SITE SERVICING & STORM WATER MANAGEMENT REPORT FOR 1050 KLONDIKE ROAD, OTTAWA, ONTARIO

May 20, 2021

Prepared by:



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1. Introduction

1.1 Site Description and Proposed Development

This report describes the site servicing and stormwater management design and calculations pertaining to a street townhouses development proposed at 1050 Klondike Street. The site contains an existing dwelling with gravel and landscaped areas.



Figure 1 - Site Location Plan

Proposed grading and servicing is shown on the drawings included in **Appendix A**.

1.1.1 Statement of Objectives and Servicing Criteria

The objective of this Site Servicing and Stormwater Management Report is to demonstrate that the proposed design meets the servicing requirements for the proposed development, while adhering to the appropriate regulatory requirements.

1.1.2 Location Map and Plan

The location of the site is illustrated in Figure 1. A detailed site layout is provided within the drawings in Appendix A

1.2 Background Documents

Existing conditions are shown on the Topographic and Legal Survey (Appendix G).



1.3 Consultation and Permits

1.3.1 Pre-consultation Meetings

A pre-consultation meeting was held with the City of Ottawa in May 2020. The comments were received for a condominium building which was later changed to street townhouses. Most of the comments are still relevant to the new proposal and are summarized as follows,

Stormwater Management:

- There is an available 675mm diameter concrete storm sewer located on Sandhill Road conveying flow to a ditch upstream of "Pond C".
- Based on both the Shirley's Brook Floodplain Analysis and SWM Report (Klondike Road Development Lands, prepared by Novatech, May 2006) and the Shirley's Brook SWM Facility "C" Detailed Design Report (prepared by Novatech, 2006), it appears that Pond "C" was sized to service the 1050 Klondike Road parcel. Please demonstrate that the existing storm sewer and pond have capacity to service this proposed development (quantity and quality control).
- Refer to the SWM design criteria in the Shirley's Brook SWM Facility "C" Detailed Design Report (prepared by Novatech, 2006) for the proposed development area:
 - Minor system allowable release rate of 85 L/s/ha;
 - Onsite major system storage of 50 m3/ha (please see the note below);
 - ICDs [are] installed in the roadway catchbasins to ensure flow into the storm sewer system does not exceed the 5-year runoff rates; and
 - HGL for 100-year event must have at least 0.3 m freeboard to the underside of footings.
- IDF information derived from the Meteorological Services of Canada rainfall data, taken from the MacDonald Cartier Airport, collected 1966 to 1997.
- The pre-development runoff coefficient or a maximum equivalent 'C' of 0.5, whichever is less (§ 8.3.7.3).
- A calculated time of concentration (Cannot be less than 10 minutes).
- Use of rooftop controls are recommended for this site, but are not limited to them, to meet the requirements.

Watermain:

- There is an available 305mm diameter PVC watermain fronting the site along Sandhill Road. However, looping of the Klondike Road watermain (from March Road stub to the Sandhill Road stub) is preferred.
- If a watermain extension along Klondike Road is pursued an MECP Form 1 will need to be completed.
- Drinking Water Boundary condition requests must include the location of the service connection and the expected loads required by the proposed development.
- Determine the total water demand based on maximum demand and required fire flow for water boundary conditions.

Sanitary:

- There is an available 200mm diameter PVC sanitary sewer located on Klondike Road. However, it currently does not front the proposed site.
- A sanitary sewer extension within the Klondike Road Right-Of-Way (ROW) will be required to service this site.



- The proponent will be required to demonstrate what the expected sanitary flows from the proposed site will be and show that the existing sanitary sewer infrastructure can accommodate the proposed site flows without any adverse affects.
- The existing sanitary sewer on Klondike Road connects to the Briar Ridge Pump Station (BRPS). This pump station currently has limited capacity. Upgrades to the BRPS are expected to be completed by Dec 2021 or early 2022.
- Due to the municipal sanitary sewer extension a Ministry of Environment, Conservation and Parks
 Environmental Compliance Approval (MECP ECA) will be required and will be reviewed under the
 Transfer of Review program (Standard Works) with the City of Ottawa.
- Also due to the municipal sanitary extension, a Municipal Consent (MC) circulation will be required after or in the later stages of the Site Plan Application stage. The ROW Approvals Department at the City, may, to their review and discretion, exempt the proposed extension from the MC Circulation process.

The full comments regarding site-servicing and stormwater management-specific requirements can be found in **Appendix B**.

1.4 Available Existing Infrastructure

Sewer and watermain mapping collected from the City of Ottawa indicate that the following services exist across the property frontages and the Sandhill Road intersection.

Klondike Road

200mm diameter PVC sanitary sewer (up to Sandhill Road Intersection)

Sandhill Road

- 305mm diameter PVC watermain
- 675mm diameter Conc. storm sewer

2. Geotechnical Study

A Geotechnical Investigation was completed by GEMTEC and is documented in Report No. 65153.01 dated April 7, 2020.

A total of 3 boreholes were drilled to a maximum depth of 6.7 - 8.5m below the existing ground surface. The subsurface profile at the borehole locations consists of 100mm topsoil layer underlain by a fill layer to approximately 1.2 to 2.9m depth.

The fill material below the topsoil and/or granular fill material can be described as brown, fine to coarse grained sand with trace to some silt. The fill material extends to depths ranging from about 1.2 to 2.9 meters below existing grade (elevation 73.5 to 76.1 meters)

Groundwater was encountered at depths of 3.8 to 5.3m below the existing ground surface.

The geotechnical report provides recommendations for excavation, backfill, pavement structure and pipe bedding and backfill.



3. Water Services

3.1 Design Criteria

The water service will be designed in accordance with the 2010 City of Ottawa Water Design Guidelines as well as MOE Design Guidelines for Drinking Water Systems.

The required domestic water demand and pressure design parameters for the development has been calculated based in **Table 1**:

Table 1– Summary of Water Demand Parameters

Design Parameter	Value	
	Residential	
Average Daily Demand	350 L/d/P1	
Max. Daily Peaking Factor	9.5 x Average Daily ²	
Max. Hourly Peaking Factor	14.3 x Average Daily ²	
Minimum Watermain Size	150mm diameter	
Minimum Depth of Cover	2.4m from top of watermain to finished grade	
Min. pressure during normal operating conditions	345kPa	
Max. pressure during normal operating conditions	552kPa	
Min. pressure during maximum hourly demand	276kPa	
Min. pressure during maximum daily demand + fire flow	140kPa	

¹ Daily average based on Appendix 4-A from Water Supply Guidelines

Total No. Townhouse Units = 9 units

Population = $2.7 \times 9 = 24 \text{ persons}$

Daily Average Water Demand = 24 x 350 1/cap/day = 84,00 L/Day = 0.097 L/sec

Maximum Daily Demand = $0.097 \times 9.5 = 0.92 \text{ L/sec}$

Maximum Hourly Demand = $0.097 \times 14.3 = 1.39 \text{ L/sec}$

The water demand/fire flow for the development based on the Ottawa Design Guidelines (2010 incl. Technical Bulletins) and the Fire Underwriters Survey (1999) is summarized below;

Table 2– Summary of Water Demand Calculations

Design Parameter	Water Demand (L/s)
	Residential
Average Daily Demand	0.097
Maximum Daily Demand	0.92
Maximum Hourly Demand	1.39
Fire Flow	216.67
Total Max Daily Demand + Fire Flow	217.59

² Residential Max. Daily and Max. Hourly peaking factors per MOE Guidelines for Drinking-Water Systems Table 3-3 for 0 to 500 person



Fire flow calculations are provided in **Appendix C**.

3.2 Adequacy of Supply for Domestic and Fire Flows

Preliminary water demands and fire flow requirements for the proposed development were provided to the City of Ottawa (Table 2) . The City of Ottawa was contacted to obtain boundary conditions associated with the estimated water demand, as indicated in the boundary request correspondence included in Appendix B.

The City provided both the anticipated minimum and maximum water pressures, as well as, the estimated water pressure during fire flow, as indicated by the correspondence in Appendix B and results of boundary conditions (Appendix C).

Fire flow calculated using the ISTDB-2018-02 method used the following assumptions from the Architect:

- Type of construction Combustible;
- Occupancy type Limited Combustibility;
- Sprinkler Protection None; and
- Single block considered for the townhouses block.

The above assumptions result in a maximum estimated fire flow of approximately 13,000 L/min. See Appendix C for detailed calculations using the ISDTB-2018-02 method. The minimum and maximum pressures fall within the required range identified in Table 1.

Table 3 - Results from Boundary Condition Analysis

Demand Scenario	Head (m)	Pressure (psi)
Maximum HGL	130.0	78.3
Peak Hour	126.3	73.1
Max Day plus Fire 1	121.2	65.8

Ground Elevation = 74.9 m

3.3 Pressure Check

The site is within Pressure Zone 1W, which operates at a maximum head of 115 m (City of Ottawa Water Master Plan, 2013). This would result in a maximum pressure above the finished floor elevation of approximately 519kPa, which falls under the maximum 552kPa defined in the guidelines.

3.4 Reliability Requirements

A shut off valve for the water service will be provided at the property line.

3.5 Watermain Extension on Klondike Road

In order to service the townhouse block for water, multiple options were discussed with the city staff which consisted of servicing through the laneway as private services or from Klondike Road as municipal services. The servicing option from Klondike Road was preferred and adopted for further design. This option would require extension of 200mm watermain from Sandhill Road intersection up to the site west limit.



The same watermain extension is also part of proposed servicing for 1051 Klondike Road development. Coordination with Novatech was done to obtain the design and implement part of the watermain extension under 1050 Klondike Road development. The final sequence of construction and cost sharing would depend on the timing of both developments which will be further coordinated during site plan approval.

The watermain extension on Klondike Road and servicing for the townhouses are shown on Drawing C101 & C104, Appendix A.

3.6 Reliability Requirements

A shut off valve for the water service will be provided at the property line.

3.7 Water Supply Conclusion

It is proposed to service the private development from the proposed watermain extension on Klondike Road. The anticipated water demand was submitted to the City of Ottawa for establishing boundary conditions. The City provided both the anticipated minimum and maximum water pressures, as well as, the estimated water pressure during fire flow. As demonstrated by Table 2 & 3, based on the City's model, the municipal system is capable of delivering water within the pressure range prescribed in the Water Supply Guidelines.

The available pressure during the fire flow scenario as per the OBC and ISDTB-2018-02 calculations exceeds 140 kPa. The proposed water supply design conforms to all relevant City Guidelines and Policies.

4. Sanitary Servicing

4.1 Background and Existing Infrastructure

Sanitary sewer along the property frontage on Klondike Road is not available. As per pre consultation comments, extension of sanitary sewer from the Sandhill intersection will be required as part of the development works. The sanitary service will be designed in accordance with the 2012 Ottawa City Sewer Design Guidelines.

4.2 Proposed Servicing and Calculations

The proposed development will require individual service connections to the townhouses from the proposed sanitary sewer extension on Klondike Road. The sanitary servicing design parameters are defined in Table 4.

Table 4 - Summarization of Sanitary Servicing Design Parameters

Design Parameter	Value		
Residential Average Flow	280 l/c.d		
Residential Peaking Factor	Based on the Harmon Equation $P.F.=1 + \left(\frac{14}{4 + \left(\frac{P}{1000}\right)^{\frac{1}{2}}}\right) * K$		
Infiltration and Inflow Allowance	0.33 L/ha/s		



Design Parameter	Value	
Manning's Coefficient 'n' 0.013		
Minimum Depth of Cover 2.5m from obvert of sewer to grade		
Minimum Full Flowing Velocity 0.6m/s		
Maximum Full Flowing Velocity 3.0m/s		
As per Sections 4 and 6 of the City of Ottawa Sewer Design Guidelines, October 2012 incl. all Tech. Bulletins as of November		

As per Sections 4 and 6 of the City of Ottawa Sewer Design Guidelines, October 2012 incl. all Tech. Bulletins as of November 2019

Total No. of Townhouse Units = 9 units

Population = $2.7 \times 9 = 24 \text{ persons}$

Average Daily Flow = $24 \times 280 \text{ l/c/d} = 6{,}720 \text{ l/day} = 0.078 \text{ l/sec}$

Infiltration Allowance = $0.16 \times 0.33 \text{ l/day} = 0.053 \text{ l/sec}$

Harmon's Peaking Factor = 3.5

Peak Flow = $0.078 \times 3.5 + 0.053 = 0.326 \text{ l/sec.}$

Nine (9) sanitary service connections are proposed to be connected to the sanitary sewer extension with built in tees on Klondike Road. The arrangement of service connections are shown on Drawing C101.

4.3 Sanitary Sewer Extension on Klondike Road

As per pre consultation comments, extension of sanitary sewer on Klondike Road is required to service the site. Sanitary sewer extension is shown on Drawing C104 which is based on the design proposed by Novatech for 1051 Klondike Road development. Sanitary Sewer sizing calculations are attached in **Appendix D**.

4.4 Effect of Proposed Development on Downstream Sanitary Infrastructure

The proposed development is not part of the contributing area for Briar Ridge Pump station. As per sanitary flow calculations, an additional flow of 0.5 l/sec is added to the sanitary sewer on Klondike Road. The additional flow gets reduced to 0.3 l/sec downstream due to the peak factor calculations at higher population counts. The pre and post development sanitary flows are shown in Appendix D.

4.5 Summary and Conclusions

The proposed development requires extension of sanitary sewer west of Sandhill street intersection. An additional flow of 0.5 l/sec is added to the existing sanitary infrastructure which is considered a small addition that will not compromise the sanitary sewer/ pump station capacity or result in significant change to the sanitary hydraulic grade line.



5. Storm Servicing and Stormwater Management

5.1 Background

The existing site does not have a piped storm connection. The site sheet drains to Klondike Road without any storm water management controls.

5.2 Storm Servicing Strategy

The proposed stormwater management system will provide the necessary detention storage on site to meet the stormwater management requirements. Quantity control will be provided to control the post development flows to the stipulated subdivision criteria of 85 l/sec/ha.

5.3 Proposed Storm Servicing

A new 300 mm diameter storm service will extend from the east side of the proposed development to connect to the existing 675mm storm sewer on Sandhill Street. The proposed pre-development and post-development catchment areas, runoff coefficients and catchment total areas are indicated in **Appendix E**.

5.4 Design Criteria (Minor and Major Systems)

The site specific SWM criteria as per the comments from the city's pre consultation meeting are as follows,

- Refer to the SWM design criteria in the Shirley's Brook SWM Facility "C" Detailed Design Report (prepared by Novatech, 2006) for the proposed development area:
 - Minor system allowable release rate of 85 L/s/ha;
 - Onsite major system storage of 50 m³/ha

5.5 Stormwater Quantity Control

5.5.1 Peak Flows

Table E1 attached in Appendix E shows the overall pre development site runoff coefficient as 0.50 which is in line with the pre consultation comments limiting the pre development runoff coefficient to 0.5 or less. As per sanitary catchment plan of Pond C storm sewers, the site is included in the catchment Area 59 (Refer Brookside Sub division Storm Drainage Plan attached in Appendix E) at a runoff coefficient of 0.45. Further a minor system flow rate of 85 l/sec/ha is recommended as per pre consultation comments. The allowable flow as per these limiting criteria are presented in Table 5 below to demonstrate that the site has been over controlled to the most stringent case.

Table 5– Allowable Flow Summary

Return Period	Catchment	Pre Dev Flows	Pre Dev Flows
(yrs)	Area*	@ R =0.45	@ 85 l/sec/ha
	(ha)	(1/sec)	(1/sec)
2	0.128	12	10.88
5	0.128	17	10.88
10	0.128	20	10.88
25	0.128	23	10.88
50	0.128	26	10.88
100	0.128	29	10.88

^{*-} Site Area A1 & A2(0.128ha) is the controlled area. Area A3 (0.029ha) is uncontrolled due to grading constraints and is deducted from pre and post development flow calculations.

As per orifice sizing (Refer Table E6, Appendix E), an allowable flow of 10.21 l/sec has been used for storage calculations using Rational formulae .



Intensity is calculated by the following formulae,

$$i = \underbrace{A \atop (Td+C)B}$$

where A, B and C are all factors of the IDF Return Period, T_d being the time of concentration and A the drainage area (Detailed calculations provided in **Appendix E**).

Time of concentration is determined using the inlet time graph (Appendix 5D Ottawa City Sewer Design Guidelines) which results in a value less than 10 minutes. Therefore 10 minutes will be used to calculate peak flows.

As per subdivision criteria, the site will be controlled to 85 l/sec/ha which provides an allowable release rate of 13.6 l/sec.

5.5.2 Stormwater Management Concept

The roof will be controlled to 9.0 l/sec with the help of flow control roof drains. The total roof area is 520 m². Storage area calculations (Table E5, Appendix E) shows that the roof will provide 8.6 m³ storage for a restricted flow of 9.0 l/sec.

Flow will be detained on the roof by installing parabolic weirs, (Zurn Z105 Control Flo Roof Drain), using 9 numbers of proposed roof drains limiting the flow from the roof to 9.0 l/s. The maximum ponding depth on the roof will be 50mm and the roof detention will clear in a maximum time of 40 minutes. Drain specs are attached in Appendix E.

5.5.3 Summary

Table 6 summarizes the proposed release rates and confirms that the total release rate does not exceed the allowable release rate.

Table 6 – Post-Development Controlled Peak Flows

	Post-Development Controlled Peak Flows (L/s)
Allowable Release Rate (I/sec)	10.88
Release Rate from Controlled Drainage Areas (I/sec)	10.21
Required Storage (m³)	27.96
Provided Storage (m³)	30.5

The required storage of 27.96 m³ (Table E4, Appendix E) is met by the available onsite parking storage of 30.50 m³ (8.6m³ of roof storage & 21.9 m³ of infiltration tank storage).

5.5.4 Impact on Existing Stormwater Infrastructure

The proposed development was included as Catchment Area 59 (Refer Brookside Sub division Storm Drainage Plan in Appendix E). The plan shows that the site was accounted as a catchment area with runoff coefficient of 0.45 which allows a 5 year flow of 17.0 l/sec. As described in



section 5.5.1, the onsite quantity controls limit the site discharge to 10.21 l/sec to ensure that the downstream storm sewers and storm water pond "C" capacity and hydraulic grade line is not effected by the proposed development.

Storm Sewer Design Calculations are provided in Appendix E.

5.6 Storm Water Quality Control

The required water quality treatment is achieved with the help of a treatment train approach comprising of the following measures,

- 1- RVCA considers run-off from building roof areas to be "clean", and therefore not require quality control.
- 2- An infiltration tank consisting of below ground modular structure is proposed to be installed to fulfill the quantity control storage requirement. As the infiltration tank has an open bottom configuration, all flow that gets infiltrated will achieve 100% quality improvement.
- 3- Oil/grit separator(OGS) has been proposed as Stormceptor EF-4 unit shown on Drawing C101, Appendix A. The sizing calculations are attached in Appendix E which shows that the unit is capable of achieving 90% TSS removal for site flows.

