

TECHNICAL MEMORANDUM

DATE September 13, 2022 **Project No.** 21493887

TO City of Ottawa

FROM Scott Taylor, PEng EMAIL Scott_Taylor@golder.com

NEW SEPTIC SYSTEM HYDRO ONE OPERATIONS CENTRE, PHASE 2 3440 FRANK KENNY ROAD, OTTAWA, ONTARIO

Golder Associates Ltd. (Golder) was retained by J.L. Richards & Associates Limited (JLR) to design the new sewage system at the proposed Hydro One Networks Inc. (HONI) Operations Centre (OC), Phase 2, located at 3440 Frank Kenny Road in Ottawa, Ontario. This technical memorandum has been prepared to support the Site Plan Approval application with the City of Ottawa.

Sewage System Design Flows

HONI has provided the following information for the proposed building use:

- Office staff will consist of 5 employees on one (1) 8-hour shift during normal operations and 10 employees constantly occupying the building over a 24-hour duration during emergency operations.
- Field staff will consist of 30 employees on an 8-hour shift during normal operations and 30 employees on a
 16-hour shift during emergency operations.
- There is one (1) loading dock and deliveries to the warehouse will occur once per week or once every two weeks.
- Vehicle washing will be limited to removal of mud from the wheels of the vehicles and will be completed outside of the building.

Golder has pre-consulted with the Ottawa Septic System Office regarding the sewage system design flows. The following was determined during the pre-consultation:

- The building is split into multiple uses. The uses are separated by Gridlines as indicated below (Refer to Appendix A). Each area of the building will be calculated separately as follows:
 - Office (Gridlines 9 to 11): The office will be based on the number of employees and the floor area of the
 office portion of the building.
 - Warehouse (Gridlines 5 to 9): The common facilities (washrooms, locker rooms, etc.) and warehouse space will be calculated as a warehouse.

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Vehicle Storage Canopy and Indoor Vehicle Storage (Gridlines 1 to 5): No additional flows have been considered from the vehicle storage areas of the building, as vehicle washing is to be completed outside of the building.

Based on the above, the total daily design sanitary sewage flow (Q) has been calculated as follows, in accordance with Table 8.2.1.3.B of the Ontario Building Code (OBC):

Normal Operations

Office (Staff) = 5 employees * 75 L/d/employee (8-hour shift) = 375 L/d

Office (Floor Space) = $295 \text{ m}^2 * 75 \text{ L/d/9.3 m}^2 = 2,379 \text{ L/d}$

Warehouse (Loading Dock) = 1 * 150 L/d = 150 L/d

Warehouse (Water Closets) = 4 * 950 L/d = 3,800 L/d

 $Q = 2,379 L/d^{1} + 150 L/d + 3,800 L/d$

Q = 6,329 L/d

Emergency Operations

Office (Staff) = 10 employees * 75 L/d/employee (8-hour shift) * 3 shifts = 2,250 L/d

Office (Floor Space) = $295 \text{ m}^2 * 75 \text{ L/d/}9.3 \text{ m}^2 = 2{,}379 \text{ L/d}$

Warehouse (Loading Dock) = 1 * 150 L/d = 150 L/d

Warehouse (Water Closets) = 4 * 950 L/d = 3,800 L/d

 $Q = 2,379 L/d^{1} + 150 L/d + 3,800 L/d$

Q = 6,329 L/d

The total daily design sanitary sewage flow has been calculated to be 6,329 L/d for both normal and emergency operations as the floor area of the office governs the calculations, and also since the staffing for field staff has not been included directly, but instead assessed based on the warehouse facilities.

Treatment Units

A Class 4 Sewage System, as per Section 8.6 of the OBC, is proposed to service the new building and will consist of a Waterloo Biofilter basket tank system, model number BT-15500. The system will also consist of an anaerobic digester (septic tank) with a volume of 13,625 L (model number 13625AD), followed by a separate 6,000 L pump tank that will be used to dose the final 15,500 L Biofilter basket tank. Refer to Sewage System Plan, Figure 1 and Detail Sheet, Figure 2 in Appendix B.



¹ The total daily design sanitary sewage flow includes the highest flow from the office area.

