HYDROGEOLOGICAL ASSESSMENT AND TERRAIN ANALYSIS 273-275 RUSS BRADLEY ROAD, CARP, ONTARIO



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Prepared for:

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EXECUTIVE SUMMARY

McIntosh Perry ('MP') was retained by Trevor Watkins ('the Client') to conduct a Hydrogeological Assessment and Terrain Analysis in support of a proposed storage facility development for the property located at 273-275 Russ Bradley Road (previously known as 1500 Thomas Argue Road) in Carp, Ontario. It is our understanding that this hydrogeological assessment and terrain analysis is needed based on a requirement from the City of Ottawa as a condition for a privately serviced development, as part of the site plan application process.

Based on documentation provided, the Site is located immediately south of Russ Bradley Road and approximately 70 metres southwest from Carp Road. It is our understanding that the client is looking to develop a private storage facility, which includes twelve (12) self storage buildings, a small office area, and washroom facilities. The area in which this private storage facility will be placed is approximately 2.4 hectares (ha.) in size.

This report has been prepared using data collected from a drilled test well at 273-275 Russ Bradley Road (Test Well 1, TW1) by Mcintosh Perry staff on September 13, 2022. It is our understanding that this well (TW1) is the well that will be utilized to service the proposed development. Therefore, the hydrogeological data gathered during the pumping test and subsequent analyses are deemed to be wholly representative of hydrogeological conditions at the Site and future groundwater to be utilized by occupants.

Ground surface at the Site gently slopes throughout the Site towards the south. Site elevation ranges from approximately 111 – 114 metres above sea level (m asl). Surface drainage is interpreted to reflect surface topography and is likely controlled via areas of permeable ground surface. An unnamed creek runs along the south border of the Site, flowing southwest. Surface water and shallow groundwater in the vicinity of the Site likely flows toward this creek.

Test Well 1 was pumped for a duration of 420 minutes and was sampled twice during this time. The pumping rate changed throughout the pumping test in order to adequately reflect a stabilized quantity of water being pumped from the well. The pumping rate at the start of the test was 60 L/min, which was maintained for changed approximately 35 minutes, at which time the pumping rate was to 53.3 L/min for an additional 157 minutes. The pumping rate was changed again 192 minutes after the start of the test to 48 L/min – this rate was maintained for three minutes and was then changed as water levels were not stabilizing. The pumping rate was changed to 42 L/min 195 minutes after the start of the test and remained at that rate until the pump was shut off. The cumulative weighted average pumping rate was 47.8 L/min for the duration of the test, which is considered sufficient to supply future development of a private commercial development.

Water quality results indicate that the bedrock aquifer provides good quality water, which may be considered generally suitable for human consumption. All analytical results were compared to the Ontario Drinking Water Standards, Objectives, and Guidelines (ODWS). Based on the analytical results from TW1 on September 13, 2022, the following exceedances were noted:

- Hardness (OG: 100 mg/L): TW1-1 (271 mg/L) and TW1-2 (265 mg/L)
- Sulphide: (AO: 0.05 mg/L): TW1-1 (3.14 mg/L) and TW1-2 (3.36 mg/L)
- Turbidity: (AO: 5 NTU): TW1-1 (34.8 NTU)
- Aluminum: (AO: 0.1 mg/L): TW1-1 (0.68 mg/L) and TW1-2 (0.14 mg/L)
- Iron (AO: 0.3 mg/L): TW1-1 (0.82 mg/L); and
- The health warning limit for sodium (20 mg/L) was exceeded in sample TW1-1 (22.7 mg/L) and TW1-2 (24.1 mg/L)

All aforementioned exceedances are of an aesthetic or operational nature, are not health related, and can be readily treated if so desired.

On-site overburden in the area of the proposed severance is listed by the Ontario Geological Survey (OGS) as coarse-textured glaciomarine deposits of sand, gravel, minor silt and clay. This is supported by the MECP WWIS records, which indicate mainly sand, clay, and gravel overburden for wells listed within 500 m of the Site. On-site bedrock is generally characterized as limestone, dolostone, shale, arkose, and sandstone of the Simcoe Group of the Shadow Lake Formation (OGS, 2021), which is supported by a majority of well records in the area that list the bedrock as either "shale" or "limestone". The average depth to bedrock is approximately 34 m below ground surface (bgs) for listed wells within 500 m of the Site.

MECP Procedure D-5-4 (Technical Guideline for Individual On-Site Sewage Systems: Water Quality Impact Risk Assessment) outlines the provision for predictive assessment of attenuation. This predictive assessment utilizes a 3-step process where each "step" must be assessed if the previous "step" has not been met. In reference to this Site, Step 1 details whether lot size has sufficient spatial area for the natural attenuation of nitrate-nitrogen. This step has been met as the average lot size will be greater than 1.0 ha with no lot being less than 0.8 ha. Step 2 outlines system isolation consideration, which has additionally been met as there is sufficient spatial area on the retained lot. The thickness of overburden warrants the Site as not hydrogeologically sensitive. As Step 1 and 2 have been met, contaminant attenuation considerations and calculations were not completed for this report.

Based on the analyses performed for this hydrogeological assessment, McIntosh Perry is of the opinion that the aquifer for which the test well intersects can adequately supply water for the proposed private development on-Site.

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1.0 INTRODUCTION

McIntosh Perry ('MP') was retained by Trevor Watkins ('the Client') to conduct a Hydrogeological Assessment and Terrain Analysis in support of a proposed storage facility development for the property located at 273-275 Russ Bradley Road ('the Site', previously known as 1500 Thomas Argue Road) in Carp, Ontario. It is our understanding that the client is looking to develop a private storage facility, which includes twelve (12) self storage buildings. The area in which this private storage facility will be placed is approximately 2.4 hectares (ha.) in size.

The Site location is shown on Figure 1 – Site Location, and an outline of the Site showing the neighbouring properties and the proposed area of future development is presented on Figure 2 – Site Layout.

This report has been prepared using data collected by Mcintosh Perry staff on September 13, 2022, from a drilled test well (A342436) located at 273-275 Russ Bradley Road. Hydrogeological data from this well are considered representative of the subject Site, as this well will be utilized for servicing the proposed development.

This Hydrogeological Evaluation addresses the following:

- Well Record search and evaluation;
- Background hydrogeological evaluation;
- Oversight of a 420-minute pumping test at 273-275 Russ Bradley Road;
- Water level and flow monitoring, field water quality analyses;
- Sampling and analysis includes 2 sample analyzed for the 'Subdivision Supply Suite' of parameters (including trace metals and volatiles);
- Summary of infiltration data throughout portions of the Site, completed as part of the infiltration assessment of subsurface materials; and
- Data Evaluation and Report.

1.1 Consultation

McIntosh Perry conducted a pre-consultation with a representative from the City of Ottawa via phone call on August 19, 2022. Michel Kearney, P.Geo. from the City of Ottawa provided information on what would be required for this Hydrogeological Report and Terrain Analysis, including the following:

- The Hydrogeological Report prepared for the Site must follow the guidelines stipulated in Procedure D-5-5 (Private Wells: Water Supply Assessment);
- It was communicated that a 6-hour pumping test would be acceptable if the drilled test well shows sufficient water quality and quantity (proper rate and recovery);
- Volatile organic carbons (VOCs) and metals are to be included in the subdivision package for the water quality analysis; and
- The terrain analysis needs to provide an impact of the septic system at the property line.

2.0 BACKGROUND

2.1 Site Setting

The Site is located in the community of Carp, located in West-Carleton-March Ward in the City of Ottawa, Ontario (Figure 1). The Site is currently unoccupied, vacant land. The Site is unused, with the Carp Airport located in close proximity (west) of the Site. Due to the proximity of the airport, the Site is designated as "Air Transportation Facility Zone" per the City of Ottawa Zoning By-Law No. 2008-250.

At the time of investigation, on-site conditions consisted primarily of a grassed and forested area. Based on a review of aerial photos and field observations, it appears that the Site has never been contemporarily developed.

2.2 Neighbouring Properties and Land Uses

The Site is located south of the intersection of Carp Road and Russ Bradley Road. The Site is within a rural land use area, and is surrounded by Carp Road to the north/northeast, William Mooney Road to the South, the Carp Airport to the west. Land-use on all sides from the Site include mainly commercial and industrial properties.

The proposed total area of the Site, which includes the private storage facility, consists of an approximate 2.4-hectare portion of land. While MECP Water Well Information System (WWIS) records for the area do not provide the detailed locations of most wells, all properties developed in proximity to the Site are assumed to be privately serviced with wells and on-site sewage systems.

Figure 3 – MECP Wells Record Summary, presents the MECP Well Tag numbers and approximate well locations, where available, for wells within approximately 500 m of the Site. Well Records within 500 m of the Site are included in Appendix A.

2.3 Hydrology

Topography was reviewed on the Atlas of Canada Toporama website. Site elevation is approximately 111 – 114 metres above sea level (m asl). Ground surface at the Site is generally gently sloped throughout the site towards the south, towards an unnamed creek which flows west.

Surface drainage is interpreted to reflect surface topography and is likely controlled via areas of permeable ground surface. An unnamed creek runs south of the Site, flowing towards the west. Shallow groundwater in the vicinity of the Site likely flows toward this creek. The closest permanent water body is Carp River, located approximately 1.6 km north of the Site, at its closest point. On a regional scale, surface water is likely to flow to the west/northwest towards Carp River, eventually flowing into Lac des Chats.

It is noted that during the fieldwork completed for the Hydrogeological Assessment, the Site appeared to be poorly drained; standing water was present in several areas of the Site, which was not consistent with the City of Ottawa's designation of the property as a high-infiltration area. This was further supported by data indicating low infiltration rates, as measured by *in-situ* testing with a Guelph Permeameter across portions of the Site (as summarized below).

2.4 Geology and Hydrogeology

On-site overburden in the area of the proposed severance is listed by the Ontario Geological Survey (OGS) as coarse-textured glaciomarine deposits of sand, gravel, minor silt and clay. This is supported by the MECP WWIS records, which indicate mainly sand, clay, and gravel overburden for wells listed within 500 m of the Site. Refer to Section 5.0 for a more detailed discussion regarding surficial geology.

On-site bedrock is generally characterized as limestone, dolostone, shale, arkose, and sandstone of the Simcoe Group of the Shadow Lake Formation (OGS, 2021), which is supported by a majority of well records in the area that list the bedrock as either "shale" or "limestone".

Based on surrounding topography, shallow groundwater is interpreted to have a west/northwest component.

2.4.1 Recharge and Discharge Areas

Based on a review of topographic data, geological maps, and Site visits, the property slopes slightly upwards to the south. Shallow groundwater and surface water likely flow towards the west/northwest.

Based on previously noted permeability testing, infiltration is relatively low across the Site. This appears to be partly due to high water levels within the overburden soils (see Appendix G), as well as relatively low hydraulic conductivities in the shallow soil. Site observations made in June and August 2022, prior to the pumping test, indicate that the property and development area is highly saturated, with many areas of stagnant standing water. The wooded area on-Site in particular appears to be a local topographic low point.

2.4.2 Potential Sources of Contamination

A windshield survey of the surrounding area was conducted in combination with a Site walkthrough and review of maps and zoning information. The Site is located in a predominantly rural commercial area. This does not appear to pose any significant source of contamination to the proposed severance. No obvious potentially contaminating activities (e.g., fuel outlets, improperly maintained bulk fuel storage, salt storage, manure piles, livestock yards, etc.) were observed in the vicinity of the Site at the time of inspection.

The Site and surrounding properties are not connected to municipal services. As such, there are likely private on-site sewage systems at nearby residences.

2.4.3 Water Well Record Review

The MECP's WWIS database indicated twenty-two (22) water wells that are located within 500 m of the centre of the Site. Five (5) of these records have no information available or are listed as abandoned wells. Nine (9) wells are listed for domestic or commercial water supply purposes, four (4) are listed as observation

wells, and one (1) well is listed as a test/monitoring well. The MECP WWIS records are shown on Figure 3, and data are summarized in Appendix A.

Wells were completed in varying subsurface materials including clay, sand, gravel, limestone, and shale, ranging in final depths of 0.3 – 48.7 m below ground surface (bgs). The average depth to bedrock was reported to be 34 m bgs. Driller-reported static groundwater levels ranged from 1.1 – 15.2 m bgs.

Driller-reported well yields ranged from 11.4 – 94.7 L/min.

For the on-Site well (TW1), the well was completed primarily in clay (mixed with gravel) from ground surface to 41.5 m bgs), followed by limestone at 41.5 m to 152 m bgs. The driller-reported static groundwater level was 60 m bgs, and the well yield (prior to hydo-fracking), was listed at 18.9 L/min.

2.4.4 Hydro-Fracking

Prior to the pumping test administered on September 13th, 2022, Test Well 1 (TW1) was hydro-fracked by a licensed well driller (Ontario Water Well Fracturing Ltd.) to increase yield. Hydro-fracking (or hydro-fracturing) is a process whereby water is injected into the well at a high pressure to create small fractures within the bedrock material in order to facilitate greater infiltration of groundwater into the well itself. Hydro-fracking was performed on this well as there were previously identified issues with regards to water supply and production.

3.0 METHODOLOGY – HYDROGEOLOGICAL ASSESSMENT

McIntosh Perry conducted a hydrogeological investigation at the Site to assess the feasibility of servicing the proposed development. The work generally followed the guidance of MECP Procedure D-5-5: Technical Guideline for Private Wells: Water Supply Assessment.

McIntosh Perry tested the drilled test well located at 273-275 Russ Bradley Road (Test Well 1, TW1 – A342436), which is representative of the hydrogeological conditions across the proposed development. The well record is saved in Appendix B, appended to this report.

A 420-minute pumping test was conducted at TW1 by McIntosh Perry staff on September 13, 2022. Based on correspondence received from the City of Ottawa (dated August 19, 2022), it was expressed that a 6-hour pumping test would be sufficient if the well indicated sufficient water quantity and quality. Based on conditions encountered at the time of the pumping test (involving changing the pumping rate to allow groundwater to stabilize), a 420-minute (7 hour) pumping test was completed.

Groundwater was pumped directly from TW1 using a pump provided and installed by Air Rock Drilling. The pumped water was directed away from the test well and was allowed to flow overland across the Site.

During the testing period, water levels in the well were measured using an electronic water level tape. Water quality (pH, temperature, conductivity, oxygen reduction potential, turbidity, dissolved oxygen, and total dissolved solids) was also monitored and recorded in the field during the test using calibrated instruments (general parameters -Horiba U-52; Turbidity - LaMotte 2020). The LaMotte 2020 turbidity meter is calibrated monthly by McIntosh Perry staff following manufacturers instructions. The calibration certificate for the Horiba U-52 completed by the rental company (Maxim) is included in Appendix C. Additional visual water quality observations were observed including colour, clarity/turbidity, odour, and effervescence, as seen in Table 1 appended to this report. Groundwater chemistry had stabilized prior to collecting samples of the well water.

One sample (TW1_1) was collected for laboratory analysis, taken 180 minutes after the start of the pumping test. An additional sample (TW1_2) was collected for laboratory analysis 415 minutes after the start of the test. These sample were analyzed for the full suite of subdivision supply parameters, including metals, microbial, and VOCs.

At the time both samples were collected from TW1, residual chlorine readings indicated a value of 0.0 mg/L using a Hach DR900 colorimeter; the Hach DR900 was zero standardized prior to collecting samples. All groundwater samples were collected unfiltered and unchlorinated, directly into clean bottles supplied by the analytical laboratories (Paracel Laboratories Ltd., Ottawa, ON). The samples were kept on ice and delivered directly to Paracel under strict chain of custody procedures. All of the samples were received by the laboratory within 24 hours of collection.

Paracel is fully accredited by the Standards Council of Canada/Canadian Association for Laboratory Accreditation (SCC/CALA) and has accreditation for Ontario Safe Drinking Water Act (OSDWA) testing.

During the pumping test, water level monitoring consisted of manual readings with an electronic water level tape. Drawdown was measured in the pumped well and measurements were made until at least 95% recovery were achieved, or 24 hours had passed (whichever came first). A data logger was not used as part of this assessment due to concerns with down-hole entanglement.

Drawdown and recovery data from the pumping tests were plotted and analyzed using the Cooper-Jacob solution. The hydraulic conductivity (K, m/s) and transmissivity (T, m²/d) and long-term yield (Farvolden and Moell Method) of the aquifer were estimated.

Storativity could not be assessed properly without the use of an additional observation well, which was not available at the time of the test.

It is noted that in addition to the pumping test completed, McIntosh Perry completed an infiltration assessment across the Site to determine the general infiltration rates of subsurface materials. Based on this assessment completed in October 2022, permeability across the Site was low given the excess of saturated soils encountered. Two infiltration studies were conducted on-Site. In June of 2022, the advancement of three (3) test locations was completed, two (2) of which were outside of the proposed infiltration infrastructure area. Results of this program indicated low infiltration rates which ranged from 3.4×10^{-6} to 4.9×10^{-7} m/s. In October, additional infiltration testing was completed on-Site where the proposed infiltration rates were again found, with rates ranging from 1.74×10^{-8} to 6.4×10^{-6} m/s. Appendix G provides additional information on the June 2022 infiltration program.

4.0 RESULTS

A drawdown curve and tabular data from the pumping test conducted at the Site are available in Appendix D. A summary of groundwater quality data and the official Laboratory Certificates of Analysis are available in Table 2 and Appendix E, respectively.

4.1 Static Conditions

Prior to the initiation of pumping, water levels were measured in the well. The static groundwater level was recorded at 9.87 m below top of casing (btoc) at the time of the pumping test (t=0). Assigning an arbitrary site benchmark of 100.00 m (local) to the top of the casing, the static water elevation in the well was 90.13 m above datum (ad). According to the MECP Well Record for TW1 (A342436) the proposed pump depth was recommended to be 91.4 m bgs – the depth used at the time of the pumping test was 85.3 m bgs. The pumping depth used during the test corresponded to an available water column of approximately 75.5 m.

Standing water or evidence of groundwater discharge was not observed at the test well location at the time of the pumping test.

4.2 Pumping Test – TW1

The pumping test was conducted at TW1 (273-275 Russ Bradley Road) was performed under the supervision of McIntosh Perry on September 13, 2022. Water was pumped directly from the test well using equipment provided by Air Rock. The water discharge was directed away from the test well and was allowed to flow overland across the Site, away from the well. At the time of the pumping test, the weather was approximately 20°C and cloudy.

At 7:40 AM, the pump was turned on and the flow rate adjusted to approximately 60 L/min. This pumping rate was maintained for approximately 35 minutes, at which time the pumping rate was changed to 53.3 L/min for an additional 157 minutes. The pumping rate was changed again 192 minutes after the start of the test to 48 L/min – this rate was maintained for three minutes and was then changed as water levels were not stabilizing. The pumping rate was changed to 42 L/min 195 minutes after the start of the test and remained at that rate until the pump was shut off (420 minutes after the start of the test).

The stepwise reductions in the pumping rate described above were performed as water levels were not stabilizing. The higher pump rate that was originally used at the start of the pumping test was reduced in order to achieve a more sustainable pumping rate which could be maintained for the remainder of the test. All pumping rates used were greater than the minimum daily water demand of approximately 13.7 L/min.

The groundwater level ranged between 9.87 – 53.95 m btoc, with a maximum drawdown of 44.08 m observed. At the end of the test, approximately 38.7 m of the available water column remained. Following pump shutoff (420 minutes), the water level was recorded at 11.7 m btoc (88.24 m ad) within 50 minutes, representing approximately 97% recovery.

All water level measurement data are presented in Table 2, appended to this report.

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4.2.1 Well Yield

The pumping test undertaken by McIntosh Perry provides a reasonable indication of the yield of the Test Well. During this test, over 20,000 L of water was pumped from the well. Given that the typical volume (daily flow) required for an individual employee per eight hour work shift is 75 L, the 20,000 L pumped would be sufficient for over 250 employees. It is anticipated that no more than two employees will staff the operations per eight hour shift.

4.2.2 Transmissivity

The transmissivity for TW1 was calculated following the Cooper-Jacob method. The calculations for Transmissivity are presented in Appendix F. Transmissivity was calculated using the following equation:

$$T = \frac{2.3 Q}{4 \pi \Delta s}$$

Where:

- T is the transmissivity (m²/day)
- Q is the pumping rate during the pumping test (L/min); and,
- Δs is the differential for residual drawdown for one log cycle (m)

Using drawdown and recovery data, a transmissivity during the drawdown period was 0.6 m²/day, and a transmissivity during the recovery phase was calculated at 0.5 m²/d using the Cooper-Jacob method.

Assuming an aquifer thickness of 109.12 m (as approximated by the interval between the bottom of the casing and the bottom of the well), the screened formation of TW1 was calculated to have an average hydraulic conductivity of 9.35×10^{-8} m/s.

Storativity (S) could not be calculated as no observation wells were available for measurement at the time of the pumping test.

A summary of the well and hydrogeological properties determined during the testing work at the Site are presented in Appendix D. The calculations for Transmissivity are presented in Appendix F.