5.7 Pre-Consultation with MECP and Conservation Authority

Due to the municipal sanitary sewer extension, a Ministry of Environment, Conservation and Parks Environmental Compliance Approval (MECP ECA) will be required and will be reviewed under the Transfer of Review program (Standard Works) with the City of Ottawa. Also due to the municipal sanitary extension, a Municipal Consent (MC) circulation will be required after or in the later stages of the Site Plan Application stage. The ROW Approvals Department at the City, may, to their review and discretion, exempt the proposed extension from the MC Circulation process.

5.8 Minor and Major Systems

The minor storm sewer system consists of the storm connection from the townhouse block up to the city storm sewer on Sandhill Road. The major system consists of flow east through the laneway on to Sandhill Road. The site will be graded to direct run-off from storms in excess of the 100-year event safely to Sandhill Road.

Individual townhouse roof areas will be connected to the private storm sewer on the laneway though service connections as shown on Drawing C101, Appendix A.

5.9 Impacts to Receiving Watercourses

No negative impacts to receiving watercourses are anticipated.

5.10 100 Year Flood Levels and Major Flow Routing

The site is not within a 100-year floodplain.

6. Grading

The proposed grading plan is shown in Drawing C102 in **Appendix A**. The development will be tied into existing sidewalk grades along Sandhill Road and Klondike Road.

The existing grades will be matched at the property limits along the south and west property boundary.



7. Erosion and Sediment Control

During all construction activities, erosion and sedimentation shall be controlled by the following techniques:

- Extent of exposed soils shall be limited at any given time;
- Exposed areas shall be re-vegetated as soon as possible;
- Minimize the area to be cleared and disruption of adjacent areas;
- Siltsack or approved equivalent shall be installed inside all catch basins, catch basin manholes, and storm manholes as identified on the erosion and sediment control plan;
- Mud matt is required at the construction entrance to prevent mud tracking on municipal roads. Mud matt to be installed and maintained as indicated on the erosion and sediment control plan;
- Visual inspection shall be completed daily on sediment control barriers and any damage repaired immediately. Care will be taken to prevent damage during construction operations;
- In some cases, barriers may be removed temporarily to accommodate the construction operations. The affected barriers will be reinstated at night when construction is completed;
- Sediment control devices will be cleaned of accumulated silt as required. The deposits will be disposed of as per the requirements of the contract;
- During construction, if the engineer believes that additional prevention methods are required
 to control erosion and sedimentation, the contractor will install additional silt fences or other
 methods as required to the satisfaction of the engineer; and,
- Construction and maintenance requirements for erosion and sediment controls are to comply with Ontario Provincial Standard Specification (OPSS) 805.

We trust you will find this submission complete and in order. Should you have any questions, please contact the undersigned.

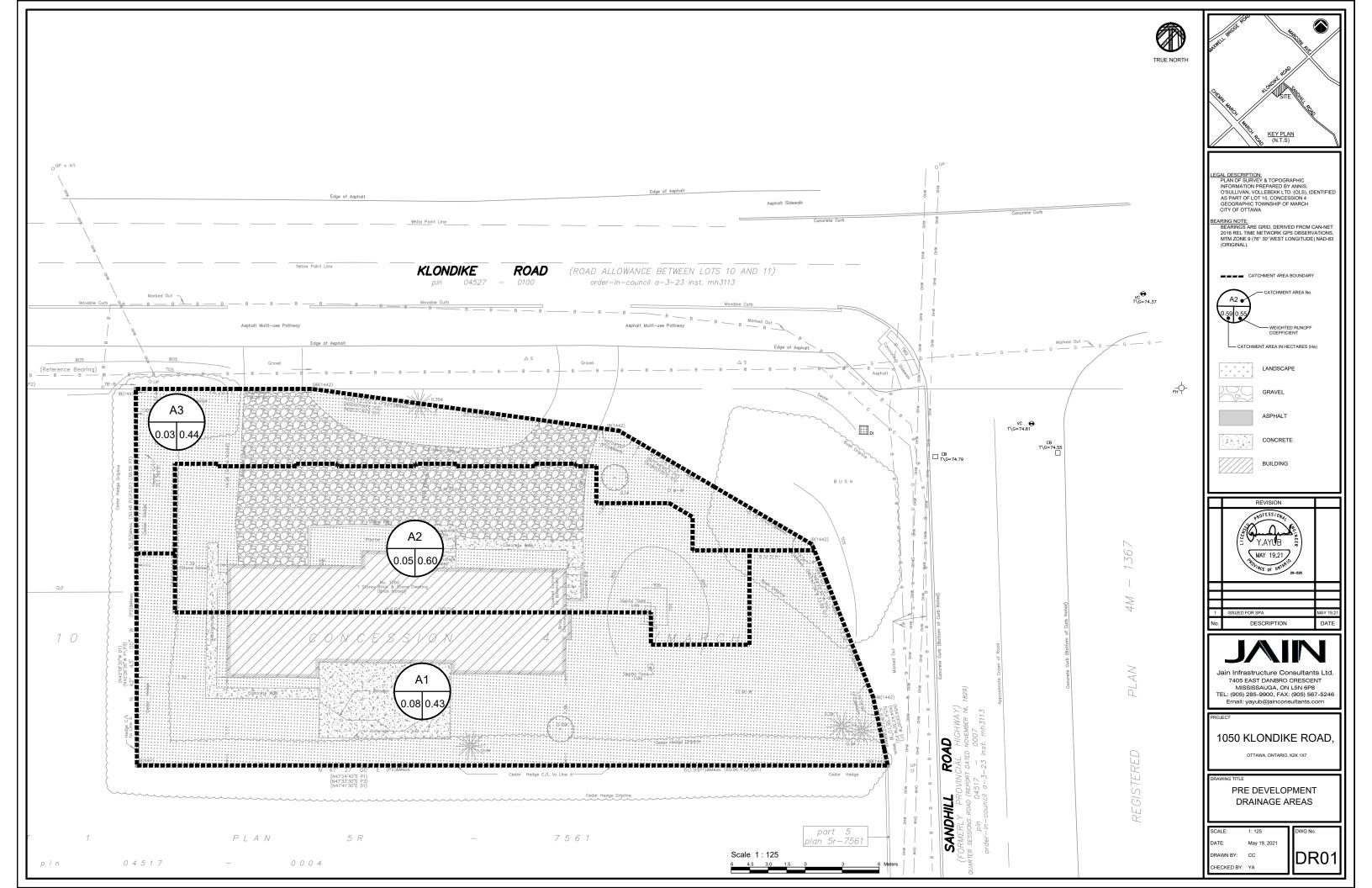
Respectfully Submitted, Jain Infrastructure Consultants Ltd.

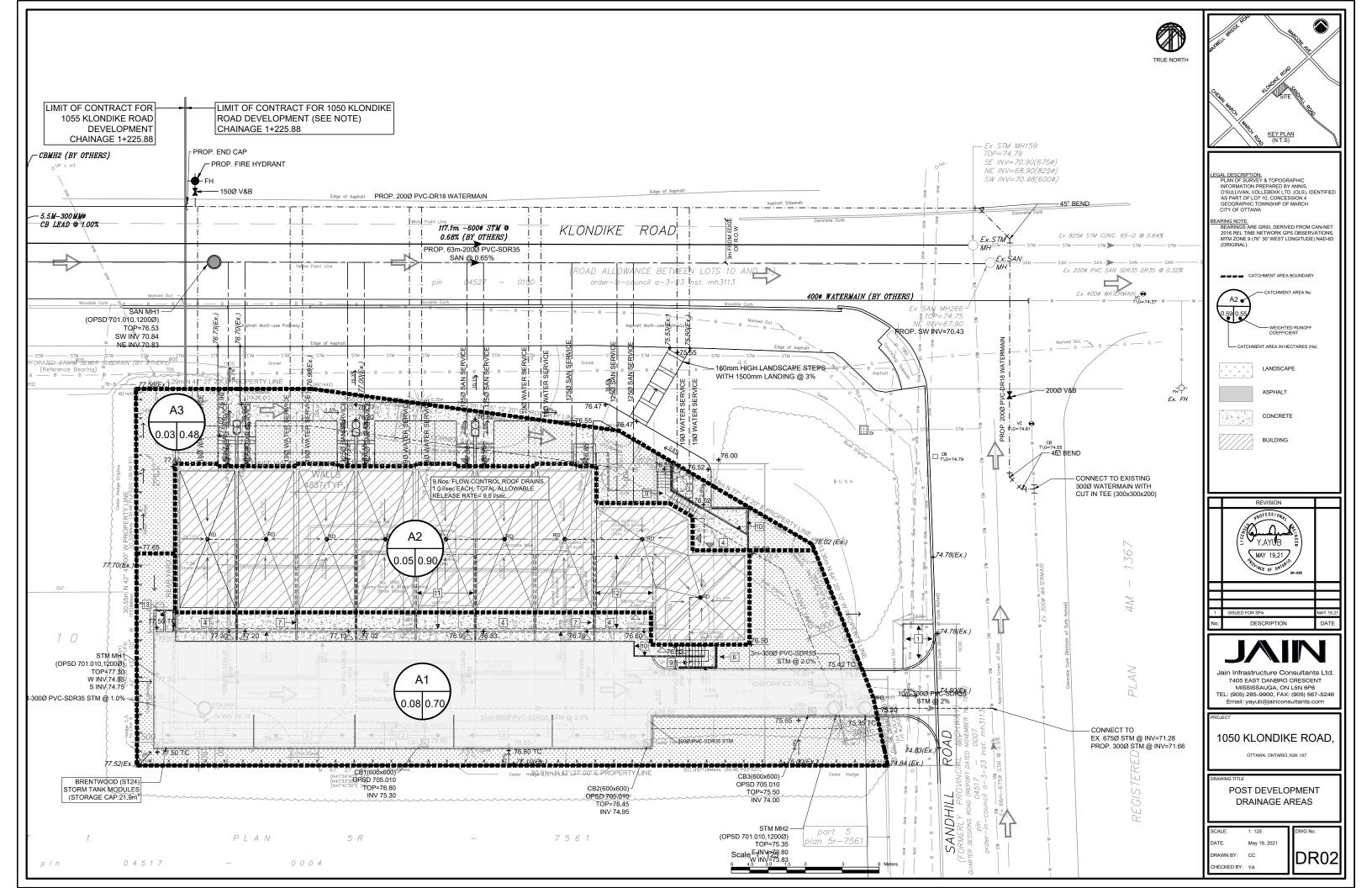


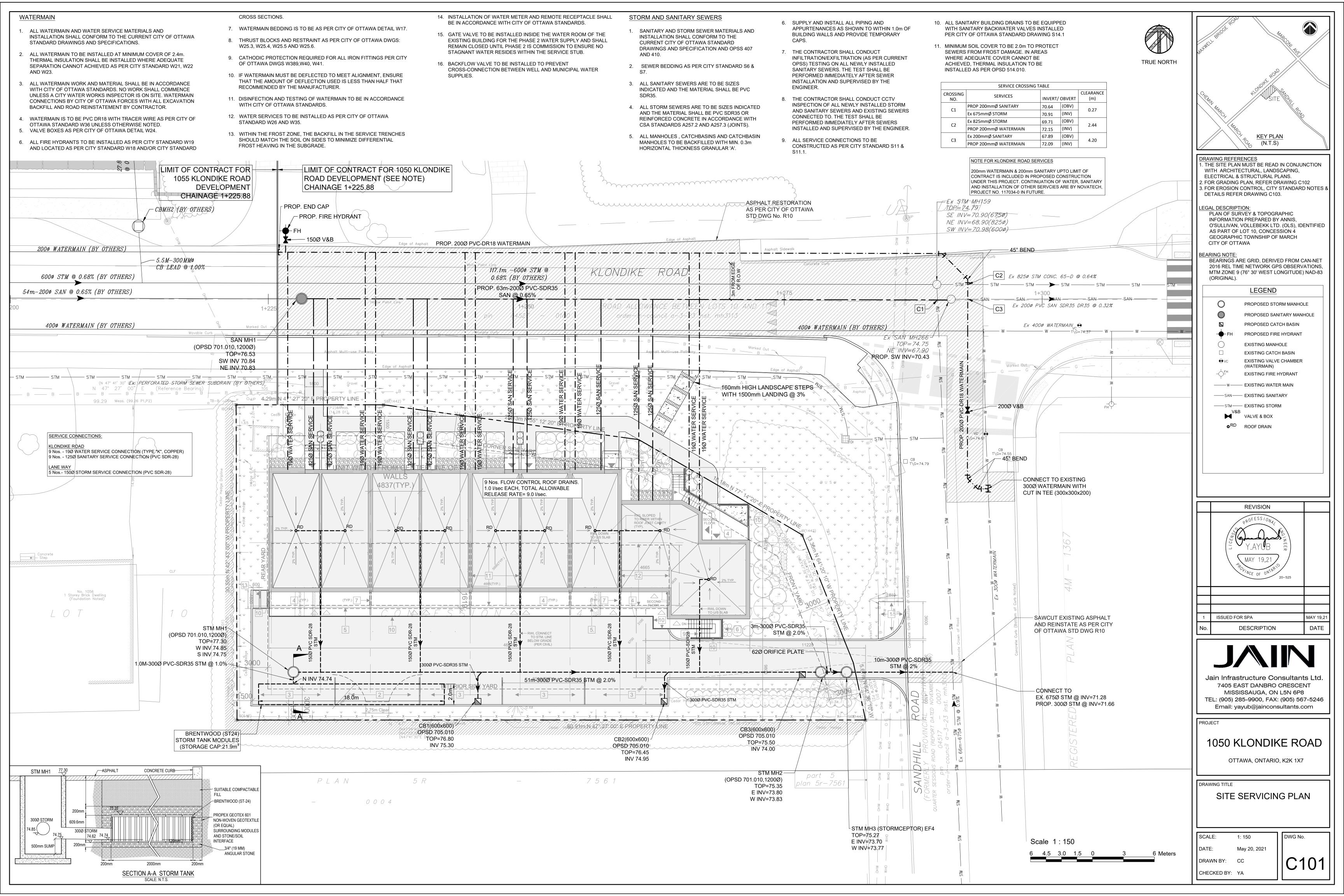
Yasar Ayub , P.Eng Project Engineer May 20, 2021

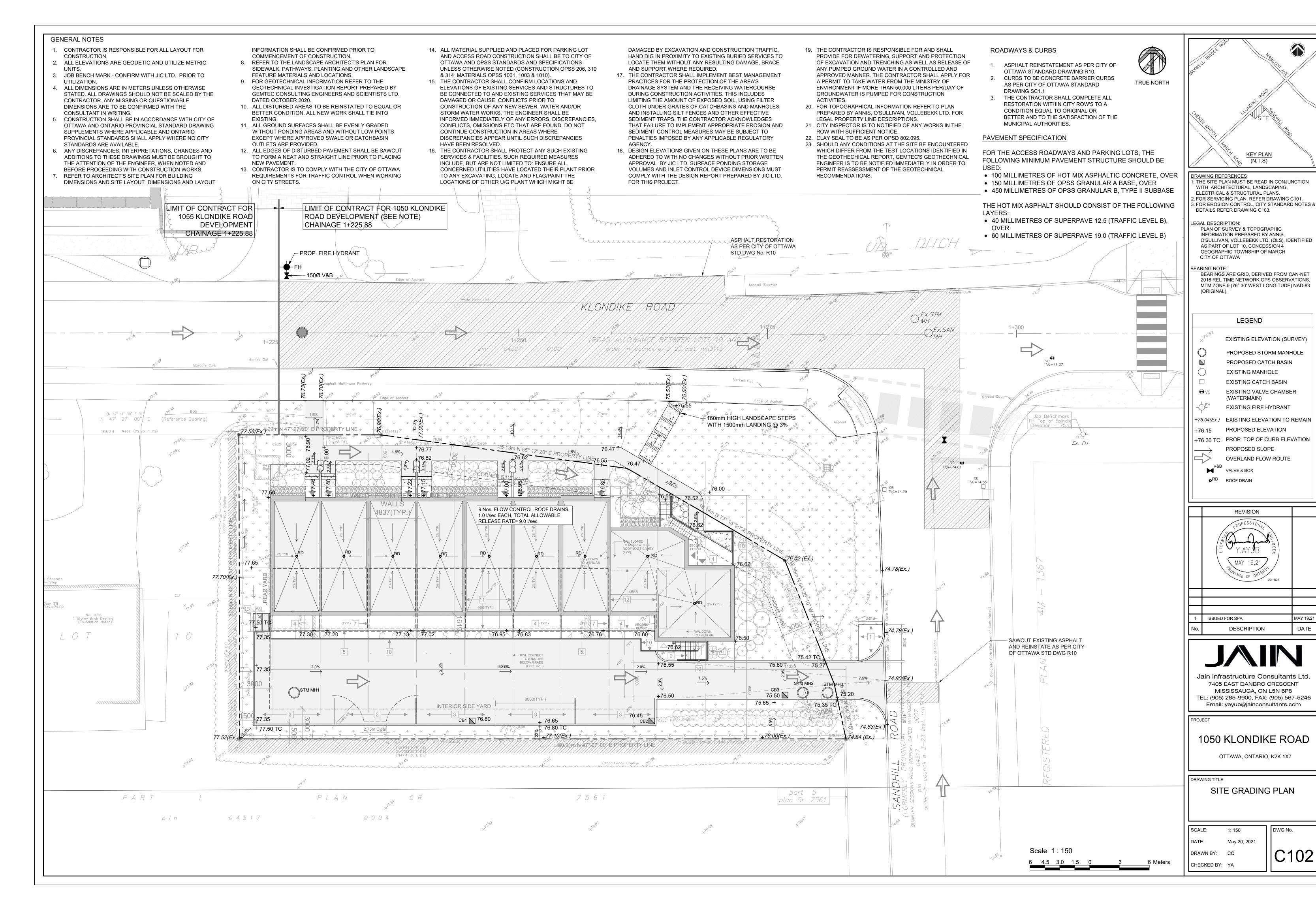
Appendix A Figures

DR01 Pre Development Drainage Areas
DR02 Post Development Drainage Areas
Site Servicing, Grading and Erosion and Sediment Control Plan



