

210 Prescott Street, Unit 1 P.O. Box 189 Kemptville, Ontario K0G 1J0 Civil • Geotechnical •

Structural • Environmental •

Hydrogeology •

(613) 860-0923 FAX: (613) 258-0475

SITE SERVICING AND STORMWATER **MANAGEMENT REPORT**

LIGHT INDUSTRIAL BUILDING 140 Reis Road OTTAWA, ONTARIO

Prepared For:

City Wye'd Electric 132 Reis Road, Carp, Ottawa, Ontario

PROJECT #: 210430

DISTRIBUTION City of Ottawa City Wye'd Electric Ltd Kollaard Associates Inc.

Rev 0 - Issued for Site Plan Approval

August 13, 2021



TABLE OF CONTENTS

TABI	LE OF	CONTEN	ITS	1
LIST	OF AF	PENDIC	ES	2
LIST	OF DE	RAWING	S	2
1	INTR	ODUCTIO	ON	3
	1.1		nsultation Meeting	
2	STOR		R DESIGN	
	2.1	Stormy	vater Management Design Criteria	4
		2.1.1	Design Criteria	4
		2.1.2	Minor System Design Criteria	4
		2.1.3	Major System Design Criteria	4
		2.1.4	Quality Control Design Criteria	4
	2.2	Stormy	vater Quantity Control	4
		2.2.1	Pre-development Site Conditions	
			2.2.1.1 Pre-development Off-Site Drainage Patterns	
		2.2.2	Runoff Coefficients	
		2.2.3	Time of Concentration	
		2.2.4	Total Allowable Runoff Rate	
		2.2.5	Post Development Site Area and Quantity Control Requirements	
			2.2.5.1 Post Development Runoff Coefficient	8
			2.2.5.2 Quantity Control Requirements	8
		2.2.6	Consideration for Post-development Runoff from Off-Site.	9
		2.2.7	Post Development Restricted Flow and Storage	
	2.3		Sewer Design	
	2.4	Stormy	vater Quality Control	
			2.4.1.1 Volumetric Sizing and Filter Size	
	0.5	0 1	2.4.1.2 Grey Water from Building	
	2.5		ion and Maintenance	
_		2.5.1	Winter Operation	
3			AND - DOMESTIC	
	3.1		Demand – Fire Fighting Supply and Storage	
4			RVICE	
5	EROS	SION ANI	O SEDIMENT CONTROL	20
c	CON	CLLICION	c	21



LIST OF APPENDICES

Appendix A: Storm Design Information

Appendix B: Product Information and Certificate of Well Compliance

Appendix C: Sewage System Design

Appendix D: Correspondence

LIST OF DRAWINGS

210430 – GRD – Site Grading Plan

210430 - SER - Site Servicing Plan

210430 – ESC – Erosion and Sediment Control Plan

210430 – SWM – Stormwater Management Plan



1 INTRODUCTION

Mr. Scott Winch of City Wye'd Electric Ltd has retained the services of Kollaard Associates Inc. to complete Site Servicing and Stormwater Management designs and prepare a report for the proposed Light Industrial Building at 140 Reis Road, Ottawa, Ontario.

The report will address the serviceability of the proposed light industrial building development with respect to the water and sanitary demands and outline the proposed design to meet these requirements.

The report shall also summarize the stormwater management (SWM) design requirements and proposed works that will address stormwater flows arising from the site under post-development conditions and will identify any stormwater servicing concerns. The report will describe any measures to be taken during construction to minimize erosion and sedimentation for the proposed development.

For the purposes of this report, Reis Road is considered to be oriented along an east west axis. The development being proposed by Mr. Scott Winch is located on the north side of Reis Road about 100 metres east of Tansley Drive within the City of Ottawa. The site is located in an industrial subdivision that is known as the Reis Business Park, is zoned RG4 and is within the Carp Road Corridor.

The site has a total area of 0.1819 hectares and is currently undeveloped. There are no watercourses or easements effecting development on the proposed site. The site is located within the Carp River subwatershed. The nearest receiving water body is the Huntley Creek about 350 metres south of the site.

The proposed works will consist of an approximately 465 square metre pre-engineered steel building with an asphalt surfaced entrance driveway and a gravel surfaced parking area and driveway at the rear of the building. The building will be utilized as an automotive service station.

1.1 Pre-consultation Meeting

A pre-consultation meeting was held with the City of Ottawa and was attended by the Client, Krishon Walker (Planner), Brian Morgan (Infrastructure Project Manager) and others from the City of Ottawa as well as Erica Ogden, (Planner) from Mississippi Valley Conservation Authority. A summary of the design requirements are provided in an email in Appendix D.

2 STORMWATER DESIGN

2.1 Stormwater Management Design Criteria

Design of the storm sewer system was completed in conformance with the City of Ottawa Design Guidelines. (October 2012). Section 5 "Storm and Combined Sewer Design".

2.1.1 Design Criteria

The development falls within the Reis Road Business Park. The allowable runoff rate from sites within the Reis Road Business Park is governed by the design assumptions used in the approved Engineering Report contained in Schedule H of the subdivision agreement.

- The design of the internal drainage for the subdivision was based on site developments that would be: 50% building (C=1.0), 25% parking (C=0.9) and 25% undeveloped (C=0.2).
- Inlet time of 20 min max.

2.1.2 Minor System Design Criteria

5-year post-development storm event is to be controlled to the runoff rate calculated for a 5-year storm event using the above design assumptions.

2.1.3 Major System Design Criteria

If the post-development C-value is below 0.775, no on-site SWM from a quantity control perspective will be required. If SWM is required, the allowable release will be based on the 5-year flow, with a C-value of 0.775.

2.1.4 Quality Control Design Criteria

The water quality objective was provided by the Mississippi Valley Conservation Authority. As per the Carp River Watershed Subwatershed Study, the water quality should include a normal level of protection which is 70% Total Suspended Solids removal.

2.2 Stormwater Quantity Control

Peak Flow for runoff quantities for the Pre-Development and Post-Development stages of the project were calculated using the rational method. The rational method is a common and straightforward calculation, which assumes that the entire drainage area is subject to uniformly distributed rainfall. The formula is:



$$Q = \frac{CiA}{360}$$

Where

Q is the Peak runoff measured in m^3/s C is the Runoff Coefficient, **Dimensionless** A is the runoff area in **hectares** i is the storm intensity measure in **mm/hr**

All values for intensity, i, for this project were derived from IDF curves provided by the City of Ottawa for data collected at the Ottawa International airport. For this project two return periods were considered, 5 and 100-year events. The formulae for each are:

5-Year Event

$$i = \frac{998.071}{\left(t_c + 6.053\right)^{0.814}}$$

100-Year Event

$$i = \frac{1735.688}{\left(t_c + 6.014\right)^{0.82}}$$

where t_c is time of concentration

2.2.1 Pre-development Site Conditions

The site is currently undeveloped and zoned as Rural General Industrial (RG4). The existing ground surface covering consists of mulch, bare earth and thin grass. The existing ground surface is sloped from west to east across the site directing runoff by sheet flow to the east side of the site. The center of the east side of the site is slightly higher than the north (back) and south (roadside) of the site directing runoff by shallow concentrated flow to the undeveloped land north of the site and to the roadside ditch south of the site.

2.2.1.1 Pre-development Off-Site Drainage Patterns

The existing property west of the site has been partially developed with a gravel surfaced parking area. Runoff from the first about 15 metres of this property is direct by sheet flow onto the site. The existing property to the east of the site has been developed with a building and gravel surfaced parking area/roadway. The building is located on the side of the property closest to the site. Runoff from half of the roof of this building and from the area between the building and the site is directed by sheet flow onto the site.

The existing ground surface north and south of the site is lower than the site so no runoff is directed onto the site from either the north or south.

2.2.2 Runoff Coefficients

Runoff coefficients for a 5 year return period for the following surfaces are:

Impervious

Roofs - C=1.0

Asphalt -C = 0.9

Gravel - C = 0.9

Pervious surfaces

Grass and Vegetative Landscaping -C = 0.20.

It is noted that Gravel is normally considered to be a semi-pervious surface with a runoff coefficient of 0.7. The design assumptions used in the approved Engineering Report contained in Schedule H of the subdivision agreement do not account for gravel surfaces. In addition, it is considered that the gravel surfaces could be paved in the future.

A 25% increase for the 100-year runoff coefficients was used as per City of Ottawa guidelines. Refer to Appendix A for pre-development and post development runoff coefficients.

2.2.3 Time of Concentration

As previously indicated, the runoff pattern during pre-development conditions is directed west to east across the site by sheet flow, then north and south by concentrated flow. The site has a width of about 30 metres with the east about 2 m portion of the site sloping back towards the centre.

The time of concentration for pre-development conditions was calculated using the Velocity method. The velocity method assumes that the time of concentration is the sum of travel times for segments along the hydraulically most distant flow path. The segments used in the velocity method may be of three types: sheet flow T_s , shallow concentrated flow T_{sc} , and open channel flow T_c . Since the area of consideration for the stormwater analysis consists of a single site, open channel flow will not be present and is not considered.

Travel time for sheet flow:

$$T_{S} = \frac{0.091(nl)^{0.8}}{(P_{2})^{0.5}S^{0.4}}$$

Where $T_s = travel time, h$

n = Manning's roughness coefficient sheet flow = 0.3



I = sheet flow length, 28 m

P₂ = 2-year 24-hour rainfall, = 48.47 mm S = Slope of land surface m/m = 0.027

 $T_s = 0.31 \text{ hours}$

Travel time for shallow concentrated flow:

The flow velocity used to calculate the time of travel for shallow concentrated flow was determined using Figure 15-4 of Chapter 15 of the USDA handbook (Included in Appendix A of this Report). This figure can be used to determine the velocity when the slope and ground cover is known. The ground cover to be used in reading Figure 15-4 was determined as follows: Short Grass (poor condition) - Manning's n for concentrated flow = 0.073. From Figure 15-4 of the USDA Handbook using a slope of 2.7% and Nearly bare conditions, the velocity is estimated at 0.34 m/s (1.1 ft/s).

$$T_{sc} = \frac{l}{3600 \, V}$$

Where $T_{sc} = travel time, h$

I = distance of shallow concentrated flow = 30 (half site length)

V = average velocity = 0.34 m/s

 $T_{sc} = 0.02 \text{ hrs}$

Total time of concentration for pre-development conditions is equal to $T_s = 0.31$ hours + $T_{sc} = 0.02$ hrs = 0.33 hrs = 20 min.

The calculated time of concentration is in keeping with the design assumptions from the approved engineering report of the subdivision.

2.2.4 Total Allowable Runoff Rate

Based on the stormwater management criteria, the stormwater management during postdevelopment conditions must be controlled to the levels that match the subdivision design assumptions.

The total allowable runoff rate was established using the rational method. A twenty-minute duration yields an intensity of 70.25 mm/hr for a 5-year storm event and of 119.95 mm/hr for a 100-year storm event. The runoff coefficients were set to C = 0.775 for both the five year and 100 year storm based on the design criteria.

The total allowable runoff for the site based on the subdivision design assumptions was calculated as follows:

For the 5-year Storm event

- $= (0.775 \times 70.25 \times 0.1819)/360$
- $= 0.0275 \text{ m}^3/\text{s}$
- = 27.7 Litres per second

For the 100-year Storm event

- $= (0.775 \times 119.95 \times 0.1819)/360$
- $= 0.0470 \text{ m}^3/\text{s}$
- = 47.0 Litres per second

2.2.5 Post Development Site Area and Quantity Control Requirements

2.2.5.1 Post Development Runoff Coefficient

The proposed development will consist of a 465 square metre building, while 475 square metres will be gravel surfaced and 120 square metres will be asphalt surfaced. All remaining areas will be grassed/landscaped areas. The proposed building will be serviced by a Class 4 onsite septic system and a drilled cased well.

The runoff coefficient for the 5 year and 100 year storm events for post-development were calculated based on a weighted average for the proposed development area as shown in the following table 2.1:

Table 2.1 – Post-Development Runoff Coefficients

Description	Surface Area	Runoff Coefficie	ent
	m ²	5 year	100 year
Roof	465	0.9	1
Asphalt and Gravel	475	0.9	1
Landscaping	759	0.2	0.2
Weighted Average	1819	0.633	0.687
Entire Site			

2.2.5.2 Quantity Control Requirements

Based on Guidance provided by the City of Ottawa as included in Appendix D:

Stormwater Management – The allowable runoff rate from sites within the Reis Industrial Park is governed by the design assumptions used in the approved Engineering Report contained in Schedule "H" of the subdivision agreement. If the resulting runoff from the proposed site will

be less than the allowable rate, no on-site SWM will be required. The design parameters used in the approved subdivision Engineering Report are as follows:

The design of the internal drainage for the subdivision was based on site developments that would be: 50% building (C=1.0), 25% parking (C=0.9) and 25% undeveloped (C=0.2). Based on City of Ottawa interpretation of design assumptions in the subdivision Engineering Report, sites in this subdivision can be developed without a requirement for on-site SWM as long as the combined C-value does not exceed 0.775.

Since the post-development runoff coefficient for the proposed development during a 100 year event using runoff coefficients increased by 25% to a maximum of 1.0 is less than 0.775, no onsite stormwater management is required from a quantity control perspective.

2.2.6 Consideration for Post-development Runoff from Off-Site.

As previously indicated, the existing property west of the site has been partially developed with a gravel surfaced parking area. Runoff from the first about 15 metres of this property is direct by sheet flow onto the site. The existing property to the east of the site has been developed with a building and gravel surfaced parking area/roadway. The building is located on the side of the property closest to the site. Runoff from half of the roof of this building and from the area between the building and the site is directed by sheet flow onto the site.

Since a portion of the adjacent properties direct runoff onto the subject site, the proposed grading of the subject site has to accommodate this runoff. The development of the subject site cannot negatively impact the adjacent properties.

The proposed grading of the subject site will incorporate shallow sub-drained swales along both the west and east sides of the site. These swales will direct runoff to the roadside ditch along the front of the site.

2.2.7 Post Development Restricted Flow and Storage

Since there is no requirement for on-site stormwater management from a quantity control perspective, there is no quantity control storage volume required.

Storage is required in order to achieve the required quality control for the site. The quality control storage has been divided between two subdrained swales on either side of the site. The swales will discharge by infiltration and by means of the subdrain during minor storm events and by overflow over a weir during major storm events.

The quality storage swales have been designed as follows:



- The storage swale along the west side of the site will have a flat bottom with a width of 0.5 metres beginning 0.5 metres from the adjacent property.
- The side slopes of the storage swale will extend down to the bottom of the swale from the existing ground surface along the property line and from the edge of the parking lot/driveway pavement structure.
- The side slopes will be covered with a topsoil layer having a minimum thickness of 0.1 metres and will be seeded with grass.
- The subdrain for the swale will be constructed as follows:
 - The clear stone will be exposed to the surface in the flat part of the bottom of the swale.
 - The subdrain will extend a total of a 1.5 metres below the topsoil towards the pavement structure and will be comprised of a 1.0 metres width of clearstone followed by a 0.5 metre width of filter sand then a 0.5 metre width of clearstone.
 - A 200 mm diameter HDPE perforated pipe will be located in the 0.5 metre width of clearstone closest to the pavement structure.
 - The clear stone will have a minimum depth of 0.7 metres below the flat bottom of the swale a layer and minimum depth of 0.6 metres below the topsoil.
 - o The bottom of the clearstone will extend 0.25 metres below the perforated pipe.
 - The clear stone and sand will be wrapped with a 6 ounce per square yard non-woven geotextile fabric.
- Discharge from the swale and subdrain will be by means of infiltration through the bottom of the subdrain, through the perforated pipe and by overflow.
- For the purposes of the design, infiltration is only assumed to occur through the bottom of each subdrain. The depth of infiltration is only considered for the upper metre of soil below the subdrain due to the low permeability of the soil.
- Discharge from the perforated pipe will be controlled by the rate at which water flows through the sand filter to the perforated pipe. Since the bottom 0.25 metres of the sand layer is below the invert of the perforated pipe, it was not considered as part of the filter area.
- Overflow through the weir will occur once the water level in the swale reaches the invert of the weir.

Since there is no quantity storage requirement from a stormwater management perspective, the rate of discharge from the filter is only significant to ensure that the swale and subdrain will empty within the allowable range of draw down times following a storm event.

2.3 Storm Sewer Design

The storm sewers on site consist of the perforated HDPE pipe in the subdrains. The perforated pipe will have a diameter of 200 mm and will be installed at a slope of 0.1 percent.



The Runoff from the west half of the roof, the portion of the parking area and driveway west of the building and the adjacent grassed surface will be directed to the swale west of the building. This catchment has an area of about 708 square metres.

The runoff from the east side of the building, the parking area and driveway north of the building, and the adjacent grassed surface will be directed to the swale east of the building. This catchment has an area of about 829 square metres.

Calculations showing the capacity of the perforated storm pipes in each subdrain are shown in Appendix A. From the appendix, the perforated pipe does not have sufficient capacity to convey the flow from a 5 year storm event. It is noted that the perforated pipe in not intended to convey the flow resulting from the 5 year design storm event. The perforated pipe is intended to convey the flow that passes through the filter and is intended to facilitate the low slope of the swales.

2.4 Stormwater Quality Control

Stormwater treatment of 70% TSS removal will be provided by a treatment train approach. The treatment train consists of sedimentation within the grass surfaced side slopes of the storage swales followed by filtration through a sand filter.

In the Ministry of Environment Stormwater Management Planning and Design Manual (March 2003) (MOE Manual) provides guidance on design for stormwater quality control. Quality control design is completed with the fundamental understanding that the majority of sediment and particulate pollutants are washed from the site surfaces during minor (frequent) storm events. Section 3.3.1 of the MOE Manual indicates that in most cases, quality control design storms range from 12.5 mm to 25 mm. The MOE Manual also indicates that an alternate approach to the volumetric sizing of stormwater facilities for quality control has been applied in Ontario. The alternate approach is summarized in Table 3.2 *Water Quality Storage Requirements Based on Receiving Waters* which provides the required quality control volume as a function of protection level, SWMP type and impervious level.

In Part 4, the MOE Manual details the design requirements of several types of end of pipe stormwater management facilities. The proposed stormwater management design for quality control will consist of filtration. Design guidance for filtration is provided in Part 4 Section 4.6.7 Filters of the MOE Manual.

As previously indicated, the stormwater management design consists of directing runoff by means of sheet flow to subdrained swales along the east and west sides of the site. The

subdrained swales provide quality control storage and discharge to the roadside ditch at the front of the site. The quality storage swales have been designed to outlet the quality storage volume horizontally through a sand filter and vertically through infiltration. Section 4.6.7 provides the design guidance with respect to the use of a filter as summarized in the table below. A column has been added to indicate how the proposed design conforms to the Criteria.