4.2.3 Long Term Yield

The theoretical long-term safe yield was calculated using both the Farvolden and Moell methods. Drawdown data were used, as they are likely more representative of aquifer conditions (see above Section 4.2.2).

It is important to note that the safe yield may be less than the values calculated below, due to well-field interference that may be present in the final lot/supply well configuration.

Farvolden Equation

The long-term yield (Q₂₀) was calculated using the following Farvolden equation:

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$$Q_{20} = 0.68 T Ha S_f$$

Where:

- Q₂₀ is the twenty-year safe yield;
- T is the transmissivity;
- Ha is the available water column height (above the pump); and
- S_f is a safety factor (0.7).

Based on the Farvolden Method, calculations indicate that a twenty-year safe yield is on the order of 14 L/min. This means that TW1 could theoretically sustain continuous pumping for 20 years at this rate.

Moell Method

The Moell Method was also used to calculate the theoretical long-term safe yield for the pumping well. The long-term yield (Q₂₀) was calculated using the following Moell equation:

$$(Q_{20}) = (Q Ha Sf) / (s100 + 5 \Delta s)$$

Where:

- Q₂₀ is the twenty-year safe yield (m³/day);
- Ha is the available water column height (m);
- S_f is a safety factor (0.7);
- s100 is the drawdown at 100 minutes (semi-log long-term graph);
- Δs is the change in hydraulic head over one log cycle (drawdown vs. log time, see Appendix D); and
- Q is the pumping rate during the pumping test (L/min).

Using the Moell Method, calculations indicate that a twenty-year safe yield for the well is on the order of 12 L/min.

The twenty-year (long-term) safe yield calculations described above for this supply well ranged from 12-14 L/min. These calculations are inherently conservative, as the pump will likely cycle on and off over a shorter period of time. The peak hourly flow rates will likely be less than the calculated values above. Further, the 7-hour pumping test conducted indicates sustainable flow rates which are considered to be sufficient to support the proposed development. Therefore, Mcintosh Perry is of the opinion that the aquifer is capable of supplying water at a flow rate greater than the minimum of 13.7 L/min (as outlined in Procedure D-5-5), as well as the per-person requirements of 450 L/day, for the proposed private storage facility.

The calculations for the Farvolden and Moell method are presented in Appendix F.

4.2.4 Water Quality

Laboratory Certificates of Analysis for on-site groundwater testing are presented in Appendix E. A summary of field and laboratory results from the Test Well is presented in Tables 1A, 1B, and 2. Two samples were taken during the 420-minute pumping test of TW1 on September 13, 2022. The first sample (TW1-1) was taken 180 minutes after the start of the test, and the second sample (TW1-2) was taken 415 minutes after the start of the test. Both samples were taken directly from the pump discharge hose into laboratory supplied containers.

Prior to collection of the groundwater samples, the residual chlorine (total and free chlorine) reading using the Hach DR900 colorimeter was 0 mg/L after 164 minutes and 360 minutes after pumping. Prior to usage, the Hach DR900 was calibrated according to the manufacturer's printed instructions.

All analytical results were compared to the Ontario Drinking Water Standards, Objectives, and Guidelines (ODWS).

Based on the analytical results from TW1 on September 13, 2022, the following exceedances were noted:

- Hardness (OG: 100 mg/L): TW1-1 (271 mg/L) and TW1-2 (265 mg/L)
- Sulphide: (AO: 0.05 mg/L): TW1-1 (3.14 mg/L) and TW1-2 (3.36 mg/L)
- Turbidity: (AO: 5 NTU): TW1-1 (34.8 NTU)
- Aluminum: (AO: 0.1 mg/L): TW1-1 (0.68 mg/L) and TW1-2 (0.14 mg/L)
- Iron (AO: 0.3 mg/L): TW1-1 (0.82 mg/L); and
- The health warning limit for sodium (20 mg/L) was exceeded in sample TW1-1 (22.7 mg/L) and TW1-2 (24.1 mg/L)

No health-related maximum acceptable concentration (MAC) were exceeded.

The bacteria were all non-detectable (0 cts/100 mL for E-coli, Fecal Coliforms, and Total Coliforms), in the sample that was collected at TW1.

Field-reported turbidity was considerably lower than laboratory-reported turbidity throughout the pumping test. While turbidity dropped to acceptable levels throughout the test, elevated turbidity is likely a result of the hydrofracking process, and should improve with continued well development. With further well development (pumping and use of the well), any fine grained material is agitated, causing it to become suspended and then removed during pumping. Thus, with continued use of the well, turbidity values are expected to decrease.

The Langelier Saturation Index (LSI) and Ryznar Stability Index (RSI) were calculated for TW1 (Appendix F). These results indicate that there is potential for scale to form on pipes, and that any calcium carbonate formation is not likely to form a protective corrosion inhibitor film (LSI=0.34, RSI=7,2).

4.2.5 Water Treatment

A review of the analytical data collected for the groundwater sample revealed exceedances of the well of Aesthetic Objectives (AO) or Operational Guidelines (OG). No MACs (health related) were exceeded. While the analysis of groundwater did not reveal any health-related issues, treatment can be utilized to make the water more palatable, if so desired. All parameters which exceeded AO and OG can be treated to improve water quality. In addition, aesthetic parameters such as total dissolved solids and iron are expected to either improve with continued development and use or can be readily treated.

After review of the analytical results, the following methodologies for treatment are recommended:

Turbidity:	Carbon filtration, greensand filtration, reverse osmosis
Salts:	Reverse osmosis
Hardness:	lon exchange, reverse osmosis
Iron:	Reverse osmosis, greensand filter
Sulphide:	Adsorption, aeration, chlorination, greensand filtration, oxidation
Aluminum:	Distillation, reverse osmosis

Filtration is a treatment method that can be used to address the above noted exceedances for turbidity, iron, and sulphide. Several filtration methods exist and offer adequate treatment for issues related to well water treatment. The use of granulated activated carbon filters or greensand, for example, constitute two methods of filtration.

Coagulation is a chemical water treatment process. It involves the use of a material which precipitates into water and causes fine particles to agglomerate into larger particles, which can then be removed via settling and/or filtration.

Distillation is a treatment process in which water is converted into a vapor state, then cooled, condensed, and collected. It is done to remove solids and other impurities from the water.

Reverse osmosis is a treatment process in which dissolved ions are removed from water using a difference in pressure through a semi-permeable membrane. This membrane will filter water and prevent certain undesirable dissolved materials from passing through.

Oxidation/aeration involves the injection of oxygen into the well water, whereby granular media (such as manganese-oxide) is used and allows for the adsorption of iron and manganese.

lon exchange (often seen in the form of water softeners) is a treatment which can remove ferrous iron from the well water.

Chlorination involves the introduction of chlorine into the well. Chlorine will allow for disinfection and decrease the quantity of sulphide and other undesirable parameters.

Further development of the well is recommended. This will lower turbidity, hardness, iron, and aluminum

concentrations. As indicated in Section 4.2.4 above, with continued development (pumping and use of the well), fine-grained materials are agitated and become dissolved, which are then removed from the well during further development.

4.1 Long-term Groundwater Monitoring

As infiltration throughout the subsurface materials on the Site appears to be low (see Appendix G for the infiltration memo conducted in October 2022), additional information regarding shallow groundwater is needed in the proposed development area. McIntosh Perry has installed a shallow groundwater monitoring well (BH22-2) to assist in characterizing the shallow groundwater regime in proximity to proposed stormwater management infrastructure. This well is in addition to an existing on-site shallow groundwater monitoring well (BH21-1) installed as part of McIntosh Perry's geotechnical scope of work.

Monitoring well BH22-2, installed within the proposed infiltration gallery area, was completed on December 6, 2022. This well was installed by Strata Drilling Group using a Geoprobe to a maximum depth of 15 ft (4.5 m) bgs. It is noted that during the well installation, the saturated soils continued to slough into the open hole, causing a slight upwelling of the well casing/pipe. Immediately after the monitoring well was installed, geodetic elevations of the ground surface of the borehole and monument casing was obtained, as well as geodetic elevations of nearby supply wells.

Further groundwater level readings at BH22-2 will continue at the Site throughout the upcoming winter (2022) and spring (2023) months. Water level data will be primarily used for stormwater management purposes.

5.0 TERRAIN ANALYSIS

5.1 Preamble

A series of four (4) test holes were advanced by McIntosh Perry staff at various locations throughout the proposed septic area on November 24th, 2022 (see Figure 4). The test hole locations were advanced using a hand auger and shovel, completed to characterize subsurface materials, the depth of overburden, depth to shallow groundwater, and to permit the collection of overburden soil samples for characterization. It is noted that holes were only advanced to a maximum depth of 2.0 m bgs as required for the purposes of assessment for the future septic location.

5.2 General Site Evaluation

5.2.1 Overburden Depth

Overburden across the Site was found to be relatively thick, having an average thickness of 1.2 m. The test hole locations are outlined on Figure 4. It is important to note that moist to saturated conditions were observed within each test hole advanced within the proposed septic location.

Although overburden based on the terrain analysis alone was estimated to be a maximum of 2 m thick (see TP-2, below), overburden thickness was additionally surmised based on information from the subsurface materials encountered during the infiltration assessment, as well as an overview of well records from the Site.

In addition, based on the geotechnical investigation completed for the Site in which three (3) boreholes were advanced, bedrock was not encountered. Overburden depth was found to be at least 6.7 m bgs.

5.2.2 Overburden Characterization

The soil and groundwater conditions logged in the test holes are presented in Table 3 below. The test hole summaries indicate the subsurface conditions at the specific test hole locations only; subsurface conditions at other locations outside of the investigated area could differ from those encountered within the investigated area.

Table 3: Summary of Test Holes							
Test Pit ID	Total Depth (m)	Depth to Water (m)	Soil Characteristics				
TP-1	1.0	1.0	Grey/brown silty sand, trace clay, loose, moist to wet				
TP-2	2.0	1.5 – 2.0	Grey/brown silty sand, trace clay, loose, moist to wet				
TP-3	1.0	0.7 – 0.8	Grey/brown silty sand, trace clay, loose, moist to wet				
TP-4	1.1	1.0	Grey/brown silty sand, trace clay, loose, moist to wet				

The soil descriptions in this report are based on commonly accepted classification and identification employed in engineering practice. It is noted that no bedrock was encountered during the digging of test holes. In addition, no bedrock was encountered during the geotechnical investigation. McIntosh Perry employed judgement in the classification and description of soil and may not be exact but are accurate to what is common in current engineering practice. The grain size analysis is included in Appendix H.

5.2.3 Soil Classification for Private Sanitary Servicing

Comparison of the soil classification for the Unified Soil Classification as provided in the Ministry of Municipal Affairs and Housing (MMAH) Supplementary Standard SB-6: Time and Soil Descriptions, reveals that the main native soil underlying the upper topsoil appears to be within the following soil group:

• SM: Silty sands, sand-silt mixtures

According to Table 2 of SB-6, the SM group of soils has a coefficient of permeability (K) of 10⁻⁵ to 10⁻³ with a percolation time (T) of 8 to 20 min/cm. This soil type has a medium to low permeability and is deemed acceptable as the native receiving soil for proposed Class 4 sewage systems.

Based on the encountered overburden, it is recommended that the topsoil layer be stripped where the septic system is proposed for construction. The thickness of native overburden has been determined through an overview of well records from the Site, subsurface conditions and depths of overburden encountered during the infiltration assessment, as well as the observation of soil thicknesses encountered during the terrain assessment portion. Given the general thickness of native overburden suitable for septic disposal bed construction, partial or fully raised septic beds may be required due to the shallow depth to the overburden groundwater, to meet the Ontario Building Code (OBC) requirement of 0.9 m separation between bedrock or shallow groundwater and the underside of the disposal bed pipe.

5.2.4 Bedrock

As previously discussed, on-site bedrock is generally characterized as limestone, dolostone, shale, arkose, and sandstone of the Simcoe Group of the Shadow Lake Formation (OGS, 2021). No bedrock was encountered on-Site during the test hole advancements, nor the geotechnical investigation,

5.3 Predictive Assessment - Contaminant Attenuation

5.3.1 Contaminant Attenuation

The MECP Procedure D-5-4 (Technical Guideline for Individual On-site Sewage Systems: Water Quality Impact Risk Assessment) outlines the provision for predictive assessment of attenuation. The predictive assessment is a 3-step process where each subsequent "step" must be assessed if the previous "step" is not met. The 3-step process is as follows:

- Step 1 Lot Size Consideration
- Step 2 System Isolation Consideration
- Step 3 Contaminant Attenuation Considerations

The following outlines the results of the sewage system impact assessment undertaken by McIntosh Perry.

Step 1 - Lot Size Consideration

The area of the property is roughly 5.8 ha.

Based on the lot area noted above, Step 1 of the 3-Step process is satisfied; the proposed lot size is greater than 1 hectare, with no lot less than 0.8 hectares.

There is sufficient spatial area for the natural attenuation of nitrate-nitrogen at acceptable concentrations based on MECP Procedure D-5-4. Based on well records and observations made in the field during the terrain

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assessment, overburden thickness is on average greater than 2.0 m. In addition, the overburden thickness was found to be at least 6.7 m bgs as observed during the geotechnical investigation.

Step 2 - System Isolation Consideration

As previously outlined, the proposed lot sizes are greater than 1.0 ha., therefore System Isolation Considerations are not applicable to the proposed development. If it can be demonstrated that the sewage system effluent is hydrogeologically isolated from the existing or potential drinking water supply aquifer, then the risk to groundwater is considered to be low. The system isolation review needs to account for lands that extend up to 500 metres from the Site.

Based on a review of available geological information and mapping, and in conjunction with site observations made during the Terrain Analysis and infiltration assessment, the overburden depth on-site has a thickness of approximately 34 m bgs and consists of primarily fine -grained material (silty sand with clay). Groundwater was found at depths ranging from 0.7 to 1.5 m bgs at TP-3 and TP-2, respectively, as seen in Table 3 above. Due to the thickness of overburden, and the depth at which the supply aquifer is found (25 to 48 m bgs) the Site is not considered to be hydrogeologically sensitive. Step 1 and Step 2 have been met, and therefore contaminant attenuation considerations (as outlined in Step 3) are not necessary for this report.

6.0 CONCLUSIONS AND RECOMMENDATIONS

6.1 Conclusions

6.1.1.1 Well Yield

McIntosh Perry conducted a 420-minute pumping test at an average pumping rate of approximately 47.8 L/min.

During the pumping test, greater than 20,000 litres of groundwater was pumped from the well. Total drawdown resulting from the 420-minute pumping test was 44.08 m. Within 50 minutes following the cessation of pumping, water level recovery for the well was recorded approximately 97%.

Calculations for long term yield ranged from 12 L/min (Moell) to 14 L/min (Farvolden). These calculations are inherently conservative, as the pump will likely cycle on and off over a shorter period of time. The peak hourly flow rates will likely be less than the calculated values above. Further, the 7-hour pumping test conducted indicates sustainable flow rates which are considered to be sufficient to support the proposed development. Therefore, Mcintosh Perry is of the opinion that the aquifer is capable of supplying water at a flow rate greater than the minimum of 13.7 L/min (as outlined in Procedure D-5-5) for the proposed private storage facility.

6.1.1.2 Water Quality and Treatment

All analytical results were compared to the Ontario Drinking Water Standards, Objectives, and Guidelines (ODWS). Based on the analytical results from the groundwater sampled from the on-Site well on September 13, 2022, the following exceedances were noted:

- Hardness (OG: 100 mg/L): TW1-1 (271 mg/L) and TW1-2 (265 mg/L)
- Sulphide: (AO: 0.05 mg/L): TW1-1 (3.14 mg/L) and TW1-2 (3.36 mg/L)
- Turbidity: (AO: 5 NTU): TW1-1 (34.8 NTU)
- Aluminum: (AO: 0.1 mg/L): TW1-1 (0.68 mg/L) and TW1-2 (0.14 mg/L)
- Iron (AO: 0.3 mg/L): TW1-1 (0.82 mg/L); and
- The health warning limit for sodium (20 mg/L) was exceeded in sample TW1-1 (22.7 mg/L) and TW1-2 (24.1 mg/L)

No health-related maximum acceptable concentrations (MAC) were exceeded. All AO and OG exceedances are considered treatable, if so desired.

6.1.2 Terrain Evaluation

Soil materials encountered during the terrain assessment consisting of fine, loose, moist to wet silty sand. It was shown that thickness of soils extends to 6.7 m bgs, based only on the depth at which holes were dug for the purposes of subsurface characterization for the septic assessment, as well as subsurface conditions encountered during the infiltration assessment.

Based on the soils encountered during the terrain assessment and review of subsurface materials from the well records, as well as the proposed size of the lot (severed) it has been determined that there is sufficient spatial area for the natural attenuation of nitrate-nitrogen at acceptable concentrations based on MECP Procedure D-5-4. Due to the thickness of overburden, the Site is not considered to be hydrogeologically sensitive.

6.2 Recommendations

6.2.1 Well Construction

• Referencing the Well Record for the Site well (A342436), it has been determined that the on-Site supply well meets the requirements under 0.Reg. 903.

6.2.2 Well Yields

• Calculations for long term well yield indicate that the aquifer currently utilized can support the proposed development.

6.2.3 Water Quality Treatment

- Further development of the well prior to connection to a structure is recommended. This will likely lower turbidity, hardness, and metals concentrations;
- If water softening is desired, the use of potassium salts (i.e., KCI) is recommended. With the use of conventional water softeners, it is important to note that sodium concentrations will be elevated;
- Aesthetic parameters such as total dissolved solids and iron are expected to either improve with continued development and use or can be readily treated, if so desired. Iron can be treated through cation exchange, greensand filtration, or oxidation with filtration through proprietary filter media or chlorination followed by sand or multimedia filtration, depending on the iron concentrations; and
- It is recommended that the Client notify the local Medical Officer of Health as the sodium concentration exceeds the health-related warning limit.

6.2.4 Wastewater Treatment

- The overburden for the site is comprised of silty sand to sandy silt mixtures (SM) which have a low to medium permeability and is acceptable for construction of septic systems per the Ontario Building Code (OBC);
- The depth to bedrock or perched groundwater may be less than 2.0 m; the construction of raised or partially raised disposal beds is potentially required; and
- Construction of septic system will require conformance to the OBC for all aspects including setback distances from residences and wells.

7.0 LIMITATIONS

This report has been prepared and the work referred to in this report has been undertaken by McIntosh Perry Consulting Engineers Ltd. for the applicants and the regulatory authority. It is intended for the sole and exclusive use of the applicants, their affiliated companies and partners and their respective insurers, agents, employees, advisors, and reviewers. The report may not be relied upon by any other person or entity without the express written consent (Reliance Letter) of McIntosh Perry Consulting Engineers Ltd.

Any use which a third party makes of this report, or any reliance on decisions made based on it, without a reliance letter are the responsibility of such third parties. McIntosh Perry Consulting Engineers Ltd. accept no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions based on this report.

The investigation undertaken by McIntosh Perry Consulting Engineers Ltd. with respect to this report and any conclusions or recommendations made in this report reflect McIntosh Perry Consulting Engineers Ltd. judgment based on the Site conditions observed at the time of the site inspection on the date(s) set out in this report and on information available at the time of the preparation of this report.

This report has been prepared for specific application to this Site and it is based, in part, upon visual observation of the Site, subsurface investigation at discrete locations and depths, and specific analysis of specific chemical parameters and materials during a specific time interval, all as described in this report. Unless otherwise stated, the findings cannot be extended to previous or future Site conditions, portions of the Site which were unavailable for direct investigation, subsurface locations which were not investigated directly, or chemical parameters, materials or analysis which were not addressed. Substances other than those addressed by the investigation described in this report may exist within the Site, substances addressed by the investigation may exist in areas of the Site not investigated and concentrations of substances addressed which are different than those reported may exist in areas other than the locations from which samples were taken.

If site conditions or applicable standards change or if any additional information becomes available at a future date, modifications to the findings, conclusions and recommendations in this report may be necessary.

8.0 CLOSURE

We trust that this information is satisfactory for your present requirements. Should you have any questions or require additional information, please do not hesitate to contact the undersigned.

Respectfully submitted, McIntosh Perry Consulting Engineers Ltd.

