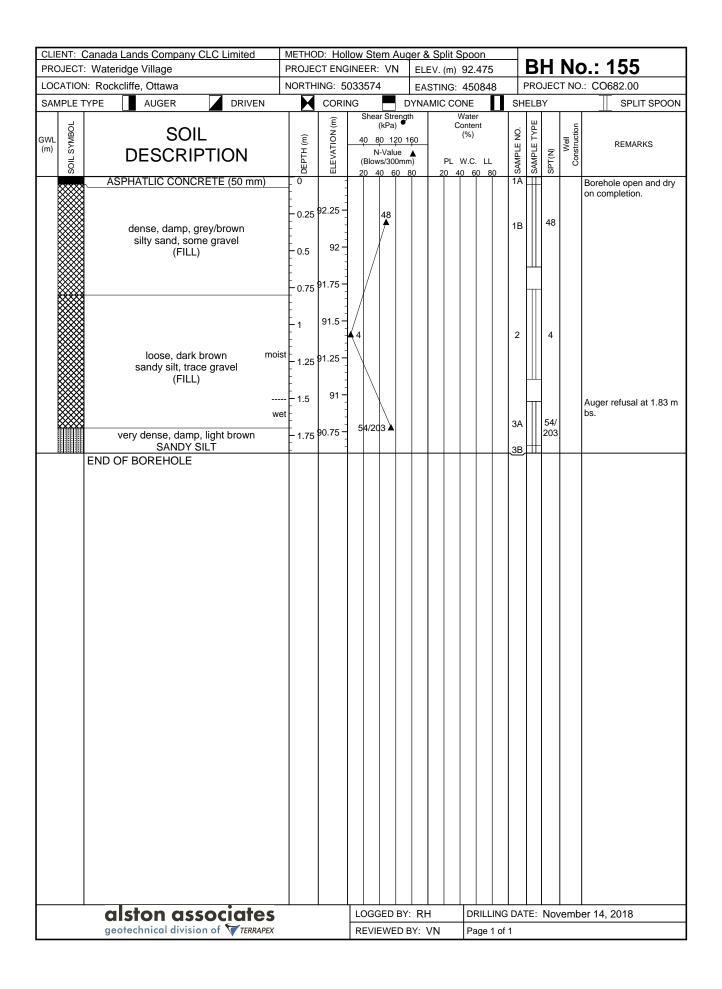
	nada Lands Company CLC Limited	METHO PROJE													R	Н	N	o.: 149
	Vateridge Village Rockcliffe, Ottawa	NORTH									90. 450			_				:: CO682.00
SAMPLE TYP		H	CORII		0-10		_		MIC			,,,,		SHI				SPLIT SPOON
GWL SYMBOL SYMBOL	SOIL DESCRIPTION	DE РТН (m)	ELEVATION (m)	4	0 8 N Blow	r Stre (kPa) 0 12 -Valu	ength	0 \		C PL	Water onter (%)	nt LL	- 1	SAMPLE NO.	SAMPLE TYPE	SPT(N)	Well	
	compact, damp, dark brown/brown gravelly sand (FILL)	- 0.25 - 0.5	90.75 — 90.5 — 90.5 — 90.25 —		28	0 6	0 80	0		0 4	0 6	0 80)	1		28		Borehole open and dry on completion.
 ro fra	compact, wet, brown/light grey SILTY SAND trace gravel cck agments	- - -1	90 - - - 89.75 - - - 89.5 -	27										2		27		Auger refusal at 1.52 m bgs.
	alston associates geotechnical division of TERRAPEX			-		ED WE					-	ge 1			ΓE:	Nov	/emb	er 14, 2018



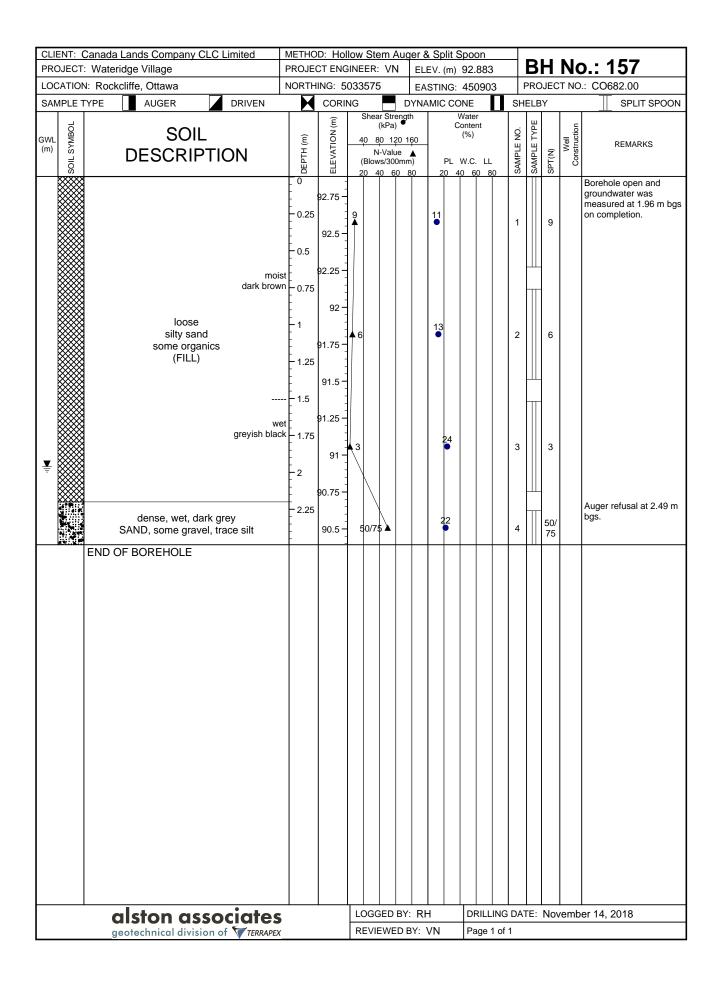


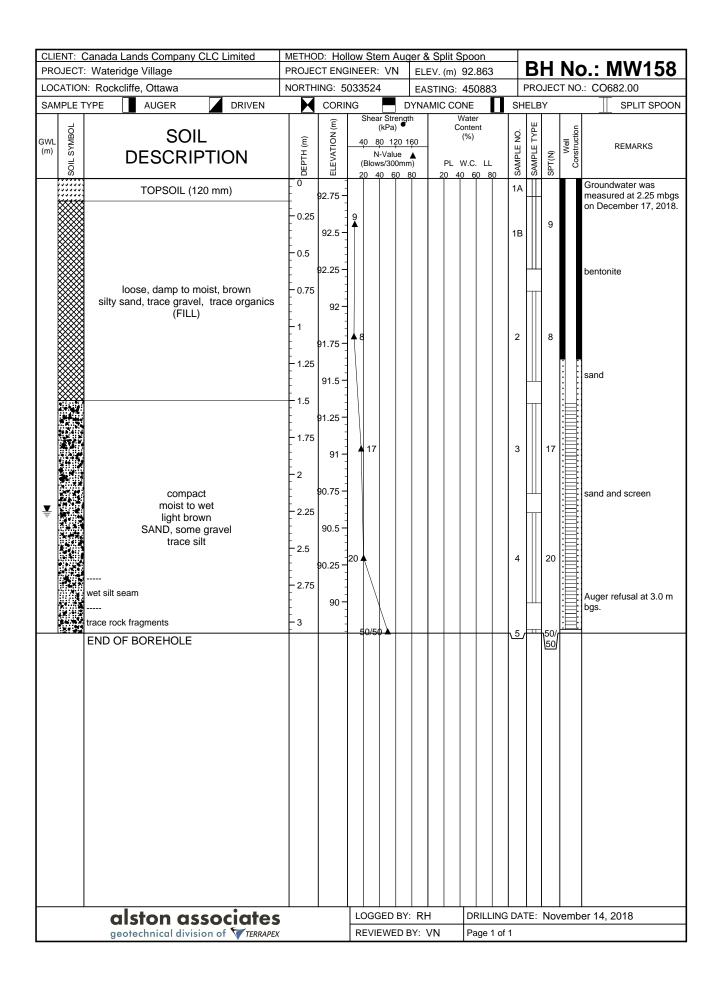






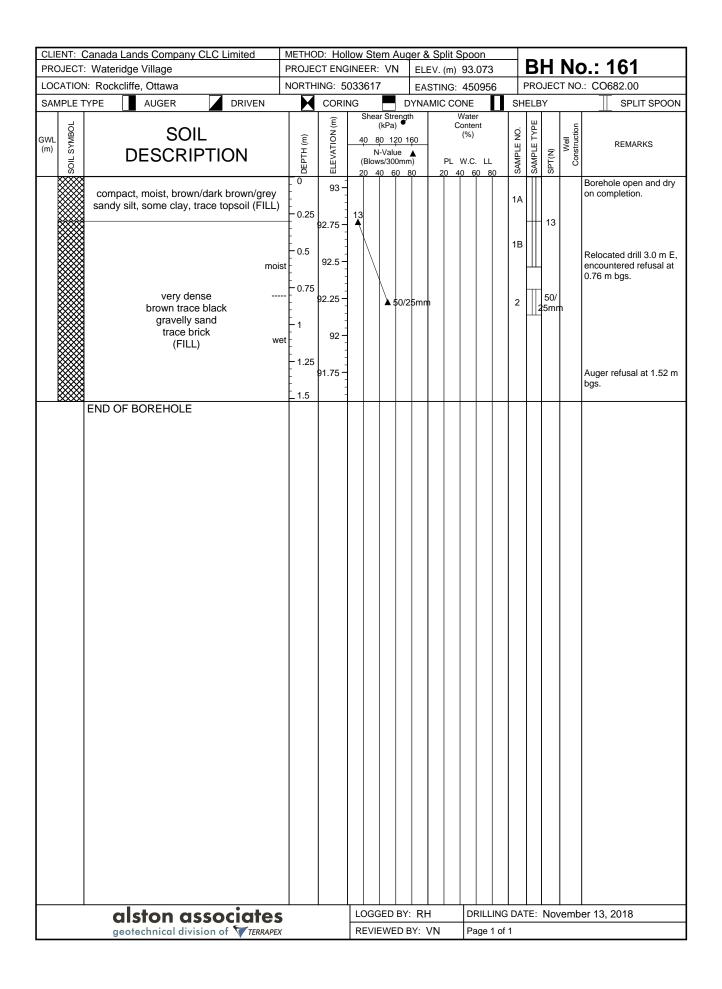
CLIENT: Canada Lands Company CLC Limited PROJECT: Wateridge Village			low Stem Au	ger & Split		BH No.: 156				
LOCATION: Rockcliffe, Ottawa			033617	EASTING:		PROJECT NO.: CO682.00				
SAMPLE TYPE AUGER DRIVEN	H	CORII		DYNAMIC CO		SHELE			SPLIT SPOON	
SOIL SOIL	DEPTH (m)	ELEVATION (m)	Shear Streng (kPa) 40 80 120 N-Value (Blows/300m	160 Anm) PL	Water Content (%)	SAMPLE NO.		Well		
The state of the s	- 0.25 - 0.5 - 0.75	92.25 - 92.25 - - - - 92 - - - 91.75 -	N-Value	nm) PL		SAMPLE SA	(V) Lds 26 50 50 63/228		Borehole open and dry on completion. Auger refusal at 1.5 m bgs.	
alston associates	i		LOGGED B'		DRILLING D	DATE:	Nov	/emb	er 14, 2018	



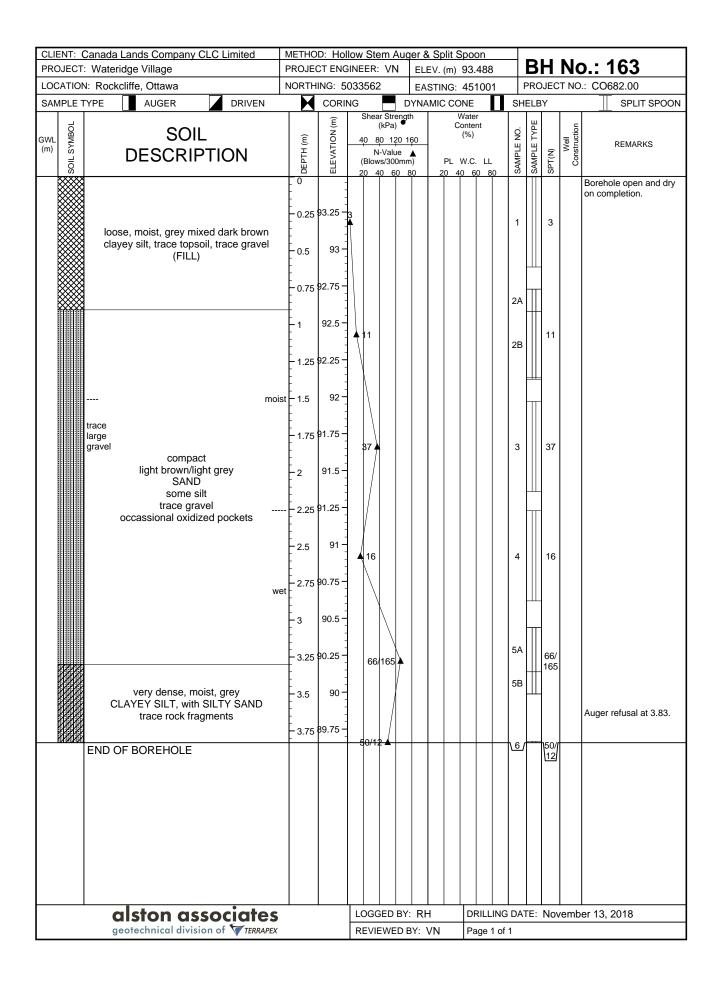


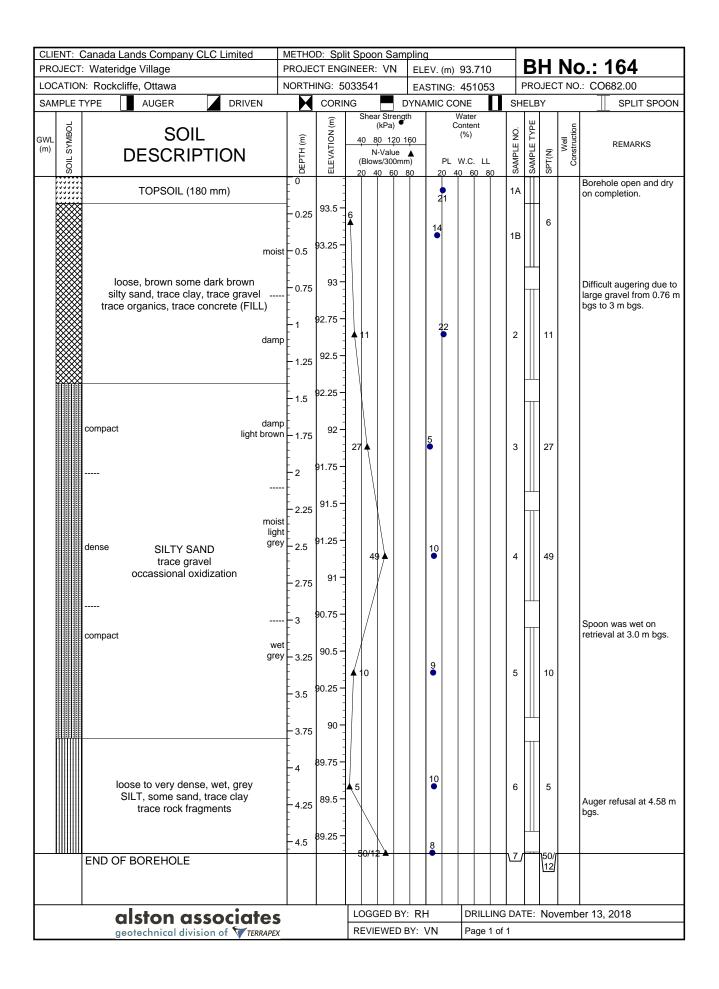
		METHO PROJE													RI	Н	No	o.: 159
		NORTH			, ,								PROJECT NO.: CO682.00					
SAMPLE T		H	CORI				_	DYNAMIC CONE						_	LB			SPLIT SPOON
SOIL SYMBOL	SOIL DESCRIPTION	DEРТН (m)	ELEVATION (m)	2	10 8 N (Blov	ar Str (kPa) 30 12 V-Valu vs/30	ength 20 16 ie	0 \	F	V Cd	Vater onten (%) V.C.	t LL	• •	Ö	SAMPLE TYPE	SPT(N)	Well	
,,,,,,	TOPSOIL (120 mm)		93.75	- 2	20 4	40 6	0 80	0	20) 40	0 60	80	\neg	A		0)		Borehole open and dry on completion.
	compact, moist, brown sandy silt, trace to some gravel, trace organics (FILL)	<u> </u>	93.5 - 93.25 -	14	7								1	В		17		on completion.
	compact, damp, light brown gravelly sand, some silt, occassional topsoi	- - - 1.25	93 - 92.75 - 92.5 -	A	11									2		11		
	pockets (FILL)	- - - 1.75	92.25 - 92 - 91.75 -	*	9									3		9		
	compact, damp, light grey rock fragments, trace to some sand	- 2.25 - - - 2.5	91.5 - 91.25 -	27										4		27		Auger refusal at 2.75 m bgs.
	END OF BOREHOLE																	
	alston associates			L	OG	GED	BY:	RH	<u> </u> 1		DR	ILLIN	IG D) AT	E:	Nov	l /emb	er 13, 2018
	geotechnical division of TERRAPEX	REVIEWED BY:																

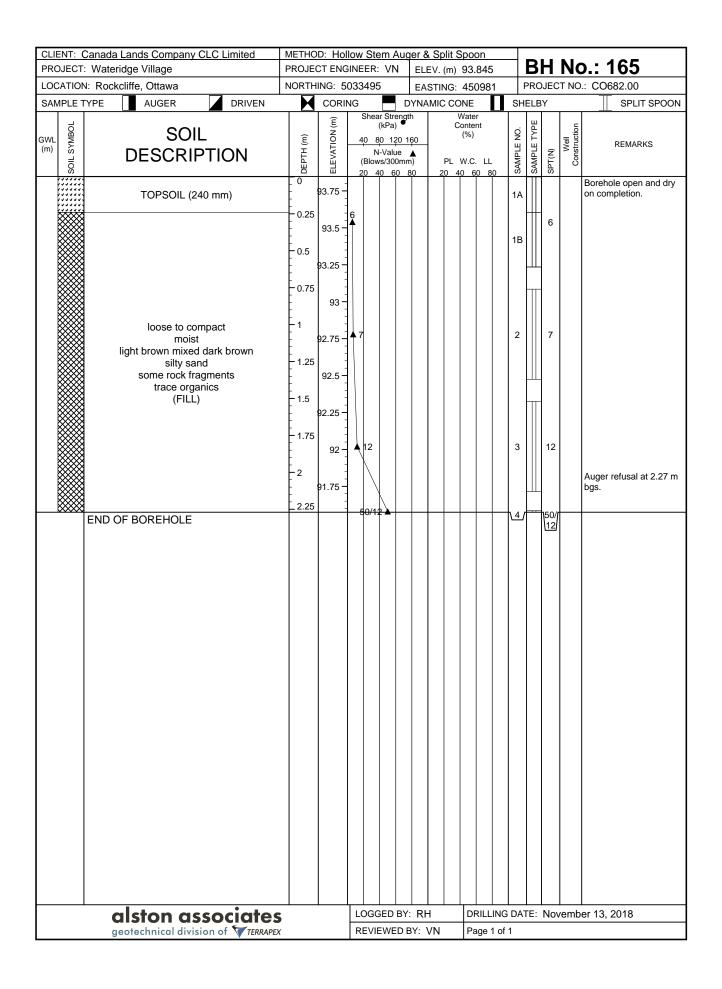
CORNID SAMPLE TYPE AUGE PRIVER CORNID CORNID		Canada Lands Company CLC Limited : Wateridge Village							uger & Split Spoon ELEV. (m) 92.688								BH No.: 160				
SOIL DESCRIPTION SOIL SOIL DESCRIPTION SOIL SOIL SOIL SOIL DESCRIPTION SOIL SOIL SOIL SOIL SOIL SOIL SOIL SOIL								$^{\cdot}$													
SOIL SOIL SOIL Solid						D,											SPLIT SPOON				
TOPSOIL (110 mm) 100se. moist, light brown silty sand, trace organics 105 92.25	GWL SYMBOL	SOIL			4	0 8 N (Blow	0 12 -Valu s/300	ength	0 ()	ſ	V C	Water onter (%)	nt LL	- 1		rype		Well			
loose, moist, light brown silty sand, trace organics 0.5 92.5 92.7 0.75 92.7 1 1 1 31.75 11.25 SILTY SAND trace gravel occassional oxidization 1.75 91 90.5 1.75 91 90.5 1.75 91 90.5 END OF BOREHOLE Difficult augening from 1.22 m bgs to refusal. 3 24 Auger refusal at 2.26 m bgs.	(33333)	TOPSOIL (110 mm)		-	2	0 4	0 60	0 8	0	20	0 4	0 6	0 80)		Ű	0)		Borehole open and dry		
light brown compact moist layered SILTY SAND trace gravel occassional oxidization rootlets light grey 2 2,25 90.5 2 4 4 2 2 4 Auger refusal at 2.26 n bgs. END OF BOREHOLE 1.75 91 24 24 24 24 24 24 25 25			0.5	92.25 -	3										1B		3				
trace gravel occassional oxidization		compact moist layered	1 - 1.25	91.5		19									2		19		Difficult augering from 1.22 m bgs to refusal.		
alston associates LOGGED BY: RH DRILLING DATE: November 14, 2018		trace gravel occassional oxidization	y - 2	90.75	24										3		24		Auger refusal at 2.26 m bgs.		
alston associates LOGGED BY: RH DRILLING DATE: November 14, 2018		END OF BOREHOLE																			
geotechnical division of **TERRAPEX** REVIEWED BY: VN Page 1 of 1		alston associates	1		-							-				LΕ:	No۱	/emb	er 14, 2018		

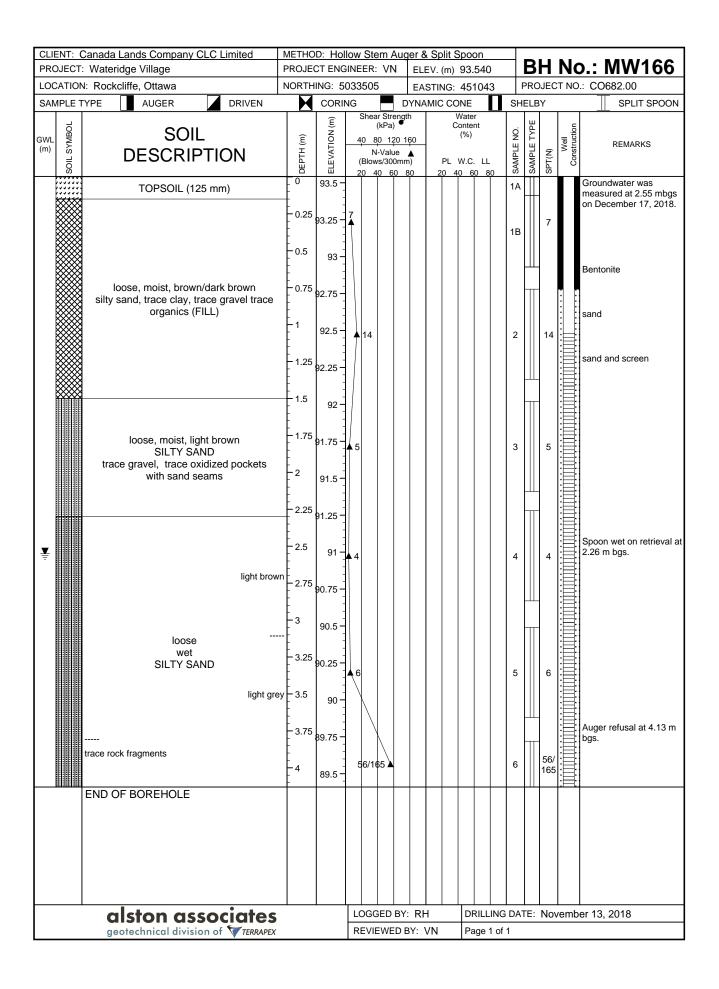


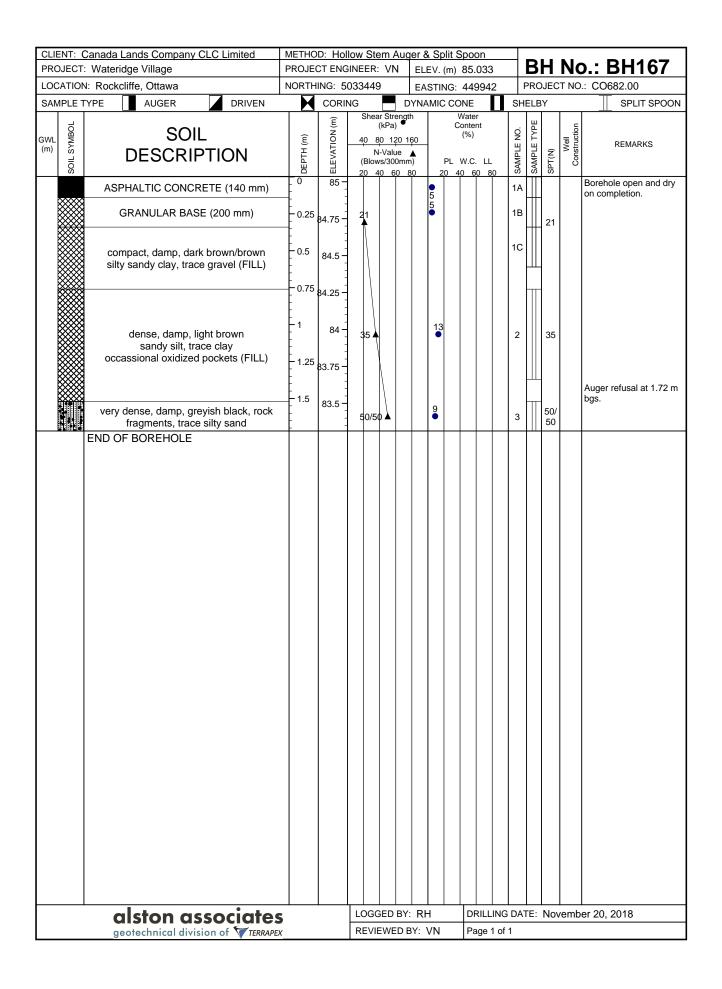
	Canada Lands Company CLC Limited : Wateridge Village	METHO PROJE											R	Н	No	n · 162			
	N: Rockcliffe, Ottawa	NORTH		ELEV. (m) 93.146 EASTING: 451005						BH No.: 162 PROJECT NO.: CO682.00									
SAMPLE T		H	CORI				DYNA				Π		SHELBY SPLIT SPOON						
GWL SYMBOL	SOIL DESCRIPTION	DEPTH (m)	ELEVATION (m)	4((E	Blows/3	trenc 2a) 120 alue 800m	160 m)		W Co	Vater ontent (%) W.C.	t LL	SAMPLE NO.	SAMPLE TYPE		Well				
й	ASPHALTIC CONCRETE (45 mm)	0	<u> </u>	20	0 40	60	80	20	0 40	0 60	80	1A		ਲ		Borehole open and dry			
	compact, moist, light brown silty sand (FILL)	- 0.25	:	13								1B		13		on completion.			
	compact, light grey SILTY SAND occassional oxidization	-0.5 -0.75 st -1 -1.25 -1.5 -1.75 et -2	92.25 - 92 - 91.75 - 91.25 -		17							1C 2		17		Auger refusal at 2.44 m bgs.			
	END OF BOREHOLE	-	90.75 -	-															
	alston associates						∕: RI	1		DRI	ILLING	G DA	TE:	Nov	/emb	er 13, 2018			
	geotechnical division of TERRAPEX			RE	EVIEW	/ED	BY:	VN		Pag	ge 1 of	f 1							

