

March 15, 2024 Project Number: 240056

Rayan Zaher 364 Wisteria Crescent Ottawa, ON K1V 0N9 Email: <u>rayanzaher52@gmail.com</u>

Re: Hydrogeological Assessment and Terrain Analysis for Septic System Suitability Commercial Site Development (Storage and Repair Facility) 5254 Bank Street, Ottawa, Ontario

Dear Mr. Zaher:

BluMetric Environmental Inc. (BluMetric[®]) was retained to conduct a hydrogeological assessment and terrain analysis to support an application for a commercial development at 5254 Bank Street, Ottawa, Ontario. The location of the site is indicated in Figure 1. The land parcel covers an area of approximately 0.17 hectares. The site is in an area that is serviced by the Ottawa municipal water supply system. The Ottawa municipal wastewater treatment system does not extend to the area where the site is located. It is proposed that the site will be developed for commercial use and will be serviced by an onsite septic wastewater system.

1. CONTEXT

1.1 TERMS OF REFERENCE

This study was conducted with general reference to the following regulations and guidelines:

- City of Ottawa Hydrogeology and Terrain Analysis Guidelines, 2021.
- Ontario Ministry of the Environment, Conservation and Parks (MECP) Procedure D-5-4, Technical Guideline for Individual On-Site Sewage Systems, Water Quality Impact Risk Assessment (MOEE, 1996).



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www.blumetric.ca



Figure 1: Site Location

1.2 SCOPE OF WORK

The scope of this assessment was developed based on requirements of Procedure D-5-4 and Procedure D-5-5 (MOE, 1996). The scope of work included the following components:

- Desktop review of background information (water well records, geological databases, hydrology information, topography).
- Pre-consultation with Lanark County peer review representative.
- Terrain analysis based on geotechnical report by LRL Engineering (LRL).
- Predictive nitrate impact assessment based on 2024 site development concept by Unpoised Architecture and engineering site plans by LRL Engineering.



1.3 PROPOSED COMMERCIAL DEVELOPMENT

The commercial site plan concept (a storage and repair facility) was updated by Unpoised Architecture in January 2024 (see site concept architectural drawings in Attachment A) and consists of the following elements:

- Slab on grade commercial storage/repair building with three garage bays and two offices.
- Paved area for access and parking
- Nitrate reducing 'tertiary treatment' septic system with leaching bed.

2. METHODOLOGY

2.1 **PRE-CONSULTATION**

A pre-submission consultation meeting was conducted with the City of Ottawa on November 1, 2023. The City of Ottawa indicated that development of the site will be challenging as the parcel area is relatively small at 0.17 hectares.

The City indicated that nitrate reducing tertiary treatment is not a preferred option from the City's perspective, but it was determined through further discussion that nitrate attenuation assessment could potentially incorporate the use of tertiary treatment since the City has previously approved tertiary treatment systems for commercial development on existing land parcels, and that tertiary treatment systems are subject to the requirements of the Ottawa Septic System Office (OSSO) who are the approval agency.

A previous terrain analysis and private sewage disposal system impact assessment report by LRL was discussed (LRL, 2020). The City of Ottawa indicated that the LRL report does not reflect the current site development design, so a new comprehensive hydrogeological and terrain analysis report reflecting the current development design plan for the site will be required.

2.2 BACKGROUND INFORMATION REVIEW

A review of available background information was conducted including:

- MECP water well records.
- MECP permit to take water (PTTW) database.
- Topographic databases.
- The Rideau Valley Conservation Authority (RVCA) geographic information system (GIS).
- Ontario Geological Survey (OGS) online geology mapping databases.



2.3 TERRAIN ANALYSIS

A review of available information from water well records and a geotechnical investigation of the site by LRL Engineering in 2019 and 2023 (LRL. 2023) was conducted. Details of the geotechnical investigation are provided in Section 4.1.

3. SITE DESCRIPTION

3.1 LAND PARCEL

The land parcel at 5254 Bank Street has an area of 1708.73 square metres (0.17 hectares). The site will be accessed from Bank Street. A topographic plan of survey (Farley, Smith & Denis Surveying, 2022) showing existing site features is included as Attachment B. The site is currently developed as a rural residential site with a one-story residence with basement, septic bed and three outbuildings (garage and two storage sheds).

The site is within the City of Ottawa and is within the boundaries of the South Nation Conservation Authority (SNCA).

Zoning at the site is RG3[900r]-h (Rural General Industrial Zone). The parcel to the north (5224 Bank Street) is RG1[290r] (Rural General Industrial Zone). The parcel to the south and west (5304 Bank Street) is ME2 (Mineral Extraction Zone).

3.2 SURROUNDING LAND USE

Surrounding land uses within 500 m of the site include:

North:

- Bank Street.
- A campground/trailer park.
- Automotive garages.
- Rural residence.
- Undeveloped areas with trees.
- Commercial use property (former Brickyards Quarry site).



East:

- Bank Street.
- Two Quarry sites.
- Forested areas / undeveloped.
- Commercial use properties.

West:

- Lumber Yard
- Undeveloped land with some trees
- Aggregate pit (5304 Bank Street) including undeveloped land.

South:

- Bank Street
- Commercial use properties.
- Residences
- A church.
- Aggregate pit (5304 Bank Street) including undeveloped land.

3.3 TOPOGRAPHY

The land parcel is undulating with a general slope from northeast to southwest. An elevation change occurs near the middle of the site, and the eastern and western ends of the site are relatively flat. The highest elevation (115 m asl) occurs at the northeastern corner of the site. The lowest elevation (109.5 M asl) occurs at the southwestern corner of the site.

The terrain at the site was analysed using 'laser imaging, detection, and ranging' (LIDAR) data. High resolution digital elevation model (HRDEM) data was obtained from the Government of Canada Open Maps website (Canada, 2024 - CanElevation Series). Digital terrain model (DTM) data was analysed using public domain software developed by the US Army Corps of Engineers, Hydrologic Engineering Center, River Analysis System (HEC-RAS). A hill shade' terrain model was generated. Figure 2 shows a 'hill shaded' DTM image covering the site and surrounding areas.





Figure 2: Hill Shaded Digital Terrain

3.4 HYDROLOGY

Onsite drainage is by infiltration and overland flow towards a drainage ditch to the southwest. The site occurs in the Castor River Watershed which is part of the South Nation Watershed. Drainage from the site flows to the southwest towards a drainage ditch that flows southwest to a drainage ditch that flows to the south. The drainage ditches in this area follow to the south and then to the east towards an unnamed creek and drainage ditches that flow into the Castor River at a point that is approximately 7.5 km to the east of the site. Surface water flow directions in the vicinity of the site are indicated on Figure 3.





Figure 3: Surface Water Flow Directions (GeoOttawa)

The SNCA online GIS (SNCA, 2024) indicates a 'regulation boundary' associated with drainage ditches to the west of the site (Figure 4). At its closet point the boundary is approximately 230 m to the west of the western boundary of the site. The SNCA GIS indicates areas of wetland swamp and marsh as shown in Figure 4 (locations are approximate). The regulation boundary appears to be a flood boundary, but the SNCA GIS does not provide any further information.



Figure 4: SNCA Regulation Boundary



4. GEOLOGY

4.1 SURFICIAL GEOLOGY

Surficial geology information from the Ontario Geological Survey was obtained from the OGS Earth website (OGS, 2023). The data shows that the site is in an area of till (stone-poor, sandy silt to silty sand-textured) on Paleozoic terrain.

This description is generally consistent with the findings of the water well records search (sand, silt, gravel, and clay) and the geotechnical study by LRL (gravel fill over native silt and sand – see below). The well record that occurs closest to the site (well record 1502205 at 5304 Bank Street – see Attachment C) encountered 1.8 m of "boulder till" above bedrock.

A geotechnical investigation of the site was conducted by LRL Engineering in 2019 and 2023 (LRL. 2023). Eight boreholes were drilled. The locations of the boreholes are indicated in Figure 5. Geotechnical borehole logs are included in Attachment D. All of the boreholes were drilled to refusal. Borehole depths varied from 0.66 m at BH4 to 3.66 m at BH3. Groundwater was not identified at any of the borehole locations.

The general stratigraphy at the site is summarized as follows:

- Asphalt at BH3 0.05 m thick
- Topsoil 0.1 to 0.45 m
- Fill material (sand/gravel) 0.5 to 1.5 m
- At all boreholes
- Silt at BH3 2.2 m thick
- Silt and sand at BH6 2.2 m thick
- Limestone bedrock at BH2 at 0.65 m below ground surface (bgs)

One sample (BH3 silt from 2.3-2.9 m bgs) was submitted for grain size (sieve) analysis. Two samples (BH6 silt and sand from 2.3-2.9 m bgs, and BH8 fill from 0.8-1.2 m bgs) were submitted for laboratory gradation analysis. Analytical results for the samples are included in the LRL geotechnical report and show that estimates of hydraulic conductivity were 7 x 10⁻⁵ m/sec, which is within in the typical range for these materials (Freeze and Cherry, 1979).





Figure 5: Geotechnical Borehole Locations

The geotechnical report by LRL indicates that excavations for building footings are not expected to exceed 2.4 m bgs, and that seepage of overburden groundwater is expected to minimal if there is any at all. BluMetric agrees with this interpretation as there is no evidence to suggest that an overburden water table exists at the site. Groundwater seepage into excavations is expected to be limited to water that is draining through the overburden unit due to any recent precipitation and/or snow melt. See Section 4.3 for a detailed description of the site hydrogeology.

4.2 BEDROCK GEOLOGY

Geological mapping information from the Ontario Geological Survey (OGS) Earth website (OGS, 2021) shows that the site is located in an area where the Oxford Formation is the uppermost bedrock unit. The Oxford Formation is part of the Beekmantown Group, and is described as dolostone, with minor shale and sandstone.



4.3 HYDROGEOLOGY

An unconfined water table was not identified by the eight geotechnical boreholes installed by LRL (LRL, 2023). Drainage within the overburden unit is expected to be influenced by topography and is inferred to have a southwesterly component (towards a drainage ditch that occurs approximately 250 m to the southwest of the site).

The highest water table elevation in the area to the southwest of the site is expected to have an elevation of approximately 108.6 m asl (based on DTM elevation at the ditch to southwest of site), which is approximately 1.4 m below the ground surface elevation at LRL borehole BH8. BH8 encountered refusal (assumed to bedrock) at 1.27 m below ground surface and no groundwater was identified, so it assumed that the water table at the site occurs within the bedrock unit.

The primary water supply aquifer in the vicinity of the site occurs within the horizontally bedded Ordovician sedimentary bedrock. The bedrock aquifer has water bearing fracture zones (i.e. horizontal bedding plane fractures) that occur between sedimentary layers of bedrock. Permeability within these strata is controlled by fractures. The primary porosity (i.e. the 'primary fracture network') is associated with horizontal bedding plane fracturing.

Overburden groundwater drainage is inferred to be to the southwest based on topography. The direction of regional groundwater flow in bedrock at the site is inferred to be to the to the north towards the Ottawa River.

Information from the Ontario Source Water Protection Atlas, (MECP, 2023) website indicates that the site is not within a wellhead protection area (WHPA) or intake protection zone (IPZ), or a significant groundwater recharge area (SGRA). A highly vulnerable aquifer occurs beneath the site (score of 6).

4.3.1 Water Well Records

18 water well records that occur within 50 m of the site were obtained from the MECP Water Well Information System (WWIS - MECP, 2023). The well record locations are shown on Figure 6. Please note that the well record locations are based on MECP database coordinates and may be subject to varying degrees of error. A summary of relevant information from the water well records is provided in Table 1. All of the records that were reviewed are for wells completed in the bedrock aquifer. The wells range in depth from 11 to 65 m and have an average depth of 31 m.



No nearby downgradient wells were identified. It is assumed that the water supply wells in the area were decommissioned when the municipal water supply system was installed.



Figure 6: Water Well Records



MECP W	ATER WI	ELL RECOR	DS SUMMARY								
Well Record ID	Year Drilled	Depth to Bedrock (m)	Overburden Material	Bedrock Material	Total Depth (m)	Casing Depth (m)	Depth to Water Bearing Zone(s) (m)	Static Water Level (m)	Drawdown after Drillers Pumping Test (m)	Recommended pumping rate (L/min)	Comments
1502270	1954			Sandstone	35.1	21.3	35.1	9.1	9.1		Clear
1502193	1955	1.8	Clay	Limestone	32.9	4.3	32.9	7.3	11.0		Clear
1502271	1955	8.2	Sand	Grey Limestone	29.0	8.2	27.1	3.0	24.4		Clear
1502205	1956	1.8	Boulder till	Sandstone	49.7	4.9	47.2	2.4	12.8	49	Clear
1502203	1956	1.8	Clay	Limestone	14.6	2.7	14.6	2.4	2.4	11	Clear
1502268	1961			Sandstone	51.8		28.0 / 44.5	15.2		15	Fresh
1502272	1958	3.7	Clay	Limestone	15.2	6.4	15.2	2.4	4.3		Clear
1502204	1959	2.4	Gravel	Limestone	15.2	3.0	15.2	2.4	6.1	19	Clear
1502273	1960	4.3	Loam / gravel	Limestone	17.7	4.9	17.7	2.7	4.3	8	Clear
1502274	1960	1.2	Clay	Grey Rock	11.0	1.2	11.0	3.0	7.9	15	Clear
1502275	1961	0.0		Grey limestone	30.5	3.0	30.5	2.4	2.4	15	Clear
1502276	1961	0.0		Limestone / sandstone	46.3	6.1	21.3 / 41.1	15.2	28.7	38	Cloudy
1502267	1964	1.5	Sandy loam	Limestone / sandstone	65.2	3.4	29.0 / 49.4 / 57.3 / 65.2	21.3	24.4	38	Clear
1502277	1964	1.5	Topsoil / sand	Limestone	46.3	10.4	46.3	6.7	18.3	8	Cloudy
1502284	1965	1.2	Clay and loam	Limestone	14.6	3.7	14.6	1.5	1.5	15	Clear
1510284	1969	4.3	Sand	Blue limestone	14.6	5.5	14.6	3.0	3.0	19	Fresh
1516460	1978	1.5	Sand	Grey limestone	41.2	7.3	39.0	3.0	15.2	19	Clear
1516981	1979	2.4	Sand	Limestone	29.9	6.7	23 / 29.9	2.4	16.8	45	Cloudy

Table 1: Water Well Records Summary

4.3.2 Water Taking Permits

A review of the MECP Permit to Take Water (PTTW) database was carried out within a 1 km radius of the site. PTTW information was obtained from the MECP interactive GIS system (MECP, 2023). The following water taking permits were identified:

- 6400-BLWMAC, Pomerleau Sand & Gravel Inc, for dewatering of pits and quarries. Taking of up to 9,000,000 L/day of surface and groundwater.
- 3754-C2GLXC, R.W. Tomlinson Limited, for dewatering and construction. Taking of up to 19,920,000 L/day of groundwater.

