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Environmental Restoration

Residential Development 1040 Somerset Street West

Servicing Design Brief



Prepared for: Claridge Homes

RESIDENTIAL DEVELOPMENT 1040 SOMERSET STREET WEST OTTAWA, ONTARIO

SERVICING DESIGN BRIEF

Prepared by:

NOVATECH ENGINEERING CONSULTANTS LTD. 240 Michael Cowpland Dr. - Suite 200 Ottawa, Ontario K2M 1P6

> File No.: 112191 Report Reference No.: R-2013-003 April 02, 2013 Revised: April 14, 2022

April 14, 2022

City of Ottawa
Development Review Central
Planning, Infrastructure and Economic Development
110 Laurier Avenue West
Ottawa, ON
K1P1J1

Attention: Mr. Jean-Charles Renaud

Reference: Residential Development

1040 Somerset Street West Servicing Design Brief Our File No.: 112191

Enclosed herein is the Servicing Design Brief for the proposed Residential development at 1040 Somerset Street West, located in the southeast quadrant of the Breezehill Avenue North / Somerset Street West intersection. This brief is submitted in support of the site plan application for the site and outlines how the site will be serviced with sanitary, and watermain.

Trusting this report is adequate for your purposes. Should you have any questions, or require additional information, please contact us.

Yours truly,

NOVATECH ENGINEERING CONSULTANTS LTD.

Greg MacDonald, P.Eng

5 Milane

Director, Land Development and Public Sector Infrastructure

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1.0 INTRODUCTION

Novatech has been retained to prepare a Servicing Design Brief for the proposed residential development located at 1040 Somerset Street West within the City of Ottawa. The purpose of this report is to support the site plan application for the subject development. This servicing design brief will outline how the site will be serviced with sanitary, storm and watermain; and will demonstrate that adequate municipal capacity is available within the existing infrastructure to service the development. The property is located in the southeast quadrant of the Breezehill Avenue North / Somerset Street West intersection in the City of Ottawa, as shown in **Figure 1a – Aerial Photo** and **Figure 1b – Key Plan**.

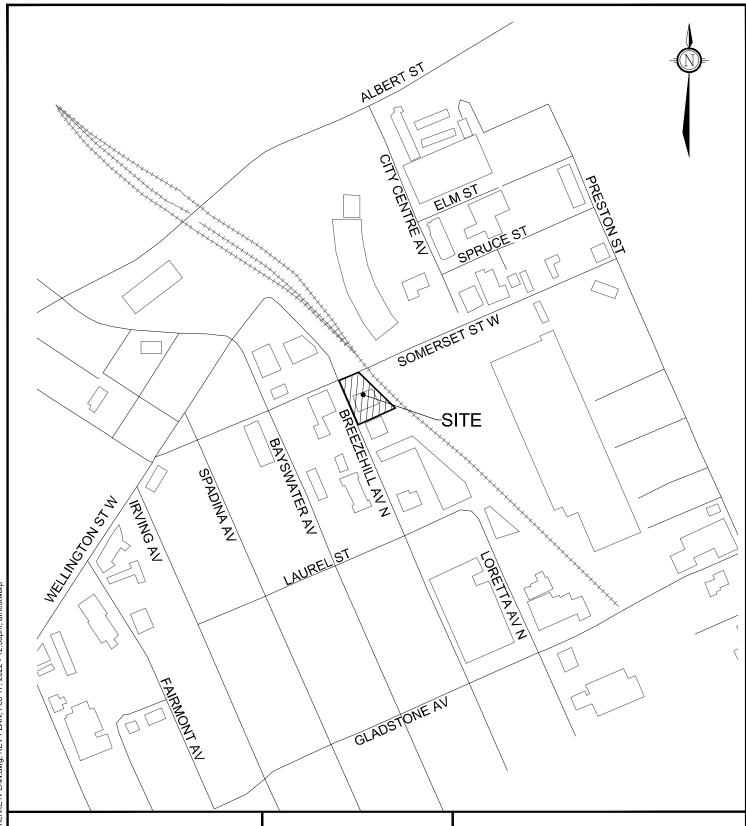
Figure 1a: Aerial Photo of Subject Site



Photo courtesy of www.bing.com/maps

The subject site is approximately 0.135 ha in area and is bound by Somerset Street West to the north, the O-Train transit corridor to the east; a meditation center and an auto repair shop (53 Breezehill Avenue North) to the south; and Breezehill Avenue N. to the west. The existing property is currently occupied by a one storey building with commercial uses.

The proposed re-development will consist of a 30-storey tower with 262 condominium units to be constructed in one phase. The building will include $105m^2$ of commercial floor space, located on the ground floor, and a total of 145 underground parking spaces will be provided on 7 levels of underground parking. **Refer to Figure 2 – Site Plan for details**. Access to the proposed site will a single two-way vehicular ramp access to the underground parking garage which will connect to Breezehill Avenue N. A copy of the topographical survey which shows the property outline is included in the back of this report. **Refer to Figure 3 – Existing Conditions**.



NOV/\TECH

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CITY OF OTTAWA 1040 SOMERSET STREET WEST

