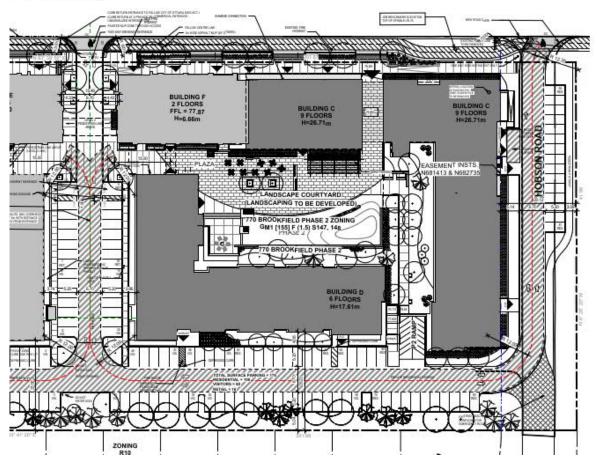
# SERVICING & STORMWATER MANAGEMENT REPORT 770 BROOKFIELD ROAD – PHASE 2, OTTAWA

#### **BROOKFIELD ROAD**



Project No.: CCO-22-3501

City File No.: D07-12-XX-XXXX

Prepared for:

Hobin Architecture Inc 63 Pamilla Street Ottawa, ON K1S 3K7

# Prepared by:

McIntosh Perry Consulting Engineers Ltd. 115 Walgreen Road Carp, ON K0A 1L0

June 24, 2022

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#### 1.0 PROJECT DESCRIPTION

#### 1.1 Purpose

McIntosh Perry (MP) has been retained by Hobin Architecture Inc. to prepare this Servicing and Stormwater Management Report in support of the Site Plan Control application for the proposed Phase II development at 770 Brookfield Road within the City of Ottawa.

The main purpose of this report is to present a servicing design for the development in accordance with the recommendations and guidelines provided by the City of Ottawa (City), the Rideau Valley Conservation Authority (RVCA), and the Ministry of the Environment, Conservation and Parks (MECP). This report will address the water, sanitary and storm sewer servicing for the development, ensuring that existing and available services will adequately service the proposed development.

This report should be read in conjunction with the following drawings:

- CCO-22-3501, C101 Site Grading and Drainage Plan, and
- CCO-22-3501, C102 Site Servicing Plan.
- CCO-22-3501, PRE Pre-Development Drainage Area Plan (Appendix E)
- CCO-22-3501, POST Post-Development Drainage Area Plan (Appendix F)

# 1.2 Site Description

The property is located at 770 Brookfield Road. It is described as Registered Plan 787, Parts 7-9 Plan 4R-28560 Ward 16 River, City of Ottawa. The Phase II land in question covers approximately 0.72 ha and is bounded by Brookfield Road to the north and Hobson Road to the east. The development area for the proposed works is approximately 0.72 ha. The site is zoned for General Mixed Use (GM1). See Site Location Plan in Appendix 'A' for more details and Phase II Severance R-Plan included in Appendix 'B'.



Figure 1: Site Map

#### 1.3 Proposed Development and Statistics

The proposed development consists of a 9-storey mixed-use residential building and a 6-storey mixed-use residential building. Visitor parking and drive aisles will be provided west and south of the proposed buildings. Underground parking will be provided for residents with site access extending from Brookfield Road and Hobson Road. Refer to Site Plan prepared by Hobin Architecture included in Appendix 'B' for details.

# 1.4 Existing Conditions and Infrastructure

The property adjacent to the existing site is currently developed with mixed-use residential buildings, approved under City Application No. D07-12-17-0140 (Functional Servicing and Stormwater Management Report). The Phase II site is currently undeveloped.

The existing Phase II site has no sanitary or water services. In accordance with the Functional Servicing and Stormwater Management Report, drainage within the Phase II site flows both west, currently being picked up by the Phase I servicing network, and east, currently being picked up by the municipal infrastructure within Hobson Road.

Sewer and watermain mapping collected from the City of Ottawa indicate that the following services exist across the property frontages within the adjacent municipal rights-of-way(s):

#### Brookfield Road

- o 305mm diameter cast iron watermain,
- o 250mm diameter concrete sanitary sewer, tributary to the Rideau River Collector, and a
- o 750mm diameter concrete storm sewer, tributary to Sawmill Creek sub-watershed with approximately 0.7 km to the outlet

#### Hobson Road

- 203mm diameter cast iron watermain,
- o 300mm diameter asbestos concrete sanitary sewer, tributary to the Rideau River Collector, and a
- o 375mm diameter concrete storm sewer, tributary to Sawmill Creek sub-watershed with approximately 1.1 Km to the outlet.

#### • Drive Aisle Within 770 Brookfield – Phase I

- o 200mm diameter concrete sanitary sewer, tributary to the Rideau River Collector, and a
- o 675mm diameter concrete storm sewer tributary to Sawmill Creek sub-watershed with approximately 0.7 km to the outlet.

#### 1.5 Approvals

The proposed development is subject to the City of Ottawa site plan control process. Site plan control requires the City to review, provided concurrence and approve the engineering design package. Permits to construct can be requested once the City has issued a site plan agreement.

An Environmental Compliance Approval (ECA) through the Ministry of Environment, Conservation and Parks (MECP) is not anticipated to be required since the development is contained within a single parcel of land and proposes independent servicing, is not within a combined sewer shed, and does not propose industrial sewage. As a result, the stormwater management system meets the exemption requirements under O.Reg 525/90.

# 2.0 BACKROUND STUDIES, STANDARDS, AND REFRENCES

## 2.1 Background Reports / Reference Information

Background studies that have been completed for the proposed site include City of Ottawa as-built drawings, a topographical survey, a geotechnical report and a Phase I Environmental Site Assessment (ESA).

As-built drawings of existing services within the vicinity of the proposed site were reviewed in order to determine accurate servicing and stormwater management schemes for the site.

A topographic survey of the site (Job No. 22509-21) was completed by Annis, O'Sullivan, Vollebekk LTD., dated May 20, 2022.

The following reports have previously been completed and are available under separate cover:

- Geotechnical Investigation completed by Paterson Group, dated May 30, 2022.
- Phase One Environmental Site Assessment completed by Paterson Group, dated December 16, 2019.
- Functional Servicing and Stormwater Management Report completed by David Schaeffer Engineering Ltd, dated May 2019. (Functional Servicing and Stormwater Management Report)
- Stormwater Management Memorandum completed by David Schaeffer Engineering Ltd, dated October 5, 2020.

# 2.2 Applicable Guidelines and Standards

City of Ottawa:

- ◆ Ottawa Sewer Design Guidelines, City of Ottawa, SDG002, October 2012. (Ottawa Sewer Guidelines)
  - Technical Bulletin ISTB-2014-01 City of Ottawa, February 2014. (ISTB-2014-01)
  - Technical Bulletin PIEDTB-2016-01 City of Ottawa, September 2016. (PIEDTB-2016-01)
  - Technical Bulletin ISTB-2018-01 City of Ottawa, January 2018. (ISTB-2018-01)
  - Technical Bulletin ISTB-2018-03 City of Ottawa, March 2018. (ISTB-2018-03)
  - Technical Bulletin ISTB-2019-01 City of Ottawa, January 2019. (ISTB-2019-01)
  - Technical Bulletin ISTB-2019-02 City of Ottawa, February 2019. (ISTB-2019-02)
- Ottawa Design Guidelines Water Distribution City of Ottawa, July 2010. (Ottawa Water Guidelines)
  - Technical Bulletin ISD-2010-2 City of Ottawa, December 15, 2010. (ISD-2010-2)
  - Technical Bulletin ISDTB-2014-02 City of Ottawa, May 2014. (ISDTB-2014-02)
  - Technical Bulletin ISTB-2018-02 City of Ottawa, March 2018. (ISTB-2018-02)

Ministry of Environment, Conservation and Parks:

- ◆ Stormwater Planning and Design Manual, Ministry of the Environment, March 2003. (MECP Stormwater Design Manual)
- ◆ Design Guidelines for Sewage Works, Ministry of the Environment, 2008. (MECP Sewer Design Guidelines)

#### Other:

• Water Supply for Public Fire Protection, Fire Underwriters Survey, 2020. (FUS Guidelines)

# 3.0 PRE-CONSULTATION SUMMARY

A pre-consultation meeting was conducted on December 16, 2014, regarding the proposed site. Specific design parameters to be incorporated within this design include the following:

- Calculate the time of concentration (Cannot be less than 10 minutes).
- Control post-development flows to the pre-development 2-year storm release rate using the pre-development runoff coefficient or a maximum equivalent 'C' of 0.5, whichever is less. Up to and including the 100-year storm event must be detained on site.
- Coordination with the RVCA is required to confirm quality control requirements.

#### 4.0 WATERMAIN

# 4.1 Existing Watermain

The site is located within the 2W2C pressure zone, as per the Water Distribution System mapping included in Appendix C. There is an existing 203mm diameter CI watermain within Hobson Road and 305 mm diameter CI watermain within Brookfield Road available to service the development.

#### 4.2 Proposed Watermain

A 150mm diameter PVC water service is proposed to service the development complete with a water valve between the building and the existing watermain. The water service is proposed to be serviced by the existing 203 mm diameter watermain within Hobson Road. The services are designed to have a minimum of 2.4m cover. Refer to drawing C102 for a detailed servicing layout.

The Fire Underwriters Survey 2020 (FUS) method was utilized to determine the required fire flow for the site. The 'C' factor (type of construction) for the FUS calculation was determined to be 0.8 (non-combustible type). The total floor area ('A' value) for the FUS calculation was determined to be 15,433.7 m². The results of the calculations yielded a required fire flow of 12,000 L/min for Building C & existing Building F (combined) and 9,000 L/min for Building D. The detailed calculations for the FUS can be found in Appendix 'C'.

The water demands for the proposed building have been calculated to adhere to the Ottawa Design Guidelines – Water Distribution manual and can be found in Appendix 'C'. The results have been summarized in Table 1, below. In accordance with Section 4.3.1 of the guidelines, service areas with a basic day demand greater than 50 m³/day require a redundant connection to the municipal system. The redundancy is proposed to be provided via a water valve located south of the development service lateral.

Table 1: Water Supply Design Criteria and Water Demands

Site Area	0.91 ha
Residential	280 L/person/day
1 Bedroom Apartment	1.4 persons/unit
2 Bedroom Apartment	2.1 persons/unit
3 Bedroom Apartment	3.1 persons/unit
4 Bedroom Apartment	3.4 persons/unit
Bachelor Apartment	1.4 persons/unit
Maximum Daily Peaking Factor	2.2 x avg day
Maximum Hour Peaking Factor	5.5 x avg day
Average Day Demand (L/s)	2.72
Maximum Daily Demand (L/s)	5.97
Peak Hourly Demand (L/s)	14.90
FUS Fire Flow Requirement (L/s)	200 (12,000 L/min)

The City provided the estimated water pressures at both for the average day scenario, peak hour scenario and the max day plus fire flow scenario for the demands indicated by the correspondence in Appendix C. The resulting pressures for the boundary conditions results are shown in Table 2, below.

Table 2: Boundary Conditions Results

Scenario	Proposed Demands (L/s)	Connection HGL (m H₂O)*/kPa		
Average Day Demand	2.72	54.5 / 534.4		
Maximum Daily + Fire Flow Demand	5.97 + 200 = 205.97	43.0 / 421.6		
Peak Hourly Demand	14.90	48.3 / 473.6		
*Adjusted for an estimated ground elevation of 75.52m above the connection point.				

The normal operating pressure range is anticipated to be 474 kPa to 5342 kPa and will not be less than 275 kPa (40 psi) or exceed 689 kPa (100 psi). The proposed watermains will meet the minimum required 20 psi (140 kPa) from the Ottawa Water Guidelines at the ground level under maximum day demand and fire flow conditions. A pressure reducing valve is required for the site since the pressure will exceed 552 kPa (80 psi) in the average day scenario.

To confirm the adequacy of fire flow to protect the proposed development, public fire hydrants within 150 m of the proposed building were analysed per City of Ottawa ISTB 2018-02 Appendix I Table 1. Based on City guidelines (ISTB-2018-02), the existing hydrants can provide adequate fire protection to the proposed development. The results are summarized in Table 3, below.

**Table 3: Fire Protection Confirmation** 

Building	Fire Flow Demand (L/min.)	Fire Hydrant(s) within 75m	Fire Hydrant(s) within 150m	Combined Fire Flow (L/min.)
770 Brookfield Road	12,000 (FUS)	2	2	19,000

#### 5.0 SANITARY DESIGN

## 5.1 Existing Sanitary Sewer

There is an existing 300mm diameter concrete sanitary sewer within Hobson Road available to service the development. There is also an existing 200mm diameter concrete sanitary sewer within the center drive aisle that currently services the Phase 1 development.

