Site Servicing and Stormwater Management Report Wilbrod Street Apartment Complex

326-332 Wilbrod St, Ottawa, Ontario



Prepared for

Dolyn Developments Inc. and Dolyn Construction Ltd. 888 Lady Ellen Place, Unit #1 Ottawa, Ontario, K1Z 5L5

SUBMISSION Rev 2 Sep 12, 2022



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1 Introduction

Jp2g Consultants Inc. was retained by Dolyn Developments Inc. and Dolyn Construction Ltd. to complete a Site Servicing and Stormwater Management Report suitable for the City of Ottawa Site Plan Control Application, for a new apartment complex development located at the southeast corner of Friel Street and Wilbrod Street Ottawa, ON.

The site is approximately **0.090 ha** in size and is bound by Wilbrod Street on the north property limit. The proposed development includes the construction of a new **470 m²** Four-storey apartment unit with a mechanical basement, and associated parking and landscaped areas.

A Pre-Consultation meeting was held with City of Ottawa staff on November 22, 2021, to determine the project constraints and requirements. The following report details the site servicing & stormwater management calculations used for capacity, water quantity and quality control in accordance with the City of Ottawa's requirements.

1.1 Design Drawings

The following reference civil design drawings are included.

- C1 Site Servicing Plan
- C2 Grading Plan
- Figure 1 Pre-Development Storm Drainage Areas
- Figure 2 Post-Development Storm Drainage Areas

1.2 Design Population

The estimated population for the proposed development is as follows using the general population densities in accordance to Table 4.2 from the City of Ottawa Sewer Design Guidelines:

Table 1: Design Population

Apartment	Design Benulation		
1 Bedroom / Bachelor Apartment Units (1.4 persons per unit)	2 Bedroom Apartment Units (2.1 persons per unit)	Design Population (persons)	
14	26	75	

2 Objective

This study will outline the servicing requirements for the development and identify the impact of the development on the existing municipal services, including water, storm and sanitary.

The stormwater management plan is to control post-development peak flows to pre-determined levels, and detain onsite, stormwater up to and including the 100-year storm event with a 25% increase of rainfall intensity (hereby referred to as 100-year* storm event) without affecting adjacent lands.

3 Stormwater Management

3.1 Pre-Development Conditions

The existing site consists of two developed residential and commercial parcels. The parcels are bounded by existing residential units on all sides.



3.2 Allowable Release Rate

Based on existing conditions the site appears to be completely hard surface, however 10% of the site was assumed to be soft surface prior to past expansions/renovations. As a result, the pre-development runoff coefficient of 0.83 an allowable release rate of Q_{allowable} = 23.4 l/s was calculated for the new site, see attached Appendix B.

3.3 Post-Development Conditions

The proposed site development includes a new apartment building, asphalt parking, hard surface walkways and landscaped areas. Site storm drainage will be conveyed through the new on-site storm sewer and connect to the existing **375mm** storm sewer on Wilbrod Street. Flows will be managed to limit the 100-year post-development flow rate to the pre-development 5-year release rate identified in section 3.2.

The site development area is approximately **0.090** ha with a post-development average weighted run-off coefficient of **C = 0.75** and **C = 0.84** for the 5-year and 100-year* storm events, respectively. Refer to calculations in **Appendix B**. Stormwater management techniques are required to reduce peak flows from the area, given that post-development peak flows will exceed the pre-development allowable release rate of **23.4** I/s.

3.4 Storm Sewer Pipe Design

Pipe diameter sizing was based on the **5-year** and **100-year** storm event, in accordance with City requirements. Under 5-year conditions, the storm sewers are not in surcharged conditions (i.e. flow/capacity <100%).

3.5 Stormwater Quality Control

No stormwater quality control will be provided for this development.

3.6 Stormwater Quantity Control

Drainage areas B2 and B3, North and West property frontage, parking lot and side access areas will all flow uncontrolled. Refer to **Figure 2**.

Table 2: Allowable Release Rate Breakdown

ID	Description	Flows		
טו	Description	5-Year Event	100-Year Event	
	Allowable Release Rate (Section 3.2)	23.4 L/s	44.5 L/s	
1.2.1	Uncontrolled flow	7.3 L/s	14.1 L/s	
1.2.2	Net-allowable release rate	16.1 L/s	9.3 L/s*	

^{*} Note: Must be controlled to net-allowable 100-year.

To meet the net-allowable release rate, flows will be detained only on the building roof by installing parabolic weirs, (Watts Drainage Adjustable Flow Control for Roof Drains, or equivalent approved product), at all roof drains limiting the total flow from the roof to 9.3 L/s for both the 5-year and 100-year. which is equal to the net-allowable release rate. On-site storage requirements for the roof were calculated to be 2m³ for the 5-year storm event and 8m³ for the 100-year storm event. The maximum available storage for the roof was calculated to be 23m³ based on a maximum ponding depth of 150mm. Refer to Appendix F product data sheets.

No on-site storage is required in the parking area. In the event the capacity of this system is exceeded, emergency runoff will overflow north through the side access entrance to Wilbrod Street. The maximum ponding depth in parking lots is up to 350mm which is in accordance to the City of Ottawa requirements.



4 Sanitary Servicing

A new **200mm** sanitary sewer conveying flows from the new building will connect to the existing **600mm** will be constructed by others on Wilbrod Street. Refer to drawing **C1 – Site Servicing Plan**.

Based on the existing commercial and residential building on-site, pre-development peak sanitary flow for the site is calculated to be **0.11 L/s**. Post-development peak sanitary flow for the site is calculated to be **1.00 l/s**. The new **200mm** sanitary sewers at minimum **1.0%** slope will have a full flow capacity of **32.8 l/s**. The sanitary demand was calculated based on the *City of Ottawa Sewer Design Guidelines 2012* and *Technical Bulletins 2018*. Refer to **Appendix C** for full calculations.

There will be a small sanitary demand increase out letting into the municipal 600mm sanitary sewer for post-development conditions.

5 Water

A **150mm** watermain will service the new building and connect to the existing **300mm** watermain on Wilbrod Street.

The domestic water demand for the new apartment complex is calculated based on Table 4.2 of the *City of Ottawa Design Guidelines for Water Distribution*.

Existing Development Calculations:

Cumulative Maximum Daily Demand: 0.03 l/s + 0.09 L/s = 0.12 L/s

Cumulative Maximum Hour Demand: 0.06 l/s + 0.16 L/s = 0.22 L/s

See calculation breakdown below.

Commercial Parcel

- Gross Commercial Area = 0.06 hectares
- Maximum Day Factor = 1.5
- Maximum Hour Factor = 1.8
- Average daily demand for commercial = 28,000 L/ha/day
- Day = 8 hours

Average Daily Demand: 28,000 L/ha/day x 0.06 ha = 0.06 L/s

8 hrs/day x 3600 s/hr

Maximum Daily Demand: 0.06 L/s x 1.5 = 0.09 L/sMaximum Hour Demand: 0.09 L/s x 1.8 = 0.16 L/s

Residential Parcel

- Average daily demand = 280 l/capita/day
- Operational Hours = 24 hours
- Maximum occupancy = 4 persons (residents)
- Maximum Day Factor = 2.5
- Maximum Hour Factor = 2.2

Average Daily Demand: 280 l/capita/day x 4 residents = 0.013 l/s 24 hrs/day x 3600 s/hr

Maximum Daily Demand: 0.013 l/s x 2.5 = 0.03 l/s Maximum Hour Demand: 0.03 l/s x 2.2 = 0.06 l/s



New Development Calculations:

• Average daily demand = 280 l/capita/day

• Operational Hours = 24 hours

• Maximum occupancy = 75 persons (residents)

• Maximum Day Factor = 2.5

• Maximum Hour Factor = 2.2

Average Daily Demand: 280 l/capita/day x 75 residents = 0.24 l/s

24 hrs/day x 3600 s/hr

Maximum Daily Demand: $0.24 \text{ l/s} \times 2.5 = 0.60 \text{ l/s}$ Maximum Hour Demand: $0.6 \text{ l/s} \times 2.2 = 1.32 \text{ l/s}$

There will be a small water demand increase drawing from the municipal **300mm** watermain for post-development conditions.

5.1 Fire Flow Demand

Based on the Fire Underwriters Survey Method, the fire flow demand for the new development is calculated to be:

Fire Flow Demand: 133.3 I/s (Refer to Appendix D- Fire Flow Calculations).

There is one (1) fire hydrant across the street on Wilbrod within 45.0m and three (3) fire hydrants along Wilbrod Street and Friel Street within 75.0m to 150.0m from the subject property. All fire hydrants are class AA and provide a cumulative fire flow contribution of **158.33** L/s which is based on Table 1 of Appendix I in Technical Bulletin ISTB-2018-02. The new building will also be equipped with an automatic sprinkler system.

As a result, the available fire flow contribution meets the fire flow demand of the new development.

Boundary conditions have been received from the City. Pressure check was performed and found ok, pressure check details are available in Appendix G.

End of Site Servicing and Stormwater Management Report.