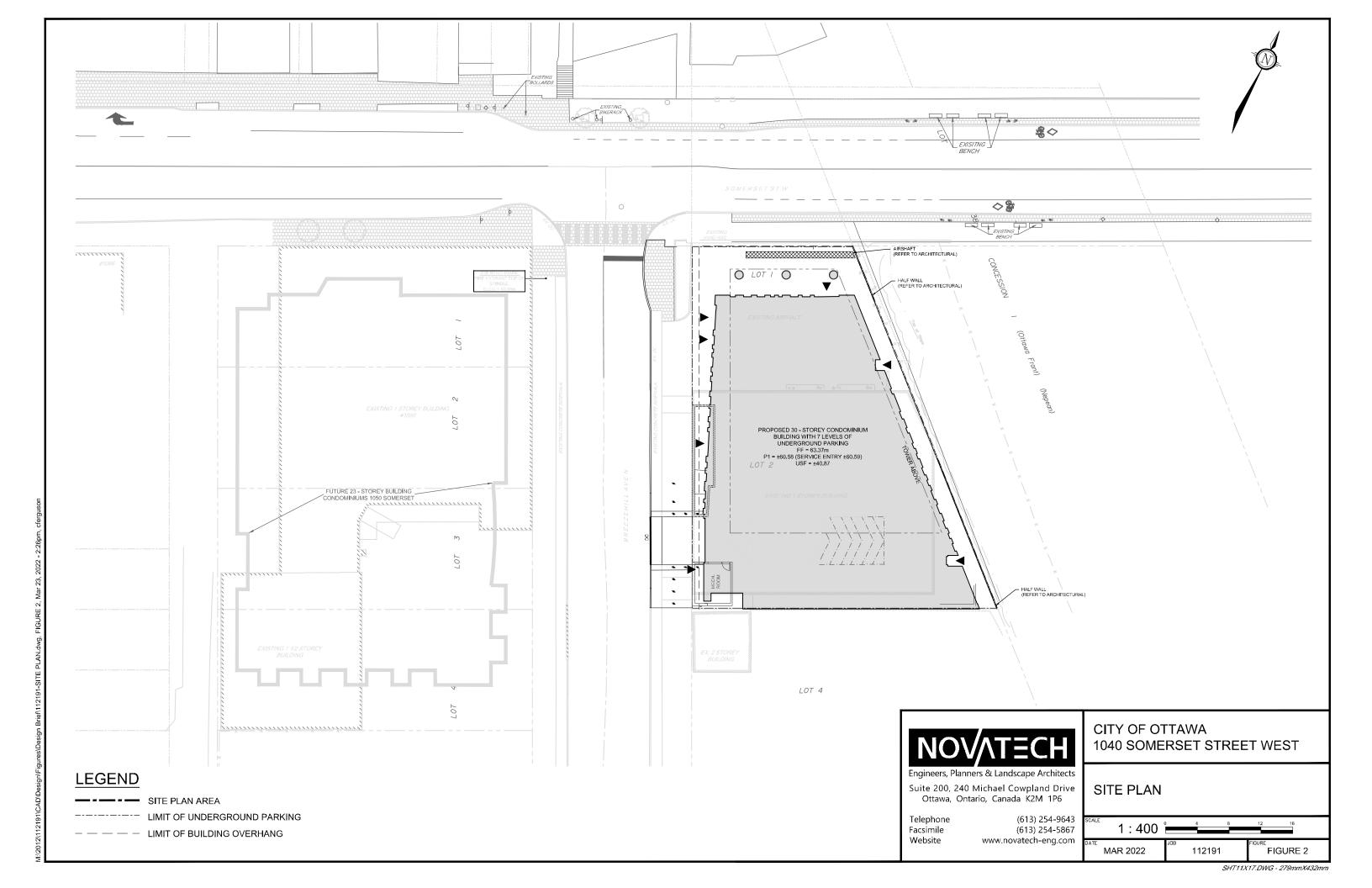
KEY PLAN

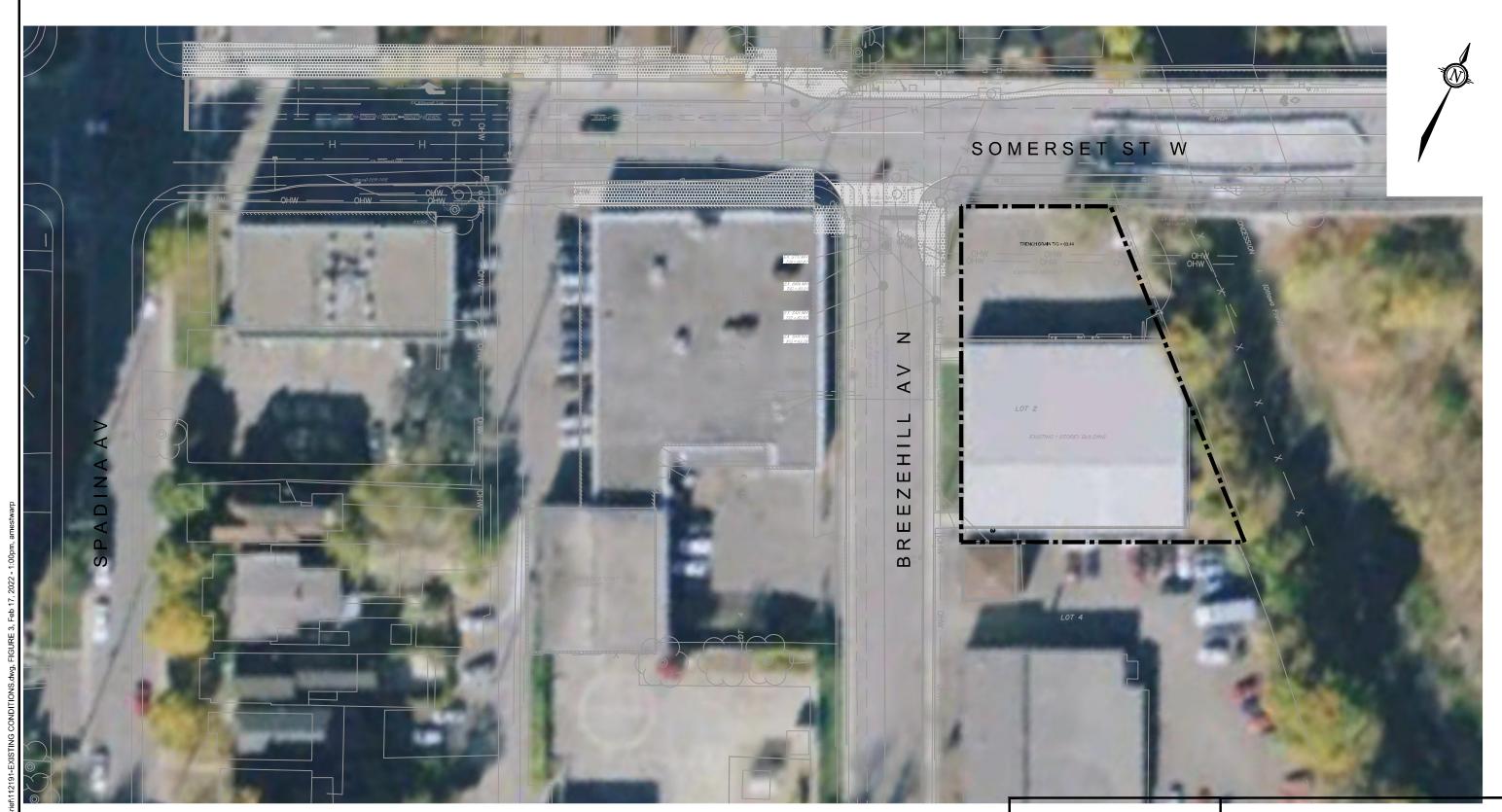
N.T.S

TE MAR 2022 JOB 112191

SHT8X11.DWG - 216mmx279mm

FIGURE 1b





LEGEND

SITE PLAN AREA

NOVATECH

Engineers, Planners & Landscape Architects Suite 200, 240 Michael Cowpland Drive Ottawa, Ontario, Canada K2M 1P6

Telephone Facsimile Website (613) 254-9643 (613) 254-5867 www.novatech-eng.com CITY OF OTTAWA 1040 SOMERSET STREET WEST

EXISTING CONDITIONS PLAN

1:500 ° 5 10 15 20 MAR 2022 JOB 112191 FIGURE 3

SHT11X17.DWG - 279mmX432mm

2.0 SITE CONSTRAINTS

A geotechnical investigation was completed by Paterson Group Inc. and a report prepared entitled 'Geotechnical Investigation, Proposed Multi-Storey Building, 1040 Somerset Street West, Ottawa, Ontario' dated October 04, 2021 (PG2674-2 Revision 4). The report included the following recommendations:

- Bedrock encountered on average 13.7-14.7m BGS, and a maximum of 27.1m BGS. Based on the RQDs of the recovered rock core, the bedrock can be classified as good to excellent in quality, generally increasing in quality with depth.
- The underside of footing of the west abutment of the Somerset Street overpass was
 observed at an approximate depth of 3.6m at the west end of the test pit, stepping down to
 an approximate depth of 4.4m at the east end of the test pit. Further, the footing was
 observed to extend outward approximately 0.3 m from the overlying abutment, with a height
 of 0.45 m.
- Groundwater was observed at depths of 3.15m to 10.01 BGS. The long-term groundwater level can also be estimated based on the observed color, moisture levels and consistency of the recovered soil samples. Based on these observations, the groundwater is expected between 5 to 6 m depth. However, groundwater levels are subject to seasonal fluctuations and therefore could vary at the time of construction.
- A temporary Ministry of Environment, Conservation and Parks (MECP) permit to take water (PTTW) may be required if more than 400,000 L/day of ground and/or surface water are to be pumped during the construction phase. At least 4 to 5 months should be allowed for completion of the application and issuance of the permit by the MECP.
- For typical ground or surface water volumes being pumped during the construction phase, typically between 50,000 to 400,000 L/day, it is required to register on the Environmental Activity and Sector Registry (EASR). A minimum of two to four weeks should be allotted for completion of the EASR registration and the Water Taking and Discharge Plan to be prepared by a Qualified Person as stipulated under O.Reg. 63/16. If a project qualifies for a PTTW based upon anticipated conditions, an EASR will not be allowed as a temporary dewatering measure while awaiting the MECP review of the PTTW application.
