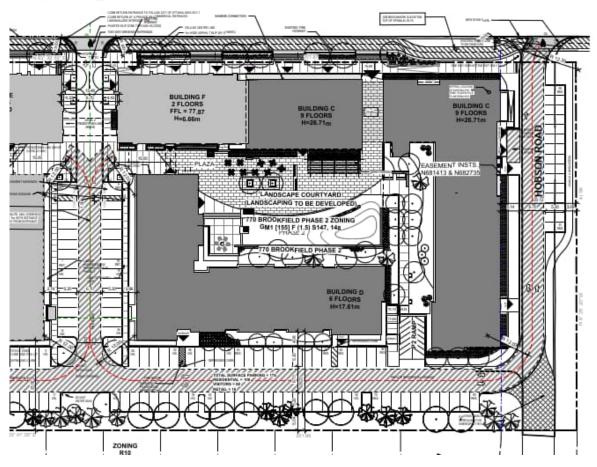
SERVICING & STORMWATER MANAGEMENT REPORT 770 BROOKFIELD ROAD – PHASE 2, OTTAWA

BROOKFIELD ROAD



Project No.: CCO-22-3501

City File No.: D07-12-22-0109

Prepared for:

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1.0 PRO4JECT DESCRIPTION

1.1 Purpose

McIntosh Perry (MP) has been retained by Hobin Architecture Inc. to prepare this Servicing and Stormwater Management Report in support of the Site Plan Control application for the proposed Phase II development at 770 Brookfield Road within the City of Ottawa.

The main purpose of this report is to present a servicing design for the development in accordance with the recommendations and guidelines provided by the City of Ottawa (City), the Rideau Valley Conservation Authority (RVCA), and the Ministry of the Environment, Conservation and Parks (MECP). This report will address the water, sanitary and storm sewer servicing for the development, ensuring that existing and available services will adequately service the proposed development.

This report should be read in conjunction with the following drawings:

- CCO-22-3501, C101 Site Grading and Drainage Plan, and
- CCO-22-3501, C102 Site Servicing Plan.
- CCO-22-3501, PRE Pre-Development Drainage Area Plan (Appendix E)
- CCO-22-3501, POST Post-Development Drainage Area Plan (Appendix F)

1.2 Site Description

The property is located at 770 Brookfield Road. It is described as Registered Plan 787, Parts 7-9 Plan 4R-28560 Ward 16 River, City of Ottawa. The Phase II land in question covers approximately 0.72 ha and is bounded by Brookfield Road to the north and Hobson Road to the east. The site is zoned for General Mixed Use (GM1). See Site Location Plan in Appendix 'A' for more details and Phase II Severance R-Plan included in Appendix 'B'.



Figure 1: Site Map

1.3 Proposed Development and Statistics

The proposed development consists of a 9-storey mixed-use residential building and a 6-storey mixed-use residential building. Visitor parking and drive aisles will be provided west and south of the proposed buildings. Underground parking will be provided for residents with site access extending from Brookfield Road and Hobson Road. Refer to Site Plan prepared by Hobin Architecture included in *Appendix 'B'* for details.

1.4 Existing Conditions and Infrastructure

The property adjacent to the existing site is currently developed with mixed-use residential buildings, approved under City Application No. D07-12-17-0140 (*Functional Servicing and Stormwater Management Report*). The Phase II site is currently undeveloped.

The existing Phase II site has no sanitary or water services. In accordance with the *Functional Servicing and Stormwater Management Report*, drainage within the Phase II site flows both west, currently being picked up by the Phase I servicing network, and east, currently being picked up by the municipal infrastructure within Hobson Road.

Sewer and watermain mapping collected from the City of Ottawa indicate that the following services exist across the property frontages within the adjacent municipal rights-of-way(s):

Brookfield Road

- o 305 mm diameter cast iron watermain,
- o 250 mm diameter concrete sanitary sewer, tributary to the Rideau River Collector, and a
- o 750 mm diameter concrete storm sewer, tributary to Sawmill Creek sub-watershed with approximately 0.7 km to the outlet

Hobson Road

- o 203 mm diameter cast iron watermain,
- o 300 mm diameter asbestos concrete sanitary sewer, tributary to the Rideau River Collector, and a
- 375 mm diameter concrete storm sewer, tributary to Sawmill Creek sub-watershed with approximately 1.1 Km to the outlet.

Drive Aisle Within 770 Brookfield – Phase I

- o 200 mm diameter concrete sanitary sewer, tributary to the Rideau River Collector, and a
- o 675 mm diameter concrete storm sewer tributary to Sawmill Creek sub-watershed with approximately 0.7 km to the outlet.

1.5 Approvals

The proposed development is subject to the City of Ottawa site plan control process. Site plan control requires the City to review, provided concurrence and approve the engineering design package. Permits to construct can be requested once the City has issued a site plan agreement.

An Environmental Compliance Approval (*ECA*) through the Ministry of Environment, Conservation and Parks (*MECP*) is not anticipated to be required since the development is contained within a single parcel of land and proposes independent servicing, is not within a combined sewer shed, and does not propose industrial sewage. As a result, the stormwater management system meets the exemption requirements under O.Reg 525/90 for the Site Plan Control application.

2.0 BACKROUND STUDIES, STANDARDS, AND REFRENCES

2.1 Background Reports / Reference Information

Background studies that have been completed for the proposed site include City of Ottawa as-built drawings, a topographical survey, a geotechnical report and a Phase I Environmental Site Assessment (ESA).

As-built drawings of existing services within the vicinity of the proposed site were reviewed in order to determine accurate servicing and stormwater management schemes for the site.

A topographic survey of the site (Job No. 22509-21) was completed by Annis, O'Sullivan, Vollebekk LTD., dated May 20, 2022.

The following reports have previously been completed and are available under separate cover:

- Geotechnical Investigation completed by Paterson Group, dated May 30, 2022.
- Phase One Environmental Site Assessment completed by Paterson Group, dated December 16, 2019.
- Functional Servicing and Stormwater Management Report completed by David Schaeffer Engineering Ltd, dated May 2019. (Functional Servicing and Stormwater Management Report)
- Stormwater Management Memorandum completed by David Schaeffer Engineering Ltd, dated October 5, 2020.

2.2 Applicable Guidelines and Standards

City of Ottawa:

- ◆ Ottawa Sewer Design Guidelines, City of Ottawa, SDG002, October 2012. (Ottawa Sewer Guidelines)
 - Technical Bulletin ISTB-2014-01 City of Ottawa, February 2014. (ISTB-2014-01)
 - Technical Bulletin PIEDTB-2016-01 City of Ottawa, September 2016. (PIEDTB-2016-01)
 - Technical Bulletin ISTB-2018-01 City of Ottawa, January 2018. (ISTB-2018-01)
 - Technical Bulletin ISTB-2018-03 City of Ottawa, March 2018. (ISTB-2018-03)
 - Technical Bulletin ISTB-2019-01 City of Ottawa, January 2019. (ISTB-2019-01)
 - Technical Bulletin ISTB-2019-02 City of Ottawa, February 2019. (ISTB-2019-02)
- Ottawa Design Guidelines Water Distribution City of Ottawa, July 2010. (Ottawa Water Guidelines)
 - Technical Bulletin ISD-2010-2 City of Ottawa, December 15, 2010. (ISD-2010-2)
 - Technical Bulletin ISDTB-2014-02 City of Ottawa, May 2014. (ISDTB-2014-02)
 - Technical Bulletin ISTB-2018-02 City of Ottawa, March 2018. (ISTB-2018-02)

Ministry of Environment, Conservation and Parks:

- ◆ Stormwater Planning and Design Manual, Ministry of the Environment, March 2003. (MECP Stormwater Design Manual)
- ◆ Design Guidelines for Sewage Works, Ministry of the Environment, 2008. (*MECP Sewer Design Guidelines*)

Other:

♦ Water Supply for Public Fire Protection, Fire Underwriters Survey, 2020. (FUS Guidelines)

3.0 PRE-CONSULTATION SUMMARY

A pre-consultation meeting was conducted on March 20th, 2022, regarding the proposed site. Specific design parameters to be incorporated within this design include the following:

- Calculate the time of concentration (Cannot be less than 10 minutes).
- Control post-development flows to the pre-development 2-year storm release rate using the pre-development runoff coefficient or a maximum equivalent 'C' of 0.5, whichever is less. Up to and including the 100-year storm event must be detained on site.
- Coordination with the RVCA is required to confirm quality control requirements.

4.0 WATERMAIN

4.1 Existing Watermain

The site is located within the 2W2C pressure zone, as per the Water Distribution System mapping included in *Appendix C*. There is an existing 203 mm diameter CI watermain within Hobson Road and 305 mm diameter CI watermain within Brookfield Road available to service the development.

4.2 Proposed Watermain

Two 150 mm diameter PVC water services are proposed to service the development complete with water valves between the building and the existing watermain. The water services are proposed to be serviced by the existing 305 mm diameter watermain within Brookfield Road. The services are designed to have a minimum of 2.4 m cover. Refer to drawing *C102* for a detailed servicing layout.

The Fire Underwriters Survey 2020 (FUS) method was utilized to determine the required fire flow for the site. The 'C' factor (type of construction) for the FUS calculation was determined to be 0.8 (non-combustible type). The total floor area ('A' value) for the FUS calculation was determined to be 15,433.7 m². The results of the calculations yielded a required fire flow of 12,000 L/min for Building C & existing Building F (combined) and 9,000 L/min for Building D. The detailed calculations for the FUS can be found in *Appendix 'C'*.

The water demands for the proposed building have been calculated to adhere to the *Ottawa Design Guidelines – Water Distribution* manual and can be found in *Appendix 'C'*. The results have been summarized in *Table 1*, below. In accordance with Section 4.3.1 of the guidelines, service areas with a basic day demand greater than 50 m³/day require a redundant connection to the municipal system. The redundancy is proposed to be provided via a water valve located south of the development service lateral.

Table 1: Water Supply Design Criteria and Water Demands

Site Area	0.91 ha
Residential	280 L/person/day
1 Bedroom Apartment	1.4 persons/unit
2 Bedroom Apartment	2.1 persons/unit
3 Bedroom Apartment	3.1 persons/unit
4 Bedroom Apartment	3.4 persons/unit
Bachelor Apartment	1.4 persons/unit
Maximum Daily Peaking Factor	2.2 x avg day
Maximum Hour Peaking Factor	5.5 x avg day
Average Day Demand (L/s)	2.53
Maximum Daily Demand (L/s)	5.55
Peak Hourly Demand (L/s)	13.85
FUS Fire Flow Requirement (L/s)	200 (12,000 L/min)

The City provided the estimated water pressures at both for the average day scenario, peak hour scenario and the max day plus fire flow scenario for the demands indicated by the correspondence in *Appendix C*. Demands have decreased by approximately 7% since the boundary condition request was received which is not anticipated to have a significant impact on the results. The resulting pressures for the boundary conditions results are shown in *Table 2*, below.

Table 2: Boundary Conditions Results

Scenario	Proposed Demands (L/s)	Connection HGL (m H₂O)*/kPa		
Average Day Demand	2.53	54.5 / 534.4		
Maximum Daily + Fire Flow Demand	5.55 + 200 = 205.55	45.0 / 441.3		
Peak Hourly Demand	13.85	48.3 / 473.6		
*Adjusted for an estimated ground elevation of 77.92m above the connection point.				

The normal operating pressure range is anticipated to be 474 kPa to 534 kPa and will not be less than 275 kPa (40 psi) or exceed 689 kPa (100 psi). The proposed watermains will meet the minimum required 20 psi (140 kPa) from the *Ottawa Water Guidelines* at the ground level under maximum day demand and fire flow conditions.

To confirm the adequacy of fire flow to protect the proposed development, public fire hydrants within 150 m of the proposed building were analysed per City of Ottawa *ISTB 2018-02* Appendix I Table 1. Based on City guidelines (*ISTB-2018-02*), the existing hydrants can provide adequate fire protection to the proposed development. The results are summarized in *Table 3*, below.

Table 3: Fire Protection Confirmation

Building	Fire Flow Demand	Fire Hydrant(s)	Fire Hydrant(s)	Combined Fire
	(L/min.)	within 75m	within 150m	Flow (L/min.)
770 Brookfield Road	12,000 (FUS)	2	2	19,000

5.0 SANITARY DESIGN

5.1 Existing Sanitary Sewer

There is an existing 300 mm diameter concrete sanitary sewer within Hobson Road and a 250 mm diameter concrete sanitary sewer within Brookfield Road available to service the development. In addition, there is an existing 200 mm diameter concrete sanitary sewer within the center drive aisle that currently services the Phase 1 development.

5.2 Proposed Sanitary Sewer

A new 200 mm diameter gravity sanitary is proposed be connected to the existing 250 mm diameter sanitary sewer within Brookfield Road to service Building C. Building D is proposed to be serviced by a 200 mm diameter gravity sanitary service connected to the existing 300 mm diameter sanitary sewer within Hobson Road. A portion of sanitary flows from Building D will be directed to the 200mm diameter sanitary service currently servicing existing Building F Based on coordination with the mechanical engineer, multiple sanitary connections are expected to be required due to the development size and internal sloping for the building plumbing system. Refer to drawing *C102* for a detailed servicing layout.

The Phase II development consists of two mixed-use residential buildings. The peak design flows for the proposed buildings were calculated using criteria from the *Ottawa Sewer Guidelines* and are summarized in *Table 4*, below. Based on the unit occupancy statistics provided by the architect, the proposed site development will generate a flow of *6.01 L/s* from Building C and *3.26 L/s* for Building D. See *Appendix 'D'* of this report for more details.

Table 4: Sanitary Design Criteria

Design Parameter	Value
Site Area	0.91 ha
Residential	280 L/person/day
Bachelor & 1 Bedroom Apartment	1.4 persons/unit
2 Bedroom Apartment	2.1 persons/unit
3 Bedroom Apartment	3.1 persons/unit
4 Bedroom Apartment	3.4 persons/unit
Residential Peaking Factor	3.37 (Building C) 3.48 (Building D)
Institutional/Commercial Peaking Factor	1.00
Extraneous Flow Allowance	0.33 L/s/ha

Table 5, below, summarizes the estimated wastewater flow from the proposed development. Refer to *Appendix D* for detailed calculations.

Table 5: Summary of Estimated Sanitary Flow

Design Parameter	Building C Flow (L/s)	Building D Flow (L/s)	Total Flow (L/s)
Total Estimated Average Dry Weather Flow	1.77	0.91	2.68
Total Estimated Peak Dry Weather Flow	5.75	3.01	8.76
Total Estimated Peak Wet Weather Flow	6.01	3.26	9.27

The proposed 200 mm diameter gravity sanitary services will be installed with a minimum full flow target velocity (cleansing velocity) of 0.6 m/s and a full flow velocity of not more than 3.0 m/s. The capacity of the laterals is 34.22 L/s at a proposed slope of 1.0%. Therefore, the building services are sufficiently sized to accommodate the development. Refer to *Appendix D* for the Building C and Building D sanitary sewer design sheets.

Due to the complexity of the downstream network, City staff will need to advise of any downstream constraints.

6.0 STORM SEWER DESIGN

6.1 Existing Storm Sewers

Storm runoff from the site is currently tributary to the Sawmill Creek sub watershed. The property is currently serviced by the adjacent Phase I storm network and municipal catch basins within Brookfield Road and Hobson Road. There is an existing 375 mm diameter concrete storm sewer within Hobson Road that is available for servicing the proposed development.

6.2 Proposed Storm Sewers

A new 375 mm storm service will be extended from the existing 750 mm diameter storm sewer within Brookfield Road. The sewer system will provide attenuation for the Building C roof area using roof drains and the internal courtyard area by an internal cistern pumped to the required release rate. A cistern detail has been provided by Hobin Architecture, refer to *Appendix G*.

A new 250 mm storm service will be extended from the existing 375mm diameter concrete storm sewer within Hobson Road. The sewer system will provide attenuation for the Building D roof area using roof drains.

Runoff collected on the roof of the proposed buildings will be stored and controlled internally using roof drains. Roof drains will be used to limit the flow from the roof to the specified allowable release rate. For calculation purposes a Watts Accutrol roof drain was used estimate a reasonable roof flow. Other products maybe specified at detailed building design so long as release rates and storage volumes are respected.

Foundation drainage is proposed to be pumped without flow attenuation via the 375 mm diameter storm service extending from Building C, downstream of any cistern controls. Roof drainage will also be downstream of any cistern controls.

See CCO-22-3501 - *POST* include in *Appendix F* of this report for more details. The Stormwater Management design for the subject property will be outlined in *Section 7.0* of this report.

7.0 PROPOSED STORMWATER MANAGEMENT

7.1 Design Criteria and Methodology

Stormwater management for the proposed site will be maintained through rooftop attenuation and an internal cistern that will collect runoff from the at-grade areas within the site. The flow will be directed to the existing 750 mm diameter storm sewer within Brookfield Road.

In summary, the following design criteria have been employed in developing the stormwater management design for the site as directed by the RVCA and City:

Quality Control

• Based on the *Functional Servicing and Stormwater Management Report* prepared by DSEL, stormwater quality controls to an enhanced level of treatment are required for the subject site.

Quantity Control

• Based on the *Functional Servicing and Stormwater Management Report* prepared by DSEL, the allowable release rate for Phase 2 of the proposed development is *80.6 L/s/Ha*.

7.2 Runoff Calculations

Runoff calculations presented in this report are derived using the Rational Method, given as:

$$Q = 2.78 CIA \text{ (L/s)}$$

Where: C = Runoff coefficient

= Rainfall intensity in mm/hr (City of Ottawa IDF curves)

A = Drainage area in hectares

It is recognized that the Rational Method tends to overestimate runoff rates. As a result, the conservative calculation of runoff ensures that any SWM facility sized using this method is expected to function as intended.

The following coefficients were used to develop an average C for each area:

Roofs/Concrete/Asphalt	0.90
Gravel	0.60
Undeveloped and Grass	0.20

As per the *City of Ottawa - Sewer Design Guidelines*, the 5-year balanced 'C' value must be increased by 25% for a 100-year storm event to a maximum of 1.0.

As per the pre-consultation meeting with the City of Ottawa the time of concentration (Tc) used for pre-development shall be calculated using a minimum Tc of 10 minutes and post-development flows shall be calculated using a Tc of 10 minutes.

7.3 Pre-Development Drainage

It has been assumed that the site contains no stormwater management controls for flow attenuation. The estimated pre-development peak flows for the 5, and 100-year events are summarized below in *Table 6*. See CCO-22-3501 - *PRE* in *Appendix E* and *Appendix G* for calculations.

Drainage Area (L/s)

Area (ha)

5-Year 100-Year

A1 0.913 52.93 109.03

Table 6: Pre-Development Runoff Summary

7.4 Post-Development Drainage

The post-development release rate has been established using the *Functional Servicing and Stormwater Management Report* and City of Ottawa design criteria. Refer to *Table 7* below for further details.

Drainage Area	Area (ha)	Q (L/s)		
		2-Year	5-Year	100-Year
Ultimate Site (Phase 1 Design)	2.523	202.77	-	-
EX-1	0.511	47.64	64.40	110.06
Total	3.034	250.41	267.17	312.84
*EX-1 is controlled to existing conditions for 2, 5, and 100-year storm events.				

Table 7: Post-Development Release Rate

The proposed site drainage limits are demonstrated on the Post-Development Drainage Area Plan. See CCO-22-3501 - *POST* in *Appendix 'F'* of this report for more details. A summary of the Post-Development Runoff Calculations can be found below.