# 5.2 Proposed Sanitary Sewer

A new 200mm diameter gravity sanitary is proposed be connected to the existing 300mm diameter sanitary sewer within Hobson Road to service Building C. In addition, a new 200mm diameter is proposed to be connected to the existing 300mm diameter sewer within Hobson Road to service Building D. Based on coordination with the mechanical engineer, multiple sanitary connections is expected to be required due to the development size and internal sloping for the building plumbing system. Refer to drawing C102 for a detailed servicing layout.

The Phase II development consists of two mixed-use residential buildings. The peak design flows for the proposed buildings were calculated using criteria from the Ottawa Sewer Guidelines and are summarized in Table 4, below. Based on the unit occupancy statistics provided by the architect, the proposed site development will generate a flow of 9.22 L/s. See Appendix 'D' of this report for more details.

Table 4: Sanitary Design Criteria

Design Parameter	Value
Site Area	0.43 ha
Residential	280 L/person/day
1 Bedroom Apartment	1.4 persons/unit
2 Bedroom Apartment	2.1 persons/unit
3 Bedroom Apartment	3.1 persons/unit
4 Bedroom Apartment	3.4 persons/unit
Bachelor Apartment	1.4 persons/unit
Residential Peaking Factor	3.28
Institutional/Commercial Peaking Factor	1.00
Extraneous Flow Allowance	0.33 L/s/ha

Table 5, below, summarizes the estimated wastewater flow from the proposed development. Refer to Appendix D for detailed calculations.

Table 5: Summary of Estimated Sanitary Flow

Design Parameter	Total Flow (L/s)
Total Estimated Average Dry Weather Flow	2.81
Total Estimated Peak Dry Weather Flow	8.96
Total Estimated Peak Wet Weather Flow	9.22

The proposed 200 mm diameter gravity sanitary service will be installed with a minimum full flow target velocity (cleansing velocity) of 0.6 m/s and a full flow velocity of not more than 3.0 m/s. The capacity of the service lateral is 33.22 L/s at a proposed slope of 1.0%. For the purpose of sizing the sanitary service, it is assumed that the entire Phase II development is conveyed through a single pipe. Due to the complexity of the downstream network, the City will need to advise of any downstream constraints.

#### 6.0 STORM SEWER DESIGN

## 6.1 Existing Storm Sewers

Storm runoff from the site is currently tributary to the Sawmill Creek sub watershed. The property is currently serviced by the adjacent Phase I storm network and municipal catch basins within Brookfield Road and Hobson Road. There is an existing 375mm diameter concrete storm sewer within Hobson Road that is available for servicing the proposed development.

#### 6.2 Proposed Storm Sewers

A new 250 mm storm service will be extended from the existing 375mm diameter storm sewer within Hobson Road. The sewer system will provide attenuation for the roof area using roof drains and the internal courtyard area by an internal cistern pumped to the required release rate.

Runoff collected on the roof of the proposed buildings will be stored and controlled internally using roof drains. Roof drains will be used to limit the flow from the roof to the specified allowable release rate. For calculation purposes a Watts Accutrol roof drain was used estimate a reasonable roof flow. Other products maybe specified at detailed building design so long as release rates and storage volumes are respected.

Foundation drainage is proposed to be pumped without flow attenuation via the 250 mm diameter storm service downstream of any cistern controls. Roof drainage will also be downstream of any cistern controls.

See CCO-22-3501 - POST include in Appendix F of this report for more details. The Stormwater Management design for the subject property will be outlined in Section 7.0 of this report.

#### 7.0 PROPOSED STORMWATER MANAGEMENT

# 7.1 Design Criteria and Methodology

Stormwater management for the proposed site will be maintained through rooftop attenuation and an internal cistern that will collect runoff from the at-grade areas within the site. The flow will be directed to the existing 375mm diameter storm sewer within Hobson Road.

In summary, the following design criteria have been employed in developing the stormwater management design for the site as directed by the RVCA and City:

#### **Quality Control**

• Based on the Functional Servicing and Stormwater Management Report prepared by DSEL, stormwater quality controls to an enhanced level of treatment are required for the subject site.

#### **Quantity Control**

• Based on the Functional Servicing and Stormwater Management Report prepared by DSEL, the allowable release rate for Phase 2 of the proposed development is 80.6 L/s/Ha.

#### 7.2 Runoff Calculations

Runoff calculations presented in this report are derived using the Rational Method, given as:

$$Q = 2.78 CIA \text{ (L/s)}$$

Where: C = Runoff coefficient

= Rainfall intensity in mm/hr (City of Ottawa IDF curves)

A = Drainage area in hectares

It is recognized that the Rational Method tends to overestimate runoff rates. As a result, the conservative calculation of runoff ensures that any SWM facility sized using this method is expected to function as intended.

The following coefficients were used to develop an average C for each area:

Roofs/Concrete/Asphalt	0.90
Gravel	0.60
Undeveloped and Grass	0.20

As per the City of Ottawa - Sewer Design Guidelines, the 5-year balanced 'C' value must be increased by 25% for a 100-year storm event to a maximum of 1.0.

As per the pre-consultation meeting with the City of Ottawa the time of concentration (Tc) used for pre-development shall be calculated using a minimum Tc of 10 minutes and post-development flows shall be calculated using a Tc of 10 minutes.

# 7.3 Pre-Development Drainage

It has been assumed that the site contains no stormwater management controls for flow attenuation. The estimated pre-development peak flows for the 5, and 100-year events are summarized below in Table 6. See CCO-22-3501 - PRE in Appendix E and Appendix G for calculations.

Drainage	Area	(	)
Area	(ha)	5-Year	's) 100-Year
A1	0.718	45.98	97.14

Table 6: Pre-Development Runoff Summary

# 7.4 Post-Development Drainage

The proposed site drainage limits are demonstrated on the Post-Development Drainage Area Plan. See CCO-22-3501 - POST in Appendix 'F' of this report for more details. A summary of the Post-Development Runoff Calculations can be found below.

Drainage Area	Area (ha)	5-year Peak Flow (L/s)	100-year Peak Flow (L/s)	100-year Storage Required (m³)	100-year Storage Available (m³)
C1	0.159	3.36	5.76	68.11	71.43
C2	0.063	1.26	2.16	27.52	28.32
C3	0.154	3.36	5.76	65.20	69.12
C4	0.222	6.33	12.41	36.07	36.07
C5	0.120	16.14	31.77	-	-
Total	0.718	30.45	57.86	196.91	204.95

Table 7: Post-Development Runoff Summary

Post development drainage will be restricted to a maximum release rate of 57.86 L/s based on the Phase I Functional Servicing and Stormwater Management Report.

Runoff for areas C1-C3 will be collected by roof drains and controlled to maximum release rate of 13.68 L/s with 204.94 m³ of storage provided.

Runoff from area C4 will be collected by area drains that will direct flow to an internal cistern. The 36.07 m³ internal cistern is anticipated to convey stormwater to the outlet at a maximum flow rate

12.41 L/s. Flows in excess of the 100-year storm event will need to be directed towards Hobson Road via a cistern overflow. Further detail pertaining to the cistern are to be confirmed by the Mechanical Engineer.

Runoff from area C5 will sheet drain without attenuation towards the Phase I storm network and towards municipal catch basins within Brookfield Road and Hobson Road.

Foundation drainage will be pumped and discharged via the 250 mm storm service, downstream of cistern controls.

# 7.5 Quality Controls

The following methods will be utilized to provide quality controls for the Phase II area:

- Areas C1-C3 will collect rooftop drainage and therefore drainage is considered clean.
- Quality controls for Area C4 will be provided via the cistern in a settling pit. Details are to be confirmed the Mechanical Engineer. Pumped water will combine with clean roof drainage before discharging to the city sewer.
- Drainage flowing towards the Phase 1 development area will be treated by the OGS unit, sized to accommodate the Phase II development.

#### 8.0 EROSION AND SEDIMENT CONTROL

## 8.1 Temporary Measures

Before construction begins, temporary silt fence, straw bale or rock flow check dams will be installed at all natural runoff outlets from the property. It is crucial that these controls be maintained throughout construction and inspection of sediment and erosion control will be facilitated by the Contractor or Contract Administration staff throughout the construction period.

Silt fences will be installed where shown on the final engineering plans, specifically along the downstream property limits. The Contractor, at their discretion or at the instruction of the City, Conservation Authority or the Contract Administrator shall increase the quantity of sediment and erosion controls on-site to ensure that the site is operating as intended and no additional sediment finds its way off site. The rock flow, straw bale & silt fence check dams and barriers shall be inspected weekly and after rainfall events. Care shall be taken to properly remove sediment from the fences and check dams as required. Fibre roll barriers are to be installed at all existing curb inlet catchbasins and filter fabric is to be placed under the grates of all existing catchbasins and manholes along the frontage of the site and any new structures immediately upon installation. The measures for the existing/proposed structures is to be removed only after all areas have been paved. Care shall be taken at the removal stage to ensure that any silt that has accumulated is properly handled and disposed of. Removal of silt fences without prior removal of the sediments shall not be permitted.

Although not anticipated, work through winter months shall be closely monitored for erosion along sloped areas. Should erosion be noted, the Contractor shall be alerted and shall take all necessary steps to rectify the situation. Should the Contractor's efforts fail at remediating the eroded areas, the Contractor shall contact the City and/or Conservation Authority to review the site conditions and determine the appropriate course of action. As the ground begins to thaw, the Contractor shall place silt fencing at all required locations as soon as ground conditions warrant. Please see the Site Grading, Drainage and Sediment & Erosion Control Plan for additional details regarding the temporary measures to be installed and their appropriate OPSD references.

#### 8.2 Permanent Measures

Rip-rap will be placed at all locations that have the potential for concentrated flow. It is crucial that the Contractor ensure that the geotextile is keyed in properly to ensure runoff does not undermine the rip rapped area. Additional rip rap is to be placed at erosion prone locations as identified by the Contractor / Contract Administrator / City or Conservation Authority.

It is expected that the Contractor will promptly ensure that all disturbed areas receive topsoil and seed/sod and that grass be established as soon as possible. Any areas of excess fill shall be removed or levelled as soon as possible and must be located a sufficient distance from any watercourse to ensure that no sediment is washed out into the watercourse. As the vegetation growth within the

site provides a key component to the control of sediment for the site, it must be properly maintained once established. Once the construction is complete, it will be up to the landowner to maintain the vegetation and ensure that the vegetation is not overgrown or impeded by foreign objects.

#### 9.0 SUMMARY

- Two mixed-use residential buildings are proposed be constructed at 770 Brookfield Road.
- A 150mm diameter water service is proposed to be connected to the existing 200mm diameter watermain within Hobson Road.
- Two 200mm diameter sanitary services are proposed to service the development via the 300mm diameter sanitary sewer within Hobson Road, tributary to the Rideau River Collector.
- A new 250mm storm service for rooftop, surface, and foundation drainage are proposed to service the developments. The storm service will connect to the 375mm diameter storm sewer within Hobson Road, tributary to the Sawmill Creek sub-watershed approximately 1.1 km downstream.
- Storage for the 5- through 100-year storm events will be provided through roof attenuation and internal cistern attenuation.
- Quality control is provided via the cistern settling pit and existing Phase I OGS unit.

#### 10.0 RECOMMENDATION

Based on the information presented in this report, we recommend that City of Ottawa approve this Servicing and Stormwater Management Report in support of the proposed development at 770 Brookfield Road.

This report is respectfully being submitted for approval.

Regards,

McIntosh Perry Consulting Engineers Ltd.