These water taking activities are not expected to have any impact on the subject site which is serviced by the Ottawa municipal water supply system.

4.3.3 Hydrogeological Sensitivity

The site is not within an area mapped as 'known, potential, or inferred karst' as determined by the OGS Karst mapping layer (OGS, 2023).

The water well records show that the overburden thickness within 500 m of the subject property varies from 0 to 8.2 m and has an average thickness of 2.4 m. The overburden material is primarily described in well records as sand, gravel and clay. LRL geotechnical boreholes varied in depth from 0.2 to 0.72 m bgs and the material encountered was mostly sand gravel fill (with native silt and sand at two locations).



Based on the terrain analysis findings, the subject site is hydrogeologically sensitive due to thin soils in some locations.

4.3.4 Potential Sources of Contamination

The following potential sources of contamination were identified:

- A Phase 1 ESA by EXP Services Inc. (EXP) identified two liquid fuel storage tanks at the site so there is a potential for some localised hydrocarbon contamination.
- Application of road salt along Bank Street is expected to have caused some limited impacts to the areas immediately bordering the roads and ditches. No onsite impact is expected as a result of road salt application activities.
- The site is in an area of commercial development including automotive garages and a wood treatment facility. The garage at 5217 Bank Street (Wallace Service Centre at 5217 Bank Street) and the wood treatment facility (Grandore Lumber at 5224 Bank Street) are directly upgradient of the site. These operations are discussed in detail a Phase One ESA by EXP (EXP, 2023).
- Neighbouring septic systems have a potential to cause some limited impacts to bedrock groundwater quality.

The site is serviced by the Ottawa municipal water supply system so potential impacts to the bedrock aquifer will not affect the potable water supply at the site.

5. DEVELOPMENT CONSIDERATIONS

5.1 SEPTIC SYSTEM SUITABILITY

MECP's Procedure D-5-4 (MOEE, 1996) provides a methodology for assessing the risks associated with individual onsite sewage systems. Developments of land parcels which average 1 hectare may not require a detailed hydrogeological assessment if it can be demonstrated that the area is not hydrogeologically sensitive. The site covers an area of 0.17 hectares, so a predictive nitrate impact assessment was completed.

The assessment is based on a reasonable estimate of groundwater recharge by infiltration from precipitation. The method relies on estimates of evaporation, evapotranspiration, infiltration and runoff and inputs regarding surficial soil type, vegetative ground cover and topography. A nitrate effluent concentration of 40 mg/L is used as per MECP Procedure D-5-4. Further details regarding the septic design flow for the proposed development are provided in Section 5.2.



A septic design flow rate of 670 L/day was used based on input from Absolute Drafting and Design Inc.). The septic design flow rate is based on Ontario Building Code (OBC, 2012) sewage system design flow elements.

A mean annual precipitation value (net of evaporation and evapotranspiration processes) of 929.8 mm/year was used (Environment Canada, Climate Normals, Ottawa Airport). An estimation of infiltration was calculated based on site specific information and the infiltration factors provided in the document MOEE Hydrogeological Technical Information Requirements for Land Development Applications (MOEE, 1995). A value for 'water surplus' was obtained from Environment Canada (see Attachment E). It should be noted that the Environment Canada calculations use a lower precipitation value for Ottawa (911 mm/year) so the value used for water surplus is conservative.

A nitrate effluent concentration of 20 mg/L can be used as the site design specifies that the onsite septic sewage system will incorporate a proprietary 'tertiary' pre-treatment component to ensure that the concentration of nitrates can be reduced by at least 50%. It is expected that the Ottawa Septic System Office (OSSO) will provide conditions as part of an approval for such a system addressing concerns about ongoing inspection and maintenance to ensure long term efficient performance.

The predictive nitrate impact assessment calculations are provided in Attachment E. The assessment shows that the nitrate impact for the proposed development will be 9.9 mg/L, which is a significant reduction compared to existing conditions.

5.2 SEWAGE SYSTEM DESIGN

Site development will include the installation of a nitrate reducing tertiary treatment system to reduce nitrate loading to the site. These systems employ various technologies from porous bacterial enriched foam and denitrifying lignocellulose mediums to microbial electrochemical septic tanks (MESTs). Tertiary treatment systems significantly reduce the size of the septic bed footprint. They are classified as Class 4 sewage systems and are therefore held to the same building code in the OBC (OBC, 2012). The following are examples of certified tertiary pre-treatments systems that may be suitable for the site:

- Waterloo Biofilter systems are manufactured in Canada and are certified by the National Sanitation Foundation (NSF).
- Eljen GSF systems are manufactured in the U.S. and are NSF certified.
- Premier Tech Ecoflo systems are manufactured in the U.S. and are NSF certified.



The site owner is advised to have the on-site wastewater system inspected regularly and to follow a wastewater system management program to minimize the risk of failure and impact to the groundwater. Best management practices are recommended such as regular pumping of the septic system, cursory inspection of break-out, and consideration as to what materials are being discharged to the septic system. It is recommended that homeowners take all reasonable measures to conserve water and promote infiltration of water into the subsurface within the site boundaries.

Civil Engineering plans for the site by LRL show the location of the septic leaching bed, and are included as Attachment F. A septic system design drawing by Absolute Drafting and Design Ltd. is included as Attachment G. A product brochure for the Eljen system that is indicated in the septic design drawing is included as Attachment H.

6. CONCLUSIONS

- The site is located in an area dominated by commercial / industrial development including automotive repair shops and aggregate extraction sites. The downgradient parcel is occupied by an aggregate pit including undeveloped land at the eastern end of the parcel.
- A geotechnical investigation by LRL (2023) did not identify an unconfined water table at the site. Drainage within the overburden unit is expected to be influenced by topography and is inferred to be to the southwest towards a drainage ditch that occurs approximately 250 m to the southwest of the site).
- Groundwater is not used as a potable water supply in the area. The site and surrounding properties are serviced by the Ottawa municipal water supply system.
- Site development is expected to include the installation of a nitrate reducing tertiary treatment system in order to reduce nitrate loading. A nitrate impact assessment was completed which shows that nitrate concentrations from treated septic system effluent will be acceptable.
- The site is suitable for commercial development based on servicing by an individual onsite septic wastewater treatment system incorporating nitrate reducing tertiary treatment technology.
- Commercial development will not cause an adverse effect to the environment and neighbouring properties.



7. RECOMMENDATIONS

- A site development design should include wastewater treatment that includes nitrate reducing technology (tertiary treatment) to ensure nitrate concentrations in effluent are maintained within acceptable levels.
- The existing septic system and leaching bed at the site should be decommissioned.
- If a well is identified during site preparation it should be decommissioned according to O.Reg. 903 requirements.

8. LIMITATIONS

The conclusions presented in this report represent our professional opinion, in light of the terms of reference, scope of work, and the limiting conditions noted herein.

The findings presented in this report are based on conditions observed at the specified dates and locations, the analysis of samples for the specified parameters, and information obtained for this project. Unless otherwise stated, the findings cannot be extended to previous or future site conditions, locations that were not investigated directly, or types of analysis not performed.

BluMetric makes no warranty as to the accuracy or completeness of the information provided by others, or of conclusions and recommendations predicated on the accuracy of that information. Nothing in this report is intended to constitute or provide a legal opinion.

This report describes the site conditions and observations made by the BluMetric team at the time of the site investigation and have been prepared solely for the use of the client. No other party may use or rely upon the above-captioned report or portion thereof without the express written consent of BluMetric. BluMetric will consent to any reasonable request to approve the use of this report by other parties as "Approved Users".



In summary, it is BluMetric's professional opinion that this site is suitable for the proposed commercial development. We trust that this assessment satisfies local requirements. If you have any questions, please do not hesitate to contact the undersigned.

Respectfully submitted, BluMetric Environmental Inc.

Russell Chown, B.Sc., P.Geo. Senior Hydrogeologist

Encl.

Ref: Zaher Terrain-Hydrog 5254 Bank St - FINAL - 15mar24.docx



9. **REFERENCES**

Absolute Drafting and Design Inc., 2024. Septic Location and Details, Warehouse / Storage Facility Drawing, 5254 Bank Street, Ottawa.

City of Ottawa, 2021. Hydrogeological and Terrain Analysis Guidelines.

- City of Ottawa, 2024. GeoOttawa (online interactive map tool / GIS portal) at: <u>https://maps.ottawa.ca/geoOttawa/</u>
- Environment Canada, 2024. Environment and Natural Resources, Climate Normals & Averages at: <u>https://climate.weather.gc.ca/climate_normals/</u>
- EXP Services Inc., 2023. Phase One Environmental Site Assessment, 5254 Bank Street, Ottawa, Ontario.
- Freeze, R.A. and Cherry, J.A., 1979. Groundwater. Prentice-Hall, Englewood Cliffs, NJ.
- Government of Canada, 2024. Canada Open Maps, High Resolution Digital Elevation Model (HRDEM), CanElevation Series at: <u>Open Maps Data Viewer (canada.ca)</u>
- Farley, Smith & Denis Surveying Ltd., 2022. Topographic Plan of Survey, Part of Lot 28, Concession 4 (Rideau Front), Geographic Township of Gloucester, City of Ottawa.
- LRL Engineering, 2020. Terrain Analysis and Private Sewage Disposal System Impact Assessment, Land Rezoning Application, 5254 Bank Street, Ottawa, Ontario.
- LRL Engineering, 2023. Geotechnical Investigation, Proposed Automotive Dealership and Body Shop, 5254 Bank Street, Ottawa, Ontario.
- LRL Engineering, 2024. Site Plan engineering drawings (2024 dated June 2022).
- Ontario Building Code (OBC), 2012 as amended. O. Reg. 332/12: Building Code under Building Code Act, 1992, S.O. 1992.

Ontario GeoHub, 2024. Ontario Watershed Boundaries (OWB) GIS portal at: <u>https://geohub.lio.gov.on.ca/maps/mnrf::ontario-watershed-boundaries-owb/</u>



Ontario Geological Survey (OGS), OGS Earth website, 2024. Various authors. <u>https://www.geologyontario.mndm.gov.on.ca/ogsearth.html</u>

- Ontario Ministry of Environment Conservation and Parks (MECP), 2024. Water Well Information System (WWIS) online GIS map. <u>https://www.ontario.ca/page/map-well-records</u>
- Ontario Ministry of Environment Conservation and Parks (MECP), 2023. Permits to Take Water (PTTW) online GIS map. <u>https://www.ontario.ca/page/map-permits-take-water</u>
- Ontario Ministry of Environment and Energy (MOEE), 1996. Procedure D-5-4, Technical Guideline for Individual On-Site Sewage Systems: Water Quality Impact Risk Assessment, August 1996 (revised).
- Ontario Ministry of Environment and Energy (MOEE), 1995. Hydrogeological Technical Information Requirements for Land Development Applications.
- Ontario Ministry of Environment Conservation and Parks (MECP), 2023. Ontario Source Protection Information Atlas. At: https://www.lioapplications.lrc.gov.on.ca/SourceWaterProtection/index.html
- South Nation Conservation Authority, 2024. SNC Public Geoportal at: <u>https://camaps.maps.arcgis.com/apps/webappviewer/index.htm</u>
- Unpoised Architecture, 2024. Storage and Repair Facility, 2024 Concept Design and Site Plan (21018-Concept_revA-2024-01-26).



