4 Campbell Reid Court, Dunrobin Site Servicing and Stormwater Management Report



Project # CW-05-21

Prepared for:

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1405 Houston Cres.,

Ottawa, ON, K2W 1B6

By:

Arch-Nova Design Inc.

September 2022

Updated April 2023

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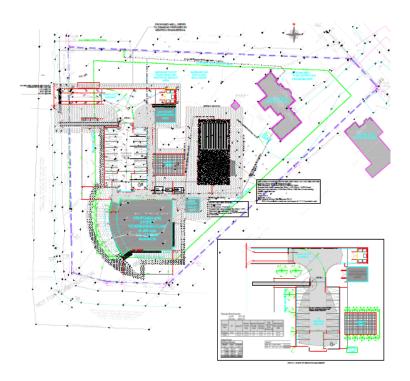
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1. Introduction

The subject property is located at 4 Campbell Reid Court, Ottawa. The proposed work comprises of a veterinary clinic building, a parking and amenity area and storage sheds.



4 Campbell Reid Court, Ottawa: Site Plan

Currently the property is used as a residential with a house located along the north edge of the property. The property is surrounded by Dunrobin Road on its west side, March Road on south and Cameron Harvey Road on its north edge. The east side borders with another residential property. Between the property and Dunrobin and March Road an existing drain runs toward south and south-east. Its purpose is to drain water from properties along Dunrobin Road. The grade of the property raises from 93.10 m on east corner to 93.49 m on its west side at the entrance to the site.

The drain's depth varies from 0.3m to 0.5 m.

"Hydrogeological Investigation and Terrain Assessment "1 report provided information on existing and proposed water well and septic systems on site. In general, the report suggested drilling a new well and installation of a new septic system for the clinic. Existing well is susceptible to increased chlorides and it is not recommended for

¹ GEMTEC: "Hydrogeological Investigation and Terrain Assessment" July 2022

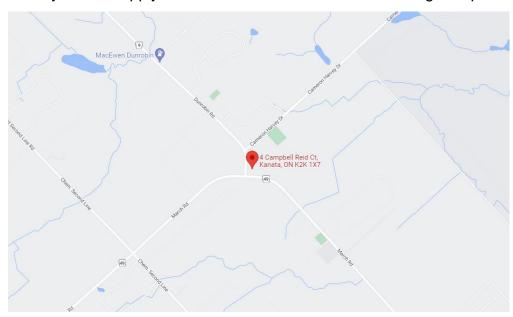
use in the clinic. A newly drilled well was tested and the flow and yield are recorded. A complete geo data as well as terrain analysis are provided in GEMTEC's report.

The new well was tested for 8 hours and samples were taken to the laboratory for: bacteriological, chemical, physical (hardness), metals, chlorides and total dissolved solids.

The water level was monitored for 30 days and fluctuation recorded was between 1.3-1.8 m below casing.

All tested materials had elevated results however, after repeated pumping some of readings decreased to acceptable levels. This trend of normalizing of all components is expected in the future.

In conclusion the report assessed the new well (TW22-1) as capable of pumping 20 m³ of water daily and to supply both: the clinic and residential building if required.



4 Campbell Reid Court, Ottawa: Location

2. Public Services Capacity

This section of the report will analyze existing municipal services and the potential impact of the proposed building at 4 Campbell Reid Court on the existing service capacity.

2.1 Water Supply

The entire site is supplied by a private well. The capacity of newly drilled well is capable of pumping 20 m³ of water daily and to supply both: the clinic and residential building.

The existing well is deemed as unsuitable for domestic water supply as the level of chlorides and nitrates is above acceptable. The well will be abandoned and capped.

The new well is proposed to be connected to the clinic by 32 mm pipe as well as a second branch 32 mm diameter to the residential building. It was recommended to have a hydrocell pumping system inside the clinic building as well as a small tank so the well pump is not running all the time. The house should have the same hydrocell system too.

Fire protection in the area is provided from Fire Station #45 at 640 Cameron Harvey Drive. Distance from the fire station to 4 Campbell Reid is 580 m.

Calculated fire demand is 3,000 l/min or 360 m³ of water for duration of 2 hours.

Following table is showing required flow for establishment like a veterinary clinic and required pressure for operation of the hydrocell pumps inside the building. It will be a responsibility of the owner and contractor to choose and install the pumping system and a reservoir, if required. Also, the pressure in the plumbing system will be determined by a mechanical engineer based on the equipment requirements.

Water Supply Design Criteria

Trater Supply Design Criteria	
Design Parameter	Value
Residential Average Apartment	1.8 P/unit
Residential Average Daily Demand	280 L/d/P
Residential Maximum Daily Demand	9.5 x Average Daily *
Residential Maximum Hourly	1.5 x Maximum Daily *
Other Occupancy OBC Table 8.2.1.3 B: Vet Clinic	275/practitioner, 75/employee (8 hour shift)
Commercial Maximum Daily Demand	1.5 x Average Daily
Commercial Maximum Hourly	1.8 x Maximum Daily
Minimum Watermain Size	
Minimum Depth of Cover	2.4m from top of watermain to finished grade
During Peak Hourly Demand operating pressure must remain within	275kPa and 552kPa (40-80 psi; 28-56m)

^{*} Residential Max. Daily and Max. Hourly peaking factors per MOE Guidelines for Drinking-Water Systems Table 3-3 for 0 to 500 persons.

Table 1: Water Supply Design Criteria



Fire Station #45: location and distance

2.2 Sanitary Sewer

Sanitary sewer service will be provided on site by a septic system. The new development is characterized as a medical practice (veterinary clinic) with total of 3 practitioners and 10 personnel for duration of one shift of 8 hours. Ontario Building Code (OBC) "Table 8.2.1.3.B - Other Occupancies" is used for sizing the onsite sanitary system: for practitioners 275 I/day and for employees per 8-hour shift 75 I/day.

Infiltration and inflow of 0.33 l/s/ha was considered for the calculation however, the property drains toward drain channels around and away from the proposed location of sewer laterals and septic tank so the infiltration rate into the sewer laterals and the septic tank is assessed as very small to insignificant.

In addition to the statement above it is anticipated that the filter bed will be fully raised construction so no impact from ground water is expected.

The estimated outflow for the new building is **0.02 l/sec** (Average Dry Weather Flow).

Detailed calculation of pre and post development flow is presented in Appendix A.

2.3 Septic System

As the area is not serviced by municipal sewage, an onsite septic system is proposed. Based on the outflow calculation of 1,575 l/day, required primary septic tank capacity is calculated to be 5,000 liters.

Existing residential building is already serviced by a septic system and fully raised filter bed. This system also has a capacity of 5,000 liters for the septic tank.

A recommendation is to install a 10,000 liters tertiary system to service both, the clinic and the residential building. The existing septic system for the residential building will be disconnected and cleaned from the property upon the new system is built. similar model for the veterinary clinic for the reason of standardized maintenance and operation.

The proposed filter bed will be Class 4 raised filter bed and it has 10 (ten) runs. Total inflow to the filter bed from the clinic and the house is calculated to be 3,900 l/day. Percolation rate is estimated to 11.5 min/cm with loading rates of 10 l/m²/day. Minimum required filter bed loading area is calculated to 78.0 m² however, the bed is sized 110 m² with extended contact area of 52.76 m². The reason for oversizing is in potential lower rate of loading.

The design will be submitted to the Ottawa Septic System Office (OSSO) upon the acceptance of conceptual design provided in this report.

As stated above, it is recommended to construct the same type of septic and filter bed as the existing one. As-built plans of existing system are presented in Appendix C.

2.4 Site Stormwater Services

Current site and the rest of surface of the lot at 4 Campbell Reid Court represent a typical rural site with a residential building on north side and forested and open space toward south. In this area the existing sewage filter bed is located. All stormwater runoff is under uncontrolled condition. Along the property's west side and Dunrobin road an existing drain runs in direction north-south. Current entrance from Dunrobin to the site will be retained. A culvert is installed at the location. It appears as a concrete pipe. As a new access driveway will be wider new culverts are proposed: twin 375 mm corrugated steel pipes, 10.4 m long. There are no other significant physical features of the area such as depressions, wet land or surface retention.

The proposed development will have large impervious areas such as roofs, parking's and driveways. Modified rational method was used to assess an excess runoff and onsite storage volume. An assumption was that the predevelopment runoff coefficient is C=0.25. The ground water level is relatively low so the infiltration is good with minimum or no surface runoff.

For the post development analysis, the sub-catchments are delineated. The uncontrolled runoff area is measured 0.3974 ha with weighted factor of 0.38 (landscape, building, amenity areas, sheds).

Surface Type	ID	Area (ha)	Percent of total Area	С	A X C (ha)
Landscape	A3	0.2297	57.8%	0.25	0.057
Amenity Area	A4	0.1172	29.5%	0.40	0.047
Building	A 5	0.0505	12.7%	0.90	0.045
TOTAL		0.3974	100.0%		0.150
Weighted C =					0.38

The controlled area is measured 0.08452 ha with weighted runoff factor of 0.9 (parking).

Surface Type	ID	Area (ha)	Percent of total Area	С	A X C (ha)
Parking	A 1	0.0757	89.6%	0.90	0.068
Shed 1	A2	0.0051	6.0%	0.90	0.005
Shed 2	A6	0.0037	4.4%	0.90	0.003
TOTAL		0.08452	4.4%		0.076
Weighted C =					0.90

The parking area will be graded to create a storage for excess of water. Total controlled runoff is calculated to be 3.77 l/sec.

Predevelopment Runoff:							
Uncontrolled Runoff							
2-year	36.01	l/sec					
100-year	104.67	l/sec					
Controlled	Controlled Runoff:						
2-year	0.00	l/sec					
100-year	0.00	l/sec					

Postdevelopment Runoff:							
Uncontrolled	Uncontrolled Runoff						
2-year	32.24	l/sec					
100-year	93.71	l/sec					
Controlled R	Controlled Runoff:						
2-year	16.24	l/sec					
100-year	41.96	l/sec					

Controlled allowable runoff					
Controlled Runoff:					
2-year	3.77	l/sec			

100-year storage volume required to be stored on site and released under predevelopment 2-year runoff is:

Stage-Storage

Parking Storage						
Depth	Volume					
m	m^2	m^3				
0.030	250.0	2.50				
0.081	324.0	8.75				
0.14	475.0	22.17				
0.194	525.0	33.95				

The 100-year predevelopment runoff is 104.67 l/sec. The post development 100-year uncontrolled runoff is 93.71 l/sec and with the controlled outflow of 3.77 l/sec it will make total of 97.48 l/sec which is less than the predevelopment 100-year runoff.