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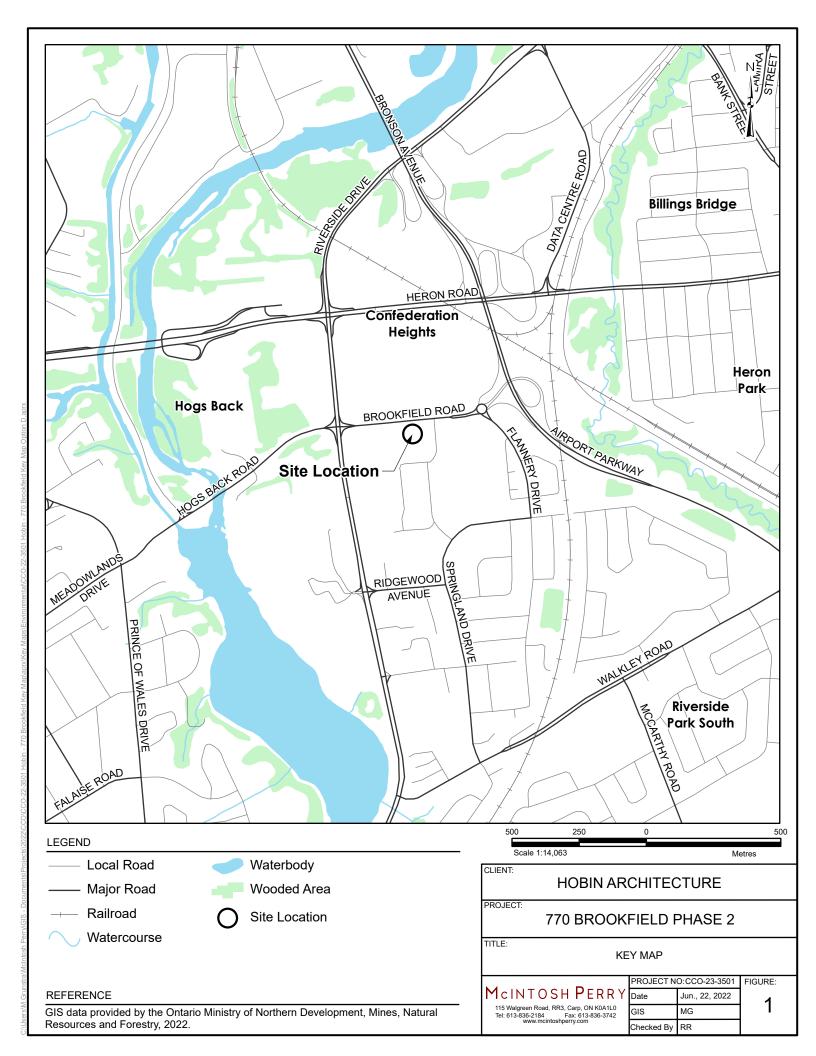
#### 11.0 STATEMENT OF LIMITATIONS

This report was produced for the exclusive use of Hobin Architecture Inc. The purpose of the report is to assess the existing stormwater management system and provide recommendations and designs for the post-construction scenario that are in compliance with the guidelines and standards from the Ministry of the Environment, Conservation and Parks, City of Ottawa and local approval agencies. McIntosh Perry reviewed the site information and background documents listed in Section 2.0 of this report. While the previous data was reviewed by McIntosh Perry and site visits were performed, no field verification/measures of any information were conducted.

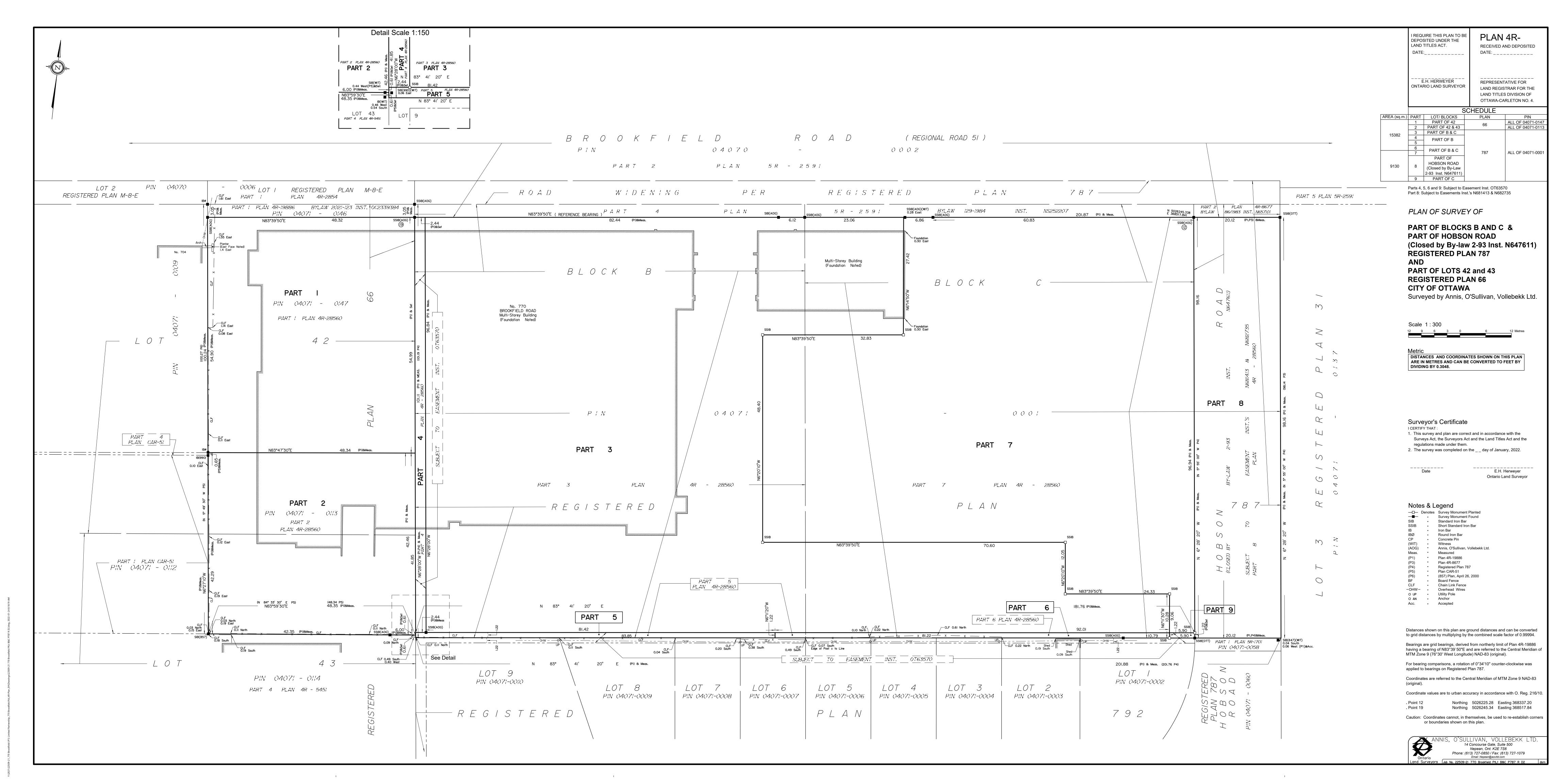
Any use of this review by a third party, or any reliance on decisions made based on it, without a reliance report is the responsibility of such third parties. McIntosh Perry accepts no responsibility for damages, if any, suffered by any third party as a result of decisions or actions made based on this review.

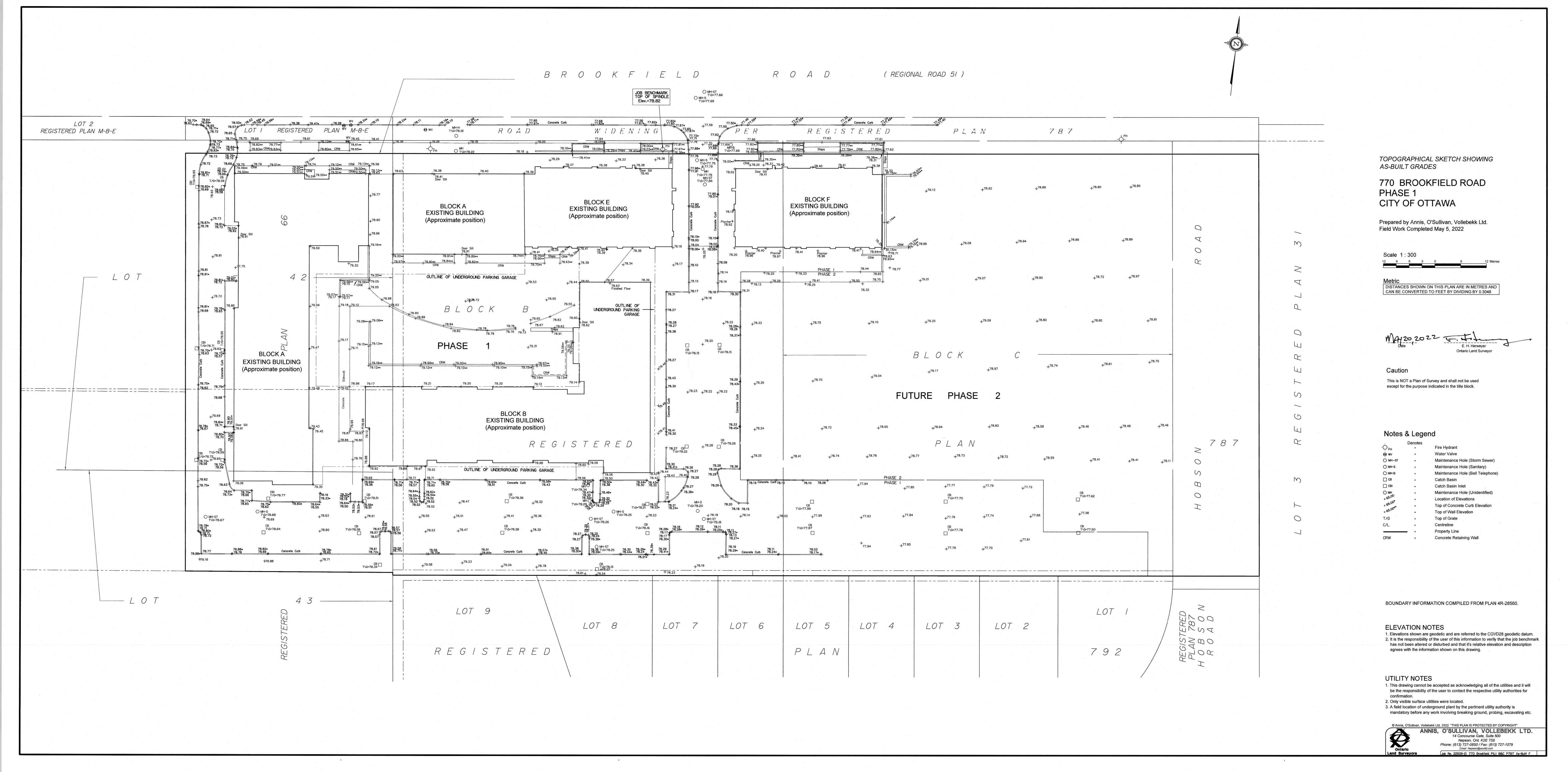
The findings, conclusions and/or recommendations of this report are only valid as of the date of this report. No assurance is made regarding any changes in conditions subsequent to this date. If additional information is discovered or becomes available at a future date, McIntosh Perry should be requested to re-evaluate the conclusions presented in this report, and provide amendments, if required.