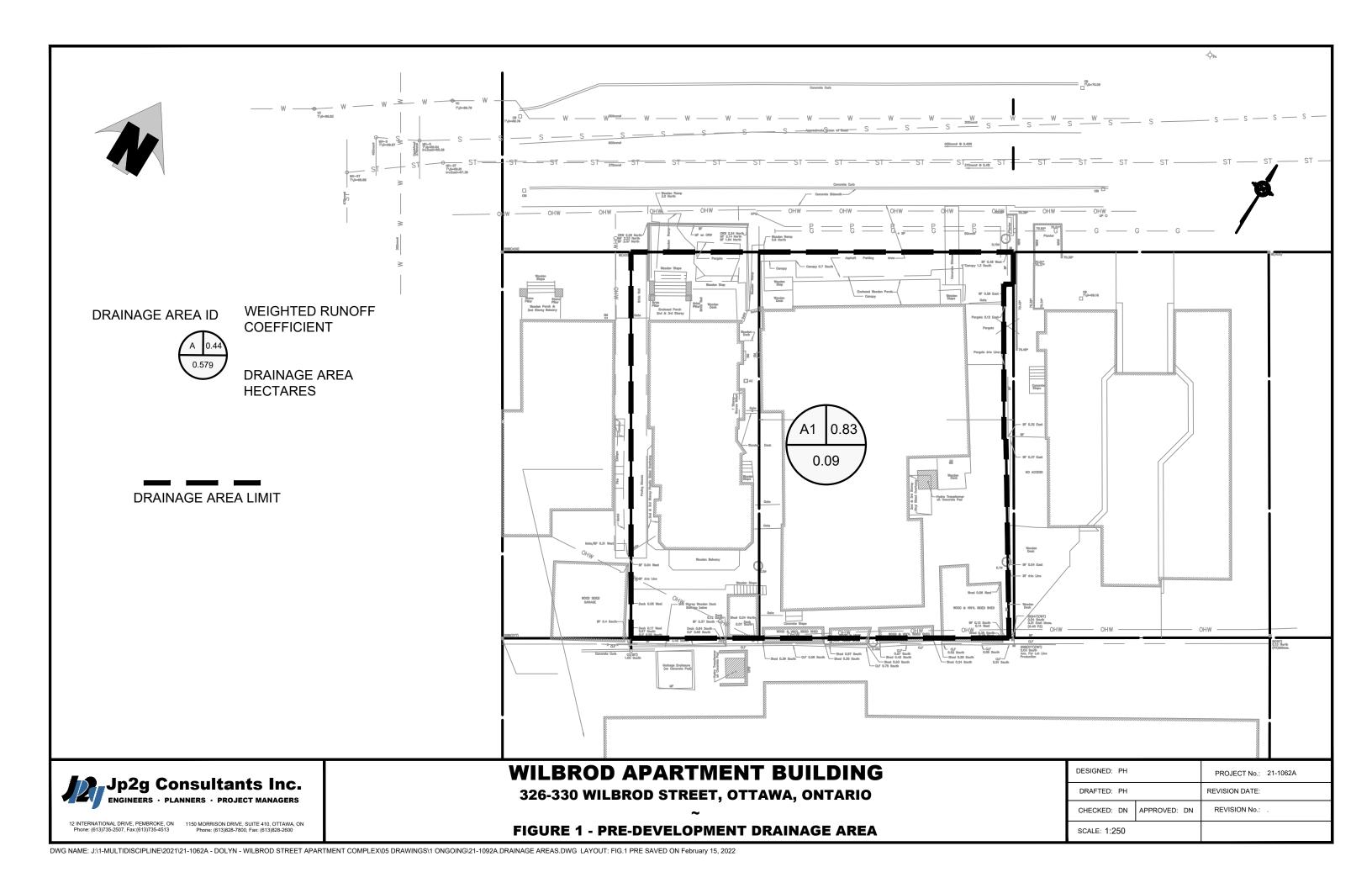
Please contact the undersigned should you require any clarification.

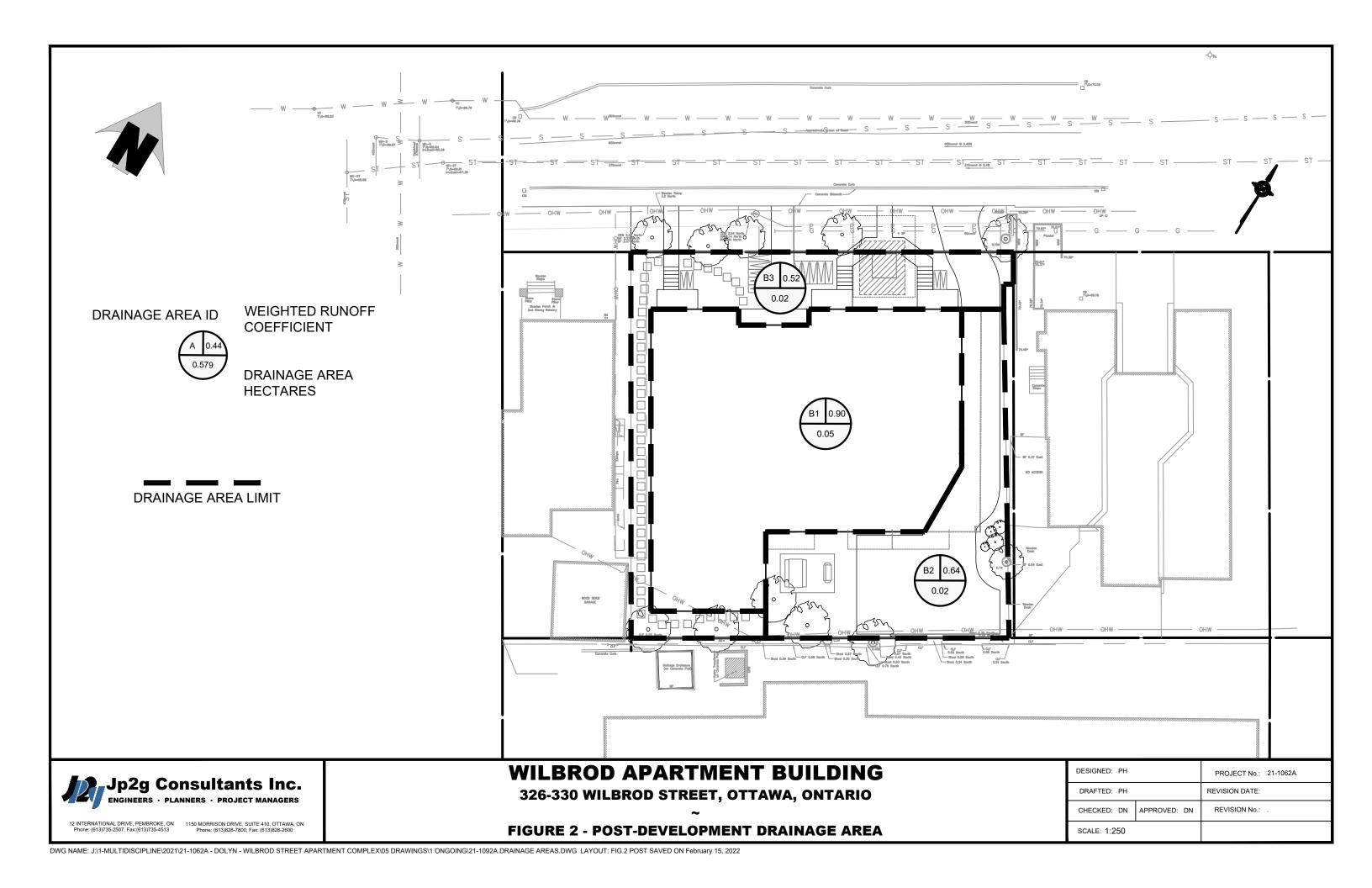
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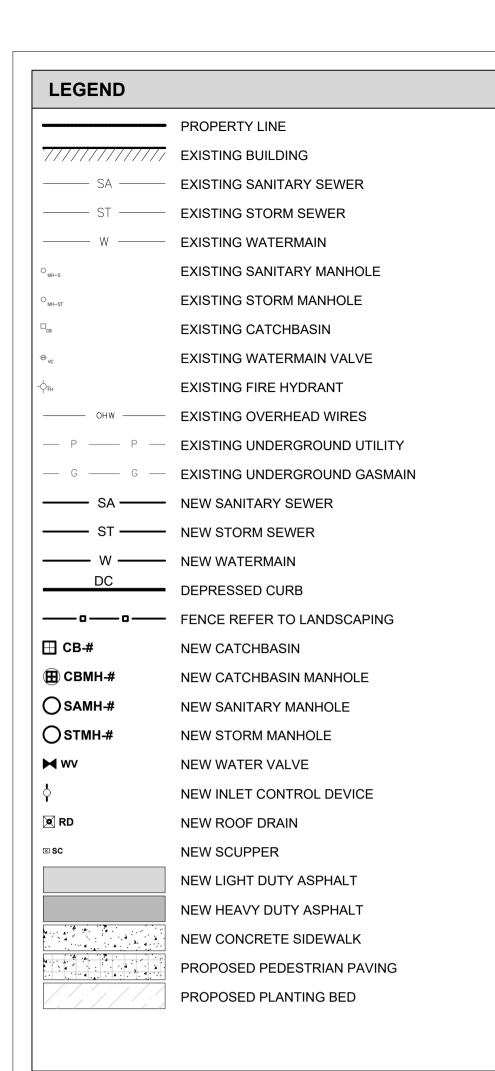


David Nguyen, P. Eng. Civil Engineer DavidN@jp2g.com 613-828-7800

Appendix A - Drawings and Figures







GENERAL NOTES

- DESIGN AND CONSTRUCTION IS TO BE IN ACCORDANCE WITH MOST RECENT ONTARIO BUILDING CODE.
- 2. THE CONTRACTOR IS RESPONSIBLE FOR CHECKING AND VERIFYING ALL DIMENSIONS WITH RESPECT TO SITE CONDITIONS AND ALL MATERIALS TO THE PROJECT. ANY DISCREPANCY SHALL BE REPORTED TO THE ENGINEER.
- 3. THIS DRAWING IS TO BE READ IN CONJUNCTION WITH ALL MATERIAL RELEVANT TO THE PROJECT.
- 4. ADDITIONAL DRAWINGS MAY BE ISSUED FOR CLARIFICATION TO ASSIST PROPER EXECUTION OF WORK. SUCH DRAWINGS WILL HAVE THE SAME MEANING AND INTENT AS IF THEY WERE INCLUDED WITH THE CONTRACT DOCUMENTS.
- 5. CONTRACTOR MUST COMPLY WITH LOCAL BY-LAWS, ONTARIO OCCUPATIONAL HEALTH AND SAFETY ACT AND ALL REGULATIONS SET BY AUTHORITIES HAVING JURISDICTION. IN CASE OF CONFLICT OR DISCREPANCY, THE MORE STRINGENT REQUIREMENTS SHALL APPLY.
- 6. CONTRACTOR RESPONSIBLE FOR OBTAINING ALL REQUIRED UTILITY LOCATES, DAYLIGHTING, INSPECTIONS, PERMITS, AND APPROVALS, INCLUDING ALL ASSOCIATED COSTS. LOCATION OF EXISTING UTILITIES ARE APPROXIMATE ONLY AND BASED ON BEST AVAILABLE INFORMATION.