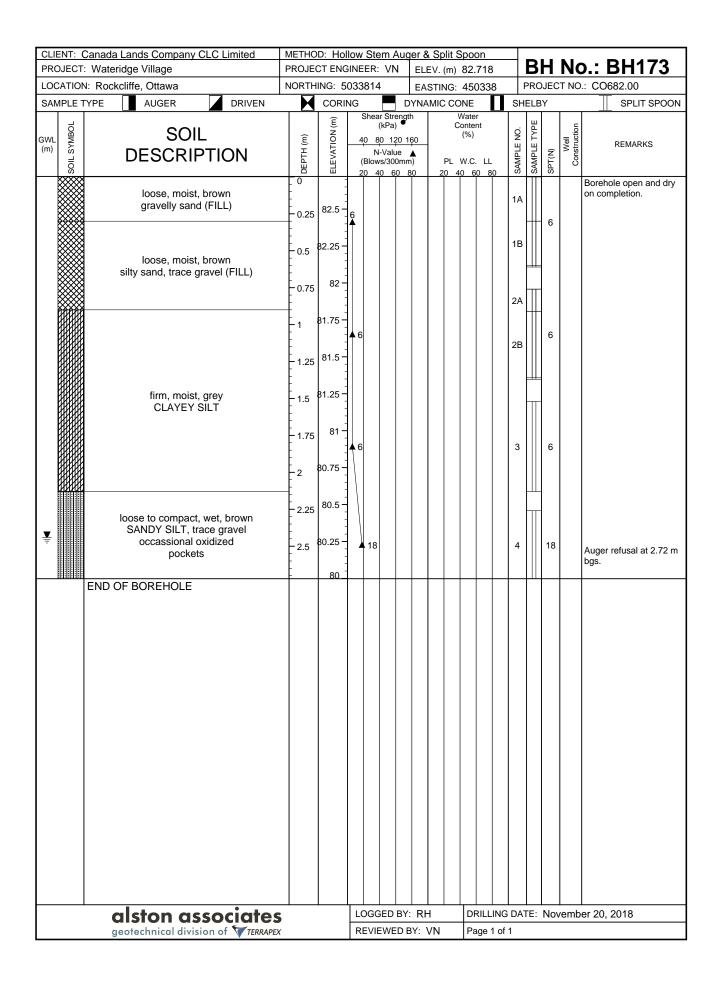












		METHO				7					\blacksquare	D	<u> </u>	N/c			
	: Wateridge Village N: Rockcliffe, Ottawa	PROJE				ELEV. (m) 89.668						BH No.: BH174 PROJECT NO.: CO682.00					
SAMPLE T		NORTH	CORII			EASTING: 450620 DYNAMIC CONE						PROJECT NO.: CO682.00 SHELBY SPLIT SPOON					
GWL SYMBOL SOIL SYMBOL	SOIL DESCRIPTION	DEPTH (m)	ELEVATION (m)	40 (BI	ear Stre (kPa) 80 12 N-Valu ows/30	ength 20 160 ue 🛦 0mm)		V Co	Vater ontent (%) W.C.	LL	SAMPLE NO.	SAMPLE TYPE	SPT(N)	Well Construction			
)5	dense dry brownish red sand and gravel, trace to some brick fragments (FILL) compact mois metal fragments trace rock fragments	- 0.25 - 0.5 - 0.75	89.5 – 89.25 – 89.25 –		40 6 53 A	0 80		20 44	0 60	80	2		53 17 50/ \75/		Borehole caved-in at 0.61 m bgs and dry on completion. Auger refusal at 1.60 m bgs.		
	alston associates	1		-	GGED				+			TE:	Nov	remb	er 15, 2018		
	geotechnical division of TERRAPEX			REVIEWED BY: VN						e 1 of	1						

	Canada Lands Company CLC Limited	METHO									1		R	Н	Nic	o.: BH175
	: Wateridge Village N: Rockcliffe, Ottawa	PROJE(IN			m) 8 IG: 4							:: CO682.00
SAMPLE 1		NORTH	CORII		,555 =				CON		П		ELB			SPLIT SPOON
GWL (m) SX	SOIL DESCRIPTION	DEРТН (m)	ELEVATION (m)	40 (E	3lows	treng a) 120 1 ilue 00mr	th 160 A n)	F	Wa Con (%	iter tent 6)		SAMPLE NO.	rype		Well Construction	
(E) (S) (S) (S) (S) (S) (S) (S) (S) (S) (S	Compact, moist, brown/grey sandy gravel (FILL) END OF BOREHOLE	0	88.75 - 88.5 -	(E	N-Va Blows/3	lue 00mr	m)	ı	PL W. 1			T AWAP	SAMPLE -	(N) LdS 20	Constr	Borehole open and dry on completion. Auger refusal at 0.61 m bgs.
	alston associates			-	GGEE				-+	DRILI			TE:	Nov	/emb	er 16, 2018

CLIENT: Canada Land PROJECT: Wateridge	ls Company CLC Limite Village	ed		HOD:			VN	E	ELE	iV. (m) 74.347	TP No.:	2	<u></u> 01		
LOCATION: Rockcliffe				THIN				_		STING: 449596	PROJECT NO.: C				
SAMPLE TYPE		VEN		_	CORI						SHELBY	T			POON
		Shea	r Stren (kPa) (kpa) (kpa	gth e160 nce		PL V		Т	SOIL SYMBOL	SC	OIL IPTION	SAMPLE TYPE			ELEVATION (m)
	Refusal @ 1.42 m bgs on Limestone Bedrock (weathered at surfac)	Tip F	Resistar	nce		PL V			**************************************	damp, dark bro trace shale	brown Y SILT e clay shale fragments	SAMPLE T	SAMPLEN		74.25 - 74 - 73.75 - 73.5 - 73.25 -
	ston associa						ED E				DRILLING DATE Page 1 of 1	: De	cem	nber	14,

PROJECT: Wateridge	ds Company CLC Limite	ed		THOE OJEC					1	ELE	EV. (m) 76.706	TP No.:	21	<u></u>		
LOCATION: Rockcliffe			_	RTHII					•	1		PROJECT NO.: C				
SAMPLE TYPE		VEN	LINO		COR		JU41		_	•	STING: 449742	SHELBY	T			POON
SAMPLE ITPE	AUGER		r Stre		T	IING			_	INA	INIIC CONE	DIELD I	#	JPL	.11 3	
E INSTRUMENTATION DATA	REMARKS	40 _{St} § Tip F	(kPa)	0 160 ince		PL 1		LL 0 80		SOIL SYMBOL	SC DESCR		SAMPLE TYPE	SAMPLE NO.	SPT(N)	ELEVATION (m)
- 0.25	On completion the test pit was dry and open.	30 1		0 200		0 4		0 80			damp, da	ark brown SOIL				76.5
-0.5											moist, brownish or silt trace gr					76.25 -
- 0.75											damp, SAND` trace clay, trac	Y SILT				76 -
-1	Refusal @ 1.15 m bgs on Limestone Bedrock (weathered at surfac)										limestone and s	shale fragments				75.75 - - -
alston associates						L	OGO	GED	ΒY	∵ RI	1	DRILLING DATE:	De	cem	ber	14,
geotechnical division of TERRAPEX						R	EVI	EWE	DE	BY: \	/N	Page 1 of 1				

	NT: Canada Land JECT: Wateridge	ds Company CLC Limite Village	ed		THOD DJEC				٧	ELE	EV. (m) 85.485	TP No.:	2	03		
	ATION: Rockcliffe			_	RTHIN						STING: 450060	PROJECT NO.: (
SAMI	PLE TYPE	AUGER DRI	VEN		A	COR	ING		С	YNA	MIC CONE	SHELBY	T	SPL	IT S	POON
DEPTH (m)	INSTRUMENTATION DATA	REMARKS	40 _{St} §	r Strer (kPa) fic Cor Resista g/cm 2	160 nce	-	PL \			SOIL SYMBOL	SC DESCR		SAMPLE TYPE	SAMPLE NO.	SPT(N)	ELEVATION (m)
-0.25 -0.75 -1.25 -1.5	DATA	On completion the test pit was dry and open. Refusal @ 1.64 m bgs on Limestone Bedrock	(k	g/cm 2	nce) 1 200 1		PL \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \			S 100S SSSSSSSSSSSSSSSSSSSSSSSSSSSSSSSS	damp, damp, damp, SAND some records and some shale.	brown Y SILT ootlets brown LY SAND e fragments	NAMPI.	SAMPL		85.25 - 85.25 - 84.75 - 84.75 - 84.25 -
		Iston associo								: RF 3Y: \		DRILLING DATE Page 1 of 1	: De	cem	ber	14,

	NT: Canada Land ECT: Wateridge	ds Company CLC Limite Village	ed	METH(l EL	.EV. (m) {	36.640	TP No.:	2	04		
	TION: Rockcliffe			NORTI				_	STING: 4		PROJECT NO.:				
	PLE TYPE		IVEN	X	COF	RING		_	AMIC CON		SHELBY	Т	SPI	IT SF	POON
DEРТН (m)	INSTRUMENTATIOI DATA		Shea	ar Strength (kPa) (kpa)	50 60	PL W.		OIL SYMBOL		SC	DIL RIPTION	SAMPLE TYPE		SPT(N)	ELEVATION (m)
0 - 0.25		On completion the test pit was dry and open.	50 10	00 150 20		20 40	80 80			sand an	ark brown nd gravel LL)				86.5 -
- 0.5 - 0.75 - 1										sand	brown dy silt gravel LL)				86.25 - 86 - 85.75 -
- 1.25 - 1.5 - 1.75		Refusal @ 1.84 m bgs on Limestone Bedrock							X	light brown silty sand, ace limesto	pist mixed grey some clay ne fragments LL)				85.5 - 85.25 - 85 -
	Q geo	Iston associa	ites ERRAPEX					 BY: RI D BY:			DRILLING DATE	: De	cem	ber	14,

	NT: Canada Land JECT: Wateridge \	s Company CLC Limite	ed		HOD:				\/N	I EI	EV. (m) 85	5.810	TP No.:	20	<u></u>		
	ATION: Rockcliffe,			_	RTHIN				V 1 4	_	STING: 45		PROJECT NO.: (
		AUGER DRI'	\/ENI	Ь.		CORI		000 I		_	AMIC CONE		SHELBY	T			POON
	INSTRUMENTATION DATA		Shea 40 _{St} Tip F	r Strer (kPa) the 20 Resistan	e160		PL W	V.C. I				SC	OIL RIPTION	AMPLE TYPE			
-0.25 -0.5 -0.75 -1.25	DATA	REMARKS On completion the test pit was dry and open. Refusal @ 1.64 m bgs on Limestone Bedrock	40 _{St} § Tip F	(kPa) fic Cor Resista	• 160 nce	2		V.C. I		SOIL SYMBOL	gra tr	moistavel some (FI	t, grey to trace sand LL) ark brown ace rootlets LL) brown Y SILT trace gravel	SAMPLE TYPE	SAMPLE NO.		(E) (A) (B) (B) (B) (B) (B) (B) (B) (B) (B) (B
	alst	on associate	S							Y: RI			DRILLING DATE Page 1 of 1	: De	cem	ber	14,

CLIENT: Canada Land PROJECT: Wateridge	ds Company CLC Limite	d	METI				tor ER: V	/NI	T = 1	EV. (m) 84.13		TP No.:	20	<u></u>		
LOCATION: Rockcliffe			NOR					/ 1 4	_	STING: 450179		PROJECT NO.: (
SAMPLE TYPE	AUGER DRIV	/ENI		_	ORI		13			MIC CONE	_	SHELBY	TT			POON
		Shea (r Strenç kPa)	gth	- OKI	ING)IL	₩ YPE		11 3	
(更) INSTRUMENTATIONエ DATA品 円	REMARKS -	Tip R	0 120 esistan g/cm 2) 00 150	ce	2	PL W 0 40	/.C. LI		SOIL SYMBOL			IPTION	SAMPLE TYPE	SAMPLE NO.	SPT(N)	ELEVATION (m)
0	On completion the test pit was dry and open.								*******	٦	TOP:	rk brown SOIL gravel				84 -
-0.25									7777	m SI	oist, LTY	brown SAND rganics				83.75 -
-0.5										\ tra	00 01	iganics				83.5
- 0.75 - 1										damp, S <i>F</i>	grey AND	yish brown Y SILT				83.25 -
-1.25	Refusal @ 1.60 m bgs											gravel				83 -
- 1.5	on Limestone bedrock with thinnly bedded shale layers															82.75
C	Iston associo	ites							Y: RH BY: \			DRILLING DATE Page 1 of 1	: De	cem	ber	14,

		s Company CLC Limite	ed				cava		\ /NI	1	E) () 00 00	TP No.:	2		,	
_	JECT: Wateridge \						GINE		VIN		EV. (m) 82.29					
-	ATION: Rockcliffe,		VEN	NOR		COR		001			STING: 450221	PROJECT NO.: C				POON
SAIVI	PLE TYPE	AUGER DRI	Shea	ar Stren		T	IING	[AIVIIC COINE	DI IELD I	#		5	
DEPTH (m)	INSTRUMENTATION DATA	REMARKS	40 _{St} § Tip F	(kPa) lific Con Resistar g/cm 2) 00 150	● e ¹⁶⁰ ice		PL V			SOIL SYMBOL	SC DESCR		SAMPLE TYPE	SAMPLE NO.	SPT(N)	ELEVATION (m)
0		On completion the test pit was dry and open.									moist,					82.25 -
- 0.25 - - - - 0.5		Refusal @ 0.64 m bgs on Limestone Bedrock (weathered at surface)									SILTY some trace limesto	gravel				82 – 81.75 –
		(weathered at surface)		\Box							END OF TEST P	T				
-		1-1					110)GGI	ED B.	 Y: R l	<u> </u> -	DRILLING DATE:	De	Cem	her	14
	ge	alston associates geotechnical division of TERRAPE								BY:		Page 1 of 1	טפ	,c c III	incl	٠¬,

	NT: Canada Land IECT: Wateridge	ls Company CLC Limite Village	ed	ı	THOD DJECT					1	ELE	EV. (m) 77.25	TP No.:	20	08		
	TION: Rockcliffe,			NOF	RTHIN	IG: 5	5033	3847	7			STING: 450162	PROJECT NO.: C				
SAME	PLE TYPE	AUGER DRI	VEN			COR	ING			D	YNA	MIC CONE S	HELBY	\mathbb{I}	SPL	IT S	POON
DEРТН (m)	INSTRUMENTATION DATA	REMARKS	40 _{St} § Tip F	r Strer (kPa) (kPa) (klic Co) (klic Co) (kesista g/cm 2	160 nce	2	PL \			1	SOIL SYMBOL	SC DESCR		SAMPLE TYPE	SAMPLE NO.	SPT(N)	ELEVATION (m)
0 - 0.25		On completion the test pit was dry and open.										moist, dark bro sandy TO trace ro	OPSOIL				77.25 .
- 0.5 - 0.75		Refusal @ 0.98 m bgs on Limestone bedrock with thinnly bedded shale layers										damp, grey CLAYE ⁻	Y SILT				76.75 - - - - 76.5 -
												END OF TEST PI					
	C	alston associ	ates	,							: RF		DRILLING DATE	De	cem	ber	14,
	g	eotechnical division of 🔽	TERRAPEX				R	EVII	EWE	D E	3Y: \	/N	Page 1 of 1				

	NT: Canada Land ECT: Wateridge \	s Company CLC Limite /illage	d				avato		١	ELE	EV. (m) 83.71	TP No.:	20	09		
LOCA	TION: Rockcliffe,	Ottawa		NOR.	THIN	G: 50	03378	38			STING: 450415	PROJECT NO.: C				
SAME	PLE TYPE	AUGER DRI	√EN		C	ORI	NG		D			SHELBY	\top	SPL	IT SI	POON
DEРТН (m)	INSTRUMENTATION DATA	REMARKS	Shea 40 _{St} 8 Tip F	r Streng (kPa) (kPa) (the Cone Resistan (a/cm 2)	oth 160 ce	F	PL W.C			SOIL SYMBOL	SC	DIL RIPTION	SAMPLE TYPE	SAMPLE NO.	SPT(N)	ELEVATION (m)
0 - - - 0.25		On completion water was entering the test pit from an old subdrain at 1.5 m bgs.	50 10	00 150	200 -	20	40	60 80)		limestone fragm (FI	ents, trace sand	0	0	8	83.5 -
0.23		1.5 11 595.									sand, trace moist, lig	brown e silt (FILL) ght brown dy silt				83.25 -
0.75												gravel LL)				83 - 82.75 -
- 1 : : : - - 1.25											sandy c	ish brown layey silt LL)				82.5 -
- - 1.5 - -		Refusal @ 1.70 m bgs on Limestone Bedrock									END OF TEST P					82.25 -
		Iston associon of the state of						GED IEWE				DRILLING DATE Page 1 of 1	De	cem	ber	14,

COCATION ROCKLITTE, CORRECTION CORRECT		NT: Canada Land	s Company CLC Limite	ed				cavat		N	FIE	EV. (m) 88.84	1	TP No.:	2	 10		
SAMPLE TYPE A JUSER ORNOTED AND SHORE SH										IN	+							
SOIL DESCRIPTION REMARKS On completion the test pat was dry and open. On completion the test pat was dry and op				\/EN!					10									DOON.
INSTRUMENTATION REMARKS Augustiance	SAIVII	TETYPE [AUGER DRI				T	NG			JYNA	IMIC CONE	3	HELBY	#	SPL	.11 5	
On completion the test pit was dry and open. O25 O25 O35 O35 Asphaltic concrete moist, dark brown organic layer true to some sand trace rootlets (FiLL) Asphaltic concrete moist, dark brown organic layer true to some sand trace rootlets (FiLL) Asphaltic concrete moist, dark brown organic layer true to some sand trace rootlets (FiLL) Asphaltic concrete moist, dark brown organic layer true to some sand trace rootlets (FiLL) Batter of the provided organic layer true to some sand organic layer trace or content or conte			REMARKS	40 Star Tip F	(kPa) fic Con Resistar g/cm 2)	• 160 ice	20				SOIL SYMBOL	DES			SAMPLE TYPE	SAMPLE NO.	SPT(N)	ELEVATION (m
0.5 0.5 0.75 1 1 Refusal @ 1.60 m bgs on Limestone Bedrock Refusal @ 1.60 m bgs on Limestone Bedrock Refusal @ 1.60 m bgs on Limestone Bedrock END OF TEST PIT END OF TEST PIT BY DEFILLING DATE: December 14.	0										\bowtie							88.75 -
Refusal © 1.60 m bgs on Limestone Bedrock Refusal © 1.50 m bgs on L	- 0.25		pit was dry and open.									crus	her run	limestone				-
1.5 Refusal @ 1.60 m bgs on Limestone Bedrock END OF TEST PIT Column	- 0.5 - 0.75											m organic la	oist, da yer, tra	rk brown ce to some sand				88.25 -
damp, light brown SANDY SILT Some gravel 87.75 Refusal © 1.60 m bgs on Limestone Bedrock 87.25. END OF TEST PIT END OF TEST PIT alston associates Logged BY: RH DRILLING DATE: December 14,												lla	ce roon	eis (FILL)				88 -
Refusal @ 1.60 m bgs on Limestone Bedrock ST.25. Refusal @ 1.60 m bgs on Limestone Bedrock END OF TEST PIT ST.25. BRILLING DATE: December 14,	- 1 - 1.25											da	SAND	/ SILT				87.75 - -
alston associates LOGGED BY: RH DRILLING DATE: December 14,	- 1.5		Refusal @ 1.60 m bgs															-
alston associates LOGGED BY: RH DRILLING DATE: December 14,																		
geotechnical division of ♥ TERRAPEX REVIEWED BY: VN Page 1 of 1		a	Iston associo	ates										DRILLING DATE: Page 1 of 1	De	cem	ber	14,

CLIENT: Canada Lands Company CLC Limited PROJECT: Wateridge Village	d		HOD JEC1				\/NI	L	EV. (m) 89.64	TP No.:	2	<u> </u>		
LOCATION: Rockcliffe, Ottawa			RTHIN				VIN		STING: 450332	PROJECT NO.: (
SAMPLE TYPE AUGER DRIV	/FN			COR		2021		_		SHELBY	TT			POON
(E) INSTRUMENTATION REMARKS DATA	Shea (40 Sta Tip R	r Stren (kPa) 0 120 1c Con tesista	160		PL V	W.C.	LL	SOIL SYMBOL	S	OIL RIPTION	SAMPLE TYPE		SPT(N)	ELEVATION (m)
On completion the test pit was caving in between 0.8- 1.35 m bgs.	50 10	00 150	200 4	2	20 40	0 60	80	O	damp, d TOF	ark brown PSOIL	S	S	S	В9.5 —
0.5									SILT\ some shal	vnish orange ' SAND e fragments organics				89.25 -
- 0.75 - 1									damp, li	ght brown				88.75 -
Refusal @ 1.35 m bgs on Limestone Bedrock									some limest	Y SILT one fragments ge gravel				88.5
alston associo	ites TERRAPEX							Y: RI BY:		DRILLING DATE Page 1 of 1	: De	ecem	ber	14,

	NT: Canada Land	s Company CLC Limite	ed		THOD DJEC1				VN	FIE	EV. (m) 89.04	TP No.:	2	12		
	TION: Rockcliffe,			_	RTHIN				•••	-	STING: 450275	PROJECT NO.: (
			VEN	Ь.	_	COR		ا ا				SHELBY	T			POON
DEРТН (m)	INSTRUMENTATION DATA	REMARKS	Shea	r Strer (kPa) the 20 Resista g/cm 2	ngth 160 nce		PL V		LL	SOIL SYMBOL	SC DESCR	OIL	SAMPLE TYPE	SAMPLE NO.	SPT(N)	ELEVATION (m)
0		On completion the test	50 1	00 150	200 '	2	0 40	60	80	ŭ	asphaltic	concrete	Ŋ	Ŋ	S	89 -
- 0.25		pit was caving in between 0.18- 0.4 m bgs.										, grey d gravel				88.75 - - 88.75 -
- 0.5 - 0.75											GRAVEL	brown LY SAND				88.5
-1		Refusal @ 1.07 m bgs on Limestone Bedrock									trace o trace shale	fragments				88.25 - - - - - 88 -
											END OF TEST P					
	а	Iston associ	ates							Y: RF BY: \		DRILLING DATE Page 1 of 1	: De	cem	per	14,
	ge	otechnical division of 🜹	TERRAPEX				K	_ VIE	vv⊏D	וסו: ۱	VIN	Fage 1011				

	Is Company CLC Limite	ed		THOD					1_		-1/ / \ 00.05	TP No.:	2	12		
PROJECT: Wateridge			-	OJEC.							EV. (m) 88.05					
SAMPLE TYPE	AUGER DRIV	//=N:	_	RTHIN	COR		5005) 			STING: 450298 MIC CONE	PROJECT NO.: C				0001
SAMPLE TYPE	AUGER DRIV		ar Strer		T	ING			T	INA	MIC CONE	SHELBY	#	SPL	.11 5	POON
E INSTRUMENTATION DATA	REMARKS	40 _{St} § Tip F	(kPa) Inc Co Resista g/cm 2	160 nce		PL \			I Odbayo II Oo	SOIL SYMBOL	SC DESCR		SAMPLE TYPE	SAMPLE NO.	SPT(N)	ELEVATION (m)
-0.25 -0.75	On completion the test pit remained open and dry. Refusal @ 0.78 m bgs on Limestone Bedrock (fractured at surface)	(k		2)				LL 0 80		**************************************	Moist, da TOPS some END OF TEST PI	rk brown SOIL sand	SAMPL	SAMPL		88
ge	ston associo	ates TERRAPEX						GED E				DRILLING DATE Page 1 of 1	De	cem	ber	14,

	NT: Canada Land ECT: Wateridge	s Company CLC Limite	ed		THOD DJECT					Len	EV. (m) 88.26	TP No.	21	1	
	TION: Rockcliffe,			-	RTHIN						STING: 450408	PROJECT NO.:			
			VEN		_	COR		5518		_	AMIC CONE	SHELBY			r enoor
SAIVIF	PLE TYPE	AUGER DRI		ar Strer		T	ING			TINA	AWIC CONE	SHELBI	ŤΤ	JPLI	SPOON
DEPTH (m)	INSTRUMENTATION DATA	REMARKS	40 _{St}	(kPa) (kpa) (kpa) (kpa) (kpa) (kpa) (kpa) (kpa) (kpa) (kpa) (kpa) (kpa) (kpa) (kpa) (kpa) (kpa) (kpa)	160 nce	4 2	PL \ 20 40			SOIL SYMBOL		OIL RIPTION	SAMPLE TYPE	SAMPLE NO.	SPT(N) ELEVATION (m)
0		On completion the test pit was open and dry.		1 1	7 200	-	1 40		00			ownish grey			88.25
- 0.25 - 0.5		pir nae opon and ary.									damp, light b sar trace to s	ome sand (FILL) rownish orange ady silt some topsoil FILL)			88 87.75
- 0.75											moi	st, grey DY SILT			87.5
- 1 - 1.25		Refusal @ 1.30 m bgs on Limestone Bedrock									some to	otrace clay irge gravel			87.25 87
	a	İston assoçi	ates							Y: RH		DRILLING DAT	≣: Dec	emb	er 14,
	ge	otechnical division of 🜹	TERRAPEX				R	EVIE	WED	BY: '	VN	Page 1 of 1			