- As an extra measure, a monitoring program is required to ensure the lateral support zone of the watermain has not been impacted. The monitoring program will consist of installation of 2 utility monitoring points installed directly on top of the 1,372 mm diameter watermain. Further, it is recommended that two (2) inclinometers be installed adjacent to the watermain and the west shoring face for monitoring lateral deflection. In addition, the temporary shoring system should be monitored by on a daily basis until tie backs are stressed and weekly until the foundation extends above exterior finished grade. An alert level for settlement of the watermain greater than 3 mm should be assessed immediately. An action level for movement of 6 mm will require immediate investigation and possible mitigation measures. Weekly reporting including inspection findings and recommendations should be provided to the owner and the City by the geotechnical consultant.

3.0 SANITARY SEWER

There are two (2) existing 300mm diameter sanitary sewer within Breezehill Avenue N, along with the 1050mm dia. Mooney's Bay Collector. It is proposed to service the condominium development with a proposed 300 mm dia. sanitary service that will connect to the existing 300 mm dia. sanitary sewer closest to the proposed property within Breezehill Avenue North which ultimately outlets to the 1050 mm dia. Mooney's Bay Collector. Refer to the General Plan of Services drawing (112191-GP) for servicing details.

Sanitary flows for the proposed development were calculated using criteria from Section 4 of the City of Ottawa Sewer Design Guidelines and the Ontario Building Code as follows:

- Residential Average Flow = 280 L/capita/day
- 1 Bed apartment = 1.4 Person/unit
- 2 Bed apartment = 2.1 Person/unit
- Cafe Flow = 125 L/day/seat
- Residential Peaking Factor = Harmon Equation (max peaking factor = 4.0)
- Commercial Peaking Factor = 1.0
- Peak Extraneous Flows (Infiltration) = 0.33L/s/ha

The peak sanitary flow including infiltration for the proposed development was calculated to be 5.06 L/s. Since flows are directly connected to the City's Mooney's Bay Collector, we do not anticipate capacity issues within the receiving sewer system. Detailed sanitary flow calculations are provided in **Appendix A** for reference.

4.0 STORMWATER

Stormwater flows from the site are currently conveyed to the existing storm sewer system within Breezehill Avenue N., and the neighboring railway block via overland flows. As part of this development, all stormwater will be controlled on site and discharged via a 250 mm dia. storm service from the proposed condominium development that will connect to the existing 1350 mm dia. storm sewer on Breezehill Avenue North. The proposed storm service connection to the building will be equipped with a backwater valve.