Design Element	Design Objective	Minimum Criteria	Design Conformance
Drainage Area		< 5 hectares	~ 0.1819 hectares
Pre- treatment	Longevity	Pre-treatment by means of sedimentation chamber, or forebay, vegetated filter strip, swale or oil/grit separator	Pre-treatment by vegetated filteration on grassed side slope of swale.
Storage Depth	Avoid Filter Compaction	Subsurface sand and organic filters: 0.5 m Maximum 1.0 m	Maximum storage depth of 0.6 m
Filter Media Depth	Filtering	Sand: 0.5 m	Filter width 0.5m
Under-drain	Discharge	Minimum 100 mm perforated pipes bedded in 150 – 300 mm of 50 mm gravel	200 mm perforated pipe in minimum 200 mm of 25-50 mm clear stone.
Land use		any land use, often employed for commercial and industrial	light industrial
Volumetric Sizing		provided in Table 3.2 under infiltration. By-pass flows should not occur below a 4 hr 15 mm design event	Quality storage volume sufficient to contain entire volume of a 15 mm storm event before by-pass for the catchment area of each swale
Filter Size		Determined using the Darcy Equation	Determined using the Darcy Equation
Filter Lining	prevent clogging	liner to prevent native material from entering filter	Non-woven geotextile filter clothe used between native material and filter and between filter and clearstone
Overflow / by-pass		required	overflow is provided above the quality storage requirement
Drawdown time	prevent standing water	maximum from 24 to 48 hours 24 hours preferred	Design drawdown time of between 9 and 11 hours



2.4.1.1 Volumetric Sizing and Filter Size

From Table 3.2 under infiltration it was determined that the water quality storage requirement for a 58 percent impervious ratio at an enhanced level of treatment is 31 cubic metres per hectare. Based on a quality storage requirement of 31 cubic metres per hectare and the surface area of the site, the total water quality storage requirement is 5.6 cubic metres. The manual however requires that by-pass does not occur below a 4 hr 15 mm design event. In order to ensure that by-pass would not occur below a 4 hr 15 mm design event, each quality storage swale was designed to accommodate the entire volume of a 15 mm rainfall assuming all of the rainfall originating on the catchment area of each respective swale runs off into the quality storage swale. It is noted that a runoff coefficient of 0.69 indicates that only 69% of the rainfall will result in runoff. Further this design conservatively assumes no discharge through the filter during the 4 hr 15 mm design event.

The MOE Manual indicates that the size of the filter be designed to ensure a specified volume is discharged within a specified time period using the Darcy Equation. The size of the filter and storage volume must be sufficient to ensure that no overflow or by-pass occurs below the 4 hr 15 mm design storm.

The total area contributing to the west swale is 708 square metres and to the east swale is 829 square metres. A 15 mm storm event will result in a runoff volume of 10.6 m^3 in the west swale and 12.4 m^3 in the east swale. The west quality storage swale has a storage volume of 10.8 m^3 below the outlet weir and the east quality storage swale has a storage volume of 13.0 m^3 below the outlet weir.

The proposed filter has been sized based on the space available for the filter. The flow rate through the filter was calculated and the drawdown time was determined based on the volume of the quality storage.

Quality assurance will be provided by filtration through horizontal sand filters located below each quality storage swale. The proposed filters will be constructed with a width of 0.5 metres. The sand used to construct the filter will consist of a septic sand having a percolation rate "T" time of 8 min/cm and a maximum of 3 percent passing the 0.08 millimetre sieve size. This corresponds to a coefficient of permeability of k = 75 millimetres per hour. The sand will be placed as shown in the details on Kollaard Associates Inc. drawing # 210430-GRD will have a depth of 0.5 metres. The filter will be protected with 25-50 mm clear stone. A non-woven

geotextile filter fabric (such as Terrafix 270R or an approved alternative) will be placed between the sand and the clearstone and around the clearstone and sand to avoid contamination of the filter sand from the underlying native material and mixing of the filter sand with the clearstone. This fabric offers medium tensile strength at high elongation and good filtration, coupled with high permeability to allow for proper filtration, while holding the filter sand in place as designed. The Terrafix Geosynthetics Inc. specification Sheet can be found in Appendix B.

The flow rate through the sand filter was calculated using Darcy's Equation to be:

Q = Aki

Where A = cross-sectional area of filter = 0.35 (height) * 50 (min perimeter Length) = 17.5 m^2 for the swale along the west side and $0.35 \times 60 = 21 \text{ m}^2$ for swale along the east side.

k = coefficient of permeability = 2.1×10^{-5} m/s

i = hydraulic gradient = average head across the filter / flow path across the filter = varies

At a ponding level equal to the overflow over the weir the flow rate through the filter equals West swale:

 $Q = 17.5 \times 0.000021 \times (0.55)/0.5 = 0.0004 \text{ m}^3/\text{sec}$

East swale

 $Q = 21 \times 0.000021 \times (0.55)/0.5 = 0.0005 \text{ m}^3/\text{sec}$

Additional Calculations are provided in Appendix A.

From initial field investigation done by Kollaard Associates Inc, the underlying soils consist mostly of silty sand, silt or silty clay within the first 1 metre below the ground surface consist of grey brown silty sand having a percolation rate of 15 min/cm. From Ontario Building Code, SB-6 Table 2, the average coefficient of permeability for this type of soil would be expected to be in the range of 1.0×10^{-4} cm/sec.

The flow rate through the bottom of the quality storage subdrained swales would be:

Q = Aki

Where A = combined surface area of the bottom of the clearstone and sand = 100 m^2 for the west swale and 120 m^2 for the east swale.

 $k = coefficient of permeability = 1 \times 10^{-6} \text{ m/s}$

i = varies = ((h+d)/d) where d is the upper 1.0 m of soil below the storage swale and h is the ponding depth above the bottom of the clearstone and equals

At a ponding level equal to the overflow over the weir the flow rate through the bottom equals West swale:

 $Q = 100 \times 0.000001 \times (0.8+1)/1 = 0.0002 \text{ m}^3/\text{sec}$



East swale

 $Q = 120 \times 0.000001 \times (0.8+1)/1 = 0.0002 \text{ m}^3/\text{sec}$

With a combined flow rate of 0.4 L/s through the filter and 0.2 L/s through bottom of the subdrained swale, the draw down time for the $10.8~\text{m}^3$ in the west swale would be approximately 9.4 hours and for the $13~\text{m}^3$ in the east swale would be approximately 10.3~hours.

Since there is not quantity control requirement, the outlet rate from each swale is appropriate to ensure that the swales drain at a sufficient rate to prevent standing water and to ensure sufficient available volume for subsequent storm events.

2.4.1.2 Grey Water from Building

There are no proposed floor drains within the building. As such there is not anticipated to be any grey water generated within the proposed building.

Notwithstanding the current plans, if floor drains are to be installed and grey water is generated from a proposed use within the building, the grey water should be collected within the building in a storage tank below the floor slab of the building. The storage tank will then be emptied by a company licensed to collect, transport and dispose of waste water. As such the interior building use will not contribute flow to the storm water management facility.

2.5 Operation and Maintenance

During winter operation, the predominant sediment load on the storage area will result from sand placed during de-icing salting/sanding of the parking and gravel surfaces of the site and from sand carried onto the site from vehicles. During spring melt, the sediment will be transported towards the storage area. The runoff will be directed over the grasses side slopes of the swales and through the clearstone prior to encountering the filter. Sedimentation within the grassed side slope and through the clearstone will provide pre-treatment reducing the sediment load on the filters.

The subdrained swales should be inspected on a weekly basis and after any rain fall event during and after construction until vegetation is well established. Any areas of erosion or distress should be repaired immediately.

The subdrained swales should be inspected after major storm events and after snow melt in the spring. Water ponding within the upper portion of the clearstone would indicate that the swale and/or subdrain is either partially or completely blocked. If the subdrained swale becomes filled with sediment, the clearstone and subdrain will require maintenance. The



maintenance would consist of excavating the swale and subdrain and either cleaning and returning the cleaned clearstone or replacing the clearstone.

Once the vegetation is well established, the storage areas should be visually inspected on a bimonthly basis and following significant storm events. Any debris should be removed from the storage areas if present.

The grassed side slopes of the swales should be subjected to the same maintenance schedule as the remainder of the grass covered landscaped "lawn" surfaces. That is, the grass should be mowed and cared for as required to maintain a normal healthy appearance. Minimum recommended grass height in the swales is 75 mm.

Removal of accumulated sediment from the grassed storage areas should be conducted when the accumulation of the sediment begins to significantly affect the quality of the grass growth and/or the drainage patterns along the grassed surfaces. The sand filter should be replaced when the drawdown time increases such that there is visible surface ponding above the clear stone more than 1 day after the rainfall event.

If long term ponding occurs within the storage area upstream of the filter, the engineer should be notified. At this point the engineer could make an assessment of the material in the upper portion of the subdrain and filter. If the assessment indicates that the subdrain and filter has become compromised with sediment, the filter will require maintenance.

2.5.1 Winter Operation

The MOE Manual indicates that filters suffer in performance during winter operation due to freezing of the filter medium. As previously indicated, Filters receive runoff from parking areas and roads which are subject to sanding and salting.

The sediment and particulate matter resulting from these sanding and salting operations tend to be coarser in nature and are more prone to sedimentation within the grass surfaces immediately adjacent to swales. As such, during winter operation, the primary quality control mechanism will be storage and sedimentation as opposed to filtration.

3 WATER DEMAND - DOMESTIC

The facility is to be serviced by a drilled well to be located 4 metres from the east property line about 2 metres from the northeast corner of the building. Information regarding the quality and quantity capabilities of this well can be found in the Hydrogeology Report prepared by Kollaard Associates, *Hydrogeological Study 140 Reis Road, City of Ottawa, Ontario, File Number 210430* dated August 13, 2021. This report also contains a copy of the Ministry of Environment Conservation and Parks (MECP) Certificate of Well Compliance.

The water demand is calculated using the information from the sewage system daily design flow and the City of Ottawa Water Distribution Guidelines, 2010. The sewage design flows are provided below, based on the sewage design which was carried out by Kollaard Associates Inc.

Daily sewage design flow:

- Office building, per employee per eight hour shift = 75 Litres/employee/day x 7 = 525
 L/day
- Warehouse, per water closet (1) And per loading bay (3) = 950 L/day + 150 L/bay/day x 3
 = 1400 L/day
- Total daily design flow = 1,925 litres / day

Since sewage system design is based on the maximum expected daily use, it is equivalent to the Average Daily Demand (ADD). The ADD is based on an eight hour operation schedule (i.e. full day occurs over an eight hour period and not over 24 hours

City of Ottawa calculates the Maximum Hour Demand (MHD) for a commercial or industrial demand to be 1.8 x ADD

ADD = 1925 litres/day x 1 day / 8 hours x 1 hour / 60 minutes = 4.0 litres/minute

 $MHD = 1.8 \times ADD$

- = 1.8 x 4.0 litres/minute
- = 7.2 litres/minute

Alternatively, the City of Ottawa Water Distribution Guideline Section 4.2.8 indicates that the average daily demand for light industrial usage is 35,000 L/gross ha/day. The gross area of the developable area of the site is 0.1819 hectares.

ADD = $0.1819 \times 35,000 = 6,367 \text{ L/day} = 4.4 \text{ L/min}$ MHD = $4.4 \text{ L/min} \times 1.8 = 7.9 \text{ L/min}$.



Since the calculated demand using Section 4.2.8 of the Water Distribution Guideline is greater than the water demand using the sewage design, the average daily demand and maximum hourly demand for the site will be considered to be 4.4 L/m and 7.9 L/min respectively.

The Maximum Hourly Demand for the site based on its proposed use is expected to be about 7.9 litres/minute, compared to the pumping test rate which was 13.7 litres/minute.

The water system shall be pressurized with a submersible well pump, capable of supplying water at a minimum flow rate of about 13.7 litres/minute (3.5 usgpm) and no greater than the recommended pump rate of 6 GPM found in the certificate of well compliance. The pump should be set at a depth of about 83.8 metres aslo as recommended in the certificate of well compliance. The well shall be fitted with a pitless adapter and protrude from the ground at least 400mm. The top of the well casing shall be extended to a minimum elevation of at least 115.63 metres to ensure that it is at least 400 millimetres above the finished grade of 115.23 at the well location. Additionally, the ground surface shall be graded such that it is the highest point on the ground surface within 3 metres radially from the exterior of the well casing and shall ensure that water does not collect or pond near the well head. A seamless 1.25" polyethylene pipe rated at 160psi shall be installed between the well and the building at a depth of at least 2.4m.

3.1 Water Demand - Fire Fighting Supply and Storage

Fire water supply and storage on site is a requirement under Part 3 of the Ontario Building Code. Since the proposed building is under 600 square metres and has a major occupancy of F2/D, the building is considered to be a Part 9 Building with respect to the Ontario Building Code. As such, onsite fire water supply and storage is not required for this site.



4 SANITARY SERVICE

No municipal sanitary services are available at this site.

As per Ontario Building Code (OBC) table 8.2.1.3.B, the daily design sanitary sewage flow for the proposed occupancy is 1,925 litres/day. Sanitary sewage will be disposed of in an onsite Class 4 sewage system with a level IV treatment unit. The onsite system will include a partially raised Type A disposal field preceded by an Ecoflo STB-730PR treatment unit. A sewage system application has been prepared for approval through the Ottawa Septic System Office. Details can be found on the septic design plan prepared by Kollaard Associates.

The septic system design has been submitted to the Ottawa Septic Office for Permit. The septic system design and permit has been added to the report in Appendix C for reference purposes. It is noted that the permit lapses 12 months following the date of issue. As such the permit will be reapplied for with no changes to the original application.



5 EROSION AND SEDIMENT CONTROL

The owner (and/or contractor) agrees to prepare and implement an erosion and sediment control plan at least equal to the stated minimum requirements and to the satisfaction of the City of Ottawa, appropriate to the site conditions, prior to undertaking any site alterations (filling, grading, removal of vegetation, etc.) and during all phases of site preparation and construction in accordance with the current best management practices for erosion and sediment control. It is considered to be the owners and/or contractors responsibility to ensure that the erosion control measures are implemented and maintained.

In order to limit the amount of sediment carried in stormwater runoff from the site during construction, it is recommended to install a silt fence along the property, as shown in Kollaard Associates Inc. Drawing #210430-ESC Erosion and Sediment Control Plan. The silt fence may be polypropylene, nylon, and polyester or ethylene yarn.

If a standard filter fabric is used, it must be backed by a wire fence supported on posts not over 2.0 m apart. Extra strength filter fabric may be used without a wire fence backing if posts are not over 1.0 m apart. Fabric joints should be lapped at least 150 mm (6") and stapled. The bottom edge of the filter fabric should be anchored in a 300 mm (1 ft) deep trench, to prevent flow under the fence. Sections of fence should be cleaned, if blocked with sediment and replaced if torn.

The proposed landscaping works should be completed as soon as possible. The proposed granular and asphaltic concrete surfaced areas should be surfaced as soon as possible.

The silt fences should only be removed once the site is stabilized and landscaping is completed.

These measures will reduce the amount of sediment carried from the site during storm events that may occur during construction.

6 CONCLUSIONS

Based on the analysis provided in this report, the conclusions are as follows:

SWM for the proposed development will be provided in keeping with the design assumptions used in the approved engineering report for the Reis Business Park.

Quantity Control measures are not required as the post-development level of imperviousness is in keeping with the approved engineering report as interpreted by the City of Ottawa.

A normal level of Quality Control will be achieved by means of vegetative filtration followed by filtration through a sand filter.

Discharge from the site will be conveyed to the roadside ditch in accordance with the Reis Business Park design.

The daily design sanitary sewage flow rate from the proposed development will be 1,925 litres/day. Sanitary sewage will be disposed of in an onsite Class 4 sewage system with a level IV treatment unit.

The facility is to be serviced by a drilled cased well.

During all construction activities, erosion and sedimentation shall be controlled.

We trust that this report provides sufficient information for your present purposes. If you have any questions concerning this report or if we can be of any further assistance to you on this project, please do not hesitate to contact our office.

Sincerely, Kollaard Associates, Inc.



Steven deWit, P.Eng.



Appendix A: Storm Design Information

- · Figure 15-4 of Chapter 15 of the USDA handbook
- · Post-Development Runoff Coefficient Calculation And Unrestricted Flow
- · Outlet Control Design Sheet West Swale
- · Outlet Control Design Sheet –East Swale
- · Sewer Design Sheet

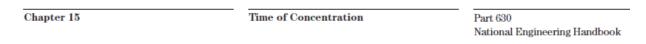
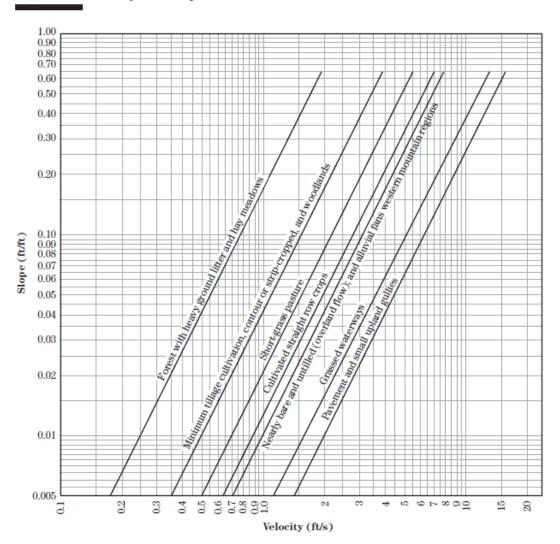


Figure 15-4 Velocity versus slope for shallow concentrated flow



Civil •

210 Prescott Street, Unit 1 P.O. Box 189

Kemptville, Ontario K0G 1J0

Geotechnical •

Hydrogeological •

Inspection Testing •

Septic Systems Grading •

APPENDIX A: STORMWATER MANAGEMENT MODEL Structural • Environmental •

POST-DEVELOPMENT RUNOFF COEFFICIENT CALCULATION AND UNRESTRICTED FLOW

Client: City Wye'd Electric

Job No.: 210430

Location: 140 Reis Road Date: August 13, 2021

CA1 - CONTROLLED AREA

Post Dev run-off Coefficient "C"

			5 Ye	ear Event	100 Year E	vent
Area (ha)	Surface	Area (ha)	"C"	C_{avg}	"C" x 1.25	C _{100 avg}
Total	Roof	0.0465	1.00	0.633	1.00	0.687
0.1819	Asphalt	0.0120	0.90		1.00	
	Gravel	0.0475	0.90		1.00	
	Grass	0.0759	0.20		0.25	

Impervious Ratio

0.58

Post-development unrestricted flow

2 Year Event

Pre Dev.	С	Intensity	Area	
2 Year 2.78CIA= 0.65 0.6 L/S	0.63	2.02	0.182	48.47317392

**Use a 1440 minute time of concentration for 5 year

5 Year Event

Pre Dev.	С	Intensity	Area
5 Year	0.63	104.19	0.182
2.78CIA= 33	3.38		
33.4 L/	S		

**Use a 10 minute time of concentration for 5 year

100 Year Event

Pre Dev.	C*	Intensity	Area
100 Year 2.78CIA= (0.69 62.04	178.56	0.182
62.0	L/S		
4411	4.0		

**Use a 10 minute time of concentration for 100 year *C value multiplied by 1.25 for 100 year event

Equations:

Flow Equation

 $Q = 2.78 \times C \times I \times A$

Where:

C is the runoff coefficient

I is the intensity of rainfall, City of Ottawa IDF

A is the total drainage area

Notes: * City of Ottawa Sewer Design Guidelines October 2012 - Section 5.4.5.2.1

** Post-Development Time of Concentration discussed in the text of the Report



Geotechnical • Hydrogeological • Inspection Testing • Septic Systems Grading • Structural • Environmental •

Kemptville, Ontario K0G 1J0 210 Prescott Street, Unit 1

APPENDIX A: STORMWATER MANAGEMENT MODEL

OUTLET CONTROL DESIGN SHEET - WEST SWALE

City Wye'd Electric 210430 Job No.:

