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REPORT ON

HYDROGEOLOGICAL STUDY PROPOSED COACH HOUSE 5812 RED CASTLE RIDGE OSGOODE WARD CITY OF OTTAWA, ONTARIO

Submitted to:

Hassan Sannoufi 5812 Red Castle Ridge Manotick, Ontario K4M 0A4

REVISION DATE September 7, 2022 DATE July 20, 2022

DISTRIBUTION

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220067



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July 20, 2022 (Sept. 7, 2022)

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Hassan Sannoufi 5812 Red Castle Ridge Manotick, Ontario K4M 0A4

RE: HYDROGEOLOGICAL AND TERRAIN STUDY

PROPOSED COACH HOUSE 5812 RED CASTLE RIDGE OSGOODE WARD CITY OF OTTAWA, ONTARIO

Kollaard Associates Inc. was retained by Mr. Hassan Sannoufi to undertake a hydrogeological and terrain study for a proposed coach house on Red Castle Ridge in Manotick, Ontario (Key Plan, Figure 1).

It is understood that it is being proposed to construct a coach house on the existing 0.67 hectare (~1.7 acre) property. It is the intention of the owner that the existing well is to be shared between the coach house and the existing dwelling. A new sewage system is to be constructed to service the coach house. It is understood that the proposed coach house is located east of the existing house with the proposed sewage system for the coach house located southeast of the coach house. The attached drawing (Attachment A) is a Proposed Septic Design Plan, prepared by Kollaard Associates Inc, that shows the location of the proposed coach house, the existing dwelling, septic bed and well and the proposed sewage system location.

Kollaard Associates Inc. carried out a six hour pumping test on the existing well at the site and obtained a water sample that was tested for the subdivision list of parameters to confirm that water quantity and quality are acceptable to service the existing and proposed residential development. Information provided by the client from the sewage system design including test pit and topographic survey were used to establish soil conditions with consideration for sewage system design and the potential for sewage system impacts.

This report consists of an evaluation of the water quality and quantity of the existing well at the subject site, and an assessment of the sewage system impact, to ensure that the water quality and quantity of the existing well is acceptable using the following documents; Ministry of the Environment, Conservation and Parks (MECP) Guideline D-5-5 and the Ontario Drinking Water Standards, Objectives and Guidelines (ODWSOG). Consideration has also been given to the groundwater impact assessment guidelines under MECP D-5-4. The scope of work carried out for this assessment was prepared in consideration of the City of Ottawa document "Terms of Reference Scoped Hydrogeological Study for Coach Houses".

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HYDROGEOLOGICAL STUDY

Background

A bedrock geology map for the site area indicates the bedrock at the site consists of dolostone and sandstone of the Beekmantown Group.

The surficial geology map indicates that the soil at the property consists of till on Paleozoic terrain.

One test pit was put down as part of a proposed sewage system design to service the proposed coach house. The test pit was put down by a member of Kollaard Associates Inc. as part of the sewage design for the coach house on February 11, 2022. The test pit encountered about 0.40 metres of topsoil overlying glacial till. The test pit was terminated in the glacial till at about 0.80 metres, where refusal was encountered on a large boulder. The total depth of soil at the site, based on the information from the well record, is some 9.0 metres, consisting of glacial till (described as sand, gravel and boulders in the well record).

The existing well that services the existing dwelling at the site was assessed to determine whether the well is capable of supplying the water demand for the proposed coach house and the existing dwelling. According to the well record, the well is about 54.9 metres deep with 12.2 metres of casing. The pump for the test was installed at about 15 metres below the existing ground surface due to encountering an obstruction. The well record and Certificate of Well Compliance are provided (Attachment B).

Area Well Records

A review of five area well records was carried out. The well records are provided (Attachment B). The depths of the wells are indicated to be between 55 and 83 metres, obtaining water from a limestone aquifer. Test pumping rates for the area wells were 45.4 to 75.7 litres per minute. Recommended pumping rates were between 45.4 and 75.7 litres per minute. Overburden was identified as sand, gravel, clay, and boulders between 4.6 to 9.2 metres in thickness. All area wells had between 12.2 to 13.1 metres of casing below the ground surface.

Water Quantity

A pumping test was carried out on May 19, 2022, at the existing well on the site. The well is a drilled, cased well with about 0.6 metres of casing above the ground surface.

The testing consisted of a 6 hour duration pumping test. During the pumping test, manual water level measurements were made on a regular basis to monitor the drawdown of the water level in the well in response to pumping and water levels were monitored at one minute intervals using a pressure transducer. Groundwater samples were collected from the well after six hours to characterize groundwater quality. Hourly field water quality readings were recorded for the water temperature, pH, total dissolved solids (conductivity) and turbidity. Chlorine residuals were measured prior to obtaining a water sample for lab submission and free chlorine was measured to be zero. After the pump was shut off, the recovery of the water level in the well was measured until 95% recovery of static water level had been achieved or for 24 hours, whichever was less.

The well was pumped for about 360 minutes at a pumping rate of about 41.5 litres per minute. Over the course of the pumping test, the water level in the well dropped some 1.53 metres. At the end of pumping, 95% recovery of the total drawdown in the static water level created during pumping was measured after about 72 minutes.

The pumping test drawdown and recovery data and plots for TW1 are provided as Attachment C. The drawdown and recovery data provided were measured with reference to the top of the well casing at the test well location.

The pumping test data for the test well was analyzed using the method of Cooper and Jacob (1946). Although the assumptions on which these equations are based are not strictly met, this method provides a reasonable estimate of the aquifer transmissivity.

Transmissivity was calculated using the following relationship:

$$T = \frac{2.3Q}{4\pi ds}$$

where

Q is the pump rate, m³/day

ds is the change in drawdown over one time log cycle, m

T is the transmissivity, m²/day

Based on the pumping test drawdown and recovery data, the transmissivity of the aquifer is estimated to be between about 27.4 and 19.9 m²/day, respectively.

Based on the data obtained during the six hour pumping test, it can be concluded that the well is capable of sustaining a short term yield of at least 41.5 litres per minute. During the course of the 6 hour pumping period, 6 percent of the available drawdown in the test well was utilized, based on the recommended pump depth of 30.5 metres and the initial static water level measured at the time of the pumping test (4.85 metres).

The expected water demand for the site was calculated using the total expected residential occupancy. It is understood that the main (existing) house has five bedrooms and that the proposed coach house will contain two bedrooms. Using Guideline D-5-5, total occupancy will consist of six people in the main house and up to three people in the coach house (assuming number of bedrooms plus one for each dwelling). The peak water demand (obtained from MECP D-5-5) is taken as 3.75 litres per person per minute, equivalent to 33.75 litres per minute. This peak demand rate is assumed to occur for a period of two hours each day. The pump test rate was 41.5 litres per minute. Therefore, there is sufficient water quantity available to service the peak water demands at the site.

Water Quality

To determine the water quality of the groundwater supply, groundwater samples were obtained from the well after six hours during the pumping test and prepared/preserved in the field using appropriate techniques and submitted to Eurofins Environmental Testing in Ottawa, Ontario, for the chemical, physical and bacteriological analyses listed in the Ministry of the Environment (MECP) guideline entitled Procedure D-5-5, Technical Guideline for Private Wells: Water Supply Assessment, August 1996. The results of the trace metals, chemical, physical and bacteriological analyses of the water samples obtained from the test well are provided in Attachment D. A summary of the water quality measured in the field are provided as Table I, Water Quality Measurements for Test Well.

The water quality as determined from the results of the analyses is favourable. The water meets all the Ontario Drinking Water Standards, Objectives and Guidelines (ODWSOG) health and aesthetic parameters tested for at the test well except for hardness, total dissolved solids, and total coliforms.

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Sodium level is at the 20 mg/l medical advisory limit but well within the aesthetic objective. When sodium levels exceed 20 mg/l, the local Medical Officer of Health should be informed so that the information can be relayed to local physicians.

Hardness

The water is considered to be unacceptable for most domestic purposes, according to the information provided in the ODWSOG. Water with hardness above 80 to 100 milligrams per litre as CaC0₃ is often softened for domestic use. The hardness at the well was 530 milligrams per litre. According to MECP D-5-5, the ODWO is 500 mg/l and there is no maximum concentration considered reasonably treatable (MCCRT) for hardness. Water softening by conventional sodium ion exchange may introduce relatively high concentrations of sodium into the drinking water, which may contribute a significant percentage to the daily sodium intake for a consumer on a sodium restricted diet. Due to the excessive hardness, it is expected that sodium will be elevated in the treated water. Where ion exchange water softeners are used, a separate unsoftened water supply should be used for drinking and culinary purposes.

Total Dissolved Solids

Total dissolved solids (TDS) level was 625 milligrams per litre and is above the ODWS aesthetic objective (AO) of 500 milligrams per litre. Where TDS levels exceed the AO, comments regarding treatment include "written rationale that corrosion, encrustation or taste problems will not occur", according to the MECP D-5-5 Guideline. The Technical Support Document for Ontario Drinking-Water Quality Standards, Objectives and Guidelines, states the following with regards to TDS.

"The term total dissolved solids refer to inorganic substances dissolved in water. The principal constituents of TDS are chloride, sulphates, calcium, magnesium and bicarbonates. The effects of TDS on drinking water quality depend on the levels of the individual components. Excessive hardness, taste, mineral deposition or corrosion are common properties of highly mineralized water. The palatability of drinking water with a TDS level less than 500 mg/L is generally considered to be good."

To provide the required rationale regarding the TDS level of 625 mg/L measured at the well, the Ryznar Stability Index (RSI) and Langelier Saturation Index (LSI) were calculated for the water sample to determine the corrosivity or scale formation potential of the water. The RSI value is 6.59, and LSI is 0.39, respectively, indicating that the water has little scale potential and is not expected to be corrosive. In this case, the other constituents that contribute to TDS, including sodium, sulphates and chlorides are all well within their aesthetic objectives. The aesthetic objectives are established for sodium and chlorides based on water palatability. A sodium level of 20 mg/L and a chloride level of 63 mg/L are well within the aesthetic objectives of 200 mg/L and 250 mg/L, respectively. As such, they are not present at sufficient levels to contribute to taste. Sulphates are also present at a level of 131 mg/L. Sulphate at less than 150 mg/L does not result in noticeable taste, as stated in the Technical Support Document. TDS is also contributed to by calcium, magnesium and bicarbonates. These are the components of TDS that also cause high hardness. Consequently, the way to reduce the TDS levels is to improve excessive hardness through the reduction of hardness. The Technical Support document states that hard water has a tendency to form scale deposits and can cause scum with soap. It does not state taste issues in association with high levels of hardness. Therefore, it is considered that treatment to reduce hardness will also reduce the potential for scale formation associated with TDS.

Manganese

Manganese has an aesthetic objective (AO) of 0.05 mg/L and was measured at 0.06 mg/L at the well. The colour related AO for manganese is due to black staining or discolouration of laundry and fixtures and at excessive concentration causes undesirable taste in beverages. At the level that is



present at the well, it is only slightly above the AO and as such is less likely to cause taste issues than if manganese level were excessively high. Manganese can be effectively removed using a water softener or manganese greensand filter at levels of up to 5.0 mg/L.

Total Coliforms

The water sample obtained on May 19, 2022, had total coliforms of 4 counts/100 ml with E. Coli absent.

MECP Procedure D-5-5 states the following with regards to total coliforms:

While the stated ODWS for Total Coliforms is 0 counts per 100 ml of sample, it is recognized that the objective had been set as an indicator of inadequate disinfection within the distribution systems associated with water works. For private water wells not subject to approval under the OWRA, the MOEE and Health Units have historically used the limit of <5 counts per 100 ml in the absence of a chlorine residual as indicating acceptable water quality.

Based on the above noted information, it is considered that the total coliform level is acceptable.

Trace Metals

The results of the trace metals testing indicates that, where present, all trace metals are indicated to be within allowable limits. The strontium level is of particular concern in the Ottawa area, due to its association as naturally occurring in some sedimentary bedrock, such as limestone and sandstone. Strontium currently has a proposed Maximum Acceptable Concentration (MAC) by Health Canada of 7.0 mg/L. The level of strontium measured in the water supply at this site is 0.143 mg/L, which is well within the acceptable limit. There are no concerns with any of the trace metals concentrations in the water supply at the site.

Groundwater Impact Assessment

The Ministry of the Environment, Conservation and Parks (MECP) in the MOE Procedure D-5-4 provides guidelines for evaluating "the ability of the lands identified by and restricted to the development to treat sewage effluent to meet acceptable limits". The guideline requires that the representative background nitrate levels in the receiving groundwater be determined. Where background levels are greater than 10 milligrams per litre the ministry indicates development of the site should not be supported unless it can be demonstrated that existing levels of nitrates are the results of historical agricultural practices on the site. In addition, the guideline requires demonstration that the site is not obviously hydrogeologically sensitive such as karstic areas, areas of fractured bedrock exposed at the surface, areas of thin soil cover or areas of highly permeable soils.

The guideline indicates that the assessment involves a three step process.

Step 1 regards lot size considerations. Where the lot size for each private residence within the development is an average of one hectare or larger and no lot is smaller than 0.8 hectares, and provided the site is not hydrogeologically sensitive, the risk that impact limits may be exceeded by individual systems is considered acceptable.