EROSION AND SEDIMENT CONTROL NOTES

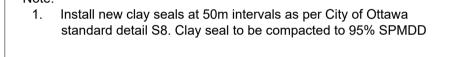
- 1. THE CONTRACTOR SHALL IMPLEMENT BEST MANAGEMENT PRACTICES TO PROVIDE FOR PROTECTION OF THE AREA DRAINAGE SYSTEM AND THE RECEIVING WATER COURSE, DURING CONSTRUCTION ACTIVITIES; THIS INCLUDES LIMITING THE AMOUNT OF EXPOSED SOIL, INSTALLING SILT FENCES AND OTHER EFFECTIVE SEDIMENT TRAPS, AND INSTALLING AND MAINTAINING MUD MATS FOR OUTGOING CONSTRUCTION TRAFFIC DURING CONSTRUCTION ACTIVITIES.
- 2. PREVENT SOIL LOSS DURING CONSTRUCTION (BY STORM WATER RUNOFF OR WIND EROSION).
- 3. PROTECT TOPSOIL BY STOCKPILING FOR REUSE.

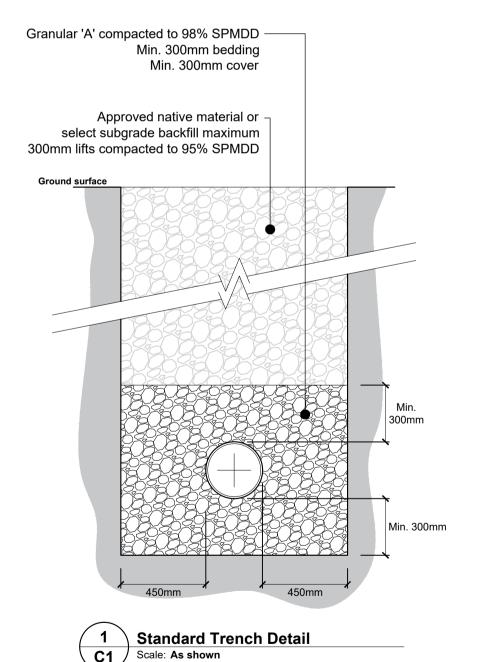
CATCH BASINS IN THE RIGHT OF WAY.

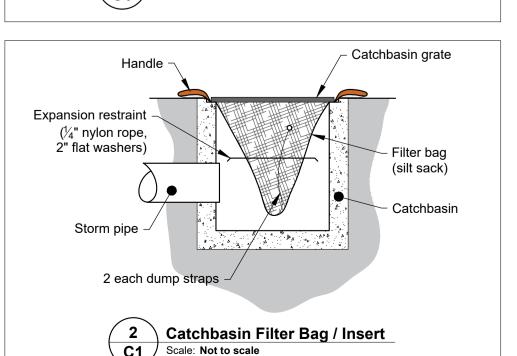
- 4. PREVENT SEDIMENTATION OF STORM SEWERS AND RECEIVING
- 5. PREVENT AIR POLLUTION FROM DUST AND PARTICULATE MATTER.6. ALL STORM MANHOLES AND CATCHBASIN MANHOLES TO HAVE
- 300mm SUMPS; ALL CATCHBASINS TO HAVE 600mm SUMPS.
 7. INSTALL FILTER BAG INSERT IN ALL STORM MANHOLES AND CATCH BASINS IMPACTED DURING CONSTRUCTION, INCLUDING
- 8. SEDIMENT AND EROSION CONTROL MEASURES MAY BE MODIFIED IN THE FIELD AT THE DISCRETION OF THE CITY OF OTTAWA INSPECTOR OR CONSERVATION AUTHORITY.
- 9. STORM WATER PUMPED INTO CITY SERVICE SHALL FLOW THROUGH A FILTER SOCK.
- 10. THE CONTRACTOR ACKNOWLEDGES THAT FAILURE TO IMPLEMENT APPROPRIATE EROSION AND SEDIMENTATION CONTROL MEASURES MAY BE SUBJECT TO PENALTIES IMPOSED BY ANY APPLICABLE REGULATORY AGENCY.

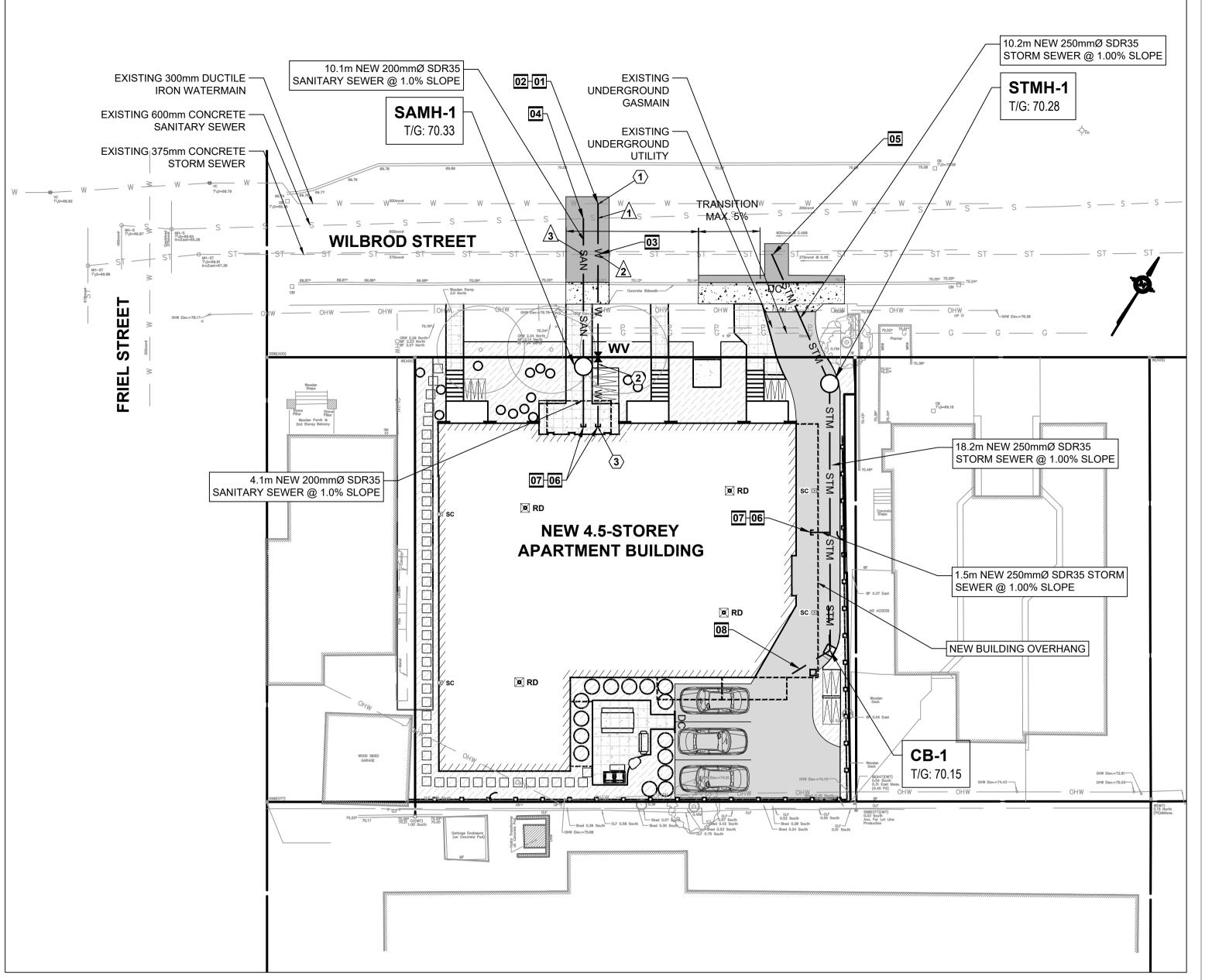
DRAWING NOTES

- ONNECT NEW WATER SERVICE TO EXISTING 305mm DUCTILE IRON WATERMAIN. APPROXIMATE TOP OF EXISTING WATERMAIN ELEVATION: 67.63. CONTRACTOR TO HYDROVAC TO CONFIRM OBVERT PRIOR TO CONSTRUCTION. WATER CONNECTIONS BY CITY; EXCAVATION, BACKFILLING AND REINSTATEMENT BY THE CONTRACTOR. CONTRACTOR TO COORDINATE WITH CITY OF OTTAWA FORCES.
- SUPPLY AND INSTALL NEW 150mm Ø PVC DR18 WATER MAIN SERVICE, MINIMUM 2.4m COVER, PROVIDE HL40 THERMAL INSULATION IN ACCORDANCE WITH CITY OF OTTAWA STANDARD DETAIL W22 WHERE 2.4m COVER CANNOT BE MET. COORDINATE NEW WATER SERVICE CONNECTION WITH MECHANICAL PLANS.
- SUPPLY AND INSTALL NEW WATERMAIN VERTICAL BENDS AND INSULATION TO CROSS UNDER EXISTING 375mm CONCRETE STORM SEWER IN ACCORDANCE WITH CITY OF OTTAWA STANDARD DETAIL W25.
- CONNECT TO EXISTING 600mm CONCRETE SANITARY SEWER WITH NEW VERTICAL RISER IN ACCORDANCE WITH CITY OF OTTAWA STANDARD DETAIL S11. PROVIDE WATERTIGHT CONNECTION. APPROXIMATE CONNECTION INVERT: 65.52. CONTRACTOR TO CONFIRM EXISTING SANITARY SEWER INVERTS PRIOR TO CONSTRUCTION.
- CONNECT TO EXISTING 375mm CONCRETE STORM SEWER WITH NEW VERTICAL RISE IN ACCORDANCE WITH CITY OF OTTAWA STANDARD DETAIL S11. PROVIDE WATERTIGHT CONNECTION. APPROXIMATE CONNECTION INVERT: 67.80. CONTRACTOR TO CONFIRM MUNICIPAL STORM SEWER INVERTS PRIOR TO CONSTRUCTION.
- CONNECT SERVICES TO INTERIOR PLUMBING 1.0m FROM BUILDING FOUNDATION. PERIMETER FOUNDATION DRAIN TO BE CONNECTED TO NEW STORM SEWER SERVICE. REFER TO MECHANICAL AND ARCHITECTURAL PLANS. CONNECTION ELEVATIONS:
 - STORM INVERT: 68.15
 - SANITARY INVERT: 68.65
- WATERMAIN OBVERT: 68.00
- SUPPLY AND INSTALL BACKFLOW VALVES ON SANITARY AND STORM BUILDING CONNECTION AS PER CITY OF OTTAWA STANDARD DETAILS \$14, AND ONE OF \$14.1 OR \$14.2.
- INSTALL 3.0m LONG 100mm Ø PERFORATED SUBDRAIN WRAPPED IN GEOTEXTILE SOCK EXTENDING FROM CB/CBMH AT PAVEMENT SUBGRADE LEVEL. PROVIDE WATERTIGHT CONNECTION.
- SUPPLY AND INSTALL WATTS RD-100 FLOW CONTROL ROOF DRAINS. MAXIMUM DISCHARGE 9.3 I/s TOTAL. REFER TO MECHANICAL FOR SPECIFIC WEIR SETTINGS.