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HYDROGEOLOGICAL ASSESSMENT AND TERRAIN ANALYSIS 273-275 RUSS BRADLEY ROAD, CARP, ONTARIO



TABLES

McINTOSH PERRY

Table 1Summary of Field Water Quality Parameters273-275 Russ Bradley Road (TW1)

Pumping Test at:	TW1	[Date:			13-Sep)-22		
					Dissolved				
Time Elapsed	Turbidity	рН	Conductivity	Temperature	Oxygen (DO)	TDS	Odour	Effervesence	Flow Rate
(min)	(NTU)		(us/cm)	(°C)	mg/L	(ppm)			(L/min)
8	15.4	7.55	596	10.31	2.41	381	Sulfur	N/A	60
11	37.1	7.94	563	9.26	1.13	359	Sulfur	N/A	60
15	30.5	8.03	540	9.02	0.79	349	Sulfur	N/A	60
19	28.4	7.89	546	8.41	0.6	349	Sulfur	N/A	60
24	29.4	7.5	550	8.41	0.37	352	Sulfur	N/A	60
30	32.7	7.47	555	8.43	0.55	355	Sulfur	N/A	60
42	38.8	7.93	563	8.48	1.91	360	Sulfur	N/A	53.3
57	52.3	7.67	565	8.4	0.3	362	Sulfur	N/A	53.3
68	56.6	7.56	560	8.4	0.5	358	Sulfur	N/A	53.3
79	65.1	7.52	562	8.4	1.0	360	Sulfur	N/A	53.3
94	66.9	7.53	562	8.4	1.1	360	Sulfur	N/A	53.3
108	62.6	7.56	562	8.41	0.89	360	Sulfur	N/A	53.3
128	53.8	7.58	563	8.41	0.7	360	Sulfur	N/A	53.3
143	50.7	7.63	563	8.44	-	360	Sulfur	N/A	53.3
170	46.1	7.66	562	8.45	0.84	360	Sulfur	N/A	53.3
180	44.8	7.55	563	8.47	0.98	360	Sulfur	N/A	48
218	41.3	7.45	568	8.68	0.98	364	Sulfur	N/A	42
228	38.4	7.38	570	8.6	0.32	365	Sulfur	N/A	42
266	17.7	7.48	573	8.57	0.93	367	Sulfur	N/A	42
285	18	7.55	584	8.54	0.36	374	Sulfur	N/A	42
300	12.8	7.6	584	8.51	0.37	374	Sulfur	N/A	42
334	12.4	7.7	583	8.51	0.37	373	Sulfur	N/A	42
355	10.1	7.7	577	8.52	-	369	Sulfur	N/A	42
368	7.8	7.73	574	8.56	1	368	Sulfur	N/A	42
376	7.3	7.75	572	8.56	-	366	Sulfur	N/A	42
413	6.6	7.87	572	8.64	0.33	0.366	Sulfur	N/A	42
Notes:									

(us/cm) (°C) mg/L L/min N/A Microsiemens per centimetre Degrees celsius Milligrams per litre Litres per minute Not Analyzed

Table 2 Summary of Laboratory Water Quality Results 273-275 Russ Bradley Road

Sample ID					T14/4_4	T14/4_0
Sample Date					TW1-1	TW1-2
Location	Units	MDL	IDL ODWSOG		13-Sen-22	13-Sen-22
Parameter:					10 000 22	10 000 22
Microbiological Parameters						
E. Coli	CFU/100 mL	1	0 CFU/100 mL (0 CFU/100mL)	MAC	ND (1)	ND (1)
Fecal Coliforms	CFU/100 mL	1	-	-	ND (1)	ND (1)
Total Coliforms	CFU/100 mL	1	0 CFU/100 mL (0 CFU/100mL)	MAC	ND (1)	ND (1)
General Inorganics			``````````````````````````````````````			
Alkalinity (as CaCO3)	mg/L	5	500 mg/L	OG	187	186
Ammonia as N (N-NH3)	mg/L	0.01	-	-	0.11	0.07
Dissolved Organic Carbon (DOC)	mg/L	0.5	5 mg/L	AO	1.4	1.5
Colour	TCU	2	5 TCU	AO	4	ND (2)
Conductivity	uS/cm	5	-	-	499	509
Hardness	mg/L	0.824	100 mg/L	OG	271	265
рН	pH Units	0.1	-	-	7.9	7.9
Phenols	mg/L	0.001	-	-	ND (0.001)	ND (0.001)
Total Dissolved Solids	mg/L	10	500 mg/L	AO	278	270
Sulphide (S2)	mg/L	0.02	0.05 mg/L	AO	3.14	3.36
Tannin & Lignin	mg/L	0.1	0.05 mg/L	AO	ND (0.1)	ND (0.1)
Total Kjeldahl Nitrogen	mg/L	0.1	-	-	0.1	ND (0.1)
Turbidity	NTU	0.1	5 NTU	AO	34.8	3.3
Anions				_		
Chloride (Cl)	mg/L	1	250 mg/L	AO	22.5	25.6
Fluoride (F)	mg/L	0.1	1.5 mg/L	MAC	0.8	1.4
Nitrate as N (N-NO3)	mg/L	0.1	10 mg/L	MAC	ND (0.1)	ND (0.1)
Nitrite as N (N-NO2)	mg/L	0.05	1 mg/L	MAC	ND (0.05)	ND (0.05)
Phosphate as P	mg/L	0.2	-	-	ND (0.2)	0.3
Sulphate (SO4)	mg/L	1	500 mg/L	AO	35.1	34.3
Metals						
Mercury	ug/L	0.1	0.001 mg/L (1 ug/L)	MAC	ND (0.1)	ND (0.1)
Aluminum	ug/L	1	0.1 mg/L (100 ug/L)	AO	680	140
Antimony	ug/L	0.5	0.006 mg/L (6 ug/L)	MAC	ND (0.5)	ND (0.5)
Arsenic	ug/L	1	0.01 mg/L (10 ug/L)	MAC	ND (1)	ND (1)
Barium	ug/L		2 mg/L (2000 ug/L)	MAC	295 ND (0 E)	2//
Berghlum	ug/L	0.5	E ma/L (E000 ug/L)	NAAC	ND (0.5)	ND (0.5)
DUIUII	ug/L	10	5 IIIg/L (5000 ug/L)	IVIAC	07 ND (0.1)	94 ND (0.1)
	ug/L	100	0.007 mg/L (7 ug/L)	IVIAC	ND (0.1) 72 200	71.600
Chromium	ug/L	100	0.05 mg/l (50 Jg/l)	MAC	72,200	ND (1)
Cobalt	ug/L	0.5	0.03 mg/E (30 dg/E)	MAC	ND (0.5)	ND (0.5)
Copper	ug/L	0.5	1 mg/L (1000 µg/L)	40	ND (0.5)	ND (0.5)
Iron	ug/L	100	0.3 mg/L (300 ug/L)	AO	820	139
Lead	ug/L	0.1	0.005 mg/L (5 ug/L)	MAC	0.2	ND (0 1)
Magnesium	ug/L	200	01000 mg/ 2 (0 dg/ 2)		22,100	21,000
Manganese	ua/L	5	0.05 mg/L (50 µg/L)	AO	19	6
Molybdenum	ua/L	0.5			ND (0.5)	- ND (0.5)
Nickel	uq/L	1			ND (1)	ND (1)
Potassium	ug/L	100			5,330	4,940
Selenium	uğ/L	1	0.05 mg/L (50 ug/L)	MAC	ND (1)	ND (1)
Silver	uğ/L	0.1	<u> </u>		ND (0.1)	ND (0.1)
Sodium	ug/L	200	20 mg/L (20,000 ug/L)	AO	22,700	24,100
Strontium	ug/L	10	7 mg/L (7000 ug/L)	MAC	3120	3290
Thallium	ug/L	0.1			ND (0.1)	ND (0.1)
Tin	ug/L	5			ND (5)	ND (5)
Titanium	ug/L	5			77	15
Tungsten	ug/L	10			ND (10)	ND (10)
Uranium	ug/L	0.1	0.02 mg/L (20 ug/L)	MAC	0.1	ND (0.1)
Vanadium	ug/L	0.5			2.5	ND (0.5)
Zinc	ug/L	5	5 mg/L (5000 ug/L)	AO	9	ND (5)
Volatiles		= -		,		
Acetone	ug/L	5.0	0.001 (1.11)		N/A	ND (5.0)
Benzene	ug/L	0.5	0.001 mg/L (1 ug/L)	MAC	N/A	ND (0.5)
Bromodichioromethane	ug/L	0.5			N/A	ND (0.5)
Bromotorm	ug/L	0.5			N/A	ND (0.5)
Di Uni Uni e Inane Carbon Totrachlorida	ug/L	0.5	0.002 mg/l (2.15/l)	NAAC	N/A	
	ug/L	U.2	0.002 mg/L (2 ug/L)	IVIAU	N/A	
Chioropenzene	ug/L	0.5	0.08 mg/L (80 ug/L)	IVIAC	N/A	ND (U.5)

Table 2 Summary of Laboratory Water Quality Results 273-275 Russ Bradley Road

Sample ID					TW1-1	TW1-2
Sample Date	Units	MDI	ODWSOG	Limit Type		
Location	onits	MBE	0011000	Linit Typo	13-Sep-22	13-Sep-22
Parameter:						
Chloroethane	ug/L	1.0			N/A	ND (1.0)
Chloroform	ug/L	0.5			N/A	ND (0.5)
Chloromethane	ug/L	3.0			N/A	ND (3.0)
Dibromochloromethane	ug/L	0.5			N/A	ND (0.5)
Dichlorodifluoromethane	ug/L	1.0			N/A	ND (1.0)
Ethylene dibromide (dibromoethane, 1,	ug/L	0.2			N/A	ND (0.2)
1,2-Dichlorobenzene	ug/L	0.5	0.2 mg/L (200 ug/L)	MAC	N/A	ND (0.5)
1,3-Dichlorobenzene	ug/L	0.5			N/A	ND (0.5)
1,4-Dichlorobenzene	ug/L	0.5	0.005 mg/L (5 ug/L)	MAC	N/A	ND (0.5)
1,1-Dichloroethane	ug/L	0.5			N/A	ND (0.5)
1,2-Dichloroethane	ug/L	0.5	0.005 mg/L (5 ug/L)	MAC	N/A	ND (0.5)
1,1-Dichloroethylene	ug/L	0.5	0.014 mg/L (14 ug/L)	MAC	N/A	ND (0.5)
cis-1,2-Dichloroethylene	ug/L	0.5			N/A	ND (0.5)
trans-1,2-Dichloroethylene	ug/L	0.5			N/A	ND (0.5)
1,2-Dichloroethylene, total	ug/L	0.5			N/A	ND (0.5)
1,2-Dichloropropane	ug/L	0.5			N/A	ND (0.5)
cis-1,3-Dichloropropylene	ug/L	0.5			N/A	ND (0.5)
trans-1,3-Dichloropropylene	ug/L	0.5			N/A	ND (0.5)
1,3-Dichloropropene, total	ug/L	0.5			N/A	ND (0.5)
Ethylbenzene	ug/L	0.5	0.14 mg/L (140 ug/L)	MAC	N/A	ND (0.5)
Hexane	ug/L	1.0			N/A	ND (1.0)
Methyl Ethyl Ketone (2-Butanone)	ug/L	5.0			N/A	ND (5.0)
Methyl Butyl Ketone (2-Hexanone)	ug/L	10.0			N/A	ND (10.0)
Methyl Isobutyl Ketone	ug/L	5.0			N/A	ND (5.0)
Methyl tert-butyl ether	ug/L	2.0			N/A	ND (2.0)
Methylene Chloride	ug/L	5.0	0.05 mg/L (50 ug/L)	MAC	N/A	ND (5.0)
Styrene	ug/L	0.5			N/A	ND (0.5)
1,1,1,2-Tetrachloroethane	ug/L	0.5			N/A	ND (0.5)
1,1,2,2-Tetrachloroethane	ug/L	0.5			N/A	ND (0.5)
Tetrachloroethylene	ug/L	0.5	0.01 mg/L (10 ug/L)	MAC	N/A	ND (0.5)
Toluene	ug/L	0.5	0.06 mg/L (60 ug/L)	MAC	N/A	ND (0.5)
1,1,1-Trichloroethane	ug/L	0.5			N/A	ND (0.5)
1,1,2-Trichloroethane	ug/L	0.5			N/A	ND (0.5)
Trichloroethylene	ug/L	0.5	0.005 mg/L (5 ug/L)	MAC	N/A	ND (0.5)
Trichlorofluoromethane	ug/L	1.0			N/A	ND (1.0)
1,3,5-Trimethylbenzene	ug/L	0.5			N/A	ND (0.5)
Vinyl Chloride	ug/L	0.5	0.001 mg/L (1 ug/L)	MAC	N/A	ND (0.5)
m/p-Xylene	ug/L	0.5			N/A	ND (0.5)
o-Xylene	ug/L	0.5		1	N/A	ND (0.5)
Xylenes, total	ug/L	0.5	0.09 mg/L (90 ug/L)	MAC	N/A	ND (0.5)

Notes:	
1050	Exceeds Ontario Drinking Water Standards, Objectives, and Guidelines
21	Exceeds health warning limit for sodium (20 mg/L)
MDL	Method Detection Limit
ODWSOG	Ontario Drinking Water Standards, Objectives, and Guidelines (MOECC, 2003 rev. 2006; PIBs 4449e01)
AO	Aesthetic Objective
MAC	Maximum Allowable Concentration (Health-Related Parameter)
OG	Operational Guideline
ug/L	Micrograms per litre
mg/L	Milligrams per litre
TCU	True Colour Units
uS/cm	Microsemens per centimeter
NTU	Nephelometric Turbidity Units
CFU/100 mL	Colony-forming units (bacteria) per 100 mL

HYDROGEOLOGICAL ASSESSMENT AND TERRAIN ANALYSIS 273-275 RUSS BRADLEY ROAD, CARP, ONTARIO



FIGURES

McINTOSH PERRY





Checked By RL

Resources and Forestry, 2022.