Step 2 is in regards to septic system isolation considerations. Developments are considered low risk when it can be demonstrated that sewage effluent is hydrogeologically isolated from existing or potential supply aquifers. For this case the most probable groundwater receiver for sewage is to be defined through information obtained through a test pit or test hole program, and the most probable

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lower hydraulic or physical boundary of the groundwater receiving sewage effluent is to be defined. The guideline indicates hydrogeological information concerning lands up to 500 metres beyond the actual development boundary may be required. When it can be demonstrated that the sewage will not enter supply aquifers the lot density of the proposed development is determined based on the space required to install a suitable septic system at each lot in accordance with the Ontario Building Code.

Step 3 is in regards to contaminant attenuation considerations. For this case, it is required to assess the risk that the on-site sewage systems within the proposed development will cause a concentration of nitrate in groundwater above 10 milligrams per litre at the down gradient boundary of the site.

The existing residential lot occupies an area of about 1.7 acres (0.67 hectares). A test pit put down in the proposed sewage system area for the coach house encountered about 0.40 metres of topsoil over 0.40 metres of glacial till. Surficial geology maps, combined with the well record for the site indicate that the soil thickness is about 4.6 to 9.0 metres in thickness, and is identified as some combination of sand, gravel, boulders, clay. This is generally consistent with glacial till. The City of Ottawa considers any site with less than 2.0 metres of soil cover to be potentially hydrogeologically sensitive. As such, the site is not considered to be potentially hydrogeologically sensitive. Due to the lot size being less than 1.0 hectares, the consideration of sewage concentrations down gradient of the site is also considered.

To obtain a general indication as to the potential impact of septic effluent on the properties adjoining the proposed development, a nitrate dilution model was used. A daily effluent loading of 1000 litres per day per septic system was assumed and the total expected impact of septic systems at this site was determined by considering the attenuation of nitrate in the effluent from each of the sewage systems at the site. The existing (main) dwelling has a tertiary treatment system that does not rely on denitrification and is not tested for denitrification (Clearstream). The impact from that system is considered to be from an assumed 40 milligrams per litre (mg/l) (NO₃ as N), after the septic system treatment to the property boundary by dilution as a result of the infiltration of meteoric water only. The proposed sewage system to service the coach house is designed for nitrogen reduction using a Waterloo Biofilter WaterNO_x-LS. The information and third party testing for this type of system is provided (Attachment F). Based on the information provided, the total nitrogen reduction that can be achieved with this type of system is some 80% to 90% removal. As such, the treated effluent from the proposed coach house sewage system is expected have a Total Nitrogen concentration of some 8 mg/L as N or less. This is due to the treatment level. The following discusses the resulting dilution of the treated effluent due to infiltration and consideration of meteoric water and the site area and other factors.

The following provides the basis whereby the infiltration reduction factors for the site were chosen for the dilution calculations.

Topographic, soil and land cover infiltration factors were selected from *Table 2* of the MOE *Hydrological Technical Information Requirements for Land Development Applications*. The following is a discussion of each of the infiltration reduction factors chosen for the site.

The site and surrounding area is characterized by flat terrain with a slope infiltration factor of 0.30.

The type of land cover observed at the site at the time of site visits using the topographical survey and by use of satellite imagery consists of cultivated lands, with mature trees on the edges and in the rear yard of the property. It is expected that the post-development conditions at the site will

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include treed areas over about 30% of the site. The land cover infiltration factor of 0.13 was selected, which corresponds to a mixture of cultivated lands and woodland.

In order to determine water surplus estimates for the site area, a water surplus model was obtained using published information from Environment Canada (EC) for the City of Ottawa. The water balance model output the average yearly moisture surplus value, based on monthly moisture surplus averages for the period from 1993 to 2002. The expected moisture surplus or net potential infiltration for the site area was estimated 328 millimetres, which corresponds to glacial till.

Hard Surfaced Area post-development was calculated as follows. The roofs of the two dwellings cover about 403 square metres. The driveway and other paved areas cover an area of about 709 square metres. The total hard surfaced areas were considered to be 1111 square metres. The resulting Net Infiltration Area is some ~5639 square metres.

In order to determine the impact from the two sewage systems, which have different concentrations in the treated effluent, the impact from each sewage system was considered to occur over half the lot area. Then the combined impact of two sewage systems over the site considering the concentration from each system and the volume of effluent from each system were calculated to determine the final concentration of sewage effluent that can be expected from the combined sewage effluent at the down gradient property boundaries. The existing sewage system, when considering dilution by meteoric water only over half the available lot area is some 15.4 mg/L N-NO₃. The coach house sewage system will contribute an estimated additional input of some 3.1 N-NO₃. Each system is considered to discharge some 1,000 litres of sewage effluent daily for a combined sewage input of 2,000 litres daily. The resulting concentration, based on the combined systems is expected to be 9.2 mg/L N-NO₃.

The results of the sewage dilution calculations indicate that the expected concentration of nitrate at the down gradient property boundaries from the combined sewage effluent is expected to be about 9.2 mg/L N-NO₃. This is within the Ministry of the Environment acceptable nitrate impact limit of 10 milligrams per litre.

Based on the predictive impact assessment and consideration of a tertiary sewage system capable of nitrogen reduction of at least 80% for the proposed coach house, the two private sewage disposal systems are not expected to have an adverse impact on groundwater resources in the site area.

Results and Recommendations

The following is for consideration for water treatment for the proposed coach house:

Hardness

• The water is considered to be excessively hard by water treatment standards. Water with hardness above 80 to 100 milligrams per litre as CaC0₃ is often softened for domestic use. The hardness at the well is 530 milligrams per litre. This level of hardness is "considered to be unacceptable for most domestic purposes". The treatment to reduce hardness is the use of ion exchange water softeners. Where water hardness is excessive, the water softener can introduce even higher sodium concentrations in the water than for water that is not excessively hard (i.e. hardness of less than 200 mg/L). Of concern, is that the water softener treated water may have sodium levels that exceed the aesthetic objective for sodium in the treated drinking water, which may contribute a significant percentage to the daily sodium intake for a consumer on a sodium restricted diet and increase the corrosive

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potential of the treated water. Sodium treated water may be more corrosive to plumbing fixtures and water pipes. Copper concentrations can increase in the treated water due to dissolution of metals in copper water supply pipes. In order to achieve an acceptable balance between reducing incrustation (scale) and corrosive potential, the following options for water treatment should be considered:

- Consider using an ion exchange water softener on the hot water only. This will reduce the scale in the dishwasher and hot water tank (as scale tends to form with heated water) but allow for water that is consumed (cold water faucets) to not have excessive sodium levels. This option would reduce the use and consumption of salt and provide an acceptable balance between incrustation and corrosion in the water supply pipes, fittings and fixtures;
- If the whole water supply is treated using a water softener using sodium chloride salts, consider a bypass for the kitchen for cooking and drinking purposes or a point-of-use reverse osmosis system in the kitchen;
- Consider the use of plastic (PEX) water supply pipes which do not corrode.

Sodium

- The sodium level in the untreated water supply is 20 mg/L, which is at the 20 mg/L medical advisory limit but well within the aesthetic objective of 200 mg/L. When sodium levels exceed 20 mg/L, the local Medical Officer of Health should be informed so that the information can be relayed to local physicians.
- See comments above on elevated sodium in treated water due to hardness.

Total Dissolved Solids

• The total dissolved solids were present at 625 milligrams per litre, exceeding the aesthetic objective of 500 mg/l. The elevated TDS is due to high hardness, which contributes calcium, magnesium and bicarbonates to the TDS levels. The elevated TDS and hardness are reduced through the water softening which will reduce potential for scale formation.

Manganese

• Manganese has an aesthetic objective (AO) of 0.05 mg/L and was measured at 0.06 mg/L at the well. The colour related AO for manganese is due to black staining or discolouration of laundry and fixtures and at excessive concentration causes undesirable taste in beverages. At the level that is present at the well, it is only slightly above the AO and as such is less likely to cause taste issues than if manganese level were excessively high. Manganese can be effectively removed using a water softener or manganese greensand filter at levels of up to 5.0 mg/L.

The following is required for the proposed sewage system to service the coach house:

 Based on the above noted site conditions and consideration of a minimum of 80% nitrogen reduction for the coach house sewage system, Kollaard Associates Inc. considers that the groundwater impact of the proposed development is within the impact limits established by the MECP and the water supply is adequate to provide for the existing dwelling and the proposed coach house. We trust this letter provides sufficient information for your purposes. If you have any questions concerning this letter, please do not hesitate to contact our office.

Yours truly,

Kollaard Associates Inc.



Colleen Vermeersch, P. Eng.

Attachments: Table I Summary of Hourly Field Water Quality

Figure 1 Key Plan

Attachment A Proposed Sewage System Design

Attachment B TW1-Well Record for Site and Area Wells

Attachment C TW1-Pumping Test Data

Attachment D TW1-Laboratory Water Testing Results
Attachment E Sewage Attenuation Calculations

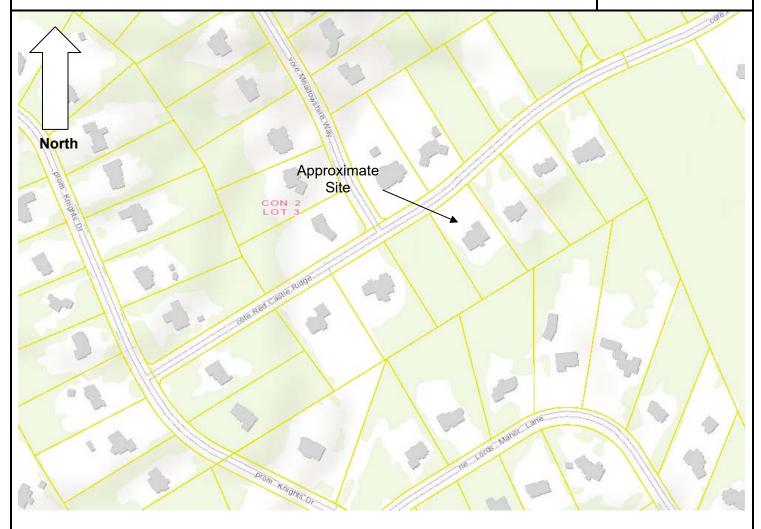
Attachment F Waterloo Biofilter WaterNOx-LS Third Party Testing Summary

May 19, 2022 220067

TABLE I
FIELD WATER QUALITY MEASUREMENTS
FOR TEST WELL 1

Time Since Pumping Test Started (min)	Temperature (°C)	рН	Turbidity (NTU)	Total Dissolved Solids (ppm)	Conductivity (μS)	Free Chlorine (ppm)
60	11.0	7.54	4.74	529	1061	0.00
120	11.0	7.43	1.76	515	1029	-
180	10.7	7.50	0.68	521	1045	0.00
240	10.9	7.47	0.61	521	1037	-
300	10.7	7.49	0.62	518	1034	-
360	10.7	7.46	0.52	514	1029	0.00