The City requires that on-site stormwater management be implemented to control post-development stormwater discharge for both the 5 & 100 year storm events based on an allowable runoff coefficient (C) of 0.50, a time of concentration (t_c) of 20 minutes, and a 5-year storm event. Stormwater management will be achieved with an internal cistern within the P1 mezzanine parking level.

The site will be graded such that flows in excess of the 100-year storm event will be conveyed overland to Breezehill Avenue North, and the existing railway block as per existing conditions. Erosion and sediment control measures will be implemented during all phases of construction and inspected regularly.

A detailed stormwater management report addressing these requirements is also submitted under separate cover as part of the site plan application.

5.0 WATERMAIN

The subject property is within the City of Ottawa 1W pressure zone. There is an existing 150mm diameter local watermain, and a 1350mm diameter trunk watermain within the Breezehill Avenue North right-of-way. The proposed development includes a three (3) 150mm watermain connections. One connection is for the commercial feed, and the remaining two (2) are for the residential development. As per the City of Ottawa Technical Bulletin ISDTB-2014-02, the water services will be separated by an isolation valve in the right-of-way. The proposed building is sprinklered and equipped with a Siamese connection located near the parking entrance and is within 45m of a fire hydrant. Refer to the General Plan of Services drawing (112191-GP) for servicing details.

Water demand calculations have been calculated using criteria from Section 4 of the City of Ottawa Water Distribution Guidelines and the Ontario Building Code. The required fire demand was calculated using the Fire Underwriters Survey (FUS) Guidelines. The water demand and fire flow calculations are provided in **Appendix B** for reference. A summary of the water demand and fire flows are provided in **Table 4.1**.

Table 4.1: Domestic Water Demand Summary

Population	Commercial Area (m²)	Ave. Daily Demand (L/s)	Max. Daily Demand (L/s)	Peak Hour Demand (L/s)	Fire Flow (L/s)
452	105	1.50	3.72	8.15	100

This water demand information was submitted to the City for boundary conditions from the City's water model. The proposed boundary conditions from the City assumes that the site will connect to the 150mm dia. watermain in Breezehill Ave. which is in the 1W pressure zone of the City of Ottawa water distribution network. Refer to **Table 4.2** for a summary of the proposed boundary conditions and hydraulic analysis.

Table 4.2 Water Boundary Conditions and Hydraulic Analysis Summary

Criteria	Head (m)	Pressure ¹ (psi)	Pressure Requirements (psi)
Connection 1 (150mm dia. Bre			
Max HGL	115.1	73.57	< 80psi
Min HGL	107.3	62.48	> 40psi
Max Day + Fire Flow	86.6	33.04	> 20psi

¹Pressures based on proposed finished floor elevation of 63.37m

These boundary conditions were used for analyzing the performance of the proposed and existing watermain systems for three theoretical conditions:

- 1) High Pressure check under Average Day conditions
- 2) Peak Hour demand
- 3) Maximum Day + Fire Flow demand.

The hydraulic analysis indicates that the system can provide adequate pressures and flow to meet the domestic and fire flow requirements for the site. Refer to **Appendix B** for detailed water demand calculations, and City of Ottawa boundary conditions.

6.0 CONCLUSIONS

Based on the foregoing, adequate sanitary, and water services are available to support this development.

NOVATECH ENGINEERING CONSULTANTS LTD.

Prepared by:

Anthony Mestwarp, P.Eng. Project Engineer

Reviewed by:

