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## NOISE IMPACT STUDY - Project: 21443.00

## **1305 Maritime Way Proposed Commercial Hotel Development** Kanata, Ontario

Prepared for:

## **McIntosh Perry Consulting Engineers**

115 Wallgreen Road, RR#3 Carp, ON K0A 1L0

Prepared by:

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September 14, 2023

## **Revision History**

Version	Description	Author	Reviewed	Date
	Initial Report	SZ	DF	April 18, 2022
1	Revised Assessment per July 2023 Site Plan	SZ	KC	September 14, 2023

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# **Table of Contents**

1	Introduction	1
2	Guidelines and Criteria	1
3	Noise Level Predictions	3
4	Noise Predictions	7
5	Noise Control Recommendations	8
6	Conclusions	9
7	Warning Clauses	9

# **Appendix A**

Site Plan & Drawings

# **Appendix B**

Road Traffic Data & Sample Calculations

## Appendix C

Sound Power Level Data

## **Appendix D**

**Stationary Noise Sample Calculations** 



## 1 Introduction

McIntosh Perry Consulting Engineers (McIntosh Perry) has retained Aercoustics Engineering Limited to prepare a Noise Impact Study (NIS) to support a Site Plan Control application for a six-storey, 102-room hotel with associated parking at 1305 Maritime Way, Kanata, Ontario.

The study has been carried out to evaluate the impact potential of the surrounding noise environment on future receptors associated with the proposed development as well as the potential impact of noise generated by the development on existing noise sensitive receptors in the study area. This report also investigates the noise controls required for the development to abide by the noise guidelines of Ontario's Ministry of the Environment, Conservation and Parks (MECP) and to satisfy the requirements of the City of Ottawa. This report considers the MECP guideline NPC-300 "Stationary and Transportation Sources – Approval and Planning" (August 2013) and the City of Ottawa guideline "Environmental Noise Control Guidelines" ("ENCG") (September 2016).

The subject site is located on the north side of Maritime Way and approximately 115 m north of arterial roadway Kanata Avenue and 300 m northwest of Highway 417. Adjacent land uses include hotels and residences immediately north, east and south of the site on Canadian Shield Avenue and Maritime Way.

The dominant road traffic sources in the subject study area are Maritime Way, Kanata Avenue and Highway 417. The dominant stationary noise sources are mechanical rooftop equipment serving the existing neighbouring hotels and residences. Mechanical equipment proposed for the subject site has also been considered. The study area is not significantly affected by rail traffic or aircraft traffic.

Figure 1 provides a key plan showing the proposed development location. Figure 2 shows the concept plan of the proposed development, including the critical noise sensitive receptors.

## 2 Guidelines and Criteria

## 2.1 Transportation Noise – Outdoor Living Area (OLA)

MECP guidelines and the ENCG state that equivalent noise levels ( $L_{eq}$ -16hr) in outdoor living areas should not exceed 55 dBA. If it is not technically, economically, or administratively feasible to achieve a level of 55 dBA, predicted noise levels between 55 dBA and 60 dBA may be acceptable at the discretion of the City of Ottawa. Noise levels above 60 dBA are generally not acceptable and will warrant noise control measures.

All unenclosed balconies that are less than 4 m in depth and outside the exterior of the building façade are exempt from meeting the MECP outdoor noise criteria with regards to

transportation noise sources. Should the depth of the future balconies and terraces be greater than 4 m, they will be subject to the MECP noise level limit of 55 dBA.

#### 2.2 Transportation Noise – Indoor Living Spaces

Hotel sleeping quarters are required to meet an indoor road traffic noise level ( $L_{eq}$ -8hr) of 45 dBA during nighttime hours only. The indoor daytime noise level ( $L_{eq}$ -16hr) must not exceed 45 dBA in individual or semi-private offices, conference rooms and reading rooms, or 50 dBA inside general offices and reception areas. To achieve these levels, the MECP guidelines provide a basis for the types of windows, exterior walls, and doors that will be required based on projected outdoor noise levels.

The MECP guidelines also provide the following recommendations for the installation of or provision for adding central air conditioning to newly constructed dwellings depending on the outdoor transportation noise levels:

- Central air conditioning should be installed if the daytime or nighttime transportation sound level in the plane of a bedroom or living room window is above 65 dBA or 60 dBA respectively.
- The provision for the future installation of air conditioning should be made if the sound level is greater than 55 dBA and less than or equal to 65 dBA daytime, or greater than 50 dBA and less than or equal to 60 dBA nighttime.

The required limits as per NPC-300 are summarized in Table 1.

Table 1: Noise Limits Due to Road Traffic

Type of Space	Time Period	Maximum L <sub>eq</sub> (dBA) Road Traffic
General offices, reception areas, retail stores (Indoor)	07:00 – 23:00	50 dBA
Individual or semi-private offices, conference rooms, reading rooms (Indoor)	07:00 – 23:00	45 dBA
Sleeping quarters of hotels/motels (Indoor)	23:00 - 07:00	45 dBA
Outdoor Living Areas (OLA)	07:00 – 23:00	55 dBA

#### 2.3 Stationary Noise Sources

For sound from a stationary source, the NPC-300 sound level limit at a point of reception, expressed in terms of the one-hour equivalent sound level ( $L_{eq}$ -1hr), is the higher of the applicable exclusion limit value given in Table 2, or the background sound level for that point of reception. Owing to the subject site's proximity to the 416/417 corridor and in accordance with the ENCG, it is located within a Class 1 area in which background sound levels are dominated by the activities of people, usually road traffic. For conservatism and

simplicity, the exclusion limit values have been used for this assessment although they are likely exceeded by the background sound level at receptors most exposed to noise from road traffic.

,,	
Time of Day	Sound Level Exclusion Limit* Class 1 Area
	Outdoor Points of Reception
Day (07:00 to 19:00)	50 dBA
Evening (19:00 to 23:00)	50 dBA
	Plane of Window of Noise Sensitive Spaces
Day (07:00 to 19:00)	50 dBA
Evening (19:00 to 23:00)	50 dBA
Night (23:00 to 07:00)	45 dBA

Table 2: Noise Exclusion Limits – Stationary Noise Sources – Class 1

\*or the minimum existing hourly background sound level Leq, whichever is higher

The outdoor sound level limits for stationary sources apply only to daytime and evening hours, while sound level limits apply at all times for the Plane of Window of a noise sensitive space. In general, outdoor points of reception will be protected during the nighttime as a consequence of meeting the sound level limits at the adjacent Plane of Window of noise sensitive spaces.

For Class 1 areas, the Plane of Window limits apply to a window that is assumed to be open. Inoperable windows associated with noise sensitive spaces in noise sensitive commercial buildings including hotels are generally not considered points of reception and thus not subject to sound level limits.

The sound level limits listed in Table 2 for an outdoor point of reception define the point of reception as any area that is amenable for use by residents and do not apply to outdoor locations associated with a noise sensitive commercial purpose including hotels. The sound level limit is also valid for a point of reception location at the centre of the plane of a residential window.

## **3** Noise Level Predictions

#### 3.1 Road Traffic Noise

#### 3.1.1 Road Traffic Noise Calculations Procedure

The dominant road traffic noise sources in the subject study area are Maritime Way, Kanata Avenue and Highway 417. Neighbouring local roads Great Lakes Avenue and Canadian Shield Avenue are considered acoustically insignificant due to their low traffic volumes.



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Road traffic noise level calculations were performed in accordance with the MECP guidelines and ENCG using the Ontario Road Noise Analysis Method for Environment and Transportation (ORNAMENT). Sample copies of the traffic noise predictions from MECP's Road and Rail Traffic Noise Prediction Model STAMSON (Version 5.04) are included in Appendix B.

The equivalent sound levels  $(L_{eq})$  due to road traffic were calculated at worst-case noise sensitive receptors on the west, east and south façades of the proposed development. No calculations were made for outdoor amenity areas as none are shown on the current Site Plan shown in Appendix A. Calculations were performed for both daytime and nighttime conditions.

#### 3.1.2 Road Traffic Data

Road traffic noise predictions were based on the road traffic data outlined in Table 3.

Road traffic volume counts and truck percentages for Kanata Avenue and Highway 417 were based on the relevant values of ENCG Appendix B: Table of Traffic and Road Parameters to be Used for Sound Level Predictions. In both cases, these values were confirmed to be more conservative than those extrapolated from data provided by the City of Ottawa and the Province of Ontario.

Since ENCG Appendix B does not provide data inputs for local roadway classes, volume counts and heavy vehicle percentages for Maritime Way were based on data provided by the City of Ottawa. Per MECP guidance, volumes were escalated by 2% per annum for a 10-year period following the estimated completion of the development to establish an ultimate AADT.

Copies of the correspondence and received data are included in Appendix B. Receptor locations and exposure angles to each road segment are shown in Figures B1 to B4.

	Maritime Way	Kanata Avenue	Highway 417
Implied Roadway Class	Local	4-Lane Urban Arterial-Undivided (4-UAU) <sup>1</sup>	Freeway, Queensway, Highway
24-hour Volume (Current AADT)	3,470	-	-
24-hour Volume (Ultimate AADT)	4,670	30,000	146,664 (18,333 per lane)
No. of Lanes	2	4 <sup>1</sup>	8
Day/Night Split (%)	92/8 <sup>2</sup>	92/8	92/8
Percentage of Trucks (%)	3.5 <sup>3</sup>	12	12
Medium/Heavy Split (%)	50/50 <sup>2</sup>	58/42	58/42
Grade (%)	0	0	0
Posted Speed (km/hr)	40	50	100

Table 3: Road Traffic Volumes

<sup>1</sup>Kanata Avenue is to be widened from two lanes to four lanes per Table A3 of the City of Ottawa Transportation Master Plan (November 2013) and has been considered as such for the purpose of this assessment <sup>2</sup>Assumed values

<sup>3</sup>Based on total number of "heavy vehicles" reported in City study

#### 3.2 Stationary Noise

#### 3.2.1 Stationary Noise Calculation Procedure

The stationary noise source prediction model was generated using Datakustik's CadnaA Noise Prediction Software. This model is based on established noise prediction methods outlined in the ISO 9613-2 standard "Acoustic – Attenuation of sound during propagation outdoors – Part 2: General method and calculation". Noise levels were predicted using conditions of downwind propagation, generally with hard ground in paved areas. The worst-case receptor heights for the proposed residential tower were determined using the Building Evaluation tool.

#### 3.2.2 Impact on Development

For the purpose of this assessment, it has been assumed that hotel suites will feature operable windows which are therefore subject to the sound level limits as set out in Section 2.3.

The dominant noise sources expected to impact the subject site are rooftop mechanical equipment serving the surrounding residence and hotels as indicated on Figure 3. The following stationary noise sources have been identified based on a review of recent satellite imagery and Aercoustics' experience of conducting similar studies:

- 15 ton HVAC unit serving 1100 Canadian Shield Avenue (S01)
- 5 ton HVAC unit serving 1100 Canadian Shield Avenue (S02)

- 10 ton HVAC unit serving 1100 Canadian Shield Avenue (S03)
- 20 ton HVAC unit serving 1251 Maritime Way (S04)
- 10 ton HVAC unit serving 1250 Maritime Way (S05)
- 10 ton HVAC unit serving 1250 Maritime Way (S06)

A 100% daytime/evening and 50% nighttime duty cycle was assumed for each unit. Equipment sound power levels retrieved from Aercoustics' internal library are shown in Appendix C.

Any assumed equipment levels were conservative and are not expected to alter the conclusions of this study.

#### 3.2.3 Impact from Development

The proposed rooftop heat recovery unit has been identified as the main item of mechanical equipment with potential to impact neighbouring noise sensitive receptors. It is understood that the unit will be oriented with the outside air intake and return air exhaust terminals facing east and west respectively as shown in Figure 4.

A 100% daytime and evening and 50% nighttime duty cycle has been assumed. Sound power levels for the supply fan inlet and return fan exhaust terminals have been based on those shown on equipment specification sheets provided by McIntosh Perry as shown in Appendix C. Sound power levels for the condenser fan bank have been based on typical levels retrieved from Aercoustics' internal library.

This above modelling assumptions should be confirmed once finalized mechanical drawings and equipment selections are available.

Additional stationary noise sources associated with the development are expected to have minimal additional impact. This should be confirmed once details of any further HVAC equipment, parking exhaust fans, cooling towers or emergency standby generator equipment becomes available.

#### Development Self-Impact

Noise sensitive receptors within the development itself at risk of being impacted by the heat recovery unit noise will be those directly below on the top floor. In this case the sound transmission path of concern will be that which occurs through the roof and ceiling assembly between the unit and point(s) of reception. Performance criteria for this transmission path are not addressed within NPC-300 and the ENCG however it is recommended that the sound isolation performance of the ceiling and roof construction be reviewed once available to ensure noise levels are kept within suitable limits.

## 4 Noise Predictions

### 4.1 Road Traffic Noise Predictions

Table 4 lists the predicted 16-hour daytime and 8-hour nighttime  $L_{eq}$  noise levels due to road traffic at noise sensitive locations within the development, labelled as locations C01 to C03 on Figure 2. Sample calculations are provided in Appendix B.

Location	Height	Dood Someont	Distance Exposure (m) (deg.)	Exposure	L <sub>eq</sub> (dBA)	
Location	(m)	Road Segment		(deg.)	Day	Night
		Maritime (EW)	25	-40 to +30		
C01		Maritime (NS)	15	-90 to -60		
West Façade	16.5	Kanata	115	+15 to +90	62	55
		Highway 417 (N)	310	+50 to +90		
		Highway 417 (S)	345	+50 to +90		
		Maritime (E)	65	-90 to -35	65	57
C02	10 5	Maritime (W)	30	-70 to -45		
East Façade	16.5	Highway 417 (N)	295	-90 to 0		
		Highway 417 (S)	330	-90 to 0		
		Maritime (E)	55	-90 to -45		
C03		Maritime (W)	15	-80 to +50		
South Façade	16.5	Kanata	100	+35 to +90	65	58
		Highway 417 (N)	295	-90 to -15		
		Highway 417 (S)	330	-90 to -15		

Table 4: Calculated Noise Levels Due to Road Traffic

## 4.2 Stationary Noise Predictions

#### 4.2.1 Impact on Development

Table 5 lists the predicted worst-case daytime and nighttime 1-hour  $L_{eq}$  noise impacts at future receptors due to the stationary noise sources outlined in Section 3.2.2. Noise Impact contours are shown in Figure 5.