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Due to the anticipated elevations of the tanks and leaching bed, a second alternating duplex pump system will be required to dose the leaching bed. Waterloo Biofilter has confirmed that these pumps can be installed within the Biofilter basket tank.

In accordance with the terrain analysis calculations included in the Technical Memorandum titled "Resampling Results, Well PW11-1 and Updated Terrain Analysis", prepared by Golder Associates Ltd., dated September 8, 2022, a 50% reduction in nitrogen will be required for the site. Therefore, the treatment unit will be constructed as a double-pass system for denitrification, which requires recirculation to the anaerobic digester. As per the literature from Waterloo Biofilter, a double-pass system can achieve between 50 to 65% nitrogen reduction. The 32 mm diameter recirculation forcemain will provide approximately 50% recirculation of treated effluent back to the anaerobic digester, in accordance with the requirements from Waterloo Biofilter.

The treatment units have been located on the site to conform with the minimum clearance distances as set out in Table 8.2.1.6.A of the OBC.

Leaching Bed

The previous geotechnical investigation (completed in 2011) included a test pit (Test Pit 11-3) in the vicinity of the proposed leaching bed. This geotechnical investigation has been updated to include recent site investigations and current standards. Refer to Geotechnical Investigation, Proposed Hydro One Operations Facility, 3440 Frank Kenny Road, Ottawa, Ontario, prepared by Golder Associates Ltd., Dated September 9, 2022. The existing soils at the proposed location of the leaching bed consist of grey brown silty clay (weathered crust), as indicated in Test Pit 11-3. Groundwater seepage was noted in Test Pit 11-3 at 2.0 m below ground surface (elevation 83.90 m). Groundwater was observed in Boreholes 11-3 and 11-5 between 1.1 and 1.3 m below ground surface (elevation of 84.40 m for both). A groundwater elevation of 85.60 m was measured in monitoring well DBW001 during GHD's investigation. Conservatively, an elevation of 85.60 m has been assumed in the vicinity of the leaching bed, which is below the maximum excavation depth.

Based on the existing soils, a percolation rate (T) has been estimated at 50 min/cm. Since this is the maximum value used in determining the size of the proposed leaching bed, it is considered a conservative estimate.

Due to space restrictions on the site, a Type A Dispersal Bed is proposed to be used as the leaching bed. The contact area (overall footprint) of the Type A Dispersal Bed has been sized in accordance with 8.7.7.1.(5) of the OBC as follows:

Contact Area (A) = Q * T / 400

A = 6.329 * 50 / 400

 $A = 791 \text{ m}^2$

Therefore, the system will require a contact area of 791 m². A contact area measuring 25.0 m x 31.7 m has been provided, which provides a contact area of 792.5 m². Refer to Sewage System Plan, Figure 1 in Appendix B.

The stone layer for the Type A Dispersal Bed has been sized in accordance with 8.7.7.1.(6) of the OBC as follows:



Stone Area $(A_s) = Q / 50$

 $A_s = 6.329 / 50$

 $A_s = 127 \text{ m}^2$

Therefore, the system will require a stone area of 127 m². A stone area measuring 6 m x 21.2 m has been provided, which provides a contact area of 127 m². Refer to Sewage System Plan, Figure 1 in Appendix B.

The effluent will be evenly distributed throughout the stone area by use of distribution piping installed to within 600 mm of the edge of stone layer, in accordance with 8.7.7.1.(8) of the OBC.

The stone layer has been located on the site to conform with the minimum clearance distances as set out in Table 8.2.1.6.B (and increased by Sentence 8.7.4.2.(11) for a raised system) of the OBC.

The leaching bed is proposed over the existing gravel parking lot for the Phase 1 building. Therefore, the gravel for the parking lot is proposed to be removed down to the native soils. The area under the contact area for the leaching bed will be scarified to a depth of 300 mm to loosen up the compacted subgrade and promote infiltration. Imported sand fill will be used to build up the area to the base of the leaching bed. As well, to prevent lateral movement of effluent through the gravel fill, an additional area extending 2.0 m around the perimeter of the leaching bed on three sides will be removed and replaced with compacted clay. This compacted clay barrier will direct the effluent in the direction of the 15 m mantle.

We trust that the above is sufficient for your purposes. If you have any questions or comments, please contact the undersigned.

Yours truly,

Golder Associates Ltd.