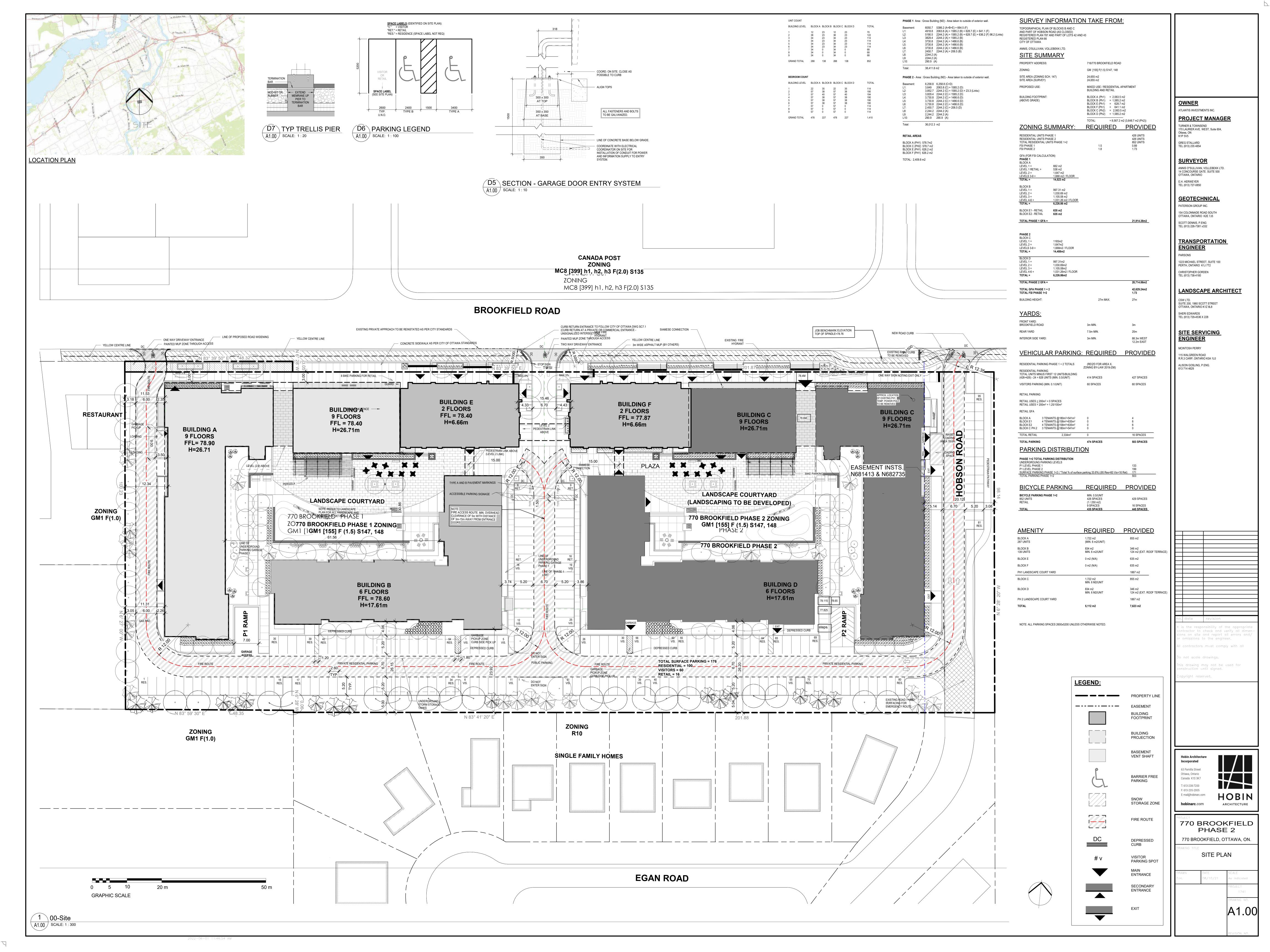
APPENDIX A KEY PLAN



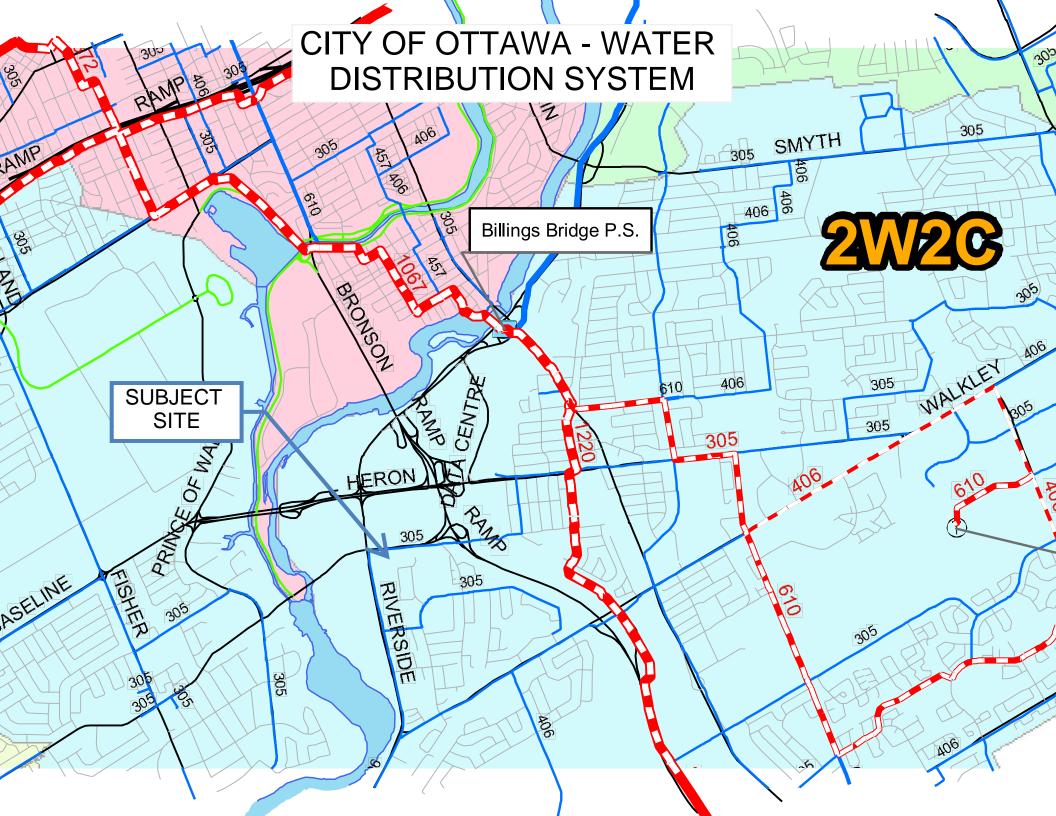
APPENDIX B BACKGROUND DOCUMENTS







APPENDIX C WATERMAIN CALCULATIONS



#### CCO-22-3501 - 770 Brookfield Phase 2 - BUILDING C & D - Water Demands

Project: 770 Brookfield Phase 2 - BUILDING C & D

 Project No.:
 CCO-22-3501

 Designed By:
 RRR

Checked By: AJG

Date: June 23, 2022

Site Area: 0.91 gross ha

<u>Residential</u>	NUMBER OF UNITS		UNIT RATE	
Single Family		homes	3.4	persons/unit
Semi-detached		homes	2.7	persons/unit
Townhouse		homes	2.7	persons/unit
Bachelor Apartment	2	41 units	1.4	persons/unit
1 Bedroom Apartment		39 units	1.4	persons/unit
2 Bedroom Apartment		70 units	2.1	persons/unit
3 Bedroom Apartment		29 units	3.1	persons/unit
4 Bedroom Apartment		60 units	3.4	persons/unit

Total Residential Population 833 persons

 Commercial
 579 m2

 Industrial - Light
 m2

 Industrial - Heavy
 m2

#### **AVERAGE DAILY DEMAND**

DEMAND TYPE	AMOUNT	UNITS	
Residential	280	L/c/d	
Industrial - Light	35,000	L/gross ha/d	
Industrial - Heavy	55,000	L/gross ha/d	
Shopping Centres	2,500	L/(1000m <sup>2</sup> /d	
Hospital	900	L/(bed/day)	
Schools	70	L/(Student/d)	
Trailer Park with no Hook-Ups	340	L/(space/d)	
Trailer Park with Hook-Ups	800	L/(space/d)	
Campgrounds	225	L/(campsite/d)	
Mobile Home Parks	1,000	L/(Space/d)	
Motels	150	L/(bed-space/d)	
Hotels	225	L/(bed-space/d)	
Tourist Commercial	28,000	L/gross ha/d	
Other Commercial	28,000	L/gross ha/d	
	Residential	2.70	L/s
AVERAGE DAILY DEMAND	Commerical/Industrial/		
	Institutional	0.02	L/s

#### **MAXIMUM DAILY DEMAND**

DEMAND TYPE	AMOUNT		UNITS	
Residential	2.2	x avg. day	L/c/d	
Industrial	1.5	x avg. day	L/gross ha/d	
Commercial	1.5	x avg. day	L/gross ha/d	
Institutional	1.5	x avg. day	L/gross ha/d	
	Residential		L/s	
MAXIMUM DAILY DEMAND	Commerical/Industrial/			
	Institutional	0.03	L/s	

#### **MAXIMUM HOUR DEMAND**

DEMAND TYPE	AMOUNT		UNITS	
Residential	5.5	x avg. day	L/c/d	
Industrial	1.8	x max. day	L/gross ha/d	
Commercial	1.8	x max. day	L/gross ha/d	
Institutional	1.8	x max. day	L/gross ha/d	
	Residential	14.85	L/s	
MAXIMUM HOUR DEMAND	Commerical/Industrial/			
	Institutional	0.05	L/s	

WATER DEMAND DESIGN FLOWS PER UNIT COUNT
CITY OF OTTAWA - WATER DISTRIBUTION GUIDELINES, JULY 2010

AVERAGE DAILY DEMAND	2.72	L/s
MAXIMUM DAILY DEMAND	5.97	L/s
MAXIMUM HOUR DEMAND	14.90	L/s

#### CCO-22-3501 - 770 Brookfield Phase 2-Building C & F - Fire Underwriters Survey

 Project:
 770 Brookfield Phase 2-Building C & F

 Project No.:
 CCO-22-3501

 Designed By:
 RRR

 Checked By:
 AJG

 Date:
 June 23, 2022

#### From the Fire Underwriters Survey (2020)

From Part II – Guide for Determination of Required Fire Flow Copyright I.S.O.: City of Ottawa Technical Bulletin ISTB-2018-02 Applied Where Applicable

A. BASE REQUIREMENT (Rounded to the nearest 1000 L/min)

F = 220 x C x VA Where: F = Required fire flow in liters per minute

 $\boldsymbol{\mathsf{C}}$  = Coefficient related to the type of construction.

A = The total floor area in square meters (including all storey's, but excluding basements at least 50 percent below grade) in

the building being considered.

**Construction Type** Non-Combustible Construction

C 0.8 A 21,294.7 m<sup>2</sup>

Total Floor Area (per the 2020 FUS Page 20 - Total Effective Area) 15,443.7 m<sup>2</sup> \*Unprotected Vertical Openings

 Calculated Fire Flow
 21,872.0 L/min

 22,000.0 L/min

**B. REDUCTION FOR OCCUPANCY TYPE (No Rounding)** 

From Page 24 of the Fire Underwriters Survey:

Limited Combustible -15%

Fire Flow 18,700.0 L/min

C. REDUCTION FOR SPRINKLER TYPE (No Rounding)

Fully Supervised Sprinklered -50%

Reduction -9,350.0 L/min

D. INCREASE FOR EXPOSURE (No Rounding)

	Separation Distance (m)	Cons.of Exposed Wall	Length Exposed Adjacent Wall (m)	Height (Stories)	Length-Height Factor		
Exposure 1	Over 30 m	Ordinary - Mass Timber (Unprotected)	100	2	200.0	0%	
Exposure 2	Over 30 m	Ordinary - Mass Timber (Unprotected)	126	2	252.0	0%	
Exposure 3	10.1 to 20	Fire Resistive - Non Combustible (Unprotected Openings)	66	6	396.0	8%	
Exposure 4	10.1 to 20	Fire Resistive - Non Combustible (Unprotected Openings)	18	6	108.0	8%	
					% Increase*	16%	

Increase\* 2,992.0 L/min

E. Total Fire Flow (Rounded to the Nearest 1000 L/min)

Fire Flow 12,342.0 L/min
Fire Flow Required\*\* 12,000.0 L/min

<sup>\*</sup>In accordance with Part II, Section 4, the Increase for separation distance is not to exceed 75%

<sup>\*\*</sup>In accordance with Section 4 the Fire flow is not to exceed 45,000 L/min or be less than 2,000 L/min

#### CCO-22-3501 - 770 Brookfield Phase 2-Building D - Fire Underwriters Survey

Project: 770 Brookfield Phase 2-Building D

Project No.: CCO-22-3501 Designed By: RRR Checked By: AJG June 23, 2022 Date:

#### From the Fire Underwriters Survey (2020)

From Part II – Guide for Determination of Required Fire Flow Copyright I.S.O.:

City of Ottawa Technical Bulletin ISTB-2018-02 Applied Where Applicable

#### A. BASE REQUIREMENT (Rounded to the nearest 1000 L/min)

 $F = 220 \times C \times VA$  Where: F = Required fire flow in liters per minute

 $\boldsymbol{\mathsf{C}}$  = Coefficient related to the type of construction.

A = The total floor area in square meters (including all storey's, but excluding basements at least 50 percent below grade) in

the building being considered.

#### **Construction Type Non-Combustible Construction**

С 9,421.9 m<sup>2</sup>

> Total Floor Area (per the 2020 FUS Page 20 - Total Effective Area) 6,296.2 m<sup>2</sup> \*Unprotected Vertical Openings

**Calculated Fire Flow** 13,965.3 L/min 14,000.0 L/min

#### **B. REDUCTION FOR OCCUPANCY TYPE (No Rounding)**

From Page 24 of the Fire Underwriters Survey:

-15% Limited Combustible

Fire Flow 11,900.0 L/min

#### C. REDUCTION FOR SPRINKLER TYPE (No Rounding)

**Fully Supervised Sprinklered** -50%

Reduction -5,950.0 L/min

#### D. INCREASE FOR EXPOSURE (No Rounding)

	Separation Distance (m)	Cons.of Exposed Wall	Length Exposed Adjacent Wall (m)	Height (Stories)	Length-Height Factor		
Exposure 1	3.1 to 10	Fire Resistive - Non Combustible (Unprotected Openings)	33	2	66.0	9%	
Exposure 2	10.1 to 20	Fire Resistive - Non Combustible (Unprotected Openings)	55	9	495.0	8%	
Exposure 3	Over 30 m	Ordinary - Mass Timber (Unprotected)	10	2	20.0	0%	
Exposure 4	10.1 to 20	Fire Resistive - Non Combustible (Unprotected Openings)	18	6	108.0	8%	
					% Increase*	25%	

2,975.0 L/min

#### E. Total Fire Flow (Rounded to the Nearest 1000 L/min)

Fire Flow	8,925.0 L/min
Fire Flow Required**	9,000.0 L/min

<sup>\*</sup>In accordance with Part II, Section 4, the Increase for separation distance is not to exceed 75%

<sup>\*\*</sup>In accordance with Section 4 the Fire flow is not to exceed 45,000 L/min or be less than 2,000 L/min

#### CCO-22-3501 - 770 Brookfield Phase 2 - Boundary Condition Unit Conversion

Project: 770 Brookfield Phase 2

Project No.: CCO-22-3501
Designed By: RRR

Checked By: AJG
Date: June 23, 2022

**Boundary Conditions Unit Conversion** 

#### BROOKFIELD ROAD & HOBSON ROAD

Scenario	Height (m)	Elevation (m)	m H <sub>2</sub> O	PSI	kPa
Avg. DD	130.0	75.5	54.5	77.5	534.4
Fire Flow - Brookfield (200 L/s or 12,000 L/min)	120.5	75.5	45.0	64.0	441.3
Fire Flow - Hobson (200 L/s or 12,000 L/min)	118.5	75.5	43.0	61.2	421.6
Peak Hour	123.8	75.5	48.3	68.7	473.6

#### **Alison Gosling**

**From:** Sharif, Golam <sharif.sharif@ottawa.ca>

**Sent:** June 23, 2022 12:25 PM

To: Ryan Robineau
Cc: Alison Gosling

**Subject:** RE: 770 Brookfield Road Boundary Condition Request

**Attachments:** 770 Brookfield Road June 2022.pdf

Follow Up Flag: Follow up Flag Status: Flagged

#### Hi Ryan,

Please see the requested BC below. I believe they had to put two connections to work the model. However, attached is the information.