ATTACHMENT A

Architectural Concept Plan



ZONING REQUIREMENTS: RG3 [900r]-h - Rural Commercial Industrial (schedule 219 and 220) + BUILDING INFORMATION

PARKING PROVISIONS (AREA D)321 sq.m service and repair shop = 11 spaces (3.4 spaces / 100 sq.m)Required: 1216 sq.m office = 1 space (2.4 spaces / 100 sq.m)	Provided 12 (6 exterior + 6 inside bays)	LOT AREA	18,342 sq.ft (1,704 sq.m)
BICYCLE PARKING PROVISIONS Required: 1 / 1500 sq.m @ 552 sq.m = 0		GROSS AREA	4,010 sq.ft (373 sq.m)
	Provided 0		2,961 sq.ft (275 sq.m)
MINIMUM FRONT YARD SETBACK Required: 15m (49'-3")	Provided 1.02 m (3'-4")	GROSS AREA building code definition	2,961 sq.ft (275 sq.m) - does not include mezzzanine
MINIMUM NORTH NTERIOR SIDE YARD SETBACK Required: 3m (9'-11") from RG ZONE	Provided 13.41 m (44'-0")	BUILDING HEIGHT	1 storey (mezzanine not included as storey)
MINIMUM SOUTH INTERIOR SIDE YARD SETBACK Required: 8m (26'-3") from ME2 ZONE	Provided 0.61 m (2'-0")	FACING STREET	1
REAR YARD SETBACK Required: 15m (49'-3")	Provided 38.30 m (125'-8")	OCCUPANCY TYPE	F2 - medium hazard industrial
	Provided 8.23 m (27'-0")	BUILDING FIRE SAFETY	Part 3 - 3.2.2.71
	Provided 16 %	PERMITTED CONSTRUCTION	Combustible or Non - Combustible





LEGEND

LC - LIGHT UNDER CANOPY	DP - DEPRESSED CURB
LW - LIGHT WALL MOUNT	WB - IN-GROUND WASTE BIN
	CU - PRECAST CONCRETE CURB STOP



DETAIL FOR IN-GROUND WASTE BIN

- DEPRESSED CURB **/B** - IN-GROUND WASTE BIN - PRECAST CONCRETE CURB STOP

^{owner} Rayan Zaher 364 Wisteria Crescent Ottawa ON

architect

unPoised Architecture INC 5-16 Sweetland Avenue Ottawa ON

unPoised Architecture INC





revisions	date
XXXXX XXXXX	XXXXX
XXXXX XXXXX	XXXXX
PROGRESS REVIEW	2023-12-20
SPC SUBMISSION	2023-09-14
PROGRESS REVIEW	2022-12-15

STORAGE and REPAIR FACILITY

project title

5254 Bank Street, Ottawa ON

drawing title SITE PLAN and

ZONING

sheet number

A01



FIRST FLOOR PLAN



MEZZANINE PLAN

owner Rayan Zaher 364 Wisteria Crescent Ottawa ON architect unPoised Architecture INC 5-16 Sweetland Avenue Ottawa ON unPoised Architecture INC (\bigwedge) project north true north

revisions	date
XXXXX XXXXX	XXXXX
PROGRESS REVIEW	2023-12-20
project title	

STORAGE and REPAIR FACILITY

5254 Bank Street, Ottawa ON

drawing title FLOOR PLANS

sheet number

A02



NORTH ELEVATION



SOUTH ELEVATION



EAST ELEVATION



WEST ELEVATION



sheet number

drawing title ELEVATIONS

5254 Bank Street, Ottawa ON

STORAGE and REPAIR FACILITY

revisions	date
XXXXX XXXXX	XXXXX
XXXXX XXXXX	XXXXX
XXXXX XXXXX	XXXXX
PROGRESS REVIEW	2023-12-20
SPC SUBMISSION	2023-09-14

revisions

project title



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^{owner} Rayan Zaher 364 Wisteria Crescent Ottawa ON

architect unPoised Architecture INC 5-16 Sweetland Avenue Ottawa ON

unPoised Architecture INC

ATTACHMENT B

Survey Plan





ATTACHMENT C

Well Records



	316/52		in the second states and a second states and the second states and	n - mini	
1502205 -	5304 Bank St	reet	¥1.04.0.171		
$M 18^{2} 45477$	OE	17 de	🖌 e 👘 SaAlije 🕰	15 N	1º 2205
9 R 5011505	ON				\wedge
		ONTAF	۱۰		4 /
Piele 05/01	The Wat	ter-well Dril	lers Act, 1954	na internet de la companya de	
Sm 12 Rst 1 1 1 1 1	D	epartment o	f Mines		
Con IV T	X7 ator	177 01	1 Recor	4	
10+ ZP	v uler	- 44 61	I Mecor	CL.	
County or Territorial District	arleton	Towns	hip, Village, Town or	CityGloucest	.er
Con \$48F.Lot \$F 2 8	Street and N	lumber (if i	n Village, Town or (City)	••••••
OwnerStLawr.encaRenda	ring.Co.L	tā	AddressSouthG	loucester	••••••
Date completedI4.	Jung				
(day)	((Jear)			
Pipe and Casing	Record			Pumping Test	
Casing diameter(s) 51n			Static level	t	•••••
Length(s)			Pumping rate	800 gph	
Type of screen			Pumping level	42 ft	
Length of screen	·····		Duration of test		I hr
Well Log				Water Record	
<u></u>		1	Depth(s)		Kind of water
Overburden and Bedrock Record	From ft.	To ft.	at which water (s)	No. of feet water rises	(fresh, salty, or sulphur)
			Iouna		
Boulder Till	0	6			
Sandstone	66	<u> </u>	155 5±	<u>I46a</u>	fresh
		_		_	
		_			
		_		_	
		_			_
	-	-			
For what nurnage (s) is the water	to be used?	I			
Domestic Cor	np>hy	2.0.1.2.0	CONY L	ocation of Well	f well from
Is water clear or cloudy?Cla	a r		road and lot lin	ne. Indicate north	n by arrow .
Is well on upland, in valley, or on	hillside?			elim i to	•
Hillside			7	1. 19	J A
Drilling firmR.HCasselma	n		J. L	H zi	IWAT Y
Address Williams.burg	••••••		3 4	HNO JIG	t'
None of Dallas Phillip Co	sselm an		No.L.	A K T	
Address Williamsburg O	ntario		1 E		
Auuress	TR R IST. (\$ 2				TP.
Licence NumberIO25			CON Y		
I certify that the	foregoing				
statements of fact	are true.				
Phil	0 1	1			
	- Uannav	man			I
Date.June14/55 /////////	lignature of Licens	man			

316/52 J. GROUND WATER BRANCH 1502268 - 5227 Bank Street UTM 118Z 454900E DECT 5121410 Ontario Water Resources Commission Act ONTARIO WATER RECORDRESOURCES COMMISSION WELL Elev. 3191 ER Basin S. (day Lot. Date completed Con. R H tawa/ ddress **Casing and Screen Record Pumping Test** 41 50 Inside diameter of casing..... Static level Total length of casing none Test-pumping rate G.P.M | 0 5 Pumping level Type of screen Duration of test pumping Length of screen..... Water clear or cloudy at end of test Clear Depth to top of screen. Diameter of finished hole $3\frac{3}{4}$ Recommended pumping rate 4 G.P.M. with pump setting of 160 feet below ground surface Water Record Well Log Kind of water Depth(s) at which water(s) found From To ft. (fresh, salty, sulphur) Overburden and Bedrock Record ft. delle 63 0 92 31 146 Location of Well For what purpose(s) is the water to be used? In diagram below show distances of well from road and lot line. In the north by arrow ann Is well on upland, in valley, or on hillside? Drilling or Boring Firm Anston Ons Address. ma Licence Number 240 Name of Driller or Borer DCC Address Date South Dlouester Form 7 OWRC COPY C55.53

ATTACHMENT D

Geotechnical Borehole Logs (LRL)



Borehole Log: BH1



LRJ

Project No.: 190271

Client: Holzman Consultants Inc.

Date: October 8, 2019

Field Personnel: BJ

Location: 5254 Bank Street, Ottawa ON

Driller: CCC Geotech and Enviro Drilling Ltd. Drilling Equipment: Truck Mount CME 55

Drilling Method: HSA

SUE		SA	MP	LE DA	TΑ				4					
Depth	Soil Description	Elev./Depth(m)	Lithology	Type	Sample Number	N or RQD	Recovery (%)	× 50 \$ 0(E 20	(kPa 100 1 6 PT N V Blows/0 40 6	ength) × 50 200 /alue .3 m)° 50 80	v (%) v 25 50 75 Liquid Limit □ (%) □ 25 50 75			Water Level (Standpipe or Open Borehole)
o ft m	Ground Surface	110.17												
	Topsoil- sandy, about 450 mm thick.	0.00 109.72 0.45	\$\\\\		SS1	7	42	φ ⁷						-
	compact.		\otimes											
		108.80			SS2	15	75	15			.49			-
5	End of Borehole	1.37												
														-
														-
														-
8-														_
-														-
9-														
10 - 3														
														-
														-
12														
13 - 4														-
														-
14														
														_
15														-
16														
5														_
Eastin	g: 454743 m	No	orthin	g: 50	15270 r	n			NOTE	S: Boreh	ole ter	minate	ed after p	actical auger refusal.
Site Da	Site Datum: Site Benchmark - 2 nails in utility pole - 116.310 m													
Groun	dsurface Elevation: 110.170 m	Тс	op of F	Riser	Elev.:	N/A								
Hole D	Groundsurface Elevation: 110.170 m Top of Riser Elev.: N/A Hole Diameter: 200 mm													

Borehole Log: BH2



LRJ

Project No.: 190271

Client: Holzman Consultants Inc.

Date: October 8, 2019

Field Personnel: BJ

Location: 5254 Bank Street, Ottawa ON

Driller: CCC Geotech and Enviro Drilling Ltd. Drilling Equipment: Truck Mount CME 55

Drilling Method: HSA

SUE	BSURFACE PROFILE		SA	MP	LE DA	TA			04	41.		- • 6		
Depth	Soil Description		Lithology	Type	Sample Number	N or RQD	Recovery (%)	× 50 •(E 20	× (kPa) × 50 100 150 200 SPT N Value °(Blows/0,3 m)° 20 40 60 80		L 2: 2:	(% 5 5 iquid (% 5 5	6) ⊽ 0 75 1 Limit 6) □ 0 75	Water Level (Standpipe or Open Borehole)
oft mo	Ground Surface	110.95												
	Topsoil- sandy, about 450 mm thick.	0.00	2)	V	991	8	33	<u>08</u>			<mark>_</mark> 12			
2	FILL- sand, brown, moist, loose.	110.30												
3	BEDROCK- limestone, weathered at surface, grey.	0.65		Y	SS2	80+	100)+		_13			
	End of Borehole	109.88 1.07						000						
5														
7														
9 - - 10 - - 3														
12														
15														
Eastin Site Da	Site Datum: Site Benchmark - 2 nails in utility pole - 116.310 m										ole ter	minat	ed after	practical auger refusal.
Groundsurface Elevation: 110.950 m Top of Riser Elev.: N/A														
Hole D	Diameter: 200 mm													





LRJ

Project No.: 190271

Client: Holzman Consultants Inc.

Date: October 8, 2019

Field Personnel: BJ

Location: 5254 Bank Street, Ottawa ON

Driller: CCC Geotech and Enviro Drilling Ltd. Drilling Equipment: Truck Mount CME 55

Mount CME 55

Drilling Method: HSA

SUBSURFACE PROFILE			SA	MPI		TA			Water Content				
Depth	Soil Description	Elev./Depth(m)	Lithology	Type	Sample Number	N or RQD	Recovery (%)	Snear Strengtn × (kPa) × 50 100 150 200 SPT N Value ° ° (Blows/0.3 m)° 20 40 60 80	Water Content ♥ (%) ♥ 25 50 75 Liquid Limit ● (%) ● 25 50 75	Water Level (Standpipe or Open Borehole)			
$0 \frac{\text{ft m}}{0}$	Ground Surface	113.65											
	Asphalt - about 50 mm thick. FILL- sand, some gravel, brown, moist, loose to compact.	. 0.00	\bigotimes		SS1	6	17	¢ ⁶	√5				
-++		112.20			SS2	12	8	12	√4				
5 1 6 1 2 7 7	SILT- some sand, trace gravel sized stone, brown, moist, dense to very dense.	1.45	**************************************		SS3	8	17		10				
⁸ 9			* * * * * * * * * * * * * * * * * * *		SS4	68	85	¢68	10				
10		109.99	**************************************		SS5	48	75	48	⊽11				
$ \begin{array}{c} 12 \\ - \\ 13 \\ - \\ 14 \\ 14 \\ 15 \\ - \\ 16 \\ - \\ 16 \\ - \\ 12 \\ - \\ 12 \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ -$	End of Borehole	3.66											
Easung: 494776 m Norming: 5015290 m NOTES: Borenoie terminated after practical auge Site Datum: Site Benchmark - 2 nails in utility pole - 116.310 m Groundsurface Elevation: 113.650 m Top of Riser Elev.: N/A Hole Diameter: 200 mm Hole Diameter: 200 mm Hole Diameter: 200 mm										actical auger refusal.			

Borehole Log: BH4



LR

Project No.: 190271

Client: Holzman Consultants Inc.

Date: October 8, 2019

Location: 5254 Bank Street, Ottawa ON

Field Personnel: BJ

Driller: CCC Geotech and Enviro Drilling Ltd. Drilling Equipment: Truck Mount CME 55

Drilling Method: HSA

SUE	BSURFACE PROFILE		SA	MPI	LE DA	TA		0	04		- W-	···· • • · ·		
Depth	Soil Description or RQD or RQD or RQD		× (kPa) × 50 100 150 200 SPT N Value •(Blows/0.3 m)° 20 40 60 80			vva 25 Li 25	(%) 50 quid Li (%) 50	75 mit 75	Water Level (Standpipe or Open Borehole)					
ftm	Ground Surface	114 14		-										
a 0 1 1 1 2 1 1 1 2 1 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 1 2 1 1 1 2 1 1 1 2 1 1 1 2 1 1 1 2 1 1 1 2 1 1 1 2 1 1 1 2 1 1 1 2 1 1 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1	Ground Surface Topsoil- sandy, about 100 mm thick. FILL- sand, some gravel, brown, moist, compact. BEDROCK- limestone, weathered at surface, grey. End of Borehole	2 114.14 0.00 0.10 113.73 0.41 113.48 0.66		TYF	SS1	44	85		40 6		25 v ¹¹			
11 12 12 13 13 14 14 15 16 5 Eastin Site Di Groun	g: 454795 m atum: Site Benchmark - 2 nails in u dsurface Elevation: 114.140 m	Nc utility pc To	porthing ble - 11 pp of F	g: 50 6.31 Riser	15306 r 0 m Elev. :	m N/A			NOTE	<u>S:</u> Boreh	ole term	ninated	after pr	actical auger refusal.
Hole D	Hole Diameter: 200 mm													





LRJ

Project No.: 190271

Client: Holzman Consultants Inc.

