

**REPORT** 

# SITE SERVICING REPORT Herongate HG-5 2851 Baycrest Drive

Project: 135142-6.03.04



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# 1 INTRODUCTION

## 1.1 Scope

The purpose of this report is to outline the required municipal services, including water supply, stormwater management and wastewater disposal, needed to support the redevelopment of the subject property. The property is approximately 1.19 hectares in area and is currently identified as 2851 Baycrest Drive.

The site is bound by future Herongate Developments phases to the west and south (previously existing residential developments have recently been demolished), Heron Road to the north, and Sandalwood Drive to the east.

This Site Servicing Study, which also includes the Stormwater Management Plan, Watermain Analysis and Erosion and Sedimentation Control Plans, is being completed in support of the Site Plan Application.

## 1.2 Subject Site

Hazelview Investments proposes to construct 3 residential towers, two at 7 stories and one at 6 stories with a total of 305 dwelling units. The proposed development also includes a common underground parking structure linking the three towner and spanning the full extent of the site limits. Vehicular access to the site will be from a new private drive linking Baycrest and Sandalwood Drives along the south limit of the site.

The site currently consists of vacant land. All existing structures within the subject property have been previously demolished to facilitate the proposed development.

#### 1.3 Previous Studies

In May 2021 Hazelview Investments completed a Functional Servicing and Stormwater Management Report (FSR) for their Herongate Community. The subject lands of this report are identified as building 2 on the FSR. It should be noted that the lands subject of this report represents 50% of the total area of the Building 2 area of the FSR. Notes from the FSR will be included in each of the following water, sanitary and storm servicing sections within this report. In general, the recommendations contained within this report follow the recommendations of the approved FSR.

IBI GROUP REPORT SITE SERVICING REPORT HERONGATE HG-5 Prepared for Hazelview Investments

Please provide a brief description of the boundary conditions received and confirm the pressures during the max day, max hourly, and max day + FF.

# 2 WATER DISTRIBUTION

Boundary conditions received from the City are now included in Appendix A and pressures now included.

## 2.1 Existing Conditions

Adjacent to the site there is an existing 305 mm diameter cast iron watermain, located within the Heron Road right of way and a 203 mm diameter cast iron watermain in the Sandalwood Drive right of way. These watermains fall within the City of Ottawa's pressure zone 2W2C which will provide the water supply to the site.

## 2.2 Design Criteria

#### 2.2.1 Water Demands

The population for apartment buildings is assumed at 1.8 persons per unit as found in Table 4.1 of the Design Guidelines. A watermain demand calculation sheet is included in **Appendix A** and the total water demands are summarized as follows:

	Subject Site
Average Day	1.78 l/s
Maximum Day	4.45 l/s
Peak Hour	9.79 l/s

#### 2.2.2 System Pressure

The Ottawa Design Guidelines – Water Distribution (WDG001), July 2010, City of Ottawa, Clause 4.2.2 states that the preferred practice for design of a new distribution system is to have normal operating pressures range between 345 kPa (50 psi) and 480 kPa (80 psi) under maximum daily flow conditions. Other pressure criteria identified in Clause 4.2.2 of the guidelines are as follows:

Minimum Pressure Minimum system pressure under peak hour demand conditions shall not

be less than 276 kPa (40 psi)

Fire Flow During the period of maximum day demand, the system pressure shall

not be less than 140 kPa (20 psi) during a fire flow event.

Maximum Pressure In accordance with the Ontario Building/Plumbing Code, the maximum

pressure should not exceed 552 kPa (80 psi). Pressure reduction controls will be required for buildings where it is not possible/feasible to

maintain the system pressure below 552 kPa.

#### 2.2.3 Fire Flow Rates

A calculation using the Fire Underwriting Survey (FUS) method was conducted on the largest building (Building A) to determine the fire flow requirement for the site. The building is considered non-combustible construction. Results of the analysis provides a maximum fire flow rate of 9,000 l/min or 150 l/s is required which less than the 12,000 l/min estimated in the FSR confirming the systems capability. A copy of the FUS calculation is included in **Appendix A**.

# 2.3 Proposed Water Plan

To service the property twin 152mm dia water services are proposed, both connections are proposed to the 203 mm watermain located within the Sandalwood Drive ROW. A new valve box separating the twin services is also proposed, see site servicing plan 135143-C-001 in **Appendix D.** The proposed 152mm dia services will provide adequate supply to the building to meet demands while twining the service will provide service redundancy for this building.

With 2 AA hydrants within 75m of the building the minimum number of hydrants needed to deliver the required fire flow to the structure is being provided in accordance with Technical Bulletin ISTB-2018-02 dated March 21, 2018. Furthermore, the fire dept. connection is located within 45m of a hydrant which is located on Heron Road at the north property line, as such a new hydrant is not needed.

BUILDING ID	FIRE FLOW DEMAND (L/MIN)	FIRE HYDRANT(S) WITHIN 75M (5,700 L/MIN)	FIRE HYDRANT(S) WITHIN 150M (3,800 L/MIN)	COMBINED FIRE FLOW (L/MIN)
HG-5	9,000	1	1	9,500

# Boundary conditions from FSR now included in Appendix B.

# 3 WASTEWATER

## 3.1 Existing Conditions

Please provide the boundary conditions that were identified in FSR.

Adjacent to the site is a 300mm concrete sanitary sewer located in the Heron Road ROW draining eastward. Additionally, there is a 250mm concrete sanitary sewer located in the Sandalwood Drive ROW draining southward. In keeping with the FSR all sanitary flows from the subject site will be directed to the Heron Road sanitary sewer.

## 3.2 Design Criteria

The sanitary sewers for the subject site will be based on the City of Ottawa design criteria. It should be noted that the sanitary sewer design for this study incorporates the latest City of Ottawa design parameters identified in Technical Bulletin ISTB-2018-01. Some of the key criteria will include the following:

Commercial/Institutional flow 28,000 l/ha/d
 Residential flow 280 l/c/d

• Peaking factor 1.5 if ICI in contributing area >20%

1.0 if ICI in contributing area <20%

Infiltration allowance 0.33 l/s/ha

• Velocities 0.60 m/s min. to 3.0 m/s max.

Given the above criteria, total wastewater flow from the proposed development will 6.37 l/s, the detailed sanitary sewer calculations are included in **Appendix B**. The detailed design peak flow noted above is less than the peak flow identified in the FSR and is therefore in keeping with the approved report.

#### 3.3 Recommended Wastewater Plan

A 200mm dia sanitary service lateral is proposed to connect to the existing sanitary sewer in Heron Road to service this site. Please refer to the site servicing plan 135142-C-001 in **Appendix D** for connection location details.

#### STORMWATER SYSTE This site appears to be 4

#### 4.1 **Existing Conditions**

Currently adjacent to the site is are two 750mm concrest based on the L/s/ha ROW and a 300mm concrete storm sewer located in the release rate identified

Further to the east within the Baycrest Drive ROW is review and revise has identified this sewer as the outlet for the subject la accordingly.

less than the 50% identified in the FSR. Release rate should be

in the FSR. Please

the Heron Road

sewer, the FSR

#### 4.2 **Design Criteria**

The approved FSR has established target release rates for the subject blocks of development. As noted above, the current application represents 50% of the FSR Block 2 lands, as such the release rate for Block 2 will be taken at 50% for the subject application.

FSR Block 2 100 Year Release Rate = 223.54 l/sec

Taken at 50% for subject application - 100 year release rate = 111.77 l/sec

Plan now included detailing proposed area to be developed and release rate revised.

The stormwater system was designed following the principles of dual drainage, making accommodations for both major and minor flow.