PROJECT Waterlige Village	LOCATION: Rockelffe, Ottowa NORTH-MINE'S 5033591 EASTING: 450502 PROJECT NO: COB22.00			s Company CLC Limite	ed		THOE				\/NI	Tei		\/ (m) 00 00	TP No.:	2	15		
SAMPLE TYPE AUGER DRIVEN CORING DYNAMIC CONE SHELBY SPLIT SPOON SOIL DESCRIPTION SOIL DESCRIPTION On completion the test pit was caving in at 0.224-0.52 m bgs. O.5 Refusal © 1.03 m bgs on Limestone Bedrock 1 Refusal © 1.03 m bgs on Limestone Bedrock 1 Refusal © 1.03 m bgs on Limestone Bedrock AUGER DYNAMIC CONE SHELBY SPLIT SPOON SOIL DESCRIPTION SOIL DESCRIPTION SANDY SILT trace gravel Limestone Bedrock (fractured at surface)	SAMPLE TYPE AUGER ORNOR Share State of Part August Share State Share					-						_							
Shear Strength (kPa) 40st8f6 220 160 Tip Resistance (kg/cm 2) 50 100 150 200 On completion the test pit was caving in at 0.224-0.52 m bgs. O.25 O.5 Refusal © 1.03 m bgs on Limestone Bedrock 1	STRUMENTATION REMARKS OF THE PROPERTY OF THE				\/ENI	LINO				1001		_							2004
INSTRUMENTATION DATA REMARKS R	Netrolive Nation Remarks 1.03 m bgs 0.15 m state 1.04 m state 1.03 m bgs 0.15 m state 1.04 m state 1.05 m state	SAIVIE	TETTPE L	AUGER DR		ar Stre		T	ING			T	AIN	WIC COINE S	DIELBY	#	SPL	11 5	
On completion the test pit was caving in at 0.224-0.52 m bgs. On completion the test pit was caving in at 0.224-0.52 m bgs. On completion the test pit was caving in at 0.224-0.52 m bgs. Sandy Silt some organics light brown SANDY Silt trace gravel Refusal @ 1.03 m bgs on Limestone Bedrock I imestone Bedrock (fractured at surface)	On completion the test pit was cavelin at 0.224-0.52 m bgs. O.25 O.5 O.75 Refusal © 1.03 m bgs on Limestone Bedrock On Limestone Bedrock The D. OF TEST PIT END OF TEST PIT Some organics Limestone Bedrock (fractured at surface) END OF TEST PIT	DEPTH (m)		REMARKS	40 _{St}	(kPa)	0.160 ance 2)					SOIL SYMBOL				SAMPLE TYPE	SAMPLE NO.	SPT(N)	ELEVATION (m)
moist, brown SANDY SILT some organics light brown SANDY SILT trace gravel Refusal @ 1.03 m bgs on Limestone Bedrock Limestone Bedrock (fractured at surface)	no.5 sAND Y SILT some organics light forwing SANDY SILT liace gravel Limestone Bedrock on Limestone Bedrock SILD OF TEST PIT			pit was caving in at	30 1	00 13	0 200		20 40	00	80	**		damp,	, grey				-
Some organics light brown SANDY SILT trace gravel Refusal @ 1.03 m bgs on Limestone Bedrock (fractured at surface)	some organics light brown SANDY SILT trace gravel trace gravel (fractured at surface) g8. END OF TEST PIT	- 0.25		0.224-0.52 III bgs.										moist,	brown				88.5 -
Trace gravel Refusal @ 1.03 m bgs on Limestone Bedrock on Limestone Bedrock (fractured at surface)	Refusal © 1.03 m bgs on Limestone Bedrock (Tractured at surface) END OF TEST PIT	0.5												some of	rganics prown				-
on Limestone Bedrock (fractured at surface)	on Limestone Bedrock (Fractured at surface) END OF TEST PIT	- 0.75												trace o	gravel				88.25 - - -
END OF TEST PIT		- 1												(fractured a	at surface)				88 -
alston associates LOGGED BY: RH DRILLING DATE: December 14,				İston associ	ntes.				LC	DOGG	ED B	Y: RI	<u> </u>		DRILLING DATE:	De	cem	ber	14,

	s Company CLC Limite	d				cavat						TD No.	24	6	
PROJECT: Wateridge							R: V	N	+	EV. (m) 89.75		TP No.: PROJECT NO.: C			
LOCATION: Rockcliffe,	AUGER DRIV	/EN		_	CORI	0336	800			STING: 4506 MIC CONE		· .			CDOON
SAMPLE TYPE	AUGER		r Stren		I	ING		_ '		IWIC CONE		SHELBY	 	SPLII	SPOON
(E) INSTRUMENTATION DATA	REMARKS	40 _{St} 8 Tip R	(kPa) 20 120 drc Con Resistar g/cm 2) 00 150	• 160 ice	1 20		.C. LL 60 8		SOIL SYMBOL	DES	SC SCR	OIL IPTION	SAMPLE TYPE	SAMPLE NO.	SPI(N) ELEVATION (m)
- 0.25 - 0.5	On completion the test pit was caving in between 0.0 and 1.60 m bgs.									brow	dai n to gre	mp eyish brown			89.75 89.5 -
-0.75 										sa trace	nd, sor brick,	ne gravel trace rebar ace concrete (FILL)			89 - 88.75 - 88.5 -
- - - 1.5	Refusal @ 1.60 m bgs on Limestone Bedrock														88.25 -
Q ge	ston associo	ites TERRAPEX							Y: RH BY: \			DRILLING DATE: Page 1 of 1	Dec	emb	er 14,

	IT: Canada Land: ECT: Wateridge \	s Company CLC Limite	ed				cavat GINEE		N	Terr	EV. (m) 88.84	TP No.	2	<u> </u>		
	TION: Rockcliffe,						50335		-	+	STING: 450595	PROJECT NO.:				
—	_		VEN	Ь.	_	COR						SHELBY	TT			POON
SAIVIF	LE ITPE	AUGER DRI		r Stren		T	IING			TINA	INIC CONE	SHELDT	#	JOPE	.11 3	
DEPTH (m)	INSTRUMENTATION DATA	REMARKS	40 Star Tip F	(kPa) flc Cor Resista g/cm 2 00 150	• 160 nce	<u> </u>	PL W.			SOIL SYMBOL		OIL RIPTION	SAMPLE TYPE	SAMPLE NO.	SPT(N)	ELEVATION (m)
0		On completion the test								***	asphaltic	c concrete , brown				88.75 -
[pit was open and dry.								\bowtie	sand and o	ravel (FILL)				-
0.25										\bowtie	moist, d	ark brown				-
										\bowtie	organic la	ayer (FILL)	4			88.5 -
0.5										\bowtie						-
-										\bowtie						88.25 -
										\bowtie						
0.75										\bowtie	moist, brov	vnish orange				-
-										\bowtie	san	dy silt				88 -
-1										\bowtie		me boulders ILL)				-
[\bowtie	(F	ILL)				87.75 -
_ - 1.25										\bowtie						-
1.23										\bowtie						87.5 -
										\bowtie						-
1.5																-
-																87.25 -
- - 1.75											moist are	eyish brown				-
											SAND	Y SILT				87 -
												gravel				-
-2											trac	e clay				-
-		Refusal @ 2.31 m bgs														86.75 -
2.25		on Limestone Bedrock														-
	-									111111111	END OF TEST F	PIT				
							Щ									<u> </u>
	а	Iston associo	ates							/: R⊦		DRILLING DATI	: De	cem	ber	14,
	ge	otechnical division of 🔽	TERRAPEX				RE'	VIEW	ΕD	BY: \	VN	Page 1 of 1				

	NT: Canada Land ECT: Wateridge \	s Company CLC Limite Village	ed		HOD:				VN	EL	.E\	/. (m) 90.64	TP No.:	: 2	 18	1	
LOCA	TION: Rockcliffe,	Ottawa		NOF	THIN	IG: 5	5033	539		_		ΓING: 450711	PROJECT NO.:				
			VEN	Ь.	_	COR				_			SHELBY	\top			POON
DEРТН (m)	INSTRUMENTATION DATA		Shea	r Stren (kPa) (kPa) (kPa) (kPa) (kPa) (kPa) (kPa) (kPa) (kPa)	gth 160		PL V	V.C.	LL	SOILSYMBOL		SC	DIL RIPTION	SAMPLE TYPE		SPT(N)	ELEVATION (m)
0		On completion the test pit was open and dry.	50 1	00 150	200	2	0 40	60	80	;;;;;	1		ark brown SOIL	0)	0)	0)	90.5
- 0.25 - 0.5												damp, gre gravel a trace limesto	yish brown Ind sand ne fragments par (FILL)				90.25 90
- 0.75 - 1		Refusal @ 1.41 m bgs										orange SA som	oist e brown ND e silt gravel				89.75 89.5
- 1.25		on Limestone Bedrock (fractured at surface)											oulders				89.25
		Ilston associon de la la la la la la la la la la la la la								Y: RI		N	DRILLING DATE	≣: De	cem	ber	14,

	NT: Canada Land IECT: Wateridge	ls Company CLC Limite Village	ed	I	HOD JEC1					٧	ELE	EV. (m) 91.02	TP No.:	2	 19		
	TION: Rockcliffe			_	RTHIN						1	STING: 450809	PROJECT NO.: (
SAMF	PLE TYPE	AUGER DRI	VEN		N	COR	ING			[OYNA	MIC CONE S	HELBY	Т	SPL	IT S	POON
DEРТН (m)	INSTRUMENTATION DATA	REMARKS	40 _{St} § Tip F	ar Strer (kPa) (kPa) (klic Cor Resista g/cm 2	• 160 nce	4 2	PL \			1	SOIL SYMBOL	SO DESCR		SAMPLE TYPE	SAMPLE NO.	SPT(N)	ELEVATION (m)
0		On completion the test	30 1	1 1	200	 	0 4	0 60	0 80	<u>, </u>				+"	, ,		91
- 0.25 - 0.5 - 0.75		pit was open and dry. Refusal @ 1.12 m bgs on Limestone Bedrock										moist, dar sand, so trace g trace l trace shale trace met	me silt Iravel brick fragments al (FILL)				90.75 - 90.5 - 90.25 -
- 1		(fractured at surface)										SAND, some to trace limeston					90 -
	C	lston associ	ates			-	1	OGC	GED	BY	': R⊦	1	DRILLING DATE	: De	cem	ber	14,
		eotechnical division of 🔽					R	EVII	EWE	D	BY: \	/N	Page 1 of 1				

	NT: Canada Land IECT: Wateridge \	s Company CLC Limite	ed		THOD OJEC					٧	ELE	EV. (m) 92.92	TP No.:	22	20		
	TION: Rockcliffe,			_	RTHIN						1	STING: 450929	PROJECT NO.: C				
SAME	PLE TYPE	AUGER DRI	VEN		H	COR	ING						HELBY	Т	SPL	IT S	POON
DEРТН (m)	INSTRUMENTATION DATA	REMARKS	40 _{St} § Tip F (k	Resista g/cm 2	0 160 ne ance		PL 20 4			<u>. </u>	SOIL SYMBOL	SO DESCRI		SAMPLE TYPE	SAMPLE NO.	SPT(N)	ELEVATION (m)
0 - 0.25		On completion the test pit was open and dry.		30 130	0 200		-0 4					moist, dar TOPS damp, light or SAND, some sil	OIL ange brown				92.75 -
- 0.5												damp, grey SANDY trace org	SILT				92.5
- 0.75		Refusal @ 0.92 m bgs on Limestone Bedrock with thinnly bedded shale layers										damp, ligh SANDY END OF TEST PIT	SILT				92.25 -
													T DDILLING DATE				
	C	Ilston associ	ates								: RI		DRILLING DATE:	De	cem	ber	14,
	ge	eotechnical division of 👣	TERRAPEX				R	EVI	EWE	DI	BY: \	VN	Page 1 of 1				

		Company CLC Limite	ed			D: Ex							TP No.:	2	 24		
	Wateridge V			_		T EN				-		EV. (m) 93.99					
	l: Rockcliffe,		/F^!	NOI		NG:			<u> </u>	_		STING: 450942	PROJECT NO.: C	<u>∏</u>			DO::
SAMPLE T	YPE A	AUGER DRI'		ır Strei	ngth	COR	ING			DY	/NA	MIC CONE S	HELBY	Н.	SPL	IT SI	POON
DEPTH (m)	RUMENTATION DATA	REMARKS	40 _{St} §	(kPa) fic Co Resista g/cm 2	160 nce			W.C.	. LL 0 80		SOIL SYMBOL	SC DESCR		SAMPLE TYPE	SAMPLE NO.	SPT(N)	ELEVATION (m)
0		On completion the test	30 1	JO 130	7 200	Τ΄		ĬĬ		73	****	moist, da					-
0.25		pit was open and dry. Refusal @ 0.38 m bgs on Shale Bedrock										TOPS moist, grey clayey si	ish brown				93.75
-	_					+				_8	₩	END OF TEST PI	Т	H			-
	a	ston associo	ates TERRAPEX						GED EWE				DRILLING DATE: Page 1 of 1	De	cem	ber	14,

	NT: Canada Land	s Company CLC Limite	ed		THOD					 	ELE	EV. (m) 93.61	TP No.:	2:	22		
-	TION: Rockcliffe,			_	RTHIN					-		STING: 451019	PROJECT NO.: C				
			VEN			COR				_			SHELBY	T			POON
			Shea	r Stre (kPa)										T _E			
DEPTH (m)	INSTRUMENTATION DATA	REMARKS	·(k	Resista a/cm 2	nce	4 2		W.C.	LL 0 80		SOIL SYMBOL	SC DESCR		SAMPLE TYPE	SAMPLE NO.	SPT(N)	ELEVATION (m)
0		On completion the test pit was open and dry.	30 1		200					8							93.5 -
- - 0.25 - - -												moist, da sandy silt, so	me organics				93.25 -
- 0.5 - - - - 0.75		Refusal @ 0.90 m bgs										trace shale (FIL	tragments _L)				93 -
- 0.70		on Shale Bedrock				-				_×	▩	END OF TEST PI	т				92.75 -
	а	Iston associ	ates						GED I				DRILLING DATE	De	cem	ber	14,
	ge	TERRAPEX				R	REVI	EWE	D BY	/: \	/N	Page 1 of 1					

	IT: Canada Land ECT: Wateridge	<u>ls Company CLC Limite</u> Village	ed		OJEC					ELE	EV. (m) 93.58	TP No.	: 2	23	}	
	TION: Rockcliffe,			NC	RTH	ING:	503	3541	I		STING: 451053	PROJECT NO.:				-
SAMP	PLE TYPE	AUGER	VEN	•	M	СО	RING	i		DYNA	MIC CONE S	SHELBY	\mathbb{I}	SPI	_IT S	POON
DEРТН (m)	INSTRUMENTATION DATA	REWARKS	40 _{St} Tip F	Resist	0 160 one ance		PL 20 4	W.C.		SOIL SYMBOL	SC DESCR		SAMPLE TYPE	SAMPLE NO.	SPT(N)	ELEVATION (m)
0 - 0.25		On completion the test pit was open and water was filtering in at base of excavation.	f							***************************************	moist, da TOPS					93.5
- 0.5																93.25
- 0.75											damp, sand trace trace o	ly silt clay				92.75
- 1 - 1.25											trace (FII	metal				92.5
- 1.5																92.25 · 92 ·
- 1.75																91.75
-2											mo bro SAND`	wn				91.5
- 2.25 - 2.5											trace to so	me gravel				91.25
- 2.75																91
-3																90.73
- 3.25											mo gre SAND` (TII	ey Y SILT				90.25
- 3.5																90
- 3.75 - 4											mo gre SAND	ev				89.75
- 4.25		Refusal @ 4.40 m bgs on Limestone Bedrock									some to t some larg trace bo	race clay e cobbles oulders				89.5 89.25
											(TII END OF TEST PI					55.20
	C	Ilston associon de la contraction de la contract	ates							BY: RED BY: \		DRILLING DAT	E: De	cen	nber	14,

						ETHOD: Excavator					EV. (m) 93.56	TP No.: 224				
						NORTHING: 5033508					STING: 451041	PROJECT NO.: CO682.00				
SAMPLE TYPE AUGER DRIVEN					CORIN							SHELBY SPLIT SP			POON	
DEPTH (m)	INSTRUMENTATION DATA	REMARKS	Shea 40Sta Tip F	r Strer (kPa) flc Cor Resista g/cm 2	gth e160 nce	-	PL V		LL	SOIL SYMBOL	SC DESCR)IL	SAMPLE TYPE	SAMPLE NO.	SPT(N)	ELEVATION (m)
0		On completion the test pit was open and dry.	50 10	00 150	200	2	20 40	60	80	0)	Asphaltic	concrete	"	- 07	0)	93.5 -
- 0.25											damp, grey, sand	and gravel (FILL)				93.25 -
0.5																93 -
- 0.75																92.75 -
-1											mo					92.5
1.25											bro sand, so some trace	ome silt gravel				92.25 -
1.5											and limestone fr					92 -
- 1.75																91.75 -
-2																91.5 -
- 2.25											moist, blac organic la					91.25 -
- 2.5										XXX	moist, lig SILTY	SAND				91 -
- 2.75											trace (gravei				90.75
-3																90.5
- 3.25											mo greyish SAND`	brown				90.25 -
- 3.5											trace (clay				90 -
- 3.75		Refusal @ 4.12 m bgs														89.75 -
- 4		on Limestone Bedrock									END OF TEST D	т				89.5 -
											END OF TEST PI	1				
	a	Iston associon	ates							Y: RH		DRILLING DATE: Page 1 of 1	De	cem	ber	14,

alston	associates
A divisio	n of Torranov Environmental Ltd

Reference CO682.00 February 5, 2019

APPENDIX D PREVIOUS BOREHOLE AND TEST PIT LOG SHEETS

DST REF. No.: IN-SO-026755
CLIENT: Canada Lands Company
PROJECT: Site Servicing Phase 1B

LOCATION: Wateridge Village, Ottawa, Ontario

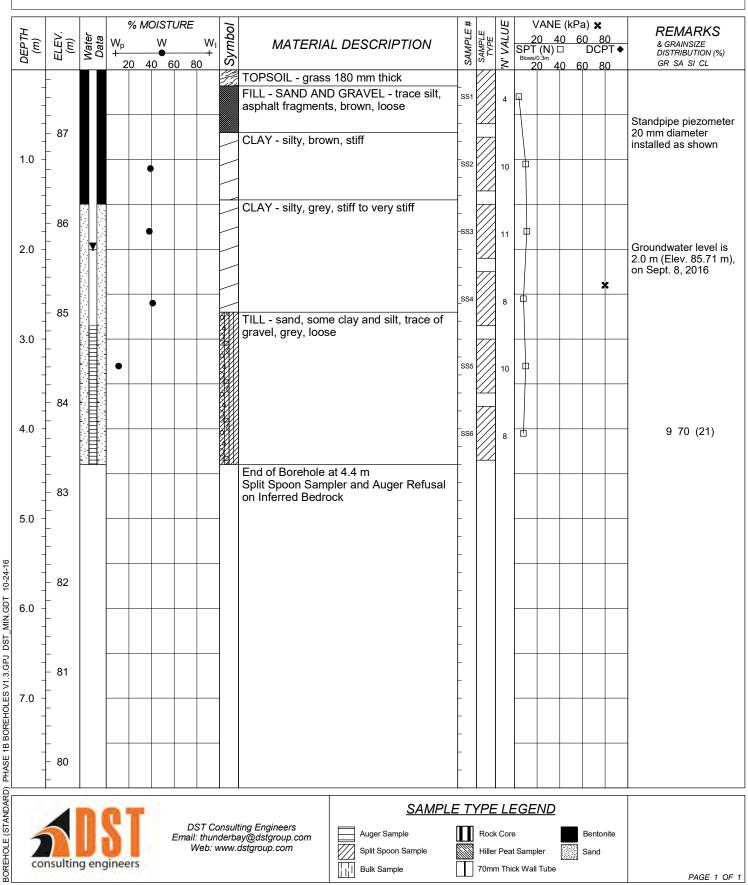
SURFACE ELEV.: 87.71 metres

Drilling Data

METHOD: Hollow Stem Auger

DIAMETER: 200 mm DATE: August 26, 2016

COORDINATES: 5035157.53 m N, 372599.17 m E



DST REF. No.: IN-SO-026755
CLIENT: Canada Lands Company
PROJECT: Site Servicing Phase 1B

LOCATION: Wateridge Village, Ottawa, Ontario

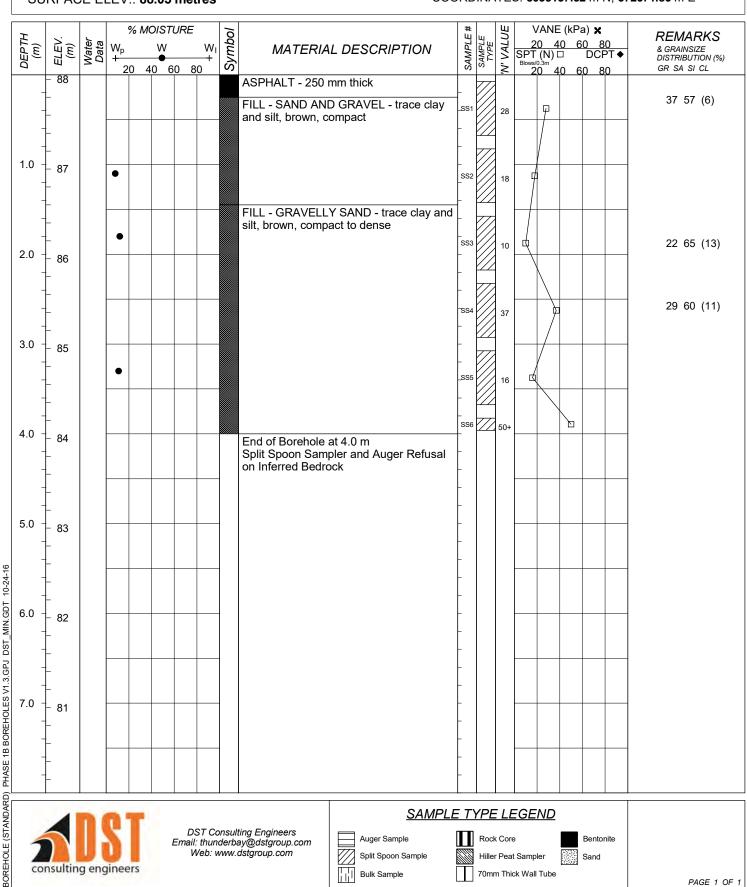
SURFACE ELEV.: 88.05 metres

Drilling Data

METHOD: Hollow Stem Auger

DIAMETER: 200 mm DATE: August 26, 2016

COORDINATES: 5035157.52 m N, 372671.86 m E



DST REF. No.: IN-SO-026755
CLIENT: Canada Lands Company
PROJECT: Site Servicing Phase 1B

LOCATION: Wateridge Village, Ottawa, Ontario

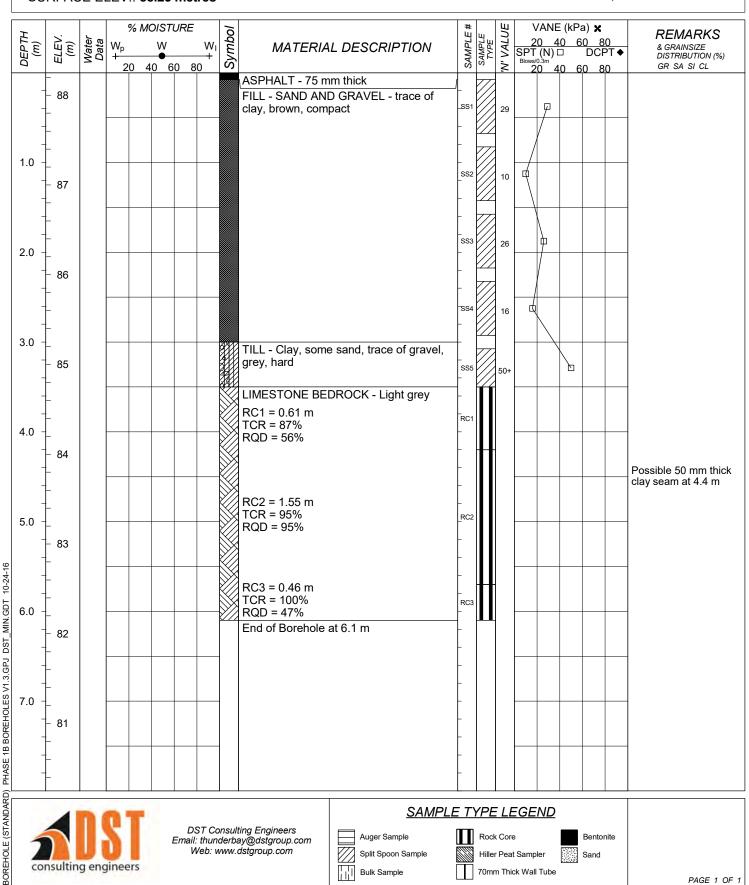
SURFACE ELEV.: 88.25 metres

Drilling Data

METHOD: Hollow Stem Auger / NQ Size Core Barrel

DIAMETER: 200 mm DATE: September 16, 2016

COORDINATES: 5035157.56 m N, 372725.95 m E



DST REF. No.: IN-SO-026755
CLIENT: Canada Lands Company
PROJECT: Site Servicing Phase 1B

LOCATION: Wateridge Village, Ottawa, Ontario

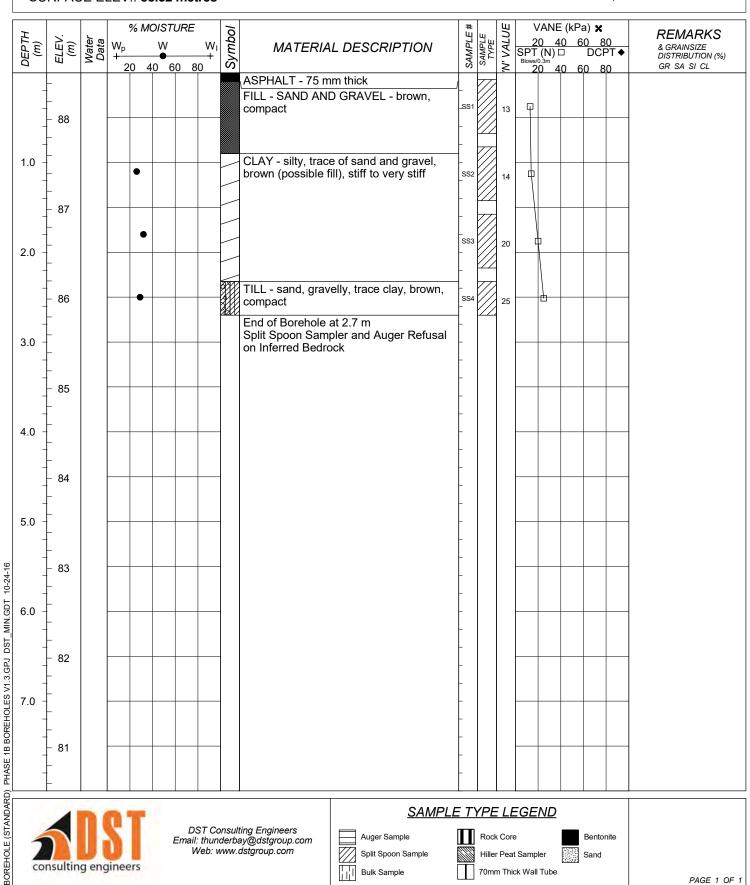
SURFACE ELEV.: 88.52 metres

Drilling Data

METHOD: Hollow Stem Auger DIAMETER: 200 mm

DATE: September 2, 2016

COORDINATES: 5035156.93 m N, 372783.61 m E



DST REF. No.: IN-SO-026755
CLIENT: Canada Lands Company
PROJECT: Site Servicing Phase 1B