Drainage 5-year Peak 100-year Peak 100-year Storage 100-year Storage Area (ha) Flow (L/s) Available (m³) Area Flow (L/s) Required (m³) 2.52 4.62 73.15 76.93 C1 0.159 C4 0.092 Α 0.904 346.33 350.00 98.87 115.56 EX-1 0.511 **BLDG** 0.491 170.60 388.70 C2 0.225 5.46 9.36 92.42 95.48 C3 0.210 15.84 31.01 16.24 16.24 32.33 U 0.215 63.17 C5 0.028 7.39 14.07 C6 0.197 38.97 75.05 Total 3.034 201.38 312.84 698.74 927.35

Table 8: Post-Development Runoff Summary

Post development drainage will be restricted to a maximum release rate of 267.2 L/s during the 5-year storm event and 312.84 L/s during the 100-year storm event, as per Table 7 above.

Runoff for area C1 (Phase II Building D) will be stored on the roof of the proposed building and restricted using seven Watts Accutrol roof drains (or equivalent product) and will provide up to $76.9 \, m^3$ of storage. Stormwater will be conveyed to the existing storm sewer within Hobson Road via the proposed 200 mm storm service at a maximum release rate of $4.62 \, L/s$.

Runoff from area C4 (Phase II) will sheet drain without attenuation towards the Phase I storm network within the south-east corner of the site.

Runoff from area A (Phase I Controlled) and BLDG (Phase I Building Controlled) will continue to sheet drain without attenuation towards the Phase I storm network. Roof areas within this area will be controlled via roof drains. No changes to site grading and/or storm sewer sizing is proposed within this area. Refer to *Functional Servicing and Stormwater Management report* for further details.

In accordance with the *Stormwater Management Memorandum – Proposed Amendment to 770 Brookfield Road* prepared by DSEL and dated October 5th, 2020, an external drainage area south of the site currently enters the property and is collected by the Phase I design. Runoff within this area will continue to be conveyed through the Phase I system. No offsite grading is proposed.

The existing ICD, installed on the outlet site of the Phase I storm structure STM102, is proposed to be replaced with a 197mm ICD to accommodate the added Phase II area (C4). Stormwater storage will continue to be provided by the existing 350 m³ stormwater storage system. No ponding is proposed on the surface during any storm event. Overland flow routes for the Phase I area are towards Hobson Road via the southern drive aisle and towards Brookfield Road via the center drive aisle. Overland flow routes are proposed to be retained.

Runoff for area C2 (Phase II Building C) will be stored on the roof of the proposed building and restricted using thirteen Watts Accutrol roof drains (or equivalent product) to a maximum release rate of 9.36 L/s and will provide up to 95.48 m³ of storage.

Runoff from area C3 will be collected by area drains within the courtyard. The internal plumbing system will direct flow to an internal cistern. The $16.24~m^3$ internal cistern is proposed to convey stormwater to the outlet via pump at a maximum flow rate 31.0~L/s. Based on coordination with the mechanical engineer, flows in excess of the 100-year storm event will need to be directed towards Hobson Road via a cistern overflow structure. Foundation drainage will be pumped and discharged via the 375 mm storm service, downstream of cistern controls. A cistern detail has been provided by Hobin Architecture, refer to *Appendix G*.

Runoff from area U (Phase I Uncontrolled) will continue to sheet drain without attenuation towards Brookfield Road.

Runoff from area C5 (Phase II Uncontrolled) will sheet drain without attenuation towards Brookfield Road.

Runoff from area C6 (Hobson Road will sheet drain without attenuation towards Hobson Road and will be collected by the existing municipal 375 mm diameter storm sewer.

7.5 Quality Controls

The following methods will be utilized to provide quality controls for the Phase II area:

- Areas C1 & C2 will collect rooftop drainage and therefore drainage is considered clean.
- Quality controls for Area C3 will be provided via the cistern in a settling pit. No surface parking is
 proposed within this area. Cistern details are to be confirmed the Mechanical Engineer. Pumped
 water will combine with clean roof drainage before discharging to the city sewer.
- Drainage flowing towards the Phase 1 development area from C4 will be treated by the OGS unit. The manufacturer has been contacted to confirm that the OGS unit will provide 80% TSS removal for the Phase 1 development, area EX-1 and area C4.

8.0 EROSION AND SEDIMENT CONTROL

8.1 Temporary Measures

Before construction begins, temporary silt fence, straw bale or rock flow check dams will be installed at all natural runoff outlets from the property. It is crucial that these controls be maintained throughout construction and inspection of sediment and erosion control will be facilitated by the Contractor or Contract Administration staff throughout the construction period.

Silt fences will be installed where shown on the final engineering plans, specifically along the downstream property limits. The Contractor, at their discretion or at the instruction of the City, Conservation Authority or the Contract Administrator shall increase the quantity of sediment and erosion controls on-site to ensure that the site is operating as intended and no additional sediment finds its way off site. The rock flow, straw bale & silt fence check dams and barriers shall be inspected weekly and after rainfall events. Care shall be taken to properly remove sediment from the fences and check dams as required. Fibre roll barriers are to be installed at all existing curb inlet catchbasins and filter fabric is to be placed under the grates of all existing catchbasins and manholes along the frontage of the site and any new structures immediately upon installation. The measures for the existing/proposed structures is to be removed only after all areas have been paved. Care shall be taken at the removal stage to ensure that any silt that has accumulated is properly handled and disposed of. Removal of silt fences without prior removal of the sediments shall not be permitted.

Although not anticipated, work through winter months shall be closely monitored for erosion along sloped areas. Should erosion be noted, the Contractor shall be alerted and shall take all necessary steps to rectify the situation. Should the Contractor's efforts fail at remediating the eroded areas, the Contractor shall contact the City and/or Conservation Authority to review the site conditions and determine the appropriate course of action. As the ground begins to thaw, the Contractor shall place silt fencing at all required locations as soon as ground conditions warrant. Please see the *Site Grading, Drainage and Sediment & Erosion Control Plan* for additional details regarding the temporary measures to be installed and their appropriate OPSD references.

8.2 Permanent Measures

Rip-rap will be placed at all locations that have the potential for concentrated flow. It is crucial that the Contractor ensure that the geotextile is keyed in properly to ensure runoff does not undermine the rip rapped area. Additional rip rap is to be placed at erosion prone locations as identified by the Contractor / Contract Administrator / City or Conservation Authority.

It is expected that the Contractor will promptly ensure that all disturbed areas receive topsoil and seed/sod and that grass be established as soon as possible. Any areas of excess fill shall be removed or levelled as soon as possible and must be located a sufficient distance from any watercourse to ensure that no sediment is washed out into the watercourse. As the vegetation growth within the

site provides a key component to the control of sediment for the site, it must be properly maintained once established. Once the construction is complete, it will be up to the landowner to maintain the vegetation and ensure that the vegetation is not overgrown or impeded by foreign objects.

9.0 SUMMARY

- Two mixed-use residential buildings are proposed be constructed at 770 Brookfield Road.
- Dual 150 mm diameter water services are proposed to be connected to the existing 305 mm diameter watermain within Brookfield Road.
- Two 200 mm diameter sanitary services are proposed to service the Phase II development. Building C will be serviced via the 250 mm diameter sanitary sewer within Brookfield Road and Building D will be serviced via the 300 mm diameter sanitary sewer within Hobson Road and the existing 200 mm diameter sanitary service from Building F.
- A new 375 mm storm service for rooftop, surface, and foundation drainage is proposed to service the
 development. The storm service will connect to the 750 mm diameter storm sewer within Brookfield
 Road.
- A new 200 mm storm service is proposed to service rooftop drainage for Building D, extending from the 375 mm diameter storm sewer within Hobson Road.
- Storage for the 5- through 100-year storm events will be provided through roof attenuation, internal cistern attenuation, and through the existing Phase I storm sewer network.
- Quality control is proposed to be provided via the cistern settling pit and existing Phase I OGS unit.

10.0 RECOMMENDATION

Based on the information presented in this report, we recommend that City of Ottawa approve this Servicing and Stormwater Management Report in support of the proposed development at 770 Brookfield Road.

This report is respectfully being submitted for approval.

Regards,

McIntosh Perry Consulting Engineers Ltd.



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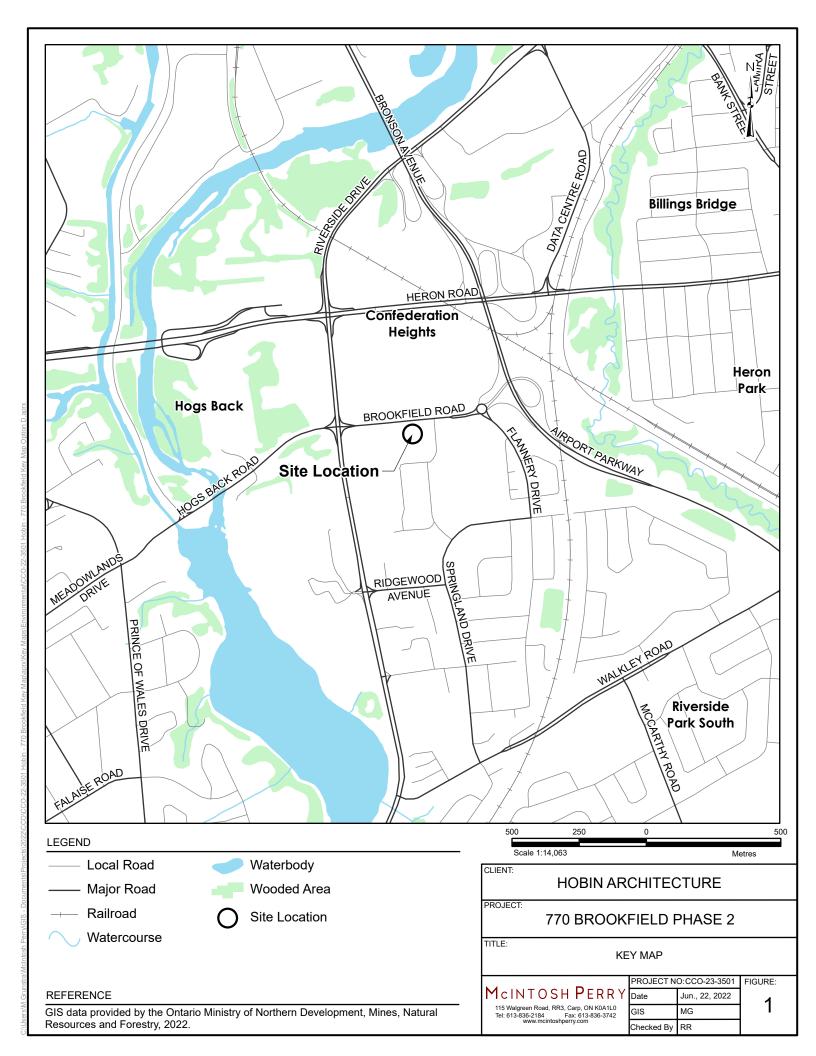
11.0 STATEMENT OF LIMITATIONS

This report was produced for the exclusive use of Hobin Architecture Inc. The purpose of the report is to assess the existing stormwater management system and provide recommendations and designs for the post-construction scenario that are in compliance with the guidelines and standards from the Ministry of the Environment, Conservation and Parks, City of Ottawa and local approval agencies. McIntosh Perry reviewed the site information and background documents listed in Section 2.0 of this report. While the previous data was reviewed by McIntosh Perry and site visits were performed, no field verification/measures of any information were conducted.

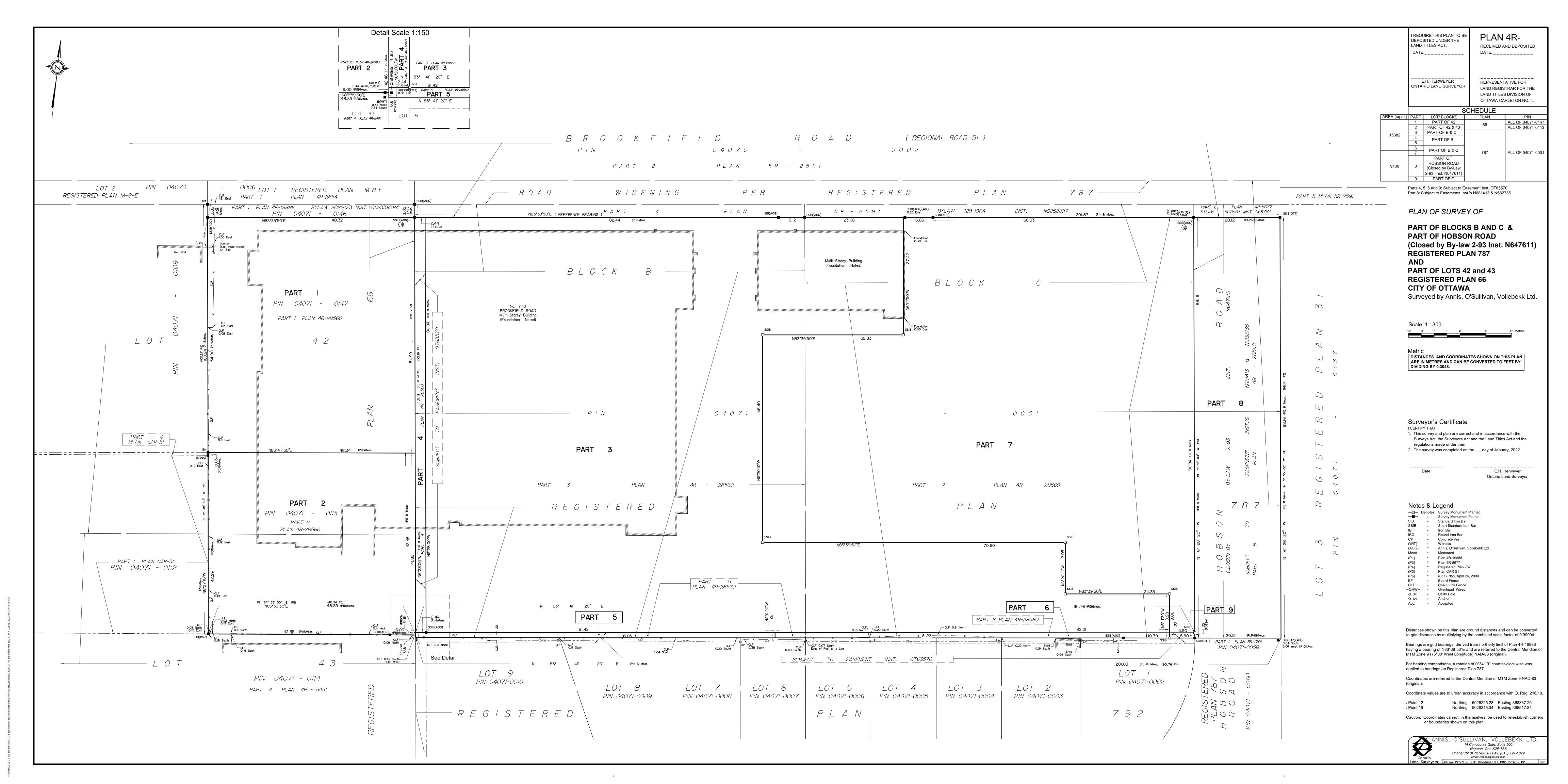
Any use of this review by a third party, or any reliance on decisions made based on it, without a reliance report is the responsibility of such third parties. McIntosh Perry accepts no responsibility for damages, if any, suffered by any third party as a result of decisions or actions made based on this review.

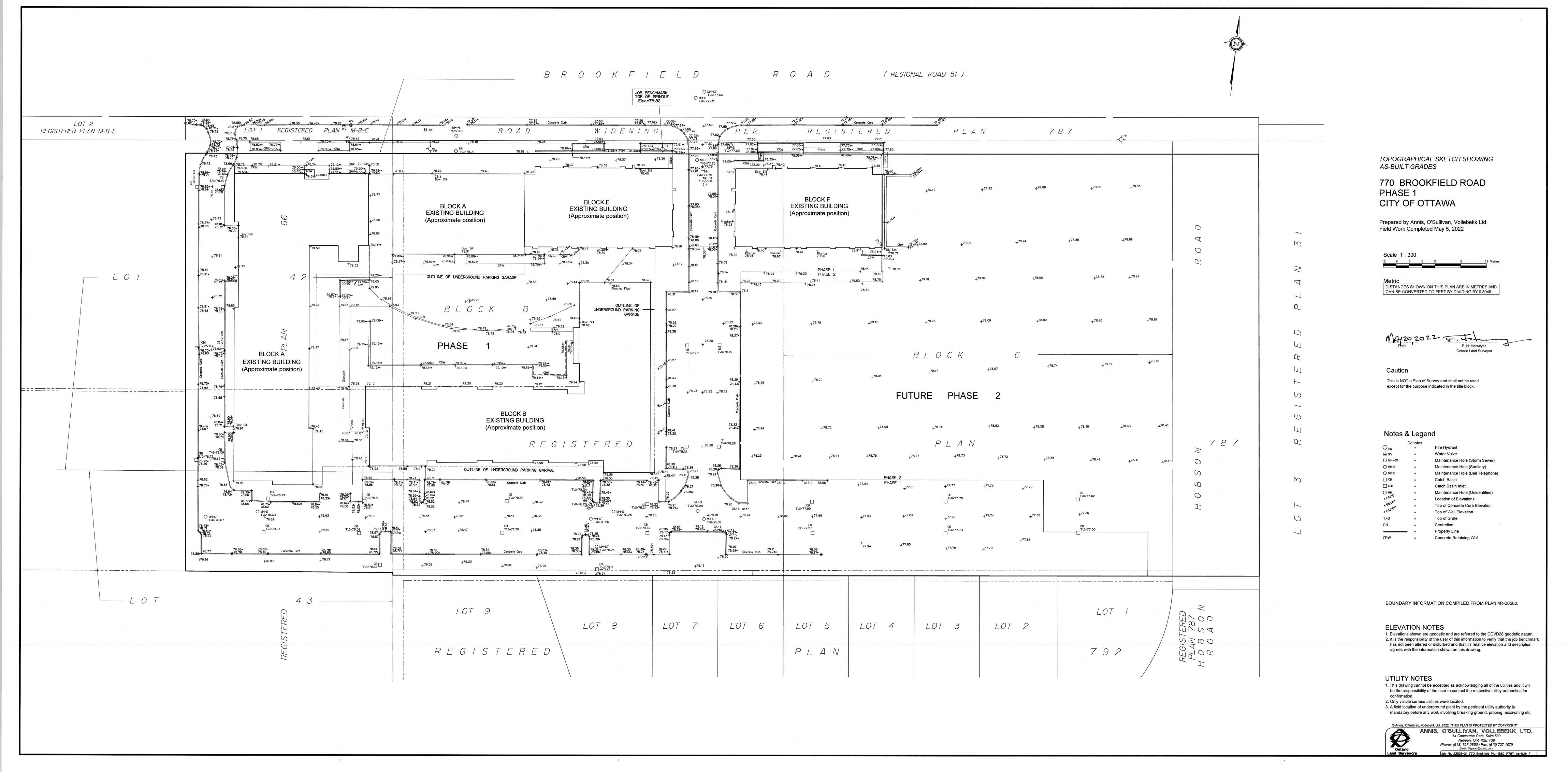
The findings, conclusions and/or recommendations of this report are only valid as of the date of this report. No assurance is made regarding any changes in conditions subsequent to this date. If additional information is discovered or becomes available at a future date, McIntosh Perry should be requested to re-evaluate the conclusions presented in this report, and provide amendments, if required.