Difference in elevations between proposed parking lot and the existing drain is only 0.5 m so any standard inlet control device cannot be installed. For such a reason a curb installed 100 mm pipe with opening of 60% was designed. It releases water into a swale 1.45 m wide and 23.0 m long at 2.1% slope, connecting the parking and the ditch. The bottom of the swale is proposed to be covered with a large river rock material. It will also serve capture small particles before water reaches the ditch.

Top of the curb is set at 0.175 m above the bottom of inlet. It will serve as the storage depth control as well as an emergency overflow point.

2.5 Site Grading

The site grading is designed to create a storage for the stormwater on the parking area and to evacuate water from the access areas to the facility. Slopes toward existing drain and the site access driveway maintained and will not change general pattern od runoff or cause erosion.

Area south-west from existing filter bed is reserved for the extension and the grading will match the existing grading of the filter bed.

3. Conclusion and Recommendation

3.1 Water Supply

The site is serviced from existing well which is deemed as not suitable based on the quality of water. A new well was drilled and it has sufficient capacity to service both: the residential house and the new veterinary clinic.

3.2 Sanitary Sewer

The site (existing house) is serviced by a septic system however a new filter bed is proposed and will serve both: the house and the clinic. A new septic tank for the clinic and the existing house with capacity of 10,000 liters will be installed beside the clinic's building and connected by forcemain the filter bed. The filter bed consists of 10 runs and with extended contact area.

The design will be submitted to the Ottawa Septic System Office (OSSO) upon the acceptance of conceptual design provided in this report.

3.3 Stormwater

The 100-year predevelopment runoff is 104.67 l/sec. The post development 100-year uncontrolled runoff is 93.71 l/sec and with the controlled outflow of 3.77 l/sec it will make total of 97.48 l/sec which is less than the predevelopment 100-year runoff.

Difference in elevations between proposed parking lot and the existing drain is only 0.5 m so any standard inlet control device cannot be installed. For such a reason a curb installed 100 mm pipe with opening of 60% was designed. It releases water into a swale 1.45 m wide and 23.0 m long at 2.1% slope, connecting the parking and the ditch. The bottom of the swale is proposed to be covered with a large river rock material. It will also serve capture small particles before water reaches the ditch.

Existing driveway/access to the site will remain in function but widened and with asphalt surface. As a new access driveway will be wider new culverts are proposed: twin 375 mm corrugated steel pipes, 10.4 m long. The existing ditch will remain unchanged as it appears operational. New swale connecting the parking and the ditch will function to direct water from the parking to the ditch as well as to dissipate water to settle particles (quality control).

Prepared by:

Zoran Mrdja, P.Eng., FEC

September, 2022 Updated: April 2023



Professional Engineers
Ontario

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Appendix A: Calculations

4 Campbell Reid Crt.



PRE-DEVELOPMENT

The pre-development time of concentration is

10 minutes

where:

 $I_2 = 732.951 / (Tc + 6.199)^{0.810}$

 $I_{100} = 1735.688 / (Tc + 6.014)^{0.820}$

 $l_2 = 76.8 \text{ mm/hr}$

 $I_{100} = 178.6 \text{ mm/hr}$

Surface Type	ID	Area (ha)	Percent of total Area	С	A X C (ha)
Site	A 1	0.48185	100.0%	0.35	0.169
			<u> </u>		
TOTAL		0.4819	100.0%	•	0.169
Weighted C =					0.35

$$Q_{2pre} = (2.78)^*(C)^*(I_5)_*(A)$$

$$Q_{2pre} = 2.78 \text{ x} 0.35 \text{ x} 76.8 \text{ x} 0.4819$$

$$Q_{2pre} = 36.01 \text{ L/s}$$

 $Q_{100pre} = (2.78)^*(C)^*(I_{100})_*(A)$

$$Q_{100pre} = 2.78 x 0.44 x 178.6 x 0.4819$$

$$Q_{100pre} = 104.67 \text{ L/s}$$

POST-DEVELOPMENT (UNCONTROLLED RUNOFF)

The post-development time of concentration is 10 minutes

where:

$$I_2 = 732.951 / (Tc + 6.199)^{0.810}$$

$$l_2 = 76.8 \text{ mm/hr}$$

 $I_{100} = 1735.688 / (Tc + 6.014)^{0.820}$

I₁₀₀ = **178.6** mm/hr

Surface Type	ID	Area (ha)	Percent of total Area	С	A X C (ha)
Landscape	A3	0.2297	57.8%	0.25	0.057
Amenity Area	A4	0.1172	29.5%	0.40	0.047
Building	A 5	0.0505	12.7%	0.90	0.045
TOTAL		0.3974	100.0%		0.150
Weighted C =					0.38

 $Q_{2post} = (2.78)^*(C)^*(I_5)_*(A)$

 $Q_{2post} = 2.78 x 0.38 x 76.8 x 0.3974$

 $Q_{2post} = 32.24 \text{ L/s}$

 $Q_{100post} = (2.78)^*(C)^*(I_{100})_*(A)$

 $Q_{100post} = 2.78 x 0.48 x 178.6 x 0.3974$

 $Q_{100post} = 93.71 \text{ L/s}$

4 Campbell Reid Crt.



PRE-DEVELOPMENT (CONTROLLED RUNOFF)

The pre-development time of concentration is

10 minutes

where:

 $I_2 = 732.951 / (Tc + 6.199)^{0.810}$

₂ = 76.8 mm/hr

l₁₀₀ = 178.6 mm/hr

Surface Type	ID	Area (ha)	Percent of total Area	С	A X C (ha)
Site	A1	0.00000	0.0%	0.25	0.000
TOTAL		0.0000	0.0%	·	0.000
Weighted C = 0.00					

C=0.6 used for predevelopment calculation (City of Ottawa requirement)

$Q_{2pre} = (2.78)$)*(C)*(I ₂) _* (A	4)			
$Q_{2pre} =$	2.78 x	0.00	Х	76.8	x 0.0000
Q _{2pre} =	0.00 L/s				

$$Q_{100pre} = (2.78)^*(C)^*(I_{100})_*(A)$$

 $Q_{100pre} =$ 2.78 x 0.00 x 178.6 x 0.0000

 $Q_{100pre} = 0.00 L/s$

POST-DEVELOPMENT (CONTROLLED RUNOFF)

The post-development time of concentration is

10 minutes

where:

 $I_2 = 732.951 / (Tc + 6.199)^{0.810}$

₂ = 76.8 mm/hr

 $I_{100} = 1735.688 / (Tc + 6.014)^{0.820}$ $I_{100} = 178.6 \text{ mm/hr}$

Surface Type	ID	Area (ha)	Percent of total Area	С	A X C (ha)
Parking	A 1	0.0757	89.6%	0.90	0.068
Shed 1	A2	0.0051	6.0%	0.90	0.005
Shed 2	A6	0.0037	4.4%	0.90	0.003
TOTAL		0.08452	4.4%		0.076
TOTAL Weighted C =		0.08452	4.4%		0.

 $\begin{aligned} &Q_{2post} = (2.78)^*(C)^*(I_2) \cdot (A) \\ &Q_{2post} = & 2.78 \ x & 0.90 \ x & 76.8 \ x & 0.0845 \end{aligned}$

 $Q_{2post} = 16.24 \text{ L/s}$

 $Q_{100post} = (2.78)^*(C)^*(I_{100})_*(A)$

 $Q_{100post} = 2.78 x 1.00 x 178.6 x 0.0845$

 $Q_{100post} = 41.96 \text{ L/s}$

ALLOWABLE RUNOFF

Predevelopment Runoff:

Uncontrolled Runoff						
2-year	36.01	l/sec				
100-year	104.67	l/sec				
Controlled Runoff:						
2-year	0.00	l/sec				
100-year	0.00	l/sec				



Postdevelopment Runoff:							
Uncontrolle	Uncontrolled Runoff						
2-year	32.24	l/sec					
100-year	93.71	l/sec					
Controlled Runoff:							
2-year	16.24	l/sec					
100-vear	41.96	l/sec					

Controlled allowable runoff Controlled Runoff: 2-year 3.77 l/sec

Comment:

Storage Volumes (2-Year Storm)

Project: 384 Frank St.

 $Tc = \underline{\qquad} 10 \qquad \text{(mins)}$

 $C_{AVG} = \frac{0.90}{\text{(dimmensionless)}}$

Area = 0.0845 (hectares)

 $Storm = \frac{2}{2} \qquad (year)$

Release Rate = 3.77 (L/sec)

Time Interval = $\frac{3.77}{10}$ (mins)

	Rainfall				_
Duration	Intensity	Peak Flow	Release Rate	Storage Rate	Storage
(min)	(mm/hr)	(L/sec)	(L/sec)	(L/sec)	(m^3)
1	148	3.1	3.77		
11	73	15.5	3.77	11.70	7.72
21	50	10.7	3.77	6.91	8.70
31	39	8.3	3.77	4.51	8.40
41	32	6.8	3.77	3.06	7.53
51	28	5.8	3.77	2.08	6.36
61	24	5.1	3.77	1.36	4.98
71	22	4.6	3.77	0.82	3.48
81	20	4.2	3.77	0.39	1.88
91	18	3.8	3.77	0.04	0.20
101	17	3.5	3.77	-0.25	-1.54
111	15	3.3	3.77	-0.50	-3.32
121	14	3.1	3.77	-0.71	-5.15
131	14	2.9	3.77	-0.89	-7.00
141	13	2.7	3.77	-1.05	-8.88
151	12	2.6	3.77	-1.19	-10.79
161	12	2.5	3.77	-1.32	-12.72
171	11	2.3	3.77	-1.43	-14.66
181	11	2.2	3.77	-1.53	-16.63
191	10	2.1	3.77	-1.62	-18.60
201	10	2.1	3.77	-1.71	-20.59
211	9	2.0	3.77	-1.78	-22.60
221	9	1.9	3.77	-1.86	-24.61
231	9	1.8	3.77	-1.92	-26.63
241	8	1.8	3.77	-1.98	-28.66
251	8	1.7	3.77	-2.04	-30.70
261	8	1.7	3.77	-2.09	-32.75
271	7.7	1.6	3.77	-2.14	-34.80

Notes

- 1) For a storm duration that is less than the time of concentration the peak flow is equal to the product of 2.78CIA and the ratio of the storm duration to the time of concentration.
- 2) Rainfall Intensity, I = 732.951 / (Tc + 6.199)^0.810 (2 year, City of Ottawa)
- 3) Peak Flow = Duration/Tc x 2.78 x C x I x A (Duration < Tc)
- 4) Peak Flow = 2.78 x C x I x A (Duration > Tc)
- 5) Storage = Duration x Storage Rate