LOCATION: Wateridge Village, Ottawa, Ontario

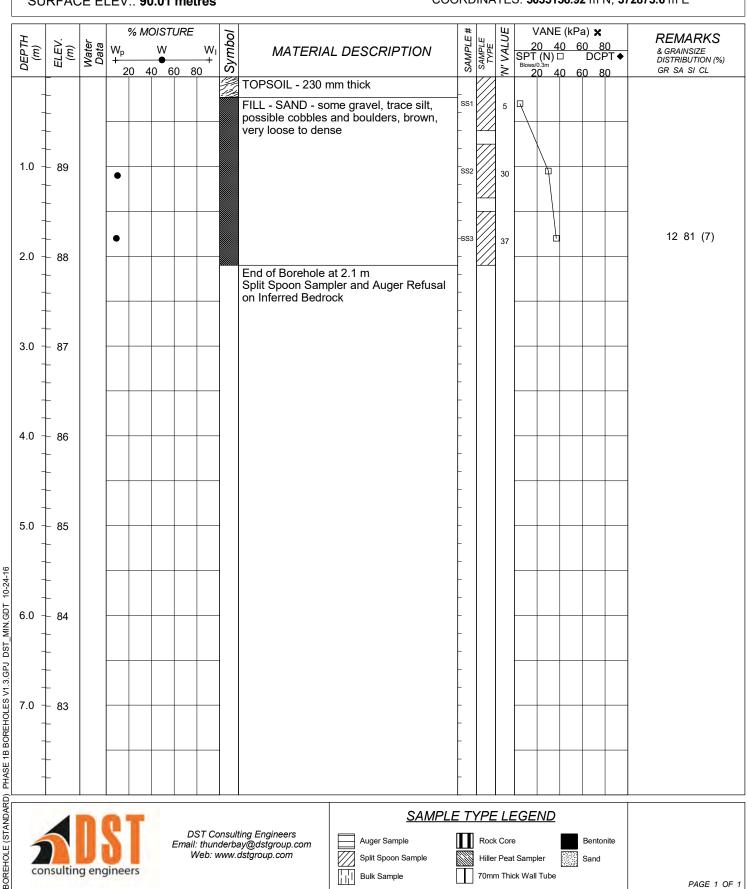
SURFACE ELEV.: 90.01 metres

Drilling Data

METHOD: Hollow Stem Auger

DIAMETER: 200 mm DATE: August 29, 2016

COORDINATES: 5035156.92 m N, 372873.6 m E



DST REF. No.: IN-SO-026755
CLIENT: Canada Lands Company
PROJECT: Site Servicing Phase 1B

LOCATION: Wateridge Village, Ottawa, Ontario

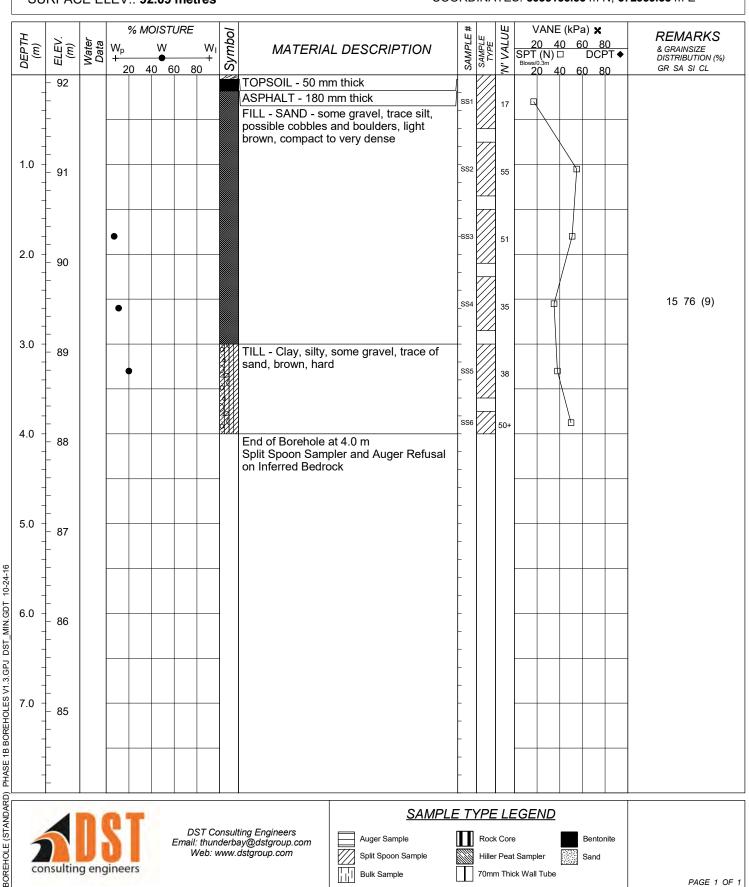
SURFACE ELEV.: 92.09 metres

Drilling Data

METHOD: Hollow Stem Auger DIAMETER: 200 mm

DATE: September 2, 2016

COORDINATES: 5035156.35 m N, 372959.35 m E



DST REF. No.: IN-SO-026755
CLIENT: Canada Lands Company
PROJECT: Site Servicing Phase 1B

LOCATION: Wateridge Village, Ottawa, Ontario

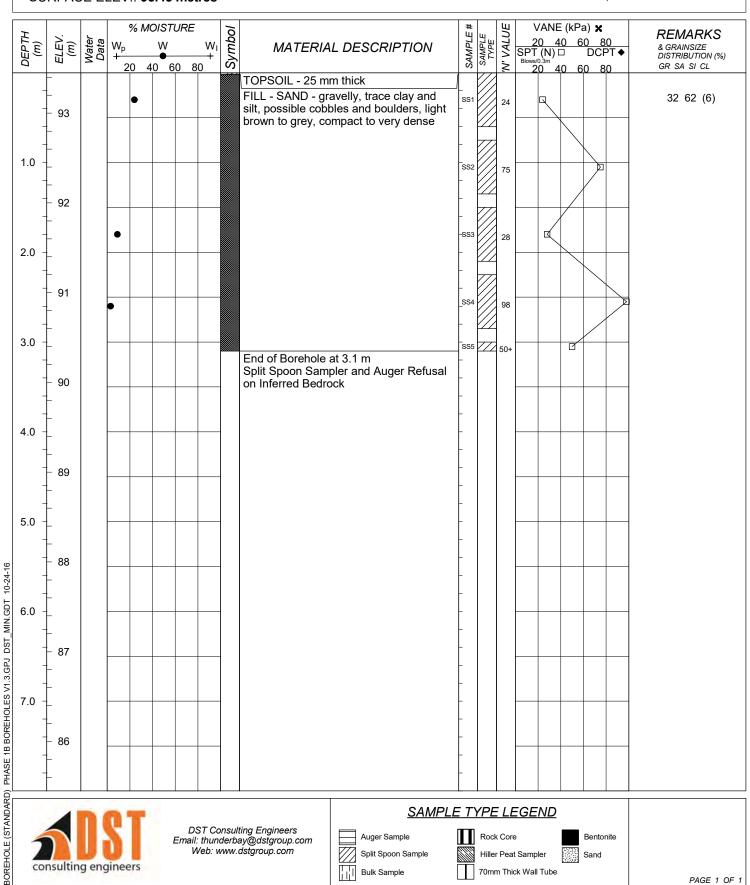
SURFACE ELEV.: 93.45 metres

Drilling Data

METHOD: Hollow Stem Auger DIAMETER: 200 mm

DATE: September 1, 2016

COORDINATES: 5035156.4 m N, 373046.35 m E



DST REF. No.: IN-SO-026755 CLIENT: Canada Lands Company PROJECT: Site Servicing Phase 1B

LOCATION: Wateridge Village, Ottawa, Ontario

SURFACE ELEV.: 93.58 metres

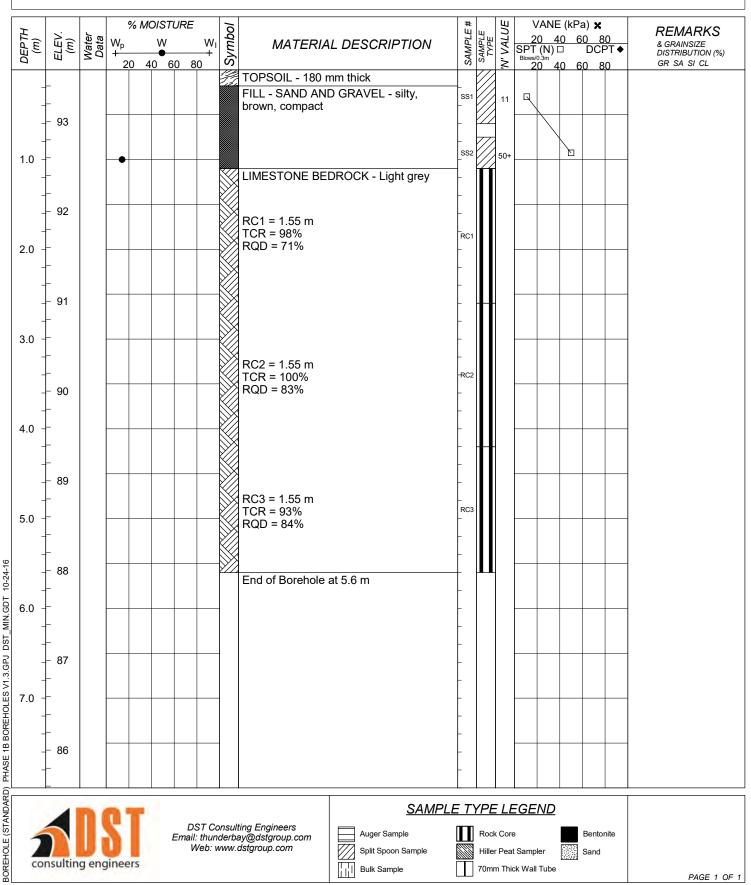
Drilling Data

METHOD: Hollow Stem Auger / NQ Size Core Barrel

DIAMETER: 200 mm

DATE: August 29, 2016

COORDINATES: 5035156.34 m N, 373117.37 m E



DST REF. No.: IN-SO-026755
CLIENT: Canada Lands Company
PROJECT: Site Servicing Phase 1B

LOCATION: Wateridge Village, Ottawa, Ontario

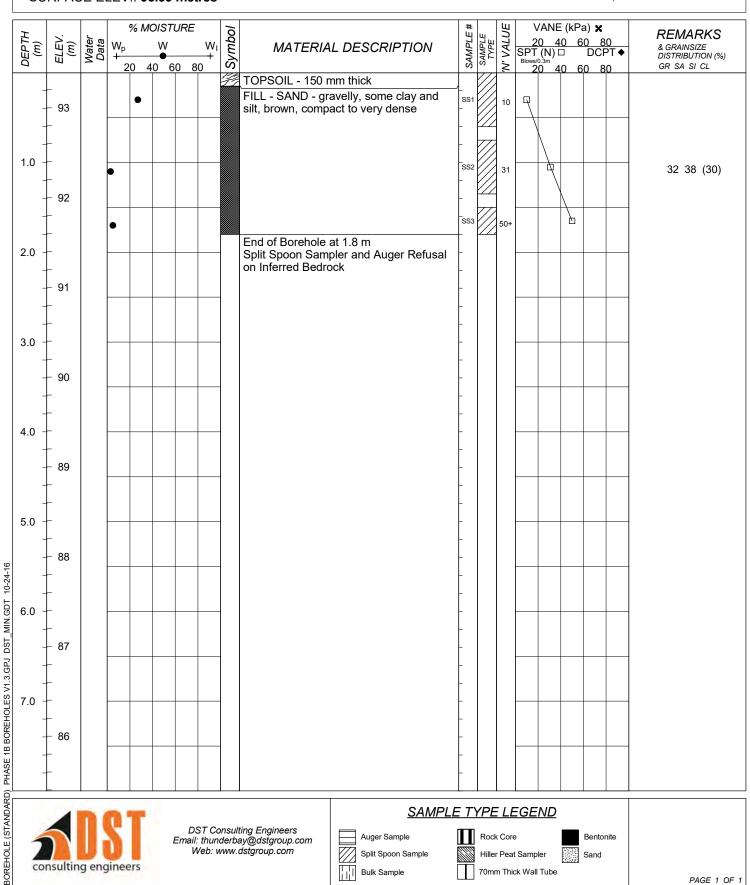
SURFACE ELEV.: 93.39 metres

Drilling Data

METHOD: Hollow Stem Auger

DIAMETER: 200 mm DATE: August 29, 2016

COORDINATES: 5035170.89 m N, 373171.56 m E



DST REF. No.: IN-SO-026755
CLIENT: Canada Lands Company

PROJECT: Site Servicing Phase 1B

LOCATION: Wateridge Village, Ottawa, Ontario SURFACE ELEV.: 88.26 metres

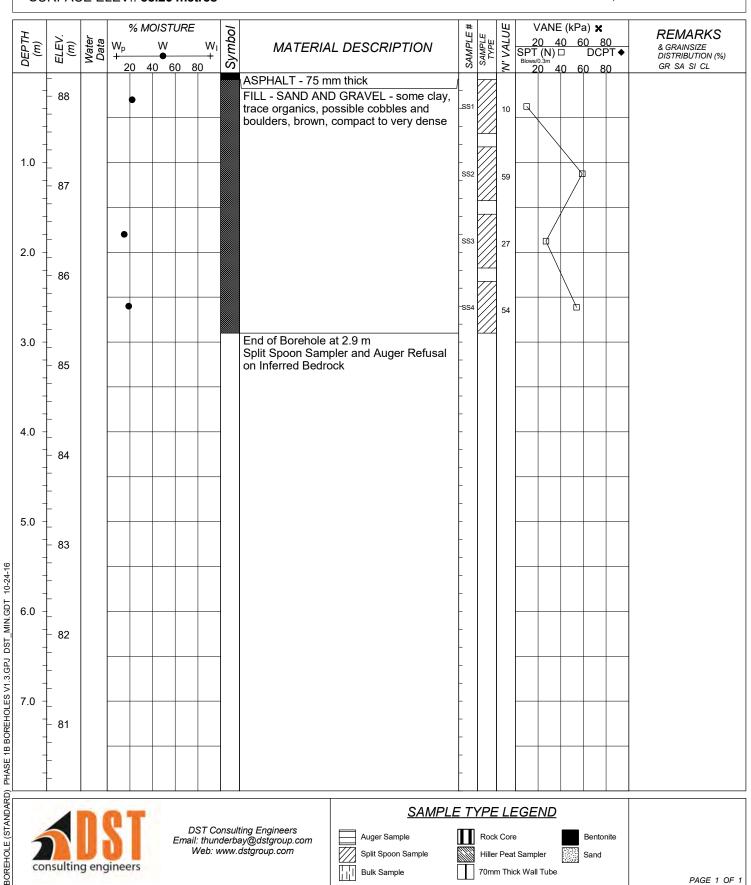
Drilling Data

METHOD: Hollow Stem Auger

DIAMETER: 200 mm

DATE:

COORDINATES: 5035209.85 m N, 372533.31 m E



DST REF. No.: IN-SO-026755 **CLIENT: Canada Lands Company** PROJECT: Site Servicing Phase 1B

LOCATION: Wateridge Village, Ottawa, Ontario

SURFACE ELEV.: 88.28 metres

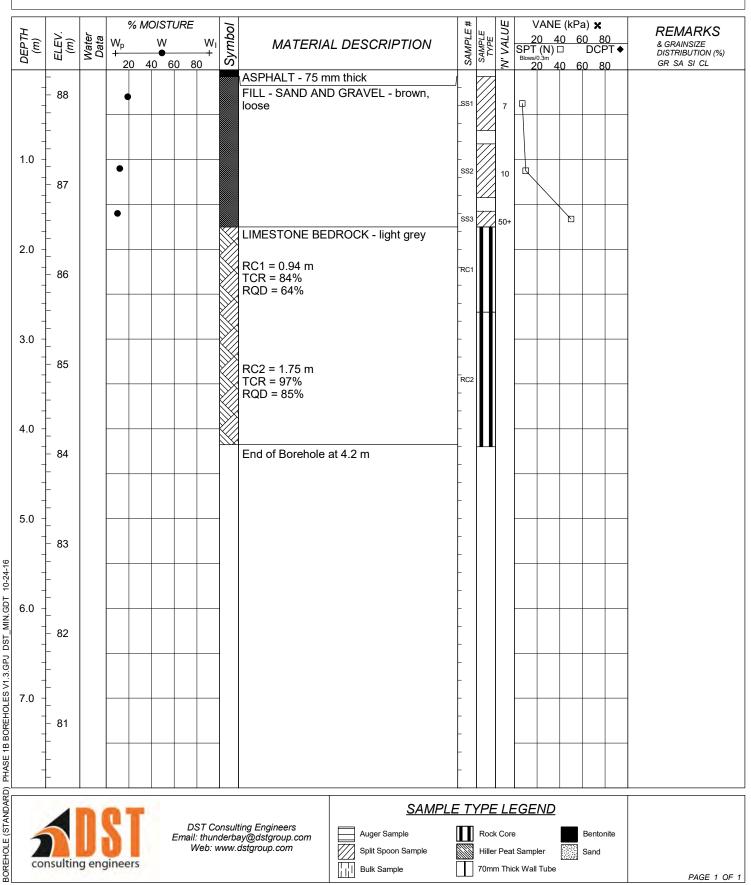
Drilling Data

METHOD: Hollow Stem Auger / NQ Size Core Barrel

DIAMETER: 200 mm

DATE: August 26, 2016

COORDINATES: 5035209.64 m N, 372567.49 m E



DST REF. No.: **OE-OT-015358**

CLIENT: Canada Lands Company (CLC)

PROJECT: Phase 1A Development - Site Servicing LOCATION: Former CFB Rockliffe, Ottawa, Ontario,

SURFACE ELEVATION: 81.20 metres

Drilling Data

METHOD: Hollow Stem Auger/Core Barrel/NQ

DIAMETER: 200 mm

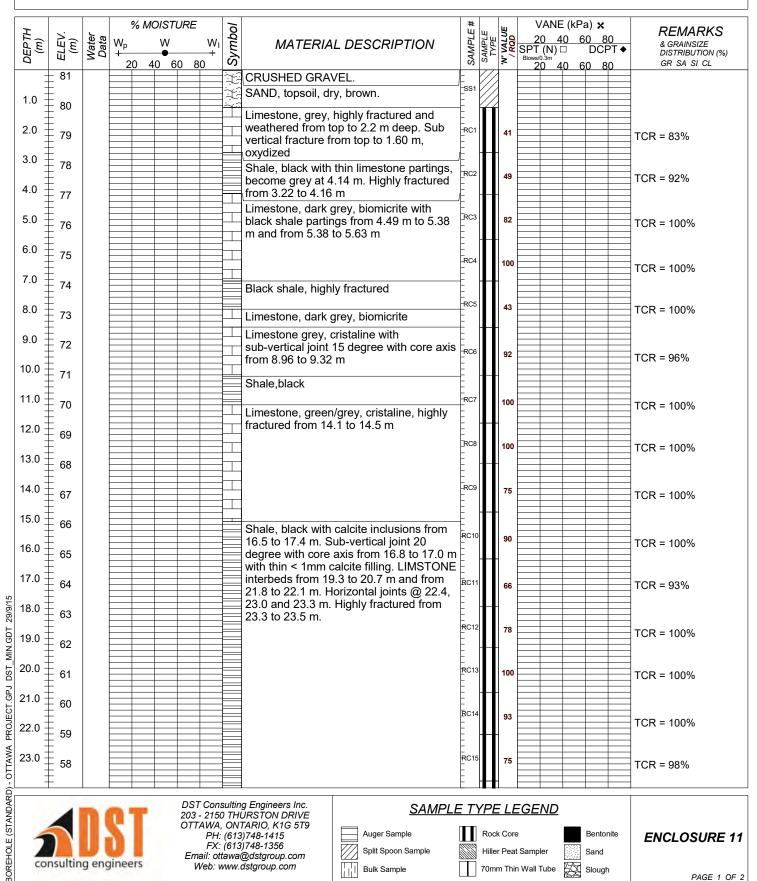
DATE: 26 August 2015

70mm Thin Wall Tube

Slough

PAGE 1 OF 2

COORDINATES: 5033823.631 m N, 450194.353 m E



Bulk Sample

DST REF. No.: **OE-OT-015358**

CLIENT: Canada Lands Company (CLC)

PROJECT: Phase 1A Development - Site Servicing LOCATION: Former CFB Rockliffe, Ottawa, Ontario,

SURFACE ELEVATION: 81.20 metres

Drilling Data

METHOD: Hollow Stem Auger/Core Barrel/NQ

DIAMETER: 200 mm

DATE: 26 August 2015

Hiller Peat Sampler

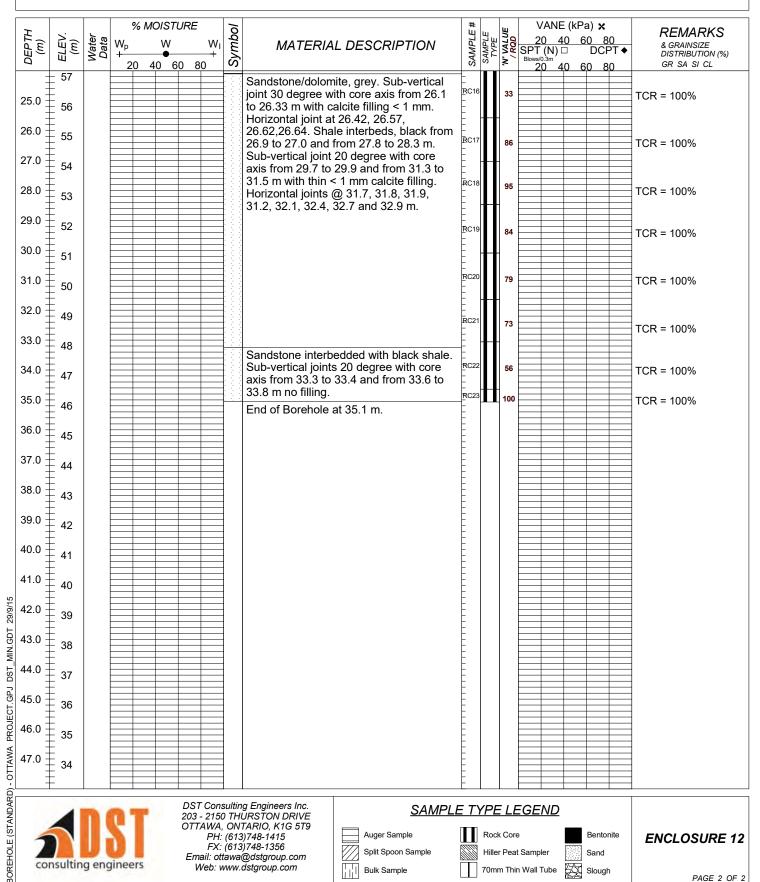
70mm Thin Wall Tube

Sand

Slough

PAGE 2 OF 2

COORDINATES: 5033823.631 m N, 450194.353 m E



Bulk Sample

Email: ottawa@dstgroup.com

Web: www.dstgroup.com

consulting engineers

DST REF. No.: **OE-OT-015358**

CLIENT: Canada Lands Company (CLC)

PROJECT: Phase 1A Development - Site Servicing LOCATION: Former CFB Rockliffe, Ottawa Ontario

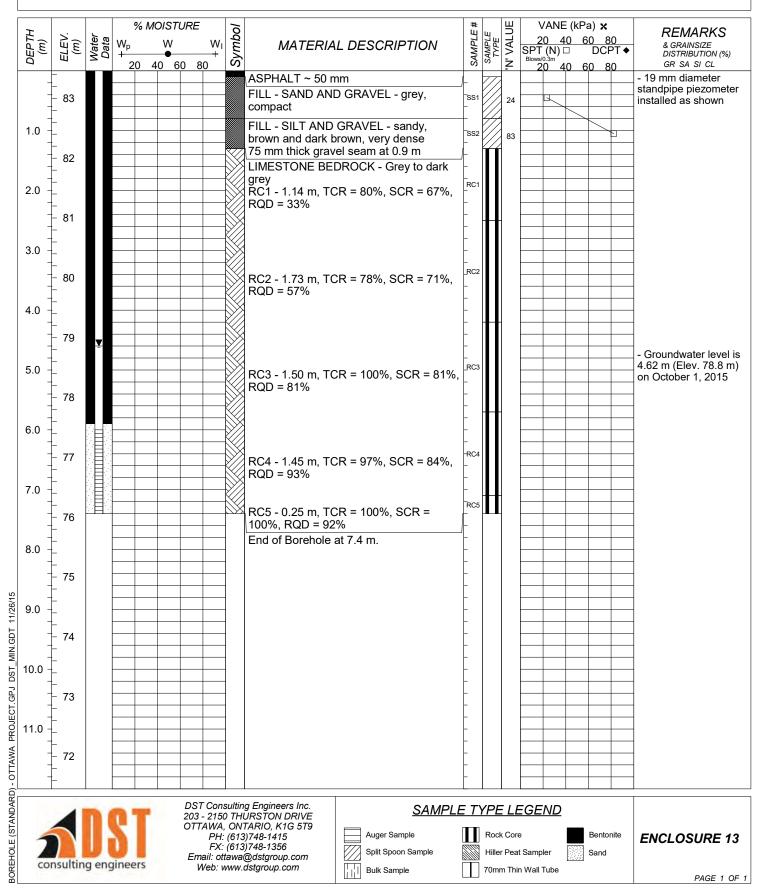
SURFACE ELEVATION: 83.46 metres

Drilling Data

METHOD: Hollow Stem Auger/ NQ Size Core Barrel DIAMETER: 200 mm

DATE: August 21, 2015

COORDINATES: 5033743.938 m N, 450109.419 m E



DST REF. No.: **OE-OT-015358**

CLIENT: Canada Lands Company (CLC)

PROJECT: Phase 1A Development - Site Servicing LOCATION: Former CFB Rockliffe, Ottawa Ontario

SURFACE ELEVATION: 85.34 metres

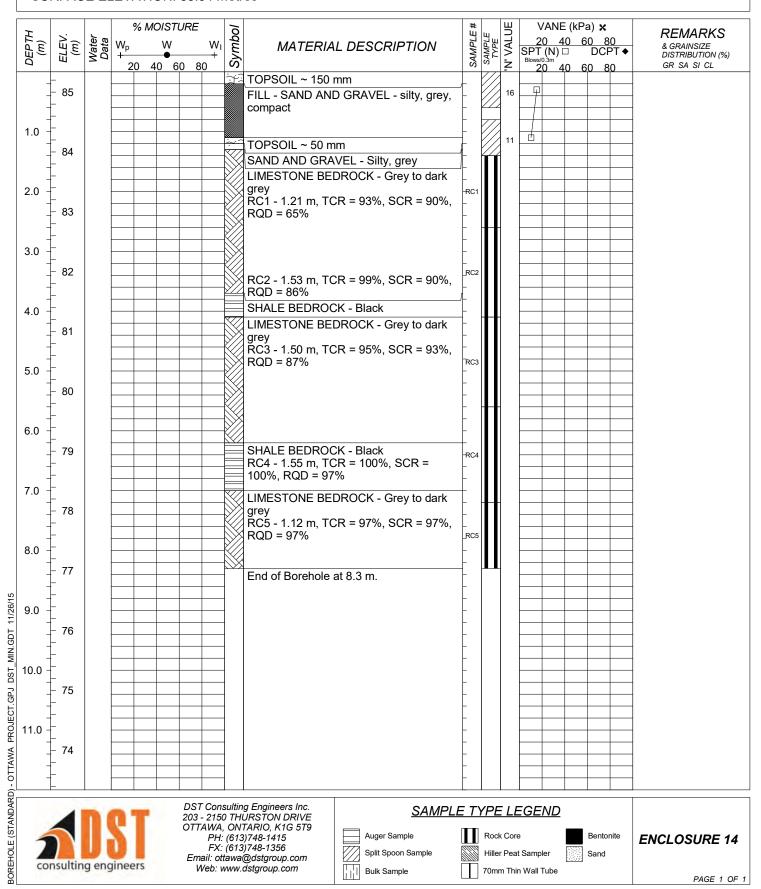
Drilling Data

METHOD: Hollow Stem Auger/ NQ Size Core Barrel

DIAMETER: 200 mm

DATE: **August 21, 2015**

COORDINATES: 5033606.53 m N, 450180.104 m E



DST REF. No.: **OE-OT-015358**

CLIENT: Canada Lands Company (CLC)