The following are boundary conditions, HGL, for hydraulic analysis at 770 Brookfield Road (zone 2W2C) assumed to connected to the 203 mm on Brookfield Road and the 203 mm on Hobson Road (see attached PDF for location).

**Both Connections:** 

Minimum HGL: 123.8 m Maximum HGL: 130.0 m

Max Day + Fire Flow (200 L/s): 120.5 m (Connection 1) Max Day + Fire Flow (200 L/s): 118.5 m (Connection 2)

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

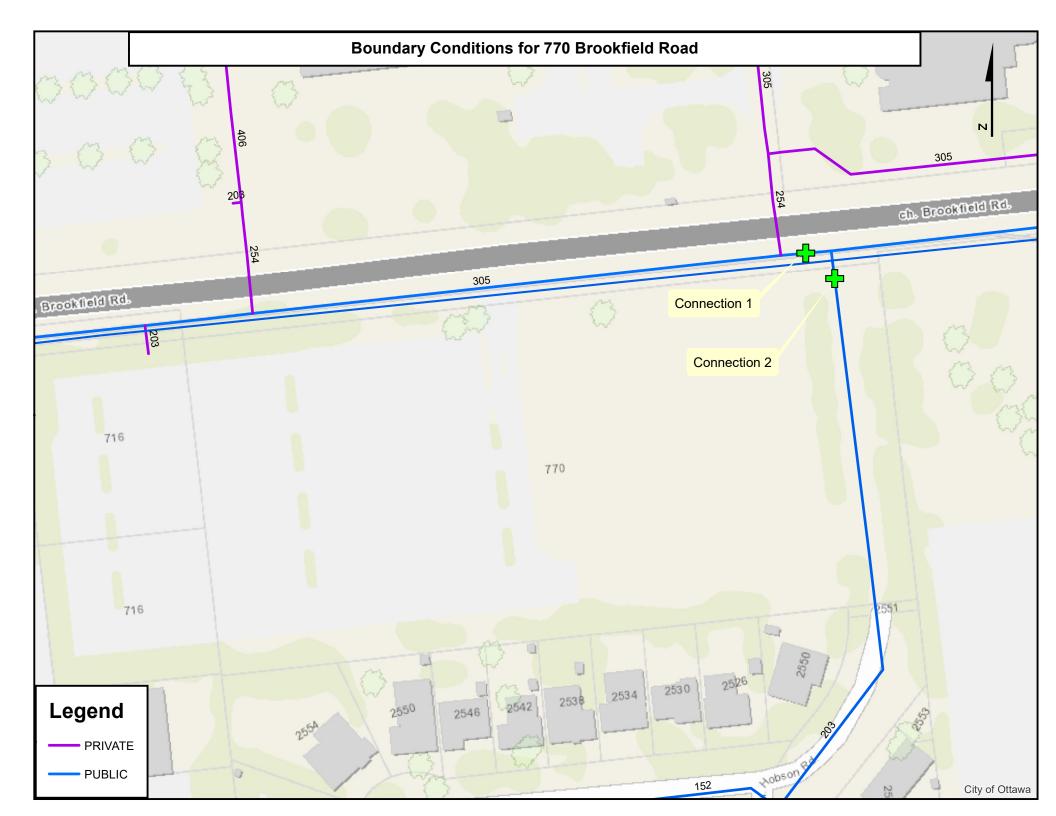
#### Thanks.

#### Sharif

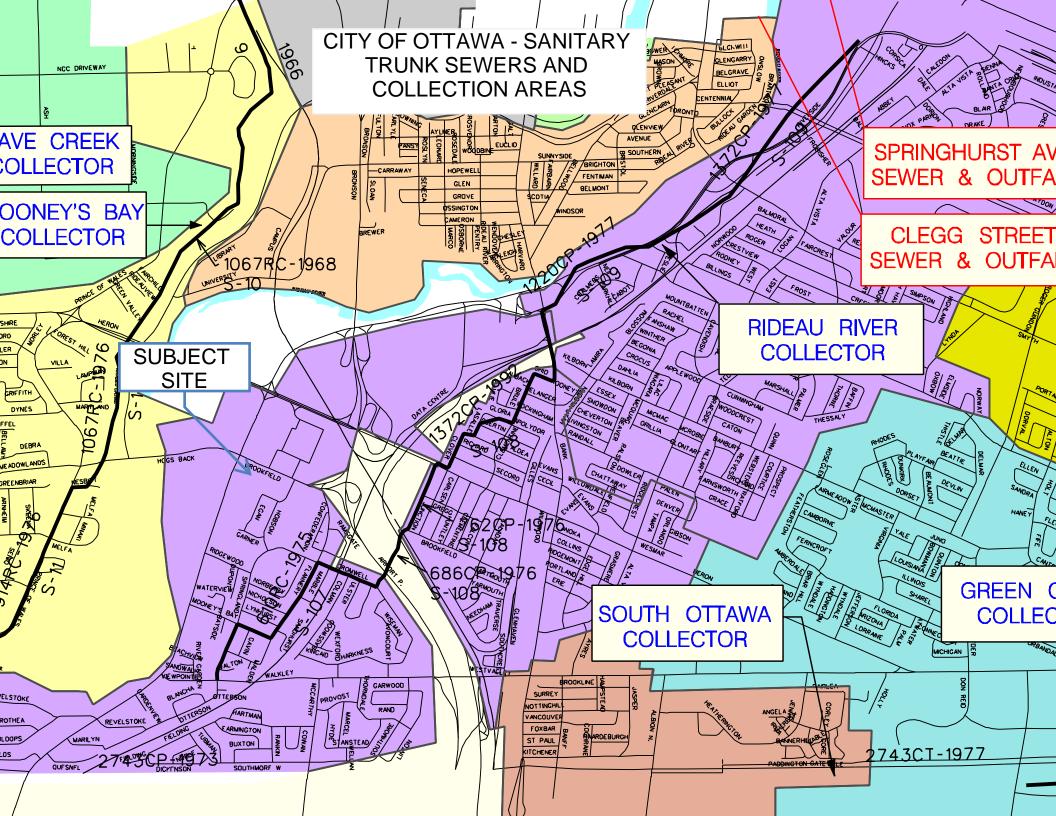
From: Ryan Robineau <r.robineau@mcintoshperry.com>

Sent: June 22, 2022 2:35 PM

To: Sharif, Golam <sharif.sharif@ottawa.ca>



APPENDIX D SANITARY CALCULATIONS



### CCO-22-3501 - 770 Brookfield Phase 2 - Block C & D - Sanitary Demands

770 Brookfield Phase 2 - Block C & D Project: CCO-22-3501 Project No.: Designed By: RRR Checked By: AJG Date: June 23, 2022 Site Area 0.91 Gross ha Bachelor 241 1.40 Persons per unit 1.40 1 Bedroom Persons per unit 70 2.10 2 Bedroom Persons per unit 29 3 Bedroom 3.10 Persons per unit 4 Bedroom 60 3.40 Persons per unit **Total Population** 833 Persons 579.00 m<sup>2</sup> Commercial Area 1325.00 m<sup>2</sup> **Amenity Space** 

#### **DESIGN PARAMETERS**

Institutional/Commercial Peaking Facto

1

**Residential Peaking Factor** 3.28 \* Using Harmon Formula =  $1+(14/(4+P^0.5))*0.8$ 

where P = population in thousands, Harmon's Correction Factor = 0.8

Mannings coefficient (n) 0.013

Demand (per capita) 280 L/day Infiltration allowance 0.33 L/s/Ha

#### **EXTRANEOUS FLOW ALLOWANCES**

Infiltration / Inflow	Flow (L/s)
Dry	0.05
Wet	0.25
Total	0.30

#### **AVERAGE DAILY DEMAND**

DEMAND TYPE	AMOUNT	UNITS	POPULATION / AREA	Flow (L/s)
Residential	280	L/c/d	833	2.70
Industrial - Light**	35,000	L/gross ha/d		0
Industrial - Heavy**	55,000	L/gross ha/d		0
Commercial / Amenity	2,800	L/(1000m² /d )	1904.00	0.06
Hospital	900	L/(bed/day)		0
Schools	70	L/(Student/d)		0
Trailer Parks no Hook-Ups	340	L/(space/d)		0
Trailer Park with Hook-Ups	800	L/(space/d)		0
Campgrounds	225	L/(campsite/d)		0
Mobile Home Parks	1,000	L/(Space/d)		0
Motels	150	L/(bed-space/d)		0
Hotels	225	L/(bed-space/d)		0
Office	75	L/7.0m <sup>2</sup> /d		0
Tourist Commercial	28,000	L/gross ha/d		0
Other Commercial	28,000	L/gross ha/d		0

AVERAGE RESIDENTIAL FLOW	2.70	L/s
PEAK RESIDENTIAL FLOW	8.85	L/s
AVERAGE ICI FLOW	0.06	L/s
PEAK INSTITUTIONAL/COMMERCIAL FLOW	0.06	L/s
PEAK INDUSTRIAL FLOW	0.00	L/s
TOTAL PEAK ICI FLOW	0.06	L/s

#### **TOTAL SANITARY DEMAND**

TOTAL ESTIMATED AVERAGE DRY WEATHER FLOW	2.81	L/s
TOTAL ESTIMATED PEAK DRY WEATHER FLOW	8.96	L/s
TOTAL ESTIMATED PEAK WET WEATHER FLOW	9.22	L/s