Storage Volumes (100-Year Storm)

 $Tc = \underline{10}$ (mins)

 $C_{AVG} = 1.00$ (dimmensionless)

Area = 0.0845 (hectares)

Storm = $\frac{100}{100}$ (year)

Release Rate = $\frac{3.77}{\text{L/sec}}$ (L/sec) Time Interval = $\frac{10}{\text{mins}}$

	ı	1	I		
Duration	Rainfall	Peak Flow	Release Rate	Storage Date	Storage
	Intensity			Storage Rate	(m^3)
(min)	(mm/hr)	(L/sec)	(L/sec)	(L/sec)	(III)
1	351	8.3	3.77	26.15	22.06
11	170	39.9	3.77	36.15	23.86
21	116	27.3	3.77	23.56	29.68
31	90	21.1	3.77	17.34	32.25
41	74	17.3	3.77	13.58	33.41
51	63	14.8	3.77	11.04	33.79
61	55	13.0	3.77	9.20	33.69
71	49	11.6	3.77	7.81	33.25
81	45	10.5	3.77	6.70	32.58
91	41	9.6	3.77	5.81	31.72
101	38	8.8	3.77	5.07	30.72
111	35	8.2	3.77	4.44	29.60
121	33	7.7	3.77	3.91	28.39
131	31	7.2	3.77	3.45	27.10
141	29	6.8	3.77	3.04	25.74
151	27	6.5	3.77	2.69	24.33
161	26	6.1	3.77	2.37	22.86
171	25	5.8	3.77	2.08	21.35
181	24	5.6	3.77	1.82	19.80
191	23	5.4	3.77	1.59	18.21
201	22	5.1	3.77	1.38	16.60
211	21	4.9	3.77	1.18	14.95
221	20	4.8	3.77	1.00	13.28
231	20	4.6	3.77	0.84	11.58
241	19	4.5	3.77	0.68	9.87
251	18	4.3	3.77	0.54	8.13
261	18	4.2	3.77	0.41	6.38
271	17	4.1	3.77	0.28	4.60
Mataa	-	-			

Notes

- 1) For a storm duration that is less than the time of concentration the peak flow is equal to the product of 2.78CIA and the ratio of the storm duration to the time of concentration.
- 2) Rainfall Intensity, I = 1735.688 / (Tc + 6.014)^0.820 (100 year, City of Ottawa)
- 3) Peak Flow = Duration/Tc x 2.78 x C x I x A (Duration < Tc)
- 4) Peak Flow = 2.78 x C x I x A (Duration > Tc)
- 5) Storage = Duration x Storage Rate



Storage Requirements

2-year **8.70 m³** 100-year **33.79 m³**

Surface Type	ID	Area (m²)	Percent of total Area	Required Storage 2 year	Required Storage 100 year	Max Allowed Drain Outflow I/s	Max Allowed Drain Outflow GPM
Parking	ICD	525.00	100.0%	8.70	33.79	3.77	59.73
TOTAL		525.00	100.0%	8.70	33.79	3.77	59.73

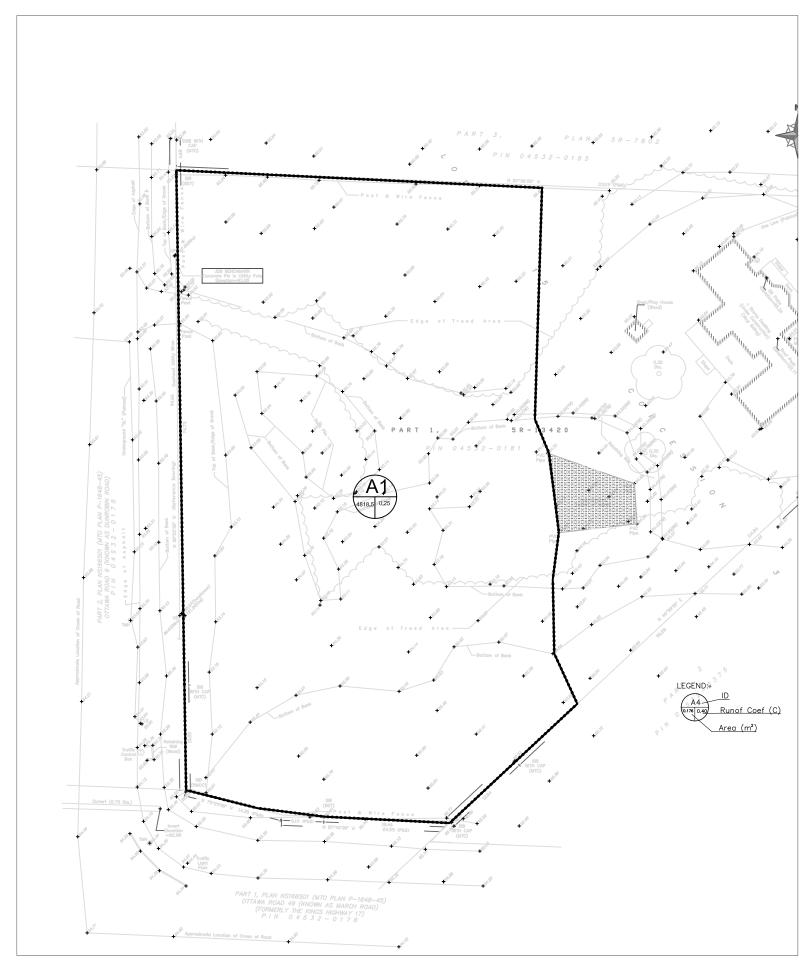
Stage-Storage

Olage-Olorage						
Parking Storage						
Depth	Area	Volume				
m	m^2	m^3				
0.030	250.0	2.50				
0.081	324.0	8.75				
0.14	475.0	22.17				
0.194	525.0	33.95				

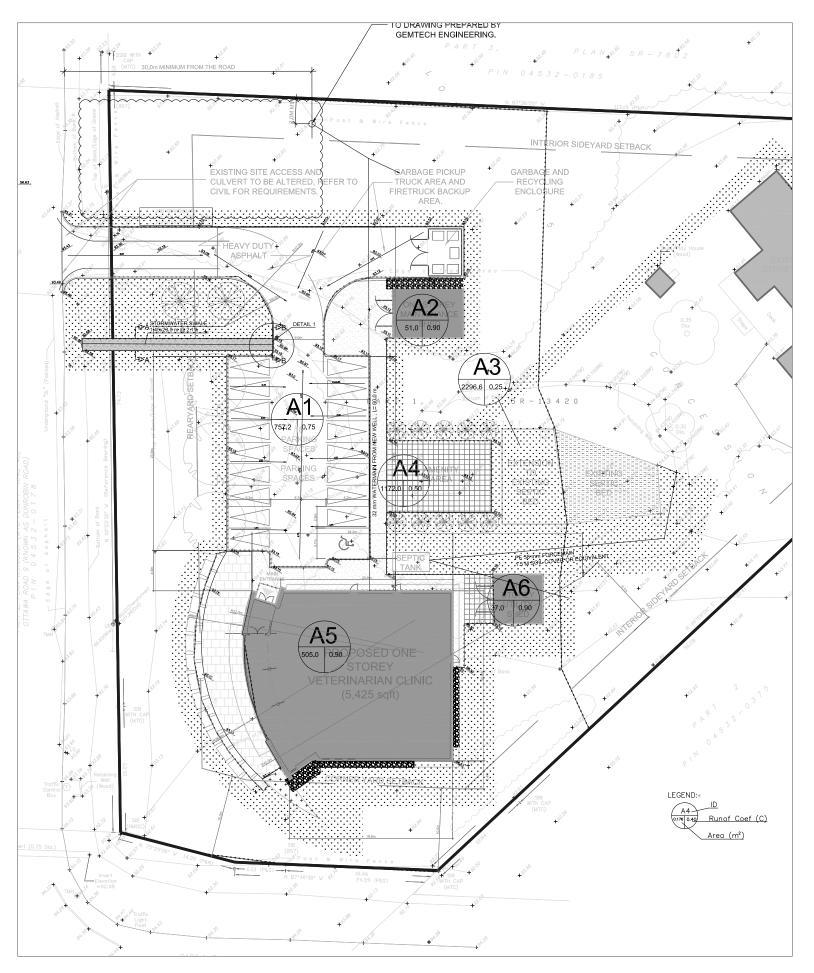
Legend:	
data for 2-year event	
data for 100-year event	

Notes:





4 Campbell Reid Crt., Donrobin SWM PREDEVELOPMENT



4 Campbell Reid Crt., Donrobin SWM POSTDEVELOPMENT

ARCH-NOVA Design Inc.

DESIGN CALCULATIONS FOR CLASS 2, 4 & 5 ON-SITE SEWAGE SYSTEM

Owner: Dr. Olander	Designer: Mrdja	2022-09-23

STEP 1

DAILY SEWAGE FLOW (Based on Hydraulic Loads for Fixtures, Floor Area, and Number of Bedrooms)

Plumbing Fixture Description	Existing Number of Fixtures	Proposed Number of Fixtures	Total x Fixture Units Value = Number of Fixture Units			
Bathroom group	2					
(toilet, sink, bathtub)			2	6	12	
Toilet (alone)	1		1	4	4	
Washbasin	2		2	1.5	3	
Bathtub or Shower	1		1	1.5	1.5	
Kitchen Sink(s)	1		1	1.5	1.5	
Bar Sink			0	1.5	0	
Dishwasher	1		1	1.5	1.5	
Washing Machine	1		1	1.5	1.5	
Bidet			0	1	0	
Laundry Tub	1		1	1.5	1.5	
Other:			0		0	
Total Fixture Units 26.5						

Proposed: 220 m² 2368.1 ft² **Existing:** 195 m² 2099 ft²

Total Finished Floor Area Excluding Area of Finished Basement

 0.00 m^2 0.00 ft^2

(Multiply $m_2 \times 10.764 = ft^2$)

From the chart below, please calculate the expected daily sewage flow for your proposed building, and mark the total in the space provided. For non-residential occupancies see Table 8.2.1.3 B O.B.C.

Residential Occupancy	Existing	Q in Litres	Calculations
1 Bedroom		750	0
2 Bedrooms		1100	0
3 Bedrooms		1600	0
4 Bedrooms	1	2000	2000
5 Bedrooms		2500	0
Additional Flow for:			0
Each Bedroom over 5		500	0
Floor Space for each 10m ² over 200 m ² up to 400 m ²	0	100	0
Floor Space for each 10m ² over 400 m ² up to 600 m ²		75	0
Floor Space for each 10m ² over 600 m ² OR*		50	0
Each fixture unit over 20 fixture units total	6.5	50	325
Total	_	_	2325

*NOTE: Where you need to do multiple calculations, signified by the "OR" in the table, do the calculation for daily sewage flow based on bedrooms and floor space first, then fixture units, and use the larger of the two calculations.