PROJECT: Phase 1A Development - Site Servicing LOCATION: Former CFB Rockliffe, Ottawa Ontario

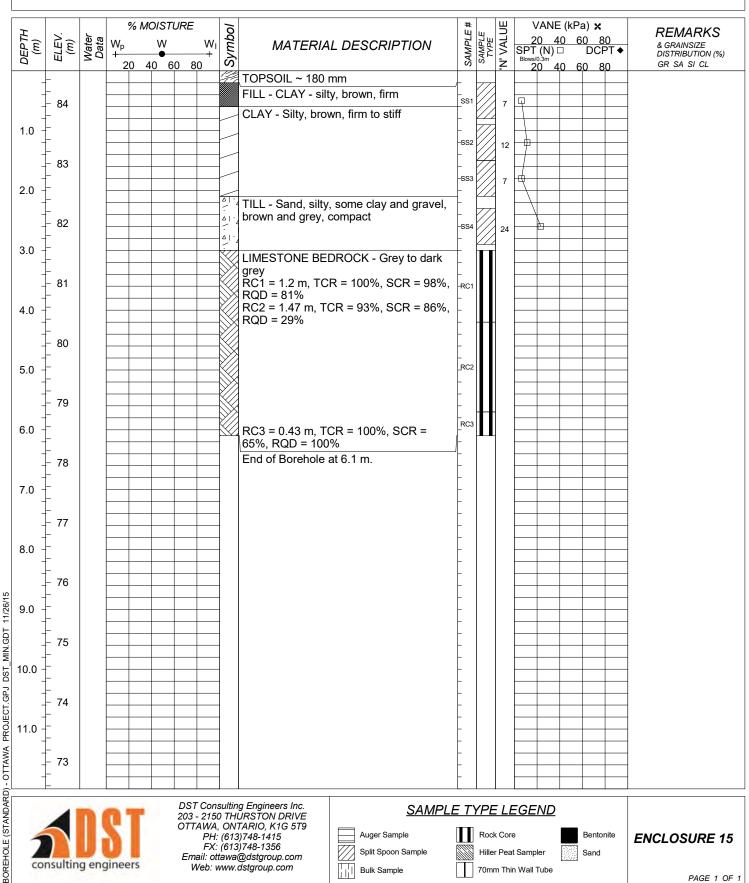
SURFACE ELEVATION: 84.55 metres

Drilling Data

METHOD: Hollow Stem Auger/ NQ Size Core Barrel

DIAMETER: 200 mm DATE: August 21, 2015

COORDINATES: 5033393.443 m N, 450130.224 m E



DST REF. No.: **OE-OT-015358**

CLIENT: Canada Lands Company (CLC)

PROJECT: Phase 1A Development - Site Servicing LOCATION: Former CFB Rockliffe, Ottawa Ontario

SURFACE ELEVATION: 86.64 metres

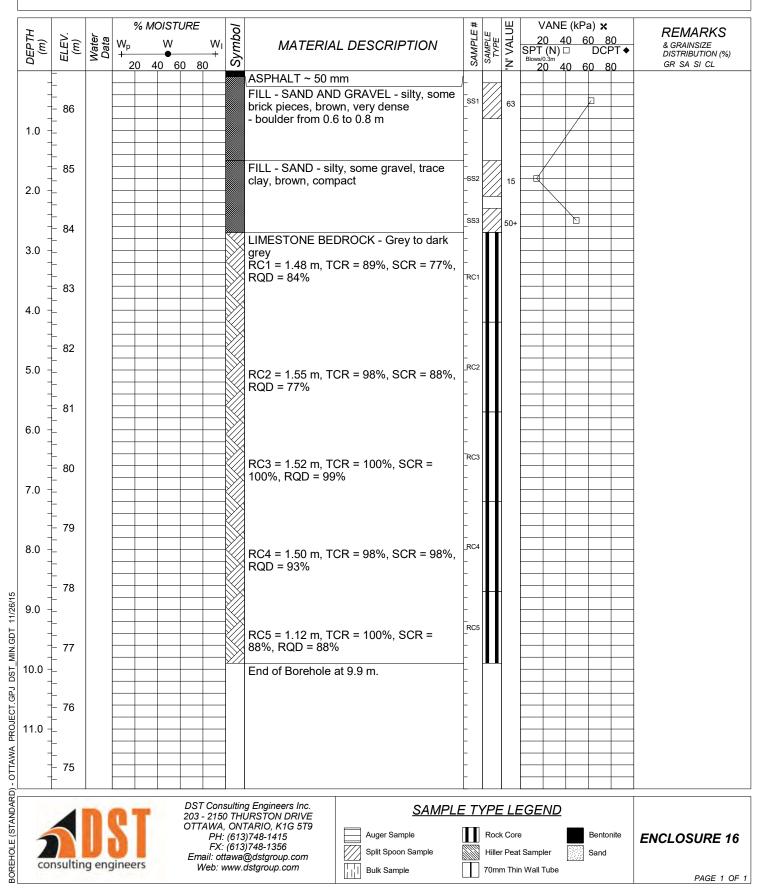
Drilling Data

METHOD: Hollow Stem Auger/ NQ Size Core Barrel

DIAMETER: 200 mm

DATE: August 21, 2015

COORDINATES: 5033444.108 m N, 450254.911 m E



DST REF. No.: **OE-OT-015358**

CLIENT: Canada Lands Company (CLC)

PROJECT: Phase 1A Development - Site Servicing LOCATION: Former CFB Rockliffe, Ottawa Ontario

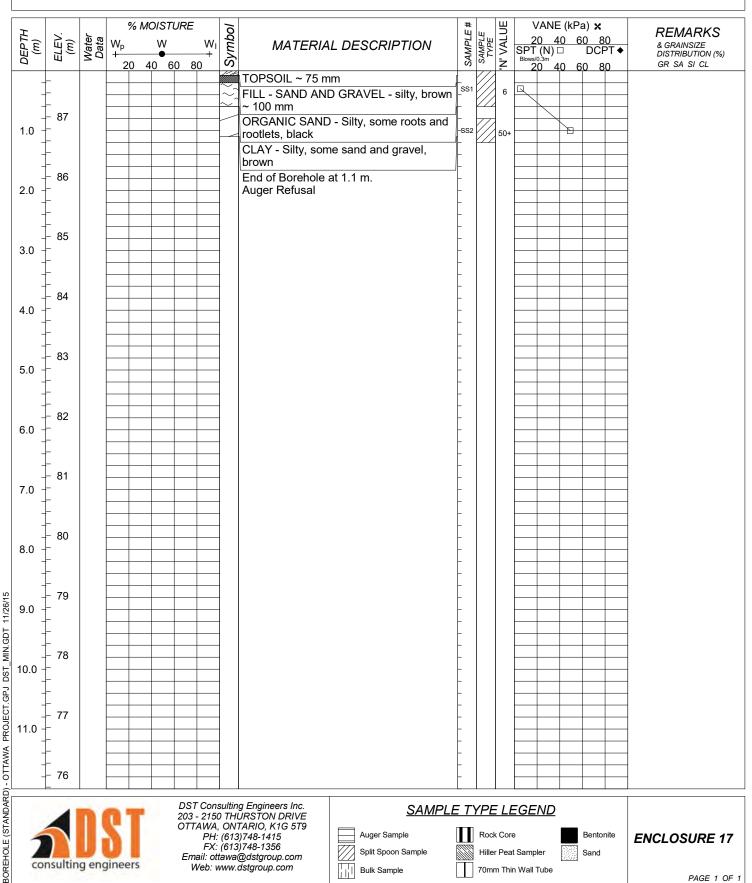
SURFACE ELEVATION: 87.77 metres

Drilling Data

METHOD: Hollow Stem Auger DIAMETER: 200 mm

DATE: August 21, 2015

COORDINATES: 5033470.374 m N, 450323.531 m E



DST REF. No.: **OE-OT-015358**

CLIENT: Canada Lands Company (CLC)

PROJECT: Phase 1A Development - Site Servicing LOCATION: Former CFB Rockliffe, Ottawa Ontario

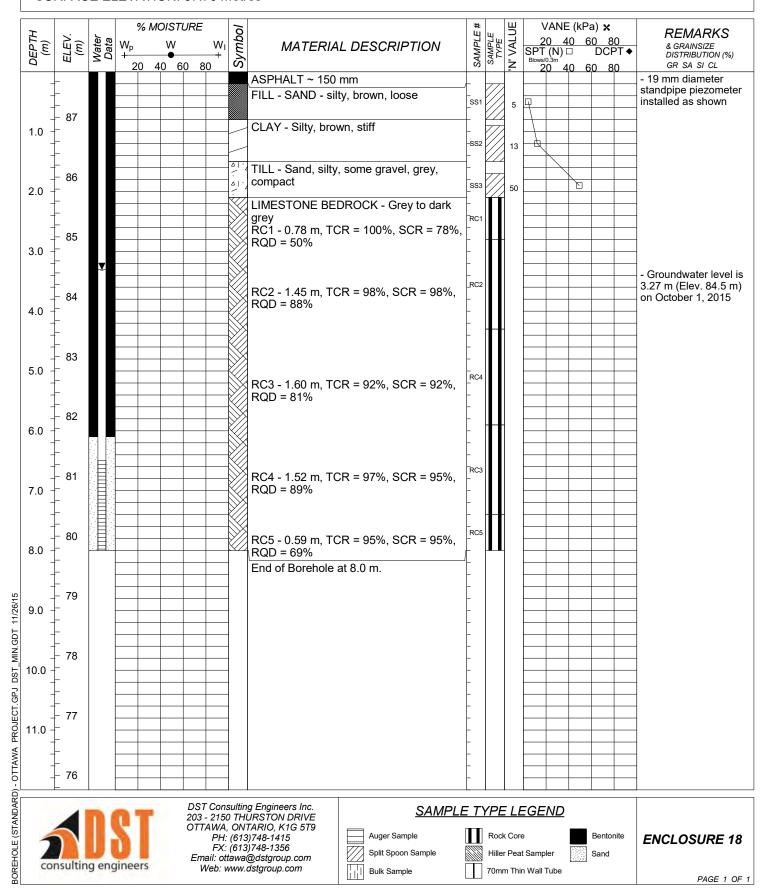
SURFACE ELEVATION: 87.76 metres

Drilling Data

METHOD: Hollow Stem Auger/ NQ Size Core Barrel DIAMETER: 200 mm

DATE: August 26, 2015

COORDINATES: 5033477.421 m N, 450420.068 m E



RECORD OF BOREHOLE: 15-1

SHEET 1 OF 1

DATUM: Geodetic

SAMPLER HAMMER, 64kg; DROP, 760mm

LOCATION: N 5034902.3 ;E 371648.9

BORING DATE: January 26, 2015

PENETRATION TEST HAMMER, 64kg; DROP, 760mm

ا رس	阜	SOIL PROFILE			SA	MPLES	RESISTA	PENETRA NCE, BLOV	. ПОМ VS/0.3п	, \	HYDRAUL k,	cm/s	JUTIVII	.,	A S	PIEZOMETER
METRES	BORING METHOD	[0]		[] [C]		NUMBER TYPE BLOWS/0.30m	20 40 60 80			10-6				ADDITIONAL LAB. TESTING	OR STANDPIPE	
Ä	NG	DESCRIPTION	ĬĀ	ELEV. DEPTH	NUMBER	TYPE WS/0.3	SHEAR S Cu. kPa	TRENGTH	nal V. rem V	. + Q -● . ⊕ U- O		R CONT			99	INSTALLATION
۱ ا	BOR		STRATA PLOT	(m)	ž	 	20	40	60	80	Wp I— 20	40_	—— الح	—J WI 80	1,2	1
\dashv		GROUND SURFACE	**	71.35		t1: "	20				20		:			
0		TOPSOIL - (SM) SILTY SAND; dark	EEE	0.00					_		T	:	<u> </u>			X
	!	brown; moist (CI/CH) SILTY CLAY to CLAY; grey	- 177	71.10 0.25	1	SS 14							İ			
	İ	(CI/CH) SILTY CLAY to CLAY; grey brown (WEATHERED CRUST); cohesive, very stiff to stilf, w>PL							:					1		
		coriesive, very suit to suit, w>FL				-						i				l 💥
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3	Power Diam.				-							:	-			
	mu.			68.00	_ ا	SS 2		•								
	200	(Cl/CH) SILTY CLAY to CLAY; grey; cohesive, w>PL, firm to stiff		3.35	,	. aa . 2 ! ;										
		55,100170; 117.1 C; 11111 (0 3011			ŀ ·	1			-		1			i		
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4						! '			1	-			i			
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	 -	End of Borehole	- KK/2	65.56 5.79				:	+ 1				_			**
6													•	j	İ	W.L. in Standpipe
										!				į		W.L. in Standpipe at Elev. 69.16 m on February 4, 2015
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RECORD OF BOREHOLE: 15-2

SHEET 1 OF 1

LOCATION: N 5034949.1 ;E 371734.0

BORING DATE: January 26, 2015

DATUM: Geodetic

SAMPLER HAMMER, 64kg; DROP, 760mm

PENETRATION TEST HAMMER, 64kg; DROP, 760mm

ų	ᅙ	SOIL PROFILE				MPLES	DYNAMIC PENETRA RESISTANCE, BLOW	TION \ VS/0.3m	HYDRAULIC CONDUCTIVITY, k, cm/s	.0
DEPTH SCALE METRES	BORING METHOD			_	æ	TYPE BLOWS/0.30m	20 40	60 80	10 ⁻⁶ 10 ⁻⁵ 10 ⁻⁴ 10 ⁻³	O PIEZOMETER OR OR STANDPIPE INSTALLATION
EE :	SING.	DESCRIPTION	STRATA PLOT	ELEV.		YPE VS/0.	SHEAR STRENGTH Cu, kPa	nat V. + Q - ● rem V. ⊕ U - O	WATER CONTENT PERCENT	STANDPIPE INSTALLATION
ដ	BOR			(m)] ≥	"IO	20 40		YVP I VVI	₹ 5
		GROUND SURFACE	+ "	73.05	 		20 40	60 80	20 40 60 80	
- 0	PA (HS)	TOPSOIL		0.00	H	SS >50				·
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		End of Borehole Auger Refusal			ŀ			i		
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RECORD OF BOREHOLE: 15-3

SHEET 1 OF 2

DATUM: Geodetic

LOCATION: N 5034983.6 ;E 371807.7 SAMPLER HAMMER, 64kg; DROP, 760mm BORING DATE: January 28, 2015

PENETRATION TEST HAMMER, 64kg; DROP, 760mm

DEPTH SCALE METRES	ᇤ		TI	1		SOIL PROFILE SAMPLES					cm/s			コブラ	PIEZOMETER
-≓I	5 1		9		œ	ĕ	20 40	60	80	10⁴	10 ⁻⁵	104	10 ⁻³	SE	OR
- 발	BORING METHOD	DESCRIPTION	STRATA PLOT	ELEV.	NUMBER	TYPE BLOWS/0.30m	SHEAR STRENGTH Cu, kPa	nat V.	+ Q - ●	WATE	R CONTE			ADDITIONAL LAB. TESTING	STANDPIPE INSTALLATION
7	BOR		Ĭ.	DEPTH (m)	Ž	⊢ Š				Wp ⊢		W		83	
\dashv	··	GROUND SURFACE	100		-		20 40	60	80	20	40	60	80		
0		FILL/TOPSOIL - (SM) SILTY SAND, some gravel; dark brown; moist	 	76.24 0.00				-				-+			
	Stem		\bowtie	75.94	1	SS 19			, i	i					
	ger	(SM/GM) SILTY SAND and GRAVEL; brown; non-cohesive, moist, compact to		0.30			•								
	Power Auger 200 mm Diam. (Hollow Stem)	dense													Bentonite Seal
	P. Bola				2	SS 31					:				
'	8				:	:	i	i			:				
-		Fresh thinks to medium hadded growto		74.89 1.35											
		Fresh, thinly to medium bedded, grey to dark grey DOLOSTONE BEDROCK, with shale and sandstone interbeds		1.00	i										
		with shale and sandstone interbeds				:	: :								
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LOCATION: N 5034922.7 ;E 371689.0

RECORD OF PROBEHOLE: 15-10

BORING DATE: January 29, 2015

SHEET 1 OF 1

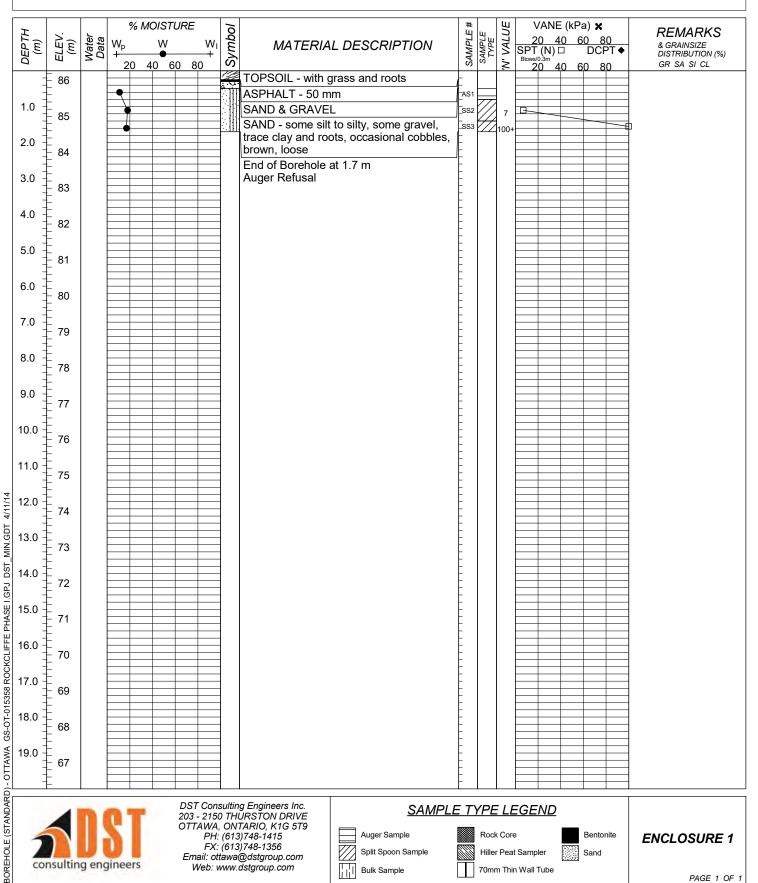
DATUM: Geodetic

щ	0	SOIL PROFILE			SAMPLES	DYNAMIC PENETRA RESISTANCE, BLOV	ATION WS/0.3m	HYDRAULIC CONDUCTIVITY, k, cm/s	
RES	MET				30m	20 40	60 80	10 ⁻⁶ 10 ⁻⁶ 10 ⁻⁶ 10 ⁻³	PIEZOMETER OR STANDPIPE
DEPTH SCALE METRES	BORING METHOD	DESCRIPTION	DEP	ELEV. DEPTH	NUMBER TYPE BLOWS/0.30m	SHEAR STRENGTH Cu, kPa	nat V Q - ● rem V. ⊖ U - ⊜	WATER CONTENT PERCENT Wp I W WI	PIEZOMETER OR OR STANDPIPE INSTALLATION
	ă	GROUND SURFACE	P.	(m)		20 40	60 80	<u>20 40 60 80</u>	
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DST REF. No.: **OE-OT-015358 CLIENT: Canada Lands Company** PROJECT: Former CFB Rockcliffe LOCATION: Ottawa, Ontario SURFACE ELEV.: 86.27 metres

Drilling Data METHOD: Hollow Stem Auger DIAMETER: 80 mm ID DATE: March 3, 2014

COORDINATES: 5033642.48 m N, 450271.46 m E





DST Consulting Engineers Inc. 203 - 2150 THURSTON DRIVE OTTAWA, ONTARIO, K1G 5T9 PH: (613)748-1415 FX: (613)748-1356 Email: ottawa@dstgroup.com

Web: www.dstgroup.com

Auger Sample Split Spoon Sample

Bulk Sample

Rock Core Hiller Peat Sampler

70mm Thin Wall Tube

SAMPLE TYPE LEGEND

Bentonite Sand

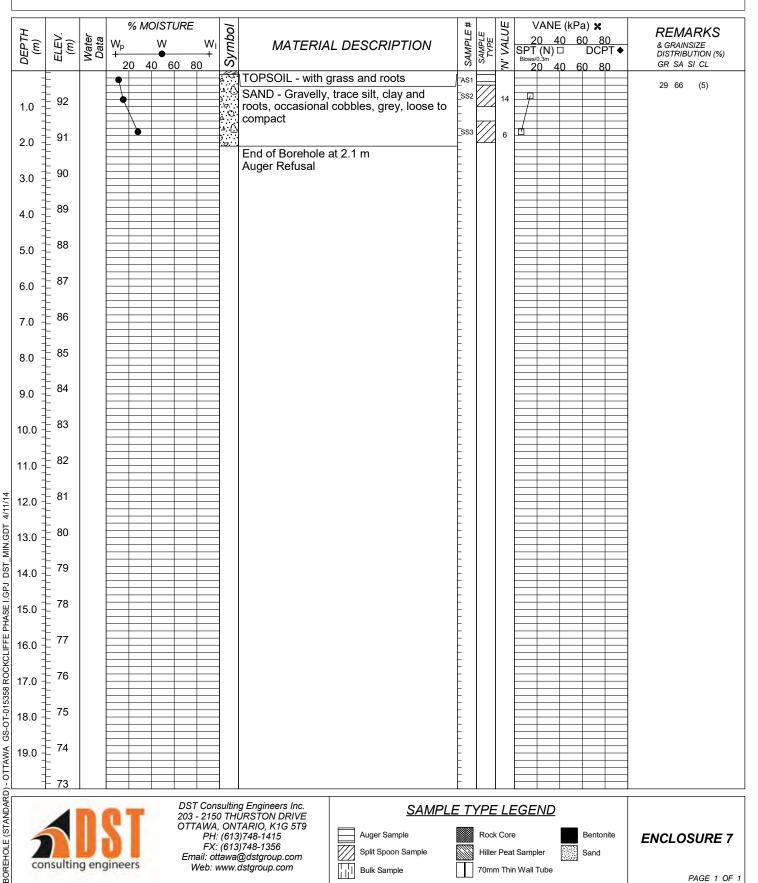
ENCLOSURE 1

DST REF. No.: **OE-OT-015358 CLIENT: Canada Lands Company** PROJECT: Former CFB Rockcliffe LOCATION: Ottawa, Ontario SURFACE ELEV.: 92.85 metres

Drilling Data

METHOD: Hollow Stem Auger DIAMETER: 80 mm ID DATE: March 5, 2014

COORDINATES: 5033592.04 m N, 450910.85 m E



consulting engineers

DST Consulting Engineers Inc. 203 - 2150 THURSTON DRIVE OTTAWA, ONTARIO, K1G 5T9 PH: (613)748-1415 FX: (613)748-1356 Email: ottawa@dstgroup.com

Web: www.dstgroup.com

SAMPLE TYPE LEGEND

Auger Sample Split Spoon Sample

Bulk Sample

Rock Core Hiller Peat Sampler

70mm Thin Wall Tube

Bentonite Sand

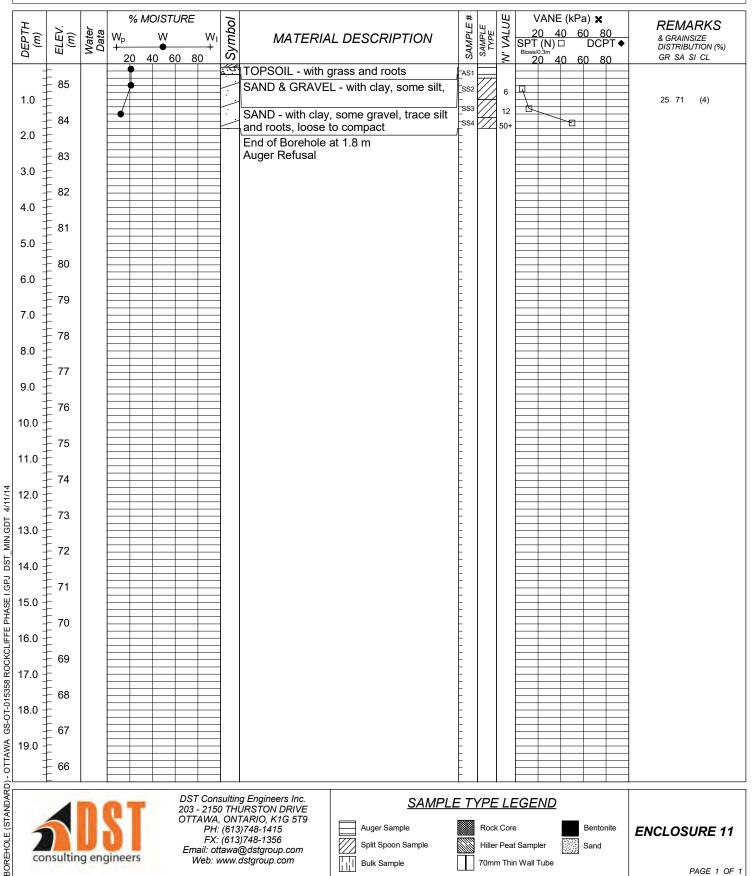
ENCLOSURE 7

DST REF. No.: **OE-OT-015358 CLIENT: Canada Lands Company** PROJECT: Former CFB Rockcliffe LOCATION: Ottawa, Ontario SURFACE ELEV.: 85.57 metres

Drilling Data

METHOD: Hollow Stem Auger DIAMETER: 80 mm ID DATE: February 26, 2014

COORDINATES: 5033475.8 m N, 450066.74 m E



203 - 2150 THURSTON DRIVE OTTAWA, ONTARIO, K1G 5T9 PH: (613)748-1415 FX: (613)748-1356 Email: ottawa@dstgroup.com

Web: www.dstgroup.com

Auger Sample Split Spoon Sample

Bulk Sample

70mm Thin Wall Tube

Rock Core Hiller Peat Sampler

Bentonite Sand

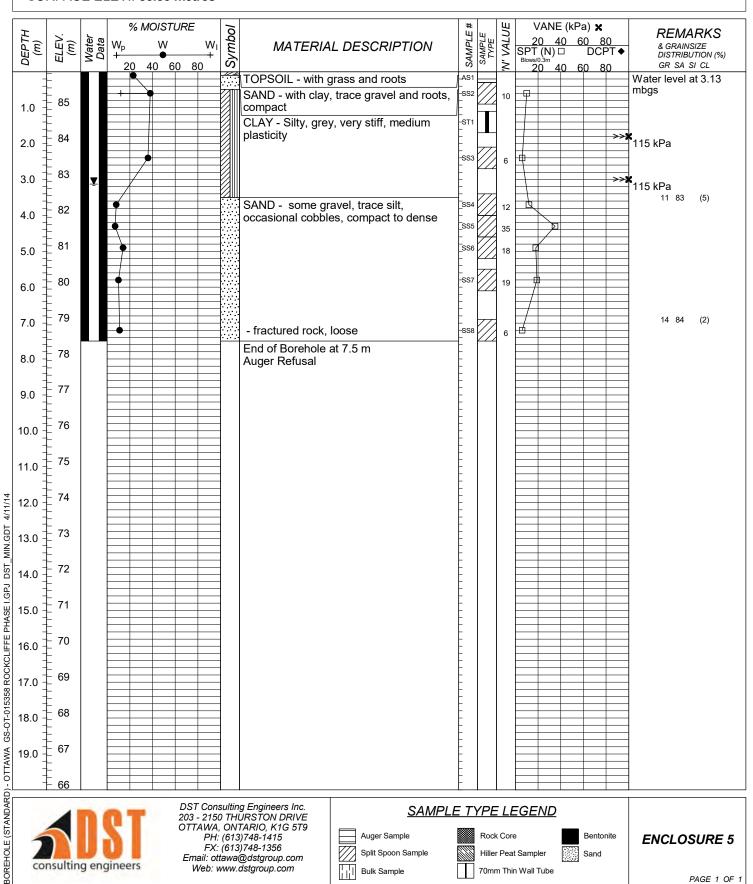
ENCLOSURE 11

DST REF. No.: **OE-OT-015358 CLIENT: Canada Lands Company** PROJECT: Former CFB Rockcliffe LOCATION: Ottawa, Ontario SURFACE ELEV.: 85.85 metres