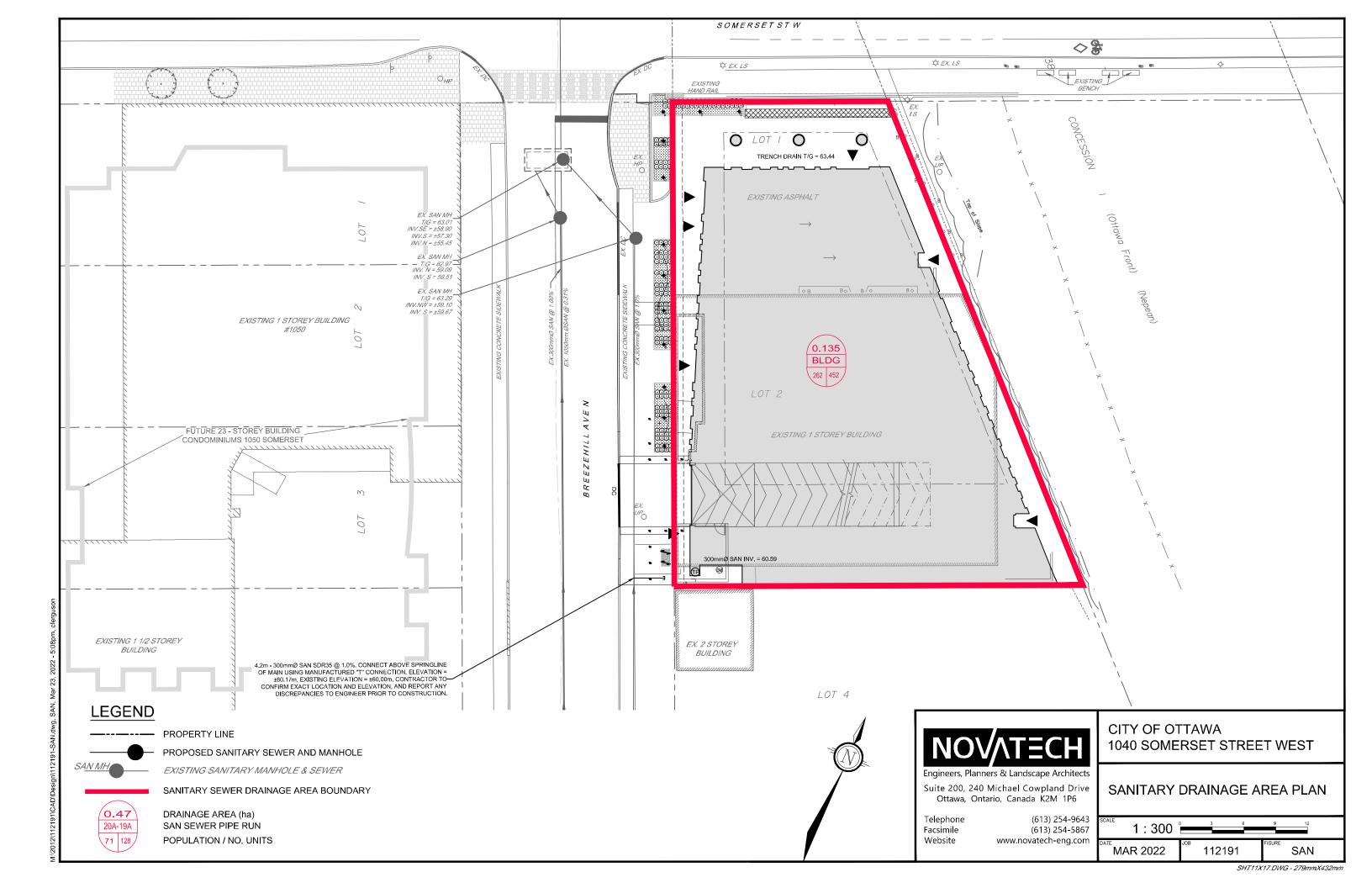
G.J. MacDONALD TO April 14, 2022

April 14, 2022

April 14, 2022

Greg MacDonald, P.Eng.
Director, Land Development
and Public Sector Infrastructure

APPENDIX A Sanitary



SANITARY SEWER DESIGN SHEET

Novatech Project #: 112191 Project Name: 1040 Somerset Street West Date Prepared: 2/10/2022

Date Prepared: 210/2022

Date Revised:
Input By: Anthony Mestwarp
Reviewed By: Greg MacDonald

Drawing Reference: 112191- SAN

Legend:

PROJECT SPECIFIC INFO
USER DESIGN INPUT
CUMULATIVE CELL
CALCULATED DESIGN CELL OUTPUT



LOCATIO	N								DEMAN	ID										DESIGN CAF	PACITY			
					RESIDEN	TIAL FLOW				COMMERC	CIAL FLOW			EXTRANEOUS F	FLOW				PROPOSED	SEWER PIP	E SIZING / DE	ESIGN		
AREA	FROM MH	TO MH	1 Bed Apartment	2 Bed Apartment	POPULATIO N (in 1000's)	PEAK FACTOR M	AVG POPULATION FLOW (L/s)	PEAKED DESIGN POP FLOW (L/s)	SEATS	DESIGN COMMERICAL FLOW (L/s)	COMMERICAL PEAK FACTOR	PEAKED COMMERCIAL FLOW	Total Area (ha.)	Accum. Area (ha.)	DESIGN EXTRAN. FLOW (L/s)	TOTAL DESIGN FLOW (L/s)	PIPE LENGTH (m)	PIPE SIZE (mm) AND MATERIAL	PIPE ID ACTUAL (m)	ROUGH. (n)	DESIGN GRADE (%)	CAPACITY (L/s)	FULL FLOW VELOCITY (m/s)	Qpeak Desigr / Qcap
	•									•	BREEZEHILL AVE	NUE	•						•					
BLDG	BLDG	MAIN	140	122	0.452	3.40	1.47	4.98	25.000	0.04	1.00	0.04	0.14	0.14	0.04	5.06	4.2	300 PVC	0.305	0.013	1.00	100.9	1.38	5.0%
Design Parameters: 1. Residential Flows -1 Bed Apartment -2 Bed Apartment 2. Commercial Flow -Cafe 3. q Avg capita flow 4. M = Harmon Formula (maximum 5. K = 6. Commercial Peak Factor -area > 20% of development -area < 20% of development 7. Extraneous Flows =	2.1 125 280 of 4.0) 0.8 1.5	5	nit																oefficient of rou (m²) imenter (m)	ghness (0.01	3)			

Page 1 of 1

APPENDIX B Water



1040 SOMERSET STREET HYDRAULIC ANALYSIS

JOB NO. 112191 DATE PREPARED: JANUARY 2022

Table 1 Water Demand										
		Unit T	ype			Tota	al Demand (L/s)			
Use	Retail Area (Seats)	1 Bed Apartment	2 Bed Apartment	Total Units	Total Population	Avg Day	Max. Daily	Peak Hour		
Residential		140	122	262	452	1.46	3.66	8.06		
Commercial	25					0.04	0.05	0.10		
Total	25	140	122			1.50	3.72	8.15		

Design Parameters:

- 1 Bed Apartment
- 2 Bed Apartment
2.1 persons/unit

City of Ottawa Water Distribution Guidelines

- Average Domestic Flow 280 L/c/day L/person/day

- Café 125 L/day/seat (assume 1 seat/4m²)

Residential Peaking Factors City of Ottawa Water Distrubution Guidelines:

Conditions	Peaking Factor		Units
Maximum Day	2.5	x avg day	L/c/day
Peak Hour	2.2	x max day	L/c/day