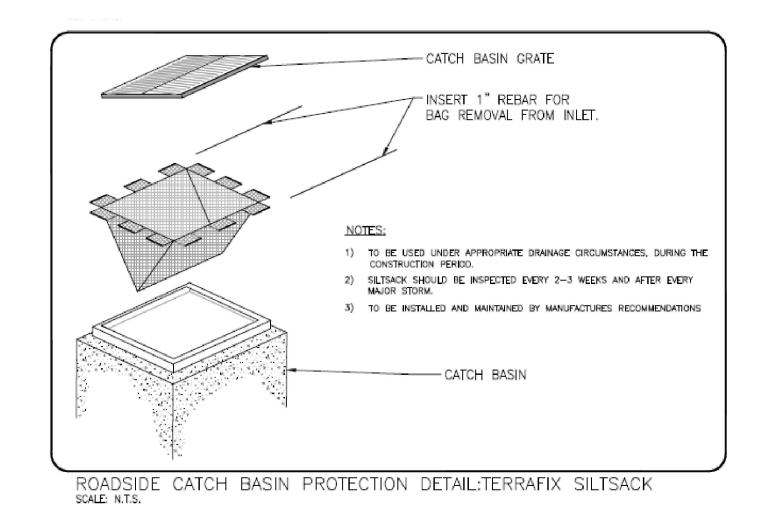






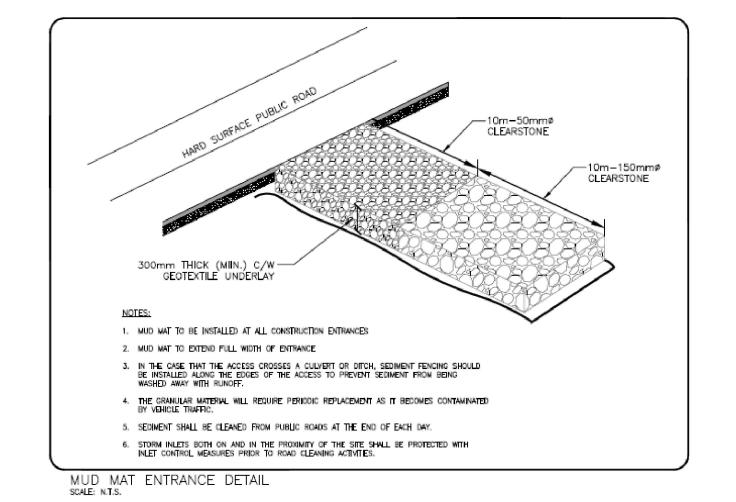
DATE





LEGEND:

SEDIMENT CONTROL FENCE



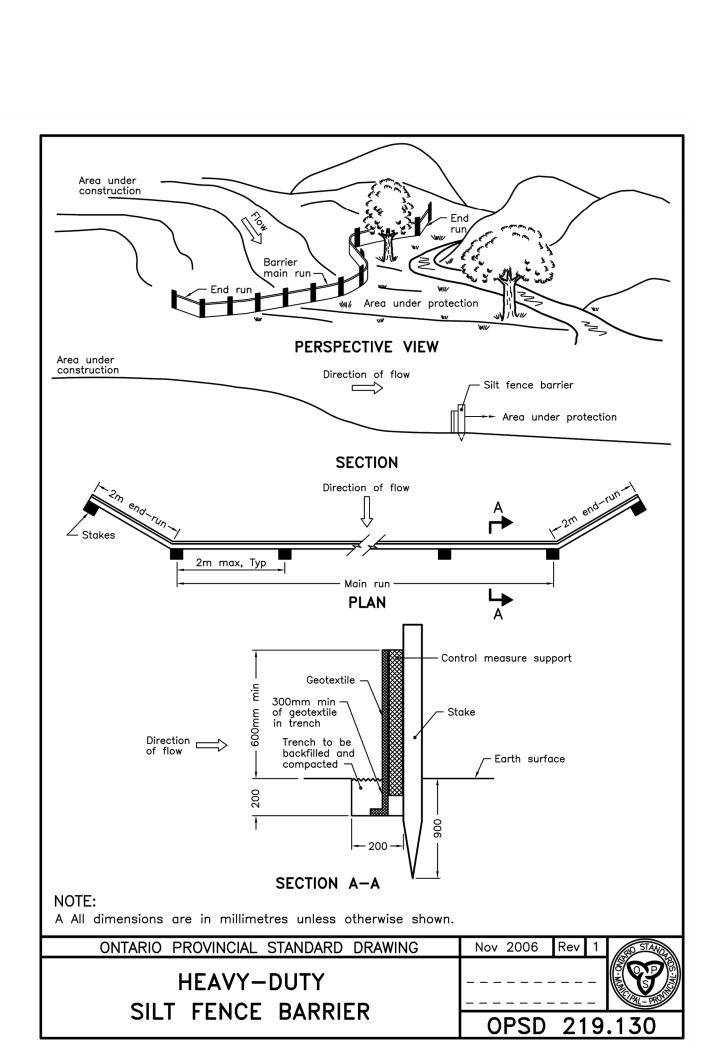
EROSION AND SEDIMENT CONTROL NOTES

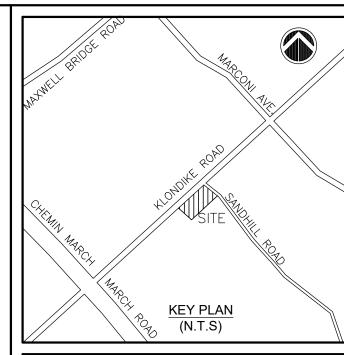
- 1. THE CONTRACTOR SHALL IMPLEMENT BEST MANAGEMENT PRACTICES, TO PROVIDE FOR PROTECTION OF THE AREA DRAINAGE SYSTEM AND THE RECEIVING WATERCOURSE, DURING CONSTRUCTION ACTIVITIES. THIS INCLUDES LIMITING THE AMOUNT OF EXPOSED SOIL, USING FILTER CLOTH UNDER THE GRATES OF CATCHBASINS AND MANHOLES, AND INSTALLING SILT FENCES AND OTHER EFFECTIVE SEDIMENT TRAPS. THE CONTRACTOR ACKNOWLEDGES THAT FAILURE TO IMPLEMENT APPROPRIATE EROSION AND SEDIMENT CONTROL MEASURES MAY BE SUBJECT TO PENALTIES IMPOSED BY ANY APPLICABLE REGULATORY AGENCY.
- 2. THE SEDIMENT CONTROL MEASURES SHALL ONLY BE REMOVED WHEN, IN THE OPINION OF THE ENGINEER, THE MEASURES ARE NO LONGER REQUIRED. NO CONTROL MEASURES MAY BE PERMANENTLY REMOVED WITHOUT PRIOR AUTHORIZATION FROM THE ENGINEER.
- REGULAR INSPECTION AND MAINTENANCE OF THE EROSION AND SEDIMENT
 MEASURES SHALL BE UNDERTAKEN. THE IMPLEMENTATION AND ADJUSTMENT
 AND/OR CORRECTIVE MAINTENANCE OF THE EROSION AND SEDIMENT MEASURES IS
 AN INTEGRAL PART OF THE PLAN AND MUST BE PERFORMED.
 GEOTEXTILE FILTER FABRIC SHALL BE PLACED BETWEEN THE STRUCTURE FRAME

AND COVER FOR ALL MANHOLES, CATCHBASINS, AND CATCHBASIN MANHOLES IN

- THE VICINITY OF WORK.

 5. THE CONTRACTOR SHALL MAINTAIN ADJACENT ROADS IN A CLEAN CONDITION AT
- 6. PROVIDE MUD MATS AT SITE CONSTRUCTION ENTRANCE(S) AND EGRESS(S).





DRAWING REFERENCES

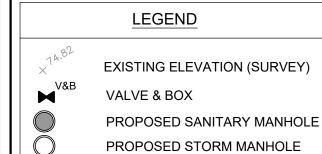
1. THE SITE PLAN MUST BE READ IN CONJUNCTION WITH ARCHITECTURAL, LANDSCAPING, ELECTRICAL & STRUCTURAL PLANS.
2. FOR SERVICING PLAN, REFER DRAWING C101.
3. FOR GRADING PLAN, REFER DRAWING C102.

EGAL DESCRIPTION:

PLAN OF SURVEY & TOPOGRAPHIC INFORMATION PREPARED BY ANNIS, O'SULLIVAN, VOLLEBEKK LTD. (OLS), IDENTIFIED AS PART OF LOT 10, CONCESSION 4 GEOGRAPHIC TOWNSHIP OF MARCH CITY OF OTTAWA

RING NOTE:

BEARINGS ARE GRID, DERIVED FROM CAN-NET 2016 REL TIME NETWORK GPS OBSERVATIONS, MTM ZONE 9 (76° 30' WEST LONGITUDE) NAD-83 (ORIGINAL).



EXISTING MANHOLE

EXISTING CATCH BASIN

EXISTING VALVE CHAMBER

+76.04(Ex.) EXISTING FIRE HYDRANT

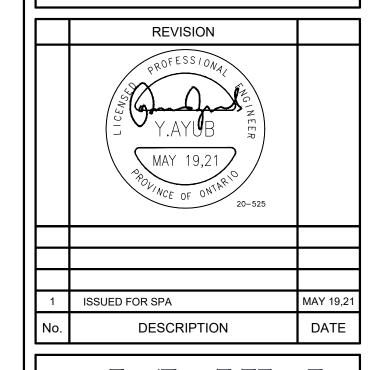
+76.04(Ex.) EXISTING ELEVATION TO REMAIN

(WATERMAIN)

+76.15 PROPOSED ELEVATION +76.30 TC PROP. TOP OF CURB ELEVATION

OVERLAND FLOW ROUTE

PROPOSED SLOPE





Jain Infrastructure Consultants Ltd.
7405 EAST DANBRO CRESCENT
MISSISSAUGA, ON L5N 6P8
TEL: (905) 285-9900, FAX: (905) 567-5246
Email: yayub@jainconsultants.com

PROJECT

1050 KLONDIKE ROAD

OTTAWA, ONTARIO, K2K 1X7

DRAWING TITLE

EROSION CONTROL PLAN & DETAILS

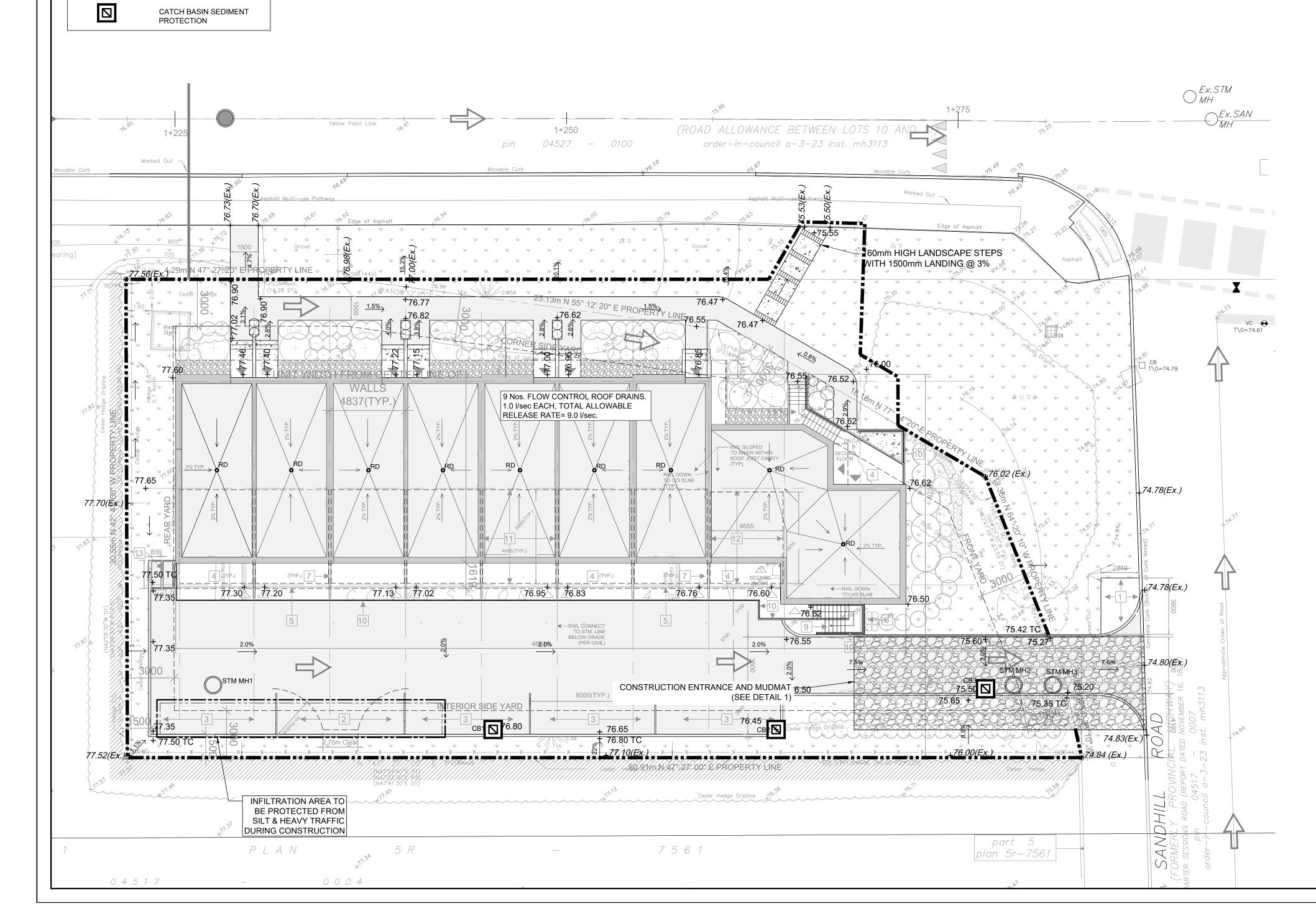
SCALE: 1: 150

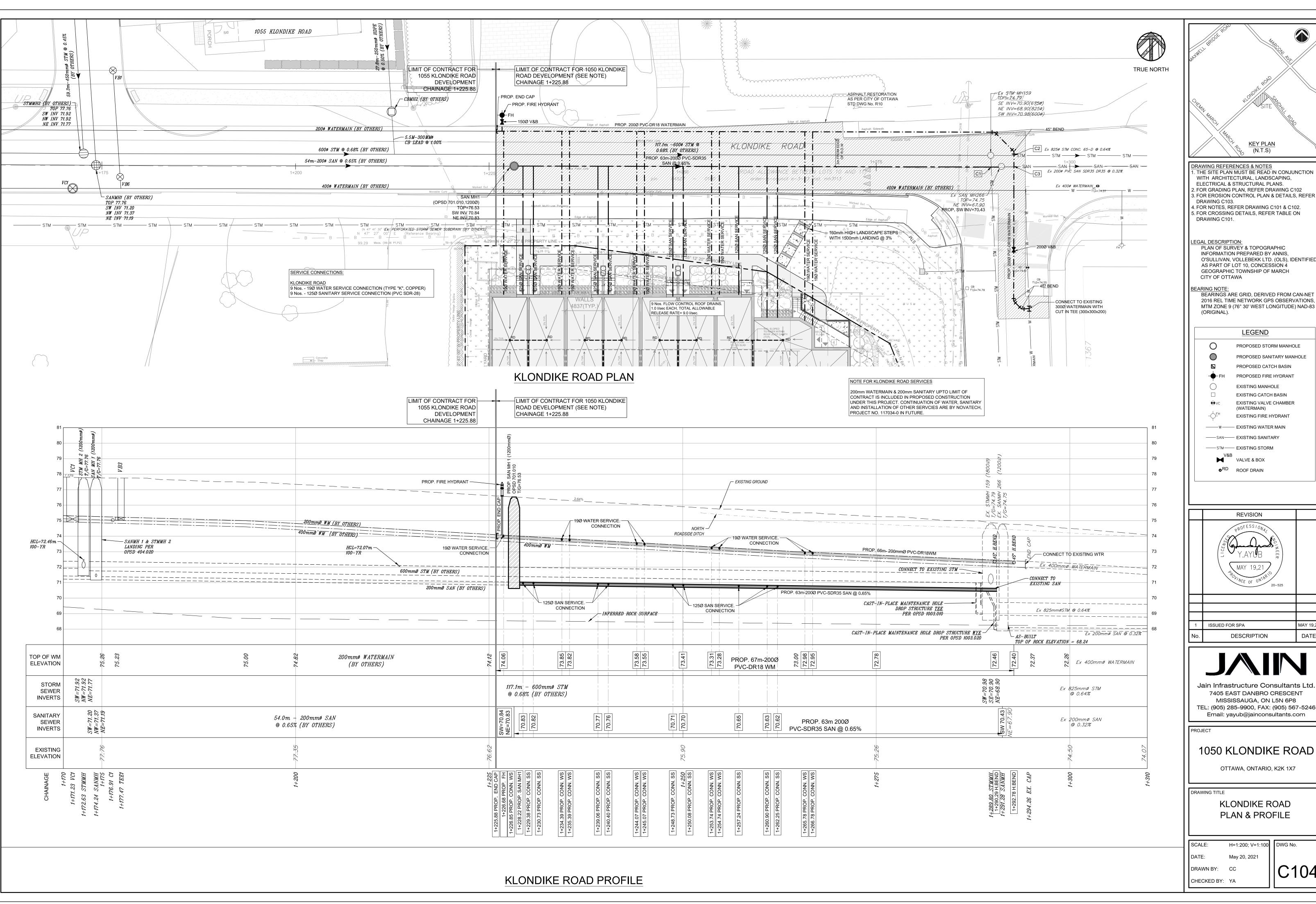
DATE: May 20, 2021

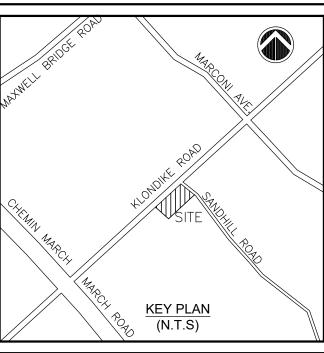
DRAWN BY: CC

DWG No.

CHECKED BY: YA







DRAWING REFERENCES & NOTES

1. THE SITE PLAN MUST BE READ IN CONJUNCTION WITH ARCHITECTURAL, LANDSCAPING, ELECTRICAL & STRUCTURAL PLANS.

DRAWING C103. 4. FOR NOTES, REFER DRAWING C101 & C102. 5. FOR CROSSING DETAILS, REFER TABLE ON

PLAN OF SURVEY & TOPOGRAPHIC INFORMATION PREPARED BY ANNIS, O'SULLIVAN, VOLLEBEKK LTD. (OLS), IDENTIFIED AS PART OF LOT 10, CONCESSION 4 GEOGRAPHIC TOWNSHIP OF MARCH

BEARINGS ARE GRID, DERIVED FROM CAN-NET 2016 REL TIME NETWORK GPS OBSERVATIONS, MTM ZONE 9 (76° 30' WEST LONGITUDE) NAD-83

<u>LEGEND</u>

PROPOSED STORM MANHOLE PROPOSED SANITARY MANHOLE

PROPOSED CATCH BASIN PROPOSED FIRE HYDRANT

EXISTING CATCH BASIN EXISTING VALVE CHAMBER (WATERMAIN)

-----SAN----- EXISTING SANITARY

VALVE & BOX

•RD ROOF DRAIN

REVISION ISSUED FOR SPA

DATE

Jain Infrastructure Consultants Ltd. 7405 EAST DANBRO CRESCENT MISSISSAUGA, ON L5N 6P8 TEL: (905) 285-9900, FAX: (905) 567-5246 Email: yayub@jainconsultants.com

1050 KLONDIKE ROAD

OTTAWA, ONTARIO, K2K 1X7

KLONDIKE ROAD PLAN & PROFILE

H=1:200; V=1:100 May 20, 2021

DWG No.