## SANITARY SEWER DESIGN SHEET

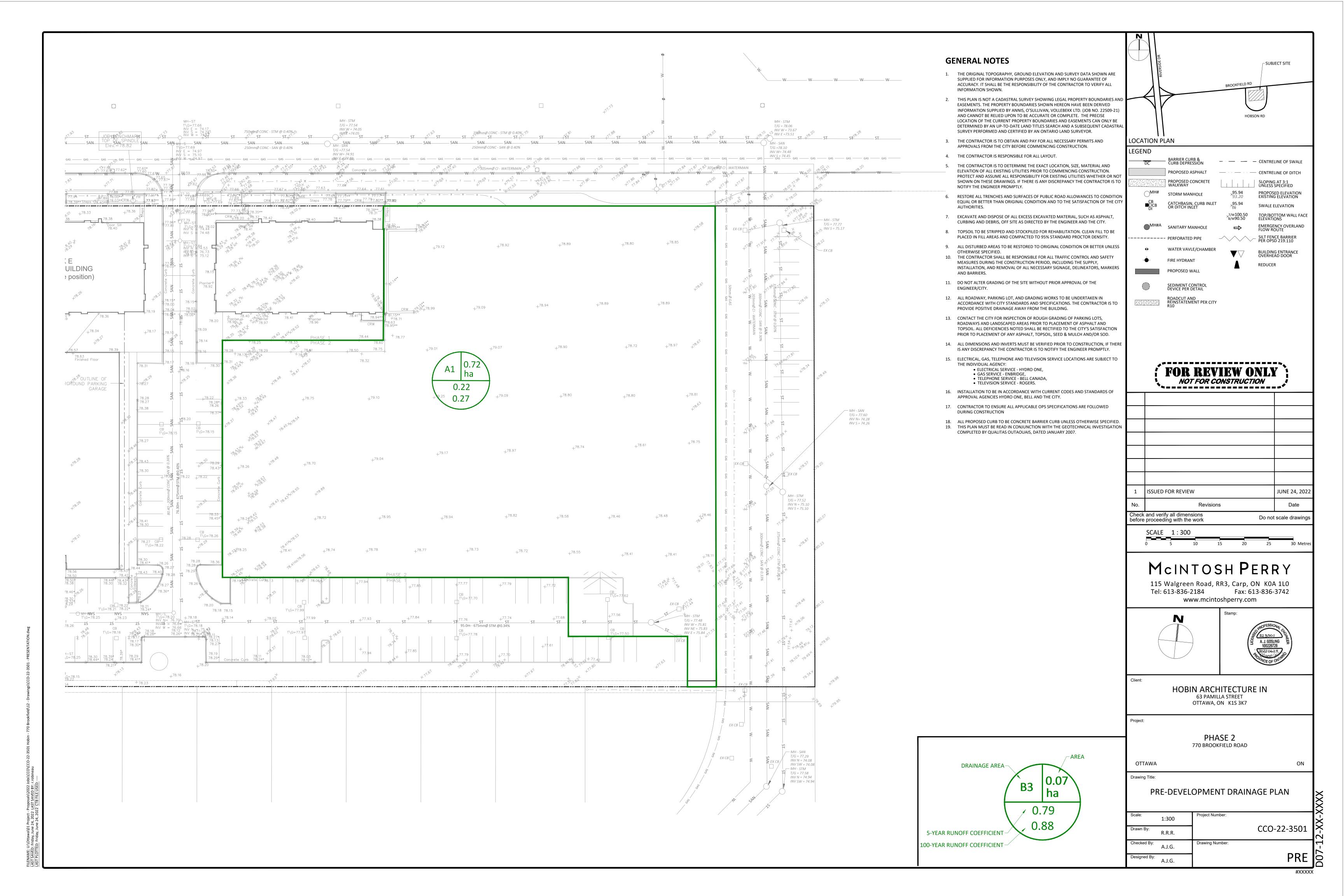
PROJECT: CCO-22-3501

LOCATION: 770 Brookfield Road - Phase 2

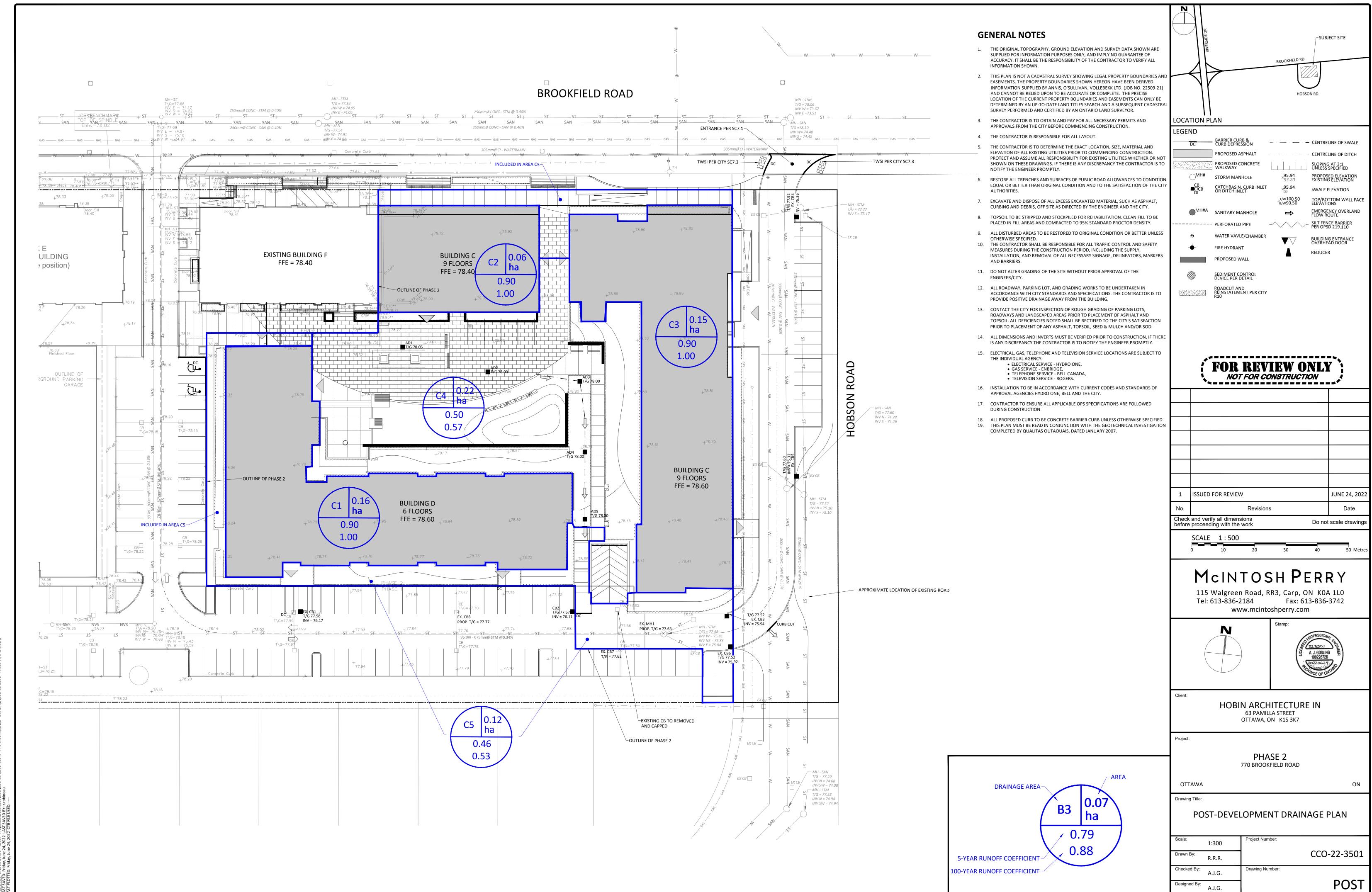
CLIENT: Hobin Architecture

	LOC	ATION							RESIDENTIA	L						ICI AREAS				INFILTR	ATION ALLC	OWANCE	FLOW				SEWER DAT	Α		
1	2	3	4		5	6	7	8	9	10	11	12	13	14 15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
						UNIT	TYPES		AREA	POPUI	LATION		PEAK		ARE	A (ha)			PEAK	AREA	4 (ha)	FLOW	DESIGN	CAPACITY	/ LENGTH	DIA	SLOPE	VELOCITY	AVAII	
STREET	AREA I		TC		BAC/1-BED	2-BED	3-BED	4-BED	(ha)	IND	CUM	PEAK	FLOW	INSTITUTIONAL	COMN	/IERCIAL	INDL	JSTRIAL	FLOW	IND	CUM	(L/s)	FLOW	(L/s)	(m)	(mm)	(%)	(full)	CAPA	<b>ACITY</b>
		MH	MI	Н	DAG/ 1-DED	Z-DLD	J-DED	T-DED	(Ha)	IIVD	COIVI	FACTOR	(L/s)	IND CUM	IND	CUM	IND	CUM	(L/s)	IND	COIVI	(L/ 3)	(L/s)	(L/ 3)	(111)	(11111)	(70)	(m/s)	L/s	(%)
		DI DC	FV C-		200	70	20	/0	0.01	022.0	022.0	2.20	0.05	0.00	0.10	0.10		0.00	0.07	1 10	1.10	0.27	0.20	24.22	0.00	200	1.00	1.055	24.04	70.00
		BLDG	EX. Se	ewer	280	70	29	60	0.91	833.0	833.0	3.28	8.85	0.00	0.19	0.19		0.00	0.06	1.10	1.10	0.36	9.28	34.22	8.93	200	1.00	1.055	24.94	72.88
				-					1										1						1	1				
																														$\overline{}$
Design Parameters:					Notes:							Designed:		RRR		No.				•	Revision		•	•				Date		
					1. Mannings				0.013							1.				ISSU	JED FOR RE\	/IEW						2022-06-24		
Residential		ICI Areas			2. Demand (	(per capita)	):	280	) L/day																					
BAC/1-																														
BED 1.4 p/p/u					3. Infiltratio			0.33	3 L/s/Ha			Checked:		AJG																
2-BED 2.1 p/p/u	INST	28,000 L/Ha/day	1		<ol><li>Residentia</li></ol>																									
3-BED 3.1 p/p/u	COM	28,000 L/Ha/day	1					14/(4+P^0.5)																						
4-BED 3.4 p/p/u	IND	35,000 L/Ha/day	MOE C	Chart	,	where P = p	population i	n thousands				Project No.	.:	CCO-22-3501																
																												Sheet No:		
																												1 of 1		

APPENDIX E PRE-DEVELOPMENT DRAINAGE PLAN



APPENDIX F POST-DEVELOPMENT DRAINAGE PLAN



XXXXX

APPENDIX G STORMWATER MANAGEMENT CALCULATIONS

### CCO-22-3501 - 770 Brookfield Phase 2 - Runoff Calculations

1 of 9

#### Pre-Development Runoff Coefficient

Drainage Area	Area (ha)	Impervious Area (m²)	С	Gravel Area (m²)	С	Pervious Area (m²)	С	C <sub>AVG</sub> 2/5-Year	C <sub>AVG</sub> 100-Year
PH2 - A1	0.718	217.36	0.90	0.00	0.60	6,958.44	0.20	0.22	0.27

### Pre-Development Runoff Calculations

Drainage Area	Area (ha)	C 5-Year	C 100 Voor	C Tc (mm/hr) Q (L/s)						
Alea	(Ha)	J-Teal	real 100-real (IIIII)		2-Year	5-Year	100-Year	2-Year	5-Year	100-Year
PH2 - A1	0.718	0.22	0.27	10	76.8	104.2	178.6	33.9	45.98	97.14
Total	0.718		-		•	•		33.89	45.98	97.14

#### Post-Development Runoff Coefficient

Drainage Area	Area (ha)	Impervious Area (m²)	С	Gravel Area (m²)	С	Pervious Area (m²)	С	C <sub>AVG</sub> 2/5-Year	C <sub>AVG</sub> 100-Year	
C1	0.159	1,587.44	0.90	0.00	0.60	0.00	0.20	0.90	1.00	Building D
C2	0.063	629.35	0.90	0.00	0.60	0.00	0.20	0.90	1.00	Building C West
C3	0.154	1,536.11	0.90	0.00	0.60	0.00	0.20	0.90	1.00	Building C East
C4	0.222	943.32	0.90	0.00	0.60	1,280.42	0.20	0.50	0.57	Controlled Cistern
C5	0.120	453.59	0.90	0.00	0.60	745.57	0.20	0.46	0.53	Uncontrolled

#### Post-Development Runoff Calculations

Drainage			Tc (min)		l (mm/hr)			Q (L/s)		
Area	(ha)	2/5-Year	100-real	(min)	2-Year	5-Year	100-Year	2-Year	5-Year	100-Year
C1	0.159	0.90	1.00	10	76.8	104.2	178.6	30.51	41.38	78.80
C2	0.063	0.90	1.00	10	76.8	104.2	178.6	12.09	16.41	31.24
C3	0.154	0.90	1.00	10	76.8	104.2	178.6	29.52	40.04	76.25
C4	0.222	0.50	0.57	10	76.8	104.2	178.6	23.60	32.01	62.72
C5	0.120	0.46	0.53	10	76.8	104.2	178.6	11.90	16.14	31.77
Total	0.718					•		95.71	145.99	280.78

### Required Restricted Flow

Drainage Area	Area (ha)	(L/s/ha) 2-Year	(L/s) 2-Year	
PH2 -A1	0.718	80.6	57.86	*Allowable release rate based on
Total	0.718		57.86	Management Report and Storm
		•		hy others

\*Allowable release rate based on Functional Servicing and Stormwater Management Report and Stormwater Management Memorandum prepared by others.