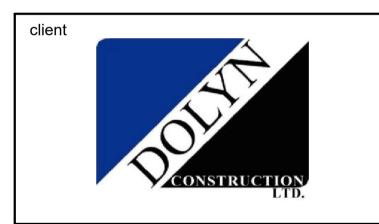
MANHOLE AND CATCHBASIN SCHEDULE								
STRUCTURE ID	TOP OF FRAME ELEVATION (m)	PIPE INVERT ELEVATION (m)	STRUCTURE DIAMETER (mm) / OPSD No.	FRAME (OPSD / CITY OF OTTAWA STANDARD)				
SAMH-1	70.33	68.61 SW / 68.59 NE	1200 / 701.010	S25 / S24				
STMH-1	70.28	68.00 NW / 68.03 SE	1200 / 701.010	S25 / S24.1				
CB-1	70.15	68.21 NW	600 x 600 / 705.010	S25 / S19				

CROSSING TABLE									
LOCATION	OVER / UNDER	INVERT	OBVERT	CLEARANCE (m)					
Á	NEW WATERMAIN / EXISTING SANITARY SEWER	67.53	65.82	1.71					
<u>^2</u>	EXISTING STORM SEWER / NEW WATERMAIN	67.70	67.20	0.50					
<u>/3</u>	NEW SANITARY SEWER / EXISTING STORM SEWER	68.52	68.18	0.34					

WATER SERVICE TABLE							
ID	DESCRIPTION	FINISHED GRADE (m)	T/O WATERMAIN (m)				
(1)	MUNICIPAL CONNECTION	70.03	67.63				
(2)	VALVE BOX	70.33	67.93				
(3)	BUILDING CONNECTION	70.40	68.00				
	NOTE: PROVIDE MINIMUM 2.4m COVER OVER T/O WATERMAIN TO WHERE MINIMUM COVER CANNOT BE MET, PROVIDE THERMA						

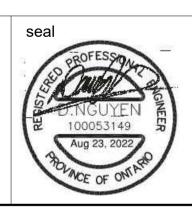






wilbrod APT. Building

326-330 WILBROD STREET, OTTAWA, ON.



drawing title

SITE SERVICING, EROSION AND SEDIMENT
CONTROL PLAN

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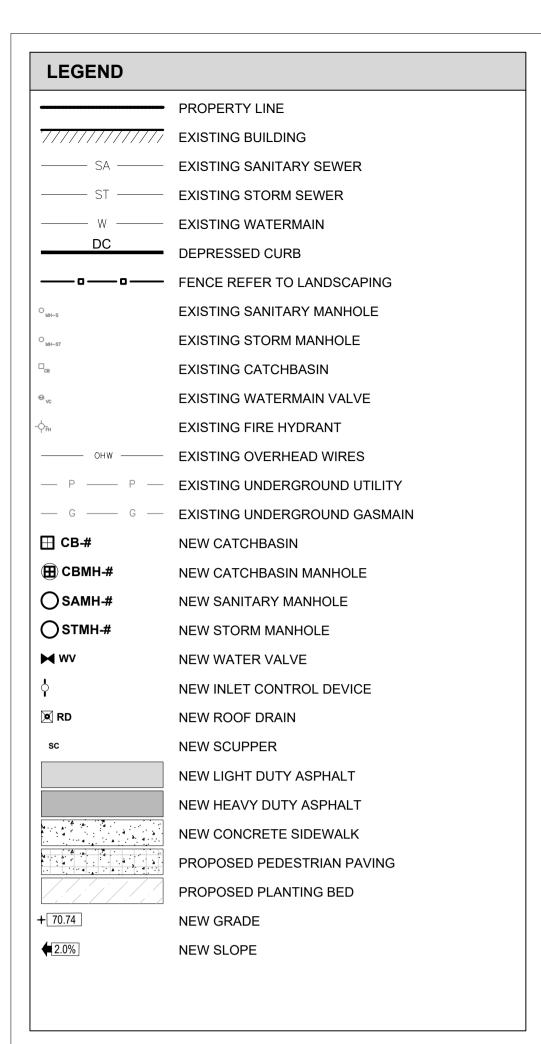
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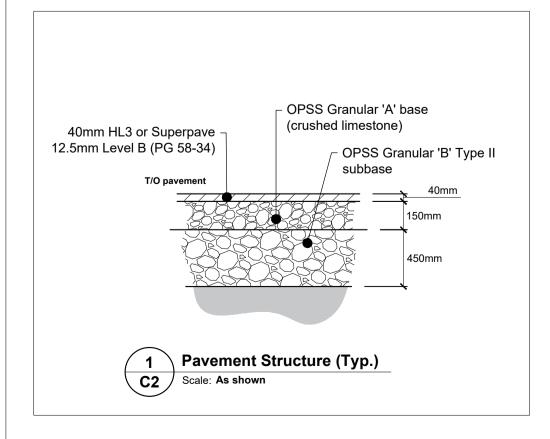
DISCREPANCIES BEFORE WORK COMMENCES.

DO NOT SCALE DRAWINGS.



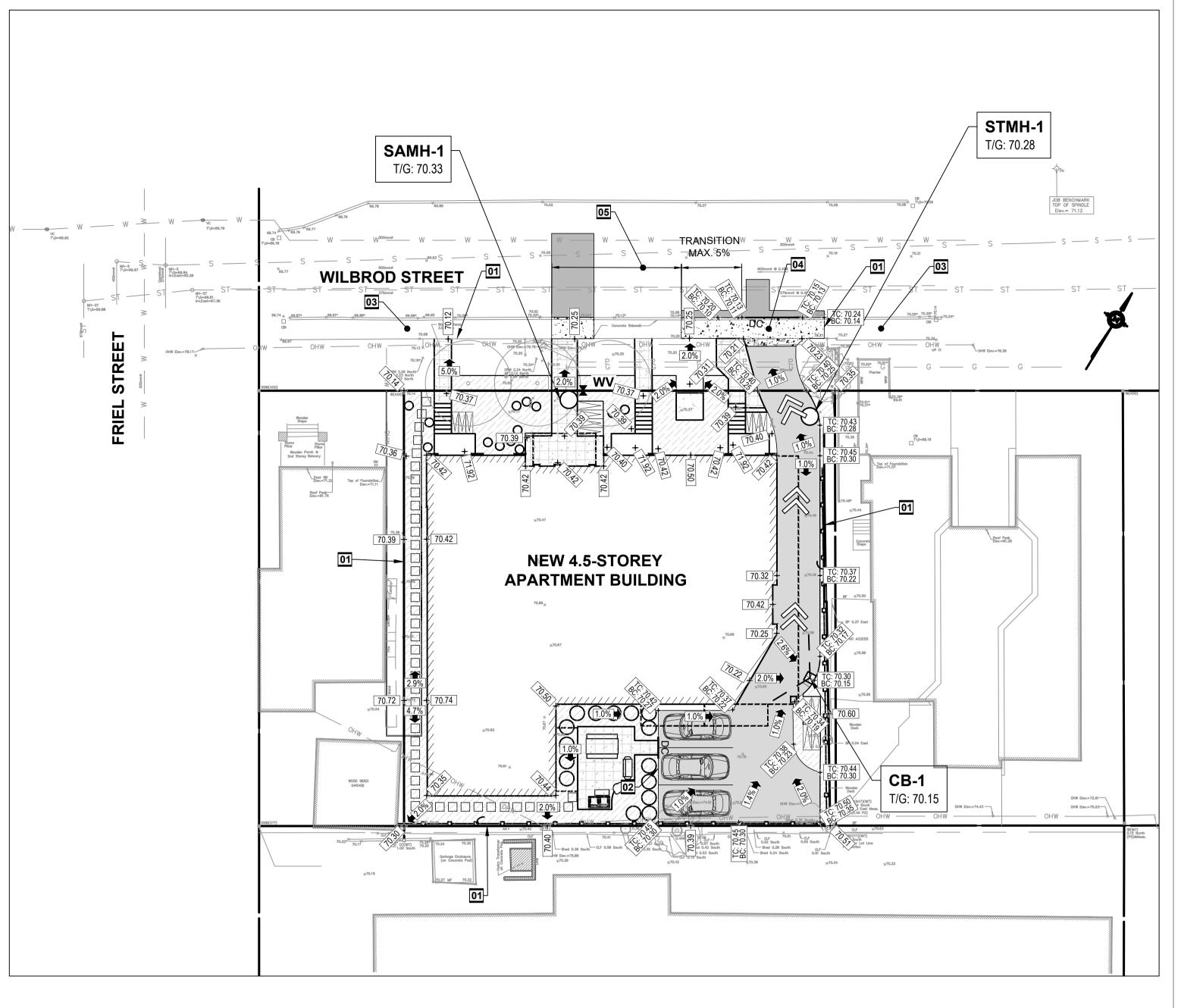
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- 7. ALL PRIVATE ACCESSES TO ROADS SHALL COMPLY WITH THE CITY'S PRIVATE APPROACH BY-LAW NO. 2003-447 AS AMENDED, OR AS APPROVED THROUGH THE SITE PLAN CONTROL PROCESS.
- 8. NO PRIVATE APPROACH SHALL BE CONSTRUCTED WITHIN 0.3 METRES OF ANY ADJACENT PROPERTY MEASURED AT THE HIGHWAY LINE, AND AT THE CURB LINE OR ROADWAY EDGE.