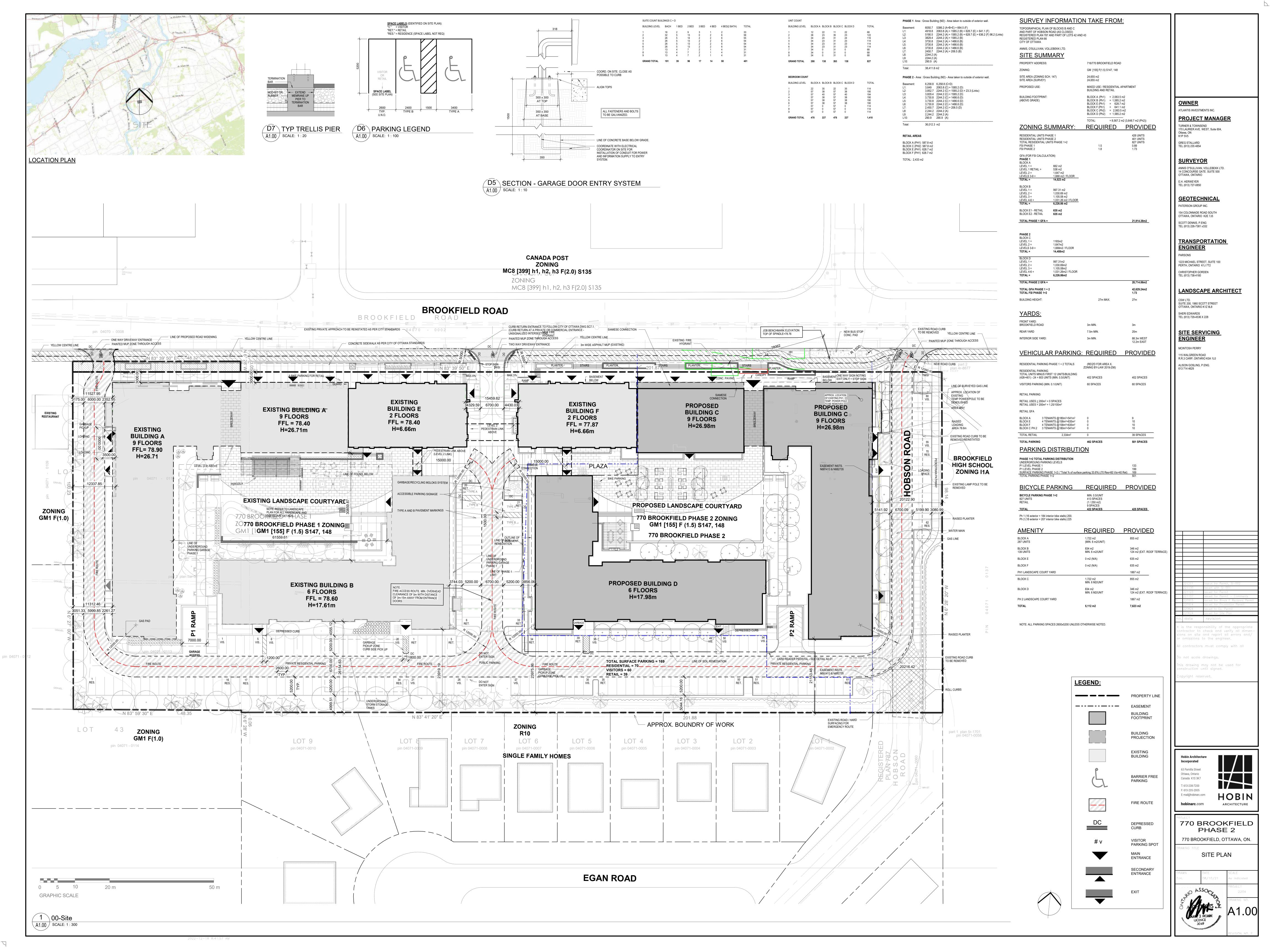
APPENDIX A KEY PLAN

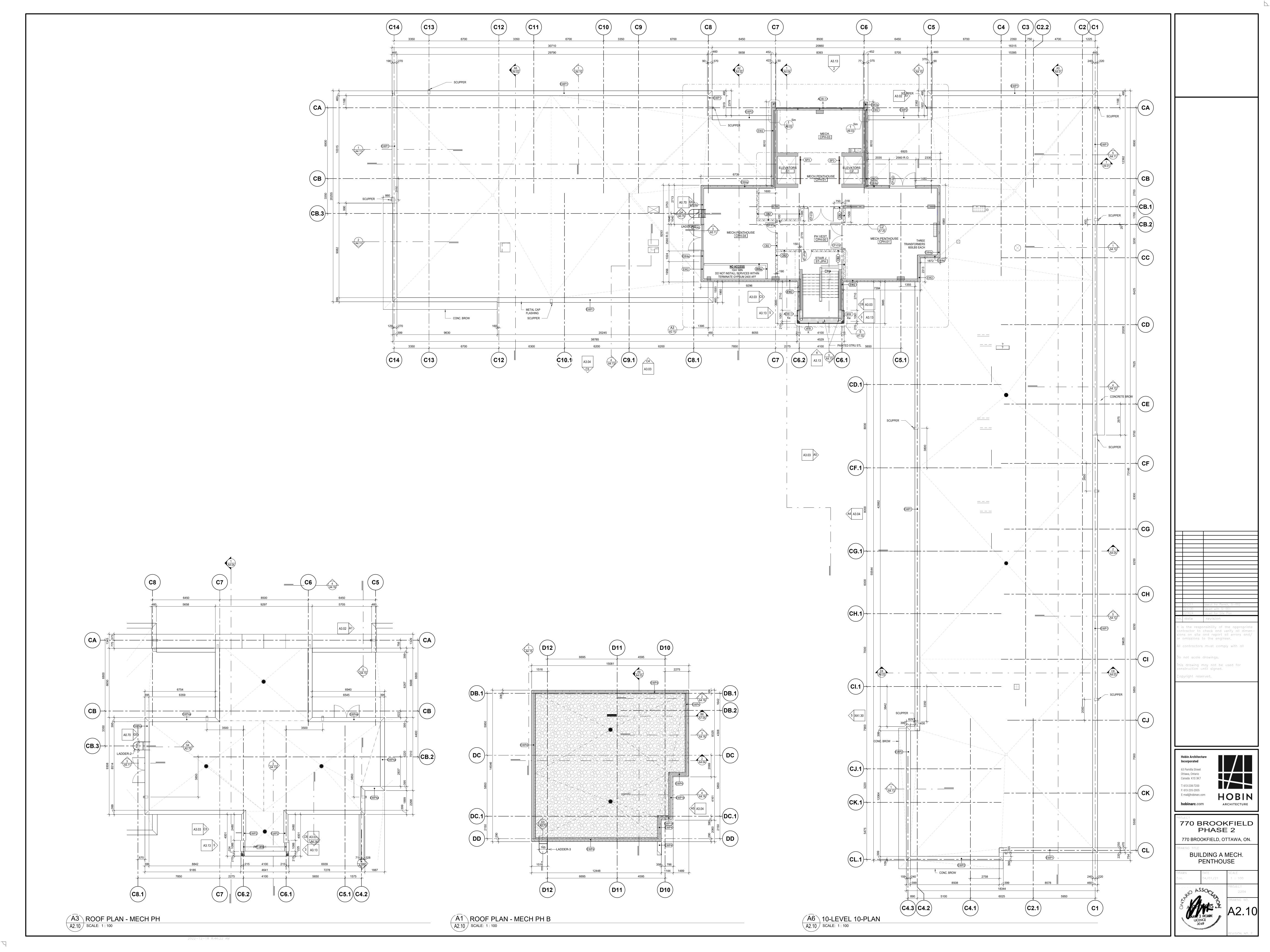


APPENDIX B BACKGROUND DOCUMENTS









FLOW CONTROL ROOF DRAINAGE DECLARATION

THIS FORM TO BE COMPLETED BY THE MECHANICAL AND STRUCTURAL ENGINEERS RESPONSIBLE FOR DESIGN

				Permit Application No.	
Project Name: Building Location:		770 Brookfield Phase 2			
		770 Brookfield Ave	770 Brookfield Ave Municipality: Ottawa		
The roof following		system has been designed in accordar	nce with the following criteria: (please check	one of the	
M1	. 🗆	Conventionally drained roof (no	flow control roof drains used).		
M2	. 🕱	Flow control roof drains meeting design:	the following conditions have been incorpo	rated in this	
		vater on the roof t more than 30m			
М3	. 🗆	A flow control drainage system tha M2 has been incorporated in this d	t does not meet the minimum drainage crite lesign	eria described in	
PROFES	SIONAL SE	EAL APPLIED BY:		PROFESS/ONLY	
Practition	er's Name:	Adrianne Mitani	Ĺ	202-11-01 % 202-11-01 % ZEE	
Firm:		Smith + Andersen			
Phone#:		613-230-1186	\	18327.002 OLINCE OF ONT AL	
City:	Ottawa	Province: Ontario	Mechanical Engineer's Seal	NCE OF OR	
S 1.	×	information provided by the Mec	ated into the overall structural design are co hanical Engineer in M2. Loads due to rain a due to snow as per Sentence 4.1.7.3 (3) Ol	re not considered	
S2 .		acting simultaneously with the sr	d incorporating the additional structural load now load. The design parameters are consist signed by the mechanical engineer.		
PROFES	SIONAL SE	EAL APPLIED BY:		SPROMA	
Practition	er's Name:	Richard Cunliffe	THE WASHINGTON	R. I. CUNLIFFE	
Firm:		Cunliffe & Associates		2022-11-01	
Phone#:		613-729-7242 x222		POVINCE OF ONTARIO	

Structural Engineer's Seal

Ottawa

City:

Province: ON

770 Brookfield Drive

Meeting Summary Notes March 30, 2022, Online Teams Meeting

Attendees:

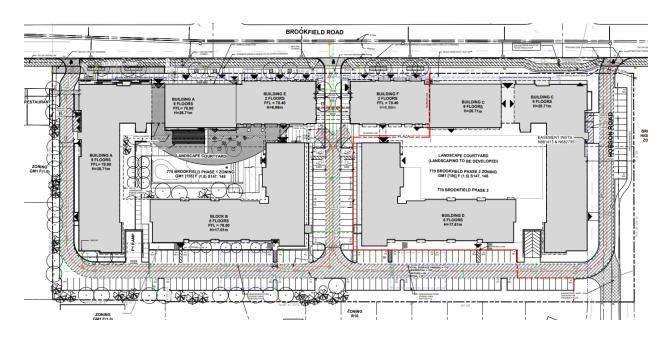
- Greg Stallard, Turner & Townsend, Owner
- Gord Lorimer, Hobin Architects
- Rheal Labelle, Hobin Architects
- Imran Shaikh, Campus Developments, Owner
- Dan Henhoeffer, Hobin Architects
- Jaime Posen, Fotenn Consultants.
- Nathan Petryshyn, Fotenn Consultants.
- Golam Sharif (Project Manager, City of Ottawa)
- Christopher Moise (Urban Designer, Architect, City of Ottawa)
- Burl Walker (Parks Planner, City of Ottawa)
- Tracey Scaramozzino (File Lead, Planner, City of Ottawa)

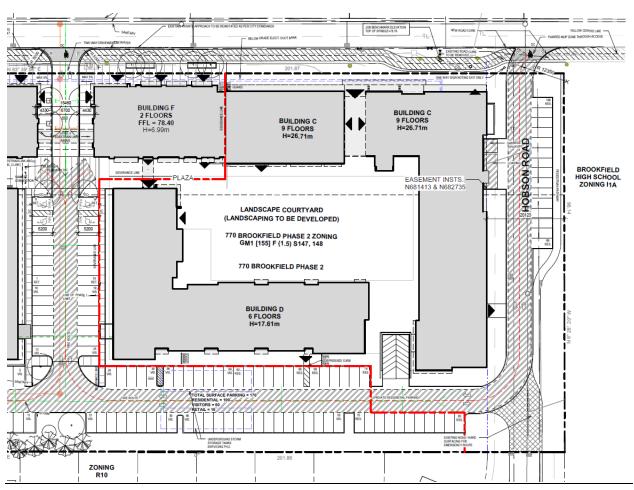
Unable to Attend:

- Mark Richardson, Planning Forester
- Jamie Batchelor, RVCA
- Wally Dubyk (Transportation Project Manager, City of Ottawa)
- Matthew Hayley, Environment Planner

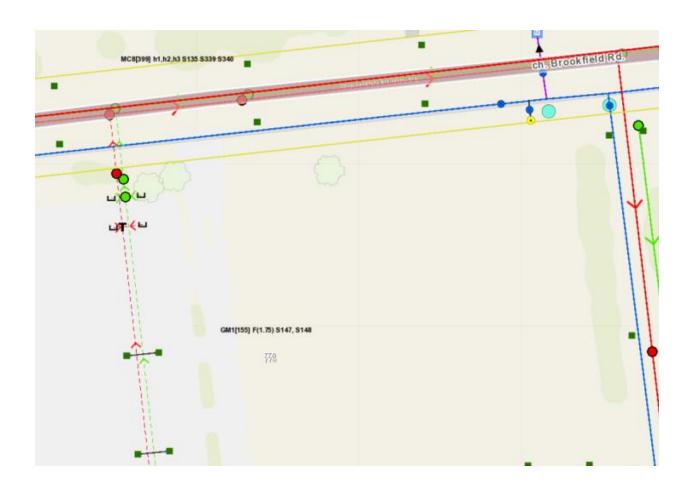
Issue of Discussion:

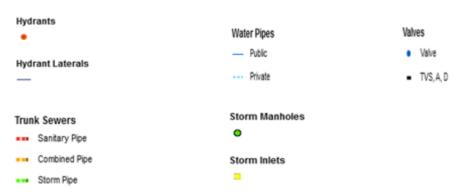
- Phase 2 of the Brookfield 'student housing' development
- Phase 1 was approved in 2019 and construction was completed in 2021.
- This is a new preconsultation meeting and a fee is req'd. The previous discussions were held several years ago and are only valid for 1 year. The fee will be refunded if an application is submitted within 1 yr.
- The legal agreement will be an amending agreement (as confirmed by Wendy Tse who was the file lead for Phase 1 of the project).
- Discussions are ongoing between the Applicant and OC Transpo regarding the placement of the permanent bus shelter in front of Phase 1.





- 1. Current Official Plan designated "General Urban Area".
- 2. **New Draft Official Plan, Approved by Council, Oct 27, 2021 –** designated Outer Urban Transect, Evolving Neighbourhod
- 3. **Zoning Information:** GM 1 [155] F(1.75) S147, S148; Schedule 147 stipulates heights and building setbacks.
- 4. Infrastructure/Servicing (Golam Sharif):
 - 1. The Servicing Study Guidelines for Development Applications are available at the following address:
 - https://ottawa.ca/en/city-hall/planning-and-development/how-developproperty/development-application-review-process-2/guide-preparing-studies-and-plans
 - 2. Servicing and site works shall be in accordance with the following documents:
 - Ottawa Sewer Design Guidelines (October 2012) and all the Technical Bulletins including, Technical Bulletin PIEDTB-2016-01 and ISTB-2018-01
 - Ottawa Design Guidelines Water Distribution (2010) and Technical Bulletins ISD-2010-2, ISDTB-2014-02 and ISTB-2018-02
 - Geotechnical Investigation and Reporting Guidelines for Development Applications in the City of Ottawa (2007)
 - City of Ottawa Slope Stability Guidelines for Development Applications (revised 2012)
 - City of Ottawa Environmental Noise Control Guidelines (January, 2016)
 - City of Ottawa Park and Pathway Development Manual (2012)
 - City of Ottawa Accessibility Design Standards (2012)
 - Ottawa Standard Tender Documents (latest version)
 - Ontario Provincial Standards for Roads & Public Works (2013)
 - 3. Record drawings and utility plans are also available for purchase from the City (Contact the City's Information Centre by email at lnformationCentre@ottawa.ca or by phone at (613) 580-2424 x 44455
 - 4. The Stormwater Management Criteria, for the subject site, is to be based on the following:
 - SWM control to 2-yr storm event.
 - The 2-yr storm event using the IDF information derived from the Meteorological Services of Canada rainfall data, taken from the MacDonald Cartier Airport, collected 1966 to 1997.
 - For separated sewer system built pre-1970 the design of the storm sewers are based on a 2 year storm.
 - The pre-development runoff coefficient or a maximum equivalent 'C' of 0.5, whichever is less (§ 8.3.7.3).
 - A calculated time of concentration (Cannot be less than 10 minutes).
 - Flows to the storm sewer in excess of the 2-year storm release rate, up to and including the 100-year storm event, must be detained on site.
 - For a combined sewer system the maximum C= 0.4 or the pre-development C value, whichever is less. In the absence of other information the allowable release rate shall be based on a 2 year storm event.
 - Please contact RVCA for specific water quality requirement.
 - 5. Deep Services:





- i. A plan view of the approximate services may be seen above. Services should ideally be grouped in a common trench to minimize the number of road cuts. The sizing of available future services is:
 - a. Connections (Brookfield):
 - i. 750 mm dia. STM (Conc)
 - ii. 300 mm dia. Watermain (CI)
 - iii. 250 mm dia. Sanitary (Conc).

- ii. Provide existing servicing information and the recommended location for the proposed connections. Services should ideally be grouped in a common trench to minimize the number of road cuts.
- iii. Connections to trunk sewers and easement sewers are typically not permitted.
- iv. Provide information on the monitoring manhole requirements should be located in an accessible location on private property near the property line (ie. Not in a parking area).
- v. Review provision of a high-level sewer.
- vi. Provide information on the type of connection permitted

 Sewer connections to be made above the springline of the sewermain as per:
 - Std Dwg S11.1 for flexible main sewers connections made using approved tee or wye fittings.
 - b. Std Dwg S11 (For rigid main sewers) *lateral must be less that 50% the diameter of the sewermain,*
 - c. Std Dwg S11.2 (for rigid main sewers using bell end insert method) for larger diameter laterals where manufactured inserts are not available; lateral must be less that 50% the diameter of the sewermain,
 - d. Connections to manholes permitted when the connection is to rigid main sewers where the lateral exceeds 50% the diameter of the sewermain. Connect obvert to obvert with the outlet pipe unless pipes are a similar size.
 - e. No submerged outlet connections.
- 6. Water Boundary condition (required to verify the current BC) requests must include the location of the service and the expected loads required by the proposed development. Please provide the following information:
 - i. Location of service
 - ii. Type of development and the amount of fire flow required (as per FUS, 1999).
 - iii. Average daily demand: I/s.
 - iv. Maximum daily demand: ____l/s.
 - v. Maximum hourly daily demand: I/s.
 - vi. Hydrant location and spacing to meet City's Water Design guidelines.
 - vii. Water supply redundancy will be required for more than 50 m3/day water demand.
- 7. Phase 1 ESAs and Phase 2 ESAs must conform to clause 4.8.4 of the Official Plan that requires that development applications conform to Ontario Regulation 153/04.
- 8. MECP ECA Requirements
 - All development applications should be considered for an Environmental Compliance Approval (ECA) by the Ministry of the Environment, Conservation, and Parks (MECP);
 - a. Consultant determines if an approval for sewage works under Section 53 of OWRA is required. Consultant then determines what type of application is required and the City's project manager confirms. (If the consultant is not clear if an ECA is required, they will work with the City to determine what is required. If the consultant it is still unclear or there is a difference of opinion only then will the City PM approach the MECP.
 - b. The project will be either transfer of review (standard), transfer of review (additional), direct submission, or exempt as per O. Reg. 525/98.

- c. Pre-consultation is not required. d. Standard Works ToR Draft ECA's are sent to the local MECP office
 - $\label{lem:continuous} ([mailto:moeccottawasewage@ontario.ca).for] moeccottawasewage@ontario.ca).for r information only$
- d. Additional ToR draft ECAs require a project summary/design brief and require a response from the local MECP (10 business day window)
- 9. Water supply redundancy will be required for more than 50 m3/day water demand.
- 10. Service connections to easement is not permitted.
- 11. PH1 sanitary servicing will have to upgrade as per the PH1 servicing report.
- 12. The site is within the Sawmill Creek sub watershed, please contact RVCA for specific SWM criteria as per the Sub watershed Study.