Drilling Data

METHOD: Hollow Stem Auger DIAMETER: 80 mm ID DATE: February 24, 2014

COORDINATES: 5033327.89 m N, 450239.28 m E



203 - 2150 THURSTON DRIVE OTTAWA, ONTARIO, K1G 5T9 PH: (613)748-1415 FX: (613)748-1356 Email: ottawa@dstgroup.com

Web: www.dstgroup.com

Auger Sample Split Spoon Sample

Bulk Sample

Rock Core Hiller Peat Sampler

70mm Thin Wall Tube

Bentonite Sand

ENCLOSURE 5

LOG OF TESTPIT TP13-03

DST REF. No.: **OE-OT-017184**

CLIENT: Canada Lands Company (CLC) PROJECT: Stormwater Management Plan

LOCATION: Former CFB Rockcliffe, Ottawa, Ontario

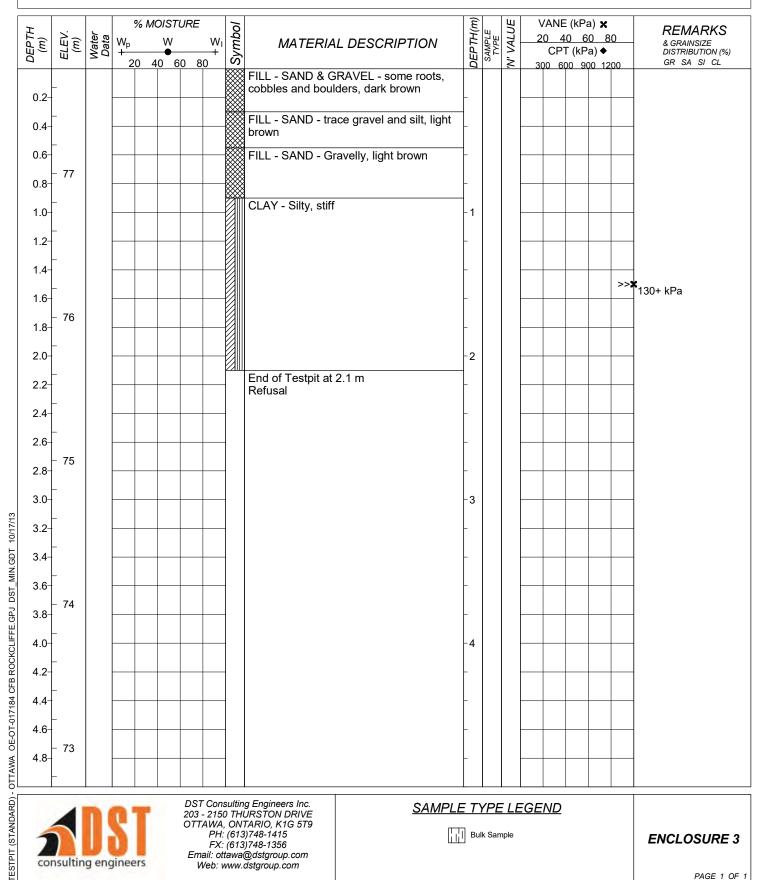
SURFACE ELEV.: 77.73 metres

Testpit Data

METHOD: Excavator

DATE: 9/6/2013

COORDINATES: 5033845.5 m N, 450226 m E





DST Consulting Engineers Inc. 203 - 2150 THURSTON DRIVE OTTAWA, ONTARIO, K1G 5T9 PH: (613)748-1415 FX: (613)748-1356 Email: ottawa@dstgroup.com Web: www.dstgroup.com

SAMPLE TYPE LEGEND



ENCLOSURE 3

LOG OF TESTPIT TP13-04

DST REF. No.: **OE-OT-017184**

CLIENT: Canada Lands Company (CLC) PROJECT: Stormwater Management Plan

LOCATION: Former CFB Rockcliffe, Ottawa, Ontario

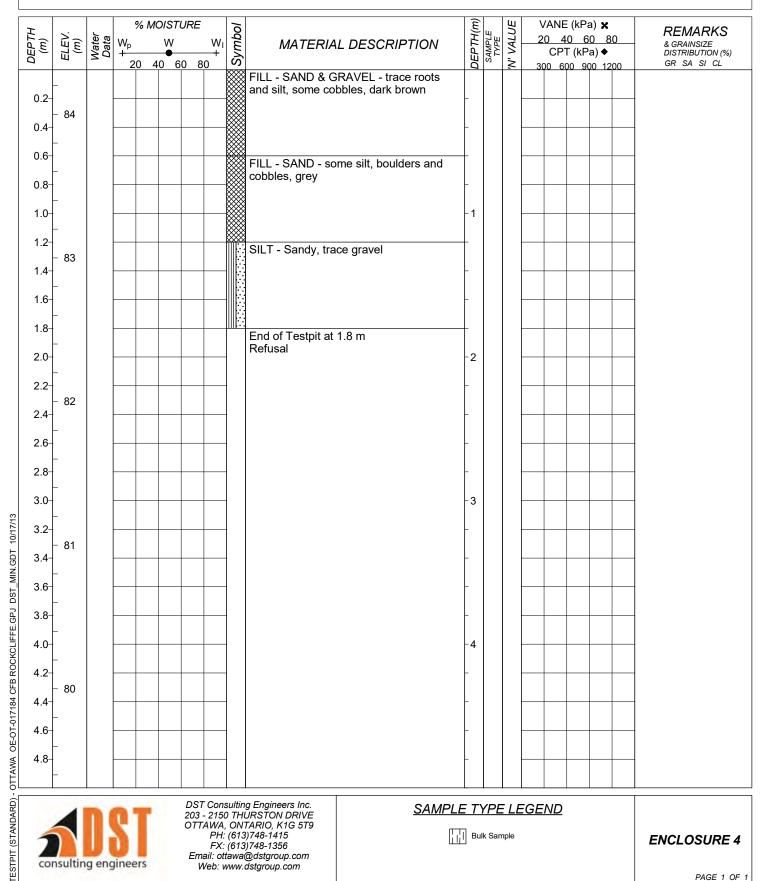
SURFACE ELEV.: 84.31 metres

Testpit Data

METHOD: Excavator

DATE: 9/6/2013

COORDINATES: 5033718.5 m N, 450202.2 m E





DST Consulting Engineers Inc. 203 - 2150 THURSTON DRIVE OTTAWA, ONTARIO, K1G 5T9 PH: (613)748-1415 FX: (613)748-1356 Email: ottawa@dstgroup.com

Web: www.dstgroup.com

SAMPLE TYPE LEGEND



ENCLOSURE 4

DST REF. No.: **OG06562**

CLIENT: Canada Lands Company

PROJECT: Preliminary Geotechnical Investigation LOCATION: CFB Rockcliffe, Ottawa, Ontario

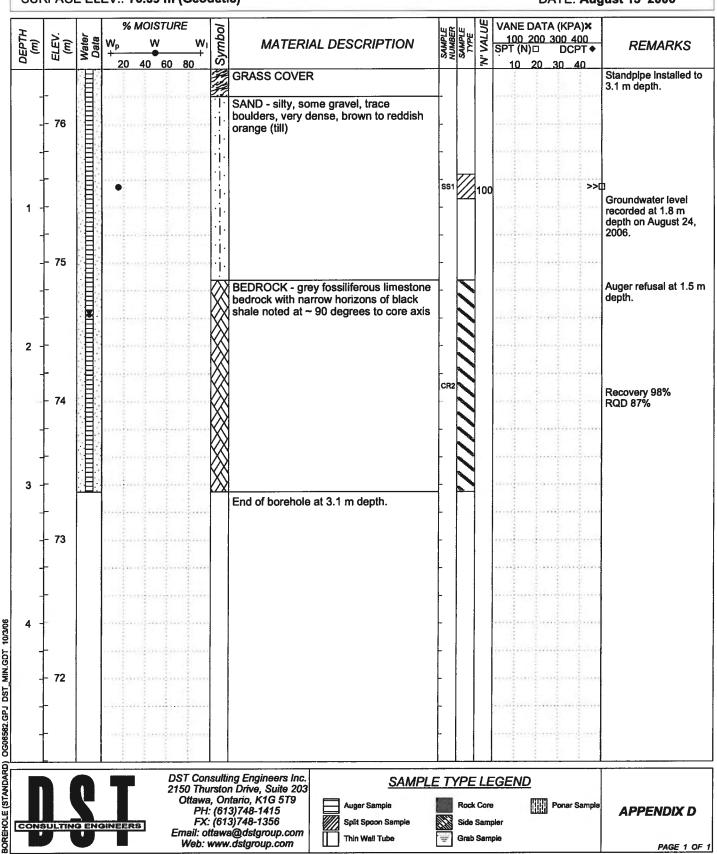
DIAMETER: 200 mm

METHOD: CME 75 Drili Rig

Drilling Data

SURFACE ELEV.: 76.39 m (Geodetic)

DATE: August 15 2006



DST REF. No.: **OG06562**

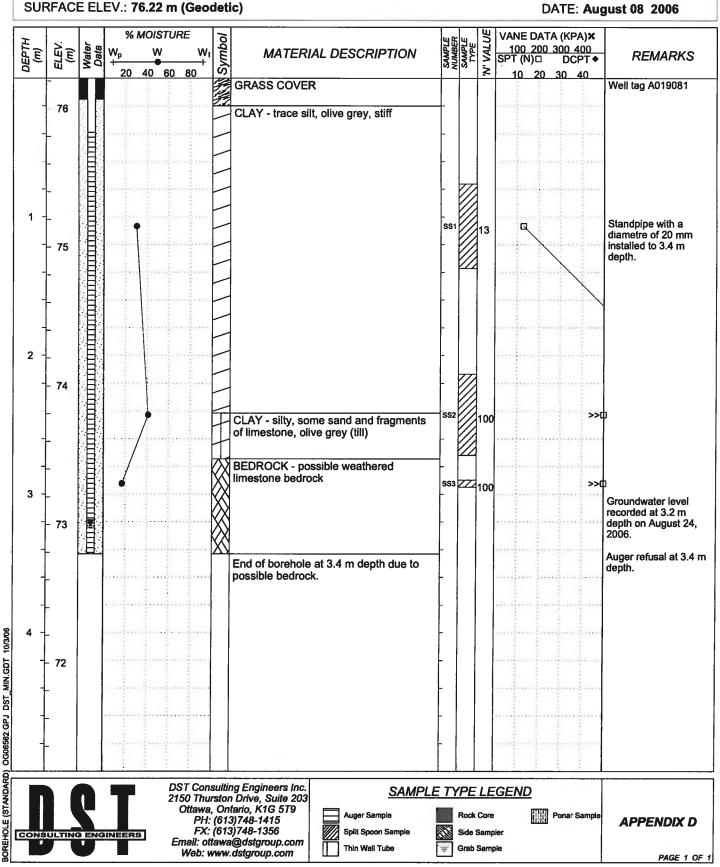
CLIENT: Canada Lands Company

PROJECT: Preliminary Geotechnical Investigation LOCATION: CFB Rockcliffe, Ottawa, Ontario

Drilling Data

METHOD: CME 75 Drill Rig DIAMETER: 200 mm

DATE: August 08 2006



DST REF. No.: **OG06562**

CLIENT: Canada Lands Company

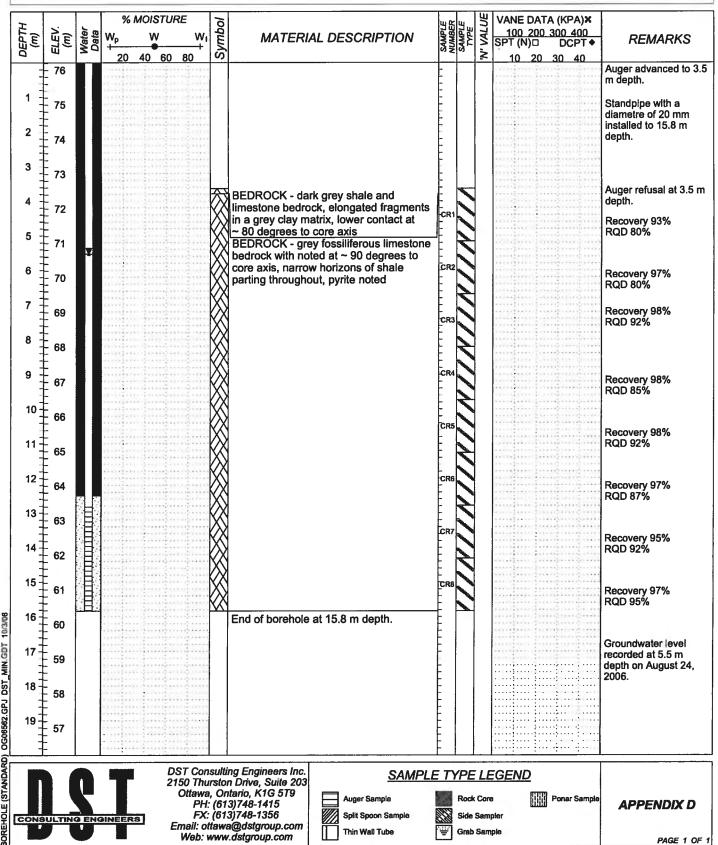
PROJECT: Preliminary Geotechnical Investigation LOCATION: CFB Rockcliffe, Ottawa, Ontario SURFACE ELEV.: 76.22 m (Geodetic)