REFERENCE

HYDROGEOLOGICAL ASSESSMENT AND TERRAIN ANALYSIS 273-275 RUSS BRADLEY ROAD, CARP, ONTARIO



APPENDIX A: MECP WATER WELL INFORMATION SYSTEM DATA

MCINTOSH PERRY
WELL ID C	COMPLETED	WELL DEPTH (m) ST	TATIC WATER LEVEL (m) DEPTH TO BEDROCK (r	m) BORE	E HOLE ID FINALSTATUS	USE1	USE2	COUNTY	MUNICIPALITY	CONN	LOT	STREET	QTY ZONE	EAST83	NORTH83 GEOLOGY	COLOR	EORMATION TOP DEPTH	FORMATION END DEPTH	UNITS OF MEASUREMENT
1503071	30-Sep-67	61	15.2	41.1	10025114 Water Supply	Domestic		OTTAWA-CARLETON	HUNTLEY TOWINSHIP	62	013		1	8 420630.5	5019702 CLAY,			0 11	0 0
1503071	30-Sep-67	61	15.2	41.1	10025114 Water Supply	Domestic		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	02	013		1	8 420630.5	5019702 MEDIUM SAND,		11	0 13	5 ft
1503129	14-Jun-58	57	8.5	46.3	10025172 Water Supply	Domestic		OTTAWA-CARLETON	HUNTLEY TOWINSHIP	03	013		1	8 420700.5	5019542 LIMESTONE,		15	2 18	17 ft
1503129	14-Jun-58	57	8.5	46.3	10025172 Water Supply 10025172 Water Supply	Domestic		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	63	013		1	8 420700.5	5019542 PREV. DRILLED		14	0 13	0 ft
1510130	27-Jun-69 27 Jun 69	61	9.8	39.9	10032160 Water Supply 10022160 Water Supply	Industrial	Irrigation	OTTAWA-CARLETON	HUNTLEY TOWNSHIP	02	014		1	8 420600.5	5019762 LIMESTONE, 5019262 MEDULIA SAND CRAVEL	GREY	13	1 20	0 11 0
1510130	27-Jun-69	61	9.8	39.9	10032160 Water Supply	Industrial	Irrigation	OTTAWA-CARLETON	HUNTLEY TOWNSHIP	02	014		1	8 420600.5	5019762 MEDIUM SAND,	GREY	10	0 11	2 ft
1510130	27-Jun-69 27-Jun-69	61	9.8	39.9	10032160 Water Supply 10032160 Water Supply	Industrial	Irrigation	OTTAWA-CARLETON OTTAWA-CARLETON	HUNTLEY TOWNSHIP	02	014		1	8 420600.5	5019762 CLAY,, 5019762 MEDILIM SAND	GREY	3	5 10	6 0
1510130	27-Jun-69	61	9.8	39.9	10032160 Water Supply	Industrial	Irrigation	OTTAWA-CARLETON	HUNTLEY TOWINSHIP	02	014		1	8 420600.5	5019762 MEDIUM SAND, CLAY,	GREY		6 3	5 ft
1514573	13-Feb-75 13-Feb-75	53.3	5.5	37.5	10036546 Water Supply 10036546 Water Supply	Domestic		OTTAWA-CARLETON OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	013		1	8 420435.5	5019162 SAND,CLAY,PACKED 5019162 LIMESTONE	GREY	11	5 12	5 ft
1514573	13-Feb-75	53.3	5.5	37.5	10036546 Water Supply	Domestic		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	013		1	8 420435.5	5019162 SAND,SILT,PACKED	BROWN		0 3	n 0
1514573	13-Feb-75 01-Nov-78	53.3 44.2	5.5	37.5	10036546 Water Supply 10038723 Water Supply	Domestic		OTTAWA-CARLETON OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	013		1	8 420435.5 8 420830.5	5019162 CLAY, LOOSE, 5019422 LIMESTONE SOFT.	BLUE GREY	3	0 11 5 14	5 ft 5 ft
1516828	01-Nov-78	44.2	12.2	10.7	10038723 Water Supply	Domestic		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	013		11	8 420830.5	5019422 CLAY, BOULDERS,	BROWN		0 2	1 11
1516828	01-Nov-78 11-Nov-81	44.2	2.4	24.1	10038723 Water Supply 10039561 Water Supply	Domestic		OTTAWA-CARLETON OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	013		1	8 420830.5	5019422 HANDHAN, BOULDERS, PACKED 5019321 CLAY, PACKED.	GREY		1 3	5 ft
1517689	11-Nov-81	65.5	2.4	24.1	10039561 Water Supply	Domestic		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	013		11	8 420929.5	5019321 SILT, STONES, PACKED	GREY	1	5 5	7 ft
1517689	11-Nov-81	65.5	2.4	24.1	10039561 Water Supply	Domestic		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	63	013		1	8 420929.5	5019321 SAND, CENTENTED, 5019321 TILL, STONES, PACKED	GREY	6	1 7	n 9
1517689	11-Nov-81 30 Sco. 04	65.5	2.4	24.1	10039561 Water Supply 11172082 Observation Wells	Domestic Not Licot		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	013	2167 0400 00	10	8 420929.5	5019321 GRANITE, MEDIUM-GRAINED, 5019325 CLAV	GREY	1	9 21	5 ft
1535240	20-Sep-04 20-Sep-04	43.9	0	38.7	11172992 Observation Walk	Not Lised		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	013	3257 CARP RD.	CARP 1	8 420424	5019205 LIMESTONE,	GREY	38	7 43.	9 m
1535787	20-Sep-05	27.4	5.9	0	11316326 Water Supply	Municipal	Public	OTTAWA-CARLETON	HUNTLEY TOWINSHIP	03	013	1508 THOMAS	CARP 1	8 420813	5019053 TOPSOIL,	BLACK		0 0.	3 m
1535287	20.5cn.05	27.4	5.9	0	11316336 Water Sumely	Municipal	PMF	OTTAWA-CARLETON	HINTLEY TOWNSHIP	03	013	1508 THOMAS	(499 1)	420813	5019053 SAND	BROWN	0	3 4	5 m
1333760	20-360-03	213	2.7	•	TISTIGED WINN SUPPLY	indiacipal.	r usin.		Institution for the second sec		013	ARQUE ROAD		446013	Jointal Jona,				
1535787	20-Sep-05	27.4	5.9	0	11316326 Water Supply	Municipal	Public	OTTAWA-CARLETON	HUNTLEY TOWNSHIP	63	013	ARQUE ROAD	CARP 1	8 420813	5019053 SAND,,	BROWN	4.	5 6.	7 m
1535787	20-Sep-05	27.4	5.9	0	11316326 Water Supply	Municipal	Public	OTTAWA-CARLETON	HUNTLEY TOWINSHIP	03	013	1508 THOMAS ARQUE ROAD	CARP 1	8 420813	5019053 GRAVEL,,	GREY	6	7 8.	2 m
1535787	20-540-05	27.4	5.9	0	11316326 Water Supply	Municipal	Public	OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	013	1508 THOMAS	CA8P 11	8 420613	5019053 SILT.	GREY	8	2 10	é m
												1508 THOMAS							
1535787	20-Sep-05	27.4	5.9	0	11316326 Water Suppry	Munopel	Public	OTTAWA-CAMETON	HUNILEY TOWISHIP	03	013	ARQUE ROAD	CA89 11	8 420813	501V053 CLAY, HAND	CARA	10.	6 14.	6 m
1535787	20-Sep-05	27.4	5.9	0	11316326 Water Supply	Municipal	Public	OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	013	ARQUE ROAD	CARP 1	8 420813	5019053 CLAY, WATER-BEARING	BLUE	14	6 21.	9 m
1535787	20-Sep-05	27.4	5.9	0	11316326 Water Supply	Municipal	Public	OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	013	1508 THOMAS	CARP 1	8 420813	5019053 CLAY, HARD	GREY	21	9 24	9 m
1535397	30.5 4-		6.0	0	11214225 Wester Count-	Municipal	D. A.G.	OTTAWA CARLETON	HINTLEY TOWNSHIP	02	012	1508 THOMAS	(100		SO100E2 CRAVEL PLOYTS	CREV			1
130101	20-sep-05	27.4	5.9	U	++310320 www.stSupply	wanopa	r sallt	OT HANNA-CARLE TON	INSINET TOWNSRIP	-13	u:3	ARQUE ROAD	1	420613	Services CRAVEL_PACKED	WE1	24	- 27.	
1536752	10-Jul-06	3.7	0	0	11691846 Observation Walls			OTTAWA-CARLETON	HUNTLEY TOWNSHIP			ROAD	OTTAWA 1	8 420326	5019172 SAND,SILTY,WATER-BEARING	GREY	2	4 3.	7 m
1536752	10-Jul-06	3.7	0	0	11691846 Observation Walls			OTTAWA-CARLETON	HUNTLEY TOWINSHIP			3257 CARP ROAD	OTTAWA 1	8 420326	5019172 SAND, FILL, FINE-GRAINED	BROWN		0	1 m
1536752	10-14-04	3.7	0	0	11691846 Observation Walk			OTTAWA-CARLETON	HUNTLEY TOWNSHIP			3257 CARP	OTTAWA **	420024	5019172 SAND WATER READING	GREY		1 2	4 m
		4.1										ROAD 3275 CARP							-
/035379	28-Jul-06	3.8	0	0	11760829			UTTAWA-CARLETON	HUNILEY TOWNSHIP			ROAD	1	8 420944	5019366 TOPSOIL,LOOSE,	BROWN		u 1.2	2 m
7035379	28-Jul-06	3.8	0	0	11760829			OTTAWA-CARLETON	HUNTLEY TOWINSHIP			3275 CARP ROAD	1	8 420944	5019366 SAND,SILT,	BROWN	1.3	2 3.6	ó m
7035379	28-14.04	3.8	0	0	11760829			OTTAWA-CARLETON	HUNTLEY TOWNSHIP			3275 CARP		440004 8	5019366 CLAY, SILT WATER, READING	GREY	• •	6 00	1 m
7127229	15.kn.00			0	1002636945 Test Hele	Monitorina		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	ROAD CARP AJRPORT	Ottama	a 410327	5019365 TOPSOIL.	BROWN	71	0 0	1 m
7127229	15-Jun-09	0	ō	0	1002636945 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWINSHIP	03	015	CARP AIRPORT	Ottana 1	8 419327	5019365 COARSE SAND, GRAVEL,	GREY	0.	1 1.	8 m
7127229	15-Jun-09 15-Jun-09	0	0	0	1002636945 Test Hole 1003636945 Test Hole	Monitoring		OTTAWA-CARLETON OTTAWA-CARLETON	HUNTLEY TOWISHIP	03	015	CARP AIRPORT	Ottawa 11 Ottawa 11	8 419327	5019365 ROCK,SAND,GRAVEL 5019365 SAND GRAVEL ROCK	GREY	1.	8 2	5 m
7127229	15-Jun-09	0	ŏ	0	1002636945 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWISHIP	03	015	CARP AIRPORT	Ottawa 1	8 419327	5019365 SILT, CLAY, SAND	GREY	2	8 3	6 m
7127229	15-Jun-09 15-Jun-09	0	0	0	1002810625 Test Hole 1002810634 Test Hole	Monitoring		OTTAWA-CARLETON OTTAWA-CARLETON	HUNTLEY TOWISHIP	03	015	CARP AIRPORT	Ottawa 11 Ottawa 11	8 420325	5019185				
7127229	15-Jun-09	0	ŏ	0	1002810643 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWISHIP	03	015	CARP AIRPORT	Ottawa 1	8 420387	5019350				
7127229	15-Jun-09	0	0	0	1002810652 Test Hole 1002810661 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 11 Ottawa 11	8 420393	5019349				
7127229	15-Jun-09	0	ŏ	0	1002810670 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWISHIP	03	015	CARP AIRPORT	Ottawa 1	8 420305	5019419				
7127229	15-Jun-09	0	0	0	1002810679 Test Hole 1002810699 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana 11 Ottana 11	8 420340	5019336				
7127229	15-Jun-09	0	0	0	1002810697 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana 1	8 420380	5019368				
7127229	15-Jun-09	0	0	0	1002636945 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	63	015	CARP AIRPORT	Ottana 1	8 419327	5019365 TOPSOIL,	BROWN		0 0.	1 m
7127229	15-Jun-09	0	0	0	1002636945 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	63	015	CARP AIRPORT	Ottana 1	8 419327	5019365 ROCK,SAND,GRAVEL	GREY	1.	8 2	5 m
7127229	15-Jun-09	0	0	0	1002636945 Test Hole 1003636945 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana 11 Ottana 11	8 419327	5019365 SAND,GRAVEL,ROCK	GREY	2	5 2	8 m
7127229	15-Jun-09	0	ŏ	0	1002810625 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWISHIP	03	015	CARP AIRPORT	Ottawa 1	8 420325	5019185	CPL I		u	2 m
7127229	15-Jun-09	0	0	0	1002810634 Test Hole 1002810642 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 11	8 420323	5019178				
7127229	15-Jun-09	0	ō	0	1002810652 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWISHIP	63	015	CARP AIRPORT	Ottawa 1	8 420393	5019349				
7127229	15-Jun-09	0	0	0	1002810661 Test Hole 1002810630 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 11	8 420400	5019342				
7127229	15-Jun-09	0	ŏ	0	1002810679 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	63	015	CARP AIRPORT	Ottana 1	8 420340	5019336				
7127229	15-Jun-09 15-Jun-09	0	0	0	1002810688 Test Hole 1002810697 Test Hole	Monitoring		OTTAWA-CARLETON OTTAWA-CARLETON	HUNTLEY TOWISHIP	03	015	CARP AIRPORT	Ottawa 11 Ottawa 11	8 420316 8 420390	5019348 5019348				
7127229	15-Jun-09	0	0	0	1002636945 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	63	015	CARP AIRPORT	Ottawa 1	8 419327	5019365 TOPSOIL,	BROWN		0 0.	1 m
7127229	15-Jun-09 15-Jun-09	0	0	0	1002636945 Test Hole 1003636945 Test Hole	Monitoring		OTTAWA-CARLETON OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 11 Ottawa 11	8 419327	5019365 COARSE SAND, GRAVEL, 5019365 DOCK SAND GRAVEL	GREY	0.	1 1.	8 m 5 m
7127229	15-Jun-09	0	0	0	1002636945 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWINSHIP	03	015	CARP AIRPORT	Ottawa 1	8 419327	5019365 SAND, GRAVEL, ROCK	GREY	2	5 2	8 m
7127229	15-Jun-09 15-Jun-09	0	0	0	1002636945 Test Hole 1002810625 Test Hole	Monitoring		OTTAWA-CARLETON OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 11 Ottawa 11	8 419327	5019365 SILT, CLAY, SAND 5019185	GREY	2	8 3.	6 m
7127229	15-Jun-09	0	0	0	1002810634 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana 1	8 420323	5019178				
7127229	15-Jun-09 15-Jun-09	0	0	0	1002810543 Test Hole 1002810552 Test Hole	Monitoring		OTTAWA-CARLETON OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana 1 Ottana 1	8 420387	5019349				
7127229	15-Jun-09	0	0	0	1002810661 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 1	8 420400	5019342				
7127229	15-Jun-09 15-Jun-09	0	0	0	1002810679 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana 1	420305 8 420340	5019336				
7127229	15-Jun-09	0	0	0	1002810688 TestHole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 1	8 420316	5019348				
7127229	15-Jun-09 15-Jun-09	0	0	0	1002636945 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana 1	a 420,990 8 419327	5019365 TOPSOIL,	BROWN		0 0.	1 m
7127229	15-Jun-09	0	0	0	1002636945 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 1	8 419327	5019365 COARSE SAND, GRAVEL,	GREY	0.	1 1.	8 m
7127229	15-Jun-09 15-Jun-09	0	0	0	1002636945 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottama 1	419327 8 419327	5019365 SAND,GRAVEL ROCK	GREY	1.	5 2	8 m
7127229	15-Jun-09	0	0	0	1002636945 Test Hole 1002810626 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 1	8 419327	5019365 SILT, CLAY, SAND	GREY	2	8 3.	6 m
7127229	15-Jun-09	0	ŏ	0	1002810634 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 1	8 420323	5019178				
7127229 7127229	15-Jun-09 15-Jun-09	0	0	0	1002810643 Test Hole 1002810652 Test Hole	Monitoring		OTTAWA-CARLETON OTTAWA-CARLETON	HUNTLEY TOWISHIP HUNTLEY TOWISHIP	03	015	CARP AIRPORT	Ottana 11 Ottana 11	8 420387 8 420393	5019350 5019349				
7127229	15-Jun-09	0	0	0	1002810661 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 1	8 420400	5019342				
r127229 7127229	15-Jun-09 15-Jun-09	0	0	0	1002810670 Test Hole 1002810679 Test Hole	Monitoring		OTTAWA-CARLETON OTTAWA-CARLETON	HUNTLEY FOWNSHIP HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana 1 Ottana 1	8 420305 8 420340	5019336				
7127229	15-Jun-09	0	0	0	1002810688 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 1	8 420316	5019348				
7127229	15-Jun-09 15-Jun-09	0	0	0	1002636945 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottama 11	a 420380 8 419327	5019365 TOPSOIL,	BROWN		0 0.	1 m
7127229	15-Jun-09	0	0	0	1002636945 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 1	8 419327	5019365 COARSE SAND, GRAVEL,	GREY	0	1 1.	8 m
7127229	15-Jun-09 15-Jun-09	0	0	0	1002636945 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottama 1	8 419327	5019365 SAND,GRAVELROCK	GREY	1.	5 2	8 m
7127229	15-Jun-09	0	0	0	1002636945 Test Hole 1002810625 Test Hole	Monitoring Monitorion		OTTAWA-CARLETON OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottama 11 Ottama	8 419327	5019365 SILT, CLAY, SAND 5019185	GREY	2	8 3	6 m
7127229	15-Jun-09	0	ŏ	0	1002810634 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 1	8 420323	5019178				
7127229	15-Jun-09	0	0	0	1002810643 Test Hole 1002810652 Test Hole	Monitoring Monitorion		OTTAWA-CARLETON OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottama 11 Ottama	8 420387	5019350 5019349				
7127229	15-Jun-09	0	ő	0	1002810661 TestHole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 1	8 420393	5019342				
7127229	15-Jun-09	0	0	0	1002810670 Test Hole 1002810679 Test Hole	Monitoring		OTTAWA-CARLETON OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 11 Ottawa	8 420305	5019419				
7127229	15-Jun-09	0	ō	0	1002810688 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWINSHIP	03	015	CARP AIRPORT	Ottana 1	8 420316	5019348				
7127229	15-Jun-09 16-km.09	0	0	0	1002810697 Test Hole 1002636945 Test Hole	Monitoring Monitoring		OTTAWA-CARLETON OTTAWA-CARLETON	HUNTLEY TOWNSHIP HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana 11 Ottana 44	8 420380 8 419377	5019368 5019365 TOPSOIL	BROWN		0	1 m
7127229	16-Jun-09	0	0	0	1002636945 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana 1	8 419327	5019365 COARSE SAND, GRAVEL,	GREY	0.	1 1.	8 m
r127229 7127229	16-Jun-09 16-Jun-09	0	0	0	1002636945 Test Hole 1002636945 Test Hole	Monitoring		OTTAWA-CARLETON OTTAWA-CARLETON	HUNTLEY TOWNSHIP HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana 11 Ottana 11	8 419327 8 419327	5019365 ROCK, SAND, GRAVEL 5019365 SAND, GRAVEL ROCK	GREY	1.	8 2. 5 2	5 m 8 m
7127229	16-Jun-09	0	0	0	1002636945 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 1	8 419327	5019365 SILT, CLAY, SAND	GREY	2	8 3.	6 m
7127229	16-Jun-09 16-Jun-09	0	0	0	1002610625 TestHole 1002810634 TestHole	munitoring Monitoring		OTTAWA-CARLETON OTTAWA-CARLETON	HUNTLEY TOWISHIP	uts 03	015	CARP AIRPORT	Ottana 1	a 420325 8 420323	5019178				
7127229	16-Jun-09	0	0	0	1002810643 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 1	8 420387	5019350				
7127229	16-Jun-09	0	0	0	1002810661 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana 1	8 420393	5019342				
7127229	16-Jun-09	0	0	0	1002810670 Test Hole 1002810679 Test Hole	Monitoring		OTTAWA-CARLETON OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana 11 Ottana	8 420305	5019419 5019336				
7127229	16-Jun-09	0	0	0	1002810688 TestHole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana 1	8 420340 8 420316	5019348				
7127229	16-Jun-09	0	0	0	1002810697 Test Hole 1003624045 Tost Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 1	8 420380	5019368	PDOM N		0	1 m
7127229	16-Jun-09	0	0	0	1002636945 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottama 1	419327 8 419327	5019365 COARSE SAND, GRAVEL,	GREY	0	1 1.	8 m
7127229	16-Jun-09	0	0	0	1002636945 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 1	8 419327	5019365 ROCK,SAND,GRAVEL	GREY	1	8 2	5 m
7127229	16-Jun-09	0	ŏ	0	1002636945 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 1	8 419327	5019365 SILT, CLAY, SAND	GREY	2	8 3.	6 m
7127229	16-Jun-09	0	0	0	1002810625 Test Hole 1002810624 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa 1	8 420325	5019185				
7127229	16-Jun-09	0	0	0	1002810643 Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottama 1	a 420323 8 420387	5019350				
7127229	16-Jun-09	0	0	0	1002810652 TestHole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottama 1	8 420393	5019349				

7127229	16-Jun-09	0		0	0	1002810661	Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana	18	420400	5019342				
7127229	16-Jun-09	0		0	0	1002810670	Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa	18	420305	5019419				
7127229	16-Jun-09	0		0	0	1002810679	Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana	18	420340	5019336				
7127229	16-Jun-09	0		0	0	1002810688	Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottama	18	420316	5019348				
7127229	16.km.09	0		0	0	1002810697	Test Hole	Monitorina		OTTAWA_CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa	18	420380	5019368				
7127229	16.km.09	0		0	0	1003636945	Test Hole	Monitorina		OTTAWA_CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa	18	419327	5019365 TOPSOIL	BROWN	0	0.1	m
7122220	16 km 00	0		0	0	10036240.45	Torthisis	Monitoriaa		OTTAMA CAR FTON	HINTICY TOWNSHIP	02	015	CADD A IDDODT	Ottawa	10	#10227	ED1024E COAREE SAND CRAVEL	CREV	0.1	1.0	an.
7127229	16-km.09	0		0	0	1003636945	TestHole	Monitorina		OTTAWA_CARLETON	HINTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana	18	419327	5019365 POCK SAND CRAVEL	CREY	18	25	m
7127220	16 kp 09	0		0	0	1003636045	Tortkiele	Monitoring		OTTAINS CARLETON	NUMBER TOWNSHIP	03	015	CARD AIRPORT	Ottama	10	410227	5010365 CAND CRAVEL DOCK	CREV	26	2.2	
7107220	16-341-09	0		*	0	1002030943	Testilais	Marihadaa		OTTAINS CARLETON	IN ACTION TO MAKE IN	60	013	CADD AND ORT	Otterna	10	410007	CONDUCT FUT CLAN CAND	CODY	2.3	2.0	
7127229	16-341-09	0		0	0	1002630945	Testilia	Monitoring		OTTAINA-CARLETON	HUNTLET TOWNSHIP	03	015	CARP AIRPORT	Ottana	10	419327	SUTVSIS SILT, CAT, SAND	UNET	2.8	3.8	
/12/229	16-Jun-09	0		0	0	1002810625	Testhole	Montoring		OTTAWA-CAMETON	HUNTLEYTOWNSHIP	03	015	CARPAINPORT	Ottania	18	420325	5019185				
/12/229	16-Jun-09	0		0	0	1002810634	TestHole	Montoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARPAINPORT	Ottavia	18	420323	501V178				
7127229	16-Jun-09	0		0	0	1002810643	TestHole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana	18	420387	5019350				
7127229	16-Jun-09	0		0	0	1002810652	TestHale	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana	18	420393	5019349				
7127229	16-Jun-09	0		0	0	1002810551	Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottania	18	420400	5019342				
7127229	16-Jun-09	0		0	0	1002810670	TestHale	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana	18	420305	5019419				
7127229	16-Jun-09	0		0	0	1002810679	TestHole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana	18	420340	5019336				
7127229	16-Jun-09	0		0	0	1002810688	Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottama	18	420316	5019348				
7127229	16-Jun-09	0		0	0	1002810697	TestHole	Monitorina		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana	18	420380	5019368				
7127229	16-km.09	0		0	0	1003636945	Test Hole	Monitorina		OTTAWA_CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa	18	419327	5019365 TOPSOIL	BROWN	0	0.1	m
7127229	16.km.09	0		0	0	1003636945	TestHole	Monitorina		OTTAWA_CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottawa	18	419327	5019345 COARSE SAND CRAVEL	CREY	0.1	18	m
7127220	16 kp 09	0		0	0	1003636045	Tortkiele	Monitoring		OTTAINS CARLETON	NUMBER TOWNSHIP	03	015	CARD AIRPORT	Ottama	10	410227	5010365 DOCK SAND CRAVEL	CREV	1.0	26	
7107220	16-341-09	0		*	0	1002030943	Testilais	Marihadaa		OTTAINS CARLETON	IN ACTION TO MAKE IN	60	013	CADD AND ORT	Otterna	10	410007	CONDUCT CAND CONNEL DOOR	CODY	1.4	2.3	
1127229	10-301-09	0		0	U	1002636945	TestPole	Montoring		DTIAWA-CARETON	HUNILET TOWNSHIP	03	015	CARP AIRPORT	Ottanta	10	419327	SU19365 SAND, GRAVEL, RUCK	GIET	2.5	2.8	
/12/229	16-Jun-09	0		0	0	1002638945	TestHale	Montoring		OTTAWA-CAMETON	HUNTLEYTOWNSHIP	03	015	CARPAINPORT	Ottania	18	419327	5019365 SILI, CLAY, SAND	CAEY	2.8	3.6	m
/12/229	16-Jun-09	0		0	0	1002810625	TestHole	Montoring		OTTAWA-CARETON	HUNTLEY TOWNSHIP	03	015	CARPAINPORT	Ottavia	18	420325	501V185				
7127229	16-Jun-09	0		0	0	1002810634	TestHale	Monitoring		OTTAWA-CARLETON	HUNTLEYTOWNSHIP	63	015	CARP AIRPORT	Ottania	18	420323	5019178				
7127229	16-Jun-09	0		0	0	1002810643	TestHale	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana	18	420387	5019350				
7127229	16-Jun-09	0		0	0	1002810652	Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottania	18	420393	5019349				
7127229	16-Jun-09	0		0	0	1002810661	TestHale	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana	18	420400	5019342				
7127229	16-Jun-09	0		0	0	1002810670	Test Hole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottama	18	420305	5019419				
7127229	16-Jun-09	0		0	0	1002810679	TestHole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottama	18	420340	5019336				
7127229	16-Jun-09	0		0	0	1002810688	TestHole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana	18	420316	5019348				
7127229	16-Jun-09	0		0	0	1002810697	TestHole	Monitoring		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	015	CARP AIRPORT	Ottana	18	420380	5019368				
7199876	20.Mar.13	48.8		19	0	1004271965	Water Sunnly	Commerical		OTTAWA_CAR FTON	HUNTLEY TOWNSHIP			3155 CARP RO	CA99	18	421059	5019065 CRAVE	BROWN	0	1	n
7199876	20.Mar.13	48.8		19	0	1004271965	Water Surrely	Commerical		OTTAWA_CAR FTON	HUNTLEY TOWNSHIP			3155 CARP RO	CASP	18	421059	5019065 SAND MEDILIM-CRAINED	BROWN	1	15.5	0
7100976	20 Mar 12	40.0		1.0	0	1004271965	Water Supply	Commonical		OTTAINS CARLETON	NUMBER TOWNSHIP			2155 CARD RD	CA99	10	421059	SOTIONS SAND CRAVEL	COEV	3.31	14.6	n fr
7100070	2010/01/12	40.0			0	1004271942	Winter County	Commission		OTTAINS CARLETON	IN ACTION TO MAKE IN			2122 0400 000	0400	10	424050	CONDUCT CLUBIC	0001881	44.5	2015	n 9
7100070	2010/01/12	40.0			0	1004271942	Winter County	Commission		OTTAINS CARLETON	IN ACTION TO MAKE IN			2122 0400 000	0400	10	424050	CONCOUR LIBERTOOK	CODY	10.3	100	n 9
1104010	20-00.02-13	40.0		1.7	U	1004271985	water suppry	CONTINUE		DTIAWA-CARETON	HUNILET TOWNSHIP			3155 CM0-90	CARP.	10	421009	SUIVUSS LINESTONE,	CAE 1	20.5	180	
1205511	05-Jun-13	48.8		1.1	0	1004473562	Water Suppry	Domestic	Test Hole	OTTAWA-CAMETON	HUNTLEYTOWNSHIP	03	012	311V CARP NO	CAMP	18	420965	5018977 SAND,	HED	8	5	п -
1205511	05-Jun-13	48.8		1.1	0	1004473562	Water Suppry	Domestic	Lest Hole	OTTAWA-CARETON	HUNTLEY TOWNSHIP	03	012	3119 CARP NO	CANP	18	420965	5018977 SAND,	BROWN	5	14	п
7205577	05-Jun-13	48.8		1.1	0	1004473562	Water Supply	Domestic	Test Hole	OTTAWA-CARLETON	HUNTLEYTOWNSHIP	63	012	3119 CARP RD	CARP	18	420965	5018977 SAND,,	CREY	14	48.5	n
7205577	05-Jun-13	48.8		1.1	0	1004473562	Water Supply	Domestic	Test Hole	OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	012	3119 CARP RD	CARP	18	420965	5018977 LIMESTONE,,	GREY	48.5	160	ft
7279014	08-Oct-13	0		0	0	1006332325				OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	013			18	420326	5019170				
7279016	08-Nov-13	0		0	0	1006332655				OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	013			18	420326	5019172				
7279017	08-Nov-13	0		0	0	1006332664				OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	013			18	420336	5019172				
														1500 THOMAS								
7290463	25-May-17	33		0	0	1006626009	Abandoned-Other			OTTAWA-CARLETON	HUNTLEY TOWNSHIP			ARGUE RD (Ottana	18	420316	5019183 UNKNOWN TYPE.		0	33	m
														CARP AIRPORT								
														1500 THOMAS								
7290426	25-May-17	0		0	0	1006629284	Abandoned-Other			OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	013	100011101000	Ottania	18	420284	5019320				
														ABULLE RU								
7290427	25-May-17	0		0	0	1006629297	Abandoned-Other			OTTAWA-CARLETON	HUNTLEY TOWNSHIP			1500 1110/045	Ottama	18	420316	5019195				
														ANGUE ND								
7336858	24-May-19	48.8		0	0	1007516881	Water Supply	Domestic		OTTAWA-CARLETON	HUNTLEY TOWNSHIP			RUSS BRADLEY	CARP	18	420491	5019311 CLAY.		0	136	ft.
														AIRPORT								
7234459	24 84 74 10	40.0			0	1007514991	Winter Supply	Domostic		OTTAWA CAR FTON	HINTICY TOWNSHIP			RUSS BRADLEY	CA99	10	430401	ED10211 LIMESTONE	CREV	124	160	
12.302.30	244may-10	40.0		~		1007310021	reason papers	DOTINETS.		UTININ CALL TON	Indenter FORMULT			AIRPORT	Course .	10	120171	JUTITITIE ENGLATORIE,	CPL I	120	130	
2004050		10.0				1003741024	Winter County	0		OTTAINS ON CTON	10.000000000000000000000000000000000000			RUSS BRADLEY	0400	40	420.404	CALORINE UN AFETTORY	0000	470	4/0	
1230008	24-May-19	48.8		0	0	100/516881	water and he	DOTINISUE		OT DAMA-CARETON	HUNLET TOWNSHIP			AIRPORT	CARP.	18	420491	SUIVATT LIMESTORE,	CART	150	160	
														1550 THOMAS								
7364122	26-Jun-20	54.9	1	3.7	0	1008415608	Water Supply	Domestic		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	013	ARQUE ROAD	CARP	18	420574	5019292 CLAY,,	GREY	0	158	n
														1550 THOMAS								
7364122	26-Jun-20	54.9		3.7	0	1008415608	Water Supply	Domestic		OTTAWA-CARLETON	HUNTLEY TOWNSHIP	03	013	ABOLIE ROAD	CARP	18	420574	5019292 SHALE,LIMESTONE,	GREY	158	180	ft
2222214	01.1x0.20	0		0	0	1009507940				OTTAMA CARLETON	NUMBER TO MAKE					10	430207	6010402				
141419	04-381-20	0		W .	0	100000/040				INTERPORT NUMBER OF A	I DATE AND I STREET					10	740307	where a strategy of the second s				