140 Reis Road Location:

August 13, 2021

8 min/cm 75 mm/hr Filter Information Percolation Time T = Percolation Rate = 50 min/cm 3.6 mm/hr Infiltration Information Percolation Time T = Percolation Rate =

Weir Width (m): Weir Coefficient:

Outflow (L/sec) Total 56.0 20.2 0.6 0.5 0.5 0.5 4.0 0.2 0.2 0.2 Outflow (m₃/sec) 0.0202 0.0006 0.0005 0.0005 0.0003 0.0560 0.0005 0.0004 0.0004 Total 0.0002 0.0002 0.0002 0.60 0.62 114.75 Weir Flow (m³/sec) 0.0000 0.0000 0.0000 0.0196 0.0000 0.0000 0.0554 0.0000 0.0000 0.0000 Weir Weir Invert (m): Head (m) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Filter Flow (m₃/sec) 0.0004 0.0004 0.0003 0.0003 0.0002 0.0002 0.0001 0.0001 0.0000 0.0005 0.0003 0.0001 Filter Flow Hydraulic Gradient 6.0 0.8 9.0 0.3 0.2 0.1 Head* 0.45 0.10 0.40 0.15 0.05 0.60 0.35 0.30 0.25 Ξ Rate (m³/sec) Infiltration 0.0002 0.0002 0.0002 0.0002 0.0002 0.0001 0.0001 0.0002 0.0001 0.0002 0.000 0.0001 Infiltration Gradient Hydraulic <u>4</u>. .3 7.3 Head* 0.70 0.60 0.85 0.65 0.40 0.35 0.30 0.90 $\widehat{\Xi}$ Storage (m3) 15.8 12.6 10.8 9.4 8.4 8.0 6.0 5.0 3.0 2.0 1.0 2.1E-05 ncremental Subdrain / Clearstone Volume in (E) 0.5 4.0 0. 1.0 0. 1.0 1.0 1.0 Permeability k = Volume in Depth of Layer = Swale (m³) 0.0 0.0 0.0 0.0 0.0 Bottom Layer Area (m²) 45.0 35.0 25.0 50.0 50.0 50.0 57.0 50.0 50.0 50.0 50.0 Layer Area 50.0 50.0 Тор 72.0 57.0 45.0 35.0 25.0 50.0 50.0 50.0 50.0 20.0 (m²)1.0E-06 m/s Thickness Layer 0.050 0.050 0.050 0.050 0.050 0.050 0.050 0.050 0.050 0.050 0.050 0.050 Ξ Permeability k = Depth of Layer = bottom of pond Comments OVERFLOW OVERFLOW Sand Filter Elev (m) 114.65 114.55 114.80 114.75 114.70 114.45 114.25 114.85 114.35 114.30 Stage, WSE 114.60

Draw Down Time (hrs) 0.0

Time

(s)

Down

Draw

0.2 9.0

2403.166 1936.873 738.472

0.7 0.8 -

0.7

2408.430 2408.430 2675.585 3009.404 3438.395 4010.025

0.0

57.425 88.168

Weir Flow

Qweir = $0.66 \text{ C B} (2 \text{ g})^{0.5} \text{ H}^{1}$ where: C = Weir Discharge Coefficient

B = Weir Width

g = Accel due to Gravity H = Head above weir crest

Draw down time (hours)

9.4

.3

4809.619

6007.509

0.0

0.000

0.0001

0.00

0.0

0.00

0.0001

0.0

0.0

50.0

50.0

0.000

Outlet of Subdrain

114.20



Kemptville, Ontario K0G 1J0 Engineers 210 Prescott Street, Unit 1 P.O. Box 189

Hydrogeological •
Inspection Testing •
Septic Systems Grading •
Structural • Environmental •

Civil • Geotechnical •

APPENDIX A: STORMWATER MANAGEMENT MODEL
OUTLET CONTROL DESIGN SHEET - EAST SWALE
Client: City Wyed Electric
Job No.: 210430
Location: 140 Reis Road

Date:

August 13, 2021

8 min/cm 75 mm/hr 2.1E-05 m/s Filter Information Percolation Time T = Percolation Rate = Permeability k = 15 min/cm 3.6 mm/hr 1.0E-06 m/s Infiltration Information Percolation Time T = Percolation Rate = Permeability k =

0.60 0.62 114.15 Weir Width (m): Weir Coefficient: Weir Invert (m):

		Draw	Down	Time	(hrs)	0.0	0.0	0.7	9.0	0.2	9.0	0.7	8.0	6.0	1.0	1.2	1.5	1.9	0.0
		Draw	Down	Time	(s)	68.794	105.346	2534.000	2047.552	783.009	2330.097	2573.727	2874.251	3254.237	3750.000	4423.963	5393.258	6906.475	0.000
			Total	Outflow	(L/sec)	56.1	20.3	2.0	9.0	9.0	9.0	0.5	4.0	4.0	0.3	0.3	0.2	0.2	0.1
			Total	Outflow	(m³/sec)	0.0561	0.0203	0.0007	9000.0	9000.0	0.0005	0.0005	0.0004	0.0004	0.0003	0.0003	0.0002	0.0002	0.0001
	Weir				(m³/sec)	0.0554	0.0196	0.000	0.0000	0.000	0.000	0.0000	0.000	0.000	0.0000	0.000	0.0000		
	M			Head	(m)	0.10	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	00.00
				Filter Flow	(m ₃ /sec)	9000'0	0.0005	0.0005	0.0004	0.0004	0.0003	0.0003	0.0003	0.0002	0.0002	0.0001	0.0001	0.0000	0.0000
	Filter Flow			Hydraulic	Gradient	1.3	1.2	1.1	1.0	6.0	8.0	2.0	9.0	9.0	4.0	6.0	0.2	0.1	0.0
				Head*	(m)	0.65	09:0	0.55	0.50	0.45	0.40	0.35	0.30	0.25	0.20	0.15	0.10	0.05	0.00
				Infiltration	Gradient Rate (m ³ /sec)	0.0002	0.0002	0.0002	0.0002	0.0002	0.0002	0.0002	0.0002	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001
	Infiltration			Hydraulic	Gradient F	1.9	1.8	1.8	1.7	1.7	1.6	1.6	1.5	1.5	1.4	1.4	1.3	1.3	1.3
				Head*	(m)	06.0	0.85	0.80	0.75	0.70	0.65	09.0	0.55	0.50	0.45	0.40	0.35	0.30	0.25
		Total	Storage	(m3)		19.0	15.1	13.0	11.3	10.0	9.6	8.4	7.2	0.9	4.8	3.6	2.4	1.2	0.0
0.5	Incremental	Volume in	Subdrain /	Clearstone	(m^3)	0.0	9.0	0.5	9.0	0.4	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	0.0
Depth of Layer =			Volume in	Swale	(m ₃)	3.9	1.5	1.2	6.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Depth		Bottom	Layer	Area	(m ²)	68.4	54.0	42.0	30.0	0.09	0.09	0.09	0.09	0.09	0.09	0.09	0.09	0.09	50.0
1		Тор	Layer	_	(m ²)	86.4	68.4	54.0	42.0	30.0	0.09	0.09	0.09	0.09	0.09	0.09	0.09	0.09	0.09
			Layer	Thickness	(m)	0.050	0.050	0.050	0.050	0.050	0.050	0.050	0.050	0.050	0.050	0.050	0.050	0.050	0.000
Depth of Layer =					Comments	OVERFLOW	OVERFLOW			bottom of pond	Sand Filter								Outlet of Subdrain
			Stage,	WSE	Elev (m)	114.25	114.20	114.15	114.10	114.05	114.00	113.95	113.90	113.85	113.80	113.75	113.70	113.65	113.60

Weir Flow Qweir = $0.66 \text{ C B } (2 \text{ g})^{0.5} \text{ H}^{1.5}$

10.3

Draw down time (hours)

where:

C = Weir Discharge Coefficient
B = Weir Width
g = Accel due to Gravity
H = Head above weir crest

APPENDIX A: STORMWATER MANAGEMENT MODEL Storm Sewer Design Sheet

City Wye'd Electric 210430

Client: Job No.:

140 Reis Road Location: August 13, 2021 Date:

Storm Sewer Design Sheet (5-yr storm)

Catchment	Catchbasin / Manhole								TIME	RAINFALL	PEAK
Area	FROM	10	Total Area	၁	ပ	Actual R	NDIN	ACCUM	OF	INTENSITY	FLOW
			(ha)	0.20	1.00	(,C,)	2.78 AR	2.78 AR	CONC.	-	Q (I/s)
CA1	West Side	Side	0.0708	0.0150	0.0558	0.83	0.16	0.16	10.00	104.19	17.03
CA2	East Side	Side	0.0829	0.0353	0.0476	99.0	0.15	0.15	10.00	104.19	15.83

_							
				South Filter	Salid File		
	Controlled Flow		(L/s)	0.4	9.0		
	Controlled /Uncontrolled			Controlled	Controlled		
		Q/Qfull		1.64	1.52		
	EXCESS	CAPACITY	(s/I)	-6.65	-5.45		
	TIME OF	FLOW	(min.)	2.52	2.52		
	FULL FLOW		(m/s)	0.33	0.33		
POSED SEWER		CAPACITY	(s/I)	10.38	10.38		
PROPC		LENGTH	(m)	0'09	0'09		
	PIPE	SLOPE	(%)	0.10	0.10		
	PIPE	SIZE	(mm)	200.00	200.00		
	TYPE	P	PIPE	PVC	PVC		

Rainfall Intensity = $998.071/(T+6.053)^{^{0.0814}}$ T= time in minutes (City of Ottawa, 5 year storm)



Appendix B: Product Information and Certificate of Well Compliance

- · Geotextile
- · Certificate of Well Compliance

Terrafix 270R - Geotextile

Function: Filtration & Drainage.

Terrafix 270R is a needle-punched nonwoven geotextile made of 100% virgin polypropylene staple fibers, which are formed into a random network for dimensional stability. Terrafix 270R resists ultraviolet deterioration, rotting, biological degradation, naturally encountered alkalis and acids. Polypropylene is stable within the pH range of 2-13.

Types of applications for 270R are: Subdrains, French Drains, Foundation Drains, Trench Drains, Blanket Drains.

270R provides good lateral drainage and is suitable for a wide spectrum of soil permeabilities.

Property	ASTM Test Method	Value Metric Units
Typical Geotextile Properties		
Weight (Typical)	D 5261	140 g / m² (4.0 oz/sqyd)
Grab Tensile Strength	D 4632	445 N
Grab Elongation	D 4632	50%
• Tear Resistance	D 4533	200 N
Puncture CBR	D 6241	1320 N
Permittivity	D 4491	2.00 sec ⁻¹
Water Flow	D 4491	6095 l/min/m ²
Apparent Opening Size	D 4751	0.300 mm
• U.V. Stability	D 4355	70% @ 500hrs

The information contained herein has been compiled by TAG Ltd. and is, to the best of our knowledge, true and accurate. This information is offered without warranty. Final determination of suitability for use contemplated is the sole responsibility of the user. This information is subject to change without notice. Terrafix is a registered trademark of Terrafix Geosynthetics Inc.

Terrafix 04-2018.

CERTIFICATE OF WELL COMPLIANCE

Shaping our future together

Ensemble, formons notre avenir

City of Ottawa

Client Service Centre

Ville d'Ottawa

Centre de service



I (Jeremy Hanna) AIR ROCK DRILLING CO. LTD. - DO HEREBY CERTIFY

that I am licensed to drill water wells in the Province of Ontario, and that I have supervised the drilling of the water well on the property of: Ottawa-Carleton / Geographical Township of I CERTIFY FURTHER that, I am aware of the well drilling requirements, the guidelines, recommendations and regulations of the Ministry of the Environment governing well installations in the Province of Ontario, and the standards specified in any subdivision agreement and hydrogeological report applicable to this site and City Standards. AND DO HEREBY CERTIFY THAT the said well has been drilled, cased, grouted (cement or bentonite) as applicable and constructed in strict conformity with the standards required. Day of MAY Jeremy Hanna (T3632) Air Rock Drilling Co. Ltd. (C-7681) The Engineer on behalf of the Landowner set out above. Certifies that he/she has inspected the well and it was constructed in accordance with the specifications in O.Reg 903, this report and the Hydrogeological Report with regards to grouting requirements. Signed this (Engineer)