Receptor	Daytime L <sub>eq</sub> (dBA)			Nighttime L <sub>eq</sub> (dBA)		
	Predicted	Limit	Exceedance	Predicted	Limit	Exceedance
R01	48	50	No	45	45	No
R02	46	50	No	43	45	No



#### 4.2.2 Impact from Development

Table 6 lists the predicted worst-case daytime and nighttime 1-hour Leq noise impacts at existing neighbouring receptors due to the stationary noise sources outlined in Section 3.2.3. Noise impact contours are shown in Figure 6.

Receptor	Daytime L <sub>eq</sub> (dBA)			Nighttime L <sub>eq</sub> (dBA)		
	Predicted	Limit	Exceedance	Predicted	Limit	Exceedance
R03	43	50	No	40	45	No
R04	42	50	No	39	45	No
R05	47	50	No	44	45	No

#### Table 6: Stationary Noise Impact from Development

## 5 Noise Control Recommendations

#### 5.1 Transportation Noise – Outdoor Living Areas

No OLAs are proposed on the current Site Plan. Further analysis will be required if they are introduced later in the design process.

#### 5.2 Transportation Noise – Indoor Living Spaces

Indoor sound levels were examined with respect to MECP Guidelines as summarized in Section 2 of this report. Based on the predicted road traffic noise levels for receptor locations C01 to C03, standard exterior wall and window components that meet the requirements of the Ontario Building Code (OBC) will be sufficient for meeting the indoor sound level limits of Table 1.

In accordance with NPC-300 Section C7.1.2, the predicted daytime and nighttime road traffic noise levels dictate that the design should make provision for the installation of central air conditioning in the future at the occupant's discretion. In this case warning clause Type C as included in Section 7 is recommended. In the case that central air conditioning is fully implemented at the building's inception, warning clause Type C may instead be replaced with Type D.

#### 5.3 Stationary Noise Sources – Impact on Development

As shown in Table 5, the MECP sound level limits are not predicted to be exceeded at any noise sensitive points of reception associated with the development. Therefore, no noise mitigation measures are required to address the impact of stationary noise sources on the development.

#### 5.4 Stationary Noise Sources – Impact from Development

As shown in Table 6, the MECP sound level limits are not predicted to be exceeded at any noise sensitive points of reception in the vicinity of the development. Therefore, no noise

mitigation measures are required based on the current design assumptions outlined in this report.

The noise impact contours as shown in Figure 6 indicate that increased noise impacts would be likely for any points of reception that are on-axis with either the outside air intake or return air exhaust terminals of the heat recovery unit. It is therefore recommended that the unit be orientated as modelled for this report to ensure that no additional mitigation is required.

## 6 Conclusions

The results of this study indicate that standard exterior wall and window components that meet the requirements of the Ontario Building Code (OBC) should be sufficient to achieve compliance with the MECP criteria for indoor sound levels due to road traffic.

Noise impacts on the proposed development from existing neighbouring stationary noise sources are predicted to be within the applicable stationary noise limits without any noise controls.

Based on the modelling assumptions set out in this study, no noise controls will be required to address impacts from the development's proposed heat recovery unit on its surrounding noise sensitive receptors.

Further analysis should be conducted to confirm the noise impact of the development on itself when detailed information is available for the proposed roof and ceiling construction separating the heat recovery unit and top floor receptors.

## 7 Warning Clauses

Where applicable, purchase, rental and lease agreements are recommended to include one of the following warning clauses:

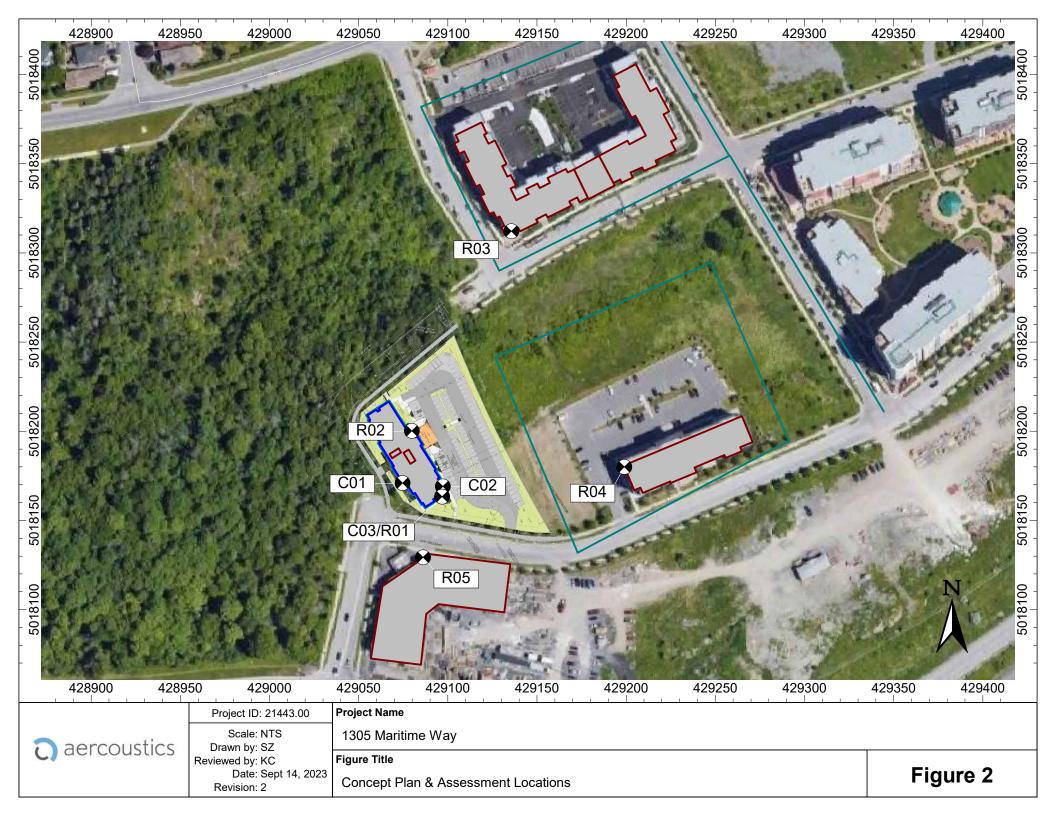
#### Warning Clause Type C:

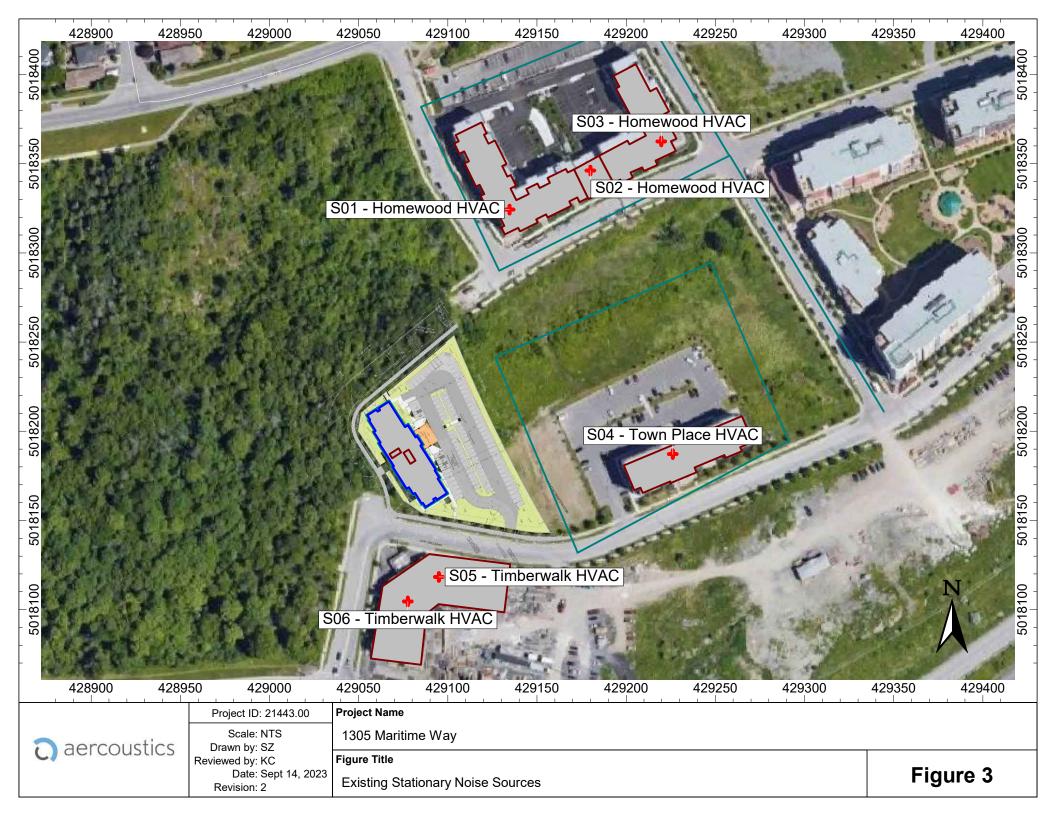
"Units have been designed with the provision for adding central air conditioning at the occupant's discretion. Installation of central air conditioning by the occupant in low and medium density developments will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the Municipality and the Ministry of the Environment."

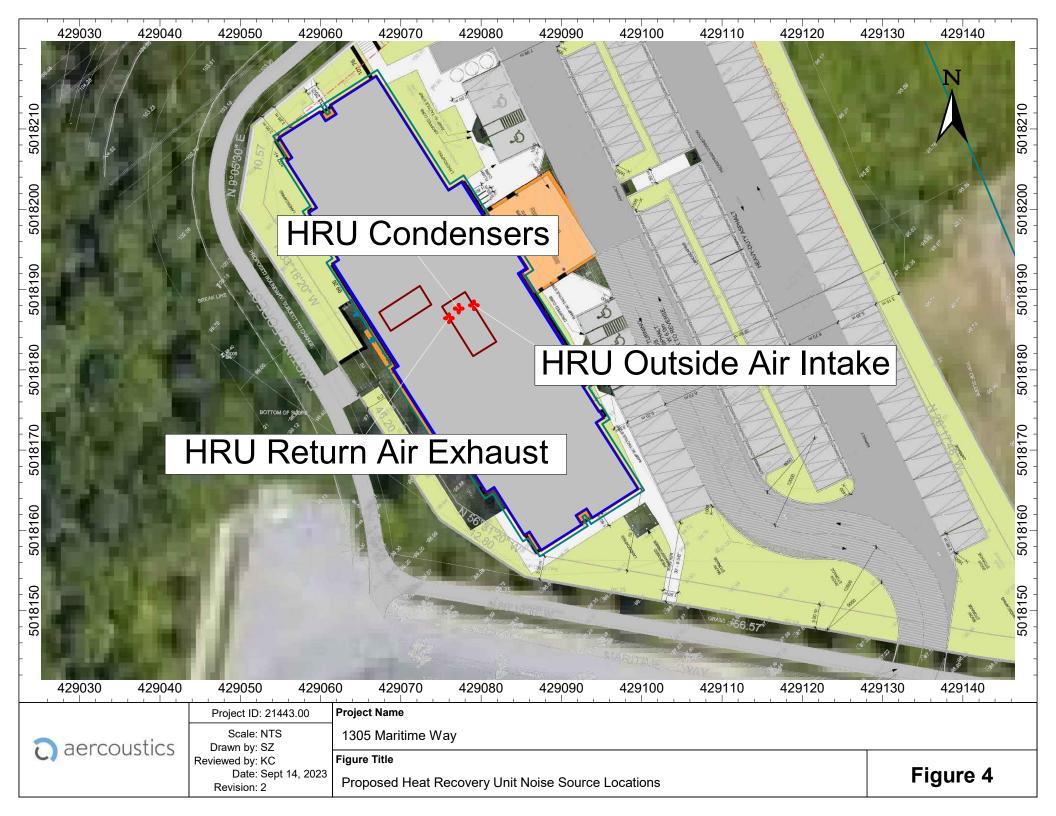
#### Warning Clause Type D:

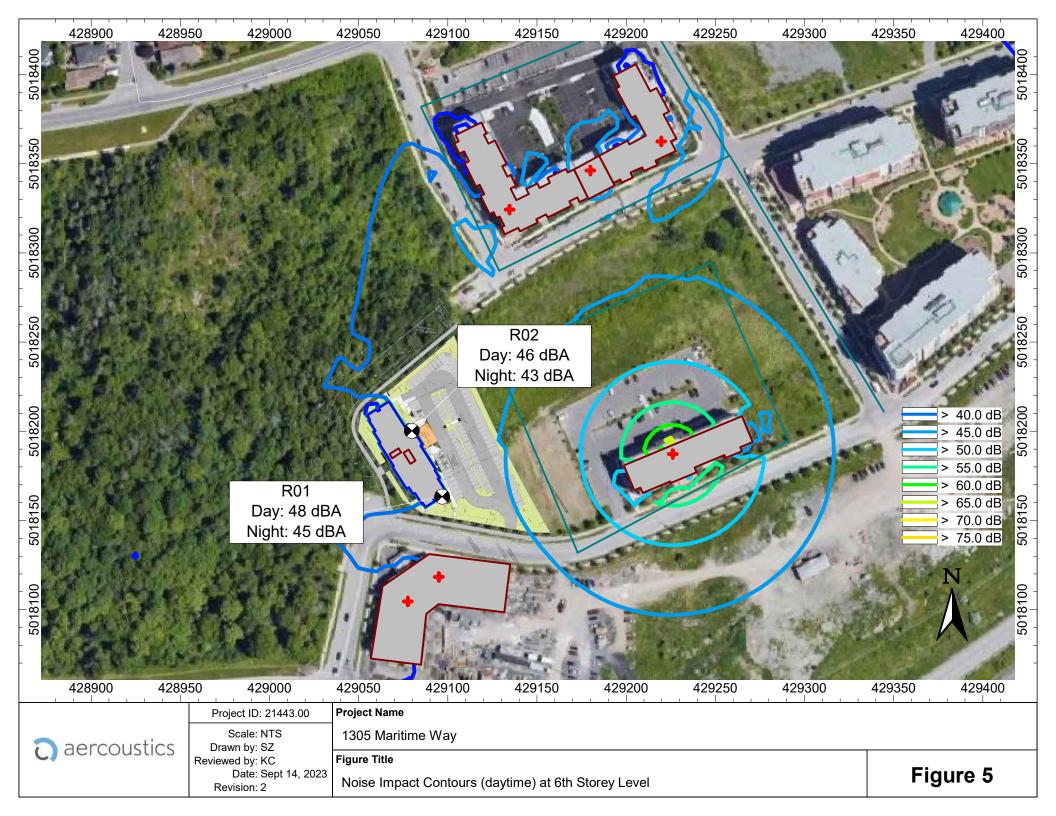
"Units have been supplied with a central air conditioning system which will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the Municipality and the Ministry of the Environment."