1000	0014045770	14511 05071 (m) (TATIO 1417	TO 10/0 (m)	0.0000000000	0005 1101		11664	11000	C40700	0007000	0.05 10 01040 7777	CUL COLLO ATC	CLOUDING DATE:	0000010170	WHAT O CTATE ACTO TOT	000000000	RUN POINC DUP LTION AD
WELL_ID	COMPLETED	WELL DEPTH (m) STATIC WAT	IERCEVEL (m) DEPTH TO	D REDHOCK (m)	BOKE_HUI	E_IU FINALSTATUS	0.000	0522	EASTES	NUMETHES	MPE_ID PUMP TEST	PUMPINGRAIE	HOWINGRAIE	RECOMINATE	WATER STATE AFTER TEST	PUMP METHOD	POMPING DURATION (h)
1503071	30-349-67	61	15.2	41.1	10	225114 Water Suppry	Damenta		420630.5	5019702	105/3004 50,50,6011	0.0044		50010	0.540	PUMP	18
1503129	14-JUI-05 37 Jun 40	57	6.5	40.3	10	125172 Water Supply	Logistical .	Intraction	420700.5	5019542	105/3742 20,45,11	3 GPM		200004	CLEAR	PLMP	15
1510130	12 5/6 75	52.2	*.0	39.9	10	132100 Water Supply	Domostic	ingation	420600.5	5010162	10500730 32,165,17011	25 GPM		20GPM	CLEAR	POMP	25
1514573	13-P4D-75	52.5	2.2	37.5	10	236346 Water Suppry	Damenta		420433.5	5019162	10365116 18,30,7011	2010974		SUPPI CORM	0.540	DAILER	28
1510020	01-NEV-76	44.2	12.2	10.7	10	136723 Water Suppry	Damenta		420630.5	5019422	10367293 40,33,6011	25 0 PM		50070	CLEAR CLEAR	PUMP	18
1517607	20.500.04	42.0	24	24.1	11	120031 Water Suppry	Notiked		420424.5	5019321	110000131 0,200,20010	4 GPM		464701	LIEAR	Pawp	18
1535787	20.Sep.05	27.4	5.0	0	11	16926 Water Sunnly	Municipal	Public	420813	5019053	11331181 5.91 m	160.11PM		IPM	CLEAR	PIMP	h
1536752	10,04,05	37	0	0	11	91846 Observation Welk			420326	5019172	11696712						h
20353.79	28.04.05	3.8		0	11	360829			420944	5019366	11368519						h
7127229	15.3m.09	0	0	0	1002	K36045 Test Hole	Monitorina		410327	5019365	1002810706						h
7127229	15 km 00	0		0	1003	Page 25 Test Hole	Monitoring		430225	5010303	1002010/00						h
7127229	15.km/09	0		0	1000	R10634 Test Hole	Monitoring		420323	5019178	1002810639						h
7127229	15.km/09	0		0	1000	R10643 Test Hole	Monitoring		420387	5019350	1002810648						h
7127229	15.km/09	0		0	1000	k10652 Test Hole	Monitoring		420393	5019349	1002810457						h
7127229	15.km/09	0		0	1000	R10661 Test Hole	Monitoring		420400	5019342	1002810666						h
7127229	15.km/09	0		0	1000	k10620 Test Hole	Monitoring		420305	5019419	1002810625						h
7127229	15.km/09	0		0	1000	k10679 Test Hole	Monitoring		420340	5019336	1002810684						h
7127229	15.km/09	0		0	1000	R10688 Test Hole	Monitoring		420316	5019348	1002810493						h
7127229	15.km/09	0		0	1000	k10697 Test Hole	Monitoring		420380	5019368	1002810202						h
7127229	15-Jun-09	0	0	0	1002	536945 Test Hole	Monitoring		419327	5019365	1002810706						h
7127229	15-Jun-09	0	0	0	1002	B10625 Test Hole	Monitoring		420325	5019185	1002810630						h
7127229	15-Jun-09	0	0	0	1002	B10634 Test Hole	Monitoring		420323	5019178	1002810639						h
7127229	15-Jun-09	0	0	0	1002	B10643 Test Hole	Monitoring		420387	5019350	1002810548						h
7127229	15-Jun-09	0	0	0	1002	B10652 Test Hole	Monitoring		420393	5019349	1002810657						h
7127229	15-Jun-09	0	0	0	1002	B10661 Test Hole	Monitoring		420400	5019342	1002810666						h
7127229	15-Jun-09	0	0	0	1002	B10670 Test Hole	Monitoring		420305	5019419	1002810675						h
7127229	15-Jun-09	0	0	0	1002	B10679 Test Hole	Monitoring		420340	5019336	1002810684						h
7127229	15-Jun-09	0	0	0	1002	B10688 Test Hole	Monitoring		420316	5019348	1002810693						h
7127229	15-Jun-09	0	0	0	1002	B10697 Test Hole	Monitoring		420380	5019368	1002810702						h
7127229	15-Jun-09	0	0	0	1003	636945 Test Hole	Monitoring		419327	5019365	1002810706						h
7127229	15-Jun-09	0	0	0	1003	B10625 Test Hole	Monitoring		420325	5019185	1002810630						h
7127229	15-Jun-09	0	0	0	1003	B10634 Test Hole	Monitoring		420323	5019178	1002810639						h
7127229	15-Jun-09	0	0	0	1003	B10643 Test Hole	Monitoring		420387	5019350	1002810648						h
7127229	15-Jun-09	0	0	0	1003	B10652 Test Hole	Monitoring		420393	5019349	1002810657						h
7127229	15-Jun-09	0	0	0	1003	B10661 Test Hole	Monitoring		420400	5019342	1002810666						h
7127229	15-Jun-09	0	0	0	1003	B10670 Test Hole	Monitoring		420305	5019419	1002810675						h
7127229	15-Jun-09	0	0	0	1003	B10679 Test Hole	Monitoring		420340	5019336	1002810684						h
7127229	15-Jun-09	0	0	0	1003	B10688 Test Hole	Monitoring		420316	5019348	1002810693						h
7127229	15-Jun-09	0	0	0	1003	B10697 Test Hole	Monitoring		420380	5019368	1002810702						h
7127229	15-Jun-09	0	0	0	1003	636945 Test Hole	Monitoring		419327	5019365	1002810706						h
7127229	15-Jun-09	0	0	0	1003	B10625 Test Hole	Monitoring		420325	5019185	1002810630						h
7127229	15-Jun-09	0	0	0	1003	B10634 Test Hole	Monitoring		420323	5019178	1002810639						h
7127229	15-Jun-09	0	0	0	1003	B10643 Test Hole	Monitoring		420387	5019350	1002810648						h
7127229	15-Jun-09	0	0	0	1003	B10652 Test Hole	Monitoring		420393	5019349	1002810657						h
7127229	15-Jun-09	0	0	0	1003	B10661 Test Hole	Monitoring		420400	5019342	1002810666						h
7127229	15-Jun-09	0	0	0	1003	B10670 Test Hole	Monitoring		420305	5019419	1002810675						h
7127229	15-Jun-09	0	0	0	1003	B10679 Test Hole	Monitoring		420340	5019336	1002810684						h
7127229	15-Jun-09	0	0	0	1003	B10688 Test Hole	Monitoring		420316	5019348	1002810693						h
7127229	15-Jun-09	0	0	0	1003	B106/97 Test Hole	Monitoring		420380	5019368	1002810702						h
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7127229	15-Jun-09	0	0	0	1003	B10697 Test Hole	Monitoring		420380	5019368	1002810702						h
7127229	16-Jun-09	0	0	0	1003	636945 Test Hole	Monitoring		419327	5019365	1002810706						h
7127229	16-Jun-09	0	0	0	1003	B10625 Test Hole	Monitoring		420325	5019185	1002810630						h
7127229	16-Jun-09	0	0	0	1003	B10634 Test Hole	Monitoring		420323	5019178	1002810639						h
7127229	16-Jun-09	0	0	0	1003	B10643 Test Hole	Monitoring		420387	5019350	1002810648						h
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7127229	16-Jun-09	0	0	0	1003	PROFESSION	Monitoring		420340	JU19330	5002250402						
7127229	16-Jun-09	0	0	0	1003	Process HOLDEN	Monitoring		420310	5010340	5003950303						
7127229	16-Jun-09	0	0	0	1003	ETABLE Torthink	Monitoring		420300	JU19300	5003250304						
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7127229	16-Jun-09	9	0	0	1003	B10652 Test Hole	Monitoring		420393	5019349	1002810657						h
7127229	16-Jun-09	9	0	0	1003	B10661 Test Hole	Monitoring		420400	5019342	1002810666						h
7127229	16-Jun-09	9	0	0	1003	B10670 Test Hole	Monitoring		420305	5019419	1002810675						h
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7127229	16-Jun-09	0	0	0	1003	B10688 Test Hole	Monitoring		420316	5019348	1002810693						h
7127229	16-Jun-09	0	0	0	1003	B10697 Test Hole	Monitoring		420380	5019368	1002810702						h
7199876	20-Mar-13	48.8	4.9	0	1004	271965 Water Supply	Commerical		421059	5019065	1004797174 16.07,37.89,150 ft	5 GPM		7GPM	OTHER		8h
7205577	05-Jun-13	48.8	1.1	0	1004	473562 Water Supply	Domestic	TestHale	420965	5018977	1004889467 3.66,42.48,150 ft	12 GPM		12GPM	CLEAR		1h
7290463	25-May-17	33	0	0	1008	526009 Abendoned-Other			420316	5019183	1006694088						h
7290426	25-May-17	0	0	0	1008	529284 Abendoned-Other			420284	5019320	1006691800						h
7290427	25-May-17	0	0	0	1008	629297 Abendoned-Other			420316	5019195	1006691807						h
7336858	24-May-19	48.8	0	0	1007	516881 Water Supply	Domestic		420491	5019311	1008002295 ,113,150 ft	20 GPM		20GPM			1h
7364122	26-Jun-20	54.9	87	0	1006	HIGHOR Minter Superior	Deservatio		430674	6010202	1009499117 19 E92 34 323 100 M	20.0564		2000044			16



APPENDIX B: WELL RECORD (TW1)

MCINTOSH PERRY

CERTIFICATE OF WELL COMPLIANCE



I (Jeremy Hanna) AIR ROCK DRILLING CO. LTD. - DO HEREBY CERTIFY

that I am licensed to drill water wells in the Province of Ontario, and that I have

supervised the drilling of the water well on the property of :	Tranc
OWNER: 2852569 ONTARIO NC	(Watkins)
Location: 273-275 Russ BRADLEY ROAD) Carp
LOT: Black don: -16 PLAN # 4R-1511 SIL #	\times
Ottawa-Carleton / Geographical Township of MARCH	

I CERTIFY FURTHER that, I am aware of the well drilling requirements, the guidelines, recommendations and regulations of the Ministry of the Environment governing well installations in the Province of Ontario, and the standards specified in any subdivision agreement and hydrogeological report applicable to this site and City Standards.

AND DO HEREBY CERTIFY THAT the said well has been drilled, cased, grouted (cement or bentonite) as applicable and constructed in strict conformity with the standards required.

Signed this	STH	Day of	JU	LY	, 2, 22
• -					

Jeremy Hanna (T3632)

Air Rock Drilling Co. Ltd. (<u>C-7681</u>)

The Engineer on behalf of the Landowner set out above, Certifies that he/she has inspected the well and it was constructed in accordance with the specifications in O.Reg 903, this report and the Hydrogeological Report with regards to casing length and grouting requirements.

Signed this da	y of August		2022	
Mayle	AL GEOSCIER		TAGA	22464 342436
(Engineer)	MEGHAN E. COYLE	·····		
Shaping our future together Ensemble, formons notre avenir	4-Aug-22 2831 MC Gity of Ortawa WTAR Client Service Centre 2043 Virtoria Street	Ville d'Ottawa Centre de service 8243, nue Victoria	€: ≪⊷≫	