Scott Taylor, PEng Senior Civil Engineer Douglas Kerr, PEng

Associate, Senior Civil Engineer

Voylan Ken

SWT/DVK/mp

Attachments: Appendix A – Floor Plan

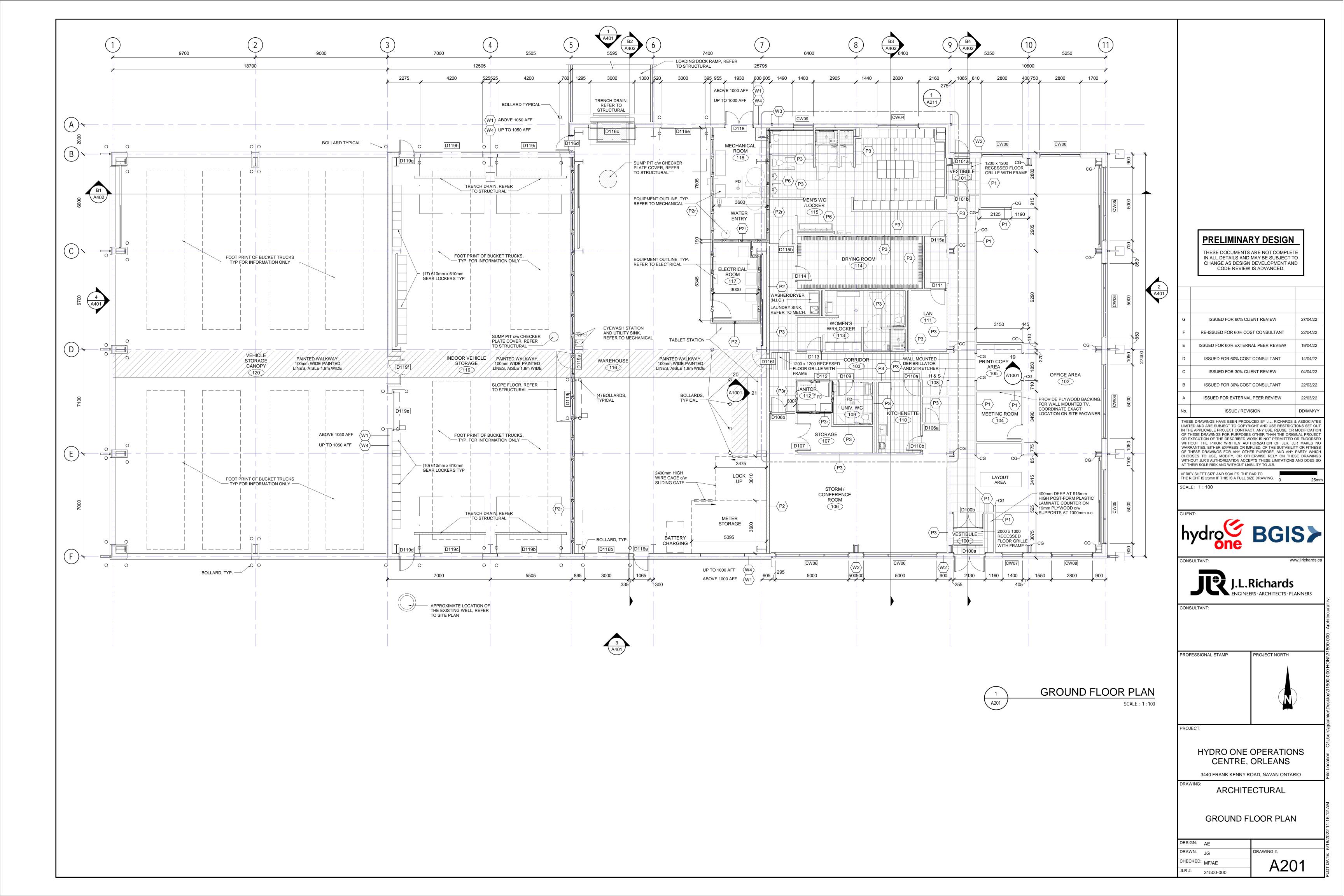
Appendix B – Figures

https://golderassociates.sharepoint.com/sites/152302/project files/6 deliverables/sewage system design/city of ottawa spa 2022.09.07/21493887-tm-rev1-sewage system design-12sept2022.docx