easurem	nents record	led in:	Metric	Imperial								Page		of
Vell Ow	ner's Info	rmation	+											
rst Name)	220000000000000000000000000000000000000	Last Name/C					E-mail Address	2000	***********	100100000000000000000000000000000000000			Constructe
piling Ada	drace (Stract	t Number/Nar	W ma)	inch Hok	dings	Ltd Municipality		Province	Poets	al Code		Telephone		ell Owner
-	502	Numberman	ille)		~	Stittsville		ON		K2S		relephone	140. (IIIC.	area coue
/ell Loca			45702004			Othrashe	54575			NZO	IMU			370.00
ddress of	Well Location	n (Street Nu	mber/Name)			Township	200 at 11 .	2	Lot	LANCE AND TANKE	1000000000	Concessio	П	AND BUT KANNED
140	Reis R	oad				West Carle	eton			8		2	10-1-	10-1-
	strict/Municip					City/Town/Village					Ont:		Posta	I Code
TM. Coord	awa Ca dinates Zone	Easting	, N	orthing		Municipal Plan and	Sublot No	umber			Other			<u> </u>
NAD		8 423		501738		4M-745					Other Blo	xk.	\mathcal{Z}	
T. C. A. C. L. C. S. C.	Familian No. No. Condition of the	To the section of the	141-170-14-170-14-7	71 4 11, 127		cord (see instructions	on the ba	- Company of the Company					D	
Seneral Co	olour	Most Com	mon Material		(Other Materials		Gen	neral Desi	cnption			From	oth (m)
			Sand	& Gravel		+ Boul	ders						0	16
Grey	& Brown		Lime	stone									16	105
Grey	& Brown		Lime	stone									105	294
Grey (& Brown		Lime	stone									294	300
										,				
			-			**								
							-							
	-											-		-
														<u> </u>
Donth Se	etat(m@10)		Annular Type of Sea			Volume Place	d At	fter test of well yield	PERSONAL PROPERTY	A ALL MAN CONTRACTOR AND A	PPTI SHEAR COM?	d Testing aw Down	l R	ecovery
From	То		(Material ar			(m³/69)		Clear and sand		.	Time	Water Leve	Time	Water Lev
22 ′	12′	Neat c	ement			10.92	11	Other, specify_	Not		(min) Static	(m/#)	(min)	(m/ft)
12 ′	o´	Bentor	nite slurry	,		4.2		pumping discontinu	jea, give n	eason:	Level	10'1"		169
-								N		70	1.	17	1.1.	15
									-	- 32				
-						-	Pt	ump intake set at (r		332	2	22.3	2	15
								280		- 32	2			4
AND LABOUR TO THE PARTY OF THE	nod of Con	Light a Margalite and and a real artis			Well L	AND STREET OF STREET	Pu	280 umping rate (l/mire)		- 22	3	27.2	3	151
Cable Too	Many and the state of the same	struction Diamond			Well L	nercial Not use	Pi Pi	280 umping rate (l/mine) 6 uration of pumping	GPM)) .	7	3 4	27.2 32	3 4	151
Cable Too Rotary (C Rotary (R	ol Conventional)	Diamond Jetting Driving	Live	mestic estock	Comm Munici Test H	nercial Not use ipal Dewate Monitor	Pued During ing	umping rate (l/mire) 6 uration of pumping 1 hrs + 0	GPM) -		3	27.2	3 4	15
Cable Too Rotary (C Rotary (R Boring	conventional)	☐ Diamond	200	mestic estock gation	Comm Munici Test H	nercial Not use	Pued During ing	umping rate (l/mind) 6 uration of pumping 4 hrs + 0 nal water level end	GPM) -		3 4	27.2 32	3 4 5	15 ⁴
Cable Too Rotary (C Rotary (R	conventional) Reverse)	Diamond Jetting Driving	Live	mestic estock gation	Comm Munici Test H	nercial Not use ipal Dewate Monitor	ed During ing Fir	umping rate (l/mire) 6 uration of pumping 1 hrs + 0	min of pumpin		3 4 5	27.2 32 36.7	3 4 5 10	15 ⁴ 14 ³ 14 ³ 126
Cable Too Rotary (C Rotary (R Rotary (R Rotary (R Rotary (R Rotary (R) Air percus Other, spe	conventional) Reverse) ssion ecify Con	Diamond Jetting Driving Digging Struction R	Live	mestic [estock [gation [lustrial ner, specify	Comm Munici Test H Coolin	nercial Not use lipal Dewate lole Monitor g & Air Conditioning	Pued During Fir	280 umping rate (l/mirct) 6 uration of pumping 1 hrs + 0 nal water level end 169 ' '' lowing give rate (l/m	min of pumpin	ng (n ©)	3 4 5 10	27.2 32 36.7 57.9 76.3	3 4 5 10 15	15 14 14 12 10
Cable Too Rotary (C Rotary (R Borning Air percus Other, spe Inside Diameter	conventional) Reverse) ssion ecif) Con Open Hole (Galvanized	Diamond Jetting Driving Digging Struction R OR Material	Condition Cond	mestic [estock [gation [lustrial ner, specify	Comm Munici Test H Coolin	nercial Not use ipal Dewate lole Monitor g & Air Conditioning	Pu P	280 umping rate (Vmirct) 6 uration of pumping 1 hrs + 0 169' ("	min of pumpin nin/GPM)	ng (n a)	3 4 5 10 15 20	27.2 32 36.7 57.9 76.3 92.2	3 4 5 10 15 20	15 14 143 126 106 94
Cable Too Rotary (C Rotary (R Rotary (R Rotary (R Rotary (R Rotary (R Rotary (R) Air percus Other, spe	conventional) Reverse) ssion ecif) Con Open Hole (Galvanized	Diamond Jetting Driving Digging Struction R OR Material	Live	mestic [estock [gation [lustrial ner, specify	Comm Munici Test H Coolin	percial Not use plant Not use	Pu P	280 umping rate (l/minct) 6 uration of pumping 1 hrs + 0 nal water level end to 169' ("' lowing give rate (l/m ecommended pumping to 169 for the second pump	min of pumpin nin/GPM)	ng (n a)	3 4 5 10 15 20 25	27.2 32 36.7 57.9 76.3 92.2 106	3 4 5 10 15 20 25	15 14 14 14 12 10 10 94 81
Cable Too Rotary (C Rotary (R Borning Air percus Other, spe Inside Diameter	conventional) Reverse) ssion ecif) Con Open Hole (Galvanized	Diamond Jetting Driving Digging Struction R OR Material	ecord Cas Wall Thickness (cmm)	mestic estock gation ustrial her, specify pepth (in From +2 f	Comm Munici Test H Coolin	percial	Pued During Fir	280 umping rate (l/minct) 6 uration of pumping 4 hrs + 0 nal water level end 169' ("' lowing give rate (l/m ecommended pump	min of pumpin nin/GPM)	ng (n a)	3 4 5 10 15 20	27.2 32 36.7 57.9 76.3 92.2	3 4 5 10 15 20	15 14 14 14 12 10 10 94 81
Cable Too Rotary (C Rotary (R Borning Air percus Other, spe Inside Diameter	conventional) Reverse) ssion cecify Con Open Hole (Galvanized Concrete, F	Diamond Jetting Driving Digging Struction R OR Material J, Fibreglass, Plastic, Steel	Livi	mestic [estock [gation [lustrial ner, specify	Comm Munici Test H Coolin	status of Wel Status of Wel Replacement W Replacement W Recharge Well Observation and	Published Distring Fire If for It is a second of the It is a secon	280 umping rate (l/mirch 6 uration of pumping 4 hrs + 0 nal water level end 169 ' ! " lowing give rate (l/m ecommended pump	min of pumpin nin/GPM) o depth (m	ng (n a)	3 4 5 10 15 20 25	27.2 32 36.7 57.9 76.3 92.2 106	3 4 5 10 15 20 25	15 14 14 12 10 94 81 68
Cable Too Rotary (C Rotary (R Borning Air percus Other, spe Inside Diameter	conventional) Reverse) ssion ecify Con Open Hote (Galvanize Concrete, F	Diamond Jetting Driving Digging Struction R OR Material J, Fibreglass, Plastic, Steel	Livi	mestic estock gation ustrial her, specify pepth (in From +2 f	Comm Munici Test H Coolin To	status of Wel Status of Wel Replacement W Rescharge Well Dewatering Well	Pued Diagramming Firm III Re (l/r) Re (l/r) W/d/or W/d/or W/d/or	280 umping rate (l/mind) 6 uration of pumping 1 hrs + 0 nal water level end to 169 (l'') lowing give rate (l/mind) ecommended pumping (lower pumping p	min of pumpin nin/GPM) o depth (m	ng (n a)	3 4 5 10 15 20 25 30	27.2 32 36.7 57.9 76.3 92.2 106	3 4 5 10 15 20 25 30	15 14 14: 12: 10: 94 81 68
Cable Too Rotary (C Rotary (R Borning Air percus Other, spe Inside Diameter	conventional) Reverse) ssion ecify Con Open Hote (Galvanize Concrete, F	Diamond Jetting Driving Digging Struction R OR Material J, Fibreglass, Plastic, Steel	Livi	mestic estock gation ustrial her, specify pepth (in From +2 f	Comm Munici Test H Coolin To	status of Wel St	Pued Diagramming Firm III Re (l/r) Re (l/r) W/d/or W/d/or W/d/or	280 umping rate (l/mind) 6 uration of pumping 1 hrs + 0 nal water level end to 189 ' ("' lowing give rate (l/m ecommended pumping to 189 bell production (l/mind) 5 sinfected?	min of pumpin nin/GPM) o depth (m	ng (n a)	3 4 5 10 15 20 25 30 40	27.2 32 36.7 57.9 76.3 92.2 106 118 140	3 4 5 10 15 20 25 30 40	15 14 14 12 10 94 81 68 47.
Cable Too Rotary (C Rotary (R Borning Air percus Other, spe Inside Diameter	conventional) Reverse) ssion ecify Con Open Hole (Galvanizec Concrete, F Steel Open 1	Diamond Jetting Driving Driving Digging Struction R OR Material Fibreglass, Plastic, Steel)	ecord Cas Wall Thickness (cmm) 188	mestic cestock gation custrial ner, specify pepth (if From +2 \frac{1}{2} \fra	Comm Munici Test H Coolin To	status of Wei	Planting Fir III Refell Refull Williams	280 umping rate (l/mind) 6 uration of pumping 1 hrs + 0 nal water level end to 169 (l'') lowing give rate (l/mind) ecommended pumping (lower pumping p	min of pumpin nin/GPM) p depth (m 28 p rate		3 4 5 10 15 20 25 30 40 50 60	27.2 32 36.7 57.9 76.3 92.2 106 118 140 156 169	3 4 5 10 15 20 25 30 40 50	15 14 14 12 10 94 81 68 47
Cable Toc Rotary (C Rotary (R Rotary	conventional) Reverse) ssion ecify Con Open Hole (Galvanizec Concrete, Steel Open 1	Diamond Jetting Dirving Digging Struction R OR Material J. Fibreglass, lastic, Steel)	ecord Cas Wall Thickness (cmm) .188	mestic Eestock Egation Eustrial ner, specify Depth (From +2' 22' /	Comm Munici Test H Coolin To To To 22	status of Wei St	Pund Distring Fir	280 umping rate (l/mind) 6 uration of pumping 1 hrs + 0 nal water level end to 189 ' ("' lowing give rate (l/m ecommended pumping to 189 bell production (l/mind) 5 sinfected?	min of pumpin nin/GPM) o depth (m	og (n@)	3 4 5 10 15 20 25 30 40 50 60 Hace	27.2 32 38.7 57.9 76.3 92.2 106 118 140 156 169	3 4 5 10 15 20 25 30 40 50	15 14 14 12 10 94 81 68 47.
Cable Toc Rotary (C Rotary (R Porting Ail percus Other, spe Inside Jameter (cm/gr)	conventional) Reverse) ssion Con Open Hole (Galvanized Concrete, F Steel Open I	Diamond Jetting Driving Driving Digging Struction R OR Material Fibreglass, Plastic, Steel)	ecord Cas Wall Thickness (cmm) 188	mestic cestock gation custrial ner, specify pepth (if From +2 \frac{1}{2} \fra	Comm Munici Test H Coolin To To To 22	status of Wei Alter Supply Replacement Wei Dewatering Wei Observation and Monitoring Hole Alteration (Construction) Abandoned, Insufficient Supp Abandoned, Pod Water Quality Abandoned, Ondoned, other	Pund Distring Fir	280 umping rate (l/mind) 6 uration of pumping 1 hrs + 0 nal water level end to 189 ' ("' lowing give rate (l/mind) ecommended pumping to 189 bell production (l/mind) 5 sinfected?	min of pumpin nin/GPM) o depth (m	og (n@)	3 4 5 10 15 20 25 30 40 50 60 Hace	27.2 32 38.7 57.9 76.3 92.2 106 118 140 156 169	3 4 5 10 15 20 25 30 40 50 160	15 14 14 12 10 94 81 68 47.
Cable Toc Rotary (C Rotary (R Rotary	conventional) Reverse) ssion Con Open Hole (Galvanized Concrete, F Steel Open I	Diamond Jetting Diving Digging Struction R OR Material Fibreglass, elastic, Steel)	ecord Cas Wall Thickness (cmm) .188	mestic cestock cyation custrial ner, specify sing Depth (in From +2 / 22 / een Depth (in Settlement (in Se	Comm Munici Test H Coolin To To 22 M/ft)	status of Wei St	Pund Distring Fir	280 umping rate (l/mind) 6 uration of pumping 1 hrs + 0 nal water level end to 189 ' ("' lowing give rate (l/mind) ecommended pumping to 189 bell production (l/mind) 5 sinfected?	min of pumpin nin/GPM) p depth (m 28 p rate Map	of Wei	3 4 5 10 15 20 25 30 40 50 60 Hace	27.2 32 36.7 57.9 76.3 92.2 106 118 140 156 169	3 4 5 10 15 20 25 30 40 50 160	15 14 14 12 10 94 81 68 47.
Cable Toc Rotary (C Rotary (R Rotary	conventional) Reverse) ssion Con Open Hole (Galvanized Concrete, F Steel Open I	Diamond Jetting Diving Digging Struction R OR Material Fibreglass, elastic, Steel)	ecord Cas Wall Thickness (cmm) .188	mestic cestock cyation custrial ner, specify sing Depth (in From +2 / 22 / een Depth (in Settlement (in Se	Comm Munici Test H Coolin To To 22 M/ft)	status of Wei Alter Supply Replacement Wei Dewatering Wei Observation and Monitoring Hole Alteration (Construction) Abandoned, Insufficient Supp Abandoned, Pod Water Quality Abandoned, Ondoned, other	Pund Distring Fir	280 umping rate (l/mind) 6 uration of pumping 1 hrs + 0 nal water level end to 189 ' ("' lowing give rate (l/mind) ecommended pumping to 189 bell production (l/mind) 5 sinfected?	min of pumpin nin/GPM) p depth (m 28 p rate Map	of Wei	3 4 5 10 15 20 25 30 40 50 60 Hace	27.2 32 36.7 57.9 76.3 92.2 106 118 140 156 169	3 4 5 10 15 20 25 30 40 50 160	15 14 14 12 10 94 81 68 47.
Cable Toc Rotary (C Rotary (R Ponno Aut perous Other, spe Inside Jameter (cmtgo) Outside Jameter	conventional) Reverse) ssion Con Open Hole (Galvanized Concrete, F Steel Open I	Diamond Jetting Diamond Diamond Jetting Driving Digging Struction R OR Material Fibreglass, Plastic, Steel) Iole struction R derial anized, Steel)	ecord Scr	mestic cestock cyation custrial ner, specify sing Depth (in From +2 / 22 / een Depth (in Settlement (in Se	Common Munician Munician Test H Coolin To 22 (1380)	Status of Wel Status of Wel Status of Wel Status of Wel Replacement W Replacement W Dewatering Well Dewatering Well Dewatering Hole Alteration (Construction) Abandoned, Insufficient Suppl Abandoned, Pow Water Quality Abandoned, oth specify Other, specify	Pund Distring Fir	280 umping rate (l/mind) 6 uration of pumping 1 hrs + 0 nal water level end to 189 ' ("' lowing give rate (l/mind) ecommended pumping to 189 bell production (l/mind) 5 sinfected?	min of pumpin nin/GPM) p depth (m 28 p rate Map	of Wei	3 4 5 10 15 20 25 30 40 50 60 Hace	27.2 32 36.7 57.9 76.3 92.2 106 118 140 156 169	3 4 5 10 15 20 25 30 40 50 160	15 14 14 12 10 94 81 68 47
Cable Toc Rotary (C Rotary (R Rotary	conventional) Reverse) ssion ccifi Con Open Hole (Galvanized Concrete, F Steel Open I Con (Plastic, Galv	Diamond Jetting Diamond Jetting Driving Digging Struction R OR Material Fibreglass, Plastic, Steel) Iole Struction R derial anized, Steel)	ecord - Scr	mestic cestock capation custrial ner, specify sing Depth (r From +2 / 22 / 22 / 22 / 22 / 22 / 22 / 22	Common Munician Munic	Status.of Wel Status.of Wel Status.of Wel Status.of Wel Agter Supply Replacement W Test Hole Dewatering Well Observation and Monitoring Hole Alteration (Construction) Abandoned, Insufficient Suppl Abandoned, oth specify Other, specify Hole Diameter	Pund Distring Fir	280 umping rate (l/mind) 6 uration of pumping 1 hrs + 0 nal water level end to 189 ' ("' lowing give rate (l/mind) ecommended pumping to 189 bell production (l/mind) 5 sinfected?	min of pumpin nin/GPM) p depth (m 28 p rate Map	of Wei	3 4 5 10 15 20 25 30 40 50 60 Hace	27.2 32 36.7 57.9 76.3 92.2 106 118 140 156 169	3 4 4 5 10 15 20 25 30 40 50 1660	15 14 14 12 10 94 81 68 47 27 10
Cable Toc Rotary (C Rotary (R Rotary (R Rotary (R Rotary (R R R R R R R R R R R R R R R R R R R	conventional) Reverse) ssion ccifi Con Open Hole (Galvanized Concrete, F Steel Open 1 Con (Plastic, Galv	Diamond Jetting Diamond Diamond Jetting Driving Digging Struction R OR Material Fibreglass, Plastic, Steel) Iole struction R derial anized, Steel)	ecord - Scr Slot No.	mestic cestock capation custrial ner, specify sing Depth (r From +2 / 22 / 22 / 22 / 22 / 22 / 22 / 22	Common Munician Munic	Status of Wel Status of Wel Status of Wel Status of Wel Replacement W Replacement W Dewatering Well Dewatering Well Dewatering Hole Alteration (Construction) Abandoned, Insufficient Suppl Abandoned, Pow Water Quality Abandoned, oth specify Other, specify	Plant de la	280 umping rate (l/mind) 6 uration of pumping 1 hrs + 0 nal water level end to 189 ' ("' lowing give rate (l/mind) ecommended pumping to 189 bell production (l/mind) 5 sinfected?	min of pumpin nin/GPM) p depth (m 28 p rate Map	og (n@)	3 4 5 10 15 20 25 30 40 50 60 Hace	27.2 32 36.7 57.9 76.3 92.2 106 118 140 156 169	3 4 4 5 10 15 20 25 30 40 50 1660	15 14 14 12 10 94 81 68 47 27 10
Cable Toc Rotary (R Rotary	Conventional) Reverse) ssion ecify Con Open Hole (Galvanized Concrete, F Steel Open I Galvanized Concrete, Galvan	Diamond Jetting Diamond Dirving Digging Struction R OR Material A, Fibreglass, lastic, Steel) Iole Struction R derial Annized, Steel) Water Det Gind of Water Other, spe Gind of Water	ecord - Scr Slot No.	mestic Eestock Egation Eustrial her, specify Eing Depth (From +2' 22'') een Depth (From Erom + 2' 22'')	Common Municial Test H Coolin To Coo	Status of Wel Status of Wel Status of Wel Status of Wel Replacement W Test Hole Dewatering Wel Dewatering Hole Abandoned, Insufficient Supp Abandoned, oth specify Other, specify Hole Diameter pth (md) To Cim	Plant de la	280 umping rate (l/mind) 6 uration of pumping 1 hrs + 0 nal water level end to 189 ' ("' lowing give rate (l/mind) ecommended pumping to 189 bell production (l/mind) 5 sinfected?	min of pumpin nin/GPM) p depth (m 28 p rate Map	of Wei	3 4 5 10 15 20 25 30 40 50 60 Hace	27.2 32 36.7 57.9 76.3 92.2 106 118 140 156 169	3 4 4 5 10 15 20 25 30 40 50 1660	15 14 14 12 10 94 81 68 47 27 10
Cable Toc Rotary (R Rotary	conventional) Reverse) ssion ecify Con Open Hole (Galvanizec Concrete, Steel Open i Con (Plastic, Galv d at Depth G G G G G G G G G G G G G G G G G G G	Diamond Jetting Dirving Digging Digging Struction R OR Material Jetting Digging Struction R OR Material Jetting Digging Struction R OR Material Jetting Digging Diggin	ecord - Scr Slot No.	mestic cestock [gation [with a color [with a color [with a color with a c	Common Municial Test H Coolin To Coo	Status of Wel Status	Plant de la	280 umping rate (l/mind) 6 uration of pumping 1 hrs + 0 nal water level end to 189 ' ("' lowing give rate (l/mind) ecommended pumping to 189 bell production (l/mind) 5 sinfected?	min of pumpin nin/GPM) p depth (m 28 p rate Map	of Wei	3 4 5 10 15 20 25 30 40 50 60 Hace	27.2 32 36.7 57.9 76.3 92.2 106 118 140 156 169	3 4 4 5 10 15 20 25 30 40 50 1660	15 14 14 12 10 94 81 68 47 27 10
Cable Toc Rotary (R R R R R R R R R R R R R R R R R R R	Conventional) Reverse) ssion ecify Con Open Hole (Galvanizec Concrete, Steel Open I Con (Plastic, Galv d at Depth G Gas d at Depth G Gas d at Depth K G G G G G G G G G G G G G G G G G G G	Diamond Jetting Dirving Digging Digging Struction R OR Material Jetting Digging Struction R OR Material Jetting Digging Struction R OR Material Jeting OR Material Jeting Struction R OR Material Jeting Struction R OR Material Jeting Other Jeting Other, spe Gind of Water Other, spe Gind of Water	ecord - Scr Slot No.	mestic cestock [gation [with a color [with a color [with a color with a c	Common Municial Test H Coolin To Coo	Status of Wel Status	Planting Fit Plant	280 umping rate (l/mind) 6 uration of pumping 1 hrs + 0 nal water level end to 189 ' ("' lowing give rate (l/mind) ecommended pumping to 189 bell production (l/mind) 5 sinfected?	min of pumpin nin/GPM) p depth (m 28 p rate Map	of Wei	3 4 5 10 15 20 25 30 40 50 60 Hace	27.2 32 36.7 57.9 76.3 92.2 106 118 140 156 169	3 4 4 5 10 15 20 25 30 40 50 1660	15' 14' 14' 120' 100' 94. 81 68. 47. 27.
Cable Toc Rotary (R R R R R R R R R R R R R R R R R R R	Conventional) Reverse) ssion ecify Con Open Hole (Galvanizec Concrete, Steel Open i Galvanizec Concrete, Galvaniz	Diamond Jetting Dirving Digging Digging Struction R OR Material Jetting Digging Struction R OR Material Jetting Digging Struction R OR Material Jetting Struction R OR Material Jeting Struction R OR Material Jeting Struction R Other Struction R Other, Specified of Water Other, specified of Water Other, specified of Water Other, specified of Water	ecord - Scr Slot No.	mestic cestock castock	Common Municial Test H Coolin Test H Coolin Test H Coolin To To To 22 (1997) To 22 (1997) To 22 (1997) To De From	Status of Wei Status	Planting Fit Plant	280 umping rate (l/mind) 6 uration of pumping 1 hrs + 0 nal water level end to 189 ' ("' lowing give rate (l/mind) ecommended pumping to 189 bell production (l/mind) 5 sinfected?	min of pumpin nin/GPM) p depth (m 28 p rate Map	of Wei	3 4 5 10 15 20 25 30 40 50 60 Hace	27.2 32 36.7 57.9 76.3 92.2 106 118 140 156 169	3 4 4 5 10 15 20 25 30 40 50 1660	15' 14' 14' 120' 100' 94. 81 68. 47. 27.
Cable Toc Rotary (R R R R R R R R R R R R R R R R R R R	Conventional) Reverse) ssion ecify Con Open Hole (Galvanizec Concrete, Steel Open i Galvanizec Concrete, Galvaniz	Diamond Jetting Dirving Digging Digging Struction R OR Material Jetting Digging Struction R OR Material Jetting Digging Digging Struction R OR Material Jetting Other Other, spe Gind of Water Other, spe Gind of Water Other, spe Gind of Water Other, spe	ecord - Scr Slot No.	mestic cestock [gation [with a color [with a color [with a color with a c	Common Municial Test H Coolin Test H Coolin Test H Coolin To To To 22 (1) To	Status of Wei Status	Plant de la	280 umping rate (l/mind) 6 uration of pumping 1 hrs + 0 nal water level end to 189 ' ("' lowing give rate (l/mind) ecommended pumping to 189 bell production (l/mind) 5 sinfected?	min of pumpin nin/GPM) p depth (m 28 p rate Map	of Wei	3 4 5 10 15 20 25 30 40 50 60 Hace	27.2 32 36.7 57.9 76.3 92.2 106 118 140 156 169	3 4 4 5 10 15 20 25 30 40 50 1660	15' 14' 14' 120' 100' 94. 81 68. 47. 27.
Cable Toc Rotary (C Rotary (R Rotary	Conventional) Reverse) ssion ecify Con Open Hole (Galvanized Concrete, F Steel Open I Gat Depth I d at Depth I	Diamond Jetting Diamond Jetting Diving Digging Digging Struction R OR Material Fibreglass, Plastic, Steel Jetting Other, Spee Gind of Water Contractor Co	ecord - Scr Slot No. ails : Fresh cify : Are the conditions and Well	mestic cestock castock	Common Municial Test H Coolin To Coo	Status of Wel Status	Plant de la	280 umping rate (l/mind) 6 uration of pumping 1 hrs + 0 nal water level end to 189 ' ("' lowing give rate (l/mind) ecommended pumping to 189 bell production (l/mind) 5 sinfected?	min of pumpin nin/GPM) p depth (m 28 p rate Map	of Wei	3 4 5 10 15 20 25 30 40 50 60 Hace	27.2 32 36.7 57.9 76.3 92.2 106 118 140 156 169	3 4 4 5 10 15 20 25 30 40 50 1660	15' 14' 14' 120' 100' 94. 81 68. 47. 27.
Cable Toc Rotary (C Rotary (R Rotary	Conventional) Reverse) ssion ecify Con Open Hole (Galvanized Concrete, F Steel Open I Gat Depth I d at Depth I	Diamond Jetting Diamond Jetting Diving Digging Digging Struction R OR Material Fibreglass, Plastic, Steel Jetting Other, Spee Gind of Water Contractor Co	ecord - Scr Slot No. ails : Fresh cify : Are the conditions and Well	mestic cestock castock	Common Municial Test H Coolin To Coo	Status of Wel Status	Plant Refer Plant	280 umping rate (l/mind) 6 uration of pumping 1 hrs + 0 nal water level end 169 ' '' lowing give rate (l/mind) ecommended pumping ecommended pum	min of pumpin nin/GPM) p depth (m 2 8 p rate	of West following	3 4 5 10 15 20 25 30 40 50 60 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	27.2 32 36.7 57.9 76.3 92.2 106 118 140 156 189	3 4 4 5 10 15 20 25 30 40 50 1660	15' 14' 14' 120' 100' 94. 81 68. 47. 27.
Cable Toc Rotary (R Rotary	Conventional) Reverse) ssion cerify Con Open Hole (Galvanized Concrete, F Steel Open i d at Depth fill Gas d at Depth fill Gas drawne of Well Orck Drilling Gress (Stree	Diamond Jetting Diamond Jetting Diving Digging Struction R OR Material Fibreglass, Plastic, Steel) Water Det Gind of Water Other, spe Gind of Water Other, spe Gind of Water Other, spe Gind of Water Contractor	ecord Cas Wall Thickness (cmm) 188 ecord Scr Slot No. ails Fresh city Fresh city Fresh city Fresh city Fresh city Thickness Thicknes	mestic estock gation [ustrial ner, specify	Common Munician Munic	Status of Wel Monitor g & Air Conditioning Status of Wel Monitoring Hole Diameter pth (monitoring Monitoring Mo	Plant Refer Plant	280 umping rate (l/mind) 6 uration of pumping 1 hrs + 0 nal water level end 169 ' '' nowing give rate (l/mind) ecommended pumping ecommended pumpi	min of pumpin nin/GPM) p depth (m 2 8 p rate	of West following	3 4 5 10 15 20 25 30 40 50 60 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	27.2 32 36.7 57.9 76.3 92.2 106 118 140 156 189	3 4 4 5 10 15 20 25 30 40 50 1660	15° 143° 143° 126° 106° 94. 81 68. 47. 27.
Cable Toc Rotary (C Rotary (R Rotary	conventional) Reverse) ssion cerify Steel Open Hole (Galvanize- Concrete, F Steel Open I Galvanize- Galvanize- Galvanize- Galvanize- Galvanize- Concrete, F Steel Open I Gas I d at Depth I (Plastic, Galv We arme of Well C ock Drilling dress (Stree- ranktowr	Diamond Jetting Diamond Jetting Diving Digging Digging Struction R OR Material Fibreglass, Plastic, Steel Jetting Other, Spee Gind of Water Contractor Co	ecord Cas Wall Thickness (cmm) 188 ecord Scr Slot No. ails Fresh city Fresh city Fresh city Fresh city Fresh city Thickness Thicknes	mestic cestock [gation [mestic cestock [gation [mestic cestock [mestic cesto	Common Municial Test H Coolin To To To 3000 To	Status of Wel Status	Planting Did in the state of th	280 umping rate (l/mind) 6 uration of pumping 1 hrs + 0 nal water level end to 169 ' (") lowing give rate (l/mind) ecommended pumping ecommended pumping ell production (l/mind) 5 5 sinfected? Oes No ease provide a mail of the pumping ell production (l/mind) 5 and the pumping ell production (l/mind) 5 and ell production (l/mind) 6 and	min of pumpin nin/GPM) p depth (m 2 8 p rate	g (na)	3 4 5 10 15 20 25 30 40 50 60 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	27.2 32 36.7 57.9 78.3 92.2 106 118 140 156 189	3 4 5 5 10 15 20 25 30 40 50 1660	15° 143° 143° 126° 108° 94. 81° 68. 47. 27. 10°
Cable Too Rotary (C Rotary (R Rotary	conventional) Reverse) ssion ecify Steel Open Hole (Galvanize- Concrete, F Steel Open I Galvanize-	Diamond Jetting Diamond Jetting Dirving Digging Struction R OR Material Jetting Struction R OR Material Jetting OR Material Jetting OR Material Jetting OR Material Jeting OR Mater OR Material Jeting OR Mater OR Mater OR Mater Jeting OR Material Jeting OR Materi	ecord - Cas Wall Thickness (cmf) 188 ecord - Scr Slot No. sails Fresh cify Fresh cify and Well Business	mestic cestock [gation [mestic cestock [gation [mestic cestock [mestic cesto	Common Municial Test H Coolin To Coo	Status of Well Mater Supply Status of Well Mater Supply Replacement Well Dewatering Well Dewater Quality Abandoned, Powater Quality Dewater Quality Diameter Dewater Quality Diameter Dewater Quality Diameter Dewater Dewat	Plant did not	280 umping rate (l/mind) 6 uration of pumping 1 hrs + 0 nal water level end 169 ' '' lowing give rate (l/mind) ecommended pumping ecommended pumpi	min of pumpin nin/GPM) p depth (m 28 p rate Map ap below	SET A	3 4 5 10 15 20 25 30 40 50 60 1 1 1 2 6 6 6 0	27.2 32 36.7 57.9 78.3 92.2 106 118 140 156 189	3 4 4 5 10 15 20 25 30 40 50 1660	15 14 14 12 10 94 81 68 47. 27. 10
Cable Toc Rotary (C Rotary (R Rotary	Conventional) Reverse) ssion ecify Con Open Hole (Galvanized Concrete, F Steel Open I Gat Depth I Gat Depth I Gas I	Diamond Jetting Diamond Jetting Diving Digging Digging Struction R OR Material Fibreglass, Plastic, Steel) Water Det Gind of Water Other, spe Gind of Water Road Stal Code KDA 2ZO Prea code) Na	ecord Cas Wall Thickness (cmm) 188 ecord Scr Slot No. ails Fresh cify cify cify cify cify cify me) Business me of Well Te	mestic cestock gation [ustrial ner, specify	Common Munician Munician Test H Coolin Test H Coolin To 22 (Status of Well Mater Supply Status of Well Mater Supply Replacement Well Dewatering Well Dewater Quality Abandoned, Powater Quality Dewater Quality Diameter Dewater Quality Diameter Dewater Quality Diameter Dewater Dewat	Plant did not	280 umping rate (l/mind) 6 uration of pumping 1 hrs + 0 nal water level end 169 ' '' lowing give rate (l/mind) ecommended pumping ecommended pumping 5 ell production (l/mind) 5 ell production (l/mind) 5 ease provide a ma	min of pumpin nin/GPM) p depth (m 2 8 p rate	SET A	3 4 5 10 15 20 25 30 40 50 60 1 1 1 2 6 6 6 0	27.2 32 36.7 57.9 76.3 92.2 106 118 140 156 169 attion	3 4 5 5 10 15 20 25 30 40 50 1660	15 14 14 12 10 94 81 68 47 27 10