Date: October 8, 2019

Field Personnel: BJ

Location: 5254 Bank Street, Ottawa ON

Driller: CCC Geotech and Enviro Drilling Ltd. Drilling Equipment: Truck Mount CME 55

Mount CME 55

Drilling Method: HSA

SUE	SAMPLE DATA							hoor Strongth Water				0			
Depth	Soil Description	Elev./Depth(m)	Lithology	Type	Sample Number	N or RQD	Recovery (%)	Sn × 50 S •(E 20	(kPa 100 1 6 PT N V Blows/0 40 6	engtn 50 200 /alue .3 m)° 50 80	₩ 2 L 2 2	ater (% 5 5 iquid 5 5	6) 75 0 75 1 Limit 6) 6	nt ⊽ 5 : 	Water Level (Standpipe or Open Borehole)
o ft m	Ground Surface	114.04													
-	Topsoil- sandy, about 250	0.00	{												
		113.79	\approx		004	10	22	_18	3		_12				
	FILL- sand, some gravel,	0.25	\otimes		551	18	33	Y			×				
	brown, moist, compact.		\otimes												
2			\bigotimes					1							
			\otimes												
3			\otimes					<mark>/</mark> 16	5		1 2				
			\otimes		SS2	16	75								
4			\otimes												
-		112.62	∞												
5	End of Borehole	1.42													
6															
2															
7-															
-															
8_															
9_															
10 - 3															
11															
12															
13															
15															
Image: Image: A54809 m Image: Northing: 5015303 m NOTES: Borehole te											l ole ter	minat	ted afte	er pra	ctical auger refusal.
Sito D	atum: Site Benchmark 2 noile in								0						
Group	Groundsurface Elevation: 114 040 m Top of Riser Elev : N/A														
Hole D	liameter: 200 mm	IC	יו ט קי	viset.	LIEV.	IN/ <i>F</i> 1									



Project No.: 220536

Borehole Log: BH6

Project: Proposed Industrial Service/Repair Building

Client: Unpoised Architecture Inc.

Date: June 9, 2023

Field Personnel: SV

Driller: CCC Geotech and Enviro Drilling Ltd. Drilling Equipment: Truck Mount CME 55 Drilling Method: Hollow Stem Auger

Location: 5254 Bank Street, Ottawa ON

SUE	SURFACE PROFILE		SA	MPLE	DATA		9	hoar Stre	nath	Wa	tor Con	tont	
Depth	Soil Description	Elev./Depth (m)	Type	Sample Number	N or RQD	Recovery (%)	× 50 • (20	(kPa) 15 SPT N Va Blows/0.3	alue 3 m) ∘ 2 80	v 25 	(%) 50 quid Li (%) 50	75 75 nit 75	Monitoring Well Details
0 ft m	Ground Surface	113.01											_
1 1 2	FILL sand and gravel, brown, loose, moist.	112 32		SS1	8	50	8 Ø			5 ▽			_
3 	SILT and SAND trace clay, greyish brown, loose to very loose, moist.	0.69	X	SS2	1	25				12			-
			X	SS3	4	50	4			10 ⊽			-
7			Y	SS4	11	50	11			15 ⊽			-
9		110.17											_
10 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	End of Borehole	2.84											
Eastin Site Da	g: 454770 m atum: Site Benchmark - 2 nails in	N e utility p	orthing	j: 501528 16.310 m	83 m 1			NOTES: Borehol	e termina	ated afte	er practi	cal aug	er refusal.
Groun Hole D	dsurface Elevation: 113.011 m iameter: 200 mm	To M	op of R onitori	iser Ele [,] ng Well	v.: NA Diamete	er: N/A							



Project No.: 220536

Borehole Log: BH7

Project: Proposed Industrial Service/Repair Building

Location: 5254 Bank Street, Ottawa ON

Client: Unpoised Architecture Inc.

 LRJ
 Date: June 9, 2023
 Field Perform

 Driller: CCC Geotech and Enviro Drilling Ltd.
 Drilling Equipment: Truck Mount CME 55

Field Personnel: SV

Drilling Method: Hollow Stem Auger

SUE	SUBSURFACE PROFILE SAMPLE DATA		Shoor Strongth		Watan Cantant		- 4						
		ţ		umber		(%)	× 5	onear S (kF 0	Pa) × 150	vvate ⊽ 25	(%) 50 7	nt ⊽ 5	Monitoring Well
Depth	Soil Description	Elev./Dept (m)	Type	Sample N	N or RQD	Recovery	° 2	SPT N (Blows) 0 40	Value /0.3 m) ○ 60 80	Liq 25	uid Limi (%) 50 7	t 5	Details
0 0	Ground Surface	110.94											
	FILL MATERIAL sand and gravel, brown, compact, moist.	0.00		SS1	11	50	-11 0			8 ▽			
3	Food of Developed	110.08											
4 <u>-</u> 1	End of Borehole												
5													
6 													
7													
8													
9 													
11													
12													
13 4													
14													
17 – 5													
18													
19													
 Eastin	g: 454771 m	N	orthing	j: 50152	80 m			NOTE	<u>ES</u> :	ated after	practical	augo	r refusal
Site Da	atum: Site Benchmark - 2 nails in	utility p	ole - 1′	16.310 m	1			Dorei		ateu alter	practical	auge	สาธิเนอิ่สไ.
Groun	dsurface Elevation: 110.94 m	Тс	op of R	iser Ele	v .: NA								
Hole D	iameter: 200 mm	M	onitori	ng Well	Diamete	e r: N/A							



Project No.: 220536

Borehole Log: BH8

Project: Proposed Industrial Service/Repair Building

Location: 5254 Bank Street, Ottawa ON

Client: Unpoised Architecture Inc.

Date: June 9, 2023

Field Personnel: SV

Driller: CCC Geotech and Enviro Drilling Ltd. Drilling Equipment: Truck Mount CME 55

Drilling Method: Hollow Stem Auger

SUBSURFACE PROFILE		SAMPLE DATA				0	o an Other with	Water Content			
Jepth	Soil Description	elev./Depth m)	ype	àample Number	l or RQD	kecovery (%)	 SI × 50 SI • (I 20 	(kPa) × 150 • • • • • • • • • • • • • • • • • • •	Liqui	%) ⊽ 50 75 d Limit %) □ 50 75	Monitoring Well Details
ftm	Cround Surface	ш <u> </u>	-	0)	~	u .	l	<u>L</u>	I	.11	-
	FILL MATERIAL silt-sand, trace gravel, brown, loose to compact, moist.	0.00	X	SS1	6	42	6 0		8		
		108.88	X	SS2	15	56	15		15 ▽		
4 5 6 2 7 8 9 10 3 11 12 13 4 14 15 16 17 18 19 19 10 3 Eastin	End of Borehole	108.88 1.27	rthing	;: 50152 ⁻	73 m			Image:		Image: state stat	er refusal.
Site Da	atum: Site Benchmark - 2 nails in	utility po	ole - 11	16.310 m	1			Borehole termina	ated after p	ractical auge	er refusal.
Groun	dsurface Elevation: 110.15 m	Тој	p of R	iser Elev	v. : NA						
Hole D	Diameter: 200 mm	Мо	nitori	ng Well	Diamete	er: N/A					