5. Initial Planning Comments (Tracey Scaramozzino):

- a. Discuss proposal with local Councillor and Community Associations
- b. Ensure ample greenspace/useable amenity space
- c. Use native species and avoid monocultures when possible
- d. Please provide a copy of the revised noise study that reviewed the enlarged and re-located HVAC system.
- e. Provide an update once the stop sign has been installed for vehicles leaving the site, prior to crossing the MUP.
- f. I am waiting to hear back from my colleague re. the desirability of painting the MUP green. Thank you for the offer.

6. Urban Design Comments (Christopher Moise):

- We appreciate the drawings and discussion at the pre-consultation meeting and have the following comments/questions about phase II of the proposal:
 - Are there any lessons learned that could be adapted for the second phase?
 - Were there any concerns by neighbouring properties that can be addressed in phase II?
- A scoped Design Brief is a required submittal for all Site Plan/Re-zoning applications and can be combined with the Planning Rationale. Please see the Design Brief Terms of Reference provided.
 - Note. The Design Brief submittal should have a section which addresses these pre-consultation comments;

7. Parks (Burl Walker):

a. The owner provided cash-in-lieu of parkland dedication in the amount of \$821,501.64 through the Phase 1 site plan agreement. The cash-in-lieu of parkland dedication requirement was based on the information included with the 1st submission of the Phase 1 site plan application. The Phase 1 parkland dedication requirement was calculated based on 355 proposed apartment dwelling units, a total site area of 24,655 m², a commercial gross floor area ratio of 4.1% and a residential gross floor area ratio of 95.9%. The total corresponding area of parkland dedication was calculated to be 2,385 m². The calculations were described in the 1st Site Plan

Review letter for 716 and 770 Brookfield Road prepared by Wendy Tse and dated April 24, 2018.

- b. Based on the information shown on the Phase 2 Site Plan, the combined Phase 1 and 2 development has a commercial gross floor area ratio of 4.2% and a residential gross floor area ratio of 95.8%. As the residential gross floor area ratio for the combined Phase 1 and 2 development is not greater than the ratio that was used to calculate the Phase 1 cash-in-lieu of parkland dedication requirement, there is no additional requirement for cash-in-lieu of parkland for the proposed Phase 2 development based on the provisions of the current Parkland Dedication By-law.
- c. Parks and Facilities Planning is currently undertaking a legislated review for the replacement of the Parkland Dedication By-law, with the new by-law to be considered by City Council in early July 2022. The applicant is encouraged to sign up for project notifications on the Engage Ottawa project page or by emailing the project lead at Kersten.Nitsche@ottawa.ca to ensure that they are aware of the provisions of the new by-law and any potential implications for the proposed Phase 2 site plan application.

8. Trees (Mark Richardson)

TCR requirements:

- a Tree Conservation Report (TCR) must be supplied for review along with the suite of other plans/reports required by the City
 - a. an approved TCR is a requirement of Site Plan approval.
 - b. The TCR may be combined with the LP provided all information is supplied
- 2. Any removal of privately-owned trees 10cm or larger in diameter, or city-owned trees of any diameter requires a tree permit issued under the Tree Protection Bylaw (Bylaw 2020 340); the permit will be based on an approved TCR and made available at or near plan approval.
- 3. The Planning Forester from Planning and Growth Management as well as foresters from Forestry Services will review the submitted TCR
 - a. If tree removal is required, both municipal and privately-owned trees will be addressed in a single permit issued through the Planning Forester
 - b. Compensation may be required for city owned trees if so, it will need to be paid prior to the release of the tree permit
- 4. the TCR must list all trees on site, as well as off-site trees if the CRZ extends into the developed area, by species, diameter and health condition
- 5. please identify trees by ownership private onsite, private on adjoining site, city owned, co-owned (trees on a property line)
- 6. If trees are to be removed, the TCR must clearly show where they are, and document the reason they cannot be retained
- 7. All retained trees must be shown, and all retained trees within the area impacted by the development process must be protected as per City guidelines available at Tree Protection Specification or by searching Ottawa.ca

- a. the location of tree protection fencing must be shown on the plan
- b. show the critical root zone of the retained trees
- c. if excavation will occur within the critical root zone, please show the limits of excavation
- 8. the City encourages the retention of healthy trees; if possible, please seek opportunities for retention of trees that will contribute to the design/function of the site.
- 9. For more information on the process or help with tree retention options, contact Mark Richardson mark.richardson@ottawa.ca or on City of Ottawa

LP tree planting requirements:

For additional information on the following please contact tracy.smith@Ottawa.ca

Minimum Setbacks

- Maintain 1.5m from sidewalk or MUP/cycle track.
- Maintain 2.5m from curb
- Coniferous species require a minimum 4.5m setback from curb, sidewalk or MUP/cycle track/pathway.
- Maintain 7.5m between large growing trees, and 4m between small growing trees. Park or open space planting should consider 10m spacing, except where otherwise approved in naturalization / afforestation areas. Adhere to Ottawa Hydro's planting guidelines (species and setbacks) when planting around overhead primary conductors.

Tree specifications

- Minimum stock size: 50mm tree caliper for deciduous, 200cm height for coniferous.
- Maximize the use of large deciduous species wherever possible to maximize future canopy coverage
- Tree planting on city property shall be in accordance with the City of Ottawa's Tree Planting Specification; and include watering and warranty as described in the specification (can be provided by Forestry Services).
- Plant native trees whenever possible
- No root barriers, dead-man anchor systems, or planters are permitted.
- No tree stakes unless necessary (and only 1 on the prevailing winds side of the tree)

Hard surface planting

- Curb style planter is highly recommended
- No grates are to be used and if guards are required, City of Ottawa standard (which can be provided) shall be used.
- Trees are to be planted at grade

Soil Volume

• Please ensure adequate soil volumes are met:

Tree Type/Size	Single Tree Soil Volume (m3)	Multiple Tree Soil Volume (m3/tree)
Ornamental	15	9
Columnar	15	9
Small	20	12
Medium	25	15
Large	30	18
Conifer	25	15

Please note that these soil volumes are not applicable in cases with Sensitive Marine Clay.

Sensitive Marine Clay

 Please follow the City's 2017 Tree Planting in Sensitive Marine Clay guidelines

Tree Canopy Cover

- The landscape plan shall show how the proposed tree planting will replace and increase canopy cover on the site over time, to support the City's 40% urban forest canopy cover target.
- At a site level, efforts shall be made to provide as much canopy cover as possible, through tree planting and tree retention, with an aim of 40% canopy cover at 40 years, as appropriate.
- Indicate on the plan the projected future canopy cover at 40 years for the site.

9. Environment (Matthew Hayley):

a) Bird-safe Design

Given the proposal for a residential building (greater than 4 stories), please review and incorporate bird safe design elements. Some of the risk factors include glass and related design traps such as corner glass and fly-through conditions, ventilation grates and open pipes, landscaping, light pollution. More guidance and solutions are available in the guidelines which can be found here: https://ottawa.ca/en/planning-development-and-construction/developing-property/development-application-review-process/development-application-submission/guide-preparing-studies-and-plans.

b) <u>Urban Heat Island</u>

Please add features that reduce the urban heat island effect (see OP 10.3.3) produced by the laneways, parking, landscaping and building footprint. For example, this impact can be reduced by adding large canopy trees, green roofs or vegetation walls, or constructing the parking lot or building differently.

10. Conservation Authority (Jamie Batchelor, RVCA):

a) There are no natural hazards identified on the property. There are also no natural heritage features identified on property which the RVCA would review in accordance with our MOA with the City.

b) Stormwater

The property falls within the Sawmill Creek Subwatershed Study area. Therefore the stormwater for this site will need to follow all of the recommendations in the subwatershed study. The appropriate water quality target is 'enhanced' (80% TSS removal). The stormwater management plan for the site should explore opportunities for LID measures on-site. The applicant is also strongly encouraged to refer to any upcoming new guidelines that may be coming from MECP.

11. Transportation (Wally Dubyk):

- Comments will be the same as phase1
- A screening report needs to be submitted asap.
- a) We are unable to provide comments until a comprehensive transportation review has been completed. For a development of this magnitude, and in accordance with the City's TIA Guidelines, a full Transportation Impact Study is required. In addition, the site traffic trip generation data is significant and we anticipate mitigation measures will be required for this development.

Update to the TIA Guideline Forecasting Report

- We would like to inform all consultants making TIA Forecasting Report submissions to the City of Ottawa as part of a development application, that all new applications (pre-consultation meetings dated after March 3, 2021) must use the NEW TRANS Trip Generation Manual when forecasting site generated trips using this manual (see attached).
- The TRANS committee (a joint transportation planning committee serving the National Capital region) finalized a new manual early in March 2021. The document will be available in French and English on the TRANS website http://www.ncr-trans-rcn.ca/surveys/2009-trip-generation.
- The new manual has simplified the conversion from vehicle trips to person trips and then trips by modal share. The City has also developed a spreadsheet that will apply the factors of location and building type to quickly provide the existing trip numbers by mode share.

12. Waste Collection

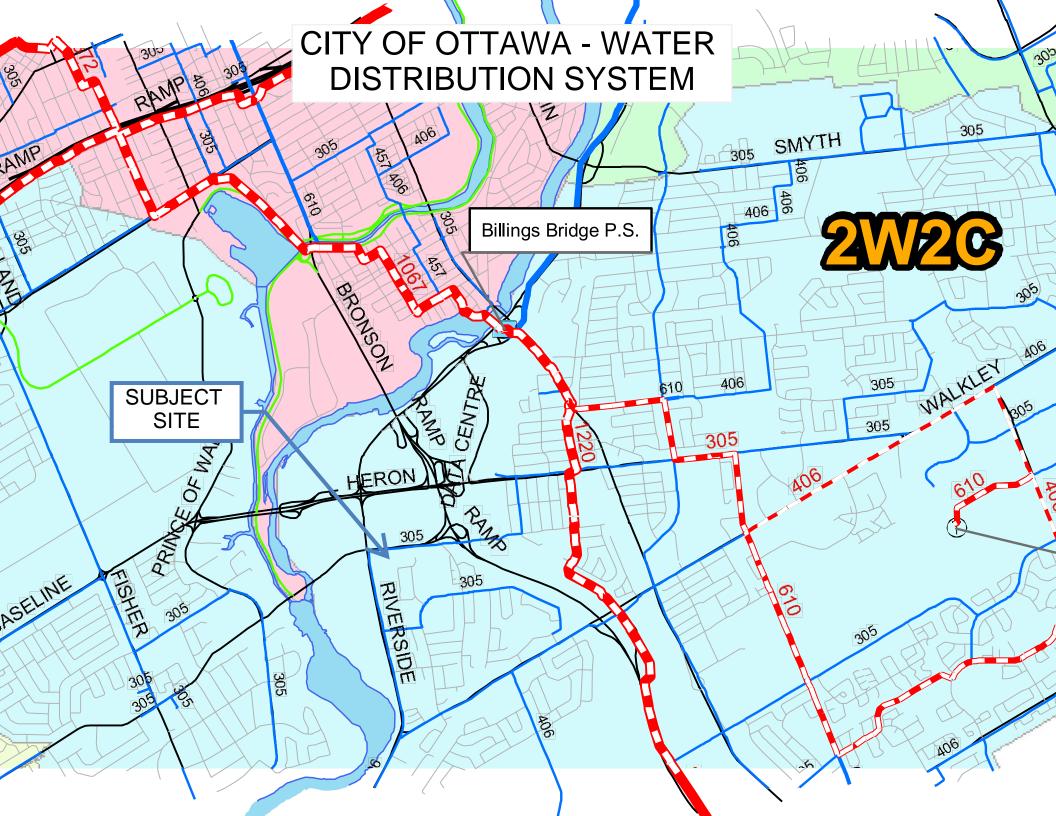
- a. Please see City's Waste Management Guidelines for multi-unit residential: http://ottawa.ca/calendar/ottawa/citycouncil/pec/2012/11-13/Solid%20Waste%20Collection%20Guidelines%20-%20Doc%201.pdf
- b) Make sure all the garbage rooms have their sizes identified
- c) Service doors must be 2.2m in width
- d) The Commercial uses will need their own waste storage area and is not to be shared with the residential uses.

13. General Information

a. Ensure that all plans and studies are prepared as per City guidelines – as available online...

https://ottawa.ca/en/city-hall/planning-and-development/information-developers/development-application-review-process/development-application-submission/guide-preparing-studies-and-plans

APPENDIX C WATERMAIN CALCULATIONS



CCO-22-3501 - 770 Brookfield Phase 2 - BUILDING C & D - Water Demands

Project: 770 Brookfield Phase 2 - BUILDING C & D

Project No.: CCO-22-3501

Designed By: RRR
Checked By: AJG

Date: November 3, 2022

Site Area: 0.91 gross ha

NUMBER OF UNITS		UNIT RATE	
	homes	3.4	persons/unit
	homes	2.7	persons/unit
	homes	2.7	persons/unit
191	units	1.4	persons/unit
39	units	1.4	persons/unit
96	units	2.1	persons/unit
17	units	3.1	persons/unit
	191 39 96	homes homes	homes 3.4 homes 2.7 homes 2.7 191 units 1.4 39 units 1.4 96 units 2.1

58 units

Total Residential Population 774 persons

 Commercial
 579 m2

 Industrial - Light
 m2

 Industrial - Heavy
 m2

AVERAGE DAILY DEMAND

4 Bedroom Apartment

DEMAND TYPE	AMOUNT	UNITS	
Residential	280	L/c/d	
Industrial - Light	35,000	L/gross ha/d	1
Industrial - Heavy	55,000	L/gross ha/d	1
Shopping Centres	2,500	L/(1000m² /d	1
Hospital	900	L/(bed/day)	
Schools	70	L/(Student/d)	1
Trailer Park with no Hook-Ups	340	L/(space/d)	1
Trailer Park with Hook-Ups	800	L/(space/d)	1
Campgrounds	225	L/(campsite/d)	1
Mobile Home Parks	1,000	L/(Space/d)	1
Motels	150	L/(bed-space/d)	1
Hotels	225	L/(bed-space/d)	1
Tourist Commercial	28,000	L/gross ha/d	1
Other Commercial	28,000	L/gross ha/d	1
	Residential	2.51	L/s
AVERAGE DAILY DEMAND	Commerical/Industrial/		
	Institutional	0.02	L/s

3.4

persons/unit

MAXIMUM DAILY DEMAND

DEMAND TYPE	AMOUNT		UNITS
Residential	2.2	x avg. day	L/c/d
Industrial	1.5	x avg. day	L/gross ha/d
Commercial	1.5	x avg. day	L/gross ha/d
Institutional	1.5	x avg. day	L/gross ha/d
	Residential	5.52	L/s
MAXIMUM DAILY DEMAND	Commerical/Industrial/		
	Institutional	0.03	L/s

MAXIMUM HOUR DEMAND

DEMAND TYPE	Д	MOUNT	UNITS
Residential	5.5	x avg. day	L/c/d
Industrial	1.8	x max. day	L/gross ha/d
Commercial	1.8	x max. day	L/gross ha/d
Institutional	1.8	x max. day	L/gross ha/d
	Residential	13.80	L/s
MAXIMUM HOUR DEMAND	Commerical/Industrial/		
	Institutional	0.05	L/s

WATER DEMAND DESIGN FLOWS PER UNIT COUNT CITY OF OTTAWA - WATER DISTRIBUTION GUIDELINES, JULY 2010

AVERAGE DAILY DEMAND	2.53	L/s
MAXIMUM DAILY DEMAND	5.55	L/s
MAXIMUM HOUR DEMAND	13.85	L/s

CCO-22-3501 - 770 Brookfield Phase 2-Building C & F - Fire Underwriters Survey

Project: 770 Brookfield Phase 2-Building C & F

Project No.: CCO-22-3501 Designed By: RRR Checked By: AJG November 3, 2022

From the Fire Underwriters Survey (2020)

Date:

From Part II – Guide for Determination of Required Fire Flow Copyright I.S.O.:

City of Ottawa Technical Bulletin ISTB-2018-02 Applied Where Applicable

A. BASE REQUIREMENT (Rounded to the nearest 1000 L/min)

 $F = 220 \times C \times VA$ Where: **F** = Required fire flow in liters per minute

C = Coefficient related to the type of construction.

A = The total floor area in square meters (including all storey's, but excluding basements at least 50 percent below grade) in

the building being considered.

Construction Type Non-Combustible Construction

c A 21,585.6 m²

Total Floor Area (per the 2020 FUS Page 20 - Total Effective Area) 13,585.5 m²

*Unprotected Vertical Openings

Calculated Fire Flow

20,514.0 L/min 21,000.0 L/min

B. REDUCTION FOR OCCUPANCY TYPE (No Rounding)

From Page 24 of the Fire Underwriters Survey:

-15% **Limited Combustible**

17,850.0 L/min Fire Flow

C. REDUCTION FOR SPRINKLER TYPE (No Rounding)

-50% Fully Supervised Sprinklered

-8,925.0 L/min

D. INCREASE FOR EXPOSURE (No Rounding)

	Separation Distance (m)	Cons.of Exposed Wall	Length Exposed Adjacent Wall (m)	Height (Stories)			
Exposure 1	Over 30 m	Ordinary - Mass Timber (Unprotected)	100	2	200.0	0%	
Exposure 2	Over 30 m	Ordinary - Mass Timber (Unprotected)	126	2	252.0	0%	
Exposure 3	10.1 to 20	Fire Resistive - Non Combustible (Unprotected Openings)	66	6	396.0	8%	
Exposure 4	10.1 to 20	Fire Resistive - Non Combustible (Unprotected Openings)	18	6	108.0	8%	
					% Increase*	16%	

2,856.0 L/min

E. Total Fire Flow (Rounded to the Nearest 1000 L/min)

Fire Flow	11,781.0 L/min
Fire Flow Required**	12,000.0 L/min

^{*}In accordance with Part II, Section 4, the Increase for separation distance is not to exceed 75%

^{**}In accordance with Section 4 the Fire flow is not to exceed 45,000 L/min or be less than 2,000 L/min

CCO-22-3501 - 770 Brookfield Phase 2-Building D - Fire Underwriters Survey

Project: 770 Brookfield Phase 2-Building D

Project No.: CCO-22-3501 Designed By: RRR Checked By: AJG November 3, 2022

From the Fire Underwriters Survey (2020)

Date:

From Part II – Guide for Determination of Required Fire Flow Copyright I.S.O.: City of Ottawa Technical Bulletin ISTB-2018-02 Applied Where Applicable

A. BASE REQUIREMENT (Rounded to the nearest 1000 L/min)

 $F = 220 \times C \times VA$ Where:

F = Required fire flow in liters per minute

C = Coefficient related to the type of construction.

A = The total floor area in square meters (including all storey's, but excluding basements at least 50 percent below grade) in

the building being considered.