Appendix C: Sewage System Design

EMAIL ONLY

**COMMERCIAL

Phone Folder Name: PickUp Canada Post to: Weekly Courier SEPTIC FILE #

20-141

OTTAWA

Ottawa Septic Bureau des systèm System Office septiques d'Ottaw 3889 Rideau Valley Drive Box 599 Manotick, ON K4M 1A5

Phone: 613-692-3571 PRESS "4" for septic office 1-800-267-3504 Fax: 613-692-1507 Email: septic@rvca.ca 140 Reis Road

Township:OSG/HUN-GLO-FIT-CUM-NEP-GOU-RID-KAN-TOR

Scott Winch Contact for pickup:

Address of property:

Phone#/Email:

INFORMATION FOR OWNER/APPLICANT

Attached is your Sewage System Permit. A minimum of two inspections are required before your proposed sewage system can be approved for use (additional inspections may be required for clay soils/bedrock and/or reinspections). Inspections must be requested in writing. Please see attached:

- Inspection fax request form (all inspections MUST be requested in writing)
- As-built components and drawing form
- Copy of the approved application and schedule pages
- Approved Part 8 permit 2x copies: Copy 1: APPLICANT + Copy 2:Plans Examiner ** Agent Deliver Direct To City

Special Note

- A permit is valid for 12 months from the original date of issuance noted in "permit date". If lapsed, it may be renewed only once for a period of 12 months from the date of expiry.
- No person shall make a material change or cause a material change to be made to a plan, specification, document or other information on the basis of which a permit was issued without notifying, filing details with and obtaining the authorization of the Chief Building Official. (Building Code Act 1992, c.23, s.8(12))

Sewage System Permit Construction Requirements

1. Clay Soils/Bedrock only (if required per issued Approval)

In clay soils/bedrock, a site preparation inspection is required. The total contact area must be properly prepared. Scarification must be done under dry conditions prior to importing leaching bed fill.

2. Installation Inspection - 2nd inspection

When the sewage system is substantially completed (i.e., before the final fill is placed over the septic tank and leaching bed system) an installation inspection is required. Prior to any inspection request, the following must be submitted:

- a) "as-built components" and "as-built drawings" see attached form
- b) "engineer letter" if the system is engineered
- c) grain size analysis and weight bills for all Filter Media types of septic systems
- d) Weigh bills for washed septic stone, where applicable
- e) Maintenance/service contract for treatment unit installed

3. Final Grading Inspection - 3rd inspection

When construction of the sewage system is complete, a final grading inspection is required. Before a Certificate of Completion can be issued, the following must be complete:

- a) The leaching bed and septic tank must be covered with sand fill and topsoil and graded
- b) All conditions of the Sewage System Permit & comments on the installation inspection report must be met
- c) The depth of cover & material type must be identified by inspection pipes or holes placed over trenches at 4 corners of bed
- d) The 4 corners of the bed must be staked

Main Phone: 613-692-3571 x 1129



Inspection Request Form

Complete and fax to: 613-692-1507 or e-mail: septic@rvca.ca

Section A. Property a	nd General Information	n				
Date Submitted			Septic File Nu	mber:		
Civic Address						
Former Township	☐ Osgoode ☐ Cumb		oulbourn 🗆 Torbo			
Property Owner	I riditacy II rides	d LI G	oucester 🗆 Fitzro	y LI Ka	anata 🗆 Ottawa	
		The Contract of the Contract o				
Section B. Requestor	Information					
Name of Requestor			Phone Number	r:		
E-mail			Fax Number:			
I am the (check one)	☐ Installer ☐ Engine	eer 🗆 Prope	rty Owner			
Section C. I am Reque	sting the following:					
☐ 1 st – Subgrade (If required - check one):	☐ 2 nd – Installation (Check all that appl		□ 3 rd – Final Grade Inspection		de Inspection	
☐ Scarification	Refer to attached:				st he applied	
☐ Clay Seal	☐ As-Built Compor	☐ As-Built Components Page		unless winter conditions exist		
☐ Subgrade	☐ As-Built Drawing		at Direct	at Director's discretion		
	☐ Engineers Letter		V20121000000000000000000000000000000000			
	☐ Filter Media Bills			All deficiencies must be addressed from installation		
	☐ Grain Size Analysis					
	☐ Maintenance Agreement		report	report		
	☐ ESA Permit Number:					
Notes/Comments						
Section D. Re-inspection	on	PASSING				
☐ Re-inspection - 1 st	☐ Re-inspection Re	quest – 2 nd (all			
	Note: Re-inspection fee applies on requests for same deficiency – Please provide payment information below					
	Card Type:	☐ Mastero] Visa		
	Card Number:			Expiry:		
	Cardholder Name:					
Notes/Comments Please Note:						

- 3-5 business day turn around for inspections
- OSSO file will be given to inspector upon receipt of this request form
- PRIORITY will be given to requests that have septic file/permit numbers

Reset	Print
	Reset

SEPTIC	PERMIT	NO.	

AS-BUILT COMPONENTS

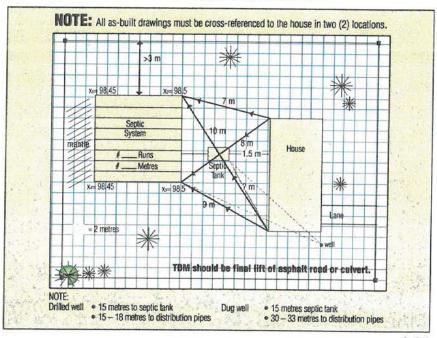
(required prior to installation inspection)

Elevations of installed system must be supplied with this report (in reference to the TBM). Exact size and location of all structures, well(s) and system(s) and its components must be shown (including neighbouring lots).

Septic/Holding Tank: ___ Name of owner: Manufacturer: _ Installer: □ concrete □ polyethylene □ other Installer Signature: _ Filter: □ no □ yes ____ License Number: _ Treatment: Make ___ Date of Installation: _ Unit: Model __ Civic Address or Legal Description of Property: Diameter of pipes Make of pipes: _ Ends: ☐ capped ☐ interconnected Township _ Number of runs: _____ Pump Systems: Length of runs: _ Volume discharge rates: ___ Alarm location: __ Filter media: Amount Purchased: _ Dimension of Pump Chamber: ___ Date Purchased: ___ Height of Float Switch: _ Supplier: _ Grease Interceptor: Grain/size analysis by: _ □ no □ yes Size: _ Analysis dated: _ Location: .

*Grain Size Analysis and weight bills must be supplied with this report.

All rights reserved. No part of this work may be reproduced or used in any form without the prior written permission of the copyright holder.



AS-BUILT DRAWING

6			SEPTIC PER	MIT NO.
0				
++++				
+				
		++++++	+++	
		+ - - - - - - - - -		
4 4 4				
				1-1-1-1-1-1
	111111	++++++		
+				
1-1-1-1				
1-1-1-1-				
ss-refeneced Meas	urments (metric only)	Ele	evations (metric only)	BM -
	A2 m	X ₁		
m		A1	X ₂	
		X.	X ₂	
m	B ₂ m	X ₃ X ₅ X ₇	X.	(toe)

Page 3 of 3



SEPTIC FILE# Civil · Geotechnical · Structural · Environmental · Hydrogeology ·

(613) 860-0923

Fax (613) 258-0475 www.kollaard.ca info@kollaard.ca

210 Prescott Street Unit 1 PO Box 189 Kemptville, Ontario **KOG 1J0**

Date: April 9, 2020

File # 200247

Attention:

Mr. Terry Davidson, P.Eng Rideau Valley Conservation 3889 Rideau Valley Drive Manotick, ON K4M 1A5

Proposed Sewage System 140 Reis Road Lot 8, Conc. 2 West Carleton (Huntley) City of Ottawa

Owner: Winch Holdings Ltd

Dear: Mr. Davidson

Please find attached the onsite septic system application package for the above noted client and property.

COMMERCIAL

Included in the package are the:

Ontario Building Code Forms Relevant Schedules Relevant Drawings

Yours Sincerely,

Kaleb Lakew, P.Eng.



Professional Engineers Ontario

Authorized by the Association of Professional Engineers Ontario to offer Professional Engineering Services

RVCA RECEIVED

SEPTIC FILE #

Ottawa Septic
System Office

Office

Ottawa

Ottawa

Office

System Office

Ottawa

Ottawa

Ottawa

For use by Principal Authority

Permit Number (if different): Application Number: Date received: Roll number: OTTAWA SEPTIC SYSTEM OFFICE Application submitted to: (Name of municipality, upper-tier municipality, board of health or conservation authority) A. Project information Building number, street name: Lot/con. Unit number: 140 Reis Road 8/2 Municipality Postal code: Plan number/other description West Carleton (Huntley) Project value est. \$ Area of work (m2) B. Purpose of application ⊠ New Addition to an existing building ☐ Alteration / ☐ Demolition Conditional construction repair Permit Proposed use of Building Current use of Building Light Industrial Building Description of proposed work On-Site Septic System C. Applicant Authorized agent of Owner Applicant is: Last name First name Corporation or partnership Kollaard Associates Inc. Street address Unit number: Lot/con. Box 189, 210 Prescott St. Municipality Postal code: Province E-mail Kemptville **K0G 1J0** ON info@kollaard.ca Telephone number Fax Cell number (613) 860-0923 (613) 258-0475 D. Owner (if different from applicant) Last name First name Corporation or partnership Winch Holdings Ltd Street address Unit number: Lot/con. PO Box 502 Municipality Postal code: Province E-mail Stittsville K2S 1A6 ON Telephone number Fax Cell number 613-831-4462

				EPTIC	FILE	华	
E. 1	Builder (optional)	DECENED	5	EL.	161		
ast	name PN	A RECEIVED MAR Tringfilme	Corporation or partne	rship (frappl	icable)	À	
tre	et address	MAN	3-1	Unit numb	per:	Lot/con.	
lun	icipality	REFER TO Postal code:	Province	E-mail			
ele	phone number	Fax		Cell numb	er		
. 1	Tarion Warranty Corporat	ion (Ontario New Home V	Varranty Program)		_		_
	Is proposed construction for a Home Warranties Plan Act? I	new home as defined in the		٥	Yes	а	No
ii.	Is registration required under t	he Ontario New Home Warra	nties Plan Act?		Yes	0	No
	Maria de de la companya de la compan						10
iii.	If yes to (ii) provide registration	on number(s):					-
-	Required Schedules	3.12					
	Attach Schedule 1 for each in		377				
	Attach Schedule 2 where appl			ystem.			
_	Completeness and completeness and completeness and complete the complete and the complete and co						
	Division C of the Building Cod owner or aurthorized agent, al application and required scher	e (the application is made in t I applicable fields have been	he correct form and by the completed on the	X	Yes		No
	Payment has been made of al resolution or regulation made paid when the application is m	under clause 7(1)(c)of Building		×	Yes	D	No
	This application is accompani the applicable by-law, resolution Code Act, 1992	described the second of the se		×	Yes	۵	No
	This application is accompani law, resolution or regulation m which enable the chief building construction or demolition will	ade under clause 7(1)(b) of the offical to determine whether	ne Building Code Act, 1992 the proposed building,	×	Yes	D	No
	The proposed building, constraint applicable law.	ruction or demolition will not co	ontravene any	Ø	Yes	0	No
D	eclaration of applicant						
	1	Kaleb Lakew, P.	Eng.	declare the	at:		
1.	The information contained in documentation is true to the If the owner is a corporation	this application, attached sch best of my knowledge. or partnership, I have authority	2	^	ns,and oth	ner attached	
	April 9	horo	Nu	(5)			