KEY PLAN FIGURE 1



NOT TO SCALE

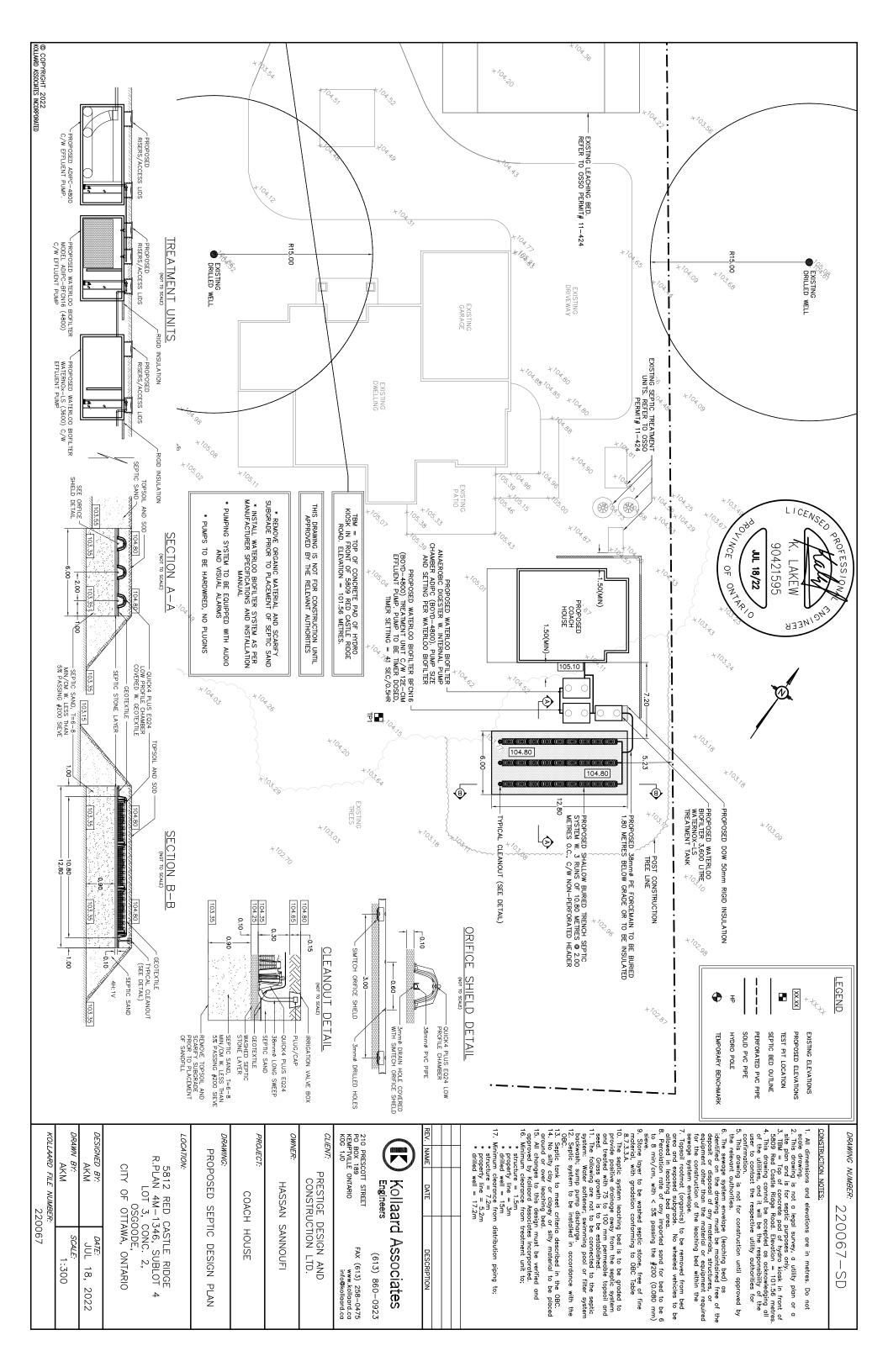


Project No. 220067

Date June 2022

ATTACHMENT A

SEWAGE SYSTEM DESIGN FOR COACH HOUSE





ATTACHMENT B

MECP WELL RECORD AND CERTIFICATE OF COMPLIANCE FOR TEST WELL AND AREA WELL RECORDS



CERTIFICATE OF WELL COMPLIANCE

	In,	Ken Desaulniers . DO HEREBY CERTIFY that I am licensed to drill
		wells in the Province of Ontario, and that I have supervised the drilling of a well on the
		PROPERTY BRENMAR CONSTRUCTION
		located at 5812 Red Castle Riche
	0	LoVPlan No.) in the City of Ottawa (Geographical Township of Osgoode).
		15-74 CONC 2 PLAN# 4M-13465/1 # A
		CERTIFY FURTHER that, I am aware of the well drilling requirements, the guidelines,
		recommendations and regulations of the Ministry of the Environment governing well
		installations in the Province of Ontario, and the standards specified in any subdivision
		agreement and hydrogeological report applicable to this site and City Standards.
		The same and the same and the standards.
		AND DO HEREBY CERTIFY THAT the said well has been drilled, eased, grouted
		(cement or bentomite) as applicable and constructed in strict conformity with the
		standards required.
		fi
		Signed this A day of NOVEMBER 2011
		Well Driller/Company Well Driller/Company
		The Engineer on behalf of the landowner set out above Certifies that he/she has inspected
	,	eport and the Hydrogeological Report with records to see O. Reg. 903, this
	1	equirements.
	(IGNED this 28 day of Marcalland
		ACUADO NOVEMBER, 2011
	E	ngineer P. Eng.
	Lud	Nov. 28/11 # 2011 727
		oule Chevrier Engineering Ltd. A.C. HOTHE & J. C. HOTHE
Shapin	g our futu Ensen	re together while, formons notre avenir
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11 11	3(0	CHERT VOTUS CENTRE CENTRE de Service 2001 FOUX 83 8 37 Forgans ON KOA 190 OTIGNA, ON KOA 200 OTIGNA, ON KOA 200 OTIGNA, ON KOA 200 OTIGNA, ON KOA 200 OTIGNA, ON KOA 200

Ministry of the Environment Well Tag No. (Place Sticker and/or Print Below)

Well Record

Regulation 903 Ontario Water Resources Act A 051510 A051510 Page Well Owner's Information 5820 Red Castle Way (lot 6) Osgoode County/District/Municipality City/Town/Village Postal Code Province Ontario Ottawa Carleton Manotick JTM Coordinates Zone , Easting GPS Unit Make Mode of Operation: Undifferentiated X Averaged Model NAD | 8 | 3 | 18 4 | 5 | 0 | 4 | 6 | 25 | 00 9 8 | 7 | 8 Differentiated, specify Garmin Overburden and Bedrock Materials (see ins ructions on the back of this form) Depth (Metres) rom To General Colour Other Materials Most Common Material General Description 0 6.09 Brown Sandy Clay Boulders Gray Till Packed 6.09 9.14 9.14 83.20 Limestone Sandstone LAyers Grav Results of Well Yield Testing Annular Space/Abandonment Sealing Record Check box if after test of well yield, Recovery Depth Set at (Matres) Type of Sealant Used Volume Placed Draw Down To (Material and Type) (Cubic Metres) From Water Level Water Level Clear and sand free (Metres) Cannot develop to sand-free 13.10 0 Grouted - Bentonite Slurry .92m3 Statio 9.28 If pumping discontinued, give reason 1 16.38 11.14 Pumping test method 12.37 14.55 submersible 13.35 13.03 Pump intake set at (Metres) Method of Construction Water Use 4 4 Cable Tool Diamond Public Commercial Not used 14.01 11.92 Pumping rate (Litres/min) Rotary (Conventional) Municipal Dewatering Jetting **☒** Domestic 5 17.54 Test Hole ☐ Monitoring 11.11 Rotary (Reverse) Driving Livestock 54.6 Duration of pumping Rotary (Air) Mud Digging Irrigation Cooling & Air Conditioning 10 10 16.53 9.74 Air percussion Boring Industrial 1 hrs + 30 min inal water level end of pumping 15 15 Other, specify Other, specify 17.54 9.47 (Metres) 19.28 Status of Well 20 20 18.01 9.32 Water Supply Dewatering Well Observation and/or Monitoring Hole Recommended pump type Replacement Well Abandoned, Insufficient Supply Alteration (Construction) 25 25 Shallow Deep 18.38 9.28 Test Hole Abandoned, Poor Water Quality Other, specify Recommended pump depth 30 Recharge Well Abandoned, other, specify 30 18.63 24.38 Metres Location of Well 40 40 ecommended pump rate itres/min) 18.89 Please provide a map below showing: all property boundaries, and measurements sufficient to locate the well in relation to fixed points,
 an arrow indicating the North direction 50 50 If flowing give rate (Litres/min) 19.06 detailed drawings can be provided as attachments no larger than legal size (8.5" by 14") vidigital pictures of inside of well can also be provided 60 60 19.10 Water Details Water found at Depth 64 | Metres Gas Water found at Depth Fresh Salty Sulphur Minerals 出5820 Kind of Water NOT TESTED Fresh Salty Sulphur Minerals 81.07 Metres Gas Water found at Depth Kind of Water Fresh Salty Sulphur Minerals Metres Gas Casing and Well Details Casing Used Screen Used Diameter of the Hole (Centimetres) Galvanized Galvanized 15.23 Depth of the Hole (Metres) X Steel Steel Fibreglass Fibreglass Plastic Was the well owner's information package delivered?

Yes □ No Date the Well Record and Package Delivered to Well Owner (yyyy/mm/dd) Plastic Date Well Completed (vvvv/mm/dd) Concrete Concrete 2008/5/13 <u> 2008/5/12</u> No Casing and Screen Used Well Contractor and Well Technician Information Open Hole Business Name of Well Contractor Well Contractor's Licence No 15.86 isinfected? Depth of the Casing (Metres) Capital Water Supply Ltd.
Business Address (Street No./Name, number, RR) 5 5 8 1 Yes No Municipality + 45 to 13.10 Box 490 Ministry Use Only Stittsville Audit No. 2 77353 Business E-mail Address Postal Code Well Contractor No. K 2S 1 A6 office capitalwater.ca Date Received (yyyy/mm/dd) Date of Inspection (yyyy/mm/dd) 6 13 8 3 6 1 7 66 JUN 0 2 2008 Miller; Stephen Date Submitted (yyyy/mm/dd) 0 2008/05/16 0 9 7

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nt Below)

Well Record

Regulation 903 Ontario Water Resources Act

Well Loc	ation	on (Street Number/Na	me)	1	ownship	<u> </u>	Lot	w/N T	Concession	<u>i i T</u>	
115	1 Mead	owshire Way			Osgoode		P/L 2		4 2	,	
-	strict/Municip				City/Town/Village			Provir Ont		Postal	Code
	awa-Ca inates Zone	1	Northing		Greeky Junicipal Plan and Subl	ot Number		Other		11	
		8 450199 Irock Materials/Aba	5009		AM-1346 ord (see instructions on the	back of this form)		LSA	_13		
General C		Most Common Mate	1	***************************************	ner Materials	1	al Description	1		Dep From	th (<i>n(xt)</i>)
Grey			3 y 2000-000	owner or a contract	어 Gravel	e Company	are making a gari	Sec. Vier	emocial established	0 4	15
Grey &		ing the second of the second s	nestone							15	53 (
Grey 6	& Brown	Lin	nestone	egisting is else.				<u> </u>		<u>53 ´</u>	158
*****	& White	Sa	ndstone							158	233
Grey &	& White	estas gravas Sa	ndstone							233 '	240′
		Ann	ular Space			R	esults of W		d Testing		
Depth Se	et at (n@#D	Type of	Sealant Used	1	Volume Placed	After test of well yield, w	ater was:	Dr	aw Down		ecovery
40	0'	Neat cement	al and Type)	z i mere er	21.8	☐ Clear and sand fre ☐ Other, <i>specify</i>	e lot teste :	(min)	Water Level (m/ft)	Time (min)	Water Level (m/ft)
				<u></u>		If pumping discontinued	l, give reason:	Static Level	18.5		70.8
				***************************************				1	28.9	1	55.7
						Pump intake set at (mt	(4)	2	37.4	2	50.5
Meti	hod of Cor	estruction		Well Us	e	Pumping rate (I/min /	EM)	3	42.6	3	46
Cable To	ool	Diamond	Public	Comme	rcial Not used	15 Duration of pumping		4	47.5	4	43.1
Rotary (F	Conventional) Reverse)	☐ Driving	Domestic Livestock	☐ Municip ☐ Test Ho		hrs+m	in .	. 5 .	52	5	40.8
☐ Boring Air percu	ussion		lrrigation Industrial	Cooling	& Air Conditioning	Final water level end of	pumping (m/ft)	10	··· 69.6	.10	31.3
Other, s	pecify		Other, specif	ý		70.8 If flowing give rate (I/m	in / GPM)	15	70.1	15	26.4
Inside	Open Hole	struction Record -	·	pth (<i>m/ft)</i>	Status of Well	Recommended pump	depth (m/ft)	20	70.5	20	23.7
Diameter <i>(cm/in)</i>	(Galvanize	d, Fibreglass, Thickner Plastic, Steel) (cm/in		То	Replacement Well	200	r of tradition to the specimen	25	70.8	25	22.1
ธ์"	Steel	188	« +2	40-	Recharge Well	Recommended pump	rate	30	70.8	30	21.1
51516		Control of Control of the Control of Control	Prince out to the second		Dewatering Well Observation and/or	15 Well production (I/min0)	(GPM)	40	70.8	40	20.3
			31.33.	300	Monitoring Hole Alteration	15 Disinfected?		. ,50	70.8	50	19.6
					(Construction) Abandoned,	Districted? Zes No		60	70.8	60	19.1
	Co	onstruction Record - S	Screen		Insufficient Supply Abandoned, Poor		Map of W				
Outside Diameter <i>(cm/in)</i>		sterial vanized, Steel) Slot N	o. From	pth (<i>m/ft)</i> To	Water Quality Abandoned, other, specify	Please provide a map b	elow following	instruct	ions on the b	ack.	
			45		Other, specify						
										51	soul Soul
Water foun	nd at Depth	Water Details Kind of Water: ☐ Free	sh Juntest	**********	th (m/ft) Diameter			•	/# (1	and the	ones,
53 (m	n∰ ∏ Gas	Other, specify	A Section	From	To (cm/in)		2	0	≥/. h	V	Son
خذيبيون بالعال الرابى براب	化间流液流流流流流 医毒毒性 🏖	Kind of Water: Free	sh Wuntest	ed C	ا ما		DK	4			
Water foun	nd at Depth	Kind of Water: Free	sh Untest	40	240 5 15/16"		P 8	0'	(
	····	II Contractor and W	/ell Technic		tion Il Contractor's Licence No.	-0	J Cas	<u>z+1</u>	e Ria	A	e
Business A		g Co. Ltd. et Number/Name) n Road, RR#1			1119 Inicipality Richmond	Comments:		·····		: *	
Province		•	ness E-mail A					·			
ON Bus Telepho	- E	KOA 2ZD name of W		ck@sympa		information	ckage Delivere	ed	Minist Audit No.	ry Use	Only
613838 Well Technic	32170 cian's Licence	F 1 1			te Submitted	Date Wo	ork Completed		z 1	28 R 29	486 2012
T348	4	Kons	0	Y		No Y	112 03	ୀତି	Received	ıtas U	