112191 FUS

FUS - Fire Flow Calculations

As per 1999 Fire Underwriter's Survey Guidelines

Novatech Project #: 112191

Project Name: 1040 Somerset Street West

Date: 1/20/2022
Input By: Curtis Ferguson
Reviewed By: Greg MacDonald

Legend

Input by User

Engineers, Planners & Landscape Architects

No Information or Input Required

Building Description: 32 Storey Mixed-Use Building

Fire Resistive Construction

Step		Choose		Value Used	Total Fire Flow (L/min)	
	la	Base Fire Flo	W	8.8141		
	Construction Ma			Multi	piler	
1	Coefficient related to type of construction	Wood frame Ordinary construction Non-combustible construction Modified Fire resistive construction (2 hrs) Fire resistive construction (> 3 hrs)	Yes	1.5 1 0.8 0.6 0.6	0.6	
	Floor Area	Fire resistive construction (> 3 firs)	res	0.0		
2	A	Building Footprint (m²) Number of Floors/Storeys Protected Openings (1 hr) Area of structure considered (m²)	1250.7 32 Yes	FLOOR #4=129 FLOOR #3 = 12 FLOOR #2=129	250.7	
	F	Base fire flow without reductions F = 220 C (A) ^{0.5}	_			6,000
		Reductions or Surc	harges			
	Occupancy haza	ard reduction or surcharge		Reduction/	Surcharge	
3	(1)	Non-combustible Limited combustible Combustible Free burning	Yes	-25% -15% 0% 15% 25%	-15%	5,100
	Sprinkler Reduc	Rapid burning		Redu	ction	
4	(2)	Adequately Designed System (NFPA 13) Standard Water Supply Fully Supervised System	Yes Yes Yes	-30% -10% -10% nulative Total	-30% -10% -10%	-2,550
	Exposure Surch	arge (cumulative %)	-		Surcharge	
North Side East Side South Side West Side		North Side East Side South Side	20.1 - 30 m 10.1 - 20 m 0 - 3 m 20.1 - 30 m Cun	nulative Total	10% 15% 25% 10% 60%	3,060
		Results				
	(4) - (6) - (7)	Total Required Fire Flow, rounded to nea	rest 1000L/mir	1	L/min	6,000
6	(1) + (2) + (3)	(2,000 L/min < Fire Flow < 45,000 L/min)		or or	L/s USGPM	100 1,585
7	Storage Volume	Required Duration of Fire Flow (hours) Required Volume of Fire Flow (m ³)			Hours m ³	2 720

From: Wu, John < John.Wu@ottawa.ca>
Sent: Tuesday, February 15, 2022 9:01 AM

To: Anthony Mestwarp <a.mestwarp@novatech-eng.com>

Subject: RE: 112191 - Boundary Conditions Request - 1040 Somerset Street

Here is the updated one on 150mm water main:

The following are boundary conditions, HGL, for hydraulic analysis at 1040 Somerset Street (zone 1W) assumed to be connected to the 152 mm watermain on Breezehill Avenue (see attached PDF for location).

Minimum HGL: 107.3 m Maximum HGL: 115.1 m

Max Day + Fire Flow (100 L/s): 86.6 m

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

Thanks.

John

From: Anthony Mestwarp <a.mestwarp@novatech-eng.com>

Sent: February 14, 2022 1:51 PM
To: Wu, John < John. Wu@ottawa.ca >

Cc: Curtis Ferguson < <u>c.ferguson@novatech-eng.com</u>>

Subject: RE: 112191 - Boundary Conditions Request - 1040 Somerset Street

CAUTION: This email originated from an External Sender. Please do not click links or open attachments unless you recognize the source.

ATTENTION : Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.

Hi John,

It is my understanding that the existing watermain in Breezehill Ave. fronting our development is a 152mm, and not a 200 (as depicted below).



Can you please confirm, and let us know if the below analysis is accurate.

Thanks,

Anthony Mestwarp, **P.Eng.**, Project Engineer | Land Development Engineering **NOVATECH** Engineers, Planners & Landscape Architects

240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 Ext. 216 | Fax: 613.254.5867 The information contained in this email message is confidential and is for exclusive use of the addressee.

From: Wu, John < <u>John.Wu@ottawa.ca</u>>
Sent: Monday, February 14, 2022 8:26 AM

To: Curtis Ferguson < c.ferguson@novatech-eng.com >

Subject: RE: 112191 - Boundary Conditions Request - 1040 Somerset Street

Here is the result:

****The following information may be passed on to the consultant, but do NOT forward this e-mail directly.****

The following are boundary conditions, HGL, for hydraulic analysis at 1040 Somerset Street (zone 1W) assumed to be connected to the 203 mm watermain on Breezehill Avenue (see attached PDF for location).

Minimum HGL: 107.3 m Maximum HGL: 115.1 m

Max Day + Fire Flow (100 L/s): 103.4 m

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

Thanks.

John

From: Curtis Ferguson

Sent: Friday, January 21, 2022 1:01 PM

To: john.wu@ottawa.ca

Cc: Greg MacDonald <g.Macdonald@novatech-eng.com>; Anthony Mestwarp <a.mestwarp@novatech-eng.com>

Subject: 112191 - Boundary Conditions Request - 1040 Somerset Street

Good Afternoon John,

Requesting boundary conditions for 1040 Somerset Street. Total demands and fire flows are listed below;