Personal information contained in this form and schedules is collected under the authority of subsection 8(1.1) of the Building Code Act, 1992, and will be used in the administration and enforcement of the Building Code Act, 1992. Questions about the collection of personal information may be addressed to: a) the Chief Building Official of the municipality or upper-tier municipality to which this application is being made, or, b) the inspector having the powers and duties of a chief building official in relation to sewage systems or plumbing for an upper-tier municipality, board of health or conservation authority to whom this application is made, or, c) Director, Building and Development Branch, Ministry of Municipal Affairs and Housing 777 Bay St., 2nd Floor. Toronto, M5G 2E5 (416) 585-5666

se one form	of for each individual who information More, street name.	Carrier 3 1	050 /	SEPT	S	CHEDULE .	1: Designer Information
. Project i	nformation	All anot	akes responsibil	lity for design activities	withres	spect to the pro	oject.
ilding numl	ber, street name	-			Hnit	number:	Lot/con.
	1000	140 Reis Ro	oad		9.	••	8 / 2
morpanty	st Carleton (Huntley)	Post	al code:	Plan number/other d	lescriptic	on	
	al who reviews and ta	akes respon	nsibility for de	sign activities			
me				Firm			
	Kaleb Lakew,	P.Eng.				rd Associate	
eet addres		89, 210 Pre	scott St.		Unit	number: 1	Lot/con.
inicipality	1950 - VOLUME		al code:	Province	E-ma		
	Kemptville		K0G 1J0	ON			@kollaard.ca
lephone nu	(613) 860-0923	Fax	(613)	258-0475	Cell	number	
Design a	ctivities undertaken	by individu			ina Co	de Table 3.5	.2.1 of Division C1
House		0	HVAC - Hou			Building St	
Small	Buildings		Building Serv	vices		Plumbing -	
	Buildings		Detection, Lig	ghting and Power		Plumbing -	- All Buildings
	lex Buildings		Fire Protection	on	×	On-site Se	wage Systems
scription (of designers work		Type 'A' Bed	~ Partially Raised		3	
escription (of designers work ion of Designer Kale	b Lakew, P	Type 'A' Bed	~ Partially Raised		thoose one as	
escription	ion of Designer Kale (pr I review and take resp Divison C of the Buildi	b Lakew, P	Type 'A' Bed .Eng.	~ Partially Raised declar	e that (c	hoose one as	appropriate):
Declarati	ion of Designer Kale (pr I review and take resp Divison C of the Buildi Individual BCIN:	b Lakew, P	Type 'A' Bed .Eng.	~ Partially Raised declar	e that (c	hoose one as	appropriate):
Declarati	ion of Designer Kale (pr I review and take resp Divison C of the Buildi	b Lakew, P	Type 'A' Bed .Eng.	~ Partially Raised declar	e that (c	hoose one as	appropriate):
Scription of	ion of Designer Kale (pr I review and take resp Divison C of the Buildi Individual BCIN:	b Lakew, P	Type 'A' Bed Eng. the design work in qualified, and the design work	~ Partially Raised declar on behalf of a firm regithe firm is registered, in	e that (c stered u n the ap	choose one as nder subsection propriate class	appropriate): on 3.2.4. of ees/categories.
Declarati	of designers work I review and take resp Divison C of the Buildi Individual BCIN: Firm BCIN: I review and take resp designer" under subse	b Lakew, P int name) onsibility for t ing Code. I an onsibility for t ection 3.2.5. o	Type 'A' Bed Eng. the design work or qualified, and the design work of Divison C of the	~ Partially Raised declar on behalf of a firm regithe firm is registered, in	e that (c stered u n the ap	choose one as nder subsection propriate class	appropriate): on 3.2.4. of ees/categories.
Declarati	of designers work Ion of Designer Kale (pr I review and take resp Divison C of the Buildi Individual BCIN: Firm BCIN: I review and take resp designer" under subse Individual BCIN:	b Lakew, P int name) onsibility for the consibility for the consistency for the consis	Type 'A' Bed Eng. the design work in qualified, and in the design work in Divison C of the design work is presented to the design work in Divisor C of the d	declar declar on behalf of a firm registered, in and am qualified in the Building Code.	e that (c	choose one as nder subsection propriate class riate category the Building C	appropriate): on 3.2.4. of es/categories. as an "other
Declarati	of designers work Ion of Designer Kale (pr I review and take resp Divison C of the Buildi Individual BCIN: Firm BCIN: I review and take resp designer" under subse Individual BCIN: Basis for exemp	b Lakew, P int name) onsibility for the consibility for the consistency for the consis	Type 'A' Bed Eng. the design work in qualified, and in the design work in Divison C of the design work is presented to the design work in Divisor C of the d	declar declar on behalf of a firm registered, in and am qualified in the Building Code.	e that (c	choose one as nder subsection propriate class riate category the Building C	appropriate): on 3.2.4. of ees/categories. as an *other
Declarati	of designers work Ion of Designer Kale (pr I review and take resp Divison C of the Buildi Individual BCIN: Firm BCIN: I review and take resp designer" under subse Individual BCIN: Basis for exemp	b Lakew, P int name) onsibility for t ing Code. I an onsibility for t ection 3.2.5. o lion from regi	Type 'A' Bed Eng. the design work in qualified, and if Divison C of the design work is the design work in the	declar de	e that (c	choose one as nder subsection propriate class riate category the Building C	appropriate): on 3.2.4. of ees/categories. as an *other
Declarati	of designers work Ion of Designer Kale (pr I review and take resp Divison C of the Buildi Individual BCIN: Firm BCIN: I review and take resp designer" under subse Individual BCIN: Basis for exemp	b Lakew, P onsibility for t ng Code. I an onsibility for t cotion 3.2.5. o tion from regi empt from the tion from regi	Type 'A' Bed Eng. the design work in qualified, and if Divison C of the design work if Divison C of the distration: e registration and qualified and qual	declar de	e that (c	choose one as nder subsection propriate class riate category the Building C	appropriate): on 3.2.4. of ees/categories. as an *other
Declarati	of designers work Ion of Designer Kale (pr I review and take resp Divison C of the Buildi Individual BCIN: Firm BCIN: I review and take resp designer" under subse Individual BCIN: Basis for exemp The design work is ex Basis for exemp	b Lakew, P onsibility for t ng Code. I an onsibility for t cotion 3.2.5. o tion from regi empt from the tion from regi	Type 'A' Bed Eng. the design work in qualified, and if Divison C of the design work if Divison C of the distration: e registration and qualified and qual	declar de	e that (c) stered u in the appropriate appropriate Lice	choose one as nder subsection propriate class riate category the Building C nsed Profes	appropriate): on 3.2.4. of ees/categories. as an *other

certificate of authorization, issueed by the Association of Professional Engineers of Ontario.

ge System Installer Information to the project. ber: Lot/con 8 / 2 ng, servicing, cleaning or staller unknown at time of applic (Continue to Section E)
ber: Lot/con 8 / 2 ng, servicing, cleaning or staller unknown at time of applic
ber: Lot/con 8 / 2 ng, servicing, cleaning or staller unknown at time of applic
ng, servicing, cleaning or staller unknown at time of applic
staller unknown at time of applic
staller unknown at time of applic
ber: Lot/con.
per
nat:
at time of application, the edule 2 now that the ership
h

富	M	
, \$	Ottawa	Septic
	System	

Bureau des systèmes septiques d'Ottawa

Do not Complete Permit No Revision No Date

	REESCHEDULE 4
	Proposed Service
1. Engineered	2. Water

Yes No

r Supply X

Proposed Existing

3. Type of work proposed

Х

New Installation Replacement Alteration

4. Type of well

Dug/bored/Standpoint well

X Drilled well

Municipal Other

5. Residential Sewage Design Flow Info.

Bedrooms

House (floor area)

Design Flow

Detail sewage flow calculations:

6. Sewage Design Flow for Other Occupancies

1925

People

Total Fixture Units

(Schedule 8)

Residential Flow

L/day

7. Type of System

Treatment Unit

Class 2 - Leaching Pit

Class 3 - Cesspool Class 4 - Shallow Buried Trench

Class 4 - Trench

Fully Raised

Partially Raised

In-ground

Class 4 - Filter Media

Fully Raised Partially Raised In-ground

Ecoflo STB-730PR

Class 4 - BMEC Bed

Fully Raised Partially Raised In-ground

Class 4 - Type A Bed X

Fully Raised Partially Raised

In-ground

Class 4 - Type B Bed Fully Raised

Partially Raised In-ground

Class 5 - Holding Tank

Tank/Treat Unit/Pump Cham ONLY Effluent Filter / Risers ONLY



File 200247



Do not Complete Permit No Revision No Date

Type of System

Type 'A' Bed ~ Partially Raised

(Schedule 4)

Septic / Holding

4800 Litres

Ecoflo STB-730PR

Septic Tank Effluent Filter

Yes

Treatment Unit -

Make & Model

Ecoflo STB-730PR

Number of Units

Refer to Typical Drawing

Type 'A' Bed ~ Partially Raised

Mantle information

Native or imported = 15 m in

N/A

direction(s)

Slope Subgrade

% slope direction(s)

None

Site to be Scarified (If in Clay)

NO

Yes / No Yes / No

Clay Seal Required (If in bedrock)

NO

m2 required

Minimum Required Contact Area

Pump(s) required Specified discharge rate required Yes

136 L/15min

Note: Alarm required for all pumping systems

Filter Bed

Trench Bed - Length of Distribution Pipe - Proposed diameter of Tile

m

mm m²

- Loading Area

- Stone - Sand

 m^2 m^2

- Filter Sand

m²

- Pipe

m

- Amount of Filter Media Sand

Kg required

SBT Bed - Length of Distribution Pipe

m

BMEC Bed - Stone

45

m²

Type A Bed - Sand Type B Bed - Pipe

45 40 m² m

Tank/Treatment Unit/ Pump Chamber replacement ONLY

TaEffluent Filter & Risers ONLY

Construction Notes:

See construction notes on Kollaard Associates Drawing No.

200247-1



File 200247

Ottawa Septic Bureau des systèmes CA PECEVED
System Office septiques d'Ottawa 1200 SCHEDULE 6

RESoil and Water Table Information (Minimum depth of test pit 2 metres)

Do not Complete Permit No Revision No Date OTTAVA

File # 200247

April 9, 2020

140 Reis Road Lot 8, Conc. 2 West Carleton (Huntley) City of Ottawa

Inspector:

Date:

Signature:

Test Pit #	Elevation / (Depth) [m]	Soil Description	Test Pit #	Elevation / (Depth) [m]	Soil Description
TP1	114.36				
	0.00 - 0.25	TOPSOIL			
	0.25 - 0.90	Grey brown SILTY SAND trace clay			
	0.90	End of TP		Test	pitsnot
		rved at about 0.9 metres below in March 31, 2020		au	ailable
TP2	114.71 0.00 - 0.30	TOPSOIL		Enginee	n assumes

Water was observed at about 0.9 metres below ground surface on March 31, 2020

End of TP

Red brown SILTY SAND

Grey brown SILTY SAND trace clay



Kollaard Associates

0.30 - 0.40

0.40 0.80

0.90



Professional Engineers Ontario

Authorized by the Association of Professional Engineers Ontario to offer Professional Engineering Services



Do not Complete SEPTIC FILE # Permit No Revision No Date

SEWAGE DESIGN FLOW CALCULATION As per O.B.C. 8.2.1.3.

File: 200247

Date: April 9, 2020

	Establishment	Volume, L	Quantity	Flow
	Warehouse			
x	a) per loading bay	150	3	450 L/day
x	b) per water closet	950	1	950 L/day
	Office Building			
	a) per employee per 8 hour shift	75	7	525 L/day
×	b) per each 9.3m ² of floor space	75	62m ² / 9.3	525 L/day

Total Daily Design Sewage Flow =

1925 litres/day

2010

Note:

Sump pumps and floor drains are not to be connected to the sewage system. Connection of such failures to a sewage system may lead to a hydraulic failure of the said system. The above mentioned fatures should be discharged separately to an approved Class 2 (leaching pit) sewage system.

Where laundry waste is not more than 20% of the total daily design sanitary sewage flow, it may dis

Signature of Owner / Agent:

Kollaard Associates

Date:

Professional Engineers Ontario

Authorized by the Association of Professional Engineers Ontario to offer Professional Engineering Services

MAR 23 2020 SEE KOLLAARD ASSOCIATES TECHNICAL DRAWING 200247-1 FOR DETAILS System Office septiques d'Ottawa
System Office septiques d'Ottawa 15 min/cm 8 min/cm 1925 L/day 33.97 m² 25.67 m⁴ Treatment Unit = Ecoflo STB-730PR 1925 x 15 850 1925 Flow Rate
Existing Soil Percolation
Rate (T)
Replacement Soil Flow rate = Flow rate x T = No Mantle Required 75 File: 200247 Stone Area Sand Area Kollaard Associates Engineers Minimum Septic Tank Working Capacity
The greater of 3600 Litres or $2 \times 1925 = 4800$ Type A Bed ~Partially Raised~ Lot 8, Conc. 2 West Carleton (Huntley) City of Ottawa April 9, 2020

140 Reis Road

SEPTIC FILE # 20-141 OTTAWA

EXISTING

APPROVED INSTALLATION

PROPOSED INSTALLATION 115.05

FINISHED GRADE

Geotextile

Remove Organic Material

Scarification Required Clay Seal Required

8 NO 114.75

114.45

SEPTIC STONE

114.40

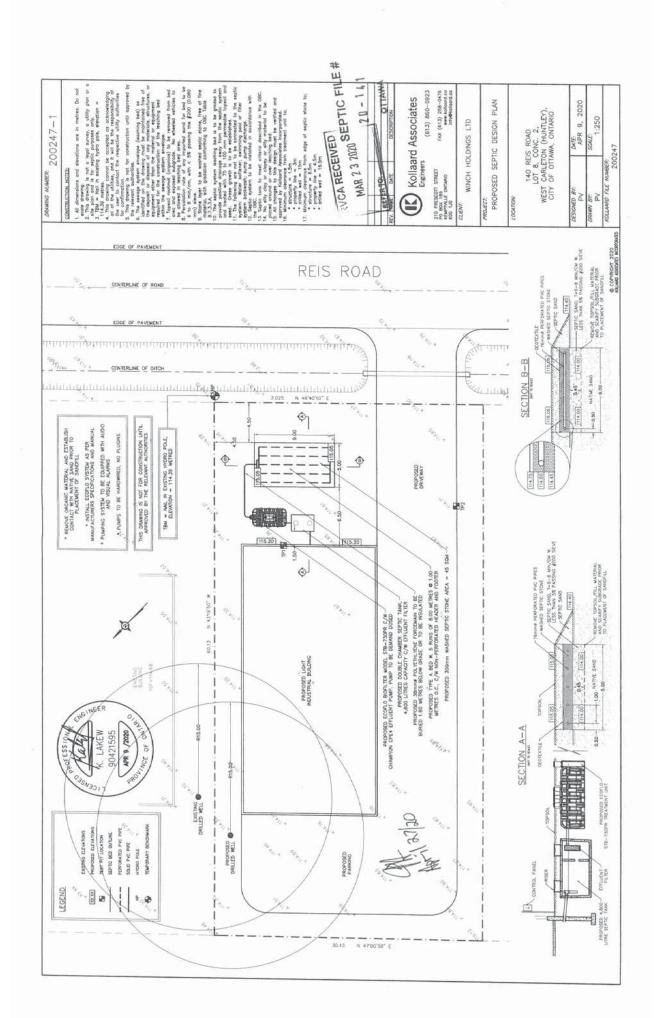
APL110/10

114.00 m

0.45 m

IMPORTED SEPTIC SAND

NATIVE SAND





PermitPart 8 – Sewage System Ontario Building Code

Do Not Comp Permit No _	20-141
Revision No	
Date	
Related Applie	cation

nspected & Recommended by:	Jason H	Hutton	Owner: Wic	h Holdings	
			Weather:		
Civic Address:	140 Reis Rd		Legal:		
			fixture units:		
inished floor area:			Q:192	5	L/da
septic tank	4800	L	weigh bills for	□ yes	■ no
effluent filter	YES		grain size analysis required	□ yes	■ no
oump rate		L/15 min	site to be scarified	☐ yes	■ no
reatment unit Ecoflo STB 73	OPR		clay seal inspection	☐ yes	■ no
number of units	1		mantle required	☐ yes	■ no
			sub-grade inspection	☐ yes	■ no
TYPE OF SYSTEM Trench Pipe and Stone or O C type of chamber loading area total trench length	00 2000 00 10 10 10 10 10 10 10 10 10 10 10	m²	 Shallow Buried Trench pipe length orifice spacing Filter Media Bed 		m
Trench Pipe and Stone or O C type of chamber loading area total trench length trench configuration Dispersal Bed BMEC Type A stone 19	Type B 45 3 (native)	m²mm²	pipe length		m
Trench Pipe and Stone or O C type of chamber loading area total trench length trench configuration Dispersal Bed BMEC Type A stone 19	Type B 45 3 (native) f 8m; 1.0m o/c	m²mm²	pipe length orifice spacing Filter Media Bed stone extended base pipe weight of filter media loading area		m
Trench Pipe and Stone or O C type of chamber loading area total trench length trench configuration Dispersal Bed BMEC Type A stone sand 19 pipe 5 runs 0	Type B 45 3 (native) If 8m; 1.0m o/c	m²m²m²m²	pipe length orifice spacing Filter Media Bed stone extended base pipe weight of filter media loading area Class 5 Holding Tank	APPRIL T	m
Trench Pipe and Stone or O C type of chamber loading area total trench length trench configuration Dispersal Bed BMEC Type A stone sand 19 pipe 5 runs O linear loading Manager, Septic System Approve	Type B 45 3 (native) If 8m; 1.0m o/c	m m m m² m² m² L/m² L/m²	pipe length	APPRIL T	m²



Appendix D: Correspondence

- · City of Ottawa Pre-consultation
- · City of Ottawa Interpretation of the Reis Business Park Stormwater Management Criteria



Pre-Application Consultation

Site Plan Control (Rural Small)

140 Reis Road

Applicant: Scott Winch Owner: Winch Holding Ltd

Ward 5 - West-Carleton-March Councillor Eli El-Chantiry

Proposal Development of a 464.52 square metre (5,000 sq. ft.) pre-engineered steel

Summary: building on the subject site. The proposed building will be used as an

automotive service station.

Attendees: Krishon Walker, Planner, PIEDD, City of Ottawa

Brian Morgan, Infrastructure Project Manager, PIEDD, City of Ottawa

Sami Rehman, Environmental Planner, PIEDD, City of Ottawa

Neeti Paudel, Transportation Project Manager, PIEDD, City of Ottawa

Erica Ogden, Planner, Mississippi Valley Conservation Authority

Meeting Notes

Planning Comments (Provided by Krishon Walker, Planner)

- As per Schedule A of the Official Plan, the site is designated Rural Employment Area. The Rural Employment Area is intended to support and encourage clustering of primarily industrial uses not suitable in the Urban Area or General Rural Area. Uses permitted in this designation includes but is not limited to new; heavy and light industrial uses, transportation uses, and warehouse and storage operations. As per Schedule 1 of the Carp Road Corridor Community Design Plan (CDP), the site is designated as Light Industrial. The proposed development is consistent with the policies of both the Official Plan and CDP.
- As per the City's Zoning By-law, the site is zoned as Rural General Industrial Zone, Subzone 4 (RG4).

The Zoning By-law defines an automotive service station as "a place that:

- has one or more service bays or facilities for a mechanic to service and repair motor vehicles other than heavy vehicles, which may also retail fuel and other automotive products; or
- b. has one or more service bays which provide one or more single or specialized service product installation for motor vehicles other than heavy vehicles such as mufflers or oil changes; and
- c. may include sales of motor vehicles other than heavy vehicles in association with the automobile service station."

Please ensure that your proposal complies with all applicable provisions of the Zoning By-law.

Additionally, please ensure that the proposed parking complies with the provisions of Part 4 of the Zoning By-law. Parking areas should be screened from the street.