Other Occupancy (Table 8.2.1.3 (B)			
Establishment Type: Veterinary Clinic	Occupant Load	Volume (Liters)	Calculations
Per practitioner	3	275	825
Per employee per 8 hours shift	10	75	750
Per stall, kennel or cage if floor drain connected		75	0
	•	Total	1575

EXPECTED DAILY DESIGN SEWAGE FLOW (Q)

3,900.00

Liters

(Use Q for the following calculations)

Soil Type	Coarse Gravel, no fines	Gravel, some small rocks	Gravel, sand mix, some fines	Sand, fairly uniform, some fines	Sandy, Loam mix	Silty, Loam, almost clay	Clay, smears well, rolls into ribbon
T-time Min/cm	0 to 1	1 to 5	5 to 10	10 to 15	15 to 25	25 to 50	> 50

ON-SITE PROFILE (Subtract useable depth of Soil from 1.5m (5') for depth of imported fill)

Soil Depth Meters	Percolation Rate T	Soil Type (see above)	Depth of Rock/Impervious Soil/GroundwaterTable √	Topsoil to	Topsoil to be removed:			
0.2				Depth		m	0	(ft)
0.4				Usable Ex	isting Soil:			
0.6	11.5	sand	1	Depth	0.25	m	0.825	(ft)
0.8				Imported	Fill:			
1.0				Depth	0.75	m	2.475	(ft)
1.2				Percolation	n Rate	(T)	10	min/cm
1.4				Excavatio	n of Existing	Soil:		
1.4				Depth		m	0	(ft)
1.6								
CONTACT ARE	A CAI CUI ATIO	N						

If you do not have a minimum of 250 mm (10") of useable soil on the property, you will need to import the mantle, or contact area. Choose T range, divide Q by Loading Rate for T.

Percolation Time (T) of Soil (min/cm)	Loading Rates (L/m ₂ /day)	Q
1 < T ≤ 20	10	3900
20 < T ≤	8	
35 < T ≤	6	
T > 50	4	
Column 1	2	

Contact Area Daily Sewage Flow (Q)+ Loading Rate = 390.00

STEP 3

A) SEPTIC TANK SIZE CALCULATION To calculate the minimum capacity of your septic tank, use the

following formulas. Minimum tank size is 3600 Litres.

Residential:	Q	=	2325	2 x Q =	4650	Litres	Tank Size:	5,000.00
Other Occupants:	Q	=	1,575.00	3 x Q =	4,725.00	Litres	Tank Size:	5,000.00

B) LEACHING BED LENGTH CALCULATION (Divide meters by 0.305 to convert to feet)

Length (m)= (QxT)/200 224.25 (m) 735.25 ft

DESCRIPTION

Number of Runs:	10	D - Box	Y	N	Header	1	Y	N
Distance between runs	1.60							
Run length	22.43							
Leaching Bed Width	33.00							
Leaching Bed Area	872.03							

FILTER BED

Where you may not have sufficient area on your property to install a leaching bed, you may install a filter bed for your distribution system.

FILTER BED CALCULATION (Multiply m₂ x 10.764 to convert T to ft₂)

If your daily sewage flow is less than 3000 litres per day, perform calculation 1), or if your daily sewage flow exceeds 3000 litres per day, perform calculation 2).

1) Filter Bed Surface Area = Q ÷75 expressed as m ²										
Q	3,900.00	/	75 =	52.00	m^2					
2) Filter Bed Surface Area = Q ÷50 expressed as m ²										
2) Filter E	Bed Surfa	ce Area	a = Q ÷50	express	sed as m²					

Where Percolation Rate T < 11.5 then Q/75 = Area of filter bed

 m^2 or m^2 or m^2 or m^2

The total square area is calculated by measuring the length, and multiplying it against the width. In most instances, the filter bed is constructed long and narrow, as opposed to a square. This helps the bed "breathe," as more oxygen can penetrate the filter bed from the sides, and from above.

Filter Bed Loading	78.00	m²	Length m	11	Width m	7.09
Area	839.59	ft ²	Length ft	36.30	Width ft	23.40

EXTENDED CONTACT AREA

Where Percolation Rate T > 11.5 then (Q x T)/850 = Extended Contact Area m₂ or **52.76** Filter Bed Loading Width m 4.80 52.76 m^2 Length m 11 ft² 36.30 15.83 567.96 Length ft Width ft

Water Supply Design Criteria

Design Parameter	Value
Residential Average Apartment	1.8 P/unit
Residential Average Daily Demand	280 L/d/P
Residential Maximum Daily Demand	9.5 x Average Daily *
Residential Maximum Hourly	1.5 x Maximum Daily *
Other Occupancy OBC Table 8.2.1.3 B: Vet Clinic	275/practitioner, 75/employee (8 hour shift)
Commercial Maximum Daily Demand	1.5 x Average Daily
Commercial Maximum Hourly	1.8 x Maximum Daily
Minimum Watermain Size	150mm diameter
Minimum Depth of Cover	2.4m from top of watermain to finished grade
must remain within	275kPa and 552kPa (40-80 psi; 28-56m)
During fire flow operating pressure must not drop below	140kPa (20 psi; 14 m)

^{*} Residential Max. Daily and Max. Hourly peaking factors per MOE Guidelines for Drinking-Water Systems Table 3-3 for 0 to 500 persons.

Water Demand and Boundary Conditions Proposed Conditions

Design Parameter	Anticipated Demand ¹ (L/min)	Boundary Condition ² (m)
Average Daily Demand	1.09	
Max Day + Fire Flow	3,001.64	
Peak Hour	2.95	

¹⁾ Water demand calculation per Water Supply Guidelines. See Appendix B for detailed calculations.

²⁾ Boundary conditions supplied by the City of Ottawa. See Appendix B for correspondence with the City.

Domestic Demand

Type of Housing	Per / Unit	Units	Pop
Single Family	3.4	0	0
Semi-detached	2.7		0
Townhouse	2.7		0
Apartment			0
Bachelor	1.4		0
1 Bedroom	1.4		0
2 Bedroom	2.1		0
3 Bedroom	3.1		0
4 Bedroom	4.2	0	0

	Pop	Avg. Daily		y Max Day		Peak Hour	
		m³/d L/min		m³/d	L/min	m³/d	L/min
Total Domestic Demand	0	0.00	0.00	0.00	0.00	0.00	0.00

Institutional / Commercial / Industrial Demand

				Avg. Daily		Max Day		Peak Hour	
Property Type	Uni	it Rate	Units	m³/d	L/min	m³/d	L/min	m³/d	L/min
Commercial floor space	2.5	L/m ² /d							
Office	75.0	L/9.3m ² /d							
Veterinary Clinic	275.0	L/practitioner/d	3	0.83	0.57	1.24	0.86	2.23	1.55
Veterinary Clinic	75.0	L/employee/d	10	0.75	0.52	1.13	0.78	2.03	1.41
Industrial -Heavy	55,000.0	L/gross ha/d							
		Total I/	C/I Demand	1.58	1.09	2.36	1.64	4.25	2.95

Total Demand	1.58	1.09	2.36	1.64	4.25	2.95

^{*} Estimated number of seats at 1seat per 9.3m²

Water Supply Design Criteria

Design Parameter	Value
Residential Average Apartment	1.8 P/unit
Residential Average Daily Demand	280 L/d/P
Residential Maximum Daily Demand	2.5 x Average Daily *
Residential Maximum Hourly	2.2 x Maximum Daily *
Commercial Demand	2.5 L / m2 /d
Commercial Maximum Daily Demand	1.5 x Average Daily
Commercial Maximum Hourly	1.8 x Maximum Daily
Minimum Watermain Size	150mm diameter
Minimum Depth of Cover	2.4m from top of watermain to finished grade
must remain within	275kPa and 552kPa
During fire flow operating pressure must not drop	
below	140kPa

^{*} Residential Max. Daily and Max. Hourly peaking factors per MOE Guidelines for Drinking-Water Systems Table 3-3 for 0 to 500 persons.

Water Demand and Boundary Conditions Proposed Conditions

Design Parameter	Anticipated Demand ¹ (L/min)	Boundary Condition ² (kPa)
Average Daily Demand	1.09	
Max Day + Fire Flow	3,002.95	
Peak Hour	2.95	

¹⁾ Water demand calculation per Water Supply Guidelines. See Appendix B for detailed calculations.

 $^{^{2)}}$ Boundary conditions supplied by the City of Ottawa. See Appendix B for correspondence with the City.

Wastewater Design Criteria

Design Parameter	Value			
Residential Average Apartment	1.8 P/unit			
Average Daily Demand	280 L/cap/day			
Peaking Factor	Harmon's Peaking Factor. Max 4.0, Min 2.0			
Correction Factor (City of Ottawa Tech.Bulletin ISTB-2018-0	0.8			
Commercial Space	28,000 L/ha/day			
Infiltration and Inflow Allowance	0.28L/s/ha			
Sanitary sewers are to be sized employing the Manning's	O (4/-) A P ^{2/3} O ^{1/2}			
Equation	$Q = (1/n)AR^{2/3}S^{1/2}$			
Minimum Sewer Size	200mm diameter			
Minimum Manning's 'n'	0.013			
Minimum Depth of Cover	2.5m from crown of sewer to grade			
Minimum Full Flowing Velocity	0.6m/s			
Maximum Full Flowing Velocity	3.0m/s			
Extracted from Sections 4 and 6 of the City of Ottawa Sewer Design Guidelines, November 2012.				

