

LeBreton Library Parcel

Constructability Report

December 2022 | TYLin Ref. 10399 **Dream Asset Management**







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1 INTRODUCTION

TYLin has been retained by Dream Asset Management to compile a Constructability Report for the proposed redevelopment of the LeBreton Library Parcel (LBLP), located at 665 Albert Street, Ottawa, Ontario ("the site").

The intent of this report is to consolidate project information relevant to protection of existing buried City infrastructure in the vicinity of the site – and to document the proposals in place for the necessary protection of this infrastructure through the construction and operation of the redeveloped site.

The report should be read in conjunction with supporting Site Plan Application materials – including, but not limited to the Geotechnical Investigation Report, Site Servicing/Grading drawing package, as well as the Architectural and Landscape Architecture drawing sets.

1.1 Existing Infrastructure

In existing conditions, the site generally consists of hard-packed gravel areas used for vehicular access – understood to remain from its previous use as a construction staging area for the City's Stage 1 Light Rail Transit (OLRT) project. The site generally falls to the north and slopes down relatively steeply along the northern edge to the elevation of the OLRT tracks.

The key pieces of City infrastructure in the vicinity of the project site are:

- ▶ 2400 mm internal diameter concrete sewer pipe ("EWT", East-West Tunnel), which crosses the northwest corner of the site and connects the diversion chamber within Booth Street to the Combined Sewer Storage Tunnel (CSST) east of the site.
 - As per City as-built drawings provided (and through reference to the City's GeoOttawa online portal data) the invert elevation of this pipe at the western edge of the site is approximately 45.7 m (and it drops at around 0.25% as it runs east).
- ▶ 1800 mm internal diameter concrete Interceptor Outfall Sewer (IOS) trunk sanitary sewer, which crosses the northwest corner of the site.
 - ▶ With reference to the City's GeoOttawa online portal data, the invert elevation of this IOS pipe at the western edge of the site is approximately 44.8 m (and it drops as it runs east).
- ▶ 3000 mm internal diameter concrete storm sewer pipe, which crosses the northwest corner of the site before turning north and passing below the OLRT tracks.
 - ► As per City as-built drawings provided (and through reference to GeoOttawa) the invert elevation of this pipe at the western edge of the site is approximately 46.7 m





(and it drops at around 0.25% as it runs east).

▶ 1220 mm internal diameter steel high pressure water main (HPWM) running east-west with Albert Street, to the south of the site.

Please refer to **Figure 1-1** for illustration of the existing infrastructure described above, relative to proposed site plan development.

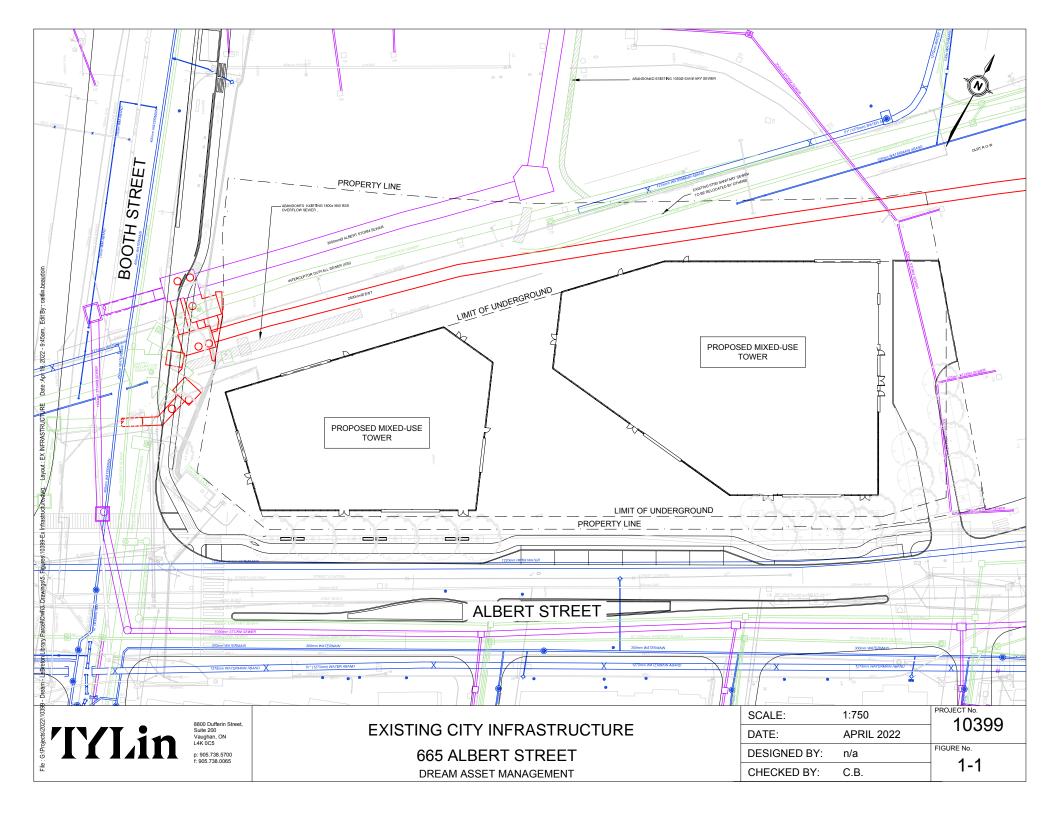
1.2 Existing Geotechnical Conditions

Golder Associates Ltd. completed a Geotechnical Investigation for the site (Golder Report Ref. 22511882, dated April 2022). The report describes the results of fieldwork investigations undertaken on site – including 6 no. boreholes (BHs) previously completed by Golder as part of a previous assignment on the project site in 2011, supplemented by an additional 5 no. BH locations advanced in February 2022.

The study documents a subsurface stratigraphy within the project area of surficial fill materials overlying glacial till, which in turn overlies limestone and shale bedrock.

- ▶ **Fill Material** was encountered in each of the boreholes from ground surface (to depths ranging from 2.1 to 3.7 m below the existing surface) generally heterogeneous in nature ranging from silty sand to sand. The fill also contained gravel, brick fragments, concrete and mortar fragments, glass, wood and layers of organic material and clay as well cobbles and boulders encountered during drilling. Testing indicated that the fill has a highly variable very loose to very dense state of packing.
- ▶ **Glacial Till** deposits were encountered beneath the fill material at all boreholes, typically consisting of a heterogeneous mixture of gravel, cobbles, and boulders in a matrix of sand and silt with a trace to some clay. The 2011 boreholes did not fully penetrate the till layer, however the five boreholes drilled during the 2022 investigation were all extended through the till and into the underlying bedrock, confirming the till extended to depths of 11.2 to 14.7 m below existing ground. Standard penetration testing indicated that the majority of the till has a dense to very dense state of packing.
- ▶ **Bedrock**: The 2011 boreholes were all terminated at refusal at depths of 4.2 m to 10.0 m below existing surface, however it is considered unlikely that these refusals were the result of encountering bedrock. The 2022 boreholes were extended through the glacial till deposit into the underlying bedrock and provided elevations of between 48.2 m and 50.5 m (masl) for bedrock elevation. The bedrock consists of limestone with shale interbeds of the Verulam formation.
- ► **Groundwater** levels have been measured (February 2022) at elevations ranging from 48.7 m to 55.1 m (masl), although it is noted that these elevations will vary seasonally.







2 PROPOSED SITE DEVELOPMENT

2.1 Overview

The proposed site development consists of two towers over low-rise podium structures, with a single two-level basement structure extending over the footprint of both towers. Vehicular access to the site will be via an extension of Empress Avenue at the eastern edge of the site (north off Albert Street) and into the basement via a ramp in the north-east corner of the structure. The current architectural design proposals have set the finished elevation of the P2 basement level 8.7 m below finished ground floor of the new structure (at 54.0 m).

The majority of the ground-level space outside the new buildings will be non-vehicular public realm. A new retaining wall structure will address the grade change between plaza level (which is continuous with Booth Street) and the new multi-use pathway (MUP) running east-west alongside the OLRT line (and passing below Booth Street) along the north edge of the site.

The podiums will contain a variety of commercial and community uses at lower levels, before a shared terrace area marks the transition to the residential apartments in the towers. The residential component will include a high proportion of affordable housing units.

Please refer to the associated Architectural drawing set (Perkins & Will and KPMB) for full details of the proposed development, and the Landscape Architectural set (PFS) for at-grade public realm design. The TYLin/TMIG engineering drawing set shows proposed grading and servicing details.

2.2 Site Grading

In the current (vacant) site conditions the lands fall to the north; at a relatively gentle grade initially, but with a steeper slope as the site approaches the OLRT corridor and transitions down to track level. Grades at the Albert Street interface are currently between 62 and 63 m, dropping to around 61 m at the top of the existing embankment, and interfacing with existing OLRT track level at approximately 56 m along the north property limits. There is a small existing retaining wall along the west edge of the site to manage grade differential between the Booth Street sidewalk elevation and the site grades. There is also an existing gabion basket wall in the northeast corner of the site constructed as part of the City's OLRT works – further discussion on this is provided in the following **Section 2.3**.

In proposed conditions the site will be raised to provide a flatter, plateau area for tower construction and surrounding public realm (also facilitating at-grade connection into the site from Booth Street). Proposed grading will tie-in to existing Albert Street elevations along the





southern limits and the finished grade will generally be maintained at elevations between 62 and 63 m throughout. As noted above, a retaining wall is proposed to manage the grade change from the public realm to the MUP (adjacent to the OLRT). The wall will be around 6-7 m high at the west end, tapering down to the east (as the MUP elevation rises to meet the site grades). These proposals will result in finished grades being raised by between 1 and 3 m over the northern portion of the site.

Appendix A contains the Site Grading plan for reference.

2.3 Retaining Walls & OLRT Interface

As described above, two retaining wall structures are required to manage the elevation transitions along the northern edge of the site. The first one of these is set back within the property limits and will separate the public realm area from the MUP running east-west along the OLRT interface. It will be approximately 7m high at the Booth Street end and taper down to zero as it runs east (and the MUP rises). Construction proposals for this structure are still being advanced, however current design intent is to use a precast block product engineered through a supplier-design arrangement.

The second retaining wall will be located directly along the property limits, managing the grade difference between the MUP (as it drops to pass below the Booth Street Bridge) and the OLRT lands to the north. As noted previously, there is an existing gabion basket wall in the north-east corner of the site (understood to have been constructed during Stage 1 OLRT works) partially fulfilling this function based on existing site grades. To implement the MUP connection, this existing retaining structure needs to be extended, both vertically and horizontally (to the west). Noting that this MUP connection along the north edge of the site has been planned for a number of years (per NCC Master Plan requirements), the LBLP team would welcome confirmation from City staff as to whether any allowances were made during initial design/construction of the gabion wall to facilitate future extension. If available, the team would seek to incorporate these allowances as part of the proposed design, to ensure the works can be completed in an expedient and cost-effective manner.

Appendix B contains drawings extracted from the Landscape Architecture package that show sections through the retaining wall proposals along the north edge of the site.

2.4 Air Ducts

To serve HVAC systems for the new building, an air vent structure is required to connect plant rooms at the first basement level to louvres on the face of the retaining wall to the north. The Project Mechanical Engineer (Smith & Anderson) has developed minimum cross-sectional area





requirements for these conduits (6.3 m² enlarging to 11.0 m² at the retaining wall face), and the team is currently developing proposals for their construction. Current intent is that precast box culvert sections will be used to create the connection. These proposals are noted here only in the context of providing an overview of all works being undertaken in the north portion of the site (crossing the deep City services).

Appendix C contains a copy of the Architectural Site Plan drawing with the Air Duct features highlighted, for reference.

2.5 Albert-Slater Reconstruction Project

It is noted that the City is currently at a relatively advanced stage in terms of planned reconstruction works for Albert Street, as part of the Albert-Slater Reconstruction Project. It is understood that there are two ongoing projects associated with this, and that the split of work occurs just west of Empress Avenue – works along Albert Street east of this point are ahead in terms of schedule, with works to the west following as part of a second design/construction process.

The LBLP design team are in the process of developing proposed modifications to the City's current Empress/Albert intersection design, to incorporate the north extension of Empress, an eastbound left turn lane, as well as the required signalization updates. These plans will be shared with City staff for review and approval via the established contacts within the Albert-Slater Reconstruction team.

Coordination is also ongoing with City staff engaged on the Albert-Slater works west of Empress. Current design plans for the LBLP site (and adjacent streetscape for frontages along Albert and Booth) have been shared with City staff here, and the understanding is that the City design will seek to incorporate these aspects as their design develops. The LBLP team will remain available to City staff in this regard to facilitate any further coordination necessary as proposals are advanced.

2.6 Albert-Booth Vault Infrastructure

The design team are aware of existing City infrastructure within the streetscape at the north-east corner of the Albert-Booth intersection (i.e. south-west corner of LBLP site), consisting of padmounted vents and control cabinet, as well as a subsurface vault. As illustrated in **Figure 2-1** (extract from Landscape Architecture Site Plan in south-west corner of the site), the design proposals have been developed to allow these features to be maintained unaffected by the works. **Appendix D** contains a drawing extracted from the Architectural package illustrating showing this City infrastructure relative to new basement construction in both plan and section.





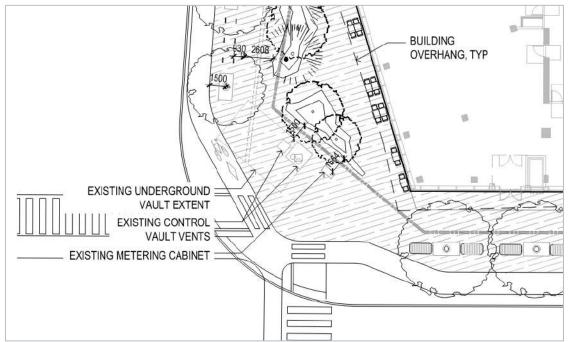


Figure 2-1 Albert-Booth Proposed Landscape Layout

2.7 Sewer Heat Recovery System

It is noted that proposals are being developed to implement a Sewer Heat Recovery system as part of the LBLP project, using the deep trunk sewers as heat sinks for the building's heating and cooling needs. These proposals are being advanced on behalf of Dream by Eequinox, with support on the Civil Engineering aspects (E.g., access chambers from surface level) from Stantec. For further details on this proposed system, reference should be made to separate discussions with City staff.



3 INFRASTRUCTURE PROTECTION REQUIREMENTS

For the Albert Street HPWM, initial City Engineering feedback provided on the bid-level submission (comments document dated December 2021) requested a 6-9 m setback from the water main, depending on depth and soil conditions. The document also noted that Vibration and Settlement Monitoring Programs will be required during construction (to be prepared by a specialist Vibration Monitoring Engineer and Geotechnical Engineer, respectively).

City staff have subsequently provided specific requirements for the Settlement and Vibration Monitoring Program, as well as confirming that the applicable limit would be a maximum vibration of up to 15 mm/s for frequencies exceeding 40 Hz (noting that exceedances require work to be ceased immediately and the City to be notified within 2 hours). Please refer to **Section 4.2** for further discussion.

It is also noted that the team has reviewed the City of Ottawa *Infrastructure Build Over Policy* document (dated January 21, 2014 and understood to have been provided as a report to Planning Committee and Council during the Confederation Line Stage 1 OLRT project). This report is supportive of Transit-Oriented Development (TOD) such as the Library Parcel project, and the recommendations direct City staff to implement a uniform, risk-based approach to the assessment of development applications that build over (or adjacent) to City infrastructure. However, no *specific* protection requirements appear to be set out in this document that would dictate provisions for the buried pipework crossing the north-west corner of the site – including the 2400 mm diameter Combined EWT Sewer Pipe (CSST connection), 1800 mm diameter Interceptor Outfall Sewer, or the 3000 mm diameter storm sewer pipe. The team therefore looks forward to working with City staff – through review/comments on this initial report and any necessary subsequent meetings – to develop a reasonable set of infrastructure protection proposals that address City concerns while advancing the project.





4 PROPOSED PROTECTION MEASURES

4.1 Setbacks and Temporary Shoring Design

As illustrated below in **Figure 4-1** the proposed basement structure along Albert Street is horizontally set back from the HPWM by a minimum of 9.0 m along the majority of the project frontage. There is an inflection point in the basement wall alignment close to the south-east corner where the setback temporarily reduces to approximately 7.7 m, however the proposals are considered compliant with the City requirement for a 6.0 to 9.0 m setback.

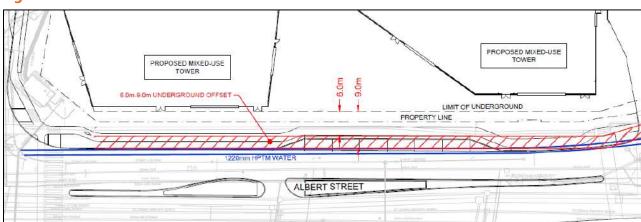


Figure 4-1 Albert Street HPWM Setback

Through discussion with the project construction partner (Ellis Don) it is understood that current intent is to provide perimeter shoring along Albert Street and Booth Street – created by driven H-piles, with standard strand cable tiebacks and walers – with the remainder of the basement extent to be constructed via open cut. While this represents the current planned approach, it is noted that construction approach remains subject to change as the design progresses and more information becomes available.

For reference, **Appendix E** contains the current shoring design package and **Appendix F** contains the current Ellis Don Construction Logistics Plan. Note that this information will continue to be developed as construction plans are advanced and updates will be provided as needed.

4.2 Settlement and Vibration Monitoring

As noted in **Section 3**, City staff have provided specific requirements for the Settlement and Vibration Monitoring Program, as well as confirming that the applicable limit would be a





maximum vibration of up to 15 mm/s for frequencies exceeding 40 Hz (noting that exceedances require work to be ceased immediately and the City to be notified within 2 hours). The City requirements received are as follows:

In order to help ensure the integrity of the high-pressure transmission main located close the west boundary of the site carries a significant portion of the entire water supply for the City of Ottawa, the Owner acknowledges and agrees to undertake the following:

- 1. A site-specific Settlement and Vibration Monitoring Program (the "Program") shall be developed and stamped by a professional Engineer in the province of Ontario and shall be submitted to the City for their review and approval before the inclusion of the Program in the contract documents.
- 2. Should monitoring levels of vibration and underground soil movement exceed the maximum limits outline in the Program, the Owner agrees to cease all construction activities immediately, and will take necessary correction option and at the same time will report to the City immediately and will resubmit a revised work plan and Program to the City.
- 3. In the event that the levels of vibration momentarily exceed the maximum limits outlined in the submitted report/plan but the Owner's on-site consultant is of the professional opinion that no danger exists, the Owner may continue to proceed with the work by a different means, consistent with the report, that does not further cause the levels of vibration /settlement to exceed the maximum limits outlined in the Program. Priors to so proceeding with the work, the exceedance shall be reported to the Construction Services Branch of the City.
- 4. In the event of any requirement for emergency repairs of this transmission main, the Owner shall reimburse the City for the cost of such repair to the satisfaction of the General Manager, Planning, Real Estate and Economic Development Department.
- 5. The City reserves the right to issue a stop work order for the construction in the event of an incident which would adversely affect the City's requirement to provide safe drinking water. This may include, but is not limited to, a leak or failure of the high pressure transmission main and /or a failure at one of the water purification plans. Where the stop work order is for a period of 24 hours or less, the City is not responsible for any delay claim billed by the developer. No inference of liability is to be taken from these conditions for any period longer than 24 hours.
- 6. A certificate of liability insurance shall be submitted to the City wherein the Owner is the named insured and the City of Ottawa is an additional insured. The limits of the policy shall be in the amount of \$25,000,000 and shall be kept in full force and effect for the term of the construction work.





The LBLP team acknowledges these requirements and commits to developing the required site-specific Settlement and Vibration Monitoring Program and submitting for City review/approval prior to the work being included in contract documents. We note that the construction team has recent experience working under similar constraints within the City of Ottawa and does not foresee any issues maintaining compliance with these requirements.

4.3 Structural Loading

Please refer to **Appendix G** for further details of the proposed structural/foundation design, developed by the Project Structural Engineer (RJC) in conjunction with the Project Geotechnical Engineer (Golder) – this appendix includes a drawing set showing current foundation design alongside estimated locations of City services (specifically EWT and IOS pipes), in both plan and section.

In summary though, the proposed structure will be supported on reinforced concrete caissons drilled down and socketed into the bedrock for all heavily loaded tower structural elements. For the lightly loaded columns and walls, smaller "pipe piles" drilled and socketed to rock will be provided. No conduits pass beneath the footprint of the proposed building. The closest service (2400mm diameter EWT concrete sewer pipe) runs approximately parallel to the north foundation wall with an invert elevation of approximately 45.6m and maintains a horizontal clearance from the proposed foundation wall of between 3 and 10m.

In accordance with Geotechnical recommendations, the deep foundation system underneath the foundation wall and adjacent columns will be socketed 1m into the bedrock, hence loading the rock in friction approximately between elevation 47m and 48m. Based on the provided as-built drawings of the existing services, the minimum horizontal distance from the buried pipe to the edge of the caisson is at least 3m (refer to RJC drawings S198-S198E-S198W-S702 included in the appendix). The invert elevation of the pipe is around elev. 45m, providing a minimum 1H:1V slope from the invert to the highest point of application of the deep foundation force in the rock. Based on Geotechnical recommendations, these conditions should not impose any significant stress increase to the existing services.

The team acknowledges receipt of City comments on the initial issue of the Constructability Report (transmitted by email on November 8th 2022), comprising a memo by Stantec with comments on various aspects of the project in relation to CSST Infrastructure. Please refer to **Appendix H** for a copy of the Stantec memo, along with a response memo from Golder describing additional analyses undertaken and point-by-point responses to the Stantec comments.





4.4 Pre and Post Construction CCTV Surveys

As per City requirements, the contractor will be responsible for undertaking pre and postdevelopment CCTV surveys of the identified buried infrastructure crossing the project site to document the existing conditions and demonstrate that works were completed without damage to City infrastructure.





5 CONCLUSIONS

This Constructability Report is provided to document the presence of existing buried City infrastructure crossing (or in close proximity to) the project site, and to summarize the current design/construction intent with respect to protection of these existing City assets through development. The LBLP team remains available to engage with City staff following their review of this submission to discuss and refine the proposals as needed to advance the project.

Respectfully submitted,

On behalf of TYLin,

Ben Worth, P.Eng.

Senior Project Manager

Disclaimer:

This report includes numerous references to investigations, findings and recommendations of third parties – specifically, from the project Geotechnical Engineer (Golder Associates Ltd.), the project Structural Engineer (RJC Ltd.), and the project construction partner (Ellis Don). This information is consolidated in the Constructability Report for the purposes of City review, however TYLin does not take responsibility for the approval, validation, or ownership of these recommendations from third parties.





APPENDIX A

Site Grading Plan





LEGEND | SEE ABBREVIATIONS BELOW

____ LIMIT OF UNDERGROUND STRUCTURE PROP ELEVATION TO MATCH EXISTING EMERGENCY OVERLAND FLOW ROUTE

MH / CBMH / DCBMH / OGS □ □ ⊠ Ø CB/DCB/AD/TD

+ HYDRANT / SIAMESE / VALVE BOX

BENCHMARK: ELEVATIONS ARE GEODETIC, IN METRES, AND DERIVED FROM THE CAN-NET VRS NETWORK MONUMENT: OTTAWA BEARINGS ARE GRID, DERIVED FROM THE CAN-NET VR NETWORK OBSERVATIONS ON NCC HORZ CONTROL MONUMENTS 19773035 & 19680191, CENTRAL MERIDIAN, 76°30' W LONGITUDE MTM ZONE 9 DRAWING NOTES

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. THE CONTRACTOR SHALL VERIFY ALL DIMENSIONS, ELEVATIONS, INVERTS AND DATA ON SITE AND REPORT ANY DISCREPANCIES OR OMISSIONS TO TMIG 48 HOURS PRIOR TO ANY CONSTRUCTION.

ABBREVIATIONS | | TW = TOP OF WALL BW = BOTTOM OF WALL CONC = CONCRETE MH = MAINTENANCE CB = CATCH BASIN DCB = DOUBLE CATCH AD = AREA DRAIN TD = TRENCH DRAIN

DRAWN BY: B.G.