Tag#: A135433 Print Below) Well Record Ministry of the Environment Regulation 903 Ontario Water Resources Act A135433 ☐ Metric M Imperial Page of easurements recorded in: **Well Owner's Information** Last Name. / Organization Princiotta Custom Built Homes First Name E-mail Address by Well Owner Mailing Address (Street Number/Name) Municipality Province Postal Code Telephone No. (inc. area code) 1491 Manotick Station Road Greely ON K4P 1P6 Well Location Concession Address of Well Location (Street Number/Name) Township P/L 2,34 5809 Red Castle Ridge Osgoode County/District/Municipality City/Town/Village Postal Code Ottawa-Carleton Greely Ontario UTM Coordinates Zone Easting Northing Municipal Plan and Sublot Number Other NAD | 8 | 3 | 18 | 452027 4M-1346 5009859 S/L 12 Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form) Depth (m/ft) General Colour Most Common Material Other Materials General Description From 0 (Sand & Gravel Boulders 17 / 4 137 ′ Grey Limestone 17 Grey & White Sandstone 172 137 Grey Limestone 172 180 Grey Limestone 180 186 Results of Well Yield Testing **Annular Space** Depth Set at (m/t) Type of Sealant Used After test of well yield, water was: Volume Placed Draw Down Recovery From To (Material and Type) (mVII) ☐ Clear and sand free ime Water Level Time Water Level (min) 40 30 (m/ft) Neat cement 10.9 Other, specify Not tested (m/ft) 109.3′′ Statio If pumping discontinued, give reason: 19.3 30 Bentonite slurry 16.8 Level 27.4 88.1 1 1 Pump intake set at (m/t) 313 817 2 2 160 39.4 74.8 3 3 Pumping rate (I/min (GPM)) **Method of Construction** Well Use 20 4 47.6 62.4 Cable Tool ☐ Public 4 Diamond Commercial ☐ Not used Duration of pumping Jetting Rotary (Conventional) Dewatering Domestic Municipal 514 Rotary (Reverse) 1 hrs + 0 min 5 5 53.4 Driving ☐ Monitoring Livestock Test Hole Borina Final water level end of pumping (m/ft) ☐ Digging Irrigation Cooling & Air Conditioning 10 61.8 10 33.8 Air percussion
Other, specify 109.3 " Industrial Other, specify 15 72.4 15 21.7 If flowing give rate (I/min / GPM) **Construction Record - Casing** Status of Well 82.5 193 Recommended pump depth (mtt)

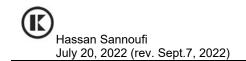
100 (3/4 HF)

Recommended pump rate (l/min / SPM)

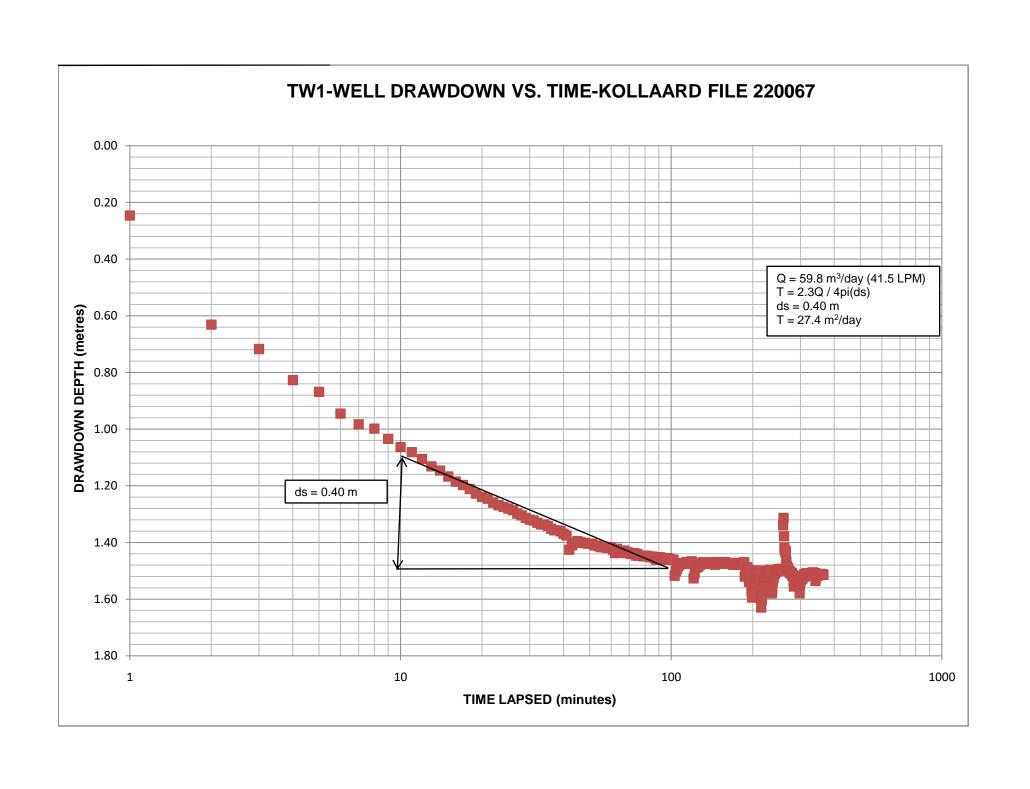
20 20 20 Depth (m(ft)) Inside Open Hole OR Material Wall Water Supply Thicknes (Galvanized, Fibreglass, Concrete, Plastic, Steel) Replacement Well 25 93.4 25 19.3 То From (cm(n) Test Hole .188' Recharge Well 30 98.6 30 19.3 Steel +2 40 ☐ Dewatering Well 103.4 Open Hole 40 103 40 186 40 Observation and/or Well production (I/min AGPM) Monitoring Hole 20 50 106.7 19.3 Alteration 50 Disinfected? (Construction) 109.3 19.3 60 Abandoned, Insufficient Supply Yes No Construction Record - Screen Map of Well Location Abandoned, Poor Outside Water Quality Please provide a map below following instructions on the back Depth (m/ft) Material Diamete Slot No (Plastic, Galvanized, Steel) Abandoned, other, From (cm/in) specify Other, specify Water Details Hole Diameter Untested Water found at Depth Kind of Water: Fresh Depth (m/ft) From 180 (mft) Gas Other, specify #5809 Red Castle Ridge 40′ Water found at Depth Kind of Water: Fresh Untested 93/41 Π (m/ft) Gas Other, specify 40 186 Water found at Depth Kind of Water: Fresh Untested (m/ft) Gas Other, specify Well Contractor and Well Technician Information Business Name of Well Contractor Well Contractor's Licence No. Air Rock Drilling Co. Ltd 1119 Business Address (Street Number/Name)
6559 Franktown Road, RR#1 Municipality Richmond Comments: 3/4 HP - 15 GPM SET @ 100 FT Postal Code Business E-mail Address KOA 2ZO ON air-rock@sympatico.ca Well owner's Date Package Delivered Ministry Use Only information Bus.Telephone No. (inc. area code) Name of Well Technician (Last Name, First Name) Audit No. nackage 2013 6402 z 155057 6|13|83|82|70 Purcell, Shannon delivered Well Technician's Licence No. Signature of Technician and/or Contractor Date-supposited 4 Work Completed Yes 03 26 30 2013 Νo 0506E (2007/12) © Queen's Printer for Ontario, 2007 Ministry's Copy