CHECKED BY: YA

Appendix B Correspondence with Regulatory Authorities

Yasar Ayub

Subject: FW: 1050 Klondike Road - preconsultation meeting notes

---- Forwarded Message -----

From: McCreight, Laurel < laurel.mccreight@ottawa.ca>

To: Deborah Belfie < belfied@rogers.com >

Sent: Tuesday, May 26, 2020, 03:52:36 p.m. EDT

Subject: Pre-Consultation Follow-Up: 1050 Klondike Road

Hi Debbie.

Please refer to the below regarding the Pre-Application meeting held on May 21, 2020 for the property at 1050 Klondike Road for a Zoning By-law Amendment and Site Plan Control Application for a 4-storey apartment building. I have also attached the required Plans & Study List for application submission.

Below are staff's preliminary comments based on the information available at the time of the pre-consultation meeting:

Planning / Urban Design

- The parking on the ground floor in the proposed design concept must be redesigned, as it will have significant negative impacts on the public realm.
- The proposed design concept requires more animation to both Klondike and Sandhill. This could include revising the proposal with:
 - o Removing the two vehicular accesses and provide only one access off Sandhill;
 - Removing the vehicle maneuvering area in the front encroaching into the public right of way;
 - o Revising the location of the garbage room that directly faces the street;
 - Providing underground parking and
 - Relocating the bike parking away from the façade of the building.
- The majority of the units, which are south facing, are approximately 3 metres away from the property line. This could be concerning depending on the development potential on the abutting property.
- The road closure at the corner of Klondike and Sandhill, if possible, can potentially alleviate some pressures and offer some flexibilities for design. Regardless of the final lot configuration, the design should:
 - Animate both public streets (neither ground floor parking nor blank walls should be allowed);
 - o Improve public realm through adequate provision of landscaping and architecture design;
 - Ensure access to natural lights for all units in the long run taking into consideration development potential on abutting properties; and
 - Provide adequate private amenities.
- A scoped Design Brief is required for the rezoning application. The Terms of Reference of the Design Brief is attached to provide guidance.
- You are encouraged to contact the Ward Councillor, Councillor Jenna Sudds, about the proposal.

Engineering

- The Servicing Study Guidelines for Development Applications are available here.
- Servicing and site works shall be in accordance with the following documents:
 - Ottawa Sewer Design Guidelines (October 2012)
 - Ottawa Design Guidelines Water Distribution (2010)
 - Geotechnical Investigation and Reporting Guidelines for Development Applications in the City of Ottawa (2007)
 - City of Ottawa Slope Stability Guidelines for Development Applications (revised 2012)
 - City of Ottawa Environmental Noise Control Guidelines (January 2016)
 City of Ottawa Park and Pathway Development Manual (2012)
 - City of Ottawa Accessibility Design Standards (2012)
 - Ottawa Standard Tender Documents (latest version)
 - o Ontario Provincial Standards for Roads & Public Works (2013)
- Record drawings and utility plans are also available for purchase from the City (Contact the City's Information Centre by <u>email</u> or by phone at (613) 580-2424 x.44455).
- For the re-zoning application, please provide a site serviceability study proving the site can be serviced
 by the existing municipal infrastructure and discuss any improvements that may be required to service
 the proposed site.
- Sanitary Infrastructure
 - There is an available 200mm diameter PVC sanitary sewer located on Klondike Road.
 However, it currently does not front the proposed site.
 - A sanitary sewer extension within the Klondike Road Right-Of-Way (ROW) will be required to service this site. The sanitary sewer can be extended solely the +/-20m required to service the site, and does not need to extend the full length of the site's Klondike Road frontage.
 - The proponent will be required to demonstrate what the expected sanitary flows from the proposed site will be and show that the existing sanitary sewer infrastructure can accommodate the proposed site flows without any adverse affects.
 - The existing sanitary sewer on Klondike Road connects to the Briar Ridge Pump Station (BRPS). This pump station currently has limited capacity. Upgrades to the BRPS are expected to be completed by Dec 2021 or early 2022.
 - Due to the municipal sanitary sewer extension a Ministry of Environment, Conservation and Parks Environmental Compliance Approval (MECP ECA) will be required and will be reviewed under the Transfer of Review program (Standard Works) with the City of Ottawa.
 - Also due to the municipal sanitary extension, a Municipal Consent (MC) circulation will be required after or in the later stages of the Site Plan Application stage. The ROW Approvals Department at the City, may, to their review and discretion, exempt the proposed extension from the MC Circulation process.

Watermain

- There is an available 305mm diameter PVC watermain fronting the site along Sandhill Road.
 However, looping of the Klondike Road watermain (from March Road stub to the Sandhill Road stub) is preferred.
- Water frontage charges will not apply.
- If a watermain extension along Klondike Road is pursued an MECP Form 1 will need to be completed.
- Drinking Water Boundary condition requests must include the location of the service connection and the expected loads required by the proposed development. Please provide the following information:
 - a. Location of service (map/plan view)
 - b. (Draft) site plan or similar plan for building location
 - c. Fire flow demand: ____L/s (as per FUS, 1999)
 - d. Average daily demand: ___ L/s.
 - e. Maximum daily demand: ____L/s.

- f. Maximum hourly daily demand: L/s.
- g. Supporting calculations for domestic demands
- h. Supporting calculations for FUS required fire flow
- The Stormwater Management Criteria, for the subject site, is to be based on the following:
 - There is an available 675mm diameter concrete storm sewer located on Sandhill Road conveying flow to a ditch upstream of "Pond C".
 - Based on both the Shirley's Brook Floodplain Analysis and SWM Report (Klondike Road Development Lands, prepared by Novatech, May 2006) and the Shirley's Brook SWM Facility "C" Detailed Design Report (prepared by Novatech, 2006), it appears that Pond "C" was sized to service the 1050 Klondike Road parcel. Please demonstrate that the existing storm sewer and pond have capacity to service this proposed development (quantity and quality control).
 - Refer to the SWM design criteria in the Shirley's Brook SWM Facility "C" Detailed Design Report (prepared by Novatech, 2006) for the proposed development area:
 - a. Minor system allowable release rate of 85 L/s/ha;
 - b. Onsite major system storage of 50 m³/ha (please see the note below);
 - c. ICDs [are] installed in the roadway catchbasins to ensure flow into the storm sewer system does not exceed the 5-year runoff rates; and
 - d. HGL for 100-year event must have at least 0.3 m freeboard to the underside of footings.
 - IDF information derived from the Meteorological Services of Canada rainfall data, taken from the MacDonald Cartier Airport, collected 1966 to 1997.
 - o The pre-development runoff coefficient or a maximum equivalent 'C' of 0.5, whichever is less (§ 8.3.7.3).
 - A calculated time of concentration (Cannot be less than 10 minutes).
 - Use of rooftop controls are recommended for this site, but are not limited to them, to meet the requirements.
- Please note that there is a Special Area Development Charge for the subject site. Please refer to the current W-2
 Development Charge Brochure attached. You can find By-Law No. 2019 163 online on the City of Ottawa
 website. Note that this is the Charge for 2019 and may change over time.
- If the site plan changes to include underground parking, a Geotechnical Report will be required for the Re-Zoning application. If not, the Geotechnical Report will be required at Site Plan Application stage.

Please contact Infrastructure Project Manager Gabrielle Schaeffer for follow-up questions.

Transportation

- Only one access off Sandhill should be provided.
- On site plan:
 - Show all details of the roads abutting the site up to and including the opposite curb; include such items as pavement markings, accesses and/or sidewalks.
 - Turning templates will be required for all accesses showing the largest vehicle to access the site; required for internal movements and at all access (entering and exiting and going in both directions).
 - o Show all curb radii measurements; ensure that all curb radii are reduced as much as possible
 - Show lane/aisle widths.
 - o Provide dedicated pedestrian paths.
 - o Grey out any area that will not be impacted by this application.

Please contact Transportation Project Manager, Mike Giampa for follow-up questions.
<u>Other</u>
Please refer to the links to "Guide to preparing studies and plans" and fees for general information. Additional information is available related to building permits, development charges, and the Accessibility Design Standards. Be aware that other fees and permits may be required, outside of the development review process. You may obtain background drawings by contacting informationcentre@ottawa.ca.
These pre-consultation comments are valid for one year. If you submit a development application(s) after this time, you may be required to meet for another pre-consultation meeting and/or the submission requirements may change. You are as well encouraged to contact us for a follow-up meeting if the plan/concept will be further refined.
Please do not hesitate to contact me if you have any questions.
Regards,
Laurel
Laurel Ma Our lake MOID, DDD
Laurel McCreight MCIP, RPP
Planner
Development Review West
Urbaniste
Examen des demandes d'aménagement ouest
City of Ottawa Ville d'Ottawa
613.580.2424 ext./poste 16587
ottawa.ca/planning_ / ottawa.ca/urbanisme

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Yasar Ayub

To: Yasar Ayub

Subject: FW: 1050 Klondike Kanata - Confirmation for Extent of Services on Klondike Road.

Hi Yasar,

Pardon the delay. As we discussed over the phone last month, the applicant can service 1050 Klondike from either Sandhill Rd (Option 2) or Klondike Road for sanitary and water, however Option 1 is not a preferred approach. Since the proposal is no longer a low-rise building, but now townhouses, services for each townhouse can be provided from either the proposed laneway or from Klondike Rd directly. The City's preference would be to service the townhouses from Klondike Road as this would extend the City infrastructure and reduces the shared maintenance costs of the townhouses for the shared private infrastructure through the rear private lane.

I also mentioned that there is a proposed development at 1055 Klondike that is proposing to extend the sanitary and water infrastructure along Klondike Road, however I am currently unsure of their timelines. Please take a look on the City of Ottawa Development Applications Search Tool (link) to find the latest plans produced by the nearby 1055 Klondike Rd under development application D07-16-19-0024 to see how they have approached the Klondike Road sewer and watermain extensions. Perhaps you can reach out to the developer of 1055 Klondike to coordinate works.

Please let me know if you have further questions.

Regards,

Gabrielle (Gabi) Schaeffer, P.Eng

Senior Engineer - Infrastructure Applications

City of Ottawa

Development Review - West Branch
Planning, Infrastructure and Economic Development Department
110 Laurier Ave., 4th Floor East;

Ottawa ON K1P 1J1 Mail Code 01-14

Tel: 613-580-2424 x 22517

Cell: 613-227-7419 Fax: 613-560-6006

During this period of uncertainty surrounding COVID-19, we are following recommended best practices to minimize the risk of exposure, while ensuring service to our clients remains as uninterrupted as possible. I am working from home, and my work hours may be affected, but I will respond to emails at my earliest opportunity. Should there be delays, I thank you for your understanding and patience.

From: Yasar Ayub < yayub@jainconsultants.com>

Sent: March 16, 2021 12:58 PM

To: Deborah Belfie < belfied@rogers.com >; Schaeffer, Gabrielle < gabrielle.schaeffer@Ottawa.ca >

Cc: Junaid Israr < jisrar@gmail.com; israr akhtar < jisrar@hotmail.com>

Subject: RE: 1050 Klondike Kanata - Confirmation for Extent of Services on Klondike Road.

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On Wednesday, February 24, 2021, 11:15:56 a.m. EST, Yasar Ayub yayub@jainconsultants.com wrote:

Hi Gabrielle.

Just checking to see if you were able to consult with other city staff and give your feedback on the servicing arrangement for the revised proposal. We will then need to discuss with our client and proceed with one of the three options.

Yasar

416.668.6367

From: Yasar Ayub

Sent: February 18, 2021 1:18 PM

To: Schaeffer, Gabrielle <gabrielle.schaeffer@Ottawa.ca>

Cc: Deborah Belfie <belfied@rogers.com>; Junaid Israr <jisrar@gmail.com>; israr akhtar <israrakhtar@hotmail.com>

Subject: RE: 1050 Klondike Kanata - Confirmation for Extent of Services on Klondike Road.

Hi Gabrielle,

We would like to request a review of the proposed sanitary connection arrangement for the revised building footprint (row townhouses instead of apartments).

Option 1- As per the pre consultation comments, we were supposed to run a small section of sanitary sewer on Klondike and connect to the existing sanitary manhole at the Klondike/ Sandhill intersection. This arrangement would involve removal of several trees on the south west corner. A gas main will also need to be crossed and the sanitary sewer on Klondike will be a short section. This option is shown as a solid line on Drawing C101.

Option 2- To go east through the laneway on to Sandhill Rd and run a sanitary sewer on Sandhill Rd to the existing sanitary manhole at the Klondike/ Sandhill intersection. This would avoid damaging the trees and involve less conflicts with existing services. This option is shown as a dashed line on Drawing C101.

Please have a look and we can always discuss it further through email or an online meeting. It would help us to avoid any abortive work later and make a coordinated submission for the sanitary servicing.

Regards,

Yasar

416.668.6367

Yasar Ayub, P.Eng., PMP

Jain Infrastructure Consultants Ltd.

7405 East Danbro Crescent, 2nd FLoor

Mississauga, ON L5N 6P8

Tel: (905) 285-9900 X 225

Fax: (905) 567-5246

Cell:(416) 668 6367

www.jainconsultants.com

A Please consider the environment before printing this email

From: Schaeffer, Gabrielle <gabrielle.schaeffer@Ottawa.ca>

Sent: October 6, 2020 12:29 PM

To: Yasar Ayub <yayub@jainconsultants.com>

Cc: Deborah Belfie <belfied@rogers.com>; Junaid Israr <jisrar@gmail.com>; israr akhtar <jsrarakhtar@hotmail.com>

Subject: RE: 1050 Klondike Kanata - Confirmation for Extent of Services on Klondike Road.

Hi Yasar,

I have attached two screenshots of the GeoOttawa site for City staff. There is one for the public, but with limited information. You will see that the infrastructure between March and Sandhill was not constructed. The second attachment provides the exist SAN MH invert information we have on record, however it is the proponent's responsibility to verify the elevations on-site. We cannot guarantee this information is correct if there are any discrepancies found.

Hope this helps,

Gabrielle

From: Yasar Ayub < yayub@jainconsultants.com >

Sent: October 06, 2020 9:57 AM

To: Schaeffer, Gabrielle <gabrielle.schaeffer@Ottawa.ca>

Cc: Deborah Belfie <belfied@rogers.com>; Junaid Israr <jisrar@gmail.com>; israr akhtar <israrakhtar@hotmail.com>

Subject: RE: 1050 Klondike Kanata - Confirmation for Extent of Services on Klondike Road.

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Please confirm if you have received my email. We would like to request your advise so that we can proceed with the SPA design.
Yasar
416.668.6367
From: Yasar Ayub Sent: September 30, 2020 3:29 PM To: gabrielle.schaeffer@ottawa.ca Cc: Deborah Belfie <belfied@rogers.com>; Junaid Israr < israr@gmail.com>; israr akhtar < israrakhtar@hotmail.com> Subject: 1050 Klondike Kanata - Confirmation for Extent of Services on Klondike Road.</belfied@rogers.com>
Hi Gabrielle,
We would like to seek clarification on the extent of services constructed on Klondike Road west of the sandhill street intersection.
The attached the engineering plans acquired from the City; Plans 14070-19& 20 (As built drawings prepared by NovaTech in November 2013) show these services .
We would like to check the city record as we need to extend the sanitary sewer 20m west of Sandhill Street intersection.
Yasar
416.668.6367

Yasar Ayub, P.Eng., PMP

Jain Infrastructure Consultants Ltd.

7405 East Danbro Crescent, 2nd FLoor

Mississauga, ON L5N 6P8
Tel: (905) 285-9900 X 225
Fax: (905) 567-5246

www.jainconsultants.com

Cell:(416) 668 6367

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5

Appendix C Water Demand and FUS Calculations

Boundary Conditions 1050 Klondike Road

Provided Information

Scenario	Demand	
	L/min	L/s
Average Daily Demand	6	0.097
Maximum Daily Demand	55	0.92
Peak Hour	83	1.39
Fire Flow Demand #1	13,000	216.67

Location



Results

Connection 1 – Klondike Rd.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	130.0	78.3
Peak Hour	126.3	73.1
Max Day plus Fire 1	121.2	65.8

Ground Elevation = 74.9 m

Disclaimer

The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation. Fire Flow analysis is a reflection of available flow in the watermain; there may be additional restrictions that occur between the watermain and the hydrant that the model cannot take into account.

Table C1 FIRE FLOW CALCULATION as per

FIRE UNDERWRITERS SURVEY (1999)

PROJECT: 1050 Klondike Road

Ottawa, ON

Date: 19-May-21 Designer: UA Checked By: YA

1. Fire Flow Equation

F = 220 C √ A

where F is the required fire flow [LPM]

C is the coefficient determined by type of construction [unitless]

A is the total protection area [sq.m]

2. Architecture Information (To be confirmed)

Type of Construction	Combustible	
Fire Rating	Wood Frame	
Sprinkler Provided (Y/N)	N	
Total Floor Area [sq.m]	1511	3
Coefficient, C [1]	1.5	٧
Fire Flow, F [LPM]	12828	

3 - Storeys Wood Frame

3. Occupancy Reduction

Occupancy Adjustment	0.85
Fire Flow, F [LPM]	10903

- 15 % reduction for residential building

4. Sprinkler Reduction

Sprinkler Reduction	0.00	No sprinkler system
Sprinkler Reduction [LPM]	0	

5. Exposure Adjustment

North	0.05	44 m
East	0.00	75 m
South	0.00	85 m
West	0.15	13 m
Total	0.20	
Exposure Adjustment [LPM]	2181	

See attachment for off set distance

6. Required Fire Flow, Duration & Volume

Fire Flow, F [LPM]	10903	
Sprinkler Reduction [LPM]	0	
Exposure Adjustment [LPM]	2181	
Required Fire Flow [LPM]	13084	
Required Fire Flow [LPM]	13000	
Required Fire Flow [LPS]	217	
Req. Duration of Fire Flow [hrs]	2	
Req. Storage [cubic.m]	1560	

Round to nearest 1000

Yasar Ayub

From: Yasar Ayub

May 4, 2021 5:02 PM Sent: To: Armstrong, Justin Cc: **USMAN ARIF**

Subject: RE: 1050 Klondike Kanata - Boundary Conditions Request

Attachments: Drinking Water Boundary condition request - 04-05-2021.pdf; Map - off set Distance.pdf; FUS

Cal.pdf

Hi Justin,

The revised FUS calculations are attached as per the Ottawa FUS procedure. Please review and forward accordingly.

Yasar Ayub, P.Eng., PMP Jain Infrastructure Consultants Ltd. 7405 East Danbro Crescent, 2nd FLoor

Mississauga, ON L5N 6P8 Tel: (905) 285-9900 X 225 Fax: (905) 567-5246 Cell:(416) 668 6367 www.jainconsultants.com



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From: Armstrong, Justin < justin.armstrong@ottawa.ca>

Sent: May 4, 2021 1:09 PM

To: Yasar Ayub <yayub@jainconsultants.com>

Subject: FW: 1050 Klondike Kanata - Boundary Conditions Request

Hi Yasar,

As Ahmed is out of the office for the next little while, I will be helping out with this boundary request. Our boundary conditions group has flagged some concerns with the required fire flow and I am wondering if you can help clarify. Without having much knowledge about this project, the required fire flow of 3000 L/min seems rather low.