DESIGNED BY: B.G. CHECKED BY: B.D. **KPMB**

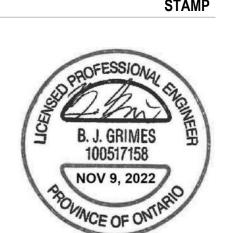
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Ottawa, ON

GRADING PLAN

SHEET NUMBER

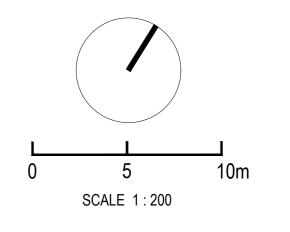
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Site Plan Control Application File Nos.: D01-01-22-0005, D02-02-22-0041 & D07-12-22-0069



APPENDIX B

Landscape Architecture Drawings (Retaining Walls)





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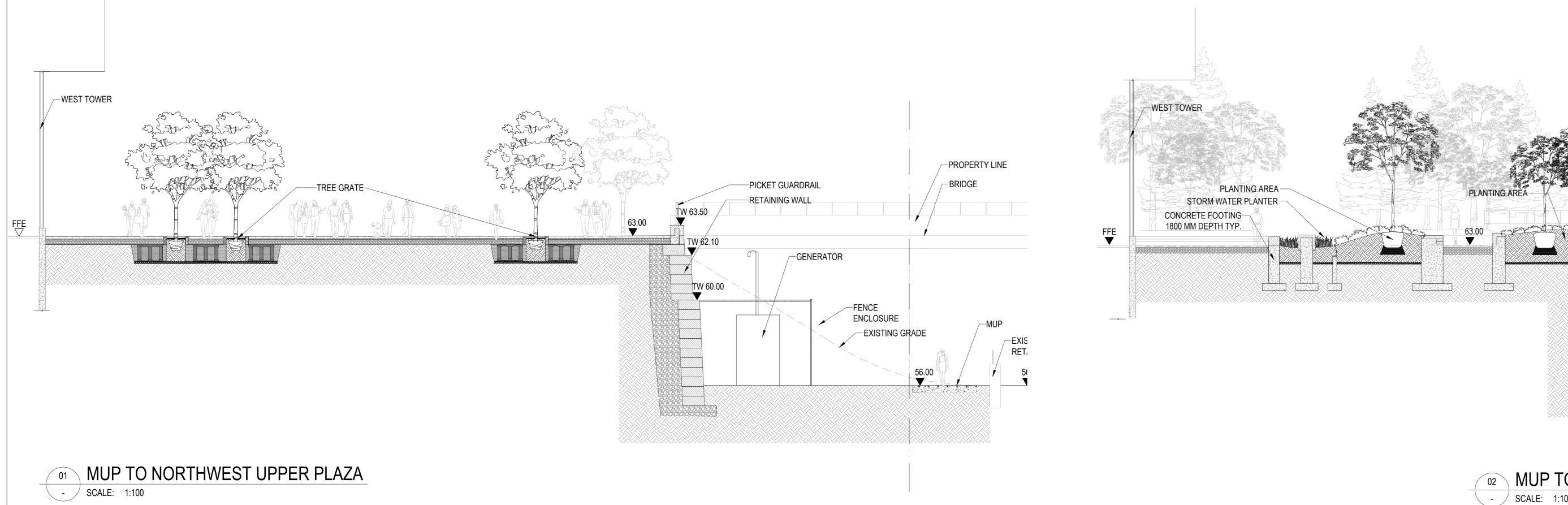
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TITLE

SECTION

L08-10



MUP TO NORTHWEST UPPER PLAZA - SCALE: 1:100

PROPERTY LINE

PROPOSED FENCE

EXISTING FENCE

PROPOSED GABION WALL

56.00 LRT

—PLANTING AREA

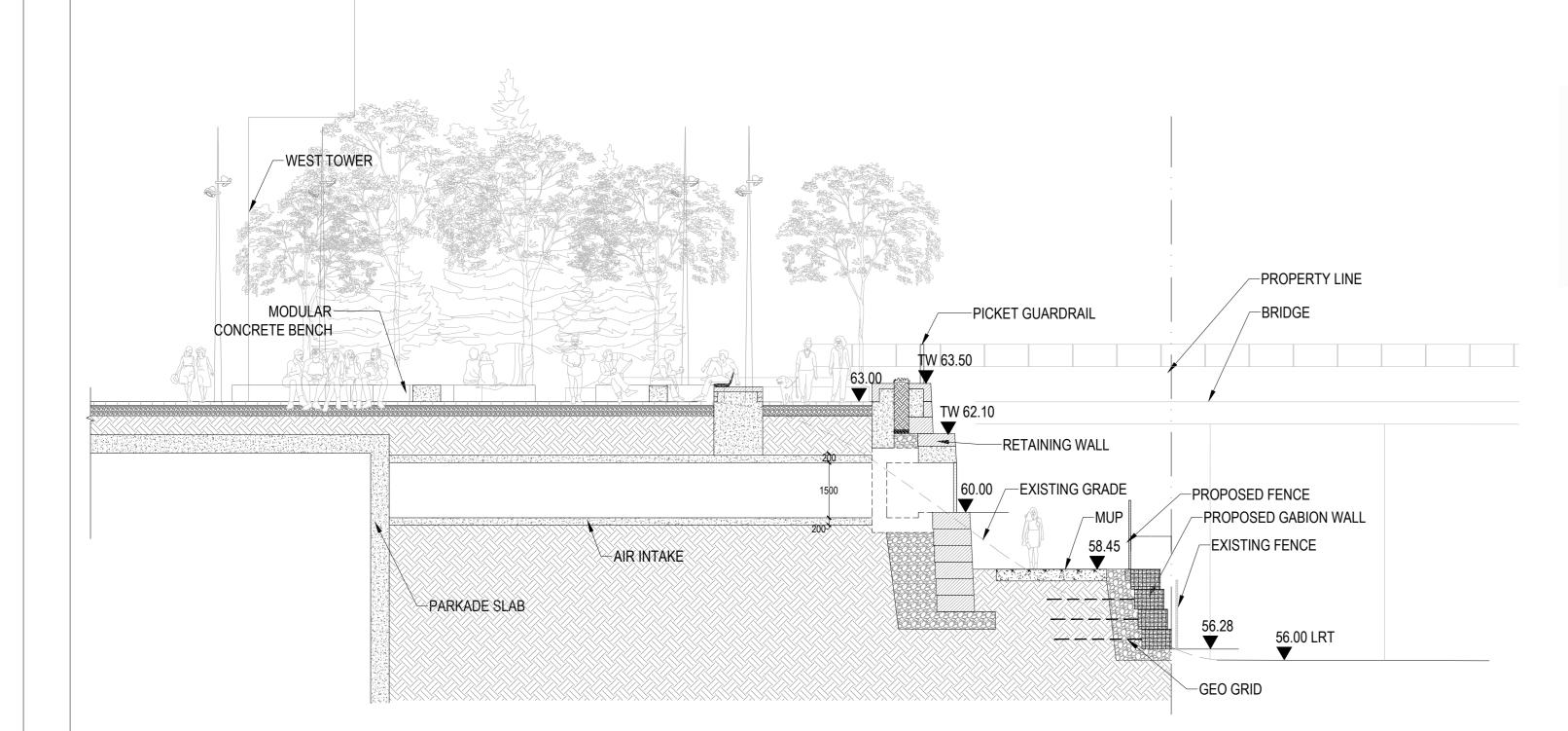
—PICKET GUARDRAIL

RETAINING WALL

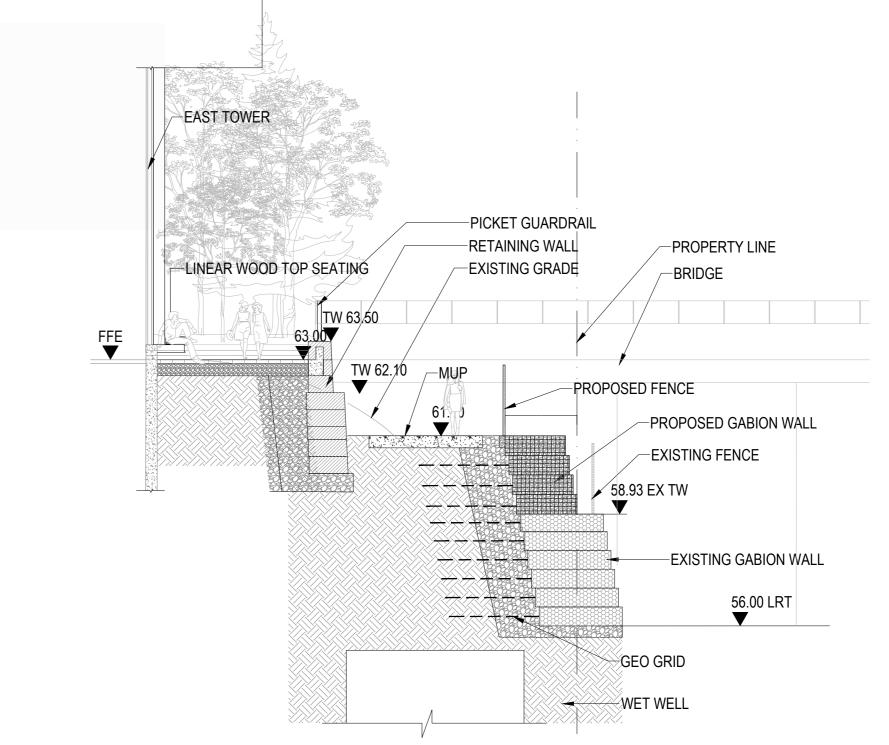
 $\neg \mathsf{MUP}$

—PICKET GUARDRAIL

RETAINING WALL







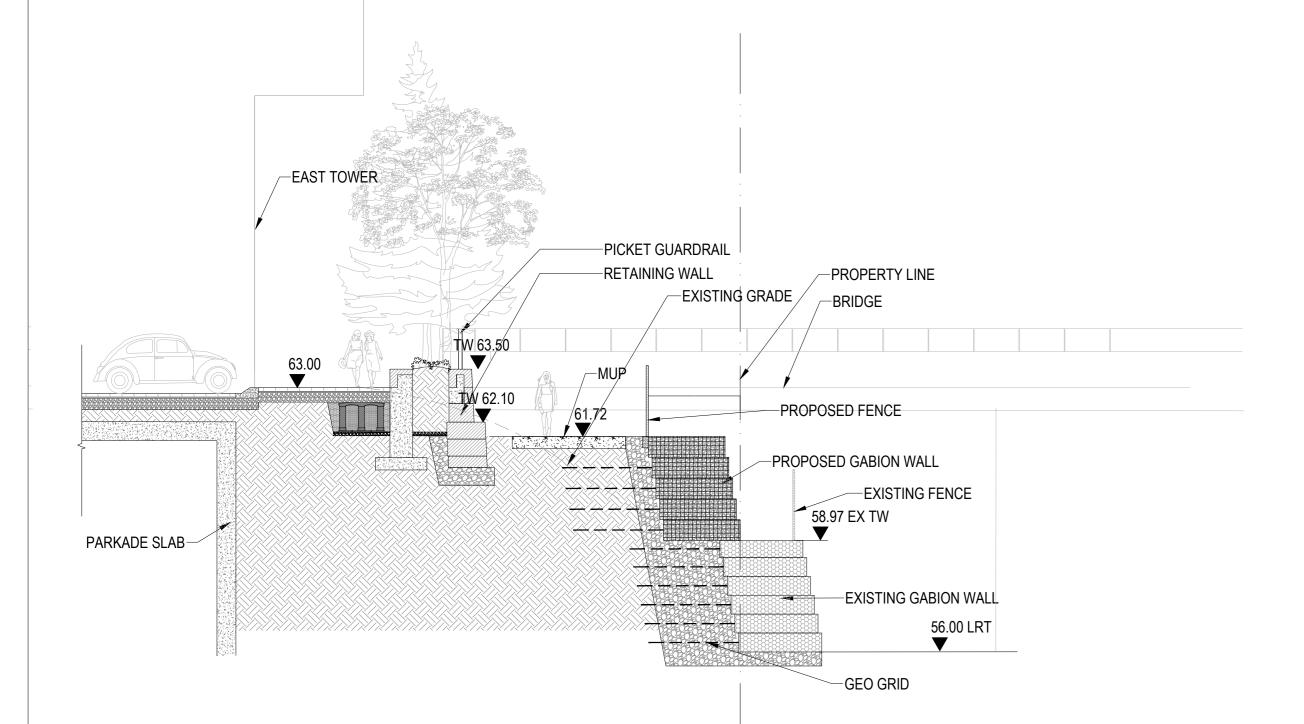
-PROPERTY LINE

PROPOSED GABION WALL

EXISTING FENCE

GEO GRID

MUP TO NORTHEAST UPPER PLAZA - SCALE: 1:100



MUP TO NORTHEAST UPPER PLAZA

SCALE: 1:100

ISSUE CHART

KPMB

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CONSULTANT

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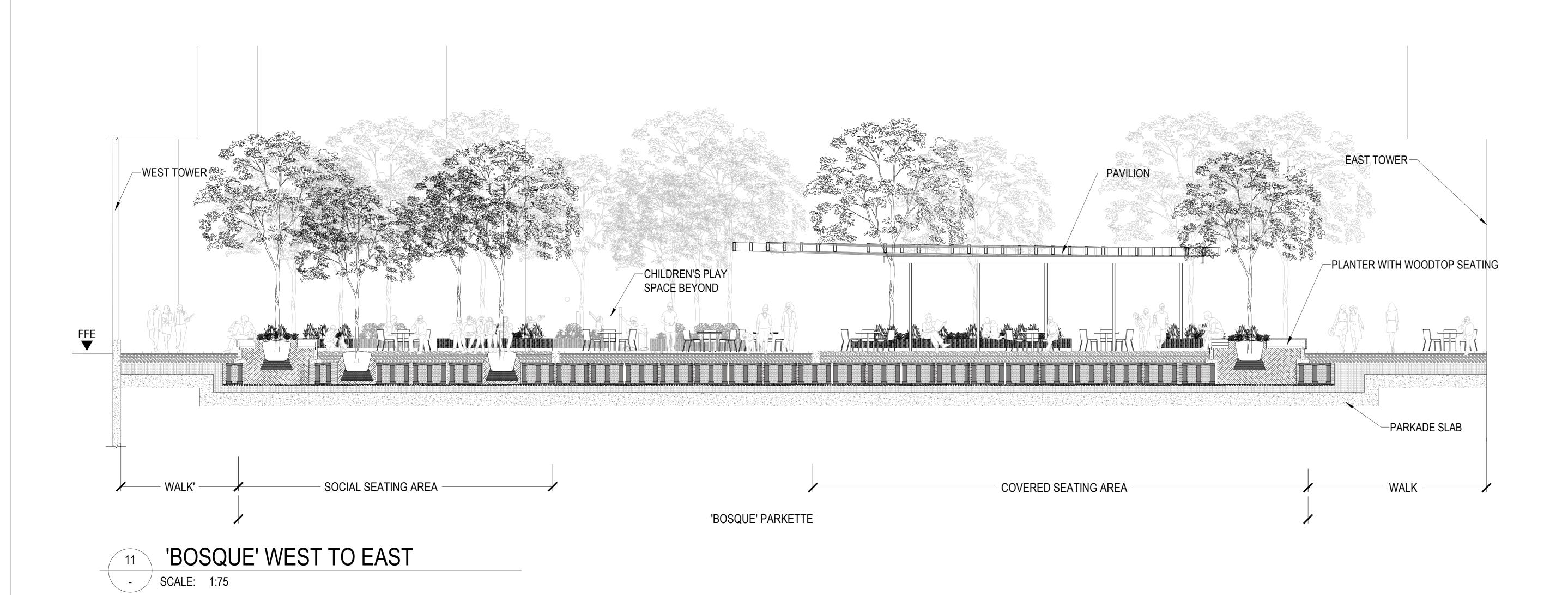
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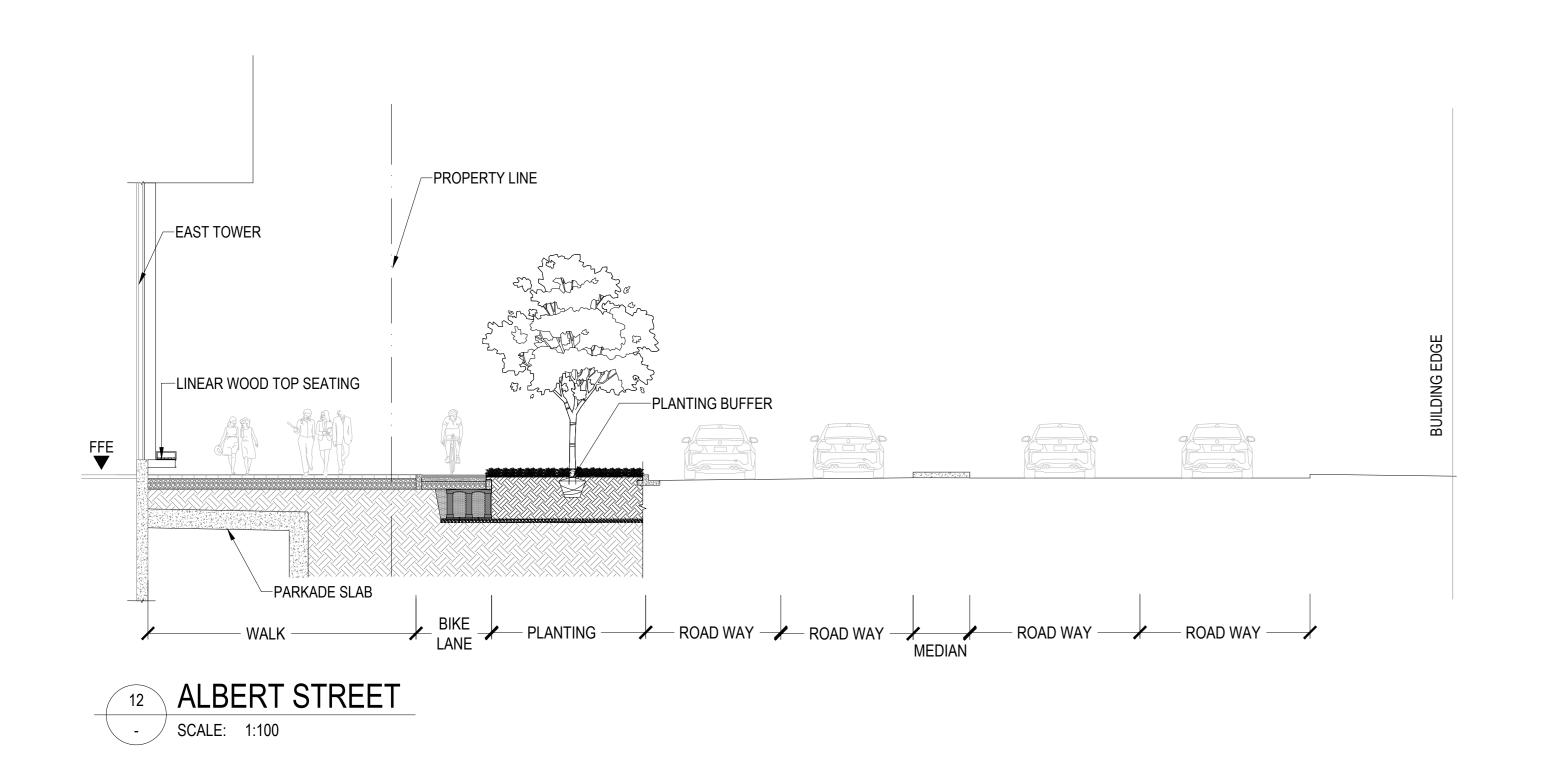
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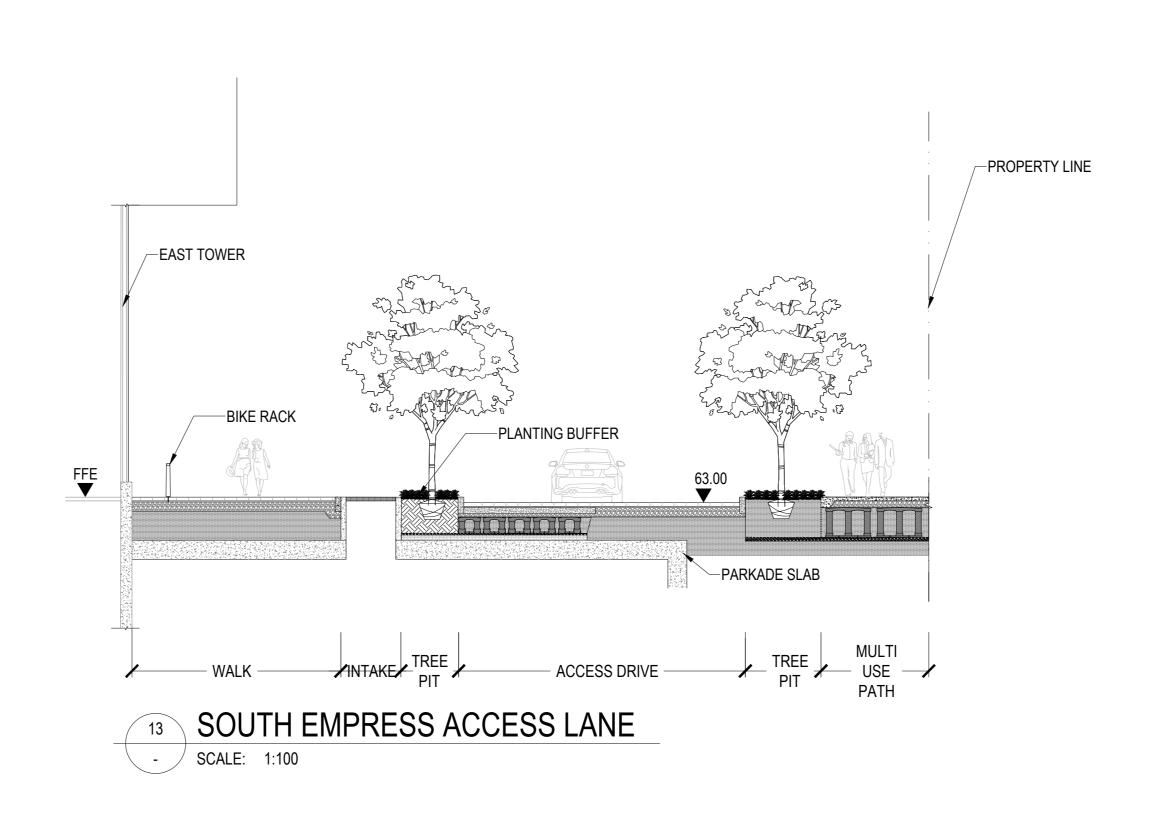
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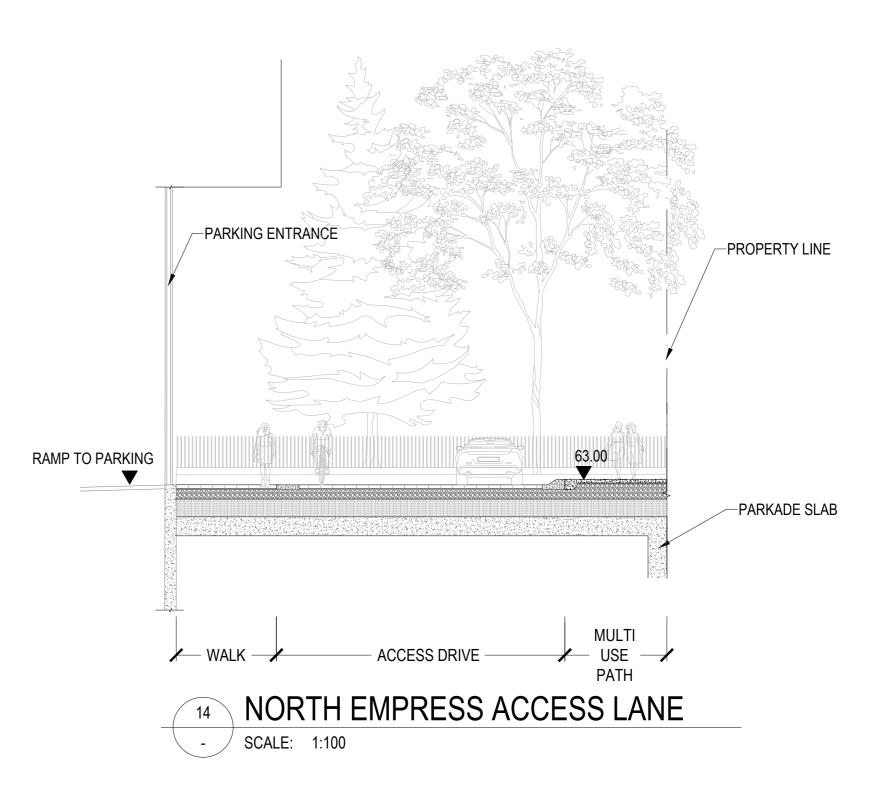
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Site Plan Control Application File Nos.:D01-01-22-0005,D02-02-22-0041 & D07-12-22-0069

TITLE

SECTION

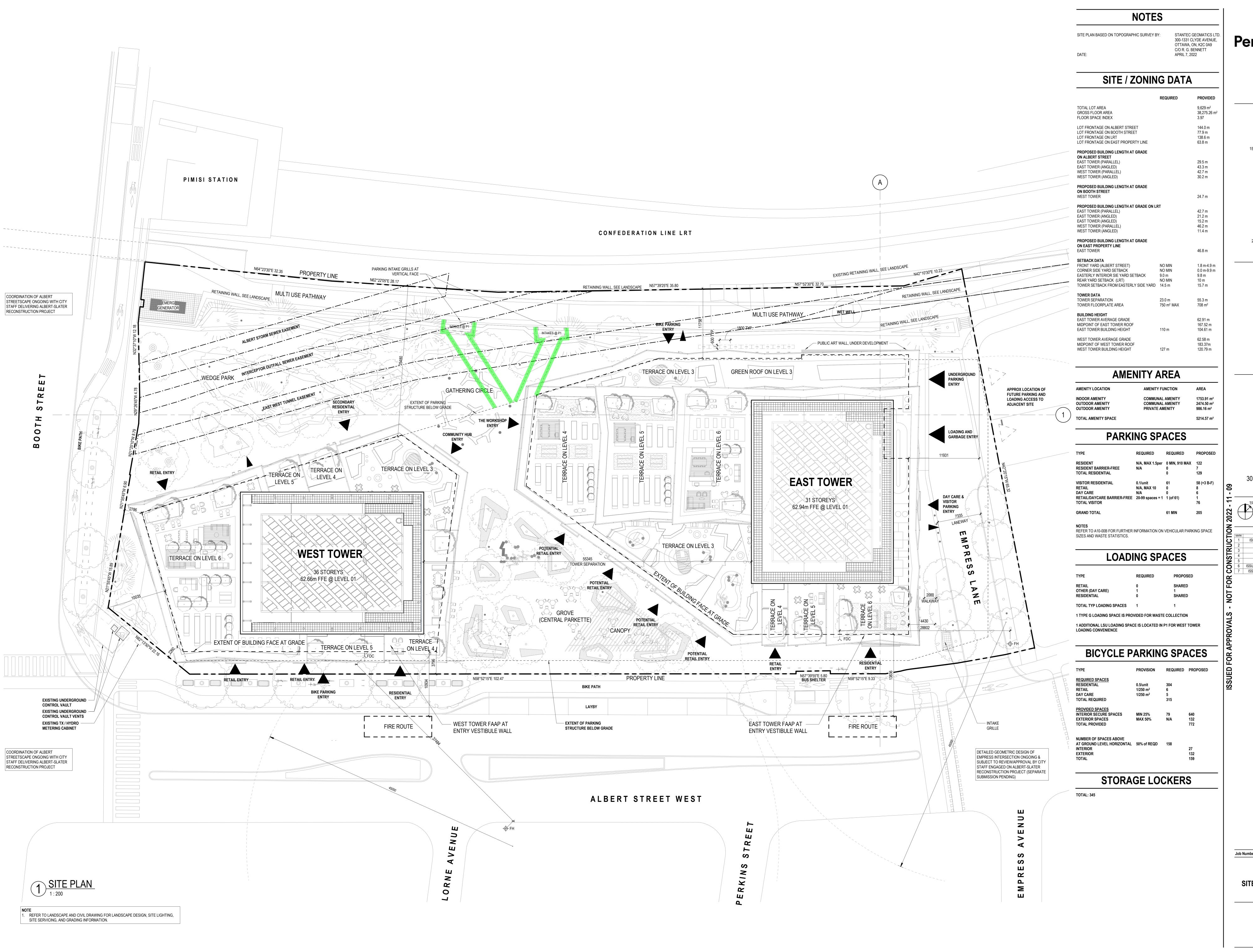
L08-13

SHEET NUMBER



APPENDIX C

Architectural Site Plan (Air Ducts)



KPMB Perkins&Will

351 King Street E, Suite 1200, Toronto, Ontario, Canada, M5A 0LA t 416.977.5104

275 Slater Street, Suite 1810, Ottawa, Ontario, Canada, K1P 5H9 t 613.563.2500

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LEBRETON LIBRARY
PARCEL
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Ottawa, ON

dream <u></u>

DREAM
30 Adelaide St. E., Suite 301,
Toronto, ON M5C 3H1
KEYPLAN

ISSUE CHART

ISSUED FOR OPA / ZBA / SPA	2022-04-22
ISSUED FOR 66% SD	2022-05-27
ISSUED FOR 100% SD	2022-06-10
ISSUED FOR 66% DD	2022-08-19
ISSUED FOR 100% DD	2022-09-30
ISSUED FOR SPA RESUBMISSION	2022-11-09
ISSUED FOR NCC 99% FLUDTA	2022-11-09

lumber 442

SITE PLAN & STATISTICS

Site Plan Control Application File Nos.: D01-01-22-0005, D02-02-22-0041 & D07-12-22-0069

SHEET NUMBER

G01-01

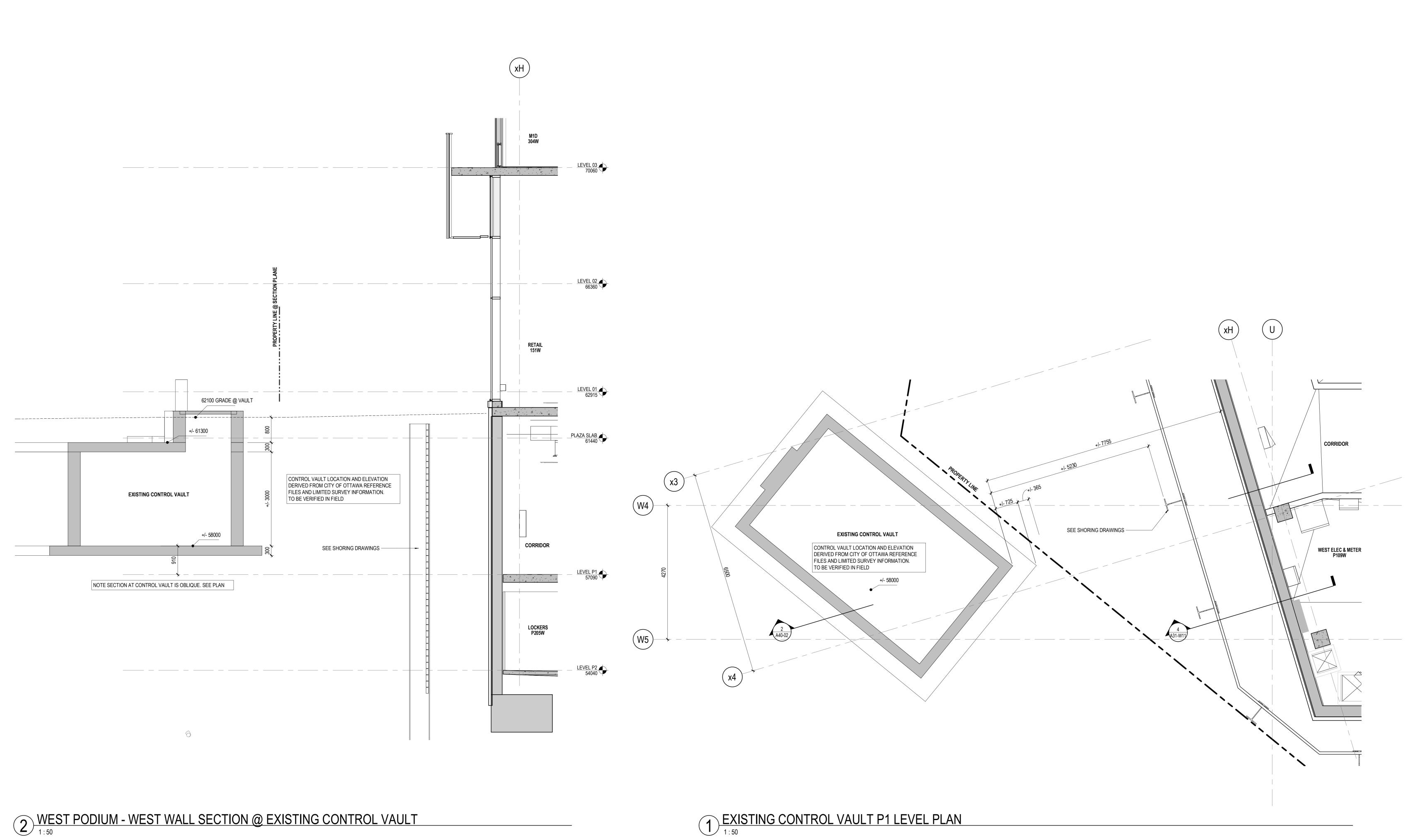
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APPENDIX D

Architectural Drg. A40-02 (City Vault, South-West Corner of Site)

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APPENDIX E

Shoring Design Package

SPECIAL NOTES:

- S1. EXACT SHORING WALL ALIGNMENT TO BE CONFIRMED PRIOR TO PILE INSTALLATION BASED ON PROPERTY LINE, ALIGNMENT OF FOUNDATION WALL, AND LOCATION OF UNDERGROUND UTILITIES.
- S2. DESIGN SHOWN ON THESE DRAWINGS IS FOR CONSTRUCTION BY MARATHON UNDERGROUND CONSTRUCTORS CORPORATION ONLY.