Measurements r	ecorded in:	Metric Mimperi	al					Page		of
Well Owner's	Information	/N					1012		a second	
First Name		Last Name/Organiz	ation	o inc. CIO Trevor	E-mail Address	3] Well	Constru
Mailing Address (Street Number/Na	2002.30 ame)	Ja Villani	Municipality	Province	Postal Code	e	Telephone I	No. (inc.	area co
971 Mel	rose Road			Shannonville	ON	KOK	3A0			
Well Location				17	6 7	TP -4		0		t in the
Address of Well Li 273-275	Russ Brac	diey Road		March	f	10ck 15-1	16	Concession	1	
County/District/Mu	unicipality	/		City/Town/Village		1745	Provin	nce	Posta	I Code
UILd Wd	Zone Easting	Northing		Municipal Plan and Sublot	Number		Other	4110		
NAD 8 3	18 420	743 501	9433	4R-18	511					
Overburden and	d Bedrock Mate	rials/Abandonmen	t Sealing Red	cord (see instructions on the	back of this form)		1. j. s.			
General Colour	Most Con	nmon Material	0	Other Materials	Ger	neral Description	n		From	
Blue		Clay	Mixed	& W/ Gravei					0	130
Grey & Bla	CK .	Limestone					_		138	200
Grey & Bla	CK	Limestone							200	500
										_
		Annular Space)			Results of W	ell Yield	d Testing	and an and a second	
Depth Set at (m From To		Type of Sealant Us (Material and Type)	Volume Placed	After test of well yield	, water was: free	Time	aw Down Water Level	Time	ecovery Water L
142 13	2' Neat c	rement		12.48	Other, specify	Not teste	(min)	(m/ft)	(min)	(m/ft
132 0	Bento	nite slurry		29.4	If pumping discontinu	ied, give reason:	Level	3314		130
					\sim		1 1	30.0	1	14
							-		1	
					Pump intake set at (n 300	n/ft)	2	39.7	2	14
					Pump intake set at (n 300 Pumping rate (V min/1	n/ft) OFM()	2	39.7 42.8	2	14 13
Method of	Construction	d Public	Well U	se Not used	Pump intake set at (n 300 Pumping rate (Uming to 5 US	n/ft) ORM()	2 3 4	39.7 42.8 45.6	2 3 4	14 13 13
Method of Cable Tool Rotary (Conventio	Construction	d Bublic Domestic	Well U	Se	Pump intake set at (m 300 Pumping rate (Vmin/4 5 US Duration of pumping 1 hrs +	n/ft) GRM) min	2 3 4 5	39.7 42.8 45.6 48.4	2 3 4 5	14 13 13 13
Method of Cable Tool Rotary (Convention Rotary (Reverse) Booling	Construction Diamon	d Bublic Domestic Livestock Irrigation	Well U Comme Municip Test Ho Cooling	se ercial Not used pal Dewatering be Monitoring & Air Conditioning	Pump intake set at (n 300 Pumping rate (<i>Iminife</i> 2005 Duration of pumping 1 hrs + 0 Final water level and of	n/ft) SRM) min of pumping (m/ft)	2 3 4 5	39.7 42.8 45.6 48.4 63.2	2 3 4 5	14 13 13 13 13 12
Method of Cable Tool Rotary (Convention Rotary (Reverse) Joong Air percussion Other, specify	Construction	d Bublic Domestic Livestock Infigation Other, spec	Well U	se ercial Not used >al Dewatering ble Monitoring a Air Conditioning	Pump intake set at (n 300 Pumping rate (<i>Iminff</i> 5 US Duration of pumping <u>1</u> hrs + <u>0</u> Final water level end of	n/ft) OFM() min of pumping (m/ft)	2 3 4 5 10	39.7 42.8 45.6 48.4 63.2 77.3	2 3 4 5 10	14 13 13 13 13 12 12
Method of Cable Tool Rotary (Conventio Rotary (Reverse) Boling Air percussion Her, specify	Construction Diamon- Diamon- Diamon- Diging Digging Digging Construction R	d Public Domestic Livestock Irrigation Other, spec	Well U Comm Municip Test Ho Cooling	Se ercial Not used pal Dewatering ole Monitoring & Air Conditioning	Pump intake set at (n 300 Pumping rate (<i>Vmin-4</i> 5 U.S Duration of pumping 1 hrs + Final water level end of 150 If flowing give rate (<i>Vm</i>	n/ft) GRM) min of pumping (m/ft) nin/GPM)	2 3 4 5 10 15	39.7 42.8 45.6 48.4 63.2 77.3 85.9	2 3 4 5 10 15	14 13 13 13 13 12 11
Method of Cable Tool Rotary (Conventic Rotary (Reverse) Points Air percussion Discreter (Gabra	Construction	d Public Domestic Livestock Infustion Other, spec	Well U Comme Municip Test Ho Cooling ify	se ercial Not used hal Dewatering he Monitoring & Air Conditioning Status of Well Water Supply	Pump intake set at (n 300 Pumping rate (<i>Imini-t</i> 2 U.S Duration of pumping 1 hrs + 0 Final water level end o If flowing give rate (<i>Im</i> Recommended pump	n/ft) GPM) of pumping (m/ft) nin/GPM) o depth (m/ft)	2 3 4 5 10 15 20	39.7 42.8 45.6 48.4 63.2 77.3 85.9 95.2	2 3 4 5 10 15 20	14 13 13 13 12 11 11
Method of Cable Tool Rotary (Conventic Potary (Reverse) Boing Air percussion Her, specify Inside Open Diameter (Carba Concr	Construction	Bublic Dornestic Direstic Livestock Inigation Industrial Other, spec Vecord - Casing Wall Thickness (cm/a) From	Weil U: Ornme Municip Test Ho Cooling ify wepth (m ²) To To	se ercial Not used bal Dewatering ble Monitoring g & Air Conditioning Status of Well Water Supply Replacement Well Test Hole	Pump intake set at (n 300 Pumping rate (<i>Iming</i> 5 US Duration of pumping <u>1</u> hrs + <u>0</u> Final water level end of If flowing give rate (<i>Im</i> Recommended pump 400	wft) GRM) of pumping (m/ft) nin/GPM) o depth (m/ft)	2 3 4 5 10 15 20 25	39.7 42.8 45.6 48.4 63.2 77.3 85.9 95.2	2 3 4 5 10 15 20 25	14 13 13 13 12 11 11 10
Method of Cable Tool Rotary (Conventic Potary (Reverse) Potrg Air percussion Diameter (Calva Concr) 1/4-11 Stee	Construction Diamon- Diamon- Diamon- Digging Digging Digging Construction R Hole OR Material anized, Fibreglass, ete, Plastic, Steel) el	d Public Dornestic Livestock Imgetion Other, spec tecord - Casing Wall Thickness (cm/a) 188 4 +2	Well U: Comme Test Ho Cooling ify Depth (mft) To 1427	se ercial Not used hal Dewatering hal Dewatering hal Monitoring taking Air Conditioning Status of Well Water Supply Replacement Well Recharge Well Dematcharge Well Dematcharge Well	Pump intake set at (n 300 Pumping rate (<i>lminf</i> 5 4.5 Duration of pumping <u>1</u> hrs + <u>0</u> Final water level end of 150 If flowing give rate (<i>lm</i> Recommended pump 400	n/ft) GPM) of pumping (m/ft) in/GPM) o depth (m/ft) o rate	2 3 4 5 10 15 20 25 30	39.7 42.8 45.6 48.4 63.2 77.3 85.9 95.2 104	2 3 4 5 10 15 20 25 30	14 13 13 12 11 11 10 10
Method of Cable Tool Rotary (Conventic Rotary (Reverse) Boing Air Vercussic Diameter Cable Conco	Construction Diamon Diamon Digging Digging Construction R Hole OR Material anized, Fibreglass, Arized, Fibreglass, el en Hole	d Public Domestic Livestock Infigation Other, spec Record - Casing Wall Thickness (cmkg) From .188 4 +2	Well U: Comm Municip Test Ho Cooling fiy Depth (mm) To 2 5007	Se ercial Not used pal Dewatering ple Monitoring s Air Conditioning Status of Weil Water Supply Replacement Weil Becharge Weil Dewatering Weil Dewatering Weil Devatering Weil	Pump intake set at (n 300 Pumping rate (<i>Imin</i> 5 <i>I S</i> Duration of pumping 1 hrs + Final water level end of 150 If flowing give rate (<i>Im</i> Recommended pump 400 Recommended pump (<i>Imin</i> /GMC fm Well production (<i>Imin</i>)	wft) SPM() min of pumping (w/tt) in/GPM() o depth (m/ft) o rate GPIM	2 3 4 5 10 15 20 25 30 40	39.7 42.8 45.6 48.4 63.2 77.3 85.9 95.2 104 122	2 3 4 5 10 15 20 25 30 40	14 13 13 12 11 11 10 10 92
Method of Cable Tool Rotary (Conventic Sotary (Reverse) Boing Air percussion Mer, specify Inside Cable Concer (Cable (Cab	Construction Diamon Diamon Driving Driving Digging Construction R Hole OR Material hole OR Material Reglass, ete, Plastic, Steel) el En Hole	d Public Domestic Livestock Infustion Other, spec ecord - Casing Wall Thickness (crrwb) From .188 +2	Well U: Comme Municip Test Ho Cooling ify Depth (m®) To 1427 5007	se ercial Not used bal Dewatering ble Monitoring g & Air Conditioning Status of Well Water Supply Replacement Well Dewatering Well Dewatering Well Observation and/or Monitoring Hole Atteration	Pump intake set at (n 300 Pumping rate (<i>Iminf</i> 5 US Duration of pumping <u>1</u> hrs + <u>0</u> Final water level end of If flowing give rate (<i>Im</i> Recommended pump (<i>Imin/GNECC</i>) Well production (<i>Iminf</i>	wft) GRM) of pumping (m/ft) nin/GPM) o depth (m/ft) o rate GRM	2 3 4 5 10 15 20 25 30 40 50	39.7 42.8 45.6 48.4 63.2 77.3 85.9 95.2 104 122 135	2 3 4 5 10 15 20 25 30 40 50	14 13 13 12 11 11 10 10 92 84
Method of Cable Tool Rotary (Conventic Potary (Reverse) Poing Air percussion Mer, specif Inside Diameter (Cabla Concr (Cabla Cabla	Construction Diamon Diamon Diating Drying Digging Construction R Hole OR Material mized, Fibreglass, ete, Plastic, Steel) el en Hole	d Public Domestic Livestock Infugation Other, spec Record - Casing Wall Thickopes (cm/op) From .188 +2	Well U: Comme Municip Test Ho Cooling ify Depth (m?) To 2 5003	se ercial Not used bal Dewatering ble Monitoring g & Air Conditioning Status of Well Status of Well Beplacement Well Dewatering Well Dewatering Well Dobservation and/or Monitoring Hole Alteration (Construction) Abandoned.	Pump intake set at (n 300 Pumping rate (/min- 5 / 2 & Duration of pumping 1 hrs + Final water level end of 150 If flowing give rate (/m Recommended pump (/min/GSNE / M Well production (/mer Diemiected?	wft) SRM) of pumping (m/ft) oin/GPM) o depth (m/ft) o rate SPIM	2 3 4 5 10 15 20 25 30 40 50 60	39.7 42.8 45.6 63.2 77.3 85.9 95.2 104 122 135 150	2 3 4 5 10 15 20 25 30 40 50 60	14 13 13 13 12 11 11 10 10 92 84 84 75
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APPENDIX C: CERTIFICATE OF CALIBRATION

McINTOSH PERRY





CERTIFICATE OF CALIBRATION

The HORIBA Instrument listed below has been inspected and calibrated following the Manufacturer's specifications and methods.

nstrument Model:	HORIBA U-52	Serial Number.	R86W200F	Calibration Date:	September 12, 2022	
2-POINT pH	CONDUCTIVITY	TURBIDITY	DISSOLVED OXYGEN	OXIDIZATION-REDUCTION POTENTIAL	TEMPERATURE	
4.00 pH, 7.00 pH	4.49mS/cm ZERO CHECKED	0 & 100 NTU	9.09 mg/L @ 20 DegC SODIUM SULFITE ZERO	240mV	Fisher Scientific s/n 210412377 exp: May 18/2023	
AutoCal 4.00 pH Solution LOT # 2GE898	AutoCal Solution LOT # 2GE898	AutoCal Solution LOT# 2GE898	Oakton Zero Solution LOT # 754262	Hanna ORP LOT # 5766		
Expiry Date: May 31, 2023	Expiry Date: May 31, 2023	Expiry Date: May 31, 2023	Expiry Date: May 1, 2023	Expiry Date: October 1, 2025		
pH 7.00 LOT # 1GF003	@25 DegC LOT # 1GF256	Turb. 100 NTU LOT # A2018				
Expiry Date: June 1, 2023	Expiry Date: May 31, 2023	Expiry Date: February 28, 2024				

The calibration standard used is considered to be a certified standard and is traceable to the National Institute of Standards and Technology (NIST). Certificate of Analysis is available upon request.

The instrument indicated above is now certified to be operating within the Manufacturer's specifications. This does not eliminate the requirement for regular maintenance and pre-use sensor response checks in order to ensure continued complete and accurate operating condition.

Certified By:

Jeff Loney

Maxim Environmental and Safety Inc.

sales@maximenvironmental.com www.maximenvironmental.com



Head Office: 9 - 170 Ambassador Dr., Mississauga, ON L5T 2H9 (905)670-1304 | Toll Free (888)285-2324 Ottawa Office: 9 - 148 Colonnade Rd., Ottawa, ON K2E 7R4 (613)224-4747 | Toll Free (888)285-2324



APPENDIX D: WATER LEVEL DATA AND PUMPING TEST ANALYSES

MCINTOSH PERRY

Summary of Water Level Data Pumping Test - TW1 September 13, 2022

TOC Elevation (assumed)
Static Water Level
Static Water Elevation
95% Recovery

Well depth Pump Depth 100 m AD (Above Datum) 9.87 m BTOC 90.13 m AD (Above Datum) 12.07405 m BTOC 87.92595 m AD (Above Datum) 152.4 m BTOC 500 FT 85.34 m BTOC 280 FT

Elapsed Time (minutes)	Water Level (m BTOC)	Elapsed Time after pump shut off(min)	T/ť	Water Level (m Datum)	Drawdown (m)	Water Column Remaining (m)	% Utilization	Notes
0.00	9.870			90.13	0	75.47	0.0%	Pump on at 7:40am
0.00	11 515			00.105	1 4 4 5	72.025	1.1%	601 DM until 25 min
0.30	11.515			00.400	1.045	73.623	1.170	do Erivi unul 35 min
1.00	13.140			86.86	3.21	12.2	2.1%	53.3 LPIVI UNTIL 192 MIN
1.50	14.590			85.41	4.72	70.75	3.1%	48 LPM until 195 min
2.00	15.978			84.022	6.108	69.362	4.0%	42 LPM until 420 min
2.50	17,293			82,707	7.423	68.047	4.9%	
3.00	18 535			81.465	8 665	66.805	5 7%	
3.00	10.335			81.403	0.005	00.005	J.776	
3.50	19.740			80.26	9.87	65.6	0.5%	
4.00	20.880			79.12	11.01	64.46	7.2%	
4.50	21.945			78.055	12.075	63.395	7.9%	
5.00	23.000			77	13.13	62.34	8.6%	
5.50	24 140			75.86	14.27	61.2	9.4%	
6.00	21.110			74 702	16.240	(0.122	10.10/	
6.00	25.216			74.702	13.340	00.122	10.1%	
7.00	26.740			/3.26	16.87	58.6	11.1%	
8.00	28.345			71.655	18.475	56.995	12.1%	
9.00	30.120			69.88	20.25	55.22	13.3%	
10.00	31.518			68.482	21.648	53.822	14.2%	
11.00	32.615			67 385	22 745	52 725	14.9%	
12.00	32.010			(/ 1/7	22.710	51.507	15.7%	
12.00	33.033			00.107	23.703	51.507	13.776	
13.00	34.970			65.03	25.1	50.37	16.5%	
14.00	36.015			63.985	26.145	49.325	17.2%	
15.00	36.990			63.01	27.12	48.35	17.8%	
18.00	39.540			60.46	29.67	45.8	19.5%	
21.00	41,810			58 19	31 94	43.53	21.0%	
22.00	12 740			57.24	32.00	42 50	21.070	
23.00	42.700			57.24	32.07	42.00	21.0%	
25.00	43.950			56.05	34.08	41.39	22.4%	
29.00	45.620			54.38	35.75	39.72	23.5%	
35.00	47.520			52.48	37.65	37.82	24.7%	
41.00	48.785			51.215	38.915	36.555	25.5%	
48.00	49.565			50.435	39.695	35 775	26.0%	İ
56.00	50.525			49.475	40.655	34.915	26.7%	
(7.50	50.323			40.7(4	41.000	34.013	20.770	
07.50	51.230			40.704	41.300	34.104	27.1/0	
77.50	51.6/3			48.327	41.803	33.667	27.4%	
93.00	52.295			47.705	42.425	33.045	27.8%	
107.00	52.560			47.44	42.69	32.78	28.0%	
129.00	52.863			47.137	42.993	32.477	28.2%	
142.00	53.097			46.903	43.227	32.243	28.4%	
167.00	53.661			46.339	43,791	31.679	28.7%	
180.00	53.865			46 135	43 995	31.475	28.0%	
104.00	53.003			44.040	44.091	21,200	20.7%	
194.00	53.951			40.047	44.001	31.309	28.9%	
198.00	52.115			47.885	42.245	33.225	27.7%	
199.00	52.225			47.775	42.355	33.115	27.8%	
202.00	51.187			48.813	41.317	34.153	27.1%	
216.00	47.885			52.115	38.015	37.455	24.9%	
220.00	47.525			52.475	37.655	37.815	24.7%	
227.00	46.980			53.02	37.11	38.36	24.4%	
242.00	46.260			E2.64	26.40	20.00	22.0%	
203.00	40.300			53.04	30.47	20.072	23.770	
204.00	40.307			53.633	30.497	30.973	23.9%	
301.50	46.405			53.595	36.535	38.935	24.0%	
333.00	46.494			53.506	36.624	38.846	24.0%	
350.00	46.530			53.47	36.66	38.81	24.1%	
375.00	46,780			53.22	36.91	38.56	24.2%	
382.00	46.550			53.45	36.68	38.70	24.1%	
400.00	46.600			E2 270	24 751	20 710	24.1%	
400.00	40.021			53.377	30.731	30.717	24.1/0	
412.00	46.568			53.432	36.698	38.772	24.1%	
420.00	46.599			53.401	36.729	38.741	24.1%	Pump off at 2:40pm
421.00	43.720	1.0	421.000	56.28	33.85	41.62	22.2%	
422.00	41.700	2.000	211.000	58.3	31.83	43.64	20.9%	
423.00	39.914	3.000	141.000	60.086	30.044	45.426	19.7%	
424.00	39,190	4,000	106.000	60.81	29.32	46 15	19.2%	
425.00	37 570	5,000	85,000	62.43	27.7	47.77	18.2%	
424.00	36.024	6,000	71,000	63 076	26 154	40.214	17.2%	
420.00	30.024	0.000	/1.000	45 4/	20.134	47.310	17.2%	
427.00	34.540	7.000	01.000	03.40	24.07	50.8	10.2%	
428.00	32.153	8.000	53.500	67.847	22.283	53.187	14.6%	
429.00	31.800	9.000	47.667	68.2	21.93	53.54	14.4%	
430.00	29.346	10.000	43.000	70.654	19.476	55.994	12.8%	
431.00	28.335	11.000	39.182	71.665	18.465	57.005	12.1%	
432.00	27.000	12.000	36.000	73	17.13	58.34	11.2%	
437.50	21,880	17,000	25,735	78 12	12.01	63.46	7.9%	
439.00	20 710	19,000	23 105	79.20	10.84	64.63	7 1%	
40.00	10.973	20	22.103	80 129	10.002	65.440	6.4%	
440.00	17.072	20	22.000	00.120	10.002	03.400	0.0%	
441.50	19.000	21.5	20.535	81	9.13	66.34	6.0%	
443.00	18.000	23	19.261	82	8.13	67.34	5.3%	
445.50	16.785	25.5	17.471	83.215	6.915	68.555	4.5%	
447.00	16.000	27	16.556	84	6.13	69.34	4.0%	
449.00	15.000	29	15.483	85	5.13	70.34	3.4%	
453.00	14.000	33	13.727	86	4.13	71.34	2.7%	
458	13.000	38	12.053	87	3.13	72.34	2.1%	
A64	12 200	44	10.545	87.9	2.32	73.14	1.5%	
404	11.745	49	0 571	88.325	1,905	73 575	1.3%	
407	11.705	47	7.371	00.233	1.075	13.373	1.270	
	1					1		
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APPENDIX E: LABORATORY CERTIFICATES OF ANALYSIS

MCINTOSH PERRY



RESPONSIVE. RELIABLE.

300 - 2319 St. Laurent Blvd Ottawa, ON, K1G 4J8 1-800-749-1947 www.paracellabs.com

Certificate of Analysis

McIntosh Perry Consulting Eng. (Carp)

115 Walgreen Rd. Carp, ON K0A 1L0 Attn: Monica Black

Client PO: Russ Bradley Project: 22-1643-01 Custody: 67014

Report Date: 22-Sep-2022 Order Date: 13-Sep-2022

Order #: 2238202

This Certificate of Analysis contains analytical data applicable to the following samples as submitted :

Paracel ID **Client ID** 2238202-01 TW1-1 2238202-02 TW1-2

Approved By:

Dale Robertson, BSc Laboratory Director

Any use of these results implies your agreement that our total liability in connection with this work, however arising, shall be limited to the amount paid by you for this work, and that our employees or agents shall not under any circumstances be liable to you in connection with this work.



Analysis Summary Table

Report Date: 22-Sep-2022 Order Date: 13-Sep-2022

Project Description: 22-1643-01

Analysis	Method Reference/Description	Extraction Date	Analysis Date
Alkalinity, total to pH 4.5	EPA 310.1 - Titration to pH 4.5	14-Sep-22	14-Sep-22
Ammonia, as N	EPA 351.2 - Auto Colour	14-Sep-22	14-Sep-22
Anions	EPA 300.1 - IC	21-Sep-22	21-Sep-22
Colour	SM2120 - Spectrophotometric	14-Sep-22	14-Sep-22
Conductivity	EPA 9050A- probe @25 °C	14-Sep-22	14-Sep-22
Dissolved Organic Carbon	MOE E3247B - Combustion IR, filtration	14-Sep-22	14-Sep-22
E. coli	MOE E3407	14-Sep-22	14-Sep-22
Fecal Coliform	SM 9222D	14-Sep-22	14-Sep-22
Mercury by CVAA	EPA 245.2 - Cold Vapour AA	14-Sep-22	14-Sep-22
Metals, ICP-MS	EPA 200.8 - ICP-MS	15-Sep-22	15-Sep-22
pН	EPA 150.1 - pH probe @25 °C	14-Sep-22	14-Sep-22
Phenolics	EPA 420.2 - Auto Colour, 4AAP	14-Sep-22	14-Sep-22
Hardness	Hardness as CaCO3	15-Sep-22	15-Sep-22
Sulphide	SM 4500SE - Colourimetric	15-Sep-22	15-Sep-22
Tannin/Lignin	SM 5550B - Colourimetric	15-Sep-22	16-Sep-22
Total Coliform	MOE E3407	14-Sep-22	14-Sep-22
Total Dissolved Solids	SM 2540C - gravimetric, filtration	14-Sep-22	15-Sep-22
Total Kjeldahl Nitrogen	EPA 351.2 - Auto Colour, digestion	15-Sep-22	16-Sep-22
Turbidity	SM 2130B - Turbidity meter	15-Sep-22	15-Sep-22
VOCs by P&T GC-MS	EPA 624 - P&T GC-MS	15-Sep-22	15-Sep-22



Certificate of Analysis

Client: McIntosh Perry Consulting Eng. (Carp)

Client PO: Russ Bradley

Order #: 2238202

Report Date: 22-Sep-2022

Order Date: 13-Sep-2022

Project Description: 22-1643-01

	Client ID: Sample Date: Sample ID: MDL/Units	TW1-1 13-Sep-22 10:40 2238202-01 Water	TW1-2 13-Sep-22 14:35 2238202-02 Water	- - -	- - -
Microbiological Parameters	MDE/Onits				
E. coli	1 CFU/100mL	ND [1]	ND [1]	-	-
Fecal Coliforms	1 CFU/100mL	ND	ND	-	-
Total Coliforms	1 CFU/100mL	ND [1]	ND [1]	-	-
General Inorganics	• •				
Alkalinity, total	5 mg/L	187	186	-	-
Ammonia as N	0.01 mg/L	0.11	0.07	-	-
Dissolved Organic Carbon	0.5 mg/L	1.4	1.5	-	-
Colour	2 TCU	4	<2	-	-
Conductivity	5 uS/cm	499	509	-	-
Hardness	0.824 mg/L	271	265	-	-
рН	0.1 pH Units	7.9	7.9	-	-
Phenolics	0.001 mg/L	<0.001	<0.001	-	-
Total Dissolved Solids	10 mg/L	278	270	-	-
Sulphide	0.02 mg/L	3.14	3.36	-	-
Tannin & Lignin	0.1 mg/L	<0.1	<0.1	-	-
Total Kjeldahl Nitrogen	0.1 mg/L	0.1	<0.1	-	-
Turbidity	0.1 NTU	34.8	3.3	-	-
Anions	• • •		•		
Chloride	1.0 mg/L	22.5	25.6	-	-
Fluoride	0.1 mg/L	0.8	1.4	-	-
Nitrate as N	0.1 mg/L	<0.1	<0.1	-	-
Nitrite as N	0.05 mg/L	<0.05	<0.05	-	-
Phosphate as P	0.2 mg/L	<0.2	0.3	-	-
Sulphate	1.0 mg/L	35.1	34.3	-	-
Metals			-		
Mercury	0.1 ug/L	<0.1	<0.1	-	-
Aluminum	1 ug/L	680	140	-	-
Antimony	0.5 ug/L	<0.5	<0.5	-	-
Arsenic	1 ug/L	<1	<1	-	-
Barium	1 ug/L	295	277	-	-
Beryllium	0.5 ug/L	<0.5	<0.5	-	-
Boron	10 ug/L	89	94	-	-
Cadmium	0.1 ug/L	<0.1	<0.1	-	-
Calcium	100 ug/L	72200	71600	-	-
Chromium	1 ug/L	2	<1	-	-