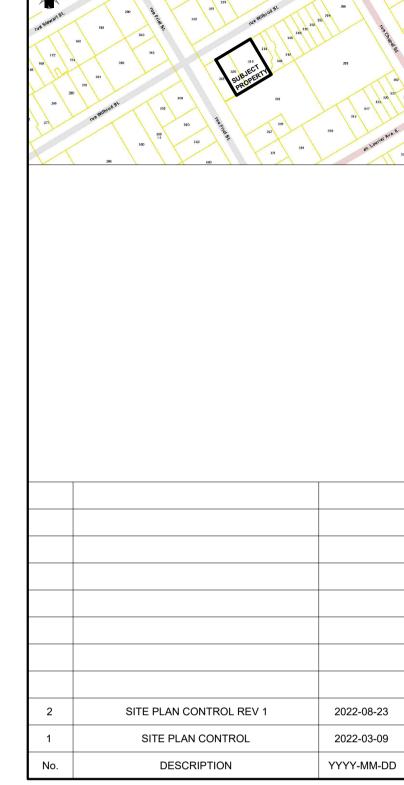


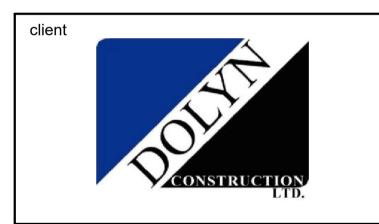
DRAWING NOTES

- MATCH EXISTING GRADES AT PROPERTY LINE AND LIMITS OF
- NEW BARRIER CURB AS PER CITY OF OTTAWA STANDARD DETAIL SC1.1.
- PROTECT EXISTING CONCRETE SIDEWALK DURING CONSTRUCTION.
- NEW CONCRETE SIDEWALK COMPLETE WITH REINFORCING MESH 150mm X 150mm, MW9.1 X MW9.1 COMPLETE WITH EXPANSION JOINT PER CITY OF OTTAWA STANDARD DETAIL SC5.
- REMOVE EXISTING DEPRESSED SIDEWALK AND REINSTATE WITH NEW 150mm RAISED SIDEWALK TO CITY STANDARDS.





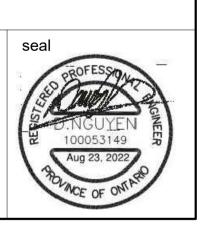




wilbrod Apt. Building

326-330 Wilbrod Street,

OTTAWA, ON.



drawing title GRADING AN	ID DRAINAGE PLAN			
scale drawn by As shown PH				
date	checked by DN			
project drawing number C2				
CONTRACTOR TO NOTIFY THE ARCH	VERIFY ALL DIMENSIONS AND ITECT OF ANY	revision	12-22-0040	

DISCREPANCIES BEFORE WORK COMMENCES.

DO NOT SCALE DRAWINGS.

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Appendix B - Stormwater Management Calculations



Appendix B - Storm Sewer Design Sheet

B.1.1 - Allowable release rate

			Area	as (m²)]		
D	Description	Type	C _{0.90}	C _{0.20}	Total (m ²)	C _{pre-5-yr}	C _{pre-100-yr} *
١	Property Grounds	uncontrolled	807	90	897	0.83	0.92
	*including 25% increase as per City of Ottawa Sewer Design Gui	delines	807	90	897	0.83	0.92
	Calculations for post-development runoff coefficient		C _{post-5-yr (col. D)}	= (column A *	0.9 + column B * (0.2) / column C	
			C _{post-100-yr} (col. E)	`	1.0 + column B * (e: 0.90 x 1.25 = 1	,	
	Calculations for average weighted runoff coefficient		C _{post-5-yr}	= ((6279*0.9)+	-(6538*0.2))/1281	7	= 0.75
			C _{post-100-yr}	= ((6279*1.0)+	-(6538*0.2*1.25))/	12817	= 0.84
	Estimated time of concentration, t_c =	10.0	minutes	***As per City o	f Ottawa Sewer De	sign Guidelines (\$	Section 5.4.5.2)
	Based on Ottawa IDF curve, i _{5-years} =	998.071/ (t _c +6.0	053) ^{0.814}				
		104.2	mm/hr				
	Based on Ottawa IDF curve, i _{100-years} =	1735.688/ (t _c +6	5.014) ^{0.820}				
		178.6	mm/hr				
	Using the Rational Method, the maximum allowable rele	ase rate is therefo	re:				
	Total Area, A =	0.09	ha				
	5-year Runoff coefficient, C =	0.90					
	Estimated time of concentration, t _c =	10.0	minutes				
	Based on Ottawa IDF curve, i _{5-years} =	998.071/ (t _c +6.0	053) ^{0.814}				
	·	104.2	mm/hr				
	$Q_{ m allowable}$	= 2.78 C x i x A					
	Q allowable (5-year		l/s	1			
	100-year Runoff coefficient, C =	1.00					
	Estimated time of concentration, t _c =	10.0	minutes				
	Based on Ottawa IDF curve, i _{100-years} =	1735.688/ (t _c +6	i.014) ^{0.820}				
	. 100 ,000	1-0	, , , , , , , , , , , , , , , , , , ,				

B.1.2 - Post-development release rate

			Are	as (m²)			
ID	Description	Туре	C _{0.90}	C _{0.20}	Total (m ²)	C _{post-5-yr}	C _{post-100-yr} *
B1	Building Roof	controlled	466	4	470	0.89	0.99
B2	Parking Lot and Side Access	uncontrolled	144	83	227	0.64	0.73
B3	North and West Property Frontage	uncontrolled	92	108	200	0.52	0.60
			702	195	897	0.75	0.84
	*including 25% increase as per City of Ottawa Sewer Design Guideline.	S	(A)	(B)	©	(D)	(E)

178.6 mm/hr

 $Q_{\text{allowable}} = 2.78 \text{ C x i x A}$ $Q_{\text{allowable (100-year)}} = 44.5 \quad \text{I/s}$

B.1.2.1 - Uncontrolled overland surface flow

Total uncontrolled area	0.043	ha	
5-year Runoff coefficient	0.59		
100-year Runoff coefficient	0.66		
Uncentralled Delegae Date Fiveer	7.2	1/0	
Uncontrolled Release Rate 5-year	7.3	l/s	2
Uncontrolled Release Rate 100-year	14.1	l/s	4

B.1.2.2 - Net-allowable release rate for storm sewers

* $\mathbf{Q}_{\text{net-allowable 100-year}}$ = 9.3 I/s $\mathbf{S} = \mathbf{O} - \mathbf{A}$ * Must be controlled to net-allowable 100-year

B.1.3 - Post-development onsite storage

B.1.3.1 - Estimated Roof detention

Total controlled area 0.047 ha
5-year Runoff coefficient 0.89

100-year Runoff coefficient 0.99

Release rate 9.3 l/s

Table 1.3.1a - 5-year estimated detention

	i abic i.o. ia o	your commuted	actorition			
_	Time	i _{5-years}	Q _{actual}	Q _{allowable}	Q _{stored}	V _{stored}
_	(minutes)	(mm/hr)	(l/s)	(l/s)	(l/s)	(m^3)
peak V _{stored} →	10	104.2	12.2	9.3	2.9	1.7
	15	83.6	9.8	9.3	0.5	0.4
	20	70.3	8.2	9.3	-1.1	-1.3
	25	60.9	7.1	9.3	-2.2	-3.3
	30	53.9	6.3	9.3	-3.0	-5.4
	35	48.5	5.7	9.3	-3.6	-7.6
	40	44.2	5.2	9.3	-4.1	-9.9
	45	40.6	4.7	9.3	-4.6	-12.3
	50	37.7	4.4	9.3	-4.9	-14.7
	55	35.1	4.1	9.3	-5.2	-17.1
	60	32.9	3.8	9.3	-5.5	-19.6

Therefore 2 m³ estimated detention

Table 1.3.1b - 100-year estimated detention

		,				
	Time	i _{100-years}	Q _{actual}	Q _{allowable}	Q _{stored}	V _{stored}
	(min)	(mm/hr)	(l/s)	(l/s)	(l/s)	(m ³)
peak V $_{\text{stored}}$ \rightarrow	10	178.6	23.2	9.3	13.9	8.3
	15	142.9	18.6	9.3	9.3	8.3
	20	120.0	15.6	9.3	6.3	7.5
	25	103.8	13.5	9.3	4.2	6.3
	30	91.9	11.9	9.3	2.6	4.7
	35	82.6	10.7	9.3	1.4	3.0
	40	75.1	9.8	9.3	0.5	1.1
	45	69.1	9.0	9.3	-0.3	-0.9
	50	64.0	8.3	9.3	-1.0	-3.0
	55	59.6	7.7	9.3	-1.6	-5.1
	60	55.9	7.3	9.3	-2.0	-7.4

Therefore 8 m³ estimated detention

B.1.4 - Site storage

		5-year required (m3)	100-year required (m3)	Ponding depth (m)	Ponding area (m2)	Max available (m3)
R	pof Detention	2	8	0.15	470	24