GENERAL NOTES:

- 1. STRUCTURAL DESIGN OF SHORING COMPLETED IN ACCORDANCE WITH:
- a. CANADIAN FOUNDATION ENGINEERING MANUAL
- b. CSA S16-09 DESIGN OF STEEL STRUCTURES (MEMBER STRENGTH PROVISIONS)
- c. OBC (2012) SECTIONS 4.2 AND 4.3
- GROUND CONDITIONS EVALUATED FROM GEOTECHNICAL REPORT "LEBRETON LIBRARY PARCEL, 665 ALBERT STREET OTTAWA, ONTARIO", BY GOLDER DATED APRIL 2022 (REF NO. 22511882).
- 3. FOUNDATION WALL POSITION FOR SHORING ALIGNMENT AND EXCAVATION/LAGGING LEVEL FROM DRAWING S198, S198E AND S198W BY READ JONES CHRISTOFFERSEN LTD, DATED 2022 12 02 (REV 4). SHORING IS SET BACK 2.0M FROM FOUNDATION WALL.
- 4. POSITIONS OF UNDERGROUND UTILITIES FROM DRAWING S1 'SERVICING PLAN' BY TMIG DATED 221109 (REV6) AND CITY AS-BUILT DRAWING PROVIDED TO MARATHON UNDERGROUND.
- 5. GENERAL BOTTOM OF LAGGING LEVEL OF EL. 52.965 DETERMINED FROM STRUCTURAL DRAWINGS.
- 6. DESIGN LOADING:
- a. SURCHARGE OF 12KPA ABOVE/BEHIND SHORING WALL. NO HEAVY EQUIPMENT TO BE OPERATED WITHIN 2m OF SHORING WITHOUT REVIEW BY SHORING DESIGN ENGINEER.
- b. EARTH PRESSURE -

MATERIAL	UNIT WEIGHT (kN/m ³)	FRICTION ANGLE (DEGREES)	ACTIVE EARTH PRESSURE COEFFICIENT
FILL	21	30	0.33
SILTY SAND	21	33	0.29
DENSE GLACIAL TILL	22	37	0.25

- c. NO GROUNDWATER PRESSURE SINCE SHORING WALL IS PERVIOUS.
- 7. MATERIALS
- a. SOLDIER PILES: H PILES SHALL CONFORM TO CSA-G40.20/G40.21 350W
- b. PIPE STRUT FOR CORNER BRACE
- 244 mm OD x 12.0 mm (9.625 x 0.472 INCH) WALL PIPE
- ii) ASTM GRADE 3, Fy = 310 MPa (MIN.)
- c. ALL OTHER STRUCTURAL STEEL: CSA G40.20/G40.21 350W, OR ASTM A992, OR ASTM A572 GR. 50 (MIN. Fy = 345 MPa).
- d. TIMBER LAGGING 4" X 6" ROUGH CUT CONSTRUCTION-GRADE HARDWOOD LUMBER (E.G., POPLAR OR SIMILAR)
- e. TIE-BACKS AND SOIL ANCHORS: SEE TIE-BACK AND SOIL ANCHOR SCHEDULE. 0.6" 7-WIRE STRAND 270 KSI PER ASTM A-416. MS CABLE GROUT (MIN. 40 MPA)
- 8. WELDING TO CSA W59-13. E49XX WELDING ELECTRODES
- 9. PROVIDE RAILING ON TOP OF WALL AS REQUIRED (REF. O/REG. 213/91).
- 10. ALL EXISTING UTILITIES TO BE LOCATED PRIOR TO SHORING INSTALLATION.
- a. IF BURIED UTILITIES ARE LOCATED WITHIN 1.5m OF SOLDIER PILE LOCATIONS, EXPOSE UTILITY (HYDROVAC) TO CONFIRM LOCATION.

- positions and depths of all buried utilities in proximity to tie-back trajectories, and in particular of hptm watermain and hydro duct along south property line, to be confirmed prior to tie-back drilling.
- 11. ANY CHANGES TO DESIGN AND CONSTRUCTION METHODOLOGY TO BE APPROVED BY SHORING DESIGNER PRIOR TO IMPLEMENTATION.
- 12. ALL DIMENSIONS SHOWN IN MILLIMETRES UNLESS NOTED. ELEVATIONS SHOWN IN METRES.
- 13. ALL WORK TO BE CARRIED OUT IN ACCORDANCE WITH THE OCCUPATIONAL HEALTH AND SAFETY ACT.

INSTALLATION PROCEDURE:

- LOCATE ALL BURIED UTILITIES. CONFIRM NO CONFLICTS WITH SOLDIER PILE LOCATIONS AND TIE-BACK TRAJECTORIES.
- 2. CONFIRM EXACT SHORING ALIGNMENT WITH OWNER, G.C., AND SURVEYOR. NOTE: ENCROACHMENT AGREEMENT FOR PILE LOCATIONS AND TIE-BACKS ARE THE RESPONSIBILITY OF THE CLIENT.
- 3. CONFIRM REQUIRED BOTTOM-OF-EXCAVATION (B.O.E.) LEVEL WITH G.C.
- PRE-DRILL PILE LOCATIONS TO BEDROCK (16" DIAMETER DTHH). MIN 3.5 m TOE REQUIRED BELOW B.O.E. OR MIN. 0.5m INTO BEDROCK, THEN DRIVE PILES TO BEDROCK.
- 5. INSTALL MONITORING TARGETS ON TOP OF PILES.
- 6. SOIL IN FRONT OF PILES TO BE EXCAVATED IN MAXIMUM 1.2m LIFTS PRIOR TO LAGGING INSTALLATION. USE SHORTER LIFTS IF NEEDED TO AVOID SLOUGHING OF BACKFILL.
- 7. INSTALL LAGGING (NO GAPS). PACK BEHIND LAGGING WITH STONE DUST AS REQUIRED TO ENSURE NO VOIDS ARE CREATED AND BACKFILL IS IN GOOD CONTACT WITH LAGGING.
- EXCAVATE TO MAXIMUM OF 0.8 m BELOW UNDERSIDE OF WALER LEVEL. DRILL, INSTALL, AND GROUT STRAND TIE-BACK AND SOIL ANCHORS WHERE INDICATED. INSTALL BRACKET AND WALER. NOTE: CONFIRM NO CONFLICT WITH EXISTING UTILITIES PRIOR TO TIE-BACK DRILLING.
- 9. POST-GROUT SOIL ANCHORS, AS REQUIRED.
- 10. STRESS, TEST, AND LOCK-OFF TIE-BACKS AND SOIL ANCHORS. SEE TIE-BACK AND SOIL ANCHOR SCHEDULE FOR DETAILS. TEST RESULTS TO BE PROVIDED TO SHORING DESIGN ENGINEER. TESTING TO GENERALLY CONFORM TO OPSS942.07.12.06.03. MEASURE WALL DEFLECTION DURING STRESSING AND TESTING. IF WALL MOVEMENT REACHES 25 mm, LOCK-OFF ANCHOR AND REPORT LOCK-OFF LOAD TO DESIGNER.
- 11. CONTINUE EXCAVATION AND LAGGING SEQUENCE TO BOTTOM-OF-EXCAVATION LEVEL.

REMOVAL PROCEDURE:

- ONCE BUILDING FOUNDATION WALL HAS BEEN CONSTRUCTED, BACKFILL BETWEEN SHORING AS NEEDED. COMPACT BACKFILL TO 95% STD. PROCTOR.
- 2. ONLY CUT TIE-BACKS AND REMOVE WALERS ONCE BACKFILL LEVEL IS WITHIN 0.8 m BELOW WALER LEVEL.
- 3. CUT PILES OFF 1.2m BELOW GRADE OR AS REQUIRED BY AGREEMENT WITH CITY/NEIGHBOURS.

MONITORING AND INSPECTIONS:

- 1. CONTINUOUS INSPECTION BY SHORING DESIGN ENGINEER DURING EXCAVATION AND REMOVAL [PER OBC 4.2.2.2(2)(a)(ii)].
- 2. MONITORING TARGETS TO BE INSTALLED AT TOPS OF PILES AT MAX. 10 m SPACING.
- 3. OBTAIN BASELINE READINGS ONCE TARGETS INSTALLED.
- 4. TARGETS TO BE MONITORED WEEKLY THEREAFTER, UNLESS DIRECTED OTHERWISE BY SHORING DESIGN ENGINEER. MONITORING BY OTHERS.
- 5. SHORING DESIGN ENGINEER TO BE NOTIFIED IMMEDIATELY IF DEFLECTION EXCEEDS 15 mm. IF DEFLECTION EXCEEDS 25 mm, EXCAVATION SHOULD STOP UNTIL CONDITIONS ARE REVIEWED BY SHORING DESIGN FNGINEER
- 5. ON-SITE STAFF SHOULD CARRY OUT DAILY VISUAL INSPECTION DURING EXCAVATION AND SHORING CONSTRUCTION, INCLUDING OF GROUND SURFACE BEHIND SHORING. IF ANY DEFORMATIONS OR GROUND SURFACE CRACKING OR SETTLEMENT ARE OBSERVED, SHORING DESIGN ENGINEER TO BE IMMEDIATELY NOTIFIED.
- 7. VIBRATION MONITORING AND PRE-CONSTRUCTION SURVEY BY OTHERS, IF REQUIRED.



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6847 Hiram Drive, Greely, ON K4P 1A2

PROJECT

LEBRETON LIBRARY PARCEL EXCAVATION SHORING

OCATION

DESCRIPTION

665 ALBERT STREET OTTAWA, ONTARIO

JOB No.

22409

NG

NOTES

DRAWN BY AC SCALE AS NOTED DESIGNED BY HB

CHECKED BY MIC

MU0

TABLE OF CONTENTS		
SHEET NUMBER	DESCRIPTION	
MU0	NOTES	
MU0A	NOTES	
MU1	SITE & UTILITIES PLAN	
MU2	SHORING PLAN	
MU3	SECTION	
MU4	SECTION	
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MU10	ELEVATION	
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MU20	SOIL ANCHOR DETAIL	



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LEBRETON LIBRARY PARCEL **EXCAVATION SHORING**

LOCATION

DESCRIPTION

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665 ALBERT STREET OTTAWA, ONTARIO

JOB No.

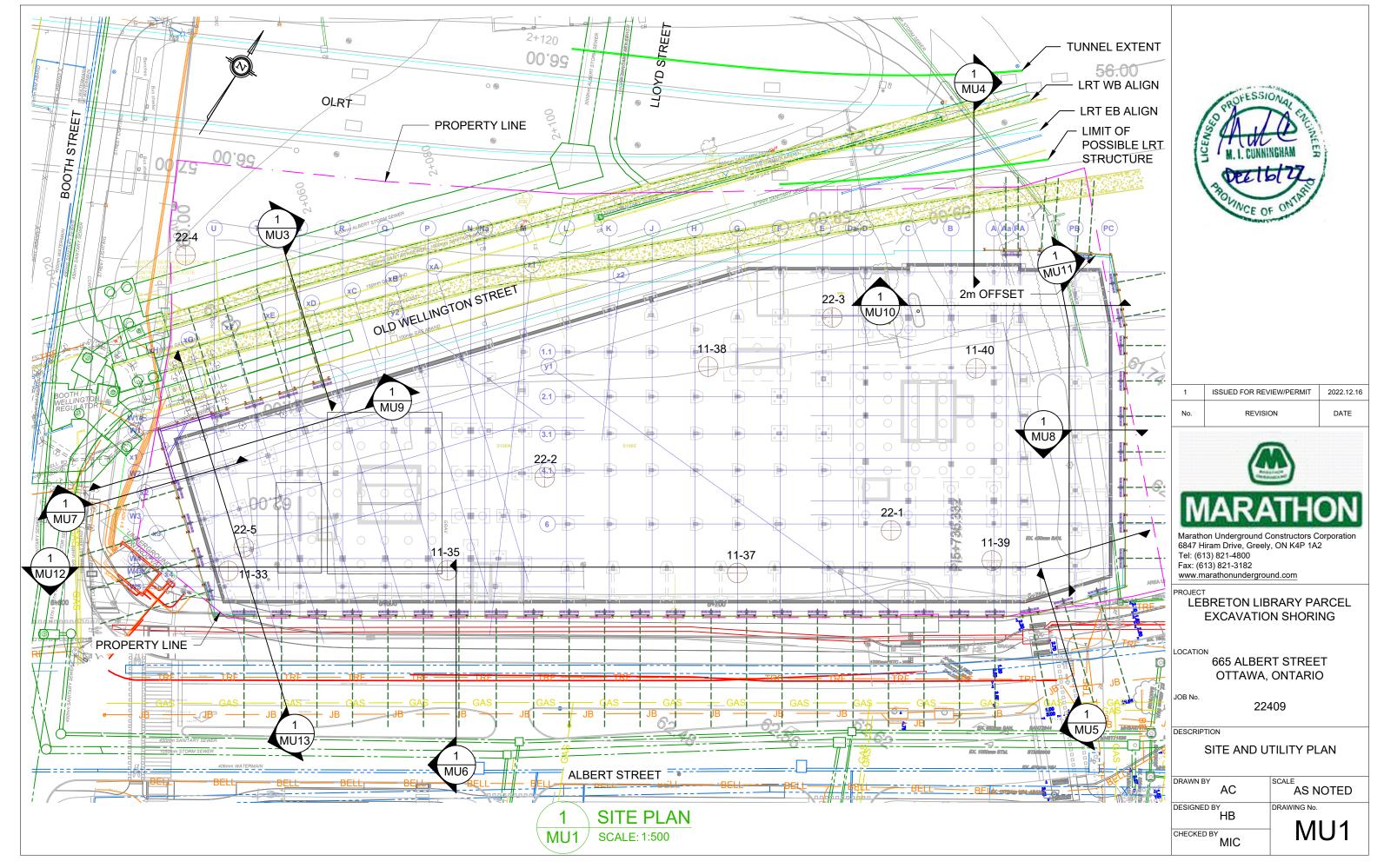
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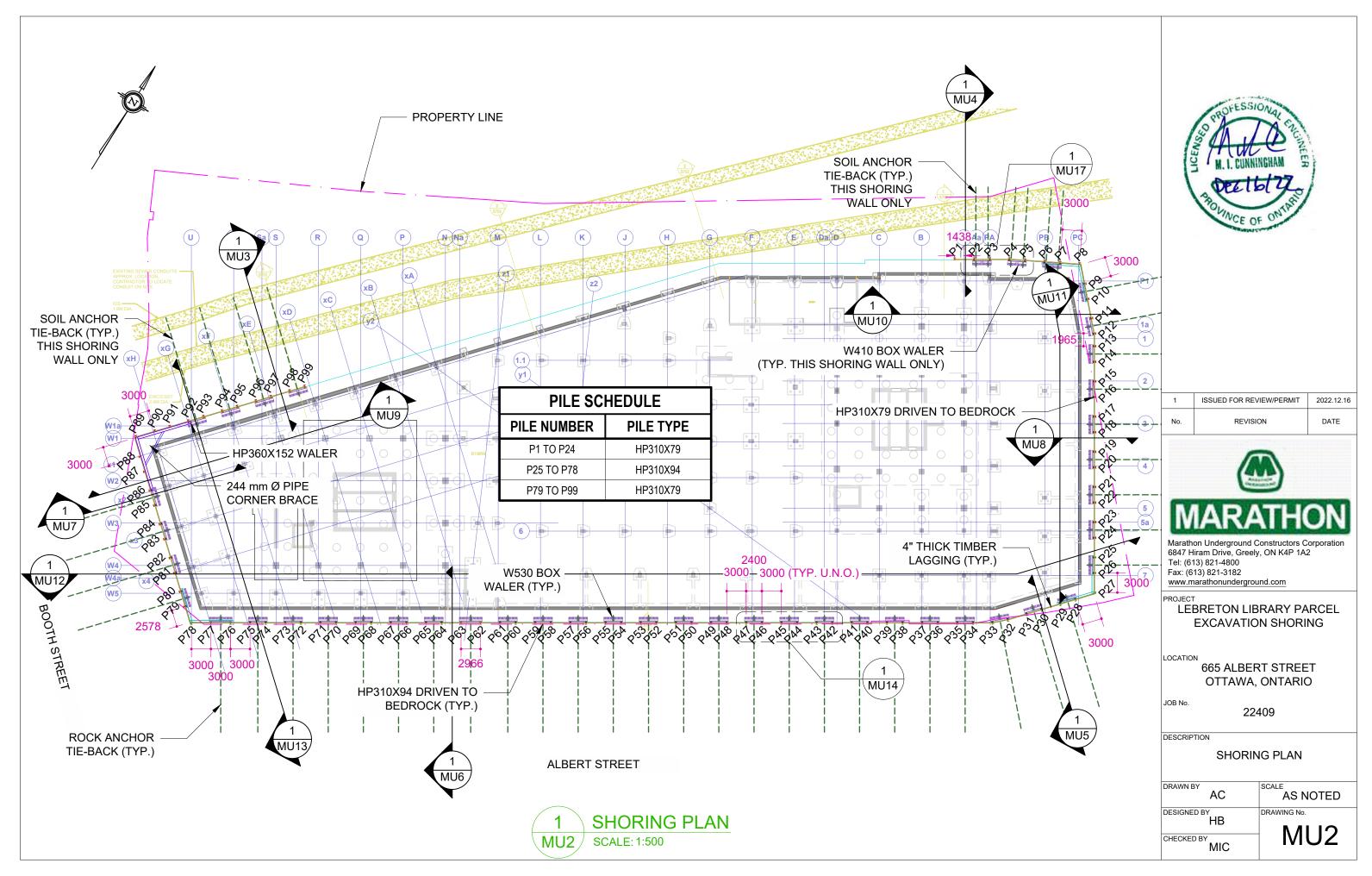
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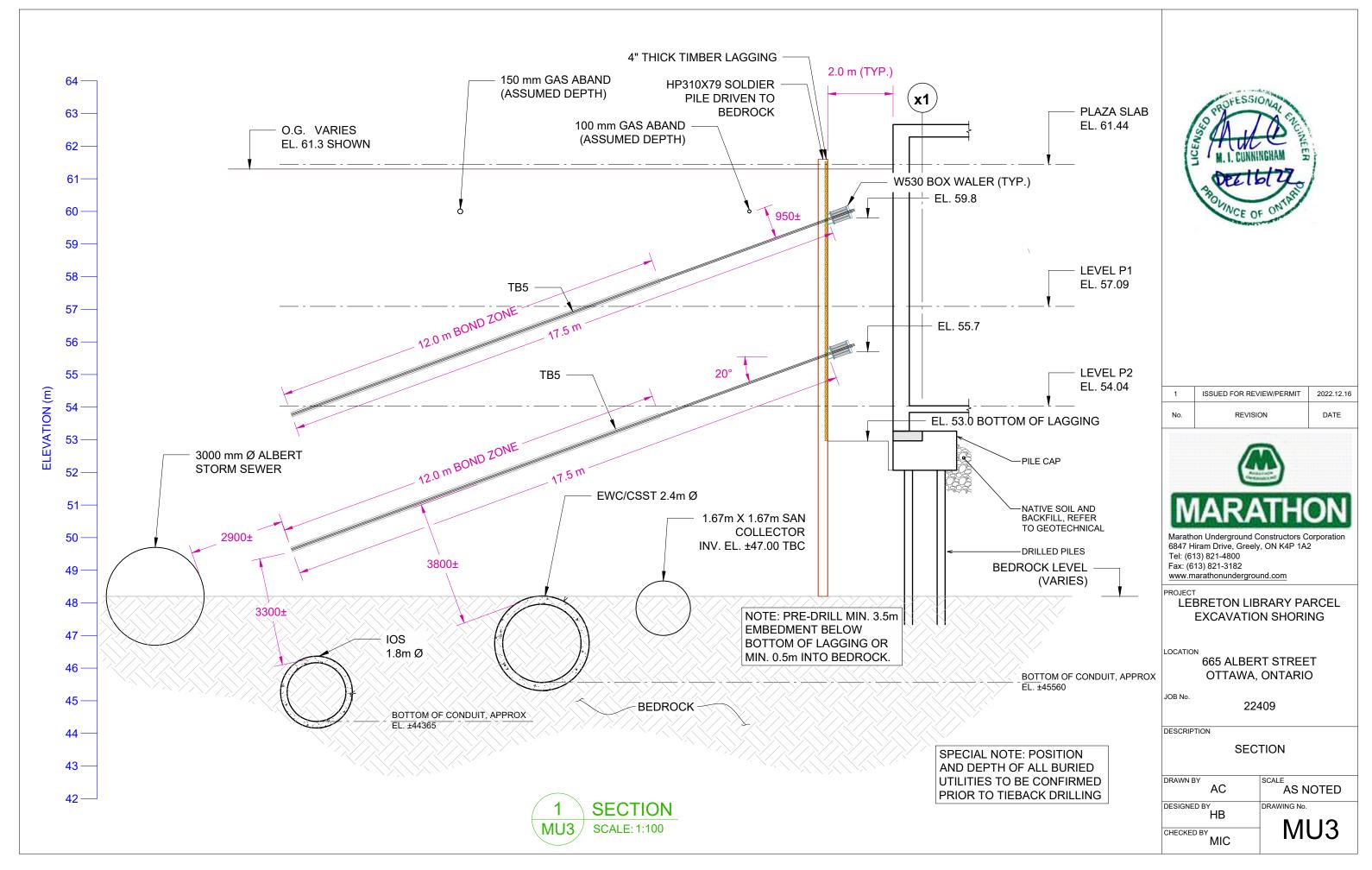
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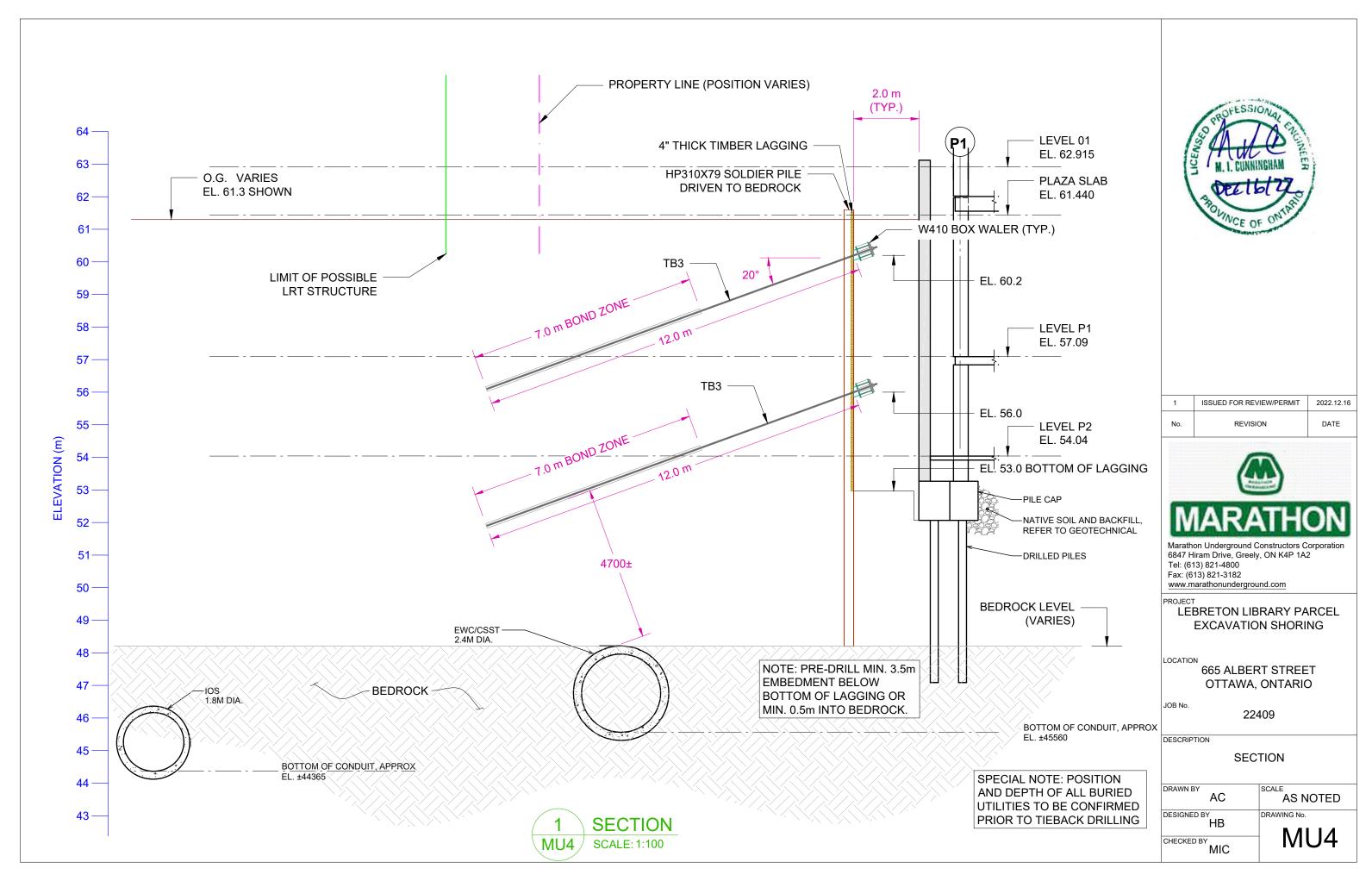
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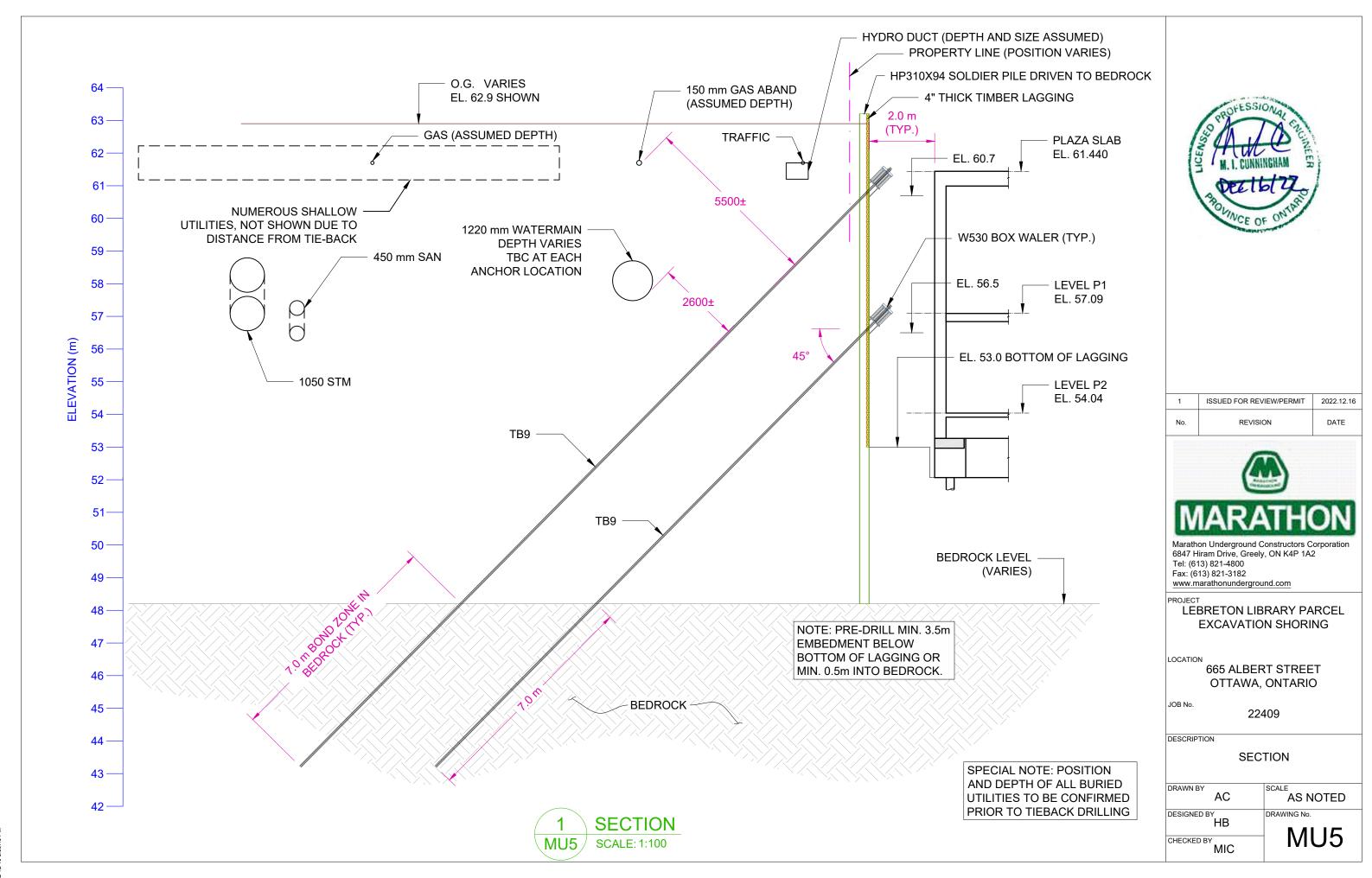
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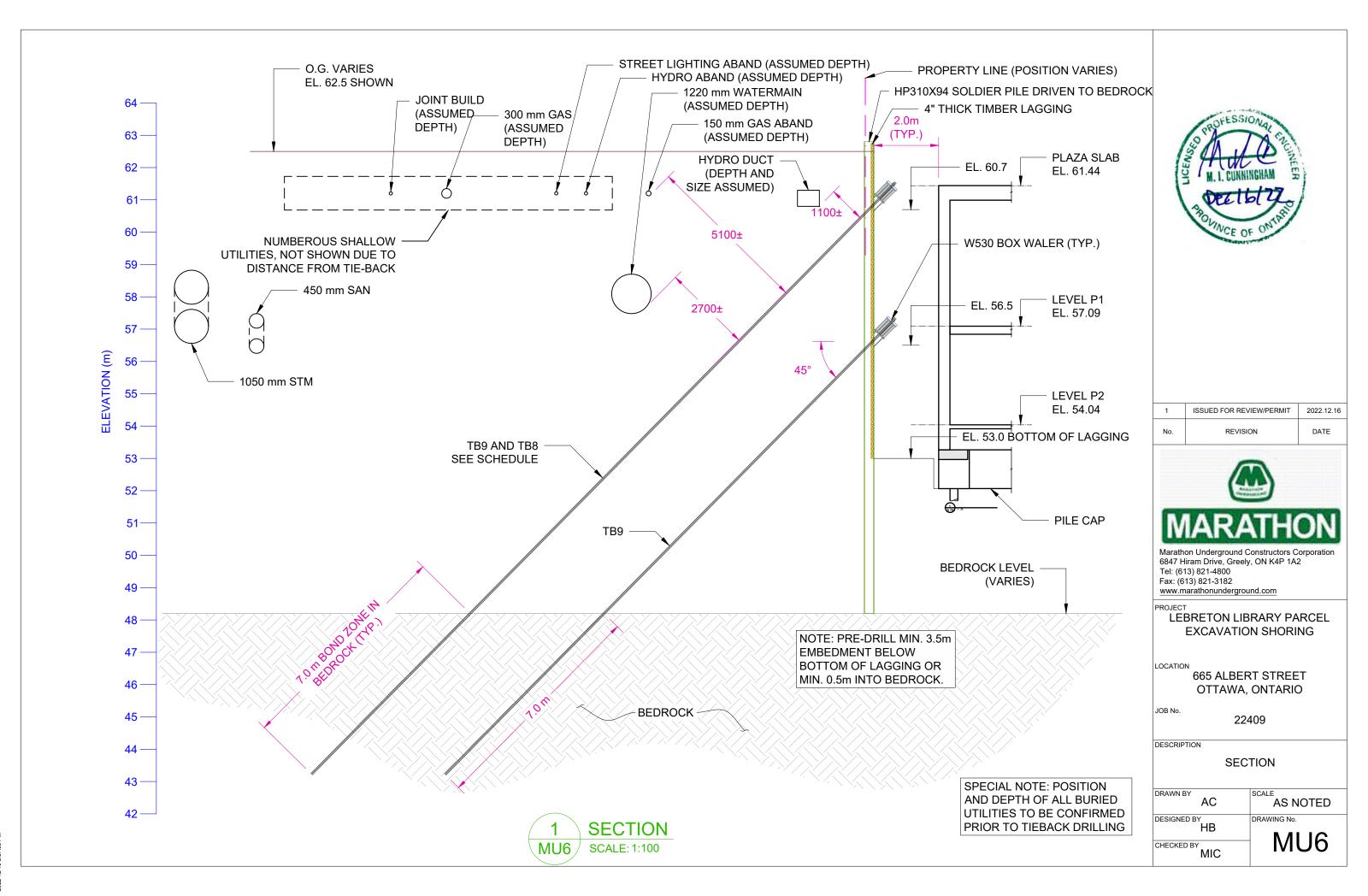