Drilling Data

METHOD: CME 75 Drill Rig

DIAMETER: 200 mm

DATE: August 09 2006



DST REF. No.: 0E04940

CLIENT: Canada Lands Company

PROJECT: Steam Line Decommissioning

LOCATION: Canadian Forces Base, Rockcliffe, Ottawa, Ontario

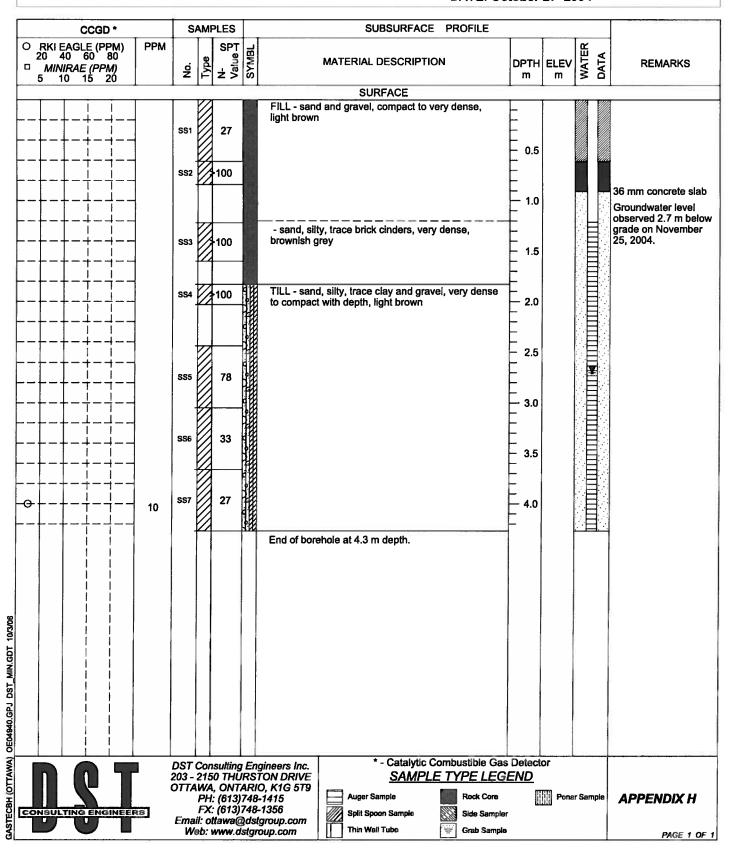
SURFACE ELEV .: --/--

Drilling Data

METHOD: CME 45 Trailer Mounted Drill Rig

DIAMETER: 200 mm

DATE: October 27 2004



DST REF. No.: **OE04940**

CLIENT: Canada Lands Company

PROJECT: Steam Line Decommissioning

LOCATION: Canadian Forces Base, Rockcliffe, Ottawa, Ontario

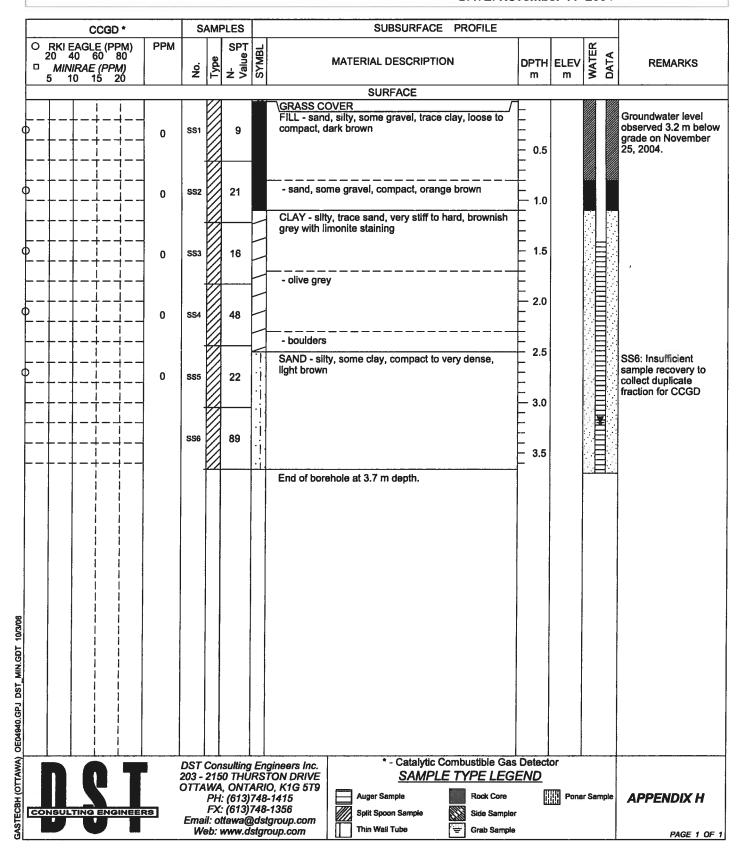
SURFACE ELEV .: --/--

Drilling Data

METHOD: CME 55 Track Mounted Drill Rig

DIAMETER: 200 mm

DATE: November 11 2004



DST REF. No.: 0E04940

CLIENT: Canada Lands Company

PROJECT: Steam Line Decommissioning

LOCATION: Canadian Forces Base, Rockcliffe, Ottawa, Ontario

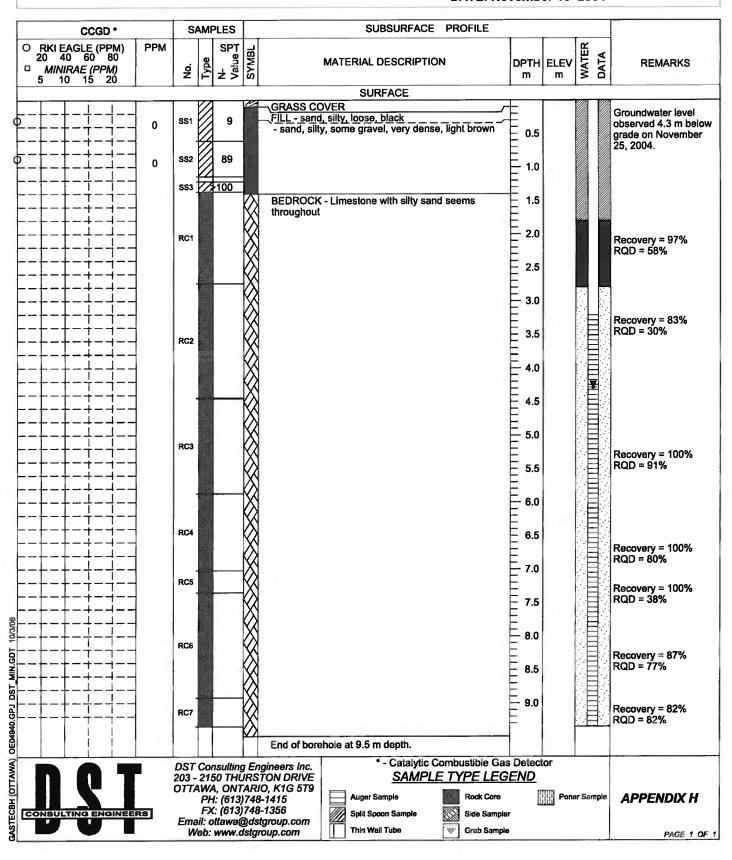
SURFACE ELEV .: --/--

Drilling Data

METHOD: CME 55 Track Mounted Drill Rig

DIAMETER: 200 mm

DATE: November 15 2004



DST REF. No.: **OE04940**

CLIENT: Canada Lands Company

PROJECT: Steam Line Decommissioning

LOCATION: Canadian Forces Base, Rockcliffe, Ottawa, Ontario

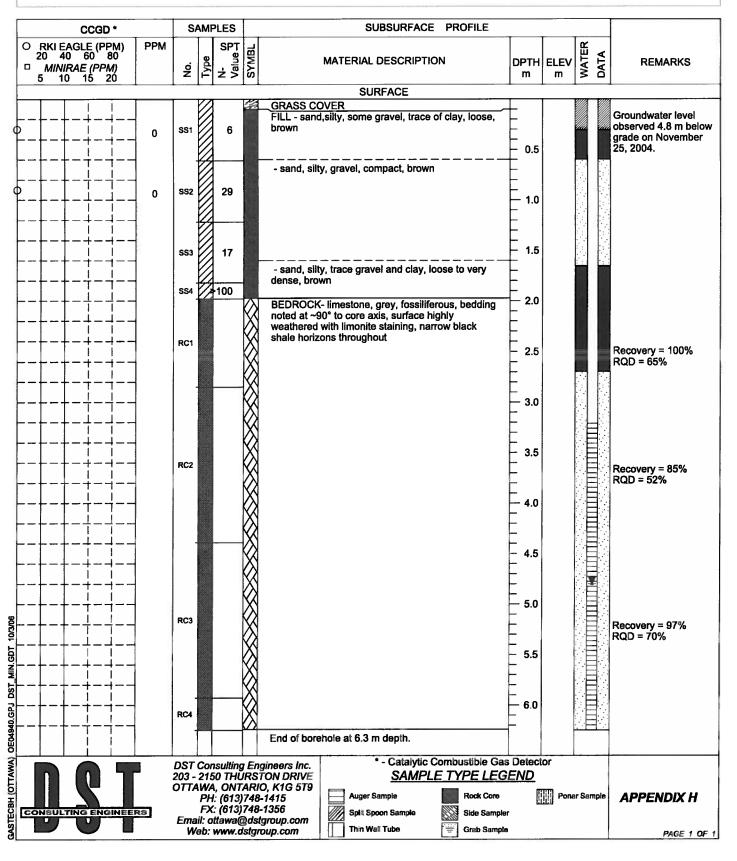
SURFACE ELEV .: --/--

Drilling Data

METHOD: CME 55 Track Mounted Drill Rig

DIAMETER: 200 mm

DATE: November 15 2004



DST REF. No.: **OE04940**

CLIENT: Canada Lands Company

PROJECT: Steam Line Decommissioning

LOCATION: Canadian Forces Base, Rockciiffe, Ottawa, Ontario

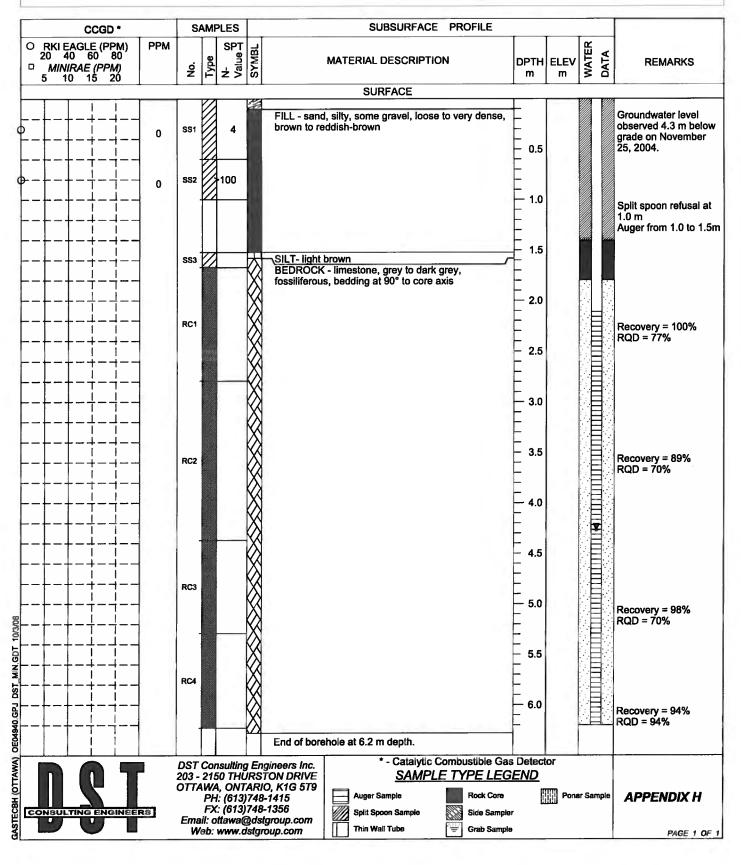
SURFACE ELEV .: --/--

Drilling Data

METHOD: CME 55 Track Mounted Drill Rig

DIAMETER: 200 mm

DATE: November 16 2004



DST REF. No.: **OE04940**

CLIENT: Canada Lands Company

PROJECT: Steam Line Decommissioning

LOCATION: Canadian Forces Base, Rockcliffe, Ottawa, Ontario

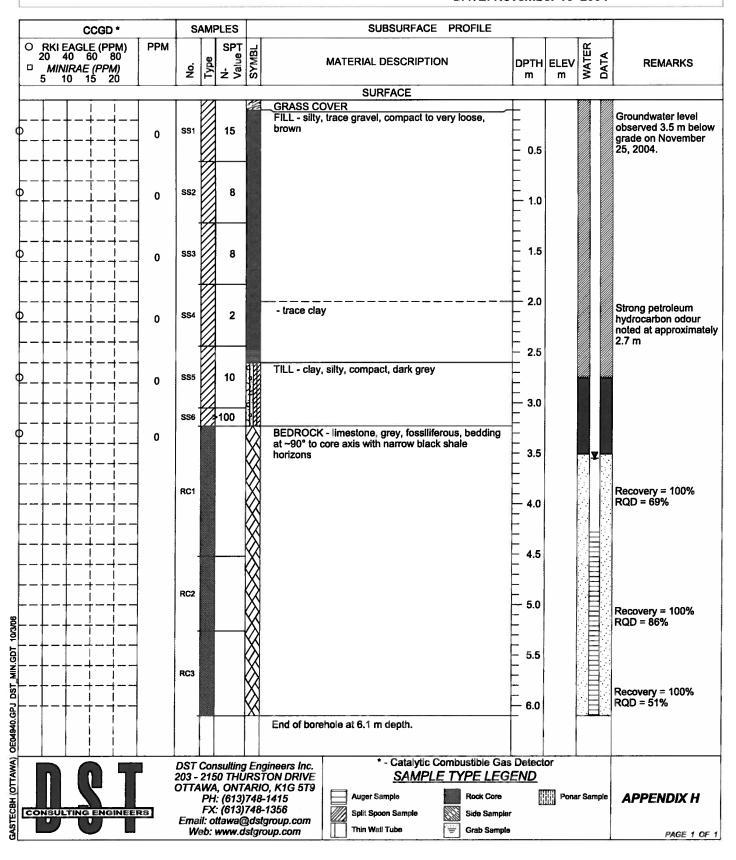
SURFACE ELEV .: --/--

Drilling Data

METHOD: CME 55 Track Mounted Drill Rig

DIAMETER: 200 mm

DATE: November 16 2004



DST REF. No.: **OE04940**

CLIENT: Canada Lands Company

PROJECT: Steam Line Decommissioning

LOCATION: Canadian Forces Base, Rockcliffe, Ottawa, Ontario

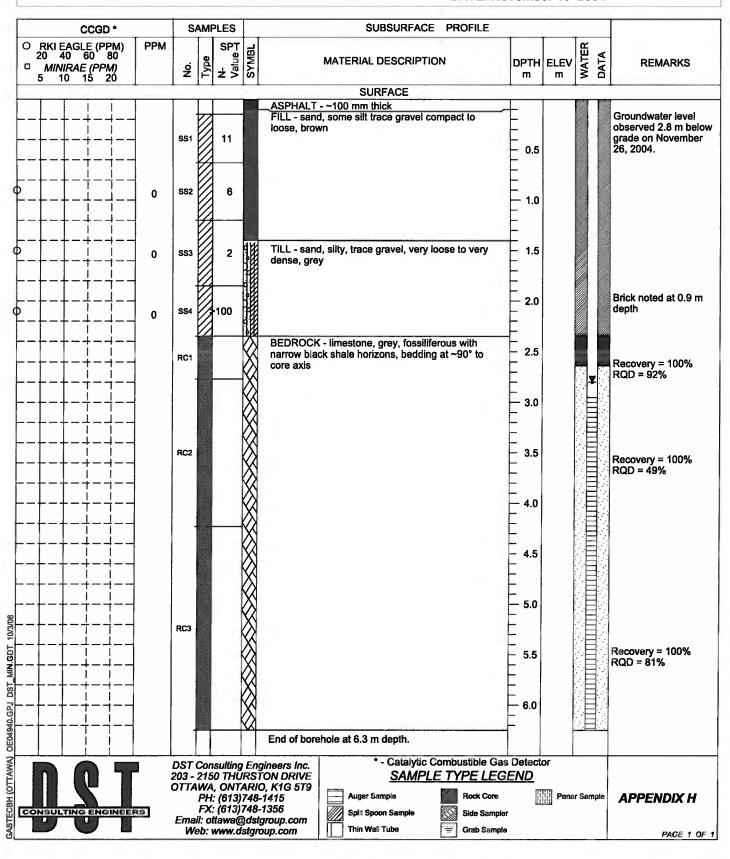
SURFACE ELEV .: --/--

Drilling Data

METHOD: CME 55 Track Mounted Drill Rig

DIAMETER: 200 mm

DATE: November 18 2004



DST REF. No.: **OE04940**

CLIENT: Canada Lands Company

PROJECT: Steam Line Decommissioning

LOCATION: Canadian Forces Base, Rockcliffe, Ottawa, Ontario

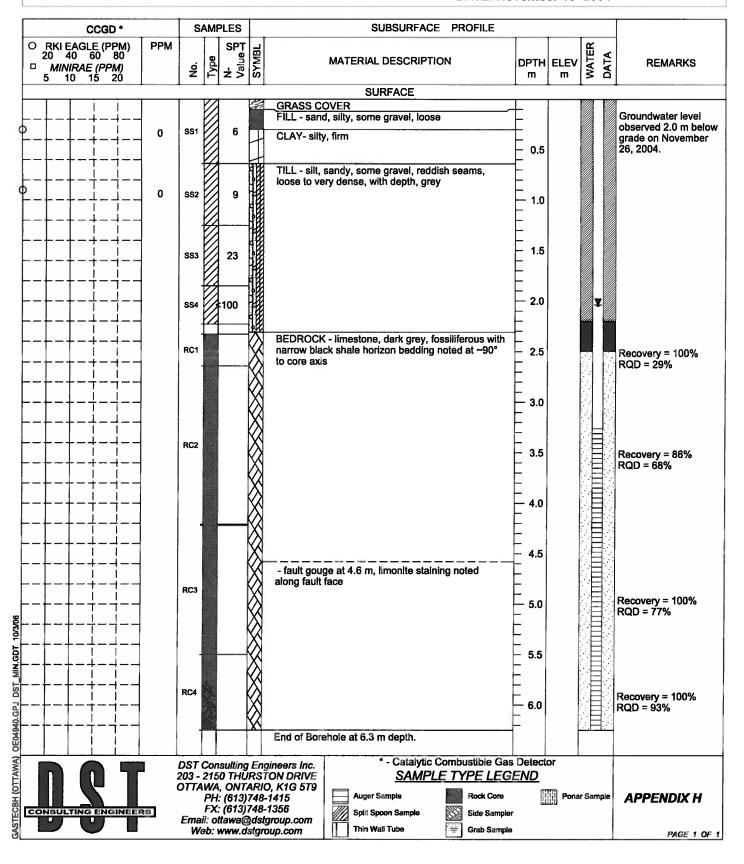
SURFACE ELEV .: --/--

Drilling Data

METHOD: CME 55 Track Mounted Drill Rig

DIAMETER: 200 mm

DATE: November 18 2004



DST REF. No.: **OE04940**

CLIENT: Canada Lands Company

PROJECT: Steam Line Decommissioning

LOCATION: Canadian Forces Base, Rockcliffe, Ottawa, Ontario

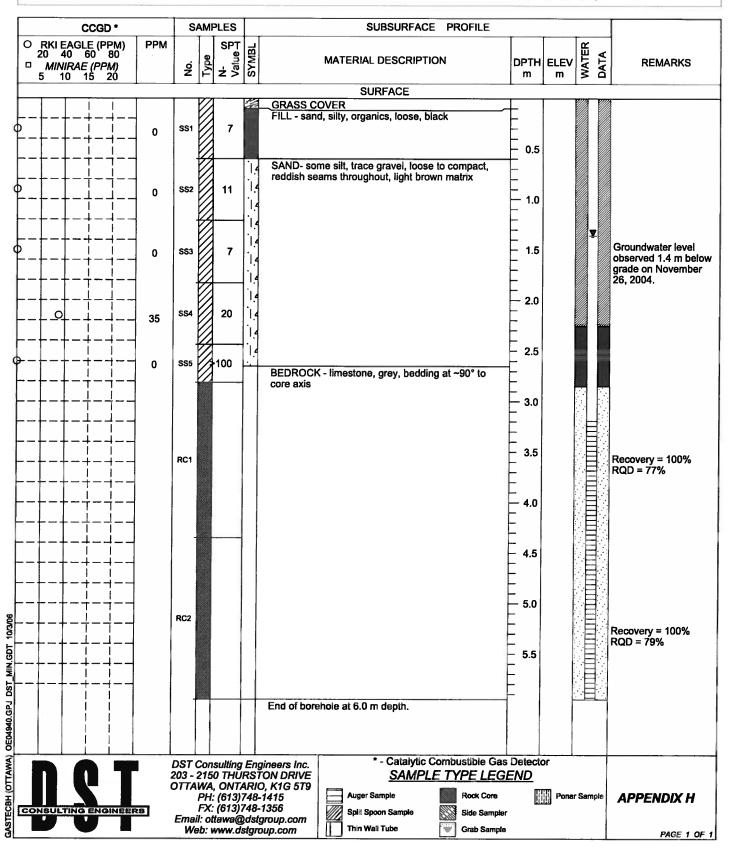
SURFACE ELEV.: --/--

Drilling Data

METHOD: CME 55 Track Mounted Drill Rig

DIAMETER: 200 mm

DATE: November 22 2004



DST REF. No.: **OE04940**

CLIENT: Canada Lands Company

PROJECT: Steam Line Decommissioning

LOCATION: Canadian Forces Base, Rockcliffe, Ottawa, Ontario

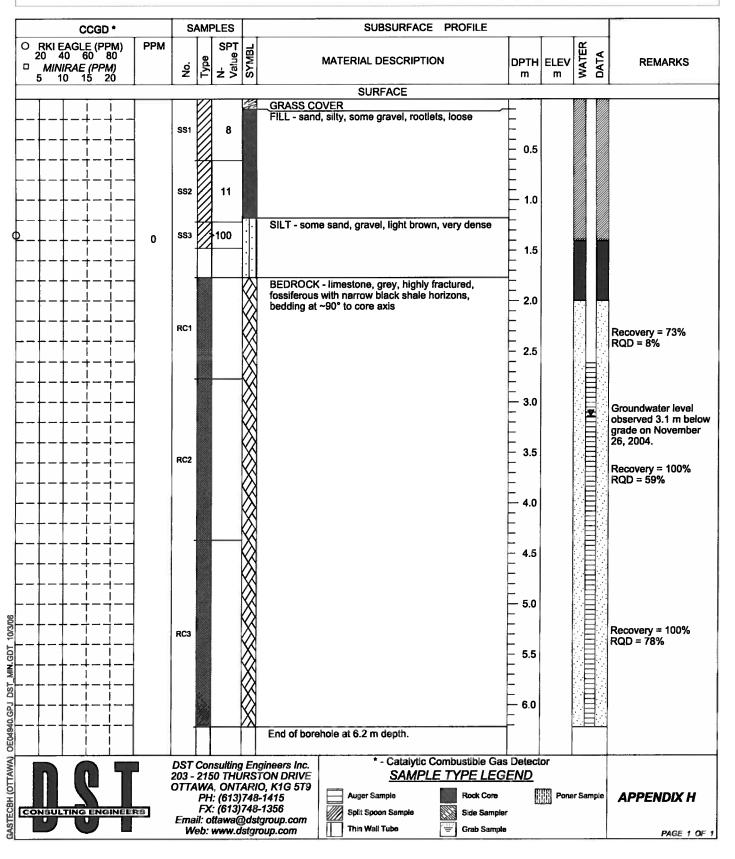
SURFACE ELEV .: --/--

Drilling Data

METHOD: CME 55 Track Mounted Drill Rig

DIAMETER: 200 mm

DATE: November 23 2004



DST REF. No.: **OE04940**

CLIENT: Canada Lands Company

PROJECT: Steam Line Decommissioning

LOCATION: Canadian Forces Base, Rockcliffe, Ottawa, Ontario

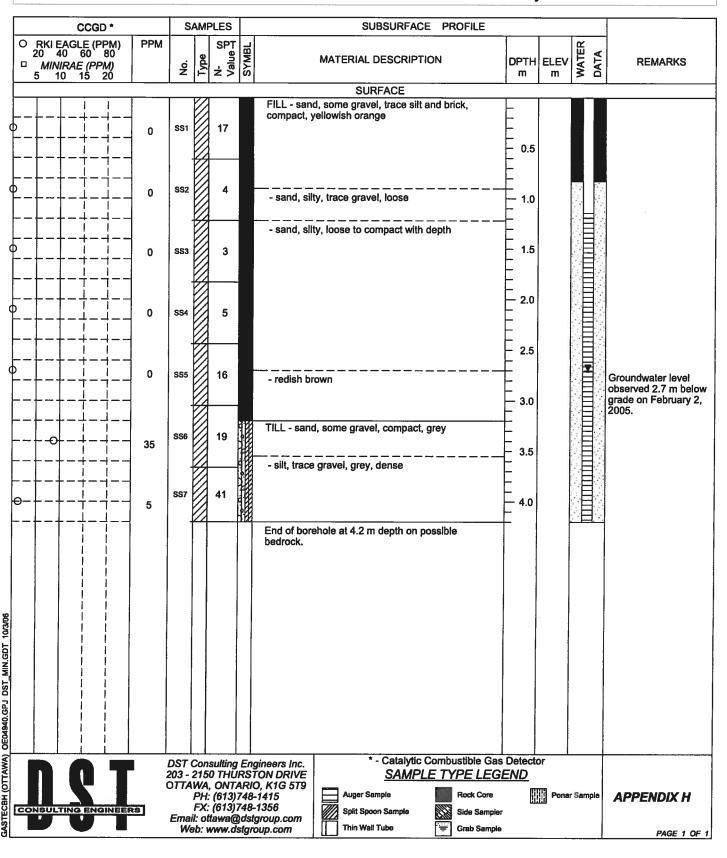
SURFACE ELEV .: --/--

Drilling Data

METHOD: CME 45c Track Mounted Drill Rig

DIAMETER: 200 mm

DATE: February 01 2005



DST REF. No.: **OE04940**

CLIENT: Canada Lands Company

PROJECT: Steam Line Decommissioning

LOCATION: Canadian Forces Base, Rockcliffe, Ottawa, Ontario

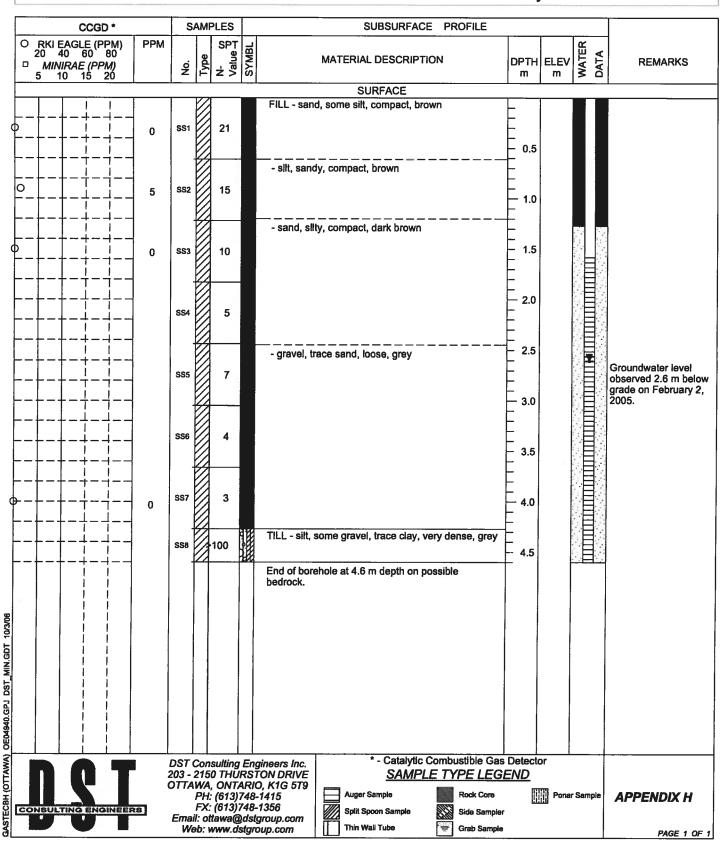
SURFACE ELEV .: --/--

Drilling Data

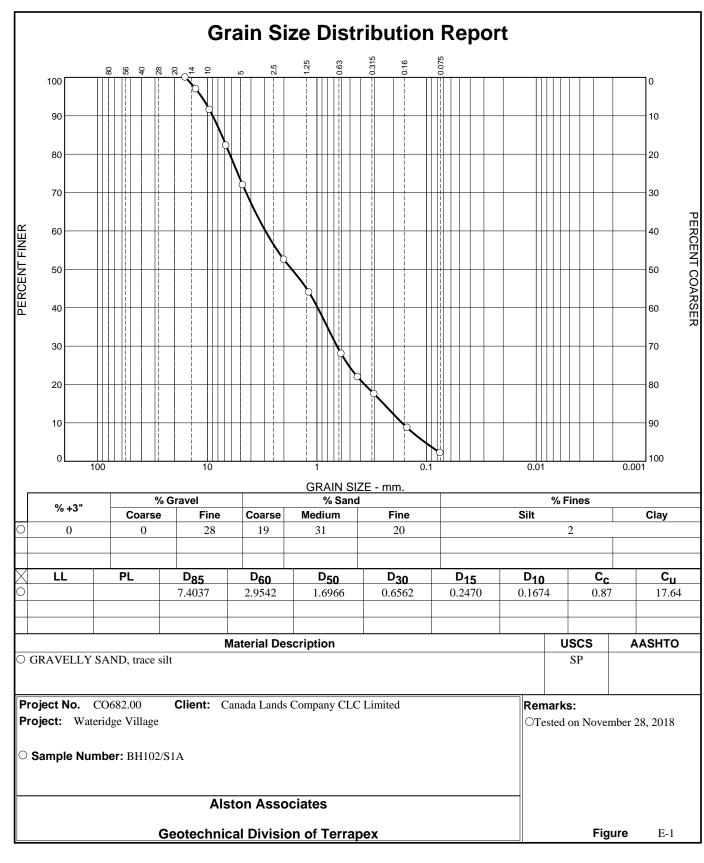
METHOD: CME 45c Track Mounted Drill Rig

DIAMETER: 200 mm

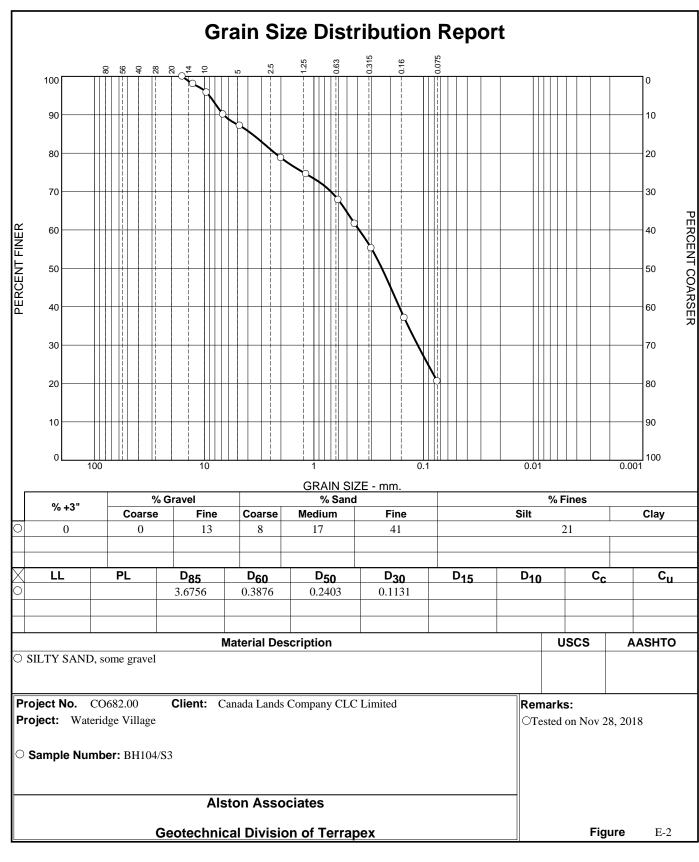
DATE: February 01 2005

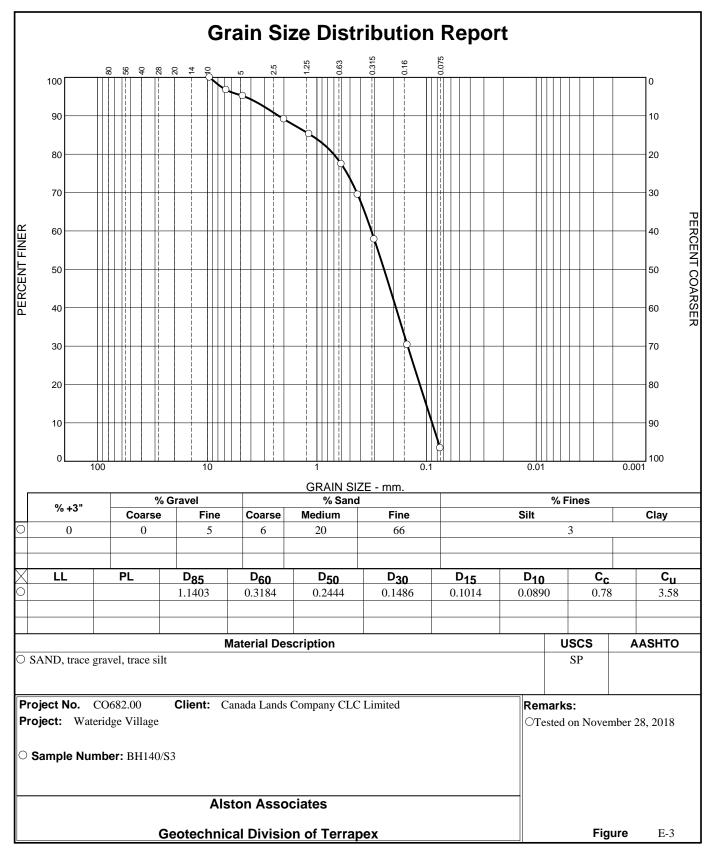


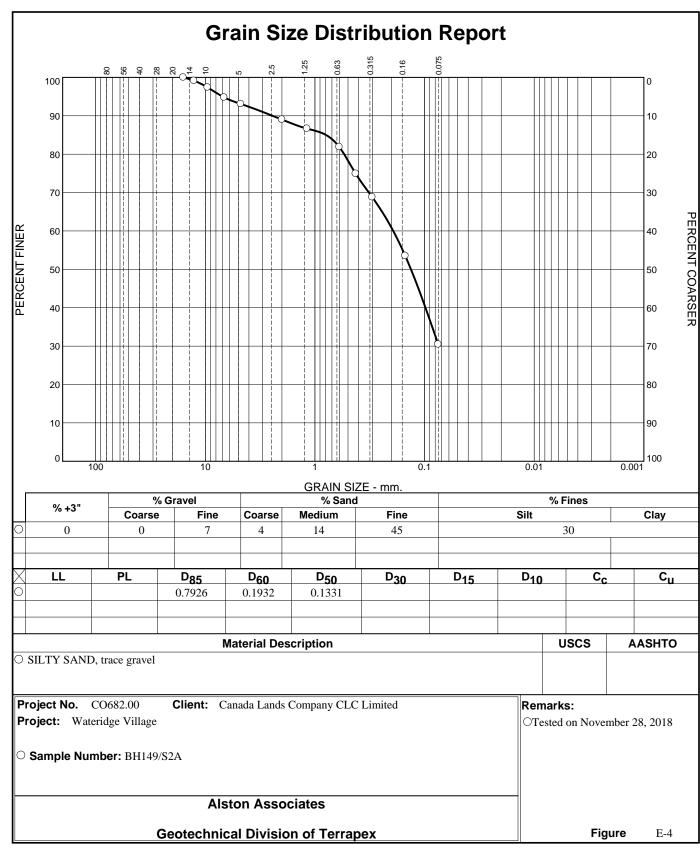
APPENDIX E LABORATORY TEST RESULTS

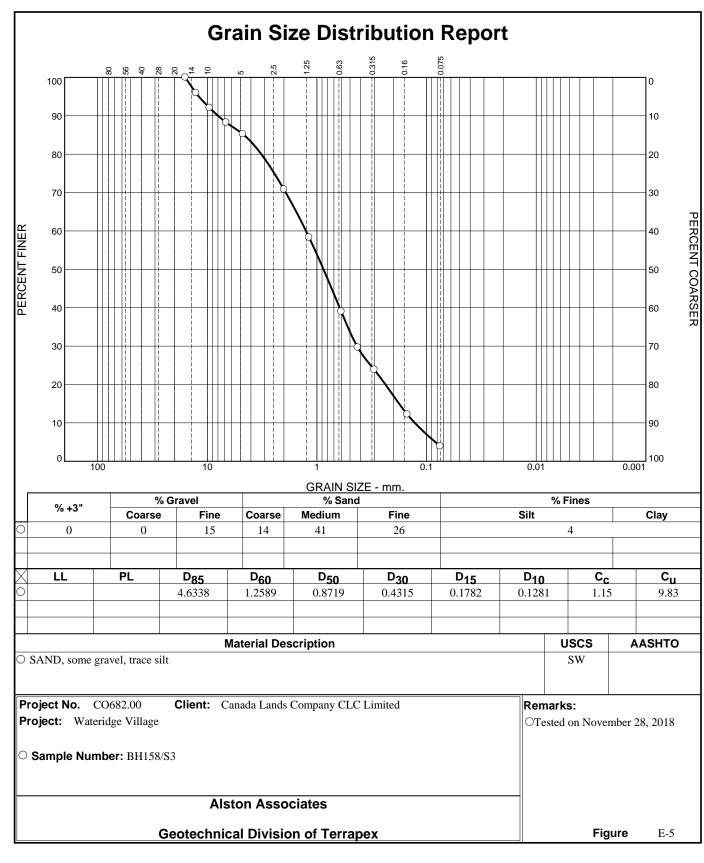


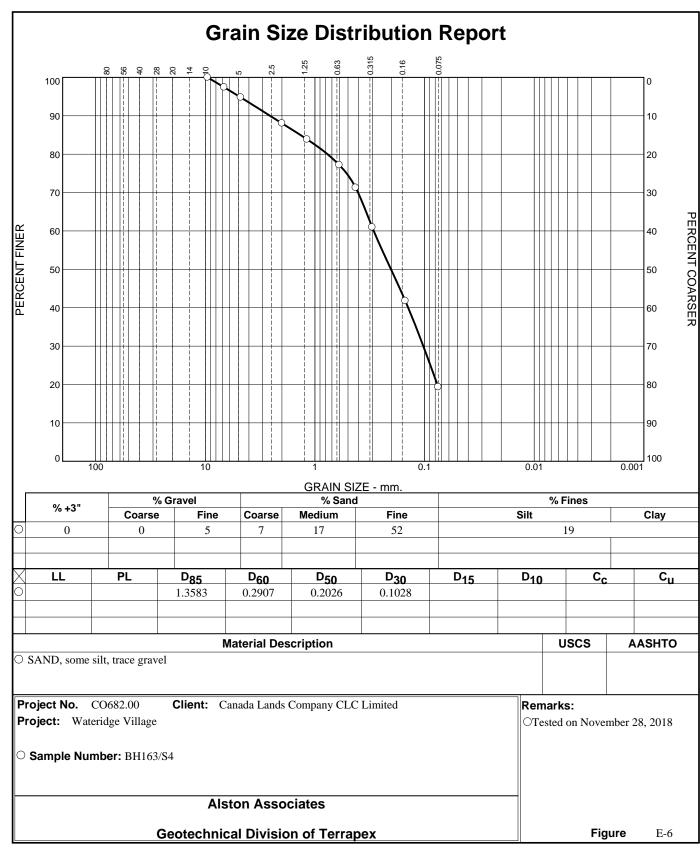
Tested By: RH

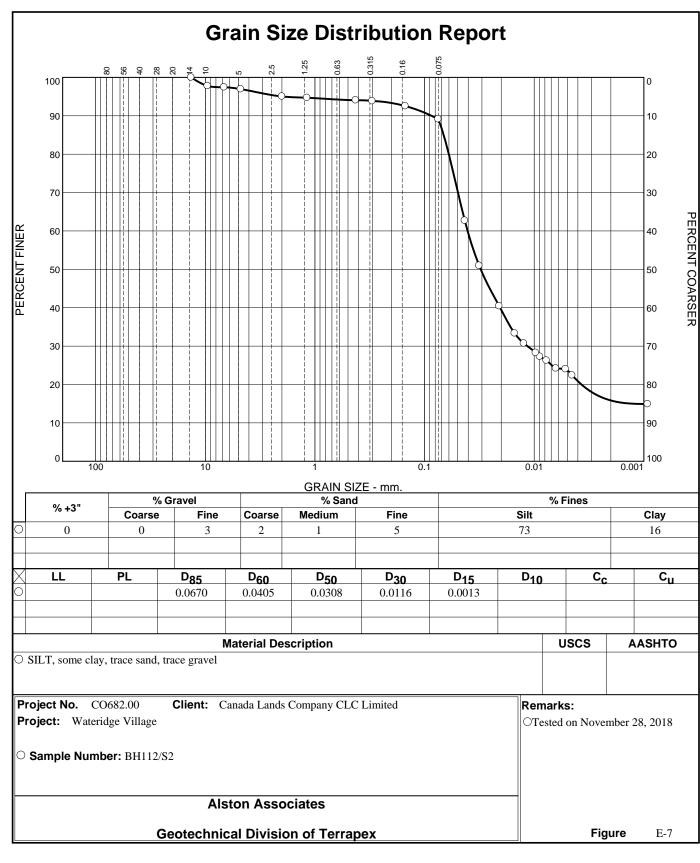


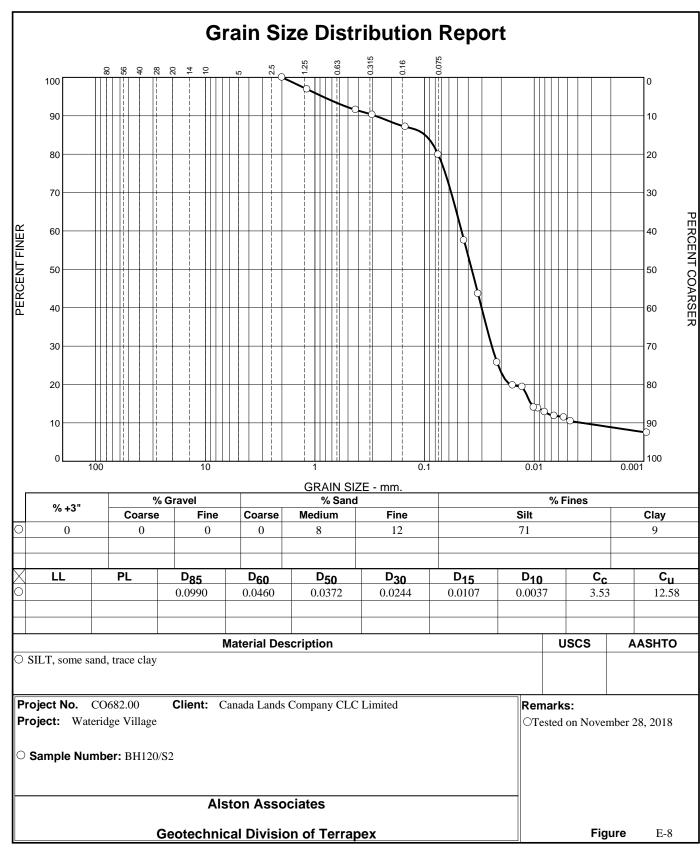


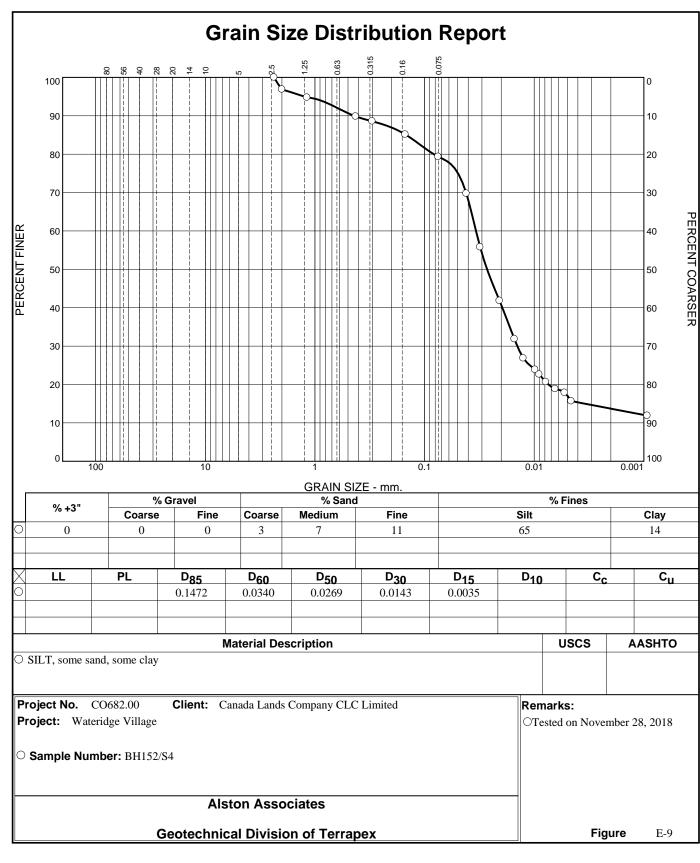


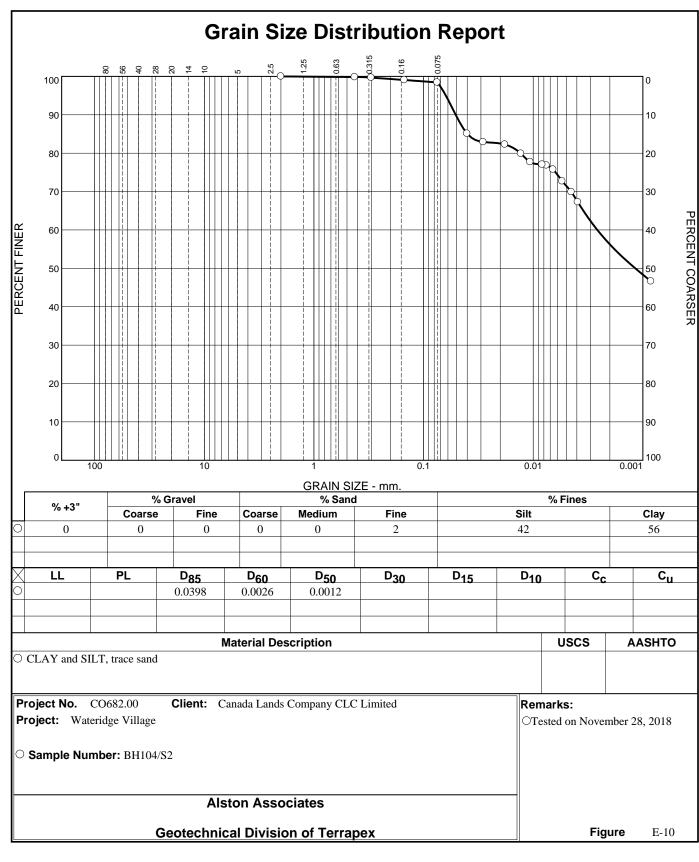


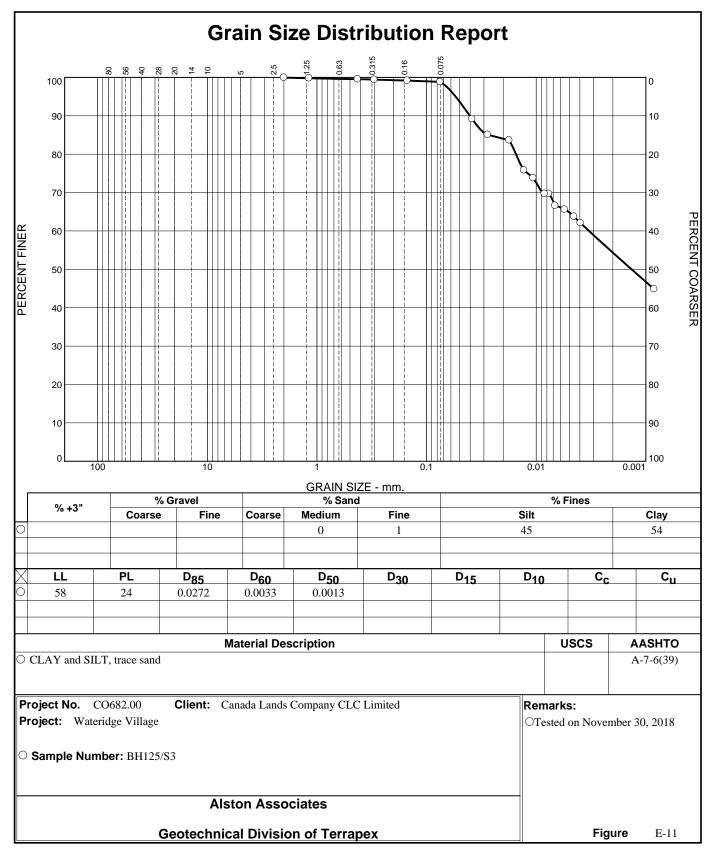


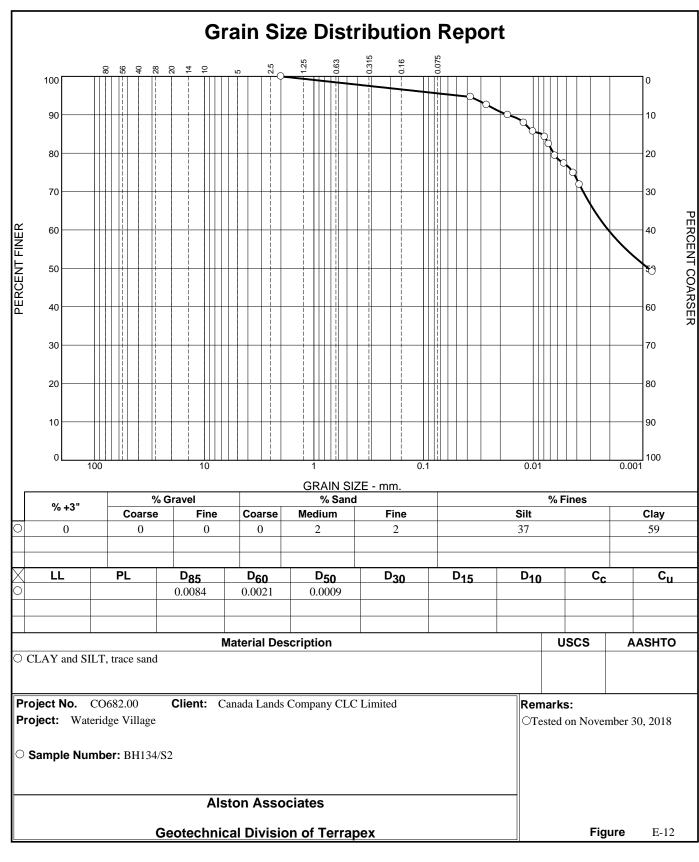


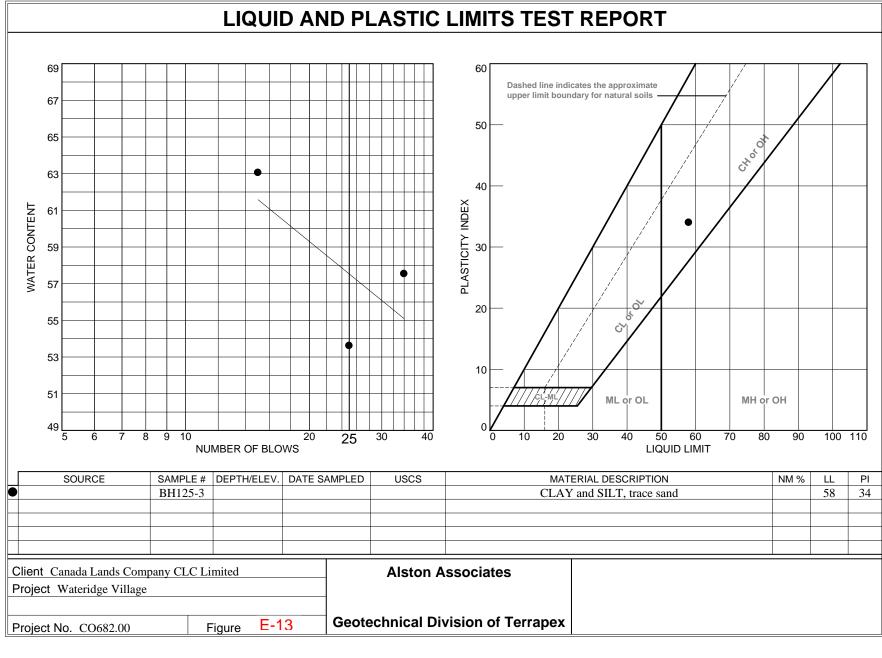


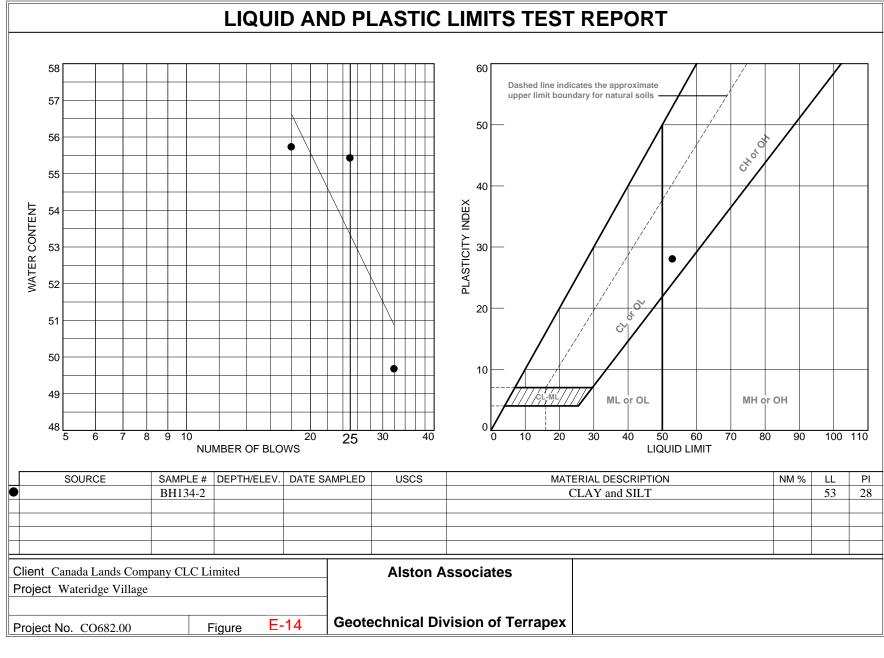






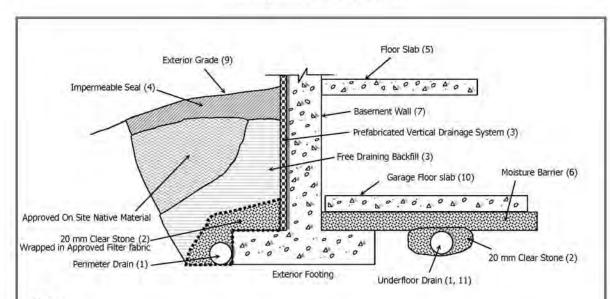






APPENDIX F TYPICAL DRAINAGE SYSTEM

Drainage and Backfill Details



Notes

- Perimeter and underfloor drains shall consist of 100 mm diameter weeping tile with fabric sock or equivalent
 perforated pipe leading to a positive sump or outlet. Invert to be a minimum of 300 mm below underside of
 garage floor slab. Perimeter drain is required for sections of garage wall installed below exterior grade.
- 20 mm Clear Stone 150 mm top and side of drain, surrounded by approved filter fabric (Terrafix 270R or equivalent).
- Free Draining backfill OPSS Granular B or equivalent compacted to the specified density. Do not use heavy compaction equipment within 450 mm of the wall. Use hand controlled light compaction equipment within 1.8 m of wall. Free draining backfill is not required if a prefabricated vertical drainage system (such as Miradrain 6000) is installed on the exterior of the basement wall.
- Impermeable backfill seal (min, 600 mm) relatively impervious compacted silty clay, clayey silt or equivalent. If on-site native backfill is impermeable, seal may be omitted.
- 5. Do not backfill until wall is supported by garage and floor slabs or adequate bracing.
- 6. Moisture barrier to be at least 200 mm of compacted 20 mm clear stone or equivalent free draining material.
- 7. Basement wall to be damp-proofed.
- 9. Exterior grade to slope away from building at minimum gradient of 2%.
- 10. Garage floor slab should not be structurally connected to the wall or footing.
- 11. Underfloor drain invert to be at least 300 mm below underside of floor slab. Drainage tile placed in parallel rows at 10 m centre to centre. Place drain on 100 mm of 20 mm clear stone with 150 mm of clear stone on top and sides. Do not connect the underfloor drains to perimeter drains.

DRAINAGE AND BACKFILL RECOMMENDATIONS

(Not to Scale)



APPENDIX G CERTIFICATE OF CHEMICAL ANALYSES



Your Project #: CO682.00

Site Location: WATERIDGE VILLAGE

Your C.O.C. #: 117522

Attention: Rachel Herzog
Terrapex Environmental Ltd
1-20 Gurdwara Rd.
Ottawa, ON
CANADA K2E 8B3

Report Date: 2018/12/20

Report #: R5534330 Version: 1 - Final

CERTIFICATE OF ANALYSIS

MAXXAM JOB #: B8X8071 Received: 2018/12/18, 11:30

Sample Matrix: Soil # Samples Received: 4

		Date	Date		
Analyses	Quantity	Extracted	Analyzed	Laboratory Method	Reference
Anions (1)	4	2018/12/20	2018/12/20	CAM SOP-00435	SM 23 4110 B m
Moisture (1)	4	N/A	2018/12/19	CAM SOP-00445	Carter 2nd ed 51.2 m
pH CaCl2 EXTRACT (1)	4	2018/12/20	2018/12/20	CAM SOP-00413	EPA 9045 D m

Remarks:

Maxxam Analytics' laboratories are accredited to ISO/IEC 17025:2005 for specific parameters on scopes of accreditation. Unless otherwise noted, procedures used by Maxxam are based upon recognized Provincial, Federal or US method compendia such as CCME, MDDELCC, EPA, APHA.

All work recorded herein has been done in accordance with procedures and practices ordinarily exercised by professionals in Maxxam's profession using accepted testing methodologies, quality assurance and quality control procedures (except where otherwise agreed by the client and Maxxam in writing). All data is in statistical control and has met quality control and method performance criteria unless otherwise noted. All method blanks are reported; unless indicated otherwise, associated sample data are not blank corrected. Where applicable, unless otherwise noted, Measurement Uncertainty has not been accounted for when stating conformity to the referenced standard.