In your e-mail below you identify that the development proposal has been revised from condominium apartment buildings to freehold townhouses. In the attached FUS calculation sheet, the gross (total) floor area for the townhouse block is identified as 159 sq.m. This seems small for the gross floor area of a townhouse block. The area that should be used in the FUS method should be the gross floor area of the entire townhouse block (i.e. townhouse block footprint * number of floors).

You have used a construction class coefficient (C) of 0.8 which reflects non-combustible construction. Typically, townhouses are wood-frame which would correspond to a construction class coefficient (C) of 1.5 (typical wood frame construction) or 1.0 (a construction class of ordinary construction (1.0) can be used for wood frame construction if the exterior walls are masonry or non-combustible). Please confirm construction class for the townhouse block.

For residential buildings, an occupancy charge of -15% should be used.

For the exposure section of the attached FUS calculation sheet, please provide the offset distance of the townhouse block to the nearest structure for each of the north, east, south, and west exposures. A site plan showing the proposed location of the townhouse block on the property and its offset distance to any adjacent building is very helpful here.

Also, for your info, the City of Ottawa's Water Distribution Guidelines Technical Bulletin ISTB-2018-02 provides a very detailed description of the FUS method and how it should be followed for City of Ottawa applications.

Regards,

During this period of uncertainty surrounding COVID-19, we are following best practices recommended to minimize the risk of exposure, while ensuring that service to our clients remains as uninterrupted as possible. For the most part I am working from home and will respond to emails at my earliest opportunity. Should there be delays due to internet connectivity, I thank your understanding and patience.

Justin Armstrong, E.I.T.

Project Manager

Planning, Infrastructure and Economic Development Department - Services de la planification, de l'infrastructure et du développement économique

Development Review - West Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste 21746, justin.armstrong@ottawa.ca

From: Yasar Ayub < yayub@jainconsultants.com>

Sent: Monday, May 3, 2021 5:09 PM

To: Elsayed, Ahmed cc: USMAN ARIF <uarif@jainconsultants.com>

Subject: RE: 1050 Klondike Kanata - Boundary Conditions Request

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The development proposal was revised and freehold townhouses are being proposed instead of the condominium apartment building.

The revised water demand and FUS calculations are attached. Requesting a review of the boundary conditions provided previously .

Regards,

Yasar 416.668.6367

From: Yasar Ayub

Sent: November 6, 2020 11:54 AM

To: Elsayed, Ahmed <ahmed.elsayed@ottawa.ca>

Subject: RE: 1050 Klondike Kanata - Boundary Conditions Request

Thanks Ahmed.

From: Elsayed, Ahmed ahmed.elsayed@ottawa.ca

Sent: November 6, 2020 11:12 AM

To: Yasar Ayub <yayub@jainconsultants.com>

Subject: FW: 1050 Klondike Kanata - Boundary Conditions Request

Hi Yasar,

Attached is the BC as requested.

Thanks, Ahmed

From: Yasar Ayub < <u>yayub@jainconsultants.com</u>>

Sent: October 26, 2020 4:29 PM

To: Elsayed, Ahmed ahmed.elsayed@ottawa.ca

Cc: Schaeffer, Gabrielle < gabrielle.schaeffer@Ottawa.ca >

Subject: RE: 1050 Klondike Kanata - Boundary Conditions Request

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The revised request documents with 100% floor area taken for FUS calculations is attached.

Yasar

From: Yasar Ayub

Sent: October 26, 2020 3:53 PM

To: 'Elsayed, Ahmed' <ahmed.elsayed@ottawa.ca>

Cc: 'Schaeffer, Gabrielle' <gabrielle.schaeffer@Ottawa.ca>

Subject: RE: 1050 Klondike Kanata - Boundary Conditions Request

Hi Ahmed,

Find attached all the documents.

Yasar

416.668.6367

From: Yasar Ayub

Sent: October 26, 2020 1:28 PM

To: 'Elsayed, Ahmed' ahmed.elsayed@ottawa.ca

Cc: Schaeffer, Gabrielle <gabrielle.schaeffer@Ottawa.ca>

Subject: RE: 1050 Klondike Kanata - Boundary Conditions Request

Hi Ahmed.

I sent the following yesterday. Please have a look if it provides this info and call me on cell to discuss further.

Yasar

416.668.6367

From: Elsayed, Ahmed <ahmed.elsayed@ottawa.ca>

Sent: October 26, 2020 1:21 PM

To: Yasar Ayub <yayub@jainconsultants.com>

Cc: Schaeffer, Gabrielle <gabrielle.schaeffer@Ottawa.ca>

Subject: RE: 1050 Klondike Kanata - Boundary Conditions Request

Hi Yasar,

Please compile all the information in the same email, also please provide some description/information about the project.

- Water Boundary condition requests must include the location of the service and the expected loads required by the proposed development. Please provide the following information:
- 1. Location map with water service connection location
- Average daily demand (l/s)
- 3. Maximum daily demand (I/s)
- 4. Maximum hourly demand (I/s)
- 5. Fire flow demand (provide fire detailed flow calculations based on the fire underwriters survey method)

Regards,

Ahmed Elsayed, P. Eng.

Project Manager, Planning Services Development Review West Branch City of Ottawa | Ville d'Ottawa

Planning, Infrastructure and Economic Development Department

110 Laurier Avenue West. 4th Floor, Ottawa ON, K1P 1J1

Tel:613.580.2424 ext. 21206

Fax: 613-580-2576

Please take note that due to current COVID situation, I am working remotely and Phone communication and messaging may not be reliable at this time. Preferred method of communications will be e-mails during this period. If your preference is telephone communication, please indicate this via e-mail and provide a contact telephone number.

I apologize for any inconvenience.

^{*}Please consider your environmental responsibility before printing this e-mail

This message, including any document or file attached, is intended only for the addressee and may contain privileged and /or confidential information. Any person is strictly prohibited from reading, using, disclosing or copying this message. If you received this message in error, please notify the sender and delete the message. Thank you.

From: Yasar Ayub <yayub@jainconsultants.com>

Sent: October 26, 2020 1:13 PM

To: Elsayed, Ahmed ahmed.elsayed@ottawa.ca

Cc: Schaeffer, Gabrielle <gabrielle.schaeffer@Ottawa.ca>

Subject: RE: 1050 Klondike Kanata - Boundary Conditions Request

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The FUS calculations are attached.

Yasar

From: Elsayed, Ahmed ahmed.elsayed@ottawa.ca

Sent: October 26, 2020 1:04 PM

To: Yasar Ayub < yayub@jainconsultants.com>

Cc: Schaeffer, Gabrielle < gabrielle.schaeffer@Ottawa.ca >

Subject: FW: 1050 Klondike Kanata - Boundary Conditions Request

Hi Yasar,

Can you please provide your calculations for the fire flow demand?

After providing the information needed, it usually takes 10 business days to receive a feed back from IPU about the BC.

If you have any more questions, please let me know.

Thanks, Ahmed

From: Schaeffer, Gabrielle <gabrielle.schaeffer@Ottawa.ca>

Sent: October 26, 2020 11:33 AM

To: Elsayed, Ahmed ahmed.elsayed@ottawa.ca

Subject: FW: 1050 Klondike Kanata - Boundary Conditions Request

Hi Ahmed,

Please review and coordinate this boundary conditions request. Please let Yasar know the BC timeline.

Thanks,

Gabi

From: Yasar Ayub <yayub@jainconsultants.com>

Sent: October 26, 2020 11:12 AM

To: Schaeffer, Gabrielle <gabrielle.schaeffer@Ottawa.ca>

Cc: Deborah Belfie < belfied@rogers.com>; Junaid Israr < jisrar@gmail.com>; israr akhtar < israrakhtar@hotmail.com>

Subject: RE: 1050 Klondike Kanata - Boundary Conditions Request

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The request for water boundary conditions is attached. PI review and let us know the turnaround time for this request.

Yasar Ayub, P.Eng., PMP Jain Infrastructure Consultants Ltd.

7405 East Danbro Crescent, 2nd FLoor Mississauga, ON L5N 6P8 Tel: (905) 285-9900 X 225 Fax: (905) 567-5246 Cell:(416) 668 6367 www.jainconsultants.com

A Please consider the environment before printing this email

From: Schaeffer, Gabrielle <gabrielle.schaeffer@Ottawa.ca>

Sent: October 6, 2020 12:29 PM

To: Yasar Ayub <yayub@jainconsultants.com>

Cc: Deborah Belfie <belfied@rogers.com>; Junaid Israr <jisrar@gmail.com>; israr akhtar <israrakhtar@hotmail.com>

Subject: RE: 1050 Klondike Kanata - Confirmation for Extent of Services on Klondike Road.

Hi Yasar.

I have attached two screenshots of the GeoOttawa site for City staff. There is one for the public, but with limited information. You will see that the infrastructure between March and Sandhill was not constructed. The second attachment provides the exist SAN MH invert information we have on record, however it is the proponent's responsibility to verify the elevations on-site. We cannot guarantee this information is correct if there are any discrepancies found.

Hope this helps, Gabrielle

From: Yasar Ayub <<u>yayub@jainconsultants.com</u>>

Sent: October 06, 2020 9:57 AM

To: Schaeffer, Gabrielle <gabrielle.schaeffer@Ottawa.ca>

Cc: Deborah Belfie <belfied@rogers.com>; Junaid Israr <jisrar@gmail.com>; israr akhtar <israrakhtar@hotmail.com>

Subject: RE: 1050 Klondike Kanata - Confirmation for Extent of Services on Klondike Road.

CAUTION: This email originated from an External Sender. Please do not click links or open attachments unless you recognize the source.

ATTENTION : Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.

Please confirm if you have received my email. We would like to request your advise so that we can proceed with the SPA design.

Yasar 416.668.6367

From: Yasar Ayub

Sent: September 30, 2020 3:29 PM To: gabrielle.schaeffer@ottawa.ca

Cc: Deborah Belfie <belfied@rogers.com>; Junaid Israr <jisrar@gmail.com>; israr akhtar <israrakhtar@hotmail.com>

Subject: 1050 Klondike Kanata - Confirmation for Extent of Services on Klondike Road.

Hi Gabrielle,

We would like to seek clarification on the extent of services constructed on Klondike Road west of the sandhill street intersection.

The attached the engineering plans acquired from the City; Plans 14070-19& 20 (As built drawings prepared by NovaTech in November 2013) show these services.

We would like to check the city record as we need to extend the sanitary sewer 20m west of Sandhill Street intersection.

Yasar 416.668.6367

Yasar Ayub, P.Eng., PMP Jain Infrastructure Consultants Ltd. 7405 East Danbro Crescent, 2nd FLoor Mississauga, ON L5N 6P8 Tel. (905) 285-9900 X 225 Fax: (905) 567-5246 Cell:(416) 668 6367 www.jainconsultants.com



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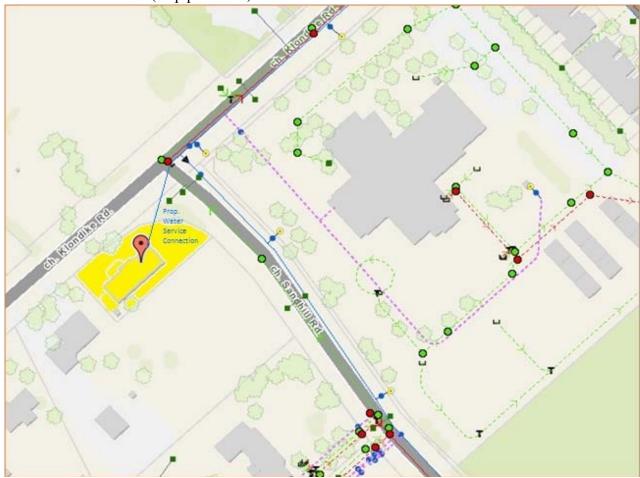
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.

Please provide the boundary conditions for the proposed water service connection for the property at 1050 Klondike Drive.

a. Location of service (map/plan view)



b. (Draft) site plan or similar plan for building location (Attached)

Design Parameter	Water Demand (L/s)
	Residential
Average Daily Demand	0.097
Maximum Daily Demand	0.92
Maximum Hourly Demand	1.39
Fire Flow	217.00
Total Max Daily Demand + Fire Flow	217.92

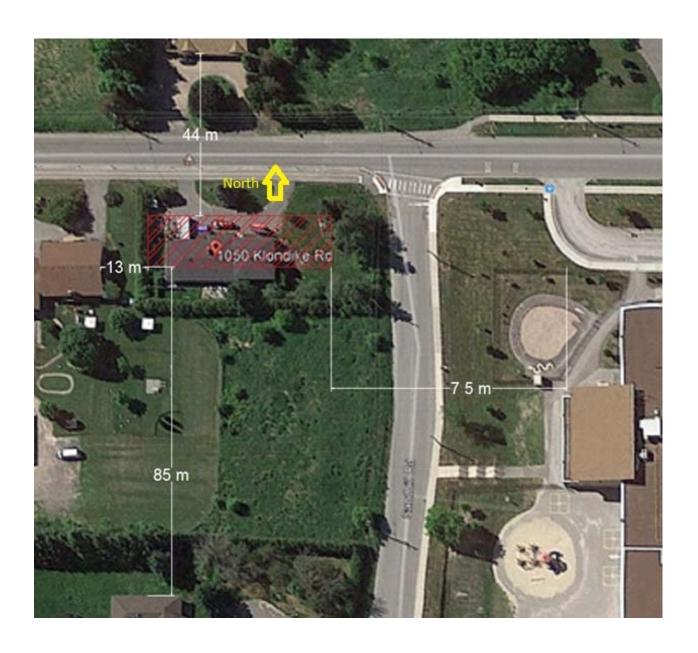
c. Supporting calculations for domestic demands

Total No. of Units = 9 units Population = $2.7 \times 9 = 24$ persons

Daily Average Water Demand = 24 x 350 l/cap/day = 84,00 L/Day (0.097 L/sec)

Maximum Daily Demand = 0.097 x 9.5 = 0.92 L/sec

Maximum Hourly Demand = 0.097 x 14.3 = 1.39 L/sec



Appendix D Sanitary Flow Calculations

1055 Klondike Road - Orr Ridge: Sanitary Sewer Design Sheet

AREA	∢					RE	RESIDENTIAL								ICI	<u> </u>				INFILT	INFILTRATION					PIPE		
			Singles	Semi-D / To	Semi-Detached / Towns					TOTAL	AL																	
Q	From Tc	To Units	ts Pop.	Units	Pop.	Future F Block 10 K	Future 1075 Klondike Rd	Pop.	A Pop.	Accum. F	Peak Pe Factor	Peak Flow In	Light Ace Industrial A Area (ha) (t	Accum. Area P (ha) Fa	Comn Peak Ar Factor (t	Commercial Instit A A (ha) (Institutional Ac Area A (ha) ((Accum. F Area F (ha)	Peak T Flow A (I/s) (Total A A Area (ha)	Accum. In Area F (ha)	Infilt. To Flow Fic (I/s) (I/	Total Size Flow (I/S) (mm)	Size Slope	ppe Length	gth Capacity	Full Flow sity Vel. (m/s)	O/Q _{full}
1055 Klondike Road Drainage Areas	Road Dr	ainage A	reas														l											
A1-1	7 5	2 0	0.0	15	40.5	0.00		0.0	40.5	40.5	3.7	0.5			0	0.00	0.00	0.00	0.0	0.64	0.64	0.2 0.	<mark>0.7</mark> 20	200 0.6	0.65 19.9	.9 27.6	3 0.85	2.5%
A1-2	5	3	0.0	29	78.3	0.00		0.0	78.3	118.8	3.6	1.4			0	0.00	0.00	0.00	0.0	0.80	1.44	0.5	1.9 20	200 0.50	100.0	0.0	2 0.75	7.7%
A1-3	3	0	0.0	14	37.8	0.00		0.0	37.8	156.6	3.5	1.8			0	0.00	0.00	0.00	0.0	0.41	1.85	0.6	2.4 20	200 0.50	50 62.3	.3 24.2	2 0.75	10.0%
A2-1, A2-2	9	0	0.0	0	0.0	53	10	128.9	128.9	128.9	3.6	1.5			0.	0.00	0.00	0.00	0.0	0.88	0.88	0.3	1.8 20	200 0.6	0.65 46.2	.2 27.6	3 0.85	6.5%
	1 26	266 0	0.0	0	0.0	0.00		0.0	0.0	285.5	3.5	3.2			0.	0.00	0.00	0.00	0.0	0.00	2.73	0.9	4.1 20	200 0.65	65 117.0	.0 27.6	3 0.85	14.9%
Off-site Drainage Areas (To Briar Ridge Pump Station)	ge Areas	s (To Bria	r Ridge Pum	p Station																								=
A3-3	266 26	265 0	0.0	22	153.9	0.00		0.0	153.9	439.4	3.4	4.8			0	0.00	0.00	0.00	0.0	2.47	5.20	1.7 6.	9	200 0.32	32 91.0	.0 19.4	1 0.60	33.9%
A3-4	265 26	264 0	0.0	0	0.0	0.00		0.0	0.0	439.4	3.4	4.8			0.	0.00	2.21 2	2.21	1.1	2.21	7.41	2.4 8.	8.4 200	0.32	32 120.0	19.4	0.60	43.2%
A3-5		206 0	0.0	107	288.9	0.00		0.0	288.9	728.3	3.3	7.8			0	0.00	0.00	2.21	1.1	3.99	11.40	3.8 12	12.6 250	50 0.24	24 306.3	30.4	1 0.60	41.6%
A3-1, A3-2, 2	206 20	205 201	1 683.4	392	1058.4	00:00		0.0	1741.8 2	2470.1	3.0	24.1			6	9.02 0	0.00	11.23	5.5 3.	37.33	48.73	16.1	45.6 450	50 0.20	20 52.5	.5 133.0	0 0.81	34.3%
A3-7, A3-8	205 20	204 0	0.0	0	0.0	0.00		0.0	0.0	2470.1	3.0	24.1	5.4	5.4	4.7 0.	0.00	0.00	11.23	15.7	5.40	54.13	17.9	57.7 450	50 0.20	20 79.7	.7 133.0	0 0.81	43.4%
- 4	204 20	203 0	0.0	0	0.0	0.00		0.0	0.0	2470.1	3.0	24.1		5.4	4.7 0.	0.00	0.00	11.23	15.7 (00.0	54.13	17.9	57.7 450	50 0.20	20 79.7	.7 133.0	0 0.81	43.4%
- 1	203 20	202 0	0.0	0	0.0	0.00		0.0	0.0	2470.1	3.0	24.1	7.9 1	13.3	3.9	0.00	0.00	11.23	26.5	7.90	62.03	20.5	71.0 450	50 0.26	26 90.0	.0 151.7	7 0.92	46.8%
. 1	202 20	201 0	0.0	0	0.0	0.00		0.0	0.0	2470.1	3.0	24.1	_	13.3	3.9 0.	0.00	0.00	11.23	26.5	0.00	62.03	20.5	71.0 450	50 0.25	25 270.0	148.7	7 0.91	47.8%
- 4	201 P:	PS 0	0.0	0	0.0	0.00		0.0	0.0	2470.1	3.0	24.1		13.3	3.9 0.	0.00	0.00	11.23	26.5	00.0	62.03	20.5	71.0 450		0.15 21.6	.6 115.2	2 0.70	61.7%
Design Parameters:	ters:										Po	Population Density:	sity:											Ą	oject: 1055	Project: 1055 Klondike Road - Orr Ridge (117034)	oad - Orr F	Ridge (117)
Avg Flow/Person =	= u	280	I/day									_	ppl/unit uni	units/ha													_	Designed: LRW
Comm./Inst. Flow =	= W	28000																										Checked: MAB
Light Industrial Flow =	= Mol_	35000							Fu	ture Block	Future Block 10 Apartment Unit	ment Unit	2.1															
Infiltration =		0.33	I/s/ha							Future 1	Future 1075 Klondike Road	like Road		35													Date: Fet	Date: February 18, 2021
Pipe Friction n =	,,	0.013										Single	3.4															
Residential Peaking Factor = Harmon Equation (max 4, min 2)	king Fact	tor = Harn	non Equation	(max 4, n	1in 2)						Se	Semi / Town	2.7															
Peaking Factor Comm./Inst. 1.5	Comm./I	Inst. 1.5																										