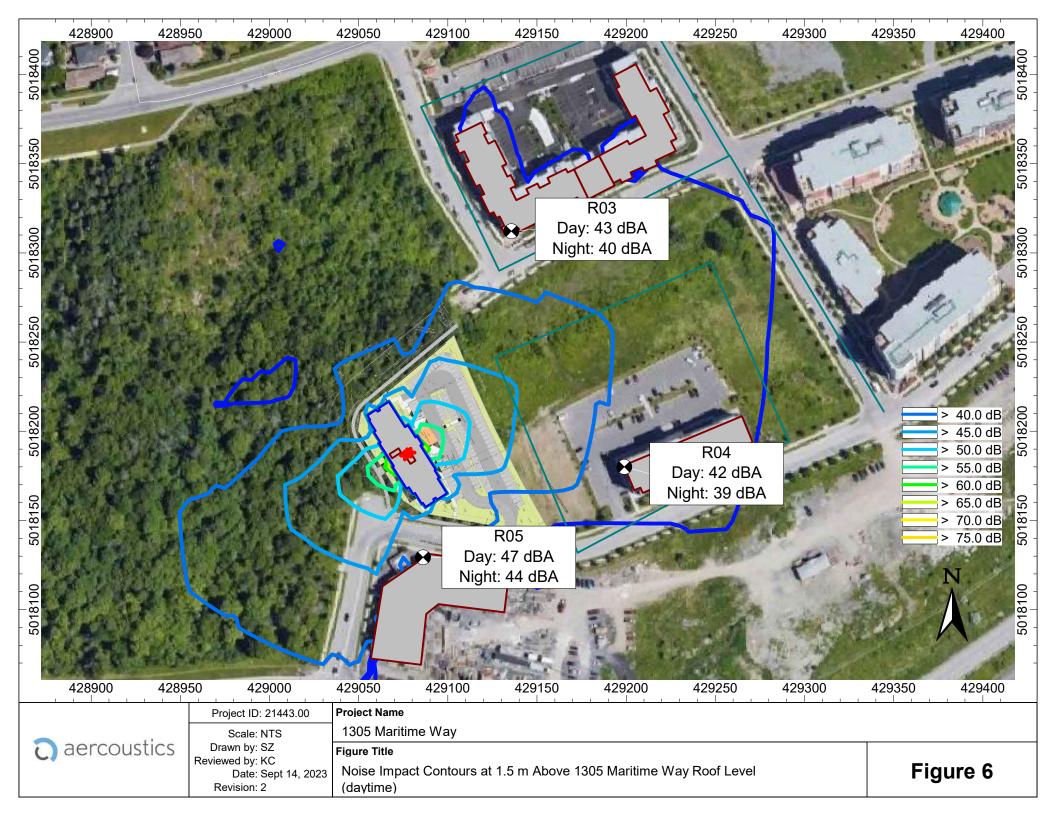






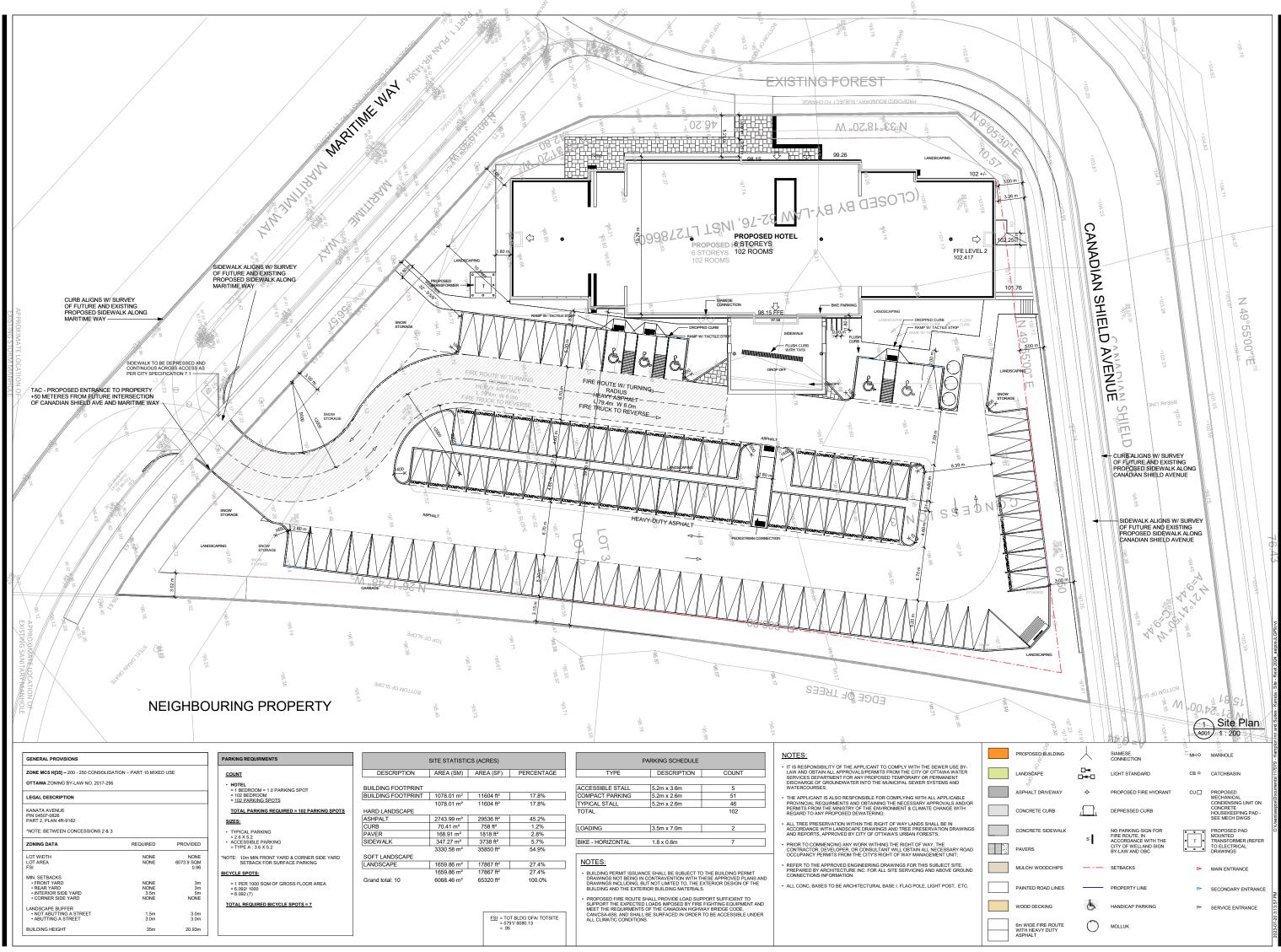






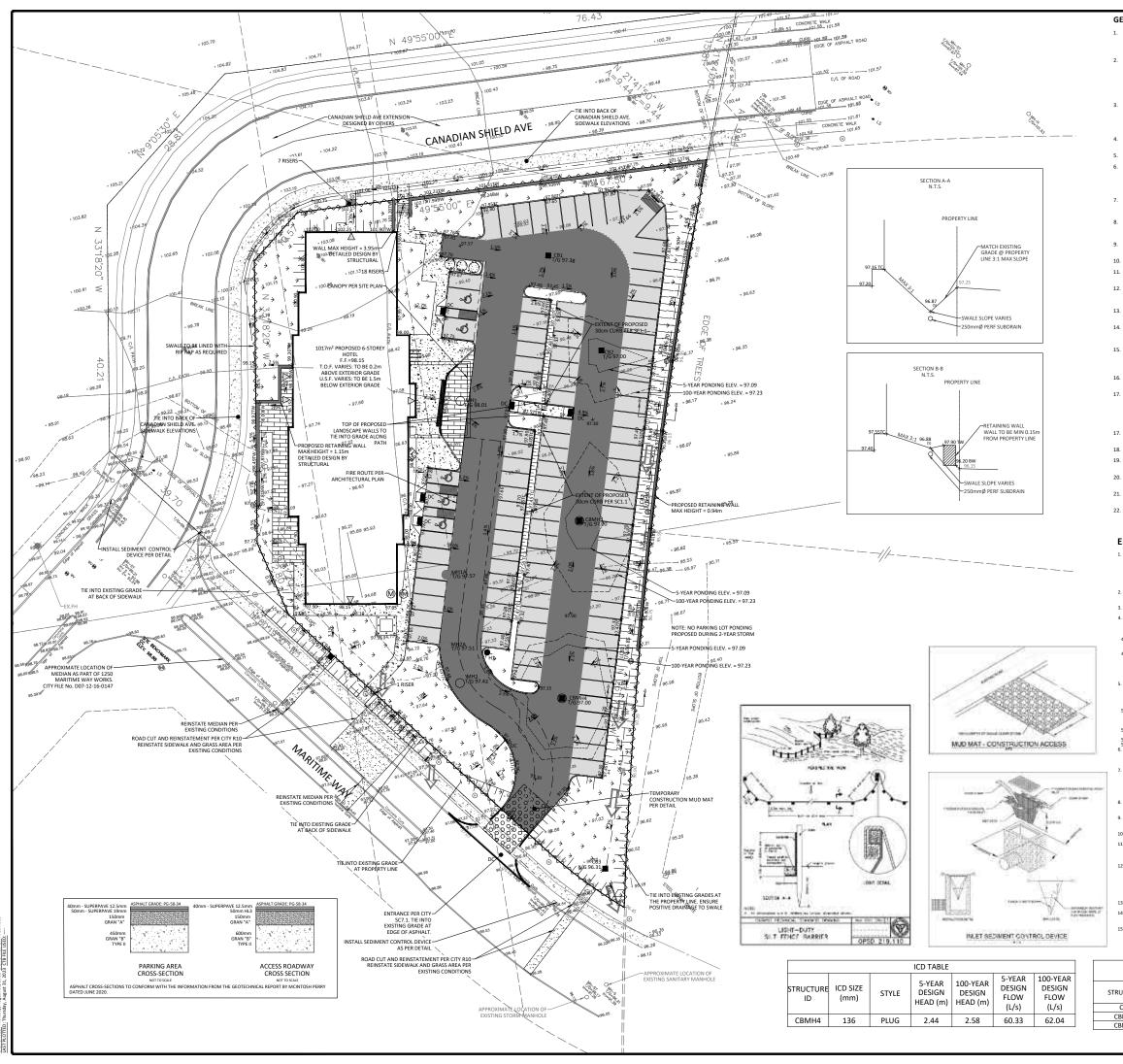
Appendix A Site Plan & Drawings





Chämberläin Architects Constructors Managers
Chamberlain Architect Services Limited
4671 Palladium Way (Unit 1) Burlington, Ontario. L7M 0W9
CANADA Phone: 905.631.7777
www.chamberlainIPD.com
NO.     ISSUED     DATE       1     SITE PLAN APPROVAL     2022 01.19
<text><text><text></text></text></text>
ALLANDA MARTIN
CONSTRUCTION NORTH TRUE NORTH
KANATA HAMPTON INN & SUITES
SHEET NAME
SITE PLAN
START DATE SEPT 19, 2019
LGJ, DM, MOR, NAL
CHECKED BY SM
As indicated
DRAWING

A001



#### GENERAL NOTES

. THE ORIGINAL TOPOGRAPHY, GROUND ELEVATION AND SURVEY DATA SHOWN ARE SUPPLIED FOR INFORMATION PURPOSES ONLY, AND IMPLY NO GUARANTEE OF ACI IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY ALL INFORMATIO

THIS PLAN IS NOT A CADASTRAL SURVEY SHOWING LEGAL PROPERTY BOUNDARIES AND EASEMENTS. THE PROPERTY BOUNDARIES SHOWN HEREON HAVE BEEN DERIVED INFORMATION SUPPLIED BY (RO SHOWN ON) LO BARNES (TL). DISON, BA10-115-00, DATED OCTOBER 16, 2018 AND CANNOT BE RELIED UPON TO BE ACCURATE OR COMPLET HER PRECISE LOCATION OF THE CURRENT PROPERTY BOUNDARIES AND EASEMENTS CAN ONCY DEO TEMMENDE THE UNRENT PROPERTY BOUNDARIES AND EASEMENTS CAN ONCY DEO TEMMENDE THE UNRENT PROFENDATION OF AND AS UBESCULDAY CADASTRAL SURVEY PERFORMED AND CERTIFIED BY AN ONTARIO LAND SURVEYOR.