Sanitary Sewer Post Development Outflow

Site Area	0.4 ha
Extraneous Flow Allowances	
Infiltration / Inflow	0.132 L/s

Domestic Contributions

Unit Type	Unit Rate	Units	Рор
Single Family	3.4	0	0
Semi-detached and duplex	2.7		0
Duplex	2.3		0
Townhouse	2.7		0
Apartment			
Bachelor	1.4		0
1 Bedroom	1.4	0	0
2 Bedroom	2.1	0	0
3 Bedroom	3.1	0	0
4 Bedroom	4.2	0	0
	Tota	al Population	0
	0.00 L/s		
	3.80		
	0.00 L/s		

Institutional / Commercial / Industrial Contributions

Property Type	Unit Rate	No. of Units	Avg Wastewater
			(L/s)
Commercial	28,000 L/gross ha/d	0.006215	0.00
Veterinary Clinic	275 l/unit/day	3	0.01
Veterinary Clinic	75 l/person/day	10	0.01
Institutional	28,000 L/gross ha/d	0	0.00
Industrial - Light	35,000 L/gross ha/d	0	0.00
Industrial - Heavy	55,000 L/gross ha/d	0	0.00
	Ave	erage I/C/I Flow	0.020
	0.030		
	0.000		
		Peak I/C/I Flow	0.030

Total Estimated Average Dry Weather Flow Rate	0.020
Total Estimated Peak Dry Weather Flow Rate	0.030
Total Estimated Peak Wet Weather Flow Rate	0.162

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^{**}Use Apendix 4B diagram

FUS Fire Flow Calculations

Project: 4 Campbell Reid Court

Calculations Based on 1999 Publication "Water Supply for Public Protection Fire Protection " by

Fire Underwriters' Survey (FUS)

Fire Flow Calculation #: 1

ate August 19, 2022 Building Type/Description/Name: Veterinary Clinic

Data input by: Zoran Mrdja, P.Eng.

	: Fire Underwriters	<u> </u>	1	Multiplier		Value		Total Fire
Step	Task	Term	Options	Associated with Option	Choose:	Used	Unit	Flow (L/min)
				Framing Mate	erial			
		Coefficient related	Wood Frame	1.50				
	Choose Frame Used	to type of construction (C)	Ordinary construction	1.00				
1	for Construction of Unit	(1)	Non-combustible construction	0.80	Fire resistive construction			
			Fire resistive construction (< 2 hrs)	0.70	(>2 hrs)			
			Fire resistive construction (> 2 hrs)	0.60		0.60		
				Floor Space A	Area			
	Choose Type of Housing (if TH, Enter		Single Family	1				
2	Number of Units Per		Townhouse - indicate # of units	1	Other (Comm, ind)	1	Units	
	TH Block)	Type of Housing	Other (Comm, Ind, etc.)	1				
2.2	# of Storeys	Number of Floors/ S	storeys in the Unit (do not include basement):			Storeys	
	Enter	Enter Ground Floor	Area (A) of One Unit Only:		area			
	Enter Ground Floor		Square Feet (ft2)	5425.0)	504	Area in Square Meters (m ₂)	
	Area of One Unit		Square Metres (m ₂)	504	dist	504		
			Hectares (ha)	0	0			
4	Obtain Required Fire Flow without Reductions	Required Fire Flow(without reductions or increases per FUS) (F = 220 * C * √A) Round to nearest 1000L/min					2,96	
5	Apply Factors Affecting Burning	Reductions/Increases Due to Factors Affecting Burning						
	Affecting Burning	Occupancy content	Non-combustible	0.25				
		hazard reduction or surcharge	Limited combustible	-0.15				
5.1	Choose Combustibility of Building Contents		Combustible	0.00	Non-combustible		N/A	
	or Building Contents		Free burning	0.15			,	
			Rapid burning	0.25		-0.25		-74
	Choose Reduction	Sprinkler reduction	Complete Automatic Sprinkler	-0.3				
5.2	Due to Presence of Sprinklers		Protection None	0	None	0.00	N/A	
	-,		North Side	30.1-45 m	0.05			
	Choose Separation		East Side	30.1-45 m	0.05			
5.3	Distance Between Units		South Side	30.1-45 m	0.05	0.20	m	
		Exposure Distance Between Units	West Side	30.1-45 m	0.05			59
		Total Required	Fire Flow, rounded to nearest 1000	D L/min, with max/n	nin limits applied:		1	3,000
	Obtain Required		Fire Flow (above) in L/s:	<u> </u>				5(
6	Fire Flow, Duration & Volume Required Duration of Fire Flow (hrs)					2.00		
		Required Volume of Fire Flow (m³)						360

Note: The most current FUS document should be referenced before design to ensure that the above figures are consistent with the intent of the Guideline

Legend				
Drop down menu - choose option, or enter value.				
No Information, No input required.				

Note

The most current FUS document should be referenced before design to ensure that the above figures are consistent with the intent of the Guideline.

Appendix B: Correspondence

Pre-application Consultation PC2019-0171 4 Campbell Crt Meeting Notes July 18, 2019

Attendees

Drs Olenders, owners
Dr Firestone, with owner
Tim Moore, agent
Sami Rehman, Environmental Planner
Kevin Hall, Project Manager
Michel Kearney, Hydrogeologist
Neeti Paudel, Transportation
Cheryl McWilliams, File Lead

Proposal:

- New 6000 sq ft veterinary hospital, combining their March and Dunrobin facilities
- Keep existing house (No basement renovation for house proposed now)
- Proposed new septic for vet building
- Access vet building off of Dunrobin Road

Transportation

In the case that the access is proposed on Dunrobin Road;

Please follow the Transportation Impact Assessment (TIA) Guidelines:

- Submit TIA Step 2 Scoping, a full TIA will be required.
- Please note that the application will not be deemed complete until it meets the
 necessary TIA components (Draft Steps 1-4 of the TIA). If roadway modifications are
 required, draft RMA package will have to be submitted with Step 4 of the TIA.

In the case that the access is proposed on Campbell Reid Court – TIA will not be required.

Right of way protection for March Road is 34m. Ensure this is protected.

Right of way to be protected for Dunrobin Road is 30m.

When submitting site plans:

- Show all details of the road abutting the site including the opposite curb. Pavement markings, accesses and sidewalks must be included.
- Turning templates are required for all accesses and internal movements. Ensure the turning templates show the largest vehicle turning in to and out of the site at all accesses.

• Curb radii at the access should be reduced as much as possible. Ensure the measurements are shown in the site plan.

Noise Impact Study is required for the following:

• Road. Dunrobin Road and March Road are both classified as arterial roads.

Corner triangles (Dunrobin Road and March Road) as per OP Annex 1 - Road Classification and Rights-of-Way at the following locations on the final plan will be required: Arterial Road to Arterial Road: 10 metre x 10 metres

Environment

- Part of the natural heritage system overlay
- Species at risk needs to be considered and woodlot linkages
- Requires Tree Conservation Report and Environmental Impact Statement
- The subject property is part of the Natural Heritage System (NHS) and as per Official Plan policies (Section 2.4.2 and 4.7.8), the proposed development requires an Environmental Impact Statement (EIS). This part of the NHS is one of the natural landscape linkages. The EIS must demonstrate that the proposed development will have no negative impacts to the natural landscape linkage and its associated ecological functions. Furthermore, the EIS should examine potential significant habitat for Species at Risk on the subject property (OP 4.7.4).
- Further details of the EIS requirements can be found in OP Section 4.7.8 and the EIS guidelines:
- https://documents.ottawa.ca/sites/default/files/documents/eis_guidelines2015_en.pdf
- The proposed development will also require a Tree Conservation Report (TCR), as per OP Section 4.7.2. Further details of the requirements for the TCR can be found in the TCR quidelines:
- https://ottawa.ca/en/residents/water-and-environment/trees-and-community-forests/protection#tree-conservation-report-guidelines
- To avoid duplications, the TCR can be combined with the EIS.

Engineering

- Stormwater management is required to demonstrate post to pre run off
- Contact Matt Craig at Mississippi Valley Conservation Authority for stormwater quality requirements
- Road side ditch should be the legal outlet NEED TO CON.
- Require a geotechnical report
- Require no light spillage onto adjacent properties
- Show any on-site snow storage
- Geotech report will be required.
- Hydro-Geological report required
- Lighting certificate confirming the site light meets our standards
- Stormwater report. The CA should be contacted to confirm the quality requirements. They need to confirm they have a legal outlet for the runoff from this site.
- Consult what the onsite fire requirements will be.
- Access from Dunrobin and possible use of an access on to Campbell Reid.

Fire

- May need storage tanks comments provided by Fire Services
- Will need fire route shown on the site plan

Private Servicing (hydrogeological report required

- Proposal would have separate well and septic for each use
- Concerns with separation distances
- Soils are thin (less than one metre)
- Septic capacity if more than 10000 l per day for the lot then needs Ministry of Environment Conservation and Parks approval (house typically 2-3000)

Planning

- Need to buffer the site and especially parking from March and Dunrobin roads, Best done through maintaining trees and undergrowth along those two roads. In particular along March and at the north west corner along Dunrobin Road.
- Looking for an enhanced building façade with any visibility to the roads. Looking to have the materials and colours for the most part 'fit' with a rural context. Some visibility from the roads for the building and signage would be appropriate.
- We will be looking for some screening off of Campbell Court abutting the property owner to the south to ensure buffering between any commercial use, access or parking and loading form that residential property.
- Access off of Campbell court may be best for safety
- The application would be a Site Plan Rural based Standard one.

Appendix C: Guidelines, Existing Reports, Studies and References, Plans

The following studies were utilized in the preparation of this report:

Ottawa Sewer Design Guidelines,

City of Ottawa, SDG002, October 2012, amended 2019 & 2020. (City Standards)

- Technical Bulletin ISTB-2018-01, City of Ottawa, March 21, 2018.
- Technical Bulletin ISTB-2018-03, City of Ottawa, March 21, 2018.