Construction Type Non-Combustible Construction

c

9,421.9 m²

Total Floor Area (per the 2020 FUS Page 20 - Total Effective Area) 6,296.2 m²

*Unprotected Vertical Openings

Calculated Fire Flow

13,965.3 L/min 14,000.0 L/min

B. REDUCTION FOR OCCUPANCY TYPE (No Rounding)

From Page 24 of the Fire Underwriters Survey:

-15% **Limited Combustible**

11,900.0 L/min Fire Flow

C. REDUCTION FOR SPRINKLER TYPE (No Rounding)

-50% Fully Supervised Sprinklered

-5,950.0 L/min

D. INCREASE FOR EXPOSURE (No Rounding)

	Separation Distance (m)	Cons.of Exposed Wall	Length Exposed Adjacent Wall (m)	Height (Stories)	Length-Height Factor		
Exposure 1	3.1 to 10	Fire Resistive - Non Combustible (Unprotected Openings)	33	2	66.0	9%	
Exposure 2	10.1 to 20	Fire Resistive - Non Combustible (Unprotected Openings)	55	9	495.0	8%	
Exposure 3	Over 30 m	Ordinary - Mass Timber (Unprotected)	10	2	20.0	0%	
Exposure 4	10.1 to 20	Fire Resistive - Non Combustible (Unprotected Openings)	18	6	108.0	8%	
					% Increase*	25%	

2.975.0 L/min

E. Total Fire Flow (Rounded to the Nearest 1000 L/min)

Fire Flow	8,925.0 L/min
Fire Flow Required**	9,000.0 L/min

^{*}In accordance with Part II, Section 4, the Increase for separation distance is not to exceed 75%

^{**}In accordance with Section 4 the Fire flow is not to exceed 45,000 L/min or be less than 2,000 L/min

CCO-22-3501 - 770 Brookfield Phase 2 - Boundary Condition Unit Conversion

Project: 770 Brookfield Phase 2

Project No.: CCO-22-3501
Designed By: RRR

Checked By: AJG
Date: November 3, 2022

Boundary Conditions Unit Conversion

BROOKFIELD ROAD & HOBSON ROAD

Scenario	Height (m)	Elevation (m)	m H ₂ O	PSI	kPa
Avg. DD	130.0	75.5	54.5	77.5	534.4
Fire Flow - Brookfield (200 L/s or 12,000 L/min)	120.5	75.5	45.0	64.0	441.3
Fire Flow - Hobson (200 L/s or 12,000 L/min)	118.5	75.5	43.0	61.2	421.6
Peak Hour	123.8	75.5	48.3	68.7	473.6

Alison Gosling

From: Sharif, Golam <sharif.sharif@ottawa.ca>

Sent: June 23, 2022 12:25 PM

To: Ryan Robineau
Cc: Alison Gosling

Subject: RE: 770 Brookfield Road Boundary Condition Request

Attachments: 770 Brookfield Road June 2022.pdf

Follow Up Flag: Follow up Flag Status: Flagged

Hi Ryan,

Please see the requested BC below. I believe they had to put two connections to work the model. However, attached is the information.

The following are boundary conditions, HGL, for hydraulic analysis at 770 Brookfield Road (zone 2W2C) assumed to connected to the 203 mm on Brookfield Road and the 203 mm on Hobson Road (see attached PDF for location).

Both Connections:

Minimum HGL: 123.8 m Maximum HGL: 130.0 m

Max Day + Fire Flow (200 L/s): 120.5 m (Connection 1) Max Day + Fire Flow (200 L/s): 118.5 m (Connection 2)

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

Thanks.

Sharif

From: Ryan Robineau <r.robineau@mcintoshperry.com>

Sent: June 22, 2022 2:35 PM

To: Sharif, Golam <sharif.sharif@ottawa.ca>

Cc: Alison Gosling <a.gosling@mcintoshperry.com>

Subject: RE: 770 Brookfield Road Boundary Condition Request

CAUTION: This email originated from an External Sender. Please do not click links or open attachments unless you recognize the source.

ATTENTION : Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.

Hello Sharif,

Just following up to see if you have received the Boundary Condition request below.

Thanks,

From: Ryan Robineau <r.robineau@mcintoshperry.com>

Sent: June 7, 2022 10:25 AM **To:** sharif.sharif@ottawa.ca

Cc: Alison Gosling <a.gosling@mcintoshperry.com>

Subject: 770 Brookfield Road Boundary Condition Request

Dear Sharif,

We would like to request Boundary Conditions for 770 Brookfield Road. The proposed development consists of two mixed use residential buildings. Building C will consist of 288 units with 14,488m² of floor area and connect to existing Building F. Building D will consist of 138 units with 6,227m² of floor area. Please provide boundary conditions for potential service connections to the 305 mm Dia. watermain on Brookfield Road and the 203 mm Diam. watermain on Hobson Road (see attached figure).

- The estimated fire flow is 12,000 L/min based on the FUS
- Total average daily demand: 2.72 l/s.
- Total maximum daily demand: 5.97 l/s.
- Total maximum hourly daily demand: 14.90 l/s.

Regards,

Ryan Robineau, EIT

Civil Engineering Technologist

T. 613.714.6611

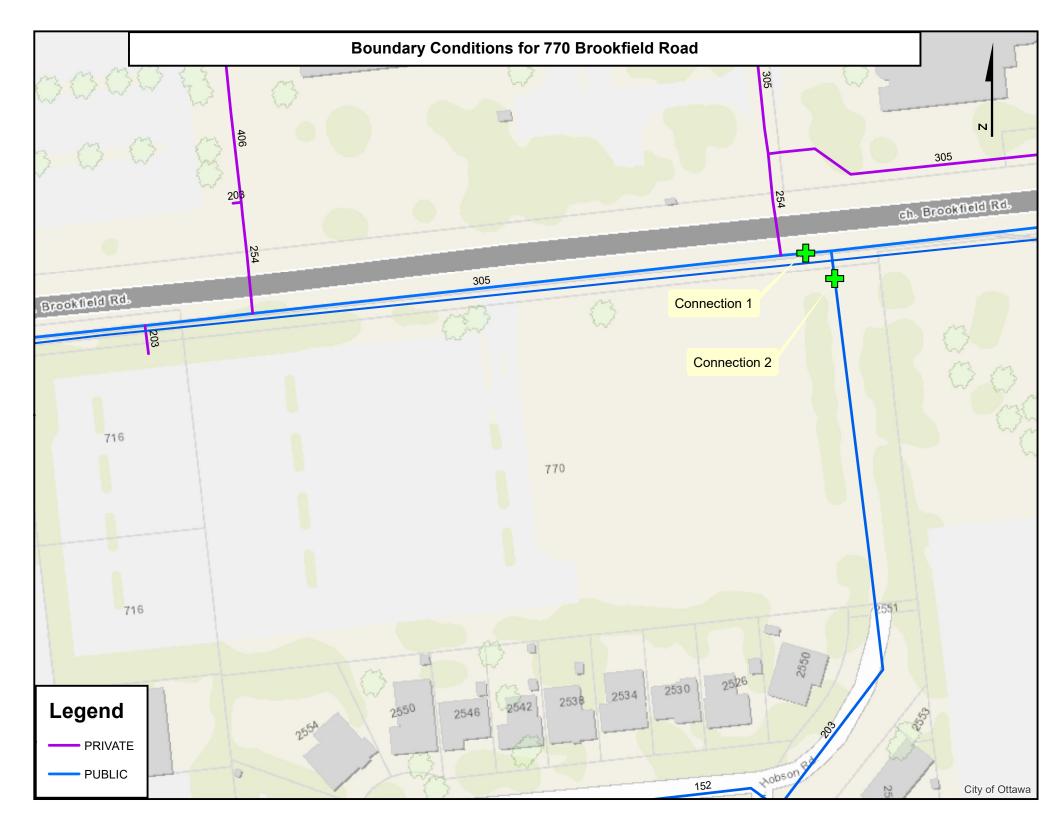
r.robineau@mcintoshperry.com | www.mcintoshperry.com

McINTOSH PERRY

Turning Possibilities Into Reality

Confidentiality Notice - If this email wasn't intended for you, please return or delete it. Click here to read all of the legal language around this concept.





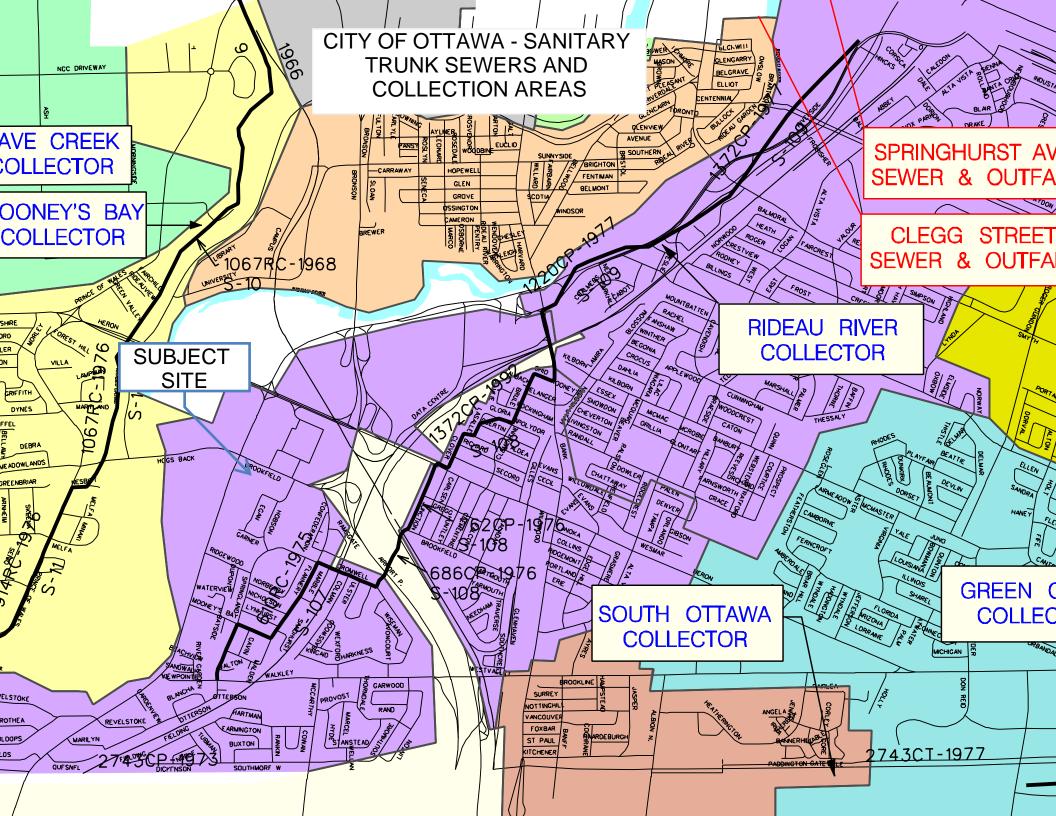
770 Brookfield Hydrant Coverage Figure



Hydrants Within 75m: 2

Hydrants Within 150m: 2

APPENDIX D SANITARY CALCULATIONS



CCO-22-3501 - 770 Brookfield Phase 2 - Block C - Sanitary Demands

770 Brookfield Phase 2 - Block C Project: Project No.: CCO-22-3501 RRR Designed By: Checked By: AJG Date: November 3, 2022 Site Area 0.91 Gross ha Bachelor 1.40 Persons per unit 1.40 1 Bedroom 33 Persons per unit 57 2 Bedroom 2.10 Persons per unit 3 Bedroom 16 3.10 Persons per unit 4 Bedroom 41 3.40 Persons per unit **Total Population** 518 Persons 579.00 m² Commercial Area 855.00 m²

DESIGN PARAMETERS

Amenity Space

Institutional/Commercial Peaking Facto

Residential Peaking Factor 3.37 * Using Harmon Formula = $1+(14/(4+P^0.5))*0.8$

1

where P = population in thousands, Harmon's Correction Factor = 0.8

Mannings coefficient (n) 0.013

Demand (per capita) 280 L/day Infiltration allowance 0.33 L/s/Ha

EXTRANEOUS FLOW ALLOWANCES

Infiltration / Inflow	Flow (L/s)
Dry	0.05
Wet	0.25
Total	0.30

AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	POPULATION / AREA	Flow (L/s)
Residential	280	L/c/d	518	1.68
Industrial - Light**	35,000	L/gross ha/d		0
Industrial - Heavy**	55,000	L/gross ha/d		0
Commercial / Amenity	2,800	L/(1000m² /d)	1434.00	0.05
Hospital	900	L/(bed/day)		0
Schools	70	L/(Student/d)		0
Trailer Parks no Hook-Ups	340	L/(space/d)		0
Trailer Park with Hook-Ups	800	L/(space/d)		0
Campgrounds	225	L/(campsite/d)		0
Mobile Home Parks	1,000	L/(Space/d)		0
Motels	150	L/(bed-space/d)		0
Hotels	225	L/(bed-space/d)		0
Office	75	L/7.0m ² /d		0
Tourist Commercial	28,000	L/gross ha/d		0
Other Commercial	28,000	L/gross ha/d		0

AVERAGE RESIDENTIAL FLOW	1.68	L/s
PEAK RESIDENTIAL FLOW	5.66	L/s
AVERAGE ICI FLOW	0.05	L/s
PEAK INSTITUTIONAL/COMMERCIAL FLOW	0.05	L/s
PEAK INDUSTRIAL FLOW	0.00	L/s
TOTAL PEAK ICI FLOW	0.05	L/s

TOTAL SANITARY DEMAND

TOTAL ESTIMATED AVERAGE DRY WEATHER FLOW	1.77	L/s
TOTAL ESTIMATED PEAK DRY WEATHER FLOW	5.75	L/s
TOTAL ESTIMATED PEAK WET WEATHER FLOW	6.01	L/s

SANITARY SEWER DESIGN SHEET

PROJECT: CCO-22-350

LOCATION: 770 Brookfield Road - Phase 2 (Building C)

CLIENT: Hobin Architecture

	LOC	ATION				RESIDENTIAL									ICI AREAS INF							RATION ALL	OWANCE	FLOW			SEWER DATA						
1	2		3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31		
						UNIT	TYPES		AREA	POPU	LATION		PEAK			ARE	4 (ha)			PEAK	ARE	A (ha)	FLOW	DESIGN	CAPACITY	LENGTH	DIA	SLOPE	VELOCITY	AVAI	ILABLE		
STREET	AREA	ID	FROM	то	BAC/1-BED	2-BED	3-BED	4-BED	(ha)	IND	сим	PEAK	FLOW	INSTITU	JTIONAL	COMM	1ERCIAL	INDUS	STRIAL	FLOW	IND	сим	(L/s)	FLOW	(L/s)	()	(mm)	(%)	(full)	CAP	ACITY		
			MH	МН	BAC/ 1-BED	Z-BED	3-DED	4-BED	(na)	IND	COIVI	FACTOR	(L/s)	IND	CUM	IND	CUM	IND	CUM	(L/s)	IND	COIVI	(L/S)	(L/s)	(L/S)	(m)	(mm)	(%)	(m/s)	L/s	(%)		
			BLDG	EX. Sewer	149	57	16	41	0.91	518.0	518.0	3.37	5.66		0.00	0.14	0.14		0.00	0.05	0.91	0.91	0.30	6.01	34.22	15.23	200	1.00	1.055	28.21	82.44		
Design Parameters:					Notes:							Designed:		RRR			No.				=	Revision		-	•				Date				
					1. Manning	gs coefficien	t (n) =		0.013								1.				ISSI	UED FOR RE	VIEW						2022-06-24				
Residential			ICI Areas		2. Demand	d (per capita)):	280	L/day								2				ISSU	UED FOR RE	VIEW						2022-11-04				
BAC/1-																																	
BED 1.4 p/p/u				Peak Factor	3. Infiltrati	ion allowanc	e:	0.33	L/s/Ha			Checked:		AJG																			
2-BED 2.1 p/p/u	INST	28,000	L/Ha/day	1	4. Residen	tial Peaking	Factor:																										
3-BED 3.1 p/p/u	COM	28,000	L/Ha/day	1		Harmon Fo	rmula = 1+(14/(4+P^0.5	5)*0.8)																								
4-BED 3.4 p/p/u	IND	35,000	L/Ha/day	MOE Chart		where P = p	opulation i	n thousands	;			Project No.	:	CCO-22-350)1																		
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																													1 of 1				

CCO-22-3501 - 770 Brookfield Phase 2 - Block D - Sanitary Demands

Project:	770 Brookfield Phase	2 - Block D		
Project No.:	CCO-22-3501			
Designed By:	RRR			
Checked By:	AJG			
Date:	November 3, 2022			
Site Area	0.91	Gross ha		
Bachelor	74		1.40	Persons per unit
1 Bedroom	6		1.40	Persons per unit
2 Bedroom	37		2.10	Persons per unit
3 Bedroom	2		3.10	Persons per unit
4 Bedroom	19		3.40	Persons per unit
Total Population	261	Persons		_
Commercial Area	0.00	m ²		_
Amenity Space	470.00	m ²		_

DESIGN PARAMETERS

Institutional/Commercial Peaking Facto

Residential Peaking Factor 3.48 * Using Harmon Formula = $1+(14/(4+P^0.5))*0.8$

where P = population in thousands, Harmon's Correction Factor = 0.8

Mannings coefficient (n) 0.013

Demand (per capita) 280 L/day Infiltration allowance 0.33 L/s/Ha

EXTRANEOUS FLOW ALLOWANCES

Infiltration / Inflow	Flow (L/s)
Dry	0.05
Wet	0.25
Total	0.30

AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	POPULATION / AREA	Flow (L/s)
Residential	280	L/c/d	261	0.85
Industrial - Light**	35,000	L/gross ha/d		0
Industrial - Heavy**	55,000	L/gross ha/d		0
Commercial / Amenity	2,800	L/(1000m² /d)	470.00	0.02
Hospital	900	L/(bed/day)		0
Schools	70	L/(Student/d)		0
Trailer Parks no Hook-Ups	340	L/(space/d)		0
Trailer Park with Hook-Ups	800	L/(space/d)		0
Campgrounds	225	L/(campsite/d)		0
Mobile Home Parks	1,000	L/(Space/d)		0
Motels	150	L/(bed-space/d)		0
Hotels	225	L/(bed-space/d)		0
Office	75	L/7.0m ² /d		0
Tourist Commercial	28,000	L/gross ha/d		0
Other Commercial	28,000	L/gross ha/d		0

AVERAGE RESIDENTIAL FLOW	0.85	L/s
PEAK RESIDENTIAL FLOW	2.95	L/s
AVERAGE ICI FLOW	0.02	L/s
PEAK INSTITUTIONAL/COMMERCIAL FLOW	0.02	L/s
PEAK INDUSTRIAL FLOW	0.00	L/s
TOTAL PEAK ICI FLOW	0.02	L/s

TOTAL SANITARY DEMAND

TOTAL ESTIMATED AVERAGE DRY WEATHER FLOW	0.91	L/s
TOTAL ESTIMATED PEAK DRY WEATHER FLOW	3.01	L/s
TOTAL ESTIMATED PEAK WET WEATHER FLOW	3.26	L/s