Some of the key criteria include the following:

Design Storm 1:2 year return (Ottawa)

1:100 year return (External

Areas)

Rational Method Sewer Sizing

Initial Time of Concentration 10 minutes

Runoff Coefficients

Landscaped Areas C = 0.30Asphalt/Concrete C = 0.90C = 0.90Roof

Pipe Velocities 0.80 m/s to 6.0 m/s

250 mm diameter Minimum Pipe Size

(200 mm CB Leads)

#### 4.3 **Proposed Minor System**

The detailed design for this site shows a storm sewer connection through the proposed/future private road to the storm sewer at Baycrest Drive as noted in section 4.1

Using the above-noted criteria, the proposed storm sewer connection was sized accordingly.

December 23, 2021 5

## 4.4 Stormwater Management

The subject site will be limited to a release rate established using the criteria described in section 4.2. This will be achieved through roof flow control devices and an inlet control device (ICD) at the outlet of the cistern and ICDs at the road catchbasins.

Flows generated that are in excess of the site's allowable release rate will be stored both on road sags outside of the building garage footprint or within the building via rooftop storage and cistern located at the parking garage structure for flows from on top of the building/garage areas.

At certain locations within the site, the opportunity to store runoff is limited due to grading constraints and building geometry. These locations are generally located at the perimeter of the site where it is necessary to tie into public boulevards and adjacent properties, and it is not always feasible to capture or store stormwater runoff.

In this case, a portion of the building frontage at the Heron Road and Sandalwood Drive intersection will discharge uncontrolled to the street CBs. This uncontrolled area, 0.009 hectares in total, have a C value of 0.45. Based on 1:100 year storm uncontrolled flows, the uncontrolled areas generate 2.01 l/s runoff (refer to Section 4.5 for calculation). The cistern (and rooftops) have been sized to control water generated during the 1:100-year event, with no overflow leaving the site. Please refer to the SWM calculations in **Appendix** This release rate will

#### 4.5 Inlet Controls

The allowable release rate for the 1.19 Ha site as estab

Q<sub>allowable</sub> = 111.77 L/sec

Revised.

As noted in Section 4.4, a portion of the site will be left to discharge to the surrounding boulevard at an uncontrolled rate.

Based on a 1:100 year event, the flow from the 0.009 Ha uncontrolled areas can be determined as:

 $Q_{uncontrolled} = 2.78 \times C \times i_{100yr} \times A \quad where:$ 

**C** = Average runoff coefficient of uncontrolled area = 0.45

i<sub>100yr</sub> = Intensity of 100-year storm event (mm/hr)

=  $1735.688 \times (T_c + 6.014)^{0.820} = 178.56 \text{ mm/hr}$ ; where  $T_c = 10 \text{ minutes}$ 

change based on the

L/s/ha release rate established in the FSR

A = Uncontrolled Area = 0.009 Ha

Therefore, the uncontrolled release rate can be determined as:

Quncontrolled =  $2.78 \times C \times i_{100yr} \times A$ =  $2.78 \times 0.45 \times 178.56 \times 0.009$ 

= 2.01L/s

The maximum allowable release rate from the remainder of the site can then be determined as:

Q<sub>max allowable</sub> = Q<sub>restricted</sub> - Q<sub>uncontrolled</sub>

= 111.77 L/s - 2.01 L/s

= 109.76 L/s

# Please provide details for the cistern design for example relevant elevations.

the water elevation in

the cistern? Please

#### 4.6 On-Site Detention

As noted in section 4.4 any excess storm water up to the 100-year event is to be stored on-site via roof top storage and within the building cistern in order to not surcharge the downstream municipal storm sewer system. As the cistern is located inside the building, coordination with the architect, structural and mechanical engineers will be needed to design the structure and associated inlet control device.

#### 4.6.1 Site Inlet Control

The following Table summarizes the on-site storage requirements during both the 1:5-year and 1:100-year events.

ICD	TRIBUTARY	AVAILABLE	100-YEAI	RSTORM	5-YEAR S	STORM
AREA	AREA	STORAGE (M³)	RESTRICTE D FLOW (L/S)	REQUIRED STORAGE (M³)	RESTRICTED FLOW (L/S)	REQUIRED STORAGE (M³)
Cistern/Roof	0.90	341	45	340.45	45	132.35
Private Drive	0.463	110	64	107.15	64	34.12
TOTAL	1.363	451	109	447.6	109	166.47

In all instances the required storage is met (with some rooftop storage needed). The cistern will be fitted with a mechanical constant flow pump set at 45 litres/second.

Revised.

#### 4.6.2 Overall Release Rate

As demonstrated above, the site uses an inlet control device to restrict the 100 clarify. to the criteria approved by the City of Ottawa. Restricted stormwater will be contained onsite by surface ponding in the private drive and rooftop storage and the building cistern. In the 100 year event, there will be no overflow off-site from restricted areas.

The sum of restrictions on the site is 109 l/s, which is less than the allowable release of 109.76 l/s noted in section 4.5.

The technical details for the rooftop storage will be provided by the mechanical engineer as part of their design submission. The surface ponding areas are now included in this report.

Please provide the technical details and calculations for the rooftop storage and surface ponding areas.

## 5 SEDIMENT AND EROSION CONTROL PLAN

During construction, existing storm water conveyance systems can be exposed to significant sediment loadings. A number of construction techniques designed to reduce unnecessary construction sediment loadings may be used such as;

- Filter socks will remain on open surface structures such as manholes and catchbasins until these structures are commissioned and put into use;
- Installation of silt fence, where applicable, around the perimeter of the proposed work area.

During construction of the services, any trench dewatering using pumps will be fitted with a "filter sock." Thus, any pumped groundwater will be filtered prior to release to the existing surface runoff. The contractor will inspect and maintain the filter sock as needed including sediment removal and disposal.

All catchbasins, and to a lesser degree manholes, convey surface water to sewers. Consequently, until the surrounding surface has been completed these structures will be protected with a sediment capture filter sock to prevent sediment from entering the minor storm sewer system. These will stay in place and be maintained during construction and build-out until it is appropriate to remove them.

The Sediment and Erosion Control Plan 135142-C-010 is included in Appendix D.

## 6 CONCLUSIONS

Municipal water, wastewater and stormwater systems required to accommodate the proposed development are available to service the proposed development. Prior to construction, existing sewers are to be CCTV inspected to assess sewer condition.

This report has demonstrated sanitary and storm flows from and water supply to the subject site can be accommodated by the existing infrastructure. Also, the proposed servicing has been designed in accordance with MECP and City of Ottawa current level of service requirements.

The use of lot level controls, conveyance controls and end of pipe controls outlined in the report will result in effective treatment of surface stormwater runoff from the site. Adherence to the sediment and erosion control plan during construction will minimize harmful impacts on surface water

Based on the information provided herein, the development can be serviced to meet City of Ottawa requirements.