• Ottawa Design Guidelines - Water Distribution

City of Ottawa, July 2010., (Water Supply Guidelines)

- Technical Bulletin ISD-2010-2, City of Ottawa, December 15, 2010.
- Technical Bulletin ISDTB-2014-02, City of Ottawa, May 27, 2014.
- Technical Bulletin ISDTB-2018-02, City of Ottawa, March 21, 2018.
- Design Guidelines for Sewage Works,

Ministry of the Environment, 2008., (MOE Design Guidelines)

Stormwater Planning and Design Manual,

Ministry of the Environment, March 2003., (SWMP Design Manual)

Ontario Building Code Compendium

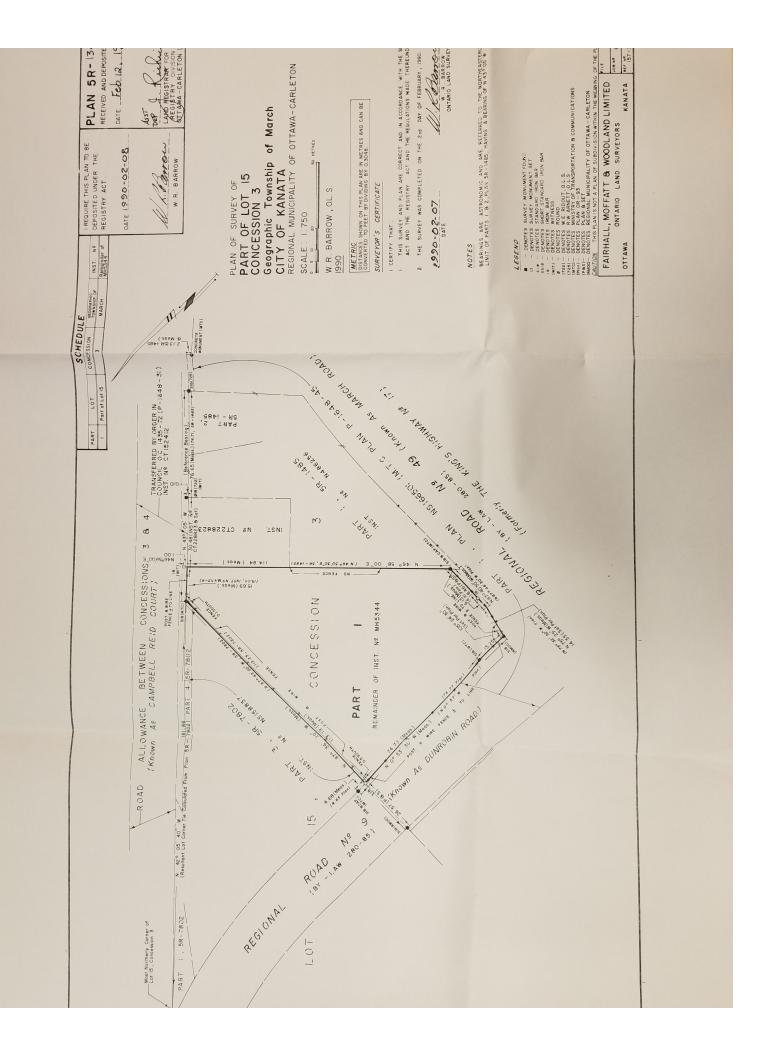
Ministry of Municipal Affairs and Housing Building Development Branch, January 1, 2010 Update.(OBC)

Water Supply for Public Fire Protection

Fire Underwriters Survey, 1999., (FUS)

NFPA 13 – Standard for the Installation of Sprinkler Systems

National Fire Protection Association, 2016., (NFPA Standards)



Installation Report • Rapport d'installation

Applicant: File #: Date: Civic Address:	7-005 Present on site: Time: 3:05	iption: Lot: 15 Conc.: 3 S.Lot: R.Plan:
Scarification Inspection and/or Clay Seal	Time: 7:15 pm Date: Weather: Sun, Warm On-site: Length: 23.5m 29 m Width: 15 Comments:	Aug 28, 2007 Approved Tyes on no Inspector: 6. Molson Elevations: Bed Area: 99, 11 marsh Mantle 98.53 mas
Section A Tank	Septic tank/holding tank size: (L) Make and model: (L) plastic concrete in fiberglass in on-site prefabricated	Filter make and model: Inlet: Outlet: Lids: Baffles:
Section B Treatment Unit	Make:	
Section C Leaching Bed	Location: Type:	Structure(s): House: Shade Mells*: 1) Watercourses: 2) Tree(s): Between Trenches: // 62 Mantles: // metres in // direction(s) thickness: 0, 25 Other: Elevations: (if required) Header: Ends: Area Bed:
Section D Pump Chamber	pump chamber pump present floats installed electrical wiring alarm: inside outside joints sealed properly	□ forced main: □ check valve □ frost protection installed □ other:
Section E Distribution Box	sealed joints	Diagram:
Domarka	aken Full On-Site Approval (additional paperwork required, etc.)	ot approved, for re-inspection, call 692-0160 or 800-459-5975. Please ensure that ALL noted ficiencies have been rectified prior to calling for re-inspection.

JAN 3 2007

Application for a Permit to Construct or Demolish#

This form is authorized under the Building Code Sentence 2.4.1.1A.(2).

07-005

Ottawa Septic Bureau des systèmes System Office septiques d'Ottawa

iii. If yes to (ii) provide registration number(s):

The state of the s	Lambara and the second		07-003
Supplementaries of freedom and the supplementaries and the supplementaries and the	For use by	y Principal Authority	BEO.
Application number:	\circ	Permit number (if different):	REQUIRED FOR ALI
Date received:	(3)/	Roll number:	

INV# 00059-2007 Application submitted to: Rideau Valley Conservation Authority (Name of municipality, upper-tier municipality, board of health or conservation authority) A. Project information Building number, street name 4 Campbell Reid Court Lot/con. 15/3 Unit number Municipality Ottawa (Kanata) Postal code K2K 1X7 Plan number/other description Part 1, Plan 5R-13420 Project value est. \$ Area of work (m2) B. Applicant Applicant is: Owner or Authorized agent of owner Last name Corporation or partnership First name Paterson Group Inc. Street address 28 Concourse Gate Unit number Lot/con. Municipality Ottawa (Nepean) Postal code Province E-mail K2E 7T7 Ontario avanschie@patersongroup.ca Telephone number Fax Cell number (613)226-7381 (613) 226-6344 C. Owner (if different from applicant) First name Geoff Corporation or partnership Simpson Street address 4 Campbell Reid Court Unit number Lot/con. Municipality Ottawa (Kanata) Postal code K2K 1X7 Province Ontario E-mail Telephone number Fax Cell number (613) 592-0692 (613) 853-3358 D. Builder (optional) Last name First name Corporation or partnership (if applicable) Street address Unit number Lot/con. Municipality Postal code Province E-mail Telephone number Fax Cell number) Purpose of application ■ New construction Addition to an Alteration/repair Demolition Conditional existing building Permit Proposed use of building Current use of building Residential Description of proposed work Install a Class 4 Sewage System DIRECTIONS - MARCH ROAD TO DUNROBIN ROAD TO CAMPBELL REID COURT Tarion Warranty Corporation (Ontario New Home Warranty Program) Is proposed construction for a new home as defined in the Ontario New Home Yes ☐ No Warranties Plan Act? If no, go to section G. ii. Is registration required under the Ontario New Home Warranties Plan Act? Yes ☐ No

Attachments Attach documents establishing compliance with applicable law as set out in Article 1.1.3.3. Attach Schedule 1 for each individual who reviews and takes responsibility for design activities. ii. Attach Schedule 2 where application is to construct on-site, install or repair a sewage system. Attach types and quantities of plans and specifications for the proposed construction or demolition that are prescribed by the by-law, resolution, or regulation of the municipality, upper-tier municipality, board of health or conservation authority to which this application is made. H. Declaration of applicant Albert Van Schie - Paterson Group Inc. certify that: (print name) The information contained in this application, attached schedules, attached plans and specifications, and other attached documentation is true to the best of my knowledge. I have authority to bind the corporation or partnership (in applicable).

Date

Signature of applicant

Personal information contained in this form and schedules is collected under the authority of subsection 8(1.1) of the Building Code Act, 1992, and will be used in the administration and enforcement of the Building Code Act, 1992. Questions about the collection of personal information may be addressed to: a) the Chief Building Official of the municipality or upper-tier municipality to which this application is being made, or, b) the inspector having the powers and duties of a chief building official in relation to sewage systems or plumbing for an upper-tier municipality, board of health or conservation authority to whom this application is made, or, c) Director, Building and Development Branch, Ministry of Municipal Affairs and Housing 777 Bay St., 2nd Floor. Toronto, M5G 2E5 (416) 585-6666.

January 2, 2007 Date



0.S.S.O. PERMIT#

Schedule 1: Designer Information

Use one form for each individual who review	s and takes res	ponsibility for design activities	with respect to the	project UIRIES		
A. Project Information	William Co., St. Co.,					
Building number, street name 4 Campbell	Unit no.	Lot/con. 15/3				
Municipality Ottawa (Kanata) Postal code K2K 1X7 Plan number/ other descript			tion Part 1, Plan	ion Part 1, Plan 5R-13420		
B. Individual who reviews and takes	responsibilit	y for design activities				
Name Albert Van Schie		Firm Paterson Group In	C.			
Street address 28 Concourse Gate			Unit no.	Lot/con.		
Municipality Ottawa. Nepean	Postal code K2E 7T7	Province Ontario	E-mail avanschie@pa	tersonaroup.ca		
Telephone number (613) 226-7381	Fax number (613) 226-	6344	Cell number			
C. Design activities undertaken by in			ding Code Table	2 20 2 11		
☐ House ☐ Small Buildings ☐ Large Buildings ☐ Complex Buildings ☐ Description of designer's work	☐ HVAC - Building ☐ Detection	– House g Services on, Lighting and Power otection	□ Building St □ Plumbing - □ Plumbing -	ructural - House		
Sewage System Design						
D. Declaration of Designer	ha juhan disebeh					
Albert Van Schie - Paterson Group	Inc.	de	clare that (choose o	one as appropriate):		
(print name		001	dare that (choose c	пе аз арргорпате).		
I review and take responsibility Building Code. I am qualified, a Individual BCIN: 24387	for the design vand the firm is re	work on behalf of a firm regist egistered, in the appropriate o	tered under subsec classes/categories.	tion 2.17.4, of the		
Firm BCIN: 29346						
☐ I review and take responsibility for the design work and am qualified in the appropriate category as an "other designer" under subsection 2.17.5. of the Building Code. Individual BCIN:						
Basis for exemption from	egistration:					
☐ The design work is exempt from Basis for exemption from I			nts of the Building	Code.		
I certify that:				OMERICA TO STATE OF THE STATE O		
The information contained in this so	hedule is true to	o the best of my knowledge.				
2. I have authority to bind the corporation or partnership (i) applicable).						
January 2, 2007 Date		Signature of Designer				

*For the purposes of this form, "individual" means the "person" referred to in Clause 2.17.4.7.(1)(d), Article 2.17.5.1. and all other persons who are exempt from qualification under Subsections 2.17.4. and 2.17.5.

NOTE:

- 1. Firm and Individual BCIN numbers are not required for building permit applications submitted prior to January 1, 2006
- 2. Schedule 1 does not need to be completed by architects, or holders of a Certificate of Practice or a Temporary License under the Architects Act.