STORM SEWER DESIGN SHEET

	LOCATION							CONTRI	BUTING AR	EA				FLO	OW							STORM	SEWER DESIG	N			
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	29	30	31	32
Note	FROM	то	AREA ID	SEWER TYPE (Lateral or Trunk)	HARD AREA (A1) (ha)	HARD RUNOFF COEFF. (C1) ()	SOFT AREA (A2) (ha)	SOFT RUNOFF COEFF. (C2) ()	TOTAL AREA (A3) (ha)	WEIGHTED RUNOFF COEFF. (C3) ()		ACC. SECTION	TIME OF CONCEN. (Tc) (min)	RAINFALL INTENSITY 5-YR (I) (mm/hr)	RAINFALL INTENSITY 100-YR (I) (mm/hr)	FLOW 5-YR	FLOW 100- YR (L/s)	LENGTH	SLOPE	DIA.	FULL FLOW CAPACITY (L/s)	FULL FLOW vs. ACTUAL FLOW (L/s)	FULL FLOW VELOCITY (m/s)	TIME OF FLOW IN PIPE (min)	TIME OF CONCEN AFT. PIPE (min)	FALL IN PIPE SECTION (m)	COMMENTS
Parking Lot	CB-1	STMH-1	B2	Trunk	0.01	0.90	0.01	0.20	0.02	0.64	0.015	0.015	10.00	104.193	178.559	4.23	7.26	18.2	1.00%	200	32.80	13%	1.04	0.29	10.29	0.18	
School Roof	Roof	Lateral Con.	B1	Lateral	0.05	0.90	0.00	0.20	0.05	0.89	0.042	0.057	10.00	104.193	178.559	12.17	28.12	1.5	1.00%	200	32.80	37%	1.04	0.02	10.02	0.02	
Municipal Connection	STMH-1	Municipal Con.		Trunk	0.01	0.90	0.01	0.20	0.02	0.52	0.010	0.067	10.29	102.683	175.946	2.98	32.81	10.2	1.00%	200	32.80	9%	1.04	0.16	10.45	0.10	
	•		•								•				, and the second												

Notes: Rainfall Data Source: Ottawa CDA RCS 5 Year Mannings, n = 0.013



Appendix C - Sanitary Servicing Calculations

Wilbrod Street Apartment Complex



Appendix C - Sanitary Sewer Design Sheet

<u>Definitions</u> <u>Manning's Formula</u>

0.013

Q = $A*R^{2/3}*S^{1/2}/n$ (l/s), where A = Areas in Hectares (ha)

R = Hydraulic Radius (m)

S = Slope

Design Parameters*

1) Average Daily Flow = 280 L/p/day

2) Commercial/Institutional Flow = 28,000 L/ha/day

3) Maximum Residential Peak Factor = 4

4) Commercial/Institutional Peak Factor = 1.50

5) Extraneous Flow = 0.33L/s/ha

6) Minimum Velocity = 0.76 m/s

C.1.1 - Pre-Development Flow

Manning's Coefficient (n) =

	Location			Residential Flow					Commercial Flow			l	nfiltration Flow	V	Total Flow		
						Cum	ulative	Average Flow	Peak Flow	Area	ı (ha)	Peak Flow	Area	(ha)	Inf. Flow	Average Flow	Peak Flow
Note	From	То	Area (ha)	Units	Population	Area	Population	(I/s)	(I/s)	Individual	Cumulative	(I/s)	Individual	Cumulative	(I/s)	(l/s)	(l/s)
Existing Buildings	Ex.	Municipal Con.	0.03	1	4	0.03	4	0.01	0.05	0.060	0.060	0.03	0.09	0.09	0.03	0.07	0.11

C.1.2 - Post Development Flow

	Location			Residential Flow						I	nfiltration Flov	v	Total Flow			Sewer Data			
						Cumi	ulative	Average Flow	Peak Flow	Area	ı (ha)	Inf. Flow	Average Flow	Peak Flow	Dia.	Slope	Capacity	Utilization	
Note	From	То	Area (ha)	Units	Population	Area	Population	(I/s)	(l/s)	Individual	Cumulative	(l/s)	(l/s)	(l/s)	(mm)		(full) (l/s)	(%)	
Apartment	Apartment	SAMH-1	0.09	40	72	0.09	75	0.24	0.97	0.09	0.09	0.03	0.27	1.00	200	1.00%	32.8	3.1	
Municipal Connection	SAMH-1	Municipal Con.	0.09	0	72	0.09	75	0.24	0.97	0.09	0.09	0.03	0.27	1.00	200	1.00%	32.8	3.1	

^{*} City of Ottawa Sewer Design Guidelines, Section 4 - Sanitary Sewer Systems



Appendix D - Fire Flow Demand Calculations



Appendix D- Fire Flow Demand Requirements

D.1.1 - Fire Flow Demand Requirements (Fire Underwritters Survey (FUS Guidelines))

Fire Flow Formula

Estimated Fire Flow Formula: F=220*C*A^{1/2}(L/min) Designed PH Checked DN

F = Required fire flow (L/min)

C = Coefficient related to the type of construction

C_{1.5} = 1.5 for wood frame construction

C_{1.0} = 1.0 for ordinary construction

C_{0.8} = 0.8 for non-combustible construction

C_{0.6} = 0.6 for fire-resistive construction

A = Total floor area in square metres

New School Building

Design Parameters*

Type of Building Construction = Non-combustible construction Floor Area*** = 470.0

Occupancy Class = Limited combustible

Sprinkler System = Automatic sprinkler system conforming to NFPA standards with standard water supply and full supervision

Sprinkler Building Coverage = Complete building coverage

Factor of Building Coverage X = Number of Storeys = 4 Exposure Parameters*

	North	East	South	West	_
Separation Distance =	25.0	6.2	8.2	2.8	m
Length of Exposed Wall =	24.5	12.4	8.8	15	m

98.0 24.8 26.4 37.5 m-storeys (up to a maximum of 5-storeys) Length-Height Factor =

							AU	ijustinents (incre	eases or decreasi	es)					
Building Construction	Floor Area***	Coefficient	Α	B = A	\ +/- %	C =	B x %			D =	B x %				Final Adjusted Fire
g			Fire Flow (F)	Occu	pancy	Spr	inkler			Expo	sure***			Flow	Flow
	,2 ₁		(L/min)	9/	Adjusted Fire	0/	Fire Adjustment	North	East	South	West	Total Exposure	Fire Adjustment	E = B - C + D	
Non-combustible construction	(m²)		(L/IIIII)	/0	Flow(s) (L/min)	/0	Flow(s) (L/min)	North	East	South	vvest	Total Exposure	Flow(s) (L/min)	(L/min)"	(L/s)
	1,880.0	0.8	8,000.0	-0.15	6,800.0	50%	3,400.0	9%	17%	17%	23%	66%	4,488.0	8,000.0	133.3

^{*}Water Supply for Public Protection (Fire Underwriters Survey, 1999).

^{***}Including all stories



Appendix E - Pre-Consultation & Development Servicing Study Checklist



APPLICANT'S STUDY AND PLAN IDENTIFICATION LIST

Legend: **S** indicates that the study or plan is required with application submission. **A** indicates that the study or plan may be required to satisfy a condition of approval/draft approval.

For information and guidance on preparing required studies and plans refer here:

S/A	Number of copies	ENG	INEERING	S/A	Number of copies
S	(15)	1. Site Servicing Plan	Site Servicing Study / Assessment of Adequacy of Public Services		3
S	<mark>(15</mark>)	3. Grade Control and Drainage Plan	4. Geotechnical Study / Slope Stability Study	S	3
	2	5. Composite Utility Plan	6. Groundwater Impact Study		3
S	3	7. Servicing Options Report	8. Wellhead Protection Study		3
	9	9. Transportation Impact Assessment (TIA)	(10.Erosion and Sediment Control Plan / Brief	S	3
S	<mark>3</mark>	11.Storm water Management Report / Brief	12.Hydro geological and Terrain Analysis		3
	3	13.Hydraulic Water main Analysis	14.Noise / Vibration Study		3
	PDF only	15.Roadway Modification Functional Design	16.Confederation Line Proximity Study		3

S/A	Number of copies	PLANNING	/ DESIGN / SURVEY	S/A	Number of copies
	15	17.Draft Plan of Subdivision	18.Plan Showing Layout of Parking Garage		2
	5	19.Draft Plan of Condominium	(20.Planning Rationale)	S	3
S	<mark>15</mark>	21.Site Plan	22.Minimum Distance Separation (MDS)		3
S	(15)	(23.Concept Plan Showing Proposed Land) Uses and Landscaping	24.Agrology and Soil Capability Study		3
	3	25.Concept Plan Showing Ultimate Use of Land	26.Cultural Heritage Impact Statement		3
S	<mark>15</mark>)	27.Landscape Plan	28.Archaeological Resource Assessment Requirements: S (site plan) A (subdivision, condo)		3
S	2	29.Survey Plan	30.Shadow Analysis		3
S	3	(31.Architectural Building Elevation Drawings) (dimensioned)	(32.Design Brief (includes the Design Review Panel) (Submission Requirements)	S	Available online
	3	33.Wind Analysis			

S/A	Number of copies	ENV	IRONMENTAL	S/A	Number of copies
S	3	34.Phase 1 Environmental Site Assessment	35.Impact Assessment of Adjacent Waste Disposal/Former Landfill Site		3
S	3	36.Phase 2 Environmental Site Assessment (depends on the outcome of Phase 1)	37.Assessment of Landform Features		3
	3	38.Record of Site Condition	39.Mineral Resource Impact Assessment		3
S	3	40.Tree Conservation Report	41.Environmental Impact Statement / Impact Assessment of Endangered Species		3
	3	42.Mine Hazard Study / Abandoned Pit or Quarry Study	43.Integrated Environmental Review (Draft, as part of Planning Rationale)		3

S/A	Number of copies	ADDITION	S/A	Number of copies	
	1	44. Applicant's Public Consultation Strategy (may be provided as part of the Planning Rationale)	45.Site Lighting Plan		3
	1	46. Site Lighting Certification Letter	47.		