If any aspect of the proposal does not comply with the zoning provisions of the applicable zone, a Minor Variance may be required through the Committee of Adjustment. If a Minor Variance is required, please note approval from the Committee of Adjustment would be required before a decision is made on the Site Plan Control application.



- Cash-in-Lieu of Parkland will be requested as a condition of Site Plan Control. CIL would be taken at 2% of the gross land area being developed, including roads, parking lot and other associated land used for the development.
- Please note that, as per Table 219 of the RG zone, any proposed outdoor storage is not permitted within the front yard and must be screened from the public street by an opaque screen at least 1.8 metres in height from finished grade.
- O Please contact the Mississippi Valley Conservation Authority (MVCA), amongst other federal and provincial departments/agencies, to identify all the necessary permits and approvals required to facilitate the development. Responsibility rests with the developer and their consultant for obtaining all external agency approvals. The address shall be in good standing with all approval agencies. Copies of confirmation of correspondence will be required by the City of Ottawa from all approval agencies that a form of assent is given. No construction shall commence until after a commence work notification is given.
- O Please ensure that the Site Plan shows the full extent of the property and that a complete zoning table is provided. The Site Plan should also clearly show the dimensions of all proposed buildings, roads, radii of turns, overhead clearances, parking areas with defined parking spaces, steps, terraces, fences, walks, aisles and private approaches.
- Please show the location for snow storage on both the Site Plan and Landscape Plan. Storage shall not interfere with approved grading and drainage patterns or servicing. If snow is to be removed from the site, then please make a note of that on the Site Plan and include where the snow will be placed in the interim. Temporary snow storage areas should not conflict with utility box, landscaping, required parking, and site circulation.
- Be sure to follow the City's guide to preparing plans and studies (see link below) to ensure a
 high quality of your submission.

Feel free to contact Krishon Walker at Krishon. Walker@ottawa.ca, for follow-up questions.

Engineering Comments (Provided by Brian Morgan, Infrastructure Project Manager)

Grading

Please provide a few more existing and proposed grades along the side property lines.

Please include details of the proposed retaining wall. Please confirm that the retaining wall is not over 1.0 metre in height. Retaining walls over 1.0m in height must be designed by an Engineer licensed in the Province of Ontario.

A short section of the drainage swale and the rear-yard graveled area drains to the west. Where does these areas outlet too?

Is the anagram TOF referring to the Top of Foundation Wall? The City will need elevations for Top of Foundation Wall and for the Top of Finished Floor.

Stormwater Management

Stormwater Management requirements for this lot are determined by the subdivision agreement. Please review Schedule H, page 44 of the Reis Road Business Park. See attached. Also, see attached City internal memo dated 06-Sep-2016.

The Stormwater Management must be designed as per page 8.11 of the 'Ottawa Sewer Design Guidelines'. Typically, this is referred to as pre-to-post, but is more accurately described as 100-year post-development to 5-year pre-development.



The Stormwater Management Report/Brief should include a drawing indicating the 5-year and the 100-year flood line contours. Please ensure that the finished floor elevation is 300mm above the 100-year flood level.

The minimum diameter for rear-yard or side-yard perforated subdrain pipes is 250 mm. Perforated pipes shall be installed in a granular trench and protected from fines by a filter cloth as per the City of Ottawa standards. Ref: Ottawa Sewer Design Guidelines. Section 5.4.9.4.

Stormwater outlet pipes must stop at the property line.

Will catch-basins be used at the top end of the side yard subdrain pipes?

o <u>Services</u>

The hydrogeological report should discuss the impact the proposed well may have on the existing well on the neighbouring lot.

- The discharge of oils, grit, VOC's, and other harmful fluids resulting from the assembly or repair of vehicles are not permitted to discharge to the septic system as these chemicals will interfere with the processes necessary for the breakdown of human waste. Development Review requires that all runoff be directed to a legal and sufficient outlet, typically the right-of-way. It is understood that an oil/grit separator requires an ECA from the MECP. Please contact the MECP for additional information regarding this application.
- The City requires a drawing note that expressly states that site elevations are referenced to a geodetic benchmark. Please include a note referencing the following:
 - 1. Original registered survey plan (4R-PLAN),
 - 2. Geodetic site benchmark (not a TBM), and
 - 3. CSRS survey monument and its geodetic elevation. (Please include sufficient information to permit a lay-person to locate these benchmarks in the field.) A sample note might read:

"Reference CSRS Survey monument no. 2212235, located at the corner of Smith and Wesson Street, in the church yard near the front steps. Geodetic elevation = 108.12 metres ASL."

Feel free to contact Brian Morgan at Brian.Morgan@ottawa.ca, for follow-up questions.

Environmental Comments (Provided by Sami Rehman, Environmental Planner)

The site plan will need to have a Tree Conservation Report (TCR). The TCR will also need to reflect current requirements regarding butternuts and other Official Plan policies.

Feel free to contact Sami Rehman at Sami.Rehman@ottawa.ca, for follow-up questions.

<u>Transportation Comments (Provided by Neeti Paudel, Transportation Project Manager)</u>

o Comments are forthcoming.

Feel free to contact Neeti Paudel at Neeti.Paudel@ottawa.ca, for follow-up questions.



Conservation Authority Comments (Provided by Erica Ogden, Planner, MVCA)

- The property is not regulated under Ontario Regulation 153/06 and there are no natural hazard or natural heritage features identified.
- As per the Carp River Watershed Subwatershed Study the site is within the moderate recharge area which has an annual infiltration target of 104 mm/yr. The water quality should include a normal level of protection which is 70% Total Suspended Solids removal.

Feel free to contact Planner, Erica Ogden, at eogden@mvc.on.ca, for follow-up questions.

Application Submission Information

Applications Type: Site Plan Control, Rural Small.

Application processing timeline generally depends on the quality of the submission. For more information on standard processing timelines, please visit: <a href="https://ottawa.ca/en/city-hall/planning-and-development/information-development-application-review-process/development-application-submission/development-application-forms#site-plan-control

Prior to submitting a formal application, it is recommended that you pre-consult with the Ward Councillor.

For information on application fees, please visit: https://ottawa.ca/en/city-hall/planning-and-development/information-development-application-review-process/development-application-fees

To request City of Ottawa plan(s) or report information please contact the City of Ottawa Information Centre: lnformationCentre@ottawa.ca or (613) 580-2424 ext. 44455

Application Submission Requirements

For information on the preparation of Studies and Plans and the City's requirements, please visit: https://ottawa.ca/en/city-hall/planning-and-development/information-development-application-review-process/development-application-submission/guide-preparing-studies-and-plans

Please provide hard copies and electronic copy (PDF) of all plans and studies required.

All plans and drawings must be produced on A1-sized paper and folded to 21.6 cm x 27.9 cm (8½"x 11").

Note that many of the plans and studies collected with this application must be signed, sealed and dated by a qualified engineer, architect, surveyor, planner or designated specialist.

Reis Business Park Stormwater Management

Ref Info: Reis Road, Tansley Road, & Maple Creek Court

15-86-3062 (Phase 1)

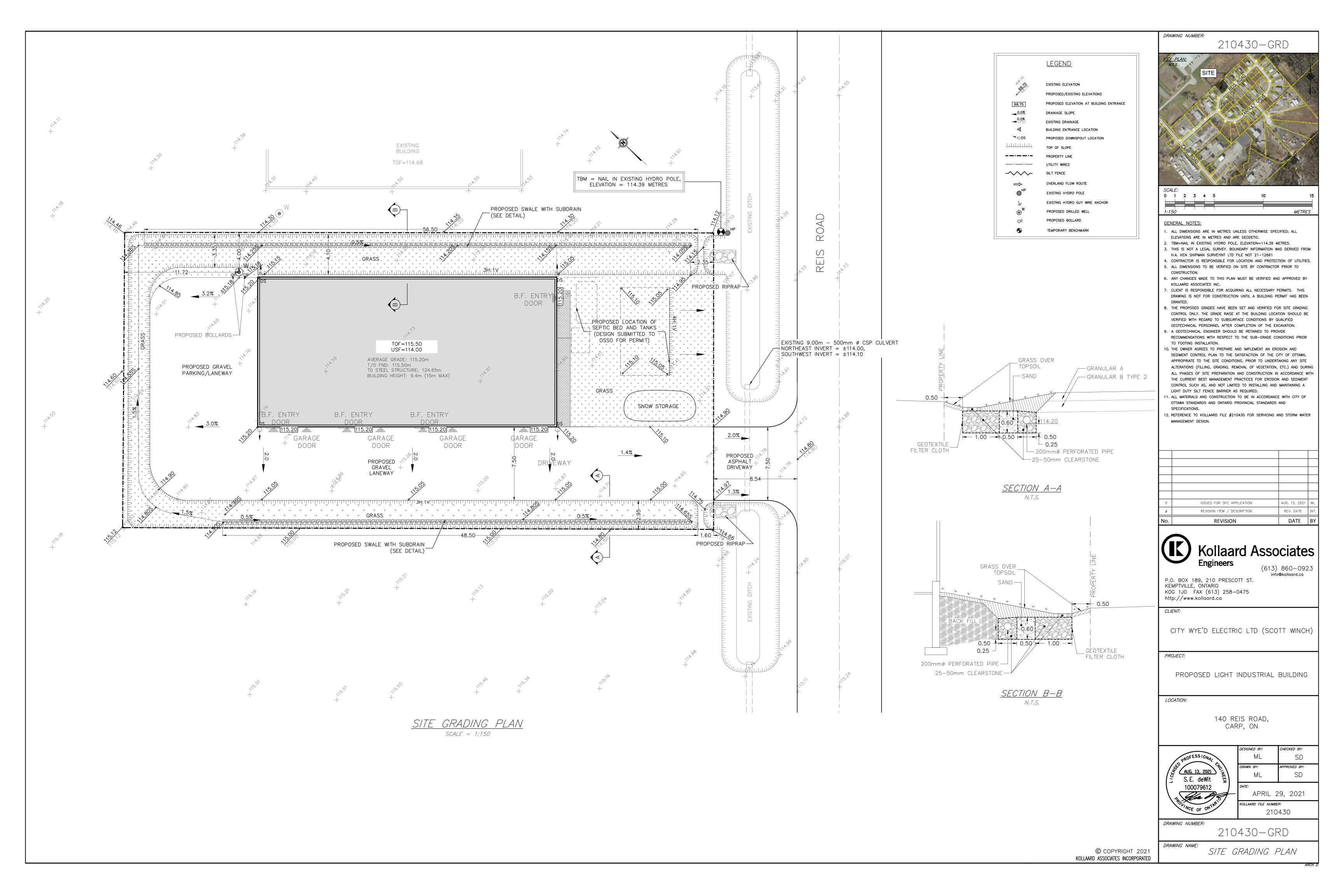
D07-17-4M745

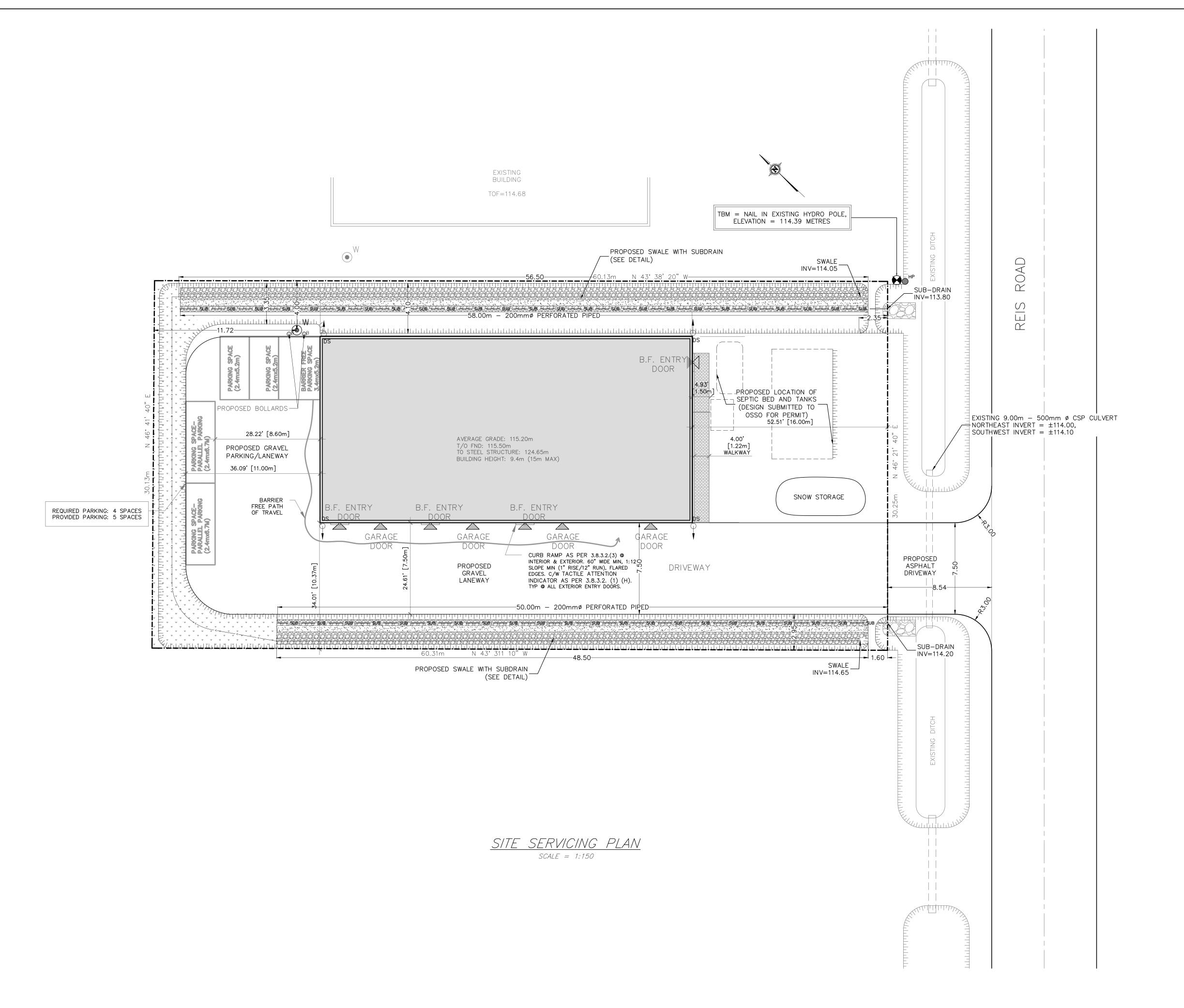
Stormwater Management – The allowable runoff rate from sites within the Reis Industrial Park is governed by the design assumptions used in the approved Engineering Report contained in Schedule "H" of the subdivision agreement. If the resulting runoff from the proposed site will be less than the allowable rate, no on-site SWM will be required. The design parameters used in the approved subdivision Engineering Report are as follows:

• The design of the internal drainage for the subdivision was based on site developments that would be: 50% building (C=1.0), 25% parking (C=0.9) and 25% undeveloped (C=0.2). By my interpretation of design assumptions in the subdivision Engineering Report, sites in this subdivision can be developed without a requirement for on-site SWM as long as the combined C-value does not exceed 0.775.

It is important to note that the original subdivision design used constant C-values, while the newer City of Ottawa Sewer Design Guidelines (see Section 5.4.5.2.1 and Table 5.7) now stipulate that C-values be increased by 25% during the 100-year event (to a maximum of C=1.0). Accordingly, I would ask that you use the City's increased 100-year runoff coefficients when determining the post-development combined C-value for the site. If the post-development C-value is below 0.775, no on-site SWM will be required. If SWM is required, the allowable release will be based on the 5-year flow, with a C-value of 0.775.

As per Tim Newton, Project Manager, City of Ottawa Edits supplied by Damien Whittaker and Brian Morgan. 06-Sep-2016





EXISTING ELEVATION PROPOSED/EXISTING ELEVATIONS PROPOSED ELEVATION AT BUILDING ENTRANCE 0.0% DRAINAGE SLOPE EXISTING DRAINAGE BUILDING ENTRANCE LOCATION **→**⊙DS PROPOSED DOWNSPOUT LOCATION TOP OF SLOPE -----UTILITY WIRES **-**OVERLAND FLOW ROUTE EXISTING HYDRO POLE EXISTING HYDRO GUY WIRE ANCHOR PROPOSED DRILLED WELL PROPOSED BOLLARD TEMPORARY BENCHMARK

<u>LEGEND</u>

DRAWING NUMBER:

210430-SER



SCALE:	2	3	4	5	10	
		_				

GENERAL NOTES:

ALL DIMENSIONS ARE IN METRES UNLESS OTHERWISE SPECIFIED; ALL ELEVATIONS ARE IN METRES AND ARE GEODETIC.

- . TBM=NAIL IN EXISTING HYDRO POLE, ELEVATION=114.39 METRES.

 THIS IS NOT A LEGAL SURVEY. BOUNDARY INFORMATION WAS DERIVED FRO
- 5. THIS IS NOT A LEGAL SURVEY. BOUNDARY INFORMATION WAS DERIVED FROM
 H.A. KEN SHIPMAN SURVEYINT LTD FILE NOT 21-12661
- 4. CONTRACTOR IS RESPONSIBLE FOR LOCATION AND PROTECTION OF UTILITIES.5. ALL DIMENSIONS TO BE VERIFIED ON SITE BY CONTRACTOR PRIOR TO
- CONSTRUCTION.

 . ANY CHANGES MADE TO THIS PLAN MUST BE VERIFIED AND APPROVED BY
- KOLLAARD ASSOCIATES INC.

 CLIENT IS RESPONSIBLE FOR ACQUIRING ALL NECESSARY PERMITS. THIS
- DRAWING IS NOT FOR CONSTRUCTION UNTIL A BUILDING PERMIT HAS BEEN GRANTED.
- 8. THE PROPOSED GRADES HAVE BEEN SET AND VERIFIED FOR SITE GRADING CONTROL ONLY. THE GRADE RAISE AT THE BUILDING LOCATION SHOULD BE VERIFIED WITH REGARD TO SUBSURFACE CONDITIONS BY QUALIFIED GEOTECHNICAL PERSONNEL AFTER COMPLETION OF THE EXCAVATION.
- A GEOTECHNICAL ENGINEER SHOULD BE RETAINED TO PROVIDE
 RECOMMENDATIONS WITH RESPECT TO THE SUB-GRADE CONDITIONS PRIOR
 TO FOOTING INSTALLATION.
 THE OWNER AGREES TO PREPARE AND IMPLEMENT AN EROSION AND
- SEDIMENT CONTROL PLAN TO THE SATISFACTION OF THE CITY OF OTTAWA, APPROPRIATE TO THE SITE CONDITIONS, PRIOR TO UNDERTAKING ANY SITE ALTERATIONS (FILLING, GRADING, REMOVAL OF VEGETATION, ETC.) AND DURING ALL PHASES OF SITE PREPARATION AND CONSTRUCTION IN ACCORDANCE WITH THE CURRENT BEST MANAGEMENT PRACTICES FOR EROSION AND SEDIMENT CONTROL SUCH AS, AND NOT LIMITED TO INSTALLING AND MAINTAINING A LIGHT DUTY SILT FENCE BARRIER AS REQUIRED.
- ALL MATERIALS AND CONSTRUCTION TO BE IN ACCORDANCE WITH CITY OF
 OTTAWA STANDARDS AND ONTARIO PROVINCIAL STANDARDS AND
 SPECIFICATIONS.
- 2. REFERENCE TO KOLLAARD FILE #210430 FOR SERVICING AND STORM WATER MANAGEMENT DESIGN.