1050 Klondike Road - Post Development Sanitary Design Sheet

AF	AREA						RES	RESIDENTIAL	J.								ICI				INFIL	NFILTRATION					PIPE		
		ភ	Singles	Semi-Detached / Towns	stached			-	1050 Klondike Rc	Rd		TOTAL		Light Industrial	< <	Peak		Institutiona	1	Peak		Accum.	Jillit.	Total Flow Size			jt Capacity	Full	
Ω	Fro T	o Units	s Pop.		Fut Blo Units Pop. 10	ck ure	<u>\$</u>	Pop.	No. OF Units Pop. @ 2.7 Persons Pop	op. Pop.	Accum. Pop.		Peak Peak Flow Facto (Vs)		Area (ha)	Factor	al Area (ha)	l Area (ha)	(ha)	(S/I)	(ha)	Area (ha)	woi (s)	(mm) (s	(%) (r	m) u		Vel. (m/s)	(%)
1055 Klondike Road Drainage Areas	ke Road	Drainage	Areas																										
A1-1	7 5	0	0.0	15	40.5	0.00		0.0	0.0	Н	.5 40.5	3.7	0.5				00.00	0.00	0.00	0.0	0.64	0.64	0.2	0.7 200	L	19.9	27.6	0.85	2.5%
A1-2	5	U	00	66	78.3	00 0		0 0	0 0	H	3 1188	36	1.4				00 0	00 0	00.0	0.0	08.0	1 44	0.5	19 20	050 0	1000	242	0.75	L
A1-3	3 1	0	0.0	14	_	0.00		0.0	0.0	37.8		3.5	1.8				00.0	00:00	0.00	0.0	0.41	1.85	9.0	2.4 200	_	-		0.75	·
A2-1, A2-2	9	0	0.0	0	0.0	53	10 1	128.9	Ö	0.0 128.9	128.9	9.8	1.5				00.0	0.00	0.00	0.0	0.88	0.88	0.3	1.8 200	0.65	5 46.2	27.6	0.85	6.5%
	1 266	0	0.0	0	0.0	0.00		0.0	9 24	24.3 0.0	309.8	3.5	3.51				00.0	00.0	0.00	0.0	0.16	2.89	1.1	4.6 200	0.65	117.0	0 27.6	0.85	14.9%
Off-site Drainage Areas (To Briar Ridge Pump Station	inage Are	as (To B	riar Ridge	Pump St	(ation)																								
A3-3	266 265	5	0.0	22	_	0.00		0.0	0.0	_	153.9 463	7 3.4	5.1				00:0	0.00	00.00	0.0	2.47	5.36	1.8	200	0.32	91.0	19.4	0.60	33.9%
A3-4	265 264	4	0.0	0	L	0.00		0.0	0.0	L	463	7 3.4	5.1				00.00	2.21	2.21	1.1	2.21	7.57	2.5	_	_	120.	19.4	09.0	43.2%
A3-5	264 206	0 9	0.0	107	288.9	00.00		0.0	0.0	0.0 288.9	3.9 752.6	3.3	8.0				00.0	00'0	2.21	1.1	3.99	11.56	3.8	13.0 250	-	306.3	3 30.4	09'0	41.6%
A3-1, A3-2, A3-6	206 205	15 201	683.4	392	1058.4	0.00		0.0	0.0	1741.8	1.8 2494.4	.4 3.0	24.3				9.02	0.00	11.23	5.5	37.33	48.89	16.1	45.9 450	0.20	52.5	133.0	0.81	34.3%
A3-7, A3-8	205 204	4 0	0.0	0	0.0	0.00		0.0	0	0.0 0.0	2494	3.0	24.3	5.4	5.4	4.7	00.00	00.0	11.23	15.7	5.40	54.29	17.9 5	57.9 450	0.20	79.7	133.0	0.81	43.4%
	204 203	3 0	0.0	0	0.0	0.00		0.0	0.0	0.0 0.0	2494	3.0	24.3		5.4	4.7	00.00	00.00	11.23	15.7	0.00	54.29	17.9 5	57.9 450	H	79.7	133.0	0.81	43.4%
	203 202	2 0	0.0	0	0.0	0.00		0.0	0.0	0.0	2494	3.0	24.3	6.7	13.3	3.9	00.00	00.00	11.23	26.5	7.90	62.19	20.5 7	1.3 450	H	90.0	151.7	0.92	Ц
	202 201	1	0.0	0	0.0	0.00		0.0	0.0	0.0	2494.4	.4 3.0	24.3		13.3		0.00	0.00	11.23	26.5	0.00	62.19	20.5	71.3 450	0.25	270.0	148.7	0.91	47.8%
	201 PS	0	0.0	0	0.0	00.00		0.0	0	0.0 0.0	2494.4	.4 3.0	24.3		13.3	3.9	00.0	00:00	11.23	26.5	0.00	62.19	20.5 71.3	1.3 450	0.15	21.6	115.2	0.70	61.7%
Design Parameters:	ters:											١	Population Density:	nsity:	units/ha													roject: 105(Project: 1050 Klondike Roac
Avg Flow/Person = 280 l/day Comm/Inst. Flow = 28000 l/ha/day Light	n = 280 l/da	ty Comm./	nst. Flow = 2a	8000 l/ha/da;	y Light									ypl/unit														Designed:	Designed: UA Checked: YA
Industrial Flow = 35000 l/ha/day Infiltration = 0.33 l/s/ha	: 35000 l/ha/du	tay Infiltrat	ion = 0.33 l/s.	/ha							Future B	Future Block 10 Apartment Unit		2.1														ă	Date: May 20,2027
Pipe Friction n = 0.013	0.013										Futu	Future 1075 Klondike Road		8.	32														
Residential Peaking Factor = Harmon Equation (max 4, min 2) Peaking	king Factor =	Harmon Eq	uation (max 4,	, min 2) Peak	guis							ď		4. 6															
ractor comm./inst. 1.5	S											0		7.7															
																											Jain	nfrastructure	Jain Infrastructure Consultants Ltd
	Shaded Cell	'Is show rev	Shaded Cells show revised numbers as per 1050 Klondike Rd Flows	s as per 105	O Klondike R.	d Flows																							

Appendix E
Storm Sewer Design Calculations
SWM Catchments for Brookside Subdivision & Pond "C"
Stormceptor Sizing Calculations
Flow Control Roof Drain Specs

TABLE E1. Land use Breakdown and Composite Runoff Coefficients Calculations Existing Conditions

Project: 1050 Klondike Drive, Ottawa, ON **Date:** 20-May-21

By: YA

TABLE E1.1 EXISTING LAND USE COVER AND RUNOFF COEFFICIENTS

Existing	A, Area	R, Runoff	AxR
Land Use Cover	(hectares)	Coefficient	
Bldg/ Roof	0.0240	0.90	0.02
Concrete	0.011	0.90	0.01
Gravel	0.017	0.80	0.013
Landscape	0.077	0.25	0.02
Overall	0.128	0.50	0.06

TABLE E1.2 AREA A1

Proposed	A, Area	R, Runoff	AxR
Land Use/ Cover	(hectares)	Coefficient	
Bldg/ Roof	0.013	0.90	0.01
Concrete	0.008	0.90	0.01
Landscape	0.055	0.25	0.01
Overall	0.076	0.43	0.033

TABLE E1.3 AREA A2

Proposed	A, Area	R, Runoff	AxR
Land Use/ Cover	(hectares)	Coefficient	
Bldg/ Roof	0.011	0.90	0.010
Concrete	0.003	0.90	0.003
Gravel	0.017	0.80	0.013
Landscape	0.022	0.25	0.005
Overall	0.052	0.60	0.031

TABLE E1.4 AREA A3

Proposed	A, Area	R, Runoff	AxR
Land Use/ Cover	(hectares)	Coefficient	
Building	0.001	0.90	0.00
Gravel	0.009	0.80	0.01
Landscape	0.019	0.25	0.00
Overall	0.029	0.44	0.013

Note: As per pre consultation commnets, Pre development runoff coefficient "R" is recommended as a maximum equivalent of "0.5". However as per Brookside Subdivision Storm Drainage Area Plan, R is considered as "0.45" and same has been adopted for current design

^{*} Catchment Area "A3 =0.029" is Excluded from SWM calculations as it is uncontrolled in pre and post development

TABLE E2. Land use Breakdown and Composite Runoff Coefficients Calculations Proposed Conditions

Project: 1050 Klondike Drive, Ottawa, ON Date: 20-May-21

By: YA

TABLE E2.1 PROPOSED LAND USE COVER AND RUNOFF COEFFICIENTS

Proposed	A, Area	R, Runoff	AxR
Land Use/ Cover	(hectares)	Coefficient	
Bldg/ Roof	0.052	0.90	0.047
Concrete/Asphalt	0.053	0.90	0.048
Landscape	0.023	0.25	0.006
Overall	0.128	0.78	0.100

TABLE E2.2 AREA A1

Proposed	A, Area	R, Runoff	AxR
Land Use/ Cover	(hectares)	Coefficient	
Asphalt	0.041	0.90	0.037
Concrete	0.012	0.90	0.011
Landscape	0.023	0.25	0.006
Overall	0.076	0.70	0.053

TABLE E2.3 AREA A2

Proposed Land Use/ Cover	A, Area (hectares)	R, Runoff Coefficient	AxR
Bldg/ Roof	0.052	0.90	0.047
Overall	0.052	0.90	0.047

TABLE E2.4 AREA A3

Proposed	A, Area	R, Runoff	AxR
Land Use/ Cover	(hectares)	Coefficient	
Concrete	0.011	0.90	0.010
Landscape	0.018	0.25	0.005
Overall	0.029	0.49	0.014

 $^{^{*}}$ Catchment Area "A3 =0.029" is Excluded from SWM calculations as it is uncontrolled in pre and post development

TABLE E3 PEAK FLOWS CALCULATION USING RATIONAL METHOD **EXISTING AND PROPOSED CONDITIONS**

Project: 1050 Klondike Drive, Ottawa, ON Date: 20-May-21

By: YA

TABLE E3.1 Intensity-Duration-Frequency Parameters, Ottawa

 $I=A/(td+C)^B$ 10 min

Return Period	Α	В	С
2 year	732.951	0.810	6.199
5 year	998.071	0.814	6.053
10 year	1174.184	0.816	6.014
25 year	1402.884	0.819	6.018
50 year	1569.580	0.820	6.014
100 year	1735.688	0.820	6.041

TABLE E3	3.2 Peak Flows	s - Existing Co	ondition for Ad	Idition Areas	;		
E	Existing Condi	tion	Area (ha.)	R	AxR		
			0.076	0.45	0.03	Area A1	As per pre consultation comments,pre development runoff coefficient "R" is recommended as "0.5" max. As per Brookside Subdivision Storm Drainage Area
			0.052	0.45	0.02	Area A2	Plan, "R" is considered as "0.45". Quantity control of 85 l/sec/ha has been used for actual orifice sizing.
		T c = 10	minutes				
		Storm	Event				
2 year	5 year	10 year	25 year	50 year	100 year		
Intensity (mm/hr)						Ī	
76.8	104.2	122.1	144.7	161.5	178.3		
		Peak Flo	w (cms)				
0.007	0.010	0.012	0.014	0.015	0.017	Area A1	
0.005	0.007	0.008	0.009	0.011	0.012	Area A2	
0.012	0.017	0.020	0.023	0.026	0.029	Total	

TABLE E3.3 Peak Flows - Proposed Condition

В	roposed Cond	lition	Area (ha.)	R	AxR	
Г	roposeu conc	illion	0.076	0.70	0.05	Area A1
			0.052	0.90	0.05	Area A2 - Bldg/ Roof
		T c = 10	minutes			
		Storm	Event			
2 year	5 year	10 year	25 year	50 year	100 year	
		Intensity	(mm/hr)			
76.8	104.2	122.1	144.7	161.5	178.3	
	Pe	ak Flow (cms) - Uncontrolle	d		
0.011	0.015	0.018	0.021	0.024	0.026	A1
0.010	0.014	0.016	0.019	0.021	0.023	A2- Bldg/ Roof
0.021	0.029	0.034	0.040	0.045	0.050	Total
	F	Peak Flow (cm	s) - Controlled			
0.0400	0.0400	0.0400	0.0400	0.0400	0.0400	Allowable @ Release rate 85 L/s/ha (0.85X0.128) -
0.0102	0.0102	0.0102	0.0102	0.0102	0.0102	Orifice Control

TABLE E3.4 Change in Peak Flows (Reduction -ve; Increase +ve)

					,
		Percent CI	hange (%)		
-17.0%	-38.8%	-47.8%	-56.0%	-60.5%	-64.3%

On-Site Storage Calculator

Table E4 -Overall Site

Ottawa, ON

Project: 1050 Klondike Drive

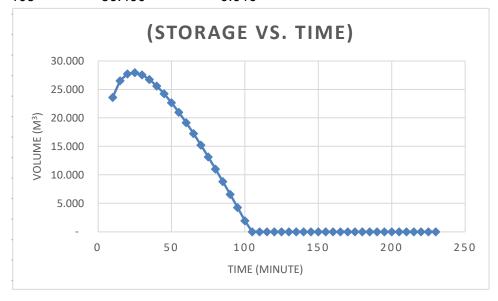
By: UA

Date: 20-May-21

R =	0.78
A =	0.128 ha
Q _{release} =	$0.010 \text{ m}^3/\text{s}$
	10 21 1/s

T.C	i ₁₀₀	Q ₁₀₀	Q _{stored}	Peak Volume	
(min)	(mm/hr)	(m³/s)	(m ³ /s)	(m ³)	
10	178.313	0.050	0.039	23.619	
15	142.744	0.040	0.029	26.529	
20	119.848	0.033	0.023	27.733	
25	103.773	0.029	0.019	27.962	***
30	91.812	0.026	0.015	27.569	
35	82.534	0.023	0.013	26.747	
40	75.109	0.021	0.011	25.614	
45	69.020	0.019	0.009	24.245	
50	63.929	0.018	0.008	22.692	
55	59.602	0.017	0.006	20.991	
60	55.876	0.016	0.005	19.170	
65	52.630	0.015	0.004	17.248	
70	49.775	0.014	0.004	15.241	
75	47.243	0.013	0.003	13.161	
80	44.979	0.013	0.002	11.018	
85	42.943	0.012	0.002	8.820	
90	41.101	0.011	0.001	6.573	
95	39.426	0.011	0.001	4.283	
100	37.895	0.011	0.000	1.955	
105	36.490	0.010	-	-	

100 yr rainfall:



On-Site Storage Calculator

Ottawa, ON Table E5 -Roof Project: 1050 Klondike Drive

By: UA

Date: 20-May-21

R =	0.90
<i>A</i> =	0.052 ha
Q release =	$0.009 \text{ m}^3/\text{s}$
	9.00 1/s

T.C	i ₁₀₀	Q ₁₀₀	Q _{stored}	Peak Volume	
(min)	(mm/hr)	(m ³ /s)	(m³/s)	(m ³)	
10	178.313	0.023	0.014	8.508	
15	142.744	0.019	0.010	8.601	***
20	119.848	0.016	0.007	7.896	
25	103.773	0.013	0.004	6.736	
30	91.812	0.012	0.003	5.284	
35	82.534	0.011	0.002	3.632	
40	75.109	0.010	0.001	1.834	
45	69.020	0.009	-	-	
50	63.929	0.008	-	-	
55	59.602	0.008	-	-	
60	55.876	0.007	-	-	
65	52.630	0.007	-	-	
70	49.775	0.006	-	-	
75	47.243	0.006	_	-	
80	44.979	0.006	-	-	
85	42.943	0.006	-	-	
90	41.101	0.005	_	-	
95	39.426	0.005	_	-	
100	37.895	0.005	_	-	
105	36.490	0.005	_	-	

100 yr rainfall:

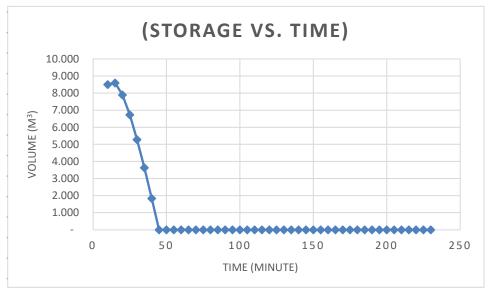


TABLE E6 ORIFICE SIZING CALCULATIONS

Project: 1050 Klondike Drive, Ottawa, ON Date: 20-May-21

 Date:
 May 20, 2021
 Designer: UA

 Checked By: YA
 Checked By: YA

Location	HWL	Orifice Inv.	С	а	g	Orifice dia.	h		Q
	(m)	(m)		(m²)		(m)	(m)	(I/sec)	(m³/sec)
STM MH2	75.35	73.80	0.62	0.003	9.81	0.062	1.52	10.21	0.01021

Proposed 62 mm Dia. Orifice plate with rated capacity 10.21 lit/sec

Table E7 - Storm Drainage Design Chart

	MA	MANHOLES	4	O		ACC.			a	a	STO	RM SEWE	R DESIGN	STORM SEWER DESIGN INFORMATION	TION	TIME	
LOCATION	FROM MH#	TO TW	area (ha)	runoff Coeffi.	A×C	A×C	(min)	I (mm/hr)	(5-YR) (I/s)	(@85 Vsec/ha) (Vs)	size (mm)	slope (%)	length (m)	Q full (Vs)	V full	SECT. (min)	REMARKS
Buliding	Plug	STM MH1	0.02	67.0	0.01	0.01	10.00	104.19	4	1.7	300	2.00	00.9	137	1.93	0.05	
Parking	STM MH1	STM MH2	0.11	0.73	0.08	0.09	10.05	104.66	27	10.9	300	2.00	51.00	137	1.93	0.44	
Parking	STM MH2	STM MH3	00.00	0.73	0.00	60.0	10.49	102.57	27	10.9	300	2.00	3.00	137	1.93	0.03	
Parking	STM MH3	EX. STM Sewer Dia 675mm Line (Sandhill Boad)	00:00	62.0	0.00	0.09	10.52	102.45	27	10.9	300	2.00	10.00	137	1.93	60:0	Orifice Control