ELEVATIONS SHOWN DERIVED FROM INFORMATION SUPPLIED BY (OR SHOWN ON) J.D.BARNES LTD. JOB No. 18-10-115-00, DATE OCTOBER 16, 2018 WIRE ESTABLISHED USING GLOBAL POSITIONING SYSTEM (GFS) GUIPMENT TO ESTABLISH ELIPSOIDAL HEIGHTS. ELIPSOIDAL HEIGHTS WERE TRANSFORMED TO CGVD-1928 DATUM (GEODETIC) USING THE FEDERAL HT2. DU HEIGHT TRANSFORMED TO CGVD-1928 DATUM (GEODETIC)

THE CONTRACTOR IS TO OBTAIN AND PAY FOR ALL NECESSARY PERMITS AND APPROVALS FROM THE CITY OR TOWNSHIP BEFORE COMMENCING CONSTRUCTION. 5. THE CONTRACTOR IS RESPONSIBLE FOR ALL LAYOUT.

6. THE CONTRACTOR IS TO DETERMINE THE EXACT LOCATION, SIZE, MATERIAL AND ELEVATION OF ALL EXISTING UTILITIES PRIOR TO COMMENCING CONSTRUCTION. PROTECT AND ASSUME ALL RESPONSIBILITY FOR EXISTING UTILITIES WHETHER OR NOTSTHOWN ON THESE DRAWINGS. IF THERE IS ANY DISCREPANCY THE CONTRACTOR IS TO NOTIFY THE ENGINEER PROMPTIV.

. RESTORE ALL TRENCHES AND SURFACES OF PUBLIC ROAD ALLOWANCES TO CONDITION EQUAL OR BETTER THAN ORIGINAL CONDITION AND TO THE SATISFACTION OF THE CITY OR TOWNSHIP AUTHORITIES.

EXCAVATE AND DISPOSE OF ALL EXCESS EXCAVATED MATERIAL, SUCH AS ASPHALT CURBING AND DEBRIS, OFF SITE AS DIRECTED BY THE ENGINEER AND THE CITY OR TOWNSHIP.

 TOPSOIL TO BE STRIPPED AND STOCKPILED FOR REHABILITATION. CLEAN FILL TO BE PLACED IN FILL AREAS AND COMPACTED TO 95% STANDARD PROCTOR DENSITY. 10. CONTRACTOR IS RESPONSIBLE TO KEEP ROAD FREE AND CLEAN FROM MUD OR DEBRIS 11. ALL DISTURBED AREAS TO BE RESTORED TO ORIGINAL CONDITION OR BETTER UNLESS OTHERWISE SPECIFIED.

THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL TRAFFIC CONTROL AND SAFETY MEASURES DURING THE CONSTRUCTION PERIOD, INCLUDING THE SUPPLY, INSTALLATION, AND REMOVAL OF ALL NECESSARY SIGMAGE, DELINEATORS, MARKERS AND BARRIERS.

13. DO NOT ALTER GRADING OF THE SITE WITHOUT PRIOR APPROVAL OF THE CITY OR TOWNSHIP.

ALL ROADWAY, PARKING LOT, AND GRADING WORKS TO BE UNDERTAKEN IN ACCORDANCE WITH CITY OR TOWNISHIP STANDARDS AND SPECIFICATIONS. THE CONTRACTOR IS TO PROVIDE POSITIVE DRAINAGE AWAY FROM THE BUILDING.

15. CONTACT THE CITY OR TOWNSHIP FOR INSPECTION OF ROUGH GRADING OF PARKING LOTS, ROADWAYS AND LANDSCAPED AREAS PRIOR TO PLACEMENT OF ASPHALT AND TOPSOIL. ALL DEFICIENCIES NOTED SHALL BE RECIFIED TO THE CITY OR TOWNSHIP SATISFACTION PRIOR TO PLACEMENT OF ANY ASPHALT, TOPSOIL, SEED & MULCH AND/OR SOD.

ALL DIMENSIONS AND INVERTS MUST BE VERIFIED PRIOR TO CONSTRUCTION, IF THERE IS ANY DISCREPANCY THE CONTRACTOR IS TO NOTIFY THE ENGINEER PROMPTLY.

17. ELECTRICAL, GAS, TELEPHONE AND TELEVISION SERVICE LOCATIONS ARE SUBJECT TO THE

VIDUAL AGENCY: • ELECTRICAL SERVICE - HYDRO OTTAWA, GAS SERVICE - ENBRIDGE, • TELEPHONE SERVICE - BELL CANADA, • TELEVISION SERVICE - ROGERS.

17. INSTALLATION TO BE IN ACCORDANCE WITH CURRENT CODES AND STANDARDS OF APPROVAL AGENCIES HYDRO OTTAWA, BELL AND THE CITY OR TOWNSHIP.

18. ALL PROPOSED CURB SHALL BE CONCRETE BARRIER CURB UNLESS SPECIFIED.

ALL EXISTING REDUNDANT PRIVATE APPROACHES FRONTING THIS DEVELOPMENT MUST BE REMOVED TO THE SATISFACTION OF THE CITY OR TOWNSHIP.

NO EXCESS DRAINAGE, EITHER DURING OR AFTER CONSTRUCTION, WILL BE DIRECTED TOWARDS NEIGHBOURING PROPERTIES.

NO ALTERATION OF EXISTING GRADES AND DRAINAGE PATTERNS ON PROPERTY BOUNDARIES AS PER CITY OF OTTAWA SITE ALTERATION BY-LAW 2018-164.

22. THIS PLAN MUST BE READ IN CONJUNCTION WITH GEOTECHNICAL REPORT BY MCINTOSH PERRY REPORT MCP-38-0056, DATED MAY 2018 AND THE SITE SERVICING REPORT BY MCINTOSH PERRY REPORT MCP-38-0534, DATED AUGUST 2019.

#### EROSION AND SEDIMENT CONTROL

1. THE CONTRACTOR SHALL IMPLEMENT BEST MANAGEMENT PRACTICES, TO PROVIDE FOR PROTECTION OF THE AREA DRAINAGE SYSTEM AND THE RECEIVING WATERCOURSE, DURING CONSTRUCTION ACTIVITIES. THIS JDES LIMITING THE AMOUNT OF EXPOSED SOIL, TEMPORARY SEDIMENT CONTROL (GEOSOCK IN AN OVERFLOW UNDER GRATE OR COVER) TO BE IMPLEMENTED DURING CONSTRUCTION ON A SEDIMENT TRAPS. NO RECYCLED GEOSOCK MATERIAL SHALL BE PERMITTED FOR USE ON SITE.

 AT THE DISCRETION OF THE PROJECT MANAGER OR MUNICIPAL STAFF, ADDITIONAL SILT CONTROL DEVICES SHALL BE INSTALLED AT DESIGNATED LOCATIONS. 3 FOR SILT FENCE BARRIER, USE OPSD 219 110. GEOTEXTILE FOR SILT FENCE AS PER OPSS 1860. TABLE 3

PLORE DIFFERENCE DARABER, DEC LOS DE JEJULIO. GEOLEXILE-FUNSILI FENCE AS PER UN-SS LEBU, IABLE 3.
EXCEPT AS ROYONEE DIN PARAGRAPHS 4.1, and 4.2. BELOW, STABILIZATION MEASURES STALL BE INITIATED AS SOON AS FEASIBLE. IN PORTIONS OF THE SITE WHERE CONSTRUCTION MACTIWITIES HAVE TEMPORARILY OR PERMANENTLY CASED, BUT IN A OL CASE MORE THAN 14 DAYS AFTER THE CONSTRUCTION ACTIVITY THE TEMPORARILY OR PERMANENTLY CEASED.
WHER THE INITIATION OF STABILIZATION MEASURES SY THE 14TH DAY AFTER CONSTRUCTION ACTIVITY TEMPORARILY OR PERMANENTLY CEASED.
WHER ALE INITIATION OF STABILIZATION MEASURES BY THE 14TH DAY AFTER CONSTRUCTION ACTIVITY TEMPORARILY OR PERMANENTLY CEASED.
WHER CONSTRUCTION ACTIVITY WILL RESUME ON A PORTION OF THE SITE WITHING J DAYS FROM WHEN ACTIVITIES CEASED, E.G. THE TOTAL TIME PERIOD THAT CONSTRUCTION ACTIVITY S TEMPORARILY CEASED ES STHAW 21 DAYS STHAW 31 DAYS AFTER MACHINE TO A THAT PORTION OF SITE BY THE 14TH DAY AFTER CONSTRUCTION ACTIVITY S TEMPORARILY CEASED IS ESTIMAN 21 DAYS FROM WHEN ACTIVITIES CONTINUE AND ADDITION ACTIVITY TEMPORARILY CEASED.

SEDIMENT THAT IS ACCUMULATED BY THE TEMPORARY EROSION AND SEDIMENT CONTROL MEASURES SI BE REMOVED IN A MANNER THAT AVDIDS SECARE OF THE SEDIMENT TO THE DOWNSTREAM SIDE OF THE CONTROL MEASURE AND AVDIDS DAMAGE TO THE CONTROL MEASURE. SEDIMENT SHALL BE REMOVED T THE LEVEL OF THE GRADE EXISTING AT THE TIME THE CONTROL MEASURE WAS CONSTRUCTED AND BE ACCORDING TO THE FOLLOWING:

5.1.1

ACCORDING TO THE FOLLOWING: 1. FOR LIGHT-OUT SEDIMENT BARRIERS, ACCUMULATED SEDIMENT SHALL BE REMOVED ONCE IT REACHES 1. FOR LIGHT-OUT SEDIMENT BARRIERS, ACCUMULATED SEDIMENT SHALL BE REMOVED ONCE IT REACHES 1. FLE LESSER OF THE FOLLOWING: 1. FLE LESSER OF THE FOLLOWING: 1. A DEPTH OF 300 AMI MINIMENTER UNDER THE ON THE CONTROL MEASURE: 1. A DEPTH OF 300 AMI MINIMENTER UNDER THE ON THE CONTROL MEASURE: 1. FLE ADDREAD OF 300 AMI MINIMENTER UNDER THE ADDREAD OF THE CONTROL MEASURE: 1. A DEPTH OF 300 AMI MINIMENTER ENDOUGH DRIVEN THE CONTROL MEASURE: 1. A DEPTH OF 300 AMI MINIMENTER ENDOUGH DRIVEN TO THE CONTROL MEASURE: 1. A DEPTH OF 300 AMI MINIMENTER ENDOUGH DRIVEN TO THE CONTROL MEASURE: 1. A LIEMPORARY REGISION AND SEDIMENT STOLE RE ENDOUGH DRIVEN TO THE CONTROL MEASURE: 1. A LIEMPORARY REGISION AND SEDIMENT CONTROL MEASURES SHALL BE MONTORED TO ENSURE THEY ARE IN EFFECTIVE WORKING ORDER. THE CONTROL MEASURES SHALL BE MONTORED TO ENSURE THEY ARE IN EFFECTIVE WORKING STORE THE CONTROL MEASURES SHALL BE MONTORED TO ENSURE THEY ARE IN EFFECTIVE WORKING STORE THE CONTROL MEASURES SHALL BE MONTORED TO ENSURE THEY ARE IN EFFECTIVE WORKING STORE THE CONTROL MEASURES SHALL BE MONTORED TO ENSURE THEY ARE IN EFFECTIVE WORKING STORE THE CONTROL MEASURES SHALL BE MONTORED TO ENSURE THEY ARE IN EFFECTIVE WORKING STORE THE CONTROL MEASURES SHALL BE MONTORED TO ENSURE THEY ARE IN EFFECTIVE WORKING STORE THE CONTROL MEASURES SHALL BE MONTORED TO ENSURE THEY ARE IN EFFECTIVE WORKING STORE THE CONTROL MEASURES SHALL BE MONTORED TO ENSURE THEY ARE IN EFFECTIVE WORKING STORE THE CONTROL MEASURES SHALL BE MONTORED TO ENSURE THEY ARE IN EFFECTIVE WORKING STORE THE CONTROL MEASURES SHALL BE MONTORED TO ENSURE THEY ARE IN EFFECTIVE WORKING STORE THE CONTROL MEASURE SHALL BE MONTORED THEY ARE

DUST CONTROL MEASURES SHOULD BE CONSIDERED PRIOR TO CLEARING A WATER, CALCIUM CHLORIDE FLAKES/SOLUTION OR MAGNESIUM CHLORIDE FLAKES/SOLUTION SHALL BE USE AS DUST SUPPRESSANTS AS PER DOSS SOR. THIS IS TO LIMIT WIND BORSION OF SOLUS WHICH MAY TRANSPORT SEDIMENTS OFFSITE, WHERE THEY MAY BE WASHED INTO THE RECEIVING WATER BY THE NEXT RINISTORM.

ALL 'GREEN AREAS' TO BE TREATED WITH 150mm TOPSOIL OPSS 570.

TOPSOIL TO BE STRIP

10. ALL DISTURBED AREAS TO BE RESTORED TO ORIGINAL CONDITION OR BETTER UNLESS OTHERWISE SPECIFIED STOCKPILED MATERIAL IS TO BE STORED AWAY FROM POTENTIAL RECEIVERS (E.G. STORM CATCHASINS, MANHOLES), AND BE SURROUNDED BY EROSION CONTROL MEASURES WHERE MATERIAL IS LEFT IN PLACE IN EXCESS OF 14 DAYS.