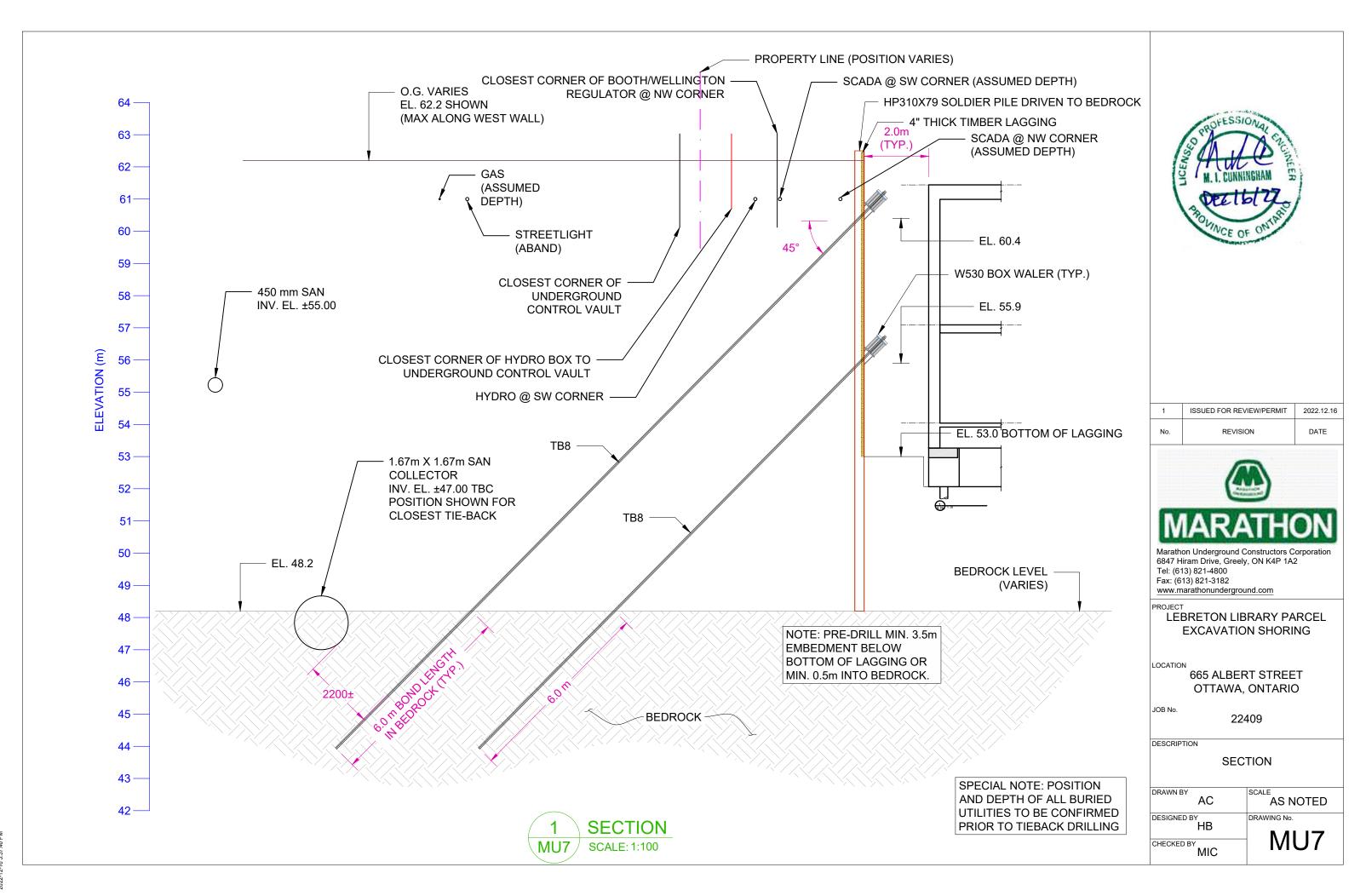


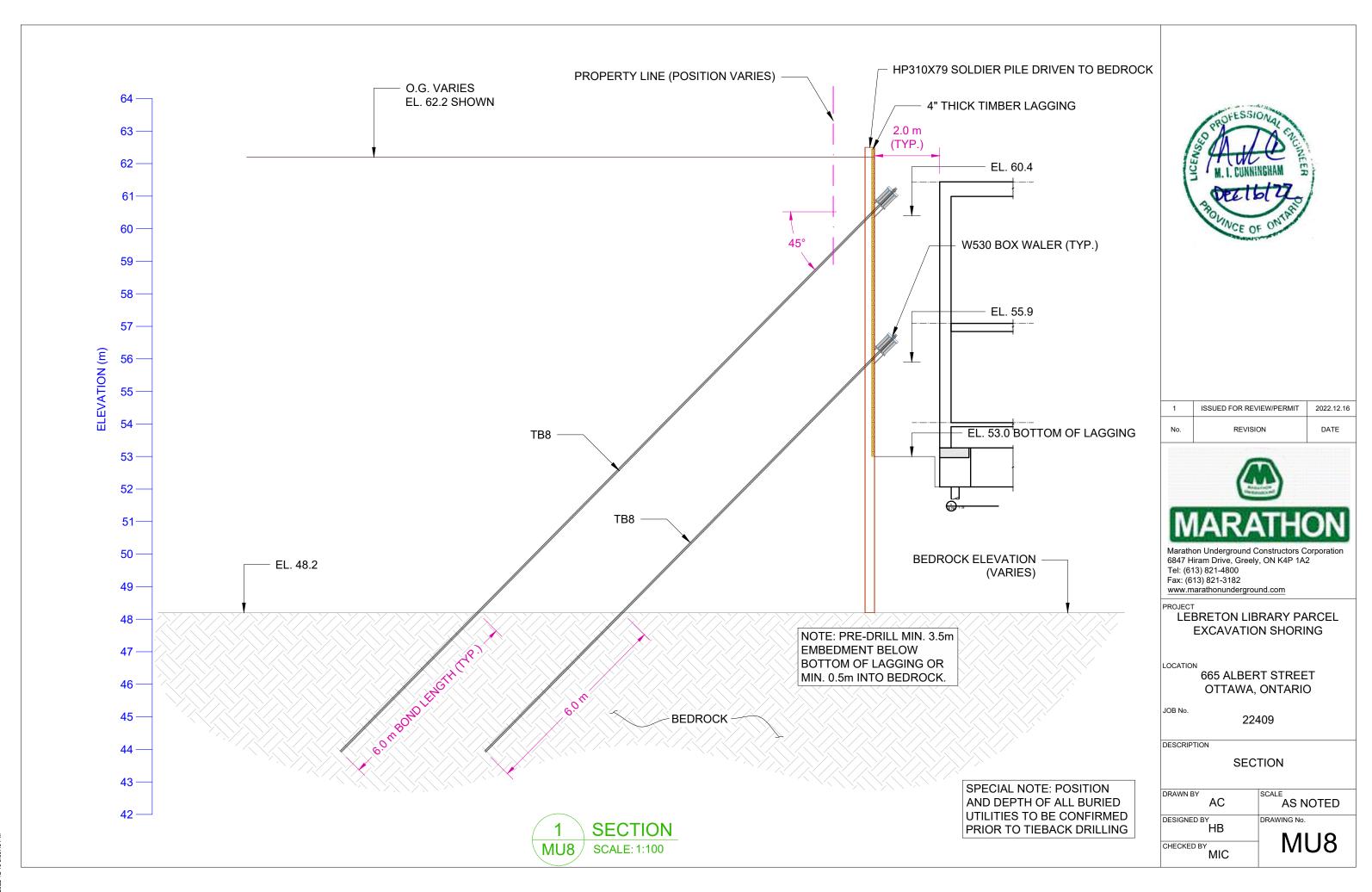


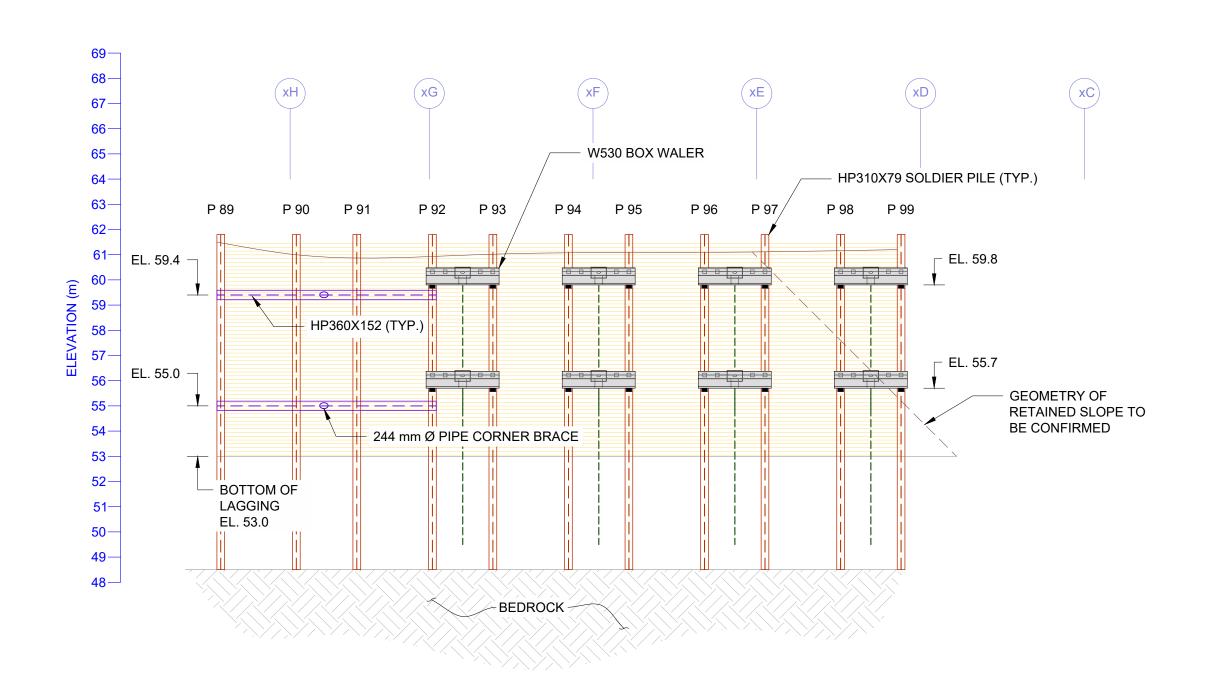












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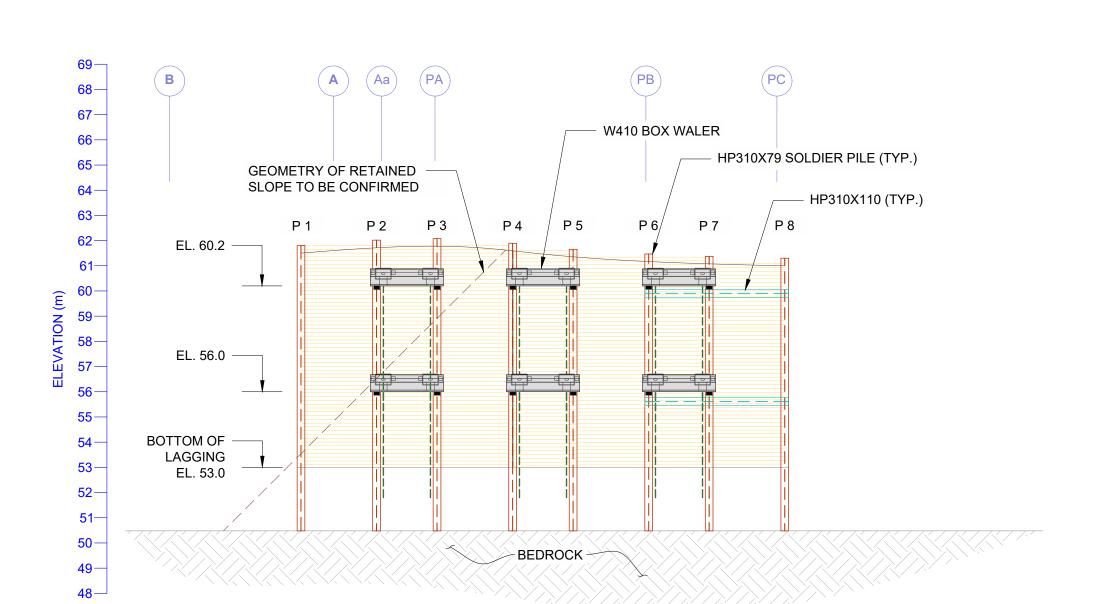
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LOCATION

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22409

DESCRIPTION

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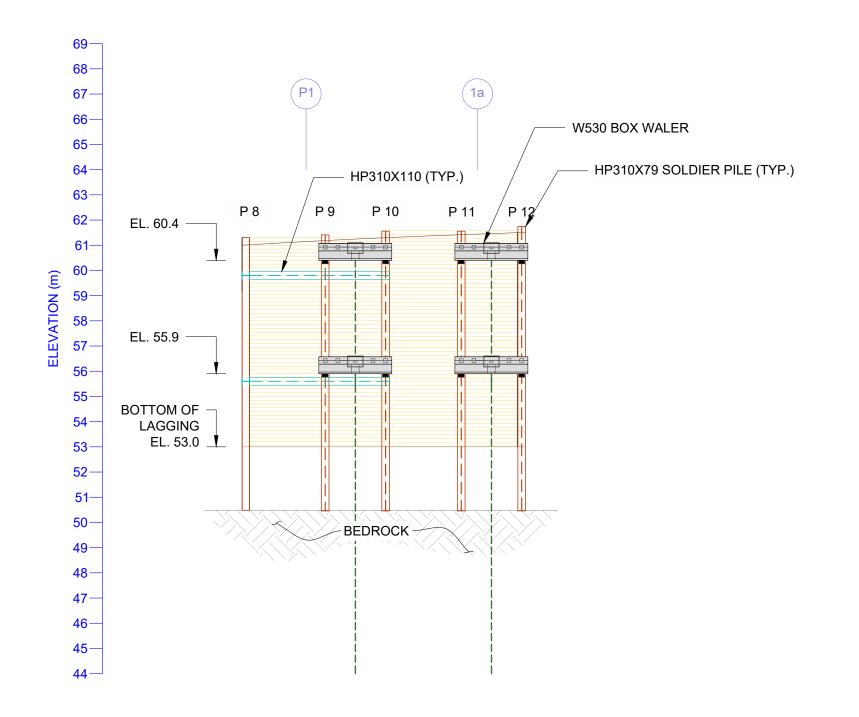
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LOCATION