DESIGN STORM: I (5-YEAR): td (start):		5 YEAR RETURN = A / (td +C) ^B (mm/hr) 10.0 minutes				-	able E7 - Storm Drainage Design Chart	orm Drainage	Design Cha	턴				Jain Infrastructure PROJECT: PREPARED BY: FILE No.: DATE PREPARED	S O	Jain Infrastructure Consultants Ltd. PROJECT: 1050 Klondike Drive PREPARED BY: UA FILE No.: 20-525 DATE PREPARED 20-May-21	Drive
	M	MANHOLES	٧	ပ		ACC.			Ø	ø	STO	RM SEWE	R DESIGN	STORM SEWER DESIGN INFORMATION	NOI	TIME	
LOCATION	FROM MH#	TO MF#	area (ha)	runoff Coeffi.	A×C	A×C	ta (min)	I (mm/hr)	(5-YR) (Vs)	(@85 Vsec/ha) (Vs)	size (mm)	slope (%)	length (m)	Q full (Vs)	V full (m/s)	SECT. (min)	REMARKS
Buliding	Plug	STM MH1	0.02	0.73	0.01	0.01	10.00	104.19	4	1.7	300	2.00	00.9	137	1.93	0.05	
Parking	STM MH1	STM MH2	0.11	0.73	0.08	0.09	10.05	104.66	27	10.9	300	2.00	51.00	137	1.93	0.44	
Parking	STM MH2	STM MH3	0.00	0.73	0.00	60.0	10.49	102.57	22	10.9	300	2.00	3.00	137	1.93	0.03	
Parking	STM MH3	EX. STM Sewer Dia 675mm Line (Sandhill	0.00	0.73	0.00	60:0	10.52	102.45	27	10.9	300	2.00	10.00	137	1.93	60.0	Orifice Control

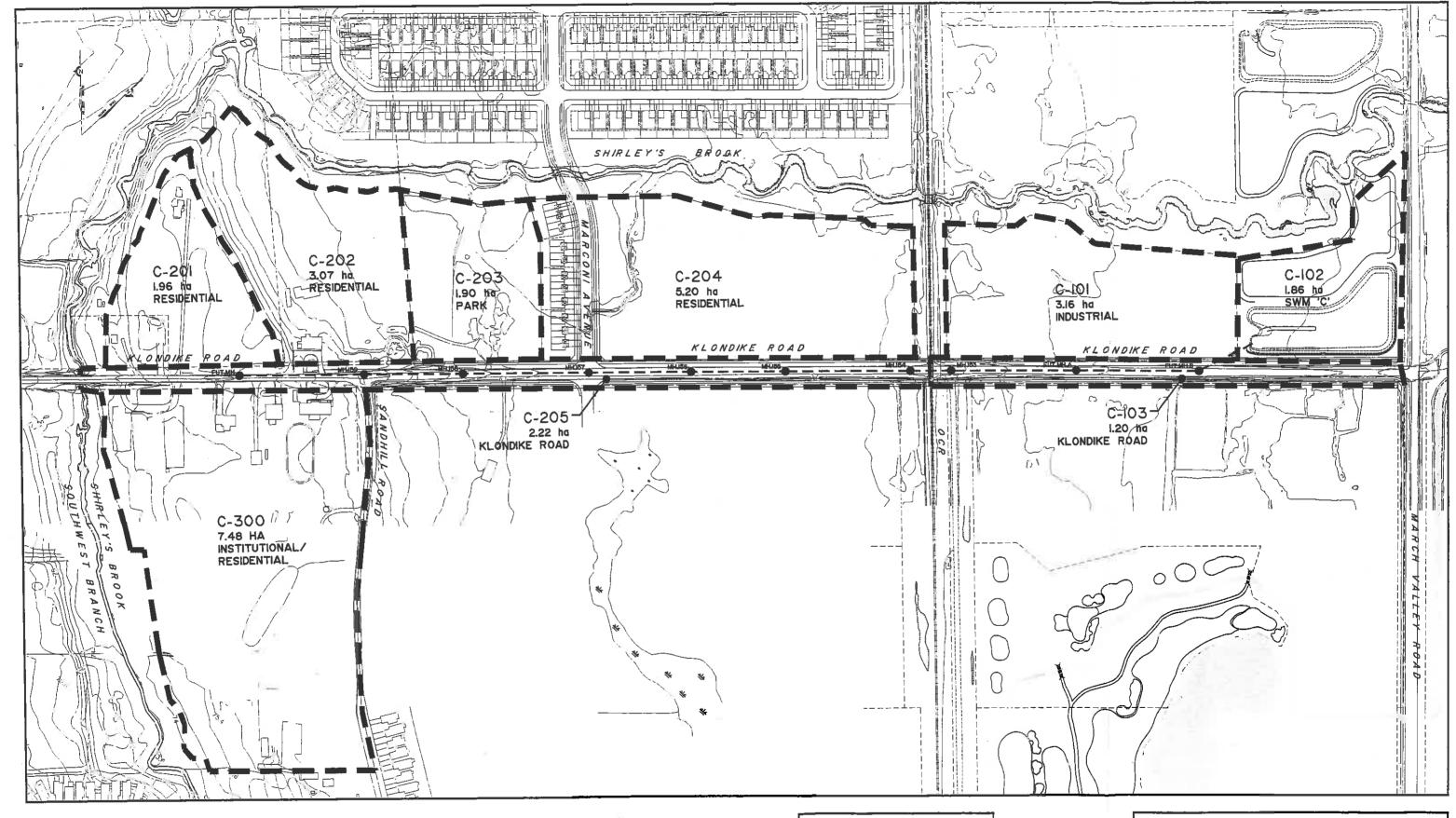
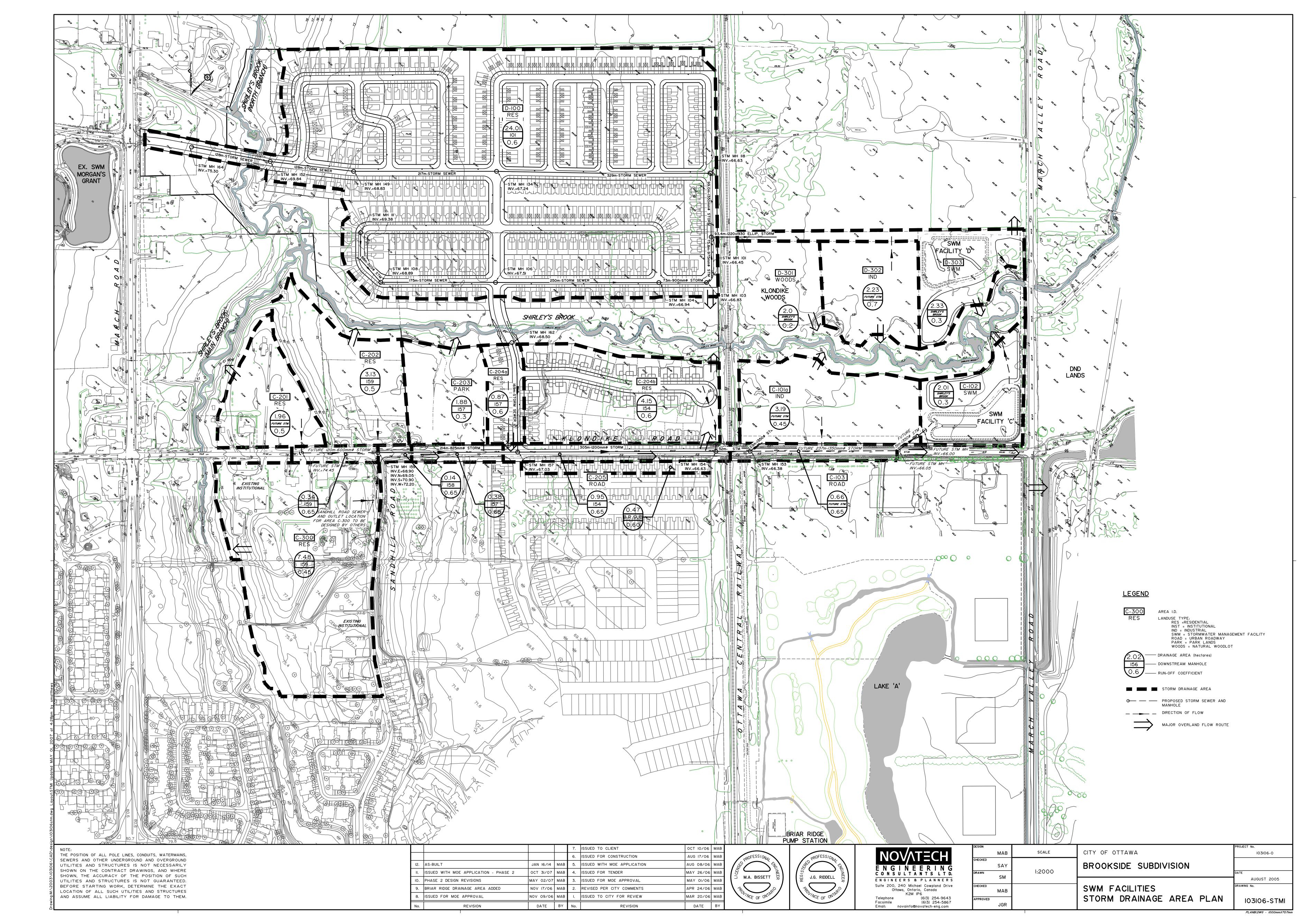




FIGURE 3
STORM DRAINAGE AREAS
TO SWM FACILITY 'C'
103106 MAY 2006 N.T.S.





Drainage Area (ha):
Runoff Coefficient 'c':



Stormceptor EF Sizing Report

STORMCEPTOR® ESTIMATED NET ANNUAL SEDIMENT (TSS) LOAD REDUCTION

05/11/2021

Province:	Ontario
City:	OTTAWA
Nearest Rainfall Station:	OTTAWA MACDONALD-CARTIER INT'L AP
NCDC Rainfall Station Id:	6000
Years of Rainfall Data:	37
Site Name:	

Project Name:	1050 KLONDIKE DRIVE
Project Number:	45336
Designer Name:	Usman Arif
Designer Company:	JIC
Designer Email:	cad1@jainconsultants.com
Designer Phone:	647-510-0353
EOR Name:	
EOR Company:	
EOR Email:	
EOR Phone:	

Particle Size Distribution: Fine

Target TSS Removal (%): 80.0

0.13

0.78

Required Water Quality Runoff Volume Capture (%):	90.00
Estimated Water Quality Flow Rate (L/s):	3.66
Oil / Fuel Spill Risk Site?	No
Upstream Flow Control?	Yes
Upstream Orifice Control Flow Rate to Stormceptor (L/s):	10.90
Peak Conveyance (maximum) Flow Rate (L/s):	
Site Sediment Transport Rate (kg/ha/yr):	

Net Annual Sediment (TSS) Load Reduction Sizing Summary						
Stormceptor	TSS Removal					
Model	Provided (%)					
EF4	90					
EF6	92					
EF8	93					
EF10	93					
EF12	93					
Model EF4 EF6 EF8 EF10	90 92 93 93					

Recommended Stormceptor EF Model: EF4

Estimated Net Annual Sediment (TSS) Load Reduction (%):

Water Quality Runoff Volume Capture (%):

90 > 90





THIRD-PARTY TESTING AND VERIFICATION

► Stormceptor® EF and Stormceptor® EFO are the latest evolutions in the Stormceptor® oil-grit separator (OGS) technology series, and are designed to remove a wide variety of pollutants from stormwater and snowmelt runoff. These technologies have been third-party tested in accordance with the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators and performance has been third-party verified in accordance with the ISO 14034 Environmental Technology Verification (ETV) protocol.

PERFORMANCE

▶ Stormceptor® EF and EFO remove stormwater pollutants through gravity separation and floatation, and feature a patent-pending design that generates positive removal of total suspended solids (TSS) throughout each storm event, including high-intensity storms. Captured pollutants include sediment, free oils, and sediment-bound pollutants such as nutrients, heavy metals, and petroleum hydrocarbons. Stormceptor is sized to remove a high level of TSS from the frequent rainfall events that contribute the vast majority of annual runoff volume and pollutant load. The technology incorporates an internal bypass to convey excessive stormwater flows from high-intensity storms through the device without resuspension and washout (scour) of previously captured pollutants. Proper routine maintenance ensures high pollutant removal performance and protection of downstream waterways.

PARTICLE SIZE DISTRIBUTION (PSD)

► The Canadian ETV PSD shown in the table below was used, or in part, for this sizing. This is the identical PSD that is referenced in the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators for both sediment removal testing and scour testing. The Canadian ETV PSD contains a wide range of particle sizes in the sand and silt fractions, and is considered reasonably representative of the particle size fractions found in typical urban stormwater runoff.

Particle	Percent Less	Particle Size	Dawsont
Size (µm)	Than	Fraction (µm)	Percent
1000	100	500-1000	5
500	95	250-500	5
250	90	150-250	15
150	75	100-150	15
100	60	75-100	10
75	50	50-75	5
50	45	20-50	10
20	35	8-20	15
8	20	5-8	10
5	10	2-5	5
2	5	<2	5





Upstream Flow Controlled Results

Rainfall Intensity (mm / hr)	Percent Rainfall Volume (%)	Cumulative Rainfall Volume (%)	Flow Rate (L/s)	Flow Rate (L/min)	Surface Loading Rate (L/min/m²)	Removal Efficiency (%)	Incremental Removal (%)	Cumulative Removal (%)
1	51.3	51.3	0.28	17.0	14.0	93	47.7	47.7
2	8.7	60.0	0.56	34.0	28.0	93	8.1	55.8
3	5.8	65.8	0.85	51.0	42.0	93	5.4	61.2
4	4.6	70.4	1.13	68.0	56.0	92	4.2	65.4
5	4.2	74.6	1.41	85.0	70.0	90	3.8	69.2
6	3.2	77.8	1.69	101.0	85.0	89	2.8	72.1
7	2.6	80.4	1.97	118.0	99.0	88	2.3	74.3
8	2.4	82.8	2.26	135.0	113.0	86	2.1	76.4
9	1.9	84.7	2.54	152.0	127.0	85	1.6	78.0
10	1.6	86.3	2.82	169.0	141.0	83	1.3	79.3
11	1.3	87.6	3.10	186.0	155.0	81	1.1	80.4
12	1.1	88.7	3.38	203.0	169.0	79	0.9	81.3
13	1.3	90.0	3.66	220.0	183.0	78	1.0	82.3
14	1.1	91.1	3.95	237.0	197.0	77	0.8	83.1
15	0.6	91.7	4.23	254.0	211.0	75	0.5	83.6
16	0.8	92.5	4.51	271.0	226.0	74	0.6	84.2
17	0.7	93.2	4.79	288.0	240.0	72	0.5	84.7
18	0.5	93.7	5.07	304.0	254.0	72	0.4	85.0
19	0.6	94.3	5.36	321.0	268.0	71	0.4	85.5
20	0.5	94.8	5.64	338.0	282.0	69	0.3	85.8
21	0.2	95.0	5.92	355.0	296.0	68	0.1	85.9
22	0.4	95.4	6.20	372.0	310.0	66	0.3	86.2
23	0.5	95.9	6.48	389.0	324.0	65	0.3	86.5
24	0.4	96.3	6.77	406.0	338.0	64	0.3	86.8
25	3.7	100.0	7.05	423.0	352.0	63	2.3	89.1

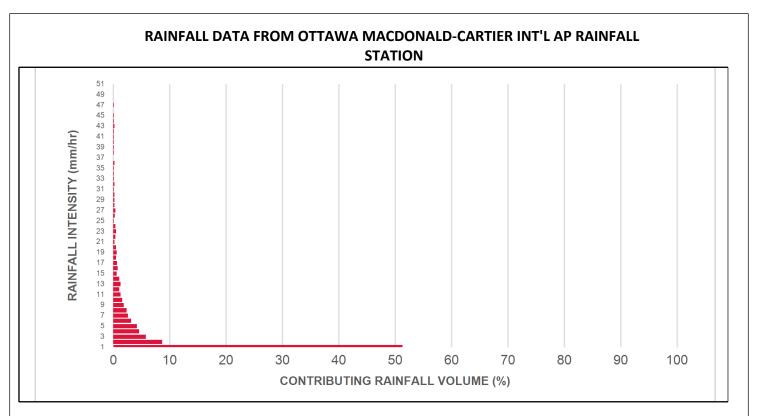




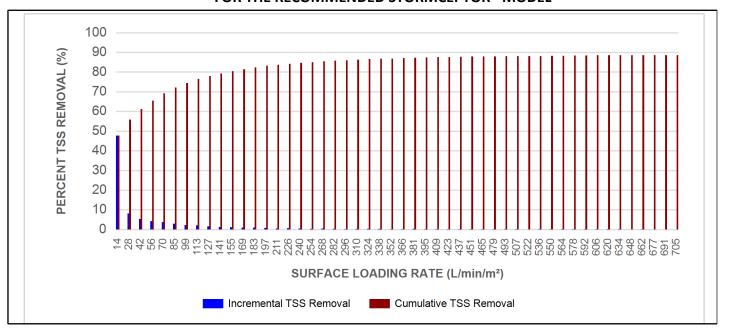
Rainfall Intensity (mm / hr)	Percent Rainfall Volume (%)	Cumulative Rainfall Volume (%)	Flow Rate (L/s)	Flow Rate (L/min)	Surface Loading Rate (L/min/m²)	Removal Efficiency (%)	Incremental Removal (%)	Cumulative Removal (%)
26	0.3	100.3	7.33	440.0	366.0	62	0.2	89.3
27	0.4	100.7	7.61	457.0	381.0	60	0.2	89.5
28	0.2	100.9	7.89	474.0	395.0	59	0.1	89.6
29	0.2	101.1	8.17	490.0	409.0	58	0.1	89.8
30	0.2	101.3	8.46	507.0	423.0	58	0.1	89.9
31	-1.3	100.0	8.74	524.0	437.0	58	N/A	89.1
32	0.2	100.2	9.02	541.0	451.0	58	0.1	89.2
33	-0.2	100.0	9.30	558.0	465.0	57	N/A	89.1
34	0.0	100.0	9.58	575.0	479.0	57	0.0	89.1
35	0.0	100.0	9.87	592.0	493.0	57	0.0	89.1
36	0.2	100.2	10.15	609.0	507.0	57	0.1	89.2
37	0.0	100.2	10.43	626.0	522.0	57	0.0	89.2
38	-0.2	100.0	10.71	643.0	536.0	57	N/A	89.1
39	0.0	100.0	10.99	660.0	550.0	57	0.0	89.1
40	0.0	100.0	11.00	660.0	550.0	57	0.0	89.1
41	0.0	100.0	11.00	660.0	550.0	57	0.0	89.1
42	0.0	100.0	11.00	660.0	550.0	57	0.0	89.1
43	0.0	100.0	11.00	660.0	550.0	57	0.0	89.1
44	0.0	100.0	11.00	660.0	550.0	57	0.0	89.1
45	0.0	100.0	11.00	660.0	550.0	57	0.0	89.1
46	0.0	100.0	11.00	660.0	550.0	57	0.0	89.1
47	0.0	100.0	11.00	660.0	550.0	57	0.0	89.1
48	0.0	100.0	11.00	660.0	550.0	57	0.0	89.1
49	0.0	100.0	11.00	660.0	550.0	57	0.0	89.1
50	0.0	100.0	11.00	660.0	550.0	57	0.0	89.1
Estimated Net Annual Sediment (TSS) Load Reduction =								







INCREMENTAL AND CUMULATIVE TSS REMOVAL FOR THE RECOMMENDED STORMCEPTOR® MODEL









Maximum Pipe Diameter / Peak Conveyance

Stormceptor EF / EFO	Model Diameter		Min Angle Inlet / Outlet Pipes	Max Inle Diame	•	Max Outl	•		nveyance Rate
	(m)	(ft)		(mm)	(in)	(mm)	(in)	(L/s)	(cfs)
EF4 / EFO4	1.2	4	90	609	24	609	24	425	15
EF6 / EFO6	1.8	6	90	914	36	914	36	990	35
EF8 / EFO8	2.4	8	90	1219	48	1219	48	1700	60
EF10 / EFO10	3.0	10	90	1828	72	1828	72	2830	100
EF12 / EFO12	3.6	12	90	1828	72	1828	72	2830	100

SCOUR PREVENTION AND ONLINE CONFIGURATION

► Stormceptor® EF and EFO feature an internal bypass and superior scour prevention technology that have been demonstrated in third-party testing according to the scour testing provisions of the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators, and the exceptional scour test performance has been third-party verified in accordance with the ISO 14034 ETV protocol. As a result, Stormceptor EF and EFO are approved for online installation, eliminating the need for costly additional bypass structures, piping, and installation expense.