IF REQUIRED, DEWATEF ON FLAT GRADE UPSTR

13. ALL EROSION AND SEDIMENT CONTROL MEASURES SHALL CONFORM TO OPSS

 WHERE DEWATERING IS REQUIRED, THE DISCHARGED WATER SHALL BE CONTROLLED IN ACCORI OPSS 518. . ALL SETTLING/FILTRATION BASINS SHALL BE EQUIPPED WITH TERRAFI EQUIVALENT) AND SHALL BE CLEANED AND REPLACED AS REQUIRED

#### SURFACE STORAGE SUMMARY

UCTURE	5-YEAR ELEV. (m)	5-YEAR VOL. (m <sup>3</sup> )	100-YEAR ELEV. (m)	100-YEAR VOL. (m)		
CB2	97.09	1.00	97.23	13.40		
вмнз	97.09	1.10	97.23	18.80		
3MH4	97.09	1.30	97.23	21.00		
PLEASE NOTE: NO SURFACE STORAGE PONDING PROPOSED DURING 2-YEAR STORM EVENT						

RD PERFORATED PIP MH7A SANITARY MANHOLE WATER VAVLE/CHAMBER PARKING AREA ASPHALT FIRE HYDRANT ACCESS ROAD/FIRE ROUT - CENTRELINE OF SWALE SLOPING AT 3:1 (UNLESS SPECIFIED) PROPOSED ELEVATIO EXISTING ELEVATION ×100.35 100.20 SWALE ELEVATION XT/W100.50 B/W99.50 TOP OF WALL ELEVATION BOTTOM OF WALL ELEVATION EMERGENCY OVERLAND FLOW ROUTE ⇒ RETAINING WALL  $\mathbb{M}$ WATER METER/REMOTE METER LOCAITON FOR REVIEW ONLY NOT FOR CONSTRUCTION 3 ISSUED FOR REVIEW SEP 01, 2023 SSUED FOR REVIEW FEB 23, 2022 FEB 11, 2022 ISSUED FOR REVIEW No Revision Date eck and verify all dir Do not scale drawing e proceeding with the wo SCALE 1:300 MCINTOSH PERRY 115 Walgreen Road, RR3, Carp, ON KOA 1LO Tel: 613-836-2184 Fax: 613-836-3742 www.mcintoshperry.com Λ SILVER HOTELS (KANATA) INC 100 DIDSBURY ROAD #77 OTTAWA, ON K2T 0C2 **PROPOSED 6-STOREY HOTEL** 1305 MARITIME WAY OTTAWA, ON

LOCATION PLAN

BARRIER CURB DEPRESSED CURB

CB6 DI6 CRATCHBASIN OR DITCH INLET c/w 3.0m SUBDRAIN STUBS

CBMH# T/G CATCHBASIN MANHOLE

ETCB4 - LANDSCAPE CATCHBASIN

PROPERTY LINE

-O<sup>MH7</sup> STORM MANHOLE

FIRE DEPARTMENT CONNECTION

BUILDING ENTRANCE

ROOF DRAIN LOCAITON

TWSI PER CITY SC7.3

F

T

FGEND

Drawing Title:			
G	RADING,	DRAINAGE, SEDIMENT &	
	EROS	ION CONTROL PLAN	ò
			0001
Scale:	1:300	Project Number:	22-0
Drawn By:	R.R.R.	CCO-18-0534	<u> </u>
Checked By:	B.S.C.	Drawing Number:	5
Designed By:	A.J.G.	C101	207

Appendix B Road Traffic Data & Sample Calculations







# Appendix B: Table of Traffic and Road Parameters To Be Used For Sound Level Predictions

Row Width (m)	Implied Roadway Class	AADT Vehicles/Day	Posted Speed Km/Hr	Day/Night Split %	Medium Trucks %	Heavy Trucks % <sup>1</sup>	
NA <sup>2</sup>	Freeway, Queensway, Highway	18,333 per lane	100	92/8	7	5	
37.5-44.5	6-Lane Urban Arterial-Divided (6 UAD)	50,000	50-80	92/8	7	5	
34-37.5	4-Lane Urban Arterial-Divided (4-UAD)	35,000	50-80	92/8	7	5	
23-34	4-Lane Urban Arterial-Undivided (4-UAU)	30,000	50-80	92/8	7	5	
23-34	4-Lane Major Collector (4-UMCU)	24,000	40-60	92/8	7	5	
30-35.5	2-Lane Rural Arterial (2-RAU)	15,000	50-80	92/8	7	5	
20-30	2-Lane Urban Arterial (2-UAU)	15,000	50-80	92/8	7	5	
20-30	2-Lane Major Collector (2-UMCU)	12,000	40-60	92/8	7	5	
30-35.5	2-Lane Outer Rural Arterial (near the extremities of the City) (2-RAU)	10,000	50-80	92/8	7	5	
20-30	2-Lane Urban Collector (2-UCU)	8,000	40-50	92/8	7	5	

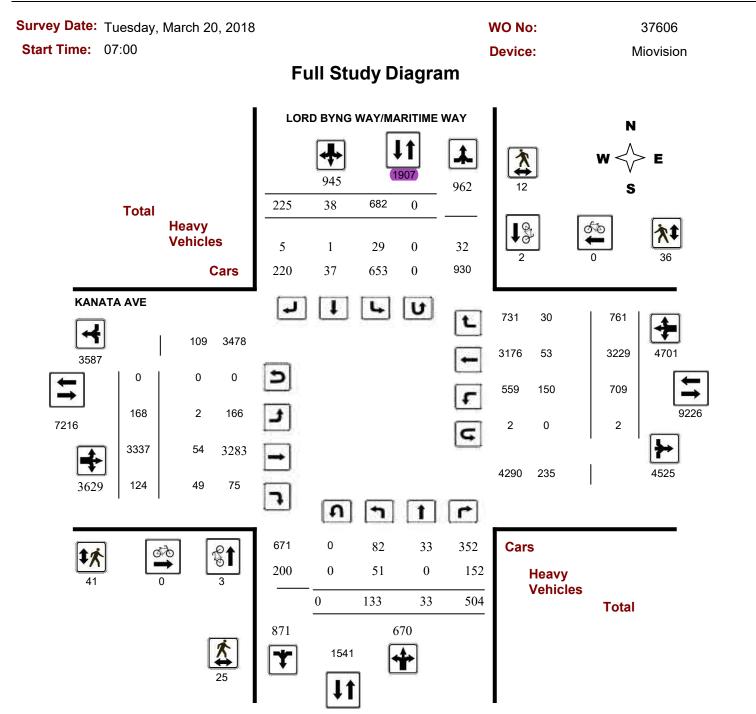
<sup>1</sup> The MOE Vehicle Classification definitions should be used to estimate automobiles, medium trucks and heavy trucks.

 $^{2}\,$  The number of lanes is determined by the future mature state of the roadway.

Environmental Noise Control Guidelines Part 4: Technical Requirements For Environmental Noise Control Studies And Implementation



## Turning Movement Count - Study Results KANATA AVE @ LORD BYNG WAY/MARITIME WAY





## Turning Movement Count - Study Results KANATA AVE @ LORD BYNG WAY/MARITIME WAY

Survey Da Start Tin			y, Ma	rch 20	, 2018				WO No:						37606 Miovision					
Start Th	ie: 0	1.00				<b>1</b>					04-	Devi				MIO	/Ision			
0		<b>-</b>					y 51	umma	• •				ra)							
Survey Da	ite: I	uesaa	ay, ivia	arch Zu	), 2018	5		T Northbound		bserv	red U-	Turns	0					T Facto	or	
								Eastbound	0			bound:	0 2				1.00			
	10	ים חס			ARITI			Lastbound	. U		1103									
				VAT/IV									NATA		/ +					
Period	LT	thboui ST	RT	NB	LT	uthbou ST	RT	SB	STR	LT	astbou ST	RT	EB	LT	/estbo ST	RT	WB	STR	Grand	
	45			TOT				TOT	TOT		100		TOT				тот	TOT	Total	
07:00 08:00	15	1	50	66	81	2	24	107	173	2	482	12	496	44	163	65	272	768	941	
08:00 09:00	18	6	35	59	92	4	20	116	175	14	423	14	451	79	214	119	412	863	1038	
09:00 10:00	11	5	55	71	69	1	33	103	174	15	323	14	352	57	256	67	380	732	906	
11:30 12:30	14	3	54	71	79	6	38	123	194	28	355	12	395	87	432	70	589	984	1178	
12:30 13:30	12	3	60	75	76	4	20	100	175	17	451	12	480	77	416	74	567	1047	1222	
15:00 16:00	15	5	75	95	93	4	27	124	219	27	397	18	442	99	533	116	748	1190	1409	
16:00 17:00	24	3	93	120	101	8	34	143	263	26	448	21	495	122	598	130	850	1345	1608	
17:00 18:00	24	7	82	113	91	9	29	129	242	39	458	21	518	144	617	120	881	1399	1641	
Sub Total	133	33	504	670	682	38	225	945	1615	168	3337	124	3629	709	3229	761	4699	8328	9943	
U Turns	0			0	0			0	0	0			0	2			2	2	2	
Total	133	33	504	670	682	38	225	945	1615	168	3337	124	3629	711	3229	761	4701	8330	9945	
EQ 12Hr Note: These v	185 ralues ar	46 e calcul	701 lated by	<b>932</b> y multipl	948 ying the	53 totals b	313 y the a	<b>1314</b> ppropriate	2246 expans	234 ion fact	4638 or.	172	5044	988 <b>1.39</b>	4488	1058	6534	11578	13824	
AVG 12Hr	185	46	701	932	948	53	313	1314	2246	234	4638	172	5044	988	4488	1058	6534	11578	13824	
Note: These v	olumes	are calo	culated	by mult	plying th	e Equiv	alent 1	2 hr. totals	s by the	AADT	factor.		<u>.</u>	1.00						
AVG 24Hr	242	60	918	1220	1242	69	410	1721	2941	307	6076	225	6608	1294	5879	1386	8559	15167	18108	
Note: These v				-			-	-			-		tor.	1.31						

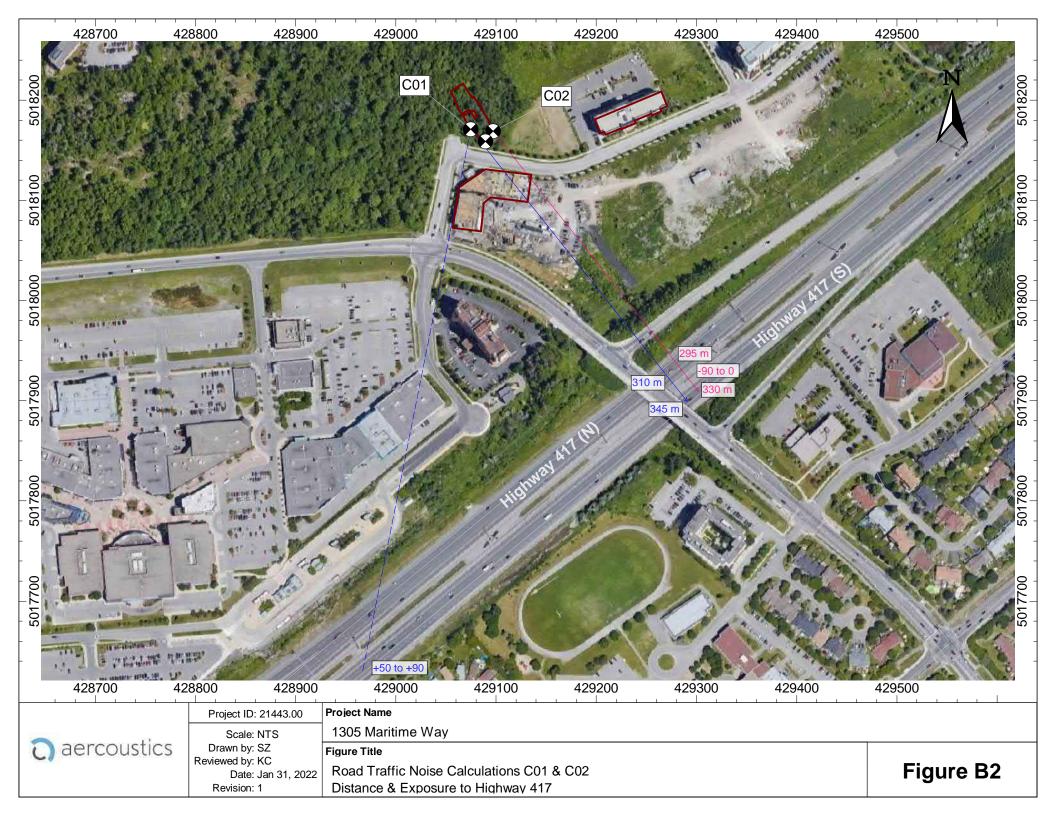
Note: U-Turns provided for approach totals. Refer to 'U-Turn' Report for specific breakdown.