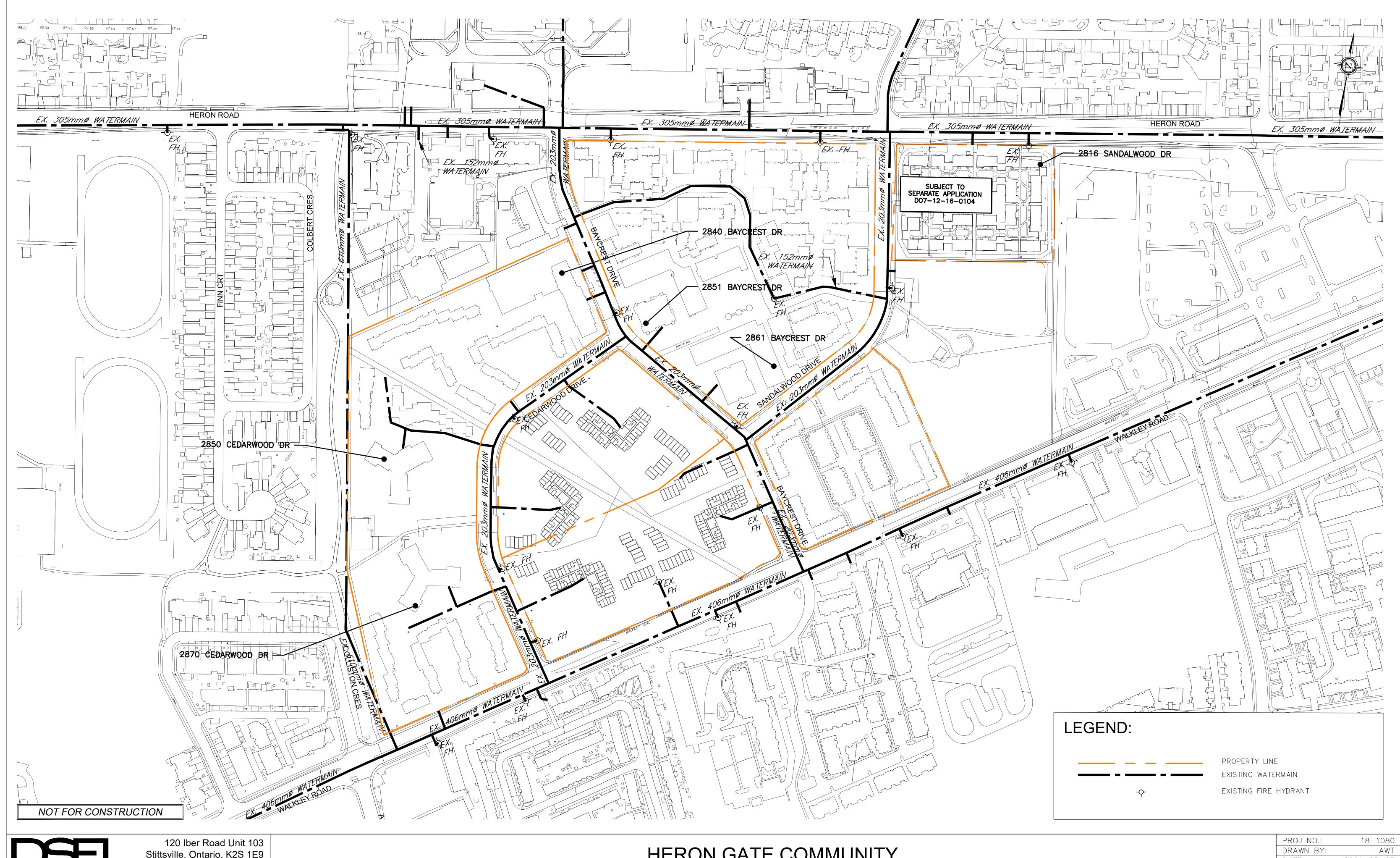
Report prepared by:

J. I. MOFFATT TO THE TOTAL PROPERTY OF ONTARIO

James Battison C.E.T

Jim Moffatt P. Eng. Associate

# **APPENDIX A**





120 Iber Road Unit 103 Stittsville, Ontario, K2S 1E9 Tel. (613) 836-0856 Fax. (613) 836-7183 www.DSEL.ca

HERON GATE COMMUNITY EXISTING WATER SERVICING

PROJ NO.:	18-1080
DRAWN BY:	AWT
DATE:	2021-05-07
SCALE:	1:1500
FIGURE NO.:	
	EX-WTR

#### WATERMAIN DEMAND CALCULATION SHEET

IBI GROUP

333 PRESTON STREET
OTTAWA, ON
K1S 5N4

PROJECT: 2851 Baycrest Drive - HG-5

LOCATION: City of Ottawa

DATE PRINTED: 2021-12-23
DESIGN: 2021-12-23

FILE:

PAGE: 1 OF 1

135142-6.4.4

		RESIDE	ENTIAL		NON	N-RESIDEN	TIAL	A۱	/ERAGE D	AILY	MA	XIMUM DA	AILY	MAX	IMUM HOU	JRLY	FIRE
NODE					INDTRL	COMM.	RETAIL		DEMAND (I/s)			EMAND (I	/s)	D	EMAND (I	DEMAND	
NOBE	Single	Town	Apt	POP'N	(ha.)	(ha.)	(m <sup>2</sup> )	Res.	Res. Non-res. Total		Res. Non-res. Total		Res.	Non-res. Total		(I/min)	
Site			305	549				1.78	0.00	1.78	4.45	0.00	4.45	9.79	0.00	9.79	9,000

#### **ASSUMPTIONS**

RESIDENTIAL DEN	SITIES		AVG. DAILY DEM	AND
Apartment (ave)	1.8	p/p/u	Residential:**	280

\*\* Residential Daily Demand reduced to coincide with

current waste water guidelines

Residential:\*\* 280 I / cap / day
Industrial: I / ha / day
Commercial: I / ha / day

Retail: 2,500 I / 1000m<sup>2</sup> / day

MAX. DAILY DEMAND

Residential: 700 I / cap / day

MAX. HOURLY DEMAND

Industrial:

Commercial:

Residential: 1,540 I / cap / day

Retail: 11,250 I / 1000m<sup>2</sup> / day

I / ha / day

I / ha / day

From FUS Calculation 9,000 I / min

#### Fire Flow Requirement from Fire Underwriters Survey

#### 2851 Baycrest Drive - Building A

	Total Floor Area	7,187 m <sup>2</sup>	
F = 220C√	A		
C A	0.8 7,187 m <sup>2</sup>	C =	1.5 wood frame 1.0 ordinary 0.8 non-combustible
F use	14,921 l/min 15,000 l/min		0.6 fire-resistive

Occupancy Adjustment

-15% Use

Adjustment -2250 l/min Fire flow 12,750 l/min

Sprinkler Adjustment

Use -30%

-3825 I/min Adjustment

-25% non-combustible

-15% limited combustible

0% combustible

+15% free burning

+25% rapid burning

-30% system conforming to NFPA 13

-50% complete automatic system

# **Exposure Adjustment**

Building	Separation	Adja	ed Wall	Exposure	
Face	(m)	Charge *			

north east

south west

Total

Use

Adjustment	- I/min
Total adjustments	(3,825) l/min
Fire flow	8,925 l/min

9,000 l/min

150 l/s

0% (Note: According to Page G-104 in Tech bulletin ISTB-2018-02 Revisions to Ottawa Design Guidelines - Water Distribution, "If the exposing wall of the building being considered is taller than the exposed wall of the adjacent structure, no exposure charge applies".)

Two Largerst

Floor

1813

1813

Floor

1

3

4

6

Total

Area (m2)

1813

1813

1513

1513

1513

1513

1070

10748

(Note: For fire-resistive buildings, consider two largest adjoining floors plus 50% of each of any floors

immediately above them up to eight.)