Application for a Permit to Construct or Demolish Schedule 1 06/07/05

R.V.C.A. RECEIVED

O.S.S.O. PERMIT #

JAN 3 2007 Schedule 2: Sewage System Installer Information

A. Project Information LEFER 18.					
Building number, street name 4 Campb	ell Reid Court	Court Unit number Lot/con. 15/3			
Municipality Ottawa (Kanata)	Postal code K2K 1X7	Plan number/ other description Part 1, Plan 5R-13420			
B. Sewage system installer					
Is the installer of the sewage system engagemptying sewage systems, in accordance Yes (Continue to Section C)	with Building Co	ess of constructing on-site, in de Article 2.18.1.1? (Continue to Section E)	☑ Installer	servicing, cleaning or runknown at time of ion (Continue to Section E)	
C. Registered installer information	n (where answe	er to B is "Yes")			
Name			BCIN		
Street address			Unit number	Lot/con.	
Municipality	Postal code	Province	E-mail		
Telephone number ()	Fax ()		Cell number		
D. Qualified supervisor information	n (where answ	er to section B is "Yes")		
Name of qualified supervisor(s) Building Code Identification Number (BCIN)					
E. Declaration of Applicant:	richerst versien der				
Albert Van Schie - Paterson Grou (print name)	up Inc.			declare that:	
 I am the applicant for the permit to construct the sewage system. If the installer is unknown at time of application, I shall submit a new Schedule 2 prior to construction when the installer is known; OR I am the holder of the permit to construct the sewage system, and am submitting a new Schedule 2 now that the installer is known. 					
I certify that:					
The information contained in this schedule is true to the best of my knowledge.					
2. I have authority to bind the corpo	oration or partners	ship (If applicable).			
		gracero or apprount			

Ottawa Septic Bureau des systèmes System Office septiques d'Ottawa

R.V.C.A. REGLIVED

Schedule 4 Proposed Services

0.0.5
0 0 5

	HACOIKIES
1. Engineered	2. Water supply
X Yes	Proposed
No	X Existing
3. Type of work proposed	4. Type of Well
New Installation	Dug/bored/Sandpoint well
X Replacement	X Drilled well
Alteration	Municipal
	Other
	_
5. Residential Sewage Design Flow Info. Bedrooms 4 House (floor area) 220 m ²	6. Sewage Design Flow for Other Occupancies Design Flow L/day
House (floor area) 220 m ² People	Detailed sewage flow calculations:
Total Fixture Units 15.5 (Schedule 8)	
Residential Flow 2200 L/day	
7. Type of System	
Treatment Unit	Class 4 – Area Bed
Class 2 – Leaching Pit	Fully raised
Class 3 – Cesspool	Partially raised
Class 4 – Shallow Buried Trench	In-ground
	Class 4 – Aerobic with Trench
\underline{X} Class 4 – Trench	**************************************
X Fully raised	Fully raised
Partially raised	Partially raised
In-ground	In-ground
Class 4 – Filter Media	Class 4 – Aerobic with Filter Media
— Fully raised	Fully raised
Partially raised	Partially raised
In-ground	In-ground
- ground	Class 5 – Holding Tank





Sewage System Details

Do Not Comple	ete
Permit No	. PERMIT
Revision No 7	005
Date	0 0 3
REQUIR	ED FOR ALI
ING	HIBIES

Type of System Class 4 - Trench	(Schedule 4)
Septic/Holding Tank L	
Septic Tank Effluent Filter Yes	
Treatment Unit – Make & Model	
Number of Units	
Refer to Typical Drawing PH0547-1&2	
Mantle Information:	
Native or imported =15m inW_direction(s)	
Slope subgrade % slope	
Westerly direction(s)	
Site to be Scarified (If in clay) YES /NO	
Clay Seal Required (If in bedrock) YES /NO	
☑ Trench □ S	Shallow Buried Trench
Distribution Pipe Length 88 m	Pipe Length m
Loading Area 423 m ²	
Type of Chamber	Filter Media Bed
Length of Chamber m	Stonem ²
☐ Area Bed	Extended Base m ²
Stone m ²	Pipe m
Sand m ²	Weight of Filter Media Kg
Pipe m	Loading Area m ²
Note: Alarm required for all pumping systems	
Construction Notes:	

Version 01/06

Ottawa Septic
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REFER TO:

Schedule 6 Soil and Water Table Information (Minimum depth of test pit: 2 metres)

Do Not Complete
Permit No
Revision No
Date
REQUIRED FOR ALL
INQUIRIES

Name of Applicant/Agent: Paterson Group Inc. Date: November 24, 2006 Time: Applicant/Agent Signature:	Inspector: Time: Date:Time:
EG () Soil Description	T EG () Soil Description
REFER TO PATERSON GROUP DRAWING PH0547-2	1.0 m AS PER ENGINEER
1.5m	1.5m
2.0 m	2.0 m
EG () Soil Description	T EG () Soil Description
.5m	.5m
1.0 m	1.0 m
1.5m	1.5m
+ +	
2.0 m	2.0 m
LEGEND BR = Bedrock GWT = Ground water table HGWT = High ground water table M = metres	ter table EG = Existing grade T = percolation rate



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Schedule 7 **Layout Section**

Do Not	Complete	
Permit		March 1
Revisio	n No O. PERMI	TH
Date _	07 00 8	

Scale: 1Block =	Layout Section	Date07-005
		REQUIRED FOR ALL
N		MAGIRIES
RI	EFER TO PATERSON GROUP DRAWING PHOS	547-1
_Dug Well _Drilled Well _Neig	hbouring Homes &BenchmarkTile Draina	geProperty Line
Elevations (metric only)	Min. of 5 elevation	ons in proposed system area
B.M 100.00 m	(in X pattern)	proposed system area
B.M Description Top of Deck @	Rear Left Corner of X ₁	X ₂
House	X_3	X ₄
Exact Location	X ₅	X _{6 (toe)}
	X_7	X ₈

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Y.V	.C.A	. 1		C	V	Ei
	IAN	_	3	71	7	

Schedule 8 Fixture unit count

Do Not Compl Permit No	ete D.S.S.O. PERMIT #
Revision No Date	07-0 05
	REQUIRED FOR ALL

Total:

15.5

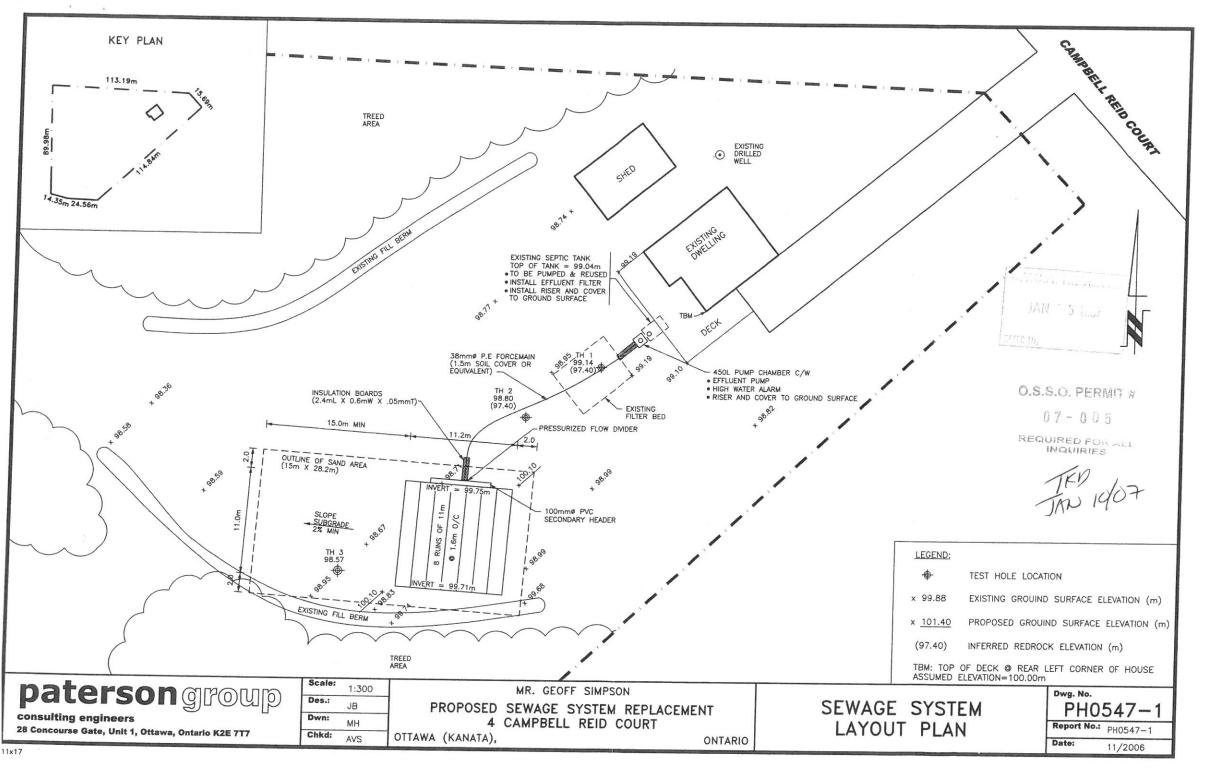
Fixtures	# Existing	+ #	Proposed	X	unit count	=	Fixture Count
Bathroom REFER 10:							- Intuit Count
Bathroom group (toilet, sink and tub or shower) with flush tank	2	+		Х	6	=	12.0
Bathtub with/without overhead shower		+		Х	1.5	=	
Shower stall		+		X	1.5	=	
Wash basin (1_inch trap)		+		X	1.5	=	
Watercloset (toilet) tank operated		+		X	4	=	
Bidet		+		X	1	=	
Kitchen			10				
Dishwasher	1	+) i	X	0.5	=	0.5
Sink with/without garbage grinder(s), domestic and other small type single, double or 2 single with a common trap	1	+		X	1.5	=	1.5
Other							
Domestic washing machine	1	+		X	1.5	=	1.5
Combination sink and laundry tray single or double (Installed on 1_ trap)		+		X	1.5	=	

Insert the TOTAL in section 5 of Schedule 4 (0.Reb.403/97 Table 7.4.9.3)

1. Sump pumps and floor drains are not to be connected to the sewage system. Connection of such fixtures to a sewage system may lead to a hydraulic failure of the said system. The above mentioned fixtures should be discharged separately to an approved Class 2 (leaching pit) sewage system.

2. Where laundry waste is not more than 20% of the total daily design sanitary sewage flow, it may discharge to a sewage system (Part 8, OBC, 8.1.3.1(2)).

AlV	January 2, 2007
Agent/Owner signature	Date



CLASS 4 ABSORPTION TRENCH STYLE BED

NOTES:

- 1) ESTIMATE OF DAILY SEWAGE FLOW (Q)
- NO. OF BEDROOMS = 4
- LIVING AREA OF DWELLING = 220 m2 • FIXTURE COUNT = 15.5
- DESIGN SEWAGE FLOW = 2200 L/DAY
- 2) SUBSURFACE CONDITIONS

SOILS INFORMATION GATHERED BY PATERSON GROUP INC.