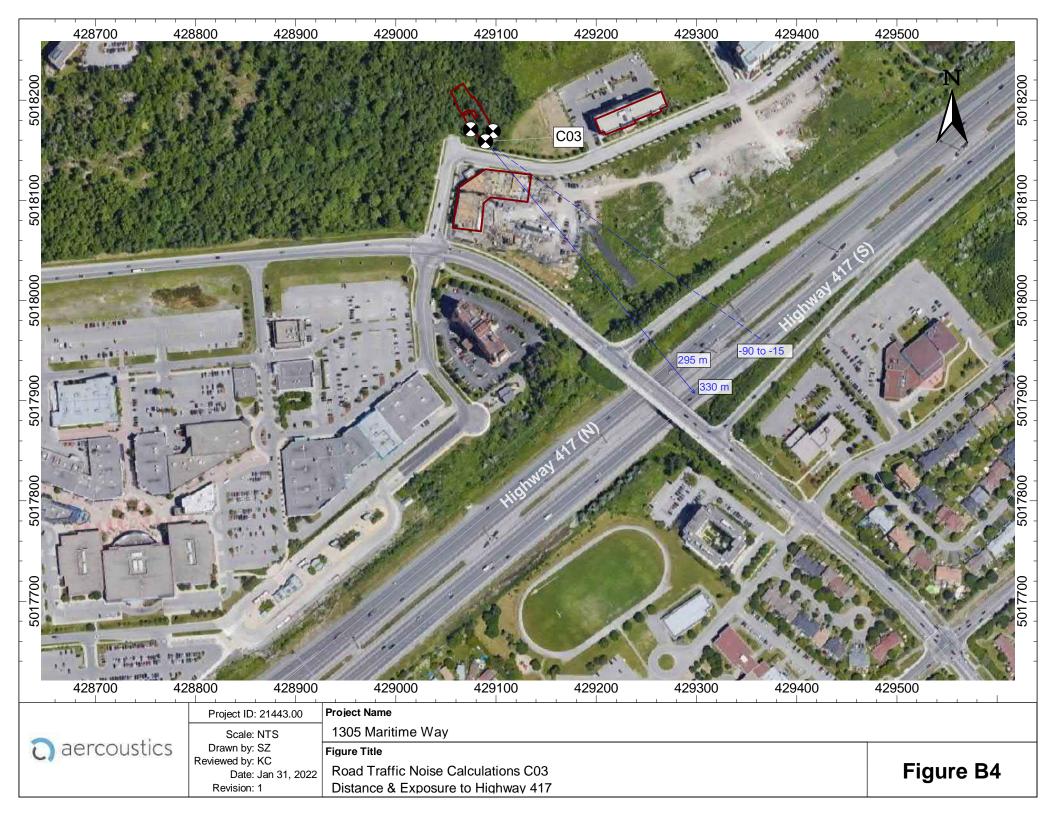
## Turning Movement Count - Study Results KANATA AVE @ LORD BYNG WAY/MARITIME WAY

Survey Date: Tuesday, March 20, 2018												wo	No:			37606			
Start Time: 07:00											Dev	ice:			Miovision				
	Full Study Heavy Vehicles																		
	LORD BYNG WAY/MARITIME WAY KANATA AVE																		
Northbound Southbound Eastbound Westbound																			
N 9. 910 E W 910 (												Grand							
Time Period	LT	ST	RT	тот	LT	ST	RT	тот	тот	LT	ST	RT	тот	LT	ST	RT	тот	тот	Total
07:00 07:15	1	0	8	9	0	0	1	1	10	0	0	1	1	7	0	0	7	8	18
07:15 07:30	1	0	5	6	3	0	0	3	9	0	2	1	3	3	1	1	5	8	17
07:30 07:45	1	0	5	6	1	0	2	3	9	0	1	2	3	5	8	0	13	16	25
07:45 08:00	1	0	9	10	0	0	0	0	10	0	3	2	5	5	2	0	7	12	22
08:00 08:15	3	0	4	7	1	0	0	1	8	0	0	2	2	5	0	7	12	14	22
08:15 08:30	2	0	2	4	2	0	0	2	6	0	2	2	4	3	3	1	7	11	17
08:30 08:45	2	0	5	7	3	0	0	3	10	0	1	2	3	6	2	0	8	11	21
08:45 09:00	0	0	5	5	0	0	0	0	5	0	2	1	3	6	1	2	9	12	17
09:00 09:15	3	0	8	11	2	0	0	2	13	2	4	2	8	4	4	3	11	19	32
09:15 09:30	1	0	4	5	1	0	0	1	6	0	1	1	2	6	0	0	6	8	14
09:30 09:45	1	0	6	7	1	0	0	1	8	0	1	1	2	6	3	0	9	11	19
09:45 10:00	0	0	7	7	0	0	0	0	7	0	0	3	3	6	2	4	12	15	22
11:30 11:45	2	0	2	4	1	0	0	1	5	0	2	1	3	4	1	1	6	9	14
11:45 12:00	0	0	4	4	2	0	1	3	7	0	2	1	3	3	2	2	7	10	17
12:00 12:15	3	0	5	8	2	0	0	2	10	0	2	2	4	2	3	0	5	9	19
12:15 12:30	0	0	4	4	0	0	0	0	4	0	2	3	5	6	2	1	9	14	18
12:30 12:45	3	0	5	8	1	0	0	1	9	0	1	0	1	3	3	0	6	7	16
12:45 13:00	0	0	4	4	0	0	0	0	4	0	3	3	6	5	1	3	9	15	19
13:00 13:15	0	0	4	4	3	0	0	3	7	0	3	0	3	3	1	3	7	10	17
13:15 13:30	0	0	3	3	2	0	1	3	6	0	3	3	6	5	3	1	9	15	21
15:00 15:15	2	0	6	8	1	0	0	1	9	0	4	3	7	3	2	0	5	12	21
15:15 15:30	1	0	3	4	1	0	0	1	5	0	3	2	5	4	2	0	6	11	16
15:30 15:45	2	0	5	7	0	1	0	1	8	0	1	1	2	4	1	1	6	8	16
15:45 16:00	3	0	5	8	0	0	0	0	8	0	1	0	1	7	1	0	8	9	17
16:00 16:15	3	0	3	6	0	0	0	0	6	0	1	2	3	2	3	0	5	8	14
16:15 16:30	2	0	4	6	0	0	0	0	6	0	1	2	3	6	2	0	8	11	17
16:30 16:45	2	0	4	6	0	0	0	0	6	0	1	0	1	4	0	0	4	5	11
16:45 17:00	3	0	4	7	0	0	0	0	7	0	2	0	2	6	0	0	6	8	15
17:00 17:15	3	0	5	8	0	0	0	0	8	0	2	2	4	5	0	0	5	9	17
17:15 17:30	2	0	3	5	1	0	0	1	6	0	2	1	3	3	0	0	3	6	12
17:30 17:45	3	0	5	8	1	0	0	1	9	0	1	2	3	7	0	0	7	10	19
17:45 18:00	1	0	6	7	0	0	0	0	7	0	0	1	1	6	0	0	6	7	14
Total: None	51	0	152	203	29	1	5	35	238	2	54	49	105	150	53	30	233	338	576

	428950	429000	429050	429100	429150	429200	429250	429300
5018250								
5018200		C01			C02	TRI		- 50182000
5018150			15 m -90 to -60 +30 25 m					
5018100			AN	-40 30 m -45	-10 Pill	to -35		5018100
5018050 5	Kanata A	Ave	+15 to +90 11	5 m				
20.	R	-						- 20. 20.
	428950	429000	429050	429100	429150	429200	429250	429300
		Project ID: 2144 Scale: NTS						
0	aercoustics	Drawn by: SZ Reviewed by: KC Date: Jan 3 Revision: 1	Figure Title 31, 2022 Road Traft	fic Noise Calculatio	ns C01 & C02 ime Way & Kanata A	venue		Figure B1



428950	429000	429050	429100	429150	429200	429250	429300
5018250 5018250			rt in			1994	- 5018250
- un	38.24						
2018200				E. S. C.	STIN P		5018200 5018200
2018				P 3			- 2018
				СС	3	-	-
2018150 5018150		+50	15 m Maritin	ne-Way	-		5018150
-		6-May	1.17	-Way -80	-90 to -45		et a se
5018100 5018100	Y.P.	aritim a	55 m				5018100
- 00					E B		- C
Kanat	a Ave	i to +90	100 m			C. Carl	- 5018050
201	• 1			Alert	All Car	the age	- 501
H	- *	1 Alexan	Charles and a second	1.		E. at	
428950	429000	429050	429100	429150	429200	429250	429300
	Project ID: Scale: I		ne aritime Way	i			
C) aercoust	ICS Drawn by: S Reviewed by: I	SZ Figure Title	)				
	Date: Cate:	Jan 31, 2022   Road I ra	affic Noise Calculati & & Exposure to Mar	ons C03 itime Way & Kanata	Avenue		Figure B3



STAMSON 5.0 SUMMARY REPORT Date: 14-09-2023 18:10:18 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: c01.te Time Period: Day/Night 16/8 hours Description: CO1 WEST FACADE Road data, segment # 1: Maritime EW (day/night) \_\_\_\_\_ Car traffic volume : 4149/361 veh/TimePeriod \* Medium truck volume : 75/7 veh/TimePeriod \* Heavy truck volume : 75/7 veh/TimePeriod \* Posted speed limit : 40 km/h Road gradient : 0 % Road pavement : 1 (Typical asphalt or concrete) \* Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 3472 Percentage of Annual Growth : 2.00 Number of Years of Growth: 15.00Medium Truck % of Total Volume: 1.75Heavy Truck % of Total Volume: 1.75Day (16 hrs) % of Total Volume: 92.00 Data for Segment # 1: Maritime EW (day/night) \_\_\_\_\_ Angle1Angle2: -40.00 deg30.00 degWood depth: 0(No woods.)No of house rows: 0 / 0Surface: 1(Absorptive) (Absorptive ground surface) Receiver source distance:25.00 / 25.00 mReceiver height:16.50 / 16.50 mTopography:1 : 0.00 Reference angle Road data, segment # 2: Maritime NS (day/night) \_\_\_\_\_ Car traffic volume : 4149/361 veh/TimePeriod \* Medium truck volume : 75/7 veh/TimePeriod \* Heavy truck volume : 75/7 veh/TimePeriod \* Posted speed limit : 40 km/h Road gradient : 0 % Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 3472 Percentage of Annual Growth : 2.00 Number of Years of Growth : 15.00 Number of fears of Growth: 15.00Medium Truck % of Total Volume: 1.75Heavy Truck % of Total Volume: 1.75Day (16 hrs) % of Total Volume: 92.00 Data for Segment # 2: Maritime NS (day/night) \_\_\_\_\_ Angle1Angle2: -90.00 deg-60.00 degWood depth:0(No woods.)No of house rows:0 / 0Surface:1(Absorptive ground surface) Receiver source distance : 15.00 / 15.00 m Receiver height: 16.50 / 16.50 mTopography: 1Reference angle: 0.00 Road data, segment # 3: Kanata (day/night) \_\_\_\_\_ Car traffic volume : 24288/2112 veh/TimePeriod \* Medium truck volume : 1932/168 veh/TimePeriod \* Heavy truck volume : 1380/120 veh/TimePeriod \* Posted speed limit : 50 km/h : 0 % : 1 (Typical asphalt or concrete) Road gradient : Road pavement \* Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 30000 Percentage of Annual Growth : 0.00 Number of Years of Growth:0.00Medium Truck % of Total Volume:7.00 Heavy Truck % of Total Volume : 5.00 Day (16 hrs) % of Total Volume : 92.00 Data for Segment # 3: Kanata (day/night) \_\_\_\_\_ Angle1Angle2:15.00 deg90.00 degWood depth:0(No woodsNo of house rows:0 / 0Surface:1(Absorptive) (No woods.) (Absorptive ground surface) Receiver source distance : 115.00 / 115.00 m Receiver height: 16.50 / 16.50 mTopography: 1Reference angle: 0.00

aercoustics

Road data, segment # 4: Hwy 417 N (day/night) \_\_\_\_\_ Car traffic volume : 59370/5163 veh/TimePeriod \* Medium truck volume : 4723/411 veh/TimePeriod \* Heavy truck volume : 3373/293 veh/TimePeriod \* Posted speed limit : 100 km/h Road gradient : 0 % Road pavement : 1 (Typical asphalt or concrete) \* Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 73332 Percentage of Annual Growth : 0.00 : 0.00 Number of Years of Growth Medium Truck % of Total Volume:0.00Heavy Truck % of Total Volume:5.00Day (16 hrs) % of Total Volume:92.00 Data for Segment # 4: Hwy 417 N (day/night) -----Angle1Angle2: 50.00 deg90.00 degWood depth: 0(No woods.)No of house rows: 0 / 0Surface: 1(Absorptive ground surface) Receiver source distance : 310.00 / 310.00 m Receiver height : 16.50 / 16.50 m : 1 (Flat/gentle slope; no barrier) Topography Reference angle : 0.00 Road data, segment # 5: Hwy 417 S (day/night) \_\_\_\_\_ Car traffic volume : 59370/5163 veh/TimePeriod \* Medium truck volume : 4723/411 veh/TimePeriod \* Heavy truck volume : 3373/293 veh/TimePeriod \* Posted speed limit : 100 km/h Road gradient : 0 % Road pavement : 1 (Typical asphalt or concrete) \* Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 73332 Percentage of Annual Growth : 0.00 Number of Years of Growth : 0.00 Medium Truck % of Total Volume:0.00Heavy Truck % of Total Volume:7.00Day (16 hrs) % of Total Volume:92.00

Data for Segment # 5: Hwy 417 S (day/night) -----Angle1Angle2: 50.00 deg90.00 degWood depth: 0(No woods.)No of house rows: 0 / 0Surface: 1(Absorptive) (Absorptive ground surface) Receiver source distance : 345.00 / 345.00 m Receiver height: 16.50 / 16.50 mTopography: 1 (Flat/gentle slope; no barrier)Reference angle: 0.00 Result summary (day) \_\_\_\_\_ ! source ! Road ! Total ! height ! Leq ! Leq ! (m) ! (dBA) ! (dBA) 1.Maritime EW!1.15 !51.14 !51.142.Maritime NS!1.15 !48.74 !48.743.Kanata!1.50 !56.30 !56.304.Hwy 417 N!1.50 !57.76 !57.765.Hwy 417 S!1.50 !57.20 !57.20 Total 62.44 dBA Result summary (night) \_\_\_\_\_ ! source ! Road ! Total ! height ! Leq ! Leq ! (m) ! (dBA) ! (dBA) \_\_\_\_\_+ 1.Maritime EW!1.17 !43.75 !43.752.Maritime NS!1.17 !41.35 !41.353.Kanata!1.50 !48.70 !48.704.Hwy 417 N!1.49 !50.17 !50.175.Hwy 417 S!1.49 !49.60 !49.60 \_\_\_\_\_+ Total 54.87 dBA TOTAL Leq FROM ALL SOURCES (DAY): 62.44 (NIGHT): 54.87