Floors Above

at 50%

757

757 757

757

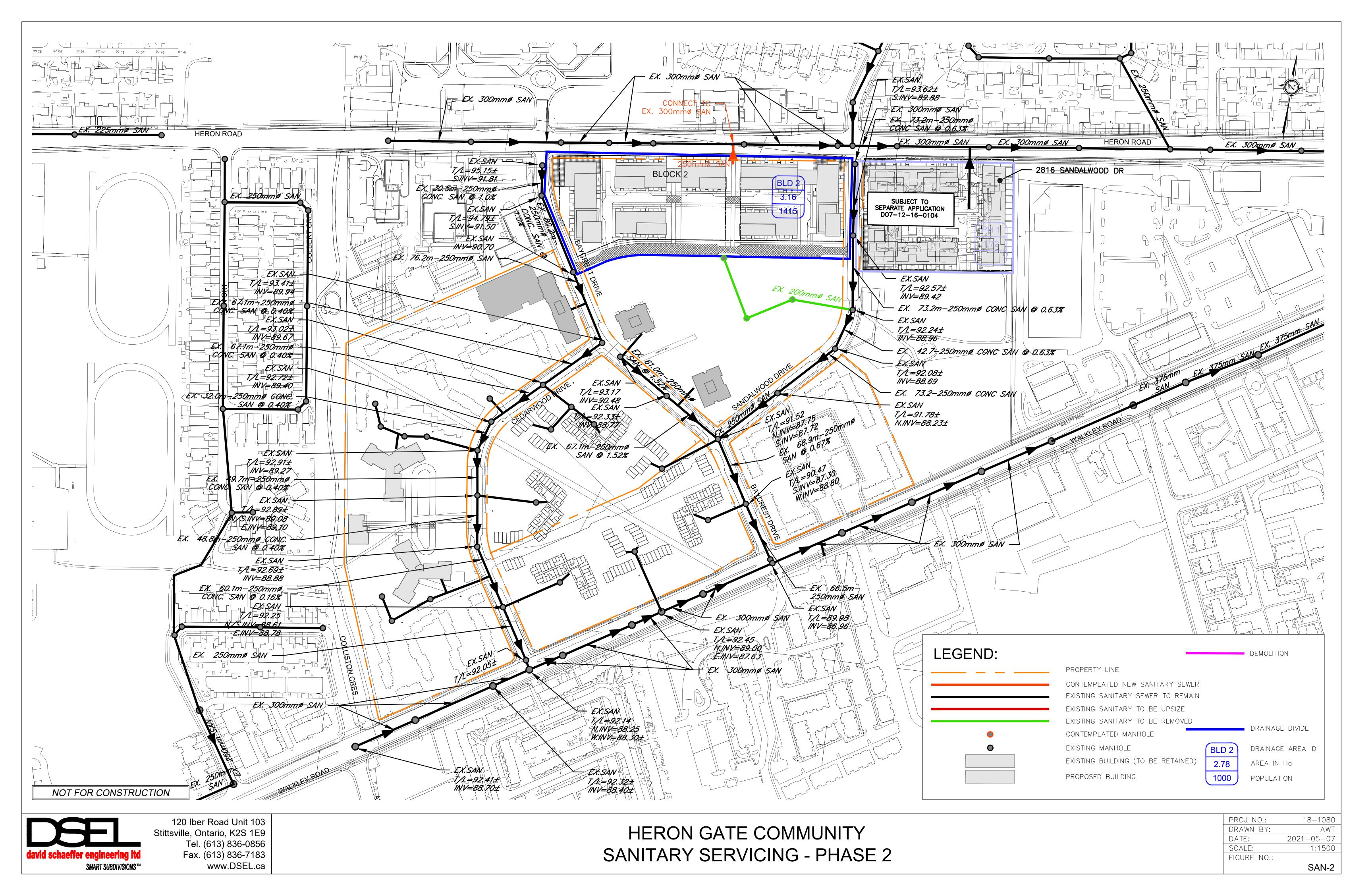
535

7187

FUS calculations shall be completed for each tower separately and exposure factors shall be calculated accordingly. Please note, a standard water supply reduction of 10% should be considered and the floor area reduction is only applicable to fire resistive buildings with a construction coefficient of 0.6. Please provide revised FUS calculations.

Revised.

# **APPENDIX B**



SANITARY SEWER DESIGN SHEET

2851 Baycrest Drive - HG 5 CITY OF OTTAWA



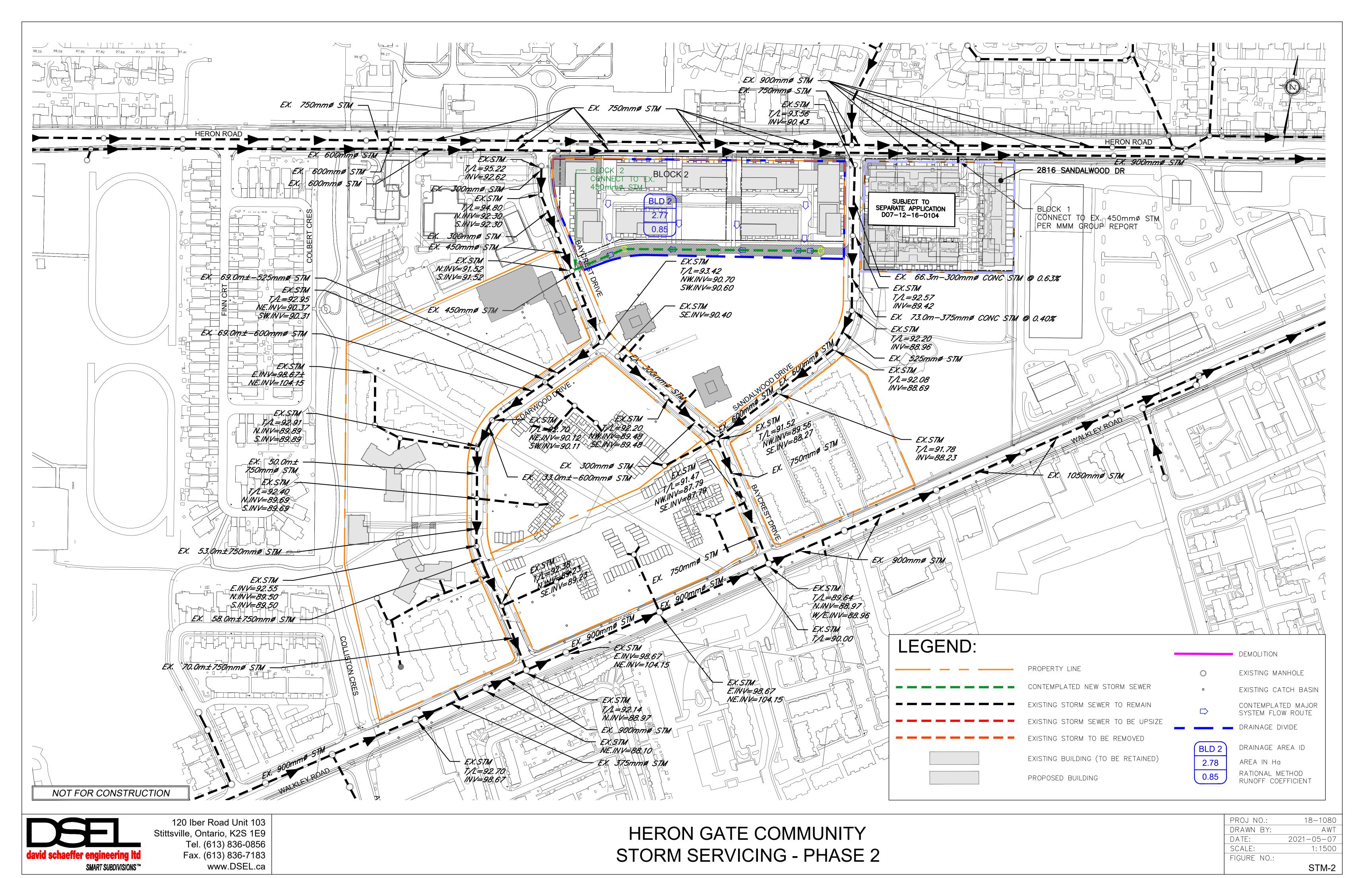
IBI GROUP 400-333 Preston Street Ottawa, Ontario K1S 5N4 Canada tel 613 225 1311 fax 613 225 9868