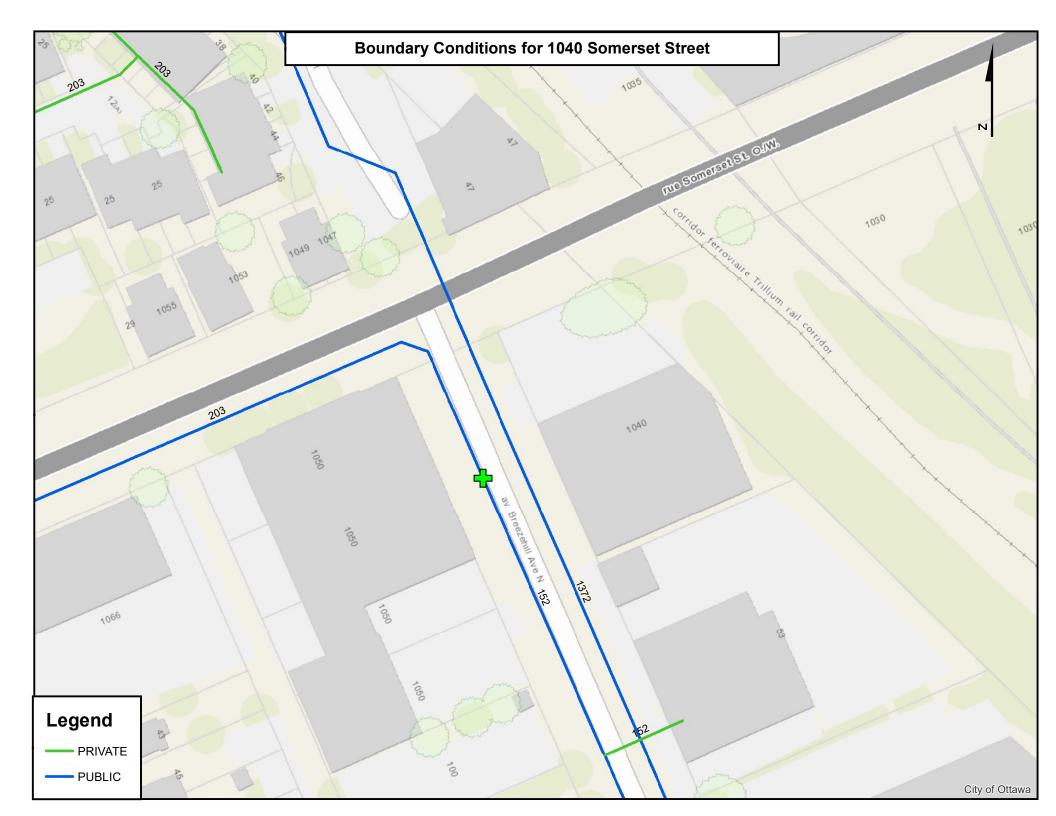
Average Daily Demand: 1.50 L/s
 Max Daily Demand: 3.72 L/s
 Peak Hour Demand: 8.15 L/s
 Fire Flow (FUS): 100 L/s

I've also attached a PDF with proposed connection locations. Please advise if you require anything else.

Curtis Ferguson, B.A.Sc., E.I.T. | Land Development

NOVATECH Engineers, Planners & Landscape Architects

240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 EXT: 331 | Fax: 613.254.5867 The information contained in this email message is confidential and is for exclusive use of the addressee.



APPENDIX C Servicing Study Guidelines Checklist



Project Name: 1040 Somerset Street West Project Number: 112191

4.1 General Content	Addressed (Y/N/NA)	Section	Comments
Executive Summary (for larger reports only).	NA		
Date and revision number of the report.	Υ	Cover	
Location map and plan showing municipal address,	Υ		Figures 1, 2 and 2
boundary, and layout of proposed development.	Y		Figures 1, 2 and 3
Plan showing the site and location of all existing	Υ		Figures 2 and 3
Development statistics, land use, density, adherence to			
zoning and official plan, and reference to applicable	V	1.0	
subwatershed and watershed plans that provide context	Υ	1.0	
to which individual developments must adhere.			
Summary of Pre-consultation Meetings with City and	N		
other approval agencies.	IN		
Reference and confirm conformance to higher level			
studies and reports (Master Servicing Studies,			
Environmental Assessments, Community Design Plans),	Υ	2.0 - 5.0	
or in the case where it is not in conformance, the	Y	2.0 - 5.0	
proponent must provide justification and develop a			
defendable design criteria.			
Statement of objectives and servicing criteria.	Υ		Addressed in Section 3.0, 4.0. 4.0.
Identification of existing and proposed infrastructure	Υ		Figures 2 and 2
available in the immediate area.	Y		Figures 2 and 3
Identification of Environmentally Significant Areas,			
watercourses and Municipal Drains potentially impacted	NA		
by the proposed development (Reference can be made	NA		
to the Natural Heritage Studies, if available).			
Concept level master grading plan to confirm existing			
and proposed grades in the development. This is			
required to confirm the feasibility of proposed			
stormwater management and drainage, soil removal and	Υ		112101 CD
fill constraints, and potential impacts to neighboring	Y		112191-GR
properties. This is also required to confirm that the	Ì		
proposed grading will not impede existing major system			
flow paths.			



Project Name: 1040 Somerset Street West Project Number: 112191

4.1 General Content	Addressed (Y/N/NA)	Section	Comments
Identification of potential impacts of proposed piped			
services on private services (such as wells and septic	NIA		
fields on adjacent lands) and mitigation required to	NA		
address potential impacts.			
Proposed phasing of the development, if applicable.	NA		
Reference to geotechnical studies and recommendations	γ	2.0	
concerning servicing.	r	2.0	
All preliminary and formal site plan submissions should			
have the following information:			
Metric scale	Υ	ALL	
North arrow (including construction North)	Υ	ALL	
Key plan	Υ	ALL	
Name and contact information of applicant	γ	ALL	
and property owner	ī	ALL	
Property limits including bearings and	Υ	ALL	
Existing and proposed structures and parking	Υ	ALL	
Easements, road widening and rights-of-way	Υ	ALL	
Adjacent street names	Υ	ALL	