665 ALBERT STREET OTTAWA, ONTARIO

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DESCRIPTION

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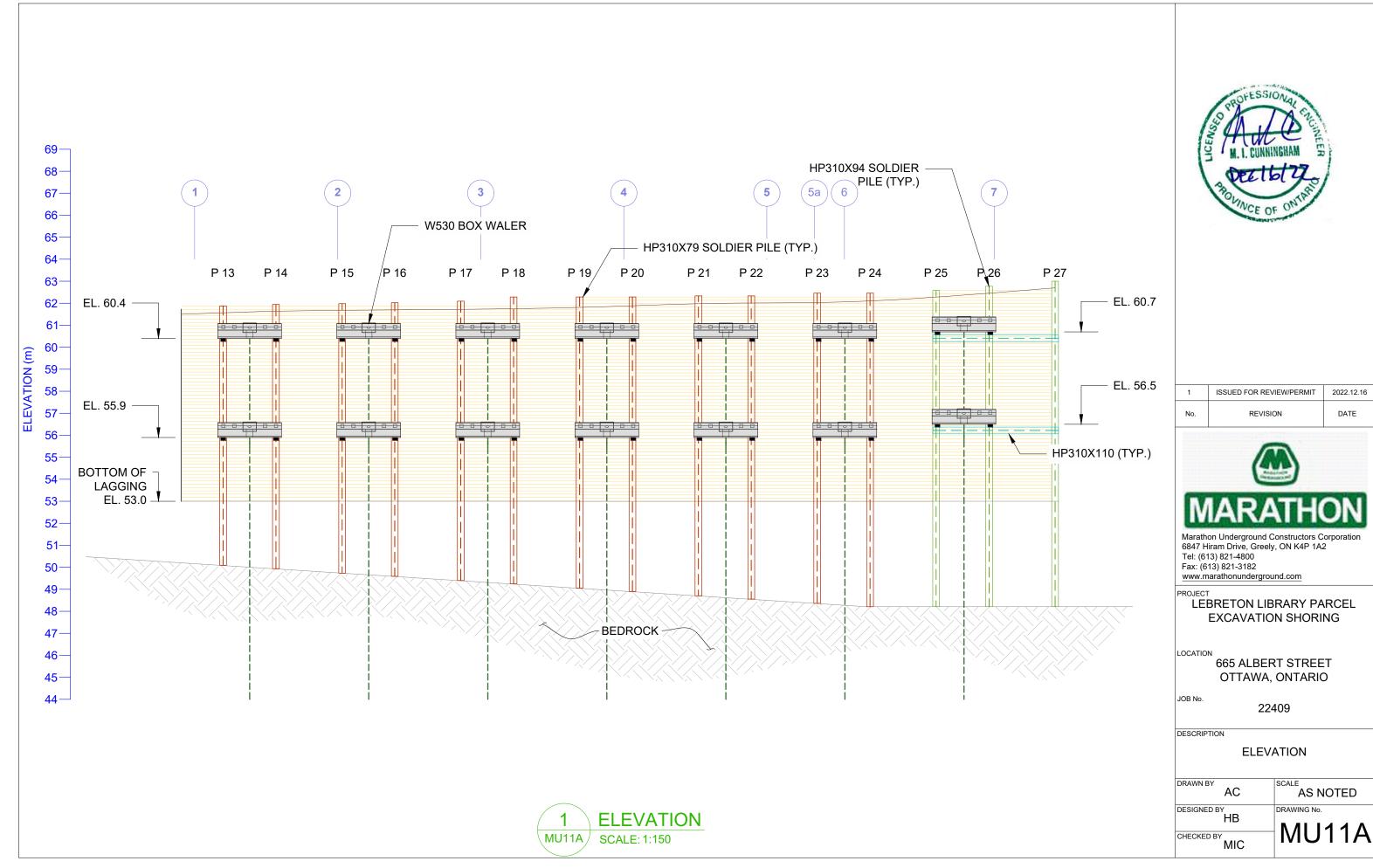
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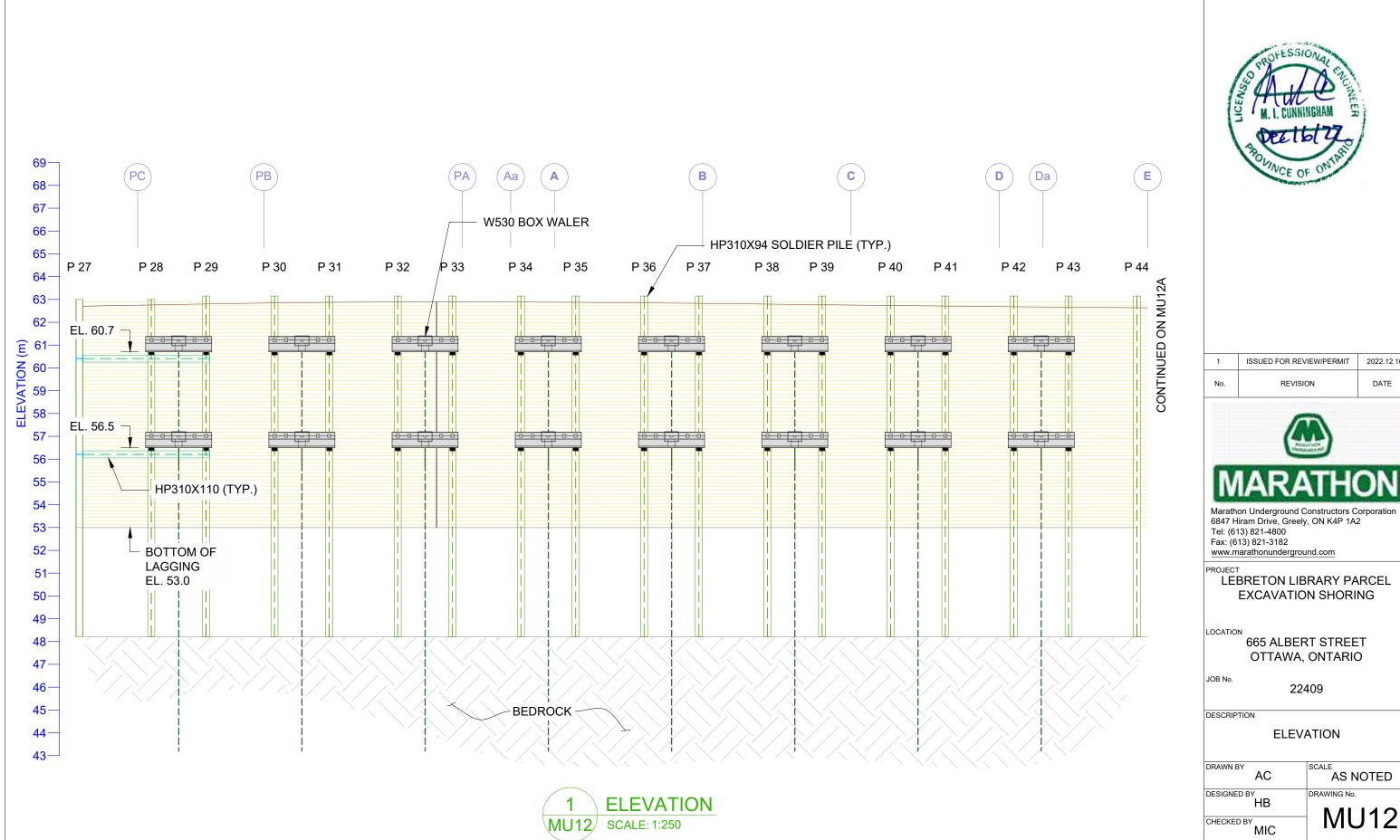
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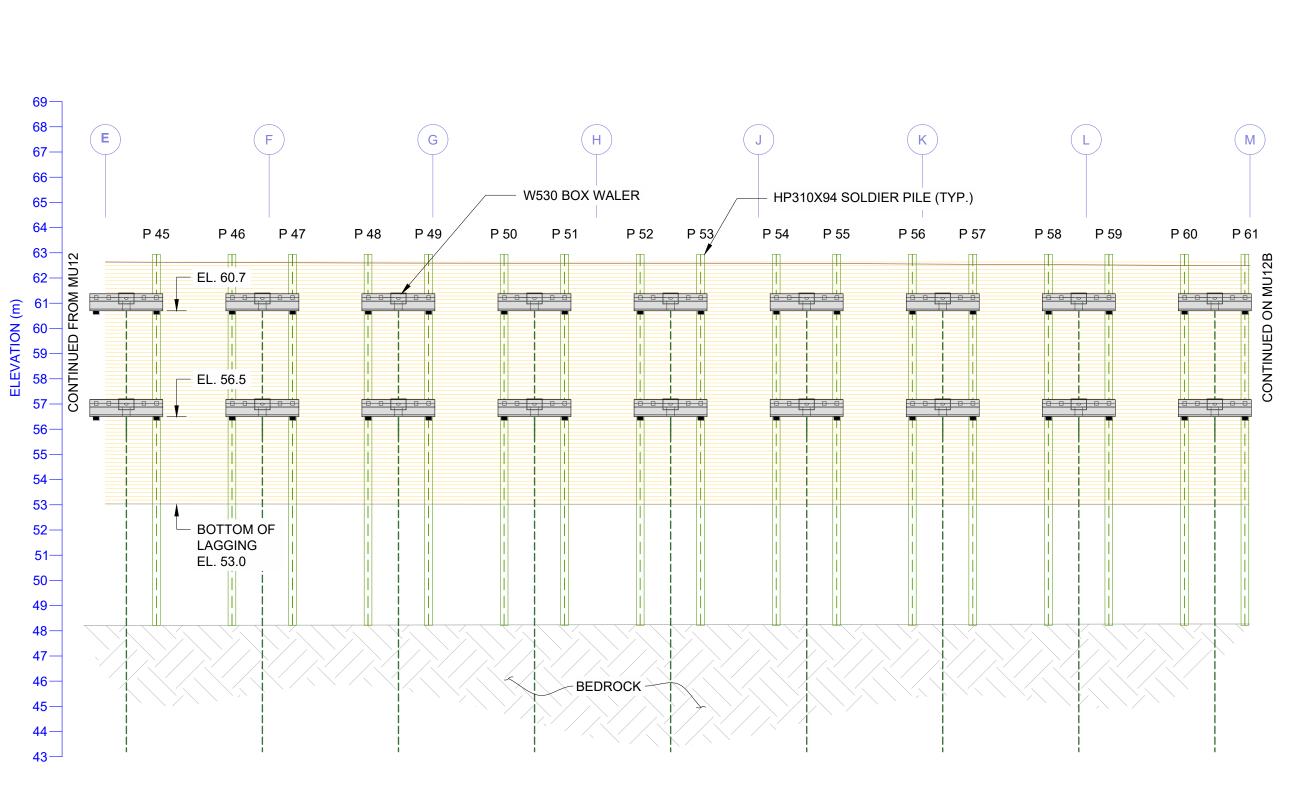
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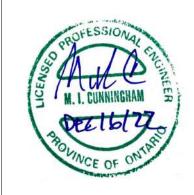
LEBRETON LIBRARY PARCEL **EXCAVATION SHORING**

665 ALBERT STREET

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665 ALBERT STREET OTTAWA, ONTARIO

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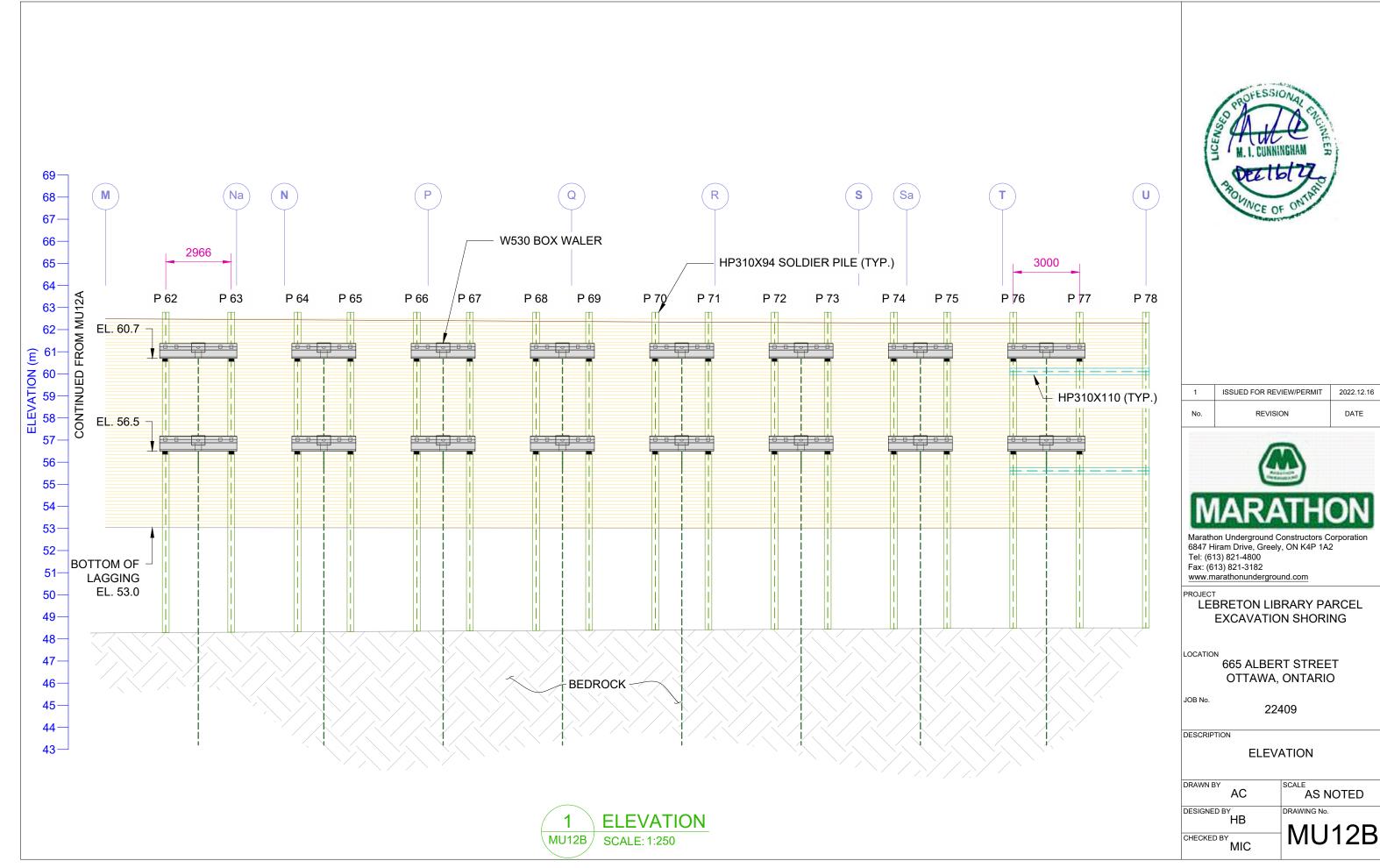
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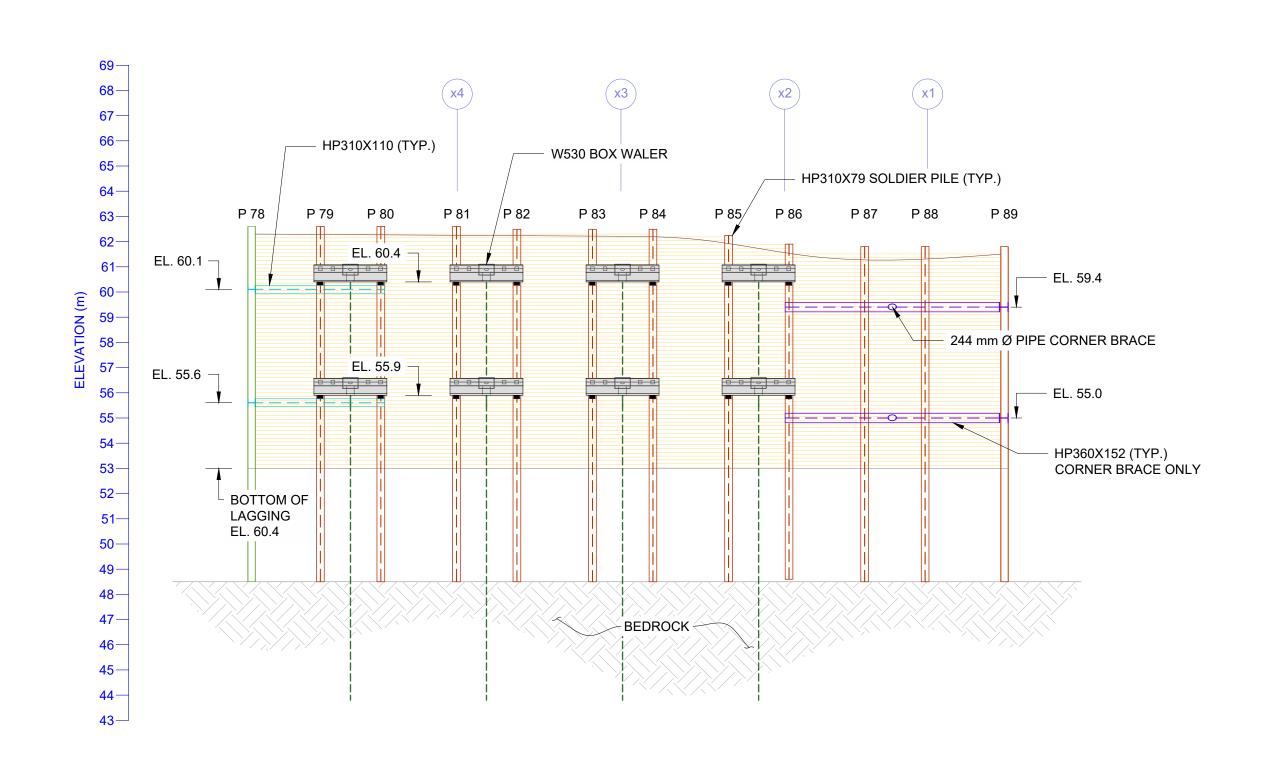
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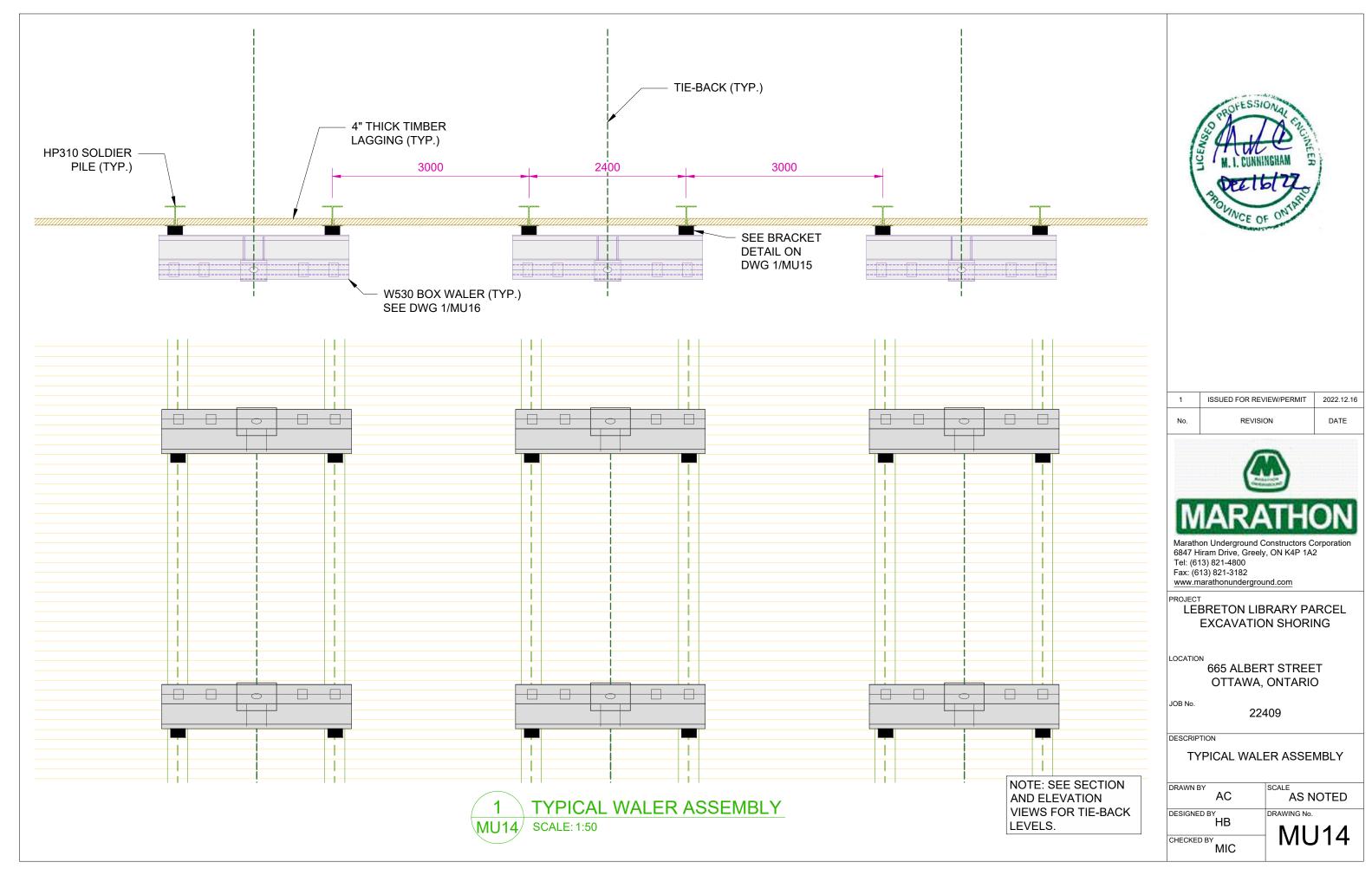
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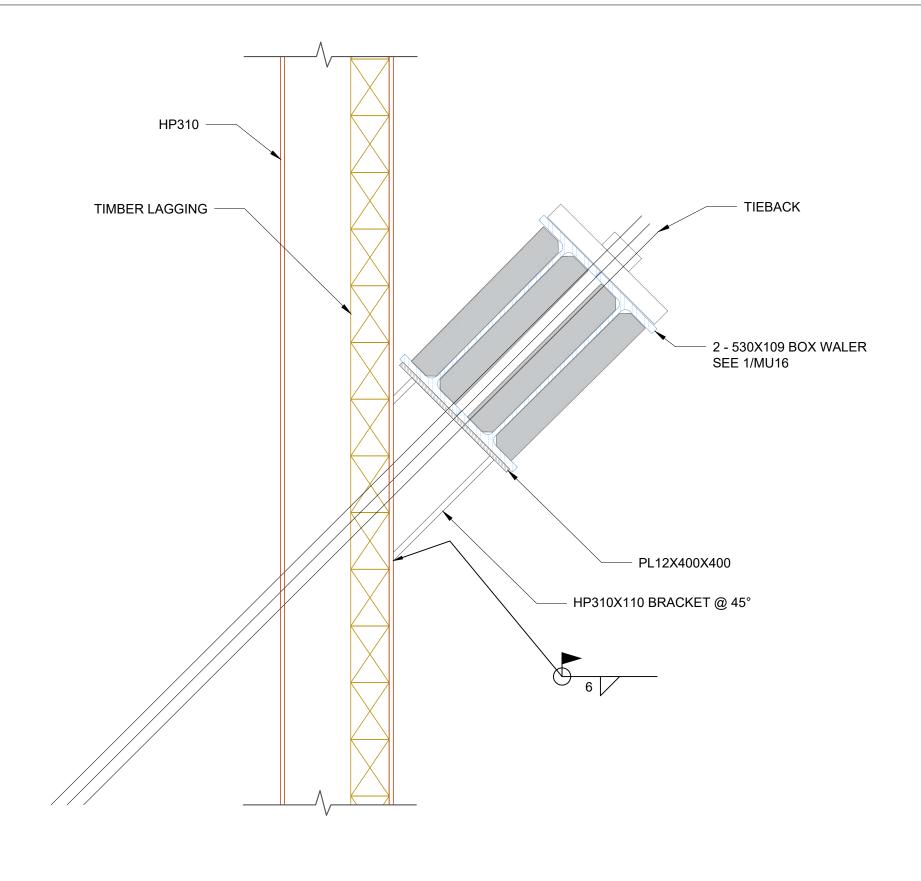
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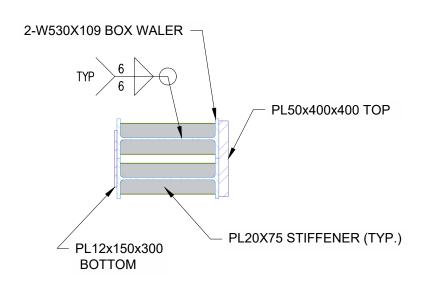
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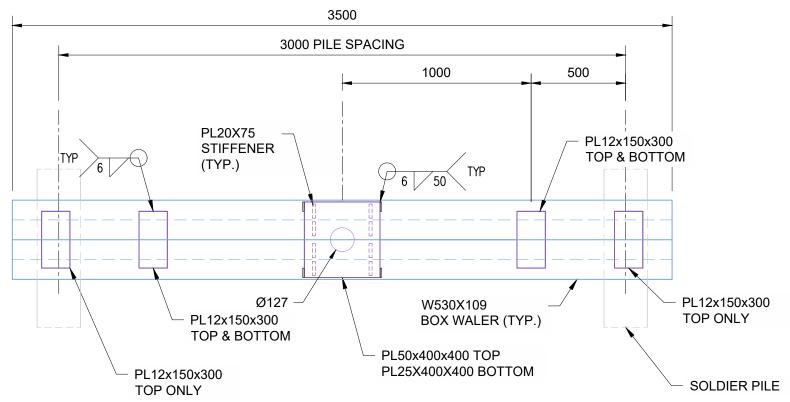
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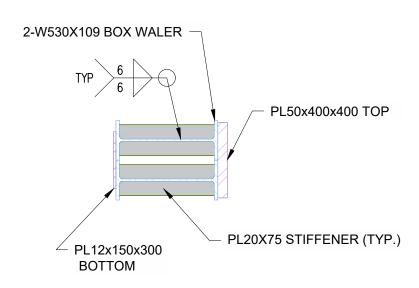
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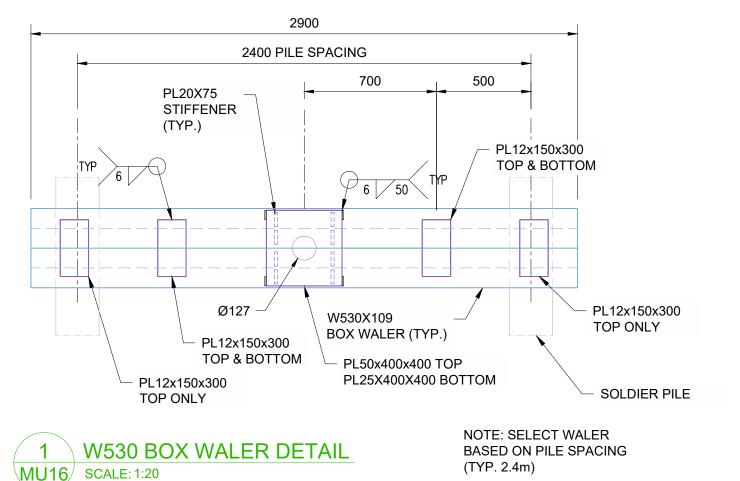
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LOCATION

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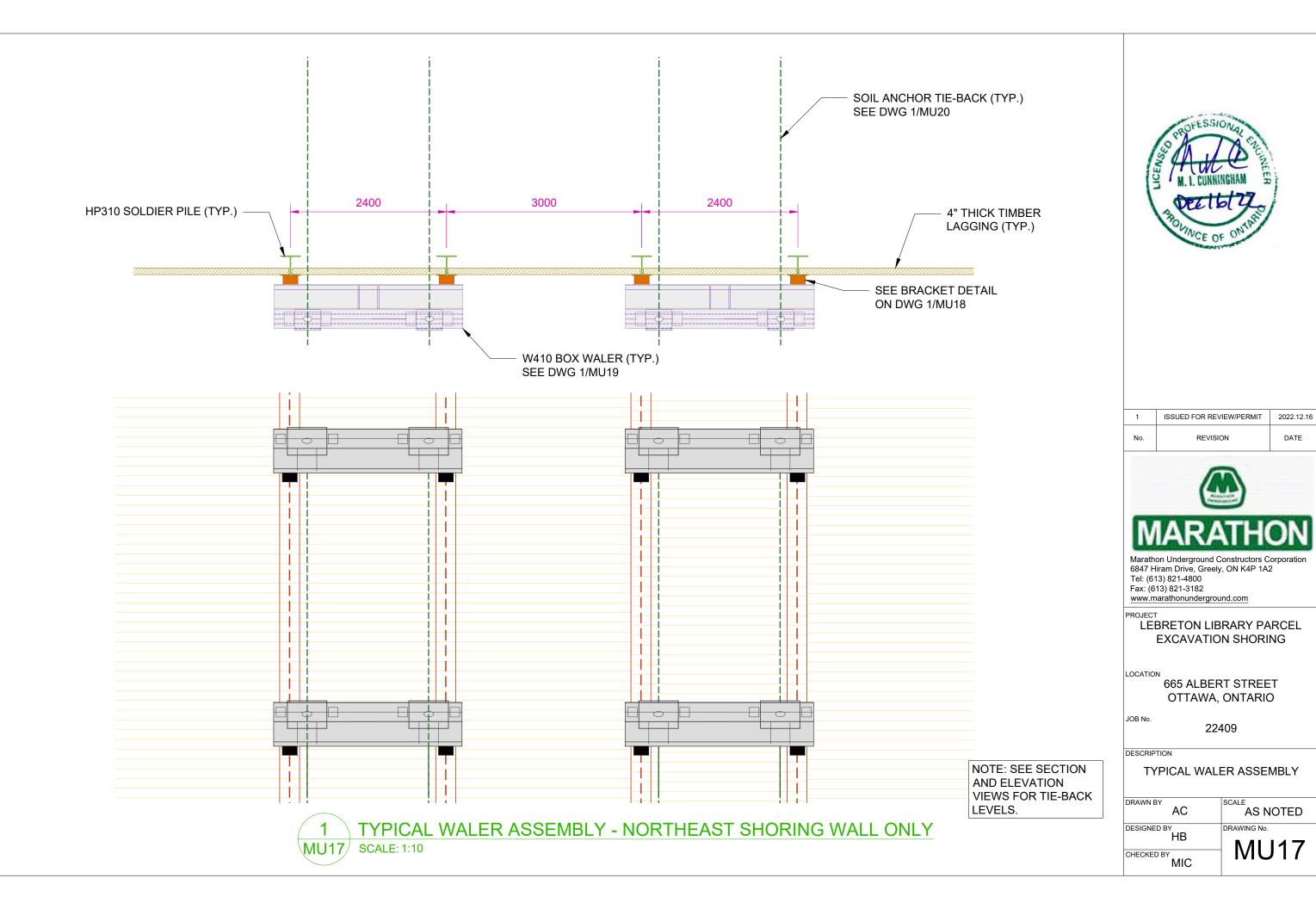
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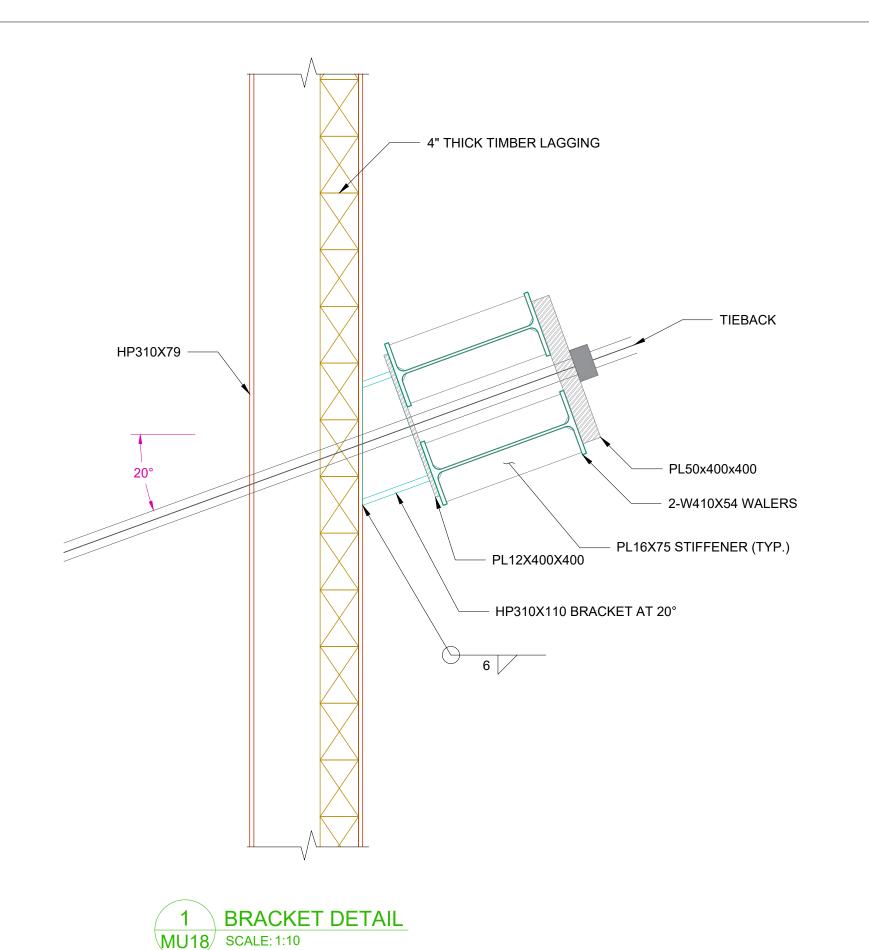
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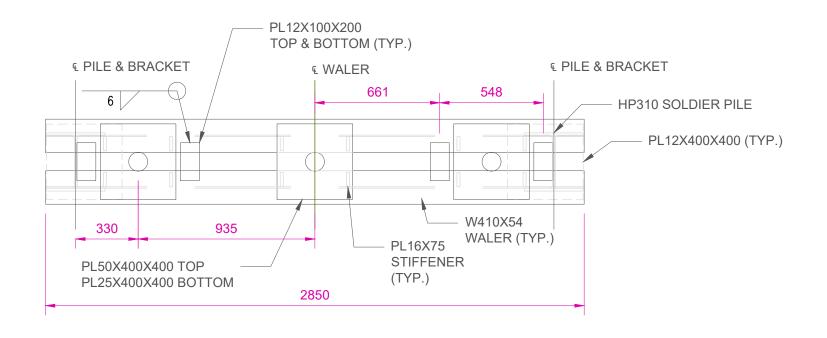
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BRACKET DETAIL