ATTACHMENT E

Nitrate Impact Assessment



PRE DEVELOPMENT CONDITIONS POST DEVELOPMENT CONDITIONS Intraction factors 0.2 undulating Topography 0.2 undulating Soil 0.4 und / sit Cover 0.1 rubineded Cover 0.1 rubineded Cover 0.1 rubineded Cover 0.1 rubineded Site Characteristics 1719 m ² (See/Ollaws) Area of Site : 1719 m ² (See/Ollaws) 0.7 Instars Site Characteristics Area of site : 1719 m ² (See/Ollaws) 0.7 Instars Site Characteristics Area of sath root 276 m ² Total of driveway/ parking area (approx). 521 m ² Importious Area (approx) 600 m ² Intertainer Area = 46.37 % Infiltration Area = 46.37 % Infiltration Calculation m ² Daily Sewage flow (Co) = 0 mg/L Committation of Tithuret (Co) - 0 mg/L Distribution factors 1 m ² Daily Sewage flow (Co) = 0 mg/L Distribution factored factors formation of Tithuret (Co) - <td< th=""><th colspan="9">Predictive Nitrate Impact Assessment</th></td<>	Predictive Nitrate Impact Assessment								
Infitiation Factor infitiation Factor infitiation Factor infitiation Factor infitiation Factor 0.2 undating Soil Cover 0.3 cultivated 0.7 100 100 100 100 100 100 100 10	PRE DEVELOPMENT CONDITIONS		POST DEVELOPMENT CONDITIONS						
Topography O.2 unclusting Topography O.2 unclusting Solt O.4 sact / sits O.4 sact / sits Cover O.1 cultivated Cover O.1 cultivated Topography Cover O.1 cultivated Cover O.1 cultivated Site Characteristics Total O.7 Total O.7 Site Characteristics Total O.7 Para of site : 1.719 m ² Ass of Site : 1.719 m ² (GeoOttawa) O.6 Para of site : 1.719 m ² Note area 0.17 hoctares 2.26 m ² Para of site : 1.719 m ² Impervious Area (pprox.) 640 m ² Para of site : 1.719 m ² Integration of Site : 1.719 m ² Covers of site of site : 1.719 m ² Impervious Area (pprox.) 640 m ² Para of site : 1.719 m ² Integration of Site : 1.719 m ² Para of site : 1.719 m ² Impervious Area (pprox.) 640 mgtt. Explite Effluent Explite Effluent	Infiltration Factors		Infiltration Factors						
Solt 0.4 and / sitt Solt 0.4 and / sitt Cover 0.1 autivated Cover 0.1 autivated Total 0.7 Total 0.7 Site Characteristics 17.9 m ² (CeOCitave) 0.17 heters Area of Site : 17.9 m ² Area of Site : 17.9 m ² (CeOCitave) 0.17 heters Area of each nocic 2.26 m ² Area of Site : 0.17 heters Area of each nocic 2.26 m ² Interview Area of site : 0.17 heters 0.01 m ² Area of each nocic 2.27 m ² Importion Area (pprox) 600 m ² Total of orizeway: 0 m 0 m Importion Area (pprox) 600 m ² Total orizeway: 0 m 0 m Septic Effluent Septic Effluent 2.27 m ² 0 mg/L Concentration or Effluent (Co) = 0 mg/L Concentration or Effluent (Co) = 0 mg/L Daily Sewage Flow (Ca) - 0 mg/L Concentration or Effluent (Co) = 0 mg/L Environment Canada Climate Normak: CTTAWA AIRPORT TSTAIN Orizin Concentration or propitation (Co) = 0 mg/L Environment Canada Climate Normak: CTTAWA AIRPORT TSTAINO Norizin <td>Topography</td> <td>0.2 undulating</td> <td>Topography</td> <td>0.2 undulating</td>	Topography	0.2 undulating	Topography	0.2 undulating					
Cover 0.1 cutivated Total Cover 0.1 cutivated Total O.1 cutivates Total O.1 cutivate	Soil	0.4 sand / silt	Soil	0.4 sand / silt					
Total0.7Total0.7Site Characteristics Area of Site :1710 m^2 (GeoOttawa) 0.17hectaresSite Characteristics Area of Site :1.710 m^2 Area of site :1.710 m^2 Area of site :1.710 m^2 Area of site :1.710 m^2 Area of site :1.710 m^2 Total of of readways: tength of readways: total of or adways: total of of readways: total of or readways: total of and readways: total of readways: total area of readways: <br< td=""><td>Cover</td><td>0.1 cultivated</td><td>Cover</td><td>0.1 cultivated</td></br<>	Cover	0.1 cultivated	Cover	0.1 cultivated					
Site Characteristics Site Characteristics Area of Site : 1719 m ² (GeoOfIzawa) Area of Site : 1.770 m ² O.7.7 hectares 0.77 hectares Area of Site : 0.77 hectares Area of Site : 0.77 hectares 0.77 hectares Area of Site : 0.77 hectares Integration of Site : 0.76 m ² 0.76 m ² 0.76 m ² Total of of Neway: 0 m 0 m 0 m Impervious Area (approx.) 640 m ² 100 m ² 0 m Inflittation Area - 1.029 m ² Inflittation Area - 40.37 % Inflittation Area - 1.029 m ² Inflittation Area - 40.27 m ² Septic Effluent Consentration of Effluent (CQ) - 40 mg/L Consentration in probalitation (C) = 0 mg/L Inflittation Calculation Inflittation Calculation 11 m ³ Daily Sevage Flow (QQ) - 0.67 m ³ Static Way Area of Probalitation (C) = 0 mg/L Inflittation Calculation 0 mg/L Inflittation Calculation 11 m/Y Static Mark area - 20.8 mn/y Static Way Area of Probalitation 1 mm/y Static Mark area - 20.8 mn/y	Tota	0.7	Total	0.7					
Area of Site : 1719 m ² (GeoOttawn) Area of Site : 1,719 m ² (GeoOttawn) Area of Site : 0.17 hectares Area of Site : 0.17 hectares Area of Site : 0.17 hectares Area of Site : 0.17 hectares Area of Site : 0.17 hectares Area of site : 0.17 hectares Area of other cool: 276 m ² Total of orod areas. 276 m ² Impervious Area (approx.) 690 m ² 0 m 0 m Impervious Area (approx.) 690 m ² mererious Area = 922 m ² Inflittation Area = 1.029 m ² inflittation Area = 922 m ² Septic Effluent Concentration of ffluent (Co) = 0 mg/L Concentration of ffluent (Co) = 0 mg/L Concentration of ffluent (Co) = 0 mg/L Inflittation Calculation Inflittation Calculation Nintate concentration in procipitation (C) = 0 mg/L Forvicencent Canada (Ottawa Aipport) Procipitation 929 d mm/yr Soil mobiume referition (shaftow rooted crops) 75 mm/yr Soil mobiume referition (shaftow rooted crops) 75 mm/yr Soil mobiume referition (shaftow rooted crops) 75 mm/yr Soil mobiume referiting the system from inflation <td< td=""><td></td><td></td><td></td><td></td></td<>									
Area Of Site : 1,1/9 in (GoucoLaw) Area Of Site : 1,1/9 in $(-1)^{-1}$ in $(-1)^{-1}$ hectares $(-1)^{-1}$ hectar	Site Characteristics	m^2 (CooOttown)	Site Characteristics	· - · · · · · · · · · · · · · · · · · ·					
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Area of Site :	1/19 III (GeoOttawa)	Area of Site :	1,719					
$ \begin{array}{ccccc} \begin{tabular}{l l l l l l l l l l l l l l l l l l l $		0.17 hectares		0.17 hectares					
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			Area of each root:	$2/6 \text{ m}^2$					
$ \begin{array}{ccccc} Total of driveway / parking areas (approx): 521 m2 largh of rad/ways: 0 m Total area of road/ways: 0 m Total area of road/ways: 0 m Total area o$			Total of roof areas:	276 111					
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Infiltration flow entering the system $(Q_i) =$ 1 m ³ /day Infiltration Flow Entering the System $(Q_i) =$ 0.68 m ³ /day Mass Balance Model (MOEE, 1995) $C_T = (Q_b C_b + Q_c C_e + Q_c C_c)/(Q_b + Q_e + Q_c) = Cumulative Nitrate Concentration Mass Balance Model (MOEE, 1995) C_T = (Q_b C_b + Q_c C_e + Q_c C_c)/(Q_b + Q_e + Q_c) = Cumulative Nitrate Concentration C_T = (Q_b C_b + Q_c C_e + Q_c C_c)/(Q_b + Q_e + Q_c) = Cumulative Nitrate Concentration Q_b = flow entering the system across the upgradient area 0 m3/day C_b = background nitrate concentration 0 mg/L Q_e = flow entering the system from the septic drainfield 1 m3/day Q_e = flow entering the system from the septic drainfield 0.67 m3/day Q_e = flow entering the system from infiltration 1 m3/day Q_e = flow entering the system from the septic drainfield 0.67 m3/day Q_i = flow entering the system from infiltration 1 m3/day Q_e = flow entering the system from infiltration 1 m3/day Q_i = flow entering the system from infiltrate 0 mg/L C_e = concentration of nitrates in the septic effluent 40 mg/L Q_i = flow entering the system from infiltrate 0 mg/L C_i = Concentration of nitrates in the infiltrate 0$				mm/yr					
Mass Balance Model (MOEE, 1995) $C_T = (Q_bC_b + Q_cC_e + Q_iC_j)/(Q_b + Q_e + Q_i) = Cumulative Nitrate ConcentrationQ_b = flow entering the system across the upgradient areaMass Balance Model (MOEE, 1995)C_T = (Q_bC_b + Q_cC_e + Q_iC_j)/(Q_b + Q_e + Q_i) = Cumulative Nitrate ConcentrationQ_b = flow entering the system across the upgradient areaMass Balance Model (MOEE, 1995)C_T = (Q_bC_b + Q_cC_e + Q_iC_j)/(Q_b + Q_e + Q_i) = Cumulative Nitrate ConcentrationQ_b = flow entering the system across the upgradient area0m³/dayQ_e = flow entering the system from the septic drainfield1m³/dayQ_e = flow entering the system from the septic drainfield0.67m³/dayQ_e = flow entering the system from infiltration1m³/dayQ_e = concentration of nitrates in the septic effluent40mg/LQ_i = flow entering the system from infiltration1m³/dayQ_e = flow entering the system from infiltration1m³/dayC_i = Concentration of nitrates in the infiltrate0mg/LQ_i = flow entering the system from infiltration1m³/dayC_i = Concentration of nitrates in the infiltrate0mg/LC_i = Concentration of nitrates in the infiltrate0mg/LC_T = 22.8 mg/LC_T = 19.9 mg/LC_T = 19.9 mg/L11111With 50% nitrate reduction (tertiary treatment)9.9 mg/L$	Infiltration flow entering the system (Ω_i) =	1 m³/day	Infiltration Flow Entering the System (Q_i) =	0.68 m³/day					
$C_T = (Q_b C_b + Q_c C_e + Q_c C_j)/(Q_b + Q_e + Q_i) = Cumulative Nitrate Concentration Q_b = flow entering the system across the upgradient area 0 m³/day C_b = background nitrate concentration 0 mg/L Q_e = flow entering the system from the septic drainfield 1 m³/day Q_e = flow entering the system from the septic drainfield 1 m³/day Q_e = flow entering the system from the septic drainfield 1 m³/day Q_e = flow entering the system from the septic drainfield 0 mg/L Q_e = flow entering the system from infiltration 1 m³/day Q_i = flow entering the system from infiltration 1 m³/day Q_i = flow entering the system from infiltration 1 m³/day Q_i = flow entering the system from infiltration 1 m³/day C_T = 22.8 mg/L C_T = 19.9 mg/L Estimate Number of Lots 1 1 1 V_i = 50^\circ intrate reduction (tertiary treatment) 9.9 mg/L $	Mass Balance Model (MOEE, 1995)		Mass Balance Model (MOEE, 1995)						
Q_b = flow entering the system across the upgradient area 0 m ³ /day Q_b = flow entering the system across the upgradient area 0 m ³ /day C_b = background nitrate concentration 0 mg/L Q_o = flow entering the system from the septic drainfield 1 m ³ /day Q_o = flow entering the system from the septic drainfield 1 m ³ /day Q_o = flow entering the system from the septic drainfield 0.67 m ³ /day Q_o = flow entering the system from the septic drainfield 0.67 m ³ /day Q_o = flow entering the system from infiltration 1 m ³ /day Q_i = flow entering the system from infiltration 1 m ³ /day Q_i = flow entering the system from infiltration 1 m ³ /day Q_i = flow entering the system from infiltrate 0 mg/L C_T = 22.8 mg/L C_i = Concentration of nitrates in the infiltrate 0 mg/L C_T = 22.8 mg/L C_T = 1.04s 1.04s 1.04s 1.04s with 50% nitrate reduction (tertilary treatment) 9.9 mg/L	$C_{T} = (Q_h C_h + Q_n C_n + Q_i C_i)/(Q_h + Q_n + Q_i) = Cumi$	ulative Nitrate Concentration	$C_T = (Q_h C_h + Q_c C_a + Q_i C_i)/(Q_h + Q_a + Q_i) = Cumulative N$	itrate Concentration					
$ \begin{array}{c} L_{b} = background nitrate concentration & 0 mg/L \\ C_{b} = background nitrate concentration & 0 mg/L \\ C_{e} = flow entering the system from the septic drainfield & 1 m^{3}/day \\ C_{e} = concentration of nitrates in the septic effluent & 40 mg/L \\ C_{i} = flow entering the system from infiltration & 1 m^{3}/day \\ C_{i} = Concentration of nitrates in the infiltrate & 0 mg/L \\ C_{i} = Concentration of nitrates in the infiltrate & 0 mg/L \\ C_{i} = Concentration of nitrates in the infiltrate & 0 mg/L \\ C_{T} = 22.8 mg/L \\ C_{T} = 22.8 mg/L \\ C_{T} = 10 to the third $	$O_{\rm b}$ = flow entering the system across the upgradient area	o m ³ /day	$O_{\rm r} =$ flow entering the system across the upgradient area	o m ³ /day					
$\begin{aligned} & G_{q} = flow entering the system from the septic drainfield & 1 m^{3}/day \\ G_{e} = flow entering the system from the septic drainfield & 0 mg/L \\ G_{e} = concentration of nitrates in the septic effluent & 40 mg/L \\ G_{i} = flow entering the system from infiltration & 1 m^{3}/day \\ G_{i} = Concentration of nitrates in the infiltrate & 0 mg/L \\ C_{T} = & 22.8 mg/L \\ \hline C_{T} = & 22.8 mg/L \\ \hline C_{T} = & 1 lots \\ \hline C_{T} = & 0 mg/L \\ \hline C_{T} = $	$C_{t} = background nitrate concentration$	0 mg/l	$C_{\rm b}$ = background nitrate concentration	0 ma/l					
C_e = concentration of nitrates in the septic effluent 40 mg/L C_e = concentration of nitrates in the septic effluent 40 mg/L Q_i = flow entering the system from infiltration 1 m³/day Q_i = flow entering the system from infiltration 1 m³/day C_i = Concentration of nitrates in the infiltrate 0 mg/L C_r = Concentration of nitrates in the infiltrate 0 mg/L C_T = 22.8 mg/L C_T = 19.9 mg/L Estimate Number of Lots 1 lots with 50% nitrate reduction (tertiary treatment) with 50% nitrate reduction (tertiary treatment)	$\Omega_{\rm c}$ = flow entering the system from the sentic drainfield	1 m ³ /day	$\Omega_{\rm r}$ = flow entering the system from the sentic drainfield	0.67 m ³ /day					
$O_i = $ concentration of initiates in the split endent 40 mg/L $O_i = $ concentration of initiates in the split endent 40 mg/L $O_i = $ flow entering the system from infiltration 1 m ³ /day $O_i = $ flow entering the system from infiltration 1 m ³ /day $C_i = $ Concentration of nitrates in the infiltrate 0 mg/L $C_i = $ Concentration of nitrates in the infiltrate 0 mg/L $C_T = $ 22.8 mg/L $C_T = $ 19.9 mg/L Estimate Number of Lots 1 lots Estimate Number of Lots 1 lots with 50% nitrate reduction (tertiary treatment)	$C_{\rm e}$ = concentration of nitrates in the sentic effluent	40 mg/l	$C_{\rm e}$ = concentration of nitrates in the sentic effluent	40 mg/l					
$C_{I} = Concentration of nitrates in the infiltrate 0 mg/L C_{I} = Concentration of nitrates in the infiltrate 0 mg/L C_{I} = Concentration of nitrates in the infiltrate 0 mg/L C_{I} = Concentration of nitrates in the infiltrate 0 mg/L C_{I} = 10.9 mg/L C_{I} = 10.9 mg/L C_{I} = 10.9 mg/L C_{I} = 10.9 mg/L$ Estimate Number of Lots 1 l	Ω_{e} = concentration of matters in the septe condent	1 m ³ /day	Q_{e} = flow entering the system from infiltration	1 m ³ /day					
$C_{T} = 22.8 \text{ mg/L}$ $C_{T} = 22.8 \text{ mg/L}$ $C_{T} = 22.8 \text{ mg/L}$ $C_{T} = 19.9 \text{ mg/L}$	C_{i} = now entering the system from initiation	0 mg//	$Q_i =$ now entering the system non-initiation $Q_i = Concentration of nitrates in the infiltrate$	0 mg/l					
CT = 22.8 mg/L CT = 19.9 mg/L Estimate Number of Lots 1 lots Estimate Number of Lots 1 lots with 50% nitrate reduction (tertiary treatment) 9.9 mg/L	$C_{i} = Concentration of initiates in the initiate$	0 mg/L	$C_i = Concentration of initiates in the initiate$	0 mg/L					
Estimate Number of Lots 1 lots Estimate Number of Lots 1 lots with 50% nitrate reduction (tertiary treatment) 9.9 mg/L	C _T =	22.8 mg/L	C _T =	19.9 mg/L					
with 50% nitrate reduction (tertiary treatment) 9.9 mg/L	Estimate Number of Lots	1 lots	Estimate Number of Lots	1 lots					
			with 50% nitrate reduction (tertiary treatment)	9.9 mg/L					

The washrooms are proposed within the office space, so volume is calculated as per B.15.

Total daily septic design flow rate = 670 L/day as per Absolute Drafting & Design communications 2024.

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ATTACHMENT F

Civil Engineering Plans (LRL)



EROSION AND SEDIMENT CONTROL MEASURES:

** CONTRACTOR IS RESPONSIBLE FOR ALL INSTALLATION, MONITORING, REPAIR AND REMOVAL OF ALL EROSION AND SEDIMENT CONTROL FEATURES *

. PRIOR TO START OF CONSTRUCTION:

- PRIOR TO THE REMOVAL OF ANY VEGETATIVE COVER, MOVING OF SOIL AND CONSTRUCTION: - INSTALL SILT FENCE IMMEDIATELY DOWNSTREAM FROM AREAS TO BE DISTURBED (SEE PLAN FOR LOCATION). - INSTALL GEOSOCK INSERTS WITH AN OVERFLOW IN ALL THE DOWNSTREAM CATCHBASINS AND MANHOLES INSTALL SILTSACK FILTERS IN ALL CONCRETE CATCH BASINS STRUCTURES
- INSPECT MEASURES IMMEDIATELY AFTER INSTALLATION.