#### Post-Development Restricted Runoff Calculations

Drainage Area	Unrestricted Flow (L/s)		Restricted Flow (L/s)		Storage Required (m³)		9	Provided n <sup>3</sup> )
Area	5-Year	100-Year	5-Year	100-Year	5-Year	100-Year	5-Year	100-Year
C1	41.38	78.80	3.36	5.76	34.95	68.11	41.67	71.43
C2	16.41	31.24	1.26	2.16	14.15	27.52	16.52	28.32
C3	40.04	76.25	3.36	5.76	33.42	65.20	40.32	69.12
C4	32.01	62.72	6.33	12.41	18.57	36.07	36.07	36.07
C5	16.14	31.77	16.14	31.77				
Total	145.99	280.78	30.45	57.86	101.09	196.91	134.59	204.95

## CCO-22-3501 - 770 Brookfield Phase 2 - Runoff Calculations

### Storage Requirements for Area C1

5-Year Storm Event

5-Teal Storm Event					
Tc (min)	l (mm/hr)	Runoff (L/s) C1	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
30	53.9	21.41	3.36	18.05	32.49
40	44.2	17.56	3.36	14.20	34.07
50	37.7	14.97	3.36	11.61	34.84
60	32.9	13.07	3.36	9.71	34.95
70	29.4	11.68	3.36	8.32	34.93

Maximum Storage Required 5-year = 35 m<sup>3</sup>

#### 100-Year Storm Event

Tc (min)	l (mm/hr)	Runoff (L/s) C1	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
30	91.9	40.56	5.76	34.80	62.63
40	75.1	33.14	5.76	27.38	65.72
50	64.0	28.24	5.76	22.48	67.45
60	55.9	24.67	5.76	18.91	68.07
70	49.8	21.98	5.76	16.22	68.11
80	45.0	19.86	5.76	14.10	67.67
90	41.1	18.14	5.76	12.38	66.84
100	37.9	16.73	5.76	10.97	65.79
110	35.2	15.53	5.76	9.77	64.51
120	32.9	14.52	5.76	8.76	63.06

Maximum Storage Required 100-year = 68 m

### 5-Year Storm Event Storage Summary

Roof Storage						
Location	Area*	Depth	Volume (m³)			
Roof	1190.58	0.035	41.67			

Storage Available ( $m^3$ ) = 41.67 Storage Required ( $m^3$ ) = 34.95 2 of 9

### 100-Year Storm Event Storage Summary

Roof Storage					
Location	Area*	Depth	Volume (m³)		
Roof	1190.58	0.060	71.43		

Storage Available (m³) = 71.43 Storage Required (m³) = 68.11

<sup>\*</sup>Area is 75% of the total roof area

#### CCO-22-3501 - 770 Brookfield Phase 2 - Runoff Calculations

3 of 9

#### Roof Drain Flow (C1)

Roof Drains Summary					
Type of Control Device	ype of Control Device Watts Drainage - Accutrol Weir				
Number of Roof Drians	8				
5-Year 100-Year					
Rooftop Storage (m <sup>3</sup> )	41.67	71.43			
Storage Depth (m)	0.035	0.060			
Flow (Per Roof Drain) (L/s)	0.42	0.72			
Total Flow (L/s)	3.36	5.76			

Flow Rate Vs. Build-Up (One Weir)				
Depth (mm)	Flow (L/s)			
15	0.18			
20	0.24			
25	0.30			
30	0.36			
35	0.42			
40	0.48			
45	0.54			
50	0.60			
55	0.66			

<sup>\*</sup>Roof Drain model to be Accutrol Weirs, See attached sheets

### **CALCULATING ROOF FLOW EXAMPLES**

1 roof drain during a 5 year storm elevation of water = 25mm Flow leaving 1 roof drain = (1 x 0.30 L/s) = 0.30 L/s

1 roof drain during a 100 year storm elevation of water = 50mm Flow leaving 1 roof drain = (1 x 0.60 L/s) = 0.60 L/s

4 roof drains during a 5 year storm elevation of water = 25mm Flow leaving 4 roof drains = (4 x 0.30 L/s) = 1.20 L/s

4 roof drains during a 100 year storm elevation of water = 50mm Flow leaving 4 roof drains = (4 x 0.60 L/s) = 2.40 L/s

Roof Drain Flow					
Flow (I/s)	Storage Depth (mm)	Drains Flow (I/s)			
0.18	15	1.44			
0.24	20	1.92			
0.30	25	2.40			
0.36	30	2.88			
0.42	35	3.36			
0.48	40	3.84			
0.54	45	4.32			
0.60	50	4.80			
0.66	55	5.28			
0.72	60	5.76			
0.78	65	6.24			
0.84	70	6.72			
0.90	75	7.20			
0.96	80	7.68			
1.02	85	8.16			
1.08	90	8.64			
1.14	95	9.12			
1.20	100	9.60			
1.26	105	10.08			
1.32	110	10.56			
1.38	115	11.04			
1.44	120	11.52			
1.50	125	12.00			
1.56	130	12.48			
1.62	135	12.96			
1.68	140	13.44			
1.74	145	13.92			
1.80	150	14.40			

<u>Note:</u> The flow leaving through a restricted roof drain is based on flow vs. head information

<sup>\*</sup>Roof Drain Flow information taken from Watts Drainage website

#### CCO-22-3501 - 770 Brookfield Phase 2 - Runoff Calculations

### Storage Requirements for Area C2

5-Year Storm Event

Storage Runoff to Runoff Allowable Required (L/s) be Stored Outflow (min) (mm/hr) (L/s) (m<sup>3</sup>)(L/s)40 44.2 5.70 6.96 1.26 13.68

50 37.7 5.94 1.26 4.68 14.03 60 32.9 5.18 1.26 3.92 14.11 70 29.4 4.63 1.26 3.37 14.15 80 26.6 4.19 1.26 2.93 14.06

Maximum Storage Required 5-year = 14 m<sup>3</sup>

#### 100-Year Storm Event

Tc (min)	l (mm/hr)	Runoff (L/s) C2	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
30	91.9	16.08	2.16	13.92	25.05
40	75.1	13.14	2.16	10.98	26.35
50	64.0	11.20	2.16	9.04	27.11
60	55.9	9.78	2.16	7.62	27.43
70	49.8	8.71	2.16	6.55	27.52
80	45.0	7.87	2.16	5.71	27.42
90	41.1	7.19	2.16	5.03	27.17
100	37.9	6.63	2.16	4.47	26.83
110	35.2	6.16	2.16	4.00	26.39
120	32.9	5.76	2.16	3.60	25.89

Maximum Storage Required 100-year = 28 m<sup>3</sup>

### 5-Year Storm Event Storage Summary

Roof Storage						
Location	Area*	Depth	Volume (m³)			
Roof	472.01	0.035	16.52			
	•					

Storage Available (m³) = 16.52 Storage Required (m³) = 14.15 4 of 9

### 100-Year Storm Event Storage Summary

Roof Storage					
Area*	Depth	Volume (m³)			
472.01	0.060	28.32			
	Area*	Area* Depth			

Storage Available (m³) = 28.32 Storage Required (m³) = 27.52

<sup>\*</sup>Area is 75% of the total roof area

#### CCO-22-3501 - 770 Brookfield Phase 2 - Runoff Calculations

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#### Roof Drain Flow (C2)

Roof Drains Summary					
Type of Control Device	ol Device Watts Drainage - Accutrol Weir				
Number of Roof Drians	3				
	5-Year 100-Year				
Rooftop Storage (m <sup>3</sup> )	16.52	28.32			
Storage Depth (m)	0.035	0.060			
Flow (Per Roof Drain) (L/s)	0.42	0.72			
Total Flow (L/s)	1.26	2.16			

Flow Rate Vs. Build-Up (One Weir)		
Depth (mm)	Flow (L/s)	
15	0.18	
20	0.24	
25	0.30	
30	0.36	
35	0.42	
40	0.48	
45	0.54	
50	0.60	
55	0.66	

<sup>\*</sup>Roof Drain model to be Accutrol Weirs, See attached sheets

### **CALCULATING ROOF FLOW EXAMPLES**

1 roof drain during a 5 year storm elevation of water = 25mm Flow leaving 1 roof drain = (1 x 0.30 L/s) = 0.30 L/s

1 roof drain during a 100 year storm elevation of water = 50mm Flow leaving 1 roof drain = (1 x 0.60 L/s) = 0.60 L/s

4 roof drains during a 5 year storm elevation of water = 25mm Flow leaving 4 roof drains = (4 x 0.30 L/s) = 1.20 L/s

4 roof drains during a 100 year storm elevation of water = 50mm Flow leaving 4 roof drains = (4 x 0.60 L/s) = 2.40 L/s

Roof Drain Flow				
Flow (I/s)	Storage Depth (mm)	Drains Flow (I/s)		
0.18	15	0.54		
0.24	20	0.72		
0.30	25	0.90		
0.36	30	1.08		
0.42	35	1.26		
0.48	40	1.44		
0.54	45	1.62		
0.60	50	1.80		
0.66	55	1.98		
0.72	60	2.16		
0.78	65	2.34		
0.84	70	2.52		
0.90	75	2.70		
0.96	80	2.88		
1.02	85	3.06		
1.08	90	3.24		
1.14	95	3.42		
1.20	100	3.60		
1.26	105	3.78		
1.32	110	3.96		
1.38	115	4.14		
1.44	120	4.32		
1.50	125	4.50		
1.56	130	4.68		
1.62	135	4.86		
1.68	140	5.04		
1.74	145	5.22		
1.80	150	5.40		

Note: The flow leaving through a restricted roof drain is based on flow vs. head information

<sup>\*</sup>Roof Drain Flow information taken from Watts Drainage website

32.29

 $m^3$ 

#### CCO-22-3501 - 770 Brookfield Phase 2 - Runoff Calculations

### Storage Requirements for Area C3

24.3

5-Year Storm Event

Storage Runoff to Runoff Allowable Required (L/s) Outflow be Stored (min) (mm/hr) (L/s) (m<sup>3</sup>)(L/s)50 37.7 14.49 33.39 3.36 11.13 32.9 12.64 3.36 9.28 33.42 60 70 29.4 11.30 3.36 7.94 33.35 80 26.6 10.22 3.36 6.86 32.94

9.34

Maximum Storage Required 5-year = 33 m<sup>3</sup>

3.36

5.98

#### 100-Year Storm Event

90

Tc (min)	l (mm/hr)	Runoff (L/s) C3	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
30	91.9	39.24	5.76	33.48	60.27
40	75.1	32.07	5.76	26.31	63.15
50	64.0	27.33	5.76	21.57	64.71
60	55.9	23.87	5.76	18.11	65.20
70	49.8	21.27	5.76	15.51	65.13
80	45.0	19.22	5.76	13.46	64.59
90	41.1	17.55	5.76	11.79	63.67
100	37.9	16.18	5.76	10.42	62.55
110	35.2	15.03	5.76	9.27	61.19
120	32.9	14.05	5.76	8.29	59.68

Maximum Storage Required 100-year = 65

5-Year Storm Event Storage Summary

Roof Storage			
Location Area* Depth (			
Roof	1152.08	0.035	40.32

Storage Available (m³) = 40.32 Storage Required (m³) = 33.42

100-Year Storm Event Storage Summary

Roof Storage				
Location Area* Depth Volume (m³)				
Roof	1152.08	0.060	69.12	

Storage Available (m³) = 69.12 Storage Required (m³) = 65.20

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<sup>\*</sup>Area is 75% of the total roof area

#### CCO-22-3501 - 770 Brookfield Phase 2 - Runoff Calculations

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#### Roof Drain Flow (C3)

Roof Drains Summary				
Type of Control Device	Type of Control Device Watts Drainage - Accutrol Weir			
Number of Roof Drians	Number of Roof Drians 8			
	5-Year	100-Year		
Rooftop Storage (m <sup>3</sup> )	40.32	69.12		
Storage Depth (m)	0.035	0.060		
Flow (Per Roof Drain) (L/s)	0.42	0.72		
Total Flow (L/s)	3.36	5.76		

Flow Rate Vs. Build-Up (One Weir)		
Depth (mm)	Flow (L/s)	
15	0.18	
20	0.24	
25	0.30	
30	0.36	
35	0.42	
40	0.48	
45	0.54	
50	0.60	
55	0.66	

<sup>\*</sup>Roof Drain model to be Accutrol Weirs, See attached sheets

### **CALCULATING ROOF FLOW EXAMPLES**

1 roof drain during a 5 year storm elevation of water = 25mm Flow leaving 1 roof drain = (1 x 0.30 L/s) = 0.30 L/s

1 roof drain during a 100 year storm elevation of water = 50mm Flow leaving 1 roof drain = (1 x 0.60 L/s) = 0.60 L/s

4 roof drains during a 5 year storm elevation of water = 25mm Flow leaving 4 roof drains = (4 x 0.30 L/s) = 1.20 L/s

4 roof drains during a 100 year storm elevation of water = 50mm Flow leaving 4 roof drains = (4 x 0.60 L/s) = 2.40 L/s

	Roof Drain Flow				
Flow (I/s)	Storage Depth (mm)	Drains Flow (I/s)			
0.18	15	1.44			
0.24	20	1.92			
0.30	25	2.40			
0.36	30	2.88			
0.42	35	3.36			
0.48	40	3.84			
0.54	45	4.32			
0.60	50	4.80			
0.66	55	5.28			
0.72	60	5.76			
0.78	65	6.24			
0.84	70	6.72			
0.90	75	7.20			
0.96	80	7.68			
1.02	85	8.16			
1.08	90	8.64			
1.14	95	9.12			
1.20	100	9.60			
1.26	105	10.08			
1.32	110	10.56			
1.38	115	11.04			
1.44	120	11.52			
1.50	125	12.00			
1.56	130	12.48			
1.62	135	12.96			
1.68	140	13.44			
1.74	145	13.92			
1.80	150	14.40			

<u>Note:</u> The flow leaving through a restricted roof drain is based on flow vs. head information

<sup>\*</sup>Roof Drain Flow information taken from Watts Drainage website

### CCO-22-3501 - 770 Brookfield Phase 2 - Runoff Calculations

## Storage Requirements for Area C4

5-Year Storm Event

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Tc (min)	l (mm/hr)	Runoff (L/s) C4	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
20	70.3	21.60	6.33	15.27	18.32
25	60.9	18.71	6.33	12.38	18.57
30	53.9	16.56	6.33	10.23	18.41
35	48.5	14.90	6.33	8.57	18.00
40	44.2	13.58	6.33	7.25	17.40