Project Name: 1040 Somerset Street West Project Number: 112191

4.2 Water	Addressed (Y/N/NA)	Section	Comments
Confirm consistency with Master Servicing Study, if	Υ	5.0	Also refer to Appendix B for Hydrant Flow data.
available.	·	5.0	- The reserve to repetition 2 for the automotive automo
Availability of public infrastructure to service proposed	Υ		Figures 2 and 3
development.	·		1184163 2 4114 3
Identification of system constraints.	Υ	5.0	
Identify boundary conditions.	Υ	5.0	
Confirmation of adequate domestic supply and pressure.	Υ	5.0	
Confirmation of adequate fire flow protection and			
confirmation that fire flow is calculated as per the Fire	Υ	5.0	
Underwriter's Survey. Output should show available fire	'	5.0	
flow at locations throughout the development.			
Provide a check of high pressures. If pressure is found to			
be high, an assessment is required to confirm the	Υ	5.0	
application of pressure reducing valves.			
Definition of phasing constraints. Hydraulic modeling is			
required to confirm servicing for all defined phases of	NA		
the project including the ultimate design.			
Address reliability requirements such as appropriate	.,	- 0	
location of shut-off valves.	Υ	5.0	
Check on the necessity of a pressure zone boundary			
modification.	NA		
Reference to water supply analysis to show that major			
infrastructure is capable of delivering sufficient water for			
the proposed land use. This includes data that shows			
that the expected demands under average day, peak	Υ	5.0	
hour and fire flow conditions provide water within the			
required pressure range.			
Description of the proposed water distribution network,			
including locations of proposed connections to the			
existing system, provisions for necessary looping, and			
appurtenances (valves, pressure reducing valves, valve	Υ	5.0	
chambers, and fire hydrants) including special metering			
provisions.			
Description of off-site required feedermains, booster	1		
pumping stations, and other water infrastructure that			
will be ultimately required to service proposed	NA		
development, including financing, interim facilities, and	INA.		
timing of implementation.			
Confirmation that water demands are calculated based			
on the City of Ottawa Design Guidelines.	Υ	5.0	
Provision of a model schematic showing the boundary			
conditions locations, streets, parcels, and building	N		Figure 3 shows main.
locations for reference.	18		riguic 3 silows main.



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4.3 Wastewater	Addressed (Y/N/NA)	Section	Comments
Summary of proposed design criteria (Note: Wet-			
weather flow criteria should not deviate from the City of			
Ottawa Sewer Design Guidelines. Monitored flow data	Υ	3.0	
from relatively new infrastructure cannot be used to			
justify capacity requirements for proposed			
Confirm consistency with Master Servicing Study and/or	.,	2.0	
justifications for deviations.	Υ	3.0	
Consideration of local conditions that may contribute to			
extraneous flows that are higher than the recommended	.,	2.0	
flows in the guidelines. This includes groundwater and	Υ	3.0	
soil conditions, and age and condition of sewers.			
Description of existing sanitary sewer available for	.,	2.0	
discharge of wastewater from proposed development.	Υ	3.0	
Verify available capacity in downstream sanitary sewer			
and/or identification of upgrades necessary to service			
the proposed development. (Reference can be made to	Υ	3.0	
previously completed Master Servicing Study if			
applicable)			
Calculations related to dry-weather and wet-weather			
flow rates from the development in standard MOE	Υ	3.0	
sanitary sewer design table (Appendix 'C') format.			
Description of proposed sewer network including			
sewers, pumping stations, and forcemains.	Υ	3.0	Figures 2 and 3
Discussion of previously identified environmental			
constraints and impact on servicing (environmental			
constraints are related to limitations imposed on the	N1.0		
development in order to preserve the physical condition	NA		
of watercourses, vegetation, soil cover, as well as			
protecting against water quantity and quality).			
Pumping stations: impacts of proposed development on			
existing pumping stations or requirements for new	NA		
pumping station to service development.			
Forcemain capacity in terms of operational redundancy,	NIA		
surge pressure and maximum flow velocity.	NA		
Identification and implementation of the emergency			
overflow from sanitary pumping stations in relation to	NA		
the hydraulic grade line to protect against basement	NA		
flooding.			
Special considerations such as contamination, corrosive	NA		
environment etc.	INA		



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constraints including legality of outlet (i.e. municipal driani, right-of-way, watercourse, or private property). Analysis of the available capacity in existing public infrastructure. A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns and proposed drainage patterns. Water quantity control objective (e.g. controlling post-development peak flows to pre-development level for storm events ranging from the 2 or 5 year event (dependent on the receiving sewer design) to 100 year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects. Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements. Description of stormwater management concept with facility locations and descriptions with references and supporting information. See-back from private sewage disposal systems. NA Watercourse and hazard lands setbacks. NA Watercourse and hazard since the consensual of pre-consultation with the Ontario Ministry of forniorment and the Conservation Authority that has burisdiction on the affected watershed. Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists. Storage requirements (complete with calcs) and conveyance capacity for 5 yr and 100 yr events. dentification of watercourse within the proposed development with applicable approvals. Calcilulate pre and post development peak flow rates including a description of drainage catchments in comparison to existing conditions. NA Proposed dinversion of drainage catchment areas from one outlet to another. Proposed minor and major systems including locations and proposed dimpervious areas and durinage catchments in comparison to existing conditions. NA If quantity control is not proposed, demonstration that downstre	4.4 Stormwater	Addressed (Y/N/NA)	Section	Comments
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return period storm event.	return period storm event.			



Project Name: 1040 Somerset Street West Project Number: 112191

4.4 Stormwater	Addressed (Y/N/NA)	Section	Comments
Identification of municipal drains and related approval	NA		
requirements.			
Description of how the conveyance and storage capacity	Υ	4.0	
will be achieved for the development.	T		
100 year flood levels and major flow routing to protect			
proposed development from flooding for establishing	Υ	4.0	
minimum building elevations (MBE) and overall grading.			
Inclusion of hydraulic analysis including HGL elevations.	N		
Description of approach to erosion and sediment control			
during construction for the protection of receiving	Υ	4.0	
watercourse or drainage corridors.			
Identification of floodplains – proponent to obtain			
relevant floodplain information from the appropriate			
Conservation Authority. The proponent may be required			
to delineate floodplain elevations to the satisfaction of	NA		
the Conservation Authority if such information is not			
available or if information does not match current			
conditions.			
Identification of fill constrains related to floodplain and	NA		
geotechnical investigation.			



Project Name: 1040 Somerset Street West Project Number: 112191

4.5 Approval and Permit Requirements	Addressed (Y/N/NA)	Section	Comments
Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act.	NA		
Application for Certificate of Approval (CofA) under the Ontario Water Resources Act.	N		
Changes to Municipal Drains.	N		
Other permits (National Capital Commission, Parks Canada, Public Works and Government Services Canada, Ministry of Transportation etc.)	NA		

4.6 Conclusion	Addressed (Y/N/NA)	Section	Comments
Clearly stated conclusions and recommendations.	Υ	6.0	
Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency.	NA		
All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario.	Υ	6.0	