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LOCATION

665 ALBERT STREET OTTAWA, ONTARIO

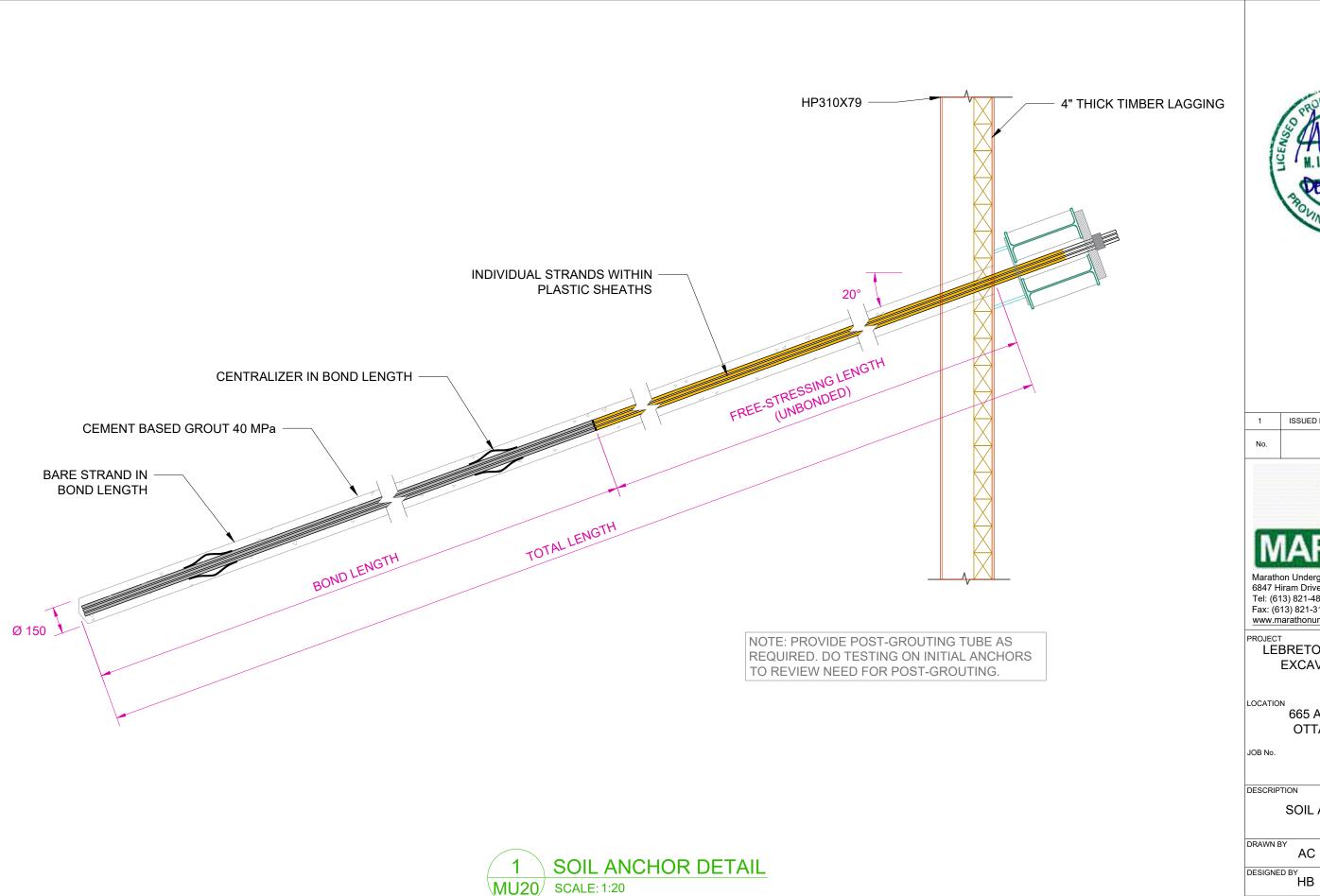
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DESCRIPTION

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> 665 ALBERT STREET OTTAWA, ONTARIO

> > 22409

SOIL ANCHOR DETAIL

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APPENDIX F

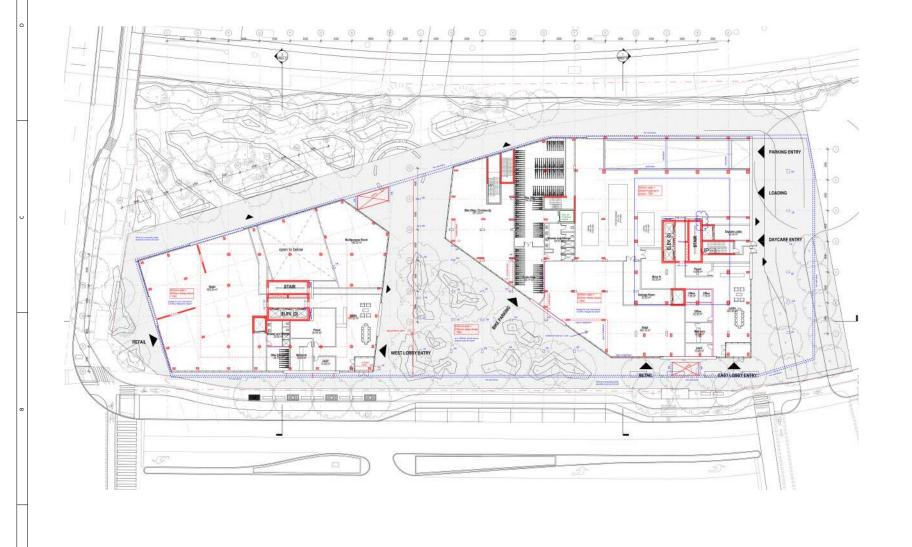
Construction Logistics Plan

LEBRETON LIBRARY PARCEL

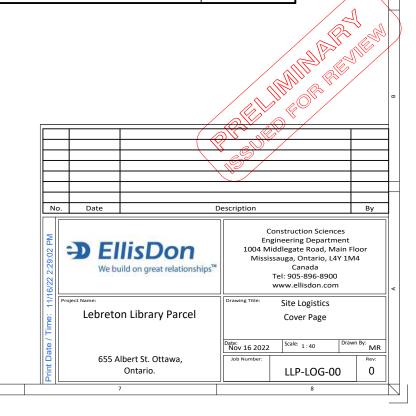
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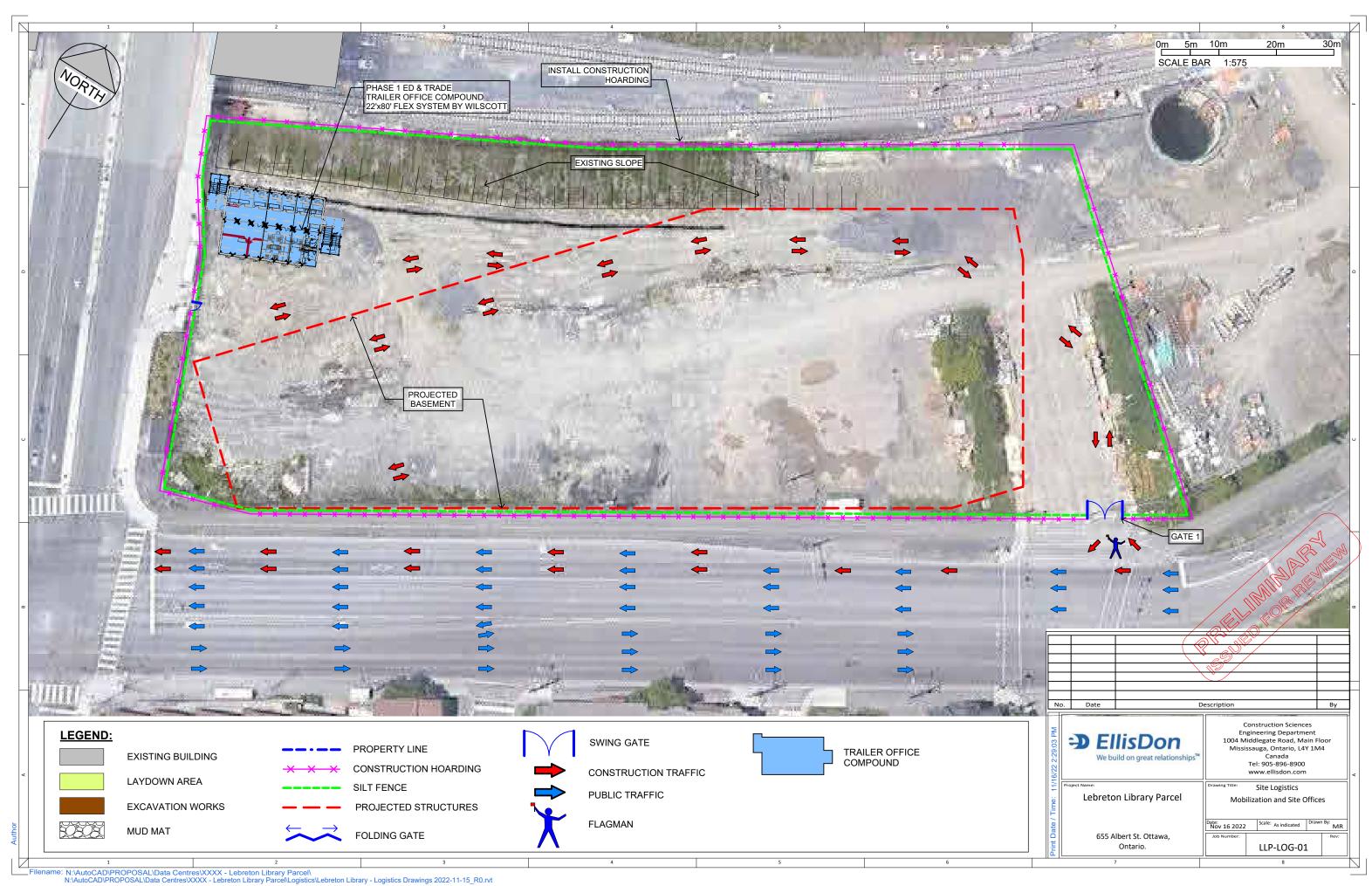
LOGISTICS DRAWINGS

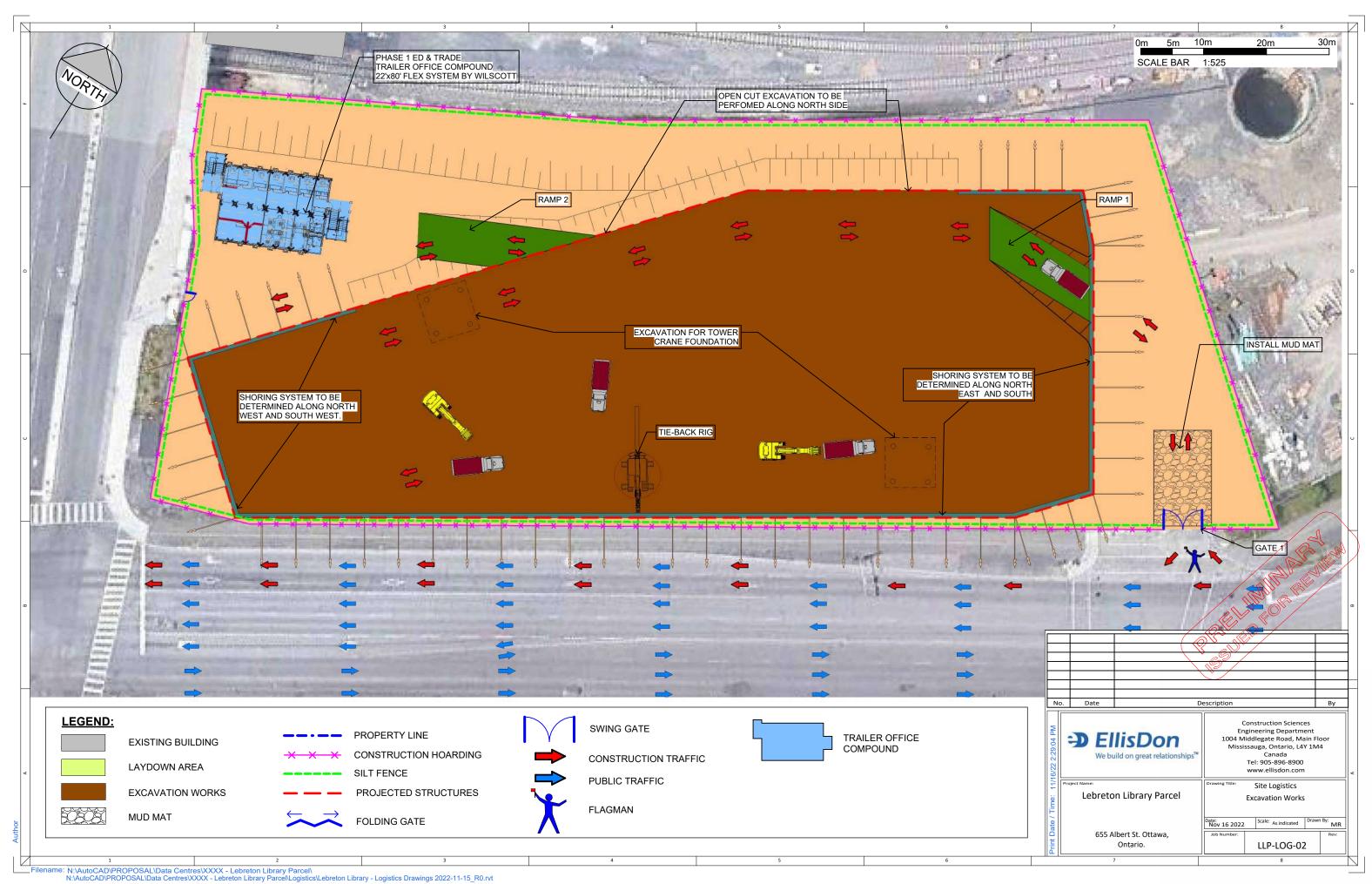
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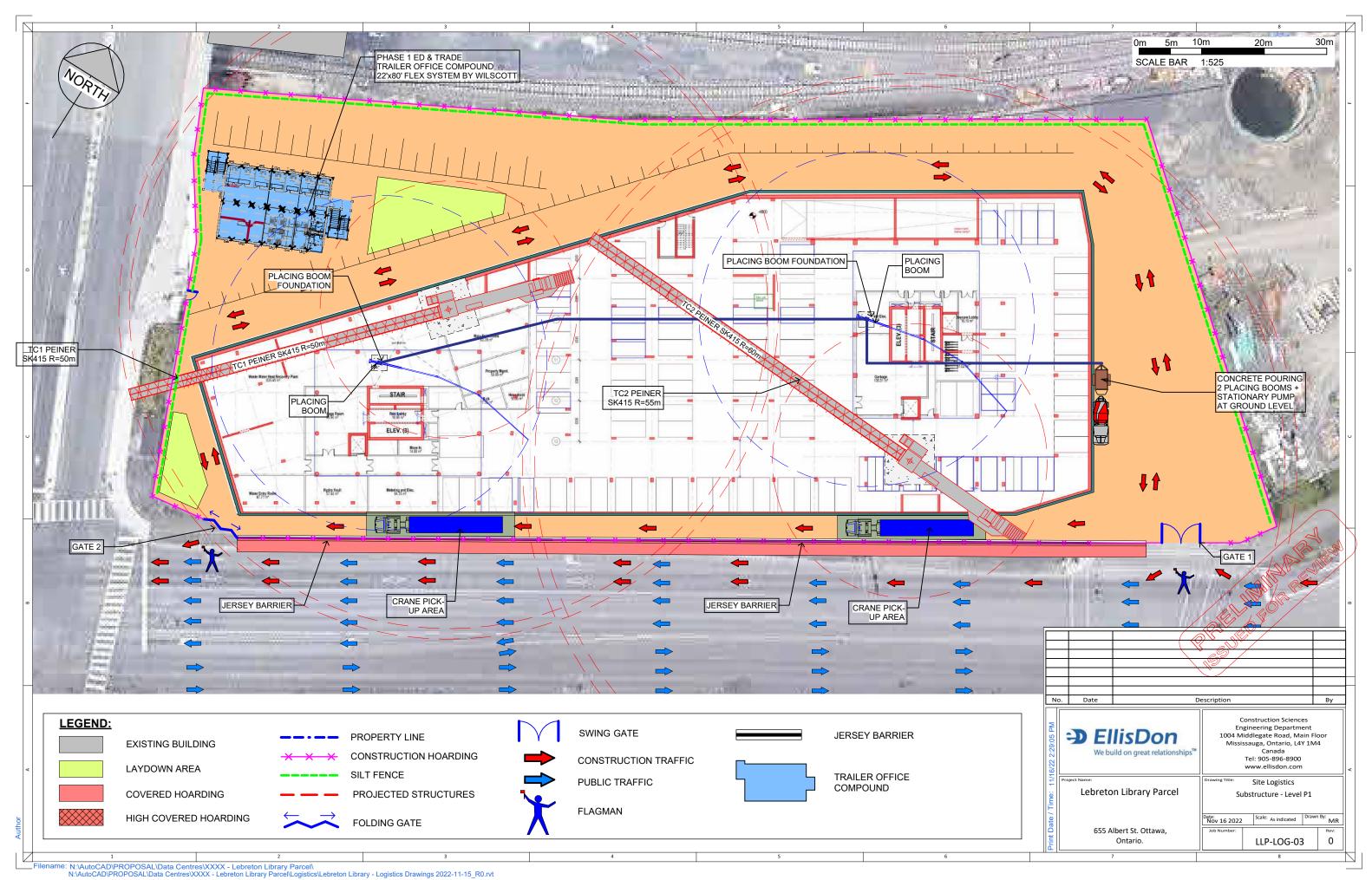


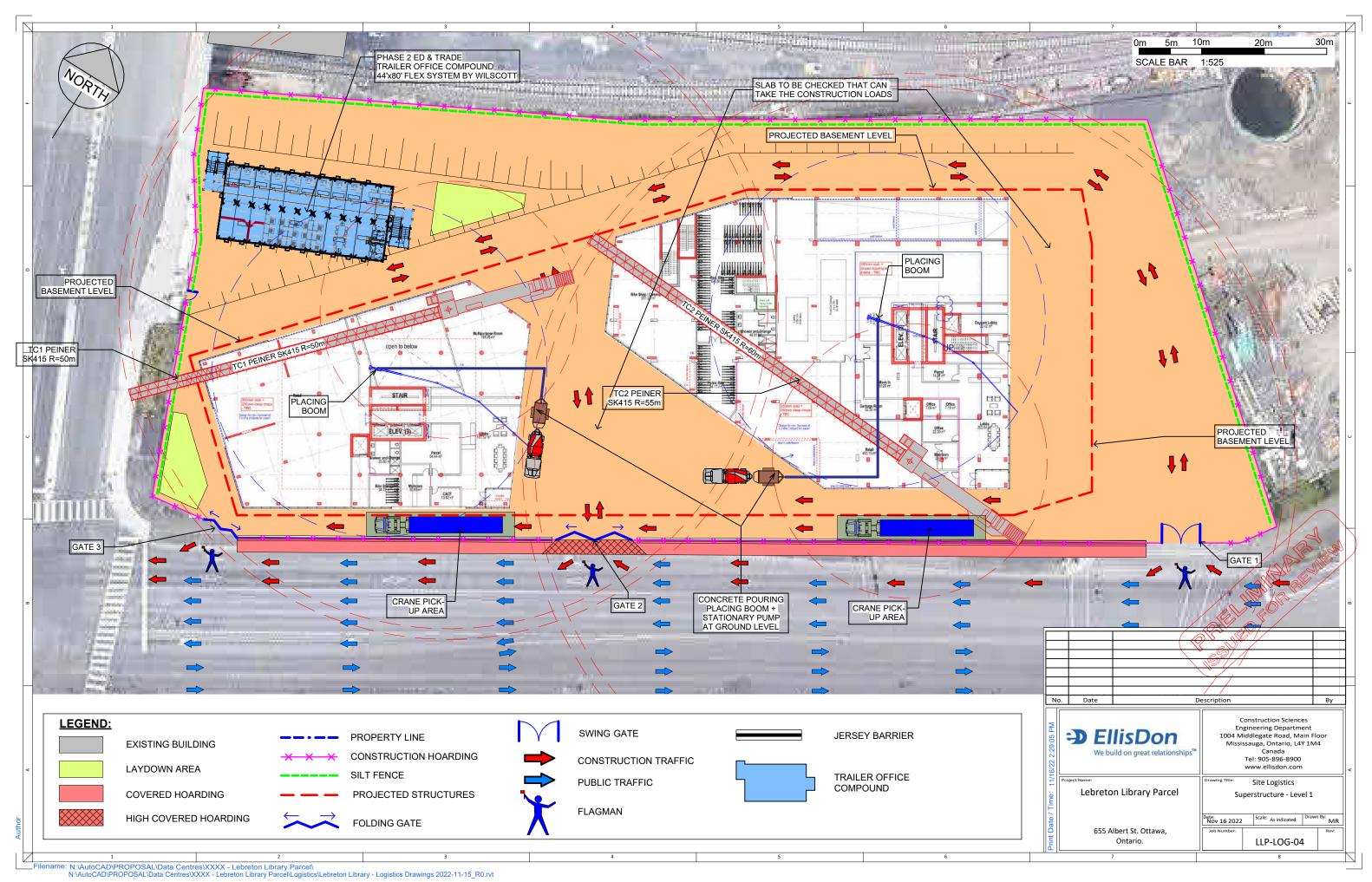
DRAWINGS LIST		
DRAWING #	DRAWING TITLE	ISSUE DATE
LLP-LOG-00	Cover Page	Nov 16 2022
LLP-LOG-01	Mobilization and Site Offices	Nov 16 2022
LLP-LOG-02	Excavation Works	Nov 16 2022
LLP-LOG-03	Substructure - Level P1	Nov 16 2022
LLP-LOG-04	Superstructure - Level 1	Nov 16 2022
LLP-LOG-05	Superstructure - Level 3	Nov 16 2022
LLP-LOG-06	Superstructure - Towers Construction	Nov 16 2022
LLP-LOG-07	Site Safety Plan COVID-19	Nov 16 2022
LLP-LOG-08	South Elevation	Nov 16 2022