APPENDIX A

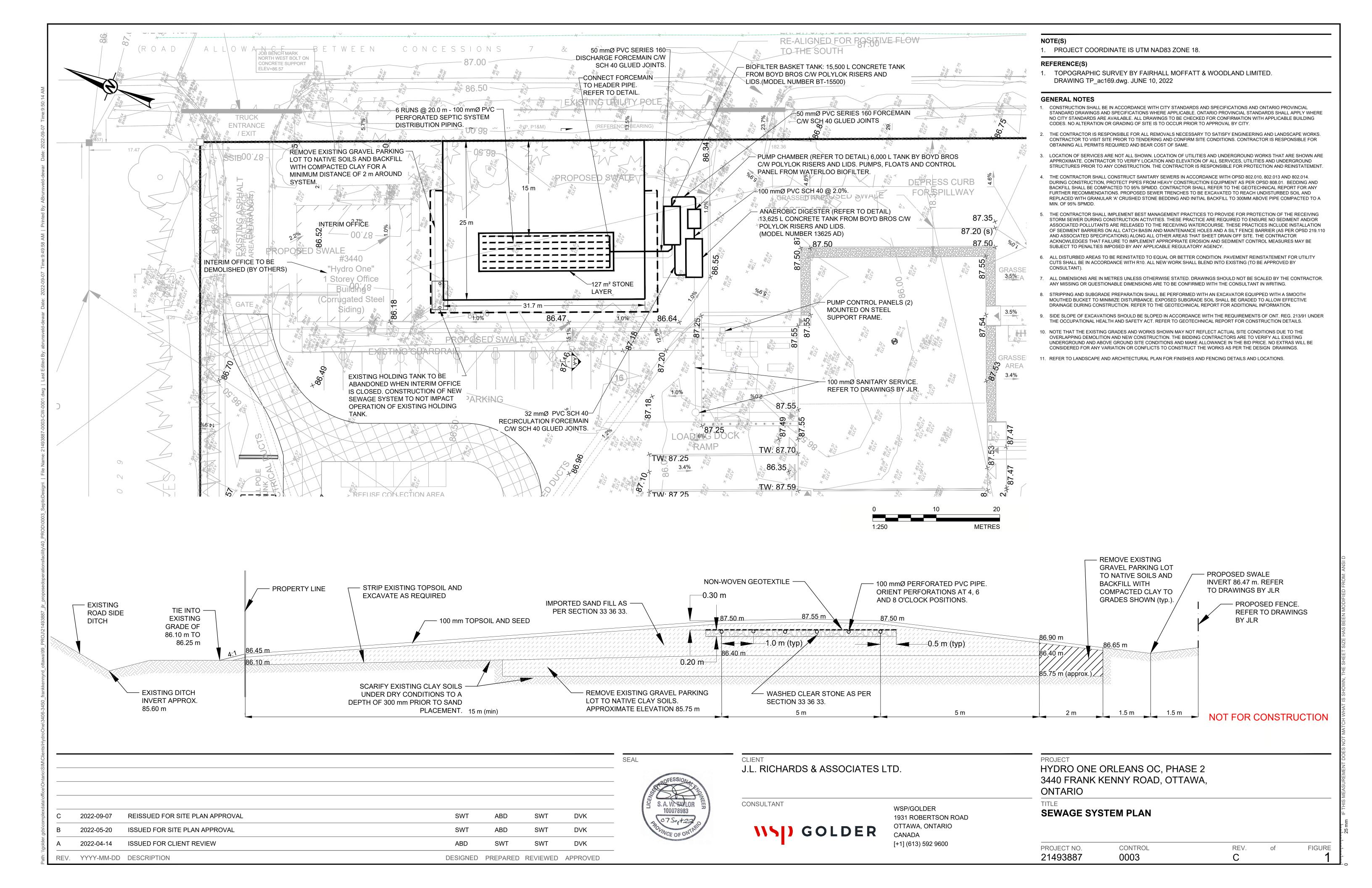
Floor Plan

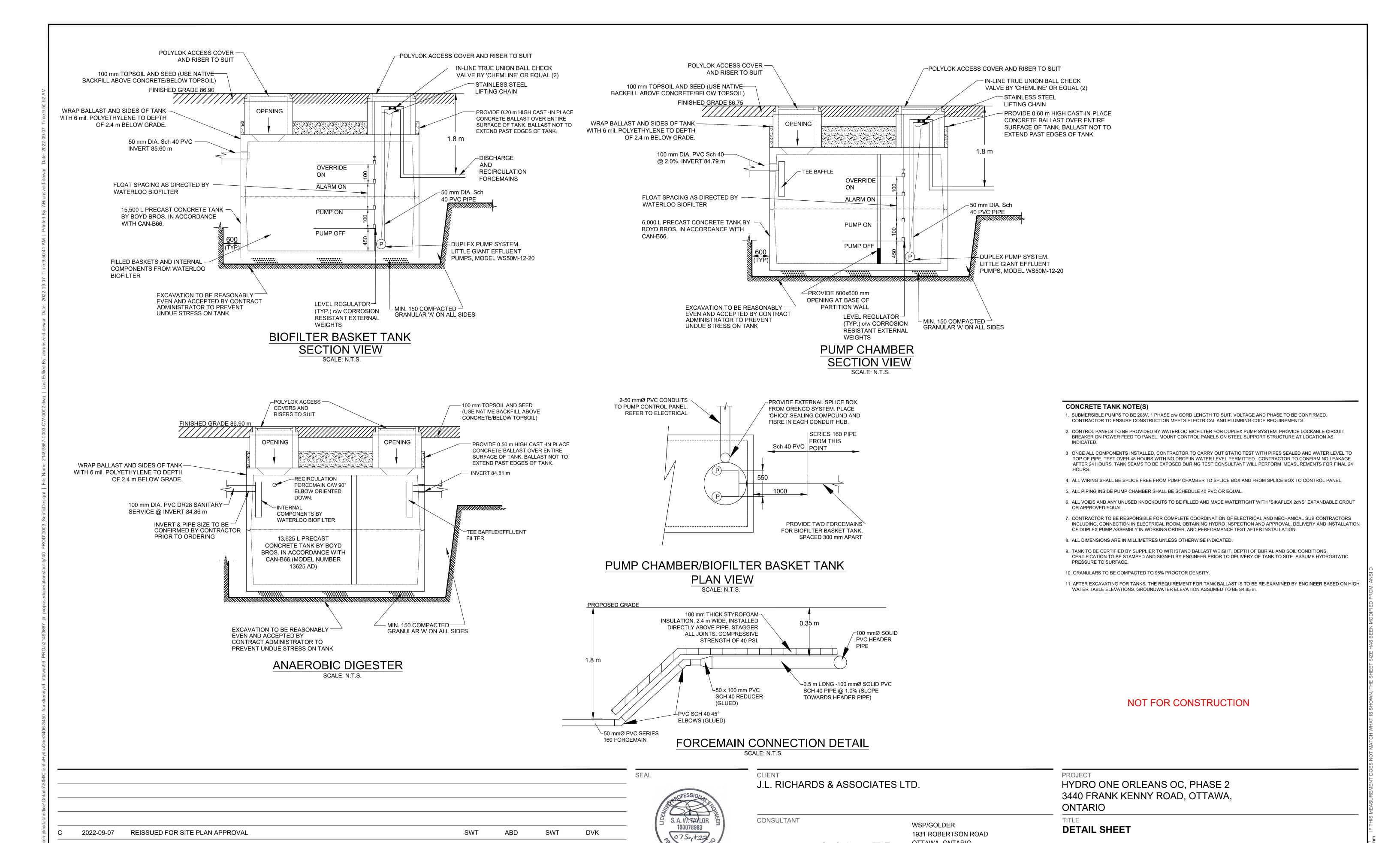


APPENDIX B

Figures







2022-05-20

2022-04-14

REV. YYYY-MM-DD DESCRIPTION

ISSUED FOR SITE PLAN APPROVAL

ISSUED FOR CLIENT REVIEW

SWT

SWT

SWT

SWT

DESIGNED PREPARED REVIEWED APPROVED

ABD

DVK

DVK

PROJECT NO. CONTROL REV. **FIGURE** 0003 21493887

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CANADA

NSD GOLDER