Ontari Measurements rec	the Elly	ironment	nperial	N T	ag#: A1869 A186929	29 (Below)	Regulation	903 Ontario		Record esources Act
Well Owner's In										
First Name	La	st Name / O J oh	rganizatio n Ger i	ard Ho	mes	E-mail Address			,	II Constructed Well Owner
Mailing Address (Str PO Box 4	reet Number/Name	e)			Municipality Greely	Province On	Postal Code K4N 1		ne No. (ir	nc. area code)
Well Location Address of Well Loc 5813 Re	ation (Street Num d Castle Ric	ber/Name) ige			Township Osqoode		Lot P/L 2	Conces ,344 2		
County/District/Mun	icipality				City/Town/Village			Province		tal Code
Ottawa-C		Nor	thing	7.0	Greely Municipal Plan and Sub	lot Number		Ontario Other	ary continued to	
NAD 8 3	18 45034	1	50098	882	4M-1346	ior identifica		S/L 11		
***************************************		······································	ment Se		ord (see instructions on th	1				epth (na/fi)
General Colour	Most Commo	******************************			ther Materials Sand	Gene	eral Description		From	19 7
Grey		Clay Limest	nne	d -	Jailu	e de la constante de la consta	*	. · · · · · · · · · · · · · · · · · · ·	19	132
Grey		Limest		- B	Sand _s	reasonage and the second secon			132	
Grey		Limest			CVAN Sands	}			178	
Grey		Limest			COUN Sands			***************************************	185	
Grey	A THE STATE OF THE	Limest	one		Sand S	12002			188	195
				1 14-71		**************************************	\$\$\$\$\$\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	,		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
			100							and the second s
Constitution of the Consti						de la constante de la constant				Control of the Contro
***************************************		Annular S	pace				Results of Wel	l Yield Testi	na	
Depth Set at (m @ From To	The state of the s	ype of Seala Material and	int Used		Volume Placed (m∰)	After test of well yield,	water was:	Draw Dow	*******	Recovery Water Level
40 / 30 /	Neat cer		- YPG	visioni visioni visita ivim bili	E.36	Other, specify	Not tested	(min) (m/f) (min) (m/ft)
30 0 7	Bentonit	e slurry			16.8	If pumping discontinue	ea: aive reason: u	Level	25 , 3"	114.97
		and a familiary as a standard or a sample is a destinate of a familiary	inidanin'i winamana Araba	vinciam (radahan mbartaini dan		\parallel $ imes$		1 34	.4 1	84
				vocamentes de la estada de la composição d	omda dan yan miran i washalin wa main turi vinamura Adelin ta Livalin wa midalo a 12 Adelina (Pump intake set at (i	(1)	2 39	1.5 2	75.6
Method of C				Well L	F = = -	Pumping rate (I/min (EDD.	3 43	3.7	69
Cable Tool	Diamond	, □ Publi	o erene erene	Comm	nercial	12		4 47	.4 4	61.8
☐ Rotary (Convention ☐ Rotary (Reverse)	nal) ☐ Jetting ☐ Driving	Dome		☐ Munic	The second state of the first term of the second of the	Duration of pumping 1 hrs + 0	min	5 50	7 5	53.6
□Boring	☐ Digging	☐ Irriga	tion		g & Air Conditioning	Final water level end o	of pumping (m/ft)	10 63	1.3 10	35
Air percussion Other, specify	iridar ooo daanaa rahiinka sa rahiinka	☐ Indus ☐ Other				114(9 1	min / GPMI	15 74	.9 15	25.3
	onstruction Rec	ord - Casir			Status of Well			20 82	. 6 20	25.3
Diameter (Galvan	lole OR Material ized, Fibreglass,	Wall Thickness	Depth From	r(n ⊘ I To	Water Supply Replacement Well	Recommended pump		₁₂₅ 89	1.3 25	25.3
- the commendation of the	e, Plastic, Šteel)	(cm @ .188"	+2	407	Test Hole		448-10-7PM	30 94		25.3
614	n Hole	. 100	40′	1957	Dewatering Mell	(Vmin / 95M)	-	4.5	11.8 40	25.3
6'/g" Oper	Trole		40	187	Observation and/or Monitoring Hole	Well production (I/mir	I/QEAP			25.3
					Alteration (Construction)	Disinfected?		00	4'9'60	
					Abandoned, Insufficient Supply	Yes No			60	20.3
Outrida	Construction Rec	ord - Screer		ı (<i>m\ft</i>)	Abandoned, Poor Water Quality	Please provide a map	Map of Well below following in		ne back.	Historiae actologae
	Material Salvanized, Steel)	Slot No.	From	То	Abandoned, other, specify	Control of the Contro	4.0			
					apassy	-				
					Other, specify			er/mon.		
A	Water Detai	İsaayaşa			Hole Diameter	Med outsing		(7)	· 1	
Water found at Dept	in the second of		Untested	De From	pth (<i>m/ft</i>) Diameter To (<i>cm/in</i>)		\	7	15	and the state of t
Waler found at Dept	s Other, <i>specif</i> h Kind of Water:		Untested		0' 40' 93/4"	4 3	1 iver	">\\/	2	3 SK
185 (mott □ Ga				4		1 5 %			200	810
Was ound at Dept	h Kind of Water: { s ::: Other, <i>specif</i>	······	Untested				15	XX		
	Vell Contractor a		chnicia	n Informa	ition		and the same of th	C^{R}	? -	BUSE
Business Name of We Air Rock Drill	ell Contractor		***************************************	W	ell Contractor's Licence No.		(SO		
Bus 6659 Addess (S)	<u> </u>		······································	M	u bno Kilesirian	Comments:				
	•					3/4 HP - 10 (GPM SET @	150 FT		
Province	Postal Code KOA 220	Business E	-mail Add air-roc	(@symp	patico.ca		ackage Delivered	Mir	nistry Us	se Only
Bus.Telephone No. (inc. 6138382170	area code) Name	e of Well Tec Hogan, I		ast Name	, First Name)	information package 2				1440
	e No. Signaturé of		77.1973	ntractor D:	ate S1546 ted 5 29	delivered Date W	/ork Completed			
	Ker	<u> </u>	2			No		' vee M	<u>lN 1 5</u>	2015
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Ontario	Ministry of the Environm and Climate Change	nent W . T	ag#: A 2291	136 Below)	Regulation	903 On	tario Wate	r Reso	
easurements record	ed in: Metric Mmpe	erial					Page		of
Vell Owner's Info									
irst Name	Last Name / Orga	inization Tar Constru	ation	E-mail Address					onstructed I Owner
lailing Address (Street			Municipality	Province	Postal Code	Te	elephone N	o. (inc. a	area code)
1341 -1 Cok			Greely	On	KAP 1	A1			220000000000000000000000000000000000000
Vell Location		100 000 000 000			1 -4		Concession		
ddress of Well Location 5816 Red C	n (Street Number/Name)		Township Osgoode		Lot P/L 2	, -	oncession Z		
county/District/Municipal			City/Town/Village		3 2 5 5 5	Provinc	e	Postal	Code
Ottawa-Car			Greely			Onta	rio		
ITM Coordinates Zone	1 -	-	Municipal Plan and Sublot	Number		Other	E		
NAD 8 3 18	3 450425 50 Irock Materials/Abandonm)09829	4M-1346	hack of this form)		S/L	<u>J</u>		
General Colour	Most Common Material	1	ther Materials		eral Description	#6411359/11050		Dept From	h (<i>m@b</i>)
	Sand	- d	Gravel) /	30 /
Con.	Limeston							30 ⁷	177′
Grey	Limeston							177 (181'
Grey	Sandstor							181	188 '
Grey =								189 /	193 /
Grey	Sandstor							183 '	200′
Grey	Sandstor	16						185	200
			orner						<u></u>
	Annular Sp	ace			Results of Wo	Chicago Company (1963)		200 - 190 -	
Depth Set at (mat) From To	Type of Sealan (Material and 7		Volume Placed (m³/€2)	After test of well yield			w Down Water Level		ecovery Water Level
From To 40 / 32 /	Nest cement	ype)	9.36	Other, specify		(min)	(m/ft)	(min)	(m/ft)
32' 0'	Bentonite slumy		16.8	If pumping discontinu	ıed, give reason:	Static Level	20:6		31!9"
32 0.				X		1	24.4	1	25.3
				Pump intake set at (r	m/m	2	25.5	2	24.6
				180		3	28.2	3	24.2
Method of Co	nstruction	Well L	Jse	Pumping rate (Vmin A	GEM)		28.7	4	23.7
Cable Tool	Diamond Public		=	Duration of pumping		4		-	
Rotary (Conventional Rotary (Reverse))			f hrs+		5	27.1	5	23.4
Boring	☐ Digging ☐ Irrigati		ng & Air Conditioning	Final water level end	of pumping (m/ft)	10	28.4	10	22.4
Air percussion Other, specify	Indust			If flowing give rate (Vi	(min / GPM)	15	29.2	15	21.3
Co	instruction Record - Casin	G.	Status of Well	×	,	20	29.8	20	20.8
	le OR Material Wall ed, Fibreglass, Thickness	Depth (m ©	Water Supply Replacement Well	Recommended pum	np depth (matt)	25	30.2	25	 20.6
	, Plastic, Steel) (cm@)	From To	Test Hole	100 (Recommended pur	n rate	╢	30.5		20.6
Ly Steel	.188	+2' 40'	Recharge Well	(I/min / GRIA) 20	ip rate	30		30	
6 /8" Open 1	Hole	40 200		Well production (Vmi	n/GPM)	40	31	40	20.5
0/8			Monitoring Hole	20		50	31.5	50	20.5
			(Construction) Abandoned,	Disinfected? Yes, No		60	S1.9	60	20.6 %
	onstruction Record - Scree		Insufficient Supply		Map of V	/ell Loc	ation		100 000 000 000 000
Or delide	Aaterial Classic	Depth (<i>m/ft</i>)	Abandoned, Poor Water Quality	Please provide a m				the bac	Κ.
	alvanized, Steel) Slot No	From To	Abandoned, other, specify	<u> </u>	# 4	58	16		
				Mezekowsking				LE	
			Other, specify	148	RED	, <u> </u>		=	-
	<u> </u>		Hole Diameter	1 20		+	(M	 	
Water found at Depth	Water Details Kind of Water: ☐ Fresh	Untested D	epth (<i>m/ft</i>) Diameter				<u>~</u>		
	olther, specify	From	-31.			>7	160	Ο,	
	A	Untested	401 974		1	^	W		
)	S Other, specify Kind of Water: Fresh	Untested	49 200 6/8	- 4	-0.2KM	<i>!</i> \	(<u>(</u> (<u>(</u> (<u>(</u> ()))		
	S Other, specify	Concolod	· · · · · · · · · · · · · · · · · · ·						
	Well Contractor and Well To	echnician Inform	nation						
Business Name of We			Well Contractor's Licence No	-					
Air Rock Drillin				Comments:					
Business Address (St	LESENTARIO EN LA		M## Cipalitynd	1 HP - 20 G	FM CPS SE	et @.	100 FT		
Province ON	Postal Code Business E KOA. 2ZU	E-mail Address air-rock @sym	nation ca						
				information	e Package Delive		Mini Audit No.	stry US	ie Only 76989
Bus.Telephone No. (inc.) 8/13/83/82/17/0	c. area code) Name of Well Tec Purcell,	chnician (Last Nan Shannon	не, гизтианте)	delivered		ાં		Com l	UJOJ
Well Technician's Licence	ce No. Signature of Technician			Yes Date	e Work Complete 2018 C 7 Y Y Y M M	0.6		SEP '	I 6 2018
	033		TYYY MMDC	No Y	Y Y Y M M	D D	Received		for Ontario, 2014
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ATTACHMENT C PUMPING TEST DATA



Kollaard File 220067

Rate 41.5 litres/minute

Kollaard File 220067	Pump R
DRAWDOWN DATA 1	ΓW1

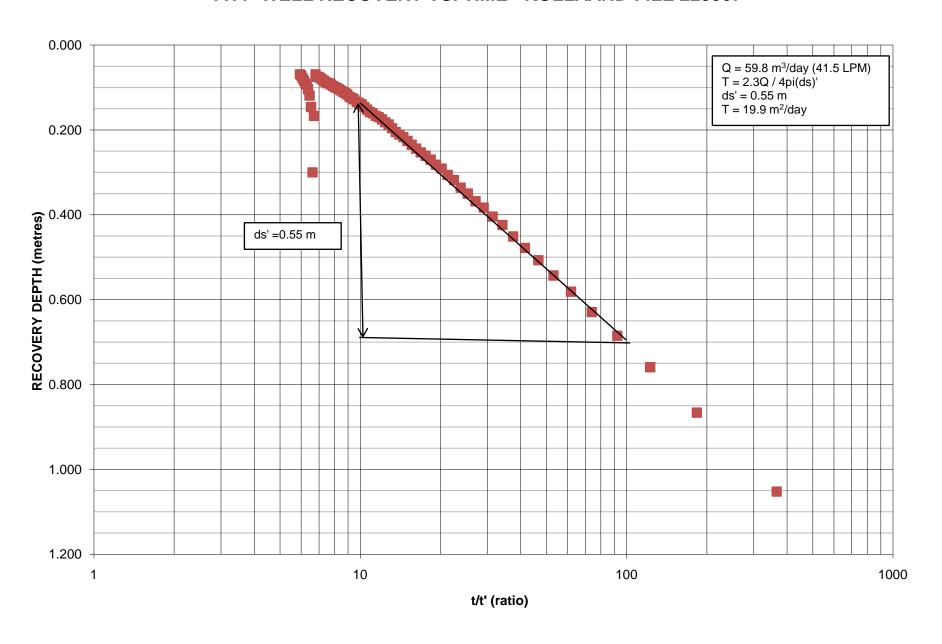
Time Lapsed (minutes) Abs Pres (kPa) Temp (c) Water Level (m) Drawdow (m) 0 348.345 9.275 -4.85 0.00 1 345.933 9.275 -5.096 0.25 2 342.156 9.275 -5.481 0.63 3 341.314 9.275 -5.567 0.72 4 340.239 9.275 -5.677 0.83 5 339.833 9.275 -5.718 0.87 6 339.078 9.275 -5.795 0.95 7 338.701 9.275 -5.833 0.98 8 338.207 9.275 -5.848 1.00 9 338.701 9.275 -5.848 1.03 10 337.917 9.275 -5.948 1.03 11 337.743 9.275 -5.931 1.08 12 337.511 9.275 -5.981 1.13 13 337.249 9.275 -5.981 1.13	
1 345.933 9.275 -5.096 0.25 2 342.156 9.275 -5.481 0.63 3 341.314 9.275 -5.567 0.72 4 340.239 9.275 -5.677 0.83 5 339.833 9.275 -5.718 0.87 6 339.078 9.275 -5.795 0.95 7 338.701 9.275 -5.833 0.98 8 338.207 9.275 -5.848 1.00 9 338.207 9.275 -5.848 1.03 10 337.917 9.275 -5.984 1.03 11 337.743 9.275 -5.931 1.08 12 337.511 9.275 -5.995 1.11 13 337.249 9.275 -5.995 1.11 14 337.104 9.275 -5.996 1.15 15 336.901 9.275 -6.037 1.21 16 336.727	
2 342.156 9.275 -5.481 0.63 3 341.314 9.275 -5.567 0.72 4 340.239 9.275 -5.677 0.83 5 339.833 9.275 -5.718 0.87 6 339.078 9.275 -5.795 0.95 7 338.701 9.275 -5.848 1.00 9 338.207 9.275 -5.848 1.03 10 337.917 9.275 -5.941 1.06 11 337.743 9.275 -5.951 1.06 12 337.511 9.275 -5.981 1.13 13 337.249 9.275 -5.981 1.13 14 337.104 9.275 -5.955 1.11 13 336.727 9.275 -6.035 1.19 17 36.611 9.275 -6.035 1.19 17 36.611 9.275 -6.047 1.20 18 336.466	
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52 334.515 9.176 -6.26 1.41	
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54 334.486 9.176 -6.263 1.41 55 334.457 9.176 -6.266 1.42	
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58 334.428 9.176 -6.269 1.42 59 334.457 9.176 -6.266 1.42	
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61 334.37 9.176 -6.275 1.43	
62 334.254 9.176 -6.287 1.44	
63 334.399 9.176 -6.272 1.42 64 334.283 9.176 -6.284 1.43	
65 334.341 9.176 -6.278 1.43	
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68 334.254 9.176 -6.287 1.44 69 334.283 9.176 -6.284 1.43	
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73 334.254 9.176 -6.287 1.44 74 334.167 9.176 -6.296 1.45	
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82 334.138 9.176 -6.299 1.45 83 334.138 9.176 -6.299 1.45	
83 334.138 9.176 -6.299 1.45 84 334.109 9.176 -6.302 1.45	
85 334.138 9.176 -6.299 1.45	
86 334.109 9.176 -6.302 1.45	