	LOCA	TION			RESIDENTIAL ICI AREAS INFILTRATION ALLOWANCE FIXED FLOW (L/s) TOTAL										PROPOSED SEWER DESIGN																							
	LUCA	IION			AREA	ı	JNIT T	YPES		AREA	POPU	LATION	RES	PEAK		ARE			AREA (Ha)				ICI		PEAK	ARE	A (Ha)	FLOW	FIXED F	LOW (L/s)	FLOW	CAPACITY	LENGTH	DIA	SLOPE	VELOCITY	AVA	ILABLE
STREET	AREA	ID	FROM MH	TO	w/ Units	SF S	D	TH	APT	w/o Units (Ha)	IND	CUM	PEAK FACTOR	FLOW		UTIONAL	COMM	CUM	INDU	STRIAL	PEAK	FLOW	IND	CUM	(L/s)	IND	CUM	(L/s)	(L/s)	(m)	(mm)	(%)	(full)		PACITY (%)			
			MH	MH	(Ha)					(Ha)			FACTOR	(L/s)	IND	CUM	IND	CUM	IND	CUM	FACTOR	(L/s)											(m/s)	L/s	(%)			
					1.10		_								<b>!</b>																							
2851 Baycrest Drive			BLDG	MH1A	1.19				305		549.0	549.0	3.36	5.98	<u> </u>		0.00	0.00					1.19	1.19	0.39			6.37	48.39	4.35	200	2.00	1.492	42.01	86.83%			
2851 Baycrest Drive			MH1A	Main							0.0	549.0	3.36	5.98			0.00	0.00						1.19	0.39			6.37	34.22	16.20	200	1.00	1.055	27.84	81.37%			
Design Parameters:					Notes:								Designed	:	JEB			No.						F	Revision								Date					
-					1. Mannings	s coefficient (n) =			0.013				-					1.						Issued for S	lite Plan Appli	ication							2021-12-23					
Residential		ICI	Areas		2. Demand	(per capita):		280	L/day	200	L/day																											
SF 3.4 p/p/u						allowance:			L/s/Ha				Checked:		JM																							
TH/SD 2.7 p/p/u	INST	28.000 I	/Ha/dav		4. Residenti	ial Peaking Factor:																																
APT 1.8 p/p/u	COM	28,000 I	/Ha/day			Harmon Formula	= 1+(1	4/(4+(P/10	00)^0.5))0.	8																												
Other 60 p/p/Ha		35,000 I		MOE Chart		where K = 0.8 Co			,,,.				Dwg. Refe	erence:	135142-C	-001																						
		17000 I			5 Commerci	ial and Institutional	Peak	Factors has	sed on tota	al area			1					F	ile Referen	ce:						Date:							Sheet No:					
						1.5 if greater t													135142.6.0							2021-12-2	3						1 of 1					

This design sheet needs to include all proposed flows to Heron Road using the same outlet.

Further to discussions with the Mechanical Engineer it is not feasible to service all the buildings included in Block 2 of the DSEL FSR with one sanitary connection. One sanitary connection will be required for the current phase and at least one more connection will be required for the remainder of Block 2.

# **APPENDIX C**





IBI GROUP 333 PRESTON STREET OTTAWA, ON K1S 5N4

PROJECT: 2851 Baycrest Drive DATE: 2021-12-23 FILE: 135142.6.04 REV #: 1 DESIGNED BY: JB CHECKED BY: JM

45.00

 $Q_p - Q_r$ 

(L/s)

150.76 136.18

64.00

 $Q_p$ - $Q_r$ 

Volume

5yr (m³)

#### STORMWATER MANAGEMENT

#### Formulas and Descriptions

 $i_{2yr}$  = 1:2 year Intensity = 732.951 /  $(T_c$ +6.199) $^{0.810}$ 

 $i_{5yr}$  = 1:5 year Intensity = 998.071 /  $(T_c+6.053)^{0.814}$ 

 $i_{100yr} = 1.5$  year intensity = 998.0/1 /  $(I_c + 6.053)^{0.0520}$   $i_{100yr} = 1:100$  year Intensity = 1735.688 /  $(T_c + 6.014)^{0.820}$   $T_c = Time of Concentration (min)$ 

C = Average Runoff Coefficient A = Area (Ha) Q = Flow = 2.78CiA (L/s)

#### Maximum Allowable Release Rate

Flow Allocation

Taken from Functional Servicing and Stormwater Report Table 16

100 Year Flow Block 2

223.54 L/sec 50% of FSR block 2

Q TOTAL = 111.77 L/s

Uncontrolled Release (Q<sub>uncontrolled</sub> = 2.78\*C\*i<sub>100yr</sub>\*A<sub>uncontrolled</sub>)

C = T<sub>c</sub> = 0.45 10 min 178.56 mm/hr 0.009 Ha

Maximum Allowable Release Rate (Q max allowable = Q restricted - Q uncontrolled)

Q max allowable = 109.76 L/s

#### MODIFIED RATIONAL METHOD (100-Year & 5-YearPonding)

Overflo 0.00

Drainage Area	Cisteri	n			
Area (Ha)	0.90				
C =	0.9	9 Restricted Flow Q <sub>r</sub> (I	_/s)=	45.00	1
		100-Year Pondir	ıg		
T <sub>c</sub> Variable	i <sub>100yr</sub>	Peak Flow Q <sub>p</sub> =2.78xCi <sub>100yr</sub> A	Q,	$Q_p$ - $Q_r$	Volume 100yr
(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m³)
44	70.18	173.84	45.00	128.84	340.13
46	67.96	168.34	45.00	123.34	340.41
47	66.91	165.73	45.00	120.73	340.45
48	65.89	163.21	45.00	118.21	340.44
50	63.95	158.41	45.00	113.41	340.24

Storage (m³)				
Overflow	Required	Roof	Cistern	Balance
0.00	340.45	155.00	186.00	0.00

Storage (m³) Surface 110.00

Cistern 0.00

Balance 0.00

	Overflow	Required	age (m <sup>3</sup> ) Roof	Cistern	Balance	-
		04	(3)			
20	70.25	158.19	45.00	113.19	135.83	
18	74.97	168.82	45.00	123.82	133.72	

icted Flow Q<sub>r</sub> (L/s)

5-Year Ponding

Qp=2.78xCi5yr A

5-Year Ponding

Peak Flow

Q p=2.78xCi 5yr A

(L/s)

Q,

Cistern 0.900

i<sub>5yr</sub>

86.93

Private Road

i<sub>5yr</sub>

0.90

Drainage Area

T <sub>c</sub> Variable

(min)

Drainage Area

T <sub>c</sub> Variable

Diamage Area	i iivate itoat	4			
Area (Ha)	0.46				
C =	0.9	9 Restricted Flow Q <sub>r</sub> (I	L/s)=	64.00	
100-Year Ponding					
T <sub>c</sub> Variable	i <sub>100yr</sub>	Peak Flow Q <sub>p</sub> =2.78xCi <sub>100yr</sub> A	Q,	Q <sub>p</sub> -Q <sub>r</sub>	Volume 100yr
(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m³)
15	142.89	182.09	64.00	118.09	106.28
17	132.63	169.00	64.00	105.00	107.10
18	128.08	163.21	64.00	99.21	107.15
19	123.87	157.84	64.00	93.84	106.98
21	116.20	1/0 10	64.00	9/ 10	106.00