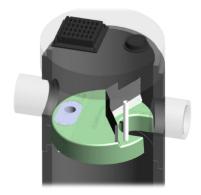
DESIGN FLEXIBILITY

► Stormceptor® EF and EFO offers design flexibility in one simplified platform, accepting stormwater flow from a single inlet pipe or multiple inlet pipes, and/or surface runoff through an inlet grate. The device can also serve as a junction structure, accommodate a 90-degree inlet-to-outlet bend angle, and can be modified to ensure performance in submerged conditions.

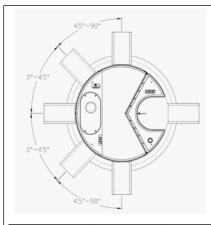
OIL CAPTURE AND RETENTION

▶ While Stormceptor® EF will capture and retain oil from dry weather spills and low intensity runoff, **Stormceptor® EFO** has demonstrated superior oil capture and greater than 99% oil retention in third-party testing according to the light liquid reentrainment testing provisions of the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators**. Stormceptor EFO is recommended for sites where oil capture and retention is a requirement.









INLET-TO-OUTLET DROP

Elevation differential between inlet and outlet pipe inverts is dictated by the angle at which the inlet pipe(s) enters the unit.

 0° - 45° : The inlet pipe is 1-inch (25mm) higher than the outlet pipe.

45° - 90°: The inlet pipe is 2-inches (50mm) higher than the outlet pipe.

HEAD LOSS

The head loss through Stormceptor EF is similar to that of a 60-degree bend structure. The applicable K value for calculating minor losses through the unit is 1.1. For submerged conditions the applicable K value is 3.0.

Pollutant Capacity

Stormceptor EF / EFO	Mod Diam	_	Depth (Pipe In Sump	vert to	Oil Vo		Recommended Sediment Maintenance Depth *		Sediment Sediment Volume		Sediment Mass **	
	(m)	(ft)	(m)	(ft)	(L)	(Gal)	(mm)	(in)	(L)	(ft³)	(kg)	(lb)
EF4 / EFO4	1.2	4	1.52	5.0	265	70	203	8	1190	42	1904	5250
EF6 / EFO6	1.8	6	1.93	6.3	610	160	305	12	3470	123	5552	15375
EF8 / EFO8	2.4	8	2.59	8.5	1070	280	610	24	8780	310	14048	38750
EF10 / EFO10	3.0	10	3.25	10.7	1670	440	610	24	17790	628	28464	78500
EF12 / EFO12	3.6	12	3.89	12.8	2475	655	610	24	31220	1103	49952	137875

^{*}Increased sump depth may be added to increase sediment storage capacity

^{**} Average density of wet packed sediment in sump = 1.6 kg/L (100 lb/ft³)

Feature	Benefit	Feature Appeals To
Patent-pending enhanced flow treatment and scour prevention technology	Superior, verified third-party performance	Regulator, Specifying & Design Engineer
Third-party verified light liquid capture	Proven performance for fuel/oil hotspot	Regulator, Specifying & Design Engineer,
and retention for EFO version	locations	Site Owner
Functions as bend, junction or inlet structure	Design flexibility	Specifying & Design Engineer
Minimal drop between inlet and outlet	Site installation ease	Contractor
Large diameter outlet riser for inspection and maintenance	Easy maintenance access from grade	Maintenance Contractor & Site Owner

STANDARD STORMCEPTOR EF/EFO DRAWINGS

For standard details, please visit http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef

STANDARD STORMCEPTOR EF/EFO SPECIFICATION

For specifications, please visit http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef









STANDARD PERFORMANCE SPECIFICATION FOR "OIL GRIT SEPARATOR" (OGS) STORMWATER QUALITY TREATMENT DEVICE

PART 1 – GENERAL

1.1 WORK INCLUDED

This section specifies requirements for selecting, sizing, and designing an underground Oil Grit Separator (OGS) device for stormwater quality treatment, with third-party testing results and a Statement of Verification in accordance with ISO 14034 Environmental Management – Environmental Technology Verification (ETV).

1.2 REFERENCE STANDARDS & PROCEDURES

ISO 14034:2016 Environmental management – Environmental technology verification (ETV)

Canadian Environmental Technology Verification (ETV) Program's **Procedure for Laboratory Testing of Oil-Grit Separators.**

1.3 SUBMITTALS

- 1.3.1 All submittals, including sizing reports & shop drawings, shall be submitted upon request with each order to the contractor then forwarded to the Engineer of Record for review and acceptance. Shop drawings shall detail all OGS components, elevations, and sequence of construction.
- 1.3.2 Alternative devices shall have features identical to or greater than the specified device, including: treatment chamber diameter, treatment chamber wet volume, sediment storage volume, and oil storage volume.
- 1.3.3 Unless directed otherwise by the Engineer of Record, OGS stormwater quality treatment product substitutions or alternatives submitted within ten days prior to project bid shall not be accepted. All alternatives or substitutions submitted shall be signed and sealed by a local registered Professional Engineer, based on the exact same criteria detailed in Section 3, in entirety, subject to review and approval by the Engineer of Record.

PART 2 - PRODUCTS

2.1 OGS POLLUTANT STORAGE

The OGS device shall include a sump for sediment storage, and a protected volume for the capture and storage of petroleum hydrocarbons and buoyant gross pollutants. The **minimum** sediment & petroleum hydrocarbon storage capacity shall be as follows:

2.1.1 4 ft (1219 mm) Diameter OGS Units: 1.19 m³ sediment / 265 L oil 6 ft (1829 mm) Diameter OGS Units: 3.48 m³ sediment / 609 L oil 8 ft (2438 mm) Diameter OGS Units: 8.78 m³ sediment / 1,071 L oil 10 ft (3048 mm) Diameter OGS Units: 17.78 m³ sediment / 1,673 L oil 12 ft (3657 mm) Diameter OGS Units: 31.23 m³ sediment / 2,476 L oil

PART 3 - PERFORMANCE & DESIGN

3.1 GENERAL







The OGS stormwater quality treatment device shall be verified in accordance with ISO 14034:2016 Environmental management – Environmental technology verification (ETV). The OGS stormwater quality treatment device shall remove oil, sediment and gross pollutants from stormwater runoff during frequent wet weather events, and retain these pollutants during less frequent high flow wet weather events below the insert within the OGS for later removal during maintenance. The Manufacturer shall have at least ten (10) years of local experience, history and success in engineering design, manufacturing and production and supply of OGS stormwater quality treatment device systems, acceptable to the Engineer of Record.

3.2 SIZING METHODOLOGY

The OGS device shall be engineered, designed and sized to provide stormwater quality treatment based on treating a minimum of 90 percent of the average annual runoff volume and a minimum removal of an annual average 60% of the sediment (TSS) load based on the Particle Size Distribution (PSD) specified in the sizing report for the specified device. Sizing shall be determined using historical rainfall data and a sediment removal performance curve derived from the actual third-party verified laboratory testing data. The OGS device shall also have sufficient annual sediment storage capacity as specified and calculated in Section 2.1.

3.3 CANADIAN ETV or ISO 14034 ETV VERIFICATION OF SCOUR TESTING

The OGS device shall have Canadian ETV or ISO 14034 ETV Verification of third-party scour testing conducted in accordance with the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators**.

3.3.1 To be acceptable for on-line installation, the OGS device must demonstrate an average scour test effluent concentration less than 10 mg/L at each surface loading rate tested, up to and including 2600 L/min/m².



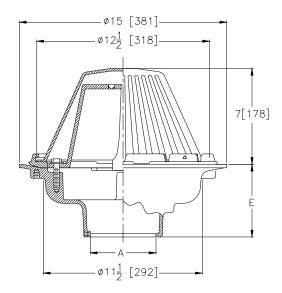


Z-105 CONTROL-FLO ROOF DRAIN w/ Parabolic Weir

TAG_____



Dimensional Data (inches and [mm]) are Subject to Manufacturing Tolerances and Change Without Notice



Pipe Size Inches / [mm]	Approx. Wt. Lbs. / [kg]	Dome Open Area Sq. In. / [sq cm]
2 - 3 - 4	34	148
[51 - 76 - 102]	[15]	[955]

*REGULARLY FURNISHED UNLESS OTHERWISE SPECIFIED

ENGINEERING SPECIFICATION: ZURN Z-105 "Control-Flo" roof drain for dead -level roof construction, Dura-Coated cast iron body. "Control-Flo" weir shall be linear functioning with integral membrane flashing clamp/gravel guard and Poly-Dome. All data shall be verified proportional to flow rates.

OPTIONS (Check/specify appropriate options)

PIPE SIZE	(Specify size/typ	oe) OUTLET	E BODY HT. DIM.		
2,3,4 [50,75,1 2,3,4 [50,75,1 2,3,4 [50,75,1 2,3,4 [50,75,10	00]		Inside Caulk Threaded No-Hub Neo-Loc	5 1/4 [133] 3 3/4 [95] 5 1/4 [133] 4 5/8 [117]		
PREFIXES Z- ZA-	D.C.C.I. Body with Poly-Dome* D.C.C.I. Body with Aluminum Dome	e				
SUFFIXES	Waterproof Flange Acid Resistant Epoxy Coated Finis Underdeck Clamp Top Set® Roof Deck Plate (Replace-C and -R) Adjustable Drain Riser Extension A 3-5/8" [92] to 7-1/4" [184] Static Extension 1 [25] thru 4 [102] (Sp Adjustable Extension Assembly 1 3/4 [44] thru 3 1/2 [89]	es both the	EB G R VP 90	Elevating Body Plate Galvanized Cast Iron Roof Sump Receiver Vandal Proof Secured Top 90° Threaded Side Outlet Body		
			REV. A DA	ATE: 09/14/05 C.N. NO. 89837		

DWG. NO. 63601

PRODUCT NO. Z-105

Appendix F Site Servicing Checklist





Servicing study guidelines for development applications

4. Development Servicing Study Checklist

The following section describes the checklist of the required content of servicing studies. It is expected that the proponent will address each one of the following items for the study to be deemed complete and ready for review by City of Ottawa Infrastructure Approvals staff.

The level of required detail in the Servicing Study will increase depending on the type of application. For example, for Official Plan amendments and re-zoning applications, the main issues will be to determine the capacity requirements for the proposed change in land use and confirm this against the existing capacity constraint, and to define the solutions, phasing of works and the financing of works to address the capacity constraint. For subdivisions and site plans, the above will be required with additional detailed information supporting the servicing within the development boundary.

4.1 General Content

□ Executive Summary (for larger reports only).
 □ Date and revision number of the report.

×	Location map and plan showing municipal address, boundary, and layout of proposed development.
×	Plan showing the site and location of all existing services.
×	Development statistics, land use, density, adherence to zoning and official plan, and reference to applicable subwatershed and watershed plans that provide context to which individual developments must adhere.
×	Summary of Pre-consultation Meetings with City and other approval agencies.
×	Reference and confirm conformance to higher level studies and reports (Master Servicing Studies, Environmental Assessments, Community Design Plans), or in the case where it is not in conformance, the proponent must provide justification and develop a defendable design criteria.
×	Statement of objectives and servicing criteria.
×	Identification of existing and proposed infrastructure available in the immediate area.
	Identification of Environmentally Significant Areas, watercourses and Municipal Drains potentially impacted by the proposed development (Reference can be made to the Natural Heritage Studies, if available).
	Concept level master grading plan to confirm existing and proposed grades in the development. This is required to confirm the feasibility of proposed stormwater management and drainage, soil removal and fill constraints, and potential impacts to neighbouring properties. This is also required to confirm that the proposed grading will not impede existing major system flow paths.
	Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts.
	Proposed phasing of the development, if applicable.





- ☑ Reference to geotechnical studies and recommendations concerning servicing.
- ☑ All preliminary and formal site plan submissions should have the following information:
 - Metric scale
 - North arrow (including construction North)
 - Key plan
 - Name and contact information of applicant and property owner
 - Property limits including bearings and dimensions
 - Existing and proposed structures and parking areas

☐ Confirm consistency with Master Servicing Study if available

- Easements, road widening and rights-of-way
- Adjacent street names

4.2 Development Servicing Report: Water

	the contraction of the contracti
×	Availability of public infrastructure to service proposed development
×	Identification of system constraints
×	Identify boundary conditions
×	Confirmation of adequate domestic supply and pressure
×	Confirmation of adequate fire flow protection and confirmation that fire flow is calculated as per the Fire Underwriter's Survey. Output should show available fire flow at locations throughout the development.
×	Provide a check of high pressures. If pressure is found to be high, an assessment is required to confirm the application of pressure reducing valves.
	Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defined phases of the project including the ultimate design
	Address reliability requirements such as appropriate location of shut-off valves
	Check on the necessity of a pressure zone boundary modification.
×	Reference to water supply analysis to show that major infrastructure is capable of delivering sufficient

water for the proposed land use. This includes data that shows that the expected demands under average day, peak hour and fire flow conditions provide water within the required pressure range





×	Description of the proposed water distribution network, including locations of proposed connections to the existing system, provisions for necessary looping, and appurtenances (valves, pressure reducing valves, valve chambers, and fire hydrants) including special metering provisions.
	Description of off-site required feedermains, booster pumping stations, and other water infrastructure tha will be ultimately required to service proposed development, including financing, interim facilities, and timing of implementation.
×	Confirmation that water demands are calculated based on the City of Ottawa Design Guidelines.
×	Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference.
	4.3 Development Servicing Report: Wastewater
×	Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitored flow data from relatively new infrastructure cannot be used to justify capacity requirements for proposed infrastructure).
	Confirm consistency with Master Servicing Study and/or justifications for deviations.
	Consideration of local conditions that may contribute to extraneous flows that are higher than the recommended flows in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers.
×	Description of existing sanitary sewer available for discharge of wastewater from proposed development.
×	Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable)
×	Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format.
×	Description of proposed sewer network including sewers, pumping stations, and forcemains.
	Discussion of previously identified environmental constraints and impact on servicing (environmental constraints are related to limitations imposed on the development in order to preserve the physical condition of watercourses, vegetation, soil cover, as well as protecting against water quantity and quality).
	Pumping stations: impacts of proposed development on existing pumping stations or requirements for new pumping station to service development.
	Forcemain capacity in terms of operational redundancy, surge pressure and maximum flow velocity.
	Identification and implementation of the emergency overflow from sanitary pumping stations in relation to the hydraulic grade line to protect against basement flooding.
	Special considerations such as contamination, corrosive environment etc.





4.4 Development Servicing Report: Stormwater Checklist

×	Description of drainage outlets and downstream constraints including legality of outlets (i.e. municipal drain, right-of-way, watercourse, or private property)
×	Analysis of available capacity in existing public infrastructure.
×	A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns, and proposed drainage pattern.
×	Water quantity control objective (e.g. controlling post-development peak flows to pre-development level for storm events ranging from the 2 or 5 year event (dependent on the receiving sewer design) to 100 year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects.
×	Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements.
×	Description of the stormwater management concept with facility locations and descriptions with references and supporting information.
	Set-back from private sewage disposal systems.
	Watercourse and hazard lands setbacks.
	Record of pre-consultation with the Ontario Ministry of Environment and the Conservation Authority that has jurisdiction on the affected watershed.
×	Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists.
×	Storage requirements (complete with calculations) and conveyance capacity for minor events (1:5 year return period) and major events (1:100 year return period).
	Identification of watercourses within the proposed development and how watercourses will be protected or, if necessary, altered by the proposed development with applicable approvals.
×	Calculate pre and post development peak flow rates including a description of existing site conditions and proposed impervious areas and drainage catchments in comparison to existing conditions.
	Any proposed diversion of drainage catchment areas from one outlet to another.
×	Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and stormwater management facilities.
	If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post-development flows up to and including the 100 year return period storm event.
	Identification of potential impacts to receiving watercourses
	Identification of municipal drains and related approval requirements.

☑ Descriptions of how the conveyance and storage capacity will be achieved for the development.
 ☑ 100 year flood levels and major flow routing to protect proposed development from flooding for

establishing minimum building elevations (MBE) and overall grading.





×	Inclusion of hydraulic analysis including hydraulic grade line elevations.
×	Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors.
	Identification of floodplains – proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions.
	Identification of fill constraints related to floodplain and geotechnical investigation.
	4.5 Approval and Permit Requirements: Checklist
	The Servicing Study shall provide a list of applicable permits and regulatory approvals necessary for the proposed development as well as the relevant issues affecting each approval. The approval and permitting shall include but not be limited to the following:
	Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act.
	Application for Certificate of Approval (CofA) under the Ontario Water Resources Act.
	Changes to Municipal Drains.
	Other permits (National Capital Commission, Parks Canada, Public Works and Government Services Canada, Ministry of Transportation etc.)
	4.6 Conclusion Checklist
×	Clearly stated conclusions and recommendations
	Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency.
×	All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario

Appendix G Topographic and Legal Survey