SANITARY SEWER DESIGN SHEET

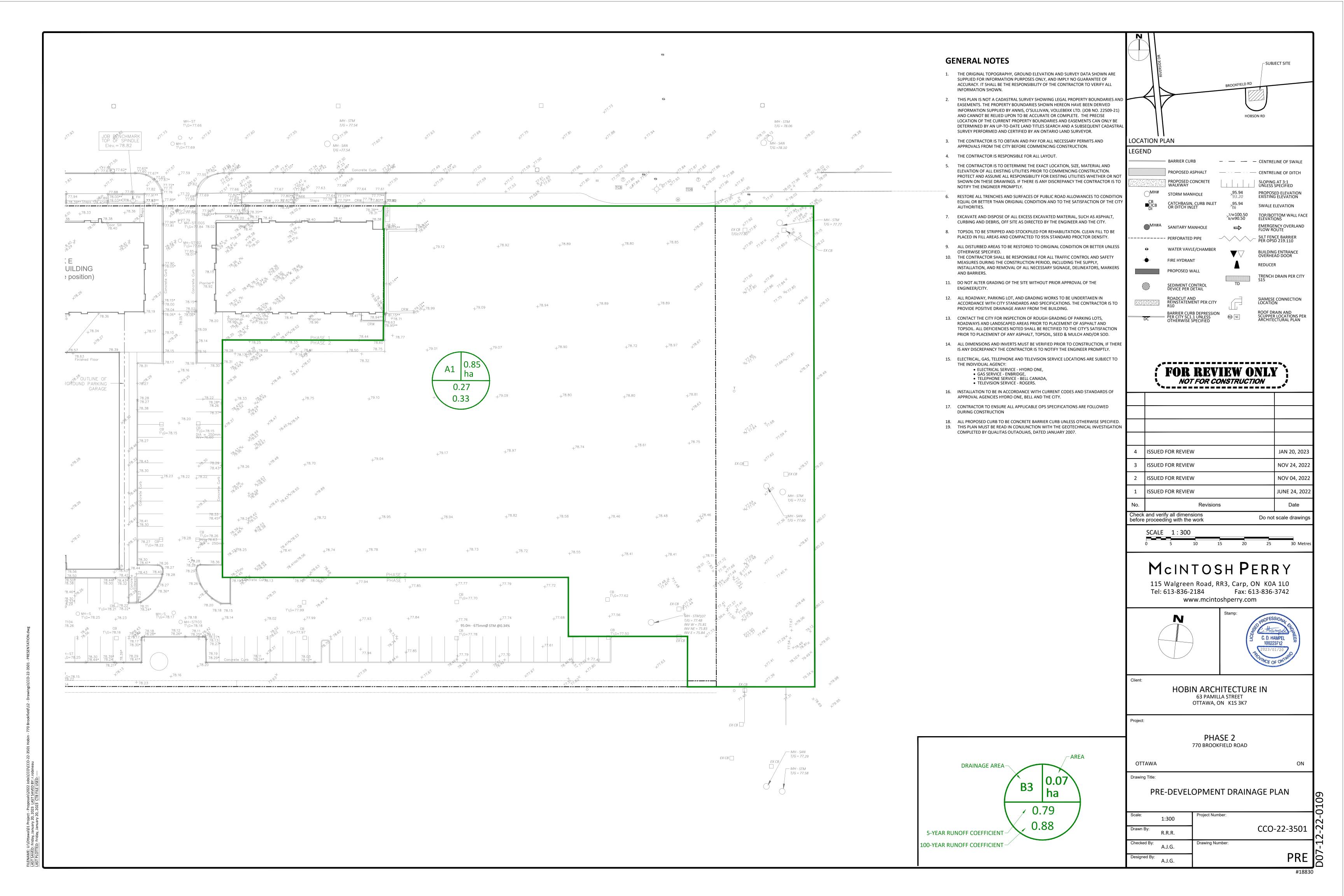
PROJECT: CCO-22-3501

LOCATION: 770 Brookfield Road - Phase 2 (Building D)

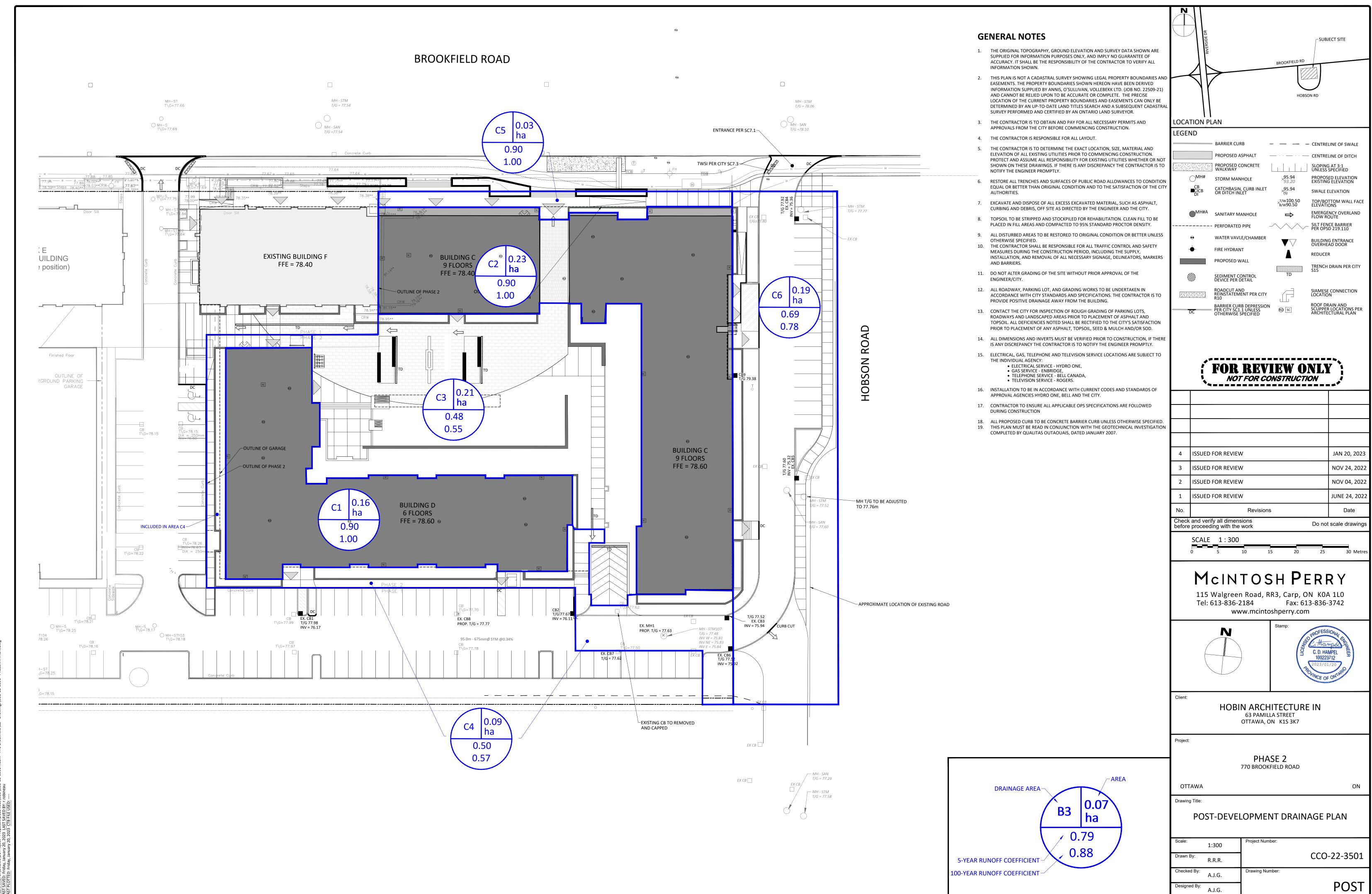
CLIENT: Hobin Architecture

	LOC	ATION			RESIDENTIAL											ICI AREAS				INFILTR	ATION ALLC	WANCE	FLOW	W SEWER DATA								
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31		
					UNIT	T TYPES		AREA	POPU	LATION		PEAK			ARE	4 (ha)			PEAK	AREA	\ (ha)	FLOW	DESIGN	CAPACITY	LENGTH	DIA	SLOPE	VELOCITY	AVAI	ILABLE		
STREET	AREA	ID FROM	TO	BCH/1-BED	2 DED	3-BED	4-BED	(ha)	IND	CUM	PEAK	FLOW	INSTIT	UTIONAL	COMM	1ERCIAL	INDU:	STRIAL	FLOW	IND	CUM	(L/s)	FLOW	(L/s)	(m)	(mm)	(%)	(full)	CAP	PACITY		
		MH	MH	DUT/ I-DED	Z-DED	3-DED	4-DED	(Ha)	IND	CUIVI	FACTOR	(L/s)	IND	CUM	IND	CUM	IND	CUM	(L/s)	IND	CUIVI	(L/S)	(L/s)	(L/S)	(111)	(111111)	(%)	(m/s)	L/s	(%)		
	BUILDIN	IG D BLDG	EX Sewer	80	37	2	19	0.91	261	261	3.48	2.94		0.00	0.05	0.05		0.00	0.02	0.91	0.91	0.30	3.26	34.22	5.91	200	1.00	1.055	30.95	90.46		
																														<u> </u>		
Design Parameters:				Notes:							Designed:		RRR			No.					Revision							Date				
					s coefficien			0.013								1.					ued For Rev							2022-11-04				
Residential		ICI Areas		2. Demand	(per capita	a):	280) L/day								2				lss	ued For Revi	iew						2023-01-20				
BCH/1-																														,		
BED 1.4 p/p/u			Peak Factor	_			0.33	B L/s/Ha			Checked:		AJG																			
2-BED 2.1 p/p/u	INST	28,000 L/Ha/day	1.5	Resident																												
3-BED 3.1 p/p/u	COM	28,000 L/Ha/day	1.5			ormula = 1+(
4-BED 3.4 p/p/u	IND	35,000 L/Ha/day	MOE Chart			population in					Project No	.:	CCO-22-35	01	·													-				
				5	Refer to FL	UNCTIONAL :	SERVICING A	ND STOWM	WATER MAN	NAGEMENT																		Sheet No:				
					REPORT b	y DSEL																						1 of 1				

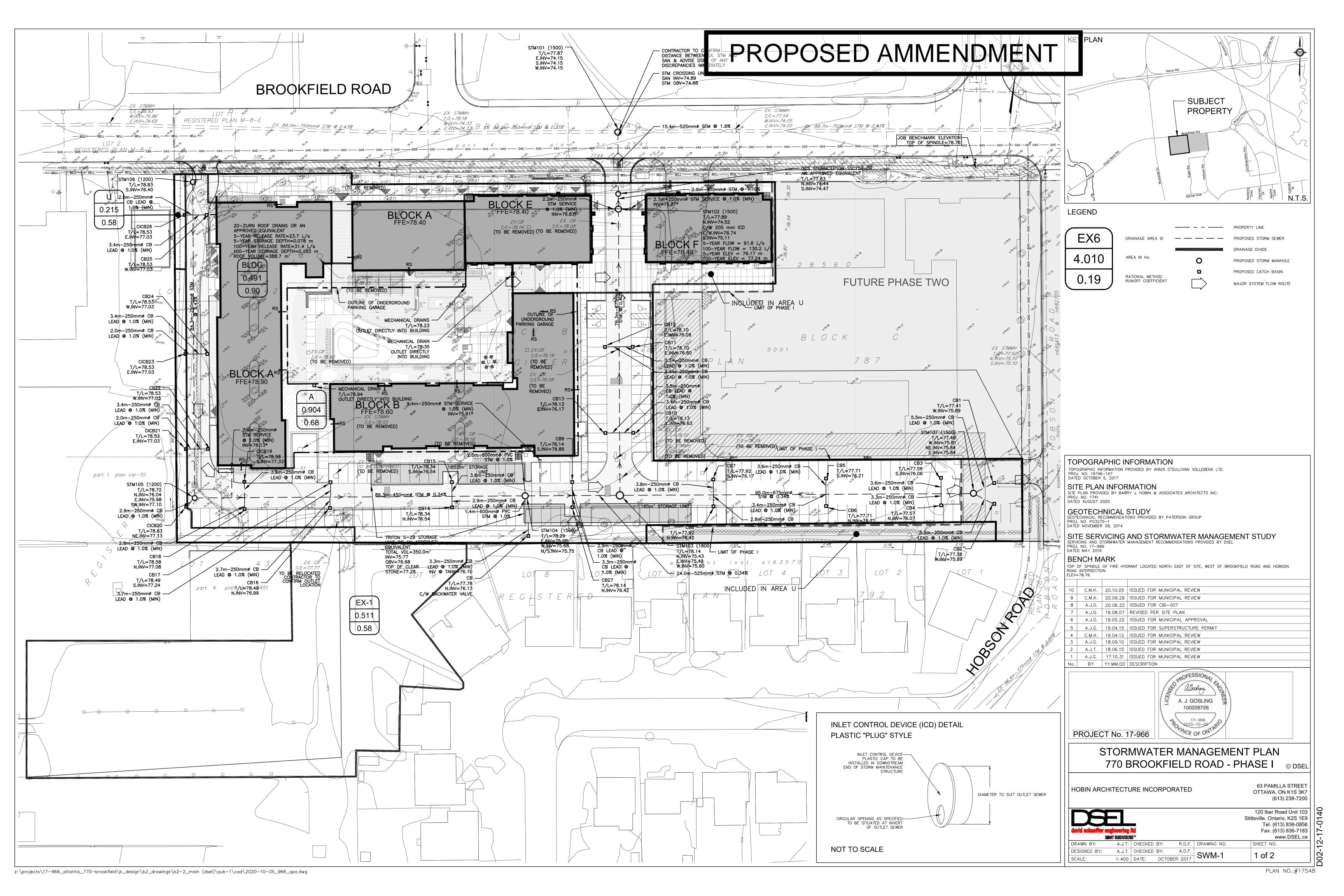
APPENDIX E PRE-DEVELOPMENT DRAINAGE PLAN



APPENDIX F POST-DEVELOPMENT DRAINAGE PLAN



<u>___</u>__



APPENDIX G STORMWATER MANAGEMENT CALCULATIONS

CCO-22-3501 - 770 Brookfield Phase 2 - Runoff Calculations

1 of 9

Pre-Development Runoff Coefficient

Drainage Area	Area (ha)	Impervious Area (m²)	С	Gravel Area (m²)	С	Pervious Area (m²)	С	C _{AVG} 2/5-Year	C _{AVG} 100-Year	
PH2 - A1	0.913	871.73	0.90	0.00	0.60	8,257.57	0.20	0.27	0.32	l

Pre-Development Runoff Calculations

Drainage Area	Area (ha)	C 5-Year	C 100-Year	Tc (min)	l (mm/hr)			Q (L/s)		
Area (na) s	5-Teal	100-Teal	o-real (IIIII)	2-Year	5-Year	100-Year	2-Year	5-Year	100-Year	
PH2 - A1	0.913	0.27	0.32	17	57.8	78.2	133.6	39.2	52.93	109.03
Total	0.913							39.16	52.93	109.03

Post-Development Runoff Coefficient

Drainage Area	Area (ha)	Impervious Area (m²)	С	Gravel Area (m²)	С	Pervious Area (m²)	С	C _{AVG} 2/5-Year	C _{AVG} 100-Year	
C1	0.159	1,587.44	0.90	0.00	0.60	0.00	0.20	0.90	1.00	Phase II Building D
C2	0.225	2,254.37	0.90	0.00	0.60	0.00	0.20	0.90	1.00	Phase II Building C
C3	0.210	854.42	0.90	0.00	0.60	1,249.33	0.20	0.48	0.55	Phase II Controlled Cistern Drainage
C4	0.092	399.51	0.90	0.00	0.60	524.65	0.20	0.50	0.57	Phase II Attenuated Surface Drainage
А	0.904	6,230.00	0.90	0.00	0.60	2,810.00	0.20	0.68	0.77	Phase I Attenuated Surface Drainage
EX-1	0.511	2,780.00	0.90	0.00	0.60	2,330.00	0.20	0.58	0.66	External Drainage Area
BLDG	0.491	4,910.00	0.90	0.00	0.60	0.00	0.20	0.90	1.00	Phase I Roof Area
U	0.215	980.00	0.90	0.00	0.60	1,170.00	0.20	0.52	0.59	Phase I Unattenuated Area
C5	0.028	283.48	0.90	0.00	0.60	0.00	0.20	0.90	1.00	Unattenuated North of Building C
C6	0.197	1,358.27	0.90	0.00	0.60	614.73	0.20	0.68	0.77	Unattenuated Hobson Road

Post-Development Runoff Calculations

Drainage	Area	C 2/E Voor	C 100-Year	Tc (min)		l (mm/hr)			Q (L/s)		
Area	(ha)	2/5-Year	100-Year	(min)	2-Year	5-Year	100-Year	2-Year	5-Year	100-Year	
C1	0.159	0.90	1.00	10	76.8	104.2	178.6	30.51	41.38	78.80	Phase II Building D
C2	0.225	0.90	1.00	10	76.8	104.2	178.6	43.32	58.77	111.91	Phase II Building C
C3	0.210	0.48	0.55	10	76.8	104.2	178.6	21.75	29.51	57.92	Phase II Controlled
C4	0.092	0.50	0.57	10	76.8	104.2	178.6	9.92	13.45	26.34	Phase II Attenuated Drainage
Α	0.904	0.68	0.77	10	76.8	104.2	178.6	131.72	178.69	344.13	Phase I Attenuated Drainage
EX-1	0.511	0.58	0.66	10	76.8	104.2	178.6	63.37	85.97	166.91	External Drainage
BLDG	0.491	0.90	1.00	10	76.8	104.2	178.6	94.35	128.00	243.73	Phase I Roof Area
U	0.215	0.52	0.59	10	76.8	104.2	178.6	23.83	32.33	63.17	Phase I Unattenuated
C5	0.028	0.90	1.00	10	76.8	104.2	178.6	5.45	7.39	14.07	Unattenuated North Building C
C6	0.197	0.68	0.77	10	76.8	104.2	178.6	28.73	38.97	75.05	Unattenuated Hobson Road
Total	3.034							452.95	614.46	1,182.02	

Required Restricted Flow 2 of 9

Drainage Area	Area (ha)	C 2-Year	Tc (min)	l (mm/hr)			Q (L/s)		
Alea	(114)	2-1641	(111111)	2-Year	5-Year	100-Year	2-Year	5-Year	100-Year
Ultimate Site*	2.523	0.50	16.80	57.8	78.2	133.6	202.77	N/A	N/A
EX-1	0.511	0.58	16.80	57.8	78.2	133.6	47.64	64.40	110.06
Total	3.034					**Total	250.41	267.17	312.84

^{*}Note: *Ultimate Site* drainage area comprised of Phase I, EX1 (per reports by others) and Phase II development area.

^{**}Note: Area EX-1 to be controlled to existing conditions for 2, 5 and 100-year events.