Required 107.15

	Variable	1 5yr	Q <sub>p</sub> =2.78xCi <sub>5yr</sub> A	Q,	$Q_p - Q_r$	5yr
	(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m³)
	6	131.57	152.41	64.00	88.41	31.83
	8	116.11	134.51	64.00	70.51	33.84
	9	109.79	127.19	64.00	63.19	34.12
	10	104.19	120.70	64.00	56.70	34.02
	12	94.70	109.70	64.00	45.70	32.90
			Stora	age (m³)		
_		Overflow	Required	Surface	Cistern	Balance
		0.00	34.12	110.00	0.00	0.00

# **APPENDIX D**

C-001 CITY PLAN No. xxxxx

# **UTILITY LEGEND**

	TRANSFORMER
	TRANSFORMER C/W CONCRETE WINGS
HSG	HYDRO SWITCHGEAR
НМН	HYDRO MANHOLE
	BELL PEDESTAL
GLB	BELL GRADE LEVEL BOX (I=600mm, w=1200mm, d=750mm) C/W 1.5 x 3.0m eas
FC	BELL FIBER CABINET (I=1200mm, w=750mm, d=500mm)
CSP	BELL CENTRAL SPLITTING POINTS (I=1175mm, w=1200mm, d=500mm)
	ROGERS PEDESTAL
$\boxtimes$	ROGERS VAULT (I=1000mm, w=1000mm, d=1200mm) C/W 1m x 2m easement
P30	STREET LIGHT
D	STREET LIGHT DISCONNECT
— <b> </b>   -	STREET LIGHT GROUNDING
——————————————————————————————————————	JOINT UTILITY TRENCH
———Н———	HYDRO CABLE AND DUCTS
——В——	BELL CABLE
BB	BELL DUCTS
T	ROGERS CABLE
TT	ROGERS DUCTS
G	GAS
s	STREET LIGHT CABLE
	UTILITY DROP LOCATIONS
10-DUCTS 6-H	CONCRETE ENCASED DUCT BANK C/W NUMBER OF DUCTS
4-T CMB	COMMUNITY MAILBOX
	PROPOSED TREE LOCATION
1	ROOT MANAGEMENT BARRIER

# SEDIMENT EROSION LEGEND

HEAVY DUTY SILT FENCE

	SNOW FENCE
₩	STRAW BALE CHECK DAM
Marris Control Colors Marris (1988)	STRAW BALE CHECK DAM WITH FILTER CLOTH
	ROCK CHECK DAM
	SEDIMENT SACK PLACED UNDER EXISTING CB COVER
	TEMPORARY MUD MAT 0.15m THICK 50mm CLEAR STONE ON NON WOVEN FILTER CLOTH

# **GENERAL LEGEND**

	LIMIT OF CONSTRUCTION
	PHASING LINE
	BARRIER CURB
	MOUNTABLE CURB
	DEPRESSED BARRIER CURB
	CONCRETE SIDEWALK
	- TACTILE WALKING SURFACE INDICATOR
	ASPHALT SIDEWALK / PATHWAY
BUS	BUS STOP CONCRETE / ASPHALT

# SERVICING LEGEND

MH118A	SANITARY MANHOLE
200mmØ SAN	SANITARY SEWER
MH109 MH118	STORM MANHOLE
825mmØ STM	STORM SEWER - LESS THAN 900Ø
900mmØ STM	STORM SEWER - 900Ø AND GREATER
200Ø WATERMAIN	WATERMAIN
■ CB100	STREET CATCHBASIN C/W TOP OF GRATE
T/G 104.10 CICB101	CURB INLET CATCHBASIN C/W GUTTER GRADE
G/G 104.25 DCB100	DOUBLE CATCHBASIN C/W TOP OF GRATE
T/G 104.10 DCICB101	DITCH INLET CATCHBASIN C/W GUTTER GRADE
G/G 104.25 CBMH100	
T/G 103.59 CBMH101	CATCHBASIN MANHOLE C/W TOP OF GRATE
T/G 103.59 CB100	DITCH INLET MANHOLE C/W TOP OF GRATE
T/G 104.10	ICD LOCATION
RYCB T/G 104.35	REAR YARD CATCHBASIN IN ROAD CONNECTING STRUCTURE C/W SOLID GRATE
<del>O</del> T/G 104.35 NV 103.35	REAR YARD "TEE" CATCHBASIN (300Ø) C/W TOP OF GRATE AND INVERT OUT
OT/G 104.50 NV 103.50	REAR YARD "END" CATCHBASIN (300Ø) C/W TOP OF GRATE AND INVERT OUT
₫ <u>T/G</u> 104.35 ĪNV 103.35	REAR YARD "CUSTOM ANGLED " CATCHBASIN (450Ø) C/W TOP C GRATE AND INVERT OUT
T/G 104.35 INV 103.35	REAR YARD "THREE WAY" CATCHBASIN (450Ø) C/W TOP OF GRATE AND INVERT OUT
200mm@ CSD	PERFORATED REAR YARD SUBDRAIN
300mmØ CSP	CSP CULVERT C/W DIAMETER
<b>⊗</b> <sup>V&amp;VB</sup>	VALVE AND VALVE BOX
<b>⊚</b> V&VC	VALVE AND VALVE CHAMBER
→ HYD 104.35	FIRE HYDRANT C/W BOTTOM OF FLANGE ELEVATION
200Ø WM RED 150Ø WM	WATERMAIN REDUCER
2 VBENDS	VERTICAL BEND LOCATION
$\triangleleft$	SINGLE SERVICE LOCATION
$\triangleleft$	DOUBLE SERVICE LOCATION
BH 12 102.00	INFERRED BEDROCK (SEE GEOTECHNICAL REPORT)
HGL	100 YEAR STORM HYDRAULIC GRADE LINE AT MANHOLE
101.79 S/T HGL	STRESS TEST STORM HYDRAULIC GRADE LINE AT MANHOLE
101.79 108 102.40	
102.40	UNDERSIDE OF FOOTING ELEVATION (WITH LOT #)
	CLAY SEAL IN SEWER / WATERMAIN TRENCH

# GRADING LEGEND

$\rightarrow$ $\rightarrow$	PROPOSED SWALE C/W FLOW DIRECTION
	PROPOSED DITCH C/W FLOW DIRECTION AND SLOPE
1.3%	SLOPE C/W FLOW DIRECTION
<≒ □	MAJOR OVERLAND FLOW ROUTE
× 104.62	PROPOSED SPOT GRADE
×104.40 (S)	PROPOSED SWALE GRADE
×104.50 (S)HP	PROPOSED SWALE HIGH POINT GRADE
104.60 103.59 ×	LOT CORNER GRADE C/W EXISTING GRADE
86.45 EX ×	TIE INTO EXISTING GRADE
96.79	FULL STATIC PONDING GRADE
103.50 LILILI	RETAINING WALL C/W TOP OF WALL AND GRASS GRADE TERRACING 3:1 MAXIMUM UNLESS NOTED OTHERWISE
<b>№</b>	PRESSURE REDUCING VALVE
F.FL. 96.32 T.FND. 95.96 U.S.F. 93.36 RISERS 0 M.U.S.F M.G.G.	- FINISHED FLOOR ELEVATION - TOP OF FOUNDATION ELEVATION - UNDERSIDE OF FOOTING ELEVATION - NUMBER OF ADDITIONAL RISERS - MINIMUM UNDERSIDE OF FOOTING (Based on the higher of the sewer obverts, or hydraulic grade line) - MINIMUM GARAGE GRADE
(M.R.G. 107.10	MINIMUM GRASS GRADE
WU	WALKUP UNIT
WO	WALKOUT UNIT
NS	NON-STANDARD FOUNDATION (Frost cover not provided for standard unit)
BS	BACKSPLIT UNIT (1.5m frost cover on footings)
———F———F———	NOISE FENCE LOCATION
—FFF	NOISE FENCE GATE