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Certificate of Analysis Client: McIntosh Perry Consulting Eng. (Carp)

Client PO: Russ Bradley

Order #: 2238202

Report Date: 22-Sep-2022 Order Date: 13-Sep-2022

Project Description: 22-1643-01

	Client ID: Sample Date: Sample ID:	TW1-1 13-Sep-22 10:40 2238202-01 Water	TW1-2 13-Sep-22 14:35 2238202-02 Water	- - -	
Cobalt	0.5 ug/L	<0.5	<0.5		-
Copper	0.5 ug/L	<0.5	<0.5	-	-
Iron	100 ug/L	820	139	-	_
Lead	0.1 ug/L	0.2	<0.1	-	-
Magnesium	200 ug/L	22100	21000	-	-
Manganese	5 ug/L	19	6	-	-
Molybdenum	0.5 ug/L	<0.5	<0.5	-	-
Nickel	1 ug/L	<1	<1	-	-
Potassium	100 ug/L	5330	4940	-	-
Selenium	1 ug/L	<1	<1	-	-
Silver	0.1 ug/L	<0.1	<0.1	-	-
Sodium	200 ug/L	22700	24100	-	-
Strontium	10 ug/L	3120	3290	-	-
Thallium	0.1 ug/L	<0.1	<0.1	-	-
Tin	5 ug/L	<5	<5	-	-
Titanium	5 ug/L	77	15	-	-
Tungsten	10 ug/L	<10	<10	-	-
Uranium	0.1 ug/L	0.1	<0.1	-	-
Vanadium	0.5 ug/L	2.5	<0.5	-	-
Zinc	5 ug/L	9	<5	-	-
Volatiles					
Acetone	5.0 ug/L	-	<5.0	-	-
Benzene	0.5 ug/L	-	<0.5	-	-
Bromodichloromethane	0.5 ug/L	-	<0.5	-	-
Bromoform	0.5 ug/L	-	<0.5	-	-
Bromomethane	0.5 ug/L	-	<0.5	-	-
Carbon Tetrachloride	0.2 ug/L	-	<0.2	-	-
Chlorobenzene	0.5 ug/L	-	<0.5	-	-
Chloroethane	1.0 ug/L	-	<1.0	-	-
Chloroform	0.5 ug/L	-	<0.5	-	-
Chloromethane	3.0 ug/L	-	<3.0	-	-
Dibromochloromethane	0.5 ug/L	-	<0.5	-	-
Dichlorodifluoromethane	1.0 ug/L	-	<1.0	-	-
1,2-Dibromoethane	0.2 ug/L	-	<0.2	-	-
1,2-Dichlorobenzene	0.5 ug/L	-	<0.5	-	-
1,3-Dichlorobenzene	0.5 ug/L	-	<0.5	-	-

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Certificate of Analysis Client: McIntosh Perry Consulting Eng. (Carp)

Client PO: Russ Bradley

Report Date: 22-Sep-2022 Order Date: 13-Sep-2022

Project Description: 22-1643-01

	Client ID:	TW1-1	TW1-2	-	-
	Sample Date:	13-Sep-22 10:40	13-Sep-22 14:35	-	-
	Sample ID:	2238202-01	2238202-02	-	-
	MDL/Units	Water	Water	-	-
1,4-Dichlorobenzene	0.5 ug/L	-	<0.5	-	-
1,1-Dichloroethane	0.5 ug/L	-	<0.5	-	-
1,2-Dichloroethane	0.5 ug/L	-	<0.5	-	-
1,1-Dichloroethylene	0.5 ug/L	-	<0.5	-	-
cis-1,2-Dichloroethylene	0.5 ug/L	-	<0.5	-	-
trans-1,2-Dichloroethylene	0.5 ug/L	-	<0.5	-	-
1,2-Dichloroethylene, total	0.5 ug/L	-	<0.5	-	-
1,2-Dichloropropane	0.5 ug/L	-	<0.5	-	-
cis-1,3-Dichloropropylene	0.5 ug/L	-	<0.5	-	-
trans-1,3-Dichloropropylene	0.5 ug/L	-	<0.5	-	-
1,3-Dichloropropene, total	0.5 ug/L	-	<0.5	-	-
Ethylbenzene	0.5 ug/L	-	<0.5	-	-
Hexane	1.0 ug/L	-	<1.0	-	-
Methyl Ethyl Ketone (2-Butanone)	5.0 ug/L	-	<5.0	-	-
Methyl Butyl Ketone (2-Hexanone)	10.0 ug/L	-	<10.0	-	-
Methyl Isobutyl Ketone	5.0 ug/L	-	<5.0	-	-
Methyl tert-butyl ether	2.0 ug/L	-	<2.0	-	-
Methylene Chloride	5.0 ug/L	-	<5.0	-	-
Styrene	0.5 ug/L	-	<0.5	-	-
1,1,1,2-Tetrachloroethane	0.5 ug/L	-	<0.5	-	-
1,1,2,2-Tetrachloroethane	0.5 ug/L	-	<0.5	-	-
Tetrachloroethylene	0.5 ug/L	-	<0.5	-	-
Toluene	0.5 ug/L	-	<0.5	-	-
1,1,1-Trichloroethane	0.5 ug/L	-	<0.5	-	-
1,1,2-Trichloroethane	0.5 ug/L	-	<0.5	-	-
Trichloroethylene	0.5 ug/L	-	<0.5	-	-
Trichlorofluoromethane	1.0 ug/L	-	<1.0	-	-
1,3,5-Trimethylbenzene	0.5 ug/L	-	<0.5	-	-
Vinyl chloride	0.5 ug/L	-	<0.5	-	-
m,p-Xylenes	0.5 ug/L	-	<0.5	-	-
o-Xylene	0.5 ug/L	-	<0.5	-	-
Xylenes, total	0.5 ug/L	-	<0.5	-	-
4-Bromofluorobenzene	Surrogate	-	115%	-	-
Dibromofluoromethane	Surrogate	-	93.0%	-	-
Toluene-d8	Surrogate	-	107%	-	-



Tin Titanium

Tungsten

Uranium

Zinc

E. coli

Volatiles Acetone

Benzene

Fecal Coliforms

Total Coliforms

Bromodichloromethane

Vanadium

Microbiological Parameters

Certificate of Analysis Client: McIntosh Perry Consulting Eng. (Carp) Client PO: Russ Bradley

Metho

Method Quality Control: Blank							
Analyte	Result	Reporting Limit	Units	Source Result	%REC	%REC Limit	RPD
Anions							
Chloride	ND	10	ma/l				
Fluoride	ND	0.1	mg/L				
Nitrate as N	ND	0.1	ma/l				
Nitrite as N	ND	0.05	ma/L				
Phosphate as P	ND	0.2	ma/L				
Sulphate	ND	1.0	ma/L				
General Inorganics			0				
Alkalinity, total	ND	5	ma/L				
Ammonia as N	ND	0.01	ma/L				
Dissolved Organic Carbon	ND	0.5	mg/L				
Colour	ND	2	ΤČU				
Conductivity	ND	5	uS/cm				
Phenolics	ND	0.001	mg/L				
Total Dissolved Solids	ND	10	mg/L				
Sulphide	ND	0.02	mg/L				
Tannin & Lignin	ND	0.1	mg/L				
Total Kjeldahl Nitrogen	ND	0.1	mg/L				
Turbidity	ND	0.1	NŤU				
Metals							
Mercury	ND	0.1	ug/L				
Aluminum	ND	1	ug/L				
Antimony	ND	0.5	ug/L				
Arsenic	ND	1	ug/L				
Barium	ND	1	ug/L				
Beryllium	ND	0.5	ug/L				
Boron	ND	10	ug/L				
Cadmium	ND	0.1	ug/L				
Calcium	ND	100	ug/L				
Chromium	ND	1	ug/L				
Cobalt	ND	0.5	ug/L				
Copper	ND	0.5	ug/L				
Iron	ND	100	ug/L				
Lead	ND	0.1	ug/L				
Magnesium	ND	200	ug/L				
Manganese	ND	5	ug/L				
Molybdenum	ND	0.5	ug/L				
Nickel	ND	1	ug/L				
Potassium	ND	100	ug/L				
Selenium	ND	1	ug/L				
Silver	ND	0.1	ug/L				
Sodium	ND	200	ug/L				
Strontium	ND	10	ug/L				
I hallium	ND	0.1	ug/L				
Tin	ND	5	ug/L				

ND

5

10

0.1

0.5

5

1

1

1

5.0

0.5

0.5

Order #: 2238202

Report Date: 22-Sep-2022

Order Date: 13-Sep-2022

Notes

Project Description: 22-1643-01

RPD

Limit

ug/L

ug/L

ug/L ug/L

ug/L

CFU/100mL

CFU/100mL

CFU/100mL

ug/L

ug/L

ug/L



Method Quality Control: Blank

Report Date: 22-Sep-2022

Order Date: 13-Sep-2022

Project Description: 22-1643-01

Analyte	Result	Reporting	Units	Source Result	%REC	%REC	RPD	RPD Limit	Notes
Deservationer	ND	0.5		rtoour					
Bromomothana		0.5	ug/L						
Bromometnane		0.5	ug/L						
		0.2	ug/L						
Chlorobenzene		0.5	ug/L						
Chloroetnane		1.0	ug/L						
Chlorotorm		0.5	ug/L						
		3.0	ug/L						
		0.5	ug/L						
		1.0	ug/L						
1,2-Dibromoetnane		0.2	ug/L						
1,2-Dichlorobenzene	ND	0.5	ug/L						
1,3-Dichlorobenzene	ND	0.5	ug/L						
1,4-Dichlorobenzene	ND	0.5	ug/L						
	ND	0.5	ug/L						
1,2-Dichloroethane	ND	0.5	ug/L						
	ND	0.5	ug/L						
		0.5	ug/L						
trans-1,2-Dichloroethylene	ND	0.5	ug/L						
	ND	0.5	ug/L						
1,2-Dichloropropane	ND	0.5	ug/L						
cis-1,3-Dichloropropylene	ND	0.5	ug/L						
trans-1,3-Dichloropropylene	ND	0.5	ug/L						
1,3-Dichloropropene, total	ND	0.5	ug/L						
Etnyibenzene	ND	0.5	ug/L						
Hexane	ND	1.0	ug/L						
Methyl Ethyl Ketone (2-Butanone)	ND	5.0	ug/L						
Methyl Butyl Ketone (2-Hexanone)	ND	10.0	ug/L						
Methyl Isobutyl Ketone	ND	5.0	ug/L						
Methyl tert-butyl ether	ND	2.0	ug/L						
Methylene Chloride	ND	5.0	ug/L						
Styrene	ND	0.5	ug/L						
	ND	0.5	ug/L						
	ND	0.5	ug/L						
Theread	ND	0.5	ug/L						
	ND	0.5	ug/L						
	ND	0.5	ug/L						
1,1,2-Irichloroethane	ND	0.5	ug/L						
Irichloroethylene	ND	0.5	ug/L						
Irichlorofluoromethane	ND	1.0	ug/L						
1,3,5- I rimethylbenzene	ND	0.5	ug/L						
Vinyl chloride	ND	0.5	ug/L						
m,p-Xylenes	ND	0.5	ug/L						
o-Xylene	ND	0.5	ug/L						
Xylenes, total	ND	0.5	ug/L			50 4 40			
Surrogate: 4-Bromofluorobenzene	88.0		ug/L		110	50-140			
Surrogate: Dibromofluoromethane	73.4		ug/L		91.8	50-140			
Surrogate: Toluene-d8	84.7		ug/L		106	50-140			



Method Quality Control: Duplicate

Report Date: 22-Sep-2022 Order Date: 13-Sep-2022

Project Description: 22-1643-01

		Reporting		Source		%REC		RPD	
Analyte	Result	Limit	Units	Result	%REC	Limit	RPD	Limit	Notes
Anions									
Chloride	22.0	1.0	ma/L	22.5			2.3	10	
Fluoride	0.87	0.1	ma/L	0.81			6.6	10	
Nitrate as N	ND	0.1	ma/L	ND			NC	10	
Nitrite as N	ND	0.05	mg/L	ND			NC	10	
Phosphate as P	0.28	0.2	ma/L	ND			NC	10	
Sulphate	35.0	1.0	ma/L	35.1			0.5	10	
General Inorganics									
Alkalinity, total	312	5	ma/L	319			2.1	14	
Ammonia as N	0.096	0.01	ma/L	0.098			2.1	18	
Dissolved Organic Carbon	3.3	0.5	ma/L	3.8			14.7	37	
Colour	ND	2	ΤČU	2			NC	12	
Conductivity	35300	5	uS/cm	36000			1.9	5	
pH	7.6	0.1	pH Units	7.5			1.1	3.3	
Phenolics	ND	0.001	mg/L	ND			NC	10	
Total Dissolved Solids	280	10	mg/L	278			0.7	10	
Sulphide	0.02	0.02	mg/L	0.02			9.1	10	
Tannin & Lignin	ND	0.1	mg/L	ND			NC	11	
Total Kjeldahl Nitrogen	0.37	0.1	mg/L	0.31			15.7	16	
Turbidity	34.0	0.1	NŤU	34.8			2.3	10	
Metals									
Mercury	ND	0.1	ug/L	ND			NC	20	
Aluminum	15.5	1	ug/L	12.3			22.8	20	QR-05
Antimony	0.51	0.5	ug/L	0.72			NC	20	
Arsenic	2.6	1	ug/L	2.5			4.6	20	
Barium	127	1	ug/L	126			0.5	20	
Beryllium	ND	0.5	ug/L	ND			NC	20	
Boron	107	10	ug/L	108			0.3	20	
Cadmium	ND	0.1	ug/L	ND			NC	20	
Calcium	146000	100	ug/L	147000			1.3	20	
Chromium	ND	1	ug/L	ND			NC	20	
Cobalt	1.79	0.5	ug/L	1.81			1.2	20	
Copper	1.29	0.5	ug/L	1.38			6.6	20	
Iron	275	100	ug/L	275			0.2	20	
Lead	1.74	0.1	ug/L	1.73			0.6	20	
Magnesium	27200	200	ug/L	27500			1.0	20	
Manganese	159	5	ug/L	159			0.1	20	
Molybdenum	8.17	0.5	ug/L	8.33			1.9	20	
Nickel	3.3	1	ug/L	3.3			1.6	20	
Potassium	6030	100	ug/L	6000			0.6	20	
Selenium	ND	1	ug/L	ND			NC	20	
Silver	ND	0.1	ug/L	ND			NC	20	
Sodium	112000	200	ug/L	113000			0.3	20	
Strontium	2130	10	ug/L	2120			0.5	20	
Thallium	0.15	0.1	ug/L	0.15			3.8	20	
lin Tri	ND	5	ug/L	ND			NC	20	
	ND	5	ug/L	ND			NC	20	
lungsten	ND	10	ug/L	ND			NC	20	
Uranium	1.6	0.1	ug/L	1.6			1.0	20	
vanadium Zin -	0.53	0.5	ug/L	0.54			2.1	20	
Zinc Microbiological Parameters	ND	5	ug/L	5			NC	20	
		1	CELI/100ml				NC	20	BAC14
		1					NC	3U 20	DAU 14
Total Colliforms		1					NC	3U 20	BAC14
Volatiles	UN	I		ND			NC	30	
Acetone		5.0	uc/I	ND			NC	30	
	שא	5.0	ug/L	ND			NC	30	

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OTTAWA - MISSISSAUGA - HAMILTON - KINGSTON - LONDON - NIAGARA - WINDSOR - RICHMOND HILL



Method Quality Control: Duplicate

Report Date: 22-Sep-2022 Order Date: 13-Sep-2022

Project Description: 22-1643-01

		Reporting		Source		%REC		RPD	
Analyte	Result	Limit	Units	Result	%REC	Limit	RPD	Limit	Notes
	ND	0.5		ND			NO	00	
Benzene	ND	0.5	ug/L	ND			NC	30	
Bromodicniorometnane	4.10	0.5	ug/L	4.03			3.2	30	
Bromolorm		0.5	ug/L	ND			NC	30	
Bromometnane	ND	0.5	ug/L	ND			NC	30	
	ND	0.2	ug/L	ND			NC	30	
Chlorobenzene	ND	0.5	ug/L	ND			NC	30	
Chloroethane	ND	1.0	ug/L	ND			NC	30	
Chloroform	8.50	0.5	ug/L	9.99			16.1	30	
Chloromethane	ND	3.0	ug/L	ND			NC	30	
Dibromochloromethane	4.18	0.5	ug/L	3.88			7.4	30	
Dichlorodifluoromethane	ND	1.0	ug/L	ND			NC	30	
1,2-Dibromoethane	ND	0.2	ug/L	ND			NC	30	
1,2-Dichlorobenzene	ND	0.5	ug/L	ND			NC	30	
1,3-Dichlorobenzene	ND	0.5	ug/L	ND			NC	30	
1,4-Dichlorobenzene	ND	0.5	ug/L	ND			NC	30	
1,1-Dichloroethane	ND	0.5	ug/L	ND			NC	30	
1,2-Dichloroethane	ND	0.5	ug/L	ND			NC	30	
1,1-Dichloroethylene	ND	0.5	ug/L	ND			NC	30	
cis-1,2-Dichloroethylene	ND	0.5	ug/L	ND			NC	30	
trans-1,2-Dichloroethylene	ND	0.5	ug/L	ND			NC	30	
1,2-Dichloropropane	ND	0.5	ug/L	ND			NC	30	
cis-1,3-Dichloropropylene	ND	0.5	ug/L	ND			NC	30	
trans-1,3-Dichloropropylene	ND	0.5	ug/L	ND			NC	30	
Ethylbenzene	ND	0.5	ug/L	ND			NC	30	
Hexane	ND	1.0	ug/L	ND			NC	30	
Methyl Ethyl Ketone (2-Butanone)	ND	5.0	ug/L	ND			NC	30	
Methyl Butyl Ketone (2-Hexanone)	ND	10.0	ug/L	ND			NC	30	
Methyl Isobutyl Ketone	ND	5.0	ug/L	ND			NC	30	
Methyl tert-butyl ether	ND	2.0	ug/L	ND			NC	30	
Methylene Chloride	ND	5.0	ug/L	ND			NC	30	
Styrene	ND	0.5	ug/L	ND			NC	30	
1,1,1,2-Tetrachloroethane	ND	0.5	ug/L	ND			NC	30	
1,1,2,2-Tetrachloroethane	ND	0.5	ug/L	ND			NC	30	
Tetrachloroethylene	ND	0.5	ug/L	ND			NC	30	
Toluene	ND	0.5	ug/L	ND			NC	30	
1,1,1-Trichloroethane	ND	0.5	ug/L	ND			NC	30	
1,1,2-Trichloroethane	ND	0.5	ug/L	ND			NC	30	
Trichloroethylene	ND	0.5	ug/L	ND			NC	30	
Trichlorofluoromethane	ND	1.0	ug/L	ND			NC	30	
1,3,5-Trimethylbenzene	ND	0.5	ug/L	ND			NC	30	
Vinyl chloride	ND	0.5	ug/L	ND			NC	30	
m,p-Xylenes	ND	0.5	ug/L	ND			NC	30	
o-Xylene	ND	0.5	ug/L	ND			NC	30	
Surrogate: 4-Bromofluorobenzene	90.4		ug/L		113	50-140			
Surrogate: Dibromofluoromethane	71.9		ug/L		89.8	50-140			
Surrogate: Toluene-d8	85.7		ua/L		107	50-140			
			3- =						