Maximum Storage Required 5-year = 19

19 m<sup>3</sup>

#### 100-Year Storm Event

Tc (min)	l (mm/hr)	Runoff (L/s) C4	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
20	120.0	42.15	12.41	29.74	35.69
25	103.8	36.46	12.41	24.05	36.07
30	91.9	32.28	12.41	19.87	35.76
35	82.6	29.01	12.41	16.60	34.86
40	75.1	26.38	12.41	13.97	33.52
45	69.1	24.27	12.41	11.86	32.02
50	64.0	22.48	12.41	10.07	30.21
55	59.6	20.93	12.41	8.52	28.13
60	55.9	19.63	12.41	7.22	26.01
65	52.6	18.47	12.41	6.06	23.65

Maximum Storage Required 100-year = 36.07

## Cistern Storage

Storage Available (m³) =	36.07
Storage Required (m³) =	36.07

#### CCO-22-3501 - 770 Brookfield Phase 2 - Runoff Calculations

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#### Time of Concentration Pre-Development

Drainage Area	Sheet Flow	Slope of	Tc (min)	Tc (min)
ID	Distance (m)	Land (%)	(5-Year)	(100-Year)
A1	21	2.10	10	2

\*Therefore, a Tc of 10 can be used

Tc= (3.26(1.1-c)L^0.5/S^0.33)

c= Balanced Runoff Coefficient
 L= Length of Drainage Area
 S= Average Slope of Watershed

## STORM SEWER DESIGN SHEET

PROJECT: CCO-22-3501
LOCATION: 770 Brookfield
CLIENT: Hobin Architecture

	LOCATION				CONTRIBUTING AREA (ha)							RATIO	ONAL DESIGN	FLOW									SEWER DATA	١			
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28
STREET	AREA ID	FROM	TO	C-VALUE	AREA	INDIV	CUMUL	INLET	TIME	TOTAL	i (5)	i (10)	i (100)		10yr PEAK		FIXED		CAPACITY	LENGTH		PIPE SIZE (mr	n)	SLOPE	VELOCITY	AVAIL C	AP (5yr)
JIKEET	ANLATO	MH	MH	C-VALUE	ANLA	AC	AC	(min)	IN PIPE	(min)	(mm/hr)	(mm/hr)	(mm/hr)	FLOW (L/s)	(L/s)	(m)	DIA	W	Н	(%)	(m/s)	(L/s)	(%)				
Hobson Road	C1, C2, C3	BLDG	EX. 375mn	0.90	0.38	0.34	0.34	10.00	0.17	10.17	104.19	122.14	178.56	7.98					62.04	12.25	250			1.00	1.224		
	C4		Sewr	0.50	0.22	0.11	0.45	10.00	0.17	10.17	104.19	122.14	178.56	6.33				14.31	62.04	12.25	250			1.00	1.224	47.73	76.93%
Definitions:				Notes:				Designed:		RRR			No.					Revision							Date		
Q = 2.78CiA, where:				1. Mannings coefficient (n) =	:		0.013						1.				ISS	SUED FOR REVI	EW								
Q = Peak Flow in Litre																											
A = Area in Hectares								Checked:		AJG																	
	in millimeters per hour (m																										
[i = 998.071 / (TC+		5 YEAR																									
[i = 1174.184 / (TC	+6.014)^0.816]	10 YEAR		1				Project No.:		CCO-22-3501																	
[i = 1735.688 / (TC	+6.014)^0.820]	100 YEAR		1													Da	ite:		_		_			Sheet No:		•
																	2022	-06-24							1 of 1		

APPENDIX H
CITY OF OTTAWA DESIGN CHECKLIST

# City of Ottawa

# 4. Development Servicing Study Checklist

The following section describes the checklist of the required content of servicing studies. It is expected that the proponent will address each one of the following items for the study to be deemed complete and ready for review by City of Ottawa Infrastructure Approvals staff.

The level of required detail in the Servicing Study will increase depending on the type of application. For example, for Official Plan amendments and re-zoning applications, the main issues will be to determine the capacity requirements for the proposed change in land use and confirm this against the existing capacity constraint, and to define the solutions, phasing of works and the financing of works to address the capacity constraint. For subdivisions and site plans, the above will be required with additional detailed information supporting the servicing within the development boundary.

## 4.1 General Content

Criteria	Location (if applicable)
Executive Summary (for larger reports only).	N/A
Date and revision number of the report.	On Cover
<ul> <li>Location map and plan showing municipal address, boundary, and layout of proposed development.</li> </ul>	Appendix A
$\ \square$ Plan showing the site and location of all existing services.	Site Servicing Plan (C102)
Development statistics, land use, density, adherence to zoning and official plan, and reference to applicable subwatershed and watershed plans that provide context to which individual.	<ul><li>1.1 Purpose</li><li>1.2 Site Description</li></ul>
watershed plans that provide context to which individual developments must adhere.	·
	6.0 Stormwater Management
<ul> <li>Summary of pre-consultation meetings with City and other approval agencies.</li> </ul>	Appendix B
<ul> <li>Reference and confirm conformance to higher level studies and reports (Master Servicing Studies, Environmental Assessments,</li> </ul>	1.1 Purpose
Community Design Plans), or in the case where it is not in conformance, the proponent must provide justification and	1.2 Site Description
develop a defendable design criteria.	6.0 Stormwater Management
$\square$ Statement of objectives and servicing criteria.	3.0 Pre-Consultation Summary



☐ Identification of existing and proposed infrastructure available in the immediate area.	N/A
☐ Identification of Environmentally Significant Areas, watercourses and Municipal Drains potentially impacted by the proposed development (Reference can be made to the Natural Heritage Studies, if available).	Site Grading Plan (C101)
☐ Concept level master grading plan to confirm existing and proposed grades in the development. This is required to confirm the feasibility of proposed stormwater management and drainage, soil removal and fill constraints, and potential impacts to neighbouring properties. This is also required to confirm that the proposed grading will not impede existing major system flow paths.	Site Grading Plan (C101)
<ul> <li>Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts.</li> </ul>	N/A
☐ Proposed phasing of the development, if applicable.	N/A
Reference to geotechnical studies and recommendations concerning servicing.	Section 2.0 Background Studies, Standards and References
<ul> <li>All preliminary and formal site plan submissions should have the following information:</li> <li>Metric scale</li> <li>North arrow (including construction North)</li> <li>Key plan</li> <li>Name and contact information of applicant and property owner</li> <li>Property limits including bearings and dimensions</li> <li>Existing and proposed structures and parking areas</li> <li>Easements, road widening and rights-of-way</li> <li>Adjacent street names</li> </ul>	Site Grading Plan (C101)

# 4.2 Development Servicing Report: Water

Criteria	Location (if applicable)
☐ Confirm consistency with Master Servicing Study, if available	N/A
<ul> <li>Availability of public infrastructure to service proposed development</li> </ul>	N/A
☐ Identification of system constraints	N/A
☐ Identify boundary conditions	Appendix C
☐ Confirmation of adequate domestic supply and pressure	N/A
<ul> <li>Confirmation of adequate fire flow protection and confirmation that fire flow is calculated as per the Fire Underwriter's Survey.</li> <li>Output should show available fire flow at locations throughout the development.</li> </ul>	Appendix C
<ul> <li>Provide a check of high pressures. If pressure is found to be high, an assessment is required to confirm the application of pressure reducing valves.</li> </ul>	N/A
<ul> <li>Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defined phases of the project including the ultimate design</li> </ul>	N/A
☐ Address reliability requirements such as appropriate location of shut-off valves	N/A
☐ Check on the necessity of a pressure zone boundary modification.	N/A
Reference to water supply analysis to show that major infrastructure is capable of delivering sufficient water for the proposed land use. This includes data that shows that the expected demands under average day, peak hour and fire flow conditions provide water within the required pressure range	Appendix C, Section 4.2

<ul> <li>Description of the proposed water distribution network, including locations of proposed connections to the existing system, provisions for necessary looping, and appurtenances (valves, pressure reducing valves, valve chambers, and fire hydrants) including special metering provisions.</li> </ul>	Site Servicing Plan (C101)
<ul> <li>Description of off-site required feedermains, booster pumping stations, and other water infrastructure that will be ultimately required to service proposed development, including financing, interim facilities, and timing of implementation.</li> </ul>	N/A
☐ Confirmation that water demands are calculated based on the City of Ottawa Design Guidelines.	Appendix C
<ul> <li>Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference.</li> </ul>	N/A

# 4.3 Development Servicing Report: Wastewater

Criteria	Location (if applicable)
☐ Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitored flow data from relatively new infrastructure cannot be used to justify capacity requirements for proposed infrastructure).	N/A
Confirm consistency with Master Servicing Study and/or justifications for deviations.	N/A
☐ Consideration of local conditions that may contribute to extraneous flows that are higher than the recommended flows in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers.	N/A
Description of existing sanitary sewer available for discharge of wastewater from proposed development.	Section 5.2 Proposed Sanitary Sewer

☐ Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable)	Section 5.3 Proposed Sanitary Design
☐ Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format.	N/A
<ul> <li>Description of proposed sewer network including sewers, pumping stations, and forcemains.</li> </ul>	Section 5.2 Proposed Sanitary Sewer
☐ Discussion of previously identified environmental constraints and impact on servicing (environmental constraints are related to limitations imposed on the development in order to preserve the physical condition of watercourses, vegetation, soil cover, as well as protecting against water quantity and quality).	N/A
<ul> <li>Pumping stations: impacts of proposed development on existing pumping stations or requirements for new pumping station to service development.</li> </ul>	N/A
☐ Forcemain capacity in terms of operational redundancy, surge pressure and maximum flow velocity.	N/A
☐ Identification and implementation of the emergency overflow from sanitary pumping stations in relation to the hydraulic grade line to protect against basement flooding.	N/A
☐ Special considerations such as contamination, corrosive environment etc.	N/A

# 4.4 Development Servicing Report: Stormwater Checklist

Criteria	Location (if applicable)
<ul> <li>Description of drainage outlets and downstream constraints including legality of outlets (i.e. municipal drain, right-of-way, watercourse, or private property)</li> </ul>	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
☐ Analysis of available capacity in existing public infrastructure.	N/A
<ul> <li>A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns, and proposed drainage pattern.</li> </ul>	Pre & Post-Development Plans
☐ Water quantity control objective (e.g. controlling post-development peak flows to pre-development level for storm events ranging from the 2 or 5-year event (dependent on the receiving sewer design) to 100-year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
☐ Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
<ul> <li>Description of the stormwater management concept with facility locations and descriptions with references and supporting information.</li> </ul>	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
Set-back from private sewage disposal systems.	N/A
☐ Watercourse and hazard lands setbacks.	N/A
Record of pre-consultation with the Ontario Ministry of Environment and the Conservation Authority that has jurisdiction on the affected watershed.	N/A
☐ Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists.	N/A
☐ Storage requirements (complete with calculations) and conveyance capacity for minor events (1:5-year return period) and major events (1:100-year return period).	Appendix G

☐ Identification of watercourses within the proposed development and how watercourses will be protected, or, if necessary, altered by the proposed development with applicable approvals.	Site Grading Plan
Calculate pre-and post development peak flow rates including a description of existing site conditions and proposed impervious areas and drainage catchments in comparison to existing conditions.	Section 7.0 Proposed Stormwater Management Appendix G
Any proposed diversion of drainage catchment areas from one outlet to another.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
<ul> <li>Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and stormwater management facilities.</li> </ul>	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
☐ If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post-development flows up to and including the 100-year return period storm event.	N/A
☐ Identification of potential impacts to receiving watercourses	N/A
Identification of municipal drains and related approval requirements.	N/A
<ul> <li>Descriptions of how the conveyance and storage capacity will be achieved for the development.</li> </ul>	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
100-year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading.	Site Grading Plan (C101)
☐ Inclusion of hydraulic analysis including hydraulic grade line elevations.	N/A

<ul> <li>Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors.</li> </ul>	Section 8.0 Sediment & Erosion Control
☐ Identification of floodplains – proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions.	N/A
<ul> <li>Identification of fill constraints related to floodplain and geotechnical investigation.</li> </ul>	N/A

## 4.5 Approval and Permit Requirements: Checklist

The Servicing Study shall provide a list of applicable permits and regulatory approvals necessary for the proposed development as well as the relevant issues affecting each approval. The approval and permitting shall include but not be limited to the following:

Criteria	Location (if applicable)
☐ Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act.	N/A
<ul> <li>Application for Certificate of Approval (CofA) under the Ontario Water Resources Act.</li> </ul>	N/A
☐ Changes to Municipal Drains.	N/A
☐ Other permits (National Capital Commission, Parks Canada, Public Works and Government Services Canada, Ministry of Transportation etc.)	N/A

# 4.6 Conclusion Checklist

Criteria	Location (if applicable)
☐ Clearly stated conclusions and recommendations	Section 9.0 Summary
	Section 10.0 Recommendations
☐ Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency.	All are stamped
☐ All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario	All are stamped