# NOTES:

- 1. ALL MATERIALS AND CONSTRUCTION IS TO BE IN ACCORDANCE WITH THE CURRENT CITY OF OTTAWA STANDARD DRAWINGS & SPECIFICATIONS OR OPSD/OPSS IF CITY DRAWINGS AND SPECIFICATIONS DO NOT APPLY.
- 2. THE CONTRACTOR IS RESPONSIBLE FOR DETERMINING THE EXACT LOCATION, SIZE, MATERIAL AND ELEVATION OF ALL EXISTING SERVICES AND UTILITIES PRIOR TO CONSTRUCTION AND SHALL PROTECT AND ASSUME RESPONSIBILITY FOR ALL UTILITIES WHETHER OR NOT SHOW ON THESE DRAWINGS.
- FOR GEOTECHNICAL INFORMATION REFER TO GEOTECHNICAL REPORT
- 3. FOR GEODETIC BENCHMARK AND GEOMETRIC LAYOUT OF STREET AND LOTS, REFER TO TOPOGRAPHICAL SURVEY AND PLAN OF SUBDIVISION PREPARED BY LEGAL SURVEYOR BENCHMARK BASED ON CAN--NET VIRTUAL REFERENCE SYSTEM NETWORK.
- 4. ROADWAY SECTIONS REQUIRING GRADE RAISE TO PROPOSED SUB GRADE LEVEL TO BE FILLED WITH ACCEPTABLE NATIVE EARTH BORROW OR IMPORTED OPSS SELECTED SUBGRADE MATERIAL IF NATIVE MATERIAL IS DEFICIENT AS PER RECOMMENDATION OF GEOTECHNICAL ENGINEER.
- RECOMMENDATIONS OF THE GEOTECHNICAL REPORT. AS PER CITY GUIDELINES ALL WATERMAINS IN FILL AREAS ARE TO BE TIED WITH RESTRAINING JOINTS AND THRUST

6. CONTRACTORS SHALL BE RESPONSIBLE FOR KEEPING CLEAN ALL ROADS WHICH BECOME

5. IN AREAS WHERE EXISTING GROUND IS BELOW THE PROPOSED ELEVATION OF SEWER AND WATERMAINS, GRADE RAISING AND FILLING IS TO BE IN ACCORDANCE WITH THE

- COVERED IN DUST, DEBRIS AND/OR MUD AS A RESULT OF ITS CONSTRUCTION OPERATIONS. 7. SILT FENCE TO BE ERECTED PRIOR TO EARTH WORKS BEING COMMENCED. SILT FENCE TO BE MAINTAINED UNTIL VEGETATION IS ESTABLISHED OR UNTIL START OF SUBSEQUENT
- 8. STRAW BALE SEDIMENT TRAPS TO BE PLACED AND MAINTAINED IN EXISTING AND CONSTRUCTED ROADSIDE DITCHES. TRAPS TO REMAIN AND BE MAINTAINED UNTIL VEGETATION IS ESTABLISHED (IF APPLICABLE).
- 9. SILT SACK TO BE PLACED AND MAINTAINED UNDER COVER OF ALL CATCHBASINS. GEOTEXTILE SILT SACK IN STREET CBs TO REMAIN UNTIL ALL CURBS ARE CONSTRUCTED. GEOTEXTILE FABRIC IN RYCBs TO REMAIN UNTIL VEGETATION IS ESTABLISHED. ALL CATCHBASINS TO BE REGULARLY INSPECTED AND CLEANED, AS NECESSARY, UNTIL SOD AND CURBS ARE CONSTRUCTED.
- 10. ALL CONNECTIONS TO EXISTING WATERMAINS ARE TO BE COMPLETED BY CITY FORCES. CONTRACTOR IS TO EXCAVATE, BACKFILL, COMPACT AND REINSTATE.
- 13.ANY WATERMAIN WITH LESS THAN 2.4M DEPTH OF COVER REQUIRES THERMAL INSULATION AS PER CITY OF OTTAWA STANDARD W22, OR AS APPROVED BY THE ENGINEER.
- 14. ALL LEADS FOR STREET CB's TO AND CICB'S CONNECTED TO MAIN SHALL BE 200mmØ PVC DR35 @ MIN 2% SLOPE UNLESS NOTED OTHERWISE. ALL LEADS FOR RYCB's CONNECTED TO MAIN SHALL BE 200mmØ PVC DR35 @ MIN 1% SLOPE UNLESS NOTED OTHERWISE.
- 15. EACH BUILDING SHALL BE EQUIPPED WITH A SANITARY AND STORM SEWER BACKWATER VALVE AND CLEAN-OUT ON ITS PRIMARY SERVICE, AS PER ONTARIO BUILDING CODE
- 16. THESE DRAWINGS ARE NOT TO BE SCALED OR USED FOR LAYOUT PURPOSES.

REQUIREMENTS (BY OTHERS).

- 17. THE COMPOSITE UTILITY PLAN HAS BEEN REVIEWED BY IBI GROUP FOR CONFORMITY TO THE DESIGN CONCEPT FOR THE DEVELOPMENT AND FOR GENERAL ARRANGEMENT ONLY AND AS SUCH SHALL NOT RELIEVE THE CONTRACTOR OF RESPONSIBILITY FOR ERRORS OR OMISSIONS IN EITHER LAYOUT OR WORKMANSHIP.
- 18. ALL UTILITY BOXES (I.E. PEDESTALS, TRANSFORMERS, ETS) ARE TO BE INSTALLED IN ACCORDANCE WITH THE LATEST EDITION OF THE CITY OF OTTAWA'S "GUIDELINES FOR UTILITY PEDESTALS WITHIN THE ROAD RIGHT OF WAY"
- 19. THIS DRAWING IS A COMPILATION OF OTHER UTILITY DESIGNS AND DOES NOT INDICATE IN ANY WAY THAT THE PARTY SIGNING THIS DRAWING HAS DESIGNED OR APPROVED THE RESPECTIVE UTILITY PLANTS INDICATED ON THIS DRAWING. THE DRAWING WAS PREPARED TO BE USED AS REFERENCE ONLY AS PER REQUIREMENTS OF THE CITY OF OTTAWA. IT IS THE CONTRACTORS RESPONSIBILITY TO ENSURE IT HAS REVIEWED THE CURRENT AND EXISTING DESIGNS BY HYDRO, STREET LIGHTING, BELL, CANADA POST, O.C. TRANSPO, CABLE TV AND ANY OTHER PARTIES INCLUDED BUT NOT MENTIONED AND COMPLETE THE INSTALLATION IN ACCORDANCE WITH THE REQUIREMENTS OF THE STAKEHOLDER UTILITY DESIGNS.