TH 2. ELEV. 98.80m

TH 3. ELEV. 98.57m

0-0.10 TOPSOIL 0.10-1.36 SILTY CLAY 0-0.10 TOPSOIL
0.10-0.50 ROCK FILL INTERMIXED

1.36 REFUSAL ON INFERRED BEDROCK

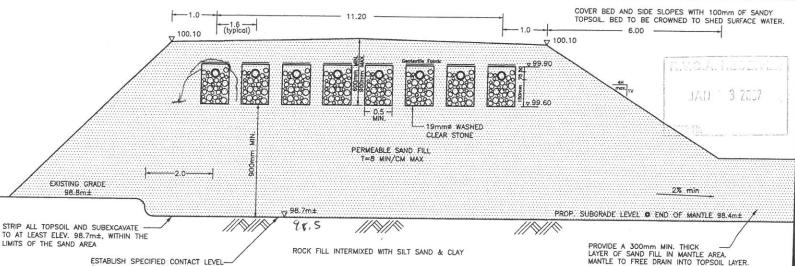
WITH SILT, SAND & CLAY REFUSAL ON ROCK FILL

- EFFLUENT @ 1.00m

- DRY UPON COMPLETION

0.50

- DISTRIBUTION PIPING NETWORK
- LENGTH OF PIPE REQUIRED = QT/200 = 2200(8)/200 = 88m
- . USE 8 RUNS OF 11m EACH RUN.
- . TOTAL LENGTH OF PIPE PROVIDED = 88 LINEAR METRES
- 4) HYDRAULIC LOADING RATE
- TOTAL BED AREA = 423 m2
- HYDRAULIC LOADING RATE = 5.2 L/DAY/m2
- 5) SEPTIC TANK
- . PUMP & RE-USE EXISTING SEPTIC TANK
- AN EFFLUENT FILTER SHALL BE INSTALLED ON THE OUTLET PIPE IN THE EXISTING SEPTIC TANK.
- . INSTALL RISERS AND COVER TO PROVIDE ACCESS FROM GROUND SURFACE OVER FILTER.
- 6) PUMP CHAMBER
- INSTALL A 450L MINIMUM PUMP CHAMBER IN SERIES AND DOWNSTREAM FROM THE TREATMENT UNIT.
- AN EFFLUENT PUMP (MYERS ME40 OR EQUIVALENT) AND A HIGH WATER ALARM SHALL BE INSTALLED IN THE PUMP CHAMBER.
- . THE RECOMMENDED PUMP DUTY CYCLE IS 290L.
- A 3mmø DRAIN HOLE SHALL BE INSTALLED IN THE BOTTOM OF THE FORCEMAIN IN THE PUMP CHAMBER.
- RISERS WITH A COVER SHALL BE INSTALLED OVER THE CHAMBER TO PROVIDED ACCESS FROM THE GROUND SURFACE.
- 7) PRESSURIZED FLOW DIVIDER/FORCEMAIN
 - A 38mmø (NOMINAL) FORCEMAIN SHALL BE USED TO CARRY THE EFFLUENT FROM THE PUMP CHAMBER TO THE LEACHING BED.
 - THE FORCEMAIN SHALL BE PROVIDED WITH 1.5m SOIL COVER OR EQUIVALENT.
 - THE FORCEMAIN SHALL BE OVERLAIN WITH 50mm T x 600mm W INSULATION BOARDS
 AT THE PIPE CONNECTIONS.
- THE FORCEMAIN SHALL DISCHARGE INTO A PRESSURIZED FLOW DIVIDER (PREMIER TECH PSF-200) WHICH SHALL BE INSTALLED INTO A SECONDARY HEADER PIPE.
- . THE FLOW DIVIDING TEE SHALL BE INSTALLED LEVEL ON A BED OF COMPACTED SAND.
- 8) LEACHING BED
- A FULLY-RAISED FILL BASED ABSORPTION TRENCH STYLE LEACHING BED TO BE INSTALLED.
 A MINIMUM THICKNESS OF 0.9m OF IMPORTED SAND FILL, HAVING A PERCOLATION RATE OF NOT GREATER 8 min./cm, SHALL BE PROVIDED BELOW THE BASE OF THE TRENCHES.
- THE SUBGRADE SURFACE FOR THE BED AND MANTLE AREAS SHOULD BE PREPARED BY REMOVAL OF ALL EXISTING TOPSOIL AND SUBEXCAVATING TO AT LEAST ELEV. 98.7m±.
- THE SPECIFIED CONTACT LEVEL, ELEV. 98.7m±, SHALL BE ESTABLISHED USING PERMEABLE SAND FILL, WHERE REQUIRED.

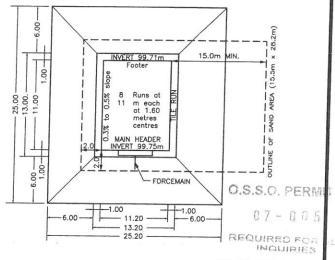


ESTABLISH SPECIFIED CONTACT LEVEL—/
(ELEV. 98.90m) USING PERMEABLE SAND FILL, WHERE REQUIRED

PROFILE NOT TO SCALE

- THE DISTRIBUTION PIPES SHOULD CONSIST OF 75mmø PERFORATED SEPTIC PIPE WHICH SHOULD BE EMBEDDED IN A 300mm THICK BY 500mm (MIN.) WIDE LAYER OF 19mmø WASHED CLEAR STONE.
- THE DISTRIBUTION PIPES SHOULD BE INSTALLED WITH A UNIFORM DOWNWARD SLOPE FROM ELEV. 99.75m AT THE HEADER TO ELEV. 99.71m AT THE FOOTER.
- . THE ENDS OF EACH RUN SHALL BE INTERCONNECTED WITH A FOOTER PIPE
- . THE CLEAR STONE LAYER SHOULD BE COVERED WITH AN APPROVED GEOTEXTILE FABRIC.
- THE SURFACE OF THE BED SHOULD BE COVERED WITH PERMEABLE SAND FOLLOWED BY APPROXIMATELY 100mm OF SANDY TOPSOIL. THE BED AREA SHOULD BE VEGETATED.
 THE TOTAL THICKNESS OF THE COVER OVER THE BASE OF THE TRENCHES SHOULD BE
- WITHIN THE RANGE OF 0.6m TO 0.9m.

 THE SIDES OF THE BED SHOULD BE SLOPED IN THE RANGE OF 4H:1V OR SHALLOWER.
- 9) MINIMUM CLEARANCE FROM LEACHING BED
- . 6.0m FROM ANY PROPERTY LINE.
- . 8.0m FROM ANY STRUCTURE
- . 18.0m FROM ANY DRILLED WELL.
- . 5.0m FROM ANY TREES UNLESS OTHERWISE APPROVED.
- 5.0m FROM DRIVEWAY
- 10) MINIMUM CLEARANCE FROM TANK(S)
- . 1.5m FROM ANY STRUCTURE
- . 15.0m FROM ANY DRILLED WELL
- . 3.0m FROM ANY PROPERTY LINE
- 11) OTHER PERTINENT DETAILS
 - POOLS AND ALL APPURTENANCES, SUCH AS FENCES, PATIOS, ETC. SHOULD BE LOCATED A MINIMUM OF 5m FROM THE DISTRIBUTION SYSTEM OF LEACHING BED.
- THE BACKWASH WATERS FROM ANY TREATMENT UNIT, SUCH AS A WATER SOFTENER, SHOULD NOT DISCHARGE INTO THE SEPTIC TANK SYSTEM.
- THE CONTRACTOR IS RESPONSIBLE TO LOCATE AND PROTECT ALL EXISTING UNDERGROUND SERVICES.
- THE FIRM OF PATERSON GROUP INC. HAS PROVIDED DESIGN SERVICES ONLY FOR THE SUBJECT SEWAGE SYSTEM. THE DESIGN HAS BEEN CARRIED OUT IN ACCORDANCE WITH OUR INTERPRETATION OF PART 8 OF THE ONTARIO BUILDING CODE, 1997. INSPECTIONS BY THE CONSULTANT DURING THE INSTALLATION OF THE SYSTEM IS A REQUIREMENT OF SOME REGULATING AUTHORITIES AND IS STRONGLY RECOMMENDED BY THIS FIRM.



PLAN VIEW

JAN 1907

patersongroup

consulting engineers

28 Concourse Gate, Unit 1, Ottawa, Ontario K2E 7T7

Scale:	N.T.S.	
Des.:	JB	
Dwn:	МН	
Chkd:	AVS	

MR. GEOFF SIMPSON

PROPOSED SEWAGE SYSTEM REPLACEMENT
4 CAMPBELL REID COURT

OTTAWA (KANATA),

ONTARIO

SEWAGE SYSTEM DETAILS & NOTES

PH0547-2

Report No.: PH0547-1

Date: 12/2006



Do Not Complete	
Permit No_/) 7_005	
Revision No	
Date	

Permit Part 8 - Sewage System Ontario Building Code

Inspected & Recommended by: 1KD Inspection Date & time: 1411007 C 915		Owner: SIMPSON		
Inspection Date & time: JAX	10/07 C 9:50	On Weather: SUX		
Civic Address: 4 CAMPBE	ZL REIN COUR	CT Legal:		
Design T	min/cm	Percolation test required	Yes/No	
Design HGWT	m	Grain size analysis required		
Subgrade Elevation	m	Site to be Scarified	Yes/No	
Depth to rock/impervious soil	m	Clay Seal Inspection	Yes(No	
E)	XISTING	Mantle required	Yes/No	
Septic/Holding Tank/Pretreatment			109111	
Septic Tank Effluent Filter				
Pump Rate		1		
Treatment Unit – Make & Model_				
		. /		
ELEVATION In Groun	nd 🗖 Partiall	y Raised Fully R	aised	
TYPE OF SYSTEM		/		
Trench		☐ Shallow Buried Trench		
Distribution Pipe Length	8 m	Pipe Length	m	
Loading Area	m²	☐ Filter Media Bed		
Type of Chamber		Stone	m ²	
Length of Chamber	m	Extended Base		
□ Area Bed		Pipe		
Stone	m²	Weight of Filter Media_		
Sand	m ²	Loading Area	_	
Pipe	m			
Manager, Septic System Approvals: _	/ emy x	Javrosen		
Permit Issued Date:	/ FJA	NUXRY 10, 20	07.	
Comments:				
☐ Maintenance Contract Required ☐ Engineer		eer to Verify Subgrade		
		□ Soil		
		☐ Squirt Height		
Manager, Septic System Approvals: _			0	
Revision Issued Date:				
Comments:				

NOV 0 2 2007