STAMSON 5.0 SUMMARY REPORT Date: 14-09-2023 18:11:25 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: c02.te Time Period: Day/Night 16/8 hours Description: CO2 EAST FACADE Road data, segment # 1: Maritime E (day/night) \_\_\_\_\_ Car traffic volume : 4149/361 veh/TimePeriod \* Medium truck volume : 75/7 veh/TimePeriod \* Heavy truck volume : 75/7 veh/TimePeriod \* Posted speed limit : 40 km/h Road gradient : 0 % Road pavement : 1 (Typical asphalt or concrete) \* Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 3472 Percentage of Annual Growth : 2.00 Number of Years of Growth15.00Medium Truck % of Total Volume1.75Heavy Truck % of Total Volume1.75Day (16 hrs) % of Total Volume92.00 Data for Segment # 1: Maritime E (day/night) \_\_\_\_\_ Angle1Angle2: -90.00 deg-35.00 degWood depth: 0(No woods.)No of house rows: 0 / 0Surface: 1(Absorptive) (Absorptive ground surface) Receiver source distance : 65.00 / 65.00 m Receiver height : 16.50 / 16.50 m Topography : 1 (Flat/gentle slope; no barrier) : 0.00 Reference angle Road data, segment # 2: Maritime W (day/night) \_\_\_\_\_ Car traffic volume : 4149/361 veh/TimePeriod \* Medium truck volume : 75/7 veh/TimePeriod \* Heavy truck volume : 75/7 veh/TimePeriod \* Posted speed limit : 40 km/h Road gradient : 0 % Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 3472 Percentage of Annual Growth : 2.00 Number of Years of Growth : 15.00 Number of Years of Growth: 15.00Medium Truck % of Total Volume: 1.75Heavy Truck % of Total Volume: 1.75Day (16 hrs) % of Total Volume: 92.00 Data for Segment # 2: Maritime W (day/night) \_\_\_\_\_ Angle1Angle2: -70.00 deg-45.00 degWood depth:0(No woods.)No of house rows:0 / 0Surface:1(Absorptive ground surface) Receiver source distance : 30.00 / 30.00 m Receiver height:16.50 / 16.50 mTopography:1Reference angle:0.00 Road data, segment # 3: 417 N (day/night) \_\_\_\_\_ Car traffic volume : 59370/5163 veh/TimePeriod \* Medium truck volume : 4723/411 veh/TimePeriod \* Heavy truck volume : 3373/293 veh/TimePeriod \* Posted speed limit : 100 km/h Road gradient : 0 % Road pavement : 1 (Typical asphalt or concrete) \* Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 73332 Percentage of Annual Growth : 0.00 Number of Years of Growth0.00Medium Truck % of Total Volume7.00Heavy Truck % of Total Volume5.00Day (16 hrs) % of Total Volume92.00 Data for Segment # 3: 417 N (day/night) \_\_\_\_\_ Angle1Angle2: -90.00 deg0.00 degWood depth: 0(No woods.)No of house rows: 0 / 0Surface: 1(Absorptive) (Absorptive ground surface) Receiver source distance : 295.00 / 295.00 m Receiver height: 16.50 / 16.50 mTopography: 1Reference angle: 0.00

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Road data, segment # 4: 417 S (day/night) -----Car traffic volume : 59370/5163 veh/TimePeriod \* Medium truck volume : 4723/411 veh/TimePeriod \* Heavy truck volume : 3373/293 veh/TimePeriod \* Posted speed limit : 100 km/h Road gradient : 0 % Road pavement : 1 (Typical asphalt or concrete) \* Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 73332 Percentage of Annual Growth : 0.00 : 0.00 Number of Years of Growth Medium Truck % of Total Volume7.00Heavy Truck % of Total Volume5.00Day (16 hrs) % of Total Volume92.00 Data for Segment # 4: 417 S (day/night) \_\_\_\_\_ Angle1Angle2: -90.00 deg0.00 degWood depth:0(No woods.)No of house rows:0 / 0Surface:1(Absorptive ground surface) Receiver source distance : 330.00 / 330.00 m Receiver height : 16.50 / 16.50 m : 1 (Flat/gentle slope; no barrier) Topography Reference angle : 0.00 Result summary (day) \_\_\_\_\_ ! source ! Road ! Total ! height ! Leq ! Leq ! (m) ! (dBA) ! (dBA) \_\_\_\_\_+ 1.Maritime E!1.15 !44.14 !44.142.Maritime W!1.15 !45.15 !45.153.417 N!1.50 !62.17 !62.174.417 S!1.50 !61.58 !61.58 4.417 S \_\_\_\_\_+ Total 64.98 dBA

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Result summary (nig	ght)			
	2	! Road ! Leq ! (dBA)	!	
1.Maritime E 2.Maritime W 3.417 N 4.417 S	! 1.49	! 37.76 ! 54.57 ! 53.98	! ! !	36.75 37.76 54.57 53.98
	Total	-+	-+-	57.38 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 64.98 (NIGHT): 57.38



STAMSON 5.0 SUMMARY REPORT Date: 14-09-2023 18:12:07 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: c03.te Time Period: Day/Night 16/8 hours Description: CO3 EAST FACADE Road data, segment # 1: Maritime E (day/night) \_\_\_\_\_ Car traffic volume : 4149/361 veh/TimePeriod \* Medium truck volume : 75/7 veh/TimePeriod \* Heavy truck volume : 75/7 veh/TimePeriod \* Posted speed limit : 40 km/h Road gradient : 0 % Road pavement : 1 (Typical asphalt or concrete) \* Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 3472 Percentage of Annual Growth : 2.00 Number of Years of Growth15.00Medium Truck % of Total Volume1.75Heavy Truck % of Total Volume1.75Day (16 hrs) % of Total Volume92.00 Data for Segment # 1: Maritime E (day/night) \_\_\_\_\_ Angle1Angle2: -90.00 deg-45.00 degWood depth: 0(No woods.)No of house rows: 0 / 0Surface: 1(Absorptive) (Absorptive ground surface) Receiver source distance : 55.00 / 55.00 m Receiver height : 16.50 / 16.50 m Topography : 1 (Flat/gentle slope; no barrier) : 0.00 Reference angle Road data, segment # 2: Maritime W (day/night) \_\_\_\_\_ Car traffic volume : 4149/361 veh/TimePeriod \* Medium truck volume : 75/7 veh/TimePeriod \* Heavy truck volume : 75/7 veh/TimePeriod \* Posted speed limit : 40 km/h Road gradient : 0 % Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 3472 Percentage of Annual Growth : 2.00 Number of Years of Growth : 15.00 Number of Years of Growth: 15.00Medium Truck % of Total Volume: 1.75Heavy Truck % of Total Volume: 1.75Day (16 hrs) % of Total Volume: 92.00 Data for Segment # 2: Maritime W (day/night) \_\_\_\_\_ Angle1Angle2: -80.00 deg50.00 degWood depth: 0(No woods.)No of house rows: 0 / 0Surface: 1(Absorptive ground surface) Receiver source distance : 15.00 / 15.00 m Receiver height: 16.50 / 16.50 mTopography: 1Reference angle: 0.00 Road data, segment # 3: Kanata (day/night) \_\_\_\_\_ Car traffic volume : 24288/2112 veh/TimePeriod \* Medium truck volume : 1932/168 veh/TimePeriod \* Heavy truck volume : 1380/120 veh/TimePeriod \* Posted speed limit : 50 km/h : 0 % : 1 (Typical asphalt or concrete) Road gradient : Road pavement \* Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 30000 Percentage of Annual Growth : 0.00 Number of Years of Growth: 0.00Medium Truck % of Total Volume: 7.00 Heavy Truck % of Total Volume : 5.00 Day (16 hrs) % of Total Volume : 92.00 Data for Segment # 3: Kanata (day/night) \_\_\_\_\_ Angle1Angle2: 35.00 deg90.00 degWood depth: 0(No woodsNo of house rows: 0 / 0Surface: 1(Absorptive) (No woods.) (Absorptive ground surface) Receiver source distance : 100.00 / 100.00 m Receiver height: 160.00 / 160.00 mTopography: 16.50 / 16.50 mReference angle: 1 (Flat/gentle slope; no barrier): 0.00

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Road data, segment # 4: 417 N (day/night) \_\_\_\_\_ Car traffic volume : 59370/5163 veh/TimePeriod \* Medium truck volume : 4723/411 veh/TimePeriod \* Heavy truck volume : 3373/293 veh/TimePeriod \* Posted speed limit : 100 km/h Road gradient : 0 % Road pavement : 1 (Typical asphalt or concrete) \* Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 73332 Percentage of Annual Growth : 0.00 : 0.00 Number of Years of Growth Medium Truck % of Total Volume:0.00Heavy Truck % of Total Volume:5.00Day (16 hrs) % of Total Volume:92.00 Data for Segment # 4: 417 N (day/night) \_\_\_\_\_ Angle1Angle2: -90.00 deg-15.00 degWood depth:0(No woods.)No of house rows:0 / 0Surface:1(Absorptive ground surface) Receiver source distance : 295.00 / 295.00 m Receiver height : 16.50 / 16.50 m : 1 (Flat/gentle slope; no barrier) Topography Reference angle : 0.00 Road data, segment # 5: 417 S (day/night) \_\_\_\_\_ Car traffic volume : 59370/5163 veh/TimePeriod \* Medium truck volume : 4723/411 veh/TimePeriod \* Heavy truck volume : 3373/293 veh/TimePeriod \* Posted speed limit : 100 km/h Road gradient : 0 % Road pavement : 1 (Typical asphalt or concrete) \* Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 73332 Percentage of Annual Growth : 0.00 Number of Years of Growth : 0.00 : 0.00 Medium Truck % of Total Volume:0.00Heavy Truck % of Total Volume:7.00Day (16 hrs) % of Total Volume:92.00

Data for Segment # 5: 417 S (day/night) -----Angle1Angle2: -90.00 deg-15.00 degWood depth:0(No woods.)No of house rows:0 / 0Surface:1(Absorptive (Absorptive ground surface) Receiver source distance : 330.00 / 330.00 m Receiver height : 16.50 / 16.50 m Topography : 1 (Flat/gentle slope; no barrier) Reference angle : 0.00 Result summary (day) \_\_\_\_\_ ! source ! Road ! Total ! height ! Leq ! Leq ! (m) ! (dBA) ! (dBA) 1.Maritime E!1.15 !43.98 !43.982.Maritime W!1.15 !56.31 !56.313.Kanata!1.50 !55.45 !55.454.417 N!1.50 !61.26 !61.265.417 S!1.50 !60.67 !60.67 \_\_\_\_\_+ Total 65.19 dBA Result summary (night) \_\_\_\_\_ ! source ! Road ! Total ! height ! Leq ! Leq ! (m) ! (dBA) ! (dBA) \_\_\_\_\_+ 1.Maritime E!1.17 !36.59 !36.592.Maritime W!1.17 !48.92 !48.923.Kanata!1.50 !47.86 !47.864.417 N!1.49 !53.66 !53.665.417 S!1.49 !53.07 !53.07 Total 57.62 dBA TOTAL Leq FROM ALL SOURCES (DAY): 65.19 (NIGHT): 57.62

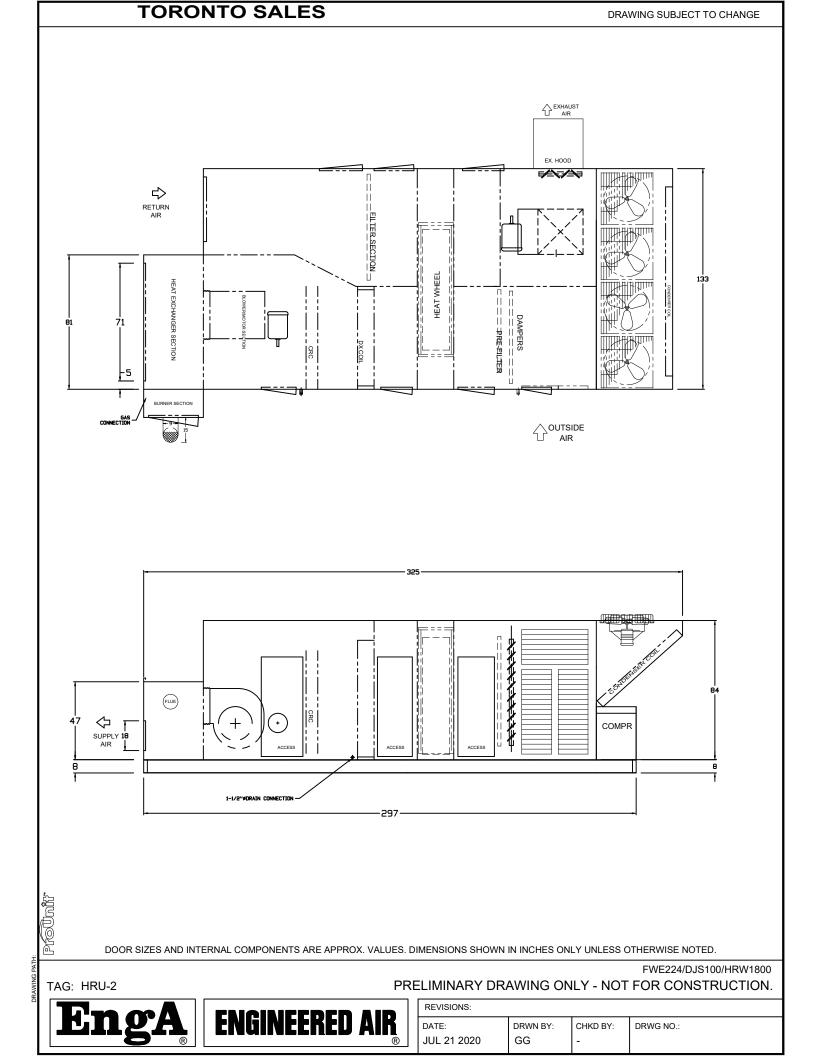
# Appendix C Sound Power Level Data



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Course	Sound Power level dB									
Source	63	125	250	500	1k	2k	4k	8k	Α	
5 ton HVAC	57	76	72	73	75	75	71	69	81	
10 ton HVAC	98	90	86	85	84	78	71	66	88	
15 ton HVAC	87	90	86	84	83	79	74	69	87	
20 ton HVAC	100	99	97	95	92	89	85	78	97	
Condenser Fans	93	95	90	86	81	75	71	66	88	