87	334.08	9.176	-6.305	1.46
88	334.022	9.176	-6.311	1.46
89	334.109	9.176	-6.302	1.45
90	334.08	9.176	-6.305	1.46
91	334.109	9.176	-6.302	1.45
92	334.051	9.176	-6.308	1.46
93	334.022		-6.311	1.46
		9.176		
94	334.022	9.176	-6.311	1.46
95	334.08	9.176	-6.305	1.46
96	334.051	9.176	-6.308	1.46
97	334.08	9.176	-6.305	1.46
98	334.022	9.176	-6.311	1.46
	334.051		-6.308	
99		9.176		1.46
100	334.022	9.176	-6.311	1.46
101	334.022	9.176	-6.311	1.46
102	334.022	9.176	-6.311	1.46
103	333.471	9.176	-6.367	1.52
104	333.616	9.176	-6.352	1.50
105	333.703	9.176	-6.343	1.49
106	333.79	9.176	-6.334	1.48
107	333.848	9.176	-6.328	1.48
108	333.877	9.176	-6.325	1.48
109	333.906	9.176	-6.322	1.47
110	333.877	9.176	-6.325	1.48
111	333.906	9.176	-6.322	1.47
112	333.906	9.176	-6.322	1.47
113	333.877	9.176	-6.325	1.48
114	333.935	9.176	-6.319	1.47
115	333.906	9.176	-6.322	1.47
116	333.906	9.176	-6.322	1.47
117	333.906	9.176	-6.322	1.47
				1.47
118	333.935	9.176	-6.319	
119	333.964	9.176	-6.316	1.47
120	333.906	9.176	-6.322	1.47
121	333.384	9.176	-6.376	1.53
122	333.558	9.176	-6.358	1.51
123	333.732	9.176	-6.34	1.49
124		9.176		
	333.761		-6.337	1.49
125	333.761	9.176	-6.337	1.49
126	333.79	9.176	-6.334	1.48
127	333.877	9.176	-6.325	1.48
128	333.848	9.176	-6.328	1.48
129	333.877	9.176	-6.325	1.48
130	333.877	9.176	-6.325	1.48
131	333.935	9.176	-6.319	1.47
132	333.906	9.176	-6.322	1.47
133	333.906	9.176	-6.322	1.47
134	333.906	9.176	-6.322	1.47
135	333.906	9.176	-6.322	1.47
136	333.906	9.176	-6.322	1.47
137	333.906	9.176	-6.322	1.47
138	333.877	9.176	-6.325	1.48
139	333.906	9.176	-6.322	1.47
140	333.906	9.176	-6.322	1.47
141	333.906	9.176	-6.322	1.47
142	333.906	9.176	-6.322	1.47
143	333.935	9.176	-6.319	1.47
144	333.935	9.176	-6.319	1.47
145	333.848	9.176	-6.328	1.48
146	333.906	9.176	-6.322	1.47
147	333.906	9.176	-6.322	1.47
148				
	333.906	9.176	-6.322	1.47
149	333.906	9.176	-6.322	1.47
150	333.906	9.176	-6.322	1.47
151	333.906	9.176	-6.322	1.47
152	333.935	9.176	-6.319	1.47
153	333.906	9.176	-6.322	1.47
154	333.877	9.176	-6.325	1.48
155	333.877	9.176	-6.325	1.48
	333.935		-6.319	1.47
156		9.176		
157	333.906	9.176	-6.322	1.47
158	333.935	9.176	-6.319	1.47
159	333.877	9.176	-6.325	1.48
160	333.906	9.176	-6.322	1.47
161	333.877	9.176	-6.325	1.48
162	333.906	9.176	-6.322	1.47
163	333.877	9.176	-6.325	1.48
164	333.877	9.176	-6.325	1.48
165	333.906	9.176	-6.322	1.47
166	333.877	9.176	-6.325	1.48
167	333.877	9.176	-6.325	1.48
168	333.877	9.176	-6.325	1.48
169	333.848	9.176	-6.328	1.48
170	333.906	9.176	-6.322	1.47
171	333.906	9.176	-6.322	1.47
172	333.877	9.176	-6.325	1.48
173	333.877	9.176	-6.325	1.48
174	333.906	9.176	-6.322	1.47
175	333.848	9.176	-6.328	1.48
176	333.877	9.176	-6.325	1.48
177	333.848	9.176	-6.328	1.48
178	333.906	9.176	-6.322	1.47
179	333.906	9.176	-6.322	1.47

180	333.848	9.176	-6.328	1.48
181	333.877	9.176	-6.325	1.48
182	333.906	9.176	-6.322	1.47
183	333.877	9.176	-6.325	1.48
184	333.877	9.176	-6.325	1.48
185	333.848	9.176	-6.328	1.48
186	333.935	9.176	-6.319	1.47
187	333.442	9.176	-6.37	1.52
	333.5			1.51
188		9.176	-6.364	
189	333.587	9.176	-6.355	1.51
190	333.703	9.176	-6.343	1.49
191	333.761	9.176	-6.337	1.49
192	333.645	9.176	-6.349	1.50
193	333.674	9.176	-6.346	1.50
194	333.267	9.176	-6.388	1.54
195	333.238	9.176	-6.39	1.54
196	333.442	9.176	-6.37	1.52
197	333.5	9.176	-6.364	1.51
198	332.919	9.176	-6.423	1.57
199	332.716	9.176	-6.444	1.59
200	333.093	9.176	-6.405	1.56
201	333.296	9.176	-6.385	1.54
202	333.151	9.176	-6.399	1.55
203	333.006	9.176	-6.414	1.56
204	333.209	9.176		1.54
			-6.393	
205	333.384	9.176	-6.376	1.53
206	333.413	9.176	-6.373	1.52
207	333.5	9.176	-6.364	1.51
208	333.587	9.176	-6.355	1.51
209	333.587	9.176	-6.355	1.51
210	333.645	9.176	-6.349	1.50
211	333.558	9.176	-6.358	1.51
212	333.238	9.176	-6.39	1.54
213	333.122	9.176	-6.402	1.55
214	332.687	9.176	-6.447	1.60
215	332.368	9.176	-6.479	1.63
216	332.629	9.176	-6.453	1.60
217	332.977	9.176	-6.417	1.57
218	333.122	9.176	-6.402	1.55
219	333.325	9.176	-6.382	1.53
220	333.325	9.176	-6.382	1.53
	333.413			
221		9.176	-6.373	1.52
222	333.442	9.176	-6.37	1.52
223	333.529	9.176	-6.361	1.51
224	333.558	9.176	-6.358	1.51
225	333.587	9.176	-6.355	1.51
226	333.616	9.176	-6.352	1.50
227	333.616	9.176	-6.352	1.50
228	333.645	9.176	-6.349	1.50
229	333.616	9.176	-6.352	1.50
230	333.645	9.176	-6.349	1.50
231	333.645	9.176	-6.349	1.50
232	333.674	9.176	-6.346	1.50
233	333.674	9.176	-6.346	1.50
234	333.296	9.176	-6.385	1.54
235	332.861	9.176	-6.429	1.58
236	332.948	9.176	-6.42	1.57
237	333.209	9.176	-6.393	1.54
238	333.355	9.176		1.53
239			-6.379	
	333.413	9.176	-6.373	1.52
240	333.5	9.176	-6.364	1.51
241	333.558	9.176	-6.358	1.51
242	333.558	9.176	-6.358	1.51
243	333.616	9.176	-6.352	1.50
244	333.645	9.176	-6.349	1.50
245	333.674	9.176	-6.346	1.50
246	333.616	9.176	-6.352	1.50
247	333.645	9.176	-6.349	1.50
248	333.645	9.176	-6.349	1.50
249	333.703	9.176	-6.343	1.49
250	333.645	9.176	-6.349	1.50
251	333.674	9.176	-6.346	1.50
252	333.674	9.176	-6.346	1.50
253	333.674	9.176	-6.346	1.50
254	333.674	9.176	-6.346	1.50
255	333.703	9.176	-6.343	1.49
256	333.703	9.176	-6.343	1.49
257	333.674	9.176	-6.346	1.50
258	333.674	9.176	-6.346	1.50
259	335.211	9.176	-6.189	1.34
260	335.473	9.176	-6.163	1.34
261	334.834	9.176	-6.228	1.38
262	334.428	9.176	-6.269	1.42
263	334.341	9.176	-6.278	1.43
264	334.283	9.176	-6.284	1.43
265	334.312	9.176	-6.281	1.43
266	333.964	9.176	-6.316	1.47
267	333.819	9.176	-6.331	1.48
268	333.761	9.176	-6.337	1.49
269	333.703	9.176	-6.343	1.49
270	333.732	9.176	-6.34	1.49
271	333.645	9.176	-6.349	1.50
272	333.645	9.176	-6.349	1.50

272	222.646	0.476	6.353	4.50
273	333.616	9.176	-6.352	1.50
274	333.616	9.176	-6.352	1.50
275	333.558	9.176	-6.358	1.51
276	333.587	9.176	-6.355	1.51
277	333.558	9.176	-6.358	1.51
278	333.558	9.176	-6.358	1.51
279	333.558	9.176	-6.358	1.51
280	333.471	9.176	-6.367	1.52
281	333.471	9.176	-6.367	1.52
282	333.5	9.176	-6.364	1.51
283	333.267	9.176	-6.388	1.54
284	333.093	9.176	-6.405	1.56
285	333.151	9.176	-6.399	1.55
286	333.238	9.176	-6.39	1.54
287	333.267	9.176	-6.388	1.54
288 289	333.355	9.176	-6.379	1.53
	333.355	9.176	-6.379 6.376	1.53
290 291	333.384 333.355	9.176 9.176	-6.376 -6.379	1.53 1.53
292	333.384	9.176	-6.376	1.53
293	333.413	9.176	-6.373	1.52
294	333.413	9.176	-6.373	1.52
295	333.267	9.176	-6.388	1.54
296	333.325	9.176	-6.382	1.53
297	333.355	9.176	-6.379	1.53
298	332.861	9.176	-6.429	1.58
299	333.122	9.176	-6.402	1.55
300	333.238	9.176	-6.39	1.54
301	333.325	9.176	-6.382	1.53
302	333.355	9.176	-6.379	1.53
303	333.355	9.176	-6.379	1.53
304	333.413	9.176	-6.373	1.52
305	333.355	9.176	-6.379	1.53
306	333.442	9.176	-6.37	1.52
307	333.442	9.176	-6.37	1.52
308	333.471	9.176	-6.367	1.52
309	333.471	9.176	-6.367	1.52
310	333.529	9.176	-6.361	1.51
311	333.442	9.176	-6.37	1.52
312	333.471	9.176	-6.367	1.52
313	333.471	9.176	-6.367	1.52
314 315	333.5 333.5	9.176 9.176	-6.364 -6.364	1.51 1.51
316	333.558	9.176	-6.358	1.51
317	333.5	9.176	-6.364	1.51
318	333.5	9.176	-6.364	1.51
319	333.529	9.176	-6.361	1.51
320	333.5	9.176	-6.364	1.51
321	333.5	9.176	-6.364	1.51
322	333.5	9.176	-6.364	1.51
323	333.5	9.176	-6.364	1.51
324	333.5	9.176	-6.364	1.51
325	333.529	9.176	-6.361	1.51
326	333.529	9.176	-6.361	1.51
327	333.529	9.176	-6.361	1.51
328	333.558	9.176	-6.358	1.51
329 330	333.558 333.529	9.176 9.176	-6.358 -6.361	1.51 1.51
331	333.529	9.176	-6.361	1.51
332	333.558	9.176	-6.358	1.51
333	333.587	9.176	-6.355	1.51
334	333.558	9.176	-6.358	1.51
335	333.529	9.176	-6.361	1.51
336	333.529	9.176	-6.361	1.51
337	333.5	9.176	-6.364	1.51
338	333.558	9.176	-6.358	1.51
339	333.558	9.176	-6.358	1.51
340	333.558	9.176	-6.358	1.51
341	333.296	9.176	-6.385	1.54
342	333.384	9.176	-6.376	1.53
343	333.442	9.176	-6.37	1.52
344	333.471	9.176	-6.367	1.52
345 346	333.471	9.176	-6.367 -6.367	1.52
346 347	333.471 333.471	9.176 9.176	-6.367 -6.367	1.52 1.52
348	333.5	9.176	-6.364	1.52
349	333.5	9.176	-6.364	1.51
350	333.5	9.176	-6.364	1.51
351	333.5	9.176	-6.364	1.51
352	333.529	9.176	-6.361	1.51
353	333.529	9.176	-6.361	1.51
354	333.529	9.176	-6.361	1.51
355	333.529	9.176	-6.361	1.51
356	333.5	9.176	-6.364	1.51
357	333.529	9.176	-6.361	1.51
358	333.529	9.176	-6.361	1.51
359 360	333.5	9.176	-6.364 -6.361	1.51
360 361	333.529 333.529	9.176 9.176	-6.361 -6.361	1.51 1.51
362	333.529	9.176	-6.361 -6.361	1.51
363	333.5	9.176	-6.364	1.51
364	333.5	9.176	-6.364	1.51
365	333.5	9.176	-6.364	1.51

TW1- WELL RECOVERY VS. TIME - KOLLAARD FILE 220067



Kollaard File 220067

RECOVERY DATA TW-1

ť'	t/t'	Abs Pres	Temp	Water Level	Drawdown	Recovery
		(kPa)	(°C)	(m)	(m)	(%)
1	366	338.027	9.176	-5.902	1.05	31%
2	183.5	339.856	9.176	-5.716	0.87	43%
3	122.7	340.901	9.176	-5.609	0.76	50%
4	92.3	341.627	9.176	-5.535	0.69	55%
5	74.0	342.179	9.176	-5.479	0.63	58%
6	61.8	342.643	9.176	-5.431	0.58	62%
7	53.1	343.021	9.176	-5.393	0.54	64%
8	46.6	343.369	9.176	-5.357	0.51	67%
9	41.6	343.66	9.176	-5.328	0.48	68%
10	37.5	343.921	9.176	-5.301	0.45	70%
11	34.2	344.183	9.176	-5.274	0.42	72%
12	31.4	344.386	9.176	-5.254	0.40	73%
13	29.1	344.59	9.176	-5.233	0.38	75%
14	27.1	344.735	9.176	-5.218	0.37	76%
15	25.3	344.909	9.176	-5.2	0.35	77%
16	23.8	345.054	9.176	-5.186	0.34	78%
17	22.5	345.229	9.176	-5.168	0.32	79%
18	21.3	345.345	9.176	-5.156	0.31	80%
19	20.2	345.49	9.176	-5.141	0.29	81%
20	19.3	345.577	9.176	-5.132	0.28	81%
21	18.4	345.694	9.176	-5.12	0.27	82%
22	17.6	345.781	9.176	-5.111	0.26	83%
23	16.9	345.868	9.176	-5.103	0.25	83%
24	16.2	345.955	9.176	-5.094	0.24	84%
25	15.6	346.042	9.176	-5.085	0.24	84%
26	15.0	346.13	9.176	-5.076	0.23	85%
27	14.5	346.217	9.176	-5.067	0.22	86%
28	14.0	346.275	9.176	-5.061	0.21	86%
29	13.6	346.333	9.176	-5.055	0.21	86%
30	13.2	346.42	9.176	-5.046	0.20	87%
31	12.8	346.507	9.176	-5.037	0.19	88%
32	12.4	346.565	9.176	-5.032	0.18	88%
33	12.1	346.624	9.176	-5.025	0.18	88%
34	11.7	346.682	9.176	-5.02	0.17	89%
35	11.4	346.711	9.176	-5.017	0.17	89%
36	11.1	346.769	9.176	-5.011	0.16	89%
37	10.9	346.798	9.176	-5.008	0.16	90%
38	10.6	346.856	9.176	-5.002	0.15	90%
39	10.4	346.914	9.176	-4.996	0.15	90%
40	10.1	346.972	9.176	-4.99	0.14	91%
41	9.9	347.001	9.176	-4.987	0.14	91%
42	9.7	347.03	9.176	-4.984	0.13	91%
43	9.5	347.089	9.176	-4.978	0.13	92%
44	9.3	347.118	9.176	-4.975	0.13	92%
45	9.1	347.147	9.176	-4.972	0.12	92%
46	8.9	347.205	9.176	-4.966	0.12	92%