Meeting Date: November 22, 2021	Application Type: Site Plan Control, Zoning
File Lead (Assigned Planner): Jessica Button	Infrastructure Approvals Project Manager: John Wu
Site Address (Municipal Address): 326 Wilbrod	*Preliminary Assessment: 1 2 3 4 5

*One (1) indicates that considerable major revisions are required before a planning application is submitted, while five (5) suggests that proposal appears to meet the City's key land use policies and guidelines. This assessment is purely advisory and does not consider technical aspects of the proposal or in any way guarantee application approval.

It is important to note that the need for additional studies and plans may result during application review. If following the submission of your application, it is determined that material that is not identified in this checklist is required to achieve complete application status, in accordance with the Planning Act and Official Plan requirements, the Planning, Infrastructure and Economic Development Department will notify you of outstanding material required within the required 30 day period. Mandatory pre-application consultation will not shorten the City's standard processing timelines, or guarantee that an application will be approved. It is intended to help educate and inform the applicant about submission requirements as well as municipal processes, policies, and key issues in advance of submitting a formal development application. This list is valid for one year following the meeting date. If the application is not submitted within this timeframe the applicant must again preconsult with the Planning, Infrastructure and Economic Development Department.



Design Brief

Description:

A Design Brief is the core submission document that illustrates how the development is designed to work with its existing and planned context, to improve its surroundings and also demonstrate how the proposal supports the overall goals of the Official Plan, relevant secondary plans, Council approved plans and design guidelines. The purpose of the Terms of Reference is to assist the applicant to organize and substantiate the design justification in support of the proposed development and to assist staff and the public in the review of the proposal.

Authority to Request a Design Brief:

The *Planning Act* gives municipalities the authority to require that a Design Brief be prepared. Under Sections 22(4), (5) and Section 41(4) of the *Planning Act*, a Council has the authority to request such other information or material that the authority needs in order to evaluate and make a decision on an application. Section 5.2.6 of the Official Plan sets out the general requirement for a Design Brief.

Preparation:

The Design Brief should be signed by an urban designer, licenced architect, landscape architect, or a full member of the Canadian Institute of Planners.

When Required:

A Design Brief is required for a Site Plan Control planning application.

A Scoped Design Brief* is required when the following planning applications are applied for and not accompanied by a Site Plan Control application:

- Official Plan Amendment
- Zoning By-law Amendment (exception: a change in use which does not result in an increase in height or massing)

The requirement and scope of a Design Brief will be determined at the formal pre-application consultation meeting. Should an application be required to go to the <u>Urban Design Review Panel (UDRP)</u>, the Design Brief may be submitted as part of the submission materials to the panel.

Contents for Design Brief Submissions:

A Design Brief will contain and/or address the points identified during the pre-consultation meeting. Failure to address the critical elements identified in the pre-consultation meeting may result in the application being considered incomplete.

- * A Scoped Design Brief is composed of:
 - Section 1 should be combined into the Planning Rationale submission, and
 - Section 2 items will be confirmed in the pre-application consultation meeting.



Design Brief

SECTION 1 Note: This section can be combined with the Planning Rationale.

Application Subr Not Required	mission: Required	
	X	State the: type of application, legal description, municipal address, purpose of the application and provide an overall vision statement and goals for the proposal.
Response to Cit		<u>ts</u> :
Not Required	Required	
	X	State the Official Plan land use designation for the subject property and demonstrate how the proposal conforms to the Official Plan as it relates to the design of the subject site. Reference specific policy numbers from the Official Plan to show consistency. Justify areas of non-compliance and explain why there is non-compliance.
	X	State the applicable plans which apply to the subject proposal: community design plan, secondary plan, concept plan and design guideline. Reference the relevant design related polices within the applicable plans/guidelines and provide a comprehensive analysis as to how the proposed development incorporates the objectives or why it does not incorporate the objectives.
Context Plan:		
Not Required	Required X	Provide a contextual analysis that discusses/illustrates abutting properties, key destinations and linkages within a 100 meter radius (a larger radius may be requested for larger/more complex projects), such as transit stations, transportation networks for cars, cyclists, and pedestrians, focal points/nodes, gateways; parks/open spaces, topography, views towards the site, the urban pattern (streets, blocks), future and current proposals (if applicable), public art and heritage resources.
	X	Photographs to illustrate existing site conditions and surrounding contexts. Include a map pinpointing (with numbers) where each photo is taken and correspond these numbers with the site photos. Arrows illustrating the direction the photo is taken is also useful.



Design Brief

SECTION 2

TO BE CONSOLIDATED INTO COMBINED PLANNING RATIONALE and DESIGN BRIEF

Design Proposal:

The purpose of the Design Proposal is to show the building elevations, exterior details, transitions in form, treatment of the public realm and compatibility with adjacent buildings, using 3-D models, illustrations, diagrams, plans, and cross sections. Referencing Official Plan, Section 5.2.1, as determined at time of pre-application consultation meeting, submissions will need to address the following in the form of labelled graphics and written explanation:

Massing and So Not Required	cale Required	
	X	 Images which show: <u>Building massing</u> – from: at least two sides set within it current context (showing the entire height and width of the building) OR all four sides set within it current context (showing the entire height and width of the building).
	X	 Views – of the entire block, from: at least two perspectives to show how the proposed building is set within its current context OR all four perspectives to show how the proposed building is set within its current context.
	X	<u>Building transition</u> – to adjacent uses, with labelled explanation of the transition measures used.
X		<u>Grading</u> – if grades are an issue.
	X	Alternative building massing – additional imagery and site layouts considered and provide justification for the ultimate proposal sought.
Public Realm Not Required	Required	Labelled graphics and a written explanation which show: Streetscape – cross sections which illustrate the street design and right of way (referencing the City's design manuals).
	X	Relationship to the public realm – illustrating how the first few storeys of the proposed development responds to and relates to the existing context (e.g. through a podium plan and first floor plan). This is to include detailed explanation on: • Architectural responses • Landscaping details • Public art features (in accordance with Official Plan, Section 4.11) • For developments in Design Priority Areas, detail the building and site features, (in accordance with Official Plan, Section 4.11) which will enhance the public realm. Provide explanation for features

which are not provided.



Design Brief

Building Design Not Required	Required X	Labelled graphics (e.g. building elevations and floor plans) and a written explanation which document the proposed exterior architectural details and design (in accordance with Official Plan, Section 5.2.1).
Low-Rise Proposed	X	For high-rise development applications, detail the building design and massing and scale elements and how they relate to the proposed high-rise development (in accordance with Official Plan, Section 5.2.1).
Sustainability Not Required	Required X	Any sustainable design features to be incorporated, such as green roofs or walls, sun traps, reflective or permeable surfaces.
Heritage Not Required	Required X	How the building relates to the historic details, materials, site and setting of any existing historic resources on or adjacent to the subject property (if applicable).

Additional Contents:

Some proponents may be requested to provide submission material which complements the Design Brief. These additional requirements could be incorporated into the Design Brief submission for ease of review. These will be identified at the time of application consultation meeting:

- X Site Plan
- X Landscape Plan
 - Plan showing existing and proposed servicing
 - Shadow Analysis
 - Wind Analysis

Submission Requirements

Six hard copies and one digital copy



Appendix F - Roof Drain Product Data Sheet



RD-100

Tag: _____

Large Capacity Roof Drain

Components:



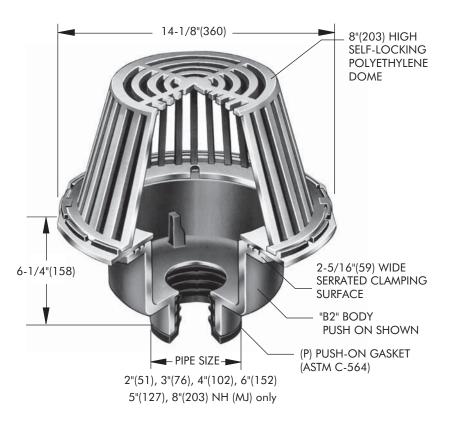






Order Code: RD-10

SPECIFICATION: Watts Drainage Products RD-100 epoxy coated cast iron roof drain with deep sump, wide serrated flashing flange, flashing clamp device with integral gravel stop and self-locking polyethylene (standard) dome strainer.



Free Area Sq. In.

Deck opening 10" (254) with sump receiver 13-1/4" (337)

** Side Outlet (-SO) option only available in 2"(51), 3"(76), 4"(102) pipe sizes. Underdeck Clamp (-BED and -D options) are not available when -SO is selected.

Ex. KL)-102P-K	
Pipe Sizing (Select One)		
Suffix	Description	
2	2"(51) Pipe Size	
3	3"(76) Pipe Size	
4	4"(102) Pipe Size	
5	5"(127) Pipe Size	
6	6"(152) Pipe Size	
8	8"(203) Pipe Size	
Outlet Type (Select One)		

Outlet Type (Select One)		
Suffix	Description	
NH	No Hub (MJ)	
Р	Push On	
Т	Threaded Outlet	
Χ	Inside Caulk	

Options (Select One or More)

JUILLY	Description	
-A	Accutrol weir (specify # 1-6 slots) 🔲
-B	Sump Receiver Flange	Ш
-BED	Sump Receiver, Adj Ext., Deck Clamp	
-C	Secondary Membrane Clamp	
-D	Underdeck Clamp	
-E	Adjustable Extension	
-GSS	Stainless Steel Ballast Guard	
-H	Adj. to 6" IRMA Ballast Guard	
-K	Ductile Iron Dome	
-K80	Aluminum Dome	
-L	Vandal Proof Dome	
-R	2" High External Water Dam	
-SO	Side Outlet**	
-V	Fixed Extension (1-1/2",2",3",4")	
-W	Adj. Water Level Regulator	
-W-1	Waterproofing Flange	
-Z	Extended Integral Wide Flange	
-5	Sediment Bucket	

Optional Body Material (NH Only)		
Suffix	Description	
-60	PVC Body w/Socket Outlet	
-61	ABS Body w/Socket Outlet	

Galvanized Dome

Mesh Covered Dome

-113M Special Epoxy from 3M Range

All Galvanized

-12

-13

Job Name	Contractor
Job Location	Contractor's P.O. No.
Engineer	Representative

WATTS Drainage reserves the right to modify or change product design or construction without prior notice and without incurring any obligation to make similar changes and modifications to products previously or subsequently sold. See your WATTS Drainage representative for any clarification. Dimensions are subject to manufacturing tolerances.