2. DURING CONSTRUCTION:

- WORK TO BE DONE IN THE VICINITY OF MAJOR WATERWAYS TO BE CARRIED OUT FROM JULY TO SEPTEMBER ONLY. - MINIMIZE THE EXTENT OF DISTURBED AREAS AND THE DURATION OF EXPOSURE. PROTECT DISTURBED AREAS FROM RUNOFF. PROVIDE TEMPORARY COVER SUCH AS SEEDING OR MULCHING IF DISTURBED AREA WILL NOT BE REHABILITATED
- WITHIN 30 DAYS. INSPECT SILT FENCES, FILTER CLOTHS AND CATCH BASIN SUMPS WEEKLY AND AFTER EVERY MAJOR STORM EVENT. CLEAN AND REPAIR WHEN NECESSARY CONSTRUCT SWALES AS PER DETAIL
- PLAN TO BE REVIEWED AND REVISED AS REQUIRED DURING CONSTRUCTION
- EROSION CONTROL FENCING TO BE ALSO INSTALLED AROUND THE BASE OF ALL STOCKPILES. - DO NOT LOCATE TOPSOIL PILES AND EXCAVATION MATERIAL CLOSER THAN 2.5m FROM ANY PAVED SURFACE, OR ONE WHICH IS TO BE PAVED BEFORE THE PILE IS REMOVED. ALL TOPSOIL PILES ARE TO BE SEEDED IF THEY ARE TO REMAIN ON SITE LONG ENOUGH FOR SEEDS TO GROW (LONGER THAN 30 DAYS). CONTROL WIND-BLOWN DUST OFF SITE TO ACCEPTABLE LEVELS BY SEEDING TOPSOIL PILES AND OTHER AREAS TEMPORARII Y (PROVIDE WATERING AS REQUIRED) - ALL EROSION CONTROL STRUCTURE TO REMAIN IN PLACE UNTIL ALL DISTURBED GROUND SURFACES HAVE BEEN STABILIZED EITHER BY PAVING OR RESTORATION OF VEGETATIVE GROUND COVER.
- NO ALTERNATE METHODS OF EROSION PROTECTION SHALL BE PERMITTED UNLESS APPROVED BY THIS CONSULTING ENGINEER AND THE CITY DEPARTMENT OF PUBLIC WORKS.
- CONTRACTOR RESPONSIBLE FOR CITY ROADWAY AND SIDEWALK TO BE CLEANED OF ALL SEDIMENT FROM VEHICULAR TRACKING ETC. AT THE END OF EACH WORK DAY.
- -PROVIDE GRAVEL ENTRANCE WHEREVER EQUIPMENT LEAVES THE SITE TO PREVENT MUD TRACKING ONTO PAVED SURFACES, GRAVEL BED SHALL BE A MINIMUM OF 15m LONG, 4M WIDE AND 0.3m DEEP AND SHALL CONSIST OF COARSE (50mm CRUSHERT-RUN LIMESTONE) MATERIAL, MAINTAIN GRAVEL ENTRANCE IN CLEAN CONDITION. DURING WET CONDITIONS, TIRES OF ALL VEHICLES/EQUIPMENT LEAVING THE SITE ARE TO BE SCRAPED. ANY MUD/MATERIAL TRACKED ONTO THE ROAD SHALL BE REMOVED IMMEDIATELY BY HAND OR RUBBER TIRE
- TAKE ALL NECESSARY STEPS TO PREVENT BUILDING MATERIAL, CONSTRUCTION DEBRIS OR WASTE BEING SPILLED OR TRACKED ONTO ABUTTING PROPERTIES OR PUBLIC STREETS DURING CONSTRUCTION AND PROCEED IMMEDIATELY TO CLEAN UP ANY AREAS SO AFFECTED.

3. AFTER CONSTRUCTION:

PROVIDE PERMANENT COVER CONSISTING OF TOPSOIL AND SEED TO DISTURBED AREAS. - REMOVE STRAW BALE FLOW CHECK DAMS, SILT FENCES AND FILTER CLOTHS ON CATCH BASINS AND MANHOLE COVERS AFTER DISTURBED AREAS HAVE BEEN REHABILITATED AND STABILIZED. - INSPECT AND CLEAN CATCH BASIN SUMPS AND STORM SEWERS

GENERAL

THE CONTRACTOR SHALL IMPLEMENT BEST MANAGEMENT PRACTICES, TO PROVIDE FOR PROTECTION OF THE AREA DRAINAGE SYSTEM AND THE RECEIVING WATERCOURSE, DURING CONSTRUCTION ACTIVITIES. THE CONTRACTOR ACKNOWLEDGES THAT FAILURE TO IMPLEMENT APPROPRIATE EROSION AND SEDIMENT CONTROL MEASURES MAY BE SUBJECT TO PENALTIES IMPOSED BY ANY APPLICABLE REGULATORY AGENCY.

THE CONTRACTOR ACKNOWLEDGES THAT SURFACE EROSION AND SEDIMENT RUNOFF RESULTING FROM THEIR CONSTRUCTION OPERATIONS HAS POTENTIAL TO CAUSE A DETRIMENTAL IMPACT TO ANY DOWNSTREAM WATERCOURSE OR SEWER AND THAT ALL CONSTRUCTION OPERATIONS THAT MAY IMPACT UPON WATER QUALITY SHALL BE CARRIED OUT IN MANNER THAT STRICTLY MEETS THE REQUIREMENT OF ALL APPLICABLE LEGISLATION AND REGULATIONS.

AS SUCH, THE CONTRACTOR SHALL BE RESPONSIBLE FOR CARRYING OUT THEIR OPERATIONS, AND SUPPLYING AND INSTALLING ANY APPROPRIATE CONTROL MEASURES, SO AS TO PREVENT SEDIMENT LADEN RUNOFF ENTERING ANY SEWER OR WATERCOURSE WITHIN OR DOWNSTREAM OF THE WORKING AREA.

THE CONTRACTOR ACKNOWLEDGES THAT NO ONE MEASURE IS LIKELY TO BE 100% EFFECTIVELY FOR EROSION PROTECTION AND CONTROLLING SEDIMENT RUNOFF AND DISCHARGES FROM THE SITE. THEREFORE. WHERE NECESSARY THE CONTRACTOR SHALL IMPLEMENT ADDITIONAL MEASURES ARRANGED IN SUCH MANNER AS TO MITIGATE SEDIMENT RELEASE FROM THE CONSTRUCTION OPERATIONS AND ACHIEVE SPECIFIC MAXIMUM PERMITTED CRITERIA WHERE APPLICABLE. SUGGESTED ON-SITE MEASURES MAY INCLUDE. BUT SHALL NOT BE LIMITED TO. THE FOLLOWING METHODS: SEDIMENT PONDS, FILTER BAGS, PUMP FILTERS, SETTLING TANKS, SILT FENCE, STRAW BALES, FILTER CLOTHS, CATCH BASIN FILTERS, CHECK DAMS AND/OR OTHER RECOGNIZED TECHNOLOGIES AND METHOD AVAILABLE AT THE TIME OF CONSTRUCTION. SPECIFIC MEASURES SHALL BE INSTALLED IN ACCORDANCE WITH REQUIREMENTS OF OPSS 577 WHERE APPROPRIATE, OR IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS

WHERE, IN THE OPINION OF THE CONTRACT ADMINISTRATOR OR REGULATORY AGENCY, THE INSTALLED CONTROL MEASURES FAIL TO PERFORM ADEQUATELY, THE CONTRACTOR SHALL SUPPLY AND INSTALL ADDITIONAL OR ALTERNATIVE MEASURES AS DIRECTED BY THE CONTRACT ADMINISTRATOR OR REGULATORY AGENCY, AS SUCH, THE CONTRACTOR SHALL HAVE ADDITIONAL CONTROL MATERIALS ON SITE AT ALL TIME WHICH ARE EASILY ACCESSIBLE AND MAY BE IMPLEMENTED BY HIM AT THE MOMENT'S NOTICE.

PRIOR TO COMMENCING WORK, THE CONTRACTOR SHALL SUBMIT TO THE CONTRACT ADMINISTRATOR SIX COPIES ONTROL PLAN (ESCP). THE ESCP WILL (AND DETAILED DRAWINGS INDICATING THE ON-SITE ACTIVITIES AND MEASURES TO BE USED TO CONTROL EROSION AND SEDIMENT MOVEMENT FOR EACH STEP OF THE WORK.

CONTRACTOR'S RESPONSIBILITIES

THE CONTRACTOR SHALL ENSURE THAT ALL WORKERS, INCLUDING SUB-CONTRACTOR, IN THE WORKING ARE ARE AWARE OF THE IMPORTANCE OF THE EROSION AND SEDIMENT CONTROL MEASURES AND INFORMED OF THE CONSEQUENCES OF THE FAILURE TO COMPLY WITH THE REQUIREMENTS OF ALL REGULATORY AGENCIES.

THE CONTRACTOR SHALL PERIODICALLY, AND WHEN REQUESTED BY THE CONTRACT ADMINISTRATOR, CLEAN OUT ACCUMULATED SEDIMENT DEPOSITS AS REQUIRED AT THE SEDIMENT CONTROL DEVICES. INCLUDING THOSE DEPOSITS THAT MAY ORIGINATE FROM OUTSIDE THE CONSTRUCTION AREA. ACCUMULATED SEDIMENT SHALL BE REMOVED IN SUCH A MANNER THAT PREVENTS THE DEPOSITION OF THIS MATERIAL INTO THE SEWER WATERCOURSE AND AVOIDS DAMAGE TO CONTROL MEASURES. THE SEDIMENT SHALL BE REMOVED FROM THE SITE AT THE CONTRACTOR'S EXPENSE AND MANAGED IN COMPLIANCE WITH REQUIREMENTS FRO EXCESS EARTH MATERIAL, AS SPECIFIED ELSEWHERE IN THE CONTRACT.

THE CONTRACTOR SHALL IMMEDIATELY REPORT TO THE CONTRACT ADMINISTRATOR ANY ACCIDENTAL DISCHARGES OF SEDIMENT MATERIAL INTO EITHER THE WATERCOURSE OR THE STORM SEWER SYSTEM. FAILURE TO REPORT WILL BE CONSTITUTE A BRACH OF THIS SPECIFICATION AND THE CONTRACTOR MAY ALSO BE SUBJECT TO THE PENALTIES IMPOSED BY THE APPLICABLE REGULATORY AGENCY, APPROPRIATE RESPONSE MEASURES, INCLUDING ANY REPAIRS TO EXISTING CONTROL MEASURES OR THE IMPLEMENTATION OF ADDITIONAL CONTROL MEASURES, SHALL BE CARRIED OUT BY THE CONTRACTOR WITHOUT DELAY.

THE SEDIMENT CONTROL MEASURES SHALL ONLY BE REMOVED WHEN, IN THE OPINION OF THE CONTRACT ADMINISTRATOR, THE MEASURE OR MEASURES, IS NO LONGER REQUIRED. NO CONTROL MEASURE MAY BE PERMANENTLY REMOVED WITHOUT PRIOR AUTHORIZATION FROM THE CONTRACT ADMINISTRATOR. ALL SEDIMENT AND EROSION CONTROL MEASURES SHALL BE REMOVED IN A MANNER THAT AVOIDS THE ENTRY OF ANY EQUIPMENT. OTHER THAN HAND-HELD EQUIPMENT, INTO ANY WATERCOURSE, AND PREVENTS THE RELEASE OF ANY SEDIMENT OR DEBRIS INTO ANY SEWER OR WATERCOURSE WITHIN OR DOWNSTREAM OF THE WORKING AREA. ALL ACCUMULATED SEDIMENT SHALL BE REMOVED FROM THE WORKING AREA AT THE CONTRACTOR'S EXPENSE AND MANAGED IN COMPLIANCE WITH THE REQUIREMENTS FOR EXCESS EARTH MATERIAL

WHERE, IN THE OPINION OF EITHER THE CONTRACT ADMINISTRATOR OR A REGULATORY AGENCY, ANY OF THE TERMS SPECIFIED HEREIN HAVE NOT BEEN COMPLIED WITH OR PERFORMED IN A SUITABLE MANNER. OR TAT ALL. THE CONTRACTOR ADMINISTRATOR OR A REGULATORY AGENCY HAS THE RIGHT TO IMMEDIATELY WITHDRAW ITS PERMISSION TO CONTINUE THE WORK BUT MAY RENEW ITS PERMISSION UPON BEING SATISFIED THAT THE DEFAULTS OR DEFICIENCIES IN THE PERFORMANCE OF THIS SPECIFICATION BY THE CONTRACTOR HAVE BEEN REMEDIED.

SPILL CONTROL NOTES

- 1. ALL CONSTRUCTION EQUIPMENT SHALL BE RE-FUELED, MAINTAINED, AND STORED NO LESS THAN 30 METRES FROM WATERCOURSE, STEAMS, CREEKS, WOODLOTS, AND ANY ENVIRONMENTALLY SENSITIVE AREAS, OR AS
- OTHERWISE SPECIFIED. THE CONTRACTOR MUST IMPLEMENT ALL NECESSARY MEASURES IN ORDER TO PREVENT LEAKS, DISCHARGES OR
- SPILLS OF POLLUTANTS, DELETERIOUS MATERIALS, OR OTHER SUCH MATERIALS OR SUBSTANCES WHICH WOULD OR COULD CAUSE AN ADVERSE IMPACT TO THE NATURAL ENVIRONMENT. 3. IN THE EVENT OF A LEAK, DISCHARGE OR SPILL OF POLLUTANT, DELETERIOUS MATERIAL OR OTHER SUCH MATERIAL OR SUBSTANCE WHICH WOULD OR COULD CAUSE AN ADVERSE IMPACT TO THE NATURAL ENVIRONMENT,
- THE CONTRACTOR SHALL 3.1. IMMEDIATELY NOTIFY APPROPRIATE FEDERAL, PROVINCIAL, AND LOCAL GOVERNMENT MINISTRIES, DEPARTMENTS, AGENCIES, AND AUTHORITIES OF THE INCIDENT IN ACCORDANCE WITH ALL CURRENT LAWS,
- LEGISLATION, ACTS, BY-LAWS, PERMITS, APPROVALS, ETC. 3.2. TAKE IMMEDIATE MEASURES TO CONTAIN THE MATERIAL OR SUBSTANCE, AND TO TAKE SUCH MEASURES
- TO MITIGATE AGAINST ADVERSE IMPACTS TO THE NATURAL ENVIRONMENT. 3.3. RESTORE THE AFFECTED AREA TO THE ORIGINAL CONDITION OR BETTER TO THE SATISFACTION OF THE AUTHORITIES HAVING JURISDICTION.

MUD MAT NOTES

- . THE GRANULAR MATERIAL WILL REQUIRE PERIODIC REPLACEMENT AS IT BECOMES CONTAMINATED BY VEHICLE
- TRAFFIC 2. SEDIMENT SHALL BE CLEANED FROM PUBLIC ROADS AT THE END OF EACH DAY
- 3. SEDIMENT SHALL BE REMOVED FROM PUBLIC ROADS BY SHOVELING OR SWEEPING AND DISPOSED OR PROPERLY IN A CONTROLLED SEDIMENT DISPOSAL AREA.