	1	1	1	1	ſ	1
47	8.8	347.234	9.176	-4.963	0.11	93%
48	8.6	347.263	9.176	-4.96	0.11	93%
49	8.4	347.292	9.176	-4.957	0.11	93%
50	8.3	347.321	9.176	-4.954	0.10	93%
51	8.2	347.35	9.176	-4.951	0.10	93%
52	8.0	347.379	9.176	-4.949	0.10	93%
53	7.9	347.408	9.176	-4.946	0.10	94%
54	7.8	347.437	9.176	-4.943	0.09	94%
55	7.6	347.466	9.176	-4.94	0.09	94%
56	7.5	347.466	9.176	-4.94	0.09	94%
57	7.4	347.495	9.176	-4.937	0.09	94%
58	7.3	347.524	9.176	-4.934	0.08	94%
59	7.2	347.554	9.176	-4.931	0.08	95%
60	7.1	347.583	9.176	-4.928	0.08	95%
61	7.0	347.612	9.176	-4.925	0.08	95%
62	6.9	347.612	9.176	-4.925	0.08	95%
63	6.8	347.67	9.176	-4.919	0.07	95%
64	6.7	346.711	9.176	-5.017	0.17	89%
65	6.6	345.403	9.176	-5.15	0.30	80%
66	6.5	346.914	9.176	-4.996	0.15	90%
67	6.4	347.176	9.176	-4.969	0.12	92%
68	6.4	347.321	9.176	-4.954	0.10	93%
69	6.3	347.437	9.176	-4.943	0.09	94%
70	6.2	347.466	9.176	-4.94	0.09	94%
71	6.1	347.524	9.176	-4.934	0.08	94%
72	6.1	347.583	9.176	-4.928	0.08	95%
73	6.0	347.641	9.176	-4.922	0.07	95%
74	5.9	347.67	9.176	-4.919	0.07	95%



ATTACHMENT D WATER QUALITY TEST RESULTS



Certificate of Analysis

Environment Testing

210 Prescott St., Box 189 Kollaard Associates Inc. Kemptville, ON Client:

Ms. Colleen Vermeersch Attention:

K0G 1J0

2022-06-03 220067 891018 2022-05-20 1977709

Report Number: Date Submitted: Date Reported: Project: COC #:

Kollaard Associates Inc. Invoice to:

Page 1 of 8

Dear Colleen Vermeersch:

Please find attached the analytical results for your samples. If you have any questions regarding this report, please do not hesitate to call (613-727-5692).

Report Comments:

Emma-

Dawn

Ferguson 2022.06.0

3 15:32:30

-04'00'

Emma-Dawn Ferguson, Chemist

APPROVAL:

All analysis is completed at Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) unless otherwise indicated.

Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) is accredited by CALA, Canadian Association for Laboratory Accreditation to ISO/IEC 17025 for tests which appear on the scope of accreditation. The scope is available at: http://www.cala.ca/scopes/2602.pdf Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) is licensed by the Ontario Ministry of the Environment, Conservation, and Parks (MECP) for specific tests in drinking water (license #2318). A copy of the license is available upon request.

Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) is accredited by the Ontario Ministry of Agriculture, Food, and Rural Affairs for specific tests in agricultural soils.

ease of use (informational purposes) only. Eurofins recommends consulting the official provincial or federal guideline as required. Unless otherwise stated, measurement uncertainty is not taken into account when determining guideline or regulatory exceedances. Please note: Field data, where presented on the report, has been provided by the client and is presented for informational purposes only. Guideline values listed on this report are provided for





Environment Testing

210 Prescott St., Box 189 Kollaard Associates Inc. Client:

Kemptville, ON K0G 1J0

Ms. Colleen Vermeersch Attention: PO#:

Kollaard Associates Inc. Invoice to:

2022-05-20 1977709 Date Submitted: Date Reported: Report Number:

2022-06-03 220067 891018 Project: COC #:

1627129 Water 2022-05-19 TW1-6hrs		63	<0.10	<0.10	0.15	131	346	<2	962	7.37	<0.001	<0.01	625*	2.7	530*	1.00	<0.0001	<0.01	<0.001	<0.01	0.10	<0.0005	125	<0.0001	0.0004	<0.001
Lab I.D. Sample Matrix Sample Type Sampling Date Sample I.D.	Guideline	AO 250	MAC 1.5	MAC 1.0	MAC 10.0	AO 500	OG 30-200			6.5-8.5		AO 0.05	AO 500	AO 5	OG 80-100			06 0.1	IMAC 0.01	IMAC 5.0	MAC 1.0			MAC 0.005		MAC 0.05
	Units	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	TCU	nS/cm		mg/L	mg/L	mg/L	NTO	mg/L		mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
	MRL	_	0.10	0.10	0.10	_	2	2	2	1.00	0.001	0.01	_	0.1	_	0.01	0.0001	0.01	0.001	0.01	0.01	0.0005	_	0.0001	0.0002	0.001
	Analyte	ō	Ш	N-NO2	N-NO3	804	Alkalinity as CaCO3	Colour (True)	Conductivity	Hd	Phenols	S2-	TDS (COND - CALC)	Turbidity	Hardness as CaCO3	lon Balance	Ag	A	As	В	Ba	Be	Ca	Cd	လ	C
	Group	Anions					General Chemistry								Hardness	Indices/Calc	Metals									

Guideline = ODWSOG

* = Guideline Exceedence

Results relate only to the parameters tested on the samples submitted. Methods references and/or additional QA/QC information available on request.

MRL = Method Reporting Limit, AO = Aesthetic Objective, OG = Operational Guideline, MAC = Maximum Acceptable Concentration, IMAC = Interim Maximum Acceptable Concentration, STD = Standard, PWQO = Provincial Water Quality Guideline, IPWQO = Interim Provincial Water Quality Objective, TDR = Typical Desired Range





Environment Testing

210 Prescott St., Box 189 Kollaard Associates Inc. Client:

Kemptville, ON K0G 1J0

Ms. Colleen Vermeersch

Attention: PO#:

Kollaard Associates Inc. Invoice to:

1977709 Report Number:

)5-20)6-03

891018	COC#:
220067	Project:
2022-06	Date Reported:
2022-05	Date Submitted:

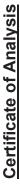
1627129 Water	2022-05-19 TW1-6hrs		<0.001	0.15	<0.0001	_	53	*90.0	<0.005	20	<0.005	<0.001	<0.0005	<0.001	0.143	<0.0001	0.004	<0.001	<0.01	<0.010	0.312	_	1.7
Lab I.D. Sample Matrix	Sample Type Sampling Date Sample I.D.	Guideline	AO 1	AO 0.3	MAC 0.001			AO 0.05		AO 200		MAC 0.010	IMAC 0.006	MAC 0.05			MAC 0.02		AO 5				AO 5
		Units	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
		MRL	0.001	0.03	0.0001	_	_	0.01	0.005	_	0.005	0.001	0.0005	0.001	0.001	0.0001	0.001	0.001	0.01	0.010	0.100	_	0.2
		Analyte	Cu	Fe	Hg	ス	Mg	Mn	Mo	Na	Ż	Pb	Sb	Se	S	I	ח	>	Zn	N-NH3	Total Kjeldahl Nitrogen	Tannin & Lignin	DOC
		Group	Metals	1	1			1			1	1	1	1	1					Nutrients		Subcontract	Subcontract-Inorg

Guideline = ODWSOG

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Results relate only to the parameters tested on the samples submitted. Methods references and/or additional QA/QC information available on request.

MRL = Method Reporting Limit, AO = Aesthetic Objective, OG = Operational Guideline, MAC = Maximum Acceptable Concentration, IMAC = Interim Maximum Acceptable Concentration, STD = Standard, PWQO = Provincial Water Quality Guideline, IPWQO = Interim Provincial Water Quality Objective, TDR = Typical Desired Range





Environment Testing

210 Prescott St., Box 189 Kollaard Associates Inc. Client:

Kemptville, ON K0G 1J0

Ms. Colleen Vermeersch

Attention: PO#:

Invoice to:

Kollaard Associates Inc.

2022-05-20 2022-06-03 1977709 Date Submitted: Date Reported: Report Number:

891018 220067 Project: COC #:

QC Summary

Analyte	Blank		QC % Rec	QC Limits
Run No 422498 Analysis/Extraction Date 2022-05-21 Method C SM2130B		Analyst	Š	
Turbidity	<0.1 NTU		66	70-130
Run No 422509 Analysis/Extraction Date 2022-05-27 Method C SM2120C		Analyst	AsA	
Colour (True)	<2 TCU		104	80-120
Run No 422512 Analysis/Extraction Date 2022-05-24 Method SUBCONTRACT-A		Analyst	AET	
Tannin & Lignin	<1.0 mg/L		66	
Run No 422533 Analysis/Extraction Date 2022-05-27 Method C SM4500-S2-D		Analyst	AsA	
S2-	<0.01 mg/L			80-120
Run No 422569 Analysis/Extraction Date 2022-05-28 Method SM 4110		Analyst	AaN	
Chloride	<1 mg/L		100	90-110
N-NO2	<0.10 mg/L		100	90-110
N-NO3	<0.10 mg/L		101	90-110
Run No 422635 Analysis/Extraction Date 2022-05-27 Method SM2320.2510.4500H/F		Analyst	AsA	

Guideline = ODWSOG

* = Guideline Exceedence





210 Prescott St., Box 189 Kollaard Associates Inc. Kemptville, ON Client:

K0G 1J0

Ms. Colleen Vermeersch Attention: PO#:

Kollaard Associates Inc. Invoice to:

2022-05-20 1977709 Date Submitted: Date Reported: Report Number:

2022-06-03 220067

891018 Project: COC #:

QC Summary

Analyte	Blank	QC % Rec	QC Limits
Alkalinity (CaCO3)	7/6ш 5 >	26	90-110
Conductivity	<5 uS/cm	66	90-110
L	<0.10 mg/L	102	90-110
Hd		100	90-110
Run No 422640 Analysis/Extraction Date 2022-05-30 Method SM 4110		Analyst AaN	
SO4	<5 mg/L	110	90-110
Run No 422650 Analysis/Extraction Date 2022-05-28 Method EPA 350.1		Analyst SKH	
N-NH3	<0.010 mg/L	06	80-120
Run No 422655 Analysis/Extraction Date 2022-05-28 Method EPA 351.2		Analyst SKH	
Total Kjeldahl Nitrogen	<0.100 mg/L	105	70-130
Run No 422713 Analysis/Extraction Date 2022-05-29 Method SM5530D/EPA420.2		Analyst IP	
Phenols	<0.001 mg/L	96	50-120
Run No 422754 Analysis/Extraction Date 2022-05-30 Method M SM3120B-3500C		Analyst Z S	
Calcium	<1 mg/L	102	90-110

Guideline = ODWSOG





210 Prescott St., Box 189 Kollaard Associates Inc. Kemptville, ON Client:

K0G 1J0

Ms. Colleen Vermeersch Attention: PO#:

Kollaard Associates Inc. Invoice to:

2022-05-20 1977709 Date Submitted: Date Reported: Report Number:

2022-06-03 891018 220067 Project: COC #:

QC Summary

Analyte	Blank	QC % Rec	QC Limits
Potassium	<1 mg/L	109	87-113
Magnesium	<1 mg/L	97	76-124
Sodium	<1 mg/L	113	82-118
Run No 422756 Analysis/Extraction Date 2022-05-30 Method C SM2340B		Analyst AET	
Hardness as CaCO3			
lon Balance			
TDS (COND - CALC)			
Run No 422838 Analysis/Extraction Date 2022-05-30 Method EPA 200.8		Analyst SD	
Silver	<0.0001 mg/L	68	80-120
Aluminum	<0.01 mg/L	117	80-120
Arsenic	<0.001 mg/L	103	80-120
Boron (total)	<0.01 mg/L	108	80-120
Barium	<0.01 mg/L	102	80-120
Beryllium	<0.0005 mg/L	111	80-120
Cadmium	<0.0001 mg/L	106	80-120
Cobalt	<0.0002 mg/L	106	80-120

Guideline = ODWSOG

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Results relate only to the parameters tested on the samples submitted. Methods references and/or additional QA/QC information available on request.