## ENTHALPY WHEEL PERFORMANCE DATA

Version 1.1.18

JOB NAME:			JOB NO:	
CUSTOMER:			ENGINEER:	
LOCATION:	Toronto, ON		ALTITUDE:	578 ft (176.2 m)
EngA MODEL:		QTY:	TAG:	ERW HRU-2

	Enthalpy Wheel Selection Data - Mo	del AEW10-1800 (Note 1)	)	] Si	ummer	
		Supply	Exhaust			
	Inlet Static Pressure	-0.5"Wc	-1.25"Wc	Supply Outlet		Supply Inlet
	Air Flow Through wheel	8850 Scfm Outlet	7900 Scfm Inlet	8850 Scfm		9583 Scfm
	Entering Temperature DB(RH)/WB	90.0/73.0°F	75.0/62.5°F	79.7/66.4°F(49%)		90.0/73.0°F
	Leaving Temperature DB/WB(RH)	79.7/66.4°F(49%)	86.5/70.3°F(45%)			0° Purge Angle
Summer	Air Pressure Drop	1.07"Wc	0.94"Wc			
Design	Enthalpy Recovery	220.89 Mbh		Exhaust Inlet	→	Exhaust Outlet
	Sensible Recovery	98.01 Mbh		7900 Scfm		8633 Scfm
	Moisture Removal	107.75 Lb/Hr		75.0/62.5°F		86.5/70.3°F(45%)
	S/A Sensible/Total Efficiency	68.4 / 64.6%				
	ASHRAE Sensible/Total Effectiveness	76.6 / 72.4%				
	Inlet Static Pressure	-0.5"Wc	-1.25"Wc	<b>`</b>	Vinter	
	Air Flow Through wheel	8850 Scfm Outlet	7900 Scfm Inlet			
	Entering Temperature DB(RH)/WB	-4.0/-5.0°F	72.0/54.0°F	Supply Outlet	←	Supply Inlet
	Leaving Temperature DB/WB(RH)	38.4/32.4°F(51%)	24.5/24.2°F(94%)	8850 Scfm 38.4/32.4°F(51%)		9583 Scfm -4.0/-5.0°F
Winter	Air Pressure Drop	0.93"Wc	0.88"Wc	30.4/32.4 1 (31/8)		
Design (Note 2)	Enthalpy Recovery	496.38 Mbh		l		0° Purge Angle
(	Sensible Recovery	404.85 Mbh		Exhaust Inlet		Exhaust Outlet
	Moisture Addition	84.4 Lb/Hr		7900 Scfm		8633 Scfm
	Frost Point	7.0°F		72.0/54.0°F		24.5/24.2°F(94%)
	ASHRAE Sensible/Total Effectiveness	76.6 / 74.4%(Note 3)				. ,

Notes: 1. Energy recovery component certified to the ARI Air-to-Air Energy Recovery Ventilation Equipment Certification Program in accordance with ARI Standard 1060-2001

2. Wheel performance in the winter design section includes the effects of frost control.

3. Values are under no frost condition



Version 3.5.40.S

Job Name:		Job No.:	
Customer:		Tag No.:	
Location:	Toronto, ON	Altitude:	578 feet

Coil Tag	CC-2
Unit Model	FWE224 *
DX Coil Size, in (H x L x R x FPI)	60 x 40 x 8R 8 (1/2")
DX Coil Size, mm (H x L x R x FPI)	1524 x 1025 x 8R 8 (13 mm)
DX Coil Blank Tube	0
Header Qty. & Size, in (mm)	(4) 7/8 (22 mm)
Distributors Qty. & Size	(4) 4-3-4
# of HGBP / Ton/Circ (Ton)	1 / 1.45
Design Ambient, °F (°C) DB	95.0 (35.0)
Net Capacity, MBH (kw)	278 (81.5)
Total / Sensible Capacity, MBH (kw)	278 (81.5) / 217 (63.5)
Air Flow Conditions	Standard CFM
Total / DX Air Flow, CFM (I/s)	8850 (4177.2) / 8850 (4177.2)
Air EDBT, °F (°C) / EWBT, °F (°C)	79.7 (26.5) / 66.4 (19.1)
DX LDBT / LWBT, °F (°C)	57.0 (13.9) / 56.4 (13.6)
D/A LDBT / LWBT, °F (°C)	57.0 (13.9) / 56.4 (13.6)
Water Removal, Ib/h (kg/h)	53.2 (24.1)
Drain Pan, in (mm) / No. of Mid. Pan	9 (239) / 1
Leaving Coil Velocity, AFPM (m/s)	532 (2.70)
Coil Pressure Drop, in.wc. (pa)	0.84 (209.0)
SST / SCT, °F (°C)	51.6 (10.9) / 126.2 (52.3)
S/A Motor Information	
R/A Motor Information	
	10.0 / 11.6
CSA C746-17 EER / IEER (Min. Requirement)	10.0 / 11.6
AHRI 340/360-2007 EER / IEER Rating	
Notes	4,5,11

### Notes:

[4] The coil performance data is based on R-410A refrigerant.

[5] Make-up application.

[11] Standard components listed above may change at Engineered Air's discretion provided that the unit model listed efficiency & capacity are maintained.

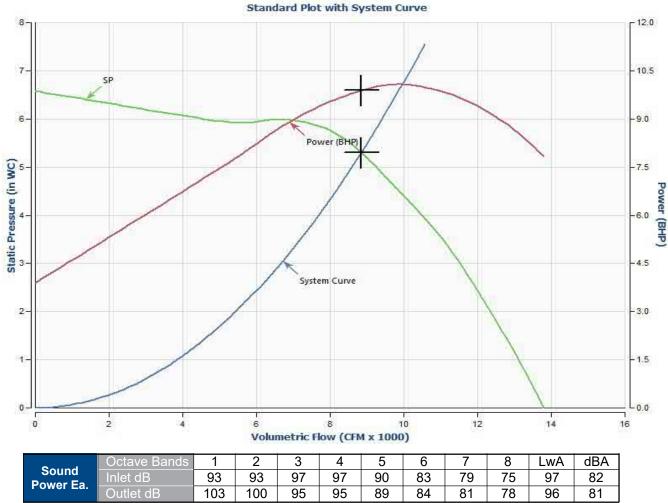


## Tag: S/A HRU-1

## Fan information

Size/Model 182/BAE-DW	Class	Outlet Vel (FPM) 2565
Volumetric Flow (CFM) 8850	Speed (RPM)	Density (lb/ft³) 0.075
SP (in WC) 5.3	Max Speed 2,930 RPM @ 70 °F	FEG FEG90
	Power (BHP) 9.89	

## Adjusted for



LwA: The overall (single value) fan sound power level in dB re. 10<sup>-12</sup> Watts, 'A' weighted.

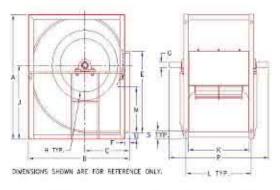
dBA: Estimated sound pressure level (re:0.0002 microbar) based on a single ducted installation at 5 ft., using a directivity factor of 1.

Ver 10.1 October 2018 - Created Updated Owner

All quotations per Twin City Fan Terms and Conditions found at www.twincityfan.com/TC\_TCF.pdf



				11/2/10Ca2111	notes				
odel IODEL A20-18H	Flow 8633 CFM	Pressure (Ps) 3.30 in-wg	Temperature 70 °F	Attitude 0 ft	Density 0.075 lb/ft <sup>3</sup>	Q Derate 0 cfm	P Derate 0.00 in-wg	VAV Set Point 0.00 in-wg	Date 07-21-2020
ın Táç	Flow 8633 CFM	Pressure (Ps) 3,30 in-wg	Power 7.04 hp	Static Efficience 63.8 %	Total Efficiency 69.7 %	Speed 889 rpm	Outlet Velocity 2225 fpm	Efficiency Rating FEG75	
	Impeller Dia 20.0 in	Outliet Area 3.88 ft <sup>2</sup>	Max Speed 1020 rpm	AMCA Class	Drive Belt Drive	Blades 37	P Volume 25,4 ft <sup>3</sup>	Turndown 100 %	
4.00	Pressure Power		/			/			30.0 25.0 20.0 Shaf
(bm-u) ansau 2.50 2.00 1.50 1.00 0.50 0.00 0 2500	5000	7500	10000 F	12500 lowrate (cfr		17500	20000 22		20.0 Shaft Power (hp) 10.0 5.0 0.0
0.50	5000	7500		lowrate (cfr	n)	C. MARK	20000 22	500 2500	5.0 0.0



## Options Available

Available Bores: 1: 3/16, 1: 7/16, 1: 11/16, 1: 15/16, 2: 1/4, 2: 3/16, 2: 7/16, 2: 11/16, 2: 15/16, 3, 4, 4: 1/2 and 5 inch Wheels available separately

A	В	С	E	F	G	н	្រា	K	L	M	P	S	U
38.00	32.75	14.44	24.75	1.50	1.44	16.25	22.53	22.75	24.25	15.00	35.25	2.50	2.00

Dimensions in inches



Law Industries, Inc. certifies that the H-Series 8D shown herein is licenced to bear the AMCA Seal. The ratings shown are based on test and procedures performed in accordance with AMCA Publication 211 and comply with the requirements of the AMCA certified ratings program.

Performance certified is for the installation 8: Free Inlet, Ducted Outlet, Performance ratings do not include the effects of appurtenances (accessories). Power ratings (hp or kW) do not include transmission losses.

The AMCA Certified Ratings Seal applies to air performance only

## Appendix D Stationary Noise Sample Calculations



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#### Receiver: R01 Project: 1305 Maritime Way Project Number: 21443

Time Period	Total (dBA)			
Day	48			
	5 			
Receiver Name	Receiver ID			Z
R01	R01	429096.81 m	5018163.33 m	115.15 m

Source ID	Source Name	Х	Y	Z	Refl.	Lw	L/A	Freq	Adiv	K0	Agr	Abar	Aatm	Afol	Ahous	Cmet	Dc	RL	Lr
S01	S01 - Homewood HVAC	429134.6	5018324.3	123.0	0	87	0.0	А	55.4	0.0	-3.0	13.1	0.9	0.0	0.0	0.0	0.0	0.0	21
S03	S03 - Homewood HVAC	429219.7	5018362.6	123.0	0	88	0.0	А	58.4	0.0	-3.0	10.1	0.9	0.0	0.0	0.0	0.0	0.0	21
S04	S04 - Town Place HVAC	429226.2	5018187.2	115.0	0	97	0.0	А	53.4	0.0	-3.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	46
S05	S05 - Timberwalk HVAC	429095.0	5018118.3	123.0	0	88	0.0	А	44.2	0.0	-3.0	5.7	0.2	0.0	0.0	0.0	0.0	0.0	41
S06	S06 - Timberwalk HVAC	429077.6	5018104.5	123.0	0	88	0.0	А	46.9	0.0	-3.0	7.5	0.3	0.0	0.0	0.0	0.0	0.0	36

#### Receiver: R02 Project: 1305 Maritime Way Project Number: 21443

Time Period	Total (dBA)			
Day	46			
· · · · · · · · · · · · · · · · · · ·				
Receiver Name	Receiver ID			Z
R02	R02	429079.84 m	5018200.19 m	115.15 m

Source ID	Source Name	Х	Y	Z	Refl.	Lw	L/A	Freq	Adiv	K0	Agr	Abar	Aatm	Afol	Ahous	Cmet	Dc	RL	Lr
S01	S01 - Homewood HVAC	429134.6	5018324.3	123.0	0	87	0.0	А	53.7	0.0	-3.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	36
S03	S03 - Homewood HVAC	429219.7	5018362.6	123.0	0	88	0.0	А	57.6	0.0	-3.0	0.0	0.8	0.0	0.0	0.0	0.0	0.0	32
S04	S04 - Town Place HVAC	429226.2	5018187.2	115.0	0	97	0.0	А	54.3	0.0	-3.0	0.0	0.8	0.0	0.0	0.0	0.0	0.0	45
S05	S05 - Timberwalk HVAC	429095.0	5018118.3	123.0	0	88	0.0	Α	49.4	0.0	-3.0	15.9	0.4	0.0	0.0	0.0	0.0	0.0	25
S06	S06 - Timberwalk HVAC	429077.6	5018104.5	123.0	0	88	0.0	А	50.6	0.0	-3.0	20.0	0.4	0.0	0.0	0.0	0.0	0.0	20

# Project: 1305 Maritime Way Project Number: 21443

		Point of	Reception R01	Point of Reception R02			
Source ID	Source Name	Distance to POR (m)	Sound Level at POR (dBA) Day	Distance to POR (m)	Sound Level at POR (dBA) Day		
S01	S01 - Homewood HVAC	166	21	136	36		
S02	S02 - Homewood HVAC	201	5	177	7		
S03	S03 - Homewood HVAC	234	21	214	32		
S04	S04 - Town Place HVAC	132	46	147	45		
S05	S05 - Timberwalk HVAC	46	41	84	25		
S06	S06 - Timberwalk HVAC	62	36	96	20		
Total Level	[dBA]		48		46		

# End of Report