Drainage Area		cted Flow /s)	Restricted Flow (L/s)		Ŭ	Required n³)	J	Provided n³)	
Alea	5-Year	100-Year	5-Year	100-Year	5-Year	100-Year	5-Year	100-Year	
C1	41.38	78.80	2.52	4.62	38.46	73.15	41.96	76.93	Phase II Building D
C4	13.45	26.34							Phase II Attenuated
Α	178.69	344.13			135.01	346.33	350.00	350.00	Phase I Attenuated
EX-1	85.97	166.91	98.87	115.56	133.01	340.33	330.00	330.00	External Drainage
EV-1	03.97	100.91	70.07	113.30				Area	
BLDG	128.00	243.73			76.50	170.60	388.70	388.70	Phase I Roof Area
C2	58.77	111.91	5.46	9.36	47.41	92.42	55.70	95.48	Phase II Building C
C3	29.51	57.92	15.84	31.01	8.24	16.24	16.24	16.24	Phase II Controlled Cistern Drainage
U	32.33	63.17	32.33	63.17					Phase I Unattenuated Area
									Unattenuated North
C5	7.39	14.07	7.39	14.07					of Building C
C6	38.97	75.05	38.97	75.05					Unattenuated Hobson Road
Total	614.46	1,182.02	201.38	312.84	305.62	698.74	852.59	927.35	

CCO-22-3501 - 770 Brookfield Phase 2 - Runoff Calculations

Storage Requirements for Area C1

5-Year Storm Event

Storage Runoff to Runoff Allowable Required (L/s) be Stored Outflow (min) (mm/hr) (L/s) (m³)(L/s)53.9 18.89 34.00 30 21.41 2.52 40 44.2 17.56 2.52 15.04 36.08 50 37.7 14.97 2.52 12.45 37.36 60 32.9 13.07 2.52 10.55 37.97 70 29.4 11.68 2.52 9.16 38.46

Maximum Storage Required 5-year = 38 m³

100-Year Storm Event

Tc (min)	l (mm/hr)	Runoff (L/s) C1	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
30	91.9	40.56	4.62	35.94	64.68
40	75.1	33.14	4.62	28.52	68.45
50	64.0	28.24	4.62	23.62	70.87
60	55.9	24.67	4.62	20.05	72.18
70	49.8	21.98	4.62	17.36	72.90
80	45.0	19.86	4.62	15.24	73.15
90	41.1	18.14	4.62	13.52	73.00
100	37.9	16.73	4.62	12.11	72.63
110	35.2	15.53	4.62	10.91	72.03
120	32.9	14.52	4.62	9.90	71.27

Maximum Storage Required 100-year = 73 m³

5-Year Storm Event Storage Summary

Roof Storage									
Location	Area*	Depth	Volume (m³)						
Roof	1398.81	0.030	41.96						

Storage Available (m³) = 41.96 Storage Required (m³) = 38.46 3 of 9

100-Year Storm Event Storage Summary

Roof Storage									
Location	Area*	Depth	Volume (m³)						
Roof	1398.81	0.055	76.93						

Storage Available (m^3) = 76.93 Storage Required (m^3) = 73.15

^{*}Area is 75% of the total roof area

CCO-22-3501 - 770 Brookfield Phase 2 - Runoff Calculations

4 of 9

Roof Drain Flow (C1)

Roof Drains Summary					
Type of Control Device	Watts Drainage - Accutrol Weir				
Number of Roof Drains	7				
	5-Year 100-Yea				
Rooftop Storage (m³)	41.96	76.93			
Storage Depth (m)	0.030	0.055			
Flow (Per Roof Drain) (L/s)	0.36	0.66			
Total Flow (L/s)	2.52 4.62				

Flow Rate Vs. Build-Up (One Weir)				
Depth (mm)	Flow (L/s)			
15	0.18			
20	0.24			
25	0.30			
30	0.36			
35	0.42			
40	0.48			
45	0.54			
50	0.60			
55	0.66			

^{*}Roof Drain model to be Accutrol Weirs, See attached sheets

CALCULATING ROOF FLOW EXAMPLES

1 roof drain during a 5 year storm elevation of water = 25mm Flow leaving 1 roof drain = (1 x 0.30 L/s) = 0.30 L/s

1 roof drain during a 100 year storm elevation of water = 50mm Flow leaving 1 roof drain = (1 x 0.60 L/s) = 0.60 L/s

4 roof drains during a 5 year storm elevation of water = 25mm Flow leaving 4 roof drains = (4 x 0.30 L/s) = 1.20 L/s

4 roof drains during a 100 year storm elevation of water = 50mm Flow leaving 4 roof drains = (4 x 0.60 L/s) = 2.40 L/s

Roof Drain Flow						
Flow (I/s)	Storage Depth (mm)	Drains Flow (I/s)				
0.18	15	1.26				
0.24	20	1.68				
0.30	25	2.10				
0.36	30	2.52				
0.42	35	2.94				
0.48	40	3.36				
0.54	45	3.78				
0.60	50	4.20				
0.66	55	4.62				
0.72	60	5.04				
0.78	65	5.46				
0.84	70	5.88				
0.90	75	6.30				
0.96	80	6.72				
1.02	85	7.14				
1.08	90	7.56				
1.14	95	7.98				
1.20	100	8.40				
1.26	105	8.82				
1.32	110	9.24				
1.38	115	9.66				
1.44	120	10.08				
1.50	125	10.50				
1.56	130	10.92				
1.62	135	11.34				
1.68	140	11.76				
1.74	145	12.18				
1.80	150	12.60				

<u>Note:</u> The flow leaving through a restricted roof drain is based on flow vs. head information

^{*}Roof Drain Flow information taken from Watts Drainage website

45.81

CCO-22-3501 - 770 Brookfield Phase 2 - Runoff Calculations

Storage Requirements for Area C2

26.6

5-Year Storm Event

Storage Runoff to Runoff Allowable Required (L/s) be Stored Outflow (min) (mm/hr) (L/s) (m³)(L/s)40 44.2 24.93 19.47 46.73 5.46 50 37.7 21.26 5.46 15.80 47.41 60 32.9 18.56 5.46 13.10 47.15 70 29.4 16.58 5.46 11.12 46.72

Maximum Storage Required 5-year = $47 m^3$

5.46

9.54

15.00

100-Year Storm Event

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Tc (min)	l (mm/hr)	Runoff (L/s) C2	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
30	91.9	57.59	9.36	48.23	86.82
40	75.1	47.07	9.36	37.71	90.49
50	64.0	40.11	9.36	30.75	92.25
60	55.9	35.03	9.36	25.67	92.42
70	49.8	31.21	9.36	21.85	91.77
80	45.0	28.20	9.36	18.84	90.44
90	41.1	25.76	9.36	16.40	88.55
100	37.9	23.75	9.36	14.39	86.35
110	35.2	22.06	9.36	12.70	83.82
120	32.9	20.62	9.36	11.26	81.06

Maximum Storage Required 100-year = 92 m³

5-Year Storm Event Storage Summary

Roof Storage					
Location	Area*	Depth	Volume (m³)		
Roof	1591.34	0.035	55.70		

Storage Available (m³) = 55.70 Storage Required (m³) = 47.41 5 of 9

100-Year Storm Event Storage Summary

Roof Storage					
Location	Area*	Depth	Volume (m³)		
Roof	1591.34	0.060	95.48		

Storage Available (m³) = 95.48 Storage Required (m³) = 92.42

^{*}Area is 75% of the total roof area

CCO-22-3501 - 770 Brookfield Phase 2 - Runoff Calculations

Roof Drain Flow (C2)

Roof Drains Summary						
Type of Control Device Watts Drainage - Accutrol Weir						
Number of Roof Drains	13					
	5-Year	100-Year				
Rooftop Storage (m ³)	55.70	95.48				
Storage Depth (m)	0.035	0.060				
Flow (Per Roof Drain) (L/s)	0.42	0.72				
Total Flow (L/s)	5.46	9.36				

Flow Rate Vs. Build-Up (One Weir)				
Depth (mm)	Flow (L/s)			
15	0.18			
20	0.24			
25	0.30			
30	0.36			
35	0.42			
40	0.48			
45	0.54			
50	0.60			
55	0.66			

^{*}Roof Drain model to be Accutrol Weirs, See attached sheets

CALCULATING ROOF FLOW EXAMPLES

1 roof drain during a 5 year storm elevation of water = 25mm Flow leaving 1 roof drain = (1 x 0.30 L/s) = 0.30 L/s

1 roof drain during a 100 year storm elevation of water = 50mm Flow leaving 1 roof drain = (1 x 0.60 L/s) = 0.60 L/s

4 roof drains during a 5 year storm elevation of water = 25mm Flow leaving 4 roof drains = (4 x 0.30 L/s) = 1.20 L/s

4 roof drains during a 100 year storm elevation of water = 50mm Flow leaving 4 roof drains = (4 x 0.60 L/s) = 2.40 L/s

	Roof Drain Flow						
Flow (I/s)	Storage Depth (mm)	Drains Flow (I/s)					
0.18	15	2.34					
0.24	20	3.12					
0.30	25	3.90					
0.36	30	4.68					
0.42	35	5.46					
0.48	40	6.24					
0.54	45	7.02					
0.60	50	7.80					
0.66	55	8.58					
0.72	60	9.36					
0.78	65	10.14					
0.84	70	10.92					
0.90	75	11.70					
0.96	80	12.48					
1.02	85	13.26					
1.08	90	14.04					
1.14	95	14.82					
1.20	100	15.60					
1.26	105	16.38					
1.32	110	17.16					
1.38	115	17.94					
1.44	120	18.72					
1.50	125	19.50					
1.56	130	20.28					
1.62	135	21.06					
1.68	140	21.84					
1.74	145	22.62					
1.80	150	23.40					

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Note: The flow leaving through a restricted roof drain is based on flow vs. head information

^{*}Roof Drain Flow information taken from Watts Drainage website

CCO-22-3501 - 770 Brookfield Phase 2 - Runoff Calculations

Storage Requirements for C1, C5, & Phase I Attenuated Areas

5-Year Storm Event

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Tc (min)	l (mm/hr)	Runoff (L/s) C4	Runoff (L/s) A	Runoff (L/s) BLDG	Runoff (L/s) EX-1	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
10	104.2	13.46	178.70	23.73	85.98	98.87	202.99	121.80
15	83.6	10.79	143.37	23.73	68.98	98.87	148.01	133.21
20	70.3	9.08	120.56	23.73	58.00	98.87	112.51	135.01
25	60.9	7.86	104.44	23.73	50.25	98.87	87.42	131.12
30	53.9	6.96	92.44	23.73	44.47	98.87	68.73	123.72

Maximum Storage Required 5-year = 135 m³

100-Year Storm Event

Tc (min)	l (mm/hr)	Runoff (L/s)	Runoff (L/s)	Runoff (L/s)	Runoff (L/s)	Allowable Outflow	Runoff to be Stored	Storage Required
()	(!!!!!/	C4	A	BLDG	EX-1	(L/s)	(L/s)	(m³)
10	178.6	26.35	344.20	31.39	166.95	115.56	453.33	272.00
15	142.9	21.08	275.40	31.39	133.58	115.56	345.89	311.30
20	120.0	17.70	231.27	31.39	112.17	115.56	276.97	332.37
25	103.8	15.31	200.05	31.39	97.03	115.56	228.22	342.33
30	91.9	13.56	177.11	31.39	85.91	115.56	192.41	346.33
35	82.6	12.19	159.19	31.39	77.21	115.56	164.42	345.28
40	75.1	11.08	144.74	31.39	70.20	115.56	141.85	340.43
45	69.1	10.19	133.17	31.39	64.59	115.56	123.79	334.23
50	64.0	9.44	123.34	31.39	59.83	115.56	108.44	325.32
55	59.6	8.79	114.86	31.39	55.71	115.56	95.20	314.15

Maximum Storage Required 100-year = 346.33 m³

Tank Storage

raint otorage			
	Storage Available (m³) =	350.00	
	Storage Required (m³) =	346.33	

CCO-22-3501 - 770 Brookfield Phase 2 - Runoff Calculations

For Orifice Flow, C= 0.60
For Weir Flow, C= 1.84

 Orifice 1
 Orifice 2
 Weir 1
 Weir 2

 invert elevation center of crest elevation orifice width / weir length weir height orifice area (m²)
 74.63
 X
 X
 X

 X
 X
 X
 X
 X
 X

 X
 X
 X
 X
 X

 X
 X
 X
 X
 X

Elevation Discharge Table - Storm Routing

				Elevatio	on Discharge	Table - Storm	Routing				
772	Elevation	Orit	fice 1	Orif	ice 2	We	Weir 1 Weir 2		Total	Incremental Tank Volume	
772		H [m]	O [m ³ /s]	H [m]	O [m ³ /s]	H [m]	O [m ³ /s]	H [m]	O [m ³ /s]	Q [L/s]	V [m³]
1.16	75.77	1.14		Х		Х		Х		86.21	
80	75.78			Х	Х	Х	Х	Х	Х	86.58	
118	75.79										
1.19	75.80										
120	75.81										
121	75.82										
122	75.84										
1.23	75.85										
1.24	75.86										
1.25	75.87										
	75.88										
1 128	75.89	1.26	0.09	Х	Х	Х	Х	Х	Х	90.62	46
129	75.90	1.27	0.09	Х	Х	Х	Х	Х	Х	90.98	50
1.30	75.91										
1.31	75.92										
1.32	75.93										
133	75.94										
1,34	75.95										
1.35	75.96										
1.36	75.97 75.98										
1.37	75.98 75.99										
138	76.00										
1.39	76.00										
1.40	76.02										
1.41	76.03										
1.43	76.04	1.41									104
1.44	76.05	1.42	0.10	Х	Х	Х	Х	Х	Х	96.20	108
1.45	76.06		0.10	Х	Х	Х	Х	Х	Х	96.53	112
1.46	76.07					Х	Х	Х			
1.47	76.08										
.11 1.48 0.10 x x x x x x y	76.09										
.12 1.49 0.10 x	76.10										
.13 1.50 0.10 x x x x x x x y 98.87 138 .14 1.51 0.10 x x x x x x y 99.20 142 .15 1.52 0.10 x x x x x x x y 99.85 146 .16 1.53 0.10 x x x x x x x y 99.85 150 .17 1.54 0.10 x<	76.11										
.14 1.51 0.10 x	76.12										
.15 1.52 0.10 x x x x x x y9.52 146 .16 1.53 0.10 x											
.16 1.53 0.10 x	76.14										
.17 1.54 0.10 x	76.16										
.18 1.55 0.10 x	76.17										
.19 1.56 0.10 x	76.18										
1.20 1.57 0.10 x	76.19										
.21 1.58 0.10 x	76.20										
1.22 1.59 0.10 x	76.21										
1.23 1.60 0.10 x	76.22										
.24 1.61 0.10 x	76.23										
.25 1.62 0.10 x	76.24										
.26 1.63 0.10 x	76.25										
.27 1.64 0.10 x	76.26										
1.28 1.65 0.10 x x x x x x x x 196 1.29 1.66 0.10 x x x x x x x 104.00 200 3.30 1.67 0.10 x x x x x x x 104.31 204 3.31 1.68 0.10 x x x x x x x x x 104.62 208 3.32 1.69 0.10 x x x x x x x x x x 104.93 212 3.33 1.70 0.11 x x x x x x x x 105.94 215 3.34 1.71 0.11 x x x x x x x x x 105.55 219 3.35 1.72 0.11 x x x x x x x x x x x x 105.86 223 3.36 1.73 0.11 x x x x x x x	76.27										
.29 1.66 0.10 x x x x x x x x 104.00 200 .30 1.67 0.10 x x x x x x x x 104.31 204 .31 1.68 0.10 x x x x x x x x 104.62 208 .32 1.69 0.10 x x x x x x x x 104.93 212 .33 1.70 0.11 x x x x x x x x x 105.24 215 .34 1.71 0.11 x x x x x x x x x x 105.55 219 .35 1.72 0.11 x x x x x x x x x x x x x x 105.55 219 .35 1.72 0.11 x x x x x x x x x x x x x x x x x x	76.28										
.30 1.67 0.10 x	76.29										
.31 1.68 0.10 x	76.30										
.32 1.69 0.10 x x x x x x 104.93 212 .33 1.70 0.11 x x x x x x x 105.24 215 .34 1.71 0.11 x x x x x x 105.55 219 .35 1.72 0.11 x x x x x x x 105.86 223 .36 1.73 0.11 x x x x x x x 106.17 227 .37 1.74 0.11 x x x x x x x x 106.47 231 .38 1.75 0.11 x x x x x x x x 107.08 235 .39 1.76 0.11 x x x x x x x x x x x 107.08 238 .40 1.77 0.11 x x x x x x x x x x x x x x x x	76.31										
.33 1.70 0.11 x x x x x x x x 105.24 215 .34 1.71 0.11 x x x x x x x x x 105.55 219 .35 1.72 0.11 x x x x x x x x x 105.86 223 .36 1.73 0.11 x x x x x x x x x 106.17 227 .37 1.74 0.11 x x x x x x x x x x 106.47 231 .38 1.75 0.11 x x x x x x x x x 106.78 235 .39 1.76 0.11 x x x x x x x x x 107.08 238 .40 1.77 0.11 x x x x x x x x x x 107.09 242	76.32										
.34 1.71 0.11 x x x x x x 105.55 219 .35 1.72 0.11 x x x x x x x 105.86 223 .36 1.73 0.11 x x x x x x x 106.17 227 .37 1.74 0.11 x x x x x x 106.47 231 .38 1.75 0.11 x x x x x x x 106.78 235 .39 1.76 0.11 x x x x x x x x 107.08 238 .40 1.77 0.11 x x x x x x x 107.39 242	76.33						,		,		
.35 1.72 0.11 x x x x x x x 105.86 223 .36 1.73 0.11 x x x x x x 106.17 227 .37 1.74 0.11 x x x x x x 106.47 231 .38 1.75 0.11 x x x x x x x 106.78 235 .39 1.76 0.11 x x x x x x x 107.08 238 .40 1.77 0.11 x x x x x x x 107.39 242	76.34										
.36 1.73 0.11 x x x x x x 106.17 227 .37 1.74 0.11 x x x x x x x 106.47 231 .38 1.75 0.11 x x x x x x x 106.78 235 .39 1.76 0.11 x x x x x x x x 107.08 238 .40 1.77 0.11 x x x x x x x x 107.39 242	76.35										
.37 1.74 0.11 x x x x x x 106.47 231 .38 1.75 0.11 x x x x x x x 106.78 235 .39 1.76 0.11 x x x x x x x 107.08 238 .40 1.77 0.11 x x x x x x x 107.39 242	76.36										
.38 1.75 0.11 x x x x x x 106.78 235 .39 1.76 0.11 x x x x x x x 107.08 238 .40 1.77 0.11 x x x x x x x 107.39 242	76.37										
.39	76.38										
.40 1.77 0.11 x x x x x x 107.39 242	76.39										
	76.40										
.41 1.78 U.II X X X X X X X 107.69 246	76.41	1.78	0.11	Х	X	X	X	X	X	107.69	246
	76.42										

76.43	1.80	0.11	Х	Х	Х	Х	Х	Х	108.29	254
76.44	1.81	0.11	Х	Х	Х	Х	Х	Х	108.59	258
76.45	1.82	0.11	Х	Х	Х	Х	Х	Х	108.89	262
76.46	1.83	0.11	Х	Х	Х	Х	Х	Х	109.19	265
76.47	1.84	0.11	Х	Х	Х	Х	Х	х	109.49	269
76.48	1.85	0.11	Х	Х	Х	Х	Х	Х	109.79	273
76.49	1.86	0.11	Х	Х	Х	Х	Х	Х	110.08	277
76.50	1.87	0.11	Х	Х	Х	Х	Х	Х	110.38	281
76.51	1.88	0.11	Х	Х	Х	Х	Х	Х	110.67	285
76.52	1.89	0.11	Х	Х	Х	Х	Х	х	110.96	288
76.53	1.90	0.11	Х	Х	Х	Х	Х	х	111.26	292
76.54	1.91	0.11	Х	Х	Х	Х	Х	х	111.55	296
76.55	1.92	0.11	Х	Х	Х	Х	Х	х	111.84	300
76.56	1.93	0.11	Х	Х	Х	Х	Х	Х	112.13	304
76.57	1.94	0.11	Х	Х	Х	Х	Х	х	112.42	308
76.58	1.95	0.11	Х	Х	Х	Х	Х	х	112.71	312
76.59	1.96	0.11	Х	Х	Х	Х	Х	х	113.00	315
76.60	1.97	0.11	Х	Х	Х	Х	Х	х	113.29	319
76.61	1.98	0.11	Х	Х	Х	Х	Х	Х	113.57	323
76.62	1.99	0.11	х	Х	х	х	х	х	113.86	327
76.63	2.00	0.11	х	Х	х	х	х	х	114.15	331
76.64	2.01	0.11	Х	Х	Х	Х	Х	х	114.43	335
76.65	2.02	0.11	Х	Х	Х	Х	х	Х	114.71	338
76.66	2.03	0.11	Х	Х	Х	Х	Х	Х	115.00	342
76.67	2.04	0.12	Х	Х	Х	Х	Х	Х	115.28	346
76.68	2.05	0.12	Х	Х	Х	Х	Х	Х	115.56	350

Notes: 1. For Orifice Flow, User is to Input an Elevation Higher than Crown of Orifice. 2. Orifice Equation: $Q = cA(2gh)^{1/2}$

- 3. Weir Equation: Q = CLH^{3/2}
- 4. These Computations Do Not Account for Submergence Effects Within the Pond Riser.
- 5. H for orifice equations is depth of water above the centroide of the orifice.
- 6. H for weir equations is depth of water above the weir crest.