210 Prescott St., Box 189 Kollaard Associates Inc. Client:

Kemptville, ON K0G 1J0

Ms. Colleen Vermeersch

Attention: PO#:

Kollaard Associates Inc. Invoice to:

2022-05-20 1977709 Date Submitted: Date Reported: Report Number:

2022-06-03 220067 Project: COC #:

891018

QC Summary

Analyte	Blank	QC % Rec	QC Limits
Chromium Total	<0.001 mg/L	108	80-120
Copper	<0.001 mg/L	111	80-120
Iron	<0.03 mg/L	26	80-120
Mercury	<0.0001 mg/L	66	80-120
Manganese	<0.01 mg/L	108	80-120
Molybdenum	<0.005 mg/L	102	80-120
Nickel	<0.005 mg/L	109	80-120
Lead	<0.001 mg/L	101	80-120
Antimony	<0.0005 mg/L	101	80-120
Selenium	<0.001 mg/L	109	80-120
Strontium	<0.001 mg/L	107	80-120
Thallium	<0.0001 mg/L	101	80-120
Uranium	<0.001 mg/L	91	80-120
Vanadium	<0.001 mg/L	108	80-120
Zinc	<0.01 mg/L	110	80-120
Run No 423131 Analysis/Extraction Date 2022-06-02 Method SUBCONTRACT-CA-INORG	22-06-02 Analyst	ılyst RS	
DOC			

Guideline = ODWSOG

* = Guideline Exceedence

Results relate only to the parameters tested on the samples submitted. Methods references and/or additional QA/QC information available on request.



Certificate of Analysis

Environment Testing

Client: Kollaard Associates Inc.

210 Prescott St., Box 189

Kemptville, ON

K0G 1J0 Attention: Ms. Colleen Vermeersch

PO#:

Invoice to: Kollaard Associates Inc.

Report Number: Date Submitted:

1977709

Date Submitted: 2022-05-20
Date Reported: 2022-06-03
Project: 220067

COC #: 891018

Sample Comment Summary

Sample ID: 1627129 TW1-6hrs Due to a power outage true color, pH, conductivity, alkalinity, F, anions, N-NO3, N-NO3, N-NH3, TKN, and S2- were analyzed after being held outside of recommended temperature for a prolonged period of time. pH, akalinity, conductivity, N-NO2 and N-NO3 were analyzed past the holding time. SO4 MRL elevated due to matrix interference (dilution was done). DOC analysis subcontracted.

Guideline = ODWSOG

* = Guideline Exceedence

Results relate only to the parameters tested on the samples submitted. Methods references and/or additional QA/QC information available on request.



Certificate of Analysis

Environment Testing

210 Prescott St., Box 189 Kollaard Associates Inc. Client:

Kemptville, ON

Ms. Colleen Vermeersch Attention:

Kollaard Associates Inc. Invoice to:

220067 891018 Report Number: Date Submitted: Date Reported: Project: COC #:

2022-05-20 2022-05-27

9692261

Page 1 of 3

Dear Colleen Vermeersch:

Please find attached the analytical results for your samples. If you have any questions regarding this report, please do not hesitate to call (613-727-5692).

Report Comments:

Emma-

Dawn

2022.05.27 Ferguson

12:54:39 04,00 Emma-Dawn Ferguson, Chemist

APPROVAL:

All analysis is completed at Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) unless otherwise indicated.

Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) is accredited by CALA, Canadian Association for Laboratory Accreditation to ISO/IEC 17025 for tests which appear on the scope of accreditation. The scope is available at: http://www.cala.ca/scopes/2602.pdf.

Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) is licensed by the Ontario Ministry of the Environment, Conservation, and Parks (MECP) for specific tests in drinking water (license #2318). A copy of the license is available upon request.

Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) is accredited by the Ontario Ministry of Agriculture, Food, and Rural Affairs for specific tests in agricultural soils.

Please note: Field data, where presented on the report, has been provided by the client and is presented for informational purposes only. Guideline values listed on this report are provided for ease of use (informational purposes) only. Eurofins recommends consulting the official provincial or federal guideline as required. Unless otherwise stated, measurement uncertainty is not taken into account when determining guideline or regulatory exceedances.





210 Prescott St., Box 189 Kollaard Associates Inc. Client:

Kemptville, ON

Ms. Colleen Vermeersch Attention:

K0G 1J0

Kollaard Associates Inc. Invoice to:

PO#:

2022-05-20 1977696 Report Number: Date Submitted: Date Reported: Project: COC #:

2022-05-27 220067 891018

Guideline = ODWSOG

* = Guideline Exceedence

Results relate only to the parameters tested on the samples submitted. **Analytical Method: AMBCOLM1** additional QA/QC information available on request.

146 Colonnade Rd. Unit 8, Ottawa, ON K2E 7Y1

Page 2 of 3



Certificate of Analysis

Environment Testing

Kollaard Associates Inc. Client:

210 Prescott St., Box 189

Kemptville, ON

Ms. Colleen Vermeersch Attention:

K0G 1J0

Kollaard Associates Inc. Invoice to:

PO#:

1977696

2022-05-20 2022-05-27 220067 Report Number: Date Submitted: Date Reported: Project: COC #:

891018

Sample Comment Summary

NDLA: No data, lab accident (power outage). Sample ID: 1627103 TW1-6hrs

Guideline = ODWSOG

* = Guideline Exceedence

Results relate only to the parameters tested on the samples submitted. **Analytical Method: AMBCOLM1** additional QA/QC information available on request.

146 Colonnade Rd. Unit 8, Ottawa, ON K2E 7Y1

Page 3 of 3

Ryznar Stability Index

$$RSI = 2(pH_s) - pH$$

RSI $<< 6 \rightarrow$ the scale tendency increases as the index decreases

RSI >> 7 → the calcium carbonate formation probably does not lead to a protective corrosion inhibitor film

RSI >> 8 → mild steel corrosion becomes an increasing problem

Langelier Saturation Index

$$LSI = pH - pH_s$$

If LSI is negative → no potential to scale, the water will dissolve CaCO₃

If LSI is positive → scale can form and CaCO₃ precipitation may occur

If LSI is close to zero → borderline scale potential, water quality or temperature change or evaporation could change the index

where pH measured from sample

pH_s = pH at saturation in calcite or calcium carbonate

$$pH_{s} = (9.3 + A + B) - (C + D)$$

$$A = \frac{\log_{10}[TDS] - 1}{10}$$

$$B = -13.12 \times \log_{10}(^{\circ}C + 273) + 34.55$$

$$C = \log_{10}[Ca^{2+}asCaCO_{3}] - 0.4$$

$$D = \log_{10}[alkalinityasCaCO_{3}]$$

TW1-final

	1 * * * 1 111101
рН	7.37
hardness [mg/l as CaCo ₃]	530
Alkalinity [mg/l as CaCo ₃]	346
total dissolved solids [mg/l]	625
temperature (°C)	11
A	0.179588002
В	2.362463379
C	2.32427587
D	2.539076099
pH_s	6.978699412
→→ RSI	6.59
ightarrow ightarrow LSI	0.39



ATTACHMENT E SEWAGE ATTENUATION CALCULATIONS

June 2022 220067

SEPTIC EFFLUENT DILUTION CALCULATIONS

Number of Lots	1				
Gross Site Area	6750 m ²				
Env. Can. Water Surplus (NPI-glacial till)	328 mm				
Hard Surface Area (Post-Development)					
Roofs	403				
Driveway	<u>709</u>				
Total	1111 m ²				
Net Infiltration Area = Gross Site Area - Hard Surface & Each system is expected to use half the infiltration are Infiltration Reduction Factor:	5638.84 m ²				
Topography (flat)	0.30				
Soil (medium combinations clay and loam)	0.20				
Cover (cultivated/wood)	<u>0.13</u>				
Total IRF	0.63				
Nitrate Concentration for main house					

C _H =	365 m ³ Effluent Per Year x 40 mg/L NO ₃		15.4	mg/L NO ₃ -N
	365 m³ Effluent Per Year + (1/2 x Net Infiltration Area x NPI x IRF)			
	Nitrate Dilution for coach house (with denitrification-effluent Nitrate concentration-8 mg/L)			
C _c =	365 m ³ Effluent Per Year x 8 mg/L NO ₃	=	3.1	mg/L NO ₃ -N
	365 m³ Effluent Per Year + (1/2 x Net Infiltration Area x NPI x IRF)			

Total Concentration C_T = $C_H V_H$ + $C_c V_c$ / V_t V_H and V_c each = 365 m³/year C_T = 9.2 mg/L N-NO₃



ATTACHMENT F

WATERLOO BIOFILTER WATER NO_X-LS THIRD PARTY TESTING SUMMARY



WaterNOx-LS Third Party Testing Summary

In the fall of 2016, Waterloo Biofilter Systems Inc. installed their WaterNOx-LS™ denitrification unit at the Bureau de Normalisation du Quebec (BNQ) test site located in Quebec City. The system underwent BNQ 3680-600 test protocol which includes two parts - Period A and Period B. Period A is based on the methodology of NSF/ANSI Standards 40 and 245, containing the same flow patterns and stress tests. Period B provides for a further 6 months of seasonal reliability testing to ensure that the test includes cold weather results.

The WaterNOx-LS is a passive autotrophic denitrification process using sulphur-limestone minerals in a submerged, up-flow configuration. The WaterNOx-LS, which was sized for 1,600 L/day (350 gpd) followed a Waterloo Biofilter nitrifying treatment unit.

Period A Test Results

During Period A wastewater is dosed according to the hydraulic loading specified in NSF-40. Period A includes the wash-day, working-parent, power failure, and vacation period stress tests. All sample results taken during stress tests are included in the analysis. Influent wastewater temperature values ranged from 10.0 °C (50 °F) to 16.5 °C (62 °F) with an average value of 13.3 °C (56 °F). Influent pH averaged 7.9 and effluent pH averaged 7.2.

Table 1 - Period A Results for the WaterNOx-LS

Parameters	Influent	Effluent	Removal
(c)BOD ₅	260	6	97.6%
TSS	312	3	99.2%
Fecal Coliforms	2,403,000	4,900	99.8%
NO _{2,3}	0.08	0.20	
TKN	57.1	4.6	92.0%
TN	57.1	4.8	91.6%

n = 123; n = 357 for fecals

All parameters in mg/L except Fecal Coliforms in cfu/100mL

All values arithmetic averages except Fecal Coliforms in geometric average

Weekly influent total nitrogen concentrations ranged from 43.0 mg/L to 68.8 mg/L with a six-month average concentration of 57.1 mg/L.

Weekly effluent $NO_{2,3}$ concentrations ranged from < 0.02 mg/L to 3.33 mg/L with a six-month average of 0.20 mg/L. Weekly effluent TKN concentrations ranged from 1.5 mg/L to 16.9 mg/L with a six-month average of 4.6 mg/L. Weekly effluent total nitrogen concentrations ranged from 1.7 mg/L to 17.1 mg/L with a six-month average of 4.8 mg/L. The total nitrogen reduction over the six-month period was 91.6%.



Period B Test Results

Weekday hydraulic loading is modified during Period B to a strenuous 'working parent' schedule where 40% of the flow is delivered over three hours in the morning, and 60% is delivered over three hours in the evening. All samples taken during Period B are included in the analysis. Influent wastewater temperature values ranged from 10.1 °C (50 °F) to 15.8 °C (60 °F) with an average value of 12.3 °C (54 °F). Influent pH averaged 8.0 and effluent pH averaged 7.1.

Table 2 – Period B Results for the WaterNOx-LS

Parameters	Influent	Effluent	Removal
(c)BOD ₅	248	4	98.2%
TSS	304	3	99.1%
Fecal Coliforms	2,142,000	2,800	99.9%
NO _{2,3}	0.17	3.38	
TKN	60.3	8.5	85.9%
TN	60.4	11.9	80.3%

n = 59 except Fecal Coliforms n = 118

All parameters in mg/L except Fecal Coliforms in cfu/100mL

All values arithmetic averages except Fecal Coliforms in geometric average

Weekly influent total nitrogen concentrations ranged from 21.2 mg/L to 85.6 mg/L with a six-month average concentration of 60.4 mg/L.

Weekly effluent $NO_{2,3}$ concentrations ranged from < 0.04 mg/L to 15.2 mg/L with a six-month average of 3.38 mg/L. Weekly effluent TKN concentrations ranged from 1.2 mg/L to 21.2 mg/L with a weekly average of 8.5 mg/L. Weekly effluent total nitrogen concentrations ranged from 3.7 mg/L to 22.2 mg/L with a six-month average of 11.9 mg/L. The total nitrogen reduction over the six-month period was 80.3%.

Conclusion

In summary, the WaterNOx-LS system can successfully remove very high levels of total nitrogen passively, while buffering pH to neutral and keeping cBOD₅ and TSS levels below 10 mg/L.