GENERAL NOTES

- 1. ALL WORKS MATERIALS SHALL CONFIRM TO THE LAST REVISION OF THE STANDARDS AND SPECIFICATIONS FOR THE CITY OF OTTAWA
- ONTARIO PROVINCIAL STANDARD DRAWINGS (OPSD) AND SPECIFICATIONS (OPSS), WHERE APPLICABLE. LOCAL UTILITY STANDARDS AND MINISTRY OF TRANSPORTATION STANDARDS WILL APPLY WHERE REQUIRED
- 2. THE CONTRACTORS SHALL CONFIRM THE LOCATION OF ALL EXISTING UTILITIES WITHIN THE SITE AND ADJACENT WORK AREAS. CONTRACTORS SHALL BE RESPONSIBLE FOR PROTECTING ALL EXISTING UTILITIES TO THE SATISFACTION OF THE AUTHORITY
- HAVING JURISDICTION. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE REPAIR OR REPLACEMENT OF ANY SERVICES OR UTILITIES DISTURBED DURING CONSTRUCTION, TO THE SATISFACTION OF THE AUTHORITY HAVING JURISDICTION.
- 3. ALL DIMENSIONS SHALL BE CHECKED AND VERIFIED IN THE FIELD BY THE CONTRACTOR PRIOR TO THE START OF CONSTRUCTION, ANY DISCREPANCIES SHALL BE REPORTED IMMEDIATELY TO THE ENGINEER. LOST TIME DUE TO FAILURE OF THE CONTRACTORS TO CONFIRM UTILITY LOCATIONS AND NOTIFY ENGINEER OF POSSIBLE CONFLICTS PRIOR TO CONSTRUCTION WILL BE AT
- CONTRACTORS EXPENSE. 4. ANY AREA BEYOND THE LIMIT OF THE SITE DISTURBED DURING CONSTRUCTION SHALL BE RESTORED TO ORIGINAL CONDITION
- BETTER TO THE SATISFACTION OF THE AUTHORITY HAVING JURISDICTION AT THE CONTRACTOR'S EXPENSE. RELOCATING OF EXISTING SERVICES AND/OR UTILITIES SHALL BE AS SHOWN ON THE DRAWINGS OR DETECTED BY THE ENGINEER AT THE EXPENSE OF DEVELOPERS.
- 5. ALL WORK SHALL BE COMPLETED IN ACCORDANCE WITH THE 'OCCUPATIONAL HEALTH AND SAFETY ACT AND REGULATIONS FOR CONSTRUCTION PROJECTS'. THE GENERAL CONTRACTORS SHALL BE DEEMED TO BE THE 'CONTRACTOR' AS DEFINED IN THE ACT. 6. ALL THE CONSTRUCTION SIGNAGE MUST CONFIRM TO THE MINISTRY OF TRANSPORTATION OF ONTARIO MANUAL OF UNIFORM
- TRAFFIC CONTROL DEVICES PER LATEST AMENDMENT. 7. THE CONTRACTOR IS ADVISED THAT WORKS BY OTHERS MAY BE ONGOING DURING THE PERIOD OF THE CONTRACT. THE
- CONTRACTOR SHALL COORDINATE CONSTRUCTION ACTIVITIES TO PREVENT CONFLICTS.
- 8. ALL DIMENSIONS ARE IN METRES UNLESS SPECIFIED OTHERWISE.
- 9. THERE WILL BE NO SUBSTITUTION OF MATERIALS UNLESS PRIOR WRITTEN APPROVAL IS RECEIVED FROM THE ENGINEER. 10. ALL CONSTRUCTION SHALL BE CARRIED OUT IN ACCORDANCE WITH THE RECOMMENDATIONS MADE IN THE GEOTECHNICAL REPOR1
- 11.FOR DETAILS RELATING TO STORMWATER MANAGEMENT REFER TO THE SITE SERVICING AND STORMWATER
- MANAGEMENT REPORT 12. ALL SEWERS CONSTRUCTED WITH GRADES LESS THAN 1.0% SHALL BE INSTALLED USING LASER ALIGNMENT AND CHECKED WITH LEVEL
- INSTRUMENT PRIOR TO BACKFILLING. 13. THE CONTRACTOR IS RESPONSIBLE FOR OBTAINING ALL PERMITS REQUIRED AND TO BEAR THE COST OF THE SAME. 14. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ADDITIONAL BEDDING, OR ADDITIONAL STRENGTH PIPE IF THE MAXIMUM
- TRENCH WIDTH AS SPECIFIED BY OPSD IS EXCEEDED.
- 15. ALL PIPE/CULVERT SECTION SIZES REFER TO INSIDE DIMENSIONS.
- 16. SHOULD DEEPLY BURIED ARCHAEOLOGICAL REMAINS BE FOUND ON THE PROPERTY DURING CONSTRUCTION ACTIVITIES, THE HERITAGE OPERATIONS UNIT OF THE ONTARIO MINISTRY OF CUI TURE MUST BE NOTIFIED IMMEDIATELY 17. ALL NECESSARY CLEARING AND GRUBBING SHALL BE COMPLETED BY THE CONTRACTOR. REVIEW WITH CONTRACT
- ADMINISTRATOR AND THE CITY OF OTTAWA PRIOR TO ANY TREE CUTTING/REMOVAL
- 18. DRAWINGS SHALL BE READ ON CONJUNCTION WITH ARCHITECTURAL SITE PLAN.
- 19. THE CONTRACTOR SHALL PROVIDE THE PROJECT ENGINEER ON SET OF AS CONSTRUCTED SITE SERVICING AND GRADING DRAWINGS.
- 20.BENCHMARKS: IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY THAT THE SITE BENCHMARK(S) HAS NOT BEEN ALTERED OR
- DISTURBED AND THAT ITS RELATIVE ELEVATION AND DESCRIPTION AGREES WITH THE INFORMATION DEPICTED ON THIS PLAN.
- 04327 --P. I. N. 0122 PLAN *****. 4 R -- 1 3 8 9 7 PART 3 PROPOSED 1.0m WIDE RIP-RAP BUFFER -PROPOSED ALONG P/L CONTRACTOR DEPRESS CURB TO CREATE EMERGENCY SC1.1 SPILLOVER POINT PROP CB01 GRASS AREAS TO BE SPILLOVER ELEV = 113.65 - T/G = 113.60REINSTATED WITH MIN. -NE INV = 112.10 100mm TOPSOIL & SOD PROPOSED NATURALIZED AREA (REFER TO LANDSCAPE ARCHITECT PLANS) ♥ EAQHING BED AREA ↓ ±90m2 Gaze \bigcirc BH> PROPOSED RETAINING WALL (DESIGN BY OTHERS).
 - TOP OF WALL TO BE EQUIPPED WITH - FENCE/RAMING (DESIGN BY OTHERS). BASE OF RETAINING WALL TO BE MINIMUM 0.15m FROM P/I

 - 04327 -- 0078 P. /. M.

SITE GRADING NOTES

- 1. ALL GRANULAR AND PAVEMENT FOR ROADS/PARKING AREAS SHALL BE CONSTRUCTED IN ACCORDANCE WITH GEOTECHNICAL ENGINEER'S RECOMMENDATIONS (AS APPLICABLE). 2. ALL TOPSOIL AND ORGANIC MATERIAL SHALL BE STRIPPED WITHIN THE ROAD AND PARKING AREAS ALLOWANCE PRIOR TO THE
- COMMENCEMENT OF CONSTRUCTION. 3. PAVEMENT REINSTATEMENT FOR SERVICE AND UTILITY CUTS SHALL BE IN ACCORDANCE WITH THE CITY OF OTTAWA STD. R10 AND OPSD 509.010 AND OPSS 310.
- 4. GRANULAR 'A' SHALL BE PLACED TO A MINIMUM THICKNESS OF 300MM AROUND ALL STRUCTURES WITHIN THE PAVEMENT AREA. 5. SUB-EXCAVATE SOFT AREAS AND FILL WITH GRANULAR 'B' COMPACTED IN MAXIMUM 300MM LIFTS.
- 6. ALL WORK ON THE MUNICIPAL RIGHT OF WAY AND EASEMENTS TO BE INSPECTED BY THE MUNICIPALITY PRIOR BACKFILLING. 7. CONTRACTOR TO OBTAIN A ROAD OCCUPANCY PERMIT 48 HOURS PRIOR TO COMMENCING ANY WORK WITHIN THE MUNICIPAL ROAD ALLOWANCE, IF REQUIRED BY THE MUNICIPALITY 8. ALL PAVEMENT MARKING FEATURES AND SITE SIGNAGE SHALL BE PLACED PER ARCHITECTURAL SITE PLAN. LINE PAINTING AND
- DIRECTIONAL SYMBOLS SHALL BE APPLIED WITH A MINIMUM OF TWO COATS OF ORGANIC SOLVENT PAINT. 9. REFER TO ARCHITECTURAL SITE PLAN FOR DIMENSIONS AND SITE DETAILS.
- 10. STEP JOINTS ARE TO BE USED WHERE PROPOSED ASPHALT MEETS EXISTING ASPHALT. ALL JOINTS MUST BE SEALED. 11. WHERE APPLICABLE THE CONTRACTOR IS TO SUBMIT SHOP DRAWINGS TO THE ENGINEER FOR APPROVAL PRIOR TO CONSTRUCTION, SHOP DRAWINGS MUST BE SITE SPECIFIC, SIGNED AND SEALED BY A LICENSED ENGINEER.

ROADWORK SPECIFICATIONS

12. ROADWORK TO BE COMPLETED IN ACCORDANCE WITH GEOTECHNICAL REPORT. 13. ALL TOPSOIL AND ORGANIC MATERIAL SHALL BE STRIPPED WITHIN THE ROAD ALLOWANCE PRIOR TO THE COMMENCEMENT OF CONSTRUCTION AND STOCK PILLED ON SITE AS DIRECTED BY THE MUNICIPAL AUHTORITY. 14. THE SUBGRADE SHALL BE CROWNED AND SLOPED AT LEAST 2% AND PROOF ROLLED WITH HEAVY ROLLERS. 15. SUB-EXCAVATE SOFT AREAS AND FILL WITH GRANULAR 'A'. TYPE II COMPACTED IN MAXIMUM 300MM LIFTS. ALL GRANULAR FOR ROADS SHALL BE COMPACTED TO MINIMUM OF 100% STANDARD PROCTOR DENSITY MAXIMUM DRY DENSITY (SPMDD).

REQUIRED GRADING.

PAVEMENT STRUCTURE

LEGEND:

		THICKNESS (mm)						
COURSE	MATERIAL	AUTOMOBILE PARKING	TRUCK ROUTE (HEAVY TRAFFIC)					
SURFACE	HL.3 A/C (PG 58-28)	50	40					
BINDER	HL.8 A/C (PG 58-28)		50					
BASECOURSE	OPSS GRANULAR "A"	150	150					
SUBBASE	OPSS GRANULAR "B" TYPE II	350	450					

N PREPARATION FOR PAVEMENT CONSTRUCTION AT THIS SITE, ANY SURFICIAL OR NEAR SURFACE/SUBGRADE LEVEL TOPSOIL AND ANY SOFT, WET OR DELETERIOUS MATERIALS SHOULD BE REMOVED FROM THE PROPOSED PAVED AREAS. THE EXPOSED SUBGRADE SHOULD BE INSPECTED AND APPROVED BY GEOTECHNICAL PERSONNEL AND ANY SOFT AREAS EVIDENT SHOULD BE SUBEXCAVATED AND REPLACED WITH SUITABLE EARTH BORROW APPROVED BY THE GEOTECHNICAL ENGINEER. THE SUBGRADE SHOULD BE SHAPED AND CROWNED TO PROMOTE DRAINAGE OF THE SITE DRAINAGE STRUCTURES. FOLLOWING APPROVAL OF THE PREPARATION OF THE SUBGRADE, THE PAVEMENT GRANULARS MAY BE PLACED. REFER TO GEOTECHNICAL INVESTIGATION REPORT PREPARED BY LRL ASSOCIATES DATED JULY 2021.



PROPOSED CURB PROPOSED DEPRESSED CURB

EXISTING PROPERTY LINE TO REMAIN

PROPOSED DOOR ENTRANCE/EXIT

PROPOSED HEAVY DUTY ASPHALT

PROPOSED CONCRETE FEATURES/SLAB

PROPOSED GRASS AREA

(100mm TOP SOIL & SOD)

T * * * * * * * * * * * *

×50.00 ×50.00HP

> ×50.00BC ×50.00TC



PROPOSED CATCHBASIN PROPOSED CURB STOP

PROPOSED 100 YEAR HIGH WATER LEVEL STORM WATERSHED EXTENT

> - WATERSHED NAME -RUNOFF COEFFICIENT

AREA IN HECTARES

Topographical Information

Topographic information provided by Farley, Smith and Denis Surveying Ltd. File No: 67-19

Metric Note

Distances and coordinates on this plan are in metres and can be converted to feet by dividing by 0.3048.

Distance Note

Distances shown on this plan are ground distances and can be converted to grid distances by multiplying by the combined scale factor of 0.99995.

Bearing Note

Bearings are MTM grid, derived from the Can-Net Real Time

GPS observations on reference points A and B, shown hereon,

having a bearing of N 22° 16' 20" W and are referred to the Central Meridian of MTM Zone 9 (76°30' West Longitude) Nad-83 (Original).

For bearing comparisons, a rotation of 6°16'20" counter-clockwise was applied to bearings on P1.

For bearing comparisons, a rotation of 0°39'20" counter-clockwise was applied to bearings on P2, P3, P4 & P5.

Elevation Notes

- 1. Elevations shown are geodetic and are referred to Geodetic Datum CGVD-1928 :1978.
- 2. It is the responsibility of the user of this information to verify that the job benchmark has not been altered or disturbed and that it's relative elevation and description agrees with the information shown on this drawing.

Utility Notes

- 1. This drawing cannot be accepted as acknowledging all of the utilities and it will be the responsibility of the user to contact the respective utility authorities for confirmation. 2. Only visible surface utilities were located.
- 3. Underground utility data derived from City of Ottawa utility sheet reference: 7123 (sheet 6).
- 4. A field location of underground plant by the pertinent utility authority is mandatory before any work involving breaking ground, probing, excavating etc.