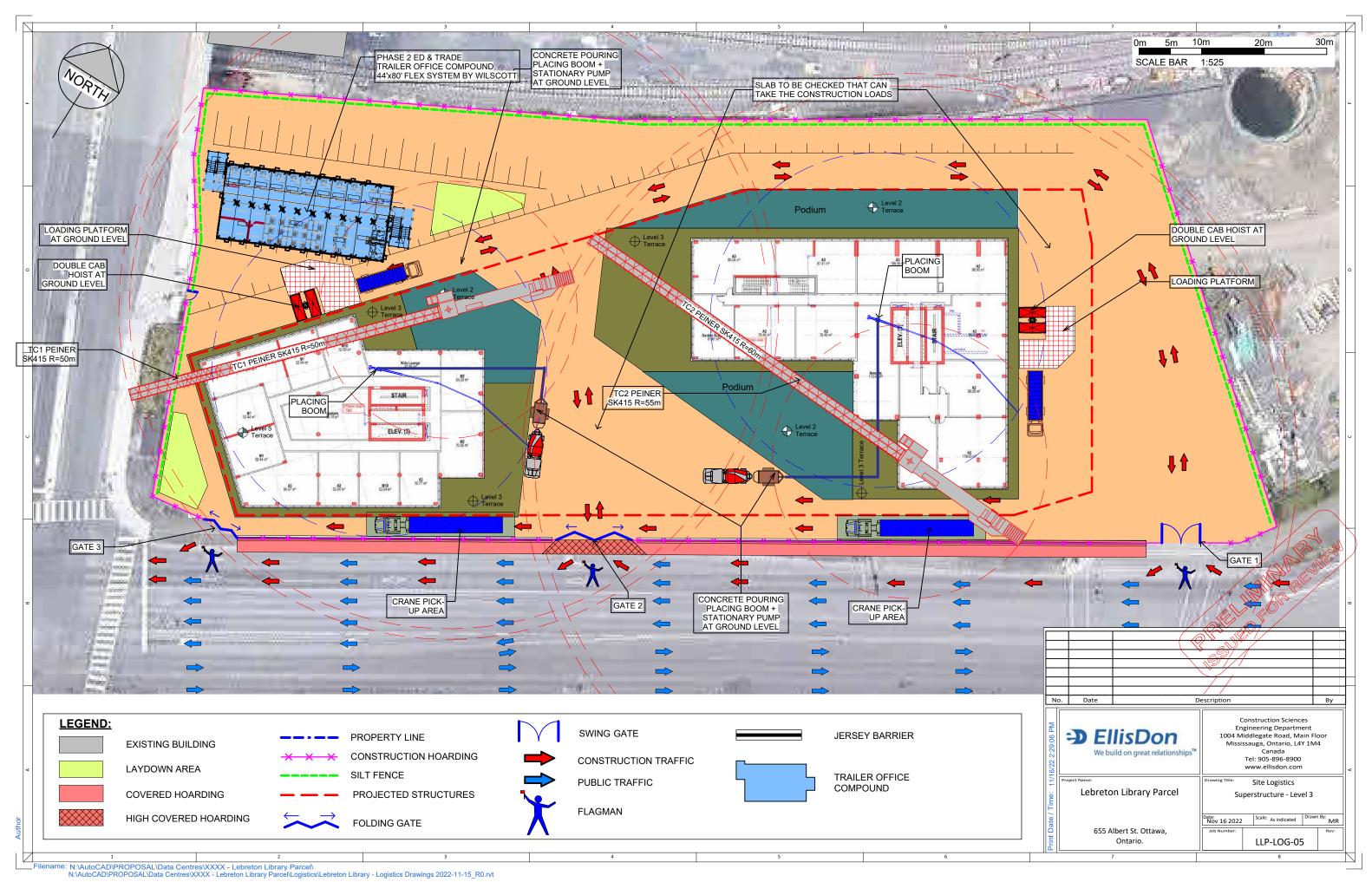


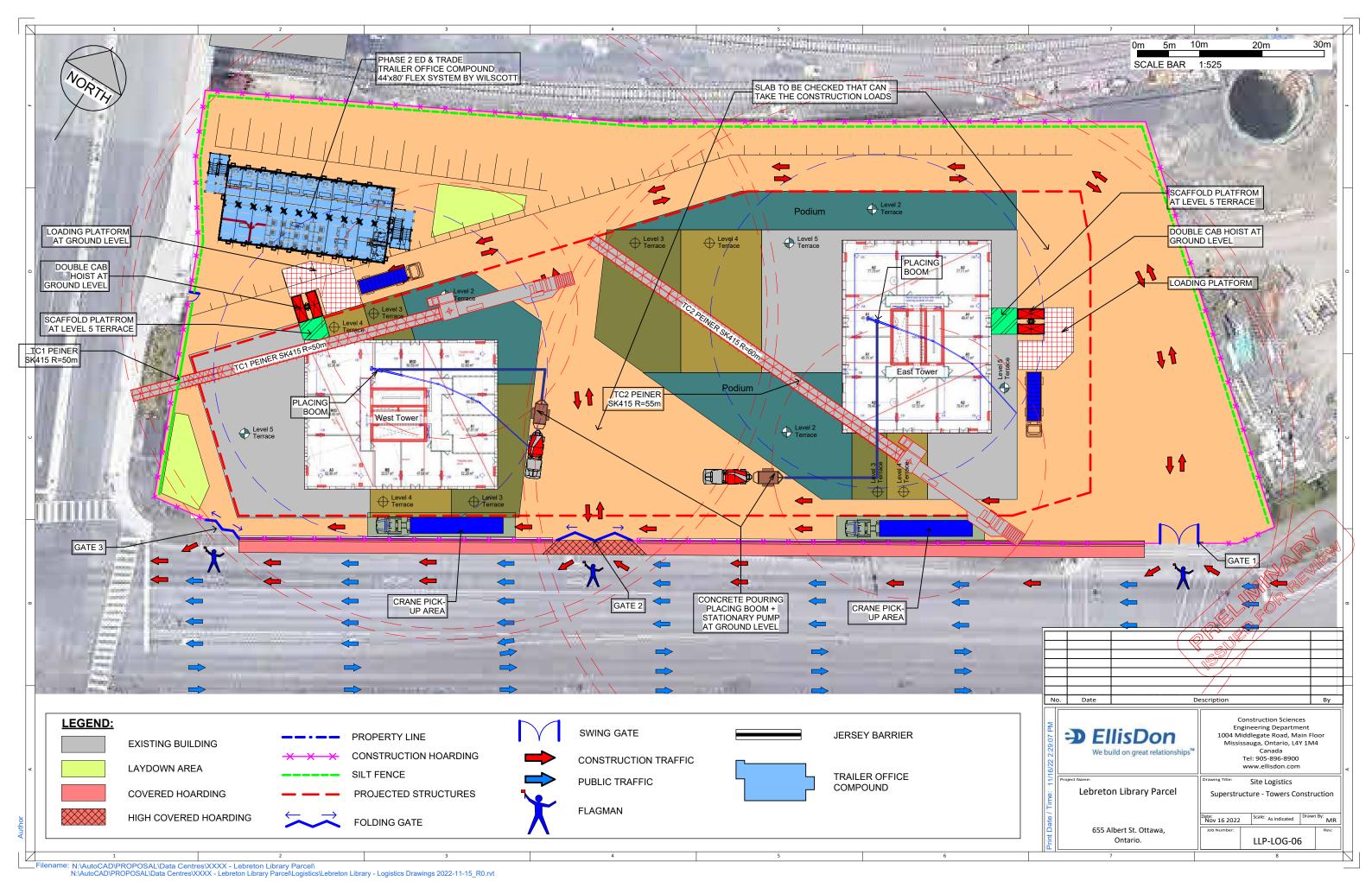


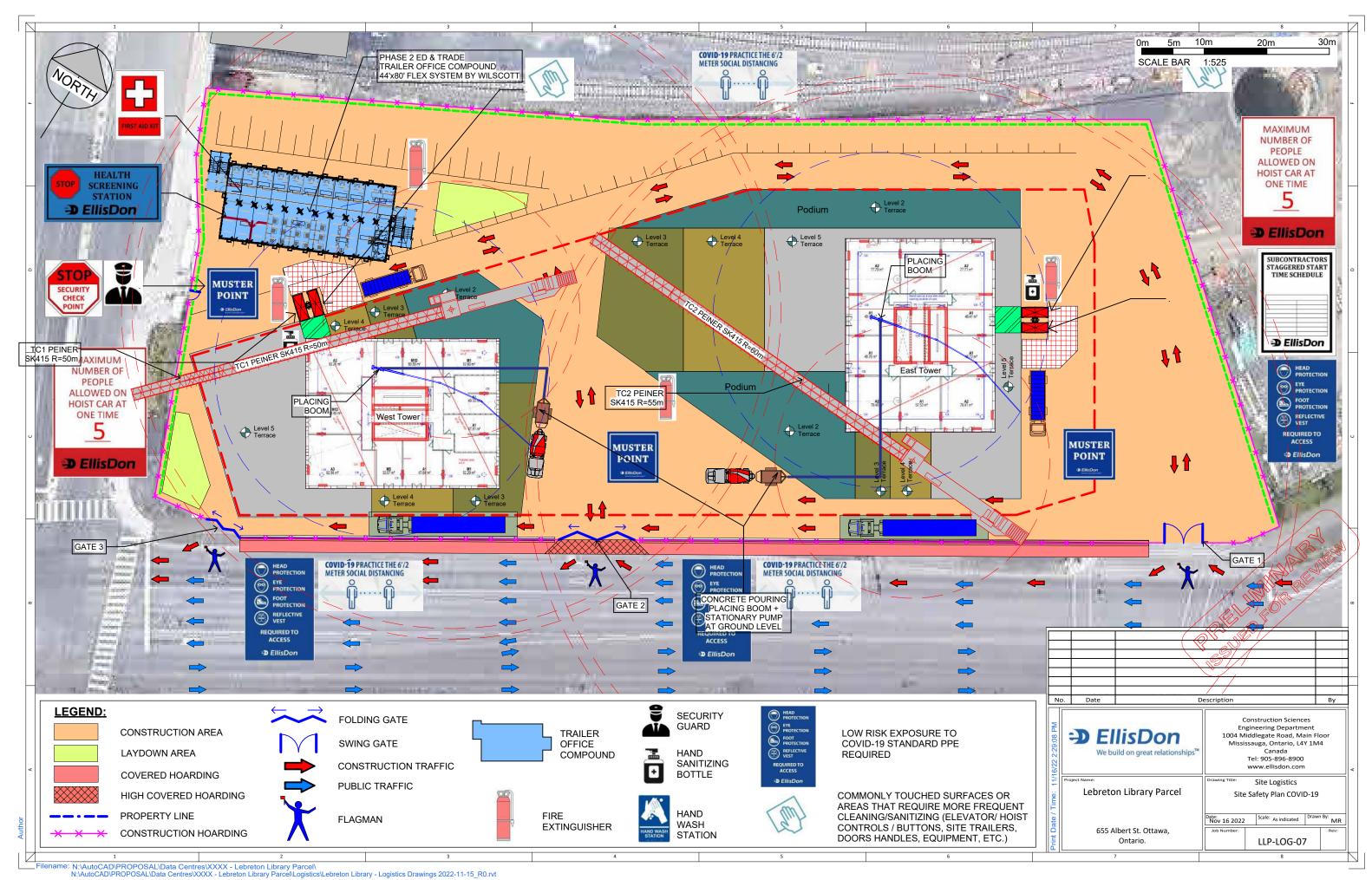


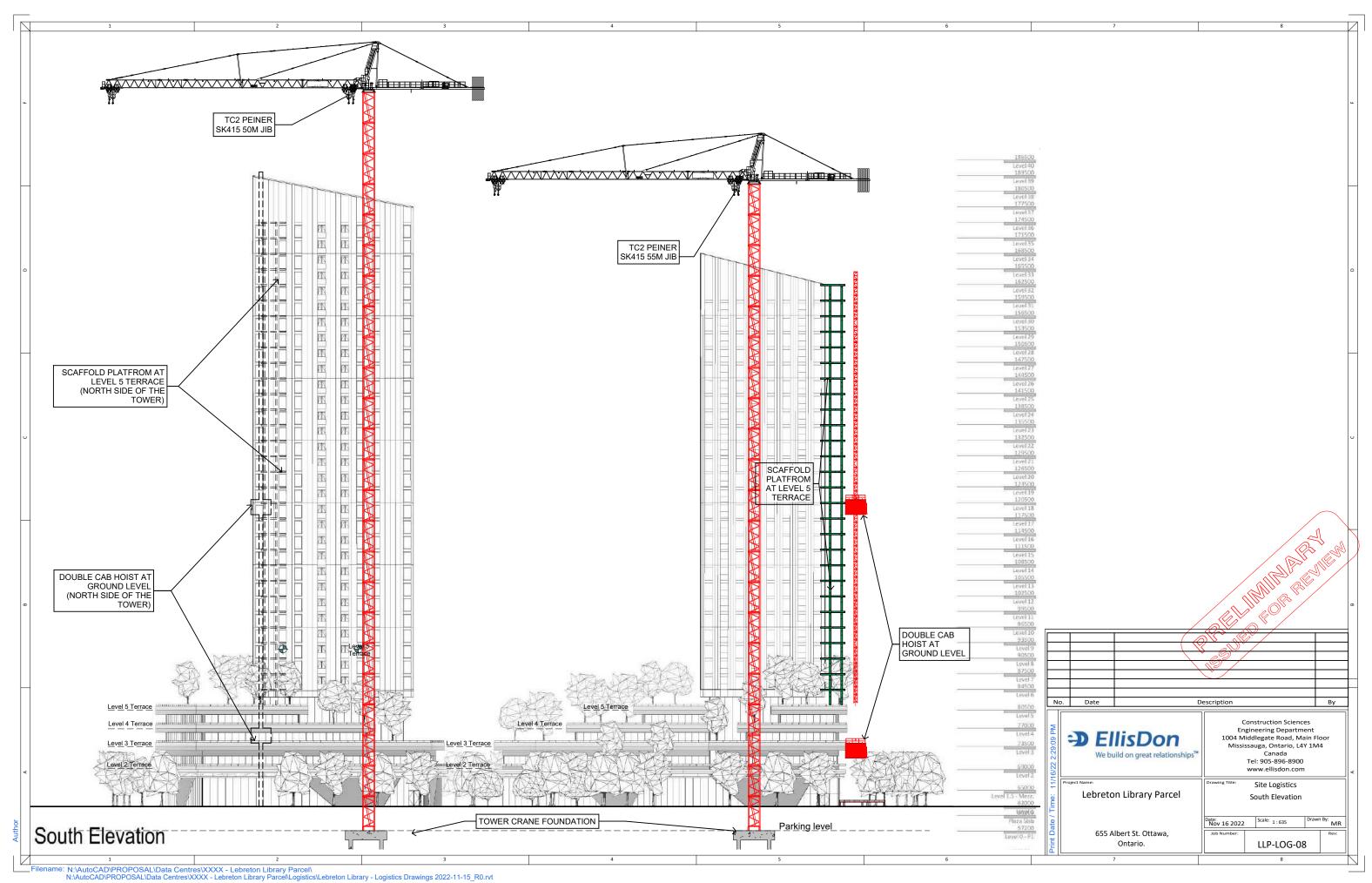














APPENDIX G

Structural Engineering Documentation



November 2, 2022

Justin Robitaille
Dream
30 Adelaide st. E
Toronto, ON, M5C 3H1
jrobitaille@dream.ca

Dear Justin Robitaille,

RE: LeBreton Library Parcel

RJC No. [OTT.128984.0001]

Structural approach for construction adjacent to existing City infrastructure 665 Albert St. Ottawa

The intent of this letter is to describe the approach taken by the design team to mitigate any structural impact of the proposed development to the existing City infrastructure running in the vicinity of the site.

The proposed structure will be supported on reinforced concrete caissons drilled down and socketed into the bedrock for all heavily loaded tower structural elements. For the lightly loaded columns and walls, smaller "pipe piles" drilled and socketed to rock will be provided.

Based on the as-built drawings available to RJC, three key pieces of City infrastructure run along the north foundation wall of the proposed development site. The closest service is the 2400mm EWT concrete sewer pipe running parallel to the north foundation wall with an invert elevation of approximately 45560. The conduit runs at a distance of 3 to 10m from the foundation wall. No existing conduit is to remain within the footprint of the proposed development.

As per Golder's geotechnical recommendations, the deep foundation system underneath the foundation wall and adjacent columns will be socketed 1m into the bedrock, hence loading the rock in friction approximately between elevation 47000 and 48000. Based on the provided as-built drawings of the existing services, the minimum horizontal distance from the buried pipe to the edge of the caisson is at least 3m (refer to RJC drawings S198-S198E-S198W-S702 attached to this letter). The invert elevation of the pipe is around elev. 45m, providing a minimum 1H:1V slope from the invert to the highest point of application of the deep foundation force in the rock. Based on Golder's geotechnical recommendations, these conditions should not impose any significant stress increase to the existing services.

LeBreton Library Parcel
Structural approach for construction adjacent to existing City infrastructure
665 Albert St. Ottawa

RJC No. [0TT.128984.0001]

November 2, 2022

Page 2

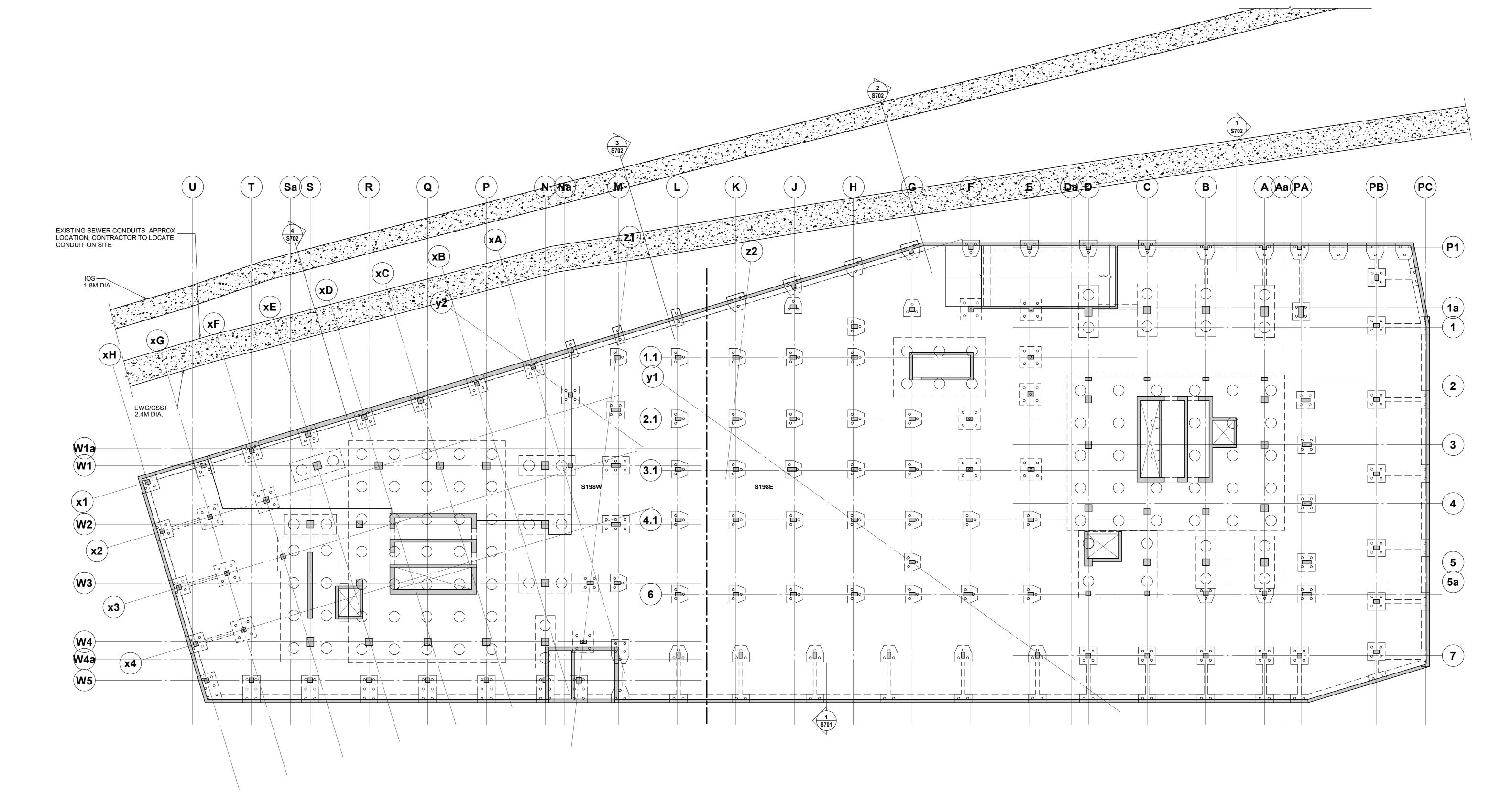


Trusting this letter is sufficient to confirm that the proposed structural foundation system is being designed to mitigate any structural impact on the existing city infrastructure running north of the site. RJC remains available to respond to any questions on this matter.

B. BOULANGER 100215168

Best regards,

Benoit Boulanger, MASc, P.Eng. Regional Manager, Associate



OVERALL FOUNDATION PLAN

FOUNDATION PLAN NOTES		
1.	FOUNDATION ELEVATIONS, BEARING STRATA,	
••	BEDROCK DEPTH AND SOCKET LENGTH TO BE	
	VERIFIED BY GEOTECHNICAL ENGINEER ON SITE AND	
	MAY NEED TO BE ADJUSTED ON SITE.	
2.	FOUND TOP OF CAISSONS (OR PILE) CAP (T.O.C.C.) AT	
	ELEVATIONS SHOWN ON PLAN. BOTTOM OF CAISSON	
	OR PILES TO BE DETERMINED BASED MINIMUM SOCKET	
	LENGTH INDICATED IN CAISSONS AND PILES	
	SCHEDULES.	
3.	THE RESULTING BOTTOM OF CAISSON AND PILES	
	ELEVATIONS ARE ESTIMATES BASED ON THE	
	GEOTECHNICAL REPORT. ALLOWANCE SHOULD BE	
	CARRIED BASED ON VARIATIONS FROM THE ASSUMED	
	SITE CONDITIONS	
4.	BORE HOLE LOCATIONS ARE SHOWN FOR	
	INFORMATION ONLY. REFER TO GEOTECHNICAL	
_	REPORT FOR EXACT LOCATIONS	
5.	CENTRE ALL CAPS, PILASTERS, AND FOOTINGS UNDER	
^	COLUMNS EXCEPT AS NOTED ON PLAN.	
6.	SUBGRADE PREPARATION BELOW THE SLAB ON GRADE	
	IS PER THE GEOTECHNICAL REPORTS. SUB-FLOOR	
7	DRAINAGE IS PER THE MECHANICAL DRAWINGS REFER TO MECHANICAL DRAWINGS FOR PITS SIZE AND	
7.	LOCATIONS. REFER TO GENERAL NOTES	
0	THE SHORING SYSTEM WHERE SHOWN CONCEPTUALLY	
8.	IS ONLY TO CLARIFY THE INTERFACE BETWEEN	
	STRUCTURE AND THE EXCAVATION SHORING SYSTEM	
	USED. REFER TO EXCAVATION SHORING PERMIT	
	DRAWINGS FOR LOCATION, SIZE AND DETAILS OF THE	
	TEMPORARY SHORING WALL.	
9.	PROVIDE GROUND SEAL WHERE REQUIRED BY SITE	
0.	CONDITIONS, GEOTECHNICAL REPORT, OR	
	GEOTECHNICAL CONSULTANT.	
10.		
-	GENERAL NOTES – \$100 SERIES	
	 COLUMN SCHEDULE - S300 SERIES 	
	 SHEAR WALL ELEVATIONS, ZONE 	
	SCHEDULE - S400 SERIES	

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Two Row Architect

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EllisDon 2680 Queensview Dr., Ottawa, ON K2B 8J9

tes

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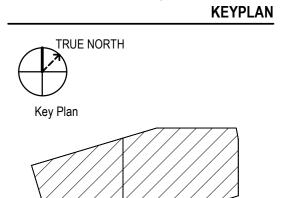


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Designed By M.C. Date 2022-10-27
Checked By B.B.

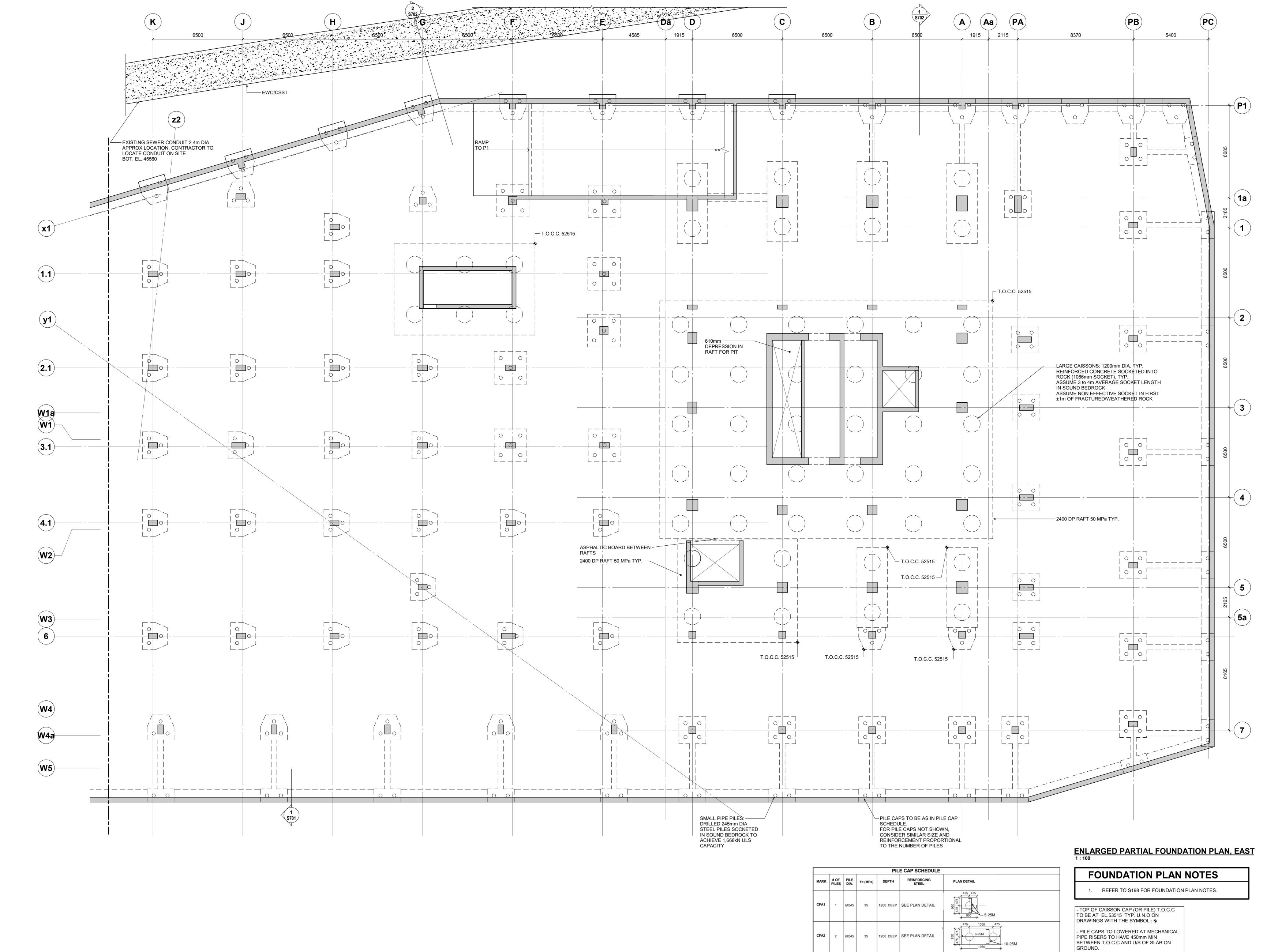
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TITLE

OVERALL FOUNDATION

SHEET NUMBER

S198



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Two Row Architect 1804 6th Line, Ohsweken, ON N0A 1M0 CONTRACTOR

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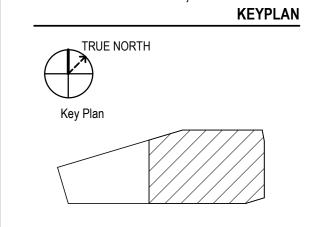
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CFA4 4 Ø245 35 1200 DEEP SEE PLAN DETAIL

- TOP OF ROCK AVERAGE IS APPROX. AT ELEV. 48.0m, REFER TO GEOTECHNICAL

- EXCAVATION AND SHORING SYSTEM

DRAWINGS

SHOWN SCHEMATICALLY ONLY, REFER TO

GENERAL CONTRACTOR'S LOGISTIC PLAN AND SHORING SPECIALTY ENGINEER'S

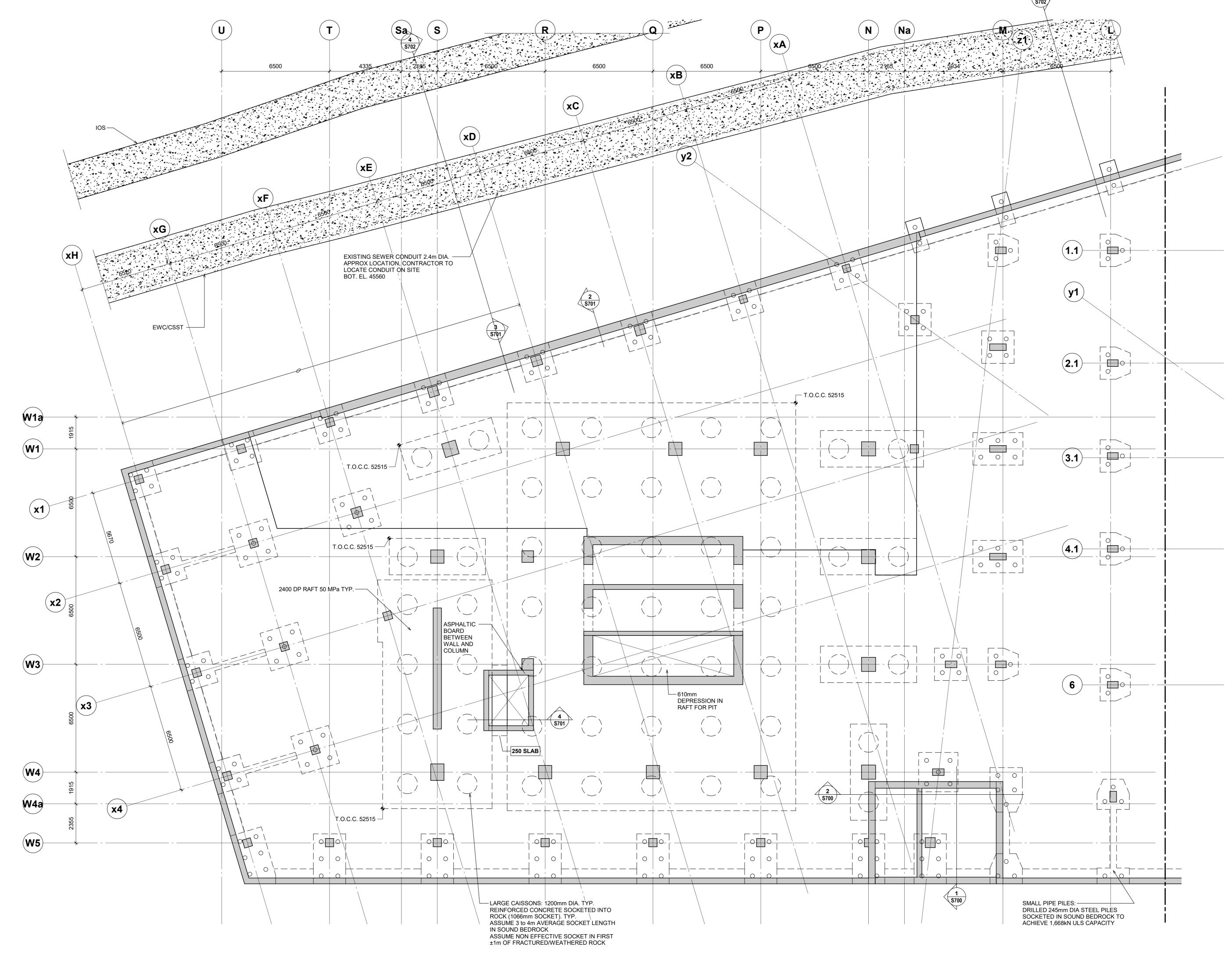
> **ENLARGED PARTIAL FOUNDATION PLAN, EAST**

Job Number

SHEET NUMBER

S198E

TITLE



ENLARGED PARTIAL FOUNDATION PLAN, WEST

FOUNDATION PLAN NOTES

1. REFER TO S198 FOR FOUNDATION PLAN NOTES.

- TOP OF CAISSON CAP (OR PILE) T.O.C.C TO BE AT EL.53515 TYP. U.N.O ON DRAWINGS WITH THE SYMBOL : ◆

- PILE CAPS TO LOWERED AT MECHANICAL

PIPE RISERS TO HAVE 450mm MIN BETWEEN T.O.C.C AND U/S OF SLAB ON GROUND.