OTTAWA - MISSISSAUGA - HAMILTON - KINGSTON - LONDON - NIAGARA - WINDSOR - RICHMOND HILL



Method Quality Control: Spike

Report Date: 22-Sep-2022 Order Date: 13-Sep-2022

Project Description: 22-1643-01

Analyte	Result	Reporting Limit	Units	Source	%REC	%REC	RPD	RPD Limit	Notes
,				Result		Linnt			
Anions									
Chloride	31.9	1.0	mg/L	22.5	94.2	77-123			
Fluoride	1.85	0.1	mg/L	0.81	104	79-121			
Nitrate as N	1.17	0.1	mg/L	ND	117	79-120			
Nitrite as N	1.06	0.05	mg/L	ND	106	84-117			
Phosphate as P	5.19	0.2	mg/L	ND	104	59-141			
Sulphate	45.2	1.0	mg/L	35.1	100	74-126			
General Inorganics									
Ammonia as N	0.338	0.01	mg/L	0.098	96.0	81-124			
Dissolved Organic Carbon	12.3	0.5	mg/L	3.8	85.1	60-133			
Phenolics	0.028	0.001	mg/L	ND	110	67-133			
Total Dissolved Solids	90.0	10	mg/L	ND	90.0	75-125			
Sulphide	0.48	0.02	mg/L	0.02	90.8	79-115			
Tannin & Lignin	1.1	0.1	mg/L	ND	108	71-113			
Total Kjeldahl Nitrogen	2.38	0.1	mg/L	0.31	103	81-126			
Metals									
Mercury	2.74	0.1	ug/L	ND	91.2	70-130			
Aluminum	55.9	1	ug/L	12.3	87.2	80-120			
Arsenic	52.2	1	ug/L	2.5	99.5	80-120			
Barium	167	1	ug/L	126	82.0	80-120			
Beryllium	41.7	0.5	ug/L	ND	83.4	80-120			
Boron	57	10	ug/L	16	81.9	80-120			
Cadmium	40.2	0.1	ug/L	ND	80.4	80-120			
Calcium	133000	100	ug/L	124000	87.7	80-120			
Chromium	53.0	1	ug/L	ND	105	80-120			
Cobalt	50.5	0.5	ug/L	1.81	97.4	80-120			
Copper	45.3	0.5	ug/L	1.38	87.9	80-120			
Iron	2690	100	ug/L	275	96.6	80-120			
Lead	43.6	0.1	ug/L	1.73	83.7	80-120			
Magnesium	37700	200	ug/L	27900	97.4	80-120			
Manganese	363	5	ug/L	313	99.2	80-120			
Molybdenum	53.0	0.5	ug/L	8.33	89.4	80-120			
Nickel	49.9	1	ug/L	3.3	93.0	80-120			
Potassium	16600	100	ug/L	6000	106	80-120			
Selenium	45.9	1	ug/L	ND	91.3	80-120			
Silver	49.3	0.1	ug/L	ND	98.7	80-120			
Sodium	27700	200	ug/L	17900	98.0	80-120			
Strontium	334	10	ug/L	291	85.6	80-120			
Thallium	42.9	0.1	ug/L	0.15	85.5	80-120			
Tin	45.9	5	ug/L	ND	91.2	80-120			
Titanium	57.9	5	ug/L	ND	114	80-120			
Tungsten	51.3	10	ug/L	ND	91.2	80-120			
Uranium	48.0	0.1	ug/L	1.6	92.8	80-120			
Vanadium	54.3	0.5	ug/L	0.54	108	80-120			
Zinc	46	5	ug/L	ND	91.1	80-120			
Volatiles									
Acetone	71.9	5.0	ug/L	ND	71.9	50-140			
Benzene	35.6	0.5	ug/L	ND	89.1	60-130			
Bromodichloromethane	35.5	0.5	ug/L	ND	88.8	60-130			
			2						

OTTAWA . MISSISSAUGA . HAMILTON . KINGSTON . LONDON . NIAGARA . WINDSOR . RICHMOND HILL



Method Quality Control: Spike

Report Date: 22-Sep-2022

Order Date: 13-Sep-2022

Project Description: 22-1643-01

Analyte	Result	Reporting Limit	Units	Source Result	%REC	%REC Limit	RPD	RPD Limit	Notes
Bromoform	41.5	0.5	ug/L	ND	104	60-130			
Bromomethane	41.3	0.5	ug/L	ND	103	50-140			
Carbon Tetrachloride	33.0	0.2	ug/L	ND	82.6	60-130			
Chlorobenzene	42.2	0.5	ug/L	ND	105	60-130			
Chloroethane	34.9	1.0	ug/L	ND	87.4	50-140			
Chloroform	40.5	0.5	ug/L	ND	101	60-130			
Chloromethane	35.8	3.0	ug/L	ND	89.4	50-140			
Dibromochloromethane	40.2	0.5	ug/L	ND	100	60-130			
Dichlorodifluoromethane	37.4	1.0	ug/L	ND	93.6	50-140			
1,2-Dibromoethane	39.2	0.2	ug/L	ND	98.0	60-130			
1,2-Dichlorobenzene	42.1	0.5	ug/L	ND	105	60-130			
1,3-Dichlorobenzene	40.4	0.5	ug/L	ND	101	60-130			
1,4-Dichlorobenzene	40.2	0.5	ug/L	ND	101	60-130			
1,1-Dichloroethane	36.2	0.5	ug/L	ND	90.6	60-130			
1,2-Dichloroethane	37.0	0.5	ug/L	ND	92.5	60-130			
1,1-Dichloroethylene	32.2	0.5	ug/L	ND	80.5	60-130			
cis-1,2-Dichloroethylene	40.0	0.5	ug/L	ND	100	60-130			
trans-1,2-Dichloroethylene	36.1	0.5	ug/L	ND	90.2	60-130			
1,2-Dichloropropane	35.6	0.5	ug/L	ND	89.0	60-130			
cis-1,3-Dichloropropylene	38.2	0.5	ug/L	ND	95.5	60-130			
trans-1,3-Dichloropropylene	42.6	0.5	ug/L	ND	106	60-130			
Ethylbenzene	37.2	0.5	ug/L	ND	93.0	60-130			
Hexane	44.1	1.0	ug/L	ND	110	60-130			
Methyl Ethyl Ketone (2-Butanone)	97.9	5.0	ug/L	ND	97.9	50-140			
Methyl Butyl Ketone (2-Hexanone)	66.6	10.0	ug/L	ND	66.6	50-140			
Methyl Isobutyl Ketone	97.3	5.0	ug/L	ND	97.3	50-140			
Methyl tert-butyl ether	66.1	2.0	ug/L	ND	66.1	50-140			
Methylene Chloride	35.6	5.0	ug/L	ND	88.9	60-130			
Styrene	37.1	0.5	ug/L	ND	92.7	60-130			
1,1,1,2-Tetrachloroethane	35.5	0.5	ug/L	ND	88.7	60-130			
1,1,2,2-Tetrachloroethane	33.8	0.5	ug/L	ND	84.6	60-130			
Tetrachloroethylene	38.6	0.5	ug/L	ND	96.6	60-130			
Toluene	38.1	0.5	ug/L	ND	95.3	60-130			
1,1,1-Trichloroethane	31.1	0.5	ug/L	ND	77.8	60-130			
1,1,2-Trichloroethane	40.8	0.5	ug/L	ND	102	60-130			
Trichloroethylene	30.0	0.5	ug/L	ND	75.0	60-130			
Trichlorofluoromethane	39.0	1.0	ug/L	ND	97.6	60-130			
1,3,5-Trimethylbenzene	37.7	0.5	ug/L	ND	94.3	60-130			
Vinyl chloride	40.0	0.5	ug/L	ND	99.9	50-140			
m,p-Xylenes	77.9	0.5	ug/L	ND	97.4	60-130			
o-Xylene	37.4	0.5	ug/L	ND	93.4	60-130			
Surrogate: 4-Bromofluorobenzene	89.3		ug/L		112	50-140			
Surrogate: Dibromofluoromethane	69.4		ug/L		86.7	50-140			
Surrogate: Toluene-d8	70.8		ug/L		88.5	50-140			

OTTAWA - MISSISSAUGA - HAMILTON - KINGSTON - LONDON - NIAGARA - WINDSOR - RICHMOND HILL



Login Qualifiers :

Container and COC sample IDs don't match - Nutrients and metals bottles read TW1-1; chain of custody reads TW1-2.

Applies to samples: TW1-2

Sample Qualifiers :

1: A2C - Background counts greater than 200

QC Qualifiers :

- BAC14 A2C Background counts greater than 200
- QR-05 Duplicate RPDs higher than normally accepted. Remaining batch QA\QC was acceptable. May be sample effect.

Sample Data Revisions

None

Work Order Revisions / Comments:

None

Other Report Notes:

n/a: not applicable ND: Not Detected MDL: Method Detection Limit Source Result: Data used as source for matrix and duplicate samples %REC: Percent recovery. RPD: Relative percent difference. NC: Not Calculated Report Date: 22-Sep-2022 Order Date: 13-Sep-2022 Project Description: 22-1643-01

GPARACEL	Par	acel	ID:	2238202		Pa	(Lab	Order N Use O	Numb nly)	er Q		Cha	(Lab Us NO	Cust e Only 67	ody 014
Client Name: MCINTOSH Perry Contact Name: MONICA BIQOK Address:		Proje Quot	et Ref: e #:	Russ Bradle 22-334	ý	2.		1			1	Tu	Page rnarou	l_of Ind Tin	L ne
Telephone: 613 227 6953	- -	E-mail: m.black@mcintoshperry.com j.bowman @mcintoshperry.com						☐ 1 day ☐ 3 day ☐ 2 day 🕅 Regu Date Required:			□ 3 day				
	N	Matrix ' SW (Su	Type: Irface P (I	S (Soil/Sed.) GW (Water) SS (Storm/S Paint) A (Air) O (O	Ground Water) anitary Sewer) ther)					Re	quired	Analys	is		
□ Table 3 □ Agri/Other □ SU - Sani □ SU - Storm □ Table _ Mun: For RSC: □ Yes □ No	trix	Volume	f Containers	Samp	e Taken	div package,	FC,TC	e metals	1000	- 7. - 7.				12	
Sample ID/Location Name	N I	Air	0 #	Date .	Time	gins	Ľ,	Hall	_						
2 Tul 2	GW	/	9	13.09.22	10:40 AM	X	X	Х		-		_			
3	GW	/		13.09.22	2:35 PM	X	X	Х	X						
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$\frac{1}{10000000000000000000000000000000000$	aren	aw, (inhe	ated groundw	ater samples				1	Method	of Deliv	erv:	ภา	$\Big)$	
elinquished By (Sign): Ma A	ver/Des	oot:	. 1		Receiver	()	~		N	Verified	RE	100	SM		2
ate/Time: 13.09.22 4:06 om Temperature:	Ø	SP	Xe	2°C	Date/Tme Sep 17 Temperature: 17	2	2	17:0	\mathcal{O}_{μ}^{μ}	Date/Ti	me:	+1	4,2	12	8-



APPENDIX F: TRANSMISSIVITY, FARVOLDEN, AND MOELL CALCULATIONS, AND LANGELIER SATURATION INDEX (LSI) AND RYZNAR STABILITY INDEX (RSI) CALCULATIONS

McINTOSH PERRY

Cooper-Jacob Analysis: Calculations TW1 - 273-275 Russ Bradley Road

47.79 l/min Transmissivity TW1 (Drawdown) T = 2.3 Q / 4π Δ S Q = 47.79 L/min T = 2.3 (68.83 m3/day)/4π (20 m) Q = ((47.79 L/min)/(1000L))*(60 min)(24 hour)) T = 0.6 m2/day 7.29093E-06 m2/s Δ s = TW1 (Recovery) Δ s = T = 2.3 Q / 4π Δ S Q = 47.79 L/min

Q uses a weighted average from the pumping rates used within the pumping test.

Cumulative Average			
60 L/min	35	2100	
53.3 L/min	157	8368.1	
48 L/min	3	144	20062.1
42 L/min	225	9450	47.7669

T= 2.3 Q / 4	πΔS	Q = 47.79 L/mir	1	Total	20062.1
T= 2.3 (68.8	m3/day)/4π (25 m)	Q=((47.79 L/mii	n)/(1000L))*(60 min)(24 hour))	Cum. Average	47.7669 L/min
T= 0.5	m2/day	68	8.8 m3/day		
5.8327	74E-06 m2/s				
		Δs =	25 m		

Farvolden

Pumping Rate

Q20= 0.68 T Ha Sf

Ha=	the available water column heigh	t (m)		
Sf=	safety factor			
T=	Transmissivity (m2/day)		Avera	ge
		T= 0.5 m2/day	Recovery	0.55
		T= 0.6 m2/day	Drawdown	
TW1 (dra	wdown)	Safety Factor	0.7	
Q20= 0.6	8 (1.12 m2/day)(75.47 m)(0.5)			
		Rec'd Pump Settin	85.34 m	
Q20=	20 m3/day	static WL	9.87 m	
Q20=	19758 L/day	Ha (avail. head)=	75.47 m	
Q20=	14 L/min			

Moell

Q20 = (Q Ha Sf) / (s100 + 5 ∆s)

- Q= the pumping rate (m3/day)
- Ha= the available water column height (m)
- Sf= safety factor
- s100= the drawdown at 100 minutes (semi-log long-term graph)
- Δs = the change in hydraulic head over one log cycle (drawdown vs. log time)

TW1 (dra	wdown)			Q= Ha=	47.8 m3/day 75.47 m		
Q20= Q20= Q20= Q20=	((47.8 m3/day)(75.47 m 18 m3/day 17655 L/day 12 L/min)(0.7))/(43 m + 5(11.2 m)		Safety I	Factor s100 Δs	0.7 43 20	
<u>Hydraulic Conductivity</u> b = aquifer thickness T = transmissivity K = hydraulic conductivity			b=	109.12 m	e	end of casing =142 ft end of hole = 500 ft	43.28 m 152.4 m
K=T/b K=	6.68E-08 m/s 5.35E-08 m/s	Drawdown Recovery		9.3	5E-08		

Comments: Aquifer thickness of 109.12 m corresponds to the interval between the bottom of the casing and the bottom of the well (casing to 43.28 m BGS, WL at 9.87 mBTOC and end of hole at 152.4)

Langelier Saturation Index (LSI)

If LSI is negative: No potential to scale, the water will dissolve CaCO₃

If LSI is positive: Scale can form and CaCO₃ precipitation may occur

If LSI is close to zero: Borderline scale potential. Water quality or changes in

temperature, or evaporation could change the index.

The LSI is probably the most widely used indicator of cooling water scale potential. It is purely an pH is the measured water pH equilibrium index and deals only with the thermodynamic driving force for calcium carbonate scale formation and growth.

 $LSI = pH - pH_s$

Where:

pH is the measured water pH

 \mathbf{pH}_{s} is the pH at saturation in calcite or calcium carbonate and is defined as:

 $pH_s = (9.3 + A + B) - (C + D)$

Where:

 $A = (Log_{10} [TDS] - 1) / 10$ $B = -13.12 \text{ x } Log_{10} (^{\circ}C + 273) + 34.55$ $C = Log_{10} [Ca^{2+} as CaCO_3] - 0.4$ D = Log₁₀ [alkalinity as CaCO₃]

lest Well	1			
рН	7.9		А	0.143136
TDS	270		В	2.411629
Hardness	265		С	2.023246
Alkalinity	186		D	2.269513
Temp.	8.56			
pHs =				7.562007
LSI =				0.337993
RSI=				7.224013

Ryznar Stability Index (RSI)

RSI = 2(pHs) - pH

Where:

pHs is the pH at saturation in calcite or calcium carbonate

The empirical correlation of the Ryznar stability index can be summarized as follows:

RSI << 6 the scale tendency increases as the index decreases

RSI >> 7 the calcium carbonate formation probably does not lead to a protective corrosion inhibitor film

RSI >> 8 mild steel corrosion becomes an increasing problem.

Project No.: CCO-22-1643-01



APPENDIX G: INFILTRATION WORK SUMMARY FOR 273-275 RUSS BRADLEY ROAD

MCINTOSH PERRY

McINTOSH PERRY

September 7, 2022

To Whom it May Concern:

Re: Infiltration Work Summary for 273-275 Russ Bradley, Ottawa, ON

McIntosh Perry staff completed infiltration testing on June 7, 2022, at the locations shown on Figure 1, below. A Guelph Permeameter (a constant head permeameter used to measure in-situ vertical hydraulic conductivities of soil) was set up in three separate locations (TP1, TP2, TP3) for a total of three double-head infiltration tests. Additional tests were attempted (TP4, TP5) however a majority of the proposed development area was saturated and deemed unsuitable for testing. Test locations were selected based on the permeability of soils and subsequent capacity to complete the infiltration testing. In this case, only one (1) hole (TP1) was completed within the proposed infiltration area, while the remaining (TP2, TP3) were completed in close proximity to Carp Road – outside of the desired infiltration area. Holes were advanced using a hand auger.



Figure 1 – Guelph Permeameter Test Locations

Where possible, each infiltration test consisted of at least a 5-7 cm head test, based on the level of saturation and presence of water in each hole where testing was attempted. Water was added to the Guelph Permeameter reservoir and allowed to infiltrate into the soil at the specified head pressure. Changes in reservoir water level (h) were recorded at regular intervals and normalized for change in time (t). Each test was considered complete when dh/dt (change in head / change in time) reached a steady-state for at least three consecutive measurements.

Appendix C.2 of the Toronto Region Conservation Authority's (TRCA) Stormwater Management Criteria (August 2012) provides guidance on the calculation of infiltration rates using field saturated hydraulic conductivity (K_{fs}). The recommended calculation is as follows:

 $K_{fs} = (6 \times 10^{-11}) (I^{3.7363})$

Where:

- K_{fs} is the field saturated hydraulic conductivity (in cm/s), as measured by a Guelph Permeameter, double-ring infiltrometer, single-ring infiltrometer, or other accepted method
- I is the infiltration rate (in mm/hr)

Based on the above calculation, the estimated soil infiltration rate (I) from the data collected at TP1, TP2, and TP3 is shown in the table below.

Borehole ID	K _{fs} cm/s	Corrected I* (mm/hr)
TP1	3.4 x 10 ⁻⁶	5.35
TP2	1.02 x 10 ⁻⁷	2.09
TP3	4.9 x 10 ⁻⁷	3.18

Table 1: Infiltration Rates

*Includes a safety factor calculated per TRCA guidance

As shown, the highest infiltration rate was observed in TP1 at a depth of approximately 0.05 m bgs (approximately 113.85 m asl). The lowest infiltration rate was observed in TP2 at a depth of approximately 0.15 m bgs (approximately 113.75 m asl). These values are generally consistent with the observed stratigraphy, in that fine-grain materials will typically have lower hydraulic conductivity rates.

It is noted that the field infiltration testing for TP2 and TP3 were conducted outside of the proposed infiltration infrastructure area, and are situated in close proximity to Card Road. Based on Site observations from June 7 and August 30, 2022, the property and development area appear to be highly saturated, with many areas of stagnant standing water. In particular, the wooded area of the Site appears to be a local topographic low point, and is not considered suitable for infiltration trenches or galleries in its current state. In several instances where infiltration tests were attempted, excess water logging caused no movement in the water column. As noted above, additional testing was done in subsequent holes TP2 and TP3 within an area closer to Carp Road.

TP2 and TP3 were advanced to depths of approximately 0.15 and 0.2 m bgs, respectively. The soil stratigraphy was consistent at all depths, consisting of wet, silty sand with trace clay.

It is McIntosh Perry's opinion that at this particular Site, alternate options for stormwater management should be investigated. It is expected that any infiltrative solutions to stormwater management will be hampered by high groundwater levels, standing water, and fine-grained overburden that is not conducive to infiltration.

Sincerely,

Original Signed

Jordan Bowman, P.Geo., P.Biol. Manager (Geo-Environmental) (613) 714-4602 j.bowman@mcintoshperry.com



APPENDIX H: GRAIN SIZE ANALYSIS

MCINTOSH PERRY


GRAIN SIZE DISTRIBUTION TEST DATA

Client: Trever Watkins Project: 273&275 Russ Bradley Rd. Project Number: CCO-221643-01 Location: TP SS-2 Depth: 25cm-1m Sample Number: SS-2 Material Description: Silty/Clayey Sand some fine Gravel Sample Date: Nov 24,2022 Date Received: Nov 24,2022 Tested By: R.C Test Date: Nov 28,2022 Checked By: J.Hopwood-Jones Title: Lab Manager

Sieve Test Data										
Dry Sample and Tare (grams)	Tare (grams)	Cumulative Pan Tare Weight (grams)	Sieve Opening Size	Cumulative Weight Retained (grams)	Percent Finer	Percent Retained				
926.14	0.00	0.00	26.5mm	0.00	100.0	0.0				
			19.0mm	7.84	99.2	0.8				
			16.0mm	22.03	97.6	2.4				
			13.2mm	46.69	95.0	5.0				
			9.5mm	73.48	92.1	7.9				
			4.75mm	116.36	87.4	12.6				
			2.36mm	149.73	83.8	16.2				
			1.18mm	188.07	79.7	20.3				
			0.600mm	248.42	73.2	26.8				
			0.300mm	345.28	62.7	37.3				
			0.150mm	495.39	46.5	53.5				
			0.075mm	656.59	29.1	70.9				
			Fractional C	omponents						

Cobbles	Gravel				Sa	nd	Fines			
	Coarse	Fine	Total	Coarse	Medium	Fine	Total	Silt	Clay	Total
0.0	0.8	11.8	12.6	4.4	14.3	39.6	58.3			29.1

D ₅	D ₁₀	D ₁₅	D ₂₀	D ₃₀	D ₄₀	D ₅₀	D ₆₀	D ₈₀	D ₈₅	D ₉₀	D ₉₅
				0.0777	0.1158	0.1723	0.2630	1.2299	2.9939	7.0505	13.2424

Fineness Modulus

1.75

2022-11-29