USE AND INTERPRETATION OF DRAWINGS

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BY USE OF THE DRAWINGS FOR CONSTRUCTION OF THE PROJECT, THE OWNER ONFIRMS THAT HE HAS REVIEWED AND APPROVED THE DRAWINGS. TH NTRACTOR CONFIRMS THAT HE HAS VISITED THE SITE, FAMILIARIZED HIMSEL VITH THE LOCAL CONDITIONS, VERIFIED FIELD DIMENSIONS AND CORRELATED HIS SERVATIONS WITH THE REQUIREMENTS OF THE CONTRACT DOCUMENTS.

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IN ADDITION, THE CLIENT AGREES, TO THE FULLEST EXTENT PERMITTED BY LAW, O INDEMNIFY AND HOLD HARMLESS LRL FROM ANY DAMAGES, LIABILITIES OR COST, INCLUDING REASONABLE ATTORNEY'S FEES AND COST OF DEFENSE, ARISING FROM SUCH CHANGES

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5430 Canotek Road | Ottawa, ON, K1J 9G2 www.lrl.ca l (613) 842-3434

UNPOISED ARCHITECTURE INC

DESIGNED BY:	DRAWN BY:	APPROVED BY:						
К.Н.	К.Н.	M.B.						
PROJECT								
ΡΒΟΡΟΣΕΟ ΜΗΙΤΗΝΙΤ								

PROPOSED MULTI-UNIT COMMERCIAL DEVELOPMENT 5254 BANK STREET, OTTAWA

RAWING TITLE

GRADING AND DRAINAGE PLAN



JUNE2022

PROJECT NO 220536

Dated: April 24th, 2019

- PROCTOR DENSITY. A MINIMUM OF 300MM AROUND STRUCTURES.



PROPOSED SILT FENCE AS PER OPSD 219.110 PROPOSED DOOR ENTRANCE/EXIT PROPOSED GRASS AREA (100mm TOP SOIL & SOD) PROPOSED CONCRETE FEATURES/SLAB PROPOSED HEAVY DUTY ASPHALT PROPOSED LIGHT DUTY ASPHALT PROPOSED RIP RAP PROPOSED ELEVATION PROPOSED HIGH POINT ELEVATION PROPOSED BOTTOM OF CURB / ASPHALT ELEVATION PROPOSED TOP OF CURB ELEVATION PROPOSED EXPOSED BOTTOM OF RETAINING WALL PROPOSED TOP OF RETAINING WALL MATCH INTO EXISTING ELEVATION EXISTING ELEVATION

PROPOSED OVERLAND MAJOR FLOW ROUTE

— STM — STM — PROPOSED STORM SEWER EXISTING CATCHBASIN-MANHOLE/MANHOLE EXISTING CATCHBASIN PROPOSED CATCHBASIN-MANHOLE/MANHOLE PROPOSED CATCHBASIN PROPOSED CURB STOP PROPOSED 100 YEAR HIGH WATER LEVEL

STORM WATERSHED EXTENT -RUNOFF COEFFICIENT

- AREA IN HECTARES

PROPOSED WATER SERVICE _ CONNECTION TO CITY WATERMAIN. WATER CONNECTION AS PER CITY OF OTTAWA DETAIL W26.

L CONTRACTOR TO REINSTATE ASPHALT ROAD AFTER WATER SERVICE INSTALLATION TO MATCH EXISTING MAINTAINING A MINIMUM PAVEMENT STRUCTURE OF;

CONTRACTOR TO COMPLETE ROAD CUT AS PER CITY OF OTTAWA DETAIL R10. LINE PAINTING IS TO BE INCLUDED

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5430 Canotek Road | Ottawa, ON, K1J 9G2 www.lrl.ca I (613) 842-3434

UNPOISED ARCHITECTURE INC

APPROVED BY: DRAWN B M.B. К.Н. К.Н. PROJECT PROPOSED MULTI-UNIT COMMERCIAL DEVELOPMENT 5254 BANK STREET, OTTAWA DRAWING TITLE

SERVICING PLAN

PROJECT NO 220536

JUNE2022





EXISTING PROPERTY LINE TO REMAIN PROPOSED DEPRESSED CURB PROPOSED DOOR ENTRANCE/EXIT PROPOSED GRASS AREA (100mm TOP SOIL & SOD) PROPOSED CONCRETE FEATURES/SLAB PROPOSED HEAVY DUTY ASPHALT PROPOSED LIGHT DUTY ASPHALT PROPOSED RIP RAP PROPOSED ELEVATION PROPOSED HIGH POINT ELEVATION PROPOSED BOTTOM OF CURB / ASPHALT ELEVATION

PROPOSED TOP OF CURB ELEVATION PROPOSED EXPOSED BOTTOM OF RETAINING WALL PROPOSED TOP OF RETAINING WALL MATCH INTO EXISTING ELEVATION EXISTING ELEVATION

PROPOSED OVERLAND MAJOR FLOW ROUTE

— STM — STM — PROPOSED STORM SEWER ----- STM ----- STM ---- EXISTING STORM SEWER EXISTING CATCHBASIN-MANHOLE/MANHOLE EXISTING CATCHBASIN PROPOSED CATCHBASIN-MANHOLE/MANHOLE PROPOSED CATCHBASIN PROPOSED CURB STOP PROPOSED 100 YEAR HIGH WATER LEVEL

STORM WATERSHED EXTENT

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UNPOISED ARCHITECTURE INC

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К.Н.	К.Н.	M.B.						
PROJECT								
PROPOSED MULTI-UNIT COMMERCIAL DEVELOPMENT 5254 BANK STREET, OTTAWA								
DRAWING TITLE								
STORMWA	TER MANAG	EMENT PLAN						

C601

JUNE2022

PROJECT NO. 220536



EXISTING PROPERTY LINE TO REMAIN PROPOSED DEPRESSED CURB X PROPOSED SILT FENCE AS PER OPSD 219.110 PROPOSED DOOR ENTRANCE/EXIT PROPOSED GRASS AREA (100mm TOP SOIL & SOD) PROPOSED CONCRETE FEATURES/SLAB PROPOSED HEAVY DUTY ASPHALT PROPOSED LIGHT DUTY ASPHALT PROPOSED RIP RAP PROPOSED ELEVATION PROPOSED HIGH POINT ELEVATION PROPOSED BOTTOM OF CURB / ASPHALT ELEVATION PROPOSED TOP OF CURB ELEVATION PROPOSED EXPOSED BOTTOM OF RETAINING WALL PROPOSED TOP OF RETAINING WALL MATCH INTO EXISTING ELEVATION EXISTING ELEVATION PROPOSED OVERLAND MAJOR FLOW ROUTE

— STM — STM — PROPOSED STORM SEWER EXISTING CATCHBASIN-MANHOLE/MANHOLE EXISTING CATCHBASIN PROPOSED CATCHBASIN-MANHOLE/MANHOLE PROPOSED CATCHBASIN PROPOSED CURB STOP PROPOSED 100 YEAR HIGH WATER LEVEL

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> > -RUNOFF COEFFICIENT - AREA IN HECTARES

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5430 Canotek Road | Ottawa, ON, K1J 9G2 www.lrl.ca | (613) 842-3434

UNPOISED ARCHITECTURE INC

APPROVED BY: ESIGNED B DRAWN B M.B. К.Н. К.Н. PROJECT PROPOSED MULTI-UNIT COMMERCIAL DEVELOPMENT 5254 BANK STREET, OTTAWA DRAWING TITLE PRE-DEVELOPMENT

WATERSHED PLAN

PROJECT NO. 220536

JUNE2022

DATE





EXISTING PROPERTY LINE TO REMAIN PROPOSED DEPRESSED CURB PROPOSED SILT FENCE AS PER OPSD 219.110 PROPOSED DOOR ENTRANCE/EXIT PROPOSED GRASS AREA (100mm TOP SOIL & SOD) PROPOSED CONCRETE FEATURES/SLAB PROPOSED HEAVY DUTY ASPHALT PROPOSED LIGHT DUTY ASPHALT PROPOSED RIP RAP PROPOSED ELEVATION PROPOSED HIGH POINT ELEVATION PROPOSED BOTTOM OF CURB / ASPHALT ELEVATION

PROPOSED TOP OF CURB ELEVATION PROPOSED EXPOSED BOTTOM OF RETAINING WALL PROPOSED TOP OF RETAINING WALL MATCH INTO EXISTING ELEVATION EXISTING ELEVATION

PROPOSED OVERLAND MAJOR FLOW ROUTE

- STM - STM PROPOSED STORM SEWER ----- SAN ------ PROPOSED SANITARY SEWER ----- STM ----- EXISTING STORM SEWER EXISTING CATCHBASIN-MANHOLE/MANHOLE EXISTING CATCHBASIN PROPOSED CATCHBASIN-MANHOLE/MANHOLE PROPOSED CATCHBASIN PROPOSED CURB STOP PROPOSED 100 YEAR HIGH WATER LEVEL

STORM WATERSHED EXTENT

- AREA IN HECTARES

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UNPOISED ARCHITECTURE INC

APPROVED BY DRAWN B M.B. K.H. К.Н. PROJECT PROPOSED MULTI-UNIT COMMERCIAL DEVELOPMENT 5254 BANK STREET, OTTAWA DRAWING TITLE

POST-DEVELOPMENT WATERSHED PLAN

PROJECT NO. 220536

C702

JUNE2022



















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UNPOISED ARCHITECTURE INC

M.B.								
PROPOSED MULTI-UNIT COMMERCIAL DEVELOPMENT 5254 BANK STREET, OTTAWA								

DRAWING TITLE

CONSTRUCTION DETAIL PLAN

PROJECT NO. 220536

date JUNE2022



ATTACHMENT G

Septic Design Drawing (Absolute Drafting and Design)







L.

ATTACHMENT H

Eljen GSF Product Brochure

Geotextile Sand Filter

Eljen GSF System Overview

Innovative Onsite Products & Solutions Since 1970

www.eljen.com

Eljen GSF System Description

Each GSF Module is made up of geotextile fabric and a plastic core material that work together to provide vertical surface area and oxygen transfer. The GSF System applies secondary treated effluent to the soil, increasing the soil's long-term acceptance rate. A Specified Sand layer provides additional filtration, and prevents saturated conditions.

PRIMARY TREATMENT ZONE

- Perforated pipe is centered above the GSF Module to distribute septic effluent over and into corrugations created by the plastic core of the GSF Module.
- The Module's unique design provides increased surface area for biological treatment of nutrients and contaminants.
- Open air channels within the Module support aerobic bacterial growth on the Module's geotextile fabric interface, and promote oxygen in the system.
- An anti-siltation geotextile fabric covers the top and sides of the GSF Module to protect the system from the migration of fines.
- The GSF Module provides biomat management, and takes the burden of treatment and biomat development off of the native soil.

SECONDARY TREATMENT ZONE

- Effluent drips into the Specified Sand layer and supports unsaturated flow into the native soil.
- The Specified Sand layer also protects the soil from compaction and helps maintain cracks and crevices in the soil.
- Native soil provides final filtration and allows for groundwater recharge.

GSF SYSTEM OPERATION

Testing Overview and Performance

Certified to NSF/ANSI Standard 40

NSF Standard 40

This standard determines whether treatment systems product secondary treatment effluent quality, with Class I systems achieving a 30-day average ef-

fluent quality of 25 mg/L CBOD5 and 30 mg/L TSS or less, and pH 6.0-9.0. Testing and certification are done at an independent third party testing facility.

SETUP: Gravity GSF system with 6" of ASTM C33 sand in a bed configuration. 450 gal/day, (2.0 gal/ ft² loading rate).

RESULTS: The Eljen GSF is Tested and Certified by NSF to NSF Standard 40 Class 1 since 2014.

More information can be found at www.NSF.org.

NSF Standard 245

This standard includes Total Nitrogen reduction requirements with Class I systems achieving a 30-day average

effluent quality of more than 50% Total Certified to NSF/ANSI Standard 245 Nitrogen removal, 25 mg/L CBOD5 and 30 mg/L TSS or less, and PH 6.0-9.0. Testing and certification are done at an independent third party testing facility.

SETUP: Gravity GSF system in a bed configuration with 18" of ASTM C33 sand, 12" of sand/woodchip mixture, and 2" of limestone. 450 gal/day (2.0 gal/ft² loading rate).

RESULTS: Tested and Certified by NSF to NSF Standard 245 Class 1 since 2018.

More information can be found at www.NSF.org.

The third-party testing results listed below were taken over a 12 month consecutive period. This extended sampling period provided verification to the stability and consistency of the Eljen GSF's performance and capability to handle colder weather conditions. A summary of the test results from the independent third-party evaluation are listed below:

Eljen GSF A42 Modules Treatment Performance during third party 12 months testing (includes 12 consecutive weeks with influent temperature below 50° F)							
	CBOD (mg/L)	TSS (mg/L)	Fecal Coliform (MPN/100ml)				
Average	2.0	2.7	66*				
Average (cold water period)	1.2	1.7	13*				
Median	1.0	2.5	71*				
Min Value	1.0	2.5	2*				
Max Value	7.2	7.0	10 965*				

*Geometric average

Eljen GSF - A42 Influent and Effluent Temperature (degree F)

---- In ue nt Temperature ----- E°u ent Temperature

COMPANY HISTORY

Established in 1970, Eljen Corporation created the world's first prefabricated drainage system for foundation drainage and erosion control applications. In the mid-1980s, we introduced our Geotextile Sand Filter products for the passive advanced treatment of onsite wastewater in both residential and commercial applications. Today, Eljen is a global leader in providing innovative products and solutions for protecting our environment and public health.

COMPANY PHILOSOPHY

Eljen Corporation is committed to advancing the onsite industry through continuous development of innovative new products, delivering high-quality products and services to our customers at the best price, and building lasting partnerships with our employees, suppliers, and customers.

Innovative Onsite Products & Solutions Since 1970

Tel: 800-444-1359 • Fax: 860-610-0427

www.eljen.com

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