Maxxam Analytics' liability is limited to the actual cost of the requested analyses, unless otherwise agreed in writing. There is no other warranty expressed or implied. Maxxam has been retained to provide analysis of samples provided by the Client using the testing methodology referenced in this report. Interpretation and use of test results are the sole responsibility of the Client and are not within the scope of services provided by Maxxam, unless otherwise agreed in writing. Maxxam is not responsible for the accuracy or any data impacts, that result from the information provided by the customer or their agent.

Solid sample results, except biota, are based on dry weight unless otherwise indicated. Organic analyses are not recovery corrected except for isotope dilution methods.

Results relate to samples tested. When sampling is not conducted by Maxxam, results relate to the supplied samples tested.

This Certificate shall not be reproduced except in full, without the written approval of the laboratory.

 $Reference\ Method\ suffix\ "m"\ indicates\ test\ methods\ incorporate\ validated\ modifications\ from\ specific\ reference\ methods\ to\ improve\ performance.$

- * RPDs calculated using raw data. The rounding of final results may result in the apparent difference.
- (1) This test was performed by Maxxam Analytics Mississauga

Encryption Key

Please direct all questions regarding this Certificate of Analysis to your Project Manager. Alisha Williamson, Project Manager Email: AWilliamson@maxxam.ca Phone# (613) 274-0573



Your Project #: CO682.00

Site Location: WATERIDGE VILLAGE

Your C.O.C. #: 117522

Attention: Rachel Herzog
Terrapex Environmental Ltd
1-20 Gurdwara Rd.

Ottawa, ON CANADA K2E 8B3

Report Date: 2018/12/20

Report #: R5534330 Version: 1 - Final

CERTIFICATE OF ANALYSIS

MAXXAM JOB #: B8X8071 Received: 2018/12/18, 11:30

Maxxam has procedures in place to guard against improper use of the electronic signature and have the required "signatories", as per section 5.10.2 of ISO/IEC 17025:2005(E), signing the reports. For Service Group specific validation please refer to the Validation Signature Page.



Terrapex Environmental Ltd Client Project #: CO682.00

Site Location: WATERIDGE VILLAGE

Sampler Initials: RH

RESULTS OF ANALYSES OF SOIL

	2018/12/11	2018/12/11							1
l l		2010,12,11	2018/12/11	2018/12/11			2018/12/11		
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	117522	117522	117522	117522			117522		
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рН	7.58	7.54	7.66	7.77		5898613			
ug/g	ND	ND	ND	ND	10	5898620	ND	10	5898620
ug/g	98	26	ND	ND	20	5898620	24	20	5898620
	% pH ug/g	117522 UNITS BH108-2 % 20 pH 7.58 ug/g ND	117522 117522 UNITS BH108-2 BH127-2	117522 117522 117522 UNITS BH108-2 BH127-2 BH153-3	117522 117522 117522 117522 117522	117522 117522 117522 117522	117522 117522 117522 117522	117522 1	117522 117522 117522 117522 117522 117522

RDL = Reportable Detection Limit

QC Batch = Quality Control Batch

Lab-Dup = Laboratory Initiated Duplicate

ND = Not detected



Terrapex Environmental Ltd Client Project #: CO682.00

Site Location: WATERIDGE VILLAGE

Sampler Initials: RH

TEST SUMMARY

Maxxam ID: IOS514 Sample ID: BH108-2 Matrix: Soil

2018/12/11 Collected:

Shipped:

Received: 2018/12/18

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Anions	IC	5898620	2018/12/20	2018/12/20	Fari Dehdezi
Moisture	BAL	5896681	N/A	2018/12/19	Prgya Panchal
pH CaCl2 EXTRACT	AT	5898613	2018/12/20	2018/12/20	Gnana Thomas

Maxxam ID: IOS515 Sample ID: BH127-2 Matrix: Soil

Collected: 2018/12/11

Shipped:

Received: 2018/12/18

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Anions	IC	5898620	2018/12/20	2018/12/20	Fari Dehdezi
Moisture	BAL	5896681	N/A	2018/12/19	Prgya Panchal
pH CaCl2 EXTRACT	AT	5898613	2018/12/20	2018/12/20	Gnana Thomas

Maxxam ID: IOS516 Sample ID: BH153-3 Matrix: Soil

Collected: 2018/12/11

Shipped:

Received: 2018/12/18

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Anions	IC	5898620	2018/12/20	2018/12/20	Fari Dehdezi
Moisture	BAL	5896681	N/A	2018/12/19	Prgya Panchal
nH CaCl2 EXTRACT	ΛТ	5808613	2018/12/20	2018/12/20	Gnana Thomas

Maxxam ID: IOS517 Sample ID: BH156-2 Matrix: Soil

Matrix: Soil

Collected:

Shipped:

Received: 2018/12/18

2018/12/11

Test Description Instrumentation **Extracted Date Analyzed** Batch Analyst Anions IC 5898620 2018/12/20 2018/12/20 Fari Dehdezi Prgya Panchal Moisture BAL 5896681 N/A 2018/12/19 pH CaCl2 EXTRACT ΑТ 5898613 2018/12/20 2018/12/20 **Gnana Thomas**

Maxxam ID: IOS517 Dup Sample ID: BH156-2

Collected: 2018/12/11

Shipped:

Received: 2018/12/18

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Anions	IC	5898620	2018/12/20	2018/12/20	Fari Dehdezi



Terrapex Environmental Ltd Client Project #: CO682.00

Site Location: WATERIDGE VILLAGE

Sampler Initials: RH

GENERAL COMMENTS

Each to	emperature is the	average of up to t	hree cooler temperatures taken at receipt
	Package 1	1.0°C	
Result	s relate only to the	e items tested.	



Terrapex Environmental Ltd Client Project #: CO682.00

Site Location: WATERIDGE VILLAGE

Sampler Initials: RH

QUALITY ASSURANCE REPORT

QA/QC								
Batch	Init	QC Type	Parameter	Date Analyzed	Value	Recovery	UNITS	QC Limits
5896681	JS9	RPD	Moisture	2018/12/19	2.4		%	20
5898613	GTO	Spiked Blank	Available (CaCl2) pH	2018/12/20		100	%	97 - 103
5898613	GTO	RPD	Available (CaCl2) pH	2018/12/20	0.40		%	N/A
5898620	FD	Matrix Spike [IOS517-01]	Chloride (Cl-)	2018/12/20		NC	%	70 - 130
			Sulphate (SO4)	2018/12/20		NC	%	75 - 125
5898620	FD	Spiked Blank	Chloride (Cl-)	2018/12/20		98	%	70 - 130
			Sulphate (SO4)	2018/12/20		99	%	75 - 125
5898620	FD	Method Blank	Chloride (Cl-)	2018/12/20	ND,		ug/g	
					RDL=10			
			Sulphate (SO4)	2018/12/20	ND,		ug/g	
					RDL=20			
5898620	FD	RPD [IOS517-01]	Chloride (Cl-)	2018/12/20	NC		%	35
			Sulphate (SO4)	2018/12/20	19		%	35

N/A = Not Applicable

Duplicate: Paired analysis of a separate portion of the same sample. Used to evaluate the variance in the measurement.

Matrix Spike: A sample to which a known amount of the analyte of interest has been added. Used to evaluate sample matrix interference.

Spiked Blank: A blank matrix sample to which a known amount of the analyte, usually from a second source, has been added. Used to evaluate method accuracy.

Method Blank: A blank matrix containing all reagents used in the analytical procedure. Used to identify laboratory contamination.

NC (Matrix Spike): The recovery in the matrix spike was not calculated. The relative difference between the concentration in the parent sample and the spike amount was too small to permit a reliable recovery calculation (matrix spike concentration was less than the native sample concentration)

NC (Duplicate RPD): The duplicate RPD was not calculated. The concentration in the sample and/or duplicate was too low to permit a reliable RPD calculation (absolute difference <= 2x RDL).



Terrapex Environmental Ltd Client Project #: CO682.00

Site Location: WATERIDGE VILLAGE

Sampler Initials: RH

VALIDATION SIGNATURE PAGE

The analytical data and all QC contained in this report were reviewed and validated by the following individual(s).



Maxxam has procedures in place to guard against improper use of the electronic signature and have the required "signatories", as per section 5.10.2 of ISO/IEC 17025:2005(E), signing the reports. For Service Group specific validation please refer to the Validation Signature Page.