CANADA: 5435 North Service Road, Burlington, ON, L7L 5H7 TEL: 905-332-6718 TOLL-FREE: 1-888-208-8927 Website: www.wattsdrainage.ca



Accutrol Weirs

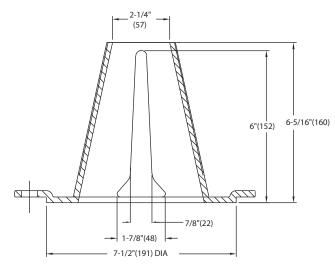
Flow Control for Roof Drains

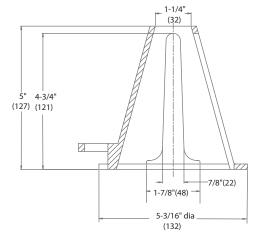
Tag: _____

ACCUTROL WEIR FLOW CONTROL

SPECIFICATION: Watts Drainage Products epoxy coated cast iron Accutrol Weir is designed with parabolic openings which limit the flow of rain water off a roof. Each weir slot controls flow to 5 gpm per inch of head to a maximum of 30 gpm at 6" head(for large sump), 25 gpm at 5" head(for small sump). The Accutrol Weir is secured to the flashing clamp of the roof drain. The Accutrol Weir is available with 1 to 4 slots for the large sump drain and up to 3 slots for the small sump drain.

For Large Sump Roof Drains Specify the "-A" option and number of slots required. (ie. "RD-100-A2" for two slot weir) For Small Sump Roof Drains Specify the "-A" option and number of slots required. (ie. "RD-200-A1" for one slot weir)





LARGE SUMP ACCUTROL WEIR

SMALL SUMP ACCUTROL WEIR

Job Name	Contractor
Job Location	Contractor's P.O. No.
Engineer	Representative

WATTS Drainage reserves the right to modify or change product design or construction without prior notice and without incurring any obligation to make similar changes and modifications to products previously or subsequently sold. See your WATTS Drainage representative for any clarification. Dimensions are subject to manufacturing tolerances.



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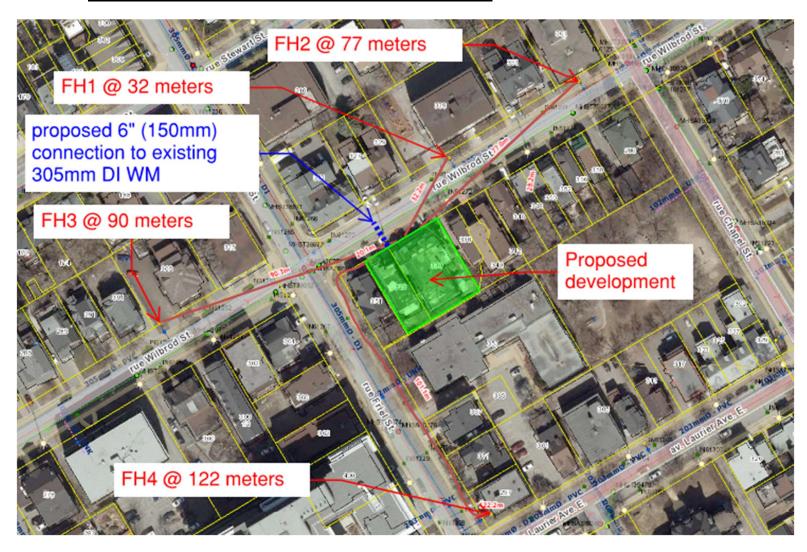
Appendix G - Boundary Conditions

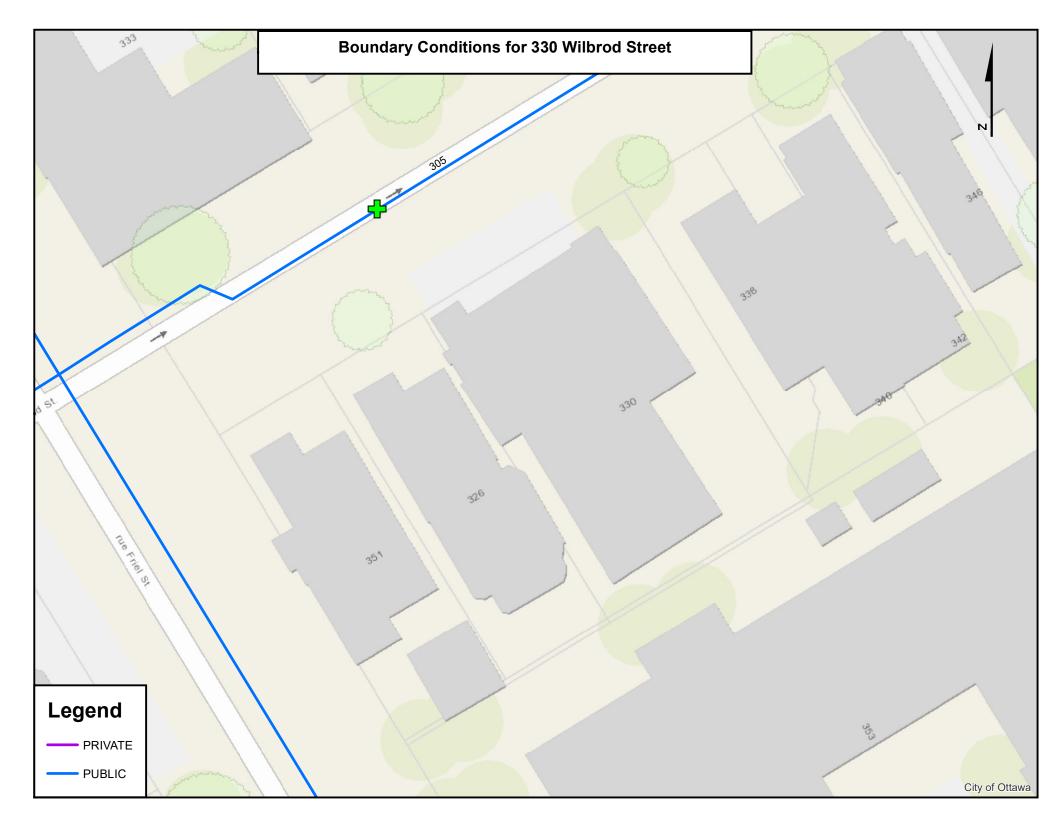
Request for Boundary Conditions 326-330 Wilbrod Street

Provided Information

Saanaria	Demand		
Scenario	L/min	L/s	
Average Daily Demand	14.5	0.24	
Maximum Daily Demand	36	0.60	
Peak Hour	80	1.32	
Fire Flow Demand	8,000	133.3	

Location, proposed connection & Near by Hydrants Distribution





Ali Sammour

From: Wu, John <John.Wu@ottawa.ca> **Sent:** September 12, 2022 11:59 AM

To: Ali Sammour

Subject: RE: 326-330 Wilbrod Street / File # D02-02-22-0027/D07-12-22-0049 / Jp2g Ref#

21-1062A

EXTERNAL EMAIL Please use caution.

****The following information may be passed on to the consultant, but do NOT forward this e-mail directly.****

The following are boundary conditions, HGL, for hydraulic analysis at 330 Wilbrod Street (zone 1W) assumed to be connected to the 305 mm watermain on Wilbrod Street (see attached PDF for location).

Both Connections:

Minimum HGL: 106.1 m

Maximum HGL: 115.4 m

Max Day + Fire Flow (133 L/s): 107.1 m

John

Existing Water Boundary Conditions: 326-300 Wilbrod St.

Water Demands	<u>Design Parameters</u>	<u>Design Parameters</u>			Boundary Conditions		
					m		
Average Daily Demand:	0.24 l/s	Pipe Diameter:	150 mm	Max. HGL:	115.4	m	
Maximum Daily Demand:	0.60 l/s	Pipe Material:	PVC	Min HGL:	106.1	m	
Maximum Hour Demand:	1.32 l/s	Pipe Length (total network):	15.3 m	Max. Day + Fire:	107.1	m	
Fire Flow Demand:	133.30 l/s	Basement Mech.room Elevation:	67.31				
Maximum Daily + Fire Flow Demand:	133.90 l/s	Pavement (R.O.W.) Elevation:	70.05				

Boundary Condition Check

Check water pressure at municipal connection:

Min. HGL - Pavement elevation = 36.05 m

= 51.26 psi* = 353.44 kPa* *Normal operating pressure ranges between 345 kPa (50 psi) and 552 kPa (80 psi) under a condition of maximum daily flow as per City of Ottawa Design Guidelines - Water Distribution (Section 4.2.2)

Pressure at municipal connection

OK

Check water pressure at building connection (at max. hour demand):

Min. HGL - Basement Mech.room Elevation - Friction Loss** = 38.79 m **Friction loss calculated using the Hazen-Williams Equation

= 55.16 psi*** = 380.30 kPa*** ***Under maximum hourly demand conditions the pressures shall not be less than 276 kPa (40 psi) as per City of Ottawa Design Guidelines - Water Distribution (Section 4.2.2)

Pressure at building connection (at max. hour demand)

OK

Check water pressure at building connection (at max. day + fire demand):

Min. HGL - Basement Mech.room Elevation - Friction Loss** = 35.97 m **Friction loss calculated using the Hazen-Williams Equation

= 51.14 psi**** = 352.63 kPa****

*****Under maximum day and fire flow demand conditions the residual pressure at any point in the system shall not be less than 140 kPa (20 psi) as per City of Ottawa Design Guidelines - Water Distribution (Section 4.2.2)

Pressure at building connection (at max. day + fire demand)

OK