- TOP OF ROCK AVERAGE IS APPROX. AT ELEV. 48.0m, REFER TO GEOTECHNICAL

- EXCAVATION AND SHORING SYSTEM SHOWN SCHEMATICALLY ONLY, REFER TO GENERAL CONTRACTOR'S LOGISTIC PLAN AND SHORING SPECIALTY ENGINEER'S DRAWINGS

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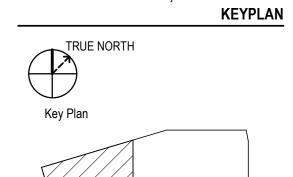


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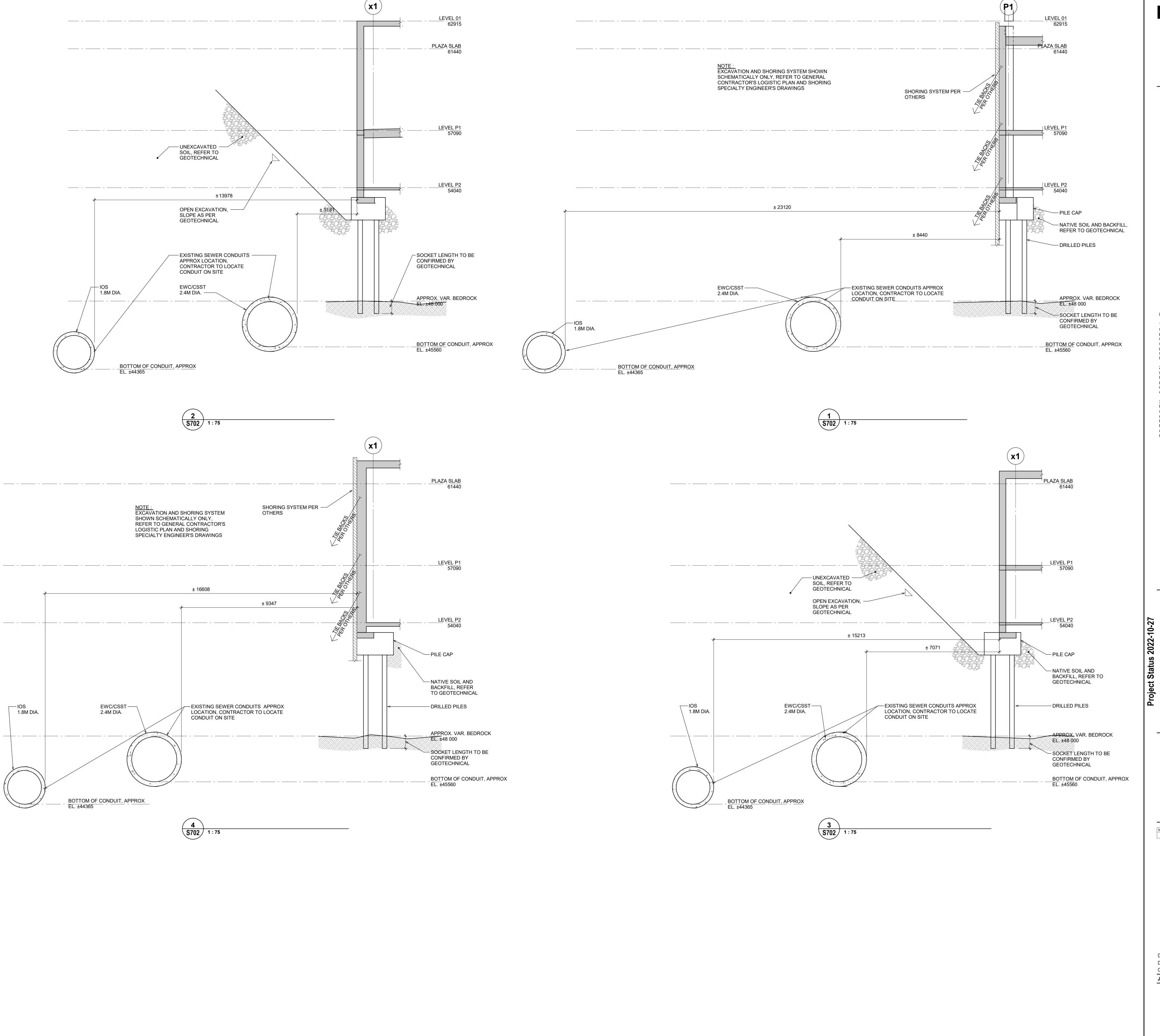
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L4K 0C5
CONSULTANT
Two Row Architect

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CONTRACTOR
EllisDon
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Key Plan

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 Scale
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 Designed By
 M.C.
 Date
 2022-10-27

 Checked By
 B.B.
 OTT.128984.0001

SECTION

SHEET NUMBER

S702



APPENDIX H

H1: City Comments (Stantec Memo)

H2: Golder Response (Geotechnical Analysis Memo)





To: Steven Courtland From: Colin Goodwin, Shawn Ireland

City of Ottawa Ottawa ON Office

File: CSST: 665 Albert Development Review Date: November 2, 2022

Package

Reference: CSST: 665 Albert Development Review Package, Stantec Review of Interfacing with CSST Infrastructure

The City requested Stantec complete a review of the development review package submitted for 665 Albert as it relates to potential impacts to adjacent CSST infrastructure at the site. This memo summarizes Stantec's review. Two documents were provided by the City for the review as follows:

- 1. LeBreton Library Parcel, Constructability Report (TYLin Ref. 10399), dated April 2022, Prepared by TYLin for Dream Asset Management; and
- 2. Geotechnical Investigation, LeBreton Library Parcel, 665 Albert Street, Ottawa, Ontario, dated April 2022, Prepared by Golder Associates Ltd. for Dream Impact Master LP.

SUMMARY OF STANTEC REVIEW

The City asked Stantec to review the developer's constructability report and accompanying geotechnical report, which discusses proximity of the development's shoring, excavation, footings, permanent structures etc. on the adjacent 2400mm East-West-Tunnel. Comments are provided as follows:

- 1. Background on the EWT pipe: The East-West-Tunnel (EWT) section in question was installed in 2015-2016 under the Lebreton Flats Diversion Chamber project. As-built drawings prepared for City Contract No. ISD13-2007 depict the pertinent infrastructure. The EWT pipe is Class 185D precast concrete pipe, the pipe depth is around 15m, and was installed via open cut within a rock trench.
- 2. Drawings and Construction Plans: The developer should provide plans showing details of the proposed shoring system and permanent underground works, showing details on proximity to the EWT at several cross sections along the development. The cross section should also include any required temporary shoring and/tie backs that may be required to perform the work, including limits of excavation.
- 3. Confirming no loads are applied to the EWT from the proposed development:
 - a. The EWT was installed via open cut, where the bottom portion of the pipe was installed within a bedrock trench and the pipe was backfilled in concrete within the bedrock trench. Since the pipe/concrete backfill is essentially in direct contact with the rock, the developer should review and confirm that there are no additional loads which will be applied to the EWT from the proposed permanent and/or temporary works.
 - b. The constructability report states that the caissons will be embedded 1 m into rock and that the caisson will be "at least 3 m (3 times the diameter of the proposed caisson)" but the report does not actually state the caissons will have a 1 m diameter.
 - c. In the supplied Golder geotechnical report, we could not locate a statement that corroborates the following statement from the constructability report "Based on Golder's geotechnical"

Reference: CSST: 665 Albert Development Review Package, Stantec Review of Interfacing with CSST Infrastructure

recommendations, these conditions should not impose any significant stress increase to the existing services".

- d. Is full fixity of the caissons required? Per 5.2.1.4 of the Golder report, if full fixity is required, the caisson depth may need to be increased.
- e. The report also states "should not impose any significant stress increase to the existing services.". The increase stress should be quantified.

4. Miscellaneous comments:

- a. The plans included within the constructability report (Figure 1-1) appears to show the existing Real Time Control (RTC) underground control vault at Booth/Albert and the associated underground ductbanks from this vault to the RTC facilities. It is unclear how/if the infrastructure is affected by the work, but this should be reviewed and addressed by the proponent. Excavations may extend into the footprint of the vault and the ductbanks, potentially requiring temporary support and protection.
- b. The West tower excavation proposes a shoring system with what appears to be tie-backs (see Excavation Works drawings). Some of these tie-backs appear to be in conflict with the existing RTC regulator and CSST chambers under Booth Street. Shoring system design to consider the location of existing City infrastructure, prevent conflicts with the structures, and confirm that no additional loads will be applied to the structures.
- c. Site laydown areas and access roads appear to cross over the existing EWT, IOS and Albert Storm Sewer in various locations. It is unclear from the excavation drawings what the site elevations will be at various stages of excavation and construction. The developer should confirm the minimum amount of cover that will remain above the existing sewers within the site and if any protective measures would be required to protect the sewers from construction activity.
- d. Excavations in proximity to the existing RTC regulator and CSST chambers west of the site should consider the existing CIP retaining wall adjacent to the chambers. The bottom of this wall does not extend very far below existing grade, and may need to be supported if excavation slopes cannot match existing grades at the perimeter of the development site.
- e. Existing temporary shoring systems in proximity to the RTC and CSST chambers could be in conflict with the proposed works, depending on the required depths of excavation in the area. Developer to consider risk of load transfer to nearby existing infrastructure (EWT, IOS, Albert Storm Sewer) during excavation and removal of pre-existing temporary shoring if conflicts are identified. Pertinent as-built drawings are attached to this memo for clarity.
- f. The developer should provide drawings of proposed retaining wall along north side of site, and clarify its position relative to the EWT, IOS and Albert Storm Sewer and demonstrate that no additional loads will be imposed on the existing sewers.
- Vibration limits and monitoring: typical OPSS/City of Ottawa limits should apply to the development work. Developer to establish a vibration monitoring plan that considers the EWT, IOS,

November 2, 2022 Steven Courtland Page 3 of 3

Reference: CSST: 665 Albert Development Review Package, Stantec Review of Interfacing with CSST Infrastructure

Albert Storm Sewer, and associated chambers including response measures and contingency plans in the event of vibration threshold exceedances.

Pre and post condition surveys: pre-construction CCTV should be completed along with postconstruction CCTV.

SUMMARY

Stantec's review was limited in nature to the documents provided and was intended to identify key areas for consideration by the City and the developer in mitigating impacts to existing CSST related infrastructure adjacent to the development at 665 Albert.

Should you have any question or concerns with the comments provide in this memo, please reach out to Colin or Shawn directly.

Stantec Consulting Ltd.

Colin Goodwin P.Eng. Environmental Engineer

Phone: 613.697.5124 Colin.Goodwin@stantec.com

Attachment: ISD13-2007 As-Built Drawing C-03

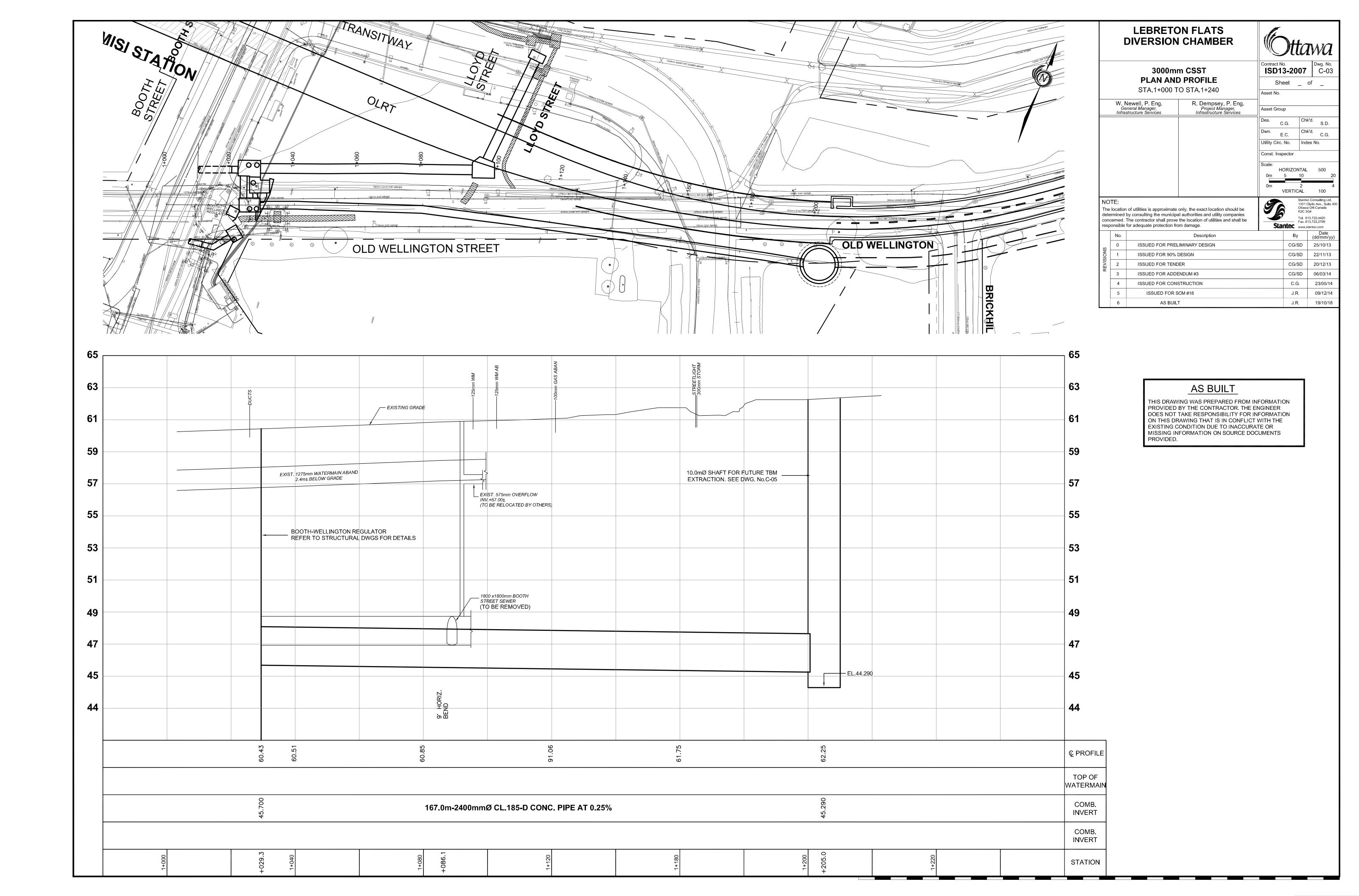
ISD13-2007 As-Built Drawing S-401

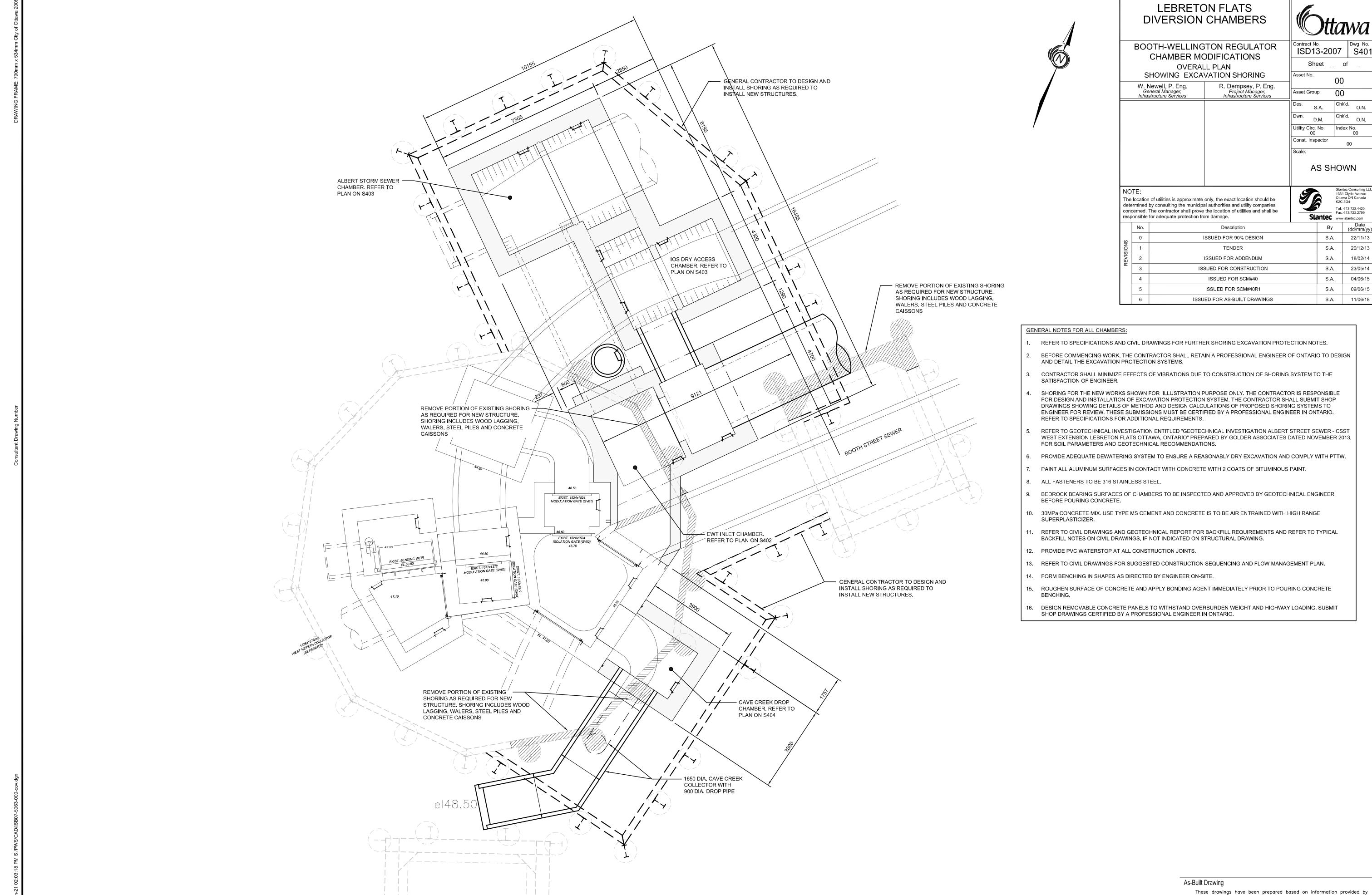
c. Adrien Comeau

Shawn Ireland P.Eng. Environmental Engineer

Lucy Polard

Phone: 613-218-4845 Shawn.Ireland@stantec.com





These drawings have been prepared based on information provided by others. Stantec has not verified the accuracy and/or completeness of this information and shall not be responsible for any errors or omissions which may be incorporated herein as a result.



TECHNICAL MEMORANDUM

DATE December 19, 2022 **Project No.** 22511882 (20141216)

TO Justin Robataille, Dream Properties

CC Ben Worth, TY Lin

FROM Chris Hendry EMAIL chris.hendry@wsp.com

REVIEW OF PROPOSED FOUNDATIONS AND CSST INFRASTRUCTURE - DREAM LEBRETON PROJECT

Ben,

As requested, Golder has reviewed the proposed foundations for the Dream LeBreton project and their potential impact on the existing CSST infrastructure.

The following documents have been reviewed:

- A letter prepared by RJC Engineers (RJC) titled "LeBreton Library Parcel, Structural Approach for Construction Adjacent to Existing City Infrastructure", dated November 2, 2022. This letter contains foundation plans and cross sections for the proposed new development.
- A memo prepared by Stantec Consulting Ltd. (Stantec) titled "CSST: 665 Albert Development Review Package, Stantec Review of Interfacing with CSST Infrastructure", dated November 2, 2022.

Proposed Foundations

There are two types of foundations proposed for the new development:

- The high-rise towers (which are in the interior of the overall structure) are supported on 1200 mm diameter caissons, socketed 3 m to 4 m into rock.
- The podium and exterior walls are supported on groups of 245 mm diameter pipe piles, also socketed into bedrock. Along the northern perimeter wall (which is the area relevant to a discussion of the CSST Infrastructure) the piles are installed in groups of three. These pipe piles are intended to carry factored ULS loads of 1,668 kN. The piles have also been designed to carry horizontal loads of 75 kN to account for possible eccentricity of loading as well as small lateral loads.

The foundation locations and cross sections are shown on the plans prepared by RJC and attached to their November 2 letter.

Existing CSST Infrastructure

Based on information contained in the Stantec memo as well as the RJC drawings, there is an existing 2.4 m diameter precast concrete sewer which forms part of the CSST infrastructure. This sewer is referred to as the EWT tunnel. The EWT tunnel is located 3.2 m from the exterior wall at its closest point to the new building (see Section 2 on Sheet 702 of the RJC foundation drawings). At all other locations the distance is greater than 3.2 m.

The EWT was installed in a trench within the bedrock at the site, and the sewer obvert is at an elevation roughly coincident with the anticipated bedrock surface (and therefore the sewer is at a similar elevation to the proposed rock sockets).

There is a second, slightly deeper, 1.8 m diameter sewer (identified as the IOS) located some 7 m north (further from the building).

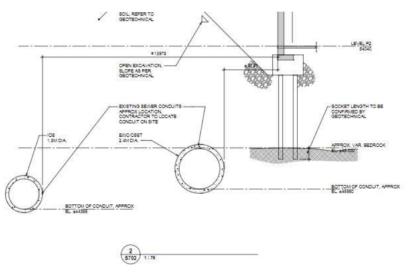


Figure 1 - Example Cross Section Along North Foundation Wall

Impact of the Proposed Foundations on the EWT

As part of this review, Golder as evaluated the potential for the proposed new building foundations to impact the existing EWT.

Large Diameter Interior Caissons

The closest large interior caissons which support the towers are located approximately 12 to 15 m from the EWT. This corresponds to approximately 10 to 12 times the diameter of the piles¹. This distance is beyond the area identified in the CSST guidance as requiring specific consideration. Regardless, at these distances, no meaningful interaction between the EWT and the interior caissons should be expected, even if the caissons are resisting large lateral loads.

¹ The zone of influence of a pile or foundation is proportional to the loaded area; for a given load intensity, larger foundations will cause stress changes in a larger mass of soil/rock. Typically, individual footings will cause stress changes within 2 – 3 times their width, while continuous strip footings may cause stress changes within 4 to 6 times their width.



Small Diameter Pipe Piles

The smaller pipe pile groups supporting the north foundation wall are located approximately 3.2 m from the EWT (at the location of the closest group to the sewer; other pile groups are further away).

A conservative approach commonly adopted to determine the potential for vertical foundation loads to impact the ground below them is to assume that the foundations could impact an area below a 1:1 line extending down and out from the edge of the foundation. A less conservative (but more accurate) approach is presented in the Canadian Foundation Engineering Manual which presents stress contours below a uniformly loaded area obtained from elastic solutions presented in Poulos and Davis (1974). A similar method for calculating stress distributions within the ground due to imposed loading (the Boussinesq stress distribution) is also common.

Both of these methods (a simple assumed 1:1 line and series of stress contours as per the CFEM) are presented on the cross-sections attached. As can be seen from these cross sections, there is no expectation that any meaningful loading would be transferred to the EWT by the foundation piles. It should also be noted that the stress contours presented treat the pile group as a single foundation unit. If consideration was given to the individual 245 mm diameter piles the stressed area would be dramatically smaller. As can be seen in the attached figures, there is no potential for the exterior piles to transfer any significant vertical loading to the EWT.

The exterior piles are designed to accommodate nominal lateral loads due to eccentricities in construction as well as minor lateral loads applied to the pile caps. The majority of the small lateral loads would typically be resisted by the approximately 8 m of soil between the bedrock and the top of pile cap. This soil is above the EWT and lateral stresses in the upper soil have no potential to impact the EWT.

In addition, the 245 mm diameter piles are located approximately 3.2 m from the edge of the EWT. This corresponds to approximately 13 pile diameters at their closest point. Given the distances and the lengths of the piles, there is no significant risk of the small diameter exterior piles transferring any meaningful lateral loads to the EWT.

Additional Comments Related to Stantec Review

The following provides additional discussion related to specific comments contained in the November 2 Stantec Review. Note that not all comments are related to the foundations and so only responses relevant to the geotechnical aspects of the pile foundations are provided.

- Comment 3a: Golder has reviewed the foundation drawings and confirms that there are no additional loads expected to be applied to the EWT by the proposed foundations.
- Comment 3b: The current RJC drawings indicate that the caisson foundations will have a diameter of 1.2 m and will have a rock socket depth of 3 to 4 m.
- Comment 3c: The statement is not included in the geotechnical report because the foundations were not
 designed at the time of preparing the report. We believe this statement in the constructability report refers
 to subsequent correspondence and discussion. Regardless, it is Golder's opinion that the currently
 proposed foundations should not impose any significant stress increase to the existing services in
 question and, notwithstanding the reference, the statement in the constructability report is generally valid.



- Comment 3d: The caissons are designed to have a rock socket depth of 3 to 4 m which is approximately 3 times the proposed diameter. This would typically be sufficient to be considered fixed (though the quality of the rock sockets does need to be confirmed during construction).
- Comment 3e: Given the discussion above, the increase in stress due to the permanent foundations is expected to be essentially zero.
- Comments 4a to 4e: These comments relate to shoring and temporary works which are designed by
 others. Golder would be pleased to provide additional review as required as these aspects of the project
 are designed in further detail.
- Comment 5: Golder agrees that a vibration monitoring plan should be developed for the project. Golder can assist with development of a vibration monitoring plan if required.
- Comment 6: Golder agrees that pre- and post-construction CCTV inspections should be carried out.

Closure

We trust this provides the information you require at this time. Should you require anything further, or have any questions please feel free to contact the undersigned at your convenience.

Golder Associates Ltd.

Alledo

Chris Hendry, M.Eng., P.Eng. Sr. Principal Geotechnical Engineer

CH/ljv

Attachments: Figure 1 - Cross-Sections

https://golderassociates.sharepoint.com/sites/158117/project files/7 correspondence/20221214 response to city comments re foundations and csst/22511882 20141216 tm rev0 2022'12'19 lblp foundation review.docx