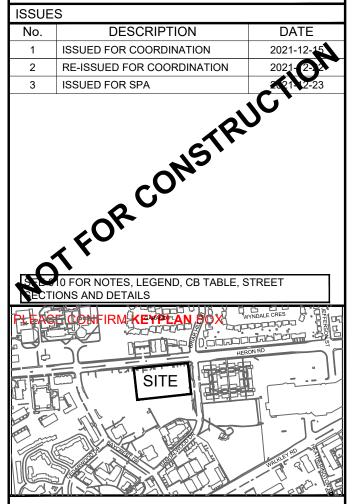
CLIENT HAZELVIEW **INVESTMENTS** 

1133 Younge St. 4th Floor, Toronto On, M4T 1W1

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PROJECT

Heron Gate 5

PROJECT NO: 135142 DRAWN BY: CHECKED BY: PROJECT MGR: APPROVED BY:

SHEET TITLE

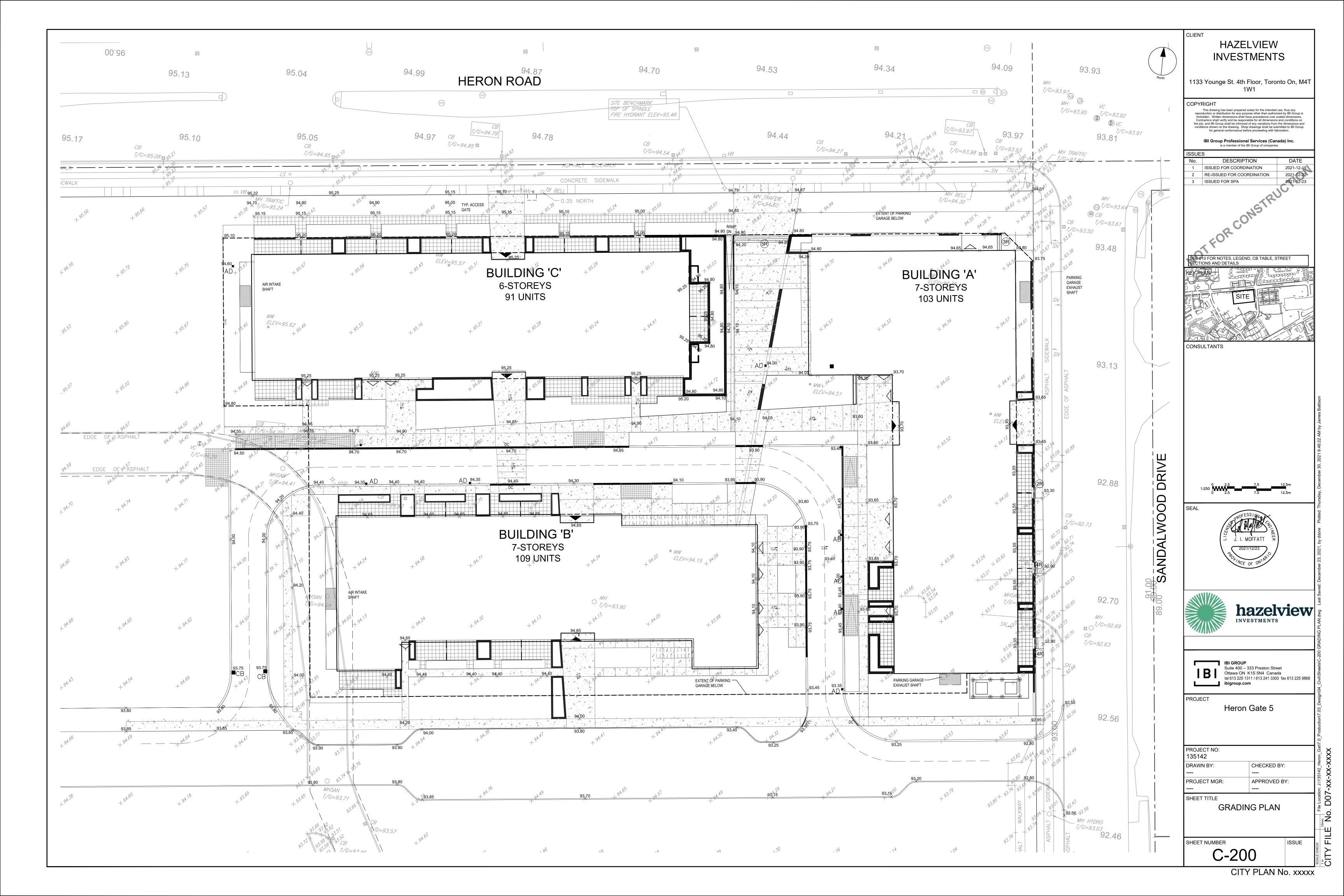
GENERAL NOTES, LEGEND AND CB DATA TABLE

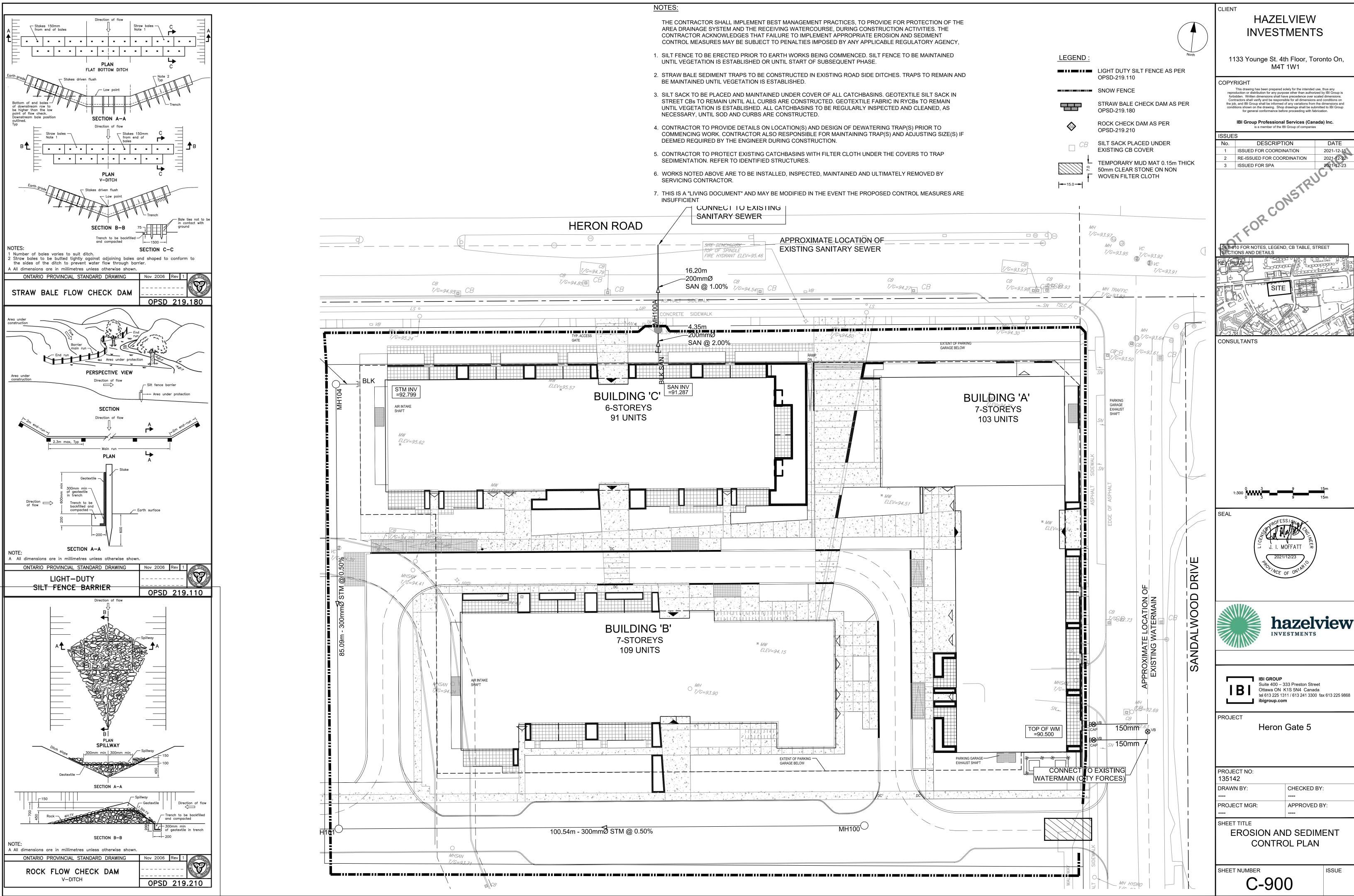
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CITY PLAN No. xxxxx