No.	REVISION	DATE	ВҮ
#	REVISION ITEM / DESCRIPTION	REV. DATE	INT.
0	ISSUED FOR SPC APPLICATION	AUG. 13, 2021	ML



info@kollaa P.O. BOX 189, 210 PRESCOTT ST.

KEMPTVILLE, ONTARIO KOG 1JO FAX (613) 258-0475 http://www.kollaard.ca

CLIENT:

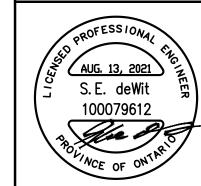
CITY WYE'D ELECTRIC LTD (SCOTT WINCH)

PROJECT:

PROPOSED LIGHT INDUSTRIAL BUILDING

LOCATION:

140 REIS ROAD, CARP, ON



	DRAWN BY:		APPROVED BY:			
		ML	SD			
	DATE:					
_		APRIL 2	29, 2021			
	KOLLAARD FILE NUMBER:					
	210430					

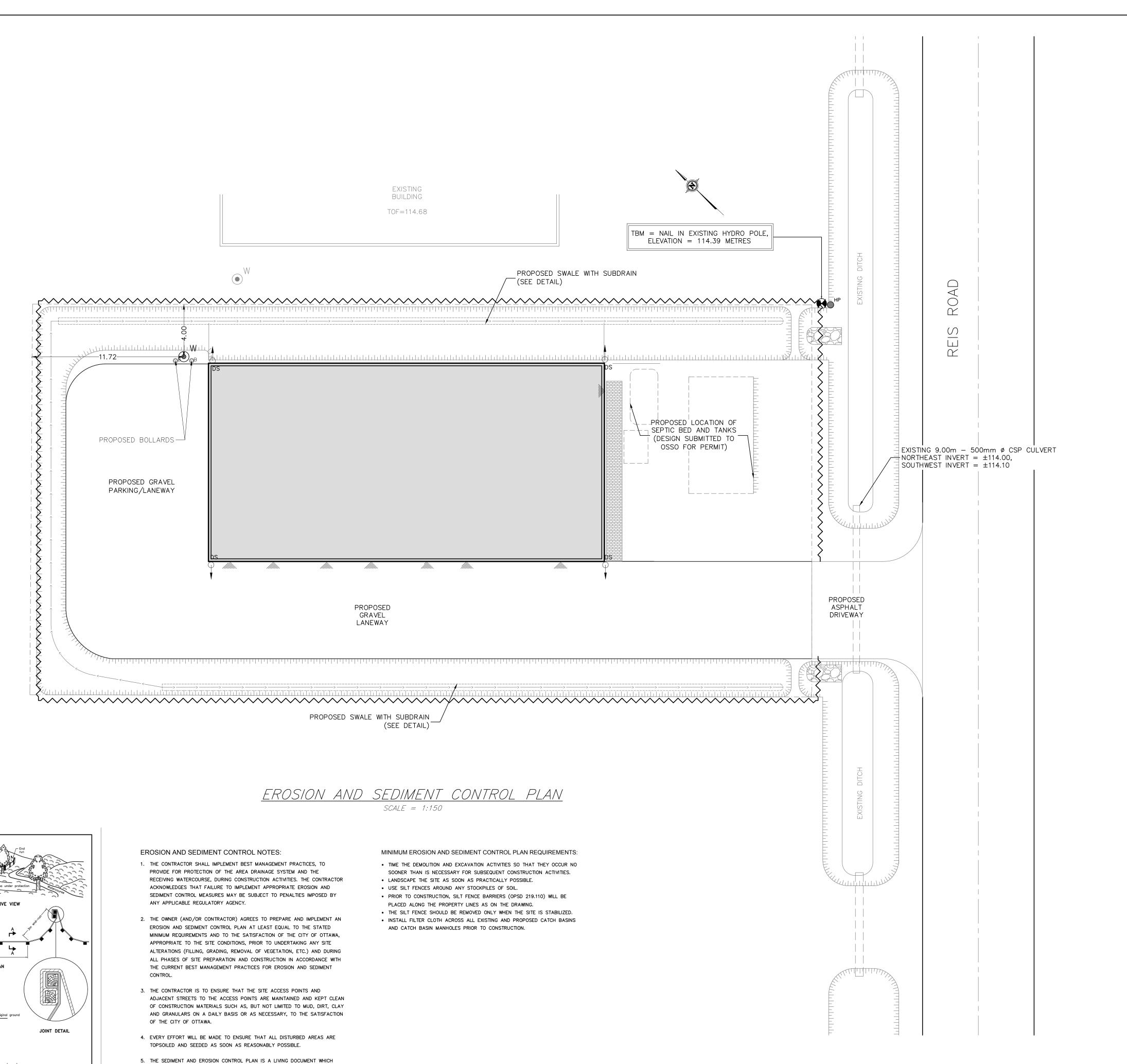
SD

DRAWING NUMBER:

210430-SER

DRAWING NAME:

SITE SERVICING PLAN



300mm min of geotextile in trench

A All dimensions are in millimetres unless otherwise shown.

LIGHT-DUTY
SILT FENCE BARRIER

OPSD 219.110

MAY BE AMENDED BY ONSITE REQUIREMENTS AT THE APPROVAL OF THE

MUNICIPALITY AND THE CONSERVATION AUTHORITY.

<u>LEGEND</u> EXISTING ELEVATION PROPOSED/EXISTING ELEVATIONS PROPOSED ELEVATION AT BUILDING ENTRANCE 0.0% DRAINAGE SLOPE EXISTING DRAINAGE BUILDING ENTRANCE LOCATION **→**⊙DS PROPOSED DOWNSPOUT LOCATION -----UTILITY WIRES **-**OVERLAND FLOW ROUTE EXISTING HYDRO POLE EXISTING HYDRO GUY WIRE ANCHOR PROPOSED DRILLED WELL PROPOSED BOLLARD

TEMPORARY BENCHMARK

MEY PLAN:
N.T.S.

SI

DRAWING NUMBER:

SCALE:

210430-ESC

SCA	4 <i>LE:</i>							
0	1	2	3	4	5	1	0	
					-			
1:1	150							METRES

GENERAL NOTES:

ALL DIMENSIONS ARE IN METRES UNLESS OTHERWISE SPECIFIED; ALL ELEVATIONS ARE IN METRES AND ARE GEODETIC.

- TBM=NAIL IN EXISTING HYDRO POLE, ELEVATION=114.39 METRES.
 THIS IS NOT A LEGAL SURVEY. BOUNDARY INFORMATION WAS DERIVED FROM
- H.A. KEN SHIPMAN SURVEYINT LTD FILE NOT 21-12661

 4. CONTRACTOR IS RESPONSIBLE FOR LOCATION AND PROTECTION OF UTILITIES.
- ALL DIMENSIONS TO BE VERIFIED ON SITE BY CONTRACTOR PRIOR TO CONSTRUCTION.
- ANY CHANGES MADE TO THIS PLAN MUST BE VERIFIED AND APPROVED BY KOLLAARD ASSOCIATES INC.
- KOLLAARD ASSOCIATES INC.

 7. CLIENT IS RESPONSIBLE FOR ACQUIRING ALL NECESSARY PERMITS. THIS
- DRAWING IS NOT FOR CONSTRUCTION UNTIL A BUILDING PERMIT HAS BEEN GRANTED.

 8. THE PROPOSED GRADES HAVE BEEN SET AND VERIFIED FOR SITE GRADING
- CONTROL ONLY. THE GRADE RAISE AT THE BUILDING LOCATION SHOULD BE VERIFIED WITH REGARD TO SUBSURFACE CONDITIONS BY QUALIFIED GEOTECHNICAL PERSONNEL AFTER COMPLETION OF THE EXCAVATION.
- A GEOTECHNICAL ENGINEER SHOULD BE RETAINED TO PROVIDE
 RECOMMENDATIONS WITH RESPECT TO THE SUB—GRADE CONDITIONS PRIOR
 TO FOOTING INSTALLATION.
 THE OWNER AGREES TO PREPARE AND IMPLEMENT AN EROSION AND
- SEDIMENT CONTROL PLAN TO THE SATISFACTION OF THE CITY OF OTTAWA, APPROPRIATE TO THE SITE CONDITIONS, PRIOR TO UNDERTAKING ANY SITE ALTERATIONS (FILLING, GRADING, REMOVAL OF VEGETATION, ETC.) AND DURING ALL PHASES OF SITE PREPARATION AND CONSTRUCTION IN ACCORDANCE WITH THE CURRENT BEST MANAGEMENT PRACTICES FOR EROSION AND SEDIMENT CONTROL SUCH AS, AND NOT LIMITED TO INSTALLING AND MAINTAINING A LIGHT DUTY SILT FENCE BARRIER AS REQUIRED.
- ALL MATERIALS AND CONSTRUCTION TO BE IN ACCORDANCE WITH CITY OF
 OTTAWA STANDARDS AND ONTARIO PROVINCIAL STANDARDS AND
 SPECIFICATIONS.
- 12. REFERENCE TO KOLLAARD FILE #210430 FOR SERVICING AND STORM WATER MANAGEMENT DESIGN.

No.	REVISION	DATE	ВУ
#	REVISION ITEM / DESCRIPTION	REV. DATE	INT.
0	ISSUED FOR SPC APPLICATION	AUG. 13, 2021	ML



(613) 860-09

P.O. BOX 189, 210 PRESCOTT ST. KEMPTVILLE, ONTARIO KOG 1J0 FAX (613) 258-0475

http://www.kollaard.ca

CLIENT:

CITY WYE'D ELECTRIC LTD (SCOTT WINCH)

PROJECT:

PROPOSED LIGHT INDUSTRIAL BUILDING

LOCATION:

140 REIS ROAD, CARP, ON



DRAWN BY:	APPROVED BY:				
ML	SD				
DATE:					
 APRIL 2	9, 2021				
KOLLAARD FILE NUMBER:					
210430					

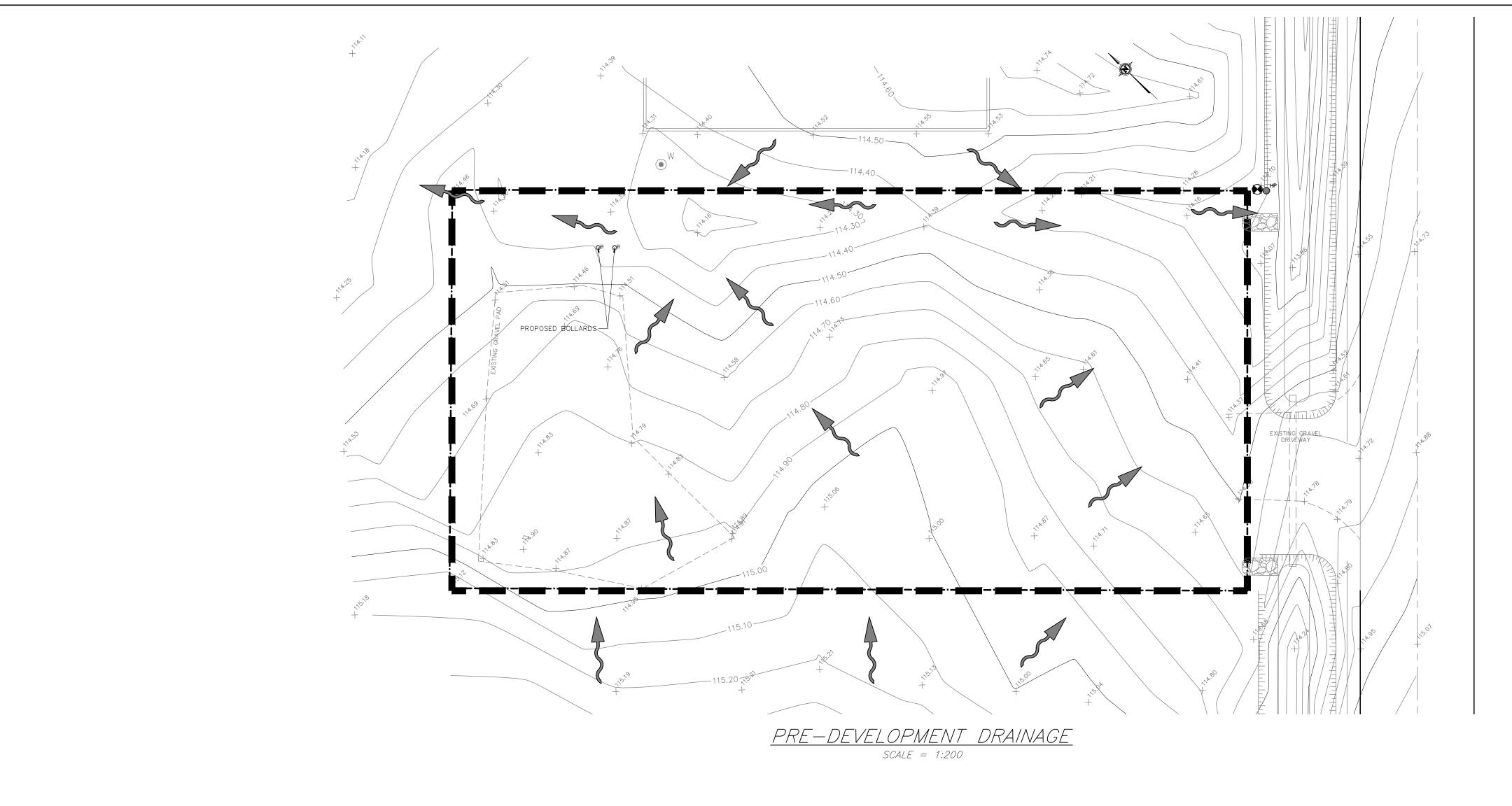
DRAWING NUMBER:

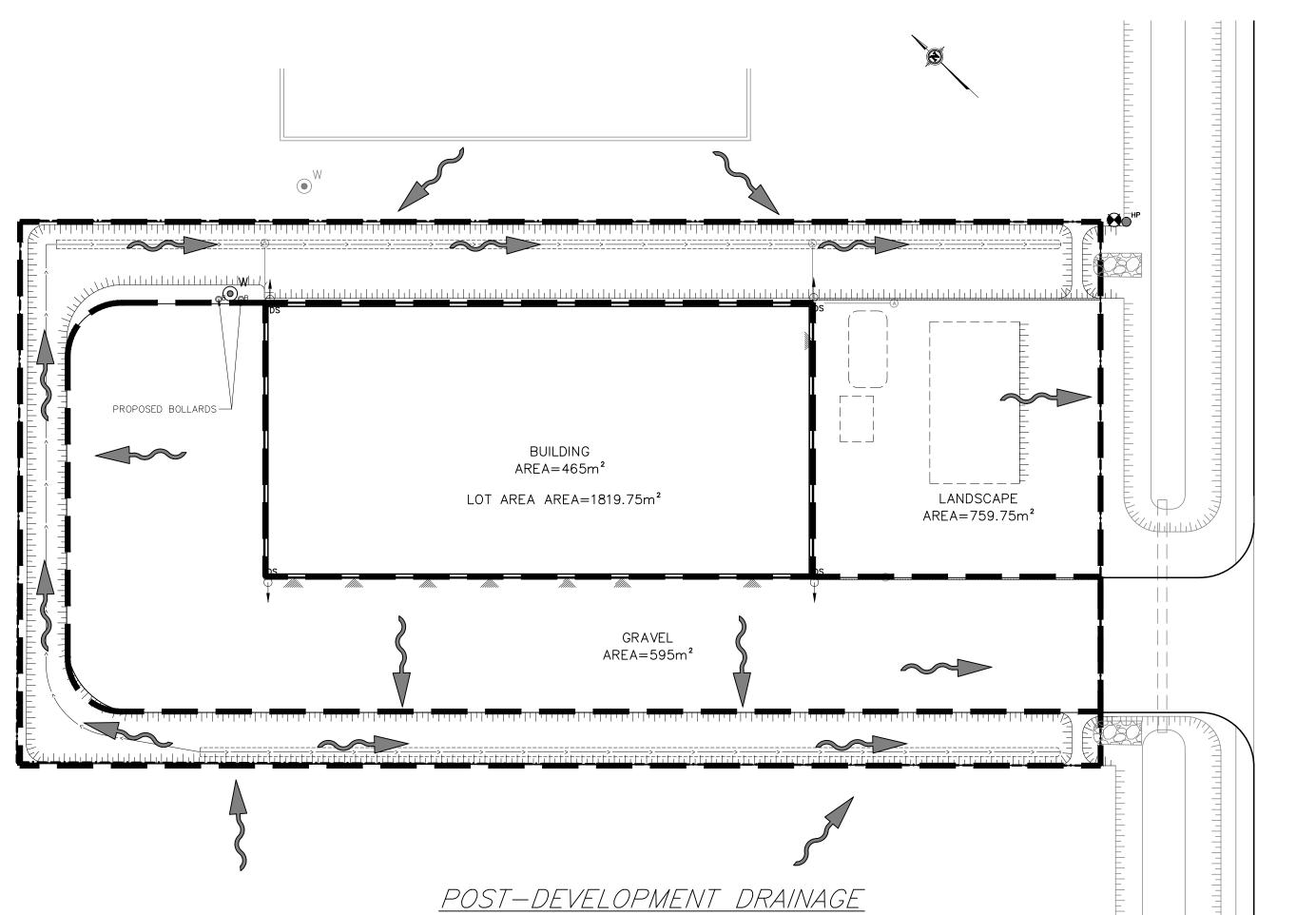
210430-ESC

© COPYRIGHT 2021

KOLLAARD ASSOCIATES INCORPORATED

DRAWING NAME:
EROSION & SEDIMENT CONTROL PLAN





SCALE = 1:200

DRAWING NUMBER: 210430-SWM



AS NOTED

LEGEND (STORM WATER MANAGEMENT)

CATCHMENT AREA (HECTARES)

CONTROLLED CATCHMENT LABEL 0.39

IMPERVIOUS RATIO CATCHMENT AREA BOUNDARY

DIRECTION OF FLOW

CONTROLLED AREA

UNCONTROLLED AREA

DIRECTION OF FLOW

0 #	ISSUED FOR SPC APPLICATION REVISION ITEM / DESCRIPTION	AUG. 13, 2021 REV. DATE	ML INT
0	ISSUED FOR SPC APPLICATION	AUG. 13, 2021	ML



P.O. BOX 189, 210 PRESCOTT ST. KEMPTVILLE, ONTARIO KOG 1JO FAX (613) 258-0475 http://www.kollaard.ca

CLIENT:

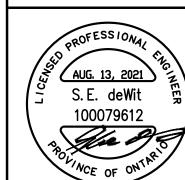
CITY WYE'D ELECTRIC LTD (SCOTT WINCH)

PROJECT:

PROPOSED LIGHT INDUSTRIAL BUILDING

LOCATION:

140 REIS ROAD, CARP, ON



	DESIGNED BY:	CHECKED BY:
0N ₄ / (N ₀) NEE Wit	ML	SD
18	DRAWN BY:	APPROVED BY:
2021 \ [\	ML	SD
Wit 🖫		
612	DATE:	
P)	AUG. 1	1, 2021
180	KOLLAARD FILE NUMBE	

210430

DRAWING NUMBER:

210430-SWM

DRAWING NAME:

STORMWATER MANAGEMENT PLAN