CCO-22-3501 - 770 Brookfield Phase 2 - Runoff Calculations

Storage Requirements for Area C3

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5-Year Storm Event

Tc (min)	l (mm/hr)	Runoff (L/s) C3	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
7	123.3	34.92	15.84	19.08	8.01
8	116.1	32.88	15.84	17.04	8.18
9	109.8	31.10	15.84	15.26	8.24
10	104.2	29.51	15.84	13.67	8.20
11	99.2	28.10	15.84	12.26	8.09

Maximum Storage Required 5-year =

 m^3

100-Year Storm Event

Tc (min)	l (mm/hr)	Runoff (L/s) C3	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
5	242.7	78.72	31.01	47.71	14.31
6	226.0	73.30	31.01	42.29	15.23
7	211.7	68.67	31.01	37.66	15.82
8	199.2	64.61	31.01	33.60	16.13
9	188.3	61.08	31.01	30.07	16.24
10	178.6	57.93	31.01	26.92	16.15
11	169.9	55.11	31.01	24.10	15.90
12	162.1	52.58	31.01	21.57	15.53
13	155.1	50.31	31.01	19.30	15.05
14	148.7	48.23	31.01	17.22	14.47

Maximum Storage Required 100-year = 16.24

Cistern Storage

Storage Available (m³) =	16.24	
Storage Required (m³) =	16.24	

STORM SEWER DESIGN SHEET

PROJECT:

CCO-22-3501

LOCATION: Phase 2 - 770 Brookfield CLIENT: Hobin Architecture

Refer to DSEL FUNCTIONAL SERVICING AND STORMWATER MANAGMEENT REPORT PROJECT NO. 17-966 FOR FULL PHASE 1 SEWER CALCULATIONS

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	LOCATION				CONTRIBUTING AREA (ha))		RATIONAL DESIGN FLOW					IONAL DESIGN	SEWER DATA													
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28
STREET	AREA ID	FROM	TO	C-VALUE	AREA	INDIV	CUMUL	INLET	TIME	TOTAL	i (5)	i (10)	i (100)	5yr PEAK		100yr PEAK	FIXED	DESIGN	CAPACITY	LENGTH		PIPE SIZE (mm	1)	SLOPE	VELOCITY	AVAIL 0	AP (5yr)
SIKLLI	AKLATO	MH	MH	C-VALUE	ANLA	AC	AC	(min)	IN PIPE	(min)	(mm/hr)	(mm/hr)	(mm/hr)	FLOW (L/s)	(L/s)	(m)	DIA	W	Н	(%)	(m/s)	(L/s)	(%)				
	PH1-B4		-					1	-						-												
	PH2 - C4	STM107	STM103	0.50	0.09	0.05	0.05	10.00	1.14	11.14	104.19	122.14	178.56	13.45				13.45	511.34	95.00	675			0.34	1.384	497.88	97.37%
	F112 - C4			0.50	0.07	0.03	0.03	10.00	1.14	11.14	104.17	122.14	170.30	13.43				13.43	311.34	73.00	0/3			0.34	1.304	477.00	77.3770
	PH1-BLDG A			0.90	0.21	0.19																					
	PH1-BLDG A	+		0.90	0.16	0.14		1									-										$\overline{}$
	PH1-B1			0.78	0.07	0.06	+						-	+			-					+					
	PH1-B2			0.70	0.18	0.12								1													
	PH1-B3	STM104	STM103	0.60	0.13	0.08							1	1	1	1											
	PH1-B6	1		0.04	0.20	0.01																					i l
	PH1-COURT	1		0.52	0.21	0.11																					
	EX-1			0.51	0.58	0.30	1.00	13.20	0.34	13.54	89.86	105.27	153.78	36.61				36.61	261.61	24.00	525			0.34	1.171	225.00	86.00%
	PH1-B5	STM103	STM102	0.86	0.10	0.08								.													
	PH2-C1			0.90	0.16	0.14	1.27	13.54	0.84	14.38	88.59	103.77	151.58	47.87				47.87	561.51	76.20	675			0.41	1.520	513.64	91.47%
	PH1-BLDG-E1			0.90	0.06	0.06		0.00	0.02	0.02	230.48	271.61	398.62	0.00				0.00	840.09	2.90	600			1.72	2.878		
	PH1-BLDG-E2	STM102	OGS	0.90	0.06	0.06	1.39	14.38	0.02	14.39	85.63	100.28	146.46	55.36				55.36	840.09	2.90	600			1.72	2.878	784.73	93.41%
		OGS	STM101	-	-	-	1.39	14.39	0.11	14.50	85.57	100.22	146.36	55.42				55.42	542.11	15.40	525			1.46	2.426	486.69	89.78%
Definitions:				Notes:				Designed:		RR			No.		1			Revision							Date		
Q = 2.78CiA, where:				Mannings coefficient (n)	_		0.013	besigned.		KK			1 1					ED FOR REVIE	E/M/						2022-06-24		
Q = Peak Flow in Litres p	or Second (L/s)			1. Marinings Coemicient (11)	=		0.013						1.	1				ED FOR REVIE							2022-00-24		
A = Area in Hectares (ha)								Checked:		CH			3	†				ED FOR REVIE							2022-11-04		
i = Rainfall intensity in n		n/hr)						CHECKEU.		CIT			4	+				ED FOR REVIE							2022-11-24		
[i = 998.071 / (TC+6.05		5 YEAR															13301	ED TOR REVIE							2020 01 20		
[i = 1174.184 / (TC+6.0	014)^0.816]	10 YEAR						Project No.:		CCO-22-3501				İ													
[i = 1735.688 / (TC+6.0	014)^0.820]	100 YEAR															Date								Sheet No:		
																	2023-01	1-19							1 of 1		



Adjustable Accutrol Weir

Adjustable Flow Control for Roof Drains

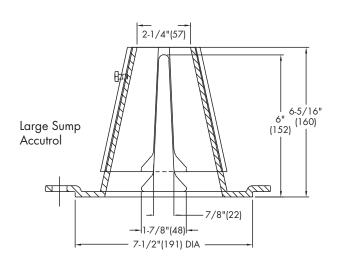
ADJUSTABLE ACCUTROL (for Large Sump Roof Drains only)

For more flexibility in controlling flow with heads deeper than 2", Watts Drainage offers the Adjustable Accutrol. The Adjustable Accutrol Weir is designed with a single parabolic opening that can be covered to restrict flow above 2" of head to less than 5 gpm per inch, up to 6" of head. To adjust the flow rate for depths over 2" of head, set the slot in the adjustable upper cone according to the flow rate required. Refer to Table 1 below. Note: Flow rates are directly proportional to the amount of weir opening that is exposed.

EXAMPLE:

For example, if the adjustable upper cone is set to cover 1/2 of the weir opening, flow rates above 2"of head will be restricted to 2-1/2 gpm per inch of head.

Therefore, at 3" of head, the flow rate through the Accutrol Weir that has 1/2 the slot exposed will be: [5 gpm (per inch of head) \times 2 inches of head] + 2-1/2 gpm (for the third inch of head) = 12-1/2 gpm.



Upper Cone

Fixed Weir

Adjustable

1/2 Weir Opening Exposed Shown Above

TABLE 1. Adjustable Accutrol Flow Rate Settings

Weir Onenin -	1"	2"	3"	4"	5"	6"						
Weir Opening Exposed	Flow Rate (gallons per minute)											
Fully Exposed	5	10	15	20	25	30						
3/4	5	10	13.75	17.5	21.25	25						
1/2	5	10	12.5	15	17.5	20						
1/4	5	10	11.25	12.5	13.75	15						
Closed	5	5	5	5	5	5						

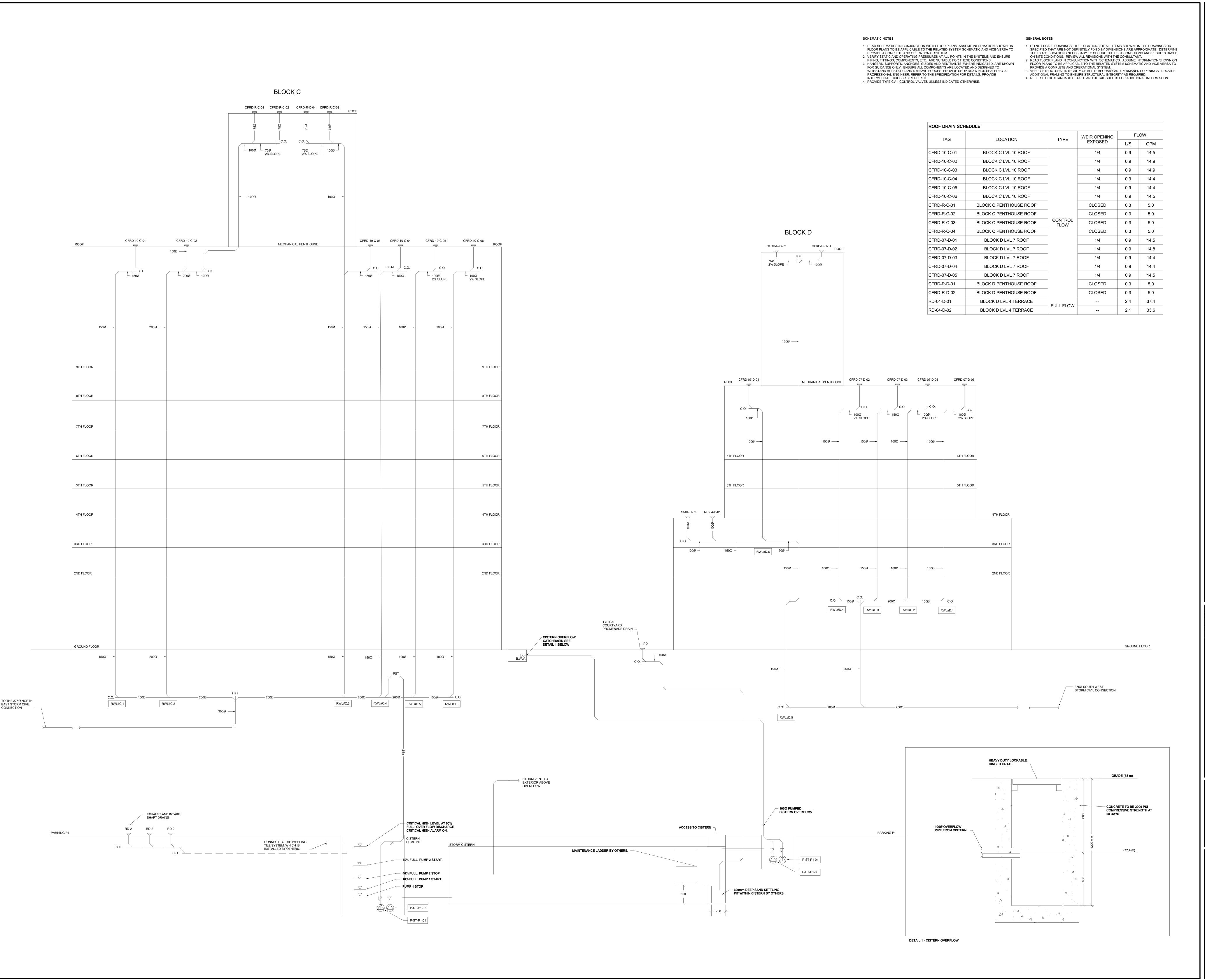
Job Name	Contractor
Job Location	Contractor's P.O. No.
Engineer	Representative

Watts product specifications in U.S. customary units and metric are approximate and are provided for reference only. For precise measurements, please contact Watts Technical Service. Watts reserves the right to change or modify product design, construction, specifications, or materials without prior notice and without incurring any obligation to make such changes and modifications on Watts products previously or subsequently sold.



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BROOKFIELD COURTYARD Building D

PARKING

9 ISSUED FOR TENDER 9 ISSUED FOR PRICING - SI M01 no. date revision

It is the responsibility of the appropriate contractor to check and verify all dimensions on site and report all errors and/ or omissions to the engineer. All contractors must comply with all

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RAWING TITLE STORM SCHEMATIC

> SCALE As indicated PROJECT DRAWING NO.

APPENDIX H
CITY OF OTTAWA DESIGN CHECKLIST

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City of Ottawa

4. Development Servicing Study Checklist

The following section describes the checklist of the required content of servicing studies. It is expected that the proponent will address each one of the following items for the study to be deemed complete and ready for review by City of Ottawa Infrastructure Approvals staff.

The level of required detail in the Servicing Study will increase depending on the type of application. For example, for Official Plan amendments and re-zoning applications, the main issues will be to determine the capacity requirements for the proposed change in land use and confirm this against the existing capacity constraint, and to define the solutions, phasing of works and the financing of works to address the capacity constraint. For subdivisions and site plans, the above will be required with additional detailed information supporting the servicing within the development boundary.

4.1 General Content

Criteria	Location (if applicable)
Executive Summary (for larger reports only).	N/A
Date and revision number of the report.	On Cover
 Location map and plan showing municipal address, boundary, and layout of proposed development. 	Appendix A
$\ \square$ Plan showing the site and location of all existing services.	Site Servicing Plan (C102)
Development statistics, land use, density, adherence to zoning and official plan, and reference to applicable subwatershed and watershed plans that provide context to which individual.	1.1 Purpose1.2 Site Description
watershed plans that provide context to which individual developments must adhere.	·
	6.0 Stormwater Management
 Summary of pre-consultation meetings with City and other approval agencies. 	Appendix B
 Reference and confirm conformance to higher level studies and reports (Master Servicing Studies, Environmental Assessments, 	1.1 Purpose
Community Design Plans), or in the case where it is not in conformance, the proponent must provide justification and	1.2 Site Description
develop a defendable design criteria.	6.0 Stormwater Management
\square Statement of objectives and servicing criteria.	3.0 Pre-Consultation Summary



☐ Identification of existing and proposed infrastructure available in the immediate area.	N/A
☐ Identification of Environmentally Significant Areas, watercourses and Municipal Drains potentially impacted by the proposed development (Reference can be made to the Natural Heritage Studies, if available).	Site Grading Plan (C101)
☐ Concept level master grading plan to confirm existing and proposed grades in the development. This is required to confirm the feasibility of proposed stormwater management and drainage, soil removal and fill constraints, and potential impacts to neighbouring properties. This is also required to confirm that the proposed grading will not impede existing major system flow paths.	Site Grading Plan (C101)
 Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts. 	N/A
☐ Proposed phasing of the development, if applicable.	N/A
Reference to geotechnical studies and recommendations concerning servicing.	Section 2.0 Background Studies, Standards and References
 All preliminary and formal site plan submissions should have the following information: Metric scale North arrow (including construction North) Key plan Name and contact information of applicant and property owner Property limits including bearings and dimensions Existing and proposed structures and parking areas Easements, road widening and rights-of-way Adjacent street names 	Site Grading Plan (C101)

4.2 Development Servicing Report: Water

Criteria	Location (if applicable)
☐ Confirm consistency with Master Servicing Study, if available	N/A
 Availability of public infrastructure to service proposed development 	N/A
☐ Identification of system constraints	N/A
☐ Identify boundary conditions	Appendix C
☐ Confirmation of adequate domestic supply and pressure	N/A
 Confirmation of adequate fire flow protection and confirmation that fire flow is calculated as per the Fire Underwriter's Survey. Output should show available fire flow at locations throughout the development. 	Appendix C
 Provide a check of high pressures. If pressure is found to be high, an assessment is required to confirm the application of pressure reducing valves. 	N/A
 Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defined phases of the project including the ultimate design 	N/A
☐ Address reliability requirements such as appropriate location of shut-off valves	N/A
☐ Check on the necessity of a pressure zone boundary modification.	N/A
Reference to water supply analysis to show that major infrastructure is capable of delivering sufficient water for the proposed land use. This includes data that shows that the expected demands under average day, peak hour and fire flow conditions provide water within the required pressure range	Appendix C, Section 4.2

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 Description of the proposed water distribution network, including locations of proposed connections to the existing system, provisions for necessary looping, and appurtenances (valves, pressure reducing valves, valve chambers, and fire hydrants) including special metering provisions. 	Site Servicing Plan (C101)
 Description of off-site required feedermains, booster pumping stations, and other water infrastructure that will be ultimately required to service proposed development, including financing, interim facilities, and timing of implementation. 	N/A
☐ Confirmation that water demands are calculated based on the City of Ottawa Design Guidelines.	Appendix C
 Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference. 	N/A

4.3 Development Servicing Report: Wastewater

Criteria	Location (if applicable)
☐ Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitored flow data from relatively new infrastructure cannot be used to justify capacity requirements for proposed infrastructure).	N/A
Confirm consistency with Master Servicing Study and/or justifications for deviations.	N/A
☐ Consideration of local conditions that may contribute to extraneous flows that are higher than the recommended flows in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers.	N/A
Description of existing sanitary sewer available for discharge of wastewater from proposed development.	Section 5.2 Proposed Sanitary Sewer

☐ Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable)	Section 5.3 Proposed Sanitary Design
☐ Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format.	N/A
 Description of proposed sewer network including sewers, pumping stations, and forcemains. 	Section 5.2 Proposed Sanitary Sewer
☐ Discussion of previously identified environmental constraints and impact on servicing (environmental constraints are related to limitations imposed on the development in order to preserve the physical condition of watercourses, vegetation, soil cover, as well as protecting against water quantity and quality).	N/A
 Pumping stations: impacts of proposed development on existing pumping stations or requirements for new pumping station to service development. 	N/A
☐ Forcemain capacity in terms of operational redundancy, surge pressure and maximum flow velocity.	N/A
☐ Identification and implementation of the emergency overflow from sanitary pumping stations in relation to the hydraulic grade line to protect against basement flooding.	N/A
☐ Special considerations such as contamination, corrosive environment etc.	N/A

4.4 Development Servicing Report: Stormwater Checklist

Criteria	Location (if applicable)
 Description of drainage outlets and downstream constraints including legality of outlets (i.e. municipal drain, right-of-way, watercourse, or private property) 	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
☐ Analysis of available capacity in existing public infrastructure.	N/A
 A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns, and proposed drainage pattern. 	Pre & Post-Development Plans
☐ Water quantity control objective (e.g. controlling post-development peak flows to pre-development level for storm events ranging from the 2 or 5-year event (dependent on the receiving sewer design) to 100-year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
☐ Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
 Description of the stormwater management concept with facility locations and descriptions with references and supporting information. 	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
Set-back from private sewage disposal systems.	N/A
☐ Watercourse and hazard lands setbacks.	N/A
Record of pre-consultation with the Ontario Ministry of Environment and the Conservation Authority that has jurisdiction on the affected watershed.	N/A
☐ Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists.	N/A
☐ Storage requirements (complete with calculations) and conveyance capacity for minor events (1:5-year return period) and major events (1:100-year return period).	Appendix G

☐ Identification of watercourses within the proposed development and how watercourses will be protected, or, if necessary, altered by the proposed development with applicable approvals.	Site Grading Plan
Calculate pre-and post development peak flow rates including a description of existing site conditions and proposed impervious areas and drainage catchments in comparison to existing conditions.	Section 7.0 Proposed Stormwater Management Appendix G
Any proposed diversion of drainage catchment areas from one outlet to another.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
 Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and stormwater management facilities. 	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
☐ If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post-development flows up to and including the 100-year return period storm event.	N/A
☐ Identification of potential impacts to receiving watercourses	N/A
Identification of municipal drains and related approval requirements.	N/A
 Descriptions of how the conveyance and storage capacity will be achieved for the development. 	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
100-year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading.	Site Grading Plan (C101)
☐ Inclusion of hydraulic analysis including hydraulic grade line elevations.	N/A

 Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors. 	Section 8.0 Sediment & Erosion Control
☐ Identification of floodplains – proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions.	N/A
 Identification of fill constraints related to floodplain and geotechnical investigation. 	N/A

4.5 Approval and Permit Requirements: Checklist

The Servicing Study shall provide a list of applicable permits and regulatory approvals necessary for the proposed development as well as the relevant issues affecting each approval. The approval and permitting shall include but not be limited to the following:

Criteria	Location (if applicable)
Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act.	N/A
 Application for Certificate of Approval (CofA) under the Ontario Water Resources Act. 	N/A
☐ Changes to Municipal Drains.	N/A
☐ Other permits (National Capital Commission, Parks Canada, Public Works and Government Services Canada, Ministry of Transportation etc.)	N/A

4.6 Conclusion Checklist

Criteria	Location (if applicable)
Clearly stated conclusions and recommendations	Section 9.0 Summary
	Section 10.0 Recommendations
☐ Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency.	All are stamped
☐